

Annual Data Summary for 1995 CHL Field Research Facility

Volume I: Main Text and Appendixes A and B

by Michael W. Leffler, Clifford F. Baron, Brian L. Scarborough, Paul R. Hodges, C. Ray Townsend

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Prepared for Headquarters, U.S. Army Corps of Engineers

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Technical Report CHL-98-14 May 1998

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Volume I: Main Text and Appendixes A and B

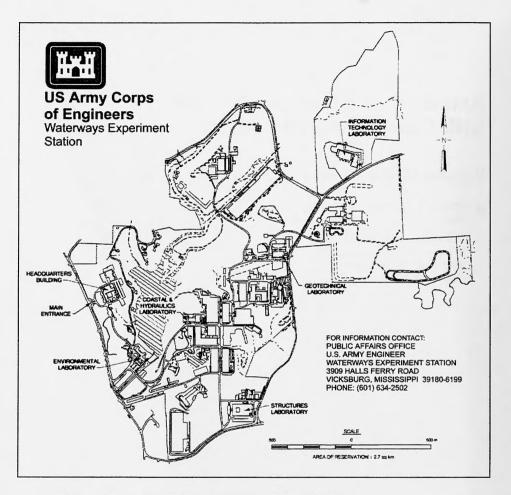
by Michael W. Leffler, Clifford F. Baron, Brian L. Scarborough, Paul R. Hodges, C. Ray Townsend

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¹ A limited number of copies of Appendixes C-E (Volume II) were published under separate cover. Copies are available from National Technical Information Service, 5285 Port Royal Road, Springfield, VA 22161.

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Preface

This report is the 17th in a series of annual data summaries authorized by Headquarters, U.S. Army Corps of Engineers (HQUSACE), under the Civil Works Research and Development Program, Work Unit 32525, "Field Research Facility Analysis." Funds were provided through the U.S. Army Engineer Waterways Experiment Station (WES), Coastal and Hydraulics Laboratory (CHL), under the program management of Ms. Carolyn M. Holmes. The HQUSACE Technical Monitors were Messrs. John H. Lockhart, Jr., Charles Chesnutt, and Barry W. Holliday.

Data for the report were collected and analyzed at the WES/CHL Field Research Facility (FRF) in Duck, NC. The report was prepared by Mr. Michael W. Leffler, FRF, under the direct supervision of Mr. William A. Birkemeier, Chief, FRF Group, Engineering Development Division (EDD), and Mr. Thomas W. Richardson, Chief, EDD; and under the general supervision of Dr. James R. Houston and Mr. Charles C. Calhoun, Jr., Director and Assistant Director, CHL, respectively. Messrs. Kent K. Hathaway and Paul Hodges assisted with instrumentation. Messrs. Brian L. Scarborough and C. Raymond Townsend, FRF, with Messrs. Christopher Goshow and Kevin M. Kremkau assisted with data collection. Mr. Clifford F. Baron assisted with data analysis. The National Oceanic and Atmospheric Administration/National Ocean Service maintained the tide gauge and provided statistics for summarization.

At the time of publication of this report, Director of WES was Dr. Robert W. Whalin. Commander was COL Robin R. Cababa, EN.

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1 Introduction

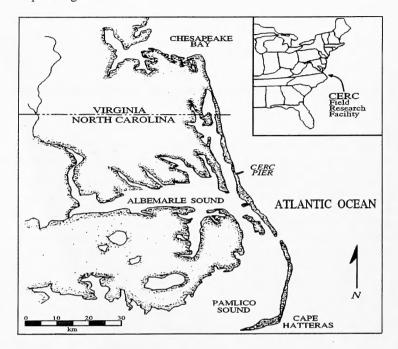
Background

The U.S. Army Engineer Waterways Experiment Station, Coastal and Hydraulics Laboratory's¹ (CHL), Field Research Facility (FRF), located on 0.7 km² at Duck, NC (Figure 1), consists of a 561-m-long research pier and accompanying office and field support buildings. The FRF is located near the middle of Currituck Spit along a 100-km unbroken stretch of shoreline extending south of Rudee Inlet, VA, to Oregon Inlet, NC. The FRF is bordered by the Atlantic Ocean to the east and Currituck Sound to the west. The facility is designed to (a) provide a rigid platform from which waves, currents, water levels, and bottom elevations can be measured, especially during severe storms; (b) provide CHL with field experience and data to complement laboratory and analytical studies and numerical models; (c) provide a manned field facility for testing new instrumentation; and (d) serve as a permanent field base of operations for physical and biological studies of the site and adjacent region.

The research pier is a reinforced concrete structure supported on 0.9-m-diam steel piles spaced 12.2 m apart along the pier's length and 4.6 m apart across the width. The piles are embedded approximately 20 m below the ocean bottom. The pier deck is 6.1 m wide and extends from behind the duneline to about the 6-m water depth contour at a height of 7.8 m above the National Geodetic Vertical Datum (NGVD). The pilings are protected against sand abrasion by concrete erosion collars and against corrosion by a cathodic system.

An FRF Measurements and Analysis Program has been established to collect basic oceanographic and meteorological data at the site, reduce and analyze these data, and publish the results.

¹ Formerly the Coastal Engineering Research Center



This report, which summarizes data for 1995, continues a series of reports begun in 1977.

Figure 1. FRF location map

Organization of Report

This report is organized into nine chapters and five appendixes. Chapter 1 is an introduction; Chapters 2 through 8 discuss the various data collected during the year; and Chapter 9 describes the storms that occurred. Appendix A presents the bathymetric surveys, Appendix B summarizes deepwater wave statistics, and Appendixes C through E (published under separate cover as Volume II) contain summary statistics for other gauges.

In each chapter of this report, the respective instruments used for monitoring the meteorological or oceanographic conditions are briefly described, along with data collection and analysis procedures and data results. The instruments were interfaced with the primary data acquisition system, a Digital Equipment Corporation (Maynard, MA) VAX-11/750 minicomputer until June 1994 when it was replaced with a Digital Equipment Corporation VAXstation 4000 located in the FRF laboratory building. More detailed explanations of the design and the operation of the instruments may be found in Miller (1980). Readers' comments on the format and usefulness of the data presented are encouraged.

Availability of Data

Table 1 summarizes the available data. In addition to the wave data summaries in the main text, more extensive summaries for each of the wave gauges are provided in Appendixes B through E.

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The annual data summary herein summarizes daily observations by month and year to provide basic data for analysis by users. Daily measurements and observations have already been reported in a series of monthly Preliminary Data Summaries (FRF 1995). If individual data for the present year are needed, the user can obtain detailed information (as well as the monthly and previous annual reports) from the following address:

USAE Waterways Experiment Station Field Research Facility 1261 Duck Rd. Kitty Hawk, NC 27949-4472

Much of this data is now also available via the World Wide Web at:

http://www.frf.usace.army.mil

Although the data collected at the FRF are designed primarily to support ongoing CHL research, use of the data by others is encouraged. Tidal data other than the summaries in this report can be obtained directly from the following address:

National Oceanic and Atmospheric Administration National Ocean Service ATTN: Tide Analysis Branch Rockville, MD 20852

A complete explanation of the exact data desired for specific dates and times will expedite filling any request; an explanation of how the data will be used will help CHL or the National Oceanic and Atmospheric Administration (NOAA)/National Ocean Service (NOS) determine whether other relevant data are available. For information regarding the availability of data for all years, contact the FRF at (252) 261-3511. Costs for collecting, copying, and mailing will be borne by the requester.

2 Meteorology

This chapter summarizes the meteorological measurements made during the current year and in combination with all previous years. Meteorological measurements during storms are given in Chapter 9.

Mean air temperature, atmospheric pressure, and wind speed and direction were computed for each data file, which consisted of data sampled two times per second for 34 min every 6 hr beginning at or about 0100, 0700, 1300, and 1900 hr eastern standard time (EST); these hours correspond to the time that the National Weather Service (NWS) creates daily synoptic weather maps. During storms, data recordings were made more frequently. Meteorological data are summarized in Table 2.

Table 2 Meteorological Statistics

	M	ean	M	ean						Wind_Res	sultants	
		mperature		neric Pres.	P	recipit	ation, m	m		1995	198	0-1995
		deg C		mb	1995	_	1978-199		Speed	Direction	Speed	Direction
Month		1983-1995	1995	1983-1995	Total	Mean	Maxima	Minima	m/sec	deg	_m/sec	deg
Jan	7.1	6.2	1016.1	1017.8	76	110	210	44	1.9	316	2.2	331
Feb	4.8	6.6	1016.0	1017.3	123	74	123	20	2.4	309	1.9	341
Mar	9.5	9.5	1018.7	1016.0	43	106	231	35	2.9	5	1.3	351
Apr	14.5	14.0	1015.1	1014.2	39	90	182	0	0.7	77	0.2	320
May	19.0	18.7	1014.8	1015.7	122	79	239	20	0.5	136	0.3	150
Jun	23.5	23.7	1015.3	1015.1	142	91	142	27	1.5	65	1.0	184
Jul	26.8	26.5	1016.2	1015.9	91	- 96	275	19	2.2	181	2.0	206
Aug	25.1	25.5	1015.6	1016.3	122	111	253	30	2.8	30	0.5	84
Sep	22.4	22.8	1017.3	1017.6	92	82	226	5	4.4	43	2.0	39
Oct	19.3	18.0	1017.2	1018.6	193	82	193	17	0.5	68	2.3	26
Nov	9.4	13.2	1018.0	1018.4	146	93	146	26	3.1	293	1.7	347
Dec	4.4	7.9	1018.6	1019.2	67	68	131	4	2.9	322	2.4	331
Mean	15.5	16.0	1016.6	1016.8	105	90			1.1	359	0.8	351
Total					1256	1082						

Air Temperature

The FRF enjoys a typical marine climate that moderates the temperature extremes of both summer and winter.

Measurement instruments

A Yellow Springs Instrument Company, Inc. (YSI) (Yellow Springs, OH), electronic temperature probe with analog output interfaced to the FRF's computer was operated beside the NWS's meteorological instrument shelter located 43 m behind the dune (Figure 2). To ensure proper temperature readings,

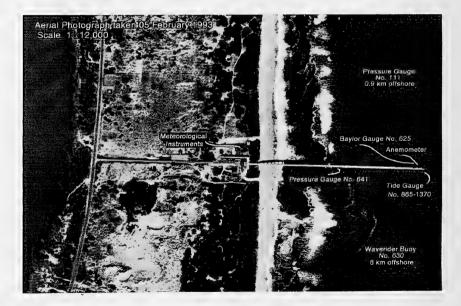


Figure 2 . FRF gauge locations

the probe was installed 3 m above ground inside a protective cover to shade it from direct sun, yet provide proper ventilation.

Results

Daily and average air temperature values are tabulated in Table 2 and shown in Figure 3.

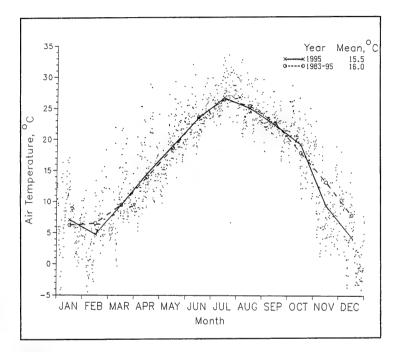


Figure 3. Daily air temperature values with monthly means

Atmospheric Pressure

Measurement instruments

Electronic atmospheric pressure sensor. Atmospheric pressure was measured with a YSI electronic sensor with analog output located in the laboratory building at 9 m above NGVD. Data were recorded on the FRF computer. Data from this gauge were compared with those from an NWS aneroid barometer to ensure proper operation. **Microbarograph.** A Weathertronics, Incorporated (Sacramento, CA), recording aneroid sensor (microbarograph) located in the laboratory building was also used to continuously record atmospheric pressure variation.

The microbarograph was compared daily with the NWS aneroid barometer, and adjustments were made as necessary. Maintenance of the microbarograph consisted of inking the pen, changing the chart paper, and winding the clock every 7 days. During the summer, a meteorologist from the NWS checked and verified the operation of the barometer.

The microbarograph was read and inspected daily using the following procedure:

- a. The pen was zeroed (where applicable).
- b. The chart time was checked and corrected, if necessary.
- c. The daily reading was marked on the chart for reference.
- d. The starting and ending chart times were recorded, as necessary.
- e. New charts were installed, when needed.

Results

Daily and average atmospheric pressure values are presented in Figure 4, and summary statistics are presented in Table 2.

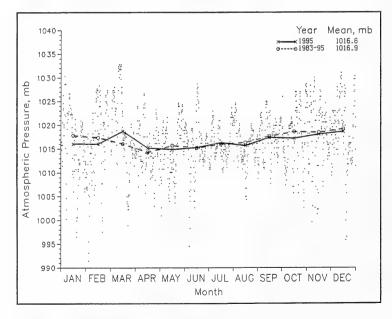


Figure 4. Daily barometric pressure values with monthly means

Precipitation

Precipitation is generally well distributed throughout the year. Precipitation from mid-latitude cyclones (northeasters) predominates in the winter, whereas local convection (thunderstorms) accounts for most of the summer rainfall.

Measurement instruments

Electronic rain gauge. A Belfort Instrument Company (Baltimore, MD) 30-cm weighing rain gauge, located near the instrument shelter 47 m behind the dune, measured daily precipitation. According to the manufacturer, the instrument's accuracy was 0.5 percent for precipitation amounts less than 15 cm and 1.0 percent for amounts greater than 15 cm.

The rain gauge was inspected daily; however, the analog chart recorder was inoperable the entire year.

Plastic rain gauge. An Edwards Manufacturing Company (Alberta Lea, MN) True Check 15-cm-capacity clear plastic rain gauge with a 0.025-cm resolution was used to monitor the performance of the weighing rain gauge. This gauge was located near the weighing gauge, and the gauges were compared on a daily basis. Very few discrepancies were identified during the year.

Results

Daily and monthly average precipitation values are shown in Figure 5. Statistics of total precipitation for each month during this year and average totals for all years combined are presented in Table 2.

Wind Speed and Direction

Winds at the FRF are dominated by tropical maritime air masses that create low to moderate, warm southern breezes; arctic and polar air masses that produce cold winds from northerly directions; and smaller scale cyclonic, low pressure systems, which originate either in the tropics (and move north along the coast) or on land (and move eastward offshore). The dominant wind direction changes with the season, being generally from northern directions in the fall and winter and from southern directions in the spring and summer. It is common for fall and winter storms (northeasters) to produce winds with average speeds in excess of 15 m/sec.

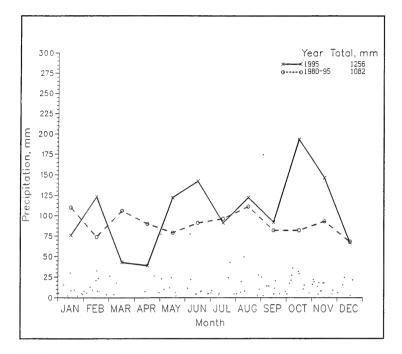


Figure 5. Daily precipitation values with monthly totals

Measurement instrument

Winds were measured at the seaward end of the pier at an elevation of 19.1 m (Figure 2) using a Weather Measure Corporation (Sacramento, CA) Skyvane Model W102P anemometer. Wind speed and direction data were collected on the FRF computer. The anemometer manufacturer specifies an accuracy of ± 0.45 m/sec below 13 m/sec and 3 percent at speeds above 13 m/sec, with a threshold of 0.9 m/sec. Wind direction accuracy is ± 2 deg, with a resolution of less than 1 deg. The anemometer is calibrated annually at the National Bureau of Standards in Gaithersburg, MD, and is within the manufacturer's specifications.

Results

Annual and monthly joint probability distributions of wind speed versus direction were computed. Wind speeds were resolved into 3-m/sec intervals, whereas the directions were at 22.5-deg intervals (i.e., 16-point compass direction specifications). These distributions are presented as wind "roses," such that the length of the petal represents the frequency of occurrence of wind blowing from the specified direction, and the width of the petal is indicative of the speed. Resultant directions and speeds were also determined by vector-averaging the data (see Table 2). Wind statistics are presented in Figures 6-8.

