



UNIVERSITY OF CALIFORNIA  
AT LOS ANGELES



EX LIBRIS

GIFT OF  
Mrs. E. H. Wood

Wm B. Hubbard,  
2400 Bancroft Way,  
Berkeley, Cal.

Jan. 20, 1912





ELEMENTS OF  
PLANE AND SPHERICAL  
TRIGONOMETRY



THE MACMILLAN COMPANY  
NEW YORK • BOSTON • CHICAGO  
ATLANTA • SAN FRANCISCO

MACMILLAN & CO., LIMITED  
LONDON • BOMBAY • CALCUTTA  
MELBOURNE

THE MACMILLAN CO. OF CANADA, LTD.  
TORONTO

ELEMENTS OF  
PLANE AND SPHERICAL  
TRIGONOMETRY

BY

DAVID A. ROTHROCK, PH.D.

PROFESSOR OF MATHEMATICS, INDIANA UNIVERSITY  
BLOOMINGTON, INDIANA

NEW YORK  
ALBION  
NEW YORK

New York  
THE MACMILLAN COMPANY

1911

*All rights reserved*

COPYRIGHT, 1910,  
By THE MACMILLAN COMPANY.

---

Set up and electrotyped. Published September, 1910. Reprinted  
January, 1911.

AMERICAN TO VARI  
ZELONA ZOLTA  
YRARI

**Norwood Press**  
J. S. Cushing Co. — Berwick & Smith Co.  
Norwood, Mass., U.S.A.

QA

531

RTHe

## PREFACE

IN this work the author has endeavored to prepare a text which would serve as a basis for a fifty- or sixty-hour course in Plane and Spherical Trigonometry as ordinarily presented in advanced secondary and elementary college courses.


Emphasis is placed upon drill work in the trigonometric identities, upon the applications of trigonometry to practical problems, and upon approximate calculations by means of natural functions. The more accurate results obtained by logarithmic calculations are emphasized in the solutions of oblique triangles; a uniform style of tabulating logarithmic calculations is suggested.

For the benefit of those who may wish to pursue advanced courses in mathematics, a brief discussion of analytic trigonometry is presented in Chapter IX. In Part II the elements of spherical trigonometry are developed in so far as to include the ordinary formulæ necessary in the solution of right and oblique spherical triangles.

DAVID A. ROTHROCK.

BLOOMINGTON, INDIANA,  
December, 1909.

*Gift of Mrs. M.H. Wood*



Digitized by the Internet Archive  
in 2007 with funding from  
Microsoft Corporation

# CONTENTS

## PART I

### PLANE TRIGONOMETRY

#### CHAPTER I

##### Trigonometric Functions of Acute Angles

ART.		PAGE
1.	Trigonometry . . . . .	1
2.	Functions of Acute Angles . . . . .	2
3.	Functions of Complementary Angles . . . . .	3
	Exercises . . . . .	5
4.	Fundamental Relations among the Trigonometric Functions . . . . .	6
5.	Fundamental Identities . . . . .	7
6.	Variation of the Trigonometric Functions . . . . .	7
7.	Transformation of Identities . . . . .	7
	Exercises . . . . .	8
	Exercises . . . . .	10
8.	Functions of Particular Angles: $0^\circ$ , $30^\circ$ , $45^\circ$ , $60^\circ$ , $90^\circ$ . . . . .	13
	Exercises . . . . .	14
9.	Table of Trigonometric Functions . . . . .	15

#### CHAPTER II

##### Solution of Right Triangles

10.	Fundamental Formulas . . . . .	16
11.	Projections . . . . .	17
12.	Components . . . . .	18
13.	Resultant . . . . .	18
14.	Projected Areas . . . . .	21
15.	Areas of Right Triangles . . . . .	21
16.	The Isosceles Triangle . . . . .	22
17.	Notations of Direction . . . . .	23
18.	To solve Right Triangles . . . . .	25
	Exercises . . . . .	26

#### CHAPTER III

##### Trigonometric Functions of Any Angle

19.	Axes. Quadrants . . . . .	31
20.	Coördinates, Abscissa, Ordinate . . . . .	31
21.	Definitions of the Functions . . . . .	32

ART.	PAGE
22. Laws of Signs . . . . .	33
Exercises . . . . .	34
23. Functions of Negative Angles . . . . .	34
Exercises . . . . .	35
24. Functions of $90^\circ - \theta$ and $90^\circ + \theta$ . . . . .	36
25. Functions of $180^\circ - \theta$ and $180^\circ + \theta$ . . . . .	37
Exercises . . . . .	38
26. Line Values of the Functions . . . . .	39
Exercises . . . . .	41
27. Graphs of the Trigonometric Functions . . . . .	42

## CHAPTER IV

## Measurement of Angles

28. Units of Measure . . . . .	44
29. Relations between Degree and Radian Measure . . . . .	44
Exercises . . . . .	45
30. The Length of any Arc . . . . .	46
31. Segment and Sector Areas . . . . .	47
Exercises . . . . .	47

## CHAPTER V

## Functions of Two Angles. Multiple Angles

32. To develop $\sin(\alpha + \beta)$ and $\cos(\alpha + \beta)$ . . . . .	50
33. To develop $\tan(\alpha + \beta)$ . . . . .	51
34. Important Formulas . . . . .	52
Exercises . . . . .	52

## Functions of Multiple and Sub-Multiple Angles

35. Functions of $2\alpha$ . . . . .	53
36. Functions of $3\alpha$ . . . . .	54
37. Half-angle Formulas . . . . .	54
Exercises . . . . .	55

## Sum and Difference Formulas

38. Converting to Products . . . . .	56
39. Converting to Sum or Difference . . . . .	57
Exercises . . . . .	57

## CHAPTER VI

## Logarithms

40. The Index Laws . . . . .	60
41. Definition of Logarithms . . . . .	61



## CONTENTS

ix

ART.	PAGE
42. Systems of Logarithms . . . . .	62
43. Laws governing the Use of Logarithms . . . . .	62
44. Characteristic and Mantissa . . . . .	63
45. Use of Tables . . . . .	65
46. Conversion of Common to Napierian Logarithms . . . . .	67
Exercises in Use of Logarithms . . . . .	67

### CHAPTER VII

#### Solution of Triangles in General

47. The Theorem of Sines . . . . .	69
Applications of the Theorem of Sines . . . . .	71
48. The Theorem of Tangents . . . . .	73
Applications of the Theorem of Tangents . . . . .	74
49. The Theorem of Cosines . . . . .	75
Exercises . . . . .	77
50. The Half-angle Theorems . . . . .	77
Application of the Half-angle Theorems . . . . .	79

#### Areas of Triangles

51. Area in Terms of Sides and Angles . . . . .	80
52. Area in Terms of $r$ . . . . .	81
53. Expressions for Area . . . . .	82
Exercises . . . . .	82

### CHAPTER VIII

#### Inverse Functions. Trigonometric Equations

54. Inverse Notation . . . . .	87
55. Inverse Identities . . . . .	88
Exercises . . . . .	89
56. Definitions . . . . .	90
57. Solutions . . . . .	91
58. Simple Equations . . . . .	91
Exercises . . . . .	92
59. Equations of the Form $r \cos \phi = a$ , $r \sin \phi = b$ . . . . .	93
60. Equations of the Form $r \sin \theta \cos \phi = a$ , $r \sin \theta \sin \phi = b$ , $r \cos \theta = c$ . . . . .	94
61. To solve $a \cdot \sin x + b \cdot \cos x = c$ . . . . .	95
62. To solve $\sin(x + \phi) = a \sin x$ . . . . .	95
63. To solve $\tan(x + \phi) = a \tan x$ . . . . .	96
64. To solve $x = \alpha + \beta \sin x$ . . . . .	97

### CHAPTER IX

#### Complex Numbers. DeMoivre's Theorem. Trigonometric Series.

#### Exponential and Hyperbolic Functions

65. Roots of Quadratic Equations . . . . .	99
Exercises . . . . .	100

ART.	PAGE
66. Complex Numbers expressed Trigonometrically . . . . .	100
67. DeMoivre's Theorem . . . . .	101
68. Raising to Powers and extracting Roots . . . . .	102
69. Value of $\sin x$ , $\cos x$ in Terms of $x$ . . . . .	104
70. Summation of Series . . . . .	108
Examples . . . . .	109
71. The Exponential Series . . . . .	110
72. Euler's Formulas . . . . .	111
Exercises . . . . .	112
73. The Hyperbolic Functions . . . . .	112
74. The Gudermannian . . . . .	116

## PART II

## SPHERICAL TRIGONOMETRY

## CHAPTER X

## General Definitions. The Right Triangle

75. Definitions and Geometric Properties . . . . .	117
76. The Polar Triangle . . . . .	118

## The Right Spherical Triangle

77. Definitions . . . . .	119
78. Trigonometric Relations . . . . .	119
79. Important Formulas . . . . .	120
80. Napier's Rules of Circular Parts . . . . .	121
81. Relative Dimensions of Sides and Angles . . . . .	122
82. The Isosceles and Quadrantal Triangles . . . . .	122
83. Solution of Right Spherical Triangles . . . . .	123
Exercises . . . . .	124

## CHAPTER XI

## The Oblique Spherical Triangle

84. The Theorem of Sines . . . . .	126
85. The Theorem of Cosines. Side and One Angle . . . . .	127
Modified Formula . . . . .	128
86. The Theorem of Cosines. Angles and One Side . . . . .	128
87. The Half-angle Formulæ . . . . .	129
1) The Half-angles in Terms of the Sides . . . . .	129
2) The Half-sides in Terms of the Angles . . . . .	130
88. Napier's Analogies . . . . .	131
89. The Area of a Spherical Triangle . . . . .	133
90. Solution of Oblique Spherical Triangles . . . . .	133
Exercises . . . . .	135

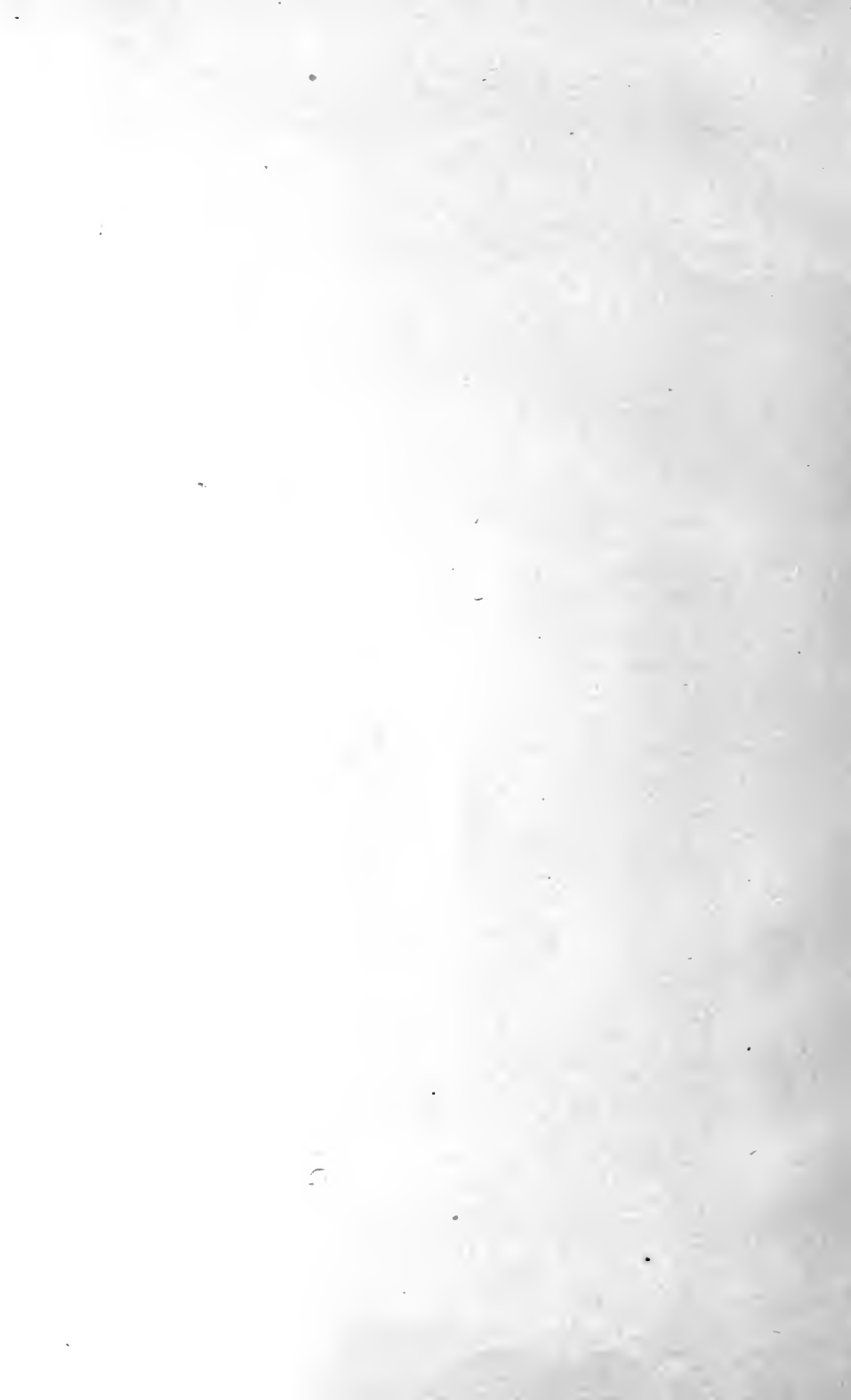
CONTENTS

**Applications of Spherical Trigonometry**

ART.		PAGE
91.	The Earth as a Sphere. Definitions and Notation . . . . .	137
92.	The Terrestrial Triangle . . . . .	138
93.	The Celestial Sphere . . . . .	140
94.	The Celestial Triangle . . . . .	141
	Exercises . . . . .	142

CHAPTER XII

FORMULAS . . . . .	143
--------------------	-----



# TRIGONOMETRY

## PART I

### PLANE TRIGONOMETRY

#### CHAPTER I

##### TRIGONOMETRIC FUNCTIONS OF ACUTE ANGLES

1. **Trigonometry.** The word *Trigonometry* is derived from two Greek words, *triangle* (*τρίγωνον*) and *measurement* (*μέτρον*), which would suggest that the subject has to do with the measurement of the triangle. At the present time the subject of trigonometry, though treating of the measurement of the triangle, has a much wider scope, and includes all manner of investigations depending upon certain functions of angles called **Trigonometric Functions**. These functions are called *sine*, *cosine*, *tangent*, *cotangent*, *secant*, and *cosecant*. For any angle  $\theta$ \* these words are abbreviated into  $\sin \theta$ ,  $\cos \theta$ ,  $\tan \theta$ ,  $\cot \theta$ ,  $\sec \theta$ ,  $\csc \theta$ , respectively. In the next section definitions are given for the trigonometric functions of an acute angle, but it should be borne in mind that similar definitions are applicable for any angle whatever, and later will be extended to angles varying from  $0^\circ$  to  $360^\circ$ .

\* In trigonometric notation, angles are frequently denoted by Greek letters. The Greek alphabet is here inserted.

Letters	Names	Letters	Names	Letters	Names
A $\alpha$	Alpha	I $\iota$	Iota	P $\rho$	Rho
B $\beta$	Beta	K $\kappa$	Kappa	$\Sigma$ $\sigma$ $\varsigma$	Sigma
$\Gamma$ $\gamma$	Gamma	$\Lambda$ $\lambda$	Lambda	T $\tau$	Tau
$\Delta$ $\delta$	Delta	M $\mu$	Mu	$\Upsilon$ $\upsilon$	Upsilon
E $\epsilon$	Epsilon	N $\nu$	Nu	$\Phi$ $\phi$	Phi
Z $\zeta$	Zeta	$\Xi$ $\xi$	Xi	X $\chi$	Chi
H $\eta$	Eta	O $\omicron$	Omicron	$\Psi$ $\psi$	Psi
$\Theta$ $\theta$	Theta	$\Pi$ $\pi$ $\varpi$	Pi	$\Omega$ $\omega$	Omega

## 2. The Trigonometric Functions of an Acute Angle.

(1) *Definitions.* For an acute angle  $\theta$  constructed in a right triangle, Fig. 1, with  $x$ ,  $y$ ,  $r$ , as the base, altitude, and hypotenuse, respectively, we define

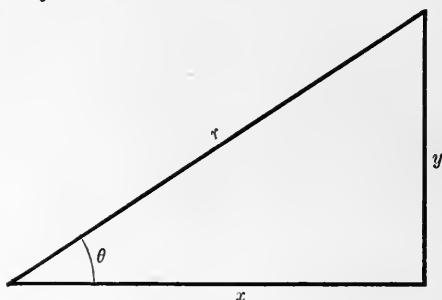


Fig. 1.

$$\sin \theta = \frac{\text{opposite side}}{\text{hypotenuse}} = \frac{y}{r}, \quad \csc \theta = \frac{\text{hypotenuse}}{\text{opposite side}} = \frac{1}{\sin \theta} = \frac{r}{y},$$

$$\cos \theta = \frac{\text{adjacent side}}{\text{hypotenuse}} = \frac{x}{r}, \quad \sec \theta = \frac{\text{hypotenuse}}{\text{adjacent side}} = \frac{1}{\cos \theta} = \frac{r}{x},$$

$$\tan \theta = \frac{\text{opposite side}}{\text{adjacent side}} = \frac{y}{x}, \quad \cot \theta = \frac{\text{adjacent side}}{\text{opposite side}} = \frac{1}{\tan \theta} = \frac{x}{y}.$$

To these six functions are sometimes added :

$$\text{versed sine } \theta = 1 - \cos \theta, \text{ written vers } \theta,$$

$$\text{coversed sine } \theta = 1 - \sin \theta, \text{ written covers } \theta.$$

These six functions of the angle  $\theta$  are called trigonometric functions (trigonometric ratios) of that angle. The symbols  $\sin \theta$ ,  $\cos \theta$ ,  $\tan \theta$ ,  $\cot \theta$ ,  $\sec \theta$ ,  $\csc \theta$ , are usually read *sine*  $\theta$ , *cosine*  $\theta$ , *tangent*  $\theta$ , *cotangent*  $\theta$ , *secant*  $\theta$ , *cosecant*  $\theta$ , respectively.

(2) *Elementary relations among the functions.* The six functions  $\sin \theta$ ,  $\cos \theta$ ,  $\tan \theta$ ,  $\cot \theta$ ,  $\sec \theta$ ,  $\csc \theta$ , are not independent. By comparing the definitions we find :

$$(1) \quad \tan \theta = \frac{1}{\cot \theta}, \text{ or } \tan \theta \cdot \cot \theta = 1,$$

$$(2) \quad \cos \theta = \frac{1}{\sec \theta}, \text{ or } \cos \theta \cdot \sec \theta = 1,$$

$$(3) \quad \sin \theta = \frac{1}{\csc \theta}, \text{ or } \sin \theta \cdot \csc \theta = 1.$$

(3) *Exponents.* When the trigonometric functions are to be affected by exponents, the following notation is usually employed: (1) if the exponent be positive, the index is placed thus,  $\sin^2\theta$ ,  $\tan^3\theta$ ,  $\sec^n\theta$ , and read *sine square*  $\theta$ , etc.; (2) if the exponent be negative, the index is usually attached to a bracket as in bracketed expressions in algebra, thus  $(\sin \theta)^{-1} = \frac{1}{\sin \theta}$ ,  $(\cot \theta)^{-2} = \frac{1}{\cot^2 \theta}$ ,  $(\cos \theta)^{-n} = \frac{1}{\cos^n \theta}$ . These are read *sin*  $\theta$  *exponent minus one*, *cot*  $\theta$  *exponent minus two*, *cos*  $\theta$  *exponent minus n*.

(4) *Functions are constant for any given angle.* The trigonometric functions of an acute angle are ratios of lines in a right triangle. They are constant for any fixed angle, and do not change value for different lengths of the sides of the triangle. Thus, Fig. 2,

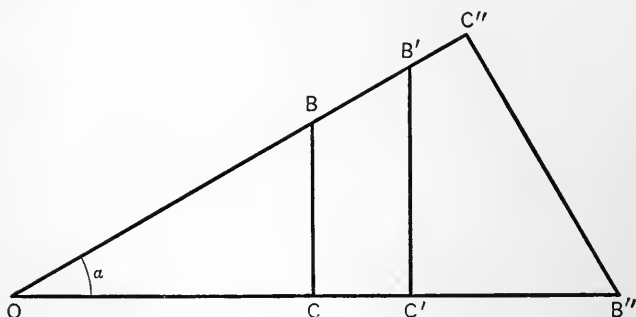


Fig. 2.

$$\sin \alpha = \frac{BC}{OB} = \frac{B'C'}{OB'} = \frac{B''C''}{OB''},$$

$$\cos \alpha = \frac{OC}{OB} = \frac{OC'}{OB'} = \frac{OC''}{OB''},$$

$$\tan \alpha = \frac{BC}{OC} = \frac{B'C'}{OC'} = \frac{B''C''}{OC''}.$$

Tables of these ratios have been constructed, showing their numerical values for all angles from  $0^\circ$  to  $90^\circ$  (see Table p. 15).

**3. Functions of Complementary Angles.** In Fig. 3,  $\theta$  and  $\phi$  are complementary angles:  $\theta + \phi = 90^\circ$ .

$$\sin \theta = \frac{y}{r} = \cos \phi,$$

$$\csc \theta = \frac{r}{y} = \sec \phi,$$

$$\cos \theta = \frac{x}{r} = \sin \phi,$$

$$\sec \theta = \frac{r}{x} = \csc \phi,$$

$$\tan \theta = \frac{y}{x} = \cot \phi,$$

$$\cot \theta = \frac{x}{y} = \tan \phi.$$

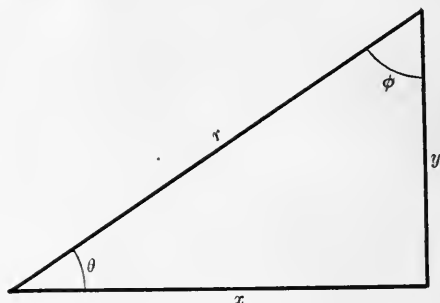


Fig. 3.

The cosine, cotangent, and cosecant of an angle are co-functions of the sine, tangent, and secant, respectively.

From the definitions we see that *any function of an angle equals the co-function of the complement of that angle.*

For example,  $\sin 30^\circ = \cos 60^\circ$ ,  $\tan 35^\circ = \cot 55^\circ$ ,  $\csc 32^\circ = \sec 58^\circ$ ,

$$\sin (90^\circ - A) = \cos A,$$

$$\csc (90^\circ - A) = \sec A,$$

$$\cos (90^\circ - A) = \sin A,$$

$$\sec (90^\circ - A) = \csc A,$$

$$\tan (90^\circ - A) = \cot A,$$

$$\cot (90^\circ - A) = \tan A.$$

EXAMPLES. Fill the blanks in the following with the proper co-function :

1.  $\sin 48^\circ =$

7.  $\cos (99^\circ - x) =$

2.  $\sin 84^\circ =$

8.  $\tan (90^\circ - 10^\circ) =$

3.  $\tan 25^\circ 48' =$

9.  $\sin (90^\circ - 100^\circ) =$

4.  $\cot 87^\circ 50' =$

10.  $\cot (80^\circ - x) =$

5.  $\cos 41^\circ 50' =$

11.  $\csc 67^\circ 10' =$

6.  $\sec 10^\circ 15' =$

12.  $\tan (90^\circ - x + y) =$



EXERCISES

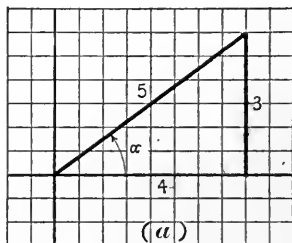
1. Construct an acute angle  $\alpha$  such that  $\sin \alpha = \frac{3}{5}$ , and write the remaining trigonometric functions.

*Solution.*  $\sin \alpha = \frac{3}{5}$  tells us that the side of the triangle opposite  $\alpha$  is 3, and the hypotenuse is 5; hence, the construction is as shown. Writing the functions of  $\alpha$  from the drawing, we have

$$\sin \alpha = \frac{3}{5}, \quad \cos \alpha = \frac{4}{5},$$

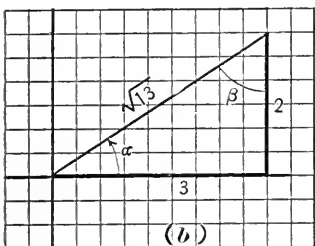
$$\tan \alpha = \frac{3}{4}, \quad \cot \alpha = \frac{4}{3},$$

$$\sec \alpha = \frac{5}{4}, \quad \csc \alpha = \frac{5}{3}.$$



2. Construct  $\alpha$  when  $\tan \alpha = \frac{2}{3}$ , and write the other functions of  $\alpha$ . Write the functions of  $90^\circ - \alpha$ .

*Solution.*  $\alpha$  is constructed as shown in figure.



$$\sin \alpha = \frac{2}{\sqrt{13}}, \quad \cos \alpha = \frac{3}{\sqrt{13}},$$

$$\tan \alpha = \frac{2}{3}, \quad \cot \alpha = \frac{3}{2},$$

$$\sec \alpha = \frac{\sqrt{13}}{3}, \quad \csc \alpha = \frac{\sqrt{13}}{2},$$

$$90^\circ - \alpha = \beta; \quad \sin \beta = \cos \alpha = \frac{3}{\sqrt{13}}, \text{ etc.}$$

Construct the angle  $\alpha$  in the following cases and write the remaining functions:

3.  $\sin \alpha = \frac{5}{13}$ .

5.  $\cot \alpha = \frac{5}{3}$ .

7.  $\tan \alpha = \frac{4}{5}$ .

4.  $\cos \alpha = \frac{3}{5}$ .

6.  $\sec \alpha = \frac{7}{5}$ .

8.  $\cot \alpha = \frac{8}{15}$ .

9.  $\sin \alpha = \frac{1}{2}$ .

16.  $\sec \alpha = 4$ .

10.  $\tan \alpha = \frac{3}{4}$ .

17.  $\sin \alpha = 0.6$ .

11.  $\sin \alpha = \frac{8}{17}$ .

18.  $\cos \alpha = \frac{2m}{1+m^2}$ .

12.  $\tan \alpha = 2$ .

19.  $\tan \alpha = \frac{\sqrt{1-m^2}}{m}$ .

14.  $\sin \alpha = \frac{1}{2}\sqrt{3}$ .

20.  $\cot \alpha = \frac{3x}{4}$ .

15.  $\tan \alpha = \frac{1}{3}\sqrt{3}$ .

In the right triangle  $ABC$ , Fig. 4, if

21.  $\sin A = \frac{2}{3}$ ,  $c = 24$ , find  $a$ .
22.  $\sin A = \frac{3}{5}$ ,  $c = 24$ , find  $a$ .
23.  $\tan A = \frac{3}{4}$ ,  $b = 16$ , find  $a$ .
24.  $\tan A = \frac{4}{3}$ ,  $c = 15$ , find  $b$ .
25.  $\tan A = 0.6$ ,  $a = 10$ , find  $b$ .
26.  $\sin A = \frac{5}{8}$ ,  $a = 15$ , find  $c$ .
27.  $\cos A = \frac{2}{3}$ ,  $c = 21$ , find  $b$  and  $a$ .
28.  $\sec A = 5$ ,  $b = 50$ , find  $c$  and  $a$ .
29.  $\tan A = 0.25$ ,  $b = 40$ , find the area.
30.  $\csc A = 2.5$ ,  $a = 100$ , find  $c$  and the area.

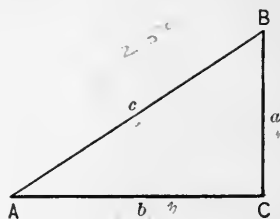


Fig. 4.

#### 4. Fundamental Relations among the Trigonometric Functions.

Let  $\theta$  denote any acute angle, Fig. 5. From plane geometry,

$$x^2 + y^2 = r^2. \quad (1)$$

Defining  $\sin \theta$  and  $\cos \theta$ ,

$$\sin \theta = \frac{y}{r}, \quad \cos \theta = \frac{x}{r},$$

we have, on squaring and adding,

$$\sin^2 \theta + \cos^2 \theta = \frac{y^2 + x^2}{r^2} = 1. \quad (A)$$

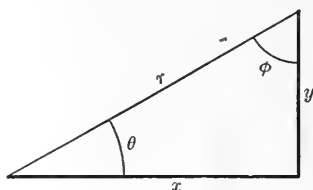


Fig. 5.

From the same figure,  $\sec \theta = \frac{r}{x}$ ,  $\tan \theta = \frac{y}{x}$ .

Squaring and subtracting,

$$\sec^2 \theta - \tan^2 \theta = \frac{r^2 - y^2}{x^2} = 1, \text{ from (1)}. \quad (B)$$

Combining  $\csc \theta$  and  $\cot \theta$  in a similar manner,

$$\csc^2 \theta - \cot^2 \theta = \frac{r^2 - x^2}{y^2} = 1. \quad (C)$$

Also, 
$$\tan \theta = \frac{y}{x} = \frac{y \div r}{x \div r} = \frac{\sin \theta}{\cos \theta}, \quad (D)$$

$$\cot \theta = \frac{x}{y} = \frac{\cos \theta}{\sin \theta}, \quad (E)$$

$$\sec \theta = \frac{r}{x} = \frac{1}{\cos \theta}, \quad (F) \qquad \csc \theta = \frac{r}{y} = \frac{1}{\sin \theta}. \quad (G)$$

As fundamental relations among the six functions, we may enumerate formulas *A*, *B*, *C*, above, and the identities coming directly from the definitions in § 2.

**5. Fundamental Identities.** Collecting important results, we have, for any angle  $\alpha$ :

$$(A) \sin^2 \alpha + \cos^2 \alpha = 1,$$

$$(B) \sec^2 \alpha - \tan^2 \alpha = 1,$$

$$(C) \csc^2 \alpha - \cot^2 \alpha = 1,$$

$$(D) \tan \alpha = \frac{\sin \alpha}{\cos \alpha},$$

$$(E) \cot \alpha = \frac{1}{\tan \alpha} = \frac{\cos \alpha}{\sin \alpha},$$

$$(F) \sec \alpha = \frac{1}{\cos \alpha},$$

$$(G) \csc \alpha = \frac{1}{\sin \alpha}.$$

These identities should be memorized.

**6. Variation of the Trigonometric Functions.** It should be noticed that as the angle increases from  $0^\circ$  to  $90^\circ$ , the functions vary as follows:

- (1) *sine increases from 0 to 1,*
- (2) *cosine decreases from 1 to 0,*
- (3) *tangent increases from 0 to  $\infty$ ,*
- (4) *cotangent decreases from  $\infty$  to 0,*
- (5) *secant increases from 1 to  $\infty$ ,*
- (6) *cosecant decreases from  $\infty$  to 1.*

These facts may be observed from the above identities, as well as from the definitions of the functions in § 2.

**7. Transformation of Identities.** By means of the fundamental identities, § 5, any trigonometric function may be changed into various forms.

For example,

$$\sin \phi = \sqrt{1 - \cos^2 \phi} = \sqrt{1 - \frac{1}{\sec^2 \phi}} = \frac{\sqrt{\sec^2 \phi - 1}}{\sec \phi} = \frac{\tan \phi}{\sec \phi}, \text{ etc.}$$

These forms for the value of the sine of an angle are obtained by using identities (*A*), (*F*), (*B*), and algebraic manipulation.

Again,

$$\sin \alpha \cdot \sec \alpha \cdot \cot \alpha = \frac{\sin \alpha}{\cos \alpha} \cdot \cot \alpha = \tan \alpha \cdot \cot \alpha = 1.$$

In verifying an identity, we may proceed, (a) by transforming the left member of the equation into the right, (b) by transforming the right into the left, or (c) by reducing each side to the same form.

For example, show  $\cos^4 x - \sin^4 x = 2 \cos^2 x - 1$ .

(a) Transform the left member into the right.

$$\begin{aligned} \cos^4 x - \sin^4 x &= (\cos^2 x + \sin^2 x)(\cos^2 x - \sin^2 x) \\ &= \cos^2 x - \sin^2 x && \text{by (A)} \\ &= \cos^2 x - (1 - \cos^2 x) && \text{by (A)} \\ &= 2 \cos^2 x - 1. \end{aligned}$$

(b) Transform the right member to the form of the left.

$$\begin{aligned} 2 \cos^2 x - 1 &= \cos^2 x - (1 - \cos^2 x) \\ &= \cos^2 x - \sin^2 x && \text{by (A)} \\ &= (\cos^2 x - \sin^2 x)(\cos^2 x + \sin^2 x), \text{ multiplying by 1,} \\ &= \cos^4 x - \sin^4 x. \end{aligned}$$

(c) Transform each side to a common form.

$$\begin{aligned} \cos^4 x - \sin^4 x &= 2 \cos^2 x - 1 \\ &= \cos^2 x - \sin^2 x. \end{aligned}$$

Remove the factor  $\cos^2 x + \sin^2 x = 1$  from the left member, and we have

$$\cos^2 x - \sin^2 x = \cos^2 x - \sin^2 x.$$

The student should attain a good degree of skill in manipulating trigonometric functions; to this end is now inserted a list of the more common forms of identities involving a single angle.

### EXERCISES

Verify the following identities:

- $\cos^2 A (1 + \tan^2 A) = 1$ .
- $(\sec^2 A - 1)(\csc^2 A - 1) = 1$ .
- $\tan A + \cot A = \sec A \times \csc A$ .
- $\sin^2 A (\csc^2 A - 1) = \cos^2 A$ .
- $\cot^2 A - \cos^2 A = \cos^2 A \cot^2 A$ .
- $\frac{\cos A}{\sin A \cot^2 A} = \tan A$ .
- $\sin A \cos A (\tan A + \cot A) = 1$ .

8.  $(\tan A + \cot A)^2 = \sec^2 A + \csc^2 A.$
9.  $\cos A \csc A \tan A = 1.$
10.  $\cos A (\cot A + \tan A) = \csc A.$
11.  $\cot A + \frac{\sin A}{1 + \cos A} = \csc A.$
12.  $\frac{\sec A}{\cos A} - \frac{\tan A}{\cot A} = 1.$
13.  $\sec^2 A - \sec^2 A \sin^2 A = 1.$
14.  $(\csc A - \cot A)^2 = \frac{1 - \cos A}{1 + \cos A}.$
15.  $\sec A - \cos A = \sin A \tan A.$
16.  $\frac{\sin A}{\csc A} + \frac{\cos A}{\sec A} = 1.$
17.  $\frac{\tan A - 1}{\tan A + 1} = \frac{1 - \cot A}{1 + \cot A}.$
18.  $\frac{\sec A - \csc A}{\sec A + \csc A} = \frac{\tan A - 1}{\tan A + 1}.$
19.  $\cos^4 A - \sin^4 A = \cos^2 A - \sin^2 A = 1 - 2 \sin^2 A = 2 \cos^2 A - 1.$
20.  $\frac{1 + \cot^2 A}{1 + \tan^2 A} = \cot^2 A.$
21.  $(\sin A + \cos A)^2 + (\sin A - \cos A)^2 = 2.$
22.  $\sec A + \tan A = (\sec A - \tan A)^{-1}.$
23.  $\sin^4 A + \cos^4 A = 1 - 2 \sin^2 A \cos^2 A.$
24.  $\sin^3 A + \cos^3 A = (\sin A + \cos A)(1 - \sin A \cos A).$
25.  $\sec^4 A - \tan^4 A = \sec^2 A + \tan^2 A = 1 + 2 \tan^2 A.$
- 26.\* Show  $x^2 + y^2 = r^2$ , when  $x = r \cdot \cos \phi$ ,  $y = r \cdot \sin \phi$ .
27. Show  $\frac{x^2}{a^2} + \frac{y^2}{b^2} = 1$ , when  $x = a \cdot \cos \phi$ ,  $y = b \cdot \sin \phi$ .
28. Show  $\frac{x^2}{a^2} - \frac{y^2}{b^2} = 1$ , when  $x = a \cdot \sec \phi$ ,  $y = b \cdot \tan \phi$ .
29. Show  $x^2 + y^2 + z^2 = r^2$ , when  $x = r \cdot \sin \theta \cdot \cos \phi$ ,  
 $y = r \cdot \sin \theta \cdot \sin \phi$ ,  $z = r \cdot \cos \theta$ .

\* The algebraic equations in Exercises 26-29 are, respectively, the equations of a circle, ellipse, hyperbola, and sphere. The equations giving the values of  $x, y, z$  are the parametric equations of the same curves and sphere, respectively.

30. Show  $x^2 + y^2 + z^2 = r^2$ ,

$$\text{when } x = r(\cos \theta \cdot \cos \phi + \sin \theta \cdot \sin \phi \cdot \cos \psi),$$

$$y = r(\cos \theta \cdot \sin \phi \cdot \cos \psi - \sin \theta \cdot \cos \phi),$$

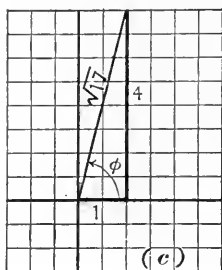
$$z = r \cdot \sin \phi \cdot \sin \psi.$$

31. Show  $x^{\frac{2}{3}} + y^{\frac{2}{3}} = a^{\frac{2}{3}}$ , when  $x = a \cdot \cos^3 \phi$ ,  $y = a \cdot \sin^3 \phi$ .

### EXERCISES

Simplify the following expressions, construct the angle  $\phi$  in each case, and read the values of the remaining functions.

NOTE. When square roots are to be taken, use only the + sign.



1.  $\sin \phi \cdot \sec \phi + 1 = 5$ .

In this exercise, we have

$$\sin \phi \cdot \sec \phi = 4,$$

or,

$$\frac{\sin \phi}{\cos \phi} = \tan \phi = 4.$$

Hence,

$$\sin \phi = \frac{4}{\sqrt{17}}, \quad \cos \phi = \frac{1}{\sqrt{17}},$$

$$\tan \phi = 4, \quad \cot \phi = \frac{1}{4}, \quad \sec \phi = \sqrt{17}, \quad \csc \phi = \frac{\sqrt{17}}{4}.$$

In the following the values of a single function should be found, then the angle may be constructed.

2.  $\tan \phi = 2 - \sin \phi \cdot \sec \phi$ .

Ans.  $\tan \phi = 1$ .

3.  $\tan \phi \cdot \cos \phi = \frac{2}{3}$ .

Ans.  $\sin \phi = \frac{2}{3}$ .

4.  $\sec \phi \cdot \cot \phi = \frac{4}{3}$ .

Ans.  $\sin \phi = \frac{3}{4}$ .

5.  $\sec \phi = 4 \cos \phi$ .

Ans.  $\sec \phi = 2$ .

6.  $\cot \phi = 3 \tan \phi$ .

Ans.  $\tan \phi = \frac{\sqrt{3}}{3}$ .

7.  $\tan \phi = 4 \cot \phi$ .

Ans.  $\tan \phi = 2$ .

8.  $\cot \phi = \frac{4}{5} \csc \phi$ .

Ans.  $\cos \phi = \frac{4}{5}$ .

9.  $\cos \phi \div \sin \phi = \frac{4}{3}$ .

Ans.  $\cot \phi = \frac{4}{3}$ .

10.  $\cot \phi \cdot \cos \phi \cdot \tan \phi = \frac{a}{b}$ .

Ans.  $\cos \phi = \frac{a}{b}$ .

11.  $\sin^2 \phi \cdot \sec \phi \cdot \cos \phi \cdot \csc \phi = \frac{5}{13}$ .

Ans.  $\sin \phi = \frac{5}{13}$ .

12.  $1 - \cos^2 \phi = \frac{4}{9}$ .

Ans.  $\sin \phi = \frac{2}{3}$ .

13.  $\sec^2 \phi - 1 = \frac{25}{144}$ . *Ans.*  $\tan \phi = \frac{5}{12}$ .

14.  $2 - 3 \sin \phi = \frac{1}{2}$ . *Ans.*  $\sin \phi = \frac{1}{2}$ .

15.  $(1 + \sin \phi)(1 - \sin \phi) = \frac{9}{16}$ . *Ans.*  $\cos \phi = \frac{3}{4}$ .

16.  $\tan^2 \phi + 1 = 2 \sec \phi$ . *Ans.*  $\sec \phi = 2$ .

17.  $\tan \phi = 2 - 2 \sec \phi \div \csc \phi$ . *Ans.*  $\tan \phi = \frac{2}{3}$ .

18.  $\tan \phi - \cos^2 \phi = \sin^2 \phi + 5$ . *Ans.*  $\tan \phi = 6$ .

19.  $\sin \phi = \frac{4}{5} \cos \phi \cdot \sec \phi \cdot \csc \phi$ . *Ans.*  $\sin \phi = \frac{2}{5}$ .

20.  $\frac{5 \tan \phi \times \cos \phi \times \csc \phi}{4 \cot \phi \times \sec \phi} = 1$ . *Ans.*  $\sin \phi = \frac{4}{5}$ .

21. When  $\tan \alpha = 4$ , find value of  $\frac{\sin \alpha \cdot \sec \alpha}{\cos^2 \alpha}$ .

22. When  $\sin \alpha = \frac{5}{6}$ , find value of  $\frac{\cos^2 \alpha + \sin^2 \alpha}{\tan \alpha}$ .

23. When  $\cos \alpha = \frac{1}{2}$ , find value of  $\frac{\sin \alpha \cdot \tan \alpha}{\sec^2 \alpha + 1}$ .

24. When  $\sec \alpha = 5$ , find value of  $\frac{\tan^2 \alpha}{\cos \alpha \cdot \csc \alpha}$ .

25. When  $\cot \alpha = \frac{5}{8}$ , find value of  $\frac{\tan \alpha}{\csc^2 \alpha - 1}$ .  $(\frac{8}{5})^3$

26. If  $\sin \alpha = \frac{5}{13}$ , what value has  $\frac{\sin^2 \alpha + \cos^2 \alpha}{1 + \tan^2 \alpha}$ ?

27. If  $\tan \alpha = \frac{1}{3} \sqrt{3}$ , what value has  $3 \sin \alpha - 4 \sin^3 \alpha$ ?

28.  $\sin 30^\circ = \frac{1}{2}$ , find the value of  $4 \cos^3 30^\circ - 3 \cos 30^\circ$ .

29.  $\sec 45^\circ = \sqrt{2}$ , find the value of  $\frac{2 \tan 45^\circ}{1 - \tan^2 45^\circ}$ .

30.  $\sin 30^\circ = \frac{1}{2}$ ,  $\cos 45^\circ = \frac{1}{2} \sqrt{2}$ , find the value of  $\tan 45^\circ \times \cot 30^\circ \div (\sec 30^\circ \times \sin 45^\circ)$ .

Change the following functions so that only  $\sin \alpha$  appears :

31.  $\sin \alpha \cos^2 \alpha - \frac{\cot \alpha}{\cos \alpha \sin \alpha} + \frac{\tan \alpha}{\cos \alpha}$ .

32.  $\csc \alpha \sin \alpha + \cos \alpha \tan \alpha - \frac{\sin \alpha}{\cos^2 \alpha}$ .

33.  $\tan^3 \alpha + 1 - \csc^2 \alpha + 2 \sin \alpha \cos \alpha$ .

34.  $\sec^4 \alpha - \tan^2 \alpha + \cos^2 \alpha - \cot^2 \alpha$ .

Change the following so that only  $\tan \alpha$  appears:

35.  $\cot \alpha + \sec \alpha - \csc \alpha$ .

36.  $(1 + \cos \alpha)(1 - \cos \alpha) + \tan \alpha(\cot^2 \alpha - 1)$ .

37.  $\sin \alpha + \cos \alpha + \cos \alpha \tan \alpha + \cot \alpha \sin \alpha$ .

38.  $(1 - \sin \alpha \cos \alpha) \div (1 + \sin \alpha \cos \alpha) - \cot \alpha \sin \alpha$ .

Change the following so that only  $\cos \alpha$  appears:

39.  $\frac{\sin^2 \alpha}{\cos \alpha} + \frac{\tan \alpha}{\cot \alpha}$ .

40.  $\sec \alpha - \frac{1}{\cos \alpha} + \frac{\tan \alpha}{\sin \alpha}$ .

41.  $\cot^2 \alpha + \tan^2 \alpha - \sin^2 \alpha - \cos^2 \alpha$ .

42.  $\sin \alpha \cos \alpha \tan \alpha \cot \alpha$ .

43. Express  $\sin x$  in terms of each of the other functions.

Thus, (1)  $\sin x = \sqrt{1 - \cos^2 x}$ , from identity (A), § 5.

(2)  $\sin x = \tan x \div \sqrt{1 + \tan^2 x}$ , from (D), (F) and (B).

(3)  $\sin x = \frac{1}{\sqrt{1 + \cot^2 x}}$ ; from (G) and (C).

(4)  $\sin x = \sqrt{1 - \frac{1}{\sec^2 x}} = \sqrt{\frac{\sec^2 x - 1}{\sec x}}$ , from (A) and (F).

(5)  $\sin x = \frac{1}{\csc x}$ , from (G).

44. Express  $\cos x$  in terms of the other functions.

45. Express  $\tan x$  in terms of the other functions.

46. Express each function in terms of  $\sin x$ .

[NOTE. Construct the angle  $x$  with hypotenuse unity, the opposite side  $\sin x$ , and the base  $\sqrt{1 - \sin^2 x}$ .]

47. Express each function in terms of (1)  $\cos x$ , (2)  $\tan x$ , (3)  $\cot x$ .

48. Prove that  $\sec A(\sin A - \cos A) + \csc A(\sin A + \cos A) = \sec A \csc A$ .

49. Show  $\sin \alpha + \cos \alpha \geq 1$ ,  $0 \leq \alpha \leq 90^\circ$ .

50. Show  $\tan \alpha + \cot \alpha \geq 2$ .

51. Show  $\sin \alpha + \cos \alpha \leq \sqrt{2}$ . 52. Show  $\sin \alpha \cos \alpha \leq \frac{1}{2}$ .



**8. Functions of Particular Angles.** The trigonometric functions of certain angles may be found from geometrical drawings.

(1) *Functions of 45°.*

From the drawing, Fig. 6, we have

$$\sin 45^\circ = \frac{1}{2}\sqrt{2}, \quad \csc 45^\circ = \sqrt{2},$$

$$\cos 45^\circ = \frac{1}{2}\sqrt{2}, \quad \sec 45^\circ = \sqrt{2},$$

$$\tan 45^\circ = 1, \quad \cot 45^\circ = 1.$$

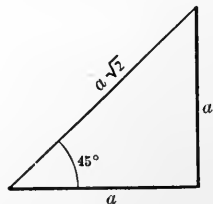


Fig. 6.

(2) *Functions of 30° and 60°.* From Fig. 7,

$$\sin 30^\circ = \frac{1}{2} = \cos 60^\circ,$$

$$\cos 30^\circ = \frac{\sqrt{3}}{2} = \sin 60^\circ,$$

$$\tan 30^\circ = \frac{\sqrt{3}}{3} = \cot 60^\circ,$$

$$\cot 30^\circ = \sqrt{3} = \tan 60^\circ,$$

$$\sec 30^\circ = \frac{2}{3}\sqrt{3} = \csc 60^\circ,$$

$$\csc 30^\circ = 2 = \sec 60^\circ.$$

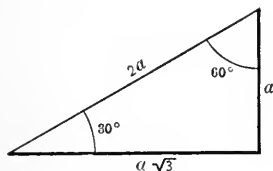


Fig. 7.

(3) *Functions of 0° and 90°.* The trigonometric functions of 0° and 90° are limiting values which may be seen from the drawing, Fig. 8.

As the side  $y$  approaches 0, the opposite angle approaches 0 and the base  $x$  approaches  $r$ .

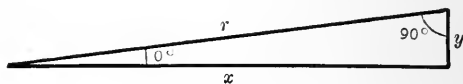


Fig. 8.

$$\sin 0^\circ = \lim_{y=0} \frac{y}{r} = 0 = \cos 90^\circ, \quad \cot 0^\circ = \lim_{y=0} \frac{x}{y} = \infty = \tan 90^\circ,$$

$$\cos 0^\circ = \lim_{x=r} \frac{x}{r} = 1 = \sin 90^\circ, \quad \sec 0^\circ = \lim_{x=r} \frac{r}{x} = 1 = \csc 90^\circ,$$

$$\tan 0^\circ = \lim_{y=0} \frac{y}{x} = 0 = \cot 90^\circ, \quad \csc 0^\circ = \lim_{y=0} \frac{r}{y} = \infty = \sec 90^\circ.$$

The angles  $0^\circ$ ,  $30^\circ$ ,  $45^\circ$ ,  $60^\circ$ ,  $90^\circ$ , occur so frequently that it will be found convenient to keep in mind the numerical values of the trigonometric functions of each.

Tabulate the values of these functions as shown in the following table:

$\theta =$	$0^\circ$	$30^\circ$	$45^\circ$	$60^\circ$	$90^\circ$
$\sin \theta$	0	.5	.707	.866	1
$\cos \theta$	1	.866	.707	.5	0
$\tan \theta$	0	.577	1	1.732	$\infty$
$\cot \theta$	$\infty$	1.732	1	.577	0
$\sec \theta$	1	1.155	1.414	2	$\infty$
$\csc \theta$	$\infty$	2	1.414	1.155	1

### EXERCISES

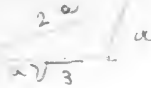
Find the values of the following by inserting numerical values of the trigonometric functions and reducing to simplest form.

- $5 \cos 60^\circ - 3 \sin 30^\circ + \tan 45^\circ$ . *Ans.* 2.
- $5 \cos 30^\circ + 4 \cos 60^\circ - 5 \sin 60^\circ$ . *Ans.* 2.
- $8 \tan 30^\circ - 4 \cot 45^\circ + \cos 90^\circ - 8 \cot 60^\circ$ . *Ans.* -4.
- $10 \cos 30^\circ + 16 \cos 60^\circ - 5\sqrt{3}$ . *Ans.* 8.
- $(4 \tan 45^\circ - 11 \tan 60^\circ)(4 \cot 45^\circ + 11 \cot 30^\circ)$ . *Ans.* -347.
- $(16 \tan 0^\circ + 10 \cot 90^\circ + 6 \sin 30^\circ) \cos 90^\circ$ . *Ans.* 0.
- $\sin 30^\circ \times \cos 0^\circ \times \tan 45^\circ \times \sec 60^\circ$ . *Ans.* 1.
- $(x + y) \cos 0^\circ - (x - y) \tan 45^\circ - 2y \sin 30^\circ$ . *Ans.*  $y$ .
- $(x + y)^2 \sin 60^\circ - (x - y)^2 \cos 30^\circ - 2xy \tan 60^\circ$ . *Ans.* 0.
- $(a + b) \sec 60^\circ + (a - b) \cos 90^\circ + a \tan 90^\circ$ . *Ans.*  $\infty$ .
- $a \sin 30^\circ - (a - b) \tan 45^\circ - b \sin 30^\circ$ . *Ans.*  $\frac{1}{2}(b - a)$ .
- $(a \sin 60^\circ - b \cos 30^\circ) \times \csc 60^\circ$ . *Ans.*  $a - b$ .

**9. Tables.** For convenience in the numerical calculations which follow on p. 26 a condensed table of trigonometric functions, true to three decimals, will now be inserted. By use of this table approximate results may be obtained for numerical problems.

NATURAL TRIGONOMETRIC FUNCTIONS

ANGLE	SIN	Csc	TAN	COT	Sec	Cos	
0°	0.000	∞	0.000	∞	1.000	1.000	90°
1	0.017	57.30	0.017	57.29	1.000	1.000	89
2	0.035	28.65	0.035	28.64	1.001	0.999	88
3	0.052	19.11	0.052	19.08	1.001	0.999	87
4	0.070	14.34	0.070	14.30	1.002	0.998	86
5°	0.087	11.47	0.087	11.43	1.004	0.996	85°
6	0.105	9.567	0.105	9.514	1.006	0.995	84
7	0.122	8.206	0.123	8.144	1.008	0.993	83
8	0.139	7.185	0.141	7.115	1.010	0.990	82
9	0.156	6.392	0.158	6.314	1.012	0.988	81
10°	0.174	5.759	0.176	5.671	1.015	0.985	80°
11	0.191	5.241	0.194	5.145	1.019	0.982	79
12	0.208	4.810	0.213	4.705	1.022	0.978	78
13	0.225	4.445	0.231	4.331	1.026	0.974	77
14	0.242	4.134	0.249	4.011	1.031	0.970	76
15°	0.259	3.864	0.268	3.732	1.035	0.966	75°
16	0.276	3.628	0.287	3.487	1.040	0.961	74
17	0.292	3.420	0.306	3.271	1.046	0.956	73
18	0.309	3.236	0.325	3.078	1.051	0.951	72
19	0.326	3.072	0.344	2.904	1.058	0.946	71
20°	0.342	2.924	0.364	2.747	1.064	0.940	70°
21	0.358	2.790	0.384	2.605	1.071	0.934	69
22	0.375	2.669	0.404	2.475	1.079	0.927	68
23	0.391	2.559	0.424	2.356	1.086	0.921	67
24	0.407	2.459	0.445	2.246	1.095	0.914	66
25°	0.423	2.366	0.466	2.145	1.103	0.906	65°
26	0.438	2.281	0.488	2.050	1.113	0.899	64
27	0.454	2.203	0.510	1.963	1.122	0.891	63
28	0.469	2.130	0.532	1.881	1.133	0.883	62
29	0.485	2.063	0.554	1.804	1.143	0.875	61
30°	0.500	2.000	0.577	1.732	1.155	0.866	60°
31	0.515	1.942	0.601	1.664	1.167	0.857	59
32	0.530	1.887	0.625	1.600	1.179	0.848	58
33	0.545	1.836	0.649	1.540	1.192	0.839	57
34	0.559	1.788	0.675	1.483	1.206	0.829	56
35°	0.574	1.743	0.700	1.428	1.221	0.819	55°
36	0.588	1.701	0.727	1.376	1.236	0.809	54
37	0.602	1.662	0.754	1.327	1.252	0.799	53
38	0.616	1.624	0.781	1.280	1.269	0.788	52
39	0.629	1.589	0.810	1.235	1.287	0.777	51
40°	0.643	1.556	0.839	1.192	1.305	0.766	50°
41	0.656	1.524	0.869	1.150	1.325	0.755	49
42	0.669	1.494	0.900	1.111	1.346	0.743	48
43	0.682	1.466	0.933	1.072	1.367	0.731	47
44	0.695	1.440	0.966	1.036	1.390	0.719	46
45°	0.707	1.414	1.000	1.000	1.414	0.707	45°
	Cos	SEC	COT	TAN	Csc	SIN	ANGLE



1.737

## CHAPTER II

### SOLUTION OF RIGHT TRIANGLES

A right triangle is known when a side and any other part are known. The use of trigonometric functions enables us to compute the unknown parts.

**10. Fundamental Formulas.** We have, Fig. 9, the following

relations :

$$(1) a^2 + b^2 = c^2,$$

$$(2) \sin A = \frac{a}{c} = \cos B,$$

$$(3) \cos A = \frac{b}{c} = \sin B,$$

$$(4) \tan A = \frac{a}{b} = \cot B,$$

$$(5) A + B = 90^\circ.$$

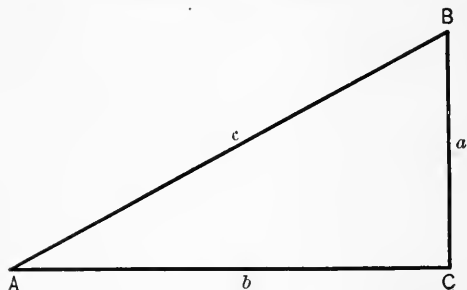


Fig. 9.

The first of these formulas is a statement of the Pythagorean Theorem ; (2), (3), (4) are results from the definition of sine, cosine, tangent.

With any two dimensions given (not  $A$  and  $B$ ) the other three dimensions may be found.

**EXAMPLES. 1.** Given  $A = 37^\circ$ ,  $c = 12$  in. ; find  $a$  and  $b$ .

*Solution.* From formula (2),

$$a = c \sin A = 12 \times \sin 37^\circ.$$

From the approximate table, p. 15,

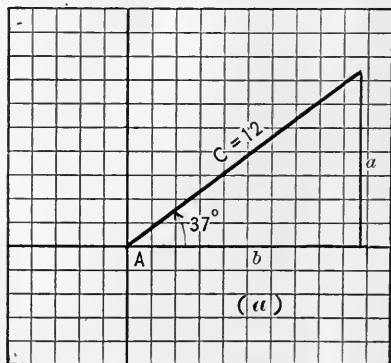
$$\sin 37^\circ = .602.$$

Therefore,

$$a = 12 \times .602 = 7.2 \text{ in.}$$

From (3),

$$\begin{aligned} b &= c \cos 37^\circ = 12 \times .799 \\ &= 9.59 \text{ in.} \end{aligned}$$



(a)

2. Given  $a = 20$  ft.,  $c = 35$  ft., find angle  $A$ .

*Solution.*  $\sin A = \frac{a}{c} = \frac{20}{35} = .571$ .

From table, p. 15, the angle whose sine is .571 is  $34^\circ 50'$  (approximately). Hence  $A = 34^\circ 50'$ .

**11. Projections.** Let perpendiculars fall from two points,  $A$  and  $B$  (Fig. 10) upon any line  $L$ , intercepting  $PQ$ .  $PQ$  is called the projection of the line  $AB$  upon  $L$ . This manner of projection is called *orthogonal*.

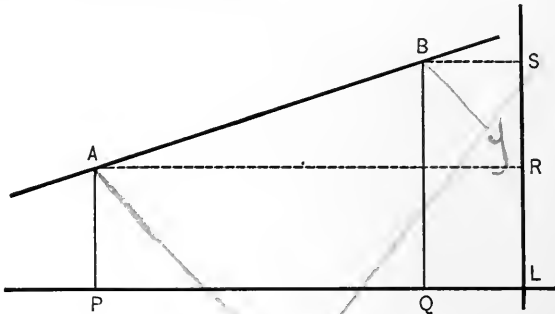


Fig. 10.

(1) *Horizontal and vertical projections.* Any line  $AB$  may be projected orthogonally in any direction; the usual projections, however, are upon the horizontal  $PQ$ , or upon the vertical  $RS$ .

(2) *Laws of orthogonal projection.* The orthogonal projection of any line upon another line involves the base and altitude of a right triangle, with the hypotenuse given. Hence,

(a) The horizontal projection,

$$x = r \cdot \cos \theta,$$

(b) The vertical projection,

$$y = r \cdot \sin \theta.$$

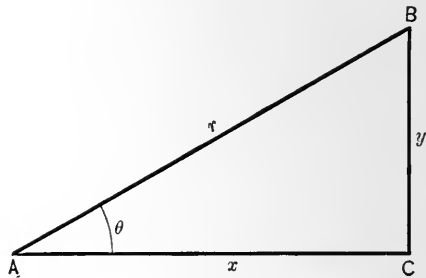


Fig. 11.

**THEOREM.** *The horizontal projection of any line segment equals the length of the segment multiplied by the cosine of the*

angle of inclination; the vertical projection equals the length of the segment multiplied by the sine of the angle of inclination.

**12. Components.** Forces, velocities, and accelerations may be represented by *directed lines*. A line of given length and fixed direction is sometimes called a *vector*. Thus, in Fig. 12,  $V$  is a vector, also  $V_x$ ,  $V_y$ .

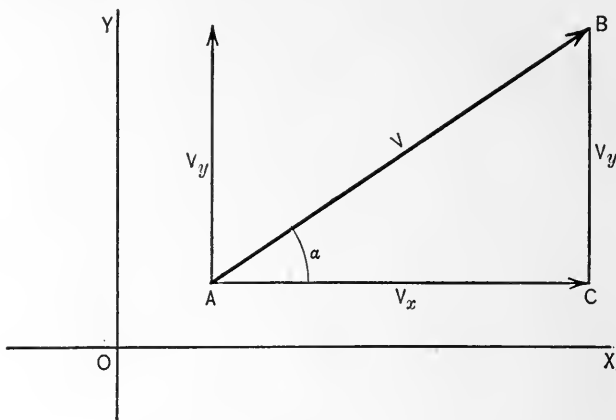


Fig. 12.

Suppose a body is moving with a velocity  $V$  in the path  $AB$ , Fig. 12, making an angle  $\alpha$  with the horizontal  $OX$ ; we may require the velocity in the horizontal  $AC$  (the horizontal component of the velocity,  $V_x$ ), also the vertical velocity  $CB$  (the vertical component of the velocity,  $V_y$ ). These components are projections of  $AB$  upon the horizontal and vertical, respectively.

$$AC = AB \cos \alpha, \text{ or } V_x = V \cos \alpha;$$

$$CB = AB \sin \alpha, \text{ or } V_y = V \sin \alpha.$$

Squaring and adding,

$$V_x^2 + V_y^2 = V^2(\cos^2 \alpha + \sin^2 \alpha) = V^2.$$

**THEOREM.** *The sum of the squares of the horizontal and vertical components of a velocity equals the square of the velocity.*

**13. Resultant.** If two forces act upon a particle at  $A$ , the one,  $AC$ , acting horizontally, the other,  $AD$ , acting vertically, the particle at  $A$  will be moved along the diagonal of the parallelogram to  $B$ , Fig. 13. The line  $AB$  is called the *re-*

*sultant* of the forces represented by the two lines  $AC$  and  $AD$ . The forces  $AC$  and  $AD$  need not act at right angles, but whatever their angle, the resultant will be the diagonal of the parallelogram constructed upon  $AC$  and  $AD$ .

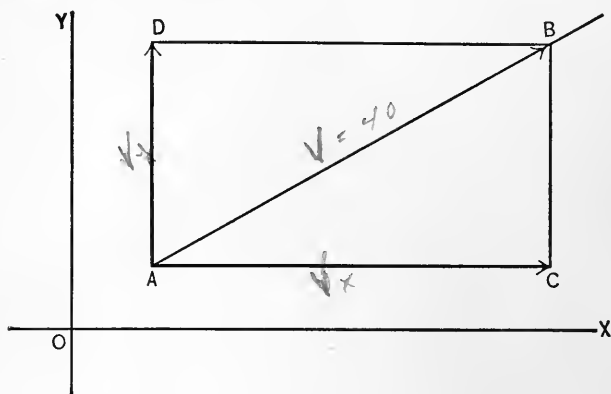


Fig. 13.

The relations between resultant and components which act at right angles to each other involve the simple trigonometric properties of right triangles.

**EXAMPLES. 1.** A train of cars is moving northeast with a velocity  $V$  of 40 mi. per hour. Find its rates of travel east and north.

*Solution.* Let the vector  $V$  represent the given velocity. Then  $V_x$ ,  $V_y$  are the velocities east and north, respectively. See Fig. 12.

$$V_x = V \cos 45^\circ = 40 \times \frac{1}{2} \sqrt{2} = 20\sqrt{2},$$

$$V_y = V \sin 45^\circ = 40 \times \frac{1}{2} \sqrt{2} = 20\sqrt{2}.$$

Hence, the velocities east and north are equal,  $20\sqrt{2}$  mi. per hour.

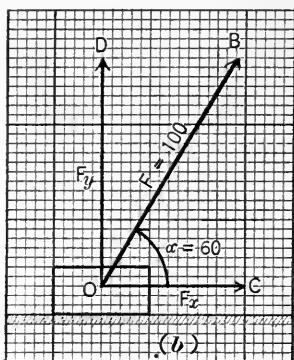
**2.** A point is moving with a velocity of 25 ft. per second along a line making an angle of  $38^\circ$  with the horizontal. Find the horizontal component. *Ans.* 19.7 ft.

**3.** Find the velocity of a point moving at an angle of  $64^\circ$  with the horizontal, if the vertical component of the velocity be 100 ft. per second. *Ans.* 111.3 ft.

**4.** A point describes a circle of radius 20 inches at a uniform rate of two revolutions per minute. Find the distance from the centre of the circle to the projection of the point upon a

horizontal diameter 5 seconds after passing the extremity of that diameter. Ans. 10 in.

5. A force  $F$  of 100 lb. is applied to a block at the point  $O$ , see Fig. (b). If the force makes an angle of  $60^\circ$  with the horizontal, what force tends to draw the block horizontally ( $OC$ )? What force tends to lift the block upwards ( $OD$ )?



*Solution.* Here the solutions called for are the horizontal component  $F_x$  and the vertical component  $F_y$  of the force  $F$ .

$$F_x = F \times \cos \alpha = 100 \cos 60^\circ = 50 \text{ lb.},$$

$$F_y = F \times \sin \alpha = 100 \sin 60^\circ = 86.6 \text{ lb.}$$

6. A balloon rising vertically at a uniform velocity of 704 ft. per minute encounters a wind blowing horizontally at the rate of 24 mi. per hour. Find the angle at which the balloon will rise and its velocity after meeting the wind.

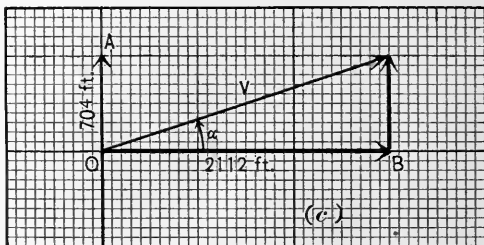
*Solution.* The angle required is represented by  $\alpha$  in Fig. c, the velocity of wind and vertical velocity of the balloon by  $OB$  and  $OA$ , respectively.

$$\tan \alpha = \frac{704}{2112} = \frac{1}{3},$$

$$\alpha = 18^\circ 26'.$$

$$V = 2112 \times \sec \alpha \\ = 2112 \times 1.054 = 2226 \text{ ft.}$$

7. A force of 400 lb. acting in a direction inclined  $40^\circ$  from the horizontal is applied to a heavy block. Find the force which tends to move the block (1) horizontally, (2) the force which tends to lift the block vertically. Ans. (1) 306.4 lb., (2) 257.2 lb.



8. The horizontal and vertical components of a force acting upon a heavy block are 160 lb. and 120 lb. respectively. Find the force and its direction of action.

$$\text{Ans. } 200 \text{ lb.}, 36^\circ 52'.$$



14. **Projected Areas.** Any plane area  $ABCD$  inclined to a

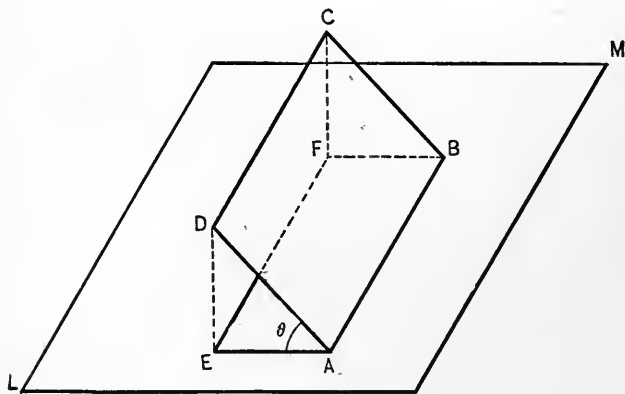


Fig. 14.

plane  $LM$  at an angle  $\theta$  may be projected orthogonally upon  $LM$  into the area  $ABFE$ .

$$ABFE = ABCD \times \cos \theta$$

*Law of projection.* The projection of a given plane area upon a plane equals the given area multiplied by the cosine of the angle of inclination of the two planes.

EXAMPLES. 1. How much horizontal area will be covered by 60 sq. yd. of roofing, the roofing making an angle of  $45^\circ$  with the horizontal? *Ans.*  $60 \cos 45^\circ = 42.42$  sq. yd.

2. Find the roofing required to cover a horizontal space 15 ft. by 24 ft., the roofing rising at an angle of  $40^\circ$ . *Ans.*  $15 \times 24 \times \sec 40^\circ = 469.8$  sq. ft.

15. **Area of the Right Triangle.** The area of a right triangle may be expressed in various ways. Let  $K$  = area; then we have,

$$(1) K = \frac{1}{2} a \times b = \frac{1}{2} ac \cos A = \frac{1}{2} bc \sin A.$$

$$(2) K = \frac{1}{2} b^2 \tan A = \frac{1}{2} a^2 \tan B.$$

$$(3) K = \frac{1}{2} c^2 \sin A \cos A = \frac{1}{2} c^2 \sin B \cos B.$$

In (1)  $a \cos A = b \sin A = p$ ; and in (2)  $b \tan A = a$ ,  
 $a \tan B = b$ .

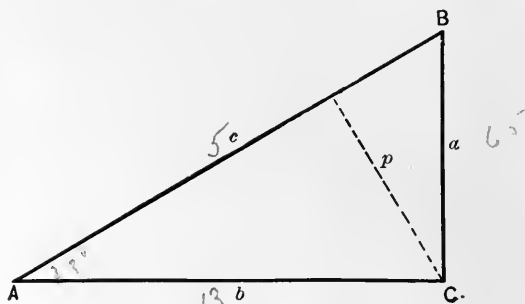


Fig. 15.

EXAMPLES. Find the area of each of the following right triangles, the lettering being shown in Fig. 15:

- |                                 |                                |
|---------------------------------|--------------------------------|
| 1. $a = 20$ , $A = 35^\circ$ .  | 6. $c = 75$ , $a = 2b$ .       |
| 2. $c = 65$ , $B = 28^\circ$ .  | 7. $p = 27$ , $A = 48^\circ$ . |
| 3. $a = 100$ , $A = 30^\circ$ . | 8. $p = 45$ , $B = 75^\circ$ . |
| 4. $b = 42$ , $B = 67^\circ$ .  | 9. $b = 48$ , $a = 52$ .       |
| 5. $c = 35$ , $A = 3B$ .        | 10. $a = 65$ , $5c = 13b$ .    |

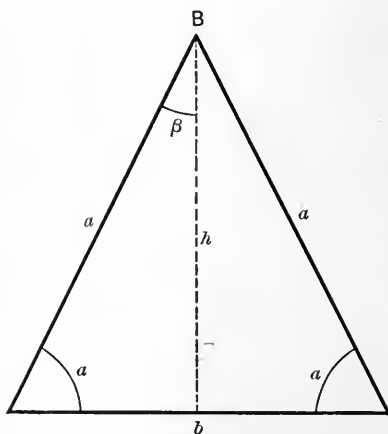


Fig. 16.

**16. The Isosceles Triangle.** Since the isosceles triangle may be divided into two equal right triangles by a perpendicular from the vertical angle  $B$  (see Fig. 16) upon the base, the solution depends only upon the solution of a right triangle.

EXAMPLES. 1. Find the base  $b$  and area of an isosceles triangle when the vertical angle  $B$  is  $80^\circ$ , and each of the equal sides is 36 ft.

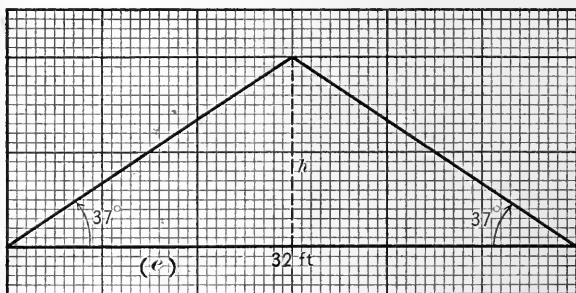
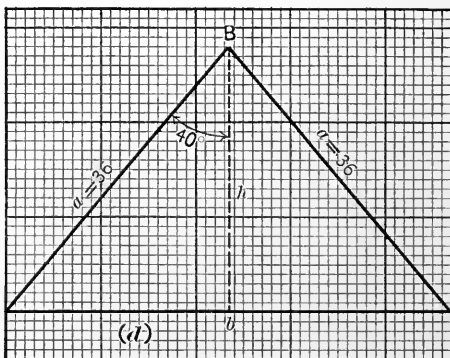
*Solution.* Construct an approximate triangle, Fig. *d*.

(1)  $b$  is the projection of the equal sides on the horizontal. Hence,

$$b = 2 a \times \sin \frac{B}{2} = 2 \times 36 \times \sin 40^\circ = 2 \times 36 \times .643 = 46.3 \text{ ft.}$$

(2) Area =  $\frac{1}{2} b \cdot h = \frac{1}{2} ab \times \cos 40^\circ = 638.2 \text{ sq. ft.}$

2. Find the length of rafters, height of ridge-pole, and area of gable from the data shown in the drawing.



- (1) Length of rafter =  $16 \times \sec 37^\circ = 16 \times 1.252 = 20.03 \text{ ft.}$
- (2) Height  $h = 16 \times \tan 37^\circ = 16 \times .754 = 12 \text{ ft.}$
- (3) Area of gable =  $16 \times h = 192 \text{ sq. ft.}$

17. **Notations of Direction.** If  $OH$ , Fig 17, be a horizontal, the angle  $POH = \phi$  is the *angle of elevation* of  $P$ ; the angle  $QOH = \psi$  is called the *angle of depression* of  $Q$ . A depression angle could also be considered as a negative elevation angle.

The direction of a line  $OP$  with respect to a north and south line  $NS$ , Fig. 18, is read North  $\alpha$  degrees East,  $N. \alpha^\circ E.$ ; the same direction with regard to the east and west line  $EW$  could be read East  $\beta$  degrees North,  $E. \beta^\circ N.$

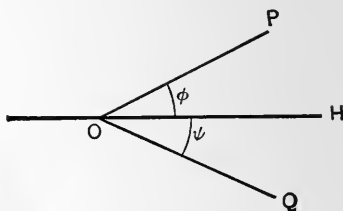


Fig. 17.

Similar readings for directions may be applied to south and

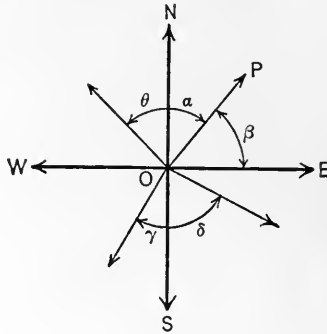
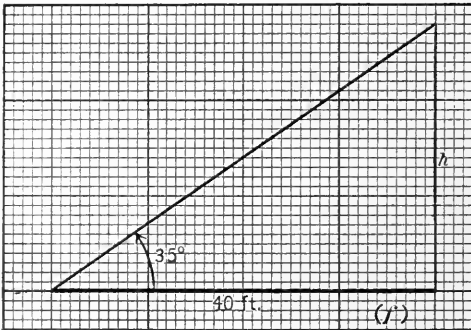


Fig. 18.

west lines. A direction of a line given as above is called the *bearing of the line when read from N. or S.*

EXAMPLES. 1. If the angle of elevation of the sun be  $35^\circ$ ,

how high is a pole whose shadow upon the ground is 40 ft. ?



*Solution.* (1) Construct drawing showing data.

(2) Select formula (4), p. 16,

$$\tan 35^\circ = \frac{h}{40},$$

$$\begin{aligned} \text{or } h &= 40 \times \tan 35^\circ \\ &= 40 \times 0.7 \\ &= 28 \text{ ft.} \end{aligned}$$

2. Find the radius of a circle in which a chord 30 in. long subtends a  $20^\circ$  arc. Also find the area of the triangle formed by the chord and the radii to its extremities.

*Solution.* (1) Construct figure; draw radius perpendicular to middle of chord. Let  $B$  be the middle point of the chord.

$$\text{Angle } AOB = 10^\circ, AB = 15 \text{ in.}$$

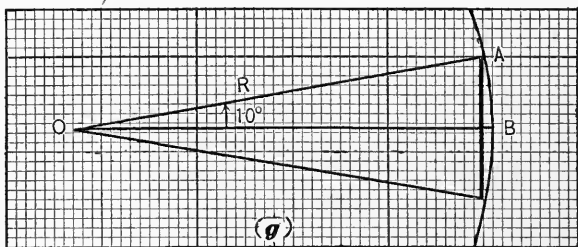
$$(2) \quad \sin AOB = \frac{AB}{R}, R = AB \div \sin AOB,$$

or,

$$R = AB \times \csc AOB.$$

(3) Substitute the values  $AB = 15$ ,  $\angle AOB = 10^\circ$ , and we have

$$R = 15 \times \csc 10^\circ = 15 \times 5.759 = 86.38 \text{ in.}$$



(4) The area is given by

$$K = \frac{1}{2} \text{ base} \times \text{altitude. } OB = 15 \times \cot 10^\circ = 85.06.$$

Then

$$K = 15 \times OB = 1275.9 \text{ sq. in.}$$

**18. To solve Right Triangles.** In the solution of right triangles the beginner should provide himself with (1) a graduated ruler, (2) squared paper, and (3) a protractor graduated to degrees. With this equipment a triangle approximating very closely to any given data may be constructed. An approximate construction will enable the student to detect any considerable error in calculation.

In solving a right triangle the following directions are suggested: (1) *Draw, on squared paper, a figure as accurately as possible from the given data, and estimate approximate values for the unknown parts.* (2) *Select formulas, § 10, each of which contains one unknown.* (3) *Substitute the given data in the proper formula, using approximate values of the trigonometric functions, p. 15, and solve for the unknowns.* (4) *Check results by using some formula not employed in the calculation.*

In many ordinary measurements approximate results only are desired. The following list of exercises involving the right triangle is inserted to give practice in approximating results. The trigonometric functions found on p. 15 give approximations to three decimals, and when employed in solution will give results true to one or two decimals. When greater accuracy is desired, the more complete tables of the natural functions should be used. For still more accurate results, the logarithmic tables, explained in Chapter VI, should be employed.

## EXERCISES

Solve the following right triangles, giving results to nearest tenth and nearest minute. Use Approximate Tables of trigonometric functions, p. 15, for solutions of Ex. 1 to 20, approximating angles to minutes. For areas employ formulas of § 15.

No.	DATA	ANSWERS	AREA = $K$
1	$a = 13$ $b = 40$	$A = 18^\circ$ $B = 72^\circ$ $c = 42$	260
2	$a = 20$ $b = 8$	$A = 68^\circ 12'$ $B = 21^\circ 48'$ $c = 21.5$	80
3	$a = 80$ $b = 30$	$A = 69^\circ 27'$ $B = 20^\circ 33'$ $c = 85.4$	1200
4	$a = 16.16$ $b = 25.28$	$A = 32^\circ 35'$ $B = 57^\circ 25'$ $c = 30$	204.3
5	$a = 10$ $c = 50$	$A = 11^\circ 32'$ $B = 78^\circ 28'$ $b = 49$	245
6	$a = 71$ $c = 78$	$A = 65^\circ 32'$ $B = 24^\circ 28'$ $b = 32.3$	1146.6
7	$a = 84.9$ $c = 93.5$	$A = 65^\circ 14'$ $B = 24^\circ 46'$ $b = 39.17$	1662.8
8	$c = 42$ $A = 81^\circ 30'$	$B = 8^\circ 30'$ $a = 41.5$ $b = 6.2$	128.9
9	$c = 100$ $A = 36^\circ$	$B = 54^\circ$ $a = 58.8$ $b = 80.9$	2378.5
10	$c = 67.7$ $A = 23^\circ 30'$	$B = 66^\circ 30'$ $a = 27$ $b = 62.08$	838.1
11	$c = 250$ $B = 47^\circ$	$A = 43^\circ$ $a = 170.5$ $b = 182.8$	15583.7
12	$c = 400$ $b = 240$	$A = 53^\circ 8'$ $B = 36^\circ 52'$ $a = 320$	38400
13	$K = 55.42$ $A = 30^\circ$	$a = 8$ $b = 8\sqrt{3}$ $c = 16$	
14	$K = 28.93$ $A = 26^\circ 45'$	$a = 5.4$ $b = 10.7$ $c = 12$	
15	$K = 145.8$ $b = 18$	$A = 42^\circ$ $c = 24.2$ $a = 16.2$	

16. A monument 283 ft. high casts a shadow 100 ft. long upon the ground. Find the angle of elevation of the sun at that instant. *Ans.*  $70^\circ 32'$ .

17. A ladder 30 ft. long resting upon the ground reaches a point 24 ft. high upon a vertical wall. Find the angle of elevation of the ladder. *Ans.*  $53^\circ 6'$ .

18. Gable rafters 20 ft. long project 2 ft. beyond the walls of a house and are set with a pitch (angle of elevation) of  $40^\circ$ . Find the height  $h$  of the ridge-pole and the width of the house. *Ans.*  $h = 11.57$  ft.,  $w = 27.57$  ft.

19. Find the bearing of a road which leads to a point 5 mi. east and 8 mi. north. *Ans.* N.  $32^\circ$  E.

20. A rectangle is 98 by 148. Find the angle made by a diagonal with the longer side. *Ans.*  $33^\circ 30'$ .

21. The sides of an isosceles triangle are 30, 45, 45, respectively. Find the angles. [Note. Use four-place tables.] *Ans.*  $70^\circ 32'$ ,  $38^\circ 56'$ .

22. Find the radius of a circle in which a 100 ft. chord subtends an angle of  $18^\circ$  at the centre. *Ans.* 319.69 ft.

23. A chord 50 in. long subtends an angle of  $36^\circ$  at the centre. Find the radius  $R$  of the circle and the area  $A$  of the inscribed square. *Ans.*  $R = 80.9$  in.,  $A = 13,089.6$  sq. in.

24. Find the height of a tree which casts a horizontal shadow 60 ft. long when the sun's elevation is  $65^\circ$ . *Ans.* 128.67 ft.

25. Find the angle of inclination of the faces of a wedge whose base is 3 in. and whose face is 14 in. long. *Ans.*  $12^\circ 18'$ .

26. The exterior angle between two 500 ft. tangents is  $72^\circ$ . Find the radius of the circle. *Ans.* 688.2 ft.

27. The length of a kite-string is 200 m. Find the height of the kite when its angle of elevation is  $34^\circ$ . *Ans.* 111.84 m.

28. The radius of a circle is 5 cm. and the length of a chord is 4 cm. Find the angle subtended by the chord at the centre. *Ans.*  $47^\circ 9' 20''$ .

29. Find the radius of a circle inscribed in an equilateral triangle whose perimeter is 42 cm. *Ans.* 4.04 cm.

30. What is the height of a tower if a 16 ft. flagpole upon the top of the tower subtends an angle of  $4^\circ$  at a point on the ground and the angle of elevation of the bottom of the pole is  $40^\circ$ ? *Ans.* 106 ft.

31. At a certain point the angle of elevation of a mountain peak is  $27^\circ$ ; at a distance of 2 mi. farther away in the same direction its elevation angle is  $25^\circ$ . Find the horizontal distance from the first point of observation to the peak. *Ans.* 21.58 mi.

32. Two consecutive milestones on a level road in the same vertical plane as a tower have depression angles of  $42^\circ$ ,  $3^\circ$ , respectively, from the top of the tower. Find the height of the top of the tower and its horizontal distance from the nearer milestone.

*Ans.*  $h = 293.8$  ft. or 261.4 ft.,  $d = 326.3$  ft. or 290.3 ft.

33. A tower stands upon the same plane as a house whose height is 60 ft. The elevation and depression of the top and bottom of the tower from the top of the house are  $41^\circ$  and  $35^\circ$ , respectively. Find the height of the tower. *Ans.* 134.49 ft.

67 34. From a point 10 ft. above the water, the angle of elevation of the top of a tree standing at the edge of the water is  $46^\circ$ , while the depression angle of its image in the water is  $50^\circ$ . Find the height of the tree, and its horizontal distance from the point of observation. *Ans.*  $h = 142.5$  ft.,  $d = 128$  ft.

67 35. In measuring the width of a river a line  $AB$  is measured 240 ft. along one bank. A perpendicular to  $AB$  at  $A$  is erected which locates a point  $C$  upon the opposite bank, and the angle  $ABC$  is found to be  $65^\circ$ . Find the width  $AC$  of the stream. *Ans.* 514.68 ft.

36. Two towers upon the same horizontal plane are of such heights that their elevation angles from a point midway between them are  $40^\circ$ ,  $60^\circ$ , respectively. Find the ratio of their heights. *Ans.*  $8391 \div 17,321$ .

37. From each of two stations a mile apart upon a north and south road, the angle of elevation of a balloon is observed to be  $30^\circ$ , and its bearings are, respectively, N.E. and S.E. Find the height of the balloon. *Ans.* 2155.5 ft.

38. A balloon is exactly over the middle point between two cities. The balloon is a mile high and the distance between the cities subtends an angle of  $136^\circ$  at the balloon. Find the distance between the cities and the distance of the balloon from either of them. *Ans.* 4.95 mi., 2.67 mi.

39. Find the height of a tree if the angle of elevation of its top changed from  $36^\circ$  to  $42^\circ$  on walking toward it 75 ft. in a horizontal line through its base. *Ans.* 282.16 ft.

40. A hill rises uniformly 4 ft. in a horizontal distance of 85 ft. What is the difference in elevation of two points 3500 ft. apart, the distance being measured along the ground? *Ans.* 164.1 ft.

41. What is the angle of incline of a railroad track if it rises 30 ft. in a horizontal distance of a mile? *Ans.*  $19' 32''$ .

42. What is the bearing of a road which leads to a point 14 mi. east and 8 mi. north? *Ans.* N.  $60^\circ 15' 20''$  E.

43. If the radius of the earth (3956 mi.) subtends  $57'$  at the moon, what is the moon's distance from the earth? *Ans.* 238,300 mi.



44. Find the radius of one's horizon if he be located 1320 ft. above the earth. How large when located 2 mi. above the earth? *Ans.* 44.48 mi., 125.8 mi.

45. How high above the earth must one be in order to see a point located on the surface 50 mi. away? *Ans.* 1668.2 ft.

✓46. The radius of a circle is 240 ft. Find the perimeter of a regular inscribed pentagon. *Ans.* 1410.72 ft.

✓47. The radius of a circle is 85 ft. What is the area of the regular inscribed decagon? *Ans.* 21,234.27 sq. ft.

48. Find the perimeter of a regular dodecagon inscribed in a circle whose radius is 25 in. *Ans.* 155.25 in.

✓49. What is the radius of a circle inscribed in an equilateral triangle whose perimeter is 99 ft.? *Ans.* 9.52 ft.

50. The area of a regular pentagon inscribed in a circle is 475.53 sq. cm. Find the area of a regular decagon inscribed in the same circle. *Ans.* 587.8 sq. cm.

51. The area of a regular pentagon is 441 sq. ft. Find the apothem; also find the radius of the circumscribed circle. *Ans.* 11 ft.; 13.6 ft.

52. What is the length of a diagonal joining the first and fourth vertices of a regular polygon of 12 sides inscribed in a circle whose radius is 30 ft.? *Ans.* 42.426 ft.

53. If  $R$  = radius of a circle, show that the area of a regular inscribed polygon of  $n$  sides is  $A = nR^2 \sin \frac{180^\circ}{n} \cos \frac{180^\circ}{n}$ .

54. From the result in Ex. 53 construct a table showing, in terms of  $R$ , areas of the regular inscribed polygons of 3, 4, 5, 9, 10, 12, sides.

55. Show that the area of a regular circumscribed polygon of  $n$  sides is given by  $A = nR^2 \tan \frac{180^\circ}{n}$ .

56. A train moving at a uniform speed of 40 mi. per hour on a straight track passes a station  $A$  at noon; at 2:15 o'clock P. M. it has arrived at a station  $B$ , 56 mi. farther north. How far east of  $A$  is  $B$ , and what is the bearing of the road?

*Ans.* 70.46 mi.; N.  $51^\circ 31' 30''$  E.

57. A boat running at a rate of 10 mi. per hour starts to steam directly across a river one mile in width. If the water be flowing uniformly at a rate of 4 mi. per hour, find the point at which the boat will land, and its velocity in the water.

*Ans.* 0.4 mi. downstream, 10.77 mi. velocity.

58. Find the projection of the altitude of an equilateral triangle upon a side. Let  $a =$  side. *Ans.*  $\frac{3}{4}a$ .

59. A line extends N.  $20^\circ$  E. 125 rd. from a point  $A$ . Find its projection upon a line extending N.  $60^\circ$  E. from  $A$ .

*Ans.* 95.75 rd.

60. Find the projection of a line 450 ft. long running N.  $47^\circ$  E. upon a line running E.  $15^\circ$  S. *Ans.* 238.45 ft.

61. Two forces of 160, 120 lb. act upon a heavy body, the first at an angle of  $30^\circ$  with the horizontal, the second at an angle of  $75^\circ$ . Find the total forces which tend to move the body (1) horizontally, (2) vertically.

*Ans.* (1) 169.6 lb., (2) 195.9 lb.

62. Find the number of square yards in a conical tent with circular base, the vertical angle being  $60^\circ$ , and the centre pole 12 ft. high. [Take  $\pi = \frac{22}{7}$ .] *Ans.* 33.5 sq. yd.

63. Find the area in acres of the following tract of land: starting from a point  $A$ , the boundary line runs N.  $24^\circ$  E. 80 rd. to  $B$ , thence N.  $65^\circ$  E. 120 rd. to  $C$ , thence S. 180 rd. to  $D$ , thence back to  $A$ . Find also the length and bearing of  $DA$ .

*Ans.* 99.157 acres;  $DA = 152.07$  rd.; N.  $68^\circ 18' 23''$  W.

64. Find the area of the following described tract of land: starting from a point  $A$ , the boundary line runs N.  $10^\circ$  E. 100 rd., thence N.  $47^\circ$  E. 150 rd., thence E. 40 rd., thence S.  $10^\circ$  W. 100 rd., thence W. 40 rd., thence to  $A$  the place of beginning.

*Ans.* 81.04 acres.

## CHAPTER III

### TRIGONOMETRIC FUNCTIONS OF ANY ANGLE. GRAPHS

In § 2 the trigonometric functions have been defined for positive acute angles only. We shall now extend these definitions to include angles of any size whatever.

**19. Axes. Quadrants.** To locate an angle which may be either acute or obtuse it is convenient to employ *Coördinate Axes* as shown in Fig. 19. The horizontal line is called the *X-axis*, the vertical is called the *Y-axis*. These axes divide the plane into four *quadrants* marked I, II, III, IV.

A *positive trigonometric angle* is described when a vector  $OP$  is rotated about  $O$  counter-clockwise from the *initial position*  $OX$  into a *terminal position*  $OP$ ;  $XOP = a$ .

If the rotation be *clockwise* about  $O$ , the angle described is *negative*;  $XOP_1 = -\beta$ . See Fig. 19.

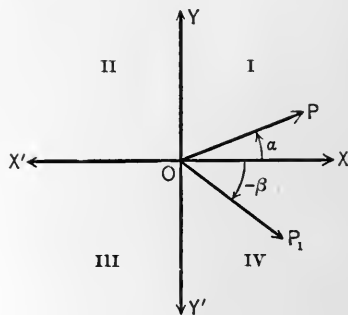


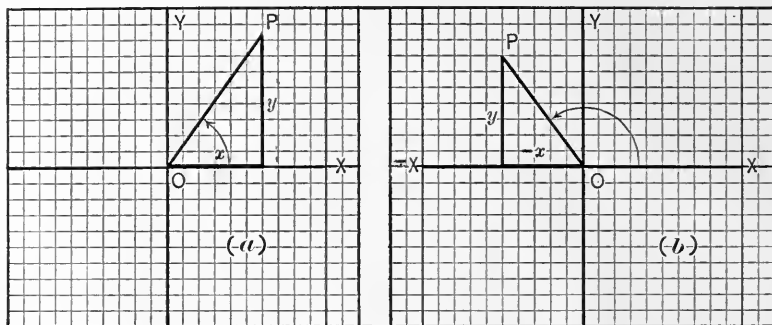
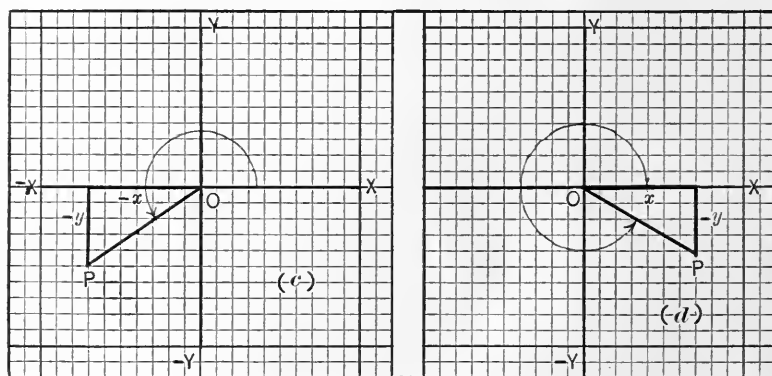
Fig. 19.

**20. Coördinates. Abscissa, Ordinate.** The position of a *terminal line*  $OP$  (Fig. 20 *a, b, c, d*) is determined by two measurements  $x, y$ , called *coördinates of the point P*. The *x-measurement* is called the *abscissa of the point P*, and is the *projection of OP on the X-axis*. If the projection of  $OP$  falls to the right of  $O$  (Fig. 20 *a, d*), the abscissa is *positive*, if to the left (Fig. 20 *b, c*), the abscissa is *negative*.

The *y-measurement* is called the *ordinate of the point P*, and is the *projection of OP upon the Y-axis*. The ordinate is posi-

tive (Fig. 20 *a, b*) when the projection of  $OP$  falls above the horizontal, and is *negative* (Fig. 20 *c, d*) when it falls below the horizontal.

In locating a point in the respective quadrants, the coördinates of any point are usually written in brackets. The symbol  $(a, b)$  means the abscissa  $x = a$ , the ordinate  $y = b$ .

Fig. 20 *a*.Fig. 20 *b*.Fig. 20 *c*.Fig. 20 *d*.

**21. Definitions of the Functions.** From the above figures, (*a*), (*b*), (*c*), (*d*), with  $\angle XOP = \alpha$  and  $OP = r$ , we define in each case:

$$\begin{array}{ll} \sin \alpha = \frac{y}{r} = \frac{\text{ordinate}}{\text{distance}}, & \csc \alpha = \frac{r}{y} = \frac{\text{distance}}{\text{ordinate}}, \\ \cos \alpha = \frac{x}{r} = \frac{\text{abscissa}}{\text{distance}}, & \sec \alpha = \frac{r}{x} = \frac{\text{distance}}{\text{abscissa}}, \\ \tan \alpha = \frac{y}{x} = \frac{\text{ordinate}}{\text{abscissa}}, & \cot \alpha = \frac{x}{y} = \frac{\text{abscissa}}{\text{ordinate}}. \end{array}$$

In this notation the signs of the abscissa and ordinate determine the algebraic signs of the trigonometric functions for angles terminating in the respective quadrants.

**22. Laws of Signs.** (1) *For all angles terminating in the first quadrant, the functions are positive.*

(2) *For angles terminating in the second quadrant, the six functions are negative except sine and cosecant.*

(3) *For angles terminating in the third quadrant, the tangent and cotangent are positive, all others are negative.*

(4) *For angles terminating in the fourth quadrant, the cosine and secant are positive, all others are negative.*

These laws are shown in the following diagram :

	SIN	Cos	TAN	Cot	SEC	Csc
I	+	+	+	+	+	+
II	+	-	-	-	-	+
III	-	-	+	+	-	-
IV	-	+	-	-	+	-

It should be noticed that these general definitions apply to angles larger than  $360^\circ$ . For example,  $\sin 400^\circ$  is the sine of an angle terminating  $40^\circ$  above the initial line; hence  $\sin 400^\circ = \sin 40^\circ$ .  $\tan 500^\circ = \tan(360^\circ + 140^\circ)$  is the tangent of an angle terminating in the second quadrant.  $\tan 500^\circ = \tan 140^\circ = -\tan 40^\circ$ .  $\sin(n360^\circ + \alpha) = \sin \alpha$ .

*The fundamental identities, § 5, hold for any angle.*

$$\begin{aligned} \sin^2 \alpha + \cos^2 \alpha &= 1, & \sin \alpha \csc \alpha &= 1, \\ \sec^2 \alpha - \tan^2 \alpha &= 1, & \cos \alpha \sec \alpha &= 1, \\ \csc^2 \alpha - \cot^2 \alpha &= 1, & \tan \alpha \cot \alpha &= 1. \end{aligned}$$

**EXAMPLES. 1.** What values have the functions when  $\sin \phi = \frac{3}{5}$ ?

*Solution.* The angle  $\phi$  may be constructed in either of two positions,  $AOP_1$  in the first quadrant, or the supplement  $AOP_2$  in the second quadrant. Let  $AOP_1 = \phi_1$ ,  $AOP_2 = \phi_2$ . In the first case,  $\sin \phi_1 = \frac{3}{5}$ ,  $\cos \phi_1 = \frac{4}{5}$ ,  $\tan \phi_1 = \frac{3}{4}$ , etc. In the second case,  $\sin \phi_2 = \frac{3}{5}$ ,  $\cos \phi_2 = -\frac{4}{5}$ ,  $\tan \phi_2 = -\frac{3}{4}$ , etc.

2. Find all the trigonometric functions when  $\cos \phi = \frac{1}{2}$ .

*Solution.* Locate angle  $\phi$  as a positive angle in the first quadrant, and as an equal negative angle in the fourth quadrant. The angle whose cosine is  $\frac{1}{2}$  is either  $\phi$  or  $-\phi$ . Then,  $\sin \phi = \pm \frac{\sqrt{3}}{2}$ ,  $\cos \phi = \frac{1}{2}$ ,  $\tan \phi = \pm \sqrt{3}$ ,  $\cot \phi = \pm \frac{1}{\sqrt{3}}$ , etc.

3. Locate the positive angle  $\phi$ , when  $P$  has the following coördinates: (a) (4, 3); (b) (-4, 5); (c) (5, -3); (d) (8, -1); (e) (-5, -6); (f) (3, -4).

4. Give the values of each trigonometric function for each angle determined in Ex. 3.

#### EXERCISES

Name the quadrant (or quadrants) in which  $\phi$  terminates when:

- |                                 |  |
|---------------------------------|--|
| 1. $\sin \phi = \frac{1}{2}$ .  | 6. $\tan \phi = -5$ .                            |
| 2. $\tan \phi = 4$ .            | 7. $\csc \phi = -2$ .                            |
| 3. $\cos \phi = \frac{3}{5}$ .  | 8. $\sin \phi = \frac{2}{3}$ , $\tan \phi < 0$ . |
| 4. $\sin \phi = -\frac{4}{5}$ . | 9. $\cos \phi = \frac{1}{3}$ , $\cot \phi < 0$ . |
| 5. $\cot \phi = 0$ .            | 10. $\tan \phi = 3$ , $\sin \phi < 0$ .          |

Express the following as functions of acute angles:

- |  |  |   |
|--|--|---|
| 11. $\sin 440^\circ = \sin (360^\circ + 80^\circ) = \sin 80^\circ$ . |  |   |
| 12. $\sin 370^\circ$ .   | 13. $\tan 430^\circ$ .                           | 14. $\cos (2\pi + 20^\circ)$ .                    |
| 15. $\tan \left( \pi + \frac{\pi}{3} \right)$ .                      | 16. $\cot \left( n\pi + \frac{\pi}{6} \right)$ . | 17. $\sin \left( 2n\pi + \frac{\pi}{4} \right)$ . |
| 18. $\sec 300^\circ$ .   | 19. $\tan 700^\circ$ .                           | 20. $\sin 500^\circ$ .                            |

**23. Functions of Negative Angles.** To express the trigonometric functions of a negative angle in terms of an equal positive angle construct the negative angle and an equal positive angle, Figs. 21 and 22. In either drawing ( $\theta$  acute, or  $\theta$  obtuse) the triangles  $AOP$  and  $AOP_1$  are equal,

$$x_1 = x, \quad y_1 = -y, \quad r_1 = r.$$

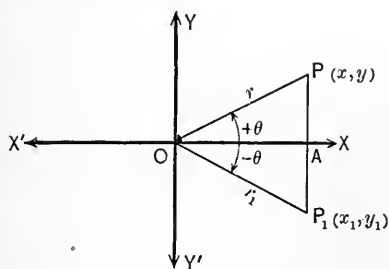


Fig. 21.

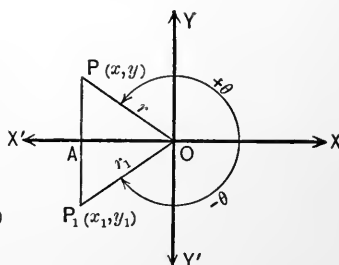


Fig. 22.

$$\sin(-\theta) = \frac{y_1}{r_1} = \frac{-y}{r} = -\sin \theta, \quad \csc(-\theta) = -\csc \theta,$$

$$\cos(-\theta) = \frac{x_1}{r_1} = \frac{x}{r} = \cos \theta, \quad \sec(-\theta) = \sec \theta,$$

$$\tan(-\theta) = \frac{y_1}{x_1} = \frac{-y}{x} = -\tan \theta, \quad \cot(-\theta) = -\cot \theta.$$

THE LAWS GOVERNING FUNCTIONS OF NEGATIVE ANGLES ARE: (1) *Any trigonometric function of a negative angle equals the same function of an equal positive angle, (2) the sign being changed in all cases except for the cosine and secant.*

### EXERCISES

1. Write equivalents of the following functions with the signs of the angles changed:

- (1)  $\cos(-48^\circ)$ ; (4)  $\cot(-87^\circ)$ ; (7)  $\sin 47^\circ$ ;  
 (2)  $\tan(-65^\circ)$ ; (5)  $\sec(-75^\circ)$ ; (8)  $\tan(\alpha - \beta)$ ;  
 (3)  $\sin(-50^\circ)$ ; (6)  $\cot(-100^\circ)$ ; (9)  $\sin(\theta - \phi)$ .

2. Write numerical values of the following:

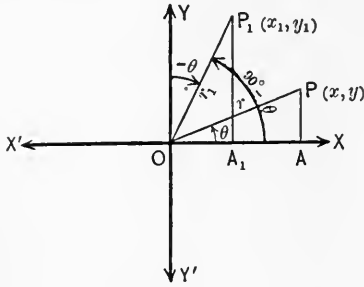
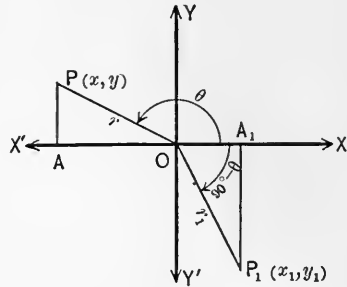
- (1)  $\sin(-30^\circ)$ ; (3)  $\cot(-60^\circ)$ ; (5)  $\cos(-60^\circ)$ ;  
 (2)  $\tan(-45^\circ)$ ; (4)  $\sec(-45^\circ)$ ; (6)  $\tan(-90^\circ)$ .

3. Reduce to numerical values:

- (1)  $\sin 90^\circ \times \sin(-90^\circ) \div \tan(-45^\circ)$ .  
 (2)  $\tan(-60^\circ) \times \sin(-30^\circ) \times \csc 60^\circ$ .  
 (3)  $\sin^2(-45^\circ) \times \cos(-60^\circ) \times \csc(-45^\circ)$ .  
 (4)  $\sin^2(-45^\circ) \div \cos^2(-45^\circ) + \tan(-45^\circ)$ .  
 (5)  $\sec^2(120^\circ) - \tan^2(120^\circ) + \sin(-90^\circ)$ .  
 (6)  $\cos(-80^\circ) \times \sin(-20^\circ) \times \sec 80^\circ \times \csc(-20^\circ)$ .

### 24. Functions of $90^\circ - \theta$ and $90^\circ + \theta$ .

(1) *Complemental angles.* The functions of  $90^\circ - \theta$  with  $\theta$  acute, Fig. 23 *a*, or  $\theta$  obtuse, Fig. 23 *b*, obey the same laws as have been developed in § 3.

Fig. 23 *a*.Fig. 23 *b*.

In the drawings, Figs. 23 *a*, *b*, the triangles  $OPA$  and  $OP_1A_1$  are equal, and

$$x_1 = y, \quad y_1 = x, \quad r_1 = r.$$

Defining the functions, we have :

$$\sin(90^\circ - \theta) = \frac{y_1}{x_1} = \frac{x}{r} = \cos \theta, \quad \csc(90^\circ - \theta) = \sec \theta,$$

$$\cos(90^\circ - \theta) = \frac{x_1}{r_1} = \frac{y}{r} = \sin \theta, \quad \sec(90^\circ - \theta) = \csc \theta,$$

$$\tan(90^\circ - \theta) = \frac{y_1}{x_1} = \frac{x}{y} = \cot \theta, \quad \cot(90^\circ - \theta) = \tan \theta.$$

**LAW FOR COMPLEMENTAL ANGLES.** *The functions of the complement of any angle equal the corresponding co-functions of the angle.*

(2) *Functions of  $90^\circ + \theta$ .* The functions of  $90^\circ + \theta$  may be derived from the above functions of  $90^\circ - \theta$  by changing  $\theta$  into  $-\theta$  and noting the results of § 23.

$$\sin(90^\circ + \theta) = \cos(-\theta) = \cos \theta, \quad \csc(90^\circ + \theta) = \sec \theta,$$

$$\cos(90^\circ + \theta) = \sin(-\theta) = -\sin \theta, \quad \sec(90^\circ + \theta) = -\csc \theta,$$

$$\tan(90^\circ + \theta) = \cot(-\theta) = -\cot \theta, \quad \cot(90^\circ + \theta) = -\tan \theta.$$

These results show that the same law holds for functions of  $90^\circ + \theta$  as for  $90^\circ - \theta$ , except the algebraic sign is changed in all cases except that of the *sine* and *cosecant*.



**25. Functions of  $180^\circ - \theta$  and  $180^\circ + \theta$ . Supplemental Angles.** The functions of the supplement of an angle  $\theta$  may be expressed in terms of the functions of  $\theta$ . Construct  $\theta$  acute, Fig. 24 a; also construct  $\theta$  obtuse, Fig. 24 b.

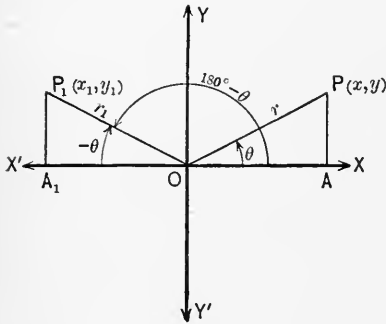


Fig. 24 a.

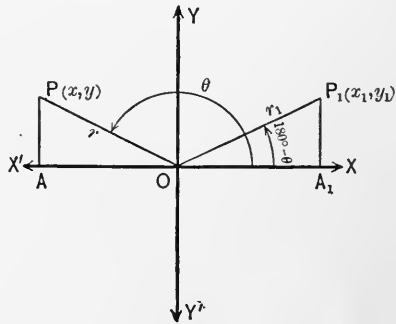


Fig. 24 b.

In either figure the triangle  $OAP$  equals the triangle  $OA_1P_1$ , and

$$x_1 = -x, \quad y_1 = y, \quad r_1 = r.$$

Hence,

$$\sin(180^\circ - \theta) = \frac{y_1}{r_1} = \frac{y}{r} = \sin \theta, \quad \csc(180^\circ - \theta) = \csc \theta,$$

$$\cos(180^\circ - \theta) = \frac{x_1}{r_1} = \frac{-x}{r} = -\cos \theta, \quad \sec(180^\circ - \theta) = -\sec \theta,$$

$$\tan(180^\circ - \theta) = \frac{y_1}{x_1} = \frac{y}{-x} = -\tan \theta, \quad \cot(180^\circ - \theta) = -\cot \theta.$$

**LAWS FOR SUPPLEMENTAL ANGLES.** Any trigonometric function of an angle equals the same function of its supplement, the algebraic sign being changed in all cases except the sine and cosecant.

The functions of  $180^\circ + \theta$  may be obtained from those of  $180^\circ - \theta$  by changing  $\theta$  to  $-\theta$  in the above formulas. We find:

$$\sin(180^\circ + \theta) = \sin(-\theta) = -\sin \theta, \quad \csc(180^\circ + \theta) = -\csc \theta,$$

$$\cos(180^\circ + \theta) = -\cos(-\theta) = -\cos \theta, \quad \sec(180^\circ + \theta) = -\sec \theta,$$

$$\tan(180^\circ + \theta) = -\tan(-\theta) = \tan \theta, \quad \cot(180^\circ + \theta) = \cot \theta.$$

**LAW.** Any trigonometric function of  $180^\circ \pm \theta$  equals the same function of the angle  $\theta$ , regard being had for the algebraic sign.

## EXERCISES

1. Fill the blanks with the proper function of the supplement of each angle :

- (1)  $\sin 150^\circ = \sin 30^\circ$                       (6)  $\csc 100^\circ 20' =$   
 (2)  $\tan 97^\circ 20' =$                               (7)  $\tan (90^\circ + \phi) =$   
 (3)  $\cos 160^\circ 40' =$                             (8)  $\sin (90^\circ - \phi) =$   
 (4)  $\cot 175^\circ 10' =$                             (9)  $\cos (45^\circ - \phi) =$   
 (5)  $\sec 120^\circ 10' =$                             (10)  $\cot (60^\circ + \phi) =$

2. By taking supplements of  $0^\circ$ ,  $30^\circ$ ,  $45^\circ$ , and  $60^\circ$  find the trigonometric functions of  $180^\circ$ ,  $150^\circ$ ,  $135^\circ$ , and  $120^\circ$ . Fill the blanks in the following table :

$\phi =$	$0^\circ$	$30^\circ$	$45^\circ$	$60^\circ$	$90^\circ$	$120^\circ$	$135^\circ$	$150^\circ$	$180^\circ$
$\sin \phi$	0	$\frac{1}{2}$	.707	$\frac{\sqrt{3}}{2}$	1	.866	.707	$\frac{1}{2}$	0
$\cos \phi$	1	.866	.707	$\frac{1}{2}$	0	-.866	-.707	-.866	-1
$\tan \phi$	0	.577	1	1.732	$\infty$	-.866	-.577	-.577	0
$\cot \phi$	$\infty$	1.732	1	.577	0	-.577	-.1.732	-.1.732	$\infty$
$\sec \phi$	1	1.155	1.414	2	$\infty$	1.155	1.414	2	-1
$\csc \phi$	$\infty$	2	1.414	1.155	1	1.155	1.414	2	$\infty$

3. Find numerical values of the following :

- (1)  $\sin 120^\circ \times \sin 60^\circ$ .  
 (2)  $\tan 45^\circ \times \cot 12^\circ \times \cos 90^\circ$ .  
 (3)  $5 \times \cos 135^\circ \times \sin 90^\circ \times \cos 180^\circ$ .  
 (4)  $\tan 135^\circ \times \cot 130^\circ \div \sin 60^\circ$ .  
 (5)  $\tan 150^\circ \times \cos 150^\circ \div \sin 30^\circ$ .  
 (6)  $2 \sin 120^\circ + \cot 150^\circ$ .  
 (7)  $\tan 135^\circ + \cot 45^\circ - \cos 180^\circ$ .  
 (8)  $\cos 30^\circ + \cos 150^\circ + \tan 60^\circ + \tan 120^\circ$ .  
 (9)  $(\tan 120^\circ - \tan 135^\circ) \times (\tan 120^\circ + \tan 135^\circ)$ .  
 (10)  $\sec(180^\circ - \theta) \times \cos \theta \times \tan(180^\circ - a) \times \cot a$ .

