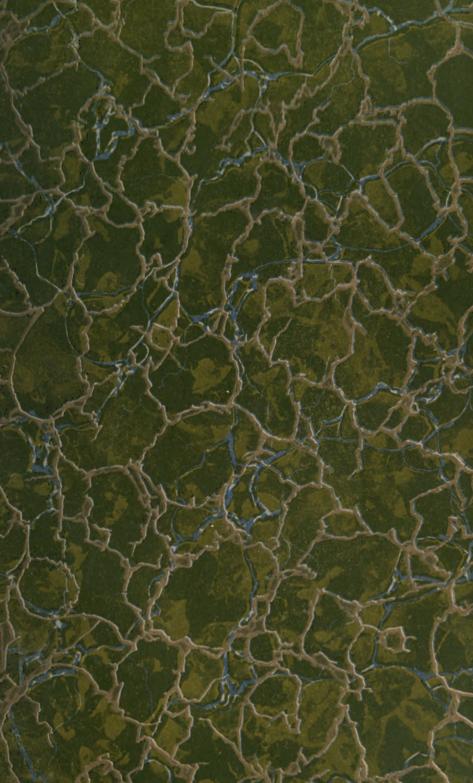
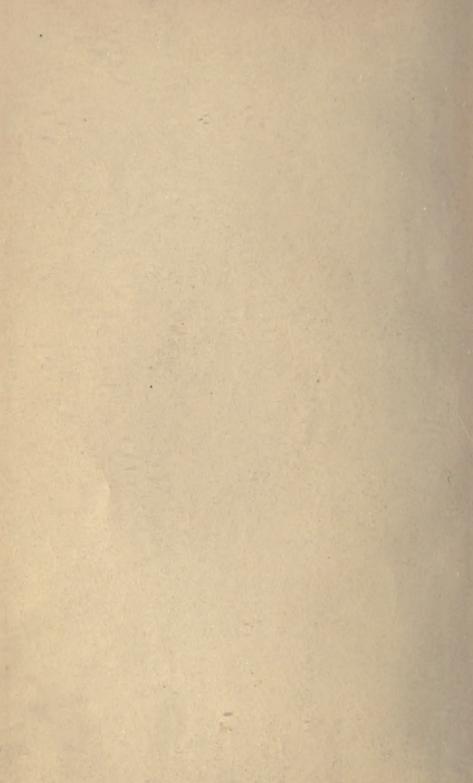


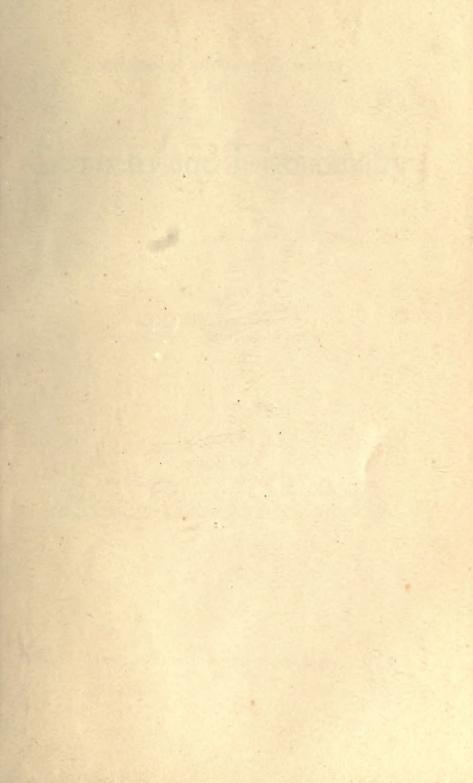


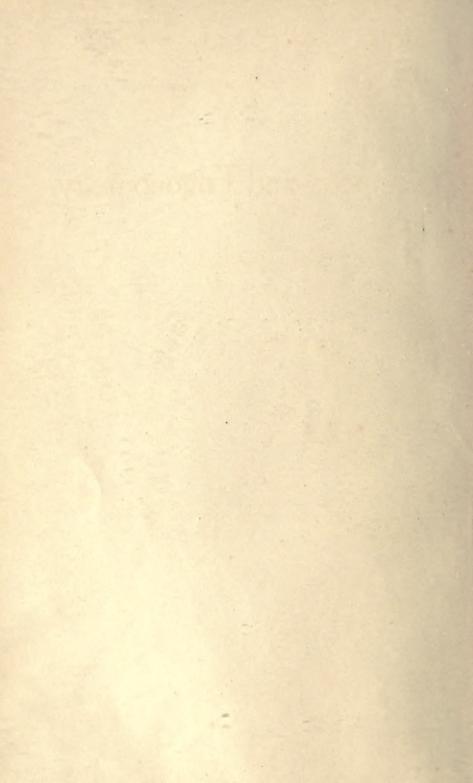
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Geometry and Trigonometry

230 ILLUSTRATIONS

By EDITORIAL STAFF

GEOMETRY PLANE TRIGONOMETRY NATURAL TRIGONOMETRIC FUNCTIONS LOGARITHMIC TRIGONOMETRIC FUNCTIONS

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PREFACE

The volumes of the International Library of Technology are made up of Instruction Papers, or Sections, comprising the various courses of instruction for students of the International Correspondence Schools. The original manuscripts are prepared by persons thoroughly qualified both technically and by experience to write with authority, and in many cases they are regularly employed elsewhere in practical work as experts. The manuscripts are then carefully edited to make them suitable for correspondence instruction. The Instruction Papers are written clearly and in the simplest language possible, so as to make them readily understood by all students. Necessary technical expressions are clearly explained when introduced.

The great majority of our students wish to prepare themselves for advancement in their vocations or to qualify for more congenial occupations. Usually they are employed and able to devote only a few hours a day to study. Therefore every effort must be made to give them practical and accurate information in clear and concise form and to make this information include all of the essentials but none of the nonessentials. To make the text clear, illustrations are used freely. These illustrations are especially made by our own Illustrating Department in order to adapt them fully to the requirements of the text.

In the table of contents that immediately follows are given the titles of the Sections included in this volume, and under each title are listed the main topics discussed.

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Note-This volume is made up of a number of separate Sections, the page numbers of which usually begin with 1. To enable the reader to distinguish between the different Sections, each one is designated by a number preceded by a Section mark (\S). which appears at the top of each page, opposite the page number. In this list of contents, the Section number is given following the title of the Section, and under each title appears a full synopsis of the subjects treated. This table of contents will enable the reader to find readily any topic covered.

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GEOMETRY

(PART 1)

Serial 778A

Edition 1

PRELIMINARY DEFINITIONS

Note.—The study of Geometry is a process of systematic and orderly reasoning rather than a matter of memory. The student is advised to study the principles and propositions stated until he understands them thoroughly and sees their relation one to another, and, when a proposition is accompanied by an explanation in small type, to read over the explanation carefully one or more times, until he clearly understands the matter, following out the references to the figure when a figure is given. If he will do this he will find Geometry to be of great benefit and assistance to him in his subsequent studies. But he is not required to commit to memory the explanations or any part of the text except a few of the more important principles and propositions, such as those to which the Examination Questions relate.

1. Every material body possesses two general properties without regard to any other condition, namely: form, or shape, which is due to the relative positions of its parts; and magnitude, or size, which is due to the distance of its parts from one another.

The form and magnitude of a body can be described by the relative positions of *points*, *lines*, and *surfaces*.

2. A point has position without magnitude. A dot is commonly used to represent a point; but a dot, no matter how small, has length, breadth, and thickness, while a theoretical point has position only.

3. A line is the path of a point in motion; it has one dimension—length. Thus, if a point is moved from the position A, Fig. 1, to the position B, its path, or trace, is the line AB.

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GEOMETRY, PART 1

4. A straight line, or right line, Fig. 2, is a line that does not change its direction.

5. The distance between two points is the length of the straight line joining them.

6. A curved line, Fig. 3, is a line that changes its direction at every point.

7. A broken line, Fig. 4, is a line that changes its direction at only certain points. It is made up wholly of different straight lines.

A

FIG. 5

The word *line*, when not qualified by any other word, is understood to mean a straight line.

8. A surface is the path of a line when moved in a direction other than its length. Thus, c , p , the line is moved from the position *A B*, Fig. 5, to the position *C D*, the line describes the surface *A B D C*.

9. A flat surface, plane surface, or simply a plane, is a surface such

that a straight line between any two of its points lies wholly in the surface. If a straightedge is laid on a plane surface in any direction, every point of the straightedge will touch the surface.

10. A figure is any combination of points and lines. A figure that lies entirely in one plane is a plane figure.

In referring to a figure, a point is designated by a letter placed conveniently near it; thus, in Fig. 1, the left end of the line is referred to as the point A. The entire line is referred to as "the line AB," the letters A and B designating two points, usually the ends of the line. If a line is broken or curved, as many points are named as are considered necessary to designate the line.

11. Geometry is that branch of mathematics that treats of the construction and properties of figures.



F10. 2

12. To produce a line is to prolong it or to increase its length. A straight line can be prolonged or produced to any extent in either direction. Thus, in Fig. 6, the straight line AB is produced to the points C and D.

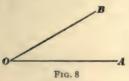
13. To bisect any given magnitude is to divide it into two equal parts. Thus, the

straight line AB. Fig. 7, is bisected at the point C if AC is equal to CB. When a given magnitude is bisected, each of the parts into which it is divided is one-half the given magnitude.

STRAIGHT-LINE FIGURES

ANGLES AND PERPENDICULARS

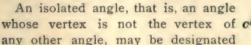
14. An angle, Fig. 8, is the opening between two straight lines that meet in a point. The two straight lines are the sides, and the point where the lines meet is the



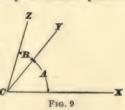
vertex, of the angle. Thus, in Fig. 8. the straight lines OA and OB form an angle at the point O: the lines OA and OB are the sides of this angle, and the point O is its vertex.

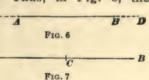
An angle is usually referred to by naming a letter on each of its sides and a third letter at the vertex, the letter at the vertex being placed between the other two. Thus, the angle in Fig. 8 is called angle AOB or angle BOA.

An angle may also be designated by a letter placed between its sides near the vertex. Thus, the two angles XCY and YCZ, Fig. 9, may be referred to as the angles A and B, respectively.

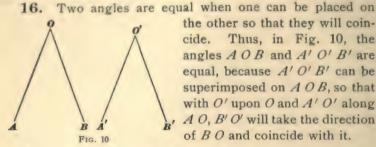


by naming the letter at its vertex. For example, the angle in Fig. 8 may be called the angle O.





15. Two angles, as A and B, Fig. 9, having the same vertex and a common side CY, are called adjacent angles.



the other so that they will coincide. Thus, in Fig. 10, the angles $A \cap B$ and $A' \cap B'$ are equal, because A' O' B' can be superimposed on A O B, so that with O' upon O and A' O' along A O, B' O' will take the direction of *BO* and coincide with it.

17. Any angle may be thought of as being formed, or generated, by a line turning about the vertex as a pivot. from the position of one side to the position of the other. Thus, the angle AOB, Fig. 8, may be conceived as generated by a line turning about O from the position OA to the position OB. The size of the angle does not depend on the length of the sides, which are supposed to be of indefinite length, but on the opening between the sides: or, what is the same thing, on the amount of turning necessary to bring one side to the position of the other.

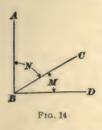
18. If a straight line, as A B, Fig. 11, meets another straight line, as CD, so as to make with it two equal adjacent angles, each of these angles is a right angle, and the first line is said to be perpendicular to the second. The point where the cn R first line meets the second is called the FIG. 11 foot of the perpendicular. It is evident that all right angles are equal.

> 19. A horizontal line is a line parallel to the horizon, or to the surface of still water.

20. A vertical line is a line perpendic-Horizonial FIG. 12 ular to a horizontal line, and having, therefore, the direction of a plumb-line. See Fig. 12.

21. An oblique angle is any angle that is not a right angle. An acute angle is an oblique angle that is less than a right angle. An obtuse angle is an oblique angle that is greater than a right angle. In Fig. 13, *BOC* and Fig. 13

AOC are oblique angles, BOC being an acute angle, and AOC an obtuse angle.

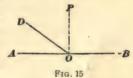


22. Two angles are said to be complementary when their sum is equal to one right angle. Each of two complementary angles is called the complement of the other. Thus, in Fig. 14, in which AB is perpendicular to BD, the angles M and Nare complementary, their sum being equal to the right angle ABD.

23. Two angles are said to be supplementary when their sum is equal to two right angles. Each of two supplementary angles is called the supplement of the other. In

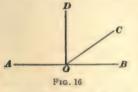
Fig. 15, AOD and DOB are supplementary angles, their sum being evidently equal to the sum of the two right angles POB and POA.

It will be seen from this illustration that two adjacent angles whose non-



common sides are in the same straight line are always supplementary. Conversely, if two adjacent angles are supplementary, their non-common sides are in the same straight line.

24. At a given point in a straight line, one perpendicular to the line and only one can be drawn.

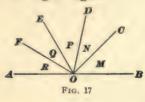


Let O, Fig. 16, be the given point in the line OB. Suppose that with the point Ofixed, the line OC starts from the position OB and revolves about O. In any position, as OC, it makes two angles with the line AB; one AOC, the other BOC. As OC revolves from the position OB to

the position OA, the angle BOC will continually increase, and the

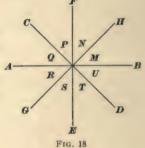
angle A O C will continually decrease. There will therefore be one position, as O D, where the two angles are equal, and there can evidently be but one such position.

25. The sum of all the angles formed on the same side of a straight line about the same point in the line is equal to two right angles.



In Fig. 17, the sum of the three angles M, N, and P is evidently equal to the angle $B \circ E$, and the sum of the angles Q and R is equal to the angle $E \circ A$. But, by Art. 23, $B \circ E + E \circ A$ is equal to two right angles. Hence, M + N + P + Q + R = two right angles.

26. The sum of all the angles formed in the same plane about one point is equal to four right angles. Thus, in Fig. 18, M + N + P + Q + R + S + T + U = four right angles.





27. When two lines, as A B and C D, Fig. 19, cut or cross each other, they are said to intersect. Their common point O is called their point of intersection, or simply their intersection.

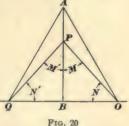
28. Two intersecting straight lines determine four angles having a common vertex. Any one of these angles and the angle on the opposite side of both lines, as the angles M and N, Fig. 19, are called **vertical angles** with respect to each other. Vertical angles may also be defined as those having a common vertex and in which the sides of the one are the prolongations of the sides of the other.

Since M and N are each the supplement of P, they are equal to each other. Any angle is equal to its vertical angle.

29. If two straight lines intersect and one of the angles is a right angle, the other three angles are right angles, and the lines are perpendicular to each other.

30. Two oblique lines drawn from the same point in a perpendicular to a line, and cutting off on that line equal distances from the foot of the perpendicular, are equal.

Let PO and PQ, Fig. 20, be two oblique lines drawn from the point P in the perpendicular AB, and let BO and BQ be equal. Then, by turning the right side of the figure about AB, it will coincide with the left side; O will fall on Q, and PO will coincide with PQ. Hence, PO is equal to PQ.



31. Every point in the perpendicular at the middle point of a straight line is equally distant from the ends of the line. Thus, in Fig. 20, P, which may be any point in the perpendicular AB at the middle point B of OQ is equally distant from Q and O.

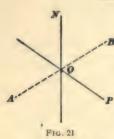
32. Two equal oblique lines drawn from the same point in the perpendicular to a straight line make equal angles with the straight line and with the perpendicular.

Since when PBO, Fig. 20, is brought to coincide with PBQ, PO coincides with PQ and BO with BQ, the angle M = angle M', and angle N = angle N'.

33. A line that divides an angle into two equal angles is called the **bisector** of that angle. In Fig. 20, *PB* is the bisector of OPQ, since M = M'.

34. Two points, each of which is equally distant from the two extremities of a line, determine a perpendicular bisecting the line. Thus, in Fig. 20, A and P are two points equally distant from Q and O and determine the perpendicular bisecting the line OQ.

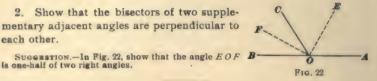
EXAMPLES FOR PRACTICE



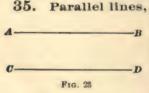
1. Show that the bisectors of two vertical angles are in the same straight line.

SUGGESTION.—In Fig. 21, show that the sum of the angles on one side of the bisector A B of the angle N O P is equal to the sum of the angles on the other side.

2 Show that the bisectors of two supplementary adjacent angles are perpendicular to each other.



PARALLELS

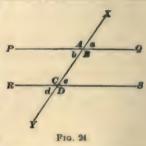


Parallel lines, Fig. 23, are straight lines that lie in the same plane and never meet, however far they are produced. Any two parallel lines have the same -D direction and are everywhere equally distant from each other.

36. When two parallel lines, as *PO* and *RS*, Fig. 24, are cut by a third line, as X Y, the cutting line X Y is called a secant line or a transversal.

The eight angles thus formed are named as follows: The

angles a, A, d, and D are exterior angles. The angles b, B, c, and Care interior angles. The pairs of angles a and d or A and Dare alternate-exterior angles. The pairs of angles b and c or B and C are alternate-interior The pairs of angles a angles. and c, A and C, b and d, or B and

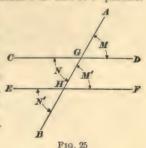


D are exterior-interior or corresponding angles.

37. When two parallel lines are cut by a transversal, the alternate-interior angles are equal.

Let CD and EF, Fig. 25, be the parallel lines and AB the transversal. The angles M and M' have their sides GD and HF parallel

and A G and G H in the same line; hence, the turning in changing from the direction HF to the direction HG is equal to the turning in changing from the direction G D to the direction G A. That is, angle A G D, or M, is equal to the angle G H F, or M', Art. 17. But angle M is *E*equal to angle N, Art. 28; therefore, angle N is equal to angle M'. In like manner, it can be shown that the angle D G His equal to the angle G H E.

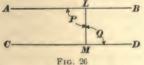


38. It follows from the preceding article that the alternate-exterior angles are equal; also, the exterior-interior angles. Thus, in Fig. 24, we have a = d, A = D; B = D, b = d; B = C, b = c.

39. In Fig. 24, the angle a and the angle A are supplementary adjacent angles, and their sum is, therefore, equal to two right angles. From this, and from the principle stated in the preceding article, it follows that any angle in Fig. 24 marked by a capital letter and any angle marked by a small letter are together equal to two right angles.

The principles stated in this and in the two preceding articles may be summed up as follows: When two parallel lines are cut by an oblique transversal, the four obtuse angles are equal to one another; the four acute angles are equal to one another; and any of the obtuse angles is the supplement of any of the acute angles.

40. If a straight line is perpendicular to one of two



parallel lines, it is perpendicular to the other also.

In Fig. 26, AB and CD are parallel, and LM is drawn perpendicular to AB. Then, since the alternate-interior angles

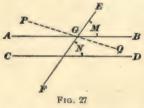
P and Q are equal, and since P is a right angle, Q must be a right angle also; that is, L M is perpendicular to C D.

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GEOMETRY, PART 1

41. The distance between two parallel lines is the length intercepted by the two parallels on any line perpendicular to them. Thus, L.M. Fig. 26, is the distance between AB and CD.

42. If two straight lines A B and C D, Fig. 27, are cut by a third straight line E F so that the exterior-interior angles M and N are equal, the two straight lines are parallel.



If AB were not parallel to CD, we might draw through G a line PQ that was parallel to C D. But then the exterior-interior angles N and E G Q would be equal (Art. 38), which is obviously inconsistent with the supposition that N is equal to M.

43. If two lines, as A B and C D. Fig. 28, are parallel to a third line.

as E F, they are parallel to each other.

Draw a transversal G H. Then, since A B is parallel to E F the alternate-interior angles M and N are equal; and, since A. CD is parallel to EF, the alternate-interior angles P and N are equal. We have, therefore, N = M, N = P, and, conse- Equently, M = P. As M and P are exteriorinterior angles, it follows, from Art. 42. that A B and C D are parallel.

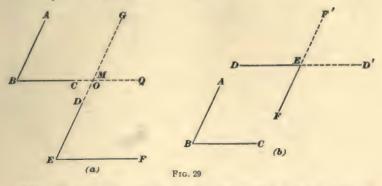


44. Two angles whose sides are respectively parallel and lie in the same or opposite directions from their vertexes are equal.

In Fig. 29 (a), BA and ED are parallel and extend in the same direction; also, BC and EF are parallel and extend in the same direction from the vertexes. Let O be the point of intersection of the sides BC and ED produced. Then, since BQ and EF are parallel, the exterior-interior angles E and M are equal; and, since BA and EG are parallel, the exterior-interior angles B and M are equal. Therefore, the angles B and E, being each equal to M, are equal to each other.

In Fig. 29 (b), BA and EF are parallel and extend in opposite d)rections; also, BC and ED are parallel and extend in opposite directions from the vertexes. Producing FE and DE, we have. by the preceding case, B = D'EF'. As DEF and D'EF' ar vertical

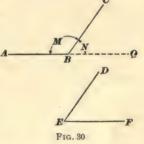
angles, they are equal, and, therefore, B, which is equal to D' E F', is also equal to D E F.



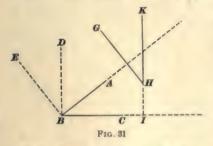
45. If one side of an angle is parallel to one side of another angle, the two extending in the same direction from the vertexes, and if the other sides of the two angles are

also parallel, but extend in opposite directions from the vertexes, the two angles are supplementary.

In Fig. 30, BC and ED are parallel and extend in the same direction, while BAand EF are parallel and extend in opposite directions from the vertexes. Producing AB, we have, by Art. 44, N = E. Now, M + N = two right angles; therefore, M + E = two right angles.



46. Two angles that have their sides perpendicular, each to each, are either equal or supplementary; they are equal



if both are acute or both obtuse; and supplementary if one is acute and the other obtuse.

In Fig. 31, let GH be perpendicular to AB, and KHperpendicular to BC. Draw BD parallel to KH, and BEparallel to GH. Then, by Art. 44, DBE is equal to right angles by taking OB.

KHG. Since EBA and DBC are right angles, by taking DBA

GEOMETRY, PART 1

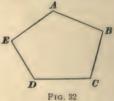
from each of them EBD is seen to be equal to ABC. Hence, the acute angle ABC is equal to the acute angle KHG. Also, when one angle is the acute angle ABC and the other is the obtuse angle GHI, since GHI is the supplement of KHG, it must be the supplement of ABC.

POLYGONS

DEFINITIONS

47. A polygon is a portion of a plane bounded by straight lines. The boundary lines are the sides of the polygon. The angles formed by the sides are the angles of the polygon. The vertexes of the

angles of the polygon are the vertexes of the angles of the polygon are the vertexes of the polygon. The broken line that bounds it, or the whole distance around it, is the **perimeter** of the polygon. Thus, ABCDE, Fig. 32, is a polygon; the sides of this polygon are AB, BC,

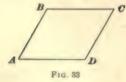


CD, DE, and EA; its angles are ABC, BCD, CDE, DEA, and EAB; and its vertexes are A, B, C, D, and E.

48. The number of vertexes of a polygon is the same as the number of sides.

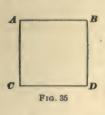
49. The least number of sides that a polygon can have is three, since two straight lines cannot enclose space.

50. Polygons are classified in various manners. One of these classifications is based on the number of sides. A polygon of three sides is a **triangle**; a polygon of four sides, a **quadrilateral**; a polygon of five sides, a **pentagon**; a polygon of six sides, a **hexagon**; a polygon of seven sides, a **heptagon**; a polygon of eight sides, an **octagon**; a polygon of nine sides, a **nonagon**; a polygon of ten sides, a **decagon**; a polygon of twelve sides, a **dodecagon**.



51. An equilateral polygon is a polygon whose sides are all equal. Thus, in Fig. 33, AB = BC = CD= DA; hence, ABCD is an equilateral polygon. 52. An equiangular polygon is Aa polygon whose angles are all equal. Thus, in Fig. 34, angle A = angle B= angle D = angle C; hence, ABDCis an equiangular polygon.

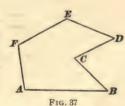




53. A regular polygon is a polygon in which all the sides and all the angles are equal. Thus, in Fig. 35, AB = BD = DC= CA; and angle A = angle B = angle D= angle C; hence, ABDC is a regular polygon. Some regular polygons are shown in Fig. 36.

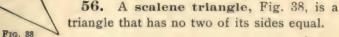


54. A reentrant angle of a polygon is an angle whose sides if produced through the vertex will enter the surface bounded by the perimeter of the polygon. Thus, BCD, Fig. 37, is a reentrant angle.



TRIANGLES

55. Triangles are classified with regard to their sides into scalene, isosceles, and equilateral triangles.

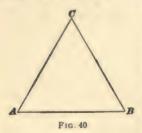


57. An isosceles triangle, Fig. 39, is a triangle that has two of its sides equal.



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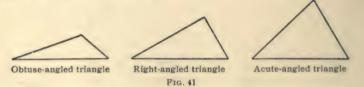
58. An equilateral triangle, Fig. 40, is a triangle that has its three sides equal. An equilateral triangle is a



particular kind of isosceles triangle. Thus, the triangle ABC, Fig. 40, may be regarded as an isosceles triangle whose equal sides are ABand AC, as an isosceles triangle whose equal sides are BA and BC, or as an isosceles triangle whose equal sides are CA and CB. All the statements made with regard to

isosceles triangles are, therefore, true of equilateral triangles.

59. Triangles are classified with regard to their angles into *right-angled*, *obtuse-angled*, and *acute-angled triangles*. See Fig. 41.



60. A right-angled triangle, or a right triangle, is a triangle having a right angle. The hypotenuse of a right triangle is the side opposite the right angle. The legs of a right triangle are the sides that include the right angle.

61. An obtuse-angled triangle is a triangle having an obtuse angle.

62. An acute-angled triangle is a triangle all the angles of which are acute.

63. An oblique triangle is a triangle that has no right angle. The class oblique triangles includes all obtuse-angled and acute-angled triangles.

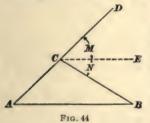
64. An equiangular triangle is a triangle whose three angles are equal.

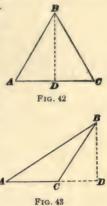
65. The base of a triangle is the side on which the triangle is supposed to stand. In a scalene triangle, any side may be considered as the base. In an isosceles triangle, the unequal side is usually, though not necessarily, taken as the base.

The angle opposite the base of a triangle is sometimes called the vertical angle of the triangle. In Figs. 42 and 43, AC is the base.

66. The altitude of a triangle is the length of a line drawn from the vertex of the angle opposite the base perpendicular to the base. Thus, in Figs. 42 and 43, the length of BD is the altitude.

67. An exterior angle of a triangle A^{2} is an angle formed by a side and the prolongation of another side. Thus, in





Figs. 43 and 44, the angle B CD, formed by the side B C and the prolongation of the side A C, is an exterior angle of the triangle A B C. The angle B CA is adjacent to the exterior angle B CD. The angles A and B are opposite-interior angles to the angle B CD.

68. In any triangle, an exterior angle is equal to the sum of the opposite-interior angles.

Let D C B, Fig. 44, be an exterior angle of the triangle A B C. Draw C E through C parallel to A B. Then, the angles M and A, being exterior-interior angles, are equal. Also, N and B, being alternate-interior angles, are equal. Hence, angle M plus angle N, that is, the exterior angle D C B, is equal to angle A plus angle B, or the sum of the opposite-interior angles.

69. The sum of the interior angles of a triangle is equal to two right angles.

In Fig. 44, the angles B C D and B C A, being supplementary adjacent angles, are together equal to two right angles. But, by the preceding article, the angle B C D is equal to the sum of the angles A and B. Hence, the sum of the three interior angles A, B, and B C A is equal to two right angles.

70. The following important propositions are immediate consequences of that stated in Art. 69:

1. If two angles of a triangle are known, or if their sum is known, the third angle can be found by subtracting their sum from two right angles.

2. If two angles of a triangle are equal, respectively, to two angles of another triangle, the third angle of the firstmentioned triangle is equal to the third angle of the other triangle.

3. A triangle can have but one right angle, or one obtuse angle.

4. In any right triangle, the two acute angles are complementary.

5. Each angle of an equiangular triangle is equal to onethird of two right angles, or two-thirds of one right angle.

6. From a point without a line, only one perpendicular to the line can be drawn.

EXAMPLES FOR PRACTICE

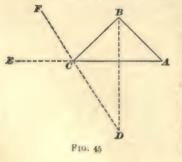
1. If one acute angle of a right triangle is one-third of a right angle, what is the value of the other? Ans. Two-thirds of a right angle

2. It one angle of a triangle is one-half of a right angle, and another is five-sixths of a right angle, what is the third angle?

Ans. Two-thirds of a right angle

3. The exterior angle of a triangle is 1² right angles, and one of the opposite-interior angles is one-fourth of a right angle; what are the other angles of the triangle?

Ans. {Other opposite-interior angle = $\frac{23}{20}$ = 1.15 right angles Angle adjacent to exterior angle = three-fifths of a right angle



4. Show that in the triangle ABC, Fig. 45, the bisector of the right angle ABC forms with the bisector of the exterior angle at Can angle that is equal to one-half of the angle A.

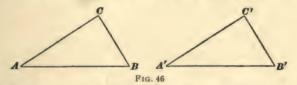
SUGGESTION.—Let B D be the bisector of A B C and F D the bisector of B C E. Then B C F is equal to C B D plus C D B, or C D B is equal to B C F minus C B D. Also, E C B is equal to C B A plus A, or A is equal to E C B minus C B A. Furthermore, E C B is equal to twice B C F and C B A is equal to twice C B D.

5. One angle of a triangle is one-half of a right angle: (a) What are the remaining two angles, if one is twice as large as the other? (δ) What kind of triangle is this?

Ans. $\begin{cases} (a) & \text{One-half of a right angle and one right angle} \\ (b) & \text{An isosceles right triangle} \end{cases}$

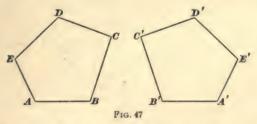
71. Two plane figures are equal when one can be placed on the other so that they will coincide in all their parts.

Thus, the triangles A B C and A' B' C, Fig. 46, are equal, because if A' B' C' is imagined to be lifted off the paper, moved over and placed on A B C, the sides A' B', B' C', and C' A' can be made to coincide



with AB, BC, and CA, respectively, and the angles A', B', and C' to coincide with the angles A, B, and C. It is evident, from the figure, that if the vertexes of the two triangles coincide, the triangles will coincide throughout, and are, therefore, equal.

The polygons ABCDE and A'B'C'D'E', Fig. 47, are equal, because A'B'C'D'E' can be imagined to be lifted, turned over, and placed on ABCDE so as to make the two polygons coincide in all their parts.

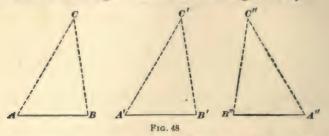


72. Two triangles are equal when a side and two adjacent angles of one are equal to a side and two adjacent angles of the other.

Let A' B', Fig. 48, equal A B, the angle A' equal the angle A, and the angle B' equal the angle B. Now, if A' B' C' is placed on A B Cso that A' B' coincides with its equal A B, with A' on A and B' on B, A' C' will take the direction A C; since the angle A' is equal to the angle A, and as B' is equal to B, B' C' will take the direction B C.

GEOMETRY, PART 1

Now, the point C will fall somewhere on the line A C, and also somewhere on the line B C, and since two lines can intersect in only one point, C must fall at the intersection of A C and B C, or at C. Hence, the vertexes of the triangles coincide and the triangles are equal.



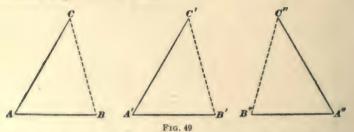
The same reasoning applies to the triangles A B C and A'' B'' C'', in which A B = A''B'', and A = A'', B = B''; but the triangle A'' B'' C'' must be imagined to be lifted and turned over before it can be placed on A B C.

73. The following important principles are consequences of the preceding proposition:

1. Two triangles are equal when one side and any two angles of one are equal, respectively, to one side and the two similarly situated angles of the other.

2. Two right triangles are equal when one side and one acute angle of the one are equal, respectively, to one side and the similarly situated acute angle of the other.

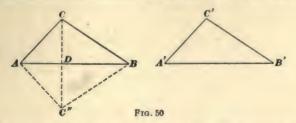
74. Two triangles are equal when two sides and the included angle of one are equal to two sides and the included angle of the other.



in Fig. 49, AB = A'B' = A''B'', AC = A'C' = A''C'', and A = A' = A''. If A'B'C' is placed on ABC, so that A' will coincide with A, and A'B' with AB, the rest of the triangles will evidently

coincide; for since A' = A, A' C' will take the direction A C, and since A' C' = A C, C' will coincide with C. The same reasoning applies to A'' B'' C'', after the latter triangle has been turned over.

75. Two triangles are equal when the three sides of the one are equal, respectively, to the three sides of the other.



In Fig. 50, let A'B', B'C', and C'A' be equal, respectively, to AB, BC, and CA. Place A'B'C' in the position ABC'', with its longest side A'B' coinciding with AB, and C'' on the opposite side of AB from C; then join C and C''. Now, AC is equal to AC'', and BC is equal to BC''; hence, A and B determine a perpendicular to CC'' at its mid-point (Art. 34). Then, by Art. 32, the angle CAD is equal to the angle C''AD, or to C'A'B', and by Art. 74 the triangles CAB and C'A'B' are equal.

76. In an isosceles triangle, the angles opposite the equal sides are equal.

Let A B C, Fig. 51, be an isosceles triangle in which A B = B C. Draw the bisector B D of the angle B. Then, by Art. 74, the triangles A B Dand C B D are equal. Therefore, A = C.



77. The equality of the triangles ABD Fig. 51 and CBD, Fig. 51, gives AD = DC, and angle M = angle N = one right angle (since M + N = two right angles). Hence,

1. The bisector of the vertical angle of an isosceles triangle bisects the base and is perpendicular to it.

2. Conversely, the perpendicular bisecting the base of an isosceles triangle passes through the vertex of the opposite angle and bisects that angle.

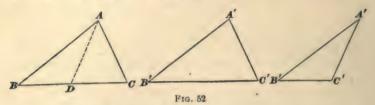
3. Also, the perpendicular drawn from the vertical angle of an isosceles triangle to the base, bisects both the base and the vertical angle.

GEOMETRY, PART 1

78. If two angles of a triangle are equal, the sides opposite these two angles are equal, and the triangle is therefore isosceles.

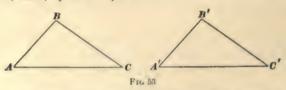
In Fig. 51, let A = C. Draw BD perpendicular to AC. The right triangles BDC and BDA have the common side BD, and acute angle A = C. Therefore (Art. 73), they are equal, and their hypotenuses BA and BC are equal.

79. It follows from Art. 76 that an equilateral triangle is also equiangular, and from the preceding article that an equiangular triangle is also equilateral.



80. If two sides of a triangle are equal, respectively, to two sides of another triangle, and the angle opposite one of these two sides in the first triangle is equal to the corresponding angle in the second triangle, the angles opposite the other two equal sides are either equal or supplementary.

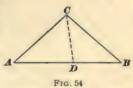
In Fig. 52, let A'C = AC, A'B' = AB, and the angle B' = B. Place A'B'C on ABC so that A'B' coincides with AB. Then since B' = B, B'C' will take the direction BC, and since A'C' joins B'C', C' must fall on BC, at either C or D. If C' falls at C, the triangles are equal and the angle C' = C; but if C' falls at D, ADBis the angle C', and ADB, the supplement of ADC, is the supplement of C, since, by Art. 76, ADC = C.



81. If two triangles have two sides of the one equal to two sides of the other, and the angles opposite one pair of the equal sides are right angles or equal obtuse angles, the triangles are equal. Since a triangle can have but one right or one obtuse angle, when the angles B and B', Fig. 53, are obtuse, the angle C cannot be the supplement of C, hence C must equal C.

82. Of two sides of a triangle, that is greater which is opposite the greater angle.

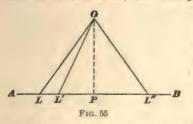
In the triangle ABC, Fig. 54, let the angle C be greater than the angle B. Draw CD, making with CB an angle BCD equal to the angle B. Then BCD is an isosceles triangle, and CD = DB. Therefore, AD + DB, or AB, is the same as AD+ DC, which is evidently greater than AC.



83. Of two angles of a triangle, that is greater which is opposite the greater side.

Let A and B be two angles of a triangle, a the side opposite A, and b the side opposite B. Suppose that a is greater than b. If A were equal to B, the triangle would be isosceles, and a = b. If B were greater than A, then by the preceding article, b would be greater than a. Therefore, since B cannot be equal to or greater than A, it must be less, or A must be greater than B.

84. If from a point O, Fig. 55, without a line A B, a perpendicular OP to the line is drawn, and also two oblique lines OL and OL', the oblique line OL, whose foot L is

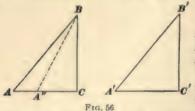


farther from the foot P of the perpendicular, is the greater of the two oblique lines.

Suppose the two oblique lines OL and OL' to be on the same side of the perpendicular. Since OL'P is a right triangle and

OPL' the right angle, the angle OL'P is acute; also, the angle OL'Lis obtuse, since it is the supplement of OL'P. As the triangle OLL'can have but one obtuse angle, OL'L is greater than OLP, and, therefore (Art. 82), OL is greater than OL'. If OL lies on the opposite side of the perpendicular from OL', as in the position OL'', and if PL'' = PL, which is greater than OL', then, by Art. 30, OL'' = OL, which is greater than OL'.

85. If the hypotenuse, as AB, Fig. 56, and one leg. as BC, of a right triangle are equal, respectively, to the hypotenuse and one leg of another right triangle, as A' B' C', , the two triangles are equal.



Place A'B'C' on ABC, so that B'C' will coincide with its equal BC. Since B'C'A' is a right angle, CA' will take the direction CA; and, since B'A' = BA, A'y' must fall on A; for if it fell to the right of A, as at A'', the hypotenuse BA'', or B'A', would be less

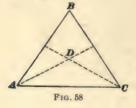
than BA (Art. 84); and, if A' fell on the left of A, the hypotenuse B'A' would be greater than BA.

EXAMPLES FOR PRACTICE

1. Show that, if two intersecting lines, as AB and DC, Fig. 57, bisect each other, the lines AC and DB are parallel.

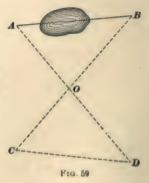


2. If the value of the unequal or vertical angle of an isosceles triangle is two-fifths of a right angle, what is the value of each of the base angles? Ans. Four-fifths of a right angle



3. Show that the bisectors of the base angles of an isosceles triangle form with the base an isosceles triangle; or that, ADC, Fig. 58, is an isosceles triangle.

4. Show that the length of the inaccessible line AB, Fig. 59, can be found by measuring AO and BO, then making OD = OB and OC = OA, and finally measuring CD.



QUADRILATERALS

86. There are three kinds of quadrilaterals: the parallelogram, the trapezoid, and the trapezium.

87. A parallelogram is a quadrilateral whose opposite sides are parallel. There are four kinds of parallelograms: the *rectangle*, the *square*, the *rhomboid*, and the *rhombus*.

88. A rectangle, Fig. 60, is a parallelogram whose angles are all right angles.

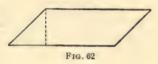


89. A square, Fig. 61, is a rectangle whose sides are equal.

FIG. 61

90. A rhomboid. Fig. 62, is a quadrilateral whose opposite sides are parallel, and whose angles are not right angles.

92. A trapezoid, Fig. 64, is a quadrilateral that has only two





of its sides parallel.

91. A rhombus, Fig. 63, is a rhomboid having equal sides.

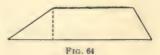




FIG. 65

93. A trapezium, Fig. 65, is a quadrilateral having no two sides parallel.

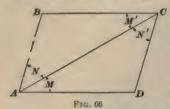
94. The altitude of a parallelogram, or of a trapezoid, is the length of the perpendicular distance between the

parallel sides. See dotted line in Figs. 62, 63, and 64.

GEOMETRY, PART 1

95. A diagonal of a quadrilateral is a straight line drawn from the vertex of any angle of the quadrilateral to the vertex of the angle opposite. A diagonal divides a quadrilateral into two triangles. See Figs. 60 and 65.

96. In a parallelogram, as ABCD, Fig. 66, the opposite sides and opposite angles are equal: that is, AB = DC, AD= BC, angle A = angle C, angle B = angle D.



Draw the diagonal AC. Then. angle M = angle M', and N = N'(Art. 37). The triangles ADC and ABC, having the common side ACand the adjacent angles M and N'equal, respectively, to M' and N, are equal (Art. 72). Therefore, A D = B C, A B = D C, and angle B = angle D. Also, since M = M' and N = N', it follows that M + N,

or BAD, is equal to M' + N', or BCD. 97. The diagonal of a parallelogram divides the parallel-

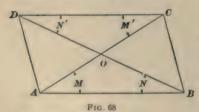
ogram into two equal triangles.

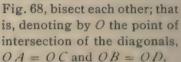
98. Parallel lines intercepted between parallel lines are equal. Thus, if the parallels AB and CD, Fig. 67. are cut by the parallels EF. GH. IJ. KL.



we have, from Art. 96. MN = OP = OR = ST.

99. The diagonals of a parallelogram, as AC and BD,





In the triangles A O B and DOC, AB = DC (Art. 96), M = M' and N = N' (Art. 37). Therefore, the triangles are equal



EXAMPLES FOR PRACTICE

1. Show that if the diagonals of a quadrilateral bisect each other the figure is a parallelogram.

SUGGESTION.—In Fig. 68, assume that OA = OC, OB = OD. Then show that triangle B OC = triangle A OD, and triangle A OB = triangle D OC.

2. Show that the diagonals of a rectangle are equal.

SUGGESTION.—Show that in any rectangle A B C D the triangle A B C = triangle A B D.

3. Show that if the opposite sides of a quadrilateral are equal, the figure is a parallelogram.

SUGGESTION.-Draw the diagonal. Then, by Art. 75, the triangles formed are equal.

4. Show that if two sides of a quadrilateral are equal and parallel, the figure is a parallelogram.

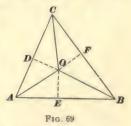
5. Show that if one angle of a parallelogram is a right angle, the parallelogram is a rectangle.

ADDITIONAL PROPERTIES OF TRIANGLES

100. The bisectors of the three angles of a triangle meet in a point.

In the triangle A B C, Fig. 69, draw the bisectors of the angles A and B and let them meet at O. Join C and O, and draw the perpen-

diculars from O to the sides of the triangle. Then, in the right triangles B O F and B O E, B O is common and the angle O B F= angle O B E. Hence, by Art. 73, these triangles are equal. Therefore, O F = O E. In a similar manner it can be shown that O D = O E. Therefore, O D = O F. The right triangles O F C and O D C, having O D = O F and O C common, are equal (Art. 85). Hence, angle O C F = angle



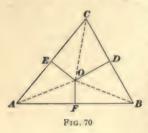
O C D; that is, O C, which meets the bisectors A O and B O in O, is the bisector of the angle C.

101. Any point in the bisector of an angle is equally distant from the sides of the angle. For it has just been shown that, in Fig. 69, OF = OE,

102. The perpendiculars erected at the middle points of the three sides of a triangle meet in a point equally distant from the vertexes of the triangle.

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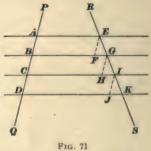
In Fig. 70, draw the perpendiculars to CB and AC at their mid-



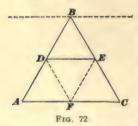
points D and E, and let O be the point in which these perpendiculars meet. Now, O, being in OD, is equally distant from Cand B (Art. **31**), that is, OB = OC: and being in OE, is equally distant from Aand C; that is, OA = OC. From these two equalities it follows that OB = OA. Therefore, the perpendicular to AB at its middle point F passes through O. (Art. **77**).

103. If several parallel lines intercept equal distances on one transversal, they intercept equal distances on any other transversal.

In Fig. 71, let the parallels A E, B G, CI, DK intercept the equal distances A B, B C, and CD on the transversal PQ, and let RS be any other transversal. Draw EF, GH, IJ, parallel to AB. Then, by Art. 98, EF = AB, GH = BC, IJ = CD. Hence, EF = GH = IJ. In the triangles EFG, GHI, and IJK, angle E = angle G = angle I (Art. 38), and angle F = angle H = angle J (Art. 44).



Hence, by Art. 72, these triangles are equal, and, therefore, EG = GI = IK.



104. A line parallel to one of the sides of a triangle and bisecting one of the other sides, bisects the third side also.

In Fig. 72, let DE bisect AB and be parallel to AC. Draw a line through B parallel to AC. Then since the three parallels intercept equal parts on AB, they intercept equal

parts on BC; that is, BE = EC.

105. A line joining the middle points of two sides of a triangle is parallel to the third side and equal to one-half of that third side.

In Fig. 72, let DE join D and E, the middle points of AB and BC. The first part of this proposition follows at once from the preceding article. Let F be the middle point of A C, and draw FE. This line is parallel to A B, and, therefore, A D E F is a parallelogram. Consequently (Art. 96), $DE = AF = \frac{1}{4}AC$.

106. The lines joining the middle points of the three sides of a triangle divide it into four equal triangles.

The diagonal DF, Fig. 72, divides the parallelogram ADEF into two equal triangles AFD and DFE. Likewise, the diagonal EFdivides DECF into two equal triangles DFE and EFC; and the diagonal DE divides the parallelogram BDFE into the two equal triangles DFE and BDE. Hence, triangle AFD = triangle DFE= triangle EFC = triangle BDE.

107. Any of the parallelograms ADEF, FCED, DBEF, Fig. 72, is equal to one-half the given triangle, since it contains two of the four equal triangles into which the given triangle is divided.

108. A line, as EF, Fig. 73, parallel to the bases AB and DC of a trapezoid and passing through the middle point E of one of the non-parallel sides, passes through the middle point of the other non-parallel side and is equal to one-half the sum of the parallel $p_{abs} = 0$

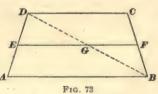
Since the parallels A B, E F, and D C intercept equal parts on A D, they intercept equal parts on B C (Art. 103); that is, BF = FC.

Draw *B D*, meeting *E F* in *G*. Then, by Art. 105, in the triangle *D C B*, *F G* is one-half *C D*. Also, in the triangle *A D B*, *G E* is one-half *B A*. Hence, FG + GE, or $FE_{,} = \frac{1}{2}(CD + BA)$.

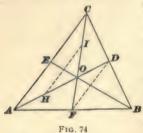
109. The medians of a triangle are the lines drawn from the vertexes to the middle points of the opposite sides.

110. The medians of a triangle meet in a point whose distance from any vertex is two-thirds the length of the median from that vertex.

In Fig. 74, AD, BE, CF are the median lines of the triangle ABC; they meet at O, and $AO = \frac{3}{2}AD$, $BO = \frac{3}{2}BE$ and $CO = \frac{3}{2}CF$.



Let A D and CF meet at O. Join I and H, the mid-points of CO and



A O, respectively; also join D and F. Then, in the triangle A O C, I H is parallel to A C and equal to one-half A C (Art. 105). Also, in triangle A B C, D F is parallel to A C and equal to one-half A C. Hence, I H and D F are equal and parallel. It follows that the triangles D O F and H O I are equal, and that, therefore, HO = OD. B But, by construction, A H = HO. Hence, A H = HO = OD, whence, $A O = \frac{2}{3}AD$. Similarly $C O = \frac{2}{3}CF$. That is, one

FIG. 74

median cuts off on the other median two-thirds of the distance from the vertex to the opposite side.

POLYGONS IN GENERAL

111. Two polygons are equal when they can be divided into the same number of triangles equal each to each and

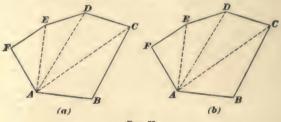
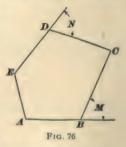


FIG. 75

similarly placed. Thus, the polygons shown at (a) and (b) in Fig. 75 are composed of the same number of triangles

equal each to each and similarly placed, and it is evident that one polygon can be placed on the other so that they will coincide throughout; hence, they are equal.

112. An exterior angle of a polygon is an angle formed by any side and the prolongation of an adjacent side. In Fig. 76, the angles M



and N are exterior angles of the polygon A B C D E.

113. A diagonal of a polygon is any line joining two vertexes not adjacent to the same side of the polygon. Thus, in Fig. 75, AC, AD, and AE are diagonals of the polygon ABCDEF.

114. The sum of the interior angles of any polygon is equal to two right angles multiplied by a number that is two less than the number of sides of the polygon.

Let (a), Fig. 75, be any polygon. Draw the diagonals from one vertex and thus divide the polygon into triangles. It is seen that the first triangle A B C and the last triangle A F E, each contains two sides of the polygon, while each of the other triangles contains but one side of the polygon. Thus, the number of triangles formed is two less than the number of the sides of the polygon. Hence (Art. 69), the sum of the angles of the triangles, or of the polygon, is two right angles multiplied by a number that is two less than the number of sides of the polygon.

115. Let n = number of sides of a polygon;
S = sum of interior angles of the polygon, expressed in right angles.

Then,

$$S = 2(n-2) = 2n-4$$

If n = 4, then $S = 2 \times 4 - 4 = 4$ right angles; that is, the sum of the angles of a quadrilateral is equal to four right angles.

EXAMPLE 1.—What is the value of one of the interior angles of an equiangular hexagon?

SOLUTION.—The number of sides of a hexagon is six; hence, applying the formula, $S = 2 \times (6 - 2) = 8$ right angles, that is, the sum of the interior angles of a hexagon is equal to eight right angles. Since the hexagon is equiangular, one of the angles is equal to one-sixth of eight right angles, or $1\frac{1}{2}$ right angles. Ans.

EXAMPLE 2.—If one of the interior angles of an equiangular polygon is equal to $1\frac{3}{7}$ right angles, what is the name of the polygon?

SOLUTION.—If one of the interior angles is equal to $1\frac{3}{7}$ or $\frac{10}{7}$ right angles, their sum S is equal to $\frac{10}{7} \times n = \frac{10}{7}$. But from the formula, S = 2n - 4. Therefore, $\frac{10}{7}n = 2n - 4$; whence, n = 7. A polygon of seven sides is a heptagon; therefore, the polygon is a heptagon. Ans.

EXAMPLES FOR PRACTICE

1. Show that if two angles of a quadrilateral are supplementary the other two angles are supplementary.

2. In a triangle A B C, the angle C is twice the angle B. Show that the line that bisects the angle C meets the line A B at a point D so that CD = BD.

SUGGESTION.—Half the angle C = angle B. Then in the triangle CDB, angle BCD = angle CBD.

3. What is the value of one of the interior angles of an equiangular octagon? Ans. 1¹/₄ right angles

4. (a) What is the value of one of the interior angles of an equiangular quadrilateral? (b) What kind of quadrilateral is it?

Ans. $\begin{cases} (a) & \text{One right angle} \\ (b) & \text{Rectangle} \end{cases}$

5. If one of the interior angles of an equiangular polygon is equal to l_{Ψ}^{δ} right angles, what is the name of the polygon? Ans. Nonagon

THE CIRCLE

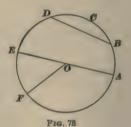
DEFINITIONS AND GENERAL PROPERTIES

116. A circle, Fig. 77, is a plane figure bounded by a curved line every point of which is equally distant from a point within called the center.



117. The circumference of a circle is the line that bounds the circle. The term circle is often used in the sense of circumference.

118. The diameter of a circle is a straight line drawn through the center and terminated at both ends by the circumference. Thus, AE, Fig. 78, is a diameter of the circle whose center is O.



119. The radius of a circle is any straight line drawn from the center to the circumference. The plural of *radius* is *radii*. Thus, OA, OE, and OF, Fig. 78, are radii of the circle whose center is O.

120. The distance from the center to the circumference is, by the definition of a circle, the same for all points in the same circle; hence, all radii are equal.

121. When any two radii, as OA and OE, Fig. 78, are in the same straight line, they form a diameter. Hence, the length of the diameter is twice the length of the radius.

122. An arc of a circle is any part of its circumference, as DCB, Fig. 78.

123. An arc equal to one-half the circumference is a semi-circumference; and an arc equal to one-fourth the circumference is a quadrant.

124. A chord is a straight line, as B D, Fig. 78, joining any two points in a circumference, or it is a line joining the extremities of an arc.

125. The longest chord that can be drawn in a circle is a chord that passes through the center and is, therefore, a diameter.

126. An arc of a circle is said to be subtended by its chord. Thus, the arc BCD, Fig. 78, is subtended by the chord BD.

Every chord in a circle subtends two arcs. Thus, BD subtends both the arcs BCD and BAFED.

When an arc and its chord are spoken of, the arc less than a semi-circumference is meant, unless the contrary is stated. The shorter arc is usually referred to by naming the letters at its extremities; thus, the arc B C D is called the arc B D.

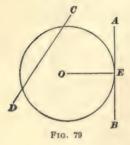
127. A segment of a circle is a part of the circle enclosed by an arc and its chord. In Fig. 78, the part of the circle between the chord BD and the arc BD is a segment.

GEOMETRY, PART 1

A segment equal to one-half the circle is a semicircle.

128. A sector of a circle is the space included between an arc and the two radii drawn to the extremities of the arc. In Fig. 78, the space included between the arc FE and the radii OF and OE is a sector.

129. Two circles are equal when the radius or diameter of one is equal to the radius or diameter of the other.



130. A tangent to a circle is a line that touches the circumference in only one point. In Fig. 79, A B is tangent to the circle whose center is O. The point E at which the tangent touches the circumference is the point of contact, or point of tangency.

131. Two circles are tangent when they touch each other in one point only, as in Fig. 80. When two circles are tangent, they are tangent to the same straight line at the point of tangency.

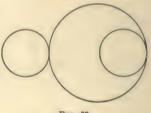
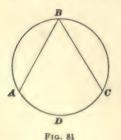


FIG. 80

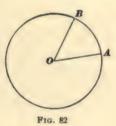
132. A secant, as the term is used in geometry, is a line that intersects the circumference of a circle in two points. In Fig. 79, CD is a secant to the circle whose center is O.

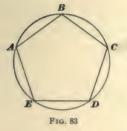


133. An inscribed angle is an angle whose vertex lies on the circumference of a circle, and whose sides are chords. In Fig. 81, *ABC* is an inscribed angle.

32

134. A central angle, or an angle at the center, is an angle whose vertex is at the center of a circle and whose sides are radii. Thus, in Fig. 82, *AOB* is a central angle.





135. An inscribed polygon is a polygon each of whose vertexes lies on the circumference of a circle, as in Fig. 83. The circle is said to be circumscribed about the polygon.

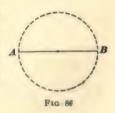
136. An inscribed circle is a circle whose circumference touches but does not intersect each of the sides of a polygon, as in Fig. 84. The polygon is said to be circumscribed about the circle.





137. Concentric circles are circles having the same center. See Fig. 85.

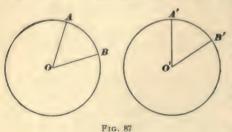
138. Every diameter of a circle bisects the circle and its circumference. Thus, in Fig. 86, both the arc and the portion of the circle on one side of the diameter AB are equal, respectively, to the arc and the portion of the circle on the other side.



GEOMETRY, PART 1

139. In the same circle, or equal circles, equal angles at the center intercept equal arcs on the circumference.

Let O and O', Fig. 87, be equal circles, and A O B and A' O' B' equal angles. Place the circle O' on O so that the point O'



coincides with O and the line O'B' takes the direction OB. Then, since OBand O'B' are equal, being radii of equal circles, B'will fall on B, and, since the angle O' is equal to the angle O, the line O'A'will take the direction of OA, and, being equal to OA, its extremity A'

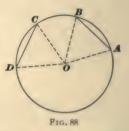
will fall on A. Hence, the arcs AB and A'B' will coincide and are equal.

140. In the same circle, or equal circles, equal arcs are intercepted by equal angles at the center.

Let O and O', Fig. 87, be equal circles, and A B and A' B' equal arcs. Place the circle O' on the circle O, with the points O' and A' on O and A, respectively. Then, since the arc A' B' is equal to the arc A B, B' will fall on B. Then the angle O' is equal to the angle O, as the vertex and the sides of the angles coincide.

141. In the same circle or equal circles, equal chords subtend equal arcs.

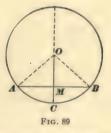
Let AB and CD, Fig. 88, be equal chords. Draw the radii AO, BO, CO, and DO, joining A, B, C and D to O. Then the triangles AOB and COD, having three sides of one equal to three sides of the other, are equal. Hence, the angle AOB is equal to the angle COD, and, therefore (Art. 139), the arc AB is equal to the arc CD.



142. In the same circle, or equal circles, equal arcs are subtended by equal chords.

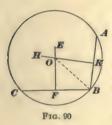
143. A perpendicular from the center of a circle to a chord bisects the chord and the arc subtended by it.

Let OM, Fig. 89, be drawn from O perpendicular to the chord AB. Join O to A and B. The triangle AOB is isosceles, since the two sides OA and OB are radii of the same circle. Therefore (Art. 77), AM = MB. Also, AOM = MOB (Art. 77); therefore (Art. 139), are $AC = \operatorname{arc} CB$.



144. The perpendicular erected at the middle of a chord passes through the center of the circle and bisects the arc subtended by the chord.

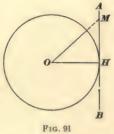
145. Through any three points not in a straight line a circumference can be passed.



Let A, B, and C, Fig. 90, be any three points. Draw AB and BC. At the middle point of ABdraw KH perpendicular to AB; at the middle point of CB draw FE perpendicular to BC and meeting KH at O. As O is a point in the perpendiculars at the middle points of AB and BC, it is equally distant from A, B, and C. Therefore, a circle with O as center and OB as radius will pass through A, B, and C.

146. A straight line perpendicular to a radius at its extremity is tangent to the circle.

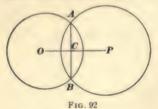
Let AB, Fig. 91, be perpendicular to OH at its extremity H. As OH is perpendicular to AB it is shorter than any other line, as OM, drawn from O to AB. Hence, M is without the circle, and any point in AB other than His without the circle. Therefore, AB touches the circle in only the point H, and is, consequently, tangent to the circle.



147. A perpendicular to a tangent at the point of tangency passes through the center of the circle.

148. A tangent to a circle is perpendicular to the radius drawn to the point of tangency.

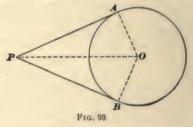
149. If two circles intersect, the line joining their centers bisects at right angles the line joining the points where the circles intersect.



Let the two circles whose centers are O and P, Fig. 92, intersect at A and B. The point P, being the center of a circle, is equally distant from A and B, points on the circumference. Similarly, O is equally distant from A and B. Hence, by Art. 34, O and P determine the perpendicular bisecting AB.

150. The two tangents from a point to a circle are equal.

Let PA and PB, Fig. 93, be tangents from P to the circle whose center is O. Draw OA, OP, OB. Then the triangles POB and POA are right triangles (Art. 148). In these triangles, PO is common and OAis equal to OB. Hence, the triangles are equal, and PA = PB.

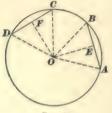


151. The line joining an external point to the center of a circle bisects the angle made by the two tangents drawn from the point to the circle. Thus, the angle OPA, Fig. 93, is equal to the angle OPB.

EXAMPLES FOR PRACTICE

1. Show that the line joining the intersection of two tangents to the center of the circle bisects the chord joining the points of tangency.

2. Show that the bisector of the angle between two tangents passes through the center of the circle,



3. Show that in the same circle, or equal circles, equal chords are equally distant from the center.

SUGGESTION.—Draw OE and OF. Fig. 94, perpendicular to the equal chords AB and CD. Then what is true of the triangles AEO and DOF?

4. Show that the tangents to a circle at the extremities of a diameter are parallel.

5. Show that in any circle a chord parallel Frg. 94 to a tangent is bisected by the diameter drawn to the point of contact.

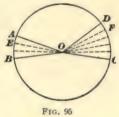
MEASUREMENT OF ANGLES

152. The ratio of one quantity to another of the same kind is the number of times that the first contains the second. When both quantities are represented by numbers, their ratio is the same as the quotient obtained by dividing one of the numbers by the other.

153. In the same circle, or equal circles, two central angles have the same ratio as their intercepted arcs; that is, in Fig. 95, angle A OB: angle C OD = arc AB: arc CD.

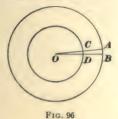
Suppose the arc AB to be three-fifths of the arc CD. Divide AB into three equal parts, and CD into five equal parts, as shown, and join the points of division with the center.

Since AB: CD = 3:5, or $\frac{AB}{CD} = \frac{3}{5}$, it follows that one-third of AB is one-fifth of CD; that is, arc $AE = \operatorname{arc} DF$, and, therefore, angle $AOE = \operatorname{angle} DOF$. We have, therefore, angle $AOB = 3 \times \operatorname{angle} AOE$, angle COD $= 5 \times \operatorname{angle} DOF = 5 \times \operatorname{angle} AOE$; whence, angle AOB $= \frac{3 \times \operatorname{angle} AOE}{\operatorname{angle} AOE} = \frac{3}{5} = \frac{\operatorname{arc} AB}{\operatorname{arc} CD}$.



154. Since the angle at the center and its intercepted arc increase and decrease in the same ratio, it is said that an angle at the center is measured by its intercepted arc.

155. The whole circumference of a circle is divided into 360 equal parts, called degrees. A degree is divided into 60 equal parts, called minutes: and a minute is divided



into 60 equal parts, called seconds. Degrees, minutes, and seconds of arc arc used as units for measuring circular arcs. Since the circumference of every circle contains 360 degrees, the length of a degree differs in different circles. Thus, if AOB, Fig. 96, is an angle of 1°, AB is an arc of 1° in the larger circle

and CD is also and arc of 1° in the smaller concentric circle. A degree of the earth's equator is a little more than 69 miles long; and a degree of the circumference of a circle whose diameter is 360 inches is 3.1416 inches long.

Degrees, minutes, and seconds are indicated by °, ', ". Thus, 25° 3' 10" means 25 degrees, 3 minutes, and 10 seconds.

Since a right angle intercepts one quarter of a circumference, the number of degrees measuring it is $360 \div 4$ = 90°. The number of degrees measuring an angle equal to one-half of a right angle is $90° \div 2 = 45°$.

Usually, the magnitude of an angle is expressed by stating the number of degrees that it subtends. Thus, a right angle is referred to as an angle of 90° ; one-third of a right angle, as an angle of 30° , etc.

156. An inscribed angle is measured by one-half the intercepted arc. Thus, in Fig. 97, the angle ABC is measured by one-half the arc ADC.

Draw the diameter BOD and the radii OC and OA. The



angle COD, the exterior angle of the triangle OBC, is equal to the angle OBC plus the angle OCB. But the angle OCB is equal to the angle OBC, as they are opposite the equal sides of an isosceles triangle. Hence, the angle COD, which is measured by the arc CD, is equal to $2 \times OBC$. Therefore, OBC is measured by one-half the arc CD. Similarly, the angle OBA is measured by one-half the arc AD. Therefore, the angle ABC is measured by one-half the arc AD plus one-half the

arc DC; that is, by one-half the arc AC.

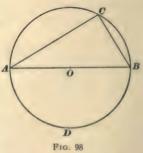
157. In the same circle, or equal circles, equal arcs are intercepted by equal inscribed angles.

158. All angles inscribed in the 4 same segment are equal.

159. Any angle inscribed in a semicircle is a right angle.

The angle A CB, Fig. 98, is measured by one-half the arc A DB, which is a semi-

circumference. As a semi-circumference contains 180° , the angle A CB is measured by one-half of 180° , or 90° , and is, therefore, a right angle.

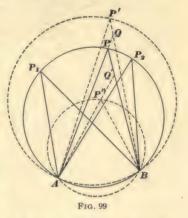


160. The vertexes of all the angles of a given magnitude whose sides pass through two fixed points, lie on a circle that passes through the two fixed points and any one of the vertexes.

In Fig. 99, let A P B be an angle of the given magnitude and A

and B the fixed points. Through A, B, and P, pass a circle. Now, any angle, as AP_1B or AP_2B , whose sides pass through A and Band whose vertex lies on the arc APB is (Art. 158) equal to the given angle A P B.

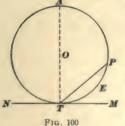
Again, any angle, as A P' B, whose sides pass through A and B and whose vertex lies without the arc APB is less than the angle APB. For if AP is produced to meet BP' at Q, the angle A PB being an exterior angle of the triangle BPQ, is equal to PQB + PBQ and is therefore greater than PQB, and, as PQB



is greater than A P' B (since POB = A P' B + O A P'), it follows that A P B is greater than A P' B.

In like manner it can be shown that any angle, as A P'' B, whose sides pass through A and B and whose vertex lies within the arc A P B. is greater than the given angle A P B.

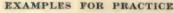
161. An angle formed by a tangent, as TM, Fig. 100,

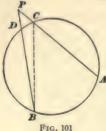


and a chord, as TP, is measured by one-half the intercepted arc TEP.

Draw the diameter TOA. Then MTAis a right angle and is, therefore, measured by one-half the semi-circumference TEPA. The angle PTA is measured by one-half the arc PA. Hence, the angle MTP, equal to MTA minus PTA, is measured by one-half the difference between the semicircumference and PA; that is, by one-

half the arc T E P.



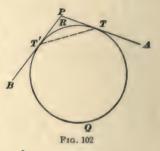


1. Prove that the angle BPA, Fig. 101, formed by two secants intersecting without the circumference is measured by one-half the difference of the intercepted arcs AB and CD; that is, by $\frac{1}{2}(AB - CD)$.

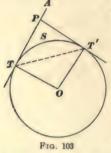
SUGGESTION.-Join C and B. Then angle BCA is an exterior angle of the triangle BCP, and angle BPC is equal to angle ACB minus angle DBC.

2. Show that the angle APB, Fig. 102, formed by two tangents PTand PT' is measured by one-half the difference of the intercepted arcs TQT'and TRT'.

SUGGESTION,—Join T and T'. Then ATT'is an exterior angle of triangle TT'P, while ATT' and PT'T are angles formed by a tangent and a chord.



162. The angle of intersection of two tangents is the angle formed by one tangent with the prolongation of the



other tangent. Thus, the angle A P T', Fig. 103, is the angle of intersection of the two tangents TP and PT'.

163. The angle of intersection of two tangents is equal to the central angle whose sides pass through the points of tangency.

In Fig. 103, join TT'. Then, the angle APT'is equal to the sum of the equal angles PTT'and PT'T. But each of these angles is made by

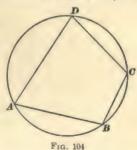
a tangent and a chord and is, therefore, measured by one-half of the arc TST'. Hence, the angle APT' is measured by the arc TST'. The central angle O is also measured by this arc; therefore, the angle O is equal to the angle APT'.

164. The opposite angles of an inscribed quadrilateral are supplementary; that is, their sum is equal to two right angles or 180° .

In Fig. 104, the angle B is measured by one-half the arc ADC, and

the opposite angle D is measured by onehalf the arc ABC. The sum of the arcs ADC and ABC is a circumference, or 360°. Hence, the sum of the angles ADC and ABC is measured by one-hal? of 360°, or 180°.

165. If the opposite angles of a quadrilateral are supplementary, the quadrilateral can be inscribed in a circle.



EXAMPLE 1.—What is the number of degrees in each angle of an equilateral triangle?

SOLUTION.—The sum of the three angles of the triangle is two right angles, or 180°. Since the three angles are equal, each angle is one-third of 180°, or $\frac{180^\circ}{3} = 60^\circ$. Ans.

EXAMPLE 2.—The unequal angle of an isosceles triangle is $75^{\circ} 32' 10''$; what is the magnitude of each of the equal angles?

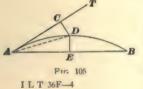
SOLUTION.—Since the sum of the three angles is 180° , the sum of the two equal angles is 180° minus the other angle, or $180^{\circ} - 75^{\circ} 32' 10'' = 104^{\circ} 27' 50''$, and each of them is one-half of this sum, or $(104^{\circ} 27' 50'') \div 2 = 52^{\circ} 13' 55''$. Ans.

EXAMPLE 3.—The exterior angle of a triangle is $124^{\circ} 3' 40''$, and one of the opposite-interior angles is 60° ; find the other two angles of the triangle.

SOLUTION.—Let the given exterior angle be denoted by A, the given interior angle by B, the other opposite-interior angle by C, and the third angle of the triangle by A'. (Let the student draw the triangle and mark these angles.) Then, A = B' + C; whence, C = A - B $= 124^{\circ} 3' 40'' - 60^{\circ} = 64^{\circ} 3' 40''$. Ans. Also, $A + A' = 180^{\circ}$; whence, $A' = 180^{\circ} - A = 180^{\circ} - 124^{\circ} 3' 40'' = 55^{\circ} 56' 20''$. Ans.

EXAMPLES FOR PRACTICE

1. Show that the only parallelogram that can be inscribed in a circle is a rectangle.



2. Show that if from a point A, Fig. 105, on the arc of a circle a chord A B and a tangent A T are drawn, the perpendiculars DC and DE drawn to them from the middle point D of the subtended arc are equal.

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3. The angle of intersection of two tangents is 100° ; find the number of degrees in each angle formed by the tangents and the chord through the points of contact. Ans. 50°

4. One of the acute angles of a right triangle is 50°; what is the magnitude of the other acute angle? Ans. 40°

5. Each of the equal angles of an isosceles triangle is 45° ; show that the triangle is right-angled.

6. Two angles of a triangle are 37° 41' 36" and 86° 51' 2"; what is the value of the other angle? Ans. 55° 27' 22"

GEOMETRY (PART 2)

Serial 778B

Edition 1

PROPORTION

DEFINITIONS AND GENERAL PRINCIPLES

1. A proportion is an equality of ratios or of fractions. Thus, the fractions $\frac{4}{5}$ and $\frac{8}{10}$, being equal, form a proportion. In general, if $\frac{a}{1}$ is equal to $\frac{c}{1}$, these two ratios or fractions form a proportion, which may be written in any of the following forms: $\frac{a}{b} = \frac{c}{d}$, a : b = c : d, a : b :: c : d. When written in either of the last two forms, the proportion is read a is to b as c is to d.

2. Properties of Proportions.—The first and the fourth term of a proportion are called the extremes; the second and the third, the means. Thus, in the proportion a:b= c : d, the extremes are a and d, and the means, b and c.

3. If any four quantities are in proportion, the product of the extremes is equal to the product of the means. This principle follows at once from the definition of a proportion. as will be explained presently. If a, b, c, and d, are in proportion, then, by the definition,

$$\frac{a}{b} = \frac{c}{d} \qquad (1)$$

This equation may be treated the same as any other algebraic equation. Both members of the equation may be

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multiplied or divided by the same quantity, or the same quantity may be added to or subtracted from both members, and the proportion may thus be changed to a great number of forms without destroying the equality of the ratios. Different names are applied to these changes, some of the most common of which are given in the following articles.

In order to show that the product of the means is equal to the product of the extremes, multiply both members of equation (1) by b d to clear of fractions; the equation then becomes

$$a d = b c$$
 (2)

4. It is evident that if two fractions are equal, their reciprocals are also equal. If $\frac{a}{b} = \frac{c}{d}$, then $\frac{b}{a} = \frac{d}{c}$; that is, if a : b = c : d, we have also b : a = d : c.

Taking the reciprocal of a fraction is called **inverting** the fraction. The operation of inverting the two fractions of a proportion is called **inversion**.

5. If both members of equation (2), Art. 3, are divided by cd, there results

$$\frac{a}{c} = \frac{b}{d}$$
, or $a: c = b: d$

Or, if both members of equation (2) are divided by ba, the result is

$$\frac{d}{b} = \frac{c}{a}$$
, or $d: b = c: a$

Therefore, either the means or the extremes of a proportion can be interchanged. This operation is called **alternation**.

6. If 1 is added to each member of equation (1), Art. 3, the equation becomes

$$\frac{a}{b}+1=\frac{c}{d}+1$$

Reducing each member to an improper fraction,

$$\frac{a+b}{b} = \frac{c+d}{d}, \text{ or } a+b: b = c+d:d$$
(1)

In a similar manner it can be shown that

 $a+b:a=c+d:c \qquad (2)$

The proportions (1) and (2) are said to be derived from the original proportion by composition.

7. If 1 is subtracted from each member of equation (1), Art. 3, the equation becomes

$$\frac{a}{b} - 1 = \frac{c}{d} - 1$$

Reducing each member to an improper fraction,

$$\frac{a-b}{b} = \frac{c-d}{d}, \text{ or } a-b: b = c-d:d$$
(1)

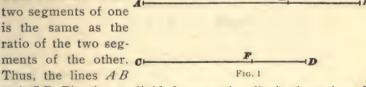
In a similar manner it can be shown that

$$a-b:a=c-d:c \qquad (2)$$

The proportions (1) and (2) are said to be derived from the original proportion by division.

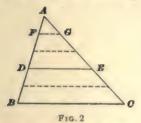
LINES DIVIDED PROPORTIONALLY

8. Two straight lines are divided proportionally when the corresponding segments or parts are in proportion; or when the ratio of the **E**



and CD, Fig. 1, are divided proportionally in the points E and F if AE : EB = CF : FD.

9. A line parallel to one of the sides of a triangle divides the other two sides proportionally. Thus, in Fig. 2, where



DE is parallel to BC, AD:DB= AE:EC.

Suppose that the ratio of AD to DB is as 3 to 2; that is, let $\frac{AD}{DB} = \frac{3}{2}$. Divide AB into five equal parts, and through the points of division draw lines parallel to BC. These lines will intercept equal distances on AC (see *Geometry*, Part 1).

As the ratio of AD to DB is that of 3 to 2, AD will contain three. and DB will contain two, of the equal parts into which AB is divided.

GEOMETRY, PART 2

Also, A E will contain three and E C two of the equal parts into which A C is divided: so that $AE = 3 \times AG$, and $EC = 2 \times AG$; whence

$$\frac{AE}{EC} = \frac{3 \times AG}{2 \times AG} = \frac{3}{2} = \frac{AD}{DB}$$
$$AE: EC = AD: DB$$

OF.

10. Any two sides of a triangle are to each other as the segments into which they are divided by any line parallel to the third side. Thus, in Fig. 2, AB: AC = AD: AE= DB : EC.

From the preceding article, we have

$$AD:DB = AE:EC$$

whence (Art. 6).

$$AD+DB:DB = AE+EC:EC$$

 $AB:DB = AC:EC$

that is. and, interchanging the means (Art. 5),

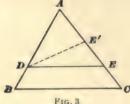
AB: AC = DB: EC

In the same manner it may be shown that

$$AB: AC = AD: AE$$

11. If a line divides two sides of a triangle proportionally, it is parallel to the third side. Thus, if DE, Fig. 3, divides AB and AC so that AD: DB = AE: EC, then DE is parallel to BC.

If DE were not parallel to BC, a line DE' could be drawn through





D parallel to BC. Then, by Art. 9, we should have $\frac{AD}{DB} = \frac{AE'}{E'C}$; whence, since we have assumed that $\frac{AD}{DB} = \frac{AE}{EC}$, $\frac{AE}{EC} = \frac{AE'}{E'C}$

By interchanging the means of this proportion, we obtain

$$\frac{AE}{AE'} = \frac{EC}{E'C}$$

This equality is evidently absurd, since A E is greater than A E', whereas EC is less than E'C Therefore, no other line than DE can pass through D and be parallel to BC.

EXAMPLE 1.—Find the length of the line AB, Fig. 4, of which the end B is inaccessible.

4

SOLUTION.—There are several ways of solving this problem in practice. The one illustrated in the figure is as follows: Any convenient distance AC is measured and the angle C observed with a transit or compass. From C, a distance CE is measured, and at E an angle AED equal to C is turned off. The point D where the line of sight ED meets AB is marked, and the dis-

tances AD and AE are measured. Then, since AED equals C, the lines ED and CBare parallel (see Geometry, Part 1) and, therefore (Art. 9),

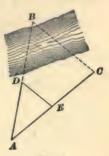
$$AB:AC = AD:AE$$

whence (Art. 3),

$$AB \times AE = AC \times AD$$

and, dividing by AE,

$$AB = \frac{AC \times AD}{AE}$$
. Ans.





EXAMPLE 2.—Divide a line AB, Fig. 1, of given length into two parts AE and EB whose ratio shall be the same as that of two given numbers m and n; that is, so that AE : EB = m : n.

SOLUTION.—Since A E : E B = m : n, we must have (Art. 6),

$$\frac{AE+EB}{EB} = \frac{m+n}{n}, \text{ or, } \frac{AB}{EB} = \frac{m+n}{n},$$

whence, solving for EB,

$$EB = \frac{n \times AB}{m+n}$$
. Ans.

AE can be found in a similar manner, or by subtracting the value of EB from AB.

EXAMPLES FOR PRACTICE

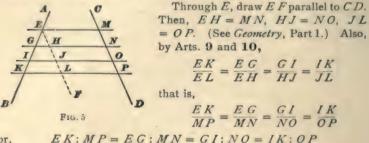
1. If the measured distances in Fig. 4 are A C = 100 feet, A E = 45.2 feet, A D = 48.36 feet, what are the distances A B and D B? Ans. $\begin{cases} A B = 106.99 \text{ ft.} \\ D B = 58.63 \text{ ft.} \end{cases}$

2. If, in Fig. 3, A D = 75 feet, D B = 16.25 feet, and A C = 80 feet, find A E and E C. Ans. $\begin{cases} A E = 65.75 \text{ ft.} \\ E C = 14.25 \text{ ft.} \end{cases}$

3. If AB, Fig. 1, is equal to 125 feet, find the distances AE and EB so that the line will be divided at E in the ratio of 5 to 2.

Ans. $\begin{cases} A E = 89.286 \text{ ft.} \\ E B = 35.714 \text{ ft.} \end{cases}$

12. If two lines, as A B and CD, Fig. 5, are cut by any number of parallel lines, as EM, GN, IO, etc., the corresponding intercepts are proportional; that is, EG:GI= MN: NO: GI: IK = NO: OP, or, by interchanging the means, EG: MN = GI: NO = IK: OP, etc.



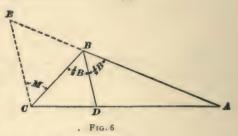
or.

In any triangle A B C. Fig. 6, the bisector B D of an 13. angle divides the side opposite proportionally to the including sides; that is, AB: BC = AD: DC.

Draw CE parallel to BD and meeting AB produced in E. Then, in the triangle A E C, by Art. 9,

$$AB:BE = AD:DC \quad (1)$$

The angles DBCand M. being alternateinterior angles, are equal; that is, $M = \frac{1}{2}B$. The angles D B A and E, being exterior-interior angles, are equal; that is, $E = \frac{1}{2}B$. Therefore, E = M, and BE = BC. (See Geometry, Part 1.)



Substituting, in equation (1), BC for its equal BE,

AB:BC = AD:DC

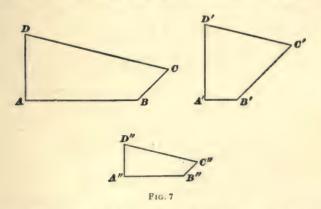
POLYGONS

SIMILAR POLYGONS

SIMILAR TRIANGLES

14. Similar polygons are those whose corresponding angles are equal and whose corresponding sides are proportional.

In order that two polygons may be similar, it is manifestly necessary that each angle of the one shall be equal to the corresponding angle of the other. But this is not sufficient; the corresponding sides must be proportional. For example,



the quadrilaterals A B C D and A' B' C' D', Fig. 7, have their corresponding angles equal, but they are not similar, because their corresponding sides are not proportional. The quadrilaterals A B C D and A'' B'' C'' D'' have their corresponding angles equal and their corresponding sides proportional, and are, therefore, similar.

The corresponding sides of similar polygons are called homologous sides.

15. Two triangles are similar when the angles of one are equal to the angles of the other.

In Fig. 8, let the angles of the triangle A B C be equal, respectively,

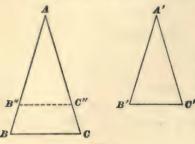


Fig. 8

to those of the triangle A' B' C'. Place the triangle A' B' C' upon A B C, so that the angle A' will coincide with its equal A. Then B' will fall along A B and C' along A C, as at B'' and C'', respectively, and B' C' will take the position B'' C''. The angle B'', which is equal to B', and the angle C'', which is equal to C', is equal to B and the angle C'', which is equal to C' is parallel

to BC (see Geometry, Part 1). Then, by Art. 10, AB: AB'' = AC: AC''

Substituting A'B' and A'C' for their respective equals AB'' and AC'',

$$AB: A'B' = AC: A'C'$$

In like manner, it can be proved that

$$AB: A'B' = BC: B'C'$$

Therefore, the triangles, having their angles equal and their corresponding sides proportional, are similar.

16. Two triangles are similar when two angles of the one are equal respectively to two angles of the other.

17. Two right triangles are similar when an acute angle of one is equal to an acute angle of the other.

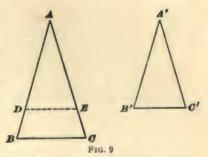
18. A triangle is similar to any triangle formed by a line parallel to one of its sides and the segments it intercepts on the other two sides or the other two sides prolonged.

19. Two triangles are similar when the three sides of one are either parallel or perpendicular to the three sides of the other.

20. Two triangles are similar when their corresponding sides are proportional.

In Fig. 9, AB: A'B' = AC: A'C' = BC: B'C'

On AB, lay off AD equal to A'B'; on AC, lay off AEequal to A'C, and join DE. Then, since AB:AD = AC: AE, DE is parallel to BC. Hence, by Art. 18, triangles ABC and ADE are similar, and, consequently, triangles ABC and A'B'C are similar if it can be shown that DE = B'C. Now,



AB: AD = BC: DE, or AB: A'B' = BC: DEAB: A'B' = BC: B'C'

But,

The last two proportions are the same, term for term, excepting the last term; hence, DE is equal to B'C', and the triangles ADE and A'B'C' are equal. Therefore, the triangles ABC and A'B'C' are similar.

21. Two triangles are similar when an angle of the one is equal to an angle of the other and the including sides are proportional.

22. In two similar triangles, corresponding altitudes have the same ratio as any two corresponding sides.

Let CD and C'D', Fig. 10, be the corresponding altitudes of the

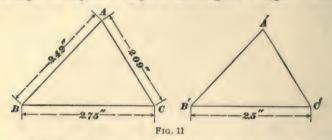
 $\mathbf{A} \underbrace{\mathbf{B}}_{\mathbf{B}} \underbrace{\mathbf{B}}_{\mathbf{F}_{16}.10} \mathbf{B} \underbrace{\mathbf{A}}_{\mathbf{B}} \underbrace{\mathbf{C}}_{\mathbf{B}} \underbrace{\mathbf{C}} \underbrace{$

Therefore,

CD: C'D' = AC: A'C' = AB: A'B' = BC: B'C'

23. As stated in Art. 14, two polygons are similar when their corresponding angles are equal and their corresponding sides are proportional. It has now been shown that, in triangles, either of these conditions includes the other. This could have been expected from the fact that either the three angles or the three sides of a triangle fix its shape. This is not true of a polygon of more than three sides, as the angles can be changed without altering the sides, or the proportions of the sides can be changed without altering the angles.

EXAMPLE 1.—In the triangles ABC and A'B'C', Fig. 11, angle A = angle A', angle B = angle B', and angle C = angle C', and the



sides BC, CA, AB, and B'C' have the dimensions that are marked on them; find the lengths of the sides C'A' and A'B'.

SOLUTION.—Since the two triangles are equiangular, they are similar, and hence the value of A'B' and that of A'C' are conveniently found as follows:

ce

$$2.75 : 2.42 = 2.5 : A' B'$$

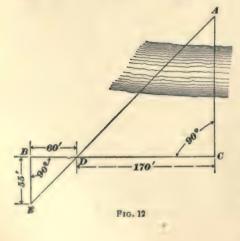
$$A'B' = \frac{2.42 \times 2.5}{2.75} = 2.2 \text{ in. Ans.}$$

$$2.75 : 2.09 = 2.5 : A' C'$$

$$A'C' = \frac{2.09 \times 2.5}{2.75} = 1.9 \text{ in. Ans.}$$

whence

when



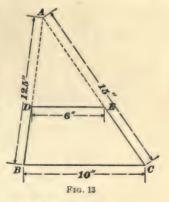
EXAMPLE 2.—In Fig. 12, CD is perpendicular to AC and is 170 feet long; DB is 60 feet; and BE, perpendicular to BD, is 55 feet long; find the distance AC.

SOLUTION.—The right triangles A C D and D B E have the angles A D C and B D E equal; hence, they are similar, and

AC:CD = BE:BD,or AC:170 = 55:60 whence,

$$AC = \frac{170 \times 55}{60} = 155.83$$
 ft. Ans.

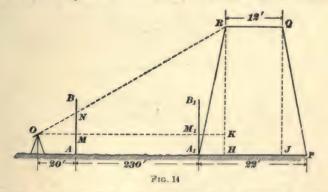
EXAMPLE 3.—It is required to cut from a triangular plate A B C, Fig. 13, having the dimensions shown, a trapezoidal plate B D E C whose upper base DE shall be 6 inches; find the distances A D and A E that must be cut off.



SOLUTION.—The similar triangles ADE and ABC give,

 $\frac{A D}{A B} = \frac{D E}{B C}; A D = \frac{A B \times D E}{B C} = \frac{12.5 \times 6}{10} = 7.5 \text{ in. Ans.}$ $\frac{A E}{A C} = \frac{D E}{B C}; A E = \frac{A C \times D E}{B C} = \frac{15 \times 6}{10} = 9 \text{ in. Ans.}$

EXAMPLE 4.—In order to measure the height R H of a pier $A_1 P Q R$, Fig. 14, whose base and top are, respectively, 22 feet and 12 feet square and whose sides all have the same inclination, a transit was set at a point O distant 250 feet from the side A_1 of the pier; that is, so that $O M_1 = 250$ feet. $A_1 B_1$ was a rod on which the horizontal line of sight $O M_1$ intercepted a distance $A_1 M_1 = 4.5$ feet. The same rod was



held at a distance OM = 20 feet from the instrument, and the height AM above the ground noted. Then the telescope of the transit was directed to the top R of the pier, and, with the rod still held at A, the height AN was read on the rod. By subtracting AM from AN, the distance MN intercepted between the lines OM_1 and OR was found to be 6 feet. What was the height KH?

SOLUTION.—The inclination of A, R and that of PQ being equal we have, A, H = JP, and HJ = RQ = 12 ft. Now,

$$A_1 P = A_1 H + HJ + JP = 2 A_1 H + 12$$
$$A_1 H = \frac{A_1 P - 12}{2} = \frac{22 - 12}{2} = 5 \text{ ft.}$$

whence,

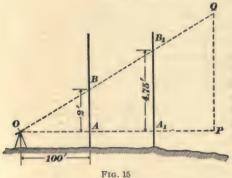
The similar triangles OMN and OKR give

$$\frac{OM}{MN} = \frac{OK}{KR}; KR = \frac{OK \times MN}{OM} = \frac{(OM_1 + M_1K) \times MN}{OM} = \frac{(OM_1 + M_1K) \times MN}{OM} = \frac{(OM_1 + A_1H) \times MN}{OM} = \frac{(250 + 5) \times 6}{20} = \frac{255 \times 6}{20} = 76.5 \text{ ft.}$$

Finally,

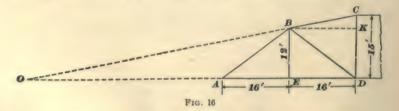
 $RH = RK + KH = RK + M_1A_1 = 76.5 + 4.5 = 81$ ft. Ans.

EXAMPLES FOR PRACTICE



1. In Fig. 15, the lines of sight OP and OQ of a transit intercept on a rod distances, AB = 2 feet and $A_1B_1 = 4.75$ feet; if the distance OA is 100 feet, what is the distance OA_1 ? Ans. 237.5 ft.

2. In order to find the stress in the member B D, Fig. 16, by the method of moments, it is necessary to find the distance D O from D to



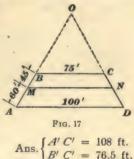
the point of intersection O of DA and CB, both produced; the dimensions being as shown, what is that distance? Ans. DO = 80 ft.

2. ABCD. Fig. 17. is a trapezoid whose non-parallel sides pro-

duced meet at O; the line MN is parallel to the bases A D and B C: the dimensions of AD, BC, BM, and MA being as shown, find O B and M N.

Ans.
$$\begin{cases} O B = 315 \text{ ft.} \\ M N = 85.714 \text{ ft.} \end{cases}$$

4. In a triangle A B C, side A B= 32 feet, BC = 34 feet, and AC = 48 feet; if side A'B' of a similar triangle A'B'C' is 72 feet long, what are the lengths of the other two sides?



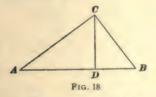
5. The base of a right triangle is 24 inches, and its altitude 72 inches: at what distance from the top is the triangle 16 inches wide?

Ans. 48 in.

IMPORTANT CONSEQUENCES OF THE THEORY OF SIMILAR TRIANGLES

24. When the first of three quantities is to the second as the second is to the third, the three quantities are in continued proportion; the second is a mean proportional between the first and third; and the third is a third **proportional** to the first and second. Thus, if a: b = b: c, the three quantities a, b, and c are in continued proportion; b is a mean proportional between a and c; and c is a third proportional to a and b.

25. In a right triangle, as ABC, Fig. 18, the perpendicular CD drawn from the vertex of the right angle to the hypotenuse, divides the triangle into two triangles A C D and C D B that are similar to the whole triangle and to each other.



The right triangles ABC and ACD are similar, by Art. 17, as the angle A is common. Also, the triangles ABCand CBD, having angle B in common, are similar. Again, the triangles ACD and CBD, being each similar to ABC are similar to each other.

26. In a right triangle, the perpendicular to the hypote nuse from the vertex of the right angle is a mean proportional between the two parts or segments into which it divides the hypotenuse; that is, Fig. 18, AD:CD= CD:DB.

As the triangles BCD and ABC are similar, and the angle B is common, the angle BCD must equal the angle A, and similarly the angle ACD must equal the angle B. The triangles ACD and BCD are similar, hence the sides opposite equal angles are in proportion; that is,

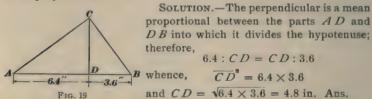
 $\frac{A D \text{ (side opposite } A CD)}{CD \text{ (side opposite } B)} = \frac{CD \text{ (side opposite } A)}{DB \text{ (side opposite } B CD)}$ Or. A D : CD = CD : DB

27. The side AC, Fig. 18, is a mean proportional between the whole hypotenuse and the segment AD on the same side of CD as the side AC; that is, AB: AC = AC: AD. Similarly, AB: BC = BC: BD.

The triangles ABC and ACD are similar, hence the sides opposite equal angles are proportional; that is,

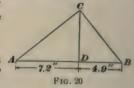
 $\frac{A B \text{ (opposite right angle)}}{A C \text{ (opposite right angle)}} = \frac{A C \text{ (opposite } B)}{A D \text{ (opposite } A C D)}$ Or, A B : A C = A C : A D

EXAMPLE 1.—In the right triangle A B C, Fig. 19, find the length of the perpendicular C D.



EXAMPLE 2.—Find the length of the sides of the right triangle ABC, Fig. 20, in which CD is the perpendicular from the vertex of the right angle to the hypotenuse.

SOLUTION. — The hypotenuse is 7.2 in. + 4.9 in. = 12.1 in. The side CB is a mean A_{f} proportional between the hypotenuse ABand the part DB; therefore,



$$12.1 : CB = CB : 4.9$$

$$\overline{CB}^{2} = 12.1 \times 4.9$$

$$CB = \sqrt{12.1 \times 4.9} = 7.7 \text{ in. Ans.}$$

14

The leg AC is a mean proportional between AB and AD; that is,

$$AB: AC = AC: AD$$
$$AC = \sqrt{AB \times AD}$$
$$= \sqrt{12.1 \times 7.2} = 9.34 \text{ in.} \text{ An}$$

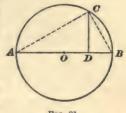
28. Since an angle inscribed in a semicircle is a right angle, it follows from Arts. 26 and 27, that:

(a) A perpendicular CD, Fig. 21, drawn from any point on the circumference of a circle to a

diameter AB, is a mean proportional between the segments into which it divides the diameter; that is,

$$AD:CD = CD:DB$$

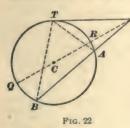
(b) A chord CA drawn from a point in a circumference to the end of a diameter is a mean proportional between the



e

whole diameter and the adjacent segment AD; that is, AB: AC = AC: AD

29. If from a point without a circle, a tangent and a secant are drawn, the tangent is a mean proportional



between the whole secant and the exterior segment; that is, in Fig. 22, PB: PT = PT: PA.

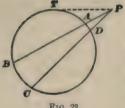
In the triangles BPT and APT, the angle P is common. The angle B, an inscribed angle, and the angle PTA, an angle formed by a tangent and a chord, are equal, since each is measured by onehalf the same arc AT. Hence, the tri-

angles are similar by Art. 16, and

 $\frac{PB \text{ (opposite angle } PTB)}{PT \text{ (opposite angle } PAT)} = \frac{PT \text{ (opposite angle } B)}{PA \text{ (opposite angle } PTA)}$ $\overline{PT}^* = PB \times PA$ $PT = \sqrt{PB \times PA}$

30. If from a point without a circle any two secants are drawn, the product of one secant and its external segment is equal to the product of the other secant and its external segment.

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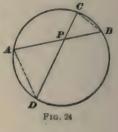


In Fig. 23, PB and PC are secants. Draw the tangent PT. Then, from Art. 29. $\overline{PT}^{3} = PA \times PR$ $\overline{PT}^* = PC \times PD$ and $PA \times PB = PC \times PD$ hence.

FIG. 28

If any two chords be drawn through a point within a 31. circle, the product of the segments of one is equal to the product of the segments of the other.

In Fig. 24, the angles D and B, being measured by one-half the arc AC, are equal. The angles BPC and DPA, being vertical angles. are equal. Hence, by Art. 16, the triangles CBP and ADP are similar. Therefore,



and

 $AP \times PB = CP \times PD$

 $\frac{AP}{CP} = \frac{PD}{PB}$

EXAMPLES FOR PRACTICE

1. The perpendicular from the vertex of the right angle of a right triangle divides the hypotenuse into parts of 23.04 inches and 1.96 inches. Find: (a) the length of the perpendicular; (b) the length of the two sides of the triangle. Ans. $\begin{cases} (a) & 6.72 \text{ in.} \\ (b) & 24 \text{ in. and } 7 \text{ in.} \end{cases}$

2. If, in Fig. 22, the distance CP of the point P from the center of the circle is 65 feet, and the radius CR is 25 feet, what is the length of the tangent PT? Ans. 60 ft.

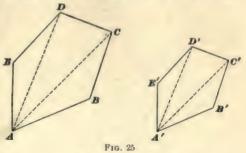
3. The chord of the arc of a segment is 14 inches long and the height of the segment is 2 inches; what is the radius? Ans. 13¹/₁ in.

OTHER SIMILAR POLYGONS

32. Two polygons are similar when they are composed of the same number of triangles similar each to each and similarly placed.

Thus, in Fig. 25, the polygons ABCDE and A' B' C' D' E' are composed of the same number of similar triangles similarly placed. Since the triangle A E D is similar to the triangle A' E' D', angle E = angle E' and angle A D E = angle A' D' E'. Also, in the similar

triangles A D C and A' D' C', angle A D C= angle A' D' C'. Hence, the sum of the angles A D E and A D C, or the angle E D C, is equal to the sum of the angles A' D' E' and A' D' C', or the angle E' D' C'. In like manner, angle D CB = angle D' C' B'.



angle B = angle B', and angle B A E = angle B' A' E'. Since the triangles are similar,

E D: E' D' = A D: A' D' and A D: A' D' = D C: D' C'hence, E D: E' D' = D C: D' C'

In like manner,

DC: D'C' = CB: C'B' = BA: B'A' = AE: A'E'

Therefore, as the angles of the one polygon are equal to the corresponding angles of the other and the sides of the one polygon are proportional to the sides of the other, the polygons are similar.

33. Two similar polygons can be divided into the same number of similar triangles similarly placed.

34. The perimeters of two similar polygons are in the same ratio as any two homologous sides.

In Fig. 25, let P be the perimeter of the polygon A B C D E, and P' the perimeter of the polygon A' B' C' D' E'. Since the polygons are similar

$$\frac{AE}{A'E'} = \frac{ED}{E'D'} = \frac{DC}{D'C'} \stackrel{\circ}{=} \frac{CB}{C'B'} = \frac{BA}{B'A'}$$
(1)

Let each of these equal ratios be denoted by R; that is, let

$$\frac{AE}{A'E'} = R, \frac{ED}{E'D'} = R, \frac{DC}{D'C'} = R, \frac{CB}{C'B'} = R, \frac{BA}{B'A'} = R.$$

From these equations we obtain,

$$A E = R \times A' E', E D = R \times E' D', D C = R \times D' C',$$

$$C B = R \times C' B', B A = R \times B' A'$$

Adding the sides of these equalities,

$$AE + ED + DC + CB + BA$$

 $= R \times A' E' + R \times E' D' + R \times D' C' + R \times C' B' + R \times B' A'$ = R (A' E' + E' D' + D' C' + C' B' + B' A')

GEOMETRY, PART 2

 $R = \frac{A E}{A' E'} = \frac{E D}{E' D'} = \frac{D C}{D' C'}, \text{ etc.};$

AE + ED + DC + CB + BAA' E' + E' D' + D' C' + C' B' + B' A' = R

whence

But

therefore.

 $\frac{P}{P'} = \frac{A_{*}E}{A'E'} = \frac{ED}{E'D'} = \frac{DC}{D'C'}$ etc. 35. Equation (1) of the preceding article is a series of equal ratios, of which the numerators are the antecedents and the denominators the consequents. The general truth was shown in that article, that in a series of equal ratios the sum of the antecedents is to the sum of the consequents as

AREAS OF POLYGONS

any antecedent is to its consequent.

36. Definitions.—The area of a surface is the superficial space included within its boundary lines. Area is expressed by the ratio of the surface to a surface of fixed value chosen as a unit and called the unit of area.

37. A square whose side is equal in length to the unit of length is usually taken as the unit of area, and its area is called the square unit. For example, if the unit of length is 1 inch, the unit of area, or square inch, is the square whose sides measure 1 inch, and the area of any surface is expressed by the number of square inches that the surface contains. If the unit of length were 1 foot, the unit of area would measure 1 foot on each side, and the area of the surface would be expressed in square feet. Square inch and square foot are abbreviated to sq. in. and sq. ft., respectively, and are often indicated by the symbols \Box'' and \Box' .

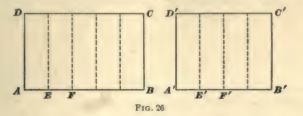
38. Two surfaces are equivalent when their areas are equal.

Comparison of the Areas of Two Rectangles. 39. The areas of two rectangles A B C D and A' B' C' D', Fig. 26, having equal altitudes are to each other as their bases; that 15, area A B C D: area A' B' C' D' = A B : A' B'.

Suppose that A'B' is four-fifths of AB, or that AB: A'B' = 5:4. Divide AB into five equal parts AE, EF, etc., and A'B' into four

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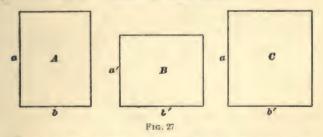
equal parts A' E', E' F', etc. It is evident that A' E' = A E, for, since A B is to A' B' in the ratio of 5 to 4, any quantity, as A E, that is contained five times in A B must be contained four times in A' B'. Through the points of division E, F, E', F', etc., draw perpendiculars



to A B and A' B'. Each large rectangle is thus divided into small rectangles, all of which are equal. As A B C D contains five, and A' B' C' D' contains four, of the small rectangles, the ratio of the two large rectangles is that of 5 to 4, which is also the ratio of their bases.

40. Since any of the sides of a rectangle can be considered as the base, it follows that the area of two rectangles having equal bases are to each other as their altitudes.

41. The areas of any two rectangles are to each other as the products of their bases by their altitudes.



Let A and B, Fig. 27, be two rectangles whose altitudes are a and a'and whose bases are b and b', respectively. Construct a rectangle C with an altitude a and a base b'. Then, by Arts. **39** and **40**,

$$A:C=b:b' \tag{1}$$

 $C: B = a: a' \tag{2}$

Multiplying equation (1) by equation (2),

$$AC:BC = ab:a'b'$$
(3)

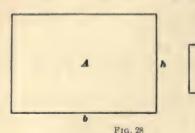
Dividing the terms of the first member of equation (3) by C_1

$$A:B=ab:a'b'$$

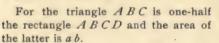
and

42. Area of a Rectangle.—The area of a rectangle is equal to its base multiplied by its altitude; that is, in Fig. 28, A = b h.

1

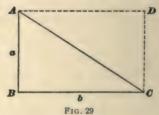


43. Area of a Triangle.—The area of a right triangle is equal to one-half the product of the two legs of the triangle; that is, in Fig. 29, area $ABC = \frac{1}{2}ab$.



41), $A: a = h \times b: 1 \times 1;$ 1 or, $\frac{A}{a} = \frac{h \times b}{1 \times 1}$ But a is a unit square, and its area is therefore equal to 1; hence, A = bh

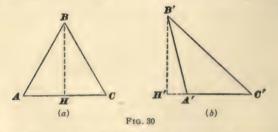
Construct a unit square a. Then (Art.



44. The area of any triangle is equal to one-half the product of its base and altitude.

In Fig. 30 (a), let AC be the base and BH the altitude of the triangle ABC. The area ABC is equal to the sum of the right triangles AHB and CHB, which, by the last article, is

 $\frac{1}{3}BH \times AH + \frac{1}{3}BH \times HC = \frac{1}{3}BH \times (AH + HC) = \frac{1}{3}BH \times AC$



In Fig. 30 (b), the area A'B'C' is the difference between the areas of the right triangles B'H'C' and B'H'A'; that is,

 $\stackrel{1}{=} B'H' \times H'C' - \stackrel{1}{=} B'H' \times H'A' = \stackrel{1}{=} B'H' \times (H'C' - H'A')$ $= \stackrel{1}{=} B'H' \times A'C'$

Let b be the base, h the altitude, and A the area of any triangle; then,

 $A = \frac{1}{2}bh$

45. Two triangles having the same base are to each other as their altitudes, and two triangles having the same altitude are to each other as their bases.

46. Two triangles having the same base and the same altitude are equivalent.

It should be borne in mind that any side of a triangle can be taken as the base, the altitude being the perpendicular to that side from the opposite vertex.

47. To find the area of a triangle from the lengths of its three sides, apply the following:

Rule.—From half the sum of the three sides subtract each side separately; multiply together the half sum and the three remainders and extract the square root of the product.

Let a, b, and c be the three sides of a triangle, and A the area; let

$$s = \frac{1}{2}(a+b+c)$$

 $A = \sqrt{s(s-a)(s-b)(s-c)}$

Then

The geometrical proof of this rule is very laborious, and will not be given here. A proof will be found in *Trigonometry*.

EXAMPLE.—What is the area of a triangle having two sides 19.8 feet long, and one side 28 feet long?

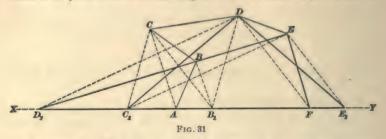
SOLUTION.—It is immaterial which side is called a, b, or c. $s = \frac{a+b+c}{2} = \frac{28+19.8+19.8}{2} = 33.8$; taking b and c as the short sides, s - a = 33.8 - 28 = 5.8, and s - b and s - c are each 33.8 - 19.8 = 14. Then, applying the formula

 $A = \sqrt{s(s-a)(s-b)(s-c)} = \sqrt{33.8 \times 5.8 \times 14 \times 14} = 196 \text{ sq. ft.},$ nearly. Ans.

48. A triangle equivalent to any given polygon may be constructed as follows:

Let ABCDEF, Fig. 31, be the given polygon. Produce any of the sides, as AF, in both directions, as indicated by XY. This line

will be referred to as the base. Starting from one of the ends of AF, as A, draw a diagonal AC forming a triangle with AB and BC. Draw BB, parallel to CA, meeting the base at B, and join C to B_1 .



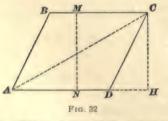
The polygon $B_1 C D E F$ has one side less than the given polygon, and is equivalent to it. For

> $A B C D E F = B_1 B C D E F$ + triangle $B_1 B A$ $B_1 C D E F = B_1 B C D E F$ + triangle $B_1 B C$

The two triangles $B_1 B A$ and $B_1 B C$ are equivalent, for they have the common base $B_1 B$, and their altitudes, being each equal to the distance between the parallels A C and $B_1 B$, are equal. Proceeding with the polygon $B_1 C D E F$ as with the original polygon, draw the diagonal $B_1 D$, forming a triangle with $B_1 C$ and C D. Draw $C C_1$ parallel to $D B_1$, and join D and C_1 . It can be shown as before that the polygon $C_1 D E F$ is equivalent to $B_1 C D E F$, and, therefore, to the original polygon. Finally, draw the diagonal $C_1 E$, and $D D_1$ parallel to it, meeting the base at D_1 . Then will the triangle $D_1 E F$ be the required triangle equivalent to the given polygon.

In practice, it is more convenient, as well as more accurate, to reduce about one-half of the polygon on one side of A and the rest on the other side of F. Thus, having reduced the polygon to the quadrilateral $C_1 D E F$, the diagonal FD is drawn from F; $E E_1$ is drawn through E parallel to DF, and E_1 joined to D. This gives $C_1 D E_1$, as the required triangle.