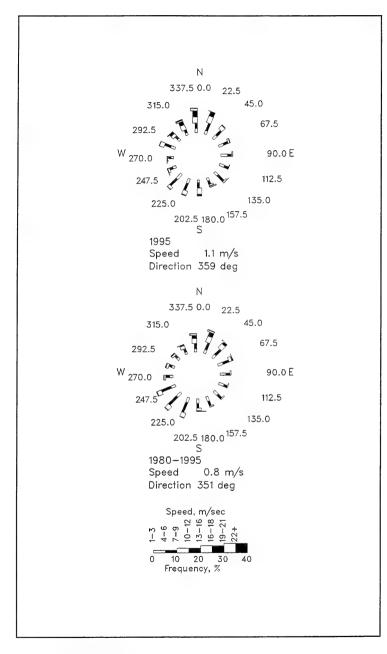


Figure 6. Annual wind roses

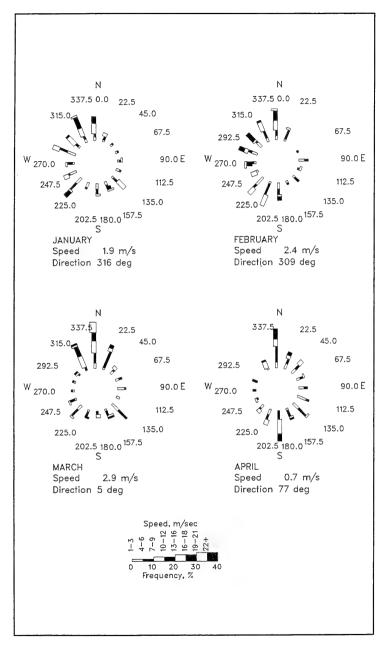


Figure 7. Monthly wind roses for 1995 (Sheet 1 of 3)

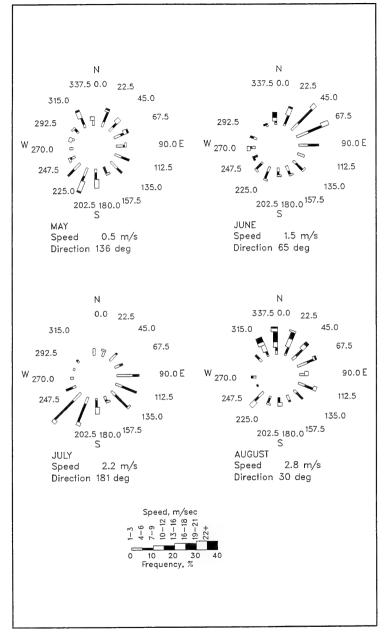


Figure 7. (Sheet 2 of 3)

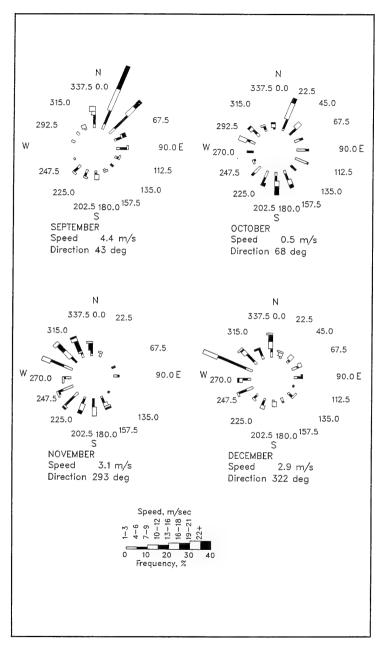


Figure 7. (Sheet 3 of 3)

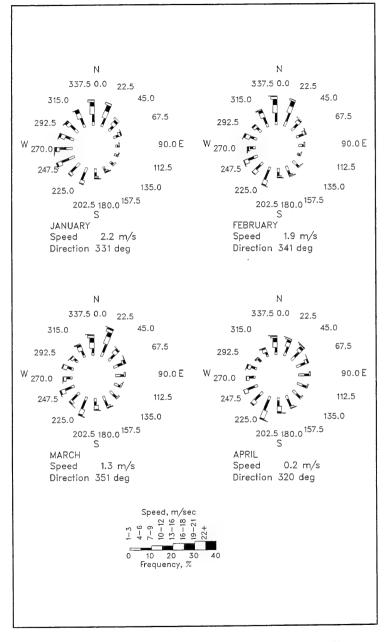


Figure 8. Monthly wind roses for 1980 through 1995 (Sheet 1 of 3)

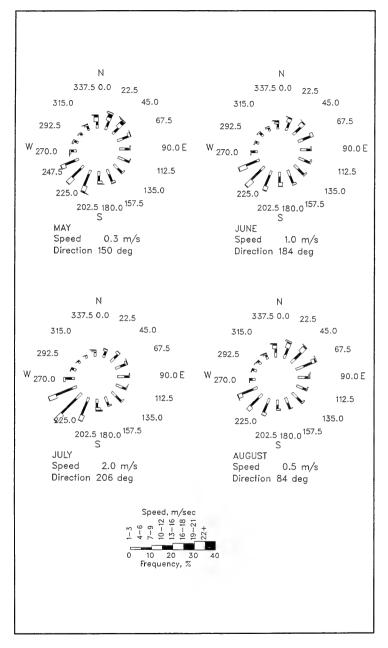


Figure 8. (Sheet 2 of 3)

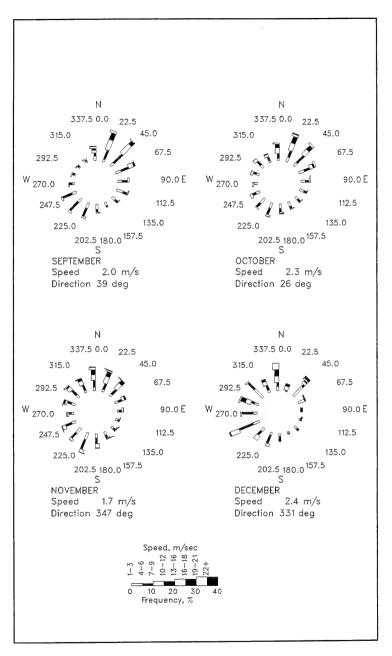


Figure 8. (Sheet 3 of 3)

3 Waves

This chapter presents summaries of the wave data. A discussion of individual major storms is given in Chapter 9 and contains additional wave data for times when wave heights exceeded 2 m at the seaward end of the FRF pier. Appendixes B through E provide more extensive data summaries for each gauge, including height and period distributions, wave direction distributions, persistence tables, and spectra during storms.

Wave directions (similar to wind directions) at the FRF are seasonally distributed. Waves approach most frequently from north of the pier in the fall and winter and south of the pier in the summer, with the exception of storm waves that approach twice as frequently from north of the pier. Annually, waves are approximately evenly distributed between north and south (resultant wave direction being almost shore-normal).

Measurement Instruments

The wave gauges included one wave staff gauge (Gauge 625), one buoy gauge (Gauge 630), and two pressure gauges (Gauges 111 and 641) as shown in Figure 2. Staff gauge 645 failed in May 1992 and was replaced by pressure gauge 641 at the same location. The gauges were located as follows:

<u>Gauge Type/Number</u> Continuous wire (645) Pressure Gauge (641) Continuous wire (625) Accelerometer buoy (630)	Distance Offshore <u>from Baseline</u> 238 m 238 m 567 m 6 km	Water Depth 	Operational <u>Period</u> 11/84-05/92 11/92-12/95 11/78-12/95 11/78-12/95
--	--	-----------------	--

Staff gauges

One Baylor Company (Houston, TX) parallel cable inductance wave gauge (Gauge 625 at sta 18+60 (Figure 2)) was mounted on the FRF pier. Rugged and reliable, this gauge requires little maintenance except to keep tension on the cables and to remove any material that may cause an electrical short between them. It was calibrated prior to installation by creating an electrical short between the two cables at known distances along the cable and recording the voltage output. Electronic signal conditioning amplifiers are used to ensure that the output signals from the gauge are within a 0- to 5-V range. Manufacturerstated gauge accuracy is about 1.0 percent, with a 0.1-percent full-scale resolution; full scale is 14 m for Gauge 625. This gauge is susceptible to lightning damage, but protective measures have been taken to minimize such occurrences. A more complete description of the gauges' operational characteristics is given by Grogg (1986).

Buoy gauge

One Datawell Laboratory for Instrumentation (Haarlem, The Netherlands) Waverider buoy gauge (Gauge 630) measures the vertical acceleration produced by the passage of a wave. The acceleration signal is double-integrated to produce a displacement signal transmitted by radio to an onshore receiver. The manufacturer stated that wave amplitudes are correct to within 3 percent of their actual value for wave frequencies between 0.065 and 0.500 Hz (corresponding to 15- to 2-sec wave periods). The manufacturer also specified that the error gradually increased to 10 percent for wave periods in excess of 20 sec. The results in this report were not corrected for the manufacturer's specified amplitude errors. However, the buoy was calibrated semiannually to ensure that it was within the manufacturer's specification.

Pressure gauges

One Senso-Metrics, Incorporated (Simi Valley, CA), pressure transduction gauge (Gauge 111) installed near the ocean bottom measures the pressure changes produced by the passage of waves creating an output signal that is linear and proportional to pressure when operated within its design limits. Predeployment and postdeployment calibrations are performed at the FRF using a static deadweight tester. The sensor's range is 0 to 25 psi (equivalent to 0 to 17 m of seawater) above atmospheric pressure with a manufacturer-stated accuracy of ± 0.25 percent. Copper scouring pads are installed at the sensor's diaphragm to reduce biological fouling, and the system is periodically cleaned by divers.

One Paroscientific, Incorporated (Redmond, WA) pressure transduction gauge (Gauge 641) was installed near the ocean bottom on an instrument pile under the pier at station 7+80. Calibration is similar to that performed on Gauge 111. The sensor's range is 0 to 45 psia (equivalent to 0 to 30 m of seawater) with a manufacturer-stated accuracy of ± 0.01 percent. A perforated copper/nickel plate protects the sensor's diaphragm from biological fouling, and the system is periodically cleaned by divers.

Digital Data Analysis and Summarization

The data were collected, analyzed, and then archived on optical disk using the FRF's VAX computer. Data sets were normally collected every 3 hr. For each gauge, a data set consisted of five contiguous records of 4,096 points recorded at 0.5 Hz (approximately 34-min long), for a total of 2 hr and 50 minutes, resulting in only a 10-min gap between data sets. Analysis was performed on individual 34-min records.

The analysis program computes the first moment (mean) and the second moment about the mean (variance) and then edits the data by checking for "jumps," "spikes," and points exceeding the voltage limit of the gauge. A jump is defined as a data value greater than five standard deviations from the previous data value, whereas a spike is a data value more than five standard deviations from the mean. If less than five consecutive jumps or spikes are found, the program linearly interpolates between acceptable data and replaces the erroneous data values. The editing stops if the program finds more than five consecutive jumps or spikes, or more than a total of 100 bad points, or the variance of the voltage is below 1×10^{-5} squared volts. The statistics and diagnostics from the analysis are saved.

Sea surface energy spectra are computed from the edited time series. Spectral estimates are computed from smaller data segments obtained by dividing the 4,096-point record into several 512-point segments. The estimates are then ensemble-averaged to produce a more accurate spectrum. These data segments are overlapped by 50 percent (known as the Welch (1967) method) which has been shown to produce better statistical properties than nonoverlapped segments. The mean and linear trends are removed from each segment prior to spectral analysis. To reduce side-lobe leakage in the spectral estimates, a data window was applied. The first and last 10 percent of data points were multiplied by a cosine bell (Bingham, Godfrey, and Tukey 1967). Spectra were computed from each segment with a discrete Fast Fourier Transform and then ensemble-averaged. Sea surface spectra from subsurface pressure gauges were obtained by applying the linear wave theory transfer function.

Unless otherwise stated, wave height in this report refers to the energybased parameter H_{mo} defined as four times the zeroth moment wave height of the estimated sea surface spectrum (i.e., four times the square root of the variance) computed from the spectrum passband. Energy computations from the spectra are limited to a passband between 0.05 and 0.50 Hz for surface gauges and between 0.05 Hz and a high-frequency cutoff for subsurface gauges. This high-frequency limit is imposed to eliminate aliased energy and noise measurements from biasing the computation of H_{mo} and is defined as the frequency where the linear theory transfer function is less than 0.1 (spectral values are multiplied by 100 or more). Smoother and more statistically significant spectral estimates are obtained by band-averaging contiguous spectral components (three components are averaged per band, producing a frequency band width of 0.0117 Hz).

Wave period T_p is defined as the period associated with the maximum energy band in the spectrum, which is computed using a 3-point running average band on the spectrum. The peak period is reported as the reciprocal of the center frequency (i.e., $T_p = 1$ /frequency) of the spectral band with the highest energy. A detailed description of the analysis techniques is presented in an unpublished report by Andrews (1987).¹

Results

The wave conditions for the year are shown in Figure 9. For all four gauges, the distributions of wave height for the current year and all years combined are presented in Figures 10 and 11, respectively. Distributions of wave period are presented in Figure 12.

Multiple-year comparisons of data for Gauge 111 actually incorporate data for 1985 and 1986 from Gauge 640 (a discontinued Waverider buoy previously located at the approximate depth and distance offshore of Gauge 111) and data for 1987 from Gauge 141, located 30 m south of Gauge 111. In addition, Gauge 511 was used from January through October 1993. Multiple-year data for Gauge 641 also include data from Gauge 645 (a Baylor staff gauge) which was mounted at the same location as Gauge 641 from November 1984 until May 1992, when it failed.

Refraction, bottom friction, and wave breaking contribute to the observed differences in height and period. During the most severe storms when the wave heights exceed 3 m at the seaward end of the pier, the surf zone (wave breaking) has been observed to extend past the end of the pier and occasionally 1 km offshore. This occurrence is a major reason for the differences in the distributions between Gauge 630 and the inshore gauges. The wave height statistics for the pressure gauge (Gauge 641), located at the landward end of the pier, were considerably lower than those for the other gauges. In all but the calmest conditions, this gauge is within the breaker zone. Consequently, these statistics represent a lower energy wave climate.

¹ M. E. Andrews. (1987). "Standard wave data analysis procedures for coastal engineering applications," unpublished report prepared for U.S. Army Engineer Waterways Experiment Station, Vicksburg, MS.

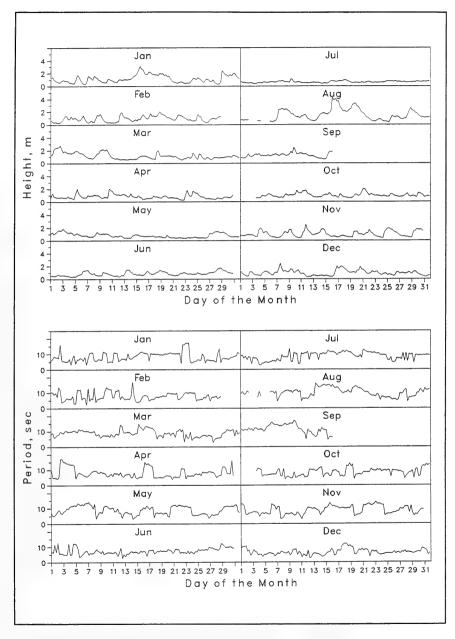


Figure 9. 1995 time-histories of wave height and period for Gauge 630

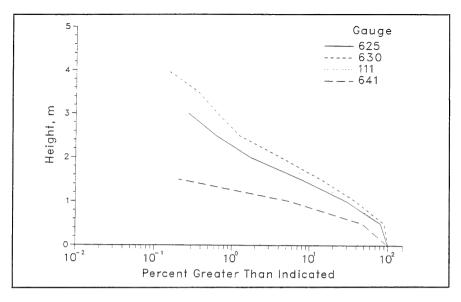


Figure 10. 1995 annual wave height distributions

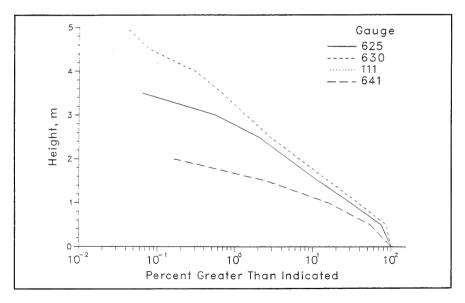


Figure 11. Annual distribution of wave heights for 1980 through 1995

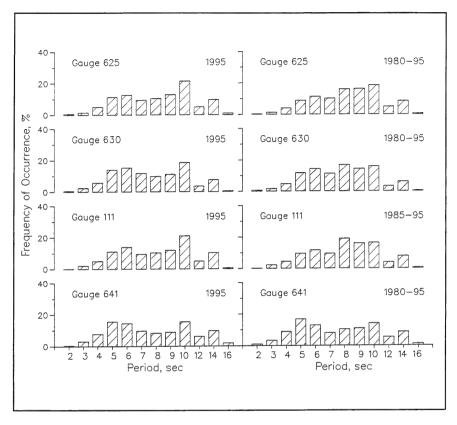


Figure 12. Annual wave period distributions for all gauges

Summary wave statistics for the current year and all years combined are presented for Gauge 630 in Table 3.

