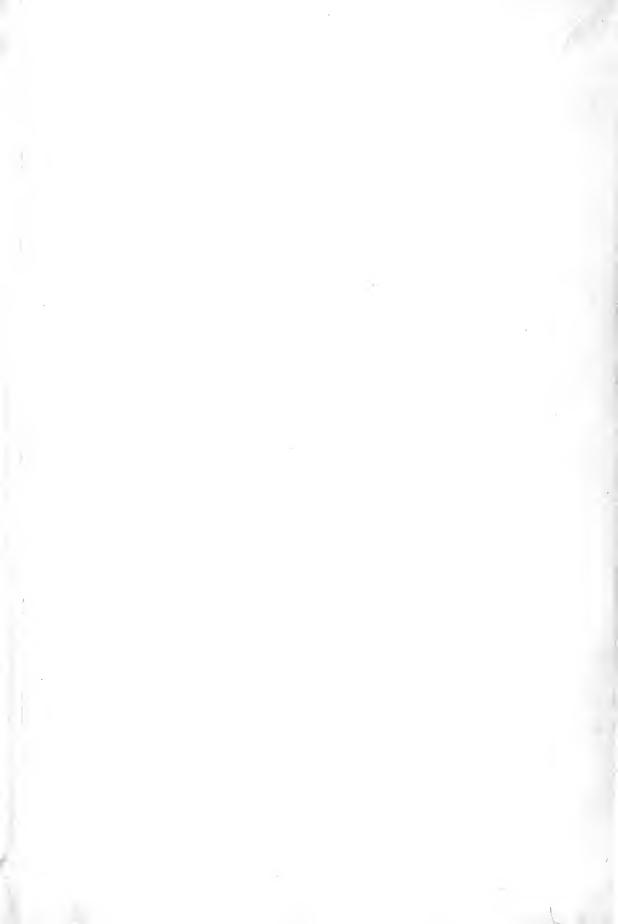
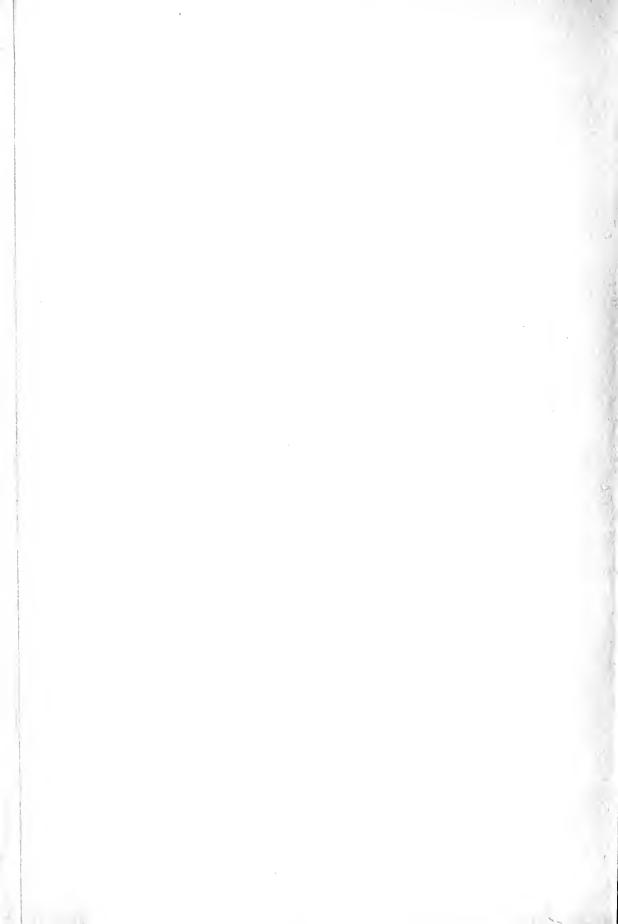


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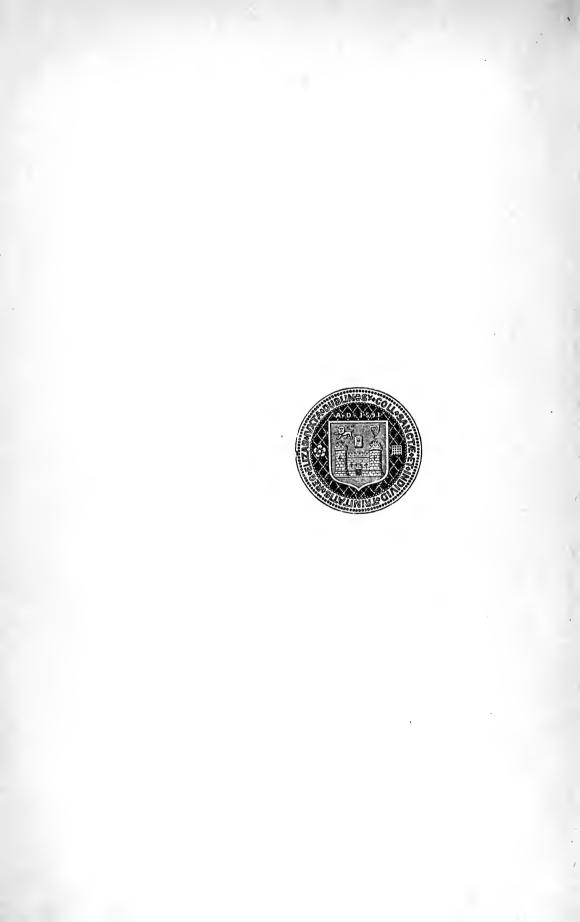








ELEMENTS OF QUATERNIONS.



ELEMENTS

OF

QUATERNIONS.

BY THE LATE

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SECOND EDITION.

EDITED BY

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ADVERTISEMENT TO THE SECOND EDITION.

I HAVE reserved for the Appendix to this Volume the longer additional and illustrative notes which I have written for the new edition of the "ELEMENTS."

Some of those notes would have been inconveniently long as footnotes; others would have been inconveniently placed. For example, although the Note on Screws relates naturally to Art. 416 and that on the Kinematical Treatment of Curves to Art. 396, I have placed the Note on Screws before the Note on Curves because Hamilton's remarks on screw motion in the earlier Article required some development in order to make the Note on Curves easily intelligible. Accordingly the order of the notes has been arranged with reference to the notes themselves rather than with reference to the text. The selection and treatment of the subjects of these notes have been subordinated to the illustration of quaternion methods. I have not hesitated to sacrifice brevity for suggestiveness, and above all I have tried to render the notation as explicit as possible. An analysis of the Appendix will be found on pages xlv-xlix.

For greater convenience I have provided an Index to the whole work referring to the pages, the volumes being distinguished by the numbers i and ii.

I take this opportunity of testifying to the extraordinary accuracy both of matter and of printing in the first edition of the "ELEMENTS." Every portion of the work bears evidence of Hamilton's unsparing pains. I cannot recall a single sentence ambiguous in its meaning, or a single case in which a difficulty is not honestly faced. I see no sign of diminished vigour or of relaxed care in those portions of the work written in his failing health. My task as editor has convinced me of the extreme eaution with which any endeavour should be made to improve or modify the calculus of Quaternions.

In conclusion, I desire to express my thanks to the College Printer, Mr. George Weldrick, for the great care he has taken in printing this edition for the Board of Trinity College, and for his unvarying courtesy to myself.

CHARLES JASPER JOLY.

THE OBSERVATORY, DUNSINK, 16th December, 1900.

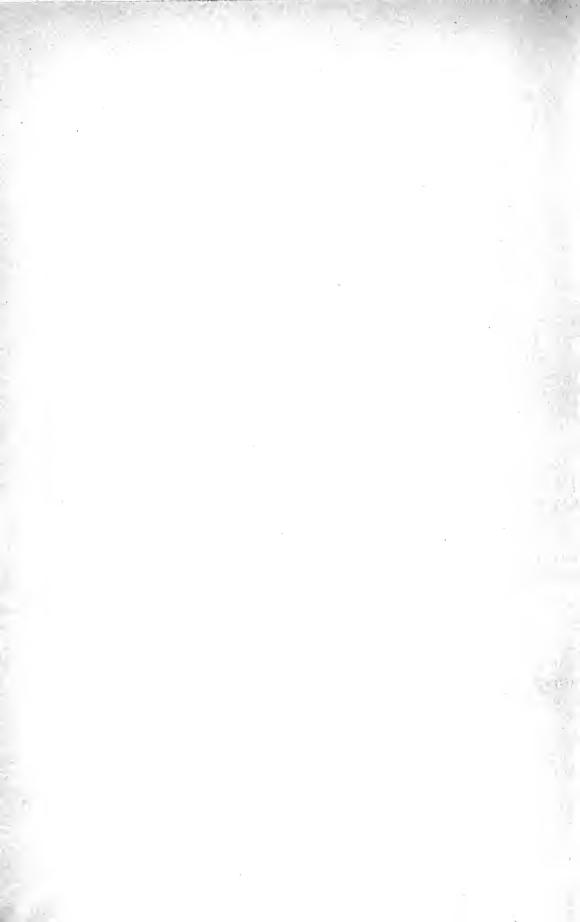


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CHAPTER III.

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Double Curvature,	•	24-29			
SECTION 5.—On Geodetic Lines, and Families of Surfaces.					

In these Sections, $d\rho$ usually denotes a *tangent to a curve*, and ν a normal to a surface. Some of the theorems or constructions may perhaps be new; for instance, those connected with the cone of parallels (pp. 6, 26, &c.) to the tangents to a curve of double curvature; and possibly the theorem (p. 42), respecting reciprocal curves in space: at least, the deductions here given of these results may serve as exemplifications of the Calculus employed. In treating of Families of Surfaces by quaternions, a sort of analogue (pp. 47, 48) to the formation and integration of Partial Differential Equations presents itself; as indeed it had done, on a similar occasion, in the Lectures (574).

SECTION	6.—On	Osculating	Circles	and	Sphe	res,	to Cu	rves in	1 Spac	e; w	ith	
son	ie conne	cted Constru	ictions,		•							50-179
The analysis however condensed of this long Section (III jii 6) cannot conveniently												

The analysis, however condensed, of this long Section (III. iii. 6), cannot conveniently be performed otherwise than under the heads of the respective *Articles* (389-401) which compose it: each Article being followed by several sub-articles, which form with it a sort of *Series.* •

* A Table of initial Pages of all the Articles will be elsewhere given, which will much facilitate reference.

ARTICLE 389.—Osculating Circle defined, as the limit of a circle, which touches a given curve (plane or of double curvature) at a given point P, and cuts the curve at a near point Q (see fig. 77, p. 24). Deduction and interpretation of general expressions for the vector κ of the centre κ of the centre so defined. The reciprocal of the radius **RP** being called the vector of curvature, we have generally,

Vector of Curvature =
$$(\rho - \kappa)^{-1} = \frac{dUd\rho}{Td\rho} = \frac{1}{d\rho} \nabla \frac{d^2\rho}{d\rho} = \&c.$$
 (8)

and if the arc (s) of the curve be made the independent variable, then

Vector of Curvature =
$$\rho'' = D_s^2 \rho = \frac{d^2 \rho}{ds^2}$$
. (S)

Examples: curvatures of helix, ellipse, hyperbola, logarithmic spiral; locus of centres of curvature of helix, plane evolute of plane ellipse,

osculates; example, hyperbola,

ARTICLE 394.—Intersection (or intersections) of a spherical curve with a small circle osculating thereto; example, spherical conic; constructions for the spherical centre (or pole) of the circle osculating to such a curve, and for the point of intersection above mentioned,

ARTICLE 395.—Osculating Sphere, to a curve of double curvature, defined as the limit of a sphere, which contains the osculating circle to the curve at a given point P, and cuts the same curve at a near point q (comp. Art. 389). The centre s, of the sphere so found, is (as usual) the point in which the polar axis (Art. 391) touches the cusp-edge of the polar developable. Other general construction for the same centre (p. 77, comp. 106). General expressions for the vector, $\sigma = os$, and for the radius, $R = s\bar{P}$; R^{-1} is the spherical curvature (comp. Art. 397). Condition of Sphericity (S = 1), and Coefficient of Non-sphericity (S - 1), for a curve in space. When this last coefficient is positive (as it is for the helix), the curve lies outside the sphere, at least in the neighbourhood of the point of osculation,

ARTICLE 396.—Notations τ , τ' , . . for $D_{s\rho}$, $D_{s}^{2\rho}$, &c. ; properties of a curve depending on the square (s²) of its arc, measured from a given point P; $\tau = unit-tangent$, $\tau' = vector$ $of curvature, <math>r^{-1} = T\tau' = curvature$ (or first curvature, comp. Art. 397), $\nu = \tau\tau' = binormal$; the three planes, respectively perpendicular to τ , τ' , ν , are the normal plane, the rectifying plane, and the osculating plane; general theory of emanant lines and planes, vector of rotation, axis of displacement, osculating screw surface; condition of developability of surface of emanants,

ARTICLE 397.—Properties depending on the cube (s^3) of the arc; Radius r (denoted here, for distinction, by a roman letter), and Vector $r^{-1}\tau$, of Second Curvature; this radius r may be either positive or negative (whereas the radius r of first curvature is always treated as positive), and its reciprocal r^{-1} may be thus expressed (pp. 92, 88),

Second Curvature* =
$$\mathbf{r}^{-1} = \mathbf{S} \frac{\mathrm{d}^3 \rho}{\mathrm{Vd} \rho \mathrm{d}^2 \rho}$$
, (T), or, $\mathbf{r}^{-1} = \mathbf{S} \frac{\tau''}{\tau \tau'}$, (T')

the independent variable being the arc in (T'), while it is arbitrary in (T): but quaternions

ARTS. 389-397.

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[•] In this Article, or Series, 397, and indeed also in 396 and 398, several references are given to a very interesting Memoir by M. de Saint-Venant, "Sur les lignes courbes non planes": in which, however, that able writer objects to such known phrases as second curvature, torsion, &c., and proposes in their stead a new name "cambrure," which it has not been thought necessary here to adopt. (Journal de l'École Polytechnique, Cahier xxx.)

ARTS. 397, 398.

or (comp. p. 125),

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supply a vast variety of *other expressions* for this important scalar (see, for instance, the *Table* in p. 108). We have also (by p. 89, comp. Arts. 389, 395, 396),

Vector of Spherical Curvature =
$$sP^{-1} = (\rho - \sigma)^{-1} = \&c.,$$
 (U)

= projection of vector (τ') of (simple or first) curvature, on radius (R) of osculating sphere: and if p and P denote the linear and angular elevations, of the centre (s) of this sphere above the osculating plane, then (by same page 89),

$$p = r \tan P = R \sin P = r'r = rD_s r. \tag{U'}$$

Again (pp. 89, 90), if we write (comp. Art. 396),

$$\lambda = V \frac{\tau}{\tau'} = r^{-1}\tau + \tau\tau' = Vector of Second Curvature plus Binormal, \qquad (V)$$

this line λ may be called the *Rectifying Vector*; and if *H* denote the *inclination* (considered first by Lancret), of this *rectifying line* (λ) to the *tangent* (τ) to the curve, then

$$\tan H = r'^{-1} \tan P = r^{-1} r. \tag{V'}$$

Known right cone with rectifying line for its axis, and with H for its semiangle, which osculates at P to the developable locus of tangents to the curve (or by p. 99 to the cone of parallels already mentioned); new right cone, with a new semiangle, C, connected with H by the relation (p. 91),

$$\tan C = \frac{3}{4} \tan H, \qquad (V'')$$

which osculates to the cone of chords, drawn from the given point P to other points Q of the given curve. Other osculating cones, cylinders, helix, and parabola; this last being (pp. 91, 96) the parabola which osculates to the projection of the curve, on its own osculating plane. Deviation of curve, at any near point q, from the osculating circle at P, decomposed (p. 96) into two rectangular deviations, from osculating helix and parabola. Additional formulæ (p. 109), for the general theory of emanants (Art. 396); case of normally emanant lines, or of tangentially emanant planes. General auxiliary spherical curve (pp. 110-112, comp. p. 28); new proof of the second expression (V') for tan H, and of the theorem that if this ratio of curvatures be constant, the proposed curve is a geodetic on a cylinder : new proof that if each curvature (r^{-1}, r^{-1}) be constant, the cylinder is right, and therefore the curve a helix,

This Series 398 is so much longer than any other in the Volume, and is supposed to contain so much original matter, that it seems necessary here to subdivide the analysis under several separate heads, lettered as (a), (b), (e), &c.

(a). Neglecting s⁵, we may write (p. 112, comp. Art. 396),

$$OP_s = \rho_s = \rho + s\tau + \frac{1}{2}s^2\tau' + \frac{1}{6}s^3\tau'' + \frac{1}{24}s^4\tau''';$$
(W)

$$\rho_s = \rho + x_s \tau + y_s r \tau' + z_s r \nu, \tag{W'}$$

with expressions (p. 126) for the *coefficients* (or *coordinates*) x_s , y_s , z_s , in terms of r, r', r'', r, r, and s. If s^5 be taken into account, it becomes necessary to add to the expression (W) the term, $\frac{1}{120}s^5\tau^{17}$; with corresponding additions to the scalar coefficients in (W'), introducing r''' and r'': the laws for forming which additional terms, and for extending them to higher powers of the are, are assigned in a subsequent Series (399, pp. 156, 163).

(b). Analogous expressions for τ''' , ν'' , κ'' , λ' , σ' , and p', R', P', H', to serve in questions in which s^5 is neglected, are assigned (in p. 113); τ'' , ν' , κ' , λ , σ , and p, R, P, H, having been previously expressed (in Series 397); while $\tau^{1\nabla}$, ν''' , κ''' , λ'' , σ'' , &c. enter into investigations which take account of s^5 : the arc s being treated as the independent variable in all *these* derivations.

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b

88, 112

112-156

ix Pages (c). One of the chief results of the present Series (398), is the introduction (p. 116, &c.) of a new auxiliary angle, J, analogous in several respects to the known angle H (397), but belonging to a higher order of theorems, respecting curves in space: because the new angle J depends on the fourth (and lower) powers of the arc s, while Lancret's angle H depends only on s^3 (including s^1 and s^2). In fact, while tan H is represented by the expressions (V'), whereof one is r'^{-1} tan P, tan J admits (with many transformations) of the following analogous expression (p. 116),

$$\tan J = R^{-1} \tan P; \tag{X}$$

where R' depends* by (b) on s^4 , while r' and P depend (397) on no higher power than s^3 .

(d). To give a more distinct geometrical meaning to this new angle J, than can be easily gathered from such a formula as (X), respecting which it may be observed, in passing, that J is in general more simply defined by expressions for its cotangent (pp. 116, 126), than for its tangent, we are to conceive that, at each point P of any proposed curve of double curvature, there is drawn a tangent plane to the sphere, which osculates (395) to the curve at that point ; and that then the envelope of all these planes is determined, which envelope (for reasons afterwards more fully explained) is called here (p. 116) the " Circumscribed Developable ": being a surface analogous to the " Rectifying Developable" of Lancret, but belonging (c) to a higher order of questions. And then, as the known angle H denotes (397) the inclination, suitably measured, of the rectifying line (λ), which is a generatrix of the rectifying developable, to the tangent (τ) to the curve; so the new angle J represents the inclination of a generating line (ϕ), of what has just been called the *circumscribed* developable, to the same tangent (τ) , measured likewise in a defined direction (p. 117), but in the tangent plane to the sphere. It may be noted as another analogy (p. 117), that while H is a right angle for a plane curve, so J is right when the curve is spherical. For the helix (p. 122), the angles H and J are equal; and the rectifying and circumscribed developables coincide, with each other and with the right cylinder, on which the helix is a geodetic line.

(e). If the recent line ϕ be measured from the given point \mathbf{r} , in a suitable direction (as contrasted with the opposite), and with a suitable length, it becomes what may be called (comp. 396) the Vector of Rotation of the Tangent Plane (d) to the Osculating Sphere; and then it satisfies, among others, the equations (pp. 114, 116, comp. (V)),

$$\phi = \mathbf{V} \frac{\nu''}{\nu}, \quad \mathbf{T}\phi = R^{-1} \operatorname{cosec} J; \quad (\mathbf{X}')$$

this last being an expression for the velocity of rotation of the plane just mentioned, or of its normal, namely the spherical radius R, if the given curve be conceived to be described by a point moving with a constant velocity, assumed = 1. And if we denote by v the point in which the given radius R or PS is nearest to a consecutive radius of the same kind, or to the radius of a consecutive osculating sphere, then this point v divides the line PS internally, into segments which may (ultimately) be thus expressed (pp. 115, 116),

$$\overline{\mathbf{P}\mathbf{v}} = R\sin^2 J, \quad \overline{\mathbf{v}\mathbf{s}} = R\cos^2 J. \tag{X''}$$

But these and other connected results, depending on s^4 , have their known analogues (with H for J, and r for R), in that earlier theory (c) which introduces only s^3 (besides s^1 and s^2): and they are all *included* in the general theory of *emanant* lines and planes (396, 397), of which some new geometrical illustrations (pp. 117, 120) are here given.

• In other words, the calculation of r' and P introduces no differentials higher than the *third* order; but that of K requires the *fourth* order of differentials. In the language of modern geometry, the former can be determined by the consideration of four consecutive points of the curve, or by that of two consecutive osculating circles; but the latter requires the consideration of two consecutive osculating spheres, and therefore of five consecutive points of the curve (supposed to be one of double curvature). Other investigations, in the present and immediately following Series (398, 399), especially those connected with what we shall shortly call the Osculating Twisted Cubic, will be found to involve the consideration of six consecutive points of a curve.

х

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(f). New auxiliary scalar $n (= p^{-1}RK' = \cot J \sec P = \&c.)$, = velocity of centre s of osculating sphere, if the velocity of the point P of the given curve be taken as unity (e); n vanishes with R', $\cot J$, and $(\operatorname{comp.} 395)$ the coefficient $S - 1 (= nrT^{-1})$ of non-sphericity, for the case of a spherical curve (p. 120). Arcs, first and second curvatures, and rectifying planes and lines, of the cusp-edges of the polar and rectifying * developables; these can all be expressed without going beyond s^5 , and some without using any higher power than s^4 , or differentials of the orders corresponding; $r_1 = nr$, and $r_1 = nr$, are the scalar radii of first and second curvature of the former cusp-edge, r_1 being positive when that curve turns its concavity at s towards the given curve at P: determination of the point R, in which the latter cusp-edge is touched by the rectifying line λ to the original curve (pp. 120), 125).

(g). Equation with one arbitrary constant (p. 125), of a cone of the second order, which has its vertex at the given point \mathbf{P} , and has contact of the third order (or four-side contact) with the cone of chords (397) from that point; equation (p. 128) of a cylinder of the second order, which has an arbitrary line \mathbf{PE} from \mathbf{P} as one side, and has contact of the fourth order (or five-point contact) with the curve at \mathbf{P} ; the constant above mentioned can be so determined, that the right line \mathbf{PE} shall be a side of the cone also, and therefore a part of the intersection of cone and cylinder; and then the remaining or curvilinear part, of the complete intersection of those two surfaces of the second order, is (by known principles) a gauche curve of the third order, or what is briefly called a Twisted Cubic: and this last curve, in virtue of its construction above described, and whatever the assumed direction of the auxiliary line \mathbf{PE} may be, has contact of the fourth order (or five-point contact) with the given curve of double curvature at \mathbf{P} (pp. 125, 129, comp. pp. 92, 104).

(\hbar). Determination (p. 129) of the constant in the equation of the cone (g), so that this cone may have contact of the fourth order (or five-side contact) with the cone of chords from **P**; the cone thus found may be called the Osculating Oblique Cone (comp. 397), of the second order, to that cone of chords; and the coefficients of its equation involve only r, r, r', r', r'', r'', but not r''', although this last derivative is of no higher order than r'', since each depends only on s⁵ (and lower powers), or introduces only fifth differentials. Again, the cylinder (g) will have contact of the fifth order (or six-point contact) with the given curve at **P**, if the line **PB**, which is by construction a side of the creating cone, of which the equation (p. 128) involves as constants not only rr'r'r'', like that of the osculating cone just determined, but also r'''. The two cones last mentioned have the tangent (r) to the given curve for a common side, \ddagger but they have also three other common sides, whereof one

* The rectifying plane, of the cusp-edge of the rectifying developable, is the plane of λ and τ' , of which the formula LIV'. in p. 124 is the equation; and the rectifying line RH, of the same cuspedge, intersects the absolute normal PK to the given curve, or the radius (r) of first curvature, in the point H in which that radius is nearest (e) to a consecutive radius of the same kind. But this last theorem, which is here deduced by quaternions, had been previously arrived at by M. de Saint-Venant (comp. the Note to p. viii), through an entirely different analysis, confirmed by geometrical considerations.

+ By Dr. Salmon, in his excellent Treatise on Analytic Geometry of Three Dimensions (Dublin, 1862), which is several times cited in the Notes to this final Chapter (III. iii.) of these Elements. The gauche curves, above mentioned, have been studied with much success, of late years, by M. Chasles, Sig. Cremona, and other geometers: but their existence, and some of their leading properties, appear to have been first perceived and published by Prof. Möbius (see his Barycentric Calculus. Leipzig, 1827, pp. 114-122, especially p. 117).

[‡] This side, however, counts as three (p. 159), in the system of the six lines of intersection (real or imaginary) of these two cones, which have a common vertex \mathbf{r} , and are respectively of the second and third orders (or degrees). Additional light will be thrown on this whole subject, in the following Series (399); in which also it will be shown that there is only one osculating twisted cubic, at a given point, to a given curve of double curvature; and that this cubic curve can be determined, without resolving any cubic or other equation.

02

at least is real, since they are assigned by a cubic equation (p. 129); and by taking this side for the line **FE** in (g), there results a new cylinder of the second order, which cuts the osculating oblique conc, partly in that right line FE itself, and partly in a gauche curve of the third order, which it is proposed to call an Osculating Twisted Cubic (comp. again (g)), because it has contact of the fifth order (or six-point contact) with the given curve at F (p. 129).

(i). In general, and independently of any question of osculation, a Twisted Cubic (g), if passing through the origin o, may be represented by any one of the vector equations (pp. 131, 132),

$$Va\rho + V\rho\phi\rho = 0, \qquad (Y); \qquad \text{or} \qquad (\phi + c)\rho = a, \qquad (Y')$$
$$\rho = (\phi + c)^{-1}a, \qquad (Y''); \qquad \text{or} \qquad Va\rho + \rho V\gamma\rho + V\rho V\lambda\rho\mu = 0, \qquad (Y''')$$

in which α , γ , λ , μ are real and constant vectors, but c is a variable scalar; while ϕp denotes (comp. the Section III. ii. 6, or p. xxxii, vol. i., a linear and vector function, which is here generally not self-conjugate, of the variable vector ρ of the cubic curve. The number of the scalar constants, in the form (Y'''), or in any other form of the equation, is found to be ten (p. 132), with the foregoing supposition that the curve passes through the origin, a restriction which it is easy to remove. The curve (Y) is cut, as it ought to be, in three points (real or imaginary), by an arbitrary secant plane; and its three asymptotes (real or imaginary) have the directions of the three vector roots β (see again the last cited Section) of the equation (same p. 131),

$$V\beta\phi\beta = 0: \tag{Z}$$

so that by (P), p. xxxii, vol. i., these three asymptotes compose a real and rectangular system, for the case of self-conjugation of the function ϕ in (Y).

(j). Deviation of a near point P_s of the given curve, from the sphere (395) which osculates at the given point P_s ; this deviation (by p. 132, comp. pp. 79, 120) is

$$\overline{sP}_s - \overline{sP} = \frac{r_1 s^4}{24 r r^2 R} = \frac{R' s^4}{24 r r p} = \frac{n s^4}{24 r r R} = \&c. \qquad (A_1)$$

it is ultimately equal (p. 134) to the quarter of the deviation (397) of the same near point \mathbf{P}_s from the osculating circle at \mathbf{P} , multiplied by the sine of the small angle SPS_s, which the small arc ss_s of the locus of the spheric centre s (or of the cusp-edge of the polar developable) subtends at the same point \mathbf{P} ; and it has an outward or an inward direction, according as this last arc is concave or convex (f) at s, towards the given curve at \mathbf{P} (pp. 122, 134). It is also ultimately equal (p. 136) to the deviation $\overline{\mathbf{PS}_s} - \overline{\mathbf{PsS}_s}$, of the given point \mathbf{P} from the near sphere, which osculates at the near point \mathbf{P}_s ; and likewise (p. 137) to the component, in the direction of SP, of the fourth of that near point from the osculating circle at \mathbf{P} , measured in a direction parallel to the normal plane at that point, if this last deviation be now expressed to the accuracy of the fourth order: whereas it has hitherto been considered sufficient to develope this deviation from the osculating circle (397) as far as the *third order* (or third dimension of s); and therefore to treat it as having a direction, tangential to the osculating sphere (comp. pp. 97, 133).

(k). The deviation (A_1) is also equal to the *third part* (p. 138) of the deviation of the near point **r**, from the given circle (which osculates at **r**), if measured in the near normal plane (at **r**), and decomposed in the direction of the radius R, of the near sphere; or to the third part (with direction preserved) of the deviation of the new near point in which the given circle is cut by the near plane, from the near sphere: or finally to the third part (as before, and still with an unchanged direction) of the deviation from the given normal plane (at **r**), and which is found to satisfy the equation,

$$\overline{sc} = 3\overline{sP_s} - 2\overline{sP}. \tag{B1}$$

Geometrical connexions (p. 140) between these various results (j) (k), illustrated by a diagram (fig. 83).

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or

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(1). The Surface, which is the Locus of the Osculating Circle to a given curve in space, may be represented rigorously by the vector expression (p. 141),

ω

$$r_{s,u} = \rho_s + r_s \tau_s \sin u + r_s^2 \tau_s' \text{ vers } u ; \qquad (C_1)$$

in which s and u are two independent scalar variables, whereof s is (as before) the arc **PP**_s of the given curve, but is not now treated as small: and u is the (small or large) angle subtended at the centre \mathbf{x}_s of the circle, by the arc of that circle, measured from its point of osculation \mathbf{P}_s . But the same superficial locus (comp. 392) may be represented also by the vector equation (p. 156) involving apparently only one scalar variable (s),

$$V \frac{2\tau_s}{\omega - \rho_s} + \nu_s = 0, \quad (D_1)$$

in which $v_s = \tau_s \tau'_s$, and $\omega = \omega_{s,u}$ = the vector of an arbitrary point of the surface. The general method (p. 11) of the Section III. iii. 3, shows that the normal to this surface (C₁), at any proposed point thereof, has the direction of $\omega_{s,u} - \sigma_s$; that is (p. 141), the direction of the radius of the sphere, which contains the circle through that point, and has the same point of osculation v_s to the given curve. The locus of the osculating circle is therefore found, by this little calculation with quaternions, to be at the same time the *Envelope of the Osculating Sphere*, as was to be expected from geometrical considerations (comp. the Note to p. 141).

(m). The curvilinear locus of the point c in (k) is one branch of the section of the surface (l), made by the normal plane to the given curve at r; and if D be the projection of c on the tangent at P to this new curve, which tangent PD has a direction perpendicular to the radius rs or R of the osculating sphere at P (see again fig. 83, in p. 140), while the ordinate DC is parallel to that radius, then (attending only to principal terms), pp. 139, 140) we have the expressions,

$$\mathbf{P}\mathbf{D} = \frac{Rs^3}{6r^2r} \mathbf{U}\tau \left(\sigma - \rho\right), \quad \mathbf{D}\mathbf{C} = \frac{-ns^3}{8r\mathbf{I}R} \mathbf{U} \left(\sigma - \rho\right), \quad (\mathbf{E}_1)$$

and therefore ultimately (p. 141),

$$\frac{DC^3}{PD^4} = \frac{81}{32} \cdot \frac{n^3 r^5 r (\sigma - \rho)}{R^3} = \text{const.};$$
 (F1)

from which it follows that **P** is a singular point of the section here considered, but not a cusp of that section, although the curvature at **P** is infinite: the ordinate DC varying ultimately as the power with exponent $\frac{4}{3}$ of the abscissa PD. Contrast (pp. 141, 142), of this section, with that of the developable Locus of Tangents, made by the same normal plane at **P** to the given curve; the vectors analogous to **PD** and **DC** are in this case nearly equal to $-\frac{1}{2}s^2\tau'$ and $-\frac{1}{3}s^3\mathbf{r}^{-1}\mathbf{v}$; so that the latter varies ultimately as the power $\frac{3}{2}$ of the former, and the point **P** is (as it is known to be) a cusp of this last section.

(n). A given Curve of double curvature is therefore generally a Singular Line (p. 143), although not a cuep-edge, upon that Surface (l), which is at once the Locus of its osculating Circle, and the Envelope of its osculating Sphere: and the new developable surface (d), as being circumscribed to this superficial locus (or envelope), so as to touch it along this singular line (p. 156), may naturally be called, as above, the Circumscribed Developable (p. 116).

(o). Additional light may be thrown on this whole theory of the singular line (n), by considering (pp. 143-155) a problem which was discussed by Monge, in two distinct Sections (xxii. xxvi.) of his well-known Analyse (comp. the Notes to pp. 144, 145, 153, 154, 155 of these Elements); namely, to determine the envelope of a sphere with varying radius R, whereof the centre s traverses a given curve in space; or briefly, to find the

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Envelope of a Sphere with One varying Parameter (comp. p. 171): especially for the Case of Coincidence (p. 145, &c.), of what are usually two distinct branches (p. 144) of a certain Characteristic Curve (or arête de rebroussement), namely the curvilinear envelope (real or imaginary) of all the circles, along which the superficial envelope of the spheres is touched by those spheres themselves.

(p). Quaternion forms (pp. 145, 146) of the condition of coincidence (o); one of these can be at once translated into Monge's equation of condition (p. 145), or into an equation slightly more general, as leaving the independent variable arbitrary; but a simpler and more easily interpretable form is the following (p. 146),

$$r_1 \mathrm{d}r = \pm R \mathrm{d}R, \tag{G_1}$$

in which r is the radius of the circle of contact, of a sphere with its envelope (o), while r_1 is the radius of (first) curvature of the curve (s), which is the locus of the centre s of the sphere.

(q). The singular line into which the two branches of the curvilinear envelope are fused, when this condition is satisfied, is in general an orthogonal trajectory (p. 151) to the osculating planes of the curve (s); that curve, which is now the given one, is therefore (comp. 391, 395) the cusp-edge (p. 151) of the polar developable, corresponding to the singular line just mentioned, or to what may be called the curve (P), which was formerly the given curve. In this way there arise many verifications of formulæ (p. 151, 152); for example, the equation (G_1) is easily shown to be consistent with the results of (f).

(r). With the geometrical hints thus gained from interpretation of quaternion results, there is now no difficulty in assigning the Complete and General Integral of the Equation of Condition (p), which was presented by Monge under the form (comp. p. 145) of a non-linear differential equation of the second order, involving three variables (ϕ, ψ, π) considered as functions of a fourth (a), namely the coordinates of the centre of the sphere, regarded as varying with the radius, but which does not appear to have been either integrated or interpreted by that illustrious analyst. The general integral here found presents itself at first in a quaternion form (p. 153), but is easily translated (p. 154) into the usual language of analysis. A less general integral is also assigned, and its geometrical signification exhibited, as answering to a case for which the singular line lately considered reduces itself to a singular point (p. 155).

(s). Among the verifications (q) of this whole theory, it is shown (pp. 152, 153) that although, when the two branches (o) of the general curvilinear envelope of the circles of the system are real and distinct, each branch is a cusp-edge (or arête de rebroussement, as Monge perceived it to be), upon the superficial envelope of the spheres, yet in the case of fusion (p) this cuspidal character is lost (as was likewise seen by Monge*): and that then a section of the surface, made by a normal plane to the singular line, has precisely the form (m), expressed by the equation (F1). In short, the result is in many ways confirmed, by calculation and by geometry, that when the condition of coincidence (p) is satisfied, the Surface is, as in (n), at once the Envelope of the osculating Sphere and the Locus of the soculating Circle, to that Singular Line on itself, into which by (q) the two branches (o) of its general cusp-edge are fused.

(t). Other applications of preceding formulæ might be given; for instance, the formula for κ'' enables us to assign general expressions (p. 155) for the centre and radius of the circle, which osculates at κ to the locus of the centre of the osculating circle, to a given curve in space: with an elementary verification, for the case of the plane evolute of the plane evolute of a plane curve. But it is time to conclude this long analysis, which however could scarcely have been much abridged, of the results of Series 398, and to pass to a more brief account of the investigations in the following Series.

* Compare the first Note to p. 153 of these Elements.

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ARTICLE 399.—Additional general investigations, respecting that gauche curve of the third order (or degree), which has been above called an Osculating Twisted Cubic (398, (h)), to any proposed curve of double curvature; with applications to the case, where the given curve is a helix,

(a). In general (p. 159) the tangent PT to the given curve is a nodal side of the cubic cone (398, (h)); one tangent plane to that cone (C_3) , along that side, being the osculating plane (P) to the curve, and therefore touching also, along the same side, the osculating oblique cone (C_2) of the second order, to the cone of chords (397) from P; while the other tangent plane to the cubic cone (C_3) crosses that first plane (P), or the quadric cone (C_2) , at an angle of which the trigonometric cotangent $(\frac{1}{2}t')$ is equal to half the differential of the radius (r) of second curvature, divided by the differential of the arc (s). And the three common sides, PE, PE', PE'', of these two cones, which remain when the tangent PT is excluded, and of which one at least must be real, are the parallels through the given point P to the three asymptotes (398, (i)) to the gauche curve sought; being also sides of three quadric cylinders, say (L_2) , (L'_2) , (L''_2) , which contain those asymptotes as other sides (or generating lines): and of which each contains the twisted cubic sought, and is cut in it by the quadric cone (C_2) .

(b). On applying this First Method to the case of a given helix, it is found (p. 159) that the general cubic cone (C_3) breaks up into the system of a new quadric cone, (C_2), and a new plane (P'); which latter is the rectifying plane (396) of the helix, or the tangent plane at r to the right cylinder, whereon that given curve is traced. The two quadric cones, (C_2) and (C_2') touch each other and the plane (P) along the tangent rr, and have no other real common side: whence two of the sought asymptotes, and two of the corresponding cylinders (a), are in this case imaginary, although they can still be used in calculation (pp. 159, 160, 162). But the plane (P') cuts the cone (C_2), not only in the tangent rr, but also in a second real side PE, to which the real asymptote is parallel (a); and which is at the same time a side of a real quadric cylinder (L_2) which has that asymptote for another side (p. 162), and contains the twisted cubic: this gauche curve being thus the curvilinear part (p. 161) of the intersection of the real cone (C_2), with the real cylinder (L_2).

(c). Transformations and verifications of this result; fractional expressions (p. 162), for the coordinates of the twisted cubic; expression (p. 161) for the deviation of the helix from that osculating curve, which deviation is directed inwards, and is of the sixth order: the least distance, between the tangent $\mathbf{T}\mathbf{T}$ and the real asymptote, is a right line \mathbf{PB} , which is cut internally (p. 162) by the axis of the right cylinder (b), in a point A such that \mathbf{PA} is to AB as three to seven.

(d). The First Method (a), which has been established in the preceding Series (398), succeeds then for the case of the helix, with a facility which arises chiefly from the circumstance (b), that for this case the general cubic cone (C_3) breaks up into two separate loci, whereof one is a plane (P). But usually the foregoing method requires, as in (398, (h)), the solution of a cubic equation: an inconvenience which is completely avoided, by the employment of a Second General Method, as follows.

(e). This Second Method consists in taking, for a second locus of the gauche osculatrix sought, a certain Cubic Surface (S_3) , of which every point is the vertex^{*} of a quadric cone,

* It is known that the locus of the vertex of a quadric cone, which passes through six given points of space, A, B, C, D, E, F, whereof no four are in one plane, is generally a Surface, say (S_4) , of the Fourth Degree: in fact, it is cut by the plane of the triangle ABC in a system of four right lines, whereof three are the sides of that triangle, and the fourth is the intersection of the two planes, ABC and DEF. If then we investigate the intersection of this surface (S_4) with the quadric cone, (A. BCDEF), or say (C_2) , which has A for vertex, and passes through the five other given points, we might expect to find (in some sense) a curve of the eighth degree. But when we set aside the five right lines, AB, AC, AD, AE, AF, which are common to the two surfaces here considered, we find that the (remaining or) curvilinear part of the complete intersection is reduced to a curve of the third degree,

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having six-point contact with the given curve at \mathbf{r} : so that this new surface is cut by the plane at infinity, in the same cubic curve as the cubic cone (C_3) . It is found (p. 166) to be a Ruled Surface, with the tangent PT for a Singular Line; and when this right line is set aside, the remaining (that is, the curvilinear) part of the intersection of the two loci, (C_2) and (S_3) , is the Osculating Twisted Cubic sought: which gauche osculatrix is thus completely and generally determined, without any such difficulty or apparent variety, as might be supposed to attend the solution of a cubic equation (d), and with new verifications for the case of the helix (p. 167).

$$S(\sigma - \rho) \rho' = 0, \quad V(\sigma - \rho) \sigma' = 0, \quad (H_1)$$

in which ρ and σ are corresponding vectors of involute and evolute; together with a theorem of Prof. De Morgan (p. 169), respecting the case when the evolute is a spherical curve.

(b). An involute in space is generally the only real part (p. 171) of the envelope of a certain variable sphere (comp. 398), which has its centre on the evolute, while its radius R is the variable intercept between the two curves: but because we have here the relation (p. 169, comp. p. 143),

$$R^{\prime 2} + \sigma^{\prime 2} = 0, \tag{H_1}$$

the circles of contact (398, (o)) reduce themselves each to a point (or rather to a pair of *imaginary right lines*, intersecting in a real point), and the preceding theory (398), of envelopes of spheres with one varying parameter, undergoes important modifications in its results, the conditions of the applications being different. In particular, the *involute* is indeed, as the equation (H_1) express, an orthogonal trajectory to the tangents of the evolute; but not to the osculating planes of that curve, as the singular line (398, (q)) of the former envelope was, to those of the curve which was the locus of the centres of the spheres before considered, when a certain condition of coincidence or of fusion, 398, (p)) was satisfied.

(c). Curvature of hodograph of evolute (p. 173): if P, P_1, P_2, \ldots and s, s_1, s_2, \ldots be corresponding points of involute and evolute, and if we draw right lines s_{T_1}, s_{T_2}, \ldots in the directions of s_1P_1, s_2P_2, \ldots and with a common length $= \overline{sP}$, the spherical curve PT_1T_2 . will have contact of the second order at P, with the involute PP_1P_2 . (p. 173).

ARTICLE 401.—Calculations abridged, by the treatment of quaternion differentials (which have hitherto been finite, comp. p. xxix, vol. i.) as infinitesimals;* new deductions of osculating plane, circle, and sphere, with the vector equation (392) of the circle; and of the first and second curvature of a curve in space,

which is precisely the twisted cubic through the six given points. In applying this general (and perhaps new) method, to the problem of the osculating twisted cubic to a curve, the osculating plane to that curve may be excluded, as foreign to the question: and then the quartie surface (S_4) is reduced to the cubic surface (S_3) , above described.

* Although, for the sake of brevity, and even of clearness, some phrases have been used in the foregoing analysis of the Series 398 and 399, such as four-side or five-side contact between cones, and five-point or six-point contact between curves, or between a curve and a surface, which are borrowed from the doctrine of consecutive points and lines, and therefore from that of infinitesimals; with a few other expressions of modern geometry, such as the plane at infinity. &c.; yet the reasonings in the text of these Elements have all been rigorously reduced, so far, or are all obviously reducible, to the fundamental conception of Limits; compare the definitions of the osculating eirele and sphere, assigned in Articles 389, 395. The object of Art. 401 is to make it visible how, without abandoning such ultimate reference to limits, it is possible to abridge calculation, in several cases, by treating (at this stage) the differential symbols, $d\rho$, $d^2\rho$, &c., as if they represented infinitely small differences, $\Delta\rho$, $\Delta^2\rho$, &c.; without taking the trouble to write these latter symbols first, as denoting finite differences, in the rigorous statement of a problem, of which statement it is not always

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ARTICLE 402 .- References to some equations of Surfaces, in earlier parts of the volume, . 179, 180

ARTICLES 403.—Quaternion equations of the Sphere ($\rho^2 = -1$, &c.), . 180, 182 In some of these equations, the Notation N for norm is employed (comp. the Section II. i. 6.)

ABTICLE 404.—Quaternion equations of the Ellipsoid, 183, 185 One of the simplest of these forms is (pp. 325, vol. i., 185) the equation,

$$T(\iota\rho + \rho\kappa) = \kappa^2 - \iota^2, \tag{I}_1$$

in which ι and κ are real and constant vectors, in the directions of the cyclic normals. This form (I1) is intimately connected with, and indeed served to suggest, that Construction of the Ellipsoid (II. i. 13), by means of a Diacentric Sphere and a Point (p. 234, vol. i., comp. fig. 53, pp. 234, vol. i., and 184), which was among the earliest geometrical results of the Quaternions. The three semiaxes, a, b, c, are expressed (comp. p. 238) interms of ι , κ as follows:

$$a = \mathbf{T}\iota + \mathbf{T}\kappa; \quad b = \frac{\kappa^2 - \iota^2}{\mathbf{T}(\iota - \kappa)}; \quad c = \mathbf{T}\iota - \mathbf{T}\kappa;$$
 (I1')

$$ab^{-1}c = \mathbf{T}(\iota - \kappa). \tag{I}_1)$$

ARTICLE 405.-General Central Surface of the Second Order (or central quadric), $S\rho\phi\rho = f\rho = 1,$ 186-189 Auticle 406.—General Cone of the Second Order (or quadric cone), $S_{\rho}\phi_{\rho} = f_{\rho} = 0$, ARTICLE 407 .- Bifocal Form of the equation of a central but non-conical surface of the

second order : with some quaternion formulæ, relating to Confocal Surfaces, .

(a). The bifocal form here adopted (comp. the Section III. ii. 6) is the equation,

$$Cf\rho = (Sa\rho)^2 - 2eSa\rho Sa'\rho + (Sa'\rho)^2 + (1 - e^2)\rho^2 = C,$$
 (J₁)

$$C = (e^2 - 1) (e + Saa')l^2.$$
 (J₁')

a, a' are two (real) focal unit-lines, common to the whole system of confocals; the (real and positive) scalar l is also constant for that system : but the scalar e varies, in passing from surface to surface, and may be regarded as a parameter, of which the value serves to distinguish one confocal, say (e), from another (pp. 196, 197).

(b). The squares (p. 197) of the three scalar semiaxes (real or imaginary), arranged in algebraically descending order, are

 $l^2 = \frac{a^2 - c^2}{c^2}, \quad e = \frac{a^2 + c^2}{c^2};$

 $a^2 = (e+1) l^2$, $b^2 = (e + Saa') l^2$, $c^2 = (e-1) l^2$; (K1)

whence
$$l^2 = \frac{a^2 - b}{2}, e = \frac{a^2 - b}{a^2 - e^2}$$

and the three vector semiaxes corresponding are,

$$a \mathbf{U} (\mathbf{a} + \mathbf{a}'), \quad b \mathbf{U} \mathbf{V} a \mathbf{a}', \quad c \mathbf{U} (\mathbf{a} - \mathbf{a}').$$
 (M₁)

(c). Rectangular, unifocal, and cyclic forms (pp. 197, 203, 205) of the scalar function $f\rho$, to each of which corresponds a form of the vector function $\phi\rho$; deduction, by a new

easy to assign the proper form, for the case of points, &c., at finite distances : and then having the additional trouble of reducing the complex expressions so found to simpler forms, in which differentials sball finally appear. In short, it is shown that in Quaternions, as in other parts of Analysis, the rigour of limits can be combined with the facility of infinitesimals.

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 (L_1)

in which,

whence

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analysis, of several known theorems * (pp. 197, 198, 202, 208) respecting confocal surfaces and their focal conics; the lines α , α' are asymptotes to the focal hyperbola (p. 202), whatever the species of the surface may be: references (in Notes to pp. 203, 204) to the Lectures, \dagger for the focal ellipse of the Ellipsoid, and for several different generations of this last surface.

(d). General Exponential Transformation (p. 206) of the equation of any central quadric;

$$\rho = x\alpha + y \nabla \alpha^t \beta, \quad (N_1), \quad \text{with } x^2 f \alpha + y^2 f U \nabla \alpha \alpha' = 1, \quad (N_1')$$

$$\beta = \frac{(a' - ea) \operatorname{UVaa'}}{e + \operatorname{Saa'}}; \qquad (N_1'')$$

this anxiliary vector β is constant, for any one confocal (e); the exponent, t, in (N_1) , is an arbitrary or variable scalar; and the coefficients, x and y, are two other scalar variables, which are however connected with each other by the relation (N_1') .

(e). If any fixed value be assigned to t, the equation (N_1) then represents the section made by a plane through α (p. 207) which section is an ellipse if the surface be an ellipsoid, but an hyperbola for either hyperboloid; and the cutting plane makes with the focal plane of α , α' , or with the plane of the focal hyperbola, an angle = $\frac{1}{2}t\pi$.

(f). If, on the other hand, we allow t to vary, but assign to x and y any constant ralues consistent with (N_1') , the equation (N_1) then represents an ellipse (p. 206) whatever the species of the surface may be; x represents the distance of its centre o of the surface, measured along the focal line a; y is the radius of a right cylinder, with a for its axis, of which the ellipse is a section, or the radius of a circle in a plane perpendicular to a, into which that ellipse can be orthogonally projected : and the angle $\frac{1}{2}t\pi$ is now the excentric anomaly. Such elliptic sections of a central quadric may be otherwise obtained from the unifocal form (c) of the equation of the surface; they are, in some points of view, almost as interesting as the known circular sections: and it is proposed (p. 204) to call them Centro-Focal Ellipses.

(g). And it is obvious that, by interchanging the two focal lines a, a' in (d) a Second Exponential Transformation is obtained, with a Second System of centro-focal ellipses, whereof the proposed surface is the locus, as well as of the first system (f), but which have their centres on the line a', and are projected into circles, on a plane perpendicular to this latter line (p. 203).

(h). Equation of Confocals (p. 207).

$$\nabla \nu_{\mu} \phi \nu_{\mu} = \nabla \nu \phi_{\mu} \nu. \tag{O1}$$

ARTICLE 408.—On Circumscribed Quadric Cones; and on the Umbilics of a central quadric,

(a). Equations (p. 209) of Conjugate Points, and of Conjugate Directions, with respect to the surface $f_{\rho} = 1$,

$$f(\rho, \rho') = 1$$
, (P₁), and $f(\rho, \rho') = 0$; (P₁')

Condition of Contact, of the same surface with the right line PP',

$$(f(\rho, \rho') - 1)^2 = (f\rho - 1) (f\rho' - 1);$$
 (Q₁)

this latter is also a form of the equation of the Cone, with vertex at P', which is *circumseribed* to the same quadric $(f\rho = 1)$.

* For example, it is proved by quaternions (p. 208), that the *focal lines* of the *focal cone*, which has any proposed point P for vertex, and rests on the focal hyperbola, are generating lines of the single-sheeted hyperboloid (of the given confocal system), which passes through that point: and an extension of this result, to the focal lines of any cone circumscribed to a confocal, is deduced by a similar analysis, in a subsequent Series (408, p. 213). But such known theorems respecting confocals can only be alluded to, in those Contents.

+ Lectures on Quaternions (by the present author), Dublin, Hodges and Smith, 1853.

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(b). The condition (Q_1) may also be thus transformed (p. 211),

$$F \nabla \rho \rho' = a^2 b^2 c^2 f(\rho - \rho'),$$
 (Q₁)

F being a scalar function, connected with f by certain relations of *reciprocity* (comp. p. 547, vol. i.); and a simple geometrical interpretation may be assigned, for this last equation.

(c). The Reciprocal Cone, or Cone of Normals σ at \mathbf{r}'_1 to the circumscribed cone (Q₁) or (Q₁), may be represented (p. 2I2) by the very simple equation,

$$F(\sigma: S\rho'\sigma) = 1; \qquad (Q_1'')$$

which likewise admits of an extremely simple interpretation.

(d). A given right line (p. 214) is touched by two confocals, and other known results are easy consequences of the present analysis; for example (pp. 216, 217), the cone circumscribed to any surface of the system, from any point of either of the two real focul curves, is a cone of revolution (real or imaginary): but a similar conclusion holds good, when the vertex is on the third (or imaginary) focal, and even more generally (p. 223), when that vertex is any point of the (known and imaginary) developable envelope of the confocal system.

(e). A central quadric has in general *Twelve Umbilics* (p. 218), whereof only *four* (at most) can be *real*, and which are its *intersections* with the *three focal curves*: and these *twolve points* are ranged, *three by three*, on *eight imaginary right lines* (p. 222), which *intersect the circle at infinity*, and which it is proposed to call the *Eight Umbilicar Generatrices* of the surface.

(f). These (imaginary) umbilicar generatrices of a quadric are found to possess several interesting properties, especially in relation to the lines of curvature: and their locus, for a confocal system, is a developable surface (p. 222), namely the known envelope (d) of that system.

ARTICLE 409.-Geodetic Lines on Central Surfaces of the Second Order, .

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(a). One form of the general differential equation of geodetics on an arbitrary surface being, by III. iii. 5 (p. 29),

 $V \nu d^2 \rho = 0$, (R₁), if $T d\rho = \text{const.}$, (R₁')

this is shown (p. 226) to conduct, for central quadrics, to the first integral,

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$$D^{-2}D^{-2} = \mathrm{T}\nu^2 f \mathrm{Ud}\rho = h = \mathrm{const.}; \qquad (S_1)$$

where P is the perpendicular from the centre o on the tangent plane, and D is the (real or imaginary) semidiameter of the surface, which is parallel to the tangent $(d\rho)$ to the curve. The known equation of Joachimstal, P.D = const., is therefore proved anew; this last constant, however, being by no means necessarily real, if the surface be not an ellipsoid.

(b). Deduction (p. 227) of a theorem of M. Chasles), that the tangents to a geodetic, on any one central quadric (e) touch also a common confocal (e); and of an integral (p. 228) of the form,

$$e_1 \sin^2 v_1 + e_2 \cos^2 v_1 = e_2 = \text{const.}, \tag{S_1'}$$

which agrees with one of M. Liouville.

(c). Without the restriction (R_1') , the differential of the scalar h in (S_1) may be thus decomposed into factors (p. 229).

$$dh = d \cdot P^{-2} D^{-2} = 2S \nu d\nu d\rho^{-1} \cdot S \nu d\rho^{-1} d^2 \rho ; \qquad (S_1'')$$

but, by the lately cited Section (III. iii. 5, p. 29), the differential equation of the second order,

$$S\nu d\rho d^2\rho = 0, \qquad (R_1'')$$

with an arbitrary scalar variable, represents the *geodetic lines* on any surface: the theorem (a) is therefore in this way reproduced.

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(d). But we see, at the same time, by (S_1'') , that the quantity h, or P. $D = h^{-1}$, is constant, not only for the geodetics on a central quadric, but also for a certain other set of curves, determined by the differential equation of the first order, $S\nu d\nu d\rho = 0$, which will be seen, in the next Series, to represent the lines of curvature.

(a). The differential equation (comp. 409, (d)),

$$\mathbf{S} \boldsymbol{\nu} \mathbf{d} \boldsymbol{\nu} \mathbf{d} \boldsymbol{\rho} = 0, \tag{T_1}$$

represents (p. 229) the Lines of Curvature upon an arbitrary surface; because it is a limiting form of this other equation,

$$S\nu\Delta\nu\Delta\rho = 0,$$
 (T₁')

which is the condition of intersection (or of parallelism), of the normals drawn at the extremities of the two vectors ρ and $\rho + \Delta \rho$.

(b). The normal vector \mathbf{v} , in the equation (T₁) may be multiplied (pp. 237, 275) by any constant or variable scalar *n*, without any real change in that equation; but in this whole theory, of the treatment of *Curvatures of Surfaces* by Quaternions, it is advantageous to consider the expression $S\nu d\rho$ as denoting the *exact differential* of some scalar function of ρ ; for then (by p. 553, vol. i.) we shall have an equation of the form,

$$d\nu = \phi d\rho = a \ self-conjugate \ function \ of \ d\rho, \tag{U1}$$

which usually involves ρ also. For instance, we may write generally (p. 233, comp. (R), p. xxxii, vol. i.),

 $\mathrm{d}\nu = g\mathrm{d}\rho + \mathrm{V}\lambda\mathrm{d}\rho\mu \; ; \qquad \qquad (\mathrm{U}_{1}')$

the scalar g, and the vectors λ , μ being *real*, and being *generally*^{*} functions of ρ , but not involving $d\rho$.

(c). This being understood, the two† directions of the tangent $d\rho$, which satisfy at once the general equation (T₁) of the lines of curvature, and the differential equation $S\nu d\rho = 0$ of the surface, are easily found to be represented by the two vector expressions (p. 233),

$$\mathbf{U}\mathbf{V}\boldsymbol{\nu}\boldsymbol{\lambda} \pm \mathbf{U}\mathbf{V}\boldsymbol{\nu}\boldsymbol{\mu}; \qquad (\mathbf{T}_{1}'')$$

they are therefore generally *rectangular* to each other, as they have long been known to be.

(d). The surface itself remaining still quite arbitrary, it is found useful to introduce the conception of an Auxiliary Surface of the Second Order (p. 234), of which the variable vector is $\rho + \rho'$, and the equation is,

$$S\rho'\phi\rho' = g\rho'^2 + S\lambda\rho'\mu\rho' = 1, \qquad (U_i'')$$

or more generally = const.; and it is proposed to call this surface, of which the centre is at the given point P, the *Index Surface*, partly because its diametral section, made by the tangent plane to the given surface at P, is a certain *Index Curve* (p. 231), which may be considered to coincide with the known "indicatrice" of Dupin.

(e) The expressions (T_1'') show (p. 234), that whatever the given surface may be, the tangents to the lines of curvature bisect the angles formed by the traces of the two

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^{*} For the case of a central quadric, g, λ , μ are constants.

⁺ Generally two; but in some cases more. It will soon be seen, that three lines of curvature pass through an umbilie of a quadric.

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eyclic planes of the Index Surface (d), on the tangent plane to the given surface; these two tangents have also (as was seen by Dupin) the directions of the axes of the Index Curve (p. 231); and they are distinguished (as he likewise saw) from all other tangents to the given surface, at the given point P, by the condition that each is perpendicular to its own conjugate, with respect to that indicating curve: the equation of such conjugation, of two tangents τ and τ' , being in the present notation (see again p. 232),

$$S\tau\phi\tau'=0, \text{ or } S\tau'\phi\tau=0.$$
 (U_1''')

(f). New proof (p. 232) of another theorem of Dupin, namely that if a developable be circumscribed to any surface, along any curve thereon, its generating lines are everywhere conjugate, as tangents to the surface, to the corresponding tangents to the curve.

(g). Case of a central quadric; new proof (p. 235) of still another theorem of Dupin, namely that the curve of orthogonal intersection (p. 198) of two confocal surfaces, is a line of curvature on each.

(h). The system of the eight umbilicar generatrices (408, (e)), of a central quadric, is the imaginary envelope of the lines of curvature on that surface (p. 235); and each such generatrix is itself an imaginary line of curvature thereon: so that through each of the twelve umbilics (see again 408, (e)) there pass three lines of curvature (comp. p. 242) whereof however only one, at most, can be real: namely two generatrices, and a principal section of the surface. These last results, which are perhaps new, will be illustrated, and otherwise proved, in the following Series (411).

ARTICLE 411.—Additional illustrations and confirmations of the foregoing theory, for the case of a Central^{*} Quadric; and especially of the theorem respecting the Three Lines of Curvature through an Umbilic, whereof two are always imaginary and rectilinear,

(a). The general equation of condition (T_1') or $S\nu\Delta\nu\Delta\rho = 0$, for the intersection of two finitely distant normals, may be easily transformed for the case of a quadric, so as to express (p. 240) that when the normals at P and P' intersect (or are parallel) the chord PP' is perpendicular to its own polar.

(b). Under the same conditions, if the point \mathbf{P} be given, the locus of the chord $\mathbf{Pr'}$ is usually (p. 241) a quadric cone, say (C); and therefore the locus of the point $\mathbf{P'}$ is usually a quartic curve, with \mathbf{P} for a double point, whereat two branches of the curve cut each other at right angles, and touch the two lines of curvature.

(c). If the point \mathbf{r} be one of a principal section of the given surface, but not an umbilic, the cone (C) breaks up into a pair of planes, whereof one, say (P), is the plane of the section, and the other, (P), is perpendicular thereto, and is not tangential to the surface; and thus the quartic (b) breaks up into a pair of conics through \mathbf{P} , whereof one is the principal section itself, and the other is perpendicular to it.

(d). But if the given point P be an umbilic, the second plane (P') becomes a tangent plane to the surface; and the second conic (c) breaks up, at the same time, into a pair of imaginary \dagger right lines, namely the two umbilicar generatrices through P (pp. 242, 245).

(e). It follows that the normal PN at a real umbilic \mathbf{r} (of an ellipsoid, or a doublesheeted hyperboloid) is not intersected by any other real normal, except those which are in the same principal section; but that this real normal PN is intersected, in an imaginary sense, by all the normals $\mathbf{r}'\mathbf{n}'$, which are drawn at points \mathbf{r}' of either of the two

* Many, indeed most, of the results apply, without modification, to the case of the *Paraboloids*; and the rest can easily be adapted to this latter case, by the consideration of infinitely distant points. We shall therefore often, for conciseness, omit the term *central*, and simply speak of *quadrics*, or surfaces of the *second order*.

+ It is well known that the single-sheeted hyperboloid, which (alone of central quadrics) has real generating lines, has at the same time no real umbilies (comp. p. 221).

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imaginary generatrices through the real umbilie P; so that each of these imaginary right lines is seen anew to be a line^{*} of curvature, on the surface (comp. 410, (h)), because all the normals P'N', at points of this line, are situated in one common (imaginary) normal plane (p. 242): and as before, there are thus three lines of curvature through an umbilic.

(f). These geometrical results are in various ways deducible from calculation with quaternions; for example, a form of the equation of the lines of curvature on a quadric is seen (p. 242) to become an *identity* at an umbilic $(\nu \parallel \lambda)$: while the *differential* of that equation breaks up into two *factors*, whereof one represents the tangent to the *principal* section, while the other $(S\lambda d^2\rho = 0)$ assigns the directions of the *two generatrices*.

(g). The equation of the cone (C), which has already presented itself as a certain locus of chords (b), admits of many quaternion transformations; for instance (see p. 240), it may be written thus,

$$\frac{S\alpha\rho\Delta\rho}{S\alpha\Delta\rho} + \frac{S\alpha'\rho\Delta\rho}{S\alpha'\Delta\rho} = 0, \qquad (V_1)$$

 ρ being the vector of the vertex P, and $\rho + \Delta \rho$ that of any other point r' of the cone; while α , α' are still, as in 407, (a), two real *focal lines*, of which the *lengths* are *here* arbitrary, but of which the directions are constant, as before, for a whole confocal system.

(h). This cone (C), or (V_1) , is also the *locus* (p. 244) of a system of *three rectangular lines*; and if it be cut by any plane perpendicular to a side, and not passing through the vertex, the *section* is an *equilateral hyperbola*.

(i). The same cone (C) has, for three of its sides PF', the normals (p. 243) to the three confocals (p. 197) of a given system which pass through its vertex r; and therefore also, by 410, (g), the tangents to the three lines of curvature through that point, which are the intersections of those three confocals.

(j). And because its equation (V_1) does not involve the constant l, of 407, (a), (b), we arrive at the following theorem (p. 243):—If indefinitely many quadrics, with a common centre 0, have their asymptotic cones biconfocal, and pass through a common point P. their normals at that point have a quadric cone (C) for their locus.

ARTICLE 412.—On Centres of Curvature of Surfaces,

(a). If σ be the vector of the centre s of curvature of a normal section of an arbitrary

* It might be natural to suppose, from the known general theory (410, (c)) of the two rectangular directions, that each such generatrix Pr' is crossed perpendicularly, at every one of its non-umbilicar points P', by a second (and distinct, although imaginary) line of curvature. But it is an almost equally well known and received result of modern geometry, paradoxical as it must at first appear, that when a right line is directed to the circle at infinity, as (by 408, (e)) the generatrices in question are, then this imaginary line is everywhere perpendicular to itself. Compare the Notes to pages 516 vol. i., 236. Quaternions are not at all responsible for the introduction of this principle into geometry, but they recognise and employ it, under the following very simple form : that if a non-evanescent vector be directed to the circle at infinity, it is an imaginary value of the symbol 0² (comp. pp. 316, 516 vol. i., 222, 236); and conversely, that when this last symbol represents a vector which is not null, the vector thus denoted is an imaginary line, which cuts that circle. It may be noted here, that such is the case with the reciprocal polar of every chord of a quadric, connecting any two umbilies which are not in one principal plane; and that thus the quadratic equation (XXI., in p. 233) from which the two directions (410, (c)) can usually be derived, becomes an identity for every umbilic, real or imaginary : as it ought to do, for consistency with the foregoing theory of the three lines through that umbilic. And as an additional illustration of the coincidence of directions of the lines of curvature at any non-umbilicar point r' of an umbilicar generatrix, it may be added that the cone of chords (C), in 411, (b), is found to touch the quadric along that generatrix, when its vertex is at any such point P'.

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surface, which touches one of the two lines of curvature thereon, at any given point P, we have the two fundamental equations (p. 247),

$$\sigma = \rho + R U \nu$$
, (W₁), and $R^{-1} d\rho + d U \nu = 0$; (W₁')

whence

$$Vd\rho dU_{\nu} = 0$$
, (W_1'') , and $\frac{T_{\nu}}{R} + S \frac{d\nu}{d\rho} = 0$; (W_1'')

the equation (W_1'') being a new form of the general differential equation of the lines of curvature.

(b). Deduction (pp. 248, 249, &c.) of some known theorems from these equations; and of some which introduce the new and general conception of the *Index Surfac* (410, (d)), as well as that of the known *Index Curve*.

(c). Introducing the auxiliary scalar (p. 251),

$$r = \frac{\mathrm{T}\nu}{R} = -\mathrm{S}\,\frac{\mathrm{d}\nu}{\mathrm{d}\rho} = -\mathrm{S}\tau^{-1}\,\phi\tau,\tag{X}_1$$

in which $\tau (\parallel d\rho)$ is a tangent to a line of curvature, while $d\nu = \phi d\rho$, as in (U₁), the two values of r, which answer to the two rectangular directions (T₁") in 410, (c), are given (p. 248) by the expression,

$$r = -g - T\lambda\mu \cdot \cos\left(\angle \frac{\nu}{\lambda} \mp \angle \frac{\nu}{\mu}\right),$$
 (X₁')

in which g, λ , μ are, for any given point \mathbf{P} , the constants in the equation (\mathbf{U}_1'') of the *index surface*; the *difference* of the *two curvatures* R^{-1} therefore *vanishes at an umbilic* of the given surface, whatever the form of that surface may be: that is, at a point, where $v \parallel \lambda$ or \parallel \mu, and where consequently the *index curve* is a circle.

(d). At any other P of the given surface, which is as yet entirely arbitrary, the values of r may be thus expressed (p. 249),

$$r_1 = a_1^{-2}, \quad r_2 = a_2^{-2},$$
 (X1")

a₁, a₂ being the scalar semiazes (real or imaginary) of the index curve (defined, comp. 410, (d), by the equations $S_{\rho'}\phi_{\rho'} = 1$, $S_{\nu\rho'} = 0$).

(e). The quadratic equation, of which r_1 and r_2 , or the inverse squares of the two last semiaxes, are the roots, may be written (p. 252) under the symbolical form,

$$S\nu^{-1} (\phi + r)^{-1}\nu = 0; \qquad (Y_1)$$

which may be developed (same page) into this other form,

$$r^{2} + r S \nu^{-1} \chi \nu + S \nu^{-1} \psi \nu = 0, \qquad (Y_{1})$$

the linear and vector functions, ψ and χ , being devived from the function ϕ , on the plan of the Section III. ii. 6 (pp. 489, 494, vol. i).

(f). Hence, generally the product of the two curvatures of a surface is expressed (p. 253) by the formula

$$R_{\mathbf{I}}^{-1}R_{\mathbf{2}}^{-1} = r_{\mathbf{1}}r_{\mathbf{2}} \operatorname{T} \nu^{-2} = -S\frac{1}{\nu}\psi \frac{1}{\nu}; \qquad (\mathbf{Z}_{\mathbf{1}})$$

which will be found useful in the following series (413), in connexion with the theory of the Measure of Curvature.

xxiii Pages (g). The given surface being still quite general, if we write (p. 256),

$$\tau = \mathrm{Ud}\rho, \ \tau' = \mathrm{U}(\nu \mathrm{d}\rho), \ (\mathrm{A}_2), \ \mathrm{and} \ \mathrm{therefore} \ \tau\tau' = \mathrm{U}\nu, \ (\mathrm{A}_2')$$

so that τ and τ' are unit tangents to the lines of curvature, it is easily proved that

$$d\tau' = \tau \ S\tau' d\tau$$
, (B₂), or that $V\tau d\tau' = 0$; (B₂')

this general parallelism of $d\tau'$ to τ being geometrically explained, by obverving that a line of curvature on any surface is, at the same time, a line of curvature on the developable normal surface, which rests upon that line, and to which τ' or $\nu\tau$ is normal, if τ be tangential to the line.

(h). If the vector of curvature (389) of a line of curvature be projected on the normal ν to the given surface, the projection (p. 257) is the vector of curvature of the normal section of that surface, which has the same tangent τ ; but this result, and an analogous one (same page) for the developable normal surface (g), are virtually included in Meusnier's theorem, which will be proved by quaternions in Series 414.

(i). The vector σ of a centre of curvature of the given surface, answering to a given point P thereon, may (by (W₁) and (X₁)) be expressed by the equation,

$$\sigma = \rho + r^{-1} \nu; \tag{C_2}$$

which may be regarded also as a general form of the Vector Equation of the Surface of Centres, or of the locus of the centre s: the variable vector ρ of the point r of the given surface being supposed (p. 11) to be expressed as a vector function of two independent and scalar variables, whereof therefore ν , r, and σ become also functions, although the two last involve an ambiguous sign, on account of the Two Sheets of the surface of centres.

(j). The normal at s, to which may be called the First Sheet, has the direction of the tangent τ to what may (on the same plan) be called the First Line of Curvature at P; and the vector v of the point corresponding to s, on the corresponding sheet of the Reciprocal (comp. pp. 19, 20) of the Surfaces of Centres, has (by p. 254) the expression,

$$v = \tau \, (\mathrm{S}\rho\tau)^{-1} \,; \tag{D}_2$$

which may also be considered (comp. (i)) to be a form of the Vector Equation of that Reciprocal Surface.

(k). The vector v satisfies generally (p. 254) the equations of reciprocity,

$$Sv\sigma = S\sigma v = 1$$
, $Sv\delta\sigma = 0$, $S\sigma\delta v = 0$, (D_2')

 $\delta\sigma$, $\delta\nu$ denoting any infinitesimal variations of the vectors σ and ν , consistent with the equations of the surface of centres and its reciprocal, or any *linear* and *vector elements* of those two surfaces, at two corresponding points; we have also the relations (p. 255),

$$S_{0}v = 1$$
, $S_{V}v = 0$, $S_{V}v\phi v = 0$. (D_2'')

(1). The equation $Sv(\omega - \rho) = 0$, or more simply,

$$Sv\omega = 1,$$
 (E₂)

in which ω is a variable vector, represents (p. 254) the normal plane to the first line (j) of curvature at P; or the tangent plane at s to the first sheet of the surface of centres: or finally, the tangent plane to that developable normal surface (g), which rests upon the the second line of curvature, and touches the first sheet along a certain curve, whereof we shall shortly meet with an example. And if ν be regarded, comp. (i), as a vector function of two scalar variables, the envelope of the variable plane (E₂) is a sheet of the

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surface of centres; or rather, on account of the ambiguous sign(i), it is that surface of centres *itself*; while, in like manner, the *reciprocal surface* (j) is the *envelope* of this other plane,

$$S\sigma\omega = 1.$$
 (E₂')

(m). The equations (W_1) , (W_1') give (comp. the Note to p. 254),

$$d\sigma = dR. \ U\nu:$$
 (F₂)

combining which with (C₂), we see that the equations (H₁) of p. xvi are satisfied, when the derived vectors ρ' and σ' are changed to the corresponding differentials, $d\rho$ and $d\sigma$. The known theorem (of Monge), that each *Line of Curvature* is generally an *involute*, with the corresponding *Curve of Centres* for one of its *evolutes* (400), is therefore in this way reproduced: and the connected theorem (also of Monge), that *this evolute* is a geodetic on *its own sheet* of the surface of centres, follows easily from what precedes.

(n). In the foregoing paragraphs of this analysis, the given surface has throughout been arbitrary, or general, as stated in (d) and (g). But if we now consider specially the case of a central quadric, several less general but interesting results arise, whereof many, but perhaps not all, are known; and of which some may be mentioned here.

(o). Supposing, then, that not only $d\nu = \phi d\rho$, but also $\nu = \phi \rho$, and $S\rho\nu = f\rho = 1$, the *Index Surface* (410, (d)) becomes simply (p. 233) the given surface, with its centre transported from 0 to P; whence many simplications follow.

(p). For example, the semiaxes a_1 , a_2 of the *index curve* are now equal (p. 249) to the semiaxes of the *diametral section* of the given surface, made by a plane parallel to the tangent plane; and $T_{\mathbf{r}}$ is, as in 409, the reciprocal P^{-1} of the perpendicular, from the centre on this latter plane; whence (by (X_1) and X_1'')) these known expressions for the two* curvatures result:

$$R_1^{-1} = Pa_1^{-2}; \quad R_2^{-1} = Pa_2^{-2}.$$
 (G₂)

(q). Hence, by (e), if a new surface be derived from a given central quadric (of any species), as the locus of the extremities of normals erected at the centre, to the planes of diametral sections of the given surface, each such normal (when real) having the length of one of the semiaxes of that section, the equation of this new surface[†] admits (p. 253) of being written thus:

$$S\rho(\phi - \rho^{-2})^{-1}\rho = 0.$$
 (H₂)

(r). Under the conditions (o), the expression (C₂) for σ gives (p. 254) the two converse forms,

$$\sigma = r^{-1}(\phi + r)\rho, \quad (I_2), \quad \rho = r (\phi + r)^{-1}\sigma; \quad (I'_2)$$

whence (pp. 254, 260),

$$\nu = r (\phi + r)^{-1} \phi \sigma, \quad (J_2), \quad \sigma = (\phi^{-1} + r^{-1}) \nu; \qquad (J_2')$$

and therefore (p. 260), by (d), (p), and by the theory (407) of confocal surfaces,

$$\sigma_1 = \phi_2^{-1} \nu = \phi_2^{-1} \phi \rho, \tag{K}_2$$

• Throughout the present series 412, we attend only (comp. (a)) to the curvatures of the *two* normal sections of a surface, which have the directions of the *two lines* of curvature: these being in fact what are always regarded as the *two principal curvatures* (or simply as *the* two curvatures) of the *swrface*. But, in a shortly subsequent Series (414), the more general case will be considered, of the curvature of *any section*, normal or oblique.

 \dagger When the given surface is an ellipsoid the derived surface is the celebrated Wave Surface of Fresnel: which thus has (H₂) for a symbolical form of its equation. When the given surface is an hyperboloid, and a semiaxis of a section is imaginary, the (scalar and now positive) square, of the (imaginary) normal crected, is still to be made equal to the square of that semiaxis.

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XXV Pages if ϕ_2 be formed from ϕ by changing the semiaxes *abe* to $a_2b_2c_2$; it being understood that the given quadric (*abe*) is cut by the two confocals ($a_1b_1c_1$) and ($a_2b_2c_2$), in the *first* and *second lines* of curvature through the given point F: and that σ_1 is here the vector of that *first centre* s of curvature, which answers to the *first line* (comp. (*j*)). Of course, on the same plan, we have the analogous expression,

$$\sigma_2 = \phi_1^{-1} \nu = \phi_1^{-1} \phi_\rho, \tag{K}_2)$$

for the vector of the second centre.

(s). These expressions for σ_1 , σ_2 include (p. 260) a theorem of Dr. Salmon, namely that the centres of curvature of a given quadric at a given point are the poles of the tangent plane, with respect to the two confocals through that point; and either of them may be regarded, by an admission of an ambiguous sign (comp. (i)), as a new Vector Form* of the Equation of the Surface of Centres, for the case (o) of a given central quadric.

(t). In connexion with the same expressions for σ_1 , σ_2 , it may be observed that if r_1 , r_2 be the corresponding values of the auxiliary scalar r in (c), and if τ , τ' still denote the unit tangents (g) to the first and second lines of curvature, while *abc*, $a_1b_1c_1$, and $a_2b_2c_2$ retain their recent significations (r), then (comp. pp. 257, 258, see also p. 208),

$$r_1 = f \tau = f \operatorname{Ud} \rho = (a^2 - a_2^2)^{-1} = \&c., \tag{L}_2$$

$$r_2 = f \tau' = f \, \mathrm{U} \nu \mathrm{d} \rho = (a^2 - a_1^2)^{-1} = \& \mathrm{c.};$$
 (L2')

this association of r_1 and σ_1 with a_2 , &c., and of r_2 and σ_2 with a_1 , &c., arising from the circumstance that the *tangents* τ and τ' have respectively the directions of the normals ν_2 and ν_1 , to the two confocal surfaces, $(a_2b_2c_2)$ and $(a_1b_1c_1)$.

(*n*). By the properties of such surfaces, the scalar here called r_2 is therefore *constant*, in the whole extent of a *first line* of curvature; and the same *constancy* of r_2 , or the equation,

$$\mathrm{d}f\,\mathrm{U}\nu\mathrm{d}\rho=0,\tag{M}_2$$

may in various ways be proved by quaternions (p. 258).

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(v). Writing simply r and r' for r_1 and r_2 , so that r' is constant, but r variable, for a *first line* of curvature, while conversely r is constant and r' variable for a second line, it is found (pp. 254, 255, 256), that the scalar equation of the surface of centres (i) may be regarded as the result of the elimination of r^{-1} between the two equations,

$$1 = S.\sigma (1 + r^{-1}\phi)^{-2}\phi\sigma, \quad (N_2), \text{ and } 0 = S.\sigma (1 + r^{-1}\phi)^{-3}\phi^2\sigma; \quad (N_2')$$

whereof the latter is the derivative of the former with respect to the scalar r^{-1} . It follows (comp. p. 259), that the First Sheet of the Surface of Centres is touched by an Auxiliary Quadrie (N₂), along a Quartie Curve (N₂) (N₂'), which curve is the Locus of the Centres of First Curvature, for all the points of a Line of Second Curvature; the same sheet being also touched (see again p. 259), along the same curve, by the developable normal surface (l), which rests on the same second line: with permission to interchange the words, first and second, throughout the whole of this enunciation.

(w). The given surface being still a central quadric (o), the vectors ρ , σ , ν can be expressed as functions of ν (comp. (j) (k) (l)), and conversely the latter can be expressed as a function of any one of the former; we have, for example, the reciprocal equations (p. 256),

 $\sigma = (1 + r^{-1}\phi)^2 \phi^{-1}v, \quad (O_2), \quad \text{and} \quad v = (1 + r^{-1}\phi)^{-2} \phi \sigma; \quad (O_2')$

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^{*} Dr. Salmon's result, that this surface of centres is of the *twelfth degree*, may be easily deduced from this form.

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from which last the formula (N_2) may be obtained anew, by observing (k) that $S\sigma v = 1$. Hence also, by (r), we can infer the expressions,*

$$\rho = (\phi^{-1} + r^{-1}) \ v = \phi_2^{-1} \ v, \quad (P_2), \text{ and } v = \phi_2 \ \rho = \nu_2; \quad (P_2')$$

and in fact it is easy to see otherwise (comp. p. 198), that $\nu_2 \parallel \tau \parallel \nu$, and $S_{\rho\nu_2} = 1 = S_{\rho\nu}$, whence $\nu_2 = \nu$ as before.

(x). More fully, the two sheets of the reciprocal (j) of the surface of centres may have their separate vector equations written thus,

$$v_1 = \phi_2 \rho = v_2, \quad v_2 = \phi_1 \rho = v_1;$$
 (P₂")

and the scalar equation \dagger of this reciprocal surface itself, considered as including both sheets, may (by page 255) be thus written, the functions f and F being related as in 408, (b),

$$v^4 = (Fv - 1) fv, (Q_2)$$

with several equivalent forms; one way of obtaining this equation being the elimination of r between the two following (same p. 256):

$$Fv + r^{-1}v^2 = 1$$
, (Q_2') ; $fv + rv^2 = 0$. (Q_2'')

(y). The two last equations may also be written thus, for the *first sheet* of the reciprocal surface,

$$F_2 v_1 = 1$$
, (R₂), and $f U v_1 = r$, (R₂')

in which (comp. pp. 255, 260),

$$F_2 v = S v \phi_2^{-1} v = S v (\phi^{-1} + r^{-1}) v; \qquad (R_2'')$$

and accordingly (comp. pp. 548, vol. i, 199), we have $F_2\nu_2 = F\nu = 1$, and $f U\nu_2 = f\tau = r$.

(z). For a line of second curvature on the given surface, the scalar r is constant, as before; and then the two equations (Q_2') , (Q_2'') , or (R_2) , (R_2') , represent jointly (comp. the slightly different enunciation in p. 259) a certain quartic curve, in which the quadric reciprocal (R_2) , of the second confocal $(a_2 b_2 c_2)$, intersects the first sheet (y) of the Reciprocal Surface (Q_2) ; this quartic curve, being at the same time the intersection of the quadric surface (Q_2') or (R_2) , with the quadric cone (Q_2'') or (R_2') , which is biconcyclic with the given quadric, f p = 1.

ARTICLE 413.—On the Measure of Curvature of a Surface,

The object of this short Series 413 is the deduction by quaternions, somewhat more briefly and perhaps more clearly than in the *Lectures*, of the principal results of Gauss (comp. Note to p. 261), respecting the *Measure of Curvature of a Surface*, and questions therewith connected.

(a). Let P, P1, P2 be any three near points on a given but arbitrary surface, and R, R1, R2 the three corresponding points (near to each other) on the unit sphere, which are determined by the parallelism of the radii OR, OR1, OR2 to the normals PN, P1N1, P2N2; then the areas of the two small triangles thus formed will bear to each other the ultimate ratio (p. 262),

$$\lim. \frac{\Delta R R_1 R_2}{\Delta P P_1 P_2} = \frac{V \cdot dU \nu \delta U \nu}{V d \rho \delta \rho} = -S \frac{1}{\nu} \psi \frac{1}{\nu}; \qquad (S_2)$$

* The equation $\nu = \nu_2$, = the normal to the confocal $(a_2 b_2 c_2)$ at ν , is not actually given in the text of Series 412; but it is easily deduced, as above, from the formulæ and methods of that Series.

[†] The equation (Q₂) is one of the *fourth degree*; and, when expanded by coordinates, it agrees perfectly with that which was first assigned by Dr. Booth (see a Note to p. 255), for the *Tangential Equation* of the *Surface of Centres* of a quadric, or for the Cartesian equation of the *Reciprocal Surface*.

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 (T_2')

whence, with Gauss's definition of the measure of curvature, as the ultimate ratio of corresponding areas on surface and sphere, we have, by the formula (Z_1) in 412, (f), his fundamental theorem,

Measure of Curvature =
$$R_1^{-1} R_2^{-1}$$
, (S₂)

= Product of the two Principal Curvatures of Sections.

(b). If the vector ρ of the surface be considered as a function of two scalar variables, t and u, and if derivations with respect to these be denoted by upper and lower accents, this general transformation results (p. 263),

Measure of Curvature =
$$S \frac{\rho''}{\nu} S \frac{\rho_u}{\nu} - \left(S \frac{\rho'_s}{\nu}\right)^2$$
 (T2)

in which

with a verification for the notation pqrst of Monge.

(c). The square of a linear element ds_i of the given but arbitrary surface, may be expressed (p. 263) as follows:

 $\nu = V \rho' \rho_i;$

$$ds^{2} = (Td\rho^{2} =)edt^{2} + 2fdtdu + gdu^{2};$$
 (U₂)

and with the recent use (b) of accents, the *measure* (T_2) is proved (same page) to be an explicit function of the ten scalars,

$$e, f, g; e', f', g'; e_0, f_0, g_1; \text{ and } e_0 - 2f_0' + g'';$$
 (U₂)

the form of this function (p. 264) agreeing, in all its details, with the corresponding expression assigned by Gauss. *

(d). Hence follow at once (p. 264) two of the most important results of that great mathematician on this subject; namely, that every Deformation of a Surface, consistent with the conception of it as an infinitely thin and flexible but inextensible solid, leaves unaltered, 1st, the Measure of Curvature at any Point, and IInd, the Total Curvature of any Area: this last being the area of the corresponding portion (a) of the unit-sphere.

(e). By a suitable choice of t and u, as certain geodetic co-ordinates, the expression (U_2) may be reduced (p. 264) to the following,

$$ds^2 = dt^2 + n^2 du^2; (U_2'')$$

where t is the length of a geodetic arc AP, from a fixed point A to a variable point P of the surface, and u is the angle BAP which this variable arc makes with a fixed geodetic AB: so that in the immediate neighbourhood of A, we have n=t, and $n'=D_t n=1$.

(f). The general expression (c) for the measure of curvature takes thus the very simple form (p. 264),

$$R_1^{-1}R_2^{-1} = -n^{-1}n'' = -n^{-1}D_t^2n; \qquad (V_2)$$

and we have (comp. (d)) the equation (p. 265),

Total Curvature of Area
$$APQ = \Delta u - (n'du;$$
 (V2)

this area being bounded by two geodetics, AP and AQ, which make with each other an angle $= \Delta u$, and by an are PQ of an arbitrary curve on the given surface, for which t, and therefore n', may be conceived to be a given function of u.

^{*} References are given, in Notes to pp. 261, &c. of the present Series 413, to the pages of Gauss's beautiful Memoir, "Disquisitiones generales circa Superficies Curvas," as reprinted in the Additions to Liouville's Monge.

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(g). If this arc PQ be itself a geodetic, and if we denote by v the variable angle which it makes at P with AP prolonged, so that $\tan v = ndu$: dt, it is found that dv = -n'du; and thus the equation (V₂') conducts (p. 266) to another very remarkable and general theorem of Gauss, for an arbitrary surface, which may be thus expressed,

Total Curvature of a Geodetic Triangle
$$ABC = A + B + C - \pi$$
, (V_2')

= what may be called the Spheroidal Excess of that triangle, the total area (4π) of the unit-sphere being represented by eight right angles : with extensions to Geodetic Polygons, and modifications for the case of what may on the same plan be called the Spheroidal Defect, when the two curvatures of the surface are oppositely directed.

ARTICLE 414.—On Curvature of Sections (Normal and Oblique) of Surfaces; and on Geodetic Curvatures,

(a). The curvatures considered in the two preceding Series having been those of the principal normal sections of a surface, the present Series 414 treats briefly the more general case, where the section is made by an arbitrary plane, such as the osculating plane at P to an arbitrary curve upon the surface.

(b). The vector of curvature (389) of any such curve or section being $(\rho - \kappa)^{-1} = D_s^2 \rho_r$, its normal and tangential components are found to be (p. 267),

$$(\rho - \sigma)^{-1} = \nu^{-1} S \frac{d\nu}{d\rho} = (\rho - \sigma_1)^{-1} \cos^2 v + (\rho - \sigma_2)^{-1} \sin^2 v, \qquad (W_2)$$

$$(\rho - \xi)^{-1} = \nu^{-1} d\rho^{-1} S \nu d\rho^{-1} d^2 \rho ; \qquad (W_2')$$

the former component being the Vector of Normal Curvature of the Surface, for the direction of the tangent to the curve: and the latter being the Vector of Geodetic Curvature of the same Curve (or section).

(c). In the foregoing expressions, σ and ξ are the vectors of the points s and x, in which the axis of the osculating circle to the curve intersects respectively the normal and the tangent plane to the surface (p. 267); s is also the centre of the sphere, which osculates to the surface in the direction dp of the tangent; σ_1 , σ_2 are the vectors of the two centres s1, s2, of curvature of the surface, considered in Series 412, which are at the same time the centres of the two osculating spheres, of which the curvatures are (algebraically) the greatest and least: and v is the angle at which the curve here considered crosses the first line of curvature.

(d). The equation (W_2) contains a theorem of Euler, under the form (p. 268),

$$R^{-1} = R_1^{-1} \cos^2 v + R_2^{-1} \sin^2 v ; \qquad (W_2'')$$

it contains also Meusnier's theorem (same page), under the form (comp. 412, (h)) that the vector of normal curvature (b) of a surface, for any given direction, is the projection on the normal v, of the vector of oblique curvature, whatever the inclination of the plane of the section to the tangent plane may be.

(e). The expression (W_2') for the vector of geodetic curvature, admits (p. 271) of various transformations, with corresponding expressions for the radius $T(\rho - \xi)$ of geodetic curvature, which is also the radius of plane curvature of the developed curve, when the developable circumscribed to the given surface along the given curve is unfolded into a plane: and when this radius is constant, so that the developed curve is a circle, or part of one, it is proposed (p. 271), to call the given curve a Didonia (as in the Lectures), from its possession of a certain isoperimetrical property, which was first considered by M. Delaunay, and is represented in quaternions by the formula (p. 271),

$$[S(U\nu . d\rho\delta\rho) + c\delta]Td\rho = 0; \qquad (X_2)$$

$$c^{-1}\mathrm{d}\rho = \mathrm{V}(\mathrm{U}\nu \cdot \mathrm{d}\mathrm{U}\mathrm{d}\rho),\tag{X'_2}$$

by the rules of what may be called the Calculus of Variations in Quaternions: c being a constant, which represents generally (p. 272) the radius of the developed circle, and becomes infinite for geodetic lines, which are thus included as a case of Didonias.

and

or

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ARTICLE 415.—Supplementary Remarks, .

(a). Simplified proof (referred to in a Note to p. xxxii, vol. i.), of the general existence of a system of *three real and rectangular directions*, which satisfy the vector equation $V\rho\phi\rho = 0$, (P), when ϕ is a linear, vector, and *self-conjugate* function; and of a system of *three real roots* of the cubic equation M = 0 (p. xxxii, vol. i.), under the same condition (pp. 272-274).

(b). It may happen (p. 276) that the differential equation,

$$S\nu d\rho = 0,$$
 (Y₂)

is integrable, or represents a system of surfaces, without the expression $Svd\rho$ being an exact differential, as it was in 410, (b). In this case, there exists some scalar factor, n, such that $Snvd\rho$ is the exact differential of a scalar function of ρ , without the assumption that this vector ρ is itself a function of a scalar variable, t; and then if we write (p. 276, comp. p. xx),

$$d\nu = \phi d\rho, \quad d \cdot n\nu = \Phi d\rho, \tag{Y2'}$$

this new vector function Φ will be self-conjugate, although the function ϕ is not such now, as it was in the equation (U₁).

(c). In this manner it is found (p. 277), that the Condition* of Integrability of the equation (Y_2) is expressed by the very simple formula,

$$S\gamma\nu = 0; \qquad (Y_2'')$$

in which γ is a vector function of ρ , not generally linear, and deduced from ϕ on the plan of the Section III. ii. 6 (p. 492, vol. i), by the relation,

$$\phi d\rho - \phi' d\rho = 2V \gamma d\rho ; \qquad (Y_2'')$$

 ϕ' being the conjugate of ϕ , but not here equal to it.

(d). Connexions (pp. 278, 279) of the Mixed Transformations in the last cited Section, with the known Modular and Umbilicar Generations of a surface of the second order.

(e). The equation (p. 279),

$$T(\rho - V \cdot \beta V \gamma a) = T(a - V \cdot \gamma V \beta \rho), \qquad (Z_2)$$

in which a, β , γ are any three vector constants, represents a central quadric, and appears to offer a new mode of generation \dagger of such a surface, on which there is not room to enter, at this last stage of the work.

(f). The vector of the centre of the quadric, represented by the equation $f\rho - 2S\epsilon\rho = \text{const.}$, with $f\rho = S\rho\phi\rho$, is generally $\kappa = \phi^{-1}\epsilon = m^{-1}\psi\epsilon$ (p. 280); case of paraboloids, and of cylinders.

(g). The equation (p. 281),

$$Sq\rho q'\rho q''\rho + S\rho \phi \rho + S\gamma \rho + C = 0, \qquad (Z_2')$$

represents the general surface of the third degree, or briefly the General Cubic Surface; C being a constant scalar, γ a constant vector, and q, q', q'' three constant quaternions, while $\phi \rho$ is here again a linear, vector, and self-conjugate function of ρ .

* It is shown, in a Note to p. 278, that this monomial equation (Y_2^n) becomes, when expanded, the known equation of six terms, which expresses the condition of integrability of the differential equation pdx + qdy + rdz = 0.

+ In a Note to p. 204 (already mentioned in p. xviii), the reader will find references to the *Lectures*, for several different generations of the ellipsoid, derived from quaternion forms of its equation.

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(h). The General Cubic Cone, with its vertex at the origin, is thus represented in quaternions by the monomial equation (same page),

$$Sq\rho q'\rho q''\rho = 0. \tag{Z}_2''$$

(i). Screw Surface, Screw Sections (p. 281); Skew Centre of Skew Arch, with illustration by a diagram (fig. 85, p. 283).

SECTION 8.—On a few Specimens of Physical Applications of Quaternions, with some Concluding Remarks, 283 to the end.

ARTICLE 416 .--- On the Statics of a Rigid Body,

(a). Equation of Equilibrium,

$$\nabla \gamma \Sigma \beta = \Sigma \nabla \alpha \beta ; \qquad (A_3)$$

each a is a vector of application; β the corresponding vector of applied force; γ an arbitrary vector; and this one quaternion formula (A₃) is equivalent to the system of the six usual scalar equations (X = 0, Y = 0, Z = 0, L = 0, M = 0, N = 0). (b.) When

$$S(\Sigma\beta \cdot \Sigma V \alpha \beta) = 0,$$
 (B₃), but not $\Sigma\beta = 0,$ (C₃)

the applied forces have an *unique resultant* = $\Sigma\beta$, which acts along the line whereof (A₃) is then the equation, with γ for its variable vector.

(c). When the condition (C₃) is satisfied, the forces compound themselves generally into one couple, of which the $axis = \Sigma V \alpha \beta$, whatever may be the position of the assumed origin o of vectors.

(d). When

$$\Sigma V \alpha \beta = 0$$
, (D₃), with or without (C₃),

the forces have no tendency to turn the body round *that* point o; and when the equation (A₃) holds good, as in (a), for an *arbitrary* vector γ , the forces do not tend to produce a rotation^{*} round *any* point c, so that they completely *balance* each other, as before, and *both* the conditions (C₃) and (D₃) are satisfied.

(c). In the general case, when neither (C_3) nor (D_3) is satisfied, if q be an auxiliary quaternion, such that

$$q \Sigma \beta = \Sigma V a \beta, \tag{E}_3$$

then Vq is the vector perpendicular from the origin, on the central axis of the system; and if e = Sq, then $c\Xi\beta$ represents, both in quantity and in direction, the axis of the central couple.

(f). If Q be another auxiliary quaternion, such that

$$Q\mathbf{\Sigma}\boldsymbol{\beta} = \mathbf{\Sigma}\boldsymbol{\alpha}\boldsymbol{\beta},\tag{F_3}$$

with $T\Sigma\beta > 0$, then SQ = c = central moment divided by total force; and VQ is the vector γ of a point c upon the central axis which does not vary with the origin o, and which there are reasons for considering as the Central Point of the system, or as the general centre of applied forces; in fact, for the case of parallelism, this point c coincides with what is usually called the centre of parallel forces.

(g). Conceptions of the Total Moment $\sum \alpha \beta$, regarded as being generally a quaternion; and of the Total Tension, $-\sum \alpha \beta$, considered as a scalar to which that quaternion with its sign changed reduces itself for the case of equilibrium (a), and of which the value is in that case independent of the origin of vectors.

* It is easy to prove that the moment of the force β , acting at the end of the vector α from α , and estimated with respect to any unit-line ι from the same origin, or the energy with which the force so acting tends to cause the body to turn round that line ι , regarded as a fixed axis, is represented by the scalar, $-S_{\iota\alpha\beta}$, or $S_{\iota}^{-1}\alpha\beta$; so that when the condition (D₃) is satisfied, the applied forces have no tendency to produce rotation round any axis through the origin: which origin becomes an arbitrary point c, when the equation of equilibrium (A₃) holds good.

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(h). Principle of Virtual Velocities,

$$S\beta\delta a = 0,$$
 (G₃)

ARTICLE 417 .- On the Dynamics of a rigid body, (a). General Equation of Dynamics,

$$\sum mS (D_t^2 \alpha - \xi) \, \delta \alpha = 0 \, ; \tag{H_3}$$

the vector ξ representing the accelerating force, or $m\xi$ the moving force, acting on a particle m of which the vector at the time t is α ; and $\delta \alpha$ being any infinitesimal variation of this last vector, geometrically compatible with the connexions between the parts of the system, which need not here be a rigid one.

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(b). For the case of a free system, we may change each δa to $\epsilon + V_{\iota a}$, ϵ and ι being any two infinitesimal vectors, which do not change in passing from one particle m to another; and thus the general equation (H_3) furnishes two general vector equations, namely,

$$\Sigma m (D_t^2 a - \xi) = 0,$$
 (I₃), and $\Sigma m V a (D_t^2 a - \xi) = 0;$ (J₃)

which contain respectively the law of the motion of the centre of gravity, and the law of description of areas.

(c) If a body be supposed to be rigid, and to have a fixed point o, then only the equation (J_3) need be retained; and we may write,

$$D_{la} = V_{la}, \tag{K_3}$$

, being here a finite vector, namely the Vector Axis of Instantaneous Rotation : its versor Us denoting the direction of that axis, and its tensor Ts representing the angular velocity of that body about it, at the time t.

(d) When the forces vanish, or balance each other, or compound themselves into a single force acting at the fixed point, as for the case of a heavy body turning freely about its centre of gravity, then

$$\Sigma m Va\xi = 0,$$
 (L₃); and if we write, $\phi_i = \Sigma m a Va_i,$ (M₃)

so that ϕ again denotes a linear, vector, and self-conjugate function, we shall have the equations,

$$\phi D_{ii} + V_i \phi_i = 0, \quad (N_3); \qquad \phi_i + \gamma = 0, \quad (O_3); \qquad S_i \phi_i = h^2; \quad (P_3)$$

whence

$$S_{i\gamma} + h^2 = 0$$
, (Q₃); and $\phi D_{i'} = V_{i\gamma}$; (R₃)

the vector γ being what we may call the Constant of Areas, and the scalar h^2 being the Constant of Living Force.

(e). Une of Poinsot's representations of the motion of a body, under the circumstances last supposed, is thus reproduced under the form, that the Ellipsoid of Living Force (P3), with its centre at the fixed point o, rolls without gliding on the fixed plane (Q3), which is parallel to the Plane of Areas $(S_{i\gamma} = 0)$; the variable semidiameter of contact, i, being the vector-axis (c) of instantaneous rotation of the body.

(f) The Moment of Inertia, with respect to any axis i through o, is equal to the living force (h^2) divided by the square (T_{s^2}) of the semidiameter of the ellipsoid (P₃), which has the direction of that axis; and hence may be derived, with the help of the first general construction of an ellipsoid, suggested by quaternions, a simple geometrical representation (p. 290) of the square root of the moment of inertia of a body, with respect to any axis AD passing through a given point A, as a certain right line $\overline{u}D$, if $\overline{c}D = \overline{c}A$, with the help of two other points n and c, which are likewise fixed in the body, but may be chosen in more ways than one.

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(g) A cone of the second degree,

$$S_{i\nu} = 0$$
, (S_3) , with $\nu = \gamma^2 \phi_i - h^2 \phi^2_i$, (T_3)

is fixed in the body, but rolls in space on that other cone, which is the locus of the instantaneous axis ι ; and thus a second representation, proposed by Poinsot, is found for the motion of the body, as the rolling of one cone on another.

(h) Some of Mac Cullagh's results, respecting the motion here considered, are obtained with equal ease by the same quaternion analysis; for example, the line γ , although fixed in space, describes in the body an easily assigned cone of the second degree (p. 291), which cuts the reciprocal ellipsoid,

$$S\gamma\phi^{-1}\gamma = h^2, \tag{U}_3$$

in a certain sphero-conic: and the cone of normals to the last mentioned cone (or the locus of the line $\iota + h^2 \gamma^{-1}$) rolls on the plane of areas (Si $\gamma = 0$).

(i). The Three (Principal) Axes of Inertia of the body, for the given point o, have the directions (p. 291) of the three rectangular and vector roots (comp. (P), p. xxxii, vol. i., and the paragraph 415, (a), p. xxx) of the equation

$$V_i\phi_i = 0$$
, (V₃), because, for each, $D_{ii} = 0$; (V₃')

and if A, B, C denote the three *Principal Moments* of inertia corresponding, then the *Symbolical Cubic* in ϕ (comp. the formula (N) in page xxxi, vol. i.) may be thus written,

$$(\phi + A) (\phi + B) (\phi + C) = 0.$$
 (W₃)

(j). Passage (p. 292), from moments referred to axes passing through a given point o, to those which correspond to respectively parallel axes, through any other point Ω of the body.

ARTICLE 418.—On the motions of a System of Bodies, considered as free particles m, m', . . which attract each other according to the law of the Inverse Square, . . (a). Equation of motion of the system,

. Equation of motion of the system,

$$\sum m SD_t^2 a \delta a + \delta P = 0, \quad (X_3), \quad \text{if } P = \sum mm' T(a - a')^{-1};$$
 (Y3)

a is the vector, at the time t, of the mass or particle m; P is the potential (or force-function); and the infinitesimal variations δa are arbitrary.

(b). Extension of the notation of derivatives,

$$\delta P = \Sigma S (D_P \cdot \delta \alpha). \tag{Z_3}$$

(c). The differential equations of motion of the separate masses m, . . become thus,

$$mD_t^2 a + D_a P = 0, \dots; \qquad (A_4)$$

and the laws of the centre of gravity, of areas, and of living force, are obtained under the forms, $\Sigma m D_{i} q = \theta_{i} \quad (B_{i}): \quad \Sigma m V q D_{i} q = \gamma : \qquad (C_{i})$

 $T = -\frac{1}{2} \Sigma m(\mathbf{D}_{t} \mathbf{a})^2 = P + H;$

$$\lim D_{I}a = \beta, \quad (B_{4}); \quad \Sigma m \nabla a D_{I}a = \gamma; \quad (C_{4})$$

 β , γ being two vector constants, and H a scalar constant.

(d). Writing,

$$F = \int_0^t (P + T) dt$$
, (E₄), and $V = \int_0^t 2T dt = F + tH$, (F₄)

F may be called the Principal* Function, and V the Characteristic Function, of the

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^{*} References are given to two Essays by the present writer, "On a General Method in Dynamics," in the Philosophical Transactions for 1834 and 1835, in which the Action (V), and a certain other function (S), which is here denoted by F, were called, as above, the Characteristic and Principal Functions. But the analysis here used, as being founded on the Calculus of Quaternions, is altogether unlike the analysis which was employed in those former Essays.

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motion of the system; each depending on the final vectors of position, a, a', ... and on the initial vectors, $a_0, a'_0, ...$; but F depending also (explicitly) on the time, t, while V (= the Action) depends instead on the constant H of living force, in addition to those final and initial vectors: the masses m, m', ... being supposed to be known, or constant.

(e). We are led thus to equations of the forms,

$$mD_{t}a + D_{a}F = 0$$
, . (G₄); $-mD_{0}a + D_{a0}F = 0$, . (H₄); (D_tF) = $-H$, (I₄)

whereof the system (G₄) contains what may be called the *Intermediate Integrals*, while the system (H₄) contains the *Final Integrals*, of the differential *Equations of Motion* (A₄).

(f). In like manner we find equations of the forms,

$$D_a V = -m D_t a, \dots (J_4); \quad D_{a0} V = m D_0 a, \dots (K_4); \quad D_H V = t;$$
 (L4)

the intermediate integrals (e) being here the result of the elimination of H, between the system (J_4) and the equation (L_4) ; and the *final integrals*, of the same system of differential equations (A_4) . being now (theoretically) obtained, by eliminating the same constant H between (K_4) and (L_4) .

(g). The functions F and V are obliged to satisfy certain Partial Differential Equations in Quaternions, of which those relative to the final vectors a, a', . . are the following,

$$(\mathbf{D}_t F) - \frac{1}{2} \Sigma m^{-1} (\mathbf{D}_a F)^2 = P, \ (\mathbf{M}_4); \ \frac{1}{2} \Sigma m^{-1} (\mathbf{D}_a V)^2 + P + H = 0; \ (\mathbf{N}_4)$$

and they are subject to certain geometrical conditions, from which can be deduced, in a new way, and as new verifications, the law of motion of the centre of gravity, and the law of description of areas.

(h). General approximate expressions (p. 298) for the functions F and V, and for their derivatives H and t, for the case of a *short motion* of the system.

ARTICLE 419.—On the Relative Motion of a Binary System; and on the Law of the Circular Hodograph,

(a). The vector of one body from the other being α , and the distance being $r (= T\alpha)$, while the sum of the masses is M, the differential equation of the relative motion is, with the law of the inverse square,

$$\mathbf{D}^2 \boldsymbol{\alpha} = \boldsymbol{M} \boldsymbol{\alpha}^{-1} \boldsymbol{r}^{-1} ; \tag{O_4}$$

D being here used as a characteristic of derivation, with respect to the time t.

(b). As a first integral, which holds good also for any other law of central force, we have

$$V \alpha D \alpha = \beta = \alpha \text{ constant vector};$$
 (P₄)

which includes the two usual laws, of the constant plane $(\perp \beta)$, and of the constant areal velocity $\begin{pmatrix} c \\ 2 & \frac{1}{2}T\beta \end{pmatrix}$.

(c). Writing $\tau = Da = vector of relative velocity, and conceiving this new vector <math>\tau$ to be drawn from that one of the two bodies which is here selected for the origin o, the locus of the extremities of the vector τ is (by earlier definitions) the Hodograph of the Relative Motion; and this hodograph is proved to be, for the Law of the Inverse Square, a Circle.

(d). In fact, it is shown (p. 302), that for any law of central force, the radius of curvature of the hodograph is equal to the force, multiplied into the square of the distance, and divided by the doubled areal velocity; or by the constant parallelogram c, under the vectors (α and τ) of position and velocity, or of the orbit and the hodograph.

(e). It follows then, conversely, that the law of the inverse square is the only law which renders the hodograph generally a circle; so that the law of nature may be characterized, as the Law of the Circular Hodograph; from which latter law, however, it is easy to deduce the form of the Orbit, as a conic section with a focus at o.

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(f). If the semiparameter of this orbit be denoted, as usual, by p, and if h be the radius of the hodograph, then (p. 301),

$$h = Mc^{-1} = cp^{-1} = (Mp^{-1})^{\frac{1}{2}}.$$
 (Q4)

(g). The orbital excentricity e is also the hodographic excentricity, in the sense that eh is the distance of the centre H of the hodograph, from the point o which is here treated as the centre of force.

(h). The orbit is an ellipse, when the point o is interior to the hodographic circle (e < 1); it is a parabola, when o is on the circumference of that circle (e = 1); and it is an hyperbola, when o is an exterior point (e > 1). And in all these cases, if we write

$$a = p(1 - e^2)^{-1} = ch^{-1}(1 - e^2)^{-1}, \tag{R_4}$$

the constant a will have its usual signification, relatively to the orbit.

(i). The quantity Mr^{-1} being here called the *Potential*, and denoted by *P*, geometrical constructions for this quantity *P* are assigned, with the help of the hodograph (p. 307); and for the harmonic mean, $2M(r + r')^{-1}$, between the two potentials, *P* and *P'*, which answer to the extremities τ , τ' of any proposed chord of that circle: all which constructions are illustrated by a new diagram (fig. 86).

(j). If u be the pole of the chord \mathbf{TT}' ; M, M' the points in which the line ou cuts the circle; L the middle point, and N the pole, of the new chord MM', one secant from which last pole is thus the line \mathbf{NTT}' ; U' the intersection of this secant with the chord MM', or the harmonic conjugate of the point u, with respect to the same chord ; and $\mathbf{NT}_{,}'$ any near secant from N, while u, (on the line ou) is the pole of the near chord \mathbf{TT}' ; then the two small arcs, $\mathbf{T}_{,}$ and $\mathbf{TT}'_{,}$ of the hodograph, intercepted between these two secants, are proved to be ultimately proportional to the two potentials, P and P'; or to the two ordinates $\mathbf{TV}, \mathbf{TV}',$ namely the perpendiculars let fall from T and T', on what may here be called the hodographic axis LN. Also, the harmonic mean between these two ordinates is obviously (by the construction) the line u'_; while uT, uT', and u, u', u, T' are four tangents to the hodograph, so that this circle is cut orthogonally, in the two points of points, T, T' and T, T', by two other circles, which have the two near points u, u, for their centres (pp. 308, 309).

(k). In general, for any motion of a point (absolute or relative, in one plane or in space, for example, in the motion of the centre of the moon about that of the earth, under the perturbations produced by the attractions of the sun and planets), with a for the variable vector (418) of position of the point, the time dt which corresponds to any vector-element dDa of the hodograph, or what may be called the time of hodographically describing that element, is the quotient obtained by dividing the same element of the hodograph, by the vector of acceleration D^2a in the orbit; because we may write generally (p. 308),

$$dt = \frac{dD\alpha}{D^2\alpha} \quad \text{,or} \quad dt = \frac{TdD\alpha}{TD^2\alpha}, \quad \text{if} \quad dt > 0.$$
 (S4)

(1). For the law of the inverse square (comp. (a) and (i)), the measure of the force, is,

$$TD^{2}a = Mr^{-2} = M^{-1}P^{2}; (T_{4})$$

the times dt, dt', of hodographically describing the small circular arcs $\mathbf{r}_i \mathbf{r}$ and $\mathbf{r}'\mathbf{r}'_i$ of the hodograph, being found by multiplying the lengths (j) of those two arcs by the mass, and dividing each product by the square of the potential corresponding, are therefore *inversely* as those *two potentials*, P, P', or *directly* as the *distances*, r, r', in the orbit: so that we have the proportion,

$$dt: dt': dt + dt' = r; r'; r + r'.$$
(U₄)

(m). If we suppose that the mass, M, and the five points o, L, M, U, U, upon the chord MM' are given, or constant, but that the radius, h, of the hodograph, or the position of the centre H on the hodographic axis LN, is altered, it is found in this way (p. 309) that

XXXV Pages although the two elements of time, dt, dt', separately vary, yet their sum remains unchanged: from which it follows, that even if the two circular arcs, T_iT , $T'T'_i$, be not small, but still intercepted (j) between two secants from the pole N of the fixed chord MM', the sum (say, $\Delta t + \Delta t'$) of the two times is independent of the radius, h.

(n). And hence may be deduced (p. 310), by supposing one secant to become a tangent, this Theorem of Hodographic Isochronism, which was communicated without demonstration, several years ago, to the Royal Irish Academy,* and has since been treated as a subject of investigation by several able writers:

If two circular hodographs, having a common chord, which passes through, or tends towards, a common centre of force, be cut perpendicularly by a third circle, the times of hodographically describing the intercepted arcs will be equal.

(o). This common time can easily be expressed (p. 310), under the form of the definite integral,

$$Time of TMT' = \frac{2M}{g^3} \int_0^w \frac{\mathrm{d}w}{(1 - e' \cos w)^2};$$
 (V4)

2g being the length of the *fixed chord* MM'; e' the quotient LO: LM, which reduces itself to -1 when o is at M', that is for the case of a *parabolic orbit*; e' lying between ± 1 for an *cllipse*, and *outside* those limits for an *hyperbola*, but being, in all these cases, *constant*; while w is a certain auxiliary angle, of which the sine $= \overline{UT}: \overline{UL}$ (p. 312), or $= s(r + r')^{-1}$, if s denote the length \overline{PP}' of the *chord of the orbit*, *corresponding* to the *chord* TT' of the *hodograph*; and w varies from 0 to π , when the whole *periodic time* $2\pi n^{-1}$ for a *closed orbit* is to be computed: with the verification, that the integral (V₄) gives, in this last case,

$$M = a^3 n^2, \text{ as usual.} \tag{W4}$$

(p). By examining the general composition of the definite integral (V_4) , or by more purely geometrical considerations, which are illustrated by fig. 87, it is found that, with the law of the inverse square, the *time* t of describing an *are* PP' of the orbit (closed or unclosed) is a *function* (p. 314) of the *three ratios*,

$$\frac{a^3}{M}, \quad \frac{r+r'}{a}, \quad \frac{s}{r+r'}; \qquad (\mathbf{X}_4)$$

and therefore simply a function of the chord $(s, \text{ or } \overline{PP'})$ of the orbit, and of the sum of the distances $(r + r', \text{ or } \overline{OP'} + \overline{OP'})$ when M and a are given: which is a form of the Theorem of Lambert.

(q). The same important theorem may be otherwise deduced, through a quite different analysis, by an employment of *partial derivatives*, and ot *partial differential equations in quaternions*, which is analogous to that used in a recent investigation (418), respecting the motions of an *attracting system* of *any number of bodies*, m, m', &c.

(r). Writing now (comp. p. xxxiii) the following expression for the relative living force, or for the mass (M = m + m'), multiplied into the square of the relative velocity (TDa),

$$2T = -MDa^{2} = 2(P + H) = M(2r^{-1} - a^{-1}); \qquad (Y_{4})$$

introducing the two new integrals (p. 314),

$$F = \int_{0}^{t} (P + T) dt$$
, (Z₄), and $V = \int_{0}^{t} 2T dt = F + tH$, (A₅)

which have thus (comp. (E4) and (F4)) the same forms as before, but with different (although analogous) significations, and may still be called the Principal and Characteristic Functions of the motion; and denoting by α , α' (instead of α_0 , α) the initial and final vectors of position, or of the orbit, while r, r' are the two distances, and τ , τ' the

* See the Proceedings of the 16th of March, 1847. It is understood that the common centre o of force is occupied by a common mass, M.

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two corresponding vectors of velocity, or of the hodograph: it is found that when Mis given, F may be treated as a function of a, a', t, or of r, r', s, t, and V as a function of a, a', a, or of r, r', s, and H; and that their partial derivatives, in the first view of these two functions, are (p. 314),

$$D_{\alpha}F = D_{\alpha}V = \tau, \quad (B_5); \quad D_{\alpha'}F = D_{\alpha'}V = -\tau'; \quad (C_5)$$

$$(\mathbf{D}_t)F = -H, \quad (\mathbf{D}_b); \text{ and } \mathbf{D}_H V = \frac{2a^2}{M}\mathbf{D}_a V = t;$$
 (E_b)

while, in the second view of the same functions, they satisfy the two partial differential equations (p. 315),

$$\mathbf{D}_{\mathbf{r}}\mathbf{F} = \mathbf{D}_{\mathbf{r}'}\mathbf{F}, \quad (\mathbf{F}_{\mathbf{5}}), \quad \text{and} \quad \mathbf{D}_{\mathbf{r}}V = \mathbf{D}_{\mathbf{r}'}V; \quad (\mathbf{G}_{\mathbf{5}})$$

along with two other equations of the same kind, but of the second degree, for cach of the functions here considered, which are analogous to those mentioned in p. xxxiv.

(s). The equations (F₅) (G₅) express, that the two distances, r and r', enter into each of the two functions only by their sum; so that, if M be still treated as given, F may be regarded as a function of the three quantities, r + r', s, and t; while V, and therefore also t by (E₅), is found in like manner to be a function of the three scalars, r + r', s, and a: which last result respecting the time agrees with (p), and furnishes a new proof of Lambert's Theorem.

(t). The three partial differential equations (r) in V conduct, by merely algebraical combinations, to expressions for the three partial derivatives, $D_r V$, $D_r' V (= D_r V)$, and DsV; and thus, with the help of (E₅), to two new definite integrals* (p. 317), which express respectively the Action and the Time, in the relative motion of a binary system here considered, namely, the two following :

$$V = \int_{-s}^{s} \left(\frac{M}{r+r'+s} - \frac{M}{4a} \right)^{\frac{1}{2}} \mathrm{d}s \; ; \tag{H}_{5}$$

$$t = \frac{1}{2} \int_{-s}^{s} \left(\frac{4M}{r+r'+s} - \frac{M}{a} \right)^{-\frac{1}{2}} \mathrm{d}s; \qquad (\mathbf{I}_{5})$$

whereof the latter is not to be extended, without modification, beyond the limits within which the radical is finite.

ARTICLE 420 .- On the determination of the Distance of a Comet, or new Planet, from the Earth,

(a). The masses of earth and comet being neglected, and the mass of the sun being denoted by M, let r and w denote the distances of earth and comet from sun, and ztheir distance from each other, while a is the heliocentric vector of the earth (Ta = r), known by the theory of the sun, and ρ is the unit-vector, determined by observation, which is directed from the earth to the comet. Then it is easily proved by quaternions, that we have the equation (p. 320),

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$$\frac{S\rho D\rho D^2 \rho}{S\rho D\rho Ua} = \frac{r}{z} \left(\frac{M}{r^3} - \frac{M}{w^3} \right), \qquad (J_5)$$

$$v^2 = r^2 + z^2 - 2z \mathrm{Sa}\rho;$$
 (K₅)

* References are given to the First Essay, &c., by the present writer (comp. the Note to p. xxxiii), in which were assigned integrals, substantially equivalent to (H5) and (I5), but deduced by a quite different analysis. It has recently been remarked to him, by his friend Professor Tait of Edinburgh, that while the area described, with Newton's Law, about the full focus of an orbit, has long been known to be proportional to the time corresponding, so the area about the empty focus represents (or is proportional to) the action.

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(N5)

eliminating w between these two formulæ, clearing of fractions, and dividing by z, we are therefore conducted in this way to an algebraical equation of the seventh degree, whereof one root is the sought distance, z.

(b). The final equation, thus obtained, differs only by its notation, and by the facility of its deduction, from that assigned for the same purpose in the *Mécanique Céleste*; and the *rule* of Laplace there given, for determining, by inspection of a celestial globe, which of the two bodies (earth and comet) is the *nearer to the sun*, results at sight from the formula (J_5) .

ANTICLE 421.—On the Development of the Disturbing Force of the Sun on the Moon; or of one Planet on another, which is nearer than itself to the Sun,

(a) Let a, σ be the geocentric vectors of moon and sun; r(=Ta), and $s(=T\sigma)$, their geocentric distances; M the sum of the masses of earth and moon; S the mass of the sun; and D (as in recent Series) the mark of derivation with respect to the time: then the differential equation of the disturbed motion of the moon about the earth is,

$$D^2a = M\phi a + \eta$$
, (L₅) if $\phi a = \phi(a) = a^{-1}Ta^{-1}$, (M₅)

and

 ϕ denoting here a vector function, but not a linear one.

(b). If we neglect η , the equation (L₅) reduces itself to the form $D^2 a = M \phi a$; which contains (comp. (O₄)) the laws of undisturbed elliptic motion.

 $\eta = Vector \ of \ Disturbing \ Force = S(\phi \sigma - \phi(\sigma - a));$

(c). If we develop the disturbing vector η , according to ascending powers of the quotient r: s, of the distances of moon and sun from the earth, we obtain an *infinite series* of terms, each representing a *finite group* of *partial disturbing forces*, which may be thus denoted

$$\eta = \eta_1 + \eta_2 + \eta_3 + \&c. \tag{O_5}$$

$$\eta_1 = \eta_1, 1 + \eta_1, 2, \quad \eta_2 = \eta_{2,1} + \eta_2, 2 + \eta_{2,3} \&c.$$
 (P₅)

these partial forces increasing in number, but diminishing in intensity, in the passage from any one group to the following; and being connected with each other, within any such group, by simple numerical ratios and angular relations.

(d). For example, the two forces $\eta_{1,1}$, $\eta_{1,2}$ of the first group are, rigorously, proportional to the numbers 1 and 3; the three forces $\eta_{2,1}$, $\eta_{2,2}$, $\eta_{2,3}$ of the second group are as the numbers 1, 2, 5; and the four forces of the third group are proportional to 5, 9, 15, 35: where the separate intensities of the first forces, in these three first group, have the expressions,

$$T_{\eta_{1,1}} = \frac{\delta r}{2s^{3}}; \qquad T_{\eta_{2,1}} = \frac{3\delta r^{2}}{3s^{4}}; \qquad T_{\eta_{3,1}} = \frac{55r^{3}}{16s^{4}}.$$
 (Q5)

(c). All these partial forces are conceived to act at the moon; but their directions may be represented by the respectively parallel unit-lines U_{η_1, η_2} , &c., drawn from the earth, and terminating on a great circle of the celestial sphere (supposed here to have its radius equal to unity), which passes through the geocentric (or apparent) places, \odot and λ , of the sun and moon in the heavens.

(f). Denoting then the geocentric elongation \bigcirc) of moon from sun (in the plane of the three bodies) by $+ \theta$; and by \bigcirc_1 , \bigcirc_2 , and \searrow_1 , \searrow_2 , \gg_3 what may be called two fictitious suns, and three fictitious moons, of which the corresponding elongations from \bigcirc , in the same great circle are $+2\theta$, -2θ , and $-\theta$, $+3\theta$, -3θ , as illustrated by fig. 88 (p. 322); it is found that the directions of the two forces of the first group are represented by the two radii of this unit-circle, which terminate in) and y_1 ; those of the three forces of the second group, by the three radii to \bigcirc_1 , \bigcirc , and \bigcirc_2 ; and those of the four forces of the third group, by the radii to \bigcirc_2 , \supset , \searrow_1 , and \bigcirc_3 ; with facilities for extending all those results (with the requisite modifications), to the fourth and subsequent groups, by the same quaternion analysis.

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(g). And it is important to observe, that no supposition is here made respecting any smallness of excentricities or inclinations (p. 323); so that all the formulæ apply, with the necessary changes of geocentric to heliocentric vectors, &c., to the perturbations of the motion of a comet about the sun, produced by the attraction of a planet, which is (at the time) more distant than the comet from the sun.

ARTICLE 422 .- On Fresnel's Wave,

(a) If ρ and μ be two corresponding vectors of ray-velocity and wave slowness, or briefly Ray and Index, in a biaxal crystal, the velocity of light in a vacuum being unity; and if $\delta\rho$ and $\delta\mu$ be any infinitesimal variations of these two vectors, consistent with the equations (supposed to be as yet unknown), of the Wave (or wave-surface), and its reciprocal, the Index-Surface (or surface of wave-slowness): we have then first the fundamental Equations of Reciprocity (comp. p. 461, vol. i.),

$$S\mu\rho = -1$$
, (R₅); $S\mu\delta\rho = 0$, (S₅); $S\rho\delta\mu = 0$, (T₅)

which are independent of any hypothesis respecting the vibrations of the ether.

(b). If $\delta\rho$ be next regarded as a *displacement* (or vibration), *tangential* to the *wave*, and if δe denote the *elastic force* resulting, there exists then, on Fresnel's principles, a *relation* between these two small vectors; which relation may (with our notations) be expressed by either of the two following equations,

$$\delta \epsilon = \phi^{-1} \delta \rho,$$
 (U₅), or $\delta \rho = \phi \delta \epsilon$; (V^{*}₅)

the function ϕ being of that linear, vector, and *self-conjugate* kind, which has been frequently employed in these Elements.

(c). The fundamental connexion, between the functional symbol ϕ , and the optical constants *abc* of the crystal, is expressed (p. 330, comp. the formula (W₃) in p. xxxiii) by the symbolic and cubic equation,

$$(\phi + a^{-2}) (\phi + b^{-2}) (\phi + c^{-2}) = 0;$$
 (W₅)

of which an extensive use is made in the present Series.

(d). The normal component, $\mu^{-1}S\mu\delta\epsilon$, of the elastic force $\delta\epsilon$, is ineffective in Fresnel's theory, on account of the supposed incompressibility of the ether; and the tangential component, $\phi^{-1}\delta\rho - \mu^{-1}S\mu\delta\epsilon$, is (in the same theory, and with present notations) to be equated to $\mu^{-2}\delta\rho$, for the propagation of a rectilinear vibration (p. 324); we obtain then thus, for such a vibration or tangential displacement, $\delta\rho$, the expression,

$$\delta \rho = (\phi^{-1} - \mu^{-2})^{-1} \mu^{-1} S \mu \delta \epsilon ; \qquad (X_5)$$

and therefore by (S_5) the equation,

or

$$0 = S\mu^{-1}(\phi^{-1} - \mu^{-2})^{-1}\mu^{-1}, \qquad (Y_5)$$

which is a Symbolical Form of the scalar Equation of the Index-Surface, and may be thus transformed,

$$1 = S\mu \,(\mu^2 - \phi)^{-1}\mu. \tag{Z_5}$$

(e). The Wave-Surface, as being the reciprocal (a) of the index-surface (d), is easily found (p. 326), to be represented by this other Symbolical Equation,

$$0 = S\rho^{-1}(\phi - \rho^{-2})^{-1}\rho^{-1}; \qquad (A_6)$$

$$1 = S\rho(\rho^2 - \phi^{-1})^{-1}\rho.$$
 (B₆)

(f). In such transitions, from one of these reciprocal surfaces to the other, it is found convenient to introduce two auxiliary vectors, v and $\omega (= \phi v)$, namely the lines ou and ow of fig. 89; both drawn from the common centre o of the two surfaces; but v terminating (p. 325) on the tangent plane to the wave, and being parallel to the direction of the elastic force $\delta \epsilon$; whereas ω terminates (p. 328) on the tangent plane to the index-surface, and is parallel to the displacement $\delta \rho$.

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(q). Besides the relation,

$$\omega = \phi v, \quad \text{or} \quad v = \phi^{-1} \omega, \tag{C_6}$$

connecting the two new vectors (f) with each other, they are connected with ρ and μ by the equations (pp. 325, 328),

$$S_{\mu\nu} = -1, (D_6); S_{\rho\nu} = 0;$$
 (E₆)

$$S\rho\omega = -1$$
, (F_6) ; $S\mu\omega = 0$; (G_6)

and generally (p. 328), the following *Rule of the Interchanges* holds good: In any formula involving ρ , μ , v, ω , and ϕ , or some of them, it is permitted to exchange ρ with μ , v with ω , and ϕ with ϕ^{-1} ; provided that we at the same time interchange $\delta\rho$ with $\delta\epsilon$, but not generally* $\delta\mu$ with $\delta\rho$, when these variations, or any of them occur.

(h). We have also the relations (pp. 328, 329),

$$-\rho^{-1} = v^{-1} \nabla v \mu = \mu + v^{-1}; \qquad (\mathbf{H}_6)$$

$$-\mu^{-1} = \omega^{-1} \mathbf{V} \omega \rho = \rho + \omega^{-1}; \qquad (\mathbf{I}_6)$$

with others easily deduced, which may all be illustrated by the above-cited fig. 89.

(i). Among such deductions, the following equations (p. 330) may be mentioned,

$$(\nabla u\phi u)^2 + Su\phi u = 0, \quad (J_6); \quad (\nabla \omega \phi^{-1} \omega)^2 + S\omega \phi^{-1} \omega = 0; \quad (K_6)$$

which show that the Locus of each of the two Auxiliary Points, u and w, wherein the two vectors v and ω terminate (f), is a Surface of the Fourth Degree, or briefly, a Quartic Surface; of which two loci the constructions may be connected (as stated in p. 330) with those of the two reciprocal ellipsoids,

$$S_{\rho\phi\rho} = 1$$
, (L₆), and $S_{\rho\phi}^{-1}\rho = 1$; (M₆)

 ρ denoting, for each, an arbitrary semidiameter.

(j). It is, however, a much more interesting use of these two ellipsoids, of which (by (W_5) , &c.) the scalar semiaxes are a, b, c for the first, and a^{-1} , b^{-1} , c^{-1} for the second, to observe that they may be employed (p. 327) for the Constructions of the Wave and the Index-Surface, respectively, by a very simple rule, which (at least for the first of these two reciprocal surfaces (a)) was assigned by Fresnel himself.

(k). In fact, on comparing the symbolical form (A_6) of the equation of the Wave, with the form (H_2) in p. xxv, or with the equation 412, XLI., in p. 253, we derive at once *Fresnel's Construction*: namely, that if the ellipsoid (abc) be cut, by an arbitrary plane through its centre, and if perpendiculars to that plane be erected at that central point, which shall have the lengths of the semiaxes of the section, then the locus of the extremities, of the perpendiculars so erected, will be the sought Wave-Surface.

(1). A precisely similar construction applies, to the derivation of the Index-Surface from the ellipsoid $(a^{-1}b^{-1}c^{-1})$: and thus the two auxiliary surfaces, (L₆) and (M₆), may be briefly called the *Generating Ellipsoid*, and the *Reciprocal Ellipsoid*.

(m). The cubic (W₆) in ϕ enables us easily to express (p. 331) the inverse function $(\phi + e)^{-1}$, where e is any scalar; and thus, by changing e to $-\rho^{-2}$, &c., new forms of the equation (A₆) of the wave are obtained, whereof one is,

$$0 = (\phi^{-1}\rho)^2 + (\rho^2 + a^2 + b^2 + c^2) \operatorname{S}\rho\phi^{-1}\rho - a^2b^2c^2;$$
 (Ne)

with an analogous equation in μ (comp. the *rule* in (g)), to represent the *index-surface*: so that each of these two surfaces is of the *fourth degree*, as indeed is otherwise known.

• This apparent exception arises (pp. 328, 329) from the circumstance, that $\delta\rho$ and $\delta\epsilon$ have their directions generally fixed, in this whole investigation (although subject to a common reversal by \pm), when ρ and μ are given; whereas $\delta\mu$ continues to be used, as in (a), to denote any infinitesimal vector, tangential to the index-surface at the end of μ .

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(n). If either $Sp\phi^{-1}p$ or p^2 be treated as constant in (N_6) , the degree of that equation is depressed from the *fourth* to the second; and therefore the Wave is cut, by each of the two concentric quadrics,

$$S\rho\phi^{-1}\rho = h^4$$
, (O₆), $\rho^2 + r^2 = 0$, (P₆)

in a (real or imaginary) curve of the fourth degree: of which two quartic curves, answering to all scalar values of the constants h and r, the wave is the common locus.

(o). The new ellipsoid (O_6) is similar to the ellipsoid (M_6) , and similarly placed, while the sphere (P_6) has r for radius: and every quartic of the second system (n) is a sphero-conic, because it is, by the equation (A_6) of the wave, the intersection of that sphere (P_6) with the concentric and quadric cone,

$$0 = S\rho(\phi + \gamma^{-2})^{-1}\rho; (Q_6)$$

or, by (B₆), with this other concentric quadric,*

$$-1 = S\rho(\phi^{-1} + r^2)^{-1}\rho, \tag{R_6}$$

whereof the conjugate (obtained by changing -1 to +1 in the last equation) has [p. 346]

$$x^2 - r^2$$
, $b^2 - r^2$, $c^2 - r^2$, (S₆)

for the squares of its scalar semiaxes, and is therefore confocal with the generating ellipsoid (L_6) .

(p). For any point P of the wave, or at the end of any ray ρ , the tangents to the two curves (n) have the directions of ω and $\mu\omega$; so that these two quartics cross each other at right angles, and each is a common orthogonal in all the curves of the other system [p. 345].

(q). But the vibration $\delta \rho$ is easily proved to be parallel to ω ; hence the curves of the first system (n) are Lines of Vibration of the Wave: and the curves of the second system are the Orthogonal Trajectories[†] to those Lines.

(r). In general, the vibration $\delta\rho$ has (on Fresnel's principles) the direction of the projection of the ray ρ on the tangent plane to the wave; and the elastic force $\delta\epsilon$ has in like manner the direction of the projection of the index-vector μ on the tangent plane to the index-surface: so that the ray is thus perpendicular to the elastic force corresponding.

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(s). When a given or first ray, ρ , prolonged or shortened, becomes a second ray, ρ_1 , at the same side of the centre o, so that $U\rho_1 = U\rho$, we can easily derive from LXIII. the expression [p. 349]

$$\mathbf{1} = \mathbf{T}\boldsymbol{\rho}_1 = abch^{-2},\tag{T_6}$$

or

$$r_1^2 = a^2 b^2 c^2 (S \rho \phi^{-1} \rho); \qquad (U_6)$$

so that the two quantities, h and r, are constant together or variable together: similarly for the two other quantities, h and r, which are obtained from these by interchanging *sheets*.

(t). It follows, then, that one sheet of the cone (Q_6) , which has its surface at the centre of the wave, and rests on a sphero-conic (r_1) traced on the wave-sheet, contains also, or may be considered as likewise resting upon, a line of vibration (h) on the other sheet, and reciprocally; so that each of these two curves is projected into the other, by rays from 0, and one would appear as superposed on the other, if we imagine them to be seen by an eye placed at that point. As a limiting case, when the projecting cone reduces itself to one of the two principal planes—for example, to the plane (a)—then the ellipse (a) in that plane may be represented by the equation $h^2 = bc$, and the circle (a) has for equation $r_1 = a$; so that the condition (T_6) is satisfied [p. 350].

* For real curves of the second system (n), this new quadric (\mathbf{R}_{b}) is an hyperboloid, with one sheet or with two, according as the constant r lies between a and b, or between b and c; and, of course, the conjugate hyperboloid (o) has two sheets or one, in the same two cases respectively.

† In a different theory of light (comp. the next Series, 423), these sphero-conics on the wave are themselves the lines of vibration.

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(u). In fact the quadric cone (Q_8) must cut the quartic wave in an octic curve, or else in a system of curves, of which the product of the dimensions is eight; and accordingly we find, as above, that the complete intersection, here considered, of the two surfaces, consists of a system of two quartic curves, namely, a sphero-conic (r_1) on one sheet, and a line of vibration (h) on the other [p. 349].

(v).* [The section of the wave by a principal plane of the generating ellipsoid (L_6) breaks up into a circle and an ellipse (p. 332)

$$\rho^{-2} + a^{-2} = 0,$$
 (V₆); $1 - b^{-2}c^{-2}S\rho\phi^{-1}\rho = 0,$ (W₆)

which we may refer to as the circle (a) and the ellipse (a). The intersections of a circle and the corresponding ellipse are nodal points on the wave. Those on the circle (b) and the ellipse (b) alone are real, and may be called by pre-eminence the *Wave-Cusps*. And the vectors $(\pm \rho_0, \pm \rho_1)$ drawn from the centre o to these four cusps may be termed *Lines* of Single Ray-Velocity, or briefly Cusp-Rays (p. 332). At a wave-cusp the vector μ is indeterminate (p. 334) but it is an edge of the cone (p. 336)

$$u^2 + S\mu\rho_0 S\mu\mu_0 = 0 \tag{X_6}$$

where μ_0 corresponds to ρ_0 as terminating on the ellipse (b) (p. 334). Analogous cusps lie on the Index Surface at the ends of the vectors $(\pm \nu_0, \pm \nu_1)$ of Single Normal Slowness (p. 335). The tangent cone to a wave-cusp (p. 335) may be thus briefly written (p. 341)

$$(S\mu_0\rho_0\rho)^2 = 4S\rho_0\rho S\mu_0\rho \qquad (Y_6)$$

with various other transformations (pp. 342-4).]

[(w). There are four real Circular Ridges on the wave along which it is touched by the four planes

$$S\rho\nu_0 = \pm 1, \quad S\rho\nu_1 = \pm 1$$
 (Z₆)

 $\pm v_0$ and $\pm v_1$ being the vectors thus designated in the last paragraph. The common length of the diameters of these circles is $b^{-1}(a^2 - b^2)^{\frac{1}{2}} (b^2 - c^2)^{\frac{1}{2}}$ and each diameter in the principal plane subtends at the wave centre the angle $\tan^{-1}b^{-2}(a^2 - b^2)^{\frac{1}{2}} (b^2 - c^2)^{\frac{1}{2}}$ (b. 337). In virtue of the law of reciprocity these ridges correspond to the conical points on the Index Surface. New determination of a circular ridge by means of its vector equation and without assuming any knowledge of the existence of a wave-cusp. The relation

$$(\phi - \rho^{-2}) (\mu + \rho^{-1})^{-1} = \rho^{-1}$$
 (A₇)

^{* [}The paragraphs (s), (t) and (u), accidentally omitted in the First Edition, were first printed by the Rev. R. P. Graves in the Appendix to the Third Volume of his Life of Hamilton p. 640. They are of peculiar interest as they show that in spite of severe illness Hamilton was occupied in his work until a few days before his death which took place on the 2nd of September. In the manuscript-book nothing follows after (v). The Rev. Charles Graves in his Presidential éloge delivered to the Royal Irish Academy referred to Hamilton's labours in the following terms :---- 'It will be a satisfaction to the members of this Academy to be told that his *Elements of Quaternions*—the work upon which he was engaged with most unceasing activity for the last two years—is all but complete. I have reason to know that at no period of his life-not even when he was in the prime of health and youthful vigour-did he apply himself to his mathematical labours with more devoted diligence. These who did not actually know how he was employed, or who had formed a false estimate of his character, might imagine him indolently reposing upon his laurels, or pursuing his studies in a desultory way. Such a conception of them would be the very opposite to the true one. His diligence of late was even excessive-interfering with his sleep, his meals, his exercise, his social enjoyments. It was, I helieve, fatally injurious to his health."-Proceedings, Royal Irish Academy, vol. ix., p. 315, and Graves's Life of Sir W. R. Hamilton, vol. iii., p. 224.]

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generally determines the index-vector μ when the ray-vector ρ is given, but when $\phi - \rho^{-2}$ is a binomial the vector μ becomes indeterminate provided ρ is perpendicular to the direction β satisfying $(\phi - \rho^{-2})\beta = 0$. The vector equation of the Index-Ridge is then (p. 338)

$$\nabla \beta (\mu + \rho_0^{-1})^{-1} - \nabla \beta (\mu_0 + \rho_0^{-1})^{-1} = 0$$
 (B₇)

and the vector equation of the Wave-Ridge is (p. 339)

$$\nabla \beta (\rho + \nu_0^{-1})^{-1} - \nabla \beta (\sigma_0 + \nu_0^{-1})^{-1} = 0$$
(C₇)

where $\sigma_0 = -a^2c^2\phi\nu_0$ (CXIII., p. 337). The existence of the circular ridges may also be manifested (p. 344) by reducing the equation of the wave-surface to

$$(2\rho^2 - (a^2 - c^2) \operatorname{Sv}_0 \rho \operatorname{Sv}_1 \rho + a^2 + c^2)^2 = (a^2 - c^2)^2 \{1 - (\operatorname{Sv}_0 \rho)^2\} \{1 - (\operatorname{Sv}_1 \rho)^2\} \quad (D_7).$$

[(x). The laws of the two sets of vibrations, at a cusp and on a ridge, are illustrated by fig. 89 and are intimately connected with the two Conical Refractions, external and internal, in a biaxial crystal (p. 341). In the first case the vibration is in the tangent plane at the cusp **P** to the ellipsoid (b) (compare W_6) and has the direction of a chord **PR** of the cone resting upon the index-ridge. In the second case the vibration at R has the direction of the chord $\kappa q'$ of the wave-ridge through the point on the circle (b) (p. 340).]

[(y). In addition to the symbolic forms of the equation of the wave (A_6) and (B_6) (paragraph e) and (N₆) (paragraph m) the cyclic transformation is employed to derive this new equation (p. 332)

$$g\rho^{2} = 1 + S\lambda\rho S\lambda'\rho \pm TV\lambda\rho TV\lambda'\rho \qquad (E_{7})$$

(the upper sign belonging to one sheet, and the lower to the other sheet) with several other expressions. The bifocal transformation affords the equation (p. 344)

$$(2\rho^2 - (a^2 - c^2) \operatorname{Sv}_0 \rho \operatorname{Sv}_1 \rho + a^2 + c^2)^2 = (a^2 - c^2)^2 \{1 - (\operatorname{Sv}_0 \rho)^2\} \{1 - (\operatorname{Sv}_1 \rho)^2\} \quad (\mathbf{F}_7)$$

already referred to (w), and the equation $T(\iota\rho + \rho\kappa)^2 = (\kappa^2 - \iota^2)^2$ has been selected by Professor Tait as the basis of his paper on "Quaternion Investigations connected with Fresnel's Wave-Surface " (p. 350). Some leading expressions are written down showing the Cartesian equivalents of quaternion forms (p. 352).]

[(z). Although the italic letters i, j, k are not now much used having been superseded by general signs of operation such as S, V, T, U, K, they may be supposed to be still familiar to the student as links between quaternions and coordinates, p. 351.]

ARTICLE 423.—MacCullagh's Theorem of the Polar Plane, [(a). The vectors ρ , ρ' and ρ'' representing respectively the ray-velocities of light incident on, and refracted and reflected by, a biaxial crystal, and μ' being the index-vector for the refracted light, by all wave theories of light (p. 353)

$$\rho^2 = S\mu'\rho' = \rho''^2 = -1,$$
 (G₇); $\rho'' = -\nu\rho\nu^{-1},$ (H₇); $\nu = \mu' - \rho,$ (J₇)

where v is a normal to the face. The corresponding vectors of vibration being τ , τ' , τ'' , by all theories of tangential vibration

$$S\rho\tau = 0,$$
 (K₇); $S\mu'\tau' = 0,$ (L₇); $S\rho''\tau'' = 0$ (M₇).

[(b). To these MacCullagh adds I. that the vibration in the crystal is perpendicular to ρ' , or

$$S\rho'\tau' = 0 ; \qquad (N_7)$$

he also assumes II. the Principle of Equivalent Vibrations expressed by

$$\tau - \tau' + \tau'' = 0, \qquad (0_7)$$

III. the Principle of Vis Viva and IV. the Principle of constant Density of the Ether, jointly expressed by S

$$\gamma(\rho\tau^{2} - \rho'\tau'^{2} + \rho''\tau''^{2}) = 0 \qquad (P_{7}).$$

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[(c). Eliminating ρ'' and τ'' and solving for τ it is found (p. 354) that

$$2\tau S \rho \nu = \nabla \rho \nu' \tau'$$
 (Q₇) if $\nu' = \mu' - \rho'$ (R₇)

which includes one form of the enunciation of the Theorem of the Polar Plane as expressed by the equation (p. 355)

$$S\nu'\tau\tau' = 0. \tag{S7}$$

[(d). If ω is an arbitrary vector (p. 356) the equations had to

$$\nabla \nu \nabla \{ (\rho - \omega)\tau - (\rho' - \omega)\tau' + (\rho'' - \omega)\tau'' \} = 0$$
 (T₇)

and this equation combined with the principle of Rectangular Vibrations contained in equations (K_7) , (M_7) and (N_7) is sufficient to give the same direction of τ' and the same dependencies of τ and τ'' thereon as those expressed by (O_7) , (P_7) , (Q_7) and (S_7) . Equation (T_7) expresses that three forces τ , $-\tau'$, τ'' applied at the extremities of ρ , ρ' , ρ'' would be equivalent to a couple having its axis parallel to ν .]

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* Hamilton has called this the coefficient of underelopability. (Theory of Systems of Rays [45.], Trans. R.I.A., vol. xv.)

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24	33	30	50	190	192	81	569	100
25	36	33	51	215	220	82	573	106
26	37	33	52	220	227	83	599	140
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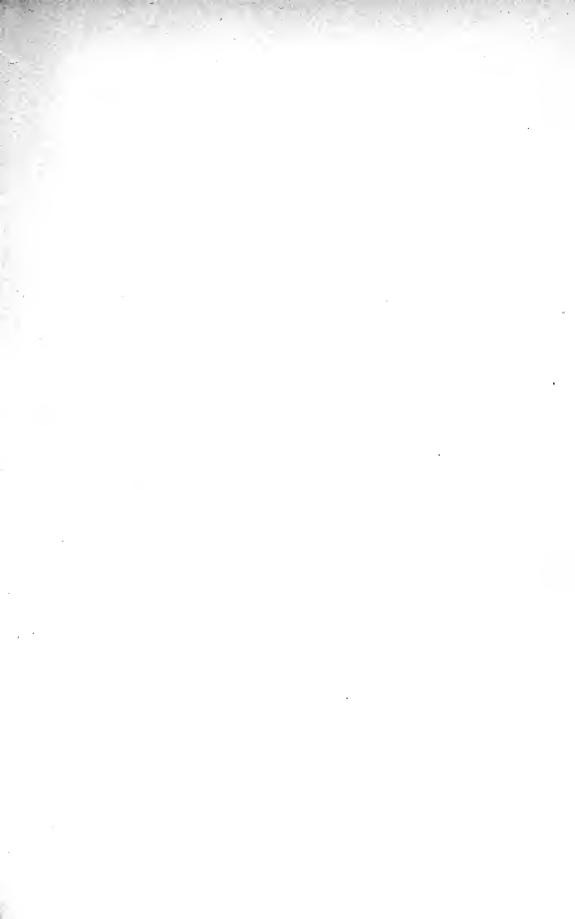
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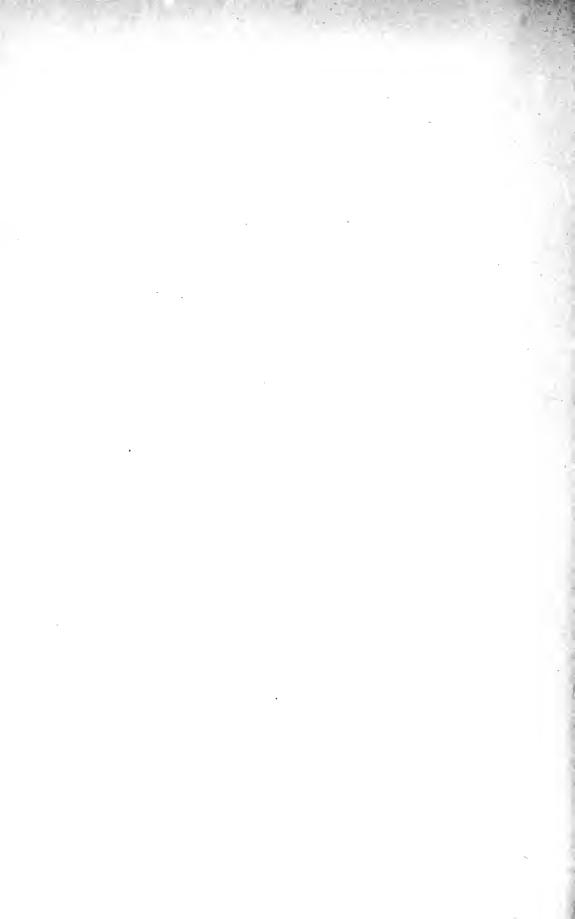
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BOOK III.

CHAPTER III.

ON SOME ADDITIONAL APPLICATIONS OF QUATERNIONS, WITH SOME CONCLUDING REMARKS

HAMILTON'S ELEMENTS OF QUATERNIONS, VOL. II.



CHAPTER III.

ON SOME ADDITIONAL APPLICATIONS OF QUATERNIONS, WITH SOME CONCLUDING REMARKS.

SECTION 1.

Remarks Introductory to this Concluding Chapter.

366. WHEN the *Third Book* of the present *Elements* was begun, it was hoped (277) that this Book might be made a much shorter one, than either of the two preceding. *That* purpose it was found impossible to accomplish, without injustice to the subject; but at least an intention was expressed (317), at the commencement of the *Second Chapter*, of rendering that Chapter the *last*: while some new *Examples* of *Geometrical Applications*, and some few *Specimens* of *Physical* ones, were promised.

367. The promise, thus referred to, has been perhaps already in part redeemed; for instance, by the investigations (315) respecting certain tangents, normals, areas, volumes, and pressures, which have served to illustrate certain portions of the theory of differentials and integrals of quaternions. But it may be admitted, that the six preceding Sections have treated chiefly of that Theory of Quaternion Differentials, including of course its Principles and Rules; and of the connected and scarcely less important theory of Linear or Distributive Functions, of Vectors and Quaternions: Examples and Applications having thus played hitherto a merely subordinate or illustrative part, in the progress of the present Volume.

368. Such was, indeed, designed from the outset to be, upon the whole, the result of the present undertaking: which was rather to teach, than to apply, the Calculus of Quaternions. Yet it still appears to be possible, without quite exceeding suitable limits, and accordingly we shall now endeavour, to condense into a short Third Chapter some Additional Examples, geometrical and

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[III. III. §§ 1, 2.

physical, of the *application* of the *principles* and *rules* of that Calculus, supposed to be already *known*, and even to have become by this time *familiar** to the reader. And then, with a few general remarks, the work may be brought to its close.

SECTION 2.

On Tangents and Normal Planes to Curves in Space.

369. It was shown (100) towards the close of the First Book, that if the *cquation* of a *curve in space*, whether *plane* or of *double* curvature, be *given* under the form,

$$\mathbf{I}...\rho=\phi(t)=\phi t,$$

where t is a scalar variable, and ϕ is a functional sign, then the *derived vector*,

II...
$$D\rho = D\phi t = \phi' t = \rho' = d\rho : dt$$
,

represents a *line* which is, or is parallel to, the *tangent* to the curve, drawn at the extremity of the variable vector ρ . If then we suppose that **T** is a point situated upon the tangent thus drawn to a curve PQ at P and that **U** is a point in the corresponding normal plane, so that the angle TPU is right, and if we denote the vectors or, or, ou by ρ , τ , v, the *equations* of the *tangent line* and *normal plane* at **P** may now be thus expressed :

III...
$$V(\tau - \rho)\rho' = 0$$
; $IV... S(\nu - \rho)\rho' = 0$;

the vector τ being treated as the only variable in III., and in like manner v as the only variable in IV., when once the curve PQ is given, and the point P is selected.

(1.) It is permitted, however, to express these last equations under other forms; for example, we may replace ρ' by $d\rho$, and thus write, for the same tangent line and normal plane,

V...
$$V(\tau - \rho)d\rho = 0$$
; VI... $S(\nu - \rho)d\rho = 0$;

where the vector differential $d\rho$ may represent any line, parallel to the tangent to the curve at \mathbf{r} , and is not necessarily small (compare again 100).

(2.) We may also write, as the equation of the tangent,

VII... $\tau = \rho + x \rho'$, where x is a scalar variable;

^{*} Accordingly, even references to former Articles will now be supplied more sparingly than before.

VIII... $d_{\rho}T(v - \rho) = 0$, or VIII'... $dT(v - \rho) = 0$, if dv = 0; because this partial differential of $T(v - \rho)$, or of \overline{PU} , is (by 334, XII., &c.),

IX... $dT(v - \rho) = S(U(v - \rho) \cdot d\rho).^*$

(3.) For the circular locus 314, (1.), or 337, (1.), of which the equation is,

X... $\rho = a^t \beta$, with Ta = 1, and Sa $\beta = 0$,

the equation of the tangent is, by VII., and by the value 337, VI. of ρ' ,

XI... $\tau = \rho + ya\rho$, where y is a new scalar variable;

the perpendicularity of the tangent to the radius being thus put in evidence.
(4.) For the plane but elliptic locus, 314, (2.), or 337, (2.), for which,

XII...
$$\rho = V.a^{t}\beta$$
, with $Ta = 1$, but not $Sa\beta = 0$,

the value 337, VIII. of ρ' shows that the tangent, at the extremity of any one semidiameter ρ , is *parallel* to the conjugate semidiameter of the curve; that is, to the one obtained by altering the excentric anomaly (314, (2.)), by a quadrant: or to the value of ρ which results, when we change t to t + 1.

(5.) For the helix, 314, (10.), of which the equation is,

XIII..., $\rho = cta + a^t\beta$, with Ta = 1, and $Sa\beta = 0$,

c being a scalar constant, we have the derived vector,

XIV...
$$\rho' = ca + \frac{\pi}{2} a^{t+1}\beta$$
; whence XV... $Sa^{-1}\rho' = c$,
XVI... $TVa^{-1}\rho' = \frac{\pi}{2}T\beta$, and XVII... $(TV:S)a^{-1}\rho' = \frac{\pi T\beta}{2c}$;

the tangent line (ρ') to the helix is therefore inclined to the axis (a) of the

* [Again we may write, as the equation of the normal plane,

(VII.) $v = \rho + \xi \rho'$, where ξ is a variable vector at right angles to ρ' ;

and as the equation of the tangent,

 $(\text{VIII.}) \quad \mathrm{d}_{\rho}\mathrm{U}(\tau-\rho)=0, \quad \text{or} \quad (\text{VIII'.}) \quad \mathrm{d}\mathrm{U}(\tau-\rho)=0, \quad \text{if} \quad \mathrm{d}\tau=0.$

Geometrically, VIII. expresses that the *length* of the line joining a point in the normal plane to the corresponding point on the curve does not vary when we pass to a consecutive point on the curve, and (VIII.) expresses that the *direction* of the line joining a point on the tangent to the corresponding point on the curve does not change when we pass to a consecutive point on the curve.]

ELEMENTS OF QUATERNIONS.

[III. III. § 2.

cylinder whereon that curve is traced, at a constant angle (a), whereof the trigonometrical tangent (tan a) is given by this formula XVII.; and accordingly, the numerator $\pi T\beta$ of that formula represents the semicircumference of the cylindric base; while the denominator 2c is an expression for half the interval between two successive spires, measured in a direction parallel to the axis. We may then write,

XVIII. . .
$$\pi T\beta = 2c \tan a = 2c \cot b$$
,

if a thus denote the constant inclination of the helix to the axis, while b denotes the constant and complementary inclination of that curve to the base, or to the circles which it crosses on the cylinder.

(6.) In general, the parallels ρ' to the tangents to a curve of double curvature, which are drawn from a fixed origin o, have a certain cone for their locus; and for the case of the helix, the equation of this cone is given by the formula XVII., or by any legitimate transformation thereof, such as the following,

XIX... SU
$$a^{-1}\rho' = \pm \cos a = \pm \sin b$$
;

it is therefore, in this case, a cone of revolution, with its semiangle = a.

(7.) As an example of the determination of a *normal plane* to a curve of double curvature, we may observe that the equation XIII. of the helix gives,

XX... $\rho^2 = \beta^2 - c^2 t^2$, and therefore XXI... $S\rho\rho' = -c^2 t$;

the equation IV. becomes therefore, for the case of this curve,

XXII... $0 = S\rho' v + c^2 t$, with the value XIV. of ρ' .

(8.) If then it be required to assign the point U in which the normal plane to the helix *meets the axis* of the cylinder, we have only to combine this equation XXII. with the condition $v \parallel a$, and we find, by XIII. and XIV.,

XXIII... $OU = v = -c^2 ta$: $Sa\rho' = cta$, XXIV... $Sa(v - \rho) = 0$;

the line PU is therefore *perpendicular* to the axis, being in fact a *normal* to the *cylinder*.

370. Another view of tangents and normal planes may be proposed, which shall connect them in calculation with Taylor's Series adapted to quaternions (342), as follows.

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ARTS. 369, 370.]

CONNEXION WITH TAYLOR'S SERIES.

(1.) Writing

I... $\rho_t = \rho_0 + u_t t \rho'_0$, or briefly, I'... $\rho_t = \rho + u t \rho'$,

the coefficient u_t or u will generally be a quaternion, but its limiting value will be positive unity, when t tends to zero as its limit; or in symbols,

II...
$$u_0 = \lim_{t=0} u = 1.$$

(2.) Admitting this, which follows either from Taylor's Series, or (in so simple a case) from the mere definition of the derived vector ρ' , we may conceive that vector ρ' to be constructed by some given line PT, without yet supposing it to be known that this line is tangential at P to the curve PQ, of which the variable vector is $oQ = \rho_t$, while $oP = \rho_0 = \rho$, so that the line PQ = $ut\rho'$ is a vector chord from P, which diminishes indefinitely with the scalar variable, t, and is small, if t be small.

(3.) Conceiving next that $\omega = \alpha R =$ the vector of some new and arbitrary point R, we may let fall a perpendicular QM on the line PR, and so decompose the chord PQ into the two rectangular lines, PM and MQ; which, when divided by the same chord, give rigorously the two (generally) quaternion quotients,

III...
$$\frac{PM}{PQ} = \frac{Su\rho'(\omega-\rho)}{u\rho'(\omega-\rho)},$$
 IV... $\frac{MQ}{PQ} = \frac{\nabla u\rho'(\omega-\rho)}{u\rho'(\omega-\rho)};$

the variable t thus disappearing through the divisions, except so far as it enters into u, which *tends* as above to 1.*

(4.) Passing then to the *limits*, we have these other rigorous equations,

V...
$$\lim_{PQ} \frac{PM}{PQ} = \frac{S\rho'(\omega-\rho)}{\rho'(\omega-\rho)}, \quad VI... \lim_{PQ} \frac{MQ}{PQ} = \frac{V\rho'(\omega-\rho)}{\rho'(\omega-\rho)};$$

* [Here $PQ = PM + MQ = PQ \cdot PR \cdot PR^{-1}$, and separately (vol. I. p. 194) $PM = S(PQ \cdot PR) \cdot PR^{-1}$ and $MQ = V(PQ \cdot PR) \cdot PR^{-1}$. So we have

$$\frac{\mathbf{PM}}{\mathbf{PQ}} = \mathbf{S}(\mathbf{PQ} \cdot \mathbf{PR}) \cdot \mathbf{PR}^{-1} + \mathbf{PQ}^{-1} = \frac{\mathbf{S}(\mathbf{PQ} \cdot \mathbf{PR})}{\mathbf{PQ} \cdot \mathbf{PR}} \text{ and } \frac{\mathbf{MQ}}{\mathbf{PQ}} = \mathbf{V}(\mathbf{PQ} \cdot \mathbf{PR}) \cdot \mathbf{PR}^{-1} \cdot \mathbf{PQ}^{-1} = \frac{\mathbf{V}(\mathbf{PQ} \cdot \mathbf{PR})}{\mathbf{PQ} \cdot \mathbf{PR}}$$

The formulæ of these sub-articles may be easily deduced from the consideration of the versor

$$U\frac{PQ}{PR} = \pm \frac{Uu\rho'}{U(\rho-\omega)},$$

or in the limit

$$\lim U \frac{PQ}{PR} = \pm U \frac{\rho'}{\rho - \omega}.$$

This reduces to a scalar when n is on the tangent, and to a right versor when it is in the normal plane. Observe that $Utu\rho' = \pm Uu\rho'$.]

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by comparing which with 369, III. and IV., we see that those two equations represent respectively, as before stated, the *tangent* and the normal plane to the proposed curve at P; because, if $\nabla \rho'(\omega - \rho) = 0$, the chord PQ tends, by V. or VI., to coincide, both in length and in direction, with its projection PM on the line PR; while on the other hand, if $S\rho'(\omega - \rho) = 0$, that projection tends to vanish, even as compared with the chord PQ; which chord tends now to coincide with its other projection MQ, or with the perpendicular to the line PR, erected so as to reach the point Q: whence PR must, in this last case, be a normal to the curve at P.

(5.) We may also investigate an equation for the normal plane, by considering it as the *limiting position* of the plane which *perpendicularly bisects the chord*. If **R** be supposed to be a point of this last plane, then, with the recent notations, the vector $\omega = \alpha \mathbf{R}$ must satisfy the condition,

VII...
$$T(\omega - \rho_t) = T(\omega - \rho_0)$$
, or VIII... $(\omega - \rho - ut\rho')^2 = (\omega - \rho)^2$,
or IX... $2Su\rho'(\omega - \rho) = t(u\rho')^2$,

in which it may be noted that $u\rho'$ is a vector (in the direction of the chord, PQ), although u itself is generally a quaternion, as before: such then is the equation of the bisecting plane, with ω for its variable vector, and its limit is,

X...
$$S\rho'(\omega - \rho) = 0$$
, as before.

(6.) The last process may also be presented under the form,

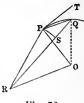
XI...
$$0 = \lim_{t \to t} t^{-1} \{T(\omega - \rho_t) - T(\omega - \rho_0)\} = D_t T(\omega - \rho_t), \text{ when } t = 0;$$

and thus the equation 369, VIII. may be obtained anew.

(7.) Geometrically, if we set off on RQ a portion RS equal in length to RP, as in the annexed fig. 76, we shall have the limiting equation,

XII. . . $\pm \overline{sq} : \overline{Pq} = (\overline{Rq} - \overline{RP}) : \overline{Pq} = (ultimately) - \cos RPT;$ which agrees with 369, IX.*

(8.) If then the point R be taken out of the normal plane at P, this *limit* of the *quotient*, $\overline{RQ} - \overline{RP}$ divided by \overline{PQ} , has a *finite value*, positive or negative; and if the *chord* PQ be called *small* of the *first order*, the *difference* of *distances* of its



[III. III. § 2.

Fig. 76.

extremities from R may then be said to be *small* of the *same* (first) order. But if R be taken *in* the normal plane at P (and not coincident with that

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^{*} $[\overline{sq} \text{ denotes the length of the vector sq.}]$

ARTS. 370, 371.]

EXAMPLES.

point **p** itself), this difference of distances may then be said to be small, of an order higher than the first: which answers to the evanescence of the first differential of the tensor, $T(\omega - \rho)$ in XI., or $T(\nu - \rho)$ in 369, VIII'.

371. A curve may occasionally be represented in quaternions, by an equation which is not of the *form*, 369, I., although it must always be conceived capable of *reduction* to that form: for instance, this new equation,

I. . .
$$\operatorname{Va}\rho$$
 . $\operatorname{V}\rho a' = (\operatorname{Va}a')^2$, with $\operatorname{TVa}a' > 0$,

is not immediately of the form $\rho = \phi t$, but it is reducible to that form as follows,

$$11...\rho = ta + t^{-1}a'.$$

An equation such as I. may therefore have its *differential* or its *derivative* taken, with respect to the scalar variable t on which ρ is thus *conceired* to depend, even if the exact *law* of such dependence be unknown: and $d\rho$, or ρ' , may then be changed to the tangential vector $\omega - \rho$ to which it is parallel, in order to form an *equation* of the *tangent*, or a *condition* which the vector ω of a point on that sought line must satisfy.

(1.) To pass from I. to II., we may first operate with the sign V, which gives,

III...
$$\rho Saa' \rho = 0$$
, or simply, III'... $Saa' \rho = 0$;

whence, t and t' being scalars, we may write,

IV...
$$\rho = ta + t'a'$$
, $Va\rho = t'Vaa'$, $V\rho a' = tVaa'$, $tt' = 1$,

and the required reduction is effected: while the *return* from II. to I., or the *elimination* of the scalar t, is an even easier operation.

(2). Under the form II., it is at once seen that ρ is the vector of a *plane hyperbola*, with the origin for *centre*, and the lines *a*, *a'* for *asymptotes*; and accordingly all the properties of such a curve may be deduced from the expression II., by the rules of the present Calculus.

(3.) For example, since the derivative of that expression is,

$$\mathbf{V}\ldots\,\boldsymbol{\rho}'\,=\,\boldsymbol{a}\,-\,t^{-2}\boldsymbol{a}',$$

the tangent may (comp. 369, VII.) have its equation thus written:

VI...
$$\omega = (t+x)a + t^{-2}(t-x)a';$$

it intersects therefore the lines a, a' in the points of which the vectors are 2ta, $2t^{-1}a'$; so that (as is well known) the *intercept*, upon the tangent,

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between the asymptotes, is bisected at the point of contact: and the intercepted area is constant, because $V(ta.t^{-1}a') = Vaa'$, &c.

(4.) But we may also operate *immediately*, as above remarked, on the form I.; and thus arrive (by substitution of $\omega - \rho$ for $d\rho$, &c.) at the equation of conjugation,

VII. . .
$$\nabla a \omega \cdot \nabla \rho a' + \nabla a \rho \cdot \nabla \omega a' = 2 (\nabla a a')^2$$
,

which expresses (comp. 215, (13.), &c.) that if $\rho = \delta P$, and $\omega = \delta R$, as before, then either R is on the *tangent* to the curve, at the point P, or at least *each* of these two points is situated on the *polar* of the other, with respect to the same hyperbola.

(5.) Again, it is frequently convenient to consider a curve as the intersection of two surfaces; and, in connexion with this conception, to represent it by a system of two scalar equations, not explicitly involving any scalar variable: in which case, both equations are to be differentiated, or derivated, with reference to such a variable understood, and $d\rho$ or ρ' deduced, or replaced by $\omega - \rho$ as before.

(6.) Thus we may substitute, for the equation I., the system of the two following (whereof the first had occurred as III'.):

VIII. . . $Saa'\rho = 0$, $\rho^2 Saa' - Sa\rho Sa'\rho = (Vaa')^2$;

and the derivated equations corresponding are,

IX. . .
$$Saa'\rho' = 0$$
, $2Saa'S\rho\rho' - Sa\rho'Sa'\rho - Sa\rhoSa'\rho' = 0$;

or, with the substitution of $\omega - \rho$ for ρ' , &c.,

X... Saa' $\omega = 0$, $2Saa'S\rho\omega - Sa\omega Sa'\rho - Sa\rho Sa'\omega = 2(Vaa')^2$;

the last of which might also have been deduced from VII., by operating with S.

(7.) And it may be remarked that the two equations VIII. represent respectively in general a *plane* and an *hyperboloid*, of which the *intersection* (5.) is the *hyperbola* I. or II.; or a plane and an *hyperbolic cylinder*, if Saa' = 0.*

• [If $\rho = \frac{\phi(t)}{f(t)}$ where $\phi(t)$ is a rational and integral vector function of degree *m* in *t*, and

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f(t) a rational and integral scalar function of degree *n*, the degree of the curve is equal to the greater of the two integers *m* and *n*. This is evident when we substitute for ρ in the equation of an arbitrary plane, $S\lambda\rho = 1$, for we obtain a scalar equation in *t* whose roots determine the points in which the curve cuts the plane. Curves of this kind are *unicursal*. In general there is some

SECTION 3.

On Normals and Tangent Planes to Surfaces.

372. It was early shown (100, (9.)), that when a *curred surface* is represented by an equation of the form,

$$\mathbf{I}\ldots\,\boldsymbol{\rho}\,=\,\boldsymbol{\phi}\,(\boldsymbol{x},\boldsymbol{y}),$$

in which ϕ is a functional sign, and x, y are two independent and scalar variables, then either the *two partial differentials*, or the two *partial derivatives*, of the *first order*,

II...
$$d_x \rho$$
, $d_y \rho$, or, III... $D_x \rho$, $D_y \rho$,

represent *two tangential vectors*, or at least vectors *parallel* to *two tangents* to the surface, drawn at the extremity or *term* \mathbf{P} of ρ ; so that the *plane* of these two differential vectors, or of lines parallel to them, is (or is parallel to) the *tangent plane* at that point: and the principle has been since exemplified, in 100, (11.) and (12.), and in the sub-articles to 345, &c. It follows that any *vector* ν , which is *perpendicular to both* of two such *non-parallel* differentials, or derivatives, must (comp. 345, (11.)) be a *normal vector* at P, or at least one having the *direction* of the normal to the surface at that point; so that each of the two vectors,

IV...
$$V \cdot d_x \rho d_y \rho$$
, $V \ldots V \cdot D_x \rho D_y \rho$,

if actual, represents such a normal.

(1.) As an additional example, let us take the case of the *ruled paraboloid*, on which a given *gauche quadrilateral* ABCD is *superscribed*. The expression for the vector ρ of a variable point P of this surface, considered as a function of two independent and scalar variables, x and y, may be thus written (comp. 99, (9.)):

VI. . .
$$\rho = xya + (1-x)y\beta + (1-x)(1-y)\gamma + x(1-y)\delta;$$

where the supposition y = 1 places the point P on the line AB; x = 0 places it on BC; y = 0, on CD; and x = 1, on DA.

As examples of the equations of curves :---

 $\rho = \frac{at^2 + 2\beta t + \gamma}{at^2 + 2bt + c}$ is a conic provided there is no common factor in the numerator or denominator;

 $\rho = (\phi + t)^m a$, in which ϕ is a linear vector function and m a constant scalar, represents a right line when m = 1, a twisted cubic when m = -1, and a twisted quartic when $m = \frac{1}{2}$.

irrationality in the functions of t, and the result of substitution in the equation of the plane must be rationalized before the degree of the curve can be determined.

VII. . .
$$D_{x\rho} = y(a-\beta) + (1-y)(\delta-\gamma);$$
 $D_{y\rho} = x(a-\delta) + (1-x)(\beta-\gamma);$

these then represent the directions of *two* distinct *tangents* to the paraboloid VI., at what may be called *the point* (x, y); whence it is easy to deduce the *tangent plane* and the *normal* at that point, by constructions on which we cannot here delay, except to remark that if (comp. fig. 31, Art. 98) we draw two right lines, qs and Rr, through P, so as to cut the sides AB, BC, CD, DA of the quadrilateral in points q, R, s, T, we shall have by VI. the vectors,

VIII...
$$\begin{cases} oQ = xa + (1-x)\beta, & OR = y\beta + (1-y)\gamma, \\ os = x\delta + (1-x)\gamma, & OT = ya + (1-y)\delta, \end{cases}$$

and therefore, by VII.,

IX...
$$D_x \rho = RT$$
, $D_y \rho = SQ$;

so that these two tangents are simply the two generating lines of the surface, which pass through the proposed point P.*

(3.) For example, at the point (1, 1), or A, the *tangents* thus found are the *sides* BA, DA, and the *tangent plane* is that of the *angle* BAD, as indeed is evident from geometry.

(4.) Again, the equation of the screw surface (comp. 314, XVI.),

X... $\rho = cxa + ya^x\beta$, with Ta = 1, and $Sa\beta = 0$,

gives the two tangents,

XI...
$$D_x \rho = ca + \frac{\pi}{2} y a^{x+1} \beta$$
, $D_y \rho = a^x \beta$,

whereof the latter is perpendicular to the former, and to the axis a of the cylinder; so that the corresponding *normal* to the surface X. at the point (x, y) is represented by the product,

XII...
$$\nu = D_x \rho$$
. $D_y \rho = c a^{x+1} \beta + \frac{\pi}{2} y \beta^2 a$.

373. Whenever a variable vector ρ is thus expressed or even conceived to be expressed, as a function of two scalar variables, x and y (or s and t, &c.),

$$\rho = y \circ q + (1 - y) \circ s$$
, or $\rho = x \circ r + (1 - x) \circ R$.]

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^{* [}In VIII, Q and s are two variable points dividing homographically AB and DC, and R and T divide nc and AD homographically. The ruled paraboloid is the locus of lines joining corresponding points of the homographic divisions on AB and DC, or on BC and AD, for VI. may be written in either of the forms

ARTS. 372, 373.] CONNEXION WITH QUATERNION DIFFERENTIALS. 13

if we assume any three diplanar vectors, such as α , β , γ (or ι , κ , λ , &c.), the three scalar expressions, $S_{\alpha\rho}$, $S_{\beta\rho}$, $S_{\gamma\rho}$ (or $S_{\iota\rho}$, $S_{\kappa\rho}$, $S_{\lambda\rho}$, &c.), will then be functions of the same two scalar variables; and will therefore be connected with each other by some one scalar equation, of the form,

I...
$$F(S_{\alpha\rho}, S_{\beta\rho}, S_{\gamma\rho}) = 0,$$

or briefly,

II... $f\rho = C$;

where C is a scalar constant, introduced (instead of zero) for greater generality of expression; and F, f are used as functional but scalar signs. If then (comp. 361, XIV.) we express the *first differential* of this scalar function $f\rho$ under the form,

III...
$$d_{f\rho} = 2S_{\nu}d\rho$$
,

in which ν is a certain *derived vector*, and is *here* considered as being (at least implicitly) a vector function (like ρ) of the *two scalar variables* above mentioned, we shall have the two equations,

IV...
$$S\nu d_x \rho = 0$$
, $S\nu d_y \rho = 0$,

or these two other and corresponding ones,

$$\mathbf{V}...\mathbf{S}\nu\mathbf{D}_{x}\rho=0, \quad \mathbf{S}\nu\mathbf{D}_{y}\rho=0;$$

from which it follows (by 372) that ν has the direction of the normal to the surface I. or II., at the point P in which the vector ρ terminates. Hence the *equation* of that *normal* (with ω for its variable vector) may, under these conditions, be thus written :

VI...
$$\nabla \nu (\omega - \rho) = 0$$
;

and the corresponding equation of the tangent plane at the same point P is,

VII...
$$S_{\nu}(\omega - \rho) = 0.$$

(1.) For example, if we take the expression 308, XVIII., or 345, X1I., namely

VIII...
$$\rho = rk^{t}j^{s}kj^{-s}k^{-t}$$
, in which $kj^{-s} = j^{s}k$, &c.,

treating the scalar r as constant, but s and t as variable, we have then (comp. 345, XIV.), the equations, a denoting any unit-vector,

$$IX...Si\rho = rS.a^{2t}S.a^{2s+1}, Sj\rho = rS.a^{2t-1}S.a^{2s+1}, Sk\rho = rS.a^{2s+2};$$

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between which s and t can be eliminated, by simply adding their squares, because $(Sa^t)^2 + (Sa^{t-1})^2 = 1$, by 315, V., if Ta = 1. In this manner then we arrive at equations of the forms I. and II., namely (comp. 357, VII., and 308, (10.) and (13.)),

X...
$$(Si\rho)^2 + (Sj\rho)^2 + (Sk\rho)^2 - r^2 = 0$$
,
XI... $f\rho = \rho^2 = -r^2 = const.$, or XI'... $T\rho = r$;

and

which last results had indeed been otherwise obtained before.*

(2.) With this form XI. of f_{ρ} , we have the differential expression of the first order,

XII...
$$df \rho = 2S\nu d\rho = 2S\rho d\rho$$
, whence XIII... $\nu = \rho$;

and if we still conceive that ρ is, as above, some vector function of two scalar variables, s and t, although the particular law VIII. of its dependence on them may now be supposed to be unknown (or to be forgotten), we may write also,

X1V. . .
$$\frac{1}{2}$$
d $f\rho = S\nu d\rho = S\rho d\rho = S\rho (d_s + d_t)\rho = S\rho D_s\rho \cdot ds + S\rho D_t\rho \cdot dt;$

if then the function $f\rho$ have (as above) a value, $= -r^2$, which is constant, or is independent of both the variables, s and t, while their differentials are arbitrary, and are independent of each other, we shall thus have separately (comp. V., and 337, XIII., XVII.),

$$XV...S\rho D_{s}\rho = 0, \quad S\rho D_{t}\rho = 0.$$

The radius ρ of the sphere XI. is therefore in this way seen to have the direction of the normal at its own extremity, because it is perpendicular to two distinct tangents, $D_{s\rho}$ and $D_{t\rho}$, at that point; which are indeed, in the present ease, perpendicular to cach other also (337, (8.)).

(3.) Instead of treating the *two* scalar variables, x and y, or s and t, &c., as both entirely arbitrary and independent, we may conceive that one is an arbitrary (but scalar) function of the other; and then the vector v, determined by the equation III., will be seen anew to be the normal at the extremity P of ρ , because it is perpendicular to the tangent at P to an arbitrary curve upon the surface, which passes through that point: or (otherwise stated)

* [Of course
$$\rho^2 = r^2 k^t j^* k j^{-s} k^{-t} \cdot k^t j^* k j^{-s} k^{-t} = r^2 k^2 = -r^2$$
.]

because it is a line in an *arbitrary normal plane* at P, if a normal plane to a *curve* on a surface be called (as usual) a normal plane to that *surface* also.

(4.) For example, if we conceive that s in VIII. is thus an arbitrary function of t, the last expression XIV. will take the form,

XVI. . .
$$0 = \frac{1}{2} d_t f \rho = S \cdot \rho (s' D_s \rho + D_t \rho) dt$$
, if $ds = s' dt$;

whence, dt being still arbitrary, we have the one scalar equation,

XVII...S.
$$\rho(s'D_s\rho + D_t\rho) = 0$$
, or XVIII... $\rho \perp s'D_s\rho + D_t\rho$,

and although, on account of the arbitrary coefficient s', this one equation XVII. is equivalent to the system of the two equations XV., yet it immediately signifies, as in XVIII., that the directed radius ρ , of the sphere XI., is perpendicular to the arbitrary tangent, $s'D_{s\rho} + D_{t\rho}$; or to the tangent to an arbitrary spherical curve through P, the centre o and tensor $T\rho$ (or undirected radius, r) remaining as before.