49. Area of a Parallelogram.—The area of a parallelo-



gram is equal to its base multiplied by its altitude; that is, in Fig. 32, area ABCD = AD $\times MN$.

For ABCD is equal to the sum of the equal triangles ABC and ADC, or to twice either of them, as ADC; that is, $ABCD = 2 \times \frac{1}{2} AD$

 $\times CH = AD \times CH = AD \times MN.$

EXAMPLE 1.—What is the cost of paving a street 1,800 feet long and 36 feet wide with asphalt, the price being \$2 per square yard?

SOLUTION.—The surface to be covered is a rectangle whose sides are 36 ft. and 1,800 ft., or 12 yd. and 600 yd., and whose area is, therefore, $12 \times 600 = 7,200$ sq. yd. The cost of paving is, then, $2 \times 7,200$ = \$14,400. Ans.

EXAMPLE 2.—One side of a triangular plot of land is 125 feet long and the perpendicular distance from the opposite vertex to this side is 174.24 feet; it is desired to find a side of a rectangle that has the same area as the triangle and one side 75 feet long.

SOLUTION.—The area of the triangle is $\frac{1}{2} \times 125 \times 174.24 = 10,890$ sq. ft. Then the other side of the rectangle is $10,890 \div 75 = 145.2$ ft. Ans.

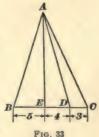
EXAMPLE 3.—Divide a triangular plot of land into any number of equal parts by lines from a vertex to the opposite side.

SOLUTION.—Divide the side opposite, the vertex through which the lines are to be run into the required number of equal parts and run lines from the vertex of the triangle to the points of division. Then, since the triangles thus formed have equal bases and their vertexes in the same point, they are equivalent. Ans.

EXAMPLE 4.—Divide a given triangle into parts proportional to any given numbers by lines run through a vertex.

SOLUTION.—Let the given triangle be ABC, Fig. 33, and let it be required to divide it into parts proportional to 3, 4, and 5, by lines drawn from the vertex A.

The base BC is divided into parts proportional to the numbers 3, 4, and 5, by dividing it into 3+4+5=12 equal parts, and then marking the third and the seventh points of division. From the points thus marked, lines are run to the vertex A. Then, by Art. 45,



and.

CAD: ADE = 3:4ADE: ABE = 4:5 Ans.

EXAMPLES FOR PRACTICE

1. Find the area of a square whose side is 5 feet 9 inches.

Ans. 33.062 sq. ft

2. Find the area of a rhombus whose length is 12.5 feet, and whose height is 9.25 feet. Ans. 115.62 sq. ft.

3. One side of a room is 16 feet long; if the floor contains 240 square feet, what is the length of the other side? Ans. 15 ft.

4. In a trapezium two not adjacent sides are 16 and 14 inches, respectively. A diagonal divides the trapezium into two triangles whose altitudes from their vertexes to the given sides as bases are 17 inches and 3 inches, respectively; what is the area of the trapezium? Ans. 157 sq. in.

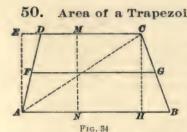
5. The base B C of a triangle is 150 chains and the perpendicular from the opposite vertex A to B C is 45 chains; it is desired to divide the triangle into two parts equal in area by a line from A to B C; how far from B is D, the intersection of this line with B C?

Ans. 75 ch.

6. From the mid-point E of the side AB of a parallelogram ABCD, lines are drawn to the vertexes D and C and to the mid-point of the side CD; show that these lines divide the parallelogram into four triangles that are equal in area.

7. Find the area of a triangle whose three sides are 13, 14, and 15 feet. Ans. 84 sq. ft.

8. Find the area of a right triangle whose hypotenuse is 50 feet and one of whose legs is 40 feet. Ans. 600 sq. ft.



Area of a Trapezoid.—The area of a trapezoid is equal to one-half the sum of the parallel sides multiplied by the altitude; that is, in Fig. 34, area of trapezoid $ABCD = \frac{1}{2}(AB + DC) \times MN$.

The area of the trapezoid is equal to the sum of the areas of C; hence.

the two triangles ABC and ADC; hence,

 $A B C D = \frac{1}{2} A B \times C H + \frac{1}{2} D C \times A E$ = $\frac{1}{2} A B \times M N + \frac{1}{2} D C \times M N'$ = $\frac{1}{2} (A B + D C) \times M N$

Let $b_1 =$ length of lower base; $b_2 =$ length of upper base; h = altitude.

Then, the area A of the trapezoid A B C D is

 $A = \frac{1}{2}(b_1 + b_2)h$

51. Since the median line FG, Fig. 34, joining the midpoints of the non-parallel sides is equal to $\frac{1}{2}(AB + DC)$, the area of a trapezoid is equal to the product of the median line by the altitude.

EXAMPLE.—Divide a plot of ground in the form of a trapezoid into any number of equal parts by lines intersecting the two bases.

SOLUTION.—Divide each of the bases into the same number of equal parts into which the trapezoid is to be divided and run lines through the corresponding points of division. The trapezoids thus formed have equal bases and the same altitude and are, therefore, equal in area. Ans.

EXAMPLES FOR PRACTICE

1. The parallel sides of a trapezoid are 321.51 and 214.24 feet, and the perpendicular distance between them is 171.16 feet; what is the area of the trapezoid? Ans. 45,849 sq. ft.

2. Find the area of a trapezoid whose parallel sides are 20.5 and 12.25 chains, the perpendicular distance between them being 10.75 chains. Ans. 17.603 A.

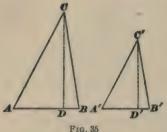
3. The parallel sides of a trapezoidal plot of ground are 400 feet and 360 feet long; the distance between the parallel sides is 100 feet. It is desired to divide this plot into five lots by lines intersecting the parallel sides; what will be the length of the front and the rear of one of the lots? Ans. 80 ft. and 72 ft.

4. How many square feet are there in a board 12 feet long, 18 inches wide at one end, and 12 inches wide at the other end?

Ans. 15 sq. ft.

52. Area of Any Polygon.—The area of any polygon can be found by dividing the polygon into triangles, determining the area of each triangle, and adding the results.

53. Comparison of the Areas of Similar Polygons. The areas of two similar triangles are to each other as the squares of their homologous sides.



In Fig. 35, Area $ABC = \frac{1}{2}AB \times CD$ (1) Area $A'B'C' = \frac{1}{2}A'B' \times C'D'$ (2) Dividing equation (1) by equation (2), $\frac{ABC}{A'B'C'} = \frac{A^*B}{A'B'} \times \frac{CD}{C'D'}$ (3) **B'** but, by Art. 22, $\frac{CD}{C'D'} = \frac{AB}{A'B'}$; hence, substituting in (3) **BC** $AB = AB = \frac{AB}{A'B'}$

 $\frac{AB}{A'B'} \text{ for } \frac{CD}{C'D'}, \quad \frac{ABC}{A'B'C'} = \frac{AB}{A'B'} \times \frac{AB}{A'B'} = \frac{AB}{A'B'}^{*}$ $ABC: \quad A'B'C' = \overline{AB}^{*} \cdot \overline{A'B'}^{*}$

that is,

The areas of two similar triangles are to each other

as the squares of any two homologous lines.

55. The areas of two similar polygons are to each other as the squares of their homologous lines.

By Art. 33, two similar polygons can be divided into the same number of similar triangles. The sums of these triangles will, by Art. 35, be to each other as any triangle of one polygon is to the corresponding triangle of the other. But these triangles are to each other as the squares of any two homologous lines. Hence, the sum of the triangles, or the polygons, are to each other as the squares of any two homologous lines.

EXAMPLE 1.—Divide a given triangle by a line parallel to the base into parts such that the given triangle shall be to the triangle cut off as m: n.

SOLUTION.—Let ABC, Fig. 36, be the given triangle, and ADEbe the triangle cut off so that ABC: ADE = m:n. By Art. 18, ADE and ABC are similar; hence, by Art. 53,

 $ABC: ADE = \overline{AB}^{\circ}: \overline{AD}^{\circ}$ But by the conditions of the problem, ABC: ADE = m: nTherefore, $\overline{AB}^{\circ}: \overline{AD}^{\circ} = m: n:$

whence, $AD = AB\sqrt{\frac{n}{m}}$. Ans.

When the triangle A B C is to be divided into B^{2} two equal parts,

$$A D = A B \sqrt{\frac{1}{2}} = .70711 A B$$

FIG. 36



EXAMPLE 2.—Let the length AB of example 1 be 32 chains and the area of ABC be 25.6 acres; what is the length of AD, if it is desired to make the triangle ADE contain 15 acres?

SOLUTION.—The area ABC is to be to the area of ADE as 25.6:15; hence, m: n = 25.6:15.

Then,
$$A D = 32 \sqrt{\frac{15}{25.6}} = 24.495$$
 ch. Ans.

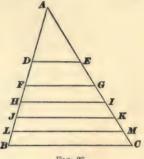
EXAMPLE 3.—Divide a given triangle A B C, by lines parallel to the base, into *n* equal parts.

SOLUTION.—Let ABC, Fig. 37, be the triangle, and DE, FG, HI, etc., divide it into *n* equal parts. Then ADE is one part, AFG is two parts, and so on. Hence,

A B C : A D E = n : 1 A B C : A F G = n : 2; etc. Then, by example 1,

$$AD = AB\sqrt{\frac{1}{n}}; AF = AB\sqrt{\frac{2}{n}};$$

 $AH = AB\sqrt{\frac{3}{n}};$ etc. Ans.



EXAMPLE 4.—Two triangles A B C and A' B' C' are similar. The sides of the triangle A B C are: A B = 10 inches, B C = 21 inches, A C = 17 inches, and in the triangle A' B' C' the side B' C' = 42 inches; what is the area of the triangle A' B' C'?

SOLUTION.—In the triangle A B C, $s = \frac{10 + 17 + 21}{2} = 24$. Then s - a = 3, s - b = 7, s - c = 14, and the area is $\sqrt{24 \times 3 \times 7 \times 14} = 84$ sq. in. By the principle of Art. 53,

	area of $A' B' C'$: area of $A B C = \overline{B' C'}$; $\overline{B C}$;
that is,	area of $A' B' C' : 84 = 42^{\circ} : 21^{\circ}$
But	$42^*:21^*=4:1$
hence,	area of $A' B' C' : 84 = 4 : 1$
whence,	area of $A' B' C' = 4 \times 84 = 336$ sq. in. Ans.

EXAMPLES FOR PRACTICE

1. Suppose that the sides of the triangle A'B'C' in example 4 of Art. 55 are A'B' = 20 inches, B'C' = 42 inches, and C'A' = 34 inches; show that the answer that is given to the example is correct.

2. The triangles A B C and A' B' C' are similar; being given B C= 13 inches, CA = 14 inches, A B = 15 inches, and B' C' = 19.5 inches; find the area of the triangle A' B' C'. Ans. 189 sq. in.

3. Let AB, one side of a triangle ABC, be 60 chains long, and let it be required to divide, by lines parallel to BC, the triangle ABCinto five equal parts. (a) What are the lengths of the lines AD, AF, AH, and AT? (b) Let the area of ABC be 120 acres; by means of Art. 53, prove your results. (AD = 26 ch. 83.3 l.)

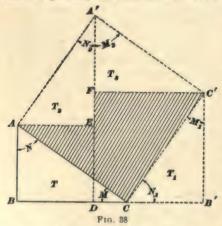
Ans. AF = 37 ch. 94.7 l. AH = 46 ch. 47.6 l. AT = 53 ch. 66.6 l.

4. Find the lengths of A D and A F when the triangle of example 3 is divided into three parts, whose areas shall be proportional to the numbers 3, 4, and 5. Ans. $\begin{cases} A D = 30 \text{ ch.} \\ A F = 45 \text{ ch.} 82.6 \text{ l.} \end{cases}$

HINT.-This is the same as if the triangle were divided into 3 + 4 + 5 equal parts and A D E contained three, and A F G, seven of these equal parts.

56. The Theorem of Pythagoras.—In any right triangle, the square described on the hypotenuse is equivalent to the sum of the squares described on the other two sides.

Let A B C, Fig. 38, be a right triangle. Draw an equal triangle in the position CB'C', so that CB' will be in the prolongation of BC. Construct the squares A B D E and B'C'FD on A B and B'C', respectively. Since M + N, (= M + N) is a right angle, A CC' is also a right angle. Produce E F to A', making FA' = BA = DE.



Then, since EF is the difference between DF and DE, or BC and AB, EA' = BC. Draw AA' and C'A'. Each of the right triangles T_s and T_s is equal to T, since their legs are respectively equal. The quadrilateral ACCA'. having all its sides equal and a right angle C, is a square—the square on the hypotenuse AC. This square is equal to the shaded figure plus the sum of the triangles T_a and T_a ; or to the shaded figure plus twice

the triangle T. The sum of the squares ABDE and B'C'FD is equal to the shaded figure plus the sum of the triangles T and T_1 , or to the shaded figure plus twice the triangle T. Therefore, square ACC'A' = square ABDE + square B'C'FD.

A particular case of the proposition just proved is shown in Fig. 39.

Let c be the hypotenuse, and a and b the other two sides of any right triangle.

Then.

C ³	_	$a^* + b^*$	(1)
С	=	$\sqrt{a^2+b^2}$	(2)
a	=	$\sqrt{c^*-b^*}$	(3)

Formula 3 may be written

$$a = \sqrt{(c-b)(c+b)}$$
(4)

EXAMPLE 1.—If AB = 3 inches

and BC = 4 inches, what is the length of the hypotenuse AC, Fig. 38? SOLUTION -

$$A C = \sqrt{\overline{A B}^{2} + \overline{B C}^{2}}$$
$$= \sqrt{3^{3} + 4^{3}} = \sqrt{25} = 5 \text{ in. Ans.}$$

EXAMPLE 2.—The side given is 3 inches (= b, say), the hypotenuse is 5 inches (= c); what is the length of the other side?

SOLUTION.-Applying formula 4, Art. 56,

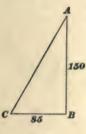
Also.

a

a

$$= \sqrt{(5-3)} (5+3) = \sqrt{16} = 4 \text{ in. Ans.}$$
$$= \sqrt{c^2 - b^2} = \sqrt{5^2 - 3^2} = 4 \text{ in. Ans.}$$

EXAMPLE 3.—If, from a church steeple that is 150 feet high, a rope



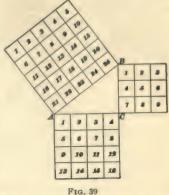
F1G. 40

is to be attached at the top and to a stake in the ground 85 feet from its foot (the ground being supposed to be level), what must be the length of the rope?

SOLUTION.-In Fig. 40, A B represents the steeple 150 ft. high; C, a stake 85 ft. from the foot of the steeple; and A C, the rope. Here we have a triangle right-angled at B, of which AC is the hypotenuse. The square of $A C = 85^{\circ} + 150^{\circ}$ = 7,225 + 22,500 = 29,725. Therefore,

$$4 C = \sqrt{29,725} = 172.4$$
 ft., nearly. Ans.

EXAMPLE 4.-Referring to Fig. 16, it is required to find the length of the post A B and that of the member B C.



SOLUTION.—Draw *B K* parallel to *E D*. Then, BK = ED = 16 ft. and CK = CD - DK = CD - EB = 15 - 12 = 3 ft. The right triangles *A E B* and *B C K* give

$$A B = \sqrt{A E^{2}} + \overline{E} B^{2} = \sqrt{16^{2} + 12^{2}} = \sqrt{400} = 20 \text{ ft. Ans.}$$
$$B C = \sqrt{\overline{B} \overline{K}^{2}} + \overline{C} \overline{K}^{2} = \sqrt{16^{2} + 3^{2}} = \sqrt{265} = 16.279 \text{ ft. Ans.}$$

EXAMPLES FOR PRACTICE

1. If the two sides about the right angle in a right triangle are 52 and 39 feet long, how long is the hypotenuse? Ans. 65 ft.

2. A ladder 65 feet long reaches to the top of a house when its foot is 25 feet from the house; how high is the house, supposing the ground to be level? Ans. 60 ft.

3. The shortest distance from a point to a line is 25 inches; the distances from this point to the extremities of the line are 54 inches and 40 inches, respectively; what is the length of the line?

Ans. 79.08 in.

4. Show that the diagonal of a square is equal to the side multiplied by $\sqrt{2}$.

REGULAR POLYGONS

57. A regular polygon is a polygon that has equal sides and equal angles, that is, it is equilateral and equiangular.

58. A circle can be circumscribed about any regular polygon.

Take any three vertexes of the regular polygon A B C D E,

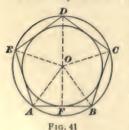


Fig. 41, as the vertexes A, B, C, and pass a circle through them. Let O be the center of this circle. Join O to A, B, C, D, and E. The polygon being equiangular, the angle ABC = angle BCD. The angles OCBand OBC, being opposite equal sides OCand OB of the triangle OBC, are equal. Hence,

$$ABC - OBC = BCD - OCB$$
$$ABO = OCD$$

The polygon being equilateral, the sides AB and CD are equal. Hence, the triangles AOB and OCD, having two sides and included angle of one equal to two sides and included angle of the other equal, are equal. Therefore, OD = OA, and a circle passing through A,

or.

B, and C must pass through D. In like manner, it can be shown that the circle passes through E.

59. A circle can be inscribed in any regular polygon.

In Fig. 41, OA, OB, OC, OD, and OE, being radii of the circumscribed circle, are equal and divide the polygon into equal isosceles triangles that have a common vertex O. The altitudes of these equal triangles are equal, hence the perpendicular distances, as OF, from O to each of the sides are the same. Therefore, a circle drawn with O as center and a radius equal to OF will be inscribed in the regular polygon.

60. The center of a regular polygon is the common center of the circumscribed and the inscribed circle.

61. The radius of a regular polygon is the radius of the circumscribed circle, as OA, Fig. 41.

62. The apothem of a regular polygon is the radius of the inscribed circle, as OF, Fig. 41.

63. The angle at the center of a regular polygon is the angle included by the radii drawn to the extremities of any side.

64. The angle at the center of any regular polygon is equal to four right angles, or 360° , divided by the number of the sides.

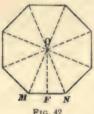
65. If *n* is the number of sides of a regular polygon, the sum of its interior angles is 2(n-2) right angles (see *Geometry*, Part 1), or, $90^{\circ} \times 2(n-2) = 180^{\circ} \times (n-2)$, and, since all the angles are equal, each angle is equal to $\frac{180^{\circ} \times (n-2)}{n} = 180^{\circ} - \frac{360^{\circ}}{n}$. Since this value depends only on the number of sides, all regular polygons of the same number of sides have the same angles.

66. Regular polygons of the same number of sides are similar; their perimeters are to each other as any two homologous lines, and their areas are to each other as the squares of any two homologous lines.

67. The area of a regular polygon is equal to one-half the product of the perimeter and the apothem.

ILT 36F-6

Let *l* be the side MN of a regular polygon, Fig. 42, *n* the number



e MN of a regular polygon, Fig. 42, n the number of sides, p(=nl) the perimeter, a(=OF) the apothem, and A the area. As A is equal to the sum of n triangles, each equal to MON, we have, $A = (\frac{1}{2}MN \times OF) \times n = \frac{1}{2}l a \times n = \frac{1}{2}nl \times a$, or, $A = \frac{1}{2}pa$

EXAMPLE.—Find the area of a regular pentagon whose side is 25 feet and apothem is 17.2 feet.

FIG. 42 SOLUTION.—The figure is a pentagon, hence it has five sides. The perimeter is 5×25 and the area is $\frac{5 \times 25 \times 17.2}{2}$

= 1,075 sq. ft. Ans.

whence,

68. The areas of regular polygons each of whose sides is equal to 1 are given in the following table:

TABLE I

AREAS OF REGULAR POLYGONS

Name	Number of Sides	Area When Side = I	Name	Number of Sides	Area When Side = 1
Triangle .	3	.4330	Octagon .	8	4.8284
Square	4	1.0000	Nonagon .	9	6.1818
Pentagon .	5	1.7205	Decagon .	10	7.6942
Hexagon' .	6	2.5981	Undecagon	11	9.3656
Heptagon .	7	3.6339	Dodecagon	12	11.1960

From the principle of Art. 55, the following rule is derived:

Rule.—To find the area of any regular polygon, square the length of a side and multiply by the area of the similar polygon whose side is equal to the unit of length.

Let A = area; l = length of side of required polygon; a = area of similar polygon whose side is 1; then, by Art. 55,

$$A: a = l^*: 1$$
$$A = a l^*$$

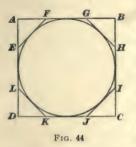
EXAMPLE.—The side of a regular octagon is 3 inches, find its area.

SOLUTION.—From the table, the area of a regular octagon whose side is 1 in. is 4.8284 sq. in. Hence, the area of the octagon whose side is 3 in. is $4.8284 \times 3^\circ = 43.456$ sq. in. Ans.

69. If the vertexes of a regular inscribed polygon are

joined to the middle points of the arcs subtended by the sides of the polygon, the joining lines form a regular inscribed polygon of double the number of sides. Thus, the octagon A FB G, etc., Fig. 43, is formed by joining the middle points of the arcs subtended by the sides of the square A B C D.





70. If tangents are drawn at the middle points of the arcs between adjacent points of contact of the sides of a regular circumscribed polygon, a regular circumscribed polygon of double the number of sides is formed. Thus, in Fig. 44, the octagon EFGH, etc., is formed by drawing tangents at the middle points of the arcs between

adjacent points of contact of the sides of the circumscribed square ABCD.

CIRCULAR MEASUREMENTS

THE CIRCLE

LENGTH OF ANY ARC

71. If any two circles are taken, and two regular polygons of the same number of sides are inscribed in them, the perimeters of these polygons are to each other as the radii of the circles (Art. 66). This relation holds whatever the number of sides of the polygon. Now, it is evident that, as this number increases, the perimeters of the two polygons approach the circumferences of their respective circles. We may, therefore, consider these circumferences as extreme cases of the perimeters of regular polygons, in which the number of sides is increased indefinitely; whence we conclude that the circumferences, also, are to each other as their radii.

If c and c' are the circumferences of any two circles, and r and r' their respective radii, we may write,

	c:c'=r:r'
whence,	c:r=c':r'
or,	$\frac{c}{r}=\frac{c'}{r'}$

Dividing both numbers by 2, and denoting the diameters by d and d'.

$$\frac{c}{2r} = \frac{c'}{2r'}$$
$$\frac{c}{d} = \frac{c'}{d'}$$

that is,

As c and c' are any two circumferences, it is seen that the ratio obtained by dividing any circumference by its diameter is the same for all circumferences. This ratio is usually

denoted by the Greek letter π (pronounced pi). We have, therefore, for any circle,

$$\frac{c}{d} = \pi$$
$$c = \pi d = 2\pi$$

whence,

72. The quantity π can be determined by elementary geometrical methods, which may be found in treatises on geometry; but these methods are very laborious. A much better method is afforded by the theory of series, which is treated in works on trigonometry and the differential calculus. It is found that π cannot be expressed as an exact fraction, either decimal or vulgar. Its value can, however, be calculated to any desired degree of approximation. The following value is approximate to fifteen decimal places:

 $\pi = 3.141592653589793 +$

For nearly all practical purposes, 3.1416 is a sufficiently close value. This value is used very generally, and will be used in this Course, unless otherwise stated. The student should commit it to memory. A value that is often used in rough calculations is $\frac{2.2}{7}$; it can be used when no more than three significant figures are required in the result.

73. The length of an arc, when the number of degrees in the arc and the radius of the circle are given, may be found as follows:

The length of the arc is evidently the same part of the length of the circumference $(2 \pi r)$ as the number of degrees in the arc is of the number of degrees in the whole circumference, or 360° . Thus, if *n* is the number of degrees in the arc, and *l* is its length, we shall have,

$$\frac{2\pi r}{l} = \frac{360}{n}$$
$$l = \frac{\pi r n}{180}$$

whence,

In applying this formula, minutes and seconds should be expressed as fractions of a degree.

EXAMPLE 1.—Find the length of a rope that will go around a wheel or drum 7.5 feet in diameter. SOLUTION.—The required length is equal to the length c of the circumference of the wheel or drum. Here d = 7.5 ft., and, taking $\pi = 3.1416$, we have, by formula of Art. 71,

$$c = 3.1416 \times 7.5 = 23.562$$
 ft. Ans.

Using $\frac{32}{7}$ for π , the result, to three significant figures, is

$$c = \frac{22}{7} \times 7.5 = 23.6$$
 ft. Ans.

EXAMPLE 2.-Find the diameter of a circular race track 1 mile in length.

SOLUTION.—Here c is given (= 1 mi. = 5,280 ft.) and the quantity required is d. From the formula $c = \pi d$, we get

$$d = \frac{c}{\pi} = \frac{5,280}{3.1416} = 1,680.7$$
 ft. Ans.

EXAMPLE 3.—What is the length of a railroad circular curve having a radius of 1,540 feet and subtending an angle at the center equal to 26° 35'?

SOLUTION.—To apply formula of Art. 73, we have r = 1,540 ft., $n = 26\frac{3}{60} = 26.583^{\circ}$, nearly. Therefore,

$$l = \frac{3.1416 \times 1,540 \times 26.583}{180} = 714.50 \text{ ft.} \text{ Ans}$$

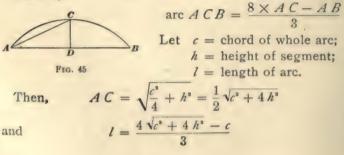
74. When only the chord AB, Fig. 45, of an arc and the height, or "rise," CD of the segment are known, the following approximate method gives good results. AC, the chord of half the arc, has the value

$$A C = \sqrt{\overline{A D}^{\circ} + \overline{C D}^{\circ}} = \sqrt{\left(\frac{\overline{A B}}{2}\right)^{\circ} + \overline{C D}^{\circ}}$$

Then, to find the length of the arc:

Rule.—From eight times the chord of half the arc, subtract the chord of the whole arc and divide the remainder by 3.

That is,



This formula gives the length of an arc less than one-sixth of the circumference correct to four figures, and it gives the length of an arc less than one-third of the circumference correct to three figures.

EXAMPLE.—Find the length of the arc ACB, Fig. 46.

Solution.—In this example, c = 72, h = 8. Therefore,

$$L = \frac{4\sqrt{72^{\circ} + 4 \times 8^{\circ} - 72}}{3} = 74.34 \text{ in.}$$
FIG. 46

75. For very flat arcs, that is, when $\frac{h}{c}$ is very small (say

not greater than .1), the following approximate formula may be used, the notation being the same as in the preceding article:

$$l = c + \frac{8h^2}{3c}$$

EXAMPLE 1.—Find the length of the arc AB, Fig. 46.

SOLUTION .-

$$l = 72 + \frac{8 \times 8^{\circ}}{3 \times 72} = 72 + 2.37 = 74.37$$
. Ans.

This is not a very close approximation, because the ratio $\frac{h}{c}\left(=\frac{8}{72}=\frac{1}{9}\right)$ is not very small; however, the approximate value thus found would be close enough for most practical purposes.

EXAMPLE 2.—The chord of a railroad curve is 675 feet long, and the rise (or, "middle ordinate," as the rise is called in railroad work) is 40 feet; what is the length of the curve?

Solution.—Here c = 675, h = 40, and therefore $l = 675 + \frac{8 \times 40^3}{3 \times 675} = 675 + 6.32 = 681.32$ ft. Ans.

76. Circular Measure of an Angle.—The following equation follows from the formula of Art. 73:

$$\frac{l}{r} = \frac{\pi n}{180} = \frac{\pi}{180} \times n$$

If we assume the radius to be 1, then

$$l = \frac{\pi}{180} \times n \qquad (1)$$

This equation gives the length of the arc that the angle subtends on a circle whose radius is equal to unity. The length of such arc is called the **circular measure** of the angle, and the angle is often referred to by stating that measure. Thus, an angle of 1.34, circular measure, means an angle that subtends an arc of length 1.34 on a circle whose radius is 1. An angle expressed in circular measure is also said to be expressed in radians.

If in equation 1 we make $n = 180^{\circ}$, we obtain, for the circular measure of 180° , $l = \pi$, that is, 180° is equivalent to π radians. Likewise, 90° is equivalent to $\frac{\pi}{2}$ radians, etc.

EXAMPLES FOR PRACTICE

1. Find the distance around the outside of a waterwheel whose outside diameter is 22 feet 8 inches. Ans. 71.21 ft.

2. The wheel of a carriage is observed to turn 375 times in going from a certain place to another; the diameter of the wheel is 3.5 feet; what is the distance between the two places? Ans. 4,123.4 ft.

3. A circular column measures 45.5 inches around the outside; what is its diameter? Ans. 14.483 in.

4. A belt covers an arc of 50° on a pulley whose diameter is 5 feet; what length of the belt is in contact with the pulley? Ans. 2.1817 ft.

5. How long will it take a train to move over a curve subtending an angle of 100°, the radius of the curve being 1,800 feet, and the train going at the rate of 20 miles an hour? Ans. 1.79 min.

6. The length of arc of a circle is equal to the radius; find the number of degrees in the arc. Ans. $57.3^\circ = 57^\circ 18'$, nearly

7. The chord of a railroad curve is 600 feet long and the middle ordinate is 80 feet; what is the length of the curve? Ans. 628 ft.

AREAS BOUNDED BY CIRCULAR ARCS

77. The area of a circle is equal to one-half the product of its circumference and radius (Art. 67). This at once iollows by considering the circle as an extreme case of a regular polygon.

Let A =area of circle;

c = circumference of circle;

r = radius of circle.

 $A = \frac{1}{2}cr$

Then, or, since $c = 2 \pi r$,

$$A = \frac{1}{2} 2 \pi r \times r$$

or, simplifying,

$$A = \pi r^3 = 3.1416 r^3$$
 (1)

Writing $\frac{d}{2}$ for r, we obtain for the area in terms of the diameter.

$$A = \frac{\pi d^{*}}{4} = .7854 d^{*} \qquad (2)$$

These formulas serve likewise to find r or d when A is given. Since $2 \pi r = c$, we have

$$r = \frac{c}{2\pi}, \text{ and } \pi r^{s} = \pi \left(\frac{c}{2\pi}\right)^{s} = \frac{c^{s}}{4\pi}$$
$$A = \frac{c^{s}}{4\pi} \qquad (3)$$

that is,

This formula gives the area of a circle when its circumference is known.

EXAMPLE 1.—The steam pressure on a piston is 75 pounds per square inch, and the diameter of the piston is 15 inches; what is the pressure on the whole surface of the piston?

Solution.—The required pressure is evidently seventy-five times the number of square inches in the surface of the piston, or seventy-five times the area A of the piston. Here d = 15 in., and formula 2 gives $A = .7854 \times 15^{\circ}$

whence the total pressure is

 $75 \times .7854 \times 15^{\circ} = 13,254$ lb. Ans.

EXAMPLE 2.—The distance around a circular park is 2.75 miles; what is the area of the park, in acres?

SOLUTION.—Here c is given equal to 2.75 mi. = (2.75×80) ch. Therefore, the area of the park, in square chains, is (formula 3)

$$\frac{(2.75 \times 80)^{\circ}}{4 \times 3.1416}$$

The area, in acres, is one-tenth of this, or

 $\frac{1}{10} \times \frac{(2.75 \times 80)^{\circ}}{4 \times 3.1416} = \frac{220^{\circ}}{125.664} = 385.15 \text{ A.} \text{ Ans.}$

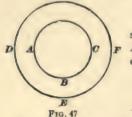
EXAMPLE 3.—What must be the diameter of a circular sewer pipe that 'ts cross-section may be 12.75 square feet?

SOLUTION.—Solving formula 2 for d,

$$d = \sqrt{\frac{A}{.7854}} = \sqrt{\frac{12.75}{.7854}} = 4.03$$
 ft. Ans.

EXAMPLES FOR PRACTICE

1 The cable of a suspension bridge measures 40 inches around its circumference: find: (a) the diameter d of the cable: (b) the area AAns. $\begin{cases} (a) \ d = 12.732 \text{ in.} \\ (b) \ A = 127.32 \text{ sq. in} \end{cases}$ of the cross-section.



2. Find a formula for the area A of the space enclosed between two circles A B C and DEF, Fig. 47, the diameter of the outer circle being D, and that of the inner circle d.

Ans.
$$\begin{cases} A = \frac{\pi}{4}(D^{*} - d^{*}) \\ A = \frac{\pi}{4}(D + d)(D - d) \end{cases}$$

3. What must be the inner diameter of a circular chimney, that Ans. 4.2221 ft its inner cross-section may be 14 square feet?

4. The diameter of a circular airway of a mine is 10 feet; find: (a) the circumference c; (b) the area A of the cross-section.

Ans. $\begin{cases} (a) \ c = 31.416 \ \text{ft.} \\ (b) \ A = 78.54 \ \text{sq. ft.} \end{cases}$

78. A sector is the same part of a circle as its arc is of the circumference.

Let A = area of circle: A' = area of sector: n = number of degrees in arc of sector.

Then,	A': A	A =	n:	360
whence,	A' =	$\frac{n A}{360}$	-	$\frac{\pi r^3 n}{360}$

EXAMPLE.—The angle of a sector of a circle is 75°; the diameter of the circle is 12 inches; what is the area of the sector?

Solution.—The area A of the circle is $12^{\circ} \times .7854$ sq. in. Then the area of the sector is

$$\frac{nA}{360} = \frac{75 \times 12^{\circ} \times .7854}{360} = 23.562 \text{ sq. in. Ans.}$$

79. The area of a sector is equal to one-half the product of its base by the radius of the circle.

$$A' = \frac{1}{2} rl$$

If l is the length of the arc, or base, of a sector, we have (Art. 73).

 $l = \frac{\pi r n}{180}$ $n = \frac{180 l}{\pi r}$

whence,

This value of n substituted in formula of Art. 78 gives

$$A' = \frac{\pi r^3}{360} \times \frac{180 l}{\pi r}$$
$$A' = \frac{1}{2} r l$$

or, reducing,

EXAMPLE.—If the radius of an arc is 5 feet and the length of the arc is 4 feet, what is the area of the sector?

SOLUTION .- By formula of Art. 79,

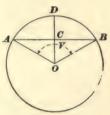
$$A' = \frac{lr}{2} = \frac{4 \times 5}{2} = 10$$
 sq. ft. Ans.

80. The area of a segment, as ADB, Fig. 48, is evidently equal to the area of the sector AOBD minus the area of the triangle AOB.

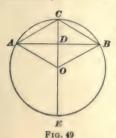
EXAMPLE 1.—The diameter of a circle is 10 inches, and the chord of the arc of a segment is 7 inches; what is the area of the segment?

SOLUTION.—In Fig. 48, let AB = 7 in. and the diameter = 10 in. Then, OB = 5 in., and CB = 3.5 in. Hence,

 $OC = \sqrt{5^2 - 3.5^2} = 3.57$ in., and CD = 5- 3.57 = 1.43 in. Then, by formula of Art. 74, arc $ADB = \frac{4\sqrt{7^2 + 4 \times 1.43^2} - 7}{3} = 7.75$ in. Hence, area of sector $AOBD = \frac{1}{2} \times 5 \times 7.75$ = 19.38 sq. in. The area of the triangle $AOB = \frac{1}{2} \times 3.57 \times 7 = 12.50$ sq. in. Therefore, the area of the segment is 19.38 - 12.50 = 6.88 sq. in. Ans.







EXAMPLE 2.—The chord of the arc of a segment is 79 inches and the height of the segment is 20 inches: find the area of the segment.

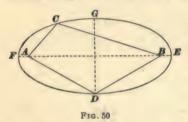
SOLUTION.—Let A CBE, Fig. 49, be the circle; let AB = 79 in. and CD = 20 in. Then. $AD = \frac{1}{2} \times 79$ in. = 39.5 in. By Art. 28,

CD: AD = AD: DEor, 20: 39.5 = 39.5 : DEwhence, DE = 78.01

Hence, the diameter = 20 + 78.01 = 98.01 in., and the radius = 49. Then the arc $A CB = \frac{4 \sqrt{79^{\circ} + 4 \times 20^{\circ} - 79}}{3} = 91.7$ in. Hence, the area of sector $A OBC = 91.7 \times \frac{1}{4} \times 49 = 2,246.65$ sq. in. The area of the triangle $A OB = \frac{1}{4} \times 79 \times 29 = 1,145.5$ sq. in. Therefore, the area of the segment = 2,246.65 - 1,145.50 = 1,101.15 sq. in. Ans.

THE ELLIPSE

81. An ellipse is a plane figure bounded by a curved line such that the sum of the distances of any point on that line from two fixed points within is always equal to the length of the line passing through the fixed points and terminating at both ends in the curved line.



In Fig. 50, the fixed points are A and B, and if C and D are any two points on the curve, AC + CB = AD+DB = FE. The two fixed points are the foci. The line FE through the foci is the transverse, or major, axis.

The line GD, which is the perpendicular bisector of FE, is the conjugate, or minor, axis. The foci may be located from G or D as a center by striking arcs with a radius equal to one-half FE.

82. There is no simple and exact method of finding the periphery (perimeter) of an ellipse. The following formula gives values very nearly exact:

Let C = periphery; a = half the major axis; b = half the minor axis; $D = \frac{a-b}{a+b}.$ Then, $C = \pi(a+b)\frac{64-3}{64-16}\frac{D^{*}}{D^{*}}$

EXAMPLE.—What is the periphery of an ellipse whose axes are 10 inches and 4 inches long?

SOLUTION.—In this example, a = 5, b = 2, $D = \frac{5-2}{5+2} = \frac{3}{7}$. Then, $C = 3.1416(5+2)\frac{64-3(\frac{3}{7})^4}{64-16(\frac{3}{7})^2} = 23.013$ Therefore, the periphery is 23.013 in. Ans.

83. The area of an ellipse is equal to the product of its two semiaxes multiplied by π .

Let a = half the major axis;

b = half the minor axis;

A = area.

Then,
$$A = \pi \ a \ b = 3.1416 \ a \ b$$

EXAMPLE.—What is the area of an ellipse whose axes are 10 inches and 6 inches?

Solution.—Here, $a = \frac{1}{4} \times 10 = 5$, $b = \frac{1}{4} \times 6 = 3$. Then, $A = 3.1416 \times 5 \times 3 = 47.124$ Therefore, the area is 47.12 sq. in. Ans.

EXAMPLES FOR PRACTICE

1. The number of degrees in the angle formed by drawing radii from the center of a circle to the extremities of an arc of the circle is 84; the diameter of the circle is 17 inches; what is the area of the sector? Ans. 52.96 sq. in.

2. Given the chord of the arc of a segment equal to 24 inches, and the height of the segment equal to 6.5 inches, find: (a) the diameter of the circle; (b) the area of the segment. Ans. $\begin{cases} (a) & 28.7 \text{ in.} \\ (b) & 109.5 \text{ sq. in.} \end{cases}$

3. (a) What is the perimeter of an ellipse whose axes are 15 inches and 9 inches? (b) What is the area? Ans. $\begin{cases} (a) & 38.29 \text{ in.} \\ (b) & 106.03 \text{ sq. in.} \end{cases}$

4. The base of a sector is 24 inches and the diameter of the circle is 54 inches; what is the area of the sector? Ans. 324 sq. in.

THE MENSURATION OF SOLIDS

84. A solid, or body, has three dimensions: length. breadth, and thickness.

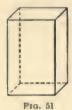
85. The entire area of a solid is the area of the whole outside of the solid.

The convex area of a solid having one or two flat ends is the same as the entire surface, except that the areas of the ends or bases are not included.

86. The volume of a solid is expressed by the number of times that it will contain another volume, called the unit of volume. Instead of the word *volume*, the expression cubical contents is frequently used.

THE PRISM AND CYLINDER

87. A prism is a solid whose ends are equal polygons in parallel planes, and whose sides are parallelograms.



88. A parallelopipedon, Fig. 51, is a prism whose bases (ends) are parallelograms.

89. A cube, Fig. 52, is a parallelopipedon whose faces and ends are squares.



90. The cube whose edges are equal to the unit of length is taken as the unit of volume when finding the volume of a solid.

Thus, if the unit of length is 1 inch, the unit of volume will be the cube each of whose edges measures 1 inch, or 1 cubic inch; and the number of cubic inches the solid contains will be its volume. If the unit of length is 1 foot, the unit of volume will be 1 cubic foot, etc. Cubic inch, cubic foot, and cubic yard are abbreviated to cu. in., cu. ft., and cu. yd., respectively.

91. Prisms take their names from their bases. Thus, a *triangular prism* is one whose bases are triangles; a *pentagonal prism* is one whose bases are pentagons, etc.

92. A cylinder, Fig. 53, is a round body of uniform diameter with circles for its ends.

93. A **right prism**, or **right cylinder**, is one whose center line (axis) is perpendicular to its bases.

94. The altitude of a prism or cylinder is the perpendicular distance between its two ends.

95. To find the convex area of any right prism, or right cylinder:

Rule.—Multiply the perimeter of the base by the altitude.

Let p = perimeter of base; h = altitude; c = convex area.

Then,

EXAMPLE 1.—What is the convex area of a right prism whose base is a square, one side of which is 9 inches, and whose altitude is 16 inches?

c = p h

SOLUTION.— $9 \times 4 = 36$ in., the perimeter of the base. Applying formula of Art. 95,

 $c = 36 \times 16 = 576$ sq. in., the convex area. Ans.

To find the entire area, add the areas of the two ends to the convex area.

EXAMPLE 2.—What is the entire area of the paraflelopipedon mentioned in the last question?

FIG. 53

SOLUTION.—The area of one end is $9^{\circ} = 81$ sq. in. $81 \times 2 = 162$ sq. in., is the area of both ends. 576 + 162 = 738 sq. in., the entire area of the parallelopipedon. Ans.

EXAMPLE 3.—What is the entire area of a right cylinder whose base is 16 inches in diameter, and whose altitude is 24 inches?

SOLUTION. $-16 \times 3.1416 = 50.27$ in., or the perimeter (circumference) of the base. $50.27 \times 24 = 1,206.48$ sq. in., the convex area.

 $16^{\circ} \times .7854 \times 2 = 402.12$ sq. in., the area of the ends.

1,206.48 + 402.12 = 1,608.6 sq. in., the entire area. Ans.

96. To find the volume of a prism, or cylinder:

Rule.—The volume of any prism or cylinder is equal to the area of the base multiplied by the altitude.

Let A = area of base; h = altitude; V = volume.

Then,

V = Ah

If the given prism is a cube, the three dimensions are all equal, and the volume equals the cube of one of the edges. Hence, if the volume is given, the length of an edge is found by extracting the cube root.

If the volume and the area of the base are given, the altitude is $h = \frac{V}{A}$. If the cylinder or prism is hollow, the volume is equal to the area of the ring or base multiplied by the altitude.

EXAMPLE 1.—What is the volume of a rectangular prism whose base is 6 inches by 4 inches, and whose altitude is 12 inches?

SOLUTION.—The base of a rectangular prism is a rectangle; hence, $6 \times 4 = 24$ sq. in., the area of the base. Applying formula of Art. 96, $V = 24 \times 12 = 288$ cu. in., or the volume. Ans.

EXAMPLE 2.—What is the volume of a cube whose edge is 9 inches?

SOLUTION. $-9^3 = 9 \times 9 \times 9 = 729$ cu. in., the volume. Ans.

EXAMPLE 3.—What is the volume of a cylinder whose base is 7 inches in diameter, and whose altitude is 11 inches?

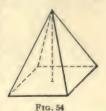
SOLUTION.— $7^9 \times .7854 = 38.48$ sq. in., the area of the base. Applying formula of Art. 96,

 $V = 38.48 \times 11 = 423.28$ cu. in., the volume. Ans.

THE PYRAMID AND CONE

97. A pyramid, Fig. 54, is a solid whose base is a

polygon, and whose sides are triangles uniting at a common point, called the vertex. If the base is a regular polygon, and the sides have the same inclination to the base, the pyramid is a regular pyramid.



98. A cone, Fig. 55, is a solid whose



base is a circle, and whose convex surface tapers uniformly to a point called the vertex.

99. The altitude of a pyramid or cone is the perpendicular distance from the vertex to the base.

FIG. 55

100. The slant height of a regular pyr-

amid is a line drawn from the vertex perpendicular to one of the sides of the base. The slant height of a cone is a straight line drawn from the vertex to the circumference of the base, and lying on the surface of the cone.

101. To find the convex area of a regular pyramid or a cone:

Rule.—The convex area of a regular pyramid or of a cone is equal to the perimeter of the base multiplied by one-half the slant height.

```
Let p = \text{perimeter};

s = \text{slant height};

c = \text{convex area.}

Then, c
```

$$=\frac{ps}{2}$$

EXAMPLE 1.—What is the convex area of a regular pentagonal pyramid, if each side of the base measures 6 inches and the slant height measures 14 inches?

SOLUTION.—The base of the pentagonal pyramid is a pentagon, and consequently it has five sides. $6 \times 5 = 30$ in., or the perimeter of the base. Applying formula of Art. 101,

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 $c = \frac{p s}{2} = \frac{30 \times 14}{2} = 210$ sq. in., the convex area. Ans.

EXAMPLE 2.—What is the entire area of a cone whose altitude is 15 inches, and whose base is 16 inches in diameter?

SOLUTION.—The slant height of the cone is the hypotenuse of a right triangle whose legs are the radius of the base and altitude of the cone, respectively. Therefore, the slant height is equal to $\sqrt{15^{\circ} + 8^{\circ}} = 17$ in. (Art. 56). The perimeter of the base is $16 \times 3.1416 = 50.2656$ in. Applying formula of Art. 101,

$$c = \frac{50.2656 \times 17}{2} = 427.26$$
 sq. in.

The area or the base is $16^{\circ} \times .7854 = 201.06$ sq. in. The entire area is, therefore, 427.26 + 201.06 = 628.32 sq. in. Ans.

102. To find the volume of any pyramid or cone:

Rule.—The volume of any pyramid or cone equals the area of the base multiplied by one-third of the altitude.

Let A = area of base; h = altitude; V = volume.

Then,

$$V = \frac{Ah}{3}$$

EXAMPLE 1.—What is the volume of a triangular pyramid, each edge of whose base measures 6 inches, and whose altitude is 8 inches?

SOLUTION.—The base is an equilateral triangle; hence, applying the rule of Art. 68, the area is $6^{\circ} \times .433 = 15.59$ sq. in. Applying formula of Art. 102,

$$V = \frac{Ah}{3} = \frac{15.59 \times 8}{3} = 41.57$$
 cu. in. Ans.

EXAMPLE 2.—What is the volume of a cone whose altitude is 18 inches, and whose base is 14 inches in diameter?

Solution.— $14^{a} \times .7854 = 153.94$ sq. in., the area of the base. Applying formula of Art. 102,

 $V = \frac{Ah}{3} = \frac{153.04 \times 18}{8} = 923.64$ cu. in., the volume. Ans.

103. It has been stated that the volume of a cone or a pyramid is equal to one-third the product of the area of the base multiplied by the altitude. Similarly, the volume of any solid whose base is a plane figure and which tapers to a

point like a cone or a pyramid is equal to one-third of the product of its base and altitude.

EXAMPLE.-Find the volume of an elliptical cone, whose base is an ellipse with diameters 8 inches and 6 inches, and the altitude is 7.5 inches.

Solution.—The area of the ellipse at the base is $3.1416 \times 4 \times 3$ The volume is equal to one-third the product of the area of the base and altitude: that is,

$$V = \frac{1}{2} \times 3.1416 \times 4 \times 3 \times 7.5 = 94.248$$

Hence, the volume is 94.248 cu. in. Ans.

EXAMPLES FOR PRACTICE

1. Find the volume of a triangular pyramid of which the altitude is 4 inches and the base is an equilateral triangle having each side 3 inches long. Ans. 5.2 cu. in.

2. Find the weight of a steel bar 16 feet long and 2 inches in diameter, the weight of steel being taken as .28 pound per cubic inch. Ans. 168.89 lb.

3. What is the entire area of a hexagonal prism 12 inches long, each side of the base being 1 inch long? Ans. 77,196 sq. in.

4. (a) Find the convex area of a cone whose altitude is 12 inches. and the circumference of whose base is 31.416 inches. (b) Find the volume of the cone. Ans. $\begin{cases} (a) & 204.2 \text{ sq. in.} \\ (b) & 314.16 \text{ cu. in} \end{cases}$

THE FRUSTUM OF A PYRAMID OR A CONE

104. If a pyramid is cut by a plane parallel to the base, as in Fig. 56, so as to form two parts, the lower part is called a frustum of the pyramid.

105. If a cone is cut in a similar manner, as in Fig. 57, the lower part is called a frustum of the cone.

106. The upper end of a frustum of a pyramid or cone is called the upper base, and the lower end the lower base. The altitude

of a frustum is the perpendicular distance between the bases.



107. To find the convex area of a frustum of a regular pyramid or of a cone:

Rule.—The convex area of a frustum of a regular pyramid or of a cone equals one-half the sum of the perimeters of its bases multiplied by the slant height of the frustum.

Let	Þ	=	perimeter of lower base;
	p	=	perimeter of upper base;
	\$	=	slant height;
	с	_	convex area.
			(p + p')

Fig. 57 Then.

EXAMPLE 1.—Given the frustum of a triangular pyramid in which each side of the lower base measures 10 inches, each side of the upper base measures 6 inches, and whose slant height is 9 inches; find the convex area.

 $c = \left(\frac{p+p}{2}\right)s$

SOLUTION.— 10 in. $\times 3 = 30$ in., the perimeter of the lower base. 6 in. $\times 3 = 18$ in., the perimeter of the upper base. Applying formula of Art. 107,

 $c = \left(\frac{p+p'}{2}\right)s = \frac{30+18}{2} \times 9 = 216$ sq. in., the convex area. Ans.

EXAMPLE 2.—If the diameters of the two bases of a frustum of a cone are 12 inches and 8 inches, respectively, and the slant height is 12 inches, what is the entire area of the frustum?

SOLUTION. $\rightarrow \frac{(12 \times 3.1416) + (8 \times 3.1416)}{2} \times 12 = 376.99 \text{ sq. in., the}}{2}$ convex area. $8^{9} \times .7854 = 50.27 \text{ sq. in.}$ $12^{9} \times .7854 = 113.1 \text{ sq. in.}$

113.1 + 50.27 = 163.37 sq. in., the area of the two ends. 376.99 + 163.37 = 540.36 sq. in., the entire area of the frustum. Ans.

108. To find the volume of the frustum of a pyramid or a cone:

Rule.—Add the areas of the upper base, the lower base, and the square root of the product of the areas of the two bases; multiply this sum by one-third of the altitude.

Let A = area of lower base; a = area of upper base; \hbar = altitude; V = volume.

Then,

$$V = (A + a + \sqrt{A a})\frac{h}{3}$$

EXAMPLE 1.—Given a frustum of a hexagonal pyramid in which each edge of the lower base measures 8 inches, and each edge of the upper base measures 5 inches, and whose altitude is 14 inches, what is its volume?

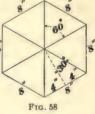
SOLUTION.—A hexagonal pyramid is one whose base is a regular hexagon, as shown in Fig. 58. Hence, applying formula of Art. 68.

 $A = 8^{\circ} \times 2.5981 = 166.28$ sq. in.

In a similar way, the area of the upper base is found to be 64.95 sq. in. Then, applying formula of Art. 108,

$$V = (166.28 + 64.95 + \sqrt{166.28 \times 64.95})^{14}$$

=
$$335.15 \times \frac{14}{3} = 1,564.03$$
 cu. in., the volume. Ans.



EXAMPLE 2.—What is the volume of a frustum of a cone whose upper base is 8 inches in diameter, whose lower base is 12 inches in diameter, and whose altitude is 15 inches?

SOLUTION.—The area of the upper base is $8^* \times .7854 = 50.27$ sq. in. The area of the lower base is $12^* \times .7854 = 113.1$ sq. in., nearly. The square root of their product is $\sqrt{50.27 \times 113.1} = 75.4$.

Then, $V = (50.27 + 113.1 + 75.4)\frac{15}{3}$ = 238.77 × $\frac{15}{3}$ = 1,193.85 cu. in., the volume. Ans.

THE WEDGE

109. A wedge, as here considered, is a solid whose base is a rectangle, two of whose opposite faces are parallel triangles, and two are parallelograms whose intersection is called the edge of the wedge. A wedge may therefore be defined as a triangular prism having one rectangular face, called the base. In Fig. 59, *ABCD* is the base and *EF* the edge of the wedge.

FIG. 59 110. The altitude of a wedge is the perpendicular distance between the base and the opposite edge. 111. To find the volume of a wedge:

Rule. - The volume of any wedge is caual to the area of the base multiplied by one-half the altitude.

Let A = area of base: h = altitude: V = volume.

Then.

$$V = \frac{Ah}{2}$$

EXAMPLE.—What is the volume of a wedge whose base is a rectangle 6 feet long and 4 feet wide, and whose altitude is 10 feet?

SOLUTION. – The area of the base is $4 \times 6 = 24$ sq. ft. Applying formula of Art. 111.

$$V = \frac{24 \times 10}{2} = 120$$
 cu. ft. Ans.

EXAMPLES FOR PRACTICE

1. Steel weighs .28 pound per cubic inch; find the weight of a steel wedge whose base is a rectangle 3 inches by 14 inches and whose altitude is 8 inches. Ans. 5.04 lb.

2. Find the volume of the frustum of a square pyramid of which the larger base is 15 inches square, the smaller base, 14 inches square. and the altitude, 3 inches. Ans. 631 cu. in.

3. A round tank is 8 feet in diameter at the top (inside) and 10 feet at the bottom; if the tank is 12 feet deep, how many gallons will it hold, there being 231 cubic inches in a gallon? Ans. 5.734.2 gal.

4. (a) What is the convex area of the frustum of a square pyramid whose altitude is 16 inches, one side of whose lower base is 28 inches long, and of the upper base 10 inches? (b) What is the volume of the Ans. $\begin{cases} (a) & 1,395.18 \text{ sq. in.} \\ (b) & 6,208 \text{ cu. in.} \end{cases}$ frustum.



FIG. 60

THE SPHERE

112. A sphere, Fig. 60, is a solid bounded by a uniformly curved surface every point of which is equally distant from a point within, called the center.

The word ball is commonly used instead of sphere.

113. To find the area of the surface of a sphere

Rule.—The area of the surface of a sphere equals the square of the diameter multiplied by π .

Let S =surface;

d = diameter.

Then,

$$S = \pi d^*$$

EXAMPLE.—What is the area of the surface of a sphere whose diameter is 14 inches?

Solution.—Applying formula of Art. 113, $S = 3.1416 \times 14^{\circ}$ = 3.1416 × 14 × 14 = 615.75 sq. in., the area. Ans.

114. To find the volume of a sphere:

Rule.—The volume of a sphere equals the cube of the diameter multiplied by $\frac{\pi}{c}$.

 $\frac{1}{6}$

Let V = volume; d = diameter.

Then,

$$V = \frac{\pi}{6}d^{\mathfrak{s}} = .5236d^{\mathfrak{s}}$$

EXAMPLE.—What is the weight of a lead cannon ball 12 inches in diameter, a cubic inch of lead weighing .41 pound?

SOLUTION.—Applying formula of Art. 114, $V = .5236 \times 12 \times 12 \times 12 = 904.78$ cu. in., the volume of the ball.

 $904.78 \times .41 = 370.96$ lb. Ans.

The volume of a spherical shell, or hollow sphere, is equal to the difference in volume between two spheres having, respectively, the outer and the inner diameter of the shell.

115. To find the diameter of a sphere of known volume:

Rule.—Divide the volume by .5236 and extract the cube root of the quotient. The result is the diameter.

$$d = \sqrt[3]{\frac{V}{.5236}} = 1.2407 \sqrt[3]{V}$$

EXAMPLE.—The volume of a sphere is 96.1 cubic inches; what is its diameter?

SOLUTION.-Applying formula of Art. 115,

$$d = \sqrt[3]{\frac{V}{.5236}} = \sqrt[3]{\frac{96.1}{.5236}} = 1.2407 \sqrt[3]{96.1} = 5.68 \text{ in.}$$
 Ans.

116. If any solid is cut into two parts by a plane, the surface of either part exposed by the removal of the other part is called a plane section of the solid.

Plane sections are divided into three classes: longitudinal sections, cross-sections, and right sections. A longitudinal section is any plane section taken lengthwise through the solid. Any other plane section is called a cross-section. If the surface exposed by taking a plane section of a solid is perpendicular to the center line of the solid, the section is called a **right section**. The surface exposed by any longitudinal section of a cylinder is a rectangle. The surface exposed by a right section of a cube is a square; of a cylinder or a cone, a circle. An oblique cross-section of a cylinder is an ellipse.

THE CYLINDRICAL RING

117. A cylindrical ring is a solid that may be generated by a circle revolving about an external axis in its plane.

118. To find the convex area of a cylindrical ring:

Rule.—Multiply the circumference of an imaginary crosssection on the line AB, Fig. 61, by the length of the center line D.

EXAMPLE.—A piece of round iron rod is bent into circular form to make a ring for a chain; if the outside diameter of the ring is 12 inches and the inside diameter is 8 inches, what is its convex area?

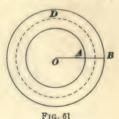
SOLUTION.—The diameter of the center circle equals one-half the sum of the inside and outside diameters, $\frac{12+8}{2} = 10$, and 10×3.1416 = 31.416 in., the length of the center line. The radius of the inside circle is 4 in., of the outside circle 6 in.; therefore, the diameter of the cross-section on the line AB is 2 in. Then, $2 \times 3.1416 = 6.2832$ in., and $6.2832 \times 31.416 = 197.4$ sq. in., or the convex area. Ans.

119. To find the volume of a cylindrical ring:

Rule.—The volume will be the same as that of a cylinder whose altitude equals the length of the dotted center line D. Fig. 61, and whose base is the same as a cross-section of the ring

on the line A B, drawn from the center O. Hence, to find the volume of a cylindrical ring, multiply the area of an imaginary cross-section on a line A B, by the length of the center line D.

EXAMPLE.—What is the volume of a cylindrical ring whose outside diameter is 12 inches, and whose inside diameter is 8 inches?



SOLUTION.—The diameter of the center circle equals one-half the sum of the inside and outside diameters, $\frac{12+8}{2} = 10$. 10×3.1416 = 31.416 in., the length of the center line. The radius of the outside circle is 6 in., of the inside circle, 4 in.; therefore, the diameter of the cross-section on the line A B is 2 in. Then, $2^{\circ} \times .7854 = 3.1416$ sq. in., the area of the imaginary cross-section; and 3.1416×31.416 = 98.7 cu. in., the volume. Ans.

EXAMPLES FOR PRACTICE

1. (a) What is the area of the surface of a sphere 30 inches in diameter? (b) What is the volume of the sphere?

Ans. $\begin{cases} (a) & 2,827.44 \text{ sq. in.} \\ (b) & 14,137.2 \text{ cu. in.} \end{cases}$

2. (a) What is the convex area of a cylindrical ring, the outside diameter of the ring being 10 inches and the inside diameter $7\frac{1}{4}$ inches? (b) What is the volume of the ring? Ans. $\begin{cases} (a) 107.95 \text{ sq. in.} \\ (b) 33.734 \text{ cu. in.} \end{cases}$

3. The volume of a sphere is 606.132 cubic inches; what is the convex area of a cone whose slant height is 10 inches, and the diameter of whose base is the same as the diameter of the sphere?

Ans. 164.934 sq. in.

THE PRISMOID

120. A prismoid is a solid whose two bases are any polygons in parallel planes, and whose lateral faces may be divided into triangles and trapezoids by lines joining the vertexes of one base with those of the other. Thus, the solid shown in Fig. 62 is a prismoid; its bases are the pentagon ABCDE and the quadrilateral FGHI, which lie in

Fig. 62

parallel planes; and its faces are the triangle G B C and the

trapezoids G C D H, H D E I, I E A F, and F A B G.

121. The altitude of a prismoid is the perpendicular distance between the bases or parallel faces.

122. The parallel faces or bases of a prismoid are commonly called its end sections.

A prismoid is also defined as a solid

having two parallel end faces, and composed of any combination of prisms, wedges, and pyramids, whose common

altitude is the perpendicular distance between the parallel faces.

123. The middle section of a prismoid is the polygon formed by a plane, parallel to the bases, and cutting the prismoid at equal distances from the two bases or end sections. Thus, polygon PQRS is the middle section of the prismoid shown in Fig. 63.

P A B FIG. 63

124. Any dimension of the middle section of a prismoid may be taken equal to one-half the sum of the corresponding dimensions of the two end sections or bases. Thus, in Fig. 63, $PQ = \frac{1}{2}(AB + FG), QR = \frac{1}{2}BC, RS = \frac{1}{2}(GH + CD),$ and $SP = \frac{1}{2}(HF + DA)$.

125. The area of the middle section of a prismoid may be measured directly, or calculated from its dimensions as determined from the dimensions of the end sections. It is not, in general, equal to one-half the sum of the areas of the bases.

The area of the middle section of a prism is the same as the area of either base; the area of the middle section of a wedge is equal to one-half the area of the base; the area of the middle section of a pyramid is equal to one-fourth the area of the base.

126. To find the volume of a prismoid:

Rule.—Multiply the sum of the areas of the two end sections plus four times the area of the middle section by one-sixth the altitude.

Let A = area of one base or end section;

A' = area of opposite base or end section;

M = area of middle section;

h = altitude;

V = volume of prismoid.

Then,
$$V = \frac{h}{6}(A + A' + 4M)$$

This formula for finding the volume of a prismoid is known as the **prismoidal formula**. It is theoretically exact for determining the volumes of those solids to which it applies.

The derivation of this formula is as follows:

A prismoid can always be divided into elementary parts that will be prisms, wedges, and pyramids. From formula of Art. 96, the volume of a prism is V = Ah; from formula of Art. 111, the volume of a wedge is $V = \frac{Ah}{2}$; and from formula of Art. 102, the volume of a pyramid is $V = \frac{Ah}{3}$. If these expressions are reduced to a common denominator, there will result,

For a prism,	$V = \frac{6Ah}{6}$	(1)
For a wedge,	$V = \frac{3Ah}{6}$	(2)
For a pyramid,	$V = \frac{2Ah}{6}$	(3)

Since any prism is of uniform cross-section throughout its length, every section will have the same area A, and equation (1) may be written

$$V = \frac{6Ah}{6} = \frac{h}{6}(A + A' + 4M)$$

For a wedge, evidently A' = 0, and $M = \frac{1}{2}A$. Hence, equation (2) may be written

$$V = \frac{3Ah}{6} = \frac{h}{6}(A+0+2A) = \frac{h}{6}(A+A'+4M)$$

For a pyramid, A' = 0, and $M = \frac{1}{4}A$. Hence, equation (3) may be written

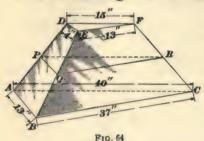
$$V = \frac{2Ah}{6} = \frac{h}{6}(A+0+A) = \frac{h}{6}(A+A'+4M)$$

GEOMETRY, PART 2

Each of these formulas is the same as the formula given in this article; which shows that the latter formula applies correctly to the volume of a prism, pyramid, or wedge, and since it applies to each, it applies also to their sum, or the volume of a prismoid.

EXAMPLE.—Find the volume of the prismoid shown in Fig. 64, whose altitude is 14 inches.

Solution.—Let PQR be the middle section. Then,



$$PQ = \frac{1}{2}(AB + DE) = \frac{1}{2}(13) + 4 = 8.5 \text{ in.}$$

$$OR = \frac{1}{2}(BC + EF) = \frac{1}{2}(37) + \frac{1}$$

- +13) = 25 in. $RP = \frac{1}{2}(AC + DF) = \frac{1}{2}(40)$
 - +15) = 27.5 in.

The areas of the triangles are calculated by formula of Art. 47, which gives the area of ABC = 240 sq. in., area of DEF = 24 sq. in., and Hence,

 $V = \frac{14}{2} \times (240 + 24 + 4 \times 105.2) = 1,597.9$ cu. in., nearly. Ans.

127. A familiar example of a prismoid is a railway cutting where the roadway is a horizontal plane, the side slopes are inclined planes, and the original surface of the ground is more or less inclined and irregular.

For calculating the volume of cuts and fills the prismoidal formula, though theoretically exact, gives results that are only approximate, on account of the inequalities of the surface of the ground. The nearer to each other the crosssections are taken, the more accurate will be the result.

EXAMPLE 1.—Find, by the prismoidal formula, the volume of the frustum of a square pyramid of which the larger base is 2.5 feet square, the smaller base is 1 foot square, and the altitude is 16 feet.

SOLUTION.—The area of the larger base is $2.5 \times 2.5 = 6.25$ sq. ft.; the area of the smaller base is $1 \times 1 = 1$ sq. ft. The middle section is a square whose side is one-half the sum of the side of the upper and lower base; that is, $\frac{1}{4} \times (2.5 + 1) = 1.75$ ft. The area of the middle section is $1.75^{\circ} = 3.0625$ sq. ft. Applying formula of Art. 126, the volume of the frustum is

 $\frac{1}{6} \times 16 \times (6.25 + 1 + 4 \times 3.0625) = 52$ cu. ft. Ans.

EXAMPLE 2.—In a railway cutting 200 feet long, the following are the areas, in square feet, of the cross-sections taken every 50 feet, namely: 2,700, 2,619, 2,556, 2,484, 2,610. What is its volume?

SOLUTION.-The volume between the first and the third cross-section is, by formula of Art. 126,

$$V = \frac{100}{6}(2,700 + 2,556 + 4 \times 2,619) = 262,200 \text{ cu. ft.}$$

The volume between the third and the fifth section is

$$V = \frac{100}{6}(2,556 + 2,610 + 4 \times 2,484) = 251,700 \text{ cu. ft.}$$

The volume of the cutting is the sum of the volumes of the two prismoids, which is 513,900 cu. ft. = 19,033 cu. yd. Ans.

128. Average End Areas.—In practice, the volume of cuts and fills is often calculated by what is known as the method by average end areas, or simply as the end area method. By this method, the volume of the solid is found by multiplying one-half the sum of the two end areas by the distance between the two sections. Thus, let

> A = area of one cross-section; A' = area of next cross-section;

h = perpendicular distance between sections;

V = volume.

$$V=\frac{h}{2}(A+A')$$

Results obtained by this formula are approximate and slightly larger than those given by the prismoidal formula. On account of its simplicity, the average end area formula is much used in practical earth-work calculations. The inequalities of the surface of the ground make it impossible to find the exact volume of a cut or fill, however accurate may be the formula applied.

EXAMPLE.—The areas of two cross-sections of a fill 50 feet apart are 2,700 and 2,619 square feet respectively; find the volume of the section, in cubic yards.

SOLUTION.—In this case, A = 2,700; A' = 2,619; and h = 50; then

$$V = \frac{50}{2}(2,700 + 2,619) = 132,975$$

Hence, the volume is 132,975 cu. ft. = 4,925 cu. yd. Ans.

GEOMETRY, PART 2

EXAMPLES FOR PRACTICE

1. Find the volume of a right prismoid whose bases are rectangles that measure 10 inches by 8 inches and 8 inches by 6 inches, and whose height is 40 inches. Ans. 2,533.3 cu. in.

2. A railway cutting is 800 feet in length; the areas, in square yards, of cross-sections taken every 100 feet are: 237, 220, 204, 187, 171, 186, 204, 210, 220. Find the number of cubic yards in the cutting: (a) by the prismoidal formula: (b) by average end areas.

Ans. { (a) 53,633 cu. yd. (b) 53,683 cu. yd.

3. Find, by the prismoidal formula, the volume of a frustum of a hexagonal pyramid, each side of the lower base being 12 inches; of the upper base, 8 inches; and the altitude being 12 inches.

Ans. 3,159.3 cu. in. 4. Find, by the prismoidal formula, the volume of a wedge whose base is a rectangle 15 feet in length and 9 feet in width, and whose altitude is 12 feet. Ans. 810 cu. ft.

PLANE TRIGONOMETRY (PART 1)

Serial 779A

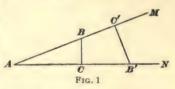
Edition 1

THE TRIGONOMETRIC FUNCTIONS

DEFINITIONS

1. Trigonometric Functions and Trigonometry Defined.—Let A, Fig. 1, be any acute angle; AM and AN, its sides; BC, a perpendicular drawn to the side AN from any point on the side AM; and B'C', a perpendicular drawn to the side AM from any point on the side AM. In the

right triangle A B C, one of the vertexes of which is the vertex of the angle A, the hypotenuse A B will be referred to as *the hypotenuse;* the perpendicular B C, opposite the vertex of the



angle A, as the side opposite; and the leg A C, containing the vertex of the angle A, as the side adjacent. Likewise, in the right triangle A B' C', the hypotenuse is A B'; the side opposite is B' C'; and the side adjacent, or the leg containing the vertex of the angle A, is A C'. It should be borne in mind that these terms are used in connection with, or with reference to, the angle A.

The two right triangles ABC and AB'C', having the acute angle A in common, are similar. Therefore,

$$\frac{AB}{AC} = \frac{AB'}{AC'}, \quad \frac{BC}{AB} = \frac{B'C'}{AB'}, \quad \frac{BC}{AC} = \frac{B'C'}{AC'}$$

It will be observed that, from whichever side the perpendicular is drawn, and whatever the point from which it is drawn, the ratio of the hypotenuse to the side adjacent

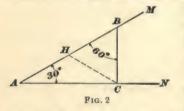
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remains unchanged, or is constant. The same is true of the ratio of the side opposite to the side adjacent, and, in general, of the ratio of any two of the three lines—hypotenuse, side adjacent, and side opposite. Evidently, these ratios are different for different angles. Thus, if A is 45°, both acute angles B and B' are also 45°; the triangles A B C and A B' C'are isosceles: and therefore

$$\frac{BC}{AC} = \frac{B'C'}{AC'} = 1$$

If A is greater than 45° , BC is greater than AC, and the ratio $\frac{BC}{AC}$, having its numerator greater than its denominator, is greater than 1.

Confining ourselves to the ratio $\frac{BC}{AC}$ of the side opposite to the side adjacent, it is seen that the value of this ratio depends on the magnitude of the angle, and may, therefore,



be used for the determination of the angle. Thus, it has just been shown that when the angle is 45° the ratio is equal to 1; hence, if in the solution of a problem it is found that the two legs of a right triangle are

equal, or that their ratio is 1, it can be at once concluded that each of the acute angles is 45° .

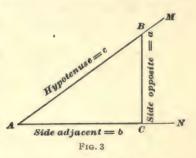
Consider now an angle A, Fig. 2, of 30°. The right triangle $A \ B \ C$ having been constructed, $B \ C$ is the side opposite and $A \ C$ the side adjacent. If H is the middle point of the hypotenuse, the line $H \ C$ is equal to $A \ H$, or $\frac{A \ B}{2}$; for, if a semicircle is described on $A \ B$ as a diameter, with $H \ A$ as a radius, that semicircle must pass through C, since the angle $A \ C \ B$ is a right angle. Now, $H \ C$ being equal to $H \ B$, the angle $H \ C \ B$ is equal to B, or 60° ; and, as the sum of the three angles of the triangle $B \ H \ C$ is 180°, the angle $B \ H \ C$ must be 60°. The triangle $H \ B \ C = B \ H = \frac{A \ B}{2}$, and the ratio of the side opposite to the hypotenuse is $\frac{BC}{AB} = \frac{\frac{1}{2}AB}{AB} = \frac{1}{2}$. Suppose, now, that in dealing with a right triangle the hypotenuse is found, by measurement, to be 1,500 feet and one of the sides 750 feet. Since the ratio of 750 to 1,500 is $\frac{1}{2}$, we at once conclude that the angle opposite the 750-foot side is 30°, and the other angle of the triangle, 60°.

These illustrations give a general idea of the practical value and use of the ratios under consideration. These ratios are determined for each angle, by methods that will be again referred to further on, and collected together in a table, from which the angle corresponding to any given ratio can be determined. Thus, if in a certain angle the ratio of the opposite side to the hypotenuse is $\frac{1}{2}$, this ratio is looked

for in the table, where it is found as that belonging to 30°.

In this manner, the value of the angle is determined from the ratio in question, that ratio being obtained from the measured lengths of certain lines.

2. The ratios considered in the preceding article are called trigonometric functions of the angle A. In the



triangle A B C, Fig. 3, two ratios are obtained by dividing any of three sides by each of the other two. Hence, there are six trigonometric functions of the angle A. This is true of any angle, since A is here used to represent any angle whatever. These functions have very important and useful properties, which make them exceedingly valuable for the solution of geometrical problems by computation.

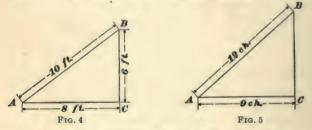
3. Trigonometry is that branch of mathematics that treats of the properties of trigonometric functions and of their application to the solution of triangles.

I L T 36F-8

4. The Sine and the Tangent.—Two of the most important of the trigonometric functions are the ratio of the side opposite to the hypotenuse, and that of the side opposite to the side adjacent; that is, $\frac{a}{c}$ and $\frac{a}{b}$, Fig. 3. They are called, respectively, the sine of A and the tangent of A. The words sine and tangent are abbreviated to sin and tan, respectively, and the expressions sin A, tan A, are for brevity read sine A, tangent A, instead of sine of A, and tangent of A. We have, then.

$$\sin A = \frac{\text{side opposite}}{\text{hypotenuse}} = \frac{a}{c} \qquad (1)$$
$$\tan A = \frac{\text{side opposite}}{\text{side adjacent}} = \frac{a}{b} \qquad (2)$$

If these formulas are fixed in the mind, little difficulty will be experienced in remembering the others that will be given. It should be noticed that the side opposite is the numerator in both ratios. The occurrence of the letter *a* in both the words *adjacent* and *tangent* will help one to remember which of the two fractions represents the tangent and which the sine.



EXAMPLE 1.—In the right triangle A B C, Fig. 4, the lengths of the sides are shown; find the sine and the tangent of A.

SOLUTION.—In this case, the hypotenuse AB = 10; the side adjacent, AC = 8; side opposite, BC = 6. These values in formulas 1 and 2 give

$$\sin A = \frac{6}{10} = .6.$$
 Ans.
 $\tan A = \frac{6}{8} = .75.$ Ans.

EXAMPLE 2.—In the right triangle A B C, Fig. 5, the hypotenuse is 12 chains, and the side A C is 9 chains; find: (a) the sine and the tangent of A; (b) the sine and the tangent of B.

Solution.--(a) For the angle A, we have hypotenuse AB = 12side adjacent. AC = 9

side opposite,
$$BC = \sqrt{AB^{2} - AC^{2}} = \sqrt{12^{2} - 9^{2}} = 7.9372$$

Substituting in formulas 1 and 2,

$$\sin A = \frac{B}{A} \frac{C}{B} = \frac{7.9372}{12} = .66143. \text{ Ans.}$$
$$\tan A = \frac{B}{A} \frac{C}{C} = \frac{7.9372}{9} = .88191. \text{ Ans.}$$

(b) For angle B, we have

hypotenuse BA = 12side opposite, AC = 9side adjacent, BC = 7.9372

Therefore,

sin $B = \frac{AC}{AB} = \frac{9}{12} = .75$. Ans. tan $B = \frac{AC}{BC} = \frac{9}{7.9372} = 1.1339$. Ans.

EXAMPLES FOR PRACTICE

1. In a right triangle ABC (make a sketch of this triangle), A and B are the two acute angles; the hypotenuse = 40 feet; side opposite B = 15 feet; find: (a) sin A and tan A; (b) sin B and tan B. Ans. $\begin{cases} (a) \sin A = .92703, \tan A = 2.47207 \\ (b) \sin B = .37500, \tan B = .40452 \end{cases}$

2. From a point on one side of an angle M, a perpendicular is drawn on the other side; it is found that this perpendicular is 12.5 inches long, and that it meets the other side at a distance of 7.75 inches from the vertex; find the sine and the tangent of the angle M. (Make a sketch of this triangle.) Ans. $\begin{cases} \sin M = .84988 \\ \tan M = 1.61290 \end{cases}$

3. From a point on one side of an angle A distant 10 inches from the vertex, a perpendicular is drawn on the other side; the distance from the vertex to the foot of the perpendicular is 6 inches; find sin A and tan A. Ans. $\begin{cases} \sin A = .80000 \\ \tan A = 1.33333 \end{cases}$

4. The two acute angles of a right triangle are P and Q; the side opposite P is 150 feet, and that opposite Q is 225 feet; find: (a) sin P and tan P; (b) sin Q and tan Q.

Ans. $\begin{cases} (a) \sin P = .55469, \tan P = .66667 \\ (b) \sin Q = .83204, \tan Q = 1.50000 \end{cases}$

5. The Cosine and Cotangent.—The cosine and cotangent of an angle are, respectively, the sine and the tangent of the complement of the angle. The words cosine and cotangent are abbreviated to cos and cot, respectively, and the expressions cos A, cot A are read cosine A, cotangent A. Denoting any angle by A, its complement is $90^{\circ} - A$; therefore, according to the definitions just given,

$$\cos A = \sin (90^{\circ} - A)$$
 (1)
 $\cot A = \tan (90^{\circ} - A)$ (2)

Since the complement of $90^{\circ} - A$ is A, it also follows that

cos	(90°	_	A)	-	sin	\mathcal{A}	(3)
cot	(90°		A)	=	tan	A	(4)

With reference to the angle B, Fig. 3, BC is the side adjacent and AC the side opposite. Therefore, by formulas 1 and 2, Art. 4,

$$\sin B = \frac{b}{c}, \tan B = \frac{b}{a}$$

and therefore, since A is the complement of B,

$$\cos A = \sin B = \frac{b}{c}$$

 $\cot A = \tan B = \frac{b}{a}$

or, again referring to the angle A, which is the angle under consideration,

$\cos A =$	side adjacent	(5)	
cos 11 -	hypotenuse	(0)	
$\cot A =$	side adjacent	(6)	
	side opposite	(0)	

The student will, after some practice, become familiar with these formulas. Whenever he forgets them, he should refer to the definitions of the cosine and cotangent, which will at once enable him to write down the formulas, pro vided that he remembers those for the sine and the tangent.

6. The Secant and Cosecant.—The secant of an angle is the reciprocal of the cosine of the angle; that is, 1 divided by the cosine.

The word secant is abbreviated to sec. According to the definition, we have

$$\sec A = \frac{1}{\cos A} \tag{1}$$

It follows that

$$\cos A = \frac{1}{\sec A} \tag{2}$$

7. The cosecant of an angle is the secant of the complement of the angle. The abbreviations *cosec* and *csc* are used for *cosecant*. According to the definition, we have

$$\csc A = \sec \left(90^\circ - A\right) \tag{1}$$

Since A is the complement of $90^{\circ} - A$, we have also

$$\csc (90^\circ - A) = \sec A \qquad (2)$$

By means of formula 1, Art. 6, this relation may be written

$$\csc A = \sec (90^\circ - A) = \frac{1}{\cos (90^\circ - A)}$$

or, since $\cos (90^\circ - A) = \sin A$ (formula 3, Art. 5),

$$\csc A = \frac{1}{\sin A} \tag{3}$$

Therefore, the cosecant of an angle may also be defined as the reciprocal of the sine. Notice very particularly that

> secant = reciprocal of cosinecosecant = reciprocal of sine

From formula 3 above follows

$$\sin A = \frac{1}{\csc A} \tag{4}$$

8. Cofunctions and Complementary Functions. The functions cosine, cotangent, and cosecant are sometimes called cofunctions of the angle considered; while the sine, tangent, and secant are called fundamental functions. As has been explained, the cofunctions of an angle are the corresponding fundamental functions of the complement of the angle. Thus, the cosine of \mathcal{A} is the sine of $90^\circ - \mathcal{A}$; the cotangent of \mathcal{A} is the tangent of $90^\circ - \mathcal{A}$; etc.

A fundamental function and its corresponding cofunction are called complementary functions of each other. The sine, for example, is the complementary function of the cosine; and the cosine is the complementary function of the sine.

EXAMPLE 1.—Find: (a) the cosine of the angle A, Fig. 5; (b) the cotangent; (c) the secant; (d) the cosecant.

SOLUTION. -(a) The cosine of A is equal to the sine of B, or

$$\frac{A}{A}\frac{C}{B} = \frac{9}{12} = .75$$
. Ans.

(b) The cotangent of A is equal to the tangent of B, or (see example 2, Art. 4)

$$\frac{A C}{B C} = \frac{9}{7.9372} = 1.1339.$$
 Ans.

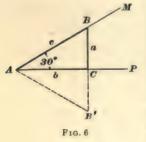
(c) The secant of A is 1 divided by $\cos A$, or

$$1 \div \frac{9}{12} = \frac{12}{9} = 1.33333$$
. Ans.

(d) The cosecant of A is 1 divided by sin A, or

$$1 \div \frac{BC}{AR} = \frac{AB}{RC} = \frac{12}{7.0279} = 1.51187$$
. An

EXAMPLE 2.—Find the functions of 30°.



SOLUTION.—Let the angle MAP, Fig. 6, be 30°. Draw BC perpendicular to AP, produce it to B', making CB' = CB, and draw AB'. The triangle BAB' thus formed is isosceles, and angle CAB'= CAB = 30°. Therefore, BAB' = 30°+ 30° = 60°. Also, angle B = 90° - 30°= 60°; and angle B' = angle B = 60°. As the three angles of ABB' are equal, the sides are also equal, and c = BB' = 2a. Now, the figure gives,

s.

$$b = \sqrt{c^2 - a^2} = \sqrt{(2a)^2 - a^2} = \sqrt{3a^2} = a\sqrt{3}$$

Bearing these values in mind, we have

$$\sin 30^{\circ} = \frac{a}{c} = \frac{a}{2a} = \frac{1}{2}. \text{ Ans.}$$
$$\tan 30^{\circ} = \frac{a}{b} = \frac{a}{a\sqrt{3}} = \frac{1}{\sqrt{3}} = \frac{\sqrt{3}}{3}. \text{ Ans.}$$
$$\cos 30^{\circ} = \frac{b}{c} = \frac{a\sqrt{3}}{2a} = \frac{\sqrt{3}}{2}. \text{ Ans.}$$

$$\cot 30^{\circ} = \frac{b}{a} = \frac{a\sqrt{3}}{a} = \sqrt{3}. \text{ Ans.}$$

$$\sec 30^{\circ} = \frac{1}{\cos 30^{\circ}} = 1 \div \frac{\sqrt{3}}{2} = \frac{2}{\sqrt{3}} = \frac{2}{3}\sqrt{3}. \text{ Ans.}$$

$$\csc 30^{\circ} = \frac{1}{\sin 20^{\circ}} = 1 \div \frac{1}{2} = 2. \text{ Ans.}$$

NOTE.-It is only in a few cases that the values of the trigonometric functions of an angle can be derived by elementary principles, as above. The general method for determining the functions of any angle is comparatively complicated, and is beyond the scope of this work. The trigonometric functions of any angle can be obtained from a table, as will be presently explained.

EXAMPLES FOR PRACTICE

1. The acute angles of a right triangle are B and C; the side opposite B is 1,200 feet; and that opposite C is 1,500 feet; find the fundamental functions of B, and from them the cofunctions of C.

Ans. { $\sin B = .62471$, $\tan B = .8$, $\sec B = 1.2806$ $\cos C = .62471$, $\cot C = .8$, $\csc C = 1.2806$

2. From example 2, Art. 8, derive the functions of
$$60^{\circ}$$

(= $90^{\circ} - 30^{\circ}$).
Ans.
$$\begin{cases} \sin 60^{\circ} = \frac{\sqrt{3}}{2}, \tan 60^{\circ} = \sqrt{3}, \cos 60^{\circ} = \frac{1}{2} \\ \cot 60^{\circ} = \frac{\sqrt{3}}{3}, \sec 60^{\circ} = 2, \csc 60^{\circ} = \frac{2}{3}\sqrt{3} \end{cases}$$

3. Given
$$\sin A = \frac{2}{3}$$
 and $\cos B = \frac{4}{5}$, find $\csc A$ and $\sec B$.
Ans. $\begin{cases} \csc A = 1.5 \\ \sec B = 1.25 \end{cases}$

4. Find the trigonometric functions of 45° . (Notice that here the side opposite is equal to the side adjacent. Denote the hypotenuse by c, and express the other two sides in terms of c.)

Ans. $\begin{cases} \sin 45^{\circ} = \cos 45^{\circ} = \frac{1}{2}\sqrt{2} \\ \tan 45^{\circ} = \cot 45^{\circ} = 1 \\ \sec 45^{\circ} = \csc 45^{\circ} = \sqrt{2} \end{cases}$

9. The Versed Sine and Coversed Sine.—The versed sine (vers) of an angle is 1 minus the cosine; and the coversed sine (covers) is 1 minus the sine.

vers
$$A = 1 - \cos A$$
 (1)
covers $A = 1 - \sin A$ (2)

These two functions are not much used, except in railroad work.

FIG. 7

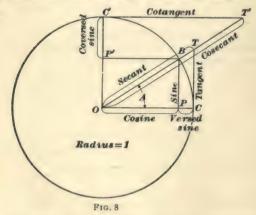
10. Summing Up. - The foregoing definitions are summed up in the table given below, which contains the expressions for the functions of the angle A. Fig. 7. in terms of the hypotenuse c_{i} the side opposite, a, and the side adjacent, b.

TA	B	L	E	I
----	---	---	---	---

Function	sin	tan	cos	cot	sec	csc	vers	covers
Value	a c	$\frac{a}{b}$	$\frac{b}{c}$	$\frac{b}{a}$	$\frac{c}{b}$	c a	$1 - \frac{b}{c}$	$1 - \frac{a}{c}$

The ratios $\frac{c}{b}$ and $\frac{c}{a}$ for the secant and cosecant are obtained from the formulas sec $A = 1 \div \cos A = 1 \div \frac{b}{c} = \frac{c}{b}$ $\csc A = 1 \div \sin A = 1 \div \frac{a}{c} = \frac{c}{a}.$

11. Representation of the Trigonometric Functions by Lines.—Let A, Fig. 8, be any angle. From its



vertex O, describe a circle of radius 1; or, otherwise, describe any circle and take its radius as unity. This circle intersects

the sides of the angle at B and C. Draw the tangent CT, meeting OB produced at T; the radius OC' perpendicular to OC; the lines BP and BP' perpendicular to OC and OC', respectively; and the tangent C'T', meeting OB produced at T'.

Since the angle A is measured by the arc CB, the trigonometric functions of the angle are said to be likewise the trigonometric functions of the arc. It is, for instance, immaterial whether we say that 1 is the tangent of an angle of 45° or of an arc of 45° .

In the figure constructed as just explained, the trigonometric functions of the angle A, or of the arc CB, may be represented by lines, as marked. For, in the right triangle OPB, in which BP, OP, and OB are, respectively, the side opposite, the side adjacent, and the hypotenuse, we have

$$\sin A = \frac{BP}{OB}, \cos A = \frac{OP}{OB}$$

or, since OB = 1,

 $\sin A = \frac{BP}{1} = BP, \cos A = \frac{OP}{1} = OP$

In the triangle OCT, in which CT and OC are, respectively, the side opposite and the side adjacent, and OT is the hypotenuse,

$$\tan A = \frac{CT}{OC} = \frac{CT}{1} = CT$$
$$\sec A = \frac{OT}{OC} = \frac{OT}{1} = OT$$

By the same reasoning, it can be shown that C'T' and OT' are, respectively, the tangent and the secant of the angle C'OT', or the cotangent and the cosecant of A, since C'OT' is the complement of A.

Let the student verify that, according to the definitions of the versed sine and coversed sine, these functions are represented by PC and P'C', respectively.

RELATIONS AMONG THE FUNCTIONS OF AN ANGLE

12. Method of Marking a Triangle.—The triangle A B C, Fig. 7, has the angles marked by the capital letters A, B, and C and the sides opposite these angles marked by the small letters a, b, and c, respectively. This method of marking a triangle is very useful and convenient, as it points out at once the relative position of the sides and the angles. In a right triangle, the right angle is usually designated by C. In the figures that follow, when only the angles are marked, the sides opposite are taken as marked by the small letters corresponding to the capital letters that mark the angles.

13. Relation Between Tangent and Cotangent. In Fig. 7,

$$\tan A = \frac{a}{b}, \cot A = \frac{b}{a}$$

Multiplying these equations together gives

 $\tan A \times \cot A = \frac{a}{b} \times \frac{b}{a} = 1$ $\cot A = \frac{1}{\tan A}$ $\tan A = \frac{1}{\cot A}$

whence,

That is, the tangent and cotangent are each the reciprocal of the other. This is a very important relation, and should be committed to memory, together with those given in the two articles following.

14. Tangent and Cotangent in Terms of Sine and Cosine.—In Fig. 7,

$$\sin A = \frac{a}{c}, \cos A = \frac{b}{c}$$

Dividing these equations member by member gives

$$\frac{\sin A}{\cos A} = \frac{a}{c} \div \frac{b}{c} = \frac{a}{b}$$

that is, since $\frac{a}{b} = \tan A$,

$$\tan A = \frac{\sin A}{\cos A} \tag{1}$$

Also, because the cotangent is the reciprocal of the tangent.

$$\cot A = \frac{\cos A}{\sin A}$$
(2)

15. Relations Between the Squares of Certain Functions.—A power of a trigonometric function is indicated by writing the exponent immediately after the abbreviation used for the function. Thus, the square of the sine of A, or of sin A, is written sin^{*} A, and read sine square A. Similarly, the cube of tan A is written tan' A, and read tangent cube A, etc.

In the right triangle ABC, Fig. 7, we have

sin

$$a^{\circ}+b^{\circ}=c^{\circ}$$

Dividing both members of this equality by c^{*} gives

$$\frac{a^2}{c^3} + \frac{b^3}{c_2} = 1$$

$$A + \cos^2 A = 1 \qquad (1)$$

Again, dividing both members of the equation $c^2 = a^2 + b^2$ by b",

 $\sec^{*} A = 1 + \tan^{*} A$

$$\frac{c^{*}}{b^{*}} = \frac{a^{*}}{b^{*}} + 1 = 1 + \frac{a^{*}}{b^{*}}$$

that is.

Similarly, if both members of the equation $c^* = a^* + b^*$ are divided by a^{*}.

(2)

 $a^{3} = 1 + \frac{1}{a^{3}}$ $\csc^{\circ} A = 1 + \cot^{\circ} A \qquad (3)$

that is.

16. To Express Any Function in Terms of Any Other Function.-In the triangle ABC, Fig. 7, we have $a^{*} + b^{*} = c^{*}$ (1)

Dividing both members of this equation by c³ gives

$$\frac{a^{*}}{c^{*}} + \frac{b^{*}}{c^{*}} = 1 \qquad (2)$$

From these two equations, any of the six ratios $\frac{a}{b}$, $\frac{a}{c}$, $\frac{b}{a}$, $\frac{b}{c}$, $\frac{b}{a}$, $\frac{b}{a}$, $\frac{b}{c}$, $\frac{b}{a}$, $\frac{b}{$

$$c^3 - 1 + b^3$$

 $\frac{c}{a}$, $\frac{c}{b}$ can be found when one of them is given. If, for instance, $\frac{a}{c}$ is given, $\frac{c}{a}$ is obtained by dividing 1 by $\frac{a}{c}$; $\frac{b}{c}$, by solving equation (2) for $\frac{b^*}{c^*}$ and taking the square root; $\frac{c}{b}$, by taking the reciprocal of the value just found for $\frac{b}{c}$. To find $\frac{a}{b}$, divide both members of equation (1) by b^* , which gives

$$\frac{a^*}{b^*}+1=\frac{c^*}{b^*}$$

whence, multiplying through by $\frac{b^2}{c^3}$,

$$\frac{b^{\mathfrak{s}}}{c^{\mathfrak{s}}}\left(\frac{a^{\mathfrak{s}}}{b^{\mathfrak{s}}}+1\right) = \frac{c^{\mathfrak{s}}}{b^{\mathfrak{s}}} \times \frac{b^{\mathfrak{s}}}{c^{\mathfrak{s}}} = 1$$

and hence, dividing through by $\frac{a^*}{b^*} + 1$,

$$\frac{b^*}{c^*} = \frac{1}{\frac{a^*}{b^*} + 1}$$

Substituting this value of $\frac{b^*}{c^*}$ in equation (2) and solving for $\frac{a}{b}$, the latter ratio is obtained in terms of $\frac{a}{c}$.

Table II gives the relation between any two functions of any angle A.

	csc A	$\frac{1}{\csc A}$	$\sqrt{\csc^2 A - 1}$ $\csc A$	$\frac{1}{\sqrt{\csc^3 A - 1}}$	$\sqrt{\csc^3 A - 1}$	$\csc A$ $\sqrt{\csc^3 A - 1}$	csc A
ANGLE	sec A	$\frac{\operatorname{vsec}^{2} A - 1}{\operatorname{sec} A}$	$\frac{1}{\sec A}$	$\sqrt{\sec^2 A - 1}$	$\frac{1}{\sqrt{\sec^* A - 1}}$	sec A	$\frac{\sec A}{\sqrt{\sec^3 A - 1}}$
TO SVIDIO	cot A	$\frac{1}{\sqrt{1 + \cot^3 A}}$	$\frac{\cot A}{\sqrt{1 + \cot^3 A}}$	$\frac{1}{\cot A}$	cot A	$\frac{\sqrt{1 + \cot^3 A}}{\cot A}$	$\sqrt{1 + \cot^3 A}$
RELATIONS BELWEEN THE FUNCTIONS OF AN ANGLE	$\tan A$	$\frac{\tan A}{\sqrt{1+\tan^3 A}}$	$\frac{1}{\sqrt{1+\tan^3 A}}$	$\tan A$	$\frac{1}{\tan A}$	$\sqrt{1 + \tan^{*} A}$	$\frac{\sqrt{1 + \tan^* A}}{\tan A}$
	cos A	$\sqrt{1-\cos^{3}A}$	$\cos A$	$\frac{\sqrt{1-\cos^{3}A}}{\cos A}$	$\frac{\cos A}{\sqrt{1-\cos^{2} A}}$	$\frac{1}{\cos A}$	$\frac{1}{\sqrt{1-\cos^3 A}}$
	sin A	$\sin A$	$\sqrt{1-\sin^{2}A}$	$\frac{\sin A}{\sqrt{1-\sin^2 A}}$	$\frac{\sqrt{1-\sin^3 A}}{\sin A}$	$\frac{1}{\sqrt{1-\sin^*A}}$	$\frac{1}{\sin .4}$
	In Terms of	= A =	$\cos A =$	$\tan A =$	$\cot A =$	sec A =	$\csc A =$

TABLE II RELATIONS BETWEEN THE FUNCTIONS OF AN ANGLE PLANE TRIGONOMETRY, PART 1

TRIGONOMETRIC TABLES

TABLES OF NATURAL FUNCTIONS

17. To facilitate calculations, tables of the trigonometric functions are used. The tables give values for the sines, cosines, tangents, and cotangents of angles from 0° to 90° . The values of the secant and cosecant are not generally given in tables; they are obtained by dividing 1 by the cosine and the sine, respectively, according to formula 1, Art. 6, and formula 3, Art. 7.

There are two kinds of trigonometric tables; namely, the table of *natural functions* and the table of *logarithmic functions*. The table of natural functions gives the actual values of the functions, while the table of logarithmic functions gives the logarithms of the functions. It may be remarked that, except in making a table, the values of the functions are never calculated directly because the process is so long and laborious that it would require considerable time to calculate even the value of one function of an angle; nor is there a simple method of calculating the angle corresponding to a given function.

NOTE.—In all that follows, the number of seconds by which an angle exceeds a whole number of degrees and minutes will be referred to as the odd seconds, or the number of odd seconds, or simply the number of seconds in the angle; while the expression total number of seconds will be applied to the number obtained by reducing the degrees and minutes to seconds, and adding the odd seconds. Thus, the odd seconds, or, for shortness, the seconds in 34° 36' 16'' are 16; while the total number of seconds is the number of seconds in 34° , 36' 16'' are 16; while the total number of seconds is the number of seconds in 34° , 16'' are 16; while the total number of seconds in 36', plus 16; that is, $34 \times 60 \times 60 + (36 \times 60) + 16 = 124,576$. A similar notation will be used with regard to minutes. The explanations that follow refer to the Trigonometric Tables used with this Course.

18. To Find the Natural Functions of an Angle Less Than 45° and Containing No Odd Seconds.—The required function is found in the double column marked at the top with the given number of degrees, in the subdivision of that column headed by the name of the given function, and horizontally opposite the number in the left-hand column (marked ') that expresses the number of odd minutes in the angle. When the function considered is a sine or a cosine, it is taken from the table headed Natural Sines and Cosines; when a tangent or cotangent, from the table headed Natural Tangents and Cotangents.

EXAMPLE.—Find the natural functions of an angle of 37° 23'.

SOLUTION.—On page 30 of the table headed Natural Sines and Cosines, the double column headed 37° is found. Looking in the lefthand minute column for 23 (number of odd minutes in the given angle), and glancing along the horizontal row to the right of 23, the number .60714 is found in the single column marked Sine under 37°; and the number .79459 is found in the column marked Cosine. Therefore,

$$\sin 37^{\circ} 23' = .60714$$
. Ans.

The tangent and cotangent are taken in a similar manner from the table headed Natural Tangents and Cotangents, page 39. The results are: $\tan 37^{\circ} 23' = .76410$. Ans.

cot 37° 23' = 1.30873. Ans.

EXAMPLES FOR PRACTICE

Verify the following values:

(a) $\sin 39^{\circ} 55' = .64167$; $\cos 39^{\circ} 55' = .76698$; $\tan 39^{\circ} 55' = .83662$; $\cot 39^{\circ} 55' = 1.19528$.

(b) $\tan 16^{\circ} 32' = .29685$; $\cos 16^{\circ} 32' = .95865$; $\sec 16^{\circ} 32' = 1.04313$; $\csc 16^{\circ} 32' = 3.51407$.

(c) $\cot 43^{\circ} 2' = 1.07112$; $\csc 43^{\circ} 2' = 1.46537$; $\tan 43^{\circ} 2' = .93360$; $\cos 43^{\circ} 2' = .73096$.

19. To Find the Natural Functions of an Angle Greater Than 45° and Containing No Odd Seconds. The required function is found in the double column marked at the bottom with the given number of degrees, in the subdivision of that column having at the bottom the name of the given function, and horizontally opposite the number in the right-hand column (marked ') that expresses the odd minutes in the angle. It will be observed that the number of degrees at the bottom of the pages decrease as the pages increase,

and that the number of minutes in the right-hand column increase from bottom to top.

EXAMPLE.—Find the functions of 53° 43'.

SOLUTION.—The double column marked 53° at the bottom is found on page 30 of Natural Sines and Cosines. Looking along the horizontal row determined by the number 43 in the right-hand minute column, the number .80610 is found in the single column marked Sine at the bottom, and the number .59178 in the single column marked Cosine at the bottom, these two columns forming the double column marked 53° at the bottom. Therefore,

> $\sin 53^{\circ} 43' = .80610$. Ans. $\cos 53^{\circ} 43' = .59178$. Ans.

The tangent and cotangent are similarly taken from page 39 of Natural Tangents and Cotangents. The results are:

 $\tan 53^{\circ} 43' = 1.36217$. Ans. $\cot 53^{\circ} 43' = .73413$. Ans.

EXAMPLES FOR PRACTICE

Verify the following values:

(a) $\sin 67^{\circ} 45' = .92554$; $\cos 67^{\circ} 45' = .37865$; $\tan 67^{\circ} 45' = 2.44433$; $\cot 67^{\circ} 45' = .40911$.

(b) $\cot 74^{\circ} 3' = .28580$; $\csc 74^{\circ} 3' = 1.04004$; $\sin 74^{\circ} 3' = .96150$.

(c) $\cos 48^\circ 9' = .66718$; $\cot 48^\circ 9' = .89567$; $\csc 48^\circ 9' = 1.34248$.

20. To Find the Natural Functions of an Angle Containing Odd Seconds.—The method of solving this problem by means of the table is founded on the following principle, which applies within the limits of approximation with which the table is constructed:

If several angles are taken within an interval not greater than 1'; that is, so that the difference between the greatest and the smallest shall not exceed 1', the ratio of the difference between any two of these angles to the difference between any other two is the same as the ratio obtained by dividing the difference between the values of any trigonometric function for the first pair of angles, by the difference between the values of the same function for the second pair of angles. For instance, if the angles $43^{\circ} 46' 32''$, $43^{\circ} 46' 34''$, $43^{\circ} 46' 40''$, and $43^{\circ} 47'$ are taken between $43^{\circ} 46'$ and $43^{\circ} 47'$, then

 $\frac{43^{\circ} 47' - 43^{\circ} 46' 40''}{43^{\circ} 46' 34'' - 43^{\circ} 46' 32''} = \frac{\sin 43^{\circ} 47' - \sin 43^{\circ} 46' 40''}{\sin 43^{\circ} 46' 34'' - \sin 43^{\circ} 46' 32''}$ In general, if *A*, *B*, *C*, *D* are any angles within an interval of 1', then

$$\frac{A-B}{C-D} = \frac{\sin A - \sin B}{\sin C - \sin D} = \frac{\cos A - \cos B}{\cos C - \cos D}$$
$$= \frac{\tan A - \tan B}{\tan C - \tan D} = \frac{\cot A - \cot B}{\cot C - \cot D}$$

Similarly,

or.

 $\frac{A-B}{B-C} = \frac{\sin A - \sin B}{\sin B - \sin C} = \frac{\cos A - \cos B}{\cos B - \cos C}, \text{ etc.}$

Let A be the number of degrees and minutes in any angle, and s the number of odd seconds. Then the angle, which will be represented by A + s'', lies between A and A + 1'or between A and A + 60''. For instance, if the angle is $25^{\circ} 15' 37''$, it lies between $25^{\circ} 15'$, which is represented by A, and $25^{\circ} 16'$, which is $25^{\circ} 15' + 1'$, or A + 1', or A + 60''. In this case s represents 37''. From the principle stated above we have,

$$\frac{(A+60'') - A}{(A+s'') - A} = \frac{\sin(A+60'') - \sin A}{\sin(A+s'') - \sin A}$$
$$\frac{60}{s} = \frac{\sin(A+1') - \sin A}{\sin(A+s'') - \sin A}$$

whence, solving this equation for $\sin (A + s'')$,

 $\sin (A + s'') = \sin A + [\sin (A + 1') - \sin A] \frac{s}{60}$ (1) Similarly,

 $\tan (A + s'') = \tan A + [\tan (A + 1') - \tan A] \frac{s}{60}$ (2) For the cosine, we have

$$\cos (A + s'') = \cos A + [\cos (A + 1') - \cos A] \frac{s}{60}$$

but, since the cosine of an angle decreases as the angle increases, $\cos A$ is greater than $\cos (A + 1')$, and therefore it is better to write the formula thus,

$$\cos (A + s'') = \cos A - [\cos A - \cos (A + 1')] \frac{s}{60}$$
(3)
Similarly,

$$\cot (A + s'') = \cot A - [\cot A - \cot (A + 1')] \frac{s}{60}$$
(4)

The functions of A and A + 1' can be readily taken from the table, as explained in the preceding articles, and from them the functions of A + s'' are determined by the formulas just given, or by the following rule, which states in words what the formulas express in symbols:

Rule.—Find, in the table, the sine, cosine, tangent, or cotangent corresponding to the degrees and minutes in the angle.

For the seconds, find the difference between this value and the value of the sine, cosine, tangent, or cotangent of an angle 1 minute greater; multiply this difference by a fraction whose numerator is the number of seconds in the given angle and whose denominator is 60.

If the sine or tangent is sought, add this correction to the value first found; if the cosine or cotangent is sought, subtract the correction.

EXAMPLE.—Find: (a) the sine of $56^{\circ} 43' 17''$; (b) the cosine; (c) the tangent; and (d) the cotangent.

Solution. -(a) Here $A = 56^{\circ} 43'$, s = 17, $A + 1' = 56^{\circ} 44'$. $\sin (A + 1') = \sin 56^{\circ} 44' = .83613$ $\sin A = \sin 56^{\circ} 43' = .83597$ Difference = .00016 $\times \frac{17}{60}$.00005. nearly Adding this product to $\sin A$, we have $\sin 56^{\circ} 43' 17'' = .83597 + .00005 = .83602.$ Ans. $\cos A = \cos 56^{\circ} 43' = .54878$ (8) $\cos{(A + 1')} = \cos{56^{\circ}} 44' = .54854$ Difference = .00024 $\times \frac{17}{60}$.00007. nearly Subtracting this product from $\cos A$, we have $\cos 56^{\circ} 43' 17'' = .54878 - .00007 = .54871$. Ans. $\tan (A + 1') = \tan 56^{\circ} 44' = 1.52429$ (c) $\tan A = \tan 56^{\circ} 43' = 1.52332$ Difference = .00097 $\times \frac{17}{60}$.00027, nearly .

Adding this product to $\tan A$, we have

tan 56° 43' 17" = 1.52332 + .00027 = 1.52359. Ans. (d) $\cot A = \cot 56^{\circ} 43' = .65646$ $\cot (A + 1') = \cot 56^{\circ} 44' = .65604$ Difference = .00042 $\times \frac{17}{60}$

.00012, nearly

Subtracting this product from $\cot A$, we have $\cot 56^{\circ} 43' 17'' = .65646 - .00012 = .65634$. Ans.

EXAMPLES FOR PRACTICE

Verify the following values:

(a) $\sin 18^{\circ} 54' 45'' = .32412$; $\tan 18^{\circ} 54' 45'' = .34262$. (b) $\cos 34^{\circ} 17' 18'' = .82621$; $\cot 34^{\circ} 17' 18'' = 1.46659$. (c) $\sin 72^{\circ} 26' 20'' = .95340$; $\cot 72^{\circ} 26' 20'' = .31647$. (d) $\cos 65^{\circ} 6' 9'' = .42100$; $\tan 65^{\circ} 6' 9'' = 2.15457$. (e) $\sin 80^{\circ} 0' 3'' = .98481$; $\cot 80^{\circ} 0' 3'' = .17631$. (f) $\tan 14^{\circ} 14' 14'' = .25373$; $\cos 14^{\circ} 14' 14'' = .96928$.