Table 3

				1995				_		19	80-199	25		
		Hei	ght		Per	iod			Heig	ht		Per	iod	
		Std.				Std.			Std.				Std.	
	Mean	Dev.	Extreme		Mean	Dev.	Number	Mean	Dev.	Extreme		Mean	Dev.	Number
Month	m	m	m	Date	sec	_sec	Obs.	m		<u>m</u>	<u>Date</u>	sec	sec	Obs.
Jan	1.2	0.6	3.1	15	8.3	3.0	123	1.2	0.7	4.5	1983	8.1	2.7	1619
Feb	1.0	0.5	2.0	18	7.8	2.7	112	1.2	0.7	5.1	1987	8.4	2.5	1464
Mar	1.2	0.6	2.8	2	8.7	2.3	120	1.2	0.7	4.7	1983	8.6	2.6	1811
Арг	0.9	0.4	2.0	10	7.9	3.2	120	1.0	0.6	5.0	1988	8.6	2.7	1790
May	0.8	0.4	1.9	3	8.8	2.8	124	0.9	0.5	3.6	1992	8.2	2.5	1837
Jun	0.9	0.4	1.8	28	7.3	2.0	120	0.8	0.4	2.7	1991	7.9	2.2	1717
Jul	0.7	0.2	1.1	9	8.6	2.5	123	0.7	0.3	2.1	1985	8.1	2.4	1752
Aug	1.5	0.9	4.2	16	10.0	2.8	113	0.8	0.5	3.6	1981	8.3	2.5	1768
Sep	1.3	0.4	2.4	9	11.5	2.9	61	1.1	0.6	6.1	1985	8.7	2.7	1715
Oct	1.0	0.3	2.0	21	8.4	2.5	114	1.2	0.7	5.4	1991	8.6	2.8	1843
Nov	1.1	0.5	2.5	11	8.7	2.7	118	1.1	0.7	5.1	1994	8.1	2.7	1588
Dec	1.0	0.5	2.4	7	6.5	1.9	124	1.2	0.8	5.6	1980	8.3	2.9	1599
Annual	1.0	0.6	4.2	Aug	8.4	2.5	1372	1.0	0.6	6.1	Sep 1985	8.3	2.6	20503

Wave Statistics for Gauge 630

Annual joint distributions of wave height versus wave period for Gauge 630 are presented for 1995 in Table 4, and for all years combined in Table 5. Similar distributions for the other gauges are included in Appendixes B-E.

Annual distributions of wave directions (relative to true north) based on daily observations of direction at the seaward end of the pier and height from Gauge 625 (or Gauge 111 when data for Gauge 625 were unavailable) are shown in Figure 13. Monthly wave roses for 1995 and all years combined are presented in Figures 14 and 15, respectively.

Table 4

Annual (1995) Joint Distribution of H_{me} versus T_p for Gauge 630¹

						Per	iod, s	ec					
	2.0-	3.0-	4.0-	5.0-	6.0-	7.0-	8.0-	9.0-	10.0-	12.0-	14.0-	16.0-	
Height, m	2.9	3.9	4.9	5.9	6.9	7.9	8.9	9.9	11.9	13.9		Longer	
0.00 - 0.49	29	14	22	65	43	115	459	416	244	158	108		1673
0.50 - 0.99	7	108	359	502	667	617	1055	861	581	57	273	14	5101
1.00 - 1.49		22	151	395	237	151	187	158	194	22	57		1574
1.50 - 1.99				172	273	115	57	36	136	29	57		875
2.00 - 2.49				14	143	86	36	29	50	7	50		415
2.50 - 2.99					14	50	36	22	22	7	36		187
3.00 - 3.49						7	7	14	50	7			85
3.50 - 3.99								22	22				44
4.00 - 4.49									7	14	7		28
4.50 - 4.99											14		14
5.00 - Greater											7		7
Total	36	144	532	1148	1377	1141	1837	1558	1306	301	609	14	

¹ Percent occurrence (x100) of height and period.

Table 5

Annual (1980-1995) Joint Distribution of H_{mo} versus T_{p} for Gauge 630¹

-						Per	iod, s	ec					
_Height, m	2.0-	3.0- <u>3.9</u>	4.0-	5.0- 5.9	6.0- <u>6.9</u>	7.0- <u>7.9</u>	8.0- <u>8.9</u>	9.0- <u>9.9</u>		12.0- 13.9		16.0- Longer	<u>Total</u>
0.00 - 0.49	25	15	28	63	80	123	356	293	194	68	119	4	1368
0.50 - 0.99	32	135	271	490	570	536	915	773	764	125	225	14	4850
1.00 - 1.49		10	147	405	404	237	274	216	318	39	112	3	2165
1.50 - 1.99			11	166	244	106	82	76	137	32	66	3	923
2.00 - 2.49			1	25	93	68	52	33	62	26	34	1	395
2.50 - 2.99				1	14	34	20	15	34	9	25	1	153
3.00 - 3.49					1	11	13	13	21	6	8	1	74
3.50 - 3.99						1	6	9	13	5	5		39
4.00 - 4.49							3	5	8	3	4	1	24
4.50 - 4.99								1	2		1	1	5
5.00 - Greater							1		1	1	1	1	5
Total	57	160	458	1150	1406	1116	1722	1434	1554	314	600	30	

¹ Percent occurrence (x100) of height and period.

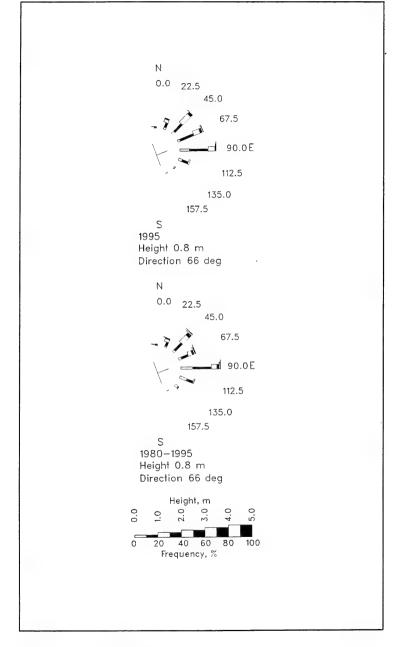


Figure 13. Annual wave roses

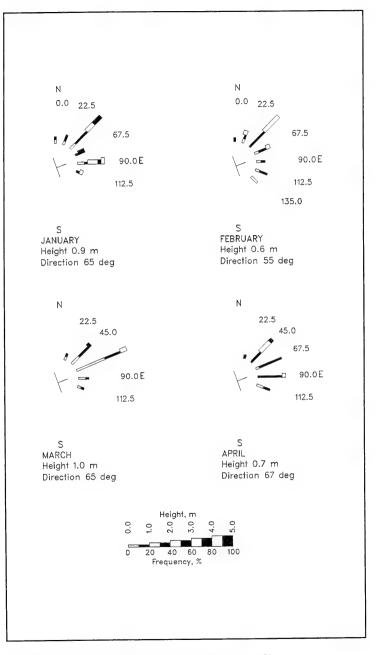


Figure 14. Monthly wave roses for 1995 (Sheet 1 of 3)

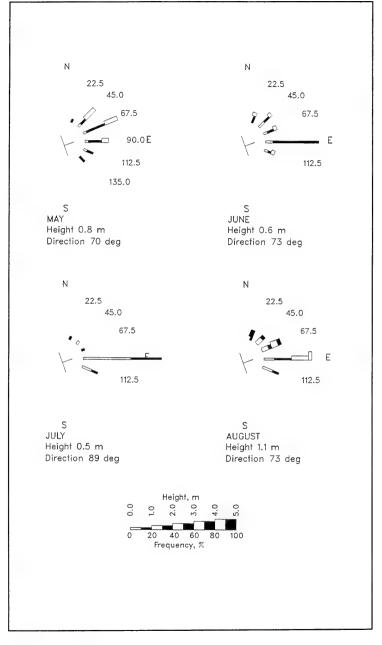


Figure 14. (Sheet 2 of 3)

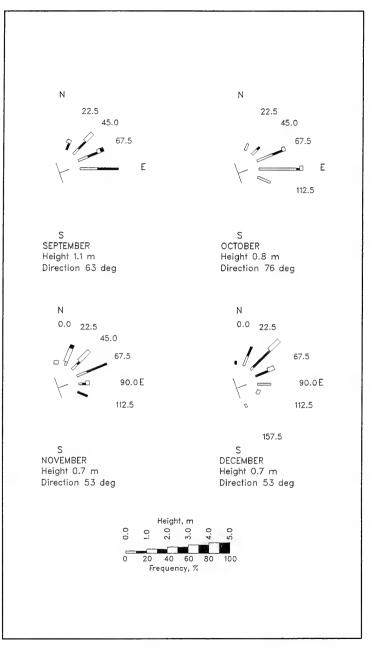
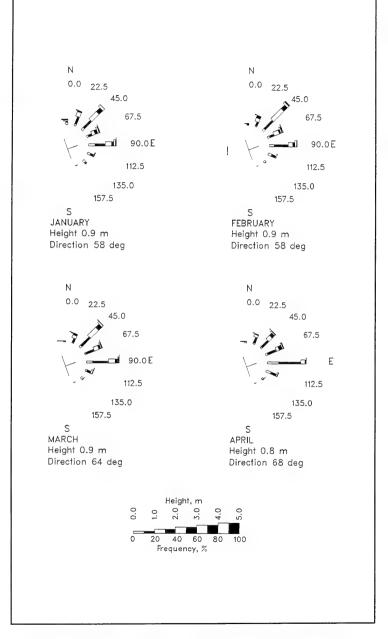
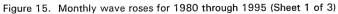


Figure 14. (Sheet 3 of 3)





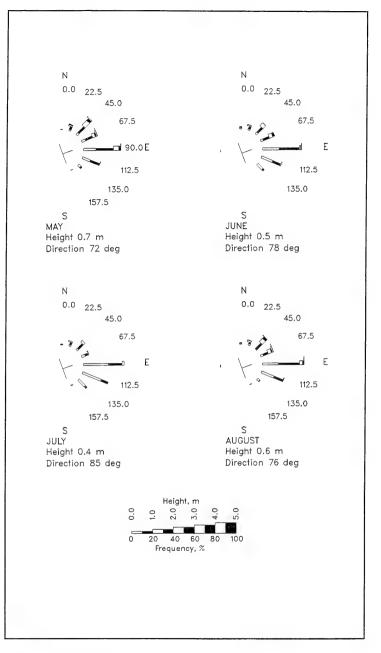


Figure 15. (Sheet 2 of 3)

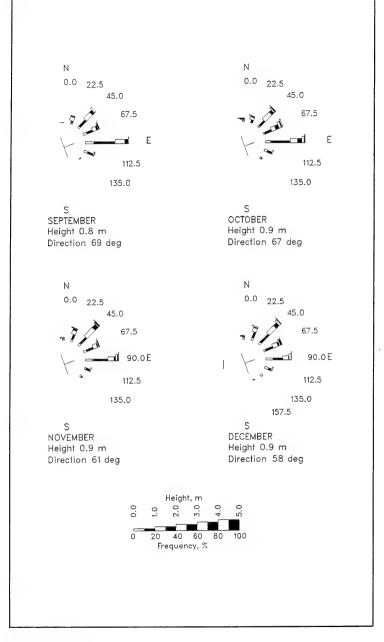


Figure 15. (Sheet 3 of 3)

4 Currents

Surface current speed and direction at the FRF are influenced by winds, waves, and, indirectly, by the bottom topography. The extent of the respective influences varies daily. However, winds tend to dominate the currents at the seaward end of the pier, whereas waves dominate within the surf zone.

Observations

Near 0700 EST, daily observations of surface current speed and direction were made at (a) the seaward end of the pier, (b) the midsurf position on the pier, and (c) 10 to 15 m from the beach 500 m updrift of the pier. Surface currents were determined by observing the movement of a small wooden block floating on the water surface.

Results

Annual mean and mean currents for 1980 through 1995 are presented in Table 6 and in Figure 16. Figure 16 shows the daily and average annual measurements at the beach, pier midsurf, and pier end locations. Since the relative influences of the winds and waves vary with position from shore, the current speeds and, to some extent, direction vary at the beach, midsurf, and pier end locations. Magnitudes generally are largest at the midsurf location and lowest at the end of the pier.

Table 6 Mean Longshore Surface Currents¹

		1980-		1980-		1980
Month	<u>1995</u>	1995	<u>1995</u>	<u> 1995 </u>	<u>1995</u>	
Jan	15	18	12	19	8	12
Feb	20	15	22	19	12	10
Mar	33	13	30	6	15	6
Apr	12	16	11	6	2	3
May	11	19	6	6	4	6 3 6 -3
Jun	15	6	5	-8	-6	-3
Jul	10	5	-11	-6	-21	-5
Aug	14	12	2	-1	-3	-2
Sep	16	11	16	3	0	-1
Oct	3	10	6	7	-7	4
Nov	17	10	27	9	18	4 3 2
Dec	28	15	30	18	25	2
Annual	15	13	15	7	4	3

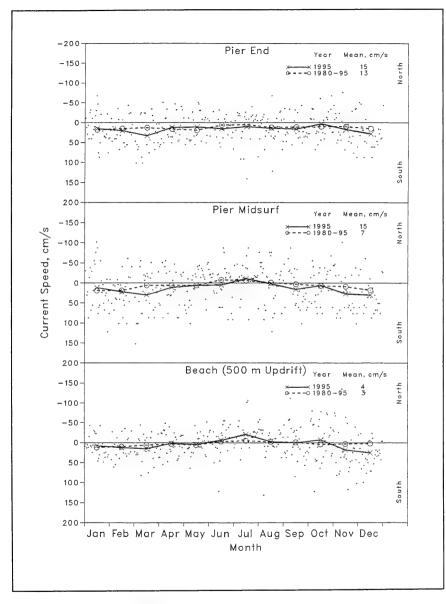


Figure 16. Daily current speeds and directions with monthly means for 1995

5 Tides and Water Levels

Measurement Instrument

From 1978 to June 1995 water level data were obtained from an NOAA/NOS control tide station (sta 865-1370) located at the seaward end of the research pier (Figure 2) by using a Leupold and Stevens, Inc. (Beaverton, OR), digital tide gauge. This analog-to-digital recorder is a float-activated, negator-spring, counterpoised instrument that mechanically converts the vertical motion of a float into a coded, punched paper tape record. The below-deck installation at pier sta 19+60 consisted of a 30.5-cm-diam stilling well with a 2.5-cm orifice and a 21.6-cm-diam float.

Operation and tending of the tide gauge conformed to NOS standards. The gauge was checked daily for proper operation of the punch mechanism and for accuracy of the time and water level information. The accuracy was determined by comparing the gauge level reading with a level read from a reference electric tape gauge. Once a week, a heavy metal rod was lowered down the stilling well and through the orifice to ensure free flow of water into the well. During the summer months, when biological growth was most severe, divers inspected and cleaned the orifice opening as required.

The tide station was inspected quarterly by an NOAA/NOS tide field group. Tide gauge elevation was checked using existing NOS control positions, and the equipment was checked and adjusted as needed. Both NOS and FRF personnel also reviewed procedures for tending the gauge and handling the data. Any specific comments on the previous months of data were discussed to ensure data accuracy.

Digital paper tape records of tide heights taken every 6 min were analyzed by the Tides Analysis Branch of NOS. An interpreter created a digital magnetic computer tape from the punch paper tape, which was then processed on a large computer. First, a listing of the instantaneous tidal height values was created for visual inspection. If errors were encountered, a computer program was used to fill in or recreate bad or missing data using correct values from the nearest NOS tide station and accounting for known time lags and elevation anomalies. When the validity of the data had been confirmed, monthly tabulations of daily highs and lows, hourly heights (instantaneous height selected on the hour), and various extreme and/or mean water level statistics were computed.

Following a year of comparison tests at the FRF the Leupold and Stevens, Inc., digital tide gauge was replaced in June 1995 by an NOS acoustic tide gauge (Next Generation Water Level Measurement System, NGWLMS) located at pier sta 19+20.

The following brief discription of the NGWLMS was condensed from a paper found on the NOAA World Wide Web site (Gill 1990).

The NGWLMS system's primary sensor is a self-calibrating, downwardlooking acoustic system that transmits a short acoustic pulse through a 1.3-cmdiameter sound tube to the water surface and to a calibration point referenced to the station's datum. Because the major potential source for errors is vertical temperature changes between the sensor and the water surface, sound tube air temperatures are monitored and accompany the transmitted data. The sensor takes 181 1-sec samples in 3-min periods centered every 6 min. A new mean value and standard deviation are computed every 6-minutes. Each NGWLMS also includes a less accurate, strain-gauge type sensor as a backup. The systems relay data every 3-hrs to NOAA's Geostationary Operational Environmental Satellite system. NOAA's NGWLMS Data Processing and Analysis System retrieves data on an hourly basis, decodes and then performs automated quality control checks.