(5.) As regards the *logic* of the subject, it may be worth while to read again the *proof* (331), of the validity of the rule for *differentiating a function* of a function; because this *rule* is virtually employed, when after thus reducing, or conceiving as reduced, the scalar function f_{ρ} of a vector ρ , to another scalar function such as Ft of a scalar t, by treating ρ as equal to some vector function ϕt of this last scalar, we infer that

XIX...
$$dFt = df\phi t = 2S \cdot \nu d\phi t$$
, if $df\rho = 2S\nu d\rho$, as before.

(6.) And as regards the *applications* of the formulæ VI. and VII., or of the equations given by them for the *normal* and *tangent plane* to a *surface* generally, the difficulty is only to *select*, out of a multitude of examples which might be given: yet it may not be useless to add a *few* such here, the case of the *sphere* having of course been only taken to illustrate the *theory*, because the normal property of its *radii* was manifest, independently of any calculation.

(7.) Taking then the equation of the ellipsoid, under the form,

XX...
$$T(\iota \rho + \rho \kappa) = \kappa^2 - \iota^2$$
, 282, XIX.,

of which the first differential may (see the sub-articles to 336) be thus written,

XXI...
$$0 = S \cdot \{(\iota - \kappa)^2 \rho + 2(\iota S \kappa \rho + \kappa S \iota \rho)\} d\rho = S \nu d\rho,$$

and introducing an auxiliary vector, on or ξ , such that

XXII... ON =
$$\xi = -2(\iota - \kappa)^{-2}(\iota S\kappa\rho + \kappa S\iota\rho)$$
,

we have $\nu \parallel \rho - \xi$, and may write, as the equation of the normal at the extremity P of ρ , the following,

XXIII...V.
$$(\xi - \rho) (\omega - \rho) = 0$$
, or XXIV... $\omega = \rho + x(\xi - \rho)$,

in which x is a scalar variable (comp. 369, VII.); making then x = 1, we see that ξ is the vector of the point N in which the normal intersects the plane of the two fixed lines ι , κ , supposed to be drawn from the origin, which is here the *centre* of the ellipsoid.

(8.) If we look back on the sub-articles to 216 and 217, we shall see that these lines ι , κ have the directions of the *two real cyclic normals*, or of the normals to the *two* (real) *cyclic planes*; which planes are now reprosented by the two equations,

$$XXV...S_{l\rho} = 0, S_{\kappa\rho} = 0.$$

Accordingly the equation XX. of the ellipsoid may be put (comp. 336, 357, 359) under the cyclic forms,

XXVI...
$$S\rho\phi\rho = (\iota^2 + \kappa^2)\rho^2 + 2S\iota\rho\kappa\rho$$

= $(\iota - \kappa)^2\rho^2 + 4S\iota\rho S\kappa\rho = (\kappa^2 - \iota^2)^2 = \text{const.};$

hence each of the two diametral planes XXV. cuts the surface in a circle, the common radius of these two circular sections being

XXVII...
$$T\rho = \frac{T\iota^2 - T\kappa^2}{T(\iota - \kappa)} = b,$$

where b denotes, as in 219, (1.), the length of the mean semiaxis of the ellipsoid; and in fact, this value of $T\rho$ can be at once obtained from the equation XX., by making either $\rho = -\rho \iota$, or $\rho \kappa = -\kappa \rho$, in virtue of XXV.

(9.) By the sub-article last cited, the greatest and least semiaxes have for their lengths,

XXVIII...
$$a = T\iota + T\kappa, \quad c = T\iota - T\kappa;$$

and the construction in 219, (2.) shows (by fig. 53, annexed to 217, (4.)) that these three semiaxes a, b, c have the respective directions of the lines,

XXIX...
$$\iota T \kappa - \kappa T \iota$$
, V $\iota \kappa$, $\iota T \kappa + \kappa T \iota$;

ART. 373.] NORMALS TO SURFACES OF THE SECOND ORDER.

all which agrees with the rectangular transformation,

$$\begin{aligned} \mathbf{XXX.} \quad & \cdot \quad \mathbf{1} = \frac{\mathbf{S}\rho\phi\rho}{(\kappa^2 - \iota^2)^2} = \left(\frac{\mathbf{T}(\iota\rho + \rho\kappa)}{\kappa^2 - \iota^2}\right)^2 \\ & = \left(\frac{\mathbf{S} \cdot \rho \,\mathbf{U}(\iota\mathbf{T}\kappa - \kappa\mathbf{T}\iota)}{\mathbf{T}\iota + \mathbf{T}\kappa}\right)^2 + \left(\frac{\mathbf{T}(\iota - \kappa)\mathbf{S} \cdot \rho \,\mathbf{U}\mathbf{V}\iota\kappa}{\mathbf{T}\iota^2 - \mathbf{T}\kappa^2}\right)^2 + \left(\frac{\mathbf{S} \cdot \rho \,\mathbf{U}(\iota\mathbf{T}\kappa + \kappa\mathbf{T}\iota)}{\mathbf{T}\iota - \mathbf{T}\kappa}\right)^2, \end{aligned}$$

in deducing which (comp. 359, (1.)) from 357, VIII., by means of the formulæ 357, XX. and XXI., we employ the values (comp. XXVI.),

XXXI...
$$y = \iota^2 + \kappa^2$$
, $\lambda = 2\iota$, $\mu = \kappa$.

(10.) The fixed plane (7.), of the cyclic normals ι and κ (8.), is therefore also the plane of the extreme semiaxes, a and c (9.), or that which may be called perhaps the principal plane* of the ellipsoid : namely, the plane of the generating triangle (218, (1.)), in that construction of the surface (217, (6.) or (7.)) which is illustrated by fig. 53, and was deduced as an interpretation of the quaternion equation XX., or of the somewhat less simple form 217, XVI., with the value $T\iota^2 - T\kappa^2$ of t^2 .

(11.) Let n denote the length of that portion of the normal, which is intercepted between the surface and the principal plane (10.), so that, by (7.),

XXXII...
$$n = \overline{NP} = T(\rho - \xi), \quad n^2 = -(\rho - \xi)^2,$$

with the value XXII. of ξ . Let $\sigma = os$ be the vector of a point s on the surface of a new or auxiliary *sphere*, described about the point N as centre, with a radius = n, and therefore *tangential* to the *ellipsoid* at P; and let us inquire in what *curve* or *curves*, real or imaginary, does this sphere *cut* the ellipsoid.

(12.) The equations (comp. 371, (5.)) of the sought intersection are the two following,

XXXIII...
$$(\sigma - \xi)^2 + n^2 = 0$$
, and XXXIV... $T(\iota \sigma + \sigma \kappa) = \kappa^2 - \iota^2$;

whereof the first expresses that s is a point of the sphere, and the second that it is a point of the ellipsoid; while ρ or or enters virtually into XXXIII., through ξ and n, but is *here* treated as a *constant*, the point P being now supposed to be a *given* one.

^{*} This plane may also be said to be the plane of the principal elliptic section (219, (9.)); or it may be distinguished (comp. the Note to page 240, vol. i.) as the plane of the *focal hyperbola*, of which important curve we shall soon assign the equation in quaternions.

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(13.) We shall remove (18.) the origin to this point P of the ellipsoid, if we write,

XXXV... $\sigma = \rho + \sigma'$, or XXXV'... $\sigma' = \sigma - \rho = Ps$;

and thus we obtain the new or transformed equations,

XXXVI... $0 = \sigma'^2 + 2S(\rho - \xi)\sigma'$, XXXVII... $0 = N(\iota\sigma' + \sigma'\kappa) + 2S\nu\sigma'$; in which (as in (7.), comp. also 210, XX.),

and

XXXVIII. . .
$$\nu = (\iota - \kappa)^2 \rho + 2(\iota S_{\kappa\rho} + \kappa S_{\ell}\rho) = (\iota - \kappa)^2 (\rho - \xi)$$

XXXIX... $N(\iota\sigma' + \sigma'\kappa) = (\iota - \kappa)^2 \sigma'^2 + 4S\iota\sigma'S\kappa\sigma'.$

(14.) Eliminating then σ'^2 , we obtain from the two equations XXXVI. and XXXVII. this other,

XL. . .
$$S\iota\sigma'$$
. $S\kappa\sigma' = 0$;

which like them is of the second degree in σ' , but breaks up, as we see, into two linear and scalar factors, representing two distinct planes, parallel by XXV. to the two diametral and cyclic planes of the ellipsoid. The sought intersection consists then of a pair of (real) circles, upon that given surface; namely, two circular (but not diametral) sections, which pass through the given point P.

(15.) Conversely, because the equations XXXVII. XXXVIII. XXXIX. XL. give XXXVI. and XXXIII., with the foregoing values of ξ and n, it follows that these *two* plane sections of the ellipsoid at P are on one common sphere, namely that which has N for centre, and n for radius, as above; and thus we might have found, without differentials, that the line PN is the normal at P; or that this normal crosses the principal plane (10.), in the point determined by the formula XXII.

(16.) In general, the cyclic form of the equation of any central surface of the second order, namely the form (comp. 357, II.),

XLI. . .
$$S\rho\phi\rho = g'\rho^2 + 2S\lambda\rho S\mu\rho = C = const.,$$

shows that the *two circles* (real or imaginary) in which that surface is cut by any *two planes*,

XLII... $S\lambda \rho = l$, $S\mu \rho = m$,

drawn *parallel* respectively to the two real *cyclic planes*, which are jointly represented (comp. XL., and 216, (7.)) by the one equation,

XLIII...
$$S\lambda\rho S\mu\rho = 0$$
,

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are homospherical, being both on that one sphere of which the equation is,

XLIV. . .
$$g'\rho^2 + 2(lS\mu\rho + mS\lambda\rho) = 2lm + C.$$

(17.) But the centre (say N) of this new sphere, has for its vector (say ξ),

XLV... ON = $\xi = -g^{\prime-1}(l\mu + m\lambda)$;

it is therefore situated in the plane of the two real cyclic normals, λ and μ ; and if l and m in XLV. receive the values XLII., then this new ξ is the vector of intersection of that plane, with the normal to the surface at P: because it is (comp. (15.)) the vector of the centre of a sphere which touches (though also cutting, in the two circular sections) the surface at that point.

(18.) We can therefore thus infer (comp. again (15.)), without the differential calculus, that the line,

XLVI...
$$g'(\rho - \xi) = g'\rho + \lambda S\mu\rho + \mu S\lambda\rho = \phi\rho$$
,

as having the direction of NP, is the normal at P to the surface XLI.; which agrees with, and may be considered as confirming (if confirmation were required), the conclusion otherwise obtained through the differential expression (361),

XLVII...
$$dS\rho\phi\rho = 2S\nu d\rho = 2S\phi\rho d\rho$$
;

the linear function $\phi \rho$ being here supposed (comp. 361, (3.)) to be selfconjugate.

(19.) Hence, with the notation 362, I., the equation of the tangent plane to a central surface of the second order, at the same point P, may by VII. be thus written,

XLVIII... $f(\omega, \rho) = C$, if $S\rho\phi\rho = C = \text{const.}$;

in which it is to be remembered, that

XLIX...
$$f(\omega, \rho) = f(\rho, \omega) = S\omega\phi\rho = S\rho\phi\omega.$$

(20.) And if we choose to *interpret* this equation XLVIII., which is only of the *first degree* (362) with respect to *each* separately of the *two vectors*, ρ and ω , or or and or, and involves them *symmetrically*, without requiring that P shall be a point on the surface, we may then say (comp. 215, (13.), and 316, (31.)), that the formula in question is an *equation of conjugation*, which expresses that *each* of the two points P and R, is situated in the *polar plane* of the other.

[III. 111., § 3.

(21.) In general, if we suppose that the *length* and *direction* of a line ν are so adjusted as to satisfy the *two* equations (comp. 336, XII. XIII. XIV.),

L... $S\nu\rho = 1$, $S\nu d\rho = 0$, and therefore also LI... $S\rho d\nu = 0$;

then, because the equation VII. of the *tangent plane* to any curved surface may now be thus written,

$$\text{LII...} S_{\nu}(\omega - \nu^{-1}) = 0,$$

it follows that ν^{-1} represents, in length and direction, the *perpendicular from* o on that tangent plane at \mathbf{P} ; so that ν itself represents the reciprocal of that *perpendicular*, or what may be called (comp. 336, (8.)) the vector of proximity, of the tangent plane to the origin. And we see, by LI., that the two vectors, ρ and ν , if drawn from a common origin, terminate on two surfaces which are, in a known and important sense (comp. the sub-arts. to 361), reciprocals* of one another : the line ρ^{-1} , for instance, being the perpendicular from o on the tangent plane to the second surface, at the extremity of the vector ν .

374. In the two preceding Articles, we have treated the symbol $d\rho$ as representing (rigorously) a tangent to a curve on a given surface, and therefore also to that surface itself; and thus the formula $S_{\nu}d\rho = 0$ has been considered as expressing that ν has the direction of the normal to that surface, because it is perpendicular to two tangents (372), and therefore generally to every tangent (373), which can be drawn at a given point P. But without at present introducing any other \dagger signification for this symbol $d\rho$, we may interpret in another way, and with a reference to chords rather than to curves, the differential equation,

I. . .
$$df\rho = 2S\nu d\rho$$
,

$$0 = \Delta f \rho = (\epsilon^{d} - 1) f \rho = d f \rho + \frac{1}{2} d^{2} f \rho + \& e.;$$

but with this meaning of the symbol $d\rho$, the equation $df\rho = 0$, or $S_{P}d\rho = 0$, is no longer rigorous, and must (for rigour) be replaced by such an equation as the following,

 $0 = 2S\nu d\rho + Sd\nu d\rho + R$, if $df\rho = 2S\nu d\rho$, as before;

the remainder R vanishing, when the surface is only of the second order (comp. 362, (3.)). Accordingly this last form is useful in some investigations, especially in those which relate to the curvatures of normal sections: but for the present it seems to be clearer to adhere to the recent signification of $d\rho$, and therefore to treat it as still denoting a tangent, which may or may not be small.

^{*} Compare the Note to page 549, vol. i.

[†] It is permitted, for example, by general principles above explained, to treat the differential dp as denoting a chordal vector, or to substitute it for $\Delta \rho$, and so to represent the differenced equation of the surface under the form (comp. 342),

ARTS. 373, 374.] CONNEXION WITH TAYLOR'S THEOREM.

supposed still to be a rigorous one (in virtue of our definitions of differentials, which do not require that $d\rho$ should be *small*); and may *still* deduce from it the normal property of the vector ν , but now with the help of Taylor's Series adapted to quaternions (comp. 342, 370). In fact, that series gives here a differenced equation, of the form,

II. . .
$$\Delta f \rho = 2 \mathrm{S} \nu \Delta \rho + R$$
;

where R is a scalar *remainder* (comp. again 342), having the property that

III... lim. $(R: T\Delta \rho) = 0$, if lim. $T\Delta \rho = 0$;

whence

IV... lim.
$$(\Delta f \rho : T \Delta \rho) = 2$$
 lim. $S \nu U \Delta \rho$,

whatever the ultimate direction of $\Delta \rho$ may be. If then we conceive that $\Delta \rho$ represents a small and indefinitely decreasing chord PQ of the surface, drawn from the extremity P of ρ , so that

V. . .
$$\Delta f \rho = f(\rho + \Delta \rho) - f \rho = 0$$
, and lim. $T \Delta \rho = 0$,

the equation IV. becomes simply,

VI. . . lim.
$$S_{\nu}U\Delta\rho = 0$$
;

and thus proves, in a new way, that v is normal to the surface at the proposed point P, by proving that it is ultimately perpendicular to all the chords PQ from that point, when those chords become indefinitely small, or tend indefinitely to vanish.

(1.) For example, if

VII... $f\rho = \rho^2$, $\nu = \rho$, then VIII... $R = \Delta \rho^2$, and $R: T\Delta \rho = -T\Delta \rho$;

thus, for every point of space, we have rigorously, with this form of f_{ρ} ,

IX...
$$\Delta f \rho$$
: $T \Delta \rho = 2 S \rho U \Delta \rho - T \Delta \rho$;

and for every point q of the spheric surface, $f_{\rho} = const.$, we have with equal rigour,

X... $2 S_{\rho} U \Delta_{\rho} = T \Delta_{\rho}$, or XI... $\overline{PQ} = 2 \overline{OP}$. cos opq;

in fact, either of these two last formulæ expresses simply, that the *projection* of a diameter of a sphere, on a conterminous chord, is equal to that chord itself, and of course diminishes with it. (2.) Passing then to the *limit*, or conceiving the point q of the surface to *approach* indefinitely to r, we derive the limiting equations,

XII... lim.
$$S\rho U\Delta \rho = 0$$
; XIII... lim. $\cos \sigma \rho = 0$;

either of which shows, in a new way, that the radii of a sphere are its normals; with the analogous result for other surfaces, that the vector v in I. has a normal direction, as before: because its projection on a chord PQ tends indefinitely to diminish with that chord.

(3.) We may also interpret the differential equation I. as expressing, through II. and III., that the *plane* 373, VII., which is drawn through the point P in a direction perpendicular to ν , is the *tangent plane* to the surface: because the projection of the chord $\Delta \rho$ on the normal ν to that plane, or the perpendicular distance,

XIV... - S(U_{$$\nu$$}. $\Delta \rho$) = $\frac{1}{2}R \cdot T\nu^{-1}$,

of a near point Q from the plane thus drawn through P, is small of an order higher than the first (comp. 370, (8.)), if the chord PQ itself be considered as small of the first order.

375. This occasion may be taken (comp. 374, I. II. III.) to give a *new Enunciation of Taylor's Theorem*, in a form *adapted to Quaternions*, which has some advantages over that given (342) in the preceding Chapter. We shall therefore now express that important *Theorem* as follows :--

" If none of the m + 1 functions,

I. . . fq,
$$dfq$$
, d^2fq . . . d^mfq , in which $d^2q = 0$,

become infinite in the immediate vicinity of a given quaternion q, then the quotient,

II...
$$Q = \left\{ f(q + dq) - fq - dfq - \frac{d^2 fq}{2} - \frac{d^3 fq}{2 \cdot 3} - \&c. - \frac{d^m fq}{2 \cdot 3 \cdot m} \right\} : \frac{dq^m}{2 \cdot 3 \cdot m},$$

can be made to tend indefinitely to zero, for any ultimate value of the versor Udq, by indefinitely diminishing the tensor Tdq."

(1.) The *proof* of the theorem, as thus enunciated, can easily be supplied by an attentive reader of Articles 341, 342, and their sub-articles; a few *hints* may however here be given.

[III. m. § 3.

ABTS. 374, 375.] NEW ENUNCIATION OF TAYLOR'S THEOREM.

(2.) We do not now suppose, as in 342, that $d^m fq$ must be different from zero; we only assume that it is not infinite: and we add, to the expression 342, VI. for Fx, the term,

III...
$$\frac{-x^m \mathrm{d}^m f q}{2 \cdot 3 \cdot \ldots \cdot m}$$
.

(3.) Hence each of the expressions 342, VII., for the successive derivatives of Fx, receives an additional term; the last of them thus becoming,

IV...
$$D^m F x = F^{(m)} x = d^m f(q + x dx) - d^m f q;$$

so that we have now (comp. 342, X.) the values

 $\mathbf{V}...F\mathbf{0} = \mathbf{0}, F'\mathbf{0} = \mathbf{0}, F''\mathbf{0} = \mathbf{0}, ... F^{(m-1)}\mathbf{0} = \mathbf{0}, F^{(m)}\mathbf{0} = \mathbf{0}.$

(4.) Assuming therefore now (comp. 342, XII.) the new auxiliary function,

VI...
$$\psi x = \frac{x^m \mathrm{d} q^m}{2 \cdot 3 \cdot \ldots \cdot m}$$
, with $\mathrm{Td} q > 0$,

which gives,

VII...
$$\psi 0 = 0$$
, $\psi' 0 = 0$, $\psi'' 0 = 0$, ... $\psi^{(m-1)} 0 = 0$, $\psi^{(m)} 0 = dq^m$,

we find (by 341, (8.), (9.), comp. again 342, XII.) that

VIII. . .
$$\lim_{x=0}$$
. $(Fx:\psi x) = 0.$

(5.) But these two new functions, Fx and ψx , are formed from the dividend and the divisor of the quotient Q in II., by changing dq to xdq; and (comp. 342, (3.)) instead of thus multiplying a given quaternion differential dq, by a small and indefinitely decreasing scalar, x, we may indefinitely diminish the tensor, Tdq, without changing the versor, Udq.

(6.) And even if Udq be changed, while the differential dq is thus made to tend to zero, we can always conceive that it tends to some limit; which limiting or ultimate value of that versor Udq may then be treated as if it were a constant one, without affecting the limit of the quotient Q.

(7.) The *theorem*, as above enunciated, is therefore fully proved; and we are at liberty to *choose*, in any application, between the two forms of statement, 342 and 375, of which one is more convenient at one time, and the other at another.

On Osculating Planes, and Absolute Normals, to Curves of Double Curvature.

376. The variable vector ρ_t of a curve in space may in general be thus expressed, with the help of Taylor's Series (comp. 370, (1.)):

I...
$$\rho_t = \rho + t\rho' + \frac{1}{2}t^2 u\rho''$$
, with $u_0 = 1$;

 ρ , ρ' , u' being here abridged symbols for ρ_0 , ρ'_0 , u_i ; and the product $u\rho''$ being a vector, although the factor u is generally a quaternion (comp. 370, (5.)). And the different terms of this expression I. may be thus constructed (compare the annexed fig. 77):

while

II...
$$\rho = OP$$
; $t\rho' = PT$; $\frac{1}{2}t^2u\rho'' = TQ$;
III... $\rho_t = OQ$, and $t\rho' + \frac{1}{2}t^2u\rho'' = PQ$;

the line rq, or the term $\frac{1}{2}l^2u\rho''$, being thus what may be called the *deflexion* of the *curve* rqu, at q, from its *tangent* rr at r, measured in a *direction* which depends on the *law* according to which ρ_l varies with t, and on the *distance*

of Q from P. The equation of the plane of the triangle PTQ is rigorously (by II.) the following, with ω for its variable vector,

IV...
$$0 = Su\rho''\rho'(\omega - \rho);$$

this plane IV. then touches the curve at P, and (generally) cuts it at q; so that if the point q be conceived to approach indefinitely to P, the resulting formula,

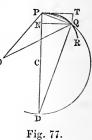
V. . . 0 = S
$$\rho''\rho'(\omega-\rho)$$
, or V'. . . 0 = S $\rho'\rho''(\omega-\rho)$

is the equation of the plane PTQ in that *limiting position*, in which it is called the osculating plane, or is said to osculate to the curve PQR, at the point P.

(1.) If the variable vector ρ be immediately given as a function ρ_s of a variable scalar, s, which is itself a function of the former scalar variable t, we shall then have (comp. 331) the expressions,

VI. . .
$$\rho'_t = s' D_s \rho_s$$
, $\rho''_t = s'' D_s \rho_s + s'^2 D_s^2 \rho_s$, with $s' = D_t s$, $s'' = D_t^2 s$;

thus the vector ρ'' may change, even in direction, when we change the independent scalar variable; but ρ'' will always be a line, either in or parallel



ART. 376.] OSCULATING PLANES TO CURVES IN SPACE.

to the osculating plane; while ρ' will always represent a tangent, whatever scalar variable may be selected.

(2.) As an example, let us take the equation 314, XV., or 369, XIII., of the *helix*. With the independent variable t of that equation, we have (comp. 369, XIV.) the derived expressions,

VII...
$$\rho' = ca + \frac{\pi}{2}a^{t+1}\beta$$
, $\rho'' = -\left(\frac{\pi}{2}\right)^2 a^t\beta = \left(\frac{\pi}{2}\right)^2 (c(a-\rho));$

 ρ'' has therefore here (comp. 369, (8.)) the direction of the normal to the cylinder; and consequently, the osculating plane to the helix is a normal plane to the cylinder of revolution, on which that curve is traced: a result well known, and which will soon be greatly extended.

(3.) When a curve of *double* curvature *degenerates* into a *plane* curve, its *osculating* plane becomes *constant*, and reciprocally. The *condition of planarity* of a *curve in space* may therefore be expressed by the equation,

VIII. . . $UV\rho'\rho'' = \pm a$ constant unit line;

or, by 335, II., and 338, VIII.,

$$\mathbf{IX.} \dots \mathbf{0} = \mathbf{V} \frac{\mathbf{V}(\boldsymbol{\rho}' \boldsymbol{\rho}'')'}{\mathbf{V} \boldsymbol{\rho}' \boldsymbol{\rho}''} = \mathbf{V} \frac{\mathbf{V} \boldsymbol{\rho}' \boldsymbol{\rho}'''}{\mathbf{V} \boldsymbol{\rho}' \boldsymbol{\rho}''};$$

or finally,

X...
$$S\rho'\rho''\rho''' = 0$$
, or XI... $\rho'''|||\rho', \rho''$.

(4.) Accordingly, for a *plane curve*, if λ be a given normal to its plane, we have the three equations,

XII...
$$S\lambda \rho' = 0$$
, $S\lambda \rho'' = 0$, $S\lambda \rho''' = 0$;

which conduct, by 294, (11.), to X.

(5.) For example, if we had not otherwise known that the equation 337 (2.) represented a *plane ellipse*, we might have perceived that it was the equation of *some* plane curve, because it gives the *three* successive derivatives,

XIII. . .
$$\rho' = \frac{\pi}{2} \nabla a^{t+1} \beta$$
, $\rho'' = -\left(\frac{\pi}{2}\right)^2 \nabla a^t \beta$, $\rho''' = -\left(\frac{\pi}{2}\right)^3 \nabla a^{t+1} \beta$,

which are complanar lines, the third having a direction opposite to the first.

(6.) And generally, the formula X. enables us to assign, on any curve of double curvature, for which ρ is expressed as a function of t, the points^{*} at

^{*} Namely, in a modern phraseology, the places of *four-point contact* with a *plane*. The equation, $\nabla \rho' \rho'' = 0$, indicates in like manner the places, if any, at which a curve has *three-point contact* with a *right line*. For curves of double curvature, these are also called points of *simple* and *double inflexion*.

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which it most resembles a plane curve, or approaches most closely to its own osculating plane.

377. An important and *characteristic property* of the osculating plane to a curve of double curvature, is that the *perpendiculars* let fall on it, from points of the curve near to the point of osculation, are *small* of an order *higher* than the *second*, if their *distances* from that *point* be considered as *small* of the *first* order.

(1.) To exhibit this by quaternions, let us begin by considering an *arbitrary plane*,

I...
$$S\lambda(\omega - \rho) = 0$$
, with $T\lambda = 1$,

drawn through a point P of the curve. Using the expression 376, I., for the vector oq, or ρ_t , of another point q of the same curve, we have, for the perpendicular distance of q from the plane I., this other rigorous expression,

II. . .
$$S\lambda(\rho_t - \rho) = tS\lambda\rho' + \frac{1}{2}t^2S\lambda u\rho'';$$

which represents, in general, a small quantity of the first order, if t be assumed to be such.

(2.) The expression II. represents however, generally, a small quantity of the second order, if the direction of λ satisfy the condition,

III...
$$S\lambda \rho' = 0$$
;

that is, if the *plane* I. touch the curve.

(3.) And if the condition,

IV...
$$S\lambda \rho'' = 0$$
,

be also satisfied by λ , then, but not otherwise, the expression II. tends to bear an evanescent ratio to t^2 , or is small of an order higher than the second.

(4.) But the combination of the *two conditions*, III. and IV., conducts to the expression,

$$V...\lambda = \pm UV\rho'\rho'';$$

comparing which with 376, V., we see that the property above stated is one which belongs to the *osculating* plane, and to *no other*.

378. Another remarkable property* of the osculating plane to a curve is, that it is the tangent plane to the cone of parallels to tangents (369, (6.)), which has its vertex at the point of osculation.

 $\mathbf{26}$

[III. III. § 4.

[•] The writer does not remember seeing this property in print; but of course it is an easy consequence from the doctrine of *infinitesimals*, which doctrine however it has not been thought convenient to adopt, as the *basis* of the present exposition.

ARTS. 376-379.]

CONE OF PARALLELS TO TANGENTS.

(1.) In general, if $\rho = \phi x$ be (comp. 369, I.) the equation of a *curve* in space, the equation of the *cone* which has its vertex at the origin, and passes through this curve, is of the form,

I...
$$\rho = y\phi x;$$

in which x and y are two independent and scalar variables.

(2.) We have thus the two partial derivatives,

II...
$$D_x \rho = y \phi' x$$
, $D_y \rho = \phi x$;

and the tangent plane along the side (x) has for equation,

III... $0 = S(\omega \cdot \phi x \cdot \phi' x)$; or briefly, III'... $0 = S\omega\phi\phi'$.

(3.) Changing then x, ϕ , ϕ' , ω to t, ρ' , ρ'' , $\omega - \rho$, we see that the equation 376, V., of the osculating plane to the curre 376, I., is also that of the tangent plane to the cone of parallels, &c., as asserted.

379. Among all the normals to a curve, at any one point, there are two which deserve special attention; namely the one which is in the osculating plane, and is called the *absolute* (or *principal*) normal; and the one which is perpendicular to that plane, and which it has been lately proposed to name the binormal.* It is easy to assign expressions, by quaternions, for these two normals, as follows.

(1.) The absolute normal, as being perpendicular to ρ' , but complanar with ρ' and ρ'' , has a direction expressed by any one of the following formulæ (comp. 203, 334):

I... $V\rho''\rho'$. ρ'^{-1} ; or II... $dU\rho'$; or III... $dUd\rho$.

(2.) There is an extensive class + of cases, for which the following equations hold good:

IV... $T\rho' = \text{const.}$; $V...\rho'^2 = \text{const.}$; $VI...S\rho'\rho'' = 0$;

and in all such cases, the expression I. reduces itself to ρ'' , which is therefore then a representative of the absolute normal.

^{*} By M. de Saint-Venant, as being perpendicular at once to two eonsecutive elements of the curve, in the infinitesimal treatment of this subject. See page 261 of the very valuable Treatise on Analytic Geometry of Three Dimensions (Hodges and Smith, Dublin), by the Rev. George Salmon, D.D., which has been published in the present year (1862), but not till after the printing of these Elements of Quaternions (begun in 1860) had been too far advanced, to allow the writer of them to profit by the study of it, so much as he would otherwise have sought to do.

⁺ Namely, those in which the arc of the curve, or that arc multiplied by a scalar constant, is taken as the *independent variable*.

[III. III. §§ 4, 5.

(3.) For example, in the case of the *helix*, with the equation several times before employed, the conditions (2.) are satisfied; and accordingly the absolute normal to that curve coincides with the normal ρ'' to the *cylinder*, on which it is traced: the *locus of the absolute normal* being here that screw surface or Helicoid, which has been already partially considered (comp. 314, (11.), and 372, (4.)).

(4.) And as regards the *binormal*, it may be sufficient here to remark, that because it is perpendicular to the osculating plane, it has the *direction* expressed by one or other of the two symbols (comp. 377, V.),

VII...
$$\nabla \rho' \rho''$$
, or $\nabla II' \dots \nabla d\rho d^2 \rho$.

(5.) There exists, of course, a system of three rectangular planes, the osculating plane being one, which are connected with the system of the three rectangular lines, the tangent, the absolute normal, and the binormal, and of which any one who has studied the Quaternions so far can easily form the expressions.

(6.) And a construction^{*} for the absolute normal may be assigned, analogous to and including that lately given (378) for the osculating plane, as an interpretation of the expression II. or III., or of the symbol $dU\rho'$ or $dUd\rho$. From any origin o conceive a system of unit lines $(U\rho' \text{ or } Ud\rho)$ to be drawn, in the directions of the successive tangents to the given curve of double curvature; these lines will terminate on a certain spherical curve; and the tangent, say ss', to this new curve, at the point s which corresponds to the point P of the old one, will have the direction of the absolute normal at that old point.

(7.) At the same time, the plane oss' of the great circle, which touches the new curve upon the unit sphere, being the tangent plane to the cone of parallels (378), has the direction of the osculating plane to the old eurve; and the radius drawn to its pole is parallel to the binomial.

(8.) As an *example* of the *auxiliary* (or *spherical*) curve, constructed as in (6.), we may take again the *helix* (369), XIII., &c.) as the *given* curve of double curvature, and observe that the expression 369, XIV., namely,

VIII. . .
$$\rho' = ca + \frac{\pi}{2}a^{l+1}\beta$$
, gives IX. . . $\rho'^2 = -c^2 + \frac{\pi^2\beta^2}{4} = \text{const. (comp. (3.))};$

 $\mathbf{28}$

^{*} This construction also has not been met with by the writer in print, so far as he remembers; but it may easily have escaped his notice, even in the books which he has seen.

ARTS. 379, 380.] ABSOLUTE NORMALS, GEODETIC LINES.

whence $T\rho'$ is constant (as in IV.), and we have the equation (comp. 369, XV. XIX.),

X... SaUp' =
$$-c\left(c^2 - \frac{\pi^2\beta^2}{4}\right)^{-\frac{1}{2}} = -\cos a = \text{const.},$$

a being again the inclination of the helix to the axis of its cylinder; which shows that the *new* curve is in *this* case a *plane* one, namely a certain *small circle* of the unit sphere.

(9.) In general, if the given curve be conceived to be an orbit described by a point, which mores with a constant velocity taken for unity, the auxiliary or spherical curve becomes what we have proposed (100, (5.)) to call the hodograph of that motion.

(10.) And if the given curve be supposed to be described with a *variable* velocity, the hodograph is still some curve upon the cone of parallels to tangents.

SECTION 5.

On Geodetic Lines, and Families of Surfaces.

380. Adopting as the *definition* of a *geodetic line*, on any proposed curved surface, the property that is one of which the *osculating plane* is always a *normal plane* to that surface, or that the *absolute normal* to the *curve* is also the *normal* to the *surface*, we have *two principal modes* of *expressing* by quaternions this general and *characteristic property*. For we may either write.

I. . .
$$S\nu\rho'\rho'' = 0$$
, or II. . . $S\nu d\rho d^2\rho = 0$,

to express that the normal ν to the surface (comp. 373) is perpendicular to the binormal $\nabla \rho' \rho''$ or $\nabla d\rho d^2 \rho$ to the curve (comp. 379, VII. VII'.); or else, at pleasure,

III. ..
$$\nabla v (\mathbf{U}\rho')' = 0$$
, or $\mathbf{I} \nabla \ldots \nabla v d \mathbf{U} d\rho = 0$,

to express that the same normal ν has the direction of the absolute normal $(U\rho')'$ or $dUd\rho$ (comp. 379, II. III.), to the same geodetic line. And thus it becomes easy to deduce the known relations of such lines (or curves) to some important families of surfaces, on which they can be traced. Accordingly, after beginning for simplicity with the sphere, we shall proceed in the following sub-articles to determine the geodetic lines on cylindrical and conical surfaces, with arbitrary bases; intending afterwards to show how

[III. III. § 5.

the corresponding lines can be investigated, upon *developable surfaces*, and surfaces of *revolution*.

(1.) On a sphere, with centre at the origin, we have $\nu \parallel \rho$, and the differential equation IV. admits of an immediate integration;* for it here becomes,

$$\mathbf{V}...\mathbf{0} = \mathbf{V}\rho \mathbf{d}\mathbf{U}\mathbf{d}\rho = \mathbf{d}\mathbf{V}\rho\mathbf{U}\mathbf{d}\rho,$$

whence

VI...
$$V\rho Ud\rho = \omega$$
, and VII... $S\omega\rho = 0$,

 ω being some constant vector; the curve is therefore in this case a great circle, as being wholly contained in one diametrical plane.

(2.) Or we may observe that the equation,

VIII...
$$S\rho\rho'\rho'' = 0$$
, or IX... $S\rho d\rho d^2\rho = 0$,

obtained by changing ν to ρ in I. or II., has generally for a first integral (comp. 335, (1.)), whether $T\rho$ be constant or variable,

X...
$$UV\rho\rho' = UV\rho d\rho = \omega = \text{const.};$$

it expresses therefore that ρ is the vector of some curve (or line) in a plane through the origin; which curve must consequently be here a great circle, as before.

(3.) Accordingly, as a verification of X., if we write

XI... $\rho = ax + \beta y$, x and y being scalar functions of t,

where t is still some independent scalar variable, and a, β are two vector constants, we shall have the derivatives,

XII...
$$\rho' = ax' + \beta y', \quad \rho'' = ax'' + \beta y'' \parallel \rho, \rho';$$

so that the equation VIII. is satisfied.

(4.) For an *arbitrary cylinder*, with generating lines parallel to a fixed line *a*, we may write,

XIII. . . $Sa\nu = 0$, XIV. . . $SadUd\rho = 0$, XV. . . $SaUd\rho = const.$;

a geodetic on a cylinder crosses therefore the generating lines at a constant angle, and consequently becomes a right line when the cylinder is unfolded

^{*} We here assume as evident, that the differential of a variable cannot be constantly zero (comp. 335, (7.)); and we employ the principle (comp. 338, (5.)), that V. $d\rho Ud\rho = -VTd\rho = 0$.

ABT. 380.] GEODETICS ON SPHERES, CONES AND CYLINDERS.

into a *plane*: both which known properties are accordingly verified (comp. 369, (5.), and 376, (2.)) for the case of a cylinder of *revolution*, in which case the geodetic is a *helix*.

(5.) For an arbitrary cone, with vertex at the origin, we have the equations,

XVI. . .
$$Sr\rho = 0$$
, XVII. . . $S\rho dUd\rho = 0$,

$$XVIII...dS\rho Ud\rho = S(d\rho . Ud\rho) = -Td\rho;$$

multiplying the last of which equations by $2S\rho Ud\rho$, and observing that $-2S\rho d\rho = -d \cdot \rho^2$, we obtain the transformations,

XIX... $0 = d\{(S\rho Ud\rho)^2 + \rho^2\} = d \cdot (V\rho Ud\rho)^2, XX... TV\rho Ud\rho = const.;$

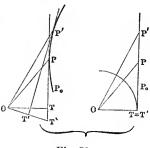
the perpendicular from the vertex, on a tangent to any one geodetic upon a cone, has therefore a constant length; and all such tangents touch also a concentric sphere,* or one which has its centre at the vertex of the cone.

(6.) Conceive then that at each point P or P' of the geodetie a tangent PT or P'T' is drawn, and that the angles oTP, or'P' are right; we shall have, by what has just been shown,

XXI. . . $\overline{\text{or}} = \overline{\text{or}}' = \text{const.} = \text{radius of concentric sphere};$

and if the cone be developed (or unfolded) into a plane, this constant or common length, of the perpendiculars from o on the tangents, will remain

unchanged, because the length $\overline{\text{op}}$ and the angle opr are unaltered by such development; the geodetic becomes therefore some plane line, with the same property as before; and although this property would belong, not only to a right line, but also to a circle with o for centre (compare the second part of the annexed figure 78), yet we have in this result merely an effect of the foreign factor $S\rho Ud\rho$, which was introduced in (5.), in order to facilitate the integration of the differential equation XVIIII, and which (by that very equation) cannot be con-



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Fig. 78.

stantly equal to zero. We are therefore to *exclude* the *curves* in which the *cone* is cut by *spheres* concentric with it: and there remain, as the sought *geodetic lines*, only those of which the *developments* are *rectilinear*, as in (4.).

^{*} When the cone is of the second order, this becomes a case of a known theorem respecting geodetic lines on a surface of the same second order, the tangents to any one of which curves touch also a confocal surface.

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(7.) Another mode of *interpreting*, and at the same time of *integrating*, the equation XVIII., is connected with the interpretation of the symbol $\mathrm{Td}\rho$; which can be proved, on the principles of the present Calculus, to represent rigorously the differential ds of the arc (s) of that curve, whatever it may be, of which ρ is the variable vector; so that we have the general and rigorous equation,

XXII... $Td\rho = ds$, if s thus denote the arc:

whether that arc *itself*, or some other scalar, t, be taken as the *independent variable*; and whether its differential ds be *small* or *large*, provided that it be *positive*.

(8.) In fact if we suppose, for the sake of greater generality, that the vector ρ and the scalar *s* are thus both functions, ρ_t and s_t , of some one independent and scalar variable, *t*, our principles direct us first to take, or to conceive as taken, a submultiple, $n^{-1}dt$, of the finite differential dt, considered as an assumed and arbitrary increment of that independent variable, *t*; to determine next the vector $\rho_{t+n^{-1}dt}$, and the scalar $s_{t+n^{-1}dt}$, which correspond to the point $P_{t+n^{-1}dt}$ of the curve on which ρ_t terminates in P_t , and of which s_t is the arc, \hat{P}_0P_t , measured to P_t from some fixed point P_0 on the same curve; to take the differences,

$$\rho_{t+n^{-1}dt} - \rho_t$$
, and $s_{t+n^{-1}dt} - s_t$,

which represent respectively the directed chord, and the length, of the are $P_t P_{t+n^{-1}dt}$, which are will generally be small, if the number n be large, and will indefinitely diminish when that number tends to infinity; to multiply these two decreasing differences, of ρ_t and s_t , by n; and finally to seek the limits to which the products tend, when n thus tends to ∞ : such limits being, by our definitions, the values of the two sought and simultaneous differentials, d ρ and ds, which answer to the assumed values of t and dt. And because the small are, Δs , and the length, $T\Delta \rho$, of its small chord, in the foregoing construction, tend indefinitely to a ratio of equality, such must be the rigorous ratio of ds and Td ρ , which are (comp. 320) the limits of their equimultiples.

(9.) Admitting then the exact equality XXII. of Td ρ and ds, at least when the latter like the former is taken *positively*, we have only to substitute - ds for - Td ρ in the equation XVIII., which then becomes immediately integrable, and gives,

XXIII... $s + S\rho Ud\rho = s - S(\rho : Ud\rho) = const.$;

where $S(\rho : Ud\rho)$ denotes the projection \overline{TP} , of the vector ρ or or, on the tangent to the geodetic at \mathbf{r} , considered as a positive scalar when ρ makes an

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acute angle with $d\rho$, that is, when the distance $T\rho$ or \overline{oP} from the vertex is *increasing*; while s denotes, as above, the *length* of the *arc* P_0P of the same curve, measured from *some fixed point* P_0 thereon, and considered as a *scalar* which *changes sign*, when the variable point P passes through the position P_0 .

(10.) But the *length* of TP does not change (comp. (6.)), when the cone is *developed*, as before; we have therefore the equations (comp. again fig. 78),

XXIV. . .
$$\widehat{\mathbf{P}_0\mathbf{P}} - \overline{\mathbf{TP}} = \text{const.} = \widehat{\mathbf{P}_0\mathbf{P}'} - \mathbf{T'P'}, \qquad \mathbf{XXV.} \dots \widehat{\mathbf{PP}'} = \overline{\mathbf{T'P'}} - \overline{\mathbf{TP}},$$

which must hold good both *before* and *after* the supposed *derelopment* of the conical surface; and it is easy to see that this can only be, by the geodetic on the cone becoming a right line, as before. In fact, if or' in the plane be supposed to intersect the tangent TP in a point T', and if P' be conceived to approach to P, the second member of XXV. bears a limiting ratio of equality to the first member, increased or diminished by $\overline{\text{TF}}$; which latter *line*, and therefore also the angle TOT' between the perpendiculars on the two near tangents, or the angle between those tangents themselves, if existing, must bear an indefinitely decreasing ratio to the *arc* $\widehat{\text{PP}}$; so that the radius of curvature of the supposed curve is infinite, or T' coincides with T, and the development is rectilinear as before.

(11.) The important and general equation, $Td\rho = ds$ (XXII.), conducts to many other consequences, and may be put under several other forms. For example, we may write generally,

also

XXVI... $TD_s\rho = 1$, XXVII... $(D_s\rho)^2 + 1 = 0$; XXVIII... $(D_l\rho)^2 + (D_{\ell}s)^2 = 0$, or XXIX... $\rho'^2 + s'^2 = 0$,

if ρ' and s' be the first derivatives of ρ and s, taken with respect to any independent scalar variable, such as t; whence, by continued derivation,

XXX...
$$S\rho'\rho'' + s's'' = 0$$
, XXXI... $S\rho'\rho''' + \rho''^2 + s's''' + s''^2 = 0$, &c.

(12.) And if the arc s be *itself* taken as the independent variable, then (comp. 379, (2.)) the equations XXIX., &c., become,

XXXII...
$$\rho'^2 + 1 = 0$$
, $S\rho'\rho'' = 0$, $S\rho'\rho''' + \rho''^2 = 0$, &c.

381. In general, if we conceive (comp. 372, I.) that the vector ρ of a given surface is expressed as a given function of two scalar variables, x and y, whereof HAMILTON'S ELEMENTS OF QUATERNIONS, Vol. II.

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one, suppose y, is regarded at first as an unknown function of the other, so that we have again,

I...
$$\rho = \phi(x, y)$$
, but now with II... $y = fx$,

where the form of ϕ is known, but that of f is sought; we may then regard ρ as being implicitly a function of the single (or independent) scalar variable, x, and may consider the equation,

III...
$$\rho = \phi(x, fx),$$

as being that of some curve on the given surface, to be determined by assigned conditions. Denoting then the unknown total derivative $p\phi(x, fx)$ by ρ' , but the known partial derivatives of the same first order by $p_x\phi$ and $p_y\phi$, with analogous notations for orders higher than the first, we have (comp. 376, VI.) the expressions,

IV...
$$\rho' = D_x \phi + y' D_y \phi$$
, $\rho'' = D_x^2 \phi + 2y' D_x D_y \phi + y'^2 D_y^2 \phi + y'' D_y \phi$, &c.

in which $y' = D_x y = f'x$, $y'' = D_x^2 y = f''x$, &c. Hence, writing for the normal ν to the surface the expression,

$$\mathbf{V}...\nu = \mathbf{V}(\mathbf{D}_x\phi \cdot \mathbf{D}_y\phi) = \mathbf{V}.\mathbf{D}_x\phi\mathbf{D}_y\phi \qquad (\text{comp. 372, V.}),$$

or this vector multiplied by any scalar, the equation 380, I. of a geodetic line takes this new form,

VI. . . 0 =
$$S_{\nu\rho}\rho^{\prime\prime} = S(V. D_x \phi D_y \phi . V \rho^{\prime} \rho^{\prime\prime});$$

or, by a general transformation which has been often employed already (comp. 352, XXXI., &c.),

VII. . . 0 =
$$S\rho' D_y \phi$$
 . $S\rho'' D_x \phi - S\rho' D_x \phi$. $S\rho'' D_y \phi$;

and thus, by substituting the expressions IV. for ρ' and ρ'' , we obtain an ordinary (or scalar) differential equation, of the second order, in x and y, which is satisfied by all the geodetics on the given surface, and of which the complete integral (when found) expresses, with two arbitrary and scalar constants, the form of the scalar function f in II., or the law of the dependence of y on x, for the geodetic curves in question.

(1.) As an example, let us take the equation,

V11I...
$$\rho = \phi(x, y) = y\psi x$$
 (comp. 378, I.),

of a cone with its vertex at the origin; which cone becomes a known one, when the form of the vector function ψ is given, that is, when we know a

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guiding curve $\rho = \psi x$, through which the sides of the cone all pass. We have here the partial derivatives,

IX...
$$D_x \phi = y D_x \psi x = y \psi', \quad D_y \phi = \psi x = \psi$$
 (comp. 378, 11.);

and

X...
$$D_x^2 \phi = y D_x^2 \psi x = y \psi''$$
, $D_x D_y \phi = \psi'$, $D_y^2 \phi = 0$;

the expressions IV. become, then,

XI...
$$\rho' = y\psi' + y'\psi, \quad \rho'' = y\psi'' + 2y'\psi' + y''\psi;$$

and since only the *direction* of the normal is important, we may divide V. by -y, and write,

XII...
$$\nu = \nabla \psi \psi'$$
.

(2.) The expressions XI. and XII. give (comp. VI. and VII.) for the *geodetics on the cone* VIII., the differential equation of the second order,

$$\begin{aligned} \mathbf{XIII.} \dots &0 = \mathbf{S}(\nabla\psi\psi' \cdot \nabla\rho'\rho'') = \mathbf{S}\rho''\psi\mathbf{S}\rho'\psi - \mathbf{S}\rho''\psi'\mathbf{S}\rho'\psi \\ &= (y\mathbf{S}\psi\psi'' + 2y'\mathbf{S}\psi\psi' + y''\psi^2) \ (y\psi'^2 + y'\mathbf{S}\psi\psi') \\ &- (y\mathbf{S}\psi\psi'' + 2y'\psi^2 + y''\mathbf{S}\psi\psi') \ (y\mathbf{S}\psi\psi' + y'\psi^2), \end{aligned}$$

in which ψ^2 and ψ'^2 are abridged symbols for $(\psi x)^2$ and $(\psi' x)^2$; but this equation in x and y may be greatly simplified, by some permitted suppositions.

(3.) Thus, we are allowed to suppose that the guiding curve (1.) is the intersection of the cone with the concentric unit sphere, so that

XIV... $T\psi x = 1$, $\psi^3 = -1$, $S\psi\psi' = 0$, $S\psi\psi'' + \psi'^2 = 0$;

and if we further assume that the *arc* of this *spherical curve* is taken as the *independent variable*, x, we have then, by 380, (12.), combined with the last equation XIV.,

XV...
$$T\psi' x = 1$$
, $\psi'^2 = -1$, $S\psi'\psi'' = 0$, $S\psi\psi'' = -\psi'^2 = 1$.

(4.) With these simplifications, the differential equation XIII. becomes,

XVI. . . 0 =
$$(y - y'') (-y) - (-2y') (-y') = yy'' - 2y'^2 - y^2;$$

and its complete integral is found by ordinary methods to be,

$$\mathbf{XVII.} \ldots y = b \sec (x + c),$$

in which b and c are two arbitrary but scalar constants.

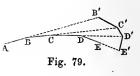
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(5.) To interpret now this integrated and scalar equation in x and y, of the geodetics on an arbitrary cone, we may observe that, by the suppositions (3.), y represents the distance, $T\rho$ or \overline{or} , from the vertex o, and x + c represents the angle AOP, in the developed state of cone and curve, from some fixed line oA in the plane, to the variable line oP; the projection of this new oP on that fixed line oA is therefore constant (being = b, by XVII.), and the developed geodetic is again found to be a right line, as before.

382. Let ABCDE . . . (see the annexed figure 79) be any given series of points in space. Draw the successive right lines, AB, BC, CD, DE, . . and

prolong them to points B', C', D', E', ... the lengths of these prolongations being arbitrary; join also B'C', C'D', D'E', We shall thus have a series of plane triangles, B'BC', C'CD', D'DE', ... all generally in different planes; so that BCD'C'B', CDE'D'C', ... are



generally gauche pentagons, while BCDE'D'C'B' is a gauche heptagon, &c. But we can conceive the first triangle B'BC' to turn round its side BCC', till it comes into the plane of the second triangle c'CD'; which will transform the first gauche pentagon into a plane one, denoted still by BCD'C'B'. We can then conceive this plane figure to turn round its side CDD', till it comes into the plane of the third triangle, D'DE'; whereby the first gauche heptagon will have become a plane one, denoted as before by BCDE'D'C'B': and so we can proceed indefinitely. Passing then to the limit, at which the points ABCDE . . . are conceived to be each indefinitely near to the one which precedes or follows it in the series, we conclude as usual (comp. 98, (12.)) that the locus of the tangents to a curve of double curvature is a developable surface: or that it admits of being unfolded (like a cone or cylinder) into a plane, without any breach of continuity. It is now proposed to translate these conceptions into the language of quaternions, and to draw from them some of their consequences: especially as regards the determination of the geodetic lines, on such a developable surface.

(1.) Let ψ_x , or simply ψ , denote the variable vector of a point upon the curve, or cusp-edge, or edge of regression of the developable, to which curve the generating lines of that surface are thus tangents, considered as a function ψ of its arc, x, measured from some fixed point A upon it; so that while the equation of the surface will be of the form (comp. 100, (8.)),

I. . .
$$\rho = \phi(x, y) = \psi_x + y\psi'_x = \psi + y\psi',$$

y being a second scalar variable, we shall have the relations (comp. 381, XV.),

II... $T\psi' = 1$, $\psi'^2 = -1$, $S\psi'\psi'' = 0$, $S\psi'\psi''' = -\psi''^2 = z^2$, if $z = T\psi''$.

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III... $D_x\phi = \psi' + y\psi'', \quad D_y\phi = \psi';$ (2.) Hence

ad

$$I\nabla \dots \rho' = (1+y')\psi' + y\psi'', \quad \rho'' = y''\psi' + (1+2y')\psi'' + y\psi''';$$

$$\nabla \dots = \nabla t'/t'' = t'/t'' \text{ multiplied by any scalar}$$

ar

 $\nabla \psi \psi' = \psi \psi'$, multiplied by any scalar.

(3.) The differential equation of the geodetics may therefore be thus written (comp. 381, XIII.),

VI. . . 0 = $S(\nabla \psi' \psi'' \cdot \nabla \rho' \rho'') = S\rho' \psi'' S\rho'' \psi' - S\rho'' \psi'' S\rho' \psi';$

in which, by (1.) and (2.),

VII. . .
$$\begin{cases} S\rho'\psi'' = -yz^2, & S\rho''\psi' = -y'' + yz^2, \\ S\rho''\psi'' = -(1+2y')z^2 - yzz', & S\rho'\psi' = -(1+y'); \end{cases}$$

the equation becomes therefore, after division by -z,

VIII...
$$0 = z \{ (1 + y')^2 + (yz)^2 \} + (1 + y') (yz)' - y''yz,$$

or simply,

IX... z + v' = 0, or IX'... $\operatorname{Td}\psi' + \mathrm{d}v = 0$, if X... $\tan v = \frac{yz}{1+v'} = \frac{y'\Gamma\psi''}{1+v'}$

(4.) To interpret now this very simple equation IX. or IX'., we may observe that z, or $T\psi''$, or $Td\psi'$: dx, expresses the limiting ratio, which the angle between two near tangents ψ' and $\psi' + \Delta \psi'$, to the cusp-edge (1.), bears to the small arc Δx of that curve which is intercepted between their points of contact; while v is, by IV., that other angle, at which such a variable tangent, or generating line of the developable, crosses the geodetic on that surface; and therefore its *derivative*, v' or dv: dx, represents the limiting ratio, which the change Δv of this last angle, in passing from one generating line to another, bears to the same small arc Δx of the curve which those lines touch.

(5.) Referring then to fig. 79, in which, instead of two continuous curves, there were two gauche polygons, or at least two systems of successive right lines, connected by prolongations of the lines of the first system, we see that the recent formula IX. or IX'. is equivalent to this *limiting equation*,

XI... lim.
$$\frac{CD'C' - BC'B'}{C'CD'} = -1;$$

but these three angles remain unaltered, in the development of the surface: the bent line B'c'D' for space becomes therefore ultimately a straight line in

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the *plane*, and similarly for *all other* portions of the original polygon, or *twisted line*, B'C'D'E'..., of which B'C'D' was a *part*.

(6.) Returning then to curves and surfaces in space, the quaternion analysis (3.) is found, by this simple reasoning,* to conduct to an expression for the known and characteristic property of the geodetics on a developable: namely that they become right lines, as those on cylinders (380, (4.)), and on cones (380, (6.) and (10.), or 381, (5.)), were lately seen to do, when the surface on which they are thus traced is unfolded into a plane.

383. This known result, respecting geodetics on developables, may be very simply verified, by means of a new determination of the absolute† normal (379) to a curve in space, as follows.

(1.) The arc s of any curve being taken for the independent variable, we may write (comp. 376, I.), by Taylor's Series, the following rigorous expressions,

I. . .
$$\rho_{-s} = \rho - s\rho' + \frac{1}{2}s^2 u_{-s}\rho'', \quad \rho_0 = \rho, \ \rho_s = \rho + s\rho' + \frac{1}{2}s^2 u_s\rho'', \quad \text{with} \quad u_0 = 1,$$

for the vectors of three *near points*, \mathbf{P}_{-s} \mathbf{P}_{0} , \mathbf{P}_{s} , on the curve, whereof the second *bisects the arc*, 2s, intercepted between the first and third.

(2.) If then we conceive the *parallelogram* $P_{-s}P_0P_sR_s$ to be completed, we shall have, for the *two diagonals* of this new figure these other rigorous expressions,

11. . .
$$P_{-s}P_s = \rho_s - \rho_{-s} = 2s\rho' + \frac{1}{2}s^2(u_s - u_{-s})\rho'';$$

111. . . $P_0R_s = \rho_s + \rho_{-s} - 2\rho_0 = \frac{1}{2}s^2(u_s + u_{-s})\rho'';$

which give the limiting equations,

IV. . .
$$\lim_{s=0} s^{-1} P_{-s} P_s = 2\rho';$$
 V. . . $\lim_{s=0} s^{-2} P_0 R_s = \rho''.$

(3.) But the length $\overline{\mathbf{P}_{s}\mathbf{P}_{s}}$ of what may be called the long diagonal, or the chord of the double arc, 2s, is ultimately equal to that double arc; we have therefore by IV., the equation,

VI...
$$T\rho' = 1$$
, If $\rho' = D_s\rho$, and if s denotes the arc,

considered as the scalar variable on which the vector ρ depends: a result agreeing with what was otherwise found in 380, (12.).

^{*} In the Lectures (page 581), nearly the same analysis was employed, for geodetics on a developable; but the *interpretation* of the result was made to depend on an equation which, with the recent significations of ψ and v, may be thus written, as the integral of IX'., $v + \int T d\psi' = \text{const.}$; where $\int T d\psi'$ represents the finite angle between the extreme tangents to the finite arc $\int T d\psi$, or Δx , of the cusp-edge, when that curve is developed into a plane one.

⁺ Called also, and perhaps more usually, the principal normal.

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(4.) At the same time, since the ultimate direction of the same long diagonal is evidently that of the tangent at Po, we see anew that the same first derived vector ρ' represents what may be called the unit tangent* to the curve at that point.

(5.) And because the lengths of the two sides $P_{-s}P_0$ and P_0P_s , considered as chords of the two successive and equal arcs, s and s, are ultimately equal to them and to each other, it follows that the parallelogram (2.) is ultimately equilateral, and therefore that its diagonals are ultimately rectangular; but these diagonals, by IV. and V., have ultimately the directions of ρ' and ρ'' ; we find therefore anew the equation,

VII. . . $S\rho'\rho'' = 0$, if the arc be the independent variable,

which had been otherwise deduced before, in 380, (12.).+

(6.) But under the same condition, we saw (379, (2.)) that the second derived vector ρ'' has the direction of the absolute normal to the curve; such then is by V. the ultimate direction of what we may call the short diagonal $P_0 R_s$, constructed as in (2.); or, ultimately, the direction of the bisector of the (obtuse) angle P-s PoPs, between the two near and nearly equal chords from the point Po: while the plane of the parallelogram becomes ultimately the osculating plane.

(7.) All this is quite independent of the consideration of any surface, on which the curve may be conceived to be traced. But if we now conceive that this curve is formed from a right line B'c'D' ... (comp. fig. 79), by urapping round a developable surface a plane on which the line had been drawn, and if the successive portions B'c', c'D', . . of that line be supposed to have been equal, then because the two right lines c'B' and c'D' originally made supplementary angles with any other line c'c in the plane, the two chords c'B' and c'D' of the curve on the developable tend to make supplementary angles with the generatrix c'c of that surface; on which account the bisector (6.) of their angle B'C'D' tends to be perpendicular to that generating line C'C, as well as to the chord B'D', or ultimately to the tangent to the curve at c', when chords and arcs diminish together. The absolute normal (6.) to the curve thus formed is therefore *perpendicular* to two distinct tangents to the surface at c', and is consequently (comp. 372) the normal to that surface at that point; whence, by the definition (380), the curve is, as before, a geodetic on the developable.

* Compare the first Note to page 152, Vol. I.

+ [See note to 396 (19.), p. 88.]

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(8.) As regards the asserted rectangularity (7.), of the bisector of the angle B'c'D' to the line c'c, when the angles cc'B' and cc'D' are supposed to be supplementary, but not in one plane, a simple proof may be given by conceiving that the right line B'c' is prolonged to c'', in such a manner that $\overline{c'c''} = \overline{c'D'}$; for then these two equally long lines from c' make equal angles with the line c'c, so that the one may be formed from the other by a rotation round that line as an axis; whence c''D', which is evidently parallel to the bisector of B'c'D', is also perpendicular to c'c.

(9.) In quaternions, if a and ρ be any two vectors, and if t be any scalar, we have the equation,

$$\mathbf{VIII.} \quad \mathbf{S} \quad \mathbf{a} \left(a^t \rho a^{-t} - \rho \right) = 0,$$

which is, by 308, (8.), an expression for the geometrical principle as stated.

384. The recent analysis (382) enables us to deduce with ease, by quaternions, other known and important properties of developable surfaces: for instance, the property that each such surface may be considered as the *envelope* of a *series of planes*, involving only one scalar and *arbitrary constant* (or *parameter*) in their common equation; and that each plane of this series osculates to the cusp-edge of the developable.

(1.) The equation of the developable surface being still,

I...
$$\rho = \phi(x, y) = \psi_x + y\psi'_x = \psi + y\psi'$$
 (as in 382, I.),

its normal ν is easily found to have, as in 382, V., the direction of $\nabla \psi' \psi''$, whether the scalar variable x be, or be not, the arc of the cusp-edge, of which curve the equation is,

II...
$$\rho = \psi_x$$
.

(2.) Hence, by 373, VII., the equation of the *tangent plane* takes the form,

III...
$$S\omega\psi'\psi'' = S\psi\psi'\psi''$$
,

from which the second scalar variable y thus disappears: this common equation, of all the tangent planes to the developable, involves therefore, as above stated, only one variable and scalar parameter, namely x; and the envelope of all these planes is the developable surface itself.

(3.) The plane III., for any given value of this parameter x, that is, for any given point of the cusp-edge, touches the surface along the whole extent of the generating line, which is the tangent to this last curve.

ARTS. 383-385.] THEOREM OF RECIPROCAL CURVES IN SPACE.

(4.) And by comparing its equation III. with the formula 376, V., we see at once that this plane *osculates* to the same cusp-edge, at the point of *contact* of that curve with the same *generatrix* of the developable.

385. If the reciprocals of the perpendiculars, let fall from a given origin, on the tangent planes to a developable surface, be considered as being themselves vectors from that origin, they terminate on a curve, which is connected with the cusp-edge of the developable by some interesting relations of reciprocity (comp. 373, (21.)): in such a manner that if this new curve be made the cusp-edge of a new developable, we can return from it to the former surface, and to its cusp-edge, by a similar process of construction.

(1.) In general, if ψ_x and χ_x , or briefly ψ and χ , be two vector functions of a scalar variable x, such that χ may be deduced from ψ by the three scalar equations,

I. . .
$$S\psi\chi = c$$
, $S\psi'\chi = 0$, $S\psi''\chi = 0$,

in which $S\psi\chi$ is written briefly for $S(\psi_x, \chi_x)$, and c is any scalar constant, we have then this *reciprocal system* of three such equations,

II...
$$S_{\chi}\psi = c$$
, $S_{\chi}'\psi = 0$, $S_{\chi}''\psi = 0$;

an intermediate step being the equation,

III...
$$S\psi'\chi' = S\chi'\psi' = 0.$$

(2.) Hence, generally,

1V... if
$$\chi = \frac{cV\psi'\psi''}{S\psi\psi'\psi''}$$
, then V... $\psi = \frac{cV\chi'\chi''}{S\chi\chi'\chi''}$.

(3.) But if ρ be the variable vector of a curve in space, and ρ' , ρ'' its first and second derivatives with respect to any scalar variable, then, by the equation 376, V. of the osculating plane to the curve, we have the general expression,

VI...
$$\frac{S\rho\rho'\rho''}{V\rho'\rho''}$$
 = perpendicular from origin on osculating plane;

so that if ψ and χ be considered as the vectors of *two curres, each* vector is $c \times$ the *reciprocal of the perpendicular*, thus let fall from a common point, on the osculating plane to the *other*.

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(4.) We have therefore this Theorem :--

If, from any assumed point, 0, there be drawn lines equal to the reciprocals of the perpendiculars from that point, on the osculating planes to a given curve of double curvature, or to those perpendiculars multiplied by any given and constant scalar; then the locus of the extremities of the lines so drawn will be a second* curve, from which we can return to the first curve by a precisely similar process.

386. The theory of developable surfaces, considered as encelopes of planes with one scalar and variable parameter (384), may be additionally illustrated by connecting it with Taylor's Series, as follows.

(1.) Let a_t denote any vector function of a scalar variable t, so that

I. . . $a_t = a_0 + tu_t a'_0 = a + tua'$, with $u_0 = 1$;

or, by another step in the expansion,

II...
$$a_t = a_0 + ta'_0 + \frac{1}{2}t^2v_ta''_0 = a + ta' + \frac{1}{2}t^2ra'', \quad v_0 = 1;$$

where u and v are generally quaternions, but ua' and va'' are rectors.

(2.) Then, as the rigorous equation of the variable plane, the reciprocal of the perpendicular on which from the origin is $-a_t$, we have either,

or

III... - 1 = $Sa_t\rho = Sa\rho + tSua'\rho$, IV... - 1 = $Sa\rho + tSa'\rho + \frac{1}{2}t^2Sra''\rho$,

according as we adopt the expression I., or the equally but not more rigorous expression II., for the variable vector a_t .

(3.) Hence, by the form III., the *line of intersection* of the *two planes*, which answer to the *two values* 0 and t of the scalar variable, or *parameter*, t, is *rigorously* represented by the system of the *two scalar equations*,

$$V...Sa\rho + 1 = 0, Sua'\rho = 0.$$

(4.) And the *limiting position* of this right line V., which answers to the conceived *indefinite approach* of the second plane to the first, is given with equal rigour by the equations,

VI. . .
$$Sa\rho + 1 = 0$$
, $Sa'\rho = 0$;

^{*} The two curves may be said to be polar reciprocals, with respect to the (real or imaginary) sphere, $\rho^2 = c$; and an analogous relation of reciprocity exists generally, when the points of one curve are the poles of the osculating planes of the other, with respect to any surface of the second order: corresponding tangents being then reciprocal polars. Compare the theory of developables reciprocal to curves, given in Salmon's Analytical Geometry of Three Dimensions, page 89; see also Chapter XI. (page 224, &c.), of the same excellent work.

ARTS. 385, 386.] DEVELOPABLE AS ENVELOPE OF PLANES.

whereof it is seen that the second may be formed from the first, by derivating with respect to t, and treating ρ as constant : although no such rule of calculation had been previously laid down, for the comparatively geometrical process which is here supposed to be adopted.

(5.) The locus of all the lines VI. is evidently some ruled surface; to determine the normal ν to which, at the extremity of the vector ρ , we may consider that vector to be a function (372) of two independent and scalar variables, whereof one is t, and the other may be called for the moment w; and thus we shall have the two partial derivatives,

VII...
$$\operatorname{SaD}_{t\rho} = 0$$
, $\operatorname{SaD}_{w\rho} = 0$, giving $\nu \parallel a$.

(6.) Hence the line a has the direction of the required normal ν ; the plane $\operatorname{Sap} + 1 = 0$ touches the surface (comp. 384, (3.)) along the whole extent of the limiting line VI.; and the locus of all such lines is the envelope of all the planes, of the system recently considered.

(7.) The *line* VI. *cuts* generally the *plane* IV., in a *point* which is rigorously determined by the three equations,

VIII...
$$\operatorname{Sa}\rho + 1 = 0$$
, $\operatorname{Sa'}\rho = 0$, $\operatorname{Sva''}\rho = 0$;

and the *limiting position* of this *intersection* is, with equal rigour, the point determined by this other system of equations,

IX. . .
$$Sa\rho + 1 = 0$$
, $Sa'\rho = 0$, $Sa''\rho = 0$;

in which it may be remarked (comp. (4.)), that the *third* is the *derivative* of the second, if ρ be treated as *constant*.

(8.) The locus of all these points IX. is generally some curve upon the surface (5.), which is the locus of the lines VI., and has been seen to be the envelope (6.) of the planes III. or IV.; and to find the tangent to this curve, at the point answering to a given value of t, or to a given line VI., we have by IX. the derived equations,

X...
$$Sa\rho' = 0$$
, $Sa'\rho' = 0$, whence $\rho' \parallel Vaa'$;

comparing which with the equations VI. we see that the lines VI. touch the eurve, which is thus their common envelope.

(9.) We see then, in a new way, that the envelope of the planes III., which have one scalar parameter (t) in their common equation, and may represent any system of planes subject to this condition, is a developable surface:

because it is in general (comp. 382) the locus of the tangents to a curve in space, although this curve may reduce itself to a point, as we shall shortly see.

(10.) We may add that if a_t in III. be considered as the vector of a given curre, this curve is the *locus of the poles*^{*} of the *tangent planes* to the *developable*, taken with respect to the *unit sphere*; and conversely, that the developable surface is the *envelope* of the *polar planes* of the *points* of the same given curve, with respect to the same sphere.

(11.) If then it happen that this given curve, with a_t for vector, is a plane one, so that we have this new condition,

XI... $S\beta a_t + 1 = 0$, β being any constant vector,

namely the vector of the pole of the supposed plane of the given curve, the variable plane III., or $S_{\rho a_t} + 1 = 0$, of which the surface (5.) is the envelope, passes constantly through this fixed pole; so that the developable becomes in this case a cone, with β for the vector of its vertex: the equations IX. giving now $\rho = \beta$.

(12.) The same *degeneration*, of a developable into a *conical* surface, may also be conceived to take place in another way, by the *cusp-edge* (or at least some finite portion thereof) tending to become *indefinitely small*, while yet the *direction* of its *tangents* does not tend to become *constant*. For example, with recent notations, the *developable* which is the locus of the tangents to the *helix* may have its equation written thus:

XII...
$$\rho = \phi(x, y) = c(x\alpha + \frac{2}{\pi} \tan \alpha \cdot \alpha^x U\beta) + y\alpha(1 + \tan \alpha \cdot \alpha^x U\beta);$$

which when the quarter interval, c, between the spires, tends to zero, without their inclination a to the axis a being changed, tends to become a cone of revolution round that axis, with its semiangle = a.

387. So far, then, we may be said to have considered, in the present section, and in connexion with *geodetic lines*, the four following *families* of *surfaces* (if the first of them may be so called). First, *spherical surfaces*, of which the characteristic *property* is expressed by the equation,

I... $V\nu(\rho - a) = 0$, if a be vector of centre;

second, cylindrical surfaces, with the property,

II. . . $S_{\nu a} = 0$, if a be parallel to the generating lines;

^{*} Compare the Note to page 42.

ARTS. 386, 387.]

FAMILIES OF SURFACES.

third, conical surfaces, with the property,

III... $S\nu(\rho - a) = 0$, if a be vector of vertex;

and fourth, *derelopable* surfaces, with the distinguishing property expressed by the more general equation,

IV... $\nabla \nu d\nu = 0$, if $d\rho$ have the direction of a generatrix;

 ν being in each the normal vector to the surface, so that

V... $S_{\nu}d\rho = 0$, for all tangential directions of $d\rho$;

and the *fourth* family *including* the *third*, which in its turn includes the *second*. A few additional remarks on these equations may be here made.

(1.) The geometrical signification of the equation I. (as regards the radii) is obvious; but on the side of calculation it may be useful to remark, that elimination of ν between I. and V. gives, for spheres,

VI... $S(\rho - a)d\rho = 0$, or VII... $T(\rho - a) = const.$

(2.) The equations II. and V. show that $d\rho$, and therefore $\Delta\rho$, may have the given direction of a; for an arbitrary cylinder, then, we have the vector equation (372),

VIII...
$$\rho = \phi(x, y) = \psi_x + y_y$$

where ψ_x is an arbitrary vector function of x.*

(3.) From VIII. we can at once infer, that

1X...
$$S\beta\rho = S\beta\psi_x$$
, $S\gamma\rho = S\gamma\psi_x$, if $a = V\beta\gamma$;

the scalar equation (373) of a cylindrical surface is therefore generally of the form (comp. 371, (6.), (7.)),

X. . .
$$0 = F(S\beta\rho, S\gamma\rho);$$

 β and γ being two constant vectors, and the generating lines being perpendicular to both.

(4.) The equation III. may be thus written,

XI... $S\nu Ua = Ta^{-1}S\nu\rho$; whence XII... $S\nu Ua = 0$, if $Ta = \infty$;

^{* [}In general $d\rho = D_x \rho \cdot dx + D_y \rho \cdot dy$, and as one direction of $d\rho$ is parallel to α , we may write without loss of generality, $d\rho = D_x \rho dx + \alpha dy$. Moreover, since α is constant, $D_x \rho$ must be a function of x, so on integration $\rho = \psi_x + y\alpha$.]

[III. III. §5.

the equation for *cones* includes therefore that for *cylinders*, as was to be expected, and reduces itself thereto, when the vortex becomes infinitely distant.

(5.) The same equation III., when compared with V., shows that $d\rho$ may have the direction of $\rho - a$, and therefore that $\rho - a$ may be multiplied by any scalar; the *rector equation* of a *conical surface* is therefore of the form,

XIII... $\rho = a + y\psi_x$, ψ_x being an arbitrary vector function.*

(6.) The scalar equation of a cone may be said to be the result of the elimination of a scalar variable t, between two equations of the forms,

XIV...
$$S(\rho - a)\chi_t = 0$$
, $S(\rho - a)\chi'_t = 0$,

which express that the cone is the envelope (comp. 386, (11.)) of a variable plane, which passes through a fixed point, and involves only one scalar parameter in its equation: with a new reduction to a cylinder, in a case on which we need not here delay.

(7.) The equation IV. implies, that for each *point* of the surface there is a *direction* along which we may move, *without changing the tangent plane*; and therefore that the surface is an *envelope of planes*, &c., as in 386, and consequently that it is *developable*, in the sense of Art. 382.[†]

(8.) The vector equation of a general developable surface may be written under the form,

XV...
$$\rho = \phi(x, y) = \psi_x + y \mathbf{U} \psi'_x;$$

the sign of a *versor* being here introduced, for the sake of facilitating the passage, at a certain *limit*, to a *cone* (comp. 386, (12.)).

(9.) And the scalar equation of the same arbitrary developable may be represented as the result of the elimination of t, between the two equations,

XVI...
$$S\rho\chi_t + 1 = 0$$
, $S\rho\chi'_t = 0$;

in which χ_t is an arbitrary vector function of t.

* [As in the last note, because one direction of $d\rho$ is parallel to $\rho - \alpha$, we may take

$$\begin{split} \mathrm{d}\rho &= (\rho - \alpha) y^{-1} \mathrm{d}y + \mathrm{D}_x \rho \cdot \mathrm{d}x, \quad \mathrm{or} \quad \mathrm{d} \cdot y^{-1} (\rho - \alpha) = y^{-1} \mathrm{D}_x \rho \cdot \mathrm{d}x = \mathrm{d} \cdot \psi_x. \\ \rho &= \alpha + y \psi_x. \end{split}$$

Hence,

^{† [}The normal at any point of the ruled surface $\rho = \psi_x + y\phi_x$ is parallel to $V(\psi'_x + y\phi'_x)\phi_x$. If the direction of the normal does not change as we pass along a generator, either $V\psi'_x\phi_x = 0$, or $V\phi'_x\phi_x = 0$. The first of these conditions requires the surface to be a developable. The second requires all the generators to be parallel, so that the surface is a cylinder. See Tait's Quaternions. Art. 311.]

ABTS. 387, 388.] ELIMINATION OF ARBITRARY FUNCTIONS.

(10.) The envelope of a *plane* with *two* arbitrary and scalar parameters, t and u, is generally a *curved* but *underelopable surface*, which may be represented by the system of the *three scalar equations*,

XVII...
$$S\rho\chi_t$$
, $u + 1 = 0$, $S\rho D_t\chi = 0$, $S\rho D_u\chi = 0$;

where $-\chi$ denotes the reciprocal of the perpendicular from the origin on the tangent plane to the surface, at what may be called *the point* (t, u).

388. It remains, on the plan lately stated (380), to consider briefly surfaces of revolution, and to investigate the geodetic lines, on this additional family of surfaces; of which the equation, analogous to those marked I. II. III. IV. in 387, for spheres, cylinders, cones, and developables, is of the form,

I. . .
$$\operatorname{Sap}\nu = 0$$
,

if a be a given line in the direction of the *axis* of revolution, supposed for simplicity to pass through the origin; but which may also be represented by either of these two other equations, not involving the normal ν ,

II. . .
$$\mathbf{T}\rho = f(\mathbf{S}a\rho)$$
, or III. . . $\mathbf{T}\mathbf{V}a\rho = F(\mathbf{S}a\rho)$,

where f and F are used as characteristics of two *arbitrary* but *scalar functions*: between which $Sa\rho$ may be conceived to be eliminated, and so a *third form* of the same sort obtained.

(1.) In fact, the equation I. expresses that $\nu \parallel \mid a, \rho$, or that the normal to the surface intersects the axis; while II. expresses that the distance from a fixed point upon that axis is a function of its own projection on the same fixed line, or that the sections made by planes perpendicular to the axis are circles; and the same circularity of these sections is otherwise expressed by III., since that equation signifies that the distance from the axis depends on the position of the cutting plane, and is constant or variable with it : while the two last forms are connected with each other in calculation, by means of the general relation (comp. 204, XXI.),

IV...
$$(Ta\rho)^2 = (Sa\rho)^2 + (TVa\rho)^2$$
.

(2.) The equation I. is analogous, in quaternions, to a partial differential equation of the first order, and either of the two other equations, II. and III., is analogous to the integral of that equation, in the usual differential calculus of scalars.

(3.) To accomplish the corresponding *integration* in *quaternions*, or to pass from the form I. to II., whence III. can be deduced by IV., we may observe that the equation I. allows us to write (because $Svd\rho = 0$),

V. . .
$$\nu = xa + y\rho$$
, VI. . . $xSad\rho + yS\rho d\rho = 0$,

so that the two scalars $Sa\rho$ and $T\rho$ are together constant, or together variable, and must therefore be functions of each other.

(4.) Conversely, to eliminate the arbitrary function from the form II., quaternion differentiation gives,

VII. . . 0 = S(U
$$\rho$$
 . d ρ) + $f'(Sa\rho)$. Sad ρ = S . (U ρ + $af'Sa\rho$)d ρ ;

hence

VIII... $\nu \parallel \mathbf{U}\rho + af'\mathbf{S}a\rho$, and IX... $\nu \parallel \mid a, \rho$, as before;

so that we can return in this way to the equation I., the functional sign f disappearing.

(5.) We have thus the germs of a *Calculus of Partial Differentials in Quaternions,*^{*} *analogous* to that employed by Monge, in his researches respecting *families of surfaces*: but we cannot attempt to pursue the subject farther here.

(6.) But as regards the *geodetic lines* upon a surface of revolution, we have only to substitute for ν , in the recent formula I., by 380, IV., the expression dUd_ρ, which gives at once the *differential equation*,

X... $0 = Sa\rho dUd\rho = d \cdot Sa\rho Ud\rho$ (because $S(ad\rho \cdot Ud\rho) = -SaTd\rho = 0$);

whence, by a first integration, c being a scalar constant,

XI... $c = Sa\rho Ud\rho = TVa\rho \cdot SU(Va\rho \cdot d\rho).$

$$\begin{split} \delta \int \mathrm{d}s &= \delta \int \mathrm{Td}\rho = \int \delta \mathrm{Td}\rho = -\int \mathrm{S} \left(\mathrm{Ud}\rho \cdot \delta \mathrm{d}\rho \right) \\ &= -\int \mathrm{S} \left(\mathrm{Ud}\rho \cdot \mathrm{d}\delta\rho \right) = -\Delta \mathrm{S} \left(\mathrm{Ud}\rho \cdot \delta\rho \right) + \int \mathrm{S} \left(\mathrm{d}\mathrm{Ud}\rho \cdot \delta\rho \right), \end{split}$$

and therefore $dUd\rho \mid\mid \nu$, or $V\nu dUd\rho = 0$, as in 380, IV., in order that the expression under the last integral sign may vanish for all variations $\delta\rho$ consistent with the equation of the surface: while the evanescence of the part which is outside that sign \int supplies the equations of limits, or shows that the shortest line between two curves on a given surface is perpendicular to both, as usual.

[III. III. § 5.

^{*} The same remark was made in page 574 of the *Lectures*, in which also was given the elimination of the arbitrary function from an equation of the recent form III. It was also observed, in page 578, that *geodetics* furnish a very simple example of what may be called the *Calculus of Variations in Quaternions*; since we may write,

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INTEGRATION.

(7.) The characteristic property of the sought curves is, therefore, that for each of them the *perpendicular distance from the axis of revolution varies inversely as the cosine*^{*} of the angle, at which the geodetic crosses a parallel, or *circular section* of the surface: because, if Ta = 1, the line $\nabla a\rho$ has the *length* of the *perpendicular* let fall from a point of the curve on the axis, and has the *direction* of a *tangent* to the parallel.

(8.) The equation XI. may also be thus written,

XII...
$$c' \Gamma \rho' = S a \rho \rho'$$
, where $\rho' = D_t \rho$;

and if the independent variable t be supposed to denote the time, while the geodetic is conceived to be a curve described by a moving point, then while $T\rho'$ evidently represents the linear velocity of that point, as being = ds : dt, if s denote the arc (comp. 100, (5.), and 380, (7.), (11.)), it is easy to prove that Sapp' represents the double areal velocity, projected on a plane perpendicular to the axis; the one of these two velocities varies therefore directly as the other : and in fact, it is known from mechanics, that each velocity would be constant,⁺ if the point were to describe the curve, subject only to the normal reaction of the surface, and undisturbed by any other force.

(9.) As regards the analysis, it is to be observed that the differential equation X. is satisfied, not only by the geodetics on the surface of revolution, but also by the parallels on that surface: which fact of calculation is connected with the obvious geometrical property, that every normal plane to such a parallel contains the axis of revolution.

(10.) In fact if we draw the normal plane to any curve on the surface, at a point where it crosses a parallel, this plane will intersect the axis, in the point where that axis is met by the normal to the surface, drawn at the same point of crossing; but this construction fails to determine that normal, if the curve coincide with, or even touch a parallel, at the point where its normal plane is drawn.

^{*} Unless it happen that this cosine is constantly zero, in which case c = 0, and the geodetic is a meridian of the surface.

[†] This remark is virtually made in page 443 of Professor De Morgan's Differential and Integral Calculus (London, 1842), which was alluded to in page 578 of the Lectures on Quaternions. [If p is the normal reaction of the surface, the differential equation of motion of the particle is $\rho'' = pU\nu$. From this equation the mechanical properties may be at once deduced.]

HAMILTON'S ELEMENTS OF QUATERNIONS, VOL. II.

SECTION 6.

On Osculating Circles and Spheres, to Curves in Space; with some connected Constructions.

389. Resuming the expression 376, I. for ρ_l , and referring again to fig. 77 [p. 24], we see that if a circle PQD be described, so as to touch a given curve POR, or its tangent PT, at a given point P, and to cut the curve at a near point q, and if PN be the projection of the chord PQ on the diameter PD, or on the radius CP, then because we have, rigorously,

I...
$$PQ = t\rho' + \frac{1}{2}t^2u\rho''$$
, with $u = 1$ for $t = 0$,
we have also
II... $PN = \frac{1}{2}t^2 V u\rho''\rho' : \rho'$,
and

and

III...
$$\frac{1}{PC} = \frac{2}{PD} = \frac{2_{PN}}{PQ^2} = \frac{Vu\rho''\rho'}{(\rho' + \frac{1}{2}tu\rho'')^2\rho'}$$

Conceiving then that the near point *q* approaches indefinitely to the given point P, in which case the ultimate state or limiting position of the circle PQD is said to be that of the osculating circle to the curve at that point P, we see that while the plane of this last circle is the osculating plane (376), the vector κ of its centre κ , or of the limiting position of the point c, is rigorously expressed by the formula:

IV. . .
$$\kappa = \rho + \frac{\rho^{\prime 3}}{\nabla \rho^{\prime \prime} \rho^{\prime \prime}};$$

which may however be in many ways transformed, by the rules of the present Calculus.

(1.) Thus, we may write, as transformations of the expression IV., the following:

V. . .
$$\kappa = \rho + \frac{\rho'}{V\rho''\rho'^{-1}} = \rho - \frac{T\rho'}{V\rho''\rho'^{-1}} = \rho - \frac{T\rho'}{(U\rho')};$$

or introducing differentials instead of derivatives, but leaving still the independent variable arbitrary,

VI. . .
$$\kappa = \rho - \frac{\mathrm{d}\rho^3}{\mathrm{Vd}\rho\mathrm{d}^2\rho} = \rho + \frac{\mathrm{d}\rho}{\mathrm{Vd}^2\rho\mathrm{d}\rho^{-1}} = \rho - \frac{\mathrm{Td}\rho}{\mathrm{d}\mathrm{U}\rho'} = \rho - \frac{\mathrm{d}s}{\mathrm{d}\mathrm{Ud}\rho},$$

if s be the arc of the curve; so that the last expression gives this very simple

ART. 389.] OSCULATING CIRCLES TO CURVES IN SPACE.

formula, for the reciprocal of the radius of curvature, or for the ultimate value of 1 : cp,

VII. . . $(\rho - \kappa)^{-1} = D_s U \rho'$, where $U \rho' = U d \rho$, as before.

(2.) To interpret this result, we may employ again that auxiliary and spherical curve, upon the cone of parallels to tangents, which has already served us to construct, in 379, (6.) and (7.), the osculating plane, the absolute normal, and the binormal, to the given curve in space. And thus we see, that while the semidiameter PC has ultimately the direction of $dU\rho'$, and therefore that of the absolute normal (379, II.) at P, the length of the same radius is ultimately equal to the arc PQ (or Δs) of the given curve, divided by the corresponding arc of the auxiliary curve; or that the radius of curvature, or radius of the osculating circle at P, is equal to the ultimate quotient of the arc PQ itself at P, and to its prolongation QR at Q, although these two tangents are generally in different planes, and have no common point, so long as PQ remains finite: because we suppose that the given curve is in general one of double curvature, although the formulæ, and the construction, above given, are applicable to plane curves also.

(3.) For the *helix*, the formula IV. gives, by values already assigned for ρ , ρ' , ρ'' , and *a*, the expression,

VIII. . .
$$\kappa = cta - a^t\beta \cot^2 a$$
, whence IX. . . $\rho - \kappa = a^t\beta \operatorname{cosec}^2 a$,

a being the inclination of the given helix to the axis; the locus of the centre of the osculating circle is therefore in this case a second helix, on the same cylinder, if $a = \frac{\pi}{4}$, but otherwise on a co-axal cylinder, of which the radius = the given radius T β , multiplied by the square of the cotangent of a; and the radius of curvature = T($\rho - \kappa$) = T $\beta \times \csc^2 a$, so that this radius alwavs exceeds the radius of the cylinder, and is cut perpendicularly (without being prolonged) by the axis.

(4.) In general, if $T\rho' = \text{const.}$, and therefore $S\rho'\rho'' = 0$ (comp. 379, (2.)), the expression IV. becomes,*

X...
$$\kappa = \rho + \frac{\rho'^2}{\rho''}$$
; whence, XI... $\kappa = \rho - \rho''^{-1}$, if $T\rho' = 1$,

^{*} The expressions X. XI. may also be easily deduced by limits, from the construction in 383, (2.).

[III. III. § 6.

that is, if the *are* be taken as the *independent variable* (380, (12.)). Under this last condition, then, the formula VII. reduces itself to the following,

XII. . .
$$(\rho - \kappa)^{-1} = \rho'' = D_s^2 \rho \cdot ultimate reciprocal of radius CP;$$

so that ρ'' (for $T\rho' = 1$) may be called the Vector of Curvature, because its tensor $T\rho''$ is a numerical measure for what is usually called the curvature^{*} at the point P, and its versor $U\rho''$ represents the ultimate direction of the semidiameter PC, of the circle constructed as above.

(5.) As an example of the application (2.) of the formula IV. for κ , to a plane curve, let us take the ellipse,

XIII...
$$\rho = \operatorname{Va}^t \beta$$
, $\operatorname{Ta} = 1$, $\operatorname{Sa} \beta < 0$, 337, (2.),

considered as an oblique section (314, (4.)) of a right cylinder. The expressions 376, (5.) for the derivatives of ρ , combined with the expression XIII. for that vector itself, give here the relations,

XIV...
$$\nabla \rho \rho^{\prime\prime} = 0$$
, $\nabla \rho^{\prime} \rho^{\prime\prime\prime} = 0$;

and therefore comp. (338, (5.)),

XV...
$$V\rho\rho' = \text{const.} \dagger = \frac{\pi}{2}\beta\gamma$$
, $V\rho'\rho'' = \text{const.} = \left(\frac{\pi}{2}\right)^3\beta\gamma$, if $\gamma = Va\beta$;

hence for the present curve we have by IV.,

XVI...
$$\kappa = \rho - \frac{\rho'^3}{\nabla \rho' \rho''} = \nabla a^t \beta - (\nabla a^{t+1} \beta)^3 (\beta \gamma)^{-1}.$$

(6.) To *interpret* this result, we may write it as follows,

XVII...
$$\kappa = \rho - \frac{{\rho_1}^2}{\nabla \rho \rho' \cdot \rho'^{-1}}, \text{ where } \text{XVIII...} \rho_1 = \frac{2}{\pi} \rho' = \nabla \dot{\mathfrak{a}}^{l+1} \beta;$$

so that ρ_1 is the conjugate semidiameter of the ellipse (comp. 369, (4.)), and $V\rho\rho':\rho'$ is the perpendicular from the centre of that curve on the tangent. We recover then, by this simple analysis, the known result, that the radius of curvature of an ellipse is equal to the square of the conjugate semidiameter, divided by the perpendicular.

^{*} It may be remarked that the quantity z, or $T\psi''$, in the investigation (382) respecting geodetics on a developable, represents thus the curvature of the cusp-edge, for any proposed value of the arc, x, of that curve.

⁺ These values XV. might have been obtained without integrations, but this seemed to be the readiest way. [The constants may be determined by putting t = 0.]

ART. 389.]

VECTOR OF CURVATURE, EXAMPLES.

(7.) We may also write the equation XVI. under the form,

XIX...
$$\kappa = \rho - \frac{\rho_1^3}{V\rho\rho_1}$$
, where XX... $V\rho\rho_1 = \beta\gamma = \text{const.}$;

and may interpret it as expressing, that the radius of curvature is equal to the cube of the conjugate semidiameter, divided by the constant parallelogram under any two such conjugates; or by the rectangle under the major and minor semiaxes, which are here the vectors β and γ (comp. 314, (2.)).

(8.) The expression XVI. or XIX. for κ is easily seen to vanish, as it ought to do, at the *limit* where the *ellipse* becomes a *circle*, by the *cylinder* being cut *perpendicularly*, or by the condition $S_{\alpha\beta} = 0$ being satisfied; and accordingly if we write,

XXI... $e = SU_{\alpha\beta} = excentricity of ellipse$, or XXII... $\gamma^2 = (1 - e^2)\beta^2$,

we easily find the expressions,

XXIII. . .
$$\rho = \beta S \cdot a^t + \gamma S \cdot a^{t-1}, \quad \rho_1 = -\beta S \cdot a^{t-1} + \gamma S \cdot a^t;$$

XXIV...
$$\rho_1^2 = \beta^2 (1 - e^2 (\mathbf{S} \cdot \mathbf{a}^t)^2), \quad \frac{\rho_1}{\mathbf{V} \rho \rho_1} = \frac{\rho_1}{\beta \gamma} = \beta^{-2} \left(\beta \mathbf{S} \cdot \mathbf{a}^t + \frac{\gamma \mathbf{S} \cdot \mathbf{a}^{t-1}}{1 - e^2} \right);$$

so that the formula XIX. becomes,

XXV...
$$\kappa = e^2 \left(\beta (\mathbf{S} \cdot \mathbf{a}^t)^3 - \frac{\gamma (\mathbf{S} \cdot \mathbf{a}^{t-1})^3}{1 - e^2} \right) = e^2 \left(\beta (\mathbf{S} \cdot \mathbf{a}^t)^3 - \frac{\beta^2}{\gamma} (\mathbf{S} \cdot \mathbf{a}^{t-1})^3 \right),$$

thus containing e^2 as a factor.

(9.) And it may be remarked in passing, that the expression XVI., or its recent transformation XXV., for κ as a function of t, may be considered as being in quaternions the vector equation (comp. 99, I., or 369, I.) of the evolute* of the ellipse, or the equation of the locus of centres of curvature of that plane curve; and that the last form gives, by elimination of t (comp. 315, (1.), and 371, (5.)), the following system of two scalar equations for the same evolute,

XXVI...
$$\left(S\frac{\kappa}{\beta}\right)^{\frac{2}{3}} + \left(S\frac{\gamma\kappa}{\beta^2}\right)^{\frac{2}{3}} = e^{\frac{4}{3}}, \quad S\beta\gamma\kappa = 0;$$

^{*} That is to say, of the *plane evolute*; for we shall soon have occasion to consider briefly those evolutes of double curvature, which have been shown by Monge to exist, even when the given curve is *plane*.

XXVI'...
$$(S\beta\kappa)^{\frac{2}{3}} + (S\gamma\kappa)^{\frac{2}{3}} = (e\beta)^{\frac{4}{3}}, \&c.$$

which will be found to agree with known results.*

(10.) As another example of application to a *plane* curve, we may consider the *hyperbola*,

XXVII...
$$\rho = t_{\alpha} + t^{-1}\beta$$
, (comp. 371, II.),

with a and β for asymptotes, and with its centre at the origin. In this case the derived vectors are,

XXVIII...
$$\rho' = a - t^{-2}\beta, \quad \rho'' = 2t^{-3}\beta,$$

whence

XXIX...
$$V\rho^{\prime\prime}\rho^{\prime} = 2t^{-3}V\beta a = t^{-2}V\rho\rho^{\prime},$$

and the formula IV. becomes,

XXX...
$$\kappa - \rho = \frac{(t\rho')^2}{\nabla \rho \rho' : \rho'} = \frac{\mathbf{PT}^2}{\mathrm{ov}},$$

where ov is the perpendicular from the centre o on the tangent to the curve at \mathbf{r} , and \mathbf{rr} is the portion of that tangent, intercepted between the same point \mathbf{r} and an asymptote (comp. (6.) and 371, (3.)).

(11.) We may also interpret the denominator in XXX. as denoting the *projection* of the *semidiameter* or *on the normal*, or as the line NP where N is the foot of the perpendicular from the centre on that normal line; if then K be the sought centre of the osculating circle, we have the *geometrical* equations,

XXXI... NP. PK = PT², XXXII...
$$\angle$$
 NTK = $\frac{\pi}{2}$;

whereof the last furnishes evidently an extremely simple construction for the centre of curvature of an hyperbola, which we shall soon find to admit of being extended, with little modification, to a spherical conic + and its cyclic arcs.

(12.) The logarithmic spiral with its pole at the origin,

XXXIII. . .
$$\rho = a^t \beta$$
, $Sa\beta = 0$, $Ta < 1$, (comp. 314, (5.))

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 \mathbf{or}

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^{* [}The expression $(e\beta)^{\frac{1}{3}}$ is perhaps a little inaccurate. The cube-root of $(e\beta)^4$ is meant.]

[†] It was in fact for the *spherical* curve that the *geometrical construction* alluded to was *first* perceived by the writer, soon after the invention of the quaternions, and as a consequence of calculation with them: but it has been thought that a sub-article or two might be devoted, as above, to the *plane case*, or *hyperbolic limit*, which may serve at least as a verification.

may be taken as a *third example* of a *plane curve*, for the application of the foregoing formulæ. A first derivation gives, by 333, VII.,

XXXIV. . .
$$\rho' = (c + \gamma)\rho = \rho(c - \gamma), \ \rho'\rho^{-1} = c + \gamma, \text{ if } c = lTa, \text{ and } \gamma = \frac{\pi}{2}Ua;$$

the constant quaternion quotient, $\rho': \rho$, here showing that the prolonged vector or makes with the tangent rT a constant angle, n, which is given by the formula,

XXXV... $\tan n = (\mathrm{TV}:\mathrm{S}) \ (\rho':\rho) = c^{-1}\mathrm{T}\gamma, \quad \mathrm{or} \quad \cot n = \frac{2}{\pi}\mathrm{l}\mathrm{T}a;^*$

and a second derivation gives next,

XXXVI...
$$\rho'' = (c + \gamma)^2 \rho$$
, $\nabla \rho'' \rho' = (c^2 - \gamma^2) \rho^2 \gamma = \rho'^2 \gamma$.

The formula IV. becomes therefore, in this case,

XXXVII...
$$\kappa = \rho + \rho' \gamma^{-1} = \rho c \gamma^{-1} = -c \gamma^{-1} \rho = \frac{2 \Pi a}{\pi \Pi a} \cdot a^{t+1} \beta;$$

the evolute is therefore a second spiral, of the same kind as the first, and the radius of curvature KP subtends a right angle at the common pole. But we cannot longer here delay on applications within the plane, and must resume the treatment by quaternions of curves of double curvature.⁺

390. When the *logic* by which the expression 389, IV. was obtained, for the vector κ of the centre of the osculating circle, has once been fully *understood*, the *process* may be conveniently and safely *abridged*, as follows. Referring still to fig. 77 [p. 24], we may write briefly, as equations which are all *ultimately true*, or true *at the limit*, in a sense which is supposed to be now distinctly seen :

I...
$$PT = d\rho$$
, $TQ = \frac{1}{2}d^2\rho$, $PN = (part of PQ \perp PT =) \frac{Vd^2\rho d\rho}{2d\rho}$,

by 203, &c.; whence, ultimately,

II. . .
$$\kappa - \rho = PC = \frac{PQ^2}{2PN} = \frac{PT^2}{2PN} = \frac{d\rho^3}{Vd^2\rho d\rho},$$

as before: this *last* expression, in which $Vd^2\rho d\rho$ denotes briefly $V(d^2\rho \cdot d\rho)$,

^{*} If r be radius vector, and θ polar angle, and if we suppose for simplicity that $T\beta = 1$, the ordinary *polar equation* of the spiral becomes $r = a^{\theta}$, with $a = Ta^{\frac{2}{n}}$, and cot n = la, as usual.

^{+ [}The differential equations $\rho'' = c\rho$, compare (5.); $\nabla\beta\rho'' = 0$ (10.); $\rho' = q\rho$ and $\rho'' = q\rho$ (12.) will afford useful exercises in integration and in geometrical and dynamical interpretation.]

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being rigorous, and permitting the choice of any scalar, to be used as the *independent variable*. And then, by writing,

III. . .
$$d\rho = \rho' dt$$
, $d^2 t = 0$, $d^2 \rho = \rho'' dt^2$,

the factor dt^3 disappears, and we pass at once to the expression,

IV. . .
$$\kappa - \rho = \frac{\rho'^3}{\nabla \rho'' \rho'}$$
, (389, IV.),

which had been otherwise found before.

(1.) When the *arc* of the curve is taken for the independent variable, then (comp. 380, (12.) &c.) the expression II. reduces itself to the following,

V...
$$\kappa - \rho = \frac{\mathrm{d}\rho^2}{\mathrm{d}^2\rho}$$
, because $\mathrm{Sd}^2\rho\mathrm{d}\rho = 0$;

and accordingly the *angle* PTQ in fig. 77 is then *ultimately right* (comp. 383, (5.)), so that we may at once write, with *this choice* of the scalar variable,

VI...
$$\kappa - \rho = (ult.) \text{ pc} = (ult.) \frac{\text{PT}^2}{2\text{TQ}} = \frac{d\rho^2}{d^2\rho}$$
, as above.

(2.) Suppose then that we have thus geometrically (and very simply) deduced the expression V. for $\kappa - \rho$, for this particular choice of the scalar variable; and let us consider how we might thence pass, in calculation, to the more general formula II., in which that variable is left arbitrary. For this purpose, we may write, by principles already stated,

VII. . .
$$(\rho - \kappa)^{-1} = \frac{\mathrm{d}^2 \rho}{(\mathrm{Td}\rho)^2} = \frac{1}{\mathrm{Td}\rho} \mathrm{d} \frac{\mathrm{d}\rho}{\mathrm{Td}\rho} = \frac{\mathrm{d}\mathrm{Ud}\rho}{\mathrm{Td}\rho} = \frac{\mathrm{Vd}^2 \rho \mathrm{d}\rho^{-1}}{\mathrm{Td}\rho} \frac{\mathrm{Ud}\rho}{\mathrm{Td}\rho}$$
$$= -\frac{\mathrm{Vd}^2 \rho \mathrm{d}\rho^{-1}}{\mathrm{d}\rho} = \frac{\mathrm{Vd}\rho \mathrm{d}^2 \rho}{\mathrm{d}\rho^3};$$

and the required transformation is accomplished.

(3.) And generally, if s denote the arc of any curve of which ρ is the variable vector, we may establish the symbolical equations,

VIII...
$$D_s = \frac{1}{\mathrm{Td}\rho} \mathrm{d}$$
; $D_s^2 = \frac{1}{\mathrm{Td}\rho} \mathrm{d} \frac{1}{\mathrm{Td}\rho} \mathrm{d} = \left(\frac{1}{\mathrm{Td}\rho} \mathrm{d}\right)^2$; &c.

(4.) For example (comp. 389, XII.), the Vector of Curvature, $D_s^*\rho$, admits of being expressed generally under any one of the five last forms VII.

[III. III. § 6.

ARTS. 390, 391.] POLAR AXIS, POLAR DEVELOPABLE.

391. Instead of determining the vector κ of the centre of the osculating circle by one vector expression, such as 389, IV., or any of its transformations, we may determine it by a system of *three scalar equations*, such as the following,

I...
$$S(\kappa - \rho)\rho' = 0$$
; II... $S(\kappa - \rho)\rho'' - \rho'^2 = 0$;
III... $S(\kappa - \rho)\rho'\rho'' = 0$,

of which it may be observed that the second is the *derivative* of the first, if κ be treated as constant (comp. 386, (4.)); and of which the first expresses (369, IV.) that the sought *centre* is in the normal plane to the curve, while the third expresses (376, V.) that it is in the osculating plane; and the second serves to fix its position on the absolute normal (379), in which those two planes intersect.

(1.) Using *differentials* instead of derivatives, but leaving still the independent variable arbitrary, we may establish this equivalent system of three equations,

IV...
$$S(\kappa - \rho)d\rho = 0$$
; V... $S(\kappa - \rho)d^2\rho - d\rho^2 = 0$;
VI... $S(\kappa - \rho)d\rho d^2\rho = 0$;

of which the second is the differential of the first, if κ be again treated as constant.

(2.) It is also permitted (comp. 369, (2.), 376, (3.), and 380, (2.)), with the same supposition respecting κ , to write these equations under the forms,

VII...
$$d\mathbf{T}(\kappa - \rho) = 0$$
; VIII... $d^{2}\mathbf{T}(\kappa - \rho) = 0$;
IX... $d\mathbf{UV}(\kappa - \rho)d\rho = 0$;

and to connect them with geometrical interpretations.

(3.) For instance, we may say that the *centre* of the osculating circle is the point, in which the osculating *plane*, III. or VI. or IX., is *intersected* by the *axis* of that circle; namely, by the *right line* which is drawn through its centre, at right angles to its plane: and which is represented by the *two* scalar equations,

I. and II., or IV. and V., or VII. and VIII.

(4.) And we may observe (comp. 370, (8.)), that whereas for a point R taken arbitrarily *in the normal plane* to a curve at a given point P, we can HAMILTON'S ELEMENTS OF QUATERNIONS, Vol. 11.

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only say in general, that if a chord PQ be called small of the first order, then the difference of distances, $RQ - \overline{RP}$, is small of an order higher than the first; yet, if the point R be taken on the axis (3.) of the osculating circle, then this difference of distance is small, of an order higher than the second, in virtue of the equations VII. and VIII.

(5.) The right line I. II., or IV. V., or VII. VIII., as being the locus of points which may be called poles of the osculating circle, on all possible spheres passing through it, is also called the *Polar Axis* of the curve itself, corresponding to the given point of osculation.

(6.) And because the equation II. is (as above remarked) the *derivative* of I., the known theorem follows (comp. 386), that the *locus* of all such *polar* axes is a *developable surface*, namely that which is called the *Polar Developable*, or the *envelope of the normal planes* to the given curve; of which surface we shall soon have occasion to consider briefly the *cusp-edge*.

392. The following is an entirely different method of investigating, by quaternions, not merely the radius or the centre of the osculating circle to a curve in space, but the vector equation of that circle itself: and in a way which is applicable alike, to plane curves, and to curves of double curvature.

(1.) In general, conceive that $oT = \tau$ is a given tangent to a circle, at a given point which is for the moment taken as the origin; and let $PP' = \rho'$ represent a variable tangent, drawn at the extremity of the variable chord $OP = \rho$: also let v be the intersection, $OT \cdot PP'$, of these two tangents. Then the isosceles triangle OUP, combined with the formula 324, XI. for the differential of a reciprocal, gives easily the equations,

I...
$$\rho' \mid \rho \tau^{-1} \rho$$
; II... $\nabla \tau \rho^{-1} \rho' \rho^{-1} = -(\nabla \tau \rho^{-1})' = 0$;
III... $\nabla \tau \rho^{-1} = \text{const.} = \nabla \tau a^{-1}$, as in 296, IX.",

if a be the vector of any second given point A of the circumference.

(2.) The vector equation of the circle PQD (389) is therefore,

IV. ...
$$V \frac{2\rho'}{\omega-\rho} = V \frac{2\rho'}{\rho_t-\rho} = \frac{2}{t} V. (1 + \frac{1}{2}tu\rho''\rho'^{-1})^{-1} = -V. u\rho''\rho'^{-1}(1 + \frac{1}{2}tu\rho''\rho'^{-1})^{-1};$$

whence, passing to the *limit* (t = 0, u = 1), the analogous equation of the osculating circle is at once found to be,

V...
$$V \frac{2\rho'}{\omega - \rho} = -V \frac{\rho''}{\rho'}, \text{ or } VI... V\left(\frac{2d\rho}{\omega - \rho} + \frac{d^2\rho}{d\rho}\right) = 0;$$

ARTS. 391, 392.] VECTOR EQUATION OF OSCULATING CIRCLE.

with the verification (comp. 296, (9.)), that when we suppose,

VII...
$$\omega - \rho = 2(\kappa - \rho) \perp \rho',$$

the vector κ of the *centre* is seen to satisfy the equation,

VIII.
$$\therefore \frac{\rho'}{\kappa - \rho} = -\nabla \frac{\rho''}{\rho'}, \text{ or } IX. \therefore \frac{d\rho}{\kappa - \rho} + \nabla \frac{d^2 \rho}{d\rho} = 0;$$

which agrees with recent results (389, IV., &c.).

(3.) Instead of conceiving that a circle is described (389), so as to touch a given curve (fig. 77) at P, and to cut it at one near point Q, we may conceive that a circle cuts the curve in the given point P, and also in two near points, Q and R, unconnected by any given law, but both tending together to coincidence with P: and may inquire what is the limiting position (if any) of the circle PQR, which thus intersects the curve in three near points, whereof one (P) is given.

(4.) In general, if α , β , ρ be three co-initial chords, OA, OB, OP, Of any ONE circle, their reciprocals α^{-1} , β^{-1} , ρ^{-1} , if still co-initial, are termino-collinear (260); applying which principle, we are led to investigate the condition for the three co-initial vectors,

X...
$$(\omega - \rho)^{-1}$$
, $(s\rho' + \frac{1}{2}s^2u_s\rho'')^{-1}$, $(t\rho' + \frac{1}{2}t^2u_t\rho'')^{-1}$,

with $u_0 = 1$, thus *ultimately* terminating on *one right line*; or for our having ultimately a relation of the form,

XI...
$$\frac{xs+yt}{\omega-\rho} = \frac{x}{\rho'+\frac{1}{2}s\rho''} + \frac{y}{\rho'+\frac{1}{2}t\rho''};$$

XII.
$$. \frac{(xs + yt)\rho'}{\omega - \rho} = \frac{x}{1 + \frac{1}{2}s\rho''\rho'^{-1}} + \frac{y}{1 + \frac{1}{2}t\rho''\rho'^{-1}} = x + y - \frac{1}{2}(xs + yt)\rho''\rho'^{-1} + \&c. :$$

in which last equation, both members are generally quaternions.*

(5.) The comparison of the scalar parts gives here no useful information, on account of the *arbitrary* character of the coefficients x and y; but *these*

* [Observe that
$$\frac{1}{\alpha + \beta} = \frac{1}{(1 + \beta \alpha^{-1})\alpha} = \frac{1}{\alpha} \cdot \frac{1}{1 + \beta \alpha^{-1}}$$
 if α and β are any two vectors.]

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or

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disappear, with the two other scalars, s and t, in the comparison of the vector parts, whence follows the determinate and limiting equation,

XIII...
$$2 \nabla \rho' (\omega - \rho)^{-1} = - \nabla \rho'' \rho'^{-1},$$

which evidently agrees with V.

(6.) It is then found, by this little quaternion calculation, as was of course to be expected,* that the *circle* (3.), through any three near points of a curve in space, coincides ultimately with the osculating circle, if the latter be still defined (389) with reference to a given tangent, and a near point, which tends to coincide with the given point of contact.

393. An osculating circle to a curve of *double* curvature does not generally meet that curve *again*; but it intersects generally a *plane* curve, of the degree *n*, to which it osculates, in 2n - 3 points, distinct from the point **P** of osculation, whereof one at least must be *real*, although it may happen to *coincide* with that point **P**: and such a circle intersects also generally a *spherical* curve of double curvature, and of the degree *n*, in n - 3 other points, namely in those where the osculating *plane* to the curve meets it again. An *example* of each of these two last cases, as treated by quaternions, may be useful.

(1.) In general, if we clear the recent equation, 392, V. or XIII., of fractions, it becomes,

I...
$$0 = 2\rho'^2 \nabla \rho'(\omega - \rho) + (\omega - \rho)^2 \nabla \rho'' \rho';$$

in which $\rho = oP =$ the vector of the given point of osculation, and ρ' , ρ'' are its first and second derivatives, taken with respect to any scalar variable t, and for the particular value (whether zero or not) of that variable, which answers to the *particular point* P; while ω denotes generally the vector of *any point* upon the circle, which osculates to the given curve at that point P.

(2.) Writing then (comp. 389, (10.)),

and

II. . .
$$\rho = ta + t^{-1}\beta$$
, $\rho' = a - t^{-2}\beta$, $\rho'' = 2t^{-3}\beta$,
III. . . $\omega = oq = xa + x^{-1}\beta$,

to express that we are seeking for the remaining intersection Q of a plane

[•] This conclusion is indeed so well-known, and follows so obviously from the doctrine of *infinite-simals*, that it is only deduced here as a *verification* of previous formulæ, and for the sake of *practice* in the present Calculus.

ARTS. 392, 393.] VECTOR EQUATION OF OSCULATING CIRCLE.

hyperbola with its osculating circle at P, the equation I. becomes, after a few easy reductions, including a division by $\nabla \alpha \beta$, the following biquadratic in x,

IV...
$$0 = (x - t)^3 (t^3 a^2 x - \beta^2);$$

in which the *cubic factor* is to be set aside, as answering only to the point **p** itself.

(3.) Substituting then, in III., the remaining value IV. of x, we find the expression,

V...
$$\omega = oQ = \frac{(ta)^2}{t^{-1}\beta} + \frac{(t^{-1}\beta)^2}{ta} = \frac{1}{2} \left\{ \frac{(2ta)^2}{2t^{-1}\beta} + \frac{(2t^{-1}\beta)^2}{2ta} \right\};$$

comparing which with 371, (3.), we see that if the tangent to the hyperbola at the given point P intersects the asymptotes in the points A, B, then the tangent at the sought point Q meets the same lines OA, OB in points A', B', such that

VI. . .
$$OA \cdot OA' = OB^2$$
, $OB \cdot OB' = OA^2$;

whence q is at once found, as the bisecting point of the line A'B'.

(4.) A still more simple construction, and one more obviously agreeing with known results, may be derived from the following expression for the chord PQ:

VII. . .
$$\mathbf{PQ} = \omega - \rho = (t^2 \beta^{-2} - t^{-2} a^{-2}) (t a^2 \beta - t^{-1} a \beta^2)$$

= $(t^3 \beta^{-2} - t^{-1} a^{-2}) a \rho' \beta || a \rho'^{-1} \beta;$

whence it follows (comp. 226) that if this chord PQ, both ways prolonged, meets the two asymptotes of and on in the points R and s, we have then the *inverse similitude of triangles* (118),

VIII...
$$\Delta$$
 ros ∞' AOB.

(5.) As regards the equality of the intercepts, RP and α s, it can be verified without specifying the second point α on the hyperbola, or the second scalar, x, by observing that the formula III., combined with the first equation II., conducts to the expressions,

IX... OR =
$$\frac{x\rho - t\omega}{x - t} = (x^{-1} + t^{-1})\beta$$
, os = $\frac{t\rho - x\omega}{t - x} = (x + t)a$;

which give, generally,

X... RP = QS =
$$ta - x^{-1}\beta$$
.

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(6.) And as regards the general reduction, of the determination of the osculating circle to a spherical curve of double curvature, to the determination of the osculating *plane*, it is sufficient to observe that when we take the centre of the sphere for the origin, and therefore write (comp. 381, XIV.),

XI...
$$\rho^2 = \text{const.}, \quad S\rho\rho' = 0, \quad S\rho\rho'' = -\rho'^2,$$

then if we operate on the vector equation I. with the symbol $\nabla . \rho$, and divide by $-\rho'^3$, there results the scalar equation,

XII...
$$0 = 2S\rho(\omega - \rho) + (\omega - \rho)^2 = \omega^2 - \rho^2$$
,

which expresses that the *circle* is entirely contained on the same spheric* surface as the curve; while the other scalar equation,

XIII. . . 0 =
$$S\rho''\rho'(\omega - \rho)$$
,

obtained by operating on I. with $S \, \rho''$, expresses (comp. 376, V.) that the same circle is in the osculating plane :+ so that its centre κ is the foot of the perpendicular let fall on that plane from the origin, and we may therefore write (comp. 385, VI.),

XIV... OK =
$$\kappa = \frac{S\rho''\rho'\rho}{V\rho''\rho'}$$
, with the relations, XV... $S\frac{\omega}{\kappa} = S\frac{\rho}{\kappa} = 1$;

and with the verification that the expression XIV. agrees with the general formula, 389, IV., because

XVI. . .
$$\rho \nabla \rho'' \rho' + \rho'^3 = S \rho'' \rho' \rho$$
,

when the conditions XI. are satisfied.

(7.) And even if the given curve be not a spherical one, yet if we retain the general expression for κ ,

XVII. . .
$$\kappa = \rho + \frac{\rho'^3}{\nabla \rho'' \rho'},$$
 (389, IV.),

and operate on I. with S. ρ'' and S. $\rho''\rho'$, we find again the equation XIII.

[•] This conclusion is geometrically evident, but is here drawn as above, for the sake of practice in the quaternions.

⁺ Compare the Note immediately preceding.

ARTS. 393, 394.

CASE OF A SPHERICAL CURVE.

of the osculating plane, combined with a new scalar equation, which may after a few reductions be written thus,

XVIII...
$$(\omega - \kappa)^2 = (\rho - \kappa)^2$$
;

and which represents a *new sphere*, whereon the osculating circle to the curve is a *great circle*.

394. To give now an *example* of a *spherical curve* of double curvature, with its osculating *circle* and *plane* for any proposed point P, and with a determination of the point Q in which these meet the curve *again* (393), we may consider that *spherical conic*, or *sphero-conic*, of which the equations are (comp. 357, II.),

I. . .
$$\rho^2 + r^2 = 0$$
, II. . . $g\rho^2 + S\lambda\rho\mu\rho = 0$;

namely the intersection of the *sphere*, which has its centre at the origin, and its radius = r, with a cone of the second order, which has the same origin for vertex, and has the given lines λ and μ for its two (real) cyclic normals. And thus we shall be led to some sufficiently simple *spherical constructions*, which *include*, as their *plane limits*, the analogous constructions recently assigned for the case of the common *hyperbola*.

(1.) Since $S\lambda\rho\mu\rho = 2S\lambda\rho S\mu\rho - \rho^2S\lambda\mu$ (comp. 357, II'.), the equations I. and II. allow us to write, as their first derivatives, or at least as equations consistent therewith,

III. . .
$$S\rho\rho' = 0$$
, $S\lambda\rho' + S\lambda\rho = 0$, $S\mu\rho' - S\mu\rho = 0$,

because the independent variable is here arbitrary, so that we may conceive the first derived vector ρ' to be multiplied by any convenient scalar; in fact, it is only the *direction* of this tangential vector ρ' which is here important, although we must *continue* the derivations consistently, and so must write, as consequences of III., the equations,

IV...
$$S\rho\rho'' + \rho'^2 = 0$$
, $S\lambda\rho'' + S\lambda\rho' = 0$, $S\mu\rho'' - S\mu\rho' = 0$.

(2.) Introducing then the auxiliary vectors,

whence $V. . . \eta = V\lambda\mu, \quad \sigma = \lambda S\mu\rho + \mu S\lambda\rho, \quad \tau = \rho + \rho', \quad \upsilon = \rho - \rho',$ $VI. . . 0 = S\eta\sigma = S\lambda\tau = S\mu\upsilon, \quad S\rho\sigma = 2S\lambda\rho S\mu\rho, \quad S\mu\tau = 2S\mu\rho,$ $S\lambda\upsilon = 2S\lambda\rho, \quad \tau^2 = \upsilon^2 = \rho^2 + \rho'^2,$ and by new derivations,

VII...
$$\sigma' = \nabla \eta \rho$$
, $\tau' = \rho' + \rho''$, $\upsilon' = \rho' - \rho''$, $S\lambda \tau' = S\mu \upsilon' = 0$,
 $S\mu \tau' = S\mu \tau$, $S\lambda \upsilon' = -S\lambda \upsilon$,

we see first that τ and v are the vectors or and ou of the points in which the *rectilinear tangent* to the curve at **P** meets the two *cyclic planes*, perpendicular respectively to λ and μ ; and because the *radius* or is seen to be the *perpendicular bisector* of the *linear intercept* TU between those two planes, so that

or

$$VIII...\rho' = PT = UP \perp OP$$
, we have IX... $UOP = POT$,
 $X... \cap AP = \cap PB$,

if the *tangent arc* on the sphere, to the same conic at the same point P, meet the two *cyclic arcs* CA and CB in the points A and B: the *intercepted arc* AB being thus *bisected* at its point of *contact* P, which is a well-known property of such a curve.

(3.) Another known property of a sphero-conic is, that for any one such curve the sum of the two spherical angles CAB and ABC, and therefore also the area of the spherical triangle ABC, is constant. We can only here remark, in passing, that quaternions recognise this property, under the form (comp. II.),

XI... $\cos (A + B) = -SU\lambda\rho\mu\rho = -g : T\lambda\mu = const.$

(4.) The scalar equations III. and IV. give immediately the vector expressions,

XII...
$$\rho' = \frac{\nabla \rho (\lambda S \mu \rho + \mu S \lambda \rho)}{S \lambda \mu \rho}$$
, XIII... $\rho'' = \rho - \frac{(\rho^2 + \rho'^2) \nabla \lambda \mu}{S \lambda \mu \rho}$

or by (2.),

XIV...
$$\rho' = \frac{\nabla \rho \sigma}{S \eta \rho}$$
, and XV... $\rho'' = \rho - \xi$, if XVI... $\xi = \frac{\tau^2 \eta}{S \eta \rho}$
= $\tau - \tau' = \upsilon + \upsilon'$,

the new auxiliary vector ξ being thus that of the point x, in which the osculating plane to the conic at r meets the line η of intersection of the cyclic planes: so that we have the geometrical expressions,

XVII...
$$\rho'' = xP$$
, $\tau' = xT$, $-\upsilon' = xU$, if $\xi = ox$,

and the lines τ' and ν' are the traces of the osculating plane on those two

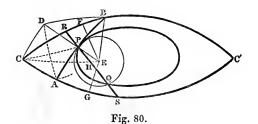
^{*} We may also consider the derived vectors τ' and v', or the lines xT and xU, as corresponding tangents, at the points T and U (2.), to the two sections, made by the cyclic planes, of that developable surface which is the locus of the tangents TPU to the spherical conic in question.

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cyclic planes, or of the latter on the former; while σ and σ' , as being perpendicular respectively to ρ' and ρ , while each $\perp \eta$, are the traces on the plane $\lambda \mu$ of the two cyclic normals, of the normal plane to the conic at the point **P**, and of the tangent plane to the sphere at that point: or at least these lines have the *directions* of those *traces*.

(5.) Already, from the expression XVI. for the portion ox of the radius oc (2.), or of that radius prolonged, which is cut off by the osculating plane at P, we can derive a simple construction for the position of the spherical centre, or pole, say E, of the small circle which osculates at that point P, to the proposed sphero-conic. For if we take the radius r for unity, we have the trigonometric expressions,

XVIII. . . See CE COS EP = $(T\xi = T\tau^2 : SU\eta^{-1}\rho =)$ sec² PB sec CP;



or letting fall (comp. fig. 80) the perpendicular CD on the normal arc PE,

XIX... $\cos DE = \cos DP \cos PB \cdot \cos PB \cos PE = \cos DB \cos BE$;

or finally,

XX... DBE (or dae) =
$$\frac{\pi}{2}$$
.

(6.) But although it is a perfectly *legitimate* process to *mix* thus *spherical* trigonometry with quaternions (since in fact the latter *include* the former), yet it may be satisfactory to deduce this last result by a more *purely* quaternionic method, which can easily be done as follows. The values (4.) of ρ' and ρ'' give,

XXI...
$$\nabla \rho' \rho'' S \eta \rho = \rho S \sigma \rho'' - \sigma S \rho \rho'' = \rho S \rho \sigma + \rho'^2 \sigma$$

= $(\tau - \rho') S \sigma \tau + \sigma S \rho' \tau = \tau S \sigma \tau + \nabla \tau \rho' \sigma ||| \tau, \quad \nabla \tau \rho' \sigma,$

in which $\rho'\sigma$ denotes a vector $\perp \rho'$ (because $S\rho'\sigma = 0$), and $||| \eta, \rho'$ (because $S\eta\rho'\rho'\sigma = 0$); this line $\rho'\sigma$ has therefore the direction of the *projection* of the line η on a plane perpendicular to ρ' , and we are thus led to draw, through

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the line oc of intersection of the cyclic planes, a *plane* cop perpendicular to the normal plane to the conic at P, or to let fall (as in fig. 80) a perpendicular *arc* cp on the normal arc PD; after which the normal to the sought osculating plane, or the *axis* of the osculating circle sought, as being $|| \nabla \rho' \rho''$, will be contained in the plane through the trace τ , or or, or ob, which is perpendicular to the plane of τ and $\rho' \sigma$, or to the plane DOB; and therefore the spherical angle DBE (or DAE) will be a right angle, as before.

(7.) We may also observe that if κ be the *centre* of the osculating circle, considered in its own plane, or the foot of the perpendicular on that plane from o, then by XXI.,

XXII... OK =
$$\kappa = \frac{S\rho\rho'\rho''}{V\rho'\rho''} = \frac{\tau^2 S\rho\sigma}{\rho S\rho\sigma + {\rho'}^2\sigma}, \quad KP = \rho - \kappa = \frac{\rho'^2 V\rho\sigma}{\rho S\rho\sigma + {\rho'}^2\sigma},$$

and therefore

XXIII...
$$\frac{\kappa_P}{\sigma\kappa} = \frac{\rho - \kappa}{\kappa} = \frac{\rho'^2 V}{\tau^2 S} \rho \sigma$$
, XXIV... $\tan \epsilon_P = \sin^2 \epsilon_P cot PD$,

which gives again the angular relation XX.; the quotient XXIII. being thus a *vector*, as it ought by 393, XV. to be; and the *trigonometric* formula XXIV. being obtained from its expression, by observing that

XXV... $T\rho'\tau^{-1} = \overline{PT}$: $\overline{oT} = \sin PoT = \sin PB$, and $(V:S)\rho\sigma = U\rho'$. cot PD, because $\sigma \perp \rho'\sigma$, but $|||\rho, \rho'\sigma$, or $\rho'\sigma \perp \sigma$, but $|||\rho, \sigma$.

(8.) The rectangularity of the planes of τ , κ and τ , $\rho'\sigma$ is also expressed by the equation,

XXVI...
$$0 = S(V_{\kappa\tau} \cdot V \rho' \sigma \tau) = S_{\kappa\tau} S \rho' \sigma \tau - \tau^2 S \rho' \sigma \kappa;$$

in proving which we may employ the values,

XXVII...
$$S\tau \kappa^{-1} = 1$$
, $S\rho'\sigma\kappa^{-1} = (-\tau^{-2}\rho'^2 S\eta\rho =) S\rho'\sigma\tau^{-1}$.

(9.) We may also interpret these equations XXVII., as expressing the system of the two relations,

XXVIII...
$$\kappa^{-1} - \tau^{-1} \perp \tau$$
, $\kappa^{-1} - \tau^{-1} \perp \rho' \sigma$;

from which it follows that κ^{-1} , and therefore also that κ , is a line in the plane so drawn through τ , as to be perpendicular to the plane through τ and $\rho'\sigma$, as before.

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(10.) And the two relations XXVIII. are both included in the following expression,

XXIX...
$$\kappa^{-1} - \tau^{-1} = \nabla \tau^{-1} \rho' \sigma : S \rho \sigma.$$

(11.) We may also easily deduce, from the foregoing spherical construction, the following trigonometric expressions, for the arcual radius r = EP of the osculating small circle (5.), and for the angle a = PAE = EBP which it subtends at A or at B:

XXX... $\tan r = \sin \frac{c}{2} \tan a$; XXXI... $\tan a = \frac{1}{2} (\cot A + \cot B)$;

A and B here denoting, as in XI., the base angles of the triangle ABC with c for vertex, and c denoting as usual the base AB, namely the portion of the arcual tangent (2.) to the conic, which is intercepted between the cyclic arcs.

(12.) The osculating *plane* and *circle* at r being thus fully and in various ways determined, we may next inquire (393) in what point Q do they meet the conic again. In symbols, denoting by ω the vector of this point, we have the three scalar equations,

XXXII...
$$S\kappa\omega = S\kappa\rho$$
, $S\lambda\omega S\mu\omega = S\lambda\rho S\mu\rho$, $\omega^2 = \rho^2$,

which are all evidently satisfied by the value $\omega = \rho$, but can in general be satisfied also by one other vector value, which it is the object of the problem to assign.

(13.) We satisfy the *two first* of these three equations XXXII., by assuming the expression,

XXXIII...
$$\omega = \xi + \frac{1}{2}(x^{-1}\tau' - x\upsilon'),$$

in which x is any scalar; in fact we have the relations,

XXXIV...
$$S\kappa\xi = S\kappa\rho$$
, $S\lambda\nu' = -2S\lambda\rho$, $S\mu\tau' = 2S\mu\rho$,
 $0 = S\lambda\xi = S\mu\xi = S\lambda\tau' = S\mu\nu' = S\kappa\tau' = S\kappa\nu'$,

whence XXXIII. gives,

And because

XXXV...
$$S\lambda\omega = xS\lambda\rho$$
, $S\mu\omega = x^{-1}S\mu\rho$, &c.
XXXVI... $\rho = \xi + \frac{1}{2}(\tau' - \nu')$,

we shall satisfy also the third equation XXXII., if we adopt for x any root of that new scalar equation, which is obtained by equating the square of

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the expression XXXIII. for ω , to what that square becomes when x is changed to 1.

(14.) To facilitate the formation of this new equation, we may observe that the relations,

 $\xi = \rho - \rho'', \quad \tau' = \rho' + \rho'', \quad \upsilon' = \rho' - \rho'', \quad S\rho\rho' = 0, \quad S\rho\rho'' = -\rho'^2,$

which have all occurred before, give

XXXVII... $48\xi\tau' = 3\tau'^2 + \upsilon'^2$, $48\xi\upsilon' = \tau'^2 + 3\upsilon'^2$;

the resulting equation is therefore, after a few slight reductions, the following biquadratic in x,

XXXVIII...
$$0 = (x - 1)^3 (v'^2 x - \tau'^2);$$

of which the *cubic factor* is to be rejected (comp. 393, (2.)), as answering only to the point P itself.

(15.) We have then the values,

XXXIX...
$$x = \tau'^2 \upsilon'^{-2}$$
, and XL... $oq = \omega = \xi + \frac{1}{2} \left(\frac{\upsilon'^2}{\tau'} - \frac{\tau'^2}{\upsilon'} \right);$

comparing which last expression with the formulæ XVII., we see that the required point of intersection a, of the sphero-conic with its osculating circle, can be *constructed* by the following rule. On the traces (4.), of the osculating plane on the two cyclic planes, determine two points τ_1 and u_1 , by the conditions,

XLI...
$$XT \cdot XT_1 = XU^2$$
, $XU \cdot XU_1 = XT^2$; then XLII... $T_1Q = QU_1$,

or in words, the right line T_1U_1 is bisected by the sought point Q.

(16.) But a still more simple or more graphic construction may be obtained, by investigating (comp. 393, (4.)) the direction of the chord PQ. The vector value of this rectilinear chord is, by XXXVI. and XL.,

XLIII...
$$PQ = \omega - \rho = \frac{1}{2} (\upsilon'^2 - \tau'^2) (\upsilon'^{-1} + \tau'^{-1}) = \frac{1}{2} (\tau'^{-2} - \upsilon'^{-2}) \tau' (\tau' + \upsilon') \upsilon'$$

$$= \left(\frac{\rho'^2}{\tau'^2} - \frac{\rho'^2}{\upsilon'^2}\right) \tau' \rho'^{-1} \upsilon', \quad \text{because} \quad \rho' = \frac{1}{2} (\tau' + \upsilon');$$

the chord rq has therefore the direction (or its opposite) of the *fourth proportional* (226) to the *three vectors*, ρ' , τ' , and $-\upsilon'$, or PT, XT, and XU; if then we

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conceive this chord or its prolongations to meet the traces xT, xu in two new points T_2 , U_2 , we shall have (comp. 393, VIII.) the two *inversely similar* triangles (118),

XLIV...
$$\Delta$$
 T₂XU₂ \propto' UXT.

(17.) To deduce hence a spherical construction for Q, we may conceive four planes, through the axis OKE, perpendicular respectively to the four following right lines in the osculating plane:

XLV...
$$\tau'$$
, $-\upsilon'$, ρ' , $\omega - \rho$, or XT, XU, PT, PQ;

which planes will cut the sphere in four great circles, whereof the four arcs,

are parts, if F, G, H (see again fig. 80) be the feet of the three arcual perpendiculars from the pole E of the osculating circle on the two cyclic arcs CB, CA, and on the arcual chord PQ.

(18.) These four arcs XLVI. are therefore connected by the same angular relation as the four lines XLV.; and we have thus the very simple formula,

$$XLVII...GEH = PEF,$$

expressing an equality between two spherical angles at the pole E, which serves to determine the direction of the arc EH, and therefore also the positions of the points H and Q, by means of the relations,

XLVIII. . . PHE = $\frac{\pi}{2}$, \circ PH = \circ HQ.

(19.) If the arcual chord PQ, both ways prolonged, or any chord of the conic, cut the cyclic arcs CB and CA in the points R and s (fig. 80), it is well-known that there exists the equality of intercepts (comp. 270, (2.)),

XLIX. . .
$$\cap$$
 RP = \cap QS;

and conversely this equation, combined with the formulæ (11.), or with the trigonometric expression,

L. . . tan PE = tan
$$r = \frac{1}{2} \sin \frac{c}{2} (\cot A + \cot B)$$
,

for the tangent of the arcual radius of the osculating circle, enables us to

determine what may be called perhaps the arcual chord of osculation PQ; by determining the spherical angle RPB, or simply P, from principles of spherical trigonometry alone, in a way which may serve as a verification of the results above deduced from quaternions.

(20.) Denoting by t the semitransversal RH = HS, and by s the semichord PH = HQ, the oblique-angled triangles RPB, SPA give the equations,

LI...
$$\begin{cases} \cot (t-s) \sin \frac{c}{2} = \cos P \cos \frac{c}{2} + \sin P \cot B, \\ \cot (t+s) \sin \frac{c}{2} = \cos P \cos \frac{c}{2} - \sin P \cot A; \end{cases}$$

while the right-angled triangle PHE gives,

LII. . .
$$\tan s = \sin P \tan r$$
.

Equating then the values of $\cot 2s$, deduced from LI. and LII., we eliminate s and t, and obtain a quadratic in tan r, of which one root is zero, when $\tan r$ has the value L.; such then might in this new way be inferred to be the tangent of the arcual radius of curvature of the conic, and the remaining root of the equation is then,

LIII...
$$\tan P = \frac{\cos \frac{c}{2} (\cot B - \cot A)}{\cot A \cot B + \cos^2 \frac{c}{2} - \tan^2 r};$$

a formula which ought to determine the inclination P, or RPB, or QPA, of the chord PQ to the tangent PA, but which does not appear at first sight to admit of any simple *interpretation*.*

(21.) On the other hand, the construction (17.) (18.), to which the quaternion analysis led us, gives

$$LIV... HEP = GEP - GEH = GEP - PEF = FEB + GEA$$
,

^{*} We might however at once see from this formula, that P = A - B at the *plane limit*; which agrees with the known construction 393, (4.), for the corresponding chord PQ in the case of the plane *hyperbola*.

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and therefore, by the four right-angled triangles, PHE, BFE, AGE, and BPE or EPA, conducts to this other formula,

LV...
$$\cot^{-1}(\cos r \cot P) = \cot^{-1}\left(\cos r \cos \frac{c}{2} \tan (B + a)\right)$$

- $\cot^{-1}\left(\cos r \cos \frac{c}{2} \tan (A + a)\right),$

in which a is the same auxiliary angle as in XXXI.; we ought therefore to find, as the proposed *verification* (19.), that this last equation LV. expresses virtually the same relation between A, B, c, and P, as the formula LIII., although there seems at first to be no connexion between them; and such agreement can accordingly be proved to exist, by a chain of ordinary trigonometric transformations, which it may be left to the reader to investigate.

(22.) A geometrical proof of the validity of the construction (17.) (18.) may be derived in the following way. The product of the sines of the arcual perpendiculars, from a point of a given sphero-conic on its two cyclic arcs, is well-known to be constant; hence also the rectangle under the distances of the same variable point from the two cyclic planes is constant, and the curve is therefore the intersection of the sphere with an hyperbolic cylinder, to which those planes are asymptotic. It may then be considered to be thus geometrically evident, that the circle which osculates to the spherical curve, at any given point P, osculates also to the hyperbola, which is the section of that cylinder, made by the osculating plane at this point; and that the point Q, of recent investigations, is the point in which this hyperbola is met again, by its own osculating circle at P. But the determination 393, (4.) of such a point of intersection, although above deduced (for practice) by quaternions, is a plane problem of which the solution was known; we may then be considered to have reduced, to this known and plane problem, the corresponding spherical problem (12.); and thus the inverse similarity of the two plane triangles XLIV., although found by the quaternion analysis, may be said to be geometrically explained, or accounted for: the traces xT and xU, or τ' and -v', of the osculating plane to the conic on the two cyclic planes (4.), being evidently the asymptotes of the hyperbola in question.

(23.) In quaternions, the constant *product of sines*, &c., is expressed by this form of the equation II. of the *cone*,

LVI. . .
$$SU\lambda\rho$$
 . $SU\mu\rho = (g - S\lambda\mu) : 2T\lambda\mu = const.$;

and the scalar equation of the hyperbolic *cylinder*, obtained by eliminating ρ^2 between I. and II., after the first substitution (1.), is

LVII... $S\lambda\rho S\mu\rho = \frac{1}{2}r^2(g - S\lambda\mu) = const.;$

while the expression XXXIII. for ω may be considered as the vector equation of the hyperbola, of which the intersection α with the *circle*, or with the *sphere*, is determined by combining that equation with the condition $\omega^2 = \rho^2 (= -r^2)$.

(24.) In the foregoing investigation, we have treated a sphero-conic in connexion with its cyclic arcs (2.); but it would have been about equally easy to have treated the same curve, with reference to its focal points: or to the focal lines of the cone, of which it is the intersection with a concentric sphere. (Compare what has been called the bifocal transformation, in 360, (2.).)

(25.) We can however only state generally here the result of such an application of quaternions, as regards the construction of the osculating small circle to a spherical conic, considered relatively to its foci: which construction^{*} can indeed be also geometrically deduced, as a certain polar reciprocal of the one given above. Two focal points (not mutually opposite) being called F and G, let PN be the normal arc at P, which is thus equally inclined, by a well-known principle, to the two vector arcs, FP, GP; so that if the focus G be suitably distinguished from its own opposite, the spherical angle FPG is bisected by the arc PN, which is here supposed to terminate on the given arc FG. At N erect an arc QNR, perpendicular to PN, and terminating in Q and R on the two vector arcs. Perpendiculars, QE, RE, to these last arcs, will meet on the normal arc PN, in the sought pole (or spherical centre) E, of the sought small circle, which osculates to the conic at the given point P.

(26.) The two *focal* and arcual *chords of curvature* from P, which pass through F and G, and terminate on the osculating circle, are evidently *bisected* at Q and R, in virtue of the foregoing *construction*, which may therefore be thus enunciated :—

The great circle QR, which is the common bisector of the two focal and arcual chords of curvature from a given point P, intersects the normal arc PN on the fixed arc FG, connecting the two foci; that is, on the arcual major axis of the conic.

^{*} The reader can easily draw the figure for himself. As regards the known rule, lately alluded to (in 393, (4.), and 394, (22.)), for determining the chord of intersection of a plane conic with its osculating circle, it will be found (for instance) in page 194 of Hamilton's Conic Sections (in Latin, London, 1758). The two spherical constructions, for the small circle osculating to a spherical conic, were carly deduced and published by the present writer, as consequences of quaternion calculations. Compare the second Note to page 54.

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(27.) The construction (5.) fails to determine the position of the auxiliary point D in fig. 80, for the case when the given point P is on the minor axis of the conic; and in fact the expressions (4.) for ρ' and ρ'' become infinite, when the denominator $S\lambda\mu\rho$ is zero. But it is easy to see that the auxiliary vector σ , which represents generally the trace of the normal plane to the curve on the plane of the two cyclic normals, becomes at the limit here considered the required axis of the osculating circle; and accordingly, if we assume simply (comp. (1.) and (2.)),

LVIII... $\rho' = V\rho\sigma$, and therefore $\rho'' = V\rho'\sigma + V\rho\sigma'$, we have LIX... $\sigma' = 0$, and $\nabla \rho' \rho'' || \sigma$, when $S\lambda \mu \rho = 0$.

(28.) In general, if we determine three points L, M, s in the plane of $\lambda \mu$, by the formulæ (comp. again (2.)),

LX...
$$oL = \frac{\lambda \rho^2}{S\lambda \rho}$$
, $oM = \frac{\mu \rho^2}{S\mu \rho}$, $os = \frac{\sigma \rho^2}{S\sigma \rho} = \frac{1}{2}(oL + oM)$,

then L and M will be the intersections of the cyclic normals λ , μ with the tangent plane to the sphere at P, and the normal plane to the curve at the same point will bisect the right line LM in the point s; we shall also have this proportion of sines,

LXI... sin los : sin som =
$$SU\lambda\rho$$
 : $SU\mu\rho$
= cos lop : cos pom = sin PP₁ : sin PP₂, (comp. (23.)),

if PP_1 , PP_2 be the arcual perpendiculars from the point P of the conic on the two cyclic arcs; and this general rule for determining the position of the line os, or σ , applies even to the *limiting case* (27.), when that variable line becomes the axis of the osculating circle, at a minor summit of the curve.

(29.) As an example, let us suppose that the constants y, λ , μ in the equation II. are connected by the relation,

LXII...
$$g = -S\lambda\mu$$
, whence LXIII... $S(V\lambda\rho . V\mu\rho) = 0$;

the cyclic normals are therefore in this case sides of the cone, and the two planes which connect them with any third side are mutually rectangular; so that the conic is now the locus of the vertex of a right-angled spherical triangle, of which the hypotenuse is given. And by applying either the formula LXI., L

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or the construction (28.) which it represents, we find that the trigonometric tangent of the arcual radius of the osculating small circle to such a conic, at either end of the given hypotenuse, is equal to half* the tangent of that hypotenuse itself.

(30.) It is obvious that every determination, of an osculating circle to a spherical curve, is at the same time the determination of what may be (and is) called an osculating right cone (or cone of revolution), to the cone which rests upon that curve, and has its vertex at the centre of the sphere. Applying this remark to the last example (29.), we arrive at the following theorem, which can however be otherwise deduced :--

If a cone be cut in a circle by a plane perpendicular to a side, the axis of the right cone which osculates to it along that side passes through the centre of the section.

395. When a given curve of double curvature is not a spherical curve, we may propose to investigate the spheric surface which approaches to it most closely, at any assigned point. An osculating circle has been defined (389) to be the *limit* of a circle, which touches a given curve, or its tangent PT, at a given point P, and cuts the same curve at a near point Q; while the tangent PT itself had been regarded (100) as the limit of a rectilinear secant, or as the ultimate position of the small chord PQ. It is natural then to define the osculating sphere, as being the limit of a spheric surface, which passes through the osculating circle, at a given point P of a curve, and also cuts that curve in a point Q, which is supposed to approach indefinitely to P, and ultimately to coincide with it. Accordingly we shall find that this definition conducts by quaternions to formulæ sufficiently simple; and that their geometrical interpretations are consistent with known results : for example, the centre of spherical curvature, or the centre of the osculating sphere, will thus be shown to be, as usual, the point in which the polar axis (391, (5.)) touches the cusp-edge of the polar developable (391, (6.)). It will also be seen, that whereas in general, if R be a point in the normal plane (370, (8.)) to a given curve at P, we can only say that the difference of distances, $\overline{RQ} - \overline{RP}$, is small of an order higher than the first, if the chord PR be small of the first order; and whereas, even if n be on the polar axis (391, (4.)), we can only say generally that this difference of distances is small, of an order higher than the second; yet, if R be placed at the centre s of spherical curvature, the difference $\overline{sq} - \overline{sp}$ is small,

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^{*} This may also be inferred by limits from the formulæ (11.); in which r and α were used, provisionally, to denote a certain spherical *arc* and *angle*.

of an order higher than the third: so that the distance of a near point Q, from the osculating sphere at the given point P, is generally small of the fourth order, the chord being still small of the first.

(1.) Operating with $S.\lambda$, where λ is an arbitrary line, on the vector equation 392, ∇ . of the osculating circle, we obtain the scalar equation of a sphere through that circle under the form,

I...
$$0 = 2S \frac{\lambda \rho'}{\omega - \rho} + S \frac{\lambda \rho''}{\rho'};$$

which may however, by 393, (7.), be brought to this other form, better suited to our present purpose,

II...
$$(\omega - \kappa)^2 = (\rho - \kappa)^2 + 2c \mathrm{S} \rho'' \rho' (\omega - \rho);$$

c being any scalar constant, while κ is still the vector of the centre κ of the circle: and the vector σ of the centre s of the sphere is given by the formula,

III...
$$\sigma = \kappa + c \nabla \rho'' \rho',$$

which evidently expresses that this last centre is on the polar axis.

(2.) To express now that this sphere cuts the curve in a near point q, we are to substitute for ω the expression,

IV...
$$\omega = \rho_t = \rho + t\rho' + \frac{1}{2}t^2\rho'' + \frac{1}{6}t^3u_t\rho''', \text{ with } u_0 = 1;$$

but κ has been seen (in 391) to satisfy the three equations,

$$\nabla \ldots 0 = \mathbf{S}\rho'(\kappa - \rho), \quad 0 = \mathbf{S}\rho''(\kappa - \rho) - \rho'^2, \quad 0 = \mathbf{S}\rho''\rho'(\kappa - \rho);$$

reducing then, dividing by $\frac{1}{3}t^3$, and passing to the limit, we find for the osculating sphere the condition,

$$\mathbf{VI.} \ldots \mathbf{S} \rho^{\prime\prime\prime} (\rho - \kappa) + 3 \mathbf{S} \rho^{\prime} \rho^{\prime\prime} = c \mathbf{S} \rho^{\prime\prime\prime} \rho^{\prime\prime} \rho^{\prime};$$

so that finally the vector σ satisfies the three scalar equations,

VII... $0 = S\rho'(\sigma - \rho), \quad 0 = S\rho''(\sigma - \rho) - \rho'^2, \quad 0 = S\rho'''(\sigma - \rho) - 3S\rho'\rho'',$

by which it is completely determined, and of which the two last are seen to be the successive derivatives of the first, while that first is the equation of the normal plane: whence the *centre* s of this *sphere* is (by the sub-arts. to 386,

L 2

comp. 391, (6.)) the point where the *polar axis* KS *touches the cusp-edge* of the polar developable.*

(3.) Differentials may be substituted for derivatives in the equations ∇ II., which may also be thus written (comp. 391, (4.)),

VIII...
$$0 = dT(\rho - \sigma), \quad 0 = d^2T(\rho - \sigma), \quad 0 = d^3T(\rho - \sigma), \quad \text{if } d\sigma = 0;$$

the distance of a near point q of the given curve from the osculating sphere is therefore small (as above said), of an order higher than the third, if the chord Pq be small of the first order.

(4.) The two first equations VII., combined with V., give also

IX...
$$0 = S\rho'(\sigma - \kappa), \quad 0 = S\rho''(\sigma - \kappa), \quad 0 = S(\kappa - \rho)(\sigma - \kappa);$$

which express that the line ks is perpendicular to the osculating plane and absolute normal at P, as it ought to be, because it is part of the polar axis.

(5.) Conceiving the three points P, K, s, or their vectors ρ , κ , σ , to vary together, the equations V. and VII., combined with their own derivatives, give among other results the following:

X...
$$0 = S_{\kappa} \rho' = S \sigma' \rho' = S \sigma' \rho'' = S \sigma' (\kappa - \rho) = S \sigma'' \rho';$$

of which the geometrical interpretations are easily perceived.

(6.) Another easy combination is the following,

XI...
$$0 = S\kappa'(\sigma + \rho - 2\kappa),$$

as appears by derivating the last equation IX., with attention to other relations; but $2\kappa - \rho$ is the vector of the extremity, say M, of the *diameter* of

$$\frac{x+y+z}{\omega-\rho}=\frac{x}{\rho_1-\rho}+\frac{y}{\rho_2-\rho}+\frac{z}{\rho_3-\rho},$$

because the coinitial vectors reciprocal to four coinitial chords of a sphere are termino-complanar.

$$\rho_1 = \rho + t_1 \rho' + \frac{1}{2} t_1^2 \rho'' + \frac{1}{6} t_1^3 u_{t1} \rho''', \&c.,$$

and the relation becomes

Let

$$(x+y+z) \frac{\rho'}{\omega-\rho} = \frac{xt_1^{-1}}{1+\frac{1}{2}t_1\rho''\rho'^{-1}+\frac{1}{6}t_1^{2}u_{t1}\rho'''\rho'^{-1}} + \&c.$$

^{* [}The equation of the osculating sphere may be obtained in a manner analogous to the instructive method of 392, (3.), p. 59. Let ρ , ρ_1 , ρ_2 , and ρ_3 be the vectors to any four points on the curve, and let ω be the vector to a variable point on the sphere which passes through these four points, then for certain scalars x, y, and z,

ART. 395. CONSTRUCTION FOR CENTRE OF SPHERE.

the osculating circle, drawn from the given point r: we have therefore this construction :---

On the tangent KK' to the locus of the centre of the osculating circle, let fall a perpendicular from the extremity \mathbf{M} of the diameter drawn from the given point \mathbf{P} ; this perpendicular prolonged will intersect the polar axis, in the centre s of the osculating sphere to the given curve at P.

(7.) In general, the three scalar equations VII. conduct to the vector expression,

XII...
$$\sigma = \rho + \frac{3\nabla \rho' \rho'' S \rho' \rho'' + \rho'^2 \nabla \rho''' \rho'}{S \rho' \rho'' \rho'''};$$

or with differentials,

XIII...
$$\sigma = \rho + \frac{3 \nabla d\rho d^2 \rho S d\rho d^2 \rho + d\rho^2 \nabla d^3 \rho d\rho}{S d\rho d^2 \rho d^3 \rho};$$

the scalar variable being still left arbitrary.

(8.) And if, as an example, we introduce the values for the helix,

XIV...
$$\rho = cta + a^t\beta$$
, $\rho' = ca + \frac{\pi}{2}a^{t+1}\beta$, $\rho'' = -\left(\frac{\pi}{2}\right)^2 a^t\beta$,
 $\rho''' = -\left(\frac{\pi}{2}\right)^3 a^{t+1}\beta$,

whereof the three first occurred before, we find after some slight reductions the expression, in which a denotes again the constant inclination of the curve to the axis of the cylinder,

XV...
$$\sigma = \rho - a^t \beta \operatorname{coseo}^2 a = cta - a^t \beta \operatorname{cot}^2 a;$$

but this is precisely what we found for κ , in 389, VIII.; for the helix, then. the two centres, K and s, of absolute and spherical curvature, coincide.

Ultimately, when the four points on the curve approach indefinitely, this reduces to

$$\begin{aligned} (x+y+z)\frac{\rho'}{\omega-\rho} &= \frac{xt_1^{-1}}{1+\frac{1}{2}t_1\rho''\rho'^{-1}+\frac{1}{8}t_1^{2}\rho'''\rho'^{-1}} + \&c. \\ &= xt_1^{-1}(1-\frac{1}{2}t_1\rho''\rho'^{-1}+\frac{1}{8}t_1^{2}(\rho''\rho'^{-1})^2 - \frac{1}{6}t_1^{2}\rho'''\rho'^{-1} + \&c.) + \&c. \\ &= (xt_1^{-1}+yt_2^{-1}+zt_3^{-1}) - \frac{1}{2}(x+y+z)\rho''\rho'^{-1} \\ &+ \frac{1}{6}(xt_1+yt_2+zt_3)(\frac{1}{2}(\rho''\rho'^{-1})^2 - z\rho'''\rho'^{-1}) + \&c. \end{aligned}$$

Taking the vector part,

hence

$$(x + y + z) \nabla \left(\frac{\rho'}{\omega - \rho} - \frac{1}{2} \rho'' \rho'^{-1} \right) = \frac{1}{6} (xt_1 + yt_2 + zt_3) (\nabla \rho'' \rho'^{-1} S \rho'' \rho'^{-1} - 3 \nabla \rho'' \rho'^{-1});$$

$$S \left(\frac{\rho'}{\omega - \rho} - \frac{1}{2} \rho'' \rho'^{-1} \right) (\rho'' S \rho'' \rho'^{-1} - 3 \rho''') = 0,$$

and

which is the equation required.]

ELEMENTS OF QUATERNIONS.

[III. m. § 6.

(9.) This known result is a consequence, and may serve as an illustration, of the general construction (6.); because it is easy to infer, from what was shown in 389, (3.), respecting the locus of the centre κ of the osculating circle to the helix, as being another helix on a co-axal cylinder, that the tangent $\kappa\kappa'$ to this locus is perpendicular to the radius of curvature κp , while the same tangent ($\kappa\kappa'$ or κ') is always perpendicular (X.) to the tangent (pp' or ρ') to the curve; $\kappa\kappa'$ is therefore here at right angles to the osculating plane of the given helix, or coincides with its polar axis: so that the perpendicular on it from the extremity \mathbf{M} of the diameter of curvature falls at the point κ itself, with which consequently the point s in the present case coincides, as found by calculation in (8.).

(10.) In general, if we introduce the expressions 376, $\nabla I.$, or the following,

XVI...
$$\rho' = s' D_s \rho$$
, $\rho'' = s'^2 D_s^2 \rho + s'' D_s \rho$, $\rho''' = s'^3 D_s^3 \rho + 3s' s'' D_s^2 \rho + s''' D_s \rho$,

in which s denotes the *arc* of the curve, but the accents still indicate derivations with respect to an *arbitrary* scalar t; and if we observe (comp. 380, (12.)) that the relations,

XVII. . .
$$D_{s}\rho^{2} = -1$$
, S. $D_{s}\rho D_{s}^{2}\rho = 0$, S. $D_{s}\rho D_{s}^{3}\rho + D_{s}^{2}\rho^{2} = 0$,

in which $D_s\rho^2$ and $D_s^2\rho^2$ denote the squares of $D_s\rho$ and $D_s^2\rho$, and $S. D_s\rho D_s^2\rho$ denotes $S(D_s\rho . D_s^2\rho)$, &c., exist independently of the *form* of the curve; we find that s'' and s''' disappear from the numerator and denominator of the expression XII. for $\sigma - \rho$, and that they have s'⁶ for a common factor: setting aside which, we have thus the simpler formulæ,

XVIII. ...
$$\sigma - \rho = \frac{\nabla . D_s \rho D_s^3 \rho}{S . D_s \rho D_s^2 \rho D_s^3 \rho} = \frac{D_s . D_s \rho D_s^2 \rho}{S . D_s \rho D_s^2 \rho D_s^3 \rho}$$

And accordingly the three scalar equations VII., which determine the centre of the osculating sphere, may now be written thus,

XIX...
$$S(\sigma - \rho)D_s\rho = 0$$
, $S(\sigma - \rho)D_s^2\rho + 1 = 0$, $S(\sigma - \rho)D_s^3\rho = 0$.

(11.) Conversely, when we have any formula involving thus the successive derivatives of the vector ρ taken with respect to the *arc*, *s*, we can always and easily *generalize* the *expression*, and introduce an *arbitrary* variable *t*, by inverting the equations XVI.; or by writing (comp. 390, VIII.),

XX...
$$D_{s}\rho = s'^{-1}\rho', \quad D_{s}^{2}\rho = s'^{-1}(s'^{-1}\rho')' = s'^{-2}\rho'' - s'^{-3}s''\rho', \&c.$$

ABT. 395.] COEFFICIENT OF DEVIATION FROM SPHERE.

(12.) It may happen (comp. 379, (2.)) that the independent variable t is only *proportional* to s, without being *equal* thereto; but as we have the general relation,

XXI...
$$D_t^n \rho = s'^n D_s^n \rho$$
, if $s' = D_t s = T \rho' = \text{const.}$,

it is nearly or quite as easy to effect the transformations (10.) and (11.) in the case here supposed, or to pass from t to s and reciprocally, as if we had s' = 1.

(13.) If the vector σ be treated as *constant* in the derivations, or if we consider for a moment the *centre* s of the *sphere* as a *fixed point*, and attend only to the *variations of distance* of a point on the *curve* from *it*, then (remembering that $T(\rho - \sigma)^2 = -(\rho - \sigma)^2$) we not only easily put (comp. VIII.) the three equations XIX. under the forms,

XXII...
$$0 = D_s T(\rho - \sigma) = D_s^2 T(\rho - \sigma) = D_s^3 T(\rho - \sigma),$$

but also obtain by XVII. this fourth equation,

XXIII. . .
$$T(\rho - \sigma) D_s^4 T(\rho - \sigma) = S \cdot (\sigma - \rho) D_s^4 \rho + D_s^2 \rho^2$$
.

(14.) If then we write, for abridgment,

XXIV...
$$r = T(\kappa - \rho) = T D_s^2 \rho^{-1} = radius of osculating circle;$$

XXV. . . $R = T(\sigma - \rho) = radius of osculating sphere;$

XXVI. . .
$$S = \frac{S(\sigma - \rho)D_s^4\rho}{-D_s^2\rho^2} = \frac{S \cdot D_s\rho^3D_s^3\rho D_s^4\rho}{S \cdot D_s\rho D_s^2\rho^3 D_s^3\rho},$$

we see that this scalar, S, must be constantly equal to unity, for every spherical curve; but that for a curve which is non-spherical, the distance \overline{sq} of a near point q, from the centre s of the osculating sphere at P, is generally given by an expression of the form,

XXVII...
$$\overline{sq} = R + \frac{(S-1)u_s s^4}{24r^2 R}$$
, with $u_0 = 1$;

so that, at least for near points Q, on each side of the given point P, the curve lies without or within the sphere which osculates at that given point, according as the scalar, S, determined as above, is greater or less than unity. (15.) In the case (12.), the formula XXVI. may be thus written,

XXVIII. . .
$$S = \frac{S \cdot \rho^{\prime 3} \rho^{\prime \prime \prime} \rho^{\prime \nu}}{S \cdot \rho^{\prime } \rho^{\prime \prime 3} \rho^{\prime \prime \prime}};$$

whence, by carrying the derivations one step farther than in (8.), we find for the *helix*,

XXIX...
$$S = \operatorname{cosec}^{2} a > 1$$
, or XXIX'... $S - 1 = \operatorname{cot}^{2} a > 0$;

and accordingly it is easy to prove that *this* curve lies *wholly without* its osculating sphere, except at the point of osculation.

(16.) In general, the scalar S - 1, which vanishes (14.) for all spherical curves, and which enters as a coefficient into the expression XXVII. for the deviation $\overline{sq} - \overline{sp}$ of a near point of any other curve from its own osculating sphere, may be called the Coefficient of Non-Sphericity; and if qr be the perpendicular from that near point q on the tangent pr to the curve at the given point P, we have then this limiting equation, by which the value of that coefficient may be expressed,

XXX...
$$S-1 = \lim_{n \to \infty} 3\left(\frac{\overline{SQ^2} - \overline{SP}^2}{\overline{QT}^2}\right)$$
.

(17.) Besides the forms XVIII., other transformations of the expressions XII. XIII. for the vector σ of the centre of an osculating sphere might be assigned; but it seems sufficient here to suggest that some useful practice may be had, in proving that those expressions for σ reduce themselves generally to zero, when the condition,

$$XXXI...T\rho = const.$$

is satisfied.

(18.) It may just be remarked, that as r^{-1} is often called (comp. 389, (4.)) the *absolute curvature*, or simply the curvature, of the curve in space which is considered, so R^{-1} is sometimes called the *spherical curvature* of that curve: while r and R are called the *radii*^{*} of those two curvatures respectively.

^{*} We shall soon have occasion to consider another scalar radius, which we propose to denote by the small roman letter r, of what is not uncommonly called the torsion, or the second curvature, of the same curve in space.

ARTS. 395, 396.] EMANANT LINES AND PLANES.

396. When the arc (s) of the curve is made the independent variable, the calculations (as we have seen) become considerably simplified, while no essential generality is lost, because the transformations requisite for the introduction of an arbitrary scalar variable (t) follow a simple and uniform law (395, (11.), &c.). Adopting then the expression (comp. 395, IV.),

I. . . $\rho_s = \rho + s\tau + \frac{1}{2}s^2\tau' + \frac{1}{6}s^3u_s\tau''$, with $u_0 = 1$,

in which

II... $\tau = D_s \rho$, $\tau' = D_s^2 \rho$, $\tau'' = D_s^3 \rho$,

and therefore

III. . .
$$\tau^2 + 1 = 0$$
, $S\tau\tau' = 0$, $S\tau\tau'' + \tau'^2 = 0$,

we shall proceed to deduce some other affections of the curve, besides its spherical curvature (395, (18.)), which do not involve the consideration of the fourth power of the arc (or chord). In particular, we shall determine expressions for that known Second Curvature (or torsion), which depends on the change of the osculating plane, and is measured by the ultimate ratio of that change, expressed as an angle, to the arc of the curve itself; and shall assign the quaternion equations of the known Rectifying Plane, and Rectifying Line, which are respectively the tangent plane, and the generating line, of that known Rectifying Developable, whereon the proposed curve is a geodetic (382): so that it would become a right line, by the unfolding of this last But first it may be well to express, in this new surface into a plane. notation, the principal affections or properties of the curve, which depend only on the three first terms of the expansion I., or on the three initial vectors ρ , τ , τ' , or rather on the *two last* of these; and which *include*, as we shall see, the rectifying plane, but not the rectifying line : nor what has been called above the second* curvature.

(1.) Using then first, instead of I., this less expanded but still rigorous expression (comp. 376, I.),

IV. . . $\rho_s = \rho + s\tau + \frac{1}{2}s^2u_s\tau'$, with $u_0 = 1$,

and with the relations II. and III., we have at once the following system of

^{*} In a Note to a very able and interesting Memoir, "Sur les lignes courbes non planes" (referred to by Dr. Salmon in the Note to page 277 of his already cited Treatise, and published in Cahier XXX. of the Journal de l'École Polytechnique), M. de Saint-Venant brings forward several objections to the use of this appellation, and also to the phrases torsion, flexion, &c., instead of which he proposes to introduce the new name, "cambrure": but the expression "second curvature" may serve us for the present, as being at least not unusual, and appearing to be sufficiently suggestive.

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three rectangular lines, which are conceived to be all drawn from the given point **P** of the curve :

V. . . τ = unit tangent; VI. . . τ' = vector of curvature (389, (4)); and

VII. . .
$$\nu = \tau \tau' = -\tau' \tau = \tau' \tau^{-1} = binormal (comp. 379, (4.))$$

 τ being a line drawn in the direction of a conceived motion along the curve, in virtue of which the arc (s) increases; while τ' is directed towards the centre of curvature, or of the osculating circle, of which centre κ the vector is now,

VIII. . . OK =
$$\kappa = \rho - \tau'^{-1} = \rho + r^2 \tau' = \rho + r U \tau'$$

if

IX... $r^{-1} = \mathbf{T}\tau' = curvature$ at P, or IX'... $r = \mathbf{T}\tau'^{-1} = radius$ of curvature;

and the third line ν (which is normal at P to the surface of tangents to the curve) has the same length $(T\nu = r^{-1})$ as τ' , and is directed so that the rotation round it from τ to τ' is positive.

(2.) At the same time, we have evidently a system of three rectangular vector units from the same point \mathbf{P} , which may be called respectively the tangent unit, the normal unit, and the binormal unit, namely the three lines,

X...
$$U\tau = \tau$$
, $U\tau' = r\tau'$, $U\nu = r\tau\tau'$;

the normal unit being thus directed (like τ') towards the centre of curvature.

(3.) The vector equation (comp. 392, (2.)) of the circle of curvature takes now the form,

XI...
$$\nabla_{r}\frac{2\tau}{\omega-\rho} = -\nu;$$

with the verification that it is satisfied by the value,

XII...
$$\omega = \mu = 2\kappa - \rho = \rho - 2\tau'^{-1}$$
,

in which μ (comp. 395, (6.)) is the vector on of the extremity of the *diameter* of curvature PM.

(4.) The normal plane, the rectifying plane, and the osculating plane, to the curve at the given point, form a rectangular system of planes (comp. 379, (5.)), perpendicular respectively to the three lines (1.); so that their scalar equations are, in the present notation,

XIII...
$$Sr(\omega - \rho) = 0$$
; XIV... $Sr'(\omega - \rho) = 0$; XV... $S\nu(\omega - \rho) = 0$;

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[III. III. § 6.

ART. 396.]

by pairing which we can represent the tangent, normal, and binormal to the curve, regarded as indefinite right lines; or by the three vector equations,

XVI...
$$\nabla \tau(\omega - \rho) = 0$$
; **XVII.**.. $\nabla \tau'(\omega - \rho) = 0$; **XVIII.**.. $\nabla \nu(\omega - \rho) = 0$.

(5.) In general, if the two vector equations,

XIX...
$$\nabla \eta(\omega - \rho) = 0$$
, and XIX'... $\nabla \eta_s(\omega_s - \rho_s) = 0$,

represent two right lines, PH and P_sH_s, which are conceived to emanate according to any given law from any given curve in space, the identical formula,*

XX. . .
$$\rho_s - \rho + \nabla \left(\nabla \eta \eta_s \cdot \nabla \frac{\rho_s - \rho}{\nabla \eta \eta_s} \right) = \frac{S \eta \eta_s (\rho_s - \rho)}{\nabla \eta \eta_s},$$

shows that the common perpendicular to these two emanants, which as a vector is represented by either member of this formula XX., intersects the two lines in the two points of which the vectors are,

XXI. . .
$$\omega = \rho + \eta S \frac{(\rho_s - \rho)\eta_s}{V_{\eta\eta_s}};$$
 XXI'. . . $\omega_s = \rho_s + \eta_s S \frac{(\rho_s - \rho)\eta}{V_{\eta\eta_s}}.$

(6.) In general also, the passage of a right line from any one given position in space to any other may be conceived to be accomplished by a sort of screw motion, with the common perpendicular for the axis of the screw, and with two proportional velocities, of translation along, and of rotation round that axis: the locus of the two given and of all the intermediate positions of the line (when thus interpolated) being a Screw Surface, such as that of which the vector equation was assigned in 314, (11.), and was used in 372, (4.).

(7.) Again, for any quaternion, q, we have (by 316, XX. and XXIII.[†]) the two equations,

XXII... $Uq = \angle q \cdot UVq$, XXII'... $VUq = \sin \angle q \cdot UVq$;

comparing which we see that

XXIII... $VUq : IUq = sin \angle q : \angle q = (very nearly) 1,$

^{*} It is obvious that we have thus an easy quaternion solution of the problem, to draw a common perpendicular to any two right lines in space.

[†] Although the expression XXII'. for VUq is here deduced from 316, XXIII., yet it might have been introduced at a much earlier stage of these *Elements*; for instance, in connexion with the formula 204, XIX., namely $TVUq = sin \angle q$.

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if the angle of the quaternion be small; so that the logarithm and the vector of the versor of a small-angled quaternion are very nearly equal to each other, and we may write the following general approximate formula for such a versor:

XXIV...
$$Uq = (\varepsilon^{iUq} =) \varepsilon^{VUq}$$
, nearly, if $\angle q$ be small;

the error of this last formula being in fact small of the third order, if the angle be small of the first.

(8.) And thus or otherwise (comp. 334, XIII. and XV.), we may perceive that if the quaternion q have the form (comp. (5.)),

XXV...
$$q = \eta_s \eta^{-1}$$
, with **XXVI.**.. $\eta_s = \eta + s\eta' + \ldots$,

and if we write for abridgment,

XXVII...
$$\theta = V \frac{\eta'}{\eta}$$
, and XXVIII... $h = S \frac{\eta'}{\eta}$,

we shall then have nearly, if s be small, the expressions,

XXIX...
$$Uq = U \frac{\eta_s}{\eta} = \epsilon^{s\theta}$$
, and XXX... $Tq = T \frac{\eta_s}{\eta} = 1 + sh;$

or, neglecting s^2 ,

XXXI...
$$\eta_s = (1 + sh) \epsilon^{s\theta} \eta = \epsilon^{s\theta} \eta + sh\eta$$
,

in which last binomial, the *first* (or *exponential*) term alone influences the *direction* of the *near emanant line* (5.).

(9.) At the same time, by supposing s to tend to 0, the formula XXI. gives, as a limit,

XXXII... OH =
$$\omega_0 = \rho + \eta S \frac{\tau \eta}{V \eta \eta'} = \rho - \eta S \frac{\tau}{\theta \eta}$$
,

for the vector of the point, say H, on the given emanant PH, in which that given line is ultimately intersected by the common perpendicular (5.), or by the axis of the screw rotation (6.); but the direction of that axis is represented by the versor $U\theta$, and the angular velocity of that rotation is represented by the tensor $T\theta$, if the velocity of motion (1.) along the given curve be taken as unity: we may therefore say that the vector θ itself, or the factor which multiplies the arc, s, in the exponential term XXXI., if set off from the point

ABT. 396.] VECTOR OF ROTATION, AXIS OF DISPLACEMENT.

H determined by XXXII., is the Vector of Rotation of the Emanant, whatever the law (5.) of the emanation may be.

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(10.) And as regards the screw translation (6.), its linear velocity is in like manner represented, in length and in direction, by the following expression (obtained by limits from XX.),

XXXIII. . . $\iota = \theta S \frac{\tau}{\theta}$ (set off from H) = Vector of Translation of Emanant, = projection of unit-tangent on screw-axis (or of τ on θ).

And the indefinite right line through the point H, of which this line ι is a part, may be called the Axis of Displacement of the Emanant.

(11.) It is easy in this manner to assign what may be called the Osculating Screw Surface to the (generally gauche) Surface of Emanants, or indeed to any proposed skew surface; namely, the screw surface which has the given emanant (or other) line for one of its generatrices, and touches the skew surface in the whole extent of that right line.

(12.) It is however more important here to observe, that in the case when the surface of emanants is developable, the vector ι of translation vanishes; and that conversely this vector ι cannot be constantly zero, if that surface be undevelopable. The Condition of Developability of the Surface of Emanants is therefore expressed by the equation,

XXXIV... $\iota = 0$, or $S\tau\theta = 0$, or XXXIV'... $S\eta\eta'\tau = 0$;

and accordingly this condition is satisfied (as was to be expected) when $\eta = \tau$, that is, for the surface of tangents.

(13.) In the same case, of $\eta = \text{ or } \| \tau$, the vector $\boldsymbol{\theta}$ of rotation becomes equal (by XXVII. and VII.) to the binormal ν ; and the expression XXXII., for the vector ω_0 of the foot H of the axis reduces itself to ρ ; and thus we might be led to see (what indeed is otherwise evident), that the passage from a given tangent to a near one may be approximately made, by a rotation round the binormal, through the small angle, $sT\nu = sr^{-1} = arc$ divided by radius of curvature.

(14.) Instead of emanating *lines*, we may consider a system of *emanating* planes, which are respectively perpendicular to those lines, and pass through the same points of the given curve. It may be sufficient here to remark, that the passage from one to another of two such near emanant planes, represented by the equations,

$$\mathbf{XXXV}\dots\mathbf{S}\eta(\boldsymbol{\omega}-\boldsymbol{\rho})=0, \qquad \mathbf{XXXV}'\dots\mathbf{S}\eta_{s}(\boldsymbol{\omega}-\boldsymbol{\rho})=0,$$

[III. III. §6.

may be conceived to be made by a rotation through an angle = $sT\theta$, round the right line,

XXXVI...
$$S\eta(\omega - \rho) = 0$$
, $S\eta'(\omega - \rho) - S\eta\tau = 0$,

or

$$XXXVI'...V\theta(\omega-\rho)+\eta^{-1}S\eta\tau=0,$$

in which the plane XXXV. touches its developable envelope, and which is parallel to the recent vector θ , or to the vector of rotation (9.) of the emanant line; so that if an equal vector be set off on this new line XXXVI., it may be said to be the Vector Axis of Rotation of the Emanant Plane.

(15.) For example, if we again make $\eta = \tau$, so that the equation XXXV. represents now the *normal plane* to the curve, we are led to combine the equation XIII. of that plane with its *derived* equation, and so to form the system of the *two* scalar equations,

XXXVII...
$$S\tau(\omega - \rho) = 0$$
, $S\tau'(\omega - \rho) + 1 = 0$,

whereof the second represents a plane *parallel* to the *rectifying plane* XIV., and *drawn through the centre of curvature* VIII.; and which jointly represent the *polar axis* (391, (5.)), considered as an *indefinite* right line, which is represented otherwise by the *one* vector equation,

XXXVIII...
$$\nabla v(\omega - \kappa) = 0$$
, or XXXVIII'... $\nabla v(\omega - \rho) = -\tau$.

(16.) And if, on this indefinite line, we set off a portion equal to the binormal ν , such portion (which may conveniently be measured from the centre κ) may be said, by (14.), to be the Vector Axis of Rotation of the Normal Plane; or briefly, the Polar Axis, considered as representing not only the direction but also the velocity of that rotation, which velocity = $T\nu = r^{-1}$ = the curvature (IX.) of the given curve : while another portion = $U\nu$ = the binormal unit (2.), set off on the same axis from the same centre of curvature, may be called the Polar Unit.

(17.) This suggests a new way of representing the osculating circle by a vector equation (comp. (3.), and 316), as follows:

XXXIX...
$$\omega_s = \kappa + \epsilon^{s\nu}(\rho - \kappa) = \rho + (\epsilon^{s\nu} - 1)\tau^{\prime-1}$$

= $\rho + s\tau + (\epsilon^{s\nu} - 1 - s\nu)\tau^{\prime-1}$
= $\rho + s\tau + \frac{1}{2}s^2\tau' + (\epsilon^{s\nu} - 1 - s\nu - \frac{1}{2}s^2\nu^2)\tau^{\prime-1};$

which agrees, as we see, with the expression I. or IV., if s^3 be neglected; and of which, when the expansion is continued, the *next term* is,

XL...
$$\frac{1}{6}s^3\nu^3\tau'^{-1} = \frac{1}{6}s^3\nu\tau' = -\frac{s^3\tau}{6r^2}$$
.

(18.) The complete expansion of the exponential form XXXIX., for the variable vector of the osculating circle, may be briefly summed up in the following trigonometric (but vector) expression:

XLI...
$$\omega_s = \kappa + \left(\cos\frac{s}{r} + U\nu \cdot \sin\frac{s}{r}\right)(\rho - \kappa),$$

in which,

XLII. . . $\rho - \kappa = -r^2 \tau'$, and $U_{\nu} . (\rho - \kappa) = r_{\nu} \tau'^{-1} = r \tau$;

so that we may also write, neglecting no power of s,

XLIII. . .
$$\omega_s = \rho + i\tau \sin \frac{s}{r} + i^2 \tau' \operatorname{vers} \frac{s}{r};$$

and if this be subtracted from the full expression for the vector ρ_s , the remainder may be called the deviation of the given curve in space, from its own circle of curvature: which deviation, as we already see, is small of the third order, and will soon be decomposed into its two principal parts, or terms, of that order, in the directions of the normal and the binormal respectively.

(19.) Meantime we may remark, that if we only neglect terms of the *fourth order*, the expansion I. gives, by III. and IX., for the *length* of a *small chord* PP_s, the formula:

XLIV...
$$\overline{PP}_{s} = T(\rho_{s} - \rho) = T(s\tau + \frac{1}{2}s^{2}\tau' + \frac{1}{6}s^{3}\tau'')$$

$$= /\{-(s\tau + \frac{1}{2}s^{2}\tau' + \frac{1}{6}s^{3}\tau'')^{2}\}$$

$$= \sqrt{\{s^{2} + s^{4}\tau'^{2}(\frac{1}{3} - \frac{1}{4})\}}$$

$$= \sqrt{\{s^{2} - \frac{s^{4}}{12r^{2}}\}} = s - \frac{s^{3}}{24r^{2}} = 2r \sin \frac{s}{2r}$$

ĵ

this length then is the same (to this degree of approximation), as that of the chord of an equally long arc of the osculating circle: and although the chord of even a small arc of a curve is always shorter than that arc itself, yet we see

that the difference is generally a small quantity of the third* order, if the arc be small of the first.

397. Resuming now the expression 396, I., but suppressing here the coefficient u_s , of which the limit is unity, and therefore writing simply,

I. . .
$$\rho_s = \rho + s\tau + \frac{1}{2}s^2\tau' + \frac{1}{6}s^3\tau'',$$

with the relations,

II...
$$\tau^2 = -1$$
, $S\tau\tau' = 0$, $S\tau\tau'' = -\tau'^2 = r^{-2}$, $S\tau'\tau'' = r^{-3}r'$,

if s = arc, and $r^{-1} = Tr' = curvature$, \dagger as before, or r = radius of curvature (> 0), while $r' = D_s r$; and introducing the new scalar,

III...
$$\mathbf{r}^{-1} = \mathbf{S} \frac{\tau''}{\tau \tau'} = \tau^{-1} \nabla \frac{\nu'}{\nu} = Second + Curvature,$$

with $\nu = \tau \tau' = binormal$, or the new vector,

IV...
$$\mathbf{r}^{-1}\boldsymbol{\tau} = \boldsymbol{\tau} \mathbf{S} \frac{\boldsymbol{\tau}^{\prime\prime}}{\boldsymbol{\tau}\boldsymbol{\tau}^{\prime}} = \mathbf{V} \frac{\boldsymbol{\nu}^{\prime}}{\boldsymbol{\nu}} = Vector \ of \ Second \ Curvature,$$

supposed to be set off tangentially from the given point P of the curve, or finally this other new scalar (> or < 0),

V...
$$\mathbf{r} = \left(\mathbf{S} \frac{\boldsymbol{\tau}^{\prime\prime}}{\boldsymbol{\tau}\boldsymbol{\tau}^{\prime}}\right)^{-1} = Radius of Second Curvature,$$

which gives the expression,

VI...
$$\tau'' = -r^{-2}\tau - r^{-1}r'\tau' + r^{-1}\tau\tau' = -r^{-2}U\tau + (r^{-1})'U\tau' + (rr)^{-1}U\nu;$$

we proceed to deduce some of the chief affections of a curve in space, which depend on the *third power* of the *arc* or chord. In doing this, although everything *new* can be *ultimately* reduced to a dependence on the *two new* scalars, r' and r, or on the one new vector τ'' , or even on $\nu' = \nabla \tau \tau''$, yet some

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^{*} This ought to have been expressly stated in the reasoning of 383, (5.), for which it was not sufficient to observe that the *arc* and *chord tend* to bear to *each other* a *ratio of equality*, without showing (or at least mentioning) that their *difference tends* to *vanish*, *even* as *compared* with a line which is ultimately of the same order as the *square* of either.