4. From proper drawings obtain values of the functions of  $180^\circ + \theta$  in terms of the functions of  $\theta$ .

5. Verify  $\sin 210^\circ = -\frac{1}{2}$ ;  $\cos 225^\circ = -\frac{1}{2}\sqrt{2}$ ;  $\tan 225^\circ = 1$ ;  $\tan 240^\circ = \sqrt{3}$ . [NOTE. Construct drawings.]

6. By adding  $180^\circ$  to the angle in the functions of  $90^\circ - \theta$  derive the functions of  $270^\circ - \theta$ . Verify the results by constructing proper drawings.

7. Find the value of  $\frac{\cos(90^\circ + \alpha)}{\sin(-\alpha)} + \frac{\tan(-\alpha)}{\tan(180^\circ + \alpha)}$ .

8. Find the value of  $\frac{\sin(180^\circ - \phi)}{\cos(90^\circ + \phi)} \times \frac{\tan(180^\circ + \theta)}{\cot(90^\circ + \theta)}$ .

9. What sign has  $\sin x + \cos x$  for the following values of  $x$ :

(1)  $x = 90^\circ$ ; (2)  $x = 120^\circ$ ; (3)  $x = 135^\circ$ ;

(4)  $x = 210^\circ$ ; (5)  $x = 300^\circ$ ?

10. Find all angles less than  $360^\circ$  which satisfy:

(1)  $\tan \theta = -1$ ; (2)  $\sin \theta = \frac{1}{2}\sqrt{3}$ ; (3)  $\cos \theta = -\frac{1}{2}$ .

### 26. Line-values of the Functions.

(1) *Acute angles.* Let the angle  $\theta$  be constructed at the centre of a circle whose radius is unity, Fig. 25. Then arc  $AB = \theta$ .

$CB = \sin \theta$ ,  $OT' = \csc \theta$ ,

$OC = \cos \theta$ ,  $OT = \sec \theta$ ,

$AT = \tan \theta$ ,  $DT' = \cot \theta$ ,

$CA = \text{vers } \theta$ ,  $ED = \text{covevs } \theta$ .

These lines represent graphically the values of the trigonometric functions when the radius of the circle is taken as unity.

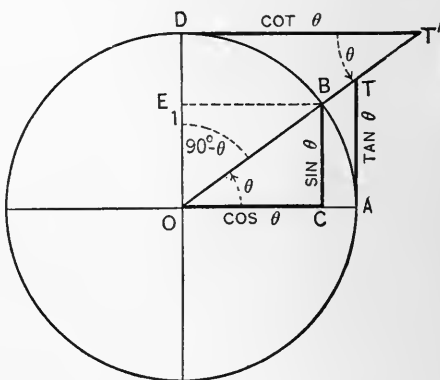


Fig. 25.

It should be noticed that trigonometric functions considered as *line-values* may be described as follows:

(1) *The sine of an angle is the length of the perpendicular let fall from the terminal end of the arc (B) upon the diameter through the initial end (A).* (2) *The cosine of an angle is the*

part of the radius ( $OC$ ) cut off by the foot of the perpendicular ( $BC$ ). (3) The tangent of an angle is the geometric tangent erected at the initial extremity ( $A$ ) of the arc and terminated by the diameter produced through the terminal extremity ( $B$ ) of the arc. (4) The secant is the line from  $O$  to the extremity of the tangent ( $OT$ ). (5) The cotangent is the geometric tangent erected at the  $90^\circ$  point ( $D$ ) of the circle, and terminated by the terminal radius produced to  $T'$ , ( $DT'$ ). (6) The cosecant is the length of the line from the centre of the circle to the extremity of the cotangent ( $OT'$ ).

*Convention of signs.* In the above definitions the sines and tangents are verticals, and are taken *positive when drawn upward, negative when drawn downward*. The cosines and cotangents are horizontals, and are *positive when drawn to the right, negative when drawn to the left*. The secants and cosecants are *positive when drawn from  $O$  along the terminal boundary  $OB$ , negative when drawn from  $O$  backward, as  $OT$  in Fig. 26 (a).*

The older text-books defined the trigonometric functions from this line-value standpoint, but at the present time the definitions are usually given, as in § 2 and § 21, from the ratio standpoint. It is often convenient to use the line-values.

(2) *Angles larger than  $90^\circ$ .* Drawings are here inserted to show the line-values of the functions for angles larger than  $90^\circ$ , Figs. 26 (a), (b), (c). In each case  $OT = \sec \theta$ ,  $OT' = \csc \theta$ .

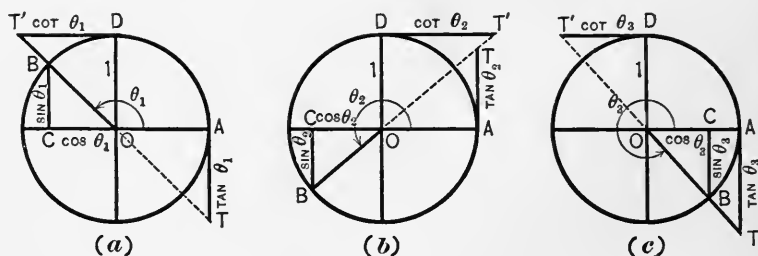


Fig. 26 (a), (b), (c).

These drawings show clearly that the fundamental relations, § 5, hold whatever the angle may be.

The following table shows the signs of the functions of  $\theta$ ,  $\theta_1$ ,  $\theta_2$ ,  $\theta_3$ , shown in Figs. 25, 26 (a), (b), (c), respectively.

	SIN	COS	TAN	COT	SEC	CSC
$\theta$	+	+	+	+	+	+
$\theta_1$	+	-	-	-	-	+
$\theta_2$	-	-	+	+	-	-
$\theta_3$	-	+	-	-	+	-

It should be remarked that the functions of an angle between  $270^\circ$  and  $360^\circ$  are the same as those of a *negative acute angle*, and that the functions of an angle between  $180^\circ$  and  $270^\circ$  are the same as those of a *negative obtuse angle*.

### EXERCISES

Draw figures and show :

1.  $\sin 70^\circ = \cos 20^\circ = \sin 110^\circ$ .
2.  $\sin 120^\circ = \cos 30^\circ = -\sin(-60^\circ)$ .
3.  $\sin 117^\circ = \cos(-27^\circ) = \cos 27^\circ$ .
4.  $\cos 300^\circ = \cos(-60^\circ) = \sin 30^\circ$ .
5.  $\sin 220^\circ = \sin(-40^\circ) = -\sin 40^\circ$ .
6.  $\cos 195^\circ = -\cos(-15^\circ) = -\cos 15^\circ$ .
7.  $\sin(-10^\circ) = \sin 190^\circ = -\sin 10^\circ$ .
8.  $\sin 60^\circ = -\cos 150^\circ = \cos 30^\circ$ .
9.  $\tan 120^\circ = -\tan 60^\circ = \tan(-60^\circ)$ .
10.  $\cot 165^\circ = -\cot 15^\circ = -\tan 75^\circ$ .

If  $A + B + C = 180^\circ$ , show :

11.  $\cos \frac{A}{2} = \sin \frac{B + C}{2}$ .
12.  $\sin \frac{B}{2} = \cos \frac{A + C}{2}$ .
13.  $\sin A = \sin(B + C)$ .
14.  $\cos B = -\cos(A + C)$ .
15.  $\tan A = -\tan(B + C)$ .
16.  $\sin A = -\sin(2A + B + C)$ .
17.  $\cos A = -\cos(2A + B + C)$ .
18.  $\cos\left(\frac{B - C}{2}\right) = \sin\left(\frac{A + 2B}{2}\right) = \sin\left(\frac{A + 2C}{2}\right)$ .

$$19. \sin\left(\frac{A-B}{2}\right) = -\cos\left(\frac{2A+C}{2}\right) = \cos\left(\frac{C+2B}{2}\right).$$

$$20. \cos B = \sin\left(\frac{A+3B+C}{2}\right).$$

Change each of the following to functions of positive acute angles:

21.  $\sin 340^\circ$ .

24.  $\cot(-160^\circ)$ .

27.  $\sec(-200^\circ)$ .

22.  $\tan 540^\circ$ .

25.  $\sin 260^\circ$ .

28.  $\tan(-280^\circ)$ .

23.  $\cos 450^\circ$ .

26.  $\cot 300^\circ$ .

29.  $\sin(-500^\circ)$ .

30.  $\cos(-490^\circ)$ .

31.  $\sin(-40^\circ) \times \tan 187^\circ$ .

**27. Graphs of the Trigonometric Functions.** The *line-values* of the functions furnish a means for constructing graphs which show to the eye the numerical values of  $\sin x$ ,  $\cos x$ ,  $\tan x$  for any angle.

(1) *Graph of  $\sin x$ .* Let us take a unit circle, Fig. 27, and, beginning at  $A$ , locate points  $B_1, B_2, B_3, \dots$  at equal intervals, say  $18^\circ$ , along the circumference. Then draw perpendiculars  $B_1C_1, B_2C_2, \dots$ . These lines are equal to the sines of the respective angles subtended by arcs  $AB_1, AB_2, \dots$ . Now, place the point  $A$  at  $O$ , Fig. 28 (a), and straighten the circumference along the line  $OX$ , the points  $B_1, B_2, B_3, \dots$  falling at equal intervals along  $OX$  as indicated. Erect perpendiculars (+ or -) equal to  $B_1C_1, B_2C_2, B_3C_3, \dots$ , respectively. These lines are the sines of the angles whose arc measures are  $AB_1, AB_2, AB_3, \dots$ . In Figs. 28 (a) and (b) the scale is  $\frac{1}{2}$  of that used in Fig. 27.

If a smooth curve be drawn through  $C_1, C_2, C_3, \dots$ , we have a locus known as the *sine curve*, or the *graph of  $\sin x$* .

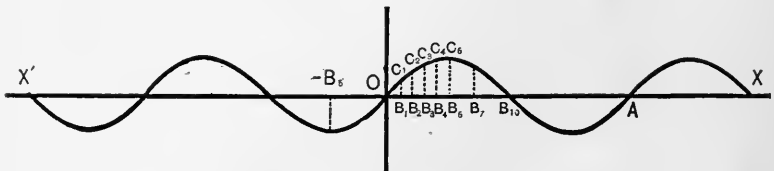


Fig. 28 (a). SINE CURVE.

If the circumference be laid off to the left of  $O$ , we have the part of the graph shown on  $OX'$ .

(2) *Graph of  $\cos x$ .* Taking the unit circle as before, Fig. 27, dividing its arc into equal intervals, laying the circumference upon  $OX$ , and erecting perpendiculars at  $O, B_1, B_2, B_3, \dots$  equal in length to  $OA, OC_1, OC_2, \dots$ , we have lines which equal the cosines of the angles subtended by arcs  $AB_1, AB_2, \dots$ , respectively. Now, connect the points  $A, C_1, C_2, \dots$  by a smooth curve, and we have the *graph of  $\cos x$* , or the *cosine curve*, Fig. 28 (b).

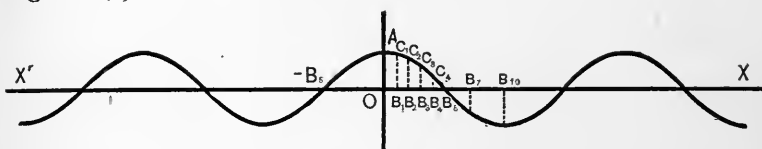


Fig. 28 (b). COSINE CURVE.

(3) *Graph of  $\tan x$  and  $\cot x$ .* If at the points  $B_1, B_2, B_3, \dots$  on  $OX$ , Fig. 28 (e), we erect perpendiculars (+ or -) equal to the lengths of the tangents at  $A$  of the arcs  $AB_1, AB_2, AB_3, \dots$ , the points  $T_1, T_2, \dots$  lie upon a curve known as the *tangent curve*, or the *graph of the  $\tan x$* . This curve consists of a series of parallel graphs, each extending to infinity at  $90^\circ, 270^\circ, 540^\circ, \dots$ .

The graph of  $\cot x$  may be constructed in a similar manner. The graphs of  $\tan x$  and  $\cot x$  are shown in Fig. 28 (e).

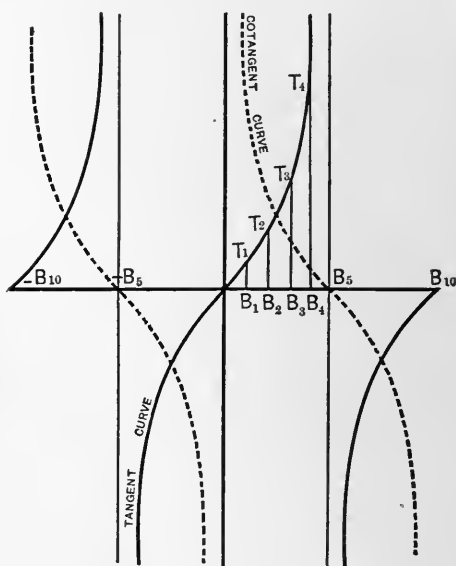


Fig. 28 (e).

## CHAPTER IV

### MEASUREMENT OF ANGLES

**28. Units of Measure.** In the measurement of angles, two units are in use, the *degree* and the *radian*.

(1) *Sexagesimal system.* The degree\* (marked by  $^{\circ}$ ) is the  $\frac{1}{90}$  of a right angle. It is the unit of *degree measure* or the *sexagesimal measure*. The degree is divided into 60 minutes (marked 60'), and the minute into 60 seconds (marked 60").

$$48 \text{ degrees } 35 \text{ minutes } 24 \text{ seconds} = 48^{\circ} 35' 24''.$$

Seconds are frequently written as decimals of a minute, and minutes and seconds may be written as decimals of a degree.

$$45^{\circ} 21' 36'' = 45^{\circ} 21.6' = 45.36^{\circ}.$$

Degree measure is used in most of the practical calculations of astronomers, engineers, and surveyors.

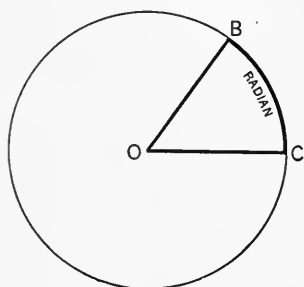


Fig. 29.

(2) *Radian measure (Circular measure).* In this system the unit of measure is the *radian*, the angle subtended at the center of a circle by an arc equal to the radius.

In Fig. 29, the arc  $BC = OC$ , hence the angle  $COB = 1$  radian. Circular measure is used almost exclusively in the theoretical work of higher mathematics.

**29. Relations between Degree and Radian Measure.** The two systems of measurement may be compared. If  $C$  = circumference,  $R$  = radius, we have

$$C = 2\pi R, \pi = 3.14159265\dots$$

\* The degree could as well be defined as the  $\frac{1}{60}$  of an angle of an equilateral triangle. In their efforts to determine direction, it is thought the ancient Babylonians used as a unit of measure the angle of an equilateral triangle; this angle was at first divided into 10 equal parts, and later into 60, which coincides with our sexagesimal system.



A circumference subtends  $360^\circ$  at the centre; if the radius be taken as the unit of measure (called a radian), we have  $360^\circ$  in angular measure equal to  $2\pi$  radians in circular measure.

$$360^\circ = 2\pi \text{ radians,}$$

$$180^\circ = \pi \text{ radians,}$$

$$1^\circ = \frac{\pi}{180} \text{ radian} = 0.0174532925199\dots \text{ radian,}$$

$$1' = 0.0002908882086\dots \text{ radian,}$$

$$1'' = 0.0000048481368\dots \text{ radian.}$$

Conversely,

$$1 \text{ radian} = \frac{180^\circ}{\pi} = 57.29577^\circ\dots = 57^\circ 17' 44.8''.$$

CONVERSION RULES. (1) *To reduce degrees to radians multiply the number of degrees by  $\frac{\pi}{180} = .01745$ , and mark the result radians.* (2) *To reduce radians to degrees multiply the number of radians by  $\frac{180}{\pi} = 57.295$ , and mark the product degrees.*

For approximations take  $\pi = \frac{22}{7}$ .

EXAMPLES. 1. Convert  $63^\circ 30'$  to radians.

$$63.5 \times 0.01745 = 1.099 \text{ radians.}$$

2. Convert  $148^\circ 20' 24''$  to radians.

$$148^\circ 20' 24'' = 148.34^\circ.$$

$$148.34 \times 0.01745 = 2.588 \text{ radians.}$$

3. Change 2.5 radians to degrees.

$$2.5 \times 57.295 = 143.239 \text{ degrees.}$$

#### EXERCISES

1. Give degree measure of  $\frac{\pi}{2}$ ;  $\frac{\pi}{3}$ ;  $\frac{\pi}{4}$ ;  $\frac{\pi}{6}$ ;  $\frac{2\pi}{3}$ ;  $\frac{3\pi}{4}$ .

2. Change from degrees to radians:  $18^\circ$ ;  $124^\circ$ ;  $290^\circ$ ;  $30^\circ$ ;  $500^\circ 45'$ .

3. Change from radian measure to degrees:  $1.5$ ;  $\frac{2}{3}$ ;  $1.65$ ;  $2.75$ ;  $-0.4$ ;  $5\frac{1}{3}$ .

4. Find the number of degrees in: (a)  $1 + \frac{\pi}{8}$ ; (b)  $1 - \frac{\pi}{6}$ ; (c)  $140^\circ - 1\frac{1}{2}$ ; (d)  $30^\circ + 2\pi$ ; (e)  $40^\circ - \frac{\pi}{10}$ ; (f)  $3 - \frac{2}{3}\pi$ .

5. What does each of the following symbols mean?

NOTE.  $n$  is any integer.

(a)  $\pm \pi$ ; (b)  $n\pi$ ; (c)  $2n\pi$ ; (d)  $n\frac{\pi}{2}$ ; (e)  $(2n+1)\frac{\pi}{2}$ ; (f)  $(2n-1)\frac{\pi}{2}$ ; (g)  $n\pi \pm \frac{\pi}{4}$ .

6. Name the quadrant in which each of the following angles terminates:

(a)  $\pi - 1$ ; (b)  $\pi + 48^\circ$ ; (c)  $240^\circ + 2$ ; (d)  $n\pi \pm \frac{\pi}{4}$ , when  $n = 0, 1, 2, 3, 4$ .

7. Determine the smallest positive angle which has the same terminal boundary as:

(a)  $440^\circ$ ; (b)  $660^\circ$ ; (c)  $378^\circ$ ; (d)  $-200^\circ$ ; (e)  $-300^\circ$ ; (f)  $\pi - 40^\circ$ ; (g)  $2\pi + 120^\circ$ .

30. **The Length of Any Arc.** In geometry it is shown that in unequal circles arcs subtending equal angles are to each other as the corresponding radii. Thus, in the figure arc  $PQ$  : arc  $AB$  ::  $OP$  :  $OA$ . Hence, if  $OA$  be taken as a unit, the arc  $AB$  is the radian measure of the angle  $AOB$ ; that is,  $AB = \theta$ ; and  $PQ = \theta \cdot OP = \theta \cdot R$ .

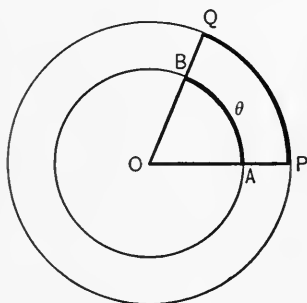


Fig. 30.

**THEOREM.** *The length of any arc equals the radius multiplied by the radian measure of the angle subtended by the arc.*

**EXAMPLES.** 1. Find the length of a  $20^\circ$  arc upon a circle of radius 27 ft.

**SOLUTION.**  $20^\circ = 20 \times \frac{\pi}{180} = \frac{\pi}{9}$  radian.

Arc of  $20^\circ = \frac{\pi}{9} \times 27$  ft. =  $3\pi$  ft. = 9.42 ft.

**NOTE.** Take  $\pi = 3\frac{1}{2}$ .

2. Find the length of an arc subtending  $135^\circ$  upon a circle whose radius is 16 in.

SOLUTION.  $135^\circ = 135 \times \frac{\pi}{180} = \frac{3}{4} \pi$  radians.

$$\text{Arc of } 135^\circ = \frac{3}{4} \pi \times 16 = 12 \pi \text{ in.} = \pi \text{ ft.}$$

3. Find the angle subtended at centre by a 6 ft. arc upon a circle whose radius is 15 ft.

SOLUTION.  $\text{Arc} = \theta \cdot R.$

$$\theta = \frac{\text{arc}}{R} = \frac{6}{15} = \frac{2}{5} \text{ radian.}$$

Hence,  $\theta$  expressed in degrees is

$$\frac{2}{5} \times 57.29^\circ = 22.91^\circ = 22^\circ 54' 36''.$$

**31. Segment and Sector Areas.** The area of a sector of a circle,  $AOB$ , equals arc  $AB$  multiplied by one half of the radius, Fig. 31.

$$\text{Sector } AOB = \frac{1}{2} \text{arc } AB \times OB = \frac{1}{2} R^2 \theta.$$

$$\begin{aligned} \text{Area of triangle } AOB &= \frac{1}{2} AB \times OD \\ &= \frac{1}{2} AE \times OB \\ &= \frac{1}{2} R^2 \sin \theta. \end{aligned}$$

Area of shaded segment

$$\begin{aligned} ADB &= \frac{1}{2} \theta R^2 - \frac{1}{2} R^2 \sin \theta \\ &= \frac{R^2}{2} (\theta - \sin \theta). \end{aligned}$$

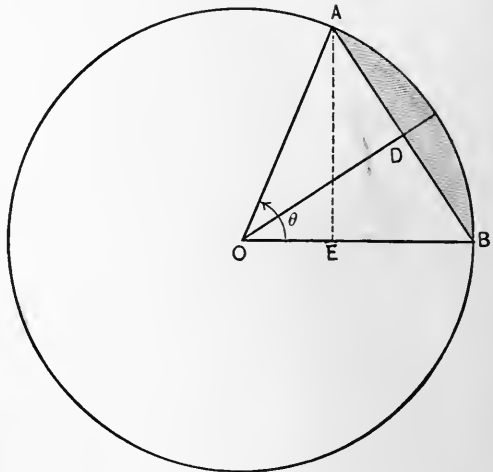


Fig. 31.

NOTE. The angle  $\theta$  is to be expressed in radian measure.

### EXERCISES

1. Find the length of an arc of  $63^\circ$  on a circle of 20-in. radius. Ans. 22 in.

NOTE. In this list of exercises, take  $\pi = \frac{22}{7}$ , except otherwise indicated.

2. Through what distance does the extremity of a 7-in. minute hand of a clock move in 10 min. ? Ans.  $3\frac{2}{3}$  in.

3. Find the radius of a circle in which a 10-ft. arc subtends an angle of 2 radians at the centre. *Ans.* 5 ft.

4. Find the angle at the centre of a circle, radius 24 in., which is subtended by an 11-in. arc. *Ans.*  $26^{\circ} 15'$ .

5. Find the area of a  $24^{\circ}$  sector whose subtending arc is 8 ft. *Ans.* 76.36 sq. ft.

6. In a circle whose radius is 10 ft., a chord is 6 ft. from the centre. Find the area of the smaller segment cut off by the chord. *Ans.* 44.73 sq. ft.

NOTE. Take radian measure from Table IV in Ex. 6, 7, 8, 9, 10, 15, 16, 17.

7. A horizontal oil tank whose length is 30 ft. and radius 4 ft. is filled to a depth of 15 in. Find the number of gallons of oil in the tank. ( $231 \text{ cu. in.} = 1 \text{ gal.}$ ) *Ans.* 1125.6 gal.

8. Find the length of a belt stretched around two pulleys whose radii are 5 ft. and  $1\frac{1}{2}$  ft., respectively, the distance between the centres of the pulleys being 20 ft. Also find the length of the belt when crossed.

*Ans.* (a) 61.03 ft.; (b) 62.55 ft.

9. Find the distance at which a foot ruler must be held so that its length will subtend one degree at the eye. *Ans.* 57.29 ft.

10. Find the length of a degree on a circle whose radius is 3956 mi. *Ans.* 69.045 mi.

11. What is the length of a degree of longitude on the 39th parallel of latitude, if one degree on the equator is 69.045 mi., the earth's radius being 3956 mi. *Ans.* 53.65 mi.

12. If  $m$  be the length of one degree upon the equator, show that the length of one degree upon any parallel of latitude is  $m \times \cos \alpha$ , when  $\alpha$  is the latitude of the parallel.

13. In radian measure two angles of a triangle are  $\frac{1}{3}$  and  $\frac{2}{5}$ . Find the third angle in degrees ( $\pi = \frac{22}{7}$ ). *Ans.*  $138^{\circ}$ .

14. The end of a 30-in. pendulum swings through a 3-in. arc. Find the angle through which it swings. *Ans.*  $5^{\circ} 43.8'$ .

15. If the diameter of the moon be 2163 mi., find the moon's distance from the earth, assuming that its diameter subtends  $31' 7''$  at the eye. See § 29. *Ans.* 238,900 mi.

16. If the sun's apparent diameter subtends an angle of  $32' 4''$  at the eye, find its diameter, assuming the sun's distance from the earth to be 92,897,000 miles. *Ans.* 866,500 mi.

17. If the earth's equatorial radius (3963 mi.) subtends  $8.8''$  at the sun (the sun's parallax), find the distance of the sun from the earth. *Ans.* 92,890,000 mi.

## CHAPTER V

### FUNCTIONS OF TWO ANGLES. MULTIPLE ANGLES

We next develop the trigonometric functions of the sum and difference of two angles.

32. To develop  $\sin(\alpha + \beta)$  and  $\cos(\alpha + \beta)$ . The angles  $\alpha$  and  $\beta$  may be both acute and such that their sum is less than  $90^\circ$ , as in Fig. 32; or they may be such that their sum is greater than  $90^\circ$  and smaller than  $180^\circ$ , as shown in Fig. 33. In each construction,  $\beta$  is made to join  $\alpha$ , the line  $PQ$  being erected perpendicular to  $OP$  and  $QN$  ( $QN'$ ), drawn perpendicular to  $OM$  at  $N$ , or to  $OM$  produced negatively at  $N'$ .

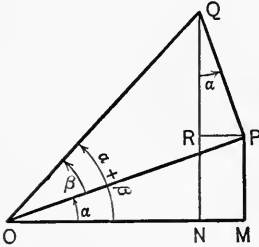


Fig. 32.

Then defining  $\sin(\alpha + \beta)$  from the figure, we have

$$\begin{aligned} \sin(\alpha + \beta) &= \frac{NQ}{OQ} = \frac{MP + RQ}{OQ} \\ &= \frac{MP}{OQ} \times \frac{OP}{OP} + \frac{QR}{OQ} \times \frac{QP}{QP} \\ &= \sin \alpha \cos \beta + \cos \alpha \sin \beta. \end{aligned}$$

Similarly,

$$\begin{aligned} \cos(\alpha + \beta) &= \frac{ON}{OQ} = \frac{OM - RP}{OQ} \\ &= \frac{OM}{OQ} \times \frac{OP}{OP} - \frac{RP}{OQ} \times \frac{QP}{QP} \\ &= \cos \alpha \cos \beta - \sin \alpha \sin \beta. \end{aligned}$$

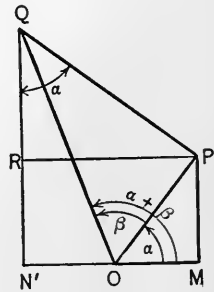


Fig. 33.

**33. To develop  $\tan(\alpha + \beta)$ .** (1) We may derive  $\tan(\alpha + \beta)$  from the drawing, thus :

$$\begin{aligned}\tan(\alpha + \beta) &= \frac{QN}{ON} = \frac{PM + QR}{OM - PR} = \frac{\frac{PM}{OM} + \frac{QR}{OM}}{1 - \frac{PR}{OM}} \\ &= \frac{\tan \alpha + \frac{PQ}{OP}}{1 - \frac{PM \cdot PQ}{OM \cdot OP}} = \frac{\tan \alpha + \tan \beta}{1 - \tan \alpha \tan \beta}.\end{aligned}$$

NOTE. The triangles  $OMP$  and  $QRP$  are similar.

(2) We may derive  $\tan(\alpha + \beta)$  analytically by dividing  $\sin(\alpha + \beta)$  by  $\cos(\alpha + \beta)$ .

$$\tan(\alpha + \beta) = \frac{\sin(\alpha + \beta)}{\cos(\alpha + \beta)} = \frac{\sin \alpha \cos \beta + \cos \alpha \sin \beta}{\cos \alpha \cos \beta - \sin \alpha \sin \beta}.$$

Dividing both numerator and denominator by  $\cos \alpha \cos \beta$ , we find

$$\tan(\alpha + \beta) = \frac{\tan \alpha + \tan \beta}{1 - \tan \alpha \tan \beta}.$$

By taking the reciprocals of  $\tan(\alpha + \beta)$ ,  $\tan \alpha$ ,  $\tan \beta$ , we have

$$\cot(\alpha + \beta) = \frac{\cot \alpha \cot \beta - 1}{\cot \alpha + \cot \beta}.$$

Since the  $\sin(-\theta) = -\sin \theta$ ,  $\cos(-\theta) = \cos \theta$ , and  $\tan(-\theta) = -\tan \theta$ , we have, on changing  $\beta$  into  $-\beta$  in each formula above:

$$\begin{aligned}\sin(\alpha - \beta) &= \sin \alpha \cos \beta - \cos \alpha \sin \beta, \\ \cos(\alpha - \beta) &= \cos \alpha \cos \beta + \sin \alpha \sin \beta, \\ \tan(\alpha - \beta) &= \frac{\tan \alpha - \tan \beta}{1 + \tan \alpha \tan \beta}.\end{aligned}$$

NOTE. The above formulas have been derived from figures in which  $\alpha + \beta$  is either acute, or lies between  $90^\circ$  and  $180^\circ$ . The same results are true for any values of  $\alpha$ ,  $\beta$ , but we shall not introduce any proof of this fact here.

**34. Important Formulas.** Collecting the results of the above demonstrations, we have the fundamental formulas:

$$(1) \quad \sin(\alpha + \beta) = \sin \alpha \cos \beta + \cos \alpha \sin \beta,$$

$$(2) \quad \cos(\alpha + \beta) = \cos \alpha \cos \beta - \sin \alpha \sin \beta,$$

$$(3) \quad \sin(\alpha - \beta) = \sin \alpha \cos \beta - \cos \alpha \sin \beta,$$

$$(4) \quad \cos(\alpha - \beta) = \cos \alpha \cos \beta + \sin \alpha \sin \beta,$$

$$(5) \quad \tan(\alpha + \beta) = \frac{\tan \alpha + \tan \beta}{1 - \tan \alpha \tan \beta},$$

$$(6) \quad \tan(\alpha - \beta) = \frac{\tan \alpha - \tan \beta}{1 + \tan \alpha \tan \beta},$$

$$(7) \quad \cot(\alpha \pm \beta) = \frac{\pm \cot \alpha \cot \beta - 1}{\cot \alpha \pm \cot \beta}.$$

#### EXERCISES

1. Show  $\sin 75^\circ = \sin(45^\circ + 30^\circ) = \frac{1}{4}(\sqrt{6} + \sqrt{2})$ .

SOLUTION.  $\sin(45^\circ + 30^\circ) = \sin 45^\circ \cos 30^\circ + \cos 45^\circ \sin 30^\circ$

$$= \frac{\sqrt{2}}{2} \cdot \frac{\sqrt{3}}{2} + \frac{\sqrt{2}}{2} \cdot \frac{1}{2}$$

Hence,  $\sin 75^\circ = \cos 15^\circ = \frac{1}{4}(\sqrt{6} + \sqrt{2})$ .

2. Show  $\sin 15^\circ = \frac{1}{4}(\sqrt{6} - \sqrt{2}) = \cos 75^\circ$ .

3. Show  $\tan 75^\circ = 2 + \sqrt{3} = \cot 15^\circ$ .

4. Show  $\tan 15^\circ = 2 - \sqrt{3} = \cot 75^\circ$ .

5. Show  $\sin(45^\circ + \alpha) = \frac{\sqrt{2}}{2}(\cos \alpha + \sin \alpha)$ .

NOTE. Apply formula (1).

6. Prove  $\cos(30^\circ - \alpha) = \frac{1}{2}(\sqrt{3} \cos \alpha + \sin \alpha)$ .

7. Prove  $\tan(45^\circ + x) = \frac{1 + \tan x}{1 - \tan x} = \cot(45^\circ - x)$ .

8. Prove  $\frac{\sqrt{3}}{2} \cos x - \frac{1}{2} \sin x = \sin(60^\circ - x)$ .

9. Prove  $\frac{1}{2} \cos x + \frac{\sqrt{3}}{2} \sin x = \cos(60^\circ - x)$ .

10. Prove  $\tan(60^\circ - x) = \frac{\sqrt{3} - \tan x}{1 + \sqrt{3} \tan x}$ .



11. Derive the formula  $\sin(\alpha + \beta + \gamma) = \sin \alpha \cos \beta \cos \gamma + \cos \alpha \sin \beta \cos \gamma + \cos \alpha \cos \beta \sin \gamma - \sin \alpha \sin \beta \sin \gamma$ .

SUGGESTION. Write  $\sin(\alpha + \beta + \gamma) = \sin(\alpha + [\beta + \gamma])$ , and apply (1).

12. Derive  $\cos(\alpha + \beta + \gamma) = \cos \alpha \cos \beta \cos \gamma - \cos \alpha \sin \beta \sin \gamma - \cos \beta \sin \alpha \sin \gamma - \cos \gamma \sin \alpha \sin \beta$ .

13. Derive  $\tan(x + y + z)$

$$= \frac{\tan x + \tan y + \tan z - \tan x \tan y \tan z}{1 - \tan x \tan y - \tan y \tan z - \tan z \tan x}$$

14. If  $\sin x = 0.5$  and  $\cos y = 0.6$ , find the value of  $\sin(x + y)$ , and  $\cos(x + y)$ .

SUGGESTION. Construct angles  $x, y$ , and expand  $\sin(x + y)$ , then substitute. Likewise with  $\cos(x + y)$ .

$$\begin{aligned} \sin(x + y) &= \sin x \cos y + \cos x \sin y \\ &= 0.5 \times 0.6 + 0.5\sqrt{3} \times 0.8 = \frac{\sqrt{3}}{10}(\sqrt{3} + 4). \end{aligned}$$

$$\begin{aligned} \cos(x + y) &= \cos x \cos y - \sin x \sin y \\ &= 0.5\sqrt{3} \times 0.6 - 0.5 \times 0.8 = \frac{\sqrt{3}}{10}(\sqrt{3} - 4). \end{aligned}$$

15. If  $\sin x = 0.8$ ,  $\tan y = 1$ , what value has  $\sin(x - y)$ ?  $\tan(x + y)$ ?

16. When  $\tan x = \sqrt{3}$ ,  $\cos y = 0.5$ , find  $\tan(x - y)$ ; also  $\cos(x - y)$ .

17. When  $\cos x = 1$ ,  $\tan y = 1$ , find  $\sin(x + y)$ ; also  $\cot(x + y)$ .

18. Show  $\cos(x + y) = 0$ , when  $\tan x = 0.5$  and  $\cot y = 0.5$ .

19. Show  $\sin(x + y) = 1$ , when  $\sin x = \cos y$ .

20. Show  $\tan(x + y) = \infty$ , when  $\cos x = \sin y$ , or  $\tan x = \cot y$ .

### FUNCTIONS OF MULTIPLE AND SUB-MULTIPLE ANGLES

The formulas enumerated in § 34 give rise to new and important results by making angle  $\beta$  equal to angle  $\alpha$ .

35. Functions of  $2\alpha$ . In the formulas,

(1)  $\sin(\alpha + \beta) = \sin \alpha \cos \beta + \cos \alpha \sin \beta$ ,

(3)  $\cos(\alpha + \beta) = \cos \alpha \cos \beta - \sin \alpha \sin \beta$ ,

(5)  $\tan(\alpha + \beta) = \frac{\tan \alpha + \tan \beta}{1 - \tan \alpha \tan \beta}$ ,

let  $\beta = \alpha$ , and we derive :

$$(7) \quad \sin 2\alpha = 2 \sin \alpha \cos \alpha,$$

$$(8) \quad \cos 2\alpha = \cos^2 \alpha - \sin^2 \alpha = 2 \cos^2 \alpha - 1 = 1 - 2 \sin^2 \alpha,$$

$$(9) \quad \tan 2\alpha = \frac{2 \tan \alpha}{1 - \tan^2 \alpha}.$$

### 36. Functions of $3\alpha$ .

Let  $\beta = 2\alpha$  in (1), (3), (5) above, and employ results of (7), (8), (9), and we obtain:

$$(10) \quad \sin 3\alpha = 3 \sin \alpha - 4 \sin^3 \alpha,$$

$$(11) \quad \cos 3\alpha = 4 \cos^3 \alpha - 3 \cos \alpha,$$

$$(12) \quad \tan 3\alpha = \frac{3 \tan \alpha - \tan^3 \alpha}{1 - 3 \tan^2 \alpha}.$$

**37. Half-angle Formulas.** In (7), (8), (9) § 35, let  $\alpha = \frac{x}{2}$ , and we find :

$$(13) \quad \sin x = 2 \sin \frac{x}{2} \cos \frac{x}{2},$$

$$(14) \quad \cos x = \cos^2 \frac{x}{2} - \sin^2 \frac{x}{2} = 2 \cos^2 \frac{x}{2} - 1 = 1 - 2 \sin^2 \frac{x}{2},$$

$$(15) \quad \tan x = \frac{2 \tan \frac{x}{2}}{1 - \tan^2 \frac{x}{2}}.$$

Solving each of the latter two values of  $\cos x$  for  $\sin \frac{x}{2}$  and  $\cos \frac{x}{2}$ , we have the important formulas :

$$(16) \quad \sin \frac{x}{2} = \sqrt{\frac{1 - \cos x}{2}},$$

$$(17) \quad \cos \frac{x}{2} = \sqrt{\frac{1 + \cos x}{2}},$$

and dividing  $\sin \frac{x}{2}$  by  $\cos \frac{x}{2}$ ,

$$(18) \quad \tan \frac{x}{2} = \sqrt{\frac{1 - \cos x}{1 + \cos x}} = \frac{\sin x}{1 + \cos x} = \frac{1 - \cos x}{\sin x}.$$

(16), (17), (18) are known as the half-angle formulas.

## EXERCISES

1. If  $\sin x = \frac{3}{5}$ , find  $\sin 2x$ ; also  $\tan 2x$ .
2. If  $\cos x = \frac{5}{13}$ , find  $\tan 2x$ ; also  $\cos 2x$ .
3. If  $\csc x = 2$ , find  $\sin 2x$ ; also  $\cos 2x$ .
4. Find  $\sin x$ , if  $\cos \frac{x}{2} = 0.3$ .
5. Find  $\tan x$ , if  $\sin \frac{x}{2} = \frac{5}{13}$ .
6. Find  $\sin x$ , if  $\cos 2x = \frac{\sqrt{3}}{2}$ .
7. Find  $\tan x$ , if  $\sin 2x = \frac{12}{13}$ .
8. Find  $\tan 60^\circ$ , knowing  $\tan 30^\circ = \frac{1}{3}\sqrt{3}$ .
9. Find  $\tan 53^\circ 8'$ , if  $\tan 26^\circ 34' = 0.5$ .
10. Find  $\cos 2x$ , if  $\sec x = \frac{3}{2}$ .
11. If  $\sin a = 0.4$ , find  $\sin 3a$ .
12. When  $\tan a = 0.1$ , find  $\tan 3a$ .
13. Find  $\sin 22\frac{1}{2}^\circ$  and  $\cos 22\frac{1}{2}^\circ$  from the functions of  $45^\circ$ .
14. Find  $\tan 15^\circ$  from the functions of  $30^\circ$ .
15. Find the  $\sin 67\frac{1}{2}^\circ$  from the functions of  $22\frac{1}{2}^\circ$ .

Verify the following identities:

$$16. (\sin x \pm \cos x)^2 = 1 \pm \sin 2x.$$

$$17. \cos^4 x - \sin^4 x = \cos 2x.$$

$$18. \sin x = \frac{2 \tan \frac{x}{2}}{1 + \tan^2 \frac{x}{2}} \quad 19. \cos x = \frac{1 - \tan^2 \frac{x}{2}}{1 + \tan^2 \frac{x}{2}}$$

$$20. 2 \sin x + \sin 2x = \frac{2 \sin^3 x}{1 - \cos x}.$$

$$21. \tan x + \cot x = 2 \csc 2x.$$

$$22. \tan \left( \frac{\pi}{4} + \frac{x}{2} \right) = \sec x + \tan x.$$

$$23. \cot x - \tan x = 2 \cot 2x.$$

24.  $\frac{\sin 2x}{\cot x} = 1 - \cos 2x.$       26.  $\sin \frac{x}{2} = \sqrt{\frac{\text{vers } x}{2}}.$
25.  $\frac{\sin 3x}{\sin x} = 1 + 2 \cos 2x.$       27.  $\tan \frac{x}{2} = \frac{1 + \sin x - \cos x}{1 + \sin x + \cos x}.$
28.  $\sin 4\theta = 4 \sin \theta \cos \theta (\cos^2 \theta - \sin^2 \theta)$   
 $= 8 \cos^3 \theta \sin \theta - 4 \cos \theta \sin \theta.$
29.  $\cos 4\theta = 8 \cos^4 \theta - 8 \cos^2 \theta + 1.$
30. When  $\sin 3\theta - \sin 6\theta = 0$ , show  $\cos 3\theta = \frac{1}{2}.$
31.  $\sin 5\theta = 16 \sin^5 \theta - 20 \sin^3 \theta + 5 \sin \theta.$
32.  $\cos 5\theta = 16 \cos^5 \theta - 20 \cos^3 \theta + 5 \cos \theta.$
33.  $\sin^2 A - \sin^2 B = \sin(A+B) \sin(A-B).$
34.  $\cos^2 A - \cos^2 B = \sin(A+B) \sin(B-A).$
35.  $\cos^2 A - \sin^2 B = \cos(A+B) \cos(A-B).$
36.  $\sin \frac{\theta}{2} + \cos \frac{\theta}{2} = \pm \sqrt{1 + \sin \theta}.$
37.  $\sin \frac{\theta}{2} - \cos \frac{\theta}{2} = \pm \sqrt{1 - \sin \theta}.$

(Explain use of double sign in 36, 37.)

### SUM AND DIFFERENCE FORMULAS

38. Converting to Products. Taking the results (1), (2), (3), (4), § 34,

$$\begin{aligned}\sin(\alpha + \beta) &= \sin \alpha \cos \beta + \cos \alpha \sin \beta, \\ \sin(\alpha - \beta) &= \sin \alpha \cos \beta - \cos \alpha \sin \beta, \\ \cos(\alpha + \beta) &= \cos \alpha \cos \beta - \sin \alpha \sin \beta, \\ \cos(\alpha - \beta) &= \cos \alpha \cos \beta + \sin \alpha \sin \beta,\end{aligned}$$

we have on adding and subtracting:

$$\left. \begin{aligned}\sin(\alpha + \beta) + \sin(\alpha - \beta) &= 2 \sin \alpha \cos \beta, \\ \sin(\alpha + \beta) - \sin(\alpha - \beta) &= 2 \cos \alpha \sin \beta, \\ \cos(\alpha + \beta) + \cos(\alpha - \beta) &= 2 \cos \alpha \cos \beta, \\ \cos(\alpha + \beta) - \cos(\alpha - \beta) &= -2 \sin \alpha \sin \beta.\end{aligned}\right\} \quad (I)$$

Let  $\alpha + \beta = X$ ,  $\alpha - \beta = Y$ , then

$$\alpha = \frac{X+Y}{2}, \quad \beta = \frac{X-Y}{2}.$$

Making these substitutions, we have :

$$(19) \quad \sin X + \sin Y = 2 \sin \frac{X+Y}{2} \cos \frac{X-Y}{2},$$

$$(20) \quad \sin X - \sin Y = 2 \cos \frac{X+Y}{2} \sin \frac{X-Y}{2},$$

$$(21) \quad \cos X + \cos Y = 2 \cos \frac{X+Y}{2} \cos \frac{X-Y}{2},$$

$$(22) \quad \cos X - \cos Y = -2 \sin \frac{X+Y}{2} \sin \frac{X-Y}{2}.$$

These formulas should be remembered as *the sum of two sines equals twice the sine of the half sum, times the cosine of the half difference*, and so on for the remaining formulas. Formulas (19)–(22) are the so-called *Sum and Difference Formulas*; when read forward they convert a sum or difference of two sines or cosines into a product; when read backwards they convert a product of two sines or cosines into a sum or difference.

**39. Converting to Sum or Difference.** The formulas (19), (20), (21), (22) should be recognized when read conversely. Writing formulas (I), § 38, conversely, and replacing  $\alpha$  by  $A$ ,  $\beta$  by  $B$ , we have :

$$(19') \quad 2 \sin A \cos B = \sin (A + B) + \sin (A - B),$$

$$(20') \quad 2 \cos A \sin B = \sin (A + B) - \sin (A - B),$$

$$(21') \quad 2 \cos A \cos B = \cos (A + B) + \cos (A - B),$$

$$(22') \quad 2 \sin A \sin B = \cos (A - B) - \cos (A + B),$$

a set of important relations which should be recognized.

#### EXERCISES

Read the following exercises, applying the sum and difference formulas, reducing answers :

1.  $\sin 10^\circ + \sin 40^\circ =$

8.  $\sin (-10^\circ) + \sin 40^\circ =$

2.  $\sin 80^\circ + \sin 30^\circ =$

9.  $\cos 80^\circ - \cos (-20^\circ) =$

3.  $\cos 60^\circ + \cos 40^\circ =$

10.  $\cos \frac{\pi}{6} + \cos \frac{\pi}{3} =$

4.  $\sin 70^\circ - \sin 40^\circ =$

11.  $\sin 4\theta + \sin 3\theta =$

5.  $\cos 28^\circ + \cos 42^\circ =$

6.  $\cos 28^\circ - \cos 42^\circ =$

12.  $\sin 3\theta - \sin \theta =$

7.  $\sin 35^\circ + \cos 25^\circ =$

$$13. \cos(n+1)\theta - \cos(n-1)\theta =$$

$$14. \sin(n+1)\frac{\pi}{4} - \sin(n-1)\frac{\pi}{4} =$$

Express as a sum or difference:

$$15. 2 \sin 40^\circ \cos 20^\circ =$$

$$18. 2 \cos 60^\circ \cos 10^\circ =$$

$$16. 2 \cos 50^\circ \sin 40^\circ =$$

$$19. 2 \sin \frac{\pi}{4} \cos \frac{3\pi}{4} =$$

$$17. 2 \sin 20^\circ \sin 40^\circ =$$

$$20. 2 \sin(n\theta) \cos(n-1)\theta =$$

Prove the following identities:

$$21. \frac{\sin 2x + \sin 2y}{\sin 2x - \sin 2y} = \frac{\tan(x+y)}{\tan(x-y)}$$

$$22. \frac{\cos 3x - \cos 5x}{\sin 3x + \sin 5x} = \tan x.$$

$$23. \frac{\sin x + \sin y}{\cos x + \cos y} = \tan \frac{(x+y)}{2}.$$

$$24. \frac{\sin 9x + \sin x}{\cos 9x + \cos x} = \tan 5x.$$

$$25. \frac{\sin x + \sin y}{\sin x - \sin y} = \frac{\tan \frac{x+y}{2}}{\tan \frac{x-y}{2}}.$$

$$26. \frac{\cos x - \cos y}{\cos x + \cos y} = -\tan \frac{x+y}{2} \tan \frac{x-y}{2}.$$

$$27. \sin\left(x + \frac{\pi}{3}\right) + \sin\left(x - \frac{\pi}{3}\right) = \sin x.$$

$$28. \sin(30^\circ + A) + \sin(30^\circ - A) = \cos A.$$

$$29. \cos\left(\frac{\pi}{3} + A\right) + \cos\left(\frac{\pi}{3} - A\right) = \cos A.$$

$$30. \frac{\sin(n-2)x + \sin(nx)}{\cos(n-2)x - \cos(nx)} = \cot x.$$

$$31. 2 \sin\left(x + \frac{\pi}{4}\right) \sin\left(x - \frac{\pi}{4}\right) = \sin^2 x - \cos^2 x.$$

$$32. \cos x + \cos 3x + \cos 5x + \cos 7x = 4 \cos x \cos 2x \cos 4x.$$

$$33. \sin x + \sin 3x + \sin 5x + \sin 7x = 4 \cos x \cos 2x \sin 4x.$$

$$34. \sin \theta + \sin \phi + \sin (\theta + \phi) = 4 \cos \frac{\theta}{2} \cos \frac{\phi}{2} \sin \frac{\theta + \phi}{2}.$$

$$35. \sin \theta + \sin \phi - \sin (\theta + \phi) = 4 \sin \frac{\theta}{2} \sin \frac{\phi}{2} \sin \frac{\theta + \phi}{2}.$$

$$36. \frac{\sin \theta + \sin \phi + \sin \psi - \sin (\theta + \phi + \psi)}{\cos \theta + \cos \phi + \cos \psi + \cos (\theta + \psi + \phi)} \\ = \tan \frac{\theta + \phi}{2} \tan \frac{\phi + \psi}{2} \tan \frac{\psi + \theta}{2}.$$

When  $A + B + C = 180^\circ$ , prove :

$$37. \sin A + \sin B + \sin C = 4 \cos \frac{A}{2} \cos \frac{B}{2} \cos \frac{C}{2}.$$

$$38. \sin A + \sin B - \sin C = 4 \sin \frac{A}{2} \sin \frac{B}{2} \cos \frac{C}{2}.$$

$$39. \cos A + \cos B + \cos C = 1 + 4 \sin \frac{A}{2} \sin \frac{B}{2} \sin \frac{C}{2}.$$

$$40. \cos A + \cos B - \cos C = -1 + 4 \cos \frac{A}{2} \cos \frac{B}{2} \sin \frac{C}{2}.$$

$$41. \tan A + \tan B + \tan C = \tan A \tan B \tan C.$$

$$42. \text{ Show } \frac{\sin (x + y)}{\cos (x - y)} = \frac{\cot x + \cot y}{1 + \cot x \cot y}.$$

$$43. \text{ Show } \frac{\tan x + \tan y}{\tan x - \tan y} = \frac{\sin (x + y)}{\sin (x - y)}.$$

$$44. \text{ Show } \frac{\tan 5x - \tan 3x}{1 + \tan 5x \tan 3x} = \frac{\tan 3x - \tan x}{1 + \tan 3x \tan x}.$$

45. Prove that in a given circle the area of a regular inscribed pentagon is to the area of a regular inscribed decagon as  $\cos 36^\circ$  is to 1.

Review next two chapters  
 on Tuesday April 20, 1912.

## CHAPTER VI

### LOGARITHMS

Calculations involving multiplication, division, raising to powers, and extracting roots may become quite laborious when performed in the ordinary way. To abbreviate the work of numerical calculation certain tables known as *Logarithmic Tables of Numbers* and of the *Trigonometric Functions* have been prepared. The use of such tables will now be explained.

**40. The Index Laws.** Let it be required to find an approximate value of the fraction

$$F = \frac{25 \times 78.6 \times \tan 65^\circ}{658.4 \times 4.75}$$

Since  $10^1 = 10$  and  $10^2 = 100$ , we may approximate a number between 1 and 2 which, when used as an exponent of 10, will produce 25. This exponent is approximately 1.39794. The number 10 may be affected by an exponent which will produce any one of the numbers in the fraction  $F$ .

We write the above fraction in exponential form thus :

$$\begin{aligned} F &= \frac{25 \times 78.6 \times \tan 65^\circ}{658.4 \times 4.75} = \frac{10^{1.39794} \times 10^{1.89542} \times 10^{0.33133}}{10^{2.81849} \times 10^{0.67669}} \\ &= \frac{10^{1.39794+1.89542+0.33133}}{10^{2.81849+0.67669}} \\ &= \frac{10^{3.62469}}{10^{3.49518}} = 10^{3.62469-3.49518} \\ &= 10^{0.12951}. \end{aligned}$$

This final result will evidently be a number smaller than 10 since the exponent is less than unity ; its approximate value is

$$F = 1.3474.$$

Thus, the operations of multiplication have been replaced by addition, and the operation of division has been performed by subtraction.



The exponents of 10 in this illustration obey the *index laws* of elementary algebra, viz. (1) the exponent of a product equals the *sum* of the exponents, (2) the exponent of a quotient equals the *difference* of the exponents (the exponent of the denominator subtracted from that of the numerator). To these two laws we attach a third, illustrated by

$$25^2 = (10^{1.39794})^2 = 10^{2.79588} = 625.$$

These three *index laws* are expressed by formula thus:

- (1)  $a^x \times a^y = a^{x+y},$   
 (2)  $a^x \div a^y = a^{x-y},$   
 (3)  $(a^x)^m = a^{mx}.$

#### 41. Definition of Logarithms.\*

(1) COMMON LOGARITHMS. *The logarithm of a number N to the base 10 is the exponent by which 10 must be affected to produce the number N.* Logarithms constructed upon 10 as a base are called *Common logarithms* (Briggian logarithms).

As illustrations of logarithmic notation,

$$\begin{aligned} 25 &= 10^{1.39794}, & \log 25 &= 1.39794, \\ 78.6 &= 10^{1.89542}, & \log 78.6 &= 1.89542, \\ \tan 65^\circ &= 10^{0.33133}, & \log \tan 65^\circ &= 0.33133. \end{aligned}$$

(2) LOGARITHMS TO ANY BASE. If we write

$$a^x = N,$$

we define  $x =$  the logarithm of  $N$  to base  $a$ ,

or more briefly  $\log_a N = x.$

*The logarithm of a number N to base a is the exponent by which a must be affected to produce N.*

\* Logarithm = ratio number. Logarithms were invented by John Napier (1550-1617), a native of Scotland. To his system of logarithms, published 1614, he applied the name *artificial numbers*. Napier's system of logarithms was not constructed upon 10 as a base. Henry Briggs (1556-1631), professor in Gresham College, London, first used 10 as a base (1617), and thus constructed a system adapted to the ordinary decimal notation. The tables first published by Briggs were constructed to 14 decimal places. Tables in ordinary use are constructed to *seven, six, five or even four decimals*. Greater degrees of accuracy will be obtained by using tables with greater numbers of decimals. The ordinary logarithms of the trigonometric functions were first constructed by Gunter, 1620.

EXAMPLES. 1. If the base is 5, what is  $\log_5 25$ ,  $\log_5 125$ ,  $\log_5(0.2)$ ,  $\log_5(0.04)$ ? *Ans.* 2, 3, -1, -2.

2. With 8 as base, what is  $\log_8 64$ ,  $\log_8(\frac{1}{8})$ ,  $\log_8 4$ ,  $\log_8 16$ ,  $\log_8 32$ ,  $\log_8 128$ ? *Ans.* 2, -1,  $\frac{2}{3}$ ,  $\frac{4}{3}$ ,  $\frac{5}{3}$ ,  $\frac{7}{3}$ .

3. With 10 as base,  $\log 2 = 0.30103$ ,  $\log 3 = 0.47712$ ,  $\log 5 = 0.69897$ . Find  $\log 4$ ,  $\log 6$ ,  $\log 9$ ,  $\log 12$ ,  $\log 15$ ,  $\log 18$ ,  $\log 20$ .

*Ans.* 0.60206, 0.77815, 0.95424, 1.07918, 1.17609, 1.25527, 1.30103.

4. From example 3 above find  $\log(\frac{9}{4})$ ,  $\log(\frac{15}{2})$ ,  $\log 1.5$ ,  $\log 1.2$ . *Ans.* 0.35218, 0.87506, 0.17609, 0.07918.

5. With 16 as base, what numbers correspond to the following logarithms: 2,  $\frac{1}{2}$ ,  $\frac{3}{2}$ ,  $\frac{1}{4}$ ,  $-\frac{1}{2}$ ,  $-\frac{3}{4}$ ? *Ans.* 256, 4, 64, 2,  $\frac{1}{4}$ ,  $\frac{1}{8}$ .

**42. Systems of Logarithms.** Any number (excluding 0 and 1) may be taken as a base for a logarithmic system. Two bases are in use, 10 and  $e$ , where  $e$  is defined by

$$e = 1 + \frac{1}{1} + \frac{1}{1 \cdot 2} + \frac{1}{1 \cdot 2 \cdot 3} + \frac{1}{1 \cdot 2 \cdot 3 \cdot 4} + \dots = 2.71828182\dots$$

Logarithms constructed with 10 as base are called *common logarithms* or *Briggian logarithms*. This system is adapted to all ordinary numerical calculations.

Logarithms constructed with  $e$  as base are called *natural logarithms*, or *Napierian logarithms*, or *hyperbolic logarithms*. This system is used in the theoretical work of higher mathematics. Tables of logarithms constructed to the base 10 will be found in the Tables compiled at the end of this book.

**43. Laws Governing the Use of Logarithms.** The interpretation of the Index Laws into logarithmic form furnishes the necessary rules for performing multiplication, division, raising to powers, and extracting roots by means of logarithms.

I. LAW OF PRODUCTS. *The logarithm of a product equals the sum of the logarithms of the factors.*

For, let  $a^x = N$ ,  $a^y = M$ ,  
then  $x = \log_a N$ ,  $y = \log_a M$ .

Also,  $N \times M = a^x \times a^y = a^{x+y}$ ,  
 $\log_a(N \times M) = x + y = \log_a N + \log_a M$ ,

which establishes the law.

EXAMPLE.  $\log_{10}(67 \times 126) = \log_{10} 67 + \log_{10} 126$   
 $= 1.82607 + 2.10037 = 3.92644.$

II. LAW OF QUOTIENTS. *The logarithm of a quotient equals the logarithm of the numerator diminished by the logarithm of the denominator.*

For, let  $a^x = N, a^y = M,$   
 then  $N \div M = a^x \div a^y = a^{x-y}.$

In logarithmic form

$$\log_a \left( \frac{N}{M} \right) = x - y = \log_a N - \log_a M.$$

EXAMPLE.  $\log_{10}(184 \div 1.56) = \log_{10} 184 - \log_{10} 1.56$   
 $= 2.26482 - 0.19312 = 2.07170.$

III. LAW OF POWERS (ROOTS). *The logarithm of  $N^n$  equals  $n$  times the logarithm of  $N$ .* This law is true for any value of the exponent  $n$ , whether positive or negative, integer or fraction.

Let  $a^x = N, x = \log_a N;$   
 then, by the third index law,

$$(a^x)^n = a^{nx} = N^n.$$

In logarithmic notation,

$$\log_a (N^n) = nx = n \cdot \log_a N.$$

EXAMPLES.  $\log 507^3 = 3 \log 507,$   
 $\log (148)^{\frac{1}{2}} = \frac{1}{2} \log 148,$   
 $\log (576)^{\frac{2}{3}} = \frac{2}{3} \log 576.$

44. Characteristic and Mantissa. From the table

$$\begin{aligned} 10^4 &= 10000 \\ 10^3 &= 1000 \\ 10^2 &= 100 \\ 10^1 &= 10 \\ 10^0 &= 1 \\ 10^{-1} &= .1 \\ 10^{-2} &= .01 \end{aligned}$$

it is obvious that the logarithm of an integral power of 10 is an integer, either positive or negative. The logarithms of numbers between 1 and 10 are evidently between 0 and 1, logarithms of numbers between 10 and 100 are between 1 and 2, and so on. For example,  $\log 8 = 0.90309$ ,  $\log 80 = 1.90309$ ,  $\log 800 = 2.90309$ ,  $\log 8000 = 3.90309$ .

*The integral part of a logarithm is called the characteristic; the decimal part of the logarithm is called the mantissa.*

I. LAW OF THE CHARACTERISTIC. From the above example, it is seen that  $\log 8$  has a characteristic 0,  $\log 80$  has 1,  $\log 800$  has 2, and so on. From this illustration, we see that *the characteristic of a logarithm of a whole number is one less than the number of digits in the number.*

Dividing a number by 10 reduces the characteristic by 1; dividing by 100 reduces its characteristic by 2, and so on. Hence, for a pure decimal, as .00567, *the characteristic is negative and equal to the number of places which the first significant figure occupies to the right of the decimal point.* Thus,

$$\log 0.00567 = -3 + .75358,$$

$$\log 0.0258 = -2 + .41162.$$

In such cases, the characteristic is negative, while the mantissa is positive. The usual notation is to place a negative sign (−) over the characteristic, leaving the form for the above illustrations thus:

$$\log 0.00567 = \bar{3}.75358,$$

$$\log 0.0258 = \bar{2}.41162.$$

II. LAW OF THE MANTISSA. *The mantissa is the same for any given sequence of digits, whatever may be the position of the decimal point.*

For example,  $\log 4896 = 3.68984$ ,  $\log 48.96 = 1.68984$ ,  $\log 4.896 = 0.68984$ ,  $\log 0.04896 = \bar{2}.68984$ .

Logarithmic tables as usually constructed show only the mantissa. The characteristic is to be supplied according to Rule I.

**45. Use of Tables. Tabulation of Logarithmic Work.** (1) *To find the logarithm of a number.* Let us find the logarithm of a number of five figures.

Take for example  $\log 58769$ .

(a) The characteristic is 4.

(b) Look in column marked *N*, of the Tables, for the first three digits 587; follow the horizontal row opposite 587 to the right to column 6 at top, and we find the mantissa .76908.

(c) The correction for the last figure 9 is approximately .9 of the difference between the mantissa for 5876 and that for 5877, *i.e.*  $.9 \times 8 = 7.2$ . Hence, add 7 to the last figure of the mantissa already found.

$$\log 58769 = 4.76915.$$

(d) In the margin, the tabular differences between any two successive mantissas are indicated; on this page these differences are 7 and 8. The corrections for 1, 2, 3, ..., 9 are indicated in the columns under the 8 and 7, respectively.

(2) *To find the number corresponding to a logarithm.* A number whose logarithm is given is found by reversing the above process.

Required the number corresponding to the logarithm 2.57682.

$$\log N = 2.57682.$$

(a) In the logarithmic tables find the mantissa next smaller than .57682. This is .57680, leaving a difference 2.

(b) The digits in column *N* and at top of column in which .57680 is found are 3774.

(c) The difference between .57680 and the next tabular number is 12.

(d) In proportional parts column, under 12, the nearest number to proportional part 2 is 2.

(e) Hence,  $N = 3774.2$ , the decimal point falling between 7 and 4, since the characteristic is 2.

(3) *To find the logarithm of trigonometric functions.*

(1) To illustrate, let us find the  $\log \sin 37^\circ 48' 15''$ .

(a) Sines and cosines are less than unity; hence, the characteristic in each case is negative. To avoid negative characteristics in the tables, 10 is added and subtracted.

(b)  $\log \sin 37^\circ 48' = 9.78739 - 10$ . Correction for  $15'' = 4$ . Hence,  
 $\log \sin 37^\circ 48' 15'' = 9.78743 - 10$ .

(c) The tabular difference is found in column marked *d*, and proportional corrections for  $6''$ ,  $7''$ ,  $8''$ ,  $9''$ ,  $10''$ ,  $20''$ ,  $30''$ ,  $40''$ ,  $50''$  are indicated in the margin under proportional parts.

(2) Find  $\log \cos 49^\circ 21' 30''$ .

(a) The  $\log \cos 49^\circ 21'$  is found by looking at bottom of page 69, reading up the column marked  $\log \cos$  and taking the minutes,  $21'$ , from the column to right of the page.

$$\log \cos 49^\circ 21' = 9.81387 - 10.$$

(b) Since the cosine decreases as the angle increases, the correction for  $30''$  must be subtracted.

Correction  $30'' = 7.5$  (count as 8); see Prop. Pts. under 15.

(c) Hence,  $\log \cos 49^\circ 21' 30'' = 9.81379 - 10$ .

The use of the tables in finding logarithms of tangents and cotangents is similar to that explained for sines and cosines.

### TABULATION OF WORK

In the work of computation by means of logarithms it is very important that the computer should economize in both time and labor. To accomplish this purpose the beginner should (1) make himself familiar with the mechanical construction of the logarithmic tables, especially the devices of marginal corrections, and (2) he should adopt and systematically carry out some convenient plan of tabulation of his work.

A plan of tabulation is suggested in the following examples.

EXAMPLES. 1. Find by means of logarithms the value of  $F = \frac{a \times b \times \tan a}{c \times d}$ , where  $a = 25$ ,  $b = 78.6$ ,  $c = 658.4$ ,  $d = 4.75$ , and  $a = 65^\circ$ .

Let the numerator be called  $N$ , the denominator  $D$ . Then we may tabulate as follows:

<i>Data and Results</i>	<i>Logarithms</i>
$a$ 25	log $a$ 1.39794
$b$ 78.6	log $b$ 1.89542
$a$ $65^\circ$	log $\tan a$ 0.33133
$c$ 658.4	log $N$ 3.62469
$d$ 4.75	log $c$ 2.81849
$F$ 1.3474	log $d$ 0.67669
	log $D$ 3.49518
	log $F$ 0.12951

} add

} add

} subtract

2. Find  $F = \frac{a \sin \alpha}{b \tan \beta}$ , where  $a = 4694.5$ ,  $b = 37.6$ ,  $\alpha = 67^\circ 20' 15''$  and  $\beta = 70^\circ 41' 10''$ .

*Data and Results*

*Logarithms*

$a$	4694.5	$\log a$	3.67154
$\alpha$	67° 20' 15"		5 correction
$b$	37.6	$\log \sin \alpha$	9.96509 - 10
$\beta$	70° 41' 10"		1 correction
$F$	40.377	$\log a \sin \alpha$	13.63669 - 10
		$\log b$	1.57519
		$\log \tan \beta$	0.45529
			6.7 correction
		$\log b \tan \beta$	2.03055
		$\log F$	1.60614

**46. Conversion of Common to Napierian Logarithms.** Logarithms of one system may easily be converted into logarithms of another system. Let us consider the systems to base 10 and  $e$ . Let

$$10^y = N, \text{ then } y = \log_{10} N.$$

Take logarithm to base  $e$  of both members of  $10^y = N$ .

$$y \log_e 10 = \log_e N,$$

or  $\log_{10} N \cdot \log_e 10 = \log_e N.$

Now,  $\log_e 10 = 2.302585$ ; hence,

(1)  $\log_e N = 2.302585 \times \log_{10} N,$

(2)  $\log_{10} N = \frac{1}{2.302585} \times \log_e N = 0.434294 \times \log_e N.$

EXERCISES IN USE OF LOGARITHMS

By means of logarithms find the value of each of the following:

✓ 1.  $Q = \frac{78.54 \times 9.6752}{8.269}$ . Ans. 91.896.

✓ 2.  $Q = \frac{(104.6)^{\frac{1}{2}} \times 0.2536}{(5.87)^{\frac{1}{2}}}$ . Ans. 0.49319.

✓ 3.

Thursday Mar 28.

$$3. \quad Q = \frac{(1848)^{\frac{2}{3}} \times 10^{-2}}{0.7854}. \quad \text{Ans. } 1.9174.$$

$$4. \quad Q = \frac{1496 \times \tan 40^{\circ} 17'}{\cos 10^{\circ} 21'}. \quad \text{Ans. } 1288.9.$$

$$5. \quad A = 32.6 \times 5.87 \times \sin 56^{\circ} 24' 15''. \quad \text{Ans. } 159.396.$$

$$6. \quad A = \pi r^2, \quad \pi = 3.1416, \quad r = 3.6. \quad \text{Ans. } 40.715.$$

7. The area of a triangle is given by  $\Delta = \frac{1}{2} ab \sin C$ , where  $a$ ,  $b$  are sides and  $C$  is the included angle. Find  $\Delta$ , when  $a = 46.7$ ,  $b = 6.91$ ,  $C = 38^{\circ} 24' 10''$ . Ans. 100.23.

8. The volume of a sphere is given by  $V = \frac{4}{3} \pi r^3$ ; find  $V$  when  $\pi = 3.1416$ ,  $r = 8.65$  cm. Ans. 2711.1 cu. cm.

9. Mass = volume  $\times$  density. Find the radius of a sphere if its mass be  $4.38 \times 10^5$  grams and its density 2.3. Ans. 35.69 cm.

10. The area of a segment of a circle is given by  $S = \frac{1}{2} r^2 (\theta - \sin \theta)$ , where the radius is  $r$ , and  $\theta$  is the angle subtended by the segment at the centre of the circle. Find  $S$ , when  $r = 4.6$  ft.,  $\theta = 126^{\circ} 30'$ . Ans. 14.85 sq. ft.

11. The volume of a right circular cone is given by  $V = \frac{1}{3} \pi R^2 h$ , where  $R$  is the radius of the base and  $h$  is the altitude. Find  $V$ , when  $R = 1.5876$  m., and  $h = 7.675$  m. Ans. 20.257 cu. m.

12. If the volume of a cone  $V = 987.6$  cu. cm., and its height  $h = 9.416$  cm., find the radius of the base. Ans. 10 cm.

13. The time of vibration of a pendulum is given by  $t = \pi \sqrt{\frac{l}{g}}$ , where  $l$  = length of the pendulum,  $g$  = the acceleration. Find the length  $l$  of a pendulum vibrating seconds if  $g = 980.19$  cm. Ans. 99.314 cm.

14. What value must  $g$  have in order that a pendulum 1 m. long shall vibrate seconds? Ans. 986.96 cm.

15. Find the length of a pendulum  $l$  which makes 80 vibrations per minute;  $g = 32.16$  ft. Ans. 1.8329 ft.

16. Find the time of vibration of a pendulum if  $l = 8.04$  ft.,  $g = 32.16$  ft. Ans. 1.57 sec.



## CHAPTER VII

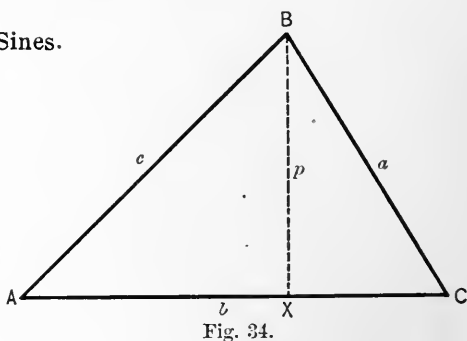
### SOLUTIONS OF TRIANGLES IN GENERAL

We shall now develop a number of theorems which are used in the solution of any plane triangle. The demonstrations of these theorems should be thoroughly mastered.

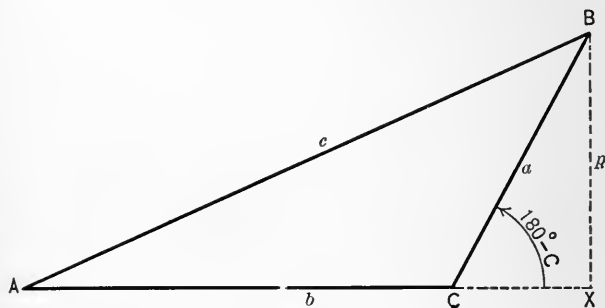
#### 47. The Theorem of Sines.

(1) *First demonstration.*

Uniform lettering of a triangle as indicated in the drawings will be found convenient. Let the angles be indicated by capitals  $A, B, C$ , and let the sides opposite be called  $a, b, c$ , respectively.



Draw a perpendicular  $p$  from the vertex upon the



opposite side  $b$ , Fig. 34, or  $b$  produced, Fig. 35. Then, from the right triangles  $AXB$  and  $CXB$ , we have

$$\sin A = \frac{p}{c}, \quad \sin C = \frac{p}{a}.$$

Dividing  $\sin A$  by  $\sin C$ ,

$$\frac{\sin A}{\sin C} = \frac{a}{c}. \quad (\text{I})$$

In Fig. 35, we have

$$\sin(180^\circ - C) = \sin C = \frac{P}{a}.$$

Drawing a perpendicular from angle  $A$  to side  $a$ , we would have, similarly,

$$\frac{\sin B}{\sin C} = \frac{b}{c}. \quad (\text{II})$$

Dividing (I) by (II),

$$\frac{\sin A}{\sin B} = \frac{a}{b}. \quad (\text{III})$$

These results may be written in the symmetrical form

$$\frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}.$$

**THEOREM.** *In any triangle the sines of the angles are proportional to the opposite sides.*

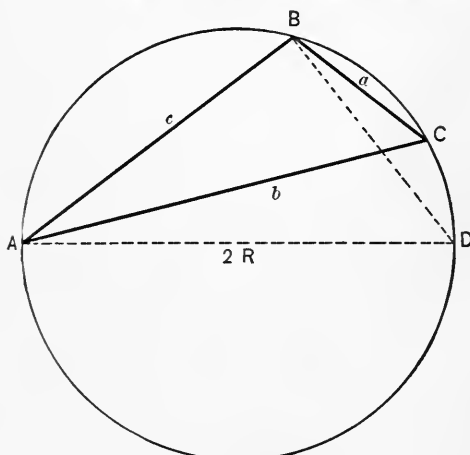


Fig. 36.

(2) *Second demonstration.* The theorem of sines may also be proved by circumscribing a circle about the given triangle, Fig. 36. Draw the diameter  $AD = 2R$ , and the line  $BD$  forming the right triangle  $ABD$ . Then, the angle  $ADB = \text{angle } C$ .

$$\sin ADB = \sin C = \frac{c}{2R}.$$

Similarly, 
$$\sin A = \frac{a}{2R}, \quad \sin B = \frac{b}{2R}.$$

Hence, 
$$\frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c} = \frac{1}{2R},$$

where  $R$  is the radius of the circumscribing circle.

It should be observed that the theorem of sines may be employed in the solution of a triangle when two angles and a side are given, or when two sides and an angle opposite one of them are given.

APPLICATIONS OF THEOREM OF SINES

CASE I. *Given a side and two angles.*

EXAMPLE. Given  $a = 148.3$ ,  $A = 37^\circ 24'$ ,  $C = 76^\circ 48' 30''$ , to find  $b$  and  $c$ .

Solution. (1) Since  
 $A + B + C = 180^\circ$ ,  
 $B = 180^\circ - (A + C)$   
 $= 65^\circ 47' 30''$ .

(2) Make an approximate construction of the triangle. (3) Select formulas, and tabulate the calculations.

$$b = \frac{a \times \sin B}{\sin A},$$

$$c = \frac{a \times \sin C}{\sin A}.$$

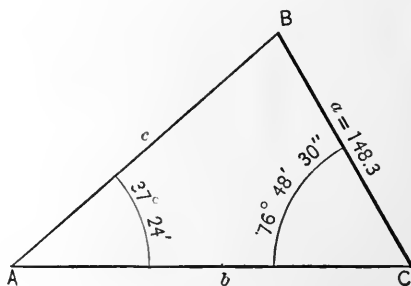


Fig. 37.

Data and Results

Given

$a$	148.3
$A$	$37^\circ 24'$
$C$	$76^\circ 48' 30''$
$B$	$65^\circ 47' 30''$
$b$	222.695
$c$	237.72

Logarithms

$\log a$	2.17114
$\log \sin A$	9.78346
$\log \left( \frac{a}{\sin A} \right)$	2.38768
$\log \sin B$	9.96003
$\log \sin C$	9.98839
$\log b$	2.34771
$\log c$	2.37607

CASE II. *Given two sides and an angle opposite one of the given sides.* This problem may have (1) one solution, (2) two

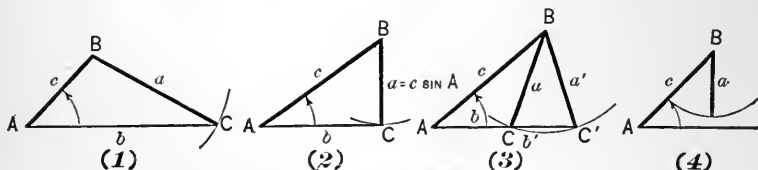


Fig. 38.

solutions, (3) or no solution. If the dimensions given be  $a$ ,  $c$ , and  $A$ , where  $A$  is acute, *one solution* will result if  $a \geq c$ , or if  $c \sin A = a$ , Fig. (1), (2); *two solutions* (triangles  $ABC$ ,  $ABC'$ ) will occur when  $a < c$  and  $a > c \sin A$ , Fig. (3). If  $a < c \sin A$ , *no solution* will exist, Fig. (4). If  $A$  be obtuse, *one solution* will exist provided  $a > c$ , otherwise the construction is impossible.

EXAMPLE. Given  $a = 556$ ,  $b = 678.4$ ,  $A = 31^\circ 10' 30''$ , to find  $B$ ,  $C$ ,  $c$ .

In this example the angle  $A$  is acute and the side  $a < b$ , hence

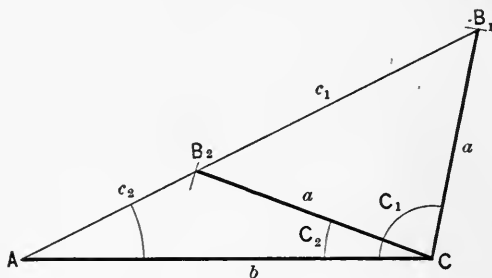


Fig. 39

two solutions will be found. In one solution the angle  $B_1$  will be acute, in the other solution  $B_2 = 180^\circ - B_1$ .

*Solution.* (1) Make an approximate construction of the data.

(2) Formulas and tabulation of the calculations.

$$\sin B = \frac{b \times \sin A}{a}, \quad C = 180^\circ - (A + B), \quad c = \frac{a \times \sin C}{\sin A}.$$

	Data and Results		Logarithms	
Given	$a$	556 .	$\log a$	2.74507
	$b$	678.4	$\log \sin A$	9.71404
	$A$	$31^\circ 10' 30''$	$\log b$	2.83149
	$B_1$	$39^\circ 10' 12''$	$\log \sin B$	9.80046
	$B_2$	$140^\circ 49' 48''$	$\log \sin C_1$	9.97393
	$C_1$	$109^\circ 39' 18''$	$\log \sin C_2$	9.14329
	$C_2$	$7^\circ 59' 42''$	$\log c_1$	3.00496
	$c_1$	1011.5	$\log c_2$	2.17432
	$c_2$	149.39		

EXERCISES

1. Given  $a = 140.6$ ,  $A = 48^\circ 30' 10''$ ,  $B = 76^\circ 24'$ ; find  $b$ ,  $c$ .
2. Given  $b = 3875.4$ ,  $A = 97^\circ 24'$ ,  $B = 40^\circ 27' 15''$ ; find  $a$ ,  $c$ .
3. Given  $a = 148.6$ ,  $b = 121.78$ ,  $A = 69^\circ 20' 10''$ ; find  $B$ ,  $C$ ,  $c$ .
4. Given  $a = 2311$ ,  $b = 1600.7$ ,  $B = 34^\circ 42' 29''$ ; find  $A$ ,  $C$ ,  $c$ .
5. Given  $a = 1906$ ,  $b = 224.8$ ,  $A = 61^\circ 24' 18''$ ; find  $B$ ,  $C$ ,  $c$ .
6. Given  $b = 1009$ ,  $c = 796.4$ ,  $C = 85^\circ$ ; find  $B$ ,  $A$ ,  $a$ .
7. Given  $A = 67^\circ 54'$ ,  $B = 34^\circ 52'$ ,  $b = 4356.7$ ; find  $a$ ,  $c$ .

48. **The Theorem of Tangents.** From the theorem of sines

$$\frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c} = \frac{1}{2R},$$

we have  $a = 2R \sin A$ ,  $b = 2R \sin B$ .

Adding and subtracting, and reducing by § 38,

$$(1) \quad a + b = 2R(\sin A + \sin B) = 4R \sin \frac{A+B}{2} \cos \frac{A-B}{2},$$

$$(2) \quad a - b = 2R(\sin A - \sin B) = 4R \cos \frac{A+B}{2} \sin \frac{A-B}{2}.$$

Dividing (1) by (2),

$$\frac{a+b}{a-b} = \frac{\tan \frac{A+B}{2}}{\tan \frac{A-B}{2}}.$$

We may derive in a similar manner, or write by symmetry,

$$\frac{b+c}{b-c} = \frac{\tan \frac{B+C}{2}}{\tan \frac{B-C}{2}}, \quad \frac{c+a}{c-a} = \frac{\tan \frac{C+A}{2}}{\tan \frac{C-A}{2}}.$$

**THEOREM.** *In any triangle the sum of two sides is to their difference as the tangent of the half sum of the opposite angles is to the tangent of their half difference.*

The theorem of tangents may be used in the solution of a triangle when two sides and their included angle are given. For example, let  $a$ ,  $b$ ,  $C$ , be given. Then we know

$$A + B + C = 180^\circ.$$

$$\frac{A+B}{2} = \frac{180^\circ - C}{2} = 90^\circ - \frac{C}{2}.$$

Hence,  $\tan \frac{A+B}{2} = \cot \frac{C}{2}$ ,

and the first formula above becomes

$$\frac{a+b}{a-b} = \frac{\cot \frac{C}{2}}{\tan \frac{A-B}{2}}.$$

This formula enables us to find the unknown  $\tan \frac{A-B}{2}$ , and then the angle  $\frac{A-B}{2}$ . The angle  $\frac{A+B}{2}$  being known, we find at once the values of  $A$  and  $B$ :

$$A = \frac{1}{2}(A+B) + \frac{1}{2}(A-B), \quad B = \frac{1}{2}(A+B) - \frac{1}{2}(A-B).$$

The application of the theorem of sines now determines side  $a$ .

#### APPLICATIONS OF THEOREM OF TANGENTS

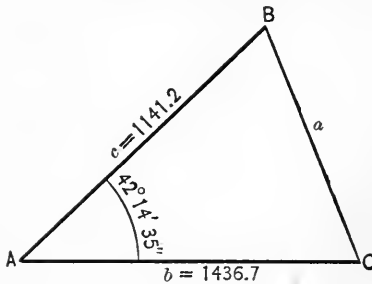


Fig. 40.

#### EXAMPLE.

Given  $b = 1436.7$ ,  
 $c = 1141.2$ ,  
 $A = 42^{\circ} 14' 35''$ ;  
 find  $B$ ,  $C$ ,  $a$ .

*Solution.* (1) Make an approximate construction.

(2) Select formulas and tabulate the calculations.

$$\tan \frac{1}{2}(B-C) = \frac{b-c}{b+c} \tan \frac{1}{2}(B+C), \quad B+C = 180^{\circ} - A, \quad a = \frac{b \times \sin A}{\sin B}.$$

#### Data and Results

Given	$b$	1436.7
	$c$	1141.2
	$A$	$42^{\circ} 14' 35''$
	$b-c$	295.5
	$b+c$	2577.9
	$\frac{B+C}{2}$	$68^{\circ} 52' 42''$
	$\frac{B-C}{2}$	$16^{\circ} 31' 40''$
	$B$	$85^{\circ} 24' 22''$
	$C$	$52^{\circ} 21' 2''$
	$a$	969.0

#### Logarithms

$\log(b-c)$	2.47056
$\log \tan \frac{B+C}{2}$	0.41308
$\log(b+c)$	3.41126
$\log \tan \frac{B-C}{2}$	9.47238
$\log b$	3.15737
$\log \sin A$	9.82755
$\log \sin B$	9.99860
$\log a$	2.98632

EXERCISES

Solve for the unknown parts of the following triangles :

1.  $a = 281, c = 153, B = 34^\circ 42' 29''.$

2.  $b = 296, c = 178, A = 78^\circ 21' 40''.$

3.  $b = 199.37, c = 642.75, A = 130^\circ 9' 24''.$

4.  $a = 101.47, b = 9936.7, C = 47^\circ 48' 12''.$

5.  $b = 1134.7, c = 2277.9, A = 19^\circ 34' 24''.$

6.  $a = 1434.2, b = 9767.2, C = 109^\circ 19' 36''.$

7.  $b = .538, c = 1.245, A = 62^\circ 14' 40''.$

8.  $b = 234.7, c = 185.4, A = 84^\circ 36'.$

9.  $a = 1896.9, b = 3463.7, C = 124^\circ 10'.$

10.  $c = 9.876, a = 4.921, B = 76^\circ 20.4'.$

49. The Theorem of Cosines. (1) *First derivation.*

Draw the perpendicular  $p$  from  $B$  to  $b$ , Fig 41. Then, from the right triangle  $BXC$  we have

$$a^2 = p^2 + \overline{CX}^2 = p^2 + (b - AX)^2 = p^2 + b^2 + \overline{AX}^2 - 2b \cdot AX.$$

But we have from the right triangle  $AXB$

$$p^2 + \overline{AX}^2 = c^2,$$

and

$$AX = c \times \cos A.$$

Making these substitutions, we find

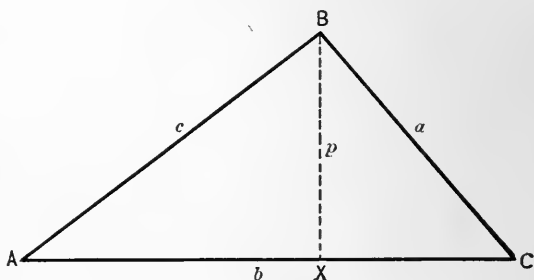


Fig. 41.

$$a^2 = b^2 + c^2 - 2bc \cos A,$$

and by symmetry,

$$b^2 = c^2 + a^2 - 2ca \cos B,$$

$$c^2 = a^2 + b^2 - 2ab \cos C.$$

If the point  $X$  should fall upon the base produced, it may readily be shown that the above results still hold.

**THEOREM.** *In any triangle the square of any side equals the sum of the squares of the other two sides diminished by twice their product into the cosine of their included angle.*

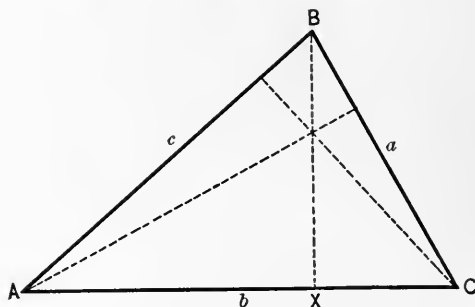


Fig. 42.

(2) *Second derivation.*

From Fig. 42, we have

$$AX = c \times \cos A, \quad CX = a \times \cos C,$$

and therefore,

$$\begin{array}{l} \text{Similarly,} \\ \left. \begin{array}{l} b = c \times \cos A + a \times \cos C, \\ c = a \times \cos B + b \times \cos A, \\ a = b \times \cos C + c \times \cos B. \end{array} \right\} \begin{array}{l} (-b) \\ (-c) \\ (a) \end{array} \end{array}$$

Multiply these equations, as indicated, by  $(-b)$ ,  $(-c)$ ,  $(a)$ , respectively, and add, giving

$$a^2 - b^2 - c^2 = -2bc \times \cos A,$$

or

$$a^2 = b^2 + c^2 - 2bc \times \cos A.$$

By similar manipulation, the other formulas may be derived.

The theorem of cosines is not adapted to logarithmic calculation. When two sides and the included angle are given, this theorem gives the third side. When the given sides are simple numbers such that their squares may readily be known, the application of the cosine formula is to be advised. Otherwise, the theorem of tangents should be employed.



## EXERCISES

Calculate from cosine theorem the following without using logarithms:

1.  $b = 12$ ,  $c = 15$ ,  $A = 45^\circ 34'$ ; find  $a$ .
2.  $c = 10$ ,  $a = 20$ ,  $B = 37^\circ 20'$ ; find  $b$ .
3.  $a = 5$ ,  $b = 7$ ,  $c = 9$ ; find  $A$ .
4.  $a = 25$ ,  $b = 40$ ,  $c = 60$ ; find  $C$ .
5.  $A = 140^\circ$ ,  $b = 100$ ,  $c = 300$ ; find  $a$ .
6.  $a = 150$ ,  $b = 180$ ,  $C = 97^\circ$ ; find  $c$ .
7. Find the perimeter of a triangle where  $a = 200$  ft.,  $b = 300$  ft.,  $C = 37^\circ 40'$ .
8. Find the area of a square whose perimeter is the same as the triangle, where  $a = 40$ ,  $b = 60$ ,  $C = 68^\circ 10'$ .

50. **The Half-angle Theorems.** From the formula

$$a^2 = b^2 + c^2 - 2bc \times \cos A \quad (\text{I})$$

we may derive results suitable for logarithmic calculation of the angle  $A$  when the three sides,  $a$ ,  $b$ ,  $c$ , are given.

Adding, and subtracting  $2bc$ , we find

$$\begin{aligned} a^2 &= b^2 + 2bc + c^2 - 2bc - 2bc \times \cos A \\ &= (b + c)^2 - 2bc(1 + \cos A) \\ &= (b + c)^2 - 2bc \left( 2 \cos^2 \frac{A}{2} \right). \end{aligned} \quad \S 37$$

Solving for  $\cos^2 \frac{A}{2}$ , and factoring the right-hand member,

$$\cos^2 \frac{A}{2} = \frac{(b + c + a)(b + c - a)}{4bc}.$$

Now, let  $a + b + c = 2s$ ,

then,  $b + c - a = 2s - 2a$ ;

substitute and extract the square root,

$$\cos \frac{A}{2} = \sqrt{\frac{s(s-a)}{bc}}.$$

Again, taking (I), subtracting and adding  $2bc$ ,

$$\begin{aligned} a^2 &= b^2 - 2bc + c^2 + 2bc - 2bc \times \cos A \\ &= (b-c)^2 + 2bc(1 - \cos A) = (b-c)^2 + 2bc \left( 2 \sin^2 \frac{A}{2} \right), \quad \S 37 \\ \text{and solving for } \sin^2 \frac{A}{2}, \end{aligned}$$

$$\sin^2 \frac{A}{2} = \frac{a^2 - (b-c)^2}{4bc} = \frac{(a+b-c)(a-b+c)}{4bc}.$$

Now, take  $a + b + c = 2s$ ,  
 then,  $a - b + c = 2s - 2b$ ,  
 $a + b - c = 2s - 2c$ ;

substitute and extract the square root,

$$\sin \frac{A}{2} = \sqrt{\frac{(s-b)(s-c)}{bc}}.$$

Dividing  $\sin \frac{A}{2}$  by  $\cos \frac{A}{2}$ , we find

$$\tan \frac{A}{2} = \sqrt{\frac{(s-b)(s-c)}{s(s-a)}}.$$

The form of this radical may be changed so as to make it symmetrical in  $a, b, c$ .

$$\tan \frac{A}{2} = \sqrt{\frac{(s-b)(s-c)}{s(s-a)}} = \frac{1}{s-a} \sqrt{\frac{(s-a)(s-b)(s-c)}{s}}.$$

The radical here employed will be the same for  $\tan \frac{B}{2}$ ,  $\tan \frac{C}{2}$ .

If we set  $\sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$ ,

$$\tan \frac{A}{2} = \frac{r}{s-a}, \quad \tan \frac{B}{2} = \frac{r}{s-b}, \quad \tan \frac{C}{2} = \frac{r}{s-c}.$$

Then, we have as results the following half-angle formulas.

(1) *The sines of the half-angles of a triangle.*

$$\sin \frac{A}{2} = \sqrt{\frac{(s-b)(s-c)}{bc}},$$

$$\sin \frac{B}{2} = \sqrt{\frac{(s-c)(s-a)}{ca}},$$

$$\sin \frac{C}{2} = \sqrt{\frac{(s-a)(s-b)}{ab}}.$$

(2) *The cosines of the half-angles of a triangle.*

$$\cos \frac{A}{2} = \sqrt{\frac{s(s-a)}{bc}},$$

$$\cos \frac{B}{2} = \sqrt{\frac{s(s-b)}{ca}},$$

$$\cos \frac{C}{2} = \sqrt{\frac{s(s-c)}{ab}}.$$

(3) *The tangents of the half-angles of a triangle.*

$$\tan \frac{A}{2} = \frac{1}{s-a} \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = \frac{r}{s-a},$$

$$\tan \frac{B}{2} = \frac{1}{s-b} \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = \frac{r}{s-b},$$

$$\tan \frac{C}{2} = \frac{1}{s-c} \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = \frac{r}{s-c}.$$

In calculating the angles of a triangle, the tangents of the half-angles should be used, as the complete calculation of  $A$ ,  $B$ ,  $C$  may be performed by taking only four logarithms from the tables, viz.  $\log s$ ,  $\log (s-a)$ ,  $\log (s-b)$ ,  $\log (s-c)$ .

#### APPLICATION OF THE HALF-ANGLE THEOREMS

EXAMPLE. Given  $a = 65.43$ ,  $b = 58.26$ ,  $c = 49.35$ ; find  $A$ ,  $B$ ,  $C$ .

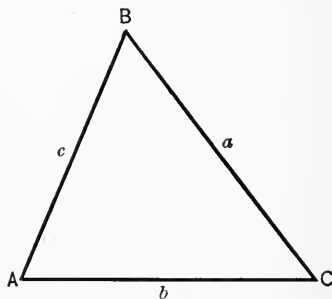


Fig. 43.

*Solution.* (1) An approximate construction with the given data will show angle  $A > B > C$ . (2) Select formulas and tabulate the calculations:

$$\tan \frac{A}{2} = \frac{r}{s-a}, \quad \tan \frac{B}{2} = \frac{r}{s-b}, \quad \tan \frac{C}{2} = \frac{r}{s-c}, \quad r = \sqrt{\frac{(s-a)(s-b)(s-c)}{s}}.$$

Data and Results		Logarithms		
Given	$a$	65.43	$\log(s-a)$	1.32408
	$b$	58.26	$\log(s-b)$	1.45117
	$c$	49.35	$\log(s-c)$	1.57019
	$2s$	173.04	$\log s$	1.93712
	$s$	86.52	$\log r^2$	2.40832
	$s-a$	21.09	$\log r$	1.20416
	$s-b$	28.26	$\log \tan \frac{A}{2}$	9.88008
	$s-c$	37.17	$\log \tan \frac{B}{2}$	9.75299
	$\frac{A}{2}$	37° 11' 18"	$\log \tan \frac{C}{2}$	9.63397
	$\frac{B}{2}$	29° 31' 10"		
	$\frac{C}{2}$	23° 17' 31"		
	$A$	74° 22' 36"		
	$B$	59° 2' 20"		
$C$	46° 35' 2"			

As a check,  
 $A + B + C \stackrel{?}{=} 180^\circ.$

## EXERCISES

Find the angles in each of the following triangles :

- $a = 98.76$ ,  $b = 104.97$ ,  $c = 140.76$ .
- $a = 57,896$ ,  $b = 49,784$ ,  $c = 35,891$ .
- $a = 5.769$ ,  $b = 9.8764$ ,  $c = 11.675$ .
- $a = 0.0587$ ,  $b = 0.09765$ ,  $c = 0.1067$ .
- $a = 94.28$ ,  $b = 112.68$ ,  $c = 180.47$ .

## AREAS OF TRIANGLES

Many expressions may be obtained for the area of a triangle. Some of these will be enumerated.

**51. Area in Terms of Sides and Angles.** Let the area be denoted by  $K$ , and let the triangle be lettered as shown in the drawing. Then, from plane geometry,

$$(1) K = \frac{1}{2} b \times h.$$

Making use of trigonometric relations

$$h = c \sin A,$$

$$(2) K = \frac{1}{2} bc \sin A.$$

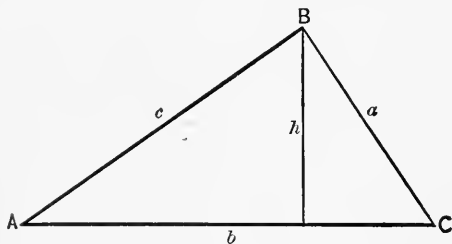


Fig. 44.

**THEOREM.** *The area of any triangle equals one half the product of two sides by the sine of the included angle.*

$$\begin{aligned}
 (3) \quad K &= \frac{1}{2} \frac{c \times \sin B}{\sin C} \times (c \sin A) && \S 47 \\
 &= \frac{1}{2} \cdot \frac{c^2 \sin A \times \sin B}{\sin C}.
 \end{aligned}$$

Since  $\sin A = 2 \sin \frac{A}{2} \cos \frac{A}{2}$ , § 37

and  $\sin \frac{A}{2} = \sqrt{\frac{(s-b)(s-c)}{bc}}$ ,  $\cos \frac{A}{2} = \sqrt{\frac{s(s-a)}{bc}}$ , § 50

we may express  $K$  directly in terms of the three sides.

$$\begin{aligned}
 (4) \quad K &= \frac{1}{2} bc \sin A = bc \sin \frac{A}{2} \cos \frac{A}{2} \\
 &= bc \sqrt{\frac{(s-b)(s-c)}{bc}} \times \sqrt{\frac{s(s-a)}{bc}} \\
 &= \sqrt{s(s-a)(s-b)(s-c)},
 \end{aligned}$$

where  $2s = a + b + c$ .

**52. Area in Terms of  $r$ .** The area of a triangle may be

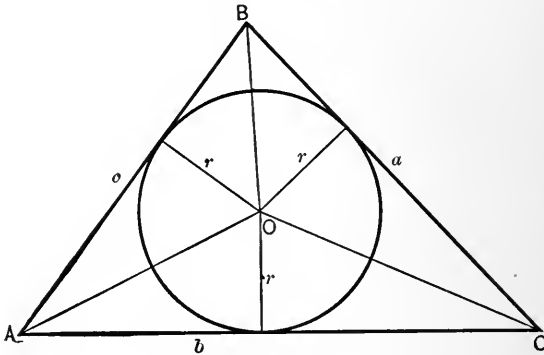


Fig. 45.

expressed in terms of the radius of the inscribed circle. Let a circle be inscribed in the triangle  $ABC$ . See Fig. 45.

Then,

$$\begin{aligned}
 \triangle AOC &= \frac{1}{2} br, \\
 \triangle BOA &= \frac{1}{2} cr, \\
 \triangle COB &= \frac{1}{2} ar.
 \end{aligned}$$

Adding, we have  $\triangle ABC = K = \frac{1}{2} (a + b + c)r = sr$ ,

$$s = \frac{1}{2} (a + b + c).$$

## 53. Expressions for the Area of a Triangle.

1.  $K = \frac{1}{2} bc \times \sin A = \frac{1}{2} ca \times \sin B = \frac{1}{2} ab \times \sin C.$

2.  $K = \frac{\frac{1}{2} c^2 \sin A \sin B}{\sin C}.$

3.  $K = \sqrt{s(s-a)(s-b)(s-c)}, 2s = a + b + c.$

4.  $K = s \times r, r = \text{radius of inscribed circle.}$

## EXERCISES

Solve the following triangles for the unknown parts :

1.  $a = 7950, A = 79^\circ 59', B = 44^\circ 41'.$

2.  $a = 80.86, A = 19^\circ 29', B = 33^\circ 1'.$

3.  $a = 62.65, b = 89.81, C = 55^\circ 5'.$

4.  $a = 2071, b = 1887, C = 55^\circ 12' 3''.$

5.  $a = 0.2034, b = 0.1123, C = 72^\circ 15' 19''.$

6.  $a = 48.5, b = 84, B = 21^\circ 31'.$

7.  $a = 838.56, b = 841.53, B = 68^\circ 10' 24''.$

8.  $a = 49, b = 45, B = 17^\circ 41' 9''.$

9.  $b = 117.4, c = 726.3, B = 80^\circ 10'.$

10.  $c = 1047.51, a = 943.27, A = 63^\circ 17' 18''.$

11.  $a = 5, b = 7, c = 8.$

12.  $a = 341, b = 260, c = 158.$

13.  $a = 40, b = 50, c = 60.$

14.  $a = 0.654, b = 1.5876, c = 0.998.$

15.  $a = 998.46, b = 1004.5, c = 1268.7.$

Find the area  $K$  in the following triangles :

16.  $b = 96, c = 108, A = 65^\circ 10'.$

17.  $a = 480.6, b = 396.4, C = 110^\circ 20'.$

18.  $b = 494, A = 114^\circ, C = 36^\circ.$

19.  $c = 493, a = 540, A = 76^\circ 40' 10''.$

20.  $a = 58, b = 65, c = 87.$

21.  $a = 375.4$ ,  $b = 460.24$ ,  $c = 584.36$ .

22.  $a = 46.2$ ,  $b = 65.8$ ,  $s = 75$ .

23.  $b = 137.6$ ,  $c = 184.5$ ,  $A = 110^\circ 24'$ .

24.  $a = 149.24$ ,  $A = 65^\circ 20'$ ,  $B = 37^\circ 28'$ .

25. To find the distance from a point  $A$  to  $S$ , a base line  $AB = 250$  ft., and the angles  $SAB = 65^\circ 10'$ ,  $SBA = 48^\circ 20'$  are measured. Find  $AS$  and the shortest distance  $h$  from  $S$  to the line  $AB$ .

*Ans.*  $AS = 203.65$  ft.;  $h = 184.82$  ft.

26.  $A$  is a point 3 mi. due north of  $B$ ; from  $A$  a point  $P$  bears N.  $68^\circ 40'$  E., and from  $B$  it bears N.  $35^\circ 50'$  E. Find  $AP$ , and the area of the triangle  $APB$  in square miles.

*Ans.* 3.239 mi.; 4.5268 sq. mi.

27. Find the sides of a parallelogram, when a diagonal 14.69 ft. long makes angles of  $35^\circ 48'$ ,  $64^\circ 27'$  with the sides.

*Ans.* 8.732 ft.; 13.468 ft.

28. A boat is steaming N.E. at a rate of 15 mi. per hour. At 10 o'clock a lighthouse bears N.  $10^\circ$  W.; at 12 o'clock it bears W.  $31^\circ$  S. Find the distance of the boat from the lighthouse at 10 o'clock.

*Ans.* 7.774 mi.

29. The line  $AB = 1460$  ft. upon shore subtends  $64^\circ 20'$  at a lighthouse which is 985 ft from  $A$ . Find the distance of the lighthouse from  $B$ .

*Ans.* 1585.7 ft.

30. A side and diagonal of a parallelogram are 690 ft. and 1248 ft. respectively. If the angle between the diagonals opposite the given side is  $124^\circ 10'$ , what is the length of the other diagonal?

*Ans.* 214.635 ft.

31. To measure across a barrier from  $A$  to  $B$  a station  $C$  is taken, and the distances  $CA$ ,  $CB$ , and the angle  $ACB$  are found to be 584.6 ft., 796.5 ft., and  $87^\circ 40'$ , respectively. Find the distance  $AB$ .

*Ans.* 968.64 ft.

32. Find the length of a straight wall which subtends an angle of  $110^\circ 45'$  at a point  $P$ , the distances of  $P$  being 487.5 ft. and 746.4 ft. from the ends of the wall.

*Ans.* 1025.94 ft.

33. To measure an inaccessible distance  $XY$  a base line  $AB = 550$  ft. is laid off and the angles  $ABY = 75^\circ 48'$ ,  $ABX = 48^\circ 25'$ ,  $BAY = 58^\circ 20'$ ,  $BAX = 98^\circ 24'$  are determined. Find the length  $XY$ .

*Ans.* 512.05 ft.

34. If the sides of a triangle are to each other as 5 : 7 : 9, how do the angles compare?

35. The sides of a triangle are 15, 18, 21. Find the length of the perpendicular from the smallest angle upon the opposite side. *Ans.* 17.636.

36. Find the area of the circle circumscribing the triangle whose sides are 10, 20, 25. *Ans.* 544.

37. From the ridge of a mountain range the depression angles of the sides are  $55^\circ 40'$ ,  $68^\circ 20'$  respectively, and the corresponding distances from the ridge to the ends of a tunnel below are 3475 ft. and 2896 ft. Find the length of the tunnel through the mountain. *Ans.* 3034.4 ft.

38. Show that the median drawn to side  $a$  of the triangle whose sides are  $a, b, c$  is given by  $m = \sqrt{\frac{1}{2}(b^2 + c^2) - \frac{1}{4}a^2}$ .

39. A grass plot in the form of a triangle has its sides 48.5 ft., 65.4 ft., 84.2 ft., respectively. Find the radius and area of the largest circular bed that can be made in the plot. *Ans.* 15.969 ft.; 801.12 sq. ft.

40. The sides of a triangle are  $AB = 24.5$  ft.,  $BC = 30$  ft.,  $CA = 36.5$  ft. If  $A, B, C$  be located upon level ground and vertical posts be erected to heights  $AP_1 = 12$  ft.,  $BP_2 = 18$  ft.,  $CP_3 = 12$  ft., what is the area of the triangle  $P_1P_2P_3$  formed by the tops of the posts? *Ans.* 381.15 sq. ft.

41. A triangle  $b = 50$  ft.,  $A = 65^\circ 24'$ ,  $C = 76^\circ 28'$ , rests with its base  $b$  on a horizontal plane, the plane of the triangle being inclined to the horizontal at an angle  $48^\circ 49'$ . Find the orthogonal projection of the triangle upon the horizontal. *Ans.* 1178.3 sq. ft.

42. A parallelogram, whose sides are 48 ft., 27 ft., and included angle  $58^\circ 48'$ , rests with its longer side upon a horizontal plane and its own plane inclined to the horizontal at an angle  $65^\circ 50'$ . Find its area, and the area of its orthogonal projection upon the horizontal. *Ans.* 1108.5 sq. ft.; 453.8 sq. ft.

43. From the top of a lighthouse 160 ft. high, the depression angle of a ship at  $A$  is  $15^\circ 48'$ , one hour later its depression angle at a point  $B$  is  $10^\circ 25'$ , and the horizontal angle



subtended at the lighthouse by  $AB$  is  $100^\circ 48'$ . Find the speed of the ship. *Ans.* 1123.2 ft. per hour.

44. To find the height  $h$  of a steeple above the plane through its base  $C$ , a line  $AB = 237.5$  ft. is measured and the angles  $CAB = 40^\circ 10' 15''$ ,  $CBA = 110^\circ 20' 10''$  determined; the angle subtended by the steeple at  $B$  is  $27^\circ 18'$ . Find the height of the steeple. *Ans.*  $h = 160.61$  ft.

45. In Ex. 44 let  $AB = a$ ,  $\angle CAB = \alpha$ ,  $\angle CBA = \beta$ , and the elevation angle of the steeple from  $B$  be  $\gamma$ . Show that

$$BC = \frac{a \sin \alpha}{\sin(\alpha + \beta)}, \text{ and } h = \frac{a \sin \alpha}{\sin(\alpha + \beta)} \times \tan \gamma.$$

46. At a horizontal distance  $a$  from a tower, the angle of elevation of the top of the tower is found to be  $\alpha$ , the angle of depression of its base is found to be  $\beta$ . Show that the height of the tower is given by

$$h = a(\tan \alpha + \tan \beta) = a \frac{\sin(\alpha + \beta)}{\cos \alpha \cos \beta}.$$

47. At a certain point in a horizontal plane the angle of elevation of a peak is  $\alpha$ ,  $a$  feet farther away and in the same vertical plane the elevation angle is  $\beta$ . Show that the distance from the first point of observation to the foot of the perpendicular dropped from the peak to the plane is

$$d = \frac{a \tan \beta}{\tan \alpha - \tan \beta} = \frac{a \cos \alpha \sin \beta}{\sin(\alpha - \beta)},$$

and that the height of the peak is given by  $h = d \times \tan \alpha$ .

48. A tower 148 ft. high stands upon the top of a hill; from a point 1100 ft. down the hill the tower subtends an angle of  $6^\circ 48' 12''$ . Find the angle of inclination of the hill.

*Ans.*  $21^\circ 29' 57''$ .

49. Two triangles are determined by  $a = 120$ ,  $b = 160$ ,  $A = 35^\circ 10'$ . Find the difference of their areas without solving for the area of either of the given triangles.

*Ans.* 7083.

50. A ladder 40 ft. long is set with one end at a point 15 ft. from the base of a buttress, the other end reaches a point

35 ft. up its face. Find the angle of inclination of the face of the buttress from the vertical. *Ans.*  $8^{\circ} 12' 44''$ .

51. Find the length of a window, if a pole resting upon the ground and making an angle of  $64^{\circ} 28'$  with the horizontal just reaches the top of the window, and when its base is moved 20 ft. farther away, making an elevation angle of  $39^{\circ} 40'$ , its top reaches the window sill. *Ans.* 15.58 ft.

52. If the angle of elevation of a balloon from a point  $A$  due north is  $\alpha$ , and at the same instant its angle of elevation from a point  $B$  due east of  $A$  is  $\beta$ , find the height  $h$  of the balloon if  $AB = a$ . *Ans.*  $h = \frac{a \sin \alpha \sin \beta}{\sqrt{\sin(\alpha + \beta) \sin(\alpha - \beta)}}$ .

## CHAPTER VIII

### INVERSE FUNCTIONS. TRIGONOMETRIC EQUATIONS

54. **Inverse Notation.** From Fig. 46 a,  $\angle POX = \phi$ ,  
 $\sin \phi = m$ ,  $\cos \phi = \sqrt{1 - m^2}$ ,  $\tan \phi = \frac{m}{\sqrt{1 - m^2}}$ .

These equations may be *expressed inversely*, i. e. solved for  $\phi$ , thus:

$$\begin{aligned} \phi &= \text{arc sin } m = \text{arc cos } \sqrt{1 - m^2} = \text{arc tan } \frac{m}{\sqrt{1 - m^2}} \\ &= \sin^{-1} m = \cos^{-1} \sqrt{1 - m^2} = \tan^{-1} \frac{m}{\sqrt{1 - m^2}}. \end{aligned}$$

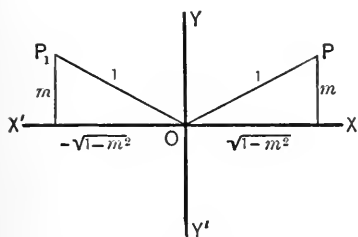


Fig. 46 a.