Results

Tides at the FRF are semidiurnal with both daily high and low tides approximately equal. Tide height statistics are presented in Table 7. Figure 17 plots the monthly tide statistics for all available data, and Figure 18 compares the distribution of daily high and low water levels and hourly tide heights. The monthly or annual mean sea level (MSL) reported is the average of the hourly heights, whereas the mean tide level is midway between mean high water (MHW) and mean low water (MLW), which are the averages of the daily high- and low-water levels, respectively, relative to NGVD. Mean range (MR) is the difference between MHW and MLW levels, and the lowest water level for the month is the extreme low (EL) water, while the highest water level is the extreme high (EH) water level.

NOTE: Due to a mistake in converting feet to centimeters the tide height statistics from 1987 through 1993 (as published in the 1987 through 1993 Annual Data Summaries) found in Table 7 and Figure 17 were in error. These were corrected beginning with the 1994 report.

Table 7

Tide Height Statistics¹

Month or <u>Year</u>	Mean High <u>Water</u>	Mean Tide <u>Level</u>	Mean Sea <u>Level</u>	Mean Low <u>Water</u>	Mean <u>Range</u>	Extreme 		Extreme Low	
					1995				
Jan	58	6	6	-46	104	107	30	-79	7
Feb	48	-2	-2	-52	100	87	22	-83	26
Mar	64	14	14	-38	102	99	2	-60	1
Apr	57	7	7	-45	102	102	18	-66	17
May	66	17	17	-34	100	114	14	-64	30
Jun	66	16	16	-33	99	127	14	-62	12
Jul	61	11	12	-40	101	98	9_	-70	30
Aug	79	28	29	-22	101	131	7	-54	5
Sep	80	30	30	-20	100	114	27	-45	1
Oct	71	19	20	-32	103	111	8	-61	25
Nov	68	16	16	-36	104	116	22	-76	24
Dec	63	13	13	-37	100	133	20	-75	22
1995	65	15	15	-36	101	133	Dec	-83	Feb
				P	<u>rior Year</u>	s			
1994	62	12	12	-39	101	122	Nov	-95	Jan
1993	67	18	19	-31	98	150	Dec	-84	Nov
1992	66	17	17	-32	98	150	Dec	-84	Nov
1991	66	18	18	-31	97	150	Oct	-100	Dec
1990	59	11	11	-38	97	131	May	-94	Feb
1989	59	11	11	-37	96	239	Mar	-92	Apr
1988	55	7	7	-40	95	155	Apr	-86	Dec
1987	66	18	19	-29	95	136	Jan	-76	Nov
1986	60	13	13	-35	95	123	Dec	-108	Jan
1985	59	10	11	-37	96	136	Dec	-93	Apr
1984	64	16	16	-32	97	147	Oct	-77	Jul
1983	68	19	19	-30	98	143	Jan	-73	Mar
1982	58	8	9	-42	99	127	Oct	-108	Feb
1981	59	8	9	-42	101	149	Nov	-110	Apr
1980	59	8	8	-43	102	118	Mar	-119	Mar
1979	60	9	9	-43	103	121	Feb	-95	Sep
1979-									
1994	62	13	13	-36	98	239	Mar 1989	-119	Mar 198
1		ents are							

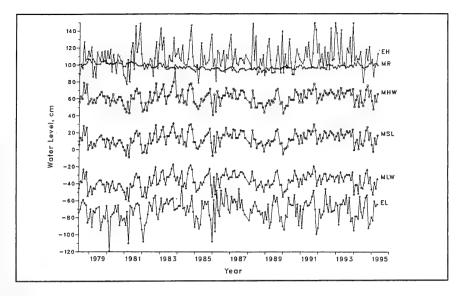


Figure 17. Monthly tide and water level statistics relative to NGVD

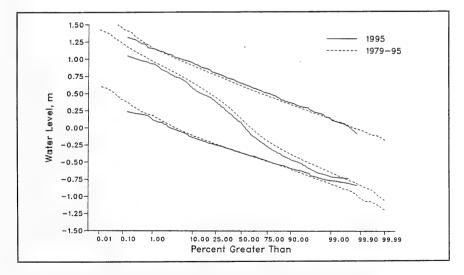


Figure 18. Distributions of hourly tide heights and high- and low-water levels

6 Water Characteristics

Monthly averages of daily measurements of surface water temperature, visibility, and density at the seaward end of the FRF pier are given in Table 8. The summaries represent single observations made near 0700 EST and, therefore, may not reflect daily average conditions since such characteristics can change within a 24-hr period. Large temperature variations were common when there were large differences between the air and water temperatures and variations in wind direction. From past experience, persistent onshore winds move warmer surface water toward the shoreline, although offshore winds cause colder bottom water to circulate shoreward, resulting in lower temperatures.

	Temperature		Visibility		Density	
	deg		m	1000	g/cm	
	1005	1980-	1005	1980-	4005	1980-
Month	<u>1995</u> 8.3	<u>1995</u> 6.5	<u>1995</u> 0.9	<u>1995</u> 1.3	<u>1995</u> 1.0247	<u>1995</u> 1.0234
Jan		5.6	1.9			
Feb	5.9			1.8 1.6	1.0251	1.0231
Mar	7.7	7.1	2.5		1.0234	
Арг	11.3	11.0	2.5	1.9	1.0243	1.0223
May	15.7	15.4	3.0	2.3	1.0233	1.0218
Jun	21.8	19.6	3.5	3.3	1.0213	1.0212
Jul	23.0	21.9	4.1	3.8	1.0226	1.0215
Aug	23.8	23.4	1.6	3.1	1.0224	1.0207
Sep	24.0	23.1	1.1	2.2	1.0214	1.0209
Oct	21.6	19.4	0.9	1.4	1.0234	1.0219
Nov	14.9	14.9	1.1	1.1	1.0246	1.0230
Dec	8.5	10.0	1.0	1.1	1.0248	1.0235
Annual	15.6	14.8	2.0	2.1	1,0234	1.0221

Temperature

Daily sea surface water temperatures (Figure 19) were measured with an NOS water sampler and thermometer. Monthly mean water temperatures (Table 8) varied with the air temperatures (see Table 2).

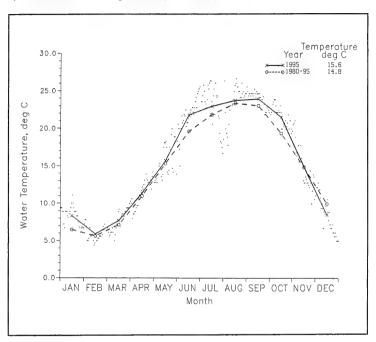


Figure 19. Daily water temperature values with monthly means

Visibility

Visibility in coastal nearshore waters depends on the amount of salts, soluble organic material, detritus, living organisms, and inorganic particles in the water. These dissolved and suspended materials change the absorption and attenuation characteristics of the water that vary daily and yearly.

Visibility was measured with a 0.3-m-diam Secchi disk, and similar to water temperature, variation was related to onshore and offshore winds. Onshore winds moved warm clear surface water toward shore, whereas offshore winds

brought up colder bottom water with large concentrations of suspended matter. Figure 20 shows the daily and monthly mean surface visibility values for the year. Large variations were common, and visibility less than 1 m was expected in any month. Monthly means are given inTable 8.

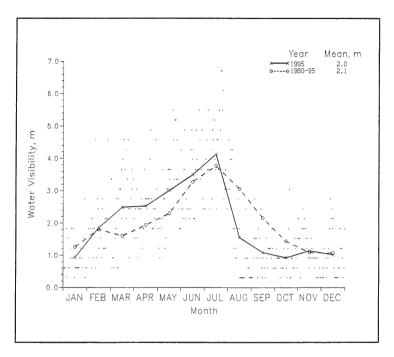


Figure 20. Daily water visibility values with monthly means

Density

Daily and monthly mean surface density values, plotted in Figure 21, were measured with a hydrometer. Monthly means are also given in Table 8. These values are direct readings from the hydrometer. Corrections for differences between ocean water temperature and jar water temperature, as well as use of

uncalibrated hydrometers and other factors, could produce an error amounting to a couple of percent in the direct hydrometer readings.

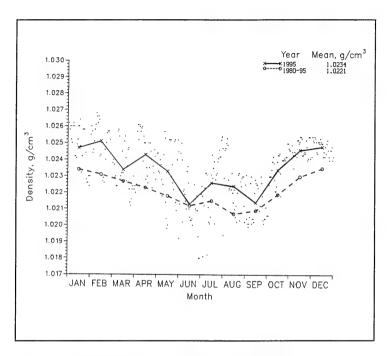


Figure 21. Daily water density values with monthly means

7 Surveys

Waves and currents interacting with bottom sediments produce changes in the beach and nearshore bathymetry. These changes can occur very rapidly in response to storms, or slowly as a result of persistent but less forceful seasonal variations in wave and current conditions.

Nearshore bathymetry at the FRF is characterized by regular shoreparallel contours, a moderate slope, and a barred surf zone (usually an outer storm bar in water depths of about 4.5 m and an inner bar in water depths between 1.0 and 2.0 m). This pattern is interrupted in the immediate vicinity of the pier where a permanent trough runs under much of the pier, ending in a scour hole where depths can be up to 3.0 m greater than the adjacent bottom (Figure 22). This trough, which apparently is the result of the interaction of waves and currents with the pilings, varies in shape and depth with changing wave and current conditions.

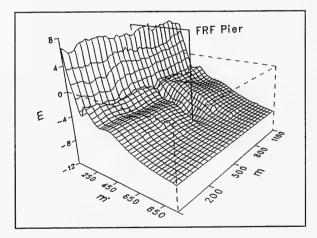


Figure 22. Permanent trough under the FRF pier, 25 January 1995

The effect of the pier on shore-parallel contours occurs as far as 300 m away, and the shoreline may be affected up to 350 m from the pier (Miller, Birkemeier, and DeWall 1983).

Approximately once a month, surveys were conducted of an area extending 600 m north and south of the pier and approximately 950 m offshore. These surveys were conducted to document the temporal and spatial variability in bathymetry. Contour maps resulting from these surveys, along with plots of change in elevation between surveys, are given in Appendix A.

All surveys used the Coastal Research Amphibious Buggy, a 10.7-m-tall amphibious tripod described by Birkemeier and Mason (1984), in combination with a Geodimeter 140-T self-tracking, electronic theodolite, distance meter. Profile locations are shown in each figure in Appendix A. Monthly soundings along both sides of the FRF pier were collected by lowering a weighted measuring tape to the bottom and recording the distance below the pier deck. Soundings were taken midway between the pier pilings to minimize errors caused by scour near the pilings.

A history of bottom elevations below Gauges 645 and 625 is presented in Figure 23 for pier stations 7+80 (238 m) and 18+60 (567 m), along with intermediate locations, 323 and 433 m.

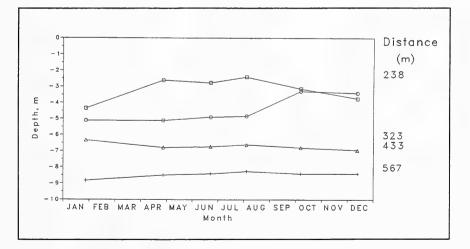
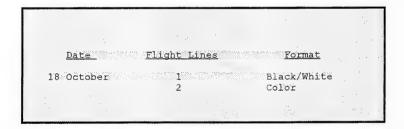


Figure 23. Time-history of bottom elevations at selected locations under the FRF pier

8 Photography

Aerial Photographs

Aerial photographs are taken annually using a 23-cm aerial mapping camera at a scale of 1:12,000. All coverage was at least 60-percent overlap, with flights flown as closely as possible to low tide between 1000 and 1400 EST with less than 10-percent cloud cover. The flight lines covered are shown in Figure 24. Figure 25 is a sample of the imagery obtained on 14 January 1991; the available aerial photographs for the year are:



Beach Photographs

Daily color slides of the beach were taken using a 35-mm camera from the same location on the pier looking north and south (Figure 26). The location from which each picture was taken, as well as the date, time, and a brief description of the picture, were marked on each of the slides.

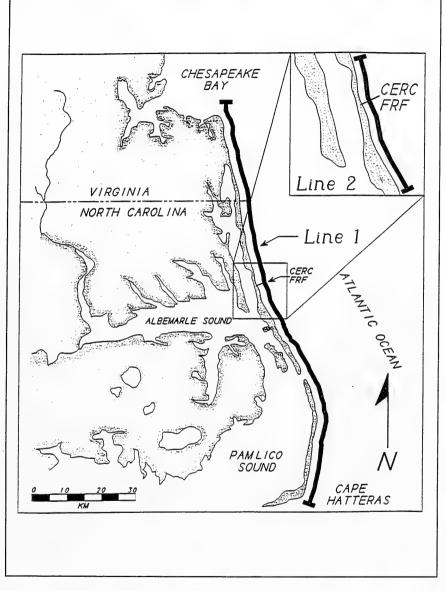


Figure 24. Aerial photography flight lines



Figure 25. Sample aerial photograph, 14 January 1991 (Scale = 1:12,000)



Figure 26. Beach photos looking north and south from the FRF pier (Sheet 1 of 4)

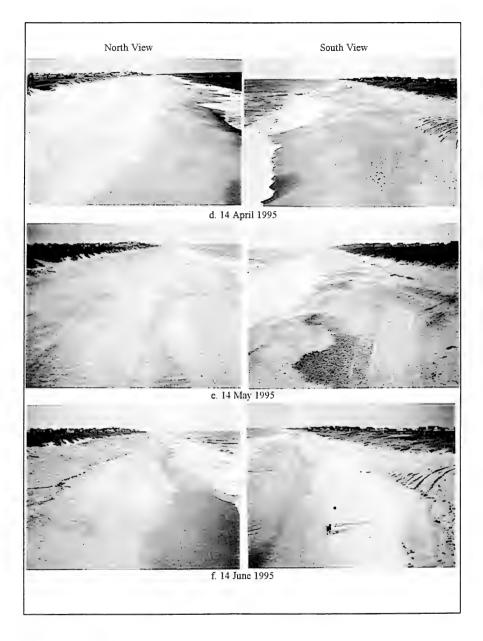




Figure 26. (Sheet 3 of 4)

Chapter 8 Photography



9 Storms

This chapter discusses storms (defined here as times when the wave height parameter H_{mo} equaled or exceeded 2 m at the seaward end of the FRF pier). Sample spectra from Gauge 630 are given in Appendix B. Prestorm and/or poststorm bathymetry diagrams are given in Appendix A. Tracking information was provided by NOAA Daily Weather Maps (U.S. Department of Commerce 1995).

15-16 January 1995 (Figure 27)

Following the passage of a cold front, onshore winds (from northeast) generated by a high pressure system reached 15 m/sec at 1216 EST on 15 January. The maximum H_{mo} (at Gauge 630) reached 3.2 m ($T_p = 11.10$ sec) at 1634 EST also on 15 January. There was 41 mm of precipitation.

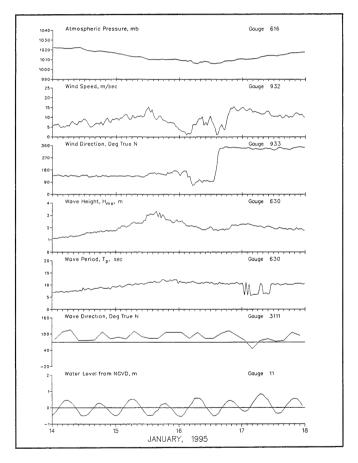


Figure 27. Data for 15-16 January 1995 storm

28-29 January 1995 (Figure 28)

A strong Canadian high pressure system in conjunction with an approaching storm produced onshore winds at the FRF beginning on 28 January. As the storm moved off the North Carolina coast it quickly intensified generating winds (from northeast) of 13 m/sec at 0208 EST on 29 January. Waves at Gauge 625 reached a maximum H_{mo} of 2.10 m ($T_p = 7.3$ sec) at 0208 EST also on 29 January. There was 5 mm of precipitation.

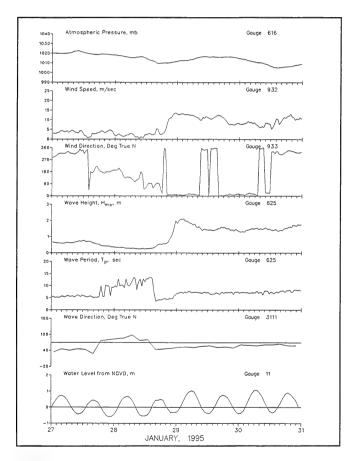


Figure 28. Data for 28-29 January 1995 storm

2 March 1995 (Figure 29)

Northerly winds funneled between a Canadian high pressure system and a small low pressure system located offshore of Cape Hatteras, NC, briefly generated storm waves at the FRF. Waves at Gauge 625 reached a maximum H_{mo} of 2.3 m ($T_p = 9.8$ sec) at 1142 EST on 2 March. Onshore winds (from the north) peaked at 16 m/sec at 0842 EST also on 2 March. The FRF received 13 mm of precipitation from this storm.