21. To Find the Angle Corresponding to a Given Function, When the Function Is in the Table.—This case does not present any difficulty. Having found the given function in the table, the degrees in the angle are taken from the top or the bottom, and the minutes from the left- or the right-hand column, according as the name of the function is at the top or at the bottom of the page.

EXAMPLE 1.- The sine of an angle is .47486; what is the angle?

SOLUTION.—Glancing down the columns marked Sine in the table of Natural Sines and Cosines, .47486 is found (on page 28) in the column headed 28° . The number of minutes, 21, is found in the lefthand minute column, horizontally opposite .47486. Therefore, .47486 = sin $28^{\circ} 21'$. Ans.

EXAMPLE 2. -- Find the angle whose cosine is .27032.

SOLUTION.—Looking in the columns marked Cosine at the top of the page, the given cosine is not found; hence, the angle is greater than 45°. Consequently, looking in the columns marked Cosine at the bottom of the page, .27032 is found (on page 26) in the double column marked 74° at the bottom, and in the horizontal row beginning with 19 in the right-hand minute column. Therefore, the angle whose cosine is .27032 is 74° 19'; or, .27032 = cos 74° 19'. Ans.

EXAMPLE 3.—Find the angle whose tangent is 2.15925.

SOLUTION.—On searching the table of Natural Tangents, the given tangent is found to belong to an angle greater than 45° , so that it must be looked for in the column marked Tangent at the bottom. It is found in the column having 65° at the bottom and opposite 9' in the right-hand minute column. Therefore, $2.15925 = \tan 65^{\circ} 9'$. Ans.

EXAMPLE 4.—Find the angle whose cotangent is .43412.

SOLUTION.—From the table of Natural Cotangents, it is found that this value is less than the cotangent of 45° , so it must be found in the column marked Cotangent at the bottom. Looking there, it is found in the column having 66° at the bottom, and opposite 32', in the righthand column of minutes. Therefore, the angle whose cotangent is .43412 is $66^{\circ} 32'$, or .43412 = cot $66^{\circ} 32'$. Ans.

EXAMPLES FOR PRACTICE

1.	Find the angle whose sine is .47486.	Ans. 28° 21′
2.	Find the angle whose cosine is .74353.	Ans. 41° 58'
3.	Find the angle whose tangent is 2.06247.	Ans. 64° 8'
4.	Find the angle whose cotangent is 1.20665.	Ans. 39° 39'
5.	Find the angle whose sine is .76903.	Ans. 50° 16'
6.	Find the angle whose tangent is 9.93101.	Ans. 84° 15'

22. To Find the Angle Corresponding to a Given Function. When the Function Is Not in the Table. Since the table includes the functions of all angles containing no odd seconds, a function not found in the table must correspond to an angle having odd seconds. Let the odd seconds that are to be determined be denoted by s, and the degrees and minutes by A, as in Art. 20. Now, two consecutive functions including the given function can always be found in the table; that is, two consecutive functions of which one is greater and the other less than the given function. The required angle must, therefore, lie between the two angles corresponding to these two consecutive functions, and its number of degrees and minutes, A, is the number of degrees and minutes in the smaller of the two angles. The larger angle is A + 1', or A + 60'', while the required angle is A + s''. Having determined A, it only remains to determine the number of odd seconds, or s. This is done by means of the following formulas, obtained by solving for s the formulas found in Art. 20.

If the given function is a sine or tangent,

$$s = \frac{\sin (A + s'') - \sin A}{\sin (A + 1') - \sin A} \times 60$$
(1)

$$s = \frac{\tan (A + s') - \tan A}{\tan (A + 1') - \tan A} \times 60$$
 (2)

If the given function is a cosine or cotangent,

$$s = \frac{\cos A - \cos \left(A + s''\right)}{\cos A - \cos \left(A + 1'\right)} \times 60$$
(3)
$$s = \frac{\cot A - \cot \left(A + s''\right)}{\cot A - \cot \left(A + 1'\right)} \times 60$$
(4)

Observe that, although A + s'' is not known, its sine, cosine, etc., as the case may be, is known, or given. Thus, if the problem is to find the angle whose cotangent is .97888, we have cot (A + s'') = .97888.

The foregoing formulas lead to the following general rule for finding the angle corresponding to a given function:

Rule.—Find the difference of the two numbers in the table between which the given function lies, and use that difference as the denominator of a fraction.

Find the difference between the function belonging to the smaller angle and the given function, and use that difference as the numerator of the fraction mentioned above. Multiply this fraction by 60. The result will be the number of seconds to be added to the smaller angle in order to obtain the required angle.

EXAMPLE 1.—Find the angle whose sine is .57698.

SOLUTION.—Looking in the table of Natural Sines, in the columns marked Sine, it is found that the given sine lies between .57691 (= sin 35° 14') and .57715(= sin 35° 15'). The difference between them is .57715 - .57691 = .00024. The difference between the sine of the smaller angle, or .57691, and the given sine, or .57698, is .57698 - .57691 = .00007. Then, $\frac{.00007}{.00024} \times 60 = \frac{7}{24} \times 60 = 18''$, nearly, and the required angle is 35° 14' 18''; or, .57698 = sin 35° 14' 18''. Ans.

NOTE. - In practice, only the significant figures of the differences forming the terms of the function are used, the decimal point being dispensed with. Thus, .57715 -.57691 = 24, it being understood that this means 24 units of the fifth decimal order, or .00024.

EXAMPLE 2.—Find the angle whose cosine is .27052.

SOLUTION.—Looking in the table of Cosines, the given cosine is found to belong to a greater angle than 45° and therefore it must be looked for in the columns marked Cosine at the bottom of the page. It is found between the numbers $.27060(=\cos 74^{\circ} 18')$ and $.27032(=\cos 74^{\circ} 19')$. The difference between the two numbers is .27060 - .27032 = 28 units of the fifth order. The cosine of the smaller angle, or $74^{\circ} 18'$, is .27060, and the difference between this and the given cosine is .27060 - .27052= 8 units of the fifth order. Hence, $\frac{8}{28} \times 60 = 17''$; and, therefore, $.27052 = \cos 74^{\circ} 18' 17''$. Ans.

EXAMPLE 3.-Find the angle whose tangent is 2.15841.

SOLUTION.— 2.15841 falls between 2.15760 (= tan 65° 08') and 2.15925 (= tan 65° 9'). The difference between these numbers is 2.15925 – 2.15760 = 165 units of the fifth order; 2.15841 – 2.15760 = 81 units of the fifth order. Hence, $\frac{81}{160} \times 60 = 30''$, nearly, and therefore 2.15841 = tan 65° 8' 30''. Ans.

EXAMPLE 4.—Find the angle whose cotangent is 1.26342.

SOLUTION.— 1.26342 falls between $1.26395 (= \cot 38^{\circ} 21')$ and 1.26319 (= $\cot 38^{\circ} 22'$). The difference between these numbers is 1.26395 - 1.26319 = .00076. Also, 1.26395 - 1.26342 = .00053. $\frac{53}{76} \times 60 = 42''$, and therefore 1.26342 = $\cot 38^{\circ} 21' 42''$. Ans.

EXAMPLES FOR PRACTICE

1. 1	Find: (a)	the sine of	48° 17'; (b)	the cosine;	(c) the t	angent	
					Ans.	(a) .74 (b) .66 (c) 1.12	644 545 2172
2. 1	Find: (a)	the sine of	13° 11′ 6″;	(b) the cosin	he; (c) th Ans.		
3. 1	Find: (a)	the sine of	72° 0′ 2″; (b) the cosin	e; (c) the Ans. $\begin{cases} c \\ c $	1 00	
4. the cos		nat angle is	.26489 the	sine? (b) (A	Of what ans. $\begin{cases} (a) \\ (b) \end{cases}$		
	. ,	0	.688 the sin is it the ta	e? (b) Of v angent?	what ang $\begin{pmatrix} (a) \\ (b) \\ (c) \end{pmatrix}$		

TABLE OF LOGARITHMIC FUNCTIONS

23. The student is already familiar with the use of the table of logarithms of numbers. As stated in Art. 17, a table of logarithmic functions is a table containing the logarithms of the natural functions, these logarithms being, for convenience, called logarithmic functions. Thus, the logarithm of the sine of an angle is referred to as the logarithmic sine of the angle.

The connection between the tables can be seen from the following:

From table of natural functions, $\cot 44^{\circ} \dots = 1.03553$ From table of logarithms, $\log 1.03553 \dots = .01516$ From table of logarithmic functions, $\log \cot 44^{\circ} = .01516$

Few tables give the logarithmic secants and cosecants. These logarithmic functions may be obtained from the relations.

$$\sec A = \frac{1}{\cos A}, \csc A = \frac{1}{\sin A}$$

which give,

 $\log \sec A = -\log \cos A, \log \csc A = -\log \sin A$

That is, instead of adding the logarithmic secant or cosecant, the logarithmic cosine or sine, respectively, may be subtracted. Likewise, instead of subtracting the logarithmic secant, the logarithmic cosine may be added, and instead of subtracting the logarithmic cosecant, the logarithmic sine may be added.

24. Description of the Table.—The table of logarithmic functions contains for every minute the logarithms, to five decimal places, of the trigonometric sines, cosines, tangents, and cotangents of angles from 0° to 90° . From 0° to 45° , the degrees are placed at the top of the page and the minutes in the column headed ' on the left. From 45° to 90° , the degrees are at the bottom of the page, the minutes in the last whole column at the right, and the name of the trigonometric function is placed at the bottom of the column.

This arrangement is similar to that in the table of natural functions. It will be observed that the numbers of degrees at the top of the pages increase in the order of the pages from 0° to 44° , while those at the bottom decrease from 89° to 44° .

The general description of the table will be better understood by referring to one of its pages. Take, for instance, the page marked 11° at the top and 78° at the bottom. The first column on the left (marked ') contains the natural numbers from 1 to 60. These numbers represent minutes. Horizontally opposite to these numbers, and in the columns marked at the top log sin, log tan, etc., are printed the logarithmic functions, each function being in the same horizontal line as the number of minutes by which the corresponding angle exceeds 11°. Thus, the logarithmic tangent of 11° 39', which is 1.31425, is found in the column marked log tan at the top, and in the same horizontal line as the number 39 in the left-hand column. Similarly, the number $\overline{1.99072}$, being in the column marked at the top log cos. and in the same horizontal line as 48 in the left-hand column, is the logarithmic cosine of 11° 48'. In some tables, several mantissas are printed under and to the right of the same characteristic, and are understood to belong with that characteristic. Thus, in the logarithm just considered, only the mantissa .99072 is printed, the characteristic being the same as the first one found above that mantissa.

The last column but one (marked ' at the bottom) contains the natural numbers from 1 to 60, increasing from bottom to top. It will be observed that any angle determined by the number of degrees at the bottom (78 in this case) and any number of minutes in the right-hand minute column, is the complement of the angle determined by the number of degrees at the top (11 in this case) and the number of minutes in the left-hand minute column, horizontally opposite the number of minutes in the right-hand minute column. Thus, the number 18 in the right-hand minute column is horizontally opposite the number 42 in the left-hand column, and we have, $78^{\circ} 18' + 11^{\circ} 42' = 90^{\circ}$. Therefore,

since the fundamental functions of an angle are equal to the cofunctions of its complement,

sin 11° 42′ = cos 78° 18′ cot 11° 42′ = tan 78° 18′, etc. and log sin 11° 42′ = log cos 78° 18′, etc.

For this reason, the notation log tan is written at the bottom of the column headed log cot, to indicate that the logarithms in this column are the logarithmic tangents of angles whose number of degrees is the number (78 in this case) at the bottom of the page, and whose number of minutes is opposite those logarithms in the right-hand minute column. Similarly, the columns marked log sin, log tan, and log cos at the top are marked, respectively, log cos, log cot, and log sin at the bottom.

25. After the column marked log sin there is a column marked d. This column contains the differences, expressed in units of the fifth decimal order, between the consecutive logarithmic sines given in the sine column. Thus, referring to the page headed 11°, the first number in the d-column following the sine column is 65; it will be observed that this number is opposite the space between the logarithmic sines 1.28125 and 1.28060, and is the difference, in units of the fifth decimal order, or expressed in hundred thousandths, between these two logarithmic sines. These differences are called tabular differences. Similar differences are printed in the column marked d after the cosine column, and in the column marked c. d. between the tangent and the cotangent column. The notation c. d. means common difference, as the differences between the successive logarithmic tangents are the same as those between the corresponding cotangents. although obtained by reversing the order in which the functions are subtracted; that is to say, log tan $A - \log \tan B$ $= \log \cot B - \log \cot A.$

The tabular differences for the cosines are not given in the first ten pages, both for want of space and because they are so small that they can be readily determined by mental subtraction.

The use of the tabular differences, the use and contents of the column marked p. p. in all pages but the first three, and the peculiarities and applications of these first three pages of the table will be explained further on.

26. To Find the Logarithmic Functions of an Angle Having No Odd Seconds.

Rule.—For an angle less than 45° , look for the degrees at the top of the page and for the minutes in the column (marked') at the left of the page on which the number of degrees is found. Then look across the page along the horizontal row containing the given number of minutes, into the column headed by the name of the function whose logarithm is required. The desired logarithm is found in this row and column.

For an angle between 45° and 90° , find the degrees at the bottom of the page and the minutes in the column (marked ') at the right of the page. Then look across the page, along the horizontal row containing the given number of minutes, into the column marked at the bottom with the name of the function whose logarithm is to be found. The row and column thus determined contain the desired logarithm.

EXAMPLE 1.—Find the logarithmic sine and the logarithmic tangent of 15° 24'.

SOLUTION.—On the page marked 15° at the top, in the column headed log sin, and in the same horizontal row with 24, the number $\overline{1.42416}$ is found; and in the column headed log tan, the number $\overline{1.44004}$ is found. Hence,

> log sin 15° $24' = \overline{1.42416}$. Ans. log tan 15° $24' = \overline{1.44004}$. Ans.

EXAMPLE 2.-Find the logarithmic tangent and cosine of 73° 10'.

SOLUTION.—As 73 is greater than 45, it is found at the bottom of the page. Looking for the number of minutes (10') in the right-hand minute column, and following the horizontal row determined by this number into the column marked log tan at the bottom, the number .51920 is found. Likewise, the number $\overline{1}.46178$ is found in the column marked log cos at the bottom, and horizontally opposite the number 10 in the right-hand minute column. Therefore,

> log tan 73° 10' = .51920. Ans. log cos 73° 10' = $\overline{1}.46178$. Ans.

EXAMPLES FOR PRACTICE

1. Find: (a) the logarithmic cosine of 36° 58'; (b) the logarithmic tangent. Ans. $\begin{cases} (a) \ \overline{1}.90254 \\ (b) \ \overline{1}.87659 \end{cases}$

2. Find: (a) the logarithmic tangent of $23^{\circ}39'$; (b) the logarithmic cotangent. Ans. $\begin{cases} (a) \ \overline{1.64140} \\ (b) \ .35860 \end{cases}$

3. Find: (a) the logarithmic sine of 79° 45'; (b) the logarithmic cosine. Ans. $\begin{cases} (a) & \overline{1.99301} \\ (b) & \overline{1.25028} \end{cases}$

4. Find: (a) the logarithmic tangent of $46^{\circ}59'$; (b) the logarithmic cotangent. Ans. $\begin{cases} (a) & .03009\\ (b) & 1.96991 \end{cases}$

27. To Find the Logarithmic Functions of an Angle Containing an Odd Number of Seconds.-Let the number of degrees and minutes in an angle any of whose logarithmic functions is required be denoted by A. and the number of odd seconds by s. Thus, if the angle is 37° 43' 19". A will equal 37° 43', and s will equal 19": also, A + 1', or A + 60'', will equal $37^{\circ} 43' + 1'$, or $37^{\circ} 44'$. (See Art. 20.) Since the table gives the logarithmic functions of any angle containing no odd seconds, the logarithmic functions of A and A + 1' may be readily found. as explained in the last article. Let these logarithmic functions be denoted by l and l', respectively, and the required logarithmic function by L. In the general theory of logarithms, treated in advanced works on mathematics, it is shown that if two consecutive angles (as 37° 43' and 37° 44') are taken from the table, the difference between any logarithmic function of the greater and the same logarithmic function of the smaller angle is to the difference between the same logarithmic function of any intermediate angle (as 37° 43' 19") and the same function of the smaller angle, as the difference between the greater and the smaller angle is to the difference between the intermediate and the smaller angle. If the notation F(A), read function of A, is employed to denote any logarithmic function of an angle A, we have. writing $A + 60^{\prime\prime}$ instead of $A + 1^{\prime}$,

 $\frac{F(A + 60'') - F(A)}{F(A + s) - F(A)} = \frac{(A + 60'') - A}{(A + s) - A} = \frac{60}{s}$ that is, whence, $\frac{l' - l}{L - l} = \frac{60}{s}$ whence, $L - l = (l' - l)\frac{s}{60}$ and $L = l + (l' - l)\frac{s}{60}$

The difference between l' and l, being the difference between two consecutive logarithmic functions, may be taken from the column of tabular differences in the table. (See Art. 25.) Denoting the tabular difference l' - l by D, the preceding equation becomes

$$L = l + D \times \frac{s}{60}$$

It should be observed that, since the sine and the tangent increase with the angle, while the cosine and cotangent decrease as the angle increases, l' - l is positive or negative according as the functions considered are fundamental functions (sine, tangent) or cofunctions (cosine, cotangent). In the latter case, D in the formula should be treated as negative; that is, the product $D \times \frac{s}{60}$ should be subtracted from l

It should also be borne in mind that the tabular difference D is expressed in units of the fifth order of decimals, or hundred thousandths. Thus, if the number of seconds s is 15, and the tabular difference is 36, the quantity to be added to l is $.00036 \times \frac{16}{60} = .00009$.

If $l = \overline{1.59812}$, the work is arranged as follows:

$$l = 1.59812$$
$$D \times \frac{s}{60} = 9$$
$$L = \overline{1.59821}$$

When, as in this case, the product $D \times \frac{s}{60}$ is small, it can readily be added or subtracted mentally. Only the significant figures of D (those given in the d-column) are used, it being understood that the result expresses units of

the fifth order of decimals. Thus, instead of writing D = .00036, and $D \times \frac{s}{60} = .00036 \times \frac{s}{60}$, the following abbreviated notation is used: D = 36; $D \times \frac{s}{60} = 36 \times \frac{s}{60}$, the latter product expressing decimal units of the fifth order, or hundred thousandths.

The foregoing formula indicates the process by which the logarithmic functions of an angle containing odd seconds are obtained. It may be stated in words as follows:

Rule.—Drop the seconds, and find the logarithmic function of the remaining angle. Find the tabular difference between this logarithmic function and the same function of the angle next higher in the table. Multiply this tabular difference by the number of seconds in the angle and divide the product by 60. Add this result to or subtract it from the logarithm found, according as the logarithm to be determined is that of a fundamental function or that of a cofunction. The result thus obtained is the required logarithmic function.

EXAMPLE 1.—Find: (a) the logarithmic sine of $15^{\circ} 40' 32''$; (b) the logarithmic cosine.

SOLUTION.—(a) Dropping the seconds, 15° 40' is obtained, whose logarithmic sine, found as in Art. 25, is $\overline{1.43143}$; that is, $l = \overline{1.43143}$. Opposite the space between this logarithm and the following, and in the column marked d, is found the tabular difference 45(=D). Applying the formula given in Art. 27,

$$L = \overline{1.43143} + .00045 \times \frac{38}{60}$$

$$I = \overline{1.43143}$$

$$D \times \frac{s}{60} = 45 \times \frac{32}{60} = 24$$

$$L = \overline{1.43167}$$

that is, $\log \sin 15^{\circ} 40' 32'' = \overline{1}.43167$. Ans.

In practice, it is not necessary to write all the figures of l before adding the correction $D \times \frac{s}{60}$. Having found the value of l in the table, one places and keeps the finger on that value and calculates the correction $D \times \frac{s}{60}$. In the majority of cases, this correction can be added mentally to l. Thus, in the example just explained, the correction is 24, which, being mentally added to the number 43 formed by the last two figures of l, gives 67 as the last two figures of L. The other figures of L are the same as those of l.

(b) The logarithmic cosine of $15^{\circ} 40'$ is $\overline{1.98356}(=l)$. Horizontally opposite the space between this logarithm and the following, the tabular difference 4(=D) is found in the column marked d on the right of the cosine column. As the function under consideration is a cofunction, the correction $D \times \frac{s}{60}$ must be subtracted for *l*. We have, then, $l = \overline{1.98256}$

$$D \times \frac{s}{60} = 4 \times \frac{32}{60} = 2$$
, to the nearest unit

 $L = \bar{1}.98354$

Therefore, $\log \cos 15^{\circ} 40' 32'' = \overline{1.98354}$. Ans.

In practice, the correction 2 would be subtracted mentally, without previously writing the value of l.

EXAMPLE 2.—Find the logarithmic tangent of 63° 39' 27".

SOLUTION.—Dropping the seconds, and referring to the page marked 63° at the bottom, the logarithmic tangent of 63° 39' is found to be .30512(=l). Since in this case the angles increase from bottom to top, the tabular difference to be used is that horizontally opposite the space between the logarithm just taken and the one immediately above it in the column (that is, .30543). This difference is 31, printed in the column marked c. d. on the left of the cotangent column. We have, therefore,

l = .30512 $\frac{s}{60} \times D = \frac{27}{60} \times 31 = 14$, to the nearest unit L = .30526

Therefore, $\log \tan 63^{\circ} 39' 27'' = .30526$. Ans.

EXAMPLE 3.-Find the logarithmic cotangent of 54° 8' 9".

SOLUTION.—Dropping the seconds, the value of l is found to be $\overline{1.85913}$. The tabular difference in the c. d. column and horizontally opposite the space between this logarithm and the one immediately above it is 26. As the cotangent is a cofunction, the correction $\frac{s}{60} \times D$ is to be subtracted from l. Then,

$$l = 1.85913$$

$$\frac{s}{60} \times D = \frac{9}{60} \times 26 = 4$$

$$L = \overline{1.85909}$$

$$\log \cot 54^{\circ} 8' 9'' = \overline{1.85909}. \text{ Ans.}$$

Therefore,

EXAMPLES FOR PRACTICE

1.	Find the logarithmic sine, tangent, and cosine of 33° 21' 46'.
	Ans. $\begin{cases} \log \sin = \bar{1}.74032 \\ \log \tan = \bar{1}.81852 \\ \log \cos = \bar{1}.92179 \end{cases}$
2.	Find the logarithmic sine and cotangent of 23° 3' 17".
	Ans. $\begin{cases} \log \sin = \bar{1}.59286 \\ \log \cot = .37100 \end{cases}$
3.	Find the logarithmic tangent and cosine of 49° 12' 12".
	Ans. $\begin{cases} \log \tan = .06395 \\ \log \cos = \overline{1}.81516 \end{cases}$
4.	Find the logarithmic sine, tangent, and cosine of 72° 52' 49".
	Ans. $\begin{cases} \log \sin = \bar{1}.98031 \\ \log \tan = .51143 \\ \log \cos = \bar{1}.46890 \end{cases}$
5.	Find the logarithmic sine and cotangent of 81° 38' 28".
	Ans. $\begin{cases} \log \sin = \bar{1}.99536 \\ \log \cot = \bar{1}.16712 \end{cases}$
6.	Find the logarithmic tangent and cosine of 65° 0' 47".
	Ans. $\begin{cases} \log \tan = .33159 \\ \log \cos = \overline{1.62574} \end{cases}$
7.	Find the logarithmic secant and cosecant of 59° 0' 9".
	Ans. $\begin{cases} \log \sec = .28819 \\ \log \csc = .06692 \end{cases}$

28. Use of the Column of Proportional Parts.-The method described in the preceding article can be applied to any table of logarithmic functions. Some tables, however, among them the table furnished with this Course, contain a column giving the products of the tabular differences by the fractions $\frac{6}{60}$, $\frac{7}{60}$, $\frac{8}{60}$, $\frac{9}{60}$, $\frac{10}{60}$, $\frac{20}{60}$, $\frac{30}{60}$, $\frac{40}{60}$, and $\frac{50}{60}$. These products are called proportional parts, and are given in the right-hand column (marked p. p. at the top) of each page. beginning with 3°. The tabular differences are here printed in heavy figures. Under each tabular difference are given the products of it by $\frac{6}{60}$, $\frac{7}{60}$, etc., the number of sixtieths being printed horizontally opposite the product, on the left of a vertical line. Thus, referring to the right-hand column of the page marked 13° at the top, the numbers 54, 53, 52, printed in heavy type, are tabular differences. The number 27, directly under 54, and horizontally opposite the

number 30 on the left of the vertical line, is the product of 54 by $\frac{3}{60}$. Likewise, 17.3, found under 52, and horizontally opposite 20, is the product of 52 by $\frac{20}{60}$. The proportional parts for 1, 2, 3, 4, 5 are obtained from those for 10, 20, 30, etc., by moving the decimal point one place to the left. Thus, the proportional part for 20, under the tabular difference 52, is 17.3, as just explained. The proportional part for 2, that is, the product of 52 by $\frac{2}{60}$, is 1.73.

In the first three pages of the logarithmic table, no proportional parts are given, the use of these pages being different from that of the others. In pages 45, 46, and 47, not all the tabular differences are given in the p. p. column, owing to want of space; but the proportional part for any tabular difference is easily obtained by means of the proportional parts for digits given at the bottom of the p. p. column. Referring, for example, to page 45, the tabular difference 215, which is found in the c. d. column, does not appear in the p. p. column. If we wish to find the product of 215 by 38, we look in the p. p. column for the tabular difference next lower than 215, which is 212. Horizontally opposite 30, and under 212, we find 106; that is, $212 \times \frac{30}{60} = 106$. As 215 = 212 + 3, we must add to the product just found (106), the product of $3 \times \frac{39}{50}$. This is taken from the column headed 3 near the bottom of the p. p. column: there we find 1.5 horizontally opposite 30; that is, $3 \times \frac{30}{60} = 1.5$. Therefore, $215 \times \frac{30}{60} = 106 + 1.5 = 107.5$. The addition of these two products can usually be effected mentally.

The correction $D \times \frac{s}{60}$ to be applied to l in order to find L (formula of Art. 27) is found from the table of proportional parts as follows:

Rule.—Having found the tabular difference D, look for this difference in the column of proportional parts. If this difference is found in that column and the number of seconds is a digit greater than 5 or a digit followed by a cipher, look for it on the left of the vertical line under D; the correction is then found horizontally opposite this number, and directly under D. If the number of seconds is a digit less than 6, add a cipher, find the proportional part corresponding to the resulting number, and move the decimal point one place to the left. If the number of seconds consists of two significant digits (as 39), find the correction for the first digit followed by a cipher, and that for the second digit, and add the two corrections. (Thus, if the number of seconds is 43, the correction is found by adding the corrections for 40 and 3.)

If the tabular difference D is not found in the p. p. column (which may happen only on pages 45 to 47), take, as just explained, the proportional part corresponding to the next lower tabular difference found in the p. p. column; then, from the digit columns found at the bottom of the p. p. column, find the proportional part corresponding to the difference between D and the tabular difference just used. Add the two proportional parts thus found.

EXAMPLE 1.—Find: (a) the logarithmic tangent of $22^{\circ} 17' 8''$; (b) the logarithmic cosine.

Solution.—(a) Dropping the seconds, we find log tan 22° 17' = $\overline{1.61256}(=l)$; D = 36. Turning to the column of proportional parts, 36 is found in heavy type near the top of the page. Following the horizontal row that begins with 8 (number of seconds) at the left of the vertical line under 36, we find in that row, and directly under 36, the correction 4.8, which may be called 5, as there are no other numbers to be combined with it. Therefore,

$$t = 1.61256$$

 $\frac{s}{60} \times D = p. p. = 5$
 $L = \overline{1.61261}$

 $\log \tan 22^\circ 17' 8'' = \overline{1.61261}$. Ans.

(b) $l = \log \cos 22^{\circ} 17' = \overline{1.96629}$; D = 5. Looking for the column headed 5 among the proportional parts, the correction .7 (or say 1) is found directly under 5 and horizontally opposite 8. Therefore,

$$l = 1.96629$$

$$\langle D = p. p. = 1$$

$$L = 1.96628$$

That is, $\log \cos 22^{\circ} 17' 8'' = \overline{1.96628}$. Ans.

s >

EXAMPLE 2.—Find the logarithmic sine of 3° 18' 9".

SOLUTION.— $l = \sin 3^{\circ} 18' = \overline{2}.76015$; D = 219. The difference 219 is not found in the p. p. column; the tabular difference in the p. p. column next lower is 216. Under 216, and horizontally opposite 9, is

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That is.

found 32.4. The difference between 219 and 216 is 3. Looking for 3 in the digit columns at the bottom of the p. p. column, .5 is found under 3, and horizontally opposite 9. Therefore, $219 \times \frac{9}{60} = 32.4 + .5 = 33$, nearly.

$$l = \overline{2.76015}$$

$$219 \times \frac{9}{60} = 33$$

$$L = \overline{2.76048}$$

$$\log 3^{\circ} 18' 9'' = \overline{2.76048}. \text{ Ans.}$$

That is,

1

EXAMPLE 3.—Find: (a) the logarithmic tangent of $53^{\circ} 47' 04''$; (b) the logarithmic cosine.

SOLUTION.—(a) $l = \log \tan 53^{\circ} 47' = .13529$; D = 26; the proportional part for 40, under D, that is, under 26, is 17.3; the proportional part for 4 is $\frac{17.3}{10}$, or 2, nearly.

$$l = .13529$$

 $26 \times \frac{4}{60} = 2$
 $L = .13531$

That is. $\log \tan 53^\circ 47' 4'' = .13531$. Ans.

(b) $l = \log \cos 53^{\circ} 47' = \overline{1.77147}$; D = 17. The number horizontally opposite 40, in the column headed 17 among the proportional parts, is 11.3; the proportional part for 4 is, therefore, $\frac{11.3}{10} = 1$, nearly.

$$l = \overline{1}.77147$$

$$17 \times \frac{4}{60} = 1$$

$$L = \overline{1}.77146$$
That is, log cos 53° 47′ 4″ = $\overline{1}.77146$. Ans

EXAMPLE 4.- To find the logarithmic cotangent of 72° 35' 47".

SOLUTION.— $l = \log \cot 72^{\circ} 35' = \overline{1.49652}; D = 45$. Looking among the proportional parts for the column headed 45, the correction for 40 is found to be 30, and that for 7 is found to be 5.3. Therefore, $l = \overline{1.49652}$

> p. p. for 40 = 30.0 p. p. for 7 = 5.3 p. p. for 47 = 35 $L = \overline{1.49617}$

That is, $\log \cot 72^{\circ} 35' 47'' = \overline{1.49617}$. Ans.

In practice, it would not be necessary to write down the corrections 30 and 5.3, which would be added mentally. The same remark applies to all similar cases.

EXAMPLES FOR PRACTICE

 Find the logarithmic sine and cotangent of 9° 39′ 17″. Ans. {log sin = 1.22456 log cot = .76924
 Find the logarithmic sine, tangent, and cosine of 39° 8′ 52″. Ans. {log sin = 1.80025 log tan = 1.91065 log cos = 1.88959
 Find the logarithmic cotangent and cosecant of 80° 3′ 46″. Ans. {log cot = 1.24352 log csc = .00657
 Find the logarithmic sine, secant, and tangent of 49° 0′ 54″. Ans. {log sin = 1.87788 log sec = .18319 log tan = .06137
 Find the logarithmic tangent and cosine of 4° 2′ 4″. Ans. {log tan = 2.84838 log cos = 1.99892

29. To Find the Angle Corresponding to Any Logarithmic Function When the Given Function Is Found in the Table.—In this case, the angle, which contains no odd seconds, is found as follows:

Rule.—Find the given logarithm in the column marked by the name of the function whose logarithm is given. Then, if the name of the given function is at the top of the column, the number of degrees in the angle is that at the top of the page, and the number of minutes is horizontally opposite the logarithm, in the left-hand minute column. If the name of the function is at the foot of the column, the number of degrees in the angle is that at the foot of the page, and the number of minutes is in the righthand minute column, horizontally opposite the given logarithm.

In searching the table for a given logarithm, it should be borne in mind that the logarithmic sines and tangents increase, and the cosines and cotangents decrease, from 0° to 90° . Therefore, in the columns marked log sin and log tan at the top, the logarithms increase, and in the columns headed log cos and log cot the logarithms decrease, from the first to the last page. The sines and tangents continue to increase, and the cosines and cotangents to decrease, from the last page to the first, in the columns marked with the names of these functions, respectively, at the bottom. Thus, the last page contains, in the column headed log sin, the logarithmic sines of the angles between 44° and 45°. The sines are continued in the column marked log sin at the bottom, which contains the logarithmic sines of the angles between 45° and 46°; the preceding page contains the sines of angles between 46° and 47°, etc. Here the logarithmic sines increase from bottom to top, and in the inverse order of the pages.

When looking for a given logarithmic sine, open the table at random. Glance at both of the sine columns, that is, the column marked log sin at the top and the column marked log sin at the bottom, and compare the logarithms in them with the given logarithm. If the given logarithm is less than those found in the column marked log sin at the top. said given logarithm must be in that column, but in a preceding page. If the given logarithm is greater than those in the column marked log sin at the bottom, said given logarithm must be in that column, but in a preceding page. If neither of these is the case, the given logarithm must be in a subsequent page. Turn a few pages forwards or backwards, as the case may be, and repeat the operation. The comparison of the two columns, however, is not usually necessary after the first three figures of the given logarithm have been found in one of them, as that logarithm is then found in that column, and can be readily seen among the logarithms beginning with those three figures.

Proceed exactly in the same manner when the given function is a cosine; that is, treat the cosine as though it were a sine; but, having found the given logarithm, treat it as that of a cosine and take the angle accordingly.

As the tangents of angles less than 45° are less than 1, their logarithmic tangents have negative characteristics, and as the tangents of angles greater than 45° are greater than 1, their logarithmic tangents have positive characteristics. Therefore, a logarithmic tangent should be looked for in the

column marked log tan at the top or at the bottom, according as its characteristic is negative or positive. For a logarithmic cotangent, the rule should be reversed.

EXAMPLE 1.—Find the angle whose logarithmic sine is 1.57669.

SOLUTION.—Opening the table at random, say at the page marked 36° at the top, it is at once seen that the logarithms in the column marked log sin at the top are greater than the given logarithm. This logarithm must, therefore, be in that column, but in a preceding page. Turning the pages backwards, a few at a time, the given logarithm is found on page 64, among those logarithms whose first three figures are $\overline{1.57}$. As the name of the function is at the head of the column, the number of degrees (22) is taken from the top of the page, and that of minutes (10) from the left-hand minute column. Therefore, the angle whose logarithmic sine is $\overline{1.57669}$ is $22^{\circ} 10'$, or $\overline{1.57669} = \log \sin 22^{\circ} 10'$.

Suppose that the table had first been opened at page 56. Since the given logarithm is greater than those in the column marked log sin at the top and less than those in the column marked log sin at the bottom (or log cos at the top), the given logarithm is to be found in a subsequent page. Suppose also that, turning the pages forwards, a few at a time, we come to page 63, and find the first three figures ($\overline{1.57}$) of the given logarithm in the column marked log sin at the top. Then, without consulting the other column, we follow the former column to the bottom, and into the next page, where we find the given logarithm, and take the corresponding angle as before.

EXAMPLE 2.—To find the angle whose logarithmic sine is $\overline{1.89810}$.

SOLUTION.—Open the table at random, say at page 73. Since the given logarithm is greater than those in the column marked log sin at the top, and less than those in the column marked log sin at the bottom, it must be found in a subsequent page. Suppose that we turn next to page 85. We see at once that the given logarithm is greater than those in the column headed log sin, and also than those in the column marked log sin at the bottom. Therefore, it must be in the latter column in some preceding page. Turning the pages backwards, we find the first three figures ($\overline{1}.89$) of the given logarithm on page 79, and among the logarithms to which these three figures are common, we find $\overline{1}.89810$. As this is a logarithmic sine, and the name sine is at the bottom of the column, the degrees in the corresponding angle are taken from the bottom of the page, and the minutes from the right-hand minute column. Therefore, 52° 16' is the angle whose logarithmic sine is $\overline{1}.89810$; that is, $\overline{1}.89810 = \log \sin 52^{\circ}$ 16'. Ans.

EXAMPLE 3.-Find the angle whose logarithmic cosine is 1.86924.

SOLUTION.—Treating this as though it were a logarithmic sine, it is found, as explained above, on page 34, in the column marked log sin

at the bottom. Since the name cosine is at the top of the column, the required angle is 42° 16'. That is, $\overline{1.86924} = \log \cos 42^{\circ} 16'$. Ans.

EXAMPLE 4.—Find the angle whose logarithmic cotangent is .15639.

SOLUTION.—As the characteristic is positive, the logarithm should be looked for in the column marked log cot at the top. After looking in a few pages, the first three figures (0.15) of the logarithm are found on page 76, and among them is found the given logarithm. The name of the function being at the head of the column, the degrees in the angle are taken from the top of the page, and the minutes from the left-hand minute column. Therefore, $.15639 = \log \cot 34^{\circ} 54'$. Ans.

EXAMPLES FOR PRACTICE

1.	Find the angle	e whose logarithmic s	sine is 1.57885.	Ans. 22° 17′
2.	Find the angle	e whose logarithmic s	sine is 1.66731.	Ans. 27° 42'
3.	Find the angle	e whose logarithmic s	ine is $\bar{2}.93740$.	Ans. 4° 58'
4.	Find the angle	whose logarithmic s	ine is 1.98345.	Ans. 74° 17'
5.	Find the angle	e whose logarithmic of	cosine is 1 .92086.	
				Ans. 33° 33
6.	Find the angle	whose logarithmic c	cosine is 1.57232.	Ans. 68° 4
7.	Find the angle	whose logarithmic c	cosine is $\overline{1}.84949$.	Ans. 45° 0'
8.	Find the angle	whose logarithmic ta	angent is 1.97649).
				Ans. 43° 27'
9.	Find the angle	e whose logarithmic c	cotangent is 2.892	274.
	0	0	0	Ans. 85° 32'
.10	Find the and	le whose logarithmic	tangent is 6737	7
.10	Find the ang	ie whose logarithmic	tangent is .oron	Ans. 78° 2'
11.	Find the ang	le whose logarithmic	cotangent is .35	517.
			9.000	Ans. 23° 49'
12	Find the ang	le whose logarithmic	tangent is 1.2806	50.
		6	0	Ans. 87° 0'

30. To Find the Angle Corresponding to a Given Logarithmic Function When the Function Is Not in the Table.—Without the Use of Proportional Parts.—From the formula given in Art. 27, the following may be obtained:

$$s = \frac{(L-l) \times 60}{D} = \frac{(L-l) \times 60}{l'-l}$$

Therefore, if the function L is given and it is found to lie between the consecutive logarithms l and l', the corresponding angle A + s is that corresponding to l increased by the number of seconds determined by the formula just given. It will be remembered (see Art. 27) that l and l' are, respectively, the logarithmic functions of two angles (A and A + 1') differing by one minute. If the function is a fundamental function (sine or tangent) l' is greater than l; and since L lies between l and l', L is also greater than l; therefore, both L - l and l' - l are positive. If the function is a cofunction, l is greater than l', and also greater than L; therefore, both L - l and l' - l are negative, and $\frac{L - l}{l' - l}$ is positive. In such case, however, it is better to write this fraction in the form $\frac{l - L}{l - l'}$.

From the formula and the explanations just given, the following rule is derived for finding the angle corresponding to any given logarithmic function:

Rule.—Find in the table the two consecutive logarithmic functions between which the given function lies. The degrees and minutes in the smaller of the angles corresponding to these two functions are the degrees and minutes in the required angle.

Find the difference between the given function and that of the smaller angle; multiply that difference by 60, and divide the product by the tabular difference between the two functions in the table. The result will be the number of odd seconds in the required angle.

As the tabular difference is expressed in units of the fifth decimal order, the difference L - l should be likewise expressed. Thus, if $L = \overline{1.25198}$, and $l = \overline{1.25168}$, the difference L - l will be called 30.

EXAMPLE 1.—Find the angle whose logarithmic sine is $\overline{1.47867}$ (= L).

SOLUTION.—The first three figures of the given logarithm are always found in the table, and this makes it easy to determine the functions between which the given logarithm lies. Searching the sine columns of the table, it is found that $\overline{1.47867}$ lies between $\overline{1.47854}(=l)$ and

1.47894(= l') on page 59. The smaller of the two angles corresponding to these two logarithms is $17^{\circ} 31'(=A)$. Now, L - l = 13, l' - l (tabular difference taken from table) = 40. Therefore,

s =
$$\frac{13 \times 60}{40}$$
 = 19.5", or, say, 20"
and $A + s = 17^{\circ} 31' + 20'' = 17^{\circ} 31' 20''$
that is, $\overline{1.47867} = \log \sin 17^{\circ} 31' 20''$. Ans.

EXAMPLE 2.—Find the angle whose logarithmic tangent is .27743 (= L).

SOLUTION.—As the characteristic is positive, the logarithms between which L lies should be looked for in the column marked log tan at the bottom. These two logarithms are .27738(=l) and .27769(=l'). The smaller angle corresponds to .27738, and is $62^{\circ} 10'(=A)$. Also,

$$L - l = 5, l' - l (= D) = 31$$

5 × 60

EXAMPLE 3:—Find the angle whose logarithmic cotangent is $\overline{1.85899}(=L)$.

Solution.— L is found to lie between $\overline{1.85887}(=l')$ and $\overline{1.85913}$ (= l). It will be noticed that here l is the greater, and l' the smaller of the two logarithms. Angle corresponding to $l = 54^{\circ} 8'(=A)$.

 $l = \overline{1.85913}$ $L = \overline{1.85899}$ $l - L = \overline{14}; \ l - l' = 26$ $A + s = 54^{\circ} 8' + \frac{14 \times 60}{26} = 54^{\circ} 8' 32'', \text{ nearly}$ $\overline{1.85899} = \log \cot 54^{\circ} 8' 32''. \text{ Ans.}$

EXAMPLES FOR PRACTICE

1. Find the angle whose logarithmic sine is 1.45566.	
Ans. 16	6° 35′ 27″
2. Find the angle whose logarithmic tangent is 1.33471.	
Ans. 12	.2° 11′ 44″
3. Find the angle whose logarithmic sine is 1.89798.	
Ans. 52	2° 14′ 42″
4. Find the angle whose logarithmic cosine is 1.67412.	
	1° 49' 23"
5. Find the angle whose logarithmic cosine is 1.92386.	
Ans. 31	2° 56′ 45″

42

that is.

6.	Find	the	angle	whose	logarithmic	cotangent	is .54	4139.			
								Ans.	16°	2' 2	20'
7.	Find	the	angle	whose	logarithmic	tangent is	Ī.86	6712.			
			-					Ans.	36°	22'	7"
8.	Find	the	angle	whose	logarithmic	cosine is I	.9978	5.			
								Ans	. 5°	42′	0'
9.	Find	the	angle	whose	logarithmic	cotangent					
	•		_				A	lns. 8	32° 2	5' E	52/

With the Use of Proportional Parts.-Having found the 31. degrees and minutes in the angle as in the preceding case, the number s of odd seconds may be 105 conveniently found from the column of propor-6 10.5 tional parts. In order to facilitate the explanations 7 12.3 that follow, the proportional parts corresponding 8 14.0 to the tabular difference 105 are here copied from 9 15.8 page 48 of the table. It will, therefore, be assumed 17.5 10 that the value of D is 105, and, for what is said 20 35.0 below, the student should refer to these propor-30 52.5 tional parts. Such being the case, the formula 70.0 40 given at the beginning of the preceding article 50 87.5 may be written,

$$s = \frac{(L-i) \times 60}{105}$$

The value L - l, which is the difference between the given logarithm and the logarithm of the degrees and minutes (A) in the required angle, is readily determined, as already explained. It is only necessary to repeat that, if the function is a cofunction, l - L should be used instead of L - l. Since the numbers on the right of the vertical line are the products of $\frac{10.5}{6.0}$ by the numbers on the left, it follows that the numbers on the left are the products of those on the right by $\frac{6.0}{10.5}$. Thus, $52.5 = \frac{10.5}{60} \times 30$, and $30 = 52.5 \times \frac{6.0}{10.5}$. $= \frac{52.5 \times 60}{10.5}$. Therefore, if L - l is found among the numbers directly under 105, the value of s is the number on the left of the vertical column horizontally opposite L - l. For example, if L - l = 35, then s = 20''. If L - l = 16, then

s = 9'', the number 9 being opposite 15.8, which, to the nearest unit, may be called 16.

It will be remembered that the proportional parts opposite 10, 20, 30, 40, 50, when divided by 10 (that is, when the period is moved one place to the left), give the products of $\frac{10.5}{60}$ by 1, 2, 3, 4, and 5. From those parts we may, therefore, find by inspection the products of $\frac{10.6}{60}$ by all the digits from 1 to 9; and, in what follows, we shall proceed as if the products 1.75, 3.50, 5.25, 7.00, 8.75 of $\frac{10.6}{60}$ by 1, 2, 3, 4, and 5 were actually printed in the table opposite those digits; that is, it will be assumed that the proportional parts run in this order: 1.75, 3.50, 5.25, 7.00, 8.75, 10.5, 12.3, 14.0, etc., up to 87.5, the corresponding numbers on the left being, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 20, 30, 40, 50. The proportional parts 1.75, 3.50, 5.25, 7.00, 8.75 will be referred to as proportional parts found in the table, corresponding to 1, 2, 3, 4, and 5 seconds, respectively.

This being understood, the number s of odd seconds in the angle is determined as follows:

Rule.—Find l, l', L - l, and l' - l (= tabular difference, or D), as before. Look for the tabular difference D in the column of proportional parts. Look for L - l in the column of proportional parts directly under D. If L - l is found there, the number horizontally opposite it on the left of the vertical line is the required number of seconds s. If L - l is not found under D, take the proportional part next lower, which call p. Find the difference between L - l and p, and look among the proportional parts under D for this difference, or the part nearest to it, whether higher or lower. Call this part p'. Add the numbers horizontally opposite p and p' on the left of the vertical line. The result will be the required number of seconds s.

EXAMPLE 1.—Find the angle whose logarithmic tangent is $\overline{1.42822}(= L)$.

SOLUTION.— l = 1.42805, $A = 15^{\circ}0'$, L - l = 17, D = 51. Looking in the column marked p. p. for 51, the number 17(=L-l) is found under it, horizontally opposite the number 20 on the left of the vertical column. Therefore, s = 20'', and

 $\overline{1.42822} = \log \tan 15^{\circ} 0' 20''$. Ans.

EXAMPLE 2.--Find the angle whose logarithmic cosine is $\overline{1.52783}(=L)$.

SOLUTION.— $l = \overline{1.52811}$, $A = 70^{\circ} 17'$, l - L = 28, D = 36. The proportional part under 36 next lower than 28 is 24; 28 - 24 = 4; the proportional part nearest 4 is 4.2; the number horizontally opposite 24 is 40; and the number horizontally opposite 4.2 is 7; hence, s = 40 + 7 = 47'', and therefore

$$\overline{1.52783} = \log \cos 70^{\circ} 17' 47''$$
. Ans.

EXAMPLE 3.—Find the angle whose logarithmic sine is $\overline{1.66191}(L)$.

SOLUTION.— $l = \overline{1.66173}$; $A = 27^{\circ} 19'$; L - l = 18; D = 24. Looking in the p. p. column for 24, the proportional part next lower than 18 is 16(=p), horizontally opposite which is 40. 18 - p = 18 - 16 = 2. This difference is found among the proportional parts in the table (since it is the same as 20 with the decimal point moved one place to the left), and corresponds to $5'' \left(=\frac{50}{10}\right)$. Therefore, s = 40 + 5 = 45'', and

$$\overline{1.66191} = \log \sin 27^{\circ} 19' 45''$$
. Ans.

EXAMPLE 4.—Find the angle whose logarithmic cotangent is $\overline{1.00375}(= L)$.

SOLUTION.— $l = \overline{1.00427}$; $A = 84^{\circ} 14'$; l - L = 52; D = 126. The proportional part under 126 next lower than 52 is 42(=p), which corresponds to 20''; 52 - 42 = 10. The proportional part nearest to 10 is $10.50 \left(=\frac{105.0}{10}\right)$, which corresponds to $5'' \left(=\frac{50}{10}\right)$. Therefore, s = 20'' + 5'' = 25'', and

 $\overline{1.00375} = \log \cot 84^{\circ} 14' 25''$. Ans.

EXAMPLES FOR PRACTICE

1. Find the angle whose logarithmic sine is 1.78988. Ans. 38° 3' 20"

2. Find the angle whose logarithmic tangent is $\overline{1.78540}$.

Ans. 31° 23' 15"

3. Find the angle whose logarithmic sine is 1.77777.

Ans. 36° 49′ 56″

4. Find the angle whose logarithmic cosine is 1.87341.

Ans. 41° 39' 21"

 Find the angle whose logarithmic cotangent is .31789. Ans. 25° 41′ 9^{//}

6. Find the angle whose logarithmic cosine is 1.34567. Ans. 77° 11' 38"

- Find the angle whose logarithmic cotangent is I.00381. Ans. 84° 14′ 22″
- Find the angle whose logarithmic tangent is 1.00300.
 Ans. 84° 19' 42"
- 9. Find the angle whose logarithmic sine is $\overline{2}.99001$.

Ans. 5° 36' 30"

32. Tabular Values Increased by 10.—To avoid calculating with negative characteristics, they may be made positive by increasing them by 10. Thus, log sin 27° may be given as 9.65705 instead of $\overline{1.65705}$. The true logarithm is, therefore, 9.65705-10; the -10 is usually not written, but is implied. In many books this method is used for the logarithms of trigonometric functions. In applying such logarithms to the solution of a problem, the characteristic in the final result must be corrected to agree with the conditions of the problem.

GENERAL PRINCIPLE OF INTERPOLATION

33. It has been explained in some of the preceding articles how to determine the natural or the logarithmic functions of any angle containing an odd number of seconds, and therefore, not found in the table: also, how to find the angle corresponding to a given function, when that function is not in the table but lies between two values given in the table. The operation by which such intermediate values are determined from a table is called interpolation. The values that are actually given in the table are called tabular values. For example, in the table of logarithmic functions already described are found all angles that lie between 0° and 90° and contain no odd seconds, and also the logarithmic sines, cosines, etc. of such angles; those are all tabular values. Angles containing odd seconds are not in the table. nor are their logarithmic functions. Both these angles and their functions are intermediate values, and it is in connection with them that interpolation is used.

34. The general principle of interpolation, to be explained presently, is of the utmost importance, and of great value to the engineer, whose work requires the frequent use of tables of various kinds. That principle, although only approximately true, applies to nearly all tables with which the engineer has to deal, and the student should endeavor to make himself thoroughly familiar with it.

Let a table be constructed on the general type shown on the margin, the left-hand column containing values of a quantity

X, and the right-hand column corresponding values of some quantity whose values depend on the values of X. Thus, the values of X may be the natural numbers 1, 2, 3, 4, etc., and the corresponding values of F may be the logarithms or the square roots of those numbers; or the values of X may be angles, and those of F may be sines, cosines, etc., either natural or logarithmic. So far

X	F
-	-
-	-
-	-
<i>x</i> 1	f_1
x	f
X _B	f s

as the principle of interpolation is concerned, it is immaterial what kind of quantity is represented by X, and what kind of quantity is tabulated under F. It should be stated, however, that the principle applies only to tables in which the differences between consecutive values of X and the differences between the corresponding values of F do not vary very rapidly.

Let x_1 and x_2 , as shown in the above general form, be two consecutive values of X given in the table, and f_1 and f_2 the corresponding values of F. Let x be a value of X lying between x_1 and x_2 , and f the corresponding value of F. Neither x nor f is in the table, but one of them is given, and the problem is to find the other by interpolation. For instance, if the table is one of natural tangents in which the angles increase by whole minutes, x_1 and x_2 may be, respectively, $31^\circ 42'$ and $31^\circ 43'$, and f_1 and f_2 their corresponding tangents; while x may be any angle between $31^\circ 42'$ and $31^\circ 43'$, and f its tangent. Either x may be given to find f; or f may be given to find x. The quantity by which the tabular value x_1 must be algebraically increased in order to obtain x will be called the **increment** of x_1 , and denoted by $i(x_1)$, read *increment* of x_1 (mathematicians use the notation Δx_1 , read *delta* x_1). We have, then,

 $x = x_1 + i(x_1) \tag{1}$

Using a similar notation for f_{i} ,

$$f = f_1 + i(f_1) \tag{2}$$

If x is given, $i(x_1)$ may be assumed as given, since $i(x_1) = x - x_1$. Then $i(f_1)$ is determined by interpolation, as explained below, and f is found from formula 2. Similarly, if f is given, $i(f_1)$ is likewise given, and x is found by interpolation.

The difference, as $x_1 - x_1$, of two consecutive values of X, will be called the **interval** of X; and that between two consecutive values of F, the interval of F. The notation $I(x_1)$. read *interval of* x_1 , will be used to denote the interval $x_1 - x_1$. Similarly, $I(f_1)$ will denote the interval $f_2 - f_1$.

The principle of interpolation is this: The increments $i(x_1)$ and $i(f_1)$ are to each other as the corresponding intervals $I(x_1)$ and $I(f_1)$; or, algebraically,

$$\frac{i(x_1)}{i(f_1)} = \frac{I(x_1)}{I(f_1)}$$
(3)

This formula is very easily remembered on account of its symmetry. The following, derived from it, serve, respectively, to find $i(f_1)$ when x is given, and $i(x_1)$ when f is given:

$$i(f_{1}) = I(f_{1}) \times \frac{i(x_{1})}{I(x_{1})}$$
(4)
$$i(x_{1}) = I(x_{1}) \times \frac{i(f_{1})}{I(f_{1})}$$
(5)

The last two formulas may be stated in the form of a general principle, as follows: *Either increment is equal to the corresponding interval multiplied by the ratio of the other increment to the other interval.* It is easy to remember what the numerator of this ratio is, by noticing that the ratio is always less than 1, and that, since the increment is always less than the interval, the former must be the numerator and the latter the denominator. It should be noted that $i(x_1)$, $i(f_1)$, $I(x_1)$, and $I(f_1)$ may be expressed in any comvenient units, it being understood that $i(f_1)$, as determined from formula 4, is in the same units as $I(f_1)$; and that $i(x_1)$, as determined from formula 5, is in the same units as $I(x_1)$. Thus, if the values of f_1 and f_1 in the table are, respectively, 4.3476 and 4.3463, then, $I(f_1) = f_2 - f_1$ = .0013, or, if one ten-thousandth is taken as the unit, we may write $I(f_1) = 13$. The value of $i(f_1)$, determined from formula 4, must be understood to express ten-thousandths. For instance, if $\frac{i(x_1)}{I(x_1)} = .3$, then, $i(f_1) = 13 \times .3 = 3.9$ (tenthousandths) = 4 (ten-thousandths), nearly.

The value of f is then found thus,

$$f_{1} = 4.3463 \\ i(f_{1}) = \frac{4}{4.3467} \\ f = 4.3467$$

Usually, the correction $i(f_1)$ can be added to f_1 mentally, in order to find f_2 .

EXAMPLE 1.—Find the logarithm of 57,846 by means of a five-place table giving the logarithms of numbers consisting of four figures.

SOLUTION.—Only the mantissas will be considered, since the characteristics are determined by inspection. The given number lies between $57,840(=x_1)$ and $57,850(=x_2)$, whose logarithms are, respectively, .76223(= f_1) and .76230(= f_2). We have, therefore, expressing $f_2 - f_1$, or $I(f_1)$, in units of the fifth order

$$\begin{array}{cccc} x = 57846 & f_{1} = .76230 \\ x_{1} = 57840 & f_{1} = .76223 \\ i(x_{1}) = & 6 & I(f_{1}) = & 7 \\ I(x_{1}) = x_{1} - x_{1} = 10 \end{array}$$

Then (formula 4),

 $i(f_1) = 7 \times \frac{6}{10} = 4.2 = 4, \text{ nearly}$ $f = \begin{cases} f_1 \\ + i(f_1) \end{cases} = \begin{cases} .76223 \\ - 4 \end{cases} = .76227. \text{ Ans.}$

and

EXAMPLE 2.—Find, by means of a five-place table, the number the mantissa of whose logarithm is .47693. SOLUTION.—Here f(=.47693) lies between the tabular values $.47683(=f_1)$ and $.47698(=f_2)$, which are, respectively, the logarithms of $29,980(=x_1)$ and $29,990(=x_2)$. We have, then,

 $\begin{array}{rcl} f_{2} &= .47698 & & & & \\ f_{2} &= .47698 & & & \\ f &= .47693 & & & \\ f_{1} &= .47683 & & \\ f_{1} &=$

Then (formula 5),

 $i(x_1) = 10 \times \frac{10}{15} = 7$, nearly $x = x_1 + i(x_1) = 29,980 + 7 = 29,987$, Ans.

and

This gives the significant figures of the number. The decimal point should be placed according to the characteristic of the given logarithm.

EXAMPLE 3.—Find the angle whose natural tangent is .56781(= 1) by means of a table giving the natural tangents of angles varying by minutes.

SOLUTION.—Here f is found to lie between .56769(= tan 29° 35' = f_1) and .56808(= tan 29° 36' = f_2). Expressing $x_2 - x_1$, or $I(x_1)$, in seconds, we have

X2	-	29°	36′		f2	=	.56808
x_1	-	29°	35′		f	-	.56781
$I(x_1)$	=		60//		11	=	.56769
					$I(f_1)$	=	39
					$i(f_1)$	=	12

Then (formula 5),

$$i(x_1) = 60'' \times \frac{12}{39} = 18''$$
, nearly
 $x = x_1 + i(x_1) = 29^\circ 35' 18''$. Ans.

and

EXAMPLE 4.—In Searles' field book is given a table of lengths of arcs for different degrees of curvature. Part of it is as follows (lengths in feet):

Degree of Curve (=X)	Length of Arc for One Station $(=F)$
10° 10'	100.131
10° 20'	100.136
10° 30'	100.140

Find the length of the arc between two stations for a 10° 26' curve

SOLUTION.—Here we have, $x = 10^{\circ} 26'$, which lies between $10^{\circ} 20'$ $(=x_1)$ and $10^{\circ} 30(=x_2)$. Expressing $I(x_1)$ and $i(x_1)$ in minutes, and $I(f_1)$ and $i(f_1)$ in thousandths, we have $I(x_1) = 10$, $i(x_1) = 6$, $I(f_1) = 140 - 136 = 4$.

Therefore (formula 4),

$$i(f_1) = 4 \times \frac{6}{10} = 2$$
, nearly
 $f = f_1 + i(f_1) = \begin{cases} 100.136 \\ +2 \end{cases} = 100.138$. Ans.

and

In all simple cases like this the operations can be performed mentally and very rapidly.

EXAMPLES FOR PRACTICE

1. From the following table, find, by interpolation, the cube root of 347.3 and that of 349.7.

Number	Cube Root	
347 348	7.0271 7.0338	
349	7.0406	. (7 0291
350	7.0473	Ans. {7.0291 7.0453

2. Find, from the following table, the diameter of a circle whose circumference is 63.57318.

Diameter	Circumference		
20.1	63.14601		
20.2 20.3	63.46017 63.77433	Ans.	20.236

SOLUTION OF RIGHT TRIANGLES

35. Fundamental Equations.—Let A B C, Fig. 9, be a right triangle, in which A, B, and C are the angles and a, b, and c are the lengths of the sides, c being the hypotenuse. Since A and B are complementary angles, we have

sin	\mathcal{A}	=	cos	B	tan	A	=	cot	B
cos	A	=	sin	B	cot	${\cal A}$	=	tan	B

Also, from the definitions of the trigonometric functions, $\sin A = \frac{a}{c}$, $\tan A = \frac{a}{b}$, $\cos B = \sin A = \frac{a}{c}$, $\cot A = \frac{b}{a}$; whence, expressing the value of a from each of these equations, $a = c \sin A$ (1)

o a	$a = c \sin A$	(1)
	$a = b \tan A$	(2)
A B C N	$a = c \cos B$	(3)
F1G. 9	$a = b \cot B$	(4)

From formulas 1 and 3, the following values are found for c:

С	=	$\frac{a}{\sin A}$	-	a	esc A	(5)
с	-	$\frac{a}{\cos B}$	=	a	sec B	(6)

Finally, from geometry,

$$c^* = a^* + b^*$$
 (7)

Of the trigonometric formulas just given, it is only necessary to commit to memory formulas 1 and 2, as the others are immediate consequences of these. These two formulas may be stated in words thus:

Either leg of a right triangle is equal to the hypotenuse multiplied by the sine, or to the other leg multiplied by the tangent. of the opposite angle.

It should be observed that, since a is either leg whose opposite angle is A, and adjacent angle B, the letters a and bmay be interchanged in the preceding formulas, provided that A and B are likewise interchanged. Thus, by interchanging a and b, A and B in formulas 1 and 5, we obtain,

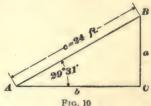
$$b = c \sin B, c = \frac{b}{\sin B} = b \csc B$$

36. Solution of a Right Triangle.—In general, when some of the parts of a triangle are given, the process of determining the others is called solving the triangle, or the solution of the triangle. The latter expression is applied also to the triangle determined in accordance with the given data.

In order to solve a right triangle, two parts, one at least of which should be a side, must be known in addition to the right angle. The two parts may be either (1) one side and one of the acute angles, or (2) two sides.

37. Case I.—Given a Side and an Acute Angle. The other acute angle is found from the relation $A + B = 90^{\circ}$, and the other two sides by means of formulas 1 to 7, Art. **35**, as illustrated by the following examples:

EXAMPLE 1.—In Fig. 10, the length of the hypotenuse A B of the right triangle A C B, right-angled at C, is 24 feet, and the angle A is 29° 31'; find the sides A C and B C, and the angle B.



Norg. - When working examples of this kind, make a sketch and mark the known parts, as shown in the figure.

Solution Without Logarithms.— $B = 90^{\circ} - A = 90^{\circ} - 29^{\circ} 31^{\circ} = 60^{\circ} 29^{\circ}$. By formula 3, Art. 35, interchanging a and b, and A and B,

 $b = c \cos A = 24 \cos 29^{\circ} 31' = 24 \times .87021 = 20.89$ ft., nearly. By formula 1, Art 35,

 $a = 24 \sin 29^{\circ} 31' = 24 \times .49268 = 11.82$ ft., nearly.

Ans. $\begin{cases} B = 60^{\circ} 29' \\ A C = 20.89 \text{ ft.} \\ B C = 11.82 \text{ ft.} \end{cases}$

(1)

(2)

SOLUTION BY LOGARITHMS .- By formulas 3 and 1, Art. 35,

 $b = 24 \cos 29^{\circ} 31'$

 $a = 24 \sin 29^{\circ} 31'$

LOGARITHMS FOR (1)	LOGARITHMS FOR (2)
$\log 24 = 1.38021$	$\log 24 = 1.38021$
$\log \cos 29^{\circ} 31' = \overline{1.93963}$	$\log \sin 29^{\circ} 31' = \overline{1.69256}$
$\log b = 1.31984$	$\log a = 1.07277$
b = 20.89	a = 11.82

In working examples of this kind, the two logarithmic functions should be taken from the table at the same time. It saves time and space to arrange the operations as follows:

> $\log a = 1.07277; a = 11.82$ $\log \sin 29^{\circ} 31' = \overline{1.69256}$ $\log 24 = 1.38021$ $\log \cos 29^{\circ} 31' = \overline{1.93963}$ $\log b = \overline{1.31984}; b = 20.89.$ Ans.

The logarithm of 24 is written first, and then the logarithms of the sine and cosine, one over, the other under, log 24, the addition being performed upwards in one case and downwards in the other.

EXAMPLE 2.-One leg of a right triangle A C B, Fig. 11, is 37 feet

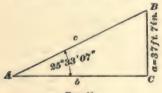


FIG. 11

7 inches long; the angle opposite is 25° 33′ 7″; what are the lengths of the hypotenuse and the side adjacent, and what is the other angle? Solution WITHOUT LOGARITHMS.

Solution without LogARITHMS. $B = 90^{\circ} - 25^{\circ} 33' 07'' = 64^{\circ} 26' 53''.$ Reducing 37 ft. 7 in. to ft., we have, a = 37.583 ft., nearly.

By formula 5, Art. 35,

$$=\frac{37.583}{\sin 25^{\circ} 33' 07''}=\frac{37.583}{43133}=87.133$$
 ft., nearly.

By formula 4, Art. 35, interchanging a and b, and A and B, $b = a \cot A = 37.583 \times 2.09166 = 78.611$ ft., nearly.

$$B = 64^{\circ} 26' 53''$$

Ans.
$$A C = 78.611$$

 $A R = 87.133$ ft

SOLUTION BY LOGARITHMS.-As before,

 $c = \frac{37.583}{\sin 25^{\circ} 33' 7''}$ $b = 37.583 \cot 25^{\circ} 33' 7''$ $\log b = 1.89548; b = A C = 78.611 \text{ ft.}$ $\log \cot 25^{\circ} 33' 7'' = .32049$ $\log 37.583 = 1.57499$ $\log \sin 25^{\circ} 33' 7'' = \overline{1.63481}$ $\log c = \overline{1.94018}; c = A B = 87.132 \text{ ft.} \text{ Ans.}$

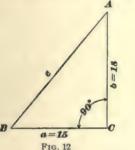
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Also,

It is to be noted that the value of A B given by logarithms is different in the fifth figure from the result given by natural functions. This is due to the fact that in using five-place tables the results can be depended on to be correct to only four figures, and to have a very close approximation to the fifth figure.

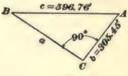
Note.-In the majority of cases, the solution by logarithms is far more expeditious than the solution by natural functions. The student is strongly advised to form the habit of solving all trigonometric problems by means of logarithms and the logarithmic functions, whenever these functions can be used.

38. Case II.—*Given Two Sides.* If the given sides are the two legs *a* and *b*, *A* is found from formula 2, Art. 35, and *B*, from the relation $A + B = 90^{\circ}$. To find *c*, tormula 7, Art. 35, may be used; but, unless *a* and *b* are convenient numbers to square, it is preferable to determine *c* by



formula 5, Art. 35, after having determined A.

If the given sides are the hypotenuse c and one leg, say a, the



angle A is found by formula 1, Art. 35, B from the relation $A + B = 90^{\circ}$, and b from either formula 4, or formula 7, Art. 35. The latter gives

$$b = \sqrt{c^2 - a^2}$$

Unless c and a are convenient numbers to square, the quantity under the radical should be replaced by the product (c+a) (c-a), and then

 $\log b = \frac{1}{2} \left[\log (c+a) + \log (c-a) \right]$ from which b can be readily determined.

EXAMPLE 1.—Given a and b as shown in Fig. 12, to find A, B, and c SOLUTION.—Formula 2, Art. 35,

$$\tan A = \frac{a}{b} = \frac{15}{18} = \frac{5}{6} = .83333$$
$$A = 39^{\circ} 48' 20''$$
$$B = 90^{\circ} - 39^{\circ} 48' 20'' = 50^{\circ} 11' 40''$$

Formula 5, Art. 35,

 $c = \frac{15}{\sin A} = \frac{15}{\sin 39^{\circ} 48' 20''}$ log 15 = 1.17609 log sin 39° 48' 20'' = Ī.80630 log c = 1.36979; c = 23.431

Otherwise,

 $c = \sqrt{15^\circ + 18^\circ} = \sqrt{(3 \times 5)^\circ + (3 \times 6)^\circ} = 3\sqrt{5^\circ + 6^\circ} = 3\sqrt{61} = 23.431.$ Ans.

EXAMPLE 2.—The hypotenuse c and the leg b having the values shown in Fig. 13, find the acute angles and the leg a.

SOLUTION.—By formula 3, Art. 35, interchanging a and b, A and B, $\cos A = \frac{b}{c} = \frac{305.45}{596.76}$

 $90^{\circ} = 89^{\circ} 59' 60''$ $\log 305.45 = 2.48494$ $\log 596.76 = 2.77580$ $A = 59^{\circ} 12' 46''$ $B = 30^{\circ} 47' 14''$ $\log \cos A = \overline{1.70914}; A = 59^{\circ} 12' 46''$ Formula 2, Art. 35, $a = 305.45 \tan 59^{\circ} 12' 46''$ $\log 305.45 = 2.48494$ $\log \tan 59^\circ 12' 46'' = .22489$ $\log a = 2.70983; a = 512.66$ $a = \sqrt{c^2 - b^2} = \sqrt{(c+b)(c-b)}$ Otherwise. c + b = 902.21 $\log (c + b) = 2.95531$ $\log(c-b) = 2.46435$ c = 596.76b = 305.452)5.41966c - b = 291.31 $\log a =$ 2.70983; a = 512.66Ans. $\begin{cases} A = 59^{\circ} \ 12' \ 46'' \\ B = 30^{\circ} \ 47' \ 14'' \end{cases}$ a = 512.66 ft.

EXAMPLES FOR PRACTICE

1. In a right triangle A CB, right-angled at C (let the student make a sketch), the hypotenuse AB = 40 inches and angle $A = 28^{\circ}$ 14' 14"; solve the triangle. Angle $B = 61^{\circ} 45' 46''$ A C = 35.239 in. B C = 18.925 in.

2. In a right triangle A C B, right-angled at C, the side B C= 10 feet 4 inches; if angle $A = 26^{\circ} 59' 6''$, what are the other parts?

Ans. Angle $B = 63^{\circ} 0' 54''$ AB = 22 ft. 91 in., nearly AC = 20 ft. 31 in., nearly

3. In a right triangle A CB, the hypotenuse AB = 00 feet and the side A C = 22 feet; solve the triangle. Ans. $\begin{cases} Angle A = 68^{\circ} 29' 22'' \\ Angle B = 21^{\circ} 30' 38'' \\ B C = 55.821 \text{ ft.} \end{cases}$

4. In a right triangle A CB, right-angled at C, side A C = .364 foot and side B C = .216 foot; solve the triangle.

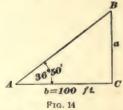
Ans. Angle $A = 30^{\circ} 41' 6''$ Angle $B = 59^{\circ} 18' 54''$ A B = .423 ft.

PRACTICAL EXAMPLES

39. When an object is viewed by an observer, the object may be either above or below a horizontal plane passing through the observer's eye. The angle made with this plane by the line of sight, that is, by the line from the observer's eye to the object, is called an **angle of elevation** if the object is above that plane; an **angle of depression** if the object is below that plane. The object is said to be seen at an angle of elevation or at an angle of depression according as it is above or below the plane in question. For example, a lighthouse is seen from a ship at sea at an angle of elevation, while the ship is seen from the lighthouse at an angle of depression.

EXAMPLE 1.—The angle of elevation of the top of a vertical cliff, CB, Fig. 14, at a point 100 feet from its base, is 36° 50'; find the height of the cliff.

SOLUTION.—By formula 2, Art. 35, required height = $a = 100 \times \tan 36^{\circ} 50' = 100 \times .74900 = 74.9$ ft. Ans.



EXAMPLE 2.—A statue is placed on the top of a column. At a point on the ground 130 feet from the base of the column, the angle of elevation of the top of the statue and that of the column are 43° 38' and 40° 58', respectively; find the height of the statue and column. (Let the student make a sketch.)

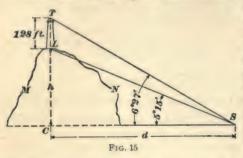
SOLUTION.—Let h = height of column;

h' = height of column and statue.

Then,	$\tan 40^{\circ} 58' = \frac{h}{130}$	
Whence,	$h = 130 \times \tan 40$	° 58' = 112.875
Also,	$\tan 43^\circ 38' = \frac{h'}{130}$	

Whence, $h' = 130 \times \tan 43^\circ 38' = 123.942$ Therefore, the height of the column is 112.875 ft. Ans. The height of the statue is 123.942 - 112.875 = 11.07 ft. Ans.

EXAMPLE 3.—The top and bottom of a lighthouse L T, Fig. 15,



located on a hill M N, are observed from a ship S with a sextant. It is found that the angles of elevation of T and Lare, respectively, 6° 27' and 5° 15'. If the height of the lighthouse is 128 feet, and the surface of the sea is assumed to be plane, what are: (a) the height A(=CL) of the

hill above sea level? (b) the horizontal distance d(= SC) of the ship from the lighthouse?

SOLUTION.—(a) In the right triangles L CS and TCS, we have $d = h \cot 5^{\circ} 15'$, and $d = (h + 128) \cot 6^{\circ} 27'$ Equating the two values of d.

Equating the two values of a,

 $h \cot 5^{\circ} 15' = (h + 128) \cot 6^{\circ} 27'$

whence,

 $h = \frac{128 \cot 6^{\circ} 27'}{\cot 5^{\circ} 15' - \cot 6^{\circ} 27'} = \frac{128 \times 8.84551}{10.8829 - 8.84551} = 555.72.$ Ans.

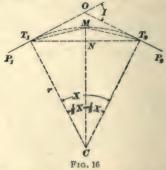
(b) From (a),

 $d = h \cot 5^{\circ} 15' = 555.72 \cot 5^{\circ} 15' = 6,047.8 \text{ ft.}$ Ans.

EXAMPLE 4.—In Fig. 16, $P_1 T_1$ is the track of a railroad that curves into a circular arc $T_1 M T_2$ at T_1 .

The chord $T_1 T_s$ of the whole arc is found, by measurement, to be 764.7 feet, and the chord $T_1 M$ of half the arc, 393.2 feet. Find: (a) the external angle I between $P_2 T_2$ and $P_1 T_1$ produced; (b) the radius $r(=C T_1)$ of the curve $T_1 M T_2$.

SOLUTION.—(a) Draw CT_1 , CM, and CT_2 , as shown. Since P_1O and P_2O are tangent to the circle, the angles OT_1C and OT_2C are right angles; and as the sum of the angles



in the quadrilateral $OT_1 CT_2$ is four right angles, we must have $X+T_1 OT_2 = 2$ right angles = 180°; we have also, $I+T_1 OT_2 = 180^\circ$; therefore, I = X. The line CM bisects both the angle X and the chord $T_1 T_2$. As the angle $MT_1 T_2$ is measured by one-half the

arc MT_2 , it is equal to one-half of MCT_2 , or to $\frac{1}{4}X$. The right triangle MT_1N gives

$$\cos\frac{1}{4}X(\sim\cos M T_1 N) = \frac{T_1 N}{T_1 M} = \frac{\frac{1}{2}T_1 T_2}{T_1 M} = \frac{382.35}{393.2}$$

whence, by either logarithms or natural functions (logarithms are far preferable in this case),

$$\frac{1}{4}X = 13^{\circ} 29' 20''; I(=X) = 4 \times 13^{\circ} 29' 20'' = 53^{\circ} 57' 20''.$$
 Ans.

(b) In the right triangles $C T_1 N_1$,

$$r(=C T_1) = \frac{T_1 N}{\sin \frac{1}{2} X} = \frac{382.35}{\sin 26^\circ 58' 40''} = 842.83$$
 ft. Ans.

EXAMPLE 5.—Fig. 17 is a cross-section of a dam, the dimensions being as shown. The batter of the face A B is 30 in 100, or .3. Find: (a) the width $w_1(=A B)$ of the face; (b) the batter of the back C D; (c) the width $w_2(=C D)$ of the back.

Note.—By the batter of one of the sides of an inclined wall is meant the rate at which that side deviates from the vertical. Thus, in Fig. 17, the side *B A* deviates from the vertical by the amount *M N* in the vertical distance *B N*, or by the amount *A P* in the distance *B P*. Either of the ratios $\frac{MN}{B N}$ or $\frac{A P}{B P}$ expresses the batter of the

wall. A batter of 30 in 100 is the same as $\frac{30}{100}$, or .3. It will be noticed that the batter is equal to the tangent of the inclination of the side of the wall to the vertical.

SOLUTION. -(a) As just explained, tan ABP = batter = .3; whence $ABP = 16^{\circ} 41' 58''$. The triangle ABP gives,

$$w_1 = \frac{BP}{\cos ABP} = \frac{95}{\cos 16^\circ 41' 58''} = 99.182 \text{ ft. Ans.}$$

(b) The triangle APB gives,

$$AP = PB \tan ABP = 95 \times .3 = 28.5$$
 ft.

From the figure,

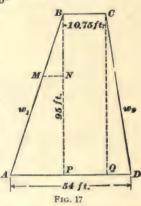
QD = AD - AP - PQ = 54 - 28.5 - 10.75 = 14.75 ft. The triangle *COD* gives,

batter of
$$CD = \tan Q CD = \frac{QD}{QC} = \frac{14.75}{95} = .15526$$

or, say, 15.5 in 100; also, $QCD = 8^{\circ} 49' 31''$. Ans.

(c)
$$w_s = \frac{CQ}{\cos Q CD} = \frac{95}{\cos 8^{\circ} 49' 31''} = 96.139$$
 ft. Ans.

EXAMPLE 6.—Fig. 18 represents a derrick; the dimensions being as shown, determine: (a) the inclination A of the boom QR to the vertical; (b) the inclination M of the rod PR to the vertical; (c) the point U at which the guy rope PU must be tied, that it may make an angle of 60° with the horizontal; (d) the length PU of the guy rope.



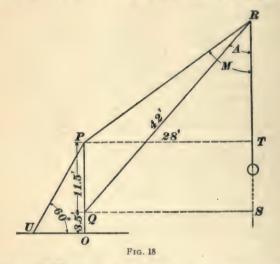
SOLUTION.—(a) The triangle RQS gives,

 $\sin A = \frac{QS}{QR} = \frac{28}{42} = \frac{2}{3}$; whence, $A = 41^{\circ} 48' 38''$. Ans.

(b) The same triangle gives,

 $RS = \sqrt{(42 + 28)} (42 - 28) = \sqrt{70 \times 14} = 31.305$ The triangle *PTR* gives,

RT = RS - ST = RS - QP = 31.305 - 11.5 = 19.805 ft.



 $\tan M = \frac{PT}{RT} = \frac{28}{19.805}$; whence, $M = 54^{\circ} 43' 38''$. Ans.

(c) In the triangle POU,
 OU = OP cot 60° = 15 cot 60° = 8.660 ft. Ans.
 (d) In the same triangle,

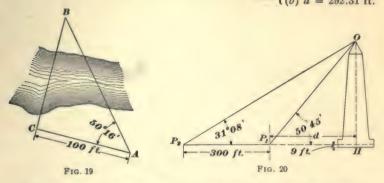
 $P U = \frac{O P}{\sin 60^\circ} = \frac{15}{\sin 60^\circ} = 17.320$ ft. Ans.

EXAMPLES FOR PRACTICE

1. In order to determine the distance CB, Fig. 19, across an intervening stream, a line CA, at right angles to CB, was measured; the angle CAB was also measured, and found to be 50° 16′. If CA = 100 feet, what is the distance CB? Ans. CB = 120.31 ft.

2. A ship was observed from the top of a lighthouse under an angle of depression of 50°; if the top of the lighthouse is 250 feet above sea level, what was the horizontal distance of the ship from the lighthouse? Ans. 209.78 ft.

3. From two points P_1 , P_2 , Fig. 20, assumed to be on the same horizontal line, the angles of elevation of the top O of a column were found to be as shown. If $P_1 P_2 = 300$ feet, and the points P_1 and P_2 are 9 feet higher than the base of the column, find: (a) the height h(= OH) of the column; (b) the horizontal distance d from P_1 to the **axis** of the column. Ans. $\begin{cases} (a) \ h = 366.77 \ \text{ft.} \\ (b) \ d = 292.31 \ \text{ft.} \end{cases}$



5. The face A B, Fig. 17, and back C D of a dam 80 feet high are to have a batter of 26 and 12 in 100, respectively; if the base A D is to be 45 feet wide, find: (a) the angles A and D

at the base; (b) the width B C of the top.

Ans. $\begin{cases} (a) \ A = 75^{\circ} 25' 33'', D = 83^{\circ} 9' 26'' \\ (b) \ B \ C = 14.6 \text{ ft.} \end{cases}$

6. Show that the base of an isosceles triangle is equal to twice one of the equal sides multiplied by the sine of one-half the vertical angle (angle opposite base).

7. A railroad curve A B C, Fig. 21, radius 1,500 feet, subtends a central angle of 49° 13'. (a) Find the length of the chord A C. (b)

A 4973' 00 Fra. 21

What will be the error in taking the length of the chord for the length of the arc? (Determine the latter length by the rules of geometry).

th by the rules of geometry). Ans. $\begin{cases} (a) \ \mathcal{A} \ C = 1,249.2 \text{ ft.} \\ (b) \ 39.3 \text{ ft.} \end{cases}$



PLANE TRIGONOMETRY

(PART 2)

Serial 779B

Edition 1

LOGARITHMIC FUNCTIONS OF SMALL ANGLES

1. Angles less than 3° are of comparatively rare occurrence in practice. When, however, they do occur, and they contain odd seconds, their logarithmic sines, tangents, and cotangents cannot be accurately determined by the general formulas and rules given in *Plane Trigonometry*, Part 1. These functions are found from a special table, which covers the first three pages of the general table of logarithmic functions furnished with this Course. These pages differ from the others in several respects, namely:

(a) The column of seconds on the left, marked " at the top, gives the total number of seconds in all angles between 0° and 3° , at intervals of 1 minute. Thus, on page 43, the number 6,360 in the column of seconds is horizontally opposite 46 in the minute column, and is, therefore, the total number of seconds in 1° 46'.

(b) The column headed S T, between the sine and the tangent column, contains the values of log tan $A - \log A''$, and log sin $A - \log A''$ for all values of A between 0° and 3°, varying from minute to minute; A'' is the total number of seconds in the angle A. The first four figures of these differences are common to the tangent and the sine and are printed near the head of the column; the other two figures are printed under S for the sine and under T for the tangent. The two figures corresponding to any angle are horizontally opposite the total number of seconds in the

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angle, this total number of seconds being given in the lefthand column. Thus, for $1^{\circ} 45'$ (= 6,300"), the value of S, or of log sin $1^{\circ} 45' - \log 6,300$, is $\overline{6}.68551$; and the value of T, or of log tan $1^{\circ} 45' - \log 6,300$, is $\overline{6}.68571$.

(c) Next to the cotangent column, there is a column marked C, containing the values of -T. The first four figures of these values are common to all angles between 0° and 3° , and are printed but once; the other two are printed horizontally opposite the number of seconds in the corresponding angles. Thus, for $1^{\circ} 51'$ (= 6,660"), the value of C is 5.31427. The values of S, T, and C will here be referred to as corrections.

2. To Find the Logarithmic Sine or Tangent of an Angle Between 0° and 3° .—If there are no odd seconds in the angle, the logarithm may be at once taken from the table, as in *Plane Trigonometry*, Part 1. Here it will be assumed that the angle contains a number of odd seconds. Let the angle be denoted by A, and the total number of seconds in it by A''; that is, let A'' be the angle reduced to seconds. (See Art. 1.)

Rule. - Open the table at the page headed by the number of degrees in the given angle. Look in the minute column for the number of minutes nearest (whether greater or less) to the number of odd minutes and seconds in the given angle. (Thus, if the given angle is 2° 36' 40", look for 2° 37'; if the given angle is 2° 36' 21", look for 2° 36'.) Take from the column headed ST the correction horizontally opposite the number of minutes found as just described, using the correction under S for the sine, and that under T for the tangent. Look in the column of seconds at the left of the page for the number horizontally opposite the number of minutes in the given angle, and to it add the number of odd seconds in that angle. The result will be the total number of seconds (A") in the given angle. Find the logarithm of this number of seconds from the table of logarithms of numbers. Add to this logarithm the correction found as above. The result will be the required logarithmic sine or tangent, according to the correction used.

EXAMPLE 1.—To find the logarithmic sine of $1^{\circ} 3' 45'' (= A)$.

SOLUTION.—Opening the table at page 43 (headed 1°), we look for 4' in the minute column, since 3' 45" is nearer to 4' than to 3'. Horizontally opposite 4, and in the column headed S T, the sine correction $\overline{6.68555}$ (= S) is found. We now look in the minute column for the number of minutes (3) in the given angle; horizontally opposite it in the left-hand column is the number 3,780, number of seconds in 1° 3'; adding 45", we obtain 3,825 (= $A^{"}$) for the total number of seconds in the given angle.

> log $A'' = \log 3,825 = 3.58263$ $S = \overline{6.68555}$ log sin $A = \overline{2.26818}$ log sin 1° 3' 45'' = $\overline{2}.26818$. Ans.

that is,

that is.

EXAMPLE 2.- To find the logarithmic tangent of 2° 36' 17".

Solution.—On page 44, the correction for the tangent, opposite 36', is $\overline{6.68587}$ (= T). Number of seconds opposite 36' in the left-hand column, 9,360; A'' = 9,360 + 17 = 9,377.

$$\log 9,377 = 3.97206$$
$$T = \overline{6.68587}$$
$$\log \tan 2^{\circ} 36' 17'' = \overline{2.65793}. \text{ Ans.}$$

3. To Find the Logarithmic Cotangent of an Angle Between 0° and 3°.

Rule.—Find C, A", and log A" exactly as in the last article, C being taken from the correction column next to the cotangent column. Subtract log A" from C. The result will be the required logarithmic cotangent.

EXAMPLE.-To find the logarithmic cotangent of 1° 52' 37".

SOLUTION.—On page 43, the correction under C, and horizontally opposite 53', is 5.31427; A'' = 6,720 + 37 = 6,757.

C = 5.31427log $A'' = \log 6,757 = 3.82975$ $C - \log A'' = 1.48452$ log cot 1° 52' 37'' = 1.48452. Ans.

4. To Find the Logarithmic Tangent, Cosine, or otangent of an Angle Between 87° and 90°.—These

Cotangent of an Angle Between 87° and 90° .—These functions also are to be taken from the first three pages of the table of logarithmic functions. The simplest way to proceed is to subtract the angle from 90° and look for the

corresponding complementary function as explained in Arts. 2 and 3. Thus, log cos $88^{\circ} 55' 38''$ is obtained by looking for log sin $(90^{\circ} - 88^{\circ} 55' 38'') = \log \sin 1^{\circ} 4' 22''$.

EXAMPLES FOR PRACTICE

1.	Find the logarithmic sine of 1° 6' 19".	Ans.	2.28532
2.	Find the logarithmic sine of 0° 2' 41".	Ans.	4.89240
3.	Find the logarithmic tangent of 2° 56' 57".	Ans.	2.71196
4.	Find the logarithmic cotangent of 1° 30' 18".	Ans.	1.58049
5.	Find the logarithmic cosine of 88° 50' 49".	Ans.	2.30370
6.	Find the logarithmic tangent of 89° 3' 9".	Ans.	1.78151
7.	Find the logarithmic cotangent of 88° 0' 25".	Ans.	2.54157

5. To Find the Angle Corresponding to a Given Logarithmic Function, When the Function Lies Between Two of the Functions in the First Three Pages of the Table.—I. Sine and Tangent.—As explained in Art. 1, $\log \sin A = S + \log A''$; therefore,

 $\log A'' = \log \sin A - S \quad (1)$

Likewise, when $\log \tan A$ is given,

 $\log A'' = \log \tan A - T \qquad (2)$

From these formulas is derived the following

Rule.—Find in the table the logarithm nearest to the given one. Take the correction horizontally opposite this logarithm, and subtract it from the given logarithm. The result will be the logarithm of the total number of seconds (A") in the given angle. Find the number corresponding to this logarithm, and reduce it to degrees, minutes, and seconds.

It is here assumed that the given function lies between two functions in the column marked log sin or log tan, as the case may be, at the top. If the names of the functions are at the bottom, the sine should be treated as in *Plane*

Trigonometry, Part 1; the tangent should be treated as if it were a cotangent, according to the directions to be given presently, and when the angle corresponding to that cotangent is found, it should be subtracted from 90° .

II. Cotangent.—Since log cot $A = C - \log A''$ (Art. 3), we have

$$\log A'' = C - \log \cot A \qquad (3)$$

From this formula is derived the following

Rule.—Find in the table the logarithmic function nearest the given cotangent. Take from the C column the correction horizontally opposite the logarithm just found, and from it subtract the given logarithmic cotangent. The result will be the logarithm of the total number of seconds in the angle.

Here, as before, it is assumed that the given cotangent lies between two of those marked log cot at the top. If it lies between two logarithms in the column marked log cot at the bottom, it should be treated as if it were a tangent, and having found the angle corresponding to this tangent, it should be subtracted from 90° to obtain the required angle.

III. Cosine.

Rule.—If the given cosine lies between two of those in the column headed log cos, apply the general rule given in Plane Trigonometry, Part 1. If it lies between two of the logarithms in the column marked log cos at the bottom, treat it as if it were a sine, find the angle corresponding to that sine as above, and subtract the result from 90°.

EXAMPLE 1.—To find the angle whose logarithmic tangent is 2.32803.

Solution.—The logarithmic tangent nearest to $\overline{2}$.32803 is $\overline{2}$.32711, found in the column headed log tan on page 43. The *T* correction horizontally opposite $\overline{2}$.32711 is $\overline{6}$.68564.

 $\log \tan A = \overline{2.32803} \\ T = \overline{6.68564} \\ \log A'' = \overline{3.64239}$

From the table of logarithms of numbers,

 $A'' = 4,389'' = 1^{\circ} 13' 9''$. Ans.

EXAMPLE 2.—To find the angle whose logarithmic cotangent is 2.49567.

1 L T 36F-12

SOLUTION.—The nearest logarithmic cotangent found in the table is 2.49488. The number opposite this logarithm in the C column is 5.31442.

$$C = 5.31442$$

log cot $A = 2.49567$
log $A'' = 2.81875$;
 $A'' = 659'' = 0^{\circ} 10' 59''$, Ans.

NOTE.-Angles are here given to the nearest whole second.

EXAMPLE 3.—To find the angle whose logarithmic cosine is 2.63723.

SOLUTION.—The nearest logarithm, $\overline{2}.63678$, is found on page 44, in the column headed log sin. The given function is, therefore, to be treated as if it were a logarithmic sine, and the angle A, corresponding to this sine is to be subtracted from 90° to obtain the required angle A. The correction horizontally opposite $\overline{2}.63678$, in the S column, is $\overline{6}.68544$.

 $\log \sin A_{1} = \overline{2}.63723$ $S = \overline{6}.68544$ $\log A_{1}'' = \overline{3.95179};$ $A_{1} = 8,949'' = 2^{\circ} 29' 9''$ $A = 90^{\circ} - 2^{\circ} 29' 9'' = 87^{\circ} 30' 51''.$ Ans.

EXAMPLES FOR PRACTICE

Verify the following values:

<i>(a)</i>	$\overline{2}.17645 = \log \sin 0^{\circ} 51' 37''$	(<i>e</i>)	$\overline{2}.48790 = \log \cot 88^{\circ} 14' 19''$
(b)	$\overline{3.94316} = \log \sin 0^{\circ} 30' 10''$	(f)	$2.47608 = \log \cot 0^{\circ} 11' 29''$
(c)	$\overline{2}.65783 = \log \cos 87^{\circ} 23' 36''$	(g)	$1.31009 = \log \tan 87^{\circ} 11' 48''$
(<i>d</i>)	$\overline{2}.58349 = \log \tan 2^{\circ} 11' 41''$	(h)	$\overline{3}.95377 = \log \cos 89^{\circ} 29' 6''$

6. Use of the Column of Seconds for Obtaining the Angle Corresponding to a Given Function.—In order to avoid confusing the student by too many rules, the reduction of A'' to degrees, minutes, and seconds was, in the preceding articles, effected by the ordinary rules of arithmetic, without any reference to the table. The following is a more expeditious method:

Let the given function lie between the functions of two consecutive angles, A_1 and $A_1 + 1'$. Then, the degrees and minutes in the required angle are those in A_1 , and may be at once written down. The number in the column of seconds on the left, horizontally opposite the number of minutes in A_1 , gives the total number of seconds in A_1 . Denoting that

number by A_i'' and the number of odd seconds in the required angle by s, we have $s = A'' - A_i''$

EXAMPLE.—To find the angle whose logarithmic tangent is $\overline{2.30217}$. SOLUTION.—The given function lies between $\overline{2.29629}$ and $\overline{2.30263}$. The angle corresponding to the first of these two functions is 1° 8' (= A_1); $A_1'' = 4,080''$.

> log tan $A = \overline{2}.30217$ $T = \overline{6}.68563$ log $A'' = \overline{3.61654}; A'' = 4.136$ $s = A'' - A_1'' = 4.136 - 4.080 = 56''$ $A = A_1 + s = 1^{\circ} 8' 56''$. Ans.

The subtraction $A'' - A_1''$ can usually be effected mentally.

EXAMPLES FOR PRACTICE

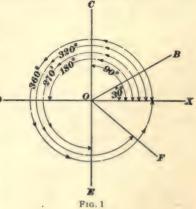
Apply the method just described to the Examples for Practice given after Art. 4.

GENERAL TRIGONOMETRIC FORMULAS

ANGLES AND THEIR TRIGONOMETRIC FUNCTIONS

7. Angle of Any Magnitude. — In trigonometry, an angle is considered as being generated by a straight line turn-

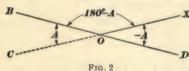
ing about one of its ends, which is the vertex of the angle. In this motion, any point in the turning line describes a circular arc, whose number of degrees is the measure of *p* the angle. The turning line is called the generating line. The position that this line occupies before it begins to turn, and from which arcs are measured, is called the initial



line, or the initial position of the generating line; and the position it occupies after turning through a certain angle

is called the final position. In Fig. 1, for example, the initial position of the generating line is OX. The turning is supposed to take place about the point O and in a direct tion opposite to that in which the hands of a clock move. When the line turns from the position OX to the final positions OB, OC, OD, OE, OF, it generates angles of 30° , 90° , 180° , 270° , 320° , respectively, as indicated or the figure. If the line makes a complete turn, so that its final position coincides with its initial position OX, the angle generated is 360° .

8. Positive and Negative Angles.—When an angle is described by a line turning in a direction contrary to that



 in which the hands of a watch move, the angle is considered positive; if described in the
 popposite direction, it is considered negative. Refer-

ring to Fig. 2, the angle XOB, whose supplement is A, may be regarded as having been described in any of the following manners:

(a) By turning the generating line about O from the position OX in the positive direction through (180 - A) degrees to the position OB.

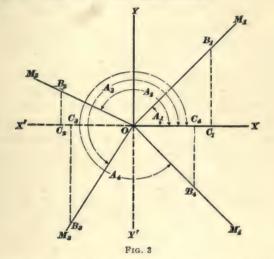
(b) By turning the generating line about O in a positive direction through an angle of 180° , when it will be in the position OC, and then turning it back from OC in the negative direction through the angle -A (negative, because turned in the negative direction) into the position OB.

(c) By turning the generating line about O in the negative direction through the angle -A, into the position OD, and then turning it back in the positive direction through 180° into the position OB.

It is to be noticed that, however the angle $(180^\circ - A)$ may be regarded as described, the resulting angle XOB is the same.

9. Quadrants.—Let OX, Fig. 3, be the initial position of the generating line, and OM_{1} , OM_{2} , OM_{3} , OM_{4} , OM_{4} , final

positions, determining, respectively, the angles A_1, A_2, A_3, A_4 , all measured from OX upwards and toward the left. Producing XO and drawing through O a perpendicular YY'to OX, the plane of the figure is divided into four right angles, called quadrants. Taking them in order, following the direction in which positive angles are reckoned, they are distinguished as follows: XOY is the first quadrant; YOX', the second quadrant; X'OY', the third quadrant; and Y'OX, the fourth quadrant.



10. Trigonometric Functions of Any Angle.—In the definitions given in *Plane Trigonometry*, Part 1, only acute angles were considered. Referring to Fig. 3, in which $B_1 C_1$ is perpendicular to OX, the trigonometric functions of the acute angle A_1 were defined by the following equations:

$\sin A_1 = \frac{\text{side opposite}}{1}$		$\tan A_1 =$	side opposite _	$B_1 C_1$
hypotenuse	$\overline{O B_1}$	tan 211 -	side adjacent	O C.
$\cos A_1 = \frac{\text{side adjacent}}{1}$		$\cot A_1 =$	side adjacent	O C1
$\cos A_1 =$ hypotenuse	$- O B_1$	cot A ₁ -	side opposite	$B_1 C_1$
$\sec A_1 = \frac{\text{hypotenuse}}{1}$	_ O B1	$\csc A_1 =$	hypotenuse	OB1
$\sec A_1 = \frac{1}{\text{side adjacent}}$	$= O C_1$	$\csc A_1 =$	side opposite	$\overline{B_1 C_1}$

These formulas serve as the definitions of the trigonometric functions of any angle; that is, the sine of any angle

is the ratio of the side opposite to the hypotenuse; the tangent is the ratio of the side opposite to the side adjacent, etc. But, in order that these definitions may be correct, it is necessary to apply to them some algebraic rules relating to signs.

In Fig. 3, the hypotenuse used for the determination of the functions of A_1 is any portion OB_1 of the side OM_1 , which is the final position of the generating line. From B_1 , a perpendicular $B_1 C_1$ is drawn on the initial line OX, thus determining the right triangle $OB_1 C_1$. The length of the perpendicular $B_1 C_1$, which is the side opposite the vertex of the angle, is the distance of B_1 above the initial line OX, and the length of the adjacent side OC_1 is the distance of the point B_1 to the right of the vertex, measured along the initial line; or, what is the same thing, OC_1 is the distance of $B_1 C_1$ from the vertex, measured toward the right.

Consider now the angle XOM_{1} , or A_{1} , in which the fina! position OM, of the generating line lies in the second quadrant. As before, the hypotenuse to be used in the definitions of the trigonometric functions of A, is any portion OB, of the side $OM_{\rm av}$ which is the final position of the generating line. As before, also, a perpendicular from B_1 is drawn on the initial line OX; but, in this case, the perpendicular falls on OX produced. In the right triangle OB, C_{3} , the perpendicular $B_1 C_1$ is the side opposite the vertex of the angle A_1 , and OC, is the side adjacent. It should be noted very particularly that the terms side opposite and side adjacent are used to describe the positions of the legs of the right triangle with reference to the vertex of the angle considered, not to the angle itself. Thus, $B_1 C_2$ is not opposite the angle A_2 . but opposite the vertex O of that angle. The length of the side opposite, $B_{1}C_{2}$, measures the distance of B_{1} above the initial line; and the length of OC_2 , or the side adjacent, measures the distance of the opposite side B, C, to the left of the vertex; or, in the language of algebra, it may be said that $-OC_{i}$ is the distance of $B_{i}C_{i}$ to the right of O.

Having defined the cosine of any angle as the ratio of the side adjacent to the hypotenuse, and the side adjacent as the

distance of the side opposite from the vertex, measured toward the right of the vertex, it is necessary, when the side opposite is to the left of the vertex, to consider its distance from the vertex, or the side adjacent, as negative. This is in accordance with the general principle of algebra, that, if distances counted in one direction are treated as positive, distances in the opposite direction must be treated as negative. In the triangle OB, C_* , therefore, OC_* should be treated as negative, and therefore, the cosine of A_* is $\frac{-OC_*}{OB_*}$.

Considering now the angle A_s , the hypotenuse is, as above, any portion OB_s of the side OM_s , which is the final position of the generating line. From B_s , the perpendicular $B_s C_s$ on the initial line (produced) is drawn, and thus a right triangle is determined, in which $B_s C_s$ is the side opposite, and OC_s the side adjacent. As previously explained, OC_s should be treated as negative. The opposite side $B_s C_{s_1}$ which is the distance of B_s below the initial line, should also be treated as negative; for if distances above the initial line are treated as positive, those below the initial line must be treated as negative.

Finally, in the angle A_* , which terminates in the fourth quadrant, $O C_*$, the side adjacent, is positive, while $B_* C_*$, the side opposite, is negative.

The foregoing explanations may be summed up as follows: The side opposite is positive or negative according as the hypotenuse is above or below the initial line. The side adjacent is positive or negative according as it extends toward the right or toward the left of the vertex. The hypotenuse is always positive.

11. Algebraic Signs of the Functions.—Referring again to Fig. 3, it will be observed that, for any angle, as A_1 , terminating in the first quadrant, both the side adjacent and the side opposite, or $O C_1$ and $B_1 C_2$, are positive, and therefore all the functions are positive; for any angle, as A_2 , terminating in the second quadrant, the side adjacent, or $O C_2$, is negative, and the side opposite, or $B_2 C_2$, is positive. Therefore

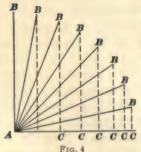
$$\sin A_{s} = \frac{+B_{s}C_{s}}{+OB_{s}}, \text{ positive} \qquad \tan A_{s} = \frac{+B_{s}C_{s}}{-OC_{s}}, \text{ negative}$$
$$\cos A_{s} = \frac{-OC_{s}}{+OB_{s}}, \text{ negative} \qquad \sec A_{s} = \frac{+OB_{s}}{-OC_{s}}, \text{ negative}$$
$$\csc A_{s} = \frac{+OB_{s}}{+B_{s}C_{s}}, \text{ positive}$$

The signs of the functions of angles terminating in the third and in the fourth quadrant are similarly determined. The results are tabulated below.

	Quadrant						
Function	First	Second	Third	Fourth			
	Sign of Function						
Sine	+ + + + + + + + + + + + + + + + + + + +	+ + +	+ +	-+-+-			

TABLE I

12. Trigonometric Functions of 0° and 90° .—In the right triangles ACB, Fig. 4, the hypotenuse AB may



be taken to have any value whatever. It is evident that BC, the side opposite, decreases as the angle CAB decreases, and becomes zero when the angle becomes zero; and that BC coincides with the hypotenuse AB when the angle CAB is 90°. Again, AC, the adjacent side, increases as c c c c c the angle decreases, and is equal to the hypotenuse AB when the angle

CAB is 0°. Also, AC becomes zero when CAB is 90°. Now, from the definitions of the trigonometric functions,

$$\sin CAB = \frac{\text{side opposite}}{\text{hypotenuse}}, \text{ whence} \begin{cases} \sin 0^\circ = \frac{0}{AB} = 0\\ \sin 90^\circ = \frac{AB}{AB} = 1 \end{cases}$$
$$\cos CAB = \frac{\text{side adjacent}}{\text{hypotenuse}}, \text{ whence} \begin{cases} \cos 0^\circ = \frac{AB}{AB} = 1\\ \cos 90^\circ = \frac{0}{AB} = 0 \end{cases}$$

In like manner,

$$\tan 0^{\circ} = \frac{0}{AC} = 0 \qquad \tan 90^{\circ} = \frac{BC}{0} = \infty$$
$$\cot 0^{\circ} = \frac{AC}{0} = \infty \qquad \cot 90^{\circ} = \frac{0}{CB} = 0$$

NOTE.—The cotangent of CAB is equal to $\frac{CA}{CB}$. Now, as the angle decreases, the side CB becomes less and less, and it is evident that, as the denominator of a fraction becomes less and less, the numerator remaining the same, the value of the fraction increases. As the denominator decreases indefinitely, the value of the fraction exceeds any known quantity, however great, it is said to be infinite. The sign ∞ is used to express an infinite number.

13. Functions of $(180^{\circ} - A)$.—Let XOM, Fig. 5, be any angle, and A (= MOX') its supplement. Draw OM' making with OX an angle equal to A, as shown. Take any part OB of OM for the hypotenuse, and draw BC perpendicular to OX produced: draw BB' parallel to Fig. 5

OX, and B'C' perpendicular to OX. Then, BC = B'C'; OB = OB'; OC = -OC' (Art. 10); and, by the definitions of the functions,

$$\sin XOM = \frac{BC}{OB} = \frac{B'C'}{OB'} = \sin A$$

$$\cos XOM = \frac{OC}{OB} = \frac{-OC'}{OB'} = -\cos A$$

that is,

 $\sin(180^\circ - A) = \sin A$ (1)

٠

 $\cos(180^\circ - A) = -\cos A$ (2)

. . .

Similarly, $\tan (180^\circ - A) = -\tan A$ (3) $\cot (180^\circ - A) = -\cot A$ (4)

These relations are especially useful for finding the logarithmic functions of angles greater than 90°, since these functions are arithmetically equal to those of the supplements of the angles; that is, when signs are disregarded, any function cf an angle and that of its supplement are equal. For example, $\sin 105^\circ = \sin (180^\circ - 105^\circ) = \sin 75^\circ$; $\cos 105^\circ = -\cos (180^\circ - 105^\circ) = -\cos 75^\circ$.

14. Functions of $(90^{\circ} + A)$.—By formula 1 of Art. 13, sin $(90^{\circ} + A) = \sin [180^{\circ} - (90 + A)] = \sin (90^{\circ} - A)$ or, since sin $(90^{\circ} - A) = \cos A$,

$$\sin \left(90^\circ + A\right) = \cos A \tag{1}$$

The following formulas may be derived in a similar manner:

$\tan\left(90^\circ + A\right) = -\cot A$	(2)
$\cos\left(90^\circ + A\right) = -\sin A$	(3)
$\cot\left(90^\circ + A\right) = -\tan A$	(4)

15. Functions of Negative Angles.—The complement of an angle is the algebraic difference between the angle and 90°. If the angle is greater than 90°, its complement is negative. Thus, the complement of 95° is 90° - 95° $= -5^{\circ}$. The cofunctions of an angle are the corresponding fundamental functions of its complement, whether that complement be positive or negative. Thus, $\cos 85^{\circ} = \sin (90^{\circ} - 85^{\circ}) = \sin 5^{\circ}$; $\cos 95^{\circ} = \sin (90^{\circ} - 95^{\circ}) = \sin (-5^{\circ})$. Similarly, $\sin 95^{\circ} = \cos (90^{\circ} - 95^{\circ}) = \cos (-5^{\circ})$. It is, therefore, necessary to know how to determine the functions of negative angles.