[†] Whenever this word *curvature* is thus used, without any qualifying adjective, it is always to be understood as denoting the *absolute* (or *first*) curvature of the curve in space.

[‡] Compare the Note to page 81.

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auxiliary symbols will be found useful, and almost necessary. Retaining then the symbols ν , κ , σ , R, as well as τ , τ' , r, and therefore writing as before (comp. 396, VIII.),

VII. . . OK =
$$\kappa = \rho - \tau'^{-1} = \rho + r \mathbf{U} \tau' = \rho + r^2 \tau'$$
,

VIII. . .
$$(\rho - \kappa)^{-1} = r^{-1} \mathbf{U}(\kappa - \rho) = \tau' = \mathbf{D}_s^2 \rho = Vector \ of \ Curvature,$$

we may now write also, by 395, XVIII.,

IX... os =
$$\sigma = \rho - \frac{\nu'}{S\tau'\nu'} = \kappa + rr'r\nu = \kappa + r'rU\nu$$
,

and 2

X. : .
$$(\rho - \sigma)^{-1} = R^{-1}\mathbf{U}(\sigma - \rho) = \nu'^{-1}\mathbf{S}\tau'\nu' = Vector of Spherical Curvature,= projection of vector (τ') of curvature on radius (R) of osculating sphere;$$

because we have now, by VI.,

or

and

XI...
$$\nu' = (\tau \tau')' = \nabla \tau \tau'' = -\mathbf{r}^{-1} \tau' - r^{-1} r' \nu,$$

XI'...
$$(U_{\nu})' = (r_{\nu})' = -rr^{-1}r' = -r^{-1}Ur',$$

XII... $Sr'\nu' = -Srr'r'' = -r^{-1}r'^2 = r^{-2}r^{-1}.$

If then we denote by p and P the linear and angular elevations, of the centre s of the osculating sphere above the osculating plane, we shall have these two new auxiliary scalars, which are positive or negative together, according as the linear height ks has the direction of $+\nu$ or of $-\nu$:

XIII...
$$p = \frac{\sigma - \kappa}{U_{\nu}} = r'\mathbf{r}$$
; XIV... $P = \kappa \mathbf{rs} = \tan^{-1}\frac{p}{r} = \sin^{-1}\frac{p}{R} = \cos^{-1}\frac{r}{R}$;
while
XV... $R = T(\sigma - \rho) = \sqrt{(r^2 + p^2)} = \sqrt{(r^2 + r'^2 \mathbf{r}^2)}$;

the angle P being treated as generally acute. Another important line, and an accompanying *angle* of elevation, are given by the formulæ,

XVI...
$$\lambda = \nabla \frac{\tau''}{\tau'} = r^2 \nabla \tau' \tau'' = r^{-1} \tau + \tau \tau' = r^{-1} \nabla \tau + r^{-1} \nabla \nu$$

= $\nabla \nu' \nu^{-1} + \nu = Rectifying Vector (set off from given point P),$
= Vector of Second Curvature plus Binormal;

XVII. . .
$$H = \angle \frac{\lambda}{\tau} = \tan^{-1} \frac{\mathbf{r}}{r} = Elevation of Rectifying Line (> 0, < \pi),$$

= the angle (acute or obtuse, but here regarded as positive).

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which that known and important line (396) makes with the tangent to the curve; so that (by XIII., XIV.) these two auxiliary angles,* H and P, from which (instead of deducing them from r' and r) all the affections of the curve depending on s^3 can be deduced, are connected with each other and with r' by the relation,

XVIII...
$$\tan P = r' \tan H$$
.

Many other combinations of the symbols offer themselves easily, by the rules of the present calculus; for instance, the vector σ may be determined by the three scalar equations (comp. 395, XIX.),

XIX...
$$S\tau(\sigma - \rho) = 0$$
, $S\tau'(\sigma - \rho) = -1$, $S\tau''(\sigma - \rho) = 0$,

whence, by XVI.,

XX...
$$r^2 \tau'' = r^2 V(\nabla \tau' \tau''. (\sigma - \rho)) = V\lambda(\sigma - \rho),$$

a result which also follows from the expressions,

XXI...
$$\tau'' = \left(\nabla \frac{\tau''}{\tau'} + S \frac{\tau''}{\tau'}\right) \tau' = (\lambda - r^{-1}r') \tau',$$

and

XXII...
$$\sigma - \rho = r^2 \tau' + r p \nu = r U \tau' + p U \nu$$
,

because

XXIII... $rp \nabla \lambda \nu = -rpr^{-1}\tau' = -rr'\tau';$

we may therefore replace the formula I. for the vector of the curve by the following, which is true to the same order of approximation,[†]

XXIV...
$$\rho_s = \rho + s\tau + \frac{s^2}{2r^2}(\kappa - \rho) + \frac{s^3}{6r^2}\nabla\lambda(\sigma - \rho):$$

and may thus exhibit, even to the eye, the dependence of all affections connected with s^3 , on the *two new lines*, λ and $\sigma - \rho$, which were not required when s^3 was neglected, but can now be determined by the *two scalars* **r** and *p*

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^{*} The angle H appears to have been first considered by Lancret, in connexion with his theory of rectifying lines, planes, and surfaces: but the angle here called P was virtually included in the earlier results of Monge.

[†] As regards the homogeneity of such expressions, if we treat the four vectors ρ_s , ρ , κ , and σ , and the five scalars s, r, R, p, and r, as being each of the first dimension, we are then to regard the dimensions of τ , r', κ' , H, and P as being each zero; those of τ' , ν , and λ as each equal to -1; and that of either τ'' or ν' as being = -2.

ART. 397.] OSC. CONES, CYLINDER, HELIX, AND PARABOLA.

(or r and r', or H and P as before). The geometrical signification of the scalar p is evident from what precedes, namely, the height (KS) of the centre of the osculating sphere above that of the osculating circle, divided by the binormal unit $(\mathbf{U}_{\mathbf{v}})$; and as regards what has been called the radius r of second curvature $(\nabla$.), we shall see that this is in fact the geometrical radius of a second circle, which osculates, at the extremity of the tangential vector $r\tau$, to the principal normal section of the developable Surface of Tangents; and thereby determines an osculating oblique cone to that important surface, and also an osculating right cone* thereto, of which latter cone the semiangle is H, and the rectifying line λ is the axis of revolution: being also a side of an osculating right cylinder, on which is traced what is called the osculating helix. We shall assign the quaternion equations of these two cones, and of this cylinder, and helix; and shall show that although the helix has not generally complete contact of the third order with the given curve, yet it approaches more nearly to that curve (supposed to be of double curvature), than does the osculating circle. But an osculating parabola will also be assigned, namely, the parabola which osculates to the projection of the curve, on its own osculating plane: and it will be shown that this parabola represents or constructs one of the two principal and rectangular components (396, (18.)), of the deviation of the curve from its osculating circle, in a direction which is (ultimately) tangential to the osculating sphere, while the helix constructs the other component. An osculating right cone to the cone of chords, drawn from a given point of the curve, will also be assigned by quaternions : and will be shown to have in general a smaller acute semiangle C (or $\pi - C$), than the acute semiangle H (or $\pi - H$), of the osculating right cone (above mentioned) to the surface of tangents, or (as will be seen) to the cone of parallels to tangents (369, (6.), &c.): the relation between these two semiangles, of two osculating right cones, being rigorously expressed by the formula,

XXV... $\tan C = \frac{3}{4} \tan H$.

A new oblique cone of the second order will be assigned, which has contact of the same order with the cone of chords, as the second right cone (C), while the latter osculates to both of them; and also an osculating parabolic cylinder, which rests upon the osculating parabola, and is cut perpendicularly in that

^{*} These two osculating cones, oblique and right, to the surface of tangents, appear to have been first assigned, in the Memoir already cited, by M. de Saint Venant: the osculating (circular) helix, and the osculating (circular) cylinder, having been previously considered by M. Olivier.

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auxiliary curve by the osculating plane to the given curve. And the intersection of these two last surfaces of the second order (oblique cone and parabolic cylinder) will be found to consist partly of the binormal at the given point, and partly of a certain twisted cubic* (or gauche curve of the third degree), which latter curve has complete contact of the third order with the given curve in space. Constructions (comp. 395, (6.)) will be assigned, which will connect, more closely than before, the tangent to the locus of centres of curvature, with other properties or affections of that given curve. And finally we shall prove, by a very simple quaternion analysis, as a consequence of the formula XI'., the known theorem,† that when the ratio of the two curvatures is constant, the curve is a geodetic on a cylinder.

(1.) The scalar expression III., for the second curvature of a curve in space, as defined in 396, may be deduced from the formulæ (396, (5.), &c.) of the recent theory of emanants, which give,

XXVI...
$$\theta = \nabla \nu' \nu^{-1} = r^{-1} \tau$$
, $\omega_0 = \rho$, $\iota = \tau$, if $\eta = \nu$,

while the line of contact (396, (14.)), of the emanant plane with its envelope, coincides in position with the tangent to the curve; in passing, then, from the given point P to the near point \mathbf{F}_s , the binormal (ν) and the osculating plane ($\perp \nu$) have (nearly) revolved together, round that tangent (τ) as a common axis, through a small angle = $\mathbf{r}^{-1}s$, and therefore with a relocity = \mathbf{r}^{-1} , if this symbol have the value assigned by III., or by the following extended expression, in which the scalar variable (t) is arbitrary (comp. 395, (11.), &c.),

XXVII...
$$\mathbf{r}^{-1} = S \frac{\rho'''}{\nabla \rho' \rho''} = S \frac{\mathrm{d}^3 \rho}{\mathrm{Vd} \rho \mathrm{d}^2 \rho} = Second Curvature :$$

while the binormal has at the same time been translated (nearly), in a direction perpendicular to the tangent τ , through the small interval is = $s\tau$, which (in the present order of approximation) represents the small chord PP_s.

(2.) As an example, if we take this new form of the equation of the helix,

XXVIII... $\rho_t = b(at \cot a + \epsilon^{at}\beta)$, with $Ta = T\beta = 1$, and $Sa\beta = 0$,

^{*} This convenient appellation (of *twisted cubic*) has been proposed by Dr. Salmon, for a curve of the kind here considered: see pages 241, &c., of his already eited Treatise. The osculating twisted cubic will be considered somewhat later.

⁺ This theorem was established, on sufficient grounds, in the cited Memoir of M. de Saint Venant (page 26); but it has also been otherwise deduced by M. Serret, in the Additions to M. Liouville's Edition of Monge (Paris, 1850, page 561, &c.).

ABT. 397.] CONTACT OF THIRD ORDER, TWISTED CUBIC.

which gives the derived vectors,

XXIX... $\rho_t' = ba(\cot a + \epsilon^{at}\beta), \quad \rho_t'' = -b\epsilon^{at}\beta, \quad \rho_t''' = a\rho_t'',$

and this expression for the arc s (supposed to begin with t),

XXX...
$$s = s't$$
, where $s' = T\rho' = b \operatorname{cosec} a = \operatorname{const.}$,

we easily find (after a few reductions) the following values for the two curvatures:

XXXI. . . $r^{-1} = b^{-1} \sin^2 a$, $r^{-1} = b^{-1} \sin a \cos a$;

while the common centre (395), of the osculating circle and sphere, has now for its vector (comp. 389, (3.)),

XXXII...
$$\kappa = \sigma = \rho_t - b\epsilon^{at}\beta \operatorname{cosec}^a a = b \cot a(at - \epsilon^{at}\beta \cot a);$$

b being here the radius of the cylinder, but a denoting still the constant inclination of the tangent (ρ') to the axis (a).

(3.) The rectifying line (396), considered merely as to its position, being the line of contact of the rectifying plane (396, XIV.) with its own envelope, is represented by the equations,

XXXIII...
$$0 = S\tau'(\omega - \rho) = S\tau''(\omega - \rho)$$
, or XXXIII'... $0 = V\lambda(\omega - \rho)$,

with the signification XVI. of λ ; and accordingly, if we treat the rectifying planes as *emanants*, or change η to τ' , we find the value $\theta = \nabla \tau'' \tau'^{-1} = \lambda$, which shows also that in the passage from P to P_s the *rectifying plane turns* (nearly) round the rectifying line, through a small angle = sT λ , or with a velocity of rotation represented by the tensor,

XXXIV...
$$T\lambda = \sqrt{(r^{-2} + r^{-2})} = r^{-1} \operatorname{cosec} H = r^{-1} \operatorname{sec} H;$$

so that what we have called the *rectifying vector*, λ , coincides in fact (by the general theory of emanants) with the vector axis (396, (14.)) of this rotation of the rectifying plane: as the vector of second curvature ($r^{-1}\tau$) has been seen to be, in the same full sense (comp. (1.)), the vector axis of rotation of the osculating plane, when velocity, direction, and position are all taken into account.

(4.) When the derivative s' of the arc is only constant, without being

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equal to unity (comp. 395, (12.)), the expression XVI. may be put under this slightly more general form,

XXXV...
$$\lambda = \nabla \frac{\rho'''}{s'\rho''} = \nabla \frac{d^3\rho}{dsd^2\rho} = Rectifying Vector;$$

and accordingly for the *helix* (2.) we have thus the values,

XXXVI...
$$\lambda = as'^{-1} = ab^{-1} \sin a = ar^{-1} \operatorname{cosec} a$$
, $U\lambda = a$;

the rectifying line is therefore, for this curve, parallel to the axis, and coincides with the generating line of the cylinder, as is otherwise evident from geometry. The value, $T\lambda = b^{-1} \sin a$, of the velocity of rotation of the rectifying plane, which is here the tangent plane to the cylinder, when compared with a conceived velocity of motion along the curve, is also easily interpreted; and the formulæ XVII., XVIII. give, for the same helix (by XXXI.), the values,

XXXVII...
$$r' = 0$$
, $H = a$, $P = 0$.

(5.) The normal (or the radius of curvature), as being perpendicular to the rectifying plane, revolves with the same velocity, and round a parallel line; to determine the position of which new line, or the point H in which it cuts the normal, we have only to change η to τ' in the formula 396, XXXII., which then becomes,

XXXVIII... OH =
$$\omega_0 = \rho - \tau' S \frac{\tau}{\lambda \tau'} = \rho - \lambda^{-2} \tau'$$

= $\rho + \frac{r^{-2}(\kappa - \rho)}{r^{-2} + r^{-2}} = \frac{r^2 \rho + r^2 \kappa}{r^2 + r^2}$
= $\rho \cos^2 H + \kappa \sin^2 H$;

the vector of rotation (396, (9.)) of the normal is therefore a line || and = λ , which divides (internally) the radius (r) of curvature into the two segments,*

XXXIX...
$$\overline{PH} = r \sin^2 H$$
, $\overline{HK} = r \cos^2 H$;

namely, into segments which are proportional to the squares $(r^{-2} \text{ and } r^{-2})$ of the first and second curvatures.

[•] This law of division of a radius of curvature into segments, by the common perpendicular to that radius and to its consecutive, has been otherwise deduced by M. de Saint Venant, in the Memoir already referred to.

ART. 397.] AXIS OF DISPLACEMENT OF NORMAL.

(6.) At the same time, what we have called generally the vector of translation of an emanant line becomes, for the normal (by 396, (10.), changing θ to λ), the line

XL...
$$\iota = \lambda S \frac{\tau}{\lambda} = U\lambda \cos H = -r^{-1}\lambda^{-1}$$
, set off from the same point H;

and the indefinite right line, or axis, through that point H,

XLI...
$$0 = \nabla \lambda(\omega - \omega_0)$$
, or XLI'... $0 = \nabla \lambda(\omega - \rho \cos^2 H - \kappa \sin^2 H)$,

along which axis the normal moves, through the small line s_i , while it turns round the same axis (as before) through the small angle $sT\lambda$, may be called (comp. again 396, (10.)) the Axis of Displacement of the Normal (or of the radius of curvature).

(7.) As a verification, for the *helix* (2.) we have thus the values,

XLII...
$$\overline{PH} = b$$
, $\omega_0 = \rho_t - b\epsilon^{at}\beta = bat \cot a$, $\iota = a \cos a$;

so that the axis of displacement (6.) coincides with the axis (a) of the cylinder, as was of course to be expected.

(8.) When the given curve is not a helix, the values VI., XVI., XXXVIII., and XL., of τ'' , λ , ω_0 , and ι , enable us to put the expression I. for ρ_s under the form,

XLIII...
$$\rho_s = \omega_0 + s\iota + \epsilon^{s\lambda}(\rho - \omega_0) - \frac{s^3 r' \tau'}{6r};$$

the curve therefore generally deviates, by this last small vector of the third order, namely by that part of the term $\frac{1}{6}s^3\tau''$ which has the direction of the normal τ' , or of $-\tau'$, and which depends on r', from the osculating helix,

XLIV...
$$\omega_s = \omega_0 + s\iota + \epsilon^{s\lambda}(\rho - \omega_0),$$

and from the osculating right cylinder,

XLV...
$$TV\lambda (\omega - \omega_0) = \sin H$$
,

whereon that helix is traced, and of which the rectifying line (XXXIII.) is a side, while its axis of revolution (comp. (7.)) is the axis of displacement (XLI.) of the normal.

(9.) Another general transformation, of the expression I. for the vector of the curve, is had by the substitution,

XLVI...
$$s = t + \frac{t^2 r'}{6r} + \frac{t^3}{6r^2}$$

in which t is a new scalar variable; for this gives the new form,

XLVII...
$$\rho_t = \rho + t\tau + \frac{1}{2}t^2\left(\tau' + \frac{r'\tau}{3r}\right) + \frac{1}{6}t^3\mathbf{r}^{-1}\nu,$$

and therefore shows that the curve deviates, by this other small vector of the third order,

$$\mathbf{XLVIII.} \quad . \quad \frac{1}{6}t^3\mathbf{r}^{-1}\nu = \frac{1}{6}s^3\mathbf{r}^{-1}\tau\tau',$$

that is, by the *part* of the *term* $\frac{1}{6}s^3\tau''$ which has the direction of the *binormal* ν , and which depends on **r**, from what we propose to call the Osculating Parabola, namely that new auxiliary curve of which the equation is,

XLIX. . .
$$\omega_t = \rho + t\tau + \frac{1}{2}t^2\left(\tau' + \frac{r'\tau}{3r}\right)$$
:

or from the *parabola* which osculates at the given point P, to the projection of the given curve on its own osculating plane.

(10.) And because the small deviation XLVIII. of the curve from the parabola is also the deviation of the same curve from this last plane, if we conceive that a near point Q of the curve is projected into three new points Q_1 , Q_2 , Q_3 , on the tangent, normal, and binormal respectively, we shall have the limiting equation,

L. . . lim.
$$\frac{3PQ_3}{PQ_1, PQ_2} = r^{-1} = Second Curvature;$$

the sign of this scalar quotient being determined by the rules of quaternions.

(11.) But we may also (comp. 396, (17.), (18.)) employ this third general transformation of I., analogous to the forms XLIII. and XLVII.,

LI. . .
$$\rho_s = \kappa + \epsilon^{s\nu}(\rho - \kappa) + \frac{s^3}{6}\nu'\tau$$
,

with the value XI. of ν' ; in which the sum of the two first terms gives the

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the third term.

vector of the point of the osculating circle, which is distant from the given point PP, by an arc of that circle equal to the arc s of the given curve; and

LII. . .
$$\frac{1}{6}s^{3}\nu'\tau = \frac{1}{6}s^{3}(\tau'' + r^{-2}\tau) = -\frac{1}{6}s^{3}r^{-1}r'\tau' + \frac{1}{6}s^{3}r^{-1}\nu,$$

which represents the *deviation* from the same circle, measured in a direction (comp. IX. or X.) tangential to the osculating sphere, is (as we see) the vector sum of two rectangular components, which represent respectively the deviations of the curve, from the osculating helix (8.), and from the osculating parabola (9.).

(12.) It follows, then, that although neither helix nor parabola has in general complete contact of the third order with a given curve in space, since the deviation from each is generally a small vector of that (third) order, yet each of these two auxiliary curves, one on a right cylinder XLV., and the other on the osculating plane, approaches in general more closely to the given curve, than does the osculating circle: while circle, helix, and parabola have, all three, complete contact of the second* order with the curve, and with each other.

(13.) As regards the geometrical signification of the new variable scalar, t, in the equation XLIX. of the parabola, that equation gives,

LIII. . .
$$\mathbf{T}\omega'_t = \mathbf{T}\left\{\left(1 + \frac{r't}{3r}\right)\mathbf{\tau} + t\mathbf{\tau}'\right\} = 1 + \frac{r't}{3r} + \frac{t^2}{2r^2} \dots,$$

and therefore (to the present order of approximation),

LIV. . . Arc of Osculating Parabola (from
$$\omega_0$$
 to ω_t)

$$= \int_0^t T \omega'_t dt = t + \frac{r't^2}{6r} + \frac{t^3}{6r^2} = s \text{ (by XLVI.)}$$

$$= Arc \text{ of Curve in Space (from } \rho_0 \text{ to } \rho_s);$$

if then an arc = s be thus set off upon the parabola, with the same initial point P, and the same initial direction, and if this parabolic arc, or its chord $\omega_t - \omega_0$, be obliquely projected on the initial tangent τ , by drawing a diameter of the

^{*} It appears then that we may say that the *helix* and *parabola* have each a *contact* with the *curve* in space, which is *intermediate between the second and third orders*: or that the *exponent* of the *order* of *each* contact is the *fractional index*, $2\frac{1}{2}$. But it must be left to mathematicians to judge, whether this phraseology can properly be adopted.

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parabola through its final point, the oblique tangential projection so obtained will be $= t\tau$ by XLIX.; and its length, or the ordinate to that diameter, will be the scalar t.

(14.) And as regards the *direction* of the *diameter* of the osculating parabola, drawn as we may suppose from P, if we denote for a moment by D its inclination to the normal $+\tau'$, regarded as positive when towards the tangent $+\tau$, we have (by XLIX. and XVIII.) the formula,

I.V...
$$\tan D = \frac{r'}{3} = \frac{1}{3} \tan P \cot H$$
:

which is an instance of the reducibility, above mentioned, of all affections of the curve depending on s^3 , to a dependence on the two angles, H and P.

(15.) Some of these affections, besides the direction of the rectifying line λ , can be deduced from the angle *H* alone. As an example, we may observe that the vector equation of the surface of tangents is of the form,

LVI. . .
$$\omega_s, t = \rho_s + t\rho'_s = \rho_s + t\tau_s$$
,

in which s and t are two independent and scalar variables, and

LVII. . .
$$\tau_s = \tau + s\tau' + \frac{s^2}{2}\tau'',$$

+ terms depending on s^4 in ρ_s . If then we cut this developable LVI. by the plane,

LVIII. . . $S_{\tau}(\omega - \rho) = -c = any$ given scalar constant,

which is, relatively to the surface, a normal plane at the extremity of the tangential vector $c\tau$ from P, while this tangent is also a generating line, we get thus a principal^{*} normal section, of which the variable vector has for its approximate expression.

LIX. . .
$$\omega_s = (\rho + c\tau) + (cs + ...)\tau' + (\frac{1}{2}cs^2r^{-1} + ...)\nu;$$

the terms suppressed being of higher orders than the terms retained, and having no influence on the *curvature* of the section. We find then thus,

[•] Some general acquaintance with the known theory of sections of surfaces is here supposed, although that subject will soon be briefly treated by quaternions.

ABT. 397.]

SECTION OF SURFACE OF TANGENTS.

that the vector of the centre of the osculating circle to this normal section of the surface of tangents to the given curve is, rigorously,

LX. . .
$$\rho + c\tau + \frac{(cs\tau')^2}{cs^2\mathbf{r}^{-1}\nu} = \rho + c(\tau + \mathbf{r}\nu) = \rho + c\mathbf{r}\lambda;$$

so that the *locus* of all such centres is the rectifying line XXXIII'. And if, in particular, we make c = r, or cut the developable at the extremity of the tangential vector $r\tau$, the expression LX. becomes then $\rho + r\tau + rU\nu$; which expresses that the radius of the circle of curvature of this normal section of the surface is precisely what has been called the Radius (r) of Second Curvature, of the given curve in space. But this radius ($\mathbf{r} = r \tan H$) depends only on the angle H, when the radius (r) of (absolute) curvature is given, or has been previously determined.

(16.) The cone of the second order, represented by the quaternion equation,

LXI...
$$0 = 2\mathbf{r}S\tau(\omega - \rho) S\nu(\omega - \rho) + (\nabla\tau(\omega - \rho))^2$$

has its vertex at the given point P, and rests upon the circle last determined; it is then the locus of all the circles lately mentioned (15.), and is therefore (in a known sense) an osculating oblique cone to the developable surface of tangents: its cyclic normals (comp. 357, &c.) being τ and $\tau + 2rv$, or τ and $r\tau + 2rUv$. But, by 394, (30.), the osculating right cone to this cone LXI., and therefore also (in a sense likewise known) to the surface of tangents itself, is one which has the recent locus of centres (15.), namely the rectifying line (λ), for its axis of revolution, while the tangent (τ) to the quaternion equation of this osculating right cone is the following (comp. XLV.),

LXII... TVU
$$\lambda(\omega - \rho) = \sin H$$
.

(17.) The right cone LXII., which thus osculates to the developable surface of tangents LVI., along the given tangent τ , osculates also along that tangential line to the cone of parallels to tangents, which has its vertex at the given point P; as is at once seen (comp. 394, (30.)), by changing ρ' and ρ'' to τ' and τ'' , in the general expression $\nabla \rho' \rho''$ (393, (6.), or 394, (6.)), for a line in the direction of the axis of the osculating circle to a curve upon a sphere. And the axis of the right cone thus determined, namely (again) the rectifying line (λ), intersects the plane of the great circle of the osculating

[III. III. § 6.

sphere, which is parallel to the osculating plane, in a point L of which the vector is,

LXIII... or = $\rho + rp\lambda = \rho + rr'\tau + rp\nu$.

(18.) We have thus, in general, a gauche quadrilateral, PKSL, right-angled except at 1., with the help of which one figure all affections of the curve, not depending on s^4 , can be geometrically represented or constructed : although it must be observed that when r' = 0, which happens for the helix (XXXVII.), the osculating circle is then itself a great circle of the osculating sphere, and the points F and L, like the points K and s, coincide.

(19.) In the general case, it may assist the conceptions to suppose lines set off, from the given point P, on the tangent and binormal, as follows :

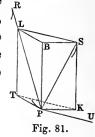
LAIV...
$$PT = BL = rr'\tau$$
; $PB = TL = KS = rpv$;

for thus we shall have a *right triangular prism*, with the two right-angled triangles, TFK and LBS, in the osculating plane and in the parallel plane (17.), for two of its faces, while the three others are the rectangles, PKSB, PBLT, KSLT, whereof the two first are situated respectively in the normal and rectifying planes.

(20.) All scalar properties of this auxiliary prism may be deduced, by our general methods, from the *three scalars*, r, r, r', or r, H, P; and all vector-properties of the same prism can in like manner be deduced from the *three vectors*, τ , τ' , τ'' , or from τ , ν , ν' , which (as we have seen) are not entirely arbitrary, but are subject to certain conditions.

(21.) As an example of such deduction (compare the annexed figure 81), the equation of the diagonal plane SPL, which contains the _R

radius (R) of spherical curvature and the rectifying line (λ) , and the equation of the trace, say PU, of that plane on the osculating plane, which trace is evidently parallel (by the construction) to the edges LS, TK of the prism are in the recent notations (comp. XX.),



LXV...
$$0 = Sr''(\omega - \rho)$$
; LXVI... $0 = V(r^{-1}r)'(\omega - \rho)$;

with the verification that $rS\tau'\tau'' = r'S\tau\tau'' = r^{-2}r'$, by II.

(22.) In general, by 204, (22.), if a and β be any two vectors, we have the expressions,

LXVII...
$$\tan \angle \frac{\beta}{a} = \tan \angle \frac{a}{\beta} = -\tan \angle \beta a = -\tan \angle a\beta$$

= $\operatorname{TV}\frac{\beta}{a}: \operatorname{S}\frac{\beta}{a} = \frac{\operatorname{TV}}{\operatorname{S}} \cdot \frac{\beta}{a} = -(\operatorname{TV}:\operatorname{S}) a\beta$,

ABT. 397.] INCLINATIONS DETERMINED BY QUATERNIONS.

the angles of quaternions here considered being supposed as usual (comp. 130) to be generally > 0, but < π ; for example, we have thus,

LXVIII...
$$\tan H = \tan \angle \frac{\lambda}{\tau} = (\mathrm{TV}:\mathrm{S})\lambda\tau^{-1} = (\mathrm{TV}:\mathrm{S})(\mathrm{r}^{-1} - \tau') = \mathrm{rT}\tau' = \mathrm{r}\tau^{-1},$$

as in XVII.; and in like manner we have generally, by principles already explained (comp. 196, XVI.),

LXIX...
$$\cos \angle \frac{\beta}{a} = \cos \angle \frac{a}{\beta} = -\cos \angle \beta a = -\cos \angle a\beta$$

= $S\frac{\beta}{a}:T\frac{\beta}{a} = SU\frac{\beta}{a} = -SUa\beta.$

(23.) Applying these principles to investigate the inclinations of the vector τ'' , which is perpendicular to the diagonal plane LXV. of the prism, to the three rectangular lines τ , τ' , ν , or the inclinations of that diagonal plane itself to the normal, rectifying, and osculating planes, with the help of the expressions deduced from VI. for the three products,* $\tau\tau''$, $\tau'\tau''$, $\nu\tau''$, we arrive easily at the following results:

LXX...
$$\cos \angle \frac{\tau''}{\tau} = \frac{-r^{-2}}{T\tau''}; \quad \cos \angle \frac{\tau''}{\tau'} = -\frac{r^{-2}r'}{T\tau''}; \quad \cos \angle \frac{\tau''}{\nu} = \frac{r^{-1}r^{-1}}{T\tau''};$$

with the verification, that the sum of the squares of these three cosines is unity, because

or

LXXI...
$$r^{2}T\tau'' = \sqrt{(1 + r^{-2}R^{2})} = \sqrt{(1 + r'^{2} + r^{2}r^{-2})};$$

LXXI... $rT\tau'' = \sqrt{(r^{-2}r'^{2} + T\lambda^{2})}, \quad T\tau'' = \sqrt{(r^{-4} + T\nu'^{2})}.$

(24.) Or we may write, on the same general plan,

LXXII... $\tan \angle \frac{\tau''}{\tau} = \frac{-R}{\mathrm{Tr}}; \quad \tan \angle \frac{\tau''}{\tau'} = \frac{-r\mathrm{T}\lambda}{r'}; \quad \tan \angle \frac{\tau''}{\nu} = \frac{\mathrm{r}}{r}\sqrt{(1+r'^2)};$ or LXXIII... $\tan \angle \tau\tau'' = R\mathrm{Tr}^{-1}; \quad \tan \angle \tau'\tau'' = rr'^{-1}\mathrm{T}\lambda; \quad \tan \angle \nu\tau'' = -\mathrm{r}r^{-1}\sqrt{(1+r'^2)};$

* A student, who should be inclined to pursue this subject, might find it useful to form for himself a *table* of all the *binary products* of the nine vectors,

$$\tau$$
, τ' , τ'' , ν , ν' , λ , $\sigma - \rho$, $\sigma - \mu$, and κ' ,

considered as so many quaternions, and reduced to the common quadrinomial form, $a + b\tau + c\tau' + e\nu$, in which a, b, c, e are scalars, whereof some may vanish, but which are generally functions of r, r, and r'.

[III. m. § 6.

and may modify the expressions, by introducing the auxiliary angles H and P, with which may be combined, if we think fit, the following angle of the prism,

LXXIV... PKT = BSL =
$$\tan^{-1} r'$$
.

(25.) Instead of thus comparing the *plane* SPL with the three rectangular planes (379, (5.)) of the construction, we may inquire what is the value of the *angle* SPL, which the radius (R) of spherical curvature makes with the rectifying line (λ); and we find, on the same plan, by quaternions, the following very simple expression for the cosine of this angle, which may however be deduced by spherical trigonometry also,

LXXV...
$$\cos \text{ spl} = -SU\lambda(\sigma - \rho) = \frac{pr^{-1}}{RT\lambda} = \sin P \sin H;$$

or

LXXV'... cos spl = cos spb cos bpl.

(26.) In general, it is easy to form, by methods already explained, the quaternion equation of a *cone* which has a *given vertex*, and *rests* on a *given curve* in space; and also to determine the *right cone* which osculates (394, (30.)) to this general cone, along any given side of it.

(27.) But if we merely wish to assign the osculating right cone to the cone of chords from \mathbf{P} , or to the locus of the line \mathbf{PP}_s , we may imitate a recent process: and may observe that if this new cone be cut by the normal plane LVIII., the vector of the section has the following approximate expression, analogous to LIX., and like it sufficient for our purpose,

LXXVI...
$$\omega_s = \rho + c\tau + \frac{1}{2}cs\tau' + \frac{1}{6}cs^2r^{-1}\nu;$$

from which it may be inferred (comp. (15.), (16.)), that the axis of revolution of the new right cone has for equation,

LXXVII...
$$0 = \nabla (\mathbf{r}^{-1} \tau + \frac{3}{4} \nu) (\omega - \rho).$$

This axis is therefore situated in the rectifying plane, between the rectifying line $(\lambda \text{ or } \mathbf{r}^{-1}\tau + \nu)$, and the tangential vector (IV.) of second curvature $(\mathbf{r}^{-1}\tau)$: while the semiangle C of the same new cone (measured like H from $+\tau$ towards $+\nu$) has the value already assigned by anticipation in the formula XXV., and is therefore less than the semiangle H if both be acute, but greater than H if both be obtuse; so that, in each case, the new right cone (C) is sharper than the old right cone (H).

ART. 397.] INTERSECTION OF OSCULATING SURFACES.

(28.) The same result may be otherwise obtained, by observing that an unit-vector in the direction of the chord PP_s has (by 396, XLIV., and 397, I.) the approximate expression,

LXXVIII...
$$\chi_s = \mathbf{U}(\rho_s - \rho) = \left(1 + \frac{s^2}{24r^2}\right) \left(\tau + \frac{s\tau'}{2} + \frac{s^2\tau''}{6}\right)$$

= $\tau + \frac{s\tau'}{2} + \frac{s^2}{6} \left(\tau'' + \frac{r^{-2}\tau}{4}\right);$

whence the axis of the osculating right cone to the cone of chords (27.) has rigorously the direction of the line $\nabla \chi' \chi''$ (for s = 0), or of the vector,

LXXIX...
$$\xi = \nabla \tau' (r^2 \tau'' + \frac{1}{4}\tau) = \lambda - \frac{1}{4}\nu = r^{-1}r + \frac{3}{4}\nu$$
, as before.

(29.) This axis ξ makes (if we neglect s³) the same angle C, with the chord PP_s, as with the tangent τ ; whereas the former axis λ makes unequal angles with those two lines, within the same order (or degree) of approximation: for our methods conduct to the expression,

LXXX...
$$\angle \frac{\rho_s - \rho}{\lambda} = H - \frac{s^2}{24rr}$$

from which the *relation* XXV, between the *two right cones*, may easily be deduced anew.

(30.) Neglecting only s⁴, and employing the substitution XLVI., the expression XLVII. for the vector of the given curve becomes,

LXXXI...
$$\rho_t = \rho + t\tau + \frac{1}{2}t^2\upsilon + \frac{1}{6}t^3\mathbf{r}^{-1}\upsilon$$
, if LXXXII... $\upsilon = \tau' + \frac{r'\tau}{3r}$;

where the variable scalar t denotes, by (13.), the ordinate of the osculating parabola, and the constant vector v has the direction, by (14.), of the diameter of that parabola.

(31.) In the present order of approximation, then, the proposed curve in space may be considered to be the common intersection of the three following surfaces of the second order, all passing through the given point P.

$$\begin{split} & \text{LXXXIII.} \dots 2(\text{S}\tau'(\omega-\rho))^2 = 3\text{r}\text{S}\nu(\omega-\rho)\text{S}\upsilon\nu(\omega-\rho); \\ & \text{LXXXIV.} \dots 2\text{S}\tau'(\omega-\rho) = -r^2(\text{S}\upsilon\nu(\omega-\rho))^2; \\ & \text{LXXXV.} \dots 3\text{r}\text{S}\nu(\omega-\rho) = -r^2\text{S}\tau'(\omega-\rho)\text{S}\upsilon\nu(\omega-\rho); \end{split}$$

[III. 111. § 6.

whereof the first represents a new osculating oblique cone, which has a contact of the same (second) order with the cone of chords, as the osculating right cone (27.); the second represents an osculating parabolic cylinder, which is cut perpendicularly in the osculating parabola (9.), by the osculating plane to the curve; and the third represents a certain osculating hyperbolic (or ruled) paraboloid, whereof the tangent (τ) is one of the generating lines, while the diameter (v) of the osculating parabola is another.

(32.) Each of these three surfaces (31.) has in fact generally a contact of the third order with the given curve; or has its equation satisfied, not only (as is obvious on inspection) by the point P itself, but also when we derivate successively with respect to the scalar variable t, and then substitute the values (comp. LXXXI.),

LXXXVI... $\omega = \rho_0 = \rho$, $\omega' = \rho_0' = \tau$, $\omega'' = \rho_0'' = v$, $\omega''' = \rho_0''' = r^{-1}v$;

r, r, ρ , τ' , ν , and v being treated as constants of the equation, or of the surface, in each of these derivations.

(33.) The cone LXXXIII., and the cylinder LXXXIV., have a common generatrix, namely the binormal^{*} (ν); and in like manner, another generating line of the same cone, namely the tangent (τ) to the curve, has just been seen (31.) to be a line on the paraboloid LXXXV.: and although the cylinder and paraboloid have no finitely distant right line common, yet each may be said to contain the line at infinity, in the diametral plane of the cylinder, namely in the plane of ν and ν , of which plane the quaternion equation is (comp. (14.)),

LXXXVII... $0 = S_{\nu\nu}(\omega - \rho)$, or LXXXVII'... $0 = S(rr'\tau' - 3\tau)(\omega - \rho)$;

or the line in which this diametral meets the parallel axial plane.

(34.) On the whole, then, it is clear, from the known theory of intersections of surfaces of the second order having a common generating line, that the given curve of double curvature (whatever it may be) has contact of the third order with the twisted cubic,[†] or gauche curve of the third degree, which is

^{*} The geometrical reason, for the osculating cone LXXXIII. to the cone of chords containing the binormal (ν) , is that if the expression LXXXI. for ρ_i were rigorous, and if the variable t were supposed to increase indefinitely, the ultimate direction of the chord PP_i would be perpendicular to the osculating plane. And the same binormal is a generating line of the parabolic cylinder also, because that cylinder passes through P, and all its generating lines are perpendicular to the last mentioned plane. It is sufficient however to observe, on the side of calculation, that the equations LXXXIII. and LXXXIV. are satisfied, when we suppose $\omega - \rho \parallel \nu$.

⁺ Compare again page 241, already eited, of Dr. Salmon's Treatise; also Art. 285, in page 225 of the same work.

ART. 397.] INTERSECTION OF OSCULATING SURFACES.

represented without ambiguity by the system of the two scalar equations,

LXXXVIII...
$$y = x^2$$
, $z = x^3$,

if we write for abridgment,

IJXXXIX...
$$\begin{cases} x = (t =) - r^2 \mathrm{S}v\nu(\omega - \rho), \\ y = (t^2 =) - 2r^2 \mathrm{S}\tau'(\omega - \rho), \\ z = (t^3 =) - 6r^2 \mathrm{S}\nu(\omega - \rho). \end{cases}$$

(35.) As another geometrical connexion between the elements of the present theory, it may be observed that while the *osculating plane* to the *curve*, of which plane the equation is,

XC...
$$S_{\nu}(\omega - \rho) = 0$$
, as in 396, XV.,

touches the oblique cone LXXXIII., along the tangent τ to the same curve, the diametral plane LXXXVII. touches the same cone along the binormal ν , which was lately seen (33.) to be, as well as τ , a side of that oblique cone; but these two sides of contact, τ and ν , are both in the rectifying plane (396, XIV.), and the two tangent planes corresponding intersect in the diameter ν of the parabola (9.); we have therefore this theorem :—

The diameter of the osculating parabola to a curve of double curvature is the polar of the rectifying plane, with respect to the osculating oblique cone LXXXIII.; that is, with respect to a certain cone of the second order, which has been above deduced from the expression LXXXI. for the vector ρ_t of the curve, as one naturally suggested thereby, and as having a contact of the third order with the curve at P, and therefore also a contact of the second order with the cone of chords from that point.

(36.) Conversely, this particular cone LXXXIII. is geometrically distinguished from all other* cones of the same (second) order, which have their vertices at the given point P, and have each a contact of the same second order,

$$2r^{2}(\mathrm{S}\tau'(\omega-\rho))^{2}=3\mathrm{r}\mathrm{S}\tau(\omega-\rho)\mathrm{S}\nu(\omega-\rho)\,;$$

and with respect to this cone (comp. (35.)), the polar of the rectifying plane is the (absolute) normal (τ') to the curve.

^{*} The cone of this system (36.), which is touched along the binormal by the normal plane, and which therefore intersects the parabolic cylinder LXXXIV. in a new twisted cubic (comp. (34.)), having also contact of the third order with the curve, is easily found to have, for its quaternion equation, the following:

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with the given cone of chords from that point, or of the third order with the given curve, by the condition that it is touched (as above), along the binormal (v), by the diametral plane (vv) of the osculating parabolic cylinder LXXXIV.

(37.) We have already considered, in 395, (5.), the simultaneous variations of the points \mathbf{r} and $\mathbf{\kappa}$, or of the vectors ρ and κ . With recent notations, including the expression $\mu = 2\kappa - \rho$, we have the following among other transformations, for the *first derivative* of the latter vector, and therefore for the *tangent* $\mathbf{\kappa}\mathbf{\kappa}'$ to the *locus of centres of curvature*, of a given curve in space:

XCI...
$$\kappa \kappa' = D_{s\kappa} = \kappa' = (\rho - \tau'^{-1})' = \tau + \tau'^{-1}\tau''\tau'^{-1}$$

$$= (\rho + r^{2}\tau')' = \tau + r^{2}\tau'' + 2rr'\tau'$$

$$= rr'\tau' + r^{2}r^{-1}\nu = rr'(\tau' + p^{-1}r\nu) = rr^{-1}(p\tau' + r\nu)$$

$$= \frac{rr'}{\rho - \kappa} - \frac{rr'}{\sigma - \kappa} = \frac{rr'(\sigma - \mu)}{(\sigma - \kappa)(\kappa - \rho)} = r^{-1}(\sigma - \mu)\tau$$

$$= \cot H(U\tau' \tan P + U\nu) = r^{-1}k(U\tau' \sin P + U\nu \cos P)$$

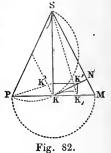
$$= r^{4}\nu\nu'\tau' = r^{4}\tau'\nu'\nu = \nu^{-1}\nu'\tau'^{-1} = \tau'^{-1}\nu'\nu^{-1}$$

$$= r^{-1}\nu(\rho - \sigma)(\kappa - \rho) = r^{-1}(\kappa - \rho)(\rho - \sigma)\nu$$

$$= r^{-1}RU(\nu(\rho - \sigma)(\kappa - \rho)) = \&c.$$

if then we draw the diameter of curvature PM, and let fall a perpendicular

KN from the centre K of the osculating circle on the new radius SM of the osculating sphere (as in the annexed figure 82), this perpendicular will touch* the locus of the centre K, a result which agrees with the construction in 395, (6.); and we see, at the same time, that the length of the line KK', or the tensor $T_{\kappa'}$, may be expressed (comp. LXXIII.) as follows,



XCII...
$$\overline{\mathbf{K}\mathbf{K}'} = \mathbf{T}_{\mathbf{K}'} = R\mathbf{T}\mathbf{r}^{-1} = r^{2}\mathbf{T}\nu' = \tan \angle \tau\tau''.$$

(38.) If we project the tangent KK', into its two rectangular components, KK, and KK', on the diameter of curvature and

^{\circ} Geometrically, and by infinitesimals, if we conceive κ' to be an infinitely near point of the locus of κ , and therefore in the normal plane at r, the angle $r\kappa's$ (like $r\kappa s$) will be right, and the point κ' will be on the semicircle $r\kappa s$; but the radius of this semicircle drawn to κ (comp. fig. 82) is parallel to the line sm, to which line the tangent $\kappa\kappa'$ is therefore perpendicular, as above.

ABT. 397.] TANGENT TO LOCUS OF CENTRES.

the polar axis, we shall have by XCI. the expressions :

XCIII... KK, =
$$rr'r'$$
 = $r'Ur'$ = $\frac{rr'}{\rho - \kappa}$ = &c.
XCIV... KK' = $r^2r^{-1}\nu = rr^{-1}U\nu = \frac{-rr'}{\sigma - \kappa}$ = &c.

these two projections then, or the vector-tangent KK' itself, would suffice to determine r and r', or H and P, and thereby all the affections of the curve which depend on s^3 , but not on s^4 .

(39.) We have also the similar triangles (see again fig. 82),

XCV... Δ K,K'K \propto K'KK' \propto KMS;

and the vector equations,

XCVI...
$$\kappa\kappa'$$
: $sM = \kappa\kappa$, : $s\kappa = \kappa\kappa'$: $\kappa = \kappa\kappa'$: $P\kappa$
= $r^{-1}\tau$ = Vector of second curvature (IV.);

whence also result the scalar expressions,

XCVII. . . tan KSK, = tan KPK' = r^{-1} = Second* Curvature (III.) :

this last scalar being *positive* or *negative*, according as the *rotation* KSK, (or KPK') appears to be positive or negative, when seen from *that side* of the *normal plane*, towards which the conceived *motion* (396, (1.)) along the given curve, or the *unit tangent* + τ , is directed.[†]

(40.) Besides the seven expressions, III., XXVII., L., and XCVII., this important scalar r^{-1} admits of many others, of which the following, numbered for reference as 8, 9, &c., and deduced from formulæ and principles already laid down, are examples: and may serve as exercises in transformation, according to the rules of the present Calculus, while some of them may also be found useful, in future geometrical applications.

^{*} In illustration it may be observed, that if ds be treated as infinitely small, and if the line $\kappa\kappa'$ be supposed to represent (not the *derivative* κ' , but) the *differential* vector $d\kappa = \kappa' ds$, then the *projections* $\kappa\kappa$, and $\kappa\kappa'$ become dr and $rr^{-1}ds$ (comp. XCIII. and XCIV.); while $\kappa\mu\kappa'$ (in fig. 82) represents the *infinitesimal angle* $r^{-1}ds$, through which the osculating plane (comp. (1.)) revolves, round the tangent τ to the curve during the change ds of the arc.

[†] This direction of $+\tau$ is to be conceived (comp. fig. 81, [p. 100]) to be towards the back of fig. 82, as drawn, if the scalars r and r (and therefore also p) be positive.

[III. III. § 6.

(41.) We have then (among others) the transformations:

$$\begin{aligned} \text{XCVIII.} \quad .. \quad Second \quad Curvature = \mathbf{r}^{-1} (= seven \ preceding \ expressions) \\ &= p^{-1}r' = r^{-1} \ \text{cot} \ H = \text{T}\lambda \ \text{cos} \ H = r^{-1}r' \ \text{cot} \ P \qquad (8, 9, 10, 11) \\ &= r^2 \text{S}\nu'\tau' = - \text{S}\nu'\tau'^{-1} = -r^2 \text{S}\tau\tau'\tau'' = \text{S}\tau\tau'^{-1}\tau'' \qquad (12, 13, 14, 15) \\ &= -r^2 \text{S}\nu\tau'' = \text{S}\nu^{-1}\tau'' = -\text{S}\nu\kappa' = \text{S}\tau\kappa'\tau' \qquad (16, 17, 18, 19) \\ &= \tau\kappa'(\sigma - \mu)^{-1} = \text{S}\lambda\tau^{-1} = (\kappa - \rho) \nabla\lambda\nu = -\tau'^{-1} \nabla\lambda\nu \qquad (20, 21, 22, 23) \\ &= r^2\tau' \nabla\lambda\nu = r^2 \text{S}\lambda\nu\tau' = \text{S}\lambda\tau'\nu^{-1} = \text{S}\lambda\tau'^{-1}\nu \qquad (24, 25, 26, 27) \\ &= r^2 \text{S}\nu'\lambda\tau = r^2 \text{S}\nu'\nu\tau = \text{S}\tau\nu^{-1}\nu' = r^2 \text{S}\nu'\nu'^{-1}\tau'' \qquad (28, 29, 30, 31) \\ &= r^4 \text{S}\nu\nu'\tau'' = \tau''^{-1} \nabla\nu'\lambda = r^3r'^{-1} \text{S}\nu'\lambda\tau' = r^3r'^{-1} \text{S}\nu\lambda\tau'' \qquad (32, 33, 34, 35) \\ &= \text{S}\nu'\lambda\tau''^{-1} = \text{T}\tau''^{-2} \text{S}\lambda\nu'\tau'' = \frac{-(r\nu)'}{r\tau'} = \frac{-r^2\nu'}{\sigma - \rho} \qquad (36, 37, 38, 39) \\ &= \frac{-r\nu\nu'}{r\tau' + p\nu} = \frac{r^2\tau'' + \tau}{\tau(\sigma - \rho)} = R^{-1} \tan \angle \mathbf{r}\tau'' = R^{-1} \tan \angle \frac{\nabla\lambda\nu'}{\tau} (40, 41, 42, 43) \\ &= \frac{rr'\nu}{\sigma - \kappa} = \frac{rr'\tau'}{(\sigma - \kappa)\tau} = \frac{r'}{r} \cdot \frac{\tau(\kappa - \rho)}{\sigma - \kappa} = \frac{rr'\tau}{(\sigma - \kappa)(\rho - \kappa)} \qquad (44, 45, 46, 47) \end{aligned}$$

$$= S \frac{ip\lambda}{(\sigma-\kappa)(\rho-\kappa)} = S \frac{\rho+ip\lambda-\kappa}{(\sigma-\kappa)(\rho-\kappa)} = S \frac{KL}{KS.KP}$$
(48, 49, 50)

$$= S \frac{SL}{PK \cdot KS} = \frac{-(Sar\nu)'}{r(Sa\tau)'} = \frac{-d \cos \angle \frac{\nu}{a}}{rd \cos \angle \frac{\tau}{a}};$$
(51, 52, 53)

PKSL, in the forms 50 and 51, being points of the same gauche quadrilateral as in (18.); and a, in 52 and 53,* denoting any constant vector: while several other varieties of form may be deduced from the foregoing by very simple processes, such as the substitution of U_{ν} for r_{ν} , &c., which gives for instance (comp. XI'.), from the form 38, these others,

XCVIII'...
$$\mathbf{r}^{-1} = \frac{-(\mathbf{U}\nu)'}{r\tau'} = \frac{-(\mathbf{U}\nu)'}{\mathbf{U}\tau'} = \frac{-d\mathbf{U}\nu}{rd\tau}$$
 (54, 55, 56)

We may also write, with the significations (10.) of q_1 and q_3 , the following expression analogous to L.,

XCVIII"...
$$r^{-1} = 6\kappa p . \lim_{PQ_1^3} \frac{PQ_3}{PQ_1^3}$$
, (57)

[•] This last form 53 corresponds to and contains a theorem of M. Serret, alluded to in the second Note to page 92.

ART. 397.] EXPRESSIONS FOR THE SECOND CURVATURE.

which contains the law of the *inflexion* of the *plane curve*, into which the proposed curve of *double curvature* is *projected*, on its own *rectifying plane*; the *sign* of the *scalar*, to which this last expression ultimately reduces itself, being determined by the rules of quaternions.

(42.) And besides the various expressions for the positive scalar r^{-2} , which are immediately obtained by *squaring* the foregoing forms, the following are a few others :

XCIX. . . Square of Second Curvature =
$$\mathbf{r}^{-2} = \mathbf{T}\mathbf{r}^{-2}$$

$$= T\lambda^{2} - r^{-2} = r^{2}S\tau''\tau'\lambda - r^{-2} = r^{2}T\nu'^{2} - r^{-2}r'^{2}$$
(1, 2, 3)

$$= r^{2} \mathrm{S} \tau \nu' \tau'' - r^{-2} r'^{2} = r^{2} \mathrm{T} \tau''^{2} - r^{-2} - r^{-2} r'^{2} = R^{-2} (r^{4} \mathrm{T} \tau''^{2} - 1) \qquad (4, 5, 6)$$

$$= R^{-2} r^4 \mathrm{T} v^{\prime 2} = R^{-2} \mathrm{T} \kappa^{\prime 2} = R^{-2} \tan^2 \angle \tau \tau^{\prime \prime}; \qquad (7, 8, 9)$$

while the important vector τ'' , besides its two original forms VI., admits of the following among other expressions (comp. XX. XXI.):

C...
$$\tau'' = D_s^{3}\rho$$
 (= the two expressions VI.)

$$= r^{-2} V \lambda(\sigma - \rho) = \lambda \tau' - r^{-1} r' \tau' = \nu' \tau - r^{-2} \tau$$
 (3, 4, 5)

$$= \mathbf{r} \nabla \nu' \lambda = r^{-2} \mathbf{r}^{-1} \tau (\sigma - \rho - \mathbf{r}) = r^{-3} p + r^{-2} \lambda (\sigma - \rho)$$
 (6, 7, 8)

$$= ((\rho - \kappa)^{-1})' = \tau'(\kappa' - \tau)\tau' = -r^{-2}\tau - \frac{r^{-1}r'}{\rho - \kappa} - \frac{r^{-1}r'}{\sigma - \kappa} \cdot$$
(9, 10, 11)

(43.) As regards the general theory (396, (5.), &c.) of emanant lines (η) from curves, it might have been observed that if we write,

CI...
$$\zeta = \nabla \frac{\tau}{\theta}$$
, with CII... $\theta = \nabla \frac{\eta'}{\eta}$, as in 396, XXVII.,

the equation 396, XXXII. takes the simplified form,

CIII... PH =
$$\omega_0 - \rho = \eta S \eta^{-1} \zeta$$
 = projection of vector ζ on emanant η ;

for example, when $\eta = \nu$, then $\theta = r^{-1}\tau$, and $\zeta = 0$, PH = 0, or $\omega_0 = \rho$, as in (1.); and when $\eta = \tau$, then $\theta = \nu$, $\zeta = r^2\tau' \perp \eta$, so that the *projection* PH again vanishes, as in 396, (13.).

(44.) In an extensive class of applications, the emanant lines are perpendicular to the given curve $(\eta \perp \tau)$; and since we have, by (43.),

CIV. . .
$$\zeta = \frac{\nabla \tau \nabla \eta' \eta}{\eta^2 \theta^2} = \eta^{-1} \theta^{-2} S \tau \eta' = \frac{\eta^{-1} S \eta \tau'}{T \theta^2}, \text{ if } S \tau \eta = 0,$$

we may write, for this case of normal emanation, the formula,

CV... PH =
$$\zeta = \frac{\text{projection of vector of curvature } (\tau') \text{ on emanant line } (\eta)}{\text{square of velocity } (T\theta) \text{ of rotation of that emanant}};$$

for example, when the emanant (η) coincides with the *absolute normal* (τ') , we have then $\theta = \lambda$, as in (3.), and the recent formula CV. becomes,

CVI. . . PH =
$$\omega_0 - \rho = \zeta = \tau' T \lambda^{-2} = r^2 \tau' \sin^2 H = (\kappa - \rho) \sin^2 H$$

which agrees with the expression XXXVIII.

(45.) And in the corresponding case of tangential emanant planes, by making $S_{\tau\eta} = 0$ in the second equation 396, XXXVI., and passing to a second derived equation, we find for the *intercept* between the point **P** of the curve, and the point, say **R**, in which the line of contact of the plane with its own envelope touches the cusp-edge of that developable surface, the expression,

CVII... PR =
$$\frac{-\nabla_{\eta\eta'}S_{\eta\tau'}}{S_{\eta\eta'\eta''}} = \frac{-S_{\eta\tau'(\text{or} + S_{\tau\eta'})}}{projection of \eta'' on \theta};$$

which accordingly vanishes, as it ought to do, when $\eta = \nu$, that is, when the emanant plane $S_{\eta}(\omega - \rho) = 0$ coincides with the osculating plane XC.

(46.) Some additional light may be thrown on this whole theory, of the affections in a curve in space depending on the third power of the arc, and even on those affections which depend on higher powers of s, by that conception of an auxiliary spherical curve, which was employed in 379, (6.) and (7.), to supply constructions (or geometrical representations) for the directions, not only of the tangent (ρ') to the given curve, to which indeed the unit-vector (τ) of the new curve is parallel, but also of the absolute normal, the binormal, and the osculating plane; while the same auxiliary curve served also, in 389, (2.), to furnish a measure of the curvature of the original curve, which is in fact the velocity* of motion in the new or spherical curve, if that in the old or given one be supposed to be constant, and be taken for unity.

(47.) We might for instance have observed, that while the normal plane to the curve in space is represented (in direction) by the tangent plane to the sphere, the rectifying plane (as being perpendicular to the absolute normal) is represented similarly by the normal plane to the spherical curve : and it is not

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^{*} Accordingly the vector of velocity τ' , of this conceived motion in the auxiliary curve, is precisely what we have called (389, (4.), comp. 396, VI.) the vector of curvature of the proposed curve in space : and its tensor $(T\tau')$ is equal to the reciprocal of the radius (r) of that curvature.

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difficult to prove that the *rectifying line* has the direction of that *new radius* of the sphere, which is drawn to the *point* (say L) where the *normal arc* to the auxiliary curve *touches its own envelope*.

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(48.) The point L thus determined is the common spherical centre (comp. 394, (5.)) of curvature, of the auxiliary curve itself, and of that reciprocal^{*} curve on the same sphere, of which the radii have the directions (comp. 379, (7.)) of the binormals to the original curve; the trigonometric tangent of the arcual radius of curvature of the auxiliary curve is therefore ultimately equal to a small arc of that curve, divided by the corresponding arc of the reciprocal curve (or rather by the latter arc with its direction reversed, if the point L fall between the two curves upon the sphere); and therefore to the first curvature (r^{-1}) of the given curve, divided by the second curvature (r^{-1}) : and thus we have not only a simple geometrical interpretation of the quaternion equation XI'., but also a geometrical proof (which may be said to require no calculation), of the important but known relation XVII., which connects the ratio (r: r) of the two curvatures, with the angle (H) between the tangent (τ) and the rectifying line (λ), for any curve in space.

(49.) In whatever manner this known relation $(\tan H = \mathbf{r} : r)$ has once been established, it is geometrically evident, that *if the ratio of the two* curvatures be constant, then, because the curve crosses the generating lines of its own rectifying developable (396) under a constant angle (H), that developable surface must be cylindrical: or in other words, the proposed curve of double curvature must, in the case supposed, be a geodetic \dagger on a cylinder (comp. 380, (4.)). Accordingly the point L, in the two last sub-articles, becomes then a fixed point upon the sphere, and is the common pole of two complementary small circles, to which the auxiliary spherical curve (46.), and the reciprocal curve (48.), in the case here considered, reduce themselves; so that the tangent and

^{*} The reciprocity here spoken of, between these two spherical curves, is of that known kind, in which each point of one is a pole of the great-circle tangent, at the corresponding point of the other: and accordingly, with our recent symbols, we have not only $\nu = V\tau\tau'$, but also, $V\nu\nu' = r^{-2}V\nu'\nu^{-1} = r^{-2}\Gamma^{-1}\tau \parallel \tau$.

[†] The writer has not happened to meet with the geometrical proof of this known theorem, which is attributed to M. Bertrand by M. Liouville, in page 558 of the already cited Additions to Monge; but the deduction of it as above, from the fundamental property (396) of the rectifying line, is sufficiently obvious, and appears to have suggested the method employed by M. de Saint-Venant, in the part (p. 26) of his Memoir sur les lignes courbes non planes, &c., before referred to, in which the result is enunciated. Another, and perhaps even a simpler method, suggested by quaternions, of geometrically establishing the same theorem, will be sketched in the present sub-article (49.); and in the following sub-article (50.), a proof by the quaternion analysis will be given, which seems to leave nothing to be desired on the side of simplicity of calculation.

the binormal to the curve in space make (in the same case) constant angles, with the fixed radius drawn to that point: and the curve itself is therefore (as before) a geodetic line, on some cylindrical surface.

(50.) By quaternions, when the *two curvatures* have thus a *constant ratio*, the equations XI'. and XVI. give,

$$\text{CVIII.} \quad (r\lambda)' = (\mathbf{U}\nu + r\mathbf{r}^{-1}\tau)' = (r\mathbf{r}^{-1})'\tau = 0,$$

or

CIX. . .
$$r\lambda = a$$
 constant vector;

the tangent (τ) makes therefore, in this case, a constant angle (H) with a constant line $(r\lambda)$: and the curve is thus seen again, by this very simple analysis, to be a geodetic on a cylinder. And because it is easy to prove (comp. XXXI.), that we have in the same case the expression,

CX... $r \sin^2 H = radius$ of curvature of base,

or of the section of the cylinder made by a plane perpendicular to the generating lines, this other known theorem results, with which we shall conclude the present series of sub-articles: When both the curvatures are constant, the curve is a geodetic on a right circular cylinder (or cylinder of revolution); or it is what has been called above, for simplicity and by eminence, a helix.*

398. When the *fourth power* (s⁴) of the arc is taken into account, the expansion of the vector ρ_s involves another term, and takes the form (comp. 397, I.),

I... $\rho_s = \rho + s\tau + \frac{1}{2}s^2\tau' + \frac{1}{6}s^3\tau'' + \frac{1}{24}s^4\tau''',$ in which II... $\tau''' = D_s^4\rho$, and III... $S\tau\tau''' = -3S\tau'\tau'' = -3r^{-3}r';$

so that the new affections of the curve, thus introduced, depend only on two new scalars, such as r' and r'', or r' and R', or H' and P', &c. We must be

^{*} In general, the expression XLIV. for the vector ω_s of the osculating helix, in which $\iota = -r^{-1}\lambda^{-1} = \tau - \lambda^{-1}\tau'$, and $\rho - \omega_0 = \lambda^{-2}\tau'$, gives ' $\mathbf{T}\omega'_s = 1$; so that the deviation (8.) may be considered (comp. (13.)) to be measured from the extremity of an arc of the helix, which is equal im length to the arc s of the eurve, and is set off from the same initial point r, with the same initial direction : while ω_0 does not here denote the value of ω_s answering to s = 0, but has a special signification assigned by the formula XXXVIII. It may also be noted that the conception, referred to in (46.), of an auxiliary spherical curve, corresponds to the ideal substitution of the motion of a point with a varying velocity upon a sphere, for a motion with an uniform velocity in space, in the investigation of the general properties of curves of double curvature : and that thus it is intimately connected (comp. 379, (9.)) with the general theory of hodographs.

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FOURTH POWER OF ARC.

content to offer here a very few remarks on the theory of *such* affections, and on the manner in which it may be extended by the introduction of derivatives of *higher orders*.

(1.) The new vector τ''' , on which everything here depends, is easily reduced to the following forms,* analogous to the expressions 397, VI. for τ'' :

$$IV...\tau''' = \frac{r(r^{-3})'}{\tau} + \frac{(r^{-3}r')' - \tau''^{2}}{\tau'} - \frac{(r^{-2}r^{-1})'}{\nu} = 3r^{-3}r'\tau + (r(r^{-1})'' + \lambda^{2})\tau' + (r^{-2}r^{-1})'r^{2}\nu.$$

(2.) The first derivatives of the four vectors, ν' , κ' , λ , σ , taken in like manner with respect to the arc s of the curve, are the following:

$$\begin{aligned} \mathbf{V}... \, \mathbf{\nu}'' &= \, (\nabla \tau r'')' = \nabla \tau r''' + r^{-2} \lambda \\ &= r^{-2} \mathbf{r}^{-1} \tau + (r^{-2} \mathbf{r}^{-1})' \tau'^{-1} + (r(r^{-1})'' - \mathbf{r}^{-2}) \nu ; \\ \mathbf{VI}... \, \mathbf{\kappa}'' &= -r^{-1} r' \tau + (r r'' - r^{2} \mathbf{r}^{-2}) \tau' + (r^{2} \mathbf{r}^{-1})' \nu ; \\ \mathbf{VII}... \, \lambda' &= \, (\mathbf{r}^{-1})' \tau + (r^{-1})' r \nu, \text{ or } \, \mathbf{VII'}... (r \lambda)' = (r \mathbf{r}^{-1})' \tau (\text{comp. 397, CVIII.}) ; \\ \mathbf{VIII}... \, \sigma' &= \, (\mathbf{\kappa} + p r \nu)' = (p' + r \mathbf{r}^{-1}) r \nu = R R' p^{-1} r \nu ; \end{aligned}$$

in which last the scalar derivatives p' and R' are determined, in terms of r'' and r', by the equations,

and

IX...
$$p' = (r'\mathbf{r})' = r''\mathbf{r} + r'\mathbf{r}',$$

X... $R' = R^{-1}(pp' + rr') = p' \sin P + r' \cos P = (p' + \cot H) \sin P$.

We have also the derivatives,

XI...
$$H' = \frac{r\mathbf{r}' - r'\mathbf{r}}{r^2 + \mathbf{r}^2} = \frac{r^{-1}r' - \mathbf{r}^{-1}\mathbf{r}'}{r\mathbf{r}\lambda^2},$$

and the relations,

XIII. . .
$$S\tau\tau'\tau''' = S\nu\tau''' = -(r^{-2}r^{-1})';$$

XIV. . . $S\tau\tau''\tau''' = S\nu'\tau''' = -r^{-3}r^{-2}(p'-r\tau\lambda^2);$
XV. . . $S\tau'\tau''\tau''' = r^{-2}S\lambda\tau''' = -r^{-5}(rr^{-1})';$

XII... $P' = \frac{rp' - r'p}{r^2 + p^2} = \frac{(rr'' - r'^2)\mathbf{r} + rr'\mathbf{r}'}{R^2};$

^{*} In these new expressions, on the plan of the second Note to page 90, the scalars r', p', R', and the vector σ' , are to be regarded as of the dimension zero; r'', H', P', and κ'' of the dimension -1; λ' of the dimension -2; and r'', and τ''' , as being each of the dimension -3.

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which may be proved in various ways, and by the two first (or the two last) of which, the derivatives \mathbf{r}' and p', and therefore also H' and P', can be separately calculated, as scalar functions of the four vectors τ , τ' , τ'' , τ''' , or of some three of them, including the new vector τ''' .

(3.) We may also deduce, from either V. or VIII., the following vector expressions, of which the geometrical signification is evident from the recent theory (396, 397) of emanant lines and planes:

XVI... Vector of Rotation of Radius (R) of Spherical Curvature

= Vector of Rotation of Tangent Plane to Osculating Sphere

$$= (say) \phi = \nabla \frac{\nu''}{\nu'} = \nabla \frac{\sigma' - \tau}{\sigma - \rho} = R^{-2} \tau (\nu^{-1} \sigma' + \sigma - \rho)$$
(1, 2, 3)

$$= \frac{\tau}{R} \left(\frac{rR'}{p} + \frac{\sigma - \rho}{R} \right) = \frac{r\tau}{R^2} \left(p' + \frac{r}{r} + r\tau' + p\nu \right) = R^{-2}r(r\lambda + p'\tau - p\tau') ; (4, 5, 6)$$

whence follows this tensor value for the common angular velocity of these two connected rotations, compared still with the velocity of motion along the curve,

XVII... Velocity of Rotation of Radius (R), or of Tangent Plane to Sphere,
=
$$T\phi = TV \frac{\nu''}{\nu'} = R^{-1} \sqrt{(1 + R'^2 \cot^2 P)} = R^{-1} \sqrt{\{1 + (p' + \cot H)^2 \cos^2 P\}};$$

with the verifications, for the case of the *helix*, for which p = 0, p' = 0, P = 0, and R = r, that these expressions XVI. and XVII. become,

XVI'... $\phi = \lambda$, and XVII'... $T\phi = T\lambda = r^{-1}$ cosec H,

which agree with those found before, for the vector and velocity of rotation of the radius (r) of absolute curvature.

(4.) As another verification, we have R' = 0 for every spherical curve, and the general expressions take then the forms,

XVI''...
$$\phi = \frac{-\tau}{\sigma - \rho}$$
, and XVII''... $T\phi = R^{-1}$,

of which the interpretation is easy.

(5.) In general, the formula XVII. may also be thus written,

XVIII. . . $R^2 \phi^2 + 1 = -R'^2 \cot^2 P = R'^2 - p^{-2} R^2 R'^2 = R'^2 + \sigma'^2 = \sigma'^2 \cos^2 P$; or thus,

XIX... $RT\phi = \sqrt{(1 + T\sigma'^2 \cos^2 P)} = \sqrt{(1 + T\sigma'^2 - R'^2)};$

ROTATION OF RADIUS R.

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or finally,

XX... $R^{2}T\phi = \sqrt{(R^{2} - r^{2}\sigma'^{2})} = \sqrt{(R^{2} + r^{2}T\sigma'^{2})};$

so that the small angle, $sT\phi$, between the two near radii of spherical curvature, R and R_s , is ultimately equal to the square root of the sum of the squares of the two small angles, in two rectangular planes, sR^{-1} and $rsR^{-2}T\sigma'$, or PSPs and SPSs, which are subtended, respectively, at the centre s of the osculating sphere by the small arc s of the given curve, and at the given point P by the small corresponding arc $sT\sigma'$ of the locus of centre s of spherical curvature, or of the cusp-edge (395, (2.)) of the polar developable; exactly* as the small angle $sT\lambda$, between two near radii (397, (5.)) of absolute curvature, r and r_s , is ultimately the square root of the sum of the squares of the two other small angles, sr^{-1} and sr^{-1} , or PKPs and KPKs, which are likewise situated in two rectangular planes, and are subtended at the centre κ of the osculating circle by the small arc s of the curve, and at the given point P by the small are s of the curve, and at the given point P by the corresponding arc $sT\kappa'$ of the locus of the centre κ (comp. 397, XXXIV., XCIV.).

(6.) The point, say v, in which the radius R of the osculating sphere at P approaches most nearly to the near radius R_s from P_s , is ultimately determined (comp. 397, CV. and X.) by the formula,

XXI...
$$PV = \zeta = \frac{Vector \ of \ Spherical \ Curvature}{Square \ of \ Angular \ Velocity \ of \ Radius \ (R)}$$

$$= (\rho - \sigma)^{-1} T \phi^{-2} = \frac{\sigma - \rho}{1 + R'^2 \cot^2 P} = \frac{\sigma - \rho}{1 + p^{-2} r^2 R'^2};$$

the vector of this point v (in its ultimate position) is therefore

XXII... ov =
$$\rho + \zeta = \frac{r^2 R'^2 \rho + p^2 \sigma}{r^2 R'^2 + p^2} = \frac{r^2 R'^2 \rho + r^2 r'^2 \sigma}{r^2 R'^2 + r^2 r'^2};$$

with the verification, that (by X., comp. XVII.) the scalar $p^{-1}rR'$ or R' cot P reduces itself to cot H, or to rr^{-1} , for the case p = 0, p' = 0, P = 0 (comp. (3.)): and that thus the expression 397, XXXVIII., for the vector of of the point of nearest approach, of a radius (r) of absolute curvature to a consecutive \dagger radius of the same kind, is reproduced.

^{*} It will soon be seen that these two results, and others connected with them, depend geometrically on one common principle, which extends to all systems of normal emanants (397, (44.)).

⁺ This usual expression, consecutive, is obviously borrowed here from the language of infinitesimals, but is supposed to be interpreted, like those used in other parts of the present series of Articles, by a reference to the conception of limits.

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(7.) In general, if we introduce a *new auxiliary angle*, J, determined by the formula,

XXIII...
$$\cot J = p^{-1}rR' = R' \cot P = (p' + \cot H) \cos P = R(r^{-1} + P'),$$

the expression XXII. takes the simplified form (comp. again 397, XXXVIII.),

XXIV...
$$ov = \rho + \zeta = \rho \cos^2 J + \sigma \sin^2 J;$$

and the segments, into which the point v divides (internally) the radius R of the sphere, have the values (comp. 397, XXXIX.),

$$XXV...\overline{PV} = R \sin^2 J, \quad \overline{VS} = R \cos^2 J.$$

(8.) A geometrical signification may be assigned for this new angle J, which is analogous to the known signification of the angle H (397, XVII.). In fact, the tangent plane to the osculating sphere at P touches its own developable envelope along a new right line, of which the scalar equations are,

XXVI... $S(\sigma - \rho) (\omega - \rho) = 0$, $S(\sigma' - \tau) (\omega - \rho) = 0$;

and because the developable locus of all such lines can be shown to be circumscribed, along the given curve, to the locus of the osculating circle, which is at the same time the envelope of the osculating sphere, we shall briefly call this locus of the line XXVI. the Circumscribed Developable. And the inclination of the generatrix of this new developable surface, to the tangent to the given curve at P, if suitably measured in the tangent plane to the sphere, is precisely the angle which has been above denoted by J.

(9.) To render this conception more completely clear, let us suppose that a finite right line PJ is set off from the given point P, on the indefinite line XXVI., so as to represent, by its length and direction, the velocity of the rotation of the tangent plane to the osculating sphere; and so to be, in the phraseology (396, (14.)) of the general theory of emanants, the vector-axis of that rotation. We shall then have the values,

XXVII... PJ =
$$\phi$$
 (= the six expressions XVI.)
= $R^{-1}\tau(\cot J + U(\sigma - \rho)) = R^{-1} \operatorname{cosec} J(\tau \cos J + \tau U(\sigma - \rho) \sin J);$ (7,8)

the angle J being determined by the formula XXIII., and a new expression, $T\phi = R^{-1}$ cosec J, being thus obtained for the velocity XVII.

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(10.) Hence the new angle J, if conceived to be included (like H) between the limits 0 and π , may be considered to be measured from τ to ϕ , or from the unit-tangent to the curve at P, to the generating line PJ of the circumscribed developable (8.), in the direction from τ to $\tau(\sigma - \rho)$: which last tangent to the osculating sphere makes generally, like the tangent ϕ or PJ itself, an acute angle with the positive binormal ν , as appears from the common sign of the scalar coefficients of that vector, in their developed expressions.

(11.) It may also be remarked, as an additional point of analogy, and as serving to verify some formulæ, that while the older angle H becomes right, when the given curve is plane, so the new angle $J = \frac{\pi}{2}$, for every spherical curve.

(12.) As another geometrical illustration of the properties of the angle J, and of some other results of recent sub-articles, which may serve to connect them, still more closely, with the general theory of normal emanants from curves (397, (44.)), let us conceive that AB, BC, CD are three successive right lines, perpendicular each to each; let us denote by a and b the angles BCA and CBD, and by c the inclination of the line AD to BC: and let us suppose that these two lines are intersected by their common perpendicular in the points G and H respectively.

(13.) Then, by completing the rectangle BCDE, and letting fall the perpendicular BF on the hypotenuse of the right-angled triangle ABE, we obtain the projections, AE and FB, of the two lines AD and GH, on the plane through B perpendicular to BC; and hence, by elementary reasonings, we can infer the relations :

and

XXVIII. . . $\tan^2 c = \tan^2 ADE = \tan^2 a + \tan^2 b$;

XXIX... $\frac{BH}{BC} = \frac{AG}{AD} = \frac{AF}{AF} = \frac{AB^2}{AF^2} = \sin^2 AEB,$

or

XX1X'... BH = BC $\sin^2 j$, if $\tan j = \tan a \cot b$;

nothing here being supposed to be *small*. It may also be observed, that the *two rectilinear angles*, BCA and CBD, or a and b, represent respectively the inclinations of the *plane* ACD to the *plane* BCD, and of the plane ABD to the plane ABC.

(14.) Conceive next that PQ and $P_{s}Q_{s}$ are two near normal emanants, touching the polar developable in the points Q and Q_{s} , where of Q is thus on

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the given polar axis KS, and Q_s is on the near polar axis K_sQ_s ; and let the second emanant be cut, in the points P' and Q', by planes through P and Q, perpendicular to the first emanant PQ. The line PP' will then be very nearly tangential to the given curve at P; and the line QQ' will be very nearly situated in the corresponding normal plane to that curve : so that these two new lines will be very nearly perpendicular to each other, and the gauche quadrilateral P'PQQ' will ultimately have the properties of the recently considered quadrilateral ABCD.

(15.) This being perceived, if we denote by e the length of the emanant line PQ, the small angle a is very nearly $= e^{-1}s$; and if the small angle b be put under the form b's, then the new coefficient b' is ultimately equal (by XX1X'.) to $e^{-1} \cot j$: where j is an auxiliary angle, not generally small, and is such that we have ultimately PH = PQ. $\sin^2 j$, if H be the point in which the given normal emanant PQ approaches most closely to the consecutive emanant P_sQ_s .

(16.) We have then the ultimate equation,

XXX...
$$\cot j = eb' = \overline{PQ} \times \lim_{s \to \infty} (s^{-1} \cdot QPQ_s)$$

= length of emanant line (PQ)
 \times angular velocity of the tangential plane (P'PQ) containing it;

this latter plane being here conceived as *turning*, for a moment, round the tangent to the given curve at P, and the velocity of *motion* along that curve being still taken for unity.

(17.) Accordingly, when we change e to r, b' to r^{-1} , and j to H, we recover in this way the fundamental value cot $H = rr^{-1}$ (397, XVII.), for the cotangent of the *older* angle H; and when, on the other hand, we treat the radius of *spherical* curvature as the normal emanant, supposing a to coincide with s, and therefore changing e to R, and b' to $r^{-1} + P'$, we recover the last of the expressions XXIII. for the cotangent of the *new* but analogous angle J, namely cot $J = R(r^{-1} + P')$, together with an *interpretation*, which may not have at first seemed obvious : although that expression *itself* was deducible, in the following among other ways, from equations previously established,

XXXI...
$$R^{-1}$$
 eot $J - \mathbf{r}^{-1} = \frac{rR'}{pR} - \frac{r'}{p} = -\frac{R}{p} \left(\frac{r}{R}\right)' = -\frac{(\cos P)'}{\sin P} = P'.$

(18.) As regards the angular velocity, say v, of the emanant line PQ, or the ultimate quotient of the angle between two such near lines, divided by

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the small arc s of the given curve, we see by XXVIII. (comp. (5.)) that this small angle vs is ultimately equal to the square root of the sum of the squares of the two other small angles, above denoted by a and b, and found to be equal, nearly, to $e^{-1}s$ and $e^{-1}s$ cot j respectively: we may then establish the general formula,

XXXII... Angular Velocity of Normal Emanant = $v = e^{-1} \operatorname{cosec} j$;

which reproduces the values, r^{-1} cosec H, and R^{-1} cosec J, already found for the angular velocities of the two radii, r and R.

(19.) And if we observe that the projection of the vector of curvature, \mathbf{KP}^{-1} , on the emanant PQ, is easily proved to be = $\mathbf{QP}^{-1} = e^{-2} \cdot \mathbf{PQ}$, we see by XXXII. that if this projection be divided by the square of the angular velocity (v) of the line PQ, the quotient is the line PQ $\cdot \sin^2 j$, or PH (15.): which reproduces the general result, 397, CV., for all systems of normal emanants, together with a geometrical interpretation.

(20.) As still another geometrical illustration of the properties of the new angle J, we may observe that in the construction (12.) and (13.) the corresponding auxiliary angle j was equal to AEB, or to ABF, and that the line BF (= HG) was perpendicular to both BC and AD, although not intersecting the latter. Substituting then, as in (14.), the quadrilateral P'PQQ' for ABCD, and passing to the limit, we may say that if a new line PJ be a common perpendicular, at the given point P, to two consecutive* normal emanants, PQ and P'Q', the general auxiliary angle j is simply the inclination P'PJ, of that common perpendicular PJ, to the tangent PP' to the curve.

(21.) And if, instead of normally emanating lines PQ, we consider a system of tangential emanant planes (as in 397, (45.)), to which those lines are perpendicular, we may then (comp. 396, (14.)) consider the recent line rs as being a generating line of the developable surface, which is the envelope of all the planes of the system; the auxiliary angle, $\dagger j$, is therefore generally by (20.) the inclination of this generatrix to the tangent: a result which agrees with, and includes, the known and fundamental property (397, XVII.) of the angle H, in connexion with the Rectifying Developable (396); and also

^{*} Compare the second Note to page 115.

[†] In these geometrical illustrations, the angle j has been treated, for simplicity, as being both positive and acute; although the general formulæ, which involve the corresponding angles H and J, permit and require that we should occasionally attribute to them obtuse (but still positive) values: while those angles may also become right, in some particular cases (comp. (11.)).

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the analogous property of the newer angle J, connected (8.) with what it has been above proposed to call the *Circumscribed Developable*.

(22.) We shall soon return briefly on the theory of that new developable surface (8.), and of the new locus (of the osculating circle, or envelope of the osculating sphere) to which it has been said to be circumscribed : but may here observe, that if we write for abridgment (comp. VIII. and XXIII.),

XXXIII...
$$n = \frac{\sigma'}{r\nu} = \frac{RR'}{p} = p' + \cot H = \cot J \sec P$$
,

then what has been called the *coefficient of non-sphericity* (comp. 395, (14.) and (16.)) is easily seen to have by XIV. the values,

XXXIV...
$$S - 1 = \frac{S\tau^{3}\tau''\tau''}{S\tau\tau'^{3}\tau''} - 1 = -r^{4}rS\nu'\tau''' - 1$$
 (1, 2)

$$= \frac{r}{r} (p' - rr\lambda^2) - 1 = \frac{r}{r} \left(p' + \frac{r}{r} \right) = nrr^{-1} \quad (3, 4, 5)$$

$$= \frac{\sigma'}{r\nu} = \cot H \cot J \sec P = \frac{rRR'}{pr}; \qquad (6, 7, 8)$$

whence also the *deviation* of a near point P_s of the curve, from the osculating sphere at P, is ultimately (by 395, XXVII.).

XXXV...
$$\overline{sP}_s - \overline{sP} = \frac{(S-1)s^4}{24r^2R} = \frac{ns^4}{24r\mathbf{r}R} = \frac{R's^4}{24r\mathbf{r}p};$$

and accordingly, the square of the vector $\rho_s - \sigma$ is given now (comp. I.) by the expression,

$$(\rho_s - \sigma)^2 = (\rho - \sigma)^2 - \frac{s^4}{12r^2} \{r^2 S(\sigma - \rho)\tau''' - 1\},$$

in which

$${}^{2}S(\sigma - \rho)\tau'' = S = 1 + n\tau^{-1} = \&c., as above.$$

(23.) The same auxiliary scalar n enters into the following expressions for the arc, and for the scalar radii of the first and second curvatures, of the locus of the centre s of the osculating sphere, or of the cusp-edge of the polar developable (comp. 391, (6.), and 395, (2.)):

XXXVI...
$$\pm \int n ds = Arc \text{ of that } Cusp-Edge \text{ (or of locus of s)};$$

XXXVI'... $r_1 = n\mathbf{r} = r + p'\mathbf{r} = \frac{RR'}{r'} = (Sealar)$ Radius of Curvature of same edge; XXXVI''... $\mathbf{r}_1 = nr = \sigma' \boldsymbol{\nu}^{-1} = (Sealar)$ Radius of Second Curvature of same curve;

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these two latter being here called scalar radii, because the first as well as the second (comp. 397, V.) is conceived to have an algebraic sign. In fact, if we denote by κ_1 the centre of the osculating circle to the cusp-edge in question, its vector is (by the general formula 389, IV.),

XXXVII...
$$OK_1 = \kappa_1 = \sigma + \frac{\sigma'^3}{V\sigma''\sigma'} = \sigma - mr\tau' = \rho - p'rr\tau' + prv = \sigma - r_1r\tau',$$

with the signification XXXVI'. of r_1 ; because by XXXIII. (comp. 397, XI'.),

XXXVIII. . . . $\sigma' = nr\nu$, $\sigma'' = n'r\nu + n(r\nu)' = n'r\nu - nrr^{-1}\tau'$,

and therefore

XXXIX... $\sigma^2 = -n^2$, $\nabla \sigma' \sigma'' = n^2 r^{-1} \tau$.

We may also observe that the relation $\sigma' \parallel \nu$ gives (by 397, IV.),

XL...
$$\nabla \frac{\sigma''}{\sigma'} = \nabla \frac{\nu'}{\nu} = r^{-1}r = Vector \text{ of Second Curvature of given curve };$$

and that we have the equation,

XLI.
$$\ldots \frac{\mathbf{K}_{1}\mathbf{S}}{\mathbf{P}\mathbf{K}} = \frac{\sigma - \kappa_{1}}{\kappa - \rho} = \frac{r_{1}}{r}, \text{ with } r > 0, \text{ but } r_{1} > \text{or } < 0,$$

according as the cusp-edge turns its concavity or its convexity towards the given curve at P.

(24.) The radius of (first) curvature of that cusp-edge, when regarded as a *positive* quantity, is therefore represented by the *tensor*,

XLII...
$$\sqrt{r_1^2} = \pm r_1 = \mathrm{T}r_1 = R\mathrm{T}\frac{R'}{r'} = \pm \frac{R\mathrm{d}R}{\mathrm{d}r} (>0);$$

and as regards the scalar radius XXXVI". of second curvature of the same cusp-edge, its expression follows by XXXVIII. from the general formula 397, XXVII., which gives here,

XLIII. . .
$$\mathbf{r}_1^{-1} = S \frac{\sigma'''}{V \sigma' \sigma''} = \frac{1}{m} S \frac{\nu''}{V \nu \nu'} = n^{-1} r^{-1}$$
, because XLIII'. . . $S \frac{\nu''}{V \nu \nu'} = 1$;

the two scalar derivatives, n' and n'', which would have introduced the derived vectors τ^{iv} and τ^{v} , or $D_s{}^{5}\rho$ and $D_s{}^{6}\rho$, of the *fifth* and *sixth* orders, R

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thus disappearing from the expressions of the two curvatures of the locus of the centre s of the osculating sphere, as was to be expected from geometrical* considerations.

(25.) For the helix, the formula XXXVII. gives $\kappa_1 = \rho$, or $\kappa_1 = P$; we have then thus, as a verification, the known result, that the given point P of this curve is itself the centre of curvature κ_1 of that other helix (comp. 389, (3.), and 395, (8.)), which is in this case the common locus of the two coincident centres, κ and s. It is scarcely necessary to observe that for the helix we have also J = H.

(26.) In general, the rectifying plane of the locus of s is parallel to the rectifying plane of the given curve, because the radii of their osculating circles are parallel; the rectifying lines for these two curves are therefore not only parallel but equal; and accordingly we have here the formula,

XLIV. . .
$$\lambda_1 = \nabla \frac{\tau_1^{\prime\prime}}{\tau_1^{\prime}} = \nabla \frac{\tau^{\prime\prime}}{\tau^{\prime}} = \lambda$$
 (by 397, XVI.),

which will be found to agree with this other expression (comp. 397, XVII.),

XLV...
$$\tan H_1 = \frac{\mathbf{r}_1}{\mathbf{T}\mathbf{r}_1} = \frac{\mathbf{r}}{\mathbf{r}}\mathbf{U}\mathbf{r}_1 = \pm \cot H,$$

the upper or lower sign being taken, according as the new curve is concave (as in figs. 81, 82 [pp. 100, 106]), or is convex at s (comp. (23.)), towards the old (or given) curve at \mathbf{r} : and the new angle H_1 being measured in the new rectifying plane, from the new tangent σ' or nr_{ν} , to the new rectifying line λ_1 , and in the direction from that new tangent to the new binormal ν_1 , or (comp. XL.) to a line from s which is equal to the vector of second curvature $\mathbf{r}^{-1}\tau$ of the given curve, multiplied by a positive scalar, namely by Tn^{-1} , or by the coefficient n^{-1} taken positively.

(27.) The former rectifying line λ touches the cusp-edge of the rectifying developable (396) of the given curve, in a new point κ (comp. fig. 81), of which by 397, (45.), and by XV., the vector from the given point is, generally,

XLVI... PR =
$$-\frac{\nabla \tau'^{3} \tau''}{S \tau' \tau'' \tau''} = \frac{r^{-2} \lambda}{S \lambda \tau''} = -\frac{r \lambda}{(r r^{-1})'} = \frac{U \lambda \sin H}{H'};$$

[•] In fact, *n* represents here the velocity of motion of the point s along its own locus, while r^{-1} and r^{-1} represent respectively the velocities of rotation of the tangent and binormal to that curve: so that *nr* and *nr* must be, as above, the radii of its two curvatures.

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with the verification that this expression becomes infinite (comp. 397, (49.), (50.)), when the curve is a geodetic on the cylinder.

(28.) In general, the vector OR of the *point of contact* R, which vector we shall here denote by v, may be thus expressed,

XLVII...
$$v = OR = \rho + lU\lambda$$
, if XLVIII... $l = \frac{\sin H}{H'} = \frac{-rT\lambda}{(rr^{-1})'}$;

and because $(r\lambda)' = (rr^{-1})'\tau$, by VII'., its first derivative is,

XLIX...
$$v' = r\lambda \left(\frac{v-\rho}{r\lambda}\right)' = U\lambda \operatorname{cosec} H(l \sin H)' = U\lambda(l' + \cos H);$$

in which however the new derived scalar l' involves H'', and so depends on τ^{1v} : while the scalar coefficient l itself represents the portion $(\pm \overline{PR})$ of the rectifying line, intercepted between the given curve, and the cusp-edge (27.) of the rectifying developable, and considered as positive when the direction of this intercept PR coincides with that of the line $+\lambda$, but as negative in the contrary case.

(29.) For abridgment of discourse, the cusp-edge *last* considered, namely that of the *rectifying developable*, as being the locus of a point which we have denoted by the letter R, may be called simply "the curve (R)"; while the *former* cusp-edge (23.), or that of the *polar* developable, may be called in like manner "the curve (s)"; the *locus* of the centre K of (absolute) curvature may be called "the curve (K)": and the given curve itself (comp. again figs. 81, 82) may be called, on the same plan, "the curve (P.)."

(30.) The arc RRs, of the curve (R), is (by XLIX., comp. XXXVI.),

L. . .
$$\pm \int_0^s \mathbf{T} \boldsymbol{v}' \mathrm{d}s = l_s - l + \int_0^s \cos H \mathrm{d}s$$
;

this arc being treated as positive, when the direction of motion along it coincides with that of $+\lambda$.

(31.) The expression VII. for λ' , combined with the former expression 397, XVI. for λ , gives easily by the general formula 389, IV.,

LI... Vector of Centre of Curvature of the Curve (R)

$$u = v + \frac{v'}{Vv''v'^{-1}} = v + \frac{v'}{V\lambda'\lambda^{-1}} = v + \frac{v'}{H'}Ur';$$

R 2

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whence

LII. . . Radius of Curvature of Curve
$$(R) = T \frac{v'}{H'} = T \frac{dv}{dH}$$

the scalar variable being here arbitrary.

(32.) We see, at the same time, that the angular velocity of the rectifying line λ , or of the tangent to this curve (R), is represented by $\pm H'$; or that the small angle^{*} between two such near lines, λ and λ_s , is nearly equal to sH', or to $H_s - H$: while the vector axis $(\nabla \lambda' \lambda^{-1})$ of rotation of the rectifying line, set off from the point R, has $- H' U\tau'$, or $- H' r\tau'$, for its expression.

(33.) As regards the second curvature of the same curve (R), we may observe that the expression (comp. VII. and LI.),

LIII...
$$\lambda'' = (\mathbf{r}^{-1})'' \mathbf{r} + (r^{-1})'' \mathbf{r} \mathbf{v} + r^{-1} (r \mathbf{r}^{-1})' \mathbf{\tau}' = (\mathbf{r}^{-1})'' \mathbf{\tau} + (r^{-1})'' r \mathbf{v} + \nabla \lambda \lambda',$$

combined with the parallelism (XLIX.) of v' to λ , gives, by the general formula 397, XXVII.,

LIV... Radius of Second Curvature of Curve (R)

$$= \left(\mathbf{S} \frac{\boldsymbol{\nu}^{\prime\prime\prime\prime}}{\nabla \boldsymbol{\nu}^{\prime} \boldsymbol{\nu}^{\prime\prime}}\right)^{-1} = \frac{\boldsymbol{\nu}^{\prime}}{\lambda} \left(\mathbf{S} \frac{\lambda^{\prime\prime}}{\nabla \lambda \lambda^{\prime}}\right)^{-1} = \frac{\boldsymbol{\nu}^{\prime}}{\lambda} = \frac{l^{\prime} + \cos H}{T\lambda};$$

with the verification, that while $l' + \cos H$ represents, by (30.), the velocity of motion along this curve (R), T λ represents, by 397, (3.), the velocity of rotation of its osculating plane, namely the rectifying plane of the given curve (P): and it is worth observing, that although each of these two radii of curvature, LII. and LIV., depends on τ^{IV} through l' (28.), yet neither of them depends on τ^{V} (comp. (24.)). As another verification, it can be shown that the plane of the two lines λ and τ' from P, namely the plane,

LIV'. . .
$$S\tau'\lambda(\omega-\rho)=0$$
,

which is the normal plane to the rectifying developable along the rectifying line, and contains the absolute normal to the given curve (P), touches its own developable envelope along the line RH, if H be the point determined by

^{*} A result substantially equivalent to this is deduced, by an entirely different analysis, in the above cited Memoir of M. de Saint-Venant, and is illustrated by geometrical considerations: which also lead to expressions for the two curvatures (or, as he calls them, the *courbure* and *cambrure*), of the cusp-edge of the rectifying developable; and to a determination of the *rectifying line* of that *cusp-edge*.

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the formula 397, XXXVIII., or the point of nearest approach of a radius of curvature (r) of that given curve to its consecutive (comp. (6.)); this line RH must therefore be the rectifying line of the curve (R); and accordingly (comp. 397, XVII.), the trigonometric tangent of its inclination to the tangent RP to this last curve has for expression (abstracting from sign),

LIV"... tan PRH =
$$\overline{PH}$$
 : $\overline{PR} = \pm t^{-1}r \sin^2 H = \pm rH' \sin H = T\lambda^{-1}H'$
Radius (LIV.) of Second Curvature of Curve (

= Radius (LIV.) of Second Curvature of Curve (R) Radius (LII.) of First Curvature of same Curve

(34.) Without even introducing τ^{1v} , we can assign as follows a *twisted* cubic (comp. 397, (34.)), which shall have contact of the fourth order with the given curve at **P**; or rather an *indefinite variety* of such cubics, or gauche curves of the *third degree*. Writing, for abridgment,

LV...
$$x = -S\tau(\omega - \rho), \quad y = -Sr\tau'(\omega - \rho), \quad z = -Sr\nu(\omega - \rho),$$

so that

$$\mathbf{L}\nabla\mathbf{I}...\omega = \rho + x\tau + yr\tau' + sr\nu,$$

the scalar equation,

LVII. . .
$$\left(\frac{2\mathbf{r}y}{r}\right)^2 = 6\left(\frac{\mathbf{r}}{r}\right)^3 xz + \left(\frac{\mathbf{r}^3}{r^2}\right)' yz + ez^2$$
,

in which e is an arbitrary but scalar constant, represents evidently, by its form, a cone of the second order, with its vertex at the given point \mathbf{r} ; and this cone can be proved to have contact of the fourth order with the curve* at that point: or of the third order with the cone of chords from it (comp. 397, (31.), (32.)). In fact the coefficients will be found to have been so determined, that the difference of the two members of this equation LVII. contains s^6 as a factor, when we change ω to ρ_s , as given by the formula I., or when we substitute for xyz their approximate values for the curve, as functions of the

[•] In the language of infinitesimals, the cone LVII. contains five consecutive points of the curve, or has five-point contact therewith: but it contains only four consecutive sides of the cone of chords from the given point, or has only four-side contact with that cone, except for one particular value of the constant, e, which we shall presently assign. It may be observed that xyz form here a (scalar) system of three rectangular coordinates, of the usual kind, with their origin at the point P of the curve, and with their positive semiaxes in the directions of the tangent τ , the vector of curvature τ' , and the binormal ν .

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arc s; namely, by the expressions IV. for τ'' , and 397, VI. for τ'' ,

LVIII. . .
$$\begin{cases} x_s = s - \frac{s^3}{6r^2} + \frac{r's^4}{8r^3}, \\ y_s = \frac{s^2}{2r} - \frac{r's^3}{6r^2} - \frac{s^4}{24}((r^{-2}r')' + r^{-3} + r^{-1}r^{-2}), \\ z_s = \frac{s^3}{6rr} + \frac{rs^4}{24}(r^{-2}r^{-1})'; \end{cases}$$

where the terms set down are more than sufficient for the purpose of the It may be added that the coefficient of $\frac{-s^4}{24}$ in y_s , which is the only proof. one at all complex here, may be transformed as follows :

LVIII'...
$$Sr\tau'\tau''' = -(r^{-1})'' - r^{-1}\lambda^2 = r^{-3}S + p(r^{-2}r^{-1})';$$

S being that scalar for which (or more immediately for its excess over unity). several expressions* have lately been assigned (22.), and which had occurred in an earlier investigation (395, (14.), &c.).

(35.) With the same significations LV. of the three scalars xyz, this other equation,

or

LIX...
$$18ry - (3x - r'y)^2 = (9 + r'^2 - 3rr'' - 3r^2r^2)y^2$$
,
LIX'... $2ry - (x - \frac{1}{3}r'y)^2 = (1 - \frac{1}{2}r^{\frac{4}{3}}(r^2)'' - \frac{1}{3}r^2r^{-2})y^2$,

will be found to be satisfied when we substitute for x and y the values LVIII. of x_s and y_s , and neglect or suppress s^5 ; it therefore represents an elliptic (or hyperbolic) cylinder, which is cut perpendicularly, by the osculating plane to the given curve at P, in an ellipse (or hyperbola), having contact of the fourth order with the projection (397, (9.)) of that given curve upon that osculating plane: and the cylinder itself has contact of the same (fourth) order with the curve in space, at the same given point P, so that we may call it (comp. 397, (31.)) the Osculating Elliptic (or Hyperbolic) Cylinder, perpendicular to the osculating plane.

(36.) As a verification, if we suppress the second member of either LIX. or LIX'., we obtain, under a new form, the equation of what has

* It might have been observed, in addition to the eight forms XXXIV., that we have also, (9, 10)

XXXIV'. . . $S - 1 = Rr^{-1} \operatorname{cot} J = n \operatorname{cot} H$.

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been already called the Osculating Parabolic Cylinder (397, LXXXIV.); and as another verification, the coefficient of y^2 in that second member vanishes, as it ought to do, when the given curve is supposed to be a parabola: that plane curve, in fact, satisfying the differential equation of the second order,

 \mathbf{or}

LX''...
$$r^{-\frac{2}{3}}\left(\left(\frac{dr}{3ds}\right)^2+1\right) = \text{const.} = p^{-\frac{2}{3}},$$

 $LX...3rr''-r'^2=9$, or $LX'...r^{\frac{4}{3}}(r^{\frac{2}{3}})''=2$,

if r be still the radius of curvature, considered as a function of the arc, s, while p is here the semiparameter.

(37.) The binormal ν is, by the construction, a generating line of the cylinder LIX.; and although this line is not generally a side of the cone LVII., yet we can make it such, by assigning the particular value zero to the arbitrary constant, e, in its equation, or by suppressing the term, ez^2 . And when this is done, the cone LVII. will intersect the cylinder LIX., not only in this common side ν (comp. 397, (33.)), but also in a certain twisted cubic, which will have contact of the fourth order with the given curve at P, as stated at the commencement of (34.).

(38.) But, as was also stated there, *indefinitely many* such cubics can be described, which shall have contact of the same (fourth) order, with the same curve, at the same point. For we may assume any point E of space, or any vector (comp. LVI.),

LXI... OE =
$$\varepsilon = \rho + a\tau + br\tau' + cr\nu$$
,

in which a, b, c are any three scalar constants; and then the vector equation,

LXII. . .
$$\omega = \rho_s + t(\varepsilon - \rho),$$

in which t is a new scalar variable, will represent a cylindric surface, not generally of the second order, but passing through the given curve, and having the line PE for a generatrix. We can then cut (generally) this new cylinder by the osculating plane to the curve at P, and so obtain (generally) a new and oblique projection of the curve upon that plane; the x and y of which new projected curve will depend on the arc s of the original curve by the relations,

LXIII...
$$x = x_s - ac^{-1}z_s, \quad y = y_s - bc^{-1}z_s;$$

with the approximate expressions LVIII. for $x_s y_s z_s$. And if we then

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determine two new scalar constants, B and C, by the condition that the substitution of these last expressions LXIII. for x and y shall satisfy this new equation,

$$LXIV...2ry = x^2 + 2Bxy + Cy^2,$$

if only s^5 be neglected (comp. (35.)), or by equating the coefficients of s^3 and s^4 , in the result of such substitution, then, on restoring the significations LV. of *xyz*, and writing for abridgment,

$$LXV...X = x - ac^{-1}z, \quad Y = y - bc^{-1}z,$$

the equation of the second degree,

$$LXVI...2rY = X^2 + 2BXY + CY^2,$$

will represent generally an oblique osculating elliptic (or hyperbolic) cylinder, which has contact of the *fourth order* with the given curve at \mathbf{P} , and contains the assumed line \mathbf{PE} . If then we determine finally the constant e in LVII., by the result of the substitution of *abc* for *xyz*, or by the condition,

LXVII. . .
$$\left(\frac{2\mathbf{r}b}{r}\right)^2 = 6\left(\frac{\mathbf{r}}{r}\right)^3 ac + \left(\frac{\mathbf{r}^3}{r^2}\right)' bc + ec^2$$
,

the cone LVII., and the cylinder LXVI., will have that line PE for a common side; and will intersect each other, not only in that line, but also (as before) in a twisted cubic, although now a new one, which will have the required (fourth) order of contact, with the given curve at the given point.

(39.) If, after the substitution (38.) in LXIV., we equate the coefficients of the *three powers*, s^3 , s^4 , s^5 , and then eliminate *B* and *C*, we are conducted to an *equation of condition*, which is found to be of the *form*,

LXVIII...
$$ab^3 + bb^2c + cbc^2 + ec^3 = ac(bg + ch);$$

in which the ratios of *abc* still serve to determine the direction of the generating line PE, while the coefficients, a, b, c, e, g, h are *assignable functions* of r, r, r', r'', r'', and r''', depending on the vector τ^{IV} : and when this condition LXVIII. is satisfied, the cylinder LXVI. has contact of the *fifth* order with the given curve at P.

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OSCULATING TWISTED CUBIC.

(40.) Again, if we improve the approximate expressions LVIII. for the three scalars x_s , y_s , z_s , by taking account of s^5 , or by introducing the new term $\frac{s}{120}$ (comp. I.) of ρ_s , and if we substitute the expressions so improved, instead of x, y, z, in the equation of the cone LVII. and then equate to zero (comp. (34.)) the coefficient of s° in the difference of the two members of that equation, we obtain a definite expression for the constant, e, which had been arbitrary before, but becomes now a given function of rrr'r'r" and r" (not involving r'''), namely the following,

LXIX...
$$e = \frac{\mathbf{r}^4}{5} \left(\frac{9}{r^4} - \frac{21}{r^2 \mathbf{r}^2} + \frac{r'^2}{r^4} - \frac{3r''}{r^3} + \frac{3r'\mathbf{r}'}{r^3\mathbf{r}} - \frac{27\mathbf{r'}^2}{4r^2\mathbf{r}^2} + \frac{9\mathbf{r''}}{r^2\mathbf{r}} \right);$$

and when the constant e receives this value,* the cone has contact of the fifth order with the curve at the given point.

(41.) Finally, if we multiply the equation LXVII. by bg + ch, we can at once eliminate a by LXVIII., and so obtain a cubic equation in b:c, which has at least one real root, answering to a real system of ratios a, b, c, and therefore to a real direction of the line PR in (38.). It is therefore possible to assign at least one real cylinder of the second order (39.), which shall have contact of the fifth order with the curve at P, and shall at the same time have one side PE common with the cone of the second order (40.), which has contact of the same (fifth) order with the curve (or of the fourth order with the cone of chords): and consequently it is possible in this way to assign, as the intersection of this cylinder with this cone, at least one real twisted cubic, which has contact of the fiftht order with the given curve of double curvature, at the given point thereof. And such a cubic curve may be called, by eminence, an Osculating[‡] Twisted Cubic.

(42.) Not intending to return, in these *Elements*, on the subject of such cubic curves, we may take this occasion to remark, that the very simple vector equation,§

LXX...
$$\nabla a \rho = \rho \nabla \beta \rho$$
,

represents a curve of this kind, if a and β be any two constant and non-parallel

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^{*} Compare the Note to page 125.

[†] Accordingly it is known (see page 242 of Dr. Salmon's Treatise, already cited), that a twisted cubic can generally be described through any six given points; and also (page 248), that three quadric cylinders (or cylinders of the second order or degree) can be described, containing a given cubic curve, their edges being parallel to the three (real or imaginary) asymptotes.

[‡] Compare the first Note to page 92.

[§] This example was given in pages 679, &c., of the Lectures, with some connected transformations, the equation having been found as a certain condition for the inscription of a gauche quadrilateral, or S

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vectors. In fact, if we operate on this equation by the symbol S. λ , in which λ is an *arbitrary* but constant vector, the *scalar equation* so obtained, namely,

LXXI...
$$S\lambda a\rho = S\lambda \rho S\beta \rho - \rho^2 S\beta \lambda$$
,

represents a surface of the second order, on which the curve is wholly contained; making then successively $\lambda = a$ and $\lambda = \beta$, we get, in particular, the two equations,

LXXII... $S(Va\rho, V\beta\rho) = 0$, and LXXIII... $(V\beta\rho)^2 + Sa\beta\rho = 0$, representing respectively a cone and cylinder of that order, with the vector β from the origin as a common side: and the remaining part of the intersection of these two surfaces, is precisely the curve LXX., which therefore is a twisted cubic, in the known sense already referred to ρ

(43.) Other surfaces of the same order, containing the same curve, would be obtained by assigning other values to λ ; for example (comp. 397, (31.)), we should get generally an hyperbolic paraboloid from the form LXXI., by taking $\lambda \perp \beta$. But it may be more important here to observe, that without supposing any acquaintance with the theory of curved surfaces, the vector equation LXX. can be shown, by quaternions, to represent a curve of the third degree, in the sense that it is cut, by an arbitrary plane, in three points (real or imaginary). In fact, we may write the equation as follows,

LXXIV... $\nabla q \rho = -\alpha$, if LXXV... $q = g + \beta$,

q being here a quaternion, of which the vector part β is given, but the scalar part g is arbitrary; and then, by resolving (comp. 347) this linear equation LXXIV., we may still further transform it as follows,

LXXVI... $g(g^2 - \beta^2)\rho = \beta S\beta a + gV\beta a - g^2 a$,

which conducts to a *cubic equation* in g, when combined with the equation

LXXVII. . . $S_{\epsilon\rho} = e$,

of any proposed secant plane.

other even-sided polygon, in a given spheric surface (comp. the sub-articles to 296): the 2n successive sides of the figure being obliged to pass through the same even number of given points of space. It was shown that the curve might be said to intersect the unit-sphere ($\rho^2 = -1$) in two imaginary points at infinity, and also in two real and two imaginary points, situated on two real right lines, which were reciprocal polars relatively to the sphere, and might be called chords of solution, with respect to the proposed problem of inscription of the polygon; and that analogous results existed for even-sided polygons in ellipsoids, and other surfaces of the second order: whereas the corresponding problem, of the inscription of an odd-sided polygon in such a surface, conducted only to the assignment of a single chord of solution, as happens in the known and analogous theory of polygons in conics, whether the number of sides be (in that theory) even or odd. But we cannot here pursue the subject, which has been treated at some length in the Lectures, and in the Appendices to them.

ART. 398.] VECTOR EQUATION OF A TWISTED CUBIC.

(44.) The vector equation LXX., however, is not sufficiently general, to represent an arbitrary twisted cubic, through an assumed point taken as origin; for which purpose, ten scalar constants ought to be disposable, in order to allow of the curve being made to pass through five* other arbitrary points: whereas the equation referred to involves only five such constants, namely the four included in Ua and U β , and the one quotient of tensors T β : Ta (comp. 358).

(45.) It is easy, however, to accomplish the generalization thus required, with the help of that theory of *linear and vector functions* $(\phi\rho)$ of vectors, which was assigned in the Sixth Section of the preceding Chapter (Arts. 347, &c.). We have only to write, instead of the equation LXX., this other but analogous form which *includes* it,

LXXVIII... $\nabla a\rho + \nabla \rho \phi \rho = 0$, or LXXVIII'... $\phi \rho + c\rho = a$, and which gives, by principles and methods already explained (comp. 354, (1.)), the transformation

LXXIX...
$$\rho = (\phi + c)^{-1}a = \frac{\psi a + c\chi a + c^2 a}{m + m'c + m''c^2 + c^3};$$

a, ψa , and χa being here fixed vectors, and m, m', m'' being fixed scalars, but c being an arbitrary and variable scalar, which may receive any value, without the expression LXXIX. ceasing to satisfy the equation LXXVIII.

(46.) The curve LXXVIII. is therefore cut (comp. (43.)) by the plane LXXVII. in three points (real or imaginary), answering to and determined by the three roots of the cubic in c, which is formed by substituting the expression LXXIX. for ρ in the equation of that secant plane; and consequently it is a curve of the third degree, the three (real or imaginary) asymptotes to which have directions corresponding to the three values of c, obtained by equating to zero the denominator of that expression LXXIX., or by making M = 0, in a notation formerly employed: so that they have the directions of the three lines β , which satisfy this other vector equation (comp. 354, I.),

LXXX...
$$V\beta\phi\beta = 0.$$

S 2

[•] Compare the second Note to page 129. In general, when a curve in space is supposed to be represented (comp. 371, (5.)) by two scalar equations, each new arbitrary point, through which it is required to pass, introduces a necessity for two new disposable constants, of the scalar kind: and accordingly each new order, say the n^{th} , of contact with such a curve, has been seen to introduce a new vector, $D_s^{n\rho}$, or $\tau^{(n-1)}$, subject to a condition resulting from the general equation $TD_s\rho = 1$, or $\tau^2 = -1$ (comp. 380, XXVI., and 396, III.), but involving virtually two new scalar constants. Thus, besides the four such constants, which enter through τ and τ' into the determination of the directions of the rectangular system of lines, tangent, normal, and tinormal (comp. 379, (5.), or 396, (2.)), and of the length of the radius of (first) curvature, τ , the three successive derivatives, τ' , τ''' , of that radius, and the radius r of second curvature, $\pi'', \tau^{\prime\prime}$, into the determination (41.) of the osculating twisted cubic.

(47.) Accordingly, if β be such a line, and if γ be any vector in the plane of a and β , the curve LXXVIII. is a part of the intersection of the two surfaces of the second order,

LXXXI... $S_{\alpha\rho\phi\rho} = 0$, and LXXXII... $S_{\gamma\alpha\rho} + S_{\gamma\rho\phi\rho} = 0$,

whereof the first is a cone, and which have the line β from the origin for a common side (comp. (42.)): the curve is therefore found anew to be a twisted cubic.

(48.) And as regards the number of the scalar constants, which are to be conceived as entering into its vector equation LXXVIII., when we take for $\phi\rho$ the form $\nabla q_{0\rho} + \nabla \lambda \rho \mu$ assigned in 357, I., in which q_0 is an arbitrary but constant quaternion, such as $g + \gamma$, and λ , μ are constant vectors, the term $g\rho$ of $\phi\rho$ disappears under the symbol of operation $\nabla \cdot \rho$, and the equation (45.) of the curve becomes,

LXXXIII... $Va\rho + \rho V\gamma\rho + V\rho V\lambda\rho\mu = 0$;

in which the *four versors*, U_a , U_γ , $U\lambda$, U_μ , introduce each *two* scalar constants, while the *two tensor quotients*, T_γ : T_a and $T\lambda_\mu$: T_a , count as *two others*: so that the required number of *ten* such *constants* (44.) is exactly made up, the *curve* being still supposed to pass through an assumed *origin*, and therefore to have *one point given*. It is scarcely worth observing, that we can at once *remove* this last *restriction*, by merely *adding* a *new constant vector* to ρ , in the last equation, LXXXIII.

(49.) Although, for the determination of the osculating twisted cubic (41.) to a given curve of double curvature, it was necessary (comp. (40)) to employ the vector τ^{iv} or $D_s^{5}\rho$, or to take account of s^{5} in the vector ρ_s , or in the connected scalars $x_sy_sz_s$ of (34.), and therefore to improve the expressions LVIII., by carrying in each of them (or at least in the two latter), the approximation one step farther, yet there are many other problems relating to curves in space, besides some that have been already considered, for which those scalar expressions LVIII. are sufficiently approximate : or for which the vector expression I. suffices.

(50.) Resuming, for instance, the questions considered in (22.) and (23.), we may throw some additional light on the *law of the deviation* of a *near point* P_{s} of the *curve*, from the *osculating sphere* at P_{s} as follows. Eliminating *n* by XXXVI'. from XXXV, we find this *new expression*,

LXXXIV...
$$\overline{sP}_s - \overline{sP} = \frac{r_1 s^4}{24 r r^2 R};$$

the direction of this deviation from the sphere (R) depends therefore on the

ART. 398.] DEVIATIONS FROM CIRCLE AND SPHERE.

sign of the scalar radius r_1 (23.) of curvature of the cusp-edge (s) of the polar developable: and it is outward or inward (comp. 395, (14.)), according as that cusp-edge turns its concavity (comp. XLI.) or its convexity, at the centre s of the osculating sphere, towards the point P of the given curve, that is, towards the point of osculation.

(51.) Again, if we only take account of s^3 , the deviation of P_s from the osculating circle at P has been seen to be a vector tangential to the osculating sphere, which may be thus expressed (comp. 397, IX., LII.),

LXXXV...
$$c_s P_s = \frac{s^3}{6} \nu' \tau = \frac{s^3 \tau (\sigma - \rho)}{6 r^2 r},$$

if c_s be the point on the circle, which is distant from the given point P by an arc of that circle = s, with the same initial direction of motion, or of departure from P, represented by the common unit tangent τ ; the quantity of this deviation is therefore expressed by the scalar $\frac{s^3R}{6r^2r}$: that is, by the deviation $\frac{s^3}{6rr}$ (comp. 397, (9.), (10.)) from the osculating plane* at P, multiplied by the secant ($r^{-1}R$) of the inclination (P) of the radius (R) of spherical curvature, to the radius (r) of absolute curvature, and positive when this last deviation has the direction of the binormal ν .

(52.) On the other hand (comp. (5.)) the small angle, which the small arc ss, of the cusp-edge (s) of the polar developable subtends at the point \mathbf{P} , is ultimately expressed by the scalar,

LXXXVI...
$$\operatorname{sps}_s = (\overline{\operatorname{ps}}_s - \overline{\operatorname{ps}}) \cdot R^{-1} \operatorname{cot} P = \frac{rR's}{pR} = \frac{mrs}{R^2} (\text{by XXXIII.}),$$

* Besides the nine expressions in 397, (42.) for the square r^{-2} of the second curvature, the following may be remarked, as containing the law of the regression of the projection of a curve of double curvature on its own normal plane:

$$r^{-2} = \frac{9}{2\kappa_F} \cdot \lim_{n \to \infty} \frac{r_{Q_3}^2}{r_{Q_2}^3},$$
 397, XCIX., (10.)

x being still the centre of the osculating circle, and a_1 , a_2 , a_3 being still (as in 397, (10.)) the projections of a near point a (or P_4), on the tangent, the absolute normal (or inward radius of curvature PK), and the binormal at P. In fact, the principal terms of the three vector projections corresponding, of the small chord Pa (or PF_4), are (comp. LVIII.):

$$PQ_1 = s\tau; \quad PQ_2 = \left(\frac{1}{2}s^2\tau'\right) = \frac{s^2}{2r} U\tau'; \quad PQ_2 = \left(\frac{1}{6}s^3\Gamma^{-1}\nu\right) = \frac{s^3}{6rr} U\nu;$$

whence, ultimately.

$$\frac{9}{2} \cdot \frac{r^{2}Q_{3}^{2}}{r^{2}Q_{2}^{3}} = -r^{-2}rU\tau' = r^{-2} \cdot \kappa r.$$

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this angle being treated as positive, when the corresponding rotation^{*} round $+\tau$ from rs to PS_s is positive: and if we multiply *this* scalar, by that which has just been assigned (51.), as an expression for the deviation $c_s P_s$ from the osculating *circle*, we get, by XXXV., the product,

LXXXVII...
$$\frac{s^3 R}{6r^2 \mathbf{r}} \cdot \frac{r R' s}{p R} = \frac{R' s^4}{6r r p} = 4 (\overline{s P_s} - \overline{s P}).$$

(53.) Combining then the recent results (50.), (51.), (52.), we arrive at the following *Theorem*:

The deviation of a near point \mathbf{P}_s of a curve in space, from the osculating sphere at the given point \mathbf{P} , is ultimately equal to the quarter of the deviation of the same near point from the osculating circle at \mathbf{P} , multiplied by the sine of the small angle which the arc ss_s, of the locus of centres of spherical curvature (s), or of the cuspedge of the polar developable, subtends at the same point \mathbf{P} ; and this deviation $(\overline{s\mathbf{P}_s} - \overline{s\mathbf{P}})$ from the sphere has an outward or an inward direction, according as the same arc ss_s is concave or convex towards the same given point.

(54.) The vector of the centre s_s , of the near osculating sphere at P_s , is (in the same order of approximation, comp. I.),

LXXVIII. . .
$$OS_s = \sigma_s = \sigma + s\sigma' + \frac{1}{2}s^2\sigma'' + \frac{1}{6}s^3\sigma''' + \frac{1}{24}s^4\sigma^{IV};$$

and although $\sigma - \rho$ is already a function (by 397, IX., &c.) of τ , τ' , τ'' , so that σ' is (as in (2.) or (22.)) a function of τ' , τ'' , τ''' , and σ'' , σ''' , σ^{1v} introduce respectively the new derived vectors τ^{1v} , τ^v , τ^{v_1} , or $D_s^{s}\rho$, $D_s^{r}\rho$, $D_s^{r}\rho$, which we are not at present employing (49.), yet we have seen, in (23.) and (24.), that some useful combinations of σ'' , and σ''' can be expressed without τ^{1v} , τ^v : and the following is another remarkable example of the same species of reduction, involving not only σ'' and σ''' but also σ^{1v} , but still admitting, like the former, of a simple geometrical interpretation.

(55.) Remembering (comp. (22.), and 397, XV.) that

LXXXIX.... $(\sigma - \rho)^2 + R^2 = 0$, and XC.... $S\tau'''(\sigma - \rho) = r^{-2}S = r^{-2} + nr^{-1}r^{-1}$,

and reducing the successive derivatives of LXXXIX. with the help of the equations 397, XIX., and of their derivatives, we are conducted easily to the

$$\frac{s^4\left(\rho-\sigma\right)}{24R}\cdot\frac{R'}{rrp}\cdot$$

[•] Considered as a rotation, this small angle may be represented by the small vector, $rp^{-1}R'R^{-1s\tau}$; and if the vector deviation LXXXV. from the osculating circle be multiplied by this, the quarter of the product is (comp. XXXV.) the vector deviation from the osculating sphere, under the form,

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following system of equations, into which the derived vectors τ , τ' , &c. do not expressly enter, but which involve σ' , σ'' , σ''' , σ^{iv} , and R' R'', R''', R^{iv} :

$$\begin{aligned} \text{XCI.} \dots \text{S}\sigma'(\sigma-\rho) + RR' &= 0; \quad \text{XCII.} \dots \text{S}\sigma'\sigma''(\sigma-\rho) &= 0; \\ \text{XCIII.} \dots \text{S}\sigma''(\sigma-\rho) + \sigma'^2 + (RR')' &= 0; \\ \text{XCIV.} \dots \text{S}\sigma'''(\sigma-\rho) + 3\text{S}\sigma'\sigma'' + (RR')'' &= 0; \\ \text{XCV.} \dots \text{S}\sigma^{\text{IV}}(\sigma-\rho) + 4\text{S}\sigma'\sigma''' + 3\sigma''^2 + (RR')''' &= -\frac{RR'}{rr\rho} &= -\frac{n}{rr}; \end{aligned}$$

auxiliary equations being,

and XCVI...
$$S\sigma'\tau = 0$$
, $S\sigma'\tau' = 0$, $S\sigma''\tau = 0$, (comp. 395, X.)

$$XCVII... S\sigma'''\tau = -S\sigma''\tau' = S\sigma'\tau'' - S(\sigma - \rho)\tau'''$$

$$= -r^{-2}(S-1) = -nr^{-1}r^{-1}.$$

(56.) But, if R_s denote the radius of the near sphere, and if we still neglect s^s , we have,

XCVIII. . .
$$\mathbf{P}_{s}\mathbf{S}_{s}^{2} = -(\sigma_{s} - \rho_{s})^{2} = R_{s}^{2}$$

= $R^{2} + 2sRR' + s^{2}(RR')' + \frac{s^{3}}{3}(RR')'' + \frac{s^{4}}{12}(RR')''';$

whence follows, by LXXXVIII., and by the recent equations, this very simple expression, from which (comp. (24.)) everything depending on τ^{IV} , τ^{V} , τ^{VI} has disappeared,

XCIX. . .
$$(\sigma_s - \rho)^2 + R_s^2 = \frac{-RR's^4}{12rrp}$$

and which gives (within the same order of approximation, attending to XXXV.) the geometrical relation,

C...
$$\overline{Ps_s} - \overline{P_ss_s} = T(\sigma_s - \rho) - R_s = \frac{R's^4}{24rrp} = \frac{ns^4}{24rrR} = \overline{sP_s} - \overline{sP};$$

C'... $\overline{s_sP} - \overline{sP_s} = \overline{s_sP_s} - \overline{sP} = R_s - R.$

or

(57.) This result might have been foreseen, from the following very simple consideration. When the coefficient S - 1 of non-sphericity (395, (16.)), or of the deviation of a curve from a sphere, is positive, so that a near point P_s of the curve is exterior to (what we may call) the given sphere, which osculates to that curve at P, by an amount which is ultimately proportional to the fourth power of the arc, s, of the curve, then the given point P must be, for the same reason, exterior to the near sphere, which osculates at the point P_s ; and the two

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deviations, $Ps_s - P_s s_s$ and $sP_s - sP$, which have been found by calculation to be equal (C.), if s^5 be neglected, must in fact bear to each other an ultimate ratio of equality, because the two arcs, +s and -s, from P to P_s , and from P_s back to P, are equally long, although oppositely directed; or because $(+s)^4 = (-s)^4$. And precisely the same reasoning applies, when the coefficient S - 1 is negative, so that the deviations, equated in the formula C., are both inwards.

(58.) As regards the deviation (51.) of the near point P_s of the curve from the osculating circle at P, we may generalize and render more exact the expression LXXXV., by considering a point c_t of that circle, which is distant by a circular arc = t from the given point P; and of which the vector is, rigorously, by 396, (18.),

CI. . .
$$\operatorname{oc}_t = \omega_t = \rho + r\tau \sin \frac{t}{r} + r^2 \tau' \operatorname{vers} \frac{t}{r};$$

or if we only neglect t^5 ,

CII...
$$\operatorname{OC}_t = \omega_t = \rho + \tau \left(t - \frac{t^3}{6r^2}\right) + r\tau' \left(\frac{t^2}{2r} - \frac{t^4}{24r^3}\right).$$

(59.) In this way we shall have (comp. (34.)) the vector deviation,

CIII... $C_t P_s = \rho_s - \omega_t = X\tau + Yr\tau' + Zr\nu,$

with the scalar coefficients,

CIV...
$$X = x_s - r \sin \frac{t}{r}$$
, $Y = y_s - r \operatorname{vers} \frac{t}{r}$, $Z = z_s$;

or, neglecting s⁵ and t⁵, and attending to the expressions LVIII. and LVIII'.,

$$CV... \begin{cases} X = s - t - \frac{s^3 - t^3}{6r^2} + \frac{r's^4}{8r^3}; \\ Y = \frac{s^2 - t^2}{2r} - \frac{p}{r} Z - \frac{s^4 - t^4}{24r^3} - \frac{ns^4}{24r^2r}; \\ Z = \frac{s^3}{6rr} + \frac{rs^4}{24} (r^{-2}r^{-1})'; \end{cases}$$

in which r, r' r, p, and n have the same significations as before.

(60.) Assuming then for the circular arc t the value,

$$\mathbf{CVI.} \ldots t = s + \frac{r's^4}{8r^3},$$

which differs (as we see) by only a quantity of the *fourth order* from the arcs of the *curve*, we shall have, to the same order of approximation, the expressions,

CV11...
$$X = 0$$
, $Y = \frac{-p}{r} Z - \frac{ns^4}{24r^2r}$, $Z = z_s = \&c.$, as before,

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the deviation at P_s from the circle being here measured in a direction parallel to the normal plane at P; and if s^4 be neglected (although the expressions enable us to take account of it), this deviation is also parallel (as before) to the tangent $\tau (\sigma - \rho)$ to the osculating sphere in that plane: while it is represented in quantity by $Rr^{-1}s_s$, which agrees with the result in (51).

(61.) The expressions CVII. give also, without neglecting s⁴,

CVIII. . .
$$\frac{rY + pZ}{R} = -\frac{ns^4}{24rrR} = \overline{sP} - \overline{sP}_s$$
;

such then is the component of the deviation from the osculating circle, which is parallel to the normal PS to the sphere at P; and we see that it only differs in sign (because it is positive when its direction is that of the inward normal, or inward radius PS), from the expression XXXV. (comp. C.), for the outward deviation $\overline{sP}_s - \overline{sP}$ of the near point P_s, from the same osculating sphere at the given point P.

(62.) This *latter* component (61.) is *small*, even as *compared* with the *former* small component (60.); and the *small quotient*, of the latter divided by the former, is ultimately (by LXXXVI.),

CIX.
$$\cdot \cdot \frac{rY + pZ}{rZ - pY} = \frac{-nrs}{4R^2} = -\frac{1}{4}$$
sps_s;

where the small angle srs_s is positive or negative, according to the rule stated in (52.), and may be replaced by its sine, or by its tangent.

(63.) Instead of cutting the given osculating circle, as in (60.), by a plane which is *parallel to the given normal plane* at P, we may propose to cut that circle by the near normal plane at P_s , or to satisfy this new condition,

$$CX...0 = S\tau_s(\rho_s - \omega_t), \quad \text{or} \quad CX'...0 = XS\tau\tau_s + YSr\tau'\tau_s + ZSr\nu\tau_s;$$

which is easily found to give by CV. the values (s and t being still supposed to be small, and s^5 being still neglected):

CXI...
$$t = s - \frac{r's^4}{24r^3}$$
, and CXII... $X = \frac{r's^4}{6r^3}$, $Y = \&c.$, $Z = \&c.$, as in CVII.;

so that in passing to this *new near point* c_t of the *circle*, we only change X from zero to a small quantity of the *fourth order*, and make *no change* in the values of Y and Z.

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(64.) The new deviation $c_i P_s$ from the given circle may be decomposed into two partial deviations, in the near normal plane, of which one has the direction of the unit-tangent $R_s^{-1}\tau_s(\sigma_s - \rho_s)$ to the near sphere at P_s , and the other has that of the unit-normal $R_s^{-1}(\sigma_s - \rho_s)$ to the same sphere at the same point (or the opposites of these two directions); and the scalar coefficients of these two vector units, if we attend only to principal terms, are easily found to be,

CXIII...
$$\frac{rZ - pY}{R} = \frac{Rs^3}{6r^2r}$$
, and CXIV... $\frac{rY + (p + ns)Z}{R} = \frac{ns^4}{8rrR}$

(65.) We may then write :

CXV... Deviation of near point P_s from given osculating circle, measured in the near normal plane to the curve at P_s ,

= new
$$c_t P_s = \frac{Rs^3}{6r^2 r} U \tau_s (\sigma_s - \rho_s) + \frac{ns^4}{8r rR} U (\sigma_s - \rho_s);$$

in which it may be observed, that the second scalar coefficient is equal to three times the scalar deviation $\overline{sP}_s - \overline{sP}$ (XXXV. or C.), of the near point P_s of the curve, from the given osculating sphere (at P).

(66.) But we may also interpret the new coefficient last mentioned, as representing a new deviation; namely, that of the point c_t of the given circle, from the near osculating sphere at P_s , considered as positive when that new point c_t is exterior to that near sphere; or as denoting the difference of distances $\overline{s_s c_t} - \overline{s_s P_s}$. We have therefore (comp. (56.)) this new geometrical relation, of an extremely simple kind:

or

CXVI. . .
$$\overline{s_s c_t} - \overline{s_s P_s} = 3(\overline{sP_s} - \overline{sP}) = 3(\overline{s_s P} - \overline{s_s P_s});$$

CXVI'. . . $\overline{s_s c_t} = 3\overline{s_s P} - 2\overline{s_s P_s}.$

(67.) Supposing, then, at first, that the coefficient of non-sphericity S - 1 is positive (comp. 395, (16.)), if we conceive a point to move backwards, upon the curve, from P_s to P_s and then forwards, upon the circle which osculates at P_s , to the new point c_t (63.), we see that it will first attain (at P) a position exterior to the sphere which osculates at P_s , or will have an amount, determined in (56.), of outward deviation, with respect to that near osculating sphere; and that it will afterwards attain (at the new point c_t) a deviation of the same

ART. 398.] RELATIONS BETWEEN THE DEVIATIONS.

character (namely outwards, if S > 1), from the same near sphere, but one of which the amount will be threefold the former: this last relation holding also when S < 1, or when both deviations are inwards.

(68.) It is easy also to infer from (65.), (comp. (57.)), that if we go back from P_s , on the near circle which osculates at that near point, through an arc (t) of that circle, which will only differ by a small quantity of the fourth order (comp. (60.)) from the arc (s) of the curve, so as to arrive at a point, which for the moment we shall simply denote by c, and in which (as well as in another point of section, not necessary here to be considered) the near osculating circle is cut by the given normal plane at P, the vector deviation of this new point c of the new circle, from the given point P of the curve, must be, nearly:

CXVII... PC =
$$\frac{Rs^3}{6r^2r}$$
 Ur $(\sigma - \rho) - \frac{ns^4}{8rrR}$ U $(\sigma - \rho)$;

the coefficients being formed from those of the formula CXV., by first changing s to -s, and then changing the signs of the results: while the relation CXVI. or CXVI'. takes now the form,

CXVIII...
$$\overline{sc} - \overline{sP} = 3(\overline{sP}_s - \overline{sP})$$
, or CXVIII'... $\overline{sc} = 3\overline{sP}_s - 2\overline{sP}$.

(69.) Accordingly if, after going from P to P, along the curve, we go forward or backward, through any positive or negative arc, t, of the circle, which osculates at that point P_s, we shall arrive at a point which we may here denote by $c_{s,t}$; and the vector (comp. again 396, (18.)) of this near point (more general than any of those hitherto considered) will be rigorously,

CXIX...
$$\omega_{s,t} = oc_{s,t} = \rho_s + r_s \tau_s \sin \frac{t}{r_s} + r_s^2 \tau'_s \text{ vers } \frac{t}{r_s}$$
.

And if we develop this new expression to the accuracy of the fourth order inclusive, we find that we satisfy the new condition (comp. (63.)),

$$\mathrm{CXX...Sr}(\omega_{s,t}-\rho)=0, \quad \mathrm{when} \quad \mathrm{CXXI...}t=-s-\frac{r's^4}{24r^3};$$

and that then the expression CXIX. agrees with CXVII., within the order of approximation here considered.

(70.) A geometrical connexion can be shown to exist, between the two equivalents which have been found above, one for the quadruple (LXXXVII.,

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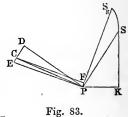
comp. (53.)), and the other for the triple (CXVIII.), of the deviation $\overline{sP}_s - \overline{sP}$ of a near point P_s of the curve, from the sphere which osculates at the given point P: in such a manner that if either of those two expressions be regarded as known, the other can be inferred from it.

(71.) In fact if we draw, in the normal plane, perpendiculars PD and PE to the lines PS and PS_s, and determine points D and E upon them by drawing a parallel to PS through the point c of (68.), letting fall also a perpendicular CF on PS_s, the *two small lines* PD and DC will ultimately represent the *two terms* or components CXVII. of PC; and the *small angle* DPC will ultimately be equal to *three quarters* of the small angle SPS_s, and will correspond to the same direction of rotation round τ , because

CXXII... $\frac{DC}{PD} = \frac{3}{4} \cdot \frac{nrs\tau}{R^2} = \frac{3}{4} \cdot \nabla \frac{\sigma's}{\sigma-\rho},$

CXXIII. . . DPC = $\frac{3}{4}$ SPS₈ = $\frac{3}{4}$ DPE ;

so that we shall have the *ultimate ratios* (comp. the annexed fig. 83^*):



CXXIV...DC: DE: CE (OF FP) = 3:4:1.

But the line CF is ultimately the *trace*, on the given normal plane, of the tangent plane at c to the near osculating sphere; the small line FP (or CE) represents therefore the *deviation* $\overline{s_sP} - \overline{s_sP_s}$ of the given point P from that near sphere, or the *equal* deviation (57.), $\overline{sP_s} - \overline{sP}$; its ultimate *quadruple*, DE, represents the *product* mentioned in (52.); and the ultimate *triple*, DC, of the same small line CE, is a geometrical representation of that other deviation $\overline{sC} - \overline{sP}$, which has been more recently considered.

(72.) When the two scalars, s and t, are supposed capable of receiving any values, the point $c_{s,t}$ in (69.) may be any point of the Locus (8.) of the Osculating Circle to the given curve of double curvature; and if we seek the direction of the normal to this superficial locus, at this point, on the plan of Art. 372, writing first the equation of the surface under the

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or

[•] In figs. 81, 82, the little arc near s is to be conceived as *terminating there*, or as being a *preceding arc* of the curve which is the locus of s, if r', r, n, and therefore also p and r₁, be *positive* (comp. the second Note to page 107). In the new figure 83, the triangle PDE is to be conceived as being in fact *much smaller* than **PKS**, though *magnified* to exhibit angular and other relations.

ART. 398.]

LOCUS OF OSCULATING CIRCLE.

slightly simplified, but equally rigorous form,

with

$$\nabla \mathbf{X} \mathbf{X} \mathbf{V} \dots \boldsymbol{\omega}_{s, u} = \rho_s + r_s \tau_s \sin u + r_s^2 \tau_s \text{ vers } u$$

$$\mathbf{CXXVI}...u = r_s^{-1}t = \mathbf{P}_s\mathbf{K}_s\mathbf{C}_s, t,$$

so that u is here a new scalar variable, representing the *angle subtended at* the centre κ_s , of the osculating circle at \mathbf{P}_s , by the arc, t, of that circle, we are led, after a few reductions, to the expression,

CXXVII. . . V(D_u
$$\omega_s$$
, _u . D_s ω_s , _u) = $r_s r_s^{-1}(\omega_s$, _u - σ_s) vers u;

which proves, by quaternions, what was to be expected from geometrical^{*} considerations, that the locus of the osculating circle is also (as stated in (8.) and (22.)) the Envelope of the Osculating Sphere.

(73.) The normal to this locus, at any proposed point $c_{s,t}$ of any one osculating circle, is thus the radius of the sphere to which that circle belongs, or which has the same point of osculation P_s with the given curve, whether the arc (s) of that curve, and the arc (t) of the circle, be small or large. We must therefore consider the tangent plane to the locus, at the given point P_r of the curve, as coinciding with the tangent plane to the osculating sphere at that point; and in fact, while this latter plane ($\bot Ps$) contains the tangent τ to the curve, which is at the same time a tangent to the locus, it contains also the tangent $\tau(\sigma - \rho)$ to the sphere, which is by CXVII. another tangent to the locus, as being the tangent at P to the section of that surface, which is made by the normal plane to the curve.

(74.) But when we come to examine, with the help of the same equation CXVII., what is the *law of the deviation* DC (comp. fig. 83) of that normal section of the *locus*, considered as a new curve (c), from its own tangent PD, we find that this law is ultimately expressed (comp. (71.)) by the formula,

CXXVIII...
$$\frac{DC^3}{PD^4} = \frac{81}{32} \cdot \frac{n^3 r^5 \mathbf{r}(\sigma - \rho)}{R^8} = \text{const.};$$

hence $\overline{\text{DC}}$ varies ultimately as the *power* of $\overline{\text{PD}}$, which has the *fraction* $\frac{4}{3}$ for its exponent; the *limit* of $\overline{\text{PD}}^2$: $\overline{\text{DC}}$ is therefore *null*, and the *curvature of the* section is *infinite at* P.

^{*} In the language of infinitesimals, two consecutive osculating spheres, to any curve in space, intersect each other in an osculating circle to that curve.

[III. III. § 6.

(75.) It follows that this point P is a singular point of the curve (c), in which the locus (8.) is cut (73.), by the normal plane to the given curve at that point; but it is not a cusp on that section, because the tangential component PD of the vector chord PC is ultimately proportional to an odd power (namely to the cube, by CXVII., comp. (71.)) of the scalar variable, s, and therefore has its direction reversed, when that variable changes sign: whereas the normal component DC of the same chord PC is proportional to an even power (namely the fourth, by the same equation CXVII.) of the same arc, s, of the given curve, and therefore retains its direction unchanged, when we pass from a near point Ps, on one side of the given point P, to a near point P_{-s} on the other side of it.

(76.) To illustrate this by a contrasted case, let G be the point in which the *tangent* to the given curve at P_s is cut by the normal plane at P; or a point of the section, by that plane, of the developable surface of tangents. We shall then have the sufficiently approximate expressions,

CXXIX... PG =
$$\rho_s - \rho - \left(s + \frac{s^3}{3r^2}\right)\tau_s = \frac{-s^2\tau'}{2} - \frac{s^3\nu}{3r} = -PQ_2 - 2PQ_3$$

with the significations 397, (10.) of q_2 and q_3 ; hence the point P of the curve is (as is well known) a cusp of the section (G) of the developable surface of tangents (comp. 397, (15.)), because the tangential component ($-Pq_2$) of the vector chord (PG) has here a fixed direction, namely that of the outward radius (KP prolonged) of the circle of curvature at P: while it is now the normal component ($-2Pq_3$) which changes direction, when the arc s of the curve changes sign. At the same time we see* that the equation of this last section (G) may ultimately be thus expressed :

CXXX...
$$\frac{(-2\mathbf{P}\mathbf{Q}_3)^2}{(-\mathbf{P}\mathbf{Q}_2)^3} = \frac{8\mathbf{P}\mathbf{K}}{9\mathbf{r}^2} = \text{const.};$$

comparing which with the equation CXXVIII., we see that although, in each case, the curvature of the section is infinite, at the point P of the curve, yet the normal component (or coordinate) varies (ultimately) as the power $\frac{3}{2}$ of the tangential component, for the section (G) of the Surface of Tangents: whereas the former component varies by (74.) as the power $\frac{4}{3}$ of the latter, for the corresponding section (c) of the Locus of the Osculating Circle.

^{*} Compare the Note to page 133.

ART. 398.] ENVELOPE OF SPHERE WITH VARYING RADIUS.

(77.) It follows also that the curve (P) itself, although it is not a cusp-edge of the last-mentioned locus (8.), while it is such on the surface of tangents, is yet a Singular Line upon that locus likewise: the nature and origin of which line will perhaps be seen more clearly, by reverting to the view (8.), (22.), (72.), according to which that Locus of a Circle is at the same time the Envelope of a Sphere.

(78.) In general, if we suppose that σ and R are any two real functions, of the vector and scalar kinds, of any one real and scalar variable, t, and that σ' , R', and σ'' , R'', &c. denote their successive derivatives, taken with respect to it, then σ may be conceived to be the variable vector of a point s of a curve in space, and R to be the variable radius of a sphere, which has its centre at that point s, but alters generally its magnitude, at the same time that it alters its position, by the motion of its centre along the curve (s).

(79.) Passing from one such sphere, with centre s and radius R, considered as given, and represented by the scalar equation,*

$$(\sigma - \rho)^2 + R^2 = 0, \qquad \qquad \text{LXXXIX.},$$

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in which ρ is now conceived to be the vector of a variable point P upon its surface, to a near sphere of the same system, for which σ , s, and R are replaced by σ_t , s_t, and R_t , where t is supposed to be small, we easily infer (comp. 386, (4.)) that the equation,

$$S\sigma'(\sigma - \rho) + RR' = 0,$$
 XCI.,

which is formed from LXXXIX. by once derivating σ and R with respect to t, but treating ρ as constant, represents the *real plane* (comp. 282, (12.)) of the (*real or imaginary*) circle, which is the *ultimate intersection* of the near sphere with the given one; the *radius* of this circle, which we shall call r, being found by the following formula,

$$CXXXI...r^2\sigma'^2 = R^2(R'^2 + \sigma'^2), \text{ or } CXXXI'...r^2T\sigma'^2 = R^2(T\sigma'^2 - R'^2),$$

and being therefore real when

CXXXII... $R'^2 + \sigma'^2 < 0$, or CXXXII'... $R'^2 < T\sigma'^2$;

^{*} This equation, and a few others which we shall require, occurred before in this series, but in a connexion so different, that it appears convenient to repeat them here.

while the centre, say K, of the circle is always real, and its vector is,

$$CXXXI''...OK = \kappa = \sigma + RR'\sigma'^{-1};$$

and the *plane* XCI. of the same circle is *parallel* to the *normal plane* of the *curve* (s).

(80.) With the condition CXXXII., the two scalar equations, LXXXIX. and XCI., represent then jointly a real circle; and the locus of all such circles (comp. 386, (6.)) is easily proved to be also the envelope of all the spheres, of which one is represented by the equation LXXXIX. alone; each such sphere touching this locus, in the whole extent of the corresponding circle of the system.

(81.) The plane XCI., considered as varying with t, has a developable surface for its envelope; and the real right line, or generatrix, along which one touches the other, is represented (comp. again 386, (6.)) by the system of the two scalar equations, XCI. and

$$S\sigma''(\sigma - \rho) + \sigma'^{2} + (RR')' = 0, \qquad XCIII.;$$

where ρ is now the variable vector of the line of contact, although it has been treated as constant (comp. 386, (4.)), in the process by which we are here conceived to pass, by a second derivation, from LXXXIX. through XCI. to XCIII.

(82.) This real right line (81.) meets generally the sphere, and also the circle (as being in its plane), in two (real or imaginary) points, say P_1 , P_2 ; and the curvilinear locus of all such points forms generally a species of singular line,* upon the superficial locus (or envelope) recently considered (80.); or rather it forms in general two branches (real or imaginary) of such a line: which generally two-branched line (or curve) is the (real or imaginary) envelope (comp. 386, (8.)), of all the circles of the system.

^{*} Called by Monge an arête de rebroussement, except in the case to which we shall next proceed, when its two branches coincide. The envelope (80.) of a varying sphere has been considered in two distinct Sections, § XXII. and § XXVI., of the Application de l'Analyse à la Géométrie; but the author of that great work does not appear to have perceived the interpretation which will soon be pointed out, of the condition of such coincidence. Meantime it may be mentioned, in passing, that quaternions are found to confirm the geometrical result, that when the two branches (P1) (P2) are distinct, then each is a cusp-edge of the surface; but that when they are coincident, the singular line (P) in which they merge has then a different character.

ART. 398.] CONDITION OF COINCIDENCE OF CUSP-EDGES,

(83.) The equation

$$S\sigma'\sigma''(\sigma-\rho)=0,$$
 XCII.,

which now represents (comp. 376, ∇ .) the osculating plane to the curve (s), shows that this plane through the centre s of the sphere is perpendicular to the right line (81.), and consequently contains the perpendicular let fall from that centre on that line: the foot P of this last perpendicular is therefore found by combining the three linear and scalar equations, XCI., XCII., XCIII., and its vector is,

CXXXIII... OP =
$$\rho = \sigma + \frac{g\sigma' + RR'\sigma''}{V\sigma'\sigma''}$$
,

 $CXXXIV...g = -\sigma^{\prime 2} - R^{\prime 2} - RR^{\prime \prime} = \mathbf{T}\sigma^{\prime 2} - (RR^{\prime})^{\prime}.$

(84.) The condition of contact of the right line (81.) with the sphere (78.), or with the circle (79.), or the condition of contact between two consecutive^{*} circles of the system (80.), or finally the condition of coincidence of the two branches (82.) of that singular line upon the surface which is touched by all those circles, is at the same time the condition of coexistence of the four scalar equations, LXXXIX., XCI., XCII., XCIII.; it is therefore expressed by the equation (comp. CXXXIII.),

$$CXXXV...R^{2}(\nabla\sigma'\sigma'')^{2} = (g\sigma' + RR'\sigma'')^{2};$$

which may also be thus written,†

or thus,

if

CXXXVI...
$$(RS\sigma'\sigma'' - R'g)^2 = (R'^2 + \sigma'^2) (R^2\sigma''^2 + g^2),$$

CXXXVII... $R^2(R'^2 + \sigma'^2) (\nabla\sigma'\sigma'')^2 = (g\sigma'^2 + RR'S\sigma'\sigma'')^2;$

the scalar variable t (78.), with respect to which the derivations are performed,

$$\left[a(\phi'\phi''+\psi'\psi''+\pi'\pi'')-h^2\right]^2+h^2\left[a^2(\phi''^2+\psi''^2+\pi''^2)-h^4\right]=0;$$

in which he writes, for abridgment,

$$h^2 = 1 - \phi'^2 - \psi'^2 - \pi'^2,$$

and ϕ , ψ , π are the three rectangular coordinates of the centre of a moving sphere, considered as

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^{*} Compare the second Note to page 115.

⁺ In page 372 of Liouville's Edition already cited, or in page 325 of the Fourth Edition (Paris, 1809), of the *Application de l'Analyse*, &c., it will be found that this condition is assigned by Monge, as that of the *evanescence* of a certain *radical*, under the form (an accidentally omitted exponent of π'' in the second part of the first member being here restored):

remaining still entirely arbitrary, but the point P, which is determined by the formula CXXXIII., being now situated on both the sphere and the circle: and its curvilinear locus, which we may call the curve (P), being now the singular line itself, in its reduced and one-branched state. And the last form CXXXVII. shows, what was to be expected from geometry, that when this condition of coincidence is satisfied, the earlier condition of reality CXXXII. is satisfied also: together with this other inequality,

CXXXVIII. . .
$$R^2 \sigma''^2 + g^2 < 0$$
,

which then results from the form CXXXVI.

(85.) The equations CXXXI., CXXXIV., and the general formula 389, IV., give the expressions,

CXXXIX...
$$\frac{rr'}{RR'} = \frac{g\sigma'^2 + RR'S\sigma'\sigma''}{-\sigma'^4};$$
 CXL... $r_1^{-2} = \frac{(\nabla\sigma'\sigma'')^2}{\sigma'^6};$

where r is still the radius of the circle of contact of the sphere with its envelope, and r_1 is the radius of curvature of the locus of the centre s of the same variable sphere; whence it is easy to infer, that the condition CXXXV. may be reduced to the following very simple form (comp. XXXVI'. and XLII.):

$$\mathrm{CXLI.} \ldots (r'r_1)^2 = (RR')^2; \quad \mathrm{or} \quad \mathrm{CXLI'.} \ldots r_1\mathrm{d}r = \pm R\mathrm{d}R;$$

the independent variable being still arbitrary.

(86.) If the *arc* of the *curve* (s) be taken as that variable t, the form CXXXVI. of the same condition is easily reduced to the following,

CXLII... $R^2 = (RR')^2 + g^2 r_1^2$, with CXLIII... g = 1 - (RR')';

derivating then, and dividing by 2g, we have this new differential equation,

functions of its radius a. Accordingly, if we change R to a, and σ to $i\phi + j\psi + k\pi$, supposing also that R' = a' = 1, and R'' = a'' = 0, whereby g is changed to $-h^2$, and $R'^2 + \sigma'^2$ to h^2 , in the condition CXXXVI., that condition takes, by the rules of quaternions, the exact form of the equation cited in this Note: which, for the sake of reference, we shall call, for the present, the Equation of Monge, although it does not appear to have been either interpreted or integrated by that illustrious author. Indeed, if Monge had not hastened over this case of coincident branches, on which he seems to have designed to return in a subsequent Memoir (unhappily not written, or not published), he would scarcely have chosen such a symbol as h^2 (instead of $-h^2$), to denote a quantity which is essentially negative, whenever (as here) the encelope of the sphere is real.

ART. 398.7 CONDITION OF COINCIDENCE OF CUSP-EDGES.

which is of linear form with respect to RR', whereas the condition itself may be considered as a differential equation of the second degree, as well as of the second order,*

CXLIV... $RR' = r_1(gr_1)'$; or CXLV... $r_1^2 u'' + r_1 r_1'(u'-1) + u = 0$, if CXLVI... $u = RR' = RD_t R$, and therefore CXLVII... $u^2 = R^2 - r^2$,

by CXXXI. or CXXXI'., because we have now,

CXLVIII... $\sigma'^2 = -1$, or $T\sigma' = 1$, or $dt = Td\sigma$:

so that the new scalar variable, RR', or u, with respect to which the linear equation CXLIV. or CXLV. is only of the second order, represents the perpendicular height \dagger of the centre s of the sphere, above the plane of the circle, considered as a function of the arc (t) of the curve (s), and as positive when the radius R of the sphere increases, for positive motion along that curve, or for an increasing value of its arc.

(87.) If the curve (s) be given, or even if we only know the *law* according to which its radius of curvature (r_1) depends on its arc (t), the coefficients of the *linear equation* CXLV. are *known*; and if we succeed in *integrating* that equation, so as to find an expression for the *perpendicular u* as a function of that arc t, we shall then be able to express also, as functions of the same arc, the radii R and r of the sphere and circle, by the formulæ,

CXLIX. . . $\pm r = gr_1 = r_1(1 - u')$, and **CL.** . . $R^2 = 2 \int u dt = u^2 + r_1^2(1 - u')^2$;

the third scalar constant, which the integral $2\int udt$ would otherwise introduce into the expression for R^2 , being in this manner determined, by means of the other two, which arise from the integration of the equation above mentioned.

(88.) For example, it may happen that the locus of the centre s of the sphere has a *constant curvature*, or that $r_1 = \text{const.}$; and then the *complete integral* of the linear equation CXLV. is at once seen to be of the form,

CLI. . .
$$u = a \sin (r_1^{-1}t + b),$$

^{*} We shall soon assign the complete integral of the differential equation in quaternions (84.), and also that of the corresponding Equation of Monge, cited in the preceding Note.

[†] It will be found that this new scalar u, if we abstract from sign, corresponds precisely to the p of earlier sub-articles, although presenting itself in a *differential connexion*: for the sphere (78.), and the circle (79.), under the condition (84.), will soon be shown to be the osculating sphere and circle to the recent curve (P), or to the singular line (84.) upon the surface at present considered, that is, on the locus or envelope (80.).

a and b being two arbitrary (but scalar) constants; after which we may write, by (87.),

CLII...
$$\pm r = r_1 - a \cos(r_1^{-1}t + b);$$

CLIII... $R^2 = r_1^2 - 2ar_1 \cos(r_1^{-1}t + b) + a^2;$

so that, in this case, both the radii, r and R, of circle and sphere, are periodical functions of the arc of the curve (s).

(89.) In general, if that curve (s) be completely given, so that the vector σ is a known function of a scalar variable, and if an expression have been found (or given) for the scalar R which satisfies any one of the forms of the condition (84.), we can then determine also the vector ρ , by the formula CXXXIII., as a function of the same variable; and so can assign the point \mathbf{P} of the singular line (84.), which corresponds to any given position of the centre s of the sphere. For this purpose we have, when the are of the curve (s) is taken, as in (86.), for the independent variable t, the formula,

CLIV...
$$\rho = \sigma - u\sigma' - (1 - u')\sigma''^{-1} = \kappa_1 - u\sigma' - r_1^2 u'\sigma'',$$

if κ_1 be the vector of the centre, say κ_1 , of the osculating circle at s to that given curve, so that (comp. 389, XI.) it has the value,

CLV...
$$OK_1 = \kappa_1 = \sigma - \sigma''^{-1} = \sigma + r_1^2 \sigma''$$
, with CLV... $\sigma''^2 + r_1^{-2} = 0$.

If then we denote by v the distance of the point P from this centre κ_1 , and attend to the linear equation CXLV., we see that

CLVI'...
$$vv' = r_1r_1'u_1'$$
, with $T\sigma' = 1$;

CLVI... $v = \overline{\mathbf{K}_1 \mathbf{P}} = \mathbf{T}(\rho - \kappa_1) = \sqrt{(u^2 + r_1^2 u'^2)},$

or more generally,

 $\mathbf{CLVII.} \dots vv's_1' = r_1r_1'u',$

if

CLVII' $u = RR's_1'^{-1}$,	and	CLVII"	$s_1 = \int \mathbf{T} d\sigma$
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while

$$\mathbf{CLVI''...} v^2 = u^2 + r_1^2 u'^2 s_1'^{-2};$$

so that s_1 denotes the *arc* of the *curve* (s), when the independent variable t is again left arbitrary. This *distance*, v, is therefore *constant* (= a) in the *case* (88.), namely when the *radius of curvature* r_1 of that curve is *itself* a constant quantity.

ABT. 398.] DETERMINATION OF THE SINGULAR LINE.

(90.) When $s_1' = T\sigma' = 1$, as in CXLVIII., the part $\sigma - u\sigma'$ of the first expression CLIV. for ρ becomes = κ , by CXXXI". and CXLVI.; attending then to CLV., we have the scalar quotient,

CLVIII.
$$\ldots \frac{\kappa - \rho}{\sigma - \kappa_1} = 1 - u';$$

whence generally,

CLVIII'...
$$\frac{\kappa - \rho}{\sigma - \kappa_1} = 1 - \frac{1}{s_1'} \left(\frac{RR'}{s_1'}\right)' = 1 - \left(\frac{\mathrm{d}}{\mathrm{d}s_1}\right)^2 \left(\frac{R^2}{2}\right),$$

the independent variable t being again arbitrary. Accordingly, if we combine the general expression CXXXIII. for ρ , with the expression CXXXI''. for κ , and with the following for κ_1 (comp. 389, IV.),

CLIX. . .
$$\kappa_1 = \sigma + \frac{{\sigma'}^3}{V{\sigma''}{\sigma'}}$$
, for an *arbitrary* scalar variable,

we easily deduce this new form of the scalar quotient,

CLIX'...
$$\frac{\kappa - \rho}{\sigma - \kappa_1} = 1 + ((RR')' - RR'S\sigma'^{-1}\sigma'')\sigma'^{-2};$$

which agrees with CLVIII'., because $-\sigma'^2 = s_1'^2$, and $S \frac{\sigma''}{\sigma'} = \frac{s_1''}{s_1'}$.

(91.) It has then been fully shown, how to determine the vector ρ as a function of the scalar t, when σ and R are two known functions of that variable, which satisfy any one of the forms of the condition (84.). It must then be possible to determine also the derived vectors, ρ' , ρ'' , &c., as functions of the same variable; and accordingly this can be done, by derivating any three of the four scalar equations, LXXXIX. XCI. XCII. XCIII., of which that condition (84.) expresses the coexistence. Now if we derivate a first time the two first of these, and then reduce by the second and fourth, we get the equations,

CLX...
$$S\rho'(\sigma - \rho) = 0$$
, $S\rho'\sigma' = 0$, whence $CLX'...\rho' \parallel V\sigma'(\sigma - \rho)$;

and although this last formula only determines the *direction* of the *tangent* to the *singular line* at P, namely that of the *common tangent* at that point to *two* consecutive circles (84.), yet it enables us to infer, by the remaining equation XCII., that

DLXI...
$$\rho' \perp \sigma'', \rho' \parallel \nabla \sigma' \sigma'', \text{ and } \text{CLXI'...} S \rho' \sigma'' = 0;$$

reducing by which the derivative of XCIII., we find,

$$S\sigma'''(\sigma - \rho) + 3S\sigma'\sigma'' + (RR')'' = 0, \qquad XCIV.,$$

the scalar variable being still arbitrary. And conversely, the system^{*} of the four equations LXXXIX. XCI. XCIII. XCIV. gives the three equations CLX. CLXI'., and so conducts to the equation XCII., and thence to the condition (84.); unless we suppose that ρ is a constant vector a, or that the variable sphere passes through a fixed point A, a case which we do not here consider, because in it the singular line (P) would reduce itself to that one point.

(92.) Derivating the two equations CLX., and reducing with the help of CLXI'., we find these new equations,

CLXII...
$$S\rho''(\sigma - \rho) - \rho'^2 = 0$$
, $S\rho''\sigma' = 0$;

whence

CLXIII. . .
$$S\rho'''(\sigma - \rho) - 3S\rho'\rho'' = 0.$$

We are led then, by elimination of the derivatives of σ , to the system of the three equations 395, VII.; and we conclude, that the point s is the centre, and the radius R is the radius, of the osculating sphere† to the singular line (P): whence it is easy to infer also, that the plane of contact (79.) of the sphere with its envelope is the osculating plane, and that the circle of contact (80.) is the osculating circle (comp. (72.)), to the same curve (P), at the point where two consecutive circles touch one another (84.).

(93.) In general, and even without the condition (84.), the tangent to a branch (82.) of the curvilinear envelope of the circles of the system, at any point P_1 of that branch, has the direction represented by the vector $\nabla \sigma'(\sigma - \rho_1)$, of the tangent to the circle at that point; but when that condition is satisfied,

ГIII. ш. § 6.

[•] In the language of infinitesimals, this system of equations expresses that four consecutive spheres intersect, in one common point P. When that point happens to be a fixed one, the condition (84.) requires that we should have the relation $S\sigma'\sigma''(\sigma-\alpha)=0$; or geometrically, that the curve (s) should be in a plane through a fixed point, which is then a singular point of the envelope.

⁺ In the language of infinitesimals (comp. the preceding Note), if every four consecutive spheres of a system intersect in one point of a curve, then each sphere passes through four consecutive points of that curve. Simple as this geometrical reasoning is, the writer is not aware that it has been anticipated; and indeed he is at present led to suppose that this whole theory, of the Locus of the Osculating Circle, as the Envelope of the Osculating Sphere, is new. Monge had however considered, but rejected (page 374 of Liouville's Edition), the case of a system of circles having each a simple contact with a curve in space.

ABT. 398.] ENVELOPE OF OSCULATING SPHERE.

so that the two branches of the singular line coincide, the point P of that line is in the osculating plane (83.) to the curve (s): and then the equation XCII. shows that the tangent ρ' , or $\nabla \sigma'(\sigma - \rho)$, to the line, is perpendicular to σ'' , or parallel to $\nabla \sigma' \sigma''$ (comp. CLXI.), and therefore that the singular line crosses that plane at right angles.

(94.) It follows that, with the condition (84.), the singular line (\mathbf{P}) is an orthogonal trajectory to the system of osculating planes to the curve (\mathbf{s}); and whereas, when this last curve is given, there ought to be one such trajectory for every point of a given osculating plane, this circumstance is analytically represented, in our recent calculations, by the biordinal form of the differential equation CXLV., of which the complete integral must be conceived (87.) to involve generally, as in the case (88.), two arbitrary constants.

(95.) It follows also that, with the same condition of coincidence of branches, the singular line (P) must have the curve (s) for the cusp-edge of its polar developable; or that the sphere, with s for centre, and with R for radius, must be the osculating sphere to the curve (P), as otherwise found by calculation in (92.): while the circle (80.) must be, as before, the osculating circle to that curve.

(96.) Accordingly, all equations, and inequalities, which have been stated in the recent sub-articles (79.), &c., respecting the envelope of a moving sphere with variable radius, under that condition (84.), and without any special selection of the independent variable, admit of being verified, by means of the earlier formulæ for the osculating circle and sphere to a curve (P) treated as a given one, when the arc (s) of that curve is taken as such a variable.

(97.) For example, we had lately the *two inequalities*, $R'^2 + \sigma'^2 < 0$, CXXXII., and $R^2\sigma''^2 + g^2 < 0$, CXXXVIII. And accordingly the earlier sub-articles (22.), (23.) give, for those two combinations, the essentially negative values,

CLXIV...
$$R'^2 + \sigma'^2 = -p^{-2}r^2 R'^2$$
; CLXV... $R^2 \sigma''^2 + g^2 = -((nr)')^2$;

in obtaining which last, the following transformations have been employed

CLXVI... $\sigma''^2 = -n'^2 - n^2 r^{-2}$; CLXVII... $g = -n'p + nrr^{-1}$.

(98.) As regards the verification of the *equations*, it may be sufficient to give one example; and we shall take for it the *last general form* CLVII

[III. III. § 6.

of the differential equation of condition (84.). For this purpose we may now write, by (22.) and (23.),

CLXVIII... $s_1' = \pm n$, $u = \pm p$, $u' = \pm p'$, $r_1u_1's_1'^{-1} = p'r_1n^{-1} = p'r$; and have only to observe that

CLXIX... $\frac{1}{2}(p^2 + p'^2r^2)' = p'r(r + p'r)'$, because p = r'r.

(99.) If we denote by c_1 , c_2 , c_3 the first members of the equations XCI., XCIII., XCIV., then besides the equation LXXXIX., which may be regarded as a mere definition of the radius R, we have $c_1 = 0$ for the whole of the superficial locus or envelope (80.); but we have not also $c_2 = 0$, except for a point on one or other of the two (generally distinct) branches of the singular line (82.) upon that locus. And if, at any other and ordinary point, we cut the surface by a plane perpendicular to the circle at that point, we find, by a process of the same kind as some which have been already employed, expressions for the tangential and normal components of the vector chord, whereof the principal terms involve the scalar c_2 as a factor, while the latter varies (ultimately) as the square of the former, so that the curvature of the section is finite and known, but tends to become infinite when c_2 tends to zero.

(100.) If the condition of coincidence (84.) be not satisfied, so that the two branches of the singular line (82.) remain distinct, and that thus $c_2 = 0$, but not $c_3 = 0$ (comp. (91.)), for any ordinary point on one of those two branches, then if we cut the surface at that point by a plane perpendicular to the branch, or to the circle which touches it there, we find an ultimate expression for the vector chord which involves the scalar c_3 as a factor, and of which the normal component varies as the sesquiplicate power of the tangential one: so that we have here the case of a semicubical cusp, and each branch of the singular line is a cusp-edge* of the surface, exactly in the same known sense (comp. (76.)) as that in which a curve of double curvature is generally such, on the developable locus of its tangents.

(101.) But when the condition (84.) is satisfied, so that the two branches *coincide*, and that thus (comp. again (91.)) we have at once the *three* equations,

$$CLXX...c_1 = 0, c_2 = 0, c_3 = 0,$$

then the terms, which were lately the principal ones (100.), disappear: and a

^{*} Compare the Note to page 144.

ART. 398.] INTEGRAL OF THE EQUATION OF CONDITION.

new expression arises, for the vector chord of a section of the surface, made by a plane perpendicular to the singular line, which (when we take t = s, as in (96.)) is found to admit of being identified with the formula CXVII., and of course conducts to precisely the same system of consequences; the tangential component now varying ultimately as the cube, and the normal component as the fourth power of a small variable, so that the cuspidal property of the point P of the section no longer exists, although the curvature at that point is still infinite, as in (74.) : and the Singular Line, reduced now to a single branch, to which all the circles of the system osculate, (92.), (95.), is not a cusp-edge of the Surface, as had been otherwise found before (77.), but a line of a different character,* which may thus be regarded, with reference to a more general Envelope (80.), as the result of a Fusion (84.) of Two Cusp-Edges.

(102.) The condition of such fusion (or coincidence) has been seen (84.) to be expressible by the differential equation of the second order, and second degree,

with

$$g = -\sigma^{\prime 2} - (RR^{\prime})^{\prime}, \qquad \text{CXXXIV}.$$

and with the independent variable arbitrary. And we are now prepared to assign the complete general integral⁺ of this differential equation; namely the system of the two following equations (comp. 395, (7.) and (14.)), of the vector and scalar kinds,

CLXXI...
$$\sigma = \rho + \frac{3 \nabla \rho' \rho'' S \rho' \rho'' + \nabla \rho''' \rho''}{S \rho' \rho'' \rho'''}$$
, and CLXXII... $R = T(\sigma - \rho)$;

in which ρ is an arbitrary vector function of any scalar variable, t, and which express, when geometrically interpreted, that σ is the variable vector of the

+ Compare the first Note to page 147. We say here, general integral, because a less general one, although involving one arbitrary function (of the scalar kind), will soon be pointed out.

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CXXXIV.

 $(RS\sigma'\sigma'' - R'g)^{2} = (R'^{2} + \sigma'^{2}) (R^{2}\sigma''^{2} + g^{2}),$ CXXXVI.

^{*} Compare the Note to page 144. Monge (in page 372 of Liouville's Edition) has the remark, that (when a certain radical vanishes) "les deux branches de la courbe touchée par toutes les caractéristiques se confondent en une seule : et cette courbe, sans cesser d'être une ligne singulière de la surface, n'est plus une arcte de rebroussement, elle est une ligne de striction." The propriety of this last name, "line of striction," appears to the present writer questionable : although he has confirmed, as above, by calculations with quaternions, the result that, in the case referred to, the singular line is not a cusp-edge. Monge does not seem to have perceived that, in the same case of fusion, the curved line in question is not merely louched, but osculated, by all the circles of the system.

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centre s, and that R is the variable radius, of the osculating sphere, to an arbitrary curve (P), of which the variable vector of a point P is ρ .

(103.) In fact, if we met the cited equation of condition CXXXVI., g representing therein the expression CXXXIV., without any previous knowledge of its meaning or origin, we might first, by the rules of quaternions, and as a mere affair of calculation, transform it to the equation CXXXV.; which would evidently allow the assumption of the formula CXXXIII., ρ being treated as an auxiliary vector, which satisfies (in virtue of the supposed condition) the system of the four scalar equations, LXXXIX., XCI., XCII., XCIII.; whence derivating and combining, as in (91.) and (92.), we are led to a new system* of four scalar equations, whereof one is again the equation LXXXIX., and may be written under the form CLXXII.; while the three others are those formerly numbered as 395, VII., and conduct (except in a particular case which we shall presently consider) to the vector expression CLXXI., which conversely is sufficient to represent them, all derivatives of σ and of R being thus eliminated.

* The Equation of Monge (comp. the second Note to page 145) may be considered as the condition of coexistence of the four following equations, in which ϕ , ψ , π are supposed to be functions of *a*, and to be differentiated or derivated as such:

(1)... $(x - \phi)^2 + (y - \psi)^2 + (z - \pi)^2 = a^2;$

(2). . . $(x - \phi)\phi' + (y - \psi)\psi' + (z - \pi)\pi' + a = 0;$

(3). . . $(x - \phi)\phi'' + (y - \psi)\psi'' + (z - \pi)\pi'' + 1 - \phi'^2 - \psi'^2 - \pi'^2 = 0;$

 $(4)...(x-\phi)(\psi'\pi''-\pi'\psi'')+(y-\psi)(\pi'\phi''-\phi'\pi'')+(z-\pi)(\phi'\psi''-\psi'\phi'')=0;$

whereof the first three have been employed by Monge himself, but the fourth does not seem to have been perceived by him, the condition of evanescence of a radical having been used in its stead. And by a translation of quaternion results, above deduced, into the usual language of analysis, it is found that the complete and general integral, of the non-linear differential equation of the second order, which is obtained by the elimination of x, y, z between these four, is expressed by a new system of four equations, the equation (1) being one of them; and the three others, in which x, y, z are now treated as arbitrary functions of a, and are derivated as such, being the following:

$$(5) \cdots (x - \phi)x' + (y - \psi)y' + (z - \pi)z' = 0;
(6) \cdots (x - \phi)x'' + (y - \psi)y'' + (z - \pi)z'' + x'^2 + y'^2 + z'^2 = 0;
(7) \cdots (x - \phi)x''' + (y - \psi)y''' + (z - \pi)z''' + 3(x'x'' + y'y'' + z'z'') = 0.$$

By treating a as a function of some other independent variable, t, the terms + a and + 1, in (2) and (3), come to be replaced by + aa' and $+ aa'' + a'^2$; and the slightly more general form, which Monge's Equation thus assumes, has still its complete general integral assigned by the system (1) (5) (6) (7), if x, y, z (as well as a) be now regarded as arbitrary functions of the new variable t, in the place of which it is permitted (for instance) to take x, and so to write x' = 1, x'' = 0: only two arbitrary functions thus entering, in the last analysis, into the general solution, as was to be expected from the form of the equation.

CASE OF SPHERE THROUGH FIXED POINT. ART. 398.]

(104.) The case just now alluded to, in which the general integral (102.) is replaced by a less general form, is the case (91.) when the variable sphere passes through a fixed point A, to which point, in that case, the singular line And the integral equations,* which then replace CLXXI. reduces itself. and CLXXII. may be thus written :

and

CLXXIII...
$$\sigma = a + t\beta + u\gamma$$
, with $u = F(t)$,
CLXXIV... $R = T(t\beta + u\gamma)$;

the second scalar coefficient, u, being here an arbitrary function of the first scalar coefficient, or of the independent variable t, and a, β , γ being three arbitrary but constant vectors : so that the curve (s) is now obliged to lie in some one planet through the fixed point A, but remains in other respects Accordingly it will be found that this last integral system, arbitrary. although less general than the former system (102.), and not properly included in it, satisfies the differential equation CXXXVI.; whereof the two members acquire, by the substitutions indicated, this common value,

CLXXV...
$$(RS\sigma'\sigma'' - R'g)^2 = \&c. = R^{-2}t^2(tu' - u)^2u''^2(V\beta\gamma)^4.$$

(105.) Other problems might be proposed and resolved, with the help of formulæt already given, respecting the properties or affections of curves

$$(et + lu)^2 + (ft + mu)^2 + (gt + nu)^2 = a^2;$$

abcefglmn being nine arbitrary constants, while t and u are two functions of a, whereof one is arbitrary, but the other is algebraically deduced from it, by means of the fourth equation. The writer is not aware that either of these integrals has been assigned before.

† Compare the first Note to page 150.

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 \ddagger We might for example employ the formula VI. for κ'' , in conjunction with one of the expressions 397, XCI. for κ' , to determine, by the general formula 389, IV., the vector (say ξ) of the centre of curvature of the curve (κ) , and therefore also the radius of curvature of that curve, which is the locus of the centres of curvature of the given curve (P), supposed to be in general one of double curvature. After a few reductions, with the help of XII., we should thus find the equations,

CLXXVII...
$$V \frac{\kappa''}{\kappa'} = \frac{-r'\tau}{r\kappa'} + (r^{-1} - P')\tau,$$

CLXXVIII... $\xi = \kappa + \frac{\kappa'}{V \frac{\kappa''}{\kappa'}} = \kappa + \frac{\sigma - 2\kappa + \rho}{1 - \frac{rdP}{ds} + \frac{\rho ds}{rd\kappa}},$

X 2

^{*} The particular integral corresponding, of the Equation of Monge, is expressed by the following system : $\phi = a + et + lu, \quad \psi = b + ft + mu, \quad \pi = c + gt + nu,$

ELEMENTS OF QUATERNIONS. [III. III. § 6.

in space which depend on the *fourth power* (s⁴) of the *arc*, or on the *fourth* derivative $D_s^4\rho$ or $\tau^{\prime\prime\prime}$ of the vector ρ_s ; but it is time to conclude this series of sub-articles, which has extended to a much greater length than was designed, by observing that, in virtue of the vector form 396, XI. for the equation of a circle of curvature, the Locus (8.) of the Osculating Circle may be concisely but sufficiently represented by the Vector Equation,

CLXXVI...V
$$\frac{2\tau_s}{\omega-\rho_s}+\nu_s=0,$$

which apparently involves only one scalar variable, s, namely, the arc of the curve (P), the other scalar variable, such as t, which corresponds (69.) to the arc of the circle, disappearing under the sign ∇ : and that the surface, which was called in (8.) the Circumscribed Developable, is now seen to be in fact circumscribed to that Locus, or Envelope, in a certain singular (or eminent) sense, as touching it along its Singular Line.

399. When we take account of the *fifth power* (s^5) of the *arc*, the expression for ρ_s receives a *new term*, and becomes (comp. 398, I.),

I...
$$\rho_s = \rho + s\tau + \frac{1}{2}s^2\tau' + \frac{1}{6}s^3\tau'' + \frac{1}{24}s^4\tau''' + \frac{1}{120}s^5\tau^{17};$$

and although some of the consequences of such an expression have been already considered, especially as regards the general determination of what has been above called the Osculating Twisted Cubic to a curve of double curvature, or the gauche curve of the third degree which has contact of the fifth order with a given curve in space, yet, without repeating any calculations already made, some additional light may be thrown on the subject as follows.

in which last the denominator is a quaternion, and the scalar variable is arbitrary : whence also,

CLXXIX. . . Radius of curvature of curve (K), or of locus of centres of osculating circles to a given curve (P) in space, $= T \left(\xi - \kappa \right) = R \left\{ \left(1 - \frac{rd P}{d_{\tau}} \right)^2 + \left(\frac{pr}{Pr} \right)^2 \right\}^{-\frac{1}{2}}$

$$= \pm \frac{Rdr}{pds} \left\{ \left(\frac{1}{r} - \frac{dP}{ds}\right)^2 + \left(\frac{p}{Rr}\right)^2 \right\}^{-\frac{1}{2}};$$

with the verification, that for the case of a *plane curve* (r), for which therefore $\frac{R}{p} = 1$, and $\frac{1}{r} = 0 = \frac{dP}{ds}$, we have thus the elementary expression,

CLXXX... Radius of Curvature of Plane Evolute = $\pm \frac{rdr}{ds}$,

r being still the radius of curvature, and s the arc, of the given curve.

VECTOR EQUATION OF LOCUS OR ENVELOPE. ARTS. 398, 399.]

(1.) As regards the successive deduction of the derived vectors in the formula I., it may be remarked that if we write (comp. 398, LVI., LXI.),

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II. . .
$$\mathbf{D}^{n+1}_{s}\rho = \tau^{(n)} = a_n\tau + b_nr\tau' + c_nr\nu$$
,

we shall have, generally,

III. . .
$$a_{n+1} = a'_n - r^{-1}b_n$$
, $b_{n+1} = b'_n + r^{-1}a_n - r^{-1}c_n$, $c_{n+1} = c'_n + r^{-1}b_n$,

with the initial values,

IV... $a_0 = 1$, $b_0 = 0$, $c_0 = 0$, or **IV'...** $a_1 = 0$, $b_1 = r^{-1}$, $c_1 = 0$;

whence

V... $\begin{cases} a_2 = -r^{-2}, & b_2 = (r^{-1})', & c_2 = r^{-1}r^{-1}, \\ a_3 = 3r^{-3}r', & b_3 = (r^{-1})'' - r^{-3} - r^{-1}r^{-2}, & c_3 = r(r^{-2}r^{-1})', \end{cases}$

as in the expressions 397, VI. for τ'' , and 398, IV. for τ''' ; the corresponding coefficients of τ^{iv} being in like manner found to be,

VI. .
$$\begin{cases} a_4 = -2 (r^{-2})'' + ((r^{-1})')^2 + r^{-2} (r^{-2} + r^{-2}); \\ b_4 = (r^{-1})''' - 2 (r^{-3})' - 3 (r^{-1}r^{-1})'r^{-1}; \\ c_4 = r^{-1} (r^{-1})'' + 3 ((r^{-1})'r^{-1})' - r^{-1}r^{-1} (r^{-2} + r^{-2}); \end{cases}$$

and being sufficient for the investigation of all affections or properties of a curve in space, which depend only on the fifth power of the arc s.