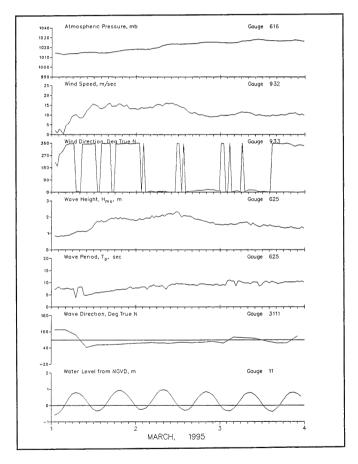


Figure 29. Data for 2 March 1995 storm

7-8 August 1995 (Figure 30)

A strong pressure gradient created by a Canadian high pressure system and a weak storm off Cape Hatteras, NC produced northeasterly winds of 10 m/sec, which peaked at 0400 EST on 8 August. The maximum H_{mo} (at Gauge 625) of 2.3 m ($T_p = 10.2$ sec) was recorded at 2116 EST on 7 August. There was 25 mm of precipitation at the FRF.

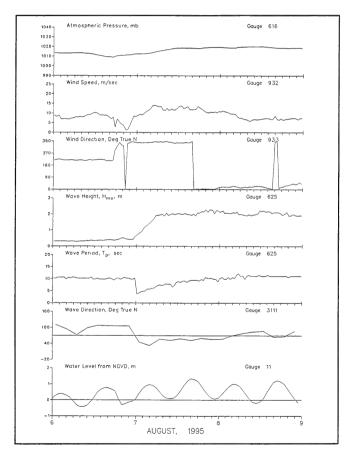


Figure 30. Data for 7-8 August 1995 storm

15-18 August 1995-Hurricane Felix (Figure 31)

Developing in the mid-Atlantic, Felix moved northwest then turned to the west on 15 August steering directly for the North Carolina coast. Downgraded from a category 3 to a 1 (on the Saffir/Simpson Scale) Felix stalled when he collided with a trough of low pressure entrenched along the East coast, then moved offshore, never making landfall. Maximum onshore winds (from northeast) at the FRF reached 17 m/sec at 1816 EST on 16 August. The maximum H_{mo} (at Gauge 630) of 4.6 m ($T_p = 15.1$ sec) was measured earlier that morning at 0208 EST. There was 6 mm of precipitation.

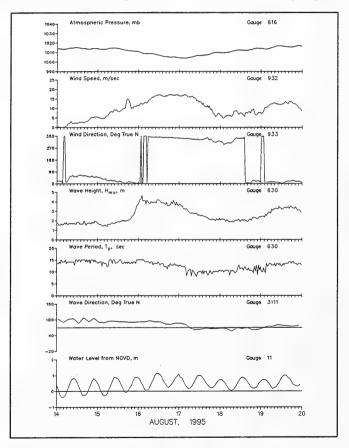


Figure 31. Data for Hurricane Felix, 15-18 August 1995

18-20 August 1995 (Figure 32)

Strong winds associated with the interaction of a Canadian high pressure system with the remnants of Hurricane Felix reached 14 m/sec (from northeast) at 1742 EST on 19 August. The maximum H_{mo} (at Gauge 630) reached 3.5 m ($T_p = 14.2 \text{ sec}$) at 1708 EST on 19 August. There was no precipitation.

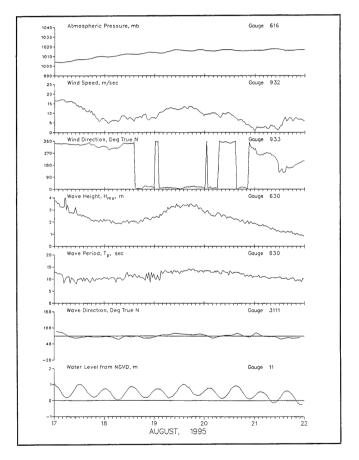


Figure 32. Data for 18-20 August 1995 storm

28 August 1995 (Figure 33)

A combination of a Canadian high pressure system and a low off the North Carolina coast produced onshore winds (from northeast) of 15 m/sec at 1934 EST on 28 August. The maximum H_{mo} (at Gauge 625) reached 2.2 m ($T_p = 6.6$ sec) at 1900 EST also on 28 August. There was 22 mm of precipitation.

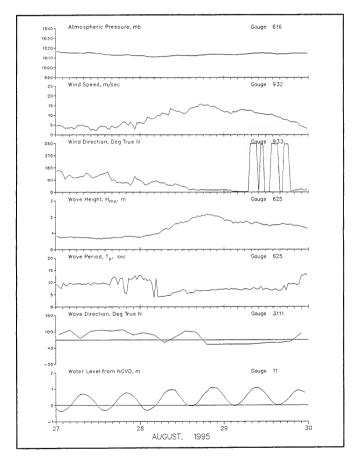


Figure 33. Data for 28 August 1995 storm

19 September 1995 (Figure 34)

Northeasterly winds associated with a Canadian high pressure system reached 13 m/sec at 1034 EST on 19 September. The maximum H_{mo} (at Gauge 625) of 2.1 m ($T_p = 8.26$ sec) followed at 1108 EST. There was no precipitation during this event.

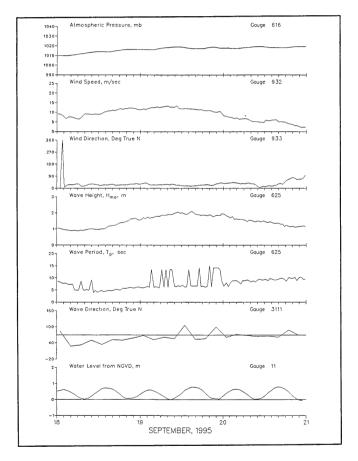


Figure 34. Data for 19 September 1995 storm

23 September 1995 (Figure 35)

Strong onshore winds were generated at the FRF preceding an advancing warm front. The maximum H_{mo} (at Gauge 625) of 2.1 m ($T_p = 6.9$ sec) was attained at 1000 EST on 23 September. Maximum winds (from the northeast) reached 15 m/sec earlier at 0916 EST. There was no precipitation.

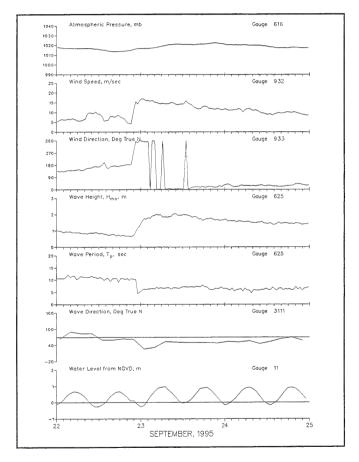


Figure 35. Data for 23 September 1995 storm

29-30 September 1995 (Figure 36)

Northeasterly winds associated with a Canadian high pressure system reached 13 m/sec at 0434 EST on 30 September. The maximum H_{mo} (at Gauge 625) was 2.1 m ($T_p = 9.5$ sec) at 0542 also on 30 September. There was 3 mm of precipitation.

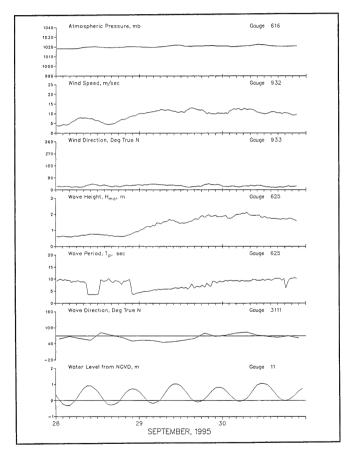


Figure 36. Data for 29-30 September 1995 storm

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Appendix A Survey Data

Contour diagrams constructed from the bathymetric survey data are presented in this appendix. The profile lines surveyed are identified on each diagram. Contours are in half-meter increments referenced to NGVD. The distance offshore is referenced to the FRF monumentation baseline behind the dune.

Changes in FRF bathymetry diagrams constructed by contouring the difference between two contour diagrams are also presented with contour intervals of 0.25 m. Wide contour lines show areas of erosion. Other areas correspond to areas of accretion. Although these change diagrams are based on considerable interpolation of the original survey data, they do facilitate comparison of the contour diagrams.

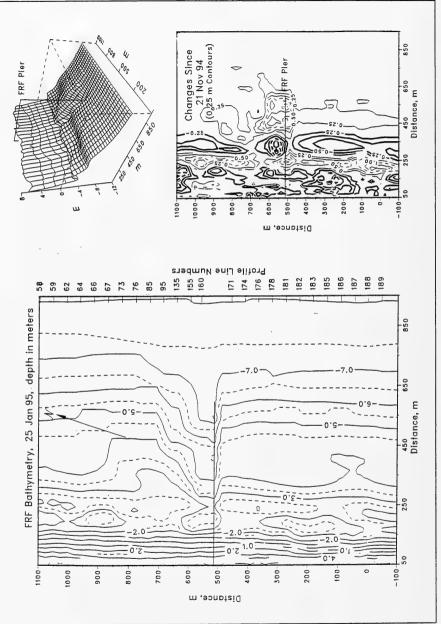


Figure A1. FRF bathymetry, 25 January 1995 (depths relative to NGVD)

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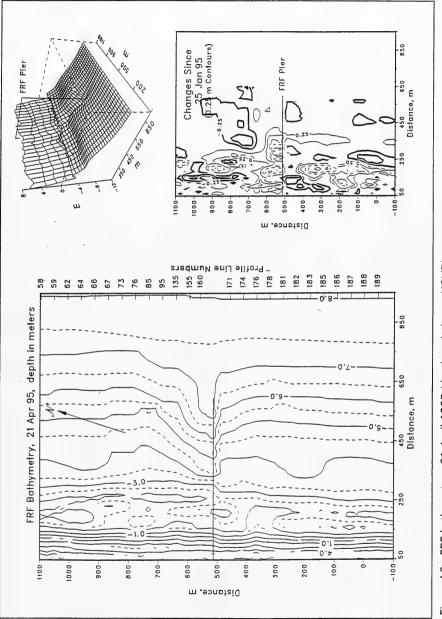
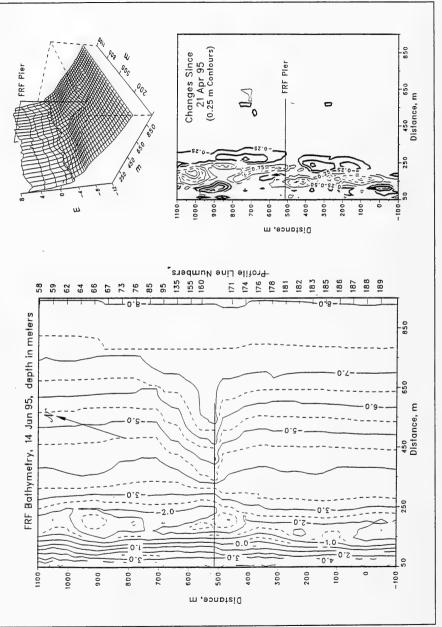
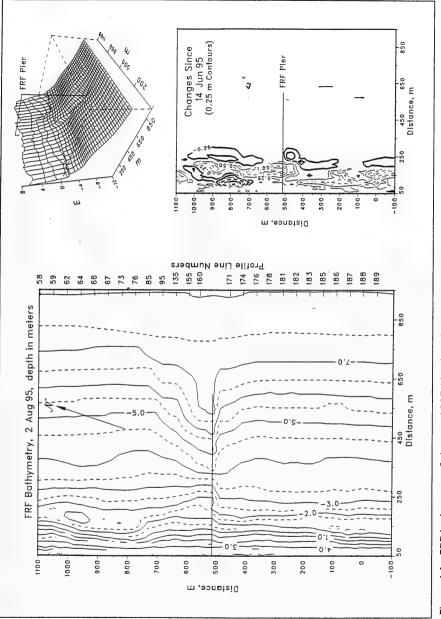


Figure A2. FRF bathymetry, 21 April 1995 (depths relative to NGVD)







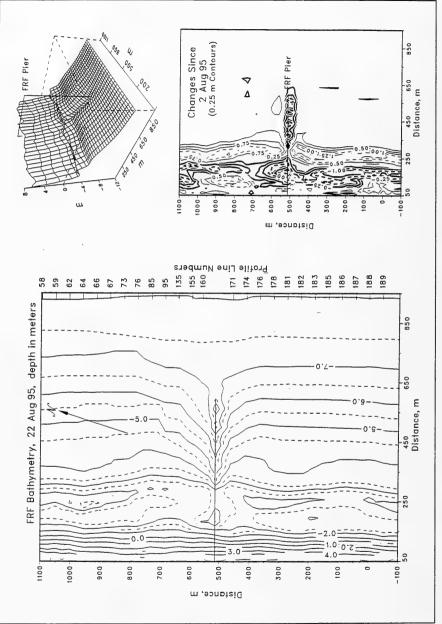
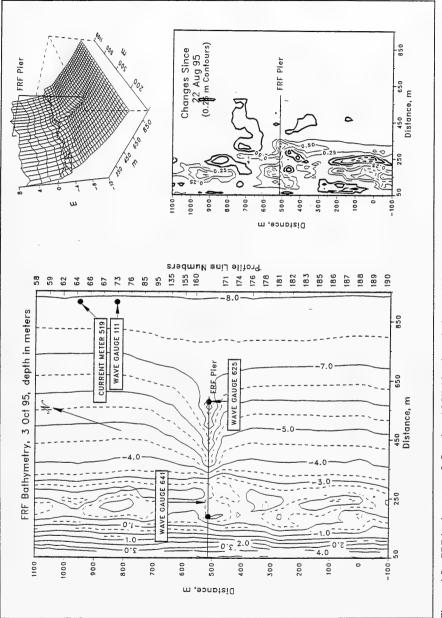


Figure A5. FRF bathymetry, 22 August 1995 (depths relative to NGVD)





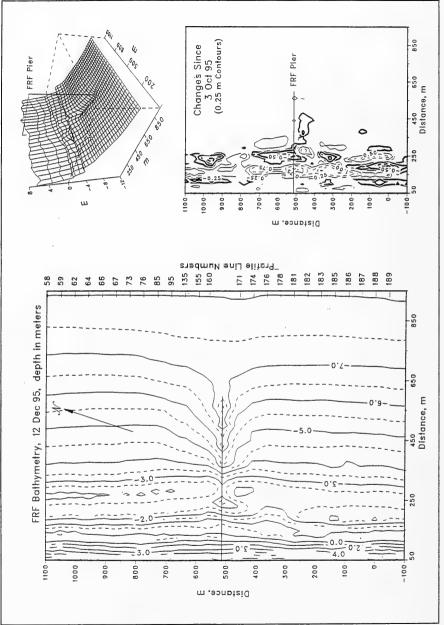


Figure A7. FRF bathymetry, 12 December 1995 (depths relative to NGVD)

Appendix B Wave Data for Gauge 630

Wave data summaries for Gauge 630 for 1995 and for 1980 through 1995 are presented in the following pages:

Daily H_{mo} and T_{p}

Figure B1 displays the individual wave height H_{mo} and peak spectral wave period T_n values, along with the monthly mean values.

Joint Distributions of H_{mo} and T_{p}

Annual and monthly joint distribution tables are presented in Tables B1 and B2, and data for 1980 through 1995 are in Tables B3 and B4. Each table gives the frequency (in parts per 10,000) for which the wave height and peak period were within the specified intervals; these values can be converted to percentages by dividing by 100. Marginal totals are also included. The row total gives the number of observations out of 10,000 that fell within each specified peak period interval. The column total gives the number of observations out of 10,000 that fell within each specified peak period interval.

Cumulative Distributions of Wave Height

Annual and monthly wave height distributions for 1995 are plotted in cumulative form in Figures B2 and B3. Data for 1980 through 1995 are plotted in Figure B4.

Peak Spectral Wave Period Distributions

Annual and monthly peak wave period T_p distribution histograms for 1995 are presented in Figures B5 and B6. Data for 1980 through 1995 are presented in Figure B7.