If $90^{\circ} + A$ is any angle, its complement is $90^{\circ} - (90^{\circ} + A) = -A$; and, therefore,

 $\cos (90^\circ + A) = \sin (-A), \cot (90^\circ + A) = \tan (-A)$ $\sin (90^\circ + A) = \cos (-A), \tan (90^\circ + A) = \cot (-A)$

.

whence, replacing the values of $\cos (90^\circ + A)$, $\cot (90^\circ + A)$, etc. from the preceding article,

$\sin\left(-A\right)=-\sin A$	(1)
$\tan\left(-A\right)=-\tan A$	(2)
$\cos\left(-A\right)=\cos A$	(3)
$\cot\left(-A\right)=-\cot A$	(4)

ADDITION OF ANGLES

16. To Express the Sine or Cosine of the Sum or Difference of Two Angles in Terms of the Sine and Cosine of the Angles.—The following formulas are fundamental; being of frequent occurrence, they are very important, and should be committed to memory:

sin	(A +	B)	=	sin	A	cos	B	+	cos	A	sin	B	(1)
cos	(A +	R)	=	cos	A	cos	R	_	sin	A	sin	R	(2)

- $\sin (A B) = \sin A \cos B \cos A \sin B$ (3)
- $\cos (A B) = \cos A \cos B + \sin A \sin B$ (4)

NOTE.—The derivation of these formulas is given in the Appendix at the end of this Section, under the Roman numeral I. That Appendix contains this and a few other demonstrations that are comparatively laborious and may be found irksome by some. They are not essential to the understanding of the formulas, and the student is not required to learn them. He is, however, advised to peruse them carefully, as they are good exercises in the handling and transforming of both algebraic and trigonometric expressions.

These formulas are not used, as they seem to imply, to determine the sine or the cosine of the sum or difference of two angles, when the sine and cosine of those angles are given. They can be used for this purpose, but there would be no advantage in so doing. Their main value consists in their application to transforming complicated trigonometric expressions into simpler ones. The student will often have occasion to employ them in this manner. In order that he may have an idea of this application of the formulas, two examples are given here.

EXAMPLE 1.—To determine the angle A from the relation $\frac{\sin(A + 28^\circ)}{\sin A} = .95$

SOLUTION.—Applying formula 1, we have $\frac{\sin (A + 28^{\circ})}{\sin A} = \frac{\sin A \cos 28^{\circ} + \cos A \sin 28^{\circ}}{\sin A}$ $= \frac{\sin A \cos 28^{\circ}}{\sin A} + \frac{\cos A \sin 28^{\circ}}{\sin A} = \cos 28^{\circ} + \cot A \sin 28^{\circ}$

replacing $\frac{\cos A}{\sin A}$ by its equal $\cot A$ (see *Plane Trigonometry*, Part 1). Substituting this value of the quotient $\frac{\sin (A + 28^{\circ})}{\sin A}$ in the given equation, we have,

whence
$$\cot A = \frac{.95 - \cos 28^{\circ}}{\sin 28^{\circ}} = \frac{.95 - .88295}{.46947} = .14282$$

and, therefore, $A = 81^{\circ} 52' 19''$. Ans.

EXAMPLE 2.—To transform the expression $\tan A + \tan B$ into the expression $\frac{\sin (A + B)}{\cos A \cos B}$.

Note.—Transformations of this kind are very often useful, when logarithms are employed. Thus, if $\tan A + \tan B$ were to be multiplied by 39.578, it would be necessary first to find the natural tangent of A, then that of B, add the two together, take the logarithm of the sum thus obtained, and add this logarithm to that of 39.578. It. however, the expression $\frac{\sin (A + B)}{\cos A \cos B}$ is used, the logarithms of $\sin (A + B)$, $\cos A$ $\cos B$ can be taken from the table, and the operation performed without having recourse to natural functions, which are often inconvenient.

SOLUTION.—We have (*Plane Trigonometry*, Part 1),

$$\tan A + \tan B = \frac{\sin A}{\cos A} + \frac{\sin B}{\cos B} = \frac{\sin A \cos B + \cos A \sin B}{\cos A \cos B}$$

According to formula 1, the numerator of this last fraction is equal to $\sin (A + B)$. Therefore,

$$\tan A + \tan B = \frac{\sin (A+B)}{\cos A \cos B}$$
. Ans.

17. Sine and Cosine of 2 A and of $\frac{1}{2}$ A.—From the formulas for the sine and cosine of the sum of two angles, the following are deduced:

si	n 2	A	=	$2 \sin A \cos A$	(1)
co	os 2	A	-	$\cos^* A - \sin^* A$	(2)
cc	os 2	A	=	$1-2\sin^{\circ}A$	(3)
cc	os 2	A	=	$2\cos^{\circ}A-1$	(4)
	sin	A	=	$2\sin\frac{1}{2}A\cos\frac{1}{2}A$	(5)

16

cos	A	-	$\cos^* \frac{1}{2} A - \sin^* \frac{1}{2} A$	(6)
cos	A	=	$1 - 2 \sin^2 \frac{1}{2} A$	(7)
cos	A	-	$2\cos^{2}\frac{1}{2}A-1$	(8)

As in the case of formulas 1 to 4, Art. 16, these formulas are used mainly for the purposes of transformation. They are very simply derived as follows:

When B is made equal to A, formula 1, Art. 16, becomes $\sin (A + A) = \sin A \cos A + \cos A \sin A$

that is, $\sin 2 A = 2 \sin A \cos A$

Similarly, formula 2, Art. 16, becomes

 $\cos (A + A) = \cos A \cos A - \sin A \sin A$ that is, $\cos 2 A = \cos^* A - \sin^* A$

Formula 3 follows from this, by writing $1 - \sin^2 A$ instead of $\cos^2 A$ (since $\sin^2 A + \cos^2 A = 1$); and formula 4, by writing $1 - \cos^2 A$ instead of $\sin^2 A$.

Formulas 1 to 4 give the sine and cosine of twice any angle in terms of the sine and cosine of the angle. If the angle is denoted by $\frac{1}{2}A$, twice the angle will be A, and formulas 1 to 4 take the forms of formulas 5 to 8.

OBLIQUE TRIANGLES

FUNDAMENTAL PRINCIPLES

NOTE.-For the general method of marking and naming the sides and angles of a triangle, see *Plane Trigonometry*, Part 1.

18. Principle of Sines.—In any triangle, the sides are proportional to the sines of the opposite angles. That is,

 $\frac{a}{b} = \frac{\sin A}{\sin B}, \ \frac{a}{c} = \frac{\sin A}{\sin C}, \ \frac{b}{c} = \frac{\sin B}{\sin C}$

Let ABC, Fig. 6, be any triangle and p the perpendicular from C on the opposite side. Then, in (a), the right triangles ACD and BCD give, respectively,

$$p = b \sin A, p = a \sin B$$

whence, putting the two values of p equal to each other, $a \sin B = b \sin A$ and, therefore, dividing by $b \sin B$,

 $\frac{a}{b} = \frac{\sin A}{\sin B}$

In (b), the right triangles A CD and B CD give, respectively, whence, $p = b \sin A, p = a \sin CBD$ $a \sin CBD = b \sin A$

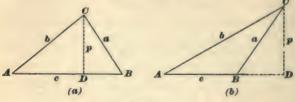


FIG. 6

But, as $CBD = 180^{\circ} - B$, we may write sin B instead of sin CBD (Art. 13), and, therefore,

 $a \sin B = b \sin A$

whence, as before,

 $\frac{a}{b} = \frac{\sin A}{\sin B} \qquad (1)$

By drawing a perpendicular from B on A C, and reasoning in the same manner, it may be shown that

a	_	sin A	(2)
C	-	sin C	(4)
Ь	_	sin B	
c	-	sin C	

Similarly,

By transforming equation (1), we obtain

$$\frac{a}{\sin A} = \frac{b}{\sin B}$$

and by a similar transformation of equation (2),

$$\frac{a}{\sin A} = \frac{c}{\sin C}$$

We have, therefore,

$$\frac{a}{\sin A} = \frac{b}{\sin B} = \frac{c}{\sin C}$$

The principle of sines may, then, be stated in this form: In every triangle, the quotient obtained by dividing the length of any side by the sine of the opposite angle is the same, whatever the side taken.

This quotient is called the modulus of the triangle, and will here be denoted by M. The modulus can be found when any of the sides and the opposite angle are known.

The principle of sines is one of the most important in trigonometry, and both forms in which it is stated in this article should be committed to memory.

19. The Cosine Principle.—In any triangle, the square of one side is equal to the sum of the squares of the other two sides minus twice the product of these two sides and the cosine of their included angle. That is (Fig. 6),

> $a^{*} = b^{*} + c^{*} - 2 b c \cos A$ $b^{*} = a^{*} + c^{*} - 2 a c \cos B$ $c^{*} = a^{*} + b^{*} - 2 a b \cos C$

These formulas are derived in Appendix II.

20. Principle of Tangents.—The sum of any two sides of a triangle is to their difference as the tangent of half the sum of the opposite angles is to the tangent of half their difference. That is (Fig. 6),

 $\frac{a+b}{a-b} = \frac{\tan\frac{1}{2}(A+B)}{\tan\frac{1}{2}(A-B)}$

The derivation of this formula is given in Appendix III. The student should have no difficulty in committing the formula to memory, as its symmetry makes it very easy to remember.

SOLUTION OF OBLIQUE TRIANGLES

21. The solution of oblique triangles is treated under four cases:

Case I: Given Two Sides and the Included Angle. Let a, b, and C, Fig. 6, be given and A, B, and c be required. Of the two methods given below, the first is preferable in most cases.

First Method.—From the formula in Art. 20, the following is readily derived:

$$\tan \frac{1}{2}(A-B) = \frac{a-b}{a+b} \tan \frac{1}{2}(A+B)$$
 (1)

Now, since $A + B + C = 180^{\circ}$, we have also, $A + B = 180^{\circ} - C$; and $\frac{1}{2}(A + B) = \frac{1}{2}(180^{\circ} - C)$ $= 90^{\circ} - \frac{1}{2}C$

Therefore, $\frac{1}{2}C$ is the complement of $\frac{1}{2}(A + B)$, and hence, tan $\frac{1}{2}(A + B) = \cot \frac{1}{2}C$. Substituting this value in equation (1), the following formula is derived:

$$\tan \frac{1}{2}(A - B) = \frac{a - b}{a + b} \cot \frac{1}{2}C \qquad (1)$$

If the student remembers the formula in Art. 20, or the principle of tangents, he will have no difficulty in remembering this formula, which is derived from the formula in Art. 20, by simply writing $\cot \frac{1}{2}C$ instead of $\tan \frac{1}{2}(A + B)$.

From this formula $\frac{1}{2}(A - B)$ can be found. Let this value of $\frac{1}{2}(A - B)$ be denoted by D. We have also, as explained above, $\frac{1}{2}(A + B) = \frac{1}{2}(180^\circ - C) = 90^\circ - \frac{1}{2}C$.

$$\frac{1}{2}(A+B) = 90^{\circ} - \frac{1}{2}C$$
(2)

$$\frac{1}{2}(A-B) = D$$
(3)

Adding equations (2) and (3) gives $A = (90^{\circ} - \frac{1}{2}C) + D$

Subtracting equation (3) from (2) gives

$$B = (90^{\circ} - \frac{1}{2} C) - D$$

Knowing A and B, the side c may be found from the relation (Art. 18),

$$\frac{c}{\sin C} = \frac{a}{\sin A}$$
, which gives $c = \frac{a \sin C}{\sin A}$

It is, however, more convenient to find c from the following formula, the derivation of which is given in Appendix IV:

$$c = \frac{(a-b)\cos\frac{1}{2}C}{\sin\frac{1}{2}(A-B)}$$
 (2)

It will be noticed that, for calculating $\tan \frac{1}{2}(A-B)$, the logarithms of (a-b) and $\cot \frac{1}{2}C$ have to be found. The logarithm of $\cos \frac{1}{2}C$ may be taken out of the table at the same time as that of $\cot \frac{1}{2}C$. Also, when the angle $\frac{1}{2}(A-B)$ is taken from the table, its logarithmic sine should be taken at the same time. This greatly simplifies the application of formula 2.

Second Method.—The third side c can be found directly from the formula in Art. 19, which gives

$$c = \sqrt{a^2 + b^2} - 2 \ a \ b \cos C$$

Then, by the principle of sines,

$$\sin A = \frac{a \sin C}{c}, \sin B = \frac{b \sin C}{c}$$

This method is of value when the only required part is the side c, especially if a and b are convenient numbers to square.

EXAMPLE 1.—In a triangle, a = 17 feet, b = 12 feet, and the included angle $C = 59^{\circ} 23'$. To find the other parts of the triangle.

Solution.—Here $\frac{1}{2} C = 29^{\circ} 41' 30''$; a + b = 17 + 12 = 29, and a - b = 17 - 12 = 5. Then, by the first method,

$$\tan \frac{1}{4} (A - B) = \frac{5}{29} \times \cot 29^{\circ} 41' 30''$$

 $\log 5 = .69897$ $\log 5 = .69897$ $\log 29 = 1.46240$ $\log \cos 29^{\circ} 41' 30'' = \overline{1.93887}$ 1.23657 .63784 $\log \cot 29^{\circ} 41' 30'' = .24397$ $\log \sin D = \bar{1}.46154$ $\log \tan \frac{1}{2}(A-B) = \overline{1}.48054$ $\log c = 1.17630$ $D = \frac{1}{2}(A - B) = 16^{\circ} 49' 25'';$ c = 15.007. Ans. $A = (90^{\circ} - 29^{\circ} 41' 30'') + 16^{\circ} 49' 25'' = 77^{\circ} 7' 55''$. Ans. $B = (90^{\circ} - 29^{\circ} 41' 30'') - 16^{\circ} 49' 25'' = 43^{\circ} 29' 5''.$ Ans. EXAMPLE 2.—Given a = 10, b = 15, and $C = 60^{\circ}$; to find c. SOLUTION.-By the second method,

> $c = \sqrt{10^{\circ} + 15^{\circ} - 2 \times 10 \times 15 \cos 60^{\circ}}$ = $\sqrt{325 - 300 \times .5} = \sqrt{175} = 13.229$ ft. Ans.

EXAMPLES FOR PRACTICE

1. Given a = 37.46 feet, b = 59.17 feet, and $C = 69^{\circ} 13'$; find A, B, and c. Ans. $\begin{cases} A = 37^{\circ} 21' 30'' \\ B = 73^{\circ} 25' 30'' \\ c = 57.72 \text{ ft.} \end{cases}$

2. Two sides of a triangle are, respectively, 687.64 and 319.58 feet long, and their included angle is 47° 15' 8"; find the other two angles and the third side. Ans. {Angles, 106° 14' 56" and 26° 29' 56" Third side = 525.97

3. Given
$$c = 4$$
 chains, $a = 6$ chains, and $B = 45^{\circ}$ 18'; find b.
Ans. $b = 4.271$ ch.

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4. Given b = 43.16 chains, c = 51.29 chains, and $A = 35^{\circ} 8' 10''$; find B, C, and a. Ans. $\begin{cases} B = 57^{\circ} 13' 20'' \\ C = 87^{\circ} 38' 30'' \\ a = 29.544 \text{ ch.} \end{cases}$

22. Case II: Given a Side and Two Angles.—Let c, A, and B be known, to find a, b, and C. The angle $C = 180^{\circ} - A - B$. By the principle of sines,

$$\frac{a}{\sin A} = \frac{c}{\sin C} \text{ whence } a = \frac{c}{\sin C} \sin A$$

Similarly,
$$b = \frac{c}{\sin C} \sin B$$

Since $\frac{c}{\sin C}$ is the modulus of the triangle (Art. 18), these formulas may be thus stated: Any side of a triangle is equal to the modulus of the triangle multiplied by the sine of the angle opposite that side.

EXAMPLE.—Given a = 98.48, $B = 60^{\circ} 45'$, and $C = 39^{\circ} 15'$; to find b, c, and A.

Solution. $A = 180^{\circ} - (60^{\circ} 45' + 39^{\circ} 15') = 80^{\circ}$. Ans.

 $M = \frac{98.48}{\sin 80^\circ}; \ b = \frac{98.48}{\sin 80^\circ} \sin 60^\circ 45'; \ c = \frac{98.48}{\sin 80^\circ} \sin 39^\circ 15'$ log 98.48 = 1.99335 log sin 80° = <u>1.99335</u> log M = <u>2.00000</u> log Sin 60° 45' = <u>1.94076</u> log M = <u>2.00000</u> log Sin 60° 45' = <u>1.94076</u> log M = <u>2.00000</u> log Sin 39° 15' = <u>1.80120</u> log c = <u>1.80120</u>; c = 63.27. Ans.

NOTE.—Attention is called to the convenient way in which the work is here arranged. Having determined log *M*, this logarithm is copied, and then one of the logarithms to be added to it is written above it, the other under it, the addition being performed upwards in one case, and downwards in the other.

EXAMPLES FOR PRACTICE

1. Given a = 45.39 feet, $B = 38^{\circ} 12'$, and $C = 11^{\circ} 11' 34''$; find *A*, *b*, and *c*. Ans. $\begin{cases} A = 130^{\circ} 36' 26'' \\ b = 36.973 \text{ ft.} \\ c = 11.605 \text{ ft.} \end{cases}$ 2. Given c = 101.11 chains, $C = 55^{\circ} 55' 55''$, and $A = 10^{\circ} 10' 10''$; find *B*, *a*, and *b*. $\begin{cases} B = 113^{\circ} 53' 55'' \\ a = 21.551 \text{ ch.} \\ b = 111.59 \text{ ch.} \end{cases}$ 23. Case III: Given Three Sides.—Let a, b, and c be given, to find A, B, and C.

First Method.—The angles can be found directly from the cosine formulas (Art. 19), which, being solved for $\cos A$, $\cos B$, and $\cos C$, respectively, give

$$\cos A = \frac{b^{*} + c^{*} - a^{*}}{2 b c}$$

$$\cos B = \frac{a^{*} + c^{*} - b^{*}}{2 a c}$$

$$\cos C = \frac{a^{*} + b^{*} - c^{*}}{2 a b}$$
(1)

These formulas are to be used when the numbers a, b, care convenient to square; otherwise, they are too cumbersome, and those given below for the functions of half the angles should be employed. It is necessary to apply the formulas in determining only two of the angles, as the third follows from the relation $A + B + C = 180^{\circ}$. As a check, however, the formulas should be applied to the third angle also.

It should be borne in mind that, if the cosine of an angle is found to be negative, this implies that the angle is obtuse (Art. 13). In such case, the cosine is treated as positive, and the corresponding angle taken from the table is subtracted from 180° to obtain the required angle. Thus, if $\cos A = -.97030$, we look for the angle whose cosine is +.97030, which is 14°. Then, $A = 180^{\circ} - 14^{\circ} = 166^{\circ}$.

EXAMPLE.—Given a = 4 inches, b = 5 inches, and c = 7 inches; to find A, B, and C.

SOLUTION.— $\cos A = \frac{b^2 + c^2 - a^2}{2 b c} = \frac{5^2 + 7^2 - 4^4}{2 \times 5 \times 7} = \frac{58}{70} = .82857$, and, therefore, $A = 34^\circ 2' 53''$. Ans. $\cos B = \frac{a^2 + c^2 - b^2}{2 a c} = \frac{4^2 + 7^2 - 5^2}{2 \times 4 \times 7} = \frac{40}{56} = .71429$ and, therefore, $B = 44^\circ 24' 54''$. Ans. $C = 180^\circ - A - B = 101^\circ 32' 13''$. Ans. As a check, we have $\cos C = \frac{a^2 + b^2 - c^2}{2 a b} = \frac{4^2 + 5^2 - 7^4}{2 \times 4 \times 5} = -\frac{8}{40} = -.20000$

The angle whose cosine is .20000 is $78^{\circ} 27' 47''$. Therefore, $C = 180^{\circ} - 78^{\circ} 27' 47'' = 101^{\circ} 32' 13''$.

Second Method.—As said before, this method is to be applied when the operations required by formula 1 involve too much labor, which happens when the lengths of the given sides consist of three or more significant figures—the usual case. If the sum of the sides is denoted by 2s, or half their sum by s, the angles A, B, C may be found by the following formulas, which are derived in Appendix V:

$\tan \frac{1}{2} A = \sqrt{\frac{(s-b)(s-c)}{s(s-a)}} \\ \tan \frac{1}{2} B = \sqrt{\frac{(s-a)(s-c)}{s(s-b)}} \\ \tan \frac{1}{2} C = \sqrt{\frac{(s-a)(s-b)}{s(s-c)}} \\ \end{bmatrix}$	(2)
$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$	
$\cos \frac{1}{2} B = \sqrt{\frac{s(s-b)}{a c}}$	(3)
$\cos \frac{1}{2} C = \sqrt{\frac{s(s-c)}{a b}} \end{bmatrix}$	

For angles differing but little from 90° (say between 85° and 90°), use the cosine formulas 3; in all other cases, the tangent formulas 2.

We have also,

$$\sin \frac{1}{2} A = \sqrt{\frac{(s-b)(s-c)}{bc}}$$
 (4)

with similar formulas for $\sin \frac{1}{2} B$ and $\sin \frac{1}{2} C$. These formulas are of value for deriving the tangent formulas 2, as well as for deriving an expression for the area of a triangle when the sides are given. They may also be used instead of the tangent formulas 2 for the determination of the angles, but the latter are preferable.

EXAMPLE.—In the triangle A B C, a = 567 feet, b = 736 feet, and c = 264 feet; to find the angles A, B, and C.

Solution.-The tangent formulas will be used. To find A $\log(s - c) = 2.71559$ a =567 $\log(s - b) = 1.67669$ b = 736 c = 264 4.39228 2s = 1.567 $\log s = 2.89404$ s = 783.5 $\log(s - a) = 2.33546$ s - a = 216.55.22950 s - b = 47.5 $2)\overline{1.16278}$ s - c = 519.5T.58139 $\log \tan \frac{1}{4} A =$ $\frac{1}{4} A = 20^{\circ} 52' 38'', A = 41^{\circ} 45' 16''$. Ans. To find C To find B $\log(s-a) = 2.33546$ $\log(s-a) = 2.33546$ $\log(s - b) = 1.67669$ $\log(s-c) = 2.71559$ 5.05105 4.01215 $\log s = 2.89404$ $\log s = 2.89404$ $\log(s-c) = 2.71559$ $\log(s-b) = 1.67669$ 4.57073 5.60963 2)0.48032 $2)\overline{2}.40252$ Ī.20126 $\log \tan \frac{1}{2}B =$ 0.24016 $\log \tan \frac{1}{2}C =$ $\frac{1}{2}B = 60^{\circ} 5' 29''; B = 120^{\circ} 10' 58''$ $\frac{1}{2} C = 9^{\circ} 1' 54''; C = 18^{\circ} 3' 48''$ Ans. Ans. To check, add the angles: 41° 45' 16"

41° 45′ 16″ 120 10 58 18 3 48 180° 00′ 2″

The triangle closes within 2 sec. This error is due to the use of fiveplace tables, and to the fact that the angle in each case was taken out to the nearest second.

EXAMPLES FOR PRACTICE

1. Given a = 1 mile, b = 2 miles, and c = 1.5 miles; find A, B, and C. (Use first method.) 2. Given a = 50 chains, b = 30 chains, and c = 45 chains; find A, B, and C. (Use first method.) $Ans. \begin{cases} A = 28^{\circ} 57' 17'' \\ B = 104^{\circ} 28' 39'' \\ C = 46^{\circ} 34' 4'' \end{cases}$ Ans. \begin{cases} A = 80^{\circ} 56' 36'' \\ B = 36^{\circ} 20' 7'' \\ C = 62^{\circ} 43' 17'' \end{cases} 3. Given a = 63.47 feet, b = 89.36 feet, and c = 109.83 feet; find *A*, *B*, and *C* (Use second method.) Ans. $\begin{cases} A = 35^{\circ} 18' 10'' \\ B = 54^{\circ} 27' 2'' \\ C = 90^{\circ} 14' 50'' \end{cases}$

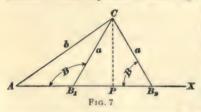
4. Given a = 2,354 feet, b = 3,115 feet, and c = 836.6 feet; find *A*, *B*, and *C*. (Use second method.) Ans. $\begin{cases} A = 21^{\circ} 7' 24'' \\ B = 151^{\circ} 31' 8'' \\ C = 7^{\circ} 21' 30'' \end{cases}$

24. Case IV: Given Two Sides and the Angle Opposite One of Them.—In the triangle ABC, let a, b, and A be given, to find B, C, and c. The angle B or C is found by means of the principle of sines; thus,

 $\frac{a}{\sin A} = \frac{b}{\sin B}, \text{ whence } \sin B = \frac{b \sin A}{a}$ Then, $C = 180^\circ - A - B, \text{ and } c = \frac{a}{\sin A} \sin C$

When the data are given as above, without any further restrictions, there may be two triangles that will answer the given conditions; and the problem is said to have two solutions. For here the angle B is determined from its sine, and as every sine corresponds to two supplementary angles, either of these angles may be taken. Thus, if sin B is found to be .64746, the corresponding angle may be either 40° 21' or $180^{\circ} - 40^{\circ} 21' = 139^{\circ} 39'$, since these angles both have the same sine (Art. 13).

The same result is obtained from geometrical considerations. On any line AX, Fig. 7, construct an angle equal



to the given angle A, and on its side A C take A C equal to one of the given sides b. From C as a center, with a radius equal to the side a, describe an arc. This arc will generally cut A X at two

points, B_1 and B_2 , and either of the triangles $A CB_1$ or $A CB_2$ will answer the conditions of the problem, for they both contain the given sides b and a, and the angle A opposite a.

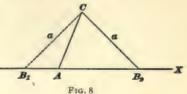
The problem will have but one solution in the following cases:

1. If $a = b \sin A$. For in this case a will be equal to the perpendicular CP, Fig. 7, and the arc described from C will touch AX at P only.

2. If a = b. For in this case the angles A and B must be equal, and therefore both acute, since a triangle cannot have two obtuse angles.

In this case B_1 coincides with A in Fig. 7, since $CB_1 = CA$.

3. When a is greater than b. For in this case A must be greater than B,



and the latter angle must therefore be acute. This is shown by Fig. 8; the arc described from C cuts A X produced at B_1 , and CB_1 , although equal to a, is not opposite $A (= CAB_1)$.

When a is less than b sin A, the problem is impossible. For then a is less than CP, Fig. 7, and the arc does not cut AXat all. This is also shown by the formula sin $B = \frac{b \sin A}{a}$, which would give sin B a value greater than 1, which is an

which would give $\sin B$ a value greater than 1, which is an impossible value, for no sine can be greater than 1.

EXAMPLE.—Given a = 273 feet, b = 392 feet, and $A = 37^{\circ} 14'$; to find B, C, and c.

SOLUTION.—Here a is less than b, and, unless sin B is found to be greater than 1 (in which case the problem is impossible), there are two solutions.

 $\sin B = \frac{b \sin A}{a} = \frac{392 \times \sin 37^{\circ} 14'}{273}; B = \begin{cases} 60^{\circ} 19' 17'', \text{ or} \\ 180^{\circ} - 60^{\circ} 19' 17'' \\ = 119^{\circ} 40' 43''. \text{ Ans.} \end{cases}$ $C = \begin{cases} 180^{\circ} - 37^{\circ} 14' - 60^{\circ} 19' 17'' \\ 180^{\circ} - 37^{\circ} 14' - 119^{\circ} 40' 43'' \\ 180^{\circ} - 37^{\circ} 14' - 119^{\circ} 40' 43'' \\ = 23^{\circ} 5' 17''. \text{ Ans.} \end{cases}$ $c = \frac{a}{\sin A} \sin C = \frac{273}{\sin 37^{\circ} 14'} \sin \begin{cases} 82^{\circ} 26' 43'', \text{ or} \\ 23^{\circ} 5' 17'' \end{cases} = 447.27 \text{ ft., or} \\ 176.93 \text{ ft. Ans.} \end{cases}$

PRACTICAL EXAMPLES

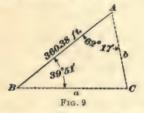
EXAMPLE 1.—The distance between two points A and B, Fig. 9, is 360.38 feet, the angles from A and B to a station C are found, with a transit, to be, respectively, 62° 17' and 39° 51'. What are the distances of C from A and B?

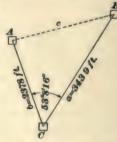
Solution. $C = 180^{\circ} - 62^{\circ} 17' - 39^{\circ} 51' = 77^{\circ} 52'$. Modulus (M) 360.38 Then (Art. 18), 360.38 $\sin 77^{\circ} 52' \sin 62^{\circ} 17' = 326.32$ ft. Ans. a :

$$b = \frac{360.38}{\sin 77^\circ 59'} \sin 39^\circ 51' = 236.2$$
 ft. Ans.

EXAMPLE 2.—The distances of a fort C from two other forts A and B are as marked in Fig. 10; the lines of sight from C to A and B make an angle of 53° 8' 16". What is the distance be-

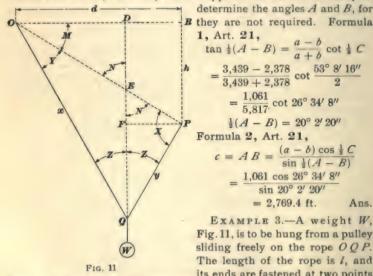
tween the two forts A and B?

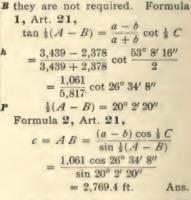






SOLUTION.-The two sides and the included angle are given, and formulas 1 and 2, Art. 21, will be applied. It is not necessary to





EXAMPLE 3.- A weight W. Fig. 11, is to be hung from a pulley sliding freely on the rope OQP. The length of the rope is I, and its ends are fastened at two points

O and P, whose horizontal distance is d and whose vertical distance is h, as shown. It being proved in mechanics that the pulley will rest in equilibrium when the vertical line WO bisects the angle OOP, what are the lengths x (= 00) and y (= P0) of the two segments of the rope for which that condition obtains?

NOTE.—This problem is given here as an illustration of the many problems that occur in practice requiring the exercise of some ingenuity and the performance of some transformations, both algebraical and trigonometrical, before the required results are obtained.

SOLUTION.—Let QD be a vertical line through Q. According to the data, this line makes equal angles with OO and OP. These angles are denoted by Z. The angles made by OQ and PQ with OP are denoted by Y and X, respectively. The line OR is horizontal, and PR vertical

As OR and R P are known, the right triangle OPR gives

$$\tan M = \frac{h}{d}$$

Also, in the triangle O E D, $N = 90^{\circ} - M$.

The angles M and N may, therefore, be assumed to be known.

Drawing PF parallel to RO, we have .

d(=OR) = OD + DR = OD + PF

or, substituting the values of OD and PF from the triangles ODQand PFQ.

 $d = x \sin Z + y \sin Z = (x + y) \sin Z = l \sin Z$

whence.

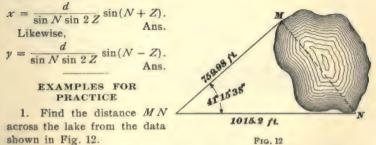
$$\sin Z = \frac{d}{1}$$

Having bound Z, we have

 $X = 180^{\circ} - (N + Z)$ (triangle PE O) Y = N - Z (triangle O E O) The modulus of the triangle OPO is OP OP $d \div \cos M$ d d $\sin 2Z =$ $\sin OQP = \sin 2Z =$ $\cos M \sin 2Z = \sin N \sin 2Z$ d Therefore (Art 38) r = nin V

sin
$$N \sin 2Z$$

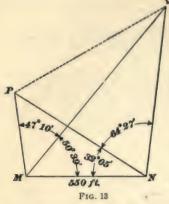
or, substituting the value of X, and noticing that $\sin[180^\circ - (N+Z)]$ = sin(N + Z),



Ans. MN = 669.51 ft.

2. The angles from two stations M and N, Fig. 13, to two inaccessible

points P and Q being as shown, and the distance MN being 550 feet find the distance PQ.



HINT. - First calculate MP, then MQ, and finally PQ.

Ans. PQ = 799.7 ft.

3. In Fig. 14, the sides ABand DE were measured and the angles were turned as marked. Find the lengths of the sides BC, CA, CF, AF, CD, FD, EF.

	BC	-	677.92 ft.
	CA	-	1,065.8 ft.
	CF	=	905.46 ft.
Ans.	AF	-	703.1 ft.
	CD		696.83 ft.
	FD	-	1,019.7 ft.
	EF	=	687.97 ft.

4. Two observers on the same side of a steeple, and in the same vertical plane with it, are 100 feet apart, and find that the angles of elevation are 26° 28' and 49° 14'. What is the height of the steeple? Ans. 87.225 ft.

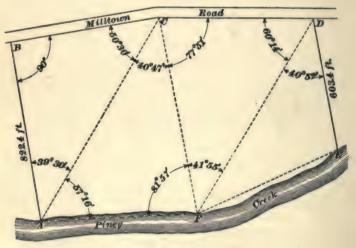


FIG. 14

5. Find the altitude h and the lengths of the sides AB and CD of the trapezoid ABCD, Fig. 15. $\begin{pmatrix} h = 62.22 \text{ ft.} \\ h = 62.22 \text{ ft.} \end{pmatrix}$

Ans. $\begin{cases} h = 62.22 \text{ ft.} \\ A B = 87.56 \text{ ft.} \\ C D = 64.579 \text{ ft.} \end{cases}$

6. The connecting-rod AB, Fig. 16, of an engine is 9 feet 3 inches, and the crank-arm CB is $10\frac{1}{3}$ inches; the figure shows the crank after

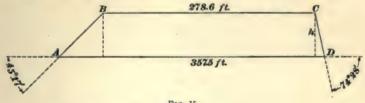


FIG. 15

it has performed one-eighth of a revolution, starting from the position CB'. Find: (a) the inclination M of the connecting-rod to the axis

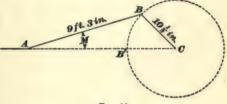


FIG. 16

ot the piston rod, which is in line with CA; (b) the distance AC of the joint A from the center of the crank-circle.

Ans. $\begin{cases} (a) \ M = 3^{\circ} \ 50' \ 7'' \\ (b) \ A \ C = 9 \ \text{ft. 10} \\ 10^{\circ} \ \text{in., nearly} \end{cases}$

AREAS

LAND MEASURE

25. In surveying the public lands of the United States and Canada, all linear measurements are made with the surveyors' chain, also known as Gunter's chain, from the name of the inventor. This chain is 66 feet in length and contains 100 links, each 7.92 inches long. In private surveys, the foot is commonly taken as the unit of linear measure, and small land areas are expressed in square feet.

Land areas of considerable extent in the countries mentioned are generally expressed in acres. Fractional parts of an acre, which formerly were expressed in roods, square rods or perches, and square links, are now expressed decimally by nearly all surveyors. Thus, 40.35 acres is written instead of 40 acres, 1 rood, and 16 square rods.

Tables of linear and square measure are given in Arithmetic, and to those tables the student is referred for detailed information regarding the subject. The following table gives the relative values of the units of area used in land surveying in the countries referred to above. As already stated, the square foot and acre are now the units most commonly employed.

TABLE OF LAND MEASURE

1	square yard (sq. yd.)	. =	: 9	square feet (sq. ft.)
1	square rod* (sq. rd)	. =	301	square yards = $272\frac{1}{4}$ square feet
1	square chain (sq. ch.) .	. =	16	square rods $= 4,356$ square feet
				square chains $= 43,560$ square feet
1	rood (R.)	. =	= 40	square rods = 10,890 square feet
1	acre	, 10	- 4	roods = 160 square rods
1	square mile (sq. mi.)	=	640	acres= 6,400 square chains
1	township (Tp.)	. =	: 36	square miles = 23,040 acres (app)

*Sometimes called a perch or pole, and designated by the abbreviation P.

As will be observed, there are 10 square chains in an acre. In order, therefore, to reduce to acres any number of square chains, it is sufficient to move the decimal point one place toward the left, which is equivalent to dividing by 10. It must also be borne in mind that, since there are 100 links in 1 chain, links are usually expressed decimally as hundredths of a chain. Thus, 6.72 chains is written instead of 6 chains 72 links.

EXAMPLE 1.—A rectangular piece of land is 1.060 feet in length by 820 feet in breadth: what is its area: (a) in acres and decimals? (b) in acres, roods, and perches?

Solution. (a) 1,060 \times 820 = 869,200 sq. ft.; 869,200 \div 43,560 = 19.954 A. Ans.

(b) .954 A. = .954 \times 4 = 3.816 R.; .816 R. is equal to .816 \times 40 = 32.64 P. Hence, the area is 19 A. 3 R. 32.64 P. Ans.

EXAMPLE 2.- A rectangular piece of land is 12 chains and 6 links (12.06 chains) in length by 8 chains and 55 links (8.55 chains) in breadth: what is its area: (a) in acres and decimals? (b) in acres. roods, and perches?

Solution. - (a) $12.06 \times 8.55 = 103.11$ sq. ch.; $103.11 \div 10$ = 10.311 A. Ans.

(b).311 A. = $.311 \times 4 = 1.244$ R.; .244 R. is equal to $.244 \times 40$ = 9.76 P. Hence, the area is 10 A. 1 R. 9.76 P. Ans.

EXAMPLES FOR PRACTICE

1. A rectangular piece of land is 1,190 feet in length by 700 feet in breadth; what is its area: (a) in acres and decimals? (b) in acres, Ans. { (a) 19.123 A. (b) 19 A. 0 R. 19.7 P. roods, and perches?

2. A rectangular piece of land is 525 feet long by 250 feet wide, what is its area: (a) in acres and decimals? (b) in acres, roods, and Ans. $\begin{cases} (a) 3.013 \text{ A}, \\ (b) 3 \text{ A}. 0 \text{ R}, 2.08 \text{ P}. \end{cases}$ perches?

3. A rectangular piece of land is 15 chains and 65 links in length by 8 chains and 16 links in breadth; what is its area: (a) in acres and decimals? (b) in acres, roods, and perches?

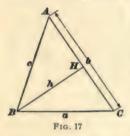
Ans. $\begin{cases} (a) & 12.77 \text{ A.} \\ (b) & 12 \text{ A.} & 3 \text{ R.} & 3.2 \text{ P.} \end{cases}$

AREAS OF POLYGONS

THE TRIANGLE

NOTE.—In all that follows, the area of any figure under consideration will be designated by S, unless otherwise stated.

26. Given the Base and Altitude.—Any of the sides of a triangle may be taken as the base, the altitude being the length of the perpendicular drawn on the base from the vertex of the opposite angle. In Fig. 17, b is taken as the base,



and the perpendicular BH, denoted by h, is the altitude.

It was shown in *Geometry*, Part 2, that the area of a triangle, when the base b and altitude h are known, is given by the formula $S = \frac{1}{2} b h$

27. Given Two Sides and the Included Angle.—Let b, c, and A,

Fig. 17, be given. In the right triangle ABH, we have $h = c \sin A$. The substitution of this value of h in the formula in Art. 26 gives

$$S = \frac{1}{2} b c \sin A$$

In words, the area of a triangle is equal to one-half the product of any two sides and the sine of their included angle.

EXAMPLE.—Two of the sides of a triangular field are 39.47 and 59.23 chains, respectively, and their included angle is 65° 10' 40". To find the contents of the field, in acres.

Solution.—By the formula, S (square chains) = $\frac{1}{2} \times 39.47 \times 59.23$ sin 65° 10′ 40″ = 1,060.9 sq. ch.; whence, dividing by 10 (Art. 25), S (acres) = 106.09 A. Ans.

28. Given One Side and Two Angles.—The other angle may be at once found by subtracting the sum of the two given angles from 180° . It may, therefore, be assumed that the three angles are known. Let b, Fig. 17, be the given side. From Art. 22, the value of c is equal to the modulus of the triangle multiplied by sin C, or,

$$c = \frac{b}{\sin B} \sin C$$

Substituting this value in the formula in Art. 27, we obtain $S = \frac{b^* \sin A \sin C}{2 \sin B}$

29. The formula in Art. **28** is convenient when logarithmic functions are employed. For the use of natural functions, the following is preferable:

In the right triangles ABH and CBH, Fig. 17, we have, $AH = h \cot A$, $CH = h \cot C$

whence, adding these two equations,

that is.

 $AH + CH = h \cot A + h \cot C$ $b = h(\cot A + \cot C)$

and, therefore,
$$h = \frac{b}{\cot A + \cot C}$$
 (1)

This formula is useful and should be committed to memory. It may be stated in words thus: The altitude of a triangle is equal to the base divided by the sum of the cotangents of the adjacent angles.

By substituting, in the formula in Art. 26, the value of h given in formula 1, we obtain

$$S = \frac{b^3}{2(\cot A + \cot C)}$$
(2)

In words, the area of a triangle is equal to the square of any side divided by twice the sum of the cotangents of the angles adjacent to that side.

EXAMPLE.—One side of a triangular field is 127.64 chains, and the adjacent angles are 46° 15' and 60° 41'. To find the area.

Solution by Logarithmic Functions.—Here, b = 127.64, $A = 46^{\circ} 15'$, $C = 60^{\circ} 41'$, and $B = 180^{\circ} - 46^{\circ} 15' - 60^{\circ} 41' = 73^{\circ} 4'$. Formula of Art. 28, $S = \frac{127.64^{\circ} \sin 46^{\circ} 15' \sin 60^{\circ} 41'}{2 \sin 73^{\circ} 4'}$

$$= 5.363.4$$
 sq. ch. $= 536.34$ A. Ans

SOLUTION BY NATURAL FUNCTIONS .- By formula 2,

$$S = \frac{127.64^{\circ}}{2(\cot 46^{\circ} 15' + \cot 60^{\circ} 41')} = \frac{127.64^{\circ}}{2(.95729 + .56156)}$$
$$= \frac{127.64^{\circ}}{3.0377} = 5,363.4 \text{ sq. ch.} = 536.34 \text{ A. Ans.}$$

Note... Even if natural functions are used, the division is advantageously per formed by means of logarithms.

EXAMPLES FOR PRACTICE

1. Two sides of a triangular field are 3,760 and 2,757 feet, respectively, and their included angle is 54° 13′ 13″. What is the area of the field, in acres? Ans. S = 96.534 A.

2. One side of a triangle is 96.34 chains; the opposite angle is 49° 10′, and one of the adjacent angles, 69° 45′ 30″. What is the area of the triangle, in acres? Ans. S = 503.69 A.

3. One side of a triangle is 8.93 inches, and the adjacent angles are 34° 16' and 17° 37' 18". What is the area of the triangle?

Ans. S = 8.638 sq. in.

4. Two sides of a triangle are 17 and 25 feet, respectively, and the included angle is 76° 13'. What is the area of the triangle?

Ans. S = 206.38 sq. ft.

30. Given the Three Sides.—Let a, b, and c, Fig. 17, be given, and denote $\frac{1}{2}(a + b + c)$ by s. The area S of the triangle is given by the following formula, which is derived in Appendix VI:

$$S = \sqrt{s(s-a)(s-b)(s-c)}$$

EXAMPLE.—The sides of a triangular tract are 1,634.6 (= a, say), 978.28 (= b, say), and 2,176.4 (= c, say) feet, respectively; to find the area, in acres.

SOLUTION.—The work may be conveniently arranged as shown below. The numbers in marks of parenthesis indicate the order in which the several quantities are set down. In (6), s is placed above a, b, c in order to facilitate the subtractions. The differences s - a, s - b, s - c are written, as the subtractions are performed, horizontally opposite a, b, and c, respectively.

(6) s ==	2,394.64
(1) $a =$	1,634.60 (7) $s - a = 760.04$
(2) $b =$	978.28 (8) $s - b = 1,416.36$
(3) $c =$	2,176.40 (9) $s-c = 218.24$
(4) $2 s =$	4,789.28
(5) s =	2,394.64
(10) $\log s = 3$	3.37924
(11) $\log(s-a) = 2$	2.88083
(12) $\log(s-b) = 3$	3.15117
$(13) \log (s-c) = 2$	2.33893
2)11	1.75017
$\log S = 5$	5.87509; $S = 750,050$ sq. ft. = 17.22 A. Ans.

EXAMPLES FOR PRACTICE

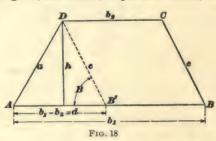
1. Find the area of a triangular tract whose sides are 54.36, 73.19, and 101.76 chains, respectively. Ans. S = 192.26 A.

2. Find the area of a triangular plate whose sides are 17.12, 12.75, and 8.95 inches, respectively. Ans. S = 55.646 sq. in.

THE TRAPEZOID

31. Notation.—In Fig. 18, the bases, or parallel sides, of

the trapezoid A B C Dare denoted by b_1 and b_3 ; the altitude, by h; and the sides A D and B C, by a and c, respectively. The angles will be designated by the letters A, B, C, D at the vertexes. The line D B' is



drawn through D parallel to CB, thus forming a parallelogram in which $B'B = DC = b_i$, and DB' = CB = c. Also, angle DB'A = B, and $AB' = AB - B'B = b_i - b_i$. For some purposes, it is convenient to represent this difference by a single letter d, as shown in the figure.

32. Given the Bases and the Altitude.—As shown in *Geometry*, Part 2, the area of a trapezoid is equal to one-half the product of the altitude by the sum of the bases; that is, $S = \frac{1}{2}(b_1 + b_2)h$

33. Given the Bases and the Angles Adjacent to One of Them.—Let b_1, b_2, A , and B, Fig. 18, be given. In the triangle ADB' we have (formula 1, Art. 29),

$$h = \frac{b_1 - b_2}{\cot A + \cot B}$$

If this value of h is substituted in the formula of Art. 32, the result is.

$$S = \frac{(b_1 - b_2)(b_1 + b_2)}{2(\cot A + \cot B)}$$
(1)

As the product of the sum of two quantities by their difference is equal to the difference between the squares of the

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quantities, $(b_1 - b_2)(b_1 + b_2)$ is equal to $b_1^* - b_2^*$; and, therefore, formula 1 may also be written:

$$S = \frac{b_1^{\circ} - b_2^{\circ}}{2(\cot A + \cot B)}$$
(2)

For the use of logarithmic functions, formula 1 may be transformed into the following (see Appendix VII):

$$S = \frac{(b_1 - b_2)(b_1 + b_2)\sin A \sin B}{2\sin (A + B)}$$
(3)

In the application of these formulas, the student should bear in mind that the cotangent of an angle greater than 90° is negative, and numerically equal to the cotangent of the supplement of the angle; also, that the sine of an angle greater than 90° is equal to the sine of its supplement. Thus, cot $105^\circ = -\cot(180^\circ - 105^\circ) = -\cot75^\circ = -.26795$; and sin $105^\circ = \sin 75^\circ = .96593$.

EXAMPLE 1.—The two bases of a trapezoid are 350 and 137 chains, respectively; the angles adjacent to the longer base are 75° 10' and 63° 54'. What is the area of the trapezoid?

Solution by NATURAL FUNCTIONS.—Let $350 = b_1$, $137 = b_2$, $A = 75^{\circ} 10'$, $B = 63^{\circ} 54'$. As b_1 and b_2 are not convenient numbers to square, formula 1, which is better adapted to logarithmic work, will be used.

 $S = \frac{(350 - 137)(350 + 137)}{2(\cot 75^{\circ} 10' + \cot 63^{\circ} 54')} = \frac{213 \times 487}{2(.26483 + .48989)} = 68,721 \text{ sq. ch.}$ = 6,872.1 A. Ans.

Solution by Logarithmic Functions.—By formula 3, $S = \frac{(350 - 137)(350 + 137) \sin 75^{\circ} 10' \sin 63^{\circ} 54'}{2 \sin 139^{\circ} 4'}$

or, replacing sin 139° 4′ by sin (180° - 139° 4′) = sin 40° 56′, $S = \frac{213 \times 487 \sin 75^{\circ} 10' \sin 63^{\circ} 54'}{2 \sin 40^{\circ} 56'} = 68,721 \text{ sq. ch.} = 6,872.1 \text{ A. Ans.}$

EXAMPLE 2.—The bases of a trapezoid are 100 and 70 feet, the angles adjacent to the shorter base being 52° 47' and 143° 14'. What is the area of the trapezoid?

SOLUTION.—Since the bases are parallel, the two angles adjacent to each of the non-parallel sides are supplementary. Thus, in Fig. 18, $A + D = 180^{\circ}$, $B + C = 180^{\circ}$; and, therefore, $A = 180^{\circ} - D$; $B = 180^{\circ} - C$. Let $52^{\circ} 47' = D$, $143^{\circ} 14' = C$. Then,

 $\begin{array}{l} \mathcal{A} \ = \ 180^\circ - \ 52^\circ \ 47' \ = \ 127^\circ \ 13' \\ \mathcal{B} \ = \ 180^\circ - \ 143^\circ \ 14' \ = \ 36^\circ \ 46' \\ \mathrm{cot} \ \mathcal{A} \ = \ - \ \mathrm{cot} \ (180^\circ - \ 127^\circ \ 13') \ = \ - \ \mathrm{cot} \ 52^\circ \ 47' \ = \ - \ .75950 \\ \mathrm{cot} \ \mathcal{B} \ = \ \mathrm{cot} \ 36^\circ \ 46' \ = \ 1.33835 \end{array}$

Formula 2.

 $S = \frac{100^{\circ} - 70^{\circ}}{2(+1.33835 - .7595)} = \frac{5,100}{1.1577} = 4,405.3 \text{ sq. ft.} \text{ Ans.}$

EXAMPLES FOR PRACTICE

1. The bases of a trapezoidal tract are 78.63 and 54.71 chains, respectively; the angles adjacent to the longer base are 55° 18' and 62° 53'. Find the area, in acres. Ans. S = 132.4 A.

2. Find the number of square feet in a trapezoidal cross-section of a canal 40 feet wide at the bottom, 65 feet wide at the top, and whose non-parallel sides are inclined to the horizontal at an angle of 50°. (The dimensions across the top and bottom are measured horizontally.) Ans. S = 782.09 sq. ft.

3. The two bases of a trapezoid are 10.25 and 18.76 inches, respectively; one of the angles adjacent to the shorter base is 76° 45′ 10″, and the angle diagonally opposite is $66^{\circ} 8' 9''$; find the area of the trapezoid. (Use logarithmic functions.) Ans. S = 596.4 sq. in.

34. Given the Four Sides.—If the difference between the two bases added to the sum of the non-parallel sides is denoted by 2s; that is, if the expression $\frac{1}{2}(a + c + d)$, Fig. 18, is denoted by s, the area of the trapezoid is given by the following formula (see Appendix VIII):

$$S = \frac{b_1 + b_2}{d} \sqrt{s(s-a)(s-c)(s-d)}$$

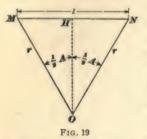
EXAMPLE FOR PRACTICE

The bases of a trapezoidal field are 136.43 and 210.18 chains, respectively; one of the non-parallel sides is 96.73 chains, and the other 164.37 chains. Find the area of the tract, in acres.

Ans. S = 864.97 A.

THE'REGULAR POLYGON

35. Given the Number of Sides and the Radius. Let MN, Fig. 19, be one of the sides of a regular polygon



of *n* sides; *O*, the center, and *r* the radius, of the circumscribed circle (called also the center and radius, respectively, of the polygon); and *A*, the angle at the center subtended by a side of the polygon. The length of the side MN will be denoted by *l*. Let *n* and *r* be given, to find the area *S* of the polygon and the length *l*

of each of its sides. From *Geometry*, Part 2, the angle MON, or A, is found by dividing 360° by the number of sides in the polygon; that is, 360°

$$A = \frac{360^{\circ}}{n}$$

The area of the triangle MON is (Art. 27) $\frac{1}{2}OM \times ON$ sin MON, or $\frac{1}{2}r \times r \sin A = \frac{1}{2}r^* \sin A = \frac{1}{2}r^* \sin \frac{360^\circ}{n}$. Since the polygon consists of *n* triangles equal to MON, its area S is equal to *n* times the area of MON; that is,

$$S = n \times \frac{1}{2} r^{s} \sin \frac{360^{\circ}}{n}$$
$$S = \frac{1}{2} n r^{s} \sin \frac{360^{\circ}}{n}$$
(1)

or

In the right triangle MOH, we have,

$$MH = r\sin\frac{A}{2}$$

or, since MH is one-half of MN, or of l,

$$\frac{l}{2} = r \sin \frac{A}{2}$$

whence, multiplying by 2,

$$l = 2r\sin\frac{A}{2}$$

Finally, $\frac{A}{2} = \frac{1}{2} \frac{360^{\circ}}{n} = \frac{180^{\circ}}{n}$. By the substitution of this

PLANE TRIGONOMETRY, PART 2

value in the expression for l just found, we get, finally,

$$l = 2r\sin\frac{180^\circ}{n} \qquad (2)$$

36. When the Number of Sides and Their Common Length Are Given.—Let n and l, Fig. 19, be given, to find the radius r and the area S. The radius is found by solving formula 2, Art. 35, for r, which gives,

$$r = \frac{l}{2\sin\frac{180^\circ}{n}} \tag{1}$$

In the triangle MOH, we have,

$$OH = MH \cot \frac{1}{2}A = \frac{MN}{2} \cot \frac{1}{2}A$$

The area of MON is $\frac{1}{2}MN \times OH$. Writing instead of OH the value just found,

$$\frac{\frac{1}{2}}{MN} \times \frac{MN}{2} \cot \frac{\frac{1}{2}}{4} = \frac{MN^{3}}{4} \cot \frac{\frac{1}{2}}{4} A$$
$$= \frac{l^{3}}{4} \cot \frac{\frac{1}{2}}{4} = \frac{l^{3}}{4} \cot \frac{180^{\circ}}{n}$$

Multiplying this by n, we obtain, for the area of the polygon,

$$S = \frac{n l^{*}}{4} \cot \frac{180^{\circ}}{n} \qquad (2)$$

EXAMPLE 1.—Find the area, and also the length of the side, of a regular decagon inscribed in a 15-inch circle.

SOLUTION.—In practice, it is usual to refer to a circle by its diameter, and so a 15-in. circle is a circle whose diameter is 15 in. We have, therefore, $r = \frac{15}{2} = 7.5$, n = 10, $\frac{360^{\circ}}{n} = \frac{360^{\circ}}{10} = 36^{\circ}$, $\frac{180^{\circ}}{n} = 18^{\circ}$, and formulas 1 and 2, Art. 35, give $S = \frac{1}{4} \times 10 \times 7.5^{\circ} \sin 36^{\circ} = 165.32$ sq. in. Ans.

 $l = 2 \times 7.5 \sin 18^{\circ} = 4.635$ in. Ans.

EXAMPLE 2.—Each of the sides of an octagonal park is 150 feet; what is the area of the park, in acres?

Solution.—Here l = 150 ft., n = 8, $\frac{180^{\circ}}{n} = \frac{180^{\circ}}{8} = 22\frac{10}{2} = 22^{\circ}$ 30', and formula 2, Art. 36, gives,

PLANE TRIGONOMETRY, PART 2

 $S = \frac{1}{2} \times 8 \times 150^{\circ} \text{ cot } 22^{\circ} 30' = 2 \times 22,500 \text{ cot } 22^{\circ} 30' = (45,000 \text{ cot } 22^{\circ})^{\circ}$ 22° 30′) sq. ft. = $\frac{45,000 \text{ cot } 22^\circ 30'}{43.560}$ A. = 2.494 A. Ans.

EXAMPLES FOR PRACTICE

1. Find the side and area of an equilateral triangle inscribed in a Ans. $\begin{cases} l = 17.321 \text{ in.} \\ S = 129.9 \text{ sq. in.} \end{cases}$ 20-inch circle.

2. What must be the length of the side and the radius of a regular pentagon, that its area may be 46.97 square feet?

Ans. $\begin{cases} l = 5.225 \text{ ft.} \\ r = 4.445 \text{ ft.} \end{cases}$

An eight-sided drive is to be built around a circular park 3. 1,500 feet in diameter, the drive to be 15 feet wide, with its outer corners on the circumference of the park. Find: (a) the length of each of the sides of the outer boundary of the drive; (b) the length of each of the sides of the inner boundary; (c) the cost of paving the drive with asphalt, at \$2.25 per square vard; (d) the difference between the exact area of the drive and the approximate area found by assuming the polygonal boundaries to coincide with the circumferences of their (a) 574.02 ft. respective circumscribed circles.

Ans. $\begin{cases} (a) & 561.60 \text{ ft.} \\ (b) & 561.60 \text{ ft.} \\ (c) & \$17,025 \\ (d) & \$44 \text{ sq. yd.} \end{cases}$

OTHER POLYGONS

37. The area of any polygon can be determined by dividing the polygon into triangles, and measuring in each triangle whatever parts are necessary for the determination of its area. The parts to be measured depend on special conditions and on the instruments used. The polygon may be divided into triangles either by diagonals or by lines drawn from a convenient interior point to the different vertexes. Illustrations of these methods of division will be given in connection with surveying. When the area is to be determined from a plat, the base and altitude of each triangle are usually the most convenient parts to measure.

AREAS BOUNDED BY IRREGULAR OUTLINES

AREA INCLUDED BETWEEN A STRAIGHT LINE AND AN IRREGULAR CURVE

38. By Selected Ordinates.—Let it be required to determine the area between the curve DC and the straight line AB, Fig. 20. A very convenient method is to draw perpendiculars on AB from the points of the curve at which

its direction charges appreciably, and to consider the portion of the curve between two consecutive perpendiculars to be a *A* straight line. The

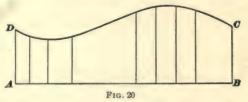


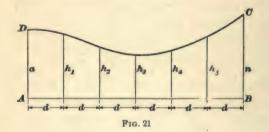
figure is then treated as if divided into a number of trapezoids, whose areas can be computed by the rules of geometry. The perpendiculars are called **ordinates**. Both the lengths of the ordinates and the distances between every two consecutive ordinates should be measured. The area of any of the (approximate) trapezoids into which the figure is thus divided is equal to one-half the sum of the two ordinates enclosing it multiplied by the distance between them. It should be understood that both this rule and those given further on relating to the same subject are only approximate. Since the bounding curve is irregular, that is, does not follow any mathematical law, no exact formula can be found for the area.

EXAMPLE.—Referring to Fig. 20, suppose that, beginning at the left of the figure, the successive ordinates measure 15, 13, 12, 13.5, 20, 21.5, 22, 20, and 16 feet, respectively, and that the successive distances between the offsets, from left to right, measure 7.5, 10, 15, 41, 10.5, 11.5, 11.5, and 21 feet, respectively; what is the area of the surface?

SOLUTION.—The area of the figure is approximately equal to the sum of the areas of the trapezoids into which it is divided, and the area of each trapezoid is equal to one-half the sum of its parallel sides multiplied by the perpendicular distance between them. Therefore, the area of the figure is equal to

$$\frac{15+13}{2} \times 7.5 + \frac{13+12}{2} \times 10 + \frac{12+13.5}{2} \times 15 + \frac{13.5+20}{2} \times 41 + \frac{20+21.5}{2} \times 10.5 + \frac{21.5+22}{2} \times 11.5 + \frac{22+20}{2} \times 11.5 + \frac{20+16}{2} \times 21 = 2,195.5 \text{ sq. ft. Ans.}$$

39. Trapezoidal Rule: Sigma Notation.—In order to facilitate the calculations, the ordinates are often measured at regular intervals along the straight line, as shown in Fig. 21. The area A B C D included between the straight line and the irregular boundary can then be more easily calculated by what is commonly known as the trapezoidal rule. This



is merely a rule for calculating the combined area of a series of trapezoids that have the same altitude, the areas being combined for convenience of calculation. The result given by this rule is closer the smaller the distance between the ordinates. The rule is as follows:

Rule.—Add together one-half the two end ordinates and all the intermediate ordinates, and multiply the sum by the common distance between the ordinates.

Let	а	=	first ordinate;
	n	===	last ordinate;
	h_1, h_2, h_3	==	intermediate ordinates;
	α	=	common distance between ordinates;
	S	-	area of surface.

Then, $S = \begin{bmatrix} \frac{1}{2}(a+n) + h_1 + h_2 + h_3 + \dots \end{bmatrix} d$

This expression may be put in a simpler form by using the sigma notation, which is as follows: As will be noticed, all the intermediate ordinates are denoted by h, different subscripts being used to indicate different values of h. We may, therefore, write the value of S thus,

 $S = [\frac{1}{2}(a+n) + \text{sum cf all values of } h]d$

Instead of the phrase sum of all values of h, the expression Σh , read sigma h, is used. The symbol Σ is the Greek letter sigma, corresponding to English S, and is very commonly used, as here, to indicate the addition of several quantities of the same character, denoted by a single symbol; hence, the name sign of summation, which also is often given to that letter.

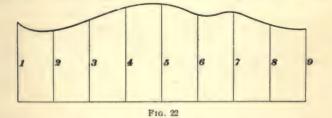
By using the sigma notation, the value of S may be written

$$S = \left(\frac{a+n}{2} + \Sigma h\right)d$$

EXAMPLE.—If the ordinates from the straight line A B to the curved boundary D C, Fig. 21, are 19, 18, 14, 12, 13, 17, and 23 links, respectively, and are at equal distances of 50 links, what is the area included between the curved boundary and the straight line?

Solution.—Area $A B C D = \left(\frac{19+23}{2} + 18 + 14 + 12 + 13 + 17\right) \times 50 = 4,750$ sq. li. Ans.

40. Simpson's Rule.—The foregoing rule assumes that all the small figures into which the area is divided are perfect trapezoids, which assumption always involves more or less error, since the irregular boundary is in nearly all cases an irregular curve. When the offsets are taken at



regular intervals, the following rule, known as Simpson's one-third rule, gives a closer approximation. In applying this rule, the base line must be divided into an even number of equal parts; the ordinates measured at the points of division are numbered consecutively, as shown in Fig. 22.

PLANE TRIGONOMETRY PART 2

Rule.—Divide the base line into an even number of equal parts, and at the points of division erect ordinates terminating in the curve. Number the ordinates 1, 2, 3, etc., from left to right, including those at the ends of the base. Add together the end ordinates, four times the sum of all intermediate evennumbered ordinates, and twice the sum of all intermediate oddnumbered ordinates: multiply the total sum by one-third the common distance between adjacent ordinates.

This rule has been used extensively: it can be expressed by a formula as follows:

Let $h_1 =$ any intermediate even-numbered ordinate:

 $h_{a} =$ any intermediate odd-numbered ordinate;

and let all other quantities be represented by the same letters as in the preceding article. Then,

$$S = (a + n + 4 \Sigma h_s + 2 \Sigma h_s) \frac{a}{2}$$

The notation will be readily understood by reference to

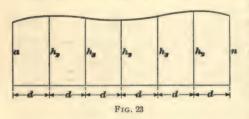


Fig. 23. The expression $4\Sigma h$, means four times the sum of all the ordinates h., or, in other words. four times the sum of all the even-numbered ordinates.

EXAMPLE.-What is the area A B C D, Fig. 21, by Simpson's rule, using the same values as in the example in Art. 39?

Solution. $S = [19 + 23 + 4(18 + 12 + 17) + 2(14 + 13)] \times \frac{59}{2}$ = 4,733 sq. li. Ans.

EXAMPLES FOR PRACTICE

1. A figure included between a straight base line, a curve, and two perpendiculars to the base at the ends has nine ordinates, including the two end perpendiculars, whose lengths are 43, 48, 39, 50, 41, 32, 37, 31, and 22 feet, respectively; the common distance between the ordinates is 60 feet. Find the area: (a) by the trapezoidal rule; (b) by Ans. $\begin{cases} (a) & 18,630 \text{ sq. ft.} \\ (b) & 18,860 \text{ sq. ft.} \end{cases}$ Simpson's rule.

2. In order to determine the area included between an irregular boundary, a straight base line, and two perpendiculars to the base at the ends, eight ordinates, including the two end perpendiculars, are measured from the straight line to the boundary. The ordinates are found to measure 16, 18, 12, 13, 15, 17, 19, and 20.5 feet, and the successive distances between them are found to measure 7.8, 10, 15, 20, 12, 40, and 5 feet, respectively. What is the area of the surface?

Ans. 1.760.9 sq. ft.

3. A surface lying between a straight base line and a curve is limited by two perpendiculars to the base line at the ends; the base line is divided into eight parts 50 feet each, and at the points of division ordinates are measured. The lengths of the successive ordinates, including the two end perpendiculars, are 10, 25, 38, 49, 58, 65, 70, 73, and 74 feet, respectively. Find the area of the surface: (a) by the trapezoidal rule; (b) by Simpson's rule. Ans. $\begin{cases} (a) 21,000 \text{ sq. ft.} \\ (b) 21,007 \text{ sq. ft.} \end{cases}$

AREA BOUNDED BY AN IRREGULAR CURVE

41. By Ordinates.—Suppose that it is required to find the area enclosed by the heavy irregular curve shown in Fig. 24. A broken line *AEFMGHIA* is drawn around

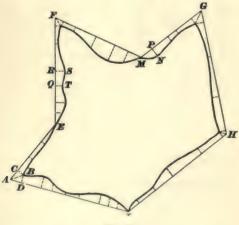
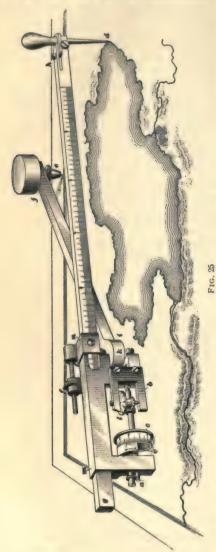


FIG. 24

the curved boundary line, and as close to it as convenient. Ordinates to the straight lines thus drawn are measured from the points where the direction of the curved boundary changes materially, as shown. The area of the polygon AEFMGHIA is calculated by one of the methods



by one of the methods explained in preceding articles, and from it is subtracted the sum of the areas included between the curved boundary and the broken line, calculated as in Art. **39**.

At such corners as A, the triangles ABC and ABD are computed from the measured bases ACand AD and the altitudes BC and BD. All the quadrilaterals, as QRST, are treated as trapezoids; and such three-sided figures as MPN, as triangles. The process is so simple that it does not require any further explanation.

42. By the Planimeter.—The most convenient way to find the area of a plane surface having an irregular boundary is by the planimeter. There are several forms of planimeters; the one most commonly used is the polar planimeter (see Fig. 25). As will be seen from the illustration, this instru-

ment has two arms ij and gh connected by a hinge joint. The point e at the end of the bar ij is called the **anchor** point: it remains stationary while the point d, called the pointer or tracer, at the end of the bar gh is moved over the outline of the figure whose area is to be determined. The movement of the pointer d causes the wheel c on the opposite end of the bar to roll on the paper: this wheel is called the measuring wheel or counter wheel. The graduated bar gh can be adjusted by sliding it in or out through the socket m in the top of the frame. This bar is clamped by means of a clamp screw, a part of which is shown back of the small movable socket n, and is set at the exact length required by means of the thumbscrew f. The bar ii is of fixed length; it is pivoted at k, the junction of the two bars. The measuring wheel c is mounted on the main axis ab, which is parallel with the bar gh. The complete revolutions of the wheel c are read on the disk *l*, and the fractional parts of revolutions are read on the wheel c and the vernier v, the tenths and hundredths being read on the wheel itself, and the thousandths on the vernier.

To use the planimeter, the anchor point e is fixed on the paper or drawing board, preferably outside the figure to be measured, the pointer d is placed on some point in the periphery of the figure, and a reading of the wheel c is taken. The point d is then moved carefully around the periphery of. the figure, in a clockwise direction, or from left to right, to the point of beginning. A second reading of the wheel cis then taken, and the difference between the two readings is the number of revolutions of the wheel. If the wheel is set to read zero, the number of revolutions is given directly by the second reading.

If the anchor point is outside the area to be measured, the distance traversed by the wheel, or the product of the number of revolutions by the circumference of the wheel, in inches, multiplied by the length of the bar nh, in inches, is the area, in square inches, bounded by the path of the pointer d.

If the anchor point is inside the area, the product just referred to must be added to the area of the zero circle, whose radius is equal to $\sqrt{p^* + q^* + 2pr}$, *p* being the length of the arm *n h*; *r*, the distance from the center of the wheel *c* to the center of the joint *k*; and *g*, the length of the bar *k j*. The bar *g h* is generally set at such a length that ten times the number of revolutions of the wheel *c* is the area measured. This area is the actual area of the figure measured, and the area *represented* by the figure is determined from the scale of the plat. The area given by the planimeter, in square inches, must be multiplied by the square of the scale of the plat, in order to get the area sought. Thus, if the plat has been drawn to a scale of 50 feet to an inch, each square inch of the plat is equivalent to $50 \times 50 = 2,500$ square feet of area.

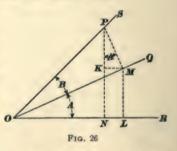
Suppose that the area bounded by the irregular line in Fig. 25, as measured by the planimeter, is 2.535 square inches, and that the scale of the plat is 100 feet to an inch; then the area represented by a square inch of the plat is $100 \times 100 = 10,000$ square feet, and the area represented by the closed figure is $10,000 \times 2.535 = 25,350$ square feet.

Full directions for using the planimeter are usually furnished by the maker.

APPENDIX: DERIVATION OF FORMULAS

I-FORMULAS 1 TO 4 OF ART. 16

Let R O Q, Fig. 26, be any angle A, and Q O S any angle B. Then, A + B = R O S. From any point Pon O S, draw PN and PM, perpendicular, respectively, to OR and OQ. Draw MK parallel to ORand therefore perpendicular to PN; also, ML perpendicular to OR. The angles MPK and R O Q, having their sides perpendicular each to each, are equal. Now,



 $\sin (A+B) = \frac{NP}{OP} = \frac{NK+KP}{OP} = \frac{ML}{OP} + \frac{KP}{OP} = \frac{OM\sin A}{OP} + \frac{PM\cos A}{OP}$

(triangles M L O and P M K) = sin $A \frac{O M}{O R} + \cos A \frac{P M}{O R} = sin A \cos B$ $+\cos A \sin B$ (triangle OPM) This is formula 1. Also. $\cos (A - B) = \sin [90^\circ - (A - B)] = \sin [(90^\circ - A) + B]$ or, by formula 1. $\cos (A - B) = \sin (90^{\circ} - A) \cos B + \cos (90^{\circ} - A) \sin B$ $= \cos A \cos B + \sin A \sin B$ which is formula 4. Formula 3 follows from this: for $\sin (A - B) = \cos [90^{\circ} - (A - B)] = \cos [(90^{\circ} + B) - A]$ $= \cos (90^{\circ} + B) \cos A + \sin (90^{\circ} + B) \sin A$ or, because $\cos(90^{\circ} + B) = -\sin B$, and $\sin(90^{\circ} + B) = \cos B(\text{Art. 14})$. $\sin (A - B) = -\sin B \cos A + \cos B \sin A = \sin A \cos B - \cos A \sin B.$ Finally, applying this formula, $\cos (A + B) = \sin [90^\circ - (A + B)] = \sin [(90^\circ - A) - B]$ $= \sin (90^{\circ} - A) \cos B - \cos (90^{\circ} - A) \sin B$

 $= \cos A \cos B - \sin A \sin B$

which is formula 2.

II-FORMULAS OF ART. 19

Referring to Fig. 6(a) and (b), Art. 18,

$${}^{\mathfrak{s}} = p^{\mathfrak{s}} + B D^{\mathfrak{s}} \tag{1}$$

In (a), BD = c - AD, whence $\overline{BD}^{\circ} = c^{\circ} - 2c \times AD + \overline{AD}^{\circ}$. In (b), BD = AD - c, whence $\overline{BD}^{\circ} = \overline{AD}^{\circ} - 2c \times AD + c^{\circ}$. Substituting this value of BD in equation (1),

$$a^{2} = p^{2} + \overline{A} D^{2} + c^{2} - 2c \times A D \qquad (2)$$

But $p^{\circ} + \overline{AD}^{\circ} = b^{\circ}$, and $AD = b \cos A$; therefore, $a^{\circ} = b^{\circ} + c^{\circ} - 2bc \cos A$

a

When the angle opposite the side is obtuse, as B in Fig. 6 (b), the same reasoning leads to the relation,

$$a^{2} = a^{2} + c^{2} + 2 a c \times \cos C B D$$

the second member of which becomes $a^* + c^* - 2 a c \cos B$, when $\cos CBD$ is replaced by its equal $-\cos B$ (Art. 13).

PLANE TRIGONOMETRY, PART 2

III-FORMULAS OF ART. 20

Let A B C, Fig. 27, be any triangle. As usual, the angles of the tri-

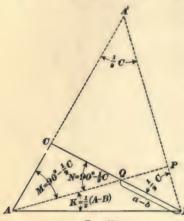


FIG. 27

angle will be denoted by A, B, C, and the opposite sides by a, b, c, respectively; that is, angle CAB= A, BC = a, etc. Produce ACto A', making CA' = BC = a. Draw BA', and AP perpendicular to it, meeting BC at Q.

Since BC = CA', the triangle BCA' is isosceles, and, therefore, the angles CA'B and CBA' are equal. The sum of these two angles, or twice either of them, is equal to the external angle BCA, or C, and therefore each of these two angles is equal to $\frac{1}{2}C$. In the right triangle APA', the angle M, being the complement of A', is equal to $90^\circ - \frac{1}{4}C$.

We have also,

 $K = A - M = A - (90^{\circ} - \frac{1}{2}C),$

or, since $C = 180^{\circ} - (A + B) = 180^{\circ} - A - B$,

 $K = A - [90^{\circ} - \frac{1}{2}(180^{\circ} - A - B)] = \frac{1}{2}(A - B)$

The angle N being external to the triangle A Q B, we have

$$N = K + B = \frac{1}{2}(A - B) + B = \frac{1}{2}(A + B)$$
$$= \frac{1}{2}(180^{\circ} - C) = 90^{\circ} - \frac{1}{2}C = M$$

Therefore, the triangle A Q C is isosceles, and Q C = A C = b; and, consequently, B Q = a - b.

The right triangle A B P gives,

$$\tan \frac{1}{2}(A-B) = \frac{BP}{AP}$$

or, writing the values of BP and AP from the triangles BQP and APA',

$$\tan \frac{1}{2}(A-B) = \frac{BQ}{AA'} \frac{\cos \frac{1}{2}C}{\sin \frac{1}{2}C} = \frac{BQ}{AA'} \cot \frac{1}{2}C$$

$$\tan \frac{1}{2}(A - B) = \frac{a - b}{a + b} \cot \frac{1}{2} C$$
(1)

Now, $\frac{1}{2}C = \frac{1}{4}[180^\circ - (A + B)] = 90^\circ - \frac{1}{4}(A + B)$, and therefore, $\cot \frac{1}{2}C = \tan \frac{1}{4}(A + B)$. By substituting this value in equation (1), and transforming, the formula in Art. 20 is obtained.

that is,

IV-FORMULA 2 OF ART. 21

This formula is derived from Fig. 27 as follows: In the triangle B P Q,

 $B P = B Q \cos \frac{1}{2} C = (a - b) \cos \frac{1}{2} C$ (1)

and, in the triangle A B P,

$$c(=AB) = \frac{BP}{\sin \frac{1}{2}(A-B)}$$

which becomes formula 2 when BP is replaced by its value (1).

V-FORMULAS 2 TO 4 OF ART. 23

We have (formula 8, Art. 17),

$$2\cos^3 \frac{1}{2}A = 1 + \cos A$$

or, substituting the value of $\cos A$ from formula 1. Art. 23.

$$2\cos^{2} \frac{1}{2}A = 1 + \frac{b^{2} + c^{2} - a^{2}}{2 b c} = \frac{2 b c + b^{2} + c^{2} - a^{2}}{2 b c} = \frac{(b + c)^{2} - a^{2}}{2 b c}$$

or, remembering that the difference between the squares of two numbers is equal to their sum multiplied by their difference,

$$2\cos^2 \frac{1}{2} A = \frac{(b+c+a)(b+c-a)}{2 b c}$$
(1)

Now, since a + b + c = 2s, we have, subtracting 2a from both members, b + c - a = 2s - 2a = 2(s - a). Likewise, a + b - c = 2(s - c), and a + c - b = 2(s - b). Substituting these values in equation (1),

$$2\cos^{*}\frac{1}{2}A = \frac{2s \times 2(s-a)}{2bc} = \frac{2s(s-a)}{bc}$$

$$\cos \frac{1}{3} A = \sqrt{\frac{s(s-a)}{bc}}$$
 (2)

13 - 13 - 13

whence,

which is formula 3, Art. 23.

Likewise (formula 7, Art. 17),

$$2 \sin^{2} \frac{1}{2} A = 1 - \cos A = 1 - \frac{b^{2}}{2bc}$$

$$= \frac{2bc - b^{2} - c^{2} + a^{2}}{2bc} = \frac{a^{2} - (b^{2} - 2bc + c^{2})}{2bc} = \frac{a^{2} - (b - c)^{2}}{2bc}$$

$$= \frac{(a + b - c)(a - b + c)}{2bc} = \frac{2(s - c) \times 2(s - b)}{2bc} = \frac{2(s - b)(s - c)}{bc}$$

whence,

$$\ln \frac{1}{2} A = \sqrt{\frac{(s-b)(s-c)}{bc}}$$
(3)

which is formula 4, Art. 23.

Formula 2 is obtained by dividing equation (3) by equation (2). I.I.T. 36F-15

VI-FORMULA OF ART. 30

Formulas 3 and 4 of Art. 23 are:

$$\sin \frac{1}{2} A = \sqrt{\frac{(s-b)(s-c)}{bc}}$$
(1)

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$
(2)

Also (formula 5, Art. 17),

 $\sin A = 2\sin \frac{1}{2}A\cos \frac{1}{2}A \tag{3}$

Substituting in equation (3) the values of $\sin \frac{1}{4} A$ and $\cos \frac{1}{4} A$ from equations (1) and (2),

$$\sin A = 2 \sqrt{\frac{(s-b)(s-c)}{bc}} \sqrt{\frac{s(s-a)}{bc}} = 2 \sqrt{\frac{s(s-a)(s-b)(s-c)}{b^*c^*}} = 2 \frac{\sqrt{s(s-a)(s-b)(s-c)}}{bc}$$

Substituting this value in formula of Art. 27, $S = \sqrt{s(s-a)(s-b)(s-c)}$

VII-FORMULA 3 OF ART. 33

We have, since $\cot = \frac{\cos}{\sin}$, $\frac{1}{\cot A + \cot B} = \frac{1}{\frac{\cos A}{\sin A} + \frac{\cos B}{\sin B}} = \frac{\sin A \sin B}{\sin B \cos A + \cos B \sin A}$ $= \frac{\sin A \sin B}{\sin (A + B)}$ By substituting this value in formula 1, we obtain $S = \frac{(b_1 - b_2)(b_1 + b_3) \sin A \sin B}{\sin A \sin B}$

$$2\sin(A+B)$$

VIII-FORMULA OF ART. 34

Let the area of the triangle A DB', Fig. 18, be denoted by T, and that of the parallelogram B C DB' by P. Then,

$$S = P + T \qquad (1)$$
$$P = b_a h, T = \frac{1}{2} dh$$

Dividing the first of these equations by the second,

$$\frac{P}{T} = \frac{b_s}{\frac{1}{2}d} = \frac{2b_s}{d} = \frac{2b_s}{b_1 - b_s}$$
$$P = \frac{2b_s}{b_s - b_s}T$$

whence,

Now.

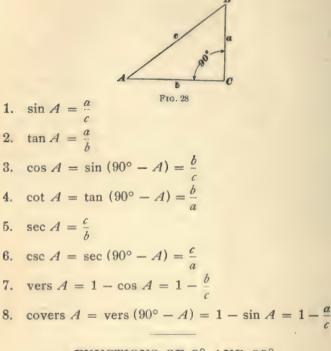
Substituting this value of
$$P$$
 in equation (1),

$$S = \frac{2b_{z}}{b_{1} - b_{z}}T + T = \left(\frac{2b_{z}}{b_{1} - b_{z}} + 1\right)T = \frac{b_{1} + b_{z}}{b_{1} - b_{z}}T = \frac{b_{1} + b_{z}}{d}T \qquad (2)$$
Let $\frac{1}{2}(a + c + d) = s$. Then (formula of Art. 30),
 $T = \sqrt{s(s - a)(s - c)(s - d)}$
and, substituting this value in equation (2),
 $S = \frac{b_{1} + b_{z}}{d}\sqrt{s(s - a)(s - c)(s - d)}$

TABLE OF TRIGONOMETRIC FORMULAS

The principal formulas occurring in the text, and others that can be readily derived from these, are tabulated in the following pages for convenient reference. As these formulas, which include those for the solution of triangles, are here systematically classified and arranged, the student will find this table useful in the solution of all kinds of problems requiring the application of trigonometry. He is advised to refer to it often, so as to become familiar with its contents and use.

FORMULAS DEFINING THE TRIGONOMETRIC FUNCTIONS



FUNCTIONS OF 0° AND 90°

9.	sin	0°	=	0	15.	sin	90°	=	1
10.	tan	0°	=	0	16.	tan	90°	=	00
11.	cos	0°	=	1	17.	cos	90°	=	0
12.	cot	0°	=	00	18.	cot	90°	=	0
13.	sec	0°	=	1	19.	sec	90°	=	00
14.	csc	0°	=	00	2 0.	csc	90°	=	1

FUNCTIONS OF NEGATIVE ANGLES

22. $\tan (-A) = -\tan A$ 25. $\sec (-A) = \sec A$ 23. $\cos (-A) = \cos A$ 26. $\csc (-A) = -\csc A$	21.	sin (.	-A) =	$= - \sin A$	24. $\cot(-A) = -\cot A$
23. $\cos(-A) = \cos A$ 26. $\csc(-A) = -\csc A$	22.	tan (-A) =	= - tan A	25. $\sec(-A) = \sec A$
	23.	cos (-	(-A) =	cos A	26. $\csc(-A) = -\csc A$

PLANE TRIGONOMETRY, PART 2

FUNCTIONS OF $90^\circ + A$

27. $\sin (90^{\circ} + A) = \cos A$ 30. $\cot (90^{\circ} + A) = -\tan A$ 28. $\tan (90^{\circ} + A) = -\cot A$ 31. $\sec (90^{\circ} + A) = -\csc A$ 29. $\cos (90^{\circ} + A) = -\sin A$ 32. $\csc (90^{\circ} + A) = \sec A$

FUNCTIONS OF $180^\circ - A$ AND OF $180^\circ + A$

 $\sin (180^\circ - A) = \sin A$ 33 34. $\tan(180^\circ - A) = -\tan A$ $\cos(180^\circ - A) = -\cos A$ 35. $\cot (180^\circ - A) = -\cot A$ 36 $\sec (180^\circ - A) = -\sec A$ 37. $\csc(180^\circ - A) = \csc A$ 38. $\sin (180^\circ + A) = -\sin A$ 39 40. $\tan(180^\circ + A) = \tan A$ 41. $\cos(180^\circ + A) = -\cos A$ 42. $\cot (180^\circ + A) = \cot A$ 43 $\sec (180^{\circ} + A) = -\sec A$ $\csc(180^\circ + A) = -\csc A$ 44.

FUNCTIONS OF $360^\circ - A$ AND OF $360^\circ + A$

45. $\sin (360^\circ - A) = -\sin A$	4 51. $\sin(360^\circ + A) = \sin A$
46. $\tan(360^\circ - A) = -\tan A$	4 52. $\tan(360^\circ + A) = \tan A$
47. $\cos(360^\circ - A) = \cos A$	53. $\cos(360^\circ + A) = \cos A$
48. $\cot(360^\circ - A) = -\cot A$	4 54. $\cot(360^\circ + A) = \cot A$
49. $\sec(360^\circ - A) = \sec A$	55. $\sec(360^\circ + A) = \sec A$
50. $\csc(360^\circ - A) = -\csc A$	4 56. $\csc(360^\circ + A) = \csc A$

FUNCTIONS OF (A + B) AND OF (A - B)

57. $\sin (A + B) = \sin A \cos B + \cos A \sin B$ 58. $\sin (A - B) = \sin A \cos B - \cos A \sin B$ 59. $\cos (A + B) = \cos A \cos B - \sin A \sin B$ 60. $\cos (A - B) = \cos A \cos B + \sin A \sin B$ 61. $\tan (A + B) = \frac{\tan A + \tan B}{1 - \tan A \tan B}$ 62. $\tan (A - B) = \frac{\tan A - \tan B}{1 + \tan A \tan B}$

FUNCTIONS OF 2 A AND OF $\frac{1}{2}A$

63.	$\sin 2A = 2 \sin A \cos A$
64.	$\cos 2A = \cos^2 A - \sin^2 A$
65.	$\cos 2A = 2\cos^2 A - 1$
66.	$\cos 2A = 1 - 2 \sin^{\circ} A$
67.	$\tan 2A = \frac{2\tan A}{1-\tan^{*}A}$
6 8.	$\sin \frac{1}{2}A = \sqrt{\frac{1 - \cos A}{2}}$
69.	$\cos \frac{1}{2}A = \sqrt{\frac{1+\cos A}{2}}$
70.	$\tan \frac{1}{2}A = \sqrt{\frac{1 - \cos A}{1 + \cos A}}$
71.	$\tan \frac{1}{2}A = \frac{1 - \cos A}{\sin A}$

SUMS AND DIFFERENCES OF FUNCTIONS

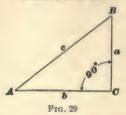
72. $\sin A + \sin B = 2 \sin \frac{1}{2}(A + B) \cos \frac{1}{2}(A - B)$ $\sin A - \sin B = 2 \sin \frac{1}{2}(A - B) \cos \frac{1}{2}(A + B)$ 73. 74. $\cos A + \cos B = 2 \cos \frac{1}{2}(A + B) \cos \frac{1}{2}(A - B)$ $\cos A - \cos B = 2 \sin \frac{1}{2}(A + B) \sin \frac{1}{2}(B - A)$ 75. $\tan A + \tan B = \frac{\sin (A+B)}{\sin (A+B)}$ 76. $\cos A \cos B$ $\tan A - \tan B = \frac{\sin (A - B)}{\sin (A - B)}$ 77. $\cos A \cos B$ 78. $\sin^{\circ} A - \sin^{\circ} B = \sin \left(A + B\right) \sin \left(A - B\right)$ $\cos^{*} A - \cos^{*} B = \sin \left(A + B\right) \sin \left(B - A\right)$ 79. $\cos^2 A - \sin^2 B = \cos \left(A + B\right) \cos \left(A - B\right)$ 80

	$\csc A =$	106. $\frac{1}{\sin A}$	$102. \sqrt{1 + \tan^3 A} \ 107. \frac{\sqrt{1 + \tan^3 A}}{\tan A}$	$108.\frac{1}{\sqrt{1-\cos^{*}A}}$	99. $\frac{1}{\sqrt{\sec^{*}A - 1}} \left[104. \frac{\sqrt{1 + \cot^{*}A}}{\cot A} \right] 109. \sqrt{1 + \cot^{*}A}$	90. $\frac{1}{\sqrt{\csc^* A - 1}} 95. \frac{\sqrt{\csc^* A - 1}}{\csc A} 100. \sqrt{\csc^* A - 1} 105. \frac{\csc A}{\sqrt{\csc^* A - 1}} 110. \frac{\sec A}{\sqrt{\sec^* A - 1}}$
ALD AN ALOUR	$\sec A =$	$101.\frac{1}{\sqrt{1-\sin^{*}A}}$	$102.\sqrt{1+\tan^{3}A}$	103. $\frac{1}{\cos A}$	$104, \frac{\sqrt{1} + \cot^4 A}{\cot A}$	$105.\frac{\csc A}{\sqrt{\csc^{*}A-1}}$
TO ONOTIONO	$\cot A =$	$96. \frac{\sqrt{1-\sin^3 A}}{\sin A}$	$\frac{1}{\tan A}$	$98. \frac{\cos A}{\sqrt{1 - \cos^2 A}}$	$9. \frac{1}{\sqrt{\sec^3 A - 1}}$	100. Vese ^a A - 1
KELATIONS AMONG THE FUNCTIONS OF AN ANGLE	$\cos A =$	81. $\frac{\tan A}{\sqrt{1 + \tan^* A}} 86. \frac{\sin A}{\sqrt{1 - \sin^* A}} 91. \sqrt{1 - \sin^* A} 96. \frac{\sqrt{1 - \sin^* A}}{\sin A} 901. \frac{1}{\sqrt{1 - \sin^* A}} 101. \frac{1}{\sqrt{1 - \sin^* A}} 106. \frac{1}{\sin A}$	82. $\sqrt{1 - \cos^3 A}$ 87. $\frac{\sqrt{1 - \cos^3 A}}{\cos A}$ 92. $\frac{1}{\sqrt{1 + \tan^3 A}}$ 97.	93. $\frac{\cot A}{\sqrt{1 + \cot^* A}}$ 98. $\frac{\cos A}{\sqrt{1 - \cos^* A}}$ 103.	$\frac{1}{\sec A}$	$95. \frac{\sqrt{\csc^3 A - 1}}{\csc A}$
KELATIONS	$\tan A =$	$86. \frac{\sin A}{\sqrt{1-\sin^* A}}$	$87. \frac{\sqrt{1-\cos^2 A}}{\cos A}$	$\frac{1}{\cot A}$	84. $\frac{\sqrt{\sec^{\circ} A - 1}}{\sec A}$ 89. $\sqrt{\sec^{\circ} A - 1}$ 94.	90. $\frac{1}{\sqrt{\csc^{*}A-1}}$
	$\sin A =$	$\frac{\tan A}{\sqrt{1+\tan^* A}}$	$\sqrt{1-\cos^{*}A}$	$83. \frac{1}{\sqrt{1 + \cot^2 A}} 88.$	$\frac{\sqrt{\sec^4 A - 1}}{\sec A}$	85. $\frac{1}{\csc A}$
		81.	82.	83.	84.	85.

RELATIONS AMONG THE FUNCTIONS OF AN ANGLE

PLANE TRIGONOMETRY, PART 2

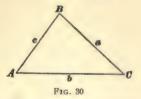
FORMULAS FOR THE SOLUTION OF RIGHT TRIANGLES



Given	Required	Formula
a, A	B, b, c	$\begin{cases} 111. B = 90^{\circ} - A \\ 112. b = a \cot A \\ 113. c = \frac{a}{\sin A} = a \csc A \end{cases}$
a, B	A, b, c	$\begin{cases} 114. A = 90^{\circ} - B \\ 115. b = a \tan B \\ 116. c = \frac{a}{\cos B} = a \sec B \end{cases}$
с, А	B, a, b	$\begin{cases} 117. B = 90^{\circ} - A \\ 118. a = c \sin A \\ 119. b = c \cos A \end{cases}$
a, b	A, B, c	$\begin{bmatrix} 113. & c &= \frac{1}{\sin A} = a \csc A \\ 114. & A = 90^{\circ} - B \\ 115. & b &= a \tan B \\ 115. & b &= a \tan B \\ 116. & c &= \frac{a}{\cos B} = a \sec B \\ \\ \begin{bmatrix} 117. & B = 90^{\circ} - A \\ 118. & a &= c \sin A \\ 119. & b &= c \cos A \\ \\ 120. & \tan A &= \frac{a}{b} \\ 121. & \tan B &= \frac{b}{a}, \text{ or } B &= 90^{\circ} - A \\ \\ 122. & c &= \sqrt{a^{\circ} + b^{\circ}} \\ 123. & c &= \frac{a}{\sin A} = a \csc A \\ \\ \\ \begin{bmatrix} 124. & \sin A &= \frac{a}{c} \\ 125. & \cos B &= \frac{a}{c}, \text{ or } B &= 90^{\circ} - A \\ \\ 126. & b &= \sqrt{c^{\circ} - a^{\circ}} = \sqrt{(c + a)(c - a)} \\ 127. & b &= a \cot A \\ \end{bmatrix}$
a, c	A, B, b	$\begin{cases} 124. & \sin A = \frac{a}{c} \\ 125. & \cos B = \frac{a}{c}, \text{ or } B = 90^{\circ} - A \\ 126. & b = \sqrt{c^{\circ} - a^{\circ}} = \sqrt{(c+a)(c-a)} \\ 127. & b = a \cot A \end{cases}$

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FORMULAS FOR THE SOLUTION OF OBLIQUE TRIANGLES



Given	Required	Formulas
a, b, C	A, B, c	$\begin{cases} 128. \begin{cases} \tan \frac{1}{2}(A-B) = \frac{a-b}{a+b} \cot \frac{1}{3}C\\ A = (90^{\circ} - \frac{1}{2}C) + \frac{1}{3}(A-B)\\ B = (90^{\circ} - \frac{1}{2}C) - \frac{1}{2}(A-B)\\ 129. c = \frac{(a-b)\cos \frac{1}{3}C}{\sin \frac{1}{2}(A-B)}\\ 130. c = \sqrt{a^{\circ} + b^{\circ} - 2 ab \cos C} \end{cases}$
c, A, B	C, a, b	$\begin{cases} 131. C = 180^{\circ} - (A + B) \\ 132. a = \frac{c}{\sin C} \sin A \\ 133. b = \frac{c}{\sin C} \sin B \end{cases}$
a, b, A	В, С, с	$\begin{cases} 134. & \sin B = \frac{b}{a} \sin A \\ 135. & C = 180^{\circ} - A - B \\ 136. & c = \frac{a}{\sin A} \sin C \end{cases}$
a, b, c $\frac{1}{2}(a+b+c) = s$	А	$\begin{cases} 137. \ \tan \frac{1}{2} A = \sqrt{\frac{(s-b)(s-c)}{s(s-a)}} \\ 138. \ \cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}} \\ 139. \ \cos A = \frac{b^s + c^s - a^s}{2 b c} \end{cases}$



NATURAL TRIGONOMETRIC FUNCTIONS



,	0	D	I	0	2	D	3	ø	4	10	,
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
0	.00000	1.	.01745	.99985	.03490	.99939	.05234	.99863	.06976	.99756	60
I	.00029	Ι.	.01774	.99984	.03519	.99938	.05263	.99861	.07005	-99754	59 58
2	.00058	I. I.	.01803	.99984 .99983	.03548	·99937 ·99936	.05292	.99860	.07034	-99752 -99750	58
4	.00116	I.	.01862	.00083	.03606	.99935	.05350	.99857	.07092	.99748	56
5	.00145	1.	.01891	.00082	.03635	.99934	.05379	.99855	.07121	.99746	55
	.00175	1. I.	.01920	.99982 .99981	.03664	.99933 .99932	.05408	.99854 .99852	.07150	-99744	54
78	.00233	1.	.01949	.99980	.03093	.99932	.05437	.99851	.07179	.99742	53 52
ÿ	.00262	I.	.02007	.99980	.03752	.99930	.05495	.99849	.07237	.99738	51
10	.00291	Ι.	.02036	.99979	.03781	,99929	.05524	.99847	.07266	.99736	80
11 12	.00320	999999	.02065	·99979 ·99978	.03810	.99927 .99926	.05553	.99846	.07295	·99734 ·99731	40 48
13	.00378	-999999	.02123	.999977	.03868	.99925	.05611	.99842	.07353	.99729	47
14	.00407	00000	.02152	.99977	.03897	.99924	.05640	.99841	.07382	.99727	46
15	.00436	99999	.02181	.99976	.03926	.99923	.05669	.99839 .99838	.07411	.99725	48
10	.00465	999999	.02211	.99976 .99975	.03955	.99922 .99921	.05698	.99838 .99836	.07440	.99723 .99721	44 43
17 18	.00524	999999	.02269	-99975	.04013	.999910	.05756	.99834	.07498	.99719	42
19	.00553	.99998	.02298	.99974	.04042	.999918	.05785	.99833	.07527	.99716	41
20	.00582	.99998	.02327	·99973	.04071	.99917	.05814	.99831	.07556	.99714	10
21	.00611	.999998	.02356	.99972	.04100	.999916	.05844	.99829	.07585	.99712	39
22 23	.00640	80000.	.02385	.99972 .99971	.04129	.99915	.05873	.99827 .99826	.07614	.99710 .99708	38 37
24	.00009	.99998	.02443	.99971	.04188	.99913	.05931	00824	.07672	.99705	36
25	.00727	.99997	.02472	.00060	.04217	11000.	.05960	.99822	.07701	.99703	35
26	.00756	00007	.02501	.99969	.04246	.999910	.05989	.99821	.07730	.99701	34
27	.00785	·99997	.02530	.99968 .99967	.04275	.99900 .99907	.06018	.99819 .99817	.07759 .07788	.99699 .99696	33
20	.008.14	.99996	.02589	.99966	.04333	.99906	.06076	.99815	.07817	.99694	31
30	.00873	.99996	.02618	.99966	.04362	-999905	.06105	.99813	.07846	.99692	30
31	.00902	.999996	.02647	.99965	.04391	.99904	.06134	.99812	.07875	.99689	20 28
32	.00931	.99996	.02676	.99964 .99963	.04420	.99902 .99901	.06163	.99810 .99808	.07904	.99687 .99685	27
34	.00989	.999995	.02734	.99963	.04478	.99900	.06221	.99806	.07962	.99683	26
35	.01018	.99995	.02763	.99962	.04507	.99898	.06250	.99804	.07991	.99680	25
36	.01047	.99995	.02792	.99961 .99960	.04536	.99897 .99896	.06279 .06308	.99803 .99801	.08020	.99678 .99676	24
37	.011070	·99994	.02850	.99959	.04505	.99894	.00308	.99799	.08078	.99673	22
39	.01134	00004	.02879	.99959	.04623	.99893	.06366	.99797	.08107	00671	21
40	.01164	-99993	.02908	.99958	.04653	.99892	.06395	.99795	.08136	.99668	20
41	.01193	199093	.02938	-99957	.04682	.99890	.06424	.99793	.08165	.99666	19 18
42 43	.01223	-99993 199992	.02907	.99956 .99955	.04740	.99888	.00453	.99792 .99790	.08223	.99661	17
44	.01280	.99992	.03025	.99954	.04769	.99886	.06511	.99788	.08252	.99659	10
45	.01309	100001	.03054	.99953	.04798	.99885	.06540	.99786	.08281	.99657	15
46	.01338	.99991 .99991	.03083	.99952 .99952	.04827	.99883 .99882	.06569	.99784	.08310 .08339	.99654 .99652	14 13
47	.01307	.999991	.03141	.99951	.04885	18800.	.06590	.99780	.08368	.99649	13
145	.01425	100000	.03170	.99950	.04914	.00870	.06656	.99778	.08397	.99647	11
50	.01454	.99989	.03199	99949	.04943	.99878	.06685	.99776	.08426	.99644	10
51 52	.01483	.99989 .99989	.03228	.99948	.04972 .05001	.99876 .99875	.06714	-99774 -99772	.08455	.99642	9
52	.01542	00088	.03257	.99947	.05030	.99873	.06773	.99770	.08513	.99637	2
54	.01571	.00088	.03316	.99945	.05059	.99872	.06802	.99768	.08542	.99635	ő
55 56	.01600	.99987	.03345	.99944	.05088	.99870 .99869	.06831 .06860	.99766	.08571	.99632	5
50 57	.01029	.00086	.03374	.99943 .99942	.05117	.99809	.00800	.99704	.08000	.99630	A B
58	.01687	.999986	.03432	.99941	.05175	.99866	.06918	.99760	.08658	.99625	3
59	.01716	.99985	.03461	.99940	.05205	.99864	.06947	.99758	.08687	.99622	1
60	.01745	.99985	.03490	.99939	.05234	.99863	.06976	.99756	.08716	.99619	0
,	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	,
1	89	0	88	30	8;	,0	80	50	8	50	,

,	5	0	6	0	7	0	8	0	9	0	,
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
0	.08716	.99619 .90617	.10453	.99452	.12187	.99255 .00251	.13917	.99027	.15643	.98769	60
1 3	.08774	.99614	.10511	.99449 .99446	.12245	.99251	.13946	.99023	.15672	.98764	59 58
3	.05803	.99612	.10540	.99443	.12274	.99244	.14004	.99015	.15730	.98755	57
4	.08831	.996c9	.10569	.99440 .99437	.12302	.99240	.14033	.99011	.15758	.98751 .98746	56 55
5	.08889	.99604	.10626	.99434	.1 1360	.99233	.14090	.99002	.15816	.98741	55
7	.08918	.99602	.10655	.99431	.12389	.99230	.14119	.98998	.15845	.087.37	53
	.08947	.99596	.10684	.99428	.12418	.99226	.14148	.98994	.15873	.98732 .98728	51
m	.09005	.99594	.10742	.99424	.12476	.99219	.14205	.98986	.15931	.98723	51
11	.09034	.99591	.10771	.99418	.12504	.99215	.14234	.98982	.15959	.98718	49
12	.09063	.99588	.10800	.99415	.12533	.99211	.14263	.9 1978	.15988	.98714	48
13 14	.09092	.99586 .99583	.10829	.99412 .99409	.12562	.99208	.14292	.98973	.16017	.98709 .98704	47 46
14	.09150	.99580	.10887	.99409	.12591	.99204	.14349	.08965	.16074	.98704	40
16	.09179	.99578	.10916	.99402	.12649	.99197	.14378	.98961	.16103	.98695	84
17	.09208	-99575	.10945	.99399	.12678	.99193	.14407	.98957	.16132	.98690	163
18	.09237	.99572 .99570	.10973	.99396 .99393	.12706	.99189 .99186	.14436	.9895.3 .98948	.16160	.98686 .98681	43
20	.09295	.99567	.11031	.99390	.12764	.99182	.14493	.98944	.16218	.98676	HU
21	.09324	.99564	.11060	.99386	.12793	.99178	.14522	.98940	.16246	.98671	39
22	.09353	.99562	.11089	.99383	.12822	.99175	.14551	.98936	.16275	.98667	38
23	.09382	-99559 -99556	.11118	.99380 .99377	.12851	.99171	.14580	.98931	.16304	.98662	37
25	.09411	.99553	.11147	.99377	.12000	.99107	.14000	.98927	.16333	.98652	36 35
25	.09469	.99551	.11205	.99370	.12937	.99160	.14600	.98919	.16390	.086.18	33
27	.09498	.99548	.11234	.99367	.12966	.99156	.14695	.98914	.16419	.98643	33
	.09527	-99545	.11263	.99364	.12995	.99152	.14723	01080.	.16447	.98638	32
29 30	.09556	.99542 .99540	.11291	.99300	.13024	.99148 .99144	.14752 .14781	.98900	.16505	.98633 .98629	31 30
31 33	.09614	·99537 ·99534	.11349	·99354 ·99351	.13081	.99141 99137	14810	.98897	.16533	.98624	10
37	09042	\$9534 \$9531	.11407	99351	.13139	.99133	.14867	.98889	.16591	.98614	27
34	.09700	.99528	.11436	.99344	,13168	.991 29	.14896	.98884	.166.20	.98609	20
35	.09729	.99526	.11465	.99341	.13197	.99125	.14925	.98880	.10648	.98604	25
30	.09758	.99523 .99520	.11494	·99337 ·99334	.13226	.99122 .99118	.14954	.98871	.16706	.98600	24 123
18	.09816	.99517	.11552	.99331	.13283	.99114	.15011	.98867	.16734	.98590	21
39	.09845	.99514	.11580	.99327	.13312	.99110	.15040	.98863	.16763	.98585	21
NG.	.09874	.99511	.11609	.99324	.13341	.99106	.15069	.98858	.16792	.98580	20
41 43	.09932	.99508	.11638	.99320	.13370	.99102 .99098	.15097	.98854	.16820	.98575 .98570	19 18
	.09932	.99503	.11696	.99314	.13427	199093	.15120	.98845	.16878	.98565	10
84	000000	.99500	.11725	.99310	.13456	10000.	.15184	.98841	.16906	.08561	17 16
45	.10019	.99497	.11754	.99307	.13485	.99087	.15212	.98836	.16935	.98556	KS.
40	.10048	.99494 .99491	.11783	.99303	.13514	.99083	.15241	.98832 .98827	.16964	.98551	14
47	.10106	.99488	.11840	.99297	.13543	.99075	.15299	.98823	.17021	.98541	13 TH
49	.10135	.99485	.11869	.99293	.13600	.99071	.15327	.98818	.17050	.98536	11
50	.10164	.99482	.11898	.99290	.13629	.99067	.15356	.93814	.17078	.98531	10
SI	.10192	.99479	.11927	.99286	.13658	.99063	.15385	.98809	.17107	.98526	9
52	.10221	.99476	.11950	.99283	.13687	.99059	.15414	.98805	.17136	.98521	
54	.10279	.99473	.12014	.99276	.13744	.99051	.15471	.08796	.17193	.98511	7
55	.10308	.99467	.12043	.99272	.13773	.99047	°.15500	.98791	.17222	.98506	A
86	.10337	.99464 .99461	.12071	.99269	.13802	.99043	.15529	.98787	.17250	.98501	4
57 58	.10300	.99458	.12100	.99262	.13860	.99039	.15586	.98778	.17308	.98491	
59	.10424	.99455	.12158	.99258	.13889	.99031	.15615	.98773	.17336	.98486	I
60	.10453	.99452	.12187	.99255	.13917	.99027	.15643	.98769	.17365	.98481	0
,	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	1
	8.	4°	8	3°	- 8:	20	8	0	8	0°	