(2.) For the helix the two curvatures are constant, so that all the derivatives of the two radii r and r vanish; the expressions become therefore greatly simplified, and a law is easily perceived, allowing us to sum the infinite series for ρ_s , and so to obtain the following rigorous expressions for the coordinates * x_s , y_s , z_s of this particular curve, instead of those which were

VII'. . .
$$\begin{cases} \mathbf{x}_{s} = l(r^{-1}x_{s} - r^{-1}z_{s}) = l^{2}r^{-1} \sin t, \\ \mathbf{y}_{s} = l^{2}r^{-1} - y_{s} = l^{2}r^{-1} \cos t, \\ z_{s} = l(r^{-1}x_{s} + r^{-1}z_{s}) = l^{2}r^{-1}t, \end{cases}$$

where $l^2r^{-1} = r \sin^2 H$ is the radius of the cylinder, with converse formulæ easily assigned.

^{*} We have here, and in this whole investigation, an instance of the facility with which quaternions can be combined with coordinates, whenever the geometrical nature of a question may render it convenient so to combine them, by offering to our notice any obvious planes of reference. If it be thought useful to pass to a system connected more immediately with the right cylinder than with the helix, we may write,

developed generally in 398, LVIII., but only as far as s⁴ inclusive :

VII. . .
$$x_s = l^3 (\mathbf{r}^{-2}t + r^{-2} \sin t); \quad y_s = l^2 r^{-1} \operatorname{vers} t; \quad z_s = l^3 r^{-1} \mathbf{r}^{-1} (t - \sin t);$$

where l and t are an auxiliary constant and variable, namely,

VIII...
$$l = (r^{-2} + r^{-2})^{-\frac{1}{2}} = r \sin H, \quad t = l^{-1}s,$$

l being thus what was denoted in earlier formulæ by $T\lambda^{-1}$, and *t* being the angle between two axial planes; while the origin is still placed at the point P of the curve, and the tangent, normal, and binormal are still made the axes of *xyz*.

(3.) The cone of the second order, 398, (40.), which has generally a contact of the fifth order with a proposed curve in space, at a point P taken for vertex, has in this case of the helix the equation (comp. 398, LVII. and LXIX.),

IX. . .
$$y^2 = \frac{3}{2} \frac{\mathbf{r}}{r} \left\{ x + \left(\frac{3}{10} \frac{\mathbf{r}}{r} - \frac{7}{10} \frac{r}{\mathbf{r}} \right) z \right\} z.$$

Accordingly it can be shown, by elementary methods, that if we write, for a moment,

X. . .
$$f(t) = 3(t - \sin t)(3t + 7\sin t) - 20 \text{ vers}^2 t$$
,

we have the *eight* evanescent values,

XI...
$$f0 = f'0 = f''0 = f'''0 = f^{\text{IV}}0 = f^{\text{V}}0 = f^{\text{V}}0 = f^{\text{V}}0 = f^{\text{V}}0 = 0$$
;

whence it is easy to infer that this cone IX. has (in the present example, although not generally) a contact as high as the sixth order* with the curve, of which the coordinates have here the expressions VII.; and consequently that the cone in question must wholly contain the osculating twisted cubic to that curve.

(4.) In general, to find a second locus for such a cubic curve, the method of recent sub-articles (398, (38.) &c.) leads us to form the equation (398,

^{*} Or in modern language, seven-point contact, in the sense that the cone passes, in this case, through seven consecutive points of the curve. It may be remarked that the gauche curve of the fourth degree, or the quartie curve, in which this cone cuts the cylinder of revolution whereon the helix is traced (cutting also in it a certain other cylinder of the second order), and which has the point r for a double point, crosses the helix by one of its two branches at that point, while it has seven-point contact with the same helix by its other branch: and that thus the fact of calculation, expressed by the formula XI., is geometrically accounted for.

ART. 399.] OSCULATING TWISTED CUBIC TO HELIX.

LXVI.) of a cylinder of the second order, or briefly of a quadric* cylinder, which like the quadric cone (3.) shall have contact of the fifth order with the proposed curve in space, at the given point P; the ratios of abc, which determine the direction of a generating line PE, being obliged for this purpose to satisfy a certain equation of condition (398, LXVIII.), of which the form indicates that the locus of this line PE is generally a certain cubic cone, having the tangent (say PT) to the curve for a nodal side : along which side it is touched, not only (like the quadric cone) by the osculating plane (z = 0) to that given curve, but also by a second plane, whereof the equation $(gy + hz = 0, or after reductions <math>y - \frac{1}{2}r'z = 0$ shows that the second branch of the cubic cone crosses the first branch, or the quadric cone, or the osculating plane to the curve, at an angle of which the trigonometric cotangent is equal to half the differential of the radius (r) of second curvature, divided by the differential of the arc (s); so that this second tangent plane to the cone coincides with the rectifying plane to the curre, when the second curvature happens to be constant. The tangent PT therefore counts as three of the six common sides of the two cones with p for vertex : and the three other common sides, for the assigning of which it has been shown (in 398, (41.)) how to form a cubic equation in b:c, are the parallels from that point P to the three real or imaginary asymptotes † of the twisted cubic, and are generating lines PE of three quadric cylinders, whereof one at least is necessarily real, and contains, as a second locus, that sought osculating gauche curve of the third degree.

(5.) In applying this general method to the case of the helix, it is found that the cubic cone breaks up, in this example, into a system of a new quadric cone, which touches the former quadric cone IX. along the tangent PT to the curve (the two other common sides of these two cones being imaginary), and of a plane (y = 0), namely the rectifying plane (comp. (4.)) of the helix, or the tangent plane to the cylinder of revolution on which that given curve is traced: and that this last plane cuts the first quadric cone in two real right lines, the tangent being again one of them, and the other having the sought direction of a real asymptote to the sought osculating twisted cubic. Without entering here into details of calculation, the resulting equation of the real‡ quadric cylinder,

^{*} So called by Dr. Salmon, in his Treatise already cited. Compare the second Note to page 129 of these *Elements*.

⁺ Compare again the Note last referred to.

[‡] As regards the two imaginary quadric cylinders, their equations can be formed by the same general method, employing as generating lines the two imaginary common sides (5.), of the cone IX.,

[III. 111. § 6.

on which that sought gauche curve is situated, may be at once stated to be (with the present system of coordinates),

XII...
$$2ry = \left\{ x + \left(\frac{3}{10} \frac{r}{r} - \frac{7}{10} \frac{r}{r} \right) z \right\}^2 + \frac{3}{5} \left(1 + \frac{r^2}{r^2} \right) y^2;$$

in such a manner that if we set aside the right line,

XIII...
$$y = 0$$
, $x + \left(\frac{3}{10}\frac{r}{r} - \frac{7}{10}\frac{r}{r}\right)z = 0$,

which is a common side of the cone IX. and of the cylinder XII., the curve, which is the remaining part of their complete intersection, is the twisted cubic sought. As an elementary verification of the fact, that this gauche curve of intersection IX. XII. has contact of the fifth order with the helix at the point P, it may be observed that if we change the coordinates xyz in XII. to the expressions VII., and write for abridgment,

XIV...
$$F(t) = (3t + 7t \sin t)^2 - 200$$
 vers $t + 60$ vers² t,

we have then (comp. X. XI.) the six evanescent values,

XV...
$$F0 = F'0 = F''0 = F'''0 = F^{\mathsf{IV}}0 = F^{\mathsf{V}}0 = 0.$$

(6.) As another verification, which is at the same time a sufficient proof, of the *à posteriori* kind, that the gauche curve IX. XII. has in fact contact of the *fifth order* with the *helix*, it can be shown that while the coordinates y_s and z_s of the *latter* may (by VII., writing simply x for x_s , and neglecting x^{τ}) be thus developed,

XVI...
$$\begin{cases} y_s = \frac{x^2}{2r} + \frac{x^4}{24r} \left(\frac{3}{r^2} - \frac{1}{r^2}\right) + \frac{x^6}{720r} \left(\frac{45}{r^4} - \frac{24}{r^2r^2} + \frac{1}{r^4}\right), \\ z_s = \frac{x^3}{6rr} + \frac{x^5}{120rr} \left(\frac{9}{r^2} - \frac{1}{r^2}\right), \end{cases}$$

and of that other quadric cone above referred to, which is here a separable part of the general cubic locus, and has for equation,

IX'...
$$\frac{20}{9} y^2 = 5 \frac{r}{r} xz + \left(3 \frac{r^2}{r^2} - 2\right) z^2.$$

It seems sufficient here to remark, that by taking the sum and difference of the equations of those two imaginary cylinders, two new real quadric surfaces are obtained, which also contain the osculating twisted cubic, and intersect each other in that gauche curve: namely two hyperbolic paraboloids, which have a common side at infinity, and of which the equations can be otherwise deduced (by way of verification), without imaginaries, through easy algebraical combinations of the two real equations IX. and XII.

ART. 399.] DEVIATION OF CUBIC FROM HELIX.

the corresponding coordinates y and z of the *former*, that is, of the *curvilinear* part of the *intersection* of the cone IX. with the cylinder XII., have (in the same order of approximation) developments which may be thus abridged,

XVII...
$$y = y_s - \frac{(r^{-2} + r^{-2})^2 x^6}{800 r}, \quad z = z_s.$$

(7.) The deviation of the helix from the gauche curve IX. XII. is therefore of the sixth order (with respect to x, or s), and it has an inward direction, or in other words, the osculating twisted cubic deviates outwardly from the helix, with respect to the right cylinder; the ultimate (or initial) amount of this deviation, or the law according to which it tends to vary, being represented by the formula,

XVII'...
$$y_s - y = \frac{(r^{-2} + r^{-2})^2 s^6}{800r} = \frac{t^4 y_s}{400};$$

where t denotes as in (2.) the *angle*, which a *plane* drawn through a near point P_s , and through the axis of the *right cylinder*,*

XVIII. . .
$$2ry = \left(x - \frac{r}{r}z\right)^2 + \left(1 + \frac{r^2}{r^2}\right)y^2$$
,

whereon the helix is traced, makes with the plane drawn through the same axis of revolution, or through the right line,

XIX...
$$x = \frac{r}{r}z$$
, $y = r^{-1}(r^{-2} + r^{-2})^{-1} = l^2 r^{-1}$,

and through the given point P: while y_s is still the (inward) distance of the same near point P_s , from the tangent plane to the same cylinder at the same given point P.

(8.) If we cut the cone IX., and the cylinder XII., by any plane,

XX...
$$2ry = w \left\{ x + \left(\frac{3}{10} \frac{\mathbf{r}}{r} - \frac{7}{10} \frac{r}{\mathbf{r}} \right) z \right\},$$

drawn through their common side XIII., we obtain two other sides, one for

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^{*} With the coordinates VII'. of a recent Note (to page 157), the equation of this cylinder would be, $XVIII'...x^2 + y^2 = l^4r^{-2}.$

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cach of these two quadric surfaces; and these two new right lines, in this plane XX., intersect each other in a new point,* of which the coordinates xyz are given, as functions of the new variable w, by the *three fractional* expressions,†

XXI...
$$x = \frac{w + \left(\frac{7}{r^2} - \frac{3}{r^2}\right)\frac{w^3}{60}}{1 + \frac{3}{20}\frac{w^2}{l^2}}; \quad 2ry = \frac{w^2}{1 + \frac{3}{20}\frac{w^2}{l^2}}; \quad 6rz = \frac{w^3}{1 + \frac{3}{20}\frac{w^2}{l^2}}$$

while the *twisted cubic*, which osculates (as above) to the helix at r, is the locus of all the points of intersection thus determined. Accordingly, if we develop xyz by XXI., in ascending powers of w, neglecting w^{τ} (or x^{τ}), we are conducted, by elimination of w, to expressions for y and z in terms of x, which agree with those found in (6.), and thereby establish in a new way the existence of the required contact of the *fifth order*, between the two curves of double curvature.

(9.) The *real asymptote* to the cubic curve is found by supposing the auxiliary variable w to tend to infinity in the expressions XXI.; it is therefore the right line (comp. XX.),

XXII...
$$y = \frac{10}{3} \frac{l^2}{r}, \quad x + \left(\frac{3}{10} \frac{r}{r} - \frac{7}{10} \frac{r}{r}\right) z = 0,$$

namely the second side in which the elliptic cylinder XII. is cut by a normal plane through the side XIII.; and by comparing the value of its y with the equation XIX., we see that the least distance between the real asymptote to the osculating twisted cubic, and the axis of revolution of the cylinder on which the helix is traced, is equal to seven-thirds of the radius of that right cylinder.

(10.) As regards the two imaginary asymptotes, they correspond to the two imaginary values of w, which cause the common denominator of the expressions

^{*} The plane XX., as containing the line XIII., is parallel to an asymptote, and therefore meets the cubic at infinity; it also passes through the given point **r**: and therefore it can only cut the twisted cubic in *one other point*, of which the position is expressed by the equations XXI.

⁺ Quaternions suggest such fractional expressions, through the formula 398, LXXIX. for the *vector* $(\phi + c)^{-1}a$; but it is proper to state that expressions of *fractional form*, for the coordinates of a curve in space of the *third order* (or degree) were given by Möbins, who appears to have been the first to discover the existence of *such* gauche curves, and who published several of their principal properties in his *Barycentric Calculus* (der barycentrische Calcul, Leipzig, 1827).

ART. 399.]

XXI. to vanish; but it may be sufficient here to observe, that because those expressions give, generally,

XXIII. . .
$$x + \left(\frac{6}{5}\frac{\mathbf{r}}{r} + \frac{1}{5}\frac{r}{\mathbf{r}}\right)z = w,$$

the two imaginary lines in question are to be considered as being contained in two imaginary planes, which are both parallel to the real plane* through P,

XXIV...
$$x + \left(\frac{6}{5}\frac{\mathbf{r}}{r} + \frac{1}{5}\frac{r}{\mathbf{r}}\right)\mathbf{z} = 0;$$

namely to a certain common normal plane to the two real cylinders XII. and XVIII., or to the elliptic and right cylinders already mentioned.

(11.) In general, instead of seeking to determine, as above, a cylinder of the second order, which shall have contact of the fifth order with any given curve of double curvature, at a given point P, we may propose to find a second cone of the same (second) order, which shall have such contact with that curve at that point, its vertex being at some other point of space (abc). Writing (comp. 398, LXVI.) the equation of such a cone under the form,

XXV. . .
$$2r(cy - bz)(c - z) = (cx - az)^2 + 2B(cx - az)(cy - bz) + C(cy - bz)^2;$$

substituting for xyz the coordinates $x_sy_sz_s$ of the curve, under the forms (comp. 398, LVIII.),

XXVI. . .
$$\begin{cases} x_s = s - \frac{s^3}{6r^2} + \frac{a_3s^4}{24} + \frac{a_4s^5}{120}, \\ y_s = \frac{s^2}{2r} - \frac{r's^3}{6r^2} + \frac{b_3s^4}{24} + \frac{b_4s^5}{120}, \\ z_s = \frac{s^3}{6rr} + \frac{c_3s^4}{24} + \frac{c_4s^5}{120}, \end{cases}$$

in which the coefficients $a_3b_3c_3$ and $a_4b_4c_4$ have the values assigned in (1.); developing according to powers of s, neglecting s⁶, and comparing coefficients of s³, s⁴, s⁵; we find first the expressions,

XXVII...
$$B = \frac{-1}{3}\left(r' + \frac{b}{c}\frac{r}{\mathbf{r}}\right), \quad C = -\frac{4}{9}\left(r' + \frac{b}{c}\frac{r}{\mathbf{r}}\right)^2 + \frac{4}{3}\left(1 + \frac{a}{c}\frac{r}{\mathbf{r}}\right) + \frac{r^3}{3}\left(b_3 - \frac{b}{c}c_3\right),$$

* The right line at infinity, in this plane XXIV., is the common side of the two hyperbolic paraboloids mentioned in the third Note to page 159, as each containing the whole twisted cubic.

which are the same for cone as for cylinder: and then are led to the new equation of condition,

XXVIII. . .
$$\frac{r}{5}\left(b_4 - \frac{b}{c}c_4\right) = a_3 - \frac{a}{c}c_3 + \frac{2}{crr} + B\left(b_3 - \frac{b}{c}c_3 - \frac{2}{r^3} - \frac{2a}{cr^2r}\right) - 2C\left(\frac{r'}{r^3} + \frac{b}{cr^2r}\right)$$

which differs from the corresponding equation for the determination of a cylinder having the same (fifth) order of contact with the curve, but only by the one term $\frac{2}{crr}$ in the second member, which term vanishes when the coordinate c of the vertex is infinite.

(12.) Eliminating B and C, and substituting for $a_3b_3c_3$ and $a_4b_4c_4$ their values V. and VI., we find that the condition XXVIII. may be thus expressed (comp. 398, LXVIII.):

XXIX...
$$ac\left(b-\frac{\mathbf{r}'}{2}c\right)-\mathbf{r}c^2=\mathbf{a}b^3+\mathbf{b}b^2c+\mathbf{c}bc^2+\mathbf{e}c^3$$
;

in which we have written, for abridgment,

XXX...
$$\begin{cases} a = \frac{4}{9} \frac{r}{r}; \quad b = \frac{r'}{3} - \frac{r}{r} \frac{r'}{2}; \\ c = \frac{1}{30} \left(6r''r - 3rr'' - 2r^{-1}r'^{2}r - 6r'r' + 6rr^{-1}r'^{2} - 18r^{-1}r + 12rr^{-1} \right); \\ e = \frac{1}{90} \left(9r'''r^{2} - 9r^{-1}r'r''r^{2} + 4r^{-2}r'^{3}r^{2} + 36r^{-2}r'r^{2} + 18r' - 27rr^{-1}r' \right). \end{cases}$$

The locus of the vertex of the sought quadric cone XXV. is therefore that cubic surface, or surface of the third order, which is represented by the equation XXIX. in abc; this surface, then, is a second locus (comp. (4.)) for the osculating twisted cubic, whatever the given curve in space may be: a first locus for that cubic curve being still the quadric cone (comp. (3.)), of which the equation in abc is (by 398, LXVII. and LXIX.),

XXXI...
$$4\left(\frac{\mathbf{r}}{r}\right)^2 b^2 = 6\left(\frac{\mathbf{r}}{r}\right)^3 ac + \left(\frac{\mathbf{r}^3}{r^2}\right)' bc$$

+ $\frac{\mathbf{r}^4}{5}\left(\frac{9}{r^4} - \frac{21}{r^2\mathbf{r}^2} + \frac{r'^2}{r^4} - \frac{3r''}{r^3} + \frac{3r'\mathbf{r}'}{r^3\mathbf{r}} - \frac{27\mathbf{r}'^2}{4r^2\mathbf{r}^2} + \frac{9\mathbf{r}''}{r^2\mathbf{r}}\right)c^2,$

ART. 399.] RULED CUBIC LOCUS, CUBIC CYLINDER.

and which has contact of the *fifth order* with the *curve*, while its *vertex* is at the given point **P** of osculation.*

(13.) Instead of thus introducing, as *data*, the *derivatives* of the two *radii* of curvature, r and r, taken with respect to the *arc*, s, it may be more convenient in many applications to treat the two coordinates y and z of the curve as functions of the third coordinate x, assumed as the independent variable : and so to write (comp. (6.)) these new developments,

XXXII...
$$y_x = \frac{x^2}{2r} + \frac{y'''x^3}{6} + \frac{y^{v}x^4}{24} + \frac{y^{v}x^5}{120}, \qquad z_x = \frac{x^3}{6rr} + \frac{z^{v}x^4}{24} + \frac{z^{v}x^5}{120};$$

and then the equation of the quadric cone XXXI. will be found to become (in xyz),

XXXIII...
$$y^2 = \frac{3}{2} \frac{r}{\mathbf{r}} xz + 2gyz + hz^2$$
,

with the coefficients,

XXXIV...
$$g = rr\left(y^{\prime\prime\prime} - \frac{3}{8}rz^{1v}\right), \quad h = \frac{3}{2}rr^{2}\left(y^{1v} - \frac{3}{10}rz^{v}\right)$$
$$- r^{2}r^{2}\left(y^{\prime\prime\prime\prime} + \frac{3}{4}rz^{1v}y^{\prime\prime\prime} - \frac{9}{16}r^{2}z^{1v^{2}}\right);$$

while the cubic surface XXIX. will also come to be represented by an equation of the same form as before, namely (in xyz) by the following,

$$XXXV. \ldots xz (y + hz) - rz^2 = ay^3 + by^2z + cyz^2 + ez^3,$$

in which the coefficients are,

$$XXXVI... \begin{cases} \mathbf{a} = \frac{4}{9} \frac{r}{\mathbf{r}} (\text{as before}); \quad \mathbf{b} = -\frac{4}{3} r^2 y''' + \frac{r^2 \mathbf{r}}{2} z^{1\mathbf{v}}; \quad \mathbf{h} = -r \mathbf{r} y''' + \frac{1}{2} r^2 z^{1\mathbf{v}}; \\ \mathbf{c} = \frac{4}{9} r^3 \mathbf{r} y'''^2 - \frac{1}{2} r^3 \mathbf{r}^2 y''' z^{1\mathbf{v}} - \frac{1}{2} r^2 \mathbf{r} y^{1\mathbf{v}} + \frac{1}{10} r^2 \mathbf{r}^2 z^{\mathbf{v}}; \\ \mathbf{e} = -\frac{4}{9} r^4 \mathbf{r}^2 y'''^3 + \frac{1}{2} r^3 \mathbf{r}^2 y''' y^{1\mathbf{v}} - \frac{1}{10} r^2 \mathbf{r}^2 y^{\mathbf{v}}. \end{cases}$$

(14.) Whichever set of expressions for the *coefficients* we may adopt, some general consequences may be drawn from the mere *forms* of the *cquations*,

^{*} The quadric cone XXXI. may be said to have *five-side contact* with the *cone of chords* of the given curve (compare the Note to page 125).

[III. III. § 6.

XXXI. and XXIX., or XXXIII. and XXXV., of the quadric cone and cubic surface, considered as two loci (12.) of the osculating twisted cubic to a given curve of double curvature. Thus, if we eliminate ac (comp. 398, (41.)) from XXIX. by XXXI., or xz by XXXIII. from XXXV., we get an equation between b, c, or between y, z, which rises no higher than the third degree, and is of the form,

XXXVII... $2\mathbf{r}z^2 = \mathbf{a}y^3 + \mathbf{b}_y y^2 z + \mathbf{c}_y z^2 + \mathbf{e}_z z^3$,

with the same value of a as before; such then is the equation of the projection of the twisted cubic, on the normal plane to the curve; and we see that, as was to be expected, the plane cubic thus obtained has a cusp at the given point P, which (when we neglect s^7 or x^7) coincides with the corresponding cusp* of the projection of the given curve of double curvature *itself*, on the same normal plane.

(15.) The equation XXXVII. may also be considered as representing a *cubic cylinder*, which is a *third locus* of the twisted cubic; and on which the *tangent* PT to the curve is a *cusp-edge*, in such a manner that an arbitrary *plane through this line*, suppose the plane

XXXVIII. \dots 3rz = vy,

where v is any assumed constant, cuts the cylinder in that line twice, and a third time in a real and parallel right line, which intersects the quadric cone in a point at infinity (because the tangent PT is a side of that cone), and in another real point, which is on the twisted cubic, and may be made to be any point of that sought curve, by a suitable value of v: in fact, the plane XXXVIII. touches both curves at P, and therefore intersects the cubic curve in one other real point. And thus may fractional expressions (comp. (8.)) for the coordinates of the osculating cubic be found generally, which we shall not here delay to write down.

(16.) Without introducing the cubic cylinder XXXVII., it is easy to see that any plane, such as XXXVIII., which is tangential to the given curve at r, cuts the cubic surface XXXV. in a section which may be said to consist of the tangent twice taken, and of a certain other right line, which varies with the direction of this secant plane, so that the locus XXXV. or XXIX. is a Ruled

^{*} Compare the first formula of the Note to page 133.

ABTS. 399, 400.] OSCULATING TWISTED CUBIC.

Cubic Surface, with the given tangent PT for a singular^{*} line, which is intersected by all the other right lines on that surface, determined as above: and if we set aside this line, the remaining part of the complete intersection of that cubic surface with the quadric cone XXXIII. or XXXI. is the twisted cubic sought. We may then consider ourselves to have completely and generally determined the Osculating Twisted Cubic to a curve of double curvature, without requiring (as in 398, (41.)), the solution of any cubic or other equation.[†]

(17.) As illustrations and verifications, it may be added that the general *ruled cubic surface*, and *cubic cylinder*, lately considered, take for the case of the *helix* (2.), the particular forms,[‡]

and

XXXIX...
$$xyz - rz^2 = \frac{4}{9}\frac{r}{r}y^3 + \left(\frac{2}{5}\frac{r}{r} - \frac{3}{5}\frac{r}{r}\right)yz^2$$
,
XL... $rz^2 = \frac{2}{9}\frac{r}{r}y^3 + \frac{3}{10}\left(\frac{r}{r} + \frac{r}{r}\right)yz^2$;

and that accordingly these two last equations are satisfied, independently of w, when the *fractional expressions* XXI. are substitued for xyz.

400. The general theory § of evolutes of curves in space may be briefly treated by quaternions, as follows: a second curve (in space, or in one plane) being defined to bear to a first curve the relation of evolute to involute, when the first cuts the tangents to the second at right angles.

(1.) Let ρ and σ be corresponding vectors, or and os, of involute and evolute, and let $\rho', \sigma', \rho'', \sigma''$ denote their first and second derivatives, taken

[‡] By suppressing the term - rz^2 , dividing by $\frac{ry}{5r}$, and transposing, we pass for the case of the

helix from the equation XXXIX. of the cubic locus, to the equation IX'. in the last Note to page 159; namely to the equation of that quadric cone which forms (in this example) a separable part of the general cubic cone, the other part being here the tangent plane (y = 0) to the right cylinder.

§ Invented by Monge.

^{*} If the cubic surface be cut by a plane perpendicular to the tangent \mathbf{r} , at any point \mathbf{r} distinct from the point \mathbf{r} itself, the section is a plane cubic, which has \mathbf{r} for a double point; and this point counts for three of the six common points, or points of intersection, of the plane cubic just mentioned with the plane conic in which the quadric conc is cut by the same secant plane, because one branch, or one tangent, of the plane cubic at \mathbf{r} touches the plane conic at that point, in the osculating plane to the given curve at \mathbf{r} , while the other branch, or the other tangent, cuts that plane conic there.

⁺ It may be remarked that, by equating the second member of XXXVII. to zero, and changing y, z to b, c, we obtain generally the *cubic equation*, referred to in 398, (41.); and that by suppressing the term $-rc^2$ in XXIX., or the term $-rz^2$ in XXXV., we pass, in like manner generally, from the *cubic surface* of recent sub-articles, to the earlier *cubic cone* (4.).

with respect to a scalar variable t, on which they are both conceived to depend. Then the two fundamental equations, which express the relation between the two curves, as above defined, are the following:

I...
$$S(\sigma - \rho)\rho' = 0$$
; II... $V(\sigma - \rho)\sigma' = 0$;

which express, respectively, that the point s is in the normal plane to the involute at P, and that the latter point is on the tangent to the evolute at s: so that the locus of P (the involute) is a rectangular trajectory to all such tangents to the locus of s (the evolute).

(2.) Eliminating $\sigma - \rho$ between the two preceding equations, and taking their derivatives, we find,

III... $S\rho'\sigma' = 0$, IV... $S(\sigma - \rho)\rho'' - \rho'^2 = 0$, $V... V(\sigma - \rho)\sigma'' - V\rho'\sigma' = 0$; whence also, $VI... S\rho'\sigma'\sigma'' = 0$.

(3.) Interpreting these results, we see first, by IV. combined with I. (comp. 391, (5.)), that the point s of the evolute is on the polar axis of the involute at P, and therefore that the evolute itself is some curve on the polar developable of the involute; and second, by VI. (comp. 380, I.), that this curve is a geodetic line on that polar surface, because the osculating plane to the evolute at s contains the tangent to the involute at P, and therefore also the (parallel) normal to the locus of evolutes.

(4.) The locus of centres of curvature (395, (6.)) of a curve in space is not generally an evolute of that curve, because the tangents* $\kappa\kappa'$ to that locus do not generally intersect the curve at all; but a given plane involute has always the locus just mentioned for one of its evolutes; and has, besides, indefinitely many others, \dagger which are all geodetics on the cylinder which rests perpendicularly on that one plane evolute as its base.

$$-\operatorname{SU}\kappa'\lambda = \pm R^{-1}\mathrm{T}\lambda^{-1} = \pm \sin H \cos P;$$

$$(\mathbf{S}\boldsymbol{\beta}^{-1}\boldsymbol{\rho})^2 + (\mathbf{S}\boldsymbol{\gamma}^{-1}\boldsymbol{\rho})^2 = 1, \quad \mathbf{S}\boldsymbol{\beta}\boldsymbol{\gamma}\boldsymbol{\rho} = 0,$$

the evolutes are geodetics on the cylinder of which the corresponding equation is,

$$(S\beta\sigma)^{\frac{3}{2}} + (S\gamma\sigma)^{\frac{3}{2}} = (\beta^2 - \gamma^2)^{\frac{3}{2}}.$$

^{*} It might have been remarked, in connexion with a recent series of sub-articles (397), that this tangent $\kappa \kappa'$ or κ' is inclined to the rectifying line λ , at an angle of which the cosine is,

upper or lower signs being taken, according as the second curvature r^{-1} is positive or negative, because $S\kappa'\lambda = -r^{-1}$.

[†] Compare the Note to page 53; from the formulæ of which page it now appears, that if the *involute* be an *ellipse*, with $\beta = oB$ and $\gamma = oc$ for its major and minor semiaxes, and therefore with the scalar equations,

ART. 400.]

INVOLUTES AND EVOLUTES IN SPACE.

(5.) An easy combination of the foregoing equations gives,

VII. . .
$$(T(\sigma - \rho))' = -S(U(\sigma - \rho) \cdot (\sigma' - \rho')) = \mp S\sigma'U\sigma' = \pm T\sigma',$$

or with differentials,

VIII. . . $dT(\sigma - \rho) = \pm T d\sigma;$

whence by an immediate integration (comp. 380, XXII. and 397, LIV.),

IX. . . $\Delta T(\sigma - \rho) = \pm \int T d\sigma = \pm \operatorname{arc} \ of \ the \ evolute :$

this arc then, between two points such as s and s_1 of the latter eurve, is equal to the difference between the lengths of the two lines, rs and r_1s_1 , intercepted between the two curves themselves.

(6.) Another quaternion combination of the same equations gives, after a few steps of reduction, the differential formula (comp. 335, VI.),

X... d cos ops =
$$- dSU \frac{\sigma - \rho}{\rho} = \frac{dT\rho}{T(\sigma - \rho)} \cdot S\frac{\sigma}{\rho};$$

if then the *involute* be a curve on a given sphere, with its centre at the origin o, so that the *evolute* is a geodetic on a concentric cone, this differential X. vanishes, and we have the integrated equation,

XI... $\cos ops = const.$, or simply, XI'... ops = const.;

the tangents rs to the evolute being thus inclined (in the case here considered) at a constant angle,* to the radii or of the sphere.

(7.) In general, if we denote by R the interval \overline{PS} between two corresponding points of involute and evolute, we shall have the equation,

XII. . . $(\sigma - \rho)^2 + R^2 = 0$, or XII'. . . T $(\sigma - \rho) = R$;

and the formula VII. may be replaced by the following,

XIII...
$$R'^2 + \sigma'^2 = 0$$
, or XIII'... $D_t R = \pm T D_t \sigma$,

in which the independent variable t is still left arbitrary.

^{*} This property of the evolutes of a spherical curve was deduced by Professor De Morgan, in a Paper On the Connexion of Involute and Evolute in Space (Cambridge and Dublin Mathematical Journal for November, 1851); in which also a definition of involute and evolute was proposed, substantially the same as that above adopted.

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XIV... $t = \int \mathrm{Td}\sigma$, XV... $\mathrm{d}R_t = \pm \mathrm{d}t$, XVI... $\mathrm{D}_t R_t = \pm 1$; whence

XVII... $D_t(R_t \mp t) = 0$, and XVIII... $R_t \mp t = \text{const.} = R_0$,

the integral IX. being thus under a new form reproduced.

(9.) In this last mode of obtaining the result,

XIX...
$$\Delta \overline{Ps} = R_t - R_0 = \pm t = \pm \operatorname{arc} s_0 s_t$$
 of evolute,

no use is made of infinitesimals,* or even of small differentials. We only infer, as in XVIII. (comp. 380, (9.)), that the quantity $R_t \mp t$ is constant, because its derivative is null: it having been previously proved (380, (8.)), as a consequence of our definition of differentials (320, 324) that if s be the arc and ρ the vector of any curve, then the equation $ds = \text{Td}\rho$ (380, XXII.) is rigorously satisfied, whatever the independent variable t may be, and whether the two connected and simultaneous differentials be small or large.

(10.) But when we employ the notation of integrals, and introduce, as above, the symbol $\int Td\sigma$, we are then led to interpret that symbol as denoting the limit of a sum (comp. 345, (12.)); or to write, generally,

XX...
$$\int T d\rho = \lim \Sigma T \Delta \rho$$
, if $\lim \Delta \rho = 0$,

with analogous formulæ for other cases of *integration in quaternions*. Geometrically, the equation,

XXI...
$$\int T d\rho = \Delta s$$
, or XXI'... $\int T d\sigma = \Delta t$,

if s and t denote arcs of curves of which ρ and σ are vectors, comes thus to be interpreted as an expression of the well-known principle, that the perimeter of any curve (or of any part thereof) is the limit of the perimeter of an inscribed polygon (or of the corresponding portion of that polygon), when the number

[•] In general, it may have been observed that we have hitherto abstained, at least in the text of this whole Chapter of Applications, from making any use of infinitesimals, although they have been often referred to in these Notes, and employed therein to assist the geometrical investigation or enunciation of results. But as regards the mechanism of calculation, it is at least as easy to use infinitesimals in quaternions as in any other system : as will perhaps be shown by a few examples, farther on.

⁺ Compare the Note to page 30.

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of the sides is indefinitely increased, and when their lengths are diminished indefinitely.

(11.) The equations I. and XII. give,

XXII...
$$S\sigma'(\sigma - \rho) + RR' = 0$$
,

the independent variable t being again arbitrary; but these equations XII. and XXII. coincide with the formulæ 398, LXXXIX. and XCI.; we may then, by 398, (79.) and (80.), consider the *locus of the point* P as the *envelope* of a variable sphere, namely of the sphere which has s for centre and R for radius, and is represented by the recent equation XII., if $\rho = oP$ be the vector of a variable point thereon.

(12.) But whereas such an envelope has been seen to be generally a surface, which is real or imaginary (398, (79.)) according as $R'^2 + \sigma'^2 < \text{or} > 0$, we have here by XIII. the intermediate or limiting case (comp. 398, CXXXI.), for which the circles of the system become points, and the surface itself degenerates into a curve, which is here the involute (P) above considered. The involutes of a given curve (s) are therefore included, as a limit, in that general system of envelopes which was considered in the lately cited subarticles, and in others immediately following.

(13.) The equation of condition, 398, CXXXVI., is in this case satisfied by XIII., both members vanishing; but we cannot now put it under the form 398, CXLI., because in the passage to that form, in 398, (85.), there was tacitly effected a division by r^2 , which is not now allowed, the radius r of the circle on the envelope being in the present case equal to zero. For a similar reason, we cannot now divide by g, as was done in 398, (86.); and because, in virtue of II., the *two* equations 398, CLX. reduce themselves to one, they no longer conduct to the formulæ 398, CLX'. CLXI. CLXI'. CLXIII. XCIV.; nor to the second equation 398, CLXIII.

(14.) The general geometrical relations of the curves (P) and (s), which were investigated in the sub-articles to 398 for the case when the condition*

$$\rho = \sigma - RR'^{-1}\sigma' + (U\sigma' + \sqrt{-1}) V\sigma'\mu;$$

^{*} If, without thinking of evolutes, we merely suppose that the condition 398, CXXXVI. is satisfied, as lately in (13.), by our having the relation $R'^2 + \sigma'^2 = 0$, it will be found (comp. the symbolical expression 274, XX. for 0^4 , and the imaginary solution in 353, (18.) of the system $S\gamma\rho = 0$, $\rho^2 = 0$), that the envelope of the sphere $(\sigma - \rho)^2 + R^2 = 0$, or the locus of the (null) circles in which such spheres are (conceived to be) cut by the (tangent) planes, $S\sigma'(\sigma - \rho) + RR' = 0$, may be said to be generally the system of all those imaginary points, of which the vectors (or the bivectors, comp. 214, (6.)) are assigned by the formula,

above referred to is satisfied, are therefore only very *partially* applicable to a system of *involute* and *evolute* in space: at least if we still consider the *former* curve (the involute) as being a *rectangular trajectory* to the *tangents* to the *latter* (the evolute), instead of being, like the curve (P) previously considered, a rectangular trajectory (398, (94.)) to the osculating planes* of the curve (s).

(15.) If the arc of the evolute be again taken for the independent variable t, and if the positive direction of motion along that arc be always towards the involute, we may write,

XXIII...
$$\rho = \sigma + R\sigma', \quad R' = -1, \quad \sigma'^2 = -1, \&c.$$

XXIV... $\rho' = R\sigma'', \quad \rho'' = R\sigma''' - \sigma'', \quad \nabla \rho'' \rho' = R^2 \nabla \sigma''' \sigma'';$

whence

if then $\kappa = 0$ k be the vector of the centre κ of the circle which osculates to the involute at P, the general formula 389, IV. gives, after a few reductions,[†] the expression (comp. 397, XVI. XXXIV., and XCVIII. (15.)),

XXV...
$$\kappa = \rho + \frac{\rho'^3}{\nabla \rho'' \rho'} = \sigma + R\left(\sigma' + \frac{\sigma''^3}{\nabla \sigma''' \sigma''}\right)$$

= $\sigma + \frac{RS\sigma'\sigma'''\sigma''}{\nabla \sigma'' \sigma''} = \sigma - \frac{RS\sigma'\sigma''^{-1}\sigma'''}{\nabla \sigma'' \sigma''^{-1}}$
= $\sigma - Rr_1^{-1}\lambda_1^{-1} = \sigma + U\lambda_1 \cdot R \cos H_1$,

if r_1 , H_1 , and λ_1 be what r, H, and λ in 397 become, when we pass from the curve (r) to the curve (s), with the present relations between those two curves; this centre of curvature κ is therefore the foot of the perpendicular let fall from the point P of the involute, on the rectifying line λ_1 of

where μ is an arbitrary vector, and $\sqrt{-1}$ is the old imaginary of algebra. By making $\mu = 0$ we reduce this expression for ρ to the real vector form,

$$\rho = \sigma - RR'^{-1}\sigma' = \sigma + RR'\sigma'^{-1},$$

= the κ of 398, CXXXI."; and thus the eurve (P), which is here the locus of the centres of the null eircles of contact, and coincides with the involute in the present series of sub-articles, may still be called a Singular Line upon the Envelope of the Sphere (with One Variable Parameter), as being in the present case the only real part of that elsewhere imaginary surface.

* The curve to the osculating planes of which another curve is thus an orthogonal trajectory, and which is therefore (398, (95.)) the cusp-edge of the polar developable of the latter curve, was called by Lancret its evolute by the plane (developpée par le plan); whereas the curve (s) of the present series (400) of sub-articles, to whose tangents the corresponding curve (r) is an orthogonal trajectory, has been called by way of distinction the evolute by the thread (developpée par le fil) of this last curve. It would be improper to delay here on subjects so well known to geometers: but the student may be invited to read again, in connexion with them, the sub-articles (88.) and (89.) to Art. 398.

† Especially by observing that $V\sigma'V\sigma''\sigma'' = -\sigma''^3$, because $S\sigma'\sigma'' = 0$, and $S\sigma'\sigma''' = -\sigma''^2$.

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ARTS. 400, 401.] CURVATURE OF HODOGRAPH OF EVOLUTE.

the evolute: as indeed is evident from geometrical considerations, because by (3.) this rectifying line of the curve (s) is the polar axis of the curve (P).

(16.) If we conceive (comp. 389, (2.)) an *auxiliary spherical curve* to be described, of which the variable unit-vector shall be,

XXVI... or
$$= \tau = \sigma' = U(\rho - \sigma) = R^{-1}(\rho - \sigma),$$

and suppose that v is the vector ou of the centre of curvature of this *new* curve, at the point τ which corresponds to the point s of the evolute, we shall then have by XXV. the expression,

XXVII...
$$TU = v - \tau = \frac{\tau'^3}{\nabla \tau'' \tau'} = \frac{\sigma''^3}{\nabla \sigma''' \sigma''} = \frac{\kappa - \rho}{R} = PK : \overline{PS};$$

we have therefore this theorem, that the inward radius of curvature of the hodograph of the evolute (conceived to be an orbit described, as in 379, (9.), with a constant velocity taken for unity) is equal to the inward radius of curvature of the involute, divided by the interval R between the two curves (P) and (s): and that these two radii of curvature, TU and PK, have one common direction, at least if the direction of motion on the evolute be supposed, as in (15.), to be towards the involute.

(17.) The following is perhaps a simpler enunciation of the theorem * just stated :—If P, P₁, P₂, ... and s, s₁, s₂, ... be corresponding points of involute and evolute, and if we draw lines $sT_1 || s_1P_1, sT_2 || s_2P_2$, ... with a common length = \overline{sP} , the spherical curve PT_1T_2 ... will then have contact of the second order with the curve PP_1P_2 ..., that is with the involute at P.

401. The fundamental formula 389, IV., for the vector of the centre of the osculating circle to a curve in space, namely the formula,

I...,
$$\kappa = \rho + \frac{\rho'^3}{\nabla \rho'' \rho'}$$
, or II..., $\kappa = \rho + \frac{d\rho^3}{\nabla d^2 \rho d\rho}$,

which has been so extensively employed throughout the present Section, has hitherto been established and used in connexion with *derivatives* and

$$\tau + \frac{\tau'}{V\tau''\tau'^{-1}} = \tau - \frac{\tau'}{\lambda} = -r^{-1}\lambda^{-1} = U\lambda \cdot \cos H.$$

^{*} Some additional light may be thrown on this theorem, by comparing it with the construction in 397, (48.); and by observing that the equations 397, XVI. XXXIV. give generally, in the notations of the Article referred to, for the vector of the centre of curvature of the hodograph of any curve, the transformations,

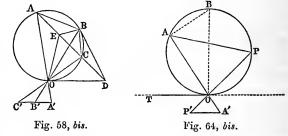
differentials of vectors, rather than with *differences*, great or small. We may however establish, in another way, an essentially *equivalent* formula, into which *differences* enter by their *limits* (or rather by their *limiting relations*), namely, the following,

III. . .
$$\kappa = \rho + \lim_{n \to \infty} \frac{\Delta \rho^3}{\nabla \Delta^2 \rho \Delta \rho}$$
, if $\lim_{n \to \infty} \Delta \rho = 0$, and $\lim_{n \to \infty} \frac{\Delta^2 \rho}{\Delta \rho} = 0$,

the denominator $\nabla \Delta^2 \rho \Delta \rho$ being understood to signify the same thing as $V(\Delta^2 \rho \cdot \Delta \rho)$; and then may, if we think fit, interpret the differential expression II. as if $d\rho$ and $d^2\rho$ in it denoted infinitesimals,* of the first and second orders : with similar interpretations

in other but analogous investigations.

(1.) If in the second expression 316, L., \dagger for the perpendicular from 0 on the line AB, we change a and β to their reciprocals (compare figures 58, 64,



pp. 293, 349, vol. i.) and then take the reciprocal of the result, we obtain this new expression [but with the letters c and D referring to points not marked in fig. 58],

IV... od =
$$\delta = \frac{a^{-1} - \beta^{-1}}{\nabla \beta^{-1} a^{-1}} = \frac{a(\beta - a)\beta}{\nabla \beta a} = \frac{OA \cdot AB \cdot OB}{V(OB \cdot OA)^2}$$

in the denominator of which, OB may be replaced by AB, or by AO + AB, for the diameter OD of the circle OAB; so that if c be the centre of this circle, its vector $\gamma = \text{OC} = \frac{1}{2}\text{OD} = \frac{1}{2}\delta = \&c$. Supposing then that P, Q, R are any three points of any given curve in space, while o is as usual an arbitrary origin, and writing

V... OP =
$$\rho$$
, OQ = $\rho + \Delta \rho$, OR = $\rho + 2\Delta \rho + \Delta^2 \rho$,

and therefore

VI...
$$PQ = \Delta \rho$$
, $QR = \Delta \rho + \Delta^2 \rho$, $\frac{1}{2}PR = \Delta \rho + \frac{1}{2}\Delta^2 \rho$,

* Compare 345, (17.), and the first Note to page 170.

† [Namely $\rho = \frac{V\beta\alpha}{\alpha - \beta}$ on page 427, vol. i.]

[III. III. § 6.

ABT. 401.] OSCULATING CIRCLES BY INFINITESIMALS.

the centre c of the circle PQR has the following rigorous expression for its vector:

VII. . . oc =
$$\gamma = \rho + \frac{\Delta \rho (\Delta \rho + \Delta^2 \rho) (\Delta \rho + \frac{1}{2} \Delta^2 \rho)}{V(\Delta^2 \rho \cdot \Delta \rho)};$$

whence passing to the *limit*, we obtain successively the expressions III. and II. for the vector κ of the *centre of curvature* to the curve PQR at P; the two other points, Q and R, being both supposed to approach indefinitely to the given point P, according to any law (comp. 392, (6.)), which allows the two successive vector chords, PQ and QR, to bear to each other an ultimate ratio of equality.

(2.) Instead of thus first forming a rigorous expression, such as VII., involving the differences $\Delta\rho$ and $\Delta^2\rho$; then simplifying the formula so found, by the rejection of terms, which become indefinitely small, with respect to the terms retained; and finally changing differences to differentials (comp. 344, (2.)), namely $\Delta\rho$ to $d\rho$, and $\Delta^2\rho$ to $d^2\rho$, in the homogeneous expression which results, and of which the limit is to be taken : we may abridge the calculation, by at once writing the differential symbols, in place of differences, and at once suppressing any terms, of which we foresee that they must disappear from the final result. Thus, in the recent example, when we have perceived, by quaternions, that if κ be the centre of the circle PQR, the equation

VIII. . . PK =
$$\frac{PQ \cdot QR \cdot \frac{1}{2}(PQ + QR)}{V\{(QR - PQ)PQ\}}$$

is rigorous, we may at once change each of the three factors of the numerator to $d\rho$, while the factor QR – PQ in the denominator is to be changed to $d^2\rho$; and thus the differential expression II., for the inward vector-radius of curvature $\kappa - \rho$, is at once obtained.

(3.) It is scarcely necessary to observe, that this expression for that radius, as a vector, agrees with and includes the known expressions for the same radius of curvature of a curve in space, considered as a (positive) scalar, which has been denoted in the present Section by the italic letter r (because the more usual symbol ρ would have here caused confusion). Thus, while the formula II. gives immediately (because $Td\rho = ds$) the equation,

IX. . .
$$r^{-1}ds^3 = T\nabla d\rho d^2\rho$$
,

it gives also (because $d\rho^2 = -ds^2$, and $Sd\rho d^2\rho = -dsd^2s$) the transformed equation,

X...
$$r^{-1}ds^2 = \sqrt{(Td^2\rho^2 - d^2s^2)};$$

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and it conducts (by 389, VI.) to this still simpler formula (comp. the equation $r^{-1} = T\tau'$, 396, IX.),

$$XI...r^{-1}ds = TdUd\rho.$$

(4.) Accordingly, if we employ the standard trinomial form (295, I.) for a vector,

XII...
$$\rho = ix + jy + kz$$

which gives, by the laws of the symbols ijk (182, 183),

$$XIII. \dots \begin{cases} d\rho = idx + jdy + kdz, & ds = Td\rho = \sqrt{(dx^2 + dy^2 + dz^2)}, \\ d^2\rho = id^2x + jd^2y + kd^2z, & Td^2\rho = \sqrt{(d^2x^2 + d^2y^2 + d^2z^2)}, \\ Vd\rho d^2\rho = i(dyd^2z - dzd^2y) + j(dzd^2x - dxd^2z) + k(dxd^2y - dyd^2x), \\ Ud\rho = i\frac{dx}{ds} + j\frac{dy}{ds} + k\frac{dz}{ds}, & dUd\rho = id\frac{dx}{ds} + \dots, \end{cases}$$

the recent equations IX. X. XI. take these known forms :

$$\begin{split} \mathbf{IX'.} & . \ r^{-1}\mathrm{d}s^3 = \sqrt{((\mathrm{d}y\mathrm{d}^2z - \mathrm{d}z\mathrm{d}^2y)^2 + . .)};\\ \mathbf{X'.} & . \ r^{-1}\mathrm{d}s^2 = \sqrt{(\mathrm{d}^2x^2 + \mathrm{d}^2y^2 + \mathrm{d}^2z^2 - \mathrm{d}^2s^2)};\\ \mathbf{XI'.} & . \ r^{-1}\mathrm{d}s = \sqrt{((\mathrm{d}\frac{\mathrm{d}x}{\mathrm{d}s})^2 + (\mathrm{d}\frac{\mathrm{d}y}{\mathrm{d}s})^2 + (\mathrm{d}\frac{\mathrm{d}z}{\mathrm{d}s})^2)}. \end{split}$$

(5.) The formula IV., which lately served us to determine a diameter of a circle through three given points, may be more symmetrically written as follows. If AD be a diameter of the circle ABC, then

$$XIV...AD.V(AB.BC) = AB.BC.CA;$$

an equation^{*} in which V(AB.BC) may be changed to V(AB.AC), &c., and in

* A student might find it useful practice to verify, that if we write in like manner,

XIV'. . . BE .V(BC . CA) = BC . CA . AB,

so that BE is a second diameter, then AB = ED, or ANDE is a parallelogram. He may employ the principles, that $\alpha\beta\gamma = \gamma\beta\alpha$, if $S\alpha\beta\gamma = 0$, and that $\beta\gamma - \gamma\beta = 2V\beta\gamma$; in virtue of which, after subtracting XIV'. from XIV., and dividing by V(BC.CA), or by its equal V(AB.BC), the equation AD - BE = 2AB is obtained, and proves the relation mentioned. It is easy also to prove that

$$XIV''$$
... BD. $V(BC.CA) = AB.S(BC.CA)$,

and therefore that ABDE is a rectangie.

which it may be remarked that each member is an expression (comp. 296, V.) for a vector AT, which touches at A the segment ABC: while its length is at once a representation of the product of the lengths of the sides of the triangle ABC, and also of the double area of that triangle (comp. 281, XIII.), multiplied by the diameter of the circumscribed circle.

(6.) In general, if PQRS be any four concircular points, they satisfy (by 260, IX., comp. 296, (3.)) the condition of concircularity,

$$\mathbf{X}\mathbf{V}$$
... $\mathbf{V}\left(\frac{\mathbf{PS}}{\mathbf{SQ}}\cdot\frac{\mathbf{QR}}{\mathbf{RP}}\right)=0$,

which may be thus transformed :*

$$XVI...V\left(\frac{PQ}{PS} + \frac{QP + QR}{PR}\right) = V\left(\frac{1}{PS} \cdot PQ \cdot \frac{QP + QR}{PR}\right)$$

Writing then (comp. VI., and the remarks in (2.)),

XVII. . . PS = $\omega - \rho$, PQ = $d\rho$, PR = $2d\rho + d^2\rho$, QP + QR = $d^2\rho$,

the second member is seen to be, on the present plan, an infinitesimal of the second order, which is therefore to be suppressed, because the first member is only of the first order; and thus we obtain at once the following rector equation of the osculating circle to the curve PQR at P,

XVIII...
$$V\left(\frac{\mathrm{d}\rho}{\omega-\rho}+\frac{\mathrm{d}^{2}\rho}{2\mathrm{d}\rho}\right)=0;$$

which agrees with the equation 392, VI., although deduced in a quite different manner, and conducts anew to the expression II. for $\kappa - \rho$, under the form,

XIX. . .
$$\frac{\mathrm{d}\rho}{\kappa-\rho}$$
 + $V\frac{\mathrm{d}^2\rho}{\mathrm{d}\rho}$, as in 392, VIII.

* Without having recourse to this transformation XVI., we might treat the condition XV. by infinitesimals, as follows:

XVII'...
$$\begin{cases} \frac{\mathrm{PS}}{\mathrm{QS}} = 1 + \frac{\mathrm{PQ}}{\mathrm{QS}} = 1 + \frac{\mathrm{d}\rho}{\omega - \rho - \mathrm{d}\rho} = 1 + \frac{\mathrm{d}\rho}{\omega - \rho};\\ \frac{2\mathrm{QR}}{\mathrm{PR}} = 1 + \frac{\mathrm{QP} + \mathrm{QR}}{\mathrm{PR}} = 1 + \frac{\mathrm{d}^2\rho}{2\mathrm{d}\rho + \mathrm{d}^2\rho} = 1 + \frac{\mathrm{d}^2\rho}{2\mathrm{d}\rho} \end{cases}$$

equating then to zero the vector part of the product of these two expressions, and suppressing the infinitesimal of the second order, the equation XVIII. of the osculating circle is obtained anew.

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2 A

(7.) Again, if $oD = \delta$ be the *diameter* from the origin, of any sphere through that point o, which passes also through any three other given points A, B, C, with oA = a, &C., we have by 296, XXVI. the formula,

XX...
$$\delta S \alpha \beta \gamma = V \alpha (\beta - \alpha) (\gamma - \beta) \gamma;$$

writing then (comp. XVII.),

and $\begin{aligned} XXI...a = d\rho, \quad \beta - a = d\rho + d^2\rho, \quad \gamma - \beta = d\rho + 2d^2\rho + d^3\rho, \\ XXII...\delta = 2Ps = 2(\sigma - \rho), \end{aligned}$

where σ is (as in 395, &c.) the vector os (from an *arbitrary origin* o) of the *centre* s of the *osculating sphere* to a curve of double curvature at P, we have by *infinitesimals*, suppressing terms which are of the *seventh* and higher *orders*, because the first member is only of the *sixth* order, and reducing* by the rules of quaternions,

XXIII. . .
$$(\sigma - \rho) \mathrm{Sd}\rho \mathrm{d}^2\rho \mathrm{d}^3\rho = \frac{1}{2} \mathrm{Vd}\rho (\mathrm{d}\rho + \mathrm{d}^2\rho) (\mathrm{d}\rho + 2\mathrm{d}^2\rho + \mathrm{d}^3\rho)$$

 $(3\mathrm{d}\rho + 3\mathrm{d}^2\rho + \mathrm{d}^3\rho) = 3 \mathrm{Vd}\rho \mathrm{d}^2\rho \mathrm{Sd}\rho \mathrm{d}^2\rho + \mathrm{d}\rho^2 \mathrm{Vd}^3\rho \mathrm{d}\rho;$

which agrees precisely with the formula 395, XIII., although obtained by a process so different.

(8.) Finally as regards the osculating plane, and the second curvature, of a curve in space, *infinitesimals* give at once for that plane the equation,

XXIV...
$$S(\omega - \rho)d\rho d^2\rho = 0$$
, agreeing with 376, V.;

and if *three consecutive elements* of the curve be represented (comp. XXI.) by the differential expressions,

XXV...
$$PQ = d\rho$$
, $QR = d\rho + d^2\rho$, $RS = d\rho + 2d^2\rho + d^3\rho$,

the second curvature r⁻¹, defined as in 396, is easily seen to be connected as

and
$$\frac{{}^{3}_{2}V.(d\rho d^{2}\rho)^{2}}{2} = 3Vd\rho d^{2}\rho \cdot Sd\rho d^{2}\rho,$$

 $\frac{1}{2}\mathrm{d}\rho^2 \mathrm{V}(\mathrm{d}\rho\mathrm{d}^3\rho + 3\mathrm{d}^3\rho\mathrm{d}\rho) = \mathrm{d}\rho^2 \mathrm{V}\mathrm{d}^3\rho\mathrm{d}\rho\,;$

and thus the third member of XXIII. is obtained.

^{*} Of the eighteen terms which would follow the sign of operation $\frac{1}{2}$ V, if the second member of XXIII. were fully developed, one is of the fourth order, but is a scalar : three are of the fifth order, but have a scalar sum; nine are of orders higher than the sixth; and two terms of the sixth order are scalars, so that there remain only three terms of that order to be considered. In this manner it is found that the second member in question reduces itself to the sum of the two vector parts,

ARTS. 401, 402.7 OSCULATING SPHERES BY INFINITESIMALS.

follows with the angle of a certain auxiliary quaternion q, which differs infinitely little from unity :

XXVI... $\mathbf{r}^{-1}\mathbf{d}s = \angle q$, if **XXVII...** $q = \frac{\mathbf{V}(\mathbf{QR} \cdot \mathbf{Rs})}{\mathbf{V}(\mathbf{PQ} \cdot \mathbf{QR})} = 1 + \frac{\mathbf{V}\mathbf{d}\rho\mathbf{d}^{3}\rho}{\mathbf{V}\mathbf{d}\rho\mathbf{d}^{2}\rho}$;

we have then the expression,

XXVIII. . . Second Curvature = $\mathbf{r}^{-1} = \frac{\mathbf{V}q}{\mathbf{d}\rho} = \mathbf{S} \frac{\mathbf{d}^{3}\rho}{\mathbf{V}\mathbf{d}\rho\mathbf{d}^{2}\rho}$

which agrees with the formula 397, XXVII., and has been illustrated, in the sub-articles to 397 and 398, by numerous geometrical applications.

(9.) On the whole, then, it appears that although the logic of derived vectors, and of differentials of vectors considered as finite lines, proportional to such derivatives, is perhaps a little clearer than that of infinitesimals, because it shows more evidently (especially when combined with Taylor's Series adapted to Quaternions, 342, 375) that nothing is neglected, yet it is perfectly possible to combine* quaternions, in practice, with methods founded on the more usual notion of Differentials, as infinitely small differences: and that when this combination is judiciously made, abridgments of calculation arise, without any ultimate error.

SECTION 7.

On Surfaces of the Second Order ; and on Curvatures of Surfaces.

402. As early as in the First Book of these *Elements*, some specimens were given of the treatment or expression of *Surfaces of the Second Order* by *Vectors*; or by *Anharmonic Equations* which were *derived* from the theory of vectors, without any introduction, at that stage, of *Quaternions* properly so called. Thus it was shown, in the sub-articles to 98, that a very simple anharmonic equation (xz = yw) might represent either a ruled paraboloid, or a ruled hyperboloid, according as a certain condition (ac = bd)was or was not satisfied, by the constants of the surface. Again, in the

2 A 2

^{*} Compare the first Note to page 170. It will however be of course necessary, in any future applications of quaternions, to specify in which of these two senses, as a finite differential, or as an infinitesimal, such a symbol as $d\rho$ is employed.

sub-articles to 99, two examples were given, of vector expressions for cones of the second order (and one such expression for a cone of the third order, with a conjugate ray (99, (5.)); while an expression of the same sort, namely,

I...
$$\rho = xa + y\beta + z\gamma$$
, with $x^2 + y^2 + z^2 = 1$,

was assigned (99, (2.)) as representing generally an ellipsoid,* with α , β , γ , or OA, OB, OC, for three conjugate semidiameters. And finally, in the subarticles (11.) and (12.) to Art. 100, an instance was furnished of the determination of a tangential plane to a cone, by means of partial derived vectors.

403. In the Second Book, a much greater range of expression was attained, in consequence of the introduction of the peculiar symbols, or characteristics of operation, which belong to the present Calculus; but still with that limitation which was caused, by the conception and notation of a Quaternion being confined, in that Book, to Quotients of Vectors (112, 116, comp. 307, (5.)), without yet admitting Products or Powers of Directed Lines in Space: although versors, tensors, and even norms⁺ of such vectors were already introduced (156, 185, 273).

(1.) The Sphere,[‡] for instance, which has its centre at the origin, and has the vector OA, or a, with a length Ta = a, for one of its radii, admitted of being represented, not only (comp. 402, I.) by the vector expression,

1. . .
$$\rho = xa + y\beta + z\gamma$$
, $x^2 + y^2 + z^2 = 1$,

I'...
$$Ta = T\beta = T\gamma = a$$
, and I''... $S\frac{\beta}{a} = S\frac{\gamma}{a} = S\frac{\gamma}{\beta} = 0$,

* In like manner the expression,

11...
$$\rho = xa + y\beta + z\gamma$$
, with $x^2 + y^2 - z^2 = 1$, or $= -1$,

represents a general hyperboloid, of one sheet, or of two, with $\alpha\beta\gamma$ for conjugate semi-diameters: while, with the scalar equation $x^2 + y^2 - z^2 = 0$, the same vector expression represents their common asymptotic cone (not generally of revolution).

† The notation Na, for $(Ta)^2$, although not formally introduced before Art. 273, had been used by anticipation in 200, (3.), page 191, vol. i.

[‡] That is to say, the *spheric surface* through A, with o for centre. Compare the Note to page 199, vol. i.

ABTS. 402, 403.] QUATERNION EQUATIONS OF SPHERE.

but also by any one of the following equations, in which it is permitted to change a to -a:

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 $II...\frac{a}{\rho} = K\frac{\rho}{a}; \qquad III...\frac{\rho}{a}K\frac{\rho}{a} = 1; \\IV...N\frac{\rho}{a} = 1; \quad 145, (8.), (12.) \qquad V...T\rho = a; \\VI...T\rho = Ta; \qquad VII...T\frac{\rho}{a} = 1; \quad 186, (2.), 187, (1.) \\VIII...S\frac{\rho-a}{\rho+a} = 0; \qquad IX...N\frac{\rho}{\epsilon} = N\frac{a}{\epsilon}; \\X...N\rho = Na; \quad \begin{array}{c}200, (11.),\\215, (10.),\\273, (1.)\end{array} \qquad XI...\left(S\frac{\rho}{a}\right)^2 - \left(V\frac{\rho}{a}\right)^2 = 1; \end{array}$

XII... $\operatorname{NS} \frac{\rho}{a} + \operatorname{NV} \frac{\rho}{a} = 1$; 204, (6.), XXV., XXVI.

XIII... $N\left(S\frac{\rho}{a}+V\frac{\rho}{a}\right)=1$; XIV... $T\left(S\frac{\rho}{a}+V\frac{\rho}{a}\right)=1$; 204, (9.)

or by the system of equations,

XV...
$$\operatorname{S} \frac{\rho}{a} = x$$
, $\left(\operatorname{V} \frac{\rho}{a}\right)^2 = x^2 - 1 \ (\leq 0)$, 204, (4.)

representing a system of circles, with the spheric surface for their locus.

(2.) Other forms of equation, for the same spheric surface, may on the same principles be assigned; for example we may write,

 $XVI...\frac{\rho}{a} = K\frac{a}{\rho}; \qquad XVII...N\frac{a}{\rho} = 1; \qquad XVIII...T\frac{a}{\rho} = 1;$ $XIX...\frac{\rho-a}{\rho+a} = \frac{\pi}{2}; \qquad XX...S\frac{2a}{\rho+a} = 1; \qquad XXI...S\frac{2\rho}{\rho+a} = 1;$

or (comp. 186, (5.), and 200, (3.)),

XXII...
$$T(\rho - ca) = T(c\rho - a), \quad c^2 < 1;$$

under which last form, the sphere may be considered to be generated by

[III. III. § 7.

the revolution of the circle, which has been already spoken of as the Apollonian^{*} Locus.

(3.) And from any one to any other, of all these various forms, it is possible, and easy to pass, by general Rules of Transformation,[†] which were established in the Second Book : while each of them is capable of receiving, on the principles of the same Book, a Geometrical Interpretation.

(4.) But we could not, on the principles of the Second Book alone, advance to such subsequent equations of the same sphere, as

XXIII...
$$\rho^2 = a^2$$
, or XXIV... $\rho^2 + a^2 = 0$, 282, VII. XIII.

whereof the latter includes (282, (9.)) the important equation $\rho^2 + 1 = 0$, or $\rho^2 = -1$, of what we have called the Unit-Sphere (128); nor to such an exponential expression for the variable vector ρ of the same spheric surface, as

$$XXV\dots \rho = \alpha k^t j^s k j^{-s} k^{-t}, \qquad 308, XVIII.$$

in which j and k belong to the fundamental system ijk of three rectangular unit-lines (295), connected by the fundamental Formula A of Art. 183, namely,

$$i^2 = j^2 = k^2 = ijk = -1,$$
 (A)

while s and t are two arbitrary and scalar variables, with simple geometrical[‡] significations: because we were not then prepared to introduce any symbol, such as ρ^2 , or k^t , which should represent a square or other power of a vector.§ And similar remarks apply to the representation, by quaternions, of other surfaces of the second order.

‡ Compare the second Note to page 398, vol. i.

§ It is true that the formula A was established in the course of the Second Book (page 160, vol. i.); but it is to be remembered that the symbols *ijk* were *there* treated as denoting a system of *three right versors*, in *three mutually rectangular planes* (181): although it has *since* been found possible and useful, in this Third Book, to *identify* these right versors with their own *indices* or axes (295), and so to treat them as a system of *three rectangular lines*, as above.

^{*} Compare the first Note to page 130, vol. i.

⁺ This richness of transformation, of quaternion expressions or equations, has been noticed, by some friendly critics, as a characteristic of the present Calculus. In the preceding parts of this work, the reader may compare pages 130, 141, 185, vol. i., and pages 106, 108, 109, vol. ii.; in the two last of which, the variety of the expressions for the second curvature (r^{-1}) of a curve in space may be considered worthy of remark. On the other hand, it may be thought remarkable that, in this Calculus, a single expression, such as that given by the first formula (389, IV.) of page 50, vol. ii., adapts itself with equal case to the determination of the vector (κ) of the centre of the osculating circle, to a plane curve, and to a curve of double curvature, as has been sufficiently exemplified in the foregoing Section.

ARTS. 403, 404.] EQUATION OF ELLIPSOID RESUMED.

404. A brief review, or *recapitulation*, of some of the chief expressions connected with the *Ellipsoid*, for example, which have been already established in these *Elements*, with *references* to a few others, may not be useless here.

(1.) Besides the vector expression $\rho = xa + y\beta + z\gamma$, with the scalar relation $x^2 + y^2 + z^2 = 1$, and with arbitrary vector values of the constants a, β, γ , which was lately cited (402) from the First Book, or the equations 403, I., without the conditions 403, I'., II'. which are peculiar to the sphere, there were given in the Second Book (204, (13.), (14.)) equations which differed from those lately numbered as 403, XI. XII. XIII. XIV. XV., only by the substitution of $\nabla \frac{\rho}{\beta}$ for $\nabla \frac{\rho}{a}$; for instance, there was the equation,

I. . .
$$\left(S\frac{\rho}{a}\right)^2 - \left(V\frac{\rho}{\beta}\right)^2 = 1,$$
 204, (14.)

analogous to 403, XI., and representing generally^{*} an *ellipsoid*, regarded as the *locus* of a certain system of *ellipses*, which were thus substituted for the *circles*[†] (403, XV.) of the *sphere*, by a species of geometrical *deformation*, which led to the establishment of certain *homologies* (developed in the subarticles to 274).

(2.) Employing still only quotients of vectors, but introducing two other pairs of vector-constants, γ , δ and ι , κ , instead of the pair a, β in the equation I., which were however connected with that pair and with each other by certain assigned relations, that equation was transformed successively to

II. . .
$$T\left(\frac{\rho}{\gamma} + K \frac{\rho}{\delta}\right) = 1,$$
 216, X.

[†] The equation I. might also have been thus written, on the principles of the Second Book,

I'. . .
$$\left(S\frac{\rho}{\alpha} + S\frac{\rho}{\beta}\right)\left(S\frac{\rho}{\alpha} - S\frac{\rho}{\beta}\right) + \left(T\frac{\rho}{\beta}\right)^2 = 1;$$

whence it would have followed at once (comp. 216, (7.)), that the ellipsoid I. is cut in two circles, with a common radius = $T\beta$, by the two diametral planes,

I''...
$$S\frac{\rho}{\alpha} + S\frac{\rho}{\beta} = 0$$
, $S\frac{\rho}{\alpha} - S\frac{\rho}{\beta} = 0$.

In fact, this equation I'. is what was called in 359 a cyclic form, while I. itself is what was there called a *focal form*, of the equation of the surface; the lines $\alpha^{-1} \pm \beta^{-1}$ being, by the Third Book, the *two* (real) cyclic normals, while β is one of the two (real) focal lines of the (imaginary) asymptotic cone. Compare the Note to page 535, vol. i.

^{*} In the case of parallelism of the two vector constants ($\beta \parallel \alpha$), the equation I. represents generally a Spheroid of revolution, with its axis in the direction of α ; while in the contrary case of perpendicularity ($\beta \perp \alpha$), the same equation I. represents an elliptic Cylinder, with its generating lines in the direction of β . Compare 204, (10.), (11.), and the Note to page 231, vol. i.

and to a form which may be written thus (comp. 217, (5.)),

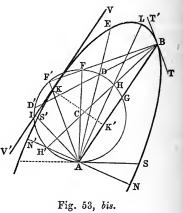
III...
$$T\left(\iota + K\frac{\kappa}{\rho} \cdot \rho\right) T\rho = T\iota^2 - T\kappa^2;$$
 217, XVI.

and this last form was interpreted, so as to lead to a Rule of Construction* (217, (6.), (7.)), which was illustrated by a Diagram (fig. 53), and from

which many geometrical properties of that surface were deduced (218, 219) in a very simple manner, and were confirmed by calculation with quaternions : the equation and construction being also modified afterwards, by the introduction (220) of a new pair of vector-constants, ι' and κ' , which were shown to admit of being substituted for ι and κ , in the recent form III.

(3.) And although the Equation of Con- v^{\prime} ingation

IV...
$$8\frac{\lambda}{a}S\frac{\mu}{a} - S\left(V\frac{\lambda}{\beta}, V\frac{\mu}{\beta}\right) = 1, 316, LXIII.$$



which connects the vectors λ , μ of any two points L, M, whereof one is on the polar plane of the other, with respect to the ellipsoid I., was not assigned till near the end of the First Chapter of the present Book, yet it was there deduced by principles and processes of the Second Book alone: which thus were adequate, although not in the most practically convenient way, to the treatment of questions respecting tangent planes and normals to an ellipsoid, and similarly for other surfaces + of the same second order.

† The following are a few other references, on this subject, to the Second Book. Expressions for a *Right Cone* (or for a single *sheet* of such a cone) have been given in vol. *i*. in pages 121, 180, 226, 227. In page 181 the equation $S \frac{\rho}{a} S \frac{\beta}{\rho} = 1$, has been assigned, with a transformation in page 182, to represent generally a *Cyclic Cone*, or a cone of the *second order*, with its vertex at the origin; and to exhibit its *cyclic planes*, and *subcontrary sections* (pp. 182, 184). *Right Cylinders* have occurred in pages 195, 199, 201, 202, 223. A case of an *Elliptic Cylinder* has been already mentioned (the case when $\beta \perp a$ in I.); and a transformation of the equation III. of the *Ellipsoid*, by means of *reciprocals* and *norms* of vectors, was assigned in pages 314. And several expressions (comp. 403), for a *Sphere* of which the origin was not the centre, occurred in pages 165, 180, 192, vol. i., and perhaps elsewhere, without any employment of products of vectors.

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^{*} This Construction of the Ellipsoid, by means of a Generating Triangle and a Diacentric Sphere (page 234, vol. i.), is believed to have been new, when it was deduced by the writer in 1846, and was in that year stated to the Royal Irish Academy (see its *Proceedings*, vol. iii., pp. 288, 289), as a result of the Method of Quaternions, which had been previously communicated by him to that Academy (in the year 1843).

ART. 404.] TRANSFORMATIONS OF THE EQUATION.

(4.) But in this Third Book we have been able to write the equation III. under the simpler form,*

$$\nabla \dots T(\iota \rho + \rho \kappa) = \kappa^2 - \iota^2, \qquad 282, XXIX.$$

which has again admitted of numerous transformations; for instance, of all those which are obtained by equating $(\kappa^2 - i^2)^2$ to any one of the expressions 336, (5.), for the square of this last tensor in V., or for the norm of the quaternion $i\rho + \rho\kappa$; cyclic forms \dagger of equation thus arising, which are easily converted into focal forms (359); while a rectangular transformation (373, XXX.) has subsequently been assigned, whereby the lengths (abc), and also the directions, of the three semiaxes of the surface, are expressed in terms of the two vector-constants, i, κ : the results thus obtained by calculation being found to agree with those previously deduced, from the geometrical construction (2.) in the Second Book.

(5.) The equation V. has also been *differentiated* (336), and a normal vector $v = \phi \rho$ has thus been deduced, such that, for the ellipsoid in question,

$$\nabla I... S \nu d\rho = 0$$
, and $\nabla II... S \nu \rho = 1$;

a process which has since been extended (361), and appears to furnish one of the best general methods of treating surfaces[‡] of the second order by quaternions: especially when combined with that theory of linear and vector functions ($\phi\rho$) of vectors, which was developed in the Sixth Section§ of the Second Chapter of the present Book.

§ It appears that this Section may be conveniently referred to, as III. ii. 6; and similarly in other cases.

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2 B

^{*} Mentioned by anticipation in the Note to page 241, vol. i.

⁺ Compare the second Note to page 183. The vectors ι and κ are here the cyclic normals, and $\iota - \kappa$ is one of the focal lines; the other being the line $\iota' - \kappa'$ of the page 241, vol. i.

[‡] The following are a few additional references to preceding parts of this Third Book, which has extended to a much greater length than was designed (page 322, vol. i.). In the First Chapter, the reader may consult pages 325, 326, 327, 328, vol. i., for some other forms of equation of the ellipsoid and the sphere. In the Second Chapter, pages 460, 461, vol. i., contain some useful practice, above alluded to, in the differentiation and transformation of the equation $r^2 = T(i\rho + \rho\kappa)$. As regards the Sixth Section of that Chapter, which we are about to use (405), as one supposed to be familiar to the reader, it may be sufficient here to mention Arts. 357-362, and the Notes (or some of them) to pages 523, 525, 527, 535, 546, 549, vol. i. In this Third Chapter, the sub-articles (7.)-(21.) to 373 (pages 15, &c.) might be re-perused; and perhaps the investigations respecting cones and sphero-conics, in 394, and its sub-articles (pages 63, &c.), including remarks on an hyperbolic cylinder, and its asymptotic planes (in page 72). Finally, in a few longer and later series of sub-articles, to Arts. 397, &c., a certain degree of familiarity with some of the chief properties of surfaces of the second order has been assumed; as in pages 103, 126, 129, and generally in the recent investigations respecting the osculating twisted cubic (pages 129, 166, &c.), to a helix, or other curve in space.

ELEMENTS OF QUATERNIONS. [III. m. §7.

405. Dismissing then, at least for the present, the *special* consideration of the *ellipsoid*, but still confining ourselves, for the moment, to *Central* Surfaces of the Second Order, and using freely the principles of this Third Book, but especially those of the Section (III. ii. 6) last referred to, we may denote any such central and non-conical surface by the scalar equation (comp. 361, [p. 547, vol. i.]),

$$I...f\rho = S\rho\phi\rho = 1;$$

the *asymptotic cone* (real or imaginary) being represented by the connected equation,

$$II...f\rho = S\rho\phi\rho = 0;$$

and the equation of conjugation, between the vectors ρ , ρ' of any two points P, P', which are conjugate relatively to this surface I. (comp. 362, and 404, (3.), see also 373, (20.)), being,

III. . .
$$f(\rho, \rho') = f(\rho', \rho) = S\rho\phi\rho' = S\rho'\phi\rho = 1;$$

while the differential equation of the surface is of the form (361),

IV...
$$0 = df\rho = 2S\nu d\rho$$
, with V... $\nu = \phi\rho$;

this vector-function $\phi \rho$, which represents the normal ν to the surface, being at once linear and self-conjugate (361, (3.)); and the surface itself being the locus of all the points \mathbf{r} which are conjugate to themselves, so that its equation I. may be thus written,

I'...
$$f(\rho, \rho) = 1$$
, because $f(\rho, \rho) = f\rho$, by 362, IV.

(1.) Such being the form of $\phi \rho$, it has been seen that there are always three real and rectangular unit-lines, a_1 , a_2 , a_3 , and three real scalars, c_1 , c_2 , c_3 , such as to satisfy (comp. 357, III.) the three vector equations,

VI...
$$\phi a_1 = -c_1 a_1$$
, $\phi a_2 = -c_2 a_2$, $\phi a_3 = -c_3 a_3$;

whence also these three scalar equations are satisfied,

VII. . .
$$fa_1 = c_1$$
, $fa_2 = c_2$, $fa_3 = c_3$;

and therefore (comp. 362, VII.),

VIII...
$$f(c_1^{-\frac{1}{2}}a_1) = f(c_2^{-\frac{1}{2}}a_2) = f(c_3^{-\frac{1}{2}}a_3) = 1.$$

ART. 405.]

(2.) It follows then that the three (real or imaginary) rectangular lines,

IX...
$$\beta_1 = c_1^{-\frac{1}{2}}a_1, \quad \beta_2 = c_2^{-\frac{1}{2}}a_2, \quad \beta_3 = c_3^{-\frac{1}{2}}a_3,$$

are the three (real or imaginary) vector semiaxes of the surface I.; and that the three (positive or negative) scalars, c_1 , c_2 , c_3 , namely the three roots of the scalar and cubic equation* M = 0 (comp. 357, (1.)), are the (always real) inverse squares of the three (real or imaginary) scalar semiaxes, of the same central surface of the second order.

(3.) For the reality of that surface I., it is necessary and sufficient that one at least of the three scalars c_1 , c_2 , c_3 should be positive; if all be such, the surface is an ellipsoid; if two, but not the third, it is a single-sheeted hyperboloid; and if only one, it is a double-sheeted hyperboloid: those scalars being here supposed to be each finite, and different from zero.

(4.) We have already seen (357, (2.)) how to obtain the rectangular transformation,

X...
$$f\rho = c_1(Sa_1\rho)^2 + c_2(Sa_2\rho)^2 + c_3(Sa_3\rho)^2$$
,

which may now, by IX., be thus written,

XI...
$$f\rho = (S\beta_1^{-1}\rho)^2 + (S\beta_2^{-1}\rho)^2 + (S\beta_3^{-1}\rho)^2;$$

but it is to be remembered that, by (2.) and (3.), one or even two of these three vectors $\beta_1\beta_2\beta_3$ may become *imaginary*, without the surface ceasing to be real.

(5.) We had also the cyclic transformation (357, II. II'.),

XII...
$$f\rho = g\rho^2 + S\lambda\rho\mu\rho = \rho^2(g - S\lambda\mu) + 2S\lambda\rho S\mu\rho,$$

in which the scalar g and the vector λ , μ are *real*, and the latter have the directions of the two (real) cyclic normals; \dagger in fact it is obvious on inspection, that the surface is *cut in circles*, by *planes perpendicular* to these *two last lines*.

^{*} It is unnecessary here to write $M_0 = 0$, as in page 520, vol. i., &c., because the function ϕ is here supposed to be self-conjugate; its constants being also real.

[†] Compare the Note to page 527, vol. i., see also the proof by quaternions, in 373, (16.), &c., of the known theorem, that any two subcontrary circular sections are homospherical, with the equation (373, XLIV.) of their common sphere, which is found to have its centre in the diametral plane of the two cyclic normals λ , μ .

[III. III. § 7.

(6.) It has been proved that the four real scalars, $c_1c_2c_3g$, and the five real vectors, $a_1a_2a_3\lambda\mu$, are connected by the relations* (357, XX. and XXI.),

$$\begin{aligned} \text{XIII.} \dots c_1 &= -g - \mathrm{T}\lambda\mu, \qquad c_2 &= -g + \mathrm{S}\lambda\mu, \quad c_3 &= -g + \mathrm{T}\lambda\mu; \\ \text{XIV.} \dots a_1 &= \mathrm{U}(\lambda\mathrm{T}\mu - \mu\mathrm{T}\lambda), \quad a_2 &= \mathrm{U}\mathrm{V}\lambda\mu, \qquad a_3 &= \mathrm{U}(\lambda\mathrm{T}\mu + \mu\mathrm{T}\lambda); \end{aligned}$$

at least if the *three roots* $c_1c_2c_3$ of the cubic M = 0 be arranged in *algebraically* ascending order (357, IX.), so that $c_1 < c_2 < c_3$.

(7.) It may happen (comp. (3.)), that one of these three roots vanishes; and in that case (comp. (2.)), one of the three semiaxes becomes infinite, and the surface I. becomes a cylinder.

(8.) Thus, in particular, if $c_1 = 0$, or $g = -T\lambda\mu$, so that the *two other* roots are both *positive*, the equation takes (by XII., comp. 357, XXII.) a form which may be thus written,

XV...
$$(S\lambda\mu\rho)^2 + (S\lambda\rho T\mu + S\mu\rho T\lambda)^2 = T\lambda\mu - S\lambda\mu > 0;$$

and it represents an elliptic cylinder.+

(9.) Again, if $c_2 = 0$, or $g = S\lambda\mu$, the equation becomes,

$$XVI...2S\lambda\rho S\mu\rho = 1,$$

and represents an hyperbolic cylinder; the root c_1 being in this case negative, while the remaining root c_3 is positive.

(10.) But if we suppose that $c_3 = 0$, or $g = T\lambda\mu$, so that c_1 and c_2 are both negative, the equation may (by 357, XXIII.) be reduced to the form,

XVII. . .
$$(S\lambda\mu\rho)^2 + (S\lambda\rho T\mu - S\mu\rho T\lambda)^2 = -T\lambda\mu - S\lambda\mu < 0;$$

it represents therefore, in *this* case, *nothing real*, although it may be *said* to bo, in the same case, the equation of an *imaginary*; *elliptic cylinder*.

^{*} These relations and a few others mentioned are so useful that, although they occurred in an earlier part of the work, it seems convenient to restate them here.

^{+ [}XV. and XVII. may be directly obtained by means of the identity $\rho = (V\lambda\mu)^{-1} (S\lambda\mu\rho + VV\lambda\mu, \rho)$.]

[‡] In the Section (III. ii. 6) above referred to, many symbolical results have been established, respecting *imaginary cyclic normals*, or *focal lines*, &c., on which it is unnecessary to return. But it it may be remarked that as, when the scalar function $f\rho$ admits of changing sign, for a change of direction of the real vector ρ , so as to be positive for some such directions, and negative for others, although $f(-\rho) = f(+\rho)$, the two equations, $f\rho = +1$, $f\rho = -1$, represent then two real and conjugate hyperboloids, of different species: so, when the function $f\rho$ is either essentially positive, for real values of ρ , the equation $f\rho = 1$ and $\rho = -1$ may then be said to represent two conjugate ellipsoids, one real, and the other imaginary.

ARTS. 405, 406.] CONES OF THE SECOND ORDER.

(11.) It is scarcely worth while to remark, that we have here supposed each of the two vectors λ and μ to be not only real but actual (Art. 1); for if either of them were to vanish, the equation of the surface would take by XII. the form,

XVIII... $\rho^2 = g^{-1}$, or XVIII'... $T\rho = (-g)^{-\frac{1}{2}}$,

and would represent a real or imaginary sphere, according as the scalar constant g was negative or positive: λ and μ have also distinct directions, except in the case of surfaces of revolution.

(12.) In general, it results from the relations (6.), that the plane of the two (real) cyclic normals, λ , μ , is perpendicular to the (real) direction of that (real or imaginary) semiaxis, of which, when considered as a scalar (2.), the inverse square c_2 is algebraically intermediate between the inverse squares c_1 , c_3 of the other two; or that the two diametral and cyclic planes (S $\lambda \rho = 0$, S $\mu \rho = 0$) intersect in that real line (V $\lambda \mu$) which has the direction of the real unit-vector a_2 (1.), corresponding to the mean root c_2 of the cubic equation M = 0: all which agrees with known results, respecting the circular sections of the (real) ellipsoid, and of the two hyperboloids.

406. Some additional light may be thrown on the theory of the *central* surface 405, I., by the consideration of its asymptotic cone 405, II.; of which cone, by 405, XII., the equation may be thus written,

I. . .
$$f\rho = g\rho^2 + S\lambda\rho\mu\rho = \rho^2(g - S\lambda\mu) + 2S\lambda\rho S\mu\rho = 0$$
;

and which is real or imaginary, according as we have the inequality,

II. . .
$$g^2 < \lambda^2 \mu^2$$
, or III. . . $g^2 > \lambda^2 \mu^2$;

that is, by 405, (6.), according as the product c_1c_3 of the extreme roots of the cubic M = 0 is negative or positive; or finally, according as the surface $f\rho = 1$ is a (real) hyperboloid, or an ellipsoid (real or imaginary*).

(1.) As regards the asserted *reality* of the cone I., when the *condition* II. is satisfied, it may suffice to observe that if we cut the cone by the *plane*,

IV...
$$S\lambda(\rho - \mu) = -g$$
,

the section is a circle of the real and diacentric sphere,

$$V..., \rho^2 = 2S\mu\rho, \text{ or } V'..., (\rho - \mu)^2 = \mu^2;$$

* Compare the Note immediately preceding; also the second Note to page 535, vol. i.

and a real circle, because it is on the real cylinder of revolution,

VI...
$$\mathrm{TV}(\rho - \mu)\mathrm{U}\lambda = (\mathrm{T}\mu^2 - g^{2'}\mathrm{T}\lambda^{-2})^{\frac{1}{2}},$$

so that its radius is equal to this last real radical.

(2.) For example, the cone

VII...
$$S \frac{\rho}{a} S \frac{\beta}{\rho} = 1$$
, or VII'... $2(Sa\rho S\beta\rho - a^2\rho^2) = 0$,

which under the form VII. occurred as early as 196, (8.), and for which $\lambda = a$, $\mu = \beta$, $g = Sa\beta - 2a^2$, and therefore $T\lambda\mu + g > 0$, the condition II. reduces itself to $T\lambda\mu - g > 0$; or after division by $2Ta^2$, &c., to the form (comp. 199, XII.),

VIII...
$$\frac{1}{2}(T+S)\frac{\beta}{a} > 1$$
, or VIII'... $S\sqrt{\frac{\beta}{a}} > 1$;

and accordingly, when either of these two last inequalities exists, it will be found that the sphere $S\frac{\beta}{\rho} = 1$ is cut by the plane $S\frac{\rho}{a} = 1$ in a real circle, the base of a real cone VII.

(3.) As an example of the variety of processes by which problems in this Calculus may be treated, we might propose to determine, by the general formula 389, IV., the vector κ of the centre of the osculating circle to the curve IV. V., considered merely as an intersection of two surfaces. The first derivatives of the equations would allow us to assume $\rho' = V\lambda(\rho - \mu)$, and therefore $\rho'' = \lambda \rho'$; whence, by the formula, we have

IX. . .
$$\kappa = \rho + \frac{\rho'^3}{\nabla \rho'' \rho'} = \rho + \frac{\rho'}{\lambda} = \frac{S \rho \lambda + \nabla \mu \lambda}{\lambda} = \mu - g \lambda^{-1};$$

the section is therefore a circle, because its centre of curvature is constant; and its radius is,

X...
$$r = \mathbf{T}(\rho - \kappa) = \mathbf{T}(\rho - \mu + g\lambda^{-1}) = (\mathbf{T}\mu^2 - g^2\mathbf{T}\lambda^{-2})^{\frac{1}{2}},$$

= the radius of the cylinder VI.

(4.) When the opposite inequality III. exists, the radius X., the cylinder VI., the circle IV. V., and the cone I., become all four imaginary; the plane IV. being then wholly external to the sphere ∇ ., as happens, for instance, with the plane and sphere in (2.), when the condition VIII. or VIII'. is reversed.

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ART. 406.]

CONES OF THE SECOND ORDER.

(5.) In the intermediate case, when

XI...
$$g^2 = \lambda^2 \mu^2$$
, or XI'... $g = \mp T \lambda \mu$,

the radius r in X. vanishes; the right cylinder VI. reduces itself to its axis; and the circle IV. V. becomes a point, in which the sphere is touched by the plane. In this case, then, the cone I. is reduced to a single (real*) right line, which has (compare the equations of the elliptic cylinders, 405, XV. XVII.) the direction of $\lambda T\mu - \mu T\lambda$, if $g = -T\lambda\mu$, but the perpendicular direction of $\lambda T\mu + \mu T\lambda$, if $g = +T\lambda\mu$.

(6.) In general (comp. 405, X.), the equation of the cone I. admits of the rectangular transformation,

XII...
$$f\rho = c_1(\mathbf{S}\alpha_1\rho)^2 + c_2(\mathbf{S}\alpha_2\rho)^2 + c_3(\mathbf{S}\alpha_3\rho)^2 = 0$$
;

and the two sub-cases last considered (5.) correspond respectively (by 405, (6.)) to the exanescence of the roots c_1 , c_3 of the cubic M = 0, with the resulting directions a_1 , a_3 of the only real side of the cone. An analogous but intermediate case (comp. 405, (9.)) is that when $c_2 = 0$, or $g = S\lambda\mu$; in which case, the cone I. reduces itself to the pair of (real) planes,

XIII. . .
$$S\lambda\rho$$
 . $S\mu\rho = 0$,

namely to the asymptotic planes of the hyperbolic cylinder 405, XVI., or to those which are usually the two cyclic \dagger planes of the cone.

(7.) The case (comp. 394, (29.)),

XIV...
$$g = -S\lambda\mu$$
, or XIV'... $c_1 - c_2 + c_3 = 0$,

for which the equation I. of the cone becomes,

$$\mathbf{X}\mathbf{V}...0 = f\rho = 2(\mathbf{S}\lambda\rho\mathbf{S}\mu\rho - \rho^2\mathbf{S}\lambda\mu) = 2\mathbf{S}(\mathbf{V}\lambda\rho \cdot \mathbf{V}\mu\rho),$$

may deserve a moment's attention. In this case, the *two planes*, of $\lambda \rho$ and $\mu \rho$, which connect the *two cyclic normals* λ and μ with an *arbitrary side* ρ of the cone, are always *rectangular* to each other; and these two *normals* to the cyclic planes are at the same time *sides* of the cone, which thus is *cut in*

^{*} It may however be said, that in this case the cone consists of a pair of imaginary planes, which intersect in a real right line.

⁺ The cones and surfaces which have a common centre, and common values of the vectors λ and μ , but different values of the scalar g, may thus be said, in a known phraseology, to be *biconcyclic*.

circles, by planes perpendicular to those two sides. And because the equation of the cone may (in the same case) be thus written,

XVI...
$$TV(\lambda + \mu)\rho = TV(\lambda - \mu)\rho$$
,

while the lengths of λ and μ may vary, if their product $T\lambda\mu$ be left unchanged, so that $\lambda + \mu$ and $\lambda - \mu$ may represent any two lines from the vertex, in the plane of the two cyclic normals, and harmonically conjugate with respect to them, it follows that, for this cone XV., the sines of the inclinations of an arbitrary side ρ , to these two new lines, have a constant ratio to each other.

(8.) In general, the second form I. of $f\rho$ shows (comp. 394, (23.)), that the constant product of the sines of the inclinations, of a side ρ of the cone to the two cyclic planes, has for expression,

XVII. . .
$$\cos \angle \frac{\rho}{\lambda}$$
. $\cos \angle \frac{\rho}{\mu} = \frac{1}{2} \left(\frac{g}{T\lambda\mu} + \cos \angle \frac{\mu}{\lambda} \right);$

while the first form I. of the same function $f\rho$ reproduces the condition of reality II., by showing that $g: T\lambda\mu$ is (for a real cone) the cosine of a real angle, namely, that of the quaternion product $\lambda\rho\mu\rho$, since it gives the relation,

XVIII. . .
$$\frac{g}{T\lambda\mu} = SU\lambda\rho\mu\rho = \cos \angle \lambda\rho\mu\rho = \cos \angle \frac{\rho\mu^{-1}\rho}{\lambda}$$
.

(9.) We may also observe that in the case of reality II., with exclusion of the sub-case (6.), if a_3 have the direction of the *internal axis* of the cone, so that

XIX...
$$c_1 < 0$$
, $c_2 < 0$, $c_3 > 0$, or XIX'... $g > S\lambda\mu$, $g < T\lambda\mu$,

the two sides (of one sheet) in the plane of $\lambda \mu$ have the directions,

XX...
$$\rho_1 = c_3^{-\frac{1}{2}}a_3 + (-c_1)^{-\frac{1}{2}}a_1, \quad \rho_2 = c_3^{-\frac{1}{2}}a_3 - (-c_1)^{-\frac{1}{2}}a_1;$$

if then their mutual *inclination*, or the *angle of the cone* in the *plane of the* cyclic normals, be denoted by 2b, we have the values,

XXI...
$$\tan^2 b = \frac{c_3}{-c_1}$$
, XXI'... $\cos 2b = \frac{-c_1 - c_3}{-c_1 + c_3} = \frac{g}{T\lambda\mu}$; -

the angle of the quaternion $\lambda\rho\mu\rho$ is therefore (by XVIII.), equal to this angle 2b, namely to the arcual minor axis of the sphero-conic, in which the cone is cut by the concentric unit-sphere.

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ART. 406.] ARCUAL AXES AND FOCI OF A SPHERO-CONIC.

(10.) The same condition of reality II. may be obtained in a quite different way, as that of the reality of the *reciprocal cone*, which is the *locus of the normal vector*,

XXII...
$$\nu = \phi \rho = g \rho + V \lambda \rho \mu$$
.

Inverting this linear function ϕ , by the method of the Section III. ii. 6, we find first the expression (comp. 354, (12.), and 361, (6.)),

XXIII. . .
$$m\rho = \psi \nu = \mu^2 \lambda S \lambda \nu + \lambda^2 \mu S \mu \nu - g(\lambda S \mu \nu + \mu S \lambda \nu) + (g^2 - \lambda^2 \mu^2) \nu$$

in which XXIV... $m = (g - S\lambda\mu) (g^2 - \lambda^2\mu^2) = -c_1c_2c_3;$

and next the reciprocal equation (comp. 361, XXVII.),

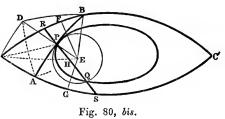
XXV. . . 0 =
$$Sv\psi\nu = \mu^2(S\lambda\nu)^2 + \lambda^2(S\mu\nu)^2 - 2gS\lambda\nu S\mu\nu + (g^2 - \lambda^2\mu^2)\nu^2$$
,

which may be put under the form,

XXVI...
$$\cos\left(\angle \frac{\nu}{\lambda} + \angle \frac{\nu}{\mu}\right) = \frac{-g}{T\lambda\mu};$$

the quotient $g: T\lambda\mu$ thus presenting itself anew as a cosine, namely as that of the supplement of the sum of the

inclinations of the normal ν (to the cone I.), to the two cyclic normals λ , μ (of that cone); or as the cosine^{*} of ck $\pi - A - B$, if A and B denote (comp. fig. 80 [vol. ii., p. 65] the two spherical angles, which the tangent arc to the sphero-conic (9.) makes



with the two *cyclic arcs*: so that by comparison of XXI'. and XXVI. we have the relation,

XXVII. . . A + B =
$$\angle \frac{\nu}{\lambda} + \angle \frac{\nu}{\mu} = \pi - 2b.$$

^{*} This relation was mentioned by anticipation in 394, (3.); and the relation in XXVII. may easily be verified, by conceiving the point of contact P in fig. 80 (vol. ii., page 65) to tend towards a minor summit of the conic, or the tangent arc APB to tend to pass through the two points c, c', in which the cyclic arcs intersect.

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(11.) Comparing the expression XXI'. for cos 2b, with the last expression XVIII. for $g: T\lambda\mu$, we derive the following construction for a sphero-conic, which may easily be verified by geometry :*

Having assumed two points (L, M) on a sphere, and having described a small circle round one of them (say L), bisect the arcs (MQ) which are drawn to its circumference from the other point; the locus of the bisecting points (P) will be a sphero-conic, with the two fixed points for its two cyclic poles (or for the poles of its cyclic arcs), and with an arcual minor axis (2b) equal to the arcual radius of the small circle.[†]

(12.) As regards the *arcual major axis* (say 2a) of the same sphero-conio, it is (with the conditions XIX.) the angle between the two sides (comp. XX.),

XXVIII...
$$\rho_3 = c_3^{-\frac{1}{2}}a_3 + (-c_2)^{-\frac{1}{2}}a_2, \quad \rho_4 = c_3^{-\frac{1}{2}}a_3 - (-c_2)^{-\frac{1}{2}}a_2;$$

whence (comp. XXI.),

XXIX...
$$\tan^2 a = \frac{c_3}{-c_2}$$
, or XXIX'... $\cos 2a = \frac{-c_2 - c_3}{-c_2 + c_3} = (say) e$,

and therefore, a few easy reductions being made,

XXX...
$$\frac{\sin b}{\sin a} = \sqrt{\left\{\frac{1}{2}\left(1 + SU\frac{\mu}{\lambda}\right)\right\}} = \cos \frac{1}{2} \angle \frac{\mu}{\lambda};$$

from which we can at once infer, that if a *focus* of the conic be determined, by drawing from a minor summit to the major axis an arc equal to the major semiaxis a, *the minor axis subtends at this focus* (or at the other) *a spherical angle equal to the angle between the two cyclic arcs.*

(13.) For the two real unifocal transformations of the equation of the cone, or the forms,

XXXI...
$$a(\nabla a\rho)^2 + b(S\beta\rho)^2 = 0$$
, and XXXI'... $a(\nabla a'\rho)^2 + b(S\beta'\rho)^2 = 0$,

with one common set of real values of the scalar coefficients, a and b, but with two real focal unit lines a, a', and two real directive normals β , β' corresponding, it may be sufficient here to refer to the sub-articles to 358; except that it should be noticed, that if the cone be real, and if the line a_3 have the direction

[•] In fact, the bisecting radii or are parallel to the supplementary chords μ'q, if μμ' be a diameter of the sphere; and the locus of all such chords is a cyclic cone, resting on the small circle as its base.

^{+ [}By quaternions, if $oq = \kappa$, $\upsilon \kappa \mu^{-1} = \upsilon (\rho \mu^{-1})^2$ or $\upsilon \kappa = - \upsilon \rho \mu \rho$, &c.]

ABT. 406.] ARCUAL AXES AND FOCI OF A SPHERO-CONIC.

of its internal axis, so that the inequalities XIX. are satisfied, and therefore also (by 405, (6.)),

XXXII. . .
$$c_3^{-1} > 0 > c_1^{-1} > c_2^{-1}$$
,

instead of the inequalities 358, III., or 359, XXXVII., we are now to change, in the earlier formulæ referred to, the symbols $c_1c_2c_3a_1a_2a_3$ to $c_3c_1c_2a_3a_1a_2$, so that we have now the values,

XXXIII.
$$a = -c_1$$
, $b = c_3 - c_1 + c_2$, if $T\beta = T\beta' = 1$.

(14.) And as regards the *interpretation* of the *unifocal form* XXXI., with these last values, it is evidently contained in this other equation,

XXXIV...
$$\sin \angle \frac{\rho}{a} \cdot \sec \angle \frac{\rho}{\beta} = \frac{\mathrm{TV}a\rho}{-S\beta\rho} = \left(\frac{c_3 - c_1 + c_2}{-c_1}\right)^{\frac{1}{2}} = \mathrm{const.};$$

the sines of the inclinations of an arbitrary side (ρ) of the cone, to a focal line (a), and to the corresponding director plane $(\perp \beta)$, thus bearing to each other (as is well known) a constant ratio, which remains unchanged when we pass to the other (real) focal line (a'), and at the same time to the other (real) director plane $(\perp \beta')$: and the focal plane of these two lines (a, a') being perpendicular to that one of the three axes, which corresponds to the root (here c_1 by XXXII.) of the cubic, of which the reciprocal is algebraically intermediate between the reciprocals of the other two.

(15.) It is, however, more symmetric to employ the bifocal transformation (comp. 360, VI.*),

XXXV... 0 =
$$(Sa\rho)^2 - 2eSa\rho Sa'\rho + (Sa'\rho)^2 + (1 - e^2)\rho^2$$
;

in which the scalar constant e has the value (comp. XXIX'.),

XXXVI. . .
$$e = \cos 2a$$
;

and a, a' are the two \dagger real and focal unit lines, recently considered (15.).

^{*} It is to be remembered that, in the formula here cited, the symbols a, a' did not denote unit-vectors.

 $[\]dagger$ When those two vectors a, a' remain constant, but the scalar *e changes*, there arises a system of *biconfocal cones*: or, by their intersections with a concentric sphere, a system of *biconfocal sphero-conics*. Compare the second Note to page 191.

(16.) The equation XXXV., for the case of a *real cone*, may be thus written (comp. XXVI. XXXVI.),

XXXVII...
$$\angle \frac{\rho}{a} + \angle \frac{\rho}{a'} = \cos^{-1} e = 2a;$$

the sum* of the inclinations of the side ρ to the two focal lines a, a' being thus constant, and equal (as is well known) to the major axis of the spherical conic: and although, when e > 1, the cone becomes imaginary, yet it is then asymptotic to a real ellipsoid, as we shall shortly see.

407. The *bifocal form* (406, XXXV.) of the equation of a *cone* may suggest the corresponding *form*,

I...
$$C = Cf\rho = (Sa\rho)^2 - 2eSa\rho Sa'\rho + (Sa'\rho)^2 + (1 - e^2)\rho^2$$

in which a and a' are given and generally non-parallel unit-lines, while e and C are scalar constants, as capable of representing generally (comp. 360, (2.), (3.)) a central but non-conical surface $(f\rho = 1)$ of the second order. And we shall find that if, in passing from one such surface to another, we suppose a and a' to remain unchanged, but e and C to vary together, so as to be always connected by the relation,

II...
$$C = (e^2 - 1) (e + Saa')l^2$$
,

in which l is some real, positive, and *given scalar*, then all the surfaces I. so deduced, or in other words the surfaces represented by the common equation,

III...
$$l^2 = l^2 f \rho = \frac{(Sa\rho)^2 - 2eSa\rho Sa'\rho + (Sa'\rho)^2 + (1 - e^2)\rho^2}{(e^2 - 1)(e + Saa')},$$

with e for the only variable parameter, compose a Confocal System.

(1.) The scalar form III. of f_{ρ} gives the connected vector form,

IV...
$$l^2 v = l^2 \phi \rho = \frac{aS(a - ea')\rho + a'S(a' - ea)\rho + (1 - e^2)\rho}{(e^2 - 1)(e + Saa')},$$

[•] Or the difference, according to the choice between two opposite directions, for one of the two focal lines. The angular transformation XXXVII. may be accomplished, by resolving the equation XXXV. as a quadratic in e, and then interpreting the result.

ABTS. 406, 407.] SYSTEM OF CONFOCAL SURFACES.

which may also be thus written, with the value II. of C,

$$\nabla \ldots C\nu = C\phi\rho = (a - ea')\mathrm{S}a\rho + (a' - ea)\mathrm{S}a'\rho + (1 - e^2)\rho,$$

so that the function ϕ is self-conjugate, as it ought to be.

(2.) And because we have thus,

VI...
$$(e^2 - 1) l^2 \phi a = a' - ea, \quad (e^2 - 1) l^2 \phi a' = a - ea',$$

if we write, for abridgment,

VII... $a^2 = (e+1)l^2$, $b^2 = (e+Saa')l^2$, $c^2 = (e-1)l^2$,

we shall have the values,

VIII. . .
$$\begin{cases} \phi (a + a') = -a^{-2}(a + a'), \\ \phi Vaa' = -b^{-2}Vaa', \\ \phi (a - a') = -c^{-2}(a - a'); \end{cases}$$

comparing which with 405, (1.), (2.), we see that the three (real or imaginary) lines,

IX... aU(a + a'), bUVaa', cU(a - a'),

of any one of which the direction may be reversed, are the *three vector* semiaxes of the surfaces $f\rho = 1$; and therefore, by VII., that the system III. is one of confocals, as asserted.

(3.) The rectangular transformations, scalar and vector, are now (comp. 405, X., and 357, V. VIII.):

$$\begin{aligned} \mathbf{X}...l^{2} &= l^{2}/\rho = \frac{(\mathbf{S}\rho\mathbf{U}(a+a'))^{2}}{e+1} + \frac{(\mathbf{S}\rho\mathbf{U}\mathbf{V}aa')^{2}}{e+\mathbf{S}aa'} + \frac{(\mathbf{S}\rho\mathbf{U}(a-a'))^{2}}{e-1};\\ \mathbf{X}I...l^{2}\nu &= l^{2}\phi\rho = \frac{\mathbf{U}(a+a').\mathbf{S}\rho\mathbf{U}(a+a')}{e+1} + \frac{\mathbf{U}\mathbf{V}aa'.\mathbf{S}\rho\mathbf{U}\mathbf{V}aa'}{e+\mathbf{S}aa'} \\ &+ \frac{\mathbf{U}(a-a').\mathbf{S}\rho\mathbf{U}(a-a')}{e-1}; \end{aligned}$$

which can both be established, by the rules of the present Calculus, in several other ways, and from the first of which it follows that (as is well known) through any proposed point P of space there can in general be drawn three confocal surfaces, of a given system III.; one an ellipsoid, for which e > 1,

and therefore $a^2 > b^2 > c^2 > 0$; another a single-sheeted hyperboloid, for which e < 1, e > -Saa', $a^2 > b^2 > 0 > c^2$; and the third a double-sheeted hyperboloid, for which e < -Saa', e > -1, $a^2 > 0 > b^2 > c^2$.

(4.) From the other rectangular transformation XI. it follows, that if we denote by $\nu_1 = \phi_1 \rho$ what the normal vector $\nu = \phi \rho$ becomes, when ρ remains the same, but *e* is changed to a second root e_1 of the equation III. or X. of the surface, considered as a cubic in *e*, then

XII. . .
$$\frac{\nu_1 - \nu}{e_1 - e} = l^2 \phi \nu_1 = l^2 \phi_1 \nu = l^2 \phi_1 \phi \rho = l^2 \phi \phi_1 \rho;$$

 \mathbf{but}

$$XIII...S\rho\nu_1 = S\rho\nu = f_1\rho = f\rho = 1,$$

 $f_1\rho$ being formed from $f\rho$, by the substitution of e_1 for e; therefore,

 $XIV...0 = S\rho\phi\nu_1 = S\nu_1\phi\rho = S\nu_1\nu,$

and the known theorem results, that confocal surfaces cut each other orthogonally.*

(5.) It follows, from V. and VI., that the *inverse function* $\phi^{-1}\rho$ can be expressed as follows:

$$XV...\phi^{-1}\rho = l^2(aSa'\rho + a'Sa\rho) - b^2\rho;$$

or that ρ may be deduced from ν by the formula,

$$XVI...\rho = \phi^{-1}\nu = l^2(aSa'\nu + a'Sa\nu) - b^2\nu,$$

which can easily be otherwise established. Hence (comp. 361, (4.)), the equation of the surface *reciprocal* to the surface I. or III., or of that *new* surface which has ν (instead of ρ) for its *variable vector*, is

XVII...
$$1 = F\nu = S\nu\phi^{-1}\nu = 2l^2Sa\nu Sa'\nu - b^2\nu^2;$$

the fixed focal lines a, a' of the confocal system III., or of the corresponding system of the asymptotic cones, becoming thus (in agreement with known results) the fixed cyclic normals (or cyclic lines, eomp. 361, (6.)) of the reciprocal system XVII.

^{*} We shall soon see that the same formula XII., by expressing that v, v_1 , and ϕv_1 or $\phi_1 v$ are complanar, contains this other part of the known theorem referred to, that the intersection is a line of curvature, on each of the two confocals. [Compare 410, (12.).]

ART. 407.] RECTANGULAR SYSTEM OF THREE NORMALS.

(6.) In thus deducing the equation XVII. from III., no use has been made of the rectangular transformations X. XI., of the functions $f\rho$ and $\phi\rho$. Without the transformations last referred to, we could therefore have inferred, by a slight modification of the form XVII., that the reciprocal surface ($F\nu = 1$) with ν for its variable vector, which has the same rectangular system of directions for its three semiaxes as the original surface ($f\rho = 1$), but with inverse squares (the roots of its cubic) equal to the direct squares of the original semiaxes, has for equation (comp. 405, XII.),

if

$$X \vee III. \dots I = F \nu = l^2 (Sava' \nu - e\nu^2) = S \lambda \nu \mu \nu + g\nu^2,$$

XIX...
$$\lambda = la$$
, $\mu = la'$, $g = -el^2 = -eT\lambda\mu$;

the values VII. of a^2 , b^2 , c^2 being thus deduced *anew*, but by a process quite different from that employed in (2.), under the forms (comp. 405, XIII.),

XX...
$$a^2 = c_3 = -g + T\lambda\mu$$
; $b^2 = c_2 = -g + S\lambda\mu$; $c^2 = c_1 = -g - T\lambda\mu$;

while the *directions* IX. of the corresponding semiaxes may be deduced as those of a_3 , a_2 , a_1 , from the formulæ 405, XIV.

(7.) If the symbol $\omega(\nu)$, or simply $\omega\nu$, be used to denote a *new* linear and self-conjugate vector function of ν , defined by the equation,

XXI...
$$\omega \nu = \rho S \rho \nu - l^2 (a S a' \nu + a' S a \nu),$$

with ρ here treated as a vector constant, then (because $S\rho\nu = 1$) the equation XVI. may be thus written (comp. 354, &c.),

XXII...
$$(\omega + b^2)\nu = 0$$
;

the three rectangular directions, of the three normals ν , ν_1 , ν_2 to the three confocals through P, are therefore those which satisfy (comp. again 354) the vector quadratic equation,

XXIII. . .
$$\nabla \nu \omega \nu = 0$$
;

and they are the *directions* of the axes of this new surface of the second order (comp. 357, &c.),

$$XXIV...S\nu\omega\nu = (S\rho\nu)^2 - 2l^2Sa\nu Sa'\nu = 1,$$

in which ρ is still treated as a constant vector, but ν as a variable one.

(8.) The inverse squares of the scalar semiaxes of this new surface $(S_{\nu\omega\nu} = 1)$ are the direct squares b^2 , b_1^2 , b_2^2 of what may be called the mean semiaxes of

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the three confocals; these latter squares must therefore be the roots of this new cubic,

XXV...
$$0 = m + m'b^2 + m''(b^2)^2 + (b^2)^3$$
,

in which the coefficients m, m', m'', deduced here from the *new function* ω , as they were deduced from ϕ in the Section III. ii. 6, have the values,

XXVI...
$$\begin{cases} m = l^4 (\operatorname{Saa'}\rho)^2; \\ m' = l^4 (\operatorname{Vaa'})^2 + 2l^2 \operatorname{S}(\operatorname{Vap} \cdot \operatorname{Va'}\rho); \\ m'' = \rho^2 - 2l^2 \operatorname{Saa'}. \end{cases}$$

Accordingly, if we observe that (because Ta = Ta' = 1) we have among others the transformation,

XXVII...
$$(\operatorname{Saa'}\rho)^2 = \rho^2 (\operatorname{Vaa'})^2 - (\operatorname{Sap})^2 - 2\operatorname{Saa'}\operatorname{Sap}\operatorname{Sa'}\rho - (\operatorname{Sa'}\rho)^2$$
,

we can express this last cubic equation XXV., with these values XXVI. of its coefficients, under the form,

XXVIII...
$$0 = (b^2 + \rho^2) \{ (b^2 - l^2 Saa')^2 - l^4 \} + 2l^2 (b^2 - l^2 Saa') Sa\rho Sa'\rho - l^4 ((Sa\rho)^2 + (Sa'\rho)^2);$$

which, when we change b^2 by VII. to its value $l^2(e + Saa')$, and divide by l^4 , becomes the *cubic* in *e*, or the equation III. under the form,

XXIX...
$$0 = (e^2 - 1) \{ l^2(e + Saa') + \rho^2 \} + 2eSa\rho Sa'\rho - (Sa\rho)^2 - (Sa'\rho)^2.$$

(9.) As an additional test of the consistency of this whole theory and method, the directions of the three axes of the new surface XXIV., or those of the three normals (7.) to the confocals, or the three vector roots (354) of the equation XXIII., ought to admit of being assigned by three expressions of the forms,

XXX...
$$\begin{cases} n\nu = \psi \sigma + b^2 \chi \sigma + b^4 \sigma, \\ n_1 \nu_1 = \psi \sigma_1 + b_1^2 \chi \sigma_1 + b_1^4 \sigma_1, \\ n_2 \nu_2 = \psi \sigma_2 + b_2^2 \chi \sigma_2 + b_2^4 \sigma_2; \end{cases}$$

in which b^2 , b_1^2 , b_2^2 are the three scalar roots of the cubic XXV. or XXVIII., while σ , σ_1 , σ_2 are three arbitrary vectors; n, n_1 , n_2 are three scalar coefficients, which can be determined by the conditions $S\rho\nu = S\rho\nu_1 = S\rho\nu_2 = 1$ (comp. XIII.); and ψ , χ are two new auxiliary linear and vector functions, to be deduced here from the function ω , in the same manner as they were deduced from ϕ in the Section lately referred to.

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(10.) Accordingly, by the method of that Section, taking for convenience the given^{*} vector ρ (instead of the arbitrary vectors σ , σ_1 , σ_2) as the subject of the operations ψ and χ , we find the expressions,

XXXI...
$$\psi \rho = l^4 \nabla a a' \operatorname{Saa'} \rho$$
, $\chi \rho = l^2 (a \operatorname{Sa'} \rho + a' \operatorname{Sap} - 2\rho \operatorname{Saa'})$;

whence, after a few reductions, with elimination of n by the relation $S\rho\nu = 1$, and by the cubic in b^2 , the first equation XXX. becomes:

XXXII. . . 0 =
$$(b^2\nu + \rho)$$
 { $(b^2 - l^2Saa')^2 - l^4$ }
+ $l^2(b^2 - l^2Saa')$ ($aSa'\rho + a'Sa\rho$) - $l^4(aSa\rho + a'Sa'\rho)$;

which is in fact a *form* of the relation between ν and ρ , for any one of the confocals, as appears (for instance) by again changing b^2 to $l^2(e + Saa')$, and comparing with the equation IV.

(11.) Another and a more interesting *auxiliary surface*, of which the axes have still the directions of the normals ν , is found by *inverting* the new linear function ω , or by forming from XXII. the *inverse equation*,

in which,

$$XXXIII...(\omega^{-1}+b^{-2})\nu=0;$$

XXXIV...
$$\omega^{-1}\nu$$
. $(Saa'\rho)^2 = Vaa'Saa'\nu + l^{-2}(Va\rho Sa'\rho\nu + Va'\rho Sa\rho\nu);$

and from which it follows that the normals v to the confocals through P have the directions of the axes of this new cone,

XXXV... $S\nu\omega^{-1}\nu = 0$, or XXXVI... $0 = l^2(Saa'\nu)^2 + 2Sa\rho\nu Sa'\rho\nu$,

with ρ treated as a constant, as before.

(12.) The vertex of this auxiliary cone being placed at the given point P, of intersection of the three confocals, we may inquire in what curve is the cone cut, by the plane of the given focal lines, a, a', drawn through the common centre o of all the surfaces III. Denoting by $\sigma = ta + t'a'$ the vector of a point s of this sought section, and writing

XXXVII... $\nu = \sigma - \rho = ta + t'a' - \rho$,

the equation XXXVI. gives the relation,

XXXVIII...
$$tt' = \frac{l^2}{2} = \frac{a^2 - c^2}{4} = \text{const.};$$

* The general expressions for $\psi \sigma$ and $\chi \sigma$ include terms, which vanish when $\sigma = \rho$.

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the section is therefore an hyperbola, which is independent of the point P, and has the focal lines of the system for its asymptotes. And because its vector equation may be thus written (comp. 371, II.),

$$XXIX...\sigma = ta + \frac{1}{2}l^2t^{-1}a',$$

or what may be called its quaternion equation as follows (comp. 371, I.),

XL. . .
$$2\nabla a\sigma \cdot \nabla \sigma a' = l^2 (\nabla aa')^2$$
,

it satisfies the two scalar equations,

XLI...
$$m = 0, m' = 0,$$

with the significations XXVI. of m and m'; it is therefore that important curve, which is known by the name of the *Focal Hyperbola*:* namely the *limit* to which the section of the confocal surface by the plane of its extreme axes tends, when the mean axis (2b) tends to vanish. We are then led thus to the known theorem, that if, with any assumed point P for vertex, and with the focal hyperbola[‡] for base, a cone be constructed, the axes of this focal cone have the directions of the normals to the confocals through P.

(13.) As regards the *Focal Ellipse*, its two scalar equations may be deduced from the rectangular form X., by equating to zero both the numerator and the denominator of its last term; they are therefore,

XLII...
$$S(a - a')\rho = 0$$
, $2l^2 = (S\rho U(a + a'))^2 + \left(\frac{S\rho UVaa'}{S\sqrt{aa'}}\right)^2$;

the curve being thus given as a *perpendicular section* of an *elliptic cylinder*, with $l\sqrt{2}$ and $l\sqrt{(1 + Saa')}$, or $(a^2 - c^2)^{\frac{1}{2}}$ and $(b^2 - c^2)^{\frac{1}{2}}$, for the semiaxes of its base, or of the ellipse itself.

(14.) The same curve may also be represented by the equations,

 \mathbf{or}

XLIII... $Sa\rho = Sa'\rho$, $TVa\rho = (b^2 - c^2)^{\frac{1}{2}}$, XLIII'... $Sa'\rho = Sa\rho$, $TVa'\rho = (b^2 - c^2)^{\frac{1}{2}}$;

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^{*} Compare the Notes to pages 240, vol. i., and 17, vol. ii.

⁺ Namely, those two of which the squares algebraically include between them that of the third; this latter being, for the same reason, considered here as the mean.

[‡] We shall soon see that quaternions give, with equal ease, a more general known theorem, in which this is included as a limit. [Compare 408, (13.), page 214.]

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FOCAL ELLIPSE.

which express that it is the common intersection of its own plane $(\perp a - a')$ with two right cylinders,* which have the two focal lines a, a' of the system for their axes of revolution, and have equal radii, denoted each by the radical last written.

(15.) In general, the *unifocal form* (comp. 406, (13.)) of the equation III., namely,

XLIV...
$$0 = (1 - e^2) ((\nabla a \rho)^2 + b^2) + (S(a' - ea)\rho)^2$$
,

in which a and a' may be interchanged, shows that the two equal right cylinders,

or

XLV... $(\nabla a \rho)^2 + b^2 = 0$, XLV'... $(\nabla a' \rho)^2 + b^2 = 0$, XLVI... $T\nabla a \rho = b$, XLVI'... $T\nabla a' \rho = b$,

which are real if their common radius b be such, that is, if the confocal (e) be either an ellipsoid (supposed to be real), or else a single-sheeted hyperboloid, and which have the focal lines a, a' of the system for their axes of revolution, envelopet that confocal surface; the planes of the two ellipses of contact (which again are real curves, if b be real) being given by the equations,

XLVII. ... $S(a' - ea)\rho = 0$, **XLVII'.** ... $S(a - ea')\rho = 0$;

so that they pass through the centre o of the surface (or of the system), and are the (real) director planes (comp. 406, (14.)) of the asymptotic cone (real or imaginary), to the particular confocal (e).

(16.) Whether the mean semiaxis (b) be real or imaginary, the surface III. (supposed to be itself *real*) is always, by the form XLIV. of its equation, the *locus* of a system of *real ellipses* (comp. 404, (1.)), in planes parallel to the director plane XLVII., which have their centres on the focal line a, and are orthogonally projected into circles on a plane perpendicular to that line.

(17.) The same surface is also the locus of a second system of such ellipses, related similarly to the second focal line a', and to the second director

$$\rho = (a^2 - c^2)^{\frac{1}{2}} \operatorname{V.} a^t \operatorname{U} (a + a');$$

or by the same expression, with a and a' interchanged.

+ Compare pages 202, 236, 241, 315, vol. i.

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^{*} The reader may consult page 513 of the *Lectures*, for the case of this theorem which answers to a given *ellipsoid*. The *focal ellipse* may also be represented generally by the expression (comp. page 417, vol. i., of these *Elements*),

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plane XLVII'.; and it appears that *these two systems* of *elliptic sections* of a surface of the second order, which from some points of view are nearly as interesting as the *circular sections*, may conveniently be called its *Centro-Focal Ellipses*.

(18.) For example, when the first quaternion form (204, (14.), or 404, I.) of the equation of the ellipsoid is employed, one system of such ellipses coincides with the system (204, (13.)) of which, in the first generation^{*} of the surface, the ellipsoid was treated as the locus; and an analogous generation of the two hyperboloids, by geometrical deformation of two corresponding surfaces of revolution, with certain resulting homologies (comp. sub-arts. to 274), through substitution of (centro-focal) ellipses for circles, conducts to equations of those hyperboloids of the same unifocal form; namely, if a and β have significations analogous to those in the cited equation of the ellipsoid (so that β and not a is here a focal line),

XLVIII...
$$\left(S\frac{\rho}{a}\right)^2 + \left(V\frac{\rho}{\beta}\right)^2 = \mp 1;$$

the upper or the lower sign being taken, according as the surface consists of one sheet or of two.

(19.) It may also be remarked that as, by changing β to *a* in the corresponding equation of the *ellipsoid*, we could return (comp. 404, (1.)) to a form (403, XI.) of the equation of the *sphere*, so the same change in

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^{*} Besides that *first generation* (I) of the Ellipsoid, which was a *double* one, in the sense that a second system (17.) of generating ellipscs might be employed, and which served to connect the surface with a concentric sphere, by certain relations of homology (274); and the second double generation or construction (II), by means of either of two diacentric spheres (217, (4.), (6.), (7.), and 220, (3.)), which was illustrated by fig. 53 (page 234, vol. i., and page 184, vol. ii.) : several other generations of the same important surface were deduced from quaternions in the Lectures to which it is only possible here to refer. A reader, then, who happens to have a copy of that earlier work, may consult page 499 for a generation (III) of a system of two reciprocal ellipsoids, with a common mean axis (2b), by means of a moving sphere, of which the radius (= b) is given, but of which the centre has the original ellipsoid for its locus; while the corresponding point on the reciprocal surface, and also the normals at the two points, are easily deduced from the construction. In page 502, he will find another and perhaps a simpler generation (IV), of the same pair of reciprocal ellipsoids, by means of quadrilaterals inscribed in a fixed sphere (the common mean sphere, comp. 216, (10.)); the directions of the four sides of such a quadrilateral being given, and one pair of opposite sides intersecting in a point of one surface, while the other pair have for their intersection the corresponding point of the other (or reciprocal) ellipsoid. In the page last cited, and in the following page, there is given a new double generation (V) of any one ellipsoid; its circular sections (of either system) being constructed as intersections of two equal spheres (or spheric surfaces), of which the line of centres retains a fixed direction, while the spheres slide within two equal and right cylinders, whose axes intersect each other

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XLVIII. conducts to equations of the equilateral hyperboloids of revolution, of one sheet and of two, under the very simple forms* (comp. 210, XI.),

XLIX...
$$S\left(\frac{\rho}{a}\right)^2 = -1$$
, and L... $S\left(\frac{\rho}{a}\right)^2 = +1$;

in which it seems unnecessary to insert *points* after the signs S, and of which the geometrical *interpretations* become obvious when then they are written thus (comp. 199, ∇ .),

LI. . .
$$T\frac{\rho}{a} = \sqrt{\sec 2\left(\frac{\pi}{2} - \angle \frac{\rho}{a}\right)}, \quad LII. . . T\frac{\rho}{a} = \sqrt{\sec 2} \angle \frac{\rho}{a};$$

where $T\frac{\rho}{a} = \overline{\text{oP}} : \overline{\text{oA}}$, while $\angle \frac{\rho}{a}$ is the inclination AOP of the semidiameter or to the axis of revolution oA, and $\frac{\pi}{2} - \angle \frac{\rho}{a}$ is the inclination of the same semidiameter to a *plane* perpendicular to that axis.

(20.) The *real cyclic forms* of the equation of the surface III. might be deduced from the *unifocal form* XLIV., by the general method of the sub-articles to 359; but since we have ready the *rectangular form* X., it is simpler to obtain them from that form, with the help of the identity,

LIII...
$$-\rho^2 = (S\rho U(a + a'))^2 + (S\rho U Vaa')^2 + (S\rho U(a - a'))^2$$

by eliminating the first of these three terms for the case of a single-sheeted

(in the centre of the generated surface), and of which the common radius is the mean semiaxis (b). Finally, in page 699 of the same volume, there will be found a new generation (VI) of the original ellipsoid (abc), analogous to the generation (IV) by the fixed (mean) sphere, but with new directions of the sides of the quadrilaterals, which are also (in this last generation) inscribed in the circles of a certain mean ellipsoid (or prolate spheroid) of revolution, which has the mean axis (2b) for its major axis; and has two medial foci on that axis, whose common distance from the centre is represented by the expression,

$$\frac{\sqrt{(a^2-b^2)}\sqrt{(b^2-c^2)}}{\sqrt{(a^2-b^2+c^2)}};$$

the common tangent plancs, to this mean (or medial) ellipsoid, and to the given (or generated) ellipsoid (abc), which are parallel to their common axis (2b), being parallel also to the two umbilicar diameters of the latter surface.

* The same forms, but with σ for ρ , and β for a, may be deduced from XLVIII. on the plan of 274, (2.), (4.), by assuming an auxiliary vector σ such that $S\frac{\sigma}{\beta} = \pm S\frac{\rho}{a}$, and $V\frac{\sigma}{\beta} = V\frac{\rho}{\beta}$; the homologies, above alluded to, between the general hyperboloid of either species, and the equilateral hyperboloid of revolution of the same species, admitting also thus of being easily exhibited.

hyperboloid (for which $b^{-2} > a^{-2} > 0 > c^{-2}$); the second for an ellipsoid $(c^{-2} > b^{-2} > a^{-2} > 0)$; and the third for a double-sheeted hyperboloid $(a^{-2} > 0 > c^{-2} > b^{-2})$.

(21.) Whatever the species of the surface III. may be, we can always derive from the unifocal form XLIV. of its equation what may be called an *Exponential Transformation*; namely the vector expression,

LIV...
$$\rho = xa + y \nabla a^t \beta$$
, with LV... $x^2 fa + y^2 f \nabla a a' = 1$;

the scalar exponent, t, remaining arbitrary, but the two scalar coefficients, x and y, being connected by this last equation of the second degree: provided that the new constant vector β be derived from a, a', and e, by the formula,

$$L\nabla I...\beta = \frac{(a'-ea)UVaa'}{e+Saa'},$$

which gives after a few reductions (comp. the expression 315, III. for a^t , when Ta = 1),

LVII... $\nabla a\beta = U\nabla aa', \quad S(a' - ea)\beta = 0, \quad Saa'\beta = 0;$ LVIII... $\nabla a^t\beta = \beta S \cdot a^t + U\nabla aa' \cdot S \cdot a^{t-1};$ LIX... $\nabla \cdot a\nabla a^t\beta = a^tU\nabla aa' = T^{-1}1;$ LX... $S(a' - ea)\rho = x(e + Saa'), \quad \nabla a\rho = ya^tU\nabla aa';$ LXI... $fa = a^{-2}b^2c^{-2}, \quad \text{and} \quad LXII... f\beta = fU\nabla aa' = b^{-2}.$

while

(22.) If we treat the exponent, t, as the only variable in the expression LIV. for ρ , then (comp. 314, (2.)) that exponential expression represents what we have called (17.) a centro-focal ellipse; the distance of its centre (or of its plane) from the centre of the surface, measured along the focal line a, being represented by the coefficient x; and the radius of the right cylinder, of which the ellipse is a section, or the radius of the circle (16.) into which that ellipse is projected, on a plane $\perp a$, being represented by the other coefficient, y: while $\frac{1}{2}t\pi$ is the excentric anomaly.

(23.) If, on the contrary, we treat the exponent t as given, but the coefficients x and y as varying together, so as to satisfy the equation LV. of the second degree, the expression L1V, then represents a different section

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of the surface III., made by a plane through the line a, which makes with the focal plane (of a, a') an angle $=\frac{t\pi}{2}$; this latter section (like the former) being always real, if the surface itself be such : but being an ellipse for an ellipsoid, and an hyperbola for either hyperboloid, because

LXIII... $fa \cdot f U V aa' = a^{-2}c^{-2}$ by LXI. and LXII.

(24.) And it is scarcely necessary to remark, that by interchanging a and a' we obtain a Second Exponential Transformation, connected with the second system (17.) of centro-focal ellipses, as the first exponential transformation LIV. is connected with the first system (16.).

(25.) The asymptotic cone $f\rho = 0$ has likewise its two systems of centrofocal ellipses, and its equation admits in like manner of two exponential transformations, of the form LIV.; the only difference being, that the equation LV. is replaced by the following,

LXIV. . .
$$x^2 f a + y^2 f' U V a a' = 0$$
,

in which, for a *real cone*, the coefficients of x^2 and y^2 have opposite signs by (23.).

(26.) Finally, as regards the *confocal relation* of the surfaces III., which may represent *any confocal system* of surfaces of the second order, it may be perceived from (4.) that an *essential character* of such a relation is expressed by the equation,

$$\mathbf{LXV...V}\nu,\phi\nu = \mathbf{V}\nu\phi,\nu;$$

which may perhaps be called, on that account, the Equation of Confocals.

(27.) It is understood that the *two confocal surfaces* here considered, are represented by the two scalar equations,

LXVI...
$$S\rho\phi\rho = 1$$
, $S\rho\phi\rho = 1$, or LXVI'... $f\rho = 1$, $f\rho = 1$;

and that the two linear and vector functions, v and v, of an arbitrary vector ρ , which represent normals to the two concentric and similar and similarly posited surfaces,

LXVII...
$$f\rho = \text{const.}, f_{\rho} = \text{const.},$$

passing through any proposed point P, are expressed as follows,

LXVIII...
$$\nu = \phi \rho$$
, $\nu_{i} = \phi_{i} \rho$.

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(28.) It is understood also, that the two surfaces LXVI. or LXVI'. are not only *concentric*, as their equations show, but also *coaxal*, so far as the *directions* of their *axcs* are concerned: or that the *two vector quadratics* (comp. 354),

LXIX...
$$\nabla \rho \phi \rho = 0$$
, and LXX... $\nabla \rho \phi_{\rho} \rho = 0$,

are satisfied by one common system of three rectangular unit lines. And with these understandings, it will be found that the equation LXV., which has been called above the Equation of Confocals, is not only necessary but sufficient, for the establishment of the relation required.

(29.) It is worth while however to observe, before closing the present series of sub-articles, that the equations XII., and those formed from them by introducing e_2 and ν_2 , give the following among other relations :

LXXI...
$$f U_{\nu_1} = (b^2 - b_1^2)^{-1} = -f_1 U_{\nu}; f_1 U_{\nu_2} = (b_1^2 - b_2^2)^{-1} = -f_2 U_{\nu_1};$$
 &c.
and
and LXXII... $f(\nu_1, \nu_2) = f_1(\nu_2, \nu) = f_2(\nu, \nu_1) = 0;$
and therefore,
LXXIII... $f_1\{(b_2^2 - b_1^2)^{\frac{1}{2}}U_{\nu_2} \pm (b_1^2 - b^2)^{\frac{1}{2}}U_{\nu}\} = 0;$

whence it is easy to see that the *two vectors* under the functional sign f_1 in this last expression have the directions of generating lines of the single-sheeted hyperboloid (e₁) through P, if we suppose that $b_2^2 > b_1^2 > 0 > b^2$, so that the confocal (e₂) is here an ellipsoid, and (e) a double-sheeted hyperboloid.

(30.) But if σ be taken to denote the variable vector of the *auxiliary* surface XXIV., the equation of that surface may by (7.) and (8.) be brought to the following rectangular form, with the meaning XXI. of ω ,

LXXIV...1 =
$$S\sigma\omega\sigma = (S\rho\sigma)^2 - 2l^2Sa\sigma Sa'\sigma = b^2(S\sigma U\nu)^2 + b_1^2(S\sigma U\nu_1)^2 + b_2^2(S\sigma U\nu_2)^2;$$

hence, with the inequalities (29.), its cyclic normals, or those of its asymptotic cone $S_{\sigma\omega\sigma} = 0$, or the focal lines of the reciprocal cone $S_{\sigma\omega^{-1}\sigma} = 0$, that is of the cone XXXVI., or finally the focal lines of the focal^{*} cone (12.), which rests on the focal hyperbola, have the directions of the lines LXXIII.; those focal lines are therefore (by what has just been seen) the generating lines of the hyperboloid (e₁), which passes through the given point P.

(31.) And for an arbitrary σ we have the transformation,

LXXV... $l^{-2}(S\rho\sigma)^2 - Sa\sigma a'\sigma = e(S\sigma U\nu)^2 + e_1(S\sigma U\nu_1)^2 + e_2(S\sigma U\nu_2)^2$.

^{*} A more general known theorem, including this, will soon be proved by quaternions [page 213].

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EQUATIONS OF CONJUGATION.

408. The general equation* of conjugation,

I. . .
$$f(\rho, \rho') = 1$$
, 405, III.

connecting the vectors ρ , ρ' of any two points P, P' which are conjugate with respect to the central but non-conical surface $f\rho = 1$, may be called for that reason the Equation of Conjugate Points; while the analogous equation,

II...
$$f(\rho, \rho') = 0$$
,

which replaces the former for the case of the asymptotic cone $f\rho = 0$, may be called by contrast the Equation of Conjugate Directions: in fact, it is satisfied by any two conjugate semidiameters, as may be at once inferred from the differential equation $f(\rho, d\rho) = 0$ of the surface $f\rho = \text{const.}$ (comp. 362). Each of these two formulæ admits of numerous applications, among which we shall here consider the deduction, and some of the transformations, of the Equation of a Circumscribed Cone,

III. . .
$$(f(\rho, \rho') - 1)^2 = (f\rho - 1) (f\rho' - 1);$$

which may also be considered as the Condition of Contact, of the right line PP' with the surface $f\rho = 1$.

(1.) In this last view, the equation III. may be at once deduced, as the condition of *equal roots* in the scalar and *quadratic* equation (comp. 216, (2.), and 316, (30.)),

or

IV. . . 0 =
$$f(x\rho + x'\rho') - (x + x')^2$$
,
V. . . 0 = $x^2(f\rho - 1) + 2xx'(f(\rho, \rho') - 1) + x'^2(f\rho' - 1)$;

which gives in general the *two vectors of intersection*, as the two values of the expression $\frac{x\rho + x'\rho'}{x + x'}$.

• For the notation used, Art. 362 may be again referred to. [On page 550, vol. i., are printed the formulæ

and

$$f(\rho, \rho') = f(\rho', \rho) = S\rho\phi\rho' = S\rho\phi\rho$$
$$f(\rho, \rho) = f\rho,$$

which sufficiently explain the notation employed.]

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(2.) If we treat the point P' as given, and denote the two secants drawn from it in any given direction τ by $t_1^{-1}\tau$ and $t_2^{-1}\tau$, then t_1 and t_2 are the roots of this other quadratic, $f(\rho' + t^{-1}\tau) = 1$, or

VI...
$$0 = f(t\rho' + \tau) - t^2 = t^2(f\rho' - 1) + 2tf(\rho', \tau) + f\tau;$$

denoting then by $t_0^{-1}\tau$ the harmonic mean of these two secants, so that $2t_0 = t_1 + t_2$, and writing $\rho = \rho' + t_0^{-1}\tau$, we have

VII. . .
$$t_0(1 - f\rho') = f(\rho', \tau), \quad f(\rho, \rho') = 1;$$

we are then led in this way to the formula I., as the Equation of the Polar Plane of the point r', if that plane be here supposed to be defined by its well-known harmonic property (comp. 215, (16.), and 316, (31.), (32.)).

(3.) At the same time we obtain this other form of the condition of contact III., as that of equal roots in VI.,

VIII...
$$f(\rho', \tau)^2 = f\tau \cdot (f\rho' - 1),$$

the first member being an abridgment of $(f(\rho', \tau))^2$: and because this last equation VIII. is homogeneous with respect to τ , it represents a cone, namely the Cone of Tangents (τ) to the given surface $f\rho = 1$, from the given point \mathbf{r}' . Accordingly it is easy to prove that the equation III. may be thus written,

IX. . . $f(\rho', \rho - \rho')^2 = f(\rho - \rho') \cdot (f\rho' - 1),$

under which last form it is seen to be homogeneous with respect to $\rho - \rho'$.

(4.) Without expressly introducing τ , the transformation IX. shows that the equation III. represents some cone, with the given point r' for its vertex; and because the *intersection* of this cone with the given surface is expressed by the square of the equation I. of the polar plane of that point, the cone must be (as above stated) circumscribed to the surface $f_{\rho} = 1$, touching it along the curve (real or imaginary) in which that surface is cut by that plane I.

(5.) Another important transformation, or set of transformations, of the equation III. may be obtained as follows. In general, for any two vectors ρ and ρ' , if the scalar constant *m*, the vector function ψ , and the scalar function *F*, be derived from the linear and vector function ϕ , which is here *self-conjugate* (405), by the method of the Section III. ii. 6, we have successively,

$$\begin{aligned} \mathbf{X}. \dots f(\rho, \rho')^2 - f\rho \cdot f\rho' &= \mathbf{S}\rho\phi\rho' \cdot \mathbf{S}\rho'\phi\rho - \mathbf{S}\rho\phi\rho \cdot \mathbf{S}\rho'\phi\rho' &= \mathbf{S}\left(\nabla\rho\rho' \cdot \nabla\phi\rho\phi\rho'\right) \\ &= \mathbf{S} \cdot \rho\rho' \psi \nabla\rho\rho' = m\mathbf{S} \cdot \rho\rho' \phi^{-1} \nabla\rho\rho' = mF \nabla\rho\rho'; \end{aligned}$$

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and thus the equation III. of the circumscribed cone becomes,

XI...
$$mF\nabla\rho\rho' + f(\rho - \rho') = 0$$
, or XII... $mF\nabla\tau\rho' + f\tau = 0$,

if $\tau = \rho - \rho'$ be a tangent from P'. Or because $\phi \psi = m$, and $m = -c_1 c_2 c_3 = -\alpha^{-2} b^{-2} c^{-2}$, by 406, XXIV., we may write (with $\tau = \rho - \rho'$) either

XIII...
$$0 = S\tau\psi^{-1}\tau + S\upsilon\phi^{-1}\upsilon$$
, if $\upsilon = \nabla\tau\rho' = \nabla\rho\rho'$,

XIV...
$$F \nabla \rho \rho' = a^2 b^2 c^2 f(\rho - \rho')$$

or

as the condition of contact of the line PP' with the surface $f\rho = 1.*$

(6.) A geometrical interpretation, of this last form XIV. of that condition, can easily be assigned as follows. Supposing at first for simplicity that the surface is an ellipsoid, let P be the point of contact, so that $f\rho = 1$, $f(\rho, \tau) = 0$; and let the tangent PF' be taken equal to the parallel semidiameter or, so that $f\tau = f(\rho - \rho') = 1$. Then, with the signification XIII. of ν , the equation XIV. becomes,

$$XV...\sqrt{Fv} = Tv.\sqrt{FUv} = abc;$$

in which the factor Tv represents the area of the parallelogram under the conjugate semidiameters or, or of the given surface $f\rho = 1$; while the other factor \sqrt{FUv} represents the reciprocal of the semidiameter of the reciprocal surface Fv = 1, which is perpendicular to their plane ror; or the perpendicular distance between that plane, and a parallel plane which touches the given ellipsoid: so that their product \sqrt{Fv} is equal, by elementary principles, to the product of the three semiaxes, as stated in the formula XV. And the result may easily be extended by squaring, to other central surfaces.

(7.) It may be remarked in passing, that if ρ , σ , τ be any three conjugate semidiameters of any central surface $f\rho = 1$, so that

XVI. . . $f\rho = f\sigma = f\tau = 1$, and **XVII.** . . $f(\rho, \sigma) = f(\sigma, \tau) = f(\tau, \rho) = 0$,

^{• [}The constituents of these auxiliary vectors v and τ correspond to Plücker's six coordinates of a right line. A scalar equation of the type $f(v, \tau) = 0$ represents a complex of right lines provided the relation is independent of the absolute magnitudes of the tensors of v and τ . The lines of the complex which pass through the extremity of a given vector \dot{p}' lie on the cone $f(\nabla \tau p', \tau) = 0$, τ being variable. Moreover, if $S\lambda \rho = 1$, $S\lambda' \rho = 1$ are the equations of any pair of planes through the right line (v, τ) , and if we take the new auxiliary vectors $\tau_1 = \lambda - \lambda'$ and $v_1 = \nabla \lambda \lambda'$, it is easy to prove that $\tau_1 = xv$ and $v_1 = x\tau$, x being a scalar. Thus we may replace v and τ by τ_1 and v_1 respectively in the equations of the complex, and we have $f(\tau_1, v_1) = 0$ or $f(\tau_1, \nabla \tau_1 \lambda') = 0$. The second of these equations when λ' is regarded as known, and τ_1 as variable represents the reciprocal of the cone whose vertex is at the origin and which is touched by the lines of the complex which lie in the arbitrary plane $S\lambda' \rho = 1$.]

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and if $x\rho + y\sigma + z\tau$ be any other semidiameter of the same surface, we have then the scalar equation,

XVIII...
$$f(x\rho + y\sigma + z\tau) = x^2 + y^2 + z^2 = 1$$
;

a relation between the coefficients, x, y, z, which has been already noticed for the *ellipsoid* in 99, (2.), and in 402, I., and is indeed deducible for *that* surface, from principles of *real scalars* and *real vectors* alone: but in extending which to the *hyperboloids*, one at least of those three *coefficients* becomes *imaginary*, as well as one at least of the three vectors ρ , σ , τ .

(8.) Under the same conditions XVI. XVII., we have also,

XIX...
$$\nabla \rho \sigma = \pm abc\phi \tau = \pm (-m)^{-\frac{1}{2}}\phi \tau$$
;
XX... $\tau = \pm (-m)^{\frac{1}{2}}\phi^{-1}\nabla \rho \sigma = \mp (-m)^{-\frac{1}{2}}\nabla \phi \rho \phi \sigma$;
XXI... $S\rho\sigma\tau = \pm abc = \pm (-m)^{-\frac{1}{2}}$;

together with this very simple relation,

XXII. . .
$$S\rho\sigma\tau$$
 . $S\phi\rho\phi\sigma\phi\tau = -1$.

(9.) Under the same conditions, if $x_{\rho} + y_{\sigma} + z_{\tau}$ and $x'_{\rho} + y'_{\sigma} + z'_{\tau}$ have only conjugate directions, that is, if they have the directions of any two conjugate semidiameters, the six scalar coefficients must satisfy (comp. II.) the equation,

$$XXIII. \dots xx' + yy' + zz' = 0.$$

(10.) The equation VIII., with ρ for ρ' , may be written under the form,

XXIV... $0 = S\sigma \tau = S\tau \omega \tau$, if XXV... $\sigma = \omega \tau = \phi \rho S \rho \phi \tau + \phi \tau (1 - f \rho)$,

= a new linear and vector function, which represents a normal to the cone of tangents from \mathbf{r} , to the surface $f\rho = 1$. Inverting this last function, we find

XXVI...
$$\tau = \omega^{-1}\sigma = \frac{\phi^{-1}\sigma - \rho S \rho \sigma}{1 - f \rho};$$

the equation in σ of the reciprocal cone, or of the cone of normals to the circumscribed cone from P, is therefore,

or finally
$$\begin{array}{c} XXVII. \ldots S\sigma\omega^{-1}\sigma = 0, \quad \text{or} \quad XXVIII. \ldots F\sigma = (S\rho\sigma)^2, \\ XXVIII'. \ldots F(\sigma: S\rho\sigma) = 1; \end{array}$$

a remarkably simple form, which admits also of a simple interpretation. In

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fact, the line σ : Sp σ is the reciprocal of the perpendicular, from the centre o, on a tangent plane to the cone, which is also a tangent plane to the surface; it is therefore one of the values of the vector ν (comp. (6.), and 373, (21.)), and consequently it is a semidiameter of the reciprocal surface $F\nu = 1$.

(11.) As an application of the equation XXVIII., let the surface be the *confocal* (e), represented by the equation 407, III. or X., of which the *reciprocal* is represented by 407, XVII. or XVIII. Substituting for $F\sigma$ its value thus deduced, the equation of the *reciprocal cone* (10.), with σ for a *side*, becomes,*

XXIX. . . $2l^2 \mathrm{Sa}\sigma \mathrm{Sa}'\sigma - (\mathrm{S}\rho\sigma)^2 = b^2\sigma^2$, or

XXIX'... Sava'
$$\sigma - l^{-2}(S\rho\sigma)^2 = e\sigma^2$$
;

if then the vertex P be fixed, but the confocal vary, by a change of e, or of b^2 which varies with it, the cone XXIX. will also vary, but will belong to a biconcyclic system; whence it follows that the (direct or) circumscribed cones from a given point are all biconfocal: and also, by 407, (30.), that their common focal lines are the generating lines of the confocal hyperboloid \dagger of one sheet, which passes through their common vertex.

(12.) Changing e to e, in XXIX'., and using the transformation 407, LXXV., with the identity (comp. 407, LIII.),

$$-\sigma^{2} = (\mathrm{S}\sigma\mathrm{U}\nu)^{2} + (\mathrm{S}\sigma\mathrm{U}\nu_{1}) + (\mathrm{S}\sigma\mathrm{U}\nu_{2})^{2},$$

we find that if σ be a normal to the cone of tangents from **p** to (e_i) , it satisfies the equation,

XXX...
$$0 = (e - e_i) (S\sigma U\nu)^2 + (e_1 - e_j) (S\sigma U\nu_1)^2 + (e_2 - e_j) (S\sigma U\nu_2)^2;$$

and therefore that if τ be a *tangent* from the same point P, to the same confocal (e_i) , it satisfies this other condition,

XXXI...
$$0 = (e - e_j)^{-1} (S \tau U \nu)^2 + (e_1 - e_j)^{-1} (S \tau U \nu_1)^2 + (e_2 - e_j)^{-1} (S \tau U \nu_2)^2,$$

which thus is a form of the equation of the *circumscribed cone* to (e_i) , with its *vertex* at a given point **P**: the confocal character (11.) of all such cones being hereby exhibited anew.

^{*} It may be observed that, when b = 0, this equation XXIX. represents the *ymptotic cone* the *auxiliary surface* 407, XXIV.; and at the same time the *reciprocal* of that *focal cone*, 407, XXXVI., which rests on the *focal hyperbola*.

[†] This theorem (which includes that of 407, (30.)) is cited from Jacobi, and is proved, in page 143 of Dr. Salmon's Treatise, referred to in several former Notes.

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(13.) It follows also from XXXI., that the axes of every cone thus circumscribed have the directions of the normals ν , ν_1 , ν_2 to the three confocals through P; and this known theorem^{*} may be otherwise deduced, from the Equation of Confocals (407, LXV.), by our general method, as follows. That equation gives

 $\nu_{i} - \nu \parallel \phi_{i} \nu$ (because $\phi \nu_{i} = \phi_{i} \nu$), and therefore,

XXXII... $(\nu_i - \nu)$ S $\nu\nu_i = \phi_i \nu (f_i \rho - 1)$, $\nabla \nu \nu_i$ S $\nu\nu_i + \nabla \nu \phi_i \nu (1 - f_i \rho) = 0$;

changing then ∇ to S, and ν to τ , we see that ν , ν_1 , ν_2 , as being the roots (354) of this last vector quadratic XXXII., have the directions of the axes of the cone, with τ for side,

XXXIII. . .
$$f_{\mu}(\rho, \tau)^{2} + f_{\mu}\tau \cdot (1 - f_{\mu}\rho) = 0;$$

that is, by VIII., the directions of the axes of the cone of tangents, from P to (c_i) .

(14.) As an application of the formula XIV., with the abridged symbols τ and v of (5.) for $\rho - \rho'$ and $\nabla \rho \rho'$, the condition of contact of the line PF with the confocal (e) becomes, by the expressions 407, III., XVIII., and VII. for the functions f, F, and the squares a^2 , b^2 , c^2 , the following quadratic in e:

XXXIV...
$$(\mathrm{Sa}\tau)^2 - 2e\mathrm{Sa}\tau\mathrm{Sa}\tau + (\mathrm{Sa}'\tau)^2 + (1-e^2)\tau^2 = l^{-2}(\mathrm{Sa}\upsilon a'\upsilon - e\upsilon^2);$$

there are therefore in general (as is known) two confocals, say (e) and (e,), of a given system, which touch a given right line; and their parameters, \dagger e and e, are the two roots of the last equation: for instance, their sum is given by the formula,

XXXV...
$$(e + e_i)\tau^2 = l^{-2}v^2 - 2\mathrm{Sar}\mathrm{Sa'}\tau$$
.

(15.) Conceive then that ρ is a given semidiameter of a given confocal (e), and that $d\rho$ is a tangent, given in direction, at its extremity; the equation XXXIV. will then of course be satisfied,[‡] if we change τ to $d\rho$, and v to $V\rho d\rho$, retaining the given value of e; but it will also be satisfied, for the same

$$f\rho \cdot f \mathrm{d}\rho - a^{-2}b^{-2}c^{-2}F \mathrm{V}\rho \mathrm{d}\rho = f(\rho, \mathrm{d}\rho)^2.$$

^{*} Compare the third Note to page 202.

t This name of *parameter* is here given, as in 407, to the arbitrary constant $e = \frac{a^2 + c^2}{a^2 - c^2}$ of which the value distinguishes *one* confocal (e) of a system from another.

[‡] In fact it follows easily from the transformations (5.), that

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 ρ and d ρ (or for the same τ and v), when we change e to this new parameter,

XXXVI. . .
$$e_{l} = -e + 2SaUd\rho \cdot Sa'Ud\rho - l^{-2}(V\rho Ud\rho)^{2};$$

that is to say, the new confocal (e_i) , with a parameter determined by this last formula, will touch the given tangent to the given confocal (e).

(16.) If we at once make $l^2 = 0$ in the equation 407, III. of a Confocal System of Central Surfaces, leaving the parameter *e finite*, we fall back on the system 406, XXXV. of Biconfocal Cones; but if we conceive that l^2 only tends to zero, and that *e* at the same time tends to positive infinity, in such a manner that their product tends to a finite limit, r^2 , or that

XXXVII... $\lim l = 0$, $\lim e = \infty$, $\lim el^2 = r^2$,

then the equation of the surface (e) tends to this limiting form,

XXXVIII...
$$\rho^2 + r^2 = 0$$
, or XXXVIII'... $T\rho = r$;

a system of biconfocal cones is therefore to be combined with a system of concentric spheres, in order to make up a complete confocal system.

(17.) Accordingly, any given right line PP' is in general touched by only one cone of the system just referred to, namely by that particular cone (e), for which (comp. XXXIV.) we have the value,

XXXIX...
$$e = Sava'v^{-1}$$
, or XXXIX'... $e + Saa' = 2SavSa'v^{-1}$,

with $v = \nabla \rho \rho'$, as before, so that v is perpendicular to the given plane OPP', which contains the vertex and the line; in fact, the reciprocals of the biconfocal cones 406, XXXV., when a, a' are treated as given unit lines, but e as a variable parameter, compose the biconcyclic* system (comp. 407, XVIII.),

XL... Sava'
$$\nu = e\nu^2$$
.

But, besides the *tangent cone* thus found, there is a *tangent sphere* with the same centre o; of which, by passing to the limits XXXVII., the radius r may be found from the same formula XXXIV. to be,

XLI...
$$r = T \frac{v}{\tau} = T \frac{\nabla \rho \rho'}{\rho - \rho'};$$

and such is in fact an expression (comp. 316, L.) for the length of the perpendicular from the origin on the given line PP'.

^{*} The bifocal form o the equation of this reciprocal system of cones XL. was given in 406, XXV., but with other constants (λ, μ, g) , connected with the cyclic form (406, I.) of the equation of the given system.

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(18.) In general, the equation XXXIV. is a form of the equation of the cone, with ρ for its variable vector, which has a given vertex r', and is circumscribed to a given confocal (e). Accordingly, by making e = -Saa' in that formula, we are led (after a few reductions, comp. 407, XXVII.) to an equation which may be thus written,

XLII...
$$0 = l^2 (Saa'\tau)^2 + 2Sa\rho'\tau Sa'\rho'\tau$$
,

with the variable side $\tau = \rho - \rho'$, as before; and which differs only by the substitution of ρ' and τ for ρ and ν , from the equation 407, XXXVI. for that *focal cone*, which rests on the *focal hyperbola*. The other (real) *focal cone* which has the same arbitrary vertex \mathbf{P}' , but rests on the *focal ellipse*, has for equation,

XLIII. . .
$$l^2(S(a - a')\tau)^2 = Sava'v - v^2$$
,

as is found by changing e to 1 in the same formula XXXIV.

(19.) It is however simpler, or at least it gives more symmetric results, to change e_i in XXXI. to -Saa' for the focal hyperbola, and to +1 for the focal ellipse, in order to obtain the *two real focal cones* with P for vertex, which rest on those two curves; while that *third* and wholly *imaginary focal cone*, which has the same vertex, but rests on the known *imaginary focal curve*, in the plane of b and c, is found by changing e_i to -1. This imaginary focal cone, and the two real ones which rest as above on the hyperbola and ellipse respectively, may thus be represented by the three equations,

XLIV. . . 0 =
$$a^{-2}(S_T U_\nu)^2 + a_1^{-2}(S_T U_{\nu_1})^2 + a_2^{-2}(S_T U_{\nu_2})^2$$
;
XLV. . . 0 = $b^{-2}(S_T U_\nu)^2 + b_1^{-2}(S_T U_{\nu_1})^2 + b_2^{-2}(S_T U_{\nu_2})^2$;
XLVI. . . 0 = $c^{-2}(S_T U_\nu)^2 + c_1^{-2}(S_T U_{\nu_1})^2 + c_2^{-2}(S_T U_{\nu_2})^2$;

 τ being in each case a side of the cone, and ν , ν_1 , ν_2 having the same significations as before.

(20.) On the other hand, if we place the vertex of a circumscribed cone at a point r of a *focal curve*, real or imaginary, the *enveloped surface* being the confocal (e_i) , we find first, by XXX., for the *reciprocal* cones, or *cones of* normals σ , with the same order of succession as in (19.), the three equations,

XLVII. . .
$$a^2(SU\nu\sigma)^2 = a_r^2$$
;
XLVIII. . . $b^2(SU\nu\sigma)^2 = b_r^2$;
XLIX. . . $c^2(SU\nu\sigma)^2 = c_r^2$;

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and next, for the *circumscribed cones* themselves, or cones of *tangents* τ , the connected equations:

L. . .
$$a^{2}(\nabla U \nu \tau)^{2} + a_{r}^{2} = 0$$
;
LI. . . $b^{2}(\nabla U \nu \tau)^{2} + b_{r}^{2} = 0$;
LII. . . $c^{2}(\nabla U \nu \tau)^{2} + c_{r}^{2} = 0$;

all which have the *forms* of equations of *cones of revolution*, but on the geometrical *meanings* of the three last of which it may be worth while to say a few words.

(21.) The cone L. has an *imaginary vertex*, and is always *itself* imaginary; but the *two other cones*, LI. and LII., have *each* a *real vertex* P, with $b^2 > 0$ for the first, and $c^2 < 0$ for the second; b being the mean semiaxis of the *ellipsoid*, which passes through a given point of the *focal hyperbola*, and c^2 being the negative and algebraically least square of a scalar semiaxis of the *doublesheeted hyperboloid*, which passes through a given point of the *focal ellipse*: while, *in each case*, ν has the direction of the *normal* to the *surface*, which is also the *tangent* to the *curve* at that point, and is at the same time the *axis* of revolution of the *cone*.

(22.) The semiangles of the two last cones, LI. and LII., have for their respective sines the two quotients,

LIII...
$$b_{j}: b_{j}$$
 and LIV... $(-c_{j}^{2})^{\frac{1}{2}}: (-c^{2})^{\frac{1}{2}};$

each of those two cones is therefore real, if circumscribed to a single-sheeted hyperboloid, because, for such an enveloped surface (e_i) , b_i is real, and less than the b of any confocal ellipsoid, while c_i is imaginary, and its square is algebraically greater (or nearer to zero) than the square of the imaginary semiaxis c of every double-sheeted hyperboloid, of the same confocal system; but the cone LI. is imaginary, if the enveloped surface (e_i) be either an hyperboloid of two sheets $(b_i \text{ imaginary})$, or an exterior ellipsoid $(b_i > b)$; and the other cone LII. is imaginary, if the surface (e_i) be either any ellipsoid $(c_i \text{ real})$, or else an exterior and double-sheeted hyperboloid $(a_i^2 < a_i^2, c_i^2 < c_i^2, -c_i^2 > -c_i^2)$. Accordingly it is known that the focal hyperbola, which is the locus of the vertex of the cone LI., lies entirely inside every double-sheeted hyperboloid of the system; while the focal ellipse, which is in like manner the locus of the vertex of the cone LII., is interior to every ellipsoid : and real tangents to a single-sheeted hyperboloid can be drawn, from every real point of space.

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(23.) The twelve points (whereof only four at most can be real), in which a surface (e) or (abc) is cut by the three focal curves, are called the Umbilics of that surface; the vectors, say ω , ω_{μ} , ω_{μ} , of three such umbilies, in the respective planes of ca, ab, bc, are:

LV...
$$\omega = \frac{a}{2}(a + a') + \frac{c}{2}(a - a');$$

LVI... $\omega_{\prime} = \frac{a(a + a')}{1 - Saa'} + \frac{\sqrt{-1}bVaa'}{1 - Saa'};$
LVII... $\omega_{\prime\prime} = \frac{c(a - a')}{1 + Saa'} - \frac{\sqrt{-1}bVaa'}{1 + Saa'};$

and the others can be formed from these, by changing the signs of the terms, or of some of them. The four *real* umbilies of an *ellipsoid* are given by the formula LV., and those of a *double-sheeted hyperboloid* by LVI., with the changes of sign just mentioned.

(24.) In transforming expressions of this sort, it is useful to observe that the expressions for the squares of the semiaxes,

$$a^2 = l^2(e+1), \quad b^2 = l^2(e+Saa'), \quad c^2 = l^2(e-1),$$
 407, VII.

combined with Ta = Ta' = 1, give not only $a^2 - c^2 = 2l^2$, but also,

LVIII. . . T
$$\frac{a+a'}{2} = \sqrt{\frac{1-Saa'}{2}} = \cos \frac{1}{2} \angle \frac{a'}{a} = \left(\frac{a^2-b^2}{a^2-c^2}\right)^{\frac{1}{2}};$$

LIX. . . T $\frac{a-a'}{2} = \sqrt{\frac{1+Saa'}{2}} = \sin \frac{1}{2} \angle \frac{a'}{a} = \left(\frac{b^2-c^2}{a^2-c^2}\right)^{\frac{1}{2}};$

and

LX...
$$TVaa' = \sqrt{(1 - (Saa')^2)} = \sin \angle \frac{a'}{a} = t^{-2}(a^2 - b^2)^{\frac{1}{2}}(b^2 - c^2)^{\frac{1}{2}},$$

with the verification, that because

LXI...
$$(a - a') (a + a') = 2 \nabla a a',$$

therefore

LXI'...
$$T(a - a') \cdot T(a + a') = 2'TVaa'.$$

We have also the relations,

LXII...
$$T(a + a')^{-2} + T(a - a)^{-2} = (TVaa')^{-2};$$

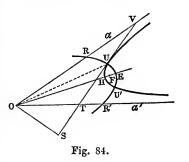
LXIII... $T(a + a')^{-2} - T(a - a')^{-2} = Saa'. ('TVaa')^{-2}:$

with others easily deduced.

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(25.) The expression LV. conducts to the following among other consequences, which all admit of elementary verifications,* and may be illustrated by the annexed fig. 84. Let u, u' be the two real points in

which an ellipsoid (abc) is cut by one branch of the focal hyperbola, with H for summit, and with F for its interior focus; the adjacent major summit of the surface being E, and R, \mathbf{x}' being (as in the figure) the adjacent points of intersection of the same surface with the focal lines a, a', that is, with the asymptotes to the hyperbola. Let also v, T be the points in which the same asymptotes a, a' meet the tangent to the hyperbola at U, or the normal



to the ellipsoid at that real umbilic, of which we may suppose that the vector ou is the ω of the formula LV.; and let s be the foot of the perpendicular on this normal to the surface, or tangent TV to the curve, let fall from the centre o. Then, besides the obvious values,

LXIV...
$$\overline{OE} = a$$
, $\overline{OF} = (a^2 - c^2)^{\frac{1}{2}}$, $\overline{OH} = (a^2 - b^2)^{\frac{1}{2}}$,

and the obvious relations, that the intercept TV is bisected at U, and that the point F is at once a summit of the focal ellipse, and a focus of that other ellipse in which the surface is cut by the plane (*ac*) of the figure, we shall have these vector expressions (comp. 371, (3.), and 407, VIII. LXI.):

LXV... ov =
$$(a + c)a$$
, or = $(a - c)a'$, rv = $a(a - a') + c(a + a')$

LXVI...
$$SU^{-1} = \phi \omega = -\frac{a}{2} (a + a') - \frac{c}{2} (a - a'), \quad SU = -ac: TU;$$

LXVII... OR =
$$\frac{a}{\sqrt{fa}} = ab^{-1}ca$$
, OR' = $\frac{a'}{\sqrt{fa'}} = ab^{-1}ca'$;

whence follow by (24.) these other values,

LXVIII...
$$\overline{ov} = a + c$$
, $\overline{oT} = a - c$, $\overline{Tv} = 2b$;
LXIX... $\overline{TU} = \overline{Uv} = b$, $\overline{sU} = \overline{oR} = \overline{oR'} = ab^{-1}c$;
LXX... $\overline{oU} = T\omega = (a^2 - b^2 + c^2)^{\frac{1}{2}}$;
LXXI... $\overline{os} = (a^2 - b^2 + c^2 - a^2b^{-2}c^2)^{\frac{1}{2}} = b^{-1}(a^2 - b^2)^{\frac{1}{2}}(b^2 - c^2)^{\frac{1}{2}}$.

2 F 2

^{*} Some such verifications were given in the *Lectures*, pages 691, 692, in connexion with fig. 102 of that former volume, which answered in several respects to the present fig. 84.

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(26.) It follows that the lengths of the sides ov, or, rv of the umbilicar triangle rov are equal to the sum and difference $(a \pm c)$ of the extreme semiaxes, and to the mean axis (2b) of the ellipsoid; while the area of that triangle $= \overline{\text{os}} \cdot \overline{\text{ru}} = (a^2 - b^2)^{\frac{1}{2}} (b^2 - c^2)^{\frac{1}{2}} =$ the rectangle under the two semiaxes of the hyperbola, if both be treated as real. The length $(T\phi\omega)^{-1}$, or $\overline{\text{su}}$, or the perpendicular from the centre o, on the tangent plane at an umbilie u, is $ab^{-1}c$; and the sphere concentric with the ellipsoid, which touches the four umbilicar tangent planes, passes through the points R, R' of intersection of that ellipsoid with the focal lines a, a', that is, as before, with the asymptotes to the hyperbola; or, by (21.) (22.), with the axes of the two circumscribed right cylinders.* And finally the length, say u, of the umbilicar semidiameter ou, is given by the formula,

LXII. . .
$$u^2 = a^2 - b^2 + c^2$$
;

all which agrees (25.) with known results.

(27.) An umbilic of a surface of the second order may be otherwise defined (comp. (23.)), as a real or imaginary point at which the tangent plane is parallel to a cyclic plane; and accordingly it is easy to prove (comp. 407, (20.)) that the umbilicar normal $\phi \omega$ in LXVI. has the direction of a cyclic normal. To employ this known property in verification of the recent expressions (25.), (26.), for the lengths of ou and su, it is only necessary to observe that the common radius of the diametral and circular sections of the ellipsoid is the mean semiaxis b (comp. 216, (7.) (9.), &c.); and that, by a slight extension of the analysis in (7.), (8.), (9.), it can be shown that if ρ, σ, τ and ρ', σ', τ' be any two systems of three conjugate semidiameters of any central surface, $f\rho = 1$, then

and

LXXIII... $\rho'^2 + \sigma'^2 + \tau'^2 = \rho^2 + \sigma^2 + \tau^2$,

LXXIV... $(S\rho'\sigma'\tau')^2 = (S\rho\sigma\tau)^2$.

* Compare 218, (5.), and 220, (4.); in which the points B, B' (comp. also fig. 53, p. 234, vol. i. [and p. 184, vol. ii.]) may now be conceived to coincide with the points R, R' of the new figure 84. It is obvious that the theory of *circumscribed cylinders* is included in that of circumscribed *cones*; so that the cylinder circumscribed to the confocal (e), with its generating lines parallel to a given (real or imaginary) semidiameter γ of that surface ($f\gamma = 1$), may be represented (comp. III. XIV.) by the equation.

III'... $f(\rho, \gamma)^2 = f\rho - 1$; or XIV'... $F \nabla \gamma \rho = a^2 b^2 c^2$;

with interpretations easily deduced, from principles already established.

ART. 408.] EIGHT UMBILICAR GENERATRICES.

(28.) A less elementary verification of the value LXXII. of u^2 , but one which is useful for other purposes, may be obtained from either the cubic in b^2 , or that in e, assigned in 407, (8.). For if b_0^2 , b_1^2 , b_2^2 be the roots of the former cubic, and e_0 , e_1 , e_2 the roots of the latter, inspection of those equations shows at once that we have generally,

LXXV... $-\rho^2 = b_0^2 + b_1^2 + b_2^2 - 2l^2 Saa' = l^2(e_0 + e_1 + e_2 + Saa');$

or

LXXVI...
$$\overline{OP}^2 = T\rho^2 = a_0^2 + b_1^2 + c_2^2 = b_0^2 + c_1^2 + a_2^2 = \&o.,$$

where the semiaxes a_0 , b_1 , c_2 belong to the three confocals through any proposed point P. Making then,

LXXVII...
$$a_0^2 = a^2$$
, $b_1^2 = 0$, $c_2^2 = c^2 - b^2$,

we recover the expression assigned above, for the square of the length u of an *umbilicar semidiameter* of an *ellipsoid*.

(29.) For any central surface, the principle (27.) shows that if λ , μ be, as in 405, (5.), &c., the *two real cyclic normals*, and if g be the *real scalar* associated with them as before, then the vectors of the *four real umbilics* (if such exist) must admit of being thus expressed:

LXXVIII...
$$\pm \phi^{-1}\lambda$$
: $\sqrt{F\lambda} = \pm abc (gU\lambda + \mu T\lambda)$;

LXXIX...
$$\pm \phi^{-1}\mu : \sqrt{F\mu} = \pm abc \left(gU\mu + \lambda T\mu\right);$$

and thus we see anew, that an hyperboloid with one sheet has (as is well known) no real umbilic, because for that surface the product abc of the semiaxes is imaginary; or because it has no real tangent planc parallel to either of its two real planes of circular section.

(30.) Of whatever species the surface may be, the three umbilicar rectors (23.), of which only one at most can be real, with the particular signs there given, but which have the forms of lines in the three principal planes, must be conceived, in virtue of their expressions LV. LVI. LVII., to terminate on an imaginary right line, of which the vector equation is,

LXXX...
$$\rho = \frac{-a(e'+1)}{a+a'} - \sqrt{-1} \frac{b(e'+Saa')}{Vaa'} + \frac{c(e'-1)}{a-a'};$$

e' being a scalar variable, which receives the three values, -Saa', +1, and -1, when ρ comes to coincide with ω , $\omega_{,}$, and $\omega_{,}$ respectively. And such an imaginary right line, which is easily proved to satisfy, for all values of the

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variable e', both the rectangular and the bifocal forms of the equation of the surface (e), or to be (in an imaginary sense) wholly contained upon that surface, may be called an Umbilicar Generatrix.

(31.) There are in general eight such generatrices of any central surface of the second order, whereof each connects three umbilics, in the three principal planes, two passing through each of the twelve umbilicar points (23.); and because e'^2 disappears from the square of the expression LXXX. for ρ , which square reduces itself to the following,

LXXXI...
$$\rho^2 = -l^2(2e' + e + Saa') = -b^2 - 2l^2e'$$
,

they may be said to be the eight generating lines through the four imaginary points, in which the surface meets the circle at infinity.

(32.) In general, from the cubics in e and in b^2 , or from either of them, it may be without difficulty inferred (comp. (28.)), that the *eight intersections* (real or imaginary) of *any three confocals* (e_0) (e_1) (e_2) have their vectors ρ represented by the formula:

LXXXII...
$$\rho = \frac{\pm a_0 a_1 a_2}{l^2 (a + a')} \pm \frac{\sqrt{-1} b_0 b_1 b_2}{l^2 V a a'} \pm \frac{c_0 c_1 c_2}{l^2 (a - a')};$$

comparing which with the vector expression LXXX., we see that the three confocals, through the point determined by that former expression, for any given value of e', are (e), (e'), and (e') again; and therefore that two of the *three* confocal surfaces through any point of an umbilicar generatrix (30.) coincide: a result which gives in a new way (comp. LXXV.) the expression LXXXI. for ρ^2 .

(33.) The *locus* of all *such* generatrices, for *all* the confocals (e) of the system, is a certain *ruled surface*, of which the doubly variable *vector* may be thus expressed, as a function of the *two* scalar variables, e and e':

LXXXIII. . .
$$\rho_{e,e'} = \frac{\pm l(e+1)^{\frac{1}{2}}(e'+1)}{a+a'} \pm \frac{\sqrt{-1}l(e+Saa')^{\frac{1}{2}}(e'+Saa')}{Vaa'} \pm \frac{l(e-1)^{\frac{1}{2}}(e'-1)}{a-a'};$$

and because we have thus, for any one set of signs, the differential relation,

LXXXIV...
$$D_e \rho_{e,e} = \frac{3}{2} D_{e'}, \rho_{e,e'}, \epsilon'$$

it follows that this ruled locus is a Developable Surface : its edge of regression

ART. 408.] DEVELOPABLE LOCUS AND ENVELOPE.

being that wholly *imaginary curve*, of which the *rector* is ρ_{e} , e_{e} , and which is therefore by (32.) the *locus* of all the *imaginary points*, through each of which pass three coincident confocals.

(34.) The only real part of this imaginary developable consists of the two real focal curves, which are double lines upon it, as are also the imaginary focal, and the circle at infinity (31.); and the scalar equation of the same imaginary surface, obtained by elimination of the two arbitrary scalars e and e', is found to be of the eighth degree, namely the following:

LXXXV...
$$\begin{cases} 0 = \sum m^2 x^8 + 2\sum m(m-n)x^6y^2 + \sum (p^2 - 6mn)x^4y^4 \\ + 2\sum (3m^2 - np)x^4y^2z^2 + 2\sum m^2(n-p)x^6 + 2\sum m(mp - 3n^2)x^4y^2 \\ + 2(m-n)(n-p)(p-m)x^2y^2z^2 + \sum m^2(m^2 - 6np)x^4 \\ + 2\sum mn(mn - 3p^2)x^2y^2 + 2\sum m^2np(p-n)x^2 + m^2n^2p^2; \end{cases}$$

in which we have written, for abridgment,

LXXXVI... $x = -S\rho U(a + a'), \quad y = -S\rho UVaa', \quad z = -S\rho U(a - a'),$ and so that LXXXVII... $m = b^2 - c^2, \quad n = c^2 - a^2, \quad p = a^2 - b^2,$ LXXXVIII... m + n + p = 0;

while each sign Σ indicates a sum of three or of six terms, obtained by cyclical or binary^{*} interchanges.

(35.) From the manner in which the equation of this *imaginary surface* (33.) or (34.) has been deduced, we easily see by (32.) that it has the double property: I.st of being (comp. (20.)) the *locus* of the *vertices* of all the (real or imaginary) *right cones*, which can be *circumscribed* to the *confocals* of the system; and II.nd of being at the same time the *common envelope* of all those confocals: which *envelope* accordingly is known to be a *developable*† *surface*.

^{*} When xyz and *abe* are *cyclically* changed to yzx and *bca*, then *mnp* are similarly changed to *npm*; but when, for instance, retaining x and a unchanged, we make only *binary interchanges* of y, z, and of b, c, we then change m, n, and p, to -m, -p, and -n respectively.

⁺ This theorem is given, for instance, in page 157 [Art. 221] of the several times already cited Treatise by Dr. Salmon, who also mentions the *double lines* &c. upon the surface; but the present writer does not yet know whether the theory above given, of the *eight umbilicar generatrices*, has been anticipated: the *locus* (33.) of which *imaginary right lines* (30.) is *here* represented by the *vector equation* LXXXIII., from which the *scalar equation* LXXXV. has been above deduced (34.), and onght to be found to agree (notation excepted) with the known coordinate equation of the *developable envelope* (35.) of a *confocal system*.

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(36.) The eight imaginary lines (31.) will come to be mentioned again, in connexion with the lines of curvature of a surface of the second order^{*}; and before closing the present series of sub-articles, it may be remarked that the equation in (15.), for the determination of the second confocal (e_i) which touches a given tangent, $d\rho$ or PP', to a given surface (e) of the same system, will soon appear under a new form, in connexion with that theory of geodetic lines, on surfaces of the second order, to which we next proceed.[†]

If in this equation we replace λ by $x\lambda$ where x is a variable scalar, we see at once that the locus of points of contact of a system of parallel planes is a rectangular hyperboloid, and if we replace λ by $(\lambda + x\lambda')(1 + x)^{-1}$, we find the locus of the points of contact of planes through a given line to be a twisted cubic. In this case also the locus of poles of the planes is a hyperbolic paraboloid $\rho = -(\Phi + u)(\lambda + x\lambda')(1 + x)^{-1}$, since the form of the equation shows that it is the locus of lines dividing the line loci for any two of the planes in the same ratio.

If u_1 , u_2 , and u_3 are the parameters of the three confocals which pass through the extremity of a given vector a, and v_1 , v_2 , and v_3 the corresponding vectors of proximity, $-a = (\Phi + u_1)v_1 = (\Phi + u_1)v_2 = (\Phi + u_3)v_3$, and $Sav_1 = Sav_2 = Sav_3 = 1$. Combining the three expressions for a, we deduce $u_1Sv_2v_1 + Sv_2\Phi v_1 = Sr_1\Phi v_2 + u_2Sv_1v_2$, so $Sr_1v_2 = 0$, since u_1 is not equal to u_2 , or the surfaces cut at right angles. Again $(\Phi + u_1)(v_1 - v_2) = (u_2 - u_1)v_2$, and on inversion $v_1 - v_2 = (u_2 - u_1)(\Phi + u_1)^{-1}v_2$. Operating on this by Sv_3 , we see that v_2 and v_3 as well as being at right angles are conjugate with respect to the quadric u_1 , and therefore parallel to the principal axes of the section of that quadric made by $S\rho v_1 = 0$; operating by Sv_2^{-1} , we find $-1 = -(u_1 - u_2)Sv_2^{-1}(\Phi + u_1)^{-1}v_2 = (u_1 - u_3)^{\frac{1}{2}}$, respectively.