Persistence of Wave Heights

Table B5 shows the number of times in 1995 when the specified wave height was equaled or exceeded at least once during each day for the duration (consecutive days). Data for 1980 through 1995 are averaged and given in Table B6. An example is shown below:

Height										Day(s						_			
<u> </u>	_1	_2	3		_5	_6	_7	_8	_9	<u>10</u>	<u>11</u>	<u>12</u>	<u>13</u>	14	<u>15</u>	<u>16</u>	<u>17</u>	<u>18</u>	<u>19+</u>
0.5	18	15		14	13	12		11	10	9				8		7			
1.0	50	34	24	21	18	14	12	8	7	3			2						
1.5	41	19	8	6	2	1													
2.0	22	9	5	1															
2.5	10	5	2																
3.0	6	1																	
3.5		1																	
4.0	1																		
4.0	•																		

This example indicates that wave heights equaled or exceeded 1.0 m 50 times for at least 1 day; 34 times for at least 2 days; 24 times for at least 3 days, etc. Therefore, on 16 occasions the height equaled or exceeded 1.0 m for 1 day exactly (50 - 34 = 16); on 10 occasions for 2 days; on 3 occasions for 3 days, etc. Note that the height exceeded 1 m 50 times for 1 day or longer, while heights exceeded 0.5 m only 18 times for this same duration. This change in durations occurred because the longer durations of lower waves may be interspersed with shorter, but more frequent, intervals of higher waves. For example, one of the times that the wave height exceeded 0.5 m for 16 days may have represented three times the height exceeded 1 m for shorter durations.

Spectra

Monthly spectra for the offshore Waverider buoy (Gauge 630) are presented in Figure B8. The plots show "relative" energy density as a function of wave frequency. These figures summarize the large number of spectra for each month. The figures emphasize the higher energy density associated with storms, as well as the general shifts in energy density to different frequencies. As used here, "relative" indicates the spectra have been smoothed by the threedimensional surface drawing routine. Consequently, extremely high- and lowenergy density values are modified to produce a smooth surface. The figures are not intended for quantitative measurements; however, they do provide the energy density as a function of frequency relative to the other spectra for the month.

Monthly and annual wave statistics for Gauge 630 for 1995 and for 1980 through 1995 are presented in Table B7.

Figure B9 plots monthly time-histories of wave height and period.

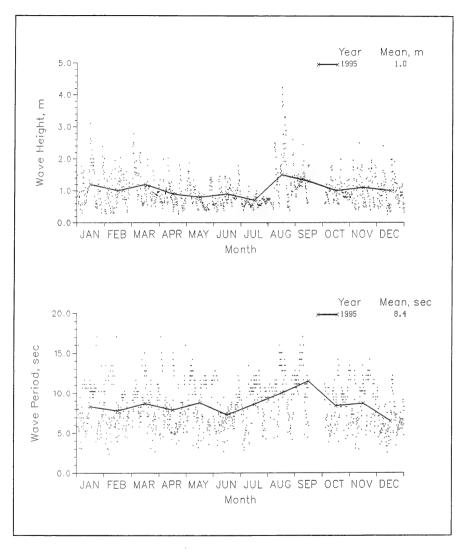


Figure B1. 1995 daily wave height and period values with monthly means for Gauge 630

Table B1 Annual Joint Distribution of H_{mo} versus T_p

Height(m)						Per	riod(s	ec)					Tota
	2.0-	3.0-	4.0-	5.0-	6.0-		8.0-	9.0- 9.9	10.0- 	12.0- 13.9		16.0- Longer	
0.00 - 0.49	15	15	44	95	146	117	95	66	219	36	131	22	1001
0.50 - 0.99	29	204	343	714	634	503	503	671	904	138	350	22	5015
.00 - 1.49		22	168	430	517	328	233	219	408	109	146		2580
.50 - 1.99			7	124	160	175	117	87	211	22	80		983
.00 - 2.49				22	51	51	22	44	87	7	7	7	298
.50 - 2.99					7		7	7	22	7	7		57
.00 - 3.49									7	15	7		29
.50 - 3.99								•		15	7		22
.00 - 4.49						•			•	•	15	•	15
.50 - 4.99							•		•		•	•	0
.00 - Greater			•				•		:				0
Total	44	241	562	1385	1515	1174	977	1094	1858	349	750	51	

Table B2 Monthly Joint Distribution of H_{mo} versus T_p

			P	ercent	Occur				ght and	1 Perio	20			
Height (m)							riod(s							Tota
	2.0-	3.0- <u>3.9</u>	4.0-	5.0-	6.0-	7.0-	8.0-	9.0- <u>9.9</u>	10.0- 11.9	12.0-	14.0-	16.0- Longer		
.00 - 0.49			81	81		81	81	81	163	81	81	163		893
.50 - 0.99		325	325	976	488	244	325		894		163	81		3821
.00 - 1.49			163	569	732	163			569	•				2196
.50 - 1.99		•	-		407	325	325	244	813	•	•	-		2114
.00 - 2.49 .50 - 2.99	•	•	•	81	81	81	81	163	244 163	:	:			16:
.00 - 3.49	:		:	:	:	:	:		81	:	:			8
.50 - 3.99														-
.00 - 4.49														
.50 - 4.99														
.00 - Greater														
Total	0	325	569	1707	1708	894	812	488	2927	81	244	244		
			Pe	ercent	Occur	Februa rence (3	ry 1999 X100) (5, Gaug of Heig	ge 630 ght and	l Perio	bd			
Height(m)							riod(s							Tot
	2.0-	3.0- 3.9	4.0-	5.0- 5.9	6.0- 6.9	7.0-	8.0- 8.9	9.0- 9.9	10.0-	12.0- 13.9	14.0- 15.9	16.0- Longer		
.00 - 0.49			89	89	179	179	268	89	357	268	446	89		205
.50 - 0.99	89	268	536	179	536	446	179	804	446		179			366
.00 - 1.49		179	89	536	1250	446	268	357						312
50 - 1.99				536	89	268	179							107
.00 - 2.49						89								8
50 - 2.99												-		
00 - 3.49												•	-	
50 - 3.99								•						
00 - 4.49		•					•	•	•	•	•	•		
50 - 4.99		•		•	•	•	•	•	•	•	•			
00 - Greater Total	89	447		1340				1250	803	268	625	89		
IOLAI	09		/14	1310	2031	1110								
			Pe	ercent	Occur			5, Gaug of Heig	ge 630 ght and	l Perio	od			
Height(m)						Pe	riod(s	ec)						Tot
	2.0-	3.0- <u>3.9</u>	4.0- <u>4.9</u>	5.0- <u>5.9</u>	6.0- <u>6.</u> 9	7.0-	8.0-	9.0- <u>9.9</u>	10.0-	12.0- 	14.0- 15.9	16.0- Longer		
.00 - 0.49														
.50 - 0.99	83	83	167	500	417	667		1083	833	167	333	•		508
00 - 1.49				167	333	417	417	250	583	83	333	•		258
50 - 1.99		•	•	167		250	167	417	500	•	•	•		150
00 - 2.49		•	•*	167	167	250	83	83 83	:	•	•	•		16
50 - 2.99 00 - 3.49	-	•	•		•	•	83	ده .	:	:	:	:		Te
.00 - 3.49	•	:	:	:	:	:	:		:	:	:			
.00 - 4.49	:			:	:						:			
.50 - 4.99														
.00 - Greater										:	:	:		
Total	83	83	167	1001	917	1584	1417	1916	1916	250	666	0		

Table B2 (Continued)

Height(m)							x100) (_			Tot
	2.0-	3.0-	4.0-	5.0-	6.0-	7.0-	8.0-	9.0- 9.9	10.0-	12.0~ 	14.0-	16.0- Longer	:	
0.00 - 0.49				167	83 750	83 833	333	83 167	333	83	167			133
0.50 - 0.99 1.00 - 1.49		83	250	333	500	833 417	833 333	167	83	583	500	167		616 200
1.50 - 1.99				167	83	167					:	:		41
2.00 - 2.49					83									8
2.50 - 2.99 3.00 - 3.49	•	:	:	:	:	:	:	:	:	:		•		
3.50 - 3.99		:					:	:	:	:	:	:		
4.49														
4.50 - 4.99 5.00 - Greater	•	•	•	•	•	•	•	•	·	•	•	•		
Total	0	83	1000	2084	1499	1500	1499	417	416	666	667	167		
			Pe	ercent	Occur:	Ma rence ()	ay 1995 K100) d	5, Gaug of Heig	ge 630 ght and	l Perio	od			
Height(m)						Pei	riod(se	ec)						Tot
	2.0-	3.0- <u>3.9</u>	4.0-	5.0-	6.0-	7.0- 7.9	8.0-	9.0- <u>9.9</u>	10.0-	12.0-	14.0- 15.9	16.0- Longer		
0.00 - 0.49				323	726	161			645		323			
0.50 - 0.49	:	323	323	3∠3 403	323	565	242	565	1048	242	323	:		217 476
L.00 - 1.49			81	565	242	242	242	242	887	81	81			266
1.50 - 1.99	•	•	•		81	81	161	81	•		•			40
2.00 - 2.49 2.50 - 2.99	•	:	:	:	:	:	:	÷	:	:	:	•		
3.00 - 3.49					:		:	:	:	:	:	:	-	
3.50 - 3.99														
4.00 - 4.49		•	•	•	•			•	•	•	•	•		
4.50 - 4.99 5.00 - Greater	:			•	•	•	-	•		•	-	•		
Total	٥	323	404	1291	1372	1049	645	888	2580	323	1130	0		
						Jun	ne 1995 (100) c	, Gaug	e 630					
Height(m)			Pe	ercent	Occuri		iod(se		ht and	Perio	d			Tot
	2.0-	3.0- <u>3.9</u>	4.0-	5.0-	6.0-	7.0- 7.9	8.0-	9.0-	10.0-	12.0-	14.0-	16.0- Longer		
0.00 - 0.49				167	167			83	167		167			75
0.50 - 0.99	83	250	167		1917	1083	917	250	83	:	167			625
00 - 1.49		•	83	333	417	833	500	417	83					266
50 - 1.99 00 - 2.49	•	·	·	:	•	83	83	•	83	·	83	•		33
.50 - 2.99	:	:	:		:	:	:	:	:	:	:			
.00 - 3.49					:			:	:					
.50 - 3.99		•	·			•	•	•		•				
.00 - 4.49 .50 - 4.99	•	•	•		•	•	•	:	:	:	:	•		
.00 - Greater	:				:		:		:			:		
Total	83	250	250	1833	2501	1999	1500	750	416	0	417	0		
						(Con	tinued	.)					neet 2	

Table B2 (Continued)

Height(m)						Pe	riod(s	ec)						To
	2.0-	3.0-	4.0-	5.0- <u>5.9</u>	6.0-	7.0-	8.0-	9.0- 9.9	10.0-	12.0- _13.9	14.0- 15.9	16.0- Longer		
0.00 - 0.49		:	81		:	244		244	407		81			10
0.50 - 0.99 1.00 - 1.49	81	325	732	813 81	569	407	1057	1545	2927	81	325	:		88
1.50 - 1.49	•	:	:	01				:	•		:			
2.00 - 2.49														
2.50 - 2.99														
3.00 - 3.49			•			•	•		•	-	•			
3.50 - 3.99 1.00 - 4.49			•	•	•	•	•	•	•	•	•	•		
1.50 - 4.49	•	•	•		•	•	-	•	:	:		:		
5.00 - Greater	:	:		:		:	÷		:					
Total	81	325	813	894	569	651	1057	1789	3334	81	406	0		
			P	ercent	Occuri	Augus rence (1	st 199! (100) (5, Gau of Heig	ge 630 ght and	l Perio	bđ			
Height (m)						Per	riod(se	ec)						т
	2 0-	3 0-	4 0-	5 0-	6.0-	7.0-	8.0-	9.0-	10.0-	12.0-	14.0-	16.0-		
	2.9	3.9	4.9	5.9	6.9	7.9	8.9	9.9	11.9	13.9	15.9	Longer		_
0.00 - 0.49					177	177	88	•	177	•		•		e
0.50 - 0.99				177	177	442	442	796	619		265	•		29
1.00 - 1.49	•	•	354	354	177 88	88	•	177 177	796 442	88 265	265 442	•		22
1.50 - 1.99 2.00 - 2.49	•	:	:	•	177	177	88	265	796	283	88	:		16
2.50 - 2.99		:		:	88			205	88	88	88			3
3.00 - 3.49										177	88		-	2
3.50 - 3.99										177	88			2
1.00 - 4.49					-				-	-	177			1
1.50 - 4.99				•			•	•	•		•	·		
5.00 - Greater Total	0	ò	354	531	884	884	618	1415	2918	883	1501	0		
					S	eptemb	er 199	5, Gau	ge 630					
Height (m)			P	ercent	Occur:		K100) (riod(s		ght and	d Peri	bd			To
Height (m)	2 0.	3.0-	4 0-	5.0-	5.0-				10.0-	12.0-	14.0-	16.0-		
	2.9	3.9	4.9	5.9	6.9	7.9	8.9	9.9	_11.9	13.9	15.9	Longer		_
0.00 - 0.49								:	:		:	•		19
0.50 - 0.99	•			•	328			164 656	1311 1639	1967	164 1311	•		63
1.00 - 1.49 1.50 - 1.99	•	•	328	164	328	328	164	656	492	1967	492			14
2.00 - 2.49		:	:	104	320	:	:	:				164		1
2.50 - 2.99	:										-			
3.00 - 3.49														
3.50 - 3.99								•	•	•	•	•		
4.00 - 4.49				•				•	•		·	•		
4.50 - 4.99	•	•	•	•		•	·	•	•	•	•			
5.00 - Greater Total	0	0	328	164	656	328	164	820	3442	1967	1967	164		
IULAI	U	0	520	*04	000	520	203	520						

Table B2 (Concluded)