,	10	,°	II	0	12	20	13	°	I	4°	,
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
· 0	.17365	.98481	.19081	.98163	.20791	.97815	.22495	-97437	.24192	.97030	60
I	.17393	.98476	.19109	.98157	.20820	.97809	.22523	.97430	.24220	.97023	19 58
2	.17422	.98471 .98466	.19138	.98152 .98146	.20848	.97803 .97797	.22552	.97424 .97417	.24249	.97015	58 57
4	.17479	.98461	.19195	.98140	.20005	-97791	.22608	.97417	.24305	.97008	50
S	.17508	.98455	.19224	.98135	.20933	.97784	.22637	.97404	.24333	.96994	55
	.17537	.98450	.19252 .19281	.98129 .98124	.20962	.97778	.22665	.97398	.24362	.96987 .96980	54
7	.17565	.98440	.19201	.98118	.20990	.97772 .97766	.22093	.97391 .97384	.24390	.96973	51 52
ø	.17623	.98435	.19338	.98112	.21047	.97760	.22750	.97378	.24446	.96966	SI
10	.17651	.98430	.19366	.98107	.21076	-97754	.22778	.97371	.24474	.96959	50
11 12	.17680	.98425	.19395	.98101	.21104	.97748	.22807	.97365	.24503	.96952	49
13	.17708	.98414	.19423	.98090	.21134	·97742 ·97735	.22863	.97358 .97351	.24531	.96945 .96937	47
14	.17766	.98409	.19481	.98084	.21189	.97729	.22892	.97345	.24587	.96930	46
15	.17794	.98404	.19509	.98079	.21218	.97723	.22920	.\$7338	.24615	.96923	45
16 17	17852	.98399 .98394	.19538	.98073	.21246	-97717 -97711	.22948	.97331 .	.24644	.96916	43
18	.17880	.98389	.19595	.98061	.21303	.97705	.23005	.97345	.24700	.96902	43
19	.17909	.98383	.19623	.98056	.21331	.97698	.23033	.97311	.24728	.96894	41
20	.17937	.98378	.19652	.98050	.21360	.97692	.23062	.97304	.24756	.96887	40
21	.17966	.98373	.19680	.98044	.21388	.97686	.23090	.97298	.24784	.96880	39
23	.17995	.98368	.19709	.98039 .98033	.21417	.97680	.23118	.97291 .97284	.24813	.96873	18 37
24	.18052	.98357	.19766	.98027	.21474	.97667	.23175	.97278	.24869	.96858	36
25	.18081	.98352	.19794	.98021	.21502	.97661	.23203	.97271	.24897	.96851	35
26	.18109	.98347 .98341	.19823	.98016	.21530	.97655	.23231	.97264	.24925	.96844	34
27	.18166	.08336	.19851	.98010	.21559 .21587	.97648	.23200	.97257 .97251	.24954 .24982	.90837	33 32
29	.18195	.9833I	.19908	.97998	.21616	.97636	.23316	.97244	.25010	.96822	31
30	.18224	.98325	.19937	.97992	.21644	.9763c	.23345	.97237	.25038	.96815	30
31	.18252	.98320	.19965	.97987	.21672	.97623	.23373	.97230	.25066	.96807	29
32	.18281	.98315 .98310	.19994	.97981 .97975	.21701	.97617 .97611	.23401	.97223	.25094	.96800 .96793	27
34	.18338	.98304	.20051	.97969	.21758	.97604	.23458	.97210	.25151	.96786	26
35	.18367	.98299	.20079	.97963	.21786	.97598	.23486	.97203	.25179	.96778	25
36 37	.18395	.98294	.20108	.97958 .97952	.21814	.97592 .97585	.23514	.97196	.25207	.96771	23
38	.18452	.98283	.20165	.97946	.21871	.97579	.23571	.97182	.25263	.96756	23
39	.18481	.98277	.20193	.97940	.21899	.97573	.23599	.97176	.25291	.96749	21
40	.18509	.98272	.20222	.97934	.21928	.97566	.23627	.97169	.25320	.96742	190
41	.18538	.98267 .98261	20250	.97928	.21956	.97560	.23656	.97162	.25348	.96734	19 18
43	.18595	.98201	.20279	.97922 .97916	.21985	-97553 -97547	.23684	.97155 .97148	.25376	.96727	10
44	.18624	.98250	.20336	.97910	.22041	.9754I	.23740	.97141	.25432	.96712	16
45	.18652	.98245	.20364	.97905	.22070	-97534	.23769	.97134	.25460	.96705	15
40	.18681	.98240 .98234	.20393	.97899 .97893	.22098	.97528 .97521	.23797	.97127 .97120	.25488 .25516	.96697 .96690	14
48	.18738	.98229	.20450	.07887	.22155	.97515	.23853	.97113	.25545	.96682	13
49	.18767	.98223	.20478	.97881	.22183	.97508	.23882	.97106	25573	.96675	11
50	.18795	.98218	.20507	.97875	.22212	.97502	.23910	.97100	.25601	.96667	10
51	.18824	.98212	.20535	.97869	.22240	.97496	.23938	.97093 .97086	.25629	.96660	9
52	.18852	.98207	.20563	.97803	.22208	.97489	.23966	.97080	.25057	.96645	
54	.18910	.98196	.20620	.97851	.22325	.97476	.24023	.97072	.25713	.96638	76
55	.18938	.98190	.20649	.97845	.22353	.97470	.24051	.97065	.25741	.96630	5
50	.18967	.98185	.20677	.97839	.22382	.97463 .97457	.24079	.97058 .97051	.25769 .25798	.90023	N D
57 58	.19024	.98174	.20734	.97827	.22438	.97450	.24136	.97044	.25820	.96608	2
59	.19052	.98168	.20763	.97821	.22467	.97444	.24164	.97037	.25854 .25882	.96600	I
-											
1	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	1
	7	9°	7	8°	7	7°	7	6°	7	5°	

,	I	5°	1	6°	I	70	1	80	I	9°	,
	Sine	Cosine									
0	.25882	.96593	.27564	.06126	.29237	.95630	CHOQUES	.05106	.32557	.94552	60
E .	.25910	.96585	.27592	.96118	.29265	.95622	.30929	.95097	.32584	.94542	59
	.25938	.96578	.27620	.96110	.29293	.95613	.30957	.95088	.32612	-94533	58
в	.25966	.96570	.27648	.96102	.29321	.95605	.30985	.95079	.32639	-94523	57
	.25994	.96562	.27676	.96094	.29348	.95596	.31012	.95070	.32667	.94514	56
56	.26022	.96555 .96547	.27704	.96078	.29376	.95588 -95579	.31040	.95061 .95052	.32694	.94504 .94495	55
	.26079	.96540	.27759	.96070	.29432	.95571	.31095	.95043	.32749	.94495	54 83
78	.26107	.96532	.27787	.96062	.29460	.95562	.31123	.95033	.32777	.94476	52
9	.26135	.96524	.27787	.96054	.29487	.95554	.31151	.95024	.32777 .32804	.94466	51
10	.26163	.96517	.27843	.96046	.29515	-95545	.31178	.95015	.32832	-94457	20
11	.26191	.96509	.27871	.96037	.29543 .29571	.95536	.31206	.95006	.32859	.94447	40
13	.26247	.96494	.27027	.90029	.29599	.95510	.31233	.94997	.32007	.94438 .94428	47
14	.26275	.96486	.27955	.96013	.20626	.95511	.31289	.94979	.32942	.94418	46
15	.26303	.96479	.27983	.96005	.29654	.95502	.31316	.94970	.32969	04409	45
16	.26331	.96471	.28011	.95997	.29682	.95493	.31344	.94961	.32997	.94399	44
17	.26359	.96463	.28039	.95989	.29710	.95485	.31372	.94952	.33024	.94390	143
18	.26387	.96456	.28067	.95981	.29737	.95476	.31399	.94943	.33051	.94380	43
20	.26415	.90440	.28095	.95972 .95964	.29765 .29793	.95467 .95459	.31427 .31454	.94933 .94924	.33079 .33106	.94370 .94361	41
21	.26471	.96433	.28150	.95956	.29821	.95450	.31482	.94915	.33134	.94351	35
22	.26500	.96425	.28178	.95948	.29849	.95441	.31510	.94906	.33161	.94342	39
23	.26528	.96417	.28206	.95940	.29876	.95433	.31537	.94897	.33189	.94332	37
24	.26556	.96410	.28234	.95931	.29904	.95424	.31565	.94888	.33216	.94322	36
25	.26584	.96402	.28262	.95923	.29932	.95415	.31593	.94878 .94869	.33244	.94313	35
	.20012	.96394 .96386	.28318	.95915 .95907	.29960	.95407 .95398	.31648	.94869	.33271 .33298	.94303	34 33
27	.26668	.96379	.28346	.95898	.30015	.95389	.31675	.94851	.33296	.94293	32
20	.26696	.96371	.28374	.95890	.30043	.95380	.31703	.94842	.33353	.94274	31
30	.26724	.96363	.28402	.95882	.30071	.95372	.31730	.94832	.33381	.94264	30
31	.26752	.96355	.28429	.95874	.30098	.95363	.31758	.94823	.33408	.94254	29
32	.26780	.96347	.28457	.95865	.30126	-95354	.31786	.94814	.33436	.94245	18
33	,268,36	.96332	.28513	.95849	.30154	-95345 -95337	.31841	.94005	.33463 .33490	.94235	27
	,26864	.96324	.28541	.95841	.30209	.95328	.31868	.94786	.33518	.94215	25
35 36	.26892	.96316	.28569	.05832	.30237	.95319	.31896	.94777	.33545	.94206	24
37	.26920	.96308	.28597	.95824	.30265	.95310	.31923	.94768	.33573	.94196	23
	.26948	.96301	.28625	.95816	.30292	.95301	.31951	.94758	.33600	.94186	22
19 40	.26976 .27004	.96293 .96285	.28652 .28680	.95807 •95799	.30320 .30348	.95293 .95284	.31979 .32006	-94749 -94740	.33627 .33655	.94176 .94167	21 20
41	.27032	.96277	.28708	.95791	.30376	.95275	.32034	.94730	.33682	.94157	10
43	.27060	.96269	.28736	.95782	.30403	.95266	.32061	.94721	.33710	.94147	18
143	.27088	.96261	.28764	.95774	.30431	.95257	.32089	.94712	.33737	.94137	17
44	.27116	.96253	.28792	.95766	.30459	.95248	.32116	.94702	.33764	.94127	16
45	.27144	.96246	.28820	.95757	.30486	.95240	.32144	.94693	.33792	.94118	15
46	.27172	.96238 .96230	.28847	·95749 ·95740	.30514	.95231 .95222	.32171	.94684	.33819 .33846	.94108	14
47	.27228	.96222	.28003	.95732	.30544	.95213	.32227	.94665	.33040	.94088	13
49	.27256	.96214	.28931	.95724	.30597	.95204	.32254	.94656	.33901	.94078	
50	.27284	.96206	.28959	.95715	.30625	.95195	.32282	.94646	.33929	.94068	10
51	.27312	.96198	.28987	.95707	.30653	.95186	.32309	.94637	.33956	.94058	9
52	.27340	.96190	.29015	.95698	.30680	.95177	.32337	.94627	.33983	194049	
53	.27368	.96182	.29042	.95690	.30708	.95168	.32364	.94618	.34011	.94039	F 6
55	.27390	.96166	.29070	.95673	.30730	.95159	.32392	.94009	.34036	.94019	5
56	.27452	.96158	.29126	.95664	.30701	.95142	.32447	.94599	.34093	104000	4
57 58	.27480	.96150	.29154	.95656	.30819	.95133	.32474	.94580	.34120	93999	3
58	.27508	.96142	.29182	.95647	.30846	.95124	.32502	.94571	.34147	.93989	2
59	.27536	.96134	120209	.95639	.30874	.95115	.32529	.94561	.34175	.93979	1
00	.27564	.96126	.29237	.95630	.30902	.95106	.33557	.94552	.34202	.93969	0
	Cosine	Sine									
1	74	.0	73	.0	72	0	71	.0	-	0	1
	7	1	7:	- 1	72		71	-	7	0- 1	

r				-								
1	1	20)°	2	L O	2:	20	23	3°	2	4°	1
		Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
ł	0	.34202	.93969	.35837	.93358	.37461	.92718	.39073	.02050	.40674	.91355	50
L	I	.34229	.93959	.35864	.93348	.37488	.92707	.39100	.92039	.40700	.91343	59 58
L		.34257 .34284	.93949 .93939	.35091 .35918	-93337 -93327	-37515 -37542	.92697 .92686	.39127	.92028 .92016	.40727 .40753	.91331	58 57
L	4	.34311	.93939	.35945	.93316	.37569	.92675	.39180	.92005	.40780	.91307	56
L	5	-34339	.93919	.35973	.93306	.37595	.92664	.39207	.91994	.40780	.91295	55
1		-34366 -34393	.93909	.36000	.93295 .93285	.37622	.92653	.39234	.91982	.40833	.91283	54 53
L	7	.34421	.93889	.36054	.93274	.37676	.92631	.39287	.91959	.40886	.91260	52
ł	9	.34448	.93879	.36081	.93264	.37703	.92620	.39314	.91948	.40913	.91248	51
I	10	.34475	.93869	.36108	.93253	.37730	.92609	.39341	.91936	.40939	.91236	50
L	II	.34503	.93859	.36135	.93243	.37757	.92598	.39367	.91925	.40966	.91224	40
ł	E	.34530	.93849 .93839	.36162	.93232	.37784 .37811	.92587	.39394	.91914	.40992	.91212	48
i.	13 14	·34557 ·34584	.93039	.36217	.93222 .93211	.37838	.92576	.39421	.91902	.41019	.91200	47
L	15	.34612	.93819	.36244	.93201	.37865	.92554	.39474	.91879	41072	.91176	45
1	16	.34639	.93809	.36271	.93190	.37892	.92543	.39501	.91868	.41098	.91164	44
	17	.34000	.93799 .93789	.36298	.93180	.37919 .37946	.92532	.39528 .39555	.91850	.41125	.91152	43
1	10	.34721	.93779	.36352	.93159	.37973	.92510	.39581	.01833	.41178	.91128	41
	40	.34748	.93769	.36379	.93148	.37999	.92499	.39608	.91822	.41204	.91116	160
1	31	.34775	.93759	.36406	.93137	.38026	.92488	.39635	.91810	.41231	.91104	39
1	22	.34803	.93748	.36434	.93127	.38053	.92477	.39661	.01700	.41257	.91092	38
ł	23 24	.34830 .34857	.93738	.36461 .36488	.93116	.38080	.92466	.39688	.91787	.41284	.91080	37 36
L	25	.34057	.93728 .93718	.30400	.93100	.38134	.92444	-39715 -39741	.91775	.41310	.91056	30
L	26	.34912	02708	.36542	.93084	.38161	.92432	.39768	.91752	.41363	.91044	34
ł	27 28	-34939 -34966	.93698	.36569 .36596	.93074 .93063	.38188	.92421	·39795 ·39822	.91741	.41390	.91032	33 32
L	20	.34900	.03677	.36623	.93052	.38241	.92309	.39848	.91729	.41410	.91020	34 31
I	30	.35021	.93667	.36650	.93042	.38268	.92388	.39875	.91706	.41469	.90996	30
ł	31	.35048	.93657	.36677	.93031	.38295	.92377	.39902	.01604	.41496	.90984	20
1	32	.35075	.93647	.36704	.93020	.38322	.92366	.39928	.91683	.41522	.90972	28
1	33	.35102	.93637	.36731	.93010	.38349	.92355	.39955	.91671	.41549	.90960	27
T	34 35	.35130	.93626	.36758	.92999	.38376	.92343 .92332	.39982	.91660	.41575	.90948	26 25
ł	36	.35184	.03606	.36812	.92978	.38430	.92321	.40035	.91636	.41628	.90924	24
L	37 38	.35211	.93596	.36839	.92967	.38456	.92310	.40062	.91625	.41655	.90911	23 22
1	30	.35239 .35266	.93585	.36894	.92956	.30403	.92299	.40088	.91613	.41081	.90899	22
1	40	.35293	.93565	.36921	.92935	.38537	.92276	.40141	.91590	.41734	.90875	20
1	41	.35320	.93555	.36948	.02924	.38564	.92265	.40168	.91578	.41760	.90863	10
1	42	.35347	.93544	.36975	.92913	.38591	.92254	.40195	.91566	.41787	.90851	19 18
	43	-35375 .35402	-93534 -93524	.37002 .37029	.92902	.38617	.92243 .92231	.40221	.91555	.41813	.90839	17 16
	145	.35402	.93524	.37029	.92881	.38671	.92231	.40246	.91543	.41866	.90814	15
1	46	.35456	.93503	.37083	.02870	.38608	.92209	.40301	.91519	.41892	.90802	14
1	47	.35484	·93493 ·93483	.37110	.92859	.38725	.92198	.40328	.91508	.41919	.90790 .90778	13 12
1	49	.35538	.93403	.37164	.92838	.38778	.92100	.40355 .40381	.91490	.41945	.90766	II
	50	.35565	.93462	.37191	.92827	.38805	.92164	.40408	.91472	.41998	.90753	10
	51	.35592	.93452	.37218	.92816	.38832	.92152	.40434	.91461	.42024	.90741	9
	52	.35619	.93441	.37245	.92805	.38859	.92141	.40461	.91449	.42051	.90729	
	53 54	·35647 ·35674	.93431 .93420	.37272	.92794 .92784	.38886	.92130	.40488	.91437	.42077	.90717	76
	85	.35701	.93410	.37326	.92773	.38939	.92107	.40541	.91414	-42130	.90692	5
1	56	.35728	.93400	.37353	.92762	.38966	.92096	40567	.91402	.42156	.90680	4
	57	·35755 .35782	.93389 .93370	.37380	.92751	·38993 .39020	.92085	.40594	.91390	.42183	.90668	3
	59	.35782 .35810 .35837	.93368	.37434	.92729	.39046	.92062	.40647	.91366	.42235	.90643	I
	60	.35837	.93358	.37461	.92718	.39073	.92050	.40674	.91355	.42262	.90631	
		Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	
	1											1
		6	9°	6	8°	6	7°	6	6°	6	5°	
1										-		-

ILT 36F-16

1	25°		26	;•	27	,0	28	30	20	0	,
	Sine	Cosine									
0	.42262	.90631	.43837	.89879	.45399	.89101	.46947	.88295	.48481	.87462	50
1 2	.42288	.90618	.43863	.89867 .89854	.45425	.89087 .89074	.46973	.88281	.48506	.8; 448 .87434	59
8	.42341	190504	.43009	.89841	-45451 -45477	.89074	.46999	.88254	.48532	.87434	58
4	.42367	.90582	.43942	.89828	.45503	.89048	.47050	.88240	.48583	.87406	56
S	.42394	.90569	.43968	.89816	-45529 -45554	.89035	.47076 .47101	.88226	.48608	.87391 .87377	55 54
78	.42446	.90545	.44020	.89790	.45580	.80008	.47127	.88199	.48659	.87363	53
8	.42473	.90532 .90520	.44046	.89777 .89764	.45606	.88995 .88981	.47153 .47178	.88185	.48684	.87349 .87335	52 51
10	.42525	.90507	.44098	.89752	.45658	.88968	.47204	.88158	.48735	.87321	21
11	.42552	.90495	.44124	.89739	.45684	.88955	.47229	.88144	.48761	.87306	10
12	.42578	.90483 .90470	.44151 .44177	.89726	.45710 .45736	.88942	.47255 .47281	.88130	.48786	.87292 .87278	48
14	.42631	.90458	.44203	.89700	.45762	.88915	.47306	.88103	.48837	.87264	46
15 16	.42657	.90446	.44229	.89687 .89674	.45787 .45813	.88902	.47332	.88089	.48862	.87250	45
	.42003	.90433 .90421	.44255 .44281	.89662	.45830	.888875	-47358 -47383	.88075	.48888	.87235	44
37 18	.42736	.90408	.44307	.89649	.45865	.88862	.47409	,88048	.48938	.87 207	14.2
19 20	.42762 .42788	.90396 .90383	-44333 -44359	.89636 .89623	.45891	.88848	-47434 -47460	.88034	.48964	.87193 .87178	41
21	.42815	.90371	.44385	.80610	.45942	.88822	.47486	188006	.40014	.87164	30
10	.42841	.90358	.44411	.89597	.45968	88888	.47511	.87003	.49040	.87150	38
23 24	.42867	.90346	.44437	.89584	-45994 -46020	.88795	-47537 -47562	.87979	.49065	.87136	37
24	.42020	.90334	.44464	.89571 .89558	.40020	.88768	.47502	.87965 .87951	.49090	.87121	36
20	.42946	.90309	.44516	.89545	.46072	.88755	.47614	.87937	.49141	.87093	34
27 28	.42973 .42999	.90296	.44542	.89532	.46097	.88741 .88728	.47639	.87923	.49166	.87079	33
20	.42999	.90204	.44568	.89506	.40123	.88715	.47005	.87909 .87896	.49192	.87050	32 31
30	.43051	.90259	.44620	.89493	.46175	.88701	.47716	.87882	.49242	.87036	10
31 32	.43077	.90246	.44646	.89480	.46201	.88658	-47741	.87868	.49268	.87021	and BR
33	.43130	.90233	.44698	.89454	.46252	.88661	.47793	.87840	.49293	.86993	27
34	.43156	.90208	.44724	.89441	.46278	.88647	-47793 -47818	.87826	.49344	.86978	10
35	.43182	.90196	.44750 .44776	.89428	.46304	.88634	.47844 .47869	.87812 .87798	.49369	.86964	25
37	.43235	.90171	.44802	.89402	.46355	88607	.47895	.87784	.49419	.86935	23
	.43261 .43287	.90158	.44828	.89389	.46381	.88593	.47920	87770	.49445	.86921	23
39 40	.43207	.90146 .90133	.44854 .44880	.89376 .89363	.46407	.88580 .88566	.47946 .47971	.87756 .87743	.49470 .49495	.86906 .8689.2	21 20
41	.43340	.90120	.44906	.89350	.46458	.88553	.47997	.87729	.49521	.86878	19
112	.43366	.90108	.44932	.89337	.46484	.88539	.48022	.87715	.49546	.86863	12
43	.43392	.00082	.44958	.89324	.46510 .46536	.88526 .88512	.48048	.87701	-49571 -49596	.86849	17
45	.43445	.90070	.45010	.89298	.46561	.88499	.48099	.87673	.49622	.86820	15
46	-43471 -43497	.90057	.45036	.89285	.46587	.88485 .88472	.48124	.87659	.49647 .49672	.86805	14
47	.43497	.90045	.45088	.89272	.40013	.88458	.48150	.87045	.49072	.80791	13
49	.43549	.90019	.45114	.89245	.46664	.88445	.48201	.87617	.49723	.86762	111
50	-43575	.90007	.45140	.89232	.46690	.88431	.48226	.87603	.49748	.86748	10
51	.43602 .43628	.89994 .89981	.45166	.89219 .89206	.46716	.88417	.48252	.87589	.49773	.86733	9
52 53	.43654	.80068	.45192 .45218	.80103	.46742	.88404	.48277	.87575 .87561	.49798 .49824	.86719	
54	.43680	.89956	.45243	.89180	.46793	.88377	.48328	.87546	.40840	.86690	7
55	-43706 -43733	.89943 .89930	.45269	.89167	.46819	.88363	.48354	.87532 .87518	.49874	.86675	5
57	43750	81008.	.45295	.89140	.46870	.88336	.48405	.87504	.49099	.86646	3
58	.43785	.89905 .89892	.45347	.89127	.46896	.88322	.48430	.87490	.49950	.86632	
59 60	.43811 .43837	.89892	-45373	.89114 .89101	.46921 .46947	.88308 .88295	.48456 .48481	.87176 .87463	-49975 -50000	.86617 .86603	I O
-	Cosine	Sine									
1		40		3°		20		10		00	1
	0.	7	0	3	0.		0		0		

,	30°		31	0	32	20	33	,°	3	4°	,
	Sine	Cosine	-								
		.86603		.85717	.52992	.84805	.54464	.83867	.55919	.82904	60
0	.50025	.86588	.51504	.85702	.53017	.84789	.54488	.83851	-55943	.82887	59
2	.50050	.86573	.51554	.85687	.5304I	.84774	.54513	.83835	.55968	.82871	10
3	.50076	.86559	.51579	.85672	.53066	.84759	.54537	.83819	.55992	.82855	57
	.50101	.86544	.51604	.85657	.53091	.84743	.54561 .54586	.83804 .83788	.56016	.82839 .82822	56
5	.50126	.86530 .86515	.51628	.85642 .85627	.53115	.84728 .84712	.54500	.83772	.56064	.02022 R28c6	55
	.50176	.86501	.51678	.85612	.53164	.84697	.54635	.83756	.56088	.82790	53
8	.50201	.86486	.51703	.85597	.53189	.84681	.54659	.83740	.56112	.82773	52
9	.50227	.86471	.51728	.85582	.53214	.84666	.54683	.83724	.56136	.83757	51
10	.50252	.86457	-51753	.85567	.53238	.84650	.54708	.83708	.56160	.82741	50
11	.50277	.86442	.51778	.85551	.53263	.84635	.54732	.83692	.56184	.82724	49
12	.50302	.86427	.51803	.85536	.53288	.84619 .84604	-54756 -54781	.83676 .83660	.56208	.82708 .82692	48
13 14	.50327	.86413 .86398	.51852	.85521 .85506	.53312 .53337	.84588	.54805	.83645	.56256	.82675	47
IS	.50377	.86384	.51877	.85491	.53361	.84573	.54829	.83629	.56280	.82659	45
16	.50403	.86369	.51902	.85476	.53386	.84557	.54854	.83613	.56305	.82643	44
17	.50428	.86354	.51927	.85461	.53411	.84542	.54878	.83597	.56329	.82626	A3
18	.50453	.86340	.51952	.85446	-53435	.84526 .84511	.54902	.83581 .83565	.56353 .56377	.82610 .82593	44
19	.50478 .50503	.86325 .86310	.51977 .52002	.85431 .85416	.53460 .53484	.84495	.54927	.83549	.50377	.82593	41
21	.50528	.86295	.52026	.85401	.53509	.84480	.54975	.83533	.56425	.82561	39
22	.50553	.86281	.52051	.85385	.53534	.84464	-54999	.83517	.56449	.82544	38
23	.50578	86.266	.52076	.85370	.53558	.84448	.55024	.83501	.56473	.82528	37
24	.50603	.86251	.52101	.85355	.53583	.84433	.55048	.83485	.56497	.82511	36
25	.50628	.86237	.52126	.85340	.53607	.84417	.55072	.83469	.56521	.82495 .82478	35
25	.50654	.86222	.52151	.85325 .85310	.53632 .53656	.84402 .84386	.55097 .55121	.83453 .83437	.56545 .56569	.82462	33
	.50704	.86192	.52200	.85294	.53681	.84370	.55145	.83421	.56593	.82446	32
29	.50729	.86178	.52225	.85279	.53705	.84355	.55169	.83405	.56617	.82429	31
30	.50754	.86163	.52250	.85264	.53730	.84339	-55194	.83389	.56641	.82413	00
31	.50779	.86148	.52275	.85249	.53754	.84324	.55218	.83373	.56665	.82396	20 28
32	.50804	.86133	.52299	.85234 .85218	-53779 -53804	.84308 .84292	·55242 ·55266	.83356 .83340	.56689	.82380 .82363	27
34	.50854	.86104	.52349	.85203	.53828	.84277	.55291	.83324	.56736	.82347	26
35	.50879	.86089	.52374	.85188	.53853	.84261	.55315	.83308	.56760	.82330	25
36	.50904	.86074	.52399	.85173	.53877	.84245	.55339	.83292	.56784	.82314	14
37	.50929	.86059	.52423	.85157 .85142	.53902 .53926	.84230	.55363 .55388	.83276 .83260	.56808	.82297 .82281	R3 22
30	.50954	.86030	.52473	.85127	.53951	.84198	.55412	.83244	.56856	.82264	21
10	.51004	.86015	.52498	.85112	.53975	.84182	.55436	.83228	.56880	.82248	20
41	.51029	.86000	.52522	.85096	.54000	.84167	.55460	.83212	.56904	.82231	10
42	.51054	.85985	.52547	.85081	.54024	.84151	.55484	.83195	.56928	.82214	19 18
43	.51079	.85970	.52572	.85066	.54049	.84135	.55509	.83179	56952	.82198	17
84	.51104	.85956 .85941	.52597 .52621	.85051 .85035	.54073 .54097	.84120 .84104	.55533	.83163 .83147	.56976 .57000	.82181 .82165	16
45	.51129	.85926	.52021	.85035	.54097	.84088	-55557 -55581	.83131	.57000	.82105	15
47	.51179	.85911	.52671	.85005	.54146	.84072	.55605	.83115	.57047	.82132	12
47	.51204	.85896	.52696	.84989	.54171	.84057	.55630	.83008	.57071	.82115	12
R9	.51229	.85881	.52720	.84974	.54195	.84041	.55654 .55678	.83082 .83066	.57095	182098 .82082	11
20					.54220				.5/119		
SI	.51279	.85851	.52770	.84943	.54244	.84009	.55702	.83050	.57143	.82065	88
52	.51304	.85836	.52794	.84928	.54269	.83994 .83978	.55720 .55750	.83034	.57167 .57191	.82048	8
53 54	.51329	.85806	.52819	.84913	.54293	.83970	.55750	.83001	.57191	82015	8
55	.51379	.85792	.52869	.84882	.54342	.83946	.55799	.82985	.57238	.81999	5
50	.51404	.85777	.52893	.84866	.54366	.83930	.55823	.82969	.57262	.81982	
58	.51429	.85762	.52918	.84851	.54391	.83915	.55847	.82953	.57286	.81965	3
50	.51454	.85747 .85732	.52943	.84836	.54415	.83899 .83883	.55871	82936	.57310	.81949	2
50	.51504	.85717	.52992	.84805	.54464	.83867	.55919	.82904	.57358	.81915	0
-	Cosine	Sine									
1		0		80		-0		5°		-0	1
	5	9°	50	0	5	7°	5	0	5	5°	

	35	0	30	50 .	32	70	38	30	39)°	,
	Sine	Cosine	-								
	99599	.81915	.58779	.80002	.60182	.79864	.61566	.78801	.62932		60
1	.57358 .57381	.81899	.58802	.80885	.60205	.79846	.61589	.78783	.62955	.77715 .77696	58
2	.57405	.81882 .81865	.58826	.80867	.60228	.79829	.61612	.78765	.62977 .63000	.77678 .77660	58 57
3	.57453	.81848	.58873	.80833	.60274	.79793	.61658	.78729	.63022	.77641	86
5	-57477 -57501	.81832	.58896	.80816 .80799	.60298 .60321	.79776 .79758	.61681	.78711	.63045	.77623	55
7	.57524	.81798	.58943	.80782	.603.14	.79741	.61726	.78676	.63090	.77586	53
8	.57548 .57572	.81782 .81765	.58967	.80765	.60367	.79723 .79706	.61749	.78658	.63113	.77568	52 51
10	.57596	.81748	.59014	.80730	.60414	.79688	.61795	.78622	.63158	.77531	51
II	.57619	.81731	.59037	.80713	.60437	.79671	.61818	.78604	.63180	.77513	100
12 13	.57643 .57667	.81714	.59061	.80696 .80679	.60460	.79653	.61841 .61864	.78586 .78568	.63203 .63225	.77494	48
13	.57691	.81681	.59108	.80662	.60506	.79618	.61887	.78550	.63248	.77458	46
15 16	.57715	.81664	.59131	.80644	.60529	.79600 .79583	.61909	.78532	.63271	-77439 -77421	45
17	·57738 ·57762	.81047	.59154 .59178	.80027	.60553 .60576	.79583 .79565	.61932	.78496	.63293 .63316	.77402	HON HON
18	.57786	.81614	.59201	.80593	.60599	-79547	.61978	.78478	.63338	.77384	43
19 20	.57810 .57833	.81597 .81580	.59225 .59248	.80576 .80558	.60622	.79530 .79512	.62001 .62024	.78460 .78443	.63361 .63383	.77366 .77347	41 1811
21	.57857	.81563	.59272	.80541	.60668	.79494	.62046	.78424	.63406	.77329	UD
22	.57881	.81546	.59295	.80524	.60691	-79477	.62069	.78405	.63428	.77310	38
23 24	.57904 .57928	.81530	.59318	.80507	.60714	-79459 -79441	.62092	.78387	.63451	.77292	37 36
25	.57952	.81496	.59365	.80472	.60761	.79424	.62138	.78351	.63496	.77255	35
20	.57976 .57999	.81479 .81462	.59389	.80455 .80438	.60784	.79406	.62160	.78333	.63518	.77236 .77218	33
27 58	.58023	.81445	.59436	.80420	.60830	.79371	.62206	.78297	.63563	.77100	32
29	.58047	.81428	·59459 ·59482	.80403 .80386	.60853	·79353 ·79335	.62229 .62251	.78279	.63585	.77181 .77162	31 30
31	.58094	.81395	.59506	.80368	.60899	.79318	.62274	.78243	.63630	.77144	IG
32	.58118	.81378	.59529	.80351	.60922	.70300	.62297	.78225	.63653	.77125	道路
33	.58141	.81361 .81344	·59552 ·59576	.80334 .80316	.60945	.79282	.62320	.78206	.63675 .63698	.77107	27
35	.58189	.81327	.59599	.80200	.60991	.79247	.62365	.78170	.63720	.77070	25
36	.58212	.81310 .81293	.59622 .59646	.80282	.61015	.79229	.62388	.78152	.63742	.77051	24 23
37	.58230	.81293	.59669	.80247	.61061	.79193	.62433	.78116	.63787	.77014	22
39	.58283	.81259	.59693	.80230	.61084	.79176	.62456	.78098	.63810	.76996	21
40	.58307	.81242	.59716	.80212	.61107	.79158	.62479	.78079	.63832	.76977	20
41	.58330	.81225	.59739	.80195	.61130	.79140	.62502	.78061	.63854	.76959	19
43	.58378	.81191	.59763 .59786	.80160	.61176	.70105	.62547	.78025	.63899	.76921	17
44	.58401	.81174	.59809	.80143	.61199	.79087	.62570	.78007	.63922	.76903	16
45	.58425	.81157	.59832 .59856	.80125 .80108	.61222	.79069 .79051	.02592	.77988	.63944	.76866	15 14
47	.58472	.81123	.59879	.80001	.61268	.79033	.62638	.77952	.63989	.76847	13
48	.58496 .58519	.81106	.59902 .59926	.80073 .80056	.61291	.79016	.62660	·77934 .77916	.64011	.76828	12
50	.58543	.81072	.59949	.80038	.61337	.78980	.62706	.77897	.64056	.76791	10
SI	.58567	.81055	.59972	.80021	.61360	.78962	.62728	.77879	.64078	.76773	8
52	.58590	.81038	.59995	.80003	.61383	.78944	.62751	.77861	.64100	.76754	8
54	.58637	.81004	.60042	.79968	.61429	.78908	.62796	.77824	.64145	.76717	6
56	.58661	.80987 .80970	.60065	·79951 ·79934	.61451	.78891 .78873	.62819	.77806 .77788	.64167	.76698	5
57	.58708	.80953	.60112	.79916	.61497	.78855	.62864	.77709	.64212	.76661	3
	.58731	.80936	.60135	.79899	.61520	.78837	.62887	.7775I	.64234	.76642	3
59	.58755 .58779	.80919 .80902	.60158 .60182	.79881 .79864	.61543	.78819	.62909 .62932	·77733 ·77715	.64256 .64279	.70023	0
	Cosine	Sine									
1	E	4°		3°		20	e	IO	E	00	/
	1 3	4	5	3	1 5	-	5		5		

,	40°		41	1°	4:	20	43	3°	4	4°	,
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
			1-1-1		.66013		,68200		.69466		60
0	.64279	.76604	.65606	-75471 -75452	.66935	.74314 .74295	.08200	.73135	.09400	.71934	59
2	.64323	.76567	.65650	.75433	.66956	.74276	.68242	.73096	.69508	.71894	58
a	.64346	.76548	.65672	.75414	.66978	.74256	.68264	.73076	.69529	.71873	57
a l	.64368	.76530	.65694	.75395	.669999	.74237	.68285	.73056	.69549	.71853	56
N.	.64390	.76511	.65716	.75375	.67021	.74217	.68306	.73036	.69570	.71833	55
ň	.64432	.76492	.65738 .65759	·75356 ·75337	.67064	.74198	.68349	.73016 .72996	.69591 .69612	.71013	53
7	.64457	.76455	.65781	.75318	.67086	.74159	.68370	.72976	.69633	.71772	52
0	.64479	.76436	.65803	.75299	.67107	.74139	.68391	.72957	.69654	.71752	SI
10	64501	.76417	.65825	.75280	.67129	.74120	.68412	.72937	.69675	.71732	50
II	.64524	.76398	.65847	.75261	.67151	.74100	.68434	.72917	.69696	.71711	49
12	.64546	.76380	.65869	.75241	.67172	.74080	.68455	.72897	.69717	.71691	48
13	.64568	.76361	.65891	.75222	.67194	.74061	.68476	.72877	.69737	.71671	47
14	.64590	.76342	.65913	.75203	.67215	.74041	.68497	.72857	.69758	.71650	46
15	.64612	.76323	.65935 .65956	.75184	.67237 .67258	.74022	.68518	.72837	.69779	.71630	45
17	.64657	.76286	.65978	.75146	.67280	.73983	.68561	.72797	.69821	.71590	43
18	.64679	.76267	.66000	.75126	.67301	.73963	.68582	.72777	.69842	.71569	42
19	.64701	.76248	.66022	.75107	.67323	.73944	.68603	.72757	.69862	.71549	41
20	.64723	.76229	.66044	.75088	.67344	.73924	.68624	.72737	.69883	.71529	40
21 .	.64746	.76210	.66066	.75069	.67366	.73904	.68645	.72717	.69904	.71508	39
22	.64768	.76192	.66088	.75050	.67387	.73885	.68666	.72697	.69925	.71488	38
23	.64790 .64812	.76173	.66109	.75030	.67409	.73865	.68688	.72677	.69946	.71468	37 36
25	.64834	.76154 .76135	.66131 .66153	.75011 .74992	.67430	.73840	.68730	.72657	.69966 .69987	.71447	30
20	.64856	.76116	.66175	.74992	.67473	.73806	.68751	.72617	.70008	.71407	34
27	.64878	.76097	.66197	.74953	.67495	.73787	.68772	.72597	.70029	.71386	33
38	.64901	.76078	.66218	.74934	.67516	.73767	.08703	.72577	.70049	.71366	32
29	.64923	.76059	.66240	.74915	.67538	.73747	.68814	.72557	.70070	.71345	31
30	.64945	.76041	.66262	.74896	.67559	.73728	.68835	.72537	.70091	.71325	30
31	.64967	.76022	.66284	.74876	.67580	.73708	.68857	.72517	.70112	.71305	29
32	.64989	.76003	.66306	.74857 .74838	.67602 .67623	.73688 .73669	.68878 .68899	.72497	.70132	.71284	28
34	.65033	.75965	.66349	.74818	.67645	.73649	.68020	.72477	.70153	.71243	15
35	.65055	.75946	.66371	.74700	.67666	.73629	.68041	.72437	.70195	.71223	25
36	.65077	.75927	.66393	.74780	.67688	.73610	.68962	.72417	.70215	.71203	24
37	.65100	.75908	.66414	.74760	.67709	.73590	.68983	.72397	.70236	.71182	23
30	.65122	.75889	.66436	.74741	.67730	.73570 .73551	.69004	.72377	.70257	.71162	33 31
40	.65166	.75851	.66480	.74703	.67773	.73531	.69046	.72337	.70298	.71121	20
41	.65188	.75832	.66501	.74683	.67795	.73511	.69067	.72317	.70319	.71100	10
142	.65210	.75813	.66523	.74664	.67816	.73491	.69088	.72297	.70339	.71080	18
43	.65232	.75794	.66545	.74644	.67837	.73473	.69109	.72277	.70360	.71059	17
- 44	.65254	.75775	.66566	.74625	.67859	.73452	.69130	.72257	.70381	.71039	16
45	.65276 .65298	.75756 .75738	.66588	.74606	.67880	.73432	.69151	.72236	.70401	.71019	15 14
47	.65,220	.75710	.66632	.74567	.67923	.73393	.60103	.72106	.70443	.70978	13
48	.65342	.75700	.66653	.74548	.67944	.73373	.69214	.72176	.70463	.70957	12
49	.65364	.75680	.66675	.74528	.67965	.73353	.69235	.72156	.70484	.70937	II
50	.65386	.75661	.66697	.74509	.67987	.73333	.69256	.72136	.70505	.70916	10
SI	.65408	.75642	.66718	.74489	68008	.73314	.69277	./2116	.70525	.70896	2
52	.65430 .65452	.75623 .75604	.66740	.74470	.68029	.73294	.69298	.72095	.70546	.70875	
54	.05454	.75585	.66783	.74451	.68072	.73274 .73254	.69340	.72075	.70507	.70834	7
55	.65496	.75566	.66805	.74431	.68093	.73234	.69361	.72035	.70608	.70813	5
56	.65518	.75547	.66827	.74392	.68115	.73215	.69382	.72015	.70628	.70793	4
57	.65540	.75528	.66848	.74373	.68136	.73195	.69403	.71995	.70649	.70772	1
58 50	.65562	.75509	.66870	-74353	.68157	.73175	.69424	.71974	.70670	.70752	2
50	.65606	.75490 .75471	.66913	·74334 ·74314	.68200	.73135	.69466	.71954	.70711	.70711	0
	Conica		Cash	- Class	Cash	Class	Canlar	Ning	Cashr	Eine	
1	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	1
	4	9°	4	80	4	7°	40	5°	4	5°	
-			-				1				_

32 NATURAL TANGENTS AND COTANGENTS

-						_					
1	0	0	I	0	2	0	3	0	4	0	1
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.00000	Infinite		57.2900	.03492	28.6363	.05241	19.0811	.06993	14.3007	55
1 2	.000.29	3437.75	.01775	\$6.3506	.03521	28.3094 28.1664	.05270	18.9755	.07022	14.2411	58
3	.00087	1710.07	.01833	55.4415	.03570	27.9372	.05299	18.7678	.07051	14.1021	57
R.	.00116	859.436	.01862	93.7086	.03609	27.7117	.05357	18.6656	.07110	14.0655	56
8	.00145	687.549 572.957	.01891	52.8821 52.0807	.03638	27.4899	.05387	18.5645	.07139	14.0079 13.9507	55
78	.00204	491.106	.01949	51.3032	.03696	27.0566	.05445	18.3655	.07197	13.8940	53
8	.00233	429.718	.01978	50.5485	.03725 .03754	26.8450 26.6367	.05474	18.2677	.07227	13.8378	52 51
10	.00291	343-774	.02036	49.1039	.03783	26.4316	.05533	18.0750	.07285	13.7267	50
11	.00320	312.521	.02066	48.4121	.03812	26.2296	.05562	17.9802	.07314	13.6719	89
12	.00349	286.478	.02095	47.7395	.03842	26.0307	.05591	17.8863	.07344	13.6174	48
13	.00378	245.552	.02153	46.4489	.03900	25.6340	.05649	17.7934 17.7015	.07373	13.5634 13.5098	47
15	.00436	229.182	.02182	45.8294	.03929	25.4517	.05678	17.6106	.07431	13.4566	MB
	.00465	214.858 202.219	.02211	45.2261 44.6386	.03958	25.2644 25.0798	.05708	17.5205	.07461	13.4039 13.3515	43
17 18	.00495	190.984	.03240	44.0661	.03987	24.8978	.05766	17.3432	.07519	13.2996	43
19	.00553	180.932	.02298	43.5081	.04046	24.7185	.05795	17.2558	.07548	13.2480	41
30	.00582	171.885	.02328	42.9641	.04075	24.5418	.05824	17.1693	.07578	13.1969	10
2I 23	.00611	163.700	.02357	42.4335	.04104	24.3675	.05854	17.0837	.07607	13.1461	
23	.00040	156.259	.02386	41.9158	.04133	24.1957 24.0263	.05883	16.9900 16.9150	.07636	13.0958	38 37
74	.00698	143.237	.02444	40.9174	.04191	23.8593	.05941	16.8319	.07695	12.9962	36
25 26	.00727	137.507	.02473	40.4358	.04220	23.6945	.05970	16.7496	.07724	12.9469	35
	.00756	132.219	.02502	39.9655	.04250	23.5321 23.3718	.05999 .06029	16.6681 16.5874	.07753 .07782	12.8981 12.8496	34
27 28	.00815	122.774	.02560	39.0568	.04308	23.2137	.06058	16.5075	.07812	12.8014	32
29 30	.00844	118.540 114.589	.02589 .02619	38.6177 38.1885	.04337 .04366	23.0577 22.9038	.06087	16.4283 16.3499	.07841 .07870	12.7536 12.7062	31
31	.00902	110.892	.02648	37.7686	.04395	22.7519	.06145	16.2722	.07899	12.6591	IRG .
32	.00931	107.426	.02677	37-3579 36.9560	.04424	22.6020 22.454I	.06175	16.1952	.07929	12.6124	28 27
34	.00989	101.107	.02735	36.5627	.04483	22.3081	.06233	16.0435	.07987	12.5199	25
35	.01018	98.2179 95.4895	.02764	36.1776	.04512	22.1640	.06262 .06291	15.9687	.08017	12.4742	23
37	.01076	92.9085	.02822	35.4313	.04541	21.8813	.06321	15.8211	.08075	12.3838	23
38	.01105	90.4633	.02851	35.0695	.04599	21.7426	.06350	15.7483	.08104	12.3390	23
39	.01135	88.1436 85.9398	.02881	34.7151 34.3678	.04628	21.6056	.06379	15.6762	.08134	12.2946	1276 1273
41	.01193	83.8435	.02939	34.0273	.04687	21.3369	.06437	15.5340	.08102	12.2067	19
43	.01222	81.8470	.02968	33.6935	.04716	21.2049	.06467	15.4638	.08221	12.1632	18
11	.01251	79.9434	.02997	33.3662	.04745	21.0747	.06496	15.3943	.08251	12.1201	17
#4 45	.01280	78.1263	.03026	33.0452 32.7303	.04774	20.9460	.06525	15.3254	.08280	12.0772	16
46	.01338	74.7292	.03084	32.4213	.04833	20.6932	.06584	15.1893	.08339	11.9923	14
47 48	.01367	73.1390	.03114	32.1181 31.8205	.04862 .04801	20.5691	.06613	15.1222	.08368	11.9504	13
40	.01390	70.1533	.03143	31.5284	.04091	20.4465	.00042	15.0557	.08397	11.8673	12
50	.01455	68.7501	.03201	31.2416	.04949	20.2056	.06700	14.9244	.08456	11.8262	RCI.
51 52	.01484	67.4019	.03230	30.9599	.04978	20.0872 19.9702	.06730	14.8596	.08485	11.7853	8
54	.01513	64.8580	.03259	30.0033	.05037	19.8546	.06788	14.7317	.08544	11.7045	2
54	.01571	63.6567	.03317	30.1446	.05066	19.7403	.06817	14.6685	.08573	11.6645	6
55 56	.01600	62.4992 61.3829	.03346	29.8823	.05095	19.6273 19.5156	.06847	14.6059	.08602	11.6248	- 5
57 58	.01658	60.3058	.03405	29.3711	.05153	19.4051	.06905	14.4823	.08661	11.5461	3
SH FO	.01687	59.2659 58.2612	.03434	29.1220 28.8771	.05182	19.2959	.06934	14.4212	.08690 .08720	11.5072	3
59 60	.01710	58.2012 57.2900	.03463 .03492	28.8771 28.6363	.05212 .05241	19.1879 19.0811	.06963 .06993	14.3007	.08720	11.4005	0
,	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	-
1	80)°	88	30	8:	,0	80	50	8	50	2
										1	

NATURAL TANGENTS AND COTANGENTS 33

Г		5"		6	ō	7	0	8	0	0	0	,
L	1	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	'
F	-											
	0	.08749	11.4301	.10510	9.51436	.12278	8.14435 8.12481	.14054	7.11537	.15838	6.31375 6.30189	50
	2	.08807	11.3540	.10569	9.46141	.12338	8.10536	.14113	7.08546	.15898	6.29007	50 58
1		.08837	11.3163	.10599	9.43515 9.40904	.12367	8.08600	.14143	7.07059	.15928	6.27829 6.26655	57 56
L	5	.08895	11.2417	.10657	9.38307	.12426	8.04756 8.02848	.14202	7.04105	.15988	6.25486	55
		.08925	11.2048	.10687	9.35724	.12456	8.00948	.14232	7.02637	.16017	6.24321 6.23160	54 53
1	6	.08983	11.1316	.10746	9.30599 9.28058	.12515	7.99058	.14291	6.99718 6.98268	.16077	6.22003 6.20851	52
	10	.09013 09043	11.0954 11.0594	.10775 .10805	9.25530	.12544	7.95302	.14321 .14351	6.96823	.16137	6.19703	51 50
	11	.09071	11.0237	.10834	9.23016	.12603	7.93438	.14381	6.95385	.16167	6.18559	49
	11	.09101	10.9882	.10863	9.20516	.12633	7.91582	.14410	6.93952	.16196	6.17419	48
	13 14	.09130	10.9529	.10893	9.18028 9.15554	.12662	7.89734	.14440	6.92525 6.91104	.16226	6.16283 6.15151	47
	15	.09189	10.9178 10.8829 10.8483	.10952	9.13093	.12722	7.86064	.14499	6.89688 6.88278	.16286	6.14023	45
1.	17	.09218	10.8483	.10301	9.08211	.12751 .12781	7.82428	.14529	6.86874	.16316	6.11779	44
	18	.09277	10.7797	.11040	9.05789	.12810	7.80622	.14588	6.85475 6.84082	.16376	6.10664 6.09552	41
	20	.09300	10.7457 10.7119	.11070	9.03379 9.00983	.12869	7.77035	.14648	6.82694	.10405	6.08444	41
	21	.09365	10.6783	.11128	8.98598	.12899	7.75254	.14678	6.81312	.16465	6.07340	39
L	22	109394	10.6450	.11158	8.96227	.12929	7.73480	.14707	6.79936	.16495	6.06240	38
	23	.09423	10.6118	.11107	8.93867	.12958	7.71715	.14737	6.78564 6.77199	.16525	6.05143 6.04051	37 36
L	25	.09482	10.5462	.11246	8.89185	.13017	7.68208	.14796 .14826	6.75838	.16585	6.02962 6.01878	35
	27 31	09511 .09541	10.5136	.11276	8.84551	.13047 .13076	7.66466	.14856	6.74483	.10015	6.00797	34
	29	.09570	10.4491	.11335	8.82252 8.79964	.13106	7.63005	.14886	6.71789	.16674	5.99720 5.98646	32
	30	.09629	10.4172 10.3854	.11364	8.77689	.13130	7.59575	.14915	6.69116	.16734	5.98040	31
	31	.09658	10.3538	.11423	8.75425	.13195	7.57872	.14975	6.67787	.16764	5.96510	29
	32	.09688	10.3224	.11452 .11482	8.73172 8.70931	.13224	7.56176	.15005	6.66463	.16794	5.95448	28 27
1	34	.09746	10.2602	.11511	8.68701	.13284	7.52806	.15064	6.63831	.16854	5.93335	26
	35 36	.09776 .09805	10.2294	.11541	8.66482 8.64275	.13313	7.51132 7.49465	.15094	6.62523	.16884	5.92283	25 24
	37	.09834	10.1683	.11600	8.62078	.13372	7.47806	.15153	6.59921	.16944	5.90191	23
	38	.09864	10.1381	.11629	8.59893	.13402	7.46154	.15183	6.58627	.16974	5.89151 5.88114	22
	40	.09923	10.0780	.11688	8.55555	.13461	7.42871	.15243	6.56055	.17033	5.87080	20
	41	.09952	10.0483	.11718	8.53402	.13491	7.41240	.15272	6.54777	.17063	5.86051	19 18
	42 43	.10011	10.0187	.11747	8.51259 8.49128	.13521	7.39616	.15302	6.53503 6.52234	.17093	5.85024 5.84001	18
	14	.10040	9.96007	.11806	8.47007	.13580	7.36389	.15362	6.50970	.17153	5.82982	16
	46	.10069	9.93101 9.90211	.11836	8.44896	.13609	7.34786	.15391 .15421	6.49710	.17183	5.81966 5.80953	15 14
	47	.10128	9.87338	.11895	8.40705	.13669	7.31600	.15451	6.47206	.17243	5.79944	13
	45	.10158	9.84482 9.81641	.11924	8.38625	.13698 .13728	7.30018	.15481	6.45961 6.44720	.17273	5.78938 5.77936	12
	50	.10216	9.78817	.11983	8.34496	.13758	7.26873	.15540	6.43484	.17333	5.76937	10
	51	.10246	9.76009	.12013	8.32446	.13787	7.25310	.15570	6.42253	.17363	5.75941	9
	53 53	.10275	9.73217 9.70441	.12042	8.30406	.13817	7.23754	.15600	6.41026 6.39804	.17393	5-74949 5-73960	
	54	.10334	9.67680	.12101	8.26355	.13876	7.20661	.15660	6.38587	.17453	5.72974	7
	55	.10363	9.64935	.12131	8.24345 8.22344	.13906	7.19125	.15089	6.37374 6.36165	.17483	5.71992 5.71013	5
	57	.10422	9.50400	.12190	8.20352 8.18370	.13965	7.16071	.15749	6.34961	.17543	5.70037	3
	59 59	.10452 .10481	9.54106	.12249	8.16398	.13995	7.14553 7.13042	.15779	6.32566	.17573 .17603	5.68094	I
	00	.10510	9.51436	.12278	8.14435	.14054	7.11537	.15838	6.31375	.17633	5.67138	0
F	,	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	
	1	84	1°	8	3°	8:	20	8:	r°	8	o°	
L	_	04										_

34 NATURAL TANGENTS AND COTANGENTS

,	100		I	10	1:	20	I	3°	I	4°	,
	Tang	Cotang									
0	17633	5.67128	.19438	5.14455 5.13658	.21256	4.70463	.23087	4.33148	.24933	4.01078	60
1	.17693	5.65205	.19498	5.12862	.21316	4.69121	.23117 .23148	4.32573 4.32001	.24964	4.00582 4.00086	59 58
3	.17723	5.64248	.19529	5.12069	.21347	4.68452	.23179	4.31430	.25026	3.99592	57
5	.17783	5.62344	.19589	5.10490	.21408	4.67121	.23240	4.30291	.25087	3.98607	55
78	.17843	5.60452	.19649	5.08921	.21469	4.65797	.23301	4.29159	.25149	3.97627	54 53
8	.17873	5.59511 5.58573	.19680	5.08139	.21499	4.65138	.23332	4.28595	.25180	3.97139 3.96651	SI
10	.17933	5.57638	.19740	5.06584	.21560	4.63825	.23393	4.27471	.25243	3.96165	50
II	.17963	5.56706	.19770	5.05809	.21590	4.63171	.23424	4.26911	.25273	3.95680	10
12	.17993 .18023	5-55777 5-54851	.19801	5.05037	.21621 .21651	4.62518	.23455	4.26352 4.25795	.25304	3.95196 3.94713	49
14	.18053	5.53927	.19861	5.03499	.21682	4.61219	.23516	4.25239	.25366	3.94232	46
15 16	.18113	5.53007 5.52090	.19891	5.02734 5.01971	.21712	4.60572	.23547 .23578	4.24685	.25397	3.93751 3.93271	45
17	.18143	5.51176	.19952	5.01210	.21773	4.59283	.23608	4.23580	.25459	3.92793	43
19	.18203	5.50264 5.49356	.19982	5.00451 4.99695	.21834	4.58001	.23639 .23670	4.23030	.25490	3.92316 3.91839	41
50	.18233	5.48451	.2004.2	4.98940	.21864	4.57363	.23700	4.21933	.25552	3.91364	80
21	.18263	5.47548	.20073	4.98188	.21895	4.56726	.23731	4.21387	.25583	3.90890	30
22 23	.18293	5.46648 5.45751	.20103	4.97438	.21925	4.56091 4.55458	.23762	4.20842	.25614	3.90417 3.89945	37
24	.18353	5.44857	.20164	4.95945	.21986	4.54826	.23823	4.19756	.25676	3.89474	36
25 100	.18384	5.43966	.20194	4.95201	.22017	4.54196 4.53568	.23854	4.19215	.25707	3.89004 3.88536	UF5 (34
27	.18444	5.42192	:20254	4.93721	.22078	4.52941	.23916	4.18137	.25769	3.88068	33
20	.18474 .18504	5.41309	.20285 .20315	4.92984	.22108	4.52316	.23946	4.17600	.25800	3.87601 3.87136	32
BO.	.18534	5.39552	.20345	4.91516	.22169	4.51071	.24008	4.16530	.25862	3.86671	20
31 32	.18564	5.38677 5.37805	.20376	4.90785	.22200 .22231	4.50451 4.49832	.24039	4.15997	.25893 4	3.86208	20
33	.18624	5.36936	.20436	4.89330	.22261	4.49215	.24100	4.14934	.25055	3.85284	27
34 35	.18654	5.36070 5.35206	.20466	4.88605	.22292	4.48600	.24131	4.14405	.25986	3.84824	25
36	.18714	5-34345	.20527	4.87162	.22353	4.47374	.24193	4.13350	.26048	3.83906	22
37	.18745	5.33487 5.32631	.20557	4.86444	.22383	4.46764	.24223	4.12825	.26079	3.83449	23
20	.18805	5.31778	.20618	4.85013	.22444	4.45548	.24285	4.11778	.26141	3.82537	21
40	.18835	5.30928	.20648	4.84300	.22475	4.44942	.24316	4.11256	.26172	3.82083	200
41 42	.18865	5.30080	.20679	4.83590	.22505	4.44338	.24347	4.10736	.26203	3.81630	19
41	.18025	5.28393	.20739	4.82175	.22567	4.43134	.24408	4.09699	.26266	3.80726	17
44 45	.18955	5.27553	.20770	4.81471	.22597	4.42534	.24439	4.09182	.26297	3.80276 3.79827	15
46	.19016	5.25880	.20830	4.80068	.22658	4.41340	.24501	4.08152	.26359	3.79378	14
47	.19046	5.25048 5.24218	.20861	4.79370	.22689	4.40745	.24532	4.07639	.26390	3.78931 3.78485	13
40	.19106	5.23391	.20921	4.77978	.22750	4.39560	.24593	4.06616	.26452	3.78040	II
EO	.19136	5.22566	.20952	4.77286	.22781	4.38969	.24624	4.06107	.26483	3-77595	10
51 52	.19166	5.21744	.20982	4.76595	.22811	4.38381 4.37793	.24655	4.05599 4.05092	.26515	3.77152 3.76709	98
53	.19227	5.20107	.21043	4.75219	.22872	4.37207	.24717	4.04586	.26577	3.76268	7
54 55	.19257	5.19293	.21073	4.74534 4.73851	.22903	4.36623	.24747 .24778	4.04081	26630	3.75828 3.75388	6
56	.19317	5.17671	.21134	4.73170	.22964	4.35459	.24809	4.03076	.26670	3.74950	4
57 38	.19347	5.16863	.21164	4.72490	.22995	4.34879	.24840	4.02574	.26701 .26733	3.74512 3.74075	3
.59 60	.19408	5.15256	.21225	4.71137	.23056	4.33723	.24902	4.01576	.26764	3.73640	I
,	Cotang	Tang	,								
	79)°	78	30	77	70	70	5°	7!	5°	

,	I	,°	16	50	I	7 ⁰	18	3°	I	9.°	,
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.26795	3.73205	.28675	3.48741	.30573	3.27085	.32492	3.07768	.34433	2.90421	60
1	.26826	3.72771	.28706	3.48359	.30605	3.26745	.32524	3.07464	.34465	2.90147	59 58
2	.26857	3.72338	.28738	3-47977 3-47596	.30637	3.26406	.32556 .32588	3.07160 3.06857	.34498 .34530	2.89873 2.89600	58 57
3	.26920	3.71907 3.71476	.28769	3.47590	.30700	3.25729	.32500	3.06554	.34553	2.80327	56
HIG	.26951	3.71046	.28832	3.46837	.30732	3.25392	.32653	3.06252	.34596	2.80055	55
	.26982	3.70616	.28864	3.46458	.30764	3.25055	.32685	3.05950	.34628	2.88783	54
78	.27013	3.70188	.28895	3.46080	.30796 .30828	3.24719 3.24383	-32717 -32749	3.05649	.34661 .34693	2.88511 2.88240	53
9	.27044	3.69335	.28958	3.45703	.30860	3.24049	.32782	3.05049	.34093	2.87970	51
10	.37107	3.68909	.28990	3.44951	.30891	3.23714	.32814	3.04749	.34758	2.87700	50
11	.27138	3.68485	.29021	3.44576	.30923	3.23381	.32846	3.04450	.34791	2.87430	49
12	.27169	3.68061	.29053	3.44202	.30955	3.23048	.32878	3.04152	.34824	2.87161	48
13 14	.27201	3.67638	.29084	3.43829 3.43456	.30987	3.22715 3.22384	.32911	3.03854	.34856	2.86624	47 46
15	.27263	3.66796	.29147	3.43450	.31051	3.22053	.32943	3.03260	.34922	2.86356	45
16	.27294	3.66376	.29179	3.42713	.31083	3.21722	.33007	3.02963	.34954	2.86089	64
17	.27326	3.65957	.29210	3.42343	.31115	3.21392	.33040	3.02667	.34987	2.85822	43
18	.27357 .27388	3.65538	.29242	3.41973	.31147 .31178	3.21063	.33072	3.02372	.35020 .35052	2.85555	43 41
20	.27300	3.64705	.292/4	3.41236	.31210	3.20/34	.33136	3.01783	.35085	2.85023	40
21	.27451	3.64289	.29337	3.40869	.31242	3.20079	.33169	3.01489	.35118 2.84758		30
23	.27482	3.63874	.29368	3.40502	.31274	3.19752	.33201	3.01196	.35150 2.84494		38
23	.27513	3.63461	.29400	3.40136	.31306	3.19426	.33233	3.00903 3.00611	.35183 2.84229 .35216 2.83965		37
25	.27545 .27576	3.63048	.29432	3.39771 3.39406	.31338 .31370	3.19100 3.18775	.33266 .33298	3.00319	.35216 2.83965 .35248 2.83702		35
26	.27607	3.62224	29495	3.39042	.31402	3.18451	.33330	3.00028	.35281 2.83439		34
27	.27638	3.61814	.29526	3.38679	.31434	3.18127	.33363	2.99738	.35314 2.83176		33
28	.27670	3.61405 3.60996	.29558	3.38317 3.37955	.31466	3.17804	.33395	2.99447	-35346 -35379	2.82914	34
29 20	.27701	3.60990	.29590 .29621	3-37955 3-37594	.31498	3.17481 3.17159	.33427 .33460	2.99158 2.98868	·35379 ·35412	2.82053	31 30
31	.27764	3.60181	.29653	3.37234	.31562	3.16838	.33492	2.98580	.35445	2.82130	20
32	.27795	3-59775	.29685	3.36875	.31594	3.16517	.33524	2.98292	.35477	2.81870	118
33	.27826	3.59370 3.58966	.29716 .29748	3.36516 3.36158	.31626	3.16197 3.15877	·33557 ·33589	2.98004	·35510 ·35543	2.81610	27 26
35	.27889	3.58562	.29780	3.35800	.31690	3.15558	.33621	2.97430	.35576	2.81091	25
36	.27921	3.58160	.29811	3.35443	.31722	3.15240	.33654	2.97144	.35608	2.80833	24
37	.27952	3-57758	.29843	3.35087	.31754	3.14922	.33686	2.96858	.35641	2.80574	23
38	.27983	3-57357 3-56957	.29875	3-34732	.31786 .31818	3.14605 3.14288	-33718 -33751	2.96573 2.96288	-35674 -35707	2.80310	23
40	.28046	3.56557	.29938	3.34023	.31850	3.13972	.33783	2.96004	.35740	2:79802	20
41	.28077	3.56159	.29970	3.33670	.31882	3.13656	.33816	2.95721	.35772	3.79545	19
42	.28109	3.55761	.30001	3.33317	.31914	3.13341	.33848	2.95437	.35805	2.79289	18
43	.28140	3.55364	.30033 .30065	3.32965	.31946 .31978	3.13027	.33881	2.95155	.35838	2.79033	17
45	.28203	3.54573	.30007	3.32264	.32010	3.12400	.33945	2.94591	.35904	2.78523	15
46	.28234	3.54179	.30128	3.31914	.32042	3.12087	.33978	2.94309	.35937	2.78269	14
47	.28266	3.53785	.30160	3.31565	.32074	3.11775	.34010	2.94028	.35969	2.78014	13
45	.28297	3.53393 3.53001	.30192 .30224	3.31216 3.30868	.32106	3.11464	.34043 .34075	2.93748	.36002	2.77761 2.77507	12
50	.28360	3.52609	.30255	3.30521	.32139	3.10842	.34108	2.93189	.30035 2.77507 .36068 2.77254		10
51	.28391	3.52219	.30287	3.30174	.32203	3.10532	.34140	2.92910	.36101 2.77002		9
52	.28423	3.51829	.30319	3.29829	.32235	3.10223	.34173	2.92632			
53 54	.28486	3.51441	.30351 .30382	3.29483	.32267	3.09914 3.09606	.34205 .34238	2.92354 2.92076	.36199 2.76247		7
	.28517	3.50666	.30414	3.28795	.32331	3.09298	.34270	2.91799	.36232 2.75996		5
55 56	.28549	3.50279	.30446	3.28452	.32363	3.08991	.34303	2.91523	. 36265	2.75746	
57	.28580	3.49894	.30478	3.28109	.32396	3.08685	·34335 ·34368	2.91246	.36298	2.75496	2
	.28643	3.49509	.30509	3.27426	.32420	3.08073	.34300	2.90971	.30331	2.74997	I
59	.28675	3.48741	.30573	3.27085	.32492	3.07768	.34433	2.90421	.36397	2.74748	
	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	
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	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
	.36397	2.74748	.38386	2.60509	.40403	2.47509	.42447	2.35585	.44523	2.24604	50
1	.36430	2.74499	.38420	2.60283	.40436	2.47302	.42482	2.35395	-44558 -44593	2.24428	59
3	.36496	2.74004	.38487	2.59831	.40504	2.46888	.42551	2.35015	.44627	2.24077	57
N.	.36529	2.73756	.38520 .38553	2.59606	.40538	2.46682	.42585	2.34825	.44662	2.23902	56
56	.36562 .36595	2.73509 2.73263	.30553	2.59301	.40572	2.46270	.42654	2.34447	.44732	2.23553	55
78	.36628	2.73017	.38620	2.58932	.40640	2 46065	.42688	2.34258	.44767	2.23378	53
	.36661	2.72771 2.72526	.38654	2.58708	.40674	2.45860	.42722	2.34069 2.33881	.44802	2.23204 2.23030	52
03 10	.36727	2.72281	.38721	2.58261	.40741	2.45055	.42791	2.33693	.44872	2.23030	SI BO
11	.36760	2.72036	.38754	2.58038	.40775	2.45246	.42826	2.33505	.44907	4.22683	40
12	.36793	2.71792 2.71548	.38787	2.57815	.40809	2.45043	.42860	2.33317	.44942	2.22510 2.22337	45
14	.36859	2.71305	.38854	2.57371	.40877	2.44636	.42929	2.32943	.45012	2.22164	46
15	.36892	2.71062	.38888	2.57150	.40911	2.44433	.42963	2.32756	.45047	2.21992	45
	.36925 .36958	2.70819	.38921 .38955	2.56928	.40945	2.44230 2.44027	.42998 .43032	2.32570 2.32383	.45082	2.21819 2.21647	44
17	.36991	2.70335	.38988	2.56487	.41013	2.43825	.43067	2.32197	.45152	2.21475	12
19	.37024	2.70094	.39022	2.56266	.41047	2.43623	.43101	2.32012	.45187	2.21304	41
20	.37057	2.69853	.39055	2.56046	.41081	2.43422	.43136	2.31826	.45222	2.21132	40
31	.37090	2.69612	.39089	2.55827	.41115	2.43220 2.43019	.43170	2.31641 2.31456	-45257 -45292	2.20961 2.20790	38
23	.37157	2.69131	.39156	2.55389	.41183	2.42819	.43230	2.31430	.45327	2.20/90	37
24	.37190	2.68892	.39190	2.55170	.41217	2.42618	.43274	2.31086	.45362	2.20449	36
25 26	.37223	2.68653	.39223	2.54952	.41251	2.42418 2.42218	.43308 .43343	2.30902	.45397	2.20278	35
	.37256	2.08175	·39257 ·39290	2.54734 2.54516	.41205	2.42210	·43343 ·43378	2.30710	.45432	2.19938	34
27 18	.37322	2.67937	.39324	2.54200	.41353	2.41819	.43412	2.30351	.45502	2.19769	32
29 36	·37355 ·37388	2.67700	-39357 -39391	2.54082 2.53865	.41387 .41421	2.41620 2.41421	-43447 -43481	2.30167 2.29984	-45538 -45573	2.19599 2.19430	31 30
31	.37422	2.67225	.39425	2.53648	.41455	2.41223	.43516	2.29801	.45608	2.19261	'29 88
10	-37455 -37488	2.00989	·39458	2.53432	.41490	2.41025 2.40827	-43550 -43585	2.29019	.45643 .45678	2.19092	27
34	.37521	2.66516	.39526	2.53001	.41558	2.40629	.43620	2.29254	.45713	2.18755	20
35	-37554	2.66281	·39559	2.52786	.41592	2.40432 2.40235	.43654 .43689	2.29073 2.28891	.45748	2.18587	R5 24
27	.37588	2.65811	.39593	2.52357	.41660	2.40038	.43009	2.28710	.45810	2.18251	23
38	.37654	2.65576	.39660	2.52142	.41694	2.39841	.43758	2.28528	.45854	2.18084	12.0
39	.37687	2.65342	·39694	2.51929	.41728	2.39645	-43793 -43828	2.28348	.45889	2.17916	21
41	.37754	2.64875	.30761	2.51502	.41797	2.39253	.43862	2.27987	.45960	2.17582	10
42	.37787	2.64643	.39795	2.51289	.41831	2.39058	.43897	2.27806	.45995	2.17416	19 18
B	.37820	2.64410	.39829 .39862	2.51076	.41865	2.38863 2.38668	.43932	2.27626	.46030	2.17249 2.17083	17
44	.37853 .37887	2.64177	.39896	2.50604	.41899	2.38473	.43966 .44001	2.27267	.40005	2.17003	10
46	.37920	2.63714	.39930	2.50440	.41968	2.38270	.44036	2.27088	.46136	2.16751	14
47	·37953 ·37986	2.63483	.39963 .39997	2.50229	.42002 .42036	2.38084	.44071	2.26909	.46171	2.16585	13
49	.37980	2.03252	.40031	2.49807	.42030	2.37697	.44140	2.26552	.46242	2.16255	11
53	.38053	2.62791	.40065	2.49597	.42105	2.37504	.44175	2.26374	.46277	2.16090	10
51	.38086	2.62561	.40098	2.49386	.42139	2.37311	.44210	2.26196	.46312	2.15925	8
52	.38120	2.62332	.40132	2.49177	.42173	2.37118	.44244	2.26018	.46383 2.15596		
54	.38186	2.61874	.40200	2.48758	.42242	2.36733	.44314	2.25663	.46418 2.15432		76
55	.38220	2.61646	.40234	2.48549	.42276	2.36541	.44349	2.25486			5
56	.38253 .38286	2.61418	.40267	2.48340	.42310	2.36349 2.36158	.44384	2.25132	.40489	2.15104	A B
57 58	.38320	2.60963	.40335	2.47924	.42379	2.35967	44453	2.24956	.46560	2.14777	3
50	.38353	2.60736	.40369	2.47716	.42413	2.35776	.44488	2.24780	.46595	2.14614	I
	.38386	2.60509	.40403	2.47509	.42447	2.35585	.44523	2.24604	.46631	2.14451	
,	Cotang		Cotang		Cotang		Cotang		Cotang		,
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	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
	.46631	2.14451	.48773	2.05030	.50953	1.96261	.53171	1.88073	-55431	1.80405	60
I	.46666	2.14288	.48809 .48845	2.04879 2.04728	.50989	1.96120	.53208	1.87941	-55469	1.80281	59 58
3	.46702	2.14125 2.13963	.40045	2.04720	.51063	1.95979 1.95838	.53283	1.87677	.55545	1.80034	57
3	.46772	2.13801	.48917	2.04426	.51099	1.95698	.53320	1.87546	.55583	1.79911	56
5	.46808	2.13639	.48953	2.0427ú	.51136	1.95557	.53358	1.87415	.55621	1.79788	55
	.46843	2.13477	.48989	2.04125 2.03975	.51173	1.95417	.53395	1.87283	.55659 55697	1.79665	54
7	.46879	2.13316 2.13154	.49020	2.03975	.51209	1.95277 1.95137	·53432 ·53470	1.87021	.55736	1.79542	52 52
9	.46950	2.12993	.49098	2.03675	.51283	1.94997	.53507	1.86891	.55774	1.79296	51
10	.46985	2.12832	.49134	2.03526	.51319	1.94858	-53545	1.86760	.55812	1.79174	50
II	.47021	2.12671	.49170	2.03376	.51356	1.94718	.53582 .53620	1.86630 1.86499	.55850 .55888	1.79051	49 48
12 13	.47056	2.12511	.49206	2.03227 2.03078	.51393 .51430	1.94579	.53657	1.86369	.55000	1.78929	47
14	.47128	2.12190	.49278	2.02020	.51467	1.94301	.53694	1.86239	.55964	1.78685	46
15	.47163	2.12030	.49315	2.02780	.51503	1.94162	.53732	1.86109	.56003	1.78563	45
16	.47199	2.11871	.49351 .49387	2.02631 2.02483	.51540	1.94023 1.93885	.53769 .53807	1.85979	.56041	1.78441	44
17	.47234	2.11711 2.11552	.49307	2.02483	.51577	1.93885	.53807	1.85850	.50079	1.78319	43
19	.47305	2.11392	.49459	2.02187	.51651	1.93608	.53882	1.85591	.56156	1.78077	41
20	.47341	2.11233	-49495	2.02039	.51688	1.93470	.53920	1.85462	.56194	1.77955	40
21	.47377	2.11075	-49532	2.01891	.51724	1.93332	.53957	1.85333	.56232	1.77834	39
22	.47412	2.10916	.49568	2.01743	.51761	1.93195	-53995	1.85204	.56270	1.77713	38
23	.47448	2.10758	.49604	2.01596	.51798	1.93057 1.92920	*.54032	1.85075	.56309	1.77592	37
25	.47483	2.10000	.49640	2.01449	.51035	1.92920	.54070	1.84940	.56347	1.77471	36 35
25	.47555	2.10284	.49713	2.01155	.51909	1.92645	.54145	1.84689	.56424	1.77230	34
27	.47500	2.10126	.49749	2.01008	.51946	1.92508	.54183	1.84561	.56462 1.771		33
	.47626	2.09969 2.09811	.49786 .49822	2.00862	.51983	1.92371	.54220	1.84433	.56501 1.7699		32
20 30	.47662 .47698	2.09611	.49858	2.00715 2.00569	.52020 .52057	1.92235 1.92098	.54258 .54296	1.84305 1.84177	.56539 1.76869 .56577 1.76749		31 30
31	.47733	2.09498	.49894	2.00423	.52094	1.91962	.54333	1.84049	.56616	1.76629	29
32	.47769	2.09341	.49931	2.00277	.52131	1.91826	.54371	1.83922	.56654	1.76510	28
33	.47805 .47840	2.09184 2.09028	.49967 .50004	2.00131 1.99986	.52168	1.91690	.54409 .54446	1.83794	.56693 .56731	1.76390	27 26
34 35	.47876	2.09020	.50040	1.99900	.52242	1.91554	.54484	1.83540	.56769	1.76151	25
36	.47912	2.08716	.50076	1.99695	.52279	1.91282	.54522	1.83413	.50808	1.76032	24
37	.47948	2.08560	.50113	1.99550	.52316	1.91147	.54560	1.83286	.56846	1.75913	23
38	.47984	2.08405	.50149	1.99406	.52353 .52390	1.91012	·54597 .54635	1.83159	.56885	1.75794	21
20	.48055	2.08094	.50222	1.99116	.52390	1.90741	.54673	1.82906	.56962	1.75556	20
41	.48091	2.07939	.50258	1.98972	.52460	1.90607	.54711	1.82780	.57000	1.75437	19 18
42	.48127	2.07785	.50295	1.98828	.52501	1.90472	.54748	1.82654	.57039	1.75319	
43	.48163	2.07630	.50331 .50368	1.98684	.52538	1.90337 1.90203	.54786 .54824	1.82528	.57078	1.75200	17 16
44 45	.48234	2.07470	.50300	1.98396	-52575 -52613	1.90203	.54024	1.82276	.57116	1.75082	10
46	.48270	2.07167	.50441	1.98253	.52650	1.89935	.54900	1.82150	.57193	1.74846	14
47	.48306	2.07014	.50477	1.98110	.52687	1.89801	.54938	1.82025	.57232	1.74728	13
	.48342	2.06860	.50514	1.97966	.52724 .52761	1.89667 1.89533	·54975 ·55013	1.81899	.57271	1.74610	12
149 343	.48414	2.06553	.50550 .50587	1.97623	.52798	1.89533	.55051	1.81649	.57309 .57348	1.74492	10
51	.48450	2.06400	.50623	1.97538	.52836	1.89266	.55089	1.81524	.57386 1.74257		8
52	.48486	2.06247	.50660	1.97395	.52873	1.89133	.55127	1.81399	.57425 1.741		
53 54	.48521	2.05942	.50696	1.97253	.52910	1.89000	.55165	1.81274	.57464	1.74022	7
54	.40557	2.05942	.50733	1.96969	.52947 .52985	1.88734	.55203	1.81150	-57503 -57541	1.73905	5
56	.48629	2.05637	.50806	1.96827	.53022	1.88602	.55279	10008.	.57580	1.73671	
37 58	.48665	2.05485	.50843	1.96685	.53059	1.88469	.55317	1.80777	.57619	1.73555	3
58	.48701	2.05333	.50879	1.96544	.53096	1.88337	.55355	1.80653	.57057	1.73438	H I
80 60	.48773	2.05182	.50916 .50953	1.96261	-53134 -53171	1.88073	·55393 ·55431	1.80529	.57696 .57735	1.73321	5
	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	
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	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	-
			12 MZ		60-		6				-
3	-57735	1.73205	.60126	1.66428	.62487	1.60033	.64941	1.53986 1.53888	.67451	1.48256	60
2	-57774 .57813	1.72973	.60165	1.66209	.62568	1.59826	.65024	1.53791	.67536	1.48070	89
3	.57851	1.72857	.60205	1.66099	.62608	1.59723	.65065	1.53693	.67578	1.47977	57
4	.57890	1.72741	.60245	1.65990	.62689	1.59620	.65106	1.53595 1.53497	.67620	1.47885 1.47792	55
5	.57968	1.72509	.60324	1.65772	.62730	1.59414	.65189	1.53400	.67705	1.47699	54
78	.58007	1.72393	.60364	1.65663	.62770 .62811	1.59311	.65231	1.53302	.67748	1.47607	53
0	.58046	1.72278	.60403	1.65554 1.65445	.62852	1.59208	.65272	1.53205	.67790 .67832	1.47514	52 51
10	.58124	1.72047	.60483	1.65337	.62892	1.59002	.65355	1.53010	.67875	1.47330	50
11	.58162	1.71032	.60522	1.65228	.62933	1.58000	.65397	1.52913	.67917	1.47238	
12	.58201	1.71817	.60562	1.65120	.62973	1.58797	.65438	1.52816	.67960	1.47146	HQ AR
13	.58240	1.71702	.60602	1.65011	.63014	1.58695	.65480	1.52719	.68002	1.47053	47
14	.58279	1.71588	.60642	1.64903	.63055	1.58593	.65521	1.52622	.68045	1.46962 1.46870	46
15 16	.58357	1.71473	.60721	1.64687	.63136	1.58388	.05503	1.52525	.681.30	1.46778	45
17	.58396	1.71244	.60761	1.64579	.63177	1.58286	.65646	1.52332	.68173	1.46686	83
18	.58435	1.71129	.60801	1.64471	.63217	1.58184	.65688	1.52235	.68215	1.46595	42
19 20	.58474	1.71015	.60841	1.64363	.63258	1.58083	.65729	1.52139	.68258	1.46503 1.46411	41
21	.58552	1.70787	.60921	1.64148	.63340	1.57879	.65813	1.51946	.68343 1.46320 .68386 1.46229		39 38
23	.58591	1.70673	.60960	1.64041 1.63934	.63380 .63421	1.57778	.65854 .65896	1.51850	.68429 1.46137		37
24	.58670	1.70446	.61040	1.63826	.63462	1.57575	.65938	1.51658	.68471 1.46046		36
25	.58709	1.70332	.61080	1.63719	.63503	1.57474	.65980	1.51562	.68514 1.45955		35
26	.58748	1.70219	.61120	1.63612	.63544	1.57372	.66021	1.51466	.68557 1.45864 .68600 1.45773		34
27	.58787	1.70106	.61160	1.63505	.63584	1.57271	.66105	1.51370	.68600 I.45773 .68642 I.45682		32
20	.58865	1.69879	.61240	1.63292	.63666	1.57069	.66147	1.51179	.68685	1.45592	31
30	.58905	1.69766	.61280	1.63185	.63707	1.56969	.66189	1.51084	.68728	1.45501	UD.
31	.58944	1.69653	.61320	1.63079	.63748	1.56868	.66230	1.50988	.68771	1.45410	20
32	.58983	1.69541	.61360	1.62972	.63789	1.56767	.66272	1.50893	.68814	1.45320	29
33	.59022	1.69428	.61400	1.62866	.63830	1.56667	.66314	1.50797	.68857	1.45229	27
34 35	.59061 .59101	1.69316	.61440	1.62760	.63871	1.56566	.66356	1.50702	.68942	1.45139	26
36	.59140	1.60001	.61520	1.62548	.63953	1.56366	.66440	1.50512	.68985	1.44958	P.4
37	.59179	1.08979	.61561	1.62442	.63994	1.56265	.66482	1.50417	.69028	1.44868	F3
38	.59218	1.68866	.61601 .61641	1.62336	.64035	1.56165	.66524	1.50322	.69071	1.44778	22
40	.59297	1.68643	.61681	1.62125	.64117	1.55966	.66608	1.50133	.69157	1.44598	20
-		(0)			60	0//					
41	·59336 ·59376	1.68531	.61721	1.62019	.64158	1.55866	.66650	1.50038	.69200	1.44508 1.44418	19
42	.59370	1.68308	.61761 .61801	1.61808	.64240	1.55666	.66734	1.49944	.69286	1.44410	17
144	.59454	1.68196	.61842	1.61703	.64281	1.55567	.66776	1.49755	.69329	1.44239	16
45	-59494	1.68085	.61882	1.61598	.64322	1.55467	.66818	1.49661	.69372	1.44149	15
46	·59533 ·59573	1.67974	.61922	1.61493 1.61388	.64363	1.55368	.00800	1.49566	.69416	1.44060	14 13
47	.59612	1.67753	.62003	1.61283	.64446	1.55170	.66944	1.49378	.69502	1.43881	12
40	.59651	1.67641	.62043	1.61179	.64487	1.55071	.66986	1.49284	.69545	1.43793	11
50	.59691	1.67530	.62083	1.61074	.64528	1.54972	.67028	1.49190	.69588	1.43703	10
SI	.59730	1.67419	.62124	1.60970	.64569	1.54873	.67071	1.49097	.69631 1.43614		9
52	.59770	1.67309	.62164	1.60865	.64610	1.54774	.67113	1.49003	.69675 1.43525 .69718 1.43436		
N3 54	.59809	1.67198	.62204	1.60761	.64652	1.54675	.67155	1.48909	.69761 1.43347		2 A
55	.59888	1.66978	.62285	1.60553	.64734	1.54478	.67230	1.48722	2 .69804 1.43258		8
5.6	.59928	1.66867	.62325	1.60449	.64775	1.54379	.67282	1.48629	.69847	1.43169	
57	.59967	1.66757	.62366	1.60345	.64817	1.54281	.67324	1.48536 1.48442	.69891	1.43080	3
	.60046	1.66538	.62446	1.60137	.64899	1.54085	.67409	1.48349	.69934	3.42903	1
59	.60086	1.664.28	.62487	1.60033	.64941	1.53986	.67451	1.48256	.70021	1.42815	0
1	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	,
-	59	0	58	20	- 57	,0	- 4	50		-0	
	59	9	50	2	57		56° 55°		5		
Concession of the local division of the loca	-	-	the second s	-		-	-				the supervised in the local division of the

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1	3.	5°	30	5°	32	7°	38	30	3	9°	1
	Tang	Cotang									
D	.70021	1.42815	.72654	1.37638	.75355	1.32704	.78129	1.27994	.80978	1.23490	60
- 2	.70064	1.42726	.72699	I.37554 I.37470	.75401 .75447	1.32624	.78175	1.27917	.81075	1.23410 1.23343	59 58
3	.70151	1.42550	.72788	1.37386	.75492 .75538	1.32464	.78269	1.27764	.81123	1.23270	57 56
S	.70238	1.42374	.72877	1.37218	.75584	1.32304	.78363	1.27611	.81220	1.23123	50
S	.70281	1.42286	.72921 .72966	1.37134 1.37050	.75629 .75675	I.32224 I.32I44	.78410	1.27535	.81268	1.23050	54
Z	.70325 .70368	1.42110	.73010	1.30007	.75721	1.32064	.78504	1.27382	.81364	1.22904	53 52
9 10	.70412	1.42022	.73055	1.36883 1.36800	.75767 .75812	1.31984	.78551 .78598	1.27306	.81413 .81461	1.22831 1.23758	51 50
11 12	.70499	1.41847	.73144	1.36716	.75858	1.31825	.78645	I.27153 I.27077	.81510 .81558	1.22685	49
13	.70586	1.41672	.73234	1.36549	.75950	1.31666	.78739	1.27001	.81606	1.22539	47
14	.70629	1.41584	.73278 .73323	1.36466	.75996	1.31586	.78786	1.26925	.81655	1.22467	46
16	.70717	1.41409	.73368	1.36300	.76088	1.31427	.78881	1.26774	.81752	1.22321	44
17	.70760	1.41322 1.41235	.73413	1.36217 1.36134	.76134	1.31348	.78928	1.26698	.81800	1.22249	43
10	.70848	1.41235	-73457 -73502	1.30134	.76226	1.31209	.70975	1.26546	.81898	1.22170	42 41
303	.70891	1.41061	.73547	1.35968	.76272	1.31110	.79070	1.26471	.81946	1.22031	40
21	.70935	1.40974	.73592	1.35885	.76318	1.31031	.79117	1.26395	.81995	1.21959	39
23	.70979	1.40887	.73637 .73681	1.35802	.76364	1.30952	.79164	1.26319 1.26244	.82044	1.21886 1.21814	38 37
24	.71066	1.40714	.73726	1.35637	.76456	1.30795	.79259	1.26169	.82141	1.21742	36
25 26	.71110	1.40627	.73771 .73816	1.35554	.76502	1.30716	.79306	1.26093	.82190 .82238	1.21670	35
20 27	.71154	1.40540 1.40454	.73861	1.35472	.76548	1.30637	-79354 -79401	1.25943	.82230	1.21598	34 33
28	.71242	1.40367	.73906	1.35307	.76640	1.30480	.79449	1.25867	.82336	1.21454	32
20 30	.71285	1.40281 1.40195	.73951 .73996	1.35224	.76686	I.3040I I.30323	·79496 ·79544	1.25792 1.25717	.82385 .82434	1.21382	31 50
31	.71373	1.40109	.74041	1.35060	.76779	1.30244	.79591	1.25642	.82483	1.21238	29
32	.71417	1.40022	.74086	1.34978	.76825	1.30166	.79639	1.25567	.82531	1.21166	28
33 34	.71461	1.39936 1.39850	.74131 .74176	1.34896	.76871	I.30087 I.30009	.79686	1.25492 1.25417	.82580 .82629	1.21094	27 26
35	.71549	1.39764	.74221	1.34732	.76964	1.29931	.79781	1.25343	.82678	1.20051	#5
36	.71593	1.39679	.74267	1.34650	.77010	1.29853	.79829	1.25268	.82727	1.20879	24
37 38	.71637	1.39593 1.39507	.74312 .74357	1.34568	.77057	I.29775 I.29696	.79877	1.25193	.82776	1.20808 1.20736	23
39	.71725	1.39421	.74402	1.34405	.77149	1.29618	.70072	1.25044	.82874	1.20665	21
Ma	.71769	1.39336	.74447	1.34323	.77196	1.29541	.80020	1.24969	.82923	1.20593	20
41	.71813	1.39250	.74492	1.34242	.77242	1.29463	.80067	1.24895	.82972	1.20522	19 18
42	.71901	1.39165	.74538 .74583	1.34160	.77289	1.29385	.80115	1.24020	.83022 .83071	I.2045I I.20379	10
44	.71946	1.38994	.74628	1.33998	.77382	1.29229	.80211	1.24672	.83120	1.20308	16
45 46	.71990	1.38909 1.38824	.74674	1.33916	.77428	1.29152	.80258 .80306	I.24597 I.24523	.83169 .83218	1.20237	15
47	.72078	1.38738	.74764	1.33754	.77521	1.28007	.80354	1.24449	.83268	1.20095	13
48	.72122	1.38653	.74810	1.33673	.77568	1.28919	.80402 .80450	1.24375 1.24301	.83317 .83366	1.20024 1.19953	12
50	.72211	1.38484	.74055	1.33592	.77661	1.28764	.80450	1.24301	.83415	1.19882	10
51	.72255	1.38399	.74946	1.33430	.77708	1.28687	.80546	1.24153	.83465	1.19811	
52 53	.72299	1.38314	.74991	1.33349	.77754	1.28610	.80594	1.24079	.83514	I.19740 I.19669	
53	.72344	1.38145	.75037 .75082	1.33208	.77801 .77848	1.28456	.80042 .80690	1.24005	.83504	1.19009	6
55	.72432	1.38060	.75128	1.33107	.77895	1.28379	.80738	1.23858	.83662 1.19		8
56 57	.72477	1.37976	·75173 ·75219	1.33026 1.32946	-77941 -77988	1.28302	.80786 .80834	1.23784	0 .83761 1.1938		4
58	.72565	1.37807	.75264	1.32865	.78035	1.28148	80882	1.23637	.83811	1.19316	2
59	.72610 .72654	1.37722 1.37638	.75310	1.32785	.78082	1.28071	.80930 .80978	1.23563 1.23490	.83860 .83910	1.19246	1 D
1	Cotang	Tang	Cotang		Cotang	Tang	Cotang	Tang	Cotang	Tang	1
	54	4°	53	3°	5	20	5	r°	5	0 ⁰	

- /	40	°	41	1°	42	20	43	3°	4	4°	,
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.83910	1.19175	.86929	1.15037	.90040	1.11061	.93252	1.07237	.96569	1.03553	50
1.1	.83960	1.19105	.86980	1.14969	.90093	1.10996	.93306	1.07174	.96625	1.03493	59
	.84009 .84059	1.19035	.87031	1.14902	.90146	1.10931	.93360	1.07112	.96681	1.03433	
3	.84108	1.18894	.87082	1.14834	.90199	1.10802	.93415 .93469	1.07049	.96738 .96794	1.03372 1.03312	57 56
in the	.84158	1.18824	.87184	1.14699	.90304	1.10737	.93524	1.06925	.96850	1.03252	55
	.84208	1.18754	.87236	1.14632	.90357	1.10672	.93578	1.06862	.96907	1.03192	54
Z	.84258	1.18684	.87287	1.14565	.90410	1.10607	.93633	1.06800	.96963	1.03132	53
0	.84357	1.18544	.87338	1.14498	.90403	1.10543	.93688 .93742	1.06738	.97020 .97076	1.03072	52 51
10	.84407	1.18474	.87441	1.14363	.90569	1.10414	.93797	1.06613	.97133	1.02952	50
11	.84457	1.18404	.87492	1.14296	.90621	1.10349	.93852	1.06551	.97180	1.02892	49
12	.84507	1.18334	.87543	1.14229	.90674	1.10285	.93906	1.06489	.97246	1.02832	48
13	.84556	1.18264	.87595	1.14162	.90727	1.10220	.93961	1.06427	.97302	1.02772	47
14 15	.84656	1.18125	.87698	1.14095	.90781 .90834	1.10156	.94016 .94071	1.06365 1.06303	·97359 ·97416	1.02713	46
16	.84706	1.18055	.87749	1.13961	.90887	1.10027	.94125	1.06241	.97472	1.02593	45
17	.84756	1.17986	.87749 .87801	1.13894	.90940	1.09963	.94180	1.06179	.97529	1.02533	H3
15	.84806	1.17916	.87852 .87904	1.13828	.90993	1.09399	.94235	1.06117	.97586	1.02474	43
20	.84906	1.17777	.87955	1.13/01	.91040	1.09834 1.09770	.94290 .94345	1.00050	.97643 .97700	1.02414	41
21	.84956	1.17708	.88007	1.13627	.91153	1.09706	.94400	1.05932	.97756	1.02205	30
18.0	.85006	1.17638	.88059	1.13561	.91206	1.09642	.94455	1.05870	.97813 1.02236		38
23	.85057	1.17569	.88110	1.13494	.91259	1.09578	.94510	1.05809	.97870 1.02176		37
24 25	.85107 .85157	1.17500	.88162 .88214	1.13428 1.13361	.91313 .91366	1.09514	.94565	1.05747 1.05685	.97927 1.02117 .97984 1.02057		36
26	.85207	1.17361	.88265	1.13205	.91419	1.09386	.94676	1.05624	.97984 1.02057 .98041 1.01998		35
27	.85257	1.17292	.88317	1.13228	.91473	1.09322	.94731	1.05562	.98098 1.01939		33
28	.85308	1.17223	.88369	1.13162	.91526	1.09258	.94786	1.05501	.98155 1.01879		32
299 30	.85358 .85408	1.17154 1.17085	.88421 .88473	1.13096	.91580 .91633	1.09195 1.09131	.94841 .94896	1.05439	.98213 .98270	1.01820	31
JI	.85458	1.17016	.88524	1.12963	.91687	1.09067	.94952	1.05317	.98327	1.01702	29
32	.85509	1.16947	.88576 .88628	1.12897	.91740	1.09003	.95007	1.05255	.98384	1.01642	
33 34	.85559	1.16800	.88680	1.12831	.91794 .91847	1.08940	.95062	1.05194	.98441	1.01583	27
35	.85660	1.16741	.88732	1.12600	.91901	1.08813	.95173	1.05072	.98556	1.01465	25
36	.85710	1.16672	.88784	1.12633	.91955	1.08749	.95229	1.05010	.98613	1.01406	254
37 38	.85761 .85811	1.16603	.88836	1.12567	.92008	1.08686	.95284	1.04949	.98671	1.01347	23
30	.85862	1.16535	.88940	1.12501 1.12435	.92062	1.08022	.95340 .95395	1.04888	.98728 .98786	1.01288	21
140	.85912	1.16398	.88992	1.12369	.92170	1.08496	.95451	1.04766	.98843	1.01170	20
41	.85963	1.16329	.89045	1.12303	.92224	1.08432	.95506	1.04705	.98901	1.01112	19
42	.86014	1.16261	.89097	1.12238	.92277	1.08369	.95562	1.04644	.98958	1.01053	18
43	.86064	1.16192	.89149	1.12172	.92331	1.08306	.95618	1.04583	.99016	1.00994	17
44 45	.86115	1.16124	.89201 .89253	1.12106 1.12041	.92385	1.08243	.95673 .95729	1.04522	.99073	1.00935	10
46	.86216	1.15987	.89306	1.11975	.92493	1.08116	.95785	1.04401	.99189	1.00818	14
47 48	.86267	1.15919	.89358	1.11909	.92547	1.08053	.95841	1.04340	.99247	1.00759	13
	.86318	1.15851	.89410	1.11844	.92601	1.07990	.95897	1.04279	.99304	1.00701	12
10 50	.86368 .86419	1.15783 1.15715	.89463 .89515	1.11778	.92655 .92709	1.07927 1.07864	.95952 .96008	1.04218 1.04158	.99362 .99420	1.00583	11 10
51	.86470	1.15647	.89567	1.11648	.02763	1.07801	.96064	1.04097	.99478 1.00325		8
52	.86521	1.15579	.89620	1.11582	.92817	1.07738	.96120	1.04036	.99536 1.00467		
53 54	.86572	1.15511	.89672 .89725	1.11517	.92872	1.07676	.96176	1.03976	.99594 1.00408 .99652 1.00350		76
54	.86674	1.15443	.89725	1.11452	.92926	1.07013	.90232	1.03915	.99710 1.00291		5
56	.86725	1.15308	.89830	1.11321	.93034	1.07487	.96344	1.03794	.00768 1.00233		4
57	.86776	1.15240	.89883	1.11256	.93088	1.07425	.96400	1.03734	4 .99826 1.00175		3
59	.86827	1.15172	.89935 .80088	1.11191	.93143	1.07362	.96457 .96513	1.03674	.99884	1.00110	2 1
59	.86929	1.15104	.90040	1.11120	.93197 .93252	1.07299 1.07237	.96569	1.03013	1.00000	1.00000	0
-	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	
1			48	00		.0		0		-0	7
	49	1	42	,	. 47		40	46° 45°		3	

LOGARITHMIC TRIGONOMETRIC FUNCTIONS

"	1	log sin	d	s	Т	log tan	c. d.	log cot	С	log cos	
				6.	685				5.314		-
0	0									0.00000	00
60	1	4.46373	30103	57	57	4.46373	30103	3.53627	43	0.000000	59
120	2	4.76476	17609	57	57	4.76476	17609	3.23824	43	0.000000	58
180	3	4.94085	12494	57	58	4.94085	12494	3.05915	43	D. CORRECT	57
240	4	3.06579 3.10270	9691	57	58 58	3.06579	9691	2.93421	42	D. LOOKOKI	56
360	56	3.24188	7918	57 57	58	3.24188	7918	2.83730 2.75812	42	0.000000 0.000000	55 54
420		3.30882	6694	57	58	3.30882	6694	2.69118	42	0.00000	53
480	78	3.36682	5800	57	58	3.36682	5800 5115	2.63318	42	0.00000	52
540	9	3.41797	4576	57	58	3.41797	4576	2.58203	42	0.00000	51
000	10	3.46373	1	57	58	3.46373		2.53627	42	IT.COORS	50
660	11	3.50512	4139	57	58	3.50512	4139	2.49488	42	0.00000	110
720	12	3.54291	3779	57	58	3.54291	3779	2.45709	42	0.00000	48
1 780	13	3.57767	3476 3218	57	58	3.57767	3476	2.42233	42	0.000000	47
840	14	3.60985	2997	57	58	3.60986	3219 2996	2.39014	42	0.00000	46
000	15	3.63982	2802	57	58	3.63982	2803	2.36018	42	0.00000.0	15
960 1020	16	3.66784	2633	57	58 58	3.66785	2633	2.33215	42	0.00000	144
1020	17	3.69417	2483	57	58	3.69418	2482	2.30582	42	T.99999 T.99999	43
1140	10	3.74248	2348	57	58	3.74248	2348	2.25752	42	T.999999	42
1200	20	3.76475	2227	57	58	3.76476	2228	2.23524	44	I.999999	30
			2119		-		2119				
1260	21	3.78594	2021	57	58	3.78595	2026	2.21405	42	T.999999	39
1320	22	3 80615	1930	57	58	3.80615	1931	2.19385	42	T.99999	38
1380	23	3.82545 3.84393	1848	57 57	58 58	3.82546 3.84394	1848	2.17454 2.15606	42	T.999999	37
1500	25	3.86166	1773	57	58	3.86167	1773	2.13833	42	T.99999 T.99999	30
1560	26	3.87870	1704	57	58	3.87871	1704	2.12120	42	1.00000	34
1620	27	3.89509	1639	57	58	3.80510	1639	2.10490	42	T.999999	33
1680	28	3 91088	1579 1524	57	58	3.91089	1579 1524	2.08911	42	1.99999	32
1740	29	3.92612	1472	57	59	3.92613	1473	2.07387	41	T.99998	31
1800	30	3.94084		57	59	3.94086		2.05914	41	T.999998	30
1860	31	3.95508	1424	57	59	3.95510	1424	2.04490	41	¥.99998	29
1020	32	3.95300	1379	57	59	3.96889	1379	2.03111	41	T.99998	
1980	33	3.98223	1336	57	59	3.98225	1336	2.01775	41	1.99998	27
2040	34	3.99520	1 297 1 259	57	59	3.99522	1297 1259	2.00478	41	Ĩ.99998	56
2100	35	2.00779	1223	57	59	2.00781	1223	1.99219	41	T.99998	25
2160	36	2.02002	1190	57	59	2.02004	1190	1.97996	41	Ĩ.999998	24
2220	37 38	2.03192 2.04350	1158	57 57	59 59	2.03194 2.04353	1159	1.96806	4I 4I	T.99997 T.99997	23
2340	39	2.05478	1128	57	59	2.05481	1128	1.94519	41	T.99997	21
2400	40	2.06578	1100	57	59	2.06581	1100	1.93419	41	T.99997	20
			1072			1	1072				
2460	41	2.07650	1046	56	60	2.07653	1047	1.92347	40	1.99997	19
2520 2580	42	2.08696	1022	56 56	60 60	2.08700	1022	1.91300 1.00278	40	Ĩ.99997 Ĩ.99997	18
2500	43	2.09718	899	50	60	2.09722	998	1.90278	40	1.99997 T.00006	17
2700	45	2.11693	976	56	60	2.11696	976	1.88304	30	T.99996	15
2760	46	2.12647	954	56	60	2.12651	955	1.87349	40	1.99996	14
2820	47	2.13581	934 914	56	60	2.13585	934 915	1.86415	40	1.99996	13
2830	48	2.14495	896	56	60	2.14500	895	1.85500	40	1.99996	12
2940 3000	49	2.15391 2.16268	877	56 56	60 61	2.15395 2.16273	878	1.84605	40	T.99996	11
3000	50	2.10200	860	50	01	2.102/3	860	1.03727	39	T.99995	KO
3060	51	2.17128		56	61	2.17133		1.82867	39	T.99995	12
3120	52	2.17971	843	56	61	2.17976	843 828	1.82024	39	1.99995	N
3180	53	2.18798	827 812	56	61	2.18804	812	1.81196	39	ī.99995	7
3240	54	2.19610	797	56	61	2.19616	797	1.80384	39	1.99995	
3300 3360	55 56	2.20407 2.21189	782	56 56	61 61	2.20413	782	1.79587 1.78805	39	T.99994	5
3300	50	2.21109	769	50	61	2.21195	7150	1.78036	39 39	T.99994 T.99994	3
3480	58	2.22713	755	55	62	2.22720	756	1.77280	38	I.99994	2
3540	59	2.23456	743 730	55	62	2.23462	742 730	1.76538	38	T.99994	1
3600	60	2.24186	130	55	62	2.24192	130	1.75808	38	T.99993	0
				6.6	85				5.314		
		log cos	1	s	т	log cot	c. d.	log tan	c	log sin	,
					-		C. GI				

88°

"	Ø	log sin	а	S	т	log tan	c. d.	log cot	С	log cos	
				6.0	585				5.314		
3600	0	2.24186		55	62	2.24192	-	1.75808	38	T.99993	160
3660	I	2.24903	717	55	62	2.24910	718	1.75090	38	T.99993	59
3720	2	2.25609	706	55	62	2.25616	706 696	1.74384	38	T.99993	58
3780	3	2.26304	695 683	55	62	2.26312	684	1.73688	38	T.99993	57
3840	4	2.26988	673	55	63	2.26996	073	1.73004	37	1.99992	56
0,000	5	2.27661	663	55	63	2.27669	663	1.72331	37	1.99992	55
3960		2.28324	653	55	63	2.28332	654	1.71668	37	T.99992	54
4020	7	2.28977	6744	55	63 63	2.28980	643	1.71014	37	T.99992	53
4000	0	2.29621 2.30255	634	55 55	63	2.29029	634	1.70371 1.69737	37	T.99992 T.99991	52
3206	10	2.30879	624	55	63	2.30888	625	1.60112	37	1.99991	50
		2.30079	616	24		2.30000	617	1.0yinz	01	******	30
4260	II	2.31495	608	54	64	2.31505	607	1.68495	36	T.99991	10
4320	12	2.32103	500	54	64	2.32112	800	.67888	36	1.99990	48
4380	13	2.32702	599	54	64	2.32711	591	1 67289	36	ī.99990	47
4440	14	2.33292	583	54	64	2.33302	584	1.66698	36	1.99990	46
4500	15	2.33875	575	54	64	2.33886		1.66114	36	7.99990	45
4560	16	2.34450	568	54	65	2.34461	575 568	1.65539	35	1.99989	44
4680	17	2.35018 2.35578	560	54	65	2.35029 2.35590	561	1.64971	35	1.99989 1.99989	43
4740	19	2.36131	553	54	65	2.35390	553	1.63857	35	T.99989	41
4800	00	2.36678	547	54	65	2.36689	546	1.63311	35	1.99988	40
	-		539	34			540	1103300	00		
4860	21	2.37217		53	66	2.37229		1.62771	34	T.99988	39
4920	22	2.37750	533 526	53	66	2.37762	533 527	1.62238	34	ī.99988	38
4980	23	2.38276	520	53	66	2.38289	520	1.61711	34	T.99987	37
5040	24	2.38796	514	53	66	2.38809	514	1.61191	34	1.99987	36
5100	25 26	2.39310 2.39818	508	53	66 67	2.39323	500	1.60677	34	1.99987	35
5220	20	2.39010	502	53 53	67	2.39832 2.40334	502	1.60168	33	1.99986 1.99986	34
5280	58	2.40320	496	53	67	2.40830	121061	1.59000	33	1.99986	33
5340	20	2.41307	491	53	67	2.41321	491	1.58679	33	1.99985	31
5400	30	2.41792	485	53	67	2.41807	486	1.58193	33	1.99985	30
	-		480				480		00		1
5460	31	2.42272	474	52	68	2.42287	. 475	1.57713	32	T.99985	29
5520	32	2.42746	474	52	68	2.42762	470	1.57238	32	1.99984	28
5580	33	2.43216	464	52	68	2.43232	464	1.56768	32	T.99984	27
5640	34	2.43680	459	52	68	2.43696	460	1.56304	32	1.99984	26
5700	35 36	2.44139 2.44594	455	52 52	69 69	2.44156	455	1.55844	31	1.99983 1.99983	25
5760 5820	37	2.44594	450	52	69	2.45061	450	1.55389	31	T.99983	23
5880	38	2.45489	445	52	69	2.45507	446	1.54493	31	T.99982	22
5940	39	2.45930	441	51	69	2.45948	44 I	1.54052	31	1.99982	21
BERN	40	2.46366	436	51	70	2.46385	437	1.53615	30	T.99982	20
			433				432				1
6060	41	2.46799	427	51	70	2.46817	428	1.53183	30	T.99981	19
6120	42	2.47226	424	51	70	2.47245	424	1.52755	30	T.99981	18
6180 6240	43	2.47650	419	51	70	2.47669	420	1.52331	30	¥.99981	17
6300	44	2.48485	416	51 51	71	2.48089	416	1.51911	29 20	1.99980 1.99980	10
6360	45	2.48806	411	51	71	2.40505	412	1.51495	29	1.99900 T.00070	15
6420	47	2.49304	408	50	72	2.49325	408	1.50675	10	I.00070	13
6480	48	2.49708	404,	50	72	2.49729	404	1.50271	18	T.99979	12
6540	49	2.50108	400	50	72	2.50130	401	1.49870	28	1.99978	11
6600	50	2.50504	396	50	72	2.50527	397 .	1.49473	28	ī.99978	10
1111			393		1		393				
boho.	51	2.50897	390	50	73	2.50920	390	1.49080	27	1.99977	9
6720 6780	52	2.51287	386	50	73	2.51310	386	1.48690	27	T.99977	
0780 6840	53	2.51673	382	50	73	2.51696	383	1.48304	27	1.99977	76
6900	54 55	2.52055 2.52434	379	50 49	73	2.52079	380	1.47921 1.47541	27	T.99976 T.99976	5
6960	55	2.52810	.+76	49	74	2.52835	376	1.47165	20	T.99975	5
7020	57	2.53183	373	49	74	2.53208	373	1.46792	26	I.99975	3
7080	58	2.53552	369	49	75	2.53578	370	1.46422	25	I.99974	2
7140	59	2.53919	367 363	49	75	2.53945	307	1.46055	25	T.99974	1
7200	. 60	2.54282	303	49	1 75	2.54308	303	1.45692	25	T.99974	0
				6.	685				5.314		
		log cos	đ	s	т	log cot	c. d.	log tan	c	log sin	