Introducing a new linear vector function analogous to that of 407, (7.), and defined by the equation $\Theta \rho = \Phi \rho + \alpha S \alpha \rho$, we see on referring to the relations between α , ν_1 , ν_2 , and ν_3 that

$(\Theta + u_1)\nu_1 = (\Theta + u_2)\nu_2 = (\Theta + u_3)\nu_3 = 0,$

so the vectors of proximity at α are the solutions of this new function and the parameters of the surfaces are the corresponding roots. This again proves the surfaces cut at right angles, for Θ is self-conjugate, and its solutions are consequently mutually rectangular.

If $S\lambda\rho = 1$ is any plane through the extremity of α , the equation $\varpi = -(\Phi + u)\lambda$ which determines its pole with respect to the quadric u, may be replaced by $\varpi - \alpha = -(\Theta + u)\lambda$, because $S\lambda\alpha = 1$. If the pole is in the plane, $\varpi - \alpha$ is at right angles to λ , and we determine at once the parameter of the touched quadric u and the point of contact by operating on λ by $-\Theta$, and then resolving the vector obtained in and normal to the given plane. Setting off from α the component in the plane we get the point of contact, while the parameter of the quadric is the ratio which the component normal to the plane bears to the vector λ .

In this case also we have $S(\varpi - \alpha) (\Theta + u)^{-1} (\varpi - \alpha) = 0$ for the equation of the tangent cone from the point α to the surface u, and the form of the equation shows that the tangent cones are confocal, so that the quadrics appear to cut at right angles as well as actually doing so. Also the

^{* [}Compare the sub-articles to 410, page 235.]

^{† [}Although repetition is unavoidable, it seems well to supplement Arts. 407 and 408 by a few examples on the use of the general equation of confocals $S\rho(\Phi + u)^{-1}\rho = -1$, in which $-(\Phi + u)$ replaces the ϕ^{-1} of 407, XV., so that $u - b^2$ is constant. The vector ϖ to the pole of the plane $S\lambda\rho = 1$, with respect to the quadric u is given by $(\Phi + u)^{-1}\varpi = -\lambda$ or $\varpi = -(\Phi + u)\lambda$. The locus of poles of the plane is thus a right line normal to the plane, and the distance between any pair of poles is $T(\varpi - \varpi') = (u' - u)T\lambda = (b'^2 - b^2)p^{-1}$, p being the central perpendicular on the plane, and b and b' the mean semiaxes of the quadrics. The plane touches one quadric of the system whose parameter u_0 is given by $S\lambda(\Phi + u_0)\lambda = -1$, this being the condition that the corresponding pole should lie in the plane. The vector to the point of contact is $\varpi = -\lambda^{-1}(S + V)$ ($\Phi + u_0\lambda$), or, by the condition, $\varpi = \lambda^{-1} - \lambda^{-1} V\lambda\Phi\lambda$.

ARTS. 408, 409.] GEODETICS ON CENTRAL SURFACES.

409. A general theory of *geodetic lines*, as treated by quaternions, was given in the Fifth Section (III. iii. 5) of the present Chapter; and was illustrated by applications to several different *families of surfaces*. We can only here spare room for applying the same theory to the deduction, in a new way, of a few known but *principal properties* of geodetics on *central surfaces of the second order*; the differential

common principal axes of the system are along the normals at a for these are the solutions of $\nabla_{\mu}\Theta_{\nu} = 0$. Replacing $\varpi - a$ by a given vector τ , we have $S\tau(\Theta + u)^{-1}\tau = 0$ to determine the two quadries which the line touches. If λ and λ' are the vectors of proximity to the points of contact as before, we have the vectors from a to the points of contact given by $\tau = -(\Theta + u)\lambda$, and $\tau' = -(\Theta + u')\lambda'$, u and u' being roots of the quadratics, and τ being parallel to τ' . But λ and λ' are normal to the corresponding cones, hence we see $S\lambda\Theta\lambda' = 0$ as well as $S\lambda\lambda' = 0$. We may also write $\tau = -\lambda^{-1}\nabla\lambda\Theta\lambda$, and this, coupled with the condition $S\lambda\alpha = 1$, determines the locus of the points of contact, λ being supposed to vary consistently with the condition.

Another method of treatment is often useful. Any quadric may be derived from a sphere by operating on its vector radii by a self-conjugate linear vector function which is however real only when the quadric is an ellipsoid (Tait's *Quaternions*, Third Edition, page 207.)

It is obvious that if we can determine a self-conjugate linear vector function θ so that $\theta^2 = \phi$, we may write $S\rho\phi\rho = -1$ in the form $(\theta\rho)^2 = -1$ or $\theta\rho = \eta$, where $T\eta = 1$. Even in the more general case when ϕ is not self-conjugate but expressible in the form $\phi\rho = (a\alpha S\beta\gamma\rho + b\beta S\gamma\alpha\rho + c\gamma S\alpha\beta\rho)$ $(Sa\beta\gamma)^{-1}$, any one of the eight functions given by $\theta\rho = (\pm \sqrt{a\alpha}S\beta\gamma\rho \pm \sqrt{b\beta}S\gamma\alpha\rho \pm \sqrt{c\gamma}S\alpha\beta\rho)$ $(Sa\beta\gamma)^{-1}$, satisfies the condition $\theta^2 = \phi$. It is evident that all functions of this type or of the type $(\phi + u)^{\frac{1}{2}}$ are commutative in order of operation. More generally it can be shown that two functions are commutative in order of operation. More generally it can be shown that two functions are commutative in order of operation when and only when their vector solutions are parallel, a condition obviously true for the functions to be considered. We may consequently use the vector equation $\rho = (\phi + u)^{\frac{1}{2}}\eta$, where $T\eta = 1$ as the equation of a confocal system, for $\eta^2 = ((\phi + u)^{-\frac{1}{2}}\rho)^2$ $= S\rho(\Phi + u)^{-1}\rho = -1$. Points on two confocals derived from the same point on a unit sphere are called corresponding points, and it is easy to show in this notation if \mathbf{F} and \mathbf{q} on one confocal correspond respectively to \mathbf{F}' and \mathbf{q}' on another that $\overline{\mathbf{Fq}'} = \overline{\mathbf{qp}'}$.

Now three confocals pass through a given point. We have thus three different expressions for a vector $\rho = (\Phi + u_1)^{\frac{1}{2}}\eta_1 = (\Phi + u_2)^{\frac{1}{2}}\eta_2 = (\Phi + u_3)^{\frac{1}{2}}\eta_3$, $\eta_1\eta_2\eta_3$ being certain unit vectors, and u_1 , u_2 , and u_3 being the parameters of the confocals through ρ . The form of these equations suggests the new expression

$$\rho = \left[\left(\Phi + u_1 \right) \left(\Phi + u_2 \right) \left(\Phi + u_3 \right) \right]^2 \epsilon,$$

and substituting this for ρ in $S_{\rho}(\Phi + u_1)^{-1}\rho = -1$, the result is $S_{\epsilon}(\Phi + u_2)(\Phi + u_3)\epsilon = -1$. This must be satisfied for all values of u_2 and u_3 , so we see ϵ is one of eight imaginary vectors constant for the whole system, and satisfying $\epsilon^2 = 0$, $S_{\epsilon}\Phi\epsilon = 0$, and $S_{\epsilon}\Phi^2\epsilon = -1$. For a value of ϵ satisfying these equations, and for suitable choice of the three parameters ρ may be made the vector to any point in space; if one parameter is given ρ describes the corresponding quadric, and if two of the parameters are assigned, ρ describes the curve of intersection of the quadrics determined by them.

This notation is suitable for investigating the properties of the umbilical generators. When $u_3 = u_2$, we have $\rho = (\Phi + u_2) (\Phi + u_1)^{\frac{1}{2}} \epsilon$ which represents a right line of a simply infinite system when u_1 is given and u_2 variable. If for the moment $\tau = (\Phi + u_1)^{\frac{1}{2}} \epsilon$, we deduce from the properties of ϵ , $\tau^2 = S_{\tau}(\Phi + u_1)^{-1}\tau = 0$, and $S_{\tau}\Phi\tau = -1$, and from these it appears that the line is a generator of the quadric passing through one of the points in which the asymptotic cone intersects the circle at infinity (408, (30.)). Again (33.) if $t = \frac{2}{3}(u_2 - u_1)$ the equation of one of these lines becomes $\rho = \left(1 + t \frac{d}{du_1}\right) (\Phi + u_1)^{\frac{3}{2}} \epsilon$, showing that they belong to a developable whose cuspidal edge is $\rho = (\Phi + u)^{\frac{3}{2}} \epsilon$, the locus of points through each of which pass three coincident confocals.]

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equation employed being one of those formerly used, namely (comp. 380, IV.),

I...,
$$\nabla \nu d^2 \rho = 0$$
, if II..., $T d \rho = \text{const.}$;

that is, if the arc of the geodetic be made the independent variable.

(1.) In general, for any surface, of which ν is a normal vector, so that the first differential equation of the surface is $S\nu d\rho = 0$, the second differential equation $dS\nu d\rho = 0$ gives, by I., for a geodetic on that surface, the expression,

III. . .
$$d^2\rho = -\nu^{-1}Sd\nu d\rho$$
.

(2.) Again, the surface $f\rho = \text{const.}$ being still quite general, if we write (comp. 363, X'., 373, III., &c.),

IV... $df\rho = 2S\nu d\rho = 2S\phi\rho d\rho$, we shall have V... $dfd\rho = 2S(\phi d\rho \cdot d^2\rho)$; and therefore, by III., for a *geodetic*,

VI. .
$$\frac{\mathrm{d}f\mathrm{d}\rho}{\mathrm{Sd}\rho\mathrm{d}\phi\rho} + 2\mathrm{S}\frac{\phi\mathrm{d}\rho}{\phi\rho} = 0.$$

(3.) For a central surface of the second order, $\phi \rho$ is a linear function, and we may write (comp. 361, IV.),

VII...
$$\phi d\rho = d\phi \rho = d\nu$$
, $Sd\rho d\phi \rho = Sd\rho \phi d\rho = fd\rho$;

the general differential equation VI. becomes therefore here,

VIII. . .
$$\frac{\mathrm{d} f \mathrm{d} \rho}{f \mathrm{d} \rho} + 2\mathrm{S} \frac{\mathrm{d} \nu}{\nu} = 0;$$

and gives, by a first integration, with the condition II.,

IX...
$$\nu^2 f d\rho = h d\rho^2$$
, or IX'... $T\nu^2 f U d\rho = h = \text{const.}$;

 \mathbf{or}

X...
$$P^{-2}D^{-2} = h$$
, or X'... $P \cdot D = h^{-\frac{1}{2}} = \text{const.}$;

 $P = T\nu^{-1} = perpendicular$ from centre on tangent plane,

where and

$$D = (f \operatorname{Ud}_{0})^{-\frac{1}{2}} = semidiameter parallel to tangent:$$

these two last quantities being treated as scalars, whereof the latter may be real or imaginary,* together with the last scalar constant $h^{-\frac{1}{2}}$.

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^{*} For the case of the *ellipsoid*, for which the product P. D is necessarily *real*, the foregoing deduction, by quaternions, of Joachimstal's celebrated first integral, P. D = const., was given (in substance) in page 580 of the Lectures.

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(4.) The following is a quite different way of accomplishing a first integration, which conducts to another known result of not less interest, although rather of a *graphic* than of a *metric* kind. Operating on the equation 407, XVI. by S. d ρ , and remembering that $S\rho\nu = 1$, and $S\nu d\rho = 0$, we obtain the differential equation,

XI...
$$S\rho\nu S\rho d\rho = l^2 (Sa'\nu Sad\rho + Sa\nu Sa' d\rho);$$

that is, by I. and II.,

XII...
$$S\rho d\rho \cdot S\rho d^2\rho - \rho^2 Sd\rho d^2\rho = l^2 d(Sad\rho \cdot Sa'd\rho),$$

in which the first member, like the second, is an exact differential, because

XIII...
$$S(\nabla \rho d\rho \cdot \nabla \rho d^2 \rho) = \frac{1}{2} d(\nabla \rho d\rho)^2;$$

hence, for the geodetic,

or

$$\begin{split} & \text{XIV.} \dots \ell^2 (\nabla \rho d\rho)^2 - 2 \text{Sad}\rho \text{Sa'} d\rho = \hbar' d\rho^2, \\ & \text{XV.} \dots 2 \text{Sa} \text{Ud}\rho \dots \text{Sa'} \text{Ud}\rho - \ell^{-2} (\nabla \rho \text{Ud}\rho)^2 = \hbar', \end{split}$$

h' being a new scalar constant.

(5.) Comparing this last equation with the formula 408, XXXVI., we find that the new constant h' is the sum, $e + e_i$, of what have been above called the *parameters*,* of the given surface (e) on which the geodetic is traced, and of the confocal (e_i) which touches a given tangent to that curve: whence follows the known[†] theorem, that the tangents to a geodetic, on any central surface of the second order, all touch one common confocal.[‡]

(6.) The new constant $e_i(=h'-e)$ may, by 407, LXXV. and 408, LXXV. (with e for e_0), be thus transformed :

XVI. . .
$$e_{\prime} = e_1 (\mathrm{TVU}\nu_1 \mathrm{d}\rho)^2 + e_2 (\mathrm{TVU}\nu_2 \mathrm{d}\rho)^2$$

= $e_1 (\mathrm{SU}\nu_2 \mathrm{d}\rho)^2 + e_2 (\mathrm{SU}\nu_1 \mathrm{d}\rho)^2 = \mathrm{const.};$

where e_1 , e_2 are the parameters of the two confocals through the point P of the geodetic on (e), and ν_1 , ν_2 are as before the normals at that point, to those two surfaces (e_1) , (e_2) .

^{*} Compare the second Note to page 214.

⁺ Discovered by M. Chasles.

 $[\]ddagger$ This touched confocal becomes a *sphere*, when the given confocal is a *cone*. Compare 380, (5.), and 408, (16.), (17.); also the Note to page 31.

(7.) In fact, the two equations last cited give the general transformation,

XVII. . .
$$l^{-2}(\nabla\rho\sigma)^2 - 2\mathrm{Sa}\sigma\mathrm{Sa}'\sigma = e(\nabla\sigma\mathrm{U}\nu)^2 + e_1(\nabla\sigma\mathrm{U}\nu_1)^2 + e_2(\nabla\sigma\mathrm{U}\nu_2)^2$$
;

 σ being an *arbitrary* vector, which may for instance be replaced by $d\rho$. Equating then this last expression to $(e + e_i)\sigma^2$, or to $e(\nabla\sigma U\nu)^2 - e_iT\sigma^2$, since $S_{\nu\sigma} = 0$, we obtain the first and therefore also the second transformation XVI., because the three normals $\nu\nu_1\nu_2$ compose a rectangular system (comp. 407, (4.), &c.).

(8.) It is, however, simpler to deduce the second expression XVI. from the equation 408, XXXI. of the cone of tangents from P to (e_{r}) , by changing τ to Ud ρ ; and then if we write

XVIII. . .
$$v_1 = \angle \frac{\mathrm{d}\rho}{\nu_1}$$
,

so that v_1 denotes the angle at which the geodetic crosses the normal v_1 to (e_1) , considered as a tangent to the given surface (e), the first integral XVI. takes the form,*

XIX... $e_1 = e_1 \sin^2 v_1 + e_2 \cos^2 v_1$,

or

XX... $a_1^2 = a_1^2 \sin^2 v_1 + a_2^2 \cos^2 v_1$, &c.;

in which the constant a_{i} is the primary semiaxis of the touched confocal (5.).

(9.) Without supposing that $\mathrm{Td}\rho$ is constant, we may investigate as follows the differential of the real scalar h in IX. or X., or of the product P^{-2} . D^{-2} , for any curve on a central surface of the second order. Leaving at first the surface arbitrary, as in (1.) and (2.), and resolving $\mathrm{d}^2\rho$ in the three rectangular directions of ν , $d\rho$, and $\nu d\rho$, we get the general expression,

XXI...
$$d^2\rho = -\nu^{-1}Sd\nu d\rho + d\rho^{-1}Sd\rho d^2\rho + (\nu d\rho)^{-1}S\nu d\rho d^2\rho$$
;

of which, under the conditions I. and II., the two last terms vanish, as in III. Without assuming those conditions, if we now introduce the relations

* Under this form XX., the integral is easily seen to coincide with that of M. Liouville,

$$\mu^2 \cos^2 i + \nu^2 \sin^2 i = \mu'^2 = \text{const.},$$

cited in page 290 of Dr. Salmon's Treatise.

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VII. which belong to a central surface of the second order, we have by V. and IX. the expression,*

XXII. . .
$$\frac{1}{2}$$
dh . d $\rho^2 = \nu^2$ Sd ν d $^2\rho$ + S ν d ν Sd ν d ρ
- h Sd ρ d $^2\rho$ = S ν d ν d ρ^{-1} . S ν d ρ d $^2\rho$

or

XXIII... $dh = d \cdot \nu^2 S d\nu d\rho^{-1} = d \cdot P^{-2} D^{-2} = 2S \nu d\nu d\rho^{-1} S \nu d\rho^{-1} d^2 \rho$;

or finally,

XXIV... $dh \cdot d\rho^4 = 2S\nu d\nu d\rho \cdot S\nu d\rho d^2\rho$,

the scalar variable with respect to which the differentiations are performed being here entirely arbitrary.

(10.) For a geodetic line on any surface, referred thus to any scalar variable, we have by 380, II. the differential equation,

XXV... $S\nu d\rho d^2\rho = 0$;

and therefore by XXIV., for such a line on a central surface of the second order, we have again, as in (3.),

XXVI... dh = 0, or XXVI'... h = const.,

with $h = P^{-2}D^{-2}$ as in X.

(11.) But we now see, by XXIV., that for such a surface the condition XXVI. is satisfied, not only by this *differential equation* of the second order XXV. but also by this other differential equation,

$$XXVII...S\nu d\nu d\rho = 0;$$

the product $P^{-2}D^{-2}$ (or PD itself) is therefore constant, not only as in (3.) for every geodetic on the surface, but also for every curve of another set, \dagger represented by this last equation XXVII., which is only of the first order, and the geometrical meaning of which we next propose to consider.

* In deducing this expression, it is to be remembered that

 $\mathrm{dSd}\nu\mathrm{d}\rho = \mathrm{d}f\mathrm{d}\rho = 2\mathrm{Sd}\nu\mathrm{d}^2\rho ;$

in fact, the linear and self-conjugate form of $\nu = \phi \rho$ gives,

 $\mathrm{Sd}\rho\mathrm{d}^2\nu = f(\mathrm{d}\rho, \,\mathrm{d}^2\rho) = \mathrm{Sd}\nu\mathrm{d}^2\rho.$

[The second part of the transformation in XXII. may be effected by replacing $d^2\rho$ in the term $\nu^2 S d\nu d^2\rho$ by the value given in XXI.]

+ Namely, the lines of curvature, as is known, and as will presently be proved by quaternions.

ELEMENTS OF QUATERNIONS. [III. III. § 7.

410. In general, if ν and $\nu + \Delta \nu$ have the directions of the normals to any surface, at the extremities of the vectors ρ and $\rho + \Delta \rho$, the condition of intersection (or parallelism) of these two normals is, rigorously,

I. . .
$$S\nu\Delta\nu\Delta\rho = 0$$
;

the differential equation* of what are called the Lines of Curvature, on an arbitrary surface, is therefore (comp. 409, XXVII.),

II...
$$S\nu d\nu d\rho = 0$$
;

from which we are now to deduce a few general consequences, together with some that are peculiar to surfaces of the second order.

(1.) The differential equation of the surface being, as usual,

III...
$$S\nu d\rho = 0$$
,

the normal vector ν is generally some function of ρ , although not generally linear, because the surface is as yet arbitrary: its differential $d\nu$ is therefore generally some function of ρ and $d\rho$, which is linear relatively to the latter. And if, attending only to the dependence of $d\nu$ on $d\rho$, we write

IV...
$$d\nu = \phi d\rho$$
,

it results from what has been already proved (363), that this linear and vector function ϕ is at the same time self-conjugate.

(2.) Denoting then by τ a tangent \dagger PT to a line of curvature, drawn at the given extremity P of ρ , we see that the vector τ must satisfy the two following scalar equations, in which ν is supposed to be given,

V... $S_{\nu\tau} = 0$, and VI... $S_{\nu\tau\phi\tau} = 0$;

this tangent τ admits therefore (355) of two real and rectangular directions, but not in general of more: opposite directions being not here counted as

+ This symbol τ is used here partly for abridgment, and partly that the reader may not be *obliged* to interpret $d\rho$ as denoting a *finite tangent*, although the principles of this work *allow* him so to interpret it.

^{*} In this equation II., $d\rho$ and $d\nu$ are two simultaneous differentials, which may (according to the theory of the present Chapter, and of the one preceding it) be at pleasure regarded, either as two finite right lines, whereof $d\rho$ is (rigorously) tangential to the surface, and to the line of curvature; or else as two infinitely small vectors, $d\rho$ being, on this latter plan, an infinitesimal chord $\Delta\rho$. (Compare pages 97, 431, vol. i., and pages 4, 174, and the Notes to pages 170, 179, vol. ii.) The treatment of the equations is the same, in these two views, whereof one may appear clearer to some readers, and the other view to others.

ART. 410.]

LINES OF CURVATURE.

distinct. Hence, as is indeed well known, through each point of any surface there pass generally two lines of curvature : and these two curves intersect each other at right angles.

(3.) A construction for the two rectangular directions of τ can easily be assigned as follows. Assuming, as we may, that the *length* of the tangent τ varies with its *direction*, according to the law,

which gives

or briefly

VII... $S\tau\phi\tau = 1$, VIII... $S(\phi\tau \cdot d\tau) = 0$, VIII'... $S\phi\tau d\tau = 0$,

by the properties above-mentioned of ϕ ; and remembering that ν is treated as a constant in V., so that we may write,

IX... $S_{\nu}d\tau = 0$, and therefore (by VI.), X... $S_{\tau}d\tau = 0$;*

we see that, under the condition of the question, the above-mentioned *length* $T\tau$, of this tangential vector τ , is a *maximum* or *minimum*: and therefore that the *two directions* sought are those of the *two axes* of the *plane conic* V. VII., which has its *centre at the given point* P of the surface, and is *in the tangent plane* at that point.

(4.) This plane conic V. VII. may be called the *Index Curve*, for the given surface at the given point P; in fact it is easily proved to coincide, if we abstract from mere dimensions, with the known *indicatrix* (la courbe indicatrice) of Dupin,[†] who first pointed out the coincidence (3.) of the directions of its *axes*, with those of the lines of curvature; and also established a more general relation of *conjugation* between *two tangents* to a surface at one point, which exists when they have the directions of any two *conjugate semidiameters* of that curve: so that the lines of curvature are distinguished by this *characteristic property*, that the *tangent to each* is *perpendicular to its conjugate*.

(5.) In our notations, this relation of conjugation between two tangents τ , τ' , which satisfy as such the equations,

$$\mathbf{V}...\mathbf{S}_{\nu\tau} = 0$$
, and $\mathbf{V}'...\mathbf{S}_{\nu\tau'} = 0$,

* [Since $d\tau \parallel V\phi\tau\nu$ by VIII. and IX.]

† Développements de Géométrie (Paris, 1813), pages 48, 145, &c.

[III. III. § 7.

is expressed by the formula,

XI... $S\tau\phi\tau'=0$, or XI'... $S\tau'\phi\tau=0$;

we have therefore the parallelisms,*

XII...
$$\tau \parallel \nabla \nu \phi \tau'$$
, XII'... $\tau' \parallel \nabla \nu \phi \tau$;

so that the equation ∇I . may be written under the very simple form,

XIII...
$$S\tau\tau' = 0$$
,

which gives at once the *rectangularity* lately mentioned.

(6.) The parallelism XII'. may be otherwise expressed by saying (comp. (4.)) that

have the directions of *conjugate tangents*; or that the two vectors,

XV...
$$\Delta \rho$$
 and $\nabla \nu \Delta \nu$,

have ultimately such directions, when $T\Delta\rho$ diminishes indefinitely. But whatever may be this length of the chord $\Delta\rho$, the vector $\nabla\nu\Delta\nu$ has the direction of the line of intersection of the two tangent planes to the surface, drawn at its two extremities : another theorem of Dupin⁺ is therefore reproduced, namely, that if a developable be circumscribed to any surface, along any proposed curve thereon, the generating lines of this developable are everywhere conjugate, as tangents to the surface, to the corresponding tangents to the curve, with the recent definition (4.) of such conjugation.

* The conjugate character of these two parallelisms, or the relation,

 $\mathbf{V}. \boldsymbol{\nu} \boldsymbol{\phi} \mathbf{V} \boldsymbol{\nu} \boldsymbol{\phi} \boldsymbol{\tau} \parallel \boldsymbol{\tau}, \quad \text{if} \quad \mathbf{S} \boldsymbol{\nu} \boldsymbol{\tau} = \mathbf{0},$

may easily be deduced from the *self-conjugate* property of ϕ , with the help of the formula 348, VII., in page 490, vol. i. [The equation cited becomes for present purposes $\phi V \nu \phi \tau = V \psi \tau$.]

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⁺ Dupin proved first (Dév. de Géométrie, pp. 43, 44, &c.), that two such tangents as are described in the text have a relation of *reciprocity* to each other, on which account he called them "tangentes conjuguées": and afterwards he gave a sort of *image*, or construction, of this relation and of others onnected with it, by means of the curve which he named "l'indicatrice" (in his already cited page 48, &c.).

ART. 410.] INDEX CURVE AND SURFACE, CONJUGATE TANGENTS. 233

(7.) The following is a very simple mode of proving by quaternions, that if a tangent r satisfies the equation VI., then the rectangular tangent,

XVI...
$$\tau' = \nu \tau$$
,

satisfies the same equation. For this purpose we have only to observe, that the self-conjugate property of ϕ gives, by VI. and XVI.,

XVII...
$$0 = S\tau'\phi\tau = S\tau\phi\tau' = \nu^{-2}S\nu\tau'\phi\tau'.$$

(8.) Another way of exhibiting, by quaternions, the mutual rectangularity of the lines of curvature, is by employing (comp. 357, I.) the self-conjugate form,

XVIII...
$$\phi \tau = g \tau + V \lambda \tau \mu$$
;

in which the vectors λ , μ , and the scalar g, depend only on the surface and the point, and are independent of the direction of the tangent. The equation **VI**. then becomes by **V**.,

XIX...
$$0 = S_{\nu\tau}\lambda\tau\mu = S_{\nu\tau}\lambda S_{\mu\tau} + S_{\nu\tau\mu}S_{\lambda\tau};$$

assuming then the expression,

we easily find that

XX...
$$\tau = x \nabla v \lambda + y \nabla v \mu$$
,
XXI... $y^2 (\nabla v \mu)^2 = x^2 (\nabla v \lambda)^2$,

XXI'... $yT\nabla \nu \mu = \pm xT\nabla \nu \lambda$;

or

.

the two directions of τ are therefore those of the two lines,

XXII. . . $U\nabla\nu\lambda \pm U\nabla\nu\mu$,

which are evidently perpendicular* to each other.

(9.) An interpretation, of some interest, may be given to this last expression XXII., by the introduction of a certain auxiliary surface of the second order, which may be called the *Index Surface*, because the *index curve* (4.) is the diametral section of this new surface, made by the tangent plane to the given one. With the recent signification of ϕ , this *index surface* is represented by the equation VII., if τ be now supposed (comp. (2.)) to

^{*} This mode, however, of determining generally the directions of the lines of curvature, gives only an illusory result, when the normal ν has the direction of either λ or μ , which happens at an *umbilic* of the surface. Compare 408, (27.), (29.), and the first Note to page 525, vol. i.

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represent a line PT drawn in any direction from the given point P, and therefore not now obliged to satisfy the condition V. of tangency. Or if, for greater clearness, we denote by $\rho + \rho'$ the vector from the origin o to a point of the index surface, the equation to be satisfied is, by the form XVIII. of ϕ (comp. 357, II.),

XXIII... $l = S\rho'\phi\rho' = g\rho'^2 + S\lambda\rho'\mu\rho';$

the centre of this auxiliary surface being thus at ν , and its two (real) cyclic normals being the lines λ and μ : so that $\nabla \nu \lambda$ and $\nabla \nu \mu$ have the directions of the traces of its two cyclic planes, on that diametral plane ($S\nu\rho' = 0$) which touches the given surface. We have therefore, by XXII., this general theorem, that the bisectors of the angle formed by those two traces are the tangents to the two lines of curvature, whatever the form of the given surface may be.

(10.) Supposing now that the given surface is itself one of the second order, and that its centre is at the origin 0, so that it may be represented (comp. 405, XII.) by the equation,

XXIV... $1 = S\rho\phi\rho = g\rho^2 + S\lambda\rho\mu\rho$,

with constant values of λ , μ , and g, which will reproduce with those values the form XVIII. of ϕ , we see that the *index surface* (9.) becomes in this case simply that given one, with its centre transported from o to \mathbf{P} ; and therefore with a tangent plane at the origin, which is parallel to the given tangent plane. And thus the traces (9.), of the cyclic planes on the diametral plane of the index surface, become here the tangents to the circular sections of the given surface. We recover then, as a case of the general theorem in (9.), this known but less general theorem : that the angles formed by the two circular sections, at any point of a surface of the second order, are bisected by the lines of curvature, which pass through the same point.

(11.) And because the tangents to these latter lines coincide generally, by (3.) (4.) (9.), with the axes of the diametral section of the index surface, made by the tangent plane to the given surface, they are parallel, in the case (10.), as indeed is well known, to the axes of the parallel section of a given surface of the second order.

(12.) And if we now look back to the Equation of Confocals in 407, (26.), and to the earlier formulæ of 407, (4.), we shall see that because the vector v_1 , in the last cited sub-article, represents a tangent to the given surface $S\rho\phi\rho = 1$, complanar^{*} with the normal v and the derived vector ϕv_1 , so that it satisfies

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^{*} Compare the Note to page 198.

ART. 410.] LINES OF CURVATURE ON CENTRAL SURFACES.

(comp. 407, XII. XIV., and the recent formulæ V. VI.) the two scalar equations,

XXV... $S_{\nu\nu_1} = 0$, and XXVI... $S_{\nu\nu_1\phi\nu_1} = 0$,

which are likewise satisfied (comp. (7.)) when we change ν_1 to the rectangular tangent ν_2 , it follows that these two vectors, ν_1 and ν_2 , which are the normals to the two confocals to (e) through P, are also the tangents to the two lines of curvature on that given surface of the second order at that point : whence follows this other theorem^{*} of Dupin, that the curve of orthogonal intersection (407, (4.)), of two confocal surfaces, is a line of curvature on each.

(13.) And by combining this known theorem, with what was lately shown respecting the *umbilicar generatrices* (in 408, (30.), (32.), comp. also (35.), (36.)), we may see that while, on the one hand, the *lines of curvature* on a central surface of the second order have no real envelope, yet on the other hand, in an imaginary sense, they have for their common envelope[†] the system of the eight imaginary right lines (408, (31.)), which connect the twelve (real or imaginary) umbilies of the surface, three by three, and are at once generating lines of the surface itself, and also of the known developable envelope of the confocal system.

(14.) It may be added, as another curious property of these eight *imaginary right lines*, that each is, in an imaginary sense, itself a line of curvature upon the surface: or rather, each represents two coincident lines of that kind. In fact, if we denote the variable vector 408, LXXX. of such a generatrix by the expression,

XXVII. . . $\rho = e'\sigma + \sigma'$,

* Dév. de Géométrie, page 271, &c.

2 H 2

[†] The writer is not aware that this theorem, to which he was conducted by quaternions, has been enunciated before ; but it has evidently an intimate connexion with a result of Professor Michael Roberts, cited in page 290 of Dr. Salmon's Treatise, respecting the *imaginary geodetic tangents to a line of curvature*, drawn from an unbilicar point, which are analogous to the imaginary tangents to a plane conic, drawn from a focus of that curve. An illustration, which is almost a visible representation, of the theorem (13.) is supplied by Plate II. to Liouville's Monge (and by the corresponding plate in an earlier edition), in which the prolonged and dotted parts of certain ellipses, answering to the real projections of imaginary portions of the lines of curvature of the ellipsoid, are seen to touch a system of four real right lines, namely the projections (on the same plane of the greatest and least axes), of the four real unbilicar tangent planes, and therefore also of what have been above called (408, (30.), (31.)) the eight (imaginary) umbilicar generatrices of the surface. Accordingly Monge observes (page 150 of Liouville's edition), that "toutes les ellipses, projections des lignes de courbure, seront inscrites dans ce parallélogramme dont chacune d'elles touchera les quatre côtés ": with a similar remark in his explanation of the corresponding figure (page 160).

in which e' is a variable scalar, but σ , σ' are two given or constant but imaginary vectors, such that

XXVIII...
$$\sigma^2 = 0$$
, $S\sigma\sigma' = -l^2$, $\sigma'^2 = -b^2$,

and

XXIX...
$$f\sigma = S\sigma\phi\sigma = 0$$
, $f(\sigma, \sigma') = S\sigma'\phi\sigma = 0$, $f\sigma' = 1$,

we have the imaginary normal ν , with (for the case of a real umbilic) a real tensor,

XXX...
$$\nu = e'\phi\sigma + \phi\sigma' \perp \sigma$$
, XXXI... $T\nu = \pm \frac{(e-e')l^2}{abc}$;

and we find, after reductions, the imaginary expression,

whence

$$XXXII...\nu\sigma = \pm \sqrt{-1} \sigma T\nu,$$

XXXIII... $S\nu\sigma = 0$, $S\nu\sigma\phi\sigma = 0$.

The differential equations V. VI. of a line of curvature are therefore symbolically satisfied, when we substitute, for the tangential vector τ , either the imaginary line σ itself, or the apparently perpendicular but in an imaginary sense coincident* vector $\nu\sigma$; and the recent assertions are justified.

(15.) As regards the *real* lines of curvature, on a central surface of the second order, we see by comparing the general differential equation II. with the expression 409, XXIII. for the differential of h, or of $P^{-2}D^{-2}$, that this latter product, or the product P. D itself, is constant \dagger for a line of curvature, as well as for a geodetic line, on such a surface, as indeed it is well known to be : although this last constant (P. D) may become imaginary, for the case of a single-sheeted \ddagger hyperboloid, and must be such for a line of curvature on an hyperboloid of two sheets.

† Compare the second Note to page 229.

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^{*} As regards the paradox, of the *imaginary vector* σ being thus apparently *perpendicular to itself*, a similar one had occurred before, in the investigation 353, (17.), (18.), (19.); and it is explained, on the principles of modern geometry, by observing that this imaginary vector is *directed to the circle at infinity*. Compare 408, (31.), and the Note to page 516, vol. i.

[‡] Although the writer has been content to employ, in the present work, some of these usual but rather long appellations, he feels the elegance of Dupin's phraseology, adopted also by Möbius, and by some other authors, according to which the two central hyperboloids are distinguished, as *elliptie* (for the case of *two* sheets), and *hyperbolic* (for the case of *one*). The phrase "*quadric*," for the *general* surface of the second order (or second degree), employed by Dr. Salmon and Mr. Cayley, is also very convenient. It may be here remarked, that Dupin was perfectly aware of, or rather appears to have first discovered, the existence of what have since his time come to be called the *focal conics*; which important curves were considered by him, as being at once *limits of confocal surfaces*, and also *loci of umbilies*. Comp. Dév. de Géométrie, pages 270, 277, 278, 279; see also page 390 of the *Aperçu Historique*, &c., by M. Chasles (Brussels, 1837).

ART. 410.]

INDEX SURFACE.

(16.) And as regards the general theory of the index surface (9.), it is to be observed that this auxiliary surface depends primarily on the scalar function f, in the equation $f\rho = 1$, or generally $f\rho = \text{const.}$, of the given surface; and that it is not entirely determined by means of that surface alone. For if we write, for instance,

XXXIV... $f_{\rho} = f_1$, with $d_{\rho} = 2S_{\nu}d_{\rho}$ as before,

we shall have, as the new first differential equation of the same given surface, instead of III.,

with

 $XXXV...0 = df f \rho = 2Sn \nu d\rho,$

XXXVI. . . $n = f' f \rho$;

and if we then write, by analogy to IV.,

with

XXXVIII...
$$n' = 2f''_{f\rho}$$
,

the new index surface, constructed on the plan (9.), will have for its equation, analogous to XXIII., the following :

XXXVII... $d \cdot n\nu = \Phi d\rho = n\phi d\rho + n'\nu S\nu d\rho$,

XXXIX...
$$S\rho' \Phi \rho' = n S\rho' \phi \rho' + n' (S\nu \rho')^2 = \text{const.}$$

(17.) But if we take this last constant = n, the two index surfaces, XXIII. and XXXIX., will have a common diametral section, made by the given tangent plane, namely the index curve (4.); and they will touch each other, in the whole extent of that curve. And it will be found that the construction (9.), for the directions of the lines of curvature, applies equally well to the one as to the other, of these two auxiliary surfaces : in fact, it is evident that the differential equation II., namely $S_{\nu}d_{\nu}d_{\rho} = 0$, receives no real alteration, when ν is multiplied by any scalar, n, even if that scalar should be variable.

(18.) And instead of supposing that the variable vector ρ is thus obliged, as in 373, to satisfy a given scalar equation, of the form*

$$f\rho = \text{const.}$$

* If $\rho = ix + jy + kz$, and $v = f\rho = F(x, y, z)$, and if we write,

$$\begin{split} \mathrm{d} v &= p\mathrm{d} x + q\mathrm{d} y + r\mathrm{d} z, \qquad \mathrm{d} p = p'\mathrm{d} x + r''\mathrm{d} y + q''\mathrm{d} z, \\ \mathrm{d} q &= q'\mathrm{d} y + p''\mathrm{d} z + r''\mathrm{d} x, \qquad \mathrm{d} r = r'\mathrm{d} z + q''\mathrm{d} x + p''\mathrm{d} y, \end{split}$$

[III. m. § 7.

we may suppose, as in 372, that ρ is a given vector function of two scalar variables, x and y, between which there will then arise, by the same fundamental formula II., a differential equation of the first order and second degree, to be integrated (when possible) by known methods. For example, if we write,

XL...
$$\rho = ix + jy + kz$$
, $dz = pdx + qdy$,

we may then write also, on the present plan, which gives $df\rho = 2S\nu d\rho$,

$$\begin{aligned} \mathrm{d}\rho &= i\mathrm{d}x + j\mathrm{d}y + k\mathrm{d}z, & \nu &= -\frac{1}{2}(ip + jq + kr), \\ \mathrm{d}\nu &= -\frac{1}{2}(i\mathrm{d}p + j\mathrm{d}q + k\mathrm{d}r), & \mathrm{Sd}\rho\mathrm{d}\nu &= \frac{1}{2}(\mathrm{d}x\mathrm{d}p + \mathrm{d}y\mathrm{d}q + \mathrm{d}z\mathrm{d}r); \end{aligned}$$

and the *index surface*, constructed as in (9.), and with ρ' changed to $\Delta \rho = i\Delta x + j\Delta y + k\Delta z$, will thus have the equation,

(a). . .
$$\frac{1}{2}p'\Delta x^2 + \frac{1}{2}q'\Delta y^2 + \frac{1}{2}r'\Delta z^2 + p''\Delta y\Delta z + q''\Delta z\Delta x + r''\Delta x\Delta y = 1$$
,

or more generally = const.; so that it may be made in this way to depend upon, and be entirely determined by, the six partial differential coefficients of the second order, p'. p''. ., of the function v or $f\rho$, taken with respect to the three rectangular coordinates, xyz. And by comparing this equation (a) with the following equation of the same auxiliary surface, which results more directly from the principles employed in the text (comp. XVIII. XXIII.),

(b). . .
$$S\Delta\rho\phi\Delta\rho = g\Delta\rho^2 + S\lambda\Delta\rho\mu\Delta\rho = 1$$
,

we can easily deduce *expressions* for those six partial *coefficients*, in terms of g, λ , μ . Thus, for example,

$$\frac{1}{2}D_x v = \frac{1}{2}p = -g + 5\lambda i\mu i = 5\lambda\mu - g + 25i\lambda Si\mu ;$$

Si $\lambda Si\mu + Sj\lambda Sj\mu + Sk\lambda Sk\mu = -S\lambda\mu ;$ therefore,

but

(c). . .
$$\frac{1}{2}(D_x^2v + D_y^2v + D_z^2v) = S_{\lambda\mu} - 3g = c_1 + c_2 + c_3 = -m'',$$

if c_1 , c_2 , c_3 be the roots and m'' a coefficient of a certain cubic (354, III.), deduced from the linear and vector function $d\nu = \phi d\rho$, on a plan already explained. If then the function v satisfy, as in several physical questions, the *partial differential equation*,

(d). . .
$$D_x^2 v + D_y^2 v + D_z^2 v = 0$$
,

the sum of these three roots, c_1 , c_2 , c_3 , will vanish: and consequently, the asymptotic cone to the index surface, found by changing 1 to 0 in the second member of (a), is real, and has (comp. 406, XXI., XXIX.) the property that

(e). . .
$$\cot^2 a + \cot^2 b = 1$$
,

if a, b denote its two extreme semiangles. An entirely different method of transforming, by quaternions, the well known equation (d), occurred early to the present writer, and will be briefly mentioned somewhat farther on. In the mean time it may be remarked, that because m'' = 0 by (c), when the equation (d) is satisfied, we have then, by the general theory III. ii. 6 of linear and vector functions, and especially by the sub-articles to 350, remembering that ϕ is here self-conjugate, the formulæ,

(f)...
$$d\nu + \chi d\rho = 0$$
, and (g)... $\psi \sigma - \phi^2 \sigma = m' \sigma$,

 χ , ψ being auxiliary functions, and m' another coefficient of the cubic, while σ is an arbitrary vector. For the same reason, and under the same condition (d), the function ϕ itself has the properties expressed by the equations,

(h). . .
$$\phi V_{i\kappa} = \kappa \phi_i - \iota \phi \kappa$$
, and (i). . . $\phi^2 V_{i\kappa} = V \phi_i \phi \kappa - m' V_{i\kappa}$;

in which the two vectors 1, K are arbitrary, and m' is the same scalar coefficient as before.

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we shall satisfy the equation III. by assuming (with a constant factor understood),

XLI.
$$\nu = ip + jq - k$$
, whence **XLII.** $d\nu = idp + jdq$;

and thus the general equation II., for the lines of curvature on an arbitrary surface, receives (by the laws of ijk) the form,

XLIII. . .
$$dp(dy + qdz) = dq(dx + pdz);$$

which last form has accordingly been assigned, and in several important questions employed by Monge^{*}: but which is now seen to be *included* in the still more concise (and more easily deduced and interpreted) quaternion equation,

$$S\nu d\nu d\rho = 0$$

411. For a central surface of the second order, we have as usual $\nu = \phi \rho$, $\Delta \nu = \phi \Delta \rho$, and therefore (by 347, 348, and by the self-conjugate form of ϕ),

I. . .
$$\nabla \nu \Delta \nu = \nabla \phi \rho \phi \Delta \rho = \psi \nabla \rho \Delta \rho = m \phi^{-1} \nabla \rho \Delta \rho$$
;

the general condition of intersection 410, I. of two normals, at the extremities of a finite chord $\Delta \rho$, and the general differential equation 410, II. of the lines of curvature, may therefore for such a surface receive these new and special forms:

II...
$$S\Delta\rho\phi^{-1}\nabla\rho\Delta\rho = 0$$
, or II'... $S\rho\Delta\rho\phi^{-1}\Delta\rho = 0$;
III... $Sd\rho\phi^{-1}\nabla\rho d\rho = 0$, or III'... $S\rho d\rho\phi^{-1}d\rho = 0$;

which admit of geometrical interpretations, and conduct to some new theorems, especially when they are transformed as follows:

$$\begin{split} \mathrm{IV.} & . . \ \mathrm{S}\lambda\Delta\rho \ . \ \mathrm{S}\rho\Delta\rho\phi^{-1}\mu + \mathrm{S}\mu\Delta\rho \ . \ \mathrm{S}\rho\Delta\rho\phi^{-1}\lambda = 0, \\ \mathrm{V.} & . \ . \ \mathrm{S}\lambda\mathrm{d}\rho \ . \ \mathrm{S}\rho\mathrm{d}\rho\phi^{-1}\mu + \mathrm{S}\mu\mathrm{d}\rho \ . \ \mathrm{S}\rho\mathrm{d}\rho\phi^{-1}\lambda &= 0, \end{split}$$

^{*} See the enunciation of the formula here numbered as XLIII., in page 133 of Liouville's Monge: compare also the applications of it, in pages 274, 303, 305, 357. (The corresponding pages of the Fourth Edition are, 115, 240, 265, 267, 312.) The quaternion equation, $S\nu d\nu d\rho = 0$, was published by the present writer, in a communication to the Philosophical Magazine, for the month of October, 1847 (page 289). See also the Supplement to the same Volume xxxi. (Third Scries); and the Proceedings of the Royal Irish Academy for July, 1846.

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 λ and μ being (as in 405, (5.), &c.) the *two real cyclic normals* of the surface: while the same equations may also be written under the still more simple forms,

VI...
$$Sa\Delta\rho \cdot Sa'\rho\Delta\rho + Sa'\Delta\rho \cdot Sa\rho\Delta\rho = 0$$
,
VII... $Sad\rho \cdot Sa'\rho d\rho + Sa' d\rho \cdot Sa\rho d\rho = 0$,

a, a' being, as in several recent investigations, the two real focal unit lines, which are common to a whole confocal system.

(1.) The vector $\phi^{-1}V\rho\Delta\rho$ in II. has by I. the direction of $V\nu\Delta\nu$; whence, by 410, (6.), the interpretation of the recent equation II., or (for the present purpose) of the more general equation 410, I., is that the chord PP' is perpendicular to its own polar, if the normals at its extremities intersect. Accordingly, if their point of intersection be called N, the polar of PP' is perpendicular at once to PN and P'N, and therefore to PP' itself.

(2.) The equation II'. may be interpreted as expressing, that when the normals at P and P' thus intersect in a point N, there exists a point P'' in the diametral plane OPP', at which the normal P''N'' is parallel to the chord PP': a result which may be otherwise deduced, from elementary principles of the geometry of surfaces of the second order.

(3.) It is unnecessary to dwell on the converse propositions, that when either of these conditions is satisfied, there is intersection (or parallelism) of the two normals at P and P': or on the corresponding but limiting results, expressed by the equations III. and III'.

(4.) In order, however, to make any use in *calculation* of these new forms II., III., we must select some suitable expression for the self-conjugate function ϕ , and deduce a corresponding expression for the inverse function ϕ^{-1} . The *form*,*

VIII. . .
$$\phi \rho = g \rho + V \lambda \rho \mu$$
,

$$f\rho = g\rho^2 + S\lambda\rho\mu\rho, \qquad 357, \text{ II.}$$

has likewise been frequently employed.

^{*} The vector form VIII. occurred, for instance, in pages 520, 529, 535, 549, vol. i., and 193, 233, vol. ii. ; and the connected scalar form,

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which has already several times occurred, has also been more than once inverted : but the following new inverse* form,

IX...
$$(g - S\lambda\mu) \cdot \phi^{-1}\rho = \rho - \lambda S\rho\phi^{-1}\mu - \mu S\rho\phi^{-1}\lambda,$$

has an advantage, for our present purpose, over those assigned before. In fact, this form IX. gives at once the equation,

$$\mathbf{X}...(g-S\lambda\mu)\cdot\phi^{-1}\nabla\rho\Delta\rho=\nabla\rho\Delta\rho-\lambda S\rho\Delta\rho\phi^{-1}\mu-\mu S\rho\Delta\rho\phi^{-1}\lambda;$$

and so conducts immediately from II. to IV., or from III. to V. as a limit.

(5.) The equation IV. expresses generally, that the chord $\Delta \rho$, or PP', is a side of a certain cone of the second order, which has its vertex at the point P of the given surface, and passes through all the points P' for which the normals to that surface *intersect* the given normal at P; and the equation V. expresses generally, that the two sides of this last cone, in which it is cut by the given tangent plane at the same point P, are the tangents to the line of curvature.

(6.) But if the surface be an *ellipsoid*, or a *double*-sheeted hyperboloid, then (comp. 408, (29.)) the *always real vectors*, $\dagger \phi^{-1}\lambda$ and $\phi^{-1}\mu$, have the directions of *semidiameters* drawn to *two of the four real umbilics*; supposing then that ρ is *such* a semidiameter, and that it has the direction of $\pm \phi^{-1}\lambda$, the second term of the first member of the equation IV. vanishes, and the *cone* IV. breaks up into a *pair of planes*, of which the equations in ρ' are,

XI... $S\lambda(\rho' - \rho) = 0$, and **XII.**.. $S\rho'\phi^{-1}\lambda\phi^{-1}\mu = 0$;

whereof the former represents the tangent plane at the umbilic P, and the latter represents the plane of the four real umbilics.

(7.) It follows, then, that the normal at the real umbilic \mathbf{P} is not intersected by any real normal to the surface, except those which are drawn at points \mathbf{P} of that principal section, on which all the real umbilies are situated : but that the

$$\phi^{-1}\lambda = \frac{g\lambda - \lambda^2\mu}{g^2 - \lambda^2\mu^2}, \quad \phi^{-1}\mu = \frac{g\mu - \mu^2\lambda}{g^2 - \lambda^2\mu^2}.$$

† Compare the Note immediately preceding.

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^{*} Inverse forms, for $\phi^{-1}\rho$ or $m^{-1}\psi\rho$, have occurred in pages 521, 549, vol. i., and 193, vol. ii. In comparing these with the form IX., it will easily be seen (comp. page 221) that

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same real umbilicar normal PN is, in an imaginary sense, intersected by all the imaginary normals, which are drawn from the imaginary points \mathbf{P}' of either of the two imaginary generatrices through \mathbf{P} .

(8.) In fact, the locus of the point P', under the condition of intersection of its normal P'N' with a given normal PN, is generally a quartic curve, namely the intersection of the given surface with the cone IV; but when this cone breaks up, as in (6.), into two planes, whereof one is normal, and the other tangential to the surface, the general quartic is likewise decomposed, and becomes a system of a real conic, namely the principal section (7.) and a pair of imaginary right lines, namely the two umbilicar generatrices at P.

(9.) We see, at the same time, in a new way (comp. 410, (14.)), that each such generatrix is (in an imaginary sense) a line of curvature: because the (imaginary) normals to the surface, at all the points of that generatrix, are situated by (7.) in one common (imaginary) normal plane.

(10.) Hence through a real umbilic, on a surface of the second order there pass three lines of curvature: whereof one is a real conic (8.), and the two others are imaginary right lines, namely, the umbilicar generatrices as before.

(11.) If we prefer *differentials* to *differences*, and therefore use the equation V. of the lines of curvature, we find that this equation takes the form 0 = 0, if the point P be an umbilic; and that if the normal at that point be parallel to λ , the *differential of the equation* V. breaks up into *two factors*, namely,

XIII...
$$S\lambda d^2\rho = 0$$
, and XIV... $Sd\rho\phi^{-1}\lambda\phi^{-1}\mu = 0$;

whereof the former gives to imaginary directions, and the latter gives one real direction, coinciding precisely with the three directions (10.).

(12.) And if ρ , instead of being the vector of an *umbilic*, be only the vector of a point on a generatrix corresponding, we shall still satisfy the differential equation V., by supposing that $d\rho$ belongs to the same imaginary right line: because we shall then have, as at the umbilic itself,

XV...
$$S\lambda d\rho = 0$$
, $S\rho d\rho \phi^{-1}\lambda = 0$.

An umbilicar generatrix is therefore proved anew (comp. (9.)) to be, in its whole extent, a line of curvature.

(13.) The recent reasonings and calculations apply (6.), not only to an ellipsoid, but also to a double-sheeted hyperboloid, four umbilies for *each* of these two surfaces being *real*. But if for a moment we now consider

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specially the case of an *ellipsoid*, and if we denote for abridgment the real quotient $\frac{a-c}{a+c}$ by h, we may then substitute in IV. and V. for λ , μ , $\phi^{-1}\lambda$, $\phi^{-1}\mu$ the expressions,

XVI... $a - ha' = \frac{2bU\lambda}{a+c};$ $ha - a' = \frac{2bU\mu}{a+c};$ XVII... $a + ha' = \frac{-2b\phi^{-1}U\lambda}{ac(a+c)};$ $-ha - a' = \frac{-2b\phi^{-1}U\mu}{ac(a+c)};$

and then, after division by $h^2 - 1$, there remain only the two vector constants a, a', the equation IV. reducing itself to VI., and V. to VII.

(14.) The simplified equations thus obtained are not however peculiar to *ellipsoids*, but extend to a whole *confocal system*. To prove this, we have only to combine the equations II. and III. with the *inverse form*,

XVIII...
$$l^{-2}\phi^{-1}\rho = aSa'\rho + a'Sa\rho - \rho(e + Saa'),$$

which follows from 407, XV., and gives at once the equations VI. and VII., whatever the species of the surface may be.

(15.) The differential equation VII. must then be satisfied by the three rectangular directions of $d\rho$, or of a tangent to a line of curvature, which answer to the orthogonal intersections (410, (12.)) of the three confocals through a given point \mathbf{P} ; it ought therefore, as a verification, to be satisfied also, when we substitute ν for $d\rho$, ν being a normal to a confocal through that point: that is, we ought to have the equation,

XIX. . .
$$Sa\nu Sa'\rho\nu + Sa'\nu Sa\rho\nu = 0$$
.

And accordingly this is at once obtained from 407, XVI., by operating with S. $\rho\nu$; so that the *three normals* ν are all *sides of this cone* XIX., or of the cone VII. with $d\rho$ for a side, with which the cone V. is found to coincide (13.).

(16.) And because this last equation XIX., like VI. and VII., involves only the two focal lines a, a' as its constants, we may infer from it this theorem : "If indefinitely many surfaces of the second order have only their asymptotic cones biconfocal,* and pass through a given point, their normals at

^{*} That is, if the surfaces (supposed to have a common centre) be cut by the plane at infinity in biconfocal conics, real or imaginary.

that point have a cone of the second order for their locus"; which latter cone is also the locus of the tangents, at the same point, to all the lines of curvature which pass through it, when different values are successively assigned to the scalar constant $a^2 - c^2$ (or $2l^2$): that is, when the asymptotes a, a' to the focal hyperbola remain unchanged in position, but the semiaxes $(a^2 - b^2)^{\frac{1}{2}}$, $(b^2 - c^2)^{\frac{1}{2}}$ of that curve (here treated as both real) vary together.

(17.) The equation VI. of the cone of chords (5.) introduces the fixed focal lines a, a' by their directions only. But if we suppose that the lengths of those two lines are equal, without being here obliged to assume that each of those lengths is unity, we shall then have (comp. 407, (2.), (3.)), the following rectangular system of unit lines, in the directions of the axes of the system,

XX...
$$U(a + a')$$
, $UVaa'$, $U(a - a')$,

which obey in all respects the laws of ijk, and may often be conveniently *denoted* by those symbols, in investigations such as the present. And then, by decomposing the semidiameter ρ , and the chord $\Delta \rho$, in these three directions XX., we easily find the following *rectangular transformation*^{*} of the foregoing equation VI.,

XXI. . .
$$\frac{S(a + a')^{-1}\rho}{S(a + a')\Delta\rho} + \frac{S(a - a')^{-1}\rho}{S(a - a')\Delta\rho} = \frac{S \cdot (Vaa')^{-1}\rho}{S \cdot Uaa'\Delta\rho};$$

in which it is permitted to change $\Delta \rho$ to $d\rho$, in order to obtain a new form of the differential equation of the *lines of curvature*; or else at pleasure to ν , and so to find, in a new way, a *condition* satisfied by the *three normals*, to the *three confocals* through P.

(18.) The cone, VI. or XXI., is generally the locus of a system of three rectangular lines; each plane through the vertex, which is perpendicular to any real side, cutting it in a real pair of mutually rectangular sides: while, for the

* The corresponding form, in rectangular coordinates, of the condition of intersection, of normals at two points (xyz) and (x'y'z'), to the surface,

$$\frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2} = 1,$$

is the equation (probably a known one, although the writer has not happened to meet with it),

$$\frac{(b^2-c^2)x'}{x-x'} + \frac{(c^2-a^2)y'}{y-y'} + \frac{(a^2-b^2)z'}{z-z'} = 0;$$

in which it is evident that xyz and x'y'z' may be interchanged.

ART. 411.] RECTANGULAR TRANSFORMATION.

same reason, the section of the same cone, by any plane which does not pass through its vertex P, but cuts any side perpendicularly, is generally an equilateral hyperbola.

(19.) If, however, the point P be situated in any one of the three principal planes, perpendicular to the three lines XX., then the cone XXI. (as its equation shows) breaks up (comp. (6.)) into a pair of planes, of which one is that principal plane itself, while the other is perpendicular thereto. And while the former plane cuts the surface in a principal section, which is always a line of curvature through P, the latter plane usually cuts the surface in another [conic, which crosses the former section at right angles, and gives the direction of the second line of curvature.

(20.) But if we further purpose, as in (6.), that the point P is an umbilic, then (as has been seen) the second plane is a tangent plane; and the second conic (19.) is itself decomposed, into a pair of imaginary right lines: namely, as before, the two umbilicar generatrices through the point, which have been shown to be, in an imaginary sense, both lines of curvature themselves, and also a portion of the envelope of all the others.

(21.) We shall only here add, as another transformation of the general equation ∇I . of the cone of chords, which does not even assume Ta = Ta', the following:

XXII. . . $S(a + a')\Delta\rho$. $S(a + a')\rho\Delta\rho = S(a - a')\Delta\rho$. $S(a - a')\rho\Delta\rho$;

where the directions of the two new lines, a + a' and a - a', are only obliged to be harmonically conjugate with respect to the directions of the fixed focal lines of the system : or in other words, are those of any two conjugate semidiameters of the focal hyperbola.*

^{* [}In order to obtain additional illustrations of the remark made at the beginning of this Article that $S\rho\Delta\rho\phi^{-1}\Delta\rho = 0$, and the equivalent equations lead to geometrical theorems relating to a system of quadrics having the same pair of focal lines, we see in the first place if ω and ω' are any two vectors terminating on the chord, that the equation may be written in the form $S\omega\omega'\phi^{-1}(\omega-\omega')=0$. This is equivalent to the vector equation $(\phi^{-1}+h')\omega = (\phi^{-1}+h)\omega'$. Operating on this by $(\phi^{-1}+g)^{-1}$, we easily find $\overline{\varpi} = \omega + (h'-g)(\phi^{-1}+g)^{-1}\omega = \omega' + (h-g)(\phi^{-1}+g)^{-1}\omega'$. It is obvious from the form of these relations that the normal at ω to the quadric $S\rho(\phi^{-1}+g)^{-1}\rho = S\omega(\phi^{-1}+g)^{-1}\omega$ intersects the normal at ω' to the similar quadric $S\rho(\phi^{-1}+g)^{-1}\rho = S\omega'(\phi^{-1}+g)^{-1}\omega'$; and that $\overline{\omega}$ is the vector to the point of intersection. In particular, if ω and ω' happen to lie on the same quadric, the normals still intersect. Returning to the general case and allowing the arbitrarily assumed scalar g to vary, it is obvious that the point of intersection of the normals describes a twisted cubic if we remember the results of p. 131.

The relation between ω , ω' , h, and h' suggests the use of an auxiliary vector τ in terms of which we may write $\omega = (\phi^{-1} + h)\tau$ and $\omega' = (\phi^{-1} + h')\tau$. Thus τ is parallel to the chord, and the equation of the chord is $\rho = \phi^{-1}\tau + x\tau$. In terms of this vector, the vector to the point of intersection of

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412. The subject of *Lines of Curvature* receives of course an additional illustration, when it is combined with the known conception of the corresponding *Centres of Curvature*. Without yet entering on the general theory of the curvatures of sections of an arbitrary surface, we may at least consider here the curvatures of those normal sections, which touch at any given point the lines of curvature. Denoting then by σ the vector of the centre s of

normals becomes $\overline{\omega} = (\phi^{-1} + g)^{-1} (\phi^{-1} + h) (\phi^{-1} + h')\tau$. Regarding ω as fixed, we have $\overline{\omega} = (\phi^{-1} + g)^{-1} (\phi^{-1} + h')\omega$ as the vector equation of the locus of intersections of the normals at ω with the corresponding normals at the variable point $\omega' = (\phi^{-1} + h')\tau$. This surface locus which consists of right lines and twisted cubics is easily seen to be the quadric $S\overline{\omega}\omega\phi^{-1}(\overline{\omega}-\omega) = 0$. But we obtain a second interpretation for this locus since $\omega = (\phi^{-1} + g) (\phi^{-1} + h')^{-1}\overline{\omega} = \overline{\omega} + (g - h') (\phi^{-1} + h')^{-1}\overline{\omega}$ expresses that the normal at $\overline{\omega}$ to the quadric $S\rho(\phi^{-1} + h')^{-1}\rho = S\overline{\omega}(\phi^{-1} + h')^{-1}\overline{\omega}$ passes through the fixed point ω . So we may say that the quadric is the locus of points whose normals with respect to the doubly infinite system of quadrics $S\rho(\phi^{-1} + h')^{-1}\rho = C$ pass through the extremity of the given vector ω . Returning to the vector equation of the locus, we see that the locus of points whose normals pass through a fixed point is a twisted cubic when h' is constant, or when we have to do only with a system of confocal quadrics so that C is constant but h' variable, we have $S\overline{\omega}(\phi^{-1} + h')^{-1}\omega = C$, giving h' in terms of g. From this we deduce $(h' - g) ((\phi^{-1} + g)^{-1}\omega)^2 = C - S\omega(\phi^{-1} + g)^{-1}\omega$, and the vector equation of the locus of points on the system of confocals, whose normals pass through the extremity of ω , becomes

or

$$\begin{split} \varpi &= \omega + (C - \mathbf{S}\omega(\phi^{-1} + g)^{-1}\omega) \ ((\phi^{-1} + g)^{-1}\omega)^{-1}, \\ \varpi &= (C + \mathbf{V}\omega(\phi^{-1} + g)^{-1}\omega) \ ((\phi^{-1} + g)^{-1}\omega)^{-1}. \end{split}$$

We cannot delay on this curve except to state that it is a twisted quintic and unicursal, and that, being a quintic, it meets any quadric of the system in ten points, four of which must be foreign to the present inquiry as only six normals can be drawn to a quadric from a point.

Returning to the equation $\varpi = (\phi^{-1} + g)^{-1} (\phi^{-1} + h) (\phi^{-1} + h')\tau$, we shall express that the two points ω and ω' lie on the same quadric $S\rho(\phi^{-1} + g)^{-1}\rho = C$. In terms of τ and h, we see that ω lies on this quadric if $S\tau(\phi^{-1} + h)^2 (\phi^{-1} + g)^{-1}\tau = C$, and if ω' likewise lies on it, h' must be the second root of this quadratic in h. Expanding in terms of h - g for convenience, we have

$$(h-g)^{2}\mathrm{S}\tau(\phi^{-1}+g)^{-1}\tau + 2(h-g)\tau^{2} + \mathrm{S}\tau(\phi^{-1}+g)\tau = C,$$

and using this equation to eliminate h and h' from the expression for ϖ , we find

$$\varpi = (\phi^{-1} + g)\tau - \frac{2\tau^3}{S\tau(\phi^{-1} + g)^{-1}\tau} + (\phi^{-1} + g)^{-1}\tau \frac{S\tau(\phi^{-1} + g)\tau - C}{S\tau(\phi^{-1} + g)^{-1}\tau}.$$

This may be reduced to simpler forms, one being

$$\varpi = \frac{V(\phi^{-1} + g)\tau V\tau(\phi^{-1} + g)^{-1}\tau - (\phi^{-1} + g)V\tau V\tau(\phi^{-1} + g)^{-1}\tau - C(\phi^{-1} + g)^{-1}\tau}{S\tau(\phi^{-1} + g)^{-1}\tau}.$$

It is obvious when C alone varies that the locus is a right line; it is easily seen when g alone varies that the locus is a conic section, and when both vary, it may be proved that the locus is a ruled quartic having the line $\rho = \phi^{-1}\tau + x\tau$ for a triple line.

Finally, it easily follows from the equations of this note, that every line of the triply infinite system obtained by assigning all possible values to τ in the equation $\rho = \phi^{-1}\tau + x\tau$ is at every point normal to some one quadric, and at every point touches two quadrics of the doubly infinite system $S\rho(\phi^{-1} + g)^{-1}\rho = C$ along lines of curvature.]

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curvature of such a section, and by R the radius PS, considered as a scalar which is positive when it has the direction of $+\nu$, it is easy to see that we have the two fundamental equations:

I. . .
$$\sigma = \rho + R \mathbf{U} \mathbf{v}$$
;
II. . . $R^{-1} d\rho + d \mathbf{U} \mathbf{v} = 0$;

whence follows this new form of the general differential equation 410, II. of the lines of curvature,

III...
$$\nabla d\rho dU\nu = 0$$
;

with several other combinations or transformations,* among which the following may be noticed here:

$$\mathbf{IV.} \ . \ . \ \frac{\mathrm{T}\nu}{R} + \mathrm{S}\frac{\mathrm{d}\nu}{\mathrm{d}\rho} = 0.$$

(1.) The equation I. requires no proof; and from it the equation II. is obtained by merely differentiating \dagger as if σ and R were constant: after which the formula III. follows at once, and IV. is easily deduced.

(2.) To obtain from this last equation a more developed expression for R, we may assume for $d\nu$, considered as a linear and self-conjugate function of $d\rho$ (410, (1.)), the general form (comp. 410, XVIII.),

$$\nabla \ldots d\nu = g d\rho + \nabla \lambda d\rho \mu,$$

in which g, λ , μ are independent of $d\rho$; and then, while the *tangent* $d\rho$ has (by 410, XXII.) one or other of the *two directions*,

VI. . .
$$d\rho \parallel U \nabla \nu \lambda \pm U \nabla \nu \mu$$
,

the curvature R^{-1} receives one or other of the two values corresponding,

VII. . .
$$R^{-1} = -\mathbf{T}\nu^{-1}(g + \mathbf{S}\lambda\mathbf{U}\nu \cdot \mathbf{S}\mu\mathbf{U}\nu \pm \mathbf{T}\nabla\lambda\mathbf{U}\nu \cdot \mathbf{T}\nabla\mu\mathbf{U}\nu).$$

* [The expression $R^{-1}d\rho + T\nu^{-1}d\nu = x\nu$ is at times a useful transformation of II. The value of the scalar x need not generally be considered, though it is $- dT\nu^{-1}$.]

+ To students who are accustomed to *infinitesimals*, the *easiest* way is here to conceive the *differentials* to be such. But it has already been abundantly shown, that this *view* of the latter is by no means *necessary*, in the treatment of them by quaternions. (Compare the first Note to page 230.)

(3.) One mode of arriving at this last transformation, or of showing that if (comp. again 410, XXII.) we assume,

VIII... $\tau = (\text{or } \parallel) \mathbf{U} \mathbf{V} \lambda \mathbf{v} \pm \mathbf{U} \mathbf{\nabla} \mu \mathbf{v},$

then

IX. . . $S\lambda\tau\mu\tau^{-1} = S\lambda U\nu$. $S\mu U\nu \pm T\nabla\lambda U\nu$. $T\nabla\mu U\nu$,

or

 $X. . . 2S\lambda\tau . S\mu\tau^{-1} = S(V\lambda U\nu . V\mu U\nu) \pm TV\lambda U\nu . TV\mu U\nu,$ or finally,

XI. . .
$$2SU\lambda\tau$$
 . $SU\mu\tau^{-1} = S(VU\lambda\nu . VU\mu\nu) \pm TVU\lambda\nu . TVU\mu\nu$,

is to introduce the auxiliary quaternion,

XII...
$$q = VU\lambda\nu .VU\mu\nu$$
;

and to prove that, with the value (or direction) VIII. of τ , we have thus the equation (in which Vq^2 , as usual, represents the square of Vq),

XIII. . . 2SU
$$\lambda \tau$$
 . SU $\mu \tau^{-1}$ = Sq \pm Tq = $\frac{\nabla q^2}{Sq \mp Tq}$.

(4.) And this may be done, by simply observing that we have thus (with the value VIII.) the expressions,

XIV. . .
$$S\tau U\lambda = \frac{\pm SU\lambda\mu\nu}{TVU\mu\nu}, \quad S\tau U\mu = \frac{-SU\lambda\mu\nu}{TVU\lambda\nu};$$

XV. . . $S\tau U\lambda . S\tau U\mu = \frac{\mp (SU\lambda\mu\nu)^2}{TVU\lambda\nu . TVU\mu\nu} = \frac{\pm Vq^2}{Tq},$

because

$$\mathbf{X}\mathbf{V}\mathbf{I}...\mathbf{V}q = -\mathbf{U}\boldsymbol{\nu}.\mathbf{S}\mathbf{U}\boldsymbol{\lambda}\boldsymbol{\mu}\boldsymbol{\nu};$$

and

XVII...
$$\tau^2 = -2 \pm 2$$
SU $q = \pm \frac{2(\text{S}q \mp \text{T}q)}{\text{T}q}$

(5.) Admitting then the expression VII., for the curvature R^{-1} , we easily see that it may be thus transformed :

XVIII...
$$R^{-1} = -T\nu^{-1}\left(g + T\lambda\mu \cdot \cos\left(\angle \frac{\nu}{\lambda} \mp \angle \frac{\nu}{\mu}\right)\right);$$

and that the difference of the two (principal) curvatures, of normal sections of an arbitrary surface, answering generally to the two (rectangular) directions of the lines of curvature through the particular point considered, ranishes when

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the normal v has the direction of either of the two cyclic normals, λ , μ , of the index surface (410, (9.)); that is, when the index curve (410, (4.)), considered as a section of that index surface, is a circle : or finally, when the point in question is, in a received sense, an umbilic* of the given surface.

(6.) That surface, although considered to be a given one, has hitherto (in these last sub-articles) been treated as quite general. But if we now suppose it to be a central surface of the second order, and to be represented by the equation,

XIX...
$$f\rho = g\rho^2 + S\lambda\rho\mu\rho = 1$$
,

which has already several times occurred, we see at once, from the formula VII. or XVIII. (comp. 410, (10.)), that the difference of curvatures, of the two principal normal sections of any such surface, varies proportionally to the perpendicular $(T_{\nu^{-1}} \text{ or } P)$ from the centre on the tangent plane, multiplied by the product of the sines of the inclinations of that plane, to the two cyclic planes of the surface.

(7.) In general (comp. 409, (3.)), it is easy to see that

XX...
$$S \frac{\mathrm{d}\nu}{\mathrm{d}\rho} = S\tau^{-1}\phi\tau = -D^{-2},$$

if D denote the (scalar) semidiameter of the index surface, in the direction of $d\rho$ or of τ ; but for the two directions of the *lines of curvature*, these semidiameters become (410, (3.), (4.)) the semiaxes of the index curve. Denoting then by a1 and a2 these last semiaxes, the two principal radii of curvature of any surface come by IV. to be thus expressed :

XXI...
$$R_1 = a_1^{2'} \Gamma \nu$$
; $R_2 = a_2^{2'} \Gamma \nu$.

And if the surface be a central one, of the second order, then a_1 , a_2 are the semiaxes of the diametral section, parallel to the tangent plane; while T_{ν} is (comp. again 409, (3.)) the reciprocal P^{-1} of the perpendicular, let fall on that plane from the centre. Accordingly (comp. (6.), and 219, (4.)), it is known that the difference of the inverse squares of those semiaxes varies proportionally to the product of the sines of the inclinations, of the plane of the section to the two cyclic planes.

^{*} Compare the Note to page 233.

^{† [}The expressions of this sub-article enable us to deduce the equation of a system of quadrics having at a given point on an arbitrary surface the same elements of lines of curvature as the arbitrary surface, and the same values of the principal curvatures.

We know that the lines of curvature at a point on a quadric are parallel to the principal axes of the central section parallel to the tangent plane. If τ_1 and τ_2 are unit vectors touching the lines of HAMILTON'S ELEMENTS OF QUATERNIONS, VOL. II.

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(8.) And as regards the squares themselves, it follows from 407, LXXI., that they may be thus expressed, in terms of the *principal semiaxes* of the *confocal surfaces*, and in agreement with known results:

XXII...
$$a_1^2 = a^2 - a_1^2; \quad a_2^2 = a^2 - a_2^2;$$

being thus both positive for the case of an ellipsoid; both negative, for that of a double-sheeted hyperboloid; and one positive, but the other negative, for the case of an hyperboloid of one sheet (comp. 410, (15.)).

(9.) In all these cases, the normal + ν is drawn towards the same side of the tangent plane, as that on which the centre o of the surface is situated (because $S_{\nu\rho} = 1$); hence (by I. and XXI.) both the radii of curvature R_1 , R_2 are drawn in this direction, or towards this side, for the ellipsoid; but one such radius for the single-sheeted hyperboloid, and both radii for the hyperboloid of two sheets, are directed towards the opposite side, as indeed is evident from the forms of these surfaces.

curvature, and if ρ is the vector from the centre to the point, the vectors $a_1\tau_1$, $a_2\tau_2$ and ρ compose a system of mutually conjugate radii of the quadric. It is easy to prove (see below) that

$$(S\omega\beta\gamma)^2 + (S\omega\gamma\alpha)^2 + (S\omega\alpha\beta)^2 = (S\alpha\beta\gamma)^2$$

is the equation of a quadric of which α , β , and γ are conjugate radii. In particular

$$a_2^2(S\omega\tau_2\rho)^2 + a_1^2(S\omega\tau_1\rho)^2 + a_1^2a_2^2(S\omega\tau_1\tau_2)^2 = a_1^2a_2^2(S\rho\tau_1\tau_2)^2$$

is the equation of a quadric having its centre at the origin and arbitrarily assumed directions for the lines of curvature at the extremity of ρ . Now the central perpendicular on the tangent plane at ρ has its length equal to $P = S\rho\tau_1\tau_2 = S\rho U\nu$. So, by XXI., we have

 $R_2(\mathbf{S}\omega\tau_2\rho)^2 + R_1(\mathbf{S}\omega\tau_1\rho)^2 + R_1R_2(\mathbf{S}\omega\mathbf{U}\nu)^2\mathbf{S}\rho\mathbf{U}\nu = R_1R_2(\mathbf{S}\rho\mathbf{U}\nu)^3$

for the equation of a quadric with its centre at the origin, having at an assumed point arbitrarily assumed directions for the lines of curvatures and arbitrarily assumed values for the curvatures. By varying the position of the centre, we can thus determine a system of quadrics having contact of the high order described with any surface at a given point.

We cannot delay discussing this system of quadrics except to state that when the centre lies on a certain line, the lines of curvature of the quadric have four point contact with those of the surface. We can, moreover, only suggest as an exercise on the notation given in the Note to page 225, the investigation of the locus of points on a quadric or on a confocal system at which one or both of the principal curvatures are given. It seems, however, to be worth while to prove the expression for a quadric in terms of the conjugate radii. If the equation of the quadric is $S\omega\phi\omega = 1$, and if α , β , and γ are conjugate radii, among the conditions are $S\alpha\phi\alpha = 1$ and $S\beta\phi\alpha = S\gamma\phi\alpha = 0$. Thus

we have
$$\begin{split} & \phi \alpha = V \beta \gamma (S \alpha \beta \gamma)^{-1} \quad \text{and because} \quad \omega S \alpha \beta \gamma = \alpha S \beta \gamma \omega + \beta S \gamma \alpha \omega + \gamma S \alpha \beta \omega, \\ & \phi \omega (S \alpha \beta \gamma)^2 = V \beta \gamma S \beta \gamma \omega + V \gamma \alpha S \gamma \alpha \omega + V \alpha \beta S \alpha \beta \omega. \end{split}$$

The forms of the invariants of this function afford proofs of certain well-known theorems. We see also easily that $\phi^{-1}\omega = \alpha S\alpha\omega + \beta S\beta\omega + \gamma S\gamma\omega$ from which known theorems may be derived, and this function ϕ^{-1} may be used with advantage in certain questions relating to confocals. Again to find a set of directions U α , U β , and U γ conjugate to two quadries depending on two functions ϕ and ϕ_1 , we have to solve $V\phi_1\omega\phi\omega = 0$ or $V\omega\phi_1^{-1}\phi\omega = 0.$]

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(10.) The following is another method of deducing generally the two principal curvatures of a surface, from the self-conjugate function,*

$$XXIII... d\nu = \phi d\rho, \qquad 410, IV.$$

which affords some good practice in the processes of the present Calculus. Writing, for abridgment,

XXIV. . .
$$r = \frac{\nu}{\sigma - \rho} = R^{-1} \Gamma \nu = -S \frac{\mathrm{d}\nu}{\mathrm{d}\rho} = -S \tau^{-1} \phi \tau$$

where τ is still a tangent to a line of curvature, the equation II. is easily brought to the form,

$$XXV...-r\tau = \nu^{-1}V\nu\phi\tau = \phi\tau - \nu^{-1}S\tau\phi\nu = \Phi\tau,$$

where Φ denotes a new linear and vector function, which however is not in general self-conjugate, because we have not generally $\phi v \parallel v$. Treating then this new function on the plan of the Section III. ii. 6, we derive from it a new cubic equation, of the form,

$$\mathbf{XXVI.} \quad 0 = \mathbf{M} + \mathbf{M}'r + \mathbf{M}''r^2 + r^3,$$

and with the coefficients,

XXVII...
$$M = 0$$
, $M' = S\nu^{-1}\psi\nu$, $M'' = m'' - S\nu^{-1}\phi\nu$;

 ψ being a certain auxiliary function (= $m\phi^{-1}$), and m" being the coefficient +

• [Compare the Note to p. 554, vol. i., by which it appears that this function is self-conjugate only when *n* in the equation $df\rho = nS\nu d\rho$ is a constant or a function of $f\rho$ (see also 410, (16.)). As an example, if we take $n = T\nu$ and write $dU\nu = \theta d\rho$, equation II. of the present article becomes $R^{-1}d\rho + \theta d\rho = 0$. Thus the principal curvatures are two roots of the cubic of θ , and the tangents to the lines of curvature are two of the solutions of $Vd\rho d\rho = 0$. We can see that the third root is zero because $SU\nu\delta U\nu = 0$ or for any value of $\delta\rho$, $S\delta\rho\theta'U\nu = 0$. So $\theta'U\nu = 0$, and therefore a root of the conjugate θ is also zero. If then the symbolic cubic of θ is $\theta^3 - N''\theta^2 + N'\theta = 0$, we have the following expressions:

$$R_1^{-1} + R_2^{-1} = -N''$$
 and $R_1^{-1}R_2^{-1} = N'$.

We may also write $dU\nu = -Sd\rho\nabla U\nu = \theta d\rho$ where ∇ is Hamilton's operator, and from the properties of this operator it is not hard to see that

$$R_{1}^{-1} + R_{2}^{-1} = S \nabla U \nu$$
 and $R_{1}^{-1} R_{2}^{-1} = \frac{1}{2} S V \nabla \nabla' V U \nu U \nu'$,

where the accents are to be omitted when the operations indicated have been performed. The function Φ introduced in this sub-article is closely analogous to the function θ of this Note.]

[†] Compare the Note to page 237, continued in page 238. The reason of the evanescence of the coefficient M, or of the occurrence of a null root of the cubic, is that we have here $\Phi \phi^{-1} \nu = 0$, so that the symbol $\Phi^{-1}0$ may represent an actual vector (comp. 351). Geometrically, this corresponds to the circumstance that when we pass, along a semidiameter prolonged, from a surface of the second order to another surface of the same kind, concentric, similar, and similarly placed, the direction of the normal does not change.

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analogous to M'', in the cubic derived from the function ϕ itself. The root r = 0 is foreign to the present inquiry; but the two curvatures, R_1^{-1} , R_2^{-1} , are the two roots of the following quadratic in R^{-1} , obtained from the equation XXVI. by the rejection of that foreign root:

XXVIII. . . 0 =
$$(R^{-1}T\nu)^2 + M''R^{-1}T\nu + M'.$$

(11.) As a first application of this general equation XXVIII., let $\phi \tau$ have again, as in V., the form $g\tau + V\lambda\tau\mu$; we shall then have the values,

XXIX...
$$M'' = 2(g + S\lambda U\nu \cdot S\mu U\nu),$$

and

XXX...
$$M' = (g + S\lambda U\nu \cdot S\mu U\nu)^2 - (V\lambda U\nu)^2 (V\mu U\nu)^2$$

= a great variety of transformed expressions; and the two resulting curvatures agree with those assigned by VII.

(12.) As a second application, let the surface be central of the second order, with *abc* for its scalar semiaxes (real or imaginary); then the *symbolical cubic* (350) in ϕ becomes,

XXXI...
$$0 = \phi^3 - m'' \phi^2 + m' \phi - m = (\phi + a^{-2}) (\phi + b^{-2}) (\phi + c^{-2});$$

and the coefficients of the quadratic XXVIII. in R^{-1} take the values, in which N denotes the semidiameter of the surface in the direction of the normal:

XXXII...
$$R_1^{-1} + R_2^{-1} = -M'''Tv^{-1} = -(m'' + f'Uv)P = (a^{-2} + b^{-2} + c^{-2} - N^2)P;$$

XXXIII... $R_1^{-1}R_2^{-1} = M'Tv^{-2} = -mv^{-4} = a^{-2}b^{-2}c^{-2}P^4;$

both of which agree with known results, and admit of elementary verifications.*

(13.) In general, if we observe that $m'' - \phi = \chi$ (350, XVI.), we shall see that the quadratic XXVIII. in r (or in $R^{-1}T_{\nu}$) may be thus written :

XXXIV... $0 = S\nu^{-1}(r^2\nu + r\chi\nu + \psi\nu);$

or thus more briefly (comp. 398, LXXIX.),

XXXV... $0 = S\nu^{-1}(\phi + r)^{-1}\nu$.

 $f\alpha + f\beta + f\gamma = \text{const.} = c_1 + c_2 + c_3 = a^{-2} + b^{-2} + c^{-2}.$

^{*} As an easy verification by quaternions of the expression XXXII., it may be remarked (comp. 408, (27.)), that if α , β , γ be any three rectangular unit lines, then

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(14.) Accordingly, the formula XXV. gives the expression,

$$\mathbf{XXXVI.} \ldots \mathbf{\nu}^2 \mathbf{\tau} = (\mathbf{\phi} + r)^{-1} \mathbf{\nu} \cdot \mathbf{S} \mathbf{\tau} \mathbf{\phi} \mathbf{\nu} ;$$

from which, under the condition $S_{\nu\tau} = 0$, the equation XXXV. follows at once.

(15.) We have therefore generally, for the product of the two principal curvatures of sections of any surface at any point, the expression:

XXXVII...
$$R_1^{-1}R_2^{-1} = r_1r_2T\nu^{-2} = -\nu^{-4}S\nu\psi\nu = -S\frac{1}{\nu}\psi\frac{1}{\nu};$$

which contains an important theorem of Gauss, whereto we shall presently proceed.

(16.) Meanwhile we may remark that the recent analysis shows, that the squares a_1^2 , a_2^2 (7.) of the semiaxes of the index-curve are generally the roots of the following equation,

XXXVIII. . . 0 =
$$S\nu(\phi + a^{-2})^{-1}\nu$$
,

when developed as a quadratic in a².

(17.) And that the same quadratic assigns the squares of the semiaxes of a diametral section, made by a plane $\perp \nu$, of the central surface of the second order which has $S_{\rho\phi\rho} = 1$ for its equation.

(18.) Accordingly, $\nabla \rho \phi \rho$ has the direction of a tangent to this surface, which is perpendicular to ρ at its extremity; and therefore the vector,

XXXIX...
$$\sigma = \rho^{-1} \nabla \rho \phi \rho = \phi \rho - \rho^{-1} = (\phi - \rho^{-2}) \rho$$
,

is perpendicular to the plane of the diametral section, which has the semidiameter ρ for a semiaxis: so that it is perpendicular also to ρ itself. The equation,

XL...
$$S\sigma(\phi - \rho^{-2})^{-1}\sigma = 0$$
,

assigns therefore the values of the squares $(-\rho^2)$ of the scalar semiaxes of the central section $\perp \sigma$; which agrees with the formula XXXVIII.

(19.) If then a surface be derived from a given central surface of the second order, as the locus of the extremities of normals (erected at the centre) to the diametral sections of the given surface, each such normal (when real) having the length of one of the semiaxes of that section, the equation of this new surface* (or locus) will admit of being written thus:

XLI...
$$S\rho(\phi - \rho^{-2})^{-1}\rho = 0.$$

* When the given surface is an *ellipsoid*, this *derived* surface XLI. is therefore the celebrated *Wave Surface* of Fresnel, which will be briefly mentioned somewhat farther on.

(20.) The first of the values XXIV., for the auxiliary scalar r, gives the expression (if $\nu = \phi \rho$, as it is for a central surface of the second order),

XLII...
$$\sigma = \rho + r^{-1}\nu = (1 + r^{-1}\phi)\rho = r^{-1}(\phi + r)\rho;$$

whence, by inversion, and operation with ϕ ,

XLIII...
$$\rho = r(\phi + r)^{-1}\sigma$$
; XLIV... $\nu = r(\phi + r)^{-1}\phi\sigma$;

and therefore, because $S\rho\nu = 1$,

XLV...
$$r^{-2} = S((\phi + r)^{-1}\sigma \cdot (\phi + r)^{-1}\phi\sigma) = S \cdot \sigma(\phi + r)^{-2}\phi\sigma.$$

(21.) The following is a quite different way of arriving at this result, which is also useful for other purposes. Considering σ as the vector os of a point s on the *Surface of Centres*, that is, on the *locus* of all the centres of curvature of principal normal sections, the vector (say v) of the *Reciprocal Surface* is connected with σ (comp. 373, (21.)) by the equations of reciprocity,* XLVI... $S\sigma v = Sv\sigma = 1$; XLVII... $Svd\sigma = 0$; XLVIII... $S\sigma dv = 0$; which are all satisfied by the vector expression,

XLIX. . .
$$v = \frac{\tau}{S\rho\tau}$$
,

where τ is, as before, a tangent to the line of curvature: so that, if ω denote the variable vector of the normal plane to this last curve, the equation of that plane (comp. 369, IV.) may be thus written,

L. . .
$$Su(\omega - \rho) = 0$$
.

This normal plane, to the line of curvature at r, is therefore at the same time the tangent plane to the surface of centres at s, as indeed it is known to be, from simple geometrical considerations, independently of the form of the given surface, which remains here entirely arbitrary.

$$\mathrm{d}\sigma = \mathrm{d}R_1 \cdot \mathrm{U}\nu, \quad \delta\sigma = \delta\rho + \delta(R_1\mathrm{U}\nu) = (1 - R_1R_2^{-1})\nu\mathrm{d}\rho + \delta R_1 \cdot \mathrm{U}\nu;$$

so that we have both $\mathrm{Sd}\rho\mathrm{d}\sigma = 0$, and $\mathrm{Sd}\rho\delta\sigma = 0$, and therefore the tangent $\mathrm{d}\rho$ or τ to the given line of curvature has the direction of the normal v to the corresponding sheet of the surface of centres, as is otherwise visible from geometry. And when we have thus found an equation of the form $tv = \tau$, operation with S. σ gives by XLVI. the value $t = \mathrm{S}\rho\tau$, as in XLIX., because $\sigma - \rho \parallel \nu \perp \tau$.

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^{*} It is understood that $d\sigma$ and $d\nu$, in the differential equations XLVII., XLVIII., are in general only obliged to have directions *tangential* to the surface of centres, and to its reciprocal, at corresponding points: so that the equations might be in some respects more clearly written thus, $S\nu\delta\sigma = 0$, $S\sigma\delta\nu = 0$, the mark d being reserved to indicate changes which arise from motion along a given line of curvature, while δ should have a more general signification. Accordingly if, in particular, we write $\delta\rho = \nu d\rho$, for a variation answering to motion along the other line, and denote the two radii of curvature for the two directions $d\rho$ and $\delta\rho$ by R_1 and R_2 , we shall have by II., $R_1^{-1}d\rho + dU\nu = 0$, $R_2^{-1}\delta\rho + \delta U\nu = 0$, and therefore by I.,

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(22.) The expression XLIX. for v gives generally the relation,

LI...
$$S\rho v = 1$$
;

giving also, by 410, V. and VI., these two other equations,

LII...
$$S_{\nu\nu} = 0$$
, and LIII... $S_{\nu\nu\phi\nu} = 0$,

which are still independent of the form of the given surface.

(23.) But if that surface be a *central quadric*,* then the equation LI. may be thus written,

LIV. . .
$$1 = Sv\phi^{-1}v = Sv\phi^{-1}v;$$

combining which with LII. and LIII., we derive the expressions :

$$LV...\nu = \frac{v^2\phi v - vfv}{v^4 - fv \cdot Fv}; \qquad LVI...\rho = \phi^{-1}v = \frac{v^3 - \phi^{-1}vfv}{v^4 - fv \cdot Fv};$$

wherein $fv = Sv\phi v$, and $Fv = Sv\phi^{-1}v$, as usual.

(24.) Operating with S. ν on this last expression for ρ , and attending to LII. and LIV., we find the following quaternion forms of the Equation of the Reciprocal of the Surface of Centres :

LVII...
$$1 = (S_{\nu\rho} =) \frac{-fv}{v^4 - fv \cdot Fv}$$
 or LVIII... $v^4 = (Fv - 1)fv$;

or

LIX...1 =
$$(Fv - 1) f \frac{1}{v}$$
; or LX... $Fv - \frac{1}{f \frac{1}{v}} = 1$; &c.,

whereof the second, when translated into coordinates, is found to agree perfectly with a known[†] equation of the same reciprocal surface.

(25.) Differentiating the form LX., and observing that

LXI...
$$\left(f\frac{1}{v}\right)^{-1} = \frac{v^4}{fv}$$
, $d \cdot v^4 = 4Sv^3dv$, $dfv = 2S\phi v dv$, $dFv = 2S\phi^{-1}v dv$,

we find, by comparison with XLVI. and XLVIII., the expression :

LXII...
$$\sigma = \phi^{-1}\upsilon - \frac{2\upsilon^3}{f\upsilon} + \frac{\upsilon^4\phi\upsilon}{(f\upsilon)^2};$$
 or LXIII... $\sigma = \phi^{-1}\upsilon + \frac{2\upsilon}{fU\upsilon} + \frac{\phi\upsilon}{(fU\upsilon)^2};$

* Compare the last Note to page 236; see also the use made of this known name "quadric," for a surface of the second order (or degree), in the sub-articles to 399 (pages 159, &c.).

⁺ The equation alluded to, which is one of the *fourth degree*, appears to have been first assigned by Dr. Booth, in a Tract on *Tangential Coordinates* (1840), cited in page 163 of Dr. Salmon's Treatise. See also the Abstract of a Paper by Dr. Booth, in the Proceedings of the Royal Society for April, 1858.

or finally by XLIX., with the recent signification XXIV. of r,

LXIV...
$$\sigma = r^{-2}(\phi + r)^2 \phi^{-1} v$$
, because LXV... $r = f \mathbf{U} \tau = f \mathbf{U} v$:

and, for the same reason, the equation LX. of the *reciprocal surface* may be thus briefly written,

LXVI...
$$Fv + r^{-1}v^2 = 1$$
, while LXVI'... $fv + rv^2 = 0$.

(26.) Inverting the last form for σ , and using again the relation XLVI., we first find for v the expression,

LXVII...
$$v = r^2 (\phi + r)^{-2} \phi \sigma;$$

and then are conducted anew to the equation XLV., or to the following,

LXVIII... $1 = S \cdot \sigma (1 + r^{-1}\phi)^{-2}\phi\sigma.$

(27.) This last equation may also be thus written,

LXIX...
$$1 = S \cdot \sigma (1 + r^{-1}\phi)^{-3} (\phi + r^{-1}\phi^2)\sigma;$$

but by combining XLIII. LI. LXVII. we have,

LXX... 1 =
$$(S\rho v =)S \cdot \sigma (1 + r^{-1}\phi)^{-3}\phi\sigma;$$

hence

LXXI...
$$0 = S \cdot \sigma (1 + r^{-1}\phi)^{-3}\phi^2 \sigma$$
,

a result which may be otherwise and more directly deduced, under the form $S\nu v = 0$ (LII.), from the expressions XLIV. LXVII. for ν and v.

(28.) If we write,

LXXII... $\tau = Ud\rho$, $\tau' = U(\nu d\rho)$, and therefore LXXIII... $\tau \tau' = U\nu$,

 τ and τ' being thus *unit-tangents* to the lines of curvature, the equation III. gives, generally,

LXXIV...
$$0 = \nabla \tau d(\tau \tau') = -d\tau' + \tau S \tau' d\tau$$
, whence LXXIV'... $d\tau' \parallel \tau$;

of which general parallelism of $d\tau'$ to τ , the geometrical reason is (comp. again III.) that a line of curvature on an arbitrary surface is, at the same time, a line of curvature on the developable normal surface which rests upon that line, and to which the vectors τ' or $vd\rho$ are normals.

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(29.) The same substitution LXXIII. for $\mathbf{U}\nu$ gives by II., if we denote by s the arc of a line of curvature, measured from any fixed point thereof, so that (by 380, (7.), &c.),

LXXV...
$$Td\rho = ds$$
, $d\rho = \tau ds$, $D_s\rho = \tau$,

the following general expression for the curvature of the given surface, in the direction τ of the given line, which by LXXIV'. is also that of $d\tau'$:

LXXVI...
$$R^{-1} = S \cdot \tau D_s(\tau \tau') = -S \cdot \tau \tau' D_s \tau = S(U_{\nu}^{-1} \cdot D_s^2 \rho);$$

but $D_s^2 \rho$ is (by 389, (4.)) what we have called the vector of curvature of the line of curvature, considered as a curve in space, and $R^{-1}U\nu$ is the corresponding vector of curvature of the normal section of the given surface, which has the same tangent τ at the given point : hence the latter vector of curvature is (generally) the projection of the former, on the normal ν to the given surface.

(30.) In like manner, if we denote for a moment by $R_{,}^{-1}$ the curvature of the developable normal surface (28.), for the same direction τ , the general formula II. gives, by LXXIV.,

LXXVII...
$$R_{r}^{-1} = \tau D_s \tau' = -S \tau' D_s \tau = S \cdot \tau'^{-1} D_s^2 \rho;$$

the vector $R_{\prime}^{-1}\tau'$ of this new curvature is therefore the projection on the new normal τ' , of the vector of curvature $D_s^2\rho$ of the given line of curvature. But we shall soon see that these two last results are included in one more general,* respecting all plane sections of an arbitrary surface.

(31.) The general parallelism LXXIV'. conducts easily, for the case of a central quadric, to a known and important theorem, which may be thus investigated. Writing, for such a surface,

LXXVIII. . .
$$r = f\tau$$
, $r' = f\tau'$,

so that r retains here its recent signification LXV., and r' is the analogous scalar for the other direction of curvature, we have by LXXIV. the differential,

$$\mathbf{LXXIX...d} \mathbf{r}' = 2\mathbf{S}\phi \mathbf{\tau}' \mathbf{d} \mathbf{\tau}' = 2\mathbf{S}\tau \phi \mathbf{\tau}' \mathbf{S}\mathbf{\tau}' \mathbf{d} \mathbf{\tau} = 0,$$

because $S\tau\phi\tau' = 0$, by 410, XI.

^{*} Namely in Meusnier's Theorem, which can be proved generally by quaternions with about the same ease as the two foregoing cases of it.

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(32.) We have then the relation,

LXXX...
$$f U(\nu d\rho) = f\tau' = r' = \text{const.};$$

that is to say, the square (r'^{-1}) of the scalar semidiameter (D') of the surface, which is parallel to the second tangent (τ') , is constant for any one line of curvature (τ) ; and accordingly (comp. XXII., and the expression 407, LXXI. for $f U_{\nu_1}$), the value of this square is,

LXXXI...
$$(f U \nu d \rho)^{-1} = r'^{-1} = a^2 - a'^2 = b^2 - b'^2 = c^2 - c'^2$$
,

if a', b', c' be the scalar semiaxes of the confocal, which cuts the given quadric (abc) along the line of curvature, whereof the variable tangent is τ .

(33.) This constancy of $f \mathbf{U}_{\nu} d\rho$ may be proved in other ways; for instance, the general equation $S_{\nu} d_{\nu} d\rho = 0$ gives, for a line of curvature on an *arbitrary surface*,

LXXXII. . . $d\nu = \nu S \nu^{-1} d\nu + d\rho S \frac{d\nu}{d\rho}$; LXXXIII. . . $V d\nu d\rho = \nu d\rho S \nu^{-1} d\nu$; and

LXXXIV...S.
$$d\rho\phi(\nu d\rho) = 0$$
, because $d\nu = \phi d\rho$;

while for a central quadric $(f\rho = 1, \phi\rho = \nu)$ it is easy to show that we have also,

LXXXV...
$$\phi(\nu d\rho) = V\rho d\rho f(\nu U d\rho);$$

hence, for such a surface, if we suppose for simplicity that ds or $\mathrm{Td}\rho$ is constant, which gives $\nabla_{\nu} \mathrm{d}^2 \rho \parallel \mathrm{d}\rho$, we have,

LXXXVI...
$$df(\nu d\rho) = 2S(\phi(\nu d\rho), d(\nu d\rho)) = 2S\nu^{-1}d\nu \cdot f(\nu d\rho),$$

a differential equation of the second order, of which a first integral is evidently,

LXXXVII...
$$f(\nu d\rho) = C\nu^2 d\rho^2$$
, or LXXXVII'... $f U(\nu d\rho) = C = const.$

(34.) But we see that the lines of curvature on a central quadric are thus included in a more general system of curves on the same surface, represented by the differential equation LXXXVI., of which the complete integral would involve two constants: and which expresses that the semidiameters parallel to those tangents to the surface, which cross any one such curve at right angles, have a common square, and therefore (if real) a common length, so that (in this case) they terminate on a sphero-conic.*

* Compare the sub-articles (6.) (7.) (8.) to 219, in page 240, vol. i.

ART. 412.] SURFACE OF CENTRES AS AN ENVELOPE.

(35.) Admitting however, as a case of this property, the constancy LXXX. of the scalar lately called r', namely the second root of the quadratic XXXIV. or XXXV., of which the coefficients and the first root r vary, in passing from one point to another of what we may call for the moment a line of first curvature, we have only to conceive r and v to be accented in the equations LXVI. LXVI'., in order to perceive this *theorem*, which perhaps is new:

The Curve^{*} on the Reciprocal (24) of the Surface of Centres of curvature of a central quadric, which answers to the second curvature of that given surface for all the points of a given line of first curvature, or which is itself in a known sense the reciprocal (with respect to the given centre) of the developable normal surface (28.) which rests upon that line, is the intersection of two quadrics; whereof one (LXVI'.) is a cone, concyclic with the given surface $(f_{\rho} = 1)$; while the other (LXVI.) is a surface concyclic with the reciprocal of that given quadric ($F_{\nu} = 1$).

(36.) Again, the scalar Equation of the Surface of Centres (21.) may be said to be the result of the elimination of r^{-1} between the equations LXVIII. and LXXI., whereof the latter is the derivative \dagger of the former with respect to that scalar; we have therefore this theorem:

An Auxiliary Quadric (LXVIII. or XLV.) touches the Second Sheet of the Surface of Centres of a given quadric, along a Quartic Curve, which is the locus of the centres of Second Curvature for all the points of a Line of First Curvature (35.); and (for the same reason) the same auxiliary quadric is circumscribed, along the same quartic, by the Developable Normal Surface (28), which rests on that first line: with permission, of course, to interchange the words first and second, in this enunciation.

* The variable vector of this curve is easily seen (comp. XLIX.) to be,

$$v' = \frac{\tau'}{S\tau'\rho} = \frac{\nu\tau}{S\nu\tau\rho};$$

and the reciprocal surface (21.) or (24.) is by (25.) the locus of this quartic (35.).

+ The analogous relation, between the coordinate forms of the equations, was perhaps thought too obvious to be mentioned, in page 161 of Dr. Salmon's Treatise; or possibly it may have escaped notice, since the quartic curve (36.) is only mentioned there as an *intersection of two quadrics*, which is on the surface of centres, and answers to points of a *line of curvature* upon the given surface. But as regards the possible novelty, even in part, of any such geometrical deductions as those given in the text from the quaternion analysis employed, the writer wishes to be understood as expressing himself with the utmost diffidence, and as most willing to be corrected, if necessary. The power of derivating (or differentiating) any symbolical expression of the form LXVIII., or of any analogous form, with respect to any scalar which it involves explicitly, as if the expression were algebraical, is an important but an easy consequence from the principles of the Section III. ii. 6, which has been so often referred to. (37.) When the arbitrary constant r is thus allowed to take successively all values, corresponding to both systems of lines of curvature, the Surface of Centres is therefore at once the Envelope^{*} of the Auxiliary Quadric LXVIII., and the Locus of the Quartic Curve (36), in which one or other of its two sheets is touched, by that auxiliary quadric in one of its successive states, and also by one of the developable surfaces of normals to the given surface.

(38.) To obtain the vector equation of that envelope or locus we may proceed as follows, using a new expression for σ , in terms of ν or of ρ , which may then be transformed into a function of two independent and scalar variables. Denoting (comp. (32.)) by a_1 , b_1 , c_1 the semiaxes of the confocal which cuts the given surface in the given line of curvature, and by a_2 , b_2 , c_2 those of the other confocal, so that the normals ν_1 , ν_2 to these two confocals have the directions of the tangents τ' , τ lately considered, we have not only the expressions LXXXI. for r'^{-1} , with a'b'c' changed to a_1 , b_1 , c_1 , but also the analogous expressions (comp. 407, LXXI.),

LXXXVIII. . .
$$r^{-1} = a^2 - a_2^2 = b^2 - b_2^2 = c^2 - c_2^2$$
.

We have therefore by XLII., combined with 407, XVI., this very simple expression for σ :

LXXIX...
$$\sigma = (\phi^{-1} + i^{-1})\nu = \phi_2^{-1}\nu = \phi_2^{-1}\phi\rho;$$

containing, in the present notation, and as a result of the present analysis, a known and interesting theorem,[†] on which however we cannot here delay.

(39.) It follows from this last value of σ , combined with the expression 408, LXXXII. for ρ , that we may write,

XC...
$$\sigma = l^{-2} \left(\frac{a^{-1}a_1a_2^3}{a+a'} + \frac{\sqrt{-1}b^{-1}b_1b_2^3}{Vaa'} + \frac{c^{-1}c_1c_2^3}{a-a'} \right),$$

as the sought Vector Equation of the Surface of Centres of curvature of a given quadric (abc); ambiguous signs being virtually included in these three terms,

^{*} Compare the Note immediately preceding.

⁺ Namely Dr. Salmon's theorem (page 161 of his Treatise), that the centres of curvature of a given quadric at a given point are the poles of the tangent plane, with respect to the two confocals. The connected theorem (page 136), respecting the rectilinear locus of the poles of a given plane, with respect to the surfaces of a confocal system, is at once deducible from the quaternion expression 407, XVI. for $\phi^{-1}\nu$, although the theorem did not happen to be known to the present writer, or at least remembered by him, when he investigated that formula of inversion for other applications, of which some have been already given.

ARTS. 412, 413.] VECTOR EQUATION OF SURFACE OF CENTRES. 261

because in the subsequent eliminations^{*} the semiaxes enter only by their squares: while l, a, a' are constants, as in 407, &c., for the whole confocal system, and abc are also constant here, but $a^2 - a_1^2$ and $a^2 - a_2^2$, or r'^{-1} and r^{-1} (38.), are variable, and may be considered to be the two independent scalars of which σ is a vector function.⁺

413. Some brief remarks may here be made, on the connexion of the general formula,

I...
$$S\nu^{-1}(\phi + r)^{-1}\nu = 0,$$
 412, XXXV.

in which $r = R^{-1}T\nu$ (412, XXIV.), and which when developed by the rules of the Section III. ii. 6 takes (comp. 398, LXXIX.) the form of the quadratic,

II. . .
$$r^2 + rS\nu^{-1}\chi\nu + S\nu^{-1}\psi\nu = 0,$$
 412, XXXIV.

with Gauss's[‡] theory of the *Measure of Curvature of a Surface*; and especially with his fundamental result, that this *measure* is equal to the *product of the two principal curvatures of sections* of that surface: a relation which, in our notations, may be thus expressed,

III. . . V.
$$\mathrm{d}\mathbf{U}\nu\delta\mathbf{U}\nu = R_1^{-1}R_2^{-1}\mathrm{V}\mathrm{d}\rho\delta\rho.$$

(1.) As regards the deduction, by quaternions, of the equation III., in which d and δ may be regarded as two§ distinct symbols of differentiation,

$$\sigma = (\Phi + u_1)^{-\frac{1}{2}} (\Phi + u_2)^{\frac{1}{2}} (\Phi + u_3)^{\frac{3}{2}} \epsilon.$$

It may also be shown in various ways that the vector equation of the reciprocal of this surface is

$$v = - (\Phi + u_1)^{\frac{1}{2}} (\Phi + u_2)^{\frac{1}{2}} (\Phi + u_3)^{-\frac{1}{2}} \epsilon.]$$

[‡] The reader is referred to the Additions to Liouville's Monge (pages 505, &c.), in which the beautiful Memoir by Gauss, entitled: *Disquisitiones generales circa superficies curvas*, is with great good taste reprinted in the Latin, from the *Commentationes recentiores* of the Royal Society of Göttingen. He is also supposed to look back, if necessary, to the Section III. ii. 6 of these *Elements* (pages 484, vol. i., &c.), and especially to the deduction in page 486, vol. i., of ψ from ϕ , remembering that the latter function (and therefore also the former) is here self-conjugate.

§ Compare page 553, vol. i., and the Note to page 254.

^{*} The corresponding elimination in coordinates was first effected by Dr. Salmon, who thus determined the equation of the surface of centres of curvature of a quadric to be one of the *twelfth degree*. (Compare pages 161, 162 of his already cited Treatise.)

^{+ [}In the notation of the Note to page 225, the vector to the centre of curvature of the quadric u_1 along its intersection with u_2 is $\sigma = \rho + x(\Phi + u_1)^{-1}\rho$, the value of the scalar x being found by expressing that σ does not change while u_3 in the expression $\rho = \{(\Phi + u_1) (\Phi + u_2) (\Phi + u_3)\}^{\frac{1}{2}} \in$ receives a small increment. This gives at once $\frac{1}{2}(\Phi + u_1 + x)\rho du_3 + (\Phi + u_3)\rho dx = 0$, and therefore $x = u_3 - u_1$. Hence $\sigma = (\Phi + u_1)^{-1} (\Phi + u_3)\rho$, or in terms of ϵ the vector equation of the surface of centres is when u_2 and u_3 are variable

performed with respect to two independent scalar variables, we may observe that, by principles and rules already established,

IV...
$$dU_{\nu} = V \frac{d\nu}{\nu} \cdot U_{\nu}, \quad \delta U_{\nu} = V \frac{\delta \nu}{\nu} \cdot U_{\nu} = -U_{\nu} \cdot V \frac{\delta \nu}{\nu};$$

and that therefore the first member of III. may be thus transformed :

$$\nabla \dots \nabla \dots \nabla \dots \partial U_{\nu} \partial U_{\nu} = \nabla \left(\nabla \frac{\mathrm{d}_{\nu}}{\nu} \dots \nabla \frac{\partial \nu}{\nu} \right) = -\nu^{-1} \mathrm{S} \nu^{-1} \mathrm{d}_{\nu} \partial_{\nu}.$$

(2.) Again, since we have $d\nu = \phi d\rho$ (410, IV., &c.), and in like manner $\delta\nu = \phi\delta\rho$, the relations $S\nu d\rho = 0$, $S\nu\delta\rho = 0$, and the self-conjugate property of ϕ , allow us to write,

VI...
$$Vd\nu\delta\nu = \psi Vd\rho\delta\rho$$
, and VII... $Vd\rho\delta\rho = \nu^{-1}S\nu d\rho\delta\rho$;

whence follows at once by V. the formula III., if we remember the general expression, deduced from the quadratic II.,

VIII...
$$R_1^{-1}R_2^{-1} = -\nu^{-2}r_1r_2 = -S\frac{1}{\nu}\frac{\psi}{\nu}\frac{1}{\nu}$$
. 412, XXXVII.

(3.) If then we suppose that P, P₁, P₂ are any three near points on an arbitrary surface, and that R, R₁, R₂ are three near and corresponding points on the unit sphere, determined by the condition of parallelism of the radii OR, OR₁, OR₂ to the normals PN, P₁N₁, P₂N₂, the two small triangles thus formed will bear to each other the ultimate ratio,

IX... lim.
$$\frac{\Delta RR_1R_2}{\Delta PP_1P_2} = R_1^{-1}R_2^{-1}$$
;

a result which justifies (although by an entirely new analysis) the adoption by Gauss of this *product*^{*} of curvatures of *sections*, as the *measure* of the curvature of the *surface*, with his signification of the phrase.

(4.) As another form of this important product or measure, if we conceive that the vector ρ of the surface is expressed as a function (372) of two independent scalars, t and u, and if we write for abridgment,

X...
$$D_t \rho = \rho', \quad D_u \rho = \rho_i, \quad D^2_t \rho = \rho'', \quad D_t D_u \rho = \rho_i', \quad D_u^2 \rho = \rho_{i,i},$$

[•] If it be supposed to be in any manner known that a *limit* such as IX. exists, or that the *quotient* of the two vector areas in III. is a scalar independent of the directions of PP1, PP2, or of $d\rho$, $\delta\rho$, we have only to assume that these are the directions of the *lines of curvature*, in order to obtain at once, by 412, II. [page 247], the product $R_1^{-1}R_2^{-1}$ as the value of this quotient or limit.

ART. 413.]

which will allow us (comp. 372, V.) to assume for the normal vector v the expression,

XI...
$$\nu = V \rho' \rho_{,}$$

it is easy to prove* that we have generally,

XII...
$$R_1^{-1}R_2^{-1} = S\frac{\rho''}{\nu}S\frac{\rho_{\prime\prime}}{\nu} - \left(S\frac{\rho_{\prime}}{\nu}\right)^2;$$

which takes as a verification the well-known form,

XIII...
$$R_1^{-1}R_2^{-1} = \frac{rt-s^2}{(1+p^2+q^2)^2},$$

when we write (comp. 410, (18.)),

$$\mathbf{XIV}...\rho = ix + jy + kz, \quad \rho' = \mathbf{D}_x\rho = i + kp, \quad \rho_z = \mathbf{D}_y\rho = j + kq;$$
$$\mathbf{XV}...\nu = \mathbf{V}\rho'\rho_z = k - ip - jq, \quad \rho'' = kr, \quad \rho_z = ks, \quad \rho_z = kt.$$

$$\nabla \cdots \nu = \nabla \rho' \rho_{\prime} = k - ip - jq, \quad \rho'' = kr, \quad \rho_{\prime} = ks, \quad \rho_{\prime\prime} = kt.$$

(5.) In general, the equation XII. may be thus transformed,

XVI. . .
$$\nu^4 R_1^{-1} R_2^{-1} = S(\nabla \nu \rho'' \cdot \nabla \nu \rho_{\prime\prime}) - (\nabla \nu \rho_{\prime\prime})^2 + \nu^2 (S \rho'' \rho_{\prime\prime} - \rho_{\prime\prime});$$

also

if

$$XVII... Td\rho^2 = edt^2 + 2fdtdu + gdu^2,$$

whence

XVIII. . .
$$e = -\rho'_{,,}^{2}, f = -S\rho'\rho_{,}, g = -\rho_{,}^{2},$$

XIX. . . $\nu^2 = f^2 - eq$,

and if we still denote, as in X., derivations relatively to t and u by upper and lower accents, we may substitute in the quadruple of the equation XVI. the values,

> XX... $2\nabla v \rho'' = (e_{i} - 2f')\rho' + e'\rho_{i}, \quad 2\nabla v \rho_{i}' = -g'\rho' + e_{i}\rho_{i},$ $2\nabla v \rho_{\mu} = -q \rho' + (2f_{\mu} - q') \rho_{\mu}$

and

XXI...
$$2(S\rho''\rho_{\prime\prime} - \rho_{\prime}'^2) = e_{\prime\prime} - 2f_{\prime}' + g_{\prime\prime}';$$

hence the measure of curvature is an explicit function of the ten scalars,

XXII... $e, f, g; e', f', g'; e_a, f_a, g_i;$ and $e_a - 2f'_a + g''$:

^{*} The quadratic in R^{-1} may be formed by operating on 412, II. with S. ρ' and S. ρ , and then eliminating dt : du.

[III. III. § 7.

and therefore, as was otherwise proved by Gauss, this measure depends only^{*} on the expression (XVII.) of the square of a linear element, in terms of two independent scalars (t, u), and of their differentials (dt, du).

(6.) Hence follow also these two other theorems⁺ of Gauss :--

If a surface be considered as an infinitely thin solid, and supposed to be flexible but inextensible, then every deformation of it, as such, will leave unaltered, Ist, the Measure of Curvature at any Point, and IInd, the Total Curvature of any Area; that is, the area of the corresponding portion of the unit sphere, determined as in (3.) by radii parallel to normals.[‡]

(7.) Supposing now that t and u are geodetic coordinates, whereof the former represents the length of a geodetic AP from a fixed point A of the surface, and the latter represents the angle BAP which this variable geodetic makes at A with a fixed geodetic AB, it is easy to see that the general expression XVII. takes the shorter form,

XXIII... $\mathrm{Td}\rho^2 = \mathrm{d}t^2 + n^2\mathrm{d}u^2$, in which XXIV... $n = \mathrm{T}\rho_{,} = \mathrm{T}\nu$;

so that we have now the values,

XXV... e = 1, f = 0, $g = n^2$, g' = 2nn', $g'' = 2nn'' + 2n'^2$,

and the derivatives of e and f all vanish. And thus the general expression XII. for the *measure of curvature* reduces itself by (5.) to the very simple form,

XXVI...
$$R_1^{-1}R_2^{-1} = -n^{-1}n'' = -n^{-1}D_t^2n$$
;

in which n is generally a function of both t and u, although here twice derivated with respect to the former only.

* The proof by quaternions, above given, of this exclusive dependence, is perhaps as simple as the subject will allow, and is somewhat shorter than the corresponding proof in the *Lectures*; in page 605 of which is given however the equation,

which may now be deduced at sight from XVI., by the substitutions XIX. XX. XXI., and differs only in notation from the equation of Gauss (Liouville's Monge, page 523, or Salmon, page 309).

† See page 524 of Liouville's Monge.

‡ [If q is a quaternion or versor function of the two scalars t and u, and if $d\varpi = qd\rho q^{-1}$ is the differential of a vector function of t and u, the squares of the linear elements $d\varpi$ and $d\rho$ are identical. The surfaces described by ρ and ϖ correspond point to point, and the measure of curvature at any point on one surface is equal to that at the corresponding point on the other. Under these circumstances the surfaces are *applicable*. To find the condition to be satisfied by q, we express that $d\varpi$ is a differential of a function of t and u by equating $D_t D_u \varpi = D_u D_t \varpi$. This gives in the notation of the text a partial differential equation for q

$$q'\rho_i q^{-1} - q\rho_i q^{-1} q' q^{-1} = q_i \rho' q^{-1} - q\rho' q^{-1} q_i q^{-1}, \text{ or } V.V q^{-1} q'. \rho_i = V.V q^{-1} q_i \cdot \rho'.$$

ART. 413.] DEFORMATION OF A SURFACE.

(8.) The point P being denoted by the symbol (t, u), and any other point P' of the surface by $(t + \Delta t, u + \Delta u)$, we may consider the two connected points P₁, P₂, of which the corresponding symbols are $(t + \Delta t, u)$ and $(t, u + \Delta u)$; and then the quadrilateral PP₁P'P₂, bounded by two portions PP₁, P₂P' of geodetic lines from A, and (as we may suppose) by two arcs PP₂, P₁P' of geodetic circles round the same fixed point, will have its area ultimately = $n\Delta t\Delta u$ (by XXIII.), and therefore (by XXVI., comp. (3.), (6.)) its total curvature ultimately = $-n''\Delta t\Delta u$, or $= -\Delta_t n'$. Δu , when Δt and Δu diminish together, by an approach of P' to P.

(9.) Again, in the immediate neighbourhood of A, we have n = t, n' = 1; changing then $-\Delta_t n'$ to $-d_t n'$, and integrating with respect to t from t = 0, we obtain 1 - n' as the coefficient of Δu in the result, and are thus conducted to the expression:

XXVII. . . Total Curvature of Triangle APP' = $(1 - n')\Delta u$, ultimately,

if AP, AP' be any two geodetic lines, making with each other a small angle = Δu , and if PP' be any small arc (geodetic or not) on the same surface.

(10.) Conceive then that PQ is a *finite arc* of any curve upon the surface, for which therefore t, and consequently n', may be conceived to be a function of u; we shall have this other expression of the same kind,

XXVIII. . . Total Curvature of Area APQ = $\int (1 - n') du = \Delta u - \int n' du$;

the area here considered being bounded by the two geodetic lines AP, AQ, which make with each other the finite angle Δu , and by the arc PQ of the arbitrary curve.

(11.) If this curve be *itself* a *geodetic*, and if we treat its coordinates t, u, and its vector ρ , as functions of its arc, s, then the second differential of ρ , namely,

XXIX...
$$d^2\rho = \rho' d^2t + \rho_1 d^2u + \rho'' dt^2 + 2\rho_1' dt du + \rho_1 du^2$$
,

must be normal to the surface at P, and consequently perpendicular to ρ' and $\rho_{,.}$ Operating* therefore with S. ρ' , and attending to the relations XVIII. and XXV., which give

XXX. . .
$$\rho'^2 = -1$$
, $S\rho'\rho_{\prime} = S\rho'\rho'' = S\rho'\rho_{\prime} = 0$, $S\rho'\rho_{\prime\prime} = -S\rho_{\prime}\rho_{\prime} = nn'$,

^{*} To operate with S. ρ , would give a result not quite so simple, but reducible to the form XXXI., with the help of $d^2s = 0$.

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we obtain the differential equation,

XXXI... $d^2t = nn'du^2$, or XXXII... dv = -n'du,

if we observe that we may write,

XXXIII. . .
$$dt = \cos v ds$$
, $n du = \sin v ds$,

because

$$XXXIV...dt^2 + n^2 du^2 = ds^2;$$

v being here the variable angle, which the geodetic PQ makes at P with AP prolonged.

(12.) Substituting then for -n'du, in XXVIII., its value dv given by XXXII., the integration becomes possible, and the result is $\Delta u + \Delta v$; where Δu is still the angle at A, and $\pi + \Delta v = (\pi - v) + (v + \Delta v)$ is the sum of the angles at P and Q, in the geodetic triangle APQ.

(13.) Writing then B and c instead of P and Q, we thus arrive at another most remarkable Theorem* of Gauss, which may be expressed by the formula:

XXXV... Total Curvature of a Geodetic Triangle ABC = $A + B + C - \pi$,

= what may be called the Spheroidal Excess; A, B, C, in the second member, being used to denote the *three angles* of the triangle: and the *total surface* of the *unit sphere* (= 4π) being represented by 720°, when the *part* corresponding to the geodetic triangle is thus represented by the angular excess, A + B + C - 180°.

(14.) And it is easy to perceive, on the one hand, how this theorem admits of being *extended*, as it was by Gauss, to all geodetic polygons: and on the other hand, how it may require to be *modified*, as it was by the same eminent geometer, so as to give what would on the same plan be called a *spheroidal defect*, when the *measure of curvature* is *negative*, as it is for surfaces (or parts of surfaces) of which the principal sections have their curvatures *oppositely directed*.

414. The only sections of a surface, of which the curvatures have been above determined, are the *two principal normal sections* at any proposed point; but the general expressions of III. iii. 6 may be applied to find the curvature of *any plane section*, normal or oblique, and therefore also of *any curve* on a

^{*} The enunciation of this theorem, respecting which its illustrious discoverer justly says, "Hoc theorema, quod, ni fallimur, ad elegantissima in theoria superficierum curvarum referendum esse videtur," . . . is given in page 533 of the Additions to Liouville's Monge. A proof by quaternions was published in the *Lectures* (pages 606-609, see also the few preceding pages), but the writer conceives that the one given above will be found to be not only shorter, but more clear.

ABTS. 413, 414.] TOTAL CURVATURE, SPHEROIDAL EXCESS.

given surface, when only its osculating plane is known. Denoting (as in 389, &c.) by ρ and κ the vectors of the given point P, and of the centre K of the osculating circle at that point, and by s the arc of the curve, we have generally (by 389, XII. and VI.),

I. . . Vector of Curvature of Curve =
$$\mathbf{KP}^{-1} = (\rho - \kappa)^{-1} = \mathbf{D}_s^2 \rho = \frac{1}{\mathrm{d}\rho} \nabla \frac{\mathrm{d}^2 \rho}{\mathrm{d}\rho}$$
;

the independent variable in the last expression being arbitrary. And if we denote by σ and ξ the vectors of the points s and x, in which the *axis* of the osculating circle meets respectively the *normal* and the *tangent plane* to the given surface, we shall have also, by the right-angled triangles, the general decomposition, $KP^{-1} = SP^{-1} + XP^{-1}$ (as vectors), or

II. . .
$$D_s^2 \rho = (\rho - \kappa)^{-1} = (\rho - \sigma)^{-1} + (\rho - \xi)^{-1};$$

where the two components admit of being transformed as follows :

III. . . Normal Component of Vector of Curvature of Curve (or Section)

$$= (\rho - \sigma)^{-1} = \nu^{-1} S \frac{\mathrm{d}\nu}{\mathrm{d}\rho} = (\rho - \sigma_1)^{-1} \cos^2 v + (\rho - \sigma_2)^{-1} \sin^2 v$$

= Vector of Normal Curvature of Surface for the direction of the given tangent;

 σ_1 , σ_2 being the vectors of the centres s_1 , s_2 (comp. 412) of the two principal curvatures, and v being the angle at which the curve (or its tangent $d\rho$) crosses the first line of curvature (or its tangent τ_1), while σ is the vector of the centre s of the sphere which is said to osculate to the surface, in the given direction (of $d\rho$); and

IV. . . Tangential Component of Vector of Curvature $= (\rho - \xi)^{-1} = \nu^{-1}d\rho^{-1}S\nu d\rho^{-1}d^{2}\rho$ = Vector of Geodetic Curvature of Curve (or Section);

this latter vector being here so called, because in fact its tensor represents what is known by the name of the geodetic* curvature of a curve upon a surface: the independent variable being still arbitrary.

* The name, "courbure géodésique," was introduced by M. Liouville, and has been adopted by several other mathematical writers. Compare pages 568, 575, &c. of his Additions to Monge.

ELEMENTS OF QUATERNIONS.

[III. m. § 7.

(1.) As regards the decomposition II., if a, β be any two rectangular vectors on, ob, and if $\gamma = oc =$ the perpendicular from o on AB, then (comp. 316, L., and 408, XLI.),

$$\mathbf{V}...\gamma^{-1}=\frac{\beta}{\mathbf{V}a\beta}+\frac{a}{\mathbf{V}\beta a}=a^{-1}+\beta^{-1}.$$

(2.) To prove the first transformation III., we have, by I. and II., observing that $dS\nu d\rho = 0$,

VI. . .
$$\frac{\nu}{\rho - \sigma} = S \frac{\nu}{\rho - \kappa} = S \cdot \frac{\nu}{d\rho} \nabla \frac{d^2 \rho}{d\rho} = \frac{-S \nu d^2 \rho}{d\rho^2} = \frac{S d \nu d \rho}{d\rho^2} = S \frac{d \nu}{d\rho}$$

(3.) Hence, by 412, (7.), if we denote the vector III. of normal curvature by $R^{-1}U_{\nu}$, we have the general expressions (comp. 412, I. XXI.),

VII... $\sigma = \rho + R \mathbf{U} \nu$, $R = D^2 \cdot \mathbf{T} \nu$, with VIII... $\mathbf{T} \nu = P^{-1}$,

for the case of a central quadric; D being generally the semidiameter of the index surface (410, (9.), &c.), or for a quadric the semidiameter of that surface itself, which has the direction of the tangent (or of $d\rho$): and P being, for the latter surface, the perpendicular from the centre on the tangent plane, as in some earlier formulæ.

(4.) To deduce the second transformation III., which contains a theorem of Euler, let τ , τ_1 , τ_2 denote unit tangents to the section and the two lines of curvature, so that

IX... $\tau = \tau_1 \cos v + \tau_2 \sin v$, and $\tau^2 = \tau_1^2 = \tau_2^2 = -1$;

we may then write generally (comp. 412, IV.),

X...
$$R^{-1}T\nu = \frac{\nu}{\sigma - \rho} = -S \frac{d\nu}{d\rho} = -S\tau^{-1}\phi\tau = S\tau\phi\tau,$$

and shall have the values (comp. 410, XI.),

XI... $S\tau_1\phi\tau_1 = R_1^{-1}T\nu$, $S\tau_2\phi\tau_2 = R_2^{-1}T\nu$, $S\tau_1\phi\tau_2 = S\tau_2\phi\tau_1 = 0$; whence

XII...
$$R^{-1} = R_1^{-1} \cos^2 v + R_2^{-1} \sin^2 v$$
,

and the required transformation is accomplished.

(5.) The theorem of Meusnier may be considered to be a result of the elimination (2.) of $d^2\rho$ from the expressions for the normal component III. of

ART. 414.] CURVATURES OF SECTIONS, OSCULATING SPHERE. 269

what we may call the Vector $D_s^2 \rho$ of Oblique Curvature; and it may be expressed by the equation,

XIII...
$$S \frac{\rho - \sigma}{\rho - \kappa} = 1$$
, or XIII'... $S \frac{\sigma - \kappa}{\rho - \kappa} = 0$,

which gives

XIII"... pks =
$$\frac{\pi}{2}$$
,

if it be now understood that the point s, of which σ is the vector, is the centre of the circle which osculates to the normal section; or of the sphere which osculates in the same direction to the surface, as will be more clearly seen by what follows.

(6.) In general, if $\rho + \Delta \rho$ be the vector of any second point P' of the given surface, the equation

XIV... S
$$\frac{\nu}{\omega - \rho} = S \frac{\nu}{\Delta \rho}$$
, with ω for a variable vector,

represents rigorously the sphere which *touches* the surface at the given point P, and passes *through* the second point P'; conceiving then that the latter point *approaches* to the former, and observing that the development* by Taylor's Series of the equation $f\rho = \text{const.}$ gives (if $d_f\rho = 2S_\nu d\rho$, and $d\nu = \phi d\rho$),

XV... $0 = \Delta \rho^{-2} \Delta / \rho = 2S \frac{\nu}{\Delta \rho} + S \frac{\phi \Delta \rho}{\Delta \rho} + \text{terms which vanish generally with } \Delta \rho$,

even if they be not always null, we are conducted in a new way, by the known conception of the Osculating Sphere for a given direction to a surface, to the same centre s, and radius R, as before: the equation of this sphere being,

XVI...
$$S \frac{2\nu}{\omega - \rho} = \left(\lim S \frac{2\nu}{\Delta \rho} = -\lim S \frac{\phi \Delta \rho}{\Delta \rho} = \right) - S \frac{d\nu}{d\rho}.$$

^{*} Compare Art. 374, and the second Note to page 20. The occasional use, there mentioned, of the differential symbol $d\rho$ as signifying a finite and *chordal vector*, in the development of $f(\rho + d\rho)$, has appeared obscure, in the *Lectures*, to some friends of the writer; and he has therefore aimed, for the sake of clearness, in at least the *text* of these *Elements*, and especially in the geometrical applications, to confine that symbol to its *first* signification (100, 369, 373, &c.), as denoting a *tangential vector* (finite or infinitely small, and to a curve or surface): ρ itself being generally regarded as a *vector function*, and *not* as an independent variable (comp. 362, (3.)).

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(7.) Conversely, if we assume a radius R, such that R^{-1} is algebraically intermediate between R_1^{-1} and R_2^{-1} , the tangent sphere,

XVII...
$$S \frac{2\nu}{\omega - \rho} = \frac{T\nu}{R}$$
, or XVII'... $S \frac{2U\nu}{\omega - \rho} = R^{-1}$,

will cut the surface in two directions of osculation, assigned by the formula XII.; but if R^{-1} be outside those limits, there will be only contact, and not any (real) intersection, at least in the vicinity of P.

(8.) If P' be again, as in (6.), any second point of the surface, and if we denote for a moment by (Π) and (Σ) the normal plane PNP' and the normal section corresponding, we may suppose that n is the point in which the normals to the plane curve (Σ) at P and P' intersect; and if we then erect a perpendicular at N to the plane (II), it will be crossed by every perpendicular at P' to the tangent P'T' to the section, and therefore in particular by the normal at P' to the surface, in a point which we may call N': so that the line P'N is the projection, on the plane PP'N, of this second normal P'N' to the surface. Conceiving then the plane (II) to be fixed, but the point P' to approach indefinitely to P, we see that the centre s of curvature of the normal section (Σ) , which is also by (6.) the centre of the osculating sphere to the surface for the same direction, is the limiting position of the point N, in which the given normal at P is intersected by the projection* of the near normal p'N', on the given normal plane.

(9.) The two components III. and IV are included in the binomial expression,

XVIII. . . Vector of Oblique Curvature (or of Curvature of Oblique Section) $= (\rho - \kappa)^{-1} = \nu^{-1} \mathrm{Sd} \nu \mathrm{d} \rho^{-1} + \nu^{-1} \mathrm{d} \rho^{-1} \mathrm{S} \nu \mathrm{d} \rho^{-1} \mathrm{d}^2 \rho,$

which is obtained by substituting in I. the general equivalent 409, XXI. for $d^2\rho$, and in which (as before) the independent variable is arbitrary; and the tangential component IV. may be otherwise found by observing that, by I. and II.,

XIX. . .
$$\frac{\nu d\rho}{\rho - \xi} = S \frac{\nu d\rho}{\rho - \kappa} = S \frac{\nu d^2 \rho}{d\rho} = -S \nu d\rho^{-1} d^2 \rho,$$

- $(\nu d\rho)^{-1} = \nu^{-1} d\rho^{-1}, \text{ because } S \nu d\rho = 0.$

and that

^{*} The reader may compare the calculations and constructions, in pages 600, 601 of the Lectures. In the language of infinitesimals, an infinitely near normal r'N' intersects the axis of the osculating circle, to the given normal section.

AET. 414.7 VECTOR OF GEODETIC CURVATURE, DIDONIAS.

(10.) Another way of deducing the same component IV., is to resolve the following system of three scalar equations, which by the geometrical definition of the point x the vector ξ must satisfy:

XX... $S(\xi - \rho)\nu = 0$; $S(\xi - \rho)d\rho = 0$; $S(\xi - \rho)d^2\rho = d\rho^2$;

and which give,

XXI... $\xi - \rho = \frac{\nu \mathrm{d} \rho^3}{\mathrm{S} \nu \mathrm{d} \rho \mathrm{d}^2 \rho} = \frac{\nu \mathrm{d} \rho}{\mathrm{S} \nu \mathrm{d} \rho^{-1} \mathrm{d}^2 \rho},$

or $(\rho - \xi)^{-1} = \&c.$, as before. We have also the transformations,

XXII... Vector of Geodetic Curvature =
$$(\rho - \xi)^{-1}$$

= $(\nu d\rho)^{-1} S(\nu U d\rho . dU d\rho) = -\nu d\rho S \frac{d\rho^{-2} d^2 \rho}{\nu d\rho} = \&c.$

(11.) The definition of the point x shows also easily, that if a developable surface (D) be circumscribed to a given surface (S), along a given curve (C), and if, in the unfolding of the former surface, the point x be carried with the tangent plane, originally drawn to the latter surface at P, it will become the centre of curvature, at the new point (P), to the new or plane curve (C') obtained by this development : so that the radius (PX) of geodetic curvature is equal, as indeed it is known* to be, to the radius of plane curvature of the developed curve.

(12.) This plane curve (c') is therefore a circle \dagger (or part of one) if the condition,

XXIII...
$$\overline{\mathbf{Px}} = \mathbf{T} (\boldsymbol{\xi} - \boldsymbol{\rho}) = \text{const.},$$

* Compare page 576 of the Additions to Liouville's Monge.

† The curves on any given surface, which thus become circles by development, have also the isoperimetrical property expressed in quaternions (comp. the Note to page 48) by the formula,

$$XXVI...\int S(U\nu \cdot d\rho\delta\rho) + c\delta\int Td\rho = 0,$$

which conducts to the differential equation,

XXVII... $c^{-1}d\rho = V.U\nu dUd\rho$ (comp. 380, IV. [page 29]),

and in which the scalar constant c can be shown to have the value,

XXVIII... $c = (\xi - \rho)U$. $\nu d\rho = \pm T(\xi - \rho) = Radius of Geodetic Curvature,$

= radius of developed circle; and each such curve includes, by XXVI., on the given surface, a *maximum area* with a *given perimeter*: on which account, and in allusion to a well-known classical story, the writer ventured to propose, in page 582 of the *Lectures*, the *name* "Didonia" for a curve of this kind, while acknowledging that the *curves themselves* had been discovered and discussed by M. Delaunay.

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be satisfied; but it degenerates into a *right line*, if this radius of *geodetic* curvature be *infinite*, that is, if

XXIV...
$$T(\rho - \xi)^{-1} = 0$$
, or XXV... $S\nu d\rho d^2\rho = 0$,

or finally (by 380, II., comp. 409, XXV.), if the original curve (c) be a *geodetic line* on the *given surface* (s), and therefore also on the *developable* (D) : which agrees with the fundamental property (382, 383) of geodetics on a developable surface.

(13.) Accordingly it may be here observed that the general formula IV., combined with the notations and calculations of 382, conducts to the expression $(z + v') T\rho'^{-1}$, or $\frac{zdx + dv}{ds}$, for the geodetic curvature of any curve on a developable surface, whereof the element ds crosses a generating line at the variable angle v, while zdx is the angle between two such consecutive lines: a result easily confirmed by geometrical considerations, and agreeing with the differential equation z + v' = 0 (382, IX.) of geodetics on a developable.

415. We shall conclude the present Section with a few supplementary remarks, including a new and simplified proof of an important *theorem* (354), which we have had frequent occasion to employ for purposes of *geometry*, and which presents itself often in *physical* applications of quaternions also: namely, that *if the linear and vector function* ϕ *be self-conjugate*, then the *Vector Quadratic*,

$$\mathbf{I}...\nabla\rho\phi\rho=0,\qquad\qquad 354,\,\mathbf{I}.$$

represents generally a System of Three Real and Rectangular Directions; and that these (comp. 405, (1.), (2.), &c.) are the directions of the Axes of the Central Surfaces of the Second Order, which are represented by the scalar equation,

II. . .
$$S\rho\phi\rho = \text{const.}$$
;

or more generally,

III. . . $S\rho\phi\rho = C\rho^2 + C'$, where C and C' are any two scalar constants.

(1.) It is an easy consequence of the theory (350) of the symbolic and cubic equation in ϕ , that if c be a root of the derived algebraical cubic M = 0 (354), and if we write $\Phi = \phi + c$ (as in that Article), the new linear and vector function Φ_P must be reducible to the binomial form (351),

IV... $\Phi \rho = \phi \rho + c \rho = \beta S a \rho + \beta' S a' \rho$, with $\nabla ... \nabla \beta a + \nabla \beta' a' = 0$,

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as the condition (353, XXXVI.) of self-conjugation. With this condition we may then write,

$$\nabla I...\beta = Aa + Ba', \quad \beta' = A'a' + Ba;$$

and it is easy to see that no essential generality is lost, by supposing that a and a' are two rectangular vector units, which may be turned about in their own plane, if β and β' be suitably modified : so that we may assume,

VII. . . $a^2 = a'^2 = -1$, Saa' = 0; whence VIII. . . $\Phi a = -\beta$, $\Phi a' = -\beta'$, and IX. . . $\nabla \beta' a' = Baa' = -\nabla \beta a$, $\nabla \beta a' = Aaa'$, $\nabla \beta' a = -A'aa'$.

(2.) The equation I., under the form,

X... $\nabla \rho \Phi \rho = 0$, is satisfied by **XI**... $\phi \rho = 0$, or **XII**... $\nabla a a' \rho = 0$; and it cannot be satisfied otherwise, unless we suppose,

XIII...
$$\rho = xa + x'a'$$
, and XIV... $\nabla(x\beta + x'\beta') (xa + x'a') = 0$;
that is, by IX.,
XV... $B(x'^2 - x^2) + (A - A')xx' = 0$:

while conversely the expression XIII. will satisfy I., under this condition XV. But this quadratic in x' : x, of which the coefficients B and A - A' do not generally vanish, has necessarily *two real roots*, with a product = -1; hence there *always exists*, as asserted, a system of *three real and rectangular directions*, such as the following,

XVI...
$$xa + x'a'$$
, $x'a - xa'$, and aa' (or Vaa'),

which satisfy the equation I.; and this system is generally definite; which proves the first part of the Theorem.

(3.) The lines a, a' may be made by (1) to *turn* in their own plane, till they coincide with the two first directions XVI.; which will give,

XVII... B = 0, $\beta = Aa$, $\beta' = A'a'$,

and therefore,

XVIII...
$$\phi \rho = -c\rho + AaSa\rho + A'a'Sa'\rho$$

= $(c + A) aSa\rho + (c + A') a'Sa'\rho + caa'Saa'\rho;$

and thus the scalar equation II. will take the form,

XIX. . . $S\rho\phi\rho = (c + A) (Sa\rho)^2 + (c + A') (Sa'\rho)^2 + c (Saa'\rho)^2 = const.,$ Hamilton's Elements of Quaternions, Vol. II. 2 N

[III. III. § 7.

which represents generally a central surface of the second order, with its three axes in the three directions a, a', aa' of ρ ; and does not cease to represent such a surface, and with such axes, when for $S\rho\phi\rho$ we substitute, as in III., this new expression :

XX...
$$S\rho\phi\rho - C\rho^2 = S\rho\phi\rho + C\left((Sa\rho)^2 + (Sa'\rho)^2 + (Saa'\rho)^2\right) = C' = \text{const.};$$

the second surface being in fact concyclic (or having the same cyclic planes) with the first, and the new term, $-C\rho$, in $\phi\rho$, disappearing under the sign V. ρ : so that the second part of the Theorem is proved anew.

(4.) It would be useless to dwell here on the cases, in which the surfaces XIX., XX. come to be of revolution, or even to be spheres, and when consequently the directions of their axes, or of ρ in I., become partially or even wholly indeterminate. But as an example of the reduction of an equation in quaternions to the form I., without its at first presenting itself under that form, we may take the very simple equation,

XXI... $\rho\iota\rho\kappa = \iota\rho\kappa\rho$, with κ not $||\iota|$,

which may be reduced (comp. 354, (12.)) to

XXII. . .
$$\nabla \cdot \rho \nabla \iota \rho \kappa = 0$$
;

and which is accordingly satisfied (comp. 373, XXIX.) by the three rectangular directions,

XXIII... $U_{\ell} - U_{\kappa}$, $V_{\ell\kappa}$, $U_{\ell} + U_{\kappa}$,

of the axes (abc) of the ellipsoid,

XXIV...
$$T(\iota \rho + \rho \kappa) = \kappa^2 - \iota^2$$
, 282, XIX.

which is one of the surfaces of the concyclic system (comp. III.),

XXV...
$$S_{l\rho\kappa\rho} = C\rho^2 + C'$$
,

as appears from the transformations 336, XI., &c.

(5.) In applying the theorem thus recently proved anew, we have on several occasions used the expression,

XXVI...
$$d\nu = \phi d\rho$$
, 410, IV.

in which ν is a vector normal to a surface whereof ρ is the variable vector, and the function ϕ is treated as *self-conjugate* (363).

ART. 415.] CONDITION OF INTEGRABILITY, FACTOR.

(6.) It is, however, important to remark that, in order to justify the assertion of this last property, the following *expression of integral form*,

XXVII... $\int S_{\nu} d\rho$,

must admit of being equated to some scalar function of ρ , such as $\frac{1}{2}f\rho$ + const., without its being assumed that ρ itself is a function, of any determinate form, of a scalar variable, t. The self-conjugation of the linear and vector function ϕ in XXVI., is the condition of the existence of the integral XXVII., considered as representing such a scalar function (comp. again 363).

(7.) There are indeed several investigations, in which it is sufficient to regard ν as denoting some normal vector, of which only the direction is important, and which may therefore be multiplied by an arbitrary scalar coefficient, constant or variable, without any change in the results (comp. the calculations respecting geodetic lines, in the Section III. iii. 5, and many others which have already occurred).

(8.) And there have been other general investigations, such as those regarding the *lines of curvature* on an arbitrary surface, in which $d\nu$ was treated as a self-conjugate function of $d\rho$, while yet (comp. 410, (17.)) the fundamental differential equation $S\nu d\nu d\rho = 0$ was not affected by any such multiplication of ν by n.

(9.) But there are questions in which a factor of this sort may be introduced, with advantage for some purposes, while yet it is inconsistent with the self-conjugation above mentioned, unless the multiplier n be such as to render the new expression $\text{Snvd}\rho$ (comp. XXVII.) an exact differential of some scalar function of ρ .

(10.) For example, in the theory of *Reciprocal Surfaces* (comp. 412, (21.)), it is convenient to employ the system of the *three* connected equations,

XXVIII. . . $S_{\nu\rho} = 1$, $S_{\nu}d\rho = 0$, $S_{\rho}d\nu = 0$; 373, L. LI.

but when the length of ν is determined so as to satisfy the first of these equations, ν^{-1} being then the vector perpendicular from the origin on the tangent plane to the given but arbitrary surface of which ρ is the vector, while ρ^{-1} is the corresponding perpendicular for the reciprocal surface with ν for vector, the differential d ν loses generally its self-conjugate character, as a linear and vector function of d ρ : although it retains that character if the scalar function $f\rho$ be homogeneous, in the equation $f\rho = \text{const.}$ of the original surface, as it is for the

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case of a central quadric,* for which $\nu = \phi \rho$, $d\nu = \phi d\rho$, &c., as in former Articles.

(11.) In fact, the introduction of the first equation XXVIII. is equivalent to the multiplication of ν by the factor $n = (S\nu\rho)^{-1}$; and if we write (comp. 410, (16.)),

XXIX... $df\rho = 2S\nu d\rho$, $d\nu = \phi d\rho$, $dn = S\sigma d\rho$,

we shall have this new pair of conjugate linear and vector functions,

XXX...d. $n\nu = \Phi d\rho = n\phi d\rho + \nu S\sigma d\rho$, XXXI... $\Phi' d\rho = n\phi d\rho + \sigma S\nu d\rho$;

and these will not be equal generally, because we shall not in general have $\sigma \parallel \nu$. But this last parallelism exists in the case of homogeneity (10.), because we have then the relations,

$$XXIII...2S\nu\rho = rf\rho, \quad d. n^{-1} = dS\nu\rho = rS\nu d\rho,$$

if r be the number which represents the dimension of $f\rho$ (supposed to be whole).

(12.) On the other hand it may happen, that the differential equation $Svd\rho = 0$ represents a surface, or rather a set of surfaces, without the expression $Svd\rho$ being an exact differential, as in (6.); and then there necessarily exists a scalar factor, or multiplier, n, which renders it such a differential.

(13.) For example the differential equation,

XXXIII... $S_{\gamma\rho}d\rho = S_{\nu}d\rho = 0$, with XXXIV... $\nu = V_{\gamma\rho}$, $d\nu = V_{\gamma}d\rho = \phi d\rho$,

represents an arbitrary plane (or a set of planes), drawn through a given line γ ; but the expression S $\gamma \rho d\rho$ itself is not an exact differential, and the integral XXVII. represents no scalar function of ρ , with the present form of ν , of which the differential $d\nu$ is accordingly a linear function $\phi d\rho$, which is not conjugate to itself, but to its opposite (comp. 349, (4.)), so that we have here $\phi' d\rho = -\phi d\rho$.

(14.) But if we multiply v by the factor,

XXXV... $n = \nu^{-2} = (\nabla \gamma \rho)^{-2}$, which gives XXXVI... $dn = S \sigma d\rho$, $\sigma = 2n^{-2} \gamma \nabla \gamma \rho$,

^{*} It was for this reason that the symbol T_{ν} was not interpreted generally as denoting the reciprocal, P^{-1} , of the length of the perpendicular from the origin on the tangent plane, in the formulæ of 410, 412, 414 : although, in several of those formulæ, as in an equation of 409, (3.), that symbol was so interpreted, for the case of a central surface of the second order.

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and therefore $S\gamma\sigma = 0$, $S\rho\sigma = -2n$, then the new normal vector $n\nu$, or ν^{-1} , is found to have the self-conjugate differential,

XXXVII... d.
$$n\nu = d \cdot \nu^{-1} = -\nu^{-1} \nabla \gamma d\rho \cdot \nu^{-1} = \Phi d\rho = \Phi' d\rho$$
;

and accordingly the new expression,

XXXVIII...
$$Sn\nu d\rho = S\nu^{-1}d\rho = S\frac{d\rho}{\nabla\gamma\rho}$$
, with γ constant,

is easily seen to be an exact differential, namely (if $T\gamma = 1$), that of the angle which the plane of γ and ρ makes with a fixed plane through γ : so that, when ν is thus changed to $n\nu$, the integral in XXVII. acquires a geometrical signification, which is often useful in physical applications, since it then represents the change of this angle, in passing from one position of ρ to another; or the angle through which the variable plane of $\gamma\rho$ has revolved.

(15.) In fact, the general formula 335, XV. for the differential of the angle of a quaternion gives, if we write

XXXIX.
$$q = \frac{\nabla \gamma \rho}{\nabla \gamma \rho_0}, \quad \gamma = \text{const.}, \quad \rho_0 = \text{const.}, \quad \mathbf{T} \gamma = \mathbf{1},$$

the two connected expressions :

$$\mathbf{XL.} \, . \, . \, \mathbf{d} \angle q = \pm \, \mathbf{S} \, \frac{\mathrm{d} \rho}{\mathbf{V} \gamma \rho}; \qquad \mathbf{XLI.} \, . \, . \, . \, \int \mathbf{S} \, \frac{\mathrm{d} \rho}{\mathbf{V} \gamma \rho} = \pm \, \Delta \angle \left(\mathbf{V} \gamma \rho : \mathbf{V} \gamma \rho_0 \right);$$

which contain the above-stated result, and can easily be otherwise established.

(16.) In general, if the linear and vector function $d\nu = \phi d\rho$ be not selfconjugate, and if the function $d \cdot n\nu = \Phi d\rho$ be formed from it as in (11.), it results from that sub-article, and from 349, (4.), that we may write,

XLII...
$$(\phi - \phi')d\rho = 2\nabla \gamma d\rho, \quad (\Phi - \Phi')d\rho = 2\nabla \gamma d\rho,$$

with the relation,

XLIII.
$$2\gamma_{\nu} = 2n\gamma + \nabla \nu \sigma;$$

where γ , γ , are *independent* of $d\rho$, although they may depend on ρ *itself*. If then the *new* linear function $\Phi d\rho$ is to be *self-conjugate*, so that $\gamma_{,} = 0$, we must have

XLIV...
$$2n\gamma + \nabla \nu \sigma = 0$$
, and therefore **XLV...** $S\gamma \nu = 0$;

which latter very simple equation, not involving either n or σ , is thus a form,

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in quaternions, of the Condition of Integrability^{*} of the differential equation $S_{\nu}d\rho = 0$, if the vector γ be deduced from ν as above.

(17.) The Bifocal Transformation of $S\rho\phi\rho$, in 360, (2.), has been sufficiently considered in the present Section (III. iii. 7); but it may be useful to remark here, that the *Three Mixed Transformations* of the same scalar function $f\rho$, in the same series of sub-articles, include virtually the whole known theory of the Modular and Umbilicar Generations of Surfaces of the Second Order.⁺

(18.) Thus, in the formulæ of 360, (4), if we make e = 1, ϵ is the vector of an *Umbilicar Focus* of the surface $f\rho = 1$, and ζ is the vector of a point on the *Umbilicar Directrix* corresponding; whence the *umbilicar focal conic* and *dirigent cylinder* (real or imaginary) can be deduced, as the *loci* of this *point* and *line*.

(19.) Again, by making e_1 and e_3 each = 1, in the formulæ of 360, (6.), we obtain *Two Modular Transformations* of the equation of the same surface; ϵ_1 , ϵ_3 being vectors of *Modular Foci*, in two distinct planes, and ζ_1 , ζ_3 being vectors of points upon the *Modular Directrices* corresponding: whence the modular focal conics, and dirigent cylinders (real or imaginary), are found by easy eliminations.

(20.) Thus, by assuming that either

XLVI. . .
$$S\lambda(\rho - \zeta_1) = 0$$
, $S\lambda(\rho - \zeta_3) = 0$,

or

$$XLVII...S\mu(\rho-\zeta_1)=0, \quad S\mu(\rho-\zeta_3)=0,$$

* If the proposed equation be

$$S\nu d\rho = pdx + qdy + rdz = 0$$
, so that $\nu = -(ip + jq + kr)$,

we easily find that $2\gamma = iP + jQ + kR$, where

$$P = D_z q - D_y r$$
, $Q = D_z r - D_z p$, $R = D_y p - D_x q$;

the condition of integrability XLV. becomes therefore here,

$$pP + qQ + rR = 0$$
, which agrees with known results.

[In terms of the operator ∇ , the condition is $S\nu\nabla\nu = 0$. For if $nS\nu d\rho = df\rho = -Sd\rho\nabla$. $f\rho$ is true for all differentials $d\rho$, we must have $\nabla f\rho = -n\nu$. Operating on this by ∇ and remembering that ∇^2 is scalar, $\nabla^2 f\rho = -n\nabla\nu - \nabla n \cdot \nu$ gives, on operating by $S\nu$, the condition as stated above.]

+ [The formula of the three mixed transformations are

$$S\rho\phi\rho = g\left(\rho - \epsilon\right)^2 + 2S\lambda\left(\rho - \zeta\right)S\mu\left(\rho - \zeta\right) + e, \qquad 360, V11.$$

$$S\rho\phi\rho = g_1(\rho - \epsilon_1)^2 + (S\lambda_1(\rho - \zeta_1))^2 + (S\mu_1(\rho - \zeta_1))^2 + e_1, \qquad XVI$$

and

$$S_{\rho}\phi_{\rho} = g_{3}(\rho - \epsilon_{3})^{2} - (S_{\lambda_{3}}(\rho - \zeta_{3}))^{2} - (S_{\mu_{3}}(\rho - \zeta_{3})^{2} + \epsilon_{3}, \qquad XVII.$$

with obvious conditions for homogeneity in ρ . See pages 545, 546, vol. i.]

ART. 415.] MODULAR AND UMBILICAR GENERATIONS.

the equations 360, XVI., XVII. may be brought to the forms,

XLVIII. . . $(\rho - \epsilon_1)^2 = m_1^2 (\rho - \zeta_1)^2$, **XLIX.** . . $(\rho - \epsilon_3)^2 = m_3^2 (\rho - \zeta_3)^2$, with the values,

L. . .
$$m_1^2 = 1 - \frac{c^2}{c_1}$$
, and LI. . . $m_3^2 = 1 - \frac{c^2}{c_3}$;

in which c_1 , c_2 , c_3 are the *three roots* of a certain *cubic* (M = 0), or the *inverse squares* of the three scalar *semiaxes* (real or imaginary) of the surface, arranged in algebraically ascending order (357, IX., XX.; 405, (6.), &c.): and m_1 , m_3 are the *two* (real or imaginary) *Moduli*, or represent the *modular ratios*, in the *two modes of Modular Generation** corresponding.

(21.) It is obvious that an equation of the form,

LII. . .
$$T\phi\rho = C = \text{const.}$$

represents a central quadric, if $\phi \rho$ be any linear; and vector function of ρ , of the kind considered in the Section III. ii. 6, whether self-conjugate or not; but it requires a little more attention to perceive, that an equation of this other form,

LIII. . .
$$T(\rho - \nabla . \beta \nabla \gamma a) = T(a - \nabla . \gamma \nabla \beta \rho),$$

represent such a surface, whatever the three vector constants a, β, γ may be. The discussion of this last form would present some circumstances of interest, and might be considered to supply a new mode of generation, on which however we cannot enter here.

* MacCullagh's rule of modular generation, which includes both those modes, was expressed in page 437 of the *Lectures* by an equation of the form,

$$\mathbf{T}\left(\boldsymbol{\rho}-\boldsymbol{\alpha}\right)=\mathbf{T}\mathbf{V}\cdot\boldsymbol{\gamma}\mathbf{V}\boldsymbol{\beta}\boldsymbol{\rho}\,;$$

in which the origin is on a directrix, β is the vector of another point of that right line, α is the vector of the corresponding focus, γ is perpendicular to a directive (that is, generally, to a cyclic) plane, ρ is the vector of any point P of the surface, and $\pm S\beta\gamma$ is the constant modular ratio, of the distance \overline{AP} of P from the focus, to the distance of the same point P from the directrix on, measured parallel to the directive plane. The new forms (360), above referred to, are however much better adapted to the working out of the various consequences of the construction; but it cannot be necessary, at this stage, to enter into any details of the quaternion transformations: still less need we here pause to give references on a subject so interesting, but by this time so well known to geometers, as that of the modular and umbilicar generations of surfaces of the second order. But it may just be noted, in order to facilitate the applications of the formulæ L. and LI., that if we write, as usual, for all the central quadrics, $a^2 > b^2 > c^2$, whether b^2 and c^2 be positive or negative, then the roots c_1 , c_2 , c_3 coincide, for the ellipsoid, with a^{-2} , b^{-2} , c^{-2} , a^{-2} , (comp. page 206).

+ In page 226 the notation,

$$\mathrm{l} f \rho = 2 \mathrm{S} \nu \mathrm{d} \rho = 2 \mathrm{S} \phi \rho \mathrm{d} \rho, \qquad 409, \, \mathrm{IV}.$$

was employed for an arbitrary surface; but with the understanding that this function $\phi \rho$ (comp. 363)

(22.) The surfaces of the second order, considered hitherto in the present Section, have all had the *origin* for *centre*. But if, retaining the significations of ϕ , f, and F, we compare the two equations,

LIV. . .
$$f(\rho - \kappa) = C$$
, and LV. . . $f\rho - 2S_{\epsilon\rho} = C'$,

we shall see (by 362, &c.) that the constants are connected by the two relations,

LVI...
$$\varepsilon = \phi \kappa$$
, $C' = C - f \kappa = C - S \varepsilon \kappa = C - F \varepsilon$;

so that the equation,

LVII...
$$f\rho - 2S\epsilon\rho = f(\rho - \phi^{-1}\epsilon) - F\epsilon$$
,

is an *identity*.

(23.) If then we meet an equation of the form LV., in which (as has been usual) we have still $f\rho = S\rho\phi\rho = a$ scalar and homogeneous function of ρ , of the second dimension, we shall know that it represents generally a surface of that order, with the expression (comp. 347, IX., &c.),

LVIII...
$$\kappa = \phi^{-1} \varepsilon = m^{-1} \psi \varepsilon = Vector of Centre.$$

(24.) It may happen, however, that the two relations,

LIX...
$$m = 0$$
, $T\psi \varepsilon > 0$,

exist together; and then the centre may be said to be at an infinite distance, but in a definite direction: and the surface becomes a Paraboloid, elliptic or hyperbolic, according to conditions which are easy consequences from what has been already shown.

(25.) On the other hand it may happen that the two equations,

LX...
$$m = 0$$
, $\psi \varepsilon = 0$,

are satisfied together; and then the vector κ of the centre acquires, by LVIII., an *indeterminate value*, and the surface becomes a *Cylinder*, as has been already sufficiently exemplified.

was generally non-linear. It may be better, however, as a general rule, to avoid writing $\mathbf{v} = [\phi p]$, except for central quadrics; and to confine ourselves to the notation $d\mathbf{v} = \phi d\rho$, as in some recent and several earlier sub-articles, when we wish, for the sake of association with other investigations and results, to treat the function ϕ as linear (or distributive); because we shall thus be at liberty to treat the surface as general, notwithstanding this property of ϕ . As regards the methods of generating a quadric, it may be worth while to look back at the Note to page 204, respecting the Six Generations of the Ellipsoid, which were given by the writer in the Lectures, with suggestions of a few others, as interpretations of quaternion equations,

ART. 415.] CUBIC CONE, SCREW SURFACE, SKEW CENTRE.

(26.) It would be tedious to dwell here on such details; but it may be worth while to observe, that the general equation of a Surface of the Third Degree may be thus written :

LXI...
$$Sq\rho q'\rho q''\rho + S\rho\phi\rho + S\gamma\rho + C = 0;$$

C and γ being any scalar and vector constants; $\phi \rho$ any linear, vector, and self-conjugate function; and q, q', q'' any three constant quaternions: while ρ is, as usual, the variable vector of the surface.

(27.) In fact, besides the one scalar constant, C, three are included in the vector γ , and six others in the function ϕ (comp. 358); and of the ten which remain to be introduced, for the expression of a scalar and homogeneous function of ρ , of the third degree, the three versors Uq, Uq', Uq'' supply nine (comp. 312), and the tensor T. qq'q'' is the tenth.

(28.) And for the same reason the monomial equation,

LXII. . .
$$Sq\rho q'\rho q''\rho = 0$$
,

with the same significations of q, q', q'', represents the general Cone of the Third Degree, or Cubic Cone, which has its vertex at the origin of vectors.

(29.) If then we combine this last equation with that of a secant plane, such as $S_{\epsilon\rho} + 1 = 0$, we shall get a quaternion expression for a *Plane Cubic*, or *plane curve of the third degree*: and if we combine it with the equation $\rho^2 + 1 = 0$ of the unit-sphere, we shall obtain a corresponding expression for a *Spherical Cubic*,* or for a curve upon a spheric surface, which is cut by an arbitrary great circle in *three pairs* of *opposite points*, real or imaginary.

(30.) Finally, as an example of sections of surfaces, represented by transcendental equations, let us consider the Screw Surface, or Helicoid, \dagger of which the vector equation may be thus written (comp. the sub-arts. to 314):

LXIII... $\rho = c(x+a)a + ya^{x}\gamma$, with Ta - 1, $\gamma = Va\beta$, and y > 0;

^{*} Compare the Note to page 38, vol. i.; see also the *theorem* in that page, which contains perhaps a new mode of *generation* of cubic curves in a given plane; or, by an easy modification, of the corresponding curves upon a sphere.

[†] Already mentioned in pages 419, vol. i., 12, 28, 85. The condition y > 0 answers to the supposition that, in the generation of the surface, the perpendiculars from a given helix on the axis of the cylinder are not prolonged beyond that axis.

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a being the unit axis, while β , γ are two other constant vectors, a, c two scalar constants, and x, y two variable scalars.

(31.) Cutting this surface by the plane of $\beta\gamma$, or supposing that

LXIV...
$$0 = S_{\gamma}\beta_{\rho} = \beta^{2}S_{\alpha\rho} - S_{\alpha}\beta S_{\beta}\beta_{\rho}$$
, and writing LXV... $c = bS_{\alpha}\beta_{\rho}$,

we easily find that the scalar and vector equations of what we may call the *Screw Section* may be thus written :

LXVI...
$$b(x + a) = yS \cdot a^{x-1}$$
; LXVII... $\rho = y(\gamma S \cdot a^x - \beta S \cdot a^{x-1})$

(32.) Derivating these with respect to x, and eliminating β and y', we arrive at the equation,

LXVIII...
$$\rho = (x + a)\rho' + z\gamma$$
, if LXIX... $2bz = \pi y^2$;

but $z\gamma$ in LXVIII. is the vector of the point, say G, in which the tangent to the section at the point (x, y), or P, intersects the given line γ , namely the line in the plane of that section which is perpendicular to the axis a: we see then, by LXIX., that this point of intersection depends only on the constant, b, and on the variable, y, being independent of the constant, a, and of the variable, x.

(33.) To interpret this result of calculation, which might have been otherwise found with the help of the expression 372, XII. (with β changed to γ) for the normal ν to a screw-surface, we may observe, first, that the equation LXVII., which may be written as follows,

LXX... $\rho = y \nabla a^{x+1} \beta$, and gives LXXI... $\nabla a \rho = y T \gamma$,

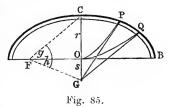
would represent an *ellipse*, if the coefficient y were treated as *constant*; namely, the section of the right *cylinder* LXXI. by the *plane* LXIV.; the *vector semiaxes* (major and minor) of this ellipse being $y\beta$ and $y\gamma$ (comp. 314, (2.)).

(34.) By assigning a new value to the constant a, we pass to a new screw surface (30.), which differs only in position from the former, and may be conceived to be formed from it by sliding along the axis a; while the value of x, corresponding to a given y, will vary by LXVI., and thus we shall have a new screw section (31.), which will cross the ellipse (33.) in a new point q: but the tangent to the section at this point will intersect by (32.) the minor axis of the ellipse in the same point q as before.

ARTS. 415, 416.]

(35.) We shall thus have a Figure^{*} such as the following (fig. 85.); in which if \mathbf{F} be a *focus* of the ellipse BC, and G (as above) the *point* of

convergence of the tangents to the screw sections at the points \mathbf{P} , \mathbf{Q} , &c., of that ellipse, it is easy to prove, by pursuing the same analysis a little farther, Ist, that the angle (g), subtended at this focus \mathbf{F} by the minor semiaxis oc, which is also a radius (r) of the cylinder LXXI., is equal to the inclination of the axis (a) of that



cylinder to the *plane* of the ellipse, as may indeed be inferred from elementary principles; and IInd, what is less obvious, that the *other angle* (h), subtended at the same focus (F) by the interval oG, or by what may be called (with reference to the present construction, in which it is supposed that b < 0, or that the angles made by $D_x\rho$ and β with a are either *both acute*, or *both obtuse*) the *Depression* (s) of the Skew Centre (G), is equal to the inclination of the same axis (a) to the *helix* on the same cylinder, which is obtained (comp. 314, (10.)) by treating y as constant, in the equation LXIII. of the Screw Surface.

SECTION 8.

On a few Specimens of Physical Application of Quaternions, with some Concluding Remarks.

416. It remains to give, according to promise (368), before concluding this work, some examples[†] of *physical applications* of the present Calculus: and as a first specimen, we shall take the *Statics of a Rigid Body*.

(1.) Let $a_1, \ldots a_n$ be *n* Vectors of Application, and let β_1, \ldots, β_n be *n* corresponding Vectors of Force, in the sense that *n* forces are applied at the points $A_1, \ldots A_n$ of a free but rigid system, and are represented as usual by so many right lines from those points, to which lines the vectors $OB_1, \ldots OB_n$ are equal, though drawn from a common origin; and let γ (= oc) be the vector

^{*} Those who are acquainted, even slightly, with the theory of Oblique Arches (or skew bridges), will at once see that this fig. 85 may be taken as representing rudely such an arch: and it will be found that the construction above deduced agrees with the celebrated *Rule of the Focal Excentricity*, discovered practically by the late Mr. Buck. This application of Quaternions was alluded to, in page 620 of the *Lectures*.

⁺ The reader may compare the remarks on hydrostatic pressure, in pages 483, 484, vol. i.

of an arbitrary point c of space. Then the Equation* of Equilibrium of the system or body, under the action of these n applied forces, may be thus written :

I. . . $\Sigma \nabla (a - \gamma)\beta = 0$; or thus, I'. . . $\nabla \gamma \Sigma \beta = \Sigma \nabla \alpha \beta$.

(2.) The supposed *arbitrariness* (1.) of γ enables us to break up the formula I. or I'., into the *two* vector equations:

II. . .
$$\Sigma \beta = 0$$
; III. . . $\Sigma V \alpha \beta = 0$;

of each of which it is easy to assign, as follows, the physical signification.

(3.) The equation II. expresses that if the forces, which are applied at the points A_1 . of the body, were all *transported* to the origin o, their statical resultant, or vector sum, would be zero.

(4.) The equation III. expresses that the resultant of all the *couples*, produced in the usual way by such a transference of the applied forces to the assumed origin, is *null*.

(5.) And the equation I., which as above includes both II. and III., expresses that if all the given forces be transported to any common point c, the couples hence arising will balance each other: which is a sufficient condition of equilibrium of the system.

(6.) When we have only the relation,

IV... $S(\Sigma\beta . \Sigma V \alpha\beta) = 0$,

without $\Sigma\beta$ vanishing, the applied forces have then an Unique Resultant = $\Sigma\beta$, acting along the line of which I. or I'. is the equation, with γ for its variable vector.

(7.) And the physical interpretation of this condition IV. is, that when the forces are transported to 0, as in (3.) and (4.) the resultant force is in the plane of the resultant couple.

(8.) When the equation II., but not III., is satisfied, the applied forces compound themselves into One Couple, of which the $Axis = \Sigma V \alpha \beta$, whatever may be the position of the origin.

(9.) When neither II. nor III. is satisfied, we may still propose so to place the auxiliary point c, that when the given forces are transferred to it,

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^{*} We say here, "equation": because the single quaternion formula, I. or I'., contains virtually the six usual scalar equations, or conditions, of the equilibrium at present considered.

ART. 416.]

as in (5.), the resultant force $\Sigma\beta$ may have the direction of the axis $\Sigma V(a-\gamma)\beta$ of the resultant couple, or else the opposite of that direction; so that, in each case, the condition,*

V... V
$$\frac{\Sigma V(\alpha - \gamma)\beta}{\Sigma \beta} = 0,$$

shall be satisfied by a suitable limitation of the auxiliary vector γ .

(10.) This last equation V. represents therefore the *Central Axis* of the given system of applied forces, with γ for the variable vector of that right line: or the *axis* of the *screw-motion* which those forces *tend* to produce, when they are *not in balance*, as in (1.), and neither tend to produce *translation alone*, as in (6.), nor *rotation alone*, as in (8.).†

(11.) In general, if q be an auxiliary quaternion, such that

$$VI. \dots q\Sigma\beta = \Sigma V \alpha\beta,$$

its vector part, ∇q , is equal by $(\nabla \cdot)$ to the Vector-Perpendicular, let fall from the origin on the central axis; while its scalar part, Sq, is easily proved to be the quotient,[‡] of what may be called the Central Moment, divided by the Total Force: so that $\nabla q = 0$ when the central axis passes through the origin, and Sq = 0 when there exists an unique resultant.

(12.) When the total force $\Sigma\beta$ does not vanish, let Q be a new auxiliary quaternion, such that

VII...
$$Q = \frac{\Sigma \alpha \beta}{\Sigma \beta} = q + \frac{\Sigma S \alpha \beta}{\Sigma \beta},$$

with

VIII...
$$c = SQ = Sq$$
, and IX... $\gamma = oc = VQ$,

for its scalar and vector parts; then $c \Sigma \beta$ represents, both in quantity and in direction, the Axis of the Central Couple (9.), and γ is the vector of a point c which is on the central axis (10.), considered as a right line having situation in space: while the position of this point on this line depends only on the given system of applied forces, and does not vary with the assumed origin o.

V'. . . $T\Sigma V(\alpha - \gamma)\beta = a$ minimum,

+ [In the expressive language of Sir Robert S. Ball the forces constitute a wrench upon a screw.]

^{*} The equation V. may also be obtained from the condition,

when γ is treated as the only variable vector; which answers to a known property of the Central Moment.

[[]This scalar has been aptly termed by Sir Robert Stawell Ball the pitch of the screw.]

[III. m. § 8.

(13.) Under the same conditions, we have the transformations,

X...
$$\Sigma \alpha \beta = (c + \gamma) \Sigma \beta$$
; XI... $T \Sigma \alpha \beta = (c^2 - \gamma^2)^{\frac{1}{2}} T \Sigma \beta$;

XII...
$$\Sigma \nabla a\beta = c\Sigma\beta + \nabla\gamma\Sigma\beta$$
; XIII... $(\Sigma \nabla a\beta)^2 = c^2(\Sigma\beta)^2 + (\nabla\gamma\Sigma\beta)^2$;

whereof XII. contains the known *law*, according to which the *axis* of the *couple* (4.), obtained by transferring all the forces to an assumed point o, *varies* generally in *quantity* and in *direction* with the *position* of that point : while XIII. expresses the known corollary from that law, in virtue of which the *quantity alone*, or the *energy* $(T \le V \alpha \beta)$ of the couple here considered, is the same for all the points o of any one *right cylinder*, which has the *central axis* of the system for its *axis of revolution*.

(14.) If we agree to call the quaternion product PA.AA' the quaternion moment, or simply the Moment, of the applied force AA' at A, with respect to the Point P, the quaternion sum $\sum \alpha \beta$ in X. may then be said to be the Total Moment of the given system of forces, with respect to the assumed origin o; and the formula XI. expresses that the tensor of this sum, or what may be called the quantity of this total moment, is constant for all points o which are situated on any one spheric surface, with the point c determined in (12.) for its centre : being also a minimum when o is placed at that point c itself, and being then equal to what has been already called the central moment, or the energy of the central couple.

(15.) For these and other reasons, it appears not improper to call generally the point c, above determined, the *Central Point*, or simply the *Centre*, of the given system of applied forces, when the total force does not vanish; and accordingly in the particular but important case, when all those forces are *parallel*, without their sum being zero, so that we may write,

XIV...
$$\beta_1 = b_1\beta_1$$
, ... $\beta_n = b_n\beta_1$, $T\Sigma\beta > 0$,

the scalar c in (12.) vanishes, and the vector γ becomes (comp. Art. 97 on bary-centres),

XV... oc =
$$\gamma = \frac{b_1a_1 + \ldots + b_na_n}{b_1 + \ldots + b_n} = \frac{\Sigma ba}{\Sigma b};$$

so that the point c, thus determined, is independent of the common direction β , and coincides with what is usually called the Centre of Parallel Forces.

ARTS. 416, 417.] GENERAL EQUATION OF DYNAMICS.

(16.) The conditions of equilibrium (1.), which have been already expressed by the formula I., may also be included in this other quaternion equation,

XVI... Total Moment = $\sum \alpha \beta$ = a scalar constant,

of which the value is independent of the origin; and which, with its sign changed represents what may perhaps be called the *Total Tension* of the system.*

(17.) Any infinitely small change, in the position of a rigid body, is equivalent to the alteration of each of its vectors a to another of the form,

XVII. . .
$$a + \delta a = a + \epsilon + V \iota a$$
,

 ϵ and ι being two arbitrary but infinitesimal vectors, which do not vary in the passage from one point Λ of the body to another \dagger : and thus the conditions of equilibrium (1.) may be expressed by this other formula,

XVIII.
$$\sum S\beta \delta a = 0$$
,

which contains, for the case here considered, the Principle of Virtual Velocities, and admits of being extended easily to other cases of Statics.

417. The general Equation of Dynamics may be thus written,

I. . .
$$\Sigma m S (D_t^2 a - \xi) \delta a = 0$$
,

with significations of the symbols which will soon be stated; but as we only propose (416) to give here some *specimens* of physical application, we shall aim chiefly, in the following sub-articles, at the deduction of a few formulæ and theorems, respecting *Axes* and *Moments* of *Inertia*, and subjects therewith connected.

(1.) In the formula I., a is the vector of position, at the time t, of an element m of the system; δa is any variation of that vector, geometrically compatible with the mutual connexions between the parts of that system;

† [Compare pages 83-85, and observe that the transformation

$$\boldsymbol{\epsilon} = \boldsymbol{\epsilon} \boldsymbol{\iota}^{-1} \cdot \boldsymbol{\iota} = (\mathrm{S} \boldsymbol{\epsilon} \boldsymbol{\iota}^{-1} + \mathrm{V} \boldsymbol{\epsilon} \boldsymbol{\iota}^{-1}) \boldsymbol{\iota} = (p + \varpi) \boldsymbol{\iota}, \ (p = \mathrm{S} \boldsymbol{\epsilon} \boldsymbol{\iota}^{-1}, \ \varpi = \mathrm{V} \boldsymbol{\epsilon} \boldsymbol{\iota}^{-1})$$

shows that the displacement of the body may be accomplished by a rotation round the axis whose equation is $\rho = \varpi + \pi i$, accompanied by a proportional translation along that axis. This screw translation is called a *twist* by Sir Robert Ball. In the same way a moving body is said to have a twist-velocity on an instantaneous screw.]

^{* [}This of course is what Clausius has since called the virial.]

ELEMENTS OF QUATERNIONS.

[III. III. § 8.

the vector $m\xi$ represents a moving force, or ξ an accelerating force, which acts on the element *m* of mass; D and S are marks, as usual, of derivating and taking the scalar; and the summation denoted by Σ extends to all the elements, and is generally equivalent to a triple integration, or to an addition of triple integrals in space. And the formula is obtained (comp. 416, (17.)), by a combination of D'Alembert's principle with the principle of virtual velocities, which is analogous to that employed in the *Mécanique Analytique* by Lagrange.

(2.) For the case of a *free* but *rigid body*, we may substitute for δa the expression $\epsilon + V_{\iota a}$, assigned by 416, XVII.; and then, on account of the arbitrariness of the two infinitesimal vectors ϵ and ι , the formula I. breaks up into the two following,

II...
$$\Sigma m(D_t^2 a - \xi) = 0$$
; III... $\Sigma m \nabla a(D_t^2 a - \xi) = 0$;

which correspond to the two statical equations 416, II. and III., and contain respectively the law of motion of the centre of gravity, and the law of description of areas.

(3.) If the body have a *fixed point*, which we may take for the origin o, we eliminate the reaction at that point, by attending only to the equation III.; and may then express the connexions between the elements m by the formula,

IV... $D_t a = V_t a$, whence $V... D_t^2 a = \iota V_t a - V a D_t \iota$;

 ι being the Vector-Axis of instantaneous Rotation of the body, in the sense that its versor U_{ι} represents the direction of the axis, and that its tensor T_{ι} represents the angular velocity, of such rotation at the time t.

(4.) By V., the equation III. becomes,

VI...
$$\sum maVaD_{t} = \sum m(V_{t}aS_{t}a - Va\xi);$$

and other easy combinations give the laws of areas and living force, under the forms,

VII. . . $\sum maD_ta - \sum mV \int a\xi dt = \gamma = a \text{ constant vector };$

VIII. . . $\frac{1}{2} \Sigma m(D_t a)^2 - \Sigma mS \int a \xi dt = c = a \text{ constant scalar.}$

(5.) When the applied forces vanish, or balance each other, or more generally when they compound themselves into a single force acting at the fixed point, so that in each case the condition

1X...
$$\Sigma m Va\xi = 0$$

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ART. 417.] MOTION OF A BODY ROUND A FIXED POINT.

is satisfied, the equations (4.) are simplified; and if we introduce a linear, vector, and self-conjugate function ϕ , such that

X...
$$\phi \iota = \Sigma m a V a \iota = \iota \Sigma m a^2 - \Sigma m a S a \iota$$

and write h^2 for -2c, they take the forms,

XI...
$$\phi D_{\iota} + \nabla_{\iota} \phi \iota = 0$$
; XII... $\phi \iota + \gamma = 0$; XIII... $S_{\iota} \phi \iota = h^2$;

 γ and h being two real constants, of the vector and scalar kinds, connected with each other and with ι by the relation,

XIV...
$$S_{\iota\gamma} + h^2 = 0$$
; also **XV.**.. $\phi D_{\iota} = V_{\iota\gamma}$.

It may be added that γ is now the vector sum of the doubled areal velocities of all the elements of the body, multiplied each by the mass *m* of that element, and each represented by a right line aD_ta perpendicular to the plane of the area described round the fixed point o in the time dt; and that h^2 is the living force, or vis viva of the body, namely the positive sum of all the products obtained by multiplying each element *m* by the square of its linear velocity, regarded as a scalar (TD_ta).*

• [The following elegant method of dealing with a body rotating about a fixed point is due to Clifford (*Dynamic*, vol. ii., page 75). If ρ is the vector to any moving point, $D_{t\rho}$ its velocity, and $d_{t\rho}$ its velocity relative to the body, it is geometrically evident that

$D_{t\rho} = d_{t\rho} + V_{t\rho}.$

This may be regarded as a formula of differentiation connecting D_t and d_t , as ρ may be any vector whatever. In particular, replacing ρ by ι ,

 $\mathbf{D}_{t} = \mathbf{d}_{t},$

or the rate of change of the angular velocity is the same whether referred to fixed axes or to axes moving in the body. (Compare Routh's *Rigid Dynamics*, Part I., Arts. 249, 250.)