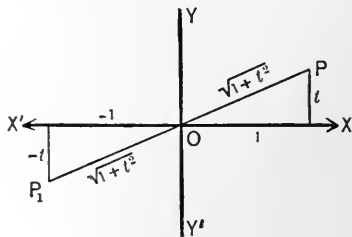


Fig. 46 b.

From Fig. 46 b, with  $\angle POX = \psi$ , we have

$$\tan \psi = t, \quad \sin \psi = \frac{t}{\sqrt{1 + t^2}}, \quad \cos \psi = \frac{1}{\sqrt{1 + t^2}}, \quad \cot \psi = \frac{1}{t},$$

$$\begin{aligned} \text{or } \psi &= \text{arc tan } t = \text{arc sin } \frac{t}{\sqrt{1 + t^2}} = \text{arc cos } \frac{1}{\sqrt{1 + t^2}} = \text{arc cot } \frac{1}{t} \\ &= \tan^{-1} t = \sin^{-1} \frac{t}{\sqrt{1 + t^2}} = \cos^{-1} \frac{1}{\sqrt{1 + t^2}} = \cot^{-1} \frac{1}{t}. \end{aligned}$$

The symbols  $\sin^{-1} m$ ,  $\cos^{-1} \sqrt{1 - m^2}$ , etc., are sometimes called *anti-sine*, *anti-cosine*, etc., but a better reading is to call these *arc sin*  $m$ , *arc cosine*  $\sqrt{1 - m^2}$ , etc.

From the above drawings it is to be noted that each inverse function has *two initial* or *primary values*. Thus

$$\sin \phi = m, \quad \text{or} \quad \phi = \text{arc sin } m$$

is satisfied by the angle  $\phi$  or  $\pi - \phi = \phi'$ . The equation

$$\tan \psi = t, \text{ or } \psi = \text{arc tan } t,$$

is satisfied by the angle  $\psi$  or  $\pi + \psi = \psi'$ .

In addition to the primary solutions, any number of solutions to a trigonometric equation may be obtained by adding any integral multiple of  $2\pi = 360^\circ$ .

EXAMPLES. 1.  $\sin x = \frac{1}{2}$ .

*Solution.*  $x = \text{arc sin } \frac{1}{2} = 30^\circ, 150^\circ$ , primary solutions.

$$x = 2n\pi + \frac{\pi}{6}, \quad 2n\pi + \frac{5}{6}\pi, \quad \text{multiple solutions,}$$

where  $n = \text{any integer}$ .

2.  $\cos \alpha = \frac{1}{2}\sqrt{2}$ .

*Solution.*  $\alpha = \cos^{-1} \frac{1}{2}\sqrt{2} = 45^\circ, -45^\circ$ ,

$$\alpha = 2n\pi + \frac{\pi}{4}, \quad 2n\pi - \frac{\pi}{4}, \quad n = \text{any integer.}$$

3.  $\tan \phi = \sqrt{3}$ .

*Solution.*  $\phi = \tan^{-1} \sqrt{3} = 60^\circ, 240^\circ$ .

$$\phi = n\pi + \frac{\pi}{3}, \quad n = \text{any integer.}$$

**55. Inverse Identities.** A number of important inverse identities will be introduced.

$$\text{I. } \sin^{-1}x + \sin^{-1}y = \sin^{-1}(x\sqrt{1-y^2} + y\sqrt{1-x^2}).$$

This identity may be established as follows: (1) construct an angle  $\phi$  whose sine is  $x$ , also an angle  $\psi$  whose sine is  $y$ . (2) The left member of the identity is  $\phi + \psi$ . Take

$$\begin{aligned} \sin(\phi + \psi) &= \sin \phi \cos \psi + \cos \phi \sin \psi \\ &= x\sqrt{1-y^2} + y\sqrt{1-x^2}. \end{aligned}$$

Hence,

$$\phi + \psi = \sin^{-1}x + \sin^{-1}y = \sin^{-1}(x\sqrt{1-y^2} + y\sqrt{1-x^2}).$$

In a similar manner

$$\sin^{-1}x - \sin^{-1}y = \sin^{-1}(x\sqrt{1-y^2} - y\sqrt{1-x^2}).$$

$$\text{II. } \cos^{-1}x \pm \cos^{-1}y = \cos^{-1}(xy \mp \sqrt{(1-x^2)(1-y^2)}).$$

This identity may be established by constructing two angles,  $\phi = \cos^{-1}x$ ,  $\psi = \cos^{-1}y$ , taking the cosine of the sum and differ-

ence, substituting as above, and then passing to inverse notation.

Prove the following:

$$\text{III. } \tan^{-1} x \pm \tan^{-1} y = \tan^{-1} \left( \frac{x \pm y}{1 \mp xy} \right).$$

$$\text{IV. } \sin^{-1} x = \frac{1}{2} \sin^{-1} (2x\sqrt{1-x^2}) = -\sin^{-1}(-x).$$

$$\text{V. } \cos^{-1} x = \frac{1}{2} \cos^{-1} (2x^2 - 1).$$

### EXERCISES

Construct the acute angles indicated in the inverse notation, and find values of the following:

1.  $\cos(\sin^{-1} \frac{1}{2})$ .

SUGGESTION. Construct  $\phi = \sin^{-1}(\frac{1}{2})$ , then  $\cos \phi = \frac{1}{2}\sqrt{3}$ .

2.  $\tan(\sin^{-1} \frac{3}{5})$ .

9.  $\cos(90^\circ - \cos^{-1} a)$ .

3.  $\tan(\operatorname{arc} \cot \frac{1}{5})$ .

10.  $\sin(\tan^{-1} \sqrt{3}) - \cos \frac{\pi}{6}$ .

4.  $\cot\left(\operatorname{arc} \sin \frac{\sqrt{3}}{2}\right)$ .

11.  $\sin(2 \cot^{-1} \sqrt{3})$ .

5.  $\sin(\operatorname{arc} \tan 1)$ .

12.  $\cos(3 \sin^{-1} \frac{1}{2})$ .

6.  $\cos(\operatorname{arc} \cot 0)$ .

13.  $\tan(90^\circ - \sec^{-1} \sqrt{2})$ .

7.  $\tan(\operatorname{arc} \cot 1)$ .

14.  $\cos(90^\circ - \sin^{-1} \frac{1}{17})$ .

8.  $\sin(90^\circ - \sin^{-1} 1)$ .

Verify the following:

15.  $\sin^{-1} \frac{1}{2} + \cos^{-1} \frac{1}{2} = 90^\circ$ .

16.  $\operatorname{arc} \tan 1 + \operatorname{arc} \cos \frac{1}{\sqrt{2}} = 90^\circ$ .

17.  $\operatorname{arc} \sin 1 - \operatorname{arc} \tan 1 = 45^\circ$ .

18.  $\operatorname{arc} \cos 1 + \operatorname{arc} \tan \infty - \operatorname{arc} \cot 1 = 45^\circ$ .

19.  $\operatorname{arc} \operatorname{vers} 1 - \operatorname{arc} \sec \sqrt{2} = 45^\circ$ .

20.  $\sin(90^\circ - \tan^{-1} \sqrt{3}) + \tan(90^\circ - \sec^{-1} \sqrt{2}) = \frac{3}{2}$ .

21.  $\operatorname{arc} \sin \frac{3}{5} + \operatorname{arc} \cos \frac{3}{5} = \frac{\pi}{2}$ .

23.  $\operatorname{arc} \tan \frac{1}{6} + \operatorname{arc} \tan \frac{5}{7} = \frac{\pi}{4}$ .

22.  $\operatorname{arc} \sin x + \operatorname{arc} \cos x = \frac{\pi}{2}$ .

24.  $\sin\left(2 \operatorname{arc} \sin \frac{1}{2}\right) = \frac{1}{2}\sqrt{3}$ .

$$25. \quad \arctan \frac{1}{2} + \arctan \frac{1}{3} = \arctan 1 = \frac{\pi}{4}.$$

$$26. \quad \arctan \frac{2x}{1-x^2} = 2 \arctan x = \arcsin \frac{2x}{1+x^2}.$$

$$27. \quad \sin^{-1} x = \frac{\pi}{2} - \cos^{-1} x = \frac{1}{2} \cos^{-1}(1-2x^2).$$

$$28. \quad \cos^{-1} x = \frac{\pi}{2} - \sin^{-1} x = 2 \tan^{-1} \sqrt{\frac{1-x}{1+x}}.$$

$$29. \quad \sin^{-1}(3x-4x^3) = 3 \sin^{-1} x.$$

$$30. \quad \cos^{-1}(4x^3-3x) = 3 \cos^{-1} x.$$

$$31. \quad \tan^{-1} \left( \frac{3x-x^3}{1-3x^2} \right) = 3 \tan^{-1} x.$$

$$32. \quad \tan^{-1} \left( \frac{x}{x-1} \right) - \tan^{-1} \frac{x+1}{x} = \tan^{-1} \left( \frac{1}{2x^2} \right).$$

$$33. \quad 2 \sin^{-1} x = \sec^{-1} \frac{1}{1-2x^2}.$$

$$34. \quad \tan^{-1} \frac{\sqrt{1+x^2} - \sqrt{1-x^2}}{\sqrt{1+x^2} + \sqrt{1-x^2}} = \frac{\pi}{4} - \frac{1}{2} \cos^{-1} x^2 = \frac{1}{2} \sin^{-1} x^2.$$

### TRIGONOMETRIC EQUATIONS

**56. Definitions.** An equation containing *one or more* trigonometric functions of an unknown angle is called a *trigonometric equation*. Thus,

$$(a) \quad \sin x = \frac{1}{2},$$

$$(b) \quad \tan x + \sin x = 5,$$

$$(c) \quad \sin x + \cos \frac{x}{2} = 0,$$

$$(d) \quad \begin{cases} \sin x + \cos y = \frac{1}{2}, \\ 3 \sin x - \cos y = 1, \end{cases}$$

are *trigonometric equations*. Equations (d) above are *simultaneous trigonometric equations*.

The operations of ordinary algebra—*clearing of fractions, transposing, multiplying by constants*—are applicable to trigonometric equations.

In addition to these operations, the transformations of trigonometric identities may also be brought into use. For example, the equation

$$\sin 2x = \cos x$$

may be changed trigonometrically into

$$2 \sin x \cos x = \cos x.$$

then transpose and factor,

$$\cos x(2 \sin x - 1) = 0.$$

Equating to zero each factor,

$$\begin{cases} \cos x = 0, & x = 90^\circ, \text{ or } 270^\circ. \\ 2 \sin x = 1, & x = 30^\circ, \text{ or } 150^\circ. \end{cases}$$

**57. Solutions.** Trigonometric equations differ from algebraic equations in one important particular, viz. they have a *multitude of solutions*, whereas algebraic equations have a *finite number of solutions*. As illustrations notice the following examples.

$$(1) \sin x = \frac{1}{2} \text{ has } x = 30^\circ, 150^\circ, \text{ or } x = 2n\pi + \frac{\pi}{6}, \text{ or}$$

$$(2n+1)\pi - \frac{\pi}{6}, \quad (n = 0, \pm 1, \pm 2, \dots).$$

$$(2) \tan x = \sqrt{3} \text{ has for solutions } x = 60^\circ, 240^\circ, \text{ or } n\pi + \frac{\pi}{3},$$

when

$$n = \text{any integer.}$$

We shall enumerate and illustrate some of the more important types of trigonometric equations.

**58. Simple Equations.** Under this heading may be included any equation which reduces readily to one of the forms :

$$\begin{cases} (1) \sin x = K, \\ (2) \cos x = K, \\ (3) \tan x = K, \end{cases} \text{ where } K \text{ is not greater numerically than } 1. \\ K = \text{any number.}$$

**EXAMPLES. 1.** Solve  $4 \sin x = \csc x$  for the angle  $x$ .

*Solution.* Multiply by  $\sin x$ , and divide by 4, giving

$$\sin^2 x = \frac{1}{4},$$

or

$$\sin x = \pm \frac{1}{2}.$$

Hence,

$$x = \sin^{-1}(\pm \frac{1}{2}) = 30^\circ, -30^\circ; 150^\circ, -150^\circ;$$

or, in general notation,

$$x = n\pi \pm \frac{\pi}{6}, \quad n = 0, 1, 2, 3, \dots$$

2. Find  $x$  from  $\tan^2 x + 4 = 2 \sec^2 x$ .

*Solution.* Replace  $\sec^2 x$  by  $1 + \tan^2 x$ , transpose, collect, and change signs,  
 $\tan^2 x = 2$ , or  $\tan x = \pm \sqrt{2}$ .

Then,

$$x = \tan^{-1}(\pm \sqrt{2}) = \tan^{-1}(\pm 1.4142) = 54^\circ 44', - (54^\circ 44'),$$

or

$$x = n\pi \pm (54^\circ 44').$$

NOTE. Take the angle  $\tan^{-1}(\sqrt{2})$  from the table of natural functions.

3. Find  $x$ , when  $6 \cot x + 5 = \tan x$ .

*Solution.* Multiply by  $\tan x$ , transpose, and change signs,

$$\tan^2 x - 5 \tan x - 6 = 0,$$

a quadratic equation with  $\tan x$  as the variable, which factors into

$$(\tan x + 1)(\tan x - 6) = 0,$$

giving

$$\left\{ \begin{array}{l} \tan x = -1, \\ \tan x = 6. \end{array} \right.$$

and

$$\left\{ \begin{array}{l} \tan x = -1, \\ \tan x = 6. \end{array} \right.$$

Hence,

$$x_1 = 135^\circ, -45^\circ,$$

or

$$x_2 = \tan^{-1} 6 = 80^\circ 32', 260^\circ 32'.$$

The general values of  $x$  are

$$x_1 = n\pi - \frac{\pi}{4}, \quad x_2 = n\pi + 80^\circ 32'.$$

### EXERCISES

Solve the following trigonometric equations, giving only the solutions which are between  $-180^\circ$  and  $+180^\circ$ , inclusive.

1.  $3 \sin x = 2$ .     *Ans.*  $\sin^{-1} \frac{2}{3} = 41^\circ 48' 35''$ , or  $138^\circ 11' 25''$ .

2.  $\sin 2x - \cos x = 0$ .      $[\sin 2x = 2 \sin x \cos x.]$

*Ans.*  $\pm 90^\circ, 30^\circ, 150^\circ$ .

3.  $\cos 2x + \sin x = 1$ .

*Ans.*  $0, \frac{\pi}{6}, \frac{5\pi}{6}, \pi$ .

4.  $\cos 2x = \sin x$ .

*Ans.*  $30^\circ, -90^\circ, 150^\circ$ .

5.  $\tan 2x + 2 \sin x = 0$ .

*Ans.*  $0, \pm 60^\circ, 180^\circ$ .

6.  $\cos 3x - \sin 2x = 0$ .

SUGGESTION. Change  $\cos 3x$  to  $4 \cos^3 x - 3 \cos x$ ,  $\sin 2x = 2 \sin x \cos x$ , giving  $4 \cos^3 x - 3 \cos x = 2 \sin x \cos x$ ; factor and solve. Or,  $\cos 3x = \sin(3x + 90^\circ)$ ; then

$$\cos 3x - \sin 2x = \sin(3x + 90^\circ) - \sin 2x$$

$$= 2 \cos\left(\frac{5}{2}x + 45^\circ\right) \cdot \sin\left(\frac{x}{2} + 45^\circ\right) = 0.$$



Hence,  $\cos\left(\frac{5}{2}x + 45^\circ\right) = 0$ , and  $\sin\left(\frac{x}{2} + 45^\circ\right) = 0$ ,

giving  $\left. \begin{aligned} \frac{5}{2}x + 45^\circ &= 90^\circ, 270^\circ, 450^\circ, \\ \text{and} \quad \frac{x}{2} + 45^\circ &= 0^\circ, 180^\circ. \end{aligned} \right\}$

Then,  $x = 18^\circ, 90^\circ, 162^\circ$ ,  
and  $x = -90^\circ$ .

7.  $\cos 3x + \sin 2x - \cos x = 0$ . *Ans.*  $0^\circ, 30^\circ, 90^\circ, 150^\circ, 180^\circ$ .

8.  $\cos(x + 60^\circ) - \sin(x + 30^\circ) = \frac{1}{2}\sqrt{3}$ . *Ans.*  $-30^\circ, -150^\circ$ .

9.  $\sin(x + 60^\circ) - \sin(x - 60^\circ) = -\frac{1}{2}\sqrt{3}$ . *Ans.*  $\pm 120^\circ$ .

10.  $\sin 4x = 2 \sin 2x$ . *Ans.*  $0^\circ, 90^\circ, 180^\circ$ .

### 59. Equations of the Form

$$\begin{cases} r \cos \phi = a, \\ r \sin \phi = b. \end{cases}$$

Here is a set of two simultaneous equations in two unknowns,  $r, \phi$ .

(1) To find  $\phi$ , divide the second equation by the first,

$$\tan \phi = \frac{b}{a}, \quad \phi = \tan^{-1}\left(\frac{b}{a}\right).$$

Or, 
$$\phi = n\pi + \tan^{-1}\left(\frac{b}{a}\right).$$

(2) To find  $r$ , square and add, recalling the identity  $\sin^2 \phi + \cos^2 \phi = 1$ ,

$$\begin{aligned} r^2 &= a^2 + b^2, \\ r &= \pm \sqrt{a^2 + b^2}. \end{aligned}$$

The proper sign of  $r$  must be chosen so that  $r \cos \phi = a$ ,  
 $r \sin \phi = b$ .

EXAMPLES. 1. Find  $r, \phi$  from

$$\begin{cases} r \cos \phi = 3, \\ r \sin \phi = 4. \end{cases}$$

We have  $\tan \phi = \frac{4}{3}$ ,  $\phi = \tan^{-1}\left(\frac{4}{3}\right) = 53^\circ 8'$ .

Squaring and adding,  $r^2 = 4^2 + 3^2 = 25$ ,

$$r = \pm 5.$$

Find  $r$ ,  $\phi$  in the following:

$$\begin{array}{ll} 2. \begin{cases} r \cos \phi = 12, \\ r \sin \phi = 5. \end{cases} & 4. \begin{cases} r \sin \phi = 5, \\ r \cos \phi = 5\sqrt{3}. \end{cases} \\ 3. \begin{cases} r \cos \phi = 6, \\ r \sin \phi = 12. \end{cases} & 5. \begin{cases} r \sin \phi = 4.876, \\ r \cos \phi = 2.396. \end{cases} \end{array}$$

### 60. Equations in the Form

$$\begin{cases} r \sin \theta \cos \phi = a, \\ r \sin \theta \sin \phi = b, \\ r \cos \theta = c, \end{cases}$$

where  $r$ ,  $\theta$ ,  $\phi$  are variables.

Divide the second equation by the first,

$$\tan \phi = \frac{b}{a}, \quad \phi = \tan^{-1} \frac{b}{a}.$$

Squaring all three equations and adding, we have

$$r^2 (\sin^2 \theta [\cos^2 \phi + \sin^2 \phi] + \cos^2 \theta) = a^2 + b^2 + c^2,$$

or

$$\begin{aligned} r^2 &= a^2 + b^2 + c^2, \\ r &= \pm \sqrt{a^2 + b^2 + c^2}. \end{aligned}$$

From the third equation,

$$\begin{aligned} \cos \theta &= \frac{c}{r} = \frac{c}{\pm \sqrt{a^2 + b^2 + c^2}}, \\ \theta &= \cos^{-1} \left( \frac{\pm c}{\sqrt{a^2 + b^2 + c^2}} \right). \end{aligned}$$

### EXERCISES

Find  $r$ ,  $\theta$ ,  $\phi$  in the following:

$$\begin{array}{ll} 1. \begin{cases} r \sin \theta \cos \phi = 2, \\ r \sin \theta \sin \phi = 2, \\ r \cos \theta = 1. \end{cases} & 4. \begin{cases} r \sin \theta \cos \phi = 12, \\ r \sin \theta \sin \phi = 12, \\ r \cos \theta = 1. \end{cases} \\ 2. \begin{cases} r \sin \theta \cos \phi = 6, \\ r \sin \theta \sin \phi = 3, \\ r \cos \theta = 2. \end{cases} & 5. \begin{cases} r \sin \theta \cos \phi = 1, \\ r \sin \theta \sin \phi = 4, \\ r \cos \theta = 8. \end{cases} \\ 3. \begin{cases} r \sin \theta \cos \phi = 2, \\ r \sin \theta \sin \phi = 6, \\ r \cos \theta = 9. \end{cases} & 6. \begin{cases} r \sin \theta \cos \phi = 5, \\ r \sin \theta \sin \phi = 2, \\ r \cos \theta = 0. \end{cases} \end{array}$$

**61.** To solve  $a \sin x + b \cos x = c$ . Divide this equation by  $\sqrt{a^2 + b^2}$ .

$$(1) \quad \frac{a \sin x}{\sqrt{a^2 + b^2}} + \frac{b \cdot \cos x}{\sqrt{a^2 + b^2}} = \frac{c}{\sqrt{a^2 + b^2}}.$$

Now let  $\frac{a}{\sqrt{a^2 + b^2}} = \sin \phi$ ,  $\frac{b}{\sqrt{a^2 + b^2}} = \cos \phi$ ,

and hence,  $\frac{a}{b} = \tan \phi$ ,  $\phi = \tan^{-1} \frac{a}{b}$ .

Then equation (1) becomes

$$(2) \quad \sin \phi \sin x + \cos \phi \cos x = \frac{c}{\sqrt{a^2 + b^2}},$$

or  $\cos(x - \phi) = \frac{c}{\sqrt{a^2 + b^2}}$ ,  $x - \phi = \pm \cos^{-1}\left(\frac{c}{\sqrt{a^2 + b^2}}\right)$ ,

$$x = \phi \pm \cos^{-1}\left(\frac{c}{\sqrt{a^2 + b^2}}\right).$$

**EXAMPLES.** 1. Solve  $5 \sin x + 12 \cos x = 6.5$ .

Divide both members by 13,

$$(1) \quad \frac{5}{13} \sin x + \frac{12}{13} \cos x = 0.5.$$

Write  $\frac{5}{13} = \sin \phi$ ,  $\frac{12}{13} = \cos \phi$ ,  $\tan \phi = \frac{5}{12}$ .

Hence,  $\phi = \tan^{-1}\left(\frac{5}{12}\right) = 22^\circ 37'$ .

Now equation (1) becomes

$$(2) \quad \sin \phi \sin x + \cos \phi \cos x = 0.5,$$

or  $\cos(x - \phi) = 0.5$ ,

$$x = \phi \pm \cos^{-1}(0.5) = 22^\circ 37' \pm 60^\circ = 82^\circ 37', -37^\circ 23'.$$

2. Solve  $3 \cos x + 5 \sin x = 4$ .

3. Solve  $12 \sin x + 5 \cos x = 3.9$ .

4. Solve  $8 \cos x + 15 \sin x = 5.1$ .

5. Solve  $3 \cos x - 2 \sin x = \frac{3}{5} \sqrt{13}$ .

6. Solve  $5 \sin x - 6 \cos x = \frac{3}{5} \sqrt{61}$ .

**62.** To solve  $\sin(x + \phi) = a \sin x$ .

We have  $\frac{\sin(x + \phi)}{\sin x} = \frac{a}{1}$ .

Take by composition and division,

$$\frac{\sin(x + \phi) + \sin x}{\sin(x + \phi) - \sin x} = \frac{a + 1}{a - 1},$$

$$\frac{2 \sin\left(x + \frac{\phi}{2}\right) \cos \frac{\phi}{2}}{2 \cos\left(x + \frac{\phi}{2}\right) \sin \frac{\phi}{2}} = \frac{a + 1}{a - 1},$$

or 
$$\tan\left(x + \frac{\phi}{2}\right) = \frac{a + 1}{a - 1} \tan \frac{\phi}{2}.$$

The right member is now known, and the solution may be written out.

EXAMPLES. 1. Solve  $\sin(x + 37^\circ 14') = 2 \sin x$ .

Substituting in the above result, and retaining the smallest angle,

$$\tan\left(x + \frac{37^\circ 14'}{2}\right) = 3 \tan \frac{37^\circ 14'}{2} = 3(0.3369),$$

$$x = \tan^{-1}(1.0107) - \frac{37^\circ 14'}{2} = 45^\circ 18' 20'' - (18^\circ 37') = 26^\circ 41' 20''.$$

2. Solve  $\sin(x + 65^\circ 21') = 3 \sin x$ .

3. Solve  $\sin(x - 28^\circ 40') = \frac{2}{3} \sin x$ .

4. Solve  $\sin(x + 56^\circ 24') = 5 \sin(x - 10^\circ 20')$ .

5. Solve  $\sin(x + 94^\circ 10') = 4 \sin x$ .

6. Solve  $\sin(x - 124^\circ) = \frac{3}{4} \sin x$ .

63. To solve  $\tan(x + \phi) = a \tan x$ .

Divide by  $\tan x$ , and take by composition and division,

$$\frac{\tan(x + \phi)}{\tan x} = a,$$

$$\frac{\tan(x + \phi) + \tan x}{\tan(x + \phi) - \tan x} = \frac{a + 1}{a - 1}.$$

Simplifying, 
$$\frac{\sin(2x + \phi)}{\sin \phi} = \frac{a + 1}{a - 1},$$

$$\sin(2x + \phi) = \frac{a + 1}{a - 1} \sin \phi.$$

EXAMPLES. 1. Solve  $\tan(x + 20^\circ) = 5 \tan x$ .

Comparing with the above result,

$$\begin{aligned}\phi &= 20^\circ, a = 5, \\ \sin(2x + \phi) &= \frac{3}{2} \sin 20^\circ \\ &= \frac{3}{2} (0.342) = 0.513, \\ 2x + \phi &= \sin^{-1}(0.513) = 30^\circ 52', \\ 2x &= 30^\circ 52' - 20^\circ = 10^\circ 52', \\ x &= 5^\circ 26' .\end{aligned}$$

2. Solve  $\tan(x + 30^\circ) = 6 \tan x$ .

3. Solve  $\tan(x + 47^\circ 20') = 7 \tan x$ .

4. Solve  $\tan(x + 25^\circ 10') = 10 \tan x$ .

5. Solve  $\tan(x + 60^\circ) = 13 \tan x$ .

64. To solve  $x = a + \beta \sin x$ .

In this equation  $a, \beta$  are usually given as angles (degrees or radians);  $\beta$  expressed in radian measure is smaller than unity. Two plans of solution will be sketched.

(1) *Trial solution.* Let  $a, \beta$  be expressed in degrees. Then an upper limit to  $x$  will be shown by  $a + \beta$ , since the multiplier  $\beta$  is smaller than unity. Take a trial solution, substitute in the equation, note the error, make another approximation, and so continue until the required degree of accuracy is attained.

(2) *Graphical solution.* Let  $a, \beta$  be expressed in radian measure:  $a^\circ = a$  radians,  $\beta^\circ = b$  radians. Then we have to determine  $x$  so that

$$x - a = b \sin x.$$

Let

$$y_1 = x - a, \quad y_2 = b \sin x.$$

Construct upon rectangular axes a curve representing each of these equations. The first is a *straight line* through the point  $a$  on the  $X$ -axis; the second is a *modified sine curve*. The  $x$  of the point of section of these two graphs is the required solution.

As an illustration of the graphical solution let us solve

$$x = 57^\circ 17' 44'' + 45^\circ \times \sin x.$$

Here,  $57^\circ 17' 44'' = 1$  radian,  $45^\circ = 0.785$  radians.

Then we are to solve  $x = 1 + 0.785 \times \sin x$ .

Let

$$y_1 = x - 1, \quad y_2 = 0.785 \sin x.$$

Now construct the *straight line*  $y_1 = x - 1$ , and the modified sine curve  $y_2 = 0.785 \sin x$ . The abscissa of the point of intersection of the straight line and curve is approximately  $x = 1.769$  radian  $= 101^\circ 27'$ .

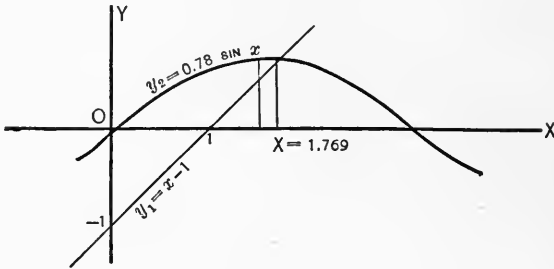


Fig. 47.

- EXAMPLES. 1. Solve  $x = 24^\circ + 30^\circ \times \sin x$ .
2. Solve  $x = 64^\circ + 28^\circ \times \sin x$ .
3. Solve  $x = 30^\circ + 50^\circ \times \sin x$ .
4. Solve  $x = 10^\circ 20' + 40^\circ \times \sin x$ .
5. Solve  $x = 45^\circ + (37^\circ 30') \times \cos x$ .
6. Show  $\sin x \geq \frac{2}{\pi}x$ ,  $0 \leq x \leq \frac{\pi}{2}$ .

## CHAPTER IX

### COMPLEX NUMBERS. DE MOIVRE'S THEOREM. TRIGONOMETRIC SERIES. EXPONENTIAL AND HYPERBOLIC FUNCTIONS

**65. Roots of Quadratic Equations.** In ordinary algebra we have such equations as

$$x^2 - 6x + 25 = 0,$$

whose roots,

$$z_1 = 3 + 4\sqrt{-1}, \quad z_2 = 3 - 4\sqrt{-1},$$

are called *complex numbers*. These numbers contain a *real unit*, 1, and a so-called *imaginary unit*,  $\sqrt{-1}$ .

(1) *Properties of  $\sqrt{-1}$ .* The imaginary unit is usually represented by  $i$ . We may easily show that when  $\sqrt{-1} = i$ ,

$$i^2 = -1, \quad i^3 = -i, \quad i^4 = 1, \quad i^5 = i \dots,$$

and generally,

$$i^{4k} = 1, \quad i^{4k+1} = i, \quad i^{4k+2} = -1, \quad i^{4k+3} = -i.$$

(2) *Graphical representation of  $x + yi$ .* To any complex number as  $3 + 4i$ ,  $3 - 4i$ ,  $x + yi$  corresponds a *point in a plane*. If we multiply a real number  $a$  by  $i$ , and this product again by  $i$ , the result is  $-a$ . Thus, multiplying twice by  $i$  changes a number to its negative. *Multiplying a number by  $i$  may be interpreted as turning its direction through  $90^\circ$ .* To locate  $3 + 4i$  upon a plane, lay off 3 units,  $OQ$ , along the real axis (horizontal in Fig. 48), then at  $Q$  erect a perpendicular 4 units long; the point  $P_1$  represents the complex number  $3 + 4i$ . Lay off  $-4$  perpendicular to  $OQ$  at  $Q$ , and we locate  $3 - 4i$ , at  $P_2$ .

Any complex number  $x + yi$  may be represented upon a plane as shown in Fig. 49. The point  $P$  may be anywhere in the plane.

(3) *Modulus, arc ( $x + yi$ ).* The line  $OP = r$  is a vector equal in length to the *modulus* of  $x + yi$ , or the *absolute value* of

$x + yi$ . The angle  $XOP = \phi$  is called the *arc* of  $x + yi$ , or *amplitude*, or *argument* of  $x + yi$ . As abbreviations

$$r = \text{mod } (x + yi), \quad \phi = \text{amp } (x + yi).$$

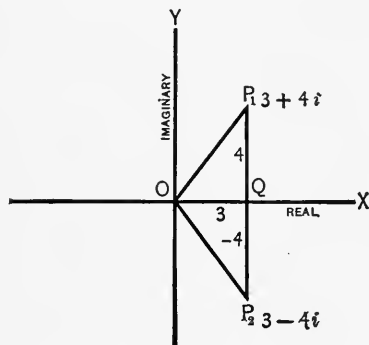


Fig. 48.

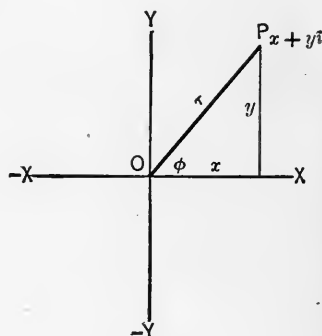


Fig. 49.

The following notation should be recognized:

$$\text{Modulus of } x + yi = r = \sqrt{x^2 + y^2} = |x + yi|.$$

$$\text{Arc of } x + yi = \phi = \tan^{-1} \frac{y}{x} = \text{amplitude } (x + yi).$$

### EXERCISES

1. Locate the following complex numbers:

(1)  $3 + 2i$ ; (2)  $2 + 6i$ ; (3)  $-3 + 3i$ ; (4)  $-4 + i$ ;

(5)  $-3 - 4i$ ; (6)  $-6i$ ; (7)  $4 - 5i$ ; (8)  $\left(\frac{1}{2} + \frac{\sqrt{3}}{2}i\right) \times 5$ .

2. Find the modulus and arc of each of the numbers in Ex. 1.

3. Solve the following equations and locate the roots as complex numbers:

(1)  $z^2 - 4z + 13 = 0$ ; (2)  $z^2 + 6z + 13 = 0$ ; (3)  $z^2 + z + 1 = 0$ ;  
(4)  $z^3 - 1 = 0$ ; (5)  $z^3 + 1 = 0$ .

4. Locate the following products: (1)  $i \times (2 + 4i)$ ;  
(2)  $i \times (-3 + 2i)$ ; (3)  $i \times (5 - 3i)$ ; (4)  $i \times i \times i(2 - i)$ .

66. **Complex Numbers expressed Trigonometrically.** From Fig. 49, we have

$$x = r \cos \phi, \quad y = r \sin \phi, \quad r = \sqrt{x^2 + y^2}, \quad \phi = \tan^{-1} \frac{y}{x}.$$



Hence,

$$x + yi = r(\cos \phi + i \sin \phi) = \sqrt{x^2 + y^2}(\cos \phi + i \sin \phi).$$

**THEOREM.** *A complex number equals its modulus multiplied by the expression  $\cos \phi + i \sin \phi$  where  $\phi$  is its amplitude.*

**EXAMPLES.** 1.  $z^2 - z + 1 = 0$  has roots,

$$z_1 = \frac{1}{2} + \frac{\sqrt{3}}{2}i, \quad z_2 = \frac{1}{2} - \frac{\sqrt{3}}{2}i.$$

The modulus of  $z_1 = 1$ , mod  $z_2 = 1$ ; the amplitude of

$$z_1 = \tan^{-1}\left(\frac{\sqrt{3}}{2} \div \frac{1}{2}\right) = \tan^{-1}\sqrt{3} = 60^\circ,$$

$$\text{am } z_2 = \tan^{-1}(-\sqrt{3}) = -60^\circ.$$

Hence,

$$z_1 = \frac{1}{2} + \frac{\sqrt{3}}{2}i = \cos 60^\circ + i \sin 60^\circ,$$

$$z_2 = \frac{1}{2} - \frac{\sqrt{3}}{2}i = \cos 60^\circ - i \sin 60^\circ.$$

2. Express the roots of the following equations in trigonometric form :

- (1)  $z^2 + 1 = 0$ ; (2)  $z^2 - 2z + 2 = 0$ ; (3)  $z^2 - \sqrt{3}z + 1 = 0$ ;  
 (4)  $z^2 + 2z - 8 = 0$ ; (5)  $z^2 + \sqrt{2}z + 1 = 0$ ; (6)  $z^2 + z + 1 = 0$ .

**67. DeMoivre's Theorem.** Let us take a complex number in trigonometric form,

$$z = x + yi = r(\cos \phi + i \sin \phi).$$

Squaring  $z$ , and recalling that  $i^2 = -1$ ,

$$z^2 = r^2(\cos \phi + i \sin \phi)^2 = r^2(\cos^2 \phi - \sin^2 \phi + 2i \sin \phi \cos \phi),$$

$$(1) \quad z^2 = r^2(\cos 2\phi + i \sin 2\phi), \quad \S 35, (7), (8).$$

Now, multiply (1) by  $z = r(\cos \phi + i \sin \phi)$ .

$$z^3 = r^3[\cos 2\phi \cos \phi - \sin 2\phi \sin \phi + i(\sin 2\phi \cos \phi + \cos 2\phi \sin \phi)].$$

$$(2) \quad z^3 = r^3(\cos 3\phi + i \sin 3\phi), \quad \S 34.$$

The law of exponents shown in (1), (2) would indicate that for  $n =$  any positive integer,

$$(3) \quad z^n = r^n(\cos n\phi + i \sin n\phi).$$

Assuming law (3) to hold for any integral  $n$ , let us see if it holds when  $n$  is replaced by  $n + 1$ .

Multiply (3) by

$$\begin{aligned} z &= r(\cos \phi + i \sin \phi), \\ z^{n+1} &= r^{n+1}[\cos n\phi \cos \phi - \sin n\phi \sin \phi + i(\sin n\phi \cos \phi \\ &\quad + \cos n\phi \sin \phi)]. \end{aligned}$$

$$(4) \quad z^{n+1} = r^{n+1}[\cos(n+1)\phi + i \sin(n+1)\phi].$$

Hence, the law assumed in (3) for the integer  $n$  holds for  $n + 1$ . We see this law holds for  $n = 2$  and  $n = 3$ , hence it holds for  $n = 4, 5, \dots, n =$  any positive integer. Hence, we have

DEMOIVRE'S THEOREM:  $(\cos \phi + i \sin \phi)^n = \cos n\phi + i \sin n\phi$ .

*DeMoivre's Theorem holds when  $n$  is an integer, a fraction, or a negative number.*

$$(\cos \phi + i \sin \phi)^{\frac{1}{n}} = \cos \frac{\phi}{n} + i \sin \frac{\phi}{n},$$

$$(\cos \phi + i \sin \phi)^{\frac{p}{q}} = \cos \frac{p}{q}\phi + i \sin \frac{p}{q}\phi,$$

$$\begin{aligned} (\cos \phi + i \sin \phi)^{-m} &= \cos(-m\phi) + i \sin(-m\phi) \\ &= \cos m\phi - i \sin m\phi. \end{aligned}$$

**68. Raising to Powers and Extracting Roots.** DeMoivre's Theorem enables us to raise

$$z = x + iy = r(\cos \phi + i \sin \phi)$$

to any power, or to extract any root of  $z$ .

Thus, 
$$z^2 = r^2(\cos 2\phi + i \sin 2\phi).$$

Hence, to square a complex number, square its modulus and double its amplitude. To cube a complex number, cube its modulus and multiply its amplitude by three.

EXAMPLES. 1. Raise  $z = 3 + 4i$  to the 2d power; to the 3d power.

$$z = 3 + 4i = 5(\cos \phi + i \sin \phi), \quad \phi = \tan^{-1} \frac{4}{3} = 53^\circ 8', \text{ nearly.}$$

$$z^2 = (3 + 4i)^2 = 25(\cos 2\phi + i \sin 2\phi).$$

$$z^3 = (3 + 4i)^3 = 125(\cos 3\phi + i \sin 3\phi).$$

2. Raise  $z = \frac{1}{2} + \frac{\sqrt{3}}{2}i$  to 2d, 3d,  $n$ th powers, and locate these respective numbers on a diagram. See Fig. 49.

3. Find  $z^2, z^4, z^6$ , when  $z = \frac{-\sqrt{3}}{2} + \frac{1}{2}i$ .

4. Find  $z^5, z^{10}$ , when  $z = -1 - i$ .

The extraction of roots may be performed by use of DeMoivre's Theorem :

$$z^{\frac{1}{n}} = r^{\frac{1}{n}} \left( \cos \frac{\phi}{n} + i \sin \frac{\phi}{n} \right).$$

This formula seems to give but one of the  $n$   $n$ th roots of  $z$ , but we may obtain  $n$  different roots by writing

$$z = r[\cos(\phi + 2k\pi) + i \sin(\phi + 2k\pi)];$$

then will

$$\frac{1}{z^n} = r^{\frac{1}{n}} \left[ \cos \frac{\phi + 2k\pi}{n} + i \frac{\phi + 2k\pi}{n} \right], \quad k = 1, 2, 3, \dots, n-1.$$

EXAMPLES 1. Extract the square root of  $i$ .

$$\text{Here,} \quad z = i = 1 \left( \cos \frac{\pi}{2} + i \sin \frac{\pi}{2} \right)$$

$$= \cos \left( \frac{\pi}{2} + 2k\pi \right) + i \sin \left( \frac{\pi}{2} + 2k\pi \right).$$

$$\text{Then,} \quad z^{\frac{1}{2}} = i^{\frac{1}{2}} = \cos \left( \frac{\frac{\pi}{2} + 2k\pi}{2} \right) + i \sin \left( \frac{\frac{\pi}{2} + 2k\pi}{2} \right).$$

Let  $z_1, z_2$  be the two roots. then

$$z_1 = \cos \frac{\pi}{4} + i \sin \frac{\pi}{4} = \frac{1}{\sqrt{2}} + \frac{1}{\sqrt{2}}i, \quad k = 0,$$

$$z_2 = \cos \left( \frac{\pi}{4} + \pi \right) + i \sin \left( \frac{\pi}{4} + \pi \right) = -\frac{1}{\sqrt{2}} - \frac{1}{\sqrt{2}}i, \quad k = 1.$$

2. Extract the cube root of  $-8$ , and locate the roots on a diagram.

$$\begin{aligned} \text{In this case } z &= -8 = 8(\cos \pi + i \sin \pi) \\ &= 8[\cos(\pi + 2k\pi) + i \sin(\pi + 2k\pi)]. \end{aligned}$$

Extract the cube root,

$$z^{\frac{1}{3}} = (-8)^{\frac{1}{3}} = 8^{\frac{1}{3}} \left[ \cos \frac{\pi + 2k\pi}{3} + i \sin \frac{\pi + 2k\pi}{3} \right].$$

Giving  $k$  values 0, 1, 2, we find the three roots,  $z_1, z_2, z_3$ ,

$$z_1 = 2 \left( \cos \frac{\pi}{3} + i \sin \frac{\pi}{3} \right) = 1 + \sqrt{3}i, \quad k = 0,$$

$$z_2 = 2(\cos \pi + i \sin \pi) = -2, \quad k = 1,$$

$$z_3 = 2 \left( \cos \frac{5\pi}{3} + i \sin \frac{5\pi}{3} \right) = 1 - \sqrt{3}i, \quad k = 2.$$

3. Find the five 5th roots of  $32$ ; of  $i$ .

4. Find the six 6th roots of  $-1$ ; the cube roots of  $\frac{-1 + \sqrt{3}i}{2}$ .

69. Value of  $\sin x, \cos x$  in Terms of  $x$ .

(1) Value of  $\frac{\sin \phi}{\phi}$  when  $\phi \doteq 0$ .

When an angle  $\phi$  is small,  $\sin \phi$  approaches arc  $\phi$ .

From the tables of natural functions and radian measure we have :

$\sin 0^\circ = 0.00000$	$0^\circ = 0.00000$ radian
$\sin 10' = 0.00291$	$10' = 0.00291$ radian
$\sin 40' = 0.01164$	$40' = 0.01164$ radian
$\sin 1^\circ = 0.01745$	$1^\circ = 0.01745$ radian
$\sin 2^\circ = 0.03490$	$2^\circ = 0.03491$ radian

which show that  $\sin \phi = \phi$  for values of  $\phi$  from  $0^\circ$  to near  $2^\circ$ , true to five decimals.

To show this property generally, we have from geometry

$$BC < BA < DA, \quad \phi < 90^\circ,$$

or, if  $OA = 1$ , Fig. 50,

$$\sin \phi < \phi < \tan \phi.$$

Divide this inequality by  $\sin \phi$ ,

$$1 < \frac{\phi}{\sin \phi} < \frac{1}{\cos \phi}.$$

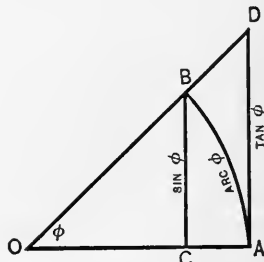


Fig. 50.

Now let  $\phi$  approach zero,  $\phi \doteq 0$ , and  $\cos \phi \doteq 1$ ; hence,

$$1 < \left[ \frac{\phi}{\sin \phi} \right]_{\phi \neq 0} < 1,$$

or,

$$\lim_{\phi \rightarrow 0} \left[ \frac{\phi}{\sin \phi} \right] = 1.$$

$$\lim_{\phi \rightarrow 0} \left[ \frac{\sin \phi}{\phi} \right] = 1, \quad \sin \phi \doteq \phi \text{ as } \phi \doteq 0.$$

(2) *Value of  $\sin n\phi$ ,  $\cos n\phi$  in terms of  $\sin \phi$ ,  $\cos \phi$ .*

In algebra it is shown that if

$$x + yi = a + bi,$$

then

$$x = a, \quad y = b.$$

**THEOREM.** *If two complex numbers are equal, the real parts are equal and the imaginary parts are equal.*

By DeMoivre's Theorem,

$$(A) \quad (\cos \phi + i \sin \phi)^n = \cos n\phi + i \sin n\phi.$$

But by the Binomial Theorem,

$$\begin{aligned} (B) \quad & (\cos \phi + i \sin \phi)^n = \cos^n \phi + n \cos^{n-1} \phi (i \sin \phi) \\ & + \frac{n(n-1)}{1 \cdot 2} \cos^{n-2} \phi (i \sin \phi)^2 + \frac{n(n-1)(n-2)}{1 \cdot 2 \cdot 3} \cos^{n-3} \phi (i \sin \phi)^3 \\ & + \frac{n(n-1)(n-2)(n-3)}{1 \cdot 2 \cdot 3 \cdot 4} \cos^{n-4} \phi (i \sin \phi)^4 + \dots, \end{aligned}$$

the series terminating if  $n$  is a positive integer, and becoming infinite if  $n$  be a fraction or negative. Now  $i^2 = -1$ ,  $i^3 = -i$ ,  $i^4 = 1$ ,  $\dots$ ; hence, the first, third, fifth,  $\dots$ , terms of the right member of (B) are free of  $i$ , and the even terms contain  $i$ . The right members of (A) and (B) are equal. Equating the real and imaginary parts, respectively, we have

$$\begin{aligned} (C) \quad \cos n\phi &= \cos^n \phi - \frac{n(n-1)}{1 \cdot 2} \cos^{n-2} \phi \sin^2 \phi \\ &+ \frac{n(n-1)(n-2)(n-3)}{1 \cdot 2 \cdot 3 \cdot 4} \cos^{n-4} \phi \sin^4 \phi - \dots, \end{aligned}$$

$$(D) \sin n\phi = n \sin^{n-1} \phi \cos \phi - \frac{n(n-1)(n-2)}{1 \cdot 2 \cdot 3} \cos^{n-3} \phi \sin^3 \phi \\ + \frac{n(n-1)(n-2)(n-3)(n-4)}{1 \cdot 2 \cdot 3 \cdot 4 \cdot 5} \cos^{n-5} \phi \sin^5 \phi - \dots$$

If in (C), (D) we give  $n$  the values 2, 3, 4, ..., we may obtain the ordinary expressions for  $\sin 2\phi$ ,  $\cos 2\phi$ ;  $\sin 3\phi$ ,  $\cos 3\phi$ ; etc., in terms of  $\sin \phi$ ,  $\cos \phi$ . See §§ 35, 36.

EXAMPLES. 1. Show from (C)  $\cos 2\phi = \cos^2 \phi - \sin^2 \phi$ ,  $n = 2$ .

2. Show from (D)  $\sin 2\phi = 2 \sin \phi \cos \phi$ .

3. Show  $\cos 3\phi = 4 \cos^3 \phi - 3 \cos \phi$ .

4. Show  $\sin 3\phi = 3 \sin \phi - 4 \sin^3 \phi$ .

(3) *Trigonometric series.* In formulas (C), (D) above, let us substitute  $n\phi = x$ , or  $n = \frac{x}{\phi}$ , and we have

$$(C') \cos x = \cos^n \phi - \frac{\frac{x}{\phi} \left( \frac{x}{\phi} - 1 \right)}{1 \cdot 2} \cos^{n-2} \phi \sin^2 \phi + \dots \\ = \cos^n \phi - \frac{x(x-\phi)}{1 \cdot 2} \cos^{n-2} \phi \left( \frac{\sin \phi}{\phi} \right)^2 + \dots,$$

$$(D') \sin x = \frac{x}{\phi} \cos^{n-1} \phi \sin \phi - \frac{\frac{x}{\phi} \left( \frac{x}{\phi} - 1 \right) \left( \frac{x}{\phi} - 2 \right)}{1 \cdot 2 \cdot 3} \cos^{n-3} \phi \sin^3 \phi + \dots \\ = x \cos^{n-1} \phi \left( \frac{\sin \phi}{\phi} \right) - \frac{x(x-\phi)(x-2\phi)}{1 \cdot 2 \cdot 3} \cos^{n-3} \phi \left( \frac{\sin \phi}{\phi} \right)^3 + \dots$$

Now let  $n \doteq \infty$  in such manner that  $n\phi \doteq x$ , then  $\frac{\sin \phi}{\phi} \doteq 1$ , see (1) above, and (C'), (D') become the *infinite trigonometric series*

$$\text{I. } \cos x = 1 - \frac{x^2}{2} + \frac{x^4}{4} - \frac{x^6}{6} + \dots,$$

$$\text{II. } \sin x = x - \frac{x^3}{3} + \frac{x^5}{5} - \frac{x^7}{7} + \dots,$$

where  $\underline{2} = 1 \cdot 2$ ,  $\underline{3} = 1 \cdot 2 \cdot 3$ ,  $\underline{4} = 1 \cdot 2 \cdot 3 \cdot 4$ , etc., these symbols being read *factorial two*, *factorial three*, *factorial four*, etc.

Dividing  $\sin x$  by  $\cos x$  and  $\cos x$  by  $\sin x$ , we find

$$\text{III. } \tan x = x + \frac{x^3}{3} + \frac{2x^5}{15} + \frac{17x^7}{315} + \dots,$$

$$\text{IV. } \cot x = \frac{1}{x} - \frac{x}{3} + \frac{x^3}{45} - \frac{2x^5}{945} + \dots.$$

The series for  $\cos x$  and  $\sin x$  are convergent for any value of  $x$ . In the expansion for any trigonometric function the *radian measure of  $x$*  must be used in the series.

Tables of the numerical values of the trigonometric functions for any set of angles may be computed by means of the series I, II, III.

EXAMPLES. 1. Compute  $\sin 10^\circ$  correct to four decimals.

$$\left(x = \frac{\pi}{18} = 0.17453\right).$$

2. Compute  $\sin 12^\circ$ .  $\left(x = \frac{\pi}{15} = 0.20944\right).$

3. Compute  $\cos 10^\circ$ ,  $\tan 10^\circ$ .

4. Compute  $\sin 20^\circ$  from Ex. 1 and 3.

5. Find  $\sin 80^\circ$ ,  $\cos 80^\circ$ ,  $\cos 78^\circ$ ,  $\cos 70^\circ$ .

(4) *Trigonometric products.*  $\sin x = 0$  when

$$x = 0, x = \pm \pi, x = \pm 2\pi, x = \pm 3\pi, \dots.$$

This fact suggests that  $\sin x$  can be expressed as a product of factors, and indeed an infinite number of factors. Likewise,  $\cos x = 0$ , when

$$x = \pm \frac{\pi}{2}, x = \pm \frac{3\pi}{2}, x = \pm \frac{5\pi}{2}, \dots.$$

Arranging the factors properly,

$$\sin x = x \left\{ 1 - \left(\frac{x}{\pi}\right)^2 \right\} \left\{ 1 - \left(\frac{x}{2\pi}\right)^2 \right\} \left\{ 1 - \left(\frac{x}{3\pi}\right)^2 \right\} \dots,$$

$$\cos x = \left\{ 1 - \left(\frac{2x}{\pi}\right)^2 \right\} \left\{ 1 - \left(\frac{2x}{3\pi}\right)^2 \right\} \left\{ 1 - \left(\frac{2x}{5\pi}\right)^2 \right\} \dots.$$

**70. Summation of Series.** In analysis it sometimes becomes necessary to sum the following series :

$$(1) S_1 = \sin \theta + \sin (\theta + \alpha) + \sin (\theta + 2 \alpha) + \dots \\ + \sin [\theta + (n - 1) \alpha],$$

$$(2) S_2 = \cos \theta + \cos (\theta + \alpha) + \cos (\theta + 2 \alpha) + \dots \\ + \cos [\theta + (n - 1) \alpha].$$

$S_1$  is a series of  $n$  sines in which the angles are in arithmetical progression, the common difference being  $\alpha$ .  $S_2$  is a similar series of cosines.

To find the sum  $S_1$ , multiply both members by  $2 \sin \frac{\alpha}{2}$ .

$$2 \sin \frac{\alpha}{2} S_1 = 2 \sin \frac{\alpha}{2} \sin \theta + 2 \sin \frac{\alpha}{2} \sin (\theta + \alpha) + \dots \\ + 2 \sin \frac{\alpha}{2} \sin [\theta + (n - 1) \alpha]$$

$$= \left\{ \cos \left( \theta - \frac{\alpha}{2} \right) - \cos \left( \theta + \frac{\alpha}{2} \right) \right\} + \left\{ \cos \left( \theta + \frac{\alpha}{2} \right) - \cos \left( \theta + \frac{3}{2} \alpha \right) \right\} \\ + \left\{ \cos \left( \theta + \frac{3}{2} \alpha \right) - \cos \left( \theta + \frac{5}{2} \alpha \right) \right\} + \dots \dots \dots \\ + \left\{ \cos \left( \theta + \frac{2n-3}{2} \alpha \right) - \cos \left( \theta + \frac{2n-1}{2} \alpha \right) \right\}, \quad \S 39 (22')$$

$$= \cos \left( \theta - \frac{\alpha}{2} \right) - \cos \left( \theta + \frac{2n-1}{2} \alpha \right)$$

$$= 2 \sin \left[ \theta + (n-1) \frac{\alpha}{2} \right] \sin \frac{n\alpha}{2}.$$

Dividing by  $2 \sin \frac{\alpha}{2}$ , we have

$$S_1 = \frac{\sin \left[ \theta + (n-1) \frac{\alpha}{2} \right] \sin \frac{n\alpha}{2}}{\sin \frac{\alpha}{2}}.$$



In a similar manner, by multiplying  $S_2$  by  $2 \sin \frac{\alpha}{2}$  and separating the double products as in  $S_1$ , we may reduce the value of  $S_2$  to

$$S_2 = \cos \theta + \cos(\theta + \alpha) + \cos(\theta + 2\alpha) + \dots + \cos[\theta + (n-1)\alpha]$$

$$= \frac{\cos\left[\theta + (n-1)\frac{\alpha}{2}\right] \sin \frac{n\alpha}{2}}{\sin \frac{\alpha}{2}}.$$

### EXAMPLES

Verify the following :

$$1. \sin x + \sin\left(x + \frac{\pi}{3}\right) + \sin\left(x + \frac{2\pi}{3}\right) + \dots + \sin\left[x + (n-1)\frac{\pi}{3}\right]$$

$$= 2 \sin\left[x + (n-1)\frac{\pi}{6}\right] \sin \frac{n\pi}{6}.$$

[SUGGESTION. Common difference =  $\frac{\pi}{3}$ , compare  $S_1$ .]

$$2. \cos x + \cos\left(x - \frac{\pi}{3}\right) + \cos\left(x - \frac{2\pi}{3}\right) + \dots + \cos\left[x - (n-1)\frac{\pi}{3}\right]$$

$$= -2 \cos\left[x - (n-1)\frac{\pi}{6}\right] \sin\left(-\frac{n\pi}{6}\right).$$

[SUGGESTION. The common difference is  $-\frac{\pi}{3}$ ; apply  $S_2$  with  $\alpha = -\frac{\pi}{3}$ .]

$$3. \sin x + \sin 2x + \sin 3x + \dots + \sin nx = \frac{\sin(n+1)\frac{x}{2} \sin \frac{nx}{2}}{\sin \frac{x}{2}}.$$

$$4. \cos x + \cos 2x + \cos 3x + \dots + \cos nx = \frac{\cos(n+1)\frac{x}{2} \sin \frac{nx}{2}}{\sin \frac{x}{2}}.$$

$$5. \sin x + \sin 3x + \sin 5x + \dots + \sin(2n-1)x = \frac{\sin^2 nx}{\sin x}.$$

$$\begin{aligned} 6. \quad \cos x + \cos 3x + \cos 5x + \cdots + \cos (2n-1)x &= \frac{\cos nx \sin nx}{\sin x} \\ &= \frac{\sin 2nx}{2 \sin x}. \end{aligned}$$

$$7. \quad \sin 2x + \sin 4x + \sin 6x + \cdots + \sin 2nx = \frac{\sin(n+1)x \sin nx}{\sin x}.$$

$$\begin{aligned} 8. \quad \cos 2x + \cos 4x + \cos 6x + \cdots + \cos 2nx \\ = \frac{\cos(n+1)x \sin nx}{\sin x}. \end{aligned}$$

$$\begin{aligned} 9. \quad \sin^2 x + \sin^2(x+\alpha) + \sin^2(x+2\alpha) + \cdots + \sin^2[x+(n-1)\alpha] \\ = \frac{n}{2} - \frac{\cos[2x+(n-1)\alpha] \sin n\alpha}{2 \sin \alpha}. \end{aligned}$$

[SUGGESTION. Multiply this series by 2 and separate each term thus:

$$2 \sin^2 x = 1 - \cos 2x, \quad 2 \sin^2(x+\alpha) = 1 - \cos(2x+2\alpha), \quad \dots$$

$$2 \sin^2[x+(n-1)\alpha] = 1 - \cos[2x+(n-1)2\alpha];$$

add and sum the cosines as in Ex. 8.]

$$\begin{aligned} 10. \quad \cos^2 x + \cos^2(x+\alpha) + \cos^2(x+2\alpha) + \cdots \\ + \cos^2[x+(n-1)\alpha] = \frac{n}{2} + \frac{\cos[2x+(n-1)\alpha] \sin n\alpha}{2 \sin \alpha}. \end{aligned}$$

**71. The Exponential Series.** If we take the Binomial Series,

$$(1+z)^n = 1 + nz + \frac{n(n-1)}{2} z^2 + \frac{n(n-1)(n-2)}{3} z^3 + \dots,$$

and substitute

$$z = \frac{1}{m}, \quad n = mx,$$

we find

$$\left(1 + \frac{1}{m}\right)^{mx} = \left\{ \left(1 + \frac{1}{m}\right)^m \right\}^x = 1 + mx \left(\frac{1}{m}\right) + \frac{mx(mx-1)}{2} \left(\frac{1}{m}\right)^2 + \dots$$

Now, divide the numerator and denominator of the respective fractions by  $m$ ,  $m^2$ ,  $m^3$ , ..., and finally let  $m = \infty$ ; then we have

$$\lim_{m=\infty} \left(1 + \frac{1}{m}\right)^{mx} = 1 + x + \frac{x^2}{2} + \frac{x^3}{3} + \frac{x^4}{4} + \dots$$

The numerical value of this series, when  $x = 1$ , is denoted by  $e$ .

$$(A) e = 1 + 1 + \frac{1}{2} + \frac{1}{3} + \frac{1}{4} + \dots = 2.7182818 \dots$$

$$(B) e^x = 1 + x + \frac{x^2}{2} + \frac{x^3}{3} + \frac{x^4}{4} + \dots = (2.7182818 \dots)^x$$

Series (B) is called the *exponential series*;  $e$  is the base of the *Napierian Logarithmic system*.

**72. Euler's Formulas.** Series (B) readily identifies the exponential functions with the trigonometric functions. In (B) substitute

$$x = i\theta, \text{ where } i = \sqrt{-1}, i^2 = -1, \dots, \quad \S 65$$

$$e^{i\theta} = 1 + i\theta - \frac{\theta^2}{2} - \frac{i\theta^3}{3} + \frac{\theta^4}{4} + \frac{i\theta^5}{5} - \dots$$

$$= 1 - \frac{\theta^2}{2} + \frac{\theta^4}{4} - \dots + i\left(\theta - \frac{\theta^3}{3} + \frac{\theta^5}{5} - \dots\right)$$

$$= \cos \theta + i \sin \theta, \quad \S 69, \text{ I, II.}$$

Changing  $i$  to  $-i$ ,

$$e^{-i\theta} = \cos \theta - i \sin \theta.$$

Subtracting and dividing by  $2i$ , and adding and dividing by 2, respectively, we have Euler's Formulas for  $\sin \theta$  and  $\cos \theta$ .  
 $\tan \theta = \sin \theta \div \cos \theta$ .

$$\text{V. } \sin \theta = \frac{e^{i\theta} - e^{-i\theta}}{2i}.$$

$$\text{VI. } \cos \theta = \frac{e^{i\theta} + e^{-i\theta}}{2}.$$

$$\text{VII. } \tan \theta = \frac{e^{i\theta} - e^{-i\theta}}{i(e^{i\theta} + e^{-i\theta})}.$$

The reciprocals of these fractions define the  $\csc \theta$ ,  $\sec \theta$ ,  $\cot \theta$ , respectively.

These analytic definitions of  $\sin \theta$ ,  $\cos \theta$ ,  $\tan \theta$ , may be employed instead of the ratio definitions given in § 2.

## EXERCISES

Prove the following identities by use of Euler's definitions, V, VI, VII.

1.  $\sin 2\theta = 2 \sin \theta \cos \theta$ .
2.  $\cos 2\theta = \cos^2 \theta - \sin^2 \theta$ .
3.  $\sin(x + y) = \sin x \cos y + \cos x \sin y$ .
4.  $\sin x + \sin y = 2 \sin \frac{x+y}{2} \cos \frac{x-y}{2}$ .
5.  $\sin^2 x + \cos^2 x = 1$ .
6.  $\sec^2 x - \tan^2 x = 1$ .

7. Write trigonometric values for each of the following :

- (1)  $e^{i\frac{\pi}{2}}$ ; (2)  $e^{i\pi}$ ; (3)  $e^{i\frac{3\pi}{2}}$ ; (4)  $e^{i\frac{\pi}{4}}$ ; (5)  $e^{-i\pi}$ ; (6)  $e^{-i\frac{\pi}{3}}$ ;  
 (7)  $e^{-i\frac{\pi}{2}}$ ; (8)  $e^{i(\pi+a)}$ .

8. Express in exponential notation : (1)  $\cos 30^\circ + i \sin 30^\circ$ ;

- (2)  $\frac{1+i}{\sqrt{2}}$ ; (3)  $\frac{-1+\sqrt{3}i}{2}$ ; (4)  $\frac{\sqrt{3}+i}{2}$ ; (5)  $\frac{-1+i}{\sqrt{2}}$ ;  
 (6)  $e^{2\left(\frac{1-\sqrt{3}i}{2}\right)}$ .

9. Prove the following: (1)  $e^{i(a+2\pi)} = e^{ia}$ ; (2)  $e^{2+i\pi} = -e^2$ ;  
 (3)  $e^{2+i\frac{\pi}{2}} = ie^2$ ; (4)  $e^{2+2\pi i} = e^2$ .

10. Find approximately the value of  $\sqrt{e}$  by substituting  $x = \frac{1}{2}$  in (B), § 71.

73. The Hyperbolic Functions. In V, VI, VII, § 72, let  $\theta = ix$ ,

$$\sin ix = \frac{e^{-x} - e^x}{2i} = i \frac{e^x - e^{-x}}{2}, \quad \cos ix = \frac{e^{-x} + e^x}{2},$$

$$\tan ix = \frac{e^{-x} - e^x}{i(e^{-x} + e^x)} = i \frac{e^x - e^{-x}}{e^x + e^{-x}}.$$

The fractions  $\frac{e^x - e^{-x}}{2}$ ,  $\frac{e^x + e^{-x}}{2}$ ,  $\frac{e^x - e^{-x}}{e^x + e^{-x}}$  are taken as definitions of the *hyperbolic sine of x*, *hyperbolic cosine of x*, and *hyperbolic tangent of x*, respectively. These functions are written:

VIII.  $\sinh x = \frac{e^x - e^{-x}}{2}$ .

IX.  $\cosh x = \frac{e^x + e^{-x}}{2}$ .

X.  $\tanh x = \frac{\sinh x}{\cosh x} = \frac{e^x - e^{-x}}{e^x + e^{-x}}$ .

(1) *Relations between trigonometric and hyperbolic functions.*  
 From the above definitions it is seen that

$\sin ix = i \sinh x,$	$\cot ix = -i \coth x,$
$\cos ix = \cosh x,$	$\sec ix = \operatorname{sech} x,$
$\tan ix = i \tanh x,$	$\csc ix = -i \operatorname{csch} x.$

This table of relations enables us to determine the identities existing among the hyperbolic functions, corresponding to the trigonometric identities.

(2) *Identities.* Let the student verify the following identities among the hyperbolic functions:

- |  |  |
|--|--|
| (1) $\cosh^2 x - \sinh^2 x = 1.$   | (6) $\tanh 2x = \frac{2 \tanh x}{1 + \tanh^2 x}.$            |
| (2) $\operatorname{sech}^2 x + \tanh^2 x = 1.$                             | (7) $\sinh(-x) = -\sinh x.$                                  |
| (3) $\operatorname{coth}^2 x - \operatorname{csch}^2 x = 1.$               | (8) $\cosh(-x) = \cosh x.$                                   |
| (4) $\sinh 2x = 2 \sinh x \cosh x.$  | (5) $\cosh 2x = \cosh^2 x + \sinh^2 x.$                      |
| (9) $\sinh(x + y) = \sinh x \cosh y \pm \cosh x \sinh y.$                  | (10) $\cosh(x \pm y) = \cosh x \cosh y \pm \sinh x \sinh y.$ |
| (11) $\tanh(x \pm y) = \frac{\tanh x \pm \tanh y}{1 \pm \tanh x \tanh y}.$ |  |
| (12) $e^x = \cosh x + \sinh x.$  |  |
| (13) $\sinh x + \sinh y = 2 \sinh \frac{x+y}{2} \cosh \frac{x-y}{2}.$      |  |
| (14) $\cosh x - \cosh y = 2 \sinh \frac{x+y}{2} \sinh \frac{x-y}{2}.$      |  |

(3) *Infinite series forms for  $\sinh x$ ,  $\cosh x$ .* Take the series for  $\sin x$ ,  $\cos x$ ,  $\tan x$ , II, I, III, § 69,

$$\sin x = x - \frac{x^3}{\underline{3}} + \frac{x^5}{\underline{5}} - \dots,$$

$$\cos x = 1 - \frac{x^2}{\underline{2}} + \frac{x^4}{\underline{4}} - \dots,$$

$$\tan x = x + \frac{x^3}{3} + \frac{2x^5}{15} + \dots,$$

and replace  $x$  by  $ix$ , giving

$$\sinh x = x + \frac{x^3}{\underline{3}} + \frac{x^5}{\underline{5}} + \dots,$$

$$\cosh x = 1 + \frac{x^2}{\underline{2}} + \frac{x^4}{\underline{4}} + \dots,$$

$$\tanh x = x - \frac{x^3}{3} + \frac{2x^5}{15} - \dots.$$

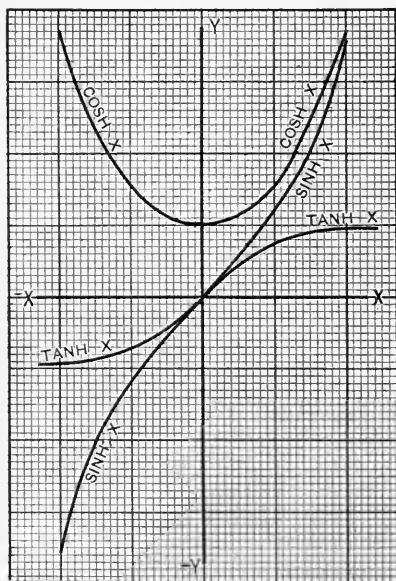


Fig. 51.

(4) *Graphs of the hyperbolic functions.* The numerical values of the hyperbolic functions for various values of the variable  $x$  are collected in Tables of Hyperbolic Functions. The approximate values of  $\sinh x$ ,  $\cosh x$ ,  $\tanh x$  are shown upon the following graphs, Fig. 51, where the ordinates parallel to the  $Y$ -axis are the values of these functions for the corresponding values of  $x$ . The graphs of the  $\operatorname{csch} x$ ,  $\operatorname{sech} x$ , and  $\operatorname{coth} x$  are not shown, but these may be easily constructed upon the same diagram by taking reciprocals of the ordinates of the  $\sinh x$ ,  $\cosh x$ , and  $\tanh x$ , respectively.

reciprocals of the ordinates of the  $\sinh x$ ,  $\cosh x$ , and  $\tanh x$ , respectively.

(5) *The inverse hyperbolic functions.* If we write

$$y = \sinh x = \frac{e^x - e^{-x}}{2},$$

we may express  $x$  in terms of  $y$  by an inverse notation similar to that employed in inverse trigonometric notation.

$$y = \sinh x, \quad x = \sinh^{-1} y.$$

By means of the exponential value of  $\sinh x$ , we may obtain another expression for  $x$  in terms of  $y$ . Thus,

$$\frac{e^x - e^{-x}}{2} = y, \quad e^{2x} - 1 = 2ye^x,$$

or 
$$e^{2x} - 2ye^x - 1 = 0, \text{ a quadratic in } e^x.$$

Solving, 
$$e^x = y \pm \sqrt{y^2 + 1},$$

the negative sign being excluded since  $e^x$  is positive. Take  $\log_e$  of each member.

$$x = \log_e(y + \sqrt{y^2 + 1}) = \sinh^{-1} y.$$

### EXERCISES

Prove the following :

1.  $\cosh^{-1} x = \log_e(x + \sqrt{x^2 - 1})$ .
2.  $\tanh^{-1} x = \frac{1}{2} \log_e \left( \frac{1+x}{1-x} \right)$ .
3.  $\operatorname{sech}^{-1} x = \cosh^{-1} \frac{1}{x} = \log_e \frac{1 + \sqrt{1 - x^2}}{x}$ .
4.  $\sinh^{-1} x = \cosh^{-1} \sqrt{1 + x^2} = \tanh^{-1} \frac{x}{\sqrt{1 + x^2}}$ .
5.  $\tanh^{-1} x + \tanh^{-1} y = \tanh^{-1} \frac{x + y}{1 + xy}$ .
6.  $\cosh 0 = 1, \cosh \frac{\pi i}{2} = 0, \sinh \pi i = 0$ .
7.  $\sinh \frac{\pi i}{2} = i, \cosh \pi i = -1, \tanh 0 = 0$ .
8.  $\sinh 2n\pi i = 0, \cosh 2n\pi i = 1, \tanh n\pi i = 0$ .

**74. The Gudermannian.** If an angle  $\theta$  is related to a number  $x$ , so that

$$\sec \theta = \cosh x,$$

then  $\theta$  is defined by

$$\theta = \text{gudermannian of } x,$$

or briefly,

$$\theta = \text{gd } x = \sec^{-1}(\cosh x).$$

Inversely,

$$x = \text{inverse gudermannian of } \theta,$$

or

$$x = \text{gd}^{-1} \theta = \cosh^{-1}(\sec \theta).$$

When

$$\sec \theta = \cosh x,$$

the following relations are true :

$$\cos \theta = \text{sech } x,$$

$$\sin \theta = \tanh x,$$

$$\tan \theta = \sinh x,$$

$$\csc \theta = \text{coth } x,$$

$$\cot \theta = \text{csch } x,$$

$$\tan \frac{\theta}{2} = \tanh \frac{x}{2}.$$

Any one of these relations defines  $\theta$  as the gudermannian of  $x$ .



# PART II

## SPHERICAL TRIGONOMETRY

### CHAPTER X

#### GENERAL DEFINITIONS. THE RIGHT TRIANGLE

**75. Definitions and Geometric Properties.** From spherical geometry we recall the following facts:

(1) The intersection of the surface of a sphere by a plane through its centre is a great circle.

(2) A great circle divides the surface of a sphere into two equal parts called hemispheres.

(3) Two great circles upon the same sphere divide its surface into four parts each of which is called a **Lune**. In Fig. 52,  $BCB'AB$  is a lune, bounded by the semi-circumferences  $BCB'$  and  $BAB'$ .

(4) The angles of a lune are equal, and are measured by the dihedral angle between the planes of the great circles forming the sides of the lune. In the drawing, angle  $B$  is measured by the dihedral angle  $CBB'A$ . Since tangents to arcs  $BC$ ,  $BA$  at  $B$  are perpendicular to the edge of the dihedral angle, the spherical angle  $B$  is measured by the plane angle between the tangents  $Bt$ ,  $Bt'$  to the arcs  $BC$  and  $BA$  at  $B$ .

(5) Any third great circle will divide a lune into two parts called **spherical triangles**. Thus, arc  $AC$ , Fig. 52, divides the lune into the spherical triangles  $ABC'$  and  $AB'C$ .

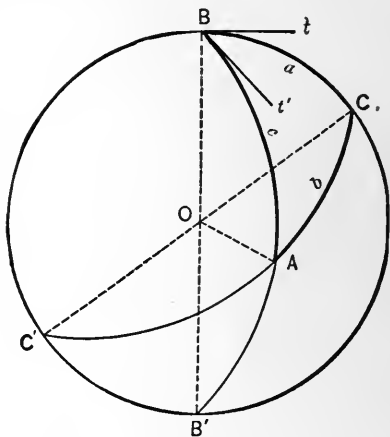


Fig. 52.

(6)  $O$  is the apex of a **spherical pyramid** whose base is the spherical triangle  $ABC$ . The face angles of this pyramid are equal to the corresponding sides (measured in degrees) of the spherical triangle; in Fig. 52,  $a = \angle BOC$ ,  $b = \angle COA$ ,  $c = \angle AOB$ . The dihedral angles of the pyramid are equal to the corresponding angles  $A, B, C$ , of the spherical triangle.

(7) The length of a side  $a$  of a spherical triangle expressed in linear units is given by arc  $a = \text{radius} \times \text{radian measure of } a$ . The length of the radius of the sphere is usually not considered in the trigonometric discussion of a spherical triangle.

(8) A side of a spherical triangle lies between  $0^\circ$  and  $180^\circ$ ; likewise an angle lies between  $0^\circ$  and  $180^\circ$ . The following limitations should be recognized (see notation, Fig. 52):

$$(1) \quad 0^\circ < a + b + c < 360^\circ,$$

$$(2) \quad 180^\circ < A + B + C < 540^\circ.$$

(9) The angles and sides of a spherical triangle are in the same order of magnitude; if  $a > b > c$ , then will  $A > B > C$ .

**76. The Polar Triangle.** To any spherical triangle  $ABC$  there corresponds another called its polar which may be constructed as follows:

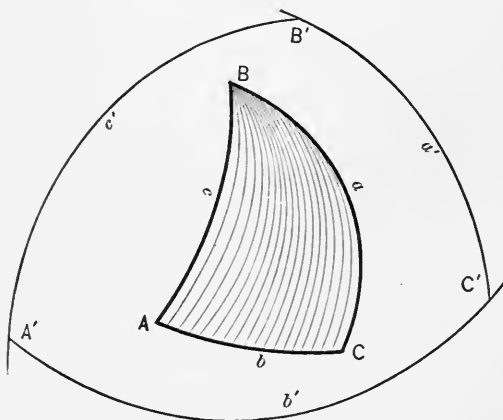


Fig. 53.

take each vertex  $A, B, C$ , as a pole and describe arcs ( $90^\circ$  away)  $B'C', C'A', A'B'$ , forming the spherical triangle  $A'B'C'$ , Fig. 53. The triangle  $A'B'C'$  is the polar of the triangle  $ABC$ .

In geometry it is shown that the sides and angles of a spherical triangle

$ABC$  and the angles and sides of its polar  $A'B'C'$  are related by the following equations:

$$(1) \quad A = 180^\circ - a', \quad B = 180^\circ - b', \quad C = 180^\circ - c',$$

$$(2) \quad a = 180^\circ - A', \quad b = 180^\circ - B', \quad c = 180^\circ - C'.$$

**THEOREM.** *The angles of a spherical triangle are the supplements of the corresponding sides of its polar; the sides of the given triangle are the supplements of the corresponding angles of the polar triangle.*

Polar triangles are so related that the vertices  $A, B, C$ , of one are poles of the corresponding sides  $a', b', c'$  of the other, and the vertices  $A', B', C'$  are poles of  $a, b, c$ .

THE RIGHT SPHERICAL TRIANGLE

**77. Definitions.** If one angle  $C$ , Fig. 54, be  $90^\circ$ , the triangle  $ABC$  is called a *right spherical triangle*. The side  $c$  opposite the right angle is called the *hypotenuse*.

(1) The angles  $A, B$ , may both be acute, both obtuse, or one acute and the other obtuse.

(2) The sides  $a, b$ , lie in the same quadrant as the opposite angles. If  $A > 90^\circ$ ,  $a > 90^\circ$ ; if  $B > 90^\circ$ ,  $b > 90^\circ$ ; if  $A < 90^\circ$ ,  $a < 90^\circ$ ; if  $B < 90^\circ$ ,  $b < 90^\circ$ .

(3) The hypotenuse  $c$  is smaller than  $90^\circ$  if  $A$  and  $B$  are both smaller or both larger than  $90^\circ$ ;  $c$  is larger than  $90^\circ$  if  $A$  is smaller than  $90^\circ$  and  $B$  larger than  $90^\circ$ , or inversely. See § 81.

**78. Trigonometric Relations.** In the spherical triangle  $ABC$ , Fig. 54, let  $C = 90^\circ$ , and let  $A, B$ , be acute. To measure the

angle  $A$  draw at any point  $A'$  in the edge of the dihedral angle  $CAOB$ , a plane perpendicular to  $OA$ ; the traces of this plane upon planes  $OAC$  and  $OAB$  are the lines  $A'C'$ ,  $A'B'$ , and the angle  $B'A'C'$  equals the angle  $A$ . Draw  $B'C'$ . The following

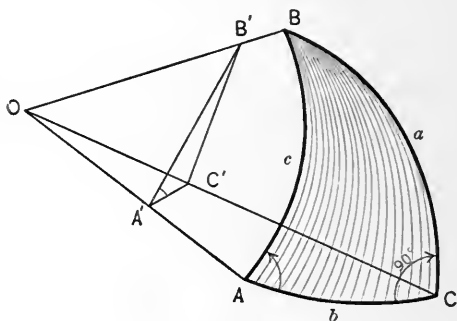


Fig. 54.

are plane right-angled triangles:  $A'C'B'$ ,  $OA'C'$ ,  $OA'B'$ ,  $OC'B'$ .

Defining  $\sin A$ ,  $\cos A$ , and  $\tan A$  from the drawing, we have

$$\sin A = \frac{B' C'}{A' B'} = \frac{B' C'}{A' B'} \times \frac{OB'}{OB'} = \frac{\sin a}{\sin c},$$

$$\cos A = \frac{A' C'}{A' B'} = \frac{A' C'}{A' B'} \times \frac{OA'}{OA'} = \frac{\tan b}{\tan c},$$

$$\tan A = \frac{B' C'}{A' C'} = \frac{B' C'}{A' C'} \times \frac{OC'}{OC'} = \frac{\tan a}{\sin b}.$$

Also, from triangle  $B' OA'$ ,

$$\cos B' OA' = \cos c = \frac{OA'}{OB'} = \frac{OA'}{OB'} \times \frac{OC'}{OC'} = \cos a \cos b.$$

By drawing perpendiculars to the edge  $OB$  and constructing a measure of angle  $B$ , we could derive similar results for the functions of  $B$ , namely :

$$\sin B = \frac{\sin b}{\sin c}, \quad \cos B = \frac{\tan a}{\tan c}, \quad \tan B = \frac{\tan b}{\sin a}.$$

Taking the reciprocals of  $\tan A$  and  $\tan B$ , and multiplying their values together,

$$\cot A \cot B = \frac{\sin b}{\tan a} \times \frac{\sin a}{\tan b} = \cos a \cos b.$$

Hence,  $\cos c = \cos a \cos b = \cot A \cot B$ .

Again,

$$\begin{aligned} \cos A &= \frac{\tan b}{\tan c} = \frac{\sin b}{\cos b} \times \frac{\cos c}{\sin c} = \frac{\sin b}{\cos b} \times \frac{\cos a \cos b}{\sin c} = \frac{\sin b}{\sin c} \times \cos a \\ &= \sin B \cos a. \end{aligned}$$

Similarly,  $\cos B = \sin A \cos b$ .

**79. Important Formulas.** Collecting the results of § 78, we have the following formulas relating to the right spherical triangle :

$$(1) \sin A = \frac{\sin a}{\sin c},$$

$$(5) \sin B = \frac{\sin b}{\sin c},$$

$$(2) \cos A = \frac{\tan b}{\tan c},$$

$$(6) \cos B = \frac{\tan a}{\tan c},$$

$$(3) \tan A = \frac{\tan a}{\sin b},$$

$$(7) \tan B = \frac{\tan b}{\sin a},$$

$$(4) \cos A = \sin B \cos a,$$

$$(8) \cos B = \sin A \cos b,$$

$$(9) \cos c = \cos a \cos b = \cot A \cot B.$$

These formulas are true for any right spherical triangle, whether the angles and sides be acute or obtuse.

It should be noticed that the values of sine, cosine, and tangent, formulas (1), (2), (3), (5), (6), (7), are very similar to the definitions of those functions in a plane triangle. This similarity enables one to remember the trigonometric relations of the angles and sides of the right spherical triangle.

*A right spherical triangle may be completely solved for all its parts when any two parts, other than the right angle, are known.*

**80. Napier's Rules of Circular Parts.** Another method of remembering the formulas (1) to (9) of § 79 is embraced in what are called *Napier's Rules of Circular Parts*.

Let a right spherical triangle be given with the usual notation, Fig. 54, the right angle being  $C$ . Then write  $a, b, \text{complement of } A, \text{ complement of } c, \text{ complement of } B$ , Fig. 55. The notation shown on the drawing consists of five parts, known as *Napier's Circular Parts*.

If any part as  $\text{co. } c$  be taken as a *middle part*, the next two parts to the right and left,  $\text{co. } A, \text{co. } B$  are called the *adjacent parts*, and the remaining two parts,  $a, b$ , are called the *opposite parts*.

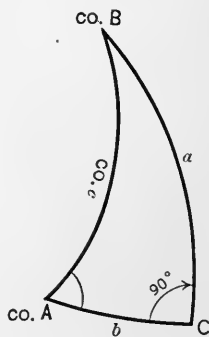


Fig. 55.

**NAPIER'S RULES.** (1) *The sine of the middle part is equal to the product of the tangents of the adjacent parts.*

$$\sin(\text{mid. pt.}) = \tan(\text{adj. pt.}) \times \tan(\text{adj. pt.}).$$

(2) *The sine of the middle part is equal to the product of the cosines of the opposite parts.*

$$\sin(\text{mid. pt.}) = \cos(\text{op. pt.}) \times \cos(\text{op. pt.}).$$

As illustration of these rules, identify each of the following with some one of the formulas (1) to (9), § 79 :

1.  $\sin(\text{co. } c) = \cos c =$
2.  $\sin(a) =$
3.  $\sin(\text{co. } B) = \cos B =$
4.  $\sin(b) =$
5.  $\sin(\text{co. } A) = \cos A =$

**81. Relative Dimensions of Sides and Angles.** (1) Given  $a < 90^\circ$ ,  $b < 90^\circ$ . In this case,

$$\overset{(+)}{\cos c} = \overset{+}{\cos a} \overset{+}{\cos b}$$

shows  $\cos c$  *positive*; hence,  $c < 90^\circ$ .

$$\text{Also, } \overset{(+)}{\cos A} = \frac{\overset{+}{\tan b}}{\overset{+}{\tan c}}, \quad \overset{(+)}{\cos B} = \frac{\overset{+}{\tan c}}{\overset{+}{\tan a}}$$

show  $\cos A$  and  $\cos B$  *positive*; hence  $A < 90^\circ$ ,  $B < 90^\circ$ .

(2) Given  $a > 90^\circ$ ,  $b < 90^\circ$ . Formula (9), § 79,

$$\overset{(-)}{\cos c} = \overset{-}{\cos a} \overset{+}{\cos b},$$

shows  $\cos c$  *negative*; hence,  $c > 90^\circ$ , the supplement of the tabular angle determined by formula (9).

Formulas (2), (6), § 79,

$$\overset{(-)}{\cos A} = \frac{\overset{+}{\tan b}}{\overset{-}{\tan c}}, \quad \overset{+}{\cos B} = \frac{\overset{-}{\tan a}}{\overset{-}{\tan c}}$$

show  $A > 90^\circ$ ,  $B < 90^\circ$ .

(3) Given  $a > 90^\circ$ ,  $b > 90^\circ$ . Formula (9),

$$\overset{(+)}{\cos c} = \overset{-}{\cos a} \overset{-}{\cos b},$$

determines  $\cos c$  *positive*; hence  $c < 90^\circ$ .

$$\text{Also, } \overset{(-)}{\cos A} = \frac{\overset{-}{\tan a}}{\overset{+}{\tan c}}, \quad \overset{(-)}{\cos B} = \frac{\overset{-}{\tan b}}{\overset{+}{\tan c}}$$

show that  $\cos A$ ,  $\cos B$  are negative; hence,  $A > 90^\circ$ ,  $B > 90^\circ$ .

**THEOREM.** *In any right spherical triangle the hypotenuse  $c$  is acute if  $a$  and  $b$  lie in the same quadrant;  $c$  is obtuse if  $a$  and  $b$  lie in opposite quadrants.*

**82. The Isosceles and Quadrantal Triangles.** If two sides of a spherical triangle be equal, the opposite angles are equal, and

the triangle is *isosceles*. An isosceles spherical triangle may be divided into two symmetrical right triangles,  $ADB$ ,  $CDB$ , by drawing the arc of a great circle from  $B$ , Fig. 56, perpendicular upon side  $b$ . This perpendicular  $p$  bisects the angle  $B$  and the opposite side  $b$ . The solution of an isosceles triangle  $ABC$  depends upon the solution of the two right triangles  $ADB$ ,  $CDB$ .

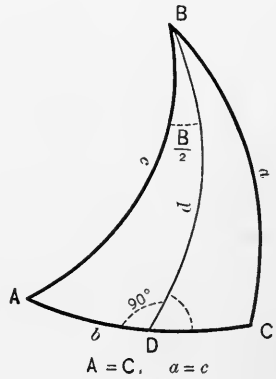


Fig. 56.

If a side be  $90^\circ$ , the triangle is called a *quadrantal spherical triangle*. The solution of a quadrantal triangle may be made to depend upon the solution of a right spherical triangle by taking the polar triangle, one of whose angles will be  $90^\circ$ , the supplement of the given side. See § 76.

*To solve a quadrantal triangle, solve its polar and take the supplement of each part of the polar.*

**83. Solution of Right Spherical Triangles.** Six cases arise in the solution of right spherical triangles.

- CASE I. Given two sides,  $a, b$ .
- CASE II. Given one side and the hypotenuse,  $a, c$ .
- CASE III. Given two angles,  $A, B$ .
- CASE IV. Given one angle and the adjacent side,  $A, b$ .
- CASE V. Given one angle and the opposite side,  $A, a$ .

Double solution.

- CASE VI. Given one angle and the hypotenuse,  $A, c$ .

That Case V has a double solution may be seen from the drawing, Fig. 57.

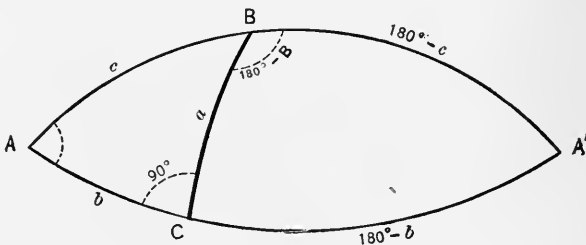


Fig. 57.

In calculating the unknown parts of a triangle falling under any one of the above Cases, (1) either select a proper set of formulas, § 79, or employ Napier's Rules to obtain the required trigonometric relations; (2) use logarithms in performing the operations of multiplication and division.

### EXERCISES

Solve the following right spherical triangles for each unknown part:

1.  $a = 64^\circ 20'$ ,  $b = 70^\circ 24'$ .
2.  $a = 49^\circ 28'$ ,  $c = 65^\circ 25'$ .
3.  $b = 100^\circ 10'$ ,  $A = 38^\circ 47'$ .
4.  $a = 120^\circ 30' 10''$ ,  $B = 98^\circ 27' 10''$ .
5.  $c = 110^\circ 30' 10''$ ,  $A = 46^\circ 21' 30''$ .
6.  $A = 41^\circ 48'$ ,  $B = 80^\circ 30'$ .
7.  $b = 140^\circ 28'$ ,  $c = 110^\circ 29'$ .
8.  $b = 72^\circ 20' 10''$ ,  $B = 80^\circ 10' 20''$ .
9.  $a = 130^\circ 20'$ ,  $b = 105^\circ 48'$ .
10.  $A = 98^\circ 25'$ ,  $B = 104^\circ 10'$ .

11. Find the perimeter of the right triangle in which  $a = 48^\circ$ ,  $b = 60^\circ$ , the radius of the sphere being 15 in.

12. Find the area of the right spherical triangle determined by  $a = 36^\circ$ ,  $A = 36^\circ$ , the radius of the sphere being 30 in.

NOTE. The surface of a sphere =  $4\pi R^2$ .

13. If a spherical triangle have two right angles, show that the opposite sides are quadrants, and explain a method for finding its area when the radius is known.

14. Solve the isosceles triangles:

- (1)  $A = B = 54^\circ 28'$ ,  $C = 68^\circ$ .
- (2)  $A = 75^\circ 34'$ ,  $a = 38^\circ 28'$ ,  $b = c$ .
- (3)  $B = 98^\circ 24'$ ,  $a = c = 124^\circ$ .

15. Solve the quadrantal triangles:

- (1)  $a = 90^\circ$ ,  $B = 48^\circ$ ,  $C = 38^\circ$ .
- (2)  $A = 100^\circ$ ,  $c = 98^\circ$ ,  $b = 90^\circ$ .



16. A vessel sails directly east from Sandy Hook (latitude,  $40^{\circ} 28' N.$ ; longitude,  $74^{\circ} 1' W.$ ) and continues upon the arc of a great circle. Find the latitude at which it crosses the meridian of  $65^{\circ} W.$  What will be the course of the vessel when crossing that meridian?

NOTE. See § 91 for definitions.

17. If a vessel sails directly west along an arc of a great circle from San Francisco (latitude,  $37^{\circ} 48' N.$ ; longitude,  $122^{\circ} 28' W.$ ), what distance will it have sailed and what direction will be its course on arriving at the 180th meridian?

NOTE. Take the radius of the earth as 3956 mi.

18. A ship sails due east from Boston (latitude,  $42^{\circ} 21' N.$ ; longitude,  $71^{\circ} 4' W.$ ) upon the arc of a great circle at the rate of 16 knots per hour. Find the latitude and longitude of the ship after 48 hours' sailing.

NOTE. 1 knot = 1 nautical mile = 1 geographical mile =  $1'$  arc of a great circle upon the earth.

19. A triangular pyramid  $O-ABC$  has the dihedral angle along the edge  $OC = 90^{\circ}$ , and the face angles  $AO C = 48^{\circ}$ , and  $BO C = 69^{\circ}$ . Find the face angle  $BOA$ , and the dihedral angles along the edges  $OA$  and  $OB$ .

20. If the three edges of a cube through a point  $O$  are  $OA$ ,  $OB$ , and  $OC$ , find the dihedral angle made by the plane  $ABC$  with either face of the cube.

## CHAPTER XI

### THE OBLIQUE SPHERICAL TRIANGLE

**84. The Theorem of Sines.** Let a spherical triangle be represented by  $ABC$ , Fig. 58. If no angle be a right angle, the triangle is called *oblique*.

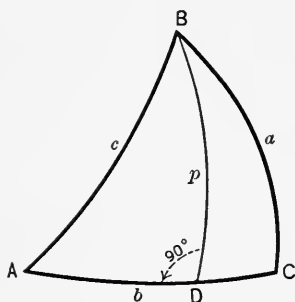


Fig. 58.

Draw through angle  $B$  the arc of a great circle to meet the side  $b$  at right angles in  $D$ . Then  $ADB$ ,  $CDB$  are right spherical triangles. From § 79,

$$\sin A = \frac{\sin p}{\sin c}, \quad \sin C = \frac{\sin p}{\sin a}.$$

Dividing, we have,

$$\frac{\sin A}{\sin C} = \frac{\sin a}{\sin c}.$$

By drawing an arc through  $A$  perpendicular to  $a$ , we may derive similarly,

$$\frac{\sin C}{\sin B} = \frac{\sin c}{\sin b}.$$

Rearranging these two formulas,

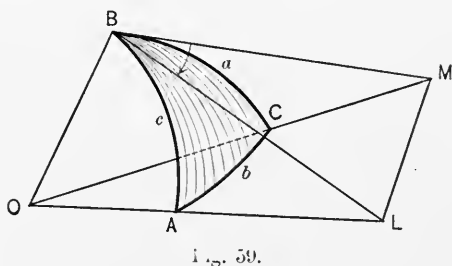
$$(1) \quad \frac{\sin A}{\sin a} = \frac{\sin B}{\sin b} = \frac{\sin C}{\sin c}.$$

**THEOREM OF SINES.** *In any spherical triangle the sines of the angles are proportional to the sines of the opposite sides.*

Observe the similarity to the corresponding theorem in plane trigonometry.

The theorem of sines enables us to compute a fourth part, when two angles and a side opposite one of the angles are known, or when two sides and an angle opposite one of the given sides are known.

85. The Theorem of Cosines. Sides and One Angle. The angle  $B$  in the triangle  $ABC$ , Fig. 59, is measured by the plane angle between the tangents to  $AB$  and  $CB$  at  $B$ . Let these tangents intersect the radii  $OA$  and  $OC$  produced in  $L$  and  $M$ .



Then from the plane triangles  $LOM$  and  $LBM$ , we have

$$\overline{LM}^2 = \overline{LO}^2 + \overline{MO}^2 - 2 LO \times MO \times \cos b,$$

$$\overline{LM}^2 = \overline{LB}^2 + \overline{MB}^2 - 2 LB \times MB \times \cos B$$

Subtracting,

$$0 = \overline{LO}^2 - \overline{LB}^2 + \overline{MO}^2 - \overline{MB}^2 - 2 LO \times MO \times \cos b + 2 LB \times MB \times \cos B,$$

or,

$$0 = \overline{OB}^2 + \overline{OB}^2 - 2 LO \times MO \times \cos b + 2 LB \times MB \times \cos B.$$

Transposing the negative term and dividing by  $2 LO \times MO$ , we find,

$$\cos b = \frac{\overline{OB}^2}{LO \times MO} + \frac{LB}{LO} \times \frac{MB}{MO} \times \cos B,$$

and substituting the ratios from the right triangles  $LBO$ ,  $MBO$ ,

$$(2) \quad \cos b = \cos c \cos a + \sin c \sin a \cos B.$$

Making symmetrical interchanges of the letters,

$$(3) \quad \cos c = \cos a \cos b + \sin a \sin b \cos C.$$

$$(4) \quad \cos a = \cos b \cos c + \sin b \sin c \cos A.$$

**THEOREM OF COSINES.** *In any spherical triangle, the cosine of any side equals the product of the cosines of the other sides increased by the product of their sines multiplied by the cosine of the included angle.*

Formulas (2), (3), or (4) will determine a side when the other two sides and their included angle are given; or they will determine the angles when the three sides are given. These formulas are not adapted to logarithmic calculation.

**MODIFIED FORMULA.** If one side only be required, with two sides and the included angle given, it is sometimes convenient to modify formulas (2), (3), (4) so as to permit logarithmic calculation.

For example, let  $b, c, A$  be given, then  $a$  is determined by (4),

$$\cos a = \cos b \cos c + \sin b \sin c \cos A.$$

Let

$$\tan \theta = \frac{\cos b}{\sin b \cos A} = \frac{\cot b}{\cos A}; \quad (A)$$

then,

$$\sin \theta = \frac{\cos b}{(\cos^2 b + \sin^2 b \cos^2 A)^{\frac{1}{2}}}.$$

With this substitution,  $\cos a$  may be written

$$\cos a = \frac{\cos b}{\sin \theta} \sin(\theta + c). \quad (B)$$

To find side  $a$ , first find  $\theta$  by equation (A), then substitute  $\theta$  in (B) and determine  $a$ . Use logarithms.

**86. The Theorem of Cosines. Angles and One Side.** By substituting in

$$\cos b = \cos c \cos a + \sin c \sin a \cos B, \quad \S 85 (2)$$

the values

$$b = 180^\circ - B', \quad c = 180^\circ - C', \quad a = 180^\circ - A', \quad B = 180^\circ - b',$$

where  $B', C', A', b'$  belong to the polar triangle, we find

$$\begin{aligned} \cos(180^\circ - B') &= \cos(180^\circ - C') \cos(180^\circ - A') \\ &\quad + \sin(180^\circ - C') \sin(180^\circ - A') \cos(180^\circ - b'); \end{aligned}$$

reducing, and changing signs,

$$\cos B' = -\cos C' \cos A' + \sin C' \sin A' \cos b'.$$

Omitting accents, we have

$$(5) \quad \cos B = -\cos C \cos A + \sin C \sin A \cos b.$$

Formulas (3) and (4), § 85, by similar substitutions become

$$(6) \quad \cos C = -\cos A \cos B + \sin A \sin B \cos c.$$

$$(7) \quad \cos A = -\cos B \cos C + \sin B \sin C \cos a,$$

**87. The Half-angle Formulas.** By transformations similar to those employed in § 50, formulas (2), (3), (4), § 85, and (5), (6), (7), § 86, may be changed so that logarithmic computation may be used to determine the angles of a spherical triangle in terms of the sides, or the sides in terms of the angles.

(1) *To derive  $\tan \frac{1}{2}B$ ,  $\tan \frac{1}{2}C$ ,  $\tan \frac{1}{2}A$ .*

Taking (2), § 85,

$$\cos b = \cos c \cos a + \sin c \sin a \cos B,$$

and solving for  $\cos B$ , we find

$$(A) \quad \cos B = \frac{\cos b - \cos c \cos a}{\sin c \sin a}.$$

Subtracting both members of equation (A) from unity, and recalling that

$$1 - \cos B = 2 \sin^2 \frac{1}{2}B, \quad \S 37$$

we have

$$\begin{aligned} 2 \sin^2 \frac{1}{2} B &= \frac{\cos c \cos a + \sin c \sin a - \cos b}{\sin c \sin a} \\ &= \frac{\cos(c-a) - \cos b}{\sin c \sin a}, \quad \S 34 \\ &= \frac{2 \sin \frac{1}{2}(b+c-a) \sin \frac{1}{2}(a+b-c)}{\sin c \sin a}. \quad \S 38 \text{ (22)} \end{aligned}$$

Dividing by 2, substituting

$$a+b+c=2s, \quad b+c-a=2(s-a), \quad a+b-c=2(s-c),$$

and extracting the square root,

$$(B) \quad \sin \frac{1}{2} B = \sqrt{\frac{\sin(s-a) \sin(s-c)}{\sin c \sin a}}.$$

Adding unity to both members of equation (A), we have

$$\begin{aligned} 1 + \cos B &= 2 \cos^2 \frac{1}{2} B = \frac{\cos b - (\cos c \cos a - \sin c \sin a)}{\sin c \sin a} \\ &= \frac{\cos b - \cos(c+a)}{\sin c \sin a} \\ &= \frac{2 \sin \frac{1}{2}(a+b+c) \sin \frac{1}{2}(c+a-b)}{\sin c \sin a}. \end{aligned}$$

Hence,

$$(C) \quad \cos \frac{1}{2} B = \sqrt{\frac{\sin s \sin(s-b)}{\sin c \sin a}}.$$

Dividing ( $B$ ) by ( $C$ ), and writing symmetric results for the angles  $C$  and  $A$ , we find:

$$(8) \quad \tan \frac{1}{2} B = \sqrt{\frac{\sin(s-a) \sin(s-c)}{\sin s \sin(s-b)}} = \frac{k}{\sin(s-b)},$$

$$(9) \quad \tan \frac{1}{2} C = \sqrt{\frac{\sin(s-b) \sin(s-a)}{\sin s \sin(s-c)}} = \frac{k}{\sin(s-c)},$$

$$(10) \quad \tan \frac{1}{2} A = \sqrt{\frac{\sin(s-c) \sin(s-b)}{\sin s \sin(s-a)}} = \frac{k}{\sin(s-a)},$$

where  $k$  is defined by

$$k = \sqrt{\frac{\sin(s-a) \sin(s-b) \sin(s-c)}{\sin s}}.$$

Formulas (8), (9), (10) are well adapted to logarithmic calculations of the angles when the sides are given.

(2) To derive  $\tan \frac{1}{2} b$ ,  $\tan \frac{1}{2} c$ ,  $\tan \frac{1}{2} a$ . Values for  $\tan \frac{1}{2} b$ ,  $\tan \frac{1}{2} c$ ,  $\tan \frac{1}{2} a$ , may be derived directly from (5), (6), (7), § 86, by manipulation similar to that employed for  $\tan \frac{1}{2} B$ ,  $\tan \frac{1}{2} C$ ,  $\tan \frac{1}{2} A$ .

Another method consists in transforming (8), (9), and (10) directly into the required values of  $\tan \frac{1}{2} b$ ,  $\tan \frac{1}{2} c$ ,  $\tan \frac{1}{2} a$  by means of the polar triangle. In (8) let us substitute

$$B = 180^\circ - b', \quad a = 180^\circ - A', \quad b = 180^\circ - B', \quad c = 180^\circ - C',$$

$$\frac{1}{2} B = 90^\circ - \frac{1}{2} b', \quad s = \frac{1}{2} (a + b + c) = 270^\circ - S,$$

$$s - b = 90^\circ - (S - B'), \quad s - c = 90^\circ - (S - C'),$$

$$s - a = 90^\circ - (S - A'),$$

where

$$S = \frac{1}{2} (A' + B' + C') > 90.$$

Then we have

$$\tan(90^\circ - \frac{1}{2} b') = \sqrt{\frac{\sin[(90^\circ - (S - A'))] \sin[90^\circ - (S - C')]}{\sin(270^\circ - S) \sin[90^\circ - (S - B')]}}$$

or,

$$\cot \frac{1}{2} b' = \sqrt{\frac{\cos(S - A') \cos(S - C')}{-\cos S \cos(S - B')}},$$

with similar expressions for  $\cot \frac{1}{2} c'$ , and  $\cot \frac{1}{2} a'$ .

Taking the reciprocal, and omitting accents, we have

$$(11) \quad \tan \frac{1}{2} b = \sqrt{\frac{-\cos S \cos(S - B)}{\cos(S - A) \cos(S - C)}} = K \cos(S - B),$$

$$(12) \quad \tan \frac{1}{2} c = \sqrt{\frac{-\cos S \cos (S-C)}{\cos (S-B) \cos (S-A)}} = K \cos (S-C),$$

$$(13) \quad \tan \frac{1}{2} a = \sqrt{\frac{-\cos S \cos (S-A)}{\cos (S-C) \cos (S-B)}} = K \cos (S-A),$$

where

$$K = \sqrt{\frac{-\cos S}{\cos (S-A) \cos (S-B) \cos (S-C)}}.$$

NOTE. It may be shown that  $k$ , used in (8), (9), (10), is equal to the tangent of the radius of the *small* circle inscribed in the spherical triangle  $ABC$ , and that  $K$ , used in (11), (12), (13), is equal to the tangent of the radius of the *small* circle circumscribing the triangle  $ABC$ .

**88. Napier's Analogies.** Dividing  $\tan \frac{1}{2} B$  by  $\tan \frac{1}{2} C$ , formulas (8), (9), § 87, we have

$$\frac{\tan \frac{1}{2} B}{\tan \frac{1}{2} C} = \frac{\sin (s-c)}{\sin (s-b)}.$$

Taking this equality by composition and division,

$$\frac{\tan \frac{1}{2} B + \tan \frac{1}{2} C}{\tan \frac{1}{2} B - \tan \frac{1}{2} C} = \frac{\sin (s-c) + \sin (s-b)}{\sin (s-c) - \sin (s-b)},$$

which reduces to

$$\frac{\sin \frac{1}{2} (B+C)}{\sin \frac{1}{2} (B-C)} = \frac{\sin \frac{1}{2} (2s-b-c) \cos \frac{1}{2} (b-c)}{\cos \frac{1}{2} (2s-b-c) \sin \frac{1}{2} (b-c)},$$

and finally,

$$(14) \quad \frac{\sin \frac{1}{2} (B+C)}{\sin \frac{1}{2} (B-C)} = \frac{\tan \frac{1}{2} a}{\tan \frac{1}{2} (b-c)}.$$

Similarly,

$$(15) \quad \frac{\sin \frac{1}{2} (C+A)}{\sin \frac{1}{2} (C-A)} = \frac{\tan \frac{1}{2} b}{\tan \frac{1}{2} (c-a)},$$

$$(16) \quad \frac{\sin \frac{1}{2} (A+B)}{\sin \frac{1}{2} (A-B)} = \frac{\tan \frac{1}{2} c}{\tan \frac{1}{2} (a-b)}.$$

Another formula may be obtained by multiplying  $\tan \frac{1}{2} B$  by  $\tan \frac{1}{2} C$ .

$$\tan \frac{1}{2} B \tan \frac{1}{2} C = \frac{\sin (s-a)}{\sin s}.$$

Write  $\tan \frac{1}{2} B$  and  $\tan \frac{1}{2} C$  in terms of sines and cosines, and take the equation by division and composition,

$$\frac{\cos \frac{1}{2} B \cos \frac{1}{2} C - \sin \frac{1}{2} B \sin \frac{1}{2} C}{\cos \frac{1}{2} B \cos \frac{1}{2} C + \sin \frac{1}{2} B \sin \frac{1}{2} C} = \frac{\sin s - \sin(s-a)}{\sin s + \sin(s-a)},$$

and reduce, giving

$$(17) \quad \frac{\cos \frac{1}{2}(B+C)}{\cos \frac{1}{2}(B-C)} = \frac{\tan \frac{1}{2} a}{\tan \frac{1}{2}(b+c)}.$$

Similarly,

$$(18) \quad \frac{\cos \frac{1}{2}(C+A)}{\cos \frac{1}{2}(C-A)} = \frac{\tan \frac{1}{2} b}{\tan \frac{1}{2}(c+a)},$$

$$(19) \quad \frac{\cos \frac{1}{2}(A+B)}{\cos \frac{1}{2}(A-B)} = \frac{\tan \frac{1}{2} c}{\tan \frac{1}{2}(a+b)}.$$

The formulas (14) to (19) are known as *Napier's Analogies*. Numbers (14) and (17) enable us to compute the sides  $b$ ,  $c$ , when the opposite angle  $B$ ,  $C$ , and the included side  $a$  are known. The Theorem of Sines, § 84, then determines the remaining angle  $A$ .

Napier's Analogies appear also in another form which may be derived by means of the polar triangle.

By substituting  $a = 180^\circ - A'$ ,  $A = 180^\circ - a'$ , and so on, let the student deduce from (14) to (19) the following:

$$(20) \quad \frac{\sin \frac{1}{2}(b+c)}{\sin \frac{1}{2}(b-c)} = \frac{\cot \frac{1}{2} A}{\tan \frac{1}{2}(B-C)},$$

$$(21) \quad \frac{\sin \frac{1}{2}(c+a)}{\sin \frac{1}{2}(c-a)} = \frac{\cot \frac{1}{2} B}{\tan \frac{1}{2}(C-A)},$$

$$(22) \quad \frac{\sin \frac{1}{2}(a+b)}{\sin \frac{1}{2}(a-b)} = \frac{\cot \frac{1}{2} C}{\tan \frac{1}{2}(A-B)},$$

and

$$(23) \quad \frac{\cos \frac{1}{2}(b+c)}{\cos \frac{1}{2}(b-c)} = \frac{\cot \frac{1}{2} A}{\tan \frac{1}{2}(B+C)},$$

$$(24) \quad \frac{\cos \frac{1}{2}(c+a)}{\cos \frac{1}{2}(c-a)} = \frac{\cot \frac{1}{2} B}{\tan \frac{1}{2}(C+A)},$$



$$(25) \quad \frac{\cos \frac{1}{2}(a+b)}{\cos \frac{1}{2}(a-b)} = \frac{\cot \frac{1}{2} C}{\tan \frac{1}{2}(A+B)}.$$

**89. The Area of a Spherical Triangle.** The sum of the three angles of a spherical triangle is greater than  $180^\circ$ . If  $A, B, C$  be the angles,

$$A + B + C - 180^\circ = E$$

determines the *spherical excess* of the triangle.

In spherical geometry it is shown that the areas of spherical triangles are to each other as their spherical excesses. A tri-rectangular triangle has an area  $\frac{1}{2} \pi R^2$  and its excess is  $90^\circ$ . Hence, if  $\Delta$  denote the area of any spherical triangle whose spherical excess is  $E^\circ$ , and  $R$  be the radius of the sphere, we have

$$\Delta : \frac{1}{2} \pi R^2 :: E : 90,$$

or

$$\Delta = \frac{\pi R^2}{180} \times E.$$

The spherical excess  $E$  is readily found when the angles of a spherical triangle are known.

The value of  $E$  may be determined directly when the three sides are known. The resulting formula is known as *L'Huilier's Theorem*, and is given by

$$\tan \frac{E}{4} = \sqrt{\tan \frac{1}{2} s \tan \frac{1}{2}(s-a) \tan \frac{1}{2}(s-b) \tan \frac{1}{2}(s-c)}.$$

The derivation of this formula will not be given here.

**90. Solution of Oblique Spherical Triangles.** When any three parts of a spherical triangle are given, the remaining parts may be found by use of the Theorem of Sines, the Half-angle Formulas, or by Napier's Analogies. Six cases occur.