7200 7260											
7260				6.0	685				5.314		
7260	0	2.54282		NO.	75	2.54308		1.45692	25	1.00074	60
	I	2.54642	360	30	75	2.54669	361	1.45331	25	T.99973	59
7320	2	2.54999	357	48	76	2.55027	358	1.44973	24	1.99973	58
7380	3	2.55354	355	48	76	2.55382	355	1.44618	24	T.99972	. 57
7440	4	2.55705	351 349	48	76	2.55734	352 349	1.44266	24	I.99972	56
7500	5	2.56054	346	48	77	2.50083	346	1.43917	23	T.99971	55
7560	6	2.56400	343	48	77	2.56429	344	1.43571	23	1.99971	1 84
7620	78	2.56743	341	48	77	2.56773	341	1.43227	23	1.99976	53
. 7680		2.57084	337	47	78	2.57114	338	1.42886	22	1.99970	52
7740	IO	2.57421 2.57757	336	47	78	2.57452 2.57788	336	1.42212	22	1.99969 1.99969	51
1000		2.3//3/	332	41	10	2.3//00	333			1.99909	am
7860	11	2.58089		47	79	2.58121		1.41879	21	T.99968	100
7920	12	2.58419	3.30	47	79	2.58451	330	1.41549	21	1.99968	48
7980	13	2.58747	328	47	79	2.58779	328 326	1.41221	21	1.99967	47
8040	14	2.59072	345	46	79 8a	2.59105	323	1.40895	21	I.99967	46
8100	15	2.59395	323	46		2.59428	343	1.40572	20	1.99967	45
8160	16	2.59715	318	46	80	2.59749	319	1.40251	20	T.99966	iit ii
8220 8280	17	2.60033	316	46	80 81	2.60068	316	1.39932	1911	1.99966	43
8280	18	2.60349 2.60662	313	40	81	2.60384 2.60608	314	1 39616	19	T.99965	HE.
8400	19	2.60073	311	45	82	2.61000	311	1.39302	19 18	T.99964 T.99964	41
oatoo		2.009/3	300	45	0.0	2.01009	310	1.30991	10	1.99904	140
8460	21	2.61282		45	82	2.61310		1.38681	18	1.99963	30
8520	22	2.61589	307	45	82	2.61626	307	1.38374	18	1.99963	88
8580	23	2.61894	305	45	83	2.61931	305	1.38069	17	T.99962	37
8640	24	2.62196	302	45	83	2.62234	303 301	1.37766	17	T.99962	36
8700	25	2.62497	298	45	83	2.62535	200	1.37465	17	1.99961	35
8760	26	2.62795	296	44	84	2.62834	297	1.37166	16	T.99961	34
8820	27	2.63091	204	44	84	2.63131	205	1.36869	16	T.99960	33
RHOMO	H	2.63385	293	44	84 85	2.63426	292	1.36574	16	T.99960	32
8940	29 30	2.63678 2.63968	290	44	85	2.63718	291	1.36282	15 15	T.99959	31
9000	30	2.03900	::88	44	05	2.04009	280	1.35991	15	T.99959	10
0060	31	2.64256		44	85	2.64208		1.35702	15	T.99958	29
0120	32	2.64543	287	43	86	2.64585	287	1.35415	14,	T.99958	28
9180	33	2.64827	284 283	43	86	2.64870	285 284	1.35130	14	T.99957	27
9240	34	2.65110	203	43	87	2.65154	281	1.34846	13	T.99956	26
9300	35	2.65391	279	43	87	2.65435	280	1.34565	13	T.99956	25
9360	36	2.65670	277	43	87	2.65715	278	1.34285	13	T.99955	253
9420	37	2.65947	276	42	88	2.65993	276	1.34007	12	T.99955	23
9480	38	2.66223	274	42	88	2.66269	274	1.33731	12	1.99954	21.5
9540 9600	39 40	2.66497 2.66769	272	42	80	2.66543	273	1.33457	12 11	T.99954	21 20
9000	40	2.00709	270	42	09	2.00010	271	1.33184	11	T.99953	20
9660	41	2.67039		42	89	2.67087		1.32913	TI	T.99952	19
9720	42	2.67308	269	41	00	2.67356	269	1.32644	10	T.99952	18
9780	43	2.67575	267 266	41	00	2.67624	268 266	1.32376	10	T.99951	17
9840	144	2.67841	200	41	00	2.67890	200	1.32110	10	T.99951	16
0000	45	2.68104	203	41	91	2.68154	204	1.31846	1042	T.99950	15
0060	46	2.68367	260	41	91	2.68417	261	1.31583	09	T.99949	14
10020	47	2.68627	259	40	92	2.68678	260	1.31322	08	T.99949	13
10080	48	2.68886	258	40	92 02	2.68938	258	1.31062	08	T.99948 T.99948	12
10141	40	2.09144 2.69400	256	40	92	2.09190	257	1.30547	07	1.99948 T.99947	10
10200	20	2.09400	254	40	23	2.09453	255	1.3034/	07.	8.999947	10
10260	51	7.69654		40	93	2.69708		1.30292	07	T.99946	0
10320	52	2.69907	253	39	94	2.69962	254	1.30038	06	1.99946	9
10380	53	2.70159	252	39	94	2.70214	252	1.29786	86	T.99945	
10440	54	2.70409	250 249	39	95	2:70465	251 249	1.29535	05	T.99944	7 6
10500	55	2.70658	249	39	95	2.70714	249	1.29286	05	T.99944	5
10560	56	2.70905	246	39	198	2.70962	246	1.200,38	05	T.99943	1
10620	57	2.71151	244	38	96	2.71208	245	1.28792	0.3	T.99942	3
10680	58	2.71395	243	38	96	2.71453	244	1.28547	04	T.99942	
10740	59	2.71638	242	38 38	97 97	2.71697 2.71940	243	1.28303	03	T.99941 T.99940	0
	ANO .	3.71000				4.71940		1.20000		1.99940	
				6.0	85				5.314		
		log cos	а	s	T	log cot	c. d.	log tan	c	log sin	,

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0	×	1	

/ log sin d log tan c. d. log cot log cot p. p. 0 27,7880 2,72450 22,7480 2,72450 27,7481 2,72450 27,7481 2,72450 27,7481 2,72450 27,7481 2,72450 27,7481 2,72450 27,7481 2,72450 27,7481 2,72450 27,7482 22,72450 23,00 23,7343 23,424,23 23,00 23,10 24,441 1,00400 1,00938 51 10 33,72430 23,00 23,10 24,441 1,00400 1,00938 51 10,01,10 11,04 27,7343 23,00 23,00 23,00 11,04 1,04,00 10,00 10,00 10,00 11,04 23,00 10,00 10,00 10,00 10,00 10,00 10,00 10,00 10,00 10,00 10,00 10,00 <td< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></td<>												
1 2	'	log sin	đ	log tan	c. d.	log cot	log cos			p	. p .	
1 2		3 *** 990		3 71040		1 28060	T 00040	60		238	294	990
2 27,250 237,250 27,250 1.9903 68 7 7.8 3.7 3.7 3.7.3									6			
3 2			239	2.72420				58		27.8		
4 27,783 23,28 37,2896 1,27184 1,99038 55 10 35.7 35.1 34.4 5 27,3909 233 27,3366 234 1,26654 1,99036 55 10 39.7 35.0 34.4 7 27,3334 233 27,366 234 1,26654 1,99036 55 10 39.7 73.0 35.1 34.4 7 27,3309 233 27,367 230 27,367 230 27,367 230 27,367 230 27,367 230 27,367 230 1,36501 100.00 110.0010 110.0010 114.5 27,575 220 21.6 225 220 21.6 22				2.72659		1.27341			8			
5 2.7.8669 4.35 2.7.312 36 166868 1.99937 55 10 9.0		2.7.2834		2.72806		1.27104			0			
n 2.73303 2.333 2.73506 2.33 1.26634 1.90936 53 30 19.0 170.0 110						1.26868		55			39.0	38.2
2 2 2 2 2 2 2 2 1 2 1	Ø			2.73366								
p 2.75907 2.3907 2.74963 2.29 1.25978 1.09934 51 10 2.74254 2.28 2.290 1.25978 1.09934 50 12 2.74650 2.26 2.74474 2.27 1.25926 1.09933 46 7 6.37 2.25 2.200 1.26 13 2.74650 2.26 2.75934 2.25 1.25926 1.09933 45 7 5.3 2.25 7.3693 3.88 3.03 3.88 3.03 3.88 3.03 1.25 1.09930 45 10 3.75 3.67 7.3 7.20 7.33 7.20 7.33 7.20 7.33 7.20 7.33 7.20 7.33 7.20 7.33 7.20 7.33 7.20 7.33 7.20 7.33 7.20 7.76 7.77 7.777 7.777 7.7777 7.33 7.2 7.7773 2.13 1.22402 1.09923 35 10 3.5.3 3.47 7.7 <t< td=""><td>7</td><td></td><td></td><td>2.73600</td><td>232</td><td></td><td></td><td></td><td></td><td>119.0</td><td></td><td></td></t<>	7			2.73600	232					119.0		
10 2.742.26 2.89 1.25768 1.99934 45 50 11 2.74454 2.26 2.26 2.26 2.26 2.20 2.16 13 2.74906 2.26 2.74474 2.27 1.25325 1.09933 46 6 2.5,5 2.5,5 2.5,5 2.5,5 2.5,5 2.23 2.75433 2.27,5			230							158.7	156.0	152.7
11 3.74456 2.26 3.74576 2.26 1.25670 T.09033 40 6 6 2.25 2.20 21.6 13 3.74660 2.26 3.74738 2.25 1.25670 T.09033 48 6 42.5 2.2.0 21.6 14 3.74265 2.224 1.25670 T.09033 46 6 3.3.6 3.3.0					229				50	1 198.3	195.0	190.8
11 3.74454 2.7650 7.9933 40 6 2.32 2.20 31.6 32 2.74906 2.26 7.44974 2.25 7.29932 47 5 33.8 33.6 33.8 33.6 33.8 33.6 33.8 33.6 33.8 33.6 33.8 33.6 33.8 33.6 33.8 33.6 33.8 33.7 7.20 33.8 33.7 7.20 33.7 7.20 7.25 7.3 7.2 7.25 7.3 7.2 <td>10</td> <td>2.74220</td> <td>228</td> <td>6.74296</td> <td>220</td> <td>1.25/00</td> <td>1.99934</td> <td>50</td> <td></td> <td>005</td> <td>000</td> <td>010</td>	10	2.74220	228	6.74296	220	1.25/00	1.99934	50		005	000	010
12 2.747680 2.3 2.74788 2.252 1.99932 48 7 45 3.5 3.5 3.5 3.5 3.5 3.5 3.30 3.8 3.30 1.12 3.1 1.09012 3.00 11.65 1.65 1.12 1.23 1.23 1.23 1.23 1.23 1.23 1.23 1.23 1.23 1.23 1.23 1.09023 35 6 2.12 2.08 2.02 2.02 2.02 2.02 2.02 2.02 2.02 2.02 2.02 2.02 </td <td>11</td> <td>2.74454</td> <td></td> <td>2.74521</td> <td></td> <td>1.25470</td> <td>1.00033</td> <td>80</td> <td>6</td> <td></td> <td></td> <td></td>	11	2.74454		2.74521		1.25470	1.00033	80	6			
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58 2.93740 140 2.93903 147 1.06097 T.99837 2 30 74.5 73.5 0.5 59 2.93885 145 2.94040 146 1.05951 T.99836 1 40 99.3 98.0 0.7 50 2.94030 145 2.94195 146 1.05805 T.99836 1 40 99.3 98.0 0.7	57	2.93594		2.93756		1.06244	T.99838	3	20 49.7 49.0 0.3
59 2.03885 143 2.94049 146 1.05951 T.99836 1 40 99.3 98.0 0.7 60 2.94030 145 2.94195 146 1.05805 T.99834 0 50 124.2 122.5 0.8		2.93740		2.93903				2	30 74.5 73.5 0.5
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log cos d log cot c. d. log tan log sin ' p. p.	60	2.94030	-45	2.94195	.40	1.05805	1.99834	0	50 124.2 122.5 0.8
log cos d log cot c. d. log tan log sin ' p. p.									
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		log cos	d	log cot	c.d.	log tan	log sin	,	p. p.
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D	2.94030		2.94195		1.05805	T.00834	60		145	141	141
I	2.94030	144	2.94195	145	1.05660	T.99833	59	6	14.5		
2	2.94317	143	2.94485	145	1.05515	T.99832	58		14.5	14.3	14.1
3	2.94461	144	2.94630	145	1.05370	1.99831	57	7問	19.3	10.7	16.5
i	2.94603	142	2.94773	143	1.63227	1.99830	56	9	21.8	21.5	21.2
	2.947.46	143	2.94917	144	1.05083	T.99829	55	10	24.2	23.8	23.5
5	2.94887	141	2.95060	143	1.04940	1.99828	54	1351	48.3	47.7	47.0
7	2.95029	142	2.95202	142	1.04798	T.99827	53	30	72.5	71.5	70.5
8	2.95170	141	2.95344	142 142	1.04656	T.99825	52	40	06.7	05 3	94.0
10	2.95310	140 140	2.95486	142	1.04514	T.99824	51	50	120.8	119.2	117.5
10	2.95450	140	2.95627	141	1.04373	T.99823	50				
		139		140					139	138	136
II	2.05580		2.95767		1.04233	T.99822	40	6	13.9	13.8	13.6
12	2.95728	139	2.95908	141	1.04092	1.99821	48		16.2	16.1	15.0
13	2.95728 2.95867	139 138	2.96047	139	1.03953	1.99820	47	7	18.5	18.4	18.1
14	2.96005	130	2.96187	140 138	1.03813	1.99819	46	0	20.9	20.7	20.4
15	2.96143	138	2.96325	130	1.03675	1.99817	45	10	23.2	23.0	22.7
16	2.96280	137	2.96464	139	1.03536	1.99816	44	20	46.3	46.0	
17	2.96417	136	2.96602	130	1.03398	1.99815	43	30	69.5	69.0	45.3 68.0
18	2.96553	136	2.96739	138	1.03261	1.99814	42	40	92.7	92.0	90.7
19	2.96689	136	2.96877	136	1.03123	1.99813	41	50	115.8	115.0	113.3
1205	2.96825		2.97013		1.02987	1.99812	40				
		135		137					135	133	131
21	2.96960	135	2.97150	135	1.02850	1.99810	39	6	13.5	13.3	13.1
22	2.97095	134	2.97285	135	1.02715	T.99809	38		15.8	15.5	15.3
23	2.97229	134	2.97421	135	1.02579	1.99808	37	78	18.0	17.7	17.5
24	2.97363	133	2.97556	135	1.02444	1.99807	36	9	20.3	20.0	19.7
25	2.97496	133	2.97691	134	1.02309	1.99806	35	IO	22.5	22.2	19.7
20	2.97629	133	2.97825	134	1.02175	1.99804	34	20	45.0	44.3	43.7
27	2.97762 2.97894	132	2.97959 2.98092	133	1.02041	T.99803 T.99802	33	30	67.5	66.5	65.5
30	2.97894	132	2.98092	133	1.01908	1.99802 1.99801	32	40	90.0	88.7	87.3
30	2.98020	131	2.98225	133	1.01775	T.99800	31	50	112.5	110.8	109.2
30	2.90157		2.90350		1.01042	1.99000	30				
	7 .0 .00	131	0	132		T			129	128	126
31 32	2.98288	131	2.98490 2.98622	132	1.01510	T.99798	29	6	12.9	12.8	12.6
	2.98549	130	2.98022	131	1.01378	1.99797	28	7	15.1	14.9	14.7
30	2.98549	130	2.98753	131	I.01247 I.01116	I.99796 I.99795	27 26		17.2	17.1	
35	2.98808	129	2.90015	131	1.00985	I.00703	25	12	19.4	19.2	18.9
36	2.98937	129	2.99015	130	1.00855	I.99793	24	10	21.5	21.3	21.0
37	2.99066	120	2.99275	130	1.00725	1.99791	23	20	43.0	42.7	42.0
38	2.99194	128	2.99405	130	1.00595	1.99790	22	30	64.5	64.0	63.0
39	2.99322	128	2.99534	129	1.00466	T.99788	21	40	86.0	85.3	84.0
180	2.99450	128	2.99662	1 28	1.00338	1.99787	283	50	107.5	106.7	105.0
		127		129						200	100
41	2.99577		2.00701		1.00200	¥.99786	10		125	128	122
42	2.99704	127	2.99919	1 28	1.00081	T.99785	18	6	12.5	12.3	12.2
43	2.99830	126 126	1.00046	127 128	0.999:1	T.99783	17	78	14.6	14.4	14.2
44	2.99956	120	T.00174	125	0.99816	T.99782	16		16.7	16.4	16.3
45	T.00082	120	T.00301	127	0.99699	1.99781	15	10	18.8	18.5	18.3
46	¥.00207	125	1.00427	1 20	0.99573	T.99780	14	10	20.8	20.5	20.3
47	T.00332	125	T.00553	120	0.99447	T.99778	13	30	62.5	61.5	40.7
48	1.00450	125	T.00679	120	0.99321	I.99777	12	30	83.3	82.0	81.3
110	T.00581	123	1.00805	125	0.99195	1.99776	11	50	104.2	102.5	
50	¥.00704		¥.00930		0.99070	1.99775	10	30	Jodie .		
		124		125					201	100	
51	1.00828	123	1.01055	124	0.98945	1.99773	9		121	120	1
52	T.00951	123	I.01179	124	0.98821	T.99772		6	12.1	12.0	0.1
53	Ī.01074	122	T.01303	124	0.98697	T.99771	7	7	14.1	14.0	0.1
54	1.01196	122	I.01427	123	0.98573	T.99769		0	16.1 18.2	18.0	0.1
55 56	T.01318 T.01440	122	1.01550 T 01672	123	0.98450	T.99768	5	10	20.2	18.0	0.2
	I.01440 T.01561	121	I.01673	123	0.98327	T.99767 T.99765	14	10	40.3	20.0	0.2
57 58	1.01501	121	T.01796 T.01918	122	0.95204	1.99705 T.99764	2	30	60.5	60.0	0.5
	I.01803	1.21	T.02040	122	0.97960	I.99763	1	40	80.7	80.0	0.7
59	I.01923	120	I.02040	122	0.97838	I.99761	D	50	80.7	100.0	0.8
	log cos	đ	log cot	c. d.	log tan	log sin	,		p	. p.	

,	log sin	a	log tan -	c. d.	log co+	log cos		p. p.
D	1.01923	120	Y.02162	121	0.97835	1.99761	60	121 120 119
1	T.02043	120	T.02283	121	0.97717	¥.99760	59	6 12.1 12.0 11.9
3	T.02163	120	T.02404	1.21	0.97596	1.99759	58	7 14.1 14.0 13.9 8 16.1 16.0 15.9
3	T.02283	119	1.02525	1.20	0.97475	T.99757	57	
4	T.02402	118	1.02645	121	0.97355	1.99756	56	18.2 18.0 17.9
56	T.02520	119	T.02766	119	0.97234	1.99755	55	10 2012 2010 19.8
	T.02639	118	T.02885	120	0.97115	I.99753	54	INI 40.3 40.0 39.7
78	T.02757	117	T.03005	119	0.96995	I.99752	53	TE 60.5 60.0 59.5
	1.02874	118	T.03124	118	0.96876	1.99751	52	40 80.7 80.0 79.3 50 100.8 100.0 99.2
0	T.02992	117	T.03242	119	0.96758	1.99749	51	50 100.8 100.0 99.2
10	T.03109		1.03361		0.96639	1.99748	50	
		117		118		_	1.00	118 117 116
II	T.03226	116	I.03479	118	0.96521	1.99747	49	6 11.8 11.7 11.6
12	T.03342	116	T.03597	117	0.96403	1.99745	48	7 13.8 13.7 13.5
13	T.03458	116	T.03714	118	0.96286	I.99744	47	8 15.7 15.6 15.5
14	T.03574	116	T.03832	116	0.96168	I.99742	46	9 17.7 17.6 17.4
15	T.03690	115	1.03948	117	0.96052	1.99741	45	10 10.7 10.5 10.3
16	¥.03805	115	1.04065	116	0.95935	T.99740	44	20 30.3 30.0 38.7
17	T.03920	II4	1.04181	116	0.95819	I.99738	43	30 50.0 58.5 58.0
18	T.04034	IIS	T.04297	116	0.95703	I.99737	42	40 78.7 78.0 77.3
19	T.04149	113	1.04413	115	0.95587	I.99736	41	50 98.3 97.5 96.7
20	1.04262		T.04528		0.95472	I.99734	40	
		114		115				115 114 113
21	T.04376		T.04643		0.95357	T.99733	39	6 11.5 11.4 11.3
22	T.04490	114	T.04758	115	0.95242	Ī.99731	38	
23	1.04603	113	I.04873	115	0.95127	T.99730	37	7 13.4 13.3 13.2 8 15.3 15.2 15.1
24	1.04715	112	1.04987	114	0.95013	1.99728	36	0 17.3 17.1 17.0
25	T.04828	113	1.05101	114	0.94899	I.99727	35	10 19.2 19.0 18.8
26	T.04940	II2	T.05214	113	0.94786	T.99726	34	20 38.3 38.0 37.7
27	1.05052	112 112	¥.05328	114	0.94672	Ĩ.99724	33	30 57.5 57.0 \$6.5
28	1.05164	112	Ī.05441	113 112	0.94559	1.99723	32	40 76.7 76.0 75.3
20	1.05275		T.05553		0.94447	T.99721	31	50 95.8 95.0 94.2
30	1.05386	III	T.05666	113	0.94334	1.99720	30	30 1 93.0 1 93.0 1 94.0
		III		112				110 1 111 1 110
31	T.05497		T.05778		0.94222	T.99718	20	112 111 110
32	1.05607	110	ï.05800	112	0.94110	1.99717	28	6 11.2 11.1 41.0
33	T.05717	IIO	1.06002	112	0.93998	1.99716	27	7 13.1 13.0 12.8 8 14.9 14.8 14.7
34	1.05827	110	1.06113	111	0.93887	1.99714	26	
34	T.05937	110	T.06224	III	0.93776	1.99713	25	9 16.8 16.7 16.5
36	T.06046	109	T.06335	III	0.93665	I.99711	24	10 18.7 18.5 18.3
37	1.06155	109	1.06445	110	0.93555	1.99710	23	37.3 37.0 36.7
37 38	T.06264	109	1.06556	III	0.93444	T.99708	22	30 56.0 55.5 55.0
39	T.06372	108	1.06666	110	0.93334	1.99707	21	10 74.7 74.0 73.3
40	1.06481	109	1.06775	109	0.93225	1.99705	10	50 93.3 92.5 91.7
		108		110				
41	T.06589		1.06885		0.93115	T.99704	19	109 108 107
41	1.00589	107	T.00005	109	0.93115	1.99704 1.99702	18	1 10.9 10.8 10.7
	T.06804	108	T.07103	109	0.93000	1.99702 T.99701	10	7 12.7 12.6 12.5 8 14.5 14.4 14.3
43	1.06011	107	1.07211	108	0.92097	1.99/01	16	
44	I.07018	107	1.07320	100	0.92680	ī.99698	15	16.4 16.2 16.1
45	T.07124	106	T.07428	108	0.92000	T.99696	14	10 18.2 18.0 17.8
40	T.07231	107	T.07536	108	0.92572	T.99695	13	36.3 36.0 35.7
48	T.07337	106	T.07643	107	0.92357	1.99693	12	30 54.5 54.0 53.5
40	I.07337	105	1.07751	108	0.92357	T.99692	11	40 72.7 72.0 71 3
50	1.07548	106	T.07751 T.07858	107	0.92142	T.99690	10	50 90.8 90.0 89.2
20	10/540	105		106	U.yarıqa			
	Tankes	105	T onch.	100	0.00006	T 00680		106 105 104
51	T.07653	105	T.07964 T.08071	107	0.92036	T.99689 T.99687	8	100 105 104
52	T.07758 T.07863	105	T.08071 T.08177	106	0.91929	1.99087 T.99686		
63	1.07803	105	1.08177 1.08283	106		1.99080	76	
54	T.07968 T.08072	104	1.08283 T.08389	106	0.91717	1.99084 T.99683		
55 56	1.08072	104	T.08495	106	0.91611	1.99003 1.99681	5	9 15.9 15.8 15.0 10 17.7 17.5 17.3
	T.08170	104	1.08495 T.08600	105	0.91505	1.99081	4	
57 58		103		105			3	
	T.08383 T.08486	103	T.08705 T.08810	105	0.91295	T.99678 T.99677	2	30 53.0 52.5 52.0 40 70.7 70.0 69.3
59	T.08480	103	I.08810 I.08914	104	0.91190 0.91086	1.99077 1.99675	1	40 70.7 70.0 69.3 50 88.3 87.5 86.7
00	1.00509		1.00914		0.91000	1.99075	0	20 1 00.3 1 07.5 1 00.7
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0	1.08589	103	1.08914	105	0.91086	T.99675		
I	T.08692	103	T.09019	104	0.90981	1.99674	59 58	
2	T.08795 T.08897	102	T.09123 T.09227	104	0.90877	T.99672 T.99670	57	7 12.3 12.1 12. 8 14.0 13.9 13.
3	1.08000	102	T.09330	103	0.90670	T.99669	56	9 15.8 15.6 15.
4	T.09101	102	I.09330	104	0.90566	T.99667	55	10 17.5 17.3 17.
56	T.09202	101	I.09434 I.09537	103	0.90463	T.99666	55	20 35.0 34.7 34.
	1.09202	102	I.09537	103	0.90360	T.99664	54	30 52.5 52.0 51.
8	T.00405	101	1.09040	101	0.90258	1.99663	52	10 70.0 69.3 68.
0	1.09506	101	T.09845	103	0.90155	T.99661	51	40 70.0 69.3 68. 50 87.5 86.7 85.
10	¥.09606	100	T.09947	102	0.90053	1.99659	50	30 1 07.5 1 00.7 1 03.
	1.09000	101	1109941	102	0.90033	1.99039	30	TES 1 202 1 20
11	Techon	101	7	102	0 90047	¥ 006+9	40	102 101 10
II I2	T.09707 T.09807	100	T.10049 T.10150	101	0.89951	T.99658	49	6 10.2 10.1 10.
		100		102	0.89748	T.99656	48	7 11.9 11.8 11. 8 13.6 13.5 13.
13 14	T.09907 T.10006	99	T.10252 T.10353	101	0.89647	T.99655 T.99653	47	
	T.10106	100	T.10353	IOI	0.89546	1.99651	45	9 15.3 15.2 15.
15 16	1.10205	99	T.10555	101	0.89340	T.99650	45	10 17.0 16.8 16.
17	I.10205	99	T.10555	101	0.89344	T.99648	44	20 34.0 33.7 33.
17	T.10304	98	T.10756	100	0.89344	1.99040 1.99647	43	30 51.0 50.5 50. 40 68.0 67.3 66.
10	T.10501	99	T.10856	100	0.89144	T.99645	41	40 68.0 67.3 66. 50 85.0 84.2 83.
20	T.10599	98	1.10050	100	0.89044	T.99643	41	50 85.0 84.2 83.
	110399	68	1110930	100	Support.	1199043	New Y	
	1.10697		T.11056	100	0.88944	¥.00642	-	99 98
21		98		99			39	6 9.9 9.8
23	T.10795 T.10893	98	1.11155 1.11254	99	0.88845	T.99640 T.99638	38	7 11.6 11.4 8 13.2 13.1
	T.10993	97		00	0.88647		37	
24 25	T.110990	97	T.11353 T.11452	99	0.88548	Ĩ.99637 Ĩ.99635	36	9 14.9 14.7
26	T.11184	97	T.11454	99	0.88449	1.99035 1.99633	35 34	10 16.5 16.3
	T.11281	97		98	0.88351			20 33.0 32.7
27	I.11201 I.11377	96	T.11649	98	0.88253	T.99632 T.99630	33	30 49.5 49.0
20	I.11377 I.11474	97	T.11747 T.11845	98	0.88155	T.99629	32	40 66.0 65.3
30	1.11474 1.11570	96	I.11045 I.11943	98	0.00155	1.99629 1.99627	31 30	50 82.5 81.7
30	1.115/0	20	1.1.1943		0.00057	1.99027	30	
	= (1)	96	-	97	. 0			97 96 95
31	1.11666	95	T.12040	80	0.87960	T.99625	29	6 9.7 9.6 9.
32	I.11761	96	¥.12138	97	0.87862	T.99624	28	
33	1.11857	05	1.12235	97	0.87765	T.99622	27	7 11.3 11.2 11. 8 12.9 12.8 12.
34	1.11952	95	I.12332	96	0.87668	1.99620	26	
35	1.12047	95	1.12428	97	0.87572	1.99618	25	9 14.6 14.4 14. 10 16.2 16.0 15.
36	Ī.12142	94	T.12525	96	0.87475	1.99617	24	32.3 32.0 31.
37	T.12236 T.12331	95	Ī.12621	96	0.87379	1.99615 T.00613	23	30 48.5 48.0 47.
30	I.12331 T.12425	94	I.12717 I.12813	96	0.87283	T.99613 T.99612	21	40 64.7 64.0 63.
39 40	1.12425 T.12519	94	1.12813 1.12909	96	0.87187	1.99012 1.99610	21	40 64.7 64.0 63. 50 80.8 80.0 79.
40	1.14519	-	1.12909		0.07091	1.99010	20	
		93		95	. 0(. (*		94 93 92
41	¥.12612	04	T.13004	05	0.86996	1.99608	19	6 9.4 9.3 9.
42	T.12706	03	T.13099	95	0.86901	T.99607	18	
43	Ī.12799 Ī.12892	03	T.13194	95	0.86806	T.99605	17	7 11.0 10.9 10. 8 12.5 12.4 12.
144		93	1.13289	95	0.86711	1.99603	16	9 14.1 14.0 13.
45	1.12985	93	T.13384	94	0.86616	T.99601	15	10 15.7 15.5 15.
46	1.13078	93	1.13478	95	0.86522	1.99600	14	ID 31.3 31.0 30.
47 48	T.13171	92	T.13573	54	0.86427	T.99598	13	30 47.0 46.5 46.
	1.13263	92	1.13667	94	0.86333	T.99596	12	40 62.7 62.0 61.
45	1.13355	9.2	1.13761	93	0.86239	1.99595	II	50 78.3 77.5 76.
50	I.13447		T.13854		0.86146	T.99593	10	55 1 10.5 1 11.5 1 10.
		92		94				
51	T.13539	QI	T.13948	93	0.86052	T.99591	9	91 90 2
52	T.13630	91	T.14041	93	0.85959	T.99589		0.0 0.0 1.0
53	I.13722	10	T.14134	93	0.85866	1.99588	7	7 10.6 10.5 0.2 B 12.1 12.0 0.1
54	T.13813	91	1.14227	93	0.85773	1.99586		
55	T.13904	90	T.14320	93	0.85680	1.99584	5	9 13.7 13.5 0.3
56	T.13994	91	I.14412	92	0.85588	1.99582	H.	10 15.2 15.0 0.3
57 58	1.14085	90	T.14504	93	0.85496	1.99581	3	30.3 30.0 0.7
8.8	I.14175	01	1.14597	93	0.85403	1.99579	8	30 45.5 45.0 1.0
59	T.14266	90	1.14688	92	0.85312	1.99577	1	40 60.7 60.0 1.3
00	1.14356		I.14780		0.85220	1.99575	0	50 75.8 75.0 1.7
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0	1.14356	85	1.14780	02	0.85220	1.99575	60	P2 91 80
1	T.14445	90	1.14872	91	0.85128	T.99574	59	6 9.3 9.1 9.0
3	T.14535 T.14624	80	T.14963 T.15054	91	0.85037	¥.99573	58	7 10.7 10.6 10.5 8 12.3 12.1 12.0
3	T.14024 T.14714	90	T.15054 T.15145	91	0.84855	T.99570 T.99568	57 56	8 12.3 12.1 12.0 9 13.8 13.7 13.5
	7.14803	89	T.15236	91	0.84764	1.99566	55	10 15.3 15.2 15.0
5	7.14891	88	T.15327	91	0.84673	1.99565	54	20 30.7 30.3 30.0
	1.14980	89	1.15417	100	0.84583	T.99563	53	30 46.0 45.5 45.0
7	T.15069	89	T.15508	91	0.84492	T.99561	52	40 61.3 60.7 60.0
0	T.15157	88	T.15508	90 90	0.84402	T.99559	51	40 61.3 60.7 60.0 50 76.7 75.8 75.0
10	T.15245		T.15688		0.84312	I.99557	50	
		88		89				88 88
II	1.15333	88	1.15777	00	0.84223	T.99556	49	6 5.9 8.8
12	T.15421	87	1.15867	80	0.84133	T.99554	48	7 10.4 10.3
13	T.15508	88	T.15956	90	0.84044	T.99552	47	
14	T.15596	87	7.16046	89	0.83954	1.99550	46	1 13.4 13.2
15	T.15683	87	1.16135	89	0.83865	¥.99548	45	10 14.8 14.7
16 17	T.15770 T.15857	87	T.16224 T.16312	88	0.83776 0.83688	T.99546 T.99545	44	20 29.7 29.3
18	I.15057 I.15944	87	T.16401	89	0.83599	T.99545 T.99543	43	30 44.5 44.0 40 59.3 58.7
10	I.16030	86	1.16489	88	0.83511	T.99543 T.99541	44	40 59.3 58.7 50 74.2 73.3
20	I.16116	86	T.16577	88	0.83423	T.99530	40	30 14.4 10/3.3
		87		88	1.04-0			0.2 1 84
21	7.16203		T.16665		0.83335	T.99537	39	87
22	1.16289	86	T.16753	88	0.83247	T.99535	38	6 8.7 8.6 7 10.2 10.0
23	T.16374	85	1.16841	88	0.83159	T.99533	37	7 10.2 10.0
24	T.16460	86	T.16928	87 88	0.83072	1.99532	36	9 13.1 12.9
25	T.16545	85	T.17016	87	0.82984	T.99530	35	10 14.5 14.3
26	T.16631	85	T.17103	87	0.82897	1.99528	34	281 29.0 28.7
27	1.16716	85	T.17190	87	0.82810	T.99526	33	30 43.5 43.0
28	T.16801	85	1.17277	86	0.82723	T.99524	32	40 58.0 57.3
20	Y.16886	84	1.17363	87	0.82637	T.99522	31	50 72.5 71.7
30	1.16970		T.17450		0.82550	T.99520	30	
	-	85		86				U5 B4
31	T.17055	84	T.17536	86	0.82464	1.99518	29 28	6 8.5 8.4
32 33	T.17139 T.17223	84	T.17622 T.17708	86	0.82378	T.99517 T.99515	20	7 9.9 9.8 8 11.3 11.2
33	T.17223	84	T.17794	86	0.82206	1.99513	26	
35	T.17391	84	T.17880	86	0.82120	1.99511	25	12.8 12.6
36	T.17474	83	T.17965	85 86	0.82035	T.99509	24	10 14.2 14.0 20 28.3 28.0
37	T.17558	84 83	T.17965 T.18051	85	0.81949	T.99507	23	
38	1.17641	83	Ī.18136	85	0.8:864	T.99505	22	30 42.5 42.0 40 56.7 56.0
39	T.17724 T.17807	83	T.18221	85	0.81779	T.99503	21	40 56.7 56.0 50 70.8 70.0
HO -	1.17807		¥.18306		0.81694	T.99501	20	30 1 7010 1 7010
	_	83		85				88 62
41	T.17890	83	¥.18391	84	0.81609	T.99499	19	6 8.3 8.2
42	I.17973	83	T.18475	85	0.81525	I.99497	18	
143	T.18055	82	T.18560	84	0.81440	T.99495	17	7 9.7 0.6 11.1 10.9
144	T.18137 T.18220	83	T.18644 T.18728	84	0.81356	T.99494	16	0 12.5 12.3
45	I.18220 I.18302	82	I.18728 I.18812	84	0.81272	T.99492 T.99490	15	10 13.8 13.7
47	1.18383	81	T.18896	84	0.81104	1.99490	14	27.7 27.3
48	T.18465	82	T.18070	83	0.81021	T.99486	12	30 41.5 41.0
140	1.18547	82	T.19063	84	0.80937	T.99484	11	40 55.3 54.7
50	1.18628	81	¥.19146	83	0.80854	1.99482	10	50 69.2 68.3
		81		83	-			
51	7.18709	81	T.19229	83	0.80771	7.99480	0	E 03 I3
52	T.18790	81	¥.19312		0.80688	1.99478	8	6 8.1 8.0 0.2
53	1.18871	81	T.19395	83 83	0.80605	¥.99476	7	7 9.5 9.3 0.2
54	¥.18952	81	Y.19478	83	0.80522	T.99474		
55	Y.19033	80	T.19561	83	0.80439	1.99472	5	9 12.2 12.0 0.3
56	T.19113	80	1.19643	82	0.80357	I.99470	34	10 13.5 13.3 0.3
57	T.19193	Ra	T.19725	82	0.80275	T.99468	3	20 27.0 26.7 0.7 30 40.5 40.0 1.0
58	T.19273	Ba	T.19807 T.19889	82	0.80193	T.99466 T.99464	1	
59	T.19353 T.19433	80	1.19889 1.19971	82	0.80029	I.99462		40 54.0 53.3 1.3 50 67.5 66.7 1.7
00	1.19433		1.199/1		0.00039	1.yydox	-	30 1 0/13 1 001/ 1 11/
	log cos	a	log cot	c. d.	log tan	log sin	1	p. p.
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0			log tan	c. d.	log cot	log cos			p. p.		
	¥.19433	80	T.19971	82	0.80029	T.99462	60		82	-	80
1	T.19513		T.20053	81	0.79947	¥.99460	59		8.2	8.1	8.0
2	¥.19592	79 80	T.20134	82	0.79866	1.99458	58		9.6	9.5	9.3
	T.19672	70	T.20216	81	0.79784	T.99456	57				10.7
H	T.19751 T.19830	79	T.20297 T.20378	81	0.79703	T.99454 T.99452	56 55			12.2	13.3
S	T.19030 T.19909	79	T.20376	81	0.79541	T.99-50	55			27.0	26.7
	T.19988	79	T.20540	81	0.79460	T.99448	53			10.5	40.0
7 8	¥.20067	79 78	1.20621	81 60	0.79379	T.99446	52	40 5		54.0	53.3
0	¥.20145	78	1.20701	81	0.79299	T.99444	51	50 6	8.3 1 (57.5	66.7
10	¥.20223	79	1.20782	Eo	0.79218	T.99442	50		79	1 7	
II	1.20302	78	T.20862		0.79138	T.99440	49	6	7.9	7.	
12	T.20380	78	¥.20942	80 80	0.79058	T.99438	48		9.2	9.	
13	1.20458	77	1.21022	80	0.78978	T.99436	47	78	10.5	10.	
14	T.20535	78	T.21102	80	0.78898	T.99434	46	9	11.9	11.	
15	T.20613 T.20601	78	T.21182 T.21261	79 80	0.78818	T.99432 T.99429	45 44	10	13.2	13.	0
	1.20091 1.20768	77	I.21201 T.21341		0.78659	1.99429 T.99427	44	20	20.3	30.	
17 18	T.20845	77	Ī.21420	79	0.78580	I.99427	43	30	39.5	52.	
19	T 20022	77	T.21499	79	0.78501	1.99423	41	50	65.8	65.	
20	T.20999	77	T.21578	79	0.78422	T.99421	40	00			
21	1.21076	77	¥.21657	79	0.78343	T.99419	39		77	1 7	
21	1.21070 1.21153	77	T.21736	79	0.78264	I.99419 I.99417	38	6	7.7	7.	0
23	Ĩ.21220	76	1.21814	78	0.78186	T.00415	37	78	9.0 10.3	10.	9
24	1.21306	77	T.21893	79 78	0.78107	T.99413	36	9	11.6	10.	
25	T.21382	76 76	T.21971	78 78	0.78029	1.99411	35	10	12.8	12.	
26	T.21458	76	T.22049	78	0.77951	Ī.99409	34	20	25.7	25.	
27	Ī.21534	76	1.22127	78	0.77873	I.99407	33	30	38.5	38.	
28	1.21610	75	1.22205	78	0.77795	Î.99404	32	412	51.3	50.	
29	1.21685	76	T.22283	78	0.77717	T.99402	31	50	64.2	63.	3
30	1.21761	75	1.22361	77	0.77639	T.99400	30				
	1.21836		¥.22438		0.77562	T.99398	29		75	1 74	
31 32	I.21030	76	T.22516	78	0.77484	I.99396	29	6	7.5	7.	4
33	1.21987	75	1.22593	77	0.77407	T.99394	27	78			
34	1.22062	75	1.22670	77	0.77330	1.99392	26		10.0	9.	
35	1.22137	75	1.22747	77	0.77253	T.99390	25	5	12.5	12.	
36	1.22211	75	¥.22824	77	0.77176	T.99388	24	20	25.0	24.	
37	T.22286	75	T.22901	76	0.77099	T.99385	23	30	37.5	37.	
	T.22361 T.22435	74	T.22977 T.23054	77	0.77023	T.99383 T.99381	22	40	50.0	49.	3
40	T.22509	74	T.23054	76	0.76870	T.99379	20	50	62.5	61.	7
		74	1 m m	76					73	1 73	2
41	1.22583	74	¥.23206	77	0.76794	I.99377	19	6			
42	1.22657	74	Ĩ.23283	76	0.76717	T.99375	18		7.3	7.	4
43	1.22731 1.22805	74	T.23359	76	0.76641 0.76565	T.99372	17 16	7 11	9.7	9.	
## 45	1.22805	73	T.23435 T.23510	75	0.70505	T.99370 T.99368	10	9	11.0	10.	8
45	1.22952	74	T.23586	76	0.76411	T.99366	14	10	12.2	12.	
47	T.23025	73	T.23661	75	0.76339	T.99364	13	20	24.3	24.	
48	T.23098	73	1.23737	76	0.76263	T.99362	12	30	36.5	36.	0
40	1.23171	73 73	T.23812	75	0.76188	T.99359	11	40 50	48.7	60.	
50	T.23244	73	T.23887		0.76113	T.99357	10	50	00.0	, 00.	
51	T.23317		T.23962	75	0.76038	¥.99355	0		71	8 1	2
52	T.23390	73	I.24037	75	0.75963	T.99353	8	6 1	7.1	0.3	0.2
53	1.23462	72 1	.24112	75	0.75888	T.99351	7			0.4	0.2
54	T.23535	73	1.24186	74	0.75814	T.99348				0.4	0.3
55	1.23607	72	T.24261	74	0.75739	T.99346	5	9 10		0.5	0.3
56	1.23679	73	T.24335 T.24410	75	0.75665	T.99344			3.7	0.5	0.3
57	1.23752 1.23823	71	1.24410 1.24484	74	0.75590	¥.99342 ¥.99340	3		3.7	1.0	0.7
50	T.23895	72	T.24558	74	0.75442	T.99340	I			2.0	1.3
59 60	1.23967	72	T.24632	74	0.75368	I.99335	D			2.5	1.7
-	1000 0000		lawart		lambar	lam ala	,				
	log cos	đ	log cot	c. d.	log tan	log sin			p. p.		

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'	log sin	a	log tan	ç. d.	log cot	log cos			p. p.	
1 2 3 4	Y.23967 I.24039 T.24110 Y.24181 Y.24253	72 71 71 73 71	T.24632 T.24706 T.24779 T.24853 T.24926	74 73 74 73 74	0.75368 0.75294 0.75221 0.75147 0.75074	T.99335 T.99333 T.99331 T.99328 T.99326	60 59 58 57 56	10 7 8	74 7.4 8.6 9.9 11.1	78 7.3 8.5 9.7 11.0
7 8 0 10	Y.24324 Y.24395 Y.24466 Y.24536 Y.24607 Y.24677	71 71 70 71 70 71	T.25000 T.25073 T.25146 T.25219 T.25292 T.25365	73 73 73 73 73 73 73	0.75000 0.74927 0.74854 0.74781 0.74708 0.74635	Y.99324 Y.99322 Y.99319 Y.99317 Y.99315 Y.99313	55 54 53 52 51 50	10 20 30 40 50	12.3 24.7 37.0 49.3 61.7	12.2 24.3 36.5 48.7 50.8
11 12 13 14 15 16 17 18 19	Y.24748 I.24818 Y.24888 Y.24958 Y.25028 Y.25098 Y.25108 Y.25168 Y.25307 Y.25307 Y.25376	70 70 70 70 70 70 69 70 69	T.25437 T.25510 T.25582 T.25655 T.25727 T.25799 T.25871 T.25943 T.25043 T.26015 T.26086	72 73 72 72 72 72 72 72 72 72 72	0.74563 0.74490 0.74418 0.74345 0.74273 0.74201 0.74201 0.74057 0.73985 0.73914	T.99310 T.99308 T.99306 T.99304 T.99301 T.99299 T.99297 T.99294 T.99292 T.99290	49 48 47 45 44 41 42 41	6 7 80 80 80 80	72 7.2 8.4 9.6 10.8 12.0 24.0 36.0 48.0 60.0	71 7.1 8.3 9.5 10.7 11.8 23.7 35.5 47.3 59.2
21 22 23 24 25 16 27 27 28 27 28 29 30	T.25445 T.25514 T.25583 T.25652 T.25721 T.25790 T.25858 T.25927 T.25995 T.26063	69 69 69 69 69 69 69 69 69 69 69 69 69 6	Y.26158 Y.26229 J.26301 Y.26372 Y.26443 J.26514 Y.26555 J.26655 Y.26726 Y.26797	72 71 72 71 71 71 71 70 71 71	0.73842 0.73771 0.73699 0.73628 0.73557 0.73486 0.73415 0.73415 0.73274 0.73203	1.99288 1.99285 1.99283 1.99281 1.99278 1.99276 1.99274 1.99271 1.99269 1.99267	10 38 37 36 35 34 33 32 31 30	5 7 8 50 20 30 40 50	70 7.0 8.2 9.3 10.5 11.7 23.3 35.0 46.7 58.3	6.9 8.1 9.2 10.4 11.5 23.0 34.5 46.0 57.5
31 32 33 34 35 36 37 38 39	I.26131 I.26199 I.26267 I.26335 I.26403 I.26403 I.26470 I.26538 I.26605 I.26672 I.26739	68 68 68 67 67 67 67	1.26867 1.20937 1.27008 1.27078 1.27148 1.27218 1.27288 1.27357 1.27427 1.27427 1.27496	70 71 70 70 70 70 69 70 69	0.73133 0.7306; 0.72992 0.72922 0.72852 0.72782 0.72712 0.72643 0.72573 0.72504	T.99264 T.99262 T.99260 T.99257 T.99255 T.99255 T.99250 T.99248 T.99245 T.99243	20 28 27 25 24 23 22 21 20	6 7 8 10 10 30 30 30 30	68 6.8 7.9 9.1 10.2 11.3 22.7 34.0 45.3 56.7	6.7 . 7.8 8.9 10.1 11.2 22.3 33.5 44.7 55.8
41 42 43 44 45 46 47 47 49 50	1.26806 1.26873 1.26940 1.27007 1.27073 1.27140 1.27206 1.27273 1.27339 1.27405	67 67 67 66 67 66 67 66 66	I.27566 I.27635 I.27704 I.27773 I.27842 I.27980 I.28049 I.28049 I.28117 I.28186	70 69 69 69 69 69 69 69 69 68 69 68 69	0.72434 0.72365 0.72296 0.72227 0.72158 0.72089 0.72020 0.71951 0.71883 0.71814	Y.99241 Y.99238 Y.99236 Y.99233 Y.99231 Y.99229 Y.99220 Y.99224 Y.99221 Y.992219	19 18 17 16 15 14 13 12 11 10	6 7 10 30 40 50	6.6 7.7 8.8 9.9 11.0 22.0 33.0 44.0 55.0	B5 6.5 7.6 8.7 9.8 10.8 21.7 32.5 43.3 54.2
51 52 53 54 55 56 57 59	T.27471 T.27537 T.27602 T.27668 T.27734 T.27799 T.27864 T.27930 T.27995 T.28060	66 65 66 65 65 65 65 65 65	Y.28254 Y.28323 Y.28323 Y.28459 Y.28527 Y.28595 Y.28662 Y.28730 J.28798 J.28865	68 69 68 68 68 68 67 88 67 67 67	0.71746 0.71677 0.71609 0.71541 0.71473 0.71405 0.71338 0.71270 0.71202 0.71135	Y.99217 Y.99214 Y.99212 Y.99209 Y.99207 Y.99204 Y.99202 Y.99200 I.99197 Y.99195	000 1410 15 14 15 15 1 4	6 7 10 20 30 40 50	0.3 0.4 0.5 0.5 1.0 1.5 2.0 2.5	2 0.2 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.7 1.0 1.3 1.7
	log cos	a	log cot	c. d.	log tan	log sin	,		p. p.	

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,	log sin	d	log tan	c. d.	log cot	log cos			p. p.	
	1.28060		1.28865		0.81145	Tonior	60		8.8	87
0	1.28000 1.28125	65	1.28805 T.28933	68	0.71135	T.99195 T.90192	00 59	б	6.8	6.7
I	1.20125 1.28100	65		67	0.71007	T.99192	59		7.9	7.8
	1.28190 T.28254	64	T.29000 T.20067	67		T.99190 T.99187		7		8.9
8	1.28254 1.28319	65		67	0.70933 0.70866	1.99187 T.99185	57 56	9	9.1 10.2	10.1
1	1.28319 1.28384	65	T.29134 T.29201	67	0.70799	T.99182		10	11.3	11.2
10	T.28448	64	I.29201 I.29268	67		1.99182	55 54	10	22.7	22.3
	1.20440	64	T.29335	67	0.70732	1.99180	54	380	34.0	33.5
7 8	1.28577	65	1.29335 1.29402	67	0.70598	I.99177	53	30		
	I.2864I	64	T.29468	66	0.70532	T.99172	51	50	45-3	44.7 55.8
10	T.28705	64	1.29400	67	0.70465	I.99170	50	20	30.7	1 33.0
10	1.20703	64	1.=9333	66	0.70403	1.99.70	30		66	85
11	1.28769		T.20601		0.70399	T.99167	40	6	6.6	6.5
12	T.28833	64	T.29668	67	0.70332	T.99165	48			7.6
13	T. 28896	63	T. 20734	66	0.70266	T.99162	47	78	7.7	7.6
14	T.28960	64	T.29734 T.29800	66	0.70200	1.99160	46	0	9.9	9.8
15	T.20024	64	1.29866	66	0.70134	T.99157	45	10	11.0	10.8
16	T.29087	63	T.29932	66	0.70068	T.99155	44	20	22.0	21.7
17	T.29150	63	T.29998	66	0.70002	T.99152	43	30	33.0	32.5
18	1.29214	64	T.30064	66	0.69936	1.99150	42	40	44.0	43.3
10	1.29277	63	1.30130	66	0.69870	Ī.99147	41	50	55.0	54.2
10	T.29340	63	T.30195	65	0.69805	1.99145	40	30	0010	
		63		66					64	1 63
21	1.29403	63	T.30261	64	0.69739	T.99142	39	б	6.4	6.3
22	T.29466	03	1.30326	65	0.69674	Ī.99140	38			
23	T.29529	63	Ī.30391	65	0.69609	1.99137	37	28	7.5	7-4 8.4
24	1.29591		T.30457	66	0.69543	1.99135	36	0	9.6	9.5
25	T.29654	63	T.30522	65	C.69478	1.99132	35	10	10.7	10.5
26	1.29716	62 63	T.30587	65	c.69413	1.99130	34	20	21.3	21.0
27	Ī.29779	03 62	T.30652	65	0.69348	1.99127	33	30	32.0	31.5
18	1.29841	02 62	T.30717	65	0.69283	T.99124	33	30	42.7	42.0
29	I.29903		T.30782	65	0.69218	1.99122	31	50	53.3	52.5
30	1.29966	63	1.30846	64	0.69154	T.99119	30	20	23.3	. 3-3
		62		65					82	61
31	T.30028	62	1.30911	64	0.69089	T.99117	29	6	6.2	6.1
32	T.30090	02 61	1.30975		0.69025	T.99114	28			7.1
33	T.30151	62	1.31040	65 64	0.68960	T.99112	27	78	7.2 8.3	7.1 8.1
34	1.30213	62	T.31104	64	0.68896	1.99109	26	0	9.3	0.1
35	1.30275	61	1.31168	65	0.68832	T.99106	25	10	10.3	10.2
36	T.30336	62	T.31233	05 64	0.68767	T.99104	24	20	20.7	20.3
37	T.30398	61	1.31297	64	0.68703	1.99101	23	30	31.0	30.5
38	T.30459	62	T.31361	64	0.68639	1.99099	22	40	41.3	40.7
39	I.30521	61	1.31425	64	0.68575	I.99096	21	50	51.7	50.8
40	1.30582		T.31489		0.68511	1.99093	20	30		
	-	61	-	63	. 10 0				60	59
41	T.30643	61	T.31552	64	0.68448	T.99091	19	6	6.0	5.9
42	I.30704	61	T.31616	63	0.68384	1.99088	18			6.0
43	1.30765	61	T.31679	64	0.68321	1.99086	17	78	7.0 8.0	
44	T.30826	61	I.31743	63	0.68257	1.99083	16	9	0.0	7.9 8.9
45	T.30887	60	1.31806	64	0.68194	1.99080	15	10	10.0	0.8
46	T.30947	61	T.31870	63	0.68130	¥.99078	14	20	20.0	10.7
47	T.31008	60	1.31933	63	0.68067	1.99975	13	30	30.0	29.5
48	1.31068	61	T.31996	63	0.68004	I.99072	12	40	40.0	39.3
89	T.31129	60	¥.32059	63	0.67941	I.99070	11	50	50.0	49.2
30	T.31189		Ī.32122		0.67878	1.99067	10	14		4.0.00
	-	61		63	- (-0	8			3.1	2
51	T.31250	60	T.32185	63	0.67815	T.99064	8	6	0.3	0.2
52	1.31310	fin	T.32248	63	0.67752	T.99062			0.3	0.2
53	I.31370	60	1.32311	62	0.67689	T.99059	7	28		
54	1.31430	60	T.32373	6,3	0.67627	T.99056		0	0.4	0.3
55	I.31490	59	T.32436	62	0.07504	T.99054	5	10	0.5	0.3
56	T.31549	60	T.32498 T.32561	63	0.07503	T.99051 T.99048	14	30	1.0	0.3
57 58	T.31609 T.31669	60	1.32501	62	0.07439	T.99048	3	30	1.5	1.0
	I.31009 I.31728	59	1.32023 T.32685	62	0.07377	1.99040 T.99043	I	30	2.0	1.3
59	1.31728 T.31788	60	I.32085 T.32747	63	0.07315	T.99043 T.99040	10	50	2.5	1.3
-end										
	log cos	а	log cot	c. d.	log tan	log sin	,		p. p.	

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'	log sin	d	log tan	c. d.	log cot	log cos			p. p.	
0	T.31788	50	¥.32747	63	0.67253	T.99040	60		63	62
I	T.31847	59	¥.32810	.62	0.67190	1.99038	89	ő	6.3	6.3
2	T.31907 T.31966	59	I.32872 I.32933	<u>É1</u>	0.67128	T.99035 T.99032	58 57	# 90	7.4 8.4	7.2 8.3
1	T.32025	59	T.32935	62	0.67005	1.99030	56	0	9.5	9.3
	1.32084	59 59	¥.33057	62 62	0.66943	T.99027	55	10	10.5	10.3
5	1.32143	59	1.33119	61	0.66881	T.99024	54	30	21.0	20.7
78	T.32202	59	T.33180	62	0.66820	T.99022	53	30	31.5	31.9
o D	T.32261 T.32319	58	Y.33242 Y.33303	61	0.00758	T.99019 T.99016	52 51	40	42.0	41.3
10	1.32378	59	T.33365	62	0.66635	T.99013	50	30	3	3
		59		61					61	60
11	1.32437	58	T.33426	61	0.66574	11000.1	49	ō	6.1	6.0
12	T.32495	58	1.33487	61	0.66513	T.99008	48	2	7.1 8.1	7.0 8.0
13	T.32553 T.32612	59	T.33548	61	0.66452	T.99005 T.99002	47 46			
14	1.32670	58	I.33609 I.33670	61	0.66330	T.99002	40	0	9.2 10.2	9.0
16	¥.32728	58	1.33731	61	0.66269	T.98997	44	20	20.3	20.0
17	1.32786	58 58	1.33792	61 61	0.66208	1.98994	43	30	30.5	30.0
18	Y.32844	58	1.33853	60	0.66147	1.98991	42	40	40.7	40.0
19	I.32902	58	T.33913	61	0.66087	T.98989 T.98986	41	50	50.8	50.0
in the	¥.32960	58	T.33974	50	0.00020	1.90900	40			a la
21	T.33018		T.34034		0.65966	T.08083	39			0
22	T.33075	57	T.34095	61	0.65905	T.98980	38			5.9
23	T.33133	58 57	T.34155	60 60	0.65845	T.98978	37		8 2	.9
84	T.33190	57	T.34215	61	0.65785	1.98975	36		9 8	3.9
25 26	I.33248	57	T.34276	60	0.65724	T.98972 T.98969	35			9.8
27	ī.33305 Ī.33362	57	T.34336 T.34396	60	0.65604	1.98967	34 33			0.7
BE	T.33420	58	T.34456	60 60	0.65544	1.98964	32).5).3
29	T.33477	57 57	1.34516	60	0.65484	¥.98961	31).2
30	T.33534		1.34576		0.65424	T.98958	30			
		57		59		T .C.			50	57
31 32	T.33591 T.33647	56	T.34635 T.34695	60	0.65365	T.98955 T.98953	28	ñ	5.8	5.7 :
32	T.33047	57	T.34095	60	0.65245	T.98950	27	78	6.8	6.7
34	1.33761	57	T.34814	59 60	0.65186	T.98947	26	8	7.7 8.7	7.6 8.6
35	T.33818	57 56	¥ 34874	59	0.65126	1.08044	25	10	9.7	9.5
36	T.33874	57	T.34933	59	0.65067	T.98941 T.98938	24	20	19.3	19.0
37	T.33931 T.33987	56	T.34992 T.35051	59	0.65008	1.98938 T.98936	23 22	30	29.0	28.5
39	T.34043	56	1.35111	60	0.64889	T.98933	21	40	38.7	38.0
10	T.34100	57	T.35170	59	0.64830	T.98930	20	EO	48.3	47.5
		56		89					56	55
41	1.34156	56	T.35229	59	0.64771	1.98927	19	8	5.6	5.5
42	T.34212	56	¥.35288	50	0.64712	1.98924 1.98921	18		6.5	6.4
43	T.34268 T.34324	56	T.35347 T.35405	58	0.64653 0.64595	T.98919	17 16	2	7.5	7.3
45	1.34380	56 56	T.35464	80	0.64536	T.98916	15	9	8.4	8.3
46	1.34436	50	T.35523	89 58	0.64477	T.98913	14	10 20	9-3 18.7	9.2 18.3
47 #图	I.34491	56	1.35581	59	0.64419	T.98910 T.98907	13	30	28.0	27.5
50	T.34547 T.34602	55	T.35640 T.35698	58	0.64360	1.98907 1.98904	12	NO	37.3	36.7
8M 50	I.34658	56	I.35090 I.35757	59	0.64302	1.98904	100	80	46.7	45.8
		55		58						
51	¥.34713	56	7.35815	58	0.64185	1.98898	9		3	2
52	T.34769	50 55	T.35873	58	0.64127	1.98896	8	ő	0.3	0.2
53	¥.34824	55	T.35931	58	0.64069	T.98893 T.98890	7	78	0.4	0.2
54 55	T.34879 T.34934	55	T.35989 T.36047	58	0.64011 0.63953	1.98890	5		0.4	0.3
56	T.34989	55	T.36105	58	0.63895	T.98884	J J	10	0.5	0.3
57	T.35044	55	T.36163	58 58	0.63837	1.98881	3	20	1.0	0.7
58	T.35099	55	T.36221	58	0.63779	1.98878	2	30	1.5	1.0
59	T.35154 T.35209	55	I.36279 I.36336	57	0.63721	T.98875 T.98872	I	40 50	2.0	1.3
ANU	1.33209		1.30330		0.03004	1.900/2		50	1 4.3	
	100 000	d	logost		logitor	log ala	,			
	log cos	a	log cot	c. d.	log tan	log sin			p. p.	
			1.							

13°

0				c. d.	log cot	'log cos			p. p.	
0	1000									
	T.35209	54	T.36336	58	0.63664	1.98872	60		68	57
	T.35263	55	T.36394	100	0.63606	1.98869	59	6	5.8	5.7
2	T.35318	55	T.36452	57	0.63548	T.98867	58	2	6.8	6.7
B	T.35373	54	T.36509	57	0.63491	1.98864	57	8	7.7 8.7	7.6
H	T.35427	54	1.36566	58	0.63434	T.98861	56	8		
B	1.35481	55	T.36624	57	0.63376	T.98858	55	10	6.2	9.5
6	T.35536	54	1.36681	57	0.63319	T.98855	54	20	13.3	1 19.0
78	T.35590	54	1.36738	57	0.63262	1.98852	53	30	29.0	28.5
	T.35644	54	1.36795	57	0.63205	1.98849	52	40	38.7	30 2
10	T.35698	54	T.36852	57	0.63148	T.98846	51	50	48.3	47.5
10	T.35752		T.36909		0.63091	1.98843	50			1
		54		57					56	55
11	T.35806	54	T.36966	57	0.63034	1.98840	40	6	5.6	5.5
12	1.35860	54	T.37023	57	0.62977	1.98837	48	7	6.5	6.4
13	1.35914	54	1.37080	57	0.62920	1.98834	47	78	7.5	7.3
14	T.35968	54	I.37137	56	0.62863	T.98831	46	9	7.5 8.4	7.3 8.3
15	T.36022	53	1.37193	57	0.62807	1.98828	45	10	9.3	9.2
16	1.36075	54	T.37250	56	0.62750	1.98825	44	20	18.7	18.3
17	T.36129	53	1.37306	57	0.62694	1.98822	43	30	28.0	27.5
18	1.36182	54	1.37363	56	0.62637	1.98819	42	40	37.3	36.7
19	T.36236	53	1.37419	57	0.62581	1.98816	41	50	46.7	45.8
20	¥.36289	_	1.37476		0.62524	1.98813	40			
		53		56					1	54
21	T.36342	53	T.37532	56	0.62468	1.98810	39			5-4
22	T.36395	53	T.37588	56	0.62412	T.98807	38			6.3
23	T.36449	53	1.37644	56	0.62356	T.98804	37		81	7.2
24	1.36502	53	I.37700	56	0.62300	1.98801	36		9 1	8.1
25	1.36555	53	T.37756	56	0.62244	1.98798	35			9.0
26	T.36608	52	1.37812	56	0.62188	1.98795	34		20 1	8.0
27	T.36660	53	T.37868	56	0.62132	1.98792	33			7.0
1	I.36713	53	1.37924	56	0.62076	1.98789	32			6.0
30	T.36766		T.37980	55	0.62020	T.98786	31			5.0
30	1.36819	53	1.38035		0.61965	1.98783	30			
		52		56					53	1 52
31	T.36871		1.38091		0.61909	T.98780	20	6		5.2
32	T.36924	53	T.38147	56	0.61853	T.98777	28		5.3	6.1
33	1.36976	52	T.38202	55	0.61798	I.98774	27	78	7.1	6.9
34	1.37028	52	1.38257	55	0.61743	1.98771	26	9	8.0	7.8
35	1.37081	53	T. 38313	56	0.61743 0.61687	1.98768	25	10	5.5	8.7
36	1.37133	52	1.38368	55	0.61632	T.98765	24	20	17.7	17.3
37	T.37185	52	T.38423	55	0.61577	1.98762	23	30	26.5	26.0
38	1.37237	52	T.38479	56	0.61521	1.98759	22	40	35.3	34.7
39	T.37289	52	T.38534	55	0.61466	1.98756	21			43.3
40	I.37341	52	1.38589	55	0.61411	1.98753	20	50	44.2	43.3
		52		55						
41	T.37393		1.38644		0.61356	1.98750	10		51	4
42	I.37445	52	T.38699	55	0.61301	1.08746	18	6	5.1	0.4
43	T.37497	52	1.38754	55	0.61246	T.98743	17	7	6.0	0.5
44	T.37549	52	T.38808	54	0.61192	T.98740	16	8	6.8	0.5
45	1.37600	51	T. 38863	55	0.61137	I.98737	15	9	7.7	0.6
46	1.37652	52	1.38918	55	0.61082	1.98734	14	10		0.7
47	T.37703	51	¥.38972	54	0.61028	T.98731	13	20	17.0	1.3
48	T.37755	52	1.39027	55	0.60973	1.98728	12	30	25.5	2.0
140	T.37806	51	1.39082	55	0.60918	T.98725	11	40	34.0	2.7
50	1.37858	52	T.39136	54	0.65864	1.98722	10	50	42.5	3.3
		51		54						
51	T.37909		T.39190		0.60810	1.08710	15		3	2
52	I.37960	51	T.39245	55	0.60755	1.98715	8	6	0.3	0.2
53	1.38011	51	T.39299	54	0.60701	1.98712	7	7	0.4	0.2
53	1.38062	SI	T.39353	54	0.60647	1.08700	6	8	0.4	0.3
55	1.38113	51	T.39407	54	0.60593	T.98706	5	9	0.5	0.3
56	T.38164	51	T.39461	54	0.60539	1.98703	4	10	0.5	0.3
57	T.38215	51	T.39515	54	0.60485	1.98700	3	20	1.0	0.7
58	T.38266	51	T.39569	54	0.60431	T.98697	2	30	1.5	1.0
89	T.38317	51	1.39623	34	0.60377	1.98694	1	40	2.0	1.3
60	I.38368	51	1.39677	54	0.60323	1.98690	0	50	2.5	1 1.7
	log cos		log cot	c. d.	log tan	log sin			p. p.	

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14°

1	log sin	ы	log tan	c. d.	10g co:	log cos	đ		p. p.
	1.38368	50	Y.3967,	54	0.60323	1.98690	3	60	
2	T.38418 T.38469	51	T.39731	54	0.60209	1.98687 1.98684	3	59 58	54 53
3	1.38519	50	T.39785 T.39838	53	0.60162	1.98681	3		
1	1.38570	51	1.39892	54	0.60102	1.98678	3	57 56	
3	1.38620	50	T.39945	53	0.60055	1.98675	3	55	7 6.3 6.2 8 7.2 7.1
-	1.38670	50	T.39999	54	0.60001	I.98671	4	55	8 7.2 7.1 9 8.1 8.0
	I.38721	51	T.40052	53	0.59948	1.98668	8	53	10 9.0 8.8
28	I.38771	50	T.40106	54	0.59894	T.98665		53	18.0 17.7
0	1.38821	50	T.40159	53	0.59841	1.98662	3	51	30 27.0 26.5
10	T.38871	50	T.40212	53	0.59788	T.98659	3	54	40 36.0 35.3
-		50		54	0.39700			24	50 45.0 44.2
11	1.38921		T.40266	24	0 50834	1.98656		40	5-1 45 1 44
12	T.38971	50	T.40319	53	0.59734 0.59681	1.98050 1.98652	M	49 48	
13	T.30021	50	T.40372	53	0.59628	T.08640	3	40	
14	T.39071	50	T.40425	53	0.59575	1.98646	3	46	52 51
15	1.39121	50	T.40478	53	0.59522	T.08643	3	45	6 5.2 5.1
16	T.39170	160	T.40531	53	0.59469	T.98640	3	44	
	T.39220	50	T.40584	53	0.59416	1.98636	4	43	7 6.1 6.0 6.9 6.8
17	T.39270	50	T.40636	52	0.59364	T.98633	3	42	
19	T.39319	49	1.40689	53	0.59311	T.98630	3	41	₽ 7.8 7.7 ₩ 8.7 8.5
20	T.39369	50	T.40742	53	0.59258	I.98627	3	40	20 17.3 17.0
		49		53			A		30 26.0 25.5
21	T.39418		T.40795		0.59205	1.98623		39	40 34.7 34.0
22	T.39467	49	T.40847	52	0.59153	T.98620	в	38	50 43.3 42.5
23	T.39517	50	T.40900	53	0.59100	1.98617	3	37	
24	T.39566	49	T.40952	52	0.59048	1.98614	8	36	
25	T.39615	49	T.41005	53	0.58995	T.98610	A	35	
26	T.39664	49	T.41057	52	0.58943	1.98607		34	50 49
37	I.39713	49	T.41109	54	0.58891	1.98604	3	33	fi 5.0 4.9
28	I.39762	49	T.41161	53	0.58839	¥.98601	4	32	7 5.8 5.7
20	1.39811	49	T.41214	52	0.58786	T.98597	8	31	
30	T.39860		T.41266	30	0.58734	1.98594		10	9 7.5 7.4 10 8.3 8.2
		49		52			8		10 8.3 8.2
31	T.39909	10	1.41318	52	0.58682	¥.98591	3	305	16.7 16.3
32	T.39958	48	Y.41370	52	0.58630	1.98588	3	28	30 25.0 24.5 40 33.3 32.7
33	T.40006	49	T.41422	52	0.58578	T.98584	3	27	50 41.7 40.8
34	T.40055	48	1.41474	52	0.58526	1.98581	3	26	50 41.7 40.0
35	T.40103	10	T.41526	52	0.58474	1.98578	4	25	
36	T.40152	48	¥.41578	51	0.58422	T.98574	3	24	
37	T.40200	40	1.41629	52	0.58371	T.98571	3	23	48 47
	T.40249	a8	T.41681	52	0.58319	1.98568	3	22	
39	I.40297	49	T.41733 T.41784	51	0.58267 0.58216	1.98565 1.98561	4	20	
411	T.40346	.0	1.41704	-	0.50210	1.90501		20	7 5.6 5.5 H 6.4 6.3
		48		52			3		
41	T.40394	48	T.41836	51	0.58164	1.98558	3	19	10 7.2 7.1 10 8.0 7.8
42	1.40442	48	1.41887	52	0.58113	T.98555	4	18	10 16.0 15.7
43	1.40490 7.40528	48	T.41939	51	0.58061	T.98551 T.98548	3	17 16	30 24.0 23.5
44	T.40538	48	T.41990	SI		1.98548 1.98545	3	10	40 32.0 31.3
45 46	T.40586 T.40634	48	T.42041 T.42093	52	0.57959 0.57907	1.98545 Y.98541	14	15	50 40.0 39.2
40	T.40682	48	T.42093	51	0.57907	T.98538	3	14	
18	I.40730	118	I.42144 I.42195	51	0.57805	1.98535	3	12	
40	1.40778	48	1.42246	51	0.57754	T.98531	14	11	
50	1.40825	47	1.42297	51	0.57703	T.98528	3	10	14 3
		18		51	0.011-0		3		6 0.4 0.3
51	T.40873	-	T.42348	-	0.57652	¥.98525		0	7 0.5 0.4 8 0.5 0.4
52	1.40073	48	T.42340	51	0.57652	1.98521	4	9	8 0.5 0.4
53	T.40968	47	T.42399	51	0.47550	1.98518	3		9 0.6 0.5
54	1.41016	48	T.42501	51	0.57499	1.08515	3	7	10 0.7 0.5
55	1.41063	47	T.42552	51	0.57448	T.98511	4	5	1.3 1.0
56	T.41111	48	T.42603	51	0.57397	1.98508		4	30 2.0 1.5
57	T.41158	47	7.42653	50	0.57347	T.98505	3	3	40 2.7 2.0
58	T.41205	47	1.42704	51	0.57296	T.98501	4	2	50 3.3 2.5
59	T.41252	48	1.42755	SI	0.57245	1.98498	3	1	
60	1.41300	40	1.42805	50	0.57195	7.98494	4	ō	
	log cos	a	log cot	c. d.	log tan	log sin	a	,	p. p.

15°

1	log sin	d	log tan	c. d.	log cot	log cos	а		p. p.
0	T.41300		¥.42805		0.57195	T.98494		50	
i l		47	T.42856	51		T.08401	3	59	
2	T.41347 T.41394	47	1.42050	50	0.57144 0.57094	T.98488	3	58	51 50
3	I.4144I	47	T.42957	51	0.57043	T.98484	4	57	6 5.1 5.0
3	T.41488	47	1.42957	50	0.56993	T.98481	3	56	
	T.41535	47	T.43057	50	0.56943	T.98477		55	7 6.0 5.8 6.8 6.7
5	Ĩ.41582	47	T.43108	51	0.56892	T.08474	3	54	9 7.7 7.5
	I.41628	46	T.43158	50	0.56842	T.98471		53	10 8.5 8.3
7	I.41675	47	Ī.43208	50	0.56792	1.98467	4	52	10 17.0 16.7
9	T.41722	47	T.43258	50	0.56742	T.98464	3	51	30 25.5 25.0
10	1.41768	46	T.43308	50	0.56692	7.98460	14	50	40 34.0 33.3
-		47		50			з		50 42.5 41.7
II	T.41815		T.43358		0.56642	7.98457	-	40	
12	T.41861	26	T.43408	50	0.56592	¥.98453	14	48	
13	T.41908	47	T.43458	50	0.56542	T.98450	3	47	
14	T.41954	MŰ	T.43508	50	0.56492	1.98447	3	46	49 48
15	T.42001	47	1.43558	50	0.56442	1.98443	4	45	6 4.9 4.8
16	T.42047	46	1.43607	49	0.56393	T.98440	3	44	7 5.7 5.6
17	T.42093	46	I.43657	50	0.56343	1.08436	A	43	5 6.5 6.4
18	T.42140	47 #6	I.43707	50	0.56293	T.98433	3	42	0 7.4 7.2
19	T.42186		1.43756	49	0.56244	1.98429	4	41	10 8.2 8.0
20	T.42232	46	T.43806	50	0.56194	1.98426	3	40	20 16.3 16.0
		46		49			A		30 24.5 24.0
21	1.42278	46	1.43855	50	0.56145	1.98422		39	40 32.7 32.0 50 40.8 40.0
22	1.42324	40	1.43905	50	0.56095	1.98419	3	38	50 40.8 40.0
23	1.42370	26	¥.43954	49 50	0.56046	Ĩ.98415	4	37	
24	T.42416	45	1.44004	49	0.55996	1.98412	3	36	
25	T.42461	45	1.44053	49	0.55947	1.98409	4	35	40
26	1.42507	40	T.44102	49	0.55898	1.98405	3	34	47 46
27	T.42553	46	1.44151	50	0.55849	7.98402	3	33	6 4.7 0.5
28	T.42599	45	1.44201	30	0.55799	T.98398	3	32	7 5.5 5.4 8 6.3 6.1
29	1.42644	45	T.44250	40	0.55750	T.98395	4	31	8 6.3 6.1
30	1.42690		Ī.44299		0.55701	ĭ.98391		30	0 7.1 6.9
		45		49			3		10 7.8 7.7
31	T.42735	46	T.44348	40	0.55652	T.98388		20	20 15.7 15.3
32	1.42781	40	1.44397	49	0.55603	T.98384	4	28	30 23.5 23.0
33	1.42826	45	1.44446	49	0.55554	1.9838 ¹	3	27	40 31.3 30.7 50 39.2 38.3
34	1.42872	45	T.44495	49	0.55505	1.98377	4	26	50 39.2 38.3
35	I.42917	45	T.44544	49	0.55456	1.98373	3	25	
36	1.42962	45	1.44592	40	0.55408	1.98370	4	24	
37	T.43008	45	1.44641	49	0.55359	1.98366	3	23	47 1 24
38	T.43053	45	T.44690	48	0.55310	T.98363	3	22	45 44
39	1.43098	45	I.44738	40	0.55262	T.98359	3	21	6 4.5 4.4
40	T.43143		1.44787		0.55213	1.98356		20	7 5.3 5.1 8 6.0 5.9
		45		49			4	-	8 6.0 5.9 0 6.8 6.6
41	T.43188	45	T.44836	86	0.55164	1.98352	3	19	10 7.5 7.3
42	T.43233	45	T.44884	49	0.55116	1.98349	4	18	10 7.5 7.3
43	I.43278	45	T.44933	118	0.55067	T.98345	3	17	30 22.5 22.0
44	I.43323	45	T.44981	48	0.55019	1.98342		16	40 30.0 29.3
45	T.43367	45	T.45029	49	0.54971	T.98338		15	50 37.5 36.7
46	1.43412	45	T.45078	48	0.54922	T.98334	3	14	30 1 31.3 : 30.1
47	T.43457	45	T.45126	48	0.54874	¥.98331	Ĩ	13	
48	T.43502	. 44	T.45174	48	0.54826	T.98327		12	
49	T.43546	45	I.45222	110	0.54778	1.98324	4	II	4 1 3
50	T.43591		I.45271	1	0.54729	T.98320		10	6 0.4 0.3
		44		48		8 .0.	3		
SI	T.43635	45	T.45319	118	0.54681	¥.98317	4	9	7 0.5 0.4 8 0.5 0.4
52	T.43680	44	I.45367	48	0.54633	¥.98313	4		9 0.6 0.5
53	I.43724	45	1.45415	48	0.54585	T.98309	1	7	10 0.7 0.5
54	T.43769	64	1.45463	48	0.54537	T.98306 T.98302	14		20 1.3 1.0
55	T.43813	44	1.45511	113	0.54489	1.98302 T.98299	3	5	30 2.0 1.5
56	1.43857	12.4	¥.45559	47	0.54441	1.98299 T.98295	4	1	40 2.7 2.0
57 58	T.43901	45	1.45606	148	0.54394	1.98295	N.	3	50 3.3 2.5
	T.43946	10	1.45654	48	0.54346	1.98291	3	2	
59	1.43990	44	T.45702 T.45750	64	0.54298	1.98284	4		
60	1.44034								
őa	¥.44034								
60	1.44034 log cos	a	log cot	c. d.	log tan	log sin	a		p. p.

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'	log sin	а	log tan	c. d.	log cot	log cos	đ		p. p.
D	T.44034		T.45750		0.54250	T.98284		60	
1	T.44078	84	T.45797 T.45845	47	0.54203	T.98281	3	59	
2	¥.44122	44	T.45845		0.54155	T.98277	4	58	4.8 4.7
3	T.44166	44	T.45892	47 #B	0.54108	1.98273	3	57	6 4.8 4.7
- 4	T.44210	43	T.45940	47	0.54060	T.98270	N.	56	7 5.6 5.5 8 6.4 6.3
5	T.44253	44	1.45987	48	0.54013	I.98266	a l	55	
	T.44297	44	T.46035	47	0.53965	Y.98262 Y.98259	3	54	9 7.2 7.1
78	T.44341 T.44385	44	T.46082 T.46130	48	0.53918	T.98255	1	53 52	10 8.0 7.8 20 16.0 15.7
0	T.44305	43	T.46177	47	0.53823	I.98251	- 4	54	20 16.0 15.7 30 24.0 23.5
m	1.44472	44	T.46224	47	0.53776	T.98248	в	50	40 32.0 31.3
		44		47			4		50 40.0 39.2
11	1.44516		1.46271		0.53729	T.98244		49	
12	T.44559	43	1.46319	48	0.53681	T.98240	4	48	
13	T.44602	43	T.46366	47	0.53634	T.98237	3	47	
14	T.44646	43	T.46413	47	0.53587	T.98233	2	46	8.6 4.5
15	T.44689	44	T.46460	47	0.53540	T.98229	1	45	6 4.6 4.5
16	T.44733	43	I.46507	47	0.53493	1.98226	4	-	7 5.4 5.3 8 6.1 6.0
17 18	T.44776	43	1.46554	47	0.53446	T.98222 T.98218	4	43	
10	T.44819 T.44862	43	T.46601 T.46648	47	0.53399 0.53352	1.98218 T.98215	3	42	9 6.9 6.8 10 7.7 7.5
19	I.44002 I.44905	45	T.46694	46	0.53352	I.98215 I.98211	H.	41	10 7.7 7.5 20 15.3 15.0
		43		47	0.33300		4		30 23.0 22.5
21	T.44948		1.46741		0.53259	1.08207		30	40 30.7 30.0
33	I.44940	44	1.46788	47	0.53212	T.98204	3	38	50 38.3 37.5
23	T.45035	43	1.46835	47	0.53165	1.98200	4	37	
24	*.45077	42	T.46881	46	0.53119	T.98196	14	36	
25	T.45120	43	T.46928	47	0.53072	T.98192	4	35	
26	T.45163	43 43	¥.46975	47	0.53025	T.98189	3	- 34	44 43
27	T 45 206	43	1 47021	47	0.52979	1.98185	4	33	6 4.4 4.3
28	1.45249	43	1.47068	46	0.52932	1.98181	4	32	7 5.1 5.0
29	1.45292	42	1.47114	46	0.52886	1.98177	3	31	
30	1.45334		1.47160		0.52840	¥.98174		30	9 6.6 6.5 10 7.3 7.2
		43		47			14		10 7.3 7.2 10 14.7 14.3
31	I.45377	42	1.47207	46	0.52793	1.98170	14	29 28	
32	T.45419 T.45462	43	T.47253	46	0.52747 0.52701	T.98166 T.98162	14	20	30 22.0 21.5 40 29.3 28.7
33 34	T.45402	42	T.47299 T.47346	47	0.52654	T.08150	3	20	50 36.7 35.8
35	T.45547	43	T.47392	46	0.52608	T.98155	14	25	
36	T.45589	42	¥.47438	46	0.52562	1.98151	14	24	
37	T.45632	43	1.47484	46	0.52516	I.98147	4	23	
38	T.45674	42	1.47530	46	0.52470	T.98144	3	23	41
39	T.45716	42	1.47576	40	0.52424	T.98140	4	21	6 4.2 4.1
140	¥.45758	4-	¥.47622	110	0.52378	1.98136	4	105	1 4.9 4.8 8 5.6 5.5
		43		46	1.0		14	-	8 5.6 5.5
41	T.45801	42	T.47668	46	0.52332	T.98132	3	19	0 6.3 6.2
42	T.45843	42	1.47714	40	0.52286	1.98129	3	18	10 7.0 6.8 Int 14.0 13.7
43	¥.45885	42	1.47760	40	0.52240	1.98125	R I	17	30 21.0 20.5
44	T.45927 T.45969	42	T.47806 T.47852	46	0.52194	T.98121 T.98117	a l	10 15	40 28.0 27.3
45	1.45909 T.46011	42	1.47852	45	0.52148	1.98117 T.08113	14	15 14	50 35.0 34.2
40	1.40011 1.46053	42	I.47097 I.47943	16	0.52103	1.98113	3	14	
28	T.46095	42	1.47989	46	0.52057	T.98106	14	12	
10	I.46136	41	T.48035	46	0.51965	1.98102	14	II	
50	T.46178	42	1.48080	45	0.51920	1.98098	н	10	4 0
		42		46			и		0 0.4 0.3
SI	T.46220		T.48126		0.51874	1.98094		0	7 0.5 0.4
52	T.46262	42 41	T.48171	45	0.51829	1.98090	H	0	
53	1.46303	41	1.48217	40	0.51783	1.98087	8	7	0 0.6 0.5 10 0.7 0.5
54	I.46345	41	1.48262	45	0.51738	1.98083	4	0	10 0.7 0.5
55	T.46386	42	T.48307	46	0.51693	1.98079	1	5	30 1.0 1.5
56	T.46428 T.46469	41	7.48353 7.48398	45	0.51647	1.98075 1.98071	4	4	40 2.7 2.0
57 58	I.40409 I.46511	42	1.48398 1.48443	45	0.51002	T.98071 T.98067	18	-	50 3.3 2.5
59	1.46552	41	T.48489	46	0.51511	1.98063	4	1	
60	T.46594	42	1.48534	45	0.51406	1.98060	3	0	
					1				
	log cos	b	log cot	c. d.	log tan	log sin	đ	'	p. p.

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1	log sin	đ	log tan	c. d.	log cor	log cos	đ		p. p.
0	T.46594		T.48534		0.51466	1.08060		60	
I	T.46635	11	1.48579	45	0.51421	T.98056	4	59	
12	1.46676	141 141	1.48624	45	0.51376	1.98052	4	58	45 44
3	T.46717	141	T.48669	45 45	0.51331	1.98048	4	57	6 4.5 4.4
1	T.46758	42	1.48714	45	0.51286	1.98044	4	56	7 5.3 5.1 6.0 5.9
E C	1.46800	11	T.48759	45	0.51241	I.98040	a	55	
	T.46841	ar	1.48804	45	0.51196	T.98036	4	54	6.8 6.6
8	T.46882	41	1.48849	45	0.51151	1.98032 1.98029	3	53	10 7.5 7.3
9	T.46923 T.46964	41	T.48894 T.48939	45	0.51106	1.98029	14	52	20 15.0 14.7 30 22.5 22.0
10	T.40904	41	T.48984	45	0.51016	T.98025	18	50	30 22.5 22.0
1	114/003	40	1100904	45	0.3.0.0		н	50	50 37.5 36.7
11	T.47045		T.49029		0.50971	T.98017		49	
12	1.47086	11 11	I.49073	44 45	0.50927	T.98013	4	48	
13	1.47127	AL.	1.49118	45	0.50882	T.98009	4	47	
14	T.47168	31	T.49163	43	0.50837	T.98005	4	46	43
15	I.47209	40	T.49207	45	0.50793	1.98001	14	45	6 4.3
16	1.47249	41	T.49252 T.49296	44	0.50748	T.97997 T.97993	4	44	7 5.0
17	T.47290 T.47330	40	I.49290 I.49341	45	0.50659	I.97993 I.97089	4	43	8 5.7 9 6.5
10	1.47371	41	1.49341	44	0.50615	1.97986	3	41	10 7.2
30	I.47411	40	I.49430	45	0.50570	I.97982	4	40	20 14.3
		41		44			н	-	30 21.5
21	T.47452	DE OE	Ī.49474		0.50526	T.97978		39	40 28.7
22	T.47492	41	Ī.49519	45	0.50481	I.97974	4	38	50 35.8
23	1.47533	40	T.49563	44	0.50437	I.97970	4	37	
24	1.47573	40	1.49607	45	0.50393	I.97966	4	36	
25	T.47613	41	1.49652	44	0.50348	1.97962	4	35	12 41
26	T.47654 T.47694	40	1.49696	84	0.50304	I.97958	14	34	5 4.2 4.1
58	T.47094	140	T.49740 T.49784	84	0.50200	T 97954 T.97950	4	32	
20	1.47774	40	1.49828	44	0.50172	T.97946	Ш	31	7 4.9 4.8 8 5.6 5.5
30	I.47774 I.47814	380	1.49872	44	0.50128	1.97942	4	30	9 6.3 6.2
		80		44			B.		10 7.0 6.8
31	1.47854		T.49916		0.50084	T.97938		20	20 14.0 13.7
32	1.47894	40	T.49960	44	0.50040	1.97934	4	28	30 21.0 20.5
33	1.47934	40	1.50004	44	0.49996	I.97930	1	27	28.0 27.3
34	I.47974	40	T.50048	44	0.49952	T.97926	14	26	50 35.0 34.2
35	1.48014	40	T.50092	10.0	0.49908	I.97922		25	-
36	T.48054	40	1.50136	44	0.49864	1.97918	4	24	
37	T.48094 T.48133	39	T.50180	43	0.49820	I.97914	H.	23	40 39
38 39	T.48173	an a	T.50223 T.50267	44	0.49777 0.49733	I.97910 I.97906		21	6 4.0 3.9
40	I.48213	40	I.50311	44	0.49689	T.97902	A	20	
		39		44			н		• 7 4.7 4.6 8 5.3 5.2 0 6.0 5.9
41	T.48252		T.50355	1	0.49645	1.97898		19	6.0 5.9
42	T.48292	40	1.50398	43	0.49602	T.97894	14	18	10 6.7 6.5
43	T.48332	39	¥.50442	44	0.49558	T.97890	N N	17	13.3 13.0 10 20.0 10.5
164	1.48371	40	T-50485	44	0.49515	1.97886	14	16	30 20.0 19.5 40 26.7 26.0
145	T.48411	39	1.50529	43	0.49471	1.97882	a l	15	50 33.3 32.5
46	1.48450 1.48490	HO.	T.50572 T.50616	44	0.49428 0.49384	1.97878 1.97874	14	14	55 . 33.3 . 34.3
47	T.48520	39	T.50659	43	0.49384	1.97870	14	13	
142	I.48568	39	I.50703	44	0.49341	1.97866	4		
50	¥.48607	30	1.50746	43	0.49254	1.97861	5	III	5 4 3
		20		43			н		6 0.5 0.4 0.3
51	T.48647		1.50789		0.49211	1.97857		Q	7 0.6 0.5 0.4
52	7.48686	39	1.50833	44	0.49167	T.97853	N.	8	
53	1.48725	30	1.50876	43	0.49124	T.97849	4	7	10 0.8 0.6 0.5 10 0.8 0.7 0.5
54	1.48754	30	T.50919	43	0.49081	I.97845	4	ñ	10 0.8 0.7 0.5 201 1.7 1.3 1.0
55	T.48803 T.48842	39	T.50962	43	0.49038	1.97841	4	5	30 2.5 2.0 1.5
56	1.48842 T.48881	19	I.51005 I.51048	43	0.48995	T.97837 T.97833	R.		40 3.3 2.7 2.0
57 58	T.48920	39	1.51048 T.51092	1414	0.48908	1.97833 1.97829	14	3	50 4.2 3.3 2.5
500	I.48959	39	1.51135	43	0.48865	1.97825	4	I	
60	1.48998	30	1.51178	43	0.48822	T.97821		0	
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	log cos	a	log cot	c. d.	log tan	log sin	a	,	
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'	log sin	a	log tan	c. d.	log cot	log cos	а		p . p.
0	T.48998	30	T.51178	43	0.48822	1.97821	4	60	
I	T.49037	30	1.51221	43	0.48779	1.97817	5	59	
2	T.49076	30	¥.51264	42	0.48736	I.97812	1 a	58	68 62
3	T.49115	38	T.51306	43	0.48694	1.97808	4	57	6 4.3 4.2
4	T.49153	30	T.51349	43	0.48651	1.97804	4	56	7 5.0 4.9 8 5.7 5.6
S 6	T.49192	39	T.51392	43	0.48608	1.97800	4	85	
	T.49231 T.49269	38	T.51435 T.51478	43	0.48522	T.97796	4	54	6.5 6.3
78	T.49308	39	T.51530	42	0.48480	T.97792 T.97788	14	53	10 7.2 7.0 100 14.3 14.0
ŭ	T.49347	39	1.51563	43	0.48437	1.97784	14	52	14.3 14.0 30 21.5 21.0
10	1.49385	38	1.51606	43	0.48394	1.97779	5	50	40 28.7 28.0
		39		42	0140394	**9///9		30	59 35.8 35.0
11	T.40424		T.51648		0 48352	¥.97775		100	Be 1 00.0 1 00.0
12	T.49462	38	T.51691	43	0.48309	I.97771	14	48	
13	T.49500	38	I.51734	43	0.48266	T.07767	4	47	
14	T.49539	00	T.51776	42	0.48224	T.97763	4	46	41
15	T.49577	38	1.51819	43	0.48181	T.97759	И	45	6 4.1
116	I.49615	38	T.51861	42	0.48139	T.97754	5	44	7 4.8
17	T.49654	39	T.51903	42	0.48097	1.97750	4	43	7 4 H 8 5.5 9 6.2
	I.49692	38 38	¥.51946	43	0.48054	T.97746	14	42	9 6.2
19	T.49730	38	1.51988	43	0.48012	T.97742	4	41	10 6.8
20	1.49768		T.52031	43	0.47969	1.97738		40	20 13.7
	_	38		42			14		30 20.5
21	1.49806	18	1.52073	42	0.47927	T.97734	5	39	40 27.3
1 23	T.49844	38	1.52115	44	0.47885	T.97729	14	38	50 34.7
23	¥.49882	30	1.52157	43	0.47843	T.97725-	4	37	
24	¥.49920	38	¥.52200	43	0.47800	T.97721	4	36	
25	1.49958	38	1.52242	42	0.47758	I.97717	4	35	39 18
20	1.49996	38	1.52284	42	0.47716	T.97713	5	34	
27	T.50034 T.50072	38	T.52326	42	4.47674	¥.97708	14	33	
20	I.50110	38	T.52368 T.52410	42	0.47632	T.97704	4	32	7 4.6 4.4 B 5.2 5.1
30	I.50148	38	1.52410	42	0.47590	T.97700 T.97696	4	30	5.9 5.7
30	1.50140		1.52454		0.47540	1.9/090		30	10 6.5 6.3
	T.50185	37		43			5		20 13.0 12.7
31 32	1.50105 T.50223	38	T.52494 T.52536	42	0.47506	7.97691	R.	28	30 19.5 19.0
33	1.50261	38	1.52530	42	0.47464	T.97687 T.97683	4	20	40 26.0 25.3
34	T.50298	37	I.52620	42	0.47380	T.97679	4	26	50 32.5 31.7
35	T.50336	38	T.52661	41	0.47339	I.97674	5	25	
36	1.50374	38	1.52703	4∎	0.47297	1.97670	N	24	
37	1.50411	37	T.52745	42	0.47255	T.97666	4	23	
38	7.50449	38	1.52787	43	0.47213	T.97662	4	22	37 88
39	1.50486	37	T.52829	42 41	0.47171	I.97657	5	21	D 3.7 3.6
40	T.50523	37	¥.52870	44.	0.47130	1.97653		20	7 4.3 4.2 8 4.9 4.8
		38		43			14		
41	1.50561	37	T.52912	41	0.47088	T.97649	14	19	5.6 · 5.4
42	T.50598	37	T.52953	41	0.47047	T.97645	5	18	20 12.3 12.0
43	1.50635	38	T.52995	42	0.47005	1.97640	iii ii	17	18.5 18.0
44	T.50673	37	I.53037	41	0.46963	1.97636	ii ii	16	24.7 24.0
45	T.50710	37	T.53078	42	0.46922	1.97632	a l	15	50 30.8 30.0
	T.50747 T.50784	37	T.53120 T.53161	41	0.46880	T.97628 T.97623	5	14 13	
47 49	1.50821	37	T.53202	41	0.40039	I.97619	14	13	
49	T.50858	37	T.53244	42	0.46756	T.97615	14	11	
50	T.50896	38	T.53285	41	0.46715	I.97610	5	10	5 4
		37		43	0.107-0		4		6 0.5 0.4
SI	T.50933		T.53327		0.46673	¥.97606		0	7 0.6 0.5
52	1.50070	37	T.53368	41	0.46633	1.97602	H	9	
53	1.51007	37	T.53409	41	0.46501	T.97597	5		
54	T.51043	36	T.53450	41	0.46550	T.97593	14	7	10 0.8 0.7
55	1.51080	37	T.53492	42	0.46508	T.97589	H	5	20 1.7 1.3
56	1.51117	37	T.53533	4I 4I	0.46467	1.97584	5	- 14	30 2.5 2.0
57	1.51154	37	1.53574	41	0.46426	¥.97580	4	3	40 3.3 2.7 50 4.2 3.3
S.H	1.51191	36	1.53615	41	0.46385	1.97576	5	2	50 4.2 3.3
50	T.51227	37	T.53656	41	0.46344	Y.97571	Ä	I	
00	T.51264		T.53697		0.46303	1.97567		0	
	log cos	d	log cot	c. d.	log tan	log sin	đ		p. p.
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'	log sin	d	log tan	c. d.	log cot	log cos	в		p. p.
	7.51264		¥.53697		0.46303	T.97567		60	
1	T.51301	37	T.53738	41	0.46262	T.97563	4	59	
2	1.51338	37		41	0.46221	T.97558	5	58	41 40
	T.51374	36 37	1.53779 1.53820	41	0.46180	I.97554	4	57	ñ 4.1 4.0
H	1.51411	36	1.53861	41	0.46139	T.97550	5	56	7 4.8 4.7 8 5.5 5.3
5	1.51447	37	I.53902	41	0.46098	Ī.97545	4	55	
	T.51484 T.51520	36	T.53943 T.53984	41	0.46057	T.97541 T.97536	5	54 53	9 6.2 6.0 10 6.8 6.7
7	I.51520	37	T.54025	41	0.45975	I.97532	14	52	20 13.7 13.3
	I.51593	36	T.54065	40	0.45935	1.97528		51	30 20.5 20.0
10	T.51629	36	1.54106	41	0.45894	I.97523	5	50	40 27.3 26.7
1.00	-	37		41			A		50 34.2 33.3
11	T.51666	36	T.54147	40	0.45853	1.97519	4	49	
12	1.51702	36	1.54187	41	0.45813	I.97515	5	48 47	
13 14	Ī.51738	36	T.54228 T.54269	41	0.45772	T.97510 T.97506	18	47	39
15	1.51774 1.51811	37	T.54309	40	0.45691	I.97501	5	45	6 3.9
16	Ī.51847	36	1.54350	41	0.45650	I.97497	1	44	. 7 4.6
17	1.51883	36 36	1.54390	40	0.45610	Ī.97492	5	43	8 5.2
18	1.51919	36	T.54431	40	0.45569	1.97488		42	9 5.9
19 20	Ī.51955 Ī.51991	36	T.54471 T.54512	41	0.45529	ī.97484 ī.97479	5	41 40	10 6.5 20 13.0
20	1.51991	36	1.54514	40	0.43400	1.9/4/9	я	40	30 19.5
21	T.52027		Ī.54552		0.45448	1.97475		39	40 26.0
22	I.52063	36	1.54552 1.54593	41	0.45407	Ī.97470	5	38	50 32.5
23	1.52099	36 36	1.54633	40	0.45367	1.97466	4	37	
24	T.52135	30	Ī.54673	40	0.45327	1.97461	5	.36	
25	1.52171	36	1.54714	40	0.45286	1.97457	14	35	37 36
26	T.52207	35	1.54754	40	0.45246	Ī.97453 Ī.97448	5	34	
27 28	Ī.52242 T.52278	36	T.54794 T.54835	41	0.45165	Ī.97444	14	33 32	
20	1.52314	36	1.54875	40	0.45125	T.97439	5	31	7 4.3 4.2 8 4.9 4.8
30	1.52350	36	Ī.54915	40	0.45085	¥.97435	- 4	30	0 5.6 5.4
1.00		35		40			5		10 6.2 6.0
31	T.52385	36	T.54955	40	0.45045	1.97430	4	29	20 12.3 12.0 30 18.5 18.0
32	1.52421	35	T.54995	40	0.45005	1.97426	5	28	30 18.5 18.0 40 24.7 24.0
33 34	T.52456 T.52492	36	T.55035 T.55075	40	0.44965	1.97421 1.97417	14	27 26	50 30.8 30.0
34	1.52492	35	1.55115	40	0.44885	1.97412	5	25	
36	1.52563	36	1.55155	40	0.44845	1.97408	14	24	
37	1.52598	35 36	Ī.55195	40	0.44805	Ī.97403	5	23	
38	I.52634	35	1.55235	40	0.44765	1.97399	5	22	35 34
39	1.5.2669	36	1.55275	40	0.44725 0.44685	1.97394 1.97390	4	21	6 3.5 3.4
40	Ī.52705	35	Ī.55315	40	0.44005	1.9/390	5	20	7 4 I 4.0 8 4.7 4.5
41	T.52740		T.55355		0.44645	1.97385		19	9 5.3 5.I
41	1.52740	35	I.55395	40	0.44605	1.97381	4	18	10 5.8 5.7
43	1.52811	36	Ī.55434	39 40	0.44566	T.97376	5	17	20 11.7 11.3
44	1.52846	35	1.55474	40	0.44526	T.97372	4	16	30 17.5 17.0 40 23.3 22.7
45	1.52881	35	1.55514	40	0.44486	1.97367	4	15	50 29.2 28.3
46	T.52916 T.52951	35	ī.55554 ī.55593	39	0.44446	T.97363 T.97358	5	14 13	50 ; eyie ; e0i3
47 48	1.52951 T.52986	35	1.55593 T.55633	40	0.44367	I.97350 I.97353	5	13	
49	T.53021	35	1.55673	40	0.44327	1.97349	1	11	
50	T.53056	35	1.55712	39	0.44288	7.97344	5	10	5 1
		36		40			a l		6 0.5 0.4
51	T.53092	34	1.55752	30	0.44248	I.97340	5	8	7 0.6 0.5
52	T.53126	35	1.55791 1.55831	40	0.44209	I.97335	3		8 0.7 0.5 9 0.8 0.6
53 54	1.53161 T.53196	35	1.55831	39	0.44169	T.97331 T.97326	5	7	EE 0.8 0.7
55	1.53190	35	Ī.55910	40	0.44090	I.97322		5	20 1.7 1.3
56	1.53266	35	ī.55949	39	0.44051	T.97317	5	4	30 2.5 2.0
57	T.53301	35	1.55989	40	0.44011	1.97312	5	3	40 3.3 2.7
58	ī.53336	35	1.56028	39	0.43972	1.97308	5	2	50 4.2 3.3
59	1.53370	35	I.56067 I.56107	40	0.43933 0.43893	I.97303 I.97299	4	1	
00	¥.53405		1.50107		0.43093	1.9/299		0	
	log cos	a	log cot	c. d.	log tan	log sin	2	,	
	IOE COS	a	TOE COL	C. G.	iog tan	108 211	6		p. p.