Again, from fundamental principles the rate of change of angular momentum of the body about the fixed point is equal to the impressed couple about that point. If then η is the couple, and if $-\phi_i$ is the angular momentum (retaining Hamilton's notation) we have, on replacing ρ by $-\phi_i$, the dynamical equation

$$-\eta = D_t \phi_i = d_t \phi_i + \nabla_i \phi_i. \quad \text{But } d_t \phi_i = \phi d_{ii},$$

because the function ϕ does not change relatively to the body, so Euler's equations are contained in

$$\phi d_{ii} + V_i \phi_i = -\eta.$$

As another example, on replacing $\dot{\rho}$ by $D_{t\rho}$ or by its equivalent $d_{t\rho} + V_{t\rho}$, we deduce the formula of acceleration

$$\begin{aligned} \mathbf{D}_t^2 \rho &= \mathbf{d}_t (\mathbf{d}_t \rho + \mathbf{V}_t \rho) + \mathbf{V}_t (\mathbf{d}_t \rho + \mathbf{V}_t \rho) \\ &= \mathbf{d}_t^2 \rho + 2 \mathbf{V}_t \mathbf{d}_t \rho + \mathbf{V} \mathbf{d}_t \rho + \mathbf{V}_t \mathbf{V}_t \rho. \end{aligned}$$

If ρ is the vector to a point fixed in the body, this becomes $D_t^2 \rho = V d_{\mu} \rho + V_t V_t \rho$, and on taking moments and summing for the various elements of the body, the dynamical equations may be easily derived anew.]

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[III. III. § 8.

(6.) When ι is regarded as a variable vector, the equation XIII. represents an *ellipsoid*, which is *fixed in the body*, but *moveable with it*; and the equation XIV. represents a *tangent plane* to this ellipsoid, which plane is *fixed in space*, but *changes* in general its position relatively to the *body*. And thus the *motion* of that body may generally be conceived, as was shown by Poinsot, to be performed by the *rolling (without gliding)* of an *ellipsoid upon a plane*; the former *carrying the body* with it, while its *centre* o remains *fixed* : and the *semidiameter* (ι) of contact being the vector-axis (3.) of *instantaneous rotation*.

(7.) The ellipsoid XIII. may be called, perhaps, the Ellipsoid of Living Force, on account of the signification (5.) of the constant h^2 in its equation; and the fixed plane XIV., on which it rolls, is parallel to what may be called the *Plane of Areas* ($S_{l\gamma} = 0$): no use whatever having hitherto been made, in this investigation, of any axes or moments of inertia. But if we here admit the usual definition of such a moment, we may say that the Moment of Inertia of the body, with respect to any axis ι through the fixed point, is equal to the living force h^2 divided by the square* of the semidiameter T_{ι} of the ellipsoid XIII.; because this moment is,

XVI...
$$\Sigma m(T \nabla a U \iota)^2 = \iota^{-2} \Sigma m(\nabla \iota a)^2 = - S \iota^{-1} \phi \iota = h^2 T \iota^{-2}.$$

(8.) The equations XII. and XIII. give,

XVII... $0 = \gamma^2 S_i \phi_i - h^2 (\phi_i)^2 = S_i \nu$, if XVIII... $\nu = \gamma^2 \phi_i - h^2 \phi^2_i$;

and this equation XVII. represents a *cone* of the second degree, fixed in the body (comp. (6.)), but moveable with it, of which the axis ι is always a *side*, and to which the *normal*, at any point of that side, has the direction of the line ν . But it follows from XI., or from XII. XV., and from the properties of the function ϕ , that D_{ι} is perpendicular to both ϕ_{ι} and ϕ^{2}_{ι} , and therefore also by XVIII. to ν ; the cone XVII. is therefore *touched*, along the side ι , by that *other cone*, which is the *locus in space* of the *instantaneous axis* of rotation. We are then led by this simple quaternion analysis, to a *second*

^{*} Hence it may easily be inferred, with the help of the general construction of an ellipsoid (217, (6.)), illustrated by fig. 53 in page 234, vol. i., and page 184, that for any solid body, and any given point A thereof, there can always be found (indeed in more ways than one) two other points, B and c, which are likewise fixed in the body, and are such that the square-root of the moment of inertia, round any axis AD, is geometrically constructed by the line BD, if the point D be determined on the axis, by the condition that A and D shall be equally distant from c. This theorem, with some others here reproduced, was given in the Abstract of a Paper read before the Royal Irish Academy on the 10th of January, 1848, and was published in the Proceedings of that date.

ABT. 417.] MOMENTS AND AXES OF INERTIA.

representation of the motion of the body, which also was proposed by Poinsot : namely, as the rolling of one cone on another.

(9.) To treat briefly by quaternions some of MacCullagh's results on this subject, it may be noted that the line γ , though fixed in space, describes in the body a cone of the second degree, of which the equation is, by what precedes,

XIX... $g^2 S \gamma \phi^{-1} \gamma + h^2 \gamma^2 = 0$, if XX... $g = T \gamma$, or XXI... $\gamma^2 + g^2 = 0$;

while, if we write $\gamma = \text{oc}$, the *point* c is indeed fixed in *space*, but describes a *sphero-conic* in the *body*, which is part of the common intersection of the *cone* XIX., the *sphere* XXI., and the *reciprocal ellipsoid* (comp. XIII.),

XXII. \therefore Sy $\phi^{-1}\gamma = h^2$.

(10.) Also, the normal to the new cone (9.), at any point of the side γ , has the direction of $g^2\phi^{-1}\gamma + h^2\gamma$, or of $\iota + h^2\gamma^{-1}$ (comp. XIV.); and if a line in this direction be drawn through the fixed point o, it will be the side of contact of the plane of areas (7.), with the cone of normals at o to the cone XIX.; which last (or reciprocal) cone rolls on that plane of areas.

(11.) As regards the Axes of Inertia, it may be sufficient here to observe that if the body revolve round a permanent axis, and with a constant velocity, the vector axis ι is constant; and must therefore satisfy the equation,

XXIII. . .
$$\nabla_{\iota}\phi_{\iota} = 0$$
, because **XXIV.** . . $D_{\iota}\iota = 0$;

it has therefore in general (comp. 415) one or other of Three Real and Rectangular Directions, determined by the condition XXIII. : namely, those of the Axes of Figure of either of the two Reciprocal Ellipsoids, XIII. XXII.

(12.) And the Three Principal Moments, say A, B, C, corresponding to those three principal axes, are by XVI. the three scalar values of $-\iota^{-1}\phi\iota$; so that the symbolical cubic (350) in ϕ may be thus written,

XXV...
$$(\phi + A)$$
 $(\phi + B)$ $(\phi + C) = 0$.

(13.) Forming then this symbolical cubic by the general method of the Section III. ii. 6, we find that the *three moments* A, B, C, are the *three roots* (always *real*, by this analysis) of the *algebraic* and *cubic equation*,

XXVI. . .
$$A^3 - 2n^2A^2 + (n^4 + n'^2)A - (n^2n'^2 - n''^2) = 0;$$

2 P 2

ELEMENTS OF QUATERNIONS.

in which, n^2 , n''^2 , n'''^2 are three positive scalars, namely,

XXVII... $n^2 = -\Sigma ma^2$; $n'^2 = -\Sigma mm'(\nabla aa')^2$; $n''^2 = \Sigma mm'm''(\operatorname{Saa'a''})^2$; and the combination $n^2n'^2 - n''^2$ is another positive scalar, of which the value may be thus expressed,

XXVIII. . .
$$ABC = n^2 n'^2 - n''^2 = \sum m^2 m' a^2 (\nabla aa')^2 + 2\sum mm' m'' (Taa'Ta'a''Ta''a + Saa'Sa'a''Sa''a).$$

if a, a', a'', &c. be the vectors of the mass-elements m, m', m'', &c.

(14.) And because the equation XXV. gives this other symbolical result,

XXIX...
$$-ABC\phi^{-1} = \phi^2 + (A + B + C)\phi + BC + CA + AB$$

it follows that
XXX... $\phi^{-1}0 = 0$:

and therefore, by XV., &c., that if a body, with a fixed point, &c., begin to revolve round one of its three principal axes of inertia, it will continue to revolve round that axis, with an unchanged velocity of rotation.

(15.) It has hitherto been supposed, that all the moments of inertia are referred to axes passing through one point o of the body; but it is easy to remove this restriction. For example, if we denote the moment XVI., by $I_{\rm e}$, and if I_{ω} be the corresponding moment for an axis parallel to ι , but drawn through a new point Ω , of which the vector is ω , then

XXXI...
$$I_{\omega} = \iota^{-2} \Sigma m (\nabla \iota (a - \omega))^2 = I_0 + 2\Sigma m \cdot S(\omega \iota^{-1} \nabla \iota \kappa) + p^2 \Sigma m,$$

if

XXXII...,
$$\kappa \Sigma m = \Sigma m \alpha$$
, and XXXIII..., $p = T \nabla \omega U \iota$,

so that κ is the vector of the *centre of inertia* (or of gravity) of the body, and p is the *distance* between the two parallel axes.

(16.) If then we suppose that the condition

XXXIV. . . $V\iota\kappa = 0$

is satisfied, that is, if the axis ι pass through the centre of inertia, we shall have the very simple relation,

XXXV. . .
$$I_{\omega} = I_0 + p^2 \Sigma m$$
;

which agrees with known results.*

* [In like manner, if

 $\phi_{\omega} \iota = \Sigma m (\alpha - \omega) \operatorname{V} (\alpha - \omega) \iota,$

we find

$$\phi_{\omega}\iota = \phi_{0}\iota - \mathbf{V}(\kappa \mathbf{V}\omega\iota + \omega \mathbf{V}\kappa\iota)\mathbf{\Sigma}m + \omega \mathbf{V}\omega\iota\mathbf{\Sigma}m$$

TIII. III. § 8.

ARTS. 417, 418.] SYSTEM OF ATTRACTING BODIES.

418. As a *third specimen* of physical applications of quaternions, we propose to consider briefly the motions of a *System of Bodies*, m, m', m'', \ldots regarded as free material points, of which the variable vectors are a, a', a'', \ldots and which are supposed to attract each other according to the law of the inverse square : the fundamental formula employed being the following,

I...
$$\Sigma m SD_t^2 a \delta a + \delta P = 0$$
, if II... $P = \Sigma \frac{mm'}{T(a-a')}$:

P thus denoting the *Potential* (or *force-function*) of the system, and the variations δa , $\delta a'$, . . . being infinitesimal, but otherwise arbitrary.

(1.) To deduce the formula I., with the signification II. of P, from the general equation 417, I. of dynamics, we have first, for the case of two bodies, the following expressions for the accelerating forces,

III...
$$\xi = \frac{m'}{(a-a')r}, \quad \xi' = \frac{m}{(a'-a)r}, \quad \text{if} \quad r = T(a-a');$$

whence follows the transformation,*

IV... - S(
$$m\xi\delta a + m'\xi'\delta a'$$
) = $\frac{-mm'}{r}$ S $\frac{\delta(a-a')}{a-a'} = \delta \frac{mm'}{r}$;

a result easily extended, as above. If the *law* of attraction were supposed different, there would be no difficulty in modifying the expression for the potential accordingly.

(2.) In general, when a scalar, f (as here P), is a function of one or more vectors, a, a', \ldots its variation (or differential) can be expressed as a linear and scalar function of their variations (or differentials), of the form $\beta\beta\delta a + \beta\beta'\delta a' + \ldots$ (or $\Sigma\beta\beta a$); in which $\beta, \beta' \ldots$ are certain new and finite vectors, and are themselves generally functions of a, a', \ldots , derived

$$\phi_{\omega}\iota = \phi_{0}\iota + M\omega V\omega\iota = (\phi_{0} - M\omega S\omega)\iota + M\omega^{2}\iota,$$

M being the mass of the body. It is evident that the linear functions ϕ_{ω} and $\phi_0 - M\omega S\omega$ have the same principal directions, and comparing XXI., page 199, and the Note to page 224, it appears that these directions are the normals to the three confocals

$$S\omega (M^{-1}\phi_0 + h)^{-1}\omega = 1$$

which pass through the point Ω (Binet's theorem). The distribution of the assemblage of these principal axes has virtually been considered in the Note to page 245.]

• It may not be useless here to compare the expression in page 461, vol. i., for the differential of a proximity.

When the point o is at the centre of inertia, so that κ is zero, this takes the simple form

from the given scalar function f. And we shall find it convenient to extend the Notation^{*} of Derivatives, so as to denote these derived vectors β , β' , &c., by the symbols, $D_{\alpha}f$, $D_{\alpha'}f$, &c. In this manner we shall be able to write,

$$\nabla \ldots \delta P = \Sigma S (D_a P \ldots \delta a);$$

and the differential equations of motion of the bodies m, m', m'', \ldots will take by I. the forms:

VI. . .
$$mD_t^2 a + D_a P = 0$$
, $m'D_t^2 a' + D_{a'} P = 0$, &c.

or more fully,

VII...
$$D_t^2 a = \frac{m'}{(a-a') T(a-a')} + \frac{m''}{(a-a'') T(a-a'')} + \ldots;$$
 &c.

(3.) The laws of the centre of gravity, of areas, and of living force, result immediately from these equations, under the forms,

 and

VIII. . . $\Sigma m D_t a = \beta$; IX. . . $\Sigma m \nabla a D_t a = \gamma$; X. . . $T = -\frac{1}{2} \Sigma m (D_t a)^2 = P + H$;

in which β , γ are constant vectors, H is a constant scalar, and 2T is the living force of the system (comp. 417, (5.)).

(4.) One mode (comp. 417, (2.)) of deducing the three equations, of which these are the first integrals, is the following. To obtain VIII., change every variation δa in I. to one common but arbitrary infinitesimal vector, ϵ . For IX., change δa to $V_{\iota a}$, $\delta a'$ to $V_{\iota a'}$, &c.; ι being another arbitrary and infinitesimal vector. Finally, to arrive at X., change variations to differentials (δa to d_a , &c.), and integrate once, as for the two former equations, with respect to the time t.

(5.) The formula I. admits of being *integrated by parts*, without any restriction on the *variations* δa , by means of the general transformation,

XI...
$$S(D_t^2 a \cdot \delta a) = D_t S(D_t a \cdot \delta a) - \frac{1}{2} \delta \cdot (D_t a)^2$$
,

combined with the introduction of the following definite integral (comp. X.),

XII...
$$F = \int_0^t (P + T) dt.$$

* In this extended notation, such a formula as $df\rho = 2S\nu d\rho$ would give, $\nu = \frac{1}{2}D_{\rho}f\rho.$

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ABT. 418.] INTERMEDIATE AND FINAL INTEGRALS.

(6.) In fact, if we denote by a_0, a'_0, \ldots the *initial values* of the vectors a, a', \ldots or their values when t = 0, and by D_0a , D_0a' , \ldots the corresponding values of D_ta , D_ta' , \ldots , we shall thus have, as a first integral of the equation I., the formula,

XIII... $\Sigma mS(D_t a \cdot \delta a - D_0 a \cdot \delta a_0) + \delta F = 0;$

in which no variation δt is assigned to t, and which conducts to important consequences.

(7.) To draw from it some of these, we may observe that if the masses m, m', \ldots be treated as constant and known, the complete integrals of the equations VI. or VII. must be conceived to give what may be called the *final vectors* of *position* a, a', \ldots and of *velocity* $D_{ta}, D_{ta'}, \ldots$ in terms of the *initial vectors* $a_0, a'_0, \ldots D_0 a, D_0 a', \ldots$ and of the *time*, t: whence, conversely, we may conceive the initial vectors of position, and of the time, t: mence, conversely, we may conceive the initial vectors of position, and of the time. In this way, then, we are led to consider P, T, and F as being *scalar functions* (whether we are or are not prepared to *express* them as such), of $a, a', \ldots a_0, a'_0, \ldots$ and t; and thus, by (2.), the recent formula XIII. breaks up into the two following systems of equations:

and

XIV...
$$mD_{t}a + D_{a}F = 0$$
, $m'D_{t}a' + D_{a'}F = 0$, &c.
XV... $-mD_{0}a + D_{a_{0}}F = 0$, $-m'D_{0}a' + D_{a'_{0}}F = 0$, &c.

whereof the former may be said to be intermediate integrals, and the latter to be final integrals, of the differential equations of motion of the system, which are included in the formula I.

(8.) In fact, the equations XIV. do not involve the final vectors of acceleration D_t^2a , .. as the differential equations VI. or VII. had done; and the equations XV. express, at least theoretically, the dependence of the final vectors of position a, .. on the time, t, and on the initial vectors of position $a_{0, \cdot}$. and of velocity D_0a , .. as by (7.) the complete integrals ought to do. And on account of these and other important properties, the function here denoted by F may be called the Principal* Function of Motion of the System.

^{*} This function was in fact so called, in two Essays by the present writer, "On a General Method in Dynamics," published in the *Philosophical Transactions* (London), for the years 1834 and 1835; although of course *coordinates*, and not *quaternions*, were *then* employed, the latter not having been discovered until 1843: and the notation S, since adopted for *scalar*, was then used instead of F.

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(9.) If the initial vectors a_0 , . . and D_0a , . . be given, that is, if we consider the actual progress in space of the mutually attracting system of masses m, . . from one set of positions to another, then the function F depends upon the *time* alone; and by its definition XII., its rate or velocity of increase, or its total derivative with respect to t, is thus expressed,

XVI. . .
$$D_t F = P + T_t$$

(10.) But we may inquire what is the *partial derivative*, say $(D_t F)$, of the same definite integral F, when regarded (7.) as a function of the final and initial vectors of position $a_1 \ldots a_0, \ldots$ which involves also the time explicitly, and is now to be derivated with respect only to that variable t, as if the final vectors a_1 . were constant: whereas in fact those vectors alter with the time, in the course of any actual motions of the system.

(11.) For this purpose, it is sufficient to observe that the *part* of the *total* derivative $D_t F$, which arises from the last-mentioned changes of a, ... is (by XIV. and X.),

$$XVII. \ldots \Sigma S(D_{a}F. D_{t}a) = 2T;$$

and therefore (by XVI. and X.), that the remaining part must be,

XVIII. . .
$$(\mathbf{D}_t F) = P - T = -H.$$

(12.) The complete variation of the function F is therefore (comp. XIII.), when t as well as a_1 ... and a_0 , ... is treated as varying,

XIX...
$$\delta F = -H\delta t - \Sigma m SD_t a \delta a + \Sigma m SD_0 a \delta a_0.$$

(13.) And hence, with the help of the equations X. XIV. XV., it is easy to infer that the principal function F must satisfy the two following *Partial Differential Equations in Quaternions*:

XX...
$$(D_t F) - \frac{1}{2} \sum m^{-1} (D_a F)^2 = P;$$

XXI... $(D_t F) - \frac{1}{2} \sum m^{-1} (D_a F)^2 = P_a;$

in which P_{o} denotes the initial value of the potential P.

(14.) If we write

XXII.
$$V = \int_0^t 2T dt$$
,

so that V represents what is called the Action, or the accumulated living

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force, of the system during the time t, then by X. and XII. the two definite integrals F and V are connected by the very simple relation,

$$\mathbf{XXIII.} \dots \mathbf{V} = \mathbf{F} + t\mathbf{H};$$

whence by XIX. the complete variation of V, considered as a function of the final and initial vectors of position, and of the constant H of living force, which does not explicitly involve the time, may be thus expressed,

$$\mathbf{XXIV}...\delta V = t\delta H - \Sigma m \mathrm{SD}_t a \delta a + \Sigma m \mathrm{SD}_0 a \delta a_0.$$

(15.) The partial derivatives of this new function V, which is for some purposes more useful than F, and may be called, by way of distinction from it, the Characteristic* Function of the motion of the system, are therefore,

XXV...
$$D_a V = -mD_t a$$
, &c.
XXVI... $D_{a0} V = +mD_0 a$, &c.

XXVII... D V = t.

and

(16.) The intermediate integrals (7.) of the differential equations of motion, which were before expressed by the formulæ XIV., may now, somewhat less simply, be regarded as the result of the elimination of H between the formulæ XXV. XXVII.; and the final integrals of those equations VI. or VII., which were expressed by XV., are now to be obtained by eliminating the same constant H between the recent equations XXVI. XXVII.

(17.) The Characteristic Function, V, is obliged (comp. (13.)) to satisfy the two following partial differential equations,

XXVIII...
$$\frac{1}{2} \sum m^{-1} (D_{\alpha} V)^2 + P + H = 0;$$

XXIX... $\frac{1}{2} \sum m^{-1} (D_{\alpha_0} V)^2 + P_0 + H = 0;$

it vanishes, like F, when t = 0, at which epoch $a = a_0$, $a' = a'_0$, &c.; each of these two functions, F and V, depends symmetrically on the initial and final vectors of position: and each does so, only by depending on the mutual configuration of all those initial and final positions.

^{*} The Action, V, was in fact so called, in the two Essays mentioned in the preceding Note. The properties of this Characteristic Function had been perceived by the writer, before those of that which he came afterwards to call the Principal Function, as above.

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(18.) It follows (comp. (4.), see also 416, (17.), and 417, (2.)), that the function F must satisfy the two conditions,

$$XXX...\Sigma(D_{\alpha}F + D_{\alpha_0}F) = 0; \quad XXXI...\Sigma V(aD_{\alpha}F + a_0D_{\alpha}a_0F) = 0;$$

which accordingly are forms, by XIV. XV., of the equations VIII. and IX., and therefore are expressions for the law of motion of the centre of gravity, and the law of description of areas. And, in like manner, the function V is obliged to satisfy these two analogous conditions,

XXXII...
$$\Sigma(D_a V + D_{a0} V) = 0$$
; XXXIII... $\Sigma V(a D_a V + a_0 D_{a0} V) = 0$;

which accordingly, by XXV. XXVI., are new forms of the same equations VIII. IX., and consequently are new expressions of the same two laws.

(19.) All the foregoing conditions are satisfied when t is *small*, that is, when the *time* of motion of the system is *short*, by the following *approximate* expressions for the functions F and V, with the respectively derived and mutually connected expressions for H and t:

XXXIV...
$$F = \frac{t}{2} (P + P_0) + \frac{s^2}{2t};$$

XXXV... $V = s (P + P_0 + 2H)^{\frac{1}{2}};$
XXXVI... $H = - (D_t F) = -\frac{1}{2} (P + P_0) + \frac{s^2}{2t^2};$
XXXVII... $t = D_H V = s (P + P_0 + 2H)^{-\frac{1}{2}};$

in which s denotes a real and positive scalar, such that

XXXVIII... $s^2 = -\Sigma m (a - a_0)^2$, or XXXIX... $s = \sqrt{\Sigma m T (a - a_0)^2}$.

419. As a *fourth specimen*, we shall take the case of a free point or particle, attracted to a fixed centre^{*} o, from which its variable vector is a, with an accelerating force = Mr^{-2} , if r = Ta = the distance of the point from the

I'...
$$D^2(a - a') = (m + m') (a - a')^{-1} r^{-1}$$
, if $r = T(a - a')$;

and this equation I'. reduces itself to I., when we write a for a - a', and M for m + m'.

^{*} When two free masses, m and m', with variable vectors a and a', attract each other according to the law of the inverse square, the differential equation of the relative motion of m about m' is, by 418, VII.,

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centre, while M is the attracting mass : the differential equation of the motion being,

$$\mathbf{I}...\mathbf{D}^{2}a=Ma^{-1}r^{-1},$$

if D (abridged from D_t) be the sign of derivation, with respect to the time t.

(1.) Operating on I. with ∇ . *a*, and integrating, we obtain immediately the equation (comp. 338, (5.)),

II. . .
$$VaDa = \beta = const.$$
;

which expresses at once that the orbit is plane, and also that the area described in it is proportional to the time; $U\beta$ being the fixed unit-normal to the plane, round which the point, in its angular motion, revolves positively; and $T\beta$ representing in quantity the double areal velocity, which is often denoted by c.

(2.) And it is important to remark, that these conclusions (1.) would have been obtained by the same analysis, if r^{-1} in I. had been replaced by any other scalar function, f(r), of the distance; that is, for any other law of central force, instead of the law of the inverse square.

(3.) In general, we have the transformation,

III. . .
$$a^{-1}Ta^{-1} = dUa : Vada$$
,

because, by 334, XV., &c., we have,

IV...
$$dUa = V(da \cdot a^{-1}) \cdot Ua = a^{-2}Ua \cdot Vada = a^{-1}Ta^{-1} \cdot Vada;$$

the equation I. may therefore by II. be transformed as follows,

V...
$$D^2 a = \gamma D U a$$
, if VI... $\gamma = -M\beta^{-1}$;

and thus it gives, by an immediate integration,

VII... $Da = \gamma (Ua - \epsilon)$, or VII'... $Da = (\epsilon - Ua)\gamma$,

 ϵ being a new constant vector, but one situated in the plane of the orbit, to which plane β and γ are perpendicular.

(4.) But a, Da, D²a are here (comp. 100, (5.) (6.) (7.)) the vectors of position, velocity, and acceleration of the moving point; and it has been defined (100, (5.)) that if, for any motion of a point, the vectors of velocity

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be set off from any common origin, the curve on which they terminate is the *Hodograph*^{*} of that motion.

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(5.) Hence a and Da, if the latter like the former be drawn from the fixed point o, are the vectors of corresponding points of orbit and hodogragh; and because the formula VII. gives,

VIII...
$$S\gamma Da = 0$$
, and IX... $(Da + \gamma \varepsilon)^2 = \gamma^2$,

it follows that the hodograph is, in the present question, a *Circle*, in the plane of the orbit, with $-\gamma\epsilon$ (or $+\epsilon\gamma$) for the vector of its *centre*, and with $T\gamma = MT\beta^{-1}$ for its *radius*, which radius we shall also denote by h.

(6.) The Law of the Circular + Hodograph is therefore a mathematical consequence of the Law of the Inverse Square; and conversely it will soon be proved, that no other law of central force would allow generally the hodograph to be a circle.

(7.) For the law of nature, the Radius (h) of the Hodograph is equal, by (1.) and (5.), to the quotient of the attracting mass (M), divided by the double areal velocity (T β or c) in the orbit; and if we write

$$\mathbf{X}...e = \mathbf{T}\epsilon$$
,

this positive scalar e may be called the *Excentricity* of the hodograph, regarded as a *circle excentrically situated*, with respect to the *fixed centre of force*, o.

(8.) Thus, if e < 1, the fixed point o is *interior* to the hodograph circle; if e = 1, the point o is *on the circumference*; and if e > 1, the centre o of force is then *exterior* to the hodograph, being however, in *all* these cases, situated *in its plane*.

(9.) The equation VII. gives,

XI...
$$\varepsilon$$
 - Ua = - γ^{-1} Da = Da. γ^{-1} ;

operating then on this with S.a, and writing for abridgment,

XII... $p = \beta \gamma^{-1} = M^{-1}T\beta^2 = c^2 M^{-1}$, and XIII... SUat = cos v,

^{*} Compare fig. 32, p. 97, vol. i. [and p. 302]; see also pages 99, vol. i., 29, 112, from the two latter of which it may be perceived, that the *conception* of the *hodograph* admits of some purely *geometrical* applications.

⁺ This law of the circular hodograph was deduced geometrically, in a paper read before the Royal Irish Academy, by the present author, on the 14th of December, 1846; but it was virtually contained in a quaternion formula, equivalent to the recent equation VII., which had formed part of an earlier communication, in July, 1845. (See the *Proceedings* for those dates; and especially pages 345, 347, and xxxix, xlix, of vol. iii.)

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so that p is a constant and positive scalar, while v is the inclination of a to $-\varepsilon$, we find,

XIV...
$$r$$
 + Sa ϵ = p ; or **XV.**.. r = $\frac{p}{1 + e \cos v}$;

the orbit is therefore a plane conic, with the centre of force o for a focus, having e for its excentricity, and p for its semiparameter.

(10.) And we see, by XII., that if this semiparameter p be multiplied by the attracting mass M, the product is the square of the double areal velocity c; so that this constant c may be denoted by $(Mp)^{\frac{1}{2}}$, which agrees with known results.

(11.) If, on the other hand, we divide the mass (M) by the semiparameter (p), the quotient is by XII. the square of the radius $(MT\beta^{-1} \text{ or } h)$ of the hodograph.

(12.) And if we multiply the same semiparameter p by this radius $M \operatorname{T} \beta^{-1}$ of the hodograph, the product is then, by the same formula XII., the constant $\operatorname{T} \beta$ or c of double areal velocity in the orbit, so that $h = Mc^{-1} = cp^{-1}$.

(13.) If we had operated with V. a on VII'., we should have found,

XVI. . .
$$\beta = \nabla . a (\varepsilon - Ua) \gamma = (Sa\varepsilon + r) \gamma;$$

which would have conducted to the same equations XIV. XV. as before.

(14.) If we operate on VII. with S.a, we find this other equation,

XVII. . . -
$$r\mathbf{D}r = \mathbf{S}a\mathbf{D}a = \gamma \nabla a\epsilon$$
;

 \mathbf{but}

XVIII. . . - $\gamma^2 = h^2 = \frac{M}{p}$ (by VI. and XII., comp. (11.)),

and

XIX. . . -
$$(\nabla a \varepsilon)^2 = e^2 r^2 - (p - r)^2 = p (2r - p - r^2 a^{-1}),$$

if we write

XX. . . $a = \frac{p}{1-e^2}$;

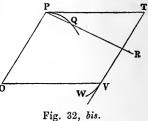
hence squaring XVII., and dividing by r^2 , we obtain the equation,

XXI.
$$\left(\frac{\mathrm{d}r}{\mathrm{d}t}\right)^2 = M\left(\frac{2}{r}-\frac{1}{a}-\frac{p}{r^2}\right)$$
.

(15.) It is obvious that this last equation, XXI., connects the *distance*, r, with the *time*, t, as the formula XV. connects the same distance r with the *true anomaly*, v; that is, with the *angular elongation* in the orbit, from the

position of least distance. But it would be improper here to delay on any of the elementary consequences of these two known equations : although it seemed useful to show, as above, how the equations themselves might easily be deduced by quaternions, and be connected with the theory of the hodograph.

(16.) The equation II. may be interpreted as expressing, that the parallelogram (comp. fig. 32, p. 97, vol. i.) under the vectors a and Da of position and velocity, or under any two corresponding vectors (5.) of the orbit and hodograph, has a constant plane and area, represented by the constant vector β , which is *perpendicular* (1.) to that plane. But of it is to be observed that, by (2.), these constancies, and this representation, are not peculiar to the



law of the inverse square, but exist for all other laws of central force. (17.) In general, if any scalar function R (instead of Mr^{-1}) represent the accelerating force of attraction, at the distance r from the fixed centre o, the differential equation of motion will be (instead of I.),

XXII. . .
$$D^2a = Rra^{-1} = -RUa;$$

and if we still write $\nabla a D a = \beta$, as in II., the formula IV. will give,

XXIII... $D^3a = -DR \cdot Ua - Rr^{-2}\beta Ua$, and XXIV... $V \frac{D^3a}{D^2a} = r^{-2}\beta$; $\beta = c \mathbf{U} \beta$, if $c = \mathbf{T} \beta$, as before.

in which

(18.) Applying then the general formula 414, I., we have, for any law* of force, the expressions,

XXV... Vector of Curvature of Hodograph = $\frac{1}{D^2 a} \nabla \frac{D^3 a}{D^2 a} = \frac{c}{Rs^2} U a \beta$;

XXVI... Radius (h) of Curvature of Hodograph = Rr^2c^{-1}

= Force × Square of Distance Double Areal Velocity in Orbit;

of which the last not only conducts, in a new way, for the law of nature, to the constant value (7.), $h = Mc^{-1}$, but also proves, as stated in (6.), that for

* The general value XXVI., of the radius of curvature of the hodograph, was geometrically deduced in the Paper of 1846, referred to in a recent Note.

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any other law of central force the hodograph cannot be a circle, unless indeed the orbit happens to be such, and to have moreover the centre of force at its centre.

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(19.) Confining ourselves however at present to the law of the inverse square, and writing for abridgment (comp. (5.)),

XXVII... $\kappa = OH = \epsilon \gamma = Vector of Centre H of Hodograph,$

which gives, by (5.) and (7.),

XXVIII. . .
$$T_{\kappa} = eh$$
,

the origin o of vectors being still the centre of *force*, we see by the properties of the *circle*, that the *product* of any two *opposite velocities* in the *orbit* is *constant*; and that this constant product* may be expressed as follows,

XXIX. . . $(e-1)h\mathbf{U}_{\kappa}$. $(e+1)h\mathbf{U}_{\kappa} = h^2(1-e^2) = Ma^{-1}$,

by XVIII. and XX.

(20.) The expression XXIX. may be otherwise written as $\kappa^2 - \gamma^2$; and if v be the vector of any point v external to the circle, but in its plane, and u the length of a *tangent* ur from that point, we have the analogous formula,

XXX...
$$u^2 = \gamma^2 - (\upsilon - \kappa)^2 = T(\upsilon - \kappa)^2 - h^2$$
.

(21.) Let τ and τ' be the vectors or, or of the *two* points of contact of tangents thus drawn to the hodograph, from an external point u in its plane; then *each* must satisfy the system of the *three* following scalar equations,

XXXI...
$$S\gamma\tau = 0$$
;
XXXII... $(\tau - \kappa)^2 = \gamma^2$;
XXXIII... $S(\tau - \kappa)(\upsilon - \kappa) = \gamma^2$;

* In strictness, it is only for a closed orbit, that is, for the case (8.) of the centre of force being *interior* to the hodograph (e < 1), that two velocities can be opposite; their vectors having then, by the fundamental rules of quaternions, a scalar and positive product, which is here found to be $= Ma^{-1}$, by XXIX., in consistency with the known theory of elliptic motion. The result however admits of an *interpretation*, in other cases also. It is obvious that when the centre o of force is exterior to the hodograph, the polar of that point divides the circle into two parts, whereof one is concave, and the other convex, towards o; and there is no difficulty in seeing, that the former part corresponds to the branch of an hyperbolic orbit, which can be described under the influence of an attracting force: while the latter part answers to that other branch of the same complete hyperbola, whereof the description would require the force to be repulsive.

;

whereof the *first alone* represents the *plane*; the *two first* jointly represent (comp. (5.)) the *circle*; and the *third* expresses the *condition of conjugation* of the points τ and υ , and may be regarded as the *scalar equation of the polar* of the latter point. It is understood that $S\gamma \upsilon = 0$, as well as $S\gamma \kappa = 0$, &c., because γ is perpendicular (3.) to the plane.

(22.) Solving this system of equations (21.), we find the two expressions,

XXXIV...
$$\tau = \kappa + \gamma (\gamma + u) (\upsilon - \kappa)^{-1};$$

XXXIV'... $\tau' = \kappa + \gamma (\gamma - u) (\upsilon - \kappa)^{-1};$

in which the scalar u has the same value as in (20.). As a verification, these expressions give, by what precedes,

$$\begin{array}{ll} \text{XXXV.} \dots \text{S}\left(\tau - \kappa\right)\left(\tau - \upsilon\right) = 0 \ ; & \text{XXXV'} \dots \text{S}\left(\tau' - \kappa\right)\left(\tau' - \upsilon\right) = 0 \\ \text{and} & \text{XXXVI.} \dots \left(\tau - \upsilon\right)^2 = \left(\tau' - \upsilon\right)^2 = -u^2. \end{array}$$

In fact it is found that

XXXVII... $\tau - \upsilon = u (u + \gamma) (\upsilon - \kappa)^{-1};$ XXXVIII... $T (u + \gamma) = T (\upsilon - \kappa);$ XXXIX... $(\tau - \upsilon) (\tau - \kappa) = u\gamma;$

and

 $u + \gamma$ being here a quaternion.

(23.) If v' be the vector ou' of any point v', on the polar of the point v with respect to the circle, then changing τ to v', and u to z, in XXXIV., we find this vector form (comp. (21.)) of the equation of that polar,

XL...
$$v' = \kappa + \gamma (\gamma + z) (v - \kappa)^{-1}$$
,

or, by an easy transformation,

XLI...
$$(h^2 + u^2)v' = h^2v + u^2\kappa + z\gamma(\kappa - v),$$

in which z is an arbitrary scalar.

(24.) If then we suppose that u' is the *intersection* of the chord $\tau r'$ with the right line ou, the condition

XLII...
$$\nabla v'v = 0$$
 will give XLIII... $z\gamma = \frac{u^2 \nabla \kappa v}{v^2 - S \kappa v};$

 \mathbf{but}

$$XLIV...V\kappa \upsilon . (\kappa - \upsilon) = \kappa S(\kappa \upsilon - \upsilon^2) + \upsilon S(\kappa \upsilon - \kappa^2);$$

ART. 419.] CONSTRUCTIONS FOR THE POTENTIAL.

the coefficient then of κ , in the expanded expression for ν' , disappears as it ought to do : and we find, after a few reductions,

XLV...
$$v' = v \left(1 + \frac{u^2}{v^2 - S_{\kappa v}}\right) = \frac{\gamma^2 - \kappa^2 + S_{\kappa v}}{v - v^{-1}S_{\kappa v}},$$

a result which might have been otherwise obtained, by eliminating a new scalar y between the two equations,

XLVI...
$$v' = yv$$
, $S(yv - \kappa)(v - \kappa) = \gamma^2$.

(25.) Introducing then two auxiliary vectors, λ , μ , such that

XLVII. . .
$$\lambda = v^{-1}S_{\kappa v}$$
, or $S_{\kappa v} = v\lambda = \lambda v$,

and therefore

XLVII'. . .
$$\lambda - \kappa = \upsilon^{-1} \nabla \kappa \upsilon$$
, $S_{\kappa \lambda} = \lambda^2$, $(\lambda - \kappa)^2 = \kappa^2 - \lambda^2$,

and

XLVIII. . .
$$\mu = \lambda \left(1 + \left(1 + \frac{\gamma^2 - \kappa^2}{\lambda^2} \right)^{\frac{1}{2}} \right)$$
, whence $\mu \parallel \lambda$, $(\mu - \kappa)^2 = \gamma^2$,

we have the very simple relation,

XLIX...
$$(v - \lambda) (v' - \lambda) = (\mu - \lambda)^2$$
, or L... $LU \cdot LU' = LM^2$,

if $\lambda = 0L$, and $\mu = 0M$. Accordingly, the point L is the foot of the perpendicular let fall from the centre H on the right line ou, while M is one of the two points M, M' of intersection of that line with the circle; so that the equation L. expresses, that the points U, U' are harmonically conjugate, with respect to the chord MM', of which L is the middle point, as is otherwise evident from geometry.

(26.) The vector a of the orbit (or of position), which corresponds to the vector τ (= Da) of the hodograph (or of velocity), and of which the length is Ta = r = the distance, may be deduced from τ by the equations,

LI. . . $a = r(\kappa - \tau)\gamma^{-1}$, and LII. . . $\nabla \tau a = -\beta = M\gamma^{-1}$;

whence follow the expressions,

LIII... Potential =
$$Mr^{-1} = (say) P = Sr(\kappa - \tau) = Sv(\kappa - \tau);$$

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the second expression for P being deduced from the first, by means of the relation XXXV.

(27.) The first expression LIII. for P shows that the potential is equal, Ist, to the rectangle under the radius of the hodograph, and the perpendicular from the centre o of force, on the tangent at τ to that circle; and IInd, to the square of the tangent from the same point τ of the hodograph, to what may be called the *Circle of Excentricity*, namely to that new circle which has of for a diameter. And the first of these values of the potential may be otherwise deduced from the equality (7.) of the mass M, to the product hc of the radius h of the hodograph, multiplied by the constant c of double areal velocity, or by the constant parallelogram (16.) under any two corresponding vectors.

(28.) The second expression LIII. for the potential P, corresponding to the point T of the hodograph, may (by XXXIV., &c.) be thus transformed, with the help of a few reductions of the same kind as those recently employed:

LIV...
$$P = \frac{M}{r} = \frac{h^2 Sq + u\gamma \nabla q}{h^2 + u^2}$$
, if LV... $q = v (\kappa - v)$,

q being thus an auxiliary quaternion; and in like manner, for the other point τ' lately considered, we have the analogous value,

LVI...
$$P' = \frac{M}{r'} = \frac{h^2 \mathrm{S}q - u\gamma \mathrm{V}q}{h^2 + u^2};$$

whence

LVII...
$$P \cdot P' = \frac{h^2(8q^2 + u^2v^2)}{h^2 + u^2};$$

and therefore,

LVIII...
$$\frac{r}{M} = P^{-1} = \frac{\mathbf{S}q + u\gamma^{-1}\mathbf{V}q}{\mathbf{S}q^2 + u^2v^2};$$

LIX. ...
$$\frac{r'}{M} = P'^{-1} = \frac{\operatorname{Sq} - u\gamma^{-1}\operatorname{Vq}}{\operatorname{Sq}^2 + u^2v^2};$$

and finally,

LX. .
$$\frac{2M}{r+r'} = \frac{2PP'}{P+P'} = Sq + \frac{u^2v^2}{Sq} = v(\lambda - v') = OU \cdot U'L.$$

(29.) In fact, the same second expression LIII. shows, that if v and v' be

ART. 419.] CONSTRUCTIONS FOR THE POTENTIAL.

the feet of perpendiculars from T and T' on HL, then the potentials are,

LXI...
$$P = ou \cdot tv$$
, and $P' = ou \cdot t'v'$;

and it is easy to prove, geometrically, that the segment U'L is the harmonic mean between what may be called the ordinates, TV, T'V', to the hodographic axis HL.

(30.) If we suppose the point v to take any new but near position v, in the plane, the polar chord $\tau\tau'$, and (in general) the length u of the tangent $v\tau$, will change; and we shall have the differential relations:

LXII...
$$d\tau = (\tau - \upsilon)^{-1}S(\tau - \kappa) d\upsilon$$
;
LXII'... $d\tau' = (\tau' - \upsilon)^{-1}S(\tau' - \kappa) d\upsilon$;
LXIII... $du = u^{-1}S(\kappa - \upsilon) d\upsilon$.

(31.) Conceiving next that u moves along the line ou, or Lu, so that we may write,

LXIV...
$$v = (x - e') (\mu - \lambda)$$
, if $x = \frac{LU}{LM} = \frac{LM}{LU'}$, and $e' = \frac{LO}{LM}$.

we shall have,

LXV...
$$d\boldsymbol{v} = (\boldsymbol{\mu} - \lambda) d\boldsymbol{x} = \boldsymbol{v} (\boldsymbol{x} - \boldsymbol{e}')^{-1} d\boldsymbol{x}, \text{ with } \boldsymbol{x} > 1 > \boldsymbol{e}',$$

if u be on LM prolonged, and if o be on the concave side of the arc TMT'; and thus, by LIII., the differential expressions (30.) become,

LXVI...
$$d\tau = (v - \tau)^{-1} P(x - e')^{-1} dx; \quad d\tau' = (v - \tau')^{-1} P'(x - e')^{-1} dx;$$

and

LXVII... $du = u^{-1}Sq \cdot (x - e')^{-1}dx$, with $Sq = v(\lambda - v)$;

LXVIII...
$$\operatorname{Td} r = \frac{P dx}{u(x-e')}, \quad \operatorname{Td} r' = \frac{P' dx}{u(x-e')}, \quad \text{if } dx > 0.$$

Such then are the *lengths* of the two *elementary arcs* TT, and T'T', of the hodograph, intercepted between two near secants NTT' and NT,T' drawn from the pole N of the chord MM', and having U and U, for their own poles; and we see that these *arcs* are proportional to the *potentials*, P and P', or by LXI. to the *ordinates*, TV, T'V', or finally to the lines NT, NT': and accordingly

2 R 2

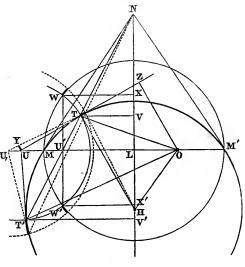
and

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we have the *inverse similarity* (comp. 118), of the two small triangles with n for vertex,

LXIX... Δ NTT, \propto' NT/T',

as appears on inspection of the annexed figure 86.





(32.) For any motion of a point, however complex, the element dt of time which corresponds to a given element dDa of the hodograph, is found by dividing the latter element by the vector D^2a of accelerating force; if then we denote by dt and dt' the times corresponding to the elements dr and $d\tau'$ (31.), we have the expressions,

LXX...
$$dt = M \cdot P^{-2} \cdot T d\tau = \frac{M dx}{P u (x - e')} = \frac{r dx}{u (x - e')},$$

LXX'... $dt' = M \cdot P'^{-2} \cdot T d\tau' = \frac{M dx}{P' u (x - e')} = \frac{r' dx}{u (x - e')},$

because, for the motion here considered, the measure or quantity of the force is, by I. and LIII.,

IXXI...
$$TD^{2}a = Mr^{-2} = M^{-1}P^{2}$$
.

(33.) The times of hodographically describing the two small circular arcs,

 T_T and $T'T'_$, are therefore *inversely* proportional to the *potentials*, or *directly* proportional to the *distances* in the *orbit*; and their sum is,

LXXII... dt + dt' =
$$\left(\frac{M}{P} + \frac{M}{P'}\right) \frac{u^{-1}dx}{x-e'} = \frac{(r+r')dx}{u(x-e')};$$

that is, by LX. and LXIV.,

LXXIII...
$$dt + dt' = \frac{2Mxdx}{u(x-e')^2g^2}$$
, if LXXIV... $g = T(\mu - \lambda) = \overline{LM}$.

(34.) We have also the relations,

LXXV...
$$u = (x^2 - 1)^{\frac{1}{2}}g$$
, and **LXXVI.**.. $\frac{M}{a} = (1 - e'^2)g^2$;

so that the sum of the two small times may be thus expressed,

LXXVII...
$$dt + dt' = \frac{2(a(1-e'^2))^{\frac{3}{4}}}{M^{\frac{1}{2}}} \cdot \frac{(1-e'x^{-1})^{-2}dx}{x(x^2-1)^{\frac{3}{2}}},$$

or finally,

LXXVIII... $dt + dt' = 2 \left(\frac{a^3(1-e'^2)^3}{M}\right)^{\frac{1}{2}} \frac{dw}{(1-e'\cos w)^2},$

if

LXXIX... $x = \sec w$, or $w = \angle \operatorname{MLW}$ in fig. 86,

in which figure u'w is an ordinate of a semicircle, with the chord MM' of the hodograph for its diameter.

(35.) The two near secants (31.), from the pole N of that chord, have been here supposed to cut the half chord LM *itself*, as in the cited figure 86; but if they were to cut the *other* half chord LM', it is easy to prove that the formulæ LXXVIII. LXXIX. would still hold good, the only difference being that the angle w, or MLW, would be now *obtuse*, and its secant x < -1.

(36.) A circle, with u for centre, and u for radius, cuts the hodograph orthogonally in the points τ and τ' ; and in like manner a near circle, with u, for centre, and u + du for radius, is another orthogonal, cutting the same hodograph in the near points τ , and τ' (31.). And by conceiving a series of such orthogonals, and observing that the differential expression LXXVIII. depends only on the four scalars, $M^{-1}a^3$, e', w, and dw, which are all known when the mass M and the five points o, L, M, u, u, are given, so that they do not change when we retain that mass and those points, but alter the radius hof the hodograph, or the perpendicular HL let fall from its centre H on the fixed chord MM', we see that the sum of the times (comp. (33.)), of hodographically describing any two circular arcs, such as τ , τ and $\tau'\tau'$, even if they be not small,

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but intercepted between any two secants from the pole N of the fixed chord, is independent of the radius (h), or of the height HL of the centre H of the hodograph.

(37.) If then two circular hodographs, such as the two in fig. 86, having a common chord MM', which passes through, or tends towards, a common centre of force o, with a common mass M there situated, be cut by any two common orthogonals, the sum of the two times of hodographically describing (33.) the two intercepted arcs (small or large) will be the same for those two hodographs.

(38.) And as a case of this general result, we have the following Theorem* of Hodographic Isochronism (or Synchronism):

"If two circular hodographs, having a common chord, which passes through, or tends towards, a common centre of force, be cut perpendicularly by a third circle, the times of hodographically describing the intercepted arcs will be equal."

For example, in fig. 86, we have the equation,

LXXX. . . . Time of TMT' = time of WMW'.

(39.) The time of thus describing the arc TMT' (fig. 86), if this arc be throughout concave† towards o (so that x > 1 > e', as in LXV.), is expressed (comp. LXXVIII.) by the definite integral,

LXXXI... Time of TMT' =
$$2\left(\frac{a^3(1-e'^2)^3}{M}\right)^{\frac{1}{2}}\int_0^w \frac{\mathrm{d}w}{(1-e'\cos w)^2}$$
;

and the time of describing the *remainder* of the hodographic circle, if *this* remaining arc T'M'T be throughout concave towards the centre o of force, is expressed by this other integral,

LXXXII... Time of
$$\mathbf{T}'\mathbf{M}'\mathbf{T} = 2\left(\frac{a^3(1-e'^2)^3}{M}\right)^{\frac{1}{2}} \int_w^{\pi} \frac{\mathrm{d}w}{(1-e'\cos w)^2}$$

(40.) Hence, for the case of a closed orbit $(e'^2 < 1, e < 1, a > 0)$, if n denote the mean angular velocity, we have the formula,

LXXXIII... Periodic Time =
$$\frac{2\pi}{n} = 2\left(\frac{a^3}{M}\right)^{\frac{1}{2}} (1-e'^2)^{\frac{3}{2}} \int_0^{\pi} \frac{\mathrm{d}w}{(1-e'\cos w)^2} = 2\pi \left(\frac{a^3}{M}\right)^{\frac{1}{2}};$$

or

^{*} This Theorem, in which it is understood that the common centre of force (o) is occupied by a common mass (M), was communicated to the Royal Irish Academy on the 16th of March, 1847. (See the *Proceedings* of that date, vol. iii., page 417.) It has since been treated as a subject of investigation by several able writers, to whom the author cannot hope to do justice on this subject, within the very short space which now remains at his disposal.

[†] Compare the Note to page 303.

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The same result, for the same case of *elliptic motion*, may be more rapidly obtained, by conceiving the chord MM' through o to be perpendicular to OH; for, in this position of that chord, its middle point L coincides with o, and e' = 0 by LXIV.

(41.) In general, by LXXVI., we are at liberty to make the substitution,

LXXXV...
$$\left(\frac{a^3(1-e'^2)^3}{M}\right)^{\frac{3}{2}} = \frac{M}{g^3}$$
, with $g = half$ chord of the hodograph;

supposing then that e' = -1, or placing o at the extremity m' of the chord, we have by LXXXI.,

LXXXVI... Parabolic time of TMT' =
$$\frac{2M}{g^3} \int_0^w \frac{\mathrm{d}w}{(1+\cos w)^2}$$
;

for, when the centre of force is thus situated on the circumference of the hodographic circle, we have by (8.) the excentricity e = 1, and the orbit becomes by XV. a parabola. For hyperbolic motion $(e'^2 > 1, e > 1, a < 0)$, the formula LXXXI. (with or without the substitution LXXXV.) is to be employed if e' < -1, that is, if o be on LM' prolonged; and the formula LXXXII., if e' > 1, $e' < \sec w$, that is, if o be situated between M and U.

(42.) For any law of central force, if P, P' be the points of the orbit which correspond to the points T, T' of the hodograph, and if Q be the point of meeting of the tangents to the orbit at P, P', as in the annexed figure 87, while the tangents to the hodograph at T, T' meet as before in U, we shall have the parallelisms,

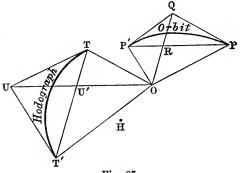


Fig. 87.

LXXXVII... OP || UT, OP' || T'U, PQ || OT, QP' || OT'; writing then,

LXXXVIII. . . OP = a, OP' = a', $OT = Da = \tau$, $OT' = Da' = \tau'$, OU = v, $OQ = \omega$,

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most of which notations have occurred before, we have the equations,

LXXXIX...
$$0 = Va(\tau - v) = Va'(v - \tau') = V\tau(\omega - a) = V\tau'(a' - \omega);$$

thus

XC...
$$\nabla av = \nabla a\tau = \beta = \nabla a'\tau' = \nabla a'v, \quad a' - a \parallel v, \quad PP' \parallel OU,$$

and

XCI...
$$\nabla \tau \omega = \nabla \tau a = -\beta = \nabla \tau' a' = \nabla \tau' \omega', \quad \tau - \tau' \parallel \omega, \quad \mathbf{T'T} \parallel \mathbf{0Q}.$$

Geometrically, the constant parallelogram (16.) under OP, OT, or under OP', OT', is equal, by LXXXVII., to each of the four following parallelograms: I. under OP, OU; II. under OP', OU; III. under OQ, OT; and IV. under OQ, OT'; whence PP' || OU, and T'T || OQ, as before.

(43.) The *parallelism* XC. may be otherwise deduced for the law of the *inverse square*, with recent notations, from the quaternion formulæ,

XCII...
$$\frac{a'-a}{r+r'} = \frac{u}{\lambda-v} = \frac{v-v'}{u}$$
, in which, XCII'... $v' = \frac{r\tau+r'\tau'}{r+r'}$,

and which may be obtained in various ways; whence it may also be inferred, that if s denote the *length* T(a' - a) of the *chord* PP' of the *orbit*, then (comp. fig. 86.),

XOIII...
$$\frac{s}{r+r'} = \frac{u}{T(\lambda-v)} = \overline{vT} : \overline{vL} = \&c. = \sin w;$$

w being the same auxiliary angle as in (34.), &c.

(44.) It is easy to prove that

XCIV. . .
$$\lambda - \tau = \left(1 + \frac{u}{\gamma}\right) \frac{P}{v}, \quad \lambda - \tau' = \left(1 - \frac{u}{\gamma}\right) \frac{P'}{v},$$

whence

XCV. . . $T\frac{r}{\tau-\lambda} = \frac{r}{P} = \frac{r}{r'}$, and XCVI. . . $P'^{-1}(r'-\lambda)v = K \cdot P^{-1}(\tau-\lambda)v$; the lines LT, LT' are therefore in *length* proportional to the *potentials*, P, P'; and their *directions* are *equally inclined* to that of ou, but at *opposite sides* of it,

and their directions are equally inclined to that of ou, but at opposite sides of it, so that the line LU bisects the angle TLT'. Accordingly (see fig. 86), the three points T, L, T' are on the circle (not drawn in the figure) which has HU for diameter; so that the angles ULT', TLU are equal to each other, as being respectively equal to the angles ULT', TT'U, which the chord TT' of the hodograph makes with the tangents at its extremities: the triangles TLV, T'LV' are therefore similar, and \overline{LT} is to $\overline{LT'}$ as TV to T'V', that is, by LXI., as P to P', or as r' to r. ABT. 419.]

LAMBERT'S THEOREM.

(45.) Again, calculation with quaternions gives,

XCVII. . .
$$\frac{(\boldsymbol{\upsilon}-\boldsymbol{\tau})(\boldsymbol{\lambda}-\boldsymbol{\tau})}{\boldsymbol{\upsilon}'-\boldsymbol{\tau}} = \frac{(\boldsymbol{\upsilon}-\boldsymbol{\tau}')(\boldsymbol{\lambda}-\boldsymbol{\tau}')}{\boldsymbol{\upsilon}'-\boldsymbol{\tau}'} = (\boldsymbol{\upsilon}-\boldsymbol{\kappa})(\boldsymbol{\upsilon}-\boldsymbol{\lambda})(\boldsymbol{\upsilon}-\boldsymbol{\kappa})^{-1},$$

whence

XCVIII...
$$T \frac{v'-\tau}{\lambda-\tau} = T \frac{v'-\tau'}{\lambda-\tau'} = T \frac{\tau-v}{\lambda-v} = \overline{vT} : \overline{vL} = \sin w;$$

such then is the common ratio, of the segments $\overline{TU'}$, $\overline{U'T'}$ of the base $\overline{TT'}$ of the triangle TLT', to the adjacent sides \overline{LT} , $\overline{LT'}$, which are to each other as r' to r (44.); and because this ratio is also that of s to r + r', by (43.), we have the proportion,

XCIX. . .
$$\overrightarrow{OP}$$
 : $\overrightarrow{OP'}$: $\overrightarrow{PP'}$ = r : r' : $s = \overrightarrow{LT'}$: \overrightarrow{LT} : $\overrightarrow{TT'}$.

and the formula of inverse similarity (118),

C. . .
$$\Delta$$
 LT'T \propto' OPP'.

Accordingly (comp. the two last figures), the base angles opp', op'P of the second triangle are respectively equal, by the parallelisms (42.), to the angles TUL, T'UL, and therefore, by the circle (44.), to the base angles TT'L, T'TL, of the first triangle : but the two rotations, round o from P to P', and round L from T' to T, are oppositely directed.

(46.) The investigations of the three last sub-articles have not assumed any knowledge of the *form* of the *orbit* (as *elliptic*, &c.), but only the *law* of *attraction* according to the *inverse square*, or by (6.) the *Law of the Circular Hodograph*. And the same general principles give not only the expression LXXVI. for the constant Ma^{-1} , but also (by LX. LXIV. LXXIV. LXXIX.) this other expression,

CI...
$$\frac{2M}{r+r'} = (1-e'\cos w)g^2$$
; whence CII... $\frac{r+r'}{2a} = \frac{1-e'^2}{1-e'\cos w}$

which last may be considered as a quadratic in e', assigning two values (real or imaginary) for that scalar, when the first member of CII. and the angle w are given; the sine of this latter angle being already expressed by XCIII.

(47.) Abstracting, then, from any ambiguity* of solution, we see, by the

^{*} That there ought to be some such ambiguity is evident from the consideration, that when a focus o, and two points P, P' of an elliptic orbit are given, it is still permitted to conceive the motion to be performed along either of the two elliptic arcs, PP', P'P, which together make up the whole periphery. But into details of this kind we cannot enter here.

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definite integrals in (39.), that the time of describing an arc \mathbf{PP}' of an orbit, with the law of the inverse square, is a function (comp. (36.)) of the three ratios,

CIII.
$$\ldots \frac{a^3}{M}, \frac{r+r'}{a}, \frac{s}{r+r'};$$

which is a form of Lambert's Theorem, but presents itself here as deduced from the recently stated Theorem of Hodographic Isochronism (38.), without the employment of any property of conic sections.

(48.) The differential equation I. of the present relative motion may be thus written (comp. 418, I., and generally the preceding Series 418):

CIV...S.
$$D^2a\delta a + \delta P = 0$$
, whence $CV...T = P + H$,

as in 418, X., if we now write,

$$C\nabla I...T = -\frac{1}{2}Da^2 = -\frac{1}{2}\tau^2$$
, and $C\nabla II...H = -\frac{M}{2a}$;

in fact (by LIII., comp. (20.) (21.)),

CVIII... -
$$2H = 2(P - T) = 2P + \tau^2 = \kappa^2 - \gamma^2 = \frac{M}{a}$$
.

(49.) Integrating CIV. by parts, &c., and writing (as in 418, XII. XXII.),

CIX...
$$F = \int_0^t (T+P) dt$$
, and CX... $V = \int_0^t 2T dt$,

so that F may again be called the *Principal Function* and V the *Characteristic Function* of the motion, we have the variations,

$$\mathbf{CXI.} \quad . \quad \delta F = \mathbf{S}\tau \delta a - \mathbf{S}\tau' \delta a' - H \delta t; \quad \mathbf{CXII.} \quad . \quad \delta V = \mathbf{S}\tau \delta a - \mathbf{S}\tau' \delta a' + t \delta H;$$

in which a, a' (instead of a_0 , a) denote now what may be called the *initial* and *final vectors* (or, or') of the *orbit*; whence follow the *partial derivatives*,

CXIII...
$$D_{\alpha}F = D_{\alpha}V = \tau$$
; CXIII'... $D_{\alpha}'F = D_{\alpha}'V = -\tau'$;
CXIV... $(D_{t}F) = -H$; and CXV... $D_{\mu}V = t$;

F being here a scalar function of a, a', t, while V is a scalar function of a, a', H, if M be treated as given.

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(50.) The two vectors a, a' can enter into these two scalar functions, only through their dependent scalars r, r', s (comp. 418, (17.)); but

 $\mathbf{CXVI.} \ldots \delta r = -r^{-1}\mathbf{S}a\delta a, \quad \delta r' = -r'^{-1}\mathbf{S}a'\delta a', \quad \delta s = -s^{-1}\mathbf{S}\left(a'-a\right)\left(\delta a'-\delta a\right);$

confining ourselves then, for the moment, to the function V, and observing that we have by CXII. the formula,

CXVII... $S(\tau \delta a - \tau' \delta a') = D_r V \cdot \delta r + D_r' V \cdot \delta r' + D_s V \cdot \delta s,$

in which the variations δa , $\delta a'$ are arbitrary, we find the expressions,

CXVIII. . . $\tau = -ar^{-1}D_rV + (a'-a)s^{-1}D_sV;$

 $\mathbf{CXVIII'}...\tau' = + \alpha' r'^{-1} \mathbf{D}_{r'} \mathcal{V} + (\alpha' - \alpha) s^{-1} \mathbf{D}_{s} \mathcal{V};$

which give these others,

CXIX... $D_r V = r \nabla (a' - a) \tau : \nabla a a';$ CXIX'... $D_r' V = r' \nabla (a - a') \tau' : \nabla a a';$

and

 $CXX...D_sV = s\beta: Vaa',$

because

$$\nabla a\tau = \nabla a'\tau' = \beta.$$

(51.) But, by XCII'.,

CXXI...
$$r\tau + r'\tau' = (r + r')v' ||v||a' - a,$$

the chord $\mathbf{T}\mathbf{T}'$ of the hodograph, in figs. 86, 87, being divided at \mathbf{U}' into segments $\mathbf{T}\mathbf{U}'$, $\mathbf{U}'\mathbf{T}'$, which are inversely as the distances r, r', or as the lines or, or' in the orbit; we have therefore the partial differential equation,

CXXII...
$$D_r V = D_{r'} V$$
, and similarly, CXXIII... $D_r F = D_{r'} F$;

so that each of the two functions, F and V, depends on the distances r, r', only by depending on their sum, r + r'.

(52.) Hence, if for greater generality we now treat M as variable, the *Principal Function* F, and therefore by CXIV. its partial derivative $H = -(D_t F)$, are functions of the *four* scalars,

$$\mathbf{CXXIV}$$
... $r + r'$, s, t, and M .

2 S 2

(53.) And in like manner, the Characteristic Function (or Action-Function) V, and its partial derivative (by CXV.) the Time, $t = D_{\pi}V$, may be considered as functions of this other system of four scalars (comp. (47.)),

$$CXXV...r + r'$$
, s, H, and M;

no knowledge whatever being here assumed, of the form or properties of the *orbit*, but only of the *law* of attraction.

(54.) But this dependence of the *time*, t, on the four scalars CXXV., is a new form of *Lambert's Theorem* (47.); which celebrated theorem is thus obtained in a new way, by the foregoing *quaternion analysis*.

(55.) Squaring the equations CXVIII. CXVIII'., attending to the relation CXXII., and changing signs, we get these new partial differential equations,

CXXVI...
$$2P + 2H = (\mathbf{D}_r \mathbf{\mathcal{V}})^2 + (\mathbf{D}_s \mathbf{\mathcal{V}})^2 + \frac{r^2 - r'^2 + s^2}{r'^8} \mathbf{D}_r \mathbf{\mathcal{V}} \cdot \mathbf{D}_s \mathbf{\mathcal{V}};$$

CXXVI'...
$$2P' + 2H = (D_r V)^2 + (D_s V)^2 + \frac{r'^2 - r^2 + s^2}{r's} D_r V. D_s V;$$

because

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CXXVII...
$$a^2 = -r^2$$
, $a'^2 = -r'^2$, $(a'-a)^2 = -s^2$.

Hence, by merely algebraical combinations (because $P = Mr^{-1}$, and $P' = Mr'^{-1}$), we find:

$$CXXVIII. \dots \frac{1}{2}((D_r V)^2 + (D_s V)^2) = H + \frac{M}{r + r' + s} + \frac{M}{r + r' - s};$$

$$CXXIX. \dots D_r V. D_s V = \frac{M}{r + r' + s} - \frac{M}{r + r' - s};$$

$$CXXX. \dots (D_r V + D_s V)^2 = 2H + \frac{4M}{r + r' + s} = M\left(\frac{4}{r + r' + s} - \frac{1}{a}\right);$$

$$CXXX'. \dots (D_r V - D_s V)^2 = 2H + \frac{4M}{r + r' - s} = M\left(\frac{4}{r + r' - s} - \frac{1}{a}\right);$$
(56.) But, by CX1I. CXVII. CXX1I., we have the variation,

$$CXXXI. \dots \delta V - t\delta H = \frac{1}{2}(D_r V + D_r V) \delta (r + r' + s)$$

 $+\frac{1}{2}(D_r V - D_s V) \delta (r + r' - s);$

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and the function V vanishes with t, and therefore with s, at least at the commencement of the motion; whence it is easy to infer the expressions,*

$$\begin{aligned} \mathbf{CXXXII.} & . \ . \ V = \int_{-s}^{s} \left(\frac{M}{r+r'+s} + \frac{H}{2} \right)^{\frac{1}{2}} \mathrm{d}s = \int_{-s}^{s} \left(\frac{M}{r+r'+s} - \frac{M}{4a} \right)^{\frac{1}{2}} \mathrm{d}s ; \\ \mathbf{CXXXIII.} & . \ . \ t = \frac{1}{4} \int_{-s}^{s} \left(\frac{M}{r+r'+s} + \frac{H}{2} \right)^{-\frac{1}{2}} \mathrm{d}s = \frac{1}{2} \int_{-s}^{s} \left(\frac{4M}{r+r'+s} - \frac{M}{a} \right)^{-\frac{1}{2}} \mathrm{d}s. \end{aligned}$$

As a verification, \dagger when t and s are small, and therefore r' nearly = r, we have thus the approximate values,

CXXXIV...
$$V = (2P + 2H)^{\frac{1}{2}s} = (2T)^{\frac{1}{2}s} = 2Tt;$$

CXXXV... $t = (2P + 2H)^{-\frac{1}{2}s} = (2T)^{-\frac{1}{2}s};$

in which s may be considered to be a small arc of the orbit, and $(2T)^{\frac{1}{2}}$ the velocity with which that arc is described.

(57.) Some not inelegant constructions, deduced from the theory of the hodograph, might be assigned for the case of a *closed orbit*, to represent the *excentric* and *mean anomalies*; but whether the orbit be closed or *not*, the *arc* **TMT'** of the *hodographic circle*, in fig. 86, represents the arc of *true anomaly* described: for it subtends at the hodographic *centre* H an *angle* THT', which is equal to the *angular motion* POF' in the orbit.

(58.) We may add that, whatever the *special form* of the orbit may be, the equations CXVIII. CXVIII'. give, by CXXII.,

$$\mathbf{CXXXVI.} \, \cdot \, \tau' - \tau = (\mathbf{U}a' + \mathbf{U}a) \mathbf{D}_r V;$$

from which it follows that the chord TT' of the hodograph is parallel to the bisector of the angle POP' in the orbit : and therefore, by XCI., that this angle is bisected by oo in fig. 87, so that the segments PR, RP', in that figure, of the chord PP' of the orbit, are inversely proportional to the segments TU', U'T' of the chord TT' of the hodograph.

^{*} Expressions by definite integrals equivalent to these, for the *action* and *time* in the relative motion of a binary system, were deduced by the present writer, but by an entirely different analysis, in the *First Essay*, &c., already eited, and will be found in the *Phil. Trans.* for 1834, Part ii., pages 285, 286. It is supposed that the radical in CXXXIII. does not become infinite within the extent of the integration; if it did so become, transformations would be required, on which we cannot enter here.

[†] An analogous verification may be applied to the definite integral LXXXI.; in which however it is to be observed that *both* r + r' and *s vary*, along with the variable w: whereas, in the secent integrals CXXXII. CXXXIII., r + r' is treated as *constant*.

[III. III. § 8.

(59.) We arrive then thus, in a new way, and as a new verification, at this known theorem : that if two tangents (QP, QP') to a conic section be drawn from any common point (Q), they subtend equal angles at a focus (O), whatever the special form of the conic may be.

(60.) And although, in several of the preceding sub-articles, geometrical constructions have been used only to illustrate (and so to confirm, if confirmation were needed) results derived through calculation with quaternions; yet the eminently suggestive nature of the present Calculus enables us, in this as in many other questions, to dispense with its own processes, when once they have indicated a definite train of geometrical investigation, to serve as their substitute.

(61.) Thus, after having in any manner been led to perceive that, for the motion above considered, the hodograph is a circle^{*} (5.), of which the radius HT is equal (7.) to the attracting mass M, divided by the constant parallelogram (16.) under the vectors or, or of position and velocity, in the recent figures 86 and 87, which parallelogram is equal to the rectangle under the distance or in the orbit, and the perpendicular oz let fall from the centre o of force on the tangent ur to the hodograph, we see geometrically that the potential P, or the mass divided by the distance, for the point r of the orbit corresponding to the point r of the hodograph, is equal (as in (27.)) to the rectangle under HT and oz, and therefore, by the similar triangles HTV, uoz, to the rectangle under ou and TV (as in (29.)).

(62.) In like manner, the three potentials corresponding to the second point \mathbf{T}' of the first hodograph, and to the points w and w' of the second hodograph, in fig. 86, are respectively equal to the rectangles under the same line ou, and the three other perpendiculars $\mathbf{T}'\mathbf{v}'$, wx, w'x', on what we have called (29.) the hodographic axis, HL; so that, for these two pairs of points, in which the two circular hodographs, with a common chord MM', are cut by a common orthogonal with u for centre, the four potentials are directly proportional to the four hodographic ordinates (29.).

(63.) And because the force (Mr^{-2}) is equal to the square of the potential (Mr^{-1}) , divided by the mass (M), the four forces are directly as the squares of the four ordinates corresponding; each force, when divided by the square of

^{*} This follows, among other ways, from the general value XXVI. for the radius of curvature of the hodograph, with any law of central force; which value was geometrically deduced, as stated in the Note to page 302, compare the Note to page 300, by the present writer, in a Paper read before the Royal Irish Academy in 1846, and published in their Proceedings. In fact, that general expression for the radius of hodographic curvature may be obtained with great facility, by dividing the element fdt of the hodograph (in which f denotes the force), by the corresponding element $er^{-2}dt$ of angular motion in the orbit.

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the corresponding hodographic ordinate, giving the constant or common quotient,

$CXXXVII...\overline{ou}^2: M.$

(64.) It has been already seen (31.) to be a geometrical consequence of the two pairs of similar triangles, NTT, NT,'T', and NTV, NT'V', that the *two* small arcs of the first hodograph, near T and T', intercepted between two near secants from the pole N of the fixed chord MM', or between two near orthogonal circles, with u and u, for centres, are proportional to the *two ordinates*, TV, T'V'.

(65.) Accordingly, if we draw, as in fig. 86, the *near radius* (represented by a dotted line from H) of the first hodograph, and also the *small perpendicular* ux, erected at the centre u of the first orthogonal to the tangent ur, and terminated in x by the tangent from the near centre u, the two new pairs of similar triangles, THT, UTY, and THV, uu_x , give the proportion,

$$CXXXVIII...TT_{,:TV} = UU_{,:UT};$$

which not merely confirms what has just been stated (64.), for the case of the *first* hodograph, but proves that the *four small arcs*, of the *two circular hodo-graphs* in fig. 86, intercepted between the two near orthogonals, are directly proportional to the *four ordinates* already mentioned.

(66.) But the time of describing any small hodographic arc is the quotient (32.) of that arc divided by the force; and therefore, by (63.), (65.), the four small times are inversely proportional to the four ordinates. And the harmonic mean U'L between the two ordinates TV, T'V' of the first hodograph, does not vary when we pass to the second, or to any other hodograph, with the same fixed chord MM', and the same orthogonal circles; it follows then, geometrically, that the sum (33.) of the two small times is the same, in any one hodograph as in any other, under the conditions above supposed : and that this sum is equal to the expression,

$$\mathbf{CXXXIX.} \dots \frac{2M \dots \overline{\mathbf{UU}'}}{\overline{\mathbf{0U}^2} \dots \overline{\mathbf{UT}} \dots \overline{\mathbf{U'L}}} = \frac{2M \dots \overline{\mathbf{UU'}} \dots \overline{\mathbf{UL}}}{\overline{\mathbf{0U}^2} \dots \overline{\mathbf{LM}^2} \dots \overline{\mathbf{UT}}},$$

which agrees with the formula LXXIII.

(67.) On the whole, then, it is found that the *Theorem of Hodographic Isochronism* (38.) admits of being geometrically^{*} proved, although by processes

^{*} It appears from an unprinted memorandum, to have been nearly thus that the author orally deduced the theorem, in his communication of March, 1847, to the Royal Irish Academy; although, as usually happens in cases of invention, his own previous processes of investigation had involved principles and methods, of a much less simple character.

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suggested (60.) by quaternions: and sufficient hints have been already given, in connexion with fig. 87, as regards the geometrical passage from that theorem to the well-known Theorem of Lambert, without necessarily employing any property of conic sections.

420. As a *fifth specimen*, we shall deduce by quaternions an equation, which is adapted to assist in the determination of the *distance* of a *comet*, or *new planet*, from the *earth*.

(1.) Let M be the mass of the sun, or (somewhat more exactly) the sum of the masses of sun and earth; and let a and ω be the heliocentric vectors of earth and comet. Write also,

I...
$$Ta = r$$
, $T\omega = w$, $T(\omega - a) = z$, $U(\omega - a) = \rho$,

so that r and w are the distances of earth and comet from the sun, while s is their distance from each other, and ρ is the unit-vector, directed from earth to comet. Then (comp. 419, I.),

and with $II...D^{2}a = -Mr^{-3}a, D^{2}\omega = -Mw^{-3}\omega,$ $III...D^{2}.z\rho = D^{2}(\omega - a) = M(r^{-3} - w^{-3})a - Mzw^{-3}\rho,$ $IV...w^{2} = -(a + z\rho)^{2} = r^{2} + z^{2} - 2zSa\rho.$

(2.) The vector a, with its tensor r, and the mass M, are given by the theory of the earth (or sun); and ρ , $D\rho$, $D^2\rho$ are deduced from three (or more) near observations of the comet; operating then on III. with $S \cdot \rho D\rho$, we arrive at the formula,

 $\nabla \ldots \frac{\mathrm{S}\rho\mathrm{D}\rho\mathrm{D}^{2}\rho}{\mathrm{S}\rho\mathrm{D}\rho\mathrm{U}a} = \frac{r}{z}\left(\frac{M}{r^{3}}-\frac{M}{w^{3}}\right);$

which becomes by IV., when cleared of fractions and radicals, and divided by z, an algebraical equation of the seventh degree, whereof one root is the sought distance^{*} z, of the comet, (or planet) from the earth.

421. As a sixth specimen, we shall indicate a method, suggested by quaternions, of developing and geometrically decomposing the disturbing force of the sun on the moon, or of a relatively superior on a relatively inferior planet.

^{*} Compare the equation in the *Mécanique Céleste* (Tom. I., p. 241, new edition, Paris, 1843). Laplace's rule for determining, by inspection of a globe, which of the two bodies is the nearer to the sur, results at once from the formula V.

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(1.) Let a, σ be the geocentric vectors of moon and sun; r, s their geocentric distances $(r = Ta, s = T\sigma)$; M the sum of the masses of earth and moon; and S the mass of the sun; then the differential equation of motion of the moon about the earth may be thus written (comp. 418, 419),

I...
$$D^2 a = M \cdot \phi a + S \cdot (\phi \sigma - \phi (\sigma - a)),$$

if D be still the mark of derivation relatively to the time, and

II...
$$\phi a = \phi(a) = a^{-1}Ta^{-1};$$

so that ϕa is here a vector-function of a, but not a linear one.

(2.) If we confine ourselves to the term $M\phi a$, in the second member of I., we fall back on the equation 419, I., and so are conducted anew to the laws of undisturbed relative elliptic motion.

(3.) If we denote the remainder of that second member by η , then η may be called the Vector of Disturbing Force; and we propose now to develope this vector, according to descending powers of $T(\sigma:a)$, or according to ascending powers of the quotient r:s, of the distances of moon and sun from the earth.

(4.) The expression for that vector may be thus transformed :*

III... Vector of Disturbing Force =
$$\eta = D^2 a - M\phi a$$

= $Ss^{-1}\sigma^{-1}\{1 - (1 - a\sigma^{-1})^{-1}T(1 - a\sigma^{-1})^{-1}\}$
= $Ss^{-1}\sigma^{-1}\{1 - (1 - a\sigma^{-1})^{-\frac{3}{2}} \quad (1 - \sigma^{-1}a)^{-\frac{3}{2}}\}$
= $Ss^{-1}\sigma^{-1}\{1 - (1 + \frac{3}{2}a\sigma^{-1} + \frac{3 \cdot 5}{2 \cdot 4}(a\sigma^{-1})^2 + ...)(1 + \frac{1}{2}\sigma^{-1}a + \frac{1 \cdot 3}{2 \cdot 4}(\sigma^{-1}a)^2 + ...)\};$
that is,
IV..., $n = n_1 + n_2 + n_3 + \&c.,$

if

$$1 \vee \ldots \eta = \eta_1 + \eta_2 + \eta_3 + \alpha c.,$$

a

$$\mathbf{V}...\eta_{1} = -Ss^{-1}\sigma^{-1}(\frac{1}{2}\sigma^{-1}a + \frac{3}{2}a\sigma^{-1}) = \frac{S}{2s^{3}}(a + 3\sigma a\sigma^{-1}) = \eta_{1,1} + \eta_{1,2};$$

VI. . .
$$\eta_2 = \frac{357^{-1}}{8s^5} (a\sigma a^{-1} + 2\sigma + 5\sigma a\sigma a^{-1}\sigma^{-1}) = \eta_{2,1} + \eta_{2,2} + \eta_{2,3};$$
 &c.

the general term+ of this development being easily assigned.

* [Observe that $(\sigma - \alpha)^{-1} = \{(1 - \alpha \sigma^{-1})\sigma\}^{-1} = \sigma^{-1}(1 - \alpha \sigma^{-1})^{-1}.$]

⁺ Such a general term was in fact assigned and interpreted in a communication of June 14, 1847, to the Royal Irish Academy (*Proceedings*, vol. iii., p. 514); and in the *Lectures*, page 616. The development may also be obtained, although less easily, by *Taylor's Series* adapted to quaternions. Compare pages 473, 475, 477, 478, vol. i. of the present work; and see page 358, vol. i., &c., for the interpretation of such symbols as $\sigma a \sigma^{-1}$.

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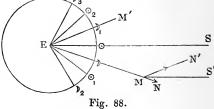
(5.) We have thus a *first group* of *two* component and disturbing forces, which are of the same order as $\frac{Sr}{s^3}$; a second group of three such forces, of the Sr^2

same order as $\frac{Sr^2}{s^4}$; a third group of four forces, and so on.

(6.) The first component of the first group has the following tensor and versor, p_{π}

VII. . .
$$T\eta_{1,1} = \frac{Sr}{2s^3}, \quad U\eta_{1,1} = Ua;$$

it is therefore a purely *ablatitious force* MN, acting along the moon's geocentric vector EM prolonged, as in the annexed figure 88.



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(7.) The second component MN', of the same first group, has an exactly triple intensity $\overline{MN'} = \overline{3MN}$; and its direction is such that the angle NMN', between these two forces of the first group, is bisected by a line MS' from the moon, which is parallel to the sun's geocentric vector ES.

(8.) If then we conceive a line EM' from the earth, having the same direction as the last force MN', this new line will meet the heavens in what may be called for the moment a *fictitious moon* \mathfrak{I}_1 , such that the *arc* \mathfrak{I}_1 of a *great circle*, connecting it with the *true moon* \mathfrak{I} in the heavens, shall be *bisected by the sun* \mathfrak{O} , as represented in fig. 88.

(9.) Proceeding to the second group (5.), we have by ∇I . for the first component of this group,

VIII...
$$T\eta_{2,1} = \frac{3Sr^2}{8s^4}, \quad U\eta_{2,1} = Ua\sigma a^{-1} = \frac{aU\sigma}{a};$$

a line from the earth, parallel to this new force, meets therefore the heavens in what may be called a *first fictitious sun*, \bigcirc_1 , such that the are of a great circle, \bigcirc_1 , connecting it with the true sun, is *bisected by the moon* \Im , as in the same fig. 88.

(10.) The second component force, of the same second group, has an *intensity* exactly double that of the first $(T\eta_{2,2} = 2T\eta_{2,1})$; and in direction it is parallel to the sun's geocentric vector ES, so that a line drawn in its direction from the earth would meet the heavens in the place of the sun \mathfrak{O} .

(11.) The third component of the present group has an intensity which is precisely *five-fold* that of the *first* component $(T_{\eta_2, 3} = 5T_{\eta_2, 1})$; and a line

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drawn in its direction from the earth meets the heavens in a second fictitious sun \bigcirc_2 , such that the arc $\bigcirc_1 \bigcirc_2$, connecting these two fictitious suns, is bisected by the true sun \bigcirc .

(12.) There is no difficulty in extending this analysis, and this interpretation, to subsequent groups of component disturbing forces, which forces increase in number, and diminish in intensity, in passing from any one group to the next; their intensities, for each separate group, bearing numerical ratios to each other, and their directions being connected by simple angular relations.

(13.) For example, the third group consists (5.) of four small forces, $\eta_{3}, \ldots, \eta_{3}, 4$, of which the intensities are represented by $\frac{Sr^{3}}{16s^{5}}$, multiplied respectively by the four whole numbers, 5, 9, 15, and 35; and which have directions respectively parallel to lines drawn from the earth, towards a second fictitious moon \mathfrak{I}_{2} , the true moon, the first fictitious moon \mathfrak{I}_{1} (8.), and a third fictitious moon \mathfrak{I}_{2} ; these three fictitious moons, like the two fictitious suns lately considered, being all situated in the momentary plane of the three bodies E, M, S: and the three celestial arcs, $\mathfrak{I}_{2}\mathfrak{I}, \mathfrak{I}\mathfrak{I}_{3}$, being each equal to double the arc \mathfrak{IO} of apparent elongation of sun from moon in the heavens, as indicated in the above cited fig. 88.

(14.) An exactly similar method may be employed to develop or decompose the disturbing force of one *planet* on another, which is nearer than it to the sun; and it is important to observe that no supposition is here made, respecting any *smallness* of *excentricities* or *inclinations*.

422. As a seventh specimen of the physical application of quaternions, we shall investigate briefly the construction and some of the properties of *Fresnel's Wave Surface*, as deductions from his principles or hypotheses* respecting light.

(1.) Let ρ be a Vector of Ray-Velocity, and μ the corresponding Vector of Wave-Slowness (or Index-Vector), for propagation of light from an origin o, within a biaxal crystal; so that

I. . . $S\mu\rho = -1$; II. . . $S\mu\delta\rho = 0$; and therefore III. . . $S\rho\delta\mu = 0$,

^{*} The present writer desires to be understood as not expressing any opinion of his own, respecting these or any rival hypotheses. In the next Series (423), as an *eighth specimen* of application, he proposes to deduce, from a *quite different set of physical principles respecting light*, expressed however still in the language of the present Calculus, MacCullagh's Theorem of the *Polar Plane*; intending then, as a *ninth* and *final specimen*, to give briefly a quaternion transformation of a celebrated equation in partial differential coefficients, of the first order and second degree, which occurs in the theory of *heat*, and in that of the *attraction of spheroids*.

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if $\delta\rho$ and $\delta\mu$ be any infinitesimal variations of the vectors ρ and μ , consistent with the scalar equations (supposed to be as yet unknown), of the *Wave-Surface* and its *Reciprocal* (with respect to the unit-sphere round o), namely the *Surface of Wave-Slowness*, or (as it has been otherwise called) the *Index*-Surface* : the velocity of light in a vacuum being here represented by unity.

(2.) The variation $\delta\rho$ being next conceived to represent a small displacement, tangential to the wave, of a particle of ether in the crystal, it was supposed by Fresnel that such a displacement $\delta\rho$ gave rise to an elastic force, say $\delta\epsilon$, not generally in a direction exactly opposite to that displacement, but still a function thereof, which function is of the kind called by us (in the Sections III. ii. 6, and III. iii. 7) linear, vector, and self-conjugate; and which there will be a convenience (on account of its connexion with certain optical constants, a, b, c) in denoting here by $\phi^{-1}\delta\rho$ (instead of $\phi\delta\rho$): so that we shall have the two converse formulæ,

IV...
$$\delta \rho = \phi \delta \varepsilon$$
; V... $\delta \varepsilon = \phi^{-1} \delta \rho$.

(3.) The *ether* being treated as *incompressible*, in the theory here considered, so that the *normal component* $\mu^{-1}S\mu\delta\varepsilon$ of the elastic force may be neglected, or rather suppressed, there remains only the *tangential component*,

VI...
$$\mu^{-1} \nabla \mu \delta \epsilon = \delta \epsilon - \mu^{-1} S \mu \delta \epsilon$$
,

as regulating the *motion*, tangential to the wave, of a disturbed and *vibrating* particle.

(4.) If then it be admitted that, for the propagation of a rectilinear vibration, tangential to a wave of which the velocity is $T\mu^{-1}$, the tangential force (3.) must be exactly opposite in direction to the displacement $\delta\rho$, and equal in quantity to that displacement multiplied by the square $(T\mu^{-2})$ of the wave-velocity, we have, by ∇ . and ∇I , the equation,

$$\begin{aligned} \mathbf{VII.} \dots \, \phi^{-1} \delta \rho \ - \ \mu^{-1} \mathbf{S} \mu \delta \varepsilon \ = \ \mu^{-2} \delta \rho, \\ \mathbf{VIII.} \dots \, \delta \rho \ = \ (\phi^{-1} \ - \ \mu^{-2})^{-1} \mu^{-1} \mathbf{S} \mu \delta \varepsilon; \end{aligned}$$

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 \mathbf{or}

^{*} This brief and expressive name was proposed by the late Prof. MacCullagh (*Transactions* R. I. A., vol. xviii., part i., page 38), for that *reciprocal* of the wave-surface which the present writer had previously called the *Surface of Components of Wave-Slowness*, and had employed for various purposes: for instance, to pass from the *conical cusps* to the *circular ridges* of the *Wave*, and so to establish a geometrical connexion between the theories of the *two conical refractions, internal* and *external*, to which his own methods had conducted him (*Transactions* R. I. A., vol. xvii., part i., pages 125–144). He afterwards found that the same Surface had been otherwise employed by M. Cauchy (*Exercises de Mathématiques*, 1830, page 36), who did not seem however to have perceived its *reciprocal relation* to the Wave.

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INDEX SURFACE.

combining which with II., we obtain at once this Symbolical Form of the scalar equation of the Index Surface,

IX... 0 =
$$S\mu^{-1}(\phi^{-1} - \mu^{-2})^{-1}\mu^{-1};$$

or by an easy transformation,

X... 1 =
$$S\mu\phi^{-1}(\phi^{-1}-\mu^{-2})^{-1}\mu^{-1}$$
;

or finally,

XI...1 =
$$S\mu(\mu^2 - \phi)^{-1}\mu$$
;

while the *direction* of the vibration $\delta \rho$, for any given tangent plane to the wave, is determined *generally* by the formula VIII.

(5.) That formula for the displacement, combined with the expression ∇ . for the elastic force resulting, gives

if

XII...
$$\delta \rho = -\phi v S \mu \delta \epsilon$$
, and XIII... $\delta \epsilon = -v S \mu \delta \epsilon$,

XIV...
$$(\phi - \mu^2) v = \mu$$
, or XV... $v = (\phi - \mu^2)^{-1} \mu$,

 ν being thus an auxiliary vector; and because the equation XI. of the index surface gives,

XVI...
$$S_{\mu\nu} = -1$$
, while XVII... $\nabla \nu \delta \epsilon = 0$, by XIII.,

it follows that the vector v, if drawn like ρ and μ from 0, terminates on the tangent plane to the wave, and is parallel to the direction of the elastic force.

(6.) The equations XIV. XVI. give,

whence

$$\mathbf{X}\mathbf{V}\mathbf{I}\mathbf{I}\mathbf{I}\mathbf{I}\mathbf{.}\ .\ .\ \mu^{2}\upsilon^{2}-\mathbf{S}\upsilon\phi\upsilon=1,$$

XIX...
$$v^2 S_\mu \delta \mu = S_\mu \delta v = -S_\nu \delta \mu$$
,

because $\delta S_{\mu\nu} = 0$, by XVI., and $\delta S_{\nu\phi\nu} = 2S(\phi\nu \cdot \delta\nu)$, by the self-conjugate property of ϕ ; comparing then XIX. with III., we see that $\pm \rho$ (as being \perp every $\delta\mu$) has the direction of $\mu + \nu^{-1}$, and therefore, by I. and XVI., that we may write,

XX...
$$\rho^{-1} = -\mu - v^{-1}$$
; XXI... $\rho^{-2} = \mu^2 - v^{-2}$; XXII...S $\rho v = 0$;

which last equation shows, by (5.), that the ray is perpendicular (on Fresnel's principles) to the elastic force $\delta \epsilon$, produced by the displacement $\delta \rho$.

(7.) The equations XX. and XXI. show by XIV. that

XXIII... $(\rho^{-2} - \phi) v = \rho^{-1}$, whence XXIV... $v = (\rho^{-2} - \phi)^{-1} \rho^{-1}$;

we have therefore, by XXII., the following Symbolical Form (comp. (4.)) of the Equation of the Wave Surface,

XXV...
$$0 = S\rho^{-1}(\phi - \rho^{-2})^{-1}\rho^{-1};$$

or, by transformations analogous to X. and XI.,

XXVI...
$$1 = S\rho\phi(\phi - \rho^{-2})^{-1}\rho^{-1};$$
 XXVII... $1 = S\rho(\rho^{2} - \phi^{-1})^{-1}\rho;$

and we see that we can return from each equation of the wave, to the corresponding equation of the index surface, by merely changing ρ to μ , and ϕ to ϕ^{-1} : but this result will soon be seen to be included in one more general, which may be called the *Rule of the Interchanges.**

(8.) The equation XXV. may also be thus written,

XXVIII...
$$S_{\rho}(\phi - \rho^{-2})^{-1}\rho = 0;$$

* [Tait finds the envelope of the plane $S\mu\rho = -1$ subject to the condition XI., $1 = S\mu(\mu^2 - \phi)^{-1}\mu$, and thus obtains the equation of the wave surface. If we differentiate XI. and introduce the auxiliary vector v of equation XIV., the result becomes $Sd\mu(v^{-1} + d\mu) = 0$. Also $S\rho d\mu = 0$, and as $d\mu$ is otherwise arbitrary

 $x\rho=v^{-1}+\mu.$

Squaring this relation we find $x^2\rho^2 = \mu^2 - v^{-2}$, and operating by S μ we have $x = \mu^2 - v^{-2} = x^2\rho^2$. Thus $x = \rho^{-2}$ and we recover XX., whence the result follows as in the text.

The equation of the electro-magnetic wave surface has been obtained by Tait on the following lines. (*Proceedings R. S. E. April 2, 1894, or Scientific Papers, vol. ii., pages 390-1.*)

A system of plane waves running with normal velocity $va = -\mu^{-1}$, (Ta = 1) is defined by

$$\theta_1 = \epsilon f(vt + Sa\rho), \quad \theta_2 = \eta f(vt + Sa\rho).$$
 (i)

These equations satisfy

so that

 $\phi_1\dot{\theta}_1 = \mathbf{V}\nabla\theta_2, \quad \phi_2\dot{\theta}_2 = -\mathbf{V}\nabla\theta_1, \tag{ii}$

the quaternion equivalents of Clerk Maxwell's electro-magnetic equations provided

$$\phi_1 \epsilon = V \mu \eta, \quad \phi_2 \eta = -V \mu \epsilon. \tag{iii}$$

Assuming the linear functions ϕ_1 and ϕ_2 to be both self-conjugate, we find on elimination of η ,

$$\phi_1 \epsilon = - \nabla \mu \phi_2^{-1} \nabla \mu \epsilon = - m_2^{-1} \nabla \mu \nabla \phi_2 \mu \phi_2 \epsilon,$$

if m_2 is the third invariant of ϕ_2 . An easy step shows that

$$m_2\phi_1\epsilon + S\mu\phi_2\mu$$
, $\phi_2\epsilon = \phi_2\mu S\mu\phi_2\epsilon$,

$$\boldsymbol{\epsilon} = (m_2 \phi_1 + \mathbf{S} \mu \phi_2 \mu \cdot \phi_2)^{-1} \phi_2 \mu \mathbf{S} \mu \phi_2 \boldsymbol{\epsilon}. \tag{iv}$$

Operating on (iv) by $S\phi_{2\mu}$, we have the equation of the index surface

$$1 = S\mu\phi_2(m_2\phi_1 + S\mu\phi_2\mu \cdot \phi_2)^{-1}\phi_2\mu.$$
 (v)

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but under this last form it coincides with the equation 412, XLI.; hence, by 412, (19.) the Wave Surface may be derived from the auxiliary or Generating Ellipsoid,

XXIX. . .
$$S\rho\phi\rho = 1$$
,

by the following Construction, which was in fact assigned by Fresnel* himself, but as the result of far more complex calculations :— Cut the ellipsoid (abc) by an arbitrary plane through its centre, and at that centre erect perpendiculars to that plane, which shall have the lengths of the semiaxes of the section; the locus of the extremities of the perpendiculars so erected will be the sought wave surface.

(9.) And we see, by IX., that the *Index Surface* may be *derived*, by an exactly similar construction, from that *Reciprocal Ellipsoid*, of which the equation is, on the same plan,

$$\mathbf{XXX.} \dots \mathbf{S}\rho\phi^{-1}\rho = 1.$$

(10.) If the scalar equations, XXVII. and XI., of the wave and index surface, be denoted by the abridged forms,

XXXI...
$$f\rho = 1$$
, and XXXII... $F\mu = 1$,

Comparing this equation with XI., we are led to assume $\mu' = \phi_2^{\frac{1}{2}}\mu$, and substitution in (v) affords the equation

$$I = S\mu'(m_2\phi_2^{-2}\phi_1\phi_2^{-2} + \mu'^2)^{-1}\mu'.$$
(vi)

The equation of the tangent plane to the wave surface is

$$S_{\mu\rho} = -1$$
, or $S_{\mu'\phi_2}^{-\frac{1}{2}}\rho = -1$, or $S_{\mu'\rho'} = -1$, (vii)

if $\rho' = \phi_2^{-\frac{1}{2}}\rho$. Comparing these results with I. and XI., we see that ρ' , μ' , and $-m_2\phi_2^{-\frac{1}{2}}\phi_1\phi_2^{-\frac{1}{2}}$ correspond respectively to Hamilton's ρ , μ , and ϕ , and we deduce the equation

$$1 = S\rho'(\rho'^2 + m_2^{-1}\phi_2^{\frac{1}{2}}\phi_1^{-1}\phi_2^{\frac{1}{2}})^{-1}\rho'$$
 (viii)

analogous to XXVII. It only remains to replace ρ' in terms of ρ by a transformation the converse of that from (v) to (vi), and we obtain the equation of the wave surface

$$1 = S_{\rho}\phi_{2}^{-1}(S_{\rho}\phi_{2}^{-1}\rho \cdot \phi_{2}^{-1} + m_{2}^{-1}\phi_{1}^{-1})^{-1}\phi_{2}^{-1}\rho, \qquad (ix)$$

or by a transformation like that from XXVII. to XXVIII.

$$S\rho(\phi_2 + m_2 S\rho \phi_2^{-1}\rho \cdot \phi_1)^{-1}\rho = 0.$$
 (x)

It will be noticed that the electro-magnetic wave-surface (ix) is produced from the Fresnel surface (viii) by the transformation or pure strain $\rho = \phi_2 \frac{1}{2} \rho'$, so that many of the theorems of these sub-articles ean be extended to this more general case.]

* See Sir John F. W. Herschel's Treatise on Light, in the *Encyclopædia Metropolitana*, page 545, Art. 1017.

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then the relations I. II. III. enable us to infer the expressions (comp. the notation in 418, (2.) [page 294]),

XXXIII...
$$\mu = \frac{-D_{\rho}f\rho}{S\rho D_{\rho}f\rho};$$
 XXXIV... $\rho = \frac{-D_{\mu}F\mu}{S\mu D_{\mu}F\mu};$

in which (comp. 412, (36.), and the Note that sub-article [page 259]),

and

$$\begin{aligned} & XXXV. \quad . \quad \frac{1}{2}D_{\rho}f\rho = (\rho^{2} - \phi^{-1})^{-1}\rho - \rho S\rho (\rho^{2} - \phi^{-1})^{-2}\rho = -\omega - \omega^{2}\rho, \\ & XXXVI. \quad . \quad \frac{1}{2}D_{\mu}F\mu = (\mu^{2} - \phi)^{-1}\mu - \mu S\mu (\mu^{2} - \phi)^{-2}\mu = -\upsilon - \upsilon^{2}\mu; \end{aligned}$$

v being the same auxiliary vector XV. as before, and ω being a new auxiliary vector, such that (by XXIV. XXVII. and IX. XV.),

XXXVII...
$$\omega = (\phi^{-1} - \rho^2)^{-1}\rho = \phi v$$
; XXXVIII... $S\rho \omega = -1$;
XXXIX... $S\mu \omega = 0$;

whence also $\omega \parallel \delta \rho$ by XII., so that (comp. (5.)) if ω be drawn (like ρ , μ , and v) from the point o, this new vector terminates on the tangent plane to the index surface, and is parallel to the displacement on the wave; also $\delta \rho : \delta \varepsilon = \omega : v$.

(11.) Hence, by XXXIII. XXXV. XXXVIII.,

XL. . .
$$\mu = \frac{\omega + \omega^2 \rho}{1 - \omega^2 \rho^2} = \frac{\omega^{-1} + \rho}{\omega^{-2} - \rho^2} = -(\omega^{-1} + \rho)^{-1}$$
, or XLI. . . $-\mu^{-1} = \rho + \omega^{-1}$;

and similarly, by XXXIV. XXXVI. and XVI.,

XLII. . .
$$\rho = \frac{\upsilon + \upsilon^2 \mu}{1 - \upsilon^2 \mu^2} = \frac{\upsilon^{-1} + \mu}{\upsilon^{-2} - \mu^2} = -(\upsilon^{-1} + \mu)^{-1}$$
, or $-\rho^{-1} = \mu + \upsilon^{-1}$, as in XX.;

so that, with the help of the expressions XV. and XXXVII. for v and ω , the ray-vector ρ and the index-vector μ are expressed as functions of each other : which functions are generally definite, although we shall soon see cases, in which one or other becomes partially indeterminate.

(12.) It is easy now to enunciate the *rule of the interchanges*, alluded to in (7.), as follows:—In any formula involving the vectors, ρ , μ , v, ω , and the functional symbol ϕ , or some of them, it is permitted to exchange ρ with μ , v with ω , and ϕ with ϕ^{-1} ; provided that we at the same time interchange $\delta\rho$ with $\delta\varepsilon$ (but not^{*} generally with $\delta\mu$), when either $\delta\rho$ or $\delta\varepsilon$ occurs.

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^{*} It is true that, in passing from II. to III. (instead of passing to XLIII.), we may be said to have exchanged not only ρ with μ , but also $\delta\rho$ and $\delta\mu$. But nsually, in the present investigation, $\delta\rho$ represents a small displacement (2.), which is conceived to have a definite direction, tangential to the wave; whereas $\delta\mu$ continues, as in (1.) to represent any infinitesimal tangent to the index surface, while $\delta\epsilon$ still denotes the elastic force (2.), resulting from the displacement $\delta\rho$.

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For example, we pass thus from XX. to XLI., and conversely from the latter to the former; from II. we pass by the same rule, to the formula,

XLIII... $S\rho\delta\epsilon = 0$, which agrees by XVII. with XXII.;

and, as other verifications, the following equations may be noticed,

XLIV. . . $\delta \rho = \mu \nabla \mu \delta \varepsilon$; **XLV.** . . $\delta \varepsilon = \rho \nabla \rho \delta \rho$; **XLVI.** . . $S \mu \delta \varepsilon = S \rho \delta \rho$.

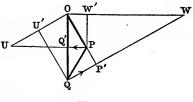
(13.) The relations between the vectors may be illustrated by the annexed figure 89; in which,

XLVII. . . $OP = \rho$, $OQ = \mu$, OU = v, $OW = \omega$, and

XLVIII. . . $OP' = -\rho^{-1}$, $OQ' = -\mu^{-1}$, $OU' = -\nu^{-1}$, $OW' = -\omega^{-1}$;

in fact it is evident on inspection, that

XLIX... $OP \cdot OP' = OQ \cdot OQ' = OU \cdot OU' = OW \cdot OW';$



and the common value of these four scalar products is here taken as negative unity.

(14.) As examples of such illustration, the equation XX. becomes $\mathbf{P}'o = \mathbf{q}\mathbf{U}'$; XLI. becomes $\mathbf{o}\mathbf{q}' = \mathbf{w}'\mathbf{P}$; XXIII. may be written as $\omega + \rho^{-1} = \rho^{-2}\boldsymbol{v}$, or as $\mathbf{P}'\mathbf{w}:\mathbf{o}\mathbf{U} = \mathbf{P}'\mathbf{o}:\mathbf{o}\mathbf{P}$; &c. And because the lines $\mathbf{Pq}'\mathbf{U}$ and $\mathbf{q}\mathbf{P}'\mathbf{w}$ are sections of the tangent planes, to the wave at the extremity \mathbf{P} of the ray, and to the index surface at the extremity \mathbf{q} of the index vector, made by the plane of those two vectors ρ and μ , while $\delta\rho$ and $\delta\epsilon$ (as being parallel to ω and \boldsymbol{v}) have the directions of \mathbf{Pq}' and $\mathbf{q}\mathbf{P}'$; we see that the displacement (or vibration) has generally, in Fresnel's theory, the direction of the projection of the ray on the tangent plane to the wave; and that the elastic force resulting has the direction of the projection of the index vector on the tangent plane to the index surface : results which might however have been otherwise deduced, from the formulæ alone.

(15.) It may be added, as regards the reciprocal deduction of the two vectors μ and ρ from each other, that (by XLI. XXXVIII., and XX. XVI.) we have the expressions,

L. . . - $\mu^{-1} = \omega^{-1} \nabla \omega \rho$, and LI. . . - $\rho^{-1} = \nu^{-1} \nabla \nu \mu$;

which answer in fig. 89 to the relations, that og' is the part (or component) of or, perpendicular to ow; and that or' is, in like manner, the part of $oq \perp ou$.

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LII. . . - $\mu^{-1} = \omega^{-1} \nabla \omega v$, and LIII. . . - $\rho^{-1} = v^{-1} \nabla v \omega$,

which may be similarly interpreted; and which conduct to the relations,

LIV... - $(\nabla v \omega)^2 = v^2 \rho^{-2} = \omega^2 \mu^{-2} = S v \omega$.

Hence, the Locus of each of the two Auxiliary Points U and w, in fig. 89, is a Surface of the Fourth Degree; the scalar equations of these two loci being,

LV...
$$(\nabla \upsilon \phi \upsilon)^2 + S \upsilon \phi \upsilon = 0$$
, and LVI... $(\nabla \omega \phi^{-1} \omega)^2 + S \omega \phi^{-1} \omega = 0$;

from which it would be easy to deduce *constructions* for those surfaces, with the help of the two *reciprocal ellipsoids*, XXIX. and XXX.

(17.) The equations XII. XXII., combined with the self-conjugate property of ϕ , give

LVII...
$$0 = S(\phi^{-1}\rho, \delta\rho)$$
, or LVIII... $0 = \delta S\rho\phi^{-1}\rho$;

hence (between suitable limits of the constant), every ellipsoid of the form,

LIX. . .
$$S\rho\phi^{-1}\rho = h^4 = \text{const.},$$

which is thus concentric and coaxal with the reciprocal ellipsoid XXX., being also similar to it, and similarly placed, contains upon its surface what may be called a Line of Vibration* on the Ware; the intersection of this new ellipsoid LIX. with the wave surface being generally such, that the tangent at each point of that line (or curve) has the direction of Fresnel's vibration.

(18.) The fundamental connexion (2.) of the function ϕ with the optical constants, a, b, c, of the crystal, is expressed by the symbolical cubic (comp. 350, I., and 417, XXV.),

LX...
$$(\phi + a^{-2}) (\phi + b^{-2}) (\phi + c^{-2}) = 0;$$

from which it is easy to infer, by methods already explained, that if e be any scalar, and if we write,

LXI...
$$E = (e - a^{-2}) (e - b^{-2}) (e - c^{-2}),$$

^{*} Such lines of vibration were discussed by the present writer, but by means of a quite different analysis, in his Memoir of 1832 (*Third Supplement on Systems of Rays*), which was published in the following year, in the *Transactions* of the Royal Irish Academy. See reference in the Note to p. 324.

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we have then this formula of inversion,

LXII...
$$E(\phi + e)^{-1} = e^2 - e(\phi + a^{-2} + b^{-2} + c^{-2}) - a^{-2}b^{-2}c^{-2}\phi^{-1}$$
.

(19.) Changing then e to $-\rho^{-2}$, the equation XXVIII. of the wave becomes,

LXIII...
$$0 = \rho^{-2} + a^{-2} + b^{-2} + c^{-2} + S\rho^{-1}\phi\rho - a^{-2}b^{-2}c^{-2}S\rho\phi^{-1}\rho$$
:

the Wave is therefore (as is otherwise known) a Surface of the Fourth Degree: and (as is likewise well known), the Index Surface is of the same degree, its equation (found by changing ρ , ϕ , a, b, c to μ , ϕ^{-1} , a^{-1} , b^{-1} , c^{-1}) being, on the same plan,

LXIV. . . 0 =
$$\mu^{-2}$$
 + a^2 + b^2 + c^2 + $S\mu^{-1}\phi^{-1}\mu$ - $a^2b^2c^2S\mu\phi\mu$.

(20.) These equations may be variously transformed, with the help of the cubic LX. in ϕ , which gives the analogous cubic in ϕ^{-1} ,

LXV...
$$(\phi^{-1} + a^2) (\phi^{-1} + b^2) (\phi^{-1} + c^2) = 0;$$

for instance, another form of the equation of the wave is,

LXVI...
$$0 = S\rho\phi^{-2}\rho + (\rho^{2} + a^{2} + b^{2} + c^{2})S\rho\phi^{-1}\rho - a^{2}b^{2}c^{2};$$

in which it may be remarked that $S\rho\phi^{-2}\rho = (\phi^{-1}\rho)^2 < 0$, whereas $S\rho\phi^{-1}\rho > 0$.

(21.) Substituting then, for $S\rho\phi^{-1}\rho$ in LXVI., its value h^4 from (17.), we find that this second variable ellipsoid, with h for an arbitrary constant or parameter,

LXVII...
$$0 = (\phi^{-1}\rho)^2 + h^4(\rho^2 + a^2 + b^2 + c^2) - a^2b^2c^2$$
,

contains upon its surface the same line of vibration as the first variable ellipsoid LIX., which involves the same arbitrary constant h; and therefore that the line in question is a quartic curve, or Curve of the Fourth Degree, as being the intersection of these two variable but connected ellipsoids: and that the wave itself is the locus of all such quartic curves.

(22.) The Generating Ellipsoid $(S_{\rho}\phi_{\rho} = 1)$ has a, b, c for its semiaxes (a > b > c > 0); and for any vector ρ , in the plane of bc, we have the symbolical quadratic (comp. 353, (9.)),

or

LXVIII...
$$(\phi + b^{-2}) (\phi + c^{-2}) = 0$$
,
LXIX... $-b^{-2}c^{-2}\phi^{-1} = \phi + b^{-2} + c^{-2}$;

making then this last substitution for $\phi + b^{-2} + c^{-2}$ in LXIII., we find, for the 2 U 2

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section of the wave by this principal plane of the ellipsoid XXIX., an equation which breaks up into the *two factors*,

LXX... $\rho^{-2} + a^{-2} = 0$, and LXXI... $1 - b^{-2}c^{-2}S\rho\phi^{-1}\rho = 0$;

whereof the *first* represents (the *plane* being understood) a *circle*, with radius = a, which we may call briefly the circle (a); while the second represents (with the same understanding) an *ellipse*, which may by analogy be called here the ellipse (a): its two semiaxes having the *lengths* of c and b, but in the directions of b and c, for which directions $\phi + b^{-2} = 0$ and $\phi + c^{-2} = 0$, respectively, so that this ellipse (a) is merely the elliptic section (bc) of the ellipsoid (abc), turned through a right angle in its own plane, as by the construction (8.) it evidently ought to be. And an exactly similar analysis shows, what indeed is otherwise known, that the plane of ca cuts the wave in the system of a circle (b), and an ellipse (b); and that the plane of ab cuts the same wave surface, in a circle (c), and an ellipse (c).

(23.) The circle (a) is entirely exterior to the ellipse (a); and the circle (c) is wholly interior to the ellipse (c); but the circle (b) cuts the ellipse (b), in four real points, which are therefore (in a sense to be soon more fully examined) cusps (or nodal points) on the wave surface, or briefly Wave-Cusps; and the vectors ρ , say $\pm \rho_0$ and $\pm \rho_1$, which are drawn from the centre o to these four cusps, may be called Lincs of Single Ray-Velocity, or briefly Cusp-Rays.

(24.) It is clear, from the construction (8.), that these lines or rays must have the directions of the *cyclic normals* of the ellipsoid (*abc*); which suggests our using here the *cyclic forms*,

and

LXXII...
$$\phi \rho = g \rho + \nabla \lambda \rho \lambda'$$
,

LXXIII. . . $S\rho\phi\rho = g\rho^2 + S\lambda\rho\lambda'\rho = 1$,

for the function ϕ , and the generating ellipsoid (8.); λ' being written, to avoid confusion, instead of the μ of 357, &c., to represent the second cyclic normal.

(25.) Changing then μ to λ' , ν to ρ , and g to $g - \rho^{-2}$, in the expression 361, XXVII.* for $F\nu$ or $S\nu\phi^{-1}\nu$; equating the result to zero, and resolving the equation so obtained, as a quadratic in g; we find this *new form* of the *Equation* XXVIII. of the Wave,

$$LXXIV...g\rho^{2} = 1 + S\lambda\rho S\lambda'\rho \pm TV\lambda\rho TV\lambda'\rho;$$

the upper sign belonging to one sheet, and the lower sign to the other sheet,

^{* [}This equation which occurs on page 549, vol. i., is $mF\nu = (g^2 - \lambda^2 \mu^2) \nu^2 + \lambda^2 (S\mu\nu)^2 + \mu^2 (S\nu\lambda)^2 - 2gS\lambda\nu S\mu\nu.]$

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of that wave surface. The new equation may also be thus written, as an expression for the *inverse square* of the *ray-velocity* T_{ρ} , or of the *radius-vector*, say r, of the wave,

$$\mathbf{LXXV}...r^{-2} = \mathbf{T}\rho^{-2} = \frac{a^{-2} + c^{-2}}{2} + \frac{a^{-2} - c^{-2}}{2}\cos\left(\angle \frac{\rho}{\lambda} \mp \angle \frac{\rho}{\lambda'}\right),$$

because, by 405, (2.), (6.), &c.,

LXXVI...
$$a^{-2} = -g - T\lambda\lambda', \quad b^{-2} = -g + S\lambda\lambda', \quad c^{-2} = -g + T\lambda\lambda';$$

and we have the verification, for a cusp-ray (23.), that

LXXVII...
$$r^{-2} = b^{-2}$$
, or $r = \mathbf{T}\rho = b$, if $\rho \parallel \lambda$ or λ' .

(26.) If we write (comp. XXXI.),

LXXVIII...
$$f\rho = -\rho^{-2}(1 + S\rho\phi\rho) + a^{-2}b^{-2}c^{-2}S\rho\phi^{-1}\rho$$
,

the equation LXIII. of the wave takes the form,

LXXIX...
$$f\rho = a^{-2} + b^{-2} + c^{-2} = \text{const.};$$

and we have the partial derivative (comp. XXXV.),

$$\begin{split} \text{LXXX.} \quad & \frac{1}{2} D_{\rho} f \rho = \rho^{-3} \left(1 + S \rho \phi \rho \right) - \rho^{-2} \phi \rho + a^{-2} b^{-2} c^{-2} \phi^{-1} \rho \\ & = \rho^{-3} \left(1 - V \rho \phi \rho \right) + a^{-2} b^{-2} c^{-2} \phi^{-1} \rho ; \end{split}$$

which gives by XXXIII. the expression,

LXXXI...
$$\mu = \frac{\rho^{-3}(\nabla \rho \phi \rho - 1) - a^{-2}b^{-2}c^{-2}\phi^{-1}\rho}{\rho^{-2} + a^{-2}b^{-2}c^{-2}S\rho\phi^{-1}\rho},$$

and therefore a generally definite value (comp. (11.)) for the index vector μ , when the ray ρ is given.

(27.) If the ray be in the plane of ac, then (comp. LXIX.),

LXXXII...
$$\phi \rho + (a^{-2} + c^{-2}) \rho + a^{-2} c^{-2} \phi^{-1} \rho = 0$$
,

whence

LXXXIII...
$$\nabla \rho \phi \rho = -a^{-2}c^{-2}\nabla \rho \phi^{-1}\rho = a^{-2}c^{-2}(S\rho \phi^{-1}\rho - \rho \phi^{-1}\rho);$$

and therefore by LXXXI.,

LXXXIV...
$$\mu = \frac{\rho^{-3} (S \rho \phi^{-1} \rho - a^2 c^2) - (\rho^{-2} + b^{-2}) \phi^{-1} \rho}{b^{-2} (S \rho \phi^{-1} \rho - a^2 c^2) + (\rho^{-2} + b^{-2}) a^2 c^2};$$

LXXXV...
$$\mu = -\rho^{-1}$$
, if LXXXVI... $\rho^{-2} + b^{-2} = 0$,
but not
LXXXVII... $S\rho\phi^{-1}\rho = a^2c^2$,

that is (comp. (22.)), if the ray terminate on the circle (b), at any point which is not also on the ellipse (b); and with equal definiteness,

LXXXVIII... $\mu = -a^{-2}c^{-2}\phi^{-1}\rho$, if LXXXVII. but not LXXXVI. hold good,

that is, if the ray terminate on the ellipse(b), at any point which is not also on the circle.

(28.) The normal then to the wave, in each of the two cases last mentioned, coincides with the normal to the section, made by the plane of ac; and if we abstract for a moment from the cusps (23.), we see that the wave is touched, along the circle (b), by the concentric sphere LXXXVI. with radius = b, which we may call the sphere (b); and along the ellipse (b) by the concentric ellipsoid LXXXVII. which may on the same plan be called the ellipsoid (b).

(29.) An exactly similar analysis shows that the wave is touched along the circles (a) and (c), by two other concentric spheres, with radii a and c, which may be briefly called *the spheres* (a) and (c); and along the ellipses (a) and (c) by two other concentric and similar ellipsoids, which may by analogy be called *the ellipsoids* (a) and (c). And by comparing the equation LXXXVII. of the ellipsoid (b) with the form LIX., we see that the *three* elliptic sections (a) (b) (c) of the wave, made by the *three principal planes* of the generating ellipsoid (abc), are *lines of vibration* (17.); the constant h^4 receiving the three values, b^2c^2 , c^2a^2 , a^2b^2 , for these three ellipses respectively.

(30.) But at a cusp the two equations LXXXVI. and LXXXVII. coexist, and the expression LXXXIV. for μ takes the *indeterminate form* $\frac{0}{0}$: in fact, there is in this case no reason for preferring *either* to the other of the two values, within the plane of ac,

LXXXIX... $\mu = -\rho_0^{-1}$, XC... $\mu = \mu_0$, if XCI... $\mu_0 = -a^{-2}c^{-2}\phi^{-1}\rho_0$;

in which ρ_0 is the *cusp-ray* (23.), and the *first* value of μ corresponds to the *circle*, but the *second* to the *ellipse* (b).

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(31.) The indetermination of μ , at a wave-cusp, is however even greater than this. For, if we observe that the equations LXXIX. and LXXX. give, for this case, by LXXXIII. LXXXVI. LXXXVII.,

XCII...
$$f_{\rho_0} = a^{-2} + b^{-2} + c^{-2}$$
, and **XCIII.**.. $D_{\rho} f_{\rho} = 0$, for $\rho = \rho_0$,

we shall see that if ρ be changed to $\rho_0 + \rho'$ in the expression LXXVIII. for f ρ , and only terms which are of the second dimension in ρ' retained, the result equated to zero will represent a cone of tangents ρ' , or a Tangent Cone to the Wave at the Cusp: which cone is of the second degree, and every normal μ to which, if limited by the condition I., is here to be considered as one value of the vector μ , corresponding to the value ρ_0 of ρ .

(32.) And it is evident, by the law (12.) of transition from the wave to the index surface, that if $\pm v_0$, $\pm v_1$ be the Lines of Single Normal Slowness, or the four values of μ which are analogous^{*} to the four cusp-rays $\pm \rho_0$, $\pm \rho_1$ (23.), then, at the end of each such new line, there must be a Conical Cusp on the Index Surface, analogous to the Conical Cusp (31.) on the Wave, which is in like manner one of four such cusps.

(33.) In forming and applying the equation above indicated (31.), of the tangent cone to the wave at a cusp, the following transformations are useful:

XCIV. . .
$$-(\rho + \rho')^{-2} = -\rho^{-2}(1 + \rho^{-1}\rho')^{-1}(1 + \rho'\rho^{-1})^{-1}$$

= $-\rho^{-2} + 2\rho^{-2}S\rho'\rho^{-1} + \rho^{-4}\rho'^{2} - 4\rho^{-6}(S\rho\rho')^{2} + \&c.$

the terms not written being of the third and higher dimensions in ρ' , and ρ , ρ' being any two vectors such that $T\rho' < T\rho$ (comp. 421, (4.)); also, without neglecting any terms the self-conjugate property of ϕ gives (comp. 362),

XCV. . .
$$S(\rho + \rho') \phi (\rho + \rho') = S\rho\phi\rho + 2S\rho'\phi\rho + S\rho'\phi\rho',$$

with an analogous transformation for the corresponding expression in ϕ^{-1} ; while the cubic LX. in ϕ , or LXV. in ϕ^{-1} , gives for an *arbitrary* ρ ,

XCVI. . .
$$\phi (\phi + a^{-2}) (\phi + c^{-2}) \rho = -b^{-2} (\phi + a^{-2}) (\phi + c^{-2}) \rho$$
,
XCVII. . . $\phi^{-1} (\phi + a^{-2}) (\phi + c^{-2}) \rho = -b^2 (\phi + a^{-2}) (\phi + c^{-2}) \rho$;

and therefore, among other transformations of the same kind,

XCVIII. . . $(\phi + a^{-2})^2 (\phi + c^{-2})^2 \rho = (a^{-2} - b^{-2}) (c^{-2} - b^{-2}) (\phi + a^{-2}) (\phi + b^{-2}) \rho$.

^{*} This word "analogous" is here more proper than "corresponding"; in fact, the cueps on each of the two surfaces will soon be seen to correspond to circles on the other, in virtue of the law of reciprocity.

We have also for a *cusp*, the values,

XCIX...
$$\phi \rho_0 = \mu_0 - (a^{-2} + c^{-2}) \rho_0$$
; XCIX'... $1 + S \rho_0 \phi \rho_0 = (a^{-2} + c^{-2}) b^2$,
C... $\mu_0^2 = a^{-4} c^{-4} S \rho_0 \phi^{-2} \rho_0 = a^{-2} b^2 c^{-2} - (a^{-2} + c^{-2})$.

(34.) In this way the equation of the tangent cone is easily found to take the form,

CI...
$$0 = b^4 S \rho'(\phi + a^{-2}) (\phi + c^{-2}) \rho' - 4 S \rho' \rho_0 S \rho' \mu_0$$

and to give, by operating with $D_{\rho'}(\text{comp. (10.) (26.) (31.)})$,

CII. . .
$$x\mu = b^4 (\phi + a^{-2}) (\phi + c^{-2}) \rho' - 2\rho_0 S \rho' \mu_0 - 2\mu_0 S \rho' \rho_0$$
,

the scalar coefficient x being determined, for each direction of the tangent ρ' to the wave at the cusp, by the condition I., which here becomes (31.)),

CIII. . .
$$S\mu\rho_0 = S\mu_0\rho_0 = -1$$
;

also, by CII., &c., we have, after some slight reductions,

$$CIV...xS\mu\rho_{0} = 2 (b^{2}S\rho'\mu_{0} + S\rho'\rho_{0});$$

$$CV...xS\mu\mu_{0} = 2 (S\rho'\mu_{0} - \mu_{0}^{2}S\rho'\rho_{0});$$

$$CVI...x^{2}\mu^{2} = 4 (b^{2}\mu_{0}^{2} + 1) S\rho'\rho_{0}S\rho'\mu_{0} + 4 (\rho_{0}S\rho'\mu_{0} + \mu_{0}S\rho'\rho_{0})^{2}$$

$$= -4b^{2} (S\rho'\mu_{0})^{2} + 4 (b^{2}\mu_{0}^{2} - 1) S\rho'\rho_{0}S\rho'\mu_{0} + 4\mu_{0}^{2} (S\rho'\rho_{0})^{2};$$

but this last expression is equal, by CIV. CV., to $-x^2 S_{\mu\rho_0}S_{\mu\mu_0}$; the equation of the cone of perpendiculars, let fall from the wave-centre o on the tangent planes at the cusp, takes then this very simple form,

$$CVII. \dots \mu^2 + S\mu\rho_0 S\mu\mu_0 = 0;$$

so that this cone of the second degree has the two vectors ρ_0 and μ_0 at once for sides and cyclic normals (comp. 406, (7.)); and it is cut, by the plane CIII., in a circle, of which the diameter is,

CVIII. . . T
$$(\mu_0 + \rho_0^{-1}) = (T\mu_0^2 - b^{-2})^{\frac{1}{2}} = b (b^{-2} - a^{-2})^{\frac{1}{2}} (c^{-2} - b^{-2})^{\frac{1}{2}};$$

and therefore subtends, at the centre o, and in the plane of ac, the angle,

UIX. . .
$$\angle \frac{\mu_0}{\rho_0} = \tan^{-1} \cdot b^2 (b^{-2} - a^{-2})^{\frac{1}{2}} (c^{-2} - b^{-2})^{\frac{1}{2}}.$$

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(35.) And by combining the equations CIII. CVII., we see that this circle (34.) is a small circle of the sphere,

CX...
$$\mu^2 = S \mu \mu_0$$
, or CX'... $S \mu^{-1} \mu_0 = 1$,

which passes through the wave-centre, and has the vector μ_0 for a diameter, passing also through the extremity of the vector $-\rho_0^{-1}$.

(36.) This circle is, by III., a curve of contact of the plane CIII. with the surface of which μ is the vector, because every vector μ of the curve corresponds, by (31.), to the one vector ρ_0 of the wave; it is therefore one of Four Circular Ridges on the Index Surface, the three others having equal diameters, and corresponding to the three remaining cusp-rays, $-\rho_0$, ρ_1 , $-\rho_1$ (23.); and there are, in like manner, Four Circular Ridges on the Wave, along which it is touched by the four planes,

CXI...
$$S\rho\nu_0 = -1$$
, $S\rho\nu_0 = +1$, $S\rho\nu_1 = -1$, $S\rho\nu_1 = +1$,

 $\pm v_0, \pm v_1$ being the four lines introduced in (32.); also the common length of the diameters, of these four circles on the wave, is (comp. CVIII.),

where

OVIT

 m_{-}

CXII...
$$T(\sigma_0 + \nu_0^{-1}) = (T\sigma_0^2 - b^2)^{\frac{1}{2}} = b^{-1}(a^2 - b^2)^{\frac{1}{2}}(b^2 - c^2)^{\frac{1}{2}},$$

CXIII... $\sigma_0 = -a^2c^2\phi\nu_0$, CXIV... $T\nu_0 = b^{-1}$, and CXV... $S\nu_0\sigma_0 = -1$:

finally, $-\nu_0^{-1}$ and σ_0 are the two values* of ρ , in the plane of *ac*, for the first of the four new circles : and the angle between these two vectors, or the angle which the diameter of the circle, in the same plane, subtends at the wave-centre, is (comp. CIX.),

CXVI. . .
$$\angle \frac{\sigma_0}{\nu_0} = \tan^{-1} \cdot b^{-2} (a^2 - b^2)^{\frac{1}{2}} (b^2 - c^2)^{\frac{1}{2}}.$$

(37.) In the recent calculations (33.) (34.), the circle of contact (36.) on the index surface was deduced from the tangent cone at a wave-cusp, as a section of a certain cone of normals CVII. to that tangent cone CI., made by the plane CIII.; but the following is a simpler, and perhaps more elegant, method of deducing and representing the same circle by means of its vector equation (comp. 392, IX. &c.), and without assuming any previous knowledge of the character, or even the existence, of that conical wave-cusp.

^{*} It is not difficult to show that these are the vectors of two points, in which the circle and ellipse (b), wherein the wave is cut by the plane of ac, are touched by a common tangent.

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(38.) In general, by eliminating the auxiliary vector v between XX. and XXIII., we arrive at the following equation,

CXVII. . .
$$(\phi - \rho^{-2}) (\mu + \rho^{-1})^{-1} = \rho^{-1};$$

which holds good for every pair of corresponding vectors ρ and μ , of the wave and index surface. And, in general, this relation is sufficient, to determine the index-vector μ , when the ray-vector ρ is given : because $(\phi + e)^{-1}0$ is generally = 0.

(39.) But when e is a root of the equation E = 0, with the signification LXI. of E, then, by the formula of inversion LXII., the symbol $(\phi + e)^{-1}0$ takes the indeterminate form $\frac{0}{0}$ and therefore, for every point of each of the three circles (a) (b) (c) of the wave, the formula CXVII. fails to determine μ : although it is only at a cusp (23.), that the value of μ becomes in fact indeterminate (comp. (27.)(28.)(29.)(30.)(31.)).

(40.) At such a cusp ($\rho = \rho_0$), the equation CXVII. takes the symbolical form,

CXVIII. . .
$$(\mu + \rho_0^{-1})^{-1} = (\phi + b^{-2})^{-1}\rho_0^{-1} = (\mu_0 + \rho_0^{-1})^{-1} + (\phi + b^{-2})^{-1}0;$$

 μ_0 retaining its recent signification XCI., and the symbol $(\phi + b^{-2})^{-1}0$ denoting any vector of the form $y\beta$, if β be the mean vector semiaxis of the generating ellipsoid XXIX., so that,

CXIX...
$$S\beta\phi\beta = 1$$
, $(\phi + b^{-2})\beta = 0$, $T\beta = b$.

(41.) Writing then for abridgment (comp. XX.),

CXX...
$$v_0 = -(\mu_0 + \rho_0^{-1})^{-1},$$

the Vector Equation of the Index Ridge (36.) is obtained under the sufficiently simple form,

CXXI...
$$V\beta (\mu + \rho_0^{-1})^{-1} + V\beta v_0 = 0;$$

and this equation does in fact represent a *Circle* (comp. 296, (7.)), which is easily proved to be the same as the *circular section* (34.), of the *cone* CVII. by the *plane* CIII.; its *diameter* CVIII. being thus found anew under the form,

CXXII...
$$Tv_0^{-1} = bTV\lambda\lambda' = b(b^{-2} - a^{-2})^{\frac{1}{2}}(c^{-2} - b^{-2})^{\frac{1}{2}}$$

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ART. 422.] DIAMETER OF CIRCLES, AND VECTOR EQUATIONS. 339 with the significations (24.) (25.) of λ , λ' ; in fact we have now the expressions,

CXXIII...
$$\rho_0 = b U \lambda$$
, $v_0 = \rho_0^{-1} (\nabla \lambda \lambda')^{-1}$,

with the verification, that

CXXIV...
$$(\phi + b^{-2}) v_0 = \lambda S \lambda' v_0 + \lambda' S \lambda v_0 = b^{-1} U \lambda = -\rho_0^{-1}$$
.

(42.) And by a precisely similar analysis, we have first the new general relation (comp. CXVII.), for any two corresponding vectors, ρ and μ ,

CXXV... $(\phi^{-1} - \mu^{-2}) (\rho + \mu^{-1})^{-1} = \mu^{-1};$

and then in particular (comp. CXVIII.), for $\mu = \nu_0$,

$$\mathbf{CXXVI.} \ . \ . \ (\rho + \nu_0^{-1})^{-1} = (\phi^{-1} + b^2)^{-1}\nu_0^{-1} = (\sigma_0 + \nu_0^{-1})^{-1} + (\phi^{-1} + b^2)^{-1}\mathbf{0};$$

so that finally, if we write for abridgment (comp. XLI. CXX.),

CXXVII...
$$\omega_0 = -(\sigma_0 + \nu_0^{-1})^{-1},$$

the Vector Equation of a Wave-Ridge is found (comp. CXXI.) to be,

$$\mathbf{CXXVIII.} \quad \mathbf{V}\boldsymbol{\beta} \left(\boldsymbol{\rho} + \boldsymbol{\nu}_0^{-1}\right)^{-1} + \mathbf{V}\boldsymbol{\beta}\boldsymbol{\omega}_0 = 0,$$

 β being still (as in CXIX.) the mean vector semiaxis of the generating ellipsoid $(S_{\rho}\phi_{\rho} = 1)$: and the diameter CXII., of this circle of contact of the wave with the first plane CXI., is thus found anew (comp. CXXII.) without any reference to cusps (37.), as the value of $T\omega_0^{-1}$.

(43.) Several of the foregoing results may be illustrated, by a new use of the last diagram (13.). Thus if we suppose, in that fig. 89, that we have the values,

CXXIX... $OP = \rho_0$, $OQ = \mu_0$, $OU = v_0$, whence CXXX... $OP' = -\rho_0^{-1}$, &c.,

then the *index-ridge* (36.), corresponding to the *wave-cusp* \mathbf{P} (23.), will be the *circle* which has $\mathbf{P'q}$ for diameter, in a *plane* perpendicular to the plane of the figure, which is here the plane of *ac*; the *cone of normals* μ (34.), to the *tungent cone* to the *wave* at \mathbf{P} , has the *wave-centre* o for its *vertex*, and *rests* on the last-mentioned circle, having also for a subcontrary *section* that *second circle* which has $\mathbf{Pq'}$ for diameter, and has its plane in like manner at right angles to the plane of \mathbf{Pq} ; also, if \mathbf{R} and \mathbf{s} be any two points on the second

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and first circles, such that ones is a right line, namely, a side μ of the cone here considered, then the *chord* PR of the second circle is *perpendicular* to this last line, and has the *direction* of the *vibration* $\delta\rho$, which answers here to the *two* vectors $\rho (= \rho_0)$ and μ : because (comp. (14.)) this chord is perpendicular to μ , but complanar with ρ and μ .

(44.) Again, to illustrate the theory of the *wave-ridge* (36.), which corresponds to a cusp (32.) on the *index-surface*, we may suppose that *this* cusp is at the point q in fig. 89, writing now (instead of CXXIX. CXXX.),

CXXXI...
$$OQ = v_0$$
, $OP = \sigma_0$, $OW = \omega_0$, $OQ' = -v_0^{-1}$, &c.

for then the *ridge* (or *circle of contact*) on the wave will coincide with the second circle (43.), and the cone of rays ρ from o, which rests upon this circle, will have the *first* circle (43.) for a sub-contrary section : also the vibration, at any point R of the wave-ridge, will have the direction of the chord Rq', for reasons of the same kind as before.

(45.) Let κ and κ' denote the bisecting points of the lines PQ' and QP', in the same fig. 89; then κ' is the centre of the index-ridge, in the case (43.); while, in the case (44.), κ is the centre of the wave-ridge.

(46.) In the first of these two cases, the point κ is not the centre of any ridge, on either wave or index-surface; but it is the centre of a certain subcontrary and circular section (43.), of the cone with o for vertex which rests upon an index-ridge; and each of its chords PR has the direction (43.), of a vibration $\delta \rho_0$, at the wave-cusp P corresponding: so that this cusp-vibration revolves, in the plane of the circle last mentioned, with exactly half the angular velocity of the revolving radius κR .

(47.) And every one of those cusp-vibrations $\delta \rho_0$, which (as we have seen) are all situated in one plane, namely, in the tangent plane at the cusp P to the ellipsoid (b) of (28.), has (as by (14.) it ought to have) the direction of the projection of the cusp-ray ρ_0 , on some tangent plane to the tangent cone to the wave, at that point P: to the determination of which last cone, by some new methods, we purpose shortly to return.

(48.) In the second of the two cases (45.), namely, in the case (44.), rq' is a diameter of a wave-ridge, with κ for the centre of that circle, and with a plane (perpendicular to that of the figure) which touches the wave at every point of the same circular ridge; and the vibration, at any such point κ , has been seen to have the direction of the chord rq', which is in fact the projection (14.) of the ray or upon the tangent plane at κ to the wave.

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(49.) And we see that, in passing from one point to another of this waveridge, the vibration Rq' revolves (comp. (46.)) round the fixed point q' of that eircle, namely, round the foot of the perpendicular from 0 on the ridge-plane, with (again) half the angular velocity of the revolving radius KR.

(50.) These laws of the two sets of vibrations, at a cusp and at a ridge upon the wave, are intimately connected with the two conical polarizations, which accompany the two conical refractions,* external and internal, in a biaxal crystal; because, on the one hand, the theoretical deduction of those two refractions is associated with, and was in fact accomplished by, the consideration of those cusps and ridges: while, on the other hand, in the theory of Fresnel, the vibration is always perpendicular to the plane of polarization. But into the details of such investigations, we cannot enter here.

(51.) It is not difficult to show, by decomposing ρ' into two other vectors, ρ'_1 and ρ'_2 , perpendicular and parallel to the plane of *ac*, that we have the general transformation, for any vector ρ' ,

CXXXII...
$$b^4 S \rho' (\phi + a^{-2}) (\phi + c^{-2}) \rho' = (S \mu_0 \rho_0 \rho')^2;$$

the equation CI. of the *tangent cone* at a *wave-cusp* may therefore be thus more briefly written,

CXXXIII...
$$(S\mu_0\rho_0\rho')^2 = 4S\rho_0\rho'S\mu_0\rho';$$

and under this form, the *cone* in question is easily proved to be the *locus* of the *normals* from the *cusp*, to that *other cone*.CVII., which has μ for a side, and the *wave-centre* o for its vertex : while the same cone CVII. is now seen, more easily than in (34.), to be reciprocally the locus of the perpendiculars from o on the tangent planes to the wave at the cusp, in virtue of the new equation CXXXIII., of the tangent cone at that point.

(52.) Another form of the equation of the cusp-cone may be obtained as follows. The equation LXXIV. of the *wave* may be thus modified (comp.

^{*} The writer's anticipation, from theory, of the two Conical Refractions, was announced at a general meeting of the Royal Irish Academy, on the 22nd of October, 1832, in the course of a final reading of that *Third Supplement on Systems of Rays*, which has been cited in a former Note (p. 324). The very elegant experiments, by which his friend, the Rev. Humphrey Lloyd, succeeded shortly afterwards in exhibiting the expected results, are detailed in a Paper On the Phenomena presented by Light, in its passage along the Axes of Biaxat Crystals, which was read before the same Academy on the 28th of January, 1833, and is published in the same first part of vol. xvii. of their Transactions. Dr. Lloyd has also given an account of the same phenomena, in a separate work since published, under the title of an Elementary Treatise on the Wave Theory of Light (London, Longmans and Co., 1857, Chapter XI.).

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LXXVI.), by the introduction of the two non-opposite cusp-rays, $\rho_0 = bU\lambda$ (CXXIII.), and $\rho_1 = bU\lambda'$:

$$\begin{aligned} \text{CXXXIV.} . . & 2a^2b^2c^2 + (a^2 + c^2) b^2\rho^2 + (a^2 - c^2) \, \text{S}\rho_0\rho \, . \, \text{S}\rho_1\rho \\ &= \mp \left(a^2 - c^2\right) \, \text{TV}\rho_0\rho \, . \, \text{TV}\rho_1\rho \, ; \end{aligned}$$

where it will be found that the first member vanishes, as well as the second, at the cusp for which $\rho = \rho_0$.

(53.) Changing then ρ to $\rho_0 + \rho'$, and retaining only terms of first dimension in ρ' (comp. (31.)), we find an equation of unifocal form (comp. 359, &c.),

$$CXXXV...S\beta_0\rho' = \mp TVa_0\rho', \text{ or } CXXXV'...(Va_0\rho')^2 + (S\beta_0\rho')^2 = 0;$$

with the two constant vectors,

CXXXVI...
$$a_0 = (b^{-2} - a^{-2})^{\frac{1}{2}} (c^{-2} - b^{-2})^{\frac{1}{2}} \rho_0$$
; CXXXVI'... $\beta_0 = \mu_0 - \rho_0^{-1}$;

and this equation CXXXV. or CXXXV'. represents the *tangent cone*, with ρ' for side, $S\beta_{0}\rho'$ being positive for one sheet, but negative for the other.

(54.) As regards the calculations which conduct to the recent expressions for a_0 , β_0 , it may be sufficient here to observe that those expressions are found to give the equations,

$$CXXXVII. \quad . \quad 2a^{2}b^{2}c^{2}a_{0} = (a^{2} - c^{2})\rho_{0}TV\rho_{0}\rho_{1};$$
$$CXXXVII'. \quad . \quad 2a^{2}b^{2}c^{2}\beta_{0} = 2(a^{2} + c^{2})b^{2}\rho_{0} + (a^{2} - c^{2})(\rho_{0}S\rho_{0}\rho_{1} - b^{2}\rho_{1});$$

and that, in deducing these, we employ the values,

CXXXVIII...
$$S\rho_0\rho_1 = \frac{b^2S\lambda\lambda'}{T\lambda\lambda'}, \quad TV\rho_0\rho_1 = \frac{b^2TV\lambda\lambda'}{T\lambda\lambda'};$$

together with the formula XCIX., and the following,

CXXXIX...
$$\phi (\rho_0 - \rho_1) = -a^{-2}(\rho_0 - \rho_1); \quad \phi (\rho_0 + \rho_1) = -c^{-2}(\rho_0 + \rho_1).$$

(55.) It is not difficult to show that the equation CXXXV. or CXXXV'., of the tangent cone at a cusp, can be transformed into the equation CXXXIII.; but it may be more interesting to assign here a geometrical interpretation, or construction, of the unifocal form last found (53.).

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(56.) Retaining then, for a moment, the use made in (43.) of fig. 89, as serving to illustrate the case of a wave-cusp at P, with the signification (45.) of the new point K' as bisecting the line P'Q, or as being the centre of the index-ridge; and conceiving a *parallel cone*, with o instead of P for vertex, and with a variable side or = ρ' ; then the cusp-ray or (= $\rho_0 \parallel a_0$) is a focal line of the new cone, and the line $OK' (= \frac{1}{2} (\mu_0 - \rho_0^{-1}) = \frac{1}{2}\beta_0)$ is the directive normal, or the normal to the director plane corresponding; and the formula CXXXV. is found to conduct to the following,

CXL. . . $\cos \kappa' \circ t = \sin \rho \circ \kappa' \sin \rho \circ t$,

which may be called a *Geometrical Equation of the Cusp-Cone*: or (more immediately) of that *Parallel Cone*, which has (as above) its vertex removed to the wave-centre o.

(57.) Verifications of CXL. may be obtained, by supposing the side or to be one of the two right lines, ρ'_1 , ρ'_2 , in which the cone is *cut* by the *plane* of the figure (or of *ac*); that is, by assuming either

CXLI... OT = $\rho'_1 = \mu_0 + \rho_0^{-1} || \text{ ou, or } \text{CXLI'... OT} = \rho'_2 = \rho_0 + \mu_0^{-1} || \text{ ow;}$

and it is easy to show, not only that these *two sides*, ou, ow, make (as in fig. 89) an *obtuse angle* with *each other*, but also that they belong to one *common sheet*, of the cone here considered, because *each* makes an *acute angle* with the directive normal $o\kappa'$.

(58.) Another way of arriving at this result, is to observe that the equation CXXXIII. takes easily the *rectangular form*,

CXLII. . . $(S\rho'(U\mu_0 + U\rho_0))^2 = (S\rho'(U\mu_0 - U\rho_0))^2 + T\mu_0\rho_0(S\rho'U\mu_0\rho_0)^2;$

the internal axis of the cusp-cone has therefore the direction of $U\mu_0 + U\rho_0$, that is, of the internal bisector of the angle roq, while the external bisector of the same angle is one of the two external axes, and the third axis is perpendicular to the plane of ρ_0, μ_0 ; but $S\rho'(U\mu_0 + U\rho_0) < 0$, whether $\rho' = \rho'_1$, or $= \rho'_2$: and therefore these two sides, ρ'_1 and ρ'_2 , belong (as above) to one sheet, because each is inclined at an acute angle to the internal axis $U\mu_0 + U\rho_0$.

(59.) It is easy to see that the second focal line of the parallel cone (56.) is μ_0 or oq; and that the second directive normal corresponding is the line ox (45.), in the same fig. 89; whence may be derived (comp. CXL.) this second geometrical equation of the cone at o,

CXLIII... $\cos \kappa o \tau = \sin \kappa o q \sin q o \tau$; with $\kappa o q = Po \kappa'$.

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(60.) And finally, as a *bifocal* but still geometrical form of the equation of the cusp-cone, with its vertex thus transferred to o, we may write,

$$CXLIV... \angle POT + \angle QOT = const. = \angle WOU.$$

(61.) Any legitimate form of any one of the four functions $\phi\rho$, $\phi^{-1}\rho$, $S\rho\phi\rho$, $S\rho\phi^{-1}\rho$, when treated by rules of the present Calculus which have been already stated and exemplified, not only conducts to the connected forms of the *three other* functions of the group, but also gives the corresponding forms of equation, of the *Ware* and the *Index-Surface*.

(62.) For instance, with the significations (32.) of ν_0 and ν_1 , the scalar function $S\rho\phi^{-1}\rho$, which is = 1 in the equation XXX. of the *Reciprocal* Ellipsoid (9.), may be expressed by the following cyclic form, with ν_0 , ν_1 for the cyclic normals of that ellipsoid,

$$CXLV...S\rho\phi^{-1}\rho = -b^{2}\rho^{2} + (a^{2} - c^{2})b^{2}S\nu_{0}\rho S\nu_{1}\rho;$$

reciprocating which (comp. 361), we are led to a bifocal form of the function $S_{\rho\phi\rho}$, which function was made = 1 in the equation XXIX. of the Generating Ellipsoid (8.), and is now expressed by this other equation (comp. 360, 407),

CXLVI...
$$\frac{4a^2c^2}{(a^2-c^2)^2}\left(\mathbf{S}\rho\phi\rho+b^{-2}\rho^2\right) = (\mathbf{S}\nu_0\rho)^2 + (\mathbf{S}\nu_1\rho)^2 - 2\frac{a^2+c^2}{a^2-c^2}\mathbf{S}\nu_0\rho\mathbf{S}\nu_1\rho;$$

 ν_0 , ν_1 being here the two (real) *focal lines* of the same ellipsoid (8.), or of its (imaginary) asymptotic cone.

(63.) Substituting then these forms (62.), of $S\rho\phi\rho$ and $S\rho\phi^{-1}\rho$, in the equation LXIII., we find (after a few reductions) this *new form* of the *Equation of the Wave*:

CXLVII. .
$$(2\rho^2 - (a^2 - c^2)S\nu_0\rho S\nu_1\rho + a^2 + c^2)^2 = (a^2 - c^2)^2 \{1 - (S\nu_0\rho)^2\} \{1 - (S\nu_1\rho)^2\};$$

whence it follows at once, that each of the four planes CXI. touches the wave, along the circle in which it cuts the quadric, with ν_0 , ν_1 for cyclic normals, which is found by equating to zero the expression squared in the first member of CXLVII. For example, the first plane CXI. touches the wave along that circle, or wave-ridge, of which on this plan the equations are,

CXLVIII... $S\nu_0\rho + 1 = 0$, $2\rho^2 + (a^2 - c^2)S\nu_1\rho - (a^2 + c^2)S\nu_0\rho = 0$; and because

CXLIX... $\phi(\nu_0 + \nu_1) = -a^{-2}(\nu_0 + \nu_1), \quad \phi(\nu_0 - \nu_1) = -c^{-2}(\nu_0 - \nu_1),$

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and therefore, with the value CXIII. of σ_0 ,

CL... $\sigma_0 = -a^2c^2\phi\nu_0 = \frac{1}{2}((a^2+c^2)\nu_0 - (a^2-c^2)\nu_1),$

the second equation CXLVIII. represents (comp. CX.) the diacentric sphere,

CLI...
$$\rho^2 = S\sigma_0\rho$$
, or CLI'... $S\sigma_0\rho^{-1} = 1$,

which passes through the *wave-centre* o, and of which the *ridge* here considered is a section. The *diameter* of that ridge may thus be shown again to have the value CXII.; and it may be observed that the circle is a section also of the *cone*,

CLII...
$$S\nu_0\rho S\sigma_0\rho = -\rho^2$$
, or CLII'... $S\nu_0\rho S\sigma_0\rho^{-1} = -1$.

(64.) It was shown in (17.) that the vibration $\delta\rho$, at any point of the wave-surface, or at the end of any ray ρ , is perpendicular to $\phi^{-1}\rho$, as well as to μ by II.; and is therefore *tangential* to the variable *ellipsoid* LIX, as well as to the *wave* itself. Hence it is easy to infer, that this vibration must have generally the direction of the auxiliary vector ω , because not only $S_{\mu\omega} = 0$, by XXXIX., but also $S_{\omega\phi} \phi^{-1}\rho = S_{\rho\phi} \phi^{-1}\omega = S_{\rho\nu} = 0$, by XXXII. and XXXVII. Indeed, this parallelism of $\delta\rho$ to ω results at once by XXXVII. from XII.

(65.) If then we denote by $\delta' \rho$ an infinitesimal vector, such as $\mu \delta \rho$, which is *tangential to the wave*, but *perpendicular to the vibration* $\delta \rho$, the parallelism $\delta \rho \parallel \omega$ will give,

CLIII... $\delta' \rho = \mu \delta \rho \parallel \mu \omega \perp \rho$, because CLIII'... $S \rho \mu \omega = 0$; whence

CLIV... $S_{\rho}\delta'_{\rho} = 0$, $\delta'T_{\rho} = 0$, or CLV... $T_{\rho} = r = \text{const.}$,

for this new direction $\delta' \rho$ of motion upon the wave.

(66.) And thus (or otherwise) it may be shown, that the Orthogonal Trajectories to the Lines of Vibration (17.) are the curves in which the Wave is cut by Concentric Spheres, such as CLV.; that is by the spheres $\rho^2 + r^2 = 0$, in which the radius r is constant for any one, but varies in passing from one to another.

(67.) The spherical curves (r), which are thus orthogonal to what we have called the *lines* (h) of vibration, are sphero-conics on the wave; either because

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each such curve (r) is, by XXVIII., situated on a concentric and quadric cone, namely,

$$\mathrm{CLVI.} \, . \, . \, 0 = \mathrm{S}\rho \, (\phi + r^{-2})^{-1}\rho ;$$

or because, by XXVII., it is on this other concentric quadric,

CLVII... - 1 =
$$S\rho (\phi^{-1} + r^2)^{-1}\rho$$
.

(68.) It is easy to prove (comp. LXXV.) that, for any *real* point of the wave, r^2 cannot be less than c^2 , nor greater than a^2 ; and that the squares of the scalar semiaxes of the new quadric CLVII. are, in algebraically ascending order, $r^2 - a^2$, $r^2 - b^2$, $r^2 - c^2$; so that this surface is generally an hyperboloid, with one sheet or with two, according as r > or < b.

(69.) And we see, at the same time, that the conjugate hyperboloid,

CLVIII... + 1 =
$$S\rho (\phi^{-1} + r^2)^{-1}\rho$$
,

which has two sheets or one, in the same two cases, r > b, r < b, and has (in descending order) the values,

CLIX...
$$a^2 - r^2$$
, $b^2 - r^2$, $c^2 - r^2$,

for the squares of *its* scalar semiaxes, is *confocal* with the generating ellipsoid XXIX.; so that the quadric CLVII. itself is the conjugate of such a confocal.

(70.) To form a distinct conception (comp. (67.)) of the course of a curve (r) upon the wave, it may be convenient to distinguish the five following cases:

CLX... (a) ...
$$r = a$$
; (β) ... $r < a, > b$; (γ) ... $r = b$;
(δ) ... $r < b, > c$; (ϵ) ... $r = c$.

(71.) In each of the *three* cases (a) (γ) (ε), the *conic* (r) becomes a *circle*, in one or other of the three principal planes: namely the circle (a), for the case (a); (b) for (γ) ; and (c) for (ε) .

(72.) In the case (β), the curve (r) is one of double curvature, and consists of two closed ovals, opposite to each other on the wave, and separated by the plane (a), which plane is not (really, met, in any point, by the complete spheroconic (r); and each separate oval crosses the plane (b) perpendicularly, in two (real) points of the ellipse (b), which are external to the circle (b): while the same oval crosses also the plane (c) at right angles, in some two real points of the ellipse (c).

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(73.) Finally, in the remaining case (δ), the ovals are separated by the plane (c), and each crosses the plane (b) at right angles, in *two* points of the ellipse (b), which are *interior* to the circle (b); crossing also perpendicularly the plane (a), in two points of the ellipse (a).

(74.) Analogous remarks apply to the *lines of vibration* (h); which are either the *ellipses* (a) (b) (c), or else *orthogonals* to the *circles* (a) (b) (c), and generally to the *sphero-conics* (r), as appears easily from foregoing results.

(75.) It may be here observed, that when we only know the direction $(U\mu)$, but not the length $(T\mu)$, of an index-vector μ , so that we have two parallel tangent planes to the wave, at one common side of the centre, the directions of the vibrations $\delta\rho$ differ generally for these two planes, according to a law which it is easy to assign as follows.

(76.) The second values of μ and $\delta\rho$ being denoted by μ , and $\delta\rho$, we have, by the equation IX. of the index-surface, these two other equations :

CLXI...
$$0 = S\mu (\phi^{-1} - \mu^{-2})^{-1}\mu;$$
 CLXI'... $0 = S\mu (\phi^{-1} - \mu^{-2})^{-1}\mu;$

of which the difference gives, suppressing the factor $\mu_{,}^{-2} - \mu^{-2}$,

or

CLXII...
$$0 = S\mu (\phi^{-1} - \mu_{\prime}^{-2})^{-1} (\phi^{-1} - \mu^{-2})^{-1}\mu;$$

CLXII'... 0 = S
$$(\phi^{-1} - \mu^{-2})^{-1} \mu (\phi^{-1} - \mu^{-2})^{-1} \mu$$
,

because $(\phi^{-1} - \mu_{,}^{-2})^{-1}$, as a functional operator, is *self-conjugate*, so that μ may be transferred from one side of it to the other; just as, if $\nu = \phi \rho$ be such a self-conjugate function of ρ , then $\nu^2 = S\nu\phi\rho = S\rho\phi\nu = S\rho\phi^2\rho$, &c.

(77.) But, by VIII., we have the parallelisms,

CLXIII... $\delta \rho \parallel (\phi^{-1} - \mu^{-2})^{-1} \mu;$ CLXIII'... $\delta \rho \parallel (\phi^{-1} - \mu^{-2})^{-1} \mu;$

hence, by CLXII'., we have the very simple relation,

CLXIV... S
$$\delta \rho \, \delta \rho_{\mu} = 0$$
;

that is, the two vibrations, in the two parallel planes, are mutually rectangular.

(78.) The following quite different method has however the advantage of not only proving anew this known relation of rectangularity, but also of assigning quaternion expressions for the two directions separately: and, at the same time, that of leading easily to what appears to be a new and elegant Geometrical Construction, simpler in some respects than the known one, which can indeed be deduced from it.

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(79.) By the first principles of Fresnel's theory (comp. (3.)), the vibration $(\delta \rho)$, on any one tangent plane to the wave, is situated in the normal plane (through μ), which contains the direction $(\delta \epsilon)$ of the elastic force; that is to say, we have the Equation of Complanarity,

$$\mathbf{CLXV...} \, \mathbf{S}\mu \delta\rho \delta\epsilon = 0.$$

(80.) We have then, by II. and V., the system of the two equations,

CLXVI...
$$S\mu\delta\rho = 0$$
, $S\mu\delta\rho\phi^{-1}\delta\rho = 0$;

comparing which with the equations of the same form,

$$S_{\nu\tau} = 0, \quad S_{\nu\tau\phi\tau} = 0, \quad 410, \nabla. \nabla I.$$

we derive at once the following Construction, which may also be expressed as a Theorem :--

"At either of the two points Q of the Reciprocal Ellipsoid XXX., the tangent plane at which is parallel to that at the given point \mathbf{P} of the Wave, the tangents to the Lines of Curvature on the Ellipsoid are parallel to the tangents to the Lines of Vibration on the Wave"; namely, to one at that given point \mathbf{P} itself, and to another at the other point \mathbf{P}' , on the same side of the centre, at which the tangent plane is parallel to each of the two others above mentioned.

(81.) Thus, for each of the two points \mathbf{P} , \mathbf{P}' the line of vibration is parallel to one of the lines of curvature at \mathbf{Q} ; and it is evident, from what precedes, that the other of these last lines has the direction of the corresponding Orthogonal (66.) at \mathbf{P} or \mathbf{P}' : nor is there any danger of confusion.

(82.) As regards quaternion expressions, for the two vibrations on a given wave-front, the sub-article, 410, (8.), with notations suitably modified, shows by its formulæ XIX. XXII. that we have here the equations,

CLXVII...
$$0 = S\mu\delta\rho\nu_0\delta\rho\nu_1 = S\mu\delta\rho\nu_0S\nu_1\delta\rho + S\mu\delta\rho\nu_1S\nu_0\delta\rho,$$

CXVIII... $\delta\rho \parallel UV\mu\nu_0 \pm UV\mu\nu_1,$

if ν_0 , ν_1 be, as in earlier formulæ of the present Series 422, the cyclic normals of the *rcciprocal ellipsoid*, which are often called the *Optic Axes* of the *Crystal*.

(83.) And hence may be deduced the known construction, namely, that "for any given direction of wave-front, the two planes of polarization, perpendicular respectively to the two vibrations in Fresnel's theory, bisect the two supplementary and diedral angles, which the two optic axes subtend at the normal to the front": or that these planes of polarization bisect, internally and externally, the angle between the two planes, $\mu\nu_0$ and $\mu\nu_1$.

and

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(84.) It may not be irrelevant here to remark, that if μ and μ , be any two index-vectors, which have (as in (76.)) the same direction, but not the same length, the equation LXIV. enables us to establish the two converse relations:

CLXIX. . .
$$abcT\mu_{\prime} = (S\mu\phi\mu)^{-\frac{1}{2}};$$
 CLXIX'. . . $abcT\mu = (S\mu_{\prime}\phi\mu_{\prime})^{-\frac{1}{2}}.$

(85.) Either by changing a, b, c, ϕ , μ to a^{-2} , b^{-2} , c^{-2} , ϕ^{-1} , ρ , or by treating the form LXIII., in (19.), of the Equation of the Wave, as we have just treated the form LXIV., of the equation of Index-Surface, in the same sub-article (19.), we see that if ρ and ρ , be any two condirectional rays $(\mathbf{U}\rho, = \mathbf{U}\rho)$, then,

and

CLXX... $(abc)^{-1}T\rho_{,} = (S\rho\phi^{-1}\rho)^{-\frac{1}{2}}, \text{ or, } abcT\rho_{,}^{-1} = (S\rho\phi^{-1}\rho)^{\frac{1}{2}};$ CLXX'... $(abc)^{-1}T\rho = S(\rho,\phi^{-1}\rho_{,})^{-\frac{1}{2}}, \text{ or, } abcT\rho^{-1} = (S\rho,\phi^{-1}\rho_{,})^{\frac{1}{2}}.$

(86.) A somewhat interesting geometrical consequence may be deduced from these last formulæ, when combined with the equation LIX. of that variable ellipsoid, $S\rho\phi^{-1}\rho = h^4$, which cuts the wave in a line of vibration (h). For if we introduce this symbol h^4 for $S\rho\phi^{-1}\rho$, and write $r_{,}$ instead of $T\rho$, to denote the length of the second ray $\rho_{,}$ the first equation CLXX. will take this simple form,

$$\mathbf{CLXXI.} \dots r_{i} = abch^{-2},$$

which shows at once that r, and h are together constant, or together variable; and therefore, that "a Line of Vibration on one Sheet of the Wave is projected into an Orthogonal Trajectory to all such Lines on the other Sheet, and conversely the latter into the former, by the Vectors ρ of the Wave": so that one of these two curves would appear to be superposed upon the other, to an eye placed at the Wave-Centre o.

(87.) The visual cone, here conceived, is represented by the equation CLVI., with some constant value of r; and as being a surface of the second degree, it ought to cut the wave, which is one of the fourth, in some curve of the eighth degree; or in some system of curves, which have the product of their dimensions equal to eight. Accordingly we now see that the complete intersection, of the cone CLVI. with the wave, consists of two curves, each of the fourth degree; one of these being, as in (67.), a complete sphero-conic (r), and the other a complete line of vibration (h): a new geometrical connexion being thus established between these two quartic curves.

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(88.) As additional verifications, we may regard the *three principal planes*, as *limits of the cutting cones*; for then, in the *plane* (a) for instance, the *circle* (a) and the *ellipse* (a), which are (in a sense) projections of each other, and of which the *latter* has been seen to be a *line of vibration*, are represented respectively by the two equations,

CLXXII...
$$r = a$$
, and CLXXII'... $bc = h^2$,

in agreement with CLXXI.; and similarly for the two other planes.

(89.) It was an early result of the quaternions, that an ellipsoid with its centre at the origin might be adequately represented by the equation (comp. 281, XXIX., or 282, XIX.),

CLXXIII...
$$T(\iota \rho + \rho \kappa) = \kappa^2 - \iota^2$$
, if $T\iota > T\kappa$;

or, without any restriction on the two vector constants, ι , κ , by this other equation,*

CLXXIII'... $T(\iota\rho + \rho\kappa)^2 = (\kappa^2 - \iota^2)^2$.

(90.) Comparing this with $S\rho\phi\rho = 1$, as the equation XXIX. of the Generating Ellipsoid, we see that we are to satisfy, independently of ρ , or as an identity, the relation (comp. 336):

CLXXIV...
$$(\kappa^2 - \iota^2)^2 \operatorname{Srpp} = (\iota \rho + \rho \kappa) (\rho \iota + \kappa \rho) = (\iota^2 + \kappa^2) \rho^2 + 2 \operatorname{Sirp} \kappa \rho;$$

which is done by assuming (comp. again 336) this cyclic form for ϕ ,

CLXXV...
$$(\kappa^2 - \iota^2)^2 \phi \rho = (\iota^2 + \kappa^2) \rho + 2\nabla \kappa \rho \iota = (\iota - \kappa)^2 \rho + 2\iota S \kappa \rho + 2\kappa S \iota \rho;$$

or as in (24.) comp. 359, III. IV.,

$$\phi \rho = g \rho + V \lambda \rho \lambda', \quad S \rho \phi \rho = g \rho^2 + S \lambda \rho \lambda' \rho = 1; \quad LXXII. \quad LXXIII.$$

^{*} This equation, CLXXIII'. or CLXXII., which had been assigned by the author as a form of the equation of an ellipsoid, has been selected by his friend Professor Peter Guthrie Tait, now of Edinburgh, as the basis of an admirable Paper, entitled: "Quaternion Investigations connected with Fresnel's Wave-Surface," which appeared in the May number for 1865, of the Quarterly Journal of Pure and Applied Mathematics; and which the present writer can strongly recommend to the careful perusal of all quaternion students. Indeed, Professor Tait, who has already published tracts on other applications of Quaternions, mathematical and physical, including some on Electro-Dynamics, appears to the writer eminently fitted to carry on, happily and usefully, this new branch of mathematical science: and likely to become in it, if the expression may be allowed, one of the chief successors to its inventor.

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CLXXVI...
$$a = T\iota + T\kappa$$
; $b = \frac{\kappa^2 - \iota^2}{T(\iota - \kappa)}$; $c = T\iota - T\kappa$;

whence conversely,

CLXXVII...
$$T_{\iota} = \frac{a+c}{2}$$
; $T_{\kappa} = \frac{a-c}{2}$; $T(\iota - \kappa) = \frac{ac}{b}$; &c.

(91.) Knowing thus the form CLXXV. of the function ϕ , which answers in the present case to the given equation CLXXIII. of the generating ellipsoid, there would be no difficulty in carrying on the calculations, so as to reproduce, in connexion with the *two* constants ι , κ , all the preceding theorems and formulæ of the present Series, respecting the Wave and the Index-Surface. But it may be more useful to show briefly, before we conclude the Series, how we can *pass* from *Quaternions* to *Cartesian Coordinates*, in any question or formula, of the kind lately considered.

(92.) The three italic letters, ijk, conceived to be connected by the four fundamental relations,

$$i^2 = j^2 = k^2 = ijk = -1,$$
 (A), 183,

were originally the only peculiar symbols of the present Calculus; and although they are not now so much used, as in the early practice of quaternions, because certain general signs of operation, such as S, V, T, U, K, have since been introduced, yet they (the symbols ijk) may be supposed to be still familiar to a student, as links between quaternions and coordinates.

(93.) We shall therefore merely write down here some leading expressions, of which the meaning and utility seem likely to be at once perceived, especially after the Calculations above performed in this Series.

^{*} The reader, at this stage, might perhaps usefully turn back to that Construction of the Ellipsoid, illustrated by fig. 53 (page 234, vol. i., and page 184), with the Remarks thereon, which were given in the few last Series of the Section II. i. 13, pages 230, 242, vol. i. It will be seen there that the three vectors, ι , κ , $\iota - \kappa$, of which the lengths are expressed by CLXXVII., are the three sides CB, CA, AB, of what may be called the Generating Triangle ABC in the figure ; and that the deduction CLXXVI., of the three semiaxes, abc, from the two vector constants, ι , κ , with many connected results, can be very simply exhibited by Geometry. The whole subject, of the equation $T(\iota\rho + \rho\kappa) = \kappa^2 - \iota^2$ of the ellipsoid, was very fully treated in the Lectures ; and the calculations may be made more general, by the transformations assigned in the long but important Section III. ii. 6 of the present Elements, so that it seems unnecessary to dwell more on it in this place.

[III. III. § 8.

(94.) The vector semiaxes of the generating ellipsoid being called a, β, γ (comp. (40.) (42.)), we may write,

$$\begin{array}{l} \text{OLXXVIII...} a = ia, \quad \beta = jb, \quad \gamma = kc; \\ \text{OLXXIX...} \phi \rho = a^{-1}\text{S}a^{-1}\rho + \beta^{-1}\text{S}\beta^{-1}\rho + \gamma^{-1}\text{S}\gamma^{-1}\rho = \Sigma a^{-1}\text{S}a^{-1}\rho = -\Sigma ia^{-2}x; \\ \text{OLXXX...} S\rho\phi\rho = \Sigma(\text{S}a^{-1}\rho)^2 = \Sigma a^{-2}x^2; \quad \text{OLXXXI...} S\rho\phi^{-1}\rho = \Sigma a^2x^2; \\ \text{OLXXXII...} (\phi + e)\rho = \Sigma a(a^{-2} + e)\text{S}a^{-1}\rho; \\ \text{OLXXXIII...} (\phi + e)^{-1}\rho = \Sigma a(a^{-2} + e)^{-1}\text{S}a^{-1}\rho; \\ \text{OLXXXIV...} \text{ if } r^2 = \text{T}\rho^2 = \Sigma r^2, \text{ then } v = r^{-2}(\phi + r^{-2})^{-1}\rho \\ = r^{-2}\Sigma \frac{a\text{S}a^{-1}\rho}{r^{-2} - a^{-2}} = -\Sigma \frac{ia^2x}{r^2 - a^2}; \\ \text{CLXXXV...} \text{ for } Wave, \quad 0 = \text{S}\rho v = \Sigma \frac{a^2x^2}{r^2 - a^2} = \frac{a^2x^2}{r^2 - a^2} + \frac{b^2y^2}{r^2 - b^2} + \frac{c^2z^2}{r^2 - c^2}; \\ \text{OR} \\ \text{CLXXXVI...} 1 = -\text{S}\rho w = -\text{S}\rho\phi v = -\text{S}v\phi\rho \\ = \Sigma \frac{x^2}{r^2 - a^2} = \frac{x^2}{r^2 - a^2} + \frac{y^2}{r^2 - b^2} + \frac{z^2}{r^2 - c^2}; \end{array}$$

and the *Index-Surface* may be treated similarly, or obtained from the *Wave* by changing *abc* to their reciprocals.

423. As an eighth specimen of physical application we shall investigate, by quaternions, Mac Cullagh's *Theorem of the Polar Plane*,* and some things therewith connected, for an important case of incidence of polarized light on a biaxal crystal: namely, for what was called by him the case of *uniradial* vibrations.

(1.) Let homogeneous light in air (or in a vacuum), with a velocity[†] taken for unity, fall on a plane face of a doubly refracting crystal, with such a polarization that only *one* refracted ray shall result ; let ρ , ρ' , ρ'' denote the *vectors of ray-velocity* of the incident, refracted, and reflected lights respectively, ρ having the direction of the *incident ray*, prolonged within the crystal, but ρ''

^{*} See pages 39, 40 of the Paper by that great mathematical and physical philosopher, "On the Laws of Crystalline Reflexion and Refraction," already referred to in the Note to page 324 (Transactions R. I. A., vol. xviii., part i.).

[†] Of course, by a suitable choice of the units of time and space, the velocities and slownesses, here spoken of, may be represented by *lines* as *short* as may be thought convenient.

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that of the reflected ray outside; and let μ' be the vector of wave-slowness, or the *index-vector* (comp. 422, (1.)), for the refracted light: these *four* vectors being all drawn from a given point of incidence o, and μ' , like ρ' , being within the crystal.

(2.) Then, by all^{*} wave theories of light, translated into the present notation, we have the equations,

I. . .
$$\rho^2 = S\mu'\rho' = \rho''^2 = -1;$$

II... $\rho'' = -\nu\rho\nu^{-1}$, with II'... $\nu = \mu' - \rho$,

where v is a normal to the face; whence also,

III. ...
$$\rho'' = \rho S \frac{\mu' + \rho}{\mu' - \rho} - 2\mu' S \frac{\rho}{\mu' - \rho};$$

IV. ... $\rho'' + \rho = 2\iota$, if IV'. ... $\iota = \nu^{-1} \nabla \mu' \rho = \nu^{-1} \nabla \nu \rho;$

and

$$\nabla \cdots \rho'' - \rho = -2\nu S\rho\nu^{-1} = -2\nu^{-1}S\rho\nu$$

so that the three vectors, ρ , μ' , ρ'' , terminate on one right line, which is perpendicular to the face of the crystal: and the bisector of the angle between the first and third of them, or between the incident and reflected rays, is the intersection ι of the plane of incidence with the same plane face.

(3.) Let τ , τ' , τ'' be the vectors of vibration for the three rays ρ , ρ' , ρ'' , conceived to be drawn from their respective extremities; then, by all theories of tangential vibration, we have the equations,

VI... $S\rho\tau = 0$; VII... $S\mu'\tau' = 0$; VIII... $S\rho''\tau'' = 0$;

to which Mac Cullagh adds the supposition (a), that the vibration in the crystal is perpendicular to the refracted ray: or, with the present symbols, that

IX...
$$S\rho'\tau' = 0$$
; whence X... $\tau' \parallel \nabla \mu' \rho'$,

the direction of the refracted vibration τ' being thus in general determined, when those of the vectors ρ' and μ' are given.

^{*} These equations may be deduced, for example, from the principles of Huyghens, as stated in his *Tractatus de Lumine* (Opera reliqua, Amst., 1728).

⁺ The equations VI. VII. VIII. hold good, for instance, on Fresnel's principles; but Fresnel's tangential vibration in the crystal has a direction *perpendicular* to that adopted by MacCullagh.

HAMILTON'S ELEMENTS OF QUATERNIONS, VOL. II.

ELEMENTS OF QUATERNIONS.

[III. m. § 8.

(4.) To deduce from τ' the two other vibrations, τ and τ'' , Mac Cullagh assumes, (b), the Principle of Equivalent Vibrations, expressed here by the formula,

XI...
$$\tau - \tau' + \tau'' = 0$$
,

in virtue of which the *three* vibrations are *parallel* to one *common plane*, and the refracted vibration is the *vector sum* (or *resultant*) of the other two; (c), the *Principle of the Vis Viva*, by which the *reflected* and *refracted lights* are *together equal* to the *incident light*, which is conceived to have *caused* them; and (d), the *Principle of Constant Density of the Ether*, whereby the masses of *ether*, disturbed by the *three lights*, are simply *proportional* to their *volumes*: the *two last* hypotheses* being here jointly expressed by the equation,

XII...
$$S_{\nu} (\rho \tau^2 - \rho' \tau'^2 + \rho'' \tau''^2) = 0.$$

(5.) Eliminating ρ'' and τ'' from XII. by V. and XI., τ^2 goes off; and we find, with the help of I. and II'., the following *linear equation* in τ ,

XIII...
$$2S\frac{\tau}{\tau'} = 1 + \frac{S\nu\rho'}{S\nu\rho} = \frac{S\rho\nu'}{S\rho\nu}$$
, if XIII'... $\nu' = \mu' - \rho'$;

a second such equation is obtained by eliminating ρ'' and τ'' by III. and XI. from VIII., and attending to I. VI. VII., namely,

XIV...
$$2S\rho\nu S\mu'\tau = (\rho^2 - \mu'^2)S\rho\tau' = -S\mu'\nu'S\rho\tau';$$

and a *third* linear equation in τ is given immediately by VI.

(6.) Solving then for τ , by the rules of the present Calculus, this system of the three linear and scalar equations VI. XIII. XIV., we find for the *incident vibration* the following vector expression, \dagger

$$\mathbf{X}\mathbf{V}...\tau = \frac{\nabla\rho\nu'\tau'}{2S\rho\nu}; \quad \text{or} \quad \mathbf{X}\mathbf{V}'...2\tau S\rho\nu = \tau'S\rho\nu' - \nu'S\rho\tau';$$

^{*} In the concluding Note (page 74) to this Paper, Professor MacCullagh refers to an elaborate Memoir by Professor Neumann, published in 1837 (in the Berlin Transactions for 1835), as containing precisely the same system of hypothetical principles respecting Light. But there was evidently a complete mutual independence, in the researches of those two eminent men. Some remarks on this subject will be found in the *Proceedings* of the R. I. A., vol. i., pages 232, 374, and vol. ii., page 96.

[†] The expressions XV. XVI. enable us to determine, not only the directions $U\tau$, $U\tau''$ of the *incident* and *reflected vibrations*, but also their *amplitudes* $T\tau$, $T\tau''$, or the *intensities* $T\tau^2$, $T\tau''^2$ of the incident and reflected *lights*, for any given or assumed amplitude $T\tau'$ of the *refracted vibration*, or intensity $'T\tau'^2$ of the *refracted light*, after having determined the *direction* $U\tau'$ of the refracted vibration X.

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MACCULLAGH'S POLAR PLANE.

and accordingly it may be verified by mere inspection, with the help of VII. and IX., that this vector value of τ satisfies the three scalar equations (5.). And when the *incident* vibration has been thus deduced from the *refracted*

vibration τ' , the *reflected* vibration τ'' is at once given by the formula XI., or by the expression,

$$XVI...\tau''=\tau'-\tau;$$

7.) The relation XV'. gives at once the equation of complanarity,

XVII. . . $S\nu'\tau\tau' = 0$, or the formula **XVIII.** . . $\mu' - \rho' \parallel \tau, \tau';$

if then a plane be anywhere so drawn, as to be parallel (4.) to the three vibrations τ , τ' , τ'' , it will be parallel also to the line $\mu' - \rho'$, which connects two corresponding points, on the wave and index-surface in the crystal : but this is one form of enunciation of Professor Mac Cullagh's Theorem of the Polar Plane, which theorem is thus deduced with great simplicity by quaternions, from the principles above supposed.

(8.) For example, if we suppose that or and oo, in fig. 89, represent the refracted ray ρ' , and the index vector μ' corresponding, and if we draw through the line ro a plane perpendicular to the plane of the figure, then the plane so drawn will contain (on the principles here considered) the refracted vibration τ' , and will be parallel to both the incident vibration τ and the reflected vibration τ'' ; whence the directions of the two latter vibrations may be in general determined, as being also perpendicular respectively to the incident and reflected rays, ρ and ρ'' : and then the relative intensities $(T\tau^2, T\tau'^2, T\tau'')$ of the three lights may be deduced from the relative amplitudes $(T\tau, T\tau', T\tau'')$ of the three vibrations, which may themselves be found from the three complanar directions, by a simple resolution of one line τ' into two others, of which it is the vector sum, as if the vibrations were forces.

(9.) The equations II'. IV'. V. and XIII'. enable us to express the four vectors, $\mu' (= \rho + \nu)$, $\iota (= \rho - \nu^{-1} S \nu \rho)$, $\rho'' (= \rho - 2\nu^{-1} S \nu \rho)$, and $\rho' (= \rho + \tau - \nu')$, in terms of the three vectors ρ , ν , ν' , which are connected with each other by the relation,

XIX...
$$\iota (= \rho - \nu^{-1} \mathrm{S} \nu \rho), \quad \rho'' (= \rho - 2\nu^{-1} \mathrm{S} \nu \rho), \quad \text{and} \quad \rho' (= \rho + \nu - \nu'),$$

XIX... $\nu^2 + 2\mathrm{S} \nu \rho = \mathrm{S} \nu' (\rho + \nu), \quad \text{because} \quad \mathrm{XIX'...} \mathrm{S} \nu \rho' = \mathrm{S} (\nu' - \nu) \rho,$

as in XIII., or because $\mu'^2 - \rho^2 = S\mu'\nu'$ by I. and XIII'.; and with which τ' is connected (VII. and IX.), by the two equations,

XX...
$$S(\rho + \nu)\tau' = 0$$
, and XXI... $S\nu'\tau' = 0$;

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while τ and τ'' are connected with the same three vectors, and with τ' , by the relations VI. VIII. XI. XIII., which conduct, by elimination of τ'' , to the

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following system (comp. (5.)) of three linear and scalar equations in
$$\tau$$
,

XXII...
$$S\rho\tau = 0$$
; $2S\nu\rho S\nu\tau = S\nu'(\rho + \nu)S\nu\tau'$; $2S\nu\rho S\tau'^{-1}\tau = S\nu'\rho$;

and therefore to the vector expression,

$$2\tau S_{\nu\rho} = \nabla \rho \nu' \tau'$$
, as in XV.

(10.) By these or other transformations, there is no difficulty in deducing this new equation, in which ω may be any vector,

XXIII...
$$\nabla \nu \nabla \{(\rho - \omega)\tau - (\rho' - \omega)\tau' + (\rho'' - \omega)\tau''\}\tau' = 0;$$

and conversely, when ω is thus treated as *arbitrary*, the formula XXIII., with the relations (9.) between the vectors ρ , ρ' , ρ'' , ν , ν' , μ' , but without any restriction (*except itself*) on τ , τ' , τ'' , is *sufficient* to give the *two* vector equations,

XI... $\tau - \tau' + \tau'' = 0$, and XXIV... $\rho \tau - \rho' \tau' + \rho'' \tau'' = x \nu^{-1} + y$, which

in which

XXV...
$$x = S\nu(\rho\tau - \rho'\tau' + \rho''\tau'') = S\nu\nu'\tau'$$
, and XXVI... $y = S(\rho\tau - \rho'\tau'\nu + \rho''\tau'')$;

and which conduct to the two scalar equations (among others),

and
XXVII...
$$S_{\kappa} (\rho \tau - \rho' \tau' + \rho'' \tau'') = 0$$
, if XXVII'... $S_{\kappa\nu} = 0$,
XXVIII... $S_{\nu\rho}(S_{\rho\tau} - S_{\rho}'' \tau'') = S_{\nu\rho}(S_{\mu} \tau' \tau')$;

so that if we now suppose the equations ∇I . ∇III . IX. to be given, the equation ∇II . will follow, by XXVIII.; while, as a case of XXVII., and with the signification IV. or IV'. of ι , we have the equation,

XXIX...
$$S_{\iota} \left(\rho \tau - \rho' \tau' + \rho'' \tau''\right) = 0.$$

(11.) And thus (or otherwise) it may be shown, that the *three* scalar equations VI. VIII. IX., combined with the *one* vector formula XXIII., which (on account of the arbitrary ω) is equivalent to *five* scalar equations, are sufficient to give the *same direction* of τ' , and the *same dependencies* of τ and τ'' thereon, as those expressed by the equations X. XV. XVI.; and therefore (among other consequences), to the formulæ XII. and XVII.