S0 - 0.99 .88 351 439 351 351 759 175 1053 351 439 .88 .351 S0 - 1.99 .88 263 .263 .88 263 <	Height(m)							riod(s		ght and					Tot
S0 - 0.99 .88 351 439 351 351 759 175 1053 351 439 .88 .351 439 .88 .351 439 .88 .351 .351 439 .88 .351 </th <th></th> <th>2.0-</th> <th>3.0-</th> <th>4.0-</th> <th>5.0-</th> <th>6.0-</th> <th>7.0-</th> <th>8.0-</th> <th>9.0- <u>9.9</u></th> <th>10.0-</th> <th>12.0- <u>13.9</u></th> <th>14.0- 15.9</th> <th>16.0- Longer</th> <th></th> <th></th>		2.0-	3.0-	4.0-	5.0-	6.0-	7.0-	8.0-	9.0- <u>9.9</u>	10.0-	12.0- <u>13.9</u>	14.0- 15.9	16.0- Longer		
D0 - 1.46	.00 - 0.49										:	:			
Sign - 1.99		•											-		596
D0 - 2.49	00 - 1.49 50 - 1.99	•													6
$ \begin{array}{c} 30 - 2.99 \\ 00 - 3.49 \\ 30 - 3.99 \\ 00 - 4.49 \\ 30 - 3.99 \\ 01 - 3.49 \\ 01 - 3.49 \\ 01 - 3.99 \\ 01 - 3.49 \\ 01 - 3.99 \\ 01 - 3.49 \\ 01 - 3.99 \\ 01 - 3.49 \\ 01 - 3.99 \\ 01 - 3.49 \\ 01 - 3.99 \\ 01 - 3.49 \\ 01 - 3.99 \\ 01 - 3.49 \\ 01 - 3.99 \\ 01 - 3.49 \\ 01 - 3.99 $	00 - 2.49														
$ \begin{array}{c} 50 - 3.99 \\ 00 - 4.49 \\ 50 - 4.99 \\ 01 - 67.449 \\ 01 - 67.449 \\ 01 - 67.6 + 4.04 + 1228 + 965 + 1227 + 2017 + 1492 + 351 + 527 + 0 \\ \end{array} \\ \begin{array}{c} \hline \\ \hline $	50 - 2.99														
D0 - 4.49	00 - 3.49							•		•	•		•		
S0 - 4.99		•						•	•	•			•		
D0 - Greater Total 0 176 614 1404 1228 965 1227 2017 1492 351 527 0 November 1995, Gauge 630 Percent Occurrence(X100) of Height and Period aight (m) Percent Occurrence(X100) of Height and Period 2.0- 3.0- 4.0- 5.0- 6.0- 7.0- 8.0- 9.0- 10.0- 12.0- 14.0- 16.0- 2.0- 3.0- 4.0- 5.0- 6.0- 7.0- 8.0- 9.0- 10.0- 12.0- 14.0- 16.0- 2.0- 3.0- 4.0- 5.0- 6.0- 7.0- 8.0- 9.0- 10.0- 12.0- 14.0- 16.0- 2.0- 3.0- 4.9 5.9 6.9 7.9 8.0 9.0- 11.9 13.2 15.9 Longer 300 - 1.49 14.92 14.1 16.9 <		•			•	•	•	•	•						
Total 0 176 614 1404 1228 965 1227 2017 1492 351 527 0 November 1995, Gauge 630 Percent Occurrence(X100) of Height and Period eight (m) Period(sec) To 2.0-3.0-4.0-5.0-6.0-7.0-8.0-9.0-10.0-12.0-14.0-16.0- 2.9 2.0-3.0-4.0-5.0-6.0-7.0-8.0-9.0-10.0-12.0-14.0-16.0- 2.9 2.0-3.0-4.0-5.0-6.0-7.0-8.0-9.0-10.0-12.0-14.0-16.0- 2.9 4.9 5.9 6.5 7.9 8.9 9.9 11.9 13.9 15.9 Longer			:			:									
Percent Occurrence(X100) of Height and Period eight (m) To 2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0 12.0 14.0 16.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0 12.0 14.0 16.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 11.9 13.9 Longer 00 0.39 169 593 593 39 254 85 254 254 <t< td=""><td></td><td>0</td><td>176</td><td>614</td><td>1404</td><td>1228</td><td>965</td><td>1227</td><td>2017</td><td>1492</td><td>351</td><td>527</td><td>0</td><td></td><td></td></t<>		0	176	614	1404	1228	965	1227	2017	1492	351	527	0		
bight (m) Period(sec) To 2.0-3.0-4.0-5.0-6.0-7.0-8.0-9.0-10.0-12.0-14.0-16.0- 2.93.94.95.96.97.98.99.91.19 13.915.9 Longer						1	Novemb	er 199	5, Gau	ge 630	Peri	-d			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	eight(m)			P	ercenc	occur.									To
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		2.0-	3.0-	4.0-	5.0-	6.0-	7.0-	8.0-	9.0-	10.0-	12.0-	14.0-	16.0-		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		2.9	3.9	4.9	5.9	6.9	7.9	8.9	9.9	11.9	13.9	15.9	Longer		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$															10
1.49 1.69 593 593 533 339 254 85 254 254 254 255 50 - 1.99 .85 85 847 339 85 85 169 85 17 50 - 2.49					254						169		•		
30 1.39 1.35 85 87 339 85 85 169 85 17 30 -2.49 85 <td>50 - 0.99</td> <td></td> <td>25</td>	50 - 0.99														25
D0 - 2.49	50 - 1 99														17
30 - 2.99	00 - 2.49							85							
50 - 3.99	50 - 2,99														
December 1995, Gauge 630 Percent Occurrence (X100) of Height and Period December 1995, Gauge 630 Percent Occurrence (X100) of Height and Period 2.0- 3.0- 4.0- 5.0- 6.0- 7.0- 8.0- 9.0- 10.0- 12.0- 14.0- 16.0- 2.9 3.9 4.9 5.9 6.9 7.9 8.9 9.9 11.9 13.9 15.9 Longer 00 - 0.49 81 161 161 242 242 323 323	00 - 3.49										•	•	•	-	
S0 - 4.99	50 - 3.99		•								•	•	•		
D0 - Greater		•	•	•							•	•	•		
Total 85 169 339 932 1949 1271 509 1017 2118 169 1440 0 December 1995, Gauge 630 Percent Occurrence(X100) of Height and Period 2.0- 3.0 To 2.0- 3.0 7.9 Period(sec) To 2.0- 3.0 6.9 7.9 8.9 9.10.0- 12.0- 16.0- 2.0- 3.0 7.9 8.9 9.11.9 13.9 Longer		•	•	•	•	•	•	•					-		
Percent Occurrence (X100) of Height and Period Period(sec) 2.0-3.0-4.0-5.0-6.0-7.0-8.0-9.0-10.0-12.0-14.0-16.0- 2.9 3.9 4.9 5.9 6.9 7.9 8.9 9.9 11.9 13.9 15.9 Longer 00-0.49 81 161 161 242 242 323 323		85	169	339	932	1949	1271	509	1017	2118	169	1440	0		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				P	ercent	Occur	Decemb rence (:	er 199 X100) (5, Gaug of Heig	ge 630 ght and	l Perio	od			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	eight(m)														То
50 -0.39 . 403 565 1613 1129 242 161 81 242 . . . 444 00 -1.49 . .323 726 887 242 403 242 242 . <		2.0-	3.0- 3.9	4.0-	5.0- 5.9	6.0- 6.9	7.0-	8.0-	9.0- <u>9.9</u>	10.0-	12.0- 13.9	14.0- 15.9	16.0- Longer		
00 -1.49	00 - 0.49	81								. :					15
00 - 161 81 323 81 161 81 8 00 - 2.49 - - 81 - - - - - - - - 0 - 0.5 - 1.99 - - - - - - - - - - - - - - 0 - 0.5 - 1.93 - <td< td=""><td>50 - 0.99</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td><td>•</td><td>•</td><td></td><td></td></td<>	50 - 0.99										-	•	•		
30 - 1.93	00 - 1.49										•		•		30
00 - 2.49 .		•	•					91					:		0
00 - 3.49		•	•	•				:			:				
50 - 3.99	00 - 3.49							-							
00 - 4.49	50 - 3.99														
00 - Greater	00 - 4.49												•		
00 - Greater	50 - 4.99		•		•	•	•	•	•	•	•	•	•		
10/01 01 1012 2/42 2420 1130 200 692 0 0 V			564	1049	2743	2420	1120	920	303	645	÷	81	p		
	TOCAT	91	204	1043	2/92	20 M 20 V	1120	200	دعد	040	5	-	-		

Table B3 Annual Joint Distribution of H_{mo} versus T_p (All Years)

			P	ercent					Gauge ght an	630 d Perio	d		
Height(m)						Pe	riod(s	ec)					Tota
	2.0-	3.0- <u>3.9</u>	4.0-	5.0- 5.9	6.0-	7.0-	8.0-	9.0-		12.0- 		16.0- Longer	
0.00 - 0.49	24	15	29	65	85	123	338	278	196	66	120	5	1344
).50 - 0.99	32	140	276	505	574	534	887	766	774	126	234	15	4863
1.00 - 1.49		11	149	407	412	243	272	217	324	44	115	2	2196
50 - 1.99			11	163	238	111	84	77	142	31	67	3	927
.00 - 2.49			1	24	90	67	50	34	63	25	33	1	388
.50 - 2.99				1	14	32	20	14	34	9	23	1	148
.00 - 3.49					1	10	12	12	20	7	8		70
.50 - 3.99							5	9	12	5	5		36
.00 - 4.49							2	4	7	3	5		21
.50 - 4.99								1	1		1		3
.00 - Greater										1	1		2
Total	56	166	466	1165	1414	1120	1670	1412	1573	317	612	27	

Table B4 Monthly Joint Distribution of H_{mo} versus T_p (All Years)

Height(m)						rence (riod(s						Tot
Height(m)	2.0-	3.0-	4.0-	5.0~	6.0-	7.0-	8.0-	9.0-	10.0-	12.0-	14.0-	16.0- Longer	10
	74	6	12	68	56	37	130	278	247	43	93	12	10
0.00 - 0.49 0.50 - 0.99	56	191	210	432	377	315	401	692	815	80	185	12	370
1.00 - 1.49		12	167	630	550	247	241	198	469	19	43	б	25
1.50 - 1.99			25	303	432	173	105	117	259	31	43		14
2.00 - 2.49				43	148	173	93	43	130	31	19	5	61
2.50 - 2.99					19	68	49	25	74	12	49		2
3.00 - 3.49		•			•	25	25	6	37	•	•	•	
3.50 - 3.99	•	•	•	•	•	•		6	12 6	•	•	•	:
4.00 - 4.49	•	•	•	•	•	•	:	:	6	:	:	:	
4.50 - 4.99 5.00 - Greater	•	•	•	•		•	•	•	0	•	•	•	
Total	130	209	414	1476	1582	1038	1044	1365	2055	216	432	36	
			P	ercent	Fel Occur	bruary rence ()	X100)	of Heig	Gauge (ght and	530 1 Perio	bđ		Tot
Height(m)							riod(s						10
	2.0-	3.0- 3.9	4.0-	5.0- <u>5.9</u>	6.0- 	7.0-	8.0-	9.0- 	10.0-	12.0-	14.0- _15.9	16.0- Longer	_
0.00 - 0.49	14		14	48	68	55	96	164	116	41	116	7	7:
0.00 - 0.49	48	96	191	369	464	328	478	710	1004	14	150	7	38
1.00 - 1.49	40	20	137	594	622	273	307	362	505	61	171		305
1.50 - 1.99			7	239	342	184	123	130	157	61	82		133
2.00 - 2.49				68	150	61	34	61	75	48	82		5
2.50 - 2.99				7	20	55	34	7	82	14	48	7	2
3.00 - 3.49						20	7	20	27	14	14		10
3.50 - 3.99								7	7		7		
4.00 - 4.49								7	27		7		4
4.50 - 4.99	•			•	•	•		•	•	•	•	•	
5.00 - Greater	. 62		349	1325	1666	976	7 1086	1468	2000	253	677	21	
Total	62	116	349	1325	1666	976	1086	1468	2000	200	6//	21	
						March	1980-	1995 /	Caure (530			
			P	ercent		rence ()					bd		
Height(m)						Pe	riod(s	ec)					Tot
						7.0-							
	2.9	3.9										Longer	
0.00 - 0.49	6	11	6	17	39	44	127	50	160	55	94	•	6
0.50 - 0.99	17	72	193	409	491	491	613	657 276	883 646	99 55	237 282	•	410
1.00 - 1.49	•	17	199 11	403 215	502 243	315 121	326	276 149	646 282	55	282	•	12
1.50 - 1.99 2.00 - 2.49	•	•	11	39	243	61	99 77	61	282	22	77	:	5
2.50 - 2.99			•		28	17	33	11	50	11	33	6	1
3.00 - 3.49	:	:	:	:	20	11	6	11	44	6	6		
3.50 - 3.99								17	44		17		
4.00 - 4.49							6	11	17		17		!
4.50 - 4.99									11			•	:
5.00 - Greater												:	
Total	23	100	409	1083	1375	1060	1287	1243	2247	303	868	6	
						(Co	ntinue	d)				(5)	neet 1 of 4

Table B4 (Continued)

			P	ercent	Occur	April rence(1980- X100)	1995, of Hei	Gauge (ght and	630 d Perio	bd			
Height(m)						Pe	riod(s	ec)						Total
	2.0-	3.0- 3.9	4.0- <u>4.9</u>	5.0- <u>5.9</u>	6.0- <u>6.9</u>	7.0- 	8.0- 8.9	9.0- <u>9.9</u>	10.0-	12.0- 13.9	14.0- 15.9	16.0- Longer		
0.00 - 0.49 0.50 - 0.99	6 67	11 168	17 263	45 542	34 609	28 531	263 899	156 771	140 944	95 257	140 391	11		935 5453
L.00 - 1.49		11	117	296	363	318	341	302	307	61	112			2228
L.50 - 1.99			6	168 28	128 67	78 22	78 39	78 45	173 78	17 22	61 6	:		787 307
2.00 - 2.49		:	:	6	17	17	28	17	39	22	11			157
.00 - 3.49						22	11 22	22	22 6	6		•		83 34
.50 - 3.99		:	:	:	:	6	22 6	:	6	:	:	:		12
.50 - 4.99								6						6
5.00 - Greater Total	73	190	403	1085	1218	1022	1687	1397	1715	480	721	11		0
The Laber / - 1			P	ercent	Occur	rence (1980- X100) riod(s	of Hei		630 d Perio	ođ			Tota
Height(m)														1004
										12.0- <u>13.9</u>		16.0- Longer		
0.00 - 0.49	5	16	38	103	180	147	332	278 980	229 702	60 98	142 240	5		1530 5623
).50 - 0.99 L.00 - 1.49	16	196 5	359 163	550 272	517 289	773 174	1187 348	980 261	310	98 16	240 76			1914
1.50 - 1.99	:		5	82	87	65	109	76	103	16	44			587
2.00 - 2.49	•	•	•	11	60 22	49 16	22 5	38	11	16 11	16	:		223 69
2.50 - 2.99 3.00 - 3.49	:	:	:	:			16	5	5	5	5		-	36
3.50 - 3.99				-				5	5			•		10
1.00 - 4.49 1.50 - 4.99	•	•	:	•		-		:	:	:	:	:		0
5.00 - Greater		:												0
Total	21	217	565	1018	1155	1224	2019	1648	1370	222	528	5		
			P	ercent	Occur		1980- X100)			630 d Perio	od			
Height(m)							riod(s							Tota
	2.0-	3.0- 3.9	4.0-	5.0- <u>5.9</u>	6.0- <u>6.9</u>	7.0-	8.9	9.0- 9.9	11.9		15.9	Longer		
0.00 - 0.49	17	23	35	105	163	280	594	454 978	268 530	29 116	35 134	•		2003 6360
0.50 - 0.99 L.00 - 1.49	41	192 6	379 111	699 262	885 221	804 210	1602 204	105	82		29	:		1230
L.50 - 1.99			12	41	76	47	29	12	76		41	•		334
2.00 - 2.49 2.50 - 2.99	•	•	•	•	17	12	35	6	:	:	:	:		6
2.50 - 2.99 3.00 - 3.49	:	:	:		:	• •	:	:		:				c
3.50 - 3.99								•			•	•		0
1.00 - 4.49 1.50 - 4.99	:	•		•	•	:	:	•	:	:	:	:		c
5.00 - Greater											:	:		c
Total	58	221	537	1107	1362	1359	2464	1555	956	145	239	0		
						(Co	ntinue	d)				(S	heet 2	of 4)
												.0		

Table B4 (Continued)

			P	ercent	Occur	rence (X100)	1995, 0 of Heig	Gauge (ght and	330 1 Perio	bđ			
Height(m)						Pe	riod(s	ec)					-	Total
		3.0- <u>3.9</u>									14.0- 15.9	16.0- Longer	:	
0.00 - 0.49	11	17	74	137	183	411	1113	719	331	91	166	11		3264
0.50 - 0.99 1.00 - 1.49	34	194 11	400 46	708 160	782 188	713 68	1301 97	959 29	537 29	160	148	46		5982 628
1.50 - 1.99				34	6	11	17	11	29					108
2.00 - 2.49 2.50 - 2.99	•		•	6		•	6	•	•	•	•	•		12
3.00 - 3.49	:	:		:	:		:	:	:	:	:	:		0
3.50 - 3.99														0
4.00 - 4.49 4.50 - 4.99	•			•	•		•	•	•	•	•	•		0
5.00 - Greater										:	:	:		ő
Total	45	222	520	1045	1159	1203	2534	1718	926	251	314	57		
								L995, C						
Height(m)			Pe	ercent	Occur:		K100) (riod(se	of Heig ec)	ght and	l Perio	bd			Total
	2.0-	3.0-	4.0-	5.0-	6.0-	7.0-	8.0-	9.0-	10.0-	12.0-	14.0-	16.0- Longer		
												Douger		
0.00 - 0.49 0.50 - 0.99	17	23	57 266	107 526	141	192 775	583 1391	436	277	57	74 255			1964
1.00 - 1.49	28	113	266	305	781 255	181	1391 221	837 141	713 136	136 17	255 45	28		5849 1448
1.50 - 1.99				62	113	51	23	23	68	17	57			414
2.00 - 2.49 2.50 - 2.99	•	•	•	11	34 11	23	17 11	17	74 17	11	11	•		198
3.00 - 3.49	:	:	:	:	6	6	-11	÷	6	11	6	:		56 41
3.50 - 3.99								6		11	6		-	23
4.00 - 4.49 4.50 - 4.99		•	•	•				•	-	•	11			11
4.50 - 4.99 5.00 - Greater	•		:	:	:			•	•		•	•		0
Total	45	142	464	1011	1341	1228	2252	1460	1291	266	476	28		
					Sept	ember	1980-1	.995, G	auge 6	30				
Height(m)			Pe	ercent	Occuri		(100) c	f Heig	ht and	Peric	d			Total
1102 Jac (m)	2.0-	3.0-	4.0-	5.0-	6.0-	7.0-	8.0-	9.0-	10.0-	12.0-	14.0-	16.0-		iotai
0.00 - 0.49	<u>2.9</u> 6	12	17	<u>5.9</u> 29	<u>6.9</u> 29	<u>7.9</u> 64	222	239	11.9	<u>13.9</u> 152	<u>15.9</u> 99	Longer		1050
0.50 - 0.99		117	233	373	478	64 548	222 921	239	991	152	286	6		4828
1.00 - 1.49 1.50 - 1.99		12	87	443	437	286	426	239	350	146	187	6		2619
1.50 - 1.99 2.00 ~ 2.49	:	:	12	152 29	257 82	111 47	76 58	93 23	76 52	17	105 52	6		905 396
2.50 - 2.99						52	35	12	6	6	6	•		117
3.00 - 3.49 3.50 - 3.99						б	12	6	6	6	6	•		42
3.50 - 3.99 1.00 - 4.49	:	:	:	:	:	:	6	6	6	6	6	:		30 12
4.50 - 4.99		:	:			:		:			:	:		0
5.00 - Greater Total	6	141	349	1026	1283	1114	1762	1382	1668	6 503	747	24		6
	·		515				1.02	2002	1000	505				
						(Cor	tinued)				(5)	neet 3 of	4)