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'	log sin	ы	log tan	c, d.	log cot	log cos	а		p. p.
0	T.53405		1.56107	-	0.43893	T.07200		20	
1	T.53440	35	1.90146	39	0.43854	I.97294	5	59	
2	T.53475	35	T.56185	30	0.43815	T.97289	5	58	40 89
B	1.53509	34	T.56224	39	0.43776	1.97285	14	57	6 4.0 3.9
15	T.53544	35	1.56264	40	0.43736	1.97280	5	56	7 4.7 4.6
5	T.53578	35	T.56303	000	0.43697	1.97276	5	55	
	I.53613	34	1.56342	39	0.43658	T.97271	5	54	0.0 5.9
8	T.53647 T.53682	35	1.56381	39	0.43619	1.97266	4	53	10 6.7 6.5
0	I.53002	34	T.56420 T.56459	080	0.43580	I.97262 I.97257	5	52 51	20 13.3 13.0 30 20.0 19.5
10	I.53751	35	1.56498	39	0.43502	I.97252	5	51	20.0 19.9
		34		39	0140500				50 33.3 32.5
11	1.53785		1.56537		0.43463	T.97248		140	
12	1.53819	34	I.56576	39	0.43424	T.97243	5	48	
13	1.53854	35	T.56615	39 39	0.43385	1.97238	8	47	
14	¥.53888	34	T.56654	39	0.43346	T.97234	5	46	38 37
15	T.53922	35	T.56693	39	0.43307	I.97229	5	45	6 3.8 3.7
	T.53957 T.53991	34	T.56732	1 39	0.43268	T.97224 T.97220	14	44 43	7 4.4 4.3
17	I.54025	34	I.56771 I.56810	39	0.43229	1.97215	5	43	8 5.1 4.9 0 5.7 5.6
10	T.54025	34	1.56849	39	0.43151	I.97210	5	42	10 6.3 6.2
20	I.54093	34	1.56887	38	0.43113	1.97206	A	40	12.7 12.3
		34		39			5		30, 19.0 18.5
21	T.54127	34	T.56926		0.43074	1.97201	-	39	10 25.3 24.7
93	1.54161	34	1.56965	39 30	0.43035	T.97196	5 4	38	50 31.7 30.8
23	T.54195	34	T.57004	38	0.42996	Ī.97192	5	37	
24	1.54229	34	1.57042	30	0.42958	1.97187	5	36	
25	T.54263 T.54297	34	I.57081 I.57120	39	0.42919 0.42880	I.97182 I.97178	14	35 34	85
27	I.5429/ I.54331	34	1.57158	38	0.42842	I.97173	5	34	6 3.5
59	1.54365	34	T.57197	39	0.42803	I.97168	5	32	7 4.1
39	T.54399	34	I.57235	38	0.42765	I.97163	5	31	7 4.1 8 4.7
30	1.54433	34	I.57274	39	0.42726	I.97159	4	30	9 5.3 10 5.8
	_	33		38			5		
31	T.54466	34	T.57312	30	0.42688	1.97154	5	29	20 11.7 30 17.5
32	T.54500	34	I.57351	38	0.42649	1.97149	4	215	30 17.5 40 23.3
33	T.54534 T.54567	33	1.57389	39	0.42611	T.97145	5	27	50 29.2
34	I.54507	34	T.57428 T.57466	38	0.42572	T.97140 T.97135	5	25	
36	T.54635	34	T.57504	38	0.42496	T.07130	5	24	
37	1.54668	33	T.57543	90	0.42457	1.97126	4	23	
38	T.54702	33	¥.57581	38 38	0.42419	1.97121	5	22	34 33
30	1.54735	33	¥.57619	30	0.42381	1.97116	5	21	6 3.4 3.3
NO	1.54769		I.57658		0.42342	1.97111		20	7 4.0 3.9
		33		38	-		М		2 4.5 4.4 9 5.1 5.0
4I 42	T.54802 T.54836	34	1.57696	38	0.42304 0.42266	I.97107	5	19	10 5.7 5.5
44	1.54030 T.54869	33	T.57734 T.57772	38	0.42200	T.97102 T.97097	5	10	20 11.3 11.0
44	T.54903	34	1.57810	38	0.42190	I.97092	5	16	30 17.0 16.5
45	1.54936	33	1.57849	39 38	0.42151	I.97087	5	15	40 22.7 22.0
46	T.54969	33	T.57887	30	0.42113	T.97083	4	14	50 28.3 27.5
47	1.55003	34	T.57925	38	0.42075	1.97078	5	13	
45	I.55036	33	1.57963	38	0.42037	T.97073	5	12	
40 50	I.55069 I.55102	33	1.58001 1.58039	38	0.41999 0.41961	T.97068 T.97063	8	10	5 1 4
	1.33105	34	1.30039	38	Sid i got	1.97003	4		6 0.5 0.4
51	T.55136		1.58077		0.41023	I.97059		0	7 0.6 0.5
52	1.55169	33	1.58115	38	0.41885	T.97054	1	8	
53	1.55202	33 33	T 58153	38 38	0.41847	T.97049	3	7	0.8 0.6 11 0.8 0.7
54	1.55235	33	T.58191	30	0.41809	I.97044	5		215 1.7 1.3
55 56	Y.55268	33	T 58229	38	0.41771	1.97039	14	5	30 2.5 2.0
	T.55301 T.55334	33	T.58267 T.58304	37	0.41733 0.41696	T.97035	5	R R	40 3.3 2.7
31	T.55334 T.55367	33	1.58304	38	0.41658	T.97030 T.97025	5	2	50 4.2 33
58		33	1.58380	38 38	0.41620	1.97020	5	I	
57 58 59	T.55400						5	ō	
	I.55400 I.55433	33	1.58418	30	0.41582	I.97015	-	0	
59		33	1.58418		0.41582	1.97015			
59		a	1.58418 log cot	c. d.	0.41582 log tan	log sin	a	,	

/ 0 II 2 3 3 4 5 6 7 7 8 9 10 10 11 12 3 14 15 16 17 18	log sin 7.55433 7.55466 7.55499 7.55532 7.55597 7.55593 7.55593 7.55793 7.55793 7.55793 7.55793 7.55928 7.5	d 33 33 33 33 33 33 33 33 33 33 33 33 33	log tan 1.58418 1.58455 1.58493 1.58531 1.58531 1.58541 1.58641 1.58794 1.58974 1.59774 1.5977575 1.5977575 1.5977575 1.5977575757575757575757575757575	c. d. 37 38 38 38 37 38 37 38 37 38 37 38 37 38 37 38	0.41582 0.41582 0.41545 0.41507 0.41450 0.41394 0.41356 0.41319 0.41281 0.41281 0.41283 0.41206	log cos 1.97015 1.97010 1.97005 1.97005 1.97005 1.96996 1.96986 1.96981 1.96971 1.96966 1.96966 1.96962	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	59 58 57 56 55 54 53 52 51 30	D-D- III 37 6 3.8 3.7 7 4.4 4.3 8 5.1 4.9 9 5.7 5.6 10 6.3 6.2 10 12.7 12.3 30 19.0 18.5 40 25.3 24.7 50 31.7 30.8
1 2 3 1 5 5 5 7 8 1 0 1 1 2 3 1 4 1 5 1 1 6 1 7	1.5546 1.55499 1.55532 1.55507 1.55507 1.55605 1.55703 1.55703 1.55826 1.55826 1.55827 1.55827 1.55827 1.55827 1.55923 1.55928	11 33 32 33 33 33 33 33 32 33 32 33 32 33 32 33 32	1.58455 7.58493 1.58509 1.58609 1.5864 1.58644 1.58681 1.58757 1.58757 1.58794 1.58832 1.58832 1.58869 1.58869	38 38 37 38 37 38 37 38 38 37 38 37 38 37	0.41545 0.41545 0.41507 0.41431 0.41394 0.41356 0.41319 0.41281 0.41243 0.41206	Y.97010 Y.97010 Y.97005 J.97001 Y.96996 Y.96996 Y.96986 Y.96986 Y.96987 Y.96971 Y.96966 Y.969671 Y.96966	5 4 5 5 10 10 10 10 10	59 58 57 56 55 54 53 52 51 50	6 3.8 3.7 7 4.4 4.3 8 5.1 4.9 9 5.7 5.6 10 6.3 6.2 10 12.7 12.3 30 19.0 18.5 40 25.3 24.7
1 2 3 1 5 5 5 7 8 1 0 1 1 2 3 1 4 1 5 1 1 6 1 7	1.5546 1.55499 1.55532 1.55507 1.55507 1.55605 1.55703 1.55703 1.55826 1.55826 1.55827 1.55827 1.55827 1.55827 1.55923 1.55928	11 33 32 33 33 33 33 33 32 33 32 33 32 33 32 33 32	1.58455 7.58493 1.58509 1.58609 1.5864 1.58644 1.58681 1.58757 1.58757 1.58794 1.58832 1.58832 1.58869 1.58869	38 38 37 38 37 38 37 38 38 37 38 37 38 37	0.41545 0.41545 0.41507 0.41431 0.41394 0.41356 0.41319 0.41281 0.41243 0.41206	Y.97010 Y.97010 Y.97005 J.97001 Y.96996 Y.96996 Y.96986 Y.96986 Y.96987 Y.96971 Y.96966 Y.969671 Y.96966	5 4 5 5 10 10 10 10 10	59 58 57 56 55 54 53 52 51 50	6 3.8 3.7 7 4.4 4.3 8 5.1 4.9 9 5.7 5.6 10 6.3 6.2 10 12.7 12.3 30 19.0 18.5 40 25.3 24.7
2 3 5 5 7 8 10 11 12 13 14 15 10 17	1.55490 Y.55532 Y.55564 Y.55564 Y.55563 Y.55563 Y.55563 Y.55563 Y.55728 Y.55761 I.55793 Y.55826 T.55856 T.55856 I.55928 Y.55956 T.55988	33 32 33 33 33 33 33 32 33 32 33 32 33 32 33 32	T.58493 T.58531 T.58560 T.58606 T.58644 T.58681 T.58757 T.58794 T.58832 T.58832 T.58869 T.58860	38 38 37 38 37 38 38 38 37 38 37 38	0.41507 0.41469 0.41431 0.41356 0.41356 0.41319 0.41281 0.41243 0.41206	T.97005 I.97001 T.96996 T.96991 T.96986 T.96981 T.96976 T.96971 T.96966	455888855	58 57 56 55 54 53 52 51 50	6 3.8 3.7 7 4.4 4.3 8 5.1 4.9 9 5.7 5.6 10 6.3 6.2 10 12.7 12.3 30 19.0 18.5 40 25.3 24.7
3 5 7 8 10 11 12 13 14 15 16 17	1.55532 1.5554 1.55597 1.5563 1.55695 1.55728 1.55728 1.55728 1.55728 1.55728 1.55728 1.55728 1.55828 1.55828 1.55828 1.55828 1.55926 1.55926	32 33 33 32 33 33 32 33 32 33 32 33 32 33 32	I.58531 I.58560 I.58606 I.58644 I.58681 I.58719 I.58757 I.58794 I.58832 I.58832 I.58869 I.58869	38 37 38 37 38 38 37 38 37 38 37	0.41469 0.41431 0.41394 0.41356 0.41319 0.41281 0.41243 0.41206	I.97001 I.96996 I.96996 I.96986 I.96986 I.96976 I.96976 I.96971 I.96966	5588888555	56 55 54 53 52 51 50	7 4.4 4.3 8 5.1 4.9 9 5.7 5.6 10 6.3 6.2 20 12.7 12.3 30 19.0 18.5 40 25.3 24.7
10 10 11 12 13 14 15 16	I.55564 Y.55597 Y.55630 J.55695 J.55728 T.55761 J.55793 J.55826 T.55891 J.55923 J.55926 T.55926 J.55926	33 33 32 33 33 33 32 33 32 33 32 33 32	T.58569 T.58606 T.58644 T.58681 T.58719 T.58757 T.58794 T.58832 T.58869 T.58809	37 38 37 38 38 37 38 37 38 37	0.41431 0.41394 0.41356 0.41319 0.41281 0.41243 0.41206 0.41168	T.96991 T.96986 T.96981 T.96976 T.96971 T.96966	5 10 10 10 15	55 54 53 52 51 50	9 5.7 5.6 10 6.3 6.2 26 12.7 12.3 30 19.0 18.5 40 25.3 24.7
5 7 8 10 11 12 13 14 15 16 17	1.55597 1.55630 1.55663 1.55695 1.55793 1.55761 1.55793 1.55828 1.55891 1.55923 1.55923 1.55923 1.55926 1.55928	33 32 33 33 33 32 33 32 33 32 33 32	I.58644 I.58681 I.58719 I.58757 I.58794 I.58832 I.58869 I.58807	38 37 38 38 37 38 37 38 37	0.41356 0.41319 0.41281 0.41243 0.41206 0.41168	1.96986 1.96981 1.96976 1.96971 1.96966	M M M M S S	54 53 52 51 50	9 5.7 5.6 10 6.3 6.2 26 12.7 12.3 30 19.0 18.5 40 25.3 24.7
7 8 10 11 12 13 14 15 16 17	T.55663 I.55695 T.55728 T.55761 I.55793 T.55826 T.55858 T.55858 I.55923 T.55926 T.55988	33 32 33 33 32 33 32 33 32 33 32	T.58681 T.58719 T.58757 T.58794 T.58832 T.58869 T.58869	37 38 38 37 38 37	0.41319 0.41281 0.41243 0.41206 0.41168	T.96981 T.96976 T.96971 T.96966	10 10 S S	53 52 51 50	10 6.3 6.2 10 12.7 12.3 30 19.0 18.5 40 25.3 24.7
10 10 11 12 13 14 15 16 17	T.55695 T.55728 T.55761 T.55826 T.55826 T.55858 T.55858 T.55923 T.55926 T.55988	32 33 33 32 33 32 33 32 33 32	T.58719 T.58757 T.58794 T.58832 T.58869 T.58807	38 38 37 38 37	0.41281 0.41243 0.41206 0.41168	T.96976 T.96971 T.96966	5 5	52 51 50	12.7 12.3 30 19.0 18.5 40 25.3 24.7
10 10 11 12 13 14 15 16 17	T.55728 T.55761 T.55826 T.55858 T.55858 T.55891 T.55923 T.55956 T.55988	33 33 32 33 32 33 32 33 32	I.58757 I.58794 I.58832 I.58869 I.58807	38 37 38 37	0.41243 0.41206 0.41168	T.96971 T.96966	5 5	51	30 19.0 18.5 40 25.3 24.7
10 11 12 13 14 15 16 17	T.55761 T.55793 T.55826 T.55858 T.55858 T.55923 T.55926 T.55988	32 33 32 33 32	T.58794 T.58832 T.58869 T.58007	38 37	0.41206	I.96966		50	40 25.3 24.7
11 12 13 14 15 16 17	T.55793 T.55826 T.55858 T.55891 T.55923 T.55956 T.55988	33 32 33 32	T.58832 T.58869 T.58007	37	0.41168		4		50 31.7 30.8
12 13 14 15 16 17	Y.55826 T.55858 T.55891 T.55923 T.55956 T.55988	33 32 33 32	T.58869 T.58007	37		1.06062			5- 1 5-1 - 5-1-
12 13 14 15 16 17	Y.55826 T.55858 T.55891 T.55923 T.55956 T.55988	32 33 32	T.58869 T.58007	37 38				80	
13 14 15 16 17	T.55858 T.55891 T.55923 T.55956 T.55988	33 32	1.58007	38		1.96957	5	48	
14 15 16 17	T.55891 T.55923 T.55956 T.55988	32	T.58044		0.41093	T.96952	5	47	
15 16 17	Ĩ.55923 Ĩ.55956 Ĩ.55988			37	0.41056	T.96947	5	46	36 53
16	1.55988		1.58981	37	0.41019	T.96942	5	45	6 3.6 3.3
17 18	I.55988		T.59019	38	0.40981	T.96937	5	44	7 4.2 3.0
18	1 7 56021	32	1.59056	37 38	0.40944	T.96932	5	43	
	1.30021	33	I.59094	37	0.40906	1.96927	5	42	0 5.4 5.0
19	T.56053	32	T.59131	37	0.40869	1.96922	S	41	10 6.0 5.5
20	1.56085		T.59168		0.40832	1.96917		40	30 12.0 11.0 30 18.0 16.5
		33	-	37			S		40 24.0 22.0
21	1.56118	32	1.59205	38	0.40795	T.96912	5	39 38	50 30.0 27.5
22	T.56150 T.56182	32	T.59243 T.59280	37	0.40757 0.40720	T.96907 T.96903	и	30	J- 1 J 1 -1-J
23 24	1.50102	33	1.59200	37	0.40683	T.96898	5	36	
25	T.56247	32	T.59354	37	0.40646	T.96893	5	35	
26	1.56279	32	T.59391	37	0.40609	T.96888	5	34	32
27	T.56311	32	I.59429	38	0.40571	1.96883	5	33	6 3.2
	I 1.56343	32	1.59466	37	0.40534	¥.96878	5	32	7 3.7 8 4.3
20	1.56375	33	I.59503	37	0.40497	T.96873	5	31	
30	1.56408		1.59540		0.40460	T.96868		30	9 4.8
		32		37			5		10 5.3 20 10.7
31	T.56440	32	1.59577	37	0.40423	T.96863	5	10	30 16.0
32	I.56472	32	¥.59614	37	0.40386	T.96858 T.96853	5	28 27	40 21.3
33 34	T.56504 T.56536	32	T.59651 T.59688	37	0.40349	1.96848	5	27	50 26.7
35	1.56568	32	1.59725	37	0.40275	T.96843	5	25	
36	T.56599	31	1.59762	37	0.40238	T.06838	5	24	
37	1.56631	32	1.59799	37 36	0.40201	1.96833	5	23	
38	T.56663	32	1.59835	30	0.40165	1.96828	5	22	31 6
39	T.56695	32	1.59872	37	0.40128	1.96823	5	21	6 3.1 0.6
40	I.56727		¥.59909		0.40091	¥.96818		20	7 3.6 0.7 8 4.1 0.8
		32		37			5		
41	T.56759	31	T.59946	37	0.40054	1.96813	5	19	9 4.7 0.9 10 5.2 1.0
42	1.56790	32	1.59983	36	0.40017	T.96808	5	18	10 10.3 2.0
43	T.56822 T.56854	32	T.60019 T.60056	37	0.39981 0.39944	T.96803 T.96798	5	17	30 15.5 3.0
44 45	I.56886	32	T.60093	37	0.39944	1.96793	5	15	40 20.7 4.0
45	T.56917	31	1.60130	37	0.39870	1.96788	5	14	50 25.8 5.0
	1.56949	32	T.60166	36	0.39834	T.96783	8	13	
47	T.56980	31 32	T.60203	37	0.39797	1.96778	5	12	
49	T.57012	32	T.60240	37 36	0.39760	T.96772	5	II	
50	1.57044		T.50276		0.39724	¥.96767		10	5 4
		31		37			5		6 0.5 0.4
51	1.57075	32	T.60313	36	0.39687	¥.96762	5	9	7 0.6 0.5 8 0.7 0.5
52	1.57107	31	T.60349	37	0.39651	1.96757	5		8 0.7 0.5 9 0.8 0.6
53	1.57138	31	1.60386 T.60422	36	0.39614	T.96752	5	7	10 0.8 0.7
54	T.57169 T.57201	32	T.60422 T.60459	37	0.39578 0.39541	T.96747 T.96742	5	5	20 1.7 1.3
55 56	T.57232	31	I.60459	36	0.39541	1.96737	5	5	30 2.5 2.0
	1.57264	32	T.60532	37	0.39468	1.96732	5	3	40 3.3 2.7
57	1.57295	31	1.60568	36	0.39432	1.96727	5	2	50 4.2 3.3
59	I.57326	31 32	1.60605	37	0.39395	I.96722	5 5	Σ	
éa	1.57358	34	1.60641	30	C.39359	1.96717	3	8	
•	1000 000	-	lam ant	_	2000 4000	lan ala		,	
	log cos	a	log cot	c. d.	log tan	log sin	a	.	p. p.

22°

log sin	ы	log tan	c₁ d.	log cot	log cos	а		D D
¥ 57359		7.60643		0 20250	T 06717		Ka	
T. 57 180								
				0.30286			58	37 36
1.57451		1.60750	30	0.39250	7.96701		57	6 3.7 3.6
¥.57482		1.60786			T.96696		56	
¥.57514		1.60823	37	0.39177	T.96691	8	55	8 4.9 4.8
							54	9 5.6 5.4
T.57576			36					10 6.2 6.0
1.57007		1.60931	36	0.39069		6		20 12.3 12.0
	31		37	0.39033				30 18.5 18.0
1.57009		1.01004	-6	0.30990	1.90005		50	40 24.7 24.0 50 30.8 30.0
	31		30	0 - (-	8 .444.	5		30 1 30.0 1 30.0
1.57700	31		36	0.38900		5	49	
1.57731	31		36	0.30924		5	40	
	31		36	0.30000		5	4/	35
T. 57824	31					5		6 3.5
1.57855	31	1.61220	36	0.38780			3.6	
1.57885		1.61256	30	0.38744	1.96629		43	7 4.1 8 4.7
T.57916		T.61292		0.38708	T.96624	5	43	9 5.3
1.57947		1.61328		0.38672	1.96619		41	10 5.8
1.57978	31	T.61364		0.38636	1.96614		40	20 11.7
	30		36			6		30 17.5
1.58008	27	T.61400	26	0.38600	1.96608	-	39	40 23.3
1.58039		T.61436			T.96603		38	50 29.2
1.58070				0.38528	1.96598		37	
1.58101				0.38492	1.96593		36	
		1.01544		0.38456		6		32 31
	30		36					6 3.2 3.1
	31		36			5		
	30					5		7 3.7 3.6 8 4.3 4.1
	31		35	0 38278		5		4.8 4.7
	30		36	5 30075	in good a	6		10 5.3 5.2
T 58214		T 61758		0 28242	T 06556		20	20 10.7 10.3
	31	1.61704				S		30 16.0 15.5
		T.61830	36			5		10 21.3 20.7
1.58406		1.61865			1.96541	5	26	50 26.7 25.8
T.58436		1.61901		0.38099	1.96535		25	
		T.61936	35				24	
		T.61972	36			5		
						6		10 29
	31		36					
1.50500		1.02079		0.37921	1.90509		20	7 3.5 3.4 8 4.0 3.9
7 -04-0	30		35	004	8 - (5		9 4.5 4.4
	30		36	0.37886		ñ		10 5.0 4.8
	30		35			5		20 10.0 9.7
	31		36			5		30 15.0 14.5
1.58730	30		35			5		40 20 1 19.3
1.58769		1.62292			1.96477		14	50 25.0 24.2
T.58799		1.62327		0.37673	T.96472		13	
T_58829		1.62362		0.37638	1.96467	5	12	
1.58859		T.62398		0.37602	T.96461		11	
1.58889		1.62433	.15	0.37567	1.96456		10	6 6
	30		35			5		6 0.6 0.5 7 0.7 0.6
	20	T.62468	26	0.37532	T.96451	ĸ	9	
				0.37496	1.96445			0.8 0.7 0 0 0.8
	30			0.37401		5	7	10 1.0 0.8
	30		35					210 2.0 1.7
	30	1.62645	36		T 06.124	5		30 3.0 2.5
	29	1.62680	35			5		40 4.0 3.3
		1.62715	35		1.96413		2	50 5.0 4.2
1.59158		T.62750		0.37250	T.96408		I	
1.59188	30	1.62785	35	0.37215	T.96403	5	D	
log cos	a	log cot	c. d.	log tan	log sin	a	,	p. p.
	I. 57358 I. 57389 I. 57482 I. 57481 I. 57482 I. 57451 I. 57451 I. 57565 I. 57566 I. 57607 I. 57607 I. 57703 I. 57937 I. 57937 I. 58008 I. 58039 I. 58040 I. 58436 I. 58446 I. 58447 I. 58446 I.	I. 57358 31 I. 57358 31 I. 57451 31 I. 57451 31 I. 57451 31 I. 57556 31 I. 57569 31 I. 57560 31 I. 57560 31 I. 57667 31 I. 57668 31 I. 57703 31 I. 57762 31 I. 57763 31 I. 57763 31 I. 57793 31 I. 57937 31 I. 57938 31 I. 57937 31 I. 57938 31 I. 57947 31 I. 58068 31 I. 58079 31 I. 58131 30 I. 58131 31 I. 58143 31 I. 58244	Y. 57358 31 Y. 60677 1.57480 31 Y. 60677 1.57480 31 Y. 60677 1.57480 31 Y. 60714 1.57481 31 Y. 60774 1.57481 31 Y. 60756 1.57543 31 Y. 60876 1.57563 31 Y. 60895 1.57563 1.60986 Y. 60977 1.57638 1.60931 Y. 60697 1.57669 31 Y. 60697 1.57763 1.60931 Y. 60677 1.57763 31 Y. 60697 1.57763 31 Y. 60497 1.57763 31 Y. 61400 1.57793 1.61122 Y. 57855 1.61202 Y. 57855 1.61220 1.57947 31 Y. 61400 1.58933 1.61436 Y. 5793 1.58903 1.61436 Y. 5793 1.58903 1.61436 Y. 57947 1.5120 Y. 58131 30 1.589	Y. 57358 31 Y. 60641 36 1.57480 31 Y. 60714 37 1.57480 31 Y. 60714 36 1.57481 31 Y. 60714 36 1.57482 31 Y. 60744 36 1.57543 31 Y. 60756 36 1.57543 31 Y. 60855 36 1.57563 31 Y. 60855 36 1.57669 31 Y. 60957 36 1.57063 31 Y. 60957 36 1.57063 31 Y. 60957 36 1.57070 31 T. 61040 36 1.57783 31 T. 61040 36 1.57793 31 T. 61122 36 1.57985 30 T. 61220 36 1.579247 31 T. 61220 36 1.579278 31 T. 61430 36 1.58131 30 T.61437 36 1.58131 30	Y. 57358 31 Y. 60641 36 0.39359 Y. 57358 31 Y. 606714 36 0.39250 Y. 57359 31 Y. 60714 36 0.39250 Y. 57545 31 Y. 60756 36 0.39214 Y. 57545 31 Y. 60756 36 0.39214 Y. 57576 31 Y. 60959 36 0.39141 Y. 57576 31 Y. 60959 36 0.39030 Y. 57760 31 Y. 60969 37 0.39059 Y. 57703 31 Y. 61040 36 0.39033 Y. 57763 1 Y. 61040 36 0.38950 Y. 57793 1 Y. 61144 36 0.38744 Y. 57855 31 Y. 61222 36 0.38768 Y. 57947 31 Y. 61346 36 0.38660 Y. 57947 31 Y. 61346 36 0.38636 Y. 57947 31 Y. 61346 36 0.38636 <	I. 57358 31 T. 60641 36 0.39359 I. 96717 I. 573480 31 T. 60774 37 0.39326 T. 96701 I. 57348 31 T. 60774 36 0.39326 T. 96701 I. 57348 31 T. 60833 36 0.39214 T. 96686 I. 57576 31 T. 60835 36 0.39035 T. 96686 I. 57763 T. 610240 36 0.39035 T. 96686 I. 57763 T. 61026 37 0.38966 T. 96685 I. 57763 T. 61026 36 0.38966 T. 96685 I. 57763 T. 61148 36 0.38924 T. 96635 T. 57762 T. 61148 36 0.38924 T. 96635 T. 57762 T. 61148 36 0.38946 T. 96635 T. 57762 T. 61148 36 0.38744 T. 96635 T. 57825 T. 61148 36 0.38744 T. 96634 T. 57828 T. 61148 36 0.3	I.S7388 31 I.60641 36 0.39359 I.96717 6 I.S7480 31 I.60750 37 0.39328 I.96706 5 I.S7482 31 I.60750 36 0.39328 I.96706 5 I.S7543 31 I.60780 37 0.39328 I.96706 5 I.S7543 31 I.60895 36 0.39037 I.96665 5 I.S7545 31 I.60895 36 0.39038 I.96665 5 I.S7669 31 I.60895 36 0.39038 I.96665 5 I.S7703 31 I.61142 36 0.38960 I.96659 5 I.S7793 31 I.61142 36 0.38785 I.96638 5 I.S7793 31 I.61220 36 0.38786 I.96649 5 I.S79743 I.61242 36 0.38785 I.96638 5 5 I.S79743 I.61242 36	1 1

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,	log sin	а	log tan	c. d.	log cot	log cos	а		p. p.
							-		
13	T.59188	30	1.62785	35	0.37215	1.96403	6	60	
1	¥.59218	30	1.62820	35	0.37180	T.96397	5	59	
	1.59247		T.62855		0.37145	¥.96392		58	86 85
3	I.59277	30	1.62890	35	0.37110	1.96387	5	57	6 3.6 3.5
4	1.59307	30	T.62926	36	0.37074	T.96381		56	7 6.2 4.1
5	T.59336	29	1.62961	35	0.37039	¥.96376	5	55	7 4.2 4.1 H 4.8 4.7
8	T.59366	30	1.62996	35	0.37004	1.96370	6	54	
	¥.59396	30	¥.63031	35	0.36060	1.96365	5	53	9 5.4 5.3 10 6.0 5.8
7	1.59425	29	T.63066	35	0.36934	1.96360	B	52	30 12.0 11.7
8	1.59455	30	1.63101	35	0.36899	1.96354	6	51	30 18.0 17.5
10	T.59484	58	T.63135	34	0.36865	I.96349	5	50	411 24.0 23.3
	1.33404	30	1103133	35	0130003		6	50	50 30.0 29.2
		30	= (33		*			30 1 30.0 1 09.5
11	1.59514	20	1.63170	35	0.36830	1.96343	5	49	
12	I.59543	30	T.63205	35	0.36795	1.96338	5	48	
13	I.59573	20	T.63240	35	0.36760	T.96333	6	47	
14	1.59602	30	1.63275	35	0.36725	1.96327	5	46	84
15	1.59632	20	T.63310	35	0.36690	T.96322	6	45	6 3.4
16	1.59661	29	T.63345	34	0.36655	T.96316	8	101	7 4.0
17	1.5969	30	T.63379	35	0.36621	1.96311	6	43	
	1.59720	20	1.63414	35	0.36586	1.96305	5	42	9 5.1
19	I.59749	29	T.63449	35	0.36551	T.96300	6	41	10 5.7
20	ī.59778	-9	T.63484	00	0.36516	T.96294		AD.	20 11.3
		30		35			5		30 17.0
21	1.59808		1.63519		0.36481	T.96289		39	10 22.7
22	1.59837	29	T.63553	34	0.36447	T.96284	56	38	50 28.3
23	1.59866	2,	T.63588	35	0.36412	T.06278		37	
24	1.59895	29	T.63623	35	0.36377	1.96273	5	36	
25	1.59924	29	I.63657	34	0.36343	1.96267		35	
26	T.59954	30	T.63692	35	0.36308	1.96262	5	34	80 29
27	1.59983	29	I.63726	34	0.36274	1.96256	6	33	6 3.0 2.9
28	1.60012	33	1.63761	35	0.36239	1.96251	5	32	
20	1.60041	29	T.63796	35	0.36204	1.96245	6	31	7 3.5 3.4 B 4.0 3.9
30	1.60070	20	T.63830	34	0.36170	1.96240	5	30	9 4.5 4.4
NO I	2.00070	-	1.03030		0.30170	1.90540	6	30	10 5.0 4.8
		29	= / 0/	35			0		20 10.0 9.7
31	T.60099	20	1.63865	34	0.36135	1.96234	5	29	30 15.0 14.5
32	1.60128	20	1.63899	35	0.36101	1.96229	5	28	40 20.0 19.3
33	1.60157	29	T.63934	34	0.36066	1.96223		27	50 25.0 24.2
34	1.60186	20	T.63968	35	0.36032	1.96218	56	26	30 1 -3.0 1 -4.4
35	1.60215	20	T.64003	34	0.35997	T.96212		25	
36	1.60244	20	T.64037	35	0.35963	1.96207	56	24	
37	1.60273	20	1.64072	34	0.35928	T.96201	5	23	
38	1.60302	20	1.64106	34	0.35894	1.96196	6	22	28
30	T.60331	28	T.64140	35	0.35860	1.96190	5	21	5 2.8
40	1.60359		I.64175		0.35825	¥.96185	-	20	7 3.3
		20		34			6		
41	1.60388		1.64209		0.35791	1.96179	-	19	9 4.2
42	1.60417	29	T.64243	34	0.35757	T.96174	5	18	10 4.7
43	1.60446	28	I.64278	35	0.35722	T.96168	6	17	20 9.3
84	1.60474		1.64212	34	0.35688	T.96162		16	30 14.0
45	T.60503	20	T.64346	34	0.35654	T.96157	56	15	40 18.7
46	1.60532	29	1.04381	35	0.35619	1.96151		14	50 23.3
47	1.60561	29	T.64415	34	0.35585	1.96146	56	13	
48	1.60589	28	T.64449	34	0.35551	T.96140		12	
40	1.60618	29 28	T.64483	34	0.35517	T.96135	5	11	
50	1.60646	20	1.64517	34	0.35483	T.96129	0	10	6 5
		20		35			ő		5 0.6 0.5
51	1.60675		1.64552	00	0.35448	¥.96123	1.00	0	7 0.7 0.6
52	I.60704	20	T.64586	34	0.35414	T.96118	5	28	8 0.8 0.7
83	I.60732	28	T.64620	34	0.35380	1.96112	6	7	9 0.9 0.8
84	ī.60761	29	T.64654	34	0.35346	1.96107	5	6	10 1.0 0.8
	1.60780	28	1.64688	34	0.35312	I.96101	6	5	20 2.0 1.7
55 56	1.60709	29	1.64722	34	0.35312	T.06005	6		30 3.0 2.5
	1.60846	28	I.64722 I.64756	34	0.35270	T.96095	5	14	10 1.0 3.3
57 58	1.00840	29	1.04750	34	0.35244	1.96084	6	3	50 5.0 4.2
30	1.60075	28	T.64824	34	0.35210	I.96070	5	1	
50 60	T.60931	28	I.64858	34	0.351/0	I.96073	6	0	
	log cos	Б	log cot	c. d.	log tan	log sin	đ	1	p. p.

	log sin	a	log tan	c, d.	log cot	log cos	đ		p. p.
0	¥.60931		¥.64858		0.35142	¥.96073		60	
x	T.60960	RU	T.64892	34	0.35108	T.96067	6	59	
2	T.60988	28	T.04920	34	0.35074	T.96062	5	58	J4 33
8	T.61016	28	T.64960	34	0.35040	1.96056	6	57	6 3.4 3.3
14	T.61045	29 28	1.64994	34	0.35006	1.96050	5	56	7 4.0 3.9
5	1.61073	28	1.65028	34	0.34972	1.96045	6	55	
	T.61101	28	1.65062	34	0.34938	T.96039		54	9 5.1 5.0
7	T.61129	20	1.65096	34	0.34904	1.96034	5	53	10 5.7 5.5
0	T.61158 T.61186	28	T.65130 T.65164	34	0.34870 0.34836	T.96028 T.96022	6	52 51	20 11.3 11.0 30 17.0 16.5
10	I.61214	28	1.65197	33	0.34803	T.96017	5	50	40 22.7 22.0
		28	0100197	34		,,	6		50 28.3 27.5
11	1.61242	28	T.65231		0.34769	T.96011	6	40	
12	1.61270	20	T.65265	34	0.34735	T.96005		48	
1,3	1.61298	28	1.65299	34 34	0.34701	T.96000	5	47	
14	7.61326	28	T.65333	33	0.34667	T.95994	6	46	20
15	T.61354	28	1.65366	34	0.34634	1.95988	6	45	6 2.9
16 17	T.61382 T.61411	29	T.65400 T.65434	34	0.34600	T.95982 T.95977	56	44	7 3-4 1 3-9
17	T.61438	27	T.65467	33	0.34500	1.95977		43	9 4.4
10	T.61466	28	T.65501	34	0.34499	T.95965	6	41	10 4.8
20	T.61494	28	1.65535	34	0.34465	T.95960	5	40	283 9.7
	-	28		33			6		30 14.5
21	T.61522	28	T.65568	34	0.34432	T.95954	6	39	40 19.3
22	1.61550	28	T.65602	34	0.34398	1.95948	6	38	BW I adva
23	1.61578	28	T.65636	33	0.34364	T.95942		37	
24 25	T.61606 T.61634	28	T.65669 T.65703	34	0.34331	1.95937	5	36 35	
26	T.61662	28	I.65736	33	0.34297	T.95931 T.95925	6	35	28
27	T.61689	27	T.65770	34	0.34230	T.95920	5	33	6 2.8
28	1.61717	28 28	T.65770 T.65803	33	0.34197	1.95914	6	32	7 3·3 3·7
29	I.61745	28	3.65837	34	0.34163	1.95908	6	31	
30	1.61773		1.65870		0.34130	I.95902		30	9 4.2
	-	27		34			5		10 4.7
31	7.61800	28	T.65904	33	0.34096	T.95897	6	29	30 9.3 30 14.0
32	T.61828	28	T.65937	34	0.34063	1.95891	6	BB	40 18.7
33	T.61856 T.61883	27	¥.65971 ¥.66004	33	0.34029	T.95885	6	27 26	50 23.3
34 35	T.61011	28	T.66038	34	0.33996	T.95879 T.95873	6	25	
36	1.61939	28	T.66071	33	0.33929	1.95868	56	24	
37	1.61966	27	T.66104	33	0.33896	1.95862		23	
38	T.61994	28 27	1.66138	34 33	0.33862	1.95856	6	22	27
39	1.62021	28	1.66171	33	0.33829	T.95850	6	21	6 ' 2.7
10	¥.62049		1.66204		0.33796	T.95844		80	7 3.2 8 3.6
		27		34			5		o 3.0 ₽ 4.1
41	1.62076	28	T.66238	33	0.33762	T.95839	6	19	10 4.5
42	T.62104 T.62131	27	T.66271 T.66304	33	0.33729	T.95833 T.95827	6	17	20 9.0
43	1.62131	28	T.66337	33	0.33696 0.33663	I.95827 I.95821	6	16	30 13.5
45	T.62186	27	1.66371	34	0.33629	1.95815	6	15	40 18.0
46	T.62214	28	1.66404	3.3	0.33596	1.95810	5	14	50 22.5
47	1 62241	27 27	T.66437	33	0.33563	1.95804	6	13	
48	1.62268	28	1.66470	33	0.33530	1.95798	6	12	
49	¥.62296	27	1.66503	34	0.33497	1.95792	6	11	015
50	I.62323		T.66537		0.33463	1.95786	5	IC	6 0.6 0.5
51	T.62350	27	1.66570	33	0.33430	T.95780			7 0.7 0.6
52	T.62377	27	I.66603	33	0.33430	1.95775	5	8	8 0.8 0.7
53	1.62405	28	1.66636	33	0.23364	I.95769	6	7	9 0.9 2.8
54	1.62432	27 27	T.66669	33 33	0.33331	1.95763	6	6	10 1.0 0.8 20 2.0 1.7
55	1.62459	27	1.66702	33	0.33298	I.95757	6	5	30 3.0 2.5
56	1.62486	27	1.66735	33	0.33265	1.95751	ŭ	I	40 4.0 3.3
57 58	T.62513 T.62541	28	T.66768 T.66801	33	0.33232 0.33199	T.95745 T.95739	6	3	50 5.0 4.2
59	T.62568	27	1.66834	33	0.33199	T.95739	6	Í	
60	1.62595	27	1.66867	33	0.33133	I.95728	E	0	
_									
	log cos	Б	log cot	c. d.	log tan	log sin	Б	1	p. p.

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,	log sin	đ	log tan	c. d.	log cot	log cos	а		p. p.
0	T.62595		1.66867		0.33133	I.95728		60	-
1	1.62622	27	1.66900	33	0.33100	¥.95722	6	59	
i i	1.62649	27	T.66933	33	0.33067	1.95716	6	58	33 32
8	1.62676	27	1.66966	33	0.33034	1.95710	6	57	6 3.3 3.2
14	¥.62703	27	T.66999	33	0.33001	1.95704	6	56	7 3.9 3.7 8 4.4 4.3
5	T.62730	27	1.67032	33	0.32968	T.95698	6	55	
	T.62757 T.62784	27	T.67065 T.67098	33	0.32935	T.95692 T.95686	ē	54 53	9 5.0 4.8 10 5.5 5.3
7	T.62811	27	1.67131	33	0.32869	I.95680	6	53	20 11.0 10.7
0	T.62838	27	1.67163	32	0.32837	1.95674	6	51	30 16.5 16.0
10	1.62865	27	1.67196	33	0.32804	1.95668		50	40 22.0 21.3
		27		33			5		50 27.5 26.7
II	1.62892	26	1.67229	33	0.32771	1.95663	6	49	
12	T.62918 T.62945	27	T.67262	33	0.32738	T.95657 T.95651	б	48	
13 14	I.62945	27	T.67295 T.67327	32	0.32673	1.95645	6	47	27
15	T.62999	27	1.67360	33	0.32640	T.95639	6	45	6 2.7
16	1.63026	27 26	T.67393	33	0.32607	1.95633	6	44	7 3.2
17	1.63052	20	1.67426	33 32	0.32574	1.95627	6	43	
18	1.63079	27	I.67458	33	0.32542	1.95621	6	42	9 4.1
19	T.63106 T.63133	27	T.67491 T.67524	33	0.32509	T.95615 T.95609	6	4I 40	10 4.5
-	1.03133	26	1.0/324	32	0.344/0	1.93009	6	40	30 13.5
21	1.63159		1.67556		0.32444	1.95603		39	40 18.0
22	T.63186	27	T.67589	33	0.32411	T.95597	6	38	50 22.5
23	1.63213	27 26	1.67622	33 32	0.32378	T.95591	6	37	
24	T.63239	20	T.67654	32	0.32346	1.95585	6	36	
25	1.63266	26	1.67687	32	0.32313	1.95579	6	35	26
26	T.63292 T.63319	27	T.67719 T.67752	33	0.32281	Ī.95573 Ī.95567	6	34	6 2.6
27	T.63345	26	T 67785	33	0.32215	I.95561	6	33	
20	T.63372	27	T.67785 T.67817	32	0.32183	1.95555	6	31	7 3.0 B 3.5
30	T.63398	26	T.67850	33	0.32150	T.95549	ő	30	9 3.9
-	1.00	27		32			6		10 4.3 100 8.7
31	1.63425	26	1.67882	33	0.32118	1.95543	6	29	200 8.7 30 13.0
32	1.63451	27	1.67915	32	0.32085	Ī.95537	6	28	40 17.3
33 34	T.63478 T.63504	26	T.67947 T.67980	33	0.32053	T.95531 T.95525	6	27 26	50 21.7
34	T.63531	27	1.68012	32	0.31988	1.95525 1.95519	6	25	
36	1.63557	26 26	1.68044	32	0.31956	1.95513	6	24	
37	1.63583	20	1.68077	33	0.31923	1.95507	7	23	_
38	I.63610	26	1.68109	33	0.31891	1.95500	6	22	7
39	T.63636	26	T.68142 T.68174	32	0.31858	T.95494	6	21	E 0.7 7 0.8
40	1.63662	27	1.00174	32	0.31020	¥.95488	6	20	7 0.8 8 0.9
41	T.63689		1.68206	32	0.31794	¥.95482		10	0 0.9 0 I.I
41	1.63069	26	T.68230	33	0.31794	1.95402 1.95476	6	19 18	10 1.2
43	1.63741	26	1.68271	32	0.31729	I.95470	6	17	20 2.3
44	T.63767	26 27	T.68303	32 33	0.31697	1.95464	ő	16	30 3.5
45	T.63794	26	T.68336	33	0.31664	T.95458	6	15	40 4.7 E0 5.8
46	T.63820 T.63846	26	T.68368 T.68400	32	0.31632	1.95452 X 05446	6	14	201 3.0
47	1.03840 1.63872	26	1.08400	32	0.31000	T.95446 T.95440	6	13	
40	T.63898	26	1.68465	33	0.31508	T.95440	16	12	
50	1.63924	26	I.68497	32	0.31503	I.95427	7	IO	6 5
		26		32			ň		6 0.6 0.5
51	T.63950	26	1.68529	32	0.31471	1 95421	6	o	7 0.7 0.6 8 0.8 0.7
52	1.63976	20	1.68561	34	0.31439	T.95415	6	8	8 0.8 0.7 9 0.9 0.8
53	T.64002 T.64028	26	T.68593 T.68626	33	0.31407	T.95409	6	7	10 1.0 0.8
54 55	T.64054	26	1.68658	32	0.31374 0.31342	¥.95403 1.95397	6	5	20 . 2.0 1.7
56	1.64080	26	T.68690	32	0.31310	T.95397	6	4	30 3.0 2.5
57	T.64106	26	T.68722	32	0.31278	1.95384	7	3	40 4.0 3.3
58	T.64132	20	¥.68754	32	0.31246	¥.95378	6	2	50 5.0 4 2
50	T.64158 T.64184	26	1.68786 1.68818	32	0.31214	T.95372	6	1	
00	1.04184		1.06818		0.31182	1.95366		0	
	log cos	đ	log cot	c. d.	log tan	log sin	đ	1	p. p.
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	log sin	а	log tan	cd.	log cot	log cos	а		p. p.
0	T.64184		T.68818		0.31182	1.95366		60	
1	1.64210	26	1.68850	32	0.31150	T.95360	6	59	
2	1.64236	26	T.68882	32	0.31118	T.95354	6	58	32 31
	1.64262	26	T.68914	32	0.31086	1.05348	6	57	6 3.2 3.1
A	1.64288	26	T.68946	32	0.31054	1.95341	76	56	
5	T.64313	25	T.68978	32	0.31022	1.95335	0	55	7 3.7 3.6 8 4.3 4.1
6	T.64339	26	T.60010	32	0.30990	1.95329	6	54	9 4.8 4.7
7	1.64365	26	1.60042	32	0.30958	T.95323	6	53	:0 5.3 5.2
8	1.64391	26	T.69074	32	0.30926	1.95317	6	52	20 10.7 10.3
8	T.64417	26	T.69106	32	0.30894	1.95310	7	51	30 16.0 15.5
10	T.64442	25	T.69138	32	0.30862	T.95304	0	50	40 21.3 20.7
		26		32			6		50 26.7 25.8
11	T.64468	26	T.69170	32	0.30830	¥.95298	6	49	
12	T.64494	25	T.69202	32	0.30798	T.95292	6	48	
13	1.64519	26	T.69234	32	0.30766	T.95286	7	47	
14	T.64545	26	T.69266	32	0.30734	T.95279	6	46	26
15	1.64571	25	1.69298	31	0.30702	T.95273	6	45	6 2.6
16	1.64596	26	T.69329	32	0.30671	1.95267	6	44	7 3.0
17	T.64622	25	T.69361	32	0.30639	T.95261	7	43	
18	1.64647	26	T.69393	32	0.30607	1.95254	6	42	9 3.9
10	I.64673	25	T.69425	32	0.30575	T.95248	6	41	10 4.3 20 8.7
20	T.64698		T.69457	-	0.30543	T.95242		40	30 13.0
	= (26	T (. 00	31			б		40 17.3
21	T.64724	25	1.69488	32	0.30512	¥.95236	7	39	50 21.7
22	1.64749	26	T.69520	32	0.30480	1.95229	6	38	30 1 01.1
23	T.64775	25	T.69552	32	0.30448	¥.95223	6	37	
24	1.64800	26	T.69584	31	0.30416	1.95217	6	36	
25	I.64826	25	1.69615	32	0.30385	1.95211		35	0.6
26	1.64851	26	T.69647	32	0.30353	T.95204	7 6	34	25
27	T.64877	25	1.69679	31	0.30321	1.95198	6	33	2.5
28	T.64902	25	1.69710	32	0.30290	1.95192		32	7 2.9
29	1.64927	26	T.69742	32	0.30258	1.95185	76	31	
30	¥.64953		1.69774		0.30226	1.95179		30	10 3.8 10 4.2
31	T.64978	25	T.69805	31	0.00000	Torres	б		10 4.2 20 8.3
32	T.65003	25	1.69837	32	0.30195	T.95173 T.95167	6	28	30 12.5
33	I.65020	26	1.69868	31	0.30103	T.95160	7		40 16.7
34	T.65054	25	T.69900	32	0.30132	1.95154	6	27	50 20.8
35	T.65079	25	1.69932	32	0.30068	T.95154	6	25	
36	T.65104	25	T.69963	31	0.30037	T.95141	76	24	
37	1.65130	26	T.69995	32	0.30005	1.95135		23	
38	1.65155	25	I.70026	31	0.20074	I.95135	6	23	04
39	I.65180	25	1.70058	32	0.29942	T.95122	76	23	6 2.4
40	T.65205	25	1.70089	31	0.29911	I.95116	6	20	
	110,2003	25		32	5109911		6		8 3.2
61	1.65230	-	1.70121	-	0.29879	T.95110		19	5 3.6
42	T.65255	25	I.70152	31	0.29845	Ī.95103	7	18	10 4.0 20 8.0
43	1.65281	26	T.70184	32	0.29816	T.95097	6	17	
44	T.65306	25	1.70215	31	0.29785	T.95090	76	16	30 12.0
15	¥.65331	25	I.70247	32	0.29753	1.95084	0	15	
16	1.65356	25	1.70278	31	0.29722	T.95078		14	BD 20.0
47	1.65381	25	T.70309	31	0.29691	¥.95071	76	13	
18	T.65406	25	T.70341	32	0.29659	1.95065	6	12	
49	T.65431	25	1.70372	31	0.29628	T.95059		II	
50	T.65456	25	I.70404	32	0.29596	T.95052	2	10	7 6
		25		31			6		6 0.7 0.6 7 0.8 0.7
51	T.65481	26	1.70435	31	0.29565	T.95046		9	7 0.8 0.7 8 0.9 0.8
52	T.65506	25	1.70466		0.29534	T.95039	76	8	9 1.1 0.9
53	¥.65531	25	1.70498	32	0.20502	T.95033	6	76	10 1.2 1.0
54	T.65556	25	T.70529	31	0.29471	1.95027			20 2.3 2.0
55	1.65580	24	1.70560	31	0.29440	T.95020	7 6	5	30 3.5 3.0
56	1.65605	25	¥.70592	34	0.29408	T.95014		14	
57	1.65630	25 25	T.70623	31	0.29377	T.95007	76	U	40 4.7 4.0 50 5.8 5.0
28	1.65655	25	1.70654	31	0.29346	T.95001	6	2	001 310 1 310
100	T.65680	25	1.70685	32	0.29315	1.94995	7	I	
ha	¥.65705	-3	I.70717	0-	0.29283	1.94988	'	0	
	log cos	d	log cot	c. d.	log tan	log sin	a	,	p. p.

,	log sin	а	log tan	c. d.	log cot	log cos	d		p. p.
10	T.65705		1.70717		0.29283	1.94988		60	
1	1.65729	24	1.70748	31	0.29252	T.94982	6	59	
2	T.65754	25	I.70779	31	0.20221	T.94975	7	58	32 31
3	T.65779	25	1.70810	31	0.29190	T.04060	6	57	6 3.2 3.1
4	7.65804	25	1.70841	31	0.20159	T.94962	7	56	7 3.7 3.6
5	1.65828	24	1.70873	32	0.29127	T.94956	6	55	8 43 41
ő	T.65853	25	1.70904	31	0.29096	1.04949	7	54	4.8 4.7
	T.65878	25	T.70935	31	0.20065	T.94943		53	10 5.3 5.2
7	1.65902	24	1.70966	31	0.20034	1.94936	7	52	10.7 10.3
9	T.65927	25	T.70997	31	0.29003	¥.94930	7	51	30 16.0 15.5
10	T.65952	25	1.71028	31	0.28972	1.94923	1	50	40 21.3 20.7
		24		31			6		50 26.7 25.8
11	T.65976		1.71059		0.28041	1.94917	6	49	
12	7.66001	25	I.71000	31	0.28910	1.94911	6	48	
13	7.66025	24	1.71121	31	0.28879	T.94904	7	47	
14	1.66050	25	1.71153	32	0.28847	1.94898		46	30
15	1.66075	25	1.71184	31	0.28816	1.94891	7	45	6 3.0
16	T.66099	24 25	1.71215	31	0.28785	1.94885	7	14.4	7 3-5
17	1.66124	24	1.71246	31	0.28754	1.94878	7	43	
18	1.66148	25	1.71277	31	0.28723	1.94871	6	42	D 4.5
19	1.66173	24	1.71308	31	0.28692	T.94865	7	41	10 5.0
20	1.66197		1.71339		0.28661	1.94858		40	30 10.0
		24		31			6		30 15.0
21	1.66221	25	1.71370	31	0.28630	T.94852	7	39	40 2010 50 25.0
22	1.66246	24	1.71401	30	0.28599	T.94845	6	38	50 25.0
23	1.66270	25	1.71431	31	0.28569	1.94839	7	37	
24	T.66295	24	1.71462	31	0.28538	1.94832	6	36	
25 26	1.66319	24	1.71493	31	0.28507	T.94826	7	35	25 24
	T.66343	25	1.71524	31	0.28476	T.94819	7	34	
27 28	ī.66368 ī.66392	24	1.71555	31 .		T.94813 T.94806	7	33	
20	1.00392	24	1.71586 1.71617	31	0.28414	1.94800 1.94799	7	32	
30	T.66441	25	1.71648	31	0.28352	I.94799 I.94793	6	31 30	8 3.3 3.2 0 3.8 3.6
30	1.00441	24	1./1040	31	0.20352	1.94793	7	30	
31	1.66465		1.71679	-	0.28321	1.94786		20	10 4.2 4.0 10 8.3 8.0
31	1.00405 1.66489	24	1.71079	30	0.28321	1.94780 1.94780	6	29	30 12.5 12.0
32	ī.66513	24	1.71709	31	0.28291 c.28260	I.94780 I.94773	76	20	40 16.7 16.0
33	ī.66537	24	1.71771	31	0.28220	I.94773 I.94767		26	40 16.7 16.0 50 20.8 20.0
35	1.66562	25	Ī.71802	31	0.28198	I.94760	7	25	
36	T.66586	34	T.71833	31	0.28167	1.94753	76	24	
37	1.66610	24	1.71863	30	0.28137	1.94747		23	
38	T.66634	24 24	T.71894	31	0.28106	1.94740	76	22	2.8
39	T.66658	24 24	1.71925	31 30	0.28075	T.94734		21	6 2.3
40	1.66682	24	I.71955	30	0.28045	¥.94727	7	20	7 2.7
		24	-	31			7		
41	T.66706		1.71986		0.28014	Ī.94720		19	3.5
42	1.66731	25	1.72017	31	0.27983	I.94714	6	18	10 3.8
43	T.66755	24	1.72048	31	0.27952	1.94707	7	17	20 7.7
44	T.66779	24 24	T.72078	30 31	0.27922	Ī.94700	76	16	30 11.5
45	T.66803	24	T.72109	31	0.27891	1.94694	7	15	40 15.3
46	T.66827	24	1.72140	30	0.27860	1.94687		14	50 19.2
47	1.66851	24	1.72170	31	0.27830	T.94680	76	13	
48	1.66875	24	1.72201	30	0.27799	1.94674	7	12	
49	T.66899	23	1.72231	31	0.27769	1.94667	7	II	7 6
50	1.66922		1.72262		0.27738	1.94660		10	6 0.7 0.6
	211 1	24	_	31			6		
SI	1.66946	24	1.72293	30	0.27707	T.94654	7	U	7 0.8 0.7 8 0.9 0.8
52	T.66970	24	1.72323	31	0.27677	1.94647		8	g 1.1 0.9
53	T.66994 T.67018	2	1.72354	30	0.27646	¥.94640	7	7	E 1.2 1.0
54 55	I.07018 I.67042	24	I.72384	31	0.27616	1.94634	7		20 2.3 2.0
55	I.07042 I.67066	24	T.72415 T.72445	36	0.27585	T.94627 T.94620		5	30 3.5 3.0
57	T.67090	24	1.72445	31	0.27555	1.94020 1.94614	7 6	4	
57	1.67090 1.67113	23	1.72470	30	0.27524	1.94014 1.94607	7	2	40 4.7 4.0 50 5.8 5.0
59	1.67137	24	1.72537	31	0.27494	T.94607 T.94600	7	I	
60	1.67161	24	I 72567	30	0.27433	T.94593	7	ō	
	log cos	a	log cot	c. d.	log tan	log sin	á	1	p. p.

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,	log sin	а	log tan	c. d.	log cot	log cos	d		p. p.
0	1.67161		1.72567		0.27433	T.94593	6	60	
1	T.67185	24	I.72598	31 30	0.37403	1.94587	7	59	
2	1.67208	24	1.72628	31	0.27372	1.94580	2	58	31 50
3	1.67232	24	1.72659	30	0.27341	T.94573	6	57	6 3.1 30
8	1.67256	24	7.72689	31	0.27311	T.94567	7	56	7 3.6 3.5
5	1.67280	23	¥.72720	30	0.27280	T.94560	7	55	
	T.67303 T.67327	24	T.72750 T.72780	30	0.27250 0.27220	T.94553	7	54	0 B-7 4-5 10 5-2 5-0
7	I.67327 I.67350	23	1.72700	31	0.27180	T.94546 T.94540		53 52	10 5.2 5.0 20 10.3 10.0
0	1.67374	24	1.72841	30	0.27159	T.94533	7	54	30 15.5 15.0
10	1.67398	24	1.72872	31	0.27128	1.94526	7	50	40 20.7 20.0
-		23		30			7		50 25.8 25.0
11	T.67421		1.72002		0.27098	1.94519	6	180	
12	1.67445	24	1.72932	30	0.27068	T.94513		48	
13	1.67468	23 24	1.72963	31	0.27037	1.94506	777	47	•
14	T.67492	23	Ī.72993	30	0.27007	T.94499	7	46	19
15	1.67515		T.73023	31	0.26977	1.94492		45	6 2.9
16	1.67539	23	T.73054	30	0.26946	I.94485	76	44	7 3.4 8 3.9
17	T.67562 T.67586	24	T.73084	30	0.26916	T.94479 T.94472	7	43	
10	1.07500 T.67600	23	T.73114 T.73144	30	0.20856	1.94472 T.94465	7	42	9 4.4
20	I.67633	24	I.73144 I.73175	31	0.26825	T.94405 T.94458	7	41	10 4.0
	10/000	23		30		1.944.55	7	40	30 14.5
21	1.67656	-	1.73205	-	0.26795	T.94451		39	10 19.3
22	1.67680	24	T.73235	30	0.26765	T.94445	6	38	50 24.2
23	T.67703	23	1.73265	30	0.26735	1.94438	7	37	
24	1.67726	23	T.73295	30	0.26705	1.94431	7	36	
25	1.67750	24 23	1.73326	31 30	0.26674	T.94424	7	35	
26	I.67773	23	T.73356	30	0.26644	1.94417		34	24 219
27	1.67796	24	1.73386	30	0.26614	1.94410	76	33	2.4 2.3
26	1.67820	23	T.73416	30	0.26584	1.94404	7	32	7 B.8 2.7 8 3.2 3.1
202	T.67843 T.67866	23	1.73446	30	0.26554	I.94397	ź	31	
30	1.07800		¥.73476		0.20524	T.94390		30	3.6 3.5 10 4.0 3.8
	T.67890	24	TRAFAT	31	0.06.000	Tarage	7		10 4.0 3.8 20 8.0 7.7
31	I.67913	23	1.73507	30	0.26493	1.94383	7	29 28	30 1210 11.5
32 33	T.67936	23	T.73537 T.73567	30	0.26433	T.94376 T.94369	7	27	40 16.0 15.3
34	1.67959	23	T.73597	30	0.26403	T.94362	7	26	50 20.0 19.2
35	1.67082	23	I.73627	30	0.26373	1.94355	7	25	
36	T.67982 T.68006	24	1.73657	30	0.36343	T.94349	6	24	
37	1.68029	23	1.73687	30	0.26313	1.94342	7	23	
38	T.68052	23	1.73717	30 30	0.26283	T.94335	2	22	22
39	1.68075	23	1.73747	30	0.26253	T.94328	7	21	6 2.2
40	1.68098		1.73777		0.26223	T.94321		20	7 2.6 8 2.9
	- 10	23		30			7		
41	1.68121	23	1.73807	30	0.26193	1.94314	7	19	9 3.3 10 3.7
42	1.68144	23	T.73837	30	0.26163	I 94307	7	18	10 3.7 IMI 7.3
43	T.68167 T.68190	23	I.73867	30	0.26133	T.94300	2	17	30 11.0
45	1.68213	23	I.73897 I.73927	30	0.20103	T.94293 T.94286	7	10	40 14.7
45	1.68237	24	I.73927 I.73957	30	0.26043	1.94200 T.94279	7	14	50 18.3
47	T.68260	23	T.73987	30	0.26013	1.94273		13	
48	1.68283	23	T.74017	30	0.25983	1.94266	7	12	
40	1.68305	22	1.74047	30 30	0.25953	T.94259	7	11	
50	1.68328		T.74077	-	0.25923	1.94252	7	10	7 6
		23		30			7		0 0.7 0.6
51	1.68251	23	T.74107	30	0.25893	1.94245	7	5	7 0.8 0.7 8 0.9 0.8
52	1.68374	23	1.74137	20	0.25863	1.94238	7	8	8 0.9 0.8 9 1.1 0.9
53	1.68397	23	T.74166	30	0.25834	¥.94231	ź	7	10 1.2 1.0
54	T.68420 T.68443	23	1.74196	30	0.25804	1.94224	2	6	20 2.3 2.0
55 56	1.08443	23	T.74226 T.74256	30	0.25774	I.94217 I.04210	7	8	30 3.5 3.0
50	1.68489	23	1.74250	30	0.25744	1.94210 T.04203	7	3	
57	1.68512	23	1.74200	30	0.25684	T.94203 T.94196	7	3	40 4.7 4.0 E0 5.8 5.0
59	I.68534	22	1.74345	29	0.25655	1.94189	7	i	
60	1.68557	23	1.74375	30	0.25625	1.94182	7	o	
	log cos	a	log cot	c. d.	log tan	log sin	a		
			100 000	ter the	TON LOLL	IVE BILL	14		p. p.

1	log sin	d	log tan	c. d.	log cot	log cos	d		p. p.
0	1.68557		T.74375		0.25625	1.04182	-	60	
1	T 68580	23	1.74375	30	0.25595	T.94175	7	59	
2	7.68603	23	I.74435	30	0.25565	1.04168	7	58	30
3	1.68025	22	T.74465	30	0.25535	1.94161	7	57	5 3.0
H	1.68648	23	T.74494	29	0.25506	T.94154	7	56	7 3.5
5	1.68671	23 .	T.74524	30	0.25476	1.94147	7	55	
	ï.68694	22	1.74554	20	0.25446	Ĩ.04140	7	54	9 4.5
7 8	1.68716	23	Ī.74583	30	0.25417	T.94133	7	53	10 5.0
	Ī.68739	23	1.74613	30	0.2538?	T.94126	7	52	20 10.0
9	I.68762 I.68784	22	T.74643 T.74673	30	0.25357	T.94119 T.94112	7	51	30 15.0 40 20.0
10	1.00/04	23	1./40/3	29	0.65367	1.94112	7	30	50 25.0
II	T.68807		1.74702	29	0.25298	1.94105		49	30 1 - 310
12	T.68820	22	1.74732	30	0.25268	T.94098	78	49	
13	1.68852	23	1.74762	30	0.25238	Ĩ.94090		47	
14	T.68875	23	1.74791	29	0.25209	1.94083	7	46	29
15	I.68897	22	1.74821	30	0.25179	T.94076	7	45	fi 2.9
16	1.68920	23 22	1.74851	30 29	0.25149	T.94069	7	44	7 3.4
17	1.68942	23	1.74880	30	0.25120	Ī.94062	7	43	
18	T.68965	22	1.74910	20	0.25090	1.94055	7	42	9 4.4
19	1.68987	23	Ī.74939	30	0.25061	1.94048	7	41	10 4.8
20	1.69010		₹.74969		0.25031	Ī.9404 I	100	40	9.7 20 14 5
		22		29		-	7		30 14.5 40 19.3
21	¥.69032	23	T.74998	30	0.25002	1.94034	7	39	50 24.2
22	1.69055	22	1.75028	30	0.24972	1.94027		38	20 1 -41-
23	T.69077	23	1.75058	29	0.24942	Ĩ.94020	78	37	
24 25	1.69100 1.69122	22	I.75087 I.75117	30	0.24913 0.24883	1.94012 1.94005	7	36 35	
26	Ī.69144	22	1.75146	29	0.24854	T.93998	7	34	23
27	1.69167	23	1.75176	30	0.24824	T.93991	7	33	6 2.3
188	T.69189	22	1.75205	29	0.24795	1.93984	7	32	7 2.7
20	1.69212	23 22	1.75235	30	0.24765	1.93977	7	31	
30	T.69234	66	1.75264	29	0.24736	1.93970	7	30	9 3.5
		22		30			7		10 3.8
31	T.69256	23	1.75294	20	0.24706	T.93963	8	29	285 7.7
32	1.69279	23	1.75323	30	0.24677	1.93955	7	28	30 11.5 40 15.3
33	1.69301	22	1.75353	20	0.24647	T.93948	7	27	50 19.2
34	1.69323	22	1.75382	20	0.24618	1.93941	7	26	30 1 .9.5
35 .	T.69345 T.69368	23	Ĩ.754II	30	0.24589	1.93934	7	25 24	
36 37	Ī.69390	22	Ī.75441 Ī.75470	29	0.24559	Ī.93927 T.93920	78	23	
38	T.69412	22	1.75500	30	0.24500	1.93912		22	22
39	T.69434	22	I.75529	29	0.24471	1.93905	7	21	6 2.2
40	1.69456	22	I.75558	29	0.24442	T.93898	7	20	7 2.6
		23		30			7		
41	T.69479	-	1.75588		0.24412	T.93891		19	9 3.3
42	1.69501	22 22	T.75617	29	0.24383	1.93884	78	18	10 3.7
43	1.69523	22	1.75647	30	0.24353	1.93876		17	20 7.3 30 11.0
44	ī.69545	22	1.75676	29	0.24324	T.93869	7	16	30 11.0 40 14.7
45	T.69567	22	T.75705	30	0.24295	1.93862		15	50 18.3
46	1.69589	22	1.75735	29	0.24265	1.93855	78	14	30 1 .0.3
4"	T.69611 T.69633	22	I.75764	29	0.24236	T.93847 T.93840	7	13 12	
48	1.09033 1.69655	22	Ī.75793 Ī.75822	29	0.24207	1.93840 T.93833	7	12	
50	1.69655	22	1.75852	30	0.24148	T.93826	7	10	- 8 7
		22		20		1.930.00	7		6 0.8 0.7
51	1.60600		1.75881		0.24110	1.93819		U	7 0.9 0.8
52	T.69721	22	1.75910	20	0.24090	1.93811	8	8	
53	1.69743	22	Ī.75939	29	0.24061	1.93804	7	7	9 1.2 1.1
54	1.69765	22	T.75969	30	0.24031	1.93797	78	6	10 1.3 1.2
55	1.69787	22	T.75998	20	0.24002	T.93789		5	20 2.7 2.3 30 4.0 3.5
56	1.69809	22	I.76027	29	0.23973	1.93782	7	4	
57	T.69831	22	1.76056	30	0.23944	1.93775		3	40 5.3 4.7 50 6.7 5.8
58	T.69853	22	1.76086	30	0.23914	1.93768	78	2	30 1 0.7 1 3.0
59	1.69875 1.69897	22	T.76115 T.76144	29	0.23885	I.93760 I.93753	7	1	
	1.0909/		1.70144		0.23030	1.93753			

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8	1			-		1			
	log sin	а	log tan	e. jd.	log cot	log cos	đ		p. p.
ø	1.60807		T.76144		0.23856	T.93753		60	
1	1.69010	22	I.76173	29	0.23827	T.93746	78	59	
2	T.6994"	22	1.76202	29	0.23798	T.93738		58	30 29
3	1.60063	22	1.76231	29	0.23769	I.93731	7	57	6 3.0 2.9
14	T.60084	21	1.76261	30	0.23739	T.93724	7	56	
5	T.70006	22	1.76200	29	0.23710	T.93717	78	55	7 3.5 3.4 8 4.0 3.9
5	1.70028	22	1.76319	29	0.23681	T.93709		54	9 4.5 4.4
78	T.70050	22	T.76348	29 29	0.23652	T.93702	7	53	10 5.0 4.8
8	¥.70072	21	1.76377	29	0.23623	1.93695	78	52	20 10.0 9.7
9	T.70093	22	1.76406	29	0.23594	T.93687	7	51	30 15.0 14.5
10	1.70115		I.76435		0.23565	T.93680	1000	20	40 20.0 19.3
		22		29			7		50 25.0 24.2
II	T.70137	22	1.76464	29	0.23536	T.93673	8	30	
12	1.70159	21	T.76493	29	0.23507	T.93665		48	
13	1.70180	22	I 76522	20	• 0.23478	1.93658	78	47	
14	1.70202	22	T.76551	20	0.23449	I.93650	7	46	28
15	1.70224	21	I.76580	20	0.23420	I.93643	7	45	E 2.8
16	1.70245	22	I.76609	30	0.23391	I.93636	78	44	7 3.3
17	I.70267 I.70288	21	T.76639	29	0.23361	T.93628 T.93621	7	43	
10	I.70288 T.70310	22	I.76668 I.76697	20	0.23332	1.93021 1.93614	78	42 41	9 4.2 10 4.7
20		22		28		1.93606	8	41	
20	1.70332	21	T.76725	29	0.23275	1.93000	-	40	10 9.3 30 14.C
21	*	21	×	-9		Touros	7		18.7
21	1.70353	22	T.76754	29	0.23246	T.93599	8	39	30 23.3
23	T.70375 T.70396	21	1.76783 1.76812	29	0.23217	T.93591 T.93584	7	38	
24	I.70390 I.70418	22	1.70812 1.76841	99	0.23100	I.93504 I.93577	78	37 36	
25	1.70418	21	1.76870	29	0.23130	T.93569		35	
26	1.70461	22	1.76899	29	0.23101	T.93562	78	34	22
27	1.70482	21	1.76928	29	0.23072	1.93554		33	6 2.2
28	1.70504	22	T.76957	29	0.23043	1.93547	78	32	
20	T.70525	21	1.76986	29	0.23014	T.93539		31	7 2.6
30	1.70547	22	1.77015	29	0.22985	T.93532	7	30	B 3.3
		21		20			7		R0 3.7
31	1.70568		T.77044		0.22056	7.93525	8	20	20 7.3
32	1.70590	22	1.77073	29	0.22027	1.03517		28	30 II.O ,
33	1.70611	21	T.77101	28	0.22899	1.93510	7	27	NO 14.7
34	1 70633	22	T.77130	30 20	0.22870	T.93502		26	50 18.3
35	I.70654	21	I.77159	19	0.22841	T.93495	78	25	
36	1.70675	22	1.77188	29	0.22812	¥.93487		24	
37	1.70697	21	1.77217	29	0.22783	1.93480	78	23	21
38	1.70718	21	1.77246	28	0.22754	T.93472	7	22	
39	T.70739	22	T.77274	29	0.22726	I.93465	8	21	0 2.1 7 2.5
40	1.70761		¥.77303		0.22697	Ĩ.93457		20	7 2.5 8 2.8
		21		29		-	7		3.2
41	I.70782	21	1.77332	29	0.22668	T.93450	8	19	10 3.5
42	1.70803	21	T.77361	29	0.22639	T.93442		18	2) 7.0
43	I.70824 I.70846	22	1.77390	28	0.22610	T.93435 T.93427	8	17 16	30 10.5
44	1.70840	21	I.77418 I.77447	29	0.22582	1.93427 1.93420	78	10	40 14.0
45	I.70807 I.70888	21	1.77447	29	0.22553	I.93420 I.93412		15	50 17.5
47	T.70909	21	I.77505	29	0.22495	T.93405	78	13	
48	T.70931	22	I.77533	28	0.22467	T.93397		12	
NO.	1.70952	21	I.77562	29	0.22438	T.93390	78	11	
50	I.70973	21	I.77591	29	0.22409	T.93382	8	10	8 7
		21		28			7		6 0.8 0.7
51	T.70094		1.77619		0.22381	T.93375		9	7 0.9 0.8
52	1.71015	21	1.77648	20	0.22352	T.93367	8		
53	1.71036	21	1.77677	29	0.22323	T.93360	78	7	9 1.2 1.1
	1.71058	22	1.77706	20 28	0.22294	T.93352	8		10 1.3 1.2
54	1.71079	21	¥.77734	20	0.22266	T.07344		5	20 2.7 2.3
54 55			1.77763	100	0.22237	T.93337	78	4	30 4.0 3.5
54 55 56	T.71100	28	Tannos	20	0.22209	1.93329		3	40 5.3 4.7 50 6.7 5.8
54 55 56 57	1.71100 1.71121	21	Ī.77791			T.93322	/	2	
54 55 56 57 58	T.71100 T.71121 T.71142	21 21 21	1.77820		0.22180		8		30 1 0.7 1 3.0
54 55 56 57 58 59	T.71100 T.71121 T.71142 T.71163	21 21	I.77820 I.77849	29 28	0.22151	I.93314	7 8 7	1	30 1 0.7 1 3.0
54 55 56 57 58	T.71100 T.71121 T.71142	21	1.77820	29			8 7		30 1 0.7 1 3.0
54 55 56 57 58 59	T.71100 T.71121 T.71142 T.71163	21 21	I.77820 I.77849	29	0.22151	I.93314		1	p. p.

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1 2 3 1 5 4 7 8 日 10 11 12 13 14 15 16 17 18	1.71205 1.71226 1.71247 1.71268 1.71289 1.71310 1.71352 1.71373 1.71393 1.71414 1.71435 1.71414 1.71435 1.71450 1.71450 1.71408 1.71408 1.71510 1.7150 1.71581	21 21 21 21 21 21 21 21 21 21 21 21 21 2	I.77906 I.77935 I.77993 I.77992 I.78020 I.78020 I.78049 I.78076 I.78135 I.78163 I.78192 I.78220 I.78229 I.78277 I.78306 I.78277 I.78304	29 28 29 11 15 29 29 28 29 29 28 29 29 28 29 29 28 29 29 28 29 29 29 29 29 29 29 29 29 29 29 29 29	0.22094 0.22055 0.22037 0.22008 0.21951 0.21951 0.21923 0.21894 0.21865 0.21837 0.21808 0.21780 0.21751	1.93299 1.93291 1.93284 1.93276 1.93269 1.93253 1.93246 1.93238 1.93238 1.93230 1.93230 1.93230 1.93223 1.93223	871 788 788	59 58 57 56 55 54 83 52 51 50 49 48	b 2.9 7 3.4 ■ 3.9 ■ 4.4 10 4.8 20 9.7 30 14.5 40 19.3
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2 3 11 5 5 6 7 8 10 11 12 13 14 15 16 17 18	Y.71226 Y.71247 Y.71269 Y.71289 Y.71310 Y.71331 Y.71352 Y.71373 Y.71393 Y.71414 Y.71456 Y.71456 Y.71477 Y.71456 Y.71459 Y.71519 Y.71550 Y.71560 Y.71561	21 21 21 21 21 21 21 20 21 21 21 21 21 20 21	I.77935 I.77963 I.77962 I.78040 I.78040 I.78047 I.78106 I.78135 I.78163 I.78192 I.78249 I.78249 I.78249 I.78249 I.78249 I.78249 I.78306 I.78334	28 29 28 29 28 29 28 29 28 29 28 29 28 29 28 29 28 29 28 29 28 29 28 29 28 29 28 29 28 29 28 29 29 29 29 29 29 29 29 29 29 29 29 29	0,22065 0,22037 0,22008 0,21951 0,21951 0,21923 0,21894 0,21865 0,21837 0,21808 0,21780 0,21751	I.03201 I.03284 I.03276 I.03260 I.03261 I.03253 I.03238 I.03238 I.03238 I.03238 I.03238 I.03235	7	58 57 56 55 54 83 52 51 50 49 48	b 2.9 7 3.4 ■ 3.9 ■ 4.4 10 4.8 20 9.7 30 14.5 40 19.3
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5 7 8 10 11 12 13 14 15 16 17 18	Y.71289 T.71310 T.71331 Y.71352 Y.71373 Y.71393 Y.71393 Y.71435 T.71435 Y.71435 Y.71435 Y.71435 Y.71498 Y.71498 Y.71539 Y.71539 Y.71581	21 21 21 21 20 21 21 21 21 21 21 21 20 21	I.78020 I.78049 I.78077 I.78106 I.78135 I.78163 I.78192 I.78220 I.78249 I.78249 I.78249 I.78306 I.78306	28 29 28 29 28 29 28 29 28 29 28 29 28 29	0.21980 0.21951 0.21923 0.21894 0.21865 0.21837 0.21808 0.21751	1.93269 1.93261 1.93261 1.93246 1.93246 1.93238 1.93230 1.93223 1.93223	878	54 83 52 51 50 49 48	4.4 10 4.8 20 9.7 30 14.5 40 19.3
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7 8 10 11 12 13 14 15 16 17 18	I.71331 I.71352 I.71373 I.71393 I.71414 I.71435 I.71456 I.71456 I.71498 I.71498 I.71519 I.71539 I.71581	21 21 20 21 21 21 21 21 21 21 21 20 21	T.78106 T.78135 T.78163 T.78192 T.78220 T.78249 T.78249 T.78277 T.78306 T.78334	29 29 28 29 28 29 28 29 28 29	0.21894 0.21865 0.21837 0.21808 0.21780 0.21751	T.93246 T.93238 T.93230 T.93223 T.93223 T.93215	788	52 51 50 49 48	20 9.7 30 14.5 40 19.3
10 11 12 13 14 15 16 17 18	I.71352 I.71373 I.71393 I.71414 I.71435 I.71456 I.71456 I.71477 I.71498 I.71519 I.71539 I.71560 I.71581	21 20 21 21 21 21 21 21 21 21 20 21	T.78135 T.78163 T.78192 T.78220 T.78249 T.78249 T.78277 T.78306 T.78334	29 28 29 28 29 28 29 28 29	0.21865 0.21837 0.21808 0.21780 0.21751	1.93238 1.93230 1.93223 1.93215	8 7 8	51 50 49 48	30 14.5 40 19.3
10 11 12 13 14 15 16 17 18	T.71393 T.71414 T.71435 T.71456 T.71456 T.71477 T.71498 T.71519 T.71539 T.71560 T.71560 T.71581	20 21 21 21 21 21 21 21 21 20 21	I.78163 I.78192 I.78220 I.78249 I.78277 I.78306 I.78334	28 29 28 29 28 29 28 29	0.21837 0.21808 0.21780 0.21751	T.93230 T.93223 T.93215	8 7 8	50 49 48	40 19.3
11 12 13 14 15 16 17 18	¹ .71414 ¹ .71435 ¹ .71456 ¹ .71477 ¹ .71498 ¹ .71519 ¹ .71539 ¹ .71560 ¹ .71581	21 21 21 21 21 21 21 20 21	T.78192 T.78220 T.78249 T.78277 T.78306 T.78334	29 28 29 28 29	0.21808 0.21780 0.21751	T.93223 T.93215	78	49 48	
12 13 14 15 16 17 18	T.71435 T.71456 T.71477 T.71498 T.71519 T.71539 T.71560 T.71581	21 21 21 21 21 21 21 20 21	I.78220 I.78249 I.78277 I.78306 I.78334	28 29 28 29	0.21780	1.93215	8	48	50 24.2
12 13 14 15 16 17 18	T.71435 T.71456 T.71477 T.71498 T.71519 T.71539 T.71560 T.71581	21 21 21 21 21 20 21	I.78220 I.78249 I.78277 I.78306 I.78334	29 28 29	0.21780	1.93215		48	-
13 14 15 16 17 18	1.71456 1.71477 1.71498 1.71519 1.71539 1.71560 1.71581	21 21 21 21 21 20 21	T.78249 T.78277 T.78306 T.78334	29 28 29	0.21751				
14 15 16 17 18	T.71477 T.71498 T.71519 T.71539 T.71560 T.71581	21 21 21 20 21	I.78277 I.78306 I.78334	28 29		1.03207		47	
15 16 17 18	ī.71498 ī.71519 T.71539 T.71560 ī.71581	21 20 21	I.78306 I.78334				7		28
16 17 18	Ī.71519 T.71539 T.71560 Ī.71581	20 21	T.78334		0.21723	T.93200	7 8	46	6 2.8
17	T.71539 T.71560 T.71581	21	1.70339	28	0.21694	T.93192 T.93184	8	45 44	
18	T.71560 T.71581		1.78363	29	0.21637	T.93177	78	44	7 3.3
	1.71581	21	T.78391	28	0.21600	Ī.93169		43	9 4.2
	1.71602		1.78419	28	0.21581	T.93161	8	41	10 4.7
20		21	1.78448	29	0.21552	T.93154	7	40	20 9.3
-		20		28			8		30 14.0
21	1.71622		1.78476		0.21524	T.93146		39	40 18.7
22	T.71643	21	1.78505	29	0.21495	T:93138	8	38	50 23.3
23	T.71664	21	1.78533	28	0.21467	T.93131	78	37	
24	1.71685	21	1,78562	29 28	0.21438	T.93123	o B	36	
25	1.71705	20	1.78590	28	0.21410	Ī.93115		35	
26	1.71726	21	1.78618	20	0.21382	T.93108	7	34	21
27	1.71747	20	T.78647	28	0.21353	1.93100	8	33	6 2.1
BH	1.71767	21	1.78675	29	0.21325	T.93092	8	32	7 2.5 8 2.8
12803	1.71788	21	1.78704	28	0.21296	1.93084	7	31	0 2.0
30	1.71809		1.78732		0.21268	Ī.93077	8	30	10 3.5
		20		28	1000		8	-	20 7.0
31	1.71829	21	1.78760	29	0.21240	T.93069	8	29	30 10.5
32	1.71850	20	1.78789	28	0.21211	Ī.93061	8	28	40 14.0
33	1.7187C 1.71891	21	Ī.78817 Ī.78845	28	0.21183 0.21155	1.93053 1.93046	78	27 26	50 17.5
34 35	1.71091	20	1.78874	29	0.21126	T.93038		25	
36	1.71932	21	1.78902	28	0.21008	T.93030	8	24	
37	1.71952	20	1.78930	28	0.21070	T.93022	8	23	
38	T.71973	21	T.78959	29 28	0.21041	T.93014	8	22	20
30	1.71994	21	1.78987	28	0.21013	T.93007	78	21	6 2.0
40	T.72014	20	T.79015		0.20985	T.92999		26	7 2.3 B 2.7
		20		28	_		8		
41	1.72034		1.79043		0.20957	1.92991	8	19	1 3.0
42	1.72055	21	T.79072	28 28	0.20928	T.92983		18	10 3.3
43	T.72075	20	T.79100	28	0.20900	T.92976	78	17	20 6.7
34	1.72096	20	1.79128	28	0.20872	T.92968	8	16	30 10.0 40 13.3
45	1.72116	20	1.79156	20	0.20844	T.92960	8	15	50 16.7
46	1.72137	20	1.79185	28	0.20815	T.92952	8	14	30 / 10./
47	1.72157	20	T.79213	28	0.20787	T.92944	8	13 12	
48	1.72177	21	T.79241 T.79269	28	0.20759	T.92936 T.92929	7	12	
40 50	I.72198 I.72218	20	I.79209 I.79297	28	0.20731	T.02021	8	10	8 7
50	1./2210	20	1./929/	29	0.20103	T.yoyol	8	10	6 0.8 0.7
	T manage	20	Troast		0.20674	Tagara	-		
51 52	1.72238	21	T.79326	28	0.20074	T.92913 T.92905	8	8	7 0.9 0.8 8 1.1 0.9
53	I.72259 I.72279	20	T.79354 T.79382	28	0.20618	T.02807	8	7	9 1.2 1.1
53	1.72200	20	T.79410	1 28	0.20590	1.92880	8	6	10 1.3 1.2
55	1.72320	21	1.79438	28	0.20561	T.92881	8	5	20 2.7 2.3
56	1.72340	20	1.79466	28	0.20534	7.92874	78	4	30 4.0 3.5
57 58	1.72360	20	Ī.79495	29 28	0.20505	T 92866	8	3	40 5.3 4.7 50 6.7 5.8
	T.72381	21	1.79523	20	0.20477	1.92858	8	2	50 6.7 5.8
50	1.72401	20	I.79551	28	0.20449	T.92850	8	1	
60	T.72421		I.79579		0.20421	¥.92842		O	
	log cos	a	log cot	c. d.	log tan	log sin	d	,	p. p.

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1	log sin	đ	log tan	e. d.	log cot	log cos	a		p. p.
1								-	
0	1.72421	20	T.79579	28	0.20421	1.92842	8	60	
1	T.72441	20	1.79607	28	0.20393	T.92834	8	59	25 28
2	T.72461 T.72482	21	1.79635	28	0.20365	1.92826 1.92818	8	58	
3	I.72502	20	I.79663 I.79691	28	0.20337	1.92010	8	57	
4	1.72522	20	T.79719	28	0.20281	1.92803	8	55	7 3.4 3.3 8 3.9 3.7
5	1.72542	20	1.79747	28	0.20253	1.92795	8	50	8 3.9 3.7
	1.72562	20	1.79776	29	0.20224	1.92787	8	53	10 4.8 4.7
78	1.72582	20	1.79804	28	0.20106	1.92779	80 80 80	52	20 9.7 9.3
10	1.72602	20	I.79832	28	0.20168	1.92771	8	51	30 14.5 14.0
10	1.72622	20	1.79860	28	0.20140	1.92763	8	50	40 19.3 18.7
1		21		28			8		50 24.2 23.3
11	1.72643		1.79888		0.20112	1.02755		49	
12	1.72663	20	1.79916	28	0.20084	T.92747	8	48	
13	I.72683	20	T.7994.	28	0.20056	T.92739	8	47	
14	1.72703	20	T.79972	28 28	0.20028	I.92731	8	46	27
15	I.72723	20	T.80000	28	DI. 300000	T.92723	8	45	6 2.7
16	1.72743	20	T.80028	20	0.19972	T.92715	8	44	7 3.2
17	I.72763	20	T.80056	28	0.19944	T.92707	8	43	
18	1.72783	20	1.80084	28	0.19916	T.92699	8	42	12 H.I
19	1.72803	20	T.80112	28	0.19888	1.92691	8	41	19 4.5
20	1.72823		1.80140		0.19860	1.92683		30	IIII 9.0
		20		28		-	8		13.5 40 18.0
21	¥.72843	20	T.80168	27	0.19832	1.92675	8	39	40 18.0 50 22.5
83	1.72863	20	T.80195	28	0.19805	1.92667	. B	38	50 1 22.5
23	1.72883	10	1.80223	28	0.19777	1.92659	8	37	
24	T.72902	00	T.80251	28	0.19749	1.92651	8	36	
25	¥.72922	210	1.80279	28	0.19721	T.92643	8	35	21 20
20	T.72942 T.72962	20	T.80307 T.80335	28	0.19693	I.92635 I.92627	8	34	6 21 2.0
27	1.72902	283	1.80335 T.80363	28	0.19005	I.92027 I.92619	8	33 32	
100	I.72902 I.73002	20	1.80303 1.80391	28	0.19037	1.92019 1.92611	8	32	· 7 2.5 2.3 8 2.8 2.7
30	I.73022	20	T.80391	28	0.19009	I.92603	8	30	9 3.2 3.0
30		19	1.00419	28	0.19301	1.92003	8	30	10 3.5 3.3
31	T.73041	.9	T.80447	20	0.19553	T.92595		20	20 7.0 6.7
32	1.73061	20	T.80474	27	0.19526	I.92587	8	28	30 10.5 10.0
33	T.73081	20	T.80502	28	0.19498	T.92579	8	27	40 14.0 13.3
34	1.73101	20	T.80530	28	0.19470	T.92571	8	26	50 17.5 16.7
35	1.73121	20	1.80558	28	0.19442	1.92563	8	25	
36	T.73140	19	1.80586	28 28	0.19414	1.92555		24	
37	T.73160	00	1.80614	20	0.19386	T.92546	8	23	
38	1.73180	20	T.80642	27	0.19358	1.92538	8	22	19
39	I.73200	19	T.80669	28	0.19331	T.92530	8	21	6 1.9
40	T.73219		1.80697		0.19303	T.92522		20	7 2.2
		20		28			8		8 2.5 0 2.9
41	1.73239	20	1.80725	28	0.19275	T.92514	8	19	10 3.2
42	1.73259	10	1.80753	28	0.19247	1.92506	8	18	20 6.3
43	I.73278 I.73298	20	1.80781 1.80808	27 28	0.19219	1.92498	8	17	30 9.5
44	I.73290 I.73318	20	1.80808		0.19192 0.19164	T.92490 T.92482	8	15	40 12.7
45	I.73310 I.73337	19	I.80864	28	0.19104	1.92402	8	14	50 15.8
47	1.73357	50	1.80802	28	0.19108	I.92465	8	13	
48	I.73377	20	T.80010	27	0.19081	1.92457	8	12	
49	T.73396	19	¥.80947	28	0.19053	T.92449	8	II	
50	I.73416	20	1.80975	20	0.19025	T.92441		10	9 8 7
		19		28		1000	8		6 0.9 0.8 0.7
51	T.73435	20	T.81003		0.18997	T.92433	8	IJ	7 1.1 0.9 0.8 8 1.2 1.1 0.9
52	T.73455	10	T.81030	27 28	0.18970	1.92425	o B	8	8 1.2 1.1 0.9 9 1.4 1.2 1.1
53	I.73474	20	1.81058	28	0.18942	T.92416	8	7	10 1.5 1.3 1.2
54	I.73494	19	T.81086		0.18914	1.92408	š		20 3.0 2.7 2.3
55	1.73513	20	1.81113	27	0.18887	1.92400	8	5	30 4.5 4.0 3.5
56	I.73533	19	T.81141 T.81169	18	0.18859	T.92392	8	8	
57 58	I.73552	20	T.81109 T.81106	27	0.18831 0.18804	I.92384 I.92376	8	2	40 6.0 5.3 4.7 50 7.5 6.7 5.8
50	T.73572 T.73591	19	1.81190	28	0.18004	1.92370 1.92367	8	1	
60	1.73611	20	1.81252	28	0.18748	T.92359	8	0	
	log cos	a	log cot	c. d.	log tan	log sin	a	,	p. p.
									1

33°

2	log sin	đ	log tan	c. d.	log cot	log cos	Б		p. p.
0	1.73611		T.81252		0.18748	T.92359	8	60	
I	T.73630	19	1.81270	27	0.18721	1.92351	8	50	
2	T.73650	20 10	T.81307	28	0.18693	T.92343	8	58	28 27
3	Ĩ.73069	20	I.81335	20	0.18665	T.92335	0	57	6 2.8 2.7
14	ī.73689	10	T.81362	28	0.18638	I.92326	8	56	7 3.3 3.2 8 3.7 3.6
56	1.73708	19	T.81390	28	0.18610	1.92318	8	55	
	I.73727	20	T.81418	27	0.18582	T.92310	8	54	9 4.2 4.1
78	1.73747	19	T.81445 T.81473	28	0.18555 0.18527	T.92302 T.92293	8	53	10 4.7 4.5 20 9.3 9.0
0	T.73766 T.73785	19	I.01473 I.81500	27	0.18500	1.92293	8	52 51	30 14.0 13.5
10	I.73805	120	T.81528	28	0.18472	I.92277	8	50	40 18.7 18.0
	11/3003	19		28	01104/1		8	30	50 23.3 22.5
II	T.73824	10	1.81556	27	0.18444	T.92269		40	
12	I.73843	19	T.81583	27	0.18417	T.92260	8	48	
13	1.73863	19	1.81611	20	0.18389	1.92252		47	
14	T.73882	19	T.81638	28	0.18362	1.92244		46	20
15	1.73901	20	1.81666	27	0.18334	1.92235	98	45	6 2.0
16	T.73921	19	1.81693	28	0.18307	1.92227	8	44	7 2.3 8 2.7
17 18	1.73940	19	1.81721	27	0.18279 0.18252	I.92219	8	43	
18	T.73959 T.73978	19	1.81748 1.81776	28	0.18252	Ī.92211 Ī.92202	8	42 41	9 3.0 10 3.3
20	I.73978 I.73997	19	I.81803	27	0.18197	T.92194	8	41	20 6.7
	11/399/	JO	1.01003	28	0.1019/	1.201.24	8	NU.	30 10.0
21	1.74017		1.81831		0.18169	T.92186		39	40 13.3
22	T.74036	19	T.81858	27	0.18142	1.92177	9	38	50 16.7
23	T.74055	19	T.81886	28	0.18114	T.92169	8	37	
24	1.74074	19	T.81913	27 28	0.18087	1.92161	8	36	
25	T.74093	19 20	1.81941	28	0.18059	Ĩ.92152	8	35	
26	1.74113	19	7.81968	27	0.18032	I.92144	8	34	19
27	1.74132	19	T.81996	27	0.18004	T.92136		33	6 1.9
1	T.74151	19	T.82023	28	0.17977	1.92127	8	32	7 2.2 8 2.5
23	T.74170	19	1.82051	27	0.17949	1.92119	8	31	
30	1.74189		1.82078		0.17922	Ĩ.92111		30	10 2.9 10 3.2
	E	19	T Parad	28	0.0000	Terrer	9		20 6.3
31 32	T.74208 T.74227	19	T.82106 T.82133	27	0.17894 0.17867	1.92102 1.92094	8	29 28	30 9.5
33	1.74227	19	T.82161	28	0.17839	T.92094	8	27	40 12.7 50 15.8
34	1.74265	19	T.82188	27	0.17812	1.02077	8	26	50 15.8
35	1.74284	19	1.82215	27	0.17785	1.92069		25	
36	T.74303	19	T.82243	8	0.17757	1.92060	8	24	
37	T.74322	19	1.82270	27 128	0.17730	T.92052	8	23	
38	I.74341	19	1.82298	27	0.17702	1.92044		22	18
019	T.74360	19	1.82325	27	0.17675	1.92035	9	21	6 1.8
40	1.74379		T.82352		0.17648	1.92027		20	7 2.1
		19		28			9		8 2.4
41	1.74398	10	1.82380	27	0.17620	1.92018	8	19	10 3.0
42	I.74417	19	T.82407	28	0.17593	¥.92010	8	18	20 6:0
43	T.74436	19	T.82435 T.82462	27	0.17565	T.92002 T.91093	8	17 16	30 9.0
44	I.74455 I.74474	19	1.82402 T.82489	27	0.17538	1.91993 T.91985		10 15	12.0
46	I.74493	19	1.82517	28	0.17483	I.91976	8	15	50 1500
47	T.74512	19	T.82544	27	0.17456	T.01068		13	
48	1.74531	19	1.82571	27	0.17429	T.91959	8	12	
49	1.74549	18	T.82599	28	0.17401	Ī.91951		11	
50	1.74568	19	1.82626	27	0.17374	I.91942	9	10	9 8
		19		27			8		6. 0.9 0.8
51	1.74587	10	T.82653	28	0.17347	T.91934		9	7 I.I 0.9 8 4.3 I.I
52	¥.74606	19	1.82681	27	0.17319	T.91925	8		9 1.4 1.2
53	T.74625 T.74644	19	1.82708	27	0.17292	T.91917		7	10 1.5 1.3
54 55	1.74044 174662	18	I.82735 I.82762	27	0.17265 0.17238	80010.T 1.91908	9 8	5	20 3.0 2.7
55	1.74681	19	1.82702	28	0.17238	1.91900 T.91891	9	5	30 4.5 4.0
	1.74700	19	T.82817	27	0.17183	T.91883		3	40 6.0 5.3
57 58	1.74719	19	1.82844	27	0.17156	T.91874	98	2	50 7.5 6.7
59	1.74737	18	1.82871	27	0.17129	1.91866		i	
60	1.74756	19	T.82899	28	0.17101	T.91857	9	ø	
	log cos	а	log cot	c. d.	log tan	log sin	d	,	p. p.