ART. 423.] PRINCIPLE OF EQUIVALENT MOMENTS.

(12.) But the equations VI. VIII. IX. contain what may be called the *Principle of Rectangular Vibrations* (or of vibrations rectangular to rays); and the formula XXIII. is easily interpreted (416.), as expressing what may be termed the *Principle of the Resultant Couple*: namely, the theorem, that if the three vibrations (or displacements), τ , τ' , τ'' , be regarded as three forces, RT, R'T', R'T'', acting at the ends of the three rays, ρ , ρ' , ρ'' , or OR, OR', OR'' (drawn in the directions (1.) from the point of incidence o), then this other system of three forces, RT, - R'T', R''T'' (conceived as applied to a solid body), is equivalent to a single couple, of which the plane is parallel (or the axis perpendicular) to the face of the crystal.

(13.) It follows then, by (10.) and (11.), that from these two principles,*(I.) and (II.), we can infer all the following :

(III.) the Principle of Tangential Vibrations (or of vibrations tangential to the waves);

(IV.) the Principle of Equivalent Vibrations (4.);

(V.) the Principle of the Vis Viva, as expressed (in conjunction with that of the Constant Density of the Ether) by the equation XII.;

(VI.) the Principle (or Theorem) of the Polar Plane;

And (VII.) what may be called the Principle of Equivalent Moments,[†] namely, theorem that the Moment of the Refracted Vibration (R'T') is equal to

* The word "Principle" is here employed with the usual latitude, as representing either an hypothesis assumed, or a theorem deduced, but made a ground of subsequent deduction. The principle (I.) of rectangular vibrations coincides, for the case of an ordinary medium, with the principle (III.) of tangential vibrations; but, for an extraordinary medium, except for the case (not here considered) of ordinary rays in an uniaxal crystal, these two principles are distinct, although both were assumed by MacCullagh and Neumann. The present writer has already disclaimed (in the Note to page 323) any responsibility for the physical hypotheses; so that the results given above are offered merely as instances of mathematical deduction and generalization attained through the Calculus of Quaternions.

† In a very clear and able Memoir, by Arthur Cayley, Esq. (now Professor Cayley), "On Professor MacCullagh's Theorem of the Polar Plane," which was read before the Royal Irish Academy on the 23rd of February, 1857, and has been printed in vol. vi. of the Proceedings of that Academy (pages 481-491), this name "principle of equivalent moments," is given to a statement (page 489), that "the moment of R't' round the axis AH, is equal to the sum of the moments of Rt and R"t" round the same axis"; the line AH being (page 487) the intersection of the plane of incidence with the plane of separation of the two media, that is, with the face of the crystal; while Rt, R't', R"t" are lines representing (page 488) the three vibrations (incident, refracted, and reflected), at the ends of the three rays AR, AR', AR", which are drawn from the point of incidence A, so as to lie, all three (page 487), within the crystal. And in fact, if this statement be modified, either by changing the sign of the moment of R't" (page 491), or by drawing the reflected ray AR", like the line ou" of the present investigation in the air (or in vacuo), instead of prolonging it backwards within the biaxal crystal, it agrees with the case XXIX. of the more general formula XXVII., which is itself included in what has been called above the Principle of the Resultant Couple. In venturing thus to point out, as the subject obliged him to do, what seemed to him to be a slight inadvertence in a Paper of such interest and value, the present writer hopes that he will not be supposed to

the Sum of the Moments of the Incident and Reflected Vibrations (\mathbf{RT} and $\mathbf{R''T''}$), with respect to any line, which is on, or parallel to, the Face of the Crystal.

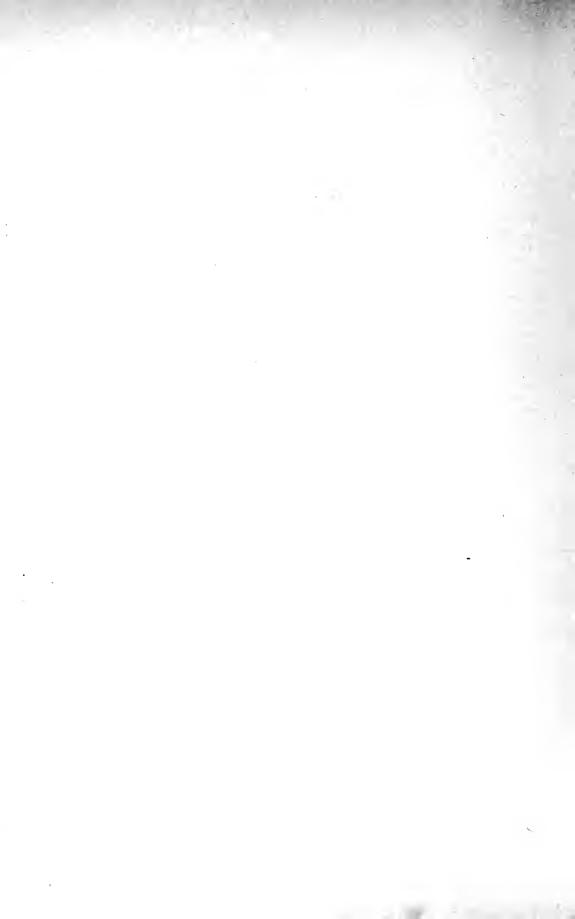
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[It appears by the Table of Initial Pages (as printed in the First Edition), that the Author had intended to complete the work by the addition of Seven Articles.]

be deficient in the admiration (long since publicly expressed by him), which is due to the vast attainments of a mathematician so eminent as Professor Cayley.

Since the preceding Series 423, including its Notes (so far), was copied and sent to the printers, the writer's attention has been drawn to a *later* Paper by MacCullagh (read December 9th, 1839, and published in vol. xxi., part i., of the *Transactions* of the Royal Irish Academy, pages 17-50), entitled "An Essay towards a Dynamical Theory of crystalline Reflexion and Refraction"; in which there is given at page 43) a theorem essentially equivalent to the above-stated "Principle of the Resultant Couple," but expressed so as to include the case where the vibrations are not uniradial, so that the double refraction of the crystal is allowed to manifest itself. MacCullagh speaks, in his enunciation of the theorem, of measuring each ray, in the direction of propagation: which agrees with, but of course anticipates, the direction of the reflected ray, adopted in the preceding investigation. The writer believes that subsequent experiments, by Jamin and others, are considered to diminish much the physical value of the theory above discussed.

APPENDIX.



NOTES.

I.-ON QUATERNION DETERMINANTS.

(1.) Quaternion determinants were first investigated by Cayley (*Phil. Mag.* xxvi., 1845, pages 141-145). Because quaternion multiplication is not commutative, a determinant whose constituents are quaternions is unmeaning until some additional convention is adopted concerning its expansion. If it be agreed that the order of the constituents in the expansion shall follow the order of the rows, all indefiniteness is removed.

(2.) On this supposition

$$\begin{vmatrix} p & q \\ p' & q' \end{vmatrix} = pq' - qp', \text{ but not } pq' - p'q ; \qquad (i)$$

$$\begin{vmatrix} p & q \\ p & q \end{vmatrix} = pq - qp = 2\nabla \cdot \nabla p \nabla q, \text{ and } \begin{vmatrix} p & p \\ q & q \end{vmatrix} = pq - pq = 0.$$
(ii)

It is also obvious that if x is any scalar

$$\begin{vmatrix} p & q \\ p' & q' \end{vmatrix} = \begin{vmatrix} p & xp + q \\ p' & xp' + q' \end{vmatrix}, \text{ but not} = \begin{vmatrix} p & q \\ xp + p' & xq + q' \end{vmatrix}.$$
 (iii)

(3.) Thus the columns may be treated as in ordinary determinants with scalar constituents; but it is not lawful to treat the rows in this manner. The former of these processes is consistent with the convention that the order of the constituents shall follow the order of the rows; the latter violates this convention.

The following example illustrates multiplication of a quaternion determinant by a scalar determinant :---

$$\begin{vmatrix} p & q \\ p' & q' \end{vmatrix} \cdot \begin{vmatrix} x & y \\ x' & y' \end{vmatrix} = \begin{vmatrix} px + qy & px' + qy' \\ p'x + q'y & p'x' + q'y' \end{vmatrix} = \begin{vmatrix} px + qx' & py + qy' \\ p'x + q'x' & p'y + q'y' \end{vmatrix}$$
(iv)

if the x and y are scalars, and the p and q determinants. This method is applicable for any order.

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APPENDIX—NOTES.

(4.) Again, when we have equations of the type

$$p_1x + q_1y + r_1z = 0$$
, $p_2x + q_2y + r_2z = 0$, $p_3x + q_3y + r_3z = 0$, (v)

in which x, y, and z are scalars, every determinant obtained by interchanging the rows in

 $\begin{vmatrix} p_1 & q_1 & r_1 \\ p_2 & q_2 & r_2 \\ p_3 & q_3 & r_3 \end{vmatrix}$ (vi)

must vanish. There are six of these. Further every determinant deducible from

$$\begin{vmatrix} p_1 & q_1 & r_1 \\ p_1 & q_1 & r_1 \\ p_2 & q_2 & r_2 \end{vmatrix} \text{ and } \begin{vmatrix} p_1 & q_1 & r_1 \\ p_1 & q_1 & r_1 \\ p_2 & q_2 & r_2 \end{vmatrix} (vii)$$

by interchange of rows and by alteration of the suffixes must be zero. For by (3.) the columns may be multiplied by x, y, and z and added together, and thus one column may be reduced to zero when equations (v) subsist.

These results may be extended to a system of linear equations of any order.

(5.) The determinants of the third order of the last section are not all independent. If the determinant (vii) with identical rows vanishes, we have by (ii)

$$p_1 \mathbf{V} \cdot \mathbf{V} q_1 \mathbf{V} r_1 + q_1 \mathbf{V} \cdot \mathbf{V} r_1 \mathbf{V} p_1 + r_1 \mathbf{V} \cdot \mathbf{V} p_1 \mathbf{V} q_1 = 0.$$
(viii)

Taking the scalar part, we see that the three vectors are coplanar, so that we may write

$$x\nabla p_1 + y\nabla q_1 + z\nabla r_1 = 0.$$

Hence, it appears by operating on this by $V.Vp_1$ and $V.Vq_1$, that (viii) may be replaced by

$$xp_1 + yq_1 + zr_1 = 0.$$
 (ix)

From this it immediately follows that the vanishing of the first determinant (vii) is equivalent to

$$xp_2+yq_2+zr_2=0.$$

If in this determinant the suffix 2 is replaced by 3, and if the new determinant vanishes, equations (v) are reproduced and all the other determinants will vanish.

In a similar manner for determinants of the second order, if we suppose that the four quaternions p_1 , q_1 , p_2 , and q_2 are not all coplanar, three of the equations

$$\begin{vmatrix} p_1 & q_1 \\ p_1 & q_1 \end{vmatrix} = 0, \qquad \begin{vmatrix} p_1 & q_1 \\ p_2 & q_2 \end{vmatrix} = 0, \qquad \begin{vmatrix} p_2 & q_2 \\ p_1 & q_1 \end{vmatrix} = 0, \qquad \begin{vmatrix} p_2 & q_2 \\ p_1 & q_1 \end{vmatrix} = 0, \qquad \begin{vmatrix} p_2 & q_2 \\ p_2 & q_2 \end{vmatrix} = 0, \quad (\mathbf{x})$$

imply the fourth, and require

$$xp_1 + yq_1 = 0, \qquad xp_2 + yq_2 = 0.$$
 (xi)

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LI.

I., II.] PROPERTIES OF TWO LINEAR VECTOR FUNCTIONS.

(6.) The determinant of the fourth order, whose rows are identical, vanishes. For if p, q, r, and s are any four quaternions, we can find scalars x, y, z, and w so that

$$xp + y\dot{q} + zr + ws = V^{-1}0 = a$$
 scalar.

One column can thus be reduced to the same scalar repeated four times, and, when we expand by the minors of the second order, every product of minors will involve a vanishing minor. By means of this result many identities may be obtained.*

II.—MISCELLANEOUS PROPERTIES OF TWO LINEAR VECTOR FUNCTIONS.

(1.) In general a pair of linear and vector functions may be simultaneously expressed in the form

$$\phi \rho = \lambda Sa\rho + \mu S\beta\rho + \nu S\gamma\rho; \quad \theta \rho = a\lambda Sa\rho + b\mu S\beta\rho + c\nu S\gamma\rho.$$
(i)

Assuming the possibility of the reduction, it is clear that

$$\theta \nabla \beta \gamma = a \phi \nabla \beta \gamma, \quad \theta \nabla \gamma a = b \phi \nabla \gamma a, \quad \theta \nabla a \beta = c \phi \nabla a \beta,$$
 (ii)

and consequently $\nabla\beta\gamma$, $\nabla\gamma a$, and $\nabla\alpha\beta$ are the axes, and *a*, *b*, and *c* the roots of the function $\phi^{-1}\theta$. The vectors *a*, β , and γ having being found, λ , μ , and ν are determined by three equations of the type

$$\lambda = \phi \nabla \beta \gamma (Sa\beta\gamma)^{-1}.$$
 (iii)

Otherwise a, β , and γ may be determined directly as the axes of the conjugate of $\phi^{-1}\theta$, that is of $\theta'\phi'^{-1}$. Combining (iii) and (ii), we see that λ , μ , and ν are the axes, and a, b, and c the roots of the new function $\theta\phi^{-1}$.

(2.) Thus it is proved that $\phi^{-1}\theta$ and $\theta\phi^{-1}$ have the same latent roots, and consequently the same symbolic cubic. More generally, all functions expressed as products of others and derivable from one another by *cyclical* transposition of the factors have the same cubic; for example, θ and $\phi\theta\phi^{-1}$.

The same thing is evident when the cubic

$$(\phi\theta)^3 - M''(\phi\theta)^2 + M'\phi\theta - M = 0$$
 (iv)

is multiplied by θ and into θ^{-1} , for it becomes

$$(\theta\phi)^3 - M''(\theta\phi)^2 + M'\theta\phi - M = 0.$$
 (v)

3 A 2

^{*} Applications and examples will be given in the Note on Invariants, and in the Note on Screws (Note V., Section 14, p. 382, and Note VIII., Section 9, page 393).

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(3.) When both functions are self-conjugate $V\beta\gamma$, $V\gamma a$, and $Va\beta$ are mutually conjugate with respect to the quadrics, $S\rho\theta\rho = const.$, $S\rho\phi\rho = const.$, at least if a, b, and c are unequal; for by (ii)

$$aSV\gamma a\phi V\beta\gamma = SV\gamma a\theta V\beta\gamma = SV\beta\gamma\theta V\gamma a = bSV\beta\gamma\phi V\gamma a,$$

$$a = b, \text{ or } SV\gamma a\phi V\beta\gamma = 0.$$
(vi)

 \mathbf{so}

From (vi) and similar relations coupled with (iii), we find in this case where the roots are unequal

$$\lambda \parallel a, \quad \mu \parallel \beta, \quad \nu \parallel \gamma. \tag{vii}$$

ſII.

(4.) Hence we can see how to reduce an arbitrary function ϕ to the product $\Phi_1 \Phi$ of two self-conjugate functions. For the axes of ϕ must be mutually conjugate to Φ and to Φ_1^{-1} , and therefore if x, y, and z are arbitrary scalars

$$\Phi \rho = x \nabla \beta \gamma S \beta \gamma \rho + y \nabla \gamma a S \gamma a \rho + z \nabla a \beta S a \beta \rho,$$

$$\Phi_1 \rho = (a x^{-1} a S a \rho + b y^{-1} \beta S \beta \rho + c z^{-1} \gamma S \gamma \rho) (S a \beta \gamma)^{-2}, \qquad (viii)$$

are the necessary forms, a, β , and γ being the axes, and a, b, and c the roots of ϕ . Even if ϕ has a pair of imaginary roots (b, c), and axes (β, γ) , the functions Φ and Φ_1 are real, provided y and s are conjugate imaginaries.*

(5.) If two functions ϕ and θ can be reduced simultaneously to the forms $\Phi_1 \Phi$ and $\Phi_2 \Phi$, the axes of ϕ and θ must be edges of a quadric cone. Let $S_{\rho} \otimes \rho = 0$ be the cone through the axes α , β , and γ of ϕ and two of the axes α' and β' of θ . Then because the axes of each function are mutually conjugate to Φ ,

$$\Phi a \parallel V \beta \gamma$$
, &c., $\Phi a' \parallel V \beta' \gamma'$, &c.

and $Sa\Theta a = 0$ is equivalent to $Sa\Theta \Phi^{-1}V\beta\gamma = 0$. Hence the first invariant of the function $\Theta \Phi^{-1}$ vanishes, or

$$Sa\Theta\Phi^{-1}V\beta\gamma + S\beta\Theta\Phi^{-1}V\gamma a + S\gamma\Theta\Phi^{-1}Va\beta = 0.$$
(ix)

Replacing α , β , γ in this invariant by α' , β' , γ' , the first and second terms vanish and the third must be zero likewise. Thus γ' is also an edge of the cone.

(6.) In the case of simple equality among the roots of $\phi^{-1}\theta$, two of its axes coincide, and the reduction (i) becomes impossible. When equality among the roots carries with it indeterminateness of the axes of $\phi^{-1}\theta$, the reduction likewise becomes indeterminate instead of being unique as in the general case.

(7.) Two functions are commutative in order of operation if, and only if, their axes coincide. The first part of the proposition is evident, and, to prove the second,

^{*} Tait shows that if the roots of ϕ are real and positive, so also are the roots of ϕ and ϕ_1 . *Proc.* R. S. E., May 18 and June 1, 1896, or *Scientific Papers*, vol. ii., p. 407.

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when the reduction (i) is possible, it is sufficient to observe that if $\phi\theta = \theta\phi$ or $\theta\phi^{-1} = \phi^{-1}\theta$, the vectors λ , μ , and ν must be parallel, respectively, to $\nabla\beta\gamma$, $\nabla\gamma\alpha$, and $\nabla\alpha\beta$. These vectors are, in this case, axes of both the functions ϕ and θ . More generally, and without postulating the possibility of the reduction, if

$$\phi \xi = g \xi$$
, then $\phi \theta \xi = \theta \phi \xi = g \theta \xi$. (x)

Thus, ξ and $\theta\xi$ are both axes of ϕ , and correspond to the same root, and this requires $\theta\xi \parallel \xi$ (so that ξ is also an axis of θ) or else, ϕ must have indeterminate axes. When the second alternative is admitted, if η is any second vector in the plane of the indeterminate axes of ϕ , $\theta\eta$ lies also in this plane, and the four vectors ξ , η , $\theta\xi$, $\theta\eta$ are coplanar. It is always possible to find two other vectors ξ' and η' in this plane, so that $\theta\xi' \parallel \xi'$ and $\theta\eta' \parallel \eta'$ and these vectors are axes of ϕ as well as of θ .

III.—THE STRAIN FUNCTION.

(1.) The application of the linear vector function to the theory of strain has been admirably developed by Professor Tait in the Tenth Chapter of Kelland and Tait's *Introduction to Quaternions*. From this source a large portion of this Note has been adapted.

When a linear vector function operates on every vector of a system, vectors originally equal remain equal after the operation; consequently, all equal similar and similarly placed figures transform into figures equal similar and similarly placed. There are two classes of this kind of transformation when the function ϕ is real. In the first rotation from ϕa to $\phi\beta$ to $\phi\gamma$ has the same sense as that from a to β to γ , whatever vectors a, β , and γ may be. In the second class the sense of rotation is reversed. The first class of transformation is identical with a homogeneous strain; the second is equivalent to a homogeneous strain accompanied by a reflection as in a plane mirror, or to a homogeneous strain accompanied by reversal of every vector. In fact, reversal of every vector is equivalent to rotation through two right angles about some axis through the origin and reflection with respect to the plane through the origin at right angles to the axis.

(2.) Hamilton's third invariant of the function ϕ

$$m = S\phi a \phi \beta \phi \gamma (Sa \beta \gamma)^{-1}$$
(i)

is the ratio which the volume of the parallelepiped, transformed from that whose edges are α , β , γ , bears to the volume of the original. It is quite independent of any particular set of vectors α , β , γ , and is, therefore, the ratio in which any volume is altered.

(3.) The sign of *m* affords the criterion concerning the class of the transformation (1.). If *m* is positive, the sense of rotation from ϕa to $\phi \beta$ to $\phi \gamma$ remains the same as that from *a* to β to γ . The contrary is the case when *m* is negative.

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(4.) In the case of a pure strain, three mutually rectangular lines preserve their directions. If unit vectors along these are i, j, and k, and if the unit vectors are strained into e_1i , e_2j , and e_3k , where e_1 , e_2 , and e_3 are three positive scalars, any other vector is strained into

$$\Phi \rho = -e_1 i \mathrm{S} i \rho - e_2 j \mathrm{S} j \rho - e_3 k \mathrm{S} k \rho. \tag{ii}$$

This is a particular case of the general theorem, that a linear vector function is determinate when the results of operating by it, on three known vectors, are given. In fact, given α , β , γ , $\phi \alpha$, $\phi \beta$, and $\phi \gamma$, we have, in general,

$$\phi \rho = (\phi \alpha S \beta \gamma \rho + \phi \beta S \gamma \alpha \rho + \phi \gamma S \alpha \beta \rho) (S \alpha \beta \gamma)^{-1}.$$

The function Φ , defined by (ii), is self-conjugate, and its latent roots e_1 , e_2 , and e_3 are all positive. A function of this nature may be said to be *ellipsoidal*.

The sphere $T\rho = r$ is changed by the transformation $\varpi = \phi \rho$ into the quadric the strain ellipsoid---determined by the equation

$$\mathrm{T}\phi^{-1}\varpi = r$$
, or $\mathrm{S}\varpi\phi'^{-1}\phi^{-1}\varpi = -r^2$ or $\mathrm{S}\varpi(\phi\phi')^{-1}\varpi = -r^2$, (iii)

since $\phi'^{-1}\phi^{-1} = (\phi\phi')^{-1}$. It is, in general, an ellipsoid, for π cannot be infinite, while ρ is finite. When the strain is pure, the equation of the strain ellipsoid is more simply

$$T\Phi^{-1}\varpi = r$$
, or $S\varpi\Phi^{-2}\varpi = -r^2$,

or again, in terms of i, j, and k, e_1, e_2 , and e_3 ,

$$\frac{(\mathrm{S}i\rho)^2}{e_1{}^2} + \frac{(\mathrm{S}j\rho)^2}{e_2{}^2} + \frac{(\mathrm{S}k\rho)^2}{e_3{}^2} = r^2.$$

Thus, *i*, *j*, and *k* are unit vectors along its axes, and e_1 , e_2 , e_3 are the ratios of the semi-axes to the radius of the sphere. In general, the axes of the ellipsoid are parallel to the axes of the self-conjugate function $\phi \phi'$.

(5.) We shall now prove that the transformation produced by any linear function ϕ is equivalent to a rotation followed by a pure strain, and accompanied in the case where *m* is negative by a reversal of every vector.

Assuming generally for all vectors ρ

$$\phi \rho = \pm \Phi q \rho q^{-1}, \qquad (iv)$$

where Φ is an ellipsoidal function, the third invariant of ϕ (i)

$$m = \pm S\Phi q a q^{-1} \Phi q \beta q^{-1} \Phi q \gamma q^{-1} (S a \beta \gamma)^{-1}$$

= \pm S\Phi q a q^{-1} \Phi q \beta q^{-1} \Phi q \gamma q^{-1} (S q a q^{-1} q \beta q^{-1} q \gamma q^{-1}) = \pm e_1 e_2 e_3, \qquad (v)

if e_1 , e_2 , and e_3 are the positive roots of Φ . Hence, if *m* is positive, the plus sign is to be taken; and, if *m* is negative, the minus sign.

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(6.) Again, taking the conjugate of ϕ

$$\phi'\rho = \pm q^{-1}\Phi\rho q, \qquad (vi)$$

and therefore

$$\phi \phi' \rho = \Phi^2 \rho \quad \text{or} \quad \phi \phi' = \Phi^2.$$
 (vii)

This equation requires $\phi \phi'$ to be ellipsoidal, and it must be so if ϕ , and therefore ϕ' , is real for

$$T (\phi' \rho)^2 = - S \rho \phi \phi' \rho \qquad (viii)$$

cannot be finite for any infinite value of ρ .

The latent roots of the self-conjugate function $\phi \phi'$ being all positive may be denoted by e_1^2 , e_2^2 , and e_3^2 , and if *i*, *j*, *k* are the axes

$$\phi\phi'\rho = \Phi^2\rho = -e_1^2 i \mathrm{S}i\rho - e_2^2 j \mathrm{S}j\rho - e_3^2 k \mathrm{S}k\rho. \qquad (\mathrm{ix})$$

(7.) We are now at liberty to define Φ by the equation

$$(\phi\phi')^{2}\rho = \Phi\rho = -e_{1}iSi\rho - e_{2}jSj\rho - e_{3}kSk\rho, \qquad (x)$$

the roots e_1 , e_2 , and e_3 being all positive. In general a function has eight square roots, and the eight square roots of $\phi\phi'$ correspond to the various combinations of signs attributable to the radicals in

$$-\sqrt{\overline{e_1}^2}i\mathrm{S}i\rho - \sqrt{\overline{e_2}^2}j\mathrm{S}j\rho - \sqrt{\overline{e_3}^2}k\mathrm{S}k\rho. \tag{xi}$$

We may speak of the function Φ as the *principal* square root as in this case positive signs are chosen throughout.

(8.) In order to justify the assumption made in equation (iv), it is necessary to prove that Uq is determinate. Writing equation (iv) in the form

$$\phi \rho = \Phi \chi \rho, \qquad (xii)$$

where χ is a linear vector function to be determined, the conjugate of $\chi = \Phi^{-1}\phi$ is likewise its inverse for

$$\chi' = \phi' \Phi^{-1}$$
, and $\Phi^{-1} \phi \cdot \phi' \Phi^{-1} = \Phi^{-1} \Phi^2 \Phi^{-1} = 1$.
So χ satisfies the equation
 $\chi \chi' = 1$. (xiii)

Now this equation shows that whatever vector ρ may be its tensor is equal to that of $\chi\rho$, and therefore all figures remain equal after the transformation represented by χ . The transformation must therefore be equivalent to a rotation, or to a rotation accompanied by a reflection or the reversal of every vector. The assumption made in (iv) is thus completely verified.

Supposing m positive, and writing (vi) in the form

$$q\phi'\rho-\Phi\rho q=0,$$

the scalar and vector parts furnish the equations

$$SVq (\phi' - \Phi)\rho = 0, \quad (\phi' - \Phi)\rho Sq + V.Vq(\phi' + \Phi)\rho = 0,$$

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and the second of these virtually includes the first. In terms of two arbitrary vectors ρ and ρ' , we find, without difficulty,

$$\nabla q = x \nabla (\phi' - \Phi) \rho (\phi' - \Phi) \rho'; \quad \Im q = -x \Im (\phi' + \Phi) \rho (\phi' - \Phi) \rho'. \quad (xiv)$$

Also Vq satisfies the equation

$$(\boldsymbol{\phi} - \boldsymbol{\Phi}) \mathbf{V} \boldsymbol{q} = \boldsymbol{0},$$

because otherwise $S(\phi - \Phi)Vq\rho = 0$ could not be satisfied for every value of ρ .

The symbolic cubic of χ must be of the form

$$(\chi \neq 1) (\chi^2 + n\chi + 1) = 0, \qquad (\mathbf{x}\mathbf{v})$$

for the symbolic cubic of a function is also satisfied by its conjugate, and in this case the conjugate is the inverse. The upper sign corresponds to the positive value of m.

(9.) Similarly if the rotation follows the pure strain, the assumption

$$\phi \rho = \pm p \Psi \rho p^{-1}, \text{ or } \phi' \rho = \pm \Psi p^{-1} \rho p$$
 (xvi)

may be justified by an analogous train of reasoning. Here $\phi'\phi\rho = \Psi^2\rho$ and Ψ is the ellipsoidal principal square root of the ellipsoidal function $\phi'\phi$. The latent roots of Ψ and Φ are identical (compare Note II., (2.), p. 363).

(10.) In every homogeneous strain one direction at least remains unchanged. When *m* is positive, one latent root of the function ϕ must be positive. This is obvious when the roots are all real; and when two of the roots are imaginary, $a + \sqrt{-1}b$ and $a - \sqrt{-1}b$, their product $a^2 + b^2$ is always positive, and therefore the remaining and real root is positive. The axis of ϕ , corresponding to the real positive root, retains its direction. It is evident by superposing a rotation upon a pure strain that any selected direction may be preserved unaltered.

If two directions Ua and U β remain unchanged, they are connected by the relation

$$SU\phi a\phi\beta = SUa\beta$$
, or $SU\Psi a\Psi\beta = SUa\beta$, (xvii)

where $\phi \rho = p \Psi \rho p^{-1}$ (xvi). Either of these equations expresses that the cosine of the angle of inclination of the strained lines is equal to that of the unstrained lines. Rationalizing the second of equations (xvii), it appears if a is given that the locus of β is one sheet of the quartic cone

$$a^{2}\beta^{2}(\mathrm{Sa}\Psi^{2}\beta)^{2} = (\mathrm{Sa}\beta)^{2}\mathrm{Sa}\Psi^{2}a\mathrm{S}\beta\Psi^{2}\beta. \qquad (\mathrm{xviii})$$

If in this we substitute $\beta = a + ta'$ where Saa' = 0, we find that a is a double edge of the cone, and discarding the factor t^2 we obtain a quadratic in t to determine the edges of the cone in the plane of a and a'. One solution only is appropriate as (xviii) includes both the conditions

$$SU\Psi a\Psi \beta = \pm SU a\beta.$$

It is easy to see that the roots of the quadratic are always real since Ψ is ellipsoidal. If two directions are unaltered, a third is likewise unaltered.

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(11.) The roots of the function ϕ , g_1 , g_2 , and g_3 may have any values (within certain limits) subject to the single condition

$$g_1g_2g_3 = e_1e_2e_3, \qquad (xix)$$

which expresses that no change of volume is produced by the rotation.

If we assume g_1, g_2 , and g_3 subject to (xix), and try to satisfy the equations

$$\phi a = p \Psi a p^{-1} = g_1 a, \quad \phi \beta = p \Psi \beta p^{-1} = g_2 \beta, \quad \phi \gamma = p \Psi \gamma p^{-1} = g_3 \gamma, \quad (xx)$$

we see that that the axes α , β , and γ must be edges, respectively, of the cones

$$T\Psi U\rho = Tg_1, \quad T\Psi U\rho = Tg_2, \quad T\Psi U\rho = Tg_3,$$
 (xxi)

where Tg_1 is the positive value of the scalar g_1 irrespective of its sign. These cones are the loci of vectors whose lengths are altered in a given ratio. Selecting, at pleasure, any vector a on the first cone, β is determined on the second cone by the aid of the relation

$$S\Psi a\Psi \beta = g_1 g_2 S a\beta \qquad (xxii)$$

implied in (xx) and equivalent to (xvii). Up, and therefore the rotation, may be found by combining the first and second of equations (xx). Hence, ϕ is determined, and the third vector γ is the result of operating by $(\phi - g_1)(\phi - g_2)$ on an arbitrary vector.

Again, by (xxi), the magnitudes of g_1, g_2 , and g_3 must lie between the greatest and least values of $T\Psi U\rho$, that is, between the greatest and least of the scalars e_1, e_2, e_3 . In fact the magnitudes of the roots are inversely proportional to the radii of the ellipsoid

$$T\Psi\rho = 1$$
 or $S\rho\Psi^2\rho = -1$, (xxiii)

which are parallel to the corresponding axes. This ellipsoid is converted by the strain into a sphere of unit radius.

(12.) It is possible to superpose a rotation upon a pure strain, so that the function ϕ may have indeterminate axes. These axes evidently must lie in one or other of the cyclic planes of the ellipsoid (xxiii). Expressing Ψ^2 in Hamilton's cyclic form

$$\Psi^2 \rho = e_2^2 \rho + \lambda S \mu \rho + \mu S \lambda \rho \qquad (xxiv)$$

has one root equal to e_2^2 , and the other roots are

$$e_1^2 = e_2^2 + S\lambda\mu + T\lambda\mu, \quad e_3^2 = e_2^2 + S\lambda\mu - T\lambda\mu.$$
 (xxv)

Assuming

$$\phi \rho = e_2 \rho + \nu S \lambda \rho; \qquad (xxvi)$$

this function has indeterminate axes in the plane $S\lambda\rho = 0$, and it appears without difficulty that $\phi'\phi = \Psi^2$ if ν satisfies the equation

$$e_2 \nu + \frac{1}{2} \nu^2 \lambda = \mu. \qquad (xxvii)$$

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Also the third invariant of ϕ being equal to that of Ψ ,

$$e_2^2(e_2 + \mathrm{S}\nu\lambda) = e_1e_2e_3. \qquad (\mathbf{x}\mathbf{x}\mathbf{v}\mathbf{i}\mathbf{i}\mathbf{i})$$

When we operate on (xxvii) by S λ and use (xxv) and (xxviii), we find,

$$\nu^2 \lambda^2 = (e_1 - e_3)^2$$
 and $e_2 \nu = \mu - \frac{1}{2} (e_1 - e_3)^2 \lambda^{-1}$. (xxix)

Thus ν is completely determined, and the assumption made as to the form of ϕ (xxvi) is justified. Also we see, by the form of the function ϕ , that the most general strain may be effected in three stages, by displacing in one direction $(U\nu)$ a system of planes perpendicular to another direction $(U\lambda)$ by amounts proportional to the distances of the planes from the origin; by uniformly altering the linear dimensions (in the ratio e_2 to unity); and by rotating the body as a whole.

(13.) When unity is included between the limits $e_1 > e_2 > e_3$, that is, when elongation and contraction both occur, a rotation may be applied to a pure strain, so that one root of ϕ is unity. In this case one root of $\phi - 1$ is zero, or this function is a binomial reducing every vector to a fixed plane. But $\phi \rho - \rho$ or $(\phi - 1)\rho$ is the *displacement* due to the strain, and accordingly under the above conditions a rotation may be superposed upon the strain so as to render the resultant displacement of every point parallel to a plane.

Again, by (xxvi), if e_2 is unity, a suitable rotation will render the displacement of every point parallel to a line. In this case the pure part of the strain is plane, for when one root of Ψ is unity, the strain is completely specified by that in the plane at right angles to the corresponding axis.

(14.) In the case of a plane strain when there is no dilatation the intermediate root e_2 is evidently unity. The condition for no dilatation is now $e_1e_3 = 1$, and this, coupled with $e_2 = 1$, shows that (xxvi) and (xxviii) are equivalent to

$$\phi \rho = \rho + \nu S \lambda \rho, \quad S \nu \lambda = 0. \tag{xxx}$$

The strain represented by (xxx) is a simple shear, the system of planes normal to λ being displaced parallel to themselves and proportionately to their distances from the origin. In general a plane strain without dilatation is equivalent to a shear and a rotation.

It also appears from (xxviii) that

$$e_2^2 = e_1 e_3 = 1 \qquad (\mathbf{x} \mathbf{x} \mathbf{x} \mathbf{i})$$

are the conditions that a strain should be equivalent to a rotation and a shear.

(15.) We shall investigate the reduction of the general strain to a dilatation, a pair of shears and a rotation. If this is possible the general linear vector function must be expressible in the form

$$\phi \rho = m^{\sharp} p \left(1 + t' a' S \beta' \right) \left(1 + t a S \beta) \rho \cdot p^{-1}, \qquad (xxxii)$$

where $Sa\beta = Sa'\beta' = 0$. For convenience we take a, β , a', β' to be unit vectors.

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Observing that

$$(1 - taS\beta)(1 + taS\beta) =$$

(xxxii) is equivalent to

$$\phi(1 - taS\beta)\rho = m^{s}p(1 + t'a'S\beta')\rho p^{-1}, \qquad (xxxiii)$$

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and taking conjugates

$$(1 - t\beta Sa)\phi'\rho = m^{*}(1 + t'\beta'Sa')p^{-1}\rho p. \qquad (xxxiv)$$

Hence eliminating p, we find

 $m^{-\frac{2}{3}}(1-t\beta Sa)\phi'\phi(1-taS\beta) = (1+t'\beta'Sa')(1+t'a'S\beta'). \quad (xxxv)$

We shall now calculate the roots of the function on the left. If we can arrange so that one root is unity, the pure part of the strain $m^{-\frac{1}{3}}\phi(1-taS\beta)$ will be plane, and if it is plane it must be a shear for neither $m^{-\frac{1}{3}}\phi$ nor $(1-taS\beta)$ produces any dilatation (14.). Obviously the function on the right has one root unity, the corresponding axis being $\gamma' = a'\beta'$.

For brevity, replacing $m^{-\frac{3}{2}}\phi'\phi$ by Θ , the roots s of the function on the right are given by

$$\mathbf{S}\left[(1-t\beta\mathbf{S}a)\Theta a-sa\right]\left[(1-t\beta\mathbf{S}a)\Theta(\beta+ta)-s\beta\right]\left[(1-t\beta\mathbf{S}a)\Theta\gamma-s\gamma\right]=0,$$

if $\gamma = a\beta$. This equation is equivalent to

$$S\left[\Theta a - s(a - t\beta)\right]\left[\Theta(\beta + ta) - s\beta\right](\Theta\gamma - s\gamma) = 0,$$

deduced from it by operating on every vector by $1 + t\beta Sa$.

Observing that the third invariant of Θ is unity, so that

$$\nabla \Theta \beta \Theta \gamma = \Theta^{-1} a$$
, $\nabla \Theta \gamma \Theta a = \Theta^{-1} \beta$, $\nabla \Theta a \Theta \beta = \Theta^{-1} \gamma$,

the equation reduces to

$$\begin{split} & \mathrm{Sa}\beta\gamma - s\mathrm{S}\left[\left(a - t\beta\right)\Theta^{-1}\left(a - t\beta\right) + \beta\Theta^{-1}\beta + \gamma\Theta^{-1}\gamma\right] \\ & \quad + s^{2}\mathrm{S}\left[a\Theta a + \left(\beta + ta\right)\Theta\left(\beta + ta\right) + \gamma\Theta\gamma\right] - s^{3}\mathrm{Sa}\beta\gamma = 0. \end{split}$$

Finally, the equation of the cubic takes the form

$$1 - sN' + s^2N'' - s^3 = 0, \qquad (xxxvi)$$

where

$$\begin{split} \mathbf{N}' &= \mathbf{M}' + \mathbf{S} a \boldsymbol{\Theta}^{-1} a - \mathbf{S} \left(a - t \boldsymbol{\beta} \right) \boldsymbol{\Theta}^{-1} \left(a - t \boldsymbol{\beta} \right), \\ \mathbf{N}'' &= \mathbf{M}'' + \mathbf{S} \boldsymbol{\beta} \boldsymbol{\Theta} \boldsymbol{\beta} - \mathbf{S} \left(\boldsymbol{\beta} + t a \right) \boldsymbol{\Theta} \left(\boldsymbol{\beta} + t a \right), \end{split}$$
 (xxxvii)

and

the first and second invariants of
$$\Theta$$
 being M'' and M' .

The condition that one root should be unity is

$$N' = N'', \qquad (xxxviii)$$

and observing that N' and N" are quadratic in the scalar t which specifies the amount of the shear, it appears that we may arbitrarily select the vectors a and β (that is the plane and direction of the shear), and that its amount is then given by a root of the

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quadratic (xxxviii) in t. The determination of the complementary shear $1 + t'a'S\beta'$, and of the rotation presents no difficulty.

(16.) It is sometimes convenient, especially in dealing with small strains, to replace ϕ by $1 + \theta$. In this notation $\theta \rho$ is the displacement of the extremity of ρ , the origin of vectors being supposed to be kept fixed.* Resolving the displacement along and at right angles to ρ , we have

$$\theta \rho = \theta \rho \rho^{-1} \cdot \rho = (e + \eta) \rho,$$
 (xxxix)

if

The scalar
$$e$$
 is called the *elongation*. It is equal to the inverse square of the corresponding radius of the elongation quadric

 $e = S\theta\rho\rho^{-1}$, and $\eta = V\theta\rho\rho^{-1}$.

$$\delta \rho \theta \rho = -1.$$
 (xli)

When the strain is pure so that θ is self-conjugate, the vectors η and ρ are parallel to the principal axes of a central section of this quadric. Thus $\eta\rho$ the component of the displacement at right angles to ρ is normal to that plane section of (xli) of which ρ is a principal axis. Also the magnitude of η is equal to the area of the triangle formed by lines along the corresponding radius and central perpendicular on the tangent plane of the quadric equal in length to the reciprocals of the radius and the perpendicular.

(17.) If the cubic of θ is

$$\theta^3 - n''\theta^2 + n'\theta - n = 0, \qquad (xlii)$$

the ratio of alteration of volume (i) is

$$m = S(1+\theta)a(1+\theta)\beta(1+\theta)\gamma(Sa\beta\gamma)^{-1} = 1 + n'' + n' + n. \quad (xliii)$$

If the strain is so small that terms involving the square and cube of the small function θ may be neglected, *m* is approximately equal to 1 + n''; n'' is the dilatation.

The ratio of lines is $T(1+\theta)Ua$ or approximately $1 + Sa^{-1}\theta a$ (compare xl). The ratio of areas is $TV(1+\theta)a(1+\theta)\beta T(Va\beta)^{-1}$, or $Tm(1+\theta')^{-1}U\lambda$ if $U\lambda = UVa\beta$. Now, for a small function θ ,

$$(1+\theta)(1-\theta) = 1$$
 or $1-\theta = (1+\theta)^{-1}$, (xliv)

so the ratio of areas is approximately

$$T(1 + n'' - \theta')U\lambda$$
 or $1 + n'' - S\lambda^{-1}\theta\lambda$.

(18.) The result of superposing the strain $1 + \theta_2$ upon $1 + \theta_1$ is $1 + \theta_1 + \theta_2 + \theta_2\theta_1$, and this is generally distinct from $1 + \theta_2 + \theta_1 + \theta_1\theta_2$ due to the strain $1 + \theta_1$ following $1 + \theta_2$. However, when both strains are small, so that $\theta_1\theta_2$ and $\theta_2\theta_1$ are negligible, the order

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^{*} Compare the Note on *Hamilton's Operator*, Section (27.), where the case of non-homogeneous small strain is considered, page 446.

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in which the strains are effected is indifferent, and the displacement, due to the resultant strain, is the resultant of the displacement due to each strain separately. In particular, a small rotation changes ρ into $(1 + V\epsilon)\rho$. If this is followed by a small pure strain $1 + \theta_0$, after the double operation ρ becomes

$$\rho + \theta_0 \rho + V \epsilon \rho \quad \text{or} \quad \rho + \theta \rho \tag{(xlv)}$$

if ϵ is the spin-vector of θ . Hence the origin of the name spin-vector. Again, for small strains

$$(1+\theta)(1+\theta') = (1+\theta')(1+\theta) = 1+\theta+\theta' = 1+2\theta_0 = (1+\theta_0)^2,$$

and the functions Φ and Ψ or $(\phi\phi')^{\frac{1}{2}}$ and $(\phi'\phi)^{\frac{1}{2}}$ are identical with $\frac{1}{2}(\phi + \phi')$. Also, the equation of the strain quadric (iii) becomes

$$T(1-\theta)\rho = r \quad \text{or} \quad \rho^2 - 2S\rho\theta_0\rho + r^2 = 0. \quad (xlvi)$$

(19.) In (12) we have given an example of the application of one of Hamilton's forms for the linear vector function. They all admit of simple interpretation. Take, for instance, the focal form

$$\theta \rho = a a V a \rho + b \beta S \beta \rho, \qquad (xlvii)$$

and we see that the most general pure strain may be compounded of a contraction $(aaVa\rho)$ round one line (Ua), and of an elongation $(b\beta S\beta\rho)$ parallel to another $(U\beta)$. (See Minchin, *Treatise on Statics*, Art. 379.)

The form

$$\theta \rho = g \rho + \lambda S \mu \rho + \mu S \lambda \rho \qquad (xlviii)$$

shows that the pure strain may be resolved into shifting planes normal to μ in a direction parallel to λ , and planes normal to λ in a direction parallel to μ , and by superposing a general dilatation 3g.

(20.) Reference has been made in the Note to page 225 to the strain which converts a quadric into a sphere. More generally if the strain ϕ converts any quadric

 $S\rho\Phi\rho = -1$ into $S\rho\Psi\rho = -1$,

the function ϕ must satisfy the equation

$$\phi'\Psi\phi=\Phi. \qquad (xlix)$$

In order to simplify this, assume

$$\phi = \Psi^{-\frac{1}{2}} \chi \Phi^{\frac{1}{2}}, \text{ or } \phi' = \Phi^{\frac{1}{2}} \chi' \Psi^{-\frac{1}{2}},$$
 (1)

and it appears that χ must be a solution of the equation

$$\chi'\chi = 1.$$

This has been considered and solved in (8.); χ must represent a rotation or a rotation combined with a reflection. We are instructed therefore by the form of the function ϕ (xlix) to strain the first quadric into a sphere; to rotate the sphere with or without reflection; and to strain the sphere into the second quadric.

IV.-ON THE SPECIFICATION OF LINEAR VECTOR FUNCTIONS.

(1.) A linear function is determinate given the vectors derived by it from three known vectors^{*}. Given the directions β_1 , β_2 , β_3 , into which three known directions a_1 , a_2 , and a_3 are changed, and the ratios a_4 , a_5 , a_6 , in which the lengths of a_4 , a_5 , and a_6 are altered, we have

$$\phi \rho = (x\beta_1 Sa_2 a_3 \rho + y\beta_2 Sa_3 a_1 \rho + z\beta_3 Sa_1 a_2 \rho) (Sa_1 a_2 a_3)^{-1}, \qquad (i)$$

where the scalars x, y, z satisfy

$$TSa_{1}a_{2}a_{3} = Ta_{4}^{-1}\Sigma x \beta_{1}Sa_{2}a_{3}a_{4} = Ta_{5}^{-1}\Sigma x \beta_{1}Sa_{2}a_{3}a_{5} = Ta_{6}^{-1}\Sigma x \beta_{1}Sa_{2}a_{3}a_{6}.$$
 (ii)

Rationalizing and solving these equations for x, y, and z, eight systems of values are obtained, and, corresponding to these, eight functions ϕ may be found. Four of these functions are simply the negatives of the remaining four, and, in general, the eight functions correspond to the eight arrangements of sign attributable to the scalars a.

(2.) Given four directions derived from four others (compare Note V., Section (6.))

$$A\phi\rho = \frac{\beta_1 Sa_2 a_3 \rho S\beta_2 \beta_3 \beta_4}{Sa_2 a_3 a_1 Sa_2 a_3 a_4} + \frac{\beta_2 Sa_3 a_1 \rho S\beta_3 \beta_1 \beta_4}{Sa_3 a_1 a_2 Sa_3 a_1 a_4} + \frac{\beta_3 Sa_1 a_2 \rho S\beta_1 \beta_2 \beta_4}{Sa_1 a_2 a_3 Sa_1 a_2 a_4}$$
(iii)

where A is an arbitrary scalar. Given the ratio in which a fifth line is altered, A is determined.

(3.) This method of representing a linear vector function leads to some remarkable expressions. For instance, if a_1 , a_2 , a_3 and a_4 , a_5 , a_6 are unit vectors along two sets of mutually conjugate radii of a quadric $S\rho\Phi\rho = 1$, we have

$$A_{4}\Phi\rho = Va_{2}a_{3}\frac{Sa_{2}a_{3}\rho Sa_{1}a_{5}a_{6}}{Sa_{2}a_{3}a_{1}Sa_{2}a_{3}a_{4}} + Va_{3}a_{1}\frac{Sa_{3}a_{1}\rho Sa_{2}a_{5}a_{6}}{Sa_{3}a_{1}a_{2}Sa_{3}a_{1}a_{4}} + Va_{1}a_{2}\frac{Sa_{1}a_{2}\rho Sa_{3}a_{5}a_{6}}{Sa_{1}a_{2}a_{3}Sa_{1}a_{2}a_{4}} \cdot (iv)$$

Hence, if for brevity $Sa_1a_2a_3$ is denoted by (123), and $Sa_1\Phi a_1$ by a_1^{-2} , we obtain

$$\frac{\mathbf{A}_4}{(123)} = a_1^2 \frac{(156)}{(234)} = a_2^2 \frac{(256)}{(314)} = a_3^2 \frac{(356)}{(124)} = a_4^2 \frac{(456)}{(123)}, \qquad (\mathbf{v})$$

together with other relations, which can easily be supplied, connecting the signs of the solid angles (a_1, a_2, a_3) with the radii $a_1, a_2, \ldots a_6$ of the quadric. These relations are due to Sir Robert Ball, and are of importance in the theory of co-reciprocal screws. Again, by (iv), we see that the shape and orientation of a quadric are determined, given the directions of three mutually conjugate diameters, and the direction of a fourth line (a_4) conjugate to the plane normal to a given direction Va_5a_6 .

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^{*} Compare Note III., Section (4.), p. 366.

[†] We suppose, for convenience, that the vectors are all of unit length.

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(4.) If we seek to determine as far as possible a linear vector function by expressing that the lengths of given vectors are to be altered in given ratios, we shall find that we may assign six directions and six ratios, and that the function remains indeterminate to the extent of an arbitrary rotation which may be superposed upon it.* For, given the centre of a quadric, six conditions determine it, and if $\phi a_1 = a_1 \beta_1$, &c., the ratios (a_1) are inversely proportional to the radii of the quadric $T\phi \rho = 1$ parallel to the corresponding directions (a_1) . In this way we can find the self-conjugate function $\phi'\phi$. Taking its square root, and superposing an arbitrary rotation, we have the general function satisfying the conditions. Or, given six ratios and one direction which a seventh vector must assume, the function is determinate.

(5.) In terms of Hamilton's *Aconic Function*[†] we can write down the relation between the seven ratios in which the lengths of seven vectors are altered by a strain. The aconic function of six vectors is

$$[7] = SV.Va_1a_2Va_4a_5V.Va_2a_3Va_5a_6V.Va_3a_4Va_6a_1.$$
(vi)

If it vanishes, the six vectors lie on a cone, and the form of the expression contains a direct proof of Pascal's theorem, for it shows that the lines of intersection of the planes $a_1, a_2; a_4, a_5$, and $a_2, a_3; a_5, a_6$; and $a_2, a_4; a_6, a_1$ are coplanar.

To fix the signs appropriate to the seven aconic functions formed by omitting one of seven vectors, mark seven points 1, 2, 3, 4, 5, 6, 7 on a circle, and go round it in this order, starting always from the point 1, and omitting one point.[‡] Then the relation between the seven unit vectors and the seven ratios is

$$[1]a_{1}^{2} - [2]a_{2}^{2} + [3]a_{3}^{2} - [4]a_{4}^{2} + [5]a_{5}^{2} - [6]a_{6}^{2} + [7]a_{7}^{2} = 0.$$
(vii)

In fact, allowing a_7 and a_7 to vary, this is the equation of a quadric concentric with the origin whose radii are inversely proportional to a_7 , and which passes through the extremities of the six vectors $a_1a_1^{-1}$, &c. To prove this, it is only necessary to show that the sign of [7] is changed whenever any two vectors in it are transposed; for, when $a_7 = a_6$, the function [6] becomes [7], and all the others vanish. When $a_7 = a_5$ all vanish except [5], which becomes - [7], with one interchange of vectors. If the six vectors happen to lie on a quadric cone [7] is zero, and the ratio a_7 is not determined. The equation (vii) (omitting the last term) must then be satisfied for every possible direction a_7 , and the six ratios cannot be arbitrarily chosen.

‡ Thus, for example, we may also write

$$[3] = \{124567\}.$$

§ The most direct way of doing this seems to be, to express a_4 , a_5 , and a_6 in terms of a_1 , a_2 , and a_3 .

^{*} Compare Note III., Section (9.), p. 368.

[†] Lectures on Quaternions, Art. 442.

The equation is then equivalent to that of the sphero-conic determined by the five vectors $a_1a_1^{-1}$, . . . $a_5a_5^{-1}$, and expresses that $a_6a_6^{-1}$ terminates on this curve. More fully draw any quadric $S\rho\theta\rho = 1$ through the extremities of the five vectors and having its centre at the origin. Let $S\rho\chi\rho = 0$ be the cone containing the five vectors. The sixth must terminate on the curve common to the system

$$S\rho(\theta + t\chi)\rho = 1.$$
 (viii)

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(6.) Hence we can see how to determine a linear vector function given five ratios and two directions. For let (viii) (compare (4.)) be the quadric whose corresponding radii (a_1, \ldots, a_5) are inversely proportional to the ratios $(a_1 \ldots a_5)$, and let β_6 and β_7 be the directions into which a_6 and a_7 are to be changed by the function ϕ . Then, if we determine t from the relation

$$SU(\theta + t\chi)a_6U(\theta + t\chi)a_7 = S\beta_6\beta_7, \qquad (ix)$$

we can superpose a rotation upon $\theta + t\chi$, so as to render the vectors derived from a_6 and a_7 parallel to β_6 and β_7 .

V.--INVARIANTS OF LINEAR VECTOR FUNCTIONS.

Before touching on the general theory of quaternion invariants of linear vector functions, it seems to be desirable to point out a few consequences of relations connecting the roots of a single function ϕ . The signification of the geometrical interpretations will, in due course, be greatly extended, and we shall come to regard the invariants of the earlier sections of this note as invariants of two linear functions ϕ and unity (compare Section 9).

(1.) Writing the symbolic cubic of ϕ in the form

$$\phi^3 - m'' \phi^2 + m' \phi - m = 0$$
, or $(\phi - g_1)(\phi - g_2)(\phi - g_3) = 0$, (i)

we know that every triad of vectors α , β , and γ satisfies the equation

$$S\beta\gamma\phi a + S\gamma a\phi\beta + Sa\beta\phi\gamma = 0,$$
 (ii)

when

$$m'' = 0$$
, or $g_1 + g_2 + g_3 = 0$. (iii)

Thus assuming at pleasure two vectors a and β , and determining a third vector γ by the equations $S\beta\gamma\phi a = S\gamma a\phi\beta = 0$, the third equation $Sa\beta\phi\gamma = 0$ must be true when m'' = 0. In other words, in this case it is possible to determine an infinite number of triads of vectors a, β , and γ , so that each vector of the derived triad ϕa , $\phi\beta$, $\phi\gamma$ is coplanar with a pair of vectors of the original. Or we may say briefly the *edges* of the derived lie on the corresponding *faces* of the original triad. Conversely, if this arrangement is possible in any one case, it is possible in an infinite number of cases.

(2.) Similarly when m' = 0, triads may be determined so that the faces of the derived triads contain the corresponding edges of the original, and the converse is also true.

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(3.) Further, if for any arrangement of signs

$$\pm \sqrt{g_1} \pm \sqrt{g_2} \pm \sqrt{g_3} = 0, \qquad (iv)$$

the sum of the roots of the corresponding square root of ϕ is zero (compare the Note on Strain, Section 7, page 367).

We can then determine triads a, β, γ , whose faces contain the edges of the triads $\sqrt{\phi}a, \sqrt{\phi}\beta, \sqrt{\phi}\gamma$, and we shall show that the faces of these derived triads contain the edges of the triads $\phi a, \phi \beta, \phi \gamma$. For if $S\beta\gamma \sqrt{\phi}a = 0$, we obtain, on multiplying by the third invariant of $\sqrt{\phi}$, this other equation $S \sqrt{\phi}\beta \sqrt{\phi}\gamma \phi a = 0$; this proves the theorem. In other words when (iv) is satisfied, it is possible to determine in an indefinite number of ways a triad a, β, γ so related to the derived triad $\phi a, \phi \beta, \phi \gamma$ that, in every case, an intermediate triad can be inscribed to the first and circumscribed to the second. On rationalizing (iv), the condition takes the form

$$(g_1 + g_2 + g_3)^2 - 4(g_2g_3 + g_3g_1 + g_1g_2) = 0$$
, or $m'^2 = 4m'$. (v)

(4.) The converse of this property is true, and the theorem admits of considerable extension. If

$$\sqrt[n]{g_1} + \sqrt[n]{g_2} + \sqrt[n]{g_3} = 0,$$
 (vi)

n being an integer, triads α , β , γ and $\phi \alpha$, $\phi \beta$, $\phi \gamma$ can be found connected by a series of inscribed and circumscribed triads derived from the original by successive applications of the operator $\sqrt[n]{\phi}$. Still more generally an interpretation can be assigned for the case in which *n* is a fraction.

(5.) Otherwise we may deduce invariants by proposing suitable geometrical conditions instead of interpreting geometrically the meaning of the vanishing of assumed invariants. For instance, we may inquire into the conditions that a linear vector transformation may leave a given quadric cone unaltered. The vectors $\phi\rho$ derived from edges of the cone $S\rho\Phi\rho = 0$ are edges of the new cone $S\phi^{-1}\rho\Phi\phi^{-1}\rho = 0$, or $S\rho\phi'^{-1}\Phi\phi^{-1}\rho = 0$. If these cones are identical, ϕ must satisfy the equation

$$\phi'^{-1}\Phi\phi^{-1} = m^{-\frac{2}{3}}\Phi, \text{ or } \phi'\Phi\phi = m^{\frac{2}{3}}\Phi,$$
 (vii)

the factor $m^{\frac{3}{2}}$ being introduced so as to render equal the third invariants of the functions in each number of the equations. A similar equation has occurred in the Note on Strain (Note III., Section (20.)), and, as in the place cited, the general relation between ϕ and Φ is of the form

$$\phi = \pm m^{\frac{1}{2}} \phi^{-\frac{1}{2}} \chi \phi^{\frac{1}{2}}, \text{ where } \chi \chi' = 1,$$
 (viii)

and the function χ produces a rotation or a rotation and a reflection. Now (Note II., Section 2) the symbolic cubics of $m^{-\frac{1}{3}}\phi$ and of χ must be identical, but the cubic of χ is reciprocal, and so therefore must be that of $m^{-\frac{1}{3}}\phi$, or we must have the invariant relation

$$mm''^3 - m'^3 = 0.$$
 (ix)

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As a rotation leaves unchanged every right cone having its axis coincident with that of the rotation, we are led to infer and can verify at once that the whole system of cones

$$S\rho\Phi\rho + u(S\kappa\rho)^2 = 0$$
, where $\phi'\kappa = m^{\frac{1}{3}}\kappa$, (x)

transforms into itself when ρ is changed to $\phi\rho$, provided the invariant (ix) vanishes, and provided ϕ is a solution of equation (viii).

(6.) It will be noticed that the foregoing interpretations depend simply on the directions of the vectors involved. If a function changes the directions of α , β , γ into the directions of λ , μ , ν , it must be of the type

$$\phi \rho = u\lambda S\beta \gamma \rho + v\mu S\gamma a\rho + w\nu Sa\beta \rho, \qquad (xi)$$

the scalars u, v, and w being arbitrary. If, in addition, the direction of δ is changed into that of π ,

$$\phi\rho = \lambda S\mu\nu\varpi \frac{S\beta\gamma\rho}{S\beta\gamma\delta} + \mu S\nu\lambda\varpi \frac{S\gamma a\rho}{S\gamma a\delta} + \nu S\lambda\mu\varpi \frac{Sa\beta\rho}{Sa\beta\delta}, \qquad (xii)$$

and in this there is nothing arbitrary except the tensor of the product $\lambda \mu \nu \pi \delta^{-1}$. (Compare Note IV., Section (2), p. 374.)

From this point of view we can see the connexion with the theory of anharmonic coordinates in a plane (pp. 23-29, vol. i.). For if $\delta = aa + b\beta + c\gamma$, $\varpi = a'\lambda + b'\mu + c'\nu$, and $\rho = xaa + yb\beta + zc\gamma$, we can verify at once that $\phi\rho = (xa'\lambda + yb'\mu + zc'\nu) S\lambda\mu\nu$. Also (compare p. 25, vol. i.),

$$(OA \cdot BDCP) = \frac{y}{z}, (OB \cdot CDAP) = \frac{z}{x}, (OC \cdot ADBP) = \frac{x}{y},$$
 (Xiii)

where (OA. BDCP) is the anharmonic of the four planes (a, β) , (a, δ) , (a, γ) , and (a, ρ) , respectively. The equations (xiii) remain true when A, B, C, D, P are changed to A', B', C', D', P', where generally OF' || ϕ OP. Thus, OF' can be found by linear constructions when OP is given as the tensors of the vectors $a, \beta, \gamma, \delta, \lambda, \mu, \nu, \pi$, and ρ may be chosen so that the extremities of these nine vectors may lie in an assumed plane.

(7.) As the axes of ϕ are the vector solutions of the equation

$$\nabla \rho \phi \rho = 0, \qquad (xiv)$$

the cone

$$Sa\rho\phi\rho = 0 \tag{xv}$$

contains three fixed lines which are quite independent of the vector a. This quadric cone is the locus of a line, so that it and its derived are coplanar with a fixed line (a). For various values of this vector, we obtain a doubly infinite system of cones having three common edges. If two of the solutions of (xiv) coincide, the cones touch one another; if all three solutions coincide they osculate, and they break up into pairs of planes, one fixed plane being common to every pair, if the solutions of (xiv) become indeterminate in a certain plane. The conditions for contact and osculation can be

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expressed at once in terms of the invariants m, m', m'', being merely the conditions that the root cubic should have two roots equal or should be a perfect cube. The condition for indeterminate axes is of a different kind. Here there must be a double root g, and $\phi - g$ must destroy every vector in the plane of the indeterminate axes. $\phi - g$ is, therefore, a monomial $\lambda S \mu \rho$; its cubic is *depressed* to a quadratic, or, what is equivalent, Hamilton's function

$$\psi_g = 0$$
, or $\phi^2 - m''\phi + m' + g(\phi - m'') + g^2 = 0$. (xvi)

This, then, is the condition for indeterminate axes. (Compare 352 (20.), p. 504, vol. i., and the remaining sub-articles.)

It is easy to show that the cone (xv) cannot degrade into a pair of planes unless a is coplanar with a pair of axes of ϕ . If the cone is a pair of planes, and if π is the vector of intersection, $Sa\rho\phi\pi + Sa\pi\phi\rho$ must vanish for every vector ρ . Hence

$$V\phi \varpi a + \phi' V a \varpi = 0. \qquad (xvii)$$

Now, as $Sa \varpi \phi \varpi = 0$, we may write $\phi \varpi = u \varpi + va$; and substitution in (xvii) shows that

$$\phi' Va \varpi = u Va \varpi, \qquad (xviii)$$

or *u* must be a root, and $Va\varpi$ the corresponding axis of the conjugate ϕ' . But the axes of ϕ' are the normals to the planes containing pairs of axes of ϕ ; hence, a must be coplanar with a pair of axes of ϕ , as it is at right angles to an axis of ϕ' .

In the case of indeterminate axes, ϕ must be of the form

$$\phi \rho = g \rho + \lambda \mathrm{S} \mu \rho, \qquad (\mathbf{x} \mathrm{i} \mathbf{x})$$

and the cones (xv) all break up into pairs of planes

$$Sa\lambda\rho S\mu\rho = 0. \tag{XX}$$

(8.) We have seen (Note II. (2.) page 363) that the roots of $\theta\phi\theta^{-1}$ and of ϕ are identical. Consequently, the theorems proved up to the present in this note are also true for $\theta\phi\theta^{-1}$ as well as for ϕ .

(9.) Again, if we write $\phi = \phi_2^{-1}\phi_1$, and

$$S\left(\phi_{1}-g\phi_{2}\right)a\left(\phi_{1}-g\phi_{2}\right)\beta\left(\phi_{1}-g\phi_{2}\right)\gamma=\left(m_{1}-gl_{1}+g^{2}l_{2}-g^{3}m_{2}\right)Sa\beta\gamma,\quad (XXI)$$

where m_1 and m_2 are the third invariants of ϕ_1 and ϕ_2 , respectively, and l_1 and l_2 are two new invariants, we obviously have the relations

$$m_2m = m_1; \quad m_2m' = l_1; \quad m_2m'' = l_2,$$
 (XXII)

since the left-hand side of (xxi) may be replaced by

$$m_{2}S(\phi_{2}^{-1}\phi_{1}-g) \alpha (\phi_{2}^{-1}\phi_{1}-g) \beta (\phi_{2}^{-1}\phi_{1}-g) \gamma = m_{2}(m-gm'+g^{2}m''-g^{3}) S\alpha\beta\gamma.$$
(xxiii)
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Furthermore, the values of the ratios

$$m_1: l_1: l_2: m_2$$

are unchanged when ϕ_1 and ϕ_2 are replaced by $\chi \phi_1 \theta$ and $\chi \phi_2 \theta$, respectively, χ and θ being two arbitrary vector functions, for

$$(\chi\phi_2\theta)^{-1}(\chi\phi_1\theta) = \theta^{-1}\phi_2^{-1}\phi_1\theta = \theta^{-1}\phi\theta, \qquad (xxiv)$$

and the functions ϕ and $\theta^{-1}\phi\theta$ have the same roots.

Thus, the invariants depending solely on the roots of $\phi_2^{-1}\phi_1$ are invariantal in a very wide sense. Not only may the vectors a, β , γ be changed in any way, but the functions ϕ_1 and ϕ_2 may also be transformed within very wide limits.

It is well to bear in mind that $\phi_2^{-1}\phi_1$, $\phi_1\phi_2^{-1}$ and their conjugates $\phi'_1\phi'_2^{-1}$ and $\phi'_2^{-1}\phi'_1$ have the same roots.

(10.) Hence, by (1),

$$l_2 = 0 \qquad (\mathbf{x}\mathbf{x}\mathbf{v})$$

is the condition that ϕ_1 and ϕ_2 (or, more generally, that $\chi\phi_1\theta$ and $\chi\phi_2\theta$) should be capable of producing from a triad of vectors α , β , γ two new triads so related that the faces of the second contain the edges of the first; also, by (2),

$$l_1 = 0, \qquad (\mathbf{x}\mathbf{x}\mathbf{v}\mathbf{i})$$

if the faces of the first can contain the edges of the second; and by (3) and (v)

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$$l_2^2 = 4m_2 l_1$$
 or $l_1^2 = 4m_1 l_2$ (xxvii)

if an intermediate triad can be inscribed to the first (or second), and circumscribed to the second (or first). Further, by (5),

$$n_1 l_2^3 = m_2 l_1^3 \tag{xxviii}$$

if the transformation represented by ϕ_2^{-1} can restore a system of cones transformed by ϕ_1 into their original state.

It would be tedious, and cannot be necessary, to elaborate this subject any further.

(11.) In the particular case in which ϕ_1 and ϕ_2 are self-conjugate, we may fall back on the invariants of a pair of cones or conics. For instance, if a triad of vectors satisfies $S\phi_2a\phi_1\beta\phi_1\gamma = 0$, and two similar equations derived from this by cyclical interchange, we may replace the equations by three of the type $S\phi_2a\phi_1^{-1}\nabla\beta\gamma = 0$. The form suggests $\phi_1^{-1}\nabla\beta\gamma \parallel a$ with the condition $Sa\phi_2a = 0$, &c., and the invariant l_1 vanishes if a triad can be found upon the cone $S\rho\phi_2\rho = 0$ self-conjugate to the cone $S\rho\phi_1\rho = 0$.

In the general case also in which the functions are not self-conjugate, the invariants of their self-conjugate parts (which are of course invariants of the functions themselves) may be regarded as invariants of cones. But there is an important distinction between the two classes of invariants. We have seen (9) that the invariants

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expressible in terms of the roots of the quotient $\phi_2^{-1}\phi_1$ are merely multiplied by a factor when ϕ_1 and ϕ_2 are replaced by $\chi\phi_1\theta$ and $\chi\phi_2\theta$. This transformation, on the other hand, completely modifies the invariants of the self-conjugate parts; in fact they cease to be invariantal for this transformation. The self-conjugate parts Φ_1 and Φ_2 cease to be self-conjugate where multiplied by χ and into θ . When we restrict the range of the transformation by supposing χ and θ to be conjugates or $\chi = \theta'$, the function ϕ_1 , its conjugate ϕ'_1 , and its self-conjugate part Φ_1 all undergo the same transformation; and $\phi_2^{-1}\phi_1$, $\phi'_2^{-1}\phi'_1$, and $\Phi_2^{-1}\Phi_1$ transform into $\theta^{-1}\phi_2^{-1}\phi_1\theta$, $\theta^{-1}\phi'_2^{-1}\phi'_1\theta$, and $\theta^{-1}\Phi_2^{-1}\Phi_1\theta$, so the roots of $\Phi_2^{-1}\Phi_1$ (upon which the cone invariants depend) are unaltered as well as those of $\phi_2^{-1}\phi_1$.

We can see a reason for this. The natural interpretation of the equation

$$S\rho\phi_1\rho = 0$$
, or $S\rho\Phi_1\rho = 0$, or $S\rho\phi'_1\rho = 0$, (xxix)

is that it is the locus of lines at *right angles* to their derived lines. Here a nonprojective element is introduced, and the latitude of transformation consistent with invariance is restricted.

(12.) The vanishing of invariants depending on the roots of $\phi_2^{-1}\phi_1$ does not, in general, imply any peculiarity in the pure parts of the strains represented by ϕ_1 and ϕ_2 . For we have seen in Note III., Section (11.), that a rotation χ can be determined which shall render the roots of $\chi\phi$ equal to any values assignable within certain limits subject to the single condition that their product shall be constant. The magnitudes of the roots may be selected so as to render any function of them zero, and a corresponding rotation χ can be found which will annul any invariant of ϕ_1 and $\phi_2\chi^{-1}$.

It may be shown also that a rotation χ can be found, so that within certain limits one at least of the roots of $\chi \phi_2^{-1} \chi^{-1} \phi_1$ may acquire a selected magnitude. This applies to the invariants of self-conjugate functions (compare the last Section).

(13.) A function ϕ compounded from two or more given functions may be said to be covariant with them, provided ϕ changes into $\chi \phi \theta$ when each of the component functions is multiplied by χ and into θ . Thus $\phi_1 \phi_2^{-1} \phi_1$ is covariant with ϕ_1 and ϕ_2 , but $\phi_1 \phi_2$ and $\phi_1 \phi_2^{-1}$ are not.

Again, if ϕ_1 , ϕ_2 , ϕ_3 , &c. are covariant, and if

$$\nabla \Sigma t_1 \phi_1 \lambda \Sigma t_1 \phi_1 \mu = \Sigma \Sigma t_1 t_2 \psi'_{12} \nabla \lambda \mu, \qquad (xxx)$$

it appears that the functions ψ' transform into $\chi'^{-1}\psi'\theta'^{-1}$ multiplied by the third invariants of θ and of χ when the functions ϕ are changed to $\chi\phi\theta$. Thus the functions ψ' are covariant among themselves, and of course their conjugates ψ which transform into $\theta^{-1}\psi\chi^{-1}$ are likewise covariant among themselves. In like manner, from the functions ψ' we obtain new functions ϕ_{12} by the equation

$$\nabla \Sigma t_1 \psi_1 \lambda \Sigma t_1 \psi_1 \mu = \Sigma \Sigma t_1 t_2 \phi_{12} \nabla \lambda \mu, \qquad (xxxi)$$

which are covariant with the original functions ϕ if we disregard a scalar factor depending on the third invariants of χ and θ .

(14.) The principles explained in the Note on Quaternion Determinants (Note I., Sections (2.) and (3.)) enable us to write down the quaternion invariants of a system of linear vector functions. By actual transformation of the vectors a, β , γ it may be shown that the quotient

$$q(\phi_1, \phi_2, \phi_3) = \begin{vmatrix} \phi_1 a & \phi_1 \beta & \phi_1 \gamma \\ \phi_2 a & \phi_2 \beta & \phi_2 \gamma \\ \phi_3 a & \phi_3 \beta & \phi_3 \gamma \end{vmatrix} \stackrel{a & \beta & \gamma}{a & \beta & \gamma}$$
(xxxii)

is quite independent of these vectors, and is therefore an invariant of the three . functions ϕ_1 , ϕ_2 , ϕ_3 . For if

e find

$$a = x\lambda + y\mu + z\nu, \quad \beta = x'\lambda + y'\mu + z'\nu, \quad \gamma = x''\lambda + y''\mu + z''\nu,$$

$$\begin{vmatrix} \phi_1 a & \phi_1 \beta & \phi_1 \gamma \\ \phi_2 a & \phi_2 \beta & \phi_2 \gamma \\ \phi_3 a & \phi_3 \beta & \phi_3 \gamma \end{vmatrix} = \begin{vmatrix} \phi_1 \lambda & \phi_1 \mu & \phi_1 \nu \\ \phi_2 \lambda & \phi_2 \mu & \phi_2 \nu \\ \phi_3 \lambda & \phi_3 \mu & \phi_3 \nu \end{vmatrix} \cdot \begin{vmatrix} x & y & z \\ x' & y' & z' \\ x'' & y'' & z'' \end{vmatrix}, \quad (xxxiii)$$

and in forming the quotient (xxxii) the scalar determinant (xy'z'') cancels.

(15.) By direct expansion of the determinant, we find

$$6q(\phi_1, \phi_2, \phi_3) Sa\beta\gamma = \Sigma \phi_1 a(\phi_2 \beta \phi_3 \gamma - \phi_2 \gamma \phi_3 \beta), \qquad (xxxiv)$$

where the sign Σ indicates summation for cyclical transposition of the vectors α , β , γ . The scalar part of the quaternion is

$$l_{123} = \operatorname{Sq}(\phi_1, \phi_2, \phi_3) = \frac{1}{6} \Sigma \operatorname{S\phi}_1 a(\phi_2 \beta \phi_3 \gamma + \phi_3 \beta \phi_2 \gamma) (\operatorname{Sa}\beta \gamma)^{-1}; \quad (\mathtt{xxxv})$$

and the vector part reduces without difficulty to

$$\begin{aligned} \nabla q(\phi_1, \phi_2, \phi_3) &= \frac{1}{6} \left[\Sigma \phi_1 a S(\phi_2 \beta \phi_3 \gamma - \phi_3 \beta \phi_2 \gamma) \right. \\ &\quad \left. - \Sigma \phi_2 a S(\phi_3 \beta \phi_1 \gamma - \phi_1 \beta \phi_3 \gamma) \right. \\ &\quad \left. + \Sigma \phi_3 a S(\phi_1 \beta \phi_2 \gamma - \phi_2 \beta \phi_1 \gamma) \right] \left(S a \beta \gamma \right)^{-1}. \end{aligned} \tag{xxxvi} \end{aligned}$$

Now if η_{32} is the spin vector of $\phi'_3\phi_2$,

$$S(\phi_2\beta\phi_3\gamma - \phi_3\beta\phi_2\gamma) = S(\phi'_3\phi_2 - \phi'_2\phi_3)\beta\gamma = 2S\eta_{32}\beta\gamma; \qquad (xxxvii)$$

and the quaternion invariant reduces to

$$q(\phi_1, \phi_2, \phi_3) = l_{123} - \frac{1}{3}(\phi_1 \eta_{23} - \phi_2 \eta_{31} + \phi_3 \eta_{12}): \qquad (xxxviii)$$

for it must be observed that the spin vectors satisfy the equations

$$\eta_{12} + \eta_{21} = 0, \quad \eta_{11} = 0. \quad (\mathbf{x} \mathbf{x} \mathbf{x} \mathbf{i} \mathbf{x})$$

It is evident that the scalar part l_{123} is unchanged when the functions are interchanged in any way. We see by (xxxviii) that briefly

$$q_{321} = \mathbf{K}q_{123}, \text{ and } \frac{2}{3}\phi_1\eta_{23} = q_{132} - q_{123}.$$
 (xl)

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INVARIANTS OF LINEAR VECTOR FUNCTIONS.

The effect of interchange of rows in determinants of the third order is thus exhibited, and we see that the six quaternion invariants obtained by every possible interchange of ϕ_1 , ϕ_2 , and ϕ_3 are equivalent to one scalar and three vector invariants, l_{123} and $\phi_1\eta_{23}$, $\phi_2\eta_{31}$, and $\phi_3\eta_{12}$.

(16.) For a single function ϕ we obtain Hamilton's three invariants as particular cases of (xxxviii) in the forms

$$q(\phi, 1, 1) = \frac{1}{3}(m'' + 2\epsilon); \quad q(\phi, \phi, 1) = \frac{1}{3}(m' + 2\phi\epsilon); \quad q(\phi, \phi, \phi) = m. \quad (xli)$$

For the first of these $\epsilon = \eta_{21} = \eta_{31}$.

(17.) Manifestly these vector invariants are totally different in character from the scalar invariants of the earlier sections of this Note. It is easy to see, when we multiply the three functions (xxxii) into θ , that the quaternion is merely multiplied by the third invariant of θ ; in fact, the determinant quotient is multiplied by the quotient q (θ , θ , θ). It may be proved, without difficulty directly, that η_{23} becomes $n\theta^{-1}\eta_{23}$ in this case. But, when the functions are multiplied by a common function χ , although the scalar part is merely multiplied by the third invariant, the vector part is, in general, completely changed. $\phi'_2\phi_3$ becomes $\phi'_2\chi'\chi\phi_3$, and the spin vector of the transformed function is quite distinct from that of the original, except in the case in which $\chi'\chi$ is a scalar. (Compare also (11.).)

(18.) It would take too long to investigate the reduction of the number of independent quaternion invariants of two or three functions. The functions may be combined in any way, such as in products $\phi_1\phi_2$, $\phi_2\phi_1$, &c., and the various invariants may be obtained by substituting those combinations for the simpler functions in (**xxxii**). It must suffice to remark that, in addition to obvious reductions obtainable by means of symbolic cubics, a simple relation connects the spin vectors of $\phi_1\phi_2$ and of $\phi'_1\phi_2$. For, if ϵ_{12} is the spin vector of $\phi_1\phi_2$, and, as before, if η_{12} is that of $\phi'_1\phi_2$,

$$\begin{aligned} 2\mathrm{V}\epsilon_{12}\rho &= (\phi_1\phi_2 - \phi_2'\phi_1')\rho = ((\phi_1 - \phi_1') + \phi_1')\phi_2\rho + \phi_2'((\phi_1 - \phi_1') - \phi_1)\rho \\ &= 2\mathrm{V}\epsilon_1\phi_2\rho + 2\phi_2'\mathrm{V}\epsilon_1\rho + 2\mathrm{V}\eta_{12}\rho. \end{aligned}$$

This affords the relation

$$\boldsymbol{\epsilon}_{12} = \boldsymbol{\eta}_{12} + (\boldsymbol{m}''_2 - \boldsymbol{\phi}_2)\boldsymbol{\epsilon}_1, \qquad (\mathbf{x}\mathbf{lii})$$

in virtue of the fundamental equation

 $\nabla \phi_2 \lambda \mu + \nabla \lambda \phi_2 \mu + \phi'_2 \nabla \lambda \mu = m''_2 \nabla \lambda \mu.$

From symmetry we may write down, in like manner,

$$\boldsymbol{\epsilon}_{21} = \boldsymbol{\eta}_{21} + (\boldsymbol{m}_{1}' - \boldsymbol{\phi}_{1})\boldsymbol{\epsilon}_{2}. \tag{xliii}$$

In the same way η'_{12} , the spin vector of $\phi_1\phi'_2$, can be expressed in terms of ϵ_{12} and simpler vector invariants. Thus the spin vectors of $\phi_1\phi_2$, $\phi_2\phi_1$, $\phi'_1\phi_2$, $\phi'_2\phi_1$, $\phi_1\phi'_2$, $\phi_2\phi'_1$, $\phi'_1\phi'_2$, $\phi'_2\phi'_1$ are all expressible in terms of η_{12} , ϵ_1 , ϵ_2 , and the results of operating on ϵ_1 and ϵ_2 by the functions ϕ_1 , ϕ_2 and their conjugates.

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By repeated application of these formulæ the spin vectors of all functions derived from a given product of functions, by cyclically transposing the functions and altering them to their conjugates, can be reduced to the spin vector of one of the products and the results of operating on simpler invariants.

19. We may also notice that the quotient

$$\begin{vmatrix} \phi_1 a & \phi_1 \beta \\ \phi_2 a & \phi_2 \beta \end{vmatrix} \div \begin{vmatrix} a & \beta \\ a & \beta \end{vmatrix} = \frac{\psi'_{12} \nabla a \beta - 2S \eta_{12} \nabla a \beta}{2 \nabla a \beta}$$
(xliv)

is unchanged when α and β are replaced by any other vectors in their plane (compare (xxx)).

VI.—ON THE SYSTEM OF LINEAR VECTOR FUNCTIONS $\phi + t\theta$.

(1.) When t is eliminated from the equation

$$V\rho(\boldsymbol{\phi} + t\boldsymbol{\theta})\rho = 0, \tag{i}$$

the locus of axes of the system $\phi + t\theta$ is found to be the cubic cone represented by

$$f = S\rho\phi\rho\theta\rho = 0. \tag{ii}$$

This is also the locus of a vector coplanar with the vectors derived from it by any two functions of the system.

(2.) The cone

$$f' = S\rho\phi'\rho\theta'\rho = 0 \tag{iii}$$

is the locus of axes of the conjugate system. Bearing in mind that the axes of a function are perpendicular to the corresponding planes containing pairs of axes of its conjugate, we see that every edge ρ_1 of the cone f corresponding to the root g_1 of the function $\phi + t\theta$ is perpendicular to ρ'_2 and ρ'_3 edges of the cone f' and axes of the conjugate function. The third edge of the cone f' may, without difficulty, be shown to be $V\rho_1\phi\rho_1$, or $V\rho_1\theta\rho_1$.

(3.) In particular, when both functions are self-conjugate the cones f and f' coincide, and every edge is at right angles to two others. Also since

$$Vi\phi i + Vj\phi j + Vk\phi k = 0, \qquad (iv)$$

when ϕ is self-conjugate, *i*, *j*, and *k* being any mutually rectangular system of unit vectors, it appears that in this case the planes containing pairs of axes of any function cut the cone again in lines which lie in a plane.

(4.) In general the reciprocal of the cone f is the envelope of the principal planes of the system, and, as this is of the third class, three principal planes are parallel to any line.

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SYSTEM OF LINEAR VECTOR FUNCTIONS $\phi + t\theta$.

(5.) The root cubic of the function $\phi + t\theta$ is of the form

$$g^3 - M_1 g^2 + M_2 g - M_3 = 0, (v)$$

and the coefficients contain t in the order indicated by their suffixes. On equating the discriminant to zero, the result is a sextic in t whose roots determine six functions having double roots and pairs of coincident axes.

(6.) No function of the system can have, in general, indeterminate axes; for if $\phi + t\theta$ were such a function, it could be reduced to the form $g\rho + \lambda S\mu\rho$; and the equation of the cone f might then be written in the form

$$S\rho\phi\rho\lambda S\mu\rho = 0. \tag{vi}$$

In this case, therefore, the cone breaks up into a quadric cone and a plane.

(7.) Moreover, if two functions have a common axis, it must be common to the whole system, and the cubic cone must have a double edge. For if in (i) two values of t correspond to a given vector ρ , we must have separately

$$V\rho\phi\rho = 0$$
, and $V\rho\theta\rho = 0$. (vii)

Hence ρ is an axis of every function, and also a double edge of the cone.

(8.) The quadric cone

$$Sa\rho(\phi + t\theta)\rho = 0 \tag{viii}$$

contains the axes of the function defined by t. Or if we regard t as arbitrary and a given, (viii) represents a singly infinite system, a particular cone being determined by the condition that it shall contain any assumed line. This singly infinite system passes through four fixed lines which may be found by combining the equations

$$Sa\rho\phi\rho = 0, \quad Sa\rho\theta\rho = 0.$$
 (ix)

From these we obtain the equation

$$x\alpha = VV\rho\phi\rho V\rho\theta\rho = -\rho S\rho\phi\rho\theta\rho, \qquad (x)$$

which must be satisfied by the four fixed vectors. One solution is obviously $\rho \parallel a$, and for the remaining lines we must have x = 0, and $S\rho\phi\rho\theta\rho = 0$. Thus three of the lines are on the cubic cone f = 0. Hence the axes of all functions of the system compose co-residual triads upon the cubic cone for a quadric cone can be drawn through any set of axes to meet the cubic again in three fixed lines.

(9.) In the notation of elliptic functions, three edges of a cubic cone lie in a plane if the sum of their elliptic parameters is zero. A quadric cone intersects a cubic in six lines, and the sum of the corresponding elliptic parameters is zero. Hence the sum of the parameters of the axes of any function of the system is constant, and the value of this sum is a characteristic of the system.

If the sum is half a *period*, the axes of any pair of functions lie upon a quadric cone. This is the case when the functions are self-conjugate, and more generally

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when the axes of one function (ϕ) are in perspective with the vectors derived from them by the operation of another function θ . This condition is expressed by the equation

$$SV\rho_1\theta\rho_1 V\rho_2\theta\rho_2 V\rho_3\theta\rho_3 = 0 ; \qquad (xi)$$

and this is also the condition that the axes of ϕ and θ should lie upon a quadric cone. In fact, dropping the suffix 3, (xi) is the equation of a cone through the three axes of θ and two of the axes ρ_1 and ρ_2 of ϕ , so, if (xi) is satisfied, it contains the third axis ρ_3 likewise.

The co-residual property shows that, if the perspective property is true for any pair of functions of the system, it is true for every pair.

The condition (xi) may be expressed by the vanishing of the invariant of the functions

$$\Sigma S \theta \phi a \phi \theta \beta \phi \theta \gamma - \Sigma S \phi \theta a \theta \phi \beta \theta \phi \gamma = 0, \qquad (xii)$$

in which α , β , and γ may be any three vectors.

This may be proved (compare *Trans.*, R.I.A., vol. xxx., p. 723, and *Proc.*, R.I.A., 3rd series, vol. iv., p. 13) by replacing α , β , and γ by ρ_1 , ρ_2 , and ρ_3 , and by writing

 $\theta \rho_1 = a_{11}\rho_1 + a_{12}\rho_2 + a_{13}\rho_3$, $\theta \rho_2 = a_{21}\rho_1 + a_{22}\rho_2 + a_{23}\rho_3$, $\theta \rho_3 = a_{31}\rho_1 + a_{32}\rho_2 + a_{33}\rho_3$, (xiii) and substituting in (xi) and in (xii). The result in both cases is proportional to

$$a_{12}a_{23}a_{31} - a_{21}a_{32}a_{13}. \tag{xiv}$$

(10.) The results already obtained admit of very considerable extension. The equation of the cone (ii) may be replaced by

$$S_{\chi_1\rho\chi_2\rho\chi_3\rho} = 0$$
, where $\chi_1 = a_1\phi + b_1\theta + c_1$, &c. (xv)

or by

$$f_1 = S \rho \phi_1 \rho \theta_1 \rho = 0$$
, where $\phi_1 = \chi_1^{-1} \chi_2$, $\theta_1 = \chi_1^{-1} \chi_3$. (xvi)

Thus, the cone is the locus of axes of all functions of the type

$$(a_1\phi + b_1\theta + c_1)^{-1} (a_2\phi + b_2\theta + c_2),$$
 (xvii)

 $a_1, b_1, c_1, a_2, b_2, c_2$ being arbitrary scalars. The cone of the axes of the conjugates

$$f'_{1} = S\rho\phi'_{1}\rho\theta'_{1}\rho = 0$$
, where $\phi'_{1} = \chi'_{2}\chi'_{1}^{-1}$, $\theta'_{1} = \chi'_{3}\chi'_{1}^{-1}$ (xviii)

is not the same as the cone f'. In fact, the equation (iii) of that cone may be replaced by

$$f' = S \rho \chi'_{1}^{-1} \chi'_{2} \rho \chi'_{1}^{-1} \chi'_{3} \rho = 0$$

and this is not the same as (xviii), because the functions χ'_1 , χ'_2 , and χ'_3 are not commutative.

(11.) It appears, from (6), that, in general, no function of the type (xvii) can have indeterminate axes; and, by (7), no pair of functions $\phi_1 = \chi_1^{-1}\chi_2$, $\theta_1 = \chi_1^{-1}\chi_3$ can have a common axis.

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(12.) We shall now extend the theorem of section (8), and show that the axes of all functions of the type (xvii) form co-residual triads. The equations (ix) are equivalent to

$$Sa\rho\chi_1\rho = 0, Sa\rho\chi_2\rho = 0,$$
 (xix)

and these equations require

$$x \nabla a \rho = \nabla \chi_1 \rho \chi_2 \rho \qquad (xx)$$

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if ρ is a common edge. Hence, we obtain the new quadric conc

$$Sa\chi_1\rho\chi_2\rho = 0$$
, or $S\chi_1^{-1}a\rho\chi_1^{-1}\chi_2\rho = 0$ (xxi)

which contains the three residual lines. But the second form of its equation shows that it contains also the axes of $\chi_1^{-1}\chi_2$, and these axes, therefore, are residual to the three intersections of the cones (xix) or (ix), and consequently co-residual with the axes of every function of the type (xvii).

VII.—ON THE GENERAL LINEAR TRANSFORMATION IN SPACE.

(1.) If π and ρ are the vectors from an assumed origin to a pair of corresponding points, the relation between the vectors may be written in the form

$$\varpi = f\rho = \frac{\phi\rho + a}{8\beta\rho + 1},\tag{i}$$

where a and β are constant vectors, and ϕ is a constant linear vector function.

There is no difficulty in verifying that

$$\rho = f^{-1}\varpi = \frac{\phi^{-1}\varpi(S\beta\phi^{-1}a - 1) - \phi^{-1}a(S\beta\phi^{-1}\varpi - 1)}{S\beta\phi^{-1}\varpi - 1}.$$
 (ii)

(2.) The united points of the transformation are the extremities of vectors satisfying the equation

$$f\rho = \rho, \tag{111}$$

$$\phi \rho + a = t \rho, \quad \text{if} \quad t = S \beta \rho + 1.$$
 (iv)

Eliminating ρ between these two equations, the result

$$t - 1 + S\beta(\phi - t)^{-1}a = 0 \qquad (\mathbf{v})$$

is equivalent to a quartic equation, and the united points correspond to the roots of this quartic and lie upon the twisted cubic

$$\rho = -(\phi - t)^{-1}a.$$
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or

(3.) If the plane $S\lambda\rho + 1 = 0$ transforms into $S\mu\omega + 1 = 0$, and if we write symbolically

$$S\mu f\rho = S\rho f'\mu,$$
 (vii)

it appears that

$$\lambda = f'\mu = \frac{\phi'\mu + \beta}{\mathrm{Sa}\mu + 1}.$$
 (viii)

It is needless to write down the equations corresponding to (ii), (iii), (iv), and (v). They are obtained by replacing ϖ , ρ , a, β , ϕ by λ , μ , β , a, ϕ' , respectively; and it will be noticed that the quartic (v) is unaltered by this interchange.

(4.) For a change of origin to the extremity of the vector ϵ , the new symbols are connected with the old by the relations

$$\phi_{\prime} = \frac{\phi - \epsilon S\beta}{S\beta\epsilon + 1}; \quad a_{\prime} = \frac{\alpha + \phi\epsilon - \epsilon(S\beta\epsilon + 1)}{S\beta\epsilon + 1};$$
$$\beta_{\prime} = \frac{\beta}{S\beta\epsilon + 1}; \quad \lambda_{\prime} = \frac{\lambda}{S\lambda\epsilon + 1}; \quad \rho_{\prime} = \rho - \epsilon, \quad (ix)$$

and a root t, of the quartic transformed from (v) is simply proportional to the corresponding root t of the original, the connexion being

$$t_{i} = \frac{t}{S\beta\epsilon + 1} \cdot \tag{x}$$

The ratios of the roots of (v) are therefore independent of the origin.

(5.) When we express an arbitrary vector ρ in terms of the vectors ρ_1 , ρ_2 , ρ_3 , and ρ_4 to the four united points ABCD by the equation (compare Art. 79, page 55, vol. i)

$$0P = \rho = \frac{x_1\rho_1 + x_2\rho_2 + x_3\rho_3 + x_4\rho_4}{x_1 + x_2 + x_3 + x_4},$$
 (xi)

the derived vector $f\rho$ can easily be seen to be expressible in the form*

$$oq = f\rho = \frac{x_1 t_1 \rho_1 + x_2 t_2 \rho_2 + x_3 t_3 \rho_3 + x_4 t_4 \rho_4}{x_1 t_1 + x_2 t_2 + x_3 t_3 + x_4 t_4}.$$
 (xii)

Thus (compare Art. 83, page 58, vol. i),

$$(BC \cdot APDQ) = \frac{t_1}{t_4}, (CA \cdot BPDQ) = \frac{t_2}{t_4}, (AB \cdot CPDQ) = \frac{t_3}{t_4},$$
 (Xiii)

where (BC. APDQ) is the anharmonic of the four planes through the line BC and the points A, P, D, and Q. Or again, the ratio of the volumes of the pyramids, whose bases are a face of the tetrahedron formed by the united points, and whose vertices are Q and P, respectively, is proportional to the corresponding value of t.

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^{*} Compare Note V., Section (6.), p. 378.

VII.] GENERAL LINEAR TRANSFORMATION IN SPACE.

(6.) If f = f' = F, so that the function f may be said to be self-conjugate,

$$F\rho = \frac{\Phi\rho + a}{8a\rho + 1}$$
(xiv)

where Φ is a self-conjugate function. The general equation of a quadric, any point being origin, may be expressed in the form,

$$\mathbf{S}\boldsymbol{\rho}\boldsymbol{F}\boldsymbol{\rho} + 1 = \mathbf{0}.\tag{xv}$$

The extremities of ω and ω' are conjugate with respect to this quadric, if

$$S\omega F\omega' = S\omega' F\omega = -1. \tag{xvi}$$

Hence $F\omega$ is the vector to the reciprocal of the polar plane of the extremity of ω with respect to the quadric, the centre of reciprocation being the origin of vectors, and the radius of reciprocation being unity. The reciprocal quadric is

$$\mathbf{S}\boldsymbol{\nu}\boldsymbol{F}^{-1}\boldsymbol{\nu}+\mathbf{1}=\mathbf{0}.$$
 (xvii)

To determine the tetradedron self-conjugate to a pair of quadrics,

$$S\rho F\rho + 1 = 0$$
 and $S\rho G\rho + 1 = 0$,

it is necessary to solve

$$F\omega = G\omega$$
, or $G^{-1}F\omega = \omega$, or $F^{-1}G\omega = \omega$; (xviii)

for the first equation expresses that the extremity of ω has identical polar planes with respect to the two quadrics.

The first equation may be solved directly. In fact, if Ψ and β in G correspond to Φ and a in F,

$$(\Phi - t\Psi)\omega = -(\alpha - t\beta)$$
 if $Sa\omega + 1 = t(S\beta\omega + 1)$, (xix)

and, therefore,

$$\omega = -(\Phi - t\Psi)^{-1} (\alpha - t\beta), \qquad (xx)$$

where

$$t-1+S(a-t\beta)(\Phi-t\Psi)^{-1}(a-t\beta)=0. \qquad (xxi)$$

We cannot delay on this subject, except to remark that the twisted cubic (xx) is the locus of the vertices of tetrahedra self-conjugate to any pair of quadrics of the doubly infinite system

 $S\omega \left(\Phi + u\Psi \right) \omega + 2S \left(a + u\beta \right) \omega + v = 0.$

(7.) It appears, from (ix), that on change of origin a self-conjugate function will, in general, cease to be self-conjugate. Under what conditions can the origin be selected so that a function may be self-conjugate?

If η is the spin-vector of ϕ , change of origin to the extremity of ϵ will render ϕ , self-conjugate, and $\alpha_i = \beta_i$ (ix), if the equations

$$2\eta = V\epsilon\beta, \quad a + \phi\epsilon - \epsilon (S\beta\epsilon + 1) = \beta$$
 (xxii)

can be satisfied. The second equation gives, by the process already employed,

$$\epsilon = (\phi - t)^{-1} (\beta - a)$$
 if $t = S\beta\epsilon + 1$, or $1 - t + S\beta(\phi - t)^{-1} (\beta - a) = 0$. (xxiii)

Thus, four points can be found for which $a_i = \beta_i$, and consequently η must be equal to one or other of four determinate vectors.

VIII.-ON THE THEORY OF SCREWS.*

(1.) If ϵ is the translation and ι the rotation, the origin being taken as base-point, for any small displacement of a body, the transformation

$$\boldsymbol{\epsilon} = \boldsymbol{\epsilon} \boldsymbol{\iota}^{-1} \cdot \boldsymbol{\iota} = (\mathbf{S} \boldsymbol{\epsilon} \boldsymbol{\iota}^{-1} + \mathbf{V} \boldsymbol{\epsilon} \boldsymbol{\iota}^{-1}) \boldsymbol{\iota} = (p + \boldsymbol{\varpi}) \boldsymbol{\iota}, \quad (p = \mathbf{S} \boldsymbol{\epsilon} \boldsymbol{\iota}^{-1}, \quad \boldsymbol{\varpi} = \mathbf{V} \boldsymbol{\epsilon} \boldsymbol{\iota}^{-1})$$
(i)

shows that the displacement may be accomplished by a rotation round the axis whose equation is $\rho = \varpi + x_i$, accompanied by a proportional translation along that axis. This screw displacement is called a *twist* by Sir Robert Ball. In the same way a moving body is said to have a *twist-velocity* on an instantaneous screw. In the following brief applications of quaternions to the admirable Theory of Screws of Sir Robert Ball, what is said of wrenches will be seen to be equally true of twistvelocities and of small twists.

(2.) If μ represents the resultant couple at the origin of vectors arising from any distribution of forces and couples, and if λ represents the resultant force, the equivalent wrench may be represented by the symbol (μ, λ) . The intensity of a wrench (or the amplitude of a twist) is measured by the tensor of the vector λ ; thus $(t\mu, t\lambda)$ or $t(\mu, \lambda)$ is a wrench having the same axis and the same pitch as (μ, λ) , but t-fold its intensity. It is obvious that the resultant of any number of wrenches $t_1(\mu_1, \lambda_1)$, $t_2(\mu_2, \lambda_2)$, &c., may be represented by the wrench $(t_1\mu_1 + t_2\mu_2 + \&c., t_1\lambda_1 + t_2\lambda_2 + \&c.)$, and by the principle of superposition of small motions this is equally true for twists provided they are small. Every wrench compounded in this manner from *n* independent wrenches is said to belong to an *n*-system, and any particular wrench of the system is determined by the values of the scalars *t*.

(3.) When a body, acted on by a wrench (μ, λ) , receives a small twist (μ', λ') , the work done by the wrench is

$$-S(\mu\lambda'+\mu'\lambda),$$
 (ii)

remembering that μ' represents a translation, and λ' a rotation. The symmetry of this expression shows that the same amount of work would have been done by (μ', λ') considered as a wrench, had the body received the twist represented by (μ, λ) . When the work done is zero, the screws are said to be *reciprocal*. It is obvious from the linear character of the condition of reciprocity that a screw reciprocal to *n* screws is reciprocal to every screw that can be compounded from them.

^{*} Sir Robert Stawell Ball. A Treatise on the Theory of Screws. Cambridge, 1900.

⁺ Compare pages 83-85, and 285-287.

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Again, in terms of the vector perpendiculars ϖ and the pitches p, the expression for the work becomes

$$-(p+p')S\lambda\lambda' - S(\varpi - \varpi')\lambda\lambda' \text{ or } (p+p')\cos A + d\sin A \quad (iii)$$

into the product of the tensors of λ and λ' , if A is the angle and d the shortest distance between the axes. Hence, if the axes of reciprocal screws intersect, they cut at right angles, or else the sum of the pitches is zero; the converse is also true.

(4.) Two screws of the two-system $(\mu + t\mu', \lambda + t\lambda')$ are reciprocal if

$$S(\mu + t\mu')(\lambda + t'\lambda') + S(\mu + t'\mu')(\lambda + t\lambda') = 0, \quad (iv)$$

and the axes cut at right angles if $S(\lambda + t\lambda')(\lambda + t'\lambda') = 0$. These equations lead to a quadratic in t, whose roots determine the pair of screws. Their axes intersect, and, if the origin is taken at the point of intersection, the screws may be represented by (ai, i) and (bj, j), a and b being the pitches. Any screw of the system can be represented by $(ai \cos \theta + bj \sin \theta, i \cos \theta + j \sin \theta)$, and from the relation $ai \cos \theta + bj \sin \theta$ $= (p + \varpi)(i \cos \theta + j \sin \theta)$, we find at once*

$$p = a \cos^2 \theta + b \sin^2 \theta$$
, and $\varpi = (b - a) k \sin \theta \cos \theta$. (v)

Hence, the equation of the cylindroid, the locus of the axes, is seen to be

 $\rho = (b-a)k\sin\theta\cos\theta + s(i\cos\theta + j\sin\theta) \text{ or } z(x^2 + y^2) = (b-a)xy.$ (vi)

(5.) Let (μ_1, λ_1) , (μ_2, λ_2) , and (μ_3, λ_3) be any three wrenches, and let θ be the linear vector function determined by the three equations

$$\mu_1 = \theta \lambda_1, \quad \mu_2 = \theta \lambda_2, \quad \text{and} \quad \mu_3 = \theta \lambda_3.$$
 (vii)

Every wrench that can be compounded from the given wrenches may be represented by $(\theta a, a)$, the vector a being an abbreviation for $t_1\lambda_1 + t_2\lambda_2 + t_3\lambda_3$. If ρ is the vector to any point on the central axis of the wrench $(\theta a, a)$,

$$\theta a = pa + V\rho a$$
, or $(\theta_0 - V(\rho - \epsilon)) a = pa$, (viii)

where θ_0 is self-conjugate, and $\theta = \theta_0 + V\epsilon$. Thus p is a root, and α is an axis of the linear function $\theta_0 - V(\rho - \epsilon)$. The cubic determining the roots of this function is

$$p^{3} - m'' p^{2} + (m' - (\rho - \epsilon)^{2}) p - (m - S(\rho - \epsilon) \theta_{0}(\rho - \epsilon)) = 0, \qquad (ix)$$

if $\theta_0^3 - m''\theta_0^2 + m'\theta_0 - m = 0$ is the symbolic cubic of θ_0 (Note, p. 520, vol. i.). Hence, the locus of axes of screws of the system, having a given pitch p, is the quadric (ix), one of a concentric system. It is also evident by (viii) and (ix) that three axes pass through an assumed point, and that the sum of the corresponding pitches is constant. Again, the pitch and the vector perpendicular are, respectively,†

$$p = S\theta a a^{-1}$$
, and $\varpi = V \theta a a^{-1}$. (x)

^{*} Compare the Note on Systems of Rays, Section 11, p. 422.

[†] Compare Note III., (16.), p. 372.

On comparison with (ix), it appears that the pitch of any screw is inversely proportional to the square of the parallel radius of the zero pitch quadric

$$m = S(\rho - \epsilon) \theta_0 (\rho - \epsilon).$$
 (xi)

We cannot delay upon the locus of the feet of the vector-perpendiculars except to state that it is a Steiner's quartie with three double lines intersecting at the origin, and that the form of the equation $\varpi = \nabla \theta (a_1 + ta_2) (a_1 + ta_2)^{-1}$ shows that the locus for axes parallel to a plane is an ellipse, t alone being variable.

(6.) The wrenches $(\theta a_1, a_1)$ and $(\theta a_2, a_2)$ are reciprocal if

$$S(a_1\theta a_2 + a_2\theta a_1) = 0$$
, or if $Sa_1\theta_0a_2 = 0$; (xii)

that is, if the directions of their axes are conjugate with respect to the zero-pitch quadric (xi). Corresponding to three mutually conjugate directions a_1 , a_2 , and a_3 are three mutually reciprocal or co-reciprocal screws.

(7.) If (μ', λ') is reciprocal to the whole system $(\theta a, a)$, the equation $S(\mu' + \theta'\lambda')a = 0$ must be satisfied for every possible vector a. Hence $\mu' + \theta'\lambda' = 0$, and further, in general, $(-\theta'a', a')$ belongs to a three-system reciprocal to the given three-system. From these considerations it is easy to refer any wrench to six co-reciprocals.

If we assume

$$\mu = \theta a - \theta' a', \text{ and } \lambda = a + a',$$
 (xiii)

where θ is any vector function whatever, and (μ, λ) any given wrench, we see that the auxiliary vectors a and a' are in general determinate, being in fact

$$a = (\theta + \theta')^{-1} (\mu + \theta' \lambda), \text{ and } a' = -(\theta + \theta')^{-1} (\mu - \theta \lambda).$$

Selecting then any two triads $a_1a_2a_3$ and $a_4a_5a_6$ of mutually conjugate directions with respect to the quadric (xi), and referring a and a' to these, so that

$$a = t_1 a_1 + t_2 a_2 + t_3 a_3$$
, and $a' = t_4 a_4 + t_5 a_5 + t_6 a_6$, (xiv)

it appears that the given wrench can be resolved into component wrenches on six arbitrary co-reciprocals. The six scalars t are proportional to the intensities of the components, and play the part of coordinates of the wrench.*

(8.) To refer a four-system to a set of co-reciprocals, determine the vector function θ from three wrenches of the system as in (vii), and reduce any fourth wrench as in (xiii). Thus a_4 is found, and for every wrench of the system t_5 and t_6 are zero. The two-system $(-\theta'(t_5a_5 + t_6a_6), t_5a_5 + t_6a_6)$ is reciprocal to the four-system. In like manner for a five-system we find a' to be of the form $t_4a_4 + t_5a_5$, and the single screw reciprocal to the system is $(-\theta'a_5, a_6)$. Similarly any wrench can be resolved into two components, one belonging to a screw-system, the other to the reciprocal system.

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^{*} Compare Note IV., Section 3, p. 374.

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(9.) The principles explained in the Note on Quaternion Determinants furnish us with a means of writing down a number of invariants for the various screw-systems. For instance, the ratios

$$\begin{vmatrix} \mu_1 & \mu_2 \\ \mu_1 & \mu_2 \end{vmatrix} : 2 \begin{vmatrix} \mu_1 & \mu_2 \\ \lambda_1 & \lambda_2 \end{vmatrix} : \begin{vmatrix} \lambda_1 & \lambda_2 \\ \lambda_1 & \lambda_2 \end{vmatrix}$$
(xv)

are quite independent of any particular screw of the two-system $(\mu_1 + t\mu_2, \lambda_1 + t\lambda_2)$.

In terms of the vector (ϵ) to the centre of the cylindroid and the screws of reference (4.) these ratios reduce to

$$[abk - \epsilon S\epsilon k - (aiS\epsilon i + bjS\epsilon j) \cdot k] : [(a+b)k + 2S\epsilon k + V\epsilon k] : k, \quad (xvi)$$

so that if we write, for brevity, (xv) in the form p:q:r,

$$\epsilon = \mathbf{V} \cdot (\mathbf{V}q + \frac{1}{2}\mathbf{S}q)r^{-1}; \ a + b = \mathbf{S} \cdot qr^{-1}; \ ab = \mathbf{S} \cdot pr^{-1} + \frac{1}{4}r^{-2}(\mathbf{S}q)^{2}.$$

On solution of the equations in a and b we can determine everything in terms of p, q, and r.

Again, for a two-system, every determinant composed of rows μ_1 , μ_2 , μ_3 , followed by rows λ_1 , λ_2 , λ_3 vanishes.

(10.) It is more interesting, however, to consider the relations for systems of higher orders. Write down a determinant, formed by three identical rows of six μ 's, followed by three identical rows of six λ 's. This is the *sexiant* of the six screws, $(\mu_1, \lambda_1) \ldots (\mu_6, \lambda_6)$. If it vanishes, the screws belong to a five-system. Write down four identical rows of seven μ 's, followed by three rows of seven λ 's. The result vanishes identically, for a determinant with four identical vector rows vanishes (Note I., (6.)), but we may expand it in the form

$$\mu_1(1) + \mu_2(2) + \mu_3(3) + \mu_4(4) + \mu_5(5) + \mu_6(6) + \mu_7(7) = 0, \qquad (xvii)$$

where (1) is the sexiant of the screws omitting the first.* Again, four identical rows (λ), followed by three identical rows (μ), form a vanishing determinant expanding into

$$\lambda_1(1) + \lambda_2(2) + \lambda_3(3) + \lambda_4(4) + \lambda_5(5) + \lambda_6(6) + \lambda_7(7) = 0, \quad (xviii)$$

the same symbols denoting the sexiants as before. We see thus how to express an arbitrary screw in terms of six given screws.

[•] It is simplest to expand a sexiant in terms of the minors of the third order when it is seen to be $\Sigma S_{\mu_1 \mu_2 \mu_3} S_{\lambda_4 \lambda_5 \lambda_6}$.

[†] Indeed, from this point of view, the theory of screws is equivalent to the theory of vector pairs (μ, λ) , every pair denoting an entity. There is a corresponding theory of vector triplets (ν, μ, λ) , &c. Writing down four identical rows of ten ν 's, followed by three of μ 's and three of λ 's, we see how to express an arbitrary triplet in terms of nine given triplets by means of functions of nine which may be called noniants in analogy to the sexiants.

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(11.) Again, write down the determinant* of three rows of five μ 's, followed by two of five λ 's, and call it μ' . Similarly, if $-\lambda'$ is the determinant of two rows of μ 's, followed by three of λ 's (the same as before), the screw (μ', λ') may be easily seen to be the reciprocal of the five given screws. If, however, the fifth screw (μ_5, λ_5) is quite arbitrary, the variable screw (μ', λ') obtained in this way generates the twosystem reciprocal to the given four-system.[†]

(12.) If a free rigid body, acted on by any system of forces, receives a small twist from a position of stable equilibrium the forces no longer equilibrate, and a certain wrench corresponding to the twist acts on the body. We shall consider the important case in which the wrench (μ, λ) is linearly expressible in terms of the twist (σ, ω) , that is, when the one-to-one relation between twist and wrench can be expressed by equations of the type

$$\mu = \phi \omega + \chi \sigma, \quad \lambda = \theta \omega + \psi \sigma, \quad (xix)$$

 ϕ , χ , θ , and ψ being four linear and vector functions. As the twist changes from (σ, ω) to $(\sigma + d\sigma, \omega + d\omega)$, the work done by the forces is

$$S(\mu d\omega + \lambda d\sigma) = -S(\phi \omega + \chi \sigma) d\omega - S(\theta \omega + \psi \sigma) d\sigma. \qquad (xx.)$$

This is a perfect differential, or the forces are conservative, if, and only if, ϕ and ψ are self-conjugate, and if χ and θ are conjugate. The truth of this property is apparent when we differentiate an expression such as $-\frac{1}{2}S\omega\Phi\omega - S\sigma\Theta\omega - \frac{1}{2}S\sigma\Psi\sigma$ and compare results on assigning arbitrary values to the four vectors σ , ω , $d\sigma$, and $d\omega$. In what follows we shall limit ourselves to the case of conservative forces, so that we may take ϕ and ψ to be self-conjugate, and

$$\mu = \phi \omega + \chi \sigma, \quad \lambda = \chi' \omega + \psi \sigma. \tag{xxi}$$

This type of relation has been called *Chiastic* by Sir Robert Ball because of the erossconnexion expressed by the equations

$$\begin{split} S\left(\mu\omega'+\lambda\sigma'\right) &= S\left(\phi\omega+\chi\sigma\right)\omega'+S\left(\chi'\omega+\psi\sigma\right)\sigma' \qquad (xxii) \\ &= S\left(\phi\omega'+\chi\sigma'\right)\omega+S\left(\chi'\omega'+\psi\sigma'\right)\sigma=S\left(\mu'\omega+\lambda'\sigma\right), \end{split}$$

which show that if (μ, λ) is reciprocal to (σ', ω') , then is (μ', λ') reciprocal to (σ, ω) .

(13.) A free rigid body is acted on by an impulsive wrench, and begins, in consequence, to twist about an instantaneous screw. Taking the centre of inertia as base-point, it appears that the wrench and twist-velocity are chiastically related, for the dynamical equations are

$$\mu = \phi \omega, \qquad \lambda = M \sigma, \qquad (xxiii)$$

if $\phi\omega$ is the linear vector function of the angular velocity ω which represents the angular momentum, and if M is the mass of the body and σ the velocity of translation of the centre of inertia. Here, as before, the chiastic conditions are satisfied, for ϕ

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^{*} This determinant is a vector as appears on expansion by minors of μ 's and minors of λ 's.

⁺ A system of screws of the most general type is partially considered in Note XII., Sections 26-31.

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is self-conjugate; also χ and θ are zero, and ψ is a scalar M. We proceed to consider the general case of chiastic relation since from this the properties of impulsive and instantaneous screws are at once deducible. We suppose ϕ , χ , and ψ to be known. When the body is not perfectly free we resolve the wrench (μ, λ) into two components, one (η, ξ) belonging to the screw system of the freedom, and the other (η', ξ') belonging to the reciprocal screw-system. The wrench (η, ξ) is the *reduced* wrench. Thus

$$\mu = \eta + \eta' = \phi \omega + \chi \sigma$$
, and $\lambda = \xi + \xi' = \chi' \omega + \psi \sigma$. (xxiv)

Obviously, when (σ, ω) is given, (η, ξ) and (η', ξ') are at once determinate. Again, when (η, ξ) is given, (η', ξ') and (σ, ω) are still determinate. For if (σ_1, ω_1) , (σ_2, ω_2) , &c., are *n* given twists determining the freedom, we may express the known wrench (η, ξ) in the form $(\Sigma a_1 \sigma_1, \Sigma a_1 \omega_1)$, and the unknown twist (σ, ω) in the form $(\Sigma x_1 \sigma_1, \Sigma x_1 \omega_1)$, and remembering that (η', ξ') is reciprocal to all the twists of the freedom, we obtain *n* equations such as

$$S(\eta\omega_1+\xi\sigma_1)=S\omega_1(\phi\omega+\chi\sigma)+S\sigma_1(\chi'\omega+\psi\sigma),$$

which afford the *n* unknown scalars $x_1, x_2, \ldots x_n$.

(14.) Again, for freedom of the n^{th} order there exist *n* principal screws upon which the reduced wrench and the corresponding twist are situated. For if we replace η and ξ by $t\sigma$ and $t\omega$ respectively in the *n* equations we find on elimination of the scalars *x* an equation of the n^{th} degree in *t*, and every root of this determines a principal screw. These screws form a co-reciprocal system. Let (σ_1, ω_1) and (σ_2, ω_2) be two principal twists corresponding to t_1 and t_2 respectively. Thus if we write

$$\begin{bmatrix} 12 \end{bmatrix} = S\omega_1 \phi \omega_2 + S\omega_1 \chi \sigma_2 + S\omega_2 \chi \sigma_1 + S\sigma_1 \psi \sigma_2 = \begin{bmatrix} 21 \end{bmatrix}, \quad (xxv)$$
$$\begin{bmatrix} 12 \end{bmatrix} = S(\eta_1 \omega_2 + \xi_1 \sigma_2) = t_1 S(\sigma_1 \omega_2 + \sigma_2 \omega_1),$$
$$\begin{bmatrix} 12 \end{bmatrix} = S(\eta_2 \omega_1 + \xi_2 \sigma_1) = t_2 S(\sigma_1 \omega_2 + \sigma_2 \omega_1); \quad (xxvi)$$

and also

we see that

hence, if
$$t_1$$
 is not equal to t_2 , we must have $S(\sigma_1\omega_2 + \sigma_2\omega_1) = 0$, and the screws are
reciprocal; and also we have $[12] = 0$, and the screws are said to be *conjugate* screws
of the potential. We shall now examine the conditions of reality of the principal
screws. They are evidently real if all the roots t are real. If, however, $t_1 = t + ht'$,
and if $t_2 = t - ht'$, where $h = \sqrt{-1}$, it appears that the corresponding twists must be
of the form

 $(\sigma_1, \omega_1) = (\sigma + h\sigma', \omega + h\omega'), \text{ and } (\sigma_2, \omega_2) = (\sigma - h\sigma', \omega - h\omega').$

If these are conjugate we must have

 $[12] = (S\omega\phi\omega + 2S\omega\chi\sigma + S\sigma\psi\sigma) + (S\omega'\phi\omega' + 2S\omega'\chi\sigma' + S\sigma'\psi\sigma') = 0. \quad (xxvii)$

But this cannot be the case when the potential function $-\frac{1}{2}S\omega\phi\omega - S\omega\chi\sigma - \frac{1}{2}S\sigma\psi\sigma$ is essentially one-signed. Under this condition therefore the principal screws are real.

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(15.) On Sir Robert Ball's suggestion I append the quaternion treatment of two important parts of the theory of screws. In general, the twist velocity of a body acted on by constraints alone is constantly changing. Under certain conditions, however, the twist velocity remains for a moment unchanged. The instantaneous screw is then said to be *permanent*. Permanent and principal screws are in general quite distinct, though they are identical in the case of a body having one point fixed. We may write the dynamical equations in the form

$$\Sigma m \rho = \xi', \quad \Sigma m \nabla \rho \ddot{\rho} = \eta',$$
 (xxviii)

m being the element of mass at the extremity of the vector ρ , and (η', ξ') being the wrench arising from the constraints referred to the origin of vectors as base point. If (σ, ω) is the twist velocity, we have

$$\dot{\rho} = \sigma + V\omega\rho$$
, and $\ddot{\rho} = \dot{\sigma} + V\dot{\omega}\rho + V\omega\dot{\rho} = \dot{\sigma} + V\dot{\omega}\rho + V\omega(\sigma + V\omega\rho)$. (xxix)

For a permanent screw $\dot{\sigma}$ and $\dot{\omega}$ vanish, and if the origin of vectors is taken at the centre of mass, we find, on summation,

$$\Sigma m \ddot{\rho} = M V \omega \sigma = \xi', \quad \Sigma m V \rho \dot{\rho} = V \omega \phi \omega = \eta', \quad (xxx)$$

where $\phi \omega = \sum m V_{\rho} V \omega_{\rho}$ is the angular momentum of the body (compare 417, X.). In particular for three degrees of freedom if $\sigma = \theta \omega$, then $\eta' = -\theta' \xi'$, because the wrenches arising from the constraints are reciprocal to the twist velocities. Hence

$$V\omega\phi\omega = \eta' = -\theta'\xi' = -M\theta'V\omega\sigma = -M\theta'V\omega\theta\omega,$$

or, if n is the third invariant of θ ,

$$\mathbf{V}\boldsymbol{\omega}\boldsymbol{\phi}\boldsymbol{\omega} = Mn^{-1}\mathbf{V}\boldsymbol{\omega}\boldsymbol{\theta}^{-1}\boldsymbol{\omega}: \qquad (\mathbf{x}\mathbf{x}\mathbf{x}\mathbf{i})$$

so the permanent screws have their axes parallel to the axes of the function $\phi - Mn^{-1}\theta^{-1}$.

(16.) In the same case of freedom of the third order the principal screws are given by

$$\phi \omega = t\sigma + \eta', \quad M\sigma = t\omega + \xi', \quad (xxxii)$$

and from these as $\eta' = -\theta'\xi'$, and $\sigma = \theta\omega$,

$$\phi \omega = t(\theta + \theta')\omega - M\theta'\theta\omega, \qquad (xxxiii)$$

so that the principal screws are parallel to the axes of the function $(\theta + \theta')^{-1} (\phi + M\theta'\theta)$.

(17.) The second point suggested by Sir Robert Ball is a proof of the theorem that "two three-systems can in general be *in one way* correlated so that each screw in one regarded as an impulsive screw, has a corresponding screw in the other regarded as an instantaneous screw" (Theory of Screws, Art. 318). This theorem arises from the determination of the dynamical constants of a free body by administering three known impulsive wrenches, and by observing the twist velocities produced. The dynamical equations are three pairs of the type

$$\phi \omega = \mu + V \lambda \rho, \quad M(\sigma + V \omega \rho) = \lambda, \quad (xxxiv)$$

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where (μ, λ) is a known wrench, (σ, ω) a known twist velocity, and where ϕ , ρ , and M, the vector function, the vector to the centre of mass and the mass of the body are unknown. The three wrenches produce a three-system $\mu = \theta_1 \lambda$, the three twist velocities another $\sigma = \theta_2 \omega$, and in terms of θ_1 and θ_2 the equations (xxxiv) become

$$\boldsymbol{\phi}\omega = (\theta_1 - \nabla \rho)\lambda, \quad M(\theta_2 - \nabla \rho)\omega = \lambda.$$
 (XXXV)

Hence, for three and therefore for all vectors ω ,

$$\phi \omega = M(\theta_1 - V\rho) (\theta_2 - V\rho)\omega. \qquad (xxxvi)$$

Now ϕ is a self-conjugate, and therefore if n''_1 and n''_2 are the first invariants of θ_1 and θ_2 respectively, by a well-known property of Hamilton's function χ ,

$$\begin{aligned} (\theta_1\theta_2 - \theta'_2\theta'_1)\omega &= \mathrm{V}\rho\theta_2\omega + \theta'_2\mathrm{V}\rho\omega + \theta_1\mathrm{V}\rho\omega + \mathrm{V}\rho\theta'_1\omega \\ &= \mathrm{V}(n''_2 - \theta_2)\rho\omega + \mathrm{V}(n''_1 - \theta'_1)\rho\omega = 2\mathrm{V}\epsilon_{12}\omega, \end{aligned}$$

if ϵ_{12} is the spin-vector of $\theta_1 \theta_2$. Thus ρ is uniquely determined by the equation

$$(n''_1 + n''_2 - \theta_2 - \theta'_1)\rho = 2\epsilon_{12}, \qquad (xxxvii)$$

which is a necessary consequence of the self-conjugate property of ϕ . The vector ρ being known, $M^{-1}\phi$ is determined by (xxxvi), and M by the second equation (xxxiv). Thus ϕ , ρ , and M are uniquely found. Also the unique correlation between the three-systems is established by (xxxv). It is very instructive to investigate step by step the amount of information afforded as to the dynamical nature of the body by observing the twist velocities produced by known wrenches.*

IX.—ON FINITE DISPLACEMENTS.

(1.) It has been shown that the operator $q(\)q^{-1}$ produces a conical rotation of a system of vectors about their common origin, the axis of the rotation having the direction of the quaternion or versor q, and the angle of the rotation being double the angle q. Any displacement of a rigid body may be effected by rotating the body about the origin of vectors until lines in the body are parallel to the positions they will ultimately occupy, and by then translating the body until one point (and therefore all points) attains its final position. Thus if τ is equal and parallel to the translation, the vectors ϖ and ρ to a point in the body, in its initial and final positions, are connected by the relation

$$\rho = \tau + q \varpi q^{-1}. \tag{1}$$

^{*} Additional illustrations of the Theory of Screws will be found in the Notes of this Appendix IX. to XII. inclusive.

(2.) We may write this equation in the form

$$\rho - \tau' + \epsilon + q(\varpi - \epsilon)q^{-1}, \quad \text{if} \quad \tau' = \tau + q\epsilon q^{-1} - \epsilon, \tag{ii}$$

with the interpretations following. The same rotation about the extremity of ϵ changes ϖ into $\epsilon + q (\varpi - \epsilon)q^{-1}$, and the translation τ' completes the displacement. Or a translation $-\epsilon$, followed by the rotation about the origin, and then by the translation $\tau' + \epsilon$, is equivalent to the displacement. For example, writing (i) in the form $\rho = q (q^{-1}\tau q + \varpi)q^{-1}$, we see that the translation $q^{-1}\tau q$, followed by the rotation about the origin, effects the displacement.

(3.) The relation (ii) connecting the translations τ' and τ , which must follow rotations about different points in any given displacement, shows that the difference of these translations $(\tau' - \tau)$ is equal to the displacement one point would receive were the body rotated about the other. The components of τ' and τ along the axis of rotation are consequently equal. Or multiplying the relation (ii) into q, we have

$$(\tau' - \tau) q = q\epsilon - \epsilon q = 2 \nabla \cdot \nabla q\epsilon;$$
 (iii)

whence

$$\mathbf{x} = -\frac{1}{2} \left(\boldsymbol{\tau}' - \boldsymbol{\tau} \right) q \left(\mathbf{V} q \right)^{-1} + x \mathbf{V} q \; ; \quad \mathbf{S} \left(\boldsymbol{\tau}' - \boldsymbol{\tau} \right) \mathbf{V} q = 0. \tag{iv}$$

Thus given τ' , the locus of the extremity of ϵ is a right line parallel to the axis of rotation.

(4). The equation of the central axis is found by expressing that the translation $\tau' = \tau_0$ is parallel to the axis of rotation. By (iv) the equation of the central axis, and the value of τ_0 , are found to be

$$\epsilon = \frac{1}{2} \nabla \tau q \, (\nabla q)^{-1} + x \nabla q ; \qquad (\nabla)$$

$$\tau_0 = (\mathbf{V}q)^{-1} \mathbf{S}\tau \mathbf{V}q. \tag{vi}$$

(5). The general decomposition of a displacement into a pair of displacements results from comparison of (i) with

$$\rho = \tau_2 + q_2(\tau_1 + q_1 \varpi q_1^{-1}) q_2^{-1}, \qquad (vii)$$

and the conditions evidently are

$$q_2 q_1 = q;$$
 $\tau = \tau_2 + q_2 \tau_1 q_2^{-1}.$ (viii)

If these displacements are a pair of rotations effected about the points \mathbf{E} and \mathbf{F} fixed in space, or the points \mathbf{E} and \mathbf{F}' fixed in the body,

$$\tau_1 = \epsilon - q_1 \epsilon q_1^{-1}; \quad \tau_2 = \epsilon + \eta - q_2(\epsilon + \eta) q_2^{-1}; \quad \eta = q_1 \eta' q_1^{-1} \quad (\mathbf{i}\mathbf{x})$$

if $\epsilon = 0E$, $\eta = EF$, $\eta' = EF'$. Thus (viii) becomes

$$\tau = \epsilon - q\epsilon q^{-1} + \eta - q_2\eta q_2^{-1} = \epsilon - q\epsilon q^{-1} + q_1\eta' q_1^{-1} - q\eta' q^{-1}.$$
(x)

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Writing for abridgment

$$\mathbf{ET}' = \tau' = \tau - \epsilon + q \epsilon q^{-1}, \qquad (\mathbf{xi})$$

if E is arbitrarily selected the point T' is determined, and by (x) the second rotation changes EF into a line equal and parallel to T'F. The locus of F is, therefore, the plane bisecting ET' at right angles, and the second rotation may be made about any line in this plane. The first rotation may be found by (viii) when q_2 is suitably selected. In like manner if $T''E = q^{-1}ET'q$, we find by (x) $q_2^{-1}EF'q_2 = T''F'$, and the locus in the body is the plane bisecting ET'' at right angles.

Again by (x) if q_1 or q_2 is arbitrarily selected, E and F must lie respectively in the planes determined by

$$S(\tau - \epsilon + q\epsilon q^{-1})Vq_2 = 0$$
 and $S(\tau - \eta + q_2\eta q_2^{-1})Vq = 0.$ (xii)

Selecting any point E in the first of these planes, T' is determined by (xi) and the axis of the second rotation is the intersection of the second plane with that bisecting ET' at right angles.

(6.) When the body is in the position (i) defined by τ and q, a rotation about the point \mathbf{r}' , followed by a translation, carries it to the position given by

$$\rho' = \tau' + \epsilon' + q'(\tau - \epsilon')q'^{-1} + q'q \varpi q^{-1}q'^{-1},$$

while the same translation, followed by the same rotation about E'', carries it to the position

$$\rho'' = \epsilon'' + q'(\tau - \epsilon'' + \tau')q'^{-1} + q'q\varpi q^{-1}q'^{-1}.$$

The difference in the positions is equivalent to a translation

$$\rho' - \rho'' = \tau' + \epsilon' - \epsilon'' - q'(\tau' + \epsilon' - \epsilon'')q'^{-1} = 2\nabla \cdot (\tau' + \epsilon' - \epsilon'')\nabla q' \cdot q'^{-1}, \quad (\text{xiii})$$

which is small and of the second order if $\tau' + \epsilon' - \epsilon''$ and $Vq' \cdot q'^{-1}$ are small and of the first order. Under these conditions the order in which the additional translation and rotation are effected is in the limit immaterial. If the additional rotation is made about the origin of the vectors ϖ , which is a point fixed in the body and at the extremity of τ , the new position is given by

$$\rho' = \tau' + \tau + q' q \varpi q^{-1} q'^{-1}. \qquad (xiv)$$

(7.) When q and τ are functions of a single parameter, the equation (i) contains full particulars of the path of the body, and if the parameter is a known function of the time, the velocity of the displacement may be completely determined. If

$$\rho + \mathrm{d}\rho = \tau + \mathrm{d}\tau + (q + \mathrm{d}q)\varpi(q + \mathrm{d}q)^{-1},$$

the two following expressions for do supposed infinitesimal,

$$d\rho = d\tau + V d\omega q \varpi q^{-1} \quad \text{where} \quad d\omega = 2V \cdot dq q^{-1}, \qquad (xv)$$

- $d\rho = d\tau + q \nabla d\iota \pi q^{-1}$ where $d\iota = 2\nabla \cdot q^{-1} dq$,* (xvi)
 - * Evidently $q^{-1}d\omega q = 2V \cdot q^{-1}(dqq^{-1})q = d\iota$.

IX.]

easily follow from the consideration that if a is any small quaternion and ξ any vector

$$(1+a)\xi(1+a)^{-1} - \xi = (1+a)\xi(1-a) - \xi = a\xi - \xi a = 2VVa\xi$$

The first of these expressions shows that the additional displacement is due to the translation $d\tau$ and to the rotation $d\omega$ about the body origin applied after the rotation $q(\)q^{-1}$. The second shows that had the body originally received the rotation about the body origin represented by $d\iota$, then the rotation $q(\)q^{-1}$, and finally the translation $\tau + d\tau$, the same position would have been attained.

(8.) If ϵ is the vector from the fixed origin to any point on the axis of the instantaneous screw, and if p is its pitch,

$$d\tau = (p + V(\epsilon - \tau))d\omega,$$
 (xvii)

because $\epsilon - \tau$ is the vector from the body origin, the base point to which $d\tau$ and $d\omega$ are referred, to a point on the axis. The pitch and the equation of the axis are, by (xv),

$$p = \frac{1}{2} \operatorname{Sd} \tau (\operatorname{V} \cdot \operatorname{d} q q^{-1})^{-1}; \qquad \epsilon = \tau + \frac{1}{2} \operatorname{V} (\operatorname{d} \tau + x) (\operatorname{V} \cdot \operatorname{d} q q^{-1})^{-1}, \qquad (\operatorname{xviii})$$

x being a variable scalar. Allowing the parameter in τ and q, as well as x, to vary, the vector equation represents the locus in space of the axes of the instantaneous screws.

The body locus of the axes may be obtained by substituting $\epsilon - \tau = q\eta q^{-1}$ in (xvii) or (xviii), when we find

$$q^{-1}\mathrm{d}\tau q = (p + \mathrm{V}\eta)\mathrm{d}\iota \tag{xix}$$

and
$$\eta = \frac{1}{2} V(q^{-1} d\tau q + x) (V \cdot q^{-1} dq)^{-1}.$$
 (xx)

If we suppose these two surfaces to be constructed and fitted with guiding threads or projections and depressions of suitable pitch, then when the body locus is suitably placed on the space locus with corresponding generators in contact and rolled over it subject to the constraint of the guides which will cause gliding along the line of contact, the body will traverse the path prescribed.

(9.) When q and τ are functions of two parameters, u and v, the body has two degrees of freedom. Given ϖ , equation (i) represents a surface which would be generated by a point fixed in the body were the body to describe every possible path. The equation (xvii) is linear in the ratio du : dv, and represents a singly infinite system of screws whose axes lie upon a cylindroid represented by the vector equation (xviii), when the ratios x : du : dv vary arbitrarily. On account of the linearity of (xvii) it appears that if two screws of the same pitch intersect, all the screws lie in a plane, and pass through a common point. When the expression for p is rendered integral by multiplying by T $(V^{-1}dqq^{-1})^2$, a quadratie in du : dv results which determines two, and, in general, only two instantaneous motions of given pitch. If three screws have the same pitch, then all have the same pitch, and it is not hard to see, by (xvii), without assuming any property of the cylindroid, that all the axes lie in a plane, and pass through a common point.

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ΓIX.

FINITE DISPLACEMENTS.

In general, for two degrees of freedom, every point of the body on one or other of two lines, will describe an element of a line, not of a surface, as the body receives every possible small displacement from a given position. The lines are the axes of the two screws of zero pitch. For every small displacement may be compounded from rotations about these lines, and a point on one line suffers displacement only on account of the rotation about the other. The normal to the element of surface described by any point in the body must intersect these two lines, for the normal is at right angles to every possible displacement of the point, and, in particular, to that due to a rotation about either of the lines.*

(10.) We arrive at the particular case of which Darboux has made an extensive use in his kinematical treatment of surfaces by expressing that a plane carried by the body constantly touches the surface described by a point fixed in the plane. Comparing (xv) and (xvi) the condition is simply

$$\mathrm{Sd}\rho q\gamma q^{-1} = 0$$
, or $\mathrm{S}\left(\mathrm{d}\tau q\gamma q^{-1} + \mathrm{d}\omega q \varpi \gamma q^{-1}\right) = 0$, or $\mathrm{S}\left(\mathrm{d}\sigma\gamma + \mathrm{d}\iota \varpi\gamma\right) = 0$, (xxi)

if γ is the direction fixed in the body of the normal to the plane, and if, for brevity, $d\sigma = q^{-1}d\tau q$. This condition must be satisfied for every possible displacement, so that if we write

$$d\sigma = \sigma_1 du + \sigma_2 dv, \quad d\iota = \iota_1 du + \iota_2 dv, \quad (xxii)$$

we must have separately

$$S(\sigma_1\gamma + \iota_1 \varpi \gamma) = 0, \quad S(\sigma_2\gamma + \iota_2 \varpi \gamma) = 0.$$
 (xxiii)

And there is no difficulty in seeing that the same results would have followed had we expressed that a line fixed in the body constantly intersects the two axes of zero pitch (9.).

It is evident that $d\iota$ may be regarded as representing the elementary angular rotation $d\omega$ referred to directions fixed in the body; indeed, it has been shown that $d\iota = q^{-1}d\omega q$. In like manner, $d\sigma$ is the small displacement in space of the body origin referred to fixed directions in the body. It must be carefully remembered that $d\sigma$, $d\omega$, and $d\iota$ are not like $d\tau$ or dq differentials of vectors σ , ω , and ι . In fact, by (7),†

$$\frac{\partial \sigma_1}{\partial v} = 2 \mathbf{V} \cdot q^{-1} \frac{\partial \tau}{\partial u} q \mathbf{V} q^{-1} \frac{\partial q}{\partial v} + q^{-1} \frac{\partial^2 \eta}{\partial u \partial v} q,$$

and

$$\frac{\partial \sigma_2}{\partial u} = 2 \mathbf{V} \cdot q^{-1} \frac{\partial \tau}{\partial v} q \mathbf{V} q^{-1} \frac{\partial q}{\partial u} + q^{-1} \frac{\partial^2 \eta}{\partial u \partial v} q,$$

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^{*} Compare Darboux, Leçons sur la Théorie Générale des Surfaces, Art. 58.

[†] Compare Darboux, loc. cit., Arts. 55 and 40.

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 $\frac{\partial \sigma_1}{\partial v} - \frac{\partial \sigma_2}{\partial u} = \nabla (\sigma_1 \iota_2 - \sigma_2 \iota_1); \quad \text{also} \quad \frac{\partial \iota_1}{\partial v} - \frac{\partial \iota_2}{\partial u} = \nabla \iota_1 \iota_2;$

so that, on subtraction,

$$2\frac{\partial}{\partial v}\nabla q^{-1}\frac{\partial q}{\partial u} - 2\frac{\partial}{\partial u}\nabla q^{-1}\frac{\partial q}{\partial v} = -2\nabla q^{-1}\frac{\partial q}{\partial v}q^{-1}\frac{\partial q}{\partial u} + 2\nabla q^{-1}\frac{\partial q}{\partial u}q^{-1}\frac{\partial q}{\partial v}$$
$$= 4\nabla \nabla q^{-1}\frac{\partial q}{\partial u}\nabla q^{-1}\frac{\partial q}{\partial v}.$$

Returning to equations (xxiii), if these are always satisfied for constant vectors γ and ϖ , we can derive four new equations by differentiating each with respect to u and v, and equating the results to zero. Thus, six equations are obtained which lead to differential equations in τ , q, u, and v, when γ and ϖ are eliminated. Observing that ϖ occurs in the equations only in the combination $\nabla \pi \gamma$, it is evident that every point on the line in the body through the extremity of ϖ parallel to γ will describe a surface constantly touched by the plane through the point and at right angles to γ .

(11.) We have noticed in Section 9 the conditions under which a point is common to the axes of all the screws corresponding to small motions with two degrees of freedom. Replacing $d\tau$ and $d\omega$ by τ_1 , ω_1 and τ_2 , ω_2 successively in (xvii), we deduce, from the resulting equations, the expression for the vectors to the point of intersection,

$$\epsilon = \tau - \frac{\mathrm{V}\left(\tau_1 - p\omega_1\right)\left(\tau_2 - p\omega_2\right)}{\mathrm{S}\left(\tau_1 - p\omega_1\right)\omega_2}, \quad \text{and} \quad 2p\mathrm{S}\omega_1\omega_2 = \mathrm{S}(\omega_1\tau_2 + \omega_2\tau_1). \quad (\mathbf{x}\mathbf{x}\mathbf{v})$$

If the pitches are everywhere equal and constant, the space and body loci of the common intersection of the axes are

$$\rho = \epsilon, \text{ and } \varpi = q^{-1}(\epsilon - \tau)q;$$
(XXVi)

and corresponding elements of these surfaces are

$$d\rho = d\epsilon$$
, and $d\varpi = q^{-1} (d\epsilon - p d\omega)q$; (xxvii)

the second expression being reduced by (xvii) from

$$\mathrm{d}\boldsymbol{\varpi} = q^{-1} \left(\mathrm{d}\boldsymbol{\epsilon} - \mathrm{d}\boldsymbol{\tau} \right) q + 2q^{-1} \left(\mathrm{V} \left(\boldsymbol{\epsilon} - \boldsymbol{\tau} \right) \mathrm{V} \mathrm{d} q q^{-1} \right) q.$$

In the case in which p is zero, the lengths of corresponding elements are equal, and we deduce the elegant theorem of M. Ribaucour,* the loci not only touch, but roll on one another without sliding. The surfaces are *applicable*.

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(xxiv)

^{*} Darboux. loc. cit., Art. 58; Ribaucour, Sur la déformation des surfaces (Comptes rendus, t. lxx.. p. 330).

IX., X.] KINEMATICAL TREATMENT OF CURVES.

(12.) The usual formulæ with respect to moving axes may be deduced from the following equations, in which the quaternion and vector, q and σ are variable in any manner. The vectors ρ and $q\pi q^{-1}$ being regarded as terminating at a common point, while the former originates at a point fixed in space, and the latter at the extremity of the vector $q\sigma q^{-1}$,

 $\rho = q (\sigma + \pi)q^{-1}$, and $d\rho = q (d\sigma + d\pi)q^{-1} + q \operatorname{Vd} \iota (\sigma + \pi)q^{-1}$. (xxviii)

Hence

$$D\rho = q^{-1}d\rho q = d\sigma + d\varpi + Vd\iota (\sigma + \varpi), \qquad (xxix)$$

if we write simply as a matter of notation, $D\rho = q^{-1}d\rho q$. This formula includes the usual formulæ of small displacement, or velocity, with respect to moving axes. Differentiating ρ a second time by the characteristic d, we may write

$$\mathbf{D}^{2}\rho = q^{-1}\mathbf{d}^{2}\rho q = \mathbf{d}^{2}\sigma + \mathbf{d}^{2}\varpi + \mathbf{V}\mathbf{d}^{2}\iota\left(\sigma + \varpi\right) + 2\mathbf{V}\mathbf{d}\iota\left(\mathbf{d}\sigma + \mathbf{d}\varpi\right) + \mathbf{V}\mathbf{d}\iota\mathbf{V}\mathbf{d}\iota\left(\sigma + \varpi\right), \quad (\mathbf{x}\mathbf{x}\mathbf{x})$$

which includes the formulæ of acceleration. Of course if π is fixed with respect to the moving axes, the terms in $d\pi$ and $d^2\pi$ disappear.

X.-ON THE KINEMATICAL TREATMENT OF CURVES.

(1.) To extend the kinematical method employed in Art. 396, imagine a point travelling with unit velocity along the curve and carrying with it three mutually rectangular unit vectors a, β , and γ , so that a continually touches the curve, while the plane of a and β preserves closest contact with it, or in other words, osculates it. If we choose we may select β , so that in its initial position it has the direction of the principal normal. Having made a selection once for all, there will be no confusion, provided the motion is continuous.

It is geometrically obvious that the angular velocity (ω) of the system may be resolved into two components round α and γ ; thus we may write

$$\omega = aa_1 + \gamma c_1. \tag{i}$$

We may regard a_1 and c_1 as the deriveds with respect to the arc s of two angles a and c. Of these a is the total angle through which the system has turned about a, starting from any initial point on the curve; in like manner c is the total angle through which the system has turned about γ ; and it is convenient to suppose that at the initial point s = 0. We shall use a_2 , c_3 , &c., to denote the second and third deriveds of a and c.

It is obvious that a_1 is the torsion, and c_1 the curvature at the point considered.

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APPENDIX—NOTES. [X.

(2.) If, as in 396 (5.), η is any emanant vector drawn from the moving point, we have by the general formula given in the note to p. 293 the relation

$$D_s \eta = \frac{d\eta}{ds} + V \omega \eta, \qquad (ii)$$

where in passing along the curve $D_s\eta$ is the absolute rate of change of the vector η , and $\frac{d\eta}{ds}$ its rate of change relative to the moving system. If η is fixed relatively to the system, (ii) reduces to

$$D_s \eta = V \omega \eta, \tag{iii}$$

and this equation by (i) gives, if $\alpha\beta = +\gamma$,

$$D_s \alpha = \beta c_1; \quad D_s \beta = \gamma a_1 - \alpha c_1; \quad D_s \gamma = -\beta a_1.$$
 (iv)

(3.) Again, if ρ is the vector to the moving point

$$D_s \rho = \alpha, \qquad (v)$$

and we may differentiate successively and obtain by (iv)

$$\begin{array}{l} \mathbf{D}_{s}^{2}\rho = \beta c_{1}, \\ \mathbf{D}_{s}^{3}\rho = \beta c_{2} + (\gamma a_{1} - ac_{1})c_{1}, \\ \mathbf{D}_{s}^{4}\rho = \beta c_{3} + 2(\gamma a_{1} - ac_{1})c_{2} + (\gamma a_{2} - ac_{2})c_{1} - \beta(a_{1}^{2} + c_{1}^{2})c_{1}. \end{array} \right\}$$
(vi)

In general, if
$$D_s n \rho = A_n \alpha + B_n \beta + C_n \gamma$$
, (vii)

the coefficients A_n , B_n , C_n are assignable functions of the scalars a_1 and c_1 and of their successive deriveds. It is evident by (vi) that the deriveds of highest order occur in the term

$$\beta c_{n-1} + \gamma a_{n-2} c_1. \tag{viii}$$

(4.) This method lends itself readily to the consideration of the contacts of curves. Writing down a few terms in the development in powers of s,

$$\rho = \rho_0 + sa + \frac{1}{2}s^2\beta c_1 + \frac{1}{6}s^3(\beta c_2 + (\gamma a_1 - ac_1)c_1) + \&c., \qquad (ix)$$

we see that the deviation from an osculating curve is $\frac{1}{3}s^3(\beta c_2 + \gamma a_1c_1)$ for a circle; $\frac{1}{3}s^3\gamma a_1c_1$ for a parabola or conic; and $\frac{1}{3}s^3\beta c_2$ for a helix (p. 97); because a_1 and c_2 are zero for the circle, a_1 for the conic and c_2 for the helix. Generally by (viii) the deviation between two curves is ultimately

$$\frac{s^{n}}{\lfloor \frac{n}{2} \rfloor} \left[\beta(e_{n-1} - e'_{n-1}) + \gamma(a_{n-2} - a'_{n-2})e_{1} \right].$$
(x)

Though the work is necessarily long, there is no difficulty in finding the equation of Hamilton's twisted cubic by assuming as its equation $V(\rho - \rho_0)\phi(\rho - \rho_0) + V\lambda(\rho - \rho_0) = 0$,

KINEMATICAL TREATMENT OF CURVES.

and differentiating until a sufficient number of equations are obtained to determine λ and ϕ . Perhaps even more briefly the result may be obtained by assuming

$$\rho = \rho_0 + (\phi - t)^{-1}\lambda$$
 where $t = s^{-1} + t_0 + t_1s + \&c.,$ (xi)

and determining λ , ϕ and the coefficients t_0 , t_1 , &c., so that λ may equal $(\phi - t) (\rho - \rho_0)$, neglecting only powers of the sixth order in s.

(5.) To illustrate integration of equations (iv), assume that the ratio of curvature to torsion is constant. If $c_1 = a_1 \tan H$, the first and third equations give immediately

$$D_{\epsilon}(a \cos H + \gamma \sin H) = 0, \text{ or } a \cos H + \gamma \sin H = k, \quad (xii)$$

k being a constant and unit vector of integration. The principal normal β is thus at right angles to a fixed direction, and the curve is traced on a cylinder whose generators are parallel to k. It is a geodesic because β is normal to the cylinder or because the curve cuts the generators at a constant angle H.

We now assume $\beta = i \cos l + j \sin l$ when the second equation (iv) shows that

$$D_s\beta = k\beta \frac{dl}{ds} = (\gamma \cos H - a \sin H) \frac{dl}{ds} = \gamma a_1 - ac_1,$$

and requires

$$\mathrm{d}l = \operatorname{cosec} H \mathrm{d}c = \operatorname{sec} H \mathrm{d}a = \sqrt{a_1^2 + c_1^2} \, \mathrm{d}s.$$

Hence if a_1 or c_1 is known in terms of s, l is determined; otherwise l is an arbitrary function of s. Since $\gamma = \alpha\beta$, we have by (xii)

$$D_{s\rho} = a = k (\cos H - (i \cos l + j \sin l) \sin H),$$

so that if ρ_0 is a new constant of integration

$$\rho = \rho_0 + \int_0^s \alpha \mathrm{d}s = \rho_0 + ks \cos H - k \sin H \int_0^s (i \cos l + j \sin l) \,\mathrm{d}l.$$

In particular for the helix $l = \sqrt{a_1^2 + c_1^2} s$, and the integration can be effected.

(6.) The vectors a, β , and γ may be expressed in terms of the deriveds of ρ either directly or by aid of (v) and (vi) in the forms

$$a = \mathbf{D}_{s}\rho; \ \beta = c_{1}^{-1}\mathbf{D}_{s}^{2}\rho; \ \gamma = a_{1}^{-1}\mathbf{D}_{s}(c_{1}^{-1}\mathbf{D}_{s}^{2}\rho) + a_{1}^{-1}c_{1}\mathbf{D}_{s}\rho; \qquad (\mathbf{x}^{1}\mathbf{i}\mathbf{i}\mathbf{i})$$

and by differentiating the expression for γ we find a differential equation of the fourth order

$$D_{s}(a_{1}^{-1}D_{s}(c_{1}^{-1}D_{s}^{2}\rho) + a_{1}^{-1}c_{1}D_{s}\rho) + a_{1}c_{1}^{-1}D_{s}^{2}\rho = 0.$$
 (xiv)

This can be integrated in certain cases.

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(7.) If the curve lies upon the sphere

$$\Gamma\left(\rho-\sigma\right)=R,\tag{xv}$$

successive differentiations with respect to s afford the equations

$$Sa(\rho - \sigma) = 0; \ S\beta(\rho - \sigma) = \frac{1}{c_1}; \ S\gamma(\rho - \sigma) = \frac{1}{a_1}\frac{d}{ds}\left(\frac{1}{c_1}\right) = \frac{d}{da}\left(\frac{1}{c_1}\right). \quad (xvi)$$

Hence

$$\sigma = \rho + \beta \frac{1}{c_1} + \gamma \frac{d}{da} \left(\frac{1}{c_1} \right) \text{ and } R^2 = \frac{1}{c_1^2} + \left(\frac{d}{da} \frac{1}{c_1} \right)^2, \quad (xvii)$$

and these equations in general determine the osculating sphere. If the curve is spherical so that σ and R are constant differentiation of either of the equations (xvii), or of the third of (xvi) gives

$$E = \frac{d^2}{da^2} \frac{1}{c_1} + \frac{1}{c_1} = 0; \text{ hence } \frac{1}{c_1} = R \cos(a - a_0), \quad (xviii)$$

 a_0 being a constant of integration.

(8.) In the general case, instead of (xviii) differentiation of (xvii) shows that

$$d\sigma = \gamma E da$$
; $R dR = E d \frac{1}{c_1}$, (xix)

so if dotted letters refer to the locus of centres of spherical curvature, we may write

$$d\sigma = a'ds'$$
 and $a' = \gamma$ if $ds' = + Eda$. (xx)

Having selected a sign (we must have $a' = \pm \gamma$) we differentiate again by the formulæ (iv) and

$$\beta' c_1' \mathrm{d} s' = -\beta a_1 \mathrm{d} s. \tag{xxi}$$

Here again there is a latitude in the choice of sign, but if we select

$$\beta' = -\beta$$
, then $c_1' = E^{-1}$; $dc' = da$, or $c' = a$; (xxii)

if the angles c' and a are measured from corresponding initial points.

Since $\alpha'\beta' = -\gamma\beta$, it follows of necessity that

$$\gamma' = a$$
, whence $-\beta' a'_1 ds' = \beta c_1 ds$ and $a'_1 = c_1 a_1^{-1} E^{-1}$ and $a' = c$. (xxiii)

Finally we may remark that as the moving point travels with unit velocity along the curve, the centre of spherical curvature travels with the velocity Ea_1 and at right angles to the osculating plane; moreover the angular velocities of the two systems have the same direction but that of the derived system is $(Ea_1)^{-1}$ times that of the original.

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(9.) To determine the sign of E geometrically, we must calculate the deviation from the osculating sphere. This may be readily done by assuming it to be

$$\frac{1}{\lfloor \frac{4}{2}} s^4 x \ (\rho - \sigma),$$

or by expressing that the curve

$$\rho - \frac{1}{\lfloor \frac{4}{2}} s^4 x \ (\rho - \sigma)$$

passes through five consecutive points on the sphere. The result is

$$x = a_1^2 c_1 R^{-2} E. \tag{xxiv}$$

(10.) On the other hand, given the locus of centres, the relation between its arc ds' and that of the sought curve ds affords the differential equation

$$\frac{ds'}{dc'} = \frac{1}{c_1} + \frac{d^2}{dc'^2} \frac{1}{c_1};$$
 (xxv)

and the solution is

$$\frac{1}{e_1} = \sin e' \int \frac{\mathrm{d}s'}{\mathrm{d}c'} \cos e' \mathrm{d}e' - \cos e' \int \frac{\mathrm{d}s'}{\mathrm{d}e'} \sin e' \mathrm{d}e', \qquad (\mathrm{xxvi})$$

arbitrary constants of integration being understood. Hence if e1-1 is any particular integral and x and y constants of integration,

$$\rho = \sigma + \beta' \left(\frac{1}{c_1} + x \cos c' + y \sin c' \right) - \alpha' \frac{\mathrm{d}}{\mathrm{d}c'} \left(\frac{1}{c_1} + x \cos c' + y \sin c' \right) \cdot \quad (\mathbf{xxvii})$$

All these curves have of course corresponding elements parallel. The ratio of the element of the arc of the curve x, y to that for which x and y are zero is

$$1 + c_1 (x \cos c' + y \sin c'). \qquad (xxviii)$$

(11.) We may inquire under what conditions the unit vectors at corresponding points on two curves can remain constantly inclined to one another. This condition, of course, is satisfied by the curves of the last Section.

Assuming

$$a' = la + m\beta + n\gamma, \qquad (xxix)$$

where l, m, and n are constant, we find on differentiation

$$\beta'c'_{1}ds' = -amc_{1}ds + \beta(lc_{1} - na_{1})ds + \gamma ma_{1}ds. \qquad (xxx)$$

If this vector is constantly inclined to a, β, γ we must have either the ratio $a_1: c_1$ constant, or m = 0 and ln = 0. The conditions in (8.) are m = l = 0. For m = n = 0corresponding elements of the curves are parallel. In every other case both curves must be geodesics on cylinders (5.).

X.]

(12.) For the emanating lines and emanant surfaces generated by them, two different notations suggest themselves. One is already given (ii), and the motion of the line is referred to the moving system. In the second notation we may suppose the line at any instant to be twisting about a certain screw (396, (10.)) of pitch p with an angular velocity θ . This vector θ is, of course, at right angles to the unit vector η , and we have (compare (ii))

$$D_s \eta = \theta \eta = \frac{d\eta}{ds} + V \omega \eta. \qquad (xxxi)$$

The shortest distance between neighbouring positions of the emanant is obviously $p\theta ds$, and for neighbouring positions we have

$$\rho + t_0 \eta + p\theta ds = \rho + D\rho + (t_0 + x ds) (\eta + D\eta), \qquad (xxxii)$$

in which $\varpi = \rho + t\eta$ is the equation of the emanant line in one position, t_0 the value of t for the point of closest approach to the next position, and x some scalar. Replacing $D\rho$ by ads and $D\eta$ by $\theta\eta ds$, and retaining only terms of the first order, (xxxii) reduces to

 $p = Sa\theta^{-1}; \quad t_0 = Sa\eta\theta^{-1}; \quad x = Sa\eta.$

$$p\theta = a + t_0\theta\eta + x\eta. \qquad (xxxiii)$$

From this,

The line of striction of the surface is the curve whose equation is

$$\boldsymbol{\varpi} = \rho + t_0 \eta = \rho + \eta \mathbf{S} a \eta \theta^{-1} = \rho - \eta \mathbf{S} a (\mathbf{D}_s \eta)^{-1}, \qquad (\mathbf{x} \mathbf{x} \mathbf{v})$$

or it is the locus of points of closest approach of consecutive generators.

The scalar p is called the *parameter of distribution*, and is usually defined as the ratio borne by the distance between two close generators to the angle between them. It vanishes for a developable.

(13.) When s and t both vary in the equation

$$\varpi = \rho + t\eta \qquad (xxxvi)$$

the element of any arc on the surface is

$$\mathbf{D}\boldsymbol{\varpi} = (\mathbf{a} + t\theta\eta)\,\mathrm{d}\boldsymbol{s} + \eta\mathrm{d}\boldsymbol{t} = (p\theta + (t - t_0)\,\theta\eta - x\eta)\,\mathrm{d}\boldsymbol{s} + \eta\mathrm{d}\boldsymbol{t} \quad (\mathbf{x}\mathbf{x}\mathbf{x}\mathbf{v}\mathbf{i}\mathbf{i})$$

by (xxxiii); and the normal vector is, consequently,

$$\nu = \operatorname{Va}\eta - t\theta = \theta \left(p\eta + t_0 - t \right) = \left(t_0 - t - p\eta \right) \theta. \qquad (\mathbf{xxxviii})$$

The anharmonic of four normals at points on a common generator is

$$\frac{\nu_1 - \nu_2}{\nu_2 - \nu_3} \cdot \frac{\nu_3 - \nu_4}{\nu_4 - \nu_1} = \frac{t_1 - t_2}{t_2 - t_3} \cdot \frac{t_3 - t_4}{t_4 - t_1}; \qquad (xxxix)$$

and in this equation, which expresses that the anharmonic of the vectors is the anharmonic of the points on the generator, we may replace the vectors ν by any linear and distributive function of them, for instance, by $S\nu(\varpi - \rho)$. Thus, the ratio is also the anharmonic of the four tangent planes.

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If we express that two of these normals are perpendicular, by (xxxviii) the condition reduces to

$$S(p\eta + t_0 - t)(t_0 - t' - p\eta) = 0$$
, or $(t - t_0)(t' - t_0) + p^2 = 0$. (x1)

The corresponding points form a system in involution having its centre on the line of striction and having imaginary foci. Moreover, as

$$\mathbf{U}\frac{\mathbf{v}}{\mathbf{v}_0} = \mathbf{U}\frac{\boldsymbol{\theta}(p\boldsymbol{\eta} + t_0 - t)}{\boldsymbol{\theta}p\boldsymbol{\eta}} = \mathbf{U}\frac{p\boldsymbol{\eta} + t - t_0}{p\boldsymbol{\eta}} = \mathbf{U}\left(1 + \frac{t_0 - t}{p}\boldsymbol{\eta}\right), \qquad (\text{xli})$$

the tangent of the angle A between the tangent plane at t and that at t_0 is

$$\tan A = \frac{t_0 - t}{p} \,. \tag{xlii}$$

It may be proved that the measure of curvature, or the product of the principal curvatures K_1 and K_2 , can be expressed by the very simple equation

$$K_1 K_2 = -\frac{p^2}{(p^2 + (t - t_0)^2)^2} = -\frac{\cos^4 A}{p^2}, \qquad (xliii)$$

but we cannot delay on this.*

(14.) We can obtain a more explicit form of the condition

$$p = 0$$
, or $Sa\theta = 0$, or $Sa\eta D_s\eta = 0$,

that the emanant surface should be a developable by assuming

$$\eta = a \cos l + \beta \sin l \cos m + \gamma \sin l \sin m, \qquad (xliv)$$

and substituting in the third form of the condition. This gives

$$\sin l \,\mathrm{d} \,(a+m) - \cos l \,\sin m \,\mathrm{d} c = 0, \quad \mathrm{or} \quad \sin l = 0. \tag{xlv}$$

Hence, the only developables generated in the plane of a and γ $(m = \frac{1}{2}\pi)$ are the tangent line developable (l = 0), and the rectifying developable $(\cot l = \tan H)$. No line except a in the plane of a and β can generate a developable. Any line whatever in the plane of β and γ is capable of generating a developable provided d(m + a) = 0, or $m = a_0 - a$, a_0 being a constant.

We thus obtain the system of developables

$$\varpi = \rho + t \left(\beta \cos\left(a - a_0\right) - \gamma \sin\left(a - a_0\right)\right), \qquad (\text{xlvi})$$

whose cuspidal edges are

$$\varpi = \rho + \frac{\beta}{c_1} - \frac{\gamma}{c_1} \tan (a - a_0). \qquad (\text{xlvii})$$

* Compare the Note immediately following (section (12.)), p. 416.

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These curves all lie on the polar developable generated by the normal planes to the curve, and they are the evolutes of the curve.

Again, by (xlv), except for a geodesic on a cylinder, no developable can be generated by a line fixed relatively to a, β , γ , except the tangent-line developable.

In general, it may be shown that the cuspidal edge of any developable is determined by

$$t_0 = \frac{\sin l}{l_1 + c_1 \cos m}.$$
 (xlviii)

Also, if the line of striction of any emanant surface coincides with the original eurve, $S\alpha D_s \eta = 0$ gives

 $dl + \cos m \, dc = 0, \quad \text{or} \quad \sin l = 0, \tag{xlix}$

and, in this case, the pitch of the surface is

$$p = -\frac{\sin l}{c_1 \cos l \sin m - (a_1 + m_1) \sin l}.$$
 (1)

XI.—ON THE KINEMATICAL TREATMENT OF SURFACES.

(1.) For the kinematical treatment of surfaces we may conceive two systems of eurves, determined by two parameters u and v, to be traced upon any surface so that the eurves of one system are orthogonal to those of the other. At any point on the surface, let a be a unit vector tangent to the eurve u variable, and β tangent to the eurve v variable. Then $a\beta = \gamma$ is a unit vector normal to the surface. These three vectors may be supposed connected with three fixed vectors i, j, and k by the equations

$$a = qiq^{-1}, \quad \beta = qjq^{-1}, \quad \gamma = qkq^{-1}, \quad (i)$$

where q is a quaternion function of u and v.

Generally (compare Note IX., Sections 7 and 12, pages 399 and 403)

if
$$\xi = q\eta q^{-1}$$
, then $d\xi = q(d\eta + Vd\iota\eta)q^{-1}$, where $d\iota = 2Vq^{-1}dq$. (ii)

And, in particular, if η is invariably connected with *i*, *j*, and *k*, the relation is simplified into $d\xi = qV d\iota \eta q^{-1}$ because $d\eta = 0$. We shall use the notation

$$du = ida + jdb + kdc = (ia_1 + jb_1 + kc_1)du + (ia_2 + jb_2 + kc_2)dv,$$
(iii)

but it must be observed that da is not the differential of a scalar function (a) of u and v, because $d\iota$ is not the differential of a vector. In this notation we find at once, by (i) and (iii),

$$da = \beta dc - \gamma db, \quad d\beta = \gamma da - a dc, \quad d\gamma = a db - \beta da.$$
 (iv)

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(2.) Now, if ρ is the vector to a point on the surface,

$$\mathrm{d}\boldsymbol{\rho} = \boldsymbol{a} A \mathrm{d}\boldsymbol{u} + \boldsymbol{\beta} \boldsymbol{B} \mathrm{d}\boldsymbol{v},\tag{v}$$

where A and B are functions of u and v, and the square of the linear element is

$$\mathrm{d}s^2 = \mathrm{Td}\rho^2 = A^2\mathrm{d}u^2 + B^2\mathrm{d}v^2 \tag{vi}$$

and elements of the orthogonal curves are Adu and Bdv, respectively.

We shall also write generally

$$d\rho = (a \cos l + \beta \sin l)ds, \qquad (vii)$$

l being the angle any curve on the surface makes with the curve *u* variable.

(3.) We shall now show that the eight scalar functions of u and v, A, B, a_1 , b_1 , c_1 , a_2 , b_2 , and c_2 are not all independent. Since ρ is a function of u and v, the condition

$$\frac{\partial^2 \rho}{\partial v \partial u} = \frac{\partial}{\partial v} (Aa) = \frac{\partial}{\partial u} (B\beta) = \frac{\partial^2 \rho}{\partial u \partial v}$$
(viii)

must be satisfied. By (iv) this becomes

$$a \frac{\partial A}{\partial v} + (\beta c_2 - \gamma b_2) A = \beta \frac{\partial B}{\partial u} + (\gamma a_1 - a c_1) B,$$

so the scalars are connected by the equations

$$\frac{\partial A}{\partial v} = -c_1 B; \quad \frac{\partial B}{\partial u} = c_2 A; \quad a_1 B + b_2 A = 0.$$
 (ix)

Moreover, we can show that

$$\frac{\partial \iota_1}{\partial v} - \frac{\partial \iota_2}{\partial u} = V \iota_1 \iota_2. \tag{X}$$

For remembering that $dq^{-1} = -q^{-1}dqq^{-1}$, we have

$$\frac{\partial \iota_1}{\partial v} = 2 \frac{\partial}{\partial v} \operatorname{V} q^{-1} \frac{\partial q}{\partial u} = 2 \operatorname{V} q^{-1} \frac{\partial^2 q}{\partial v \partial u} - 2 \operatorname{V} q^{-1} \frac{\partial q}{\partial v} q^{-1} \frac{\partial q}{\partial u}$$

and

$$\frac{\partial \iota_2}{\partial u} = 2 \frac{\partial}{\partial u} \nabla q^{-1} \frac{\partial q}{\partial v} = 2 \nabla q^{-1} \frac{\partial^2 q}{\partial u \partial v} - 2 \nabla q^{-1} \frac{\partial q}{\partial u} q^{-1} \frac{\partial q}{\partial v};$$

remembering also that q is a function of u and v (1.) so that the term involving the second differential of q cancels on subtraction, and bearing in mind that $pq - qp = 2V \cdot VpVq$, if p and q are any two quaternions, there is no difficulty in establishing equation (x).

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Hence we obtain three additional equations equivalent to (\mathbf{x}) ,

$$\frac{\partial a_1}{\partial v} - \frac{\partial a_2}{\partial u} = b_1 c_2 - b_2 c_1; \quad \frac{\partial b_1}{\partial v} - \frac{\partial b_2}{\partial u} = c_1 a_2 - c_2 a_1; \quad \frac{\partial c_1}{\partial v} - \frac{\partial c_2}{\partial u} = a_1 b_2 - a_2 b_1. \quad (xi)$$

The same equations (xi) would have been found, though somewhat less simply, had we employed this other vector $d\omega = 2Vdqq^{-1} = qd\iota q^{-1}$.

The vectors ω_1 and ω_2 , analogous to ι_1 and ι_2 , satisfy

$$\frac{\partial \omega_1}{\partial v} - \frac{\partial \omega_2}{\partial u} = - \nabla \omega_1 \omega_2.$$

(4.) If R is a principal radius of curvature the usual equation

$$\mathrm{d}\boldsymbol{\rho} + R \,\mathrm{d}\mathrm{U}\boldsymbol{\nu} = 0$$

becomes in this notation

$$aAdu + \beta Bdv + R(adb - \beta da) = 0, \qquad (xii)$$

which affords the two scalar equations

$$(A + Rb_1) du + Rb_2 dv = 0, \quad Ra_1 du - (B - Ra_2) dv = 0.$$
 (xiii)

From these, on elimination of the ratio du: dv, we obtain the quadratic

$$R^{2}(a_{1}b_{2} - a_{2}b_{1}) + R(b_{1}B - a_{2}A) + AB = 0, \qquad (xiv)$$

whose roots are the principal radii. This equation may be modified by (ix) and (xi) so as to exhibit Gauss's remarkable theorem on the measure of curvature. In fact

$$R_{1}^{-1}R_{2}^{-1} = \mathcal{A}^{-1}B^{-1}(a_{1}b_{2} - a_{2}b_{1}) = \mathcal{A}^{-1}B^{-1}\left(\frac{\partial c_{1}}{\partial v} - \frac{\partial c_{2}}{\partial u}\right) \text{ by } (\mathbf{x}i);$$

and by (ix) this reduces to

$$R_1^{-1}R_2^{-1} = -A^{-1}B^{-1}\left(\frac{\partial}{\partial v}\left(B^{-1}\frac{\partial A}{\partial v}\right) + \frac{\partial}{\partial u}\left(A^{-1}\frac{\partial B}{\partial u}\right)\right). \tag{xv}$$

The measure of curvature thus depends solely on the linear element (vi), and is unaltered when the surface is bent or twisted in any manner without altering the length of any arc.

(5.) Eliminating R from (xiii), the directions of the lines of curvature are given by

$$A \mathrm{d} u \mathrm{d} a + B \mathrm{d} v \mathrm{d} b = 0 \quad \text{or} \quad A a_1 \mathrm{d} u^2 + (A a_2 + B b_1) \mathrm{d} u \mathrm{d} v + B b_2 \mathrm{d} v^2 = 0. \quad (\mathrm{xvi})$$

Hence, by (ix), we can see that the lines of curvature cut at right angles, and if we take these lines for the orthogonal systems (1.), we must have

whence by (xiii)
$$a_{1} = 0, \qquad b_{2} = 0, \qquad (XV11)$$
$$b_{1} = -AR_{1}^{-1}, \quad a_{2} = BR_{2}^{-1},$$

or more conveniently, if K_1 and K_2 are the principal curvatures by (vii)

$$da = BK_2 dv = K_2 \sin l ds, \quad db = -AK_1 du = -K_1 \cos l ds. \quad (xviii)$$

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The relations (ix) and (xi) are equivalent to

$$c_1 = -\frac{1}{B}\frac{\partial A}{\partial v}; \quad c_2 = \frac{1}{A}\frac{\partial B}{\partial u}; \quad \frac{\partial K_2}{\partial u} = \frac{K_1 - K_2}{B}\frac{\partial B}{\partial u}; \quad \frac{\partial K_1}{\partial v} = \frac{K_2 - K_1}{A}\frac{\partial A}{\partial v}; \quad (xix)$$

together with (xv).

(6.) For any curve on the surface by (v) and (vii) a unit tangent vector is

$$\rho' = \mathbf{U} \left(a A \mathrm{d} u + \beta B \mathrm{d} v \right) = a \cos l + \beta \sin l, \qquad (\mathbf{x}\mathbf{x})$$

the accent denoting, as usual, that the vector ρ has been differentiated with respect to the arc s.

Taking the differential of the second of these expressions by (iv)

$$\mathrm{d}\rho' = \rho''\mathrm{d}s = (\beta\mathrm{d}c - \gamma\mathrm{d}b)\cos l + (\gamma\mathrm{d}a - a\mathrm{d}c)\sin l + (-a\sin l + \beta\cos l)\,\mathrm{d}l,$$

or more simply

 $\rho'' ds = \gamma \rho' (de + dl) + \gamma (\sin l da - \cos l db).$ (xxi)

From this equation may be deduced all the properties of a curve traced upon the surface depending on differentials of the second order.

(7.) The projection of the vector of curvature (ρ'') on the normal to the surface (γ) , or the component of the curvature in the plane containing the normal to the surface and the tangent to the curve is

$$K = \frac{\sin l da - \cos l db}{ds} = \frac{B dv da - A du db}{A^2 du^2 + B^2 dv^2}$$
$$= \sin l \left(\frac{a_1}{A} \cos l + \frac{a_2}{B} \sin l\right) - \cos l \left(\frac{b_1}{A} \cos l + \frac{b_2}{B} \sin l\right), \quad (xxii)$$

these transformations being effected by the relations

$$\cos l \mathrm{d}s = A \mathrm{d}u, \quad \sin l \mathrm{d}s = B \mathrm{d}v.$$

As K does not involve the differential of l, or the second differentials of u or v, it is the same for all curves having a common tangent and lying on the surface. In fact, K is the curvature of the normal section of the surface, and Meusnier's theorem is incidentally proved. Also Euler's theorem follows by (xviii) as we may write

$$\mathbf{K} = \mathbf{K}_1 \cos^2 l + \mathbf{K}_2 \sin^2 l, \qquad (\mathbf{x}\mathbf{x}\mathbf{i}\mathbf{i}\mathbf{i})$$

when we take the lines of curvatures as the curves of reference.

The curvatures of the normal sections through the curves of reference are $-\mathcal{A}^{-1}b_1$ and $B^{-1}a_2$.

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(8.) The component of the curvature in the tangent plane is, in like manner,

$$\mathbf{K}' = (\mathrm{d}c + \mathrm{d}l) \,\mathrm{d}s^{-1}. \tag{xxiv}$$

This is the geodesic curvature of the curve. It vanishes if the eurve is a geodesic; and in this case the curve projects into a curve in the tangent plane inflexionally touching the tangent. Hence

$$dc + dl = 0$$
, or $\frac{\partial A}{\partial v} \frac{du}{B} - \frac{\partial B}{\partial u} \frac{dv}{A} - d \tan^{-1} \frac{Bdv}{Adu} = 0$ (XXV)

is the equation of a geodesic, the transformation being made by the aid of (ix). As this equation involves only A and B, the coefficients of the line element (vi), geodesics remain geodesics when the surface is deformed without stretching. This, of course, is otherwise obvious.

The geodesic curvatures of the curves of reference are $A^{-1}c_1$ and $B^{-1}c_2$.

(9.) Instead of proceeding directly to a third differentiation, it is simpler to modify the results already obtained by writing in accordance with the notation used in the kinematical treatment of curves (Note X., page 404),

$$\rho' = \alpha', \ \rho'' = \beta'c'_1, \ \text{and} \ d\beta' = (\gamma'a'_1 - \alpha'c'_1) ds,$$

and also by introducing a new angle m suggested by (xxi), and defined by the equations

 $c'_1 \cos m \, \mathrm{d}s = \mathrm{d}c + \mathrm{d}l, \quad c'_1 \sin m \, \mathrm{d}s = \sin l \, \mathrm{d}a - \cos l \, \mathrm{d}b. \tag{xxvi}$

In this notation, the relation (xxi) affords

$$\beta' = \gamma a' \cos m + \gamma \sin m$$
 and $\gamma' = \gamma \cos m - \gamma a' \sin m$; (xxvii)

$$\gamma = \beta' \sin m + \gamma' \cos m, \quad \gamma \alpha' = \beta' \cos m - \gamma' \sin m.$$
 (XXVIII)

We may observe that m is zero for an asymptotic curve and a right angle for a geodesic. It is, in general, the angle between the normal to the surface, and the binormal to the curve.

Thus prepared, when we differentiate γ expressed in terms of m, β' , and γ' by (xxviii), we have

$$adb - \beta da = (\beta' \cos m - \gamma' \sin m) (dm - a'_{1}ds) - a'c'_{1} \sin m ds. \quad (xxix)$$

From this we recover the second of (xxvi), as well as the new equation,

$$da' - dm = \cos l \, da + \sin l \, db. \tag{xxx}$$

This equation may be reduced to

$$da' - dm = (K_2 - K_1) \sin l \cos l \, ds, \qquad (xxxi)$$

when, without loss of generality, we take the lines of curvature as the systems of reference (xviii).

whence,

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(10.) Thus the difference between the torsion of a curve traced upon a surface, and the rate at which the angle between its osculating plane and the tangent plane varies, is equal to half the difference of the principal curvatures multiplied by the sine of double the angle between the curve and a line of curvature. This theorem has many consequences. In the first place da' - dm is the same for all curves having a common tangent; it vanishes for a line of curvature; when a surface is cut by a plane, the rate of the variation of the angle between the plane and the tangent plane at any point of the section equals half the difference of the curvatures at the point multiplied by the sine of twice the angle between the trace and a line of curvature; when a line of curvature is plane, the surface cuts the plane at a constant angle; and when a surface cuts a plane at a constant angle, the intersection is a line of curvature or the surface is a sphere; the torsion of a geodesic is

$$(\mathbf{K}_2 - \mathbf{K}_1) \sin l \cos l;$$

and this has been called the geodesic torsion by M. O. Bonnet, to whom the important and elegant relation (xxxi) is due.*

Also for the intersection of two surfaces,

$$(\mathbf{K}_2 - \mathbf{K}_1) \sin l \cos l - (\mathbf{K}'_2 - \mathbf{K}'_1) \sin l' \cos l' = \frac{\mathrm{d}M}{\mathrm{d}s} \qquad (\mathrm{xxxii})$$

gives the rate of change of the angle at which the surfaces cut. Hence, if two surfaces cut at a constant angle along a line of curvature on one, the intersection is also a line of curvature on the other.

It is well to remark that we have now exhausted all the relations which are not obtainable by direct differentiation from those already found. We have seen (Note X.) that all the affections of a curve can be expressed in terms of the unit vector $\mathbf{a}', \beta', \gamma'$ of the curve, and in terms of the curvature and torsion and their deriveds. But we have found the curvature and the torsion, and have expressed $\mathbf{a}', \beta', \gamma'$ in terms of $\mathbf{a}, \beta, \gamma, l$, and m.

(11.) If we take the curves u variable to be geodesics, we have by $(xxv) c_1 = 0$. Hence by (ix) A is a function of u. Changing the variable u to $\int A du$, the new variable is simply the arc of the geodesics. Then A becomes unity, equation (xv) reduces to

$$K_1 K_2 = -\frac{1}{B} \frac{\partial^2 B}{\partial u^2}, \qquad (xxxiii)$$

and the geodesic curvature of any curve (xxiv) is

$$\mathbf{K}' = \frac{\sin l}{B} \frac{\partial B}{\partial u} + \frac{\partial l}{\partial s}, \quad \text{because } c_2 = \frac{\partial B}{\partial u}, \quad \mathrm{d}v = \frac{\sin l \mathrm{d}s}{B}. \quad (xxxiv)$$

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^{*} Compare Darboux, loc. cit., Art. 505.