CASE I. *Given the three sides, a, b, c.* To determine the angles  $A, B, C$ , we use the half-angle formulas

$$\tan \frac{1}{2} A = \frac{k}{\sin(s-a)}, \quad \tan \frac{1}{2} B = \frac{k}{\sin(s-b)}, \quad \tan \frac{1}{2} C = \frac{k}{\sin(s-c)},$$

where 
$$k = \sqrt{\frac{\sin(s-a) \sin(s-b) \sin(s-c)}{\sin s}}.$$

Employ logarithms in the calculation, tabulating work after the form suggested in the solution of plane triangles.

CASE II. *Given the three angles,  $A, B, C$ . Determine the sides  $a, b, c$  by use of*

$$\tan \frac{1}{2} a = K \cos (S - A),$$

$$\tan \frac{1}{2} b = K \cos (S - B),$$

$$\tan \frac{1}{2} c = K \cos (S - C),$$

where

$$K = \sqrt{\frac{-\cos S}{\cos (S - A) \cos (S - B) \cos (S - C)}}.$$

In this case  $\cos S$  is always negative.

CASE III. *Given two sides and the included angle,  $c, a, B$ . To find  $C$  and  $A$  use Napier's Analogies:*

$$\tan \frac{1}{2} (C + A) = \frac{\cos \frac{1}{2} (c - a)}{\cos \frac{1}{2} (c + a)} \cot \frac{1}{2} B,$$

$$\tan \frac{1}{2} (C - A) = \frac{\sin \frac{1}{2} (c - a)}{\sin \frac{1}{2} (c + a)} \cot \frac{1}{2} B.$$

In the first of these formulas  $\cot \frac{1}{2} B$  is positive,  $\cos \frac{1}{2} (c - a)$  is positive; if  $\cos \frac{1}{2} (c + a)$  be positive, the  $\tan \frac{1}{2} (C + A)$  is positive, and  $\frac{1}{2} (C + A) < 90^\circ$ . If  $\cos \frac{1}{2} (c + a)$  be negative, the  $\tan \frac{1}{2} (C + A)$  is negative, and  $\frac{1}{2} (C + A) > 90^\circ$ .

After the angles  $C$  and  $A$  have been found, the side  $b$  may be determined by means of the Theorem of Sines,

$$\sin b = \frac{\sin a \sin B}{\sin A}.$$

In using the Theorem of Sines care must be exercised in determining whether  $b$  lies in the first or second quadrant.

CASE IV. *Given two angles and the included side,  $B, C, a$ . Formulas (17) and (14) of Napier's Analogies determine  $b$  and  $c$ .*

$$\tan \frac{1}{2} (b + c) = \frac{\cos \frac{1}{2} (B - C)}{\cos \frac{1}{2} (B + C)} \tan \frac{1}{2} a,$$

$$\tan \frac{1}{2} (b - c) = \frac{\sin \frac{1}{2} (B - C)}{\sin \frac{1}{2} (B + C)} \tan \frac{1}{2} a.$$

The first of these formulas shows that if  $\frac{1}{2} (B + C) > 90^\circ$ , then will  $\frac{1}{2} (b + c) > 90^\circ$ , and inversely. The angle  $A$  may be determined by the Theorem of Sines.

CASE V. *Given two sides and an angle opposite one of them,  $b, c, B$ .* Here, the angle  $C$  is given by

$$\sin C = \frac{\sin c \sin B}{\sin b}.$$

(1) If  $\sin c \sin B > \sin b$ , no solution exists.

(2) If  $\sin c \sin B = \sin b$ , the angle  $C = 90^\circ$ .

(3) If  $\sin c \sin B < \sin b$ , either one or two solutions will occur; see Fig. 60.

After  $C$  has been found, angle  $A$  and side  $a$  may be obtained from

$$\cot \frac{1}{2} A = \frac{\cos \frac{1}{2} (b + c)}{\cos \frac{1}{2} (b - c)} \tan \frac{1}{2} (B + C),$$

$$\tan \frac{1}{2} a = \frac{\cos \frac{1}{2} (B + C)}{\cos \frac{1}{2} (B - C)} \tan \frac{1}{2} (b + c).$$

CASE VI. *Given two angles and a side opposite one of them,  $B, C, b$ .* The side  $c$  is given by

$$\sin c = \frac{\sin b \sin C}{\sin B}.$$

This case may also have no solution, one solution, or two solutions. After  $c$  has been determined the remaining parts,  $a, A$ , may be derived from Napier's Analogies, as in Case V.

**EXERCISES**

Solve the following spherical triangles for the unknown parts:

1.  $A = 100^\circ, B = 75^\circ, C = 65^\circ$ .
2.  $a = 27^\circ 40', b = 48^\circ, c = 50^\circ 40'$ .
3.  $a = 65^\circ 48', b = 120^\circ 21', c = 84^\circ 21'$ .
4.  $A = 96^\circ 50', B = 75^\circ 10', C = 96^\circ 50'$ .
5.  $B = 72^\circ 30', A = 41^\circ 27', c = 49^\circ 17'$ .
6.  $b = 118^\circ 48', c = 71^\circ 24', A = 51^\circ 24'$ .
7.  $a = 72^\circ 48' 12'', b = 41^\circ 38' 10'', C = 33^\circ 24' 10''$ .

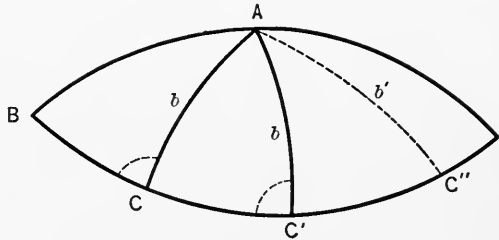


Fig. 60.

8.  $B = 129^\circ 24' 10''$ ,  $C = 31^\circ 24' 30''$ ,  $a = 42^\circ 50' 40''$ .
9.  $a = 112^\circ 40' 15''$ ,  $b = 121^\circ 10' 10''$ ,  $C = 128^\circ 44' 15''$ .
10.  $A = 100^\circ 14' 20''$ ,  $B = 140^\circ 40' 40''$ ,  $c = 39^\circ 28' 15''$ .
11.  $b = 54^\circ 21'$ ,  $c = 31^\circ 48'$ ,  $B = 100^\circ 10'$ .
12.  $A = 101^\circ 40'$ ,  $c = 62^\circ 21'$ ,  $a = 104^\circ 24'$ .
13.  $b = 40^\circ 16' 10''$ ,  $c = 46^\circ 48' 40''$ ,  $B = 56^\circ 21' 50''$ .
14.  $a = 37^\circ 10' 20''$ ,  $b = 112^\circ 48'$ ,  $A = 34^\circ 28' 15''$ .
15.  $C = 123^\circ 38'$ ,  $b = 150^\circ 40'$ ,  $c = 10^\circ 21' 30''$ .
16.  $A = 140^\circ 29'$ ,  $C = 24^\circ 40'$ ,  $a = 135^\circ 40'$ .
17.  $B = 128^\circ 40'$ ,  $C = 141^\circ 25'$ ,  $c = 125^\circ 47'$ .
18.  $A = 48^\circ 37'$ ,  $C = 34^\circ 48'$ ,  $c = 41^\circ 10'$ .
19.  $B = 99^\circ 27'$ ,  $C = 89^\circ 21'$ ,  $a = 45^\circ 37'$ .
20.  $a = 71^\circ 47'$ ,  $b = 145^\circ 47'$ ,  $C = 130^\circ 50'$ .
21. When  $b = 37^\circ 28'$ ,  $c = 65^\circ 21'$ , and  $A = 87^\circ 40'$ , find side  $a$  directly by *Modified Formula (B)*, § 85.
22. Find  $c$  directly, (*B*) § 85, when  $a = 101^\circ 48'$ ,  $b = 100^\circ$ ,  $C = 68^\circ 41'$ .
23. Find in inches the perimeter of a spherical triangle with sides  $68^\circ$ ,  $96^\circ$ ,  $120^\circ$ , on a sphere whose radius is 15 in.
24. Find the perimeter of a spherical triangle with angles  $69^\circ$ ,  $84^\circ$ ,  $100^\circ$ , upon a sphere whose radius is 10 in.
25. Find the area of the spherical triangle with angles  $120^\circ$ ,  $84^\circ$ ,  $72^\circ$ , upon a sphere whose radius is 20 in.

Find the areas of the following spherical triangles:

26.  $A = 24^\circ 30'$ ,  $B = 140^\circ$ ,  $C = 80^\circ$ , radius = 12 in.
27.  $a = 65^\circ$ ,  $b = 47^\circ$ ,  $c = 60^\circ$ ,  $r = 15$  in.
28.  $A = 100^\circ$ ,  $B = 80^\circ$ ,  $c = 60^\circ$ ,  $r = 12$  in.
29.  $b = 37^\circ$ ,  $c = 84^\circ$ ,  $A = 65^\circ$ ,  $r = 3956$  mi.
30.  $B = 104^\circ$ ,  $C = 128^\circ$ ,  $b = 138^\circ$ ,  $r = 3956$  mi.

## APPLICATIONS OF SPHERICAL TRIGONOMETRY

**91. The Earth as a Sphere. Definitions and Notation.** In what follows the earth is assumed to be a sphere with a radius of 3956 mi. The *shortest distance* between two points upon the earth is the length of the shorter arc of a great circle drawn through the two points.

(1) *The Geographical Mile and Statute Mile.* The *geographical mile* (called *nautical mile*, also *knot*) is a unit of distance along the arc of a great circle upon the earth; it is the length of an arc of one minute of a great circle, hence sixty geographical miles equal one degree. The *statute mile* is our ordinary unit of measurement equivalent to 5280 ft. The length of one degree of the arc of a great circle of the earth is given by

$$1^\circ = \frac{\pi \times 3956}{180} \text{ mi.}, \pi = 3.14159.$$

(2) *Meridian, Longitude, Latitude.* A great circle drawn through the poles  $N, S$ , and through any point  $B$ , Fig. 61, is called the *Meridian* of the point  $B$ .

Meridians are numbered to the east and west with reference to some *zero meridian*. The meridian passing through Greenwich (near London), England, is usually taken as the zero meridian,  $NGPS$ , Fig. 61. The meridian of Greenwich intersects the earth's *equator*  $ELMW$  in  $P$ .

The *Longitude* of any point  $B$  upon the earth is the number of degrees between the *zero meridian* and the *meridian through*  $B$ . This angle is measured by the arc of the equator  $PEM$ , or the spherical angle  $GNB$ . The longitude of  $F$  is the arc  $PEL$ , or the angle  $GNF$ .

The meridians are numbered by degrees, minutes, and seconds from  $0^\circ$  to  $180^\circ$  *east* (marked E.) and *west* (marked W.) of the *Greenwich* or *zero meridian*. Thus the point  $B$  is in W. longitude, also the point  $F$ .

The *Latitude* of a point  $B$  is the arc of the meridian of the point intercepted by the equator and the point. The *latitude* of  $B$  is the arc  $MB$ . Latitude is counted *positive* or *negative* according as the point is north or south of the equator; the

direction is usually indicated by attaching N. or S. to the number of degrees in the latitude.

As samples of the notation of latitude and longitude we may write :

- (1) New York, lat.  $40^{\circ} 43'$  N., long.  $74^{\circ}$  W.
- (2) Boston, lat.  $42^{\circ} 21'$  N., long.  $71^{\circ} 4'$  W.
- (3) Greenwich, lat.  $51^{\circ} 29'$  N., long.  $0^{\circ}$ .
- (4) Liverpool, lat.  $53^{\circ} 24'$  N., long.  $3^{\circ} 4'$  W.
- (5) San Francisco, lat.  $37^{\circ} 48'$  N., long.  $122^{\circ} 28'$  W.
- (6) Valparaiso, lat.  $33^{\circ} 2'$  S., long.  $71^{\circ} 41'$  W.
- (7) Calcutta, lat.  $22^{\circ} 33'$  N., long.  $88^{\circ} 19'$  E.
- (8) Sandy Hook, lat.  $40^{\circ} 28'$  N., long.  $74^{\circ} 1'$  W.

**92. The Terrestrial Triangle.** When the *latitude* and *longitude* of any two points upon the earth are known, the distance

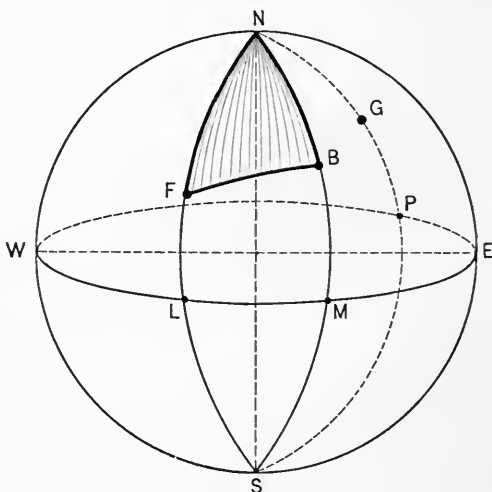


Fig. 61.

between the points may be found. Thus, in Fig. 61, if the point  $B$  be in lat.  $\alpha^{\circ}$  N., long.  $\beta^{\circ}$  W., and  $F$  be in lat.  $\alpha_1^{\circ}$  N., long.  $\beta_1^{\circ}$  W., the spherical triangle  $NFB$  is completely determined as follows :

arc  $NB = 90^\circ - \alpha^\circ =$  complement of the latitude of  $B$ ,

arc  $NF = 90^\circ - \alpha_1^\circ =$  complement of the latitude of  $F$ ,

angle  $BNF = \beta_1^\circ - \beta^\circ =$  difference in longitude of  $B$  and  $F$ .

This data gives *two sides and the included angle of the triangle NFB*.

(1) *To find the distance between two points whose latitude and longitude are given.* If the distance  $BF$ , Fig. 61, alone be required, we have to solve the spherical triangle  $BNF$  for  $BF$ . This may be done by the use of (B), § 85, in which logarithmic calculation may be employed.

$$\cos BF = \frac{\cos NF}{\sin \theta} \times \sin(\theta + NB) = \frac{\sin \alpha_1}{\sin \theta} \times \cos(\alpha - \theta),$$

$$\tan \theta = \frac{\cot NF}{\cos BNF} = \frac{\tan \alpha_1}{\cos(\beta_1 - \beta)}.$$

The arc  $BF$  may also be obtained by use of the Cosine Theorem (2), § 85,

$$\begin{aligned} \cos BF &= \cos NB \cos NF + \sin NB \sin NF \cos BNF, \\ &= \sin \alpha \sin \alpha_1 + \cos \alpha \cos \alpha_1 \cos(\beta_1 - \beta), \end{aligned}$$

but the use of this formula is not to be recommended except perhaps when the angles are such that the products  $\sin \alpha \sin \alpha_1$ ,  $\cos \alpha \cos \alpha_1 \cos(\beta_1 - \beta)$  reduce readily by ordinary multiplication.

(2) *To find the bearing and distance of two points whose latitude and longitude are known.* The angle  $NBF$ , Fig. 61, is the bearing of  $F$  from  $B$ ; the angle  $NFB$  is the bearing of  $B$  from  $F$ . The bearing of a course at a given period is usually considered as the *smaller* angle which that course makes with the meridian through the point. Thus in the figure, the bearing of  $F$  from  $B$  is N.  $\gamma^\circ$  W., if  $\gamma = \angle NBF < 90^\circ$ ; the bearing of  $F$  from  $B$  is S.  $\gamma_1^\circ$  W., if  $\gamma > 90^\circ$  and  $\gamma_1 = \angle SBF = 180^\circ - \gamma$ .

When the bearing, or bearing and distance, of two points whose latitude and longitude are given, is required, Napier's Analogies, (20), (23), § 88, may be used to find the angles  $NBF$  and  $NFB$ . The side  $BF$  may then be found by use of the Theorem of Sines, (1), § 84.

## EXERCISES

1. Find the distance in knots between Boston, lat.  $42^{\circ} 21' N.$ , long.  $71^{\circ} 4' W.$ , and Liverpool, lat.  $53^{\circ} 24' N.$ , long.  $3^{\circ} 4' W.$  Find also the bearing of each port from the other.

2. Find the distance in statute miles along the arc of a great circle from New York, lat.  $40^{\circ} 43' N.$ , long.  $74^{\circ} W.$ , to San Francisco, lat.  $37^{\circ} 48' N.$ , long.  $122^{\circ} 28' W.$

3. Find the distance in nautical miles from New York, lat.  $40^{\circ} 43' N.$ , long.  $74^{\circ} W.$ , to Greenwich, lat.  $51^{\circ} 29' N.$ , and the bearing of each point from the other.

4. If a vessel sails directly east from Sandy Hook, lat.  $40^{\circ} 28' N.$ , long.  $74^{\circ} 1' W.$ , along the arc of a great circle at the uniform rate of 16 knots per hour, find its latitude and longitude (1) at the end of 48 hours' sailing, (2) at the end of five days' sailing.

5. Find the distance in statute miles from San Francisco, lat.  $37^{\circ} 48' N.$ , long.  $122^{\circ} 28' W.$ , to Calcutta, lat.  $22^{\circ} 33' N.$ , long.  $88^{\circ} 19' E.$ , and the bearing of each point from the other.

93. **The Celestial Sphere.** Astronomical problems furnish many applications of spherical trigonometry. One class of these problems will be noticed here.

The daily rotation of the earth upon its axis from *west* to *east* causes the stars to *seem* to rotate from *east* to *west* upon the surface of an immense sphere named the *celestial sphere*. To a person located at any point upon the earth one-half of this sphere is visible. The celestial sphere is represented in Fig. 62, the earth being a mere point at the centre.

(1) *The Horizon* of any point upon the earth is the intersection of the horizontal plane through the point with the celestial sphere. In Fig. 62, the horizon is the great circle  $HLLH'$ .

(2) *The Zenith* of any point is the intersection of the perpendicular erected to the plane of the horizon at the point. The point on the celestial sphere diametrically opposite the zenith is the *Nadir*. In the figure  $Z$  is the zenith,  $Z'$  is the nadir.

(3) *The Celestial Poles* are the intersections of the line of the earth's axis with the celestial sphere. The point  $N$  is the



north pole of the celestial sphere,  $S$  is its south pole. The celestial sphere rotates (apparently) about the axis  $NS$  once in 24 hours.

(4) *The Celestial Equator* is the intersection of the plane of the earth's equator with the celestial sphere. In the figure,  $EME'$  is the celestial equator,  $N$  and  $S$  are its poles.

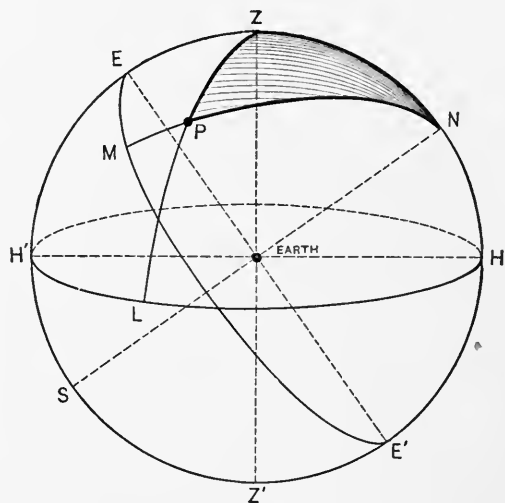


Fig. 62.

(5) *The Celestial Meridians* are the great circles through  $N$  and  $S$ . The celestial meridian through any star is called the *hour circle* of that star. Thus,  $NPM$  is the hour circle of  $P$ .

**94. The Celestial Triangle.** The position  $P$  of any star is known if we know its distance  $PL$  above the horizon, and its distance  $PM$  north or south of the celestial equator.

(1) *The Altitude*  $PL$  of a star at  $P$  is the arc of a zenith circle  $ZL$  intercepted between the point  $P$  and the horizon. See Fig. 62.

(2) *The Declination* of a star  $P$  is the arc  $PM$  of the celestial meridian  $NPM$  between the point and the celestial equator.

(3) *The Latitude of the Zenith* of any point on the earth is the arc  $EZ$  and is equal to the latitude of the observer.

(4) *The Hour Angle* of any star is the angle between the

meridian through the star and the zenith meridian. In the figure  $PNZ$  is the hour angle.

Since the celestial sphere apparently rotates through  $360^\circ$  in 24 hr., or  $15^\circ$  in one hour of time, we may express the hour angle in hours, minutes, and seconds, and thus determine the time required for a star to rotate into the meridian of the zenith.

The points  $P$ ,  $N$ ,  $Z$  determine the celestial triangle  $PNZ$ , sometimes called the astronomical triangle. This triangle is determined when the *latitude of the observer*  $EZ$ , the *altitude of the star*  $PL$ , and the *declination of the star*  $PM$  are known. We have:

$$NZ = 90^\circ - \text{latitude of the observer,}$$

$$ZP = 90^\circ - \text{altitude of the star,}$$

$$PN = 90^\circ - \text{declination of the star.}$$

If an observation of the sun's altitude be made in the forenoon, let us say, and the declination of the sun upon that day of the year be known, then we may compute the hour angle provided the latitude of the observer be known. Having the hour angle, we may find the corresponding equivalent in time, and thus determine the hour of day at which the observation was made.

The sun's declination varies from near  $23^\circ 30'$  south to near  $23^\circ 30'$  north declination. At the vernal equinox and at the autumnal equinox the sun's declination is zero.

#### EXERCISES

1. At San Francisco, lat.  $37^\circ 48' N.$ , a forenoon observation shows the sun's altitude as  $40^\circ 21'$ . If the sun's declination be  $10^\circ 41' N.$ , what is the time of observation?

2. In latitude  $40^\circ 21' N.$ , the sun's altitude in the afternoon was found to be  $35^\circ 40'$ . What was the time of observation, if the sun's declination is  $8^\circ 4' S.$ ?

3. Find the time of sunrise at Boston, lat.  $42^\circ 21' N.$ , the sun's declination being  $20^\circ 31' N.$

4. Find the time of sunrise (approximately) at a point whose latitude is  $39^\circ 10' N.$  twenty days after the vernal equinox.

## CHAPTER XII

### FORMULAS

#### PLANE TRIGONOMETRY

##### Fundamental Identities.

1.  $\sin x \csc x = \cos x \sec x = \tan x \cot x = 1.$
2.  $\sin^2 x + \cos^2 x = 1, \sec^2 x - \tan^2 x = 1, \csc^2 x - \cot^2 x = 1.$
3.  $\tan x = \frac{\sin x}{\cos x} = \frac{1}{\cot x} = \frac{\sec x}{\csc x} = \frac{\sqrt{1 - \cos^2 x}}{\cos x}.$
4.  $\sin x = \cos x \tan x = \frac{1}{\sqrt{1 + \cot^2 x}} = \frac{\tan x}{\sqrt{1 + \tan^2 x}}.$
5.  $\cos x = \sin x \cot x = \frac{1}{\sqrt{1 + \tan^2 x}} = \frac{\cot x}{\sqrt{1 + \cot^2 x}}.$

##### Sum and Difference Formulas.

6.  $\sin(x \pm y) = \sin x \cos y \pm \cos x \sin y.$
7.  $\cos(x \pm y) = \cos x \cos y \mp \sin x \sin y.$
8.  $\tan(x \pm y) = \frac{\tan x \pm \tan y}{1 \mp \tan x \tan y}.$
9.  $\cot(x \pm y) = \frac{\cot x \cot y \mp 1}{\cot y \pm \cot x}.$
10.  $\sin x + \sin y = 2 \sin \frac{1}{2}(x + y) \cos \frac{1}{2}(x - y).$
11.  $\sin x - \sin y = 2 \cos \frac{1}{2}(x + y) \sin \frac{1}{2}(x - y).$
12.  $\cos x + \cos y = 2 \cos \frac{1}{2}(x + y) \cos \frac{1}{2}(x - y).$
13.  $\cos x - \cos y = -2 \sin \frac{1}{2}(x + y) \sin \frac{1}{2}(x - y).$
14.  $\tan x \pm \tan y = \frac{\sin(x \pm y)}{\cos x \cos y}.$
15.  $\cot x \pm \cot y = \pm \frac{\sin(x \pm y)}{\sin x \sin y}.$
16.  $\frac{\sin x + \sin y}{\cos x + \cos y} = \tan \frac{1}{2}(x + y).$

17.  $\frac{\sin x + \sin y}{\sin x - \sin y} = \frac{\tan \frac{1}{2}(x+y)}{\tan \frac{1}{2}(x-y)}$ .
18.  $\sin^2 x - \sin^2 y = \sin(x+y)\sin(x-y)$ .
19.  $\cos^2 x - \cos^2 y = -\sin(x+y)\sin(x-y)$ .
20.  $\cos^2 x - \sin^2 y = \cos(x+y)\cos(x-y)$ .

### Half Angle and Multiple Angle Formulas.

21.  $\sin x = 2 \sin \frac{1}{2}x \cos \frac{1}{2}x = \frac{2 \tan \frac{1}{2}x}{1 + \tan^2 \frac{x}{2}}$ .
22.  $\cos x = \cos^2 \frac{1}{2}x - \sin^2 \frac{1}{2}x = 2 \cos^2 \frac{1}{2}x - 1 = 1 - 2 \sin^2 \frac{1}{2}x$   
 $= \frac{1 - \tan^2 \frac{1}{2}x}{1 + \tan^2 \frac{1}{2}x}$ .
23.  $\tan x = \frac{2 \tan \frac{1}{2}x}{1 - \tan^2 \frac{1}{2}x} = \frac{2 \cot \frac{1}{2}x}{\cot^2 \frac{1}{2}x - 1} = \frac{2}{\cot \frac{1}{2}x - \tan \frac{1}{2}x}$ .
24.  $\cot x = \frac{\cot^2 \frac{1}{2}x - 1}{2 \cot \frac{1}{2}x} = \frac{1}{2}(\cot \frac{1}{2}x - \tan \frac{1}{2}x)$ .
25.  $\sin \frac{1}{2}x = \sqrt{\frac{1}{2}(1 - \cos x)}$ .
26.  $\cos \frac{1}{2}x = \sqrt{\frac{1}{2}(1 + \cos x)}$ .
27.  $\tan \frac{1}{2}x = \sqrt{\frac{1 - \cos x}{1 + \cos x}} = \frac{\sin x}{1 + \cos x} = \frac{1 - \cos x}{\sin x}$ .
28.  $\sin 2x = 2 \sin x \cos x$ ,  $\cos 2x = \cos^2 x - \sin^2 x$ .
29.  $\sin 3x = 3 \sin x - 4 \sin^3 x$ ,  $\cos 3x = 4 \cos^3 x - 3 \cos x$ .
30.  $\sin 4x = \sin x(8 \cos^3 x - 4 \cos x)$ ,  
 $\cos 4x = 8 \cos^4 x - 8 \cos^2 x + 1$ .
31.  $\tan 2x = \frac{2 \tan x}{1 - \tan^2 x}$ ,  $\tan 3x = \frac{3 \tan x - \tan^3 x}{1 - 3 \tan^2 x}$ .

### Plane Triangles.

32. Theorems of sines:  $\frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c} = \frac{1}{2R}$ .
33. Theorem of cosines:  $a^2 = b^2 + c^2 - 2bc \cos A$ .
34. Theorem of tangents:  
 $\frac{a+b}{a-b} = \frac{\sin A + \sin B}{\sin A - \sin B} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$ .

35. The half angles :

$$\left. \begin{aligned} (1) \sin \frac{A}{2} &= \sqrt{\frac{(s-b)(s-c)}{bc}}, \\ (2) \cos \frac{A}{2} &= \sqrt{\frac{s(s-a)}{bc}}, \\ (3) \tan \frac{A}{2} &= \sqrt{\frac{(s-b)(s-c)}{s(s-a)}}. \end{aligned} \right\}, \text{ where } 2s = a + b + c.$$

36. Area :  $K = \frac{1}{2} bc \sin A = \frac{1}{2} c^2 \frac{\sin A \sin B}{\sin(A+B)}$   
 $= \sqrt{s(s-a)(s-b)(s-c)} = sr.$

**Analytic Trigonometry.**

37. Inverse identities :

(1)  $\sin^{-1} x \pm \sin^{-1} y = \sin^{-1} (x \sqrt{1-y^2} \pm y \sqrt{1-x^2}).$

(2)  $\cos^{-1} x \pm \cos^{-1} y = \cos^{-1} (xy \mp \sqrt{1-x^2} \sqrt{1-y^2}).$

(3)  $\tan^{-1} x \pm \tan^{-1} y = \tan^{-1} \left( \frac{x \pm y}{1 \mp xy} \right).$

(4)  $\sin^{-1} x = \frac{1}{2} \sin^{-1} (2x \sqrt{1-x^2}) = \frac{1}{2} \pi - \cos^{-1} x$   
 $= \csc^{-1} \frac{1}{x} = -\sin^{-1} (-x).$

(5)  $\cos^{-1} x = \frac{1}{2} \cos^{-1} (2x^2 - 1) = \frac{1}{2} \pi - \sin^{-1} x$   
 $= 2 \tan^{-1} \sqrt{\frac{1-x}{1+x}} = \sec^{-1} \frac{1}{x}.$

38.  $\sin x = \frac{1}{2i} (e^{ix} - e^{-ix}), \cos x = \frac{1}{2} (e^{ix} + e^{-ix}),$

$$\tan x = \frac{1}{i} \left( \frac{e^{ix} - e^{-ix}}{e^{ix} + e^{-ix}} \right).$$

39.  $\sinh x = \frac{1}{2} (e^x - e^{-x}), \cosh x = \frac{1}{2} (e^x + e^{-x}),$

$$\tanh x = \frac{e^x - e^{-x}}{e^x + e^{-x}}.$$

40.  $e^{ix} = \cos x + i \sin x, e^{-ix} = \cos x - i \sin x.$

41.  $e^x = \cosh x + \sinh x, e^{-x} = \cosh x - \sinh x.$

42.  $\sin(ix) = \frac{i}{2} (e^x - e^{-x}) = i \sinh x,$

$$\cos(ix) = \frac{1}{2} (e^x + e^{-x}) = \cosh x, \tan(ix) = i \frac{e^x - e^{-x}}{e^x + e^{-x}} = i \tanh x.$$

$$43. (\cos x + i \sin x)^n = (e^{ix})^n = e^{nix} = \cos nx + i \sin nx.$$

$$44. \sin(x \pm iy) = \sin x \cos(iy) \pm \cos x \sin(iy) \\ = \sin x \cosh y \pm i \cos x \sinh y.$$

$$45. \cos(x \pm iy)x = \cos x \cosh y \mp i \sin x \sinh y.$$

$$46. \cosh^2 x - \sinh^2 x = \operatorname{sech}^2 x + \tanh^2 x = \coth^2 x - \operatorname{csch}^2 x = 1.$$

47. Infinite series :

$$(1) (1+x)^n = 1 + nx + \frac{n(n-1)}{2} x^2 + \frac{n(n-1)(n-2)}{3} x^3 + \dots$$

$$(2) e^x = 1 + x + \frac{x^2}{2} + \frac{x^3}{3} + \frac{x^4}{4} + \frac{x^5}{5} + \dots$$

$$(3) \log(1+x) = x - \frac{x^2}{2} + \frac{x^3}{3} - \frac{x^4}{4} + \frac{x^5}{5} - \dots$$

$$(4) \sin x = x - \frac{x^3}{3} + \frac{x^5}{5} - \frac{x^7}{7} + \dots$$

$$(5) \cos x = 1 - \frac{x^2}{2} + \frac{x^4}{4} - \frac{x^6}{6} + \dots$$

$$(6) \tan x = x + \frac{x^3}{3} + \frac{2x^5}{15} + \frac{17x^7}{315} + \dots$$

$$(7) \sinh x = x + \frac{x^3}{3} + \frac{x^5}{5} + \frac{x^7}{7} + \dots$$

$$(8) \cosh x = 1 + \frac{x^2}{2} + \frac{x^4}{4} + \frac{x^6}{6} + \dots$$

$$(9) \tanh x = x - \frac{x^3}{3} + \frac{2x^5}{15} - \dots$$

$$48. \sin x = x \left\{ 1 - \left(\frac{x}{\pi}\right)^2 \right\} \left\{ 1 - \left(\frac{x}{2\pi}\right)^2 \right\} \left\{ 1 - \left(\frac{x}{3\pi}\right)^2 \right\} \dots$$

$$49. \cos x = \left\{ 1 - \left(\frac{2x}{\pi}\right)^2 \right\} \left\{ 1 - \left(\frac{2x}{3\pi}\right)^2 \right\} \left\{ 1 - \left(\frac{2x}{5\pi}\right)^2 \right\} \dots$$

50. If  $\sec \theta = \cosh x$ ,  $\theta = \operatorname{gudermannian}$  of  $x = gdx$ .

$$(1) \theta = gdx = \sec^{-1}(\cosh x).$$

$$(2) x = gd^{-1}\theta = \cosh^{-1}(\sec \theta).$$

SPHERICAL TRIGONOMETRY

The Right Spherical Triangle.

51.  $\sin A = \frac{\sin a}{\sin c}$ .    52.  $\cos A = \frac{\tan b}{\tan c}$ .    53.  $\tan A = \frac{\tan a}{\sin b}$ .

54.  $\cos c = \cos a \cos b = \cot A \cot B$ .

55.  $\cos A = \sin B \cos a$ .

56. Napier's Rules :

(1)  $\sin(\text{mid. pt.}) = \tan(\text{adj. pt.}) \cdot \tan(\text{adj. pt.})$ .

(2)  $\sin(\text{mid. pt.}) = \cos(\text{op. pt.}) \cdot \cos(\text{op. pt.})$ .

The Oblique Spherical Triangle.

57.  $\frac{\sin A}{\sin a} = \frac{\sin B}{\sin b} = \frac{\sin C}{\sin c}$ .

58.  $\cos a = \cos b \cos c + \sin b \sin c \cos A$ .

59.  $\cos A = -\cos B \cos C + \sin B \sin C \cos a$ .

60.  $\tan \frac{A}{2} = \sqrt{\frac{\sin(s-b) \sin(s-c)}{\sin s \sin(s-a)}}$ ,

$\tan \frac{a}{2} = \sqrt{\frac{-\cos S \cos(S-A)}{\cos(S-B) \cos(S-C)}}$ .

61.  $\frac{\sin \frac{1}{2}(A+B)}{\sin \frac{1}{2}(A-B)} = \frac{\tan \frac{1}{2}c}{\tan \frac{1}{2}(a-b)}$ ,

$\frac{\cos \frac{1}{2}(A+B)}{\cos \frac{1}{2}(A-B)} = \frac{\tan \frac{1}{2}c}{\tan \frac{1}{2}(a+b)}$ .

62.  $\frac{\sin \frac{1}{2}(a+b)}{\sin \frac{1}{2}(a-b)} = \frac{\cot \frac{1}{2}C}{\tan \frac{1}{2}(A-B)}$ ,

$\frac{\cos \frac{1}{2}(a+b)}{\cos \frac{1}{2}(a-b)} = \frac{\cot \frac{1}{2}C}{\tan \frac{1}{2}(A+B)}$ .

63. Area,  $\Delta = \frac{\pi R^2}{180} E$ , where  $E$  is the spherical excess.

64.  $\tan \frac{E}{4} = \sqrt{\tan \frac{1}{2}s \tan \frac{1}{2}(s-a) \tan \frac{1}{2}(s-b) \tan \frac{1}{2}(s-c)}$ .





LOGARITHMIC, TRIGONOMETRIC,  
AND OTHER TABLES



THE MACMILLAN COMPANY  
NEW YORK · BOSTON · CHICAGO  
ATLANTA · SAN FRANCISCO

MACMILLAN & CO., LIMITED  
LONDON · BOMBAY · CALCUTTA  
MELBOURNE

THE MACMILLAN CO. OF CANADA, LTD.  
TORONTO

# LOGARITHMIC, TRIGONOMETRIC

AND OTHER

## TABLES

COMPILED BY

DAVID A. ROTHROCK

INDIANA UNIVERSITY

New York

THE MACMILLAN COMPANY

1911

*All rights reserved*

COPYRIGHT, 1910,  
BY THE MACMILLAN COMPANY.

---

Set up and electrotyped. Published September, 1910. Reprinted  
January, 1911.

Norwood Press  
J. S. Cushing Co. — Berwick & Smith Co.  
Norwood, Mass., U.S.A.

## PREFACE

THE following Tables have been prepared to accompany the author's "Plane and Spherical Trigonometry." The beginner in trigonometric calculation should be taught the use of tables supplied with the most convenient means of interpolation. To secure this end, proportional parts have been inserted in the Tables of Logarithms of Numbers and Logarithms of the Trigonometric Functions. A proper use of these devices is especially recommended.

Numerical calculation is a laborious process at best. By the professional computer, as well as by the beginner in elementary trigonometric calculation, every facility for obtaining the required degree of accuracy with a minimum of time and labor should be sought. To this end it is recommended that (1) tables with a minimum of decimals consistent with accuracy be used, (2) formulas be arranged in a systematic manner, (3) data as well as logarithms be systematically tabulated, (4) a skilful use of proportional parts be acquired, (5) logarithmic calculations upon scraps of paper be at no time permitted.



## CONTENTS

	PAGE
INTRODUCTION . . . . .	ix-xiv
1. Definitions . . . . .	ix
2. Laws for the Use of Logarithms . . . . .	ix-x
3. The Co-Logarithm . . . . .	x-xi
Explanation of Tables . . . . .	xi-xiv
LOGARITHMS OF NUMBERS, TABLE I . . . . .	1-20
1. Common Logarithms of Numbers 1 to 100 . . . . .	1
2. Common Logarithms of Numbers 100 to 10,009 . . . . .	2-20
3. Proportional Parts . . . . .	2-20
LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS, TABLE II . . . . .	21-74
1. For every second $0''$ to $3'$ , and $89^\circ 57'$ to $90^\circ$ . . . . .	22
2. For every ten seconds $0^\circ$ to $2^\circ$ , and $88^\circ$ to $90^\circ$ . . . . .	23-28
3. For every minute $0^\circ$ to $90^\circ$ , and for $0^\circ$ to $360^\circ$ . . . . .	29-74
4. Proportional Parts and Differences . . . . .	29-74
NATURAL TRIGONOMETRIC FUNCTIONS, TABLE III. . . . .	75-94
MISCELLANEOUS TABLES . . . . .	95-99
1. Radian Measure, $0^\circ$ to $180^\circ$ . . . . .	96
2. Natural (Napierian) Logarithms . . . . .	97-98
(A) For integers, 0 to 200 . . . . .	97
(B) For each tenth, 1 to 9.9 . . . . .	98
3. The Hyperbolic Functions, $\sinh x$ , $\cosh x$ . . . . .	99





## INTRODUCTION

LOGARITHMS may be used to diminish the labor of numerical calculations involving *multiplication, division, involution, and evolution* by replacing these operations, respectively, by *addition, subtraction, multiplication and division*.

**1. Definitions.** (1) *The exponent by which a number  $a$  must be affected to produce a number  $N$  is called the logarithm of  $N$  to base  $a$ .*

In symbols, if

$$\begin{aligned} a^x &= N, \\ \log_a N &= x. \end{aligned}$$

(2) There are two systems of logarithms in use:

(a) *The Common System (Briggian System)* in which 10 is the base,

(b) *The Natural System (Napierian System)* in which  $e = 2.71828\dots$  is the base.

EXAMPLES.  $10^2 = 100, \log_{10} 100 = 2.$   
 $10^{2.23300} = 171, \log_{10} 171 = 2.23300.$   
 $e^{3.40120} = 30, \log_e 30 = 3.40120.$

All ordinary calculations are performed by use of logarithms to the base 10. See Tables I, II.

Theoretical calculations in the higher mathematics sometimes require the use of *natural logarithms*. See Tables IV, 2, (A), (B).

(3) A logarithm of a number usually consists of an *integer* and a *decimal*. *The integral part of a logarithm is called the characteristic, the decimal part is called the mantissa.*

### 2. Laws for the Use of Logarithms.

(1) **LAW OF FACTORS.** *The logarithm of a product equals the sum of the logarithms of the factors.*

$$\log (A \times B \times C) = \log A + \log B + \log C.$$

(2) **LAW OF QUOTIENTS.** *The logarithm of a quotient equals the logarithm of the numerator diminished by that of the denominator.*

$$\log \left( \frac{A}{B} \right) = \log A - \log B.$$

(3) **LAW OF INVOLUTION (OR EVOLUTION).** *The logarithm of a number affected by an exponent equals the exponent multiplied by the logarithm of the number.*

$$\log (A)^n = n \times \log A,$$

$$\log (A)^{\frac{p}{q}} = \frac{p}{q} \times \log A.$$

The laws of *products, quotients, and involution (or evolution)* hold for logarithms to any base.

(4) **LAW OF THE CHARACTERISTIC.** *The common logarithm of a number has a characteristic one unit smaller than the number of digits to the left of the decimal point.*

$$\begin{aligned} \text{Thus, } \log 476.8 &= 2.67834, & \log 0.4768 &= \bar{1}.67834, \\ \log 47.68 &= 1.67834, & \log 0.04768 &= \bar{2}.67834. \end{aligned}$$

In case of a pure decimal the same law of characteristic holds, the number of digits being counted as negative. A negative characteristic is usually indicated by a dash over the integer.

$$\log 0.04768 = \bar{2}.67834.$$

In calculations involving *negative characteristics*, 10 is usually added, making the characteristic positive.

$$\text{Thus, } \log 0.917 = \bar{1}.96237 = 9.96237 - 10.$$

In case of root extraction, it is convenient to add 10 multiplied by the index of the root to be extracted. Thus,

$$\begin{aligned} \log (0.0732)^{\frac{1}{3}} &= \frac{1}{3} \times \log 0.0732 = \frac{1}{3} (\bar{2}.86451) = \frac{1}{3} (28.86451 - 30) \\ &= 9.62150 - 10 = \bar{1}.62150. \end{aligned}$$

In this example, 3 or any multiple of 3 could have been added and subtracted.

(5) **LAW OF THE MANTISSA.** *The mantissæ of the logarithms of all numbers composed of the same sequence of digits are the same.*

$$\begin{aligned} \text{Thus, } \log 5297 &= 3.72403, & \log 0.5297 &= \bar{1}.72403, \\ \log 52.97 &= 1.72403, & \log 0.05297 &= \bar{2}.72403. \end{aligned}$$

**3. The Co-Logarithm (Arithmetical Complement).** The *co-logarithm* of a number is the logarithm of that number subtracted from unity or from 10. Thus,

$$\text{co-log } 824 = 10 - \log 824 = 10 - 2.91593 = 7.08407.$$

*The co-logarithm of a number may be written down by beginning at the left-hand digit of its logarithm and subtracting each digit from 9 except the last significant one, which must be taken from 10.*

In performing division by means of logarithms, the logarithm of the denominator must be taken from that of the numerator. Instead of subtracting the logarithm of the denominator, its co-logarithm may be added to the logarithm of the numerator.

$$\begin{aligned} \text{EXAMPLE.} \quad \log(564 \div 328) &= \log 564 - \log 328 \\ &= \log 564 = 2.75128 \\ &+ \text{co-log } 328 = \underline{7.48413} \\ &= 0.23541 \end{aligned}$$

The common logarithms shown in Tables I and II are approximations to five decimal places of mantissæ. Table III shows the *natural values* of the trigonometric functions to four decimal places. Table IV contains a miscellaneous collection of short tables each of which is indicated by its title.

In any one of these Tables a dash underneath a terminal 5, thus  $\underline{5}$ , indicates that the true value is smaller than 5.

EXAMPLE.  $\log 7292 = 3.8628\underline{5}$  to five decimals, but from six-place tables,  $\log 7292 = 3.862847$ .

TABLE I

This Table, pages 1–19, shows the *common* or *Briggian* logarithms of numbers from 1 to 10,009. On page 1 the characteristics and mantissæ of the logarithms of numbers from 1 to 100 are shown; pages 2–19 show the mantissæ only, the characteristics being supplied by *Law of the Characteristic* explained above.

Pages 2–19 show the first three digits of the number, whose logarithm may be required, in column marked **N**; the next digit is in a column with the proper heading, **0, 1, 2, . . . , 9**, shown in the horizontal row at top and bottom of the page. If a number consists of more than *four* digits its logarithm may be approximated by using the column marked *proportional parts* (**Prop. Pts.**). The first two digits of the mantissæ are shown in column marked **0**; an asterisk \* in this Table indicates that the first two digits of the mantissæ must be taken from the following horizontal row.

EXAMPLES. 1. Find  $\log 4876$ .

- (1) Find first three figures 487 in column **N**, p. 9.
- (2) Follow along the horizontal row of 487 to column 6.
- (3) We now have the mantissa, 68806.
- (4) Determine the characteristic, 3.

$$\therefore \log 4876 = 3.68806.$$

2. Find  $\log 54973$ .

- (1) Find the first four figures, p. 10, as above.
- (2) Determine the characteristic, 4.

$$\log 54970 = 4.74013.$$

The first two figures of the mantissa come from line below.

(3) On the same page,  $\log 54980 = 4.74020$ , showing an increase of 7 in the mantissa for 10 in the number.

(4) An increase of 3 in the number =  $\frac{3}{10} \times 7 = 2.1$  in the mantissa.

$$\therefore \log 54973 = 4.74013 + 2 = 4.74015.$$

The difference in successive mantissæ on page 10 will be found to be 7, 8, or 9; and the corrections for a fifth figure 1, 2, 3, 4, 5, 6, 7, 8, 9 are shown in the marginal column marked **Prop. Pts.**

3. Find  $\log 34.4764$ .

We find the first four digits on p. 6,

$$\begin{array}{r} \log 34.4700 = 1.53744, \text{ tabular difference } 13, \\ \text{correction } 6 = \quad \quad 7.8, \text{ from Prop. Pts. column,} \\ \text{correction } 0.4 = \underline{\quad \quad .5}, \\ \therefore \log 34.4764 = 1.53752 \end{array}$$

4. Find  $N$ , when  $\log N = 3.57824$ .

(1) The characteristic 3 shows that  $N$  has four digits to the left of the decimal point.

(2) Find the mantissa nearest to 57824, p. 7. This is 57818, which is 6 smaller than the given mantissa.

(3) From p. 7,

$$\begin{array}{l} N = 3786 + \text{corrections for 6 in a tabular difference of 12.} \\ \therefore N = 3786.5. \end{array}$$

The Prop. Pts. column shows this correction at once. A little practice will enable the computer to make the corrections mentally, merely writing down the corrected result.

## TABLE II

Table II, pages 22–73, contains five-place logarithms of the trigonometric sine, cosine, tangent, and cotangent for angles  $0^\circ$  to  $90^\circ$ . In this Table 10 has been added throughout to each characteristic.

Page 22 shows the common logarithm of the sine and tangent for each second from  $0''$  to  $3'$ , and the logarithms of cosine and cotangent for every second from  $89^\circ 57'$  to  $90^\circ$ .

Pages 23–28 show the logarithmic sine, tangent, and cosine for every  $10''$  for angles  $0^\circ$  to  $2^\circ$ , also the logarithmic cosine, cotangent, and sine for every  $10''$  for angles from  $88^\circ$  to  $90^\circ$ . Corrections for intermediate seconds may be easily interpolated.

Thus,

$\log \sin 1^\circ 6' 36'' = \log \sin 1^\circ 6' 30'' + \text{correction for } 6''$ . See p. 26.

$$\begin{aligned} \log \sin 1^\circ 6' 40'' &= 8.28761 \\ \log \sin 1^\circ 6' 30'' &= 8.28652 \\ \frac{6}{10} \text{ of difference} &= \frac{6}{10} \times (109) = 65.4 \end{aligned}$$

Hence,  $\log \sin 1^\circ 6' 36'' = 8.28652 + 65 = 8.28717$ .

Pages 29–73 contain the logarithms of the sine, tangent, cotangent and cosine for each minute of arc from  $0^\circ$  to  $90^\circ$ . The degrees are indicated at the top and bottom of each page, the minutes are in columns at the left and right of the page.

In columns marked **d**, are the tabular differences of the log sine and log cosine for each minute. In column marked **c. d.** are the tabular differences for the log tangent (log cotangent). These tabular differences show the correction for  $60''$ ; any smaller number of seconds, for example,  $35''$ , would have  $\frac{35}{60}$  of this tabular correction. In proportional parts (**Prop. Pts.**) column, these corrections are reduced to scale of  $1''$ , pages 29–34. On pages 35–73 the tabular corrections are reduced so as to show the corrections for  $6''$ ,  $7''$ ,  $8''$ ,  $9''$ ,  $10''$ ,  $20''$ ,  $30''$ ,  $40''$ ,  $50''$ . By pointing off the corrections for  $10''$ ,  $20''$ ,  $30''$ ,  $40''$ ,  $50''$ , corresponding corrections for  $1''$ ,  $2''$ ,  $3''$ ,  $4''$ ,  $5''$  may be obtained.

The corrections for seconds should be made *mentally* by aid of the proportional parts column, and the result of the corrected logarithm may be written at once.

**EXAMPLES. 1.** Find  $\log \sin 28^\circ 37' 21''$ .

$$\begin{aligned} \text{From p. 57,} \quad \log \sin 28^\circ 37' &= 9.68029, \text{ tabular difference } 23. \\ \text{Prop. Pts. for } 20'' &= \quad 7.7 \\ \text{Prop. Pts. for } 1'' &= \quad .38 \\ \therefore \log \sin 28^\circ 37' 21'' &= 9.68037 \end{aligned}$$

**2.** Find  $\log \cos 16^\circ 48' 24''$ .

$$\begin{aligned} \text{On p. 45,} \quad \log \cos 16^\circ 48' &= 9.98106, \text{ tabular difference } 4. \\ \text{Prop. Pts. for } 20'' &= \quad 1.3 \\ \text{Prop. Pts. for } 4'' &= \quad .27 \end{aligned} \left. \vphantom{\begin{aligned} \log \cos 16^\circ 48' \\ \text{Prop. Pts. for } 20'' \\ \text{Prop. Pts. for } 4'' \end{aligned}} \right\} \text{to be subtracted.}$$

$$\underline{9.98104}$$

Correction for log cosines and log cotangents are to be subtracted.

**3.** Find the angle  $x$ , when  $\log \tan x = 9.65948$ .

(1) Find in log tan column a log as near the given one as possible, p. 53.

$$(2) \quad \log \tan 24^\circ 32' = 9.65937,$$

with a difference of 11 to a tabular difference of 34.

(3) In Prop. Pts. column 11 to a scale of 34 shows a  $20''$  correction.

$$\therefore x = 24^\circ 32' 20''.$$

4. Find the angle  $x$ , when  $\log \cot x = 9.48726$ .

(1) On p. 46, in log cot column,

$$\log \cot 72^\circ 56' = 9.48714,$$

with a difference of 12 to a tabular difference of 45.

(2) In Prop. Pts. column 45,

$$\text{Correction for } 10'' = 7.5$$

$$\text{Correction for } 6'' = 4.5$$

$$\text{Hence, correction for } 16'' = 12.0$$

(3) Since cotangents increase with decrease of angle, subtract the 16'' correction, giving  $x = 72^\circ 55' 44''$ .

In addition to the acute angle set at the top and bottom of each page in the Table, pages 29–73,  $90^\circ +$  the acute angle,  $180^\circ +$  the angle, and  $270^\circ +$  the angle are printed in smaller type. Since the trigonometric functions of  $90^\circ + x$  and  $270^\circ + x$  change to co-functions of  $x$ , and the functions of  $180^\circ + x$  retain their names, we may find the logarithms of the trigonometric functions of any one of these larger angles. In each case the sign of the function must be noted as shown in the following table:

$x$	$\sin x$	$\cos x$	$\tan x$	$\cot x$	$\sec x$	$\csc x$
$90^\circ + x$	$+\cos x$	$-\sin x$	$-\cot x$	$-\tan x$	$-\csc x$	$+\sec x$
$180^\circ + x$	$-\sin x$	$-\cos x$	$+\tan x$	$+\cot x$	$-\sec x$	$-\csc x$
$270^\circ + x$	$-\cos x$	$+\sin x$	$-\cot x$	$-\tan x$	$+\csc x$	$-\sec x$

In the Table the angles marked by an asterisk (\*) are made up of  $90^\circ + x$ , or  $270^\circ + x$ ; this mark indicates that the co-function of  $x$  is to be taken. Otherwise the direct function of  $x$  is to be taken, proper regard being had for the algebraic sign in each case.

TABLE III

Pages 75–93 contain four-place tables of the natural trigonometric functions for each minute. The sines and cosines appear upon the left-hand pages, the tangents and cotangents upon the right.

TABLE IV

Table IV, pages 95–99, contains (1) a table of radian measure  $0^\circ$  to  $180^\circ$  for each degree; also for  $1'$  to  $60'$  and for  $1''$  to  $60''$ ; (2) two tables of natural logarithms of numbers from 1 to 200 and 1 to 9.9 by tenths; (3) a table of hyperbolic functions,  $\sinh x$ ,  $\cosh x$ ,  $x$  varying from 0.01 to 1 by hundredths.

LOGARITHMIC, TRIGONOMETRIC,  
AND OTHER TABLES

log of a number to a new  
base equals log to old base times  
log of old base to new base.



# TABLE I



THE

## COMMON OR BRIGGIAN LOGARITHMS

OF

### NUMBERS

From 1 to 10009

NOTE. A \* in Table I indicates that the first two digits of the mantissa are to be taken from the following line.

A dash underneath a terminal 5, thus  $\bar{5}$ , indicates that the true value is less than 5.

#### 1-100

N	log	N	log	N	log	N	log	N	log
1	0. 00 000	21	1. 32 222	41	1. 61 278	61	1. 78 533	81	1. 90 849
2	0. 30 103	22	1. 34 242	42	1. 62 325	62	1. 79 239	82	1. 91 381
3	0. 47 712	23	1. 36 173	43	1. 63 347	63	1. 79 934	83	1. 91 908
4	0. 60 206	24	1. 38 021	44	1. 64 345	64	1. 80 618	84	1. 92 428
5	0. 69 897	25	1. 39 794	45	1. 65 321	65	1. 81 291	85	1. 92 942
6	0. 77 815	26	1. 41 497	46	1. 66 276	66	1. 81 954	86	1. 93 450
7	0. 84 510	27	1. 43 136	47	1. 67 210	67	1. 82 607	87	1. 93 952
8	0. 90 309	28	1. 44 716	48	1. 68 124	68	1. 83 251	88	1. 94 448
9	0. 95 424	29	1. 46 240	49	1. 69 020	69	1. 83 885	89	1. 94 939
10	1. 00 000	30	1. 47 712	50	1. 69 897	70	1. 84 510	90	1. 95 424
11	1. 04 139	31	1. 49 136	51	1. 70 757	71	1. 85 126	91	1. 95 904
12	1. 07 918	32	1. 50 515	52	1. 71 600	72	1. 85 733	92	1. 96 379
13	1. 11 394	33	1. 51 851	53	1. 72 428	73	1. 86 332	93	1. 96 848
14	1. 14 613	34	1. 53 148	54	1. 73 239	74	1. 86 923	94	1. 97 313
15	1. 17 609	35	1. 54 407	55	1. 74 036	75	1. 87 506	95	1. 97 772
16	1. 20 412	36	1. 55 630	56	1. 74 819	76	1. 88 081	96	1. 98 227
17	1. 23 045	37	1. 56 820	57	1. 75 587	77	1. 88 649	97	1. 98 677
18	1. 25 527	38	1. 57 978	58	1. 76 343	78	1. 89 209	98	1. 99 123
19	1. 27 875	39	1. 59 106	59	1. 77 085	79	1. 89 763	99	1. 99 564
20	1. 30 103	40	1. 60 206	60	1. 77 815	80	1. 90 309	100	2. 00 000
N	log	N	log	N	log	N	log	N	log

100-150

N.	L.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
100	00	000	043	087	130	173	217	260	303	346	389	
01		432	475	518	561	604	647	689	732	775	817	44 43 42
02		860	903	945	988	*030	*072	*115	*157	*199	*242	1 4.4 4.3 4.2
03	01	284	326	368	410	452	494	536	578	620	662	2 8.8 8.6 8.4
04		703	745	787	828	870	912	953	995	*036	*078	3 13.2 12.9 12.6
05	02	119	160	202	243	284	325	366	407	449	490	4 17.6 17.2 16.8
06		531	572	612	653	694	735	776	816	857	898	5 22.0 21.5 21.0
07		938	979	*019	*060	*100	*141	*181	*222	*262	*302	6 26.4 25.8 25.2
08	03	342	383	423	463	503	543	583	623	663	703	7 30.8 30.1 29.4
09		743	782	822	862	902	941	981	*021	*060	*100	8 35.2 34.4 33.6
110	04	139	179	218	258	297	336	376	415	454	493	9 39.6 38.7 37.8
11		532	571	610	650	689	727	766	805	844	883	41 40 39
12		922	961	999	*038	*077	*115	*154	*192	*231	*269	1 4.1 4.0 3.9
13	05	308	346	385	423	461	500	538	576	614	652	2 8.2 8.0 7.8
14		690	729	767	805	843	881	918	956	994	*032	3 12.3 12.0 11.7
15	06	070	108	145	183	221	258	296	333	371	408	4 16.4 16.0 15.6
16		446	483	521	558	595	633	670	707	744	781	5 20.5 20.0 19.5
17		819	856	893	930	967	*004	*041	*078	*115	*151	6 24.6 24.0 23.4
18	07	188	225	262	298	335	372	408	445	482	518	7 28.7 28.0 27.3
19		555	591	628	664	700	737	773	809	846	882	8 32.8 32.0 31.2
120		918	954	990	*027	*063	*099	*135	*171	*207	*243	9 36.9 36.0 35.1
21	08	279	314	350	386	422	458	493	529	565	600	38 37 36
22		636	672	707	743	778	814	849	884	920	955	1 3.8 3.7 3.6
23		991	*026	*061	*096	*132	*167	*202	*237	*272	*307	2 7.6 7.4 7.2
24	09	342	377	412	447	482	517	552	587	621	656	3 11.4 11.1 10.8
25		691	726	760	795	830	864	899	934	968	*003	4 15.2 14.8 14.4
26	10	037	072	106	140	175	209	243	278	312	346	5 19.0 18.5 18.0
27		380	415	449	483	517	551	585	619	653	687	6 22.8 22.2 21.6
28		721	755	789	823	857	890	924	958	992	*025	7 26.6 25.9 25.2
29	11	059	093	126	160	193	227	261	294	327	361	8 30.4 29.6 28.8
130		394	428	461	494	528	561	594	628	661	694	9 34.2 33.3 32.4
31		727	760	793	826	860	893	926	959	992	*024	35 34 33
32	12	057	090	123	156	189	222	254	287	320	352	1 3.5 3.4 3.3
33		385	418	450	483	516	548	581	613	646	678	2 7.0 6.8 6.6
34		710	743	775	808	840	872	905	937	969	*001	3 10.5 10.2 9.9
35	13	033	066	098	130	162	194	226	258	290	322	4 14.0 13.6 13.2
36		354	386	418	450	481	513	545	577	609	640	5 17.5 17.0 16.5
37		672	704	735	767	799	830	862	893	925	956	6 21.0 20.4 19.8
38		988	*019	*051	*082	*114	*145	*176	*208	*239	*270	7 24.5 23.8 23.1
39	14	301	333	364	395	426	457	489	520	551	582	8 28.0 27.2 26.4
140		613	644	675	706	737	768	799	829	860	891	9 31.5 30.6 29.7
41		922	953	983	*014	*045	*076	*106	*137	*168	*198	32 31 30
42	15	229	259	290	320	351	381	412	442	473	503	1 3.2 3.1 3.0
43		534	564	594	625	655	685	715	746	776	806	2 6.4 6.2 6.0
44		836	866	897	927	957	987	*017	*047	*077	*107	3 9.6 9.3 9.0
45	16	137	167	197	227	256	286	316	346	376	406	4 12.8 12.4 12.0
46		435	465	495	524	554	584	613	643	673	702	5 16.0 15.5 15.0
47		732	761	791	820	850	879	909	938	967	997	6 19.2 18.6 18.0
48	17	026	056	085	114	143	173	202	231	260	289	7 22.4 21.7 21.0
49		319	348	377	406	435	464	493	522	551	580	8 25.6 24.8 24.0
150		609	638	667	696	725	754	782	811	840	869	9 28.8 27.9 27.0
N.	L.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

LOGARITHMS OF NUMBERS

150-200

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
150	17 609	638	667	696	725	754	782	811	840	869	
51	898	926	955	984	*013	*041	*070	*099	*127	*156	
52	18 184	213	241	270	298	327	355	384	412	441	29 28
53	469	498	526	554	583	611	639	667	696	724	1 2.9 2.8
54	752	780	808	837	865	893	921	949	977	*005	2 5.8 5.6
55	19 033	061	089	117	145	173	201	229	257	285	3 8.7 8.4
56	312	340	368	396	424	451	479	507	535	562	4 11.6 11.2
57	590	618	645	673	700	728	756	783	811	838	5 14.5 14.0
58	866	893	921	948	976	*003	*030	*058	*085	*112	6 17.4 16.8
59	20 140	167	194	222	249	276	303	330	358	385	7 20.3 19.6
160	412	439	466	493	520	548	575	602	629	656	8 23.2 22.4
61	683	710	737	763	790	817	844	871	898	925	9 26.1 25.2
62	952	978	*005	*032	*059	*085	*112	*139	*165	*192	27 26
63	21 219	245	272	299	325	352	378	405	431	458	1 2.7 2.6
64	484	511	537	564	590	617	643	669	696	722	2 5.4 5.2
65	748	775	801	827	854	880	906	932	958	985	3 8.1 7.8
66	22 011	037	063	089	115	141	167	194	220	246	4 10.8 10.4
67	272	298	324	350	376	401	427	453	479	505	5 13.5 13.0
68	531	557	583	608	634	660	686	712	737	763	6 16.2 15.6
69	789	814	840	866	891	917	943	968	994	*019	7 18.9 18.2
170	23 045	070	096	121	147	172	198	223	249	274	8 21.6 20.8
71	300	325	350	376	401	426	452	477	502	528	9 24.3 23.4
72	553	578	603	629	654	679	704	729	754	779	25
73	805	830	855	880	905	930	955	980	*005	*030	1 2.5
74	24 055	080	105	130	155	180	204	229	254	279	2 5.0
75	304	329	353	378	403	428	452	477	502	527	3 7.5
76	551	576	601	625	650	674	699	724	748	773	4 10.0
77	797	822	846	871	895	920	944	969	993	*018	5 12.5
78	25 042	066	091	115	139	164	188	212	237	261	6 15.0
79	285	310	334	358	382	406	431	455	479	503	7 17.5
180	527	551	575	600	624	648	672	696	720	744	8 20.0
81	768	792	816	840	864	888	912	935	959	983	9 22.5
82	26 007	031	055	079	102	126	150	174	198	221	24 23
83	245	269	293	316	340	364	387	411	435	458	1 2.4 2.3
84	482	505	529	553	576	600	623	647	670	694	2 4.8 4.6
85	717	741	764	788	811	834	858	881	905	928	3 7.2 6.9
86	951	975	998	*021	*045	*068	*091	*114	*138	*161	4 9.6 9.2
87	27 184	207	231	254	277	300	323	346	370	393	5 12.0 11.5
88	416	439	462	485	508	531	554	577	600	623	6 14.4 13.8
89	646	669	692	715	738	761	784	807	830	852	7 16.8 16.1
190	875	898	921	944	967	989	*012	*035	*058	*081	8 19.2 18.4
91	28 103	126	149	171	194	217	240	262	285	307	9 21.6 20.7
92	330	353	375	398	421	443	466	488	511	533	22 21
93	556	578	601	623	646	668	691	713	735	758	1 2.2 2.1
94	780	803	825	847	870	892	914	937	959	981	2 4.4 4.2
95	29 003	026	048	070	092	115	137	159	181	203	3 6.6 6.3
96	226	248	270	292	314	336	358	380	403	425	4 8.8 8.4
97	447	469	491	513	535	557	579	601	623	645	5 11.0 10.5
98	667	688	710	732	754	776	798	820	842	863	6 13.2 12.6
99	885	907	929	951	973	994	*016	*038	*060	*081	7 15.4 14.7
200	30 103	125	146	168	190	211	233	255	276	298	8 17.6 16.8
											9 19.8 18.9
N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.

200-250

N.	L.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
<b>200</b>	30	103	125	146	168	190	211	233	255	276	298	
01		320	341	363	384	406	428	449	471	492	514	
02		535	557	578	600	621	643	664	685	707	728	
03		750	771	792	814	835	856	878	899	920	942	
04		963	984	*006	*027	*048	*069	*091	*112	*133	*154	
05	31	175	197	218	239	260	281	302	323	345	366	
06		387	408	429	450	471	492	513	534	555	576	
07		597	618	639	660	681	702	723	744	765	785	
08		806	827	848	869	890	911	931	952	973	994	
09	32	015	035	056	077	098	118	139	160	181	201	
<b>210</b>		222	243	263	284	305	325	346	366	387	408	
11		428	449	469	490	510	531	552	572	593	613	
12		634	654	675	695	715	736	756	777	797	818	
13		838	858	879	899	919	940	960	980	*001	*021	
14	33	041	062	082	102	122	143	163	183	203	224	
15		244	264	284	304	325	345	365	385	405	425	
16		445	465	486	506	526	546	566	586	606	626	
17		646	666	686	706	726	746	766	786	806	826	
18		846	866	885	905	925	945	965	985	*005	*025	
19	34	044	064	084	104	124	143	163	183	203	223	
<b>220</b>		242	262	282	301	321	341	361	380	400	420	
21		439	459	479	498	518	537	557	577	596	616	
22		635	655	674	694	713	733	753	772	792	811	
23		830	850	869	889	908	928	947	967	986	*005	
24	35	025	044	064	083	102	122	141	160	180	199	
25		218	238	257	276	295	315	334	353	372	392	
26		411	430	449	468	488	507	526	545	564	583	
27		603	622	641	660	679	698	717	736	755	774	
28		793	813	832	851	870	889	908	927	946	965	
29		984	*003	*021	*040	*059	*078	*097	*116	*135	*154	
<b>230</b>	36	173	192	211	229	248	267	286	305	324	342	
31		361	380	399	418	436	455	474	493	511	530	
32		549	568	586	605	624	642	661	680	698	717	
33		736	754	773	791	810	829	847	866	884	903	
34		922	940	959	977	996	*014	*033	*051	*070	*088	
35	37	107	125	144	162	181	199	218	236	254	273	
36		291	310	328	346	365	383	401	420	438	457	
37		475	493	511	530	548	566	585	603	621	639	
38		658	676	694	712	731	749	767	785	803	822	
39		840	858	876	894	912	931	949	967	985	*003	
<b>240</b>	38	021	039	057	075	093	112	130	148	166	184	
41		202	220	238	256	274	292	310	328	346	364	
42		382	399	417	435	453	471	489	507	525	543	
43		561	578	596	614	632	650	668	686	703	721	
44		739	757	775	792	810	828	846	863	881	899	
45		917	934	952	970	987	*005	*023	*041	*058	*076	
46	39	094	111	129	146	164	182	199	217	235	252	
47		270	287	305	322	340	358	375	393	410	428	
48		445	463	480	498	515	533	550	568	585	602	
49		620	637	655	672	690	707	724	742	759	777	
<b>250</b>		794	811	829	846	863	881	898	915	933	950	

	22	21
1	2.2	2.1
2	4.4	4.2
3	6.6	6.3
4	8.8	8.4
5	11.0	10.5
6	13.2	12.6
7	15.4	14.7
8	17.6	16.8
9	19.8	18.9

	20
1	2.0
2	4.0
3	6.0
4	8.0
5	10.0
6	12.0
7	14.0
8	16.0
9	18.0

	19
1	1.9
2	3.8
3	5.7
4	7.6
5	9.5
6	11.4
7	13.3
8	15.2
9	17.1

	18
1	1.8
2	3.6
3	5.4
4	7.2
5	9.0
6	10.8
7	12.6
8	14.4
9	16.2

	17
1	1.7
2	3.4
3	5.1
4	6.8
5	8.5
6	10.2
7	11.9
8	13.6
9	15.3

N.	L.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
----	----	---	---	---	---	---	---	---	---	---	---	------------

250-300

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
<b>250</b>	39 794	811	829	846	863	881	898	915	933	950	
51	967	985	*002	*019	*037	*054	*071	*088	*106	*123	18
52	40 140	157	175	192	209	226	243	261	278	295	1
53	312	329	346	364	381	398	415	432	449	466	2
54	483	500	518	535	552	569	586	603	620	637	3
55	654	671	688	705	722	739	756	773	790	807	4
56	824	841	858	875	892	909	926	943	960	976	5
57	993	*010	*027	*044	*061	*078	*095	*111	*128	*145	6
58	41 162	179	196	212	229	246	263	280	296	313	7
59	330	347	363	380	397	414	430	447	464	481	8
<b>260</b>	497	514	531	547	564	581	597	614	631	647	9
61	664	681	697	714	731	747	764	780	797	814	17
62	830	847	863	880	896	913	929	946	963	979	1
63	996	*012	*029	*045	*062	*078	*095	*111	*127	*144	2
64	42 160	177	193	210	226	243	259	275	292	308	3
65	325	341	357	374	390	406	423	439	455	472	4
66	488	504	521	537	553	570	586	602	619	635	5
67	651	667	684	700	716	732	749	765	781	797	6
68	813	830	846	862	878	894	911	927	943	959	7
69	975	991	*008	*024	*040	*056	*072	*088	*104	*120	8
<b>270</b>	43 136	152	169	185	201	217	233	249	265	281	9
71	297	313	329	345	361	377	393	409	425	441	16
72	457	473	489	505	521	537	553	569	584	600	1
73	616	632	648	664	680	696	712	727	743	759	2
74	775	791	807	823	838	854	870	886	902	917	3
75	933	949	965	981	996	*012	*028	*044	*059	*075	4
76	44 091	107	122	138	154	170	185	201	217	232	5
77	248	264	279	295	311	326	342	358	373	389	6
78	404	420	436	451	467	483	498	514	529	545	7
79	560	576	592	607	623	638	654	669	685	700	8
<b>280</b>	716	731	747	762	778	793	809	824	840	855	9
81	871	886	902	917	932	948	963	979	994	*010	15
82	45 025	040	056	071	086	102	117	133	148	163	1
83	179	194	209	225	240	255	271	286	301	317	2
84	332	347	362	378	393	408	423	439	454	469	3
85	484	500	515	530	545	561	576	591	606	621	4
86	637	652	667	682	697	712	728	743	758	773	5
87	788	803	818	834	849	864	879	894	909	924	6
88	939	954	969	984	*000	*015	*030	*045	*060	*075	7
89	46 090	105	120	135	150	165	180	195	210	225	8
<b>290</b>	240	255	270	285	300	315	330	345	359	374	9
91	389	404	419	434	449	464	479	494	509	523	14
92	538	553	568	583	598	613	627	642	657	672	1
93	687	702	716	731	746	761	776	790	805	820	2
94	835	850	864	879	894	909	923	938	953	967	3
95	982	997	*012	*026	*041	*056	*070	*085	*100	*114	4
96	47 129	144	159	173	188	202	217	232	246	261	5
97	276	290	305	319	334	349	363	378	392	407	6
98	422	436	451	465	480	494	509	524	538	553	7
99	567	582	596	611	625	640	654	669	683	698	8
<b>300</b>	712	727	741	756	770	784	799	813	828	842	9
N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.

300-350

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
<b>300</b>	47 712	727	741	756	770	784	799	813	828	842	
01	857	871	885	900	914	929	943	958	972	986	
02	48 001	015	029	044	058	073	087	101	116	130	
03	144	159	173	187	202	216	230	244	259	273	
04	287	302	316	330	344	359	373	387	401	416	15
05	430	444	458	473	487	501	515	530	544	558	1 1.5
06	572	586	601	615	629	643	657	671	686	700	2 3.0
07	714	728	742	756	770	785	799	813	827	841	3 4.5
08	855	869	883	897	911	926	940	954	968	982	4 6.0
09	996	*010	*024	*038	*052	*066	*080	*094	*108	*122	5 7.5
<b>310</b>	49 136	150	164	178	192	206	220	234	248	262	6 9.0
11	276	290	304	318	332	346	360	374	388	402	7 10.5
12	415	429	443	457	471	485	499	513	527	541	8 12.0
13	554	568	582	596	610	624	638	651	665	679	9 13.5
14	693	707	721	734	748	762	776	790	803	817	
15	831	845	859	872	886	900	914	927	941	955	14
16	969	982	996	*010	*024	*037	*051	*065	*079	*092	1 1.4
17	50 106	120	133	147	161	174	188	202	215	229	2 2.8
18	243	256	270	284	297	311	325	338	352	365	3 4.2
19	379	393	406	420	433	447	461	474	488	501	4 5.6
<b>320</b>	515	529	542	556	569	583	596	610	623	637	5 7.0
21	651	664	678	691	705	718	732	745	759	772	6 8.4
22	786	799	813	826	840	853	866	880	893	907	7 9.8
23	920	934	947	961	974	987	*001	*014	*028	*041	8 11.2
24	51 055	068	081	095	108	121	135	148	162	175	9 12.6
25	188	202	215	228	242	255	268	282	295	308	
26	322	335	348	362	375	388	402	415	428	441	
27	455	468	481	495	508	521	534	548	561	574	13
28	587	601	614	627	640	654	667	680	693	706	1 1.3
29	720	733	746	759	772	786	799	812	825	838	2 2.6
<b>330</b>	851	865	878	891	904	917	930	943	957	970	3 3.9
31	983	996	*009	*022	*035	*048	*061	*075	*088	*101	4 5.2
32	52 114	127	140	153	166	179	192	205	218	231	5 6.5
33	244	257	270	284	297	310	323	336	349	362	6 7.8
34	375	388	401	414	427	440	453	466	479	492	7 9.1
35	504	517	530	543	556	569	582	595	608	621	8 10.4
36	634	647	660	673	686	699	711	724	737	750	9 11.7
37	763	776	789	802	815	827	840	853	866	879	
38	892	905	917	930	943	956	969	982	994	*007	
39	53 020	033	046	058	071	084	097	110	122	135	12
<b>340</b>	148	161	173	186	199	212	224	237	250	263	1 1.2
41	275	288	301	314	326	339	352	364	377	390	2 2.4
42	403	415	428	441	453	466	479	491	504	517	3 3.6
43	529	542	555	567	580	593	605	618	631	643	4 4.8
44	656	668	681	694	706	719	732	744	757	769	5 6.0
45	782	794	807	820	832	845	857	870	882	895	6 7.2
46	908	920	933	945	958	970	983	995	*008	*020	7 8.4
47	54 033	045	058	070	083	095	108	120	133	145	8 9.6
48	158	170	183	195	208	220	233	245	258	270	9 10.8
49	283	295	307	320	332	345	357	370	382	394	
<b>350</b>	407	419	432	444	456	469	481	494	506	518	
N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.

350-400

N.	L.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
<b>350</b>	54	407	419	432	444	456	469	481	494	506	518	
51		531	543	555	568	580	593	605	617	630	642	
52		654	667	679	691	704	716	728	741	753	765	
53		777	790	802	814	827	839	851	864	876	888	
54		900	913	925	937	949	962	974	986	998	*011	
55	55	023	035	047	060	072	084	096	108	121	133	18
56		145	157	169	182	194	206	218	230	242	255	1 1.3
57		267	279	291	303	315	328	340	352	364	376	2 2.6
58		388	400	413	425	437	449	461	473	485	497	3 3.0
59		509	522	534	546	558	570	582	594	606	618	4 5.2
<b>360</b>		630	642	654	666	678	691	703	715	727	739	5 6.5
61		751	763	775	787	799	811	823	835	847	859	6 7.8
62		871	883	895	907	919	931	943	955	967	979	7 9.1
63		991	*003	*015	*027	*038	*050	*062	*074	*086	*098	8 10.4
64	56	110	122	134	146	158	170	182	194	205	217	9 11.7
65		229	241	253	265	277	289	301	312	324	336	
66		348	360	372	384	396	407	419	431	443	455	
67		467	478	490	502	514	526	538	549	561	573	12
68		585	597	608	620	632	644	656	667	679	691	1 1.2
69		703	714	726	738	750	761	773	785	797	808	2 2.4
<b>370</b>		820	832	844	855	867	879	891	902	914	926	3 3.6
71		937	949	961	972	984	996	*008	*019	*031	*043	4 4.8
72	57	054	066	078	089	101	113	124	136	148	159	5 6.0
73		171	183	194	206	217	229	241	252	264	276	6 7.2
74		287	299	310	322	334	345	357	368	380	392	7 8.4
75		403	415	426	438	449	461	473	484	496	507	8 9.6
76		519	530	542	553	565	576	588	600	611	623	9 10.8
77		634	646	657	669	680	692	703	715	726	738	
78		749	761	772	784	795	807	818	830	841	852	
79		864	875	887	898	910	921	933	944	955	967	11
<b>380</b>		978	990	*001	*013	*024	*035	*047	*058	*070	*081	1 1.1
81	58	092	104	115	127	138	149	161	172	184	195	2 2.2
82		206	218	229	240	252	263	274	286	297	309	3 3.3
83		320	331	343	354	365	377	388	399	410	422	4 4.4
84		433	444	456	467	478	490	501	512	524	535	5 5.5
85		546	557	569	580	591	602	614	625	636	647	6 6.6
86		659	670	681	692	704	715	726	737	749	760	7 7.7
87		771	782	794	805	816	827	838	850	861	872	8 8.8
88		883	894	906	917	928	939	950	961	973	984	9 9.9
89		995	*006	*017	*028	*040	*051	*062	*073	*084	*095	
<b>390</b>	59	106	118	129	140	151	162	173	184	195	207	10
91		218	229	240	251	262	273	284	295	306	318	1 1.0
92		329	340	351	362	373	384	395	406	417	428	2 2.0
93		439	450	461	472	483	494	506	517	528	539	3 3.0
94		550	561	572	583	594	605	616	627	638	649	4 4.0
95		660	671	682	693	704	715	726	737	748	759	5 5.0
96		770	780	791	802	813	824	835	846	857	868	6 6.0
97		879	890	901	912	923	934	945	956	966	977	7 7.0
98		988	999	*010	*021	*032	*043	*054	*065	*076	*086	8 8.0
99	60	097	108	119	130	141	152	163	173	184	195	9 9.0
<b>400</b>		206	217	228	239	249	260	271	282	293	304	

400-450

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
400	60 206	217	228	239	249	260	271	282	293	304	
01	314	325	336	347	358	369	379	390	401	412	
02	423	433	444	455	466	477	487	498	509	520	
03	531	541	552	563	574	584	595	606	617	627	
04	638	649	660	670	681	692	703	713	724	735	
05	746	756	767	778	788	799	810	821	831	842	
06	853	863	874	885	895	906	917	927	938	949	
07	959	970	981	991	*002	*013	*023	*034	*045	*055	11
08	61 066	077	087	098	109	119	130	140	151	162	1 1.1
09	172	183	194	204	215	225	236	247	257	268	2 2.2
410	278	289	300	310	321	331	342	352	363	374	3 3.3
11	384	395	405	416	426	437	448	458	469	479	4 4.4
12	490	500	511	521	532	542	553	563	574	584	5 5.5
13	595	606	616	627	637	648	658	669	679	690	6 6.6
14	700	711	721	731	742	752	763	773	784	794	7 7.7
15	805	815	826	836	847	857	868	878	888	899	8 8.8
16	909	920	930	941	951	962	972	982	993	*003	9 9.9
17	62 014	024	034	045	055	066	076	086	097	107	
18	118	128	138	149	159	170	180	190	201	211	
19	221	232	242	252	263	273	284	294	304	315	
420	325	335	346	356	366	377	387	397	408	418	
21	428	439	449	459	469	480	490	500	511	521	
22	531	542	552	562	572	583	593	603	613	624	
23	634	644	655	665	675	685	696	706	716	726	10
24	737	747	757	767	778	788	798	808	818	829	1 1.0
25	839	849	859	870	880	890	900	910	921	931	2 2.0
26	941	951	961	972	982	992	*002	*012	*022	*033	3 3.0
27	63 043	053	063	073	083	094	104	114	124	134	4 4.0
28	144	155	165	175	185	195	205	215	225	236	5 5.0
29	246	256	266	276	286	296	306	317	327	337	6 6.0
430	347	357	367	377	387	397	407	417	428	438	7 7.0
31	448	458	468	478	488	498	508	518	528	538	8 8.0
32	548	558	568	579	589	599	609	619	629	639	9 9.0
33	649	659	669	679	689	699	709	719	729	739	
34	749	759	769	779	789	799	809	819	829	839	
35	849	859	869	879	889	899	909	919	929	939	
36	949	959	969	979	988	998	*008	*018	*028	*038	
37	64 048	058	068	078	088	098	108	118	128	137	9
38	147	157	167	177	187	197	207	217	227	237	1 0.0
39	246	256	266	276	286	296	306	316	326	335	2 1.8
440	345	355	365	375	385	395	404	414	424	434	3 2.7
41	444	454	464	473	483	493	503	513	523	532	4 3.6
42	542	552	562	572	582	591	601	611	621	631	5 4.5
43	640	650	660	670	680	689	699	709	719	729	6 5.4
44	738	748	758	768	777	787	797	807	816	826	7 6.3
45	836	846	856	865	875	885	895	904	914	924	8 7.2
46	933	943	953	963	972	982	992	*002	*011	*021	9 8.1
47	65 031	040	050	060	070	079	089	099	108	118	
48	128	137	147	157	167	176	186	196	205	215	
49	225	234	244	254	263	273	283	292	302	312	
450	321	331	341	350	360	369	379	389	398	408	
N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.



450-500

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
450	65 321	331	341	350	360	369	379	389	398	408	
51	418	427	437	447	456	466	475	485	495	504	
52	514	523	533	543	552	562	571	581	591	601	
53	610	619	629	639	648	658	667	677	686	696	
54	706	715	725	734	744	753	763	772	782	792	
55	801	811	820	830	839	849	858	868	877	887	
56	896	906	916	925	935	944	954	963	973	982	
57	992	*001	*011	*020	*030	*039	*049	*058	*068	*077	10
58	66 087	096	106	115	124	134	143	153	162	172	1 1.0
59	181	191	200	210	219	229	238	247	257	266	2 2.0
460	276	285	295	304	314	323	332	342	351	361	3 3.0
61	370	380	389	398	408	417	427	436	445	455	4 4.0
62	464	474	483	492	502	511	521	530	539	549	5 5.0
63	558	567	577	586	596	605	614	624	633	642	6 6.0
64	652	661	671	680	689	699	708	717	727	736	7 7.0
65	745	755	764	773	783	792	801	811	820	829	8 8.0
66	839	848	857	867	876	885	894	904	913	922	9 9.0
67	932	941	950	960	969	978	987	997	*006	*015	
68	67 025	034	043	052	062	071	080	089	099	108	
69	117	127	136	145	154	164	173	182	191	201	
470	210	219	228	237	247	256	265	274	284	293	
71	302	311	321	330	339	348	357	367	376	385	
72	394	403	413	422	431	440	449	459	468	477	9
73	486	495	504	514	523	532	541	550	560	569	1 0.9
74	578	587	596	605	614	624	633	642	651	660	2 1.8
75	669	679	688	697	706	715	724	733	742	752	3 2.7
76	761	770	779	788	797	806	815	825	834	843	4 3.6
77	852	861	870	879	888	897	906	916	925	934	5 4.5
78	943	952	961	970	979	988	997	*006	*015	*024	6 5.4
79	68 034	043	052	061	070	079	088	097	106	115	7 6.3
480	124	133	142	151	160	169	178	187	196	205	8 7.2
81	215	224	233	242	251	260	269	278	287	296	9 8.1
82	305	314	323	332	341	350	359	368	377	386	
83	395	404	413	422	431	440	449	458	467	476	
84	485	494	502	511	520	529	538	547	556	565	
85	574	583	592	601	610	619	628	637	646	655	
86	664	673	681	690	699	708	717	726	735	744	
87	753	762	771	780	789	797	806	815	824	833	8
88	842	851	860	869	878	886	895	904	913	922	1 0.8
89	931	940	949	958	966	975	984	993	*002	*011	2 1.6
490	69 020	028	037	046	055	064	073	082	090	099	3 2.4
91	108	117	126	135	144	152	161	170	179	188	4 3.2
92	197	205	214	223	232	241	249	258	267	276	5 4.0
93	285	294	302	311	320	329	338	346	355	364	6 4.8
94	373	381	390	399	408	417	425	434	443	452	7 5.6
95	461	469	478	487	496	504	513	522	531	539	8 6.4
96	548	557	566	574	583	592	601	609	618	627	9 7.2
97	636	644	653	662	671	679	688	697	705	714	
98	723	732	740	749	758	767	775	784	793	801	
99	810	819	827	836	845	854	862	871	880	888	
500	897	906	914	923	932	940	949	958	966	975	
N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.

500-550

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
<b>500</b>	69 897	906	914	923	932	940	949	958	966	975	
01	984	992	*001	*010	*018	*027	*036	*044	*053	*062	
02	70 070	079	088	096	105	114	122	131	140	148	
03	157	165	174	183	191	200	209	217	226	234	
04	243	252	260	269	278	286	295	303	312	321	
05	329	338	346	355	364	372	381	389	398	406	
06	415	424	432	441	449	458	467	475	484	492	
07	501	509	518	526	535	544	552	561	569	578	9
08	586	595	603	612	621	629	638	646	655	663	1 0.0
09	672	680	689	697	706	714	723	731	740	749	2 1.8
<b>510</b>	757	766	774	783	791	800	808	817	825	834	3 2.7
11	842	851	859	868	876	885	893	902	910	919	4 3.6
12	927	935	944	952	961	969	978	986	995	*003	5 4.5
13	71 012	020	029	037	046	054	063	071	079	088	6 5.4
14	096	105	113	122	130	139	147	155	164	172	7 6.3
15	181	189	198	206	214	223	231	240	248	257	8 7.2
16	265	273	282	290	299	307	315	324	332	341	9 8.1
17	349	357	366	374	383	391	399	408	416	425	
18	433	441	450	458	466	475	483	492	500	508	
19	517	525	533	542	550	559	567	575	584	592	
<b>520</b>	600	609	617	625	634	642	650	659	667	675	
21	684	692	700	709	717	725	734	742	750	759	
22	767	775	784	792	800	809	817	825	834	842	8
23	850	858	867	875	883	892	900	908	917	925	1 0.8
24	933	941	950	958	966	975	983	991	999	*008	2 1.6
25	72 016	024	032	041	049	057	066	074	082	090	3 2.4
26	099	107	115	123	132	140	148	156	165	173	4 3.2
27	181	189	198	206	214	222	230	239	247	255	5 4.0
28	263	272	280	288	296	304	313	321	329	337	6 4.8
29	346	354	362	370	378	387	395	403	411	419	7 5.6
<b>530</b>	428	436	444	452	460	469	477	485	493	501	8 6.4
31	509	518	526	534	542	550	558	567	575	583	9 7.2
32	591	599	607	616	624	632	640	648	656	665	
33	673	681	689	697	705	713	722	730	738	746	
34	754	762	770	779	787	795	803	811	819	827	
35	835	843	852	860	868	876	884	892	900	908	
36	916	925	933	941	949	957	965	973	981	989	
37	997	*006	*014	*022	*030	*038	*046	*054	*062	*070	7
38	73 078	086	094	102	111	119	127	135	143	151	1 0.7
39	159	167	175	183	191	199	207	215	223	231	2 1.4
<b>540</b>	239	247	255	263	272	280	288	296	304	312	3 2.1
41	320	328	336	344	352	360	368	376	384	392	4 2.8
42	400	408	416	424	432	440	448	456	464	472	5 3.5
43	480	488	496	504	512	520	528	536	544	552	6 4.2
44	560	568	576	584	592	600	608	616	624	632	7 4.0
45	640	648	656	664	672	679	687	695	703	711	8 5.6
46	719	727	735	743	751	759	767	775	783	791	9 6.3
47	799	807	815	823	830	838	846	854	862	870	
48	878	886	894	902	910	918	926	933	941	949	
49	957	965	973	981	989	997	*005	*013	*020	*028	
<b>550</b>	74 036	044	052	060	068	076	084	092	099	107	
N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.

550-600

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
550	74 036	044	052	060	068	076	084	092	099	107	
51	115	123	131	139	147	155	162	170	178	186	
52	194	202	210	218	225	233	241	249	257	265	
53	273	280	288	296	304	312	320	327	335	343	
54	351	359	367	374	382	390	398	406	414	421	
55	429	437	445	453	461	468	476	484	492	500	
56	507	515	523	531	539	547	554	562	570	578	
57	586	593	601	609	617	624	632	640	648	656	
58	663	671	679	687	695	702	710	718	726	733	
59	741	749	757	764	772	780	788	796	803	811	
560	819	827	834	842	850	858	865	873	881	889	
61	896	904	912	920	927	935	943	950	958	966	
62	974	981	989	997	*005	*012	*020	*028	*035	*043	
63	75 051	059	066	074	082	089	097	105	113	120	8
64	128	136	143	151	159	166	174	182	189	197	1 0.8
65	205	213	220	228	236	243	251	259	266	274	2 1.6
66	282	289	297	305	312	320	328	335	343	351	3 2.4
67	358	366	374	381	389	397	404	412	420	427	4 3.2
68	435	442	450	458	465	473	481	488	496	504	5 4.0
69	511	519	526	534	542	549	557	565	572	580	6 4.8
570	587	595	603	610	618	626	633	641	648	656	7 5.6
71	664	671	679	686	694	702	709	717	724	732	8 6.4
72	740	747	755	762	770	778	785	793	800	808	9 7.2
73	815	823	831	838	846	853	861	868	876	884	
74	891	899	906	914	921	929	937	944	952	959	
75	967	974	982	989	997	*005	*012	*020	*027	*035	
76	76 042	050	057	065	072	080	087	095	103	110	
77	118	125	133	140	148	155	163	170	178	185	
78	193	200	208	215	223	230	238	245	253	260	
79	268	275	283	290	298	305	313	320	328	335	
580	343	350	358	365	373	380	388	395	403	410	
81	418	425	433	440	448	455	462	470	477	485	
82	492	500	507	515	522	530	537	545	552	559	
83	567	574	582	589	597	604	612	619	626	634	7
84	641	649	656	664	671	678	686	693	701	708	1 0.7
85	716	723	730	738	745	753	760	768	775	782	2 1.4
86	790	797	805	812	819	827	834	842	849	856	3 2.1
87	864	871	879	886	893	901	908	916	923	930	4 2.8
88	938	945	953	960	967	975	982	989	997	*004	5 3.5
89	77 012	019	026	034	041	048	056	063	070	078	6 4.2
590	085	093	100	107	115	122	129	137	144	151	7 4.9
91	159	166	173	181	188	195	203	210	217	225	8 5.6
92	232	240	247	254	262	269	276	283	291	298	9 6.3
93	305	313	320	327	335	342	349	357	364	371	
94	379	386	393	401	408	415	422	430	437	444	
95	452	459	466	474	481	488	495	503	510	517	
96	525	532	539	546	554	561	568	576	583	590	
97	597	605	612	619	627	634	641	648	656	663	
98	670	677	685	692	699	706	714	721	728	735	
99	743	750	757	764	772	779	786	793	801	808	
600	815	822	830	837	844	851	859	866	873	880	
N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.

600-650

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
600	77 815	822	830	837	844	851	859	866	873	880	
01	887	895	902	909	916	924	931	938	945	952	
02	960	967	974	981	988	996	*003	*010	*017	*025	
03	78 032	039	046	053	061	068	075	082	089	097	
04	104	111	118	125	132	140	147	154	161	168	
05	176	183	190	197	204	211	219	226	233	240	
06	247	254	262	269	276	283	290	297	305	312	
07	319	326	333	340	347	355	362	369	376	383	8
08	390	398	405	412	419	426	433	440	447	455	1 0.8
09	462	469	476	483	490	497	504	512	519	526	2 1.6
610	533	540	547	554	561	569	576	583	590	597	3 2.4
11	604	611	618	625	633	640	647	654	661	668	4 3.2
12	675	682	689	696	704	711	718	725	732	739	5 4.0
13	746	753	760	767	774	781	789	796	803	810	6 4.8
14	817	824	831	838	845	852	859	866	873	880	7 5.6
15	888	895	902	909	916	923	930	937	944	951	8 6.4
16	958	965	972	979	986	993	*000	*007	*014	*021	9 7.2
17	79 029	036	043	050	057	064	071	078	085	092	
18	099	106	113	120	127	134	141	148	155	162	
19	169	176	183	190	197	204	211	218	225	232	
620	239	246	253	260	267	274	281	288	295	302	
21	309	316	323	330	337	344	351	358	365	372	
22	379	386	393	400	407	414	421	428	435	442	7
23	449	456	463	470	477	484	491	498	505	511	1 0.7
24	518	525	532	539	546	553	560	567	574	581	2 1.4
25	588	595	602	609	616	623	630	637	644	650	3 2.1
26	657	664	671	678	685	692	699	706	713	720	4 2.8
27	727	734	741	748	754	761	768	775	782	789	5 3.5
28	796	803	810	817	824	831	837	844	851	858	6 4.2
29	865	872	879	886	893	900	906	913	920	927	7 4.9
630	934	941	948	955	962	969	975	982	989	996	8 5.6
31	80 003	010	017	024	030	037	044	051	058	065	
32	072	079	085	092	099	106	113	120	127	134	
33	140	147	154	161	168	175	182	188	195	202	
34	209	216	223	229	236	243	250	257	264	271	
35	277	284	291	298	305	312	318	325	332	339	
36	346	353	359	366	373	380	387	393	400	407	
37	414	421	428	434	441	448	455	462	468	475	6
38	482	489	496	502	509	516	523	530	536	543	1 0.6
39	550	557	564	570	577	584	591	598	604	611	2 1.2
640	618	625	632	638	645	652	659	665	672	679	3 1.8
41	686	693	699	706	713	720	726	733	740	747	4 2.4
42	754	760	767	774	781	787	794	801	808	814	5 3.0
43	821	828	835	841	848	855	862	868	875	882	6 3.6
44	889	895	902	909	916	922	929	936	943	949	7 4.2
45	956	963	969	976	983	990	996	*003	*010	*017	8 4.8
46	81 023	030	037	043	050	057	064	070	077	084	9 5.4
47	090	097	104	111	117	124	131	137	144	151	
48	158	164	171	178	184	191	198	204	211	218	
49	224	231	238	245	251	258	265	271	278	285	
650	291	298	305	311	318	325	331	338	345	351	
N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.

650-700

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
650	81 291	298	305	311	318	325	331	338	345	351	
51	358	365	371	378	385	391	398	405	411	418	
52	425	431	438	445	451	458	465	471	478	485	
53	491	498	505	511	518	525	531	538	544	551	
54	558	564	571	578	584	591	598	604	611	617	
55	624	631	637	644	651	657	664	671	677	684	
56	690	697	704	710	717	723	730	737	743	750	
57	757	763	770	776	783	790	796	803	809	816	
58	823	829	836	842	849	856	862	869	875	882	
59	889	895	902	908	915	921	928	935	941	948	
660	954	961	968	974	981	987	994	*000	*007	*014	
61	82 020	027	033	040	046	053	060	066	073	079	
62	086	092	099	105	112	119	125	132	138	145	
63	151	158	164	171	178	184	191	197	204	210	7
64	217	223	230	236	243	249	256	263	269	276	1 0.7
65	282	289	295	302	308	315	321	328	334	341	2 1.4
66	347	354	360	367	373	380	387	393	400	406	3 2.1
67	413	419	426	432	439	445	452	458	465	471	4 2.8
68	478	484	491	497	504	510	517	523	530	536	5 3.5
69	543	549	556	562	569	575	582	588	595	601	6 4.2
670	607	614	620	627	633	640	646	653	659	666	7 4.9
71	672	679	685	692	698	705	711	718	724	730	8 5.6
72	737	743	750	756	763	769	776	782	789	795	9 6.3
73	802	808	814	821	827	834	840	847	853	860	
74	866	872	879	885	892	898	905	911	918	924	
75	930	937	943	950	956	963	969	975	982	988	
76	995	*001	*008	*014	*020	*027	*033	*040	*046	*052	
77	83 059	065	072	078	085	091	097	104	110	117	
78	123	129	136	142	149	155	161	168	174	181	
79	187	193	200	206	213	219	225	232	238	245	
680	251	257	264	270	276	283	289	296	302	308	
81	315	321	327	334	340	347	353	359	366	372	
82	378	385	391	398	404	410	417	423	429	436	
83	442	448	455	461	467	474	480	487	493	499	6
84	506	512	518	525	531	537	544	550	556	563	1 0.6
85	569	575	582	588	594	601	607	613	620	626	2 1.2
86	632	639	645	651	658	664	670	677	683	689	3 1.8
87	696	702	708	715	721	727	734	740	746	753	4 2.4
88	759	765	771	778	784	790	797	803	809	816	5 3.0
89	822	828	835	841	847	853	860	866	872	879	6 3.6
690	885	891	897	904	910	916	923	929	935	942	7 4.2
91	948	954	960	967	973	979	985	992	998	*004	8 4.8
92	84 011	017	023	029	036	042	048	055	061	067	9 5.4
93	073	080	086	092	098	105	111	117	123	130	
94	136	142	148	155	161	167	173	180	186	192	
95	198	205	211	217	223	230	236	242	248	255	
96	261	267	273	280	286	292	298	305	311	317	
97	323	330	336	342	348	354	361	367	373	379	
98	386	392	398	404	410	417	423	429	435	442	
99	448	454	460	466	473	479	485	491	497	504	
700	510	516	522	528	535	541	547	553	559	566	
N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.

700-750

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
<b>700</b>	84 510	516	522	528	535	541	547	553	559	566	
01	572	578	584	590	597	603	609	615	621	628	
02	634	640	646	652	658	665	671	677	683	689	
03	696	702	708	714	720	726	733	739	745	751	
04	757	763	770	776	782	788	794	800	807	813	
05	819	825	831	837	844	850	856	862	868	874	
06	880	887	893	899	905	911	917	924	930	936	
07	942	948	954	960	967	973	979	985	991	997	7
08	85 003	009	016	022	028	034	040	046	052	058	1 0.7
09	065	071	077	083	089	095	101	107	114	120	2 1.4
<b>710</b>	126	132	138	144	150	156	163	169	175	181	3 2.1
11	187	193	199	205	211	217	224	230	236	242	4 2.8
12	248	254	260	266	272	278	285	291	297	303	5 3.5
13	309	315	321	327	333	339	345	352	358	364	6 4.2
14	370	376	382	388	394	400	406	412	418	425	7 4.9
15	431	437	443	449	455	461	467	473	479	485	8 5.6
16	491	497	503	509	516	522	528	534	540	546	9 6.3
17	552	558	564	570	576	582	588	594	600	606	
18	612	618	625	631	637	643	649	655	661	667	
19	673	679	685	691	697	703	709	715	721	727	
<b>720</b>	733	739	745	751	757	763	769	775	781	788	
21	794	800	806	812	818	824	830	836	842	848	
22	854	860	866	872	878	884	890	896	902	908	6
23	914	920	926	932	938	944	950	956	962	968	1 0.6
24	974	980	986	992	998	*004	*010	*016	*022	*028	2 1.2
25	86 034	040	046	052	058	064	070	076	082	088	3 1.8
26	094	100	106	112	118	124	130	136	141	147	4 2.4
27	153	159	165	171	177	183	189	195	201	207	5 3.0
28	213	219	225	231	237	243	249	255	261	267	6 3.6
29	273	279	285	291	297	303	308	314	320	326	7 4.2
<b>730</b>	332	338	344	350	356	362	368	374	380	386	8 4.8
31	392	398	404	410	415	421	427	433	439	445	
32	451	457	463	469	475	481	487	493	499	504	
33	510	516	522	528	534	540	546	552	558	564	
34	570	576	581	587	593	599	605	611	617	623	
35	629	635	641	646	652	658	664	670	676	682	
36	688	694	700	705	711	717	723	729	735	741	
37	747	753	759	764	770	776	782	788	794	800	5
38	806	812	817	823	829	835	841	847	853	859	1 0.5
39	864	870	876	882	888	894	900	906	911	917	2 1.0
<b>740</b>	923	929	935	941	947	953	958	964	970	976	3 1.5
41	982	988	994	999	*005	*011	*017	*023	*029	*035	4 2.0
42	87 040	046	052	058	064	070	075	081	087	093	5 2.5
43	099	105	111	116	122	128	134	140	146	151	6 3.0
44	157	163	169	175	181	186	192	198	204	210	7 3.5
45	216	221	227	233	239	245	251	256	262	268	8 4.0
46	274	280	286	291	297	303	309	315	320	326	9 4.5
47	332	338	344	349	355	361	367	373	379	384	
48	390	396	402	408	413	419	425	431	437	442	
49	448	454	460	466	471	477	483	489	495	500	
<b>750</b>	506	512	518	523	529	535	541	547	552	558	
N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.

750-800

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
<b>750</b>	87 506	512	518	523	529	535	541	547	552	558	
51	564	570	576	581	587	593	599	604	610	616	
52	622	628	633	639	645	651	656	662	668	674	
53	679	685	691	697	703	708	714	720	726	731	
54	737	743	749	754	760	766	772	777	783	789	
55	795	800	806	812	818	823	829	835	841	846	
56	852	858	864	869	875	881	887	892	898	904	
57	910	915	921	927	933	938	944	950	955	961	
58	967	973	978	984	990	996	*001	*007	*013	*018	
59	88 024	030	036	041	047	053	058	064	070	076	
<b>760</b>	081	087	093	098	104	110	116	121	127	133	
61	138	144	150	156	161	167	173	178	184	190	
62	195	201	207	213	218	224	230	235	241	247	
63	252	258	264	270	275	281	287	292	298	304	6
64	309	315	321	326	332	338	343	349	355	360	1 0.6
65	366	372	377	383	389	395	400	406	412	417	2 1.2
66	423	429	434	440	446	451	457	463	468	474	3 1.8
67	480	485	491	497	502	508	513	519	525	530	4 2.4
68	536	542	547	553	559	564	570	576	581	587	5 3.0
69	593	598	604	610	615	621	627	632	638	643	6 3.6
<b>770</b>	649	655	660	666	672	677	683	689	694	700	7 4.2
71	705	711	717	722	728	734	739	745	750	756	8 4.8
72	762	767	773	779	784	790	795	801	807	812	9 5.4
73	818	824	829	835	840	846	852	857	863	868	
74	874	880	885	891	897	902	908	913	919	925	
75	930	936	941	947	953	958	964	969	975	981	
76	986	992	997	*003	*009	*014	*020	*025	*031	*037	
77	89 042	048	053	059	064	070	076	081	087	092	
78	098	104	109	115	120	126	131	137	143	148	
79	154	159	165	170	176	182	187	193	198	204	
<b>780</b>	209	215	221	226	232	237	243	248	254	260	
81	265	271	276	282	287	293	298	304	310	315	
82	321	326	332	337	343	348	354	360	365	371	5
83	376	382	387	393	398	404	409	415	421	426	1 0.5
84	432	437	443	448	454	459	465	470	476	481	2 1.0
85	487	492	498	504	509	515	520	526	531	537	3 1.5
86	542	548	553	559	564	570	575	581	586	592	4 2.0
87	597	603	609	614	620	625	631	636	642	647	5 2.5
88	653	658	664	669	675	680	686	691	697	702	6 3.0
89	708	713	719	724	730	735	741	746	752	757	7 3.5
<b>790</b>	763	768	774	779	785	790	796	801	807	812	8 4.0
91	818	823	829	834	840	845	851	856	862	867	9 4.5
92	873	878	883	889	894	900	905	911	916	922	
93	927	933	938	944	949	955	960	966	971	977	
94	982	988	993	998	*004	*009	*015	*020	*026	*031	
95	90 037	042	048	053	059	064	069	075	080	086	
96	091	097	102	108	113	119	124	129	135	140	
97	146	151	157	162	168	173	179	184	189	195	
98	200	206	211	217	222	227	233	238	244	249	
99	255	260	266	271	276	282	287	293	298	304	
<b>800</b>	309	314	320	325	331	336	342	347	352	358	
N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.

800-850

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
800	90 309	314	320	325	331	336	342	347	352	358	
01	363	369	374	380	385	390	396	401	407	412	
02	417	423	428	434	439	445	450	455	461	466	
03	472	477	482	488	493	499	504	509	515	520	
04	526	531	536	542	547	553	558	563	569	574	
05	580	585	590	596	601	607	612	617	623	628	
06	634	639	644	650	655	660	666	671	677	682	
07	687	693	698	703	709	714	720	725	730	736	
08	741	747	752	757	763	768	773	779	784	789	
09	795	800	806	811	816	822	827	832	838	843	
810	849	854	859	865	870	875	881	886	891	897	
11	902	907	913	918	924	929	934	940	945	950	
12	956	961	966	972	977	982	988	993	998	*004	
13	91 009	014	020	025	030	036	041	046	052	057	6
14	062	068	073	078	084	089	094	100	105	110	1
15	116	121	126	132	137	142	148	153	158	164	2
16	169	174	180	185	190	196	201	206	212	217	3
17	222	228	233	238	243	249	254	259	265	270	4
18	275	281	286	291	297	302	307	312	318	323	5
19	328	334	339	344	350	355	360	365	371	376	6
820	381	387	392	397	403	408	413	418	424	429	7
21	434	440	445	450	455	461	466	471	477	482	8
22	487	492	498	503	508	514	519	524	529	535	9
23	540	545	551	556	561	566	572	577	582	587	
24	593	598	603	609	614	619	624	630	635	640	
25	645	651	656	661	666	672	677	682	687	693	
26	698	703	709	714	719	724	730	735	740	745	
27	751	756	761	766	772	777	782	787	793	798	
28	803	808	814	819	824	829	834	840	845	850	
29	855	861	866	871	876	882	887	892	897	903	
830	908	913	918	924	929	934	939	944	950	955	
31	960	965	971	976	981	986	991	997	*002	*007	
32	92 012	018	023	028	033	038	044	049	054	059	5
33	065	070	075	080	085	091	096	101	106	111	1
34	117	122	127	132	137	143	148	153	158	163	2
35	169	174	179	184	189	195	200	205	210	215	3
36	221	226	231	236	241	247	252	257	262	267	4
37	273	278	283	288	293	298	304	309	314	319	5
38	324	330	335	340	345	350	355	361	366	371	6
39	376	381	387	392	397	402	407	412	418	423	7
840	428	433	438	443	449	454	459	464	469	474	8
41	480	485	490	495	500	505	511	516	521	526	9
42	531	536	542	547	552	557	562	567	572	578	
43	583	588	593	598	603	609	614	619	624	629	
44	634	639	645	650	655	660	665	670	675	681	
45	686	691	696	701	706	711	716	722	727	732	
46	737	742	747	752	758	763	768	773	778	783	
47	788	793	799	804	809	814	819	824	829	834	
48	840	845	850	855	860	865	870	875	881	886	
49	891	896	901	906	911	916	921	927	932	937	
850	942	947	952	957	962	967	973	978	983	988	



850-900

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
850	92 942	947	952	957	962	967	973	978	983	988	
51	993	998	*003	*008	*013	*018	*024	*029	*034	*039	
52	93 044	049	054	059	064	069	075	080	085	090	
53	095	100	105	110	115	120	125	131	136	141	
54	146	151	156	161	166	171	176	181	186	192	
55	197	202	207	212	217	222	227	232	237	242	
56	247	252	258	263	268	273	278	283	288	293	
57	298	303	308	313	318	323	328	334	339	344	6
58	349	354	359	364	369	374	379	384	389	394	1 0.6
59	399	404	409	414	420	425	430	435	440	445	2 1.2
860	450	455	460	465	470	475	480	485	490	495	3 1.8
61	500	505	510	515	520	526	531	536	541	546	4 2.4
62	551	556	561	566	571	576	581	586	591	596	5 3.0
63	601	606	611	616	621	626	631	636	641	646	6 3.6
64	651	656	661	666	671	676	682	687	692	697	7 4.2
65	702	707	712	717	722	727	732	737	742	747	8 4.8
66	752	757	762	767	772	777	782	787	792	797	9 5.4
67	802	807	812	817	822	827	832	837	842	847	
68	852	857	862	867	872	877	882	887	892	897	
69	902	907	912	917	922	927	932	937	942	947	
870	952	957	962	967	972	977	982	987	992	997	
71	94 002	007	012	017	022	027	032	037	042	047	5
72	052	057	062	067	072	077	082	086	091	096	1 0.5
73	101	106	111	116	121	126	131	136	141	146	2 1.0
74	151	156	161	166	171	176	181	186	191	196	3 1.5
75	201	206	211	216	221	226	231	236	240	245	4 2.0
76	250	255	260	265	270	275	280	285	290	295	5 2.5
77	300	305	310	315	320	325	330	335	340	345	6 3.0
78	349	354	359	364	369	374	379	384	389	394	7 3.5
79	399	404	409	414	419	424	429	433	438	443	8 4.0
880	448	453	458	463	468	473	478	483	488	493	9 4.5
81	498	503	507	512	517	522	527	532	537	542	
82	547	552	557	562	567	571	576	581	586	591	
83	596	601	606	611	616	621	626	630	635	640	
84	645	650	655	660	665	670	675	680	685	689	
85	694	699	704	709	714	719	724	729	734	738	
86	743	748	753	758	763	768	773	778	783	787	
87	792	797	802	807	812	817	822	827	832	836	4
88	841	846	851	856	861	866	871	876	880	885	1 0.4
89	890	895	900	905	910	915	919	924	929	934	2 0.8
890	939	944	949	954	959	963	968	973	978	983	3 1.2
91	988	993	998	*002	*007	*012	*017	*022	*027	*032	4 1.6
92	95 036	041	046	051	056	061	066	071	075	080	5 2.0
93	085	090	095	100	105	109	114	119	124	129	6 2.4
94	134	139	143	148	153	158	163	168	173	177	7 2.8
95	182	187	192	197	202	207	211	216	221	226	8 3.2
96	231	236	240	245	250	255	260	265	270	274	9 3.6
97	279	284	289	294	299	303	308	313	318	323	
98	328	332	337	342	347	352	357	361	366	371	
99	376	381	386	390	395	400	405	410	415	419	
900	424	429	434	439	444	448	453	458	463	468	
N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.