Table B4 (Concluded)

riod	630 nd Per:	30 1 Perio	riod	od				
								Tota
)- 14.0- 1 .9 <u>15.9</u>	- 12.0 <u>13.</u>	12.0- 13.9	0- 1	14.0- 	0- 16 .9 I	6.0- Longer		
	22 184							749 4118
	184					5		4118
163	81	81	31 3	163	3	22		1401
	33 16					5		662 310
	16					5		108
	16							75
						5		48
· ·	•	•	•	•	•	5		5
927	444	444	4	927	7	52		
riod	630 nd Per:	30 1 Peric	riod	od				
		_						Tota
)- 14.0- 1 9 15.9								
	57					19		1089
	107					38 19		4037 2841
	38					6		1267
	13							447
	6					•		107 113
	13					:	-	63
	6	6	6					18
6	•	•	•			•		12
	278	278				82		0
riod	630 nd Per:	30 1 Peric	eriod	od				
)- 14.0- 1	12 0	12 0-	0 - 1	14 0	0- 16	6.0-		Tota
9 15.9	13.9	13.9	3.9	15.9	.9 I	Longer		
	94 119					25		1014 3940
	31					25		2470
	44							1390
	63 6							633 207
	6 19					•		150
9 19	19	19	19	19	9			101
	31					•		75
	6					•		18
	432					31		
						(Sh	eet 4	of 4)

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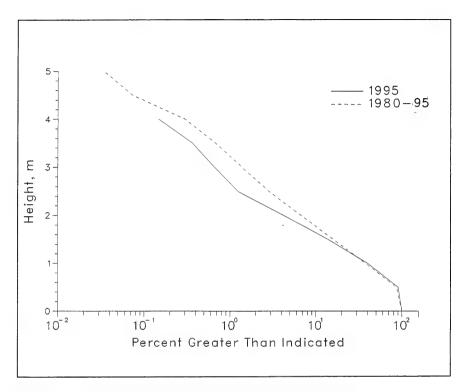


Figure B2. Annual cumulative wave height distributions for Gauge 630

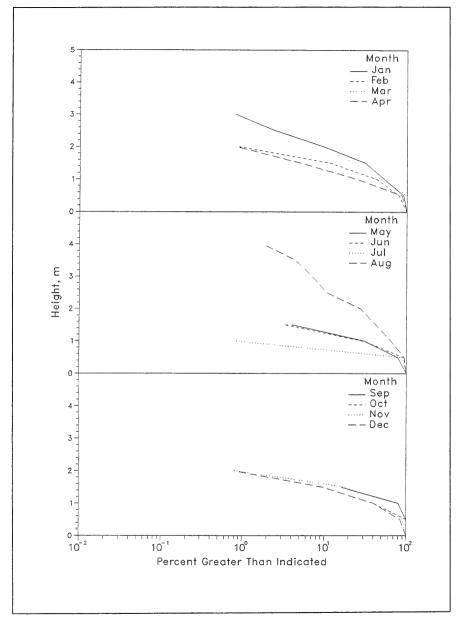


Figure B3. 1995 monthly wave height distributions for Gauge 630

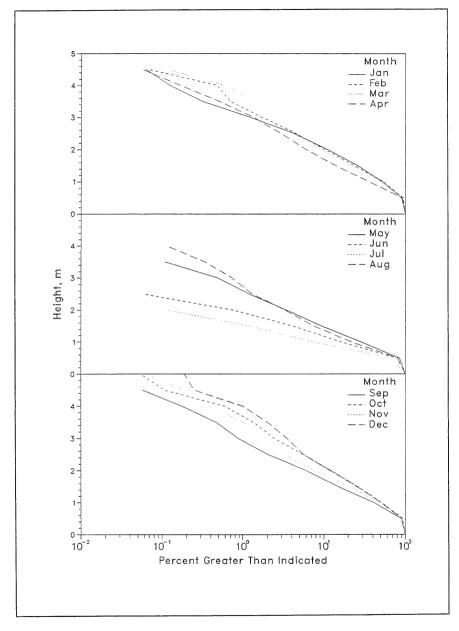


Figure B4. 1980-1995 monthly wave height distributions for Gauge 630

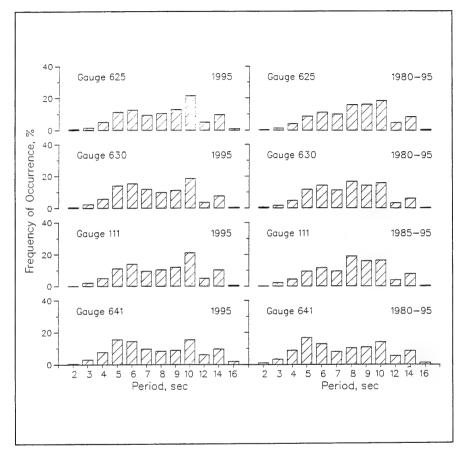


Figure B5. Annual wave period distributions for all gauges

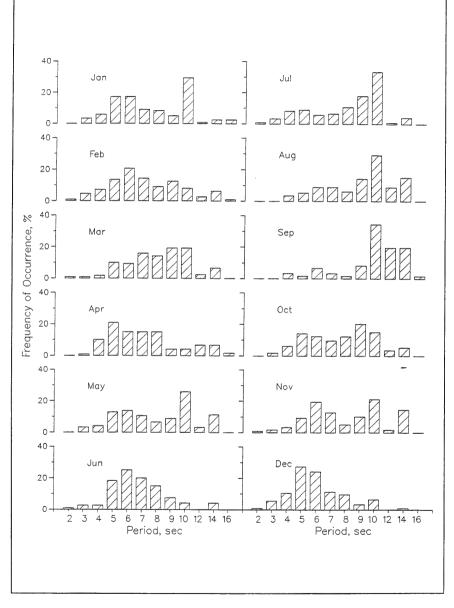


Figure B6. 1995 monthly wave period distributions for Gauge 630

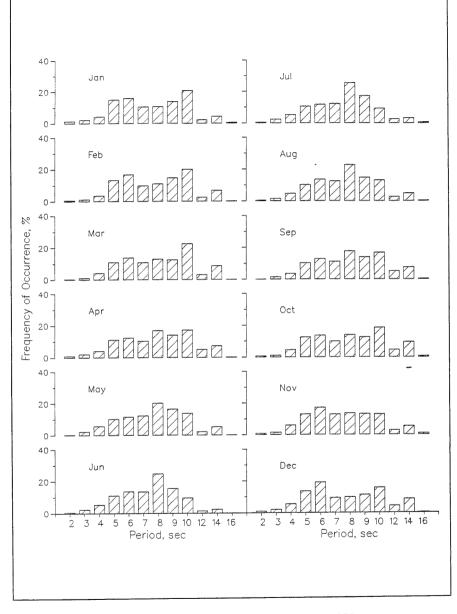


Figure B7. 1980-1995 monthly wave period distributions for Gauge 630

Height					_		Cons	ecut	ive	Day(s) or	Lon	qer				-		
(m)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19+
0.5		11		9			8		7						6		5		4
1.0	58	44	28	21	13	9	6	5	3			1							
1.5	38	22	9	4		3	2	1											
2.0	13	6	3	2		1													
2.5	5	3																	
3.0	3	1																	
3.5		1																	
4.0	1																		

								n	10	r Ga									
Height							Cons	ecut	ive	Day(s) or	Lor	ger						
(m)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19+
0.5	19	17	15	14		13	11		10		9		8	7		6			5
1.0	51	35	24	17	13	10	7	6	5		з		2				1		
1.5	39	22	11	6	4		2		1										
2.0	21	11	5	2		1													
2.5	11	5	2																
3.0	6	3	1																
3.5	з	1																	
4.0	2	1																	

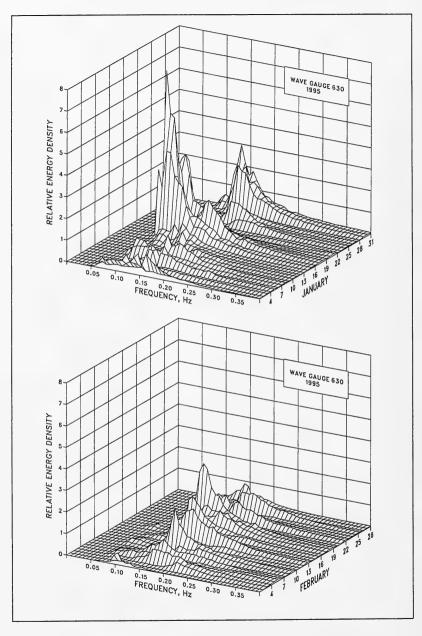


Figure B8. 1995 monthly spectra for Gauge 630 (Sheet 1 of 6)

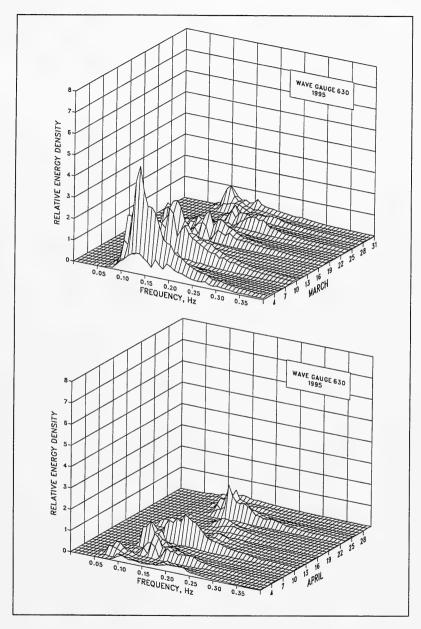


Figure B8. (Sheet 2 of 6)

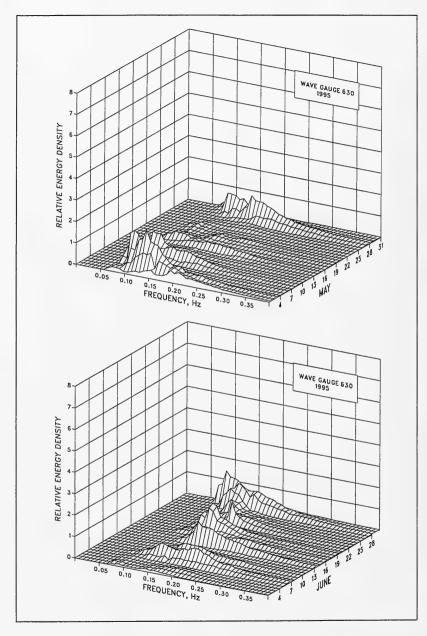


Figure B8. (Sheet 3 of 6)

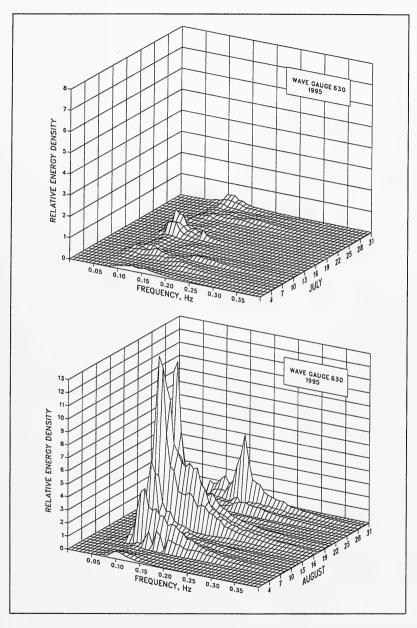


Figure B8. (Sheet 4 of 6)

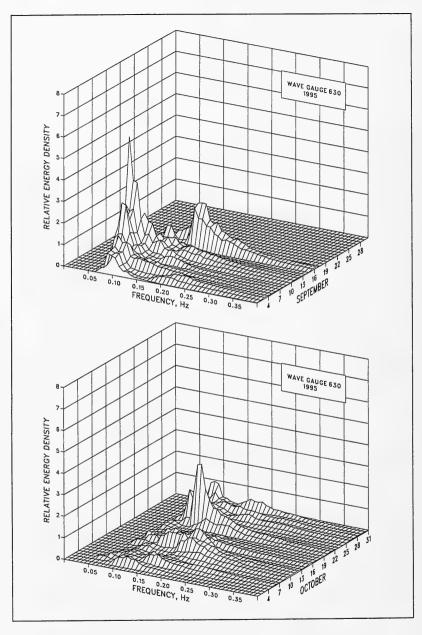


Figure B8. (Sheet 5 of 6)

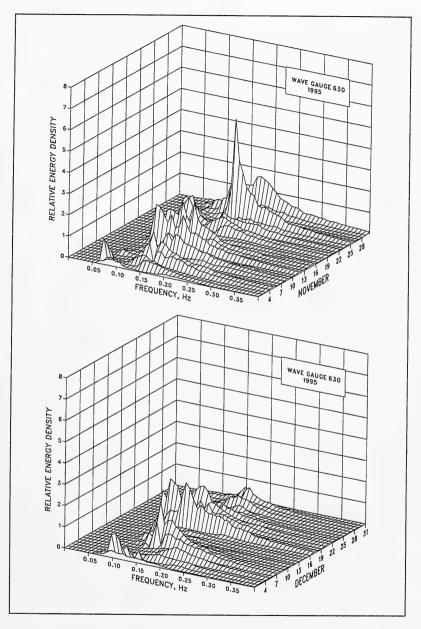


Figure B8. (Sheet 6 of 6)

Table B7 Wave statistics for Gauge 630

	1995								1980-1995							
	Height				Per	iod			He	light	Per					
		Std.				Std.			Std.				Std.			
	Mean	Dev.	Extreme		Mean	Dev.	Number	Mean	Dev.	Extreme	2	Mean	Dev.	Number		
Month	<u></u>		m	Date	sec	sec	Obs.	<u></u>	<u>m</u>	m	Date	sec	sec	Obs.		
Jan	1.2	0.6	3.1	15	8.3	3.0	123	1.2	0.7	4.5	1983	8.1	2.7	1619		
Feb	1.0	0.5	2.0	18	7.8	2.7	112	1.2	0.7	5.1	1987	8.4	2.5	1464		
Mar	1.2	0.6	2.8	2	8.7	2.3	120	1.2	0.7	4.7	1983	8.6	2.6	1811		
Apr	0.9	0.4	2.0	10	7.9	3.2	120	1.0	0.6	5.0	1988	8.6	2.7	1790		
May	0.8	0.4	1.9	з	8.8	2.8	124	0.9	0.5	3.6	1994	8.2	2.5	1837		
Jun	0.9	0.4	1.8	28	7.3	2.0	120	0.8	0.4	2.7	1991	7.9	2.2	1717		
Jul	0.7	0.2	1.1	9	8.6	2.5	123	0.7	0.3	2.1	1985	8.1	2.4	1752		
Aug	1.5	0.9	4.2	16	10.0	2.8	113	0.8	0.5	4.2	1995	8.3	2.5	1768		
Sep	1.3	0.4	2.4	9	11.5	2.9	61	1.1	0.6	6.1	1985	8.7	2.7	1715		
Oct	1.0	0.3	2.0	21	8.4	2.5	114	1.2	0.7	5.4	1991	8.6	2.8	1843		
Nov	1.1	0.5	2.5	11	8.7	2.7	118	1.1	0.7	5.1	1994	8.1	2.7	1588		
Dec	1.0	0.5	2.4	7	6.5	1.9	124	1.2	0.8	5.6	1980	8.3	2.9	1599		
nnual	1.0	0.6	4.2	Aug	8.4	2.8	1372	1.0	0.6	6.1	Sep 198	5 8.3	2.6	20503		

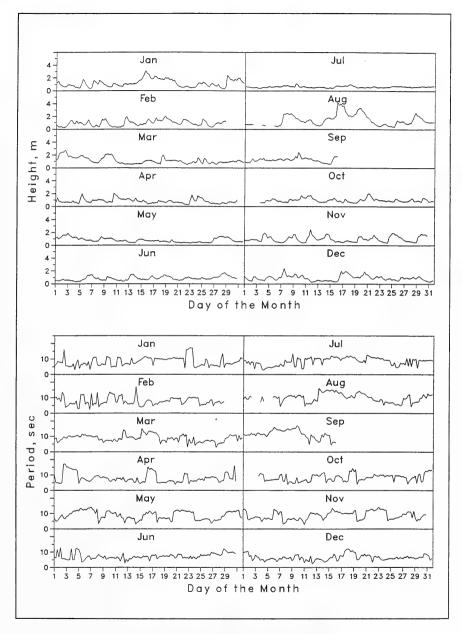


Figure B9. Time-histories of wave height and period for Gauge 630

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