Hence the total eurvature of any portion of the surface is

$$\iint \mathbf{K}_1 \mathbf{K}_2 \mathrm{d}S = -\iint \frac{\partial^2 B}{\partial u^2} \,\mathrm{d}u \mathrm{d}v = -\int \frac{\partial B}{\partial u} \,\mathrm{d}v = \int \left(\frac{\partial l}{\partial s} - \mathbf{K}'\right) \,\mathrm{d}s, \qquad (\mathbf{x}\mathbf{x}\mathbf{v})$$

the single integrals being taken over the bounding curve, using Stokes's theorem in the transformation.

If the bounding curve is made up of geodesics, K' is zero; and the integral is 2π minus the sum of the angles through which the direction of a point travelling round the boundary suddenly turns at the points of intersection of the bounding geodesics.

We may also notice the relation

$$K_1 K_2 = -\frac{\partial K'_2}{\partial u} - K'_2^2, \qquad (xxxvi)$$

where K'_2 is the geodesic curvature of the orthogonal curve v variable.

(12.) For ruled surfaces, when we take the generators to be the curves *u* variable, a is independent of u, and $b_1 = c_1 = 0$. The conditions (ix) and (xi) reduce to

$$\frac{\partial B}{\partial u} = c_2; \quad a_1 B + b_2 = 0; \quad \frac{\partial a_1}{\partial v} - \frac{\partial a_2}{\partial u} = 0; \quad \frac{\partial b_2}{\partial u} = c_2 a_1; \quad \frac{\partial c_2}{\partial u} = -a_1 b_2. \quad (xxxvii)$$

These give on combination if $G = (-K_1K_2)^{\frac{1}{2}}$ (compare (xxxiii))

$$c_2 = \frac{\partial B}{\partial u}; \quad a_1 = G; \quad b_2 = -BG; \quad \frac{\partial a_2}{\partial u} = \frac{\partial G}{\partial v}; \quad \frac{\partial}{\partial u} (B^2G) = 0.$$
 (xxxviii)

The last of these expresses that B^2 is quadratic in u. Hence a_1 , b_2 , and c_2 are unchanged when the surface is deformed without stretching.

The second equation shows how to find the measure of curvature of a ruled surface in an excessively simple manner. By (iv)

$$a_1 = \mathbf{S}\boldsymbol{\beta} \, \frac{\partial \boldsymbol{\gamma}}{\partial u} = \mathbf{S} \boldsymbol{\gamma} \mathbf{a} \, \frac{\partial \boldsymbol{\gamma}}{\partial u},$$

so if a is the direction of a generator, and ν the normal vector at any point

$$G = \mathbf{S} \alpha \nu^{-1} \frac{\partial \nu}{\partial \mu} = (-\mathbf{K}_1 \mathbf{K}_2)^{\frac{1}{2}}. \qquad (\mathbf{x} \mathbf{x} \mathbf{x} \mathbf{x})$$

Or if $\rho = \phi + ta$ is the surface (compare Note X., (xxxiv), (xxxviii), and (xliii)),

$$G = \frac{Saa'\phi'}{Va(\phi' + ta')^2} = \frac{-p}{p^2 + (t - t_0)^2},$$
 (x1)

where t_0 corresponds to the point on the line of striction.

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(13.) We may also modify (xxxvii) of the Note just cited by replacing η , θ , s, and ϖ by a, aa', v, and ρ , respectively, when we obtain

$$\mathbf{D}\boldsymbol{\rho} = (p\boldsymbol{a} + (t - t_0)) \, \boldsymbol{a}' \, \mathrm{d}\boldsymbol{v} + \boldsymbol{a} \, (\mathrm{d}\boldsymbol{t} - x \mathrm{d}\boldsymbol{v}). \tag{xli}$$

If we now take as a new variable

$$du = dt - xdv$$
, or $u = t - \int S\phi' a \, dv$, (xlii)

we find from (xli)

 $\mathbf{D}\rho = (pa + (u - u_0))a' dv + adu; \quad \mathbf{T}\mathbf{D}\rho^2 = \mathbf{T} \cdot (pa + u - u_0)^2 a'^2 dv^2 + du^2. \quad (xliii)$ Thus for a ruled surface

$$B = Ta'T(pa + u - u_0), \qquad (xliv)$$

and in particular for a developable $B = \text{Ta}'(u - u_0)$. Obviously Ta' is the angular velocity of the generator if v is taken to be the time. It is also for the developable the curvature of the cuspidal edge if v is the arc of that edge.

For a developable γ does not vary with u, hence $a_1 = 0$ and all the scalars vanish except c_2 and a_2 , the curvature and torsion of the cuspidal edge when v is its arc.

(14.) In the last section the change of variable is introduced artificially. To determine the orthogonal system directly for the surface

$$\rho = \phi + ta, \quad \mathrm{T}a = 1, \quad (\mathrm{xlv})$$

assume t = f(v) + u where f is some function of v. The direction of the tangent to the curve $\rho = \phi + af$ is $d\rho = (\phi' + a'f + af') dv$ and this is at right angles to a if

$$\operatorname{Sa}\phi' - f' = 0$$
 so $f = \int \operatorname{Sa}\phi' dv = \int \operatorname{Sa}d\phi$. (xlvi)

Thus the orthogonal system is found.

In like manner to determine the system of curves orthogonal to the system v constant on the surface

$$\rho = \phi(t, v), \qquad (xlvii)$$

assume t = f(u, v) and we see that f must be a solution of the differential equation of the first order

$$\frac{\partial f}{\partial v} + S \frac{\partial \phi}{\partial v} \left(\frac{\partial \phi}{\partial f} \right)^{-1} = 0.$$
 (xlviii)

XII.—SYSTEMS OF RAYS.

(1.) If the vector β is a given function of a variable vector a the equation

$$a = \beta + ta \tag{i}$$

represents a regulus, a congruency or a complex of lines according as one, two or three scalar variables are involved in the constitution of α , or in other words according as the vectors α when coinitial terminate upon a curve or upon a surface or are wholly arbitrary.

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A regulus of lines composes a ruled surface. We shall not consider those surfaces here as they have been dealt with in another note.*

For a congruency the simplest form of equation (i) appears to be that in which the vectors a are of constant length. They may then be considered to involve two angular parameters, and the most general congruency can be represented by an equation of this kind.

(2.) In general we shall write

$$d\beta = \phi da = (\Phi + V\epsilon) da, \qquad (ii)$$

 ϕ being a linear vector function having Φ for its self-conjugate part and ϵ for its spin-vector. We shall also use the notation

$$d\omega = \nabla \frac{da}{a} = \frac{dUa}{Ua},$$
 (iii)

so that $d\omega$ is the rotation which applied to the ray represented by a renders it parallel to the ray represented by a + da.

(3.) The simplest mode from a kinematical point of view in which a ray of the complex can be displaced into the position of a neighbouring ray is to twist it about a certain screw. We shall however find it more convenient to suppose the displacement effected by a translation combined with a twist about a screw. If $d\tau$ is the translation, and p the pitch of the screw, the resultant translation is $d\tau + pd\omega$. Expressing that this translation applied to the ray (a) makes it intersect the ray (a + da) we have the equation

$$\beta + ta + d\tau + pd\omega = \beta + \phi da + (t + dx)(a + da), \qquad (iv)$$

where dx is some small scalar, and where t determines the point on the ray (a) brought to intersection with the ray (a + da).

(4.) Now, we notice that $d\omega$ depends only on the component of da at right angles to a. This suggests that we should consider separately the two components of da; so we write in general

$$da = V daa^{-1} \cdot a + S daa^{-1} \cdot a = d\omega \cdot a + dy \cdot a, \qquad (v)$$

where dy is the scalar Sdaa⁻¹. Hence neglecting the small term of the second order dxda the relation (iv) reduces to

$$d\tau + pd\omega = \phi (d\omega a) + td\omega a + dy\phi a + (dx + tdy) a.$$
(vi)

* Note X., sections (12.) and (13.), page 408.

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We are at liberty to select $d\tau$ in any way we please. The simplest selection is

$$d\tau = a^{-1} V a \phi a dy, \qquad (vii)$$

and then (vi) reduces to

$$(p + ta) d\omega = a^{-1} Va\phi (d\omega a),$$
 (viii)

because

$$\mathrm{d}x + (t + \mathrm{S}a^{-1}\phi a)\,\mathrm{d}y + \mathrm{S}a^{-1}\phi(\mathrm{d}\omega a) = 0,$$

by (vi) when $d\tau$ is at right angles to a (vii).

(5.) A slight knowledge of the properties of the cylindroid will now give us the key to an extensive view of the arrangement of the rays of a complex or congruency in the neighbourhood of a given ray. Equation (viii) may be regarded as determining a two-system of screws, for $d\omega$ (= $Vdaa^{-1}$) can be resolved into two components having fixed directions normal to a and dy has completely disappeared from this equation. We commence then by twisting the ray (a) about any screw of this system. The position it occupies after an infinitesimal twist is that of a ray of the congruency determined by the condition dy = 0 or dTa = 0. In this way by twisting the initial ray about all the screws of the cylindroid we obtain the whole assemblage of rays of the congruency in the neighbourhood.

The ray through any point on the cylindroid near the axis may be constructed by drawing a perpendicular to the generator of the cylindroid through that point inclined to the axis at a small angle whose circular measure is the quotient of the intercept on the generator by the pitch appropriate to that generator.

Now two screws of the system have in general zero pitch. Any small twist on any screw of the system may be resolved into rotations about the axes of these screws of zero pitch. When the initial ray receives a small rotation about one of these axes its point of intersection with the second describes a small arc of a circle normal to Ua and to the axis of rotation. A small rotation about the second axis will cause this point to deviate from the arc by a small distance of the second order of magnitudes. So to the first order all the rays of the congruency intersect two fixed lines both of which are at right angles to a and each intersects one axis of zero pitch and is at right angles to the other. In particular two rays intersect the initial ray. These have been rotated about one axis only. The axes of zero pitch are the focal lines and their points of intersection with the initial ray are the principal foci of that ray.

Again the point at which the initial ray is closest to a neighbour is called by Hamilton a *virtual focus*. We see that the closest points on the neighbours lie on the cylindroid generated by the shortest distances. Hence as the cylindroid is contained between two planes normal to the initial ray the virtual foci are limited to a certain range on that ray.*

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^{*} Trans. Roy. Ir. Acad. vol. xvi. p. 52.

(6.) We now turn to equation (vii) which shows that all the rays of a complex close to a given ray may be constructed by successively displacing the rays of a certain congruency by translations in a fixed direction normal to the initial ray and of varying but small amounts. Inasmuch as the rays of the congruency intersect two elements of right lines, the rays of the complex pass through two small parallelograms situated in parallel planes each having a pair of sides equal and parallel to the translation. All the rays are parallel which intersect a line in the plane of one parallelogram parallel to one of these sides.

(7.) To verify the conclusions of section (5.), and to calculate the positions of the various lines, we re-write equation (viii) in the form

$$(\phi + t) \cdot d\omega a = p d\omega + a dz$$
 (ix)

whence

$$p = S \frac{\phi \cdot d\omega a}{d\omega}; \quad t = -S \frac{\phi \cdot d\omega a}{d\omega a}; \quad dz = S \frac{\phi \cdot d\omega a}{a}.$$
 (x)

At a principal focus two rays intersect and p is zero; therefore

$$d\omega a = (\phi + t)^{-1} a dz.$$
 (xi)

Operating on this equation by Sa we find

$$Sa(\phi + t)^{-1}a = 0, \qquad (xii)$$

which is equivalent to a quadratic in t whose roots determine the foci.

The extreme points are given by the analogous equation*

$$Sa (\Phi + t)^{-1}a = 0$$
 (xiii)

in which the self-conjugate part Φ replaces ϕ . For we see by (x) that t is the inverse square of a radius of the conic[†]

$$S\rho\Phi\rho = 1, Sa\rho = 0,$$
 (xiv)

and its greatest and least values are the inverse squares of the axes of the conic.

If the line $\rho = \beta + sa + y\tau$ (y variable) meets all the neighbouring rays

 $S (\phi \cdot d\omega a - sa) (a + d\omega a) \tau = 0$ Sd\u03c0 a (\u03c0' + s) \u03c0 \u03c0 a = 0 (xv)

terms of the second ord

when terms of the second order are rejected. If this is true for all vectors $d\omega a$ that is for all vectors at right angles to a, it is equivalent to

$$(\phi' + s) \operatorname{V} \tau a \parallel a \quad \text{or} \quad \operatorname{V} \tau a \parallel (\phi' + s)^{-1} a.$$
 (xvi)

or

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^{*} This equation and the last are given by Molenbroek, Anwendung der Quaternionen auf die Geometrie, pp. 236-238.

[†] Compare p. 253.

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Operating on this by Sa we see that $s = s_1$ one of the roots of (xii) and that the line passes through a principal focus. If $\tau = a^{-1} (\phi' + s_1)^{-1} a$ the conditions are satisfied and it is very easy to show that $a^{-1}(\phi + s_2)^{-1}a$, which (xi) is the axis of the second screw of zero pitch, is at right angles to τ .

(8.) We shall now invert the functions in (xii) and (xiii) and exhibit the relations connecting the roots of the two equations.

If for a moment we replace a by $\nabla \lambda \mu$ and $\phi + t$ by ϕ_t by Hamilton's fundamental theorem of inversion (xii) is equivalent to

$$SV\lambda\mu V\phi_t \lambda\phi_t \mu = SV\lambda\mu V (\Phi_t - V\epsilon)\lambda (\Phi_t - V\epsilon)\mu = 0. \quad (xvii)$$

A slight expansion shows that the part linear in ϵ disappears since Φ_i is self-conjugate (ii), while the part quadratic in ϵ is $-(S\epsilon V\lambda\mu)^2$.

(9.) We have therefore two forms for (xii)

 $t^{2}a^{2}+2t\operatorname{Sa}\left(m^{\prime\prime}-\phi\right)a+\operatorname{Sa}\psi a=0;\ t^{2}a^{2}+2t\operatorname{Sa}\left(m^{\prime\prime}-\Phi\right)a+\operatorname{Sa}\Psi a-(\operatorname{S}\epsilon a)^{2}=0;\ (\operatorname{xviii})$ and similarly two forms for (xiii)

$$t^{2}a^{2}+2t\operatorname{Sa}(m^{\prime\prime}-\Phi)a+\operatorname{Sa}\Psi a=0; \ t^{2}a^{2}+2t\operatorname{Sa}(m^{\prime\prime}-\phi)a+\operatorname{Sa}\Psi a+(\operatorname{Se}a)^{2}=0, \quad (\operatorname{xix})$$

remembering that by Hamilton's formula of inversion

$$\psi_{t} = m_{t}\phi_{t}^{-1} = \psi + t(m'' - \phi) + t^{2}$$

and that the first invariants (m') of a function (ϕ) and of its self-conjugate part (Φ) are the same.

Hence, if s_1 and s_2 are the roots of (xii) or (xviii), and t_1 and t_2 those of (xiii) or (xix) $2t_0 = s_1 + s_2 = t_1 + t_2 = SUa(m'' - \Phi)Ua = SUa(m'' - \phi)Ua$

and

$$t_{1}s_{2} = t_{1}t_{2} + (S\epsilon Ua)^{2} = -SUa\psi Ua; t_{1}t_{2} = s_{1}s_{2} - (S\epsilon Ua)^{2} = -SUa\Psi Ua.$$
 (xxi)

We may now write for the focal points and for the extreme points in accordance with $(\mathbf{x}\mathbf{x})$

$$s_1 = t_0 - f, \ s_2 = t_0 + f; \ t_1 = t_0 - e, \ t_2 = t_0 + e.$$
 (xxii)

Thus the four points are symmetrically situated with respect to the central point.

Again (xxi) affords the relation

$$e^2 - f^2 = (\mathbf{S} \boldsymbol{\epsilon} \mathbf{U} \boldsymbol{a})^2, \qquad (\mathbf{x} \mathbf{x} \mathbf{i} \mathbf{i} \mathbf{i})$$

which shows that the focal points are real if $e^2 > (S \in U\alpha)^2$. The extreme points are always real for t_1 and t_2 are the inverse squares of the axes of a conic (xiv) and these are real whether the conic is real or not. The reality of these points is also a geometrical consequence of section (5.).*

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^{*} The symmetrical arrangement of the four points, principal and extreme virtual foci, with respect to the central point is the only element in the arrangement of the rays which cannot be deduced from the properties of the cylindroid. This arrangement depends upon the distribution of pitch.

(10.) The directions *i* and *j* of the principal axes of the conic (xiv) afford a first natural system of lines of reference coupled with Ua = k. As we are now dealing only with a congruency we may suppose Ta = 1 without loss of generality and we may regard a = Ua = k

unless the contrary is stated.

These vectors obey the laws (compare again (xiv))

$$t_1 = \mathrm{S}i\phi i$$
; $t_2 = \mathrm{S}j\phi j$; $\mathrm{S}i\Phi j = 0$; $\mathrm{S}i\phi j = -\mathrm{S}j\phi i = -\mathrm{S}\epsilon k$. (xxiv)

If we introduce an angle u so that

$$\mathbf{U}\mathbf{d}\boldsymbol{\omega} = i\cos\,\boldsymbol{u} + j\,\sin\,\boldsymbol{u} \tag{xxv}$$

and a new scalar w the relation (ix) becomes

$$(\phi + t) (i \sin u - j \cos u) = p(i \cos u + j \sin u) + wk.$$
(xxvi)

Solving this for p and t by operating by SUd ω and SUd ωk we find on reference to (xxiv) and (xxii)

$$p = -\operatorname{S}\epsilon k + (t_2 - t_1)\sin u \cos u = p_0 + e \sin 2u \qquad (xxvii)$$

$$t = t_1 \sin^2 u + t_2 \cos^2 u = t_0 + e \cos 2u$$
 (xxviii)

where $p_0 = -S \epsilon k$ is the pitch corresponding to the extreme points $u = 0, \frac{\pi}{2}$.*

The focal points are given by

$$p_0 + e \sin 2u = 0 \qquad (xxix)$$

and are real if $e^2 > p_0^2$.

Again eliminating u from (xxvii) and (xxviii) we find t and p connected by

$$(t - t_0)^2 + (p - p_0)^2 = e^2 \text{ or } (t - t_1)(t - t_2) + (p - p_0)^2 = 0,$$
 (xxx)

which includes as a particular case

 $f^2 + p_0^2 = e^2.$

(11.) A second natural system of lines of reference is formed by Ua and the bisectors of the angles between *i* and *j*. Now the angle u = 0 at the point t_2 and $u = \frac{\pi}{2}$ at t_1 so if we take $v = u - \frac{\pi}{2}$ so that t_2 and t_1 correspond to $v = -\frac{\pi}{4}$ and $v = +\frac{\pi}{4}$, we have $p = p_0 + e \cos 2v$; $t = t_0 - e \sin 2v$. (xxxi)

If we take these three lines as Cartesian axes and put

$$\mathbf{z} = (t - t_0)$$
 and $\tan v = yx^{-1}$

the equation of the cylindroid follows from (xxxi) in its canonical form

$$\mathbf{z}(x^2 + y^2) = -2exy. \qquad (\mathbf{x}\mathbf{x}\mathbf{x}\mathbf{i}\mathbf{i})$$

 $r = r_1 (\cos w)^2 + r_2 (\sin w)^2$.

[•] Compare Hamilton, "Supplement to an Essay on the Theory of Systems of Rays," Trans. R.I.A. vol. xvi. p. 54, where (xxviii) is obtained in the form

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(12.) There is yet a third kind of focus which Hamilton calls^{*} a "focus by projection." The vector drawn from the point t on the initial ray perpendicular to it and terminating on a neighbouring ray is

$$\mathrm{d}\boldsymbol{\varpi} = a\mathrm{V}a^{-1}(\boldsymbol{\phi} + t)$$
. $\mathrm{d}\boldsymbol{\omega}a$ (xxxiii)

as may be verified without any trouble. If the perpendicular $d\pi'$ at the point t' terminating on the same near ray is at right angles to this the projection of the ray on the plane of α and $d\pi$ cuts the initial ray at the point t'. This point is a focus by projection.

(13.) To investigate the properties of this new class of foci we shall use the first natural system of lines of reference, the vectors i, j, k of section (10.). We shall also replace a by Ua or by k, and we shall write

$$d\varpi = (i \cos w + j \sin w) \operatorname{Td} \varpi, \qquad (xxxiv)$$

retaining the previous notation (xxv) for Ud ω .

The angle w is the angle between the plane upon which the projection is made (or briefly the plane of projection) and a plane of extreme virtual foci.

If then

$$P' \mathrm{Td}\omega = '\mathrm{Td}\varpi$$
 (xxxv)

equation (xxxiii) becomes

$$P(i\cos w + j\sin w) = k\nabla k(\phi + t) (j\cos u - i\sin u). \qquad (xxxvi)$$

Remembering the laws of the units (xxiv) and that $p_0 = Si\phi j = -Sj\phi i$, we find

$$P \cos w = p_0 \cos u + (t - t_1) \sin u = p_0 \cos u + (e + g) \sin u$$
,

$$P\sin w = p_0\sin u + (t_2 - t)\cos u = p_0\sin u + (e - g)\cos u, \quad (xxxvii)$$

the symbol e being given by (xxii), and the new symbol g being equal $t - t_0$.

If g' = g + h determines the focus by projection, namely the point at which w has increased by a right angle while u remains constant,

$$\tan u = \frac{p_0 \tan w - (e - g)}{p_0 - (e + g) \tan w} = -\frac{p_0 + (e - g - h) \tan w}{p_0 \tan w + (e + g + h)}, \qquad (xxxviii)$$

and solving for h in terms of w, we obtain the equivalent of Hamilton's remarkable formula[†] containing the law of the focus by projection (compare (xxx.))

$$\frac{1}{\hbar} = \frac{(e-g)\cos^2 w - (e+g)\sin^2 w}{g^2 - f^2}.$$
 (xxxix)

* Hamilton, Trans. R.I.A. vol. xvi. p. 47.

+ Hamilton's equation printed on p. 50, loc. cit., is

$$\frac{1}{p} = \frac{1}{p_1} (\cos \cdot \Pi)^2 + \frac{1}{p_2} (\sin \cdot \Pi)^2.$$

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From this we see that the foci by projection are excluded from a finite portion of the line contained within the extreme points of projection determined by

$$h_1 = -\frac{g^2 - f^2}{e + g}, \ h_2 = \frac{g^2 - f^2}{e - g} \text{ or by } g_1 = \frac{ge + f^2}{e + g}, \ g_2 = \frac{eg - f^2}{e - g};$$
 (x1)

while

$$h_0 = g \frac{g^2 - f^2}{e^2 - g^2}$$
 or $g_0 = g \frac{e^2 - f^2}{e^2 - g^2}$ and $h_2 - h_1 = 2e \frac{g^2 - f^2}{e^2 - g^2} = g_2 - g_1$ (xli)

give the central point of the excluded portion and its length. The planes of extreme projection are parallel to the planes of the extreme virtual foci no matter where the point g may be.

We cannot delay to consider the cubic ruled surface

$$\frac{x^2 + y^2}{z} = \frac{x^2}{h_1} + \frac{y^2}{h_2}$$
(xlii)

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generated by the perpendiculars to the initial ray in the planes of projection and through the corresponding foci (compare (xxxix)) except to state that the initial ray is a double line; that the surface consists of two sheets wholly exterior to the planes of extreme projection; and that it may be derived from a cylindroid by drawing lines parallel to the generators of the cylindroid from points on the axis whose distances from a fixed point (also on the axis) are inversely proportional to the corresponding distances of the generators of the cylindroid from the same point. Nor can we consider the scalars P associated with the generators of this surface corresponding to the pitch (p) associated with each generator of a cylindroid.

(14.) In order to study more closely the arrangement of the rays near a given point (t) on the initial ray, we shall show how to find a function of the variable vector a so that the surface

$$\rho = \beta + a f(a) \tag{xliii}$$

may pass through the given point and that its *element* at the point may be normal to all the contiguous rays. Differentiating (xliii)

$$d\rho = \phi \cdot d\omega a + d\omega a f + a df \qquad (xliv)$$

and we see that the condition is satisfied neglecting the second order of small quantities if when a = k,

$$f(k) = t$$
 and $(df) = Sk\phi \cdot d\omega k$ (xlv)

where (df) denotes that k has been substituted for a in the differential of f(a).

We shall now find the principal radii of curvature of a surface satisfying this condition at the point under consideration. Using the formula $d\rho + R dU\nu = 0$, we obtain at once

$$(\phi + t + R)d\omega k + k(df) = 0 \qquad (xlvi)$$

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so that (compare (xii)) R is given by the quadratic

$$Sk(\phi + t + R)^{-1}k = 0. \qquad (xlvii)$$

Hence the centres of curvature coincide with the principal foci and in the notations of (xxiv) and (xxxvii) the quadratic determining the radii of curvature is

$$(R + t - s_1) (R + t - s_2) = 0$$
, or $(R + g + f) (R + g - f) = 0$. (xlviii)

The measure of curvature of the orthogonal element of surface is the density* of the congruency being the ratio which the area traced on a unit sphere by the rays through a small normal circuit bears to the area of the circuit. This is equal to the inverse of the product of the distances of the point from the foci. We may also speak of the sum of the curvatures of the orthogonal element as the concentration of the congruency.[†]

(15.) It is not possible in general to draw a surface through an arbitrary point orthogonal to all the lines of the congruency. The condition (xlv) is equivalent to

$$\mathrm{d}f = \mathrm{Sad}\beta,\tag{xlix}$$

and if this holds continuously over a surface and not merely at a point we can differentiate again and write

$$d'df = Sad'd\beta + Sd'ad\beta = dd'f = Sadd'\beta + Sdad'\beta$$

provided the differentiations are independent.

Hence the condition is

$$Sd'ad\beta = Sdad'\beta \quad \text{or} \quad Sd'a\phi da = Sda\phi d'a$$

or again (compare (ii))
$$S\epsilon dad'a = 0 \quad \text{or} \quad S\epsilon a = 0 \tag{1}$$

because Vdad'a is parallel to a. Referring back to sections (9.) and (10.) we see that in this case the focal and the extreme points coincide and that $p_0 = 0$ and e = f.

Also an infinite number of surfaces can be drawn orthogonal to the rays because an arbitrary constant may be added to f(a). For rays of light these are the wavesurfaces when the medium is isotropic.

(16.) From any congruency it is possible to select a singly infinite system of rays on which the focal and extreme points coincide. The system may be defined by the equations

$$\rho = \beta + ta, \quad S\epsilon a = 0 \tag{1i}$$

but the second equation is not an identity as in the last section. These rays have certain other peculiarities especially in connexion with the foci by projection (compare (xli)).

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^{*} Hamilton loc. cit. used the word condensation in a similar sense.

[†] Royal Irish Academy Transactions, p. 377, vol. xxxi., 1900.

(17.) We do not determine a singly infinite system by equating to zero the discriminant of (xiii) or (xix) and thus expressing that the two extreme points coincide. For if we consider the mode in which this equation was arrived at, we see that for equal roots a must be normal to a cyclic plane of a certain quadric. Two conditions must therefore be satisfied and only a limited number of rays can possess the property in question.

Nor can the principal foei coincide except under special conditions. For the two axes of zero pitch on the cylindroid would then intersect. From this it follows that the cylindroid must reduce to a plane, and the extreme points must likewise coincide.*

(18.) Important surfaces connected with the congruency are the focal surface, the locus of the extreme points and the locus of the centres; of this last the equation is

$$\rho = \beta - \frac{1}{2} \alpha S a^{-1} (m'' - \phi) \alpha. \tag{lii}$$

We may moreover write down the differential equations of families of ruled surfaces composed of rays. For instance (compare (x))

$$p = S \frac{\phi da}{a da} = const.$$
, Sada = 0 (liii)

lead to a relation in a which coupled with $\rho = \beta + ta$ determines a family of ruled surfaces for which the parameter of distribution, or the pitch p, is constant. In particular for p = 0 we have the developables of the congruency. Geometrically, selecting any ray we can choose one of the rays into which it can be screwed with pitch p and from that another and so on and thus construct a surface included in the integral of (liii).

(19.) There is another and very useful method for the treatment of systems of rays. If ρ_1 and ρ_2 are the vectors to any two points, and if

$$\sigma = V \rho_2 \rho_1$$
 and $\tau = \rho_1 - \rho_2$ (liv)

the vectors σ , τ or any equimultiples determine the line through the two points. Its equation is

$$\rho = \sigma \tau^{-1} + x\tau, \qquad (1v)$$

and the ratio of the tensors only is important. The constituents of these vectors are equivalent to Plücker's six coordinates of a line. Thus given any pair of vectors σ and τ satisfying

$$S\sigma\tau = 0$$
 (lvi)

a definite line is determinate.

(20.) A scalar relation between σ and τ , homogeneous in the tensors, may be regarded as the equation of a complex; one restriction is imposed on the generality of the lines. Two scalar equations of this kind represent a congruency, three a regulus of lines constituting a ruled surface, and four a finite number of lines.

* Compare Sir Robert Ball, Theory of Screws, Chap. II., Cambridge 1900.

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(21.) Again a line may be determined by means of two planes intersecting in the line. If these are

$$S\lambda_1\rho + 1 = 0, \qquad S\lambda_2\rho + 1 = 0,$$
 (lvii)

it is evident or may at once be verified that λ_1 , λ_2 are connected with σ , τ by the equations

$$\tau = x \nabla \lambda_2 \lambda_1, \qquad \sigma = y(\lambda_1 - \lambda_2).$$

Also

$$\sigma = V \rho_1 \tau = x V \rho_1 V \lambda_2 \lambda_1 = -x(\lambda_1 - \lambda_2) \text{ by (lvii)}$$

$$\rho_1 - \rho_2 = \tau = x V \lambda_2 \lambda_1, \quad V \rho_2 \rho_1 = \sigma = -x(\lambda_1 - \lambda_2) \quad (1viii)$$

and therefore any function homogeneous in the tensors may be exhibited in three forms

$$f(\sigma, \tau) = 0; \quad f(\nabla \rho_2 \rho_1, \rho_1 - \rho_2) = 0; \quad f(\lambda_1 - \lambda_2, -\nabla \lambda_2 \lambda_1) = 0. \quad (\text{lix})$$

The third equation may also be regarded as that of the reciprocal complex formed by reciprocation with respect to the unit sphere $\rho^2 + 1 = 0$.

It is important to observe that change of origin is without effect on τ , but alters σ into $\sigma + V \epsilon \tau$.

(22.) The general linear and scalar relation

$$S\gamma\sigma + S\delta\tau = 0 \tag{lx}$$

reduces on change of origin to

$$S\gamma(\sigma + p\tau) = 0,$$
 (lxi)

$$p\gamma = \nabla \gamma \epsilon + \delta$$
 or $\epsilon = \nabla \delta \gamma^{-1} + x\gamma$, $p = S\delta \gamma^{-1}$. (lxii)

The equation (lx) represents the general linear complex; (lxi) is the reduced form of this equation when the origin is taken on the central axis determined by the second equation (lxii) and p is the parameter of the complex.

(23.) If ρ is the vector to any point on a ray through a given point, the extremity of $a, \sigma = Va\tau = Va\rho$, and by (1xi) the lines lie in the plane

$$S\gamma(a+p)(\rho-a)=0.$$
 (lxiii)

Identifying this equation with $S\lambda \rho + 1 = 0$ we see that

$$\gamma(a + p) + (p\lambda - 1)S\gamma a = 0$$
 whence $\gamma^2 + S\gamma\lambda S\gamma a = 0$,

or more symmetrically the equations

$$\frac{p\lambda-1}{a+p} = -\frac{\gamma}{S\gamma a} = \frac{S\gamma\lambda}{\gamma}$$
(lxiv)

give λ without ambiguity in terms of α and α in terms of λ so that the lines in a plane also pass through a point.

These equations lead to an important transformation. The equations

$$f(a) = 0, f \frac{V\gamma(p\lambda - 1)}{S\gamma\lambda} = 0$$
 (lxv)

represent respectively the locus of a point and the tangential equation of the transformed locus. For instance a line transforms into the intersection of the planes corresponding to two points on it; a surface of degree n transforms into a surface of class n.

(24.) If P is the shortest distance between the central axis and a ray, on replacing σ by $V(x\gamma + PUV\gamma\tau)\tau$ in the equation of the complex (lxi) we find

$$P = -p \frac{S\gamma\tau}{T\nabla\gamma\tau} = p \tan l \qquad (1xvi)$$

if l is the angle the ray makes with the plane normal to the axis. The rays therefore envelope helices coaxial with the complex and having the tangent of their inclination directly proportional to the radius (P) of the containing cylinder.

(25.) The theory of screws affords a vivid illustration of the arrangement of the rays of a linear complex. If a body is attached to a nut fitting a screw of pitch p and axis γ on which the origin of vectors is situated, the point in the body at the extremity of the vector ρ can only move in the direction of the vector

$$p\gamma + \nabla \gamma \rho.$$
 (lxvii)

Applying a force τ to this point no motion is produced if τ is at right angles to this direction or if (compare (lxi))

$$pS\gamma\tau + S\gamma\sigma = 0$$
, where $\sigma = V\rho\tau$. (lxviii)

Again, any point of the body is free to describe a helix whose tangent of inclination is *inversely* proportional to the radius of its cylinder. The direction of any force whose line of action touches this cylinder, and which does not disturb equilibrium must be at right angles to the helix of motion through its point of contact. The tangent of inclination of the force is consequently *directly* proportional to the radius of the cylinder.

We see thus that the linear complex is a very particular case of the general relation*

$$S(\sigma_1\omega + \sigma\omega_1) = 0,$$
 (lxix)

which expresses that the screw (σ, ω) is reciprocal to the screw (σ_1, ω_1) when we do not suppose $S\sigma\omega$ to be zero. This being so and as linear systems of screws are

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^{*} Compare the Note on Screws, section (3.), p. 390.

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discussed in the Note on Screws, we shall not here consider systems of linear complexes. Moreover in the following sections we shall consider the general complex as a particular case of the general system of screws satisfying a single condition.

(26.) The equation of such a system is of the form

$$f(\sigma, \omega) = 0 \tag{1xx}$$

homogeneous in the vectors (σ, ω) or in other words independent of the absolute magnitude of their tensors. If we write the differential as

$$df(\sigma, \omega) = S(\omega_1 d\sigma + \sigma_1 d\omega) \qquad (1xxi)$$

we may replace the equation of the system by

$$S(\omega_1 \sigma + \sigma_1 \omega) = 0 \qquad (lxxii)$$

because the function f is homogeneous.

(27.) In the language of the theory of screws^{*} we may say that the screw (σ_1, ω_1) is reciprocal to (σ, ω) . Moreover by (lxxi), σ_1 and ω_1 are determinate functions of σ and ω , or

$$\sigma_1 = \theta(\sigma, \omega), \quad \omega_1 = \chi(\sigma, \omega).$$
 (lxxiii)

Thus we may regard (lxxiii) as establishing a correspondence between a pair of screws (σ_1, ω_1) and (σ, ω) , and (lxx) or (lxxii) as representing the assemblage of screws reciprocal to their correspondents.

Further (lxxiii) implies relations

$$\boldsymbol{\sigma} = \boldsymbol{\theta}_1 \ (\boldsymbol{\sigma}_1, \ \boldsymbol{\omega}_1), \quad \boldsymbol{\omega} = \boldsymbol{\chi}_1 \ (\boldsymbol{\sigma}_1, \ \boldsymbol{\omega}_1) \tag{lxxiv}$$

and the first and third of the equations

$$f(\sigma, \omega) = 0$$
, $S(\omega_1 \sigma + \sigma_1 \omega) = 0$, $f_1(\sigma_1, \omega_1) = 0$ (lxxv)

represent the assemblage of screws and the assemblage of their reciprocal correspondents while the condition of reciprocity is expressed by the second. Or again the second equation may be regarded as determining either of the assemblages having regard to (lxxiii) or (lxxiv).

(28.) If p is the pitch and a the vector to a point on the axis of the screw (σ, ω) ,

$$\sigma = (p + Va)\omega. \qquad (lxxvi)$$

Substitution in (lxx) affords the equation

$$f((p + Va) \omega, \omega) = 0 \qquad (lxxvii)$$

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^{*} Compare again the Note on Screws, section (3.); and for the correspondence (lxxiii) compare the particular case of linear correspondence of section (12.) of the note cited, p. 394.

which admits of the following interpretations :---

- I. Given p it is the equation of the complex of axes of screws of given pitch belonging to the assemblage.
- II. It represents a singly infinite system of complexes depending on the parameter p.
- III. It represents the cone of axes of screws of given pitch p which pass through a given point (a).
- IV. It is equivalent to a scalar equation determining the pitches of the screws of the assemblage whose axes coincide with a given line (Va ω and ω given).
- V. By (lix) if we suppose

$$Va\omega = \lambda_1 - \lambda_2 = \mu, \quad \omega = -V\lambda_2\lambda_1 = V\mu\lambda_1$$
 (lxxviii)

we see that the rays of the complex (p given) which lie in the plane $S\lambda_1\rho + 1 = 0$ envelope the curve in which the plane cuts the envelope of the variable plane $S\mu\rho = 0$ where

$$f(\nabla \mu (p\lambda_1 + 1), \nabla \mu \lambda_1) = 0. \qquad (lxxix)$$

Evidently the order of the cone III., the degree of the equation IV. and the class of the curve V. are all equal to the order in which the vectors (σ, ω) jointly occur in (lxx).

(29.) If the cone III. (lxxvii) has a double edge (ω) the differential vanishes no matter what vector d ω may be; so in the notation of (lxxi),

$$S(\omega_1(p + Va)d\omega + \sigma_1 d\omega) = 0 \quad \text{or} \quad S(\sigma_1 - (-p + Va)\omega_1)d\omega = 0. \quad (1xxx)$$

Hence as $d\omega$ is quite arbitrary

$$\sigma_1 = (-p + Va)\omega_1. \qquad (lxxxi)$$

Comparing (lxxvi) we see that in this case the axes of the reciprocal correspondents $(\sigma_1, \omega_1), (\sigma, \omega)$ intersect and their pitches are equal and opposite. These two consequences are of course not independent; the latter implies the former. The symmetry of these relations shows that the locus of vertices of cones with double edges which are composed of axes of screws of pitch p, is likewise the locus of vertices of nodal cones composed of axes of the reciprocal correspondents of pitch -p.

The locus of the vertices of the nodal cones of a complex is the Kummer surface. Consequently the Kummer surfaces of the two complexes just described are identical.

(30.) The double edges of the cones of the complex form a congruency specified by the three equations

$$p = S\sigma\omega^{-1}; \quad S(\sigma\omega_1 + \omega\sigma_1) = 0; \quad p = -S\sigma_1\omega_1^{-1}$$
 (lxxxii)

If n is the order of the original equation in σ and ω , n-1 is the order of σ_1 and ω_1

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in the same vectors and 2(n-1) is that of $p\omega_1^2 = -S\sigma_1\omega_1$. The first and third equations (lxxxii) determine a complex of order 2(n-1), and the rays common to this and to the complex of order *n* determined by the first and second (lxxxii) compose a congruency whose order and class are both equal to 2(n-1)n. For the order is the number of rays through a point or the number of common edges of two cones of degree *n* and 2(n-1); and the class is the number of rays in a plane, or the number of common tangents of two curves of class *n* and 2(n-1).

The congruency is likewise specified by the vector equations in which α is the vector to a point on the Kummer surface

$$\boldsymbol{\sigma} = (p + \mathbf{V}\boldsymbol{a})\boldsymbol{\omega}; \quad \boldsymbol{\sigma}_1 = (-p + \mathbf{V}\boldsymbol{a})\boldsymbol{\omega}_1, \quad (\mathbf{I}\mathbf{X}\mathbf{X}\mathbf{I}\mathbf{I}\mathbf{I})$$

it being understood that σ_1 and ω_1 are given functions of σ and ω .

(31.) It is easy to see that the rays of the congruency touch the Kummer surface of the complex and from this property it will follow that the Kummer surface is part at least of the focal surface of the congruency.

Using the equations (lxxxiii) we have

$$d\sigma = (p + Va)d\omega + Vda\omega; \quad d\sigma_1 = (-p + Va)d\omega_1 + Vda\omega_1 \qquad (lxxxiv)$$

for the consecutive screws of pitches $\pm p$ whose axes intersect at a consecutive point (a + da) on the Kummer surface. Operating on the first by $S\omega_1$ and attending to (lxxxiii) and (lxxi) we find

$$df(\sigma, \omega) = S(\omega_1 d\sigma + \sigma_1 d\omega) = S da \omega \omega_1 = 0 \qquad (lxxxy)$$

because the screw $(\sigma + d\sigma, \omega + d\omega)$ belongs to the assemblage $f(\sigma, \omega) = 0$. In like manner exactly the same equation is found by operating on the second by S ω . Hence $\nabla \omega \omega_1$ is at right angles to all tangential vectors $(d\alpha)$ to the surface and in particular the axes of the screws $(\omega \text{ and } \omega_1)$ touch the surface.

Now if the lines of a congruency touch a surface that surface is part at least of the focal surface. For take any ray touching the surface at a and having the direction δa . The consecutive ray touching the surface at $a + \delta a$ intersects this ray and the point of intersection is a principal focus on both. The surface therefore is part of the focal surface. If da is the conjugate direction to δa , the second ray which intersects $\rho = a + t\delta a$ touches the surface at a + da and the point of intersection of these two rays lies on the other part of the focal surface. In fact if two rays intersect at ρ ,

 $da + dt\delta a + td\delta a = 0$ whence $Sda\delta ad\delta a = 0$.

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XIII.—ON THE OPERATOR ∇ .

(1.) If $f\rho$ is any scalar function of a vector ρ , corresponding differentials are connected by a relation of the form

$$\mathrm{d}f\rho = -\mathrm{S}\nu\mathrm{d}\rho,\tag{i}$$

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in which ν is a vector derived from $f\rho$ depending merely on the function f and on the value of the variable vector ρ but not at all on the differential $d\rho$.

Regarding ρ as a vector of position, the rate of change of the function of position $f\rho$ along any direction $Ud\rho$ is evidently $-S\nu Ud\rho$, in other words it is equal to the projection of the vector ν upon that direction. This rate of change is greatest along the direction $U\nu$ being then equal to $T\nu$. In any other direction it is equal to $T\nu$ multiplied by the cosine of the angle between the assumed direction and that of ν .

(2.) It is convenient to use a special notation to suggest the dependence of the vector ν on the scalar function $f\rho$. For this purpose Hamilton^{*} introduced the symbol Nabla or ∇ and connected ν with $f\rho$ by the symbolical equation

$$\boldsymbol{\nu} = \nabla f \boldsymbol{\rho}, \tag{ii}$$

in which ν is conceived to be the result of a certain operation performed on $f\rho$.

(3.) We shall now illustrate by a few examples the effect of operating by ∇ on scalar functions. It must be observed however that these are merely translations into the new notation of results already obtained in the course of this work Thus:—

(<i>a</i>)	$\nabla S\lambda ho = -\lambda$	because	$\mathrm{d}\mathrm{S}\lambda\rho=\mathrm{S}\lambda\mathrm{d}\rho.$
<i>(b)</i>	$ abla ho^2 = -2 ho$,,	$\mathrm{d}\rho^2 = 2\mathrm{S}\rho\mathrm{d}\rho.$
(c)	$\nabla S \rho \Phi \rho = - \ 2 \Phi \rho$,,	$\mathrm{d}\mathrm{S}\rho\Phi\rho=2\mathrm{S}\Phi\rho\mathrm{d}\rho.$
(d)	$\nabla \mathbf{T} \boldsymbol{\rho} = + \mathbf{U} \boldsymbol{\rho}$,,	$\mathrm{dT}\rho = -\mathrm{SU}\rho\mathrm{d}\rho.$
(e)	$ abla TV\lambda ho = + UV\lambda ho$. λ	"	$\mathrm{d} \mathrm{T} \mathrm{V} \lambda \rho = - \mathrm{S} \mathrm{U} \mathrm{V} \lambda \rho \mathrm{V} \lambda \mathrm{d} \rho.$
(f)	$ abla f \mathbf{T}(ho - \lambda) = \mathbf{U}(ho - \lambda)f' \mathbf{T}(ho - \lambda)$) ,,	$\mathrm{d}f\mathrm{T}(\rho-\lambda)=-f'\mathrm{T}(\rho-\lambda)\mathrm{SU}(\rho-\lambda)\mathrm{d}\rho.$
(g)	$\nabla T(\rho - \lambda)^{-1} = -U(\rho - \lambda) T(\rho - \lambda)$	-2 ,,	$\mathrm{d} T(\rho-\lambda)^{\text{-1}} = - T(\rho-\lambda)^{\text{-2}} \mathrm{d} T(\rho-\lambda).$
(h)	$ abla T \phi ho = \phi' U \phi ho$,,	$\mathrm{d} \mathrm{T} \phi \rho = - \mathrm{S} \phi' \mathrm{U} \phi \rho \cdot \mathrm{d} \rho.$

All these expressions are consequences of the equations

$$\nabla f \rho = \nu, \qquad \mathrm{d} f \rho = - \mathrm{S} \nu \mathrm{d} \rho,$$

which may be regarded (compare (i) and (ii)) as a definition of ∇ , the vector λ and the vector functions Φ and ϕ being supposed constant in the examples.

* Proceedings Royal Irish Academy, vol. iii., p. 291. See note, p. 548, vol. i.

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Example (g) is of fundamental importance in the theory of attractions for it shows that $\nabla T(\rho - \lambda)^{-1}$ represents in magnitude and direction the attraction at the extremity of ρ due to a unit mass at the extremity of λ .

(4.) Again if f and g are any two scalar functions of ρ

because

$$\nabla (f+g) = \nabla f + \nabla g \quad \text{and} \quad \nabla (fg) = g\nabla f + f\nabla g \quad (\text{iii})$$
$$d(f+g) = df + dg \quad \text{and} \quad d(fg) = gdf + fdg.$$

Generally as a matter of convenience it is desirable if possible to place the operand immediately to the right of the operator ∇ . This can be effected in the second equation (iii) because f and g are scalars and therefore commutative with vectors and quaternions. We shall soon see however that we can assign a definite meaning to the result of operating on a vector or quaternion by ∇ . But since we must regard ∇ as a symbolical vector or at least as possessing certain characteristics of a vector (for by definition it produces a vector from a scalar), we are not at liberty to write $p\nabla q = \nabla q \cdot p$ when p is a quaternion, nor *d* fortiori when p and q are both quaternions. Hence it is not in general possible to place the operand immediately to the right. We are therefore obliged to have recourse to brackets or accents or some temporary mark in order to distinguish the operand. For instance we may write $\nabla(f)g$ to denote that f is excluded from the operation of ∇ ; or we may accent ∇ and g and $\nabla' fg'$ will then sufficiently indicate that g and not f is the subject of operation.

(5.) Consider in the next place a scalar function of several independent variable vectors ρ , ρ_1 , ρ_2 , &c. We may in an obvious notation write (compare V, p. 294),

$$d \cdot F(\rho, \rho_1, \rho_2 \dots) = - \operatorname{Sd} \rho \nu - \operatorname{Sd} \rho_1 \nu_1 - \operatorname{Sd} \rho_2 \nu_2 - \&c.$$

= - Sd $\rho \nabla F - \operatorname{Sd} \rho_1 \nabla_1 F - \operatorname{Sd} \rho_2 \nabla_2 F - \&c.$ (iv)

where ∇_1 operates on F as if ρ_1 were the only variable. In fact $-\nabla$, $-\nabla_1$, &c. correspond precisely to Hamilton's D_{ρ} , $D_{\rho'}$ (or rather D_a , D_a') of the formula just cited. It may sometimes be even clearer to distinguish the corresponding operator by a sub-index of the vector operated on, thus (compare section (3.)) we have

$$(a') \qquad \nabla_{\rho} S\lambda \rho = -\lambda; \quad \nabla_{\lambda} S\lambda \rho = -\rho$$

(e')
$$\nabla_{\alpha} T V \lambda \rho = - U V \lambda \rho \cdot \lambda; \quad \nabla_{\lambda} T V \lambda \rho = - U V \rho \lambda \cdot \rho$$

$$(q') \qquad \nabla_{\rho} T(\rho - \lambda)^{-1} = - U(\rho - \lambda) T(\rho - \lambda)^{-2} = - \nabla_{\lambda} T(\rho - \lambda)^{-1}.$$

Also for any function of λ and ρ

I.
$$\nabla \lambda \nabla_{\rho} f = 0$$
, II. $S \lambda \nabla_{\rho} f = 0$, III. $\nabla_{\rho} f + \nabla_{\lambda} f = 0$ (v)

if f is a function of I. $S\lambda\rho$, II. $\nabla\lambda\rho$, III. $\rho - \lambda$.

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Again (compare (3.) (g) and (4.) (iii)) if P is the potential at the extremity of the vector ω of a system of attracting particles m_1 , m_2 , &c. whose position vectors are ρ_1 , ρ_2 , &c., the law of attraction being the law of nature, the force on a unit mass at ω is

$$\nabla_{\omega}P = \nabla_{\omega}\Sigma m T(\omega - \rho)^{-1} = -\Sigma m U(\omega - \rho) T(\omega - \rho)^{-2} = -\Sigma m \nabla_{\rho}T(\omega - \rho)^{-1}. \quad (vi)$$

Or if we have to do with a continuous distribution of mattter the force is given by

$$\nabla_{\omega} P = \nabla_{\omega} \int \frac{\mathrm{d}m}{\mathrm{T}(\omega-\rho)} = -\int \frac{\mathrm{U}(\omega-\rho)\mathrm{d}m}{\mathrm{T}(\omega-\rho)^2} = -\int \mathrm{d}m \nabla_{\rho} \frac{1}{\mathrm{T}(\omega-\rho)}.$$
 (vii)

(6.) Again if α , β , γ are any constant vectors and X, Y and Z any scalar functions of ρ (compare the first of (iii)),

$$\begin{aligned} \mathrm{d}(aX+\beta Y+\gamma Z) &= \mathrm{d}X.\,a+\mathrm{d}Y.\,\beta+\mathrm{d}Z.\,\gamma \\ &= -\left(\mathrm{Sd}\rho\nabla.\,X\right)a-(\mathrm{Sd}\rho\nabla.\,Y)\beta-(\mathrm{Sd}\rho\nabla.\,Z)\gamma \\ &= -\,\mathrm{Sd}\rho\nabla.\,(Xa+Y\beta+Z\gamma). \end{aligned} \right\} \tag{viii}$$

Thus for any vector function of ρ we may write generally

$$d\sigma = -Sd\rho\nabla \cdot \sigma \tag{ix}$$

for we may always resolve the two vectors σ and $d\sigma$ along three given and fixed directions. In this equation (ix) we may suppose σ replaced by any quaternion function of ρ for by the distributive property if $\sigma = \nabla q$ we may add to (ix) the equation $dSq = -Sd\rho\nabla$. Sq so that

$$\mathrm{d}q = -\mathrm{Sd}\rho\nabla \,,\,q.\tag{x}$$

It must be carefully observed that in these equations we regard σ and q as functions of ρ alone. For instance if q involves the time t as well as ρ the *total* differential is*

where the first term on the right refers to t as occurring in q but not in ρ .

(7.) We have now shown that the general formula (x) is true whether q be quaternion, vector, or scalar so that we may write generally and symbolically

$$\mathbf{d} = -\operatorname{Sd}\rho\nabla \tag{xii}$$

or what is equivalent

$$\nabla = -\frac{\mathrm{Vd}'\rho\mathrm{d}''\rho\,.\mathrm{d} + \mathrm{Vd}''\rho\mathrm{d}\rho\,.\mathrm{d}' + \mathrm{Vd}\rho\mathrm{d}'\rho\,.\mathrm{d}''}{\mathrm{Sd}\rho\mathrm{d}'\rho\mathrm{d}''\rho} \tag{xiii}$$

* We must particularly distinguish between

 $\mathrm{Sd}\rho\nabla \cdot q$ and $\mathrm{S} \cdot \mathrm{d}\rho\nabla q$.

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where $d\rho$, $d'\rho$ and $d''\rho$ are any three non-coplanar differentials of ρ , and where d, d' and d'' are the corresponding symbols of differentiation. In fact this equation (xiii) is equivalent to the three

$$d = -Sd\rho\nabla, \quad d' = -Sd'\rho\nabla, \quad d'' = -Sd''\rho\nabla$$

as appears in various ways.*

(8.) As an independent method we have (compare (6.))

$$\nabla(aX + \beta Y + \gamma Z) = \nabla X \cdot a + \nabla Y \cdot \beta + \nabla Z \cdot \gamma \qquad (xiv)$$

where we employ merely the distributive principle (iii) and the commutative property of a scalar (X) with a vector (a). But we already know how to calculate the effect of ∇ on a scalar, so we can determine its effect on a quaternion or vector by referring the vector part or vector to any three fixed directions.

To trace the relation between these two methods we have

$$\mathrm{d} X = - \operatorname{Sd} \rho \nabla \cdot X, \ \& \mathrm{c.},$$

whence without employing symbolical equations

$$\nabla X = -\frac{\operatorname{Vd'\rho d''\rho} \cdot dX + \operatorname{Vd''\rho d'\rho} \cdot d'X + \operatorname{Vd\rho d'\rho} \cdot d''X}{\operatorname{Sd\rho d'\rho d''\rho}}$$

Multiplying into a and forming similar expressions in ∇Y and ∇Z we find on addition if $\sigma = aX + \beta Y + \gamma Z$

$$\nabla \sigma = -\frac{\mathrm{Vd}' \rho \mathrm{d}'' \rho \cdot \mathrm{d}\sigma + \mathrm{Vd}'' \rho \mathrm{d}' \rho \cdot \mathrm{d}' \sigma + \mathrm{Vd} \rho \mathrm{d}' \rho \cdot \mathrm{d}'' \sigma}{\mathrm{Sd} \rho \mathrm{d}' \rho \mathrm{d}'' \rho} \qquad (\mathrm{xv})$$

which agrees with (xiii).

(9.) We give a few examples of operating on vectors with hints for verification

(a) $\nabla \rho = -3$; $\operatorname{Vd}' \rho \operatorname{d}'' \rho \cdot \operatorname{d} \rho + \operatorname{Vd}'' \rho \operatorname{d} \rho \cdot \operatorname{d}' \rho + \operatorname{Vd} \rho \operatorname{d}' \rho \cdot \operatorname{d}'' \rho = 3 \operatorname{Sd} \rho \operatorname{d}' \rho \operatorname{d}'' \rho$.

(b) $\nabla \nabla \lambda \rho = 2\lambda = -\nabla (\rho \lambda - S \rho \lambda)$ or $= -\lambda S \nabla \rho + S \lambda \nabla \cdot \rho$.

(c) $\nabla \phi \rho = 2\epsilon - m''$; $\nabla \beta \gamma \cdot \phi a + \nabla \gamma a \cdot \phi \beta + \nabla a \beta \cdot \phi \gamma = (m'' - 2\epsilon) S a \beta \gamma$.

(d)
$$\nabla U \rho = -2T \rho^{-1} = \nabla (\rho T \rho_0^{-1} + T \rho^{-1}, \rho_0).$$

(e)
$$\nabla \rho^{-1} = -\rho^{-2}; \quad \nabla (\rho^{-1}\rho) = 0.$$

- (f) $\nabla^2 T(\rho \lambda)^{-1} = 0$ if ρ is not equal λ .
- (g) $\nabla^2 f \operatorname{T} \rho = -f'' \operatorname{T} \rho 2 \operatorname{T} \rho^{-1} f' \operatorname{T} \rho.$

(h)
$$\nabla^2 T V \lambda \rho = -T (V \lambda^{-1} \rho)^{-1}$$
.

(i) $\nabla^2 \log \mathrm{TV}\lambda \rho = 0.$

* Either by verification or by multiplying these three equations by

Vd'pd"p, Vd"pdp, Vdpd'p

and adding. See also the next section.

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For one unfamiliar with the subject it is however far better to employ no short cuts except an intelligent selection of the differentials of ρ if he uses the formula (xiii). For instance in (b) he may take these to be λ , ρ and $\nabla\lambda\rho$. He must however be careful if he employs variable differentials to operate on these in subsequent operations* involving ∇ . As explained in the last section the results may all be obtained by resolving the vectors along fixed directions.

(10.) To the examples of the last article we may add the following :--

(a) $\nabla \lambda \nabla \cdot \rho = -2\lambda$. (b) $\nabla \lambda \nabla \cdot \phi \rho = (\phi' - m'')\lambda + 2S\epsilon\lambda$. (c) $\phi \nabla \cdot \rho = -(m'' + 2\epsilon)$. (d) $\phi \nabla \cdot T\rho = \phi U\rho$. (e) $\phi \nabla \cdot U\rho = -(m'' + 2\epsilon)T\rho^{-1} + \phi U\rho \cdot \rho^{-1}$. (f) $\phi \nabla \cdot \nabla \lambda \rho = (m'' - \phi')\lambda + 2S\epsilon\lambda$.

And simpler examples may be obtained by selecting special forms of ϕ .

(11.) To anyone acquainted with the Calculus of Operations[†] it is manifest immediately the form (xiii) is obtained that ∇ may be combined with vectors and quaternions just as if it were an ordinary vector. In fact we may regard the symbols of differentiation d, d', d" as mere scalars and manipulate our formulæ in any way until we see fit to operate. Of course when successive operators ∇ occur in the same equation they must in general be distinguished by suitable marks and treated as independent vectors. This implies that the symbols d, d', d" of each operator must also be car-marked whenever necessary.

We infer among other deductions that the operator ∇^2 or $\nabla \cdot \nabla$ is a scalar because the square of a vector is a scalar. In the next section we shall verify this result from an elementary point of view.

(12.) It has been abundantly shown that ∇ is totally independent of any particular coordinates, parameters or differentials. We therefore take the case most familiar and choose our differentials so that

$$d\rho = i dx, \quad d'\rho = j dy, \quad d''\rho = k dz$$
 (xvi)

and therefore

$$d = dx \frac{\partial}{\partial x}, \quad d' = dy \frac{\partial}{\partial y}, \quad d'' = dz \frac{\partial}{\partial z}$$
 (xvii)

writing $\rho = ix + jy + kz$, *i*, *j* and *k* being constant.

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^{*} Compare section (74.).

⁺ See Boole, "Differential Equations," chap. xvii., or Forsyth, "Differential Equations," chap. iii., or indeed any work on this subject which treats of symbolical methods.

The relation (xiii) reduces at once to the well-known form

$$\nabla = i \frac{\partial}{\partial x} + j \frac{\partial}{\partial y} + k \frac{\partial}{\partial z}$$
(xviii)

which shows us that the operation performed by ∇ is equivalent to taking the partial differential *coefficients* of any function with respect to the three scalars x, y and z and multiplying these respectively by i, j and k and then adding the results.

Now when we operate twice by ∇ we have

$$\nabla' \nabla = \left(i \frac{\partial'}{\partial x} + j \frac{\partial'}{\partial y} + k \frac{\partial'}{\partial z} \right) \left(i \frac{\partial}{\partial x} + j \frac{\partial}{\partial y} + k \frac{\partial}{\partial z} \right)$$
$$= - \left(\frac{\partial'}{\partial x} \frac{\partial}{\partial x} + \frac{\partial'}{\partial y} \frac{\partial}{\partial y} + \frac{\partial'}{\partial z} \frac{\partial}{\partial z} \right) + i \left(\frac{\partial'}{\partial y} \frac{\partial}{\partial z} - \frac{\partial'}{\partial z} \frac{\partial}{\partial y} \right)$$
$$+ j \left(\frac{\partial'}{\partial z} \frac{\partial}{\partial x} - \frac{\partial'}{\partial x} \frac{\partial}{\partial z} \right) + k \left(\frac{\partial'}{\partial x} \frac{\partial}{\partial y} - \frac{\partial'}{\partial y} \frac{\partial}{\partial x} \right)$$
(xix)

because the vectors i, j, k are constant. Suppressing the ear-marking accents as no longer necessary when we operate on a single function,

$$\nabla^2 = -\frac{\partial^2}{\partial x^2} - \frac{\partial^2}{\partial y^2} - \frac{\partial^2}{\partial z^2}$$
(xx)

because the order in which the partial differentiation is effected with respect to y and z is indifferent. As we have stated at the beginning of this section ∇ and therefore ∇^2 is quite independent of any particular analytical representation, and thus apart from any *à priori* inferences arising from the form (xiii) we have proved that ∇^2 is a scalar operator; it is in fact with sign changed Laplace's most important operator.

The fuller discussion of the analytical forms attributable to ∇ is postponed to a later section.*

(13.) It may be as well to print here the equation

$$\nabla q = -\frac{\partial X}{\partial x} - \frac{\partial Y}{\partial y} - \frac{\partial Z}{\partial z} + i \left(\frac{\partial W}{\partial x} + \frac{\partial Z}{\partial y} - \frac{\partial Y}{\partial z} \right) + j \left(\frac{\partial W}{\partial y} + \frac{\partial X}{\partial z} - \frac{\partial Z}{\partial x} \right) \\ + k \left(\frac{\partial W}{\partial z} + \frac{\partial Y}{\partial x} - \frac{\partial X}{\partial y} \right)$$
(xxi)

which is obtained by operating by ∇ in the form (xviii) on q in the form

$$q = W + iX + jY + kZ.$$
(xxii)

* See section (73.).

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This gives at once expressions for $S \nabla q$, $\nabla \nabla q$, $\nabla S q$, $S \nabla V q$, and $\nabla \nabla V q$. We observe that

$$S \nabla q = S \nabla V q$$
 and $V \nabla q = \nabla S q + V \nabla V q$ (xxiii)

and we notice that the form of these equations is precisely the same as if ∇ were an ordinary vector—a verification of the *à priori* inference drawn in (11.).

It may be instructive to the student to find expressions for

$$\nabla Uq$$
, ∇Tq , $T \cdot \nabla q$, ∇Kq , $K \nabla q$, $K \nabla Kq$, $q \nabla q$

and other combinations of the symbols q, ∇ and the characteristics S, V, T, U, and K.

(14.) We can at once assign an interpretation to

$$\nabla q = -\frac{\mathrm{Vd}'\rho \mathrm{d}''\rho \cdot \mathrm{d}q + \mathrm{Vd}''\rho \mathrm{d}\rho \cdot \mathrm{d}'q + \mathrm{Vd}\rho \mathrm{d}'\rho \cdot \mathrm{d}''q}{\mathrm{Sd}\rho \mathrm{d}'\rho \mathrm{d}''\rho} \qquad (\mathrm{xxiv})$$

(compare (xiii)) by considering the parallelepiped whose centre is at the extremity of ρ and whose small* vector edges are $d\rho$, $d'\rho$ and $d''\rho$. The vectors from the centre to the centres of the faces are $\pm \frac{1}{2}d\rho$, $\pm \frac{1}{2}d'\rho$, $\pm \frac{1}{2}d''\rho$ and the outwardly directed areas of these faces are $\pm Vd'\rho d''\rho$, $\pm Vd''\rho d\rho$, $\pm Vd\rho d'\rho$, the signs corresponding if $Sd\rho d'\rho d''\rho$ is negative.

Now the mean value of q over the face + $Vd'\rho d''\rho$ may be taken as its value at the centre of the face or ultimately as $q + \frac{1}{2}dq$, q being the value at the centre of the parallelepiped. But

$$-\frac{\operatorname{Vd}'\rho d''\rho \cdot dq}{\operatorname{Sd}\rho d'\rho d''\rho} = \frac{+\operatorname{Vd}'\rho d''\rho}{-\operatorname{Sd}\rho d'\rho d''\rho} \cdot (q + \frac{1}{2}dq) + \frac{-\operatorname{Vd}'\rho d''\rho}{-\operatorname{Sd}\rho d'\rho d''\rho} (q - \frac{1}{2}dq); \quad (\operatorname{xxv})$$

that is it is equal to the sum of the mean value of q over each face multiplied by the directed area of that face and divided by the volume $(-\operatorname{Sd}\rho d'\rho d''\rho)$ of the parallelepiped.

Adding up we see that ∇q equals the sum of the products of the directed elements of the surface into the corresponding values of q divided by the volume included.

(15.) We shall extend this result so as to be able to write for any small closed surface surrounding the extremity of ρ ;

$$\nabla q = \lim_{v \to \infty} \frac{1}{v} \int d\nu q \qquad (xxvi)$$

where v is the volume included by the surface and dv a directed element of area, the normal being outwardly drawn. Conceive the region enclosed by the surface divided arbitrarily into an infinite number of small parallelepipeds. For each of these

$$\nabla q \mathrm{d} v = \int \mathrm{d} v q$$

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^{*} It is not necessary in (xiii) that the differentials should be small.

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where ∇q on the left refers to the centre of the parallelepiped. On summation

$$\Sigma \nabla q \mathrm{d} v = \Sigma \int \mathrm{d} v q.$$

But over a common interface $d\nu$ regarded as referring to one parallelepiped is opposite to $d\nu$ referring to the other. Hence if there is no discontinuity in q the interfaces contribute nothing and $\sum \int d\nu q$ is due simply to the bounding faces of the extreme parallelepipeds, so that in the limit as these become indefinitely small

$$\int \nabla q \, \mathrm{d}v = \int \mathrm{d}v q \qquad (xxvii)$$

where the integral on the left is taken throughout the volume and that on the right over the surface. Conceive now the surface to shrink indefinitely and we find in the limit the required result (xxvi).

(16.) On account of the importance of this result and also as an exercise we shall calculate directly the integral taken over any small closed surface including the extremity of the vector ρ . Let τ be the variable vector drawn from this point and terminating on the surface.

Since τ is small we may put for the value of q at its extremity

$$q_{\tau} = q - S\tau \nabla \cdot q \qquad (xxviii)$$

q being the value at the extremity of ρ . Here we assume as in the last section that the function q is continuous. If $d\nu$ or $Vd\tau d'\tau$ is an outwardly directed element of the surface

$$\int d\nu q_{\tau} = \int d\nu (q - S\tau \nabla \cdot q) = -\int d\nu \cdot S\tau \nabla \cdot q \qquad (xxix)$$

because the surface is closed so that $\int dv = 0$ or $\int dv q = 0$.

In this if we choose we may regard

$$-\int d\nu \cdot S\tau \nabla$$
 (XXX)

as an operator acting on q since we have to deal with τ only so far as integration is concerned, or indeed we may take ∇ outside the sign of integration and regard

$$-(\int d\nu S\tau)\nabla$$
 (xxxi)

as a linear and vector function of ∇ .

In any case we have for any vectors τ , $d\tau$, and $d'\tau$

$$Vd\tau d'\tau S\tau \nabla + Vd'\tau\tau Sd\tau \nabla + V\tau d\tau Sd'\tau \nabla = S\tau d\tau d'\tau \cdot \nabla \qquad (xxxii)$$

and also identically when d and d' operate on τ and its differentials alone

and
$$\begin{aligned} d\left(Vd'\tau\tau S\tau\nabla\right) &= dVd'\tau\tau \cdot S\tau\nabla + Vd'\tau\tau \cdot Sd\tau\nabla \\ d'\left(V\tau d\tau S\tau\nabla\right) &= d'V\tau d\tau \cdot S\tau\nabla + V\tau d\tau \cdot Sd'\tau\nabla \end{aligned} \right\}. \qquad (xxxiii)$$

$$\mathbf{But}$$

$$dVd'\tau\tau + d'V\tau d\tau = 2Vd'\tau d\tau + Vdd'\tau\tau + V\tau d'd\tau \qquad (xxxiv)$$

and the second and third term on the right cancel if we choose $d\tau$ and $d'\tau$ to be *independent* differentials so that $dd'\tau = d'd\tau$. In this case by means of (xxxiii) and (xxxiv) the equation (xxxii) reduces to

$$3Vd\tau d'\tau \cdot S\tau \nabla + d(Vd'\tau\tau S\tau \nabla) + d'(V\tau d\tau S\tau \nabla) = S\tau d\tau d'\tau \cdot \nabla. \quad (xxxv)$$

Integrating over the surface we find

$$3 \int V d\tau d'\tau \nabla \cdot S\tau \cdot q = \int S\tau d\tau d'\tau \cdot \nabla q \qquad (xxxvi)$$

since $\int d(\nabla d'\tau\tau S\tau \nabla) \cdot q$ vanishes* if we suppose as we may that $d\tau$ (and also $d'\tau$) is an element of a closed curve drawn on the closed surface. Now $\frac{1}{3}S\tau d\tau d'\tau$ is the *negative* volume of the pyramid whose vertex is at the origin of vectors τ and whose base is the *outwardly* directed element of area $\nabla d\tau d'\tau$ or $d\nu$. Hence if v is the volume of the closed surface by (xxxvi) and (xxix) we find

$$\int \mathrm{d} \nu q_{\tau} = v \nabla q.$$

Or finally dropping the sub-index τ as not now necessary we have rigorously

$$\nabla q = lim. \frac{1}{v} \int dv q ; \qquad (xxxvii)$$

or the value of ∇q at any point is the limit of the integral of the outwardly directed elements of any small closed surface surrounding the point multiplied into the corresponding quaternion q and divided by the volume enclosed by the surface.

(17.) We proceed at once to the interpretation of the results of the last two sections.

The case of q a scalar is apply illustrated by a hydrostatic pressure p. As dv has been supposed measured outwardly, -dvp is the pressure in direction and magnitude on the directed element, and $-\int dvp = -v\nabla p$ is the resultant pressure over the surface. This urges the element in the direction $-U\nabla p$, that is in the direction in which p diminishes most rapidly for we have seen (1.) that $+U\nabla p$ is the direction in which p increases most rapidly.

(18.) In the case of q a vector (σ) unlike the former case, the integral consists of a scalar as well as a vector part. We notice that the scalar part depends merely on the components of the vectors σ normal to the surface and the vector part on the tangential components. For

$$\nabla \sigma = v^{-1} (\mathbf{S} + \mathbf{V}) \int d\nu \sigma = v^{-1} \int \mathbf{S} d\nu \sigma + v^{-1} \int \mathbf{V} d\nu \sigma \qquad (\mathbf{x} \mathbf{x} \mathbf{x} \mathbf{v} \mathbf{i} \mathbf{i})$$

because S and V are distributive, the scalar of a sum for instance being the sum of the scalars.

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^{*} We repeat that q is quite independent of τ being in fact the value of q at the origin of the vectors τ .

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We shall consider the scalar and vector integrals separately, that is the integral of the *inwardly*^{*} directed normal components + $Sd\nu\sigma$; and the integral of the tangential components turned through a right angle in the tangent plane for

$$Vd\nu\sigma = d\nu(d\nu)^{-1}Vd\nu\sigma.$$

(19.) Taking the scalar part first we have to interpret

$$S \nabla \sigma = \frac{1}{v} \int S dv \sigma.$$
 (XXXIX)

In the first place let σ represent the displacement of a point in a body—the extremity of the vector ρ —deformable in any way. The integral then represents the sum of the inward components of displacement of the elements of the small surface; in other words it is the diminution of volume. The ratio of this to the volume is the condensation. To put this in a clearer light we resort to the suffix τ (xxviii) and (compare (xxix)) we write $\int Sd\nu\sigma_{\tau} = \int Sd\nu(\sigma_{\tau} - \sigma)$ so that we only have to consider the displacement relative to the origin of vectors τ .

Secondly let σ denote any distribution of force. The integral represents the *total* normal force over the surface.

Thirdly if σ represents the *flux* of a fluid the integral measures the rate at which the inflow into the little region exceeds the outflow. The quotient of this by the volume is the rate at which the fluid accumulates in unit volume or the rate of increase of density at the point. Otherwise if σ is the *velocity* and *c* the density $S\nabla(c\sigma)$ is the rate of increase of density or

$$\frac{\partial c}{\partial t} = S\nabla(c\sigma). \tag{X1}$$

For these reasons Clerk Maxwell called $S\nabla\sigma$ the convergence of the vector σ .†

(20.) Now we may choose the small surface to be any surface we please. We shall take it to be a portion of a tube of flow according to the hydrodynamical analogy, or we shall suppose that the vectors σ are tangential to its sides and normal to its ends. The integral vanishes consequently except over the ends and

$$S\nabla\sigma = -\frac{1}{v}\int Tdv T\sigma \qquad (xli)$$

the integral being taken over the two ends.

The areas of the ends being small and the distance between them small we have ultimately

$$S\nabla\sigma = -\lim_{t \to \infty} \frac{\mathcal{A}dT\sigma + d\mathcal{A}T\sigma}{\mathcal{A}dl} = -\lim_{t \to \infty} \left(\frac{dT\sigma}{dl} + \frac{T\sigma}{\mathcal{A}}\frac{d\mathcal{A}}{dl}\right) = -\frac{1}{T\sigma}\lim_{t \to \infty} \frac{d\log_{t}\mathcal{A}T\sigma}{dl} \quad (xlii)$$

^{*} dv being outwards, Sdvo is $- TdvT\sigma \cos \theta$ if θ is the angle between the normal dv and σ .

⁺ Electricity and Magnetism, Art. 25.

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 \mathcal{A} being the mean area of a normal section and dl the length of the tube. S $\nabla \sigma$ is thus equal to the rate of diminution of T σ along a line of flow together with the rate of contraction of the normal cross-section multiplied by T σ . This is the interpretation of the transformation

$$S\nabla \sigma = SU\sigma_0 \nabla \cdot T\sigma + T\sigma_0 S \nabla U\sigma \qquad (xliii)$$

in which the suffixes denote that the marked symbol is not to be operated on by ∇ . We notice moreover that if a is any constant vector

$$S\nabla\sigma = SU(\sigma_0 - a)\nabla \cdot T(\sigma - a) + T(\sigma_0 - a)S\nabla U(\sigma - a).$$
 (xliv)

The property (xxxix) remains true if any constant velocity is added to the velocities existing.

(21.) As regards the vector part of $\nabla \sigma$ we have seen that

$$\nabla \nabla \sigma = lim. \frac{1}{v} \int \nabla dv \sigma \qquad (x lv)$$

depends only on the tangential components of σ turned through a right angle round the normal. We may indeed find interpretations of this surface integral taken over an arbitrary surface, but none are satisfactory until we choose a surface presenting a definite direction upon which to fix the attention. For instance for a sphere we find

$$\nabla \nabla \sigma = \lim_{\nu \to \tau} \int \nabla \tau \sigma T d\nu \qquad (xlvi)$$

showing that the vector is the integrated moment of σ about the centre divided by the product of radius and volume. But when we select a small portion of a cylinder whose sides have a fixed direction a and whose ends are normal, we obtain results easily interpretable. Let $d\mathcal{A}$ be an element of the small cross-section, dl an element of a generator, $d\tau$ a tangential vector on the curved boundary forming with a and $d\nu$ a mutually rectangular system so that $d\tau$, a, $d\nu$ are in positive order.* Then over the curved boundary $d\nu = dlVd\tau a$ and over the plane faces $d\nu = \pm ad\mathcal{A}$. Thus

$$\nabla \nabla \sigma = \lim \frac{1}{\mathcal{A}l} \left(\int dl \nabla . \nabla d\tau a \cdot \sigma + \int \nabla a (\sigma_2 - \sigma_1) d\mathcal{A} \right).$$
 (xlvii)

Taking *l* so small that it may be integrated by itself in the first integral, we may replace $\sigma_2 - \sigma_1$ in the second by $-l \operatorname{Sa} \nabla \cdot \sigma$.

The expression (xliv) reduces consequently to

$$\nabla \nabla \sigma = \lim_{A} \frac{1}{A} \left(\int \nabla . \nabla d\tau a \cdot \sigma - \int \nabla a \cdot Sa \nabla \cdot \sigma dA \right).$$
 (xlviii)

* That is rotation round $d\tau$ from a to $d\nu$ is positive.

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It may be further transformed since

$$\nabla \nabla d\tau a$$
, $\sigma = -aSd\tau\sigma + d\tau Sa\sigma = -aSd\tau\sigma - VaVd\tau\sigma$

because a is at right angles to every $d\tau$; thus

$$\nabla \nabla \sigma = - \lim_{A} \frac{1}{A} \left(a \int S d\tau \sigma + \nabla a \left(\int V d\tau \sigma + \int S a \nabla \cdot \sigma dA \right) \right)$$
(xlix)

which gives separately

$$\operatorname{SaV}\nabla\sigma = \lim \, \frac{1}{\mathcal{A}} \int \operatorname{Sd}\tau\sigma \, ; \, \operatorname{VaV}\nabla\sigma = -\lim \, \frac{1}{\mathcal{A}} \, \operatorname{aVa}(\int \operatorname{Vd}\tau\sigma + \int \operatorname{Sa}\nabla \, . \, \sigma \mathrm{d}\mathcal{A}).$$
(1)

As we give an independent and superior method of obtaining analogous results in the next section we shall not consider the interpretation of these until section (23.).

(22.) The transformation of the last section suggests the investigation of line integrals $\int d\rho q$. Take a small parallelogram, centre at ρ and edges $d\rho$, $d'\rho$, and circuit it in the order from $d\rho$ to $d'\rho$. In this order the vector sides are $+ d\rho$, $+ d'\rho$, $-d\rho$, $-d'\rho$ and the corresponding vectors from the centre to their middle points are $-\frac{1}{2}d'\rho$, $+\frac{1}{2}d\rho$, so the four sides contribute in order

$$+ d\rho (q + \frac{1}{2} \mathrm{Sd}' \rho \nabla \cdot q), + d' \rho (q - \frac{1}{2} \mathrm{Sd} \rho \nabla \cdot q), - d\rho (q - \frac{1}{2} \mathrm{Sd}' \rho \nabla \cdot q), - d' \rho (q + \frac{1}{2} \mathrm{Sd} \rho \nabla \cdot q)$$
(li)

and the sum of these, which we may write

$$\int d\rho q = V d\nu \nabla \cdot q ; \tag{III}$$

where $d\nu = V d\rho d'\rho$ is the directed area of the parallelogram, because

$$d_{\rho}Sd'_{\rho}\nabla . - d'_{\rho}Sd_{\rho}\nabla . = V.Vd_{\rho}d'_{\rho} . \nabla.$$

Also rotation round dv in the direction of circuiting is positive, viz. from d ρ to d' ρ .

We shall prove that the same relation (lii) is true whatever be the shape of the small plane circuit. Conceive the small area divided arbitrarily into small parallelograms, and let each be circuited in the same direction and the sum taken. Any side common to two is traversed twice in opposite directions. If there is no discontinuity in q such a side contributes nothing for $d\rho q + (-d\rho)q = 0$. Hence only the bounding sides contribute and in the limit when these approach coincidence with the curve

$$\int \mathrm{d}\rho q = \int \mathrm{Vd}\nu \nabla \cdot q$$

the first integral being taken over the bounding curve and the second over the plane area. From this in the limit we recover (lii).

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(23.) When q is a vector (lii) affords the two equations true for any small plane circuit (compare (l))

$$\int \mathrm{Sd}\rho\sigma = \mathrm{Sd}\nu \nabla\nabla\sigma \tag{liii}$$

and

$$\int V d\rho \sigma = V. V d\nu \nabla \cdot \sigma.$$
 (liv)

The first shows that what we may call the circulation in any small circuit $(-\int Sd\rho\sigma)$ is equal to the product of the area into the component of $\nabla\nabla\sigma$ along the positive normal.^{*} We shall see in the case of fluid motion that $\nabla\nabla\sigma$ is twice the angular velocity of an element. Just as the rate of change of a scalar function in any direction is the component of ∇P in that direction so the circulation in any unit plane circuit is the component of $\nabla\nabla\sigma$ along its positive normal. The circuit normal to $U\nabla\sigma$ may be called the principal circuit, the circulation therein being a maximum.

(24.) If σ represents a distribution of force, by carrying a small unit mass round a circuit we gain from the forces an amount of work represented by $-\int S\sigma d\rho$ or $-Sd\nu V\nabla \sigma$. Hence the condition that the forces should be conservative, or that no work could be gained in carrying a small mass round any complete small circuit, is $V\nabla \sigma = 0$; or what is equivalent this is the condition that $\int Sd\rho\sigma$ should be integrable without a factor, the integral being taken between arbitrary limits. In fact the integral must be a function of the vectors ρ at the limits. We may therefore write

$$P = -\int_{\rho_0}^{\rho} S\sigma d\rho = f(\rho, \rho_0). \qquad (lv)$$

Whence $\nabla P = \sigma$, because as P is a function of ρ

$$\mathrm{d}P = -\mathrm{Sd}\rho\nabla P = -\mathrm{S}\sigma\mathrm{d}\rho$$

for all vectors $d\rho$. Thus the equation

$$\nabla \nabla \sigma = 0 \quad \text{implies} \quad \sigma = \nabla P \tag{1vi}$$

just as the latter implies the former (compare (xx)). A distribution of vectors satisfying this condition is said to be irrotational.

(25.) Introducing the symbol χ' to denote a linear and vector function, we write equation (liv) in the form

$$-\chi' d\nu = V. V d\nu \nabla \cdot \sigma = \int V d\rho \sigma.$$
 (lvii)

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^{*} For brevity let the normal to the circuit about which the positive rotation is the same as that of the circuit be called the *positive* normal.

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This function χ' and its conjugate may be expressed* by

$$\chi' a = -\nabla \nabla a \nabla \cdot \sigma = -a S \nabla \sigma + \nabla S a \sigma; \quad \chi a = -\nabla \nabla \nabla \sigma a = -a S \nabla \sigma + \sigma S a \nabla.$$
(lviii)

In fact χ is Hamilton's auxiliary function for ϕ or

$$\chi a = (m'' - \phi)a$$
 where $\phi a = -Sa\nabla \cdot \sigma$ (lix)

since $m'' = -S\nabla\sigma$ (compare (27.)).

When a unit electric current flows in the small circuit $-\chi' d\nu$ is the resultant mechanical force acting on the circuit provided σ is the magnetic induction due to extraneous causes.[†] We shall therefore in the most general case briefly term $-\chi' a$ the force on the circuit a.

The force on the circuit is normal or tangential to its plane according as a satisfies

$$Va\chi'a = 0$$
 or $Sa\chi'a = 0$. (lx)

The force on the circuit a has $S\beta\chi'a$ for its component along β and this is generally different from the component along a of the force on the circuit β because χ' is not self-conjugate. The spin-vector of χ is easily seen to be $-\frac{1}{2}V\nabla\sigma$ and whenever this vanishes the force on a has the same component along β as the force on β has along a.

In a steady magnetic field

$$\nabla \sigma = 0 \quad \text{or} \quad \sigma = -\nabla \Omega \tag{lxi}$$

where Ω is the magnetic potential and (lviii)

$$\chi' a = \chi a = \nabla S a \sigma = S a \nabla \cdot \sigma \qquad (1xii)$$

or the force is the rate of change of the induction (σ) along the normal.

(26.) As the last particular case we suppose q to be a scalar P, then for all small circuits

$$\int \mathrm{d}\rho P = \mathrm{V}\mathrm{d}\nu\nabla \cdot P. \tag{lxiii}$$

The most direct illustration of this formula seems to be to suppose P the magnetic potential of the field. The expression on the right with sign changed represents the couple on a small magnet whose magnetic moment is $d\nu$. As this can be expressed as a line integral round a circuit whose directed area is $d\nu$, the equation suggests the equivalence of the magnetic action due to a unit current in the circuit and that due to the magnet. It shows moreover that the couple acting on the circuit is the negative of the integral of its elements multiplied by the corresponding potentials P.

^{*} There can be no possible objection to placing ∇ after the operand σ in an equation of this kind (lviii) as no confusion is likely to arise.

[†] Clerk Maxwell, Electricity and Magnetism, Art. 490.

(27.) We shall now consider the linear vector function and its conjugate

$$\phi a = -Sa\nabla \cdot \sigma$$
 and $\phi' a = -\nabla Sa\sigma$ (lxiv)

of which an auxiliary function has occurred in (25.). It is only necessary to find expressions for its invariants and for the second auxiliary function ψ in terms of ∇ for its meaning has been fully investigated. In fact if σ is the strain-displacement of the extremity of $\dot{\rho}$, the displacement of a near point $(\rho + d\rho)$ is $\sigma + \phi d\rho$, so that $\phi d\rho$ is the displacement of this near point with respect to the point (ρ) . The strain being supposed small we have seen* that the molecular rotation of the element at (ρ) is $\epsilon = \frac{1}{2} \nabla \nabla \sigma$; also the dilatation is given by the first invariant $m'' = -S\nabla \sigma$. The pure part of the strain is due to

$$\Phi a = -\frac{1}{2} Sa \nabla \cdot \sigma - \frac{1}{2} \nabla Sa \sigma = \frac{1}{2} (\phi + \phi') a.$$
 (lxv)

Of course now, in contrast to the case treated in the Note cited, the strain is not homogeneous.

On account of the great importance of this function we shall prove these expressions for m'' and ϵ . For three arbitrary vectors

$$V\beta\gamma \cdot \phi a + V\gamma a \cdot \phi\beta + Va\beta \cdot \phi\gamma = -(V\beta\gamma Sa\nabla + V\gamma aS\beta\nabla + Va\beta S\gamma\nabla)\sigma.$$

Hence by (xiii) and the well-known expression for the invariant of ϕ

$$m'' - 2\epsilon = -\nabla\sigma. \tag{1xvi}$$

(28.) In forming the function ψ it is necessary to use temporary marks to distinguish the corresponding operator and operand.

We write therefore

$$\psi \nabla a\beta = \nabla \phi' a \phi' \beta = \nabla \nabla S a \sigma \cdot \nabla' S \beta \sigma' = \nabla \nabla \nabla' S a \sigma S \beta \sigma'.$$

Now we may write equally well

$$\psi V a \beta = V \nabla' S a \sigma' \cdot \nabla S \beta \sigma = - V \nabla \nabla' S a \sigma' S \beta \sigma.$$

So that treating ∇ , ∇' , σ , and σ' as four distinct vectors we obtain on addition of these two forms

$$\psi \gamma = -\frac{1}{2} \nabla \nabla' S \nabla \sigma \sigma' \gamma. \qquad (lxvii)$$

* Note on Strain, sections (16.) and (17.), p. 372.

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The accents may be removed when but not till when the operations indicated have been performed.* Just as in (lxvi)

$$m' - 2\phi\epsilon = -\frac{1}{2}\nabla\nabla\nabla'$$
. $\nabla\sigma\sigma'$ (lxviii)

and this result should be compared with the former and the expressions for the vectors verified. It is also a useful exercise to verify that the third invariant is

$$m = \frac{1}{6} S \nabla \nabla' \nabla'' S \sigma \sigma' \sigma''. \tag{lxix}$$

(29.) Instead of retaining only the first term in the expansion we may, for the particular case in which q is a function of ρ , write Hamilton's expression for Taylor's series in the form[†]

$$q_{a} = e^{\mathbf{d}}q = e^{-\operatorname{Sa}\nabla}q = q - \operatorname{Sa}\nabla \cdot q + \frac{1}{2}(\operatorname{Sa}\nabla)^{2}q - \&e.$$
 (lxx)

Here as there is no danger of confusion we need not accent or distinguish the several operators there being but one operand.

If the quaternion q_a is associated with each element of mass dm of a body

$$\int q_a \mathrm{d}m = qM - \mathrm{Sa}_0 \nabla \cdot qM - \frac{1}{2} \left(\frac{1}{2} (A + B + C) \nabla^2 - \mathrm{S} \nabla \Phi \nabla \right) \cdot q + \&c. \quad (\mathrm{Ixxi})$$

where a_0 is the vector to the centre of mass; \mathcal{A} , B, and C the principal moments and Φ the momentum function of the body with respect to the origin.[‡] To prove this it is only necessary to observe that $(Sa\nabla)^2 = a^2\nabla^2 + (Va\nabla)^2$ and to employ the notation explained in the note on page 291.

In like manner

$$\int aq_a \mathrm{d}m = a_0 q M + \frac{1}{2} (A + B + C) \nabla q - \Phi \nabla \cdot q. \qquad (\mathrm{lxxii})$$

From (lxxi) we obtain Clerk Maxwell's expression for the mean value of q throughout a sphere when we put $\Phi = A = B = C$ and $a_0 = 0$.

* A device precisely similar is used in Aronhold's symbolic method of denoting a quantic by $a_x^n = 0$, $b_x^n = 0$, &c. The Hessian of a quantic is represented by

$$\Delta = n^2(n-1)^2 a_1 b_2(ab) a_x^{n-2} b_x^{n-2} = \frac{1}{2} n^2(n-1)^2 (ab)^2 a_x^{n-2} b_x^{n-2}$$

where $(ab) = a_1b_2 - a_2b_1$. (Compare Clebsch, Vorlesungen über Geometrie, p. 191, Leipzig, 1876.)

⁺ See p. 473, vol. i., and the second Note to p. 20 in the present volume. It is undoubtedly strange that Hamilton has deliberately avoided the employment of the symbol ∇ in the *Elements*. We have seen several times in the course of this Note that our results are mercly translations into this notation of investigations in which ∇ was not explicitly employed (comp. sections (2.), (5.), (27.)). He even introduces a new notation (see p. 294 and section (5.)) when ∇ was ready to his hand. The key to this neglect of ∇ seems to be contained in Art. 422, (92.), p. 351.

 $\ddagger + \Phi \omega$ is the angular momentum of the body (comp. p. 291) spinning with angular velocity ω . Hamilton uses a negative sign.

If the body is subject to the attraction of matter having a potential P we find for the force and couple at the centre of mass

$$\lambda = M\nabla P + \frac{1}{2}S\nabla\Phi\nabla \cdot \nabla P, \quad \mu = -\nabla\Phi\nabla \cdot \nabla P. \quad (\text{lxxiii})$$

Hence it is not hard to deduce, using the examples in section (10.), when $P = \int \mathbf{T}(\alpha - \alpha')^{-1} dm'$ that

$$\lambda = -M \int \beta r^{-3} \mathrm{d}m' - 3 \int ((A + B + C)\beta + 2\Phi\beta - 5\beta S\beta^{-1}\Phi\beta)r^{-5} \mathrm{d}m'$$
$$\mu = -3 \int V\beta^{-1}\Phi\beta r^{-3} \mathrm{d}m' \qquad (1xxiv)$$

and

where for brevity $\beta = \alpha - \alpha'$ and $r = T\beta$.

(30.) It is not necessary to examine in any detail the extension of the integrations of sections (14.) and (15.) to finite regions because the method is almost precisely the same as in the case of scalar integrals. If (I.) there is no discontinuity in the quaternion q, if (II.) it is single-valued and (III.) does not become infinite at any point of the region, if moreover (IV.) the region is simply-connected, we can fill it. with small parallelepipeds in any way we please and since over an interface the aspects of the corresponding directed elements of the adjoining parallelepipeds are opposed the interfaces contribute nothing. In the limit therefore when the conditions I., II., III., and IV. are satisfied, the volume integral equals the surface integral or

$$\int \nabla q \, \mathrm{d} v = \int \mathrm{d} v q. \qquad (1 \mathbf{x} \mathbf{x} \mathbf{v}) \cdot$$

(31.) I. When there is a surface of discontinuity suppose the region divided into two by that surface and apply the equation (lxxv) separately to each region and add. Then

$$\int \nabla q \mathrm{d} \boldsymbol{v} = \int \mathrm{d} \boldsymbol{v} q + \int \mathrm{d} \boldsymbol{v}_{12} (q_1 - q_2) \tag{1xxvi}$$

when over the surface of discontinuity an element affords the parts

$$dv_{12}q_1$$
 and $dv_{21}q_2$ or $dv_{12}(q_1 - q_2)$.

(32.) II. If q is not single-valued by reasoning almost precisely similar to that of Clerk Maxwell^{*} we can see when infinite values of ∇q are excluded from the region that assuming the value of q at any one point its value at every other point is determinate. In fact starting from a point Λ with a given value of q we can return to it with a different value only if we thread some circuit along which q is indeterminate; and if q is indeterminate anywhere in the region its corresponding deriveds must be infinite. In the case in which a circuit locus of indeterminate values of q exists in the region, we may enclose it in a tube but the region then becomes multiply-connected (IV.).

* Electricity and Magnetism, Art. 96 (b).

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(33.) III. If q becomes infinite at any point, we exclude that point by a small sphere and include the surface integral over the sphere in the result. Taking for the moment the origin at the point and writing $T_{\rho} = r$ let

$$q = q_0 + \frac{f_1 \mathbf{U}\rho}{r} + \frac{f_2 \mathbf{U}\rho}{r^2} + \frac{f_3 \mathbf{U}\rho}{r^3} + \&c. \qquad (\text{lxxvii})$$

Then if $d\Omega$ is an element of solid angle the integral over the sphere is

$$-\int \mathrm{d}\nu q = \int \mathrm{d}\Omega \cdot \mathbf{U}\rho r^2 \left(q_0 + \frac{f_1\mathbf{U}\rho}{r} + \frac{f_2\mathbf{U}\rho}{r^2} + \&c. \right)$$

This in general is ultimately infinite or indeterminate if $f_3 U \rho$, &c. are not zero. Excluding these cases, in the limit

$$-\int \mathrm{d}\boldsymbol{\nu}\boldsymbol{q} = \int \mathrm{d}\Omega \mathbf{U}\rho f_2 \mathbf{U}\rho.$$

We need only consider the case in which $f_2 U \rho$ is a linear function^{*} of $U \rho$, and we may take it to be

$$f_2 U \rho = S \eta' U \rho + \Sigma \lambda S \mu U \rho = S \eta' U \rho + \phi U \rho. \qquad (lxxviii)$$

It is easy to see in various ways (compare for instance (29.)) that

$$\int d\Omega U \rho Sa U \rho = -\frac{4}{3}\pi a \quad \text{and} \quad \int d\Omega U \rho f_2 U \rho = -\frac{4}{3}\pi (\eta' + \Sigma \mu \lambda).$$

Hence (lxxv) becomes modified by the infinite point into

$$\int \nabla q \, \mathrm{d}v = \int \mathrm{d}v q + \frac{4}{3}\pi (\eta' + m'' - 2\epsilon) \qquad (1 \mathrm{xxix})$$

if a term $r^{-2}f U\rho$ occurs in q, the part of $f U\rho$ linear in $U\rho$ being $S\eta' U\rho + \phi U\rho$.

(34.) IV. If the region is multiply-connected we render it simply connected by drawing diaphragms when we fall back on case I. if q is many valued. A diaphragm corresponds to a surface of discontinuity and $q_1 - q_2 = np$ where p is the cyclic increment of q and n an integer.

(35.) In order to extend the integrations of section (22.) to any closed curve directly we must be able to connect all points of the curve by a continuous net of small parallelograms for each of which q must be (I.) continuous, (II.) single-valued and (III.) without infinite differentials. Then because a common side is traversed in opposite directions

$$\int d\rho q = \int V d\nu \nabla \cdot q \qquad (lxxx)$$

where the line integral is over the curve and the surface with which the net ultimately coincides. Under these conditions the surface integral extended to a closed surface is always zero.

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^{*} By an application of a well-known theorem in spherical harmonics (72.).

(I.) In the case of discontinuity as in (31.) we take an arbitrary curve on the surface of discontinuity and when this curve is *specified* we have on adding the results for the two circuits

$$\int d\rho q + \int d\rho_{12}(q_1 - q_2) = \int V d\nu \nabla \cdot q \qquad (1xxxi)$$

where the second integral on the left is taken over the specified curve on the surface of discontinuity. Let this curve be ACB terminating on the given circuit at A and B. Draw any other curve ADB, then letting the accented line integral refer to this curve and the second surface integral to the portion DBCA of the surface of discontinuity

$$\int d\rho q + \int' d\rho_{12}(q_1 - q_2) = \int V d\nu \nabla \cdot q + \int V d\nu_{12}(q_1 - q_2) \qquad (lxxxii)$$

provided the portion of the surface of discontinuity can be covered with a continuous net. Applying (lxxx) to the surface of discontinuity it is evident we get the same value for $\int d\rho q$ in both cases.

(II.) If q is not single-valued over the continuous net, its value is definite if a definite value is chosen at some one point of the net, or else q is indeterminate at a point of the net and as a consequence its differential may become infinite (III.). This point may be surrounded by a small curve joined by a barrier to the given circuit, and the barrier must then be treated as a line of discontinuity and the value of the integral round the closed curve must be taken account of.

(36.) We shall not delay to prove the more general relations

$$\int f \mathrm{d}\nu = \int f \,\nabla \mathrm{d}\nu \,; \quad \int F \mathrm{d}\rho = \int F \,\nabla \mathrm{d}\nu \nabla \qquad (\mathrm{lxxxiii})$$

where f and F are linear functions and where ∇ operates on them in situ in the two expressions $f\nabla$ and $F' V d_{\nu} \nabla$. They may be proved exactly as in the simpler case when we have to do only with a quaternion multiplier; in fact $f' V d' \rho d'' \rho$ at the extremity of ρ becomes

$$(1 - \frac{1}{2} \mathrm{Sd}\rho \nabla) f \mathrm{Vd'}\rho \mathrm{d''}\rho$$
 or $f(1 - \frac{1}{2} \mathrm{Sd}\rho \nabla) \cdot \mathrm{Vd'}\rho \mathrm{d''}\rho$

at the extremity of $\rho + \frac{1}{2}d\rho$ it being understood that ∇ operates on the constituents of f alone. We may remark that the symbol of taking the conjugate K may be applied to the integrals (lxxx) or (lxxv).

(37.) Let the quaternion p or p_{ω} be the value of the integral

$$p = \int_{-\infty}^{\infty} \mathbf{T} (\rho - \omega)^{-1} q \mathrm{d}v \qquad (\mathrm{lxxxiv})$$

at the extremity of the vector ω , ρ being now the vector variable in the integration which is extended throughout all space or at least everywhere that q is not zero. We suppose q is never infinite and has never infinite differentials corresponding to THE OPERATOR ∇ .

finite differentials of ρ . Considering separately the parts of the integral inside and outside a small sphere, centre ω , we have on operating by ∇_{ω}^2

$$\nabla_{\omega}^{2} p = \nabla_{\omega}^{2} \int' \mathbf{T} (\rho - \omega)^{-1} q \mathrm{d} v \qquad (1 \mathrm{xxxv})$$

where the accent denotes that the integration is confined to the interior of the sphere for by 9(f), $\nabla_{\omega}^{2}T(\rho - \omega)^{-1} = 0$ wherever ω does not coincide with ρ . The sphere may be taken so small that q is sensibly constant within it. q may thus be removed outside the sign of integration and

$$\nabla_{\omega}^{2} p = \nabla_{\omega}^{2} \int T (\rho - \omega)^{-1} \mathrm{d}v \cdot q_{\omega} = 4\pi q_{\omega} \qquad (\mathrm{lxxxvi})$$

because by Poisson's theorem (compare (xx))

$$\nabla_{\boldsymbol{\omega}^2} \int T(\rho - \boldsymbol{\omega})^{-1} \mathrm{d}\boldsymbol{v} = 4\boldsymbol{\pi}.$$

(38.) From these results we infer conversely if two quaternions p and q are connected by the equation

$$q = \nabla^2 p \qquad (lxxxvii)$$

that

$$p = p_{\omega} = (4\pi)^{-1} \int^{\infty} \mathbf{T} (\rho - \omega)^{-1} q \mathrm{d}v \qquad (\mathrm{lxxxviii})$$

the integration being extended throughout all space or wherever q is not zero, and we may regard this expression as the equivalent of the inverse operation in the equation

$$p = \nabla^{-2}q. \qquad (1xxxix)$$

On this supposition the operator ∇^{-2} presents no ambiguity.

(39.) The difference between $\nabla^{-2}q$ or the integral (lxxxviii) taken over an unlimited field and the same integral taken throughout a circumscribed region may by Green's theorem be expressed as a surface integral over the boundary of the region. The extremity of ω being within this region we have by (33.) when the volume integral is taken in the limited region outside the small sphere, the first surface integral over the boundary and the accented integral over the surface of the sphere,

$$\int \nabla \cdot (\mathbf{T}(\rho - \omega)^{-1} \nabla p) \mathrm{d}v = \int \mathrm{d}\nu \mathbf{T}(\rho - \omega)^{-1} \cdot \nabla p + \int' \mathrm{d}\nu \mathbf{T}(\rho - \omega)^{-1} \cdot \nabla p \qquad (\mathrm{xe})$$

and also by (36.)

$$\int \nabla \mathbf{T}(\rho - \omega)^{-1} (\nabla) p \, \mathrm{d}v = \int \nabla \mathbf{T}(\rho - \omega)^{-1} \cdot \mathrm{d}v p + \int' \nabla \mathbf{T}(\rho - \omega)^{-1} \cdot \mathrm{d}v p.$$
(xei)

In the volume integral (xc) the first operator ∇ operates on all that follows it (except dv) and in the second the bracketed (∇) operates in situ upon p and also upon $\nabla T(\rho - \omega)^{-1}$.

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The surface integral over the sphere in (xc) vanishes; that in (xci) (comp. (3. (g)) and (33.)) becomes*

$$-\int' \mathrm{d}\Omega p = -4\pi p \text{ because } \mathrm{d}\nu = -\mathrm{U}(\rho-\omega)r^2\mathrm{d}\Omega \text{ and } \nabla\mathrm{T}(\rho-\omega)^{-1} = -\mathrm{U}(\rho-\omega)\mathrm{T}(\rho-\omega)^{-2}.$$

Also the term in the first volume integral is

$$\nabla \cdot (\mathbf{T}(\rho-\omega)^{-1}\nabla p) = \nabla \mathbf{T}(\rho-\omega)^{-1} \cdot \nabla p + \mathbf{T}(\rho-\omega)^{-1} \cdot \nabla^2 p \qquad (\mathbf{x}\mathrm{cii})$$

and that in the second is

$$\nabla \mathrm{T}(\rho-\omega)^{-1}(\nabla)p = \nabla \mathrm{T}(\rho-\omega)^{-1} \cdot \nabla p + \nabla^{2} \mathrm{T}(\rho-\omega)^{-1} \cdot p, \qquad (\mathrm{xeiii})$$

for it is easy to prove† that $\nabla T(\rho - \omega)^{-1} \nabla = \nabla^2 T(\rho - \omega)^{-1}$. Moreover this part vanishes since ω is not included in the limited field.

By these considerations (xc) and (xci) reduce to

$$\int (\nabla T(\rho - \omega)^{-1} \cdot \nabla p + T(\rho - \omega)^{-1} \cdot \nabla^2 p) dv = \int d\nu T(\rho - \omega)^{-1} \cdot \nabla p \qquad (xciv)$$

$$\int \nabla T(\rho - \omega)^{-1} \cdot \nabla p dv = \int \nabla T(\rho - \omega)^{-1} \cdot d\nu p - 4\pi p \qquad (xcv)$$

so that on subtraction

$$\int \mathbf{T}(\rho-\omega)^{-1} \cdot \nabla^2 p \mathrm{d}v - 4\pi p = \int \mathrm{d}v \mathbf{T}(\rho-\omega)^{-1} \cdot \nabla p - \int \nabla \mathbf{T}(\rho-\omega)^{-1} \cdot \mathrm{d}v p. \quad (\mathrm{xevi})$$

Or if we suppose p and q connected by the equation (lxxxvii) or (lxxxix)

$$\frac{1}{4\pi}\int \mathcal{T}(\rho-\omega)^{-1}q\,\mathrm{d}v = \nabla^{-2}q + \frac{1}{4\pi}\int \mathrm{d}\nu \mathcal{T}(\rho-\omega)^{-1} \cdot \nabla \cdot \nabla^{-2}q - \int \nabla \mathcal{T}(\rho-\omega)^{-1} \cdot \mathrm{d}\nu \cdot \nabla^{-2}q \cdot (\mathrm{xevii})$$

Thus the difference of the integral over a limited and unlimited field (lxxxviii) has been expressed as a surface integral over the boundary of the former.

(40.) We have seen (lxxxv) that when we operate with ∇_{ω}^2 on a potential function it is only necessary to take account of the element at which ρ and ω coincide. Provided therefore we introduce surface integrals wherever necessary we may limit the field of integration and write generally for all points within that field

$$q = \nabla_{\omega}^{2} \int \frac{q \mathrm{d}v}{4\pi \mathrm{T}(\rho - \omega)} \,. \tag{xeviii}$$

By the associative principle we deduce

 $4\pi q = \nabla_{\omega} \cdot \nabla_{\omega} \int \mathbf{T}(\rho - \omega)^{-1} q dv = \nabla_{\omega} \mathbf{S} \nabla_{\omega} \int \mathbf{T}(\rho - \omega)^{-1} q dv + \nabla_{\omega} \mathbf{V} \nabla_{\omega} \int \mathbf{T}(\rho - \omega)^{-1} q dv. \quad (\mathbf{xcix})$ Hence any quaternion may be expressed as the result of operating by ∇ on another

> * Hence another proof of (lxxxvi). † In fact $\rho \nabla = \nabla \rho = -3$.

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vector; or generally

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quaternion (Q) or as the sum of the results of operating by ∇ on a scalar and on a

 $q = \nabla Q. \tag{c}$

(41.) We shall transform this new quaternion Q so as to exhibit more clearly its relation to q. Integrating through the limited field and excluding the small sphere round (ω),

$$\int \nabla \mathbf{T}(\rho - \omega)^{-1} \cdot q \mathrm{d}v + \int \mathbf{T}(\rho - \omega)^{-1} \cdot \nabla q \mathrm{d}v = \int \nabla \cdot \mathbf{T}(\rho - \omega)^{-1} q \mathrm{d}v = \int \mathrm{d}\nu \mathbf{T}(\rho - \omega)^{-1} q \quad (\mathrm{ci})$$

the surface integral being taken over the boundary of the field (40.) and the surface integral over the small sphere being omitted as it ultimately vanishes (33.). Now $(\nabla + \nabla_{\omega}) T(\rho - \omega)^{-1} = 0$,

$$0 \qquad 4\pi Q = \nabla_{\omega} \int \mathcal{T}(\rho - \omega)^{-1} q \mathrm{d}v = \int \mathcal{T}(\rho - \omega)^{-1} \cdot \nabla q \mathrm{d}v - \int \mathcal{T}(\rho - \omega)^{-1} \mathrm{d}\nu q.$$
(cii)

The surface integral here disappears when the field of integration is unlimited.

(42.) This transformation is of importance in vortex motion for example.

Considering more particularly the vector part of the volume integral (cii), we have by section (20.) (xlii),

$$\nabla^2 Sq = S\nabla \nabla \nabla q = -\frac{1}{T\nabla \nabla q} \cdot lim \cdot \frac{d \log (dA \cdot T\nabla \nabla q)}{dl}$$
(ciii)

 $d\mathcal{A}$ being the small area of a cross-section of a tube formed by the vectors $\nabla \nabla q$ and dl an element of the length of the tube. Using the relation

 $T\xi \cdot dA = dm \quad \text{where} \quad \xi = V\nabla Vq \quad (\text{civ})$

and where dm is the *strength*^{*} of the tube of vectors ξ we have

$$\int \mathbf{T}(\rho-\omega)^{-1} \cdot \xi \mathrm{d}v = \int \mathbf{T}(\rho-\omega)^{-1} \cdot \mathbf{U}\xi \mathrm{d}l \mathrm{d}m = \int \mathbf{T}(\rho-\omega)^{-1} \mathrm{d}\rho \mathrm{d}m \qquad (\mathrm{cv})$$

if $d\rho = U\xi$. dl is a directed element along the tube because dv = dAdl.

(43.) For the case in which the tubes (ξ) are re-entrant and included within the limits of integration the integral on the right may be regarded as the sum of a number of integrals taken round closed curves. If then we describe any surface through one of these curves so that it does not pass through the extremity of ω , by (lxxxiii)

$$\int \nabla T(\rho - \omega)^{-1} \cdot d\rho = \int \nabla T(\rho - \omega)^{-1} \cdot V d\nu \nabla = \int \nabla S d\nu \nabla T(\rho - \omega)^{-1}$$
(cvi)

* Lamb, Hydrodynamics, p. 223, Cambridge, 1895.

because as $\nabla^2 T(\rho - \omega)^{-1} = 0$, the term involving ∇^2 in the expansion $\nabla . V d\nu \nabla = \nabla S d\nu \nabla - d\nu \nabla^2$ disappears. Again we may replace the equation (evi) by

$$\nabla_{\omega} \int \mathrm{T}(\rho - \omega)^{-1} \cdot \mathrm{d}\rho = -\int \nabla \mathrm{Sd}\nu \nabla \mathrm{T}(\rho - \omega)^{-1} = -\nabla_{\omega} \int \mathrm{Sd}\nu \mathrm{U}(\rho - \omega) \mathrm{T}(\rho - \omega)^{-2} \quad (\mathrm{cvii})$$

and if we suppose the surface built up of elementary cones through the extremity of the vector ω , it is evident that the cross-sections of these cones alone contribute so that we may replace $d\nu$ by $U(\rho - \omega) T(\rho - \omega)^2 d\Omega$ and finally*

$$\nabla_{\boldsymbol{\omega}} \int \mathbf{T}(\boldsymbol{\rho} - \boldsymbol{\omega})^{-1} \, d\boldsymbol{\rho} = \nabla_{\boldsymbol{\omega}} \int d\boldsymbol{\Omega} = \nabla_{\boldsymbol{\omega}} \boldsymbol{\Omega} \tag{cviii}$$

where Ω is the solid angle subtended by the re-entrant tube at the extremity of ω . Thus if none of the circuits pass through the extremity of ω

$$\nabla_{\omega} \int \mathbf{T}(\rho - \omega)^{-1} \cdot \xi dv = \nabla_{\omega} \int \Omega dm.$$
 (cix)

(44.) To illustrate the use of the operator we shall briefly consider the equations of motion of a continuous distribution of matter. Directing the attention to any selected portion its momentum is

$$M\sigma = \int \dot{\rho} dm \qquad (cx)$$

 σ being the velocity of the centre of mass, dm an element moving with velocity $\dot{\rho}$ and M the mass of the portion. If λ is the resultant force acting on the mass it is equal to the rate of change of momentum, or

$$D_t \sigma = M^{-1} \lambda. \qquad (exi)$$

We may evidently suppose the selected portion of such a size that the velocity of its centre of mass approaches indefinitely the velocity of the matter about that point. Again taking moments about the centre of mass we may write

$$\mathbf{D}_{i} \int \mathbf{V}(\rho - \rho_{0}) \left(\dot{\rho} - \dot{\rho}_{0}\right) \mathrm{d}m = \mu + \int \mathbf{V}(\rho - \rho_{0}) \mathrm{d}\lambda \qquad (\mathrm{exii})$$

where μ is the resultant couple arising from other causes than the force-couple $\int V(\rho - \rho_0) d\lambda$.

(45.) We shall now consider the transformations of the vector of acceleration $D_t \sigma$ (exi). If we regard τ as a function of ρ and t we have (xi) its total differential expressed by

$$\mathbf{D}\boldsymbol{\sigma} = \frac{\partial \boldsymbol{\sigma}}{\partial t} \,\mathrm{d}t - \mathrm{Sd}\boldsymbol{\rho}\nabla \,\boldsymbol{.}\,\boldsymbol{\sigma} \tag{cxiii}$$

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^{*} Hence the result of operating by ∇ on a vector of a certain kind is equivalent to the result of operating on a scalar.

⁺ Of course on the supposition made in the last section the vectors σ and $\dot{\rho}$ are identical.

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the partial derived with respect to the time being $\frac{\partial \sigma}{\partial t}$, or in other words $\frac{\partial \sigma}{\partial t}$ being the rate at which the vector σ corresponding to a point fixed in space is changing. But $\mathbf{D}_{t}\sigma$ is the rate at which the vector σ as corresponding to a definite portion of the matter is changing. So when we follow the motion of the matter, $d\rho = \sigma dt$ and

$$\mathbf{D}_t \boldsymbol{\sigma} = \frac{\partial \boldsymbol{\sigma}}{\partial t} - \mathbf{S} \boldsymbol{\sigma} \nabla \cdot \boldsymbol{\sigma} = \boldsymbol{M}^{-1} \boldsymbol{\lambda} \qquad (\text{exiv})$$

in which ∇ of course operates only on the σ to the right. In this case the appropriate form of the equation of continuity is (xl) if c is the density

$$\frac{\partial c}{\partial t} = S\nabla(c\sigma). \tag{cxv}$$

(46.) On the other hand if in Lagrange's method we suppose ρ to be a function of t and of three parameters u, v, and w which individualize any element of matter the velocity and acceleration of the centre of mass may be represented simply by $\dot{\rho}$ and $\ddot{\rho}$, the partial deriveds of ρ with respect to the time, and the equation of motion is

$$\ddot{\rho} = M^{-1}\lambda.$$
 (cxvi)

Also the appropriate form of the equation of continuity is

$$cS\rho_1\rho_2\rho_3 = const. = -C$$
 (cxvii)

which expresses that the mass $\pm c S \rho_1 \rho_2 \rho_3 du dv dw$ of a small definite parallelepiped of the matter does not vary, ρ_1 , ρ_2 , and ρ_3 being the deriveds of ρ with respect to u, v, and w.

(47.) It is easy to derive (cxvii) from (cxv) for remembering the meaning of the fluxional notation*

$$\dot{c} = \frac{\partial c}{\partial t} - S\sigma \nabla . \ c = c S \nabla \sigma = c S \nabla \dot{\rho}.$$
 (cxviii)

But exactly as in section (12.), when ρ is expressed in terms of three parameters u, v, and w, the appropriate form of ∇ derived from (xiii) by taking

$$d\rho = \rho_1 du, \quad d'\rho = \rho_2 dv, \quad and \quad d''\rho = \rho_8 dw$$
 (exix)

$$\nabla = -\frac{1}{\mathrm{S}\rho_{1}\rho_{2}\rho_{3}} \cdot \left(\nabla \rho_{2}\rho_{3} \frac{\partial}{\partial u} + \nabla \rho_{3}\rho_{1} \frac{\partial}{\partial v} + \nabla \rho_{1}\rho_{2} \frac{\partial}{\partial w} \right) \cdot \qquad (\mathrm{cxx})$$

Hence evidently

is

$$\frac{\mathrm{d}}{\mathrm{d}t}\log c = \mathrm{S}\nabla\dot{\rho} = -\frac{\mathrm{d}}{\mathrm{d}t}\log \mathrm{S}\rho_1\rho_2\rho_3 \qquad (\mathrm{exxi})$$

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^{*} As an exercise one may verify that $S\dot{\nabla}\rho = -S\nabla\dot{\rho}$.

where the differentiations have the same meaning as the fluxional notation which is not here convenient for printing.

(48.) As regards the forces acting on the element, we have in the first place bodily or external forces ξ acting at each point and generally specified with respect to unit of volume. These contribute the volume integral $\int c\xi dv$.

In the second place there are the forces due to the interaction of the parts of the substance. Their resultant is suitably represented by a surface integral $\int \Phi d\nu$ where $\Phi d\nu + \Phi(-d\nu) = 0$ because the interaction across a directed element from one side is balanced by that on the other, and where $\Phi d\nu = \Phi U d\nu$. Td ν because the force is ultimately proportional to the area. Thus (cxi) becomes

$$\mathbf{D}_{i}\sigma = M^{-1} \int c\xi \mathrm{d}v + M^{-1} \int \Phi \mathrm{d}v = M^{-1} \int c\xi \mathrm{d}v + M^{-1} \int \Phi_{0} \mathrm{d}v - M^{-1} \int \mathbf{S}\tau \nabla \cdot \Phi_{0} \mathrm{d}v \quad (\mathrm{cxxii})$$

 Φ_0 being what the function Φ becomes at the origin of the small vectors τ (16.) which may for convenience be taken centrally within the element. The integral $\int \Phi_0 d\nu$ must vanish as it is only of the second order in the linear dimensions of the element while the others are of the third order. Hence Φ (or Φ_0) must be a linear and distributive function for $\Sigma \Phi_0 d\nu = 0$ whenever $\Sigma d\nu = 0.*$ And therefore by an application of the integration theorem (lxxxiii) because Φ is distributive and linear.

$$\int \Phi d\nu = \int \Phi \nabla \cdot dv. \qquad (cxxiii)$$

From this (cxxii) gives when the element is very small

$$\mathsf{D}_t \sigma = \xi + c^{-1} \cdot \Phi \nabla \qquad (\mathrm{exxiv})$$

(where ∇ operates on Φ in situ) for ultimately M = c dv.

(49.) Again we may write the couple equation (cxii) in the form

$$\int V\tau \dot{\tau} dm = \int V\tau \xi dm + \int \eta dm + \int V\tau \Phi d\nu \qquad (exxv)$$

where the origin of vectors τ is at the centre of mass and where η is the voluminal distribution of impressed couple. By the principle of linear dimensions employed in the last section we must have separately

$$\int \eta \mathrm{d}m + \int \nabla \tau \Phi_0 \mathrm{d}\nu = 0 \qquad (\mathrm{cxxvi})$$

or ultimately if we take the element to be a small parallelepiped whose sides are parallel to α , β , γ ,

$$\eta c Sa\beta\gamma + Va\Phi_0 V\beta\gamma + V\beta\Phi_0 V\gamma a + V\gamma\Phi_0 Va\beta = 0 \qquad (\text{exxvii})$$

or simply

$$\eta c = 2\epsilon$$
 (cxxviii)

if ϵ is the spin-vector of Φ_0 .

Thus if there is no impressed couple η the function Φ (or Φ_0) must be self-conjugate.

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^{*} For example take a small tetrahedron whose directed faces are α , β , γ , and δ . Then $\Phi_0(\alpha + \beta + \gamma) = \Phi_0 \alpha + \Phi_0 \beta + \Phi_0 \gamma$ because $\alpha + \beta + \gamma = -\delta$.

(50.) Neglecting small terms of the second order in (cxxiv) and elsewhere the motion of the substance is completely given by

$$\frac{\partial \sigma}{\partial t} - S\sigma \nabla \cdot \sigma = \xi + e^{-1} \cdot \Phi \nabla ; \quad \frac{\partial e}{\partial t} = S \nabla (e\sigma) \qquad (\text{exxix})$$

when we employ Euler's method (compare (cxiv), (cxv), (cxxiv)); or by

$$\ddot{\rho} = \xi + C^{-1} \left(\frac{\partial}{\partial u} \Phi \cdot \nabla \rho_2 \rho_3 + \frac{\partial}{\partial v} \Phi \cdot \nabla \rho_3 \rho_1 + \frac{\partial}{\partial w} \Phi \cdot \nabla \rho_1 \rho_2 \right) \qquad (\text{exxx})$$

when we employ Lagrange's (compare (cxvii), (cxx)), the function Φ being linear, vector and self-conjugate, and this function, not the vectors $\nabla \rho_2 \rho_3$, &c., being differentiated with respect to u, v, and w.

(51.) We shall now apply Lord Kelvin's great conception of the *flow* along a finite curve drawn in the medium and moving with it so that it always threads the same elements. The flow is the integral of the component velocities of the various points of the curve along the corresponding tangents and is given by

$$F = -\int S\sigma d\rho = -\int S\dot{\rho} d\rho. \qquad (cxxxi)$$

It is convenient to suppose ρ and σ or its equal $\dot{\rho}$ expressed in terms of the time and the necessary parameters as in Lagrange's method. The time rate of change is thus

$$\dot{F} = -\frac{d}{dt} \int S\dot{\rho} d\rho = -\int S\ddot{\rho} d\rho - \int S\dot{\rho} d\dot{\rho}. \qquad (exxxii)$$

The second integral on the right is simply half the difference of the squares of the velocities of the extremities of the curve. The first integral depends generally on the nature of the curve connecting these extremities. It is however quite independent of the curve if (compare section (24.))

$$V\nabla \ddot{\rho} = 0 \quad \text{or} \quad V\nabla D_t \sigma = 0 \qquad (\text{exxxiii})$$

for then the expression under the sign of integration is integrable without a factor.* By (cxxiv) we have in this case

$$\nabla \nabla \xi + \nabla \nabla \cdot c^{-1} \cdot \Phi \nabla = 0 \qquad (\text{cxxxiv})$$

and when this is satisfied we may speak of the rate of change of flow from one point to another without mentioning a connecting curve.

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^{*} The vectors $\ddot{\rho}$ and $D_{t\sigma}$ are identical in as much as they represent the same acceleration. HAMILTON'S ELEMENTS OF QUATERNIONS, VOL. II. 3 N

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(52.) For a perfect fluid $\Phi d\nu = -p d\nu$ and $\Phi \nabla = -p \nabla = -\nabla p$ so (exxxiv) reduces to

$$\nabla \nabla \xi + \nabla c^{-1} \cdot \nabla p = 0 \qquad (\text{cxxxv})$$

and is satisfied if the density (c) is a function of the pressure (p) and if the forces (ξ) have a force function (P).

Under these conditions we find without trouble

$$\dot{F} = \begin{bmatrix} \frac{1}{2} \mathrm{T}\sigma^2 - P - \int \frac{\mathrm{d}p}{c} \end{bmatrix} \qquad (\mathrm{cxxxvi})$$

where the square brackets indicate that the difference is to be taken of the values of the enclosed expression at the extremities of the curve.

In general when we integrate round a closed curve the flow or circulation changes at the rate (lxxx)

$$-\frac{\mathrm{d}}{\mathrm{d}t}\int \mathrm{S}\dot{\rho}\mathrm{d}\rho = -\int \mathrm{S}\ddot{\rho}\mathrm{d}\rho = -\int \mathrm{S}\mathrm{d}\nu \nabla\nabla\ddot{\rho}. \qquad (\mathrm{exxxvii})$$

This vanishes under the supposed conditions (cxxxiii) so whenever the density of a perfect fluid is a function of the pressure conservative forces are powerless to alter the circulation in any circuit moving with the fluid.

(53.) It appears from (cxxxvii) that the component of $\nabla \nabla \ddot{\rho}$ or $\nabla \nabla D_t \sigma$ normal to any small unit circuit measures the rate of change of circulation in that circuit; and $\nabla \nabla D_t \sigma$ determines the aspect and the rate of change of circulation of the unit circuit in which this rate of change is a maximum.

On the other hand $\nabla \nabla \sigma$ determines the aspect and the circulation of the unit circuit* in which the circulation is a maximum, and $D_t \nabla \nabla \sigma$ measures the rate of change (following the motion of the fluid) from one principal unit circuit to another. A principal unit circuit obviously does not remain fixed in the fluid.

The difference between these vectors is easily seen to be

$$\nabla \nabla D_{i}\sigma - D_{i}\nabla \nabla \sigma = -\nabla \nabla_{i}S\sigma_{i}\nabla_{\cdot}\sigma = -\nabla \nabla_{i}\nabla_{\cdot}\sigma_{i}\nabla \nabla \sigma \qquad (\text{exxxviii})$$

for ∇ and $\frac{\partial}{\partial t}$ are commutative in order of operation so that as a first step the difference ist

$$- \nabla \nabla (S\sigma \nabla . \sigma) + S\sigma \nabla . \nabla \nabla \sigma.$$

It vanishes as it ought if $\nabla \nabla \sigma = 0$. In Lagrange's method the equivalent equation is

$$\nabla \nabla \ddot{\rho} - \frac{d}{dt} \nabla \nabla \dot{\rho} = - \nabla \dot{\nabla} \dot{\rho}. \qquad (\text{exxxix})$$

^{*} This has been called the principal circuit (23.).

⁺ It is useful to observe that a term such as $\nabla \nabla \nabla$, $\Im \sigma \sigma_{\sigma}$, vanishes for it should remain unchanged when the suffixes are transposed but it apparently changes sign.

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(54.) As an additional example on the application of the operator ∇ , we shall consider the nature of the stress in a viscous fluid. We assume as usual that the stress consists of a hydrostatic pressure p and a part linear in the rate of distortion or in the constituents of the strain function $\phi_0 = \frac{1}{2}(\phi + \phi')$ of section (27.), and that the principal planes of the stress-function (Φ) and the strain function ϕ_0 coincide. These considerations lead to the equation

$$\Phi a = -pa + 2n\phi_0 a + n'm''a \qquad (cxl)$$

where a is an arbitrary vector, where n and n' are scalars independent of the rate of distortion and where $m''(= -S\nabla\sigma)$ is the first invariant of ϕ_0 . For this is the most general linear function involving p in the manner specified and linear in the constituents of ϕ_0 and having the same principal planes.

(55.) Defining p more particularly by the condition that the hydrostatic pressure is equal to the mean of the magnitudes of the principal stresses, we have, for i, j, and k along the principal axes,

$$-\Sigma Si\Phi i = M'' = -3p + (2n + 3n')m''; \qquad (cxli)$$

and the condition requires

$$2n + 3n' = 0.$$
 (cxlii)

Therefore when we replace n' in terms of n and ϕ_0 in terms of ∇ and σ (section (27.))

$$\Phi a = -pa - n(Sa\nabla \cdot \sigma + \nabla \cdot Sa\sigma) + \frac{2}{3}naS\nabla\sigma. \qquad (\text{exlin})$$

If n is constant, the equation of motion (cxxiv) becomes

$$\mathbf{D}_t \boldsymbol{\sigma} = \boldsymbol{\xi} - c^{-1} \nabla p - c^{-1} n (\nabla^2 \boldsymbol{\sigma} + \frac{1}{3} \nabla \mathbf{S} \nabla \boldsymbol{\sigma}).$$
 (exliv)

(56.) In like manner for an isotropic elastic solid if σ is the displacement, the stress is given by (cxl) when p is put equal to zero, and the equation analogous to (cxliv) is

$$\mathbf{D}_t \boldsymbol{\sigma} = \boldsymbol{\xi} - \boldsymbol{c}^{-1} \boldsymbol{n} \nabla^2 \boldsymbol{\sigma} - \boldsymbol{c}^{-1} (\boldsymbol{n} + \boldsymbol{n}') \nabla \mathbf{S} \nabla \boldsymbol{\sigma}. \tag{exlv}$$

(57.) The rate of change of the kinetic energy of the substance in any region fixed in space is evidently

$$\frac{\partial}{\partial t} \int \frac{1}{2} \sigma \mathbf{T} \sigma^2 \mathrm{d}v. \qquad (\text{cxlvi})$$

This is due to the activity of the forces acting on the substance and to the transference of portions of the substance through the walls of the fixed enclosure.

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Transforming and utilizing the equations of continuity and of motion (cxxix), so as to remove the differentials with respect to the time*

$$\frac{\partial}{\partial t}\int \frac{1}{2}c\mathbf{T}\sigma^{2}\mathrm{d}v = \int (\frac{1}{2}\mathbf{T}\sigma_{0}^{2}\mathbf{S}\nabla(c\sigma) - c\mathbf{S}\sigma_{0}\nabla\mathbf{S}\sigma_{0}\sigma - \mathbf{S}\sigma_{0}\Phi\nabla - c\mathbf{S}\sigma\xi)\mathrm{d}v,$$

where σ_0 is free from the operation of ∇ . Or again this is

$$\frac{\partial}{\partial t}\int \frac{1}{2}e\mathbf{T}\sigma^{2}\mathrm{d}v = \int (\frac{1}{2}\mathbf{S}\nabla(e\sigma'\mathbf{T}\sigma^{2}) - \mathbf{S}\sigma\Phi(\nabla) + \mathbf{S}\sigma\Phi_{0}\nabla - e\mathbf{S}\sigma\xi)\mathrm{d}v,$$

where (∇) operates both on σ and Φ and where Φ_0 is free from ∇ .

Finally on integrating by parts

$$\frac{\partial}{\partial t} \int \frac{1}{2} c \mathbf{T} \sigma^2 dv = \int \frac{1}{2} c \mathbf{T} \sigma^2 \mathbf{S} \sigma dv - \int \mathbf{S} \sigma \Phi dv + \int \mathbf{S} \sigma \Phi_0 \nabla dv - \int c \mathbf{S} \sigma \xi dv. \quad (\text{exlvii})$$

The first integral on the right is the rate of increase of kinetic energy due to the influx of fresh matter; the second is the activity of the surface stress; the fourth that of the external forces; and the third with sign changed measures the rate at which energy is stored in the substance and dissipated (see section (59.)).

(58.) On the other hand for a definite portion of the substance the rate of change of kinetic energy is

$$\mathbf{D}_t \int \frac{1}{2} c \mathbf{T} \sigma^2 dv = \mathbf{D}_t \int \frac{1}{2} \mathbf{T} \sigma^2 dm = -\int \mathbf{S} \sigma \mathbf{D}_t \sigma dm = -\int \mathbf{S} \sigma (c\xi + \Phi \nabla) dv. \quad (\text{cxlviii})$$

This reduces as in the last section the only difference being that there is no contribution due to influx across the boundary.

(59.) When Φ is given by the equation (exliii),

$$-S\sigma\Phi_0\nabla = +pS\nabla\sigma + n(S\nabla\nabla_i S\sigma\sigma_i + S\nabla\sigma_i S\nabla_i\sigma) - \frac{2}{3}n(S\nabla\sigma)^2 \qquad (\text{cxlix})$$

is the rate of storage and waste of energy per unit volume.

The term in p may be modified as follows. By the equation of continuity

$$S\nabla \sigma = D_t \log c = -D_t \log b \tag{cl}$$

if b is the reciprocal of the density (c) or the bulkiness of the fluid. Hence as p is a function of c and therefore of b

$$pS\nabla\sigma = -D_t \left(pb^{-1}db. \right)$$
(cli)

Also we have for the rate of change of the intrinsic energy of a given mass

$$\int p S \nabla \sigma dv = - \int p D_t e^{-1} dm = - D_t \int dm \int p db.$$
 (clii)

• Namely from $\int \left(\frac{1}{2} \frac{\partial c}{\partial t} \operatorname{T} \sigma^2 - c \operatorname{S} \sigma \frac{\partial \sigma}{\partial t}\right) \mathrm{d} v.$

† Compare Lamb's Hydrodynamics, Art. 287.

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(60.) The part of (cxlix) quadratic in σ has been called by Lord Rayleigh the Dissipation Function. It measures the rate at which energy is wasted by the viscosity and it admits of many transformations which may serve as exercises.

It is essentially positive, for if we write the invariant m' of section (28.) in the form

$$m' = \frac{1}{2} (S \nabla \sigma)^2 - \frac{1}{2} S \nabla \sigma_i S \nabla_i \sigma \qquad (\text{cliii})$$

and

$$S\nabla\nabla_{i}S\sigma\sigma_{i} = S\nabla\sigma_{i}S\sigma\nabla_{i} - S\nabla\nabla\sigma\nabla\nabla_{i}\sigma_{i}$$
(cliv)

we have in the notation of the section cited

$$2F = n(S\nabla\nabla_{i}S\sigma\sigma_{i} + S\nabla\sigma_{i}S\nabla_{i}\sigma - \frac{2}{3}(S\nabla\sigma)^{2}) = \frac{4}{3}n(m''^{2} - 3m' - 3\epsilon^{2}) \quad (clv)$$

when we utilize (cliii) and (cliv) to eliminate $S\nabla \nabla_{\gamma}S\sigma\sigma$, and $S\nabla\sigma_{\gamma}S\nabla_{\gamma}\sigma$.

But (p. 520, vol. i.) $m' + \epsilon^2$ is the sum of the products of the roots of the selfconjugate function $\phi_0 = \frac{1}{2}(\phi + \phi')$, so if these roots are e_1 , e_2 , and e_3 ,

$$2F = \frac{2}{3}n\left((e_2 - e_3)^2 + (e_3 - e_1)^2 + (e_1 - e_2)^2\right).$$
 (clvi)

If then the dissipation function vanishes every spherical element must remain spherical, for the condition is

$$e_1 = e_2 = e_3. \tag{clvii}$$

Again as $\nabla \sigma^2 = 2\nabla S \sigma_i \sigma$ if σ_i is free from ∇_i we have

$$\nabla^2 \sigma^2 = 2\nabla^2 S \sigma_{,\sigma} \sigma + 2\nabla_{,\nu} \nabla S \sigma_{,\sigma} \sigma = 2S \sigma_{,\nu} \nabla^2 \sigma + 2S \nabla_{,\nu} \nabla S \sigma_{,\sigma} \sigma.$$
(clviii)

Hence by (cliv), we obtain the relation

$$2F = n(\nabla^2 \sigma^2 - 2S\sigma_1 \nabla^2 \sigma + (\nabla \nabla \sigma)^2 - \frac{2}{3}(S\nabla \sigma)^2)$$

in which the operator is contiguous to the operand.

Integrating and supposing n constant we may transform as follows:*

$$2\int F \mathrm{d}v = n \int \mathrm{Sd}\nu \nabla \cdot \sigma^2 - 2n \int \mathrm{S}\sigma_i \mathrm{d}\nu \nabla \sigma + n \int (\frac{4}{3}(\mathrm{S}\nabla\sigma)^2 - (\mathrm{V}\nabla\sigma)^2) \mathrm{d}v \quad (\mathrm{clix})$$

because

$$\int \mathbf{S}\boldsymbol{\sigma}_{\nu}\nabla^{2}\boldsymbol{\sigma}\mathrm{d}\boldsymbol{v} = \int \mathbf{S}\boldsymbol{\sigma}_{\nu}\mathrm{d}\boldsymbol{v}\nabla\boldsymbol{\sigma} - \int \mathbf{S}\boldsymbol{\sigma}_{\nu}\nabla_{\nu}\nabla\boldsymbol{\sigma}\mathrm{d}\boldsymbol{v}$$

and

$$S\sigma_{\nu}\nabla_{\nu}\nabla\sigma = (S\nabla\sigma)^{2} - (\nabla\nabla\sigma)^{2}.$$

(61.) Before passing on to other matters, we shall consider the expression of stress in terms of strain.[†] By Hooke's law stress is a linear function of strain and

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^{*} Compare Lamb, loc. cit.

⁺ Here, as elsewhere in this Appendix, my object is to provide suggestive illustrations of quaternion methods rather than short solutions of special problems.

therefore of the space variations of the displacement. Consequently the stress across any small plane area (ω) is a linear function of ω , of ∇ , and of the displacement σ , the operand of ∇ . Thus we may write

$$\Phi\omega = \theta(\omega, \nabla, \sigma) \tag{clx}$$

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and we shall investigate in the first place the nature of this trilinear vector function θ . We have seen that $\Phi \omega$ is a self-conjugate function of ω . Therefore for any pair of vectors ω and ϖ ,

$$S_{\varpi}\theta(\omega, \nabla, \sigma) = S_{\omega}\theta(\varpi, \nabla, \sigma).$$
 (clxi)

Again we know when a potential function exists that the expression (comp. (cxlix))

$$S\Phi\nabla_{i}\sigma_{i} = S\sigma_{i}\theta(\nabla_{i}, \nabla, \sigma)$$
 (clxii)

is symmetrical in the strain arising from the displacement σ and in that arising from the displacement $\sigma_{,,}$ it being understood that ∇ operates on σ alone and $\nabla_{,}$ on $\sigma_{,}$. Therefore identically

$$S\sigma_{\theta}(\nabla_{i}, \nabla, \sigma) = S\sigma\theta(\nabla, \nabla_{i}, \sigma_{i}).$$
 (clxiii)

The two properties expressed by the equations (elxi) and (clxiii) furnish us with sufficient data to determine the nature of the function θ , or in other words to express stress in terms of strain.

(62.) On account of the arbitrariness of the vectors σ and σ , we may replace the equations just referred to by

$$\operatorname{Sa}\theta(\beta, \gamma, \delta) = \operatorname{S}\beta\theta(a, \gamma, \delta) = \operatorname{S}\delta\theta(\gamma, \beta, a)$$
 (clxiv)

where a, β, γ , and δ are four arbitrary vectors. Using as a matter of convenience the symbol $(a, \beta, \gamma, \delta)$ defined by the equation

$$(a, \beta, \gamma, \delta) = -\operatorname{Sa}\theta(\beta, \gamma, \delta),$$
 (clxv)

we see by (clxiv) that it is permissible to reverse the order of the vectors and to transpose the first and second vectors. Hence ringing the changes on these allowable alterations we have

$$(a, \beta, \gamma, \delta) = (\beta, a, \gamma, \delta) = (\delta, \gamma, a, \beta) = (\gamma, \delta, a, \beta)$$
$$= (\beta, a, \delta, \gamma) = (a, \beta, \delta, \gamma) = (\gamma, \delta, \beta, a) = (\delta, \gamma, \beta, a), \quad (clxvi)$$

and the laws of the symbols $(a, \beta, \gamma, \delta)$ may be summed up in the statement, the pair composed of the first and second vectors is interchangeable with the pair composed of the third and fourth and the members of each pair are likewise interchangeable.

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(63.) Since $(\delta, \alpha, \beta, \gamma) = (\delta, \alpha, \gamma, \beta)$ we have generally as the vectors are arbitrary,

$$\theta(a, \beta, \gamma) = \theta(a, \gamma, \beta).$$
 (clxvii)

In particular

$$\Phi \omega = \theta(\omega, \nabla, \sigma) = \theta(\omega, \sigma, \nabla); \qquad (clxviii)$$

or more fully for any mutually rectangular system i, j, k

$$\Phi \omega = \Sigma \theta(\omega, i, i) \operatorname{Si} \nabla \operatorname{Si} \sigma + \Sigma \theta(\omega, j, k) \left(\operatorname{Sj} \nabla \operatorname{Sk} \sigma + \operatorname{Sk} \nabla \operatorname{Sj} \sigma \right) \quad (\text{clxix})$$

because $\theta(\omega, j, k) = \theta(\omega, k, j)$, or again in a usual notation for the strains,

$$\Phi \boldsymbol{\omega} = \boldsymbol{\Sigma} \boldsymbol{\theta}(\boldsymbol{\omega}, \, \boldsymbol{i}, \, \boldsymbol{i}) \, \boldsymbol{a} + \boldsymbol{\Sigma} \boldsymbol{\theta}(\boldsymbol{\omega}, \, \boldsymbol{j}, \, \boldsymbol{k}) \, . \, 2\boldsymbol{f}. \tag{clxx}$$

The constituents of the six vector functions $\theta(\omega, i, i)$, $\theta(\omega, j, k)$, &c. are the *elastic* constants. They are all of the type $(a, \beta, \gamma, \delta)$ (comp. (clxv)) where a, β, γ , and δ stand for i, j, and k; and they fall into the following groups:—three of the type (i, i, i, i); six (i, i, i, j); three (i, i, j, j); three (i, j, i, j); three (j, k, i, i); and three (j, i, k, i); twenty-one in all bearing in mind the laws of the symbol $(a, \beta, \gamma, \delta)$ (clxvi).

(64.) We saw at the beginning of the last section that the second and third vectors are interchangeable in $\theta(a, \beta, \gamma)$. We shall now investigate the effect of interchanging the first and second vectors and we shall prove that

$$\theta(a, \beta, \gamma) - \theta(\beta, a, \gamma) = 2V \otimes V a \beta \cdot \gamma$$
 (clxxi)

where Θ is a linear and self-conjugate vector function of the ordinary kind. The left-hand member obviously vanishes if a and β are parallel. We are therefore entitled to assume

$$\theta(a, \beta, \gamma) - \theta(\beta, a, \gamma) = \chi(Va\beta, \gamma)$$
 (classi)

where χ is a bi-linear function of $\nabla a\beta$ and of γ . Operating by $S\gamma$ and referring again to (clxvi) we find $S\gamma\chi(\nabla a\beta, \gamma) = 0$ for all vectors γ . The form of the right-hand member of (clxxi) is therefore justified and it only remains to prove that Θ is self-conjugate. To do so we operate by $S\delta$; and the law of interchanges again shows us that

$$\mathrm{S\delta}\theta(a, \beta, \gamma) - \mathrm{S\delta}\theta(\beta, a, \gamma) = \mathrm{Sa}\theta(\delta, \gamma, \beta) - \mathrm{Sa}\theta(\gamma, \delta, \beta)$$

when we find almost immediately

$$SV_{\gamma}\delta\Theta Va\beta = SVa\beta\Theta V\gamma\delta,$$
 (clxxiii)

and Θ is self-conjugate as asserted.

(65.) We have now at our disposal two distinct geometrical methods of investigating the arrangement of the elastic properties of a body with respect to certain natural directions of reference. The first and the most obvious method consists in the study of the quartic surface

$$(\rho, \rho, \rho, \rho) = -S\rho\theta(\rho, \rho, \rho) = const.$$
 (elxxiv)

whose radii vectors are inversely proportional to the fourth roots of the elastic constants depending on a single direction—that of the corresponding radius vector.

When the body has a plane of symmetry normal to i, the elastic constants which involve i an odd number of times must vanish. Perhaps the most instructive way of seeing the truth of this is to equate the reflection, with respect to the plane of symmetry, of the stress across any small area to the stress due to the reflection of the strain across the reflection of the area. In this case the quartic surface has also a plane of symmetry. The converse is not generally true for the quartic depends on but fifteen constants, for example 2(jijk) + (jjik).

The surface must evidently be closed and finite; otherwise the potential energy might vanish for an actual strain. To discover the planes of symmetry, when they exist, we may calculate the positions of the summits of the surface,* or the points at which a concentric sphere can touch it. The vectors to these points have the directions of the solutions of

$$V\rho\theta(\rho, \rho, \rho) = 0 \qquad (elxxv)$$

for by the rule of interchanges

$$dS\rho\theta(\rho, \rho, \rho) = 4Sd\rho\theta(\rho, \rho, \rho).$$

The normal to a plane of symmetry obviously cuts the surface at a pair of summits. The radius of a touching sphere may be obtained by equating to zero the discriminant of the cone through its intersection with the surface, the centre being the vertex.[†] It is easy to see geometrically that three at least of the vector solutions of (clxxv) must be real.

(66.) When the potential energy involves the strains only in the combinations a + b + c and the minors $bc - f^2$, &e., gh - af, &c. of the well-known determinant of a conic, that is when

$$2W = m(a + b + c)^{2} + \Sigma m_{1}(bc - f^{2}) + \Sigma l_{1}(gh - af), \qquad (clxxvi)$$

the equation of the quartic reduces to

$$m\rho^4 = const.$$
 (elxxvii)

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^{*} A more convenient process will be found in section (67.).

⁺ When the surface has three planes of symmetry the equation has thirteen roots, one quadruple and three double.

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The surface is spherical and fails to afford special directions of reference. In this case the second method to which we now proceed must be selected.

(67.) This method depends on the self-conjugate function Θ of section (64.). The coefficients of the quadric

$$S\rho \Theta \rho = const.$$
 (clxxviii)

are easily calculated in terms of the elastic constants by means of equations such as

$$\theta(j, k, \gamma) - \theta(k, j, \gamma) = 2 \nabla \Theta i \gamma$$
 (classic)

which is merely a modification of (clxxi). We find

$$2Si\Theta i = (jjkk) - (jkjk); \quad 2Sj\Theta k = (ijik) - (iijk) \quad (clxxx)$$

and the remaining coefficients may be written down from symmetry.

If the body has a plane of symmetry it must be a principal plane of this quadric, for if *i* is normal to a plane of symmetry $Sj\Theta i = Sk\Theta i = 0$ or $Vi\Theta i = 0$. The converse of course is not true. But (compare (65.)) when the quartic has a principal plane of the quadric for a plane of symmetry, we have from the equation of the quartic 2(jijk) + (jjik) = 0 and from that of the quadric (jijk) - (jjik) = 0, &c. The elastic constants vanish separately and the plane is a plane of symmetry of the body.

Thus provided the quadric has determinate axes they form a natural system of lines of reference, and planes of symmetry may be at once detected by expressing the equation of the quartic in terms of these vectors. In the most general case having selected this system of axes we have only eighteen constants to deal with, the last group of (63.) being then merged in the preceding group. As an example for the case noticed in (66.)

$$(iiii) = m; (jjkk) = m + 2n_1; (jkkj) = -n_1; (iijk) = -2l_1; (jiik) = l_1 (clxxxi)$$

but when i, j, and k are along the axes of the quadric the constants l_1, l_2 , and l_3 vanish.

(68.) It is only when the quadric is of revolution that the body can have two planes of symmetry not at right angles to one another; and moreover when the quadric is of revolution and when the quartic has a plane of symmetry through the axes of revolution it must be a plane of symmetry of the body, for every plane through the axis is a principal plane of the quadric. Taking the axis of revolution as axis of cylindrical coordinates z, p, u the equation of the quartic becomes

$$p^4 U_4 + z p^3 U_3 + z^2 p^2 U_2 + z^3 p U_1 + z^4 U_0 = \text{const.}$$
 (clxxxii)

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where the suffixes denote the order in which $\cos u$ and $\sin u$ enter in the functions U.

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If u = 0 is a plane of symmetry of the quartic the angle u must enter only in cosines and we may write

$$U_4 = a + a' \cos 2u + a'' \cos 4u$$
; $U_3 = b \cos u + b' \cos 3u$;
 $U_2 = c + c' \cos 2u$; $U_1 = d \cos u$. (clxxxiii)

If u = v is a second plane of symmetry, substitution of v + w and of v - w for u must lead to the same results. Hence

$$b \sin v = d \sin v = a' \sin 2v = c' \sin 2v = b' \sin 3v = a'' \sin 4v = 0.$$
 (claxxiv)

If the quartic is not a surface of revolution, the only admissible values of v are evidently $\frac{1}{2}\pi$, $\frac{1}{3}\pi$, and $\frac{1}{4}\pi$. Thus the planes of symmetry of the body must intersect at angles of 90°, 60°, or 45° if every plane through their intersection is not a plane of symmetry.

(69.) When the quadric is a sphere it fails of course to afford a natural system of lines of reference. This want may be supplied by the axes of the new quadric

$$\nabla^2 \cdot (\rho \rho \rho \rho) = const. \qquad (clxxxv)$$

for it is easy to see that a plane of symmetry of the quartic must be a principal plane of the quadric. In case this quadric is a sphere we can derive a third quadric by means of the operator ∇ to take its place. If for brevity $(\rho\rho\rho\rho) = f$, the equation of this quadric is

$$(S\nabla_1\nabla_2)^3 \cdot f_1 f_2 = const., \qquad (clxxxvi)$$

the suffixes being omitted after operation.

Even when this is a sphere, the quadric*

$$(S\nabla_1\nabla_3)^2 (S\nabla_2\nabla_3)^2 S\nabla_1\nabla_2 \cdot f_1 f_2 f_3 = const.$$
 (clxxvii)

is available and must of necessity determine a natural system of axes if such exists. For when any one quadric becomes a sphere five conditions are established connecting the elastic constants. If the four quadrics are spheres but one constant remains in the equation of the quartic as in the case noticed in section (66.).

$$\Sigma (\mathbf{D}_x^3 f)^2 + 3\Sigma (\mathbf{D}_x^2 \mathbf{D}_y f)^2 + 6 (\mathbf{D}_x \mathbf{D}_y \mathbf{D}_z f)^2 = const.$$

In Arouhold's notation if $f = a_x^4 = b_x^4$, the equation is

$$(a_1b_1 + a_2b_2 + a_3b_3)^3a_xb_x = const.$$

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^{*} The equations of these third and fourth quadric may be obtained by operating by ∇^6 and ∇^{10} on f^2 and f^3 respectively and rejecting terms in $T\rho^2$. In Cartesians (clxxxvi) becomes

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(70.) Although the subject is foreign to this Note on Hamilton's operator, it may be useful to offer here a few remarks on functions linear and distributive in several vectors as such functions have occurred in the treatment of stress. process is general we take the case of a trilinear function and write in analogy with

$$Sa\theta(\beta, \gamma, \delta) = S\beta\theta'(\gamma, \delta, a) = S\gamma\theta''(\delta, a, \beta) = S\delta\theta'''(a, \beta, \gamma). \quad (clxxxviii)$$

If the function is self-conjugate in the first vector so that a and β may be interchanged in these equations, we must have in general

$$\begin{aligned} \theta(a, \beta, \gamma) &= \theta'(\beta, \gamma, a); \quad \theta''(a, \beta, \gamma) = \theta''(a, \gamma, \beta); \\ \theta'''(a, \beta, \gamma) &= \theta'''(\beta, a, \gamma). \end{aligned}$$
 (classic)

If it is self-conjugate in the second vector

the notation for conjugates

$$\theta(a, \beta, \gamma) = \theta''(\gamma, \beta, a); \quad \theta'(a, \beta, \gamma) = \theta'(\gamma, \beta, a); \\ \theta'''(a, \beta, \gamma) = \theta'''(\gamma, \beta, a) \quad (cxc)$$

and if it is self-conjugate in both of these

$$\theta(a, \beta, \gamma) = \theta(\beta, a, \gamma).$$
 (exci)

If finally it is self-conjugate in all three they may be interchanged in all possible ways.

There is the closest analogy between these completely self-conjugate functions and Aronhold's notation $a_j a_k a_i a_{ij}$ (j = 1, 2, or 3). We may imitate his notation by writing

$$\theta(a, \beta, \gamma) = (\lambda)S(\lambda)aS(\lambda)\betaS(\lambda)\gamma$$
 (excii)

where (λ) is a symbolic vector devoid of interpretation unless it occurs in a term involving three other vectors (λ) . We may extend this notation to the case of non-conjugate functions by writing

$$\theta(a, \beta, \gamma) = (\lambda)S(\mu)aS(\nu)\gamma S(\varpi)\delta$$
 (exciii)

where (λ) , (μ) , (ν) , and (π) are symbolic and uninterpretable unless they occur together in a term.

Reference to Aronhold's notation is sufficient to suggest a number of interpretations of quaternion forms. For example* if

$$\theta(a, \beta) = 0 \qquad (\text{exciv})$$

where generally $\theta(\rho, \pi) = \theta(\pi, \rho)$, the vectors a and β are corresponding edges of the Hessian of a cubic cone $S_{\rho}\theta(\rho, \rho) = 0$. The equation of the Hessian is $S\theta(\rho, \xi) \theta(\rho, \eta) \theta(\rho, \zeta) = 0, \xi, \eta, \text{ and } \zeta \text{ being arbitrary constant vectors.}$

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^{*} This vector equation may be compared with the scalar $f(\alpha, \beta) = 0$, where generally $f(\rho, \varpi)$ = $f(\boldsymbol{\varpi}, \boldsymbol{\rho})$, which expresses that a and $\boldsymbol{\beta}$ are conjugate with respect to the cone $f(\boldsymbol{\rho}, \boldsymbol{\rho}) = 0$.

(71.) The operations performed in deducing the quadrics of section (69.) are related to the application of ∇ to the theory of Spherical Harmonics.* If $f_n(\nabla)$ is any integral and rational function of ∇ of degree n and with constant coefficients, $f_n\nabla$. $\mathbf{T}\rho^{-1}$ is obviously a solid harmonic of order -(n + 1). In fact this function is of the degree -(n + 1) in $\mathbf{T}\rho$ and it vanishes under the operator ∇^2 .

It is always possible to determine a function $f_{n-2}\rho$ so that

$$f_n\rho + \rho^2 f_{n-2}\rho = \mathrm{Sa}_1 \rho \mathrm{Sa}_2 \rho \quad \dots \quad \mathrm{Sa}_n \rho \qquad (\mathrm{exev})$$

For draw *n* planes through distinct pairs of the 2n common edges of the cones $f_n\rho = 0$, $\rho^2 = 0$; and through $\frac{1}{2}(n-2)(n-2+3)$ of the remaining intersections of the planes with the cone $f_n\rho = 0$ draw a cone $f_{n-2}\rho = 0$. The complex cone $\rho^2 f_{n-2}\rho = 0$ passes through $2n + \frac{1}{2}(n-2)(n+1)$ or $\frac{1}{2}n(n+3) - 1$ of the intersections of $f_n\rho = 0$ with the *n* planes; it must consequently pass through all the remaining intersections as $\frac{1}{2}n(n+3) - 1$ is one less than the number of edges requisite to determine a cone of the n^{th} degree. The relation (cxcv) is therefore justified. Again the common edges of the cones $f_n\rho = 0$, $\rho^2 = 0$, group themselves into pairs $\alpha'_1 \pm \alpha''_1 \sqrt{-1}$ and each group lies in a real plane. The reduction may therefore be uniquely effected in such a manner that the planes shall be all real. But in operating on $T\rho^{-1}$, any function $\nabla^2 f_{n-2}\nabla$ may be added to $f_n\nabla$ without altering the result. Thus we may always suppose[†]

$$f_n \nabla \cdot \mathbf{T} \rho^{-1} = \mathbf{S} a_1 \nabla \mathbf{S} a_2 \nabla \cdot \cdot \cdot \mathbf{S} a_n \nabla \cdot \mathbf{T} \rho^{-1}. \qquad (\text{excvi})$$

This enables us to expand any homogeneous function of ρ in a series of spherical harmonics. When we effect the operations indicated and multiply across by $T\rho^{2n+1}$, we have, $(F_{n-2}\rho)$ being a determinate function of degree n-2),

$$\mathbf{T}\rho^{2n+1}f_n\nabla \cdot \mathbf{T}\rho^{-1} = [n)\mathbf{S}a_1\rho\mathbf{S}a_2\rho \cdot \cdot \cdot \mathbf{S}a_n\rho + \mathbf{T}\rho^2F_{n-2}\rho. \qquad (\text{exervii})$$

where for the sake of brevity

$$[n] = (-)^n \cdot 1 \cdot 3 \cdot 5 \cdot (2n-1).$$
 (exerviii)

Comparing (cxcv) and (cxcvii) we see that

$$f_n\rho = \frac{\mathrm{T}\rho^{2n+1}}{[n]} \cdot f_n \nabla \cdot \frac{1}{\mathrm{T}\rho} + \mathrm{T}\rho^2 \cdot g_{n-2}\rho \qquad (\mathrm{cic})$$

where $g_{n-2\rho}$ is a homogeneous function of ρ . Treating this new function $g_{n-2\rho}$ in the same manner we obtain the second harmonic in the series and the process may be repeated.

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^{*} Much of the following is adapted from Clerk Maxwell's most interesting and instructive chapter on Spherical Harmonics, *Electricity and Magnetism*.

⁺ The extremities of the vectors Ua1, Ua2, &c. are the poles of the spherical harmonic.

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(72.) The potential due to any distribution of matter at any point (ρ) external to a sphere which encloses all the matter may be expressed by a relation of the form

$$P = f \nabla \cdot \mathbf{T} (\rho - \alpha)^{-1}$$
 (cc)

 $f \nabla$ being a function of ∇ expansible in ascending powers and the centre of the sphere being at the extremity of α . For if dm is the element of matter at the extremity of π ,

$$P = \int \frac{\mathrm{d}m}{\mathrm{T}(\rho - \varpi)} = \int \mathrm{d}m e^{\mathrm{S}(\varpi - \alpha)\nabla} \cdot \frac{1}{\mathrm{T}(\rho - \alpha)} = f\nabla \cdot \frac{1}{\mathrm{T}(\rho - \alpha)}.$$

If $Q_a = \int dm' T(\rho - a)^{-1}$ is the potential at the extremity of a of a second distribution of matter wholly exterior to the sphere enclosing the first, the mutual potential energy is

$$\mathcal{W} = \int \mathrm{d}m' P = \int \mathrm{d}m' f(\nabla) \cdot \mathbf{T}(\rho - \alpha)^{-1} = \int \mathrm{d}m' f(-\nabla_{\alpha}) \mathbf{T}(\rho - \alpha)^{-1} = f(-\nabla_{\alpha}) \cdot Q_{\alpha}. \quad (\mathrm{cci})$$

Or more conveniently if we take the origin at the centre of the sphere

$$W = f(-\nabla) \cdot Q_0 \tag{ecii}$$

provided we put $\rho = 0$ after the operations have been performed as indicated by the suffix.

If Q is due to a surface distribution of density s over the sphere

$$W = \int P \operatorname{sd} S = f(-\nabla) \cdot Q_0.$$
 (eciii)

When $Q = r^n Y_n$, Y_n being a spherical harmonic so that $4\pi s = (2n + 1)a^{n-1}Y_n$ if a is the radius of the sphere, this equation becomes

$$4\pi f(-\nabla)r^n Y_n = (2n+1)a^{n+1} \int P Y_n d\Omega \qquad (\text{eeiv})$$

if $d\Omega$ is an element of solid angle. It is manifest that the terms in $f(-\nabla)$ of the n^{th} order in ∇ alone contribute to the left-hand member. For the operation of terms of higher order destroys $r^n Y_n$, and the results of operation of terms of lower order vanish when r is put equal zero. Hence in particular

$$4\pi f_n(-\nabla)r^n Y_n = (2n+1) \int Z_n Y_n d\Omega; \quad \int Z_m Y_n d\Omega = 0 \quad (\text{cev})$$

if Z_n and Z_m are spherical harmonics and if

$$f_n(+\nabla) \cdot r^{-1} = r^{-n-1}Z_n$$

(73.) Up to the present we have searcely considered the analytical structure of the operator ∇ . In section (7.) we obtained an expression (xiii) depending on three arbitrary differentials and the corresponding differentiating symbols. In section (12.)

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we employed the well-known Cartesian form (xviii) for purposes of illustration, and a third form (cxx) depending like (xviii) on the highly artificial method of determining a vector by means of those systems of surfaces occurred in section (47.) in connexion with Lagrange's method in fluid motion. Of all these forms (xiii) is the most accordant with the spirit of the *Elements* because there is perfect freedom in the choice of differentials most suitable for special purposes and because the conception of a vector as an entity is not obscured by any system of coordinates.

(74.) To leave as little obscurity as possible about the method of arbitrary differentials we shall consider the square of the operator (xiii) which we write for brevity in the form

$$\nabla = \delta d + \delta' d' + \delta'' d'' \qquad (ccvi)$$

where the vectors δ , δ' , and δ'' are determined by the equations

$$\delta = -\frac{\mathrm{Vd}'\rho \mathrm{d}''\rho}{\mathrm{Sd}\rho \mathrm{d}'\rho \mathrm{d}''\rho}, \quad \delta' = -\frac{\mathrm{Vd}''\rho \mathrm{d}\rho}{\mathrm{Sd}\rho \mathrm{d}'\rho \mathrm{d}''\rho}, \quad \delta'' = -\frac{\mathrm{Vd}\rho \mathrm{d}'\rho}{\mathrm{Sd}\rho \mathrm{d}'\rho \mathrm{d}''\rho}. \quad (\mathrm{cevii})$$

It must be observed however that any advantage that may arise from the use of this form is concealed when the operator is separated from the operand; and owing to the generality of the expression the result is apparently cumbrons. Squaring we find

$$\nabla^{2} = \Sigma \delta^{2} d^{2} + \Sigma \left(\delta' \delta'' d' d'' + \delta'' \delta' d'' d' \right) + \Sigma \nabla \delta . d.$$
 (ceviii)

In the third sum ∇ operates on the vectors δ alone and not on the operand of ∇^2 .

Remembering that ∇^2 is a scalar operator this equation breaks up into two, a scalar and a vector,

$$\nabla^2 = \Sigma \delta^2 d^2 + \Sigma S \delta' \delta'' \left(d' d'' + d'' d' \right) + \Sigma S \nabla \delta' \cdot d \qquad (ccix)$$

$$0 = \Sigma \nabla \delta' \delta'' (d'd'' - d''d') + \Sigma \nabla \nabla \delta \cdot d.$$
 (ccx)

It is only when the differentials are independent that the order in which the differentiations are performed is indifferent and in this case only is it generally lawful to suppress the terms involving d'd'' - d''d' and similar expressions.

(75.) When independent differentials are employed, we may fall back on the equation (cxx) or

$$\nabla = -\frac{\nabla \rho_2 \rho_3}{S \rho_2 \rho_3 \rho_1} \cdot \frac{\partial}{\partial u} - \frac{\nabla \rho_3 \rho_1}{S \rho_3 \rho_1 \rho_2} \cdot \frac{\partial}{\partial v} - \frac{\nabla \rho_1 \rho_2}{S \rho_1 \rho_2 \rho_3} \cdot \frac{\partial}{\partial w}$$

which we shall write for brevity in the form

 $\nabla = \nu \frac{\partial}{\partial u} + \nu' \frac{\partial}{\partial v} + \nu'' \frac{\partial}{\partial w}$ (ccxi)

where v, v', v'' are normals to the surfaces determined by constant values of u, v and w

and

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respectively. The following equations among others are satisfied by these normal vectors,

$$S\rho_1\nu + 1 = 0, \quad S\rho_2\nu = 0, \quad S\rho_3\nu = 0.$$
 (ccxii)

Also when we consider u, v and w to be functions of ρ we have

$$\nabla = \nabla u \frac{\partial}{\partial u} + \nabla v \frac{\partial}{\partial v} + \nabla w \frac{\partial}{\partial w}.$$
 (cexiii)

So the vectors v may be expressed by the equations

$$\nu = \nabla u, \quad \nu' = \nabla v, \quad \nu'' = \nabla w$$
 (cexiv)

whence we find

$$\nabla \nabla \nu = 0, \quad \nabla \nabla \nu' = 0, \quad \nabla \nabla \nu'' = 0.$$
 (ccxv)

(76.) These equations may be deduced from (ccx) as a particular case. In fact

$$\nabla^2 = \sum \nu^2 \frac{\partial^2}{\partial u^2} + 2\sum S\nu'\nu'' \frac{\partial^2}{\partial v \partial w} + \sum S\nabla \nu \frac{\partial}{\partial u}$$
(ccxvi)

and

$$0 = \nabla \nabla \nu \frac{\partial}{\partial u} + \nabla \nabla \nu' \frac{\partial}{\partial v} + \nabla \nabla \nu'' \frac{\partial}{\partial v}.$$
 (cexvii)

The vector equation furnishes the three equations (ccxv) as appears by operating for example on u, v and w respectively.

(77.) But there is still another form for ∇ , namely

$$\nabla q = -\frac{1}{\mathbf{S}\rho_1\rho_2\rho_3} \left\{ \frac{\partial}{\partial u} \left(\nabla \rho_2\rho_3 \cdot q \right) + \frac{\partial}{\partial v} \left(\nabla \rho_3\rho_1 \cdot q \right) + \frac{\partial}{\partial w} \left(\nabla \rho_1\rho_2 \cdot q \right) \right\} \quad (\text{ccxviii})$$

in which for greater clearness the operand is inserted. On expansion this obviously reduces to (cxx). Hence we have

$$\nabla^{2} = + \frac{1}{S\rho_{1}\rho_{2}\rho_{3}} \left\{ \Sigma \frac{\partial}{\partial u} \left(\frac{(\nabla\rho_{2}\rho_{3})^{2}}{S\rho_{1}\rho_{2}\rho_{3}} \frac{\partial}{\partial u} \right) + \Sigma \frac{\partial}{\partial u} \left(\frac{\nabla\rho_{2}\rho_{3}\nabla\rho_{3}\rho_{1}}{S\rho_{1}\rho_{2}\rho_{3}} \frac{\partial}{\partial v} \right) \right\} \quad (\text{ccxix})$$

where the second sum includes six terms and to this the sign S may be prefixed. This may also be written in the more compact form

$$\nabla^2 = + \mathbf{S} \boldsymbol{\nu} \boldsymbol{\nu}' \boldsymbol{\nu}'' \left\{ \boldsymbol{\Sigma} \frac{\partial}{\partial u} \left(\frac{\boldsymbol{\nu}^2}{\mathbf{S} \boldsymbol{\nu} \boldsymbol{\nu}' \boldsymbol{\nu}''} \frac{\partial}{\partial u} \right) + \boldsymbol{\Sigma} \frac{\partial}{\partial u} \left(\frac{\mathbf{S} \boldsymbol{\nu} \boldsymbol{\nu}'}{\mathbf{S} \boldsymbol{\nu} \boldsymbol{\nu}' \boldsymbol{\nu}''} \frac{\partial}{\partial v} \right) \right\} .$$
 (cexx)

(78.) The analytical expression for ∇^2 becomes immensely simplified in two important cases; (I.) whenever the parameters are Cartesian coordinates, rectangular or otherwise, for then the vectors ν , ν' , ν'' are constant instead of being as in general variable with ρ ; and (II.) whenever the three families of surfaces are mutually rectangular.

In the second case, which includes the most important application of the first, we may remove at once the superfluous symbols S and V from (cxx) or the first expression of (75.) we then have

$$\nabla = -\frac{1}{\rho_1} \frac{\partial}{\partial u} - \frac{1}{\rho_2} \frac{\partial}{\partial v} - \frac{1}{\rho_3} \frac{\partial}{\partial w} \cdot \qquad (\text{cexxi})$$

Forming the square of this directly or replacing $S\rho_1\rho_2\rho_3$ by $-T\rho_1\rho_2\rho_3$ and $(V\rho_2\rho_3)^2$ by $-T\rho_2^2\rho_3^2$ in (cexix) we obtain

$$\nabla^{2} = -\frac{1}{\mathrm{T}\rho_{1}\rho_{2}\rho_{3}} \Sigma \frac{\partial}{\partial u} \left(\mathrm{T}\rho_{1}^{-1}\rho_{2}\rho_{3} \frac{\partial}{\partial u} \right) \qquad (\mathrm{ccxxii})$$

which is equivalent to the usual expression for ∇^2 in orthogonal curvilinear coordinates.

(79.) If the family of surfaces u constant is isothermal or equipotential, we must have

$$\nabla^2 f(u) = 0 \qquad (\text{cexxiii})$$

where f(u) is the potential. Operating by ∇^2 as given by (ccxxii) on f(u) we obtain

$$\frac{\partial}{\partial u} \left(\operatorname{T} \rho_1^{-1} \rho_2 \rho_3 \frac{\partial f}{\partial u} \right) = 0 \quad \text{or} \quad \operatorname{T} \rho_1^{-1} \rho_2 \rho_3 \frac{\partial f}{\partial u} = F(v, w). \quad (\operatorname{ccxxiv})$$

If the parameter u is the potential, so that $\nabla^2 u = 0$, the product $T\rho_1\rho_2^{-1}\rho_3^{-1}$ is a function of v and w. If moreover the three families are equipotential (cexxii) reduces to

$$\nabla^2 = \frac{1}{\rho_1^2} \frac{\partial^2}{\partial u^2} + \frac{1}{\rho_2^2} \frac{\partial^2}{\partial v^2} + \frac{1}{\rho_3^2} \frac{\partial^2}{\partial v^2}$$
(ccxxv)

when u, v, and w are the corresponding potentials.

(80.) More generally we shall find the condition that the family of surfaces

$$f(\rho, u) = 0 \qquad (\text{cexxvi})$$

should be isothermal. If we suppose the parameter (u) of the family to be found by solution as a function of ρ we may treat (ccxxvi) as an identity and may equate to zero the results of operating by ∇ and ∇^2 on $f(\rho, u)$ when we operate both on u and on ρ . Hence

$$\nabla f + \nabla u \cdot \frac{\partial f}{\partial u} = 0 \qquad (\text{cexxvii})$$

where ρ alone is operated on in ∇f . Again

$$\nabla^2 f + \nabla u \cdot \frac{\partial \nabla f}{\partial u} + \nabla \frac{\partial f}{\partial u} \cdot \nabla u + \nabla^2 u \cdot \frac{\partial f}{\partial u} + (\nabla u)^2 \cdot \frac{\partial^2 f}{\partial u^2} = 0. \quad (\text{cexxviii})$$

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But evidently ∇ as operating on ρ is commutative with $\frac{\partial}{\partial u}$, so we have the simpler expression

$$\nabla^2 f + 2S\nabla u \cdot \frac{\partial \nabla f}{\partial u} + \nabla^2 u \frac{\partial f}{\partial u} + (\nabla u)^2 \frac{\partial^2 f}{\partial u^2} = 0. \qquad (\text{ccxxix})$$

Now if P is a function of u which satisfies $\nabla^2 P = 0$, as a particular case of this equation

$$\frac{\partial}{\partial u} \log \frac{\partial P}{\partial u} + \frac{\nabla^2 u}{(\nabla u)^2} = 0 \qquad (\text{cexxx})$$

Eliminating ∇u and $\nabla^2 u$ between (ccxxvii), (ccxxix) and (ccxxx) we obtain without difficulty

$$\frac{\partial}{\partial u} \log \frac{\partial P}{\partial u} = \frac{\partial}{\partial u} \log \frac{\partial f}{\partial u} - \frac{\partial}{\partial u} \log (\nabla f)^2 + \frac{\nabla^2 f}{(\nabla f)^2} \cdot \frac{\partial f}{\partial u}.$$
 (ccxxxi)

When the operations^{*} indicated have been performed on the right-hand member of this equation, it must be possible to reduce it by means of the equation (cexxvi) of the family of surfaces to a function of u alone if the family is isothermal. This condition being satisfied, two integrations afford P, the temperature (or the potential) appropriate to the surfaces. The condition may be obtained explicitly, for if $F(\rho, u)$ can thus be reduced to a function of u,

$$\nabla \cdot F + \nabla u \frac{\partial F}{\partial u} || \nabla u || \nabla f \text{ or } \nabla \nabla f \nabla F = 0. \qquad (\text{ccxxxii})$$

Hence the condition may be written as a partial differential equation in the form

$$\nabla \nabla f \cdot \nabla \left\{ \frac{\partial}{\partial u} \log \left(\frac{\partial f}{\partial u} \frac{1}{(\nabla f)^2} \right) + \frac{\partial f}{\partial u} \frac{\nabla^2 f}{(\nabla f)^2} \right\} = 0.$$
 (ccxxxiii)

(81.) As an example take the system of confocals

$$f(\rho, u) = \mathrm{S}\rho(\Phi + u)^{-1}\rho - 1 = 0. \qquad (\mathrm{ccxxxiv})$$

For this

$$\nabla f = -2(\Phi + u)^{-1}\rho; \quad \nabla^2 f = 2((a^2 + u)^{-1} + (b^2 + u)^{-1} + (c^2 + u)^{-1}); \quad \frac{\partial f}{\partial u} = -\frac{1}{4}(\nabla f)^2.$$
(ccxxxv)

The differential equation for P is simply

$$\frac{\partial}{\partial u}\log\frac{\partial P}{\partial u} = -\frac{1}{4}\nabla^2 f = -\frac{1}{2}((a^2+u)^{-1}+(b^2+u)^{-1}+(c^2+u)^{-1});$$

^{*} The fact that these operations are partial must be borne in mind. This may be illustrated for the cases $f = p^2 + u^2$, $f = p^2 u^2 + 1$.

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the condition (ccxxxiii) is obviously satisfied and

$$P = P_0 \int \frac{\mathrm{d}u}{((a^2 + u)(b^2 + u)(c^2 + u))^{\frac{1}{2}}}, \qquad (\mathrm{ccxxxvi})$$

a second arbitrary constant being understood to accompany the sign of integration.

(82.) It is also easy to find in terms of ∇ the condition that the family of surfaces

$$F\rho = u$$
 (ccxxxvii)

should compose one of three mutually orthogonal systems.*

The vectors ρ_1 , ρ_2 , ρ_3 being the deriveds of ρ with respect to three parameters u, v, and w, the corresponding surfaces will be mutually orthogonal if the equations

$$S\rho_2\rho_3 = S\rho_3\rho_1 = S\rho_1\rho_2 = 0 \qquad (ccxxxviii)$$

are true for all values of u, v, and w. Under these conditions we may differentiate and equate the results to zero. Thus we obtain

$$S(\rho_{12}\rho_3 + \rho_2\rho_{31}) = S(\rho_{23}\rho_1 + \rho_3\rho_{12}) = S(\rho_{31}\rho_2 + \rho_1\rho_{23}) = 0,$$

or what is equivalent

$$S\rho_{23}\rho_1 = S\rho_{31}\rho_2 = S\rho_{12}\rho_3 = 0$$
 (ccxxix)

or again by the conditions of perpendicularity,

$$S\rho_{23}\rho_{2}\rho_{3} = S\rho_{31}\rho_{3}\rho_{1} = S\rho_{12}\rho_{1}\rho_{2} = 0.$$
 (ccxl)

These equations show that the surfaces intersect along their lines of curvature for they are of the form

$$Svdvd\rho = 0$$
 (ccxli)

which is the well-known equation of the lines of curvature. They may be replaced by vector equations, one of which is

$$\rho_{23} = y\rho_2 + z\rho_3 \tag{ccxlii}$$

where y and z are certain scalars. Differentiating with respect to u, we may write the result in the form

$$\frac{\partial^2 \rho_1}{\partial v \partial w} = y \frac{\partial \rho_1}{\partial v} + z \frac{\partial \rho_1}{\partial w} + \frac{\partial y}{\partial u} \rho_2 + \frac{\partial z}{\partial u} \rho_3 \qquad (\text{ccxliii})$$

and this implies

$$S\rho_1\left(\frac{\partial^2\rho_1}{\partial v\partial w} - y\frac{\partial\rho_1}{\partial v} - z\frac{\partial\rho_1}{\partial w}\right) = 0. \qquad (cexliv)$$

Now

$$\frac{\partial}{\partial v} = - S\rho'_{2}\nabla, \quad \frac{\partial}{\partial w} = - S\rho'_{3}\nabla, \quad \frac{\partial^{2}}{\partial v\partial w} = S\rho'_{2}\nabla S\rho'_{3}\nabla - S\rho'_{23}\nabla \qquad (\text{ccxlv})$$

* Compare Salmon's Geometry of Three Dimensions, fourth edition, pages 436-450.

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in which the accents signify that the marked vectors are free from the operation of ∇ . Hence we see immediately by (ccxlii) that generally and symbolically

$$\frac{\partial^2}{\partial v \partial w} - y \frac{\partial}{\partial v} - z \frac{\partial}{\partial w} = S \rho'_2 \nabla S \rho'_3 \nabla, \qquad (\text{cexlvi})$$

while the condition (ccxliv) may be replaced by

$$S\rho'_2 \nabla S\rho'_3 \nabla S\rho'_1 \rho_1 = 0 \qquad (ccxlvii)$$

in which ∇ operates solely upon the unaccented vector ρ_1 .

It only remains to replace ρ_1 , ρ_2 , and ρ_3 in terms of ∇ and $F\rho$ in order to obtain the differential equation which the equation of the family of surfaces $F\rho = u$ must satisfy.

In the first place (ccxxi)

$$\nabla F = \nabla u = -\rho_1^{-1}$$
 or $\rho_1 = -\nabla F^{-1}$; (cexlviii)

and again if we put $\nu = \nabla F$ and write

$$d\nu = \phi d\rho = S d\rho \nabla \nabla F \qquad (cexlix)$$

in the equation of the lines of curvature (ccxli), we find

$$\rho_n \mid\mid (\boldsymbol{\phi} + t_n)^{-1} \boldsymbol{\nu} \mid\mid (\boldsymbol{\psi} + t_n \boldsymbol{\chi} + t_n^{-2}) \boldsymbol{\nu}$$
 (ccl)

where the suffix n = 2 or 3 and where t_2 and t_3 are the roots of the quadratic

$$S_{\nu}(\phi + t_n)^{-1}\nu = 0 \quad \text{or} \quad S_{\nu}(\psi + t_n\chi + t_n^2)\nu = 0. \quad (\text{celi})$$

We may also write

$$\rho_n \mid\mid \nu^{-1} \nabla \nu (\psi + t_n \chi) \nu \mid\mid \lambda + t_n \mu, \qquad (\text{cclii})$$

the vectors λ and μ being introduced for the sake of brevity and being known in terms of ∇ and F by the results of sections (27.) and (28.). Substituting in (ccxlvii) we obtain

$$S(\lambda_0 + t_2\mu_0)\nabla S(\lambda_0 + t_3\mu_0)\nabla S(\nabla F)^{-1}(\nabla F)_0 = 0; \qquad (\text{ccliii})$$

and finally by the aid of the quadratic (celi) we arrive at the equivalent of Cayley's differential equation of the third order in the form

$$\{(\mathrm{S}\lambda_0\nabla)^2 - (\mathrm{S}\nu^{-1}\chi\nu)_0 \,\mathrm{S}\lambda_0\nabla\mathrm{S}\mu_0\nabla + (\mathrm{S}\nu^{-1}\psi\nu)_0 \,(\mathrm{S}\mu_0\nabla)^2\}\,\,\mathrm{S}(\nabla F)^{-1}\,(\nabla F)_0 = 0. \quad (\mathrm{celiv})$$

In this the suffixes are intended to indicate that the quantities distinguished by them are exempt from the operation of ∇ .

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* The words ideal and symbolical are occasionally used by Hamilton as synonymous with imaginary.

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* Clausius has called this the virial.

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