900-950

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
900	95 424	429	434	439	444	448	453	458	463	468	
01	472	477	482	487	492	497	501	506	511	516	
02	521	525	530	535	540	545	550	554	559	564	
03	569	574	578	583	588	593	598	602	607	612	
04	617	622	626	631	636	641	646	650	655	660	
05	665	670	674	679	684	689	694	698	703	708	
06	713	718	722	727	732	737	742	746	751	756	
07	761	766	770	775	780	785	789	794	799	804	
08	809	813	818	823	828	832	837	842	847	852	
09	856	861	866	871	875	880	885	890	895	899	
910	904	909	914	918	923	928	933	938	942	947	
11	952	957	961	966	971	976	980	985	990	995	
12	999	*004	*009	*014	*019	*023	*028	*033	*038	*042	
13	96 047	052	057	061	066	071	076	080	085	090	5
14	095	099	104	109	114	118	123	128	133	137	1 0.5
15	142	147	152	156	161	166	171	175	180	185	2 1.0
16	190	194	199	204	209	213	218	223	227	232	3 1.5
17	237	242	246	251	256	261	265	270	275	280	4 2.0
18	284	289	294	298	303	308	313	317	322	327	5 2.5
19	332	336	341	346	350	355	360	365	369	374	6 3.0
920	379	384	388	393	398	402	407	412	417	421	7 3.5
21	426	431	435	440	445	450	454	459	464	468	8 4.0
22	473	478	483	487	492	497	501	506	511	515	9 4.5
23	520	525	530	534	539	544	548	553	558	562	
24	567	572	577	581	586	591	595	600	605	609	
25	614	619	624	628	633	638	642	647	652	656	
26	661	666	670	675	680	685	689	694	699	703	
27	708	713	717	722	727	731	736	741	745	750	
28	755	759	764	769	774	778	783	788	792	797	
29	802	806	811	816	820	825	830	834	839	844	
930	848	853	858	862	867	872	876	881	886	890	
31	895	900	904	909	914	918	923	928	932	937	
32	942	946	951	956	960	965	970	974	979	984	4
33	988	993	997	*002	*007	*011	*016	*021	*025	*030	1 0.4
34	97 035	039	044	049	053	058	063	067	072	077	2 0.8
35	081	086	090	095	100	104	109	114	118	123	3 1.2
36	128	132	137	142	146	151	155	160	165	169	4 1.6
37	174	179	183	188	192	197	202	206	211	216	5 2.0
38	220	225	230	234	239	243	248	253	257	262	6 2.4
39	267	271	276	280	285	290	294	299	304	308	7 2.8
940	313	317	322	327	331	336	340	345	350	354	8 3.2
41	359	364	368	373	377	382	387	391	396	400	9 3.6
42	405	410	414	419	424	428	433	437	442	447	
43	451	456	460	465	470	474	479	483	488	493	
44	497	502	506	511	516	520	525	529	534	539	
45	543	548	552	557	562	566	571	575	580	585	
46	589	594	598	603	607	612	617	621	626	630	
47	635	640	644	649	653	658	663	667	672	676	
48	681	685	690	695	699	704	708	713	717	722	
49	727	731	736	740	745	749	754	759	763	768	
950	772	777	782	786	791	795	800	804	809	813	
N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.

950-1000

N.	L. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
950	97 772	777	782	786	791	795	800	804	809	813	
51	818	823	827	832	836	841	845	850	855	859	
52	864	868	873	877	882	886	891	896	900	905	
53	909	914	918	923	928	932	937	941	946	950	
54	955	959	964	968	973	978	982	987	991	996	
55	98 000	005	009	014	019	023	028	032	037	041	
56	046	050	055	059	064	068	073	078	082	087	
57	091	096	100	105	109	114	118	123	127	132	
58	137	141	146	150	155	159	164	168	173	177	
59	182	186	191	195	200	204	209	214	218	223	
960	227	232	236	241	245	250	254	259	263	268	
61	272	277	281	286	290	295	299	304	308	313	
62	318	322	327	331	336	340	345	349	354	358	
63	363	367	372	376	381	385	390	394	399	403	
64	408	412	417	421	426	430	435	439	444	448	
65	453	457	462	466	471	475	480	484	489	493	
66	498	502	507	511	516	520	525	529	534	538	
67	543	547	552	556	561	565	570	574	579	583	
68	588	592	597	601	605	610	614	619	623	628	
69	632	637	641	646	650	655	659	664	668	673	
970	677	682	686	691	695	700	704	709	713	717	
71	722	726	731	735	740	744	749	753	758	762	
72	767	771	776	780	784	789	793	798	802	807	
73	811	816	820	825	829	834	838	843	847	851	
74	856	860	865	869	874	878	883	887	892	896	
75	900	905	909	914	918	923	927	932	936	941	
76	945	949	954	958	963	967	972	976	981	985	
77	989	994	998	*003	*007	*012	*016	*021	*025	*029	
78	99 034	038	043	047	052	056	061	065	069	074	
79	078	083	087	092	096	100	105	109	114	118	
980	123	127	131	136	140	145	149	154	158	162	
81	167	171	176	180	185	189	193	198	202	207	
82	211	216	220	224	229	233	238	242	247	251	
83	255	260	264	269	273	277	282	286	291	295	
84	300	304	308	313	317	322	326	330	335	339	
85	344	348	352	357	361	366	370	374	379	383	
86	388	392	396	401	405	410	414	419	423	427	
87	432	436	441	445	449	454	458	463	467	471	
88	476	480	484	489	493	498	502	506	511	515	
89	520	524	528	533	537	542	546	550	555	559	
990	564	568	572	577	581	585	590	594	599	603	
91	607	612	616	621	625	629	634	638	642	647	
92	651	656	660	664	669	673	677	682	686	691	
93	695	699	704	708	712	717	721	726	730	734	
94	739	743	747	752	756	760	765	769	774	778	
95	782	787	791	795	800	804	808	813	817	822	
96	826	830	835	839	843	848	852	856	861	865	
97	870	874	878	883	887	891	896	900	904	909	
98	913	917	922	926	930	935	939	944	948	952	
99	957	961	965	970	974	978	983	987	991	996	
1000	00 000	004	009	013	017	022	026	030	035	039	

5  
1 0.5  
2 1.0  
3 1.5  
4 2.0  
5 2.5  
6 3.0  
7 3.5  
8 4.0  
9 4.5

4  
1 0.4  
2 0.8  
3 1.2  
4 1.6  
5 2.0  
6 2.4  
7 2.8  
8 3.2  
9 3.6



**TABLE II**



**FIVE-PLACE LOGARITHMS**

**OF THE**

**TRIGONOMETRIC FUNCTIONS**

TABLE II contains the common logarithms of the trigonometric functions for angles from  $0^\circ$  to  $90^\circ$  as follows:

(1)  $\log \sin \alpha = \log \tan \alpha$ , for every second  $0^\circ$  to  $3'$ , and  $\log \cos \beta = \log \cot \beta$ , for every second,  $89^\circ 57'$  to  $90^\circ$ , page 22.

(2) logarithms of sine, tangent, and cosine for every  $10''$  from  $0^\circ$  to  $2^\circ$ ; also the logarithms of sine, cosine, and cotangent for every  $10''$  from  $88^\circ$  to  $90^\circ$ , pages 23–28.

(3) logarithms of each function for every  $1'$  from  $0^\circ$  to  $90^\circ$ , pages 29–73.

log sin = log tan				$0^\circ$					
"	0'	1'	2'	"	"	0'	1'	2'	"
0	$-\infty$	6.46 373	6.76 476	60	30	6.16 270	6.63 982	6.86 167	30
1	4.68 557	6.47 090	6.76 836	59	31	6.17 694	6.64 462	6.86 455	29
2	4.98 660	6.47 797	6.77 193	58	32	6.19 072	6.64 936	6.86 742	28
3	5.16 270	6.48 492	6.77 548	57	33	6.20 409	6.65 406	6.87 027	27
4	5.28 763	6.49 175	6.77 900	56	34	6.21 705	6.65 870	6.87 310	26
5	5.38 454	6.49 849	6.78 248	55	35	6.22 964	6.66 330	6.87 591	25
6	5.46 373	6.50 512	6.78 595	54	36	6.24 188	6.66 785	6.87 870	24
7	5.53 067	6.51 165	6.78 938	53	37	6.25 378	6.67 235	6.88 147	23
8	5.58 866	6.51 808	6.79 278	52	38	6.26 536	6.67 680	6.88 423	22
9	5.63 982	6.52 442	6.79 616	51	39	6.27 664	6.68 121	6.88 697	21
10	5.68 557	6.53 067	6.79 952	50	40	6.28 763	6.68 557	6.88 969	20
11	5.72 697	6.53 683	6.80 285	49	41	6.29 836	6.68 990	6.89 240	19
12	5.76 476	6.54 291	6.80 615	48	42	6.30 882	6.69 418	6.89 509	18
13	5.79 952	6.54 890	6.80 943	47	43	6.31 904	6.69 841	6.89 776	17
14	5.83 170	6.55 481	6.81 268	46	44	6.32 903	6.70 261	6.90 042	16
15	5.86 167	6.56 064	6.81 591	45	45	6.33 879	6.70 676	6.90 306	15
16	5.88 969	6.56 639	6.81 911	44	46	6.34 833	6.71 088	6.90 568	14
17	5.91 602	6.57 207	6.82 230	43	47	6.35 767	6.71 496	6.90 829	13
18	5.94 085	6.57 767	6.82 545	42	48	6.36 682	6.71 900	6.91 088	12
19	5.96 433	6.58 320	6.82 859	41	49	6.37 577	6.72 300	6.91 346	11
20	5.98 660	6.58 866	6.83 170	40	50	6.38 454	6.72 697	6.91 602	10
21	6.00 779	6.59 406	6.83 479	39	51	6.39 315	6.73 090	6.91 857	9
22	6.02 800	6.59 939	6.83 786	38	52	6.40 158	6.73 479	6.92 110	8
23	6.04 730	6.60 465	6.84 091	37	53	6.40 985	6.73 865	6.92 362	7
24	6.06 579	6.60 985	6.84 394	36	54	6.41 797	6.74 248	6.92 612	6
25	6.08 351	6.61 499	6.84 694	35	55	6.42 594	6.74 627	6.92 861	5
26	6.10 055	6.62 007	6.84 993	34	56	6.43 376	6.75 003	6.93 109	4
27	6.11 694	6.62 509	6.85 289	33	57	6.44 145	6.75 376	6.93 355	3
28	6.13 273	6.63 006	6.85 584	32	58	6.44 900	6.75 746	6.93 599	2
29	6.14 797	6.63 496	6.85 876	31	59	6.45 643	6.76 112	6.93 843	1
30	6.16 270	6.63 982	6.86 167	30	60	6.46 373	6.76 476	6.94 085	0
"	59'	58'	57'	"	"	59'	58'	57'	"
				$89^\circ$ log cos = log cot					

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

0°

' "	log sin	log tan	log cos	' "	' "	log sin	log tan	log cos	' "
0 0	— ∞	— ∞	10.00000	0 60	10 0	7.46 373	7.46 373	10.00000	0 50
10	5.68 557	5.68 557	10.00000	50	10	7.47 090	7.47 091	10.00000	50
20	5.98 660	5.98 660	10.00000	40	20	7.47 797	7.47 797	10.00000	40
30	6.16 270	6.16 270	10.00000	30	30	7.48 491	7.48 492	10.00000	30
40	6.28 763	6.28 763	10.00000	20	40	7.49 175	7.49 176	10.00000	20
50	6.38 454	6 38 454	10.00000	10	50	7.49 849	7.49 849	10.00000	10
1 0	6.46 373	6.46 373	10.00000	0 59	11 0	7.50 512	7.50 512	10.00000	0 49
10	6.53 067	6.53 067	10.00000	50	10	7.51 165	7.51 165	10.00000	50
20	6.58 866	6.58 866	10.00000	40	20	7.51 808	7.51 809	10.00000	40
30	6.63 982	6.63 982	10.00000	30	30	7.52 442	7.52 443	10.00000	30
40	6.68 557	6.68 557	10.00000	20	40	7.53 067	7.53 067	10.00000	20
50	6.72 697	6.72 697	10.00000	10	50	7.53 683	7.53 683	10.00000	10
2 0	6.76 476	6.76 476	10.00000	0 58	12 0	7.54 291	7.54 291	10.00000	0 48
10	6.79 952	6.79 952	10.00000	50	10	7.54 890	7.54 890	10.00000	50
20	6.83 170	6.83 170	10.00000	40	20	7.55 481	7.55 481	10.00000	40
30	6.86 167	6.86 167	10.00000	30	30	7.56 064	7.56 064	10.00000	30
40	6.88 969	6.88 969	10.00000	20	40	7.56 639	7.56 639	10.00000	20
50	6.91 602	6.91 602	10.00000	10	50	7.57 206	7.57 207	10.00000	10
3 0	6.94 085	6.94 085	10.00000	0 57	13 0	7.57 767	7.57 767	10.00000	0 47
10	6.96 433	6.96 433	10.00000	50	10	7.58 320	7.58 320	10.00000	50
20	6.98 660	6.98 661	10.00000	40	20	7.58 866	7.58 867	10.00000	40
30	7.00 779	7.00 779	10.00000	30	30	7.59 406	7.59 406	10.00000	30
40	7.02 800	7.02 800	10.00000	20	40	7.59 939	7.59 939	10.00000	20
50	7.04 730	7.04 730	10.00000	10	50	7.60 465	7.60 466	10.00000	10
4 0	7.06 579	7.06 579	10.00000	0 56	14 0	7.60 985	7.60 986	10.00000	0 46
10	7.08 351	7.08 352	10.00000	50	10	7.61 499	7.61 500	10.00000	50
20	7.10 055	7.10 055	10.00000	40	20	7.62 007	7.62 008	10.00000	40
30	7.11 694	7.11 694	10.00000	30	30	7.62 509	7.62 510	10.00000	30
40	7.13 273	7.13 273	10.00000	20	40	7.63 006	7.63 006	10.00000	20
50	7.14 797	7.14 797	10.00000	10	50	7.63 496	7.63 497	10.00000	10
5 0	7.16 270	7.16 270	10.00000	0 55	15 0	7.63 982	7.63 982	10.00000	0 45
10	7.17 694	7.17 694	10.00000	50	10	7.64 461	7.64 462	10.00000	50
20	7.19 072	7.19 073	10.00000	40	20	7.64 936	7.64 937	10.00000	40
30	7.20 409	7.20 409	10.00000	30	30	7.65 406	7.65 406	10.00000	30
40	7.21 705	7.21 705	10.00000	20	40	7.65 870	7.65 871	10.00000	20
50	7.22 964	7.22 964	10.00000	10	50	7.66 330	7.66 330	10.00000	10
6 0	7.24 188	7.24 188	10.00000	0 54	16 0	7.66 784	7.66 785	10.00000	0 44
10	7.25 378	7.25 378	10.00000	50	10	7.67 235	7.67 235	10.00000	50
20	7.26 536	7.26 536	10.00000	40	20	7.67 680	7.67 680	10.00000	40
30	7.27 664	7.27 664	10.00000	30	30	7.68 121	7.68 121	10.00000	30
40	7.28 763	7.28 764	10.00000	20	40	7.68 557	7.68 558	9.99999	20
50	7.29 836	7.29 836	10.00000	10	50	7.68 989	7.68 990	9.99999	10
7 0	7.30 882	7.30 882	10.00000	0 53	17 0	7.69 417	7.69 418	9.99999	0 43
10	7.31 904	7.31 904	10.00000	50	10	7.69 841	7.69 842	9.99999	50
20	7.32 903	7.32 903	10.00000	40	20	7.70 261	7.70 261	9.99999	40
30	7.33 879	7.33 879	10.00000	30	30	7.70 676	7.70 677	9.99999	30
40	7.34 833	7.34 833	10.00000	20	40	7.71 088	7.71 088	9.99999	20
50	7.35 767	7.35 767	10.00000	10	50	7.71 496	7.71 496	9.99999	10
8 0	7.36 682	7.36 682	10.00000	0 52	18 0	7.71 900	7.71 900	9.99999	0 42
10	7.37 577	7.37 577	10.00000	50	10	7.72 300	7.72 301	9.99999	50
20	7.38 454	7.38 455	10.00000	40	20	7.72 697	7.72 697	9.99999	40
30	7.39 314	7.39 315	10.00000	30	30	7.73 090	7.73 090	9.99999	30
40	7.40 158	7.40 158	10.00000	20	40	7.73 479	7.73 480	9.99999	20
50	7.40 985	7.40 985	10.00000	10	50	7.73 865	7.73 866	9.99999	10
9 0	7.41 797	7.41 797	10.00000	0 51	19 0	7.74 248	7.74 248	9.99999	0 41
10	7.42 594	7.42 594	10.00000	50	10	7.74 627	7.74 628	9.99999	50
20	7.43 376	7.43 376	10.00000	40	20	7.75 003	7.75 004	9.99999	40
30	7.44 145	7.44 145	10.00000	30	30	7.75 376	7.75 377	9.99999	30
40	7.44 900	7.44 900	10.00000	20	40	7.75 745	7.75 746	9.99999	20
50	7.45 643	7.45 643	10.00000	10	50	7.76 112	7.76 113	9.99999	10
10 0	7.46 373	7.46 373	10.00000	0 50	20 0	7.76 475	7.76 476	9.99999	0 40

' "	log cos	log cot	log sin	' "	' "	log cos	log cot	log sin	' "
-----	---------	---------	---------	-----	-----	---------	---------	---------	-----

89°

0°

' "	log sin	log tan	log cos	' "	' "	log sin	log tan	log cos	' "
20 0	7.76 475	7.76 476	9.99 999	0 40	30 0	7.94 084	7.94 086	9.99 998	0 30
10	7.76 836	7.76 837	9.99 999	50	10	7.94 325	7.94 326	9.99 998	50
20	7.77 193	7.77 194	9.99 999	40	20	7.94 564	7.94 566	9.99 998	40
30	7.77 548	7.77 549	9.99 999	30	30	7.94 802	7.94 804	9.99 998	30
40	7.77 899	7.77 900	9.99 999	20	40	7.95 039	7.95 040	9.99 998	20
50	7.78 248	7.78 249	9.99 999	10	50	7.95 274	7.95 276	9.99 998	10
21 0	7.78 594	7.78 595	9.99 999	0 39	31 0	7.95 508	7.95 510	9.99 998	0 29
10	7.78 938	7.78 938	9.99 999	50	10	7.95 741	7.95 743	9.99 998	50
20	7.79 278	7.79 279	9.99 999	40	20	7.95 973	7.95 974	9.99 998	40
30	7.79 616	7.79 617	9.99 999	30	30	7.96 203	7.96 205	9.99 998	30
40	7.79 952	7.79 952	9.99 999	20	40	7.96 432	7.96 434	9.99 998	20
50	7.80 284	7.80 285	9.99 999	10	50	7.96 660	7.96 662	9.99 998	10
22 0	7.80 615	7.80 615	9.99 999	0 38	32 0	7.96 887	7.96 889	9.99 998	0 28
10	7.80 942	7.80 943	9.99 999	50	10	7.97 113	7.97 114	9.99 998	50
20	7.81 268	7.81 269	9.99 999	40	20	7.97 337	7.97 339	9.99 998	40
30	7.81 591	7.81 591	9.99 999	30	30	7.97 560	7.97 562	9.99 998	30
40	7.81 911	7.81 912	9.99 999	20	40	7.97 782	7.97 784	9.99 998	20
50	7.82 229	7.82 230	9.99 999	10	50	7.98 003	7.98 005	9.99 998	10
23 0	7.82 545	7.82 546	9.99 999	0 37	33 0	7.98 223	7.98 225	9.99 998	0 27
10	7.82 859	7.82 860	9.99 999	50	10	7.98 442	7.98 444	9.99 998	50
20	7.83 170	7.83 171	9.99 999	40	20	7.98 660	7.98 662	9.99 998	40
30	7.83 479	7.83 480	9.99 999	30	30	7.98 876	7.98 878	9.99 998	30
40	7.83 786	7.83 787	9.99 999	20	40	7.99 092	7.99 094	9.99 998	20
50	7.84 091	7.84 092	9.99 999	10	50	7.99 306	7.99 308	9.99 998	10
24 0	7.84 393	7.84 394	9.99 999	0 36	34 0	7.99 520	7.99 522	9.99 998	0 26
10	7.84 694	7.84 695	9.99 999	50	10	7.99 732	7.99 734	9.99 998	50
20	7.84 992	7.84 993	9.99 999	40	20	7.99 943	7.99 946	9.99 998	40
30	7.85 289	7.85 290	9.99 999	30	30	8.00 154	8.00 156	9.99 998	30
40	7.85 583	7.85 584	9.99 999	20	40	8.00 363	8.00 365	9.99 998	20
50	7.85 876	7.85 877	9.99 999	10	50	8.00 571	8.00 574	9.99 998	10
25 0	7.86 166	7.86 167	9.99 999	0 35	35 0	8.00 779	8.00 781	9.99 998	0 25
10	7.86 455	7.86 456	9.99 999	50	10	8.00 985	8.00 987	9.99 998	50
20	7.86 741	7.86 743	9.99 999	40	20	8.01 190	8.01 193	9.99 998	40
30	7.87 026	7.87 027	9.99 999	30	30	8.01 395	8.01 397	9.99 998	30
40	7.87 309	7.87 310	9.99 999	20	40	8.01 598	8.01 600	9.99 998	20
50	7.87 590	7.87 591	9.99 999	10	50	8.01 801	8.01 803	9.99 998	10
26 0	7.87 870	7.87 871	9.99 999	0 34	36 0	8.02 002	8.02 004	9.99 998	0 24
10	7.88 147	7.88 148	9.99 999	50	10	8.02 203	8.02 205	9.99 998	50
20	7.88 423	7.88 424	9.99 999	40	20	8.02 402	8.02 405	9.99 998	40
30	7.88 697	7.88 698	9.99 999	30	30	8.02 601	8.02 604	9.99 998	30
40	7.88 969	7.88 970	9.99 999	20	40	8.02 799	8.02 801	9.99 998	20
50	7.89 240	7.89 241	9.99 999	10	50	8.02 996	8.02 998	9.99 998	10
27 0	7.89 509	7.89 510	9.99 999	0 33	37 0	8.03 192	8.03 194	9.99 997	0 23
10	7.89 776	7.89 777	9.99 999	50	10	8.03 387	8.03 390	9.99 997	50
20	7.90 041	7.90 043	9.99 999	40	20	8.03 581	8.03 584	9.99 997	40
30	7.90 305	7.90 307	9.99 999	30	30	8.03 775	8.03 777	9.99 997	30
40	7.90 568	7.90 569	9.99 999	20	40	8.03 967	8.03 970	9.99 997	20
50	7.90 829	7.90 830	9.99 999	10	50	8.04 159	8.04 162	9.99 997	10
28 0	7.91 088	7.91 089	9.99 999	0 32	38 0	8.04 350	8.04 353	9.99 997	0 22
10	7.91 346	7.91 347	9.99 999	50	10	8.04 540	8.04 543	9.99 997	50
20	7.91 602	7.91 603	9.99 999	40	20	8.04 729	8.04 732	9.99 997	40
30	7.91 857	7.91 858	9.99 999	30	30	8.04 918	8.04 921	9.99 997	30
40	7.92 110	7.92 111	9.99 998	20	40	8.05 105	8.05 108	9.99 997	20
50	7.92 362	7.92 363	9.99 998	10	50	8.05 292	8.05 295	9.99 997	10
29 0	7.92 612	7.92 613	9.99 998	0 31	39 0	8.05 478	8.05 481	9.99 997	0 21
10	7.92 861	7.92 862	9.99 998	50	10	8.05 663	8.05 666	9.99 997	50
20	7.93 108	7.93 110	9.99 998	40	20	8.05 848	8.05 851	9.99 997	40
30	7.93 354	7.93 356	9.99 998	30	30	8.06 031	8.06 034	9.99 997	30
40	7.93 599	7.93 601	9.99 998	20	40	8.06 214	8.06 217	9.99 997	20
50	7.93 842	7.93 844	9.99 998	10	50	8.06 396	8.06 399	9.99 997	10
30 0	7.94 084	7.94 086	9.99 998	0 30	40 0	8.06 578	8.06 581	9.99 997	0 20
' "	log cos	log cot	log sin	' "	' "	log cos	log cot	log sin	' "

89°



0°

' "	log sin	log tan	log cos	' "	' "	log sin	log tan	log cos	' "
40 0	8.06 578	8.06 581	9.99 997	0 20	50 0	8.16 268	8.16 273	9.99 995	0 10
10	8.06 758	8.06 761	9.99 997	50	10	8.16 413	8.16 417	9.99 995	50
20	8.06 938	8.06 941	9.99 997	40	20	8.16 557	8.16 561	9.99 995	40
30	8.07 117	8.07 120	9.99 997	30	30	8.16 700	8.16 705	9.99 995	30
40	8.07 295	8.07 299	9.99 997	20	40	8.16 843	8.16 848	9.99 995	20
50	8.07 473	8.07 476	9.99 997	10	50	8.16 986	8.16 991	9.99 995	10
41 0	8.07 650	8.07 653	9.99 997	0 19	51 0	8.17 128	8.17 133	9.99 995	0 9
10	8.07 826	8.07 829	9.99 997	50	10	8.17 270	8.17 275	9.99 995	50
20	8.08 002	8.08 005	9.99 997	40	20	8.17 411	8.17 416	9.99 995	40
30	8.08 176	8.08 180	9.99 997	30	30	8.17 552	8.17 557	9.99 995	30
40	8.08 350	8.08 354	9.99 997	20	40	8.17 692	8.17 697	9.99 995	20
50	8.08 524	8.08 527	9.99 997	10	50	8.17 832	8.17 837	9.99 995	10
42 0	8.08 696	8.08 700	9.99 997	0 18	52 0	8.17 971	8.17 976	9.99 995	0 8
10	8.08 868	8.08 872	9.99 997	50	10	8.18 110	8.18 115	9.99 995	50
20	8.09 040	8.09 043	9.99 997	40	20	8.18 249	8.18 254	9.99 995	40
30	8.09 210	8.09 214	9.99 997	30	30	8.18 387	8.18 392	9.99 995	30
40	8.09 380	8.09 384	9.99 997	20	40	8.18 524	8.18 530	9.99 995	20
50	8.09 550	8.09 553	9.99 997	10	50	8.18 662	8.18 667	9.99 995	10
43 0	8.09 718	8.09 722	9.99 997	0 17	53 0	8.18 798	8.18 804	9.99 995	0 7
10	8.09 886	8.09 890	9.99 997	50	10	8.18 935	8.18 940	9.99 995	50
20	8.10 054	8.10 057	9.99 997	40	20	8.19 071	8.19 076	9.99 995	40
30	8.10 220	8.10 224	9.99 997	30	30	8.19 206	8.19 212	9.99 995	30
40	8.10 386	8.10 390	9.99 997	20	40	8.19 341	8.19 347	9.99 995	20
50	8.10 552	8.10 555	9.99 996	10	50	8.19 476	8.19 481	9.99 995	10
44 0	8.10 717	8.10 720	9.99 996	0 16	54 0	8.19 610	8.19 616	9.99 995	0 6
10	8.10 881	8.10 884	9.99 996	50	10	8.19 744	8.19 749	9.99 995	50
20	8.11 044	8.11 048	9.99 996	40	20	8.19 877	8.19 883	9.99 995	40
30	8.11 207	8.11 211	9.99 996	30	30	8.20 010	8.20 016	9.99 995	30
40	8.11 370	8.11 373	9.99 996	20	40	8.20 143	8.20 149	9.99 995	20
50	8.11 531	8.11 535	9.99 996	10	50	8.20 275	8.20 281	9.99 994	10
45 0	8.11 693	8.11 696	9.99 996	0 15	55 0	8.20 407	8.20 413	9.99 994	0 5
10	8.11 853	8.11 857	9.99 996	50	10	8.20 538	8.20 544	9.99 994	50
20	8.12 013	8.12 017	9.99 996	40	20	8.20 669	8.20 675	9.99 994	40
30	8.12 172	8.12 176	9.99 996	30	30	8.20 800	8.20 806	9.99 994	30
40	8.12 331	8.12 335	9.99 996	20	40	8.20 930	8.20 936	9.99 994	20
50	8.12 489	8.12 493	9.99 996	10	50	8.21 060	8.21 066	9.99 994	10
46 0	8.12 647	8.12 651	9.99 996	0 14	56 0	8.21 189	8.21 195	9.99 994	0 4
10	8.12 804	8.12 808	9.99 996	50	10	8.21 319	8.21 324	9.99 994	50
20	8.12 961	8.12 965	9.99 996	40	20	8.21 447	8.21 453	9.99 994	40
30	8.13 117	8.13 121	9.99 996	30	30	8.21 576	8.21 581	9.99 994	30
40	8.13 272	8.13 276	9.99 996	20	40	8.21 703	8.21 709	9.99 994	20
50	8.13 427	8.13 431	9.99 996	10	50	8.21 831	8.21 837	9.99 994	10
47 0	8.13 581	8.13 585	9.99 996	0 13	57 0	8.21 958	8.21 964	9.99 994	0 3
10	8.13 735	8.13 739	9.99 996	50	10	8.22 085	8.22 091	9.99 994	50
20	8.13 888	8.13 892	9.99 996	40	20	8.22 211	8.22 217	9.99 994	40
30	8.14 041	8.14 045	9.99 996	30	30	8.22 337	8.22 343	9.99 994	30
40	8.14 193	8.14 197	9.99 996	20	40	8.22 463	8.22 469	9.99 994	20
50	8.14 344	8.14 348	9.99 996	10	50	8.22 588	8.22 595	9.99 994	10
48 0	8.14 495	8.14 500	9.99 996	0 12	58 0	8.22 713	8.22 720	9.99 994	0 2
10	8.14 646	8.14 650	9.99 996	50	10	8.22 838	8.22 844	9.99 994	50
20	8.14 796	8.14 800	9.99 996	40	20	8.22 962	8.22 968	9.99 994	40
30	8.14 945	8.14 950	9.99 996	30	30	8.23 086	8.23 092	9.99 994	30
40	8.15 094	8.15 099	9.99 996	20	40	8.23 210	8.23 216	9.99 994	20
50	8.15 243	8.15 247	9.99 996	10	50	8.23 333	8.23 339	9.99 994	10
49 0	8.15 391	8.15 395	9.99 996	0 11	59 0	8.23 456	8.23 462	9.99 994	0 1
10	8.15 538	8.15 543	9.99 996	50	10	8.23 578	8.23 585	9.99 994	50
20	8.15 685	8.15 690	9.99 996	40	20	8.23 700	8.23 707	9.99 994	40
30	8.15 832	8.15 836	9.99 996	30	30	8.23 822	8.23 829	9.99 993	30
40	8.15 978	8.15 982	9.99 995	20	40	8.23 944	8.23 950	9.99 993	20
50	8.16 123	8.16 128	9.99 995	10	50	8.24 065	8.24 071	9.99 993	10
50 0	8.16 268	8.16 273	9.99 995	0 10	60 0	8.24 186	8.24 192	9.99 993	0 0

89°

1°

''	log sin	log tan	log cos	''	''	log sin	log tan	log cos	''
0 0	8.24 186	8.24 192	9.99 993	0 60	10 0	8.30 879	8.30 888	9.99 991	0 50
10	8.24 306	8.24 313	9.99 993	50	10	8.30 983	8.30 992	9.99 991	50
20	8.24 426	8.24 433	9.99 993	40	20	8.31 086	8.31 095	9.99 991	40
30	8.24 546	8.24 553	9.99 993	30	30	8.31 188	8.31 198	9.99 991	30
40	8.24 665	8.24 672	9.99 993	20	40	8.31 291	8.31 300	9.99 991	20
50	8.24 785	8.24 791	9.99 993	10	50	8.31 393	8.31 403	9.99 991	10
1 0	8.24 903	8.24 910	9.99 993	0 59	11 0	8.31 495	8.31 505	9.99 991	0 49
10	8.25 022	8.25 029	9.99 993	50	10	8.31 597	8.31 606	9.99 991	50
20	8.25 140	8.25 147	9.99 993	40	20	8.31 699	8.31 708	9.99 991	40
30	8.25 258	8.25 265	9.99 993	30	30	8.31 800	8.31 809	9.99 991	30
40	8.25 375	8.25 382	9.99 993	20	40	8.31 901	8.31 911	9.99 991	20
50	8.25 493	8.25 500	9.99 993	10	50	8.32 002	8.32 012	9.99 991	10
2 0	8.25 609	8.25 616	9.99 993	0 58	12 0	8.32 103	8.32 112	9.99 990	0 48
10	8.25 726	8.25 733	9.99 993	50	10	8.32 203	8.32 213	9.99 990	50
20	8.25 842	8.25 849	9.99 993	40	20	8.32 303	8.32 313	9.99 990	40
30	8.25 958	8.25 965	9.99 993	30	30	8.32 403	8.32 413	9.99 990	30
40	8.26 074	8.26 081	9.99 993	20	40	8.32 503	8.32 513	9.99 990	20
50	8.26 189	8.26 196	9.99 993	10	50	8.32 602	8.32 612	9.99 990	10
3 0	8.26 304	8.26 312	9.99 993	0 57	13 0	8.32 702	8.32 711	9.99 990	0 47
10	8.26 419	8.26 426	9.99 993	50	10	8.32 801	8.32 811	9.99 990	50
20	8.26 533	8.26 541	9.99 993	40	20	8.32 899	8.32 909	9.99 990	40
30	8.26 648	8.26 655	9.99 993	30	30	8.32 998	8.33 008	9.99 990	30
40	8.26 761	8.26 769	9.99 993	20	40	8.33 096	8.33 106	9.99 990	20
50	8.26 875	8.26 882	9.99 993	10	50	8.33 195	8.33 205	9.99 990	10
4 0	8.26 988	8.26 996	9.99 992	0 56	14 0	8.33 292	8.33 302	9.99 990	0 46
10	8.27 101	8.27 109	9.99 992	50	10	8.33 390	8.33 400	9.99 990	50
20	8.27 214	8.27 221	9.99 992	40	20	8.33 488	8.33 498	9.99 990	40
30	8.27 326	8.27 334	9.99 992	30	30	8.33 585	8.33 595	9.99 990	30
40	8.27 438	8.27 446	9.99 992	20	40	8.33 682	8.33 692	9.99 990	20
50	8.27 550	8.27 558	9.99 992	10	50	8.33 779	8.33 789	9.99 990	10
5 0	8.27 661	8.27 669	9.99 992	0 55	15 0	8.33 875	8.33 886	9.99 990	0 45
10	8.27 773	8.27 780	9.99 992	50	10	8.33 972	8.33 982	9.99 990	50
20	8.27 883	8.27 891	9.99 992	40	20	8.34 068	8.34 078	9.99 990	40
30	8.27 994	8.28 002	9.99 992	30	30	8.34 164	8.34 174	9.99 990	30
40	8.28 104	8.28 112	9.99 992	20	40	8.34 260	8.34 270	9.99 989	20
50	8.28 215	8.28 223	9.99 992	10	50	8.34 355	8.34 366	9.99 989	10
6 0	8.28 324	8.28 332	9.99 992	0 54	16 0	8.34 450	8.34 461	9.99 989	0 44
10	8.28 434	8.28 442	9.99 992	50	10	8.34 546	8.34 556	9.99 989	50
20	8.28 543	8.28 551	9.99 992	40	20	8.34 640	8.34 651	9.99 989	40
30	8.28 652	8.28 660	9.99 992	30	30	8.34 735	8.34 746	9.99 989	30
40	8.28 761	8.28 769	9.99 992	20	40	8.34 830	8.34 840	9.99 989	20
50	8.28 869	8.28 877	9.99 992	10	50	8.34 924	8.34 935	9.99 989	10
7 0	8.28 977	8.28 986	9.99 992	0 53	17 0	8.35 018	8.35 029	9.99 989	0 43
10	8.29 085	8.29 094	9.99 992	50	10	8.35 112	8.35 123	9.99 989	50
20	8.29 193	8.29 201	9.99 992	40	20	8.35 206	8.35 217	9.99 989	40
30	8.29 300	8.29 309	9.99 992	30	30	8.35 299	8.35 310	9.99 989	30
40	8.29 407	8.29 416	9.99 992	20	40	8.35 392	8.35 403	9.99 989	20
50	8.29 514	8.29 523	9.99 992	10	50	8.35 485	8.35 497	9.99 989	10
8 0	8.29 621	8.29 629	9.99 992	0 52	18 0	8.35 578	8.35 590	9.99 989	0 42
10	8.29 727	8.29 736	9.99 991	50	10	8.35 671	8.35 682	9.99 989	50
20	8.29 833	8.29 842	9.99 991	40	20	8.35 764	8.35 775	9.99 989	40
30	8.29 939	8.29 947	9.99 991	30	30	8.35 856	8.35 867	9.99 989	30
40	8.30 044	8.30 053	9.99 991	20	40	8.35 948	8.35 959	9.99 989	20
50	8.30 150	8.30 158	9.99 991	10	50	8.36 040	8.36 051	9.99 989	10
9 0	8.30 255	8.30 263	9.99 991	0 51	19 0	8.36 131	8.36 143	9.99 989	0 41
10	8.30 359	8.30 368	9.99 991	50	10	8.36 223	8.36 235	9.99 988	50
20	8.30 464	8.30 473	9.99 991	40	20	8.36 314	8.36 326	9.99 988	40
30	8.30 568	8.30 577	9.99 991	30	30	8.36 405	8.36 417	9.99 988	30
40	8.30 672	8.30 681	9.99 991	20	40	8.36 496	8.36 508	9.99 988	20
50	8.30 776	8.30 785	9.99 991	10	50	8.36 587	8.36 599	9.99 988	10
10 0	8.30 879	8.30 888	9.99 991	0 50	20 0	8.36 678	8.36 689	9.99 988	0 40
''	log cos	log cot	log sin	''	''	log cos	log cot	log sin	''

88°

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

1°

' "	log sin	log tan	log cos	' "	' "	log sin	log tan	log cos	' "
20 0	8.36 678	8.36 689	9.99 988	0 40	30 0	8.41 792	8.41 807	9.99 985	0 30
10	8.36 768	8.36 780	9.99 988	50	10	8.41 872	8.41 887	9.99 985	50
20	8.36 858	8.36 870	9.99 988	40	20	8.41 952	8.41 967	9.99 985	40
30	8.36 948	8.36 960	9.99 988	30	30	8.42 032	8.42 048	9.99 985	30
40	8.37 038	8.37 050	9.99 988	20	40	8.42 112	8.42 127	9.99 985	20
50	8.37 128	8.37 140	9.99 988	10	50	8.42 192	8.42 207	9.99 985	10
21 0	8.37 217	8.37 229	9.99 988	0 39	31 0	8.42 272	8.42 287	9.99 985	0 29
10	8.37 306	8.37 318	9.99 988	50	10	8.42 351	8.42 366	9.99 985	50
20	8.37 395	8.37 408	9.99 988	40	20	8.42 430	8.42 446	9.99 985	40
30	8.37 484	8.37 497	9.99 988	30	30	8.42 510	8.42 525	9.99 985	30
40	8.37 573	8.37 585	9.99 988	20	40	8.42 589	8.42 604	9.99 985	20
50	8.37 662	8.37 674	9.99 988	10	50	8.42 667	8.42 683	9.99 985	10
22 0	8.37 750	8.37 762	9.99 988	0 38	32 0	8.42 746	8.42 762	9.99 984	0 28
10	8.37 838	8.37 850	9.99 988	50	10	8.42 825	8.42 840	9.99 984	50
20	8.37 926	8.37 938	9.99 988	40	20	8.42 903	8.42 919	9.99 984	40
30	8.38 014	8.38 026	9.99 987	30	30	8.42 982	8.42 997	9.99 984	30
40	8.38 101	8.38 114	9.99 987	20	40	8.43 060	8.43 075	9.99 984	20
50	8.38 189	8.38 202	9.99 987	10	50	8.43 138	8.43 154	9.99 984	10
23 0	8.38 276	8.38 289	9.99 987	0 37	33 0	8.43 216	8.43 232	9.99 984	0 27
10	8.38 363	8.38 376	9.99 987	50	10	8.43 293	8.43 309	9.99 984	50
20	8.38 450	8.38 463	9.99 987	40	20	8.43 371	8.43 387	9.99 984	40
30	8.38 537	8.38 550	9.99 987	30	30	8.43 448	8.43 464	9.99 984	30
40	8.38 624	8.38 636	9.99 987	20	40	8.43 526	8.43 542	9.99 984	20
50	8.38 710	8.38 723	9.99 987	10	50	8.43 603	8.43 619	9.99 984	10
24 0	8.38 796	8.38 809	9.99 987	0 36	34 0	8.43 680	8.43 696	9.99 984	0 26
10	8.38 882	8.38 895	9.99 987	50	10	8.43 757	8.43 773	9.99 984	50
20	8.38 968	8.38 981	9.99 987	40	20	8.43 834	8.43 850	9.99 984	40
30	8.39 054	8.39 067	9.99 987	30	30	8.43 910	8.43 927	9.99 984	30
40	8.39 139	8.39 153	9.99 987	20	40	8.43 987	8.44 003	9.99 984	20
50	8.39 225	8.39 238	9.99 987	10	50	8.44 063	8.44 080	9.99 983	10
25 0	8.39 310	8.39 323	9.99 987	0 35	35 0	8.44 139	8.44 156	9.99 983	0 25
10	8.39 395	8.39 408	9.99 987	50	10	8.44 216	8.44 232	9.99 983	50
20	8.39 480	8.39 493	9.99 987	40	20	8.44 292	8.44 308	9.99 983	40
30	8.39 565	8.39 578	9.99 987	30	30	8.44 367	8.44 384	9.99 983	30
40	8.39 649	8.39 663	9.99 987	20	40	8.44 443	8.44 460	9.99 983	20
50	8.39 734	8.39 747	9.99 986	10	50	8.44 519	8.44 536	9.99 983	10
26 0	8.39 818	8.39 832	9.99 986	0 34	36 0	8.44 594	8.44 611	9.99 983	0 24
10	8.39 902	8.39 916	9.99 986	50	10	8.44 669	8.44 686	9.99 983	50
20	8.39 986	8.40 000	9.99 986	40	20	8.44 745	8.44 762	9.99 983	40
30	8.40 070	8.40 083	9.99 986	30	30	8.44 820	8.44 837	9.99 983	30
40	8.40 153	8.40 167	9.99 986	20	40	8.44 895	8.44 912	9.99 983	20
50	8.40 237	8.40 251	9.99 986	10	50	8.44 969	8.44 987	9.99 983	10
27 0	8.40 320	8.40 334	9.99 986	0 33	37 0	8.45 044	8.45 061	9.99 983	0 23
10	8.40 403	8.40 417	9.99 986	50	10	8.45 119	8.45 136	9.99 983	50
20	8.40 486	8.40 500	9.99 986	40	20	8.45 193	8.45 210	9.99 983	40
30	8.40 569	8.40 583	9.99 986	30	30	8.45 267	8.45 285	9.99 983	30
40	8.40 651	8.40 665	9.99 986	20	40	8.45 341	8.45 359	9.99 982	20
50	8.40 734	8.40 748	9.99 986	10	50	8.45 415	8.45 433	9.99 982	10
28 0	8.40 816	8.40 830	9.99 986	0 32	38 0	8.45 489	8.45 507	9.99 982	0 22
10	8.40 898	8.40 913	9.99 986	50	10	8.45 563	8.45 581	9.99 982	50
20	8.40 980	8.40 995	9.99 986	40	20	8.45 637	8.45 655	9.99 982	40
30	8.41 062	8.41 077	9.99 986	30	30	8.45 710	8.45 728	9.99 982	30
40	8.41 144	8.41 158	9.99 986	20	40	8.45 784	8.45 802	9.99 982	20
50	8.41 225	8.41 240	9.99 986	10	50	8.45 857	8.45 875	9.99 982	10
29 0	8.41 307	8.41 321	9.99 985	0 31	39 0	8.45 930	8.45 948	9.99 982	0 21
10	8.41 388	8.41 403	9.99 985	50	10	8.46 003	8.46 021	9.99 982	50
20	8.41 469	8.41 484	9.99 985	40	20	8.46 076	8.46 094	9.99 982	40
30	8.41 550	8.41 565	9.99 985	30	30	8.46 149	8.46 167	9.99 982	30
40	8.41 631	8.41 646	9.99 985	20	40	8.46 222	8.46 240	9.99 982	20
50	8.41 711	8.41 726	9.99 985	10	50	8.46 294	8.46 312	9.99 982	10
30 0	8.41 792	8.41 807	9.99 985	0 30	40 0	8.46 366	8.46 385	9.99 982	0 20

88°

1°

' "	log sin	log tan	log cos	' "	' "	log sin	log tan	log cos	' "
40 0	8.46 366	8.46 385	9.99 982	0 20	50 0	8.50 504	8.50 527	9.99 978	0 10
10	8.46 439	8.46 457	9.99 982	50	10	8.50 570	8.50 593	9.99 978	50
20	8.46 511	8.46 529	9.99 982	40	20	8.50 636	8.50 658	9.99 978	40
30	8.46 583	8.46 602	9.99 981	30	30	8.50 701	8.50 724	9.99 978	30
40	8.46 655	8.46 674	9.99 981	20	40	8.50 767	8.50 789	9.99 977	20
50	8.46 727	8.46 745	9.99 981	10	50	8.50 832	8.50 855	9.99 977	10
41 0	8.46 799	8.46 817	9.99 981	0 19	51 0	8.50 897	8.50 920	9.99 977	0 9
10	8.46 870	8.46 889	9.99 981	50	10	8.50 963	8.50 985	9.99 977	50
20	8.46 942	8.46 960	9.99 981	40	20	8.51 028	8.51 050	9.99 977	40
30	8.47 013	8.47 032	9.99 981	30	30	8.51 092	8.51 115	9.99 977	30
40	8.47 084	8.47 103	9.99 981	20	40	8.51 157	8.51 180	9.99 977	20
50	8.47 155	8.47 174	9.99 981	10	50	8.51 222	8.51 245	9.99 977	10
42 0	8.47 226	8.47 245	9.99 981	0 18	52 0	8.51 287	8.51 310	9.99 977	0 8
10	8.47 297	8.47 316	9.99 981	50	10	8.51 351	8.51 374	9.99 977	50
20	8.47 368	8.47 387	9.99 981	40	20	8.51 416	8.51 439	9.99 977	40
30	8.47 439	8.47 458	9.99 981	30	30	8.51 480	8.51 503	9.99 977	30
40	8.47 509	8.47 528	9.99 981	20	40	8.51 544	8.51 568	9.99 977	20
50	8.47 580	8.47 599	9.99 981	10	50	8.51 609	8.51 632	9.99 977	10
43 0	8.47 650	8.47 669	9.99 981	0 17	53 0	8.51 673	8.51 696	9.99 977	0 7
10	8.47 720	8.47 740	9.99 980	50	10	8.51 737	8.51 760	9.99 976	50
20	8.47 790	8.47 810	9.99 980	40	20	8.51 801	8.51 824	9.99 976	40
30	8.47 860	8.47 880	9.99 980	30	30	8.51 864	8.51 888	9.99 976	30
40	8.47 930	8.47 950	9.99 980	20	40	8.51 928	8.51 952	9.99 976	20
50	8.48 000	8.48 020	9.99 980	10	50	8.51 992	8.52 015	9.99 976	10
44 0	8.48 069	8.48 090	9.99 980	0 16	54 0	8.52 055	8.52 079	9.99 976	0 6
10	8.48 139	8.48 159	9.99 980	50	10	8.52 119	8.52 143	9.99 976	50
20	8.48 208	8.48 228	9.99 980	40	20	8.52 182	8.52 206	9.99 976	40
30	8.48 278	8.48 298	9.99 980	30	30	8.52 245	8.52 269	9.99 976	30
40	8.48 347	8.48 367	9.99 980	20	40	8.52 308	8.52 332	9.99 976	20
50	8.48 416	8.48 436	9.99 980	10	50	8.52 371	8.52 396	9.99 976	10
45 0	8.48 485	8.48 505	9.99 980	0 15	55 0	8.52 434	8.52 459	9.99 976	0 5
10	8.48 554	8.48 574	9.99 980	50	10	8.52 497	8.52 522	9.99 976	50
20	8.48 622	8.48 643	9.99 980	40	20	8.52 560	8.52 584	9.99 976	40
30	8.48 691	8.48 711	9.99 980	30	30	8.52 623	8.52 647	9.99 975	30
40	8.48 760	8.48 780	9.99 979	20	40	8.52 685	8.52 710	9.99 975	20
50	8.48 828	8.48 849	9.99 979	10	50	8.52 748	8.52 772	9.99 975	10
46 0	8.48 896	8.48 917	9.99 979	0 14	56 0	8.52 810	8.52 835	9.99 975	0 4
10	8.48 965	8.48 985	9.99 979	50	10	8.52 872	8.52 897	9.99 975	50
20	8.49 033	8.49 053	9.99 979	40	20	8.52 935	8.52 960	9.99 975	40
30	8.49 101	8.49 121	9.99 979	30	30	8.52 997	8.53 022	9.99 975	30
40	8.49 169	8.49 189	9.99 979	20	40	8.53 059	8.53 084	9.99 975	20
50	8.49 236	8.49 257	9.99 979	10	50	8.53 121	8.53 146	9.99 975	10
47 0	8.49 304	8.49 325	9.99 979	0 13	57 0	8.53 183	8.53 208	9.99 975	0 3
10	8.49 372	8.49 393	9.99 979	50	10	8.53 245	8.53 270	9.99 975	50
20	8.49 439	8.49 460	9.99 979	40	20	8.53 306	8.53 332	9.99 975	40
30	8.49 506	8.49 528	9.99 979	30	30	8.53 368	8.53 393	9.99 975	30
40	8.49 574	8.49 595	9.99 979	20	40	8.53 429	8.53 455	9.99 975	20
50	8.49 641	8.49 662	9.99 979	10	50	8.53 491	8.53 516	9.99 974	10
48 0	8.49 708	8.49 729	9.99 979	0 12	58 0	8.53 552	8.53 578	9.99 974	0 2
10	8.49 775	8.49 796	9.99 979	50	10	8.53 614	8.53 639	9.99 974	50
20	8.49 842	8.49 863	9.99 978	40	20	8.53 675	8.53 700	9.99 974	40
30	8.49 908	8.49 930	9.99 978	30	30	8.53 736	8.53 762	9.99 974	30
40	8.49 975	8.49 997	9.99 978	20	40	8.53 797	8.53 823	9.99 974	20
50	8.50 042	8.50 063	9.99 978	10	50	8.53 858	8.53 884	9.99 974	10
49 0	8.50 108	8.50 130	9.99 978	0 11	59 0	8.53 919	8.53 945	9.99 974	0 1
10	8.50 174	8.50 196	9.99 978	50	10	8.53 979	8.54 005	9.99 974	50
20	8.50 241	8.50 263	9.99 978	40	20	8.54 040	8.54 066	9.99 974	40
30	8.50 307	8.50 329	9.99 978	30	30	8.54 101	8.54 127	9.99 974	30
40	8.50 373	8.50 395	9.99 978	20	40	8.54 161	8.54 187	9.99 974	20
50	8.50 439	8.50 461	9.99 978	10	50	8.54 222	8.54 248	9.99 974	10
50 0	8.50 504	8.50 527	9.99 978	0 10	60 0	8.54 282	8.54 308	9.99 974	0 0
' "	log cos	log cot	log sin	' "	' "	log cos	log cot	log sin	' "

88°

						$0^\circ$	$90^\circ$	$180^\circ$	$270^\circ$								
/	log sin	d.	log tan	c. d.	log cot	log cos	Prop. Pts.										
							d	pp1''	d	pp1''							
<b>0</b>	—	—	—	—	—	0.00 000	<b>60</b>										
1	6.46 373		6.46 373		3.53 627	0.00 000	59										
2	6.76 476	30103	6.76 476	30103	3.23 524	0.00 000	58										
3	6.94 085	17600	6.94 085	17600	3.05 915	0.00 000	57										
4	7.06 579	12494	7.06 579	12494	2.93 421	0.00 000	56										
5	7.16 270	9691	7.16 270	9691	2.83 730	0.00 000	55										
6	7.24 188	7918	7.24 188	7918	2.75 812	0.00 000	54										
7	7.30 882	6694	7.30 882	6694	2.69 118	0.00 000	53										
8	7.36 682	5800	7.36 682	5800	2.63 318	0.00 000	52										
9	7.41 797	5115	7.41 797	5115	2.58 203	0.00 000	51										
		4576		4576													
<b>10</b>	7.46 373		7.46 373		2.53 627	0.00 000	<b>50</b>										
11	7.50 512	4139	7.50 512	4139	2.49 488	0.00 000	49										
12	7.54 291	3779	7.54 291	3779	2.45 709	0.00 000	48										
13	7.57 767	3476	7.57 767	3476	2.42 233	0.00 000	47										
14	7.60 985	3218	7.60 986	3219	2.39 014	0.00 000	46										
		2997		2996													
15	7.63 982	2802	7.63 982	2803	2.36 018	0.00 000	45										
16	7.66 784	2633	7.66 785	2633	2.33 215	0.00 000	44										
17	7.69 417	2483	7.69 418	2482	2.30 582	0.99 999	43										
18	7.71 900	2348	7.71 900	2348	2.28 100	0.99 999	42										
19	7.74 248	2227	7.74 248	2228	2.25 752	0.99 999	41										
<b>20</b>	7.76 475		7.76 476		2.23 524	0.99 999	<b>40</b>										
21	7.78 594	2119	7.78 595	2119	2.21 405	0.99 999	39										
22	7.80 615	2021	7.80 615	2020	2.19 385	0.99 999	38										
23	7.82 545	1930	7.82 546	1931	2.17 454	0.99 999	37										
24	7.84 393	1848	7.84 394	1848	2.15 606	0.99 999	36										
		1773		1773													
25	7.86 166	1704	7.86 167	1704	2.13 833	0.99 999	35										
26	7.87 870	1639	7.87 871	1639	2.12 129	0.99 999	34										
27	7.89 509	1579	7.89 510	1579	2.10 490	0.99 999	33										
28	7.91 088	1524	7.91 089	1524	2.08 911	0.99 999	32										
29	7.92 612	1472	7.92 613	1473	2.07 387	0.99 998	31										
		1424		1424													
<b>30</b>	7.94 084		7.94 086		2.05 914	0.99 998	<b>30</b>										
31	7.95 508	1379	7.95 510	1379	2.04 490	0.99 998	29										
32	7.96 887	1336	7.96 889	1336	2.03 111	0.99 998	28										
33	7.98 223	1297	7.98 225	1297	2.01 775	0.99 998	27										
34	7.99 520	1259	7.99 522	1259	2.00 478	0.99 998	26										
		1223		1223													
35	8.00 779	1190	8.00 781	1190	1.99 219	0.99 998	25										
36	8.02 002	1158	8.02 004	1158	1.97 996	0.99 998	24										
37	8.03 192	1128	8.03 194	1128	1.96 806	0.99 997	23										
38	8.04 350	1100	8.04 353	1100	1.95 647	0.99 997	22										
39	8.05 478	1072	8.05 481	1072	1.94 519	0.99 997	21										
		1046		1046													
<b>40</b>	8.06 578		8.06 581		1.93 419	0.99 997	<b>20</b>										
41	8.07 650	1022	8.07 653	1022	1.92 347	0.99 997	19										
42	8.08 696	999	8.08 700	998	1.91 300	0.99 997	18										
43	8.09 718	976	8.09 722	976	1.90 278	0.99 997	17										
44	8.10 717	954	8.10 720	954	1.89 280	0.99 996	16										
		934		934													
45	8.11 693	914	8.11 696	915	1.88 304	0.99 996	15										
46	8.12 647	896	8.12 651	895	1.87 349	0.99 996	14										
47	8.13 587	877	8.13 585	878	1.86 415	0.99 996	13										
48	8.14 495		8.14 500		1.85 500	0.99 996	12										
49	8.15 391		8.15 395		1.84 605	0.99 996	11										
<b>50</b>	8.16 268		8.16 273		1.83 727	0.99 995	<b>10</b>										
51	8.17 128	860	8.17 133	860	1.82 867	0.99 995	9										
52	8.17 971	843	8.17 976	843	1.82 024	0.99 995	8										
53	8.18 798	827	8.18 804	828	1.81 196	0.99 995	7										
54	8.19 610	812	8.19 616	812	1.80 384	0.99 995	6										
		797		797													
55	8.20 407	782	8.20 413	782	1.79 587	0.99 994	5										
56	8.21 189	769	8.21 195	769	1.78 805	0.99 994	4										
57	8.21 958	755	8.21 964	756	1.78 036	0.99 994	3										
58	8.22 713	743	8.22 720	742	1.77 280	0.99 994	2										
59	8.23 456	730	8.23 462	730	1.76 538	0.99 994	1										
<b>60</b>	8.24 186		8.24 192		1.75 808	0.99 993	<b>0</b>										

		1°			*91°		181°		*271°		
'	log sin	d.	log tan	c. d.	log cot	log cos		Prop. Pts.			
0	8.24 186		8.24 192		1.75 808	9.99 993	60				
1	8.24 903	717	8.24 910	718	1.75 090	9.99 993	59				
2	8.25 609	706	8.25 616	706	1.74 384	9.99 993	58				
3	8.26 304	695	8.26 312	696	1.73 688	9.99 993	57				
4	8.26 998	684	8.26 996	684	1.73 004	9.99 992	56				
		673		673							
5	8.27 661		8.27 669		1.72 331	9.99 992	55				
6	8.28 324	663	8.28 332	663	1.71 668	9.99 992	54				
7	8.28 977	653	8.28 986	654	1.71 014	9.99 992	53				
8	8.29 621	644	8.29 629	643	1.70 371	9.99 992	52				
9	8.30 255	634	8.30 263	634	1.69 737	9.99 991	51				
		624		625							
10	8.30 879		8.30 888		1.69 112	9.99 991	50				
11	8.31 495	616	8.31 505	617	1.68 495	9.99 991	49				
12	8.32 103	608	8.32 112	607	1.67 888	9.99 990	48				
13	8.32 702	599	8.32 711	599	1.67 289	9.99 990	47				
14	8.33 292	590	8.33 302	591	1.66 698	9.99 990	46				
		583		584							
15	8.33 875		8.33 886		1.66 114	9.99 990	45	718	11.07	485	8.08
16	8.34 450	575	8.34 461	575	1.65 539	9.99 989	44	717	11.95	480	8.00
17	8.35 018	568	8.35 029	568	1.64 971	9.99 989	43	706	11.77	475	7.92
18	8.35 578	560	8.35 590	561	1.64 410	9.99 989	42	696	11.60	474	7.90
19	8.36 131	553	8.36 143	553	1.63 857	9.99 989	41	695	11.58	470	7.83
		547		546				684	11.40	464	7.73
20	8.36 678		8.36 689		1.63 311	9.99 988	40	673	11.22	460	7.67
21	8.37 217	539	8.37 229	540	1.62 771	9.99 988	39	663	11.05	459	7.65
22	8.37 750	533	8.37 762	533	1.62 238	9.99 988	38	654	10.90	455	7.58
23	8.38 276	526	8.38 289	527	1.61 711	9.99 987	37	653	10.88	450	7.50
24	8.38 796	520	8.38 809	520	1.61 191	9.99 987	36	644	10.73	446	7.43
		514		514				643	10.72	445	7.42
25	8.39 310		8.39 323		1.60 677	9.99 987	35	634	10.57	441	7.35
26	8.39 818	508	8.39 832	509	1.60 168	9.99 986	34	625	10.42	437	7.28
27	8.40 320	502	8.40 334	502	1.59 666	9.99 986	33	624	10.40	436	7.27
28	8.40 816	496	8.40 830	496	1.59 170	9.99 986	32	617	10.28	433	7.22
29	8.41 307	491	8.41 321	491	1.58 679	9.99 985	31	616	10.27	432	7.20
		485		486				608	10.13	428	7.13
30	8.41 792		8.41 807		1.58 193	9.99 985	30	607	10.12	427	7.12
31	8.42 272	480	8.42 287	480	1.57 713	9.99 985	29	599	9.98	424	7.07
32	8.42 746	474	8.42 762	475	1.57 238	9.99 984	28	591	9.85	420	7.00
33	8.43 216	470	8.43 232	470	1.56 768	9.99 984	27	590	9.83	419	6.98
34	8.43 680	464	8.43 696	464	1.56 304	9.99 984	26	584	9.73	416	6.93
		459		460				583	9.72	412	6.87
35	8.44 139		8.44 156		1.55 844	9.99 983	25	575	9.58	411	6.85
36	8.44 594	455	8.44 611	455	1.55 389	9.99 983	24	568	9.47	408	6.80
37	8.45 044	450	8.45 061	450	1.54 939	9.99 983	23	561	9.35	404	6.73
38	8.45 489	445	8.45 507	446	1.54 493	9.99 982	22	560	9.33	401	6.68
39	8.45 930	441	8.45 948	441	1.54 052	9.99 982	21	553	9.22	400	6.67
		436		437				547	9.12	397	6.62
40	8.46 366		8.46 385		1.53 615	9.99 982	20	546	9.10	396	6.60
41	8.46 799	433	8.46 817	432	1.53 183	9.99 981	19	540	9.00	393	6.55
42	8.47 226	427	8.47 245	428	1.52 755	9.99 981	18	539	8.98	390	6.50
43	8.47 650	424	8.47 669	424	1.52 331	9.99 981	17	533	8.88	386	6.43
44	8.48 069	419	8.48 089	420	1.51 911	9.99 980	16	527	8.78	383	6.38
		416		416				526	8.77	382	6.37
45	8.48 485		8.48 505		1.51 495	9.99 980	15	520	8.67	380	6.33
46	8.48 896	411	8.48 917	412	1.51 083	9.99 979	14	514	8.57	379	6.32
47	8.49 304	408	8.49 325	408	1.50 675	9.99 979	13	509	8.48	376	6.27
48	8.49 708	404	8.49 729	404	1.50 271	9.99 979	12	508	8.47	373	6.22
49	8.50 108	400	8.50 130	401	1.49 870	9.99 978	11	502	8.37	370	6.17
		396		397				496	8.27	369	6.15
50	8.50 507		8.50 527		1.49 473	9.99 978	10	491	8.18	367	6.12
51	8.50 894	393	8.50 920	393	1.49 080	9.99 977	9	486	8.10	363	6.05
52	8.51 287	390	8.51 310	390	1.48 690	9.99 977	8				
53	8.51 673	386	8.51 696	386	1.48 304	9.99 977	7				
54	8.52 055	382	8.52 079	383	1.47 921	9.99 976	6				
		379		380							
55	8.52 434		8.52 459		1.47 541	9.99 976	5				
56	8.52 810	376	8.52 835	376	1.47 165	9.99 975	4				
57	8.53 183	373	8.53 208	373	1.46 792	9.99 975	3				
58	8.53 552	369	8.53 578	370	1.46 422	9.99 974	2				
59	8.53 919	367	8.53 945	367	1.46 055	9.99 974	1				
60	8.54 282	363	8.54 308	363	1.45 692	9.99 974	0				
	log cos	d.	log cot	c. d.	log tan	log sin	'	Prop. Pts.			

\*178°    268°    \*358°

88°

<b>2°</b>							*92°	182°	*272°		
'	log sin	d.	log tan	c. d.	log cot	log cos	Prop. Pts.				
0	8.54 282		8.54 308		1.45 692	9.99 974	<b>60</b>				
1	8.54 642	360	8.54 669	361	1.45 331	9.99 973	59				
2	8.54 999	357	8.55 027	358	1.44 973	9.99 973	58				
3	8.55 354	355	8.55 382	355	1.44 618	9.99 972	57				
4	8.55 705	351	8.55 734	352	1.44 266	9.99 972	56				
		349		349							
5	8.56 054		8.56 083		1.43 917	9.99 971	55				
6	8.56 400	346	8.56 429	346	1.43 571	9.99 971	54				
7	8.56 743	343	8.56 773	344	1.43 227	9.99 970	53				
8	8.57 084	341	8.57 114	341	1.42 886	9.99 970	52				
9	8.57 421	337	8.57 452	338	1.42 548	9.99 969	51				
		336		336							
<b>10</b>	<b>8.57 757</b>		<b>8.57 788</b>		<b>1.42 212</b>	<b>9.99 969</b>	<b>50</b>				
11	8.58 089	332	8.58 121	333	1.41 879	9.99 968	49				
12	8.58 419	330	8.58 451	330	1.41 549	9.99 968	48				
13	8.58 747	328	8.58 779	328	1.41 221	9.99 967	47				
14	8.59 072	325	8.59 105	326	1.40 895	9.99 967	46				
		323		323							
15	8.59 395		8.59 428		1.40 572	9.99 967	45	d	pp1''	d	pp1''
16	8.59 715	320	8.59 749	321	1.40 251	9.99 966	44	361	6.02	291	4.85
17	8.60 033	318	8.60 068	319	1.39 932	9.99 966	43	360	6.00	290	4.83
18	8.60 349	316	8.60 384	316	1.39 616	9.99 965	42	358	5.97	289	4.82
19	8.60 662	313	8.60 698	314	1.39 302	9.99 964	41	357	5.95	288	4.80
		311		311				355	5.92	287	4.78
<b>20</b>	<b>8.60 973</b>		<b>8.61 009</b>		<b>1.38 991</b>	<b>9.99 964</b>	<b>40</b>	352	5.87	285	4.75
21	8.61 282	309	8.61 319	310	1.38 681	9.99 963	39	351	5.85	284	4.73
22	8.61 589	307	8.61 626	307	1.38 374	9.99 963	38	349	5.82	283	4.72
23	8.61 894	305	8.61 931	305	1.38 069	9.99 962	37	346	5.77	281	4.68
24	8.62 196	302	8.62 234	303	1.37 766	9.99 962	36	344	5.73	280	4.67
		301		301				343	5.72	279	4.65
25	8.62 497		8.62 535		1.37 465	9.99 961	35	341	5.68	278	4.63
26	8.62 795	298	8.62 834	299	1.37 166	9.99 961	34	338	5.63	277	4.62
27	8.63 091	296	8.63 131	297	1.36 869	9.99 960	33	337	5.62	276	4.60
28	8.63 385	294	8.63 426	295	1.36 574	9.99 960	32	336	5.60	274	4.57
29	8.63 678	293	8.63 718	292	1.36 282	9.99 959	31	333	5.55	273	4.55
		290		291				332	5.53	272	4.53
<b>30</b>	<b>8.63 968</b>		<b>8.64 009</b>		<b>1.35 991</b>	<b>9.99 959</b>	<b>30</b>	330	5.50	271	4.52
31	8.64 256	288	8.64 298	289	1.35 702	9.99 958	29	328	5.47	270	4.50
32	8.64 543	287	8.64 585	287	1.35 415	9.99 958	28	326	5.43	269	4.48
33	8.64 827	284	8.64 870	285	1.35 130	9.99 957	27	325	5.42	268	4.47
34	8.65 110	283	8.65 154	284	1.34 846	9.99 956	26	323	5.38	267	4.45
		281		281				321	5.35	266	4.43
35	8.65 391		8.65 435		1.34 565	9.99 956	25	320	5.33	264	4.40
36	8.65 670	279	8.65 715	280	1.34 285	9.99 955	24	319	5.32	263	4.38
37	8.65 947	277	8.65 993	278	1.34 007	9.99 955	23	318	5.30	261	4.35
38	8.66 223	276	8.66 269	276	1.33 731	9.99 954	22	316	5.27	260	4.33
39	8.66 497	274	8.66 543	274	1.33 457	9.99 954	21	314	5.23	259	4.32
		272		273				313	5.22	258	4.30
<b>40</b>	<b>8.66 769</b>		<b>8.66 816</b>		<b>1.33 184</b>	<b>9.99 953</b>	<b>20</b>	311	5.18	257	4.28
41	8.67 039	270	8.67 087	271	1.32 913	9.99 952	19	310	5.17	256	4.27
42	8.67 308	269	8.67 356	269	1.32 644	9.99 952	18	309	5.15	255	4.25
43	8.67 575	267	8.67 624	268	1.32 376	9.99 951	17	307	5.12	254	4.23
44	8.67 841	266	8.67 890	266	1.32 110	9.99 951	16	305	5.08	253	4.22
		263		264				303	5.05	252	4.20
45	8.68 104		8.68 154		1.31 846	9.99 950	15	302	5.03	251	4.18
46	8.68 367	263	8.68 417	263	1.31 583	9.99 949	14	301	5.02	250	4.17
47	8.68 627	260	8.68 678	261	1.31 322	9.99 949	13	299	4.98	249	4.15
48	8.68 886	259	8.68 938	260	1.31 062	9.99 948	12	298	4.97	248	4.13
49	8.69 144	258	8.69 196	258	1.30 804	9.99 948	11	297	4.95	247	4.12
		256		257				296	4.93	246	4.10
<b>50</b>	<b>8.69 400</b>		<b>8.69 453</b>		<b>1.30 547</b>	<b>9.99 947</b>	<b>10</b>	295	4.92	245	4.08
51	8.69 654	254	8.69 708	255	1.30 292	9.99 946	9	294	4.90	244	4.07
52	8.69 907	253	8.69 962	254	1.30 038	9.99 946	8	293	4.88	243	4.05
53	8.70 159	252	8.70 214	252	1.29 786	9.99 945	7	292	4.87	242	4.03
54	8.70 409	250	8.70 465	251	1.29 535	9.99 944	6				
		249		249							
55	8.70 658		8.70 714		1.29 286	9.99 944	5				
56	8.70 905	247	8.70 962	248	1.29 038	9.99 943	4				
57	8.71 151	246	8.71 208	246	1.28 792	9.99 942	3				
58	8.71 395	244	8.71 453	245	1.28 547	9.99 942	2				
59	8.71 638	243	8.71 697	244	1.28 303	9.99 941	1				
		242		243							
<b>60</b>	<b>8.71 880</b>		<b>8.71 940</b>		<b>1.28 060</b>	<b>9.99 940</b>	<b>0</b>				
	log cos	d.	log cot	c. d.	log tan	log sin	'	Prop. Pts.			

\*177°    267°    \*357°

**87°**



<b>3°</b>								* 93°	183°	* 273°							
'	log sin	d.	log tan	c. d.	log cot	log cos		Prop. Pts.									
0	8.71 880		8.71 940		1.28 060	9.99 940	<b>60</b>										
1	8.72 120	240	8.72 181	241	1.27 819	9.99 940	59										
2	8.72 359	239	8.72 420	239	1.27 580	9.99 939	58										
3	8.72 597	238	8.72 659	239	1.27 341	9.99 938	57										
4	8.72 834	237	8.72 896	237	1.27 104	9.99 938	56										
5	8.73 069		8.73 132		1.26 868	9.99 937	55										
6	8.73 303	234	8.73 366	234	1.26 634	9.99 936	54										
7	8.73 535	232	8.73 600	234	1.26 400	9.99 936	53										
8	8.73 767	232	8.73 832	232	1.26 168	9.99 935	52										
9	8.73 997	230	8.74 063	231	1.25 937	9.99 934	51										
<b>10</b>	8.74 226	229	8.74 292	229	1.25 708	9.99 934	<b>50</b>										
11	8.74 454	228	8.74 521	229	1.25 479	9.99 933	49										
12	8.74 680	226	8.74 748	227	1.25 252	9.99 932	48										
13	8.74 906	226	8.74 974	226	1.25 026	9.99 932	47										
14	8.75 130	224	8.75 199	225	1.24 801	9.99 931	46										
15	8.75 353	223	8.75 423	224	1.24 577	9.99 930	45										
16	8.75 575	222	8.75 645	222	1.24 355	9.99 929	44										
17	8.75 795	220	8.75 867	222	1.24 133	9.99 929	43										
18	8.76 015	220	8.76 087	220	1.23 913	9.99 928	42										
19	8.76 234	219	8.76 306	219	1.23 694	9.99 927	41										
<b>20</b>	8.76 451	217	8.76 525	219	1.23 475	9.99 926	<b>40</b>										
21	8.76 667	216	8.76 742	217	1.23 258	9.99 926	39										
22	8.76 883	216	8.76 958	216	1.23 042	9.99 925	38										
23	8.77 097	214	8.77 173	215	1.22 827	9.99 924	37										
24	8.77 310	213	8.77 387	214	1.22 613	9.99 923	36										
25	8.77 522	212	8.77 600	213	1.22 400	9.99 923	35										
26	8.77 733	211	8.77 811	211	1.22 189	9.99 922	34										
27	8.77 943	210	8.78 022	211	1.21 978	9.99 921	33										
28	8.78 152	209	8.78 232	210	1.21 768	9.99 920	32										
29	8.78 360	208	8.78 441	209	1.21 559	9.99 920	31										
<b>30</b>	8.78 568	208	8.78 649	208	1.21 351	9.99 919	<b>30</b>										
31	8.78 774	206	8.78 855	206	1.21 145	9.99 918	29										
32	8.78 979	205	8.79 061	206	1.20 939	9.99 917	28										
33	8.79 183	204	8.79 266	205	1.20 734	9.99 917	27										
34	8.79 386	203	8.79 470	204	1.20 530	9.99 916	26										
35	8.79 588	202	8.79 673	203	1.20 327	9.99 915	25										
36	8.79 789	201	8.79 875	202	1.20 125	9.99 914	24										
37	8.79 990	201	8.80 076	201	1.19 924	9.99 913	23										
38	8.80 189	199	8.80 277	201	1.19 723	9.99 913	22										
39	8.80 388	199	8.80 476	199	1.19 524	9.99 912	21										
<b>40</b>	8.80 585	197	8.80 674	198	1.19 326	9.99 911	<b>20</b>										
41	8.80 782	197	8.80 872	198	1.19 128	9.99 910	19										
42	8.80 978	196	8.81 068	196	1.18 932	9.99 909	18										
43	8.81 173	195	8.81 264	196	1.18 736	9.99 909	17										
44	8.81 367	194	8.81 459	195	1.18 541	9.99 908	16										
45	8.81 560	193	8.81 653	194	1.18 347	9.99 907	15										
46	8.81 752	192	8.81 846	193	1.18 154	9.99 906	14										
47	8.81 944	192	8.82 038	192	1.17 962	9.99 905	13										
48	8.82 134	190	8.82 230	192	1.17 770	9.99 904	12										
49	8.82 324	190	8.82 420	190	1.17 580	9.99 904	11										
<b>50</b>	8.82 513	189	8.82 610	190	1.17 390	9.99 903	<b>10</b>										
51	8.82 701	188	8.82 799	189	1.17 201	9.99 902	9										
52	8.82 888	187	8.82 987	188	1.17 013	9.99 901	8										
53	8.83 075	187	8.83 175	188	1.16 825	9.99 900	7										
54	8.83 261	186	8.83 361	186	1.16 639	9.99 899	6										
55	8.83 446	185	8.83 547	186	1.16 453	9.99 898	5										
56	8.83 630	184	8.83 732	185	1.16 268	9.99 898	4										
57	8.83 813	183	8.83 916	184	1.16 084	9.99 897	3										
58	8.83 996	183	8.84 100	184	1.15 900	9.99 896	2										
59	8.84 177	181	8.84 282	182	1.15 718	9.99 895	1										
<b>60</b>	8.84 358	181	8.84 464	182	1.15 536	9.99 894	<b>0</b>										
	log cos	d.	log cot	c. d.	log tan	log sin	'	Prop. Pts.									

d	pp l'	d	pp l'
241	4.02	209	3.48
240	4.00	208	3.47
239	3.98	207	3.45
238	3.97	206	3.43
237	3.95	205	3.42
236	3.93	204	3.40
235	3.92	203	3.38
234	3.90	202	3.37
233	3.88	201	3.35
232	3.87	200	3.33
231	3.85	199	3.32
230	3.83	198	3.30
229	3.82	197	3.28
228	3.80	196	3.27
227	3.78	195	3.25
226	3.77	194	3.23
225	3.75	193	3.22
224	3.73	192	3.20
223	3.72	191	3.18
222	3.70	190	3.17
221	3.68	189	3.15
220	3.67	188	3.13
219	3.65	187	3.12
218	3.63	186	3.10
217	3.62	185	3.08
216	3.60	184	3.07
215	3.58	183	3.05
214	3.57	182	3.03
213	3.55	181	3.02
212	3.53		
211	3.52		
210	3.50		



<b>4°</b>							*94°	184°	*274°
'	log sin	d.	log tan	e. d.	log cot	log cos			Prop. Pts.
0	8.84 358		8.84 464		1.15 536	9.99 894	<b>60</b>		
1	8.84 539	181	8.84 646	182	1.15 354	9.99 893	59		
2	8.84 718	179	8.84 826	180	1.15 174	9.99 892	58		
3	8.84 897	179	8.85 006	180	1.14 994	9.99 891	57		
4	8.85 075	178	8.85 185	179	1.14 815	9.99 891	56		
		177		178					
5	8.85 252		8.85 363		1.14 637	9.99 890	55		
6	8.85 429	177	8.85 540	177	1.14 460	9.99 889	54		
7	8.85 605	176	8.85 717	177	1.14 283	9.99 888	53		
8	8.85 780	175	8.85 893	176	1.14 107	9.99 887	52		
9	8.85 955	175	8.86 069	176	1.13 931	9.99 886	51		
		173		174					
10	8.86 128		8.86 243		1.13 757	9.99 885	<b>50</b>		
11	8.86 301	173	8.86 417	174	1.13 583	9.99 884	49		
12	8.86 474	173	8.86 591	174	1.13 409	9.99 883	48		
13	8.86 645	171	8.86 763	172	1.13 237	9.99 882	47		
14	8.86 816	171	8.86 935	172	1.13 065	9.99 881	46		
		171		171					
15	8.86 987		8.87 106		1.12 894	9.99 880	45		
16	8.87 156	169	8.87 277	171	1.12 723	9.99 879	44	d	pp 1''
17	8.87 325	169	8.87 447	170	1.12 553	9.99 879	43	182	3.03
18	8.87 494	169	8.87 616	169	1.12 384	9.99 878	42	181	3.02
19	8.87 661	167	8.87 785	169	1.12 215	9.99 877	41	180	3.00
		168		168				179	2.98
20	8.87 829		8.87 953		1.12 047	9.99 876	<b>40</b>	178	2.97
21	8.87 995	166	8.88 120	167	1.11 880	9.99 875	39	177	2.95
22	8.88 161	166	8.88 287	167	1.11 713	9.99 874	38	176	2.93
23	8.88 326	165	8.88 453	166	1.11 547	9.99 873	37	175	2.92
24	8.88 490	164	8.88 618	165	1.11 382	9.99 872	36	174	2.90
		164		165				173	2.88
25	8.88 654		8.88 783		1.11 217	9.99 871	35	172	2.87
26	8.88 817	163	8.88 948	165	1.11 052	9.99 870	34	171	2.85
27	8.88 980	163	8.89 111	163	1.10 889	9.99 869	33	170	2.83
28	8.89 142	162	8.89 274	163	1.10 726	9.99 868	32	169	2.82
29	8.89 304	162	8.89 437	163	1.10 563	9.99 867	31	168	2.80
		160		161				167	2.78
30	8.89 464		8.89 598		1.10 402	9.99 866	<b>30</b>	166	2.77
31	8.89 625	161	8.89 760	162	1.10 240	9.99 865	29	165	2.75
32	8.89 784	159	8.89 920	160	1.10 080	9.99 864	28	164	2.73
33	8.89 943	159	8.90 080	160	1.09 920	9.99 863	27	163	2.72
34	8.90 102	159	8.90 240	160	1.09 760	9.99 862	26	162	2.70
		158		159				161	2.68
35	8.90 260		8.90 399		1.09 601	9.99 861	25	160	2.67
36	8.90 417	157	8.90 557	158	1.09 443	9.99 860	24	159	2.65
37	8.90 574	157	8.90 715	158	1.09 285	9.99 859	23	158	2.63
38	8.90 730	156	8.90 872	157	1.09 128	9.99 858	22	157	2.62
39	8.90 885	155	8.91 029	157	1.08 971	9.99 857	21	156	2.60
		155		156				155	2.58
40	8.91 040		8.91 185		1.08 815	9.99 856	<b>20</b>	154	2.57
41	8.91 195	155	8.91 340	155	1.08 660	9.99 855	19	153	2.55
42	8.91 349	154	8.91 495	155	1.08 505	9.99 854	18	152	2.53
43	8.91 502	153	8.91 650	155	1.08 350	9.99 853	17	151	2.52
44	8.91 655	153	8.91 803	153	1.08 197	9.99 852	16	150	2.50
		152		154				149	2.48
45	8.91 807		8.91 957		1.08 043	9.99 851	15	148	2.47
46	8.91 959	152	8.92 110	153	1.07 890	9.99 850	14	147	2.45
47	8.92 110	151	8.92 262	152	1.07 738	9.99 848	13	146	2.43
48	8.92 261	151	8.92 414	152	1.07 586	9.99 847	12	145	2.42
49	8.92 411	150	8.92 565	151	1.07 435	9.99 846	11		
		150		151					
50	8.92 561		8.92 716		1.07 284	9.99 845	<b>10</b>		
51	8.92 710	149	8.92 866	150	1.07 134	9.99 844	9		
52	8.92 859	149	8.93 016	150	1.06 984	9.99 843	8		
53	8.93 007	148	8.93 165	149	1.06 835	9.99 842	7		
54	8.93 154	147	8.93 313	148	1.06 687	9.99 841	6		
		147		149					
55	8.93 301		8.93 462		1.06 538	9.99 840	5		
56	8.93 448	147	8.93 609	147	1.06 391	9.99 839	4		
57	8.93 594	146	8.93 756	147	1.06 244	9.99 838	3		
58	8.93 740	146	8.93 903	147	1.06 097	9.99 837	2		
59	8.93 885	145	8.94 049	146	1.05 951	9.99 836	1		
		145		146					
60	8.94 030		8.94 195		1.05 805	9.99 834	<b>0</b>		
	log cos	d.	log cot	e. d.	log tan	log sin	'		Prop. Pts.

\* 175°    265°    \* 355°

**85°**

<b>5°</b>							*95°	185°	*275°
'	log sin	d.	log tan	c. d.	log cot	log cos		Prop. Pts.	
0	8.94 030		8.94 195		1.05 805	9.99 834	<b>60</b>		
1	8.94 174	<sup>144</sup>	8.94 340	<sup>145</sup>	1.05 660	9.99 833	59		
2	8.94 317	<sup>143</sup>	8.94 485	<sup>145</sup>	1.05 515	9.99 832	58		
3	8.94 461	<sup>144</sup>	8.94 630	<sup>145</sup>	1.05 370	9.99 831	57		
4	8.94 603	<sup>142</sup>	8.94 773	<sup>143</sup>	1.05 227	9.99 830	56		
5	8.94 746	<sup>143</sup>	8.94 917	<sup>144</sup>	1.05 083	9.99 829	55		
6	8.94 887	<sup>141</sup>	8.95 060	<sup>143</sup>	1.04 940	9.99 828	54		
7	8.95 029	<sup>142</sup>	8.95 202	<sup>142</sup>	1.04 798	9.99 827	53		
8	8.95 170	<sup>141</sup>	8.95 344	<sup>142</sup>	1.04 656	9.99 825	52		
9	8.95 310	<sup>140</sup>	8.95 486	<sup>142</sup>	1.04 514	9.99 824	51		
10	8.95 450	<sup>140</sup>	8.95 627	<sup>141</sup>	1.04 373	9.99 823	<b>50</b>		
11	8.95 589	<sup>139</sup>	8.95 767	<sup>140</sup>	1.04 233	9.99 822	49		
12	8.95 728	<sup>139</sup>	8.95 908	<sup>141</sup>	1.04 092	9.99 821	48		
13	8.95 867	<sup>139</sup>	8.96 047	<sup>139</sup>	1.03 953	9.99 820	47		
14	8.96 005	<sup>138</sup>	8.96 187	<sup>140</sup>	1.03 813	9.99 819	46		
15	8.96 143	<sup>138</sup>	8.96 325	<sup>138</sup>	1.03 675	9.99 817	45		
16	8.96 280	<sup>137</sup>	8.96 464	<sup>139</sup>	1.03 536	9.99 816	44		
17	8.96 417	<sup>137</sup>	8.96 602	<sup>138</sup>	1.03 398	9.99 815	43		
18	8.96 553	<sup>136</sup>	8.96 739	<sup>137</sup>	1.03 261	9.99 814	42		
19	8.96 689	<sup>136</sup>	8.96 877	<sup>138</sup>	1.03 123	9.99 813	41		
20	8.96 825	<sup>136</sup>	8.97 013	<sup>136</sup>	1.02 987	9.99 812	<b>40</b>		
21	8.96 960	<sup>135</sup>	8.97 150	<sup>137</sup>	1.02 850	9.99 810	39		
22	8.97 095	<sup>135</sup>	8.97 285	<sup>135</sup>	1.02 715	9.99 809	38	<sup>145</sup> 2.42	
23	8.97 229	<sup>134</sup>	8.97 421	<sup>136</sup>	1.02 579	9.99 808	37	<sup>144</sup> 2.40	
24	8.97 363	<sup>134</sup>	8.97 556	<sup>135</sup>	1.02 444	9.99 807	36	<sup>143</sup> 2.38	
25	8.97 496	<sup>133</sup>	8.97 691	<sup>135</sup>	1.02 309	9.99 806	35	<sup>142</sup> 2.37	
26	8.97 629	<sup>133</sup>	8.97 825	<sup>134</sup>	1.02 175	9.99 804	34	<sup>141</sup> 2.35	
27	8.97 762	<sup>133</sup>	8.97 959	<sup>134</sup>	1.02 041	9.99 803	33	<sup>140</sup> 2.33	
28	8.97 894	<sup>132</sup>	8.98 092	<sup>133</sup>	1.01 908	9.99 802	32	<sup>139</sup> 2.32	
29	8.98 026	<sup>132</sup>	8.98 225	<sup>133</sup>	1.01 775	9.99 801	31	<sup>138</sup> 2.30	
30	8.98 157	<sup>131</sup>	8.98 358	<sup>133</sup>	1.01 642	9.99 800	<b>30</b>	<sup>137</sup> 2.28	
31	8.98 288	<sup>131</sup>	8.98 490	<sup>132</sup>	1.01 510	9.99 798	29	<sup>136</sup> 2.27	
32	8.98 419	<sup>131</sup>	8.98 622	<sup>132</sup>	1.01 378	9.99 797	28	<sup>135</sup> 2.25	
33	8.98 549	<sup>130</sup>	8.98 753	<sup>131</sup>	1.01 247	9.99 796	27	<sup>134</sup> 2.23	
34	8.98 679	<sup>130</sup>	8.98 884	<sup>131</sup>	1.01 116	9.99 795	26	<sup>133</sup> 2.22	
35	8.98 808	<sup>129</sup>	8.99 015	<sup>131</sup>	1.00 985	9.99 793	25	<sup>132</sup> 2.20	
36	8.98 937	<sup>129</sup>	8.99 145	<sup>130</sup>	1.00 855	9.99 792	24	<sup>131</sup> 2.18	
37	8.99 066	<sup>129</sup>	8.99 275	<sup>130</sup>	1.00 725	9.99 791	23	<sup>130</sup> 2.17	
38	8.99 194	<sup>128</sup>	8.99 405	<sup>129</sup>	1.00 595	9.99 790	22	<sup>129</sup> 2.15	
39	8.99 322	<sup>128</sup>	8.99 534	<sup>128</sup>	1.00 466	9.99 788	21	<sup>128</sup> 2.13	
40	8.99 450	<sup>127</sup>	8.99 662	<sup>127</sup>	1.00 338	9.99 787	<b>20</b>	<sup>127</sup> 2.12	
41	8.99 577	<sup>127</sup>	8.99 791	<sup>128</sup>	1.00 209	9.99 786	19	<sup>126</sup> 2.10	
42	8.99 704	<sup>126</sup>	8.99 919	<sup>127</sup>	1.00 081	9.99 785	18	<sup>125</sup> 2.08	
43	8.99 830	<sup>126</sup>	9.00 046	<sup>128</sup>	0.99 954	9.99 783	17	<sup>124</sup> 2.07	
44	8.99 956	<sup>126</sup>	9.00 174	<sup>127</sup>	0.99 826	9.99 782	16	<sup>123</sup> 2.05	
45	9.00 082	<sup>125</sup>	9.00 301	<sup>126</sup>	0.99 699	9.99 781	15	<sup>122</sup> 2.03	
46	9.00 207	<sup>125</sup>	9.00 427	<sup>126</sup>	0.99 573	9.99 780	14	<sup>121</sup> 2.02	
47	9.00 332	<sup>124</sup>	9.00 553	<sup>126</sup>	0.99 447	9.99 778	13	<sup>120</sup> 2.00	
48	9.00 456	<sup>124</sup>	9.00 679	<sup>126</sup>	0.99 321	9.99 777	12		
49	9.00 581	<sup>123</sup>	9.00 805	<sup>125</sup>	0.99 195	9.99 776	11		
50	9.00 704	<sup>123</sup>	9.00 930	<sup>125</sup>	0.99 070	9.99 775	<b>10</b>		
51	9.00 828	<sup>124</sup>	9.01 055	<sup>124</sup>	0.98 945	9.99 773	9		
52	9.00 951	<sup>123</sup>	9.01 179	<sup>124</sup>	0.98 821	9.99 772	8		
53	9.01 074	<sup>123</sup>	9.01 303	<sup>124</sup>	0.98 697	9.99 771	7		
54	9.01 196	<sup>122</sup>	9.01 427	<sup>124</sup>	0.98 573	9.99 769	6		
55	9.01 318	<sup>122</sup>	9.01 550	<sup>123</sup>	0.98 450	9.99 768	5		
56	9.01 440	<sup>121</sup>	9.01 673	<sup>123</sup>	0.98 327	9.99 767	4		
57	9.01 561	<sup>121</sup>	9.01 796	<sup>122</sup>	0.98 204	9.99 765	3		
58	9.01 682	<sup>121</sup>	9.01 918	<sup>122</sup>	0.98 082	9.99 764	2		
59	9.01 803	<sup>120</sup>	9.02 040	<sup>122</sup>	0.97 960	9.99 763	1		
60	9.01 923		9.02 162	<sup>122</sup>	0.97 838	9.99 761	<b>0</b>		
	log cos	d.	log cot	c. d.	log tan	log sin	'	Prop. Pts.	

\*174°      264°      \*354°

**84°**

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

6°

\*96°

186°

\*276°

'	log sin	d.	log tan	c. d.	log cot	log cos		Prop. Pts.			
0	9.01 923		9.02 162		0.97 838	9.99 761	60				
1	9.02 043	120	9.02 283	121	0.97 717	9.99 760	59				
2	9.02 163	120	9.02 404	121	0.97 596	9.99 759	58				
3	9.02 283	120	9.02 525	121	0.97 475	9.99 757	57	"	121	120	119
4	9.02 402	119	9.02 645	120	0.97 355	9.99 756	56	6	12.1	12.0	11.9
5	9.02 520	118	9.02 766	121	0.97 234	9.99 755	55	7	14.1	14.0	13.9
6	9.02 639	119	9.02 885	120	0.97 115	9.99 753	54	8	16.1	16.0	15.9
7	9.02 757	118	9.03 005	119	0.96 995	9.99 752	53	9	18.2	18.0	17.8
8	9.02 874	117	9.03 124	120	0.96 876	9.99 751	52	10	20.2	20.0	19.8
9	9.02 992	118	9.03 242	119	0.96 758	9.99 749	51	20	40.3	40.0	39.7
10	9.03 109	117	9.03 361	118	0.96 639	9.99 748	50	30	60.5	60.0	59.5
11	9.03 226	116	9.03 479	118	0.96 521	9.99 747	49	40	80.7	80.0	79.3
12	9.03 342	116	9.03 597	117	0.96 403	9.99 745	48	50	100.8	100.0	99.2
13	9.03 458	116	9.03 714	118	0.96 286	9.99 744	47				
14	9.03 574	116	9.03 832	116	0.96 168	9.99 742	46	"	118	117	116
15	9.03 690		9.03 948		0.96 052	9.99 741	45	6	11.8	11.7	11.6
16	9.03 805	115	9.04 065	117	0.95 935	9.99 740	44	7	13.8	13.6	13.5
17	9.03 920	115	9.04 181	116	0.95 819	9.99 738	43	8	15.7	15.6	15.5
18	9.04 034	114	9.04 297	116	0.95 703	9.99 737	42	9	17.7	17.6	17.4
19	9.04 149	115	9.04 413	116	0.95 587	9.99 736	41	10	19.7	19.5	19.3
20	9.04 262	113	9.04 528	115	0.95 472	9.99 734	40	20	39.3	39.0	38.7
21	9.04 376	114	9.04 643	115	0.95 357	9.99 733	39	30	59.0	58.5	58.0
22	9.04 490	114	9.04 758	115	0.95 242	9.99 731	38	40	78.7	78.0	77.3
23	9.04 603	113	9.04 873	114	0.95 127	9.99 730	37	50	98.3	97.5	96.7
24	9.04 715	113	9.04 987	114	0.95 013	9.99 728	36	"	115	114	113
25	9.04 828		9.05 101		0.94 899	9.99 727	35	6	11.5	11.4	11.3
26	9.04 940	112	9.05 214	113	0.94 786	9.99 726	34	7	13.4	13.3	13.2
27	9.05 052	112	9.05 328	114	0.94 672	9.99 724	33	8	15.3	15.2	15.1
28	9.05 164	112	9.05 441	113	0.94 559	9.99 723	32	9	17.2	17.1	17.0
29	9.05 275	111	9.05 553	112	0.94 447	9.99 721	31	10	19.2	19.0	18.8
30	9.05 386	111	9.05 666	113	0.94 334	9.99 720	30	20	38.3	38.0	37.7
31	9.05 497	110	9.05 778	112	0.94 222	9.99 718	29	30	57.5	57.0	56.5
32	9.05 607	110	9.05 890	112	0.94 110	9.99 717	28	40	76.7	76.0	75.3
33	9.05 717	110	9.06 002	111	0.93 998	9.99 716	27	50	95.8	95.0	94.2
34	9.05 827	110	9.06 113	111	0.93 887	9.99 714	26	"	112	111	110
35	9.05 937		9.06 224		0.93 776	9.99 713	25	6	11.2	11.1	11.0
36	9.06 046	109	9.06 335	111	0.93 665	9.99 711	24	7	13.1	13.0	12.8
37	9.06 155	109	9.06 445	110	0.93 555	9.99 710	23	8	14.9	14.8	14.7
38	9.06 264	109	9.06 556	111	0.93 444	9.99 708	22	9	16.8	16.6	16.5
39	9.06 372	108	9.06 666	110	0.93 334	9.99 707	21	10	18.7	18.5	18.3
40	9.06 481	108	9.06 775	109	0.93 225	9.99 705	20	20	37.3	37.0	36.7
41	9.06 589	108	9.06 885	110	0.93 115	9.99 704	19	30	56.0	55.5	55.0
42	9.06 696	107	9.06 994	109	0.93 006	9.99 702	18	40	74.7	74.0	73.3
43	9.06 804	107	9.07 103	108	0.92 897	9.99 701	17	50	93.3	92.5	91.7
44	9.06 911	107	9.07 211	109	0.92 789	9.99 699	16	"	109	108	107
45	9.07 018		9.07 320		0.92 680	9.99 698	15	6	10.9	10.8	10.7
46	9.07 124	106	9.07 428	108	0.92 572	9.99 696	14	7	12.7	12.6	12.5
47	9.07 231	106	9.07 536	108	0.92 464	9.99 695	13	8	14.5	14.4	14.3
48	9.07 337	105	9.07 643	107	0.92 357	9.99 693	12	9	16.4	16.2	16.0
49	9.07 442	106	9.07 751	108	0.92 249	9.99 692	11	10	18.2	18.0	17.8
50	9.07 548		9.07 858		0.92 142	9.99 690	10	20	36.3	36.0	35.7
51	9.07 653	105	9.07 964	106	0.92 036	9.99 689	9	30	54.5	54.0	53.5
52	9.07 758	105	9.08 071	106	0.91 929	9.99 687	8	40	72.7	72.0	71.3
53	9.07 863	105	9.08 177	106	0.91 823	9.99 686	7	50	90.8	90.0	89.2
54	9.07 968	104	9.08 283	106	0.91 717	9.99 684	6	"	106	105	104
55	9.08 072		9.08 389		0.91 611	9.99 683	5	6	10.6	10.5	10.4
56	9.08 176	104	9.08 495	106	0.91 505	9.99 681	4	7	12.4	12.2	12.1
57	9.08 280	104	9.08 600	105	0.91 400	9.99 680	3	8	14.1	14.0	13.9
58	9.08 383	103	9.08 705	105	0.91 295	9.99 678	2	9	15.9	15.8	15.6
59	9.08 486	103	9.08 810	105	0.91 190	9.99 677	1	10	17.7	17.5	17.3
60	9.08 589		9.08 914		0.91 086	9.99 675	0	20	35.3	35.0	34.7
	log cos	d.	log cot	c. d.	log tan	log sin	'	30	53.0	52.5	52.0
								40	70.7	70.0	69.3
								50	88.3	87.5	86.7

\*173°

263°

\*353°

83°

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

7°							*97°	187°	*277°	
'	log sin	d.	log tan	c. d.	log cot	log cos		Prop. Pts.		
0	9.08 589		9.08 914		0.91 086	9.99 675	<b>60</b>			
1	9.08 692	103	9.09 019	105	0.90 981	9.99 674	59			
2	9.08 795	103	9.09 123	104	0.90 877	9.99 672	58			
3	9.08 897	102	9.09 227	104	0.90 773	9.99 670	57			" 105 104 103
4	9.08 999	102	9.09 330	103	0.90 670	9.99 669	56	6	10.5	10.4 10.3
5	9.09 101		9.09 434		0.90 566	9.99 667	55	7	12.3	12.1 12.0
6	9.09 202	101	9.09 537	103	0.90 463	9.99 666	54	8	14.0	13.9 13.7
7	9.09 304	102	9.09 640	103	0.90 360	9.99 664	53	9	15.8	15.6 15.4
8	9.09 405	101	9.09 742	102	0.90 258	9.99 663	52	10	17.5	17.3 17.2
9	9.09 506	101	9.09 845	103	0.90 155	9.99 661	51	20	35.0	34.7 34.3
10	9.09 605	100	9.09 947	102	0.90 053	9.99 659	<b>50</b>	30	52.5	52.0 51.5
11	9.09 707	100	9.10 049	101	0.89 951	9.99 658	49	40	70.0	69.3 68.7
12	9.09 807	100	9.10 150	101	0.89 850	9.99 656	48	50	87.5	86.7 85.8
13	9.09 907	99	9.10 252	102	0.89 748	9.99 655	47			
14	9.10 006	100	9.10 353	101	0.89 647	9.99 653	46			" 102 101 100
15	9.10 105		9.10 454		0.89 546	9.99 651	45	6	10.2	10.1 10.0
16	9.10 205	99	9.10 555	101	0.89 445	9.99 650	44	7	11.9	11.8 11.7
17	9.10 304	99	9.10 656	101	0.89 344	9.99 648	43	8	13.6	13.5 13.3
18	9.10 402	98	9.10 756	100	0.89 244	9.99 647	42	9	15.3	15.2 15.0
19	9.10 501	98	9.10 856	100	0.89 144	9.99 645	41	10	17.0	16.8 16.7
20	9.10 599		9.10 956		0.89 044	9.99 643	<b>40</b>	20	34.0	33.7 33.3
21	9.10 697	98	9.11 056	100	0.88 944	9.99 642	39	30	51.0	50.5 50.0
22	9.10 795	98	9.11 155	99	0.88 845	9.99 640	38	40	68.0	67.3 66.7
23	9.10 893	98	9.11 254	99	0.88 746	9.99 638	37	50	85.0	84.2 83.3
24	9.10 990	97	9.11 353	99	0.88 647	9.99 637	36			
25	9.11 087		9.11 452		0.88 548	9.99 635	35			" 99 98 97
26	9.11 184	97	9.11 551	99	0.88 449	9.99 633	34	6	9.9	9.8 9.7
27	9.11 281	97	9.11 649	98	0.88 351	9.99 632	33	7	11.6	11.4 11.3
28	9.11 377	96	9.11 747	98	0.88 253	9.99 630	32	8	13.2	13.1 12.9
29	9.11 474	96	9.11 845	98	0.88 155	9.99 629	31	9	14.8	14.7 14.6
30	9.11 570		9.11 943		0.88 057	9.99 627	<b>30</b>	10	16.5	16.3 16.2
31	9.11 666	96	9.12 040	97	0.87 960	9.99 625	29	20	33.0	32.7 32.3
32	9.11 761	95	9.12 138	98	0.87 862	9.99 624	28	30	49.5	49.0 48.5
33	9.11 857	96	9.12 235	97	0.87 765	9.99 622	27	40	66.0	65.3 64.7
34	9.11 952	95	9.12 332	96	0.87 668	9.99 620	26	50	82.5	81.7 80.8
35	9.12 047		9.12 428		0.87 572	9.99 618	25			
36	9.12 142	95	9.12 525	97	0.87 475	9.99 617	24			" 96 95 94
37	9.12 236	94	9.12 621	96	0.87 379	9.99 615	23	6	9.6	9.5 9.4
38	9.12 331	95	9.12 717	96	0.87 283	9.99 613	22	7	11.2	11.1 11.0
39	9.12 425	94	9.12 813	96	0.87 187	9.99 612	21	8	12.8	12.7 12.5
40	9.12 519		9.12 909		0.87 091	9.99 610	<b>20</b>	9	14.4	14.2 14.1
41	9.12 612	93	9.13 004	95	0.86 996	9.99 608	19	10	16.0	15.8 15.7
42	9.12 706	94	9.13 099	95	0.86 901	9.99 607	18	20	32.0	31.7 31.3
43	9.12 799	93	9.13 194	95	0.86 806	9.99 605	17	30	48.0	47.5 47.0
44	9.12 892	93	9.13 289	95	0.86 711	9.99 603	16	40	64.0	63.3 62.7
45	9.12 985		9.13 384		0.86 616	9.99 601	15	50	80.0	79.2 78.3
46	9.13 078	93	9.13 478	94	0.86 522	9.99 600	14			
47	9.13 171	93	9.13 573	95	0.86 427	9.99 598	13			" 93 92 91
48	9.13 263	92	9.13 667	94	0.86 333	9.99 596	12	6	9.3	9.2 9.1
49	9.13 355	92	9.13 761	94	0.86 239	9.99 595	11	7	10.9	10.7 10.6
50	9.13 447		9.13 854		0.86 146	9.99 593	<b>10</b>	8	12.4	12.3 12.1
51	9.13 539	92	9.13 948	94	0.86 052	9.99 591	9	9	14.0	13.8 13.6
52	9.13 630	91	9.14 041	93	0.85 959	9.99 589	8	10	15.5	15.3 15.2
53	9.13 722	92	9.14 134	93	0.85 866	9.99 588	7	20	31.0	30.7 30.3
54	9.13 813	91	9.14 227	93	0.85 773	9.99 586	6	30	46.5	46.0 45.5
55	9.13 904		9.14 320		0.85 680	9.99 584	5	40	62.0	61.3 60.7
56	9.13 994	90	9.14 412	92	0.85 588	9.99 582	4	50	77.5	76.7 75.8
57	9.14 085	91	9.14 504	92	0.85 496	9.99 581	3			
58	9.14 175	90	9.14 597	93	0.85 403	9.99 579	2			" 90 2 1
59	9.14 266	91	9.14 688	91	0.85 312	9.99 577	1	6	9.0	0.2 0.1
60	9.14 356	90	9.14 780	92	0.85 220	9.99 575	<b>0</b>	7	10.5	0.2 0.1
	log cos	d.	log cot	c. d.	log tan	log sin	'			Prop. Pts.

\*172°

262°

\*352°

82°

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

		8°						*98°	188°	*278°
'	log sin	d.	log tan	c. d.	log cot	log cos		Prop. Pts.		
0	9.14 356		9.14 780		0.85 220	9.99 575	60			
1	9.14 445	89	9.14 872	92	0.85 128	9.99 574	59			
2	9.14 535	90	9.14 963	91	0.85 037	9.99 572	58			
3	9.14 624	89	9.15 054	91	0.84 946	9.99 570	57			
4	9.14 714	90	9.15 145	91	0.84 855	9.99 568	56			
5	9.14 803	89	9.15 236	91	0.84 764	9.99 566	55			
6	9.14 891	88	9.15 327	91	0.84 673	9.99 565	54			
7	9.14 980	89	9.15 417	90	0.84 583	9.99 563	53			
8	9.15 069	88	9.15 508	91	0.84 492	9.99 561	52			
9	9.15 157	88	9.15 598	90	0.84 402	9.99 559	51			
10	9.15 245	88	9.15 688	89	0.84 312	9.99 557	50			
11	9.15 333	88	9.15 777	89	0.84 223	9.99 556	49			
12	9.15 421	87	9.15 867	89	0.84 133	9.99 554	48			
13	9.15 508	88	9.15 956	89	0.84 044	9.99 552	47			
14	9.15 596	87	9.16 046	89	0.83 954	9.99 550	46			
15	9.15 683	87	9.16 135	89	0.83 865	9.99 548	45			
16	9.15 770	87	9.16 224	88	0.83 776	9.99 546	44			
17	9.15 857	87	9.16 312	88	0.83 688	9.99 545	43			
18	9.15 944	86	9.16 401	88	0.83 599	9.99 543	42			
19	9.16 030	86	9.16 489	88	0.83 511	9.99 541	41			
20	9.16 116	87	9.16 577	88	0.83 423	9.99 539	40			
21	9.16 203	86	9.16 665	88	0.83 335	9.99 537	39			
22	9.16 289	85	9.16 753	88	0.83 247	9.99 535	38			
23	9.16 374	86	9.16 841	87	0.83 159	9.99 533	37			
24	9.16 460	85	9.16 928	88	0.83 072	9.99 532	36			
25	9.16 545	86	9.17 016	87	0.82 984	9.99 530	35			
26	9.16 631	85	9.17 103	87	0.82 897	9.99 528	34			
27	9.16 716	85	9.17 190	87	0.82 810	9.99 526	33			
28	9.16 801	85	9.17 277	86	0.82 723	9.99 524	32			
29	9.16 886	84	9.17 363	87	0.82 637	9.99 522	31			
30	9.16 970	85	9.17 450	86	0.82 550	9.99 520	30			
31	9.17 055	84	9.17 536	86	0.82 464	9.99 518	29			
32	9.17 139	84	9.17 622	86	0.82 378	9.99 517	28			
33	9.17 223	84	9.17 708	86	0.82 292	9.99 515	27			
34	9.17 307	84	9.17 794	86	0.82 206	9.99 513	26			
35	9.17 391	83	9.17 880	85	0.82 120	9.99 511	25			
36	9.17 474	84	9.17 965	86	0.82 035	9.99 509	24			
37	9.17 558	83	9.18 051	85	0.81 949	9.99 507	23			
38	9.17 641	83	9.18 136	85	0.81 864	9.99 505	22			
39	9.17 724	83	9.18 221	85	0.81 779	9.99 503	21			
40	9.17 807	83	9.18 306	85	0.81 694	9.99 501	20			
41	9.17 890	83	9.18 391	84	0.81 609	9.99 499	19			
42	9.17 973	82	9.18 475	85	0.81 525	9.99 497	18			
43	9.18 055	82	9.18 560	84	0.81 440	9.99 495	17			
44	9.18 137	83	9.18 644	84	0.81 356	9.99 494	16			
45	9.18 220	82	9.18 728	84	0.81 272	9.99 492	15			
46	9.18 302	81	9.18 812	84	0.81 188	9.99 490	14			
47	9.18 383	82	9.18 896	83	0.81 104	9.99 488	13			
48	9.18 465	82	9.18 979	84	0.81 021	9.99 486	12			
49	9.18 547	81	9.19 063	83	0.80 937	9.99 484	11			
50	9.18 628	81	9.19 146	83	0.80 854	9.99 482	10			
51	9.18 709	81	9.19 229	83	0.80 771	9.99 480	9			
52	9.18 790	81	9.19 312	83	0.80 688	9.99 478	8			
53	9.18 871	81	9.19 395	83	0.80 605	9.99 476	7			
54	9.18 952	81	9.19 478	83	0.80 522	9.99 474	6			
55	9.19 033	80	9.19 561	82	0.80 439	9.99 472	5			
56	9.19 113	80	9.19 643	82	0.80 357	9.99 470	4			
57	9.19 193	80	9.19 725	82	0.80 275	9.99 468	3			
58	9.19 273	80	9.19 807	82	0.80 193	9.99 466	2			
59	9.19 353	80	9.19 889	82	0.80 111	9.99 464	1			
60	9.19 433		9.19 971		0.80 029	9.99 462	0			
	log cos	d.	log cot	c. d.	log tan	log sin	'	Prop. Pts.		

\*171° 261° \*351°

81°

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

<b>9°</b>						*99°	189°	*279°
'	log sin	d.	log tan	c. d.	log cot	log cos	Prop. Pts.	
0	9.19 433		9.19 971		0.80 029	9.99 462	<b>60</b>	
1	9.19 513	80	9.20 053	82	0.79 947	9.99 460	59	
2	9.19 592	79	9.20 134	81	0.79 866	9.99 458	58	
3	9.19 672	80	9.20 216	82	0.79 784	9.99 456	57	
4	9.19 751	79	9.20 297	81	0.79 703	9.99 454	56	
5	9.19 830	79	9.20 378	81	0.79 622	9.99 452	55	
6	9.19 909	79	9.20 459	81	0.79 541	9.99 450	54	
7	9.19 988	79	9.20 540	81	0.79 460	9.99 448	53	" 80 79 78
8	9.20 067	79	9.20 621	80	0.79 379	9.99 446	52	6 8.0 7.9 7.8
9	9.20 145	78	9.20 701	80	0.79 299	9.99 444	51	7 9.3 9.2 9.1
10	9.20 223	78	9.20 782	80	0.79 218	9.99 442	<b>50</b>	8 10.7 10.5 10.4
11	9.20 302	78	9.20 862	80	0.79 138	9.99 440	49	9 12.0 11.9 11.7
12	9.20 380	78	9.20 942	80	0.79 058	9.99 438	48	10 13.3 13.2 13.0
13	9.20 458	77	9.21 022	80	0.78 978	9.99 436	47	20 26.7 26.3 26.0
14	9.20 535	78	9.21 102	80	0.78 898	9.99 434	46	30 40.0 39.5 39.0
15	9.20 613	78	9.21 182	79	0.78 818	9.99 432	45	40 53.3 52.7 52.0
16	9.20 691	77	9.21 261	80	0.78 739	9.99 429	44	50 66.7 65.8 65.0
17	9.20 768	77	9.21 341	80	0.78 659	9.99 427	43	
18	9.20 845	77	9.21 420	79	0.78 580	9.99 425	42	
19	9.20 922	77	9.21 499	79	0.78 501	9.99 423	41	
20	9.20 999	77	9.21 578	79	0.78 422	9.99 421	<b>40</b>	" 77 76 75
21	9.21 076	77	9.21 657	79	0.78 343	9.99 419	39	6 7.7 7.6 7.5
22	9.21 153	77	9.21 736	79	0.78 264	9.99 417	38	7 9.0 8.9 8.8
23	9.21 229	77	9.21 814	79	0.78 186	9.99 415	37	8 10.3 10.1 10.0
24	9.21 306	76	9.21 893	78	0.78 107	9.99 413	36	9 11.6 11.4 11.3
25	9.21 382	76	9.21 971	78	0.78 029	9.99 411	35	10 12.8 12.7 12.5
26	9.21 458	76	9.22 049	78	0.77 951	9.99 409	34	20 25.7 25.3 25.0
27	9.21 534	76	9.22 127	78	0.77 873	9.99 407	33	30 38.5 38.0 37.5
28	9.21 610	75	9.22 205	78	0.77 795	9.99 404	32	40 51.3 50.7 50.0
29	9.21 685	76	9.22 283	78	0.77 717	9.99 402	31	50 64.2 63.3 62.5
30	9.21 761	75	9.22 361	77	0.77 639	9.99 400	<b>30</b>	
31	9.21 836	76	9.22 438	78	0.77 562	9.99 398	29	
32	9.21 912	75	9.22 516	77	0.77 484	9.99 396	28	
33	9.21 987	75	9.22 593	77	0.77 407	9.99 394	27	" 74 73 72
34	9.22 062	75	9.22 670	77	0.77 330	9.99 392	26	6 7.4 7.3 7.2
35	9.22 137	74	9.22 747	77	0.77 253	9.99 390	25	7 8.6 8.5 8.4
36	9.22 211	75	9.22 824	77	0.77 176	9.99 388	24	8 9.9 9.7 9.6
37	9.22 286	75	9.22 901	76	0.77 099	9.99 385	23	9 11.1 11.0 10.8
38	9.22 361	74	9.22 977	76	0.77 023	9.99 383	22	10 12.3 12.2 12.0
39	9.22 435	74	9.23 054	76	0.76 946	9.99 381	21	20 24.7 24.3 24.0
40	9.22 509	74	9.23 130	76	0.76 870	9.99 379	<b>20</b>	30 37.0 36.5 36.0
41	9.22 583	74	9.23 206	77	0.76 794	9.99 377	19	40 49.3 48.7 48.0
42	9.22 657	74	9.23 283	76	0.76 717	9.99 375	18	50 61.7 60.8 60.0
43	9.22 731	74	9.23 359	76	0.76 641	9.99 372	17	
44	9.22 805	73	9.23 435	75	0.76 565	9.99 370	16	
45	9.22 878	74	9.23 510	76	0.76 490	9.99 368	15	" 71 3 2
46	9.22 952	73	9.23 586	75	0.76 414	9.99 366	14	6 7.1 0.3 0.2
47	9.23 025	73	9.23 661	75	0.76 339	9.99 364	13	7 8.3 0.4 0.2
48	9.23 098	73	9.23 737	75	0.76 263	9.99 362	12	8 9.5 0.4 0.3
49	9.23 171	73	9.23 812	75	0.76 188	9.99 359	11	9 10.7 0.5 0.3
50	9.23 244	73	9.23 887	75	0.76 113	9.99 357	<b>10</b>	10 11.8 0.5 0.3
51	9.23 317	73	9.23 962	75	0.76 038	9.99 355	9	20 23.7 1.0 0.7
52	9.23 390	72	9.24 037	75	0.75 963	9.99 353	8	30 35.5 1.5 1.0
53	9.23 462	72	9.24 112	75	0.75 888	9.99 351	7	40 47.3 2.0 1.3
54	9.23 535	72	9.24 186	74	0.75 814	9.99 348	6	50 59.2 2.5 1.7
55	9.23 607	72	9.24 261	75	0.75 739	9.99 346	5	
56	9.23 679	73	9.24 335	74	0.75 665	9.99 344	4	
57	9.23 752	72	9.24 410	75	0.75 590	9.99 342	3	
58	9.23 823	71	9.24 484	74	0.75 516	9.99 340	2	
59	9.23 895	72	9.24 558	74	0.75 442	9.99 337	1	
60	9.23 967	72	9.24 632	74	0.75 368	9.99 335	<b>0</b>	
	log cos	d.	log cot	c. d.	log tan	log sin	'	Prop. Pts.

\*170°

260°

\*350°

**80°**

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

10°

\*100°

190°

\*280°

	log sin	d.	log tan	c. d.	log cot	log cos		Prop. Pts.
0	9.23 967	72	9.24 632	74	0.75 368	9.99 335	60	
1	9.24 039	71	9.24 706	73	0.75 294	9.99 333	59	
2	9.24 110	71	9.24 779	74	0.75 221	9.99 331	58	
3	9.24 181	72	9.24 853	73	0.75 147	9.99 328	57	
4	9.24 253	71	9.24 926	74	0.75 074	9.99 326	56	
5	9.24 324	71	9.25 000	73	0.75 000	9.99 324	55	
6	9.24 395	71	9.25 073	73	0.74 927	9.99 322	54	" 74 73 72
7	9.24 466	70	9.25 146	73	0.74 854	9.99 319	53	6 7.4 7.3 7.2
8	9.24 536	71	9.25 219	73	0.74 781	9.99 317	52	7 8.6 8.5 8.4
9	9.24 607	70	9.25 292	73	0.74 708	9.99 315	51	8 9.9 9.7 9.6
10	9.24 677	71	9.25 365	73	0.74 635	9.99 313	50	9 11.1 11.0 10.8
11	9.24 748	70	9.25 437	72	0.74 563	9.99 310	49	10 12.3 12.2 12.0
12	9.24 818	70	9.25 510	72	0.74 490	9.99 308	48	20 24.7 24.3 24.0
13	9.24 888	70	9.25 582	72	0.74 418	9.99 306	47	30 37.0 36.5 36.0
14	9.24 958	70	9.25 655	72	0.74 345	9.99 304	46	40 49.3 48.7 48.0
15	9.25 028	70	9.25 727	72	0.74 273	9.99 301	45	50 61.7 60.8 60.0
16	9.25 098	70	9.25 799	72	0.74 201	9.99 299	44	
17	9.25 168	69	9.25 871	72	0.74 129	9.99 297	43	
18	9.25 237	70	9.25 943	72	0.74 057	9.99 294	42	
19	9.25 307	69	9.26 015	71	0.73 985	9.99 292	41	
20	9.25 376	69	9.26 086	72	0.73 914	9.99 290	40	" 71 70 69
21	9.25 445	69	9.26 158	71	0.73 842	9.99 288	39	6 7.1 7.0 6.9
22	9.25 514	69	9.26 229	72	0.73 771	9.99 285	38	7 8.3 8.2 8.0
23	9.25 583	69	9.26 301	71	0.73 699	9.99 283	37	8 9.5 9.3 9.2
24	9.25 652	69	9.26 372	71	0.73 628	9.99 281	36	9 10.7 10.5 10.4
25	9.25 721	69	9.26 443	71	0.73 557	9.99 278	35	10 11.8 11.7 11.5
26	9.25 790	68	9.26 514	71	0.73 486	9.99 276	34	20 23.7 23.3 23.0
27	9.25 858	69	9.26 585	71	0.73 415	9.99 274	33	30 35.5 35.0 34.5
28	9.25 927	68	9.26 655	70	0.73 345	9.99 271	32	40 47.3 46.7 46.0
29	9.25 995	68	9.26 726	71	0.73 274	9.99 269	31	50 59.2 58.3 57.5
30	9.26 063	68	9.26 797	70	0.73 203	9.99 267	30	
31	9.26 131	68	9.26 867	70	0.73 133	9.99 264	29	
32	9.26 199	68	9.26 937	71	0.73 063	9.99 262	28	
33	9.26 267	68	9.27 008	70	0.72 992	9.99 260	27	
34	9.26 335	68	9.27 078	70	0.72 922	9.99 257	26	" 68 67 66
35	9.26 403	67	9.27 148	70	0.72 852	9.99 255	25	6 6.8 6.7 6.6
36	9.26 470	68	9.27 218	70	0.72 782	9.99 252	24	7 7.9 7.8 7.7
37	9.26 538	67	9.27 288	70	0.72 712	9.99 250	23	8 9.1 8.9 8.8
38	9.26 605	67	9.27 357	69	0.72 643	9.99 248	22	9 10.2 10.0 9.9
39	9.26 672	67	9.27 427	70	0.72 573	9.99 245	21	10 11.3 11.2 11.0
40	9.26 739	67	9.27 496	69	0.72 504	9.99 243	20	20 22.7 22.3 22.0
41	9.26 806	67	9.27 566	70	0.72 434	9.99 241	19	30 34.0 33.5 33.0
42	9.26 873	67	9.27 635	69	0.72 365	9.99 238	18	40 45.3 44.7 44.0
43	9.26 940	67	9.27 704	69	0.72 296	9.99 236	17	50 56.7 55.8 55.0
44	9.27 007	66	9.27 773	69	0.72 227	9.99 233	16	
45	9.27 073	67	9.27 842	69	0.72 158	9.99 231	15	
46	9.27 140	66	9.27 911	69	0.72 089	9.99 229	14	
47	9.27 206	66	9.27 980	69	0.72 020	9.99 226	13	" 65 6 2
48	9.27 273	67	9.28 049	69	0.71 951	9.99 224	12	6 6.5 0.3 0.2
49	9.27 339	66	9.28 117	68	0.71 883	9.99 221	11	7 7.6 0.4 0.2
50	9.27 405	66	9.28 186	69	0.71 814	9.99 219	10	8 8.7 0.1 0.3
51	9.27 471	66	9.28 254	68	0.71 746	9.99 217	9	9 9.8 0.2 0.3
52	9.27 537	66	9.28 323	69	0.71 677	9.99 214	8	10 10.8 0.5 0.3
53	9.27 602	65	9.28 391	68	0.71 609	9.99 212	7	20 21.7 1.0 0.7
54	9.27 668	66	9.28 459	68	0.71 541	9.99 209	6	30 32.5 1.5 1.0
55	9.27 734	65	9.28 527	68	0.71 473	9.99 207	5	40 43.3 2.0 1.3
56	9.27 799	65	9.28 595	68	0.71 405	9.99 204	4	50 54.2 2.5 1.7
57	9.27 864	65	9.28 662	67	0.71 338	9.99 202	3	
58	9.27 930	66	9.28 730	68	0.71 270	9.99 200	2	
59	9.27 995	65	9.28 798	68	0.71 202	9.99 197	1	
60	9.28 060	65	9.28 865	67	0.71 135	9.99 195	0	
	log cos	d.	log cot	c. d.	log tan	log sin		Prop. Pts.

\*169°

259°

\*349°

79°

<b>11°</b>								*101°	191°	*281°	
'	log sin	d.	log tan	c. d.	log cot	log cos		Prop. Pts.			
0	9.28 060		9.28 865		0.71 135	9.99 195	<b>60</b>				
1	9.28 125	65	9.28 933	68	0.71 067	9.99 192	59				
2	9.28 190	65	9.29 000	67	0.71 000	9.99 190	58				
3	9.28 254	64	9.29 067	67	0.70 933	9.99 187	57				
4	9.28 319	65	9.29 134	67	0.70 866	9.99 185	56				
5	9.28 384		9.29 201		0.70 799	9.99 182	55				
6	9.28 448	64	9.29 268	67	0.70 732	9.99 180	54	"	68	67	66
7	9.28 512	64	9.29 335	67	0.70 665	9.99 177	53	6	6.8	6.7	6.6
8	9.28 577	65	9.29 402	67	0.70 598	9.99 175	52	7	7.9	7.8	7.7
9	9.28 641	64	9.29 468	66	0.70 532	9.99 172	51	8	9.1	8.9	8.8
10	9.28 705		9.29 535		0.70 465	9.99 170	<b>50</b>	9	10.2	10.0	9.9
11	9.28 769	64	9.29 601	66	0.70 399	9.99 167	49	10	11.3	11.2	11.0
12	9.28 833	64	9.29 668	67	0.70 332	9.99 165	48	20	22.7	22.3	22.0
13	9.28 896	63	9.29 734	66	0.70 266	9.99 162	47	30	34.0	33.5	33.0
14	9.28 960	64	9.29 800	66	0.70 200	9.99 160	46	40	45.3	44.7	44.0
15	9.29 024		9.29 865		0.70 134	9.99 157	45	50	56.7	55.8	55.0
16	9.29 087	63	9.29 932	66	0.70 068	9.99 155	44				
17	9.29 150	63	9.29 998	66	0.70 002	9.99 152	43				
18	9.29 214	64	9.30 064	66	0.69 936	9.99 150	42				
19	9.29 277	63	9.30 130	66	0.69 870	9.99 147	41				
20	9.29 340		9.30 195		0.69 805	9.99 145	<b>40</b>	"	65	64	63
21	9.29 403	63	9.30 261	66	0.69 739	9.99 142	39	6	6.5	6.4	6.3
22	9.29 466	63	9.30 326	65	0.69 674	9.99 140	38	7	7.6	7.5	7.4
23	9.29 529	63	9.30 391	65	0.69 609	9.99 137	37	8	8.7	8.5	8.4
24	9.29 591	62	9.30 457	66	0.69 543	9.99 135	36	9	9.8	9.6	9.4
25	9.29 654	63	9.30 522	65	0.69 478	9.99 132	35	10	10.8	10.7	10.5
26	9.29 716	62	9.30 587	65	0.69 413	9.99 130	34	20	21.7	21.3	21.0
27	9.29 779	63	9.30 652	65	0.69 348	9.99 127	33	30	32.5	32.0	31.5
28	9.29 841	62	9.30 717	65	0.69 283	9.99 124	32	40	43.3	42.7	42.0
29	9.29 903	62	9.30 782	65	0.69 218	9.99 122	31	50	54.2	53.3	52.5
30	9.29 966	63	9.30 846	64	0.69 154	9.99 119	<b>30</b>				
31	9.30 028	62	9.30 911	65	0.69 089	9.99 117	29				
32	9.30 090	62	9.30 975	64	0.69 025	9.99 114	28				
33	9.30 151	61	9.31 040	65	0.68 960	9.99 112	27				
34	9.30 213	62	9.31 104	64	0.68 896	9.99 109	26	"	62	61	60
35	9.30 275		9.31 168		0.68 832	9.99 106	25	6	6.2	6.1	6.0
36	9.30 336	61	9.31 233	65	0.68 767	9.99 104	24	7	7.2	7.1	7.0
37	9.30 398	62	9.31 297	64	0.68 703	9.99 101	23	8	8.3	8.1	8.0
38	9.30 459	61	9.31 361	64	0.68 639	9.99 099	22	9	9.3	9.2	9.0
39	9.30 521	62	9.31 425	64	0.68 575	9.99 096	21	10	10.3	10.2	10.0
40	9.30 582	61	9.31 489	64	0.68 511	9.99 093	<b>20</b>	20	20.7	20.3	20.0
41	9.30 643	61	9.31 552	63	0.68 448	9.99 091	19	30	31.0	30.5	30.0
42	9.30 704	61	9.31 616	64	0.68 384	9.99 088	18	40	41.3	40.7	40.0
43	9.30 765	61	9.31 679	63	0.68 321	9.99 086	17	50	51.7	50.8	50.0
44	9.30 826	61	9.31 743	64	0.68 257	9.99 083	16				
45	9.30 887		9.31 806		0.68 194	9.99 080	15				
46	9.30 947	60	9.31 870	64	0.68 130	9.99 078	14				
47	9.31 008	61	9.31 933	63	0.68 067	9.99 075	13	"	59	8	2
48	9.31 068	60	9.31 996	63	0.68 004	9.99 072	12	6	5.9	0.3	0.2
49	9.31 129	61	9.32 059	63	0.67 941	9.99 070	11	7	6.9	0.4	0.2
50	9.31 189		9.32 122		0.67 878	9.99 067	<b>10</b>	8	7.9	0.4	0.3
51	9.31 250	61	9.32 185	63	0.67 815	9.99 064	9	9	8.9	0.5	0.3
52	9.31 310	60	9.32 248	63	0.67 752	9.99 062	8	10	9.8	0.5	0.3
53	9.31 370	60	9.32 311	63	0.67 689	9.99 059	7	20	19.7	1.0	0.7
54	9.31 430	60	9.32 373	62	0.67 627	9.99 056	6	30	29.5	1.5	1.0
55	9.31 490		9.32 436		0.67 564	9.99 054	5	40	39.3	2.0	1.3
56	9.31 549	59	9.32 498	62	0.67 502	9.99 051	4	50	49.2	2.5	1.7
57	9.31 609	60	9.32 561	63	0.67 439	9.99 048	3				
58	9.31 669	60	9.32 623	62	0.67 377	9.99 046	2				
59	9.31 728	59	9.32 685	62	0.67 315	9.99 043	1				
60	9.31 788	60	9.32 747	62	0.67 253	9.99 040	<b>0</b>				
	log cos	d.	log cot	c. d.	log tan	log sin	'	Prop. Pts.			

\*168° 258° \*348°

**78°**



LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

12°

\*102°

192°

\*282°

'	log sin	d.	log tan	c. d.	log cot	log cos		Prop. Pts.
0	9.31 788		9.32 747		0.67 253	9.99 040	60	
1	9.31 847	59	9.32 810	63	0.67 190	9.99 038	59	
2	9.31 907	60	9.32 872	62	0.67 128	9.99 035	58	
3	9.31 966	59	9.32 933	61	0.67 067	9.99 032	57	
4	9.32 025	59	9.32 995	62	0.67 005	9.99 030	56	
5	9.32 084	59	9.33 057	62	0.66 943	9.99 027	55	
6	9.32 143	59	9.33 119	61	0.66 881	9.99 024	54	
7	9.32 202	59	9.33 180	62	0.66 820	9.99 022	53	
8	9.32 261	59	9.33 242	61	0.66 758	9.99 019	52	
9	9.32 319	58	9.33 303	62	0.66 697	9.99 016	51	
10	9.32 378	59	9.33 365	61	0.66 635	9.99 013	50	
11	9.32 437	58	9.33 426	61	0.66 574	9.99 011	49	
12	9.32 495	58	9.33 487	61	0.66 513	9.99 008	48	
13	9.32 553	58	9.33 548	61	0.66 452	9.99 005	47	
14	9.32 612	58	9.33 609	61	0.66 391	9.99 002	46	
15	9.32 670	58	9.33 670	61	0.66 330	9.99 000	45	
16	9.32 728	58	9.33 731	61	0.66 269	9.98 997	44	
17	9.32 786	58	9.33 792	61	0.66 208	9.98 994	43	
18	9.32 844	58	9.33 853	60	0.66 147	9.98 991	42	
19	9.32 902	58	9.33 913	61	0.66 087	9.98 989	41	
20	9.32 960	58	9.33 974	60	0.66 026	9.98 986	40	
21	9.33 018	57	9.34 034	61	0.65 966	9.98 983	39	
22	9.33 075	58	9.34 095	60	0.65 905	9.98 980	38	
23	9.33 133	57	9.34 155	60	0.65 845	9.98 978	37	
24	9.33 190	58	9.34 215	61	0.65 785	9.98 975	36	
25	9.33 248	57	9.34 276	60	0.65 724	9.98 972	35	
26	9.33 305	57	9.34 336	60	0.65 664	9.98 969	34	
27	9.33 362	57	9.34 396	60	0.65 604	9.98 967	33	
28	9.33 420	57	9.34 456	60	0.65 544	9.98 964	32	
29	9.33 477	57	9.34 516	60	0.65 484	9.98 961	31	
30	9.33 534	57	9.34 576	59	0.65 424	9.98 958	30	
31	9.33 591	56	9.34 635	60	0.65 365	9.98 955	29	
32	9.33 647	56	9.34 695	60	0.65 305	9.98 953	28	
33	9.33 704	57	9.34 755	60	0.65 245	9.98 950	27	
34	9.33 761	57	9.34 814	60	0.65 186	9.98 947	26	
35	9.33 818	56	9.34 874	59	0.65 126	9.98 944	25	
36	9.33 874	57	9.34 933	59	0.65 067	9.98 941	24	
37	9.33 931	56	9.34 992	59	0.65 008	9.98 938	23	
38	9.33 987	56	9.35 051	60	0.64 949	9.98 936	22	
39	9.34 043	57	9.35 111	59	0.64 889	9.98 933	21	
40	9.34 100	56	9.35 170	59	0.64 830	9.98 930	20	
41	9.34 156	56	9.35 229	59	0.64 771	9.98 927	19	
42	9.34 212	56	9.35 288	59	0.64 712	9.98 924	18	
43	9.34 268	56	9.35 347	59	0.64 653	9.98 921	17	
44	9.34 324	56	9.35 405	58	0.64 595	9.98 919	16	
45	9.34 380	56	9.35 464	59	0.64 536	9.98 916	15	
46	9.34 436	55	9.35 523	58	0.64 477	9.98 913	14	
47	9.34 491	55	9.35 581	58	0.64 419	9.98 910	13	
48	9.34 547	55	9.35 640	58	0.64 360	9.98 907	12	
49	9.34 602	56	9.35 698	59	0.64 302	9.98 904	11	
50	9.34 658	55	9.35 757	58	0.64 243	9.98 901	10	
51	9.34 713	55	9.35 815	58	0.64 185	9.98 898	9	
52	9.34 769	55	9.35 873	58	0.64 127	9.98 896	8	
53	9.34 824	55	9.35 931	58	0.64 069	9.98 893	7	
54	9.34 879	55	9.35 989	58	0.64 011	9.98 890	6	
55	9.34 934	55	9.36 047	58	0.63 953	9.98 887	5	
56	9.34 989	55	9.36 105	58	0.63 895	9.98 884	4	
57	9.35 044	55	9.36 163	58	0.63 837	9.98 881	3	
58	9.35 099	55	9.36 221	58	0.63 779	9.98 878	2	
59	9.35 154	55	9.36 279	58	0.63 721	9.98 875	1	
60	9.35 209	55	9.36 336	57	0.63 664	9.98 872	0	
	log cos	d.	log cot	c. d.	log tan	log sin	'	Prop. Pts.

" 63 62 61

6	6.3	6.2	6.1
7	7.4	7.2	7.1
8	8.4	8.3	8.1
9	9.4	9.3	9.2
10	10.5	10.3	10.2
20	21.0	20.7	20.3
30	31.5	31.0	30.5
40	42.0	41.3	40.7
50	52.5	51.7	50.8

" 60 59 58

6	6.0	5.9	5.8
7	7.0	6.9	6.8
8	8.0	7.9	7.7
9	9.0	8.8	8.7
10	10.0	9.8	9.7
20	20.0	19.7	19.3
30	30.0	29.5	29.0
40	40.0	39.3	38.7
50	50.0	49.2	48.3

" 57 56 55

6	5.7	5.6	5.5
7	6.6	6.5	6.4
8	7.6	7.5	7.3
9	8.6	8.4	8.3
10	9.5	9.3	9.2
20	19.0	18.7	18.3
30	28.5	28.0	27.5
40	38.0	37.3	36.7
50	47.5	46.7	45.8

" 3 2

6	0.3	0.2
7	0.4	0.2
8	0.4	0.3
9	0.5	0.3
10	0.5	0.3
20	1.0	0.7
30	1.5	1.0
40	2.0	1.3
50	2.5	1.7

\*167° 257° \*347°

77°

<b>13°</b>							*103°	193°	*283°	
'	log sin	d.	log tan	c. d.	log cot	log cos	Prop. Pts.			
0	9.35 209		9.36 336		0.63 664	9.98 872	<b>60</b>			
1	9.35 263	54	9.36 394	58	0.63 606	9.98 869	59			
2	9.35 318	55	9.36 452	58	0.63 548	9.98 867	58			
3	9.35 373	55	9.36 509	57	0.63 491	9.98 864	57			
4	9.35 427	54	9.36 566	57	0.63 434	9.98 861	56			
5	9.35 481		9.36 624		0.63 376	9.98 858	55			
6	9.35 536	55	9.36 681	57	0.63 319	9.98 855	54	" 58	57	56
7	9.35 590	54	9.36 738	57	0.63 262	9.98 852	53	6 5.8	5.7	5.6
8	9.35 644	54	9.36 795	57	0.63 205	9.98 849	52	7 6.8	6.6	6.5
9	9.35 698	54	9.36 852	57	0.63 148	9.98 846	51	8 7.7	7.6	7.5
10	9.35 752		9.36 909		0.63 091	9.98 843	<b>50</b>	9 8.7	8.6	8.4
11	9.35 806	54	9.36 966	57	0.63 034	9.98 840	49	10 9.7	9.5	9.3
12	9.35 860	54	9.37 023	57	0.62 977	9.98 837	48	20 19.3	19.0	18.7
13	9.35 914	54	9.37 080	57	0.62 920	9.98 834	47	30 29.0	28.5	28.0
14	9.35 968	54	9.37 137	56	0.62 863	9.98 831	46	40 38.7	38.0	37.3
15	9.36 022		9.37 193		0.62 807	9.98 828	45	50 48.3	47.5	46.7
16	9.36 075	53	9.37 250	57	0.62 750	9.98 825	44			
17	9.36 129	54	9.37 306	56	0.62 694	9.98 822	43			
18	9.36 182	53	9.37 363	57	0.62 637	9.98 819	42			
19	9.36 236	54	9.37 419	56	0.62 581	9.98 816	41			
20	9.36 289	53	9.37 476	57	0.62 524	9.98 813	<b>40</b>	" 55	54	53
21	9.36 342	53	9.37 532	56	0.62 468	9.98 810	39	6 5.5	5.4	5.3
22	9.36 395	53	9.37 588	56	0.62 412	9.98 807	38	7 6.4	6.3	6.2
23	9.36 449	54	9.37 644	56	0.62 356	9.98 804	37	8 7.3	7.2	7.1
24	9.36 502	53	9.37 700	56	0.62 300	9.98 801	36	9 8.3	8.1	8.0
25	9.36 555		9.37 756		0.62 244	9.98 798	35	10 9.2	9.0	8.8
26	9.36 608	53	9.37 812	56	0.62 188	9.98 795	34	20 18.3	18.0	17.7
27	9.36 660	52	9.37 868	56	0.62 132	9.98 792	33	30 27.5	27.0	26.5
28	9.36 713	53	9.37 924	56	0.62 076	9.98 789	32	40 36.7	36.0	35.3
29	9.36 766	53	9.37 980	55	0.62 020	9.98 786	31	50 45.8	45.0	44.2
30	9.36 819		9.38 035		0.61 965	9.98 783	<b>30</b>			
31	9.36 871	52	9.38 091	56	0.61 909	9.98 780	29			
32	9.36 924	53	9.38 147	56	0.61 853	9.98 777	28			
33	9.36 976	52	9.38 202	55	0.61 798	9.98 774	27			
34	9.37 028	52	9.38 257	55	0.61 743	9.98 771	26	" 52	51	4
35	9.37 081		9.38 313		0.61 687	9.98 768	25	6 5.2	5.1	0.4
36	9.37 133	52	9.38 368	55	0.61 632	9.98 765	24	7 6.1	6.0	0.5
37	9.37 185	52	9.38 423	55	0.61 577	9.98 762	23	8 6.9	6.8	0.5
38	9.37 237	52	9.38 479	56	0.61 521	9.98 759	22	9 7.8	7.7	0.6
39	9.37 289	52	9.38 534	55	0.61 466	9.98 756	21	10 8.7	8.5	0.7
40	9.37 341		9.38 589		0.61 411	9.98 753	<b>20</b>	20 17.3	17.0	1.3
41	9.37 393	52	9.38 644	55	0.61 356	9.98 750	19	30 26.0	25.5	2.0
42	9.37 445	52	9.38 699	55	0.61 301	9.98 746	18	40 34.7	34.0	2.7
43	9.37 497	52	9.38 754	55	0.61 246	9.98 743	17	50 43.3	42.5	3.3
44	9.37 549	52	9.38 808	54	0.61 192	9.98 740	16			
45	9.37 600	51	9.38 863	55	0.61 137	9.98 737	15			
46	9.37 652	52	9.38 918	55	0.61 082	9.98 734	14			
47	9.37 703	51	9.38 972	54	0.61 028	9.98 731	13			
48	9.37 755	52	9.39 027	55	0.60 973	9.98 728	12	" 3	2	
49	9.37 806	51	9.39 082	55	0.60 918	9.98 725	11	6 0.3	0.2	
50	9.37 858		9.39 136		0.60 864	9.98 722	<b>10</b>	7 0.4	0.2	
51	9.37 909	51	9.39 190	54	0.60 810	9.98 719	9	8 0.4	0.3	
52	9.37 960	51	9.39 245	55	0.60 755	9.98 715	8	9 0.5	0.3	
53	9.38 011	51	9.39 299	54	0.60 701	9.98 712	7	10 0.5	0.3	
54	9.38 062	51	9.39 353	54	0.60 647	9.98 709	6	20 1.0	0.7	
55	9.38 113		9.39 407		0.60 593	9.98 706	5	30 1.5	1.0	
56	9.38 164	51	9.39 461	54	0.60 539	9.98 703	4	40 2.0	1.3	
57	9.38 215	51	9.39 515	54	0.60 485	9.98 700	3	50 2.5	1.7	
58	9.38 266	51	9.39 569	54	0.60 431	9.98 697	2			
59	9.38 317	51	9.39 623	54	0.60 377	9.98 694	1			
60	9.38 368		9.39 677		0.60 323	9.98 690	<b>0</b>			
	log cos	d.	log cot	c. d.	log tan	log sin	'	Prop. Pts.		

\*166°

256°

\*346°

**76°**

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

14°

\*104°

194°

\*284°

'	log sin	d.	log tan	e. d.	log cot	log cos	d.		Prop. Pts.
0	9.38 368		9.39 677		0.60 323	9.98 690		60	
1	9.38 418	50	9.39 731	54	0.60 269	9.98 687	3	59	
2	9.38 469	51	9.39 785	54	0.60 215	9.98 684	3	58	
3	9.38 519	50	9.39 838	53	0.60 162	9.98 681	3	57	
4	9.38 570	51	9.39 892	54	0.60 108	9.98 678	3	56	
		50		53			3		
5	9.38 620		9.39 945		0.60 055	9.98 675		55	
6	9.38 670	50	9.39 999	54	0.60 001	9.98 671	4	54	" 54 53 52
7	9.38 721	51	9.40 052	53	0.59 948	9.98 668	3	53	6 5.4 5.3 5.2
8	9.38 771	50	9.40 106	54	0.59 894	9.98 665	3	52	7 6.3 6.2 6.1
9	9.38 821	50	9.40 159	53	0.59 841	9.98 662	3	51	8 7.2 7.1 6.9
		50		53			3		9 8.1 8.0 7.8
10	9.38 871		9.40 212		0.59 788	9.98 659		50	10 9.0 8.8 8.7
11	9.38 921	50	9.40 266	54	0.59 734	9.98 656	3	49	20 18.0 17.7 17.3
12	9.38 971	50	9.40 319	53	0.59 681	9.98 652	4	48	30 27.0 26.5 26.0
13	9.39 021	50	9.40 372	53	0.59 628	9.98 649	3	47	40 36.0 35.3 34.7
14	9.39 071	50	9.40 425	53	0.59 575	9.98 646	3	46	50 45.0 44.2 43.3
		50		53			3		
15	9.39 121		9.40 478		0.59 522	9.98 643		45	
16	9.39 170	49	9.40 531	53	0.59 469	9.98 640	3	44	
17	9.39 220	50	9.40 584	53	0.59 416	9.98 636	4	43	
18	9.39 270	49	9.40 636	52	0.59 364	9.98 633	3	42	
19	9.39 319	50	9.40 689	53	0.59 311	9.98 630	3	41	
		50		53			3		
20	9.39 369		9.40 742		0.59 258	9.98 627		40	" 51 50 49
21	9.39 418	49	9.40 795	53	0.59 205	9.98 623	4	39	6 5.1 5.0 4.9
22	9.39 467	49	9.40 847	52	0.59 153	9.98 620	3	38	7 6.0 5.8 5.7
23	9.39 517	50	9.40 900	53	0.59 100	9.98 617	3	37	8 6.8 6.7 6.5
24	9.39 566	49	9.40 952	52	0.59 048	9.98 614	3	36	9 7.7 7.5 7.4
		49		53			4		10 8.5 8.3 8.2
25	9.39 615		9.41 005		0.58 995	9.98 610		35	20 17.0 16.7 16.3
26	9.39 664	49	9.41 057	52	0.58 943	9.98 607	3	34	30 25.5 25.0 24.5
27	9.39 713	49	9.41 109	52	0.58 891	9.98 604	3	33	40 34.0 33.3 32.7
28	9.39 762	49	9.41 161	52	0.58 839	9.98 601	3	32	50 42.5 41.7 40.8
29	9.39 811	49	9.41 214	53	0.58 786	9.98 597	4	31	
		49		52			3		
30	9.39 860		9.41 266		0.58 734	9.98 594		30	
31	9.39 909	49	9.41 318	52	0.58 682	9.98 591	3	29	
32	9.39 958	49	9.41 370	52	0.58 630	9.98 588	3	28	
33	9.40 006	48	9.41 422	52	0.58 578	9.98 584	4	27	
34	9.40 055	49	9.41 474	52	0.58 526	9.98 581	3	26	" 48 47
		48		52			3		6 4.8 4.7
35	9.40 103		9.41 526		0.58 474	9.98 578		25	7 5.6 5.5
36	9.40 152	49	9.41 578	52	0.58 422	9.98 574	4	24	8 6.4 6.3
37	9.40 200	48	9.41 629	51	0.58 371	9.98 571	3	23	9 7.2 7.0
38	9.40 249	49	9.41 681	52	0.58 319	9.98 568	3	22	10 8.0 7.8
39	9.40 297	49	9.41 733	52	0.58 267	9.98 565	3	21	20 16.0 15.7
		48		51			4		30 24.0 23.5
40	9.40 346		9.41 784		0.58 216	9.98 561		20	40 32.0 31.3
41	9.40 394	48	9.41 836	52	0.58 164	9.98 558	3	19	50 40.0 39.2
42	9.40 442	48	9.41 887	51	0.58 113	9.98 555	3	18	
43	9.40 490	48	9.41 939	52	0.58 061	9.98 551	4	17	
44	9.40 538	48	9.41 990	51	0.58 010	9.98 548	3	16	
		48		51			3		
45	9.40 586		9.42 041		0.57 959	9.98 545		15	
46	9.40 634	48	9.42 093	52	0.57 907	9.98 541	4	14	
47	9.40 682	48	9.42 144	51	0.57 856	9.98 538	3	13	" 4 3
48	9.40 730	48	9.42 195	51	0.57 805	9.98 535	3	12	6 0.4 0.3
49	9.40 778	48	9.42 246	51	0.57 754	9.98 531	4	11	7 0.5 0.4
		47		51			3		8 0.5 0.4
50	9.40 825		9.42 297		0.57 703	9.98 528		10	9 0.6 0.5
51	9.40 873	48	9.42 348	51	0.57 652	9.98 525	3	9	10 0.7 0.5
52	9.40 921	48	9.42 399	51	0.57 601	9.98 521	4	8	20 1.3 1.0
53	9.40 968	48	9.42 450	51	0.57 550	9.98 518	3	7	30 2.0 1.5
54	9.41 016	47	9.42 501	51	0.57 499	9.98 515	3	6	40 2.7 2.0
		47		51			4		50 3.3 2.5
55	9.41 063		9.42 552		0.57 448	9.98 511		5	
56	9.41 111	48	9.42 603	51	0.57 397	9.98 508	3	4	
57	9.41 158	47	9.42 653	50	0.57 347	9.98 505	3	3	
58	9.41 205	47	9.42 704	51	0.57 296	9.98 501	4	2	
59	9.41 252	47	9.42 755	51	0.57 245	9.98 498	3	1	
60	9.41 300	48	9.42 805	50	0.57 195	9.98 494	4	0	
'	log cos	d.	log cot	e. d.	log tan	log sin	d.	'	Prop. Pts.

\*165°

255°

\*345°

75°

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

<b>15°</b>								*105°	195°	*285°
'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.	
0	9.41 300		9.42 805		0.57 195	9.98 494		<b>60</b>		
1	9.41 347	47	9.42 856	51	0.57 144	9.98 491	3	59		
2	9.41 394	47	9.42 906	50	0.57 094	9.98 488	4	58		
3	9.41 441	47	9.42 957	50	0.57 043	9.98 484	3	57		
4	9.41 488	47	9.43 007	50	0.56 993	9.98 481	4	56		
5	9.41 535		9.43 057		0.56 943	9.98 477		<b>55</b>		
6	9.41 582	47	9.43 108	51	0.56 892	9.98 474	3	54	" 51 50 49	
7	9.41 628	46	9.43 158	50	0.56 842	9.98 471	3	53	6 5.1 5.0 4.9	
8	9.41 675	47	9.43 208	50	0.56 792	9.98 467	4	52	7 6.0 5.8 5.7	
9	9.41 722	47	9.43 258	50	0.56 742	9.98 464	3	51	8 6.8 6.7 6.5	
10	9.41 768	47	9.43 308	50	0.56 692	9.98 460	4	<b>50</b>	9 7.7 7.5 7.4	
11	9.41 815	46	9.43 358	50	0.56 642	9.98 457	3	49	10 8.5 8.3 8.2	
12	9.41 861	46	9.43 408	50	0.56 592	9.98 453	4	48	20 17.0 16.7 16.3	
13	9.41 908	46	9.43 458	50	0.56 542	9.98 450	3	47	30 25.5 25.0 24.5	
14	9.41 954	46	9.43 508	50	0.56 492	9.98 447	3	46	40 34.0 33.3 32.7	
15	9.42 001	46	9.43 558	49	0.56 442	9.98 443	4	45	50 42.5 41.7 40.8	
16	9.42 047	46	9.43 607	50	0.56 393	9.98 440	3	44		
17	9.42 093	46	9.43 657	50	0.56 343	9.98 436	4	43		
18	9.42 140	46	9.43 707	49	0.56 293	9.98 433	3	42		
19	9.42 186	46	9.43 756	50	0.56 244	9.98 429	4	41	" 48 47 46	
20	9.42 232	46	9.43 806	49	0.56 194	9.98 426	3	<b>40</b>	6 4.8 4.7 4.6	
21	9.42 278	46	9.43 855	50	0.56 145	9.98 422	4	39	7 5.6 5.5 5.4	
22	9.42 324	46	9.43 905	49	0.56 095	9.98 419	3	38	8 6.4 6.3 6.1	
23	9.42 370	46	9.43 954	50	0.56 046	9.98 415	4	37	9 7.2 7.0 6.9	
24	9.42 416	45	9.44 004	49	0.55 996	9.98 412	3	36	10 8.0 7.8 7.7	
25	9.42 461	46	9.44 053	49	0.55 947	9.98 409	3	35	20 16.0 15.7 15.3	
26	9.42 507	46	9.44 102	49	0.55 898	9.98 405	4	34	30 24.0 23.5 23.0	
27	9.42 553	46	9.44 151	50	0.55 849	9.98 402	3	33	40 32.0 31.3 30.7	
28	9.42 599	46	9.44 201	49	0.55 799	9.98 398	4	32	50 40.0 39.2 38.3	
29	9.42 644	46	9.44 250	49	0.55 750	9.98 395	3	31		
30	9.42 690	45	9.44 299	49	0.55 701	9.98 391	4	<b>30</b>		
31	9.42 735	46	9.44 348	49	0.55 652	9.98 388	3	29		
32	9.42 781	45	9.44 397	49	0.55 603	9.98 384	4	28		
33	9.42 826	46	9.44 446	49	0.55 554	9.98 381	3	27	" 45 44	
34	9.42 872	45	9.44 495	49	0.55 505	9.98 377	4	26	6 4.5 4.4	
35	9.42 917	45	9.44 544	48	0.55 456	9.98 373	3	25	7 5.3 5.1	
36	9.42 962	46	9.44 592	49	0.55 408	9.98 370	4	24	8 6.0 5.9	
37	9.43 008	45	9.44 641	49	0.55 359	9.98 366	3	23	9 6.8 6.6	
38	9.43 053	45	9.44 690	48	0.55 310	9.98 363	4	22	10 7.5 7.3	
39	9.43 098	45	9.44 738	49	0.55 262	9.98 359	3	21	20 15.0 14.7	
40	9.43 143	45	9.44 787	49	0.55 213	9.98 356	4	<b>20</b>	30 22.5 22.0	
41	9.43 188	45	9.44 836	48	0.55 164	9.98 352	3	19	40 30.0 29.3	
42	9.43 233	45	9.44 884	48	0.55 116	9.98 349	4	18	50 37.5 36.7	
43	9.43 278	45	9.44 933	49	0.55 067	9.98 345	3	17		
44	9.43 323	44	9.44 981	48	0.55 019	9.98 342	4	16		
45	9.43 367	45	9.45 029	49	0.54 971	9.98 338	3	15		
46	9.43 412	45	9.45 078	48	0.54 922	9.98 334	4	14		
47	9.43 457	45	9.45 126	48	0.54 874	9.98 331	3	13	" 4 3	
48	9.43 502	45	9.45 174	48	0.54 826	9.98 327	4	12	6 0.4 0.3	
49	9.43 546	44	9.45 222	49	0.54 778	9.98 324	3	11	7 0.5 0.4	
50	9.43 591	45	9.45 271	48	0.54 729	9.98 320	4	<b>10</b>	8 0.5 0.4	
51	9.43 635	44	9.45 319	48	0.54 681	9.98 317	3	9	9 0.6 0.5	
52	9.43 680	45	9.45 367	48	0.54 633	9.98 313	4	8	10 0.7 0.5	
53	9.43 724	44	9.45 415	48	0.54 585	9.98 309	3	7	20 1.3 1.0	
54	9.43 769	45	9.45 463	48	0.54 537	9.98 306	4	6	30 2.0 1.5	
55	9.43 813	44	9.45 511	48	0.54 489	9.98 302	3	5	40 2.7 2.0	
56	9.43 857	44	9.45 559	48	0.54 441	9.98 299	4	4	50 3.3 2.5	
57	9.43 901	44	9.45 606	47	0.54 394	9.98 295	3	3		
58	9.43 946	45	9.45 654	48	0.54 346	9.98 291	4	2		
59	9.43 990	44	9.45 702	48	0.54 298	9.98 288	3	1		
60	9.44 034	44	9.45 750	48	0.54 250	9.98 284	4	<b>0</b>		
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.	

\*164°

254°

\*344°

**74°**

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

<b>16°</b>										*106°	196°	*286°	
'	log sin	d.	log tan	c. d.	log cot	log cos	d.			Prop. Pts.			
0	9.44 034		9.45 750		0.54 250	9.98 284			<b>60</b>				
1	9.44 078	44	9.45 797	47	0.54 203	9.98 281	3		59				
2	9.44 122	44	9.45 845	48	0.54 155	9.98 277	4		58				
3	9.44 166	44	9.45 892	47	0.54 108	9.98 273	4		57				
4	9.44 210	43	9.45 940	47	0.54 060	9.98 270	3		56				
5	9.44 253		9.45 987		0.54 013	9.98 266			55				
6	9.44 297	44	9.46 035	48	0.53 965	9.98 262	4		54	"	48	47	46
7	9.44 341	44	9.46 082	47	0.53 918	9.98 259	3		53	6	4.8	4.7	4.6
8	9.44 385	44	9.46 130	47	0.53 870	9.98 255	4		52	7	5.6	5.5	5.4
9	9.44 428	43	9.46 177	47	0.53 823	9.98 251	4		51	8	6.4	6.3	6.1
10	9.44 472	44	9.46 224	47	0.53 776	9.98 248	3		50	9	7.2	7.0	6.9
11	9.44 516	44	9.46 271	48	0.53 729	9.98 244	4		49	10	8.0	7.8	7.7
12	9.44 559	43	9.46 319	47	0.53 681	9.98 240	4		48	20	16.0	15.7	15.3
13	9.44 602	43	9.46 366	47	0.53 634	9.98 237	3		47	30	24.0	23.5	23.0
14	9.44 646	43	9.46 413	47	0.53 587	9.98 233	4		46	40	32.0	31.3	30.7
15	9.44 689		9.46 460		0.53 540	9.98 229			45	50	40.0	39.2	38.3
16	9.44 733	44	9.46 507	47	0.53 493	9.98 226	4		44				
17	9.44 776	43	9.46 554	47	0.53 446	9.98 222	3		43				
18	9.44 819	43	9.46 601	47	0.53 399	9.98 218	4		42				
19	9.44 862	43	9.46 648	46	0.53 352	9.98 215	3		41				
20	9.44 905		9.46 694		0.53 306	9.98 211			40	"	45	44	43
21	9.44 948	43	9.46 741	47	0.53 259	9.98 207	4		39	6	4.5	4.4	4.3
22	9.44 992	44	9.46 788	47	0.53 212	9.98 204	3		38	7	5.3	5.1	5.0
23	9.45 035	43	9.46 835	47	0.53 165	9.98 200	4		37	8	6.0	5.9	5.7
24	9.45 077	42	9.46 881	46	0.53 119	9.98 196	4		36	9	6.8	6.6	6.4
25	9.45 120	43	9.46 928	47	0.53 072	9.98 192	4		35	10	7.5	7.3	7.2
26	9.45 163	43	9.46 975	47	0.53 025	9.98 189	3		34	20	15.0	14.7	14.3
27	9.45 206	43	9.47 021	46	0.52 979	9.98 185	4		33	30	22.5	22.0	21.5
28	9.45 249	43	9.47 068	47	0.52 932	9.98 181	4		32	40	30.0	29.3	28.7
29	9.45 292	42	9.47 114	46	0.52 886	9.98 177	4		31	50	37.5	36.7	35.8
30	9.45 334		9.47 160		0.52 840	9.98 174			30				
31	9.45 377	43	9.47 207	47	0.52 793	9.98 170	4		29				
32	9.45 419	42	9.47 253	46	0.52 747	9.98 166	4		28				
33	9.45 462	43	9.47 299	46	0.52 701	9.98 162	4		27				
34	9.45 504	42	9.47 346	47	0.52 654	9.98 159	3		26	"	42	41	
35	9.45 547	43	9.47 392	46	0.52 608	9.98 155	4		25	6	4.2	4.1	
36	9.45 589	42	9.47 438	46	0.52 562	9.98 151	4		24	7	4.9	4.8	
37	9.45 632	43	9.47 484	46	0.52 516	9.98 147	4		23	8	5.6	5.5	
38	9.45 674	42	9.47 530	46	0.52 470	9.98 144	3		22	9	6.3	6.2	
39	9.45 716	42	9.47 576	46	0.52 424	9.98 140	4		21	10	7.0	6.8	
40	9.45 758		9.47 622		0.52 378	9.98 136			20	20	14.0	13.7	
41	9.45 801	43	9.47 668	46	0.52 332	9.98 132	4		19	30	21.0	20.5	
42	9.45 843	42	9.47 714	46	0.52 286	9.98 129	3		18	40	28.0	27.3	
43	9.45 885	42	9.47 760	46	0.52 240	9.98 125	4		17	50	35.0	34.2	
44	9.45 927	42	9.47 806	46	0.52 194	9.98 121	4		16				
45	9.45 969		9.47 852		0.52 148	9.98 117			15				
46	9.46 011	42	9.47 897	45	0.52 103	9.98 113	4		14				
47	9.46 053	42	9.47 943	46	0.52 057	9.98 110	3		13	"	4	3	
48	9.46 095	42	9.47 989	46	0.52 011	9.98 106	4		12	6	0.4	0.3	
49	9.46 136	41	9.48 035	45	0.51 965	9.98 102	4		11	7	0.5	0.4	
50	9.46 178		9.48 080		0.51 920	9.98 098			10	8	0.5	0.4	
51	9.46 220	42	9.48 126	46	0.51 874	9.98 094	4		9	9	0.6	0.5	
52	9.46 262	42	9.48 171	45	0.51 829	9.98 090	4		8	10	0.7	0.5	
53	9.46 303	41	9.48 217	46	0.51 783	9.98 087	3		7	20	1.3	1.0	
54	9.46 345	42	9.48 262	45	0.51 738	9.98 083	4		6	30	2.0	1.5	
55	9.46 386	41	9.48 307	45	0.51 693	9.98 079	4		5	40	2.7	2.0	
56	9.46 428	42	9.48 353	46	0.51 647	9.98 075	4		4	50	3.3	2.5	
57	9.46 469	41	9.48 398	45	0.51 602	9.98 071	4		3				
58	9.46 511	42	9.48 443	45	0.51 557	9.98 067	4		2				
59	9.46 552	41	9.48 489	46	0.51 511	9.98 063	4		1				
60	9.46 594	42	9.48 534	45	0.51 466	9.98 060	3		0				
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'		Prop. Pts.			

\*163°    253°    \*343°

**73°**

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.46 594		9.48 534		0.51 466	9.98 060		60	
1	9.46 635	41	9.48 579	45	0.51 421	9.98 056	4	59	
2	9.46 676	41	9.48 624	45	0.51 376	9.98 052	4	58	
3	9.46 717	41	9.48 669	45	0.51 331	9.98 048	4	57	
4	9.46 758	42	9.48 714	45	0.51 286	9.98 044	4	56	
5	9.46 800		9.48 759		0.51 241	9.98 040		55	
6	9.46 841	41	9.48 804	45	0.51 196	9.98 036	4	54	
7	9.46 882	41	9.48 849	45	0.51 151	9.98 032	4	53	
8	9.46 923	41	9.48 894	45	0.51 106	9.98 029	3	52	
9	9.46 964	41	9.48 939	45	0.51 061	9.98 025	4	51	
10	9.47 005		9.48 984		0.51 016	9.98 021		50	
11	9.47 045	40	9.49 029	45	0.50 971	9.98 017	4	49	
12	9.47 086	41	9.49 073	44	0.50 927	9.98 013	4	48	
13	9.47 127	41	9.49 118	45	0.50 882	9.98 009	4	47	
14	9.47 168	41	9.49 163	44	0.50 837	9.98 005	4	46	
15	9.47 209		9.49 207		0.50 793	9.98 001		45	
16	9.47 249	40	9.49 252	45	0.50 748	9.97 997	4	44	
17	9.47 290	41	9.49 296	44	0.50 704	9.97 993	4	43	
18	9.47 330	40	9.49 341	45	0.50 659	9.97 989	4	42	
19	9.47 371	41	9.49 385	44	0.50 615	9.97 986	3	41	
20	9.47 411	40	9.49 430	45	0.50 570	9.97 982	4	40	
21	9.47 452	41	9.49 474	44	0.50 526	9.97 978	4	39	
22	9.47 492	40	9.49 519	45	0.50 481	9.97 974	4	38	
23	9.47 533	41	9.49 563	44	0.50 437	9.97 970	4	37	
24	9.47 573	40	9.49 607	45	0.50 393	9.97 966	4	36	
25	9.47 613		9.49 652		0.50 348	9.97 962		35	
26	9.47 654	41	9.49 696	44	0.50 304	9.97 958	4	34	
27	9.47 694	40	9.49 740	44	0.50 260	9.97 954	4	33	
28	9.47 734	40	9.49 784	44	0.50 216	9.97 950	4	32	
29	9.47 774	40	9.49 828	44	0.50 172	9.97 946	4	31	
30	9.47 814		9.49 872		0.50 128	9.97 942		30	
31	9.47 854	40	9.49 916	44	0.50 084	9.97 938	4	29	
32	9.47 894	40	9.49 960	44	0.50 040	9.97 934	4	28	
33	9.47 934	40	9.50 004	44	0.49 996	9.97 930	4	27	
34	9.47 974	40	9.50 048	44	0.49 952	9.97 926	4	26	
35	9.48 014		9.50 092		0.49 908	9.97 922		25	
36	9.48 054	40	9.50 136	44	0.49 864	9.97 918	4	24	
37	9.48 094	40	9.50 180	44	0.49 820	9.97 914	4	23	
38	9.48 133	39	9.50 223	43	0.49 777	9.97 910	4	22	
39	9.48 173	40	9.50 267	44	0.49 733	9.97 906	4	21	
40	9.48 213		9.50 311		0.49 689	9.97 902		20	
41	9.48 252	39	9.50 355	44	0.49 645	9.97 898	4	19	
42	9.48 292	40	9.50 398	43	0.49 602	9.97 894	4	18	
43	9.48 332	40	9.50 442	44	0.49 558	9.97 890	4	17	
44	9.48 371	39	9.50 485	43	0.49 515	9.97 886	4	16	
45	9.48 411	40	9.50 529	44	0.49 471	9.97 882	4	15	
46	9.48 450	39	9.50 572	43	0.49 428	9.97 878	4	14	
47	9.48 490	40	9.50 616	44	0.49 384	9.97 874	4	13	
48	9.48 529	39	9.50 659	43	0.49 341	9.97 870	4	12	
49	9.48 568	39	9.50 703	44	0.49 297	9.97 866	4	11	
50	9.48 607		9.50 746		0.49 254	9.97 861		10	
51	9.48 647	40	9.50 789	43	0.49 211	9.97 857	4	9	
52	9.48 686	39	9.50 833	44	0.49 167	9.97 853	4	8	
53	9.48 725	39	9.50 876	43	0.49 124	9.97 849	4	7	
54	9.48 764	39	9.50 919	43	0.49 081	9.97 845	4	6	
55	9.48 803		9.50 962		0.49 038	9.97 841		5	
56	9.48 842	39	9.51 005	43	0.48 995	9.97 837	4	4	
57	9.48 881	39	9.51 048	43	0.48 952	9.97 833	4	3	
58	9.48 920	39	9.51 092	44	0.48 908	9.97 829	4	2	
59	9.48 959	39	9.51 135	43	0.48 865	9.97 825	4	1	
60	9.48 998		9.51 178		0.48 822	9.97 821		0	

"	45	44	43
6	4.5	4.4	4.3
7	5.3	5.1	5.0
8	6.0	5.9	5.7
9	6.8	6.6	6.4
10	7.5	7.3	7.2
20	15.0	14.7	14.3
30	22.5	22.0	21.5
40	30.0	29.3	28.7
50	37.5	36.7	35.8

"	42	41
6	4.2	4.1
7	4.9	4.8
8	5.6	5.5
9	6.3	6.2
10	7.0	6.8
20	14.0	13.7
30	21.0	20.5
40	28.0	27.3
50	35.0	34.2

"	40	39
6	4.0	3.9
7	4.7	4.6
8	5.3	5.2
9	6.0	5.9
10	6.7	6.5
20	13.3	13.0
30	20.0	19.5
40	26.7	26.0
50	33.3	32.5

"	5	4	3
6	0.5	0.4	0.3
7	0.6	0.5	0.4
8	0.7	0.5	0.4
9	0.8	0.6	0.5
10	0.8	0.7	0.5
20	1.7	1.3	1.0
30	2.5	2.0	1.5
40	3.3	2.7	2.0
50	4.2	3.3	2.5

	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.
*162°		252°		*342°				72°	

18°

\*108°

198°

\*288°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.48 998		9.51 178		0.48 822	9.97 821		60	
1	9.49 037	39	9.51 221	43	0.48 779	9.97 817	4	59	
2	9.49 076	39	9.51 264	43	0.48 736	9.97 812	5	58	
3	9.49 115	39	9.51 306	42	0.48 694	9.97 808	4	57	
4	9.49 153	38	9.51 349	43	0.48 651	9.97 804	4	56	
5	9.49 192	39	9.51 392	43	0.48 608	9.97 800	4	55	
6	9.49 231	38	9.51 435	43	0.48 565	9.97 796	4	54	
7	9.49 269	38	9.51 478	43	0.48 522	9.97 792	4	53	
8	9.49 308	39	9.51 520	42	0.48 480	9.97 788	4	52	
9	9.49 347	39	9.51 563	43	0.48 437	9.97 784	4	51	
10	9.49 385	38	9.51 606	43	0.48 394	9.97 779	5	50	" 43 42 41
11	9.49 424	39	9.51 648	42	0.48 352	9.97 775	4	49	6 4.3 4.2 4.1
12	9.49 462	38	9.51 691	43	0.48 309	9.97 771	4	48	7 5.0 4.9 4.8
13	9.49 500	38	9.51 734	43	0.48 266	9.97 767	4	47	8 5.7 5.6 5.5
14	9.49 539	39	9.51 776	42	0.48 224	9.97 763	4	46	9 6.4 6.3 6.2
15	9.49 577	38	9.51 819	43	0.48 181	9.97 759	4	45	10 7.2 7.0 6.8
16	9.49 615	38	9.51 861	42	0.48 139	9.97 754	5	44	20 14.3 14.0 13.7
17	9.49 654	39	9.51 903	42	0.48 097	9.97 750	4	43	30 21.5 21.0 20.5
18	9.49 692	38	9.51 946	43	0.48 054	9.97 746	4	42	40 28.7 28.0 27.3
19	9.49 730	38	9.51 988	42	0.48 012	9.97 742	4	41	50 35.8 35.0 34.2
20	9.49 768	38	9.52 031	43	0.47 969	9.97 738	4	40	
21	9.49 806	38	9.52 073	42	0.47 927	9.97 734	4	39	
22	9.49 844	28	9.52 115	42	0.47 885	9.97 729	5	38	
23	9.49 882	38	9.52 157	42	0.47 843	9.97 725	4	37	
24	9.49 920	38	9.52 200	43	0.47 800	9.97 721	4	36	
25	9.49 958	38	9.52 242	42	0.47 758	9.97 717	4	35	
26	9.49 996	38	9.52 284	42	0.47 716	9.97 713	4	34	
27	9.50 034	38	9.52 326	42	0.47 674	9.97 708	5	33	" 39 38 37
28	9.50 072	38	9.52 368	42	0.47 632	9.97 704	4	32	6 3.9 3.8 3.7
29	9.50 110	38	9.52 410	42	0.47 590	9.97 700	4	31	7 4.6 4.4 4.3
30	9.50 148	38	9.52 452	42	0.47 548	9.97 696	4	30	8 5.2 5.1 4.9
31	9.50 185	37	9.52 494	42	0.47 506	9.97 691	5	29	9 5.9 5.7 5.6
32	9.50 223	38	9.52 536	42	0.47 464	9.97 687	4	28	10 6.5 6.3 6.2
33	9.50 261	38	9.52 578	42	0.47 422	9.97 683	4	27	20 13.0 12.7 12.3
34	9.50 298	37	9.52 620	42	0.47 380	9.97 679	4	26	30 19.5 19.0 18.5
35	9.50 336	38	9.52 661	41	0.47 339	9.97 674	4	25	40 26.0 25.3 24.7
36	9.50 374	38	9.52 703	42	0.47 297	9.97 670	5	24	50 32.5 31.7 30.8
37	9.50 411	37	9.52 745	42	0.47 255	9.97 666	4	23	
38	9.50 449	38	9.52 787	42	0.47 213	9.97 662	4	22	
39	9.50 486	37	9.52 829	42	0.47 171	9.97 657	5	21	
40	9.50 523	37	9.52 870	41	0.47 130	9.97 653	4	20	
41	9.50 561	38	9.52 912	42	0.47 088	9.97 649	4	19	
42	9.50 598	37	9.52 953	41	0.47 047	9.97 645	4	18	
43	9.50 635	37	9.52 995	42	0.47 005	9.97 640	5	17	
44	9.50 673	38	9.53 037	42	0.46 963	9.97 636	4	16	" 36 5 4
45	9.50 710	37	9.53 078	41	0.46 922	9.97 632	4	15	6 3.6 0.5 0.4
46	9.50 747	37	9.53 120	42	0.46 880	9.97 628	4	14	7 4.2 0.6 0.5
47	9.50 784	37	9.53 161	41	0.46 839	9.97 623	5	13	8 4.8 0.7 0.5
48	9.50 821	37	9.53 202	41	0.46 798	9.97 619	4	12	9 5.4 0.8 0.6
49	9.50 858	37	9.53 244	42	0.46 756	9.97 615	4	11	10 6.0 0.8 0.7
50	9.50 896	38	9.53 285	41	0.46 715	9.97 610	5	10	20 12.0 1.7 1.3
51	9.50 933	37	9.53 327	42	0.46 673	9.97 606	4	9	30 18.0 2.5 2.0
52	9.50 970	37	9.53 368	41	0.46 632	9.97 602	4	8	40 24.0 3.3 2.7
53	9.51 007	37	9.53 409	41	0.46 591	9.97 597	5	7	50 30.0 4.2 3.3
54	9.51 043	36	9.53 450	41	0.46 550	9.97 593	4	6	
55	9.51 080	37	9.53 492	42	0.46 508	9.97 589	4	5	
56	9.51 117	37	9.53 533	41	0.46 467	9.97 584	5	4	
57	9.51 154	37	9.53 574	41	0.46 426	9.97 580	4	3	
58	9.51 191	37	9.53 615	41	0.46 385	9.97 576	4	2	
59	9.51 227	36	9.53 656	41	0.46 344	9.97 571	5	1	
60	9.51 264	37	9.53 697	41	0.46 303	9.97 567	4	0	

\*161°

251°

\*341°

71°

19°

\*109°

199°

\*289°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.51 264		9.53 697		0.46 303	9.97 567		60	
1	9.51 301	37	9.53 738	41	0.46 262	9.97 563	4	59	
2	9.51 338	37	9.53 779	41	0.46 221	9.97 558	5	58	
3	9.51 374	36	9.53 820	41	0.46 180	9.97 554	4	57	
4	9.51 411	37	9.53 861	41	0.46 139	9.97 550	4	56	
5	9.51 447	36	9.53 902	41	0.46 098	9.97 545	5	55	
6	9.51 484	37	9.53 943	41	0.46 057	9.97 541	4	54	
7	9.51 520	36	9.53 984	41	0.46 016	9.97 536	5	53	
8	9.51 557	37	9.54 025	41	0.45 975	9.97 532	4	52	
9	9.51 593	36	9.54 065	40	0.45 935	9.97 528	4	51	
10	9.51 629	36	9.54 106	41	0.45 894	9.97 523	5	50	" 41 40 39
11	9.51 666	37	9.54 147	40	0.45 853	9.97 519	4	49	6 4.1 4.0 3.9
12	9.51 702	36	9.54 187	41	0.45 813	9.97 515	5	48	7 4.8 4.7 4.6
13	9.51 738	36	9.54 228	41	0.45 772	9.97 510	4	47	8 5.5 5.3 5.2
14	9.51 774	37	9.54 269	41	0.45 731	9.97 506	4	46	9 6.2 6.0 5.9
15	9.51 811	36	9.54 309	40	0.45 691	9.97 501	5	45	10 6.8 6.7 6.5
16	9.51 847	36	9.54 350	41	0.45 650	9.97 497	4	44	20 13.7 13.3 13.0
17	9.51 883	36	9.54 390	40	0.45 610	9.97 492	5	43	30 20.5 20.0 19.5
18	9.51 919	36	9.54 431	41	0.45 569	9.97 488	4	42	40 27.3 26.7 26.0
19	9.51 955	36	9.54 471	40	0.45 529	9.97 484	4	41	50 34.2 33.3 32.5
20	9.51 991	36	9.54 512	41	0.45 488	9.97 479	5	40	
21	9.52 027	36	9.54 552	40	0.45 448	9.97 475	4	39	
22	9.52 063	36	9.54 593	41	0.45 407	9.97 470	5	38	
23	9.52 099	36	9.54 633	40	0.45 367	9.97 466	4	37	
24	9.52 135	36	9.54 673	40	0.45 327	9.97 461	5	36	
25	9.52 171	36	9.54 714	41	0.45 286	9.97 457	4	35	
26	9.52 207	35	9.54 754	40	0.45 246	9.97 453	4	34	
27	9.52 242	36	9.54 794	40	0.45 206	9.97 448	5	33	" 37 36 35
28	9.52 278	36	9.54 835	41	0.45 165	9.97 444	4	32	6 3.7 3.6 3.5
29	9.52 314	36	9.54 875	40	0.45 125	9.97 439	5	31	7 4.3 4.2 4.1
30	9.52 350	35	9.54 915	40	0.45 085	9.97 435	4	30	8 4.9 4.8 4.7
31	9.52 385	36	9.54 955	40	0.45 045	9.97 430	5	29	9 5.6 5.4 5.3
32	9.52 421	35	9.54 995	40	0.45 005	9.97 426	4	28	10 6.2 6.0 5.8
33	9.52 456	36	9.55 035	40	0.44 965	9.97 421	5	27	20 12.3 12.0 11.7
34	9.52 492	35	9.55 075	40	0.44 925	9.97 417	4	26	30 18.5 18.0 17.5
35	9.52 527	36	9.55 115	40	0.44 885	9.97 412	5	25	40 24.7 24.0 23.3
36	9.52 563	35	9.55 155	40	0.44 845	9.97 408	4	24	50 30.8 30.0 29.2
37	9.52 598	36	9.55 195	40	0.44 805	9.97 403	5	23	
38	9.52 634	35	9.55 235	40	0.44 765	9.97 399	4	22	
39	9.52 669	36	9.55 275	40	0.44 725	9.97 394	5	21	
40	9.52 705	35	9.55 315	40	0.44 685	9.97 390	4	20	
41	9.52 740	35	9.55 355	40	0.44 645	9.97 385	5	19	
42	9.52 775	36	9.55 395	40	0.44 605	9.97 381	4	18	
43	9.52 811	35	9.55 434	39	0.44 566	9.97 376	5	17	
44	9.52 846	35	9.55 474	40	0.44 526	9.97 372	4	16	" 34 5 4
45	9.52 881	35	9.55 514	40	0.44 486	9.97 367	5	15	6 3.4 0.5 0.4
46	9.52 916	35	9.55 554	40	0.44 446	9.97 363	4	14	7 4.0 0.6 0.5
47	9.52 951	35	9.55 593	39	0.44 407	9.97 358	5	13	8 4.5 0.7 0.5
48	9.52 986	35	9.55 633	40	0.44 367	9.97 353	4	12	9 5.1 0.8 0.6
49	9.53 021	35	9.55 673	40	0.44 327	9.97 349	5	11	10 5.7 0.8 0.7
50	9.53 056	36	9.55 712	39	0.44 288	9.97 344	4	10	20 11.3 1.7 1.3
51	9.53 092	34	9.55 752	40	0.44 248	9.97 340	5	9	30 17.0 2.5 2.0
52	9.53 126	35	9.55 791	40	0.44 209	9.97 335	4	8	40 22.7 3.3 2.7
53	9.53 161	35	9.55 831	39	0.44 169	9.97 331	5	7	50 28.3 4.2 3.3
54	9.53 196	35	9.55 870	40	0.44 130	9.97 326	4	6	
55	9.53 231	35	9.55 910	40	0.44 090	9.97 322	5	5	
56	9.53 266	35	9.55 949	39	0.44 051	9.97 317	4	4	
57	9.53 301	35	9.55 989	40	0.44 011	9.97 312	5	3	
58	9.53 336	35	9.56 028	39	0.43 972	9.97 308	4	2	
59	9.53 370	34	9.56 067	39	0.43 933	9.97 303	5	1	
60	9.53 405	35	9.56 107	40	0.43 893	9.97 299	4	0	
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.

\*160°

250°

\*340°

70°



LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

20°

\*110°

200°

\*290°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.53 405		9.56 107		0.43 893	9.97 299		60	
1	9.53 440	35	9.56 146	39	0.43 854	9.97 294	5	59	
2	9.53 475	35	9.56 185	39	0.43 815	9.97 289	5	58	
3	9.53 509	34	9.56 224	39	0.43 776	9.97 285	4	57	
4	9.53 544	35	9.56 264	40	0.43 736	9.97 280	4	56	
5	9.53 578	34	9.56 303	39	0.43 697	9.97 276	5	55	
6	9.53 613	35	9.56 342	39	0.43 658	9.97 271	5	54	" 40 39
7	9.53 647	34	9.56 381	39	0.43 619	9.97 266	5	53	6 4.0 3.9
8	9.53 682	35	9.56 420	39	0.43 580	9.97 262	4	52	7 4.7 4.6
9	9.53 716	34	9.56 459	39	0.43 541	9.97 257	5	51	8 5.3 5.2
10	9.53 751	35	9.56 498	39	0.43 502	9.97 252	5	50	9 6.0 5.9
11	9.53 785	34	9.56 537	39	0.43 463	9.97 248	4	49	10 6.7 6.5
12	9.53 819	34	9.56 576	39	0.43 424	9.97 243	5	48	20 13.3 13.0
13	9.53 854	35	9.56 615	39	0.43 385	9.97 238	5	47	30 20.0 19.5
14	9.53 888	34	9.56 654	39	0.43 346	9.97 234	4	46	40 26.7 26.0
15	9.53 922	34	9.56 693	39	0.43 307	9.97 229	5	45	50 33.3 32.5
16	9.53 957	35	9.56 732	39	0.43 268	9.97 224	5	44	
17	9.53 991	34	9.56 771	39	0.43 229	9.97 220	4	43	
18	9.54 025	34	9.56 810	39	0.43 190	9.97 215	5	42	
19	9.54 059	34	9.56 849	39	0.43 151	9.97 210	5	41	
20	9.54 093	34	9.56 887	38	0.43 113	9.97 206	4	40	" 38 37
21	9.54 127	34	9.56 926	39	0.43 074	9.97 201	5	39	6 3.8 3.7
22	9.54 161	34	9.56 965	39	0.43 035	9.97 196	5	38	7 4.4 4.3
23	9.54 195	34	9.57 004	39	0.42 996	9.97 192	4	37	8 5.1 4.9
24	9.54 229	34	9.57 042	38	0.42 958	9.97 187	5	36	9 5.7 5.6
25	9.54 263	34	9.57 081	39	0.42 919	9.97 182	5	35	10 6.3 6.2
26	9.54 297	34	9.57 120	39	0.42 880	9.97 178	4	34	20 12.7 12.3
27	9.54 331	34	9.57 158	38	0.42 842	9.97 173	5	33	30 19.0 18.5
28	9.54 365	34	9.57 197	39	0.42 803	9.97 168	4	32	40 25.3 24.7
29	9.54 399	34	9.57 235	38	0.42 765	9.97 163	5	31	50 31.7 30.8
30	9.54 433	34	9.57 274	39	0.42 726	9.97 159	4	30	
31	9.54 466	33	9.57 312	38	0.42 688	9.97 154	5	29	
32	9.54 500	34	9.57 351	39	0.42 649	9.97 149	5	28	
33	9.54 534	34	9.57 389	38	0.42 611	9.97 145	4	27	
34	9.54 567	33	9.57 428	39	0.42 572	9.97 140	5	26	" 35 34
35	9.54 601	34	9.57 466	38	0.42 534	9.97 135	5	25	6 3.5 3.4
36	9.54 635	34	9.57 504	38	0.42 496	9.97 130	5	24	7 4.1 4.0
37	9.54 668	33	9.57 543	39	0.42 457	9.97 126	4	23	8 4.7 4.5
38	9.54 702	34	9.57 581	38	0.42 419	9.97 121	5	22	9 5.3 5.1
39	9.54 735	33	9.57 619	38	0.42 381	9.97 116	5	21	10 5.8 5.7
40	9.54 769	34	9.57 658	39	0.42 342	9.97 111	5	20	20 11.7 11.3
41	9.54 802	33	9.57 696	38	0.42 304	9.97 107	4	19	30 17.5 17.0
42	9.54 836	34	9.57 734	38	0.42 266	9.97 102	5	18	40 23.3 22.7
43	9.54 869	33	9.57 772	38	0.42 228	9.97 097	5	17	50 29.2 28.3
44	9.54 903	34	9.57 810	38	0.42 190	9.97 092	5	16	
45	9.54 936	33	9.57 849	39	0.42 151	9.97 087	5	15	
46	9.54 969	33	9.57 887	38	0.42 113	9.97 083	4	14	
47	9.55 003	34	9.57 925	38	0.42 075	9.97 078	5	13	" 33 5 4
48	9.55 036	33	9.57 963	38	0.42 037	9.97 073	5	12	6 3.3 0.5 0.4
49	9.55 069	33	9.58 001	38	0.41 999	9.97 068	5	11	7 3.8 0.6 0.5
50	9.55 102	33	9.58 039	38	0.41 961	9.97 063	5	10	8 4.4 0.7 0.5
51	9.55 136	34	9.58 077	38	0.41 923	9.97 059	4	9	9 5.0 0.8 0.6
52	9.55 169	33	9.58 115	38	0.41 885	9.97 054	5	8	10 5.5 0.8 0.7
53	9.55 202	33	9.58 153	38	0.41 847	9.97 049	5	7	20 11.0 1.7 1.3
54	9.55 235	33	9.58 191	38	0.41 809	9.97 044	5	6	30 16.5 2.5 2.0
55	9.55 268	33	9.58 229	38	0.41 771	9.97 039	5	5	40 22.0 3.3 2.7
56	9.55 301	33	9.58 267	38	0.41 733	9.97 035	4	4	50 27.5 4.2 3.3
57	9.55 334	33	9.58 304	37	0.41 696	9.97 030	5	3	
58	9.55 367	33	9.58 342	38	0.41 658	9.97 025	5	2	
59	9.55 400	33	9.58 380	38	0.41 620	9.97 020	5	1	
60	9.55 433	33	9.58 418	38	0.41 582	9.97 015	5	0	
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.

\*159°

249°

\*339°

69°

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

21°

\*111°

201°

\*291°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.55 433		9.58 418		0.41 582	9.97 015		60	
1	9.55 466	33	9.58 455	37	0.41 545	9.97 010	5	59	
2	9.55 499	33	9.58 493	38	0.41 507	9.97 005	4	58	
3	9.55 532	33	9.58 531	38	0.41 469	9.97 001	5	57	
4	9.55 564	33	9.58 569	37	0.41 431	9.96 996	5	56	
5	9.55 597		9.58 606		0.41 394	9.96 991		55	
6	9.55 630	33	9.58 644	38	0.41 356	9.96 986	5	54	
7	9.55 663	33	9.58 681	37	0.41 319	9.96 981	5	53	
8	9.55 695	32	9.58 719	38	0.41 281	9.96 976	5	52	
9	9.55 728	33	9.58 757	38	0.41 243	9.96 971	5	51	
10	9.55 761		9.58 794		0.41 206	9.96 966		50	" 38 37 36
11	9.55 793	32	9.58 832	37	0.41 168	9.96 962	4	49	6 3.8 3.7 3.6
12	9.55 826	33	9.58 869	38	0.41 131	9.96 957	5	48	7 4.4 4.3 4.2
13	9.55 858	32	9.58 907	38	0.41 093	9.96 952	5	47	8 5.1 4.9 4.8
14	9.55 891	33	9.58 944	37	0.41 056	9.96 947	5	46	9 5.7 5.6 5.4
15	9.55 923		9.58 981		0.41 019	9.96 942		45	10 6.3 6.2 6.0
16	9.55 956	33	9.59 019	38	0.40 981	9.96 937	5	44	20 12.7 12.3 12.0
17	9.55 988	32	9.59 056	37	0.40 944	9.96 932	5	43	30 19.0 18.5 18.0
18	9.56 021	33	9.59 094	38	0.40 906	9.96 927	5	42	40 25.3 24.7 24.0
19	9.56 053	32	9.59 131	37	0.40 869	9.96 922	5	41	50 31.7 30.8 30.0
20	9.56 085		9.59 168		0.40 832	9.96 917		40	
21	9.56 118	33	9.59 205	37	0.40 795	9.96 912	5	39	
22	9.56 150	32	9.59 243	38	0.40 757	9.96 907	5	38	
23	9.56 182	32	9.59 280	37	0.40 720	9.96 903	4	37	
24	9.56 215	33	9.59 317	37	0.40 683	9.96 898	5	36	
25	9.56 247		9.59 354		0.40 646	9.96 893		35	
26	9.56 279	32	9.59 391	37	0.40 609	9.96 888	5	34	
27	9.56 311	32	9.59 429	38	0.40 571	9.96 883	5	33	" 33 32 31
28	9.56 343	32	9.59 466	37	0.40 534	9.96 878	5	32	6 3.3 3.2 3.1
29	9.56 375	32	9.59 503	37	0.40 497	9.96 873	5	31	7 3.9 3.7 3.6
30	9.56 408	33	9.59 540	37	0.40 460	9.96 868	5	30	8 4.4 4.3 4.1
31	9.56 440	32	9.59 577	37	0.40 423	9.96 863	5	29	9 5.0 4.8 4.6
32	9.56 472	32	9.59 614	37	0.40 386	9.96 858	5	28	10 5.5 5.3 5.2
33	9.56 504	32	9.59 651	37	0.40 349	9.96 853	5	27	20 11.0 10.7 10.3
34	9.56 536	32	9.59 688	37	0.40 312	9.96 848	5	26	30 16.5 16.0 15.5
35	9.56 568		9.59 725		0.40 275	9.96 843		25	40 22.0 21.3 20.7
36	9.56 599	31	9.59 762	37	0.40 238	9.96 838	5	24	50 27.5 26.7 25.8
37	9.56 631	32	9.59 799	37	0.40 201	9.96 833	5	23	
38	9.56 663	32	9.59 835	36	0.40 165	9.96 828	5	22	
39	9.56 695	32	9.59 872	37	0.40 128	9.96 823	5	21	
40	9.56 727		9.59 909		0.40 091	9.96 818		20	
41	9.56 759	32	9.59 946	37	0.40 054	9.96 813	5	19	
42	9.56 790	31	9.59 983	37	0.40 017	9.96 808	5	18	
43	9.56 822	32	9.60 019	36	0.39 981	9.96 803	5	17	
44	9.56 854	32	9.60 056	37	0.39 944	9.96 798	5	16	" 6 5 4
45	9.56 886		9.60 093		0.39 907	9.96 793		15	6 0.6 0.5 0.4
46	9.56 917	31	9.60 130	37	0.39 870	9.96 788	5	14	7 0.7 0.6 0.5
47	9.56 949	32	9.60 166	36	0.39 834	9.96 783	5	13	8 0.8 0.7 0.5
48	9.56 980	31	9.60 203	37	0.39 797	9.96 778	5	12	9 0.9 0.8 0.6
49	9.57 012	32	9.60 240	37	0.39 760	9.96 772	6	11	10 1.0 0.8 0.7
50	9.57 044		9.60 276		0.39 724	9.96 767		10	20 2.0 1.7 1.3
51	9.57 075	31	9.60 313	37	0.39 687	9.96 762	5	9	30 3.0 2.5 2.0
52	9.57 107	32	9.60 349	36	0.39 651	9.96 757	5	8	40 4.0 3.3 2.7
53	9.57 138	31	9.60 386	37	0.39 614	9.96 752	5	7	50 5.0 4.2 3.3
54	9.57 169	31	9.60 422	36	0.39 578	9.96 747	5	6	
55	9.57 201		9.60 459		0.39 541	9.96 742		5	
56	9.57 232	31	9.60 495	36	0.39 505	9.96 737	5	4	
57	9.57 264	32	9.60 532	37	0.39 468	9.96 732	5	3	
58	9.57 295	31	9.60 568	36	0.39 432	9.96 727	5	2	
59	9.57 326	31	9.60 605	37	0.39 395	9.96 722	5	1	
60	9.57 358	32	9.60 641	36	0.39 359	9.96 717	5	0	
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.

\*158°

248°

\*338°

68°

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

22°

\*112°

202°

\*292°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.57 358		9.60 641		0.39 359	9.96 717	6	60	
1	9.57 389	31	9.60 677	36	0.39 323	9.96 711	5	59	
2	9.57 420	31	9.60 714	37	0.39 286	9.96 706	5	58	
3	9.57 451	31	9.60 750	36	0.39 250	9.96 701	5	57	
4	9.57 482	32	9.60 786	37	0.39 214	9.96 696	5	56	
5	9.57 514		9.60 823		0.39 177	9.96 691		55	
6	9.57 545	31	9.60 859	36	0.39 141	9.96 686	5	54	
7	9.57 576	31	9.60 895	36	0.39 105	9.96 681	5	53	
8	9.57 607	31	9.60 931	36	0.39 069	9.96 676	5	52	
9	9.57 638	31	9.60 967	37	0.39 033	9.96 670	5	51	
10	9.57 669		9.61 004		0.38 996	9.96 665		50	" 37 36 35
11	9.57 700	31	9.61 040	36	0.38 960	9.96 660	5	49	6 3.7 3.6 3.5
12	9.57 731	31	9.61 076	36	0.38 924	9.96 655	5	48	7 4.3 4.2 4.1
13	9.57 762	31	9.61 112	36	0.38 888	9.96 650	5	47	8 4.9 4.8 4.7
14	9.57 793	31	9.61 148	36	0.38 852	9.96 645	5	46	9 5.6 5.4 5.3
15	9.57 824		9.61 184		0.38 816	9.96 640		45	10 6.2 6.0 5.8
16	9.57 855	31	9.61 220	36	0.38 780	9.96 634	6	44	20 12.3 12.0 11.7
17	9.57 885	30	9.61 256	36	0.38 744	9.96 629	5	43	30 18.5 18.0 17.5
18	9.57 916	31	9.61 292	36	0.38 708	9.96 624	5	42	40 24.7 24.0 23.3
19	9.57 947	31	9.61 328	36	0.38 672	9.96 619	5	41	50 30.8 30.0 29.2
20	9.57 978		9.61 364		0.38 636	9.96 614		40	
21	9.58 008	30	9.61 400	36	0.38 600	9.96 608	6	39	
22	9.58 039	31	9.61 436	36	0.38 564	9.96 603	5	38	
23	9.58 070	31	9.61 472	36	0.38 528	9.96 598	5	37	
24	9.58 101	30	9.61 508	36	0.38 492	9.96 593	5	36	
25	9.58 131		9.61 544		0.38 456	9.96 588		35	
26	9.58 162	31	9.61 579	35	0.38 421	9.96 582	6	34	
27	9.58 192	30	9.61 615	36	0.38 385	9.96 577	5	33	" 32 31 30
28	9.58 223	31	9.61 651	36	0.38 349	9.96 572	5	32	6 3.2 3.1 3.0
29	9.58 253	30	9.61 687	36	0.38 313	9.96 567	5	31	7 3.7 3.6 3.5
30	9.58 284		9.61 722		0.38 278	9.96 562		30	8 4.3 4.1 4.0
31	9.58 314	30	9.61 758	36	0.38 242	9.96 556	6	29	9 4.8 4.6 4.5
32	9.58 345	31	9.61 794	36	0.38 206	9.96 551	5	28	10 5.3 5.2 5.0
33	9.58 375	30	9.61 830	36	0.38 170	9.96 546	5	27	20 10.7 10.3 10.0
34	9.58 406	31	9.61 865	35	0.38 135	9.96 541	5	26	30 16.0 15.5 15.0
35	9.58 436		9.61 901		0.38 099	9.96 535		25	40 21.3 20.7 20.0
36	9.58 467	31	9.61 936	35	0.38 064	9.96 530	6	24	50 26.7 25.8 25.0
37	9.58 497	30	9.61 972	36	0.38 028	9.96 525	5	23	
38	9.58 527	30	9.62 008	36	0.37 992	9.96 520	5	22	
39	9.58 557	31	9.62 043	35	0.37 957	9.96 514	6	21	
40	9.58 588		9.62 079		0.37 921	9.96 509		20	
41	9.58 618	30	9.62 114	35	0.37 886	9.96 504	5	19	
42	9.58 648	30	9.62 150	36	0.37 850	9.96 498	6	18	
43	9.58 678	30	9.62 185	35	0.37 815	9.96 493	5	17	
44	9.58 709	31	9.62 221	36	0.37 779	9.96 488	5	16	" 29 6 5
45	9.58 739		9.62 256		0.37 744	9.96 483		15	6 2.0 0.6 0.5
46	9.58 769	30	9.62 292	36	0.37 708	9.96 477	6	14	7 3.4 0.7 0.6
47	9.58 799	30	9.62 327	35	0.37 673	9.96 472	5	13	8 3.0 0.8 0.7
48	9.58 829	30	9.62 362	35	0.37 638	9.96 467	5	12	9 4.4 0.9 0.8
49	9.58 859	30	9.62 398	36	0.37 602	9.96 461	6	11	10 4.8 1.0 0.8
50	9.58 889		9.62 433		0.37 567	9.96 456		10	20 9.7 2.0 1.7
51	9.58 919	30	9.62 468	35	0.37 532	9.96 451	5	9	30 14.5 3.0 2.5
52	9.58 949	30	9.62 504	36	0.37 496	9.96 445	6	8	40 19.3 4.0 3.3
53	9.58 979	30	9.62 539	35	0.37 461	9.96 440	5	7	50 24.2 5.0 4.2
54	9.59 009	30	9.62 574	35	0.37 426	9.96 435	5	6	
55	9.59 039		9.62 609		0.37 391	9.96 429		5	
56	9.59 069	30	9.62 645	36	0.37 355	9.96 424	5	4	
57	9.59 098	29	9.62 680	35	0.37 320	9.96 419	5	3	
58	9.59 128	30	9.62 715	35	0.37 285	9.96 413	6	2	
59	9.59 158	30	9.62 750	35	0.37 250	9.96 408	5	1	
60	9.59 188	30	9.62 785	35	0.37 215	9.96 403	5	0	
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.

\*157°

247°

\*337°

67°

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

<b>23°</b>										*113°	203°	*293°
<i>l</i>	log sin	d.	log tan	c. d.	log cot	log cos	d.			Prop. Pts.		
0	9.59 188		9.62 785		0.37 215	9.96 403		<b>60</b>				
1	9.59 218	30	9.62 820	35	0.37 180	9.96 397	6	59				
2	9.59 247	29	9.62 855	35	0.37 145	9.96 392	5	58				
3	9.59 277	30	9.62 890	35	0.37 110	9.96 387	5	57				
4	9.59 307	30	9.62 926	36	0.37 074	9.96 381	6	56				
		29		35			5					
5	9.59 336		9.62 961		0.37 039	9.96 376		55				
6	9.59 366	30	9.62 996	35	0.37 004	9.96 370	6	54				
7	9.59 396	30	9.63 031	35	0.36 969	9.96 365	5	53				
8	9.59 425	29	9.63 066	35	0.36 934	9.96 360	5	52				
9	9.59 455	30	9.63 101	35	0.36 899	9.96 354	6	51				
		29		34			5					
10	9.59 484		9.63 135		0.36 865	9.96 349		<b>50</b>				
11	9.59 514	30	9.63 170	35	0.36 830	9.96 343	6	49				
12	9.59 543	29	9.63 205	35	0.36 795	9.96 338	5	48				
13	9.59 573	30	9.63 240	35	0.36 760	9.96 333	5	47				
14	9.59 602	29	9.63 275	35	0.36 725	9.96 327	6	46				
		30		35			5					
15	9.59 632		9.63 310		0.36 690	9.96 322		45				
16	9.59 661	29	9.63 345	35	0.36 655	9.96 316	6	44				
17	9.59 690	29	9.63 379	34	0.36 621	9.96 311	5	43				
18	9.59 720	30	9.63 414	35	0.36 586	9.96 305	5	42				
19	9.59 749	29	9.63 449	35	0.36 551	9.96 300	6	41				
		29		35			6					
20	9.59 778		9.63 484		0.36 516	9.96 294		<b>40</b>				
21	9.59 808	30	9.63 519	35	0.36 481	9.96 289	5	39				
22	9.59 837	29	9.63 553	34	0.36 447	9.96 284	5	38				
23	9.59 866	29	9.63 588	35	0.36 412	9.96 278	5	37				
24	9.59 895	29	9.63 623	35	0.36 377	9.96 273	5	36				
		29		34			6					
25	9.59 924		9.63 657		0.36 343	9.96 267		35				
26	9.59 954	30	9.63 692	35	0.36 308	9.96 262	5	34				
27	9.59 983	29	9.63 726	34	0.36 274	9.96 256	6	33				
28	9.60 012	29	9.63 761	35	0.36 239	9.96 251	5	32				
29	9.60 041	29	9.63 796	35	0.36 204	9.96 245	6	31				
		29		34			5					
30	9.60 070		9.63 830		0.36 170	9.96 240		<b>30</b>				
31	9.60 099	29	9.63 865	35	0.36 135	9.96 234	6	29				
32	9.60 128	29	9.63 899	34	0.36 101	9.96 229	5	28				
33	9.60 157	29	9.63 934	35	0.36 066	9.96 223	6	27				
34	9.60 186	29	9.63 968	34	0.36 032	9.96 218	5	26				
		29		35			6					
35	9.60 215		9.64 003		0.35 997	9.96 212		25				
36	9.60 244	29	9.64 037	34	0.35 963	9.96 207	5	24				
37	9.60 273	29	9.64 072	35	0.35 928	9.96 201	6	23				
38	9.60 302	29	9.64 106	34	0.35 894	9.96 196	5	22				
39	9.60 331	29	9.64 140	34	0.35 860	9.96 190	6	21				
		28		35			5					
40	9.60 359		9.64 175		0.35 825	9.96 185		<b>20</b>				
41	9.60 388	29	9.64 209	34	0.35 791	9.96 179	6	19				
42	9.60 417	29	9.64 243	34	0.35 757	9.96 174	5	18				
43	9.60 446	29	9.64 278	35	0.35 722	9.96 168	6	17				
44	9.60 474	28	9.64 312	34	0.35 688	9.96 162	6	16				
		29		34			5					
45	9.60 503		9.64 346		0.35 654	9.96 157		15				
46	9.60 532	29	9.64 381	35	0.35 619	9.96 151	6	14				
47	9.60 561	29	9.64 415	34	0.35 585	9.96 146	5	13				
48	9.60 589	28	9.64 449	34	0.35 551	9.96 140	6	12				
49	9.60 618	29	9.64 483	34	0.35 517	9.96 135	5	11				
		28		34			6					
50	9.60 646		9.64 517		0.35 483	9.96 129		<b>10</b>				
51	9.60 675	29	9.64 552	35	0.35 448	9.96 123	6	9				
52	9.60 704	29	9.64 586	34	0.35 414	9.96 118	5	8				
53	9.60 732	28	9.64 620	34	0.35 380	9.96 112	6	7				
54	9.60 761	29	9.64 654	34	0.35 346	9.96 107	5	6				
		28		34			6					
55	9.60 789		9.64 688		0.35 312	9.96 101		5				
56	9.60 818	29	9.64 722	34	0.35 278	9.96 095	6	4				
57	9.60 846	28	9.64 756	34	0.35 244	9.96 090	5	3				
58	9.60 875	29	9.64 790	34	0.35 210	9.96 084	6	2				
59	9.60 903	28	9.64 824	34	0.35 176	9.96 079	5	1				
		28		34			6					
60	9.60 931		9.64 858		0.35 142	9.96 073		<b>0</b>				
log cos	d.	log cot	c. d.	log tan	log sin	d.	<i>l</i>	Prop. Pts.				

\*156° 246° \*336°

**66°**

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

24°

\*114°

204°

\*294°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.60 931		9.64 858		0.35 142	9.96 073		60	
1	9.60 960	29	9.64 892	34	0.35 108	9.96 067	6	59	
2	9.60 988	28	9.64 926	34	0.35 074	9.96 062	5	58	
3	9.61 016	28	9.64 960	34	0.35 040	9.96 056	5	57	
4	9.61 045	28	9.64 994	34	0.35 006	9.96 050	5	56	
5	9.61 073		9.65 028		0.34 972	9.96 045		55	
6	9.61 101	28	9.65 062	34	0.34 938	9.96 039	6	54	
7	9.61 129	28	9.65 096	34	0.34 904	9.96 034	5	53	
8	9.61 158	29	9.65 130	34	0.34 870	9.96 028	6	52	
9	9.61 186	28	9.65 164	34	0.34 836	9.96 022	6	51	
				33			5		" 34 33
10	9.61 214		9.65 197		0.34 803	9.96 017		50	
11	9.61 242	28	9.65 231	34	0.34 769	9.96 011	6	49	6 3.4 3.3
12	9.61 270	28	9.65 265	34	0.34 735	9.96 005	6	48	7 4.0 3.9
13	9.61 298	28	9.65 299	34	0.34 701	9.96 000	5	47	8 4.5 4.4
14	9.61 326	28	9.65 333	33	0.34 667	9.95 994	6	46	9 5.1 5.0
									10 5.7 5.5
15	9.61 354		9.65 366		0.34 634	9.95 988		45	20 11.3 11.0
16	9.61 382	28	9.65 400	34	0.34 600	9.95 982	6	44	30 17.0 16.5
17	9.61 411	29	9.65 434	34	0.34 566	9.95 977	5	43	40 22.7 22.0
18	9.61 438	27	9.65 467	33	0.34 533	9.95 971	6	42	50 28.3 27.5
19	9.61 466	28	9.65 501	34	0.34 499	9.95 965	6	41	
							5		
20	9.61 494		9.65 535		0.34 465	9.95 960		40	
21	9.61 522	28	9.65 568	33	0.34 432	9.95 954	6	39	
22	9.61 550	28	9.65 602	34	0.34 398	9.95 948	6	38	
23	9.61 578	28	9.65 636	34	0.34 364	9.95 942	6	37	
24	9.61 606	28	9.65 669	33	0.34 331	9.95 937	5	36	
				34			6		
25	9.61 634		9.65 703		0.34 297	9.95 931		35	
26	9.61 662	28	9.65 736	33	0.34 264	9.95 925	6	34	
27	9.61 689	27	9.65 770	34	0.34 230	9.95 920	5	33	" 29 28 27
28	9.61 717	28	9.65 803	33	0.34 197	9.95 914	6	32	6 2.9 2.8 2.7
29	9.61 745	28	9.65 837	34	0.34 163	9.95 908	6	31	7 3.4 3.3 3.2
				33			6		8 3.9 3.7 3.6
30	9.61 773		9.65 870		0.34 130	9.95 902		30	9 4.4 4.2 4.1
31	9.61 800	27	9.65 904	34	0.34 096	9.95 897	5	29	10 4.8 4.7 4.5
32	9.61 828	28	9.65 937	33	0.34 063	9.95 891	6	28	20 9.7 9.3 9.0
33	9.61 856	28	9.65 971	34	0.34 029	9.95 885	6	27	30 14.5 14.0 13.5
34	9.61 883	27	9.66 004	33	0.33 996	9.95 879	6	26	40 19.3 18.7 18.0
				34			6		50 24.2 23.3 22.5
35	9.61 911		9.66 038		0.33 962	9.95 873		25	
36	9.61 939	28	9.66 071	33	0.33 929	9.95 868	5	24	
37	9.61 966	27	9.66 104	33	0.33 896	9.95 862	6	23	
38	9.61 994	28	9.66 138	34	0.33 862	9.95 856	6	22	
39	9.62 021	27	9.66 171	33	0.33 829	9.95 850	6	21	
				33			6		
40	9.62 049		9.66 204		0.33 796	9.95 844		20	
41	9.62 076	27	9.66 238	34	0.33 762	9.95 839	5	19	
42	9.62 104	28	9.66 271	33	0.33 729	9.95 833	6	18	
43	9.62 131	27	9.66 304	33	0.33 696	9.95 827	6	17	
44	9.62 159	28	9.66 337	33	0.33 663	9.95 821	6	16	
				34			6		" 6 5
45	9.62 186		9.66 371		0.33 629	9.95 815		15	6 0.6 0.5
46	9.62 214	28	9.66 404	33	0.33 596	9.95 810	5	14	7 0.7 0.6
47	9.62 241	27	9.66 437	33	0.33 563	9.95 804	6	13	8 0.8 0.7
48	9.62 268	27	9.66 470	33	0.33 530	9.95 798	6	12	9 0.9 0.8
49	9.62 296	28	9.66 503	33	0.33 497	9.95 792	6	11	10 1.0 0.8
				34			6		20 2.0 1.7
50	9.62 323	27	9.66 537	33	0.33 463	9.95 786	6	10	30 3.0 2.5
51	9.62 350	27	9.66 570	33	0.33 430	9.95 780	6	9	40 4.0 3.3
52	9.62 377	27	9.66 603	33	0.33 397	9.95 775	5	8	50 5.0 4.2
53	9.62 405	28	9.66 636	33	0.33 364	9.95 769	6	7	
54	9.62 432	27	9.66 669	33	0.33 331	9.95 763	6	6	
				33			6		
55	9.62 459		9.66 702		0.33 298	9.95 757		5	
56	9.62 486	27	9.66 735	33	0.33 265	9.95 751	6	4	
57	9.62 513	27	9.66 768	33	0.33 232	9.95 745	6	3	
58	9.62 541	28	9.66 801	33	0.33 199	9.95 739	6	2	
59	9.62 568	27	9.66 834	33	0.33 166	9.95 733	6	1	
				33			5		
60	9.62 595		9.66 867		0.33 133	9.95 728		0	
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.

\*155°

245°

\*335°

65°

<b>25°</b>										*115°	205°	*295°
<i>l</i>	log sin	d.	log tan	c. d.	log cot	log cos	d.			Prop. Pts.		
0	9.62 595		9.66 867		0.33 133	9.95 728	6		<b>60</b>			
1	9.62 622	27	9.66 900	33	0.33 100	9.95 722	6		59			
2	9.62 649	27	9.66 933	33	0.33 067	9.95 716	6		58			
3	9.62 676	27	9.66 966	33	0.33 034	9.95 710	6		57			
4	9.62 703	27	9.66 999	33	0.33 001	9.95 704	6		56			
5	9.62 730		9.67 032		0.32 968	9.95 698	6		55			
6	9.62 757	27	9.67 065	33	0.32 935	9.95 692	6		54			
7	9.62 784	27	9.67 098	33	0.32 902	9.95 686	6		53			
8	9.62 811	27	9.67 131	33	0.32 869	9.95 680	6		52			
9	9.62 838	27	9.67 163	32	0.32 837	9.95 674	6		51			
10	9.62 865		9.67 196		0.32 804	9.95 668	6		<b>50</b>			
11	9.62 892	27	9.67 229	33	0.32 771	9.95 663	5		49			
12	9.62 918	26	9.67 262	33	0.32 738	9.95 657	6		48			
13	9.62 945	27	9.67 295	33	0.32 705	9.95 651	6		47			
14	9.62 972	27	9.67 327	33	0.32 673	9.95 645	6		46			
15	9.62 999		9.67 360		0.32 640	9.95 639	6		45			
16	9.63 026	26	9.67 393	33	0.32 607	9.95 633	6		44			
17	9.63 052	27	9.67 426	33	0.32 574	9.95 627	6		43			
18	9.63 079	27	9.67 458	32	0.32 542	9.95 621	6		42			
19	9.63 106	27	9.67 491	33	0.32 509	9.95 615	6		41			
20	9.63 133		9.67 524		0.32 476	9.95 609	6		<b>40</b>			
21	9.63 159	27	9.67 556	32	0.32 444	9.95 603	6		39			
22	9.63 186	27	9.67 589	33	0.32 411	9.95 597	6		38			
23	9.63 213	26	9.67 622	33	0.32 378	9.95 591	6		37			
24	9.63 239	27	9.67 654	32	0.32 346	9.95 585	6		36			
25	9.63 266		9.67 687		0.32 313	9.95 579	6		35			
26	9.63 292	26	9.67 719	32	0.32 281	9.95 573	6		34			
27	9.63 319	27	9.67 752	33	0.32 248	9.95 567	6		33			
28	9.63 345	26	9.67 785	33	0.32 215	9.95 561	6		32			
29	9.63 372	26	9.67 817	32	0.32 183	9.95 555	6		31			
30	9.63 398		9.67 850		0.32 150	9.95 549	6		<b>30</b>			
31	9.63 425	26	9.67 882	32	0.32 118	9.95 543	6		29			
32	9.63 451	27	9.67 915	33	0.32 085	9.95 537	6		28			
33	9.63 478	26	9.67 947	32	0.32 053	9.95 531	6		27			
34	9.63 504	27	9.67 980	33	0.32 020	9.95 525	6		26			
35	9.63 531		9.68 012		0.31 988	9.95 519	6		25			
36	9.63 557	26	9.68 044	32	0.31 956	9.95 513	6		24			
37	9.63 583	26	9.68 077	33	0.31 923	9.95 507	6		23			
38	9.63 610	27	9.68 109	32	0.31 891	9.95 500	7		22			
39	9.63 636	26	9.68 142	33	0.31 858	9.95 494	6		21			
40	9.63 662		9.68 174		0.31 826	9.95 488	6		<b>20</b>			
41	9.63 689	27	9.68 206	32	0.31 794	9.95 482	6		19			
42	9.63 715	26	9.68 239	33	0.31 761	9.95 476	6		18			
43	9.63 741	26	9.68 271	32	0.31 729	9.95 470	6		17			
44	9.63 767	27	9.68 303	32	0.31 697	9.95 464	6		16			
45	9.63 794		9.68 336		0.31 664	9.95 458	6		15			
46	9.63 820	26	9.68 368	32	0.31 632	9.95 452	6		14			
47	9.63 846	26	9.68 400	32	0.31 600	9.95 446	6		13			
48	9.63 872	26	9.68 432	32	0.31 568	9.95 440	6		12			
49	9.63 898	26	9.68 465	33	0.31 535	9.95 434	6		11			
50	9.63 924		9.68 497		0.31 503	9.95 427	7		<b>10</b>			
51	9.63 950	26	9.68 529	32	0.31 471	9.95 421	6		9			
52	9.63 976	26	9.68 561	32	0.31 439	9.95 415	6		8			
53	9.64 002	26	9.68 593	32	0.31 407	9.95 409	6		7			
54	9.64 028	26	9.68 626	33	0.31 374	9.95 403	6		6			
55	9.64 054		9.68 658		0.31 342	9.95 397	6		5			
56	9.64 080	26	9.68 690	32	0.31 310	9.95 391	6		4			
57	9.64 106	26	9.68 722	32	0.31 278	9.95 384	7		3			
58	9.64 132	26	9.68 754	32	0.31 246	9.95 378	6		2			
59	9.64 158	26	9.68 786	32	0.31 214	9.95 372	6		1			
60	9.64 184	26	9.68 818	32	0.31 182	9.95 366	6		<b>0</b>			
	log cos	d.	log cot	c. d.	log tan	log sin	d.	<i>l</i>		Prop. Pts.		

\*154°    244°    \*334°

**64°**

<b>26°</b>										*116°	206°	*296°
'	log sin	d.	log tan	c. d.	log cot	log cos	d.	Prop. Pts.				
0	9.64 184		9.68 818		0.31 182	9.95 366	6	<b>60</b>				
1	9.64 210	26	9.68 850	32	0.31 150	9.95 360	6	59				
2	9.64 236	26	9.68 882	32	0.31 118	9.95 354	6	58				
3	9.64 262	26	9.68 914	32	0.31 086	9.95 348	7	57				
4	9.64 288	25	9.68 946	32	0.31 054	9.95 341	6	56				
5	9.64 313		9.68 978		0.31 022	9.95 335	6	55				
6	9.64 339	26	9.69 010	32	0.30 990	9.95 329	6	54				
7	9.64 365	26	9.69 042	32	0.30 958	9.95 323	6	53				
8	9.64 391	26	9.69 074	32	0.30 926	9.95 317	7	52				
9	9.64 417	25	9.69 106	32	0.30 894	9.95 310	6	51				
10	9.64 442		9.69 138		0.30 862	9.95 304	6	<b>50</b>				
11	9.64 468	26	9.69 170	32	0.30 830	9.95 298	6	49				
12	9.64 494	25	9.69 202	32	0.30 798	9.95 292	6	48				
13	9.64 519	26	9.69 234	32	0.30 766	9.95 286	7	47				
14	9.64 545	26	9.69 266	32	0.30 734	9.95 279	6	46				
15	9.64 571		9.69 298		0.30 702	9.95 273	6	45				
16	9.64 596	25	9.69 329	31	0.30 671	9.95 267	6	44				
17	9.64 622	26	9.69 361	32	0.30 639	9.95 261	6	43				
18	9.64 647	25	9.69 393	32	0.30 607	9.95 254	7	42				
19	9.64 673	25	9.69 425	32	0.30 575	9.95 248	6	41				
20	9.64 698		9.69 457		0.30 543	9.95 242	6	<b>40</b>				
21	9.64 724	26	9.69 488	31	0.30 512	9.95 236	6	39				
22	9.64 749	25	9.69 520	32	0.30 480	9.95 229	7	38				
23	9.64 775	26	9.69 552	32	0.30 448	9.95 223	6	37				
24	9.64 800	25	9.69 584	32	0.30 416	9.95 217	6	36				
25	9.64 826	25	9.69 615	32	0.30 385	9.95 211	7	35				
26	9.64 851	26	9.69 647	32	0.30 353	9.95 204	6	34				
27	9.64 877	26	9.69 679	32	0.30 321	9.95 198	6	33				
28	9.64 902	25	9.69 710	31	0.30 290	9.95 192	6	32				
29	9.64 927	26	9.69 742	32	0.30 258	9.95 185	7	31				
30	9.64 953		9.69 774		0.30 226	9.95 179	6	<b>30</b>				
31	9.64 978	25	9.69 805	31	0.30 195	9.95 173	6	29				
32	9.65 003	25	9.69 837	32	0.30 163	9.95 167	6	28				
33	9.65 029	26	9.69 868	31	0.30 132	9.95 160	7	27				
34	9.65 054	25	9.69 900	32	0.30 100	9.95 154	6	26				
35	9.65 079		9.69 932		0.30 068	9.95 148	6	25				
36	9.65 104	25	9.69 963	31	0.30 037	9.95 141	7	24				
37	9.65 130	26	9.69 995	32	0.30 005	9.95 135	6	23				
38	9.65 155	25	9.70 026	31	0.29 974	9.95 129	6	22				
39	9.65 180	25	9.70 058	32	0.29 942	9.95 122	7	21				
40	9.65 205		9.70 089		0.29 911	9.95 116	6	<b>20</b>				
41	9.65 230	25	9.70 121	32	0.29 879	9.95 110	7	19				
42	9.65 255	26	9.70 152	31	0.29 848	9.95 103	6	18				
43	9.65 281	25	9.70 184	32	0.29 816	9.95 097	6	17				
44	9.65 306	25	9.70 215	31	0.29 785	9.95 090	7	16				
45	9.65 331		9.70 247		0.29 753	9.95 084	6	15				
46	9.65 356	25	9.70 278	31	0.29 722	9.95 078	6	14				
47	9.65 381	25	9.70 309	31	0.29 691	9.95 071	7	13				
48	9.65 406	25	9.70 341	32	0.29 659	9.95 065	6	12				
49	9.65 431	25	9.70 372	31	0.29 628	9.95 059	6	11				
50	9.65 456	24	9.70 404	32	0.29 596	9.95 052	7	<b>10</b>				
51	9.65 481	25	9.70 435	31	0.29 565	9.95 046	6	9				
52	9.65 506	25	9.70 466	31	0.29 534	9.95 039	7	8				
53	9.65 531	25	9.70 498	32	0.29 502	9.95 033	6	7				
54	9.65 556	24	9.70 529	31	0.29 471	9.95 027	6	6				
55	9.65 580		9.70 560		0.29 440	9.95 020	7	5				
56	9.65 605	25	9.70 592	32	0.29 408	9.95 014	6	4				
57	9.65 630	25	9.70 623	31	0.29 377	9.95 007	7	3				
58	9.65 655	25	9.70 654	31	0.29 346	9.95 001	6	2				
59	9.65 680	25	9.70 685	31	0.29 315	9.94 995	6	1				
60	9.65 705	25	9.70 717	32	0.29 283	9.94 988	7	0				
log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.				

\*153°    243°    \*333°

**63°**

27°

\*117°

207°

\*297°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.65 705		9.70 717		0.29 283	9.94 988	6	<b>60</b>	
1	9.65 729	24	9.70 748	31	0.29 252	9.94 982	7	59	
2	9.65 754	25	9.70 779	31	0.29 221	9.94 975	6	58	
3	9.65 779	25	9.70 810	31	0.29 190	9.94 969	7	57	
4	9.65 804	24	9.70 841	32	0.29 159	9.94 962	6	56	
5	9.65 828		9.70 873		0.29 127	9.94 956		55	
6	9.65 853	25	9.70 904	31	0.29 096	9.94 949	7	54	
7	9.65 878	25	9.70 935	31	0.29 065	9.94 943	6	53	
8	9.65 902	24	9.70 966	31	0.29 034	9.94 936	7	52	
9	9.65 927	25	9.70 997	31	0.29 003	9.94 930	6	51	
<b>10</b>	9.65 952		9.71 028		0.28 972	9.94 923		<b>50</b>	
11	9.65 976	24	9.71 059	31	0.28 941	9.94 917	6	49	
12	9.66 001	25	9.71 090	31	0.28 910	9.94 911	7	48	
13	9.66 025	24	9.71 121	31	0.28 879	9.94 904	6	47	
14	9.66 050	25	9.71 153	32	0.28 847	9.94 898	6	46	
15	9.66 075		9.71 184		0.28 816	9.94 891		45	
16	9.66 099	24	9.71 215	31	0.28 785	9.94 885	6	44	
17	9.66 124	25	9.71 246	31	0.28 754	9.94 878	7	43	
18	9.66 148	24	9.71 277	31	0.28 723	9.94 871	7	42	
19	9.66 173	25	9.71 308	31	0.28 692	9.94 865	6	41	
20	9.66 197		9.71 339		0.28 661	9.94 858		<b>40</b>	
21	9.66 221	24	9.71 370	31	0.28 630	9.94 852	6	39	
22	9.66 246	25	9.71 401	31	0.28 599	9.94 845	7	38	
23	9.66 270	24	9.71 431	30	0.28 569	9.94 839	6	37	
24	9.66 295	25	9.71 462	31	0.28 538	9.94 832	7	36	
25	9.66 319		9.71 493		0.28 507	9.94 826		35	
26	9.66 343	24	9.71 524	31	0.28 476	9.94 819	7	34	
27	9.66 368	25	9.71 555	31	0.28 445	9.94 813	6	33	
28	9.66 392	24	9.71 586	31	0.28 414	9.94 806	7	32	
29	9.66 416	24	9.71 617	31	0.28 383	9.94 799	6	31	
30	9.66 441	25	9.71 648	31	0.28 352	9.94 793	7	<b>30</b>	
31	9.66 465	24	9.71 679	31	0.28 321	9.94 786	6	29	
32	9.66 489	24	9.71 709	30	0.28 291	9.94 780	6	28	
33	9.66 513	24	9.71 740	31	0.28 260	9.94 773	7	27	
34	9.66 537	24	9.71 771	31	0.28 229	9.94 767	6	26	
35	9.66 562		9.71 802		0.28 198	9.94 760		25	
36	9.66 586	24	9.71 833	31	0.28 167	9.94 753	7	24	
37	9.66 610	24	9.71 863	30	0.28 137	9.94 747	6	23	
38	9.66 634	24	9.71 894	31	0.28 106	9.94 740	6	22	
39	9.66 658	24	9.71 925	31	0.28 075	9.94 734	7	21	
<b>40</b>	9.66 682		9.71 955		0.28 045	9.94 727		<b>20</b>	
41	9.66 706	24	9.71 986	31	0.28 014	9.94 720	7	19	
42	9.66 731	25	9.72 017	31	0.27 983	9.94 714	6	18	
43	9.66 755	24	9.72 048	31	0.27 952	9.94 707	7	17	
44	9.66 779	24	9.72 078	30	0.27 922	9.94 700	7	16	
45	9.66 803		9.72 109		0.27 891	9.94 694		15	
46	9.66 827	24	9.72 140	31	0.27 860	9.94 687	7	14	
47	9.66 851	24	9.72 170	30	0.27 830	9.94 680	6	13	
48	9.66 875	24	9.72 201	31	0.27 799	9.94 674	7	12	
49	9.66 899	24	9.72 231	30	0.27 769	9.94 667	7	11	
50	9.66 922	23	9.72 262	31	0.27 738	9.94 660	7	<b>10</b>	
51	9.66 946	24	9.72 293	31	0.27 707	9.94 654	6	9	
52	9.66 970	24	9.72 323	30	0.27 677	9.94 647	7	8	
53	9.66 994	24	9.72 354	31	0.27 646	9.94 640	7	7	
54	9.67 018	24	9.72 384	30	0.27 616	9.94 634	6	6	
55	9.67 042		9.72 415		0.27 585	9.94 627		5	
56	9.67 066	24	9.72 445	30	0.27 555	9.94 620	7	4	
57	9.67 090	24	9.72 476	31	0.27 524	9.94 614	6	3	
58	9.67 113	23	9.72 506	30	0.27 494	9.94 607	7	2	
59	9.67 137	24	9.72 537	31	0.27 463	9.94 600	7	1	
<b>60</b>	9.67 161		9.72 567		0.27 433	9.94 593		<b>0</b>	

	32	31	30
6	3.2	3.1	3.0
7	3.7	3.6	3.5
8	4.3	4.1	4.0
9	4.8	4.6	4.5
10	5.3	5.2	5.0
20	10.7	10.3	10.0
30	16.0	15.5	15.0
40	21.3	20.7	20.0
50	26.7	25.8	25.0

	25	24	23
6	2.5	2.4	2.3
7	2.9	2.8	2.7
8	3.3	3.2	3.1
9	3.8	3.6	3.5
10	4.2	4.0	3.8
20	8.3	8.0	7.7
30	12.5	12.0	11.5
40	16.7	16.0	15.3
50	20.8	20.0	19.2

	7	6
6	0.7	0.6
7	0.8	0.7
8	0.9	0.8
9	1.0	0.9
10	1.2	1.0
20	2.3	2.0
30	3.5	3.0
40	4.7	4.0
50	5.8	5.0

\*152° 242° \*332°

62°



LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

<b>28°</b>										*118°	208°	*298°
'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.			
0	9.67 161		9.72 567		0.27 433	9.94 593		60				
1	9.67 185	24	9.72 598	31	0.27 402	9.94 587	6	59				
2	9.67 208	23	9.72 628	30	0.27 372	9.94 580	7	58				
3	9.67 232	24	9.72 659	31	0.27 341	9.94 573	7	57				
4	9.67 256	24	9.72 689	30	0.27 311	9.94 567	6	56				
5	9.67 280	24	9.72 720	31	0.27 280	9.94 560	7	55				
6	9.67 303	23	9.72 750	30	0.27 250	9.94 553	7	54				
7	9.67 327	24	9.72 780	30	0.27 220	9.94 546	7	53				
8	9.67 350	23	9.72 811	31	0.27 189	9.94 540	6	52				
9	9.67 374	24	9.72 841	30	0.27 159	9.94 533	7	51				
10	9.67 398	24	9.72 872	31	0.27 128	9.94 526	7	50	" 31 30 29			
11	9.67 421	23	9.72 902	30	0.27 098	9.94 519	7	49	6 3.1 3.0 2.9			
12	9.67 445	24	9.72 932	30	0.27 068	9.94 513	6	48	7 3.6 3.5 3.4			
13	9.67 468	23	9.72 963	31	0.27 037	9.94 506	7	47	8 4.1 4.0 3.9			
14	9.67 492	24	9.72 993	30	0.27 007	9.94 499	7	46	9 4.6 4.5 4.4			
15	9.67 515	23	9.73 023	30	0.26 977	9.94 492	7	45	10 5.2 5.0 4.8			
16	9.67 539	24	9.73 054	31	0.26 946	9.94 485	7	44	20 10.3 10.0 9.7			
17	9.67 562	23	9.73 084	30	0.26 916	9.94 479	6	43	30 15.5 15.0 14.5			
18	9.67 586	24	9.73 114	30	0.26 886	9.94 472	7	42	40 20.7 20.0 19.3			
19	9.67 609	23	9.73 144	30	0.26 856	9.94 465	7	41	50 25.8 25.0 24.2			
20	9.67 633	24	9.73 175	31	0.26 825	9.94 458	7	40				
21	9.67 656	23	9.73 205	30	0.26 795	9.94 451	7	39				
22	9.67 680	24	9.73 235	30	0.26 765	9.94 445	6	38				
23	9.67 703	23	9.73 265	30	0.26 735	9.94 438	7	37				
24	9.67 726	24	9.73 295	30	0.26 705	9.94 431	7	36				
25	9.67 750	23	9.73 326	31	0.26 674	9.94 424	7	35				
26	9.67 773	23	9.73 356	30	0.26 644	9.94 417	7	34	" 24 23 22			
27	9.67 796	24	9.73 386	30	0.26 614	9.94 410	7	33	6 2.4 2.3 2.2			
28	9.67 820	23	9.73 416	30	0.26 584	9.94 404	6	32	7 2.8 2.7 2.6			
29	9.67 843	24	9.73 446	30	0.26 554	9.94 397	7	31	8 3.2 3.1 2.9			
30	9.67 866	23	9.73 476	30	0.26 524	9.94 390	7	30	9 3.6 3.5 3.3			
31	9.67 890	24	9.73 507	31	0.26 493	9.94 383	7	29	10 4.0 3.8 3.7			
32	9.67 913	23	9.73 537	30	0.26 463	9.94 376	7	28	20 8.0 7.7 7.3			
33	9.67 936	24	9.73 567	30	0.26 433	9.94 369	7	27	30 12.0 11.5 11.0			
34	9.67 959	23	9.73 597	30	0.26 403	9.94 362	7	26	40 16.0 15.3 14.7			
35	9.67 982	24	9.73 627	30	0.26 373	9.94 355	7	25	50 20.0 19.2 18.3			
36	9.68 006	23	9.73 657	30	0.26 343	9.94 349	6	24				
37	9.68 029	24	9.73 687	30	0.26 313	9.94 342	7	23				
38	9.68 052	23	9.73 717	30	0.26 283	9.94 335	7	22				
39	9.68 075	24	9.73 747	30	0.26 253	9.94 328	7	21				
40	9.68 098	23	9.73 777	30	0.26 223	9.94 321	7	20				
41	9.68 121	24	9.73 807	30	0.26 193	9.94 314	7	19				
42	9.68 144	23	9.73 837	30	0.26 163	9.94 307	7	18				
43	9.68 167	24	9.73 867	30	0.26 133	9.94 300	7	17				
44	9.68 190	23	9.73 897	30	0.26 103	9.94 293	7	16	" 7 6			
45	9.68 213	24	9.73 927	30	0.26 073	9.94 286	7	15	6 0.7 0.6			
46	9.68 237	23	9.73 957	30	0.26 043	9.94 279	7	14	7 0.8 0.7			
47	9.68 260	24	9.73 987	30	0.26 013	9.94 273	6	13	8 0.9 0.8			
48	9.68 283	23	9.74 017	30	0.25 983	9.94 266	7	12	9 1.0 0.9			
49	9.68 305	24	9.74 047	30	0.25 953	9.94 259	7	11	10 1.2 1.0			
50	9.68 328	23	9.74 077	30	0.25 923	9.94 252	7	10	20 2.3 2.0			
51	9.68 351	24	9.74 107	30	0.25 893	9.94 245	7	9	30 3.5 3.0			
52	9.68 374	23	9.74 137	30	0.25 863	9.94 238	7	8	40 4.7 4.0			
53	9.68 397	24	9.74 166	29	0.25 834	9.94 231	7	7	50 5.8 5.0			
54	9.68 420	23	9.74 196	30	0.25 804	9.94 224	7	6				
55	9.68 443	24	9.74 226	30	0.25 774	9.94 217	7	5				
56	9.68 466	23	9.74 256	30	0.25 744	9.94 210	7	4				
57	9.68 489	24	9.74 286	30	0.25 714	9.94 203	7	3				
58	9.68 512	23	9.74 316	30	0.25 684	9.94 196	7	2				
59	9.68 534	24	9.74 345	29	0.25 655	9.94 189	7	1				
60	9.68 557	23	9.74 375	30	0.25 625	9.94 182	7	0				
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.			

\*151° 241° \*331°

**61°**

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

29°

\*119°

209°

\*299°

	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.68 557		9.74 375		0.25 625	9.94 182		60	
1	9.68 580	23	9.74 405	30	0.25 595	9.94 175	7	59	
2	9.68 603	23	9.74 435	30	0.25 565	9.94 168	7	58	
3	9.68 625	22	9.74 465	30	0.25 535	9.94 161	7	57	
4	9.68 648	23	9.74 494	29	0.25 506	9.94 154	7	56	
5	9.68 671	23	9.74 524	30	0.25 476	9.94 147	7	55	
6	9.68 694	22	9.74 554	29	0.25 446	9.94 140	7	54	
7	9.68 716	23	9.74 583	30	0.25 417	9.94 133	7	53	
8	9.68 739	23	9.74 613	30	0.25 387	9.94 126	7	52	
9	9.68 762	22	9.74 643	30	0.25 357	9.94 119	7	51	
10	9.68 784		9.74 673		0.25 327	9.94 112		50	" 30 29
11	9.68 807	23	9.74 702	29	0.25 298	9.94 105	7	49	6 3.0 2.9
12	9.68 829	22	9.74 732	30	0.25 268	9.94 098	7	48	7 3.5 3.5
13	9.68 852	23	9.74 762	30	0.25 238	9.94 090	8	47	8 4.0 3.9
14	9.68 875	23	9.74 791	29	0.25 209	9.94 083	7	46	9 4.5 4.4
15	9.68 897	22	9.74 821	30	0.25 179	9.94 076		45	10 5.0 4.8
16	9.68 920	23	9.74 851	30	0.25 149	9.94 069	7	44	20 10.0 9.7
17	9.68 942	22	9.74 880	29	0.25 120	9.94 062	7	43	30 15.0 14.5
18	9.68 965	23	9.74 910	30	0.25 090	9.94 055	7	42	40 20.0 19.3
19	9.68 987	22	9.74 939	29	0.25 061	9.94 048	7	41	50 25.0 24.2
20	9.69 010		9.74 969		0.25 031	9.94 041		40	
21	9.69 032	22	9.74 998	29	0.25 002	9.94 034	7	39	
22	9.69 055	23	9.75 028	30	0.24 972	9.94 027	7	38	
23	9.69 077	22	9.75 058	30	0.24 942	9.94 020	7	37	
24	9.69 100	23	9.75 087	29	0.24 913	9.94 012	8	36	
25	9.69 122	22	9.75 117	30	0.24 883	9.94 005	7	35	
26	9.69 144	23	9.75 146	29	0.24 854	9.93 998	7	34	
27	9.69 167	22	9.75 176	30	0.24 824	9.93 991	7	33	[" 23 22
28	9.69 189	23	9.75 205	29	0.24 795	9.93 984	7	32	6 2.3 2.2
29	9.69 212	22	9.75 235	30	0.24 765	9.93 977	7	31	7 2.7 2.6
30	9.69 234	23	9.75 264	29	0.24 736	9.93 970	7	30	8 3.1 2.9
31	9.69 256	22	9.75 294	30	0.24 706	9.93 963	8	29	9 3.4 3.3
32	9.69 279	23	9.75 323	29	0.24 677	9.93 955	7	28	10 3.8 3.7
33	9.69 301	22	9.75 353	30	0.24 647	9.93 948	7	27	20 7.7 7.3
34	9.69 323	23	9.75 382	29	0.24 618	9.93 941	7	26	30 11.5 11.0
35	9.69 345	22	9.75 411	30	0.24 589	9.93 934	7	25	40 15.3 14.7
36	9.69 368	23	9.75 441	29	0.24 559	9.93 927	7	24	50 19.2 18.3
37	9.69 390	22	9.75 470	30	0.24 530	9.93 920	8	23	
38	9.69 412	23	9.75 500	29	0.24 500	9.93 912	7	22	
39	9.69 434	22	9.75 529	30	0.24 471	9.93 905	7	21	
40	9.69 456		9.75 558		0.24 442	9.93 898		20	
41	9.69 479	23	9.75 588	29	0.24 412	9.93 891	7	19	
42	9.69 501	22	9.75 617	30	0.24 383	9.93 884	7	18	
43	9.69 523	23	9.75 647	29	0.24 353	9.93 876	8	17	
44	9.69 545	22	9.75 676	30	0.24 324	9.93 869	7	16	" 8 7
45	9.69 567	23	9.75 705	29	0.24 295	9.93 862	7	15	6 0.8 0.7
46	9.69 589	22	9.75 735	30	0.24 265	9.93 855	7	14	7 0.9 0.8
47	9.69 611	23	9.75 764	29	0.24 236	9.93 847	8	13	8 1.1 0.9
48	9.69 633	22	9.75 793	30	0.24 207	9.93 840	7	12	9 1.2 1.0
49	9.69 655	23	9.75 822	29	0.24 178	9.93 833	7	11	10 1.3 1.2
50	9.69 677	22	9.75 852	30	0.24 148	9.93 826	7	10	20 2.7 2.3
51	9.69 699	23	9.75 881	29	0.24 119	9.93 819	7	9	30 4.0 3.5
52	9.69 721	22	9.75 910	30	0.24 090	9.93 811	8	8	40 5.3 4.7
53	9.69 743	23	9.75 939	29	0.24 061	9.93 804	7	7	50 6.7 5.8
54	9.69 765	22	9.75 969	30	0.24 031	9.93 797	7	6	
55	9.69 787	23	9.75 998	29	0.24 002	9.93 789	8	5	
56	9.69 809	22	9.76 027	30	0.23 973	9.93 782	7	4	
57	9.69 831	23	9.76 056	29	0.23 944	9.93 775	7	3	
58	9.69 853	22	9.76 086	30	0.23 914	9.93 768	7	2	
59	9.69 875	23	9.76 115	29	0.23 885	9.93 760	8	1	
60	9.69 897	22	9.76 144	30	0.23 856	9.93 753	7	0	
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.

\*150°

240°

\*330°

60°

30°

\*120°

210°

\*300°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.69 897		9.76 144		0.23 856	9.93 753		60	
1	9.69 919	22	9.76 173	29	0.23 827	9.93 746	7	59	
2	9.69 941	22	9.76 202	29	0.23 798	9.93 738	7	58	
3	9.69 963	21	9.76 231	30	0.23 769	9.93 731	7	57	
4	9.69 984	22	9.76 261	29	0.23 739	9.93 724	7	56	
5	9.70 006	22	9.76 290	29	0.23 710	9.93 717	8	55	
6	9.70 028	22	9.76 319	29	0.23 681	9.93 709	7	54	
7	9.70 050	22	9.76 348	29	0.23 652	9.93 702	7	53	
8	9.70 072	21	9.76 377	29	0.23 623	9.93 695	8	52	
9	9.70 093	22	9.76 406	29	0.23 594	9.93 687	7	51	
10	9.70 115	22	9.76 435	29	0.23 565	9.93 680	7	50	" 30 29 28
11	9.70 137	22	9.76 464	29	0.23 536	9.93 673	8	49	6 3.0 2.9 2.8
12	9.70 159	21	9.76 493	29	0.23 507	9.93 665	8	48	7 3.5 3.4 3.3
13	9.70 180	22	9.76 522	29	0.23 478	9.93 658	7	47	8 4.0 3.9 3.7
14	9.70 202	22	9.76 551	29	0.23 449	9.93 650	8	46	9 4.5 4.4 4.2
15	9.70 224	21	9.76 580	29	0.23 420	9.93 643	10	45	10 5.0 4.8 4.7
16	9.70 245	22	9.76 609	29	0.23 391	9.93 636	20	44	20 10.0 9.7 9.3
17	9.70 267	21	9.76 639	30	0.23 361	9.93 628	30	43	30 15.0 14.5 14.0
18	9.70 288	22	9.76 668	29	0.23 332	9.93 621	40	42	40 20.0 19.3 18.7
19	9.70 310	22	9.76 697	28	0.23 303	9.93 614	50	41	50 25.0 24.2 23.3
20	9.70 332	21	9.76 725	29	0.23 275	9.93 606		40	
21	9.70 353	22	9.76 754	29	0.23 246	9.93 599	7	39	
22	9.70 375	21	9.76 783	29	0.23 217	9.93 591	8	38	
23	9.70 396	22	9.76 812	29	0.23 188	9.93 584	7	37	
24	9.70 418	21	9.76 841	29	0.23 159	9.93 577	7	36	
25	9.70 439	22	9.76 870	29	0.23 130	9.93 569	8	35	
26	9.70 461	21	9.76 899	29	0.23 101	9.93 562	7	34	
27	9.70 482	22	9.76 928	29	0.23 072	9.93 554	8	33	" 22 21
28	9.70 504	21	9.76 957	29	0.23 043	9.93 547	7	32	6 2.2 2.1
29	9.70 525	22	9.76 986	29	0.23 014	9.93 539	8	31	7 2.6 2.4
30	9.70 547	21	9.77 015	29	0.22 985	9.93 532	7	30	8 2.9 2.8
31	9.70 568	22	9.77 044	29	0.22 956	9.93 525	9	29	9 3.3 3.2
32	9.70 590	21	9.77 073	29	0.22 927	9.93 517	10	28	10 3.7 3.5
33	9.70 611	22	9.77 101	28	0.22 899	9.93 510	20	27	20 7.3 7.0
34	9.70 633	21	9.77 130	29	0.22 870	9.93 502	30	26	30 11.0 10.5
35	9.70 654	22	9.77 159	29	0.22 841	9.93 495	40	25	40 14.7 14.0
36	9.70 675	21	9.77 188	29	0.22 812	9.93 487	50	24	50 18.3 17.5
37	9.70 697	22	9.77 217	29	0.22 783	9.93 480		23	
38	9.70 718	21	9.77 246	29	0.22 754	9.93 472	7	22	
39	9.70 739	22	9.77 274	29	0.22 726	9.93 465	8	21	
40	9.70 761	21	9.77 303	29	0.22 697	9.93 457		20	
41	9.70 782	22	9.77 332	29	0.22 668	9.93 450	7	19	
42	9.70 803	21	9.77 361	29	0.22 639	9.93 442	8	18	
43	9.70 824	22	9.77 390	28	0.22 610	9.93 435	7	17	
44	9.70 846	21	9.77 418	29	0.22 582	9.93 427	8	16	" 8 7
45	9.70 867	22	9.77 447	29	0.22 553	9.93 420	7	15	6 0.8 0.7
46	9.70 888	21	9.77 476	29	0.22 524	9.93 412	8	14	7 0.9 0.8
47	9.70 909	22	9.77 505	28	0.22 495	9.93 405	7	13	8 1.1 0.9
48	9.70 931	21	9.77 533	29	0.22 467	9.93 397	8	12	9 1.2 1.0
49	9.70 952	22	9.77 562	29	0.22 438	9.93 390	10	11	10 1.3 1.2
50	9.70 973	21	9.77 591	28	0.22 409	9.93 382	20	10	20 2.7 2.3
51	9.70 994	22	9.77 619	29	0.22 381	9.93 375	30	9	30 4.0 3.5
52	9.71 015	21	9.77 648	29	0.22 352	9.93 367	40	8	40 5.3 4.7
53	9.71 036	22	9.77 677	29	0.22 323	9.93 360	50	7	50 6.7 5.8
54	9.71 058	21	9.77 706	28	0.22 294	9.93 352		6	
55	9.71 079	22	9.77 734	29	0.22 266	9.93 344		5	
56	9.71 100	21	9.77 763	28	0.22 237	9.93 337	7	4	
57	9.71 121	22	9.77 791	29	0.22 209	9.93 329	8	3	
58	9.71 142	21	9.77 820	29	0.22 180	9.93 322	7	2	
59	9.71 163	22	9.77 849	28	0.22 151	9.93 314	8	1	
60	9.71 184		9.77 877		0.22 123	9.93 307	7	0	
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.

\*149°

239°

\*329°

59°

31°

\*121°

211°

\*301°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.71 184		9.77 877		0.22 123	9.93 307		60	
1	9.71 205	21	9.77 906	29	0.22 094	9.93 299	8	59	
2	9.71 226	21	9.77 935	29	0.22 065	9.93 291	8	58	
3	9.71 247	21	9.77 963	28	0.22 037	9.93 284	7	57	
4	9.71 268	21	9.77 992	29	0.22 008	9.93 276	8	56	
5	9.71 289		9.78 020		0.21 980	9.93 269		55	
6	9.71 310	21	9.78 049	29	0.21 951	9.93 261	8	54	
7	9.71 331	21	9.78 077	28	0.21 923	9.93 253	8	53	
8	9.71 352	21	9.78 106	29	0.21 894	9.93 246	7	52	
9	9.71 373	20	9.78 135	29	0.21 865	9.93 238	8	51	
10	9.71 393		9.78 163		0.21 837	9.93 230		50	" 29 28
11	9.71 414	21	9.78 192	29	0.21 808	9.93 223	7	49	6 2.9 2.8
12	9.71 435	21	9.78 220	28	0.21 780	9.93 215	8	48	7 3.5 3.3
13	9.71 456	21	9.78 249	29	0.21 751	9.93 207	8	47	8 3.9 3.7
14	9.71 477	21	9.78 277	28	0.21 723	9.93 200	7	46	9 4.4 4.2
15	9.71 498		9.78 306		0.21 694	9.93 192		45	10 4.8 4.7
16	9.71 519	21	9.78 334	28	0.21 666	9.93 184	8	44	20 9.7 9.3
17	9.71 539	20	9.78 363	29	0.21 637	9.93 177	7	43	30 14.5 14.0
18	9.71 560	21	9.78 391	28	0.21 609	9.93 169	8	42	40 19.3 18.7
19	9.71 581	21	9.78 419	28	0.21 581	9.93 161	8	41	50 24.2 23.3
20	9.71 602		9.78 448		0.21 552	9.93 154		40	
21	9.71 622	20	9.78 476	28	0.21 524	9.93 146	8	39	
22	9.71 643	21	9.78 505	29	0.21 495	9.93 138	8	38	
23	9.71 664	21	9.78 533	28	0.21 467	9.93 131	7	37	
24	9.71 685	20	9.78 562	29	0.21 438	9.93 123	8	36	
25	9.71 705		9.78 590		0.21 410	9.93 115		35	
26	9.71 726	21	9.78 618	28	0.21 382	9.93 108	7	34	
27	9.71 747	21	9.78 647	29	0.21 353	9.93 100	8	33	" 21 20
28	9.71 767	20	9.78 675	28	0.21 325	9.93 092	8	32	6 2.1 2.0
29	9.71 788	21	9.78 704	29	0.21 296	9.93 084	8	31	7 2.4 2.3
30	9.71 809		9.78 732		0.21 268	9.93 077		30	8 2.8 2.7
31	9.71 829	20	9.78 760	28	0.21 240	9.93 069	8	29	9 3.2 3.0
32	9.71 850	21	9.78 789	29	0.21 211	9.93 061	8	28	10 3.5 3.3
33	9.71 870	20	9.78 817	28	0.21 183	9.93 053	8	27	20 7.0 6.7
34	9.71 891	21	9.78 845	28	0.21 155	9.93 046	7	26	30 10.5 10.0
35	9.71 911		9.78 874		0.21 126	9.93 038		25	40 14.0 13.3
36	9.71 932	21	9.78 902	28	0.21 098	9.93 030	8	24	50 17.5 16.7
37	9.71 952	20	9.78 930	28	0.21 070	9.93 022	8	23	
38	9.71 973	21	9.78 959	29	0.21 041	9.93 014	8	22	
39	9.71 994	20	9.78 987	28	0.21 013	9.93 007	8	21	
40	9.72 014		9.79 015		0.20 985	9.92 999		20	
41	9.72 034	20	9.79 043	28	0.20 957	9.92 991	8	19	
42	9.72 055	21	9.79 072	29	0.20 928	9.92 983	8	18	
43	9.72 075	20	9.79 100	28	0.20 900	9.92 976	7	17	
44	9.72 096	21	9.79 128	28	0.20 872	9.92 968	8	16	" 8 7
45	9.72 116		9.79 156		0.20 844	9.92 960		15	6 0.8 0.7
46	9.72 137	21	9.79 185	29	0.20 815	9.92 952	8	14	7 0.9 0.8
47	9.72 157	20	9.79 213	28	0.20 787	9.92 944	8	13	8 1.1 0.9
48	9.72 177	20	9.79 241	28	0.20 759	9.92 936	8	12	9 1.2 1.0
49	9.72 198	21	9.79 269	28	0.20 731	9.92 929	7	11	10 1.3 1.2
50	9.72 218	20	9.79 297	28	0.20 703	9.92 921	8	10	20 2.7 2.3
51	9.72 238		9.79 326		0.20 674	9.92 913		9	30 4.0 3.5
52	9.72 259	21	9.79 354	29	0.20 646	9.92 905	8	8	40 5.3 4.7
53	9.72 279	20	9.79 382	28	0.20 618	9.92 897	8	7	50 6.7 5.8
54	9.72 299	20	9.79 410	28	0.20 590	9.92 889	8	6	
55	9.72 320		9.79 438		0.20 562	9.92 881		5	
56	9.72 340	20	9.79 466	28	0.20 534	9.92 874	7	4	
57	9.72 360	20	9.79 495	29	0.20 505	9.92 866	8	3	
58	9.72 381	21	9.79 523	28	0.20 477	9.92 858	8	2	
59	9.72 401	20	9.79 551	28	0.20 449	9.92 850	8	1	
60	9.72 421		9.79 579		0.20 421	9.92 842		0	
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.

\*148°

238°

\*328°

58°

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

32°

\*122°

212°

\*302°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.72 421		9.79 579	28	0.20 421	9.92 842	8	60	
1	9.72 441	20	9.79 607	28	0.20 393	9.92 834	8	59	
2	9.72 461	20	9.79 635	28	0.20 365	9.92 826	8	58	
3	9.72 482	20	9.79 663	28	0.20 337	9.92 818	8	57	
4	9.72 502	20	9.79 691	28	0.20 309	9.92 810	7	56	
5	9.72 522		9.79 719		0.20 281	9.92 803		55	
6	9.72 542	20	9.79 747	28	0.20 253	9.92 795	8	54	
7	9.72 562	20	9.79 776	28	0.20 224	9.92 787	8	53	
8	9.72 582	20	9.79 804	28	0.20 196	9.92 779	8	52	
9	9.72 602	20	9.79 832	28	0.20 168	9.92 771	8	51	
10	9.72 622		9.79 860		0.20 140	9.92 763		50	" 29 28 27
11	9.72 643	21	9.79 888	28	0.20 112	9.92 755	8	49	6 2.0 2.8 2.7
12	9.72 663	20	9.79 916	28	0.20 084	9.92 747	8	48	7 3.5 3.3 3.2
13	9.72 683	20	9.79 944	28	0.20 056	9.92 739	8	47	8 3.9 3.7 3.6
14	9.72 703	20	9.79 972	28	0.20 028	9.92 731	8	46	9 4.4 4.2 4.1
15	9.72 723		9.80 000		0.20 000	9.92 723		45	10 4.8 4.7 4.5
16	9.72 743	20	9.80 028	28	0.19 972	9.92 715	8	44	20 9.7 9.3 9.0
17	9.72 763	20	9.80 056	28	0.19 944	9.92 707	8	43	30 14.5 14.0 13.5
18	9.72 783	20	9.80 084	28	0.19 916	9.92 699	8	42	40 19.3 18.7 18.0
19	9.72 803	20	9.80 112	28	0.19 888	9.92 691	8	41	50 24.2 23.3 22.5
20	9.72 823		9.80 140		0.19 860	9.92 683		40	
21	9.72 843	20	9.80 168	28	0.19 832	9.92 675	8	39	
22	9.72 863	20	9.80 195	27	0.19 805	9.92 667	8	38	
23	9.72 883	19	9.80 223	28	0.19 777	9.92 659	8	37	
24	9.72 902	20	9.80 251	28	0.19 749	9.92 651	8	36	
25	9.72 922		9.80 279		0.19 721	9.92 643		35	
26	9.72 942	20	9.80 307	28	0.19 693	9.92 635	8	34	
27	9.72 962	20	9.80 335	28	0.19 665	9.92 627	8	33	" 21 20 19
28	9.72 982	20	9.80 363	28	0.19 637	9.92 619	8	32	6 2.1 2.0 1.9
29	9.73 002	20	9.80 391	28	0.19 609	9.92 611	8	31	7 2.4 2.3 2.2
30	9.73 022		9.80 419		0.19 581	9.92 603		30	8 2.8 2.7 2.5
31	9.73 041	19	9.80 447	28	0.19 553	9.92 595	8	29	9 3.2 3.0 2.9
32	9.73 061	20	9.80 474	27	0.19 526	9.92 587	8	28	10 3.5 3.3 3.2
33	9.73 081	20	9.80 502	28	0.19 498	9.92 579	8	27	20 7.0 6.7 6.3
34	9.73 101	20	9.80 530	28	0.19 470	9.92 571	8	26	30 10.5 10.0 9.5
35	9.73 121		9.80 558		0.19 442	9.92 563		25	40 14.0 13.3 12.7
36	9.73 140	19	9.80 586	28	0.19 414	9.92 555	8	24	50 17.5 16.7 15.8
37	9.73 160	20	9.80 614	28	0.19 386	9.92 546	8	23	
38	9.73 180	20	9.80 642	28	0.19 358	9.92 538	8	22	
39	9.73 200	19	9.80 669	27	0.19 331	9.92 530	8	21	
40	9.73 219		9.80 697		0.19 303	9.92 522		20	
41	9.73 239	20	9.80 725	28	0.19 275	9.92 514	8	19	
42	9.73 259	20	9.80 753	28	0.19 247	9.92 506	8	18	
43	9.73 278	19	9.80 781	28	0.19 219	9.92 498	8	17	
44	9.73 298	20	9.80 808	27	0.19 192	9.92 490	8	16	" 9 8 7
45	9.73 318		9.80 836		0.19 164	9.92 482		15	6 0.9 0.8 0.7
46	9.73 337	19	9.80 864	28	0.19 136	9.92 473	9	14	7 1.1 0.9 0.8
47	9.73 357	20	9.80 892	28	0.19 108	9.92 465	8	13	8 1.2 1.1 0.9
48	9.73 377	20	9.80 919	27	0.19 081	9.92 457	8	12	9 1.4 1.2 1.1
49	9.73 396	19	9.80 947	28	0.19 053	9.92 449	8	11	10 1.5 1.3 1.2
50	9.73 416		9.80 975		0.19 025	9.92 441		10	20 3.0 2.7 2.3
51	9.73 435	19	9.81 003	28	0.18 997	9.92 433	8	9	30 4.5 4.0 3.5
52	9.73 455	20	9.81 030	27	0.18 970	9.92 425	8	8	40 6.0 5.3 4.7
53	9.73 474	19	9.81 058	28	0.18 942	9.92 416	9	7	50 7.5 6.7 5.8
54	9.73 494	20	9.81 086	28	0.18 914	9.92 408	8	6	
55	9.73 513		9.81 113		0.18 887	9.92 400		5	
56	9.73 533	20	9.81 141	28	0.18 859	9.92 392	8	4	
57	9.73 552	19	9.81 169	28	0.18 831	9.92 384	8	3	
58	9.73 572	20	9.81 196	27	0.18 804	9.92 376	8	2	
59	9.73 591	19	9.81 224	28	0.18 776	9.92 367	9	1	
60	9.73 611	20	9.81 252	28	0.18 748	9.92 359	8	0	
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.

\*147°

237°

\*327°

57°

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

33°

\*123°

213°

\*303°

'	log sin	d.	log tan	e. d.	log cot	log cos	d.		Prop. Pts.
0	9.73 611		9.81 252		0.18 748	9.92 359	8	60	
1	9.73 630	19	9.81 279	27	0.18 721	9.92 351	8	59	
2	9.73 650	20	9.81 307	28	0.18 693	9.92 343	8	58	
3	9.73 669	20	9.81 335	27	0.18 665	9.92 335	9	57	
4	9.73 689	19	9.81 362	28	0.18 638	9.92 326	8	56	
5	9.73 708		9.81 390		0.18 610	9.92 318	8	55	
6	9.73 727	19	9.81 418	28	0.18 582	9.92 310	8	54	
7	9.73 747	20	9.81 445	27	0.18 555	9.92 302	9	53	
8	9.73 766	19	9.81 473	28	0.18 527	9.92 293	8	52	
9	9.73 785	20	9.81 500	27	0.18 500	9.92 285	8	51	
10	9.73 805		9.81 528		0.18 472	9.92 277	8	50	" 28 27 20
11	9.73 824	19	9.81 556	28	0.18 444	9.92 269	8	49	6 2.8 2.7 2.0
12	9.73 843	19	9.81 583	27	0.18 417	9.92 260	9	48	7 3.3 3.2 2.3
13	9.73 863	20	9.81 611	28	0.18 389	9.92 252	8	47	8 3.7 3.6 2.7
14	9.73 882	19	9.81 638	27	0.18 362	9.92 244	8	46	9 4.2 4.1 3.0
15	9.73 901	19	9.81 666	28	0.18 334	9.92 235	9	45	10 4.7 4.5 3.3
16	9.73 921	20	9.81 693	27	0.18 307	9.92 227	8	44	20 9.3 9.0 6.7
17	9.73 940	19	9.81 721	28	0.18 279	9.92 219	8	43	30 14.0 13.5 10.0
18	9.73 959	19	9.81 748	27	0.18 252	9.92 211	8	42	40 18.7 18.0 13.3
19	9.73 978	19	9.81 776	28	0.18 224	9.92 202	8	41	50 23.3 22.5 16.7
20	9.73 997		9.81 803		0.18 197	9.92 194	8	40	
21	9.74 017	20	9.81 831	28	0.18 169	9.92 186	8	39	
22	9.74 036	19	9.81 858	27	0.18 142	9.92 177	9	38	
23	9.74 055	19	9.81 886	28	0.18 114	9.92 169	8	37	
24	9.74 074	19	9.81 913	27	0.18 087	9.92 161	8	36	
25	9.74 093	20	9.81 941	28	0.18 059	9.92 152	9	35	
26	9.74 113	19	9.81 968	27	0.18 032	9.92 144	8	34	
27	9.74 132	19	9.81 996	28	0.18 004	9.92 136	8	33	" 19 18
28	9.74 151	19	9.82 023	27	0.17 977	9.92 127	9	32	6 1.9 1.8
29	9.74 170	19	9.82 051	28	0.17 949	9.92 119	8	31	7 2.2 2.1
30	9.74 189		9.82 078		0.17 922	9.92 111	8	30	8 2.5 2.4
31	9.74 208	19	9.82 106	27	0.17 894	9.92 102	9	29	9 2.9 2.7
32	9.74 227	19	9.82 133	28	0.17 867	9.92 094	8	28	10 3.2 3.0
33	9.74 246	19	9.82 161	27	0.17 839	9.92 086	8	27	20 6.3 6.0
34	9.74 265	19	9.82 188	28	0.17 812	9.92 077	8	26	30 9.5 9.0
35	9.74 284		9.82 215		0.17 785	9.92 069	8	25	40 12.7 12.0
36	9.74 303	19	9.82 243	27	0.17 757	9.92 060	9	24	50 15.8 15.0
37	9.74 322	19	9.82 270	28	0.17 730	9.92 052	8	23	
38	9.74 341	19	9.82 298	27	0.17 702	9.92 044	8	22	
39	9.74 360	19	9.82 325	28	0.17 675	9.92 035	9	21	
40	9.74 379		9.82 352		0.17 648	9.92 027	8	20	
41	9.74 398	19	9.82 380	27	0.17 620	9.92 018	9	19	
42	9.74 417	19	9.82 407	28	0.17 593	9.92 010	8	18	
43	9.74 436	19	9.82 435	27	0.17 565	9.92 002	8	17	
44	9.74 455	19	9.82 462	28	0.17 538	9.91 993	9	16	" 9 8
45	9.74 474		9.82 489		0.17 511	9.91 985	8	15	6 0.9 0.8
46	9.74 493	19	9.82 517	27	0.17 483	9.91 976	9	14	7 1.1 0.9
47	9.74 512	19	9.82 544	28	0.17 456	9.91 968	8	13	8 1.2 1.1
48	9.74 531	19	9.82 571	27	0.17 429	9.91 959	9	12	9 1.4 1.2
49	9.74 549	18	9.82 599	28	0.17 401	9.91 951	8	11	10 1.5 1.3
50	9.74 568		9.82 626		0.17 374	9.91 942	9	10	20 3.0 2.7
51	9.74 587	19	9.82 653	27	0.17 347	9.91 934	8	9	30 4.5 4.0
52	9.74 606	19	9.82 681	28	0.17 319	9.91 925	9	8	40 6.0 5.3
53	9.74 625	19	9.82 708	27	0.17 292	9.91 917	8	7	50 7.5 6.7
54	9.74 644	19	9.82 735	28	0.17 265	9.91 908	8	6	
55	9.74 662		9.82 762		0.17 238	9.91 900	8	5	
56	9.74 681	19	9.82 790	27	0.17 210	9.91 891	9	4	
57	9.74 700	19	9.82 817	28	0.17 183	9.91 883	8	3	
58	9.74 719	19	9.82 844	27	0.17 156	9.91 874	9	2	
59	9.74 737	18	9.82 871	28	0.17 129	9.91 866	8	1	
60	9.74 756	19	9.82 899	27	0.17 101	9.91 857	9	0	
	log cos	d.	log cot	e. d.	log tan	log sin	d.	'	Prop. Pts.

\*146°

236°

\*326°

56°

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

34°

\*124°

214°

\*304°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.74 756		9.82 899		0.17 101	9.91 857	8	60	
1	9.74 775	19	9.82 926	27	0.17 074	9.91 849	8	59	
2	9.74 794	18	9.82 953	27	0.17 047	9.91 840	8	58	
3	9.74 812	19	9.82 980	27	0.17 020	9.91 832	8	57	
4	9.74 831	19	9.83 008	27	0.16 992	9.91 823	8	56	
5	9.74 850	18	9.83 035	27	0.16 965	9.91 815	9	55	
6	9.74 868	19	9.83 062	27	0.16 938	9.91 806	8	54	
7	9.74 887	19	9.83 089	28	0.16 911	9.91 798	8	53	
8	9.74 906	18	9.83 117	27	0.16 883	9.91 789	8	52	
9	9.74 924	19	9.83 144	27	0.16 856	9.91 781	9	51	
10	9.74 943	18	9.83 171	27	0.16 829	9.91 772	9	50	" 28 27 26
11	9.74 961	19	9.83 198	27	0.16 802	9.91 763	8	49	6 2.8 2.7 2.6
12	9.74 980	19	9.83 225	27	0.16 775	9.91 755	8	48	7 3.3 3.2 3.0
13	9.74 999	18	9.83 252	27	0.16 748	9.91 746	8	47	8 3.7 3.6 3.5
14	9.75 017	19	9.83 280	27	0.16 720	9.91 738	9	46	9 4.2 4.0 3.9
15	9.75 036	18	9.83 307	27	0.16 693	9.91 729	9	45	10 4.7 4.5 4.3
16	9.75 054	19	9.83 334	27	0.16 666	9.91 720	8	44	20 9.3 9.0 8.7
17	9.75 073	18	9.83 361	27	0.16 639	9.91 712	8	43	30 14.0 13.5 13.0
18	9.75 091	19	9.83 388	27	0.16 612	9.91 703	8	42	40 18.7 18.0 17.3
19	9.75 110	18	9.83 415	27	0.16 585	9.91 695	8	41	50 23.3 22.5 21.7
20	9.75 128	19	9.83 442	28	0.16 558	9.91 686	9	40	
21	9.75 147	18	9.83 470	27	0.16 530	9.91 677	8	39	
22	9.75 165	19	9.83 497	27	0.16 503	9.91 669	9	38	
23	9.75 184	18	9.83 524	27	0.16 476	9.91 660	9	37	
24	9.75 202	19	9.83 551	27	0.16 449	9.91 651	8	36	
25	9.75 221	18	9.83 578	27	0.16 422	9.91 643	9	35	
26	9.75 239	19	9.83 605	27	0.16 395	9.91 634	9	34	
27	9.75 258	18	9.83 632	27	0.16 368	9.91 625	8	33	" 19 18
28	9.75 276	19	9.83 659	27	0.16 341	9.91 617	8	32	6 1.9 1.8
29	9.75 294	18	9.83 686	27	0.16 314	9.91 608	9	31	7 2.2 2.1
30	9.75 313	19	9.83 713	27	0.16 287	9.91 599	9	30	8 2.5 2.4
31	9.75 331	18	9.83 740	27	0.16 260	9.91 591	9	29	9 2.8 2.7
32	9.75 350	19	9.83 768	28	0.16 232	9.91 582	9	28	10 3.2 3.0
33	9.75 368	18	9.83 795	27	0.16 205	9.91 573	9	27	20 6.3 6.0
34	9.75 386	19	9.83 822	27	0.16 178	9.91 565	8	26	30 9.5 9.0
35	9.75 405	18	9.83 849	27	0.16 151	9.91 556	9	25	40 12.7 12.0
36	9.75 423	19	9.83 876	27	0.16 124	9.91 547	9	24	50 15.8 15.0
37	9.75 441	18	9.83 903	27	0.16 097	9.91 538	8	23	
38	9.75 459	19	9.83 930	27	0.16 070	9.91 530	8	22	
39	9.75 478	18	9.83 957	27	0.16 043	9.91 521	9	21	
40	9.75 496	19	9.83 984	27	0.16 016	9.91 512	9	20	
41	9.75 514	18	9.84 011	27	0.15 989	9.91 504	8	19	
42	9.75 533	19	9.84 038	27	0.15 962	9.91 495	9	18	
43	9.75 551	18	9.84 065	27	0.15 935	9.91 486	9	17	
44	9.75 569	19	9.84 092	27	0.15 908	9.91 477	8	16	" 9 8
45	9.75 587	18	9.84 119	27	0.15 881	9.91 469	9	15	6 0.9 0.8
46	9.75 605	19	9.84 146	27	0.15 854	9.91 460	9	14	7 1.0 0.9
47	9.75 624	18	9.84 173	27	0.15 827	9.91 451	9	13	8 1.2 1.1
48	9.75 642	19	9.84 200	27	0.15 800	9.91 442	9	12	9 1.4 1.2
49	9.75 660	18	9.84 227	27	0.15 773	9.91 433	9	11	10 1.5 1.3
50	9.75 678	19	9.84 254	26	0.15 746	9.91 425	8	10	20 3.0 2.7
51	9.75 696	18	9.84 280	27	0.15 720	9.91 416	9	9	30 4.5 4.0
52	9.75 714	19	9.84 307	27	0.15 693	9.91 407	9	8	40 6.0 5.3
53	9.75 733	18	9.84 334	27	0.15 666	9.91 398	9	7	50 7.5 6.7
54	9.75 751	19	9.84 361	27	0.15 639	9.91 389	8	6	
55	9.75 769	18	9.84 388	27	0.15 612	9.91 381	9	5	
56	9.75 787	19	9.84 415	27	0.15 585	9.91 372	9	4	
57	9.75 805	18	9.84 442	27	0.15 558	9.91 363	9	3	
58	9.75 823	19	9.84 469	27	0.15 531	9.91 354	9	2	
59	9.75 841	18	9.84 496	27	0.15 504	9.91 345	9	1	
60	9.75 859		9.84 523		0.15 477	9.91 336	9	0	

	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.
--	---------	----	---------	-------	---------	---------	----	---	------------

\*145°

235°

\*325°

55°

35°

\*125°

215°

\*305°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.75 859		9.84 523		0.15 477	9.91 336	8	60	
1	9.75 877	18	9.84 550	27	0.15 450	9.91 328	9	59	
2	9.75 895	18	9.84 576	27	0.15 424	9.91 319	9	58	
3	9.75 913	18	9.84 603	27	0.15 397	9.91 310	9	57	
4	9.75 931	18	9.84 630	27	0.15 370	9.91 301	9	56	
5	9.75 949	18	9.84 657	27	0.15 343	9.91 292	9	55	
6	9.75 967	18	9.84 684	27	0.15 316	9.91 283	9	54	
7	9.75 985	18	9.84 711	27	0.15 289	9.91 274	9	53	
8	9.76 003	18	9.84 738	27	0.15 262	9.91 266	8	52	
9	9.76 021	18	9.84 764	27	0.15 236	9.91 257	9	51	
10	9.76 039	18	9.84 791	27	0.15 209	9.91 248	9	50	
11	9.76 057	18	9.84 818	27	0.15 182	9.91 239	9	49	
12	9.76 075	18	9.84 845	27	0.15 155	9.91 230	9	48	
13	9.76 093	18	9.84 872	27	0.15 128	9.91 221	9	47	
14	9.76 111	18	9.84 899	26	0.15 101	9.91 212	9	46	
15	9.76 129	17	9.84 925	27	0.15 075	9.91 203	9	45	
16	9.76 146	17	9.84 952	27	0.15 048	9.91 194	9	44	
17	9.76 164	18	9.84 979	27	0.15 021	9.91 185	9	43	
18	9.76 182	18	9.85 006	27	0.14 994	9.91 176	9	42	
19	9.76 200	18	9.85 033	26	0.14 967	9.91 167	9	41	
20	9.76 218	18	9.85 059	27	0.14 941	9.91 158	9	40	
21	9.76 236	17	9.85 086	27	0.14 914	9.91 149	8	39	
22	9.76 253	18	9.85 113	27	0.14 887	9.91 141	9	38	
23	9.76 271	18	9.85 140	26	0.14 860	9.91 132	9	37	
24	9.76 289	18	9.85 166	27	0.14 834	9.91 123	9	36	
25	9.76 307	17	9.85 193	27	0.14 807	9.91 114	9	35	
26	9.76 324	18	9.85 220	27	0.14 780	9.91 105	9	34	
27	9.76 342	18	9.85 247	26	0.14 753	9.91 096	9	33	
28	9.76 360	18	9.85 273	27	0.14 727	9.91 087	9	32	
29	9.76 378	17	9.85 300	27	0.14 700	9.91 078	9	31	
30	9.76 395	18	9.85 327	27	0.14 673	9.91 069	9	30	
31	9.76 413	18	9.85 354	26	0.14 646	9.91 060	9	29	
32	9.76 431	17	9.85 380	27	0.14 620	9.91 051	9	28	
33	9.76 448	18	9.85 407	27	0.14 593	9.91 042	9	27	
34	9.76 466	18	9.85 434	26	0.14 566	9.91 033	10	26	
35	9.76 484	17	9.85 460	27	0.14 540	9.91 023	9	25	
36	9.76 501	18	9.85 487	27	0.14 513	9.91 014	9	24	
37	9.76 519	18	9.85 514	26	0.14 486	9.91 005	9	23	
38	9.76 537	17	9.85 540	27	0.14 460	9.90 996	9	22	
39	9.76 554	18	9.85 567	27	0.14 433	9.90 987	9	21	
40	9.76 572	18	9.85 594	26	0.14 406	9.90 978	9	20	
41	9.76 590	17	9.85 620	27	0.14 380	9.90 969	9	19	
42	9.76 607	18	9.85 647	27	0.14 353	9.90 960	9	18	
43	9.76 625	17	9.85 674	26	0.14 326	9.90 951	9	17	
44	9.76 642	18	9.85 700	27	0.14 300	9.90 942	9	16	
45	9.76 660	17	9.85 727	27	0.14 273	9.90 933	9	15	
46	9.76 677	18	9.85 754	26	0.14 246	9.90 924	9	14	
47	9.76 695	17	9.85 780	27	0.14 220	9.90 915	9	13	
48	9.76 712	18	9.85 807	27	0.14 193	9.90 906	9	12	
49	9.76 730	17	9.85 834	26	0.14 166	9.90 896	10	11	
50	9.76 747	18	9.85 860	27	0.14 140	9.90 887	9	10	
51	9.76 765	17	9.85 887	26	0.14 113	9.90 878	9	9	
52	9.76 782	18	9.85 913	27	0.14 087	9.90 869	9	8	
53	9.76 800	17	9.85 940	27	0.14 060	9.90 860	9	7	
54	9.76 817	18	9.85 967	26	0.14 033	9.90 851	9	6	
55	9.76 835	17	9.85 993	27	0.14 007	9.90 842	10	5	
56	9.76 852	18	9.86 020	26	0.13 980	9.90 832	9	4	
57	9.76 870	17	9.86 046	27	0.13 954	9.90 823	9	3	
58	9.76 887	17	9.86 073	27	0.13 927	9.90 814	9	2	
59	9.76 904	18	9.86 100	27	0.13 900	9.90 805	9	1	
60	9.76 922		9.86 126		0.13 874	9.90 796		0	
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.

"	27	26	18
6	2.7	2.6	1.8
7	3.2	3.0	2.1
8	3.6	3.5	2.4
9	4.1	3.9	2.7
10	4.5	4.3	3.0
20	9.0	8.7	6.0
30	13.5	13.0	9.0
40	18.0	17.3	12.0
50	22.5	21.7	15.0

"	17	10
6	1.7	1.0
7	2.0	1.2
8	2.3	1.3
9	2.6	1.5
10	2.8	1.7
20	5.7	3.3
30	8.5	5.0
40	11.3	6.7
50	14.2	8.3

"	9	8
6	0.9	0.8
7	1.1	0.9
8	1.2	1.1
9	1.4	1.2
10	1.5	1.3
20	3.0	2.7
30	4.5	4.0
40	6.0	5.3
50	7.5	6.7

\*144°

234°

\*324°

54°



<b>36°</b>										*126°	216°	*306°	
'	log sin	d.	log tan	c. d.	log cot	log cos	d.			Prop. Pts.			
0	9.76 922		9.86 126		0.13 874	9.90 796			<b>60</b>				
1	9.76 939	17	9.86 153	27	0.13 847	9.90 787	9	10	59				
2	9.76 957	18	9.86 179	26	0.13 821	9.90 777	10	9	58				
3	9.76 974	17	9.86 206	27	0.13 794	9.90 768	9	9	57				
4	9.76 991	18	9.86 232	26	0.13 768	9.90 759	9	10	56				
5	9.77 009		9.86 259		0.13 741	9.90 750			55				
6	9.77 026	17	9.86 285	26	0.13 715	9.90 741	9	10	54				
7	9.77 043	17	9.86 312	27	0.13 688	9.90 731	10	9	53				
8	9.77 061	18	9.86 338	26	0.13 662	9.90 722	9	9	52				
9	9.77 078	17	9.86 365	27	0.13 635	9.90 713	9	9	51				
10	9.77 095	17	9.86 392	27	0.13 608	9.90 704	9	10	50	" 27	26	18	
11	9.77 112	18	9.86 418	26	0.13 582	9.90 694	10	9	49	6	2.7	2.6	1.8
12	9.77 130	17	9.86 445	27	0.13 555	9.90 685	9	9	48	7	3.2	3.0	2.1
13	9.77 147	17	9.86 471	26	0.13 529	9.90 676	9	9	47	8	3.6	3.5	2.4
14	9.77 164	17	9.86 498	27	0.13 502	9.90 667	9	10	46	9	4.0	3.9	2.7
15	9.77 181	18	9.86 524	26	0.13 476	9.90 657	10	9	45	10	4.5	4.3	3.0
16	9.77 199	17	9.86 551	27	0.13 449	9.90 648	9	9	44	20	9.0	8.7	6.0
17	9.77 216	17	9.86 577	26	0.13 423	9.90 639	9	9	43	30	13.5	13.0	9.0
18	9.77 233	17	9.86 603	27	0.13 397	9.90 630	9	10	42	40	18.0	17.3	12.0
19	9.77 250	18	9.86 630	26	0.13 370	9.90 620	10	9	41	50	22.5	21.7	15.0
20	9.77 268	17	9.86 656	27	0.13 344	9.90 611	9	9	40				
21	9.77 285	17	9.86 683	26	0.13 317	9.90 602	10	9	39				
22	9.77 302	17	9.86 709	27	0.13 291	9.90 592	9	9	38				
23	9.77 319	17	9.86 736	26	0.13 264	9.90 583	9	9	37				
24	9.77 336	17	9.86 762	27	0.13 238	9.90 574	9	9	36				
25	9.77 353	17	9.86 789	26	0.13 211	9.90 565	10	9	35				
26	9.77 370	17	9.86 815	27	0.13 185	9.90 555	9	9	34				
27	9.77 387	18	9.86 842	26	0.13 158	9.90 546	9	10	33	" 17	16		
28	9.77 405	17	9.86 868	26	0.13 132	9.90 537	9	9	32	6	1.7	1.6	
29	9.77 422	17	9.86 894	27	0.13 106	9.90 527	10	9	31	7	2.0	1.9	
30	9.77 439	17	9.86 921	26	0.13 079	9.90 518	9	9	30	8	2.3	2.1	
31	9.77 456	17	9.86 947	26	0.13 053	9.90 509	9	10	29	9	2.6	2.4	
32	9.77 473	17	9.86 974	27	0.13 026	9.90 499	10	9	28	10	2.8	2.7	
33	9.77 490	17	9.87 000	26	0.13 000	9.90 490	9	9	27	20	5.7	5.3	
34	9.77 507	17	9.87 027	27	0.12 973	9.90 480	10	9	26	30	8.5	8.0	
35	9.77 524	17	9.87 053	26	0.12 947	9.90 471	9	9	25	40	11.3	10.7	
36	9.77 541	17	9.87 079	26	0.12 921	9.90 462	9	10	24	50	14.2	13.3	
37	9.77 558	17	9.87 106	27	0.12 894	9.90 452	10	9	23				
38	9.77 575	17	9.87 132	26	0.12 868	9.90 443	9	9	22				
39	9.77 592	17	9.87 158	26	0.12 842	9.90 434	9	10	21				
40	9.77 609	17	9.87 185	27	0.12 815	9.90 424	10	9	20				
41	9.77 626	17	9.87 211	26	0.12 789	9.90 415	9	9	19				
42	9.77 643	17	9.87 238	26	0.12 762	9.90 405	10	9	18				
43	9.77 660	17	9.87 264	26	0.12 736	9.90 396	9	9	17				
44	9.77 677	17	9.87 290	26	0.12 710	9.90 386	10	9	16	" 10	9		
45	9.77 694	17	9.87 317	27	0.12 683	9.90 377	9	9	15	6	1.0	0.9	
46	9.77 711	17	9.87 343	26	0.12 657	9.90 368	9	10	14	7	1.2	1.0	
47	9.77 728	17	9.87 369	26	0.12 631	9.90 358	10	9	13	8	1.3	1.2	
48	9.77 744	16	9.87 396	27	0.12 604	9.90 349	9	9	12	9	1.5	1.4	
49	9.77 761	17	9.87 422	26	0.12 578	9.90 339	10	9	11	10	1.7	1.5	
50	9.77 778	17	9.87 448	26	0.12 552	9.90 330	9	9	10	20	3.3	3.0	
51	9.77 795	17	9.87 475	27	0.12 525	9.90 320	10	9	9	30	5.0	4.5	
52	9.77 812	17	9.87 501	26	0.12 499	9.90 311	9	9	8	40	6.7	6.0	
53	9.77 829	17	9.87 527	26	0.12 473	9.90 301	10	9	7	50	8.3	7.5	
54	9.77 846	16	9.87 554	26	0.12 446	9.90 292	9	9	6				
55	9.77 862	17	9.87 580	26	0.12 420	9.90 282	10	9	5				
56	9.77 879	17	9.87 606	26	0.12 394	9.90 273	9	9	4				
57	9.77 896	17	9.87 633	27	0.12 367	9.90 263	10	9	3				
58	9.77 913	17	9.87 659	26	0.12 341	9.90 254	9	9	2				
59	9.77 930	17	9.87 685	26	0.12 315	9.90 244	10	9	1				
60	9.77 946	16	9.87 711	26	0.12 289	9.90 235	9	9	0				
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'		Prop. Pts.			

37°

\*127°

217°

\*307°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.	Prop. Pts.
0	9.77 946		9.87 711		0.12 289	9.90 235	10	60
1	9.77 963	17	9.87 738	27	0.12 262	9.90 225	10	59
2	9.77 980	17	9.87 764	26	0.12 236	9.90 216	9	58
3	9.77 997	17	9.87 790	26	0.12 210	9.90 206	10	57
4	9.78 013	16	9.87 817	27	0.12 183	9.90 197	9	56
5	9.78 030	17	9.87 843	26	0.12 157	9.90 187	10	55
6	9.78 047	16	9.87 869	26	0.12 131	9.90 178	9	54
7	9.78 063	17	9.87 895	27	0.12 105	9.90 168	10	53
8	9.78 080	17	9.87 922	26	0.12 078	9.90 159	9	52
9	9.78 097	16	9.87 948	26	0.12 052	9.90 149	10	51
10	9.78 113		9.87 974		0.12 026	9.90 139		50
11	9.78 130	17	9.88 000	26	0.12 000	9.90 130	9	49
12	9.78 147	17	9.88 027	27	0.11 973	9.90 120	10	48
13	9.78 163	16	9.88 053	26	0.11 947	9.90 111	9	47
14	9.78 180	17	9.88 079	26	0.11 921	9.90 101	10	46
15	9.78 197		9.88 105		0.11 895	9.90 091		45
16	9.78 213	16	9.88 131	26	0.11 869	9.90 082	9	44
17	9.78 230	17	9.88 158	27	0.11 842	9.90 072	10	43
18	9.78 246	16	9.88 184	26	0.11 816	9.90 063	9	42
19	9.78 263	17	9.88 210	26	0.11 790	9.90 053	10	41
20	9.78 280		9.88 236		0.11 764	9.90 043		40
21	9.78 296	16	9.88 262	26	0.11 738	9.90 034	9	39
22	9.78 313	17	9.88 289	27	0.11 711	9.90 024	10	38
23	9.78 329	16	9.88 315	26	0.11 685	9.90 014	9	37
24	9.78 346	17	9.88 341	26	0.11 659	9.90 005	10	36
25	9.78 362		9.88 367		0.11 633	9.89 995		35
26	9.78 379	16	9.88 393	26	0.11 607	9.89 985	9	34
27	9.78 395	17	9.88 420	27	0.11 580	9.89 976	10	33
28	9.78 412	16	9.88 446	26	0.11 554	9.89 966	9	32
29	9.78 428	17	9.88 472	26	0.11 528	9.89 956	10	31
30	9.78 445		9.88 498		0.11 502	9.89 947		30
31	9.78 461	16	9.88 524	26	0.11 476	9.89 937	9	29
32	9.78 478	17	9.88 550	26	0.11 450	9.89 927	10	28
33	9.78 494	16	9.88 577	27	0.11 423	9.89 918	9	27
34	9.78 510	17	9.88 603	26	0.11 397	9.89 908	10	26
35	9.78 527		9.88 629		0.11 371	9.89 898		25
36	9.78 543	16	9.88 655	26	0.11 345	9.89 888	9	24
37	9.78 560	17	9.88 681	26	0.11 319	9.89 879	10	23
38	9.78 576	16	9.88 707	26	0.11 293	9.89 869	9	22
39	9.78 592	17	9.88 733	26	0.11 267	9.89 859	10	21
40	9.78 609		9.88 759		0.11 241	9.89 849		20
41	9.78 625	16	9.88 786	26	0.11 214	9.89 840	9	19
42	9.78 642	17	9.88 812	27	0.11 188	9.89 830	10	18
43	9.78 658	16	9.88 838	26	0.11 162	9.89 820	9	17
44	9.78 674	17	9.88 864	26	0.11 136	9.89 810	10	16
45	9.78 691		9.88 890		0.11 110	9.89 801		15
46	9.78 707	16	9.88 916	26	0.11 084	9.89 791	9	14
47	9.78 723	17	9.88 942	26	0.11 058	9.89 781	10	13
48	9.78 739	16	9.88 968	26	0.11 032	9.89 771	9	12
49	9.78 756	17	9.88 994	26	0.11 006	9.89 761	10	11
50	9.78 772		9.89 020		0.10 980	9.89 752		10
51	9.78 788	16	9.89 046	26	0.10 954	9.89 742	9	9
52	9.78 805	17	9.89 073	27	0.10 927	9.89 732	10	8
53	9.78 821	16	9.89 099	26	0.10 901	9.89 722	9	7
54	9.78 837	17	9.89 125	26	0.10 875	9.89 712	10	6
55	9.78 853		9.89 151		0.10 849	9.89 702		5
56	9.78 869	16	9.89 177	26	0.10 823	9.89 693	9	4
57	9.78 886	17	9.89 203	26	0.10 797	9.89 683	10	3
58	9.78 902	16	9.89 229	26	0.10 771	9.89 673	9	2
59	9.78 918	17	9.89 255	26	0.10 745	9.89 663	10	1
60	9.78 934		9.89 281		0.10 719	9.89 653		0
	log cos	d.	log cot	c. d.	log tan	log sin	d.	Prop. Pts.

"	27	26	17
6	2.7	2.6	1.7
7	3.2	3.0	2.0
8	3.6	3.5	2.3
9	4.0	3.9	2.6
10	4.5	4.3	2.8
20	9.0	8.7	5.7
30	13.5	13.0	8.5
40	18.0	17.3	11.3
50	22.5	21.7	14.2

"	16	10	9
6	1.6	1.0	0.9
7	1.9	1.2	1.0
8	2.1	1.3	1.2
9	2.4	1.5	1.4
10	2.7	1.7	1.5
20	5.3	3.3	3.0
30	8.0	5.0	4.5
40	10.7	6.7	6.0
50	13.3	8.3	7.5

\*142°

232°

\*322°

52°

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

38°

\*128°

218°

\*308°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.78 934	16	9.89 281	26	0.10 719	9.89 653	10	60	
1	9.78 950	17	9.89 307	26	0.10 693	9.89 643	10	59	
2	9.78 967	16	9.89 333	26	0.10 667	9.89 633	9	58	
3	9.78 983	16	9.89 359	26	0.10 641	9.89 624	10	57	
4	9.78 999	16	9.89 385	26	0.10 615	9.89 614	10	56	
5	9.79 015	16	9.89 411	26	0.10 589	9.89 604	10	55	" 26 25
6	9.79 031	16	9.89 437	26	0.10 563	9.89 594	10	54	6 2.6 2.5
7	9.79 047	16	9.89 463	26	0.10 537	9.89 584	10	53	7 3.0 2.9
8	9.79 063	16	9.89 489	26	0.10 511	9.89 574	10	52	8 3.5 3.3
9	9.79 079	16	9.89 515	26	0.10 485	9.89 564	10	51	9 3.9 3.8
10	9.79 095	16	9.89 541	26	0.10 459	9.89 554	10	50	10 4.3 4.2
11	9.79 111	17	9.89 567	26	0.10 433	9.89 544	10	49	20 8.7 8.3
12	9.79 128	16	9.89 593	26	0.10 407	9.89 534	10	48	30 13.0 12.5
13	9.79 144	16	9.89 619	26	0.10 381	9.89 524	10	47	40 17.3 16.7
14	9.79 160	16	9.89 645	26	0.10 355	9.89 514	10	46	50 21.7 20.8
15	9.79 176	16	9.89 671	26	0.10 329	9.89 504	10	45	
16	9.79 192	16	9.89 697	26	0.10 303	9.89 495	9	44	
17	9.79 208	16	9.89 723	26	0.10 277	9.89 485	10	43	
18	9.79 224	16	9.89 749	26	0.10 251	9.89 475	10	42	
19	9.79 240	16	9.89 775	26	0.10 225	9.89 465	10	41	
20	9.79 256	16	9.89 801	26	0.10 199	9.89 455	10	40	" 17 16
21	9.79 272	16	9.89 827	26	0.10 173	9.89 445	10	39	6 1.7 1.6
22	9.79 288	16	9.89 853	26	0.10 147	9.89 435	10	38	7 2.0 1.9
23	9.79 304	16	9.89 879	26	0.10 121	9.89 425	10	37	8 2.3 2.1
24	9.79 319	15	9.89 905	26	0.10 095	9.89 415	10	36	9 2.6 2.4
25	9.79 335	16	9.89 931	26	0.10 069	9.89 405	10	35	10 2.8 2.7
26	9.79 351	16	9.89 957	26	0.10 043	9.89 395	10	34	20 5.7 5.3
27	9.79 367	16	9.89 983	26	0.10 017	9.89 385	10	33	30 8.5 8.0
28	9.79 383	16	9.90 009	26	0.09 991	9.89 375	10	32	40 11.3 10.7
29	9.79 399	16	9.90 035	26	0.09 965	9.89 364	10	31	50 14.2 13.3
30	9.79 415	16	9.90 061	25	0.09 939	9.89 354	10	30	
31	9.79 431	16	9.90 086	26	0.09 914	9.89 344	10	29	
32	9.79 447	16	9.90 112	26	0.09 888	9.89 334	10	28	
33	9.79 463	15	9.90 138	26	0.09 862	9.89 324	10	27	" 15 11
34	9.79 478	16	9.90 164	26	0.09 836	9.89 314	10	26	6 1.5 1.1
35	9.79 494	16	9.90 190	26	0.09 810	9.89 304	10	25	7 1.8 1.3
36	9.79 510	16	9.90 216	26	0.09 784	9.89 294	10	24	8 2.0 1.5
37	9.79 526	16	9.90 242	26	0.09 758	9.89 284	10	23	9 2.2 1.6
38	9.79 542	16	9.90 268	26	0.09 732	9.89 274	10	22	10 2.5 1.8
39	9.79 558	15	9.90 294	26	0.09 706	9.89 264	10	21	20 5.0 3.7
40	9.79 573	16	9.90 320	26	0.09 680	9.89 254	10	20	30 7.5 5.5
41	9.79 589	16	9.90 346	26	0.09 654	9.89 244	10	19	40 10.0 7.3
42	9.79 605	16	9.90 371	25	0.09 629	9.89 233	11	18	50 12.5 9.2
43	9.79 621	16	9.90 397	26	0.09 603	9.89 223	10	17	
44	9.79 636	15	9.90 423	26	0.09 577	9.89 213	10	16	
45	9.79 652	16	9.90 449	26	0.09 551	9.89 203	10	15	
46	9.79 668	16	9.90 475	26	0.09 525	9.89 193	10	14	
47	9.79 684	16	9.90 501	26	0.09 499	9.89 183	10	13	" 10 9
48	9.79 699	15	9.90 527	26	0.09 473	9.89 173	10	12	6 1.0 0.9
49	9.79 715	16	9.90 553	26	0.09 447	9.89 162	11	11	7 1.2 1.0
50	9.79 731	15	9.90 578	25	0.09 422	9.89 152	10	10	8 1.3 1.2
51	9.79 746	16	9.90 604	26	0.09 396	9.89 142	10	9	9 1.5 1.4
52	9.79 762	15	9.90 630	26	0.09 370	9.89 132	10	8	10 1.7 1.5
53	9.79 778	16	9.90 656	26	0.09 344	9.89 122	10	7	20 3.3 3.0
54	9.79 793	15	9.90 682	26	0.09 318	9.89 112	10	6	30 5.0 4.5
55	9.79 809	16	9.90 708	26	0.09 292	9.89 101	11	5	40 6.7 6.0
56	9.79 825	16	9.90 734	26	0.09 266	9.89 091	10	4	50 8.3 7.5
57	9.79 840	15	9.90 759	25	0.09 241	9.89 081	10	3	
58	9.79 856	16	9.90 785	26	0.09 215	9.89 071	10	2	
59	9.79 872	16	9.90 811	26	0.09 189	9.89 060	11	1	
60	9.79 887	15	9.90 837	26	0.09 163	9.89 050	10	0	

\*141°

231°

\*321°

51°

<b>39°</b>										*129°	219°	*309°
'	log sin	d.	log tan	c. d.	log cot	log cos	d.			Prop. Pts.		
0	9.79 887		9.90 837		0.09 163	9.89 050		<b>60</b>				
1	9.79 903	16	9.90 863	26	0.09 137	9.89 040	10	59				
2	9.79 918	15	9.90 889	26	0.09 111	9.89 030	10	58				
3	9.79 934	16	9.90 914	25	0.09 086	9.89 020	10	57				
4	9.79 950	16	9.90 940	26	0.09 060	9.89 009	11	56				
		15		26			10					
5	9.79 965		9.90 966		0.09 034	9.88 999	10	55				
6	9.79 981	16	9.90 992	26	0.09 008	9.88 989	10	54				
7	9.79 996	15	9.91 018	26	0.08 982	9.88 978	11	53				
8	9.80 012	16	9.91 043	25	0.08 957	9.88 968	10	52				
9	9.80 027	15	9.91 069	26	0.08 931	9.88 958	10	51				
		16		26			10					
<b>10</b>	9.80 043		9.91 095		0.08 905	9.88 948		<b>50</b>				
11	9.80 058	15	9.91 121	26	0.08 879	9.88 937	11	49				
12	9.80 074	16	9.91 147	26	0.08 853	9.88 927	10	48				
13	9.80 089	15	9.91 172	25	0.08 828	9.88 917	10	47				
14	9.80 105	16	9.91 198	26	0.08 802	9.88 906	11	46				
		15		26			10					
15	9.80 120		9.91 224		0.08 776	9.88 896		45				
16	9.80 136	16	9.91 250	26	0.08 750	9.88 886	10	44				
17	9.80 151	15	9.91 276	25	0.08 724	9.88 875	11	43				
18	9.80 166	15	9.91 301	25	0.08 699	9.88 865	10	42				
19	9.80 182	16	9.91 327	26	0.08 673	9.88 855	10	41				
		15		26			11					
<b>20</b>	9.80 197		9.91 353		0.08 647	9.88 844		<b>40</b>				
21	9.80 213	16	9.91 379	26	0.08 621	9.88 834	10	39				
22	9.80 228	15	9.91 404	25	0.08 596	9.88 824	10	38				
23	9.80 244	16	9.91 430	26	0.08 570	9.88 813	11	37				
24	9.80 259	15	9.91 456	26	0.08 544	9.88 803	10	36				
		15		26			10					
25	9.80 274		9.91 482		0.08 518	9.88 793		35				
26	9.80 290	16	9.91 507	25	0.08 493	9.88 782	11	34				
27	9.80 305	15	9.91 533	26	0.08 467	9.88 772	11	33				
28	9.80 320	15	9.91 559	26	0.08 441	9.88 761	11	32				
29	9.80 336	16	9.91 585	26	0.08 415	9.88 751	10	31				
		15		25			10					
<b>30</b>	9.80 351		9.91 610		0.08 390	9.88 741		<b>30</b>				
31	9.80 366	15	9.91 636	26	0.08 364	9.88 730	11	29				
32	9.80 382	16	9.91 662	26	0.08 338	9.88 720	11	28				
33	9.80 397	15	9.91 688	26	0.08 312	9.88 709	11	27				
34	9.80 412	15	9.91 713	25	0.08 287	9.88 699	11	26				
		16		26			11					
35	9.80 428		9.91 739		0.08 261	9.88 688		25				
36	9.80 443	15	9.91 765	26	0.08 235	9.88 678	10	24				
37	9.80 458	15	9.91 791	26	0.08 209	9.88 668	10	23				
38	9.80 473	15	9.91 816	25	0.08 184	9.88 657	11	22				
39	9.80 489	16	9.91 842	26	0.08 158	9.88 647	11	21				
		15		26			11					
<b>40</b>	9.80 504		9.91 868		0.08 132	9.88 636		<b>20</b>				
41	9.80 519	15	9.91 893	25	0.08 107	9.88 626	10	19				
42	9.80 534	15	9.91 919	26	0.08 081	9.88 615	10	18				
43	9.80 550	16	9.91 945	26	0.08 055	9.88 605	10	17				
44	9.80 565	15	9.91 971	26	0.08 029	9.88 594	11	16				
		15		25			10					
45	9.80 580		9.91 996		0.08 004	9.88 584		15				
46	9.80 595	15	9.92 022	26	0.07 978	9.88 573	11	14				
47	9.80 610	15	9.92 048	26	0.07 952	9.88 563	11	13				
48	9.80 625	15	9.92 073	25	0.07 927	9.88 552	10	12				
49	9.80 641	16	9.92 099	26	0.07 901	9.88 542	10	11				
		15		26			11					
<b>50</b>	9.80 656		9.92 125		0.07 875	9.88 531		<b>10</b>				
51	9.80 671	15	9.92 150	25	0.07 850	9.88 521	10	9				
52	9.80 686	15	9.92 176	26	0.07 824	9.88 510	10	8				
53	9.80 701	15	9.92 202	26	0.07 798	9.88 499	11	7				
54	9.80 716	15	9.92 227	25	0.07 773	9.88 489	10	6				
		15		26			11					
55	9.80 731		9.92 253		0.07 747	9.88 478		5				
56	9.80 746	15	9.92 279	26	0.07 721	9.88 468	10	4				
57	9.80 762	16	9.92 304	25	0.07 696	9.88 457	10	3				
58	9.80 777	15	9.92 330	26	0.07 670	9.88 447	10	2				
59	9.80 792	15	9.92 356	26	0.07 644	9.88 436	11	1				
		15		25			11					
<b>60</b>	9.80 807		9.92 381		0.07 619	9.88 425		<b>0</b>				
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.			

\*140°    230°    \*320°

**50°**

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

<b>40°</b>										*130°	220°	*310°
'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.			
0	9.80 807		9.92 381		0.07 619	9.88 425		<b>60</b>				
1	9.80 822	15	9.92 407	26	0.07 593	9.88 415	IO	59				
2	9.80 837	15	9.92 433	26	0.07 567	9.88 404	IO	58				
3	9.80 852	15	9.92 458	26	0.07 542	9.88 394	IO	57				
4	9.80 867	15	9.92 484	26	0.07 516	9.88 383	IO	56				
5	9.80 882		9.92 510		0.07 490	9.88 372		55				
6	9.80 897	15	9.92 535	25	0.07 465	9.88 362	IO	54				
7	9.80 912	15	9.92 561	26	0.07 439	9.88 351	IO	53				
8	9.80 927	15	9.92 587	26	0.07 413	9.88 340	IO	52				
9	9.80 942	15	9.92 612	25	0.07 388	9.88 330	IO	51				
10	9.80 957		9.92 638		0.07 362	9.88 319		<b>50</b>	" 26 25			
11	9.80 972	15	9.92 663	25	0.07 337	9.88 308	IO	49	6 2.6 2.5			
12	9.80 987	15	9.92 689	26	0.07 311	9.88 298	IO	48	7 3.0 2.9			
13	9.81 002	15	9.92 715	26	0.07 285	9.88 287	IO	47	8 3.5 3.3			
14	9.81 017	15	9.92 740	25	0.07 260	9.88 276	IO	46	9 3.9 3.8			
15	9.81 032	15	9.92 766	26	0.07 234	9.88 266	IO	45	10 4.3 4.2			
16	9.81 047	14	9.92 792	25	0.07 208	9.88 255	IO	44	20 8.7 8.3			
17	9.81 061	15	9.92 817	25	0.07 183	9.88 244	IO	43	30 13.0 12.5			
18	9.81 076	15	9.92 843	25	0.07 157	9.88 234	IO	42	40 17.3 16.7			
19	9.81 091	15	9.92 868	26	0.07 132	9.88 223	IO	41	50 21.7 20.8			
20	9.81 106		9.92 894		0.07 106	9.88 212		<b>40</b>				
21	9.81 121	15	9.92 920	26	0.07 080	9.88 201	IO	39				
22	9.81 136	15	9.92 945	25	0.07 055	9.88 191	IO	38				
23	9.81 151	15	9.92 971	25	0.07 029	9.88 180	IO	37				
24	9.81 166	14	9.92 996	26	0.07 004	9.88 169	IO	36				
25	9.81 180		9.93 022		0.06 978	9.88 158		35				
26	9.81 195	15	9.93 048	26	0.06 952	9.88 148	IO	34				
27	9.81 210	15	9.93 073	25	0.06 927	9.88 137	IO	33	" 15 14			
28	9.81 225	15	9.93 099	25	0.06 901	9.88 126	IO	32	6 1.5 1.4			
29	9.81 240	14	9.93 124	26	0.06 876	9.88 115	IO	31	7 1.8 1.6			
30	9.81 254		9.93 150		0.06 850	9.88 105		<b>30</b>	8 2.0 1.9			
31	9.81 269	15	9.93 175	25	0.06 825	9.88 094	IO	29	9 2.3 2.1			
32	9.81 284	15	9.93 201	26	0.06 799	9.88 083	IO	28	10 2.5 2.3			
33	9.81 299	15	9.93 227	26	0.06 773	9.88 072	IO	27	20 5.0 4.7			
34	9.81 314	14	9.93 252	25	0.06 748	9.88 061	IO	26	30 7.5 7.0			
35	9.81 328		9.93 278		0.06 722	9.88 051		25	40 10.0 9.3			
36	9.81 343	15	9.93 303	25	0.06 697	9.88 040	IO	24	50 12.5 11.7			
37	9.81 358	14	9.93 329	25	0.06 671	9.88 029	IO	23				
38	9.81 372	15	9.93 354	26	0.06 646	9.88 018	IO	22				
39	9.81 387	15	9.93 380	26	0.06 620	9.88 007	IO	21				
40	9.81 402		9.93 406		0.06 594	9.87 996		<b>20</b>				
41	9.81 417	14	9.93 431	25	0.06 569	9.87 985	IO	19				
42	9.81 431	15	9.93 457	26	0.06 543	9.87 975	IO	18				
43	9.81 446	15	9.93 482	25	0.06 518	9.87 964	IO	17				
44	9.81 461	14	9.93 508	25	0.06 492	9.87 953	IO	16	" 11 10			
45	9.81 475		9.93 533		0.06 467	9.87 942		15	6 1.1 1.0			
46	9.81 490	15	9.93 559	26	0.06 441	9.87 931	IO	14	7 1.3 1.2			
47	9.81 505	15	9.93 584	25	0.06 416	9.87 920	IO	13	8 1.5 1.3			
48	9.81 519	14	9.93 610	26	0.06 390	9.87 909	IO	12	9 1.7 1.5			
49	9.81 534	15	9.93 636	26	0.06 364	9.87 898	IO	11	10 1.8 1.7			
50	9.81 549		9.93 661		0.06 339	9.87 887		<b>10</b>	20 3.7 3.3			
51	9.81 563	14	9.93 687	26	0.06 313	9.87 877	IO	9	30 5.5 5.0			
52	9.81 578	15	9.93 712	25	0.06 288	9.87 866	IO	8	40 7.3 6.7			
53	9.81 592	14	9.93 738	26	0.06 262	9.87 855	IO	7	50 9.2 8.3			
54	9.81 607	15	9.93 763	26	0.06 237	9.87 844	IO	6				
55	9.81 622		9.93 789		0.06 211	9.87 833		5				
56	9.81 636	14	9.93 814	25	0.06 186	9.87 822	IO	4				
57	9.81 651	15	9.93 840	26	0.06 160	9.87 811	IO	3				
58	9.81 665	14	9.93 865	25	0.06 135	9.87 800	IO	2				
59	9.81 680	15	9.93 891	26	0.06 109	9.87 789	IO	1				
60	9.81 694	14	9.93 916	25	0.06 084	9.87 778	IO	<b>0</b>				
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.			

\*139°      229°      \*319°

**49°**

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

41°

\*131°

221°

\*311°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.	Prop. Pts.
0	9.81 694		9.93 916		0.06 084	9.87 778	60	
1	9.81 709	15	9.93 942	26	0.06 058	9.87 767	59	
2	9.81 723	14	9.93 967	25	0.06 033	9.87 756	58	
3	9.81 738	15	9.93 993	26	0.06 007	9.87 745	57	
4	9.81 752	14	9.94 018	25	0.05 982	9.87 734	56	
5	9.81 767	15	9.94 044	26	0.05 956	9.87 723	55	
6	9.81 781	14	9.94 069	25	0.05 931	9.87 712	54	
7	9.81 796	15	9.94 095	26	0.05 905	9.87 701	53	
8	9.81 810	14	9.94 120	25	0.05 880	9.87 690	52	
9	9.81 825	15	9.94 146	26	0.05 854	9.87 679	51	
10	9.81 839	14	9.94 171	25	0.05 829	9.87 668	50	" 26 25
11	9.81 854	15	9.94 197	26	0.05 803	9.87 657	49	6 2.6 2.5
12	9.81 868	14	9.94 222	25	0.05 778	9.87 646	48	7 3.0 2.9
13	9.81 882	15	9.94 248	26	0.05 752	9.87 635	47	8 3.5 3.3
14	9.81 897	14	9.94 273	25	0.05 727	9.87 624	46	9 3.9 3.8
15	9.81 911	15	9.94 299	26	0.05 701	9.87 613	45	10 4.3 4.2
16	9.81 926	14	9.94 324	25	0.05 676	9.87 601	44	20 8.7 8.3
17	9.81 940	15	9.94 350	26	0.05 650	9.87 590	43	30 13.0 12.5
18	9.81 955	14	9.94 375	25	0.05 625	9.87 579	42	40 17.3 16.7
19	9.81 969	15	9.94 401	26	0.05 599	9.87 568	41	50 21.7 20.8
20	9.81 983	14	9.94 426	25	0.05 574	9.87 557	40	
21	9.81 998	15	9.94 452	26	0.05 548	9.87 546	39	
22	9.82 012	14	9.94 477	25	0.05 523	9.87 535	38	
23	9.82 026	15	9.94 503	26	0.05 497	9.87 524	37	
24	9.82 041	14	9.94 528	25	0.05 472	9.87 513	36	
25	9.82 055	15	9.94 554	26	0.05 446	9.87 501	35	
26	9.82 069	14	9.94 579	25	0.05 421	9.87 490	34	
27	9.82 084	15	9.94 604	26	0.05 396	9.87 479	33	" 15 14
28	9.82 098	14	9.94 630	25	0.05 370	9.87 468	32	6 1.5 1.4
29	9.82 112	15	9.94 655	26	0.05 345	9.87 457	31	7 1.8 1.6
30	9.82 126	14	9.94 681	25	0.05 319	9.87 446	30	8 2.0 1.9
31	9.82 141	15	9.94 706	26	0.05 294	9.87 434	29	9 2.3 2.1
32	9.82 155	14	9.94 732	25	0.05 268	9.87 423	28	10 2.5 2.3
33	9.82 169	15	9.94 757	26	0.05 243	9.87 412	27	20 5.0 4.7
34	9.82 184	14	9.94 783	25	0.05 217	9.87 401	26	30 7.5 7.0
35	9.82 198	15	9.94 808	26	0.05 192	9.87 390	25	40 10.0 9.3
36	9.82 212	14	9.94 834	25	0.05 166	9.87 378	24	50 12.5 11.7
37	9.82 226	15	9.94 859	26	0.05 141	9.87 367	23	
38	9.82 240	14	9.94 884	25	0.05 116	9.87 356	22	
39	9.82 255	15	9.94 910	26	0.05 090	9.87 345	21	
40	9.82 269	14	9.94 935	25	0.05 065	9.87 334	20	
41	9.82 283	15	9.94 961	26	0.05 039	9.87 322	19	
42	9.82 297	14	9.94 986	25	0.05 014	9.87 311	18	
43	9.82 311	15	9.95 012	26	0.04 988	9.87 300	17	
44	9.82 326	14	9.95 037	25	0.04 963	9.87 288	16	" 12 11
45	9.82 340	15	9.95 062	26	0.04 938	9.87 277	15	6 1.2 1.1
46	9.82 354	14	9.95 088	25	0.04 912	9.87 266	14	7 1.4 1.3
47	9.82 368	15	9.95 113	26	0.04 887	9.87 255	13	8 1.6 1.5
48	9.82 382	14	9.95 139	25	0.04 861	9.87 243	12	9 1.8 1.7
49	9.82 396	15	9.95 164	26	0.04 836	9.87 232	11	10 2.0 1.8
50	9.82 410	14	9.95 190	25	0.04 810	9.87 221	10	20 4.0 3.7
51	9.82 424	15	9.95 215	26	0.04 785	9.87 209	9	30 6.0 5.5
52	9.82 439	14	9.95 240	25	0.04 760	9.87 198	8	40 8.0 7.3
53	9.82 453	15	9.95 266	26	0.04 734	9.87 187	7	50 10.0 9.2
54	9.82 467	14	9.95 291	25	0.04 709	9.87 175	6	
55	9.82 481	15	9.95 317	26	0.04 683	9.87 164	5	
56	9.82 495	14	9.95 342	25	0.04 658	9.87 153	4	
57	9.82 509	15	9.95 368	26	0.04 632	9.87 141	3	
58	9.82 523	14	9.95 393	25	0.04 607	9.87 130	2	
59	9.82 537	15	9.95 418	26	0.04 582	9.87 119	1	
60	9.82 551	14	9.95 444	25	0.04 556	9.87 107	0	
	log cos	d.	log cot	c. d.	log tan	log sin	d.	Prop. Pts.

\*138°

228°

\*318°

48°

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

42°

\*132°

222°

\*312°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.82 551		9.95 444		0.04 556	9.87 107		60	
1	9.82 565	14	9.95 469	25	0.04 531	9.87 096	11	59	
2	9.82 579	14	9.95 495	26	0.04 505	9.87 085	12	58	
3	9.82 593	14	9.95 520	25	0.04 480	9.87 073	11	57	
4	9.82 607	14	9.95 545	26	0.04 455	9.87 062	12	56	
5	9.82 621		9.95 571		0.04 429	9.87 050		55	
6	9.82 635	14	9.95 596	25	0.04 404	9.87 039	11	54	
7	9.82 649	14	9.95 622	26	0.04 378	9.87 028	12	53	
8	9.82 663	14	9.95 647	25	0.04 353	9.87 016	11	52	
9	9.82 677	14	9.95 672	26	0.04 328	9.87 005	12	51	
10	9.82 691		9.95 698		0.04 302	9.86 993		50	" 26 25
11	9.82 705	14	9.95 723	25	0.04 277	9.86 982	11	49	6 2.6 2.5
12	9.82 719	14	9.95 748	26	0.04 252	9.86 970	12	48	7 3.0 2.9
13	9.82 733	14	9.95 774	25	0.04 226	9.86 959	11	47	8 3.5 3.3
14	9.82 747	14	9.95 799	26	0.04 201	9.86 947	12	46	9 3.9 3.8
15	9.82 761		9.95 825		0.04 175	9.86 936		45	10 4.3 4.2
16	9.82 775	14	9.95 850	25	0.04 150	9.86 924	12	44	20 8.7 8.3
17	9.82 788	13	9.95 875	25	0.04 125	9.86 913	11	43	30 13.0 12.5
18	9.82 802	14	9.95 901	26	0.04 099	9.86 902	12	42	40 17.3 16.7
19	9.82 816	14	9.95 926	25	0.04 074	9.86 890	11	41	50 21.7 20.8
20	9.82 830		9.95 952		0.04 048	9.86 879		40	
21	9.82 844	14	9.95 977	25	0.04 023	9.86 867	12	39	
22	9.82 858	14	9.96 002	25	0.03 998	9.86 855	12	38	
23	9.82 872	14	9.96 028	26	0.03 972	9.86 844	11	37	
24	9.82 885	14	9.96 053	25	0.03 947	9.86 832	12	36	
25	9.82 899		9.96 078		0.03 922	9.86 821		35	
26	9.82 913	14	9.96 104	26	0.03 896	9.86 809	12	34	
27	9.82 927	14	9.96 129	25	0.03 871	9.86 798	11	33	" 14 13
28	9.82 941	14	9.96 155	26	0.03 845	9.86 786	12	32	6 1.4 1.3
29	9.82 955	13	9.96 180	25	0.03 820	9.86 775	11	31	7 1.6 1.5
30	9.82 968		9.96 205		0.03 795	9.86 763		30	8 1.0 1.7
31	9.82 982	14	9.96 231	26	0.03 769	9.86 752	12	29	9 2.1 2.0
32	9.82 996	14	9.96 256	25	0.03 744	9.86 740	12	28	10 2.3 2.2
33	9.83 010	14	9.96 281	25	0.03 719	9.86 728	12	27	20 4.7 4.3
34	9.83 023	13	9.96 307	26	0.03 693	9.86 717	11	26	30 7.0 6.5
35	9.83 037		9.96 332		0.03 668	9.86 705		25	40 9.3 8.7
36	9.83 051	14	9.96 357	25	0.03 643	9.86 694	12	24	50 11.7 10.8
37	9.83 065	14	9.96 383	26	0.03 617	9.86 682	11	23	
38	9.83 078	13	9.96 408	25	0.03 592	9.86 670	12	22	
39	9.83 092	14	9.96 433	25	0.03 567	9.86 659	11	21	
40	9.83 106		9.96 459		0.03 541	9.86 647		20	
41	9.83 120	14	9.96 484	25	0.03 516	9.86 635	12	19	
42	9.83 133	13	9.96 510	26	0.03 490	9.86 624	11	18	
43	9.83 147	14	9.96 535	25	0.03 465	9.86 612	12	17	
44	9.83 161	14	9.96 560	26	0.03 440	9.86 600	12	16	" 12 11
45	9.83 174		9.96 586		0.03 414	9.86 589		15	6 1.2 1.1
46	9.83 188	14	9.96 611	25	0.03 389	9.86 577	12	14	7 1.4 1.3
47	9.83 202	14	9.96 636	25	0.03 364	9.86 565	12	13	8 1.6 1.5
48	9.83 215	13	9.96 662	26	0.03 338	9.86 554	11	12	9 1.8 1.6
49	9.83 229	14	9.96 687	25	0.03 313	9.86 542	12	11	10 2.0 1.8
50	9.83 242	13	9.96 712	25	0.03 288	9.86 530	12	10	20 4.0 3.7
51	9.83 256	14	9.96 738	26	0.03 262	9.86 518	12	9	30 6.0 5.5
52	9.83 270	14	9.96 763	25	0.03 237	9.86 507	11	8	40 8.0 7.3
53	9.83 283	13	9.96 788	25	0.03 212	9.86 495	12	7	50 10.0 9.2
54	9.83 297	14	9.96 814	26	0.03 186	9.86 483	12	6	
55	9.83 310	13	9.96 839	25	0.03 161	9.86 472	11	5	
56	9.83 324		9.96 864		0.03 136	9.86 460		4	
57	9.83 338	14	9.96 890	25	0.03 110	9.86 448	12	3	
58	9.83 351	13	9.96 915	26	0.03 085	9.86 436	12	2	
59	9.83 365	14	9.96 940	25	0.03 060	9.86 425	11	1	
60	9.83 378	13	9.96 966	26	0.03 034	9.86 413	12	0	
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.

\*137°

227°

\*317°

47°

LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

43°

\*133°

223°

\*313°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.83 378		9.96 966		0.03 034	9.86 413		60	
1	9.83 392	14	9.96 991	25	0.03 009	9.86 401	12	59	
2	9.83 405	13	9.97 016	25	0.02 984	9.86 389	12	58	
3	9.83 419	14	9.97 042	26	0.02 958	9.86 377	12	57	
4	9.83 432	13	9.97 067	25	0.02 933	9.86 366	11	56	
		14		25			12		
5	9.83 446		9.97 092		0.02 908	9.86 354		55	
6	9.83 459	13	9.97 118	26	0.02 882	9.86 342	12	54	
7	9.83 473	14	9.97 143	25	0.02 857	9.86 330	12	53	
8	9.83 486	13	9.97 168	25	0.02 832	9.86 318	12	52	
9	9.83 500	14	9.97 193	25	0.02 807	9.86 306	11	51	
		13		26			12		
10	9.83 513		9.97 219		0.02 781	9.86 295		50	" 26   25
11	9.83 527	14	9.97 244	25	0.02 756	9.86 283	12	49	6 2.6 2.5
12	9.83 540	13	9.97 269	25	0.02 731	9.86 271	12	48	7 3.0 2.9
13	9.83 554	14	9.97 295	26	0.02 705	9.86 259	12	47	8 3.5 3.3
14	9.83 567	13	9.97 320	25	0.02 680	9.86 247	12	46	9 3.9 3.8
		14		25			12		10 4.3 4.2
15	9.83 581		9.97 345		0.02 655	9.86 235		45	20 8.7 8.3
16	9.83 594	13	9.97 371	26	0.02 629	9.86 223	12	44	30 13.0 12.5
17	9.83 608	14	9.97 396	25	0.02 604	9.86 211	12	43	40 17.3 16.7
18	9.83 621	13	9.97 421	25	0.02 579	9.86 200	11	42	50 21.7 20.8
19	9.83 634	13	9.97 447	26	0.02 553	9.86 188	12	41	
		14		25			12		
20	9.83 648		9.97 472		0.02 528	9.86 176		40	
21	9.83 661	13	9.97 497	25	0.02 503	9.86 164	12	39	
22	9.83 674	13	9.97 523	26	0.02 477	9.86 152	12	38	
23	9.83 688	14	9.97 548	25	0.02 452	9.86 140	12	37	
24	9.83 701	13	9.97 573	25	0.02 427	9.86 128	12	36	
		14		25			12		
25	9.83 715		9.97 598		0.02 402	9.86 116		35	
26	9.83 728	13	9.97 624	26	0.02 376	9.86 104	12	34	
27	9.83 741	13	9.97 649	25	0.02 351	9.86 092	12	33	" 14   13
28	9.83 755	14	9.97 674	25	0.02 326	9.86 080	12	32	6 1.4 1.3
29	9.83 768	13	9.97 700	26	0.02 300	9.86 068	12	31	7 1.6 1.5
		13		25			12		8 1.9 1.7
30	9.83 781		9.97 725		0.02 275	9.86 056		30	9 2.1 2.0
31	9.83 795	14	9.97 750	25	0.02 250	9.86 044	12	29	10 2.3 2.2
32	9.83 808	13	9.97 776	26	0.02 224	9.86 032	12	28	20 4.7 4.3
33	9.83 821	13	9.97 801	25	0.02 199	9.86 020	12	27	30 7.0 6.5
34	9.83 834	13	9.97 826	25	0.02 174	9.86 008	12	26	40 9.3 8.7
		14		25			12		50 11.7 10.8
35	9.83 848		9.97 851		0.02 149	9.85 996		25	
36	9.83 861	13	9.97 877	26	0.02 123	9.85 984	12	24	
37	9.83 874	13	9.97 902	25	0.02 098	9.85 972	12	23	
38	9.83 887	13	9.97 927	25	0.02 073	9.85 960	12	22	
39	9.83 901	14	9.97 953	26	0.02 047	9.85 948	12	21	
		13		25			12		
40	9.83 914		9.97 978		0.02 022	9.85 936		20	
41	9.83 927	13	9.98 003	25	0.01 997	9.85 924	12	19	
42	9.83 940	13	9.98 029	26	0.01 971	9.85 912	12	18	
43	9.83 954	14	9.98 054	25	0.01 946	9.85 900	12	17	
44	9.83 967	13	9.98 079	25	0.01 921	9.85 888	12	16	" 12   11
		13		25			12		6 1.2 1.1
45	9.83 980		9.98 104		0.01 896	9.85 876		15	7 1.4 1.3
46	9.83 993	13	9.98 130	26	0.01 870	9.85 864	12	14	8 1.6 1.5
47	9.84 006	13	9.98 155	25	0.01 845	9.85 851	13	13	9 1.8 1.6
48	9.84 020	14	9.98 180	25	0.01 820	9.85 839	12	12	10 2.0 1.8
49	9.84 033	13	9.98 206	26	0.01 794	9.85 827	12	11	20 4.0 3.7
		13		25			12		30 6.0 5.5
50	9.84 046		9.98 231		0.01 769	9.85 815		10	40 8.0 7.3
51	9.84 059	13	9.98 256	25	0.01 744	9.85 803	12	9	50 10.0 9.2
52	9.84 072	13	9.98 281	25	0.01 719	9.85 791	12	8	
53	9.84 085	13	9.98 307	26	0.01 693	9.85 779	12	7	
54	9.84 098	13	9.98 332	25	0.01 668	9.85 766	13	6	
		14		25			12		
55	9.84 112		9.98 357		0.01 643	9.85 754		5	
56	9.84 125	13	9.98 383	26	0.01 617	9.85 742	12	4	
57	9.84 138	13	9.98 408	25	0.01 592	9.85 730	12	3	
58	9.84 151	13	9.98 433	25	0.01 567	9.85 718	12	2	
59	9.84 164	13	9.98 458	25	0.01 542	9.85 706	12	1	
60	9.84 177	13	9.98 484	26	0.01 516	9.85 693	13	0	
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.

\*136°

226°

\*316°

46°



LOGARITHMS OF THE TRIGONOMETRIC FUNCTIONS

44°

\*134°

224°

\*314°

'	log sin	d.	log tan	c. d.	log cot	log cos	d.		Prop. Pts.
0	9.84 177		9.98 484		0.01 516	9.85 693		60	
1	9.84 190	13	9.98 509	25	0.01 491	9.85 681	12	59	
2	9.84 203	13	9.98 534	25	0.01 466	9.85 669	12	58	
3	9.84 216	13	9.98 560	26	0.01 440	9.85 657	12	57	
4	9.84 229	13	9.98 585	25	0.01 415	9.85 645	12	56	
5	9.84 242	13	9.98 610	25	0.01 390	9.85 632	13	55	
6	9.84 255	13	9.98 635	25	0.01 365	9.85 620	12	54	
7	9.84 269	14	9.98 661	26	0.01 339	9.85 608	12	53	
8	9.84 282	13	9.98 686	25	0.01 314	9.85 596	12	52	
9	9.84 295	13	9.98 711	25	0.01 289	9.85 583	13	51	
10	9.84 308	13	9.98 737	26	0.01 263	9.85 571	12	50	
11	9.84 321	13	9.98 762	25	0.01 238	9.85 559	12	49	
12	9.84 334	13	9.98 787	25	0.01 213	9.85 547	12	48	
13	9.84 347	13	9.98 812	25	0.01 188	9.85 534	13	47	
14	9.84 360	13	9.98 838	26	0.01 162	9.85 522	12	46	
15	9.84 373	13	9.98 863	25	0.01 137	9.85 510	12	45	" 26 25 14
16	9.84 385	12	9.98 888	25	0.01 112	9.85 497	13	44	6 2.6 2.5 1.4
17	9.84 398	12	9.98 913	25	0.01 087	9.85 485	12	43	7 3.0 2.9 1.6
18	9.84 411	13	9.98 939	26	0.01 061	9.85 473	12	42	8 3.5 3.3 1.9
19	9.84 424	13	9.98 964	25	0.01 036	9.85 460	13	41	9 3.9 3.8 2.1
20	9.84 437	13	9.98 989	25	0.01 011	9.85 448	12	40	10 4.3 4.2 2.3
21	9.84 450	13	9.99 015	26	0.00 985	9.85 436	12	39	20 8.7 8.3 4.7
22	9.84 463	13	9.99 040	25	0.00 960	9.85 423	13	38	30 13.0 12.5 7.0
23	9.84 476	13	9.99 065	25	0.00 935	9.85 411	12	37	40 17.3 16.7 9.3
24	9.84 489	13	9.99 090	25	0.00 910	9.85 399	12	36	50 21.7 20.8 11.7
25	9.84 502	13	9.99 116	26	0.00 884	9.85 386	13	35	
26	9.84 515	13	9.99 141	25	0.00 859	9.85 374	12	34	
27	9.84 528	13	9.99 166	25	0.00 834	9.85 361	13	33	
28	9.84 540	12	9.99 191	25	0.00 809	9.85 349	12	32	
29	9.84 553	13	9.99 217	26	0.00 783	9.85 337	12	31	
30	9.84 566	13	9.99 242	25	0.00 758	9.85 324	13	30	
31	9.84 579	13	9.99 267	25	0.00 733	9.85 312	12	29	
32	9.84 592	13	9.99 293	26	0.00 707	9.85 299	13	28	
33	9.84 605	13	9.99 318	25	0.00 682	9.85 287	12	27	
34	9.84 618	13	9.99 343	25	0.00 657	9.85 274	13	26	
35	9.84 630	12	9.99 368	25	0.00 632	9.85 262	12	25	
36	9.84 643	13	9.99 394	26	0.00 606	9.25 250	12	24	
37	9.84 656	13	9.99 419	25	0.00 581	9.85 237	13	23	
38	9.84 669	13	9.99 444	25	0.00 556	9.85 225	12	22	
39	9.84 682	13	9.99 469	25	0.00 531	9.85 212	13	21	" 13 12
40	9.84 694	12	9.99 495	26	0.00 505	9.85 200	12	20	6 1.3 1.2
41	9.84 707	13	9.99 520	25	0.00 480	9.85 187	13	19	7 1.5 1.4
42	9.84 720	13	9.99 545	25	0.00 455	9.85 175	12	18	8 1.7 1.6
43	9.84 733	13	9.99 570	25	0.00 430	9.85 162	13	17	9 2.0 1.8
44	9.84 745	12	9.99 596	26	0.00 404	9.85 150	12	16	10 2.2 2.0
45	9.84 758	13	9.99 621	25	0.00 379	9.85 137	13	15	20 4.3 4.0
46	9.84 771	13	9.99 646	25	0.00 354	9.85 125	12	14	30 6.5 6.0
47	9.84 784	13	9.99 672	26	0.00 328	9.85 112	13	13	40 8.7 8.0
48	9.84 796	12	9.99 697	25	0.00 303	9.85 100	12	12	50 10.8 10.0
49	9.84 809	13	9.99 722	25	0.00 278	9.85 087	13	11	
50	9.84 822	13	9.99 747	25	0.00 253	9.85 074	13	10	
51	9.84 835	13	9.99 773	26	0.00 227	9.85 062	12	9	
52	9.84 847	12	9.99 798	25	0.00 202	9.85 049	13	8	
53	9.84 860	13	9.99 823	25	0.00 177	9.85 037	12	7	
54	9.84 873	13	9.99 848	25	0.00 152	9.85 024	13	6	
55	9.84 885	12	9.99 874	26	0.00 126	9.85 012	12	5	
56	9.84 898	13	9.99 899	25	0.00 101	9.84 999	13	4	
57	9.84 911	13	9.99 924	25	0.00 076	9.84 986	13	3	
58	9.84 923	12	9.99 949	25	0.00 051	9.84 974	12	2	
59	9.84 936	13	9.99 975	26	0.00 025	9.84 961	13	1	
60	9.84 949	13	0.00 000	25	0.00 000	9.84 949	12	0	
	log cos	d.	log cot	c. d.	log tan	log sin	d.	'	Prop. Pts.

\*135°

225°

\*315°

45°



**TABLE III**



**NATURAL TRIGONOMETRIC FUNCTIONS**

**FOUR PLACES**

NATURAL SINES AND COSINES

/	0°		1°		2°		3°		4°		/
	sin	cos	sin	cos	sin	cos	sin	cos	sin	cos	
0	.0000	1.000	.0175	.9998	.0349	.9994	.0523	.9986	.0698	.9976	<b>60</b>
1	03	.000	77	98	52	94	26	86	0700	75	59
2	06	.000	80	98	55	94	29	86	03	75	58
3	09	.000	83	98	58	94	32	86	06	75	57
4	12	.000	86	98	61	93	35	86	09	75	56
5	.0015	1.000	.0189	.9998	.0364	.9993	.0538	.9986	.0712	.9975	<b>55</b>
6	17	.000	92	98	66	93	41	85	15	74	54
7	20	.000	95	98	69	93	44	85	18	74	53
8	23	.000	98	98	72	93	47	85	21	74	52
9	26	.000	0201	98	75	93	50	85	24	74	51
10	.0029	1.000	.0204	.9998	.0378	.9993	.0552	.9985	.0727	.9974	<b>50</b>
11	32	.000	07	98	81	93	55	85	29	73	49
12	35	.000	09	98	84	93	58	84	32	73	48
13	38	.000	12	98	87	93	61	84	35	73	47
14	41	.000	15	98	90	92	64	84	38	73	46
15	.0044	1.000	.0218	.9998	.0393	.9992	.0567	.9984	.0741	.9973	<b>45</b>
16	47	.000	21	98	96	92	70	84	44	72	44
17	49	.000	24	97	98	92	73	84	47	72	43
18	52	.000	27	97	0401	92	76	83	50	72	42
19	55	.000	30	97	04	92	79	83	53	72	41
20	.0058	1.000	.0233	.9997	.0407	.9992	.0581	.9983	.0756	.9971	<b>40</b>
21	61	.000	36	97	10	92	84	83	58	71	39
22	64	.000	39	97	13	91	87	83	61	71	38
23	67	.000	41	97	16	91	90	83	64	71	37
24	70	.000	44	97	19	91	93	82	67	71	36
25	.0073	1.000	.0247	.9997	.0422	.9991	.0596	.9982	.0770	.9970	<b>35</b>
26	76	.000	50	97	25	91	99	82	73	70	34
27	79	.000	53	97	27	91	0602	82	76	70	33
28	81	.000	56	97	30	91	05	82	79	70	32
29	84	.000	59	97	33	91	08	82	82	69	31
30	.0087	1.000	.0262	.9997	.0436	.9990	.0610	.9981	.0785	.9969	<b>30</b>
31	90	.000	65	96	39	90	13	81	87	69	29
32	93	.000	68	96	42	90	16	81	90	69	28
33	96	.000	70	96	45	90	19	81	93	68	27
34	99	.000	73	96	48	90	22	81	96	68	26
35	.0102	.9999	.0276	.9996	.0451	.9990	.0625	.9980	.0799	.9968	<b>25</b>
36	05	99	79	96	54	90	28	80	0802	68	24
37	08	99	82	96	57	90	31	80	05	68	23
38	11	99	85	96	59	89	34	80	08	67	22
39	13	99	88	96	62	89	37	80	11	67	21
40	.0116	.9999	.0291	.9996	.0465	.9989	.0640	.9980	.0814	.9967	<b>20</b>
41	19	99	94	96	68	89	42	79	16	67	19
42	22	99	97	96	71	89	45	79	19	66	18
43	25	99	0300	96	74	89	48	79	22	66	17
44	28	99	02	95	77	89	51	79	25	66	16
45	.0131	.9999	.0305	.9995	.0480	.9988	.0654	.9979	.0828	.9966	<b>15</b>
46	34	99	08	95	83	88	57	78	31	65	14
47	37	99	11	95	86	88	60	78	34	65	13
48	40	99	14	95	88	88	63	78	37	65	12
49	43	99	17	95	91	88	66	78	40	65	11
50	.0145	.9999	.0320	.9995	.0494	.9988	.0669	.9978	.0843	.9964	<b>10</b>
51	48	99	23	95	97	88	71	77	45	64	9
52	51	99	26	95	0500	87	74	77	48	64	8
53	54	99	29	95	03	87	77	77	51	64	7
54	57	99	32	95	06	87	80	77	54	63	6
55	.0160	.9999	.0334	.9994	.0509	.9987	.0683	.9977	.0857	.9963	<b>5</b>
56	63	99	37	94	12	87	86	76	60	63	4
57	66	99	40	94	15	87	89	76	63	63	3
58	69	99	43	94	18	87	92	76	66	62	2
59	72	99	46	94	20	86	95	76	69	62	1
60	.0175	.9998	.0349	.9994	.0523	.9986	.0698	.9976	.0872	.9962	<b>0</b>
	cos	sin	cos	sin	cos	sin	cos	sin	cos	sin	
/	89°		88°		87°		86°		85°		/

NATURAL TANGENTS AND COTANGENTS

/	0°		1°		2°		3°		4°		/
	tan	cot	tan	cot	tan	cot	tan	cot	tan	cot	
0	.0000	Infinite	.0175	57.2900	.0349	28.6363	.0524	19.0811	.0699	14.3007	60
1	03	3437.75	77	56.3506	52	3994	27	18.9755	0702	2411	59
2	06	1718.87	80	55.4415	55	1664	30	8711	05	1821	58
3	09	1145.92	83	54.5613	58	27.9372	33	7678	08	1235	57
4	12	859.436	86	53.7086	61	7117	36	6656	11	0655	56
5	.0015	687.549	.0189	52.8821	.0364	27.4899	.0539	18.5645	.0714	14.0079	55
6	17	572.957	92	0807	67	2715	42	4645	17	13.9507	54
7	20	491.106	95	51.3032	70	0566	44	3655	20	8940	53
8	23	429.718	98	50.5485	73	26.8450	47	2677	23	8378	52
9	26	381.971	0201	49.8157	75	6367	50	1708	26	7821	51
10	.0029	343.774	.0204	49.1039	.0378	26.4316	.0553	18.0750	.0729	13.7267	50
11	32	312.521	07	48.4121	81	2296	56	17.9802	31	6719	49
12	35	286.478	09	47.7395	84	0307	59	8863	34	6174	48
13	38	264.441	12	0853	87	25.8348	62	7934	37	5634	47
14	41	245.552	15	46.4489	90	6418	65	7015	40	5098	46
15	.0044	229.182	.0218	45.8294	.0393	25.4517	.0568	17.6106	.0743	13.4566	45
16	47	214.858	21	2261	96	2644	71	5205	46	4039	44
17	49	202.219	24	44.6386	99	0798	74	4314	49	3515	43
18	52	190.984	27	0661	0402	24.8978	77	3432	52	2996	42
19	55	180.932	30	43.5081	05	7185	80	2558	55	2480	41
20	.0058	171.885	.0233	42.9641	.0407	24.5418	.0582	17.1693	.0758	13.1969	40
21	61	163.700	36	4335	10	3675	85	0837	61	1461	39
22	64	156.259	39	41.9158	13	1957	88	16.9990	64	0958	38
23	67	149.465	41	4106	16	0263	91	9150	67	0458	37
24	70	143.237	44	40.9174	19	23.8593	94	8319	69	12.9962	36
25	.0073	137.507	.0247	40.4358	.0422	23.6945	.0597	16.7496	.0772	12.9469	35
26	76	132.219	50	39.9655	25	5321	0600	6681	75	8981	34
27	79	127.321	53	5059	28	3718	03	5874	78	8496	33
28	81	122.774	56	0568	31	2137	06	5075	81	8014	32
29	84	118.540	59	38.6177	34	0577	09	4283	84	7536	31
30	.0087	114.589	.0262	38.1885	.0437	22.9038	.0612	16.3499	.0787	12.7062	30
31	90	110.892	65	37.7686	40	7519	15	2722	90	6591	29
32	93	107.426	68	3579	42	6020	17	1952	93	6124	28
33	96	104.171	71	36.9560	45	4541	20	1190	96	5660	27
34	99	101.107	74	5627	48	3081	23	0435	99	5199	26
35	.0102	98.2179	.0276	36.1776	.0451	22.1640	.0626	15.9687	.0802	12.4742	25
36	05	95.4895	79	35.8006	54	0217	29	8945	05	4288	24
37	08	92.9085	82	4313	57	21.8813	32	8211	08	3838	23
38	11	90.4633	85	0695	60	7426	35	7483	10	3390	22
39	13	88.1436	88	34.7151	63	6056	38	6762	13	2946	21
40	.0116	85.9398	.0291	34.3678	.0466	21.4704	.0641	15.6048	.0816	12.2505	20
41	19	83.8435	94	0273	69	3369	44	5340	19	2067	19
42	22	81.8470	97	33.6935	72	2049	47	4638	22	1632	18
43	25	79.9434	0300	3662	75	0747	50	3943	25	1201	17
44	28	78.1263	03	0452	77	20.9460	53	3254	28	0772	16
45	.0131	76.3900	.0306	32.7303	.0480	20.8188	.0655	15.2571	.0831	12.0346	15
46	34	74.7292	08	4213	83	6932	58	1893	34	11.9923	14
47	37	73.1390	11	1181	86	5691	61	1222	37	9504	13
48	40	71.6151	14	31.8205	89	4465	64	0557	40	9087	12
49	43	70.1533	17	5284	92	3253	67	14.9898	43	8673	11
50	.0145	68.7501	.0320	31.2416	.0495	20.2056	.0670	14.9244	.0846	11.8262	10
51	48	67.4019	23	30.9599	98	0872	73	8596	49	7853	9
52	51	66.1055	26	6833	0501	19.9702	76	7954	51	7448	8
53	54	64.8580	29	4116	04	8546	79	7317	54	7045	7
54	57	63.6567	32	1446	07	7403	82	6685	57	6645	6
55	.0160	62.4992	.0335	29.8823	.0509	19.6273	.0685	14.6059	.0860	11.6248	5
56	63	61.3829	38	6245	12	5156	88	5438	63	5853	4
57	66	60.3058	40	3711	15	4051	90	4823	66	5461	3
58	69	59.2659	43	1220	18	2959	93	4212	69	5072	2
59	72	58.2612	46	28.8771	21	1879	96	3607	72	4685	1
60	.0175	57.2900	.0349	28.6363	.0524	19.0811	.0699	14.3007	.0875	11.4301	0
	cot	tan	cot	tan	cot	tan	cot	tan	cot	tan	
/	89°		88°		87°		86°		85°		/

NATURAL SINES AND COSINES

/	5°		6°		7°		8°		9°		/
	sin	cos	sin	cos	sin	cos	sin	cos	sin	cos	
0	.0872	.9962	.1045	.9945	.1219	.9925	.1392	.9903	.1564	.9877	60
1	74	62	48	45	22	25	95	02	67	76	59
2	77	61	51	45	24	25	97	02	70	76	58
3	80	61	54	44	27	24	1400	01	73	76	57
4	83	61	57	44	30	24	03	01	76	75	56
5	.0886	.9961	.1060	.9944	.1233	.9924	.1406	.9901	.1579	.9875	55
6	89	60	63	43	36	23	09	00	82	74	54
7	92	60	66	43	39	23	12	00	84	74	53
8	95	60	68	43	42	23	15	9899	87	73	52
9	98	60	71	42	45	22	18	99	90	73	51
10	.0901	.9959	.1074	.9942	.1248	.9922	.1421	.9899	.1593	.9872	50
11	03	59	77	42	50	22	23	98	96	72	49
12	06	59	80	42	53	21	26	98	99	71	48
13	09	59	83	41	56	21	29	97	1602	71	47
14	12	58	86	41	59	20	32	97	05	70	46
15	.0915	.9958	.1089	.9941	.1262	.9920	.1435	.9897	.1607	.9870	45
16	18	58	92	40	65	20	38	96	10	69	44
17	21	58	94	40	68	19	41	96	13	69	43
18	24	57	97	40	71	19	44	95	16	69	42
19	27	57	1100	39	74	19	46	95	19	68	41
20	.0929	.9957	.1103	.9939	.1276	.9918	.1449	.9894	.1622	.9868	40
21	32	56	06	39	79	18	52	94	25	67	39
22	35	56	09	38	82	17	55	94	28	67	38
23	38	56	12	38	85	17	58	93	30	66	37
24	41	56	15	38	88	17	61	93	33	66	36
25	.0944	.9955	.1118	.9937	.1291	.9916	.1464	.9892	.1636	.9865	35
26	47	55	20	37	94	16	67	92	39	65	34
27	50	55	23	37	97	16	69	91	42	64	33
28	53	55	26	36	99	15	72	91	45	64	32
29	56	54	29	36	1302	15	75	91	48	63	31
30	.0958	.9954	.1132	.9936	.1305	.9914	.1478	.9890	.1650	.9863	30
31	61	54	35	35	08	14	81	90	53	62	29
32	64	53	38	35	11	14	84	89	56	62	28
33	67	53	41	35	14	13	87	89	59	61	27
34	70	53	44	34	17	13	90	88	62	61	26
35	.0973	.9953	.1146	.9934	.1320	.9913	.1492	.9888	.1665	.9860	25
36	76	52	49	34	23	12	95	88	68	60	24
37	79	52	52	33	25	12	98	87	71	59	23
38	82	52	55	33	28	11	1501	87	73	59	22
39	85	51	58	33	31	11	04	86	76	59	21
40	.0987	.9951	.1161	.9932	.1334	.9911	.1507	.9886	.1679	.9858	20
41	90	51	64	32	37	10	10	85	82	58	19
42	93	51	67	32	40	10	13	85	85	57	18
43	96	50	70	31	43	09	15	84	88	57	17
44	99	50	72	31	46	09	18	84	91	56	16
45	.1002	.9950	.1175	.9931	.1349	.9909	.1521	.9884	.1693	.9856	15
46	05	49	78	30	51	08	24	83	96	55	14
47	08	49	81	30	54	08	27	83	99	55	13
48	11	49	84	30	57	07	30	82	1702	54	12
49	13	49	87	29	60	07	33	82	05	54	11
50	.1016	.9948	.1190	.9929	.1363	.9907	.1536	.9881	.1708	.9853	10
51	19	48	93	29	66	06	38	81	11	53	9
52	22	48	96	28	69	06	41	80	14	52	8
53	25	47	98	28	72	05	44	80	16	52	7
54	28	47	1201	28	74	05	47	80	19	51	6
55	.1031	.9947	.1204	.9927	.1377	.9905	.1550	.9879	.1722	.9851	5
56	34	46	07	27	80	04	53	79	25	50	4
57	37	46	10	27	83	04	56	78	28	50	3
58	39	46	13	26	86	03	59	78	31	49	2
59	42	46	16	26	89	03	61	77	34	49	1
60	.1045	.9945	.1219	.9925	.1392	.9903	.1564	.9877	.1736	.9848	0
/	cos	sin	cos	sin	cos	sin	cos	sin	cos	sin	/
/	84°		83°		82°		81°		80°		/

NATURAL TANGENTS AND COTANGENTS

/	5°		6°		7°		8°		9°		/
	tan	cot	tan	cot	tan	cot	tan	cot	tan	cot	
0	.0875	11.4301	.1051	9.5144	.1228	8.1443	.1405	7.1154	.1584	6.3138	60
1	78	3919	54	4878	31	1248	08	1004	87	3019	59
2	81	3540	57	4614	34	1054	11	0855	90	2901	58
3	84	3163	60	4352	37	0860	14	0706	93	2783	57
4	87	2789	63	4090	40	0667	17	0558	96	2666	56
5	.0890	11.2417	.1066	9.3831	.1243	8.0476	.1420	7.0410	.1599	6.2549	55
6	92	2048	69	3572	46	0285	23	0264	1602	2432	54
7	95	1681	72	3315	49	0095	26	0117	05	2316	53
8	98	1316	75	3060	51	7.9906	29	6.9972	08	2200	52
9	0901	0954	78	2806	54	9718	32	9827	11	2085	51
10	.0904	11.0594	.1080	9.2553	.1257	7.9530	.1435	6.9682	.1614	6.1970	50
11	07	0237	83	2302	60	9344	38	9538	17	1856	49
12	10	10.9882	86	2052	63	9158	41	9395	20	1742	48
13	13	9529	89	1803	66	8973	44	9252	23	1628	47
14	16	9178	92	1555	69	8789	47	9110	26	1515	46
15	.0919	10.8829	.1095	9.1309	.1272	7.8606	.1450	6.8969	.1629	6.1402	45
16	22	8483	98	1065	75	8424	53	8828	32	1290	44
17	25	8139	1101	0821	78	8243	56	8687	35	1178	43
18	28	7797	04	0579	81	8062	59	8548	38	1066	42
19	31	7457	07	0338	84	7882	62	8408	41	0955	41
20	.0934	10.7119	.1110	9.0098	.1287	7.7704	.1465	6.8269	.1644	6.0844	40
21	36	6783	13	8.9860	90	7525	68	8131	47	0734	39
22	39	6450	16	9623	93	7348	71	7994	50	0624	38
23	42	6118	19	9387	96	7171	74	7856	53	0514	37
24	45	5789	22	9152	99	6996	77	7720	55	0405	36
25	.0948	10.5462	.1125	8.8919	.1302	7.6821	.1480	6.7584	.1658	6.0296	35
26	51	5136	28	8686	05	6647	83	7448	61	0188	34
27	54	4813	31	8455	08	6473	86	7313	64	0080	33
28	57	4491	33	8225	11	6301	89	7179	67	5.9972	32
29	60	4172	36	7996	14	6129	92	7045	70	9.9865	31
30	.0963	10.3854	.1139	8.7769	.1317	7.5958	.1495	6.6912	.1673	5.9758	30
31	66	3538	42	7542	19	5787	97	6779	76	9651	29
32	69	3224	45	7317	22	5618	1500	6646	79	9545	28
33	72	2913	48	7093	25	5449	03	6514	82	9439	27
34	75	2602	51	6870	28	5281	06	6383	85	9333	26
35	.0978	10.2294	.1154	8.6648	.1331	7.5113	.1509	6.6252	.1688	5.9228	25
36	81	1988	57	6427	34	4947	12	6122	91	9124	24
37	83	1683	60	6208	37	4781	15	5992	94	9019	23
38	86	1381	63	5989	40	4615	18	5863	97	8915	22
39	89	1080	66	5772	43	4451	21	5734	1700	8811	21
40	.0992	10.0780	.1169	8.5555	.1346	7.4287	.1524	6.5606	.1703	5.8708	20
41	95	0483	72	5340	49	4124	27	5478	06	8605	19
42	98	0187	75	5126	52	3962	30	5350	09	8502	18
43	1001	9.9893	78	4913	55	3800	33	5223	12	8400	17
44	04	9601	81	4701	58	3639	36	5097	15	8298	16
45	.1007	9.9310	.1184	8.4490	.1361	7.3479	.1539	6.4971	.1718	5.8197	15
46	10	9021	87	4280	64	3319	42	4846	21	8095	14
47	13	8734	89	4071	67	3160	45	4721	24	7994	13
48	16	8448	92	3863	70	3002	48	4596	27	7894	12
49	19	8164	95	3656	73	2844	51	4472	30	7794	11
50	.1022	9.7882	.1198	8.3450	.1376	7.2687	.1554	6.4348	.1733	5.7694	10
51	25	7601	1201	3245	79	2531	57	4225	36	7594	9
52	28	7322	04	3041	82	2375	60	4103	39	7495	8
53	30	7044	07	2838	85	2220	63	3980	42	7396	7
54	33	6768	10	2636	88	2066	66	3859	45	7297	6
55	.1036	9.6493	.1213	8.2434	.1391	7.1912	.1569	6.3737	.1748	5.7199	5
56	39	6220	16	2234	94	1759	72	3617	51	7101	4
57	42	5949	19	2035	97	1607	75	3496	54	7004	3
58	45	5679	22	1837	99	1455	78	3376	57	6906	2
59	48	5411	25	1640	1402	1304	81	3257	60	6809	1
60	.1051	9.5144	.1228	8.1443	.1405	7.1154	.1584	6.3138	.1763	5.6713	0
/	eot	tan	eot	tan	eot	tan	eot	tan	eot	tan	/
/	84°		83°		82°		81°		80°		/

NATURAL SINES AND COSINES

/	10°		11°		12°		13°		14°		/
	sin	cos	sin	cos	sin	cos	sin	cos	sin	cos	
0	.1736	.9848	.1908	.9816	.2079	.9781	.2250	.9744	.2419	.9703	60
1	39	48	11	16	82	81	52	43	22	02	59
2	42	47	14	15	85	80	55	42	25	02	58
3	45	47	17	15	88	80	58	42	28	01	57
4	48	46	20	14	90	79	61	41	31	00	56
5	.1751	.9846	.1922	.9813	.2093	.9778	.2264	.9740	.2433	.9699	55
6	54	45	25	13	96	78	67	40	36	99	54
7	57	45	28	12	99	77	69	39	39	98	53
8	59	44	31	12	2102	77	72	38	42	97	52
9	62	43	34	11	05	76	75	38	45	97	51
10	.1765	.9843	.1937	.9811	.2108	.9775	.2278	.9737	.2447	.9696	50
11	68	42	39	10	10	75	81	36	50	95	49
12	71	42	42	10	13	74	84	36	53	94	48
13	74	41	45	09	16	74	86	35	56	94	47
14	77	41	48	08	19	73	89	34	59	93	46
15	.1779	.9840	.1951	.9808	.2122	.9772	.2292	.9734	.2462	.9692	45
16	82	40	54	07	25	72	95	33	64	92	44
17	85	39	57	07	27	71	98	32	67	91	43
18	88	39	59	06	30	70	2300	32	70	90	42
19	91	38	62	06	33	70	03	31	73	89	41
20	.1794	.9838	.1965	.9805	.2136	.9769	.2306	.9730	.2476	.9689	40
21	97	37	68	04	39	69	09	30	78	88	39
22	99	37	71	04	42	68	12	29	81	87	38
23	1802	36	74	03	45	67	15	28	84	87	37
24	05	36	77	03	47	67	17	28	87	86	36
25	.1808	.9835	.1979	.9802	.2150	.9766	.2320	.9727	.2490	.9685	35
26	11	35	82	02	53	65	23	26	93	84	34
27	14	34	85	01	56	65	26	26	95	84	33
28	17	34	88	00	59	64	29	25	98	83	32
29	19	33	91	00	62	64	32	24	.2501	82	31
30	.1822	.9833	.1994	.9799	.2164	.9763	.2334	.9724	.2504	.9681	30
31	25	32	97	99	67	62	37	23	07	81	29
32	28	31	99	98	70	62	40	22	09	80	28
33	31	31	2002	98	73	61	43	22	12	79	27
34	34	30	05	97	76	60	46	21	15	79	26
35	.1837	.9830	.2008	.9796	.2179	.9760	.2349	.9720	.2518	.9678	25
36	40	29	11	96	81	59	51	20	21	77	24
37	42	29	14	95	84	59	54	19	24	76	23
38	45	28	16	95	87	58	57	18	26	76	22
39	48	28	19	94	90	57	60	18	29	75	21
40	.1851	.9827	.2022	.9793	.2193	.9757	.2363	.9717	.2532	.9674	20
41	54	27	25	93	96	56	66	16	35	73	19
42	57	26	28	92	98	55	68	15	38	73	18
43	60	26	31	92	2201	55	71	15	40	72	17
44	62	25	34	91	04	54	74	14	43	71	16
45	.1865	.9825	.2036	.9790	.2207	.9753	.2377	.9713	.2546	.9670	15
46	68	24	39	90	10	53	80	13	49	70	14
47	71	23	42	89	13	52	83	12	52	69	13
48	74	23	45	89	15	51	85	11	54	68	12
49	77	22	48	88	18	51	88	11	57	67	11
50	.1880	.9822	.2051	.9787	.2221	.9750	.2391	.9710	.2560	.9667	10
51	82	21	54	87	24	50	94	09	63	66	9
52	85	21	56	86	27	49	97	09	66	65	8
53	88	20	59	86	30	48	99	08	69	65	7
54	91	20	62	85	33	48	.2402	07	71	64	6
55	.1894	.9819	.2065	.9784	.2235	.9747	.2405	.9706	.2574	.9663	5
56	97	18	68	84	38	46	08	06	77	62	4
57	1900	18	71	83	41	46	11	05	80	62	3
58	02	17	73	83	44	45	14	04	83	61	2
59	05	17	76	82	47	44	16	04	85	60	1
60	.1908	.9816	.2079	.9781	.2250	.9744	.2419	.9703	.2588	.9659	0
	cos	sin	cos	sin	cos	sin	cos	sin	cos	sin	
/	79°		78°		77°		76°		75°		/



NATURAL TANGENTS AND COTANGENTS

/	10°		11°		12°		13°		14°		/
	tan	cot	tan	cot	tan	cot	tan	cot	tan	cot	
0	.1763	5.6713	.1944	5.1446	.2126	4.7046	.2309	4.3315	.2493	4.0108	60
1	66	6617	47	1366	29	6979	12	3257	96	0058	59
2	69	6521	50	1286	32	6912	15	3200	99	0009	58
3	72	6425	53	1207	35	6845	18	3143	2503	3.9959	57
4	75	6329	56	1128	38	6779	21	3086	06	9910	56
5	.1778	5.6234	.1959	5.1049	.2141	4.6712	.2324	4.3029	.2509	3.9861	55
6	81	6140	62	0970	44	6646	27	2972	12	9812	54
7	84	6045	65	0892	47	6580	30	2916	15	9763	53
8	87	5951	68	0814	50	6514	33	2859	18	9714	52
9	90	5857	71	0736	53	6448	36	2803	21	9665	51
10	.1793	5.5764	.1974	5.0658	.2156	4.6382	.2339	4.2747	.2524	3.9617	50
11	96	5671	77	0581	59	6317	42	2691	27	9568	49
12	99	5578	80	0504	62	6252	45	2635	30	9520	48
13	1802	5485	83	0427	65	6187	49	2580	33	9471	47
14	05	5393	86	0350	68	6122	52	2524	37	9423	46
15	.1808	5.5301	.1989	5.0273	.2171	4.6057	.2355	4.2468	.2540	3.9375	45
16	11	5209	92	0197	74	5993	58	2413	43	9327	44
17	14	5118	95	0121	77	5928	61	2358	46	9279	43
18	17	5026	98	0045	80	5864	64	2303	49	9232	42
19	20	4936	2001	4.9969	83	5800	67	2248	52	9184	41
20	.1823	5.4845	.2004	4.9894	.2186	4.5736	.2370	4.2193	.2555	3.9136	40
21	26	4755	07	9819	89	5673	73	2139	58	9089	39
22	29	4665	10	9744	93	5609	76	2084	61	9042	38
23	32	4575	13	9669	96	5546	79	2030	64	8995	37
24	35	4486	16	9594	99	5483	82	1976	68	8947	36
25	.1838	5.4397	.2019	4.9520	.2202	4.5420	.2385	4.1922	.2571	3.8900	35
26	41	4308	22	9446	05	5357	88	1868	74	8854	34
27	44	4219	25	9372	08	5294	92	1814	77	8807	33
28	47	4131	28	9298	11	5232	95	1760	80	8760	32
29	50	4043	31	9225	14	5169	98	1706	83	8714	31
30	.1853	5.3955	.2035	4.9152	.2217	4.5107	.2401	4.1653	.2586	3.8667	30
31	56	3868	38	9078	20	5045	04	1600	89	8621	29
32	59	3781	41	9006	23	4983	07	1547	92	8575	28
33	62	3694	44	8933	26	4922	10	1493	95	8528	27
34	65	3607	47	8860	29	4860	13	1441	99	8482	26
35	.1868	5.3521	.2050	4.8788	.2232	4.4799	.2416	4.1388	.2602	3.8436	25
36	71	3435	53	8716	35	4737	19	1335	05	8391	24
37	74	3349	56	8644	38	4676	22	1282	08	8345	23
38	77	3263	59	8573	41	4615	25	1230	11	8299	22
39	80	3178	62	8501	44	4555	28	1178	14	8254	21
40	.1883	5.3093	.2065	4.8430	.2247	4.4494	.2432	4.1126	.2617	3.8208	20
41	87	3008	68	8359	51	4434	35	1074	20	8163	19
42	90	2924	71	8288	54	4373	38	1022	23	8118	18
43	93	2839	74	8218	57	4313	41	0970	27	8073	17
44	96	2755	77	8147	60	4253	44	0918	30	8028	16
45	.1899	5.2672	.2080	4.8077	.2263	4.4194	.2447	4.0867	.2633	3.7983	15
46	1902	2588	83	8007	66	4134	50	0815	36	7938	14
47	05	2505	86	7937	69	4075	53	0764	39	7893	13
48	08	2422	89	7867	72	4015	56	0713	42	7848	12
49	11	2339	92	7798	75	3956	59	0662	45	7804	11
50	.1914	5.2257	.2095	4.7729	.2278	4.3897	.2462	4.0611	.2648	3.7760	10
51	17	2174	98	7659	81	3838	65	0560	51	7715	9
52	20	2092	2101	7591	84	3779	69	0509	55	7671	8
53	23	2011	04	7522	87	3721	72	0459	58	7627	7
54	26	1929	07	7453	90	3662	75	0408	61	7583	6
55	.1929	5.1848	.2110	4.7385	.2293	4.3604	.2478	4.0358	.2664	3.7539	5
56	32	1767	13	7317	96	3546	81	0308	67	7495	4
57	35	1686	16	7249	99	3488	84	0257	70	7451	3
58	38	1606	19	7181	2303	3430	87	0207	73	7408	2
59	41	1526	23	7114	06	3372	90	0158	76	7364	1
60	.1944	5.1446	.2126	4.7046	.2309	4.3315	.2493	4.0108	.2679	3.7321	0
/	79°	tan	78°	cot	77°	cot	76°	tan	75°	cot	/

NATURAL SINES AND COSINES

/	15°		16°		17°		18°		19°		/
	sin	cos	sin	cos	sin	cos	sin	cos	sin	cos	
<b>0</b>	.2588	.9659	.2756	.9613	.2924	.9563	.3090	.9511	.3256	.9455	<b>60</b>
1	91	59	59	12	26	62	93	10	58	54	59
2	94	58	62	11	29	61	96	09	61	53	58
3	97	57	65	10	32	60	98	08	64	52	57
4	99	56	68	09	35	60	3101	07	67	51	56
<b>5</b>	.2602	.9655	.2770	.9609	.2938	.9559	.3104	.9506	.3269	.9450	<b>55</b>
6	05	55	73	08	40	58	07	05	72	49	54
7	08	54	76	07	43	57	10	04	75	49	53
8	11	53	79	06	46	56	12	03	78	48	52
9	13	52	82	05	49	55	15	02	80	47	51
<b>10</b>	.2616	.9652	.2784	.9605	.2952	.9555	.3118	.9502	.3283	.9446	<b>50</b>
11	19	51	87	04	54	54	21	01	86	45	49
12	22	50	90	03	57	53	23	00	89	44	48
13	25	49	93	02	60	52	26	9499	91	43	47
14	28	49	95	01	63	51	29	98	94	42	46
<b>15</b>	.2630	.9648	.2798	.9600	.2965	.9550	.3132	.9497	.3297	.9441	<b>45</b>
16	33	47	2801	00	68	49	34	96	3300	40	44
17	36	46	04	9599	71	48	37	95	02	39	43
18	39	46	07	98	74	48	40	94	05	38	42
19	42	45	09	97	77	47	43	93	08	37	41
<b>20</b>	.2644	.9644	.2812	.9596	.2979	.9546	.3145	.9492	.3311	.9436	<b>40</b>
21	47	43	15	96	82	45	48	92	13	35	39
22	50	42	18	95	85	44	51	91	16	34	38
23	53	42	21	94	88	43	54	90	19	33	37
24	56	41	23	93	90	42	56	89	22	32	36
<b>25</b>	.2658	.9640	.2826	.9592	.2993	.9542	.3159	.9488	.3324	.9431	<b>35</b>
26	61	39	29	91	96	41	62	87	27	30	34
27	64	39	32	91	99	40	65	86	30	29	33
28	67	38	35	90	3002	39	68	85	33	28	32
29	70	37	37	89	04	38	70	84	35	27	31
<b>30</b>	.2672	.9636	.2840	.9588	.3007	.9537	.3173	.9483	.3338	.9426	<b>30</b>
31	75	36	43	87	10	36	76	82	41	25	29
32	78	35	46	87	13	35	79	81	44	24	28
33	81	34	49	86	15	35	81	80	46	23	27
34	84	33	51	85	18	34	84	80	49	23	26
<b>35</b>	.2686	.9632	.2854	.9584	.3021	.9533	.3187	.9479	.3352	.9422	<b>25</b>
36	89	32	57	83	24	32	90	78	55	21	24
37	92	31	60	82	26	31	92	77	57	20	23
38	95	30	62	82	29	30	95	76	60	19	22
39	98	29	65	81	32	29	98	75	63	18	21
<b>40</b>	.2700	.9628	.2868	.9580	.3035	.9528	.3201	.9474	.3365	.9417	<b>20</b>
41	03	28	71	79	38	27	03	73	68	16	19
42	06	27	74	78	40	27	06	72	71	15	18
43	09	26	76	77	43	26	09	71	74	14	17
44	12	25	79	77	46	25	12	70	76	13	16
<b>45</b>	.2714	.9625	.2882	.9576	.3049	.9524	.3214	.9469	.3379	.9412	<b>15</b>
46	17	24	85	75	51	23	17	68	82	11	14
47	20	23	88	74	54	22	20	67	85	10	13
48	23	22	90	73	57	21	23	66	87	09	12
49	26	21	93	72	60	20	25	66	90	08	11
<b>50</b>	.2728	.9621	.2896	.9572	.3062	.9520	.3228	.9465	.3393	.9407	<b>10</b>
51	31	20	99	71	65	19	31	64	96	06	9
52	34	19	2901	70	68	18	34	63	98	05	8
53	37	18	04	69	71	17	36	62	3401	04	7
54	40	17	07	68	74	16	39	61	04	03	6
<b>55</b>	.2742	.9617	.2910	.9567	.3076	.9515	.3242	.9460	.3407	.9402	<b>5</b>
56	45	16	13	66	79	14	45	59	09	01	4
57	48	15	15	66	82	13	47	58	12	00	3
58	51	14	18	65	85	12	50	57	15	9399	2
59	54	13	21	64	87	11	53	56	17	98	1
<b>60</b>	.2756	.9613	.2924	.9563	.3090	.9511	.3256	.9455	.3420	.9397	<b>0</b>
	cos	sin	cos	sin	cos	sin	cos	sin	cos	sin	
/	74°		73°		72°		71°		70°		/

NATURAL TANGENTS AND COTANGENTS

/	15°		16°		17°		18°		19°		/
	tan	cot	tan	cot	tan	cot	tan	cot	tan	cot	
0	.2679	3.7321	.2867	3.4874	.3057	3.2709	.3249	3.0777	.3443	2.9042	60
1	83	7277	71	4836	60	2675	52	0746	47	9015	59
2	86	7234	74	4798	64	2641	56	0716	50	8987	58
3	89	7191	77	4760	67	2607	59	0686	53	8960	57
4	92	7148	80	4722	70	2573	62	0655	56	8933	56
5	.2695	3.7105	.2883	3.4684	.3073	3.2539	.3265	3.0625	.3460	2.8905	55
6	98	7062	86	4646	76	2506	69	0595	63	8878	54
7	2701	7019	90	4608	80	2472	72	0565	66	8851	53
8	04	6976	93	4570	83	2438	75	0535	69	8824	52
9	08	6933	96	4533	86	2405	78	0505	73	8797	51
10	.2711	3.6891	.2899	3.4495	.3089	3.2371	.3281	3.0475	.3476	2.8770	50
11	14	6848	2902	4458	92	2338	85	0445	79	8743	49
12	17	6806	05	4420	96	2305	88	0415	82	8716	48
13	20	6764	08	4383	99	2272	91	0385	86	8689	47
14	23	6722	12	4346	3102	2238	94	0356	89	8662	46
15	.2726	3.6680	.2915	3.4308	.3105	3.2205	.3298	3.0326	.3492	2.8636	45
16	29	6638	18	4271	08	2172	3301	0296	95	8609	44
17	33	6596	21	4234	11	2139	04	0267	99	8582	43
18	36	6554	24	4197	15	2106	07	0237	3502	8556	42
19	39	6512	27	4160	18	2073	10	0208	05	8529	41
20	.2742	3.6470	.2931	3.4124	.3121	3.2041	.3314	3.0178	.3508	2.8502	40
21	45	6429	34	4087	24	2008	17	0149	12	8476	39
22	48	6387	37	4050	27	1975	20	0120	15	8449	38
23	51	6346	40	4014	31	1943	23	0090	18	8423	37
24	54	6305	43	3977	34	1910	27	0061	22	8397	36
25	.2758	3.6264	.2946	3.3941	.3137	3.1878	.3330	3.0032	.3525	2.8370	35
26	61	6222	49	3904	40	1845	33	0003	28	8344	34
27	64	6181	53	3868	43	1813	36	2.9974	31	8318	33
28	67	6140	56	3832	47	1780	39	9945	35	8291	32
29	70	6100	59	3796	50	1748	43	9916	38	8265	31
30	.2773	3.6059	.2962	3.3759	.3153	3.1716	.3346	2.9887	.3541	2.8239	30
31	76	6018	65	3723	56	1684	49	9858	44	8213	29
32	80	5978	68	3687	59	1652	52	9829	48	8187	28
33	83	5937	72	3652	63	1620	56	9800	51	8161	27
34	86	5897	75	3616	66	1588	59	9772	54	8135	26
35	.2789	3.5856	.2978	3.3580	.3169	3.1556	.3362	2.9743	.3558	2.8109	25
36	92	5816	81	3544	72	1524	65	9714	61	8083	24
37	95	5776	84	3509	75	1492	69	9686	64	8057	23
38	98	5736	87	3473	79	1460	72	9657	67	8032	22
39	2801	5696	91	3438	82	1429	75	9629	71	8006	21
40	.2805	3.5656	.2994	3.3402	.3185	3.1397	.3378	2.9600	.3574	2.7980	20
41	08	5616	97	3367	88	1366	82	9572	77	7955	19
42	11	5576	3000	3332	91	1334	85	9544	81	7929	18
43	14	5536	03	3297	95	1303	88	9515	84	7903	17
44	17	5497	06	3261	98	1271	91	9487	87	7878	16
45	.2820	3.5457	.3010	3.3226	.3201	3.1240	.3395	2.9459	.3590	2.7852	15
46	23	5418	13	3191	04	1209	98	9431	94	7827	14
47	27	5379	16	3156	07	1178	3401	9403	97	7801	13
48	30	5339	19	3122	11	1146	04	9375	3600	7776	12
49	33	5300	22	3087	14	1115	08	9347	04	7751	11
50	.2836	3.5261	.3026	3.3052	.3217	3.1084	.3411	2.9319	.3607	2.7725	10
51	39	5222	29	3017	20	1053	14	9291	10	7700	9
52	42	5183	32	2983	23	1022	17	9263	13	7675	8
53	45	5144	35	2948	27	0991	21	9235	17	7650	7
54	49	5105	38	2914	30	0961	24	9208	20	7625	6
55	.2852	3.5067	.3041	3.2879	.3233	3.0930	.3427	2.9180	.3623	2.7600	5
56	55	5028	45	2845	36	0899	30	9152	27	7575	4
57	58	4989	48	2811	40	0868	34	9125	30	7550	3
58	61	4951	51	2777	43	0838	37	9097	33	7525	2
59	64	4912	54	2743	46	0807	40	9070	36	7500	1
60	.2867	3.4874	.3057	3.2709	.3249	3.0777	.3443	2.9042	.3640	2.7475	0
	cot	tan	cot	tan	cot	tan	cot	tan	cot	tan	
/	74°		73°		72°		71°		70°		/

NATURAL SINES AND COSINES

/	20°		21°		22°		23°		24°		/
	sin	cos	sin	cos	sin	cos	sin	cos	sin	cos	
0	.3420	.9397	.3584	.9336	.3746	.9272	.3907	.9205	.4067	.9135	<b>60</b>
1	23	96	86	35	49	71	10	04	70	34	59
2	26	95	89	34	51	70	13	03	73	33	58
3	28	94	92	33	54	69	15	02	75	32	57
4	31	93	95	32	57	67	18	00	78	31	56
<b>5</b>	<b>.3434</b>	<b>.9392</b>	<b>.3597</b>	<b>.9331</b>	<b>.3760</b>	<b>.9266</b>	<b>.3921</b>	<b>.9199</b>	<b>.4081</b>	<b>.9130</b>	<b>55</b>
6	37	91	3600	30	62	65	23	98	83	28	54
7	39	90	03	28	65	64	26	97	86	27	53
8	42	89	05	27	68	63	29	96	89	26	52
9	45	88	08	26	70	62	31	95	91	25	51
<b>10</b>	<b>.3448</b>	<b>.9387</b>	<b>.3611</b>	<b>.9325</b>	<b>.3773</b>	<b>.9261</b>	<b>.3934</b>	<b>.9194</b>	<b>.4094</b>	<b>.9124</b>	<b>50</b>
11	50	86	14	24	76	60	37	92	97	22	49
12	53	85	16	23	78	59	39	91	99	21	48
13	56	84	19	22	81	58	42	90	4102	20	47
14	58	83	22	21	84	57	45	89	05	19	46
<b>15</b>	<b>.3461</b>	<b>.9382</b>	<b>.3624</b>	<b>.9320</b>	<b>.3786</b>	<b>.9255</b>	<b>.3947</b>	<b>.9188</b>	<b>.4107</b>	<b>.9118</b>	<b>45</b>
16	64	81	27	19	89	54	50	87	10	16	44
17	67	80	30	18	92	53	53	86	12	15	43
18	69	79	33	17	95	52	55	84	15	14	42
19	72	78	35	16	97	51	58	83	18	13	41
<b>20</b>	<b>.3475</b>	<b>.9377</b>	<b>.3638</b>	<b>.9315</b>	<b>.3800</b>	<b>.9250</b>	<b>.3961</b>	<b>.9182</b>	<b>.4120</b>	<b>.9112</b>	<b>40</b>
21	78	76	41	14	03	49	63	81	23	10	39
22	80	75	43	13	05	48	66	80	26	09	38
23	83	74	46	12	08	47	69	79	28	08	37
24	86	73	49	11	11	45	71	78	31	07	36
<b>25</b>	<b>.3488</b>	<b>.9372</b>	<b>.3651</b>	<b>.9309</b>	<b>.3813</b>	<b>.9244</b>	<b>.3974</b>	<b>.9176</b>	<b>.4134</b>	<b>.9106</b>	<b>35</b>
26	91	71	54	08	16	43	77	75	36	04	34
27	94	70	57	07	19	42	79	74	39	03	33
28	97	69	60	06	21	41	82	73	42	02	32
29	99	68	62	05	24	40	85	72	44	01	31
<b>30</b>	<b>.3502</b>	<b>.9367</b>	<b>.3665</b>	<b>.9304</b>	<b>.3827</b>	<b>.9239</b>	<b>.3987</b>	<b>.9171</b>	<b>.4147</b>	<b>.9100</b>	<b>30</b>
31	05	66	68	03	30	38	90	69	50	9098	29
32	08	65	70	02	32	37	93	68	52	97	28
33	10	64	73	01	35	35	95	67	55	96	27
34	13	63	76	00	38	34	98	66	58	95	26
<b>35</b>	<b>.3516</b>	<b>.9362</b>	<b>.3679</b>	<b>.9299</b>	<b>.3840</b>	<b>.9233</b>	<b>.4001</b>	<b>.9165</b>	<b>.4160</b>	<b>.9094</b>	<b>25</b>
36	18	61	81	98	43	32	03	64	63	92	24
37	21	60	84	97	46	31	06	62	65	91	23
38	24	59	87	96	48	30	09	61	68	90	22
39	27	58	89	95	51	29	11	60	71	89	21
<b>40</b>	<b>.3529</b>	<b>.9356</b>	<b>.3692</b>	<b>.9293</b>	<b>.3854</b>	<b>.9228</b>	<b>.4014</b>	<b>.9159</b>	<b>.4173</b>	<b>.9088</b>	<b>20</b>
41	32	55	95	92	56	27	17	58	76	86	19
42	35	54	97	91	59	25	19	57	79	85	18
43	37	53	3700	90	62	24	22	55	81	84	17
44	40	52	03	89	64	23	25	54	84	83	16
<b>45</b>	<b>.3543</b>	<b>.9351</b>	<b>.3706</b>	<b>.9288</b>	<b>.3867</b>	<b>.9222</b>	<b>.4027</b>	<b>.9153</b>	<b>.4187</b>	<b>.9081</b>	<b>15</b>
46	46	50	08	87	70	21	30	52	89	80	14
47	48	49	11	86	72	20	33	51	92	79	13
48	51	48	14	85	75	19	35	50	95	78	12
49	54	47	16	84	78	18	38	48	97	77	11
<b>50</b>	<b>.3557</b>	<b>.9346</b>	<b>.3719</b>	<b>.9283</b>	<b>.3881</b>	<b>.9216</b>	<b>.4041</b>	<b>.9147</b>	<b>.4200</b>	<b>.9075</b>	<b>10</b>
51	59	45	22	82	83	15	43	46	02	74	9
52	62	44	24	81	86	14	46	45	05	73	8
53	65	43	27	79	89	13	49	44	08	72	7
54	67	42	30	78	91	12	51	43	10	70	6
<b>55</b>	<b>.3570</b>	<b>.9341</b>	<b>.3733</b>	<b>.9277</b>	<b>.3894</b>	<b>.9211</b>	<b>.4054</b>	<b>.9141</b>	<b>.4213</b>	<b>.9069</b>	<b>5</b>
56	73	40	35	76	97	10	57	40	16	68	4
57	76	39	38	75	99	08	59	39	18	67	3
58	78	38	41	74	3902	07	62	38	21	66	2
59	81	37	43	73	05	06	65	37	24	64	1
<b>60</b>	<b>.3584</b>	<b>.9336</b>	<b>.3746</b>	<b>.9272</b>	<b>.3907</b>	<b>.9205</b>	<b>.4067</b>	<b>.9135</b>	<b>.4226</b>	<b>.9063</b>	<b>0</b>
	<b>cos</b>	<b>sin</b>	<b>cos</b>	<b>sin</b>	<b>cos</b>	<b>sin</b>	<b>cos</b>	<b>sin</b>	<b>cos</b>	<b>sin</b>	
/	69°		68°		67°		66°		65°		/

NATURAL TANGENTS AND COTANGENTS

/	20°		21°		22°		23°		24°		/
	tan	cot	tan	cot	tan	cot	tan	cot	tan	cot	
0	.3640	2.7475	.3839	2.6051	.4040	2.4751	.4245	2.3559	.4452	2.2460	60
1	43	7450	42	6028	44	4730	48	3539	56	2443	59
2	46	7425	45	6006	47	4709	52	3520	59	2425	58
3	50	7400	49	5983	50	4689	55	3501	63	2408	57
4	53	7376	52	5961	54	4668	58	3483	66	2390	56
5	.3656	2.7351	.3855	2.5938	.4057	2.4648	.4262	2.3464	.4470	2.2373	55
6	59	7326	59	5916	61	4627	65	3445	73	2355	54
7	63	7302	62	5893	64	4606	69	3426	77	2338	53
8	66	7277	65	5871	67	4586	72	3407	80	2320	52
9	69	7253	69	5848	71	4566	76	3388	84	2303	51
10	.3673	2.7228	.3872	2.5826	.4074	2.4545	.4279	2.3369	.4487	2.2286	50
11	76	7204	75	5804	78	4525	83	3351	91	2268	49
12	79	7179	79	5782	81	4504	86	3332	94	2251	48
13	83	7155	82	5759	84	4484	89	3313	98	2234	47
14	86	7130	85	5737	88	4464	93	3294	4501	2216	46
15	.3689	2.7106	.3889	2.5715	.4091	2.4443	.4296	2.3276	.4505	2.2199	45
16	93	7082	92	5693	95	4423	4300	3257	08	2182	44
17	96	7058	95	5671	98	4403	03	3238	12	2165	43
18	99	7034	99	5649	4101	4383	07	3220	15	2148	42
19	3702	7009	3902	5627	05	4362	10	3201	19	2130	41
20	.3706	2.6985	.3906	2.5605	.4108	2.4342	.4314	2.3183	.4522	2.2113	40
21	09	6961	09	5583	11	4322	17	3164	26	2096	39
22	12	6937	12	5561	15	4302	20	3146	29	2079	38
23	16	6913	16	5539	18	4282	24	3127	33	2062	37
24	19	6889	19	5517	22	4262	27	3109	36	2045	36
25	.3722	2.6865	.3922	2.5495	.4125	2.4242	.4331	2.3090	.4540	2.2028	35
26	26	6841	26	5473	29	4222	34	3072	43	2011	34
27	29	6818	29	5452	32	4202	38	3053	47	1994	33
28	32	6794	32	5430	35	4182	41	3035	50	1977	32
29	36	6770	36	5408	39	4162	45	3017	54	1960	31
30	.3739	2.6746	.3939	2.5386	.4142	2.4142	.4348	2.2998	.4557	2.1943	30
31	42	6723	42	5365	46	4122	52	2980	61	1926	29
32	45	6699	46	5343	49	4102	55	2962	64	1909	28
33	49	6675	49	5322	52	4083	59	2944	68	1892	27
34	52	6652	53	5300	56	4063	62	2925	71	1876	26
35	.3755	2.6628	.3956	2.5279	.4159	2.4043	.4365	2.2907	.4575	2.1859	25
36	59	6605	59	5257	63	4023	69	2889	78	1842	24
37	62	6581	63	5236	66	4004	72	2871	82	1825	23
38	65	6558	66	5214	69	3984	76	2853	85	1808	22
39	69	6534	69	5193	73	3964	79	2835	89	1792	21
40	.3772	2.6511	.3973	2.5172	.4176	2.3945	.4383	2.2817	.4592	2.1775	20
41	75	6488	76	5150	80	3925	86	2799	96	1758	19
42	79	6464	79	5129	83	3906	90	2781	99	1742	18
43	82	6441	83	5108	87	3886	93	2763	4603	1725	17
44	85	6418	86	5086	90	3867	97	2745	07	1708	16
45	.3789	2.6395	.3990	2.5065	.4193	2.3847	.4400	2.2727	.4610	2.1692	15
46	92	6371	93	5044	97	3828	04	2709	14	1675	14
47	95	6348	96	5023	4200	3808	07	2691	17	1659	13
48	99	6325	4000	5002	04	3789	11	2673	21	1642	12
49	3802	6302	03	4981	07	3770	14	2655	24	1625	11
50	.3805	2.6279	.4006	2.4960	.4210	2.3750	.4417	2.2637	.4628	2.1609	10
51	09	6256	10	4939	14	3731	21	2620	31	1592	9
52	12	6233	13	4918	17	3712	24	2602	35	1576	8
53	15	6210	17	4897	21	3693	28	2584	38	1560	7
54	19	6187	20	4876	24	3673	31	2566	42	1543	6
55	.3822	2.6165	.4023	2.4855	.4228	2.3654	.4435	2.2549	.4645	2.1527	5
56	25	6142	27	4834	31	3635	38	2531	49	1510	4
57	29	6119	30	4813	34	3616	42	2513	52	1494	3
58	32	6096	33	4792	38	3597	45	2496	56	1478	2
59	35	6074	37	4772	41	3578	49	2478	60	1461	1
60	.3839	2.6051	.4040	2.4751	.4245	2.3559	.4452	2.2460	.4663	2.1445	0
	cot	tan	cot	tan	cot	tan	cot	tan	cot	tan	
/	69°		68°		67°		66°		65°		/

NATURAL SINES AND COSINES

/	25°		26°		27°		28°		29°		/
	sin	cos	sin	cos	sin	cos	sin	cos	sin	cos	
0	.4226	.9063	.4384	.8988	.4540	.8910	.4695	.8829	.4848	.8746	60
1	29	62	86	87	42	09	97	28	51	45	59
2	31	61	89	85	45	07	4700	27	53	43	58
3	34	59	92	84	48	06	02	25	56	42	57
4	37	58	94	83	50	05	05	24	58	41	56
5	.4239	.9057	.4397	.8982	.4553	.8903	.4708	.8823	.4861	.8739	55
6	42	56	99	80	55	02	10	21	63	38	54
7	45	54	4402	79	58	01	13	20	66	36	53
8	47	53	05	78	61	8899	15	19	68	35	52
9	50	52	07	76	63	98	18	17	71	33	51
10	.4253	.9051	.4410	.8975	.4566	.8897	.4720	.8816	.4874	.8732	50
11	55	50	12	74	68	95	23	14	76	31	49
12	58	48	15	73	71	94	26	13	79	29	48
13	60	47	18	71	74	93	28	12	81	28	47
14	63	46	20	70	76	92	31	10	84	26	46
15	.4266	.9045	.4423	.8969	.4579	.8890	.4733	.8809	.4886	.8725	45
16	68	43	25	67	81	89	36	08	89	24	44
17	71	42	28	66	84	88	38	06	91	22	43
18	74	41	31	65	86	86	41	05	94	21	42
19	76	40	33	64	89	85	43	03	96	19	41
20	.4279	.9038	.4436	.8962	.4592	.8884	.4746	.8802	.4899	.8718	40
21	81	37	39	61	94	82	49	01	4901	16	39
22	84	36	41	60	97	81	51	8799	04	15	38
23	87	35	44	58	99	79	54	98	07	14	37
24	89	33	46	57	4602	78	56	96	09	12	36
25	.4292	.9032	.4449	.8956	.4605	.8877	.4759	.8795	.4912	.8711	35
26	95	31	52	55	07	75	61	94	14	09	34
27	97	30	54	53	10	74	64	92	17	08	33
28	4300	28	57	52	12	73	66	91	19	06	32
29	02	27	59	51	15	71	69	90	22	05	31
30	.4305	.9026	.4462	.8949	.4617	.8870	.4772	.8788	.4924	.8704	30
31	08	25	65	48	20	69	74	87	27	02	29
32	10	23	67	47	23	67	77	85	29	01	28
33	13	22	70	45	25	66	79	84	32	8699	27
34	16	21	72	44	28	65	82	83	34	98	26
35	.4318	.9020	.4475	.8943	.4630	.8863	.4784	.8781	.4937	.8696	25
36	21	18	78	42	33	62	87	80	39	95	24
37	23	17	80	40	36	61	89	78	42	94	23
38	26	16	83	39	38	59	92	77	44	92	22
39	29	15	85	38	41	58	95	76	47	91	21
40	.4331	.9013	.4488	.8936	.4643	.8857	.4797	.8774	.4950	.8689	20
41	34	12	91	35	46	55	4800	73	52	88	19
42	37	11	93	34	48	54	02	71	55	86	18
43	39	10	96	32	51	53	05	70	57	85	17
44	42	08	98	31	54	51	07	69	60	83	16
45	.4344	.9007	.4501	.8930	.4656	.8850	.4810	.8767	.4962	.8682	15
46	47	06	04	28	59	49	12	66	65	81	14
47	50	04	06	27	61	47	15	64	67	79	13
48	52	03	09	26	64	46	18	63	70	78	12
49	55	02	11	25	66	44	20	62	72	76	11
50	.4358	.9001	.4514	.8923	.4669	.8843	.4823	.8760	.4975	.8675	10
51	60	8999	17	22	72	42	25	59	77	73	9
52	63	98	19	21	74	40	28	57	80	72	8
53	65	97	22	19	77	39	30	56	82	70	7
54	68	96	24	18	79	38	33	55	85	69	6
55	.4371	.8994	.4527	.8917	.4682	.8836	.4835	.8753	.4987	.8668	5
56	73	93	30	15	84	35	38	52	90	66	4
57	76	92	32	14	87	34	40	50	92	65	3
58	78	90	35	13	90	32	43	49	95	63	2
59	81	89	37	11	92	31	46	48	97	62	1
60	.4384	.8988	.4540	.8910	.4695	.8829	.4848	.8746	.5000	.8660	0
/	cos	sin	cos	sin	cos	sin	cos	sin	cos	sin	/
	64°		63°		62°		61°		60°		

NATURAL TANGENTS AND COTANGENTS

/	25°		26°		27°		28°		29°		/
	tan	cot	tan	cot	tan	cot	tan	cot	tan	cot	
0	.4663	2.1445	.4877	2.0503	.5095	1.9626	.5317	1.8807	.5543	1.8040	60
1	67	1429	81	0488	99	9612	21	8794	47	8028	59
2	70	1413	85	0473	5103	9598	25	8781	51	8016	58
3	74	1396	88	0458	06	9584	28	8768	55	8003	57
4	77	1380	92	0443	10	9570	32	8755	58	7991	56
5	.4681	2.1364	.4895	2.0428	.5114	1.9556	.5336	1.8741	.5562	1.7979	55
6	84	1348	99	0413	17	9542	40	8728	66	7966	54
7	88	1332	4903	0398	21	9528	43	8715	70	7954	53
8	91	1315	06	0383	25	9514	47	8702	74	7942	52
9	95	1299	10	0368	28	9500	51	8689	77	7930	51
10	.4699	2.1283	.4913	2.0353	.5132	1.9486	.5354	1.8676	.5581	1.7917	50
11	4702	1267	17	0338	36	9472	58	8663	85	7905	49
12	06	1251	21	0323	39	9458	62	8650	89	7893	48
13	09	1235	24	0308	43	9444	66	8637	93	7881	47
14	13	1219	28	0293	47	9430	69	8624	96	7868	46
15	.4716	2.1203	.4931	2.0278	.5150	1.9416	.5373	1.8611	.5600	1.7856	45
16	20	1187	35	0263	54	9402	77	8598	04	7844	44
17	23	1171	39	0248	58	9388	81	8585	08	7832	43
18	27	1155	42	0233	61	9375	84	8572	12	7820	42
19	31	1139	46	0219	65	9361	88	8559	16	7808	41
20	.4734	2.1123	.4950	2.0204	.5169	1.9347	.5392	1.8546	.5619	1.7796	40
21	38	1107	53	0189	72	9333	96	8533	23	7783	39
22	41	1092	57	0174	76	9319	99	8520	27	7771	38
23	45	1076	60	0160	80	9306	5403	8507	31	7759	37
24	48	1060	64	0145	84	9292	07	8495	35	7747	36
25	.4752	2.1044	.4968	2.0130	.5187	1.9278	.5411	1.8482	.5639	1.7735	35
26	55	1028	71	0115	91	9265	15	8469	42	7723	34
27	59	1013	75	0101	95	9251	18	8456	46	7711	33
28	63	0997	79	0086	98	9237	22	8443	50	7699	32
29	66	0981	82	0072	5202	9223	26	8430	54	7687	31
30	.4770	2.0965	.4986	2.0057	.5206	1.9210	.5430	1.8418	.5658	1.7675	30
31	73	0950	89	0042	09	9196	33	8405	62	7663	29
32	77	0934	93	0028	13	9183	37	8392	65	7651	28
33	80	0918	97	0013	17	9169	41	8379	69	7639	27
34	84	0903	5000	1.9999	20	9155	45	8367	73	7627	26
35	.4788	2.0887	.5004	1.9984	.5224	1.9142	.5448	1.8354	.5677	1.7615	25
36	91	0872	08	9970	28	9128	52	8341	81	7603	24
37	95	0856	11	9955	32	9115	56	8329	85	7591	23
38	98	0840	15	9941	35	9101	60	8316	88	7579	22
39	4802	0825	19	9926	39	9088	64	8303	92	7567	21
40	.4806	2.0809	.5022	1.9912	.5243	1.9074	.5467	1.8291	.5696	1.7556	20
41	09	0794	26	9897	46	9061	71	8278	5700	7544	19
42	13	0778	29	9883	50	9047	75	8265	04	7532	18
43	16	0763	33	9868	54	9034	79	8253	08	7520	17
44	20	0748	37	9854	58	9020	82	8240	12	7508	16
45	.4823	2.0732	.5040	1.9840	.5261	1.9007	.5486	1.8228	.5715	1.7496	15
46	27	0717	44	9825	65	8993	90	8215	19	7485	14
47	31	0701	48	9811	69	8980	94	8202	23	7473	13
48	34	0686	51	9797	72	8967	98	8190	27	7461	12
49	38	0671	55	9782	76	8953	5501	8177	31	7449	11
50	.4841	2.0655	.5059	1.9768	.5280	1.8940	.5505	1.8165	.5735	1.7437	10
51	45	0640	62	9754	84	8927	09	8152	39	7426	9
52	49	0625	66	9740	87	8913	13	8140	43	7414	8
53	52	0609	70	9725	91	8900	17	8127	46	7402	7
54	56	0594	73	9711	95	8887	20	8115	50	7391	6
55	.4859	2.0579	.5077	1.9697	.5298	1.8873	.5524	1.8103	.5754	1.7379	5
56	63	0564	81	9683	5302	8860	28	8090	58	7367	4
57	67	0549	84	9669	06	8847	32	8078	62	7355	3
58	70	0533	88	9654	10	8834	35	8065	66	7344	2
59	74	0518	92	9640	13	8820	39	8053	70	7332	1
60	.4877	2.0503	.5095	1.9626	.5317	1.8807	.5543	1.8040	.5774	1.7321	0
	cot	tan	cot	tan	cot	tan	cot	tan	cot	tan	
/	64°		63°		62°		61°		60°		/

NATURAL SINES AND COSINES

/	30°		31°		32°		33°		34°		/
	sin	cos	sin	cos	sin	cos	sin	cos	sin	cos	
0	.5000	.8660	.5150	.8572	.5299	.8480	.5446	.8387	.5592	.8290	60
1	03	59	53	70	5302	79	49	85	94	89	59
2	05	57	55	69	04	77	51	84	97	87	58
3	08	56	58	67	07	76	54	82	99	85	57
4	10	54	60	66	09	74	56	80	5602	84	56
5	.5013	.8653	.5163	.8564	.5312	.8473	.5459	.8379	.5604	.8282	55
6	15	52	65	63	14	71	61	77	06	81	54
7	18	50	68	61	16	70	63	76	09	79	53
8	20	49	70	60	19	68	66	74	11	77	52
9	23	47	73	58	21	67	68	72	14	76	51
10	.5025	.8646	.5175	.8557	.5324	.8465	.5471	.8371	.5616	.8274	50
11	28	44	78	55	26	63	73	69	18	72	49
12	30	43	80	54	29	62	76	68	21	71	48
13	33	41	83	52	31	60	78	66	23	69	47
14	35	40	85	51	34	59	80	64	26	68	46
15	.5038	.8638	.5188	.8549	.5336	.8457	.5483	.8363	.5628	.8266	45
16	40	37	90	48	39	56	85	61	30	64	44
17	43	35	93	46	41	54	88	60	33	63	43
18	45	34	95	45	44	53	90	58	35	61	42
19	48	32	98	43	46	51	93	56	38	59	41
20	.5050	.8631	.5200	.8542	.5348	.8450	.5495	.8355	.5640	.8258	40
21	53	30	03	40	51	48	98	53	42	56	39
22	55	28	05	39	53	46	5500	52	45	54	38
23	58	27	08	37	56	45	02	50	47	53	37
24	60	25	10	36	58	43	05	48	50	51	36
25	.5063	.8624	.5213	.8534	.5361	.8442	.5507	.8347	.5652	.8249	35
26	65	22	15	32	63	40	10	45	54	48	34
27	68	21	18	31	66	39	12	44	57	46	33
28	70	19	20	29	68	37	15	42	59	45	32
29	73	18	23	28	71	35	17	40	62	43	31
30	.5075	.8616	.5225	.8526	.5373	.8434	.5519	.8339	.5664	.8241	30
31	78	15	27	25	75	32	22	37	66	40	29
32	80	13	30	23	78	31	24	36	69	38	28
33	83	12	32	22	80	29	27	34	71	36	27
34	85	10	35	20	83	28	29	32	74	35	26
35	.5088	.8609	.5237	.8519	.5385	.8426	.5531	.8331	.5676	.8233	25
36	90	07	40	17	88	25	34	29	78	31	24
37	93	06	42	16	90	23	36	28	81	30	23
38	95	04	45	14	93	21	39	26	83	28	22
39	98	03	47	13	95	20	41	24	86	26	21
40	.5100	.8601	.5250	.8511	.5398	.8418	.5544	.8323	.5688	.8225	20
41	03	00	52	10	5400	17	46	21	90	23	19
42	05	8599	55	08	02	15	48	20	93	21	18
43	08	97	57	07	05	14	51	18	95	20	17
44	10	96	60	05	07	12	53	16	98	18	16
45	.5113	.8594	.5262	.8504	.5410	.8410	.5556	.8315	.5700	.8216	15
46	15	93	65	02	12	09	58	13	02	15	14
47	18	91	67	00	15	07	61	11	05	13	13
48	20	90	70	8499	17	06	63	10	07	11	12
49	23	88	72	97	20	04	65	08	10	10	11
50	.5125	.8587	.5275	.8496	.5422	.8403	.5568	.8307	.5712	.8208	10
51	28	85	77	94	24	01	70	05	14	07	9
52	30	84	79	93	27	8399	73	03	17	05	8
53	33	82	82	91	29	98	75	02	19	03	7
54	35	81	84	90	32	96	77	00	21	02	6
55	.5138	.8579	.5287	.8488	.5434	.8395	.5580	.8298	.5724	.8200	5
56	40	78	89	87	37	93	82	97	26	8198	4
57	43	76	92	85	39	91	85	95	29	97	3
58	45	75	94	84	42	90	87	94	31	95	2
59	48	73	97	82	44	88	90	92	33	93	1
60	.5150	.8572	.5299	.8480	.5446	.8387	.5592	.8290	.5736	.8192	0
/	cos sin		cos sin		cos sin		cos sin		cos sin		/
/	59°		58°		57°		56°		55°		/



NATURAL TANGENTS AND COTANGENTS

/	30°		31°		32°		33°		34°		/
	tan	cot	tan	cot	tan	cot	tan	cot	tan	cot	
0	.5774	1.7321	.6009	1.6643	.6249	1.6003	.6494	1.5399	.6745	1.4826	60
1	77	7309	13	6632	53	5993	98	5389	49	4816	59
2	81	7297	17	6621	57	5983	6502	5379	54	4807	58
3	85	7286	20	6610	61	5972	06	5369	58	4798	57
4	89	7274	24	6599	65	5962	11	5359	62	4788	56
5	.5793	1.7262	.6028	1.6588	.6269	1.5952	.6515	1.5350	.6766	1.4779	55
6	97	7251	32	6577	73	5941	19	5340	71	4770	54
7	5801	7239	36	6566	77	5931	23	5330	75	4761	53
8	05	7228	40	6555	81	5921	27	5320	79	4751	52
9	08	7216	44	6545	85	5911	31	5311	83	4742	51
10	.5812	1.7205	.6048	1.6534	.6289	1.5900	.6536	1.5301	.6787	1.4733	50
11	16	7193	52	6523	93	5890	40	5291	92	4724	49
12	20	7182	56	6512	97	5880	44	5282	96	4715	48
13	24	7170	60	6501	6301	5869	48	5272	6800	4705	47
14	28	7159	64	6490	05	5859	52	5262	05	4696	46
15	.5832	1.7147	.6068	1.6479	.6310	1.5849	.6556	1.5253	.6809	1.4687	45
16	36	7136	72	6469	14	5839	60	5243	13	4678	44
17	40	7124	76	6458	18	5829	65	5233	17	4669	43
18	44	7113	80	6447	22	5818	69	5224	22	4659	42
19	47	7102	84	6436	26	5808	73	5214	26	4650	41
20	.5851	1.7090	.6088	1.6426	.6330	1.5798	.6577	1.5204	.6830	1.4641	40
21	55	7079	92	6415	34	5788	81	5195	34	4632	39
22	59	7067	96	6404	38	5778	85	5185	39	4623	38
23	63	7056	6100	6393	42	5768	90	5175	43	4614	37
24	67	7045	04	6383	46	5757	94	5166	47	4605	36
25	.5871	1.7033	.6108	1.6372	.6350	1.5747	.6598	1.5156	.6851	1.4596	35
26	75	7022	12	6361	54	5737	6602	5147	56	4586	34
27	79	7011	16	6351	58	5727	06	5137	60	4577	33
28	83	6999	20	6340	63	5717	10	5127	64	4568	32
29	87	6988	24	6329	67	5707	15	5118	69	4559	31
30	.5890	1.6977	.6128	1.6319	.6371	1.5697	.6619	1.5108	.6873	1.4550	30
31	94	6965	32	6308	75	5687	23	5099	77	4541	29
32	98	6954	36	6297	79	5677	27	5089	81	4532	28
33	5902	6943	40	6287	83	5667	31	5080	86	4523	27
34	06	6932	44	6276	87	5657	36	5070	90	4514	26
35	.5910	1.6920	.6148	1.6265	.6391	1.5647	.6640	1.5061	.6894	1.4505	25
36	14	6909	52	6255	95	5637	44	5051	99	4496	24
37	18	6898	56	6244	99	5627	48	5042	6903	4487	23
38	22	6887	60	6234	6403	5617	52	5032	07	4478	22
39	26	6875	64	6223	08	5607	57	5023	11	4469	21
40	.5930	1.6864	.6168	1.6212	.6412	1.5597	.6661	1.5013	.6916	1.4460	20
41	34	6853	72	6202	16	5587	65	5004	20	4451	19
42	38	6842	76	6191	20	5577	69	4994	24	4442	18
43	42	6831	80	6181	24	5567	73	4985	29	4433	17
44	45	6820	84	6170	28	5557	78	4975	33	4424	16
45	.5949	1.6808	.6188	1.6160	.6432	1.5547	.6682	1.4966	.6937	1.4415	15
46	53	6797	92	6149	36	5537	86	4957	42	4406	14
47	57	6786	96	6139	40	5527	90	4947	46	4397	13
48	61	6775	6200	6128	45	5517	94	4938	50	4388	12
49	65	6764	04	6118	49	5507	99	4928	54	4379	11
50	.5969	1.6753	.6208	1.6107	.6453	1.5497	.6703	1.4919	.6959	1.4370	10
51	73	6742	12	6097	57	5487	07	4910	63	4361	9
52	77	6731	16	6087	61	5477	11	4900	67	4352	8
53	81	6720	20	6076	65	5468	15	4891	72	4344	7
54	85	6709	24	6066	69	5458	20	4882	76	4335	6
55	.5989	1.6698	.6228	1.6055	.6473	1.5448	.6724	1.4872	.6980	1.4326	5
56	93	6687	33	6045	78	5438	28	4863	85	4317	4
57	97	6676	37	6034	82	5428	32	4854	89	4308	3
58	6001	6665	41	6024	86	5418	37	4844	93	4299	2
59	05	6654	45	6014	90	5408	41	4835	98	4290	1
60	.6009	1.6643	.6249	1.6003	.6494	1.5399	.6745	1.4826	.7002	1.4281	0
/	cot tan		cot tan		cot tan		cot tan		cot tan		/
/	59°		58°		57°		56°		55°		/

NATURAL SINES AND COSINES

/	35°		36°		37°		38°		39°		/
	sin	cos	sin	cos	sin	cos	sin	cos	sin	cos	
0	.5736	.8192	.5878	.8090	.6018	.7986	.6157	.7880	.6293	.7771	60
1	38	90	80	88	20	85	59	78	95	70	59
2	41	88	83	87	23	83	61	77	98	68	58
3	43	87	85	85	25	81	63	75	6300	66	57
4	45	85	87	83	27	79	66	73	02	64	56
5	.5748	.8183	.5890	.8082	.6030	.7978	.6168	.7871	.6305	.7762	55
6	50	81	92	80	32	76	70	69	07	60	54
7	52	80	94	78	34	74	73	68	09	59	53
8	55	78	97	76	37	72	75	66	11	57	52
9	57	76	99	75	39	71	77	64	14	55	51
10	.5760	.8175	.5901	.8073	.6041	.7969	.6180	.7862	.6316	.7753	50
11	62	73	04	71	44	67	82	60	18	51	49
12	64	71	06	70	46	65	84	59	20	49	48
13	67	70	08	68	48	64	86	57	23	48	47
14	69	68	11	66	51	62	89	55	25	46	46
15	.5771	.8166	.5913	.8064	.6053	.7960	.6191	.7853	.6327	.7744	45
16	74	65	15	63	55	58	93	51	29	42	44
17	76	63	18	61	58	56	96	50	32	40	43
18	79	61	20	59	60	55	98	48	34	38	42
19	81	60	22	58	62	53	6200	46	36	37	41
20	.5783	.8158	.5925	.8056	.6065	.7951	.6202	.7844	.6338	.7735	40
21	86	56	27	54	67	49	05	42	41	33	39
22	88	55	30	52	69	48	07	41	43	31	38
23	90	53	32	51	71	46	09	39	45	29	37
24	93	51	34	49	74	44	11	37	47	27	36
25	.5795	.8150	.5937	.8047	.6076	.7942	.6214	.7835	.6350	.7725	35
26	98	48	39	45	78	41	16	33	52	24	34
27	5800	46	41	44	81	39	18	32	54	22	33
28	02	45	44	42	83	37	21	30	56	20	32
29	05	43	46	40	85	35	23	28	59	18	31
30	.5807	.8141	.5948	.8039	.6088	.7934	.6225	.7826	.6361	.7716	30
31	09	39	51	37	90	32	27	24	63	14	29
32	12	38	53	35	92	30	30	22	65	13	28
33	14	36	55	33	95	28	32	21	68	11	27
34	16	34	58	32	97	26	34	19	70	09	26
35	.5819	.8133	.5960	.8030	.6099	.7925	.6237	.7817	.6372	.7707	25
36	21	31	62	28	6101	23	39	15	74	05	24
37	24	29	65	26	04	21	41	13	76	03	23
38	26	28	67	25	06	19	43	12	79	01	22
39	28	26	69	23	08	18	46	10	81	00	21
40	.5831	.8124	.5972	.8021	.6111	.7916	.6248	.7808	.6383	.7698	20
41	33	23	74	19	13	14	50	06	85	96	19
42	35	21	76	18	15	12	52	04	88	94	18
43	38	19	79	16	18	10	55	02	90	92	17
44	40	17	81	14	20	09	57	01	92	90	16
45	.5842	.8116	.5983	.8013	.6122	.7907	.6259	.7799	.6394	.7688	15
46	45	14	86	11	24	05	62	97	97	87	14
47	47	12	88	09	27	03	64	95	99	85	13
48	50	11	90	07	29	02	66	93	6401	83	12
49	52	09	93	06	31	00	68	92	03	81	11
50	.5854	.8107	.5995	.8004	.6134	.7898	.6271	.7790	.6406	.7679	10
51	57	06	97	02	36	96	73	88	08	77	9
52	59	04	6000	00	38	94	75	86	10	75	8
53	61	02	02	7999	41	93	77	84	12	74	7
54	64	00	04	97	43	91	80	82	14	72	6
55	.5866	.8099	.6007	.7995	.6145	.7889	.6282	.7781	.6417	.7670	5
56	68	97	09	93	47	87	84	79	19	68	4
57	71	95	11	92	50	85	86	77	21	66	3
58	73	94	14	90	52	84	89	75	23	64	2
59	75	92	16	88	54	82	91	73	26	62	1
60	.5878	.8090	.6018	.7986	.6157	.7880	.6293	.7771	.6428	.7660	0
/	54°		53°		52°		51°		50°		/

NATURAL TANGENTS AND COTANGENTS

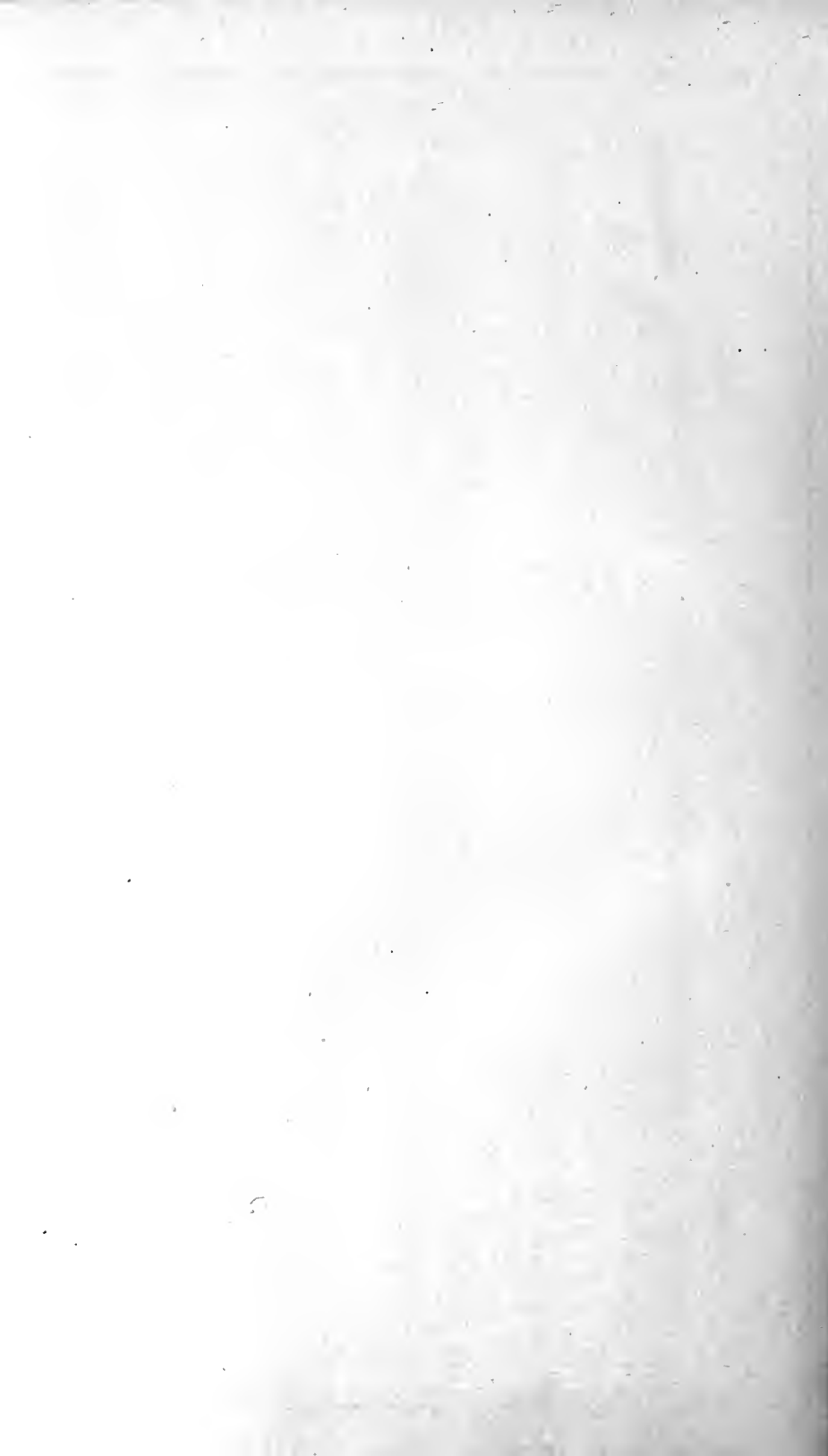
/	35°		36°		37°		38°		39°		/
	tan	cot	tan	cot	tan	cot	tan	cot	tan	cot	
0	.7002	1.4281	.7265	1.3764	.7536	1.3270	.7813	1.2799	.8098	1.2349	60
1	06	4273	70	3755	40	3262	18	2792	8103	2342	59
2	11	4264	74	3747	45	3254	22	2784	07	2334	58
3	15	4255	79	3739	49	3246	27	2776	12	2327	57
4	19	4246	83	3730	54	3238	32	2769	17	2320	56
5	.7024	1.4237	.7288	1.3722	.7558	1.3230	.7836	1.2761	.8122	1.2312	55
6	28	4229	92	3713	63	3222	41	2753	27	2305	54
7	32	4220	97	3705	68	3214	46	2746	32	2298	53
8	37	4211	7301	3697	72	3206	50	2738	36	2290	52
9	41	4202	06	3688	77	3198	55	2731	41	2283	51
10	.7046	1.4193	.7310	1.3680	.7581	1.3190	.7860	1.2723	.8146	1.2276	50
11	50	4185	14	3672	86	3182	65	2715	51	2268	49
12	54	4176	19	3663	90	3175	69	2708	56	2261	48
13	59	4167	23	3655	95	3167	74	2700	61	2254	47
14	63	4158	28	3647	7600	3159	79	2693	65	2247	46
15	.7067	1.4150	.7332	1.3638	.7604	1.3151	.7883	1.2685	.8170	1.2239	45
16	72	4141	37	3630	09	3143	88	2677	75	2232	44
17	76	4132	41	3622	13	3135	93	2670	80	2225	43
18	80	4124	46	3613	18	3127	98	2662	85	2218	42
19	85	4115	50	3605	23	3119	7902	2655	90	2210	41
20	.7089	1.4106	.7355	1.3597	.7627	1.3111	.7907	1.2647	.8195	1.2203	40
21	94	4097	59	3588	32	3103	12	2640	99	2196	39
22	98	4089	64	3580	36	3095	16	2632	8204	2189	38
23	7102	4080	68	3572	41	3087	21	2624	09	2181	37
24	07	4071	73	3564	46	3079	26	2617	14	2174	36
25	.7111	1.4063	.7377	1.3555	.7650	1.3072	.7931	1.2609	.8219	1.2167	35
26	15	4054	82	3547	55	3064	35	2602	24	2160	34
27	20	4045	86	3539	59	3056	40	2594	29	2153	33
28	24	4037	91	3531	64	3048	45	2587	34	2145	32
29	29	4028	95	3522	69	3040	50	2579	38	2138	31
30	.7133	1.4019	.7400	1.3514	.7673	1.3032	.7954	1.2572	.8243	1.2131	30
31	37	4011	04	3506	78	3024	59	2564	48	2124	29
32	42	4002	09	3498	83	3017	64	2557	53	2117	28
33	46	3994	13	3490	87	3009	69	2549	58	2109	27
34	51	3985	18	3481	92	3001	73	2542	63	2102	26
35	.7155	1.3976	.7422	1.3473	.7696	1.2993	.7978	1.2534	.8268	1.2095	25
36	59	3968	27	3465	7701	2985	83	2527	73	2088	24
37	64	3959	31	3457	06	2977	88	2519	78	2081	23
38	68	3951	36	3449	10	2970	92	2512	83	2074	22
39	73	3942	40	3440	15	2962	97	2504	87	2066	21
40	.7177	1.3934	.7445	1.3432	.7720	1.2954	.8002	1.2497	.8292	1.2059	20
41	81	3925	49	3424	24	2946	07	2489	97	2052	19
42	86	3916	54	3416	29	2938	12	2482	8302	2045	18
43	90	3908	58	3408	34	2931	16	2475	07	2038	17
44	95	3899	63	3400	38	2923	21	2467	12	2031	16
45	.7199	1.3891	.7467	1.3392	.7743	1.2915	.8026	1.2460	.8317	1.2024	15
46	7203	3882	72	3384	47	2907	31	2452	22	2017	14
47	08	3874	76	3375	52	2900	35	2445	27	2009	13
48	12	3865	81	3367	57	2892	40	2437	32	2002	12
49	17	3857	85	3359	61	2884	45	2430	37	1995	11
50	.7221	1.3848	.7490	1.3351	.7766	1.2876	.8050	1.2423	.8342	1.1988	10
51	26	3840	95	3343	71	2869	55	2415	46	1981	9
52	30	3831	99	3335	75	2861	59	2408	51	1974	8
53	34	3823	7504	3327	80	2853	64	2401	56	1967	7
54	39	3814	08	3319	85	2846	69	2393	61	1960	6
55	.7243	1.3806	.7513	1.3311	.7789	1.2838	.8074	1.2386	.8366	1.1953	5
56	48	3798	17	3303	94	2830	79	2378	71	1946	4
57	52	3789	22	3295	99	2822	83	2371	76	1939	3
58	57	3781	26	3287	7803	2815	88	2364	81	1932	2
59	61	3772	31	3278	08	2807	93	2356	86	1925	1
60	.7265	1.3764	.7536	1.3270	.7813	1.2799	.8098	1.2349	.8391	1.1918	0
	cot	tan	cot	tan	cot	tan	cot	tan	cot	tan	
/	54°		53°		52°		51°		50°		/

NATURAL SINES AND COSINES

/	40°		41°		42°		43°		44°		/
	sin	cos	sin	cos	sin	cos	sin	cos	sin	cos	
0	.6428	.7660	.6561	.7547	.6691	.7431	.6820	.7314	.6947	.7193	60
1	30	59	63	45	93	30	22	12	49	91	59
2	32	57	65	43	96	28	24	10	51	89	58
3	35	55	67	41	98	26	26	08	53	87	57
4	37	53	69	39	6700	24	28	06	55	85	56
5	.6439	.7651	.6572	.7538	.6702	.7422	.6831	.7304	.6957	.7183	55
6	41	49	74	36	04	20	33	02	59	81	54
7	43	47	76	34	06	18	35	00	61	79	53
8	46	45	78	32	09	16	37	7298	63	77	52
9	48	44	80	30	11	14	39	96	65	75	51
10	.6450	.7642	.6583	.7528	.6713	.7412	.6841	.7294	.6967	.7173	50
11	52	40	85	26	15	10	43	92	70	71	49
12	55	38	87	24	17	08	45	90	72	69	48
13	57	36	89	22	19	06	48	88	74	67	47
14	59	34	91	20	22	04	50	86	76	65	46
15	.6461	.7632	.6593	.7518	.6724	.7402	.6852	.7284	.6978	.7163	45
16	63	30	96	16	26	00	54	82	80	61	44
17	66	29	98	15	28	7398	56	80	82	59	43
18	68	27	6600	13	30	96	58	78	84	57	42
19	70	25	02	11	32	94	60	76	86	55	41
20	.6472	.7623	.6604	.7509	.6734	.7392	.6862	.7274	.6988	.7153	40
21	75	21	07	07	37	90	65	72	90	51	39
22	77	19	09	05	39	88	67	70	92	49	38
23	79	17	11	03	41	87	69	68	95	47	37
24	81	15	13	01	43	85	71	66	97	45	36
25	.6483	.7613	.6615	.7499	.6745	.7383	.6873	.7264	.6999	.7143	35
26	86	12	17	97	47	81	75	62	7001	41	34
27	88	10	20	95	49	79	77	60	03	39	33
28	90	08	22	93	52	77	79	58	05	37	32
29	92	06	24	91	54	75	81	56	07	35	31
30	.6494	.7604	.6626	.7490	.6756	.7373	.6884	.7254	.7009	.7133	30
31	97	02	28	88	58	71	86	52	11	30	29
32	99	00	31	86	60	69	88	50	13	28	28
33	6501	7598	33	84	62	67	90	48	15	26	27
34	03	96	35	82	64	65	92	46	17	24	26
35	.6506	.7595	.6637	.7480	.6767	.7363	.6894	.7244	.7019	.7122	25
36	08	93	39	78	69	61	96	42	22	20	24
37	10	91	41	76	71	59	98	40	24	18	23
38	12	89	44	74	73	57	6900	38	26	16	22
39	14	87	46	72	75	55	03	36	28	14	21
40	.6517	.7585	.6648	.7470	.6777	.7353	.6905	.7234	.7030	.7112	20
41	19	83	50	68	79	51	07	32	32	10	19
42	21	81	52	66	82	49	09	30	34	08	18
43	23	79	54	64	84	47	11	28	36	06	17
44	25	78	57	63	86	45	13	26	38	04	16
45	.6528	.7576	.6659	.7461	.6788	.7343	.6915	.7224	.7040	.7102	15
46	30	74	61	59	90	41	17	22	42	00	14
47	32	72	63	57	92	39	19	20	44	7098	13
48	34	70	65	55	94	37	21	18	46	96	12
49	36	68	67	53	97	35	24	16	48	94	11
50	.6539	.7566	.6670	.7451	.6799	.7333	.6926	.7214	.7050	.7092	10
51	41	64	72	49	6801	31	28	12	53	90	9
52	43	62	74	47	03	29	30	10	55	88	8
53	45	60	76	45	05	27	32	08	57	85	7
54	47	59	78	43	07	25	34	06	59	83	6
55	.6550	.7557	.6680	.7441	.6809	.7323	.6936	.7203	.7061	.7081	5
56	52	55	83	39	11	21	38	01	63	79	4
57	54	53	85	37	14	19	40	7199	65	77	3
58	56	51	87	35	16	18	42	97	67	75	2
59	58	49	89	33	18	16	44	95	69	73	1
60	.6561	.7547	.6691	.7431	.6820	.7314	.6947	.7193	.7071	.7071	0
	cos	sin	cos	sin	cos	sin	cos	sin	cos	sin	
	49°		48°		47°		46°		45°		

NATURAL TANGENTS AND COTANGENTS

/	40°		41°		42°		43°		44°		/
	tan	cot	tan	cot	tan	cot	tan	cot	tan	cot	
0	.8391	1.1918	.8693	1.1504	.9004	1.1106	.9325	1.0724	.9657	1.0355	60
1	96	1910	98	1497	09	1100	31	0717	63	0349	59
2	8401	1903	8703	1490	15	1093	36	0711	68	0343	58
3	06	1896	08	1483	20	1087	41	0705	74	0337	57
4	11	1889	13	1477	25	1080	47	0699	79	0331	56
5	.8416	1.1882	.8718	1.1470	.9030	1.1074	.9352	1.0692	.9685	1.0325	55
6	21	1875	24	1463	36	1067	58	0686	91	0319	54
7	26	1868	29	1456	41	1061	63	0680	96	0313	53
8	31	1861	34	1450	46	1054	69	0674	9702	0307	52
9	36	1854	39	1443	52	1048	74	0668	08	0301	51
10	.8441	1.1847	.8744	1.1436	.9057	1.1041	.9380	1.0661	.9713	1.0295	50
11	46	1840	49	1430	62	1035	85	0655	19	0289	49
12	51	1833	54	1423	67	1028	91	0649	25	0283	48
13	56	1826	59	1416	73	1022	96	0643	30	0277	47
14	61	1819	65	1410	78	1016	9402	0637	36	0271	46
15	.8466	1.1812	.8770	1.1403	.9083	1.1009	.9407	1.0630	.9742	1.0265	45
16	71	1806	75	1396	89	1003	13	0624	47	0259	44
17	76	1799	80	1389	94	0996	18	0618	53	0253	43
18	81	1792	85	1383	99	0990	24	0612	59	0247	42
19	86	1785	90	1376	9105	0983	29	0606	64	0241	41
20	.8491	1.1778	.8796	1.1369	.9110	1.0977	.9435	1.0599	.9770	1.0235	40
21	96	1771	8801	1363	15	0971	40	0593	76	0230	39
22	8501	1764	06	1356	21	0964	46	0587	81	0224	38
23	06	1757	11	1349	26	0958	51	0581	87	0218	37
24	11	1750	16	1343	31	0951	57	0575	93	0212	36
25	.8516	1.1743	.8821	1.1336	.9137	1.0945	.9462	1.0569	.9798	1.0206	35
26	21	1736	27	1329	42	0939	68	0562	9804	0200	34
27	26	1729	32	1323	47	0932	73	0556	10	0194	33
28	31	1722	37	1316	53	0926	79	0550	16	0188	32
29	36	1715	42	1310	58	0919	84	0544	21	0182	31
30	.8541	1.1708	.8847	1.1303	.9163	1.0913	.9490	1.0538	.9827	1.0176	30
31	46	1702	52	1296	69	0907	95	0532	33	0170	29
32	51	1695	58	1290	74	0900	9501	0526	38	0164	28
33	56	1688	63	1283	79	0894	06	0519	44	0158	27
34	61	1681	68	1276	85	0888	12	0513	50	0152	26
35	.8566	1.1674	.8873	1.1270	.9190	1.0881	.9517	1.0507	.9856	1.0147	25
36	71	1667	78	1263	95	0875	23	0501	61	0141	24
37	76	1660	84	1257	9201	0869	28	0495	67	0135	23
38	81	1653	89	1250	06	0862	34	0489	73	0129	22
39	86	1647	94	1243	12	0856	40	0483	79	0123	21
40	.8591	1.1640	.8899	1.1237	.9217	1.0850	.9545	1.0477	.9884	1.0117	20
41	96	1633	8904	1230	22	0843	51	0470	90	0111	19
42	8601	1626	10	1224	28	0837	56	0464	96	0105	18
43	06	1619	15	1217	33	0831	62	0458	9902	0099	17
44	11	1612	20	1211	39	0824	67	0452	07	0094	16
45	.8617	1.1606	.8925	1.1204	.9244	1.0818	.9573	1.0446	.9913	1.0088	15
46	22	1599	31	1197	49	0812	78	0440	19	0082	14
47	27	1592	36	1191	55	0805	84	0434	25	0076	13
48	32	1585	41	1184	60	0799	90	0428	30	0070	12
49	37	1578	46	1178	66	0793	95	0422	36	0064	11
50	.8642	1.1571	.8952	1.1171	.9271	1.0786	.9601	1.0416	.9942	1.0058	10
51	47	1565	57	1165	76	0780	06	0410	48	0052	9
52	52	1558	62	1158	82	0774	12	0404	54	0047	8
53	57	1551	67	1152	87	0768	18	0398	59	0041	7
54	62	1544	72	1145	93	0761	23	0392	65	0035	6
55	.8667	1.1538	.8978	1.1139	.9298	1.0755	.9629	1.0385	.9971	1.0029	5
56	72	1531	83	1132	9303	0749	34	0379	77	0023	4
57	78	1524	88	1126	09	0742	40	0373	83	0017	3
58	83	1517	94	1119	14	0736	46	0367	88	0012	2
59	88	1510	99	1113	20	0730	51	0361	94	0006	1
60	.8693	1.1504	.9004	1.1106	.9325	1.0724	.9657	1.0355	1.0000	1.0000	0
	cot	tan	cot	tan	cot	tan	cot	tan	cot	tan	
/	49°		48°		47°		46°		45°		/



## TABLE IV



### MISCELLANEOUS TABLES

1. RADIAN MEASURE,  $0^\circ$  to  $180^\circ$ .
2. NATURAL LOGARITHMS:
  - (A) Numbers from 1 to 200.
  - (B) Numbers from 1 to 9.9.
3. THE HYPERBOLIC FUNCTIONS,  $\text{SINH } x$ ,  $\text{COSH } x$ .

TABLE IV. 1. RADIAN MEASURE, 0° TO 180°, RADIUS = 1

DEGREES				MINUTES		SECONDS			
0°	0.00000 00	60°	1.04719 76	120°	2.09439 51	0'	0.00000 00	0''	0.00000 00
1	0.01745 33	61	1.06465 08	121	2.11184 84	1	0.00029 09	1	0.00000 48
2	0.03490 66	62	1.08210 41	122	2.12930 17	2	0.00058 18	2	0.00000 97
3	0.05235 99	63	1.09955 74	123	2.14675 50	3	0.00087 27	3	0.00001 45
4	0.06981 32	64	1.11701 07	124	2.16420 83	4	0.00116 36	4	0.00001 94
5	0.08726 65	65	1.13446 40	125	2.18166 16	5	0.00145 44	5	0.00002 42
6	0.10471 98	66	1.15191 73	126	2.19911 49	6	0.00174 53	6	0.00002 91
7	0.12217 30	67	1.16937 06	127	2.21656 82	7	0.00203 62	7	0.00003 39
8	0.13962 63	68	1.18682 39	128	2.23402 14	8	0.00232 71	8	0.00003 88
9	0.15707 96	69	1.20427 72	129	2.25147 47	9	0.00261 80	9	0.00004 36
10	0.17453 29	70	1.22173 05	130	2.26892 80	10	0.00290 89	10	0.00004 85
11	0.19198 62	71	1.23918 38	131	2.28638 13	11	0.00319 98	11	0.00005 33
12	0.20943 95	72	1.25663 71	132	2.30383 46	12	0.00349 07	12	0.00005 82
13	0.22689 28	73	1.27409 04	133	2.32128 79	13	0.00378 15	13	0.00006 30
14	0.24434 61	74	1.29154 36	134	2.33874 12	14	0.00407 24	14	0.00006 79
15	0.26179 94	75	1.30899 69	135	2.35619 45	15	0.00436 33	15	0.00007 27
16	0.27925 27	76	1.32645 02	136	2.37364 78	16	0.00465 42	16	0.00007 76
17	0.29670 60	77	1.34390 35	137	2.39110 11	17	0.00494 51	17	0.00008 24
18	0.31415 93	78	1.36135 68	138	2.40855 44	18	0.00523 60	18	0.00008 73
19	0.33161 26	79	1.37881 01	139	2.42600 77	19	0.00552 69	19	0.00009 21
20	0.34906 59	80	1.39626 34	140	2.44346 10	20	0.00581 78	20	0.00009 70
21	0.36651 91	81	1.41371 67	141	2.46091 42	21	0.00610 87	21	0.00010 18
22	0.38397 24	82	1.43117 00	142	2.47836 75	22	0.00639 95	22	0.00010 67
23	0.40142 57	83	1.44862 33	143	2.49582 08	23	0.00669 04	23	0.00011 15
24	0.41887 90	84	1.46607 66	144	2.51327 41	24	0.00698 13	24	0.00011 64
25	0.43633 23	85	1.48352 99	145	2.53072 74	25	0.00727 22	25	0.00012 12
26	0.45378 56	86	1.50098 32	146	2.54818 07	26	0.00756 31	26	0.00012 61
27	0.47123 89	87	1.51843 64	147	2.56563 40	27	0.00785 40	27	0.00013 09
28	0.48869 22	88	1.53588 97	148	2.58308 73	28	0.00814 49	28	0.00013 57
29	0.50614 55	89	1.55334 30	149	2.60054 06	29	0.00843 58	29	0.00014 06
30	0.52359 88	90	1.57079 63	150	2.61799 39	30	0.00872 66	30	0.00014 54
31	0.54105 21	91	1.58824 96	151	2.63544 72	31	0.00901 75	31	0.00015 03
32	0.55850 54	92	1.60570 29	152	2.65290 05	32	0.00930 84	32	0.00015 51
33	0.57595 87	93	1.62315 62	153	2.67035 38	33	0.00959 93	33	0.00016 00
34	0.59341 19	94	1.64060 95	154	2.68780 70	34	0.00989 02	34	0.00016 48
35	0.61086 52	95	1.65806 28	155	2.70526 03	35	0.01018 11	35	0.00016 97
36	0.62831 85	96	1.67551 61	156	2.72271 36	36	0.01047 20	36	0.00017 45
37	0.64577 18	97	1.69296 94	157	2.74016 69	37	0.01076 29	37	0.00017 94
38	0.66322 51	98	1.71042 27	158	2.75762 02	38	0.01105 38	38	0.00018 42
39	0.68067 84	99	1.72787 60	159	2.77507 35	39	0.01134 46	39	0.00018 91
40	0.69813 17	100	1.74532 93	160	2.79252 68	40	0.01163 55	40	0.00019 39
41	0.71558 50	101	1.76278 25	161	2.80998 01	41	0.01192 64	41	0.00019 88
42	0.73303 83	102	1.78023 58	162	2.82743 34	42	0.01221 73	42	0.00020 36
43	0.75049 16	103	1.79768 91	163	2.84488 67	43	0.01250 82	43	0.00020 85
44	0.76794 49	104	1.81514 24	164	2.86234 00	44	0.01279 91	44	0.00021 33
45	0.78539 82	105	1.83259 57	165	2.87979 33	45	0.01309 00	45	0.00021 82
46	0.80285 15	106	1.85004 90	166	2.89724 66	46	0.01338 09	46	0.00022 30
47	0.82030 47	107	1.86750 23	167	2.91469 99	47	0.01367 17	47	0.00022 79
48	0.83775 80	108	1.88495 56	168	2.93215 31	48	0.01396 26	48	0.00023 27
49	0.85521 13	109	1.90240 89	169	2.94960 64	49	0.01425 35	49	0.00023 76
50	0.87266 46	110	1.91986 22	170	2.96705 97	50	0.01454 44	50	0.00024 24
51	0.89011 79	111	1.93731 55	171	2.98451 30	51	0.01483 53	51	0.00024 73
52	0.90757 12	112	1.95476 88	172	3.00196 63	52	0.01512 62	52	0.00025 21
53	0.92502 45	113	1.97222 21	173	3.01941 96	53	0.01541 71	53	0.00025 70
54	0.94247 78	114	1.98967 53	174	3.03687 29	54	0.01570 80	54	0.00026 18
55	0.95993 11	115	2.00712 86	175	3.05432 62	55	0.01599 89	55	0.00026 66
56	0.97738 44	116	2.02458 19	176	3.07177 95	56	0.01628 97	56	0.00027 15
57	0.99483 77	117	2.04203 52	177	3.08923 28	57	0.01658 06	57	0.00027 63
58	1.01229 10	118	2.05948 85	178	3.10668 61	58	0.01687 15	58	0.00028 12
59	1.02974 43	119	2.07694 18	179	3.12413 94	59	0.01716 24	59	0.00028 60
60	1.04719 76	120	2.09439 51	180	3.14159 27	60	0.01745 33	60	0.00029 09

DEGREES

MINUTES

SECONDS



**A. THE NATURAL LOGARITHMS**

OF

**INTEGERS FROM 1 TO 200**



Base  $e = 2.7182818284\dots$   
 $\log_{10} e = 0.4342944819\dots$   
 $\log_e 10 = 2.3025850929\dots$   
 $\log_e \pi = 1.1447298858\dots$

*Conversion Laws :*

$$\log_e N = \log_e 10 \times \log_{10} N.$$

$$\log_{10} N = \log_{10} e \times \log_e N.$$

N	log <sub>e</sub>	N	log <sub>e</sub>	N	log <sub>e</sub>	N	log <sub>e</sub>	N	log <sub>e</sub>
<b>0</b>	— ∞	<b>40</b>	3.68 888	<b>80</b>	4.38 203	<b>120</b>	4.78 749	<b>160</b>	5.07 517
1	0.00 000	41	3.71 357	81	4.39 445	121	4.79 579	161	5.08 140
2	0.69 315	42	3.73 767	82	4.40 672	122	4.80 402	162	5.08 760
3	1.09 861	43	3.76 120	83	4.41 884	123	4.81 218	163	5.09 375
4	1.38 629	44	3.78 419	84	4.43 082	124	4.82 028	164	5.09 987
5	1.60 944	45	3.80 666	85	4.44 265	125	4.82 831	165	5.10 595
6	1.79 176	46	3.82 864	86	4.45 435	126	4.83 628	166	5.11 199
7	1.94 591	47	3.85 015	87	4.46 591	127	4.84 419	167	5.11 799
8	2.07 944	48	3.87 120	88	4.47 734	128	4.85 203	168	5.12 396
9	2.19 722	49	3.89 182	89	4.48 864	129	4.85 981	169	5.12 990
<b>10</b>	2.30 259	<b>50</b>	3.91 202	<b>90</b>	4.49 981	<b>130</b>	4.86 753	<b>170</b>	5.13 580
11	2.39 790	51	3.93 183	91	4.51 086	131	4.87 520	171	5.14 166
12	2.48 491	52	3.95 124	92	4.52 179	132	4.88 280	172	5.14 749
13	2.56 495	53	3.97 029	93	4.53 260	133	4.89 035	173	5.15 329
14	2.63 906	54	3.98 898	94	4.54 329	134	4.89 784	174	5.15 906
15	2.70 805	55	4.00 733	95	4.55 388	135	4.90 527	175	5.16 479
16	2.77 259	56	4.02 535	96	4.56 435	136	4.91 265	176	5.17 048
17	2.83 321	57	4.04 305	97	4.57 471	137	4.91 998	177	5.17 615
18	2.89 037	58	4.06 044	98	4.58 497	138	4.92 725	178	5.18 178
19	2.94 444	59	4.07 754	99	4.59 512	139	4.93 447	179	5.18 739
<b>20</b>	2.99 573	<b>60</b>	4.09 434	<b>100</b>	4.60 517	<b>140</b>	4.94 164	<b>180</b>	5.19 296
21	3.04 452	61	4.11 087	101	4.61 512	141	4.94 876	181	5.19 850
22	3.09 104	62	4.12 713	102	4.62 497	142	4.95 583	182	5.20 401
23	3.13 549	63	4.14 313	103	4.63 473	143	4.96 284	183	5.20 949
24	3.17 805	64	4.15 888	104	4.64 439	144	4.96 981	184	5.21 494
25	3.21 888	65	4.17 439	105	4.65 396	145	4.97 673	185	5.22 036
26	3.25 810	66	4.18 965	106	4.66 344	146	4.98 361	186	5.22 575
27	3.29 584	67	4.20 469	107	4.67 283	147	4.99 043	187	5.23 111
28	3.33 220	68	4.21 951	108	4.68 213	148	4.99 721	188	5.23 644
29	3.36 730	69	4.23 411	109	4.69 135	149	5.00 395	189	5.24 175
<b>30</b>	3.40 120	<b>70</b>	4.24 850	<b>110</b>	4.70 048	<b>150</b>	5.01 064	<b>190</b>	5.24 702
31	3.43 399	71	4.26 268	111	4.70 953	151	5.01 728	191	5.25 227
32	3.46 574	72	4.27 667	112	4.71 850	152	5.02 388	192	5.25 750
33	3.49 651	73	4.29 046	113	4.72 739	153	5.03 044	193	5.26 269
34	3.52 636	74	4.30 407	114	4.73 620	154	5.03 695	194	5.26 786
35	3.55 535	75	4.31 749	115	4.74 493	155	5.04 343	195	5.27 300
36	3.58 352	76	4.33 073	116	4.75 359	156	5.04 986	196	5.27 811
37	3.61 092	77	4.34 381	117	4.76 217	157	5.05 625	197	5.28 320
38	3.63 759	78	4.35 671	118	4.77 068	158	5.06 260	198	5.28 827
39	3.66 356	79	4.36 945	119	4.77 912	159	5.06 890	199	5.29 330
<b>40</b>	3.68 888	<b>80</b>	4.38 203	<b>120</b>	4.78 749	<b>160</b>	5.07 517	<b>200</b>	5.29 832

**B. NATURAL LOGARITHMS 1 TO 9.9**



The following table shows the Natural or Napierian logarithms, for each tenth, of numbers 1 to 9.9. Interpolation may be made for hundredths. The logarithms of numbers larger than 9.9 may be found as shown in the following illustration: *Let us find the  $\log_e 450$ :*

$$\begin{aligned} \log_e 450 &= \log_e(4.5 \times 10^2) = \log_e 4.5 + 2 \log_e 10 \\ &= 1.5041 + 2(2.3026) = 6.1093. \end{aligned}$$

No.	$\log_e$	No.	$\log_e$	No.	$\log_e$	No.	$\log_e$	No.	$\log_e$	No.	$\log_e$
1.0	0.0000	2.5	0.9163	4.0	1.3863	5.5	1.7048	7.0	1.9459	8.5	2.1401
1.1	.0953	2.6	.9555	4.1	.4110	5.6	.7228	7.1	.9601	8.6	.1518
1.2	.1823	2.7	.9933	4.2	.4351	5.7	.7405	7.2	.9741	8.7	.1633
1.3	.2624	2.8	1.0296	4.3	.4586	5.8	.7579	7.3	.9879	8.8	.1748
1.4	.3365	2.9	.0647	4.4	.4816	5.9	.7750	7.4	2.0015	8.9	.1861
1.5	0.4055	3.0	1.0986	4.5	1.5041	6.0	1.7917	7.5	2.0149	9.0	2.1972
1.6	.4700	3.1	.1314	4.6	.5261	6.1	.8083	7.6	.0282	9.1	.2083
1.7	.5306	3.2	.1632	4.7	.5476	6.2	.8246	7.7	.0412	9.2	.2192
1.8	.5878	3.3	.1939	4.8	.5686	6.3	.8406	7.8	.0541	9.3	.2300
1.9	.6419	3.4	.2238	4.9	.5892	6.4	.8563	7.9	.0669	9.4	.2407
2.0	0.6932	3.5	1.2528	5.0	1.6094	6.5	1.8718	8.0	2.0794	9.5	2.2513
2.1	.7419	3.6	.2809	5.1	.6292	6.6	.8871	8.1	.0919	9.6	.2618
2.2	.7885	3.7	.3083	5.2	.6487	6.7	.9021	8.2	.1041	9.7	.2721
2.3	.8329	3.8	.3350	5.3	.6677	6.8	.9169	8.3	.1163	9.8	.2824
2.4	.8755	3.9	.3610	5.4	.6864	6.9	.9315	8.4	.1282	9.9	.2925

TABLE IV

$$3. \text{ HYPERBOLIC } \sinh x = \frac{e^x - e^{-x}}{2}, \cosh x = \frac{e^x + e^{-x}}{2}.$$

$x$	$\sinh x$	$\cosh x$	$x$	$\sinh x$	$\cosh x$
0.00	0.0000	1.0000	0.50	0.5211	1.1276
.01	.0100	1.0000	.51	.5324	1.1329
.02	.0200	1.0002	.52	.5438	1.1383
.03	.0300	1.0004	.53	.5552	1.1438
.04	.0400	1.0008	.54	.5666	1.1494
.05	.0500	1.0013	.55	.5782	1.1551
.06	.0600	1.0018	.56	.5897	1.1609
.07	.0701	1.0025	.57	.6014	1.1669
.08	.0801	1.0032	.58	.6131	1.1730
.09	.0901	1.0041	.59	.6248	1.1792
.10	.1002	1.0050	.60	.6367	1.1855
.11	.1102	1.0061	.61	.6485	1.1919
.12	.1203	1.0072	.62	.6605	1.1984
.13	.1304	1.0085	.63	.6725	1.2051
.14	.1405	1.0098	.64	.6846	1.2119
.15	.1506	1.0113	.65	.6967	1.2188
.16	.1607	1.0128	.66	.7090	1.2258
.17	.1708	1.0145	.67	.7213	1.2330
.18	.1810	1.0162	.68	.7336	1.2402
.19	.1911	1.0181	.69	.7461	1.2476
.20	.2013	1.0201	.70	.7586	1.2552
.21	.2115	1.0221	.71	.7712	1.2628
.22	.2218	1.0243	.72	.7838	1.2706
.23	.2320	1.0266	.73	.7966	1.2785
.24	.2423	1.0289	.74	.8094	1.2865
.25	.2526	1.0314	.75	.8223	1.2947
.26	.2629	1.0340	.76	.8353	1.3030
.27	.2733	1.0367	.77	.8484	1.3114
.28	.2837	1.0395	.78	.8615	1.3199
.29	.2941	1.0423	.79	.8748	1.3286
.30	.3045	1.0453	.80	.8881	1.3374
.31	.3150	1.0484	.81	.9015	1.3464
.32	.3255	1.0516	.82	.9150	1.3555
.33	.3360	1.0549	.83	.9286	1.3647
.34	.3466	1.0584	.84	.9423	1.3740
.35	.3572	1.0619	.85	.9561	1.3835
.36	.3678	1.0655	.86	.9700	1.3932
.37	.3785	1.0692	.87	.9840	1.4029
.38	.3892	1.0731	.88	.9981	1.4128
.39	.4000	1.0770	.89	1.0122	1.4229
.40	.4108	1.0811	.90	1.0265	1.4331
.41	.4216	1.0852	.91	1.0409	1.4434
.42	.4325	1.0895	.92	1.0554	1.4539
.43	.4434	1.0939	.93	1.0700	1.4645
.44	.4543	1.0984	.94	1.0847	1.4753
.45	.4653	1.1030	.95	1.0995	1.4862
.46	.4764	1.1077	.96	1.1144	1.4973
.47	.4875	1.1125	.97	1.1294	1.5085
.48	.4986	1.1174	.98	1.1446	1.5199
.49	.5098	1.1225	.99	1.1598	1.5314
0.50	0.5211	1.1276	1.00	1.1752	1.5431



# First Course in Differential and Integral Calculus

BY WILLIAM F. OSGOOD, PH.D.  
Professor of Mathematics in Harvard University

---

*Revised Edition. Cloth, xv + 462 pages, \$2.00 net*

---

The treatment of this calculus by Professor Osgood is based on the courses he has given in Harvard College for a number of years. The chief characteristics of the treatment are the close touch between the calculus and those problems of physics, including geometry, to which it owed its origin; and the simplicity and directness with which the principles of the calculus are set forth. It is important that the formal side of the calculus should be thoroughly taught in a first course, and great stress has been laid on this side. But nowhere do the ideas that underlie the calculus come out more clearly than in its applications to curve tracing and the study of curves and surfaces, in definite integrals, with their varied applications to physics and geometry, and in mechanics. For this reason these subjects have been taken up at an early stage and illustrated by many examples not usually found in American text-books. From the beginning the book has been a favorite with the academic classes, and it has now been adopted by some of the best-known and best-thought-of engineering schools in the country.

---

THE MACMILLAN COMPANY

64-66 Fifth Avenue, New York

# Applied Mechanics for Engineers

*A Text-book for Engineering Students*

BY

F. L. HANCOCK

Professor of Applied Mechanics, Worcester Polytechnic Institute

*Illustrated, cloth, 12mo, xii + 388 pages, \$2.00 net*

*A new edition with typographical corrections*

In the preparation of this book the author has had in mind the fact that the student finds much difficulty in seeing the applications of theory to practical problems. For this reason each new principle developed is followed by a number of applications. In many cases these are illustrated, and they all deal with matters that directly concern the engineer. It is believed that the problems in mechanics should be practical engineering work. The author has endeavored to follow out this idea in writing the present volume. Accordingly, the title "Applied Mechanics for Engineers" has been given to the book. The book is intended as a text-book for engineering students of the Junior year. The subject-matter is such as is usually covered by the work of one semester. In some chapters more material is presented than can be used in this time. With this idea in mind the articles in these chapters have been arranged so that those coming last may be omitted without affecting the continuity of the work. The book contains more problems than can usually be given in any one semester. An appendix giving tables for the use of the student is of importance. These tables include the following: Hyperbolic Functions, Trigonometric Functions, Logarithms of Numbers, Squares, Cubes, etc., and Conversion Tables.

---

THE MACMILLAN COMPANY

64-66 Fifth Avenue, New York

# Co-ordinate Geometry

BY

HENRY BURCHARD FINE

AND

HENRY DALLAS THOMPSON

*Cloth, 12mo, x + 316 pages, \$1.60 net*

“It surprised me to see that the authors could put the treatment of the plane into less than two hundred pages, and my surprise increased to find that no important topic had been omitted.”—VIRGIL SNYDER, Ithaca, New York.

“After teaching this book one year I want to say that it is the most teachable book of its kind that I have seen in some time. We expect to use it again next year.”—A. M. HARDING, Fayetteville, Arkansas.

“I am just finishing a half year with a class of twenty-one in Fine and Thompson’s Co-ordinate Geometry, having found the book one of the freshest and most teachable I ever put into a student’s hands.

“Their methods of treatment are a distinct departure from those found in the usual texts, being more direct, more concrete, and more lucid. The examples, solved and unsolved, are beautiful and thoroughly representative. In fact, it is every way an uncommonly good beginner’s book.”—IRA M. DELONG, Boulder, Colorado.

---

THE MACMILLAN COMPANY

64-66 Fifth Avenue, New York

THE UNIVERSITY LIBRARY

This book is DUE on the last date stamped below

MAR 16 1948

OCT 20 1957

MAR 14 1949

OCT 6

MAR 31 1950

APR 30 1951

OCT 6 RECD

OCT 25 1951

DEC 22 1953

APR 14 1954

APR 15 1958  
AUG 13 1958

AUG 15 1958

SEP 8 1958

JAN

MAY 10 1963

AUG 5 1964

AUG 11 RECD

Form L-6  
250-10-44(210)

UNIVERSITY OF CALIFORNIA

LOS ANGELES

LIBRARY

Johanne  
Geo.  
Visser  
Chug  
Bill  
Tong  
Bernie



Engineering &  
Mathematical  
Sciences  
Library



A 000 257 690 8

QA  
S31  
R742

ADDITIONAL  
STACK

72