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Jog sin 1 Jog sin 1 1.74755 1 1.74755 1 1.74765 3 1.74785 4 1.74812 4 1.74887 5 1.74887 8 1.74887 9 1.74987 10 1.74987 11 1.74987 12 1.74980 13 1.74981 14 1.74981 15 1.75036 16 1.75017 17 1.75031 18 1.75017 19 1.75110 20 1.75128 21 1.75147 22 1.75221 23 1.75228 24 1.75230 27 1.75231 31 1.75333 32 1.75343 33 1.75485 1.7548 1.75486 33 1.7548 34								1	
1 1.74775 1 1.74794 3 1.74872 4 1.74872 5 1.74887 5 1.74887 8 1.74896 9 1.74887 9 1.74887 10 1.74924 10 1.74924 10 1.74924 11 1.74943 11 1.74943 11 1.74943 11 1.74943 11 1.74960 12 1.74980 13 1.74980 14 1.75017 15 1.75036 16 1.75031 21 1.75147 22 1.75242 23 1.75320 24 1.75230 25 1.75243 32 1.75368 34 1.75368 34 1.75443 37 1.75443 37 1.75443 <	sin	đ	log tan	c. d.	log cot	log cos	đ		p. p.
1 1.74775 1 1.74794 2 1.74812 4 1.74832 5 1.74850 5 1.74850 6 1.749612 15 1.74850 9 1.74924 10 1.74924 11 1.74943 12 1.74943 13 1.74943 14 1.75017 15 1.75031 16 1.75031 17 1.75073 18 1.75073 18 1.75031 21 1.75147 22 1.75128 21 1.75147 22 1.75221 23 1.75343 31 1.75343 32 1.75303 33 1.75368 34 1.75441 32 1.75428 33 1.75448 40 1.754303 37 1.75448	756	19	1.82899		0.17101	T.91857	8	60	
3 1.7481 4 1.74831 5 1.74850 6 1.74880 7 1.74880 9 1.74880 9 1.74980 9 1.74981 10 1.74924 10 1.74924 11 1.74961 12 1.74993 11 1.749943 11 1.749943 11 1.74990 13 1.74990 14 1.75071 15 1.75036 16 1.75073 17 1.75073 18 1.75128 21 1.75128 23 1.75128 24 1.75202 25 1.75212 26 1.75238 17 1.75202 27 1.752313 31 1.75331 31 1.75331 31 1.75343 32 1.75343	775	10	1.82926	27	0.17074	T.91849		59	
4 I.74831 5 I.74886 7 I.74887 8 I.74887 9 I.74987 9 I.74987 10 I.74981 10 I.74943 11 I.74943 12 I.74980 13 I.74980 14 I.75017 15 I.75036 16 I.75036 17 I.75037 18 I.75017 19 I.75110 20 I.75128 21 I.75147 22 I.75202 23 I.75202 24 I.75202 25 I.75204 30 I.75308 31 I.75308 32 I.75308 33 I.75308 34 I.75308 35 I.75405 36 I.75430 37 I.75441 38 I.75533	794	18	T.82953	27	0.17047	T.91840	9	58	28 27
S 1.74850 I 1.74888 I 1.74888 I 1.74987 B I.74987 I I.74984 IO I.74984 IO I.74984 IO I.74984 IO I.74924 IO I.74981 II I.74961 IZ I.74990 IA I.75036 I.75031 I.750147 I.75128 I.75228 I.75226 I.75221 I.75238 I.75230 I.75238 I.75230 I.75313 I.75331 II I.75442 I.75445 I.75445 I.75428 I.75445 II I.75448 II </td <td>512</td> <td>10</td> <td>1.82980</td> <td>28</td> <td>0.17020</td> <td>1.91832</td> <td></td> <td>57</td> <td>6 2.8 2.7</td>	512	10	1.82980	28	0.17020	1.91832		57	6 2.8 2.7
iii I.74808 7 I.74906 9 I.74906 10 I.74924 10 I.74924 10 I.74924 11 I.74961 12 I.74934 13 I.74960 13 I.74960 14 I.75017 15 I.75034 17 I.75034 19 I.75110 20 I.75128 21 I.75147 22 I.75128 21 I.75142 22 I.75202 23 I.75143 24 I.75202 25 I.75202 26 I.75230 27 I.75230 29 I.75230 31 I.75366 32 I.75368 33 I.75368 34 I.75533 37 I.75441 38 I.75533 34 I.755514 </td <td></td> <td>19</td> <td>1.83008</td> <td>27</td> <td>0.16992</td> <td>1.91823</td> <td>8</td> <td>56</td> <td>7 3.3 3.2 8 3.7 3.6</td>		19	1.83008	27	0.16992	1.91823	8	56	7 3.3 3.2 8 3.7 3.6
7 I.74887 8 I.74904 10 I.74924 10 I.74924 11 I.74924 12 I.74980 13 I.74980 13 I.74980 14 I.75037 15 I.75036 16 I.75031 17 I.75128 21 I.75147 22 I.75128 21 I.75236 22 I.75238 23 I.75238 24 I.75328 25 I.75238 26 I.75238 27 I.75288 28 I.75331 31 I.75331 31 I.75333 32 I.75334 33 I.75437 34 I.75438 40 I.75438 41 I.75542 33 I.75437 44 I.75543 45 I.75542 <td></td> <td>18</td> <td>T.83035 T.83062</td> <td>27</td> <td>0.16965 0.16938</td> <td>T.91815 T.91806</td> <td>8</td> <td>55</td> <td></td>		18	T.83035 T.83062	27	0.16965 0.16938	T.91815 T.91806	8	55	
8 I.74006 9 I.74061 10 I.74943 11 I.74961 12 I.74983 13 I.74980 13 I.74980 14 I.75017 15 I.75031 16 I.75031 17 I.75031 18 I.75091 19 I.75110 21 I.75147 22 I.75221 23 I.75128 21 I.75147 22 I.75230 23 I.75230 24 I.75230 27 I.75233 31 I.75313 31 I.75333 32 I.75386 33 I.75441 36 I.75428 41 I.75533 41 I.75544 41 I.75564 41 I.75564 31 I.75733 34 I.75733 <td>287</td> <td>19</td> <td>1.83082 1.83089</td> <td>27</td> <td>0.16911</td> <td>1.91798</td> <td></td> <td>54 53</td> <td>9 4.2 4.1 10 4.7 4.5</td>	287	19	1.83082 1.83089	27	0.16911	1.91798		54 53	9 4.2 4.1 10 4.7 4.5
I I.74024 IO I.74043 II I.74943 II I.74960 II I.74960 II I.74960 II I.74970 II I.75036 IO I.75036 IO I.75037 IF I.75037 IF I.75037 IF I.75037 IF I.75038 II I.75110 II I.75128 II I.75128 II I.75202 I.75276 I.75230 II I.75308 II I.75303 II I.75308 II I.75308 II I.75308 II I.75308 II I.75331 II I.75331 II I.75338 II I.75441 II I.75544 II I.75544 II I.75554	006	19	T.83117	28	0.16883	T.91789	8	53	10 4.7 4.5 20 9.3 9.0
10 I.74943 11 I.74961 12 I.74980 13 I.74980 14 I.7507 15 I.75036 16 I.75037 17 I.75036 18 I.75017 19 I.75110 20 I.75128 21 I.75128 21 I.75128 23 I.75128 24 I.75221 25 I.75221 26 I.75221 27 I.75238 10 I.75308 29 I.75331 31 I.75331 31 I.75331 31 I.75331 31 I.75432 35 I.75433 36 I.75438 37 I.75443 38 I.75587 40 I.75587 41 I.75587 44 I.75733 354 I.75731 </td <td></td> <td>18</td> <td>1.83144</td> <td>27</td> <td>0.16856</td> <td>T.91781</td> <td></td> <td>51</td> <td>30 14.0 13.5</td>		18	1.83144	27	0.16856	T.91781		51	30 14.0 13.5
11 I.74961 12 I.74980 13 I.74980 14 I.75017 15 I.75017 16 I.75034 17 I.75036 16 I.75031 17 I.75033 18 I.75017 19 I.75110 20 I.75128 21 I.75147 22 I.75128 21 I.75128 21 I.75147 22 I.75202 25 I.75230 27 I.75230 29 I.75230 20 I.75230 21 I.75343 31 I.75368 35 I.75368 35 I.75441 36 I.75430 37 I.75443 36 I.75443 37 I.75544 41 I.75544 41 I.75544 41 I.75544 </td <td></td> <td>19</td> <td>1.83171</td> <td>27</td> <td>0.16829</td> <td>T.91772</td> <td>10</td> <td>50</td> <td>40 18.7 18.0</td>		19	1.83171	27	0.16829	T.91772	10	50	40 18.7 18.0
12 1.74980 13 1.74990 14 1.75017 15 1.75037 16 1.75037 17 1.75031 18 1.75091 19 1.75102 21 1.75103 22 1.75102 21 1.75147 22 1.75128 21 1.75128 21 1.75242 22 1.75230 23 1.75230 24 1.75230 25 1.75230 26 1.75230 27 1.75233 30 1.75313 31 1.75313 32 1.75386 34 1.75386 35 1.75441 36 1.75428 37 1.75443 36 1.75589 37 1.75544 34 1.75533 41 1.75544 42 1.75564 </td <td></td> <td>18</td> <td></td> <td>27</td> <td></td> <td></td> <td>9</td> <td></td> <td>50 23.3 22.5</td>		18		27			9		50 23.3 22.5
13 V.74090 14 V.75017 15 V.75036 16 V.75037 17 V.75038 17 V.75037 18 V.75037 17 V.75037 18 V.75037 19 V.75132 21 V.75132 21 V.75132 21 V.75147 22 V.75142 23 V.75128 24 V.75302 25 V.75294 30 V.75308 31 V.75308 32 V.75304 33 V.75303 34 V.75308 35 V.75441 36 V.75449 40 V.75449 41 V.75544 35 V.75544 34 V.75544 34 V.75544 34 V.75544 34 V.75544 35 V.75605 </td <td>100</td> <td></td> <td>¥.83198</td> <td></td> <td>0.16802</td> <td>¥ 91763</td> <td>8</td> <td>49</td> <td></td>	100		¥.83198		0.16802	¥ 91763	8	49	
14 I.75017 15 I.75036 17 I.75036 18 I.75031 18 I.75031 19 I.75110 20 I.75128 21 I.75128 21 I.75128 23 I.75128 24 I.75220 25 I.75221 26 I.75226 29 I.75236 29 I.75238 31 I.75303 32 I.75303 33 I.75303 34 I.75303 35 I.75204 30 I.75303 31 I.75303 32 I.75303 34 I.75304 35 I.75423 37 I.75428 39 I.75428 40 I.754296 41 I.75502 42 I.75527 43 I.75502 44 I.75602 <	80	19	1.83225	27	0.16775	T.91755		48	
15 I.75036 16 I.75073 17 I.75073 18 I.75073 19 I.75073 19 I.75073 19 I.75073 19 I.75010 20 I.75010 21 I.75147 22 I.75128 21 I.75147 22 I.75221 26 I.75230 27 I.75230 29 I.75230 29 I.75230 20 I.75313 31 I.75368 35 I.75447 36 I.75488 37 I.754896 37 I.75447 36 I.75508 37 I.75448 40 I.75503 41 I.75504 41 I.75504 41 I.75502 41 I.75503 51 I.75606 50 I.75787 <		19 18	T.83252	27	0.16748	¥.91746	98	47	
16 1.75054 17 1.75073 18 1.75073 18 1.75073 19 1.75110 21 1.75112 21 1.75128 22 1.75128 23 1.75128 24 1.75202 25 1.75228 26 1.75230 27 1.75236 29 1.75230 30 1.75303 31 1.75303 32 1.75303 33 1.75303 34 1.75303 35 1.75304 36 1.75405 37 1.75403 38 1.75403 39 1.75403 40 1.75423 37 1.75424 37 1.75424 41 1.75507 42 1.75507 43 1.75507 44 1.75507 45 1.75606 </td <td>017</td> <td>10</td> <td>T.83280</td> <td>27</td> <td>0.16720</td> <td>1.91738</td> <td>9</td> <td>46</td> <td>26</td>	017	10	T.83280	27	0.16720	1.91738	9	46	26
17 I.25073 18 I.75091 19 I.75110 21 I.75110 221 I.75121 23 I.75132 24 I.75122 25 I.75230 26 I.75230 27 I.75230 28 I.75230 29 I.75230 29 I.75230 31 I.752313 31 I.75313 32 I.75333 34 I.75333 35 I.75441 36 I.75438 37 I.75436 37 I.75438 37 I.75533 34 I.75533 35 I.75569 31 I.75606		18	1.83307	27	0.16693	T.91729		45	6 2.6
18 I.75001 19 I.75110 20 I.75128 21 I.75147 22 I.75168 23 I.75182 24 I.75162 25 I.75128 24 I.75126 25 I.75226 26 I.75230 27 I.75230 29 I.75244 30 I.75301 31 I.75303 32 I.75304 33 I.75305 34 I.75304 35 I.75405 36 I.75407 37 I.75441 38 I.75514 40 I.75544 41 I.75514 42 I.75544 43 I.75504 44 I.75504 45 I.75605 54 I.75678 51 I.75787 54 I.75782 551 I.75823 <		19	I.83334	27	0.16666	T.91720	19 100	44	7 3.0
19 I.75100 20 I.75128 21 I.75128 22 I.75165 23 I.75128 24 I.75128 25 I.75128 26 I.75221 27 I.75228 29 I.75230 29 I.75231 30 I.75333 31 I.75333 32 I.75333 33 I.75443 34 I.75436 37 I.75478 38 I.75433 37 I.75443 37 I.75443 37 I.75443 38 I.75443 39 I.75444 41 I.75504 41 I.75504 41 I.75604 41 I.75605 51 I.75606 52 I.75713 54 I.75733 54 I.75707 551 I.75787 <		18	1.83361	27	0.16639	T.91712	9 20	43	
20 Y.75128 21 I.75147 22 I.75163 23 Y.75184 24 I.75105 25 Y.75184 24 I.75202 25 Y.75294 20 I.75294 30 I.75313 31 I.75308 32 I.75308 33 I.75308 34 I.75308 35 I.75308 36 I.75308 37 I.75308 38 I.75308 39 I.75308 31 I.75308 32 I.75308 33 I.75308 34 I.75441 35 I.75498 40 I.75498 41 I.75504 42 I.75504 43 I.75505 44 I.75608 50 I.75678 51 I.75782 54 I.75823 </td <td></td> <td>19</td> <td>1.83388 1.83415</td> <td>27</td> <td>0.10012</td> <td>T.91703 T.91695</td> <td></td> <td>42</td> <td>10 3.9 10 4.3</td>		19	1.83388 1.83415	27	0.10012	T.91703 T.91695		42	10 3.9 10 4.3
21 I.75147 22 I.75165 23 I.75163 24 I.75163 25 I.75221 26 I.75236 27 I.75236 29 I.75302 29 I.75303 30 I.75303 31 I.75303 33 I.75303 34 I.75303 35 I.75303 36 I.75303 37 I.75306 38 I.75308 39 I.75308 30 I.75405 31 I.75405 32 I.75405 34 I.75405 35 I.75423 37 I.75405 38 I.75405 34 I.75507 35 I.75502 44 I.75503 45 I.75704 54 I.75705 55 I.75760 56 I.75787 </td <td>28</td> <td>18</td> <td>1.03415 T.83442</td> <td>27</td> <td>0.16558</td> <td>I.01686</td> <td>9</td> <td>41</td> <td>HI 4.3</td>	28	18	1.03415 T.83442	27	0.16558	I.01686	9	41	HI 4.3
22 I.75165 23 I.75184 24 I.75202 25 I.75202 26 I.75202 27 I.75204 30 I.75204 30 I.75303 31 I.75303 32 I.75303 33 I.75303 34 I.75303 35 I.75303 36 I.75306 37 I.75308 38 I.75308 39 I.75308 31 I.75308 32 I.75308 33 I.75405 34 I.75405 35 I.75441 36 I.75514 40 I.75533 41 I.75514 42 I.75504 43 I.75505 44 I.75605 54 I.75708 51 I.75709 51 I.75705 561 I.75823 <		19	1.03442	86	0.10330	1.91000	9	40	30 13.0
22 1.75165 23 1.75184 24 1.75202 25 1.75202 26 1.75204 20 1.75204 30 1.75204 30 1.75303 31 1.75303 32 1.75303 33 1.75303 34 1.75303 35 1.75303 36 1.75306 37 1.75308 38 1.75308 39 1.75308 31 1.75308 32 1.75308 33 1.75405 36 1.75405 37 1.75404 38 1.75490 40 1.75514 41 1.75514 42 1.75504 43 1.75505 44 1.75505 54 1.75605 55 1.75748 54 1.75787 556 1.758787	47		1.83470	*0	0.16530	¥.91677		20	40 17.3
23 I.75184 24 I.75202 25 I.75221 26 I.75236 27 I.75236 29 I.75331 31 I.75336 32 I.75331 31 I.75333 32 I.75333 33 I.75336 34 I.75368 35 I.75425 36 I.75433 37 I.75465 36 I.75465 37 I.754425 37 I.754425 37 I.754425 38 I.75542 40 I.75542 31 I.75542 40 I.75542 41 I.75542 42 I.75542 43 I.75587 44 I.75587 45 I.75562 54 I.75733 54 I.75733 54 I.75769 51 I.75769		18	1.83470 1.83497	27	0.16530	T.91669	8	39 38	30 21.7
24 I.75202 25 I.75221 26 I.75230 27 I.75230 29 I.75230 20 I.75230 20 I.75230 20 I.75330 30 I.75333 31 I.75333 32 I.75333 33 I.75368 34 I.75363 35 I.75405 36 I.75438 37 I.75438 40 I.75533 41 I.75534 42 I.75534 43 I.75562 44 I.75624 47 I.75625 51 I.75733 54 I.75733 54 I.75733 54 I.75787 </td <td>84</td> <td>19</td> <td>1.83524</td> <td>27</td> <td>0.16476</td> <td>T.91660</td> <td>9</td> <td>30</td> <td></td>	84	19	1.83524	27	0.16476	T.91660	9	30	
25 I.75221 26 I.75236 27 I.75236 29 I.75236 29 I.75331 31 I.75333 32 I.75333 33 I.75336 34 I.75368 35 I.75368 36 I.75368 37 I.75423 37 I.75436 36 I.75423 37 I.75437 38 I.75423 37 I.75423 37 I.75423 37 I.75423 37 I.75423 37 I.75423 37 I.75423 38 I.75542 40 I.75428 41 I.75542 42 I.75542 43 I.75542 44 I.75542 45 I.75587 46 I.75567 51 I.75769 51 I.75769 </td <td></td> <td>18</td> <td>1.83551</td> <td>27</td> <td>0.16449</td> <td>1.91651</td> <td>9</td> <td>36</td> <td></td>		18	1.83551	27	0.16449	1.91651	9	36	
26 Y.75330 27 Y.75258 141 Y.75276 29 Y.75333 30 Y.75333 31 Y.75333 32 Y.75333 33 Y.75333 34 Y.75333 35 Y.75303 36 Y.75303 37 Y.75441 38 Y.75478 39 Y.75478 30 Y.75478 31 Y.75478 32 Y.75478 33 Y.75478 34 Y.75478 35 Y.75478 34 Y.75533 34 Y.75533 34 Y.75560 54 Y.75606 55 Y.75708 51 Y.75696 51 Y.75789 51 Y.75823 54 Y.75823		19	F 82578	27	0.16422	Y.91643		35	
27 I.75236 WI I.75276 30 I.75294 30 I.75234 31 I.75313 32 I.75313 33 I.75313 34 I.75313 35 I.75308 34 I.75308 35 I.75308 36 I.75405 37 I.75435 38 I.75445 39 I.75445 30 I.75445 31 I.75445 32 I.75514 42 I.75533 43 I.75533 44 I.75554 45 I.75564 54 I.75678 51 I.75769 51 I.75787 54 I.75787 55 I.75823 54 I.75823	239	18	1.83605	27	0.16395	T.91634	9	34	19
20 I.75204 30 I.75313 31 I.75313 32 I.75306 33 I.75306 34 I.75306 35 I.75306 36 I.75306 37 I.75405 36 I.75405 37 I.75407 38 I.75407 39 I.75407 30 I.75407 41 I.75594 42 I.75594 43 I.75594 44 I.75594 45 I.75594 46 I.75594 47 I.75694 58 I.75696 59 I.75797 51 I.75796 51 I.75797 54 I.75787 57 I.75823	258	19	1.83632	27	0.16368	1.91625	9	33	6 I.9
30 1.75313 31 1.75331 32 1.75360 33 1.75360 34 1.75363 35 1.75405 36 1.75405 37 1.75405 37 1.75423 37 1.75423 38 1.75424 39 1.75426 40 1.75426 41 1.75542 42 1.75537 43 1.75587 44 1.75587 45 1.75587 46 1.75587 47 1.75604 50 1.75678 51 1.75763 54 1.75751 55 1.75751 54 1.75787 55 1.75823 54 1.75782 55 1.75823 54 1.75823		18	T.83659	27	0.16341	T.91617	9	32	7 2.2
31 I.75331 32 I.75320 33 I.75360 34 I.75386 35 I.75405 36 I.75486 37 I.7547 38 I.7547 397 I.7547 37 I.7547 38 I.7547 39 I.7547 34 I.7547 40 I.75496 41 I.75514 42 I.75533 43 I.75564 44 I.75564 47 I.75642 48 I.75660 50 I.75678 51 I.75787 54 I.75787 551 I.75823		19	1.83686	27	0.16314	1.91608	9	31	
32 I.753360 33 I.753483 34 I.753485 35 I.754423 37 I.754323 37 I.754323 37 I.754323 38 I.754323 39 I.754323 34 I.754343 35 I.754323 40 I.755387 41 I.75533 42 I.755387 43 I.75560 54 I.75602 57 I.75602 50 I.75678 51 I.75743 53 I.75713 53 I.75743 53 I.75743 54 I.75769 51 I.75769 51 I.75769 51 I.75769 55 I.75787 57 I.75823	313		1.83713		0.16287	T.91599	-	30	9 2.9
32 I.753360 33 I.753483 34 I.753485 35 I.754423 37 I.754323 37 I.754323 37 I.754323 38 I.754323 39 I.754323 34 I.754343 35 I.754323 40 I.755387 41 I.75533 42 I.755387 43 I.75560 54 I.75602 57 I.75602 50 I.75678 51 I.75743 53 I.75713 53 I.75743 53 I.75743 54 I.75769 51 I.75769 51 I.75769 51 I.75769 55 I.75787 57 I.75823		18		27			8		10 3.2 20 6.3
33 1.75368 34 1.75386 35 1.75405 36 1.75405 37 1.75405 38 1.75405 39 1.75405 39 1.75405 39 1.75405 38 1.75405 39 1.75406 40 1.75503 41 1.75533 43 1.75504 44 1.75504 45 1.75604 46 1.75605 51 1.75606 52 1.75708 51 1.75787 54 1.75787 55 1.75787 56 1.75787 57 1.75823		10	T.83740	28	0.16260	T.91591	9	29	30 9.5
34 I.75386 35 I.75405 36 I.75423 37 I.75423 38 I.75423 39 I.75423 39 I.75423 39 I.75423 39 I.75423 39 I.75423 40 I.75496 41 I.75533 42 I.75587 44 I.75587 45 I.75587 46 I.75604 57 I.75678 51 I.75573 53 I.75769 51 I.75769 54 I.75787 57 I.75882 54 I.75823		18	T.83768	27	0.16232	T.91582		28	40 12.7
35 I.75405 26 I.75423 37 I.75441 38 I.75478 390 I.75478 40 I.75496 41 I.75514 42 I.75531 43 I.75551 44 I.75569 45 I.75602 47 I.75603 50 I.75678 51 I.75787 54 I.75787 55 I.75787 56 I.75787 57 I.75802		18	T.83795 T.83822	27	0.16205	T.91573	8	27	BO 15.8
36 I.75443 37 I.75441 38 I.75450 39 I.75450 39 I.75495 40 I.75496 41 I.75533 42 I.75533 43 I.75534 44 I.75533 45 I.75594 46 I.75504 47 I.75605 50 I.75678 51 I.75749 51 I.75769 51 I.75769 51 I.75769 51 I.75769 51 I.75796 53 I.75787 54 I.75787 57 I.75823		19	1.83849	27	0.16151	T.91565 T.91556	9	20	
37 I.75441 38 I.75428 390 I.75478 40 I.75478 40 I.75478 41 I.75514 42 I.75531 43 I.755514 43 I.75551 44 I.75531 45 I.75587 46 I.75602 47 I.75642 48 I.75660 50 I.75733 54 I.75733 54 I.75787 55 I.75787 56 I.75787 57 I.75802	122	18	1.83876	27	0.16124	T.01547	9	25	
38 I.75438 19 I.75478 40 I.75436 41 I.75533 43 I.75533 44 I.75533 45 I.75533 46 I.75533 47 I.75564 48 I.75664 49 I.75664 50 I.75678 51 I.75787 53 I.75787 54 I.75787 55 I.75787 56 I.75787 57 I.75823		18	1.82002	27	0.16097	T.01538	9	23	
NU I.75478 40 I.755496 41 I.75533 42 I.75533 43 I.75533 44 I.75569 45 I.75587 46 I.75569 57 I.75624 48 I.75605 50 I.75678 51 I.75733 53 I.75733 54 I.75760 55 I.757387 56 I.75769 51 I.75769 55 I.75769 56 I.75789 57 I.78823		18	1.83930	27	0.16070	T.91530	8	22	18
41 1.75514 42 1.75533 43 1.75533 44 1.75569 45 1.75569 46 1.75669 47 1.75664 40 1.75669 50 1.75678 51 1.75769 51 1.75748 53 1.75748 53 1.75748 53 1.75769 54 1.75769 55 1.75789 57 1.75789 57 1.7589	178	19 18	1.83957	27	0.16043	1.91521	9	21	6 1.8
42 I.75533 43 I.75551 44 I.75569 45 I.75569 47 I.75667 47 I.75664 48 I.75664 49 I.75664 49 I.75666 50 I.75767 51 I.75769 51 I.75733 54 I.75733 54 I.75787 57 I.75823	196	10	1.83984	27	0.16016	1.91512		20	7 2.1 B 2.4
42 I.75533 43 I.75551 44 I.75569 45 I.75569 47 I.75667 47 I.75664 48 I.75664 49 I.75664 49 I.75666 50 I.75767 51 I.75769 51 I.75733 54 I.75733 54 I.75787 57 I.75823		18		27			8		
42 I.75533 43 I.75551 44 I.75569 45 I.75569 47 I.75667 47 I.75664 48 I.75664 49 I.75664 49 I.75666 50 I.75767 51 I.75769 51 I.75733 54 I.75733 54 I.75787 57 I.75823	514		1.84011		0.15989	T.91504	a	19	2.7
43 I.75550 44 I.75569 45 I.75587 46 I.75587 47 I.75624 48 I.75604 50 I.75604 50 I.75606 50 I.75678 51 I.75748 53 I.75748 53 I.75748 53 I.75759 54 I.75769 55 I.75769 55 I.75769 57 I.75787 57 I.75823	533	19 18	7.84038	27 27	0.15962	T.91495	9	18	10 3.0
45 I.75887 46 I.75605 47 I.75604 48 I.75605 48 I.75605 50 I.75678 51 I.75769 53 I.75718 53 I.75718 53 I.75733 54 I.75769 56 I.75787 57 I.75823	551	18	1.84065	27	0.15935	T.91486	0	17	10 6.0 30 9.0
46 I.75602 47 I.75624 48 I.75624 49 I.75662 50 I.75678 51 I.75793 52 I.75714 53 I.75733 54 I.75736 55 I.75787 56 I.75787 57 I.75823 58 I.75823		18	1.84092	27	0.15908	Y.91477	Ř	16	30 9.0 40 12.0
47 I.75624 48 I.75642 49 I.75660 50 I.75678 51 I.7578 53 I.75733 54 I.75733 54 I.75787 55 I.75787 57 I.75823		18	1.84119	27	0.15881	1.91469	Ū	15	50 15.0
AR T.75642 40 T.75660 50 T.75678 51 T.75696 52 T.75714 53 T.75733 54 T.75769 53 T.75733 54 T.75769 55 T.75769 56 T.75769 57 T.75769 57 T.75805 58 T.75805 58 T.75823		19	T.84146 T.84173	27	0.15854 0.15827	¥.91460	0	14	an 1 13.0
40 Y.75660 S0 I.75678 51 I.75678 52 I.75714 53 I.75733 54 I.75750 55 I.75787 57 I.757805 57 I.75805 58 I.758805		18	I.84173 I.84200	27	0.15827	T.91451	9	13 12	
SO I.75678 51 J.75696 52 I.75714 53 I.75733 54 I.75751 55 I.75769 56 I.75787 57 I.75805 58 I.758805		18	I.84200 I.84227	27	0.15800	T.91442 T.91433	9	12	
51 J.75696 52 J.75714 53 J.75733 54 J.75735 55 J.75769 56 J.75787 57 J.75805 58 J.75805		18	1.84254	27	0.15746	I.91433	Ň	10	8 8
52 I.75714 53 I.75733 54 I.75751 55 I.75769 56 I.75787 57 I.75805 58 I.75823		18		26	5745		9		6 0.9 0.8
52 I.75714 53 I.75733 54 I.75751 55 I.75769 56 I.75787 57 I.75805 58 I.75823	506		¥.84280		0.15720	1.01416			7 1.1 0.9
53 I.75733 54 I.75751 55 I.75769 56 I.75787 57 I.75805 5 ^H I.75823		18	1.84307	27	0.15693	T.01407	9	8	
54 T.75751 55 T.75769 56 T.75787 57 T.75805 58 T.75823		19 18	1.84334	27	0.15666	1.91398	0		9 1.4 1.2
SS T.75769 56 Y.75787 57 Y.75805 58 Y.75823	751	18	1.84361	27	0.15639	T.91389	8	7	10 1.5 1.3
57 I.75805 58 I.75823	769	18	T.84388	27	0.15612	1.91381	0 g	5	20 3.0 2.7
SH 1.75823		18	Y.84415	27	0.15585	1.91372	9		30 4.5 4.0 40 6.0 5.3
	505	18	1.84442	27	0.15558	1.91363		8	40 6.0 5.3 50 7.5 6.7
		18	1.84469	27	0.15531	1.91354	9	2	30 1 7.3 1 0.7
		18	T.84496 T.84523	27	0.15504	T.91345	9	1	
56 T.75859	-59		1.04533		0.15477	1.91336		0	
		_							
log cos	COS	a	log cot	c. d.	log tan	log sin	a	'	p. p.

35°

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1	log sin	` a	log tan	c. d.	log cot	log cos	а		p. p.
	1.75859		1.84523			1.91336	-	60	
0	1.75059	18	1.84550	27	0.15477 0.15450	I.91330	8	80	
	ī.75895	18	1.84576	26	0.15424	1.91319	Ð	58	27 26
3	1.75913	18	T.84603	27	0.15397	T.91310	9	57	6 2.7 2.6
	1.75931	18	1.84630	27	0.15370	T.91301	9	56	
56	1.75949	18	T.84657	27	0.15343	T.91292	9	55	7 3.2 3.0 8 3.6 3.5
	1.75967	10	T.84684	27	0.15316	¥.91283	0	54	9 4.1 3.9
78	T.75985	18	¥.84711	27	0.15289	1.91274	8	53	10 . 4.5 4.3 20 9.0 8.7
	1.76003	18	1.84738	26	0.15262	T.91266	9	52	
10	1.76021	18	1.84764	2"	0.15236	1.91257 1.91248	9	51	30 13.5 13.0 40 18.0 17.3
10	1.76039	18	T.84791		0.15209	1.91240	o	20	40 18.0 17.3 50 22.5 21.7
11	1.76057		T.84818	27	0.15182	1.01230	y	40	30 1 22.3 1 21.7
12	1.70057	18	I.84845	27	0.15162	I.91239	9	48	
13	I.76093	18	1.84872	27	0.15128	I.91221	9	47	
14	1.76111	18	T.84899	27	0.15101	Ī.01212	9	46	18
15	1.76129	18	T.84925	26	0.15075	7.91203	9	45	6 1.8
16	1.76146	17	T.84952	27	0.15048	Ĩ.91194	9	44	7 2.1 8 2.4
17	I.76164	18	1.84979	27	0.15021	1.91185	0	43	
16	T.76182	18	1.85006	27	0.14994	T.91176	õ	42	9 2.7
19	T.76200	18	T.85033	26	0.14967	1.91167	9	41	10 3.0
30	1.76218	18	1.85059		0.14941	Ĩ.91158	o	40	20 6.0 30 9.0
21	7 26006	10	T.85086	27		T OT T O	-	20	40 12.0
22	T.76236 T.76253	17	1.85080	27	0.14914 0.14887	T.91149 T.91141	8	39 38	50 15.0
23	1.76271	18	1.85140	27	0.14860	T.01132	9	37	
24	1.76289	18	1.85166	26	0.14834	1.91123	9	36	
25	1.76307	18	1.85193	27	0.14807	1.91114	0	35	
26	1.76324	17 18	1.85220	27	0.14780	Ī.91105	9	34	17
27	1.76342	18	1.85247	27	0.14753	¥0010.1	9	33	6 I.7
28	1.76360	18	1.85273	27	0.14727	1.91087	ö	32	7 I.O 8 2.3
29	1.76378	17	1.85300	27	0.14700	T.91078	9	31	
30	1.76395		1.85327		0.14673	¥.91069		30	9 2.6 10 2.8
		18	- 0	27		T avala	9		
31 32	1.76413 1.76431	18	T.85354 T.85380	26	0.14646	T.91060 T.91051	9	29 48	20 5.7 30 8.5
33	T.76448	17	1.85407	27	0.14593	I.91042	9	27	40 11.3
34	T.76466	18	T.85434	27	0.14566	I.91033	9	26	50 14.2
35	1.76484	18	1.85460	26	0.14540	T.91023	10	25	
36	1.76501	17	T.85487	27	0.14513	Ĩ.91014	9	24	
37	1.76519	18	1.85514	27 26	0.14486	T.91005	ö	23	10
38	1.76537	17	1.85540	27	0.14460	1.90996	9	22	10
40	Ī.76554 Ī.7657 2	18	T.85567 T.85594	27	0.14433	T.90987 T.90978	9	21	6 I.O 7 I.2
40	1.70572	18	1.05594	26	0.14406	1.909/0	ø	20	7 I.2 8 I.3
41	1.76500	10	1.85620	20	0.14380	T.00060	9	10	y 1.5
42	1.76590	17	T.85647	27	0.14353	T.90960	9	18	10 1.7
43	T.76625	18	1.85674	27	0.14353	T.90951	9	17	10 3.3
14	1.76642	17 18	1.85700	26	0.14300	T.90942	9	16	30 5.0
45	T.76660	18	1.85727	27	0.14273	T.90933	9	15	40 6.7
46	T.76677	17	T.85754	27	0.14246	T.90924	9	14	50 8.3
47	T.76695	17	1.85780	27	0.14220	1.90015	9	13	
48	1.76712	18	1.85807	27	0.14193	1.90906	10	12	
49	I.76730 I.76747	17	1.85834 7.85860	26	0.14166	T.90896 T.90887	9	11	9 8
50	1./0/4/	18	1.03000	27	0.14140	1.90007	9	10	6 0.9 0.8
51	1.76765		1.85887		0.14113	T.00878		D	7 1.1 0.9
52	1.76782	37	1.85913	26	0.14087	1.90869	9	Ē	8 1.2 1.1
53	1.76800	18	T.85940	27	0.14060	1.90860	9		9 I.4 I.2
54	1.76817	17 18	1.85907	27 26	0.14033	1.90851	9	76	IC 1.5 1.3
55	1.76835	10	T.85993	20	0.14007	T.90842	10	5	20 3.0 2.7 30 4.5 4.0
56	1.76852	18	1.86020	26	0.13980	1.90832	0	4	
57 58	I.76870 I.76887	17	T.86046 T.86073	27	0.13954	T.90823 T.00814	9	2	40 6.0 5.3 50 7.5 6.7
58	1.70887 1.76904	17	1.80073 1.86100	27	0.13927	1.90814 1.90805	9	2	
55	1.76922	18	I.80100 I.86126	26	0.13900	1.90805 T.90796	9	o	
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1	log sin	а	log tan	c. d.	log cot	log cos	а		p. p.
			= 0/ /						100
	T.76922	17	T.86126 T.86153	27	0.13874	1.90796	0	60	
1	1.70939 1.70957	18	1.86179	26	0.13847	I.90787 I.90777	10	59 58	27 26
3	1.70974	17	1.86206	27	0.13794	T.90768	19	57	6 2.7 2.6
3	1.76991	17	Y 80.22	26	0.13768	I.90759	- 19	56	
	T.77009	18	1.86259	27	0.13741	T.90750	M	55	7 3.2 3.0 8 3.6 3.5
56	1.770.26	17	1.86285	26	0.13715	T.90741	10	54	9 4.1 3.9
7	1.77043	17	T.86312	27	0.13688	T.90731	9	53	10 4.5 4.3
	1.77061	17	1.86338	27	0.13662	1.90722	9	52	20 9.0 8.7
9	1.77078	17	1.86365	27	0.13635	T.90713	9	51	30 13.5 13.0
10	1.77095	17	T.86392	26	0.13608	¥.90704	10	50	40 18.0 17.3 50 22.5 21.7
11	¥.77112	18	T.86418	27	0.13582	T.90694	0	49	
12	I.77130	17	T.86445	27	0.13555	1.90685	9	48	
13	1.77147	17	1.86471	27	0.13529	T.90676	9	47	
14	1.77164	17	1.86498	26	0.13502	1.90667	10	46	18
15 16	T.77181	18	1.86524 1.86551	27	0.13476	1.90657 1.90648	9	45	5 1.8
10	I.77199 I.77216	17	T.86577	26	0.13449 0.13423	1.90048 T.90639	9	43	7 2.1 8 2.4
18	T.77233	17	T.86603	26	0.13423	T.90630	9	43	9 2.7
19	T.77250	17	1.86630	27	0.13370	1.90620	10	41	10 3.0
20	1.77268	18	T.86656	26	0.13344	1.90611	9	100	200 6.0
	T an Q-	17	T 9440-	27	0.14415	Tachar	9		30 9.0 40 12.0
2I 22	I.77285 I.77302	17	T.86683 T.86709	26	0.13317 0.13291	T.90602 T.90592	10	39 38	50 15.0
23	I.77319	17	ī.86736	27	0.13264	I.90592 I.90583	9	30	
24	I.77336	17	1.86762	:::6	0.13238	1.90574	10	36	
25	1.77353	17	T.86789	27	0.13211	T.90565	9	35	
26	1.77370	17	1.86815	26	0.13185	T.90555	10	34	17
27	I.77387	17 18	1.86842	27	0.13158	T.90546	9	33	6 1.7
38	1.77405	17	1.86868	26	0.13132	1.90537	10	32	7 2.0 8 2.3
29	1.77422	17	1.86894	27	0.13106	1.90527	9	31	
30	1.77439	17	T.86921	26	0.13079	1.90518	o	30	10 2.8
31	T.77456		T.86947		0.13053	T.90509	-	20	2113 5.7
32	1.77473	17	1.86974	27	0.13026	T.90499	10	28	30 8.5
33	I.77490	17	1.87000	26 27	0.13000	T.90490	10	27	40 11.3
34	T.77507	17	T.87027	27	0.12973	T.90480	9	26	50 14.2
35	1.77524	37	1.87053	26	0.12947	T.90471	9	25	
36	I.77541 I 77558	17	1.87079 1.87106	27	0.12921	1.90462 1.00452	10	24	
37 38	I 77550 I.77575	17	1.87100	26	0.12894	T.90452	9	23	18
39	I.77592	17	1.87158	26	0.12842	T.90443	9	22	6 1.6
10	T.77609	17	T.87185	27	0.12815	T.90424	FO	20	7 1.9
		17	- 0	26	0	-	9		8 2.I 9 2.4
41	T.77626	17	I.87211	27	0.12789	1.90415	10	19	10 2.7
42	T.77643 T.77660	17	1.87238 1.87264	26	0.12762	T.90405 T.90396	9	18	
43 44	T.77677	17	1.87204	26	0.12736	T.90390 T.90386	10	17	20 5.3 30 8m
45	1.77694	17	1.87317	27	0.12683	I.90377	9	15	和日 10.7
46	1.77711	17	T.87343	26	0.12657	1.90368	10	14	50 13.3
47	I.77728	17 16	1.87309	26	0.12631	Ĩ.90358	10	13	
WB	1.77744	17	T.87396	26	0.12604	T.90349	10	1.2	
20	1.77761	17	I.87422	26	0.12578	T.90339	U	11	10 1 0
50	I.77778	17	T.87448	27	0.12552	T.90330	10	10	6 1.0 0.9
51	1.77795		T.87475		0.12525	1.90320		0	7 1.2 1.1
52	1.77812	17	1.87501	26 26	0.12499	T.90311	U 10	Ĕ	
53	1.77829	17	1.87527	20 27	0.12473	T.90301	0	7	9 1.5 1.4
54	1.77846	16	T.87554	26	0.12446	T.90292	10		10 1.7 1.5 20 3.3 3.0
55	1.77862	17	1.87580	26	0.12420	T.90282	N	Е	30 5.0 4.5
56	I.77879 I.77896	17	1.87606 1.87633	27	0.12394 0.12367	T.90273 T.90263	10	14	40 6.7 6.0
57 58	I.77090 I.77913	17	1.87033 1.87659	26	0.12307	1.90203	υ.	3	50 8.3 7.5
59	I.77930	17	1.87685	26	0.12341	T.90244	10	I	
60	1.77946	r6	1.87711	26	0.12289	¥.90235	9	0	
	log cos	a	log cot	c. d.	log tan	log sin	đ	'	p. p.
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,	log sin	а	log tan	c. d.	log cot	log cos	a		p. p.
0	I.77946	17	1.87711	27	0.12289	T.90235	10	60	
1	1.77963	17	1.87738	26	0.12262	1.90225	9	59	
2	1.77980	17	1.87764	26	0.12236	1.90216	10	58	27
3	1.77997	16	1.87790	27	0.12210	1.90206	9	57	5 2.7
14	1.78013	17	1.87817	26	0.12183	1.90197	10	56	7 3.2 B 3.6
5	I.78030	17	1.87843	26	0.12157	1.90187	9	55	
	1.78047	16	I.87869	26	0.12131	1.90178	10	54	0 4.1 10 4.5
2	1.78063 1.78080	17	1.87895	27	0.12105	T.90168	0	53	
		17	T.87922 T.87948	26	0.12078	I.90159	10	52 51	
10	T.78097 T.78113	16	1.87974	26	0.12026	T.90149 T.90139	10	50	30 13.5 40 18.0
8.03	1./0113		1.0/9/4	26	0.12020	1.90139	-	26	50 22.5
	0	17	= 00	20			9		30 1 00.3
II	T.78130	17	1.88000	27	0.12000	1.90130	IO	NO O	
12	1.78147	16	1.88027	26	0.11973	1.90120	9	48	
13	1.78163	17	T.88053 T.88079	26	0.11947	1.90111	10	47	28
14	1.78180 1.78197	17	1.88105	26	0.11921	1.90101 1.00001	10	46	5 2.6
15 16	1.78213	16	1.88131	26	0.11869	T.00082	73	45	
	1.78213 T.78230	17	1.88131 T.88158	27	0.11809	1.90082 1.90072	10	44	7 3.0
17 18	1.78230 1.78246	ró	1.88184	26	0.11816		9	43	
	1.78240	17	T.88210	26	0.11790	T.90053	10	42	
19	1.78280	17	1.88236	26	0.11790	1.90053 T.90043	10	41	10 4.3
100	1.70200	.6	1.00230	-6	0.11704	1.90043	-	qu	30 13.0
-		16	= 00 (26			10		40 17.3
21	1.78296	17	1.88262	27	0.11738	1.90034	10	39	50 21.7
22	Ĩ.78313	16	T.88289	26	0.11711	1.90024	10	38	30 1 21.7
23	1.78329	17	1.88315	26	0.11685	1.90014	0	37	
24	1.78346	16	1.88341	26	0.11659	1.90005	10	36	
25	T.78362	17	1.88367	26	0.11633	1.89995	10	35	17
20	T.78379	16	1.88393	27	0.11607	1.89985	0	34	
27	T.78395	17	1.88420	26	0.11580	T.89976	10	33	6 1.7
38	1.78412	16	T.88446	26	0.11554	T.89966	10	32	7 2.0
29	T.78428	17	1.88472	26	0.11528	ī.89956	9	31	
30	1.78445		T.88498		0.11502	T.89947		30	9 2.6
		16		26			10		10 2.8
31	1.78461	17	T.88524	26	0.11476	7.89937	10	20	100 5.7 30 8.5
32	1.78478	17	T.88550	20	0.11450	T.89927	9	28	
33	1.78494	16	1.88577	26	0.11423	1.89918	10	27	40 11.3
34	1.78510	17	T.88603	20	0.11397	1.89908	10	26	50 14.2
35	¥.78527	16	ī.88629	26	0.11371	ī.89898	10	25	-
36	T.78543	17	1.88655	26	0.11345	1.89888	9	24	
37	1.78560	16	7.88681	26	0.11319	1.89879	10	23	
38	1.78576	16	¥.88707	26	0.11293	T.89869	10	22	16
39	1.78592	17	T.88733	26	0.11267	ī.89859	10	21	6 1.6
10	I.78609		T.88759		0.11241	1.89849		20	7 1.9 8 2.1
		16		27			19		
41	T.78625	17	T.88786	26	0.11214	T.89840	10	19	0 2.4
42	1.78642	17	1.88812	20 26	0.11188	T.80830	10	18	10 2.7
43	T.78658	10	7.88838	20	0.11162	1.89820	10	17	20 5.3 30 8.0
44	I.78674	10	1.88864	20	0.11136	1.89810	10	16	
45	1.78691	16	1.88890	20	0.11110	1.89801	10	15	40 10.7
46	1.78707	10	T.88916	20	0.11084	T.89791	10	14	50 13.3
47	1.78723	16	1.88942	20	0.11058	1.89781	10	13	
48	1.78739	17	1.88968	20	0.11032	T.89771	10	12	
40	1.78756	16	T.88994	26	0.11006	1.89761	10	11	10 1 0
50	1.78772		I.89020		0.10980	T.89752		10	10 9
		16		26			10		6 1.0 0.9
51	1.78788	10	T.89046	200	0.10954	7.89742	871	10	7 1.2 1.1 8 1.3 1.2
52	1.78805	17	T.89073	27 26	0.10927	T.89732	10	И	
53	1.78821	10	1.80000	20	0.10001	1.80722	10	7	9 1.5 1.4
54	1.78837	16	1.89125	20	0.10875	1.89712	10		10 1.7 1.5
55	ī.78853	16	T.89151	20	0.10849	I.89702	10	5	20 3.3 3.0
56	T.78869	17	I.89177	20	0.10823	1.89693	10	4	30 5.0 4.5
57	T.78886	17	1.89203	20	0.10797	T.89683	10	3	40 6.7 6.0
58	1.78962	10	1.89229	0f	0.10771	T.89673	TO TO	2	50 8.3 7.5
89	1.78918	16	T.89255	26	0.10745	7.89663	10	I	
60	I.78934	.0	T.89281	-	0.10719	1.89653	.0	0	
							-		
	log cos	Ы	log cot	c. d.	log tan	log sin	а	1	p. p.

2	log sin	a	log tan	c.d.	log cot	log cos	d		p. p.
n	T.78934	16	T.89281	26	0.10719	¥.89653	FC	60	
1	1.78950	17	¥.89307	20	0.10693	T.89643	10	.59	00
2	T.78967 T.78983	16	T.89333 T.89359	26	0.10667	T.80633 T.80624	9	58 57	26 2.6 2.5
3	T.78993	16	I.89385	26	0.10041	T.80614	10	57	
	1.70015	16	T.80411	26	0.10589	T.80604	10	55	7 3.0 2.9 8 3.5 3.3
56	1.79031	16	1.89437	26	0.10563	T.89594	10	54	9 3.9 3.8
7	1.79047	16	1.89463	26	0.10537	1.80584	10	5.3	10 4.3 4.2 20 8.7 8.3
0	T.79063 T.79070	16	1.89489 T.89515	26	0.10511	T.89574 T.89564	0.0	52	20 8.7 8.3 30 13.0 12.5
10	T.79079	16	I.89541	26	0.10485	T.89554	10	50	40 17.3 16.7
		16		26			10	5-	50 21.7 20.8
11	T.79111	17	ī.89567	26	0.10433	T.89544	10	49	
12	1.79128	17	Y.89593	20	0.10407	1.89534	10	48	
13	T.79144	16	T.89619	26	0.10381	T.89524	10	47	17
14	T.79160 T.79176	16	T.89645 T.89671	26	0.10355 0.10329	T.89514 T.89504	10	46	8 1.7
16	1.79192	16	1.89697	26	0.10329	T.89504 T.89495	9	45	
17	1.79208	16 16	1.89723	26 26	0.10277	T.89485	10	43	7 2.0 8 2.3
18	1.79224	16	T.89749	20	0.10251	7.89475	10	42	12 2.6
19	T.79240	16	1.89775	26	0.10225	1.89465	10	41	10 2.8
20	1.79256	16	T.89801	26	0.10199	Ĩ.89455	10	40	BO 5.7 10 8.5
21	T.79272		1.80827		0.10173	T.89445	10	39	10 11.3
22	T.79288	16	T.89853	26	0.10147	1.80425	10	39	50 14.2
23	1.79304	16	T.80870	26 26	0.10121	1.80425	10	37	
24	1./9319	15 16	T.89905	20	0.10095	1.80415	10	36	
25	T.79335	10	1.89931	26	0.10069	1.89405	10	35	10 . 10
26 27	T.79351 T.79367	16	¥.89957 ¥.89983	26	0.10043	T.89395 T.89385	10	34 33	16 15 6 1.6 1.5
1	I.79383	16	T.90009	26	0.00017	T.89305	10	33	6 1.6 1.5 7 1.9 1.8
29	T.79399	16	T.90035	26 26	0.09965	1.89364	11	31	8 2.1 2.0
30	T.79415		¥.90061	-	0.09939	T.89354		30	9 2.4 2.3
		16		25			10	-	10 2.7 2.5 20 5.3 5.0
31	1.79431	16	¥.90086	26	0.09914	1.89344	10	29	20 5.3 5.0 30 8.0 7.5
32	T.79447 T.79463	16	T.90112 T.90138	26	0.09888	T.89334 T.89324	10	28 27	40 10.7 10.0
33 34	1.79403	15	T.00164	26	0.09836	T.89314	10	26	50 13.3 1 12.5
35	T.79494	16	1.90190	26 26	0.09810	1.89304	10 10	25	
36	1.79510	16	1.90216	26	0.09784	1.89294	10	24	
37 38	¥.79526	16	T.90242	26	0.09758	1.89284 1.89274	10	23	11
30	I.79542 I.79558	16	T.90268	26	0.09732	1.89274 T.89264	10	22	6 1.1
40	I.79573	15	1.90320	26	0.09680	1.89254	10	20	7 1.3
-		16		26			10		
41	¥.79589	16	1.90346		0.09654	T.89244	11	19	U 1.7 10 1.8
42	1.79605	10	T.90371	25 26	0.09629	1.89233	11	18	10 1.8 10 3.7
43	Ĩ.79621	15	T.90397	26	0.09603	T.89223	10	17	30 5.5
44	T.79636 T.79652	16	T.90423 T.90449	26	0.09577 0.09551	T.89213 T.89203	10	16 15	40 7.3
46	1.79668	10	I.90449 I.90475	26	0.09531	1.89193	10	14	50 9.2
47 48	1.79684	10	1.90501	26 26	0.09499	T.89183	10	13	
	1.79699	15	1.90527	20	0.09473	1.89173	10	13	
40	I.79715	16	T.90553	25	0.00447	T.89162 T.89152	10	11	10 : 9
50	1.79731	15	1.90578	25	0.09422	1.09152	10	10	6 1.0 0.9
51	1.79746	-	¥.00604		0.09396	T.80142		0	7 1.2 1.1
52	1.79762	16	¥.90630	100	0.09370	¥.89132	10	9	
53	¥.79778	15	1.90656	26 26	0.09344	T.80122	10 10	76	9 1.5 1.4 10 1.7 1.5
54	T.79793	16	1.90682	26	0.09318	7.80112	11		20 3.3 3.0
55 56	1.79809	16	T.90708 T.90734	26	0.09292	1.89101 1.89001	10	5	30 5.0 4.5
57	1.79840	15	1.90734	25	0.09200	1.80081	10	3	40 6.7 6.0
58	1.79856	16	1.90785	26	0.09215	7.89071	10	2	50 8.3 7.5
59	1.79872	10	7.90811	20	0.09189	1.89060	11	I	
60	1.79887	13	1.90837	-	0.09163	1.89050		Ø	

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	log sin	a	log tan	c. d.	log cot	log cos	đ		p. p.
0	T.79887		T.90837		0.09163	T.89050		60	
I	Ĩ.79903	16	T.90863	26	0.09137	T.80040	IO		
2	1.79918	15	T.90889	26	0.00111	Y.89030	10	59 58	26
U	1.79934	16	T.90914	25 26	0.09086	T.89020	10	57	6 2.6
4	I.79950	15	1.90940	20	0.09060	T.89009	IO	56	7 3.0
5	1.79965	16	T.90966	26	0.09034	T.88999	10	55	- 00
	T.79981	15	T.90992	26	0.09008	1.88989	11	54	9 3.9
78	T.79996 T.80012	16	1.91018	25	0.08982	T.88978 T.88968	10	53	10 4.3
ö	I.80012	15	I.91043 I.91069	26	0.08957	1.88958	10	52 51	30 8.7
10	T.80043	16	T.91005	26	0.08905	1.88948	IO	50	40 17.3
		15	1191095	26	0.00903	1100940	II	30	50 21.7
11	1.80058		1.01121		0.08879	T.88937		30	
12	¥.80074	16	1.91147	26	0.08853	7.88927	10	48	
13	ī.80089	15 16	T.91172	25 06	0.08828	T.88917	10 11	47	
14	1.80105	10	1.91198	26	0.08802	T.88906	11	46	25
15	T.80120	16	Y.91224	26	0.08776	T.88896	10	45	6 2.5
16	T.80136	15	1.91250	26	0.08750	T.88886	11	44	7 2.9
17	T.80151 T.80166	15	T.91276	25	0.08724	T.88875 T.88865	10	43	
10	T.80182	16	T.91301 T.91327	26	0.08699	1.88855	10	42	0 3.8 10 4.2
19	T.80102	15	I.91327 I.91353	26	0.08647	1.00055	11	41	10 4.2
		16		26	510004/		10	40	30 12.5
21	7.80213		1.91379		0.08621	T.88834		39	40 16.7
22	T.80228	15 16	1.91404	25 26	0.08596	1.88824	IO	38	50 20.8
23	1.80244	10	T.91430	20	0.08570	1.88813	11	37	
24	Y.80259	15	T.91456	26	0.08544	1.88803	10	36	
25	1.80274	iń	T.91482	25	0.08518	T.88793	11	35	16
20	T.80290 T.80305	15	I.91507	26	0.08493	T.88782 T.88772	10	34	6 1.6
27	T.80320	15	T.91533 T.91559	26	0.08407	1.88761	II	33 32	
29	T.80336	16	T.91585	26	0.08415	T.88751	IO	32	7 1.9
30	T.80351	15	T.91610	25	0.08390	1.88741	10	30	0 2.4
0-		15		26	0100390		II	30	10 2.7
31	T.80366	16	1.91636	26	0.08364	T.88730		29	20 5.3
32	1.80382	10	1.91662	26	0.08338	1.88720	10	28	
33	1.80397	15	ĩ.91688	20	0.08312	1.88709	11	27	#0 10.7
34	T.80412	iń	1.91713	26	0.08287	T.88699	11	26	50 13.3
35	T.80428 T.80443	15	1.91739	26	0.08261	1.88688	10	25	
36	1.80443	15	T.91765	26	0.08235	T.88678 T.88668	10	24	
38	1.80458	15	1.91791 1.91816	25	0.08209	I.88657	II	23	15
30	T.80489	16	1.91842	26	0.08158	1.88647	10	21	
40	T.80504	15	T.91868	36	0.08132	T.88636	11	20	
		15		25			10		8 2.0
41	T.80519	15	1.91893	26	0.08107	T.88626	11	19	9 2.3
42	T.80534	16	T.91919	20	0.08081	1.88615	ID	18	10 2.5
43	T.80550	15	T.91945	26	0.08055	T.88605	II	17	30 7.5
44	1.80565 7.80580	15	T.91971 T.91996	25	0.08029	1.88594 1.88584	10	16	40 10.0
45 46	1.80500 T.80595	15	1.91990 T.02022	26	0.08004	I.88584 I.88573	II	15 14	50 12.5
47	T.80610	15	I.02048	шó	0.07978	T.88563	10	14	
48	1.80625	15	1.92073	25	0.07952	T.88552	II	13	
49	T.80641	16	T.92099	26	0.07901	1.88542	100	11	
50	1.80656	15	T.92125	26	0.07875	T.88531	II	10	11 10
		15		25			10		6 1.1 1.0
51	1.80671	15	1.92150	26	0.07850	7.88521	11	8	7 1.3 1.2 B 1.5 1.3
52	1.80686	15	1.92176	20	0.07824	1.88510	11		
53 54	T.80701 T.80716	15	T.92202 T.92227	25	0.07798	T.88499 T.88489	10	76	9 1.7 1.5 10 1.8 1.7
54	T.80731	15	T.92227 T.92253	26	0.07773 0.07747	1.88478	11	5	20 3.7 3.3
56	T.80746	15	T.92279	86	0.07721	T.88468	10	4	30 5.5 5.0
57	T.80762	16	1.92304	25	0.07696	1.88457	11	3	40 7.3 6.7
57 58	1.80777	15 15	T.92330	26 26	0.07670	T.88447	16	2	50 9.2 8.3
59	1.80792	15	¥.92356	20	0.07644	1.88436	11	1	
00	1.80807	-3	¥.92381	-3	0.07619	T.88425		a	
	log cos	d	log cot	c. d.	log tan	log sin	a	,	p. p.
			108 000	A1 181	toP com	108 DIT	-		Bar Bar

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*	log sin	Ø	log tan	c. đ.	log cot	log cos	đ		p. p.
			X		0.000	7.90		-	
ō	T.80807 T.80822	15	1.92381	26	0.07619	1.88425 1.88415	10	60	
1	T.80837	15	T.92407 T.92433	26	0.07593	1.88404	II	59 58	26
3	1.80852	15	T.92458	25	0.07542	T.88304	IO	57	6 2.6
4	7.80867	15	1.92484	26	0.07516	1.88383	II	56	
5	1.80882	15	T.92510	26	0.07490	T.88372	11	55	7 3.0 8 3.5
5	I.80897	15 15	T.92535	25	0.07465	T.88362	10	54	9 3.9
7	1.80912	15	¥.92561	26	0.07439	T.88351	11	53	10 4.3 20 8.7
	1.80927	15	1.92587	25	0.07413	1.88340	10	52	
10	T.80942 T.80957	15	T.92612 T.92638	26	0.07388	1.88330 1.88319	11	51	30 13.0
10	1.00957		1.92030		0.07302	1.00319	II	50	40 17.3 50 21.7
11	T.80972	15	T.92663	25	0.05005	T.88308	**		30 1 21.1
12	1.80972	15	1.92003	26	0.07337	1.88208	10	40	
13	T.81002	15	T.92715	26	0.07285	1.88287	11	47	
14	T.81017	15	1.92740	25	0.07260	T.88276	11	46	25
15	1.81032	15	T.92766	26	0.07234	T.88266	10	45	6 2.5
16	1.81047	15 14	1.92792	25	0.07208	T.88255	11	33	7 2.9
17	1.81061	14	1.92817	26	0.07183	Y.88244	10	43	8 3.3
18	1.81076	15	1.92843	25	0.07157	¥.88234	11	42	9 3.8
19	1.81091	15	1.92868	26	0.07132	1.88223	11	41	10 4.2 20 8.3
20	7.81106		I.92894	26	0.07106	1.88212	11	40	20 8.3 30 12.5
	T.81121	15	Tanan	20	0.00090	T.88201	11	10	40 16.7
21	1.81121 T.81136	15	T.92920 T.92945	25	0.07080	1.88201 7.88101	10	39 38	50 20.8
23	1.81151	15	I.92945 I.92971	26	0.07055	1.88180	11	30	
24	T.81166	15	1.92996	25	0.07004	T.88160	11	36	
25	T.81180	14	T.03022	26	0.06978	1.88158	II	35	
26	1.81195	15	1.93048	26 25	0.06952	1.88148	10	34	15
27	1.81210	15 15	T.93073	26	0.06927	T.88137	11	33	6 I.5 7 I.8
28	1.81225	15	T.93099	25	0.06901	T.88126	11	32	
23	1.81240	14	T.93124	26	0.06876	T.88115	10	31	
30	1.81254		1.93150		0.06850	T.88105		30	10 2.3 10 2.5
	1.81260	15		25	0.06825	7.88004	11	20	201 5.0
31 32	1.81284	15	T.93175 T.93201	26	0.00825	T.88083	11	29	30 7.5
33	1.81200	15	I.93201 I.93227	26	0.00799	1.88072	11	20	10.0
34	1.81314	15	T.93252	25	0.06748	1.88061	11	26	50 12.5
35	1.81328	14	T.93278	10	0.06722	T.88051	10	25	
36	I.81343	15 15	T.93303	25 26	0.06697	1.88040	11	24	
37	1.81358	14	1.93329	25	0.06671	T.38029	II	23	14
38	T.81372 T.81387	15	T.93354	26	0.06646	T.88018 T.88007	II	22	6 1.4
39 40	I.81307 I.81402	15	T.93380 T.93406	26	0.06620	I.88007 I.87996	11	21	
40	1.01402		1.93400	25	0.00594	1.0/990	11	20	7 I.6 1.9
41	1.81417	15	Torres	25	0.06560	T.87985		10	10 2.I
41 42	1.81417 1.81431	14	T.93431 T.93457	26	0.00509	1.87985 1.87975	10	19 18	10 2.3
43	1.81446	15	I.93457 I.93482	25	0.00543	1.87964	11	17	III 4.7
44	7.81461	15	1.93508	26	0.06492	T.87953	11	16	30 7.0
45	1.81475	14 15	T.93533	25 26	0.06467	1.87942	II	15	40 9.3
46	T.81490	15	T.93559	20	0.06441	T.87931	II	14	10 11.7
47	1.81505	14	7.93584	26	0.06416	1.87920	II	13	
48	T.81519 T.81534	15	T.93610 T.93636	16	0.06390	T.87909 T.87898	11	12 11	
49 50	T.81549	15	1.93030 T.93661	25	0.00304	1.87887	11	11	11 10
30	101349	14	1193001	156	0.00333	1.07007	10		6 1.1 1.0
51	1.81563		1.93687	1 1	0.06313	T.87877		ø	7 1.3 1.2
52	1.81578	15	I.93712	25	0.06288	1.87866	11	8	
53	1.81592	14 15	1.93738	26 25	0.06262	1.87855	11	7	9 1.7 1.5 10 1.8 1.7
54	1.81607	15	1.93763	25	0.06237	T.87844	II		10 1.8 1.7 20 3.7 3.3
55	1.81622	14	1.93789	25	0.06211	1.87833	II	Б	30 5.5 5.0
56 57	I.81636 I.81651	15	1.93814 1.93840	26	0.06186	T.87822 T.87811	11	4	40 7.3 6.7
57 58	1.81051 T.81665	14	1.93840	25	0.00100	T.87800	II	8	50 9.2 8.3
59	I.81680	15	1.93891	26	0.06109	1.87789	11	1	
60	1.81694	14	¥.93916	25	0.06084	I.87778	II	D	
	log cos	a	log cot	c. d.	log tan	log sin	a	,	p. p.

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J	log sin	d	log tan	c. d.	log cot	log cos	a		p. p.
0	¥.81694		T.03016		0.06084	T.87778		60	
1	1.81709	15	T.93942	26	0.06058	T.87767	II	59	
2	I.81723	14	T.93967	25	0.06033	I.87756	II	59	26
	T.81738	15	T.93993	26	0.06007	I.87745	II	57	6 2.6
4	1.81752	14	T.94018	25	0.05982	1.877.34	11	56	
	1.81767	15	1.94044	26	0.05956	1.87723	II	55	7 3.0 8 3.5
56	1.81781	14 15	1.94069	25 26	0.05931	7.87712	11	54	9 3.9
7	ī.81796	14	T.94095	25	0.05905	1.87701	11	53	10 4.3 20 8.7
	T.81810	15	T.94120	26	0.05880	I.87690	II	52	
Ø	1.81825	14	T.94146	25	0.05854	T.87679 T.87668	11	51	30 13.0
10	T.81839	15	1.94171	26	0.05829	1.07000	11	50	40 17.3 50 21.7
11	T.81854		T.94197		0.05803	1.87657		49	201000
12	T.81868	14	1.94222	25	0.05778	1.87646	II	48	
13	T.81882	14	T.94248	26	0.05752	T.87635	11	47	
14	1.81897	15	T.94273	25 26	0.05727	T.87624	11 11	46	25
15	T.81911	14 15	T.94299	20	0.05701	T.87613	11	45	6 2.5
16	T.81926	15	Ī.94324	26	0.05676	1.87601	12	44	7 2.9
17	1.81940	15	1.94350	25	0.05650	1.87590	II	43	
18	1.81955	14	1.94375	26	0.05625	1.87579 1.87568	II	42	9 3.8
19 20	T.81969 T.81983	14	1.94401 7.04426	25	0.05599	1.87568 1.87557	11	41 40	10 4.2 20 8.3
20	1.01903	15	T.94426	16	0.05574	1.0/55/	11	40	30 12.5
21	¥.81998		T.94452		0.05548	T.87546		39	40 16.7
22	1.82012	14	1.94477	25	0.05523	1.87535	11	38	50 20.8
23	1.82026	14	1.94503	26	0.05497	I.87524	II	37	
24	T.82041	15	T.94528	25 26	0.05472	1.87513	11	36	
25	1.82055	14 14	1.94554	20	0.05446	1.87501	12	35	
26	¥.82069	14	T.94579	25	0.05421	1.87490	II	34	15
27	1.82084	14	T.94604	26	0.05396	1.87479	11	33	6 1.5 7 1.8
28	1.82098	14	T.94630	25	0.05370	1.87468	II	32	
19 30	T.82112 T.82126	14	T.94655 T.94681	26	0.05345	1.87457 1.87446	II	31	8 2.0
30	1.02120		1.94001	25	0.05319	1.07440	12	30	9 2.3
31	T.82141	15	1.94706		0.05204	1.87434		20	20 5.0
32	1.82155	14	I.94732	26	0.05268	1.87423	II	28	30 7.5
33	T.82169	14	1.94757	25	0.05243	1.87412	II	27	40 10.0
34	1.82184	15	Ī.94783	26	0.05217	1.87401	II	26	50 12.5
35	1.82198	14	1.94808	25 26	0.05192	T.87390	11	25	
36	1.82212	14	1.94834	25	0.05166	1.87378	12	24	
37	T.82226	14	1.94859	25	0.05141	1.87367	II	23	
38	1.82240	15	1.94884	26	0.05116	1.87356	11	22	14
210 HD	1.82255 1.82269	14	T.94910 T.94935	25	0.05090	T.87345 T.87334	II	21	6 I.4 7 I.6
HELD .	1.02209	14	**99933	36	0.03003	1.07334	12	-	7 1.6 8 1.9
41	¥.82283		1.94961		0.05039	T.87322		10	9 2.1
42	1.82207	14	1.94986	25	0.05014	1.87311	II	18	10 2.3
43	1.82311	14	T.95012	26	0.04988	1.87300	II	17	20 4-7
44	I.82326	15 14	Ĩ.95037	25	0.04963	1.87288	12	16	20 7.0
45	T.82340	14	1.95062	25	0.04938	1.87277	11	15	40 9.3
46	T.82354	14	1.95088	25	0.04912	T.87266	11	14	50 11.7
47	1.82368	14	1.95113	26	0.04887	1.87255	12	13	
48	T.82382 T.82396	14	Ĩ.95139	25	0.04861	T.87243 T.87232	11	12	
49	I.82390 I.82410	14	T.95164 T.95190	26	0.04836	I.87232 I.87221	II	10	12 11
200	1.02410	14	1.93190	25	0.04010	1.0/201	12		6 1.2 1.1
51	T.82424		T.95215	-	0.04785	1.87209		σ	7 1.4 1.3
52	T.82439	15	1.95240	25	0.04760	1.87108	II	8	8 1.6 1.5
53	T.82453	14	T.95266	26 25	0.04734	T.87187	11	7	9 1.8 1.7
54	1.82467	14	1.95291	25	0.04700	T.87175	12	6	
55	1.82481	14	1.95317	25	0.04683	1.87164	11	5	20 4.0 3.7 30 6.0 5.5
56	T.82495	14	I.95342	26	0.04658	Y.87153	12	H.	40 8.0 7.3
57 58	1.82509 1.82523	14	T.95368	25	0.04632	T.87141 T.87130	11	3	50 10.0 9.2
50 59	1.82523 1.82537	14	T.95393 T.95418	25	0.04007	T.87130	11	I	
59	I.82551	14	T.95444	26	0.04556	1.87107	12	ò	
	log cos	a	log cot	c. d.	log tan	log sin	a	,	p. p.
	INE COS		TOR COL	G. U.	10g tall	IOE SIT	u		p. p.

7	log sin	a	log tan	c. d.	log cot	log cos	a		p. p.
	1 82551					1.87107		60	
0	1.82565	14	T.95444 T.05460	25	0.04556	1.87107	11		
	T.82579	14	1.95409	26	0.04531	1.87085	11	59 58	26
1 8	1.82593	14	1.95520	25	0.04480	1.87073	12	57	6 2.6
1	1.82607	LI	T.95545	25	0.04455	T.87062	11	56	
5	7.82621	14	1.95571	106	0.04429	1.87050	12	55	7 3.0 3.5
16	1.82635	14	T.95596	25 26	0.04404	1.87030	II	54	3.9
7	T.82649	14	T.95622	25	0.04378	T.87028	12	53	110 4.3 150 8.7
	T.82663	Id	I.95647	25	0.04353	I.87016	11	52	
15	1.82677	14	I.95672	26	0.04328	1.87005	12	51	30 13.0
10	¥.82691		I.95698		0.04302	T.86993	1	20	470 17.3 300 21.7
i	-	14		25		- 01 0	11		30 21.7
11	T.82705 T.82719	14	1.95723	25	0.04277	T.86982 T.86970	12	40	
12	I.82719 I.82733	14	T.95748 T.95774	26	0.04252	1.80970 T.80950	II	48	
13	I.82747	14	I.95774 I.95799	25	0.04220	T.86947	12	47	06
15	T.82761	14	Ī.95825	UM	0.04175	1.86936	II	45	6 2.5
16	T.82775	14	1.95850	25	0.04150	1.86924	12	45	7 2.9
17	1.82788	13	T.95875	25	0.04125	T.86913	II	43	8 3.3
18	1.82802	14	T.95901	26	0.04099	1.86902	II	42	3.8
10	1.82816	14	T.95926	25	0.04074	1.86890	12 11	41	10 4.2
20	T.82830		¥.95952		0.04048	T.86879		40	20 8.3 30 12.5
21	T.82844	14	1.95977	25	0.04023	1.86867	12	IIQ	#0 16.7
22	T.82858	14	1.96002	25	0.03998	7.86855	12	38	ão 20.8
23	T.82872	14	T.96028		0.03972	T.86844	II	37	
24	T.82885	13	T.96053	25 25	0.03947	ī.86832	12 11	36	
25	1.82899	14	T.96078	25	0.03922	7.86821	11	35	
26	T.82913	Id	7.96104	25	0.03896	1.86809	12	34	14
27	I.82927 I.82941	14	1.96129	26	0.03871	I.86798	12	33	6 1.4
25	1.82941 1.82955	14	T.96155 T.96180	25	0.03845	7.86786 7.86775	11	32	7 1.6
30	1.82955	13	T.96205	25	0.03820	T.86775 T.86763	12	31 30	西 1.9 元 2.1
10	1.02900	14	1.90205	26	0.03795	1.00/03	11	30	10 2.3
31	T.82982	14	T.96231	203	0.02760	1.86752	11	20	20 4.7
32	1.82992	14	T.96256	25	0.03769	1.80752	12	29	30 7.0 .
33	T.83010	14	1.96281	25	0.03719	T.86728	12	27	9.3
34	¥ 82022	13	1.96307	26	0.03693	1.86717	II	26	50 11.7
35	T.83037	14	T.96332	25	0.03668	T.86705	12	25	
36	1.83051	14	1.96357	25	0.03643	T.86694	11	24	
37	1.83005	13	1.96383	25	0.03617	1.86682	12	23	
38	1.83078	14	1.96408	25	0.03592	1.86670	II	22	13
30	I.83092	14	1.96433	26	0.03567	T.86659	12	21	6 1.3
40	I.83106		I.9 6459		0.03541	1.86647	100	20	7 I.5 I I.7
47	1.83120	14	¥ 06.9.	25	0.00016	¥ 966ar	12	10	1.7
41	1.83120 T.83133	13	T.96484 T.96510	зó	0.03516	T.86635 T.86624	11	19	10 2.2
43	T.83147	14	1.96535	25	0.03490	T.86612	12	17	20 4.3
44	T.83161	14	T.96560	25	0.03440	1.86600	12	16	30 6.5
45	T.83174	13	T.96586	26	0.03414	T.86589	II	15	AN 8.7
46	7.83188	14	7.96611	25 25	0.03389	T.86577	12 12	14	Ma 10.8
47	1.83202	14	T.96636	25	0.03364	T.86565	12	13	
48	1.83215	13	1.96662	25	0.03338	T.86554	11	12	
49	I.83229 I.83242	13	1.96687	25	0.03313	T.86542	12	11	12 11
50	1.03243	14	T 96712	26	0.03288	1.86530	12	10	6 1.2 1.1
51	¥.83256		T.96738		0.03262	¥.86518			7 1.4 1.3
52	T.83270	14	1.96763	25	0.03237	1.86507	11	6	
5.3	1.83283	13	1.96788	25 106	0.03212	1.86495	12	7	9 1.8 1.7 10 2.0 1.8
54	T.83297	13	1.96814	25	0.03186	1.86483	11	iii i	20 4.0 3.7
55 56	T.83310	14	T.96839	25	0.03161	T.86472	12	3	30 6.0 5.5
50	1.83324 1.83338	14	1.96864 1.96890	26	0.03136	T.86460 T.86448	12		40 8.0 7.3
57	T 82251	13	1.90590 T.96915	25	0.03110	1.80448 1.86436	12	13	50 10.0 9.2
	T.83365	14	1.96940	25	0.03065	T.86425	11	I	
59 60	1.83378	13	T.96966	26	0.03034	T.86413	12	ò	and the second se
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	log cos	đ	log cot	c. d.	log tan	log sin	а	1	p. p.

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,	log sin	đ	log tan	c. d.	log cot	log cos	a		p. p.
Ð	I.83378	14	1.96966	25	0.03034	1.86413	12	60	
I	1.83392	13	1.96991	25	0.03009	1.86401	12	59	
2	1.83405	14 -	T.97016	26	0.02984	1.86389	12	58	28
3	1.83419	13	1.97042	25	0.02958	1.86377	11	57	6 2.6
R.	T.83432 T.83446	14	1.97067	25	0.02933	T.86366 T.86354	12	56	7 3.0 B 3.5
5	T.83440	13	1.97092 1.97118	26	0.02908	1.00354 T.86342	12	55	
	T.83473	14	1.97113	25	0.02857	T.86330	12	53	9 3.9
7	1.034/3	13	1.97143 1.97168	25	0.02832	1.86318	12	53	10 4.3 20 8.7
0	T.83500	14	I.97103	25	0.02807	1.86306	12	51	30 13.0
10	1.83513	13	1.97219	26	0.02781	1.86295	II	50	40 17.3
		14		25	0.00,00		12	5-	50 21.7
11	T.83527	- 10	T.97244	*3	0.02756	T.86283		49	
12	T.83540	13	1.97269	25	0.02731	1.86271	12	48	
13	T.83554	14	1.97295	26	0.02705	T.86250	12	47	
14	I.83567	13	I.97320	25	0.02680	1.86247	12	46	25
14	7 82581	14	1.97345	25	0.02655	1.86235	12	45	6 2.5
16	T.83594	13	T.97345	26	0.02620	1.86223	12	43	
17	1.83608	14	T.97396	25	0.02604	1.86211	12	43	7 2.9 8 3.3
18	1.83621	13	1.97421	25	0.02579	1.86200	11	42	8 3.3 9 3.8
19	1.83634	13	Ī.97447	26	0.02553	1.86188	12	41	10 4.2
20	1.83648	14	T.97472	25	0.02528	1.86176	12	40	20 8.3
		13		25			12		30 12.5
21	1.83661	-	T.97497		0.02503	T.86164		39	48 16.7
22	1.83674	13	T.07523	26	0.02477	1.86152	12	38	50 20.8
23	T.83688	14	I.97548	25	0.02452	1.86140	12	37	
24	1.83701	13	Ī.97573	25	0.02427	1.86128	12	36	
25	1.83715	14 13	1.97598	25 26	0.02402	T.86116	12	35	
26	1.83728	13	1.97624	25	0.02376	1.86104	12	34	14
27	1.83741	13	T.97649	25	0.02351	T.86092	12	33	· 6 1.4
58	1.83755	13	T.97674	26	0.02326	T.86080	12	32	7 16
129	1.83708	13	I.97700	25	0.02300	T.86068	12	31	
30	1.83781		Ī.97725	-	0.02275	1.86056		30	5 2.1
		14		25	-		12		10 2.3
31	1.83795	13	T.97750	26	0.02250	T.86044	12	29	20 4.7
32	1.83808	13	Ī.97776	25	0.02224	1.86032	12	28	30 7.0
33	1.83821	13	1.97801	25	0.02199	1.86020	12	27	40 9.3
34	1.83834	14	1.97826	25	0.02174	1.86008	12	26	50 1 11-7
35	1.83848	13	1.97851	26	0.02149	1.85996	12	25	
36	I.83861 I.83874	13	I.97877	25	0.02123	1.85984 1.85972	12	24 23	
37 38	I.83887	13	I.97902	25	0.02098	1.85972 T.85960	12	23	13
30	1.03007	14	T.97927 T.97953	26	0.02073	T.85948	12	22	6 1.3
40	1.83914	13	I.97953	25	0.0204/	1.85936	12	21	
40	1.039.0	13	1.9/9/5	25	5105086	1103930	12		7 1.S B 1.7
41	T.83927	13	7.08003	-	0.01997	T.85924	14	19	0 2.0
41 42	1.83927 1.83940	13	1.98003 T.98020	26	0.01997	T.85912	12	19	10 2.2
42	I.83940 I.83954	14	T.98029 T.98054	25	0.01946	1.85900	12	10	20 4.3
43	1.83967	13	1.98079	25	0.01921	1.85888	12	16	30 6.5
45	T.83980	13	1.98104	25	0.01896	1.85876	12	15	40 8.7
46	7.83993	13	1.98130	26	0.01870	T.85864	12	14	B0 10.8
47	1.84006	13	1.98155	25	0.01845	1.85351	13	13	
48	1.84020	14	T.98180	25	0.01820	1.85839	12	13	
149	I.84033	13	7.98206	20	0.01794	1.85827	12	II	
50	I.84046	13	1.98231	63	0.01769	1.85815	1.0	10	12 11
		13		25			12		6 1.2 1.1
51	T.84059	_	1.98256		0.01744	T.85803	12	9	7 1.4 1.3 8 1.6 1.5
52	1.84072	13	1.98281	25 26	0.01719	1.85791	12	8	
53	¥.84085	13	1.98307	20	0.01693	T.85779	12	7 15	9 1.8 1.7
54	T.84098	13	T.98332	25	0.01668	1.85766	13		10 2.0 1.8 20 4.0 3.7
55	1.84112	13	T.98357	20	0.01643	1.85754	12	5	30 6.0 5.5
56	1.84125	13	1.98,183	25	0.01617	1.85742	12		40 8.0 7.3
57	1.84138	13	1.08408	25	0.01592	T.85730	12	8	50 10.0 9.2
58	T.84151 T.84164	13	T.98433 T.98458	25	0.01567 0.01542	T.85718 T.85706	12	2	Do I coud I ha
59	T.84177	13	I.98484	26	0.01516	I.85693	13	0	
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1 2 3 14 5 16 7 18 19 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 24 25 6 27 18 19 20 21 24 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 24 25 6 27 18 19 20 20 21 24 24 25 6 27 18 19 20 20 21 24 25 6 27 18 19 20 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 20 21 24 25 6 27 18 19 20 20 21 24 25 6 27 18 19 20 20 21 24 25 6 27 18 19 20 20 20 21 24 25 6 27 18 19 20 20 20 20 20 20 20 20 20 20 20 20 20	I.84100 I.84203 I.84220 I.84229 I.84229 I.84229 I.84255 I.84255 I.84255 I.84255 I.84308 I.84308 I.84321 I.84309 I.84321 I.84309 I.84321 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.8437 I.84327	13 13 13 13 13 13 13 13 13 13 13 13 13 1	1.98509 1.98534 1.98560 1.98585 1.98685 1.98611 1.98686 1.98711 1.98737 7.98762 1.98787 1.98812 1.98838	25 26 25 25 25 25 25 25 25 26 25 25 25	0.01491 0.01466 0.01440 0.01415 0.01390 0.01365 0.01339 0.01314 0.01289 0.01263	1.85681 1.85669 1.85657 1.85645 1.85632 1.85608 1.85506 1.85596 1.85583	12 12 12 12 12 12 12 12 13	59 57 56 55 54 53 52 51	7 8 10	2.6 3.0 3.5 3.9 4.3
1 2 3 14 5 16 7 18 19 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 24 25 6 27 18 19 20 21 24 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 24 25 6 27 18 19 20 20 21 24 24 25 6 27 18 19 20 20 21 24 25 6 27 18 19 20 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 21 24 25 6 27 18 19 20 20 21 24 25 6 27 18 19 20 20 21 24 25 6 27 18 19 20 20 21 24 25 6 27 18 19 20 20 20 21 24 25 6 27 18 19 20 20 20 20 20 20 20 20 20 20 20 20 20	I.84100 I.84203 I.84220 I.84229 I.84229 I.84229 I.84255 I.84255 I.84255 I.84255 I.84308 I.84308 I.84321 I.84309 I.84321 I.84309 I.84321 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.84326 I.84327 I.8437 I.84327	13 13 13 13 13 13 13 13 13 13 13 13 13 1	1.98509 1.98534 1.98560 1.98585 1.98685 1.98611 1.98686 1.98711 1.98737 7.98762 1.98787 1.98812 1.98838	25 26 25 25 25 25 25 25 25 26 25 25 25	0.01491 0.01466 0.01440 0.01415 0.01390 0.01365 0.01339 0.01314 0.01289 0.01263	1.85681 1.85669 1.85657 1.85645 1.85632 1.85608 1.85506 1.85596 1.85583	12 12 12 12 12 12 12 12 13	59 57 56 55 54 53 52 51	7 8 10	2.6 3.0 3.5 3.9 4.3
2 3 4 5 6 7 6 9 10 11 2 13 4 5 16 7 18 9 20 21 22 23 4 25 6 27 1 19 20 21 22 23 24 25 6 27 1 19 20 21 22 23 24 25 6 27 1 19 20 20 20 20 20 20 20 20 20 20 20 20 20	$\begin{array}{c} 1.84_{203}\\ 1.84_{204}\\ 1.84_{204}\\ 1.84_{204}\\ 1.84_{205}\\ 1.84_{205}\\ 1.84_{205}\\ 1.84_{205}\\ 1.84_{205}\\ 1.84_{205}\\ 1.84_{205}\\ 1.84_{305}\\ 1.84_{304}\\ 1.84_{304}\\ 1.84_{305}\\ 1.84_{305}\\ 1.84_{305}\\ 1.84_{405}\\$	13 13 13 13 14 13 13 13 13 13 13 13 13 13 13 13 13 13	1.98534 7.98560 7.98585 7.98610 7.98635 7.98661 7.98781 7.98787 7.98787 7.98787 7.98787 7.98812 7.98838	20 25 25 25 25 25 25 25 26 25 25 25	0.01466 0.01440 0.01415 0.01390 0.01365 0.01339 0.01314 0.01289 0.01263	T 85669 T.85657 T.85645 T.85632 T.85620 T.85608 T.85596 T.85596 T.85583	12 12 13 12 12 12 12 13	58 57 56 55 54 53 52 51	7 8 10	2.6 3.0 3.5 3.9 4.3
3 素 5 6 7 8 9 1 1 1 1 1 1 1 1 1 1 1 1 1	I.84246 I.84242 I.84242 I.84252 I.84269 I.84282 I.84282 I.84283 I.84308 I.84334 I.84334 I.84347 I.84362 I.84373 I.84385 I.84373 I.84385 I.84374 I.84424 I.84424 I.84437	13 13 14 13 13 13 13 13 13 13 13 13 13 13 13 13	I.98560 I.98585 I.98610 I.98635 I.98661 I.98661 I.98711 I.98737 I.98787 I.98787 I.98787 I.98812 I.98838	25 25 25 26 25 26 25 25 25 25	0.01440 0.01415 0.01390 0.01365 0.01339 0.01314 0.01289 0.01263	T.85657 T.85645 T.85632 T.85620 T.85608 T.85596 T.85596 T.85583	12 13 12 12 12 12 12	57 56 55 54 53 52 51	7 8 10	2.6 3.0 3.5 3.9 4.3
11 5 1 7 10 11 12 13 14 15 16 17 18 9 20 21 22 23 24 25 60 27 10 10 10 10 10 10 10 10 10 10 10 10 10	$\begin{array}{c} 1.8_{4229}\\ 1.8_{4242}\\ 1.8_{4255}\\ 1.8_{4269}\\ 1.8_{4269}\\ 1.8_{4282}\\ 1.8_{4205}\\ 1.8_{4308}\\ 1.8_{4308}\\ 1.8_{4308}\\ 1.8_{4347}\\ 1.8_{4347}\\ 1.8_{4308}\\ 1.8_{4308}\\ 1.8_{4308}\\ 1.8_{4308}\\ 1.8_{4437}\\$	13 13 14 13 13 13 13 13 13 13 13 13 13 13 13 13	1.98585 1.98610 1.98635 1.98686 1.98711 1.98737 7.98762 1.98762 1.98838	25 25 25 25 25 26 25 25 25	0.01415 0.01390 0.01365 0.01339 0.01314 0.01289 0.01263	T.85645 T.85632 T.85620 T.85608 T.85596 T.85583	13 12 12 12 13	56 55 54 53 52 51	7 8 10	3.0 3.5 3.9 4.3
5 7 11 12 13 14 15 17 19 20 21 22 23 24 25 27 19 20	I.84242 I.84269 I.84269 I.84282 I.84282 I.84325 I.84326 I.84326 I.84321 I.84334 I.84347 I.84360 I.84373 I.84365 I.84398 I.84437 I.84424 I.84427	13 14 13 13 13 13 13 13 13 13 13 13 13 13 13	1.98610 1.98635 1.98661 1.98686 1.98711 1.98737 1.98762 1.98787 1.98812 1.98838	25 26 25 25 26 25 26 25 25	0.01390 0.01365 0.01339 0.01314 0.01289 0.01263	T.85632 T.85620 T.85608 T.85596 T.85583	12 12 12 13	55 54 53 52 51	10 10	3.5 3.9 4.3
7 10 11 12 13 14 15 16 7 18 19 20 21 22 24 25 27 39	I.84269 I.84282 I.84295 I.84308 I.84308 I.84347 I.84347 I.84360 I.84373 I.84385 I.84398 I.84398 I.84398 I.84411 I.84424 I.84437	14 13 13 13 13 13 13 13 13 13 13 13 13	1.98635 1.98661 1.98686 1.98711 1.98737 1.98762 1.98787 1.98812 1.98838	26 25 25 26 25 25	0.01339 0.01314 0.01289 0.01263	T.85620 T.85608 T.85596 T.85583	12 12 13	54 53 52 51	10	3.9
11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 39	I.84269 I.84282 I.84295 I.84308 I.84308 I.84347 I.84347 I.84360 I.84373 I.84385 I.84398 I.84398 I.84398 I.84411 I.84424 I.84437	13 13 13 13 13 13 13 13 13 13 13 13	1.98686 1.98711 1.98737 7.98762 7.98787 7.98787 1.98812 1.98838	25 25 26 25 25	0.01339 0.01314 0.01289 0.01263	T.85596 T.85583	12 13	52 51		4.3
11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 39	I.84205 I.84308 I.84347 I.84347 I.84360 I.84373 I.84385 I.84385 I.84308 J.84385 I.84308 J.84411 I.84424 I.84437	13 13 13 13 13 13 13 13 12 13 13	T.98711 T.98737 T.98762 T.98787 T.98812 T.98838	25 26 25 25	0.01289 0.01263	1.85583	13	51	20	87
10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 30 30 30 30 30 30 30 30 30 30	Y.84308 Y.84321 Y.84334 Y.84347 Y.84360 Y.84373 Y.84373 Y.84385 Y.84398 Y.84411 Y.84424 Y.84437	13 13 13 13 13 13 13 12 13 13	T.98737 T.98762 T.98787 T.98812 T.98838	26 25 25	0.01263	1.85583 1.85571				
11 12 13 14 15 17 18 19 20 21 22 23 24 25 26 27 30	Y.84321 Y.84334 Y.84347 Y.84360 Y.84365 Y.84385 Y.84398 Y.84411 T.84424 Y.84437	13 13 13 13 13 13 12 13 13	T.98762 T.98787 T.98812 T.98838	25		1.05571			1305	13.0
12 13 14 15 16 17 19 20 21 22 23 24 25 26 27 30	T.84334 T.84347 T.84360 T.84373 T.84385 T.84398 T.84398 T.84411 T.84424 T.84437	13 13 13 13 12 13 13	T.98787 T.98812 T.98838	25	0.01238		12	50	10 50	17.3
12 13 14 15 16 17 19 20 21 22 23 24 25 26 27 30	T.84334 T.84347 T.84360 T.84373 T.84385 T.84398 T.84398 T.84411 T.84424 T.84437	13 13 13 12 13 13	T.98787 T.98812 T.98838		0.01230	7.0	12		50 1	41.1
13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 27 20	T.84347 T.84360 T.84373 T.84385 T.84398 T.84411 T.84424 T.84437	13 13 12 13 13	¥.98812 T.98838	25	0.01213	T.85559 T.85547	12	49 48		
14 15 16 17 18 19 20 21 22 23 24 25 26 27 27 20 21 22 23 24 25 26 27 20 20	I.84360 I.84373 I.84385 I.84398 I.84398 I.84411 I.84424 I.84424 I.84437	13 12 13 13	T.98838	25	0.01213	1.85534	13	40		
15 16 17 18 19 20 21 22 23 24 25 26 27 29 20	T.84373 T.84385 T.84398 T.84411 T.84424 T.84437	12 13 13		26	0.01162	T.85522	12	46		25
16 17 18 19 20 21 22 23 24 25 26 27 27 27 29	I.84385 I.84398 I.84411 I.84424 I.84437	13 13	1.96603	25	0.01137	1.85510	12	45	6	2.5
18 19 20 21 22 23 24 25 26 27 27 29	T.84411 T.84424 T.84437	13	1.98888	25 25	0.01112	1.85497	13	44		2.9
19 20 21 22 23 24 25 26 27 27	T.84424 T.84437		T.98913	25	0.01087	1.85485	12	43	7 M	3.3
20 21 22 23 24 25 26 27 27	T.84437		T.98939	25	0.01061	T.85473	12	42	9	
21 22 23 24 25 26 27 39		13	T.98964	25	0.01036	1.85460	12	41	10	4.2 8.3
22 23 24 25 26 27 27			T.98989		0.01011	1.85448		40	290	8.3
22 23 24 25 26 27 27		13	-	26	-		12		10	16.7
23 24 25 26 27	T.84450 T.84463	13	1.99015	25	0.00985	1.85436	13	39	50	20.8
24 25 26 27 27	1.04403 T.84476	13	T.99040 T.99065	25	0.00960	T.85423 T.85411	12	38	30	5010
25 26 27 38 29	I.84489	13	1.99005 1.99090	25	0.00935	T.85399	12	37 36		
26 27 38 39	T.84502	13	T.99116	26	0.00884	1.85386	13	35		
29	T.84515	13	1.99141	25	0.00859	1.85374	12	34		14
20	1.84526	13	¥.99166	25	0.00834	1.85301	13	33	6	1.4
	1.84540	12	T.99191	25	0.00809	I.85349	12	32	78	1.6
30	1.84553	13	T.99217	25	0.00783	T.85337	13	31		1.9
	T.84566		I.99242		0.00758	1.85324		30	9	2.1
	- 0	13	-	25		- 0	12		10 20	2.3
31	T.84579	13	T.99267	26	0.00733	T.85312	13	29	20	4.7
32	T.84592	13	1.99293	25	0.00707	1.85299	12	28	30	9.3
33 34	T.84605 T.84618	13	T.99318 T.99343	25	0.00682	T.85287 T.85274	13	27	50	11.7
34	I.84630	12	T.99343 T.99368	25	0.00632	1.85274 1.85262	12	20		
36	T.84643	13	T.99304	26	0.00606	1.85250	12	24		
37	1.84656	13	T.99419	25	0.00581	I.85237	13	23		
38	1.84669	13 13	T.99444	25 25	0.00556	T.85225	12 13	22		13
39	T.84682	13	T.99469	25	0.00531	T.85212	13	21	б	1.3
40	T.84694		I.99495		0.00505	1.85200		20	78	1.5
		13		25			13			1.7
41	T.84707	13	1.99520	25	0.00480	1.85187	12	19	10	2.0
42	T.84720	13	T.99545	25	0.00455	1.85175	13	18	10	4.3
43	T.84733 T.84745	12	T.99570 T.99596	26	0.00430	I.85162 T.85150	12	17 16	. 30	6.5
45	1.04745 T.84758	13	1.99590 T.99621	25	0.00404	1.85150 T.85137	13	10	40	8.7
46	T.84771	13	T.99646	25	0.00354	I.85125	12	14	50	10.8
47	T.84784	13	T.99672	26	0.00328	1.85112	13	13		
48	1.84706	12 13	T.99697	25 25	0.00303	T.85100	12	12		
40	T.84809	13	T.99722	25	0.00278	1.85087	13	11		
50	T.84822		¥.99747	-	0.00253	I.85074		10		12
		13		26			12		6	1.2
51	1.84835	12	1.99773	25	0.00227	1.85062	13	0	7	1.4
52	1.84847	13	1.99798	25	0.00202	1.85049	12	8	U U	1.8
53	¥.84860 ¥.84873	13	T.99823 T.99848	25	0.00177 0.00152	T.85037 T.85024	13	76	10	2.0
54 55	1.04073 T.84885	12	1.99874	26	0.00152	1.85012	12	5	10	4.0
56	1.84808	13	T.99899	25	0.00101	T.84999	13	S II	30	6.0
57	1.84911	13	I.99924	25	0.00076	1.84986	13	3	40	8.0
58	T.84923	12	1.99949	25	0.00051	1.84974	12		50	10.6
59	¥.84936	13	I.99975	26 25	0.00025	T.84961	13	1		
60	I.84949	13	0.00000	-3	0.00000	T.84949		0		

TABLE

OF

COMMON LOGARITHMS OF NUMBERS

From 1 to 10,000.

N.	Log.	N.	Log.	N.	Log.	N.	Log.	N.	Log.
Ū		20	30 103	40	60 206	60	77 815	80	90 309
I	00 000	21	32 222	41	61 278	61	78 533	81	90 849
2	30 103	22	34 242	42	62 325	62	. 79 239	82	91 381
3	47 712	23	36 173	43	63 347	63	79 934	83	91 908
4	60 206	24	38 021	44	64 345	64	80 618	84	92 428
5	69 897	25	39 794	45	65 321	65	81 291	85	92 942
6	77 815	26	41 497	46	66 276	66	81 954	86	93 450
7	84 510	27	43 136	47	67 210	67	82 607	87	93 952
8	90 309	28	44 716	48	68 124	68	83 251	88	94 448
9	95 424	29	46 240	49	69 020	69	83 885	89	94 939
10	00 000	30	47 712	50	69 897	70	84 510	90	95 424
II	04 139	31	49 136	51	70 757	71	85 126	91	95 904
12	07 918	32	50 515	52	71 600	72	85 733	92	96 379
13	11 394	33	51 851	53	72 428	73	86 332	93	96 848
14	14 613	34	53 148	54	73 239	74	86 923	94	97 313
15	17 609	35	54 407	55	71 036	75	87 506	95	97 772
16	20 412	36	55 630	56	74 819	76	88 081	96	98 227
17	23 045	37	56 820	57	75 387	77	88 649	97	98 677
18	25 527	38	57 978	58	76 343	78	89 209	98	99 123
19	27 875	39	59 106	59	77 085	79	89 763	99	99 564
20	30 103	40	60 206	60	77 815	80	90 309	100	00 000

N.	L. 0	I	2	3	4	5	6	7	8	9		P.	P .	
100	00 000	043	087	130	173	217	260	303	346	389				
101	432	475	518	561	604	647	689	732	775	817				
102	860	903	945	988	*030	*072	*115	*157	*199	*242		44	43	42
103	01 284	326	368	410	452	494	536	578	620	662	z	4.4	4.3	4.2 8.4
104	703	745	787	828	870	912	953	995	*036	*078	2			
105	02 119	160	202	243	284	325	366	407	449	490	3	13.2	12.9	10.8
106	531	572	612	653	694	735	776	816	857	898	5	22.0	21.5	21.0
107	938	979	*019	*060	*100	*141	*181	*222	*262	*302		26.4	25.8 30.1	25.2
100	03 342 743	782	423 822	463	503	543	081	*021	*060	703 *100	7 8	35.2	34.4	33.6
110			218								10	39.6	38.7	37.8
	04 139	179		258	297	336	376	415	454	493				
111	532 922	571 961	610	650 *038	689 *077	727 *115	766	805 *192	844 *231	*200				
113	05 308	346	999	423	461	500	538	576	614	652		41	40	39
114	690	729	767	805	843	881	918	956	994	*032	1 2	4.1	4.0	3.0
115	06 070	108	145	183	221	258	206	333	371	408	3	12.3	12.0	11.7
116	446	483	521	558	595	633	670	707	744	781	8	16.4	16.0	15.0
117	819	856	893	930	967	+004	*041	*078	*115	*151	ō	24.6	24.0	23.4
118	07 188	225	262	298	335	372	408	445	482	518	78	28.7	28.0	27.3
119	555	591	628	664	700	737	773	809	846	882	9	36.9	36.0	35.1
120	918	954	990	*027	*063	*099	*135	*171	*207	*243				
121	08 279	314	350	386	422	458	493	529	565	600				
122	636	672	707	.743	_778	418	849	884	920	.955		38	37	36
123	991	*026	*061	*096	*132	*167	*202	*237	*272	*307.	1	3.8	3.7	3.6
124	09 342	377	412	447	482	517	552	587	621	656	3	7.6	7.4	7.2
125 126	691	726	760	795	830	864	899	934	968	*003	н	15.2	14.8	14.4
120	10 037 380	072	106	140	175	209 551	243	278	312	346	5	19.0	18.5	18.0
128	721	755	780	823	857	890	024	958	992	*025	7	26.6	25.9	25.2
129	11 059	093	126	160	193	227	261	294	327	361	N U	30.4	24.0	32.4
130	394	428	461	494	528	561	594	628	661	694				
131	727	760	793	826	860	893	926	959	992	*024				
132	12 057	000	123	156	189	222	254	287	320	352		35	34	33
133	385	418	450	483	516	548	581	613	646	678	I	3.5	3.4	3.3
134	710	743	775	808	840	872	905	937	969	*001	2	7.0	0.8	9.9
135	13 033	066	098	130	102	194	226	258	290	322	-4	14.0	13.6	13.2
136	354	386	418	450	481	513	545	577	609	640	56	17.5	17.0	10.5
137	672	704	735	767	799	830	862	893 *208	925 *239	950	7	24.5	23.8	23.1
138	988 14 301	*019	*051	395	*114 426	*145	489	520	551	*270	0	28.0	27.2 30.6	26.4
140	613	333	675	706		768		820	860	801	4	. 3	30.0	
140	922		983	*014	737 *045	*076	799 *106	*137	*168	*198				
141	15 229	953	200	320	351	381	412	442	473	503		20	21	30
142	534	564	594	625	655	685	715	746	776	806	7	32	31	
144	836	866	897	927	957	087	*017	*047	*077	*107	2	3.2	6.2	3.0
145	16 137	167	197	227	256	286	316	346	376	406	3	9.6	9.3	9.0 12.0
140	435	465	495	524	554	584	613	643	673	702	5	16.0	15.5	15.0
147	732	761	791	820	850	879	909	938	967	997	Ó 7	19.2	18.6	18.0
148	17 026	056	085	114	143	173	202	231	260	289	7 8	25.6	24.8	24.0
149	319	348	377	400	435	464	493	522	551	580	9	28.8	27.9	27.0
150	609	638	667	696	725	754	782	811	640	869				
N.	L. 0	I	2	3	4	5	6	7	8	9		<u>P.</u>	P.	

N.	L.O	I	2	3	4	5	6	7	8	9	P. P.
150	17 600	638	667	696	725	754	782	811	840	860	
151	808	030	955	984	*013	*041	#070	#099	*127	*150	
151	18 184	213	955 24I	270	208	327	355	384	412	441	29 25
153	460	498	526	554	583	611	630	667	696	72.1	1 2.9 2.8
154	752	780	808	837	865	893	921	949	977	*005	2 5.8 5.6 3 8.7 8.4
155	19 033	061	089	117	145	173	201	229	257	285	4 11.6 11.2
156	312	340	368	396	424	451	479	507	535	562	5 14.5 14.0 6 17.4 16.8
157	590	618	645	673	700	728	756	783	811	838	7 20.3 19.6
158	866	893	921	948	976	*003	*030	*058	*085	*112	1 23.2 22.4 1 26.1 25.2
159	20 140	167	194	222	249	276	303	330	358	385	W texts tests
160	412	439	466	493	520	548	575	602	629	656	
161	683	710	737	703	790	817	844	871	898	.925	
162	952	978	*005	*032	*059	*085	*112	*139	*165	*192	27 26 1 2.7 2.6
163	21 219	245	272	299	325	352	378	405	431	458	2 5.4 5.2
164	484	511	537	564	590	617	643	669	696	722	3 8.1 7.8
165 166	748	775	801	827	854	880	906	932 194	958	985 246	4 10.8 10.4 5 13.5 13.0
167	22 011	208	324	350	376	101	427	453	479	505	6 16.2 15.6
168	531	557	583	608	634	660	686	712	737	763	7 18.9 18.2
169	789	814	840	866	891	917	943	968	994	*010	9 24.3 23.4
170	23 045	070	016	121	147	172	198	223	249	274	
171	300	325	350	376	401	426	452	477	502	528	
172	553	578	603	620	654	670	704	729	754	779	25
173	805	830	855	880	905	930	955	980	*005	*030	1 2.5
174	24 055	080	105	130	155	180	204	229	254	279	2 5.0
175	304	329	353	378	403	428	452	477	502	527	3 7.5 4 10.0
176	551	576	601	625	650	674	699	724	748	773	5 12.5
177	797	822	846	871	895	920	944	969	993	*018	
178	25 042	066	100	IIS	139	164	138	212	237	261	7 17.5 8 20.0
179	285	310	334	358	382	406	431	455	479	503	9 22.5
180	527	551	575	600	624	648	672	696	720	744	
181	768	792	816	840	864	888	912	935	959	983	
182	26 007	031	055	079	102	126	150	174	198	221	24 23
183	245	269	293	316	340	364	387	411	435	458	I 2.4 2.3 2 4.8 4.6
184	482	505	529	553	576	600	623 858	647 881	670 905	694 928	3 7.2 6.9
186	717 951	74I 975	004	788	*045	834	*001	*114	*138	*161	4 9.6 9.2 5 12.0 11.5
187	27 184	207	231	254	277	300	323	346	370	393	6 14.8 13.8
185	416	439	462	485	508	531	554	577	600	623	7 10.8 16.1 E 19.2 18.4
189	646	669	692	715	738	761	784	807	830	852	9 21.0 20.7
190	875	898	921	944	967	989	[#] 012	*035	*058	*081	
191	28 103	126	149	171	194	217	240	262	285	307	
192	330	353	375	398	421	443	466	488	511	533	22 21
193	556	578	601	623	646	668	691	713	735	758	I 2.2 2.1
194	780	803	825	847	870	892	914	937	959	981	2 4.4 4.2 3 6 6 6.3
195	29 003	026	048	070	092	II5	137	159	ISI	203	8.8 8.4
196	226	248	270	292	314	336	358	380	403	425	5 11.0 10.5
197 193	447 667	469	491 710	513	535	557	579	601 820	623 842	645 863	7 15.4 14.7
195	885	907	929	951	973	994	*016	+038	*060	*081	8 17.6 16.8 9 19.8 18.9
200	30 103	125	146	168	100	211	233	255	276	298	9 19.0 10.9
N.	L. 0	I	1 2	3	4	5	6	1 7	8	9	P. P.
14.	L	-	-	10	4	13	0		0	19	Г. Г .

N.	L.O	I	2	3	4	5	6	7	8	9	P. P.	
200		125	146	168	100	211	000		276	298		
201	30 103		363	384	406	428	233	255	402	514		
201	320	341	578	600	621	643	449 664	471 685	492	728		
203	535	771	792	814	835	856	878	899	020	942	22	21
204	963	984	*006	+027	*048	*060	*001	*112	*133	*154	1 2.2	2.1
205	31 175	197	218	239	260	281	302	323	345	366	3 6.6	4 2 6.3
206	387	408	429	450	471	492	513	534	555	576	4 8.8	8.4
207	597	618	639	660	681	702	723	744	765	785	6 13.2	12.6
208	806	827	848	869	890	911	931	952	973	994	7 15.4	14.7
209	32 015	035	056	077	098	118	139	160	181	201	9 19.8	18.9
210	222	243	263	284	305	325	346	366	387	408		
211	428	449	469	490	510	531	552	572	593	613		
212	634	654	675	695	715	736	756	777	797	818	20	
213	838	858	879	899	919	940	960	980	*001	*021	1 2. 2 4.	
214 215	33 041 244	062	082	102 304	I 22 325	143	163	183	203 405	224 425	3 6.	D
216	445	465	486	506	526	345	566	586	606	626	4 8. 5 10.	
217	646	666	686	706	726	746	766	786	806	826	6 12.	800
218	846	866	885	905	925	945	965	985	*005	*025	7 14. 8 16.	na Ri
219	34 044	064	084	104	124	143	163	183	203	223	19 18.	ö
220	242	262	282	301	321	341	361	380	400	420		
221	439	459	479	498	518	5,37	557	577	596	616		
222	635	655	674	694	713	733	753	772	792	811	19 I I.	
223	830	850	869	889	908	928	947	967	986	*005	2 1.	8
224	35 025	044	064	083	102	122	141	160	180	199	3 1.	7
225	218	238	257	276	295	315	334	353	372	392	5 9.	5
226	411	430	449	468	488	507	526	545	564	583		4
228	603	622 813	641 832	660 851	679 870	698 880	717 908	736	755	774	7 13. E 15.	3 ,
229	793 984	*003	*021	*040	*059	*078	*097	927 *116	946 *135	*154	10 17.	I
230	36 173	192	211	220	248	267	286	305	324	342		
231	361	380	399	418	436	455	474	493	511	530	18	
232	549	568	586	605	624	642	661	680	608	717	x 1.	8
233	736	754	773	791	810	829	847	866	884	903	2 J. 3 5.	
234	922	940	959	977	996	*014	*033	*051	*070	*088	4 7.	2
235	37 107	125	144	162	181	199	218	236	254	273	5 P. 6 IO.	8
236	291	310	328	346	365	383	401	420	438	457	7 12.	6
237 238	475 658	493	511	530	548	566	585	603 785	621 803	639 822	D 14.	4
239	840	676 858	694 876	712	731	749 931	767 949	967	985	*003		
240	38 021	030	057	075	003	<u>931</u> 112	130	148	166	184		
241	202	220	238	256	274	202	310	328	346	364	17	
242	382	399	417	435	453	471	480	507	525	543	I I. 2 3.	
243	561	578	596	614	632	650	668	686	703	721	3 5.	I
244	739	757	775	792	810	828	846	863	881	899		
245	917	934	952	970	987	*005	*023	*041	÷058	*076	6 10.:	2
246	39 094	III	129	146	164	182	199	217	235	252	7 II. 8 I3.	
247 248	270	287	305	322	340	358	375	393	410	428	5 15.	
240	445 620	463	480 655	498 672	515	533	550	568	585	602		
250	794	811	829	846	863	707 881	724	915	<u>759</u> 933	<u>777</u> 950		
N.	L. 0	I	2	3	4	5	6	7	8	930	P. P.	

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1_	N.	L.	0	I	2	3	4	5	6	7	8	9	P. P.
1	250	39	794	811	829	846	863	SSI	898	915	933	950	
	251		967	985	*002	*019	*037	*054	*071	*055	*106	*123	
	252	40	140	157	175	192	209	226	243	261	278	295	18
	253		312	329	346	364	381	398	415	432	449	466	1 1.8
	254		483	500	518	535	552	569	586	603	620	637	2 3.0
	255		654	071	688	705	722	739	756	773	790	807	3 5.4
	250		824	841	858	875	892	909	926	943	960	976	
I.	257		993	*010	*027	*044	*061	*075	*095	*III	*128	*145	5 9.0 6 10.8
L	258	41	162	179	196	212	229	246	263	280	296	313	7 12.6 14.4
	259	_	330	347	363	380	397	414	430	447	464	481	9 16.2
	260		497	514	531	547	564	581	597	614	631	647	
	201		664	681	697	714	731	747	764	780	797	814	
	202		830	847	863	880	896	913	929	946	963	979	17
	263		996	*012	*029	*045	*062	*078	*095	*III	*127	*144	I I.7
	264	42	160	177	193	210	226	243	259	275	292	308	2 3.4
	265		325	341	357	374	3.90	406	423	439	455	472	3 5.1 4 6.8
	266		488	504	521	537	553	570	586	602	619	635	5 8.5
	267		651	667	684	700	716	732	749	765	781	797	
	268		813	830	846	862	878	894	911	927	943	.959	7 11.9 8 13.6
	269		975	991	*008	*024	*040	*056	*072	*088	*104	*120	15.3
	270	43	136	152	169	185	201	217	233	249	265	281	
	271		297	313	329	345	361	377	393	409	425	441	
	272		457	473	489	505	521	537	553	569	584	600	16
	273		616	632	648	664	680	696	712	727	743	759	I 1.6
	274		775	791	807	823	838	854	870	886	902	917	2 3.2
	275		933	949	965	981	996	*012	*028	140*	-059	*075	3 4.8 4 6.4
1	276	-44	091	107	122	138	154	170	185	201	217	232	5 8.0
	277		248	264	279	295	311	326	342	358	373	389	
	278		404	420	436	451	467	483	498	514	529	545	7 11.2 8 12.8
	279	-	560	576	592	607	623	638	654	669	685	700	9 14.4
	280		716	731	747	762	778	793	809	824	840	855	
	281		571	886	902	917	932	948	963	979	994	*010	
	282	45	025	040	056	071	086	102	117	133	148	163	15
	283		179	194	209	225	240	255	271	286	301	317	I I.5
	284		332	347	362	378	393	408	423	439	454	469	2 3.0
	285		484	500	515	530	545	561	576	591	606	621	3 4.5 3 6.0
	286		637	652	667	682	697	712	728	743	758	773	5 7.5
	287		788	803	815	834	849	864	879	894	909	924	
	288		939	954	969	984	*000	*015	*030	*045	*060	*075	8 12.0
	289	40	090	105	120	135	150	165	180	195	210	225	9 13.5
	290	-	240	255	270	285	300	315	330	345	359	374	
	291		389	404	419	434	449	464	479	494	509	523	
	292		538	553	568	583	598	613	627	642	657	672	14
	293		687	702	716	731	746	761	776	790	805	820	I 1.4
	294		835	850	864	879	894	909	923	938	953	967	2 2.8 3 4.2
	295		982	997	*012	*026	140*	*056	*070	*085	*100	*114	x 5.6
	296	47	129	144	159	173	188	202	217	232	246	261	5 7.0
1	297		276	290	305	319	334	349	363	378	392	407	7 9.8
	298		422	436	451	465	480	494	509	524	538	553	B 11.2
	299 300	-	567	582	596	011	625	640	654		828	698	9 12.6
-		-	712	727	741	756	770	784	799	813		842	
1_	N.	L	. 0	I	2	3	4	5	6	7	8	9	<u>P. P.</u>

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<u>N.</u>	L. 0	I	2	3	4	5	6	7	8	9	 P. P.
300	47 712	727	741	756	770	784	799	813	828	842	
301	857	871	885	900	914	929	943	958	972	986	
302	48 001	015	029	044	058	073	087	101	116	130	
303	144	159	173	187	202	216	230	244	259	273	
304	287	302	316	330	344	359	373	387	101	416	15
305	430	444	458	473	487	501	515	530	544 686	558	1 1.5
306 307	572	586 728	001 742	615 756	629 770	643 785	657 799	671 813	827	700 841	2 3.0
308	855	860	883	897	QII	026	940	954	968	982	3 4.5 7 6.0
309	996	*010	*024	*038	*052	°066	*080	*004	*108	*122	5 7.5
310	49 136	150	164	178	192	206	220	234	248	262	7 10.5
311	276	200	304	318	332	346	360	374	388	402	1 12.0 9 13.5
312	415	420	443	457	471	485	499	513	527	541	
313	554	568	582	596	610	624	638	651	665	679	
314	693	707	721	734	748	762	776	790	803	817	
315	831	845	859	872	886	900	914	927	941	955	14
316	969	982	996	*010	*024	*037	*051	*065	*079	*092	
317 318	50 106	120 256	133	147 284	161	174	188	202	215	229 365	2 2.8
319	379	393	406	420	297 433	311 447	325	338	188	501	3 4.2 4 5.6
320	515	529	542	556	569	583	596	610	623	637	5 7.0
321	651	664	678	601	705	718	732	745	759	772	7 98
322	786	799	813	826	840	853	866	880	893	907	11.2 9 12.6
323	920	934	947	961	974	987	*001	*014	*028	*041	
324	51 055	068	081	095	108	121	135	148	162	175	
325	188	202	215	228	242	255	268	282	295	308	
326	322	335	348	362	375	388	402	415	128	441	12
327	455	468	481	495	508	521	534 667	548 680	501	574	13 -
320	587	733	746	627	640	654	799	812	693 825	838	2 2.6
330	851	865	878	801	904	017	930	943	957	970	3 3.9
331	083	996	*000	*022	*035	*018	*061	*075	*088	*10I	5 6.5 7.8
332	52 114	127	140	153	166	179	192	205	218	231	7 9.1
333	244	257	270	284	297	310	323	336	349	362	10.4 9 11.7
334	375	388	401	414	427	440	453	466	479	492	717
335	504	517	530	543	556	569	582	595	608	621	
336	634	647	660	673	686	699	711	724	737	750	
337	763	776	789	802	815	827	840	853 982	866	879 *007	12
338	892 53 020	905 033	917	930 058	943	956	969	110	994	135	12 1 1.2
340	148	161	173	186	199	212	224	237	250	263	2 2.4 3 3.6
341	275	288	301	314	326	339	352	364	377	300	4.8
342	403	415	428	441	453	466	479	491	504	517	
343	529	542	555	567	580	593	605	618	631	643	6 7.2 7 8.4 8 9.6
344	656	668	681	694	706	719	732	744	757	769	9 10.8
345	782	794	807	820	832	845	857	870	882	895	
346	908	920	933	945	958	970	983	995	*008	*020	
347	54 033 158	045	058	070	083	095	108	120	133	145	
340	283	295	307	320	332	345	357	370	382	394	
350	407	410	432	444	450	460	481	494	506	518	
N.	L. 0			3	4	5	6	7	8	9	 P. P.
LIV.	1. 0	1		13	4	1.5	0		10	19	 1.1.

N.	L. 0	I	2	3	4	5	6	7	8	9	P. P.
350	54 407	419	432	444	456	469	481	494	506	518	
351	531	543	555	568	580	593	605	617	630	642	
352	654	667	679	601	704	716	728	741	753	765	
353	777	790	802	SI4	827	839	851	864	876	888	
354	900	913	925	937	949	962	974	986	998	*011	13
355	55 023	035	047	000	072	084	096	108	121	133	1 1.3 2 2.6
356	145	157	169	182	194	206	218	230	242	255	3 3.9
357	267	279	291	303	315	328	340	352	364	376	5 - 2 5 - 6.5 6 - 7.8
358	388	400	413	425	437	449	461	473	485	497	
359	509	522	534	546	558	570	582	594	606	618	7 9.1
360	630	642	654	666	678	691	703	715	727	739	9 11.7
361	751	763	775	787	799	SII	823	835	847	859	
362 363	871	883	895 *015	907 *027	919 *038	93I *050	943 *062	955 *074	967 *086	979 *098	
303	56 110	122	134	146	158	170	182	1014	205	217	
365	220	2.11	253	265	277	280	301	312	324	330	
366	348	360	372	384	396	407	419	431	443	455	12
367	467	478	490	502	514	526	538	549	561	573	1 1.2
368	585	597	608	620	632	644	656	667	679	691	3 3.6
369	703	714	726	738	750	761	773	785	797	808	4 4.8
370	\$20	832	844	855	867	879	891	902	914	926	6 7.2
371	937	949	961	972	984	996	*008	*019	*031	*043	7 8.4 E 9.6
372	57 054	066	078	089	IOI	113	124	136	148	159	9 10.8
373	171	183	194	206	217	229	241	252	264	276	
374	287	299	310	322	334	345	.357	368	380	392	
375 376	403	415	426	438	449	461	473 588	484	496	507 623	
377	634	530 646	542 657	553	565	576	703	715	726	738	
378	749	761	772	784	795	807	818	830	841	852	11
379	864	875	887	808	910	921	933	944	955	967	1 I.I 2 2.2
380	978	990	*001	*013	*024	*035	*047	*058	*070	*081	3 3.3
381	58 002	101	IIS	127	138	140	161	172	184	195	4 4-4
382	206	218	220	240	252	263	274	286	297	300	5 5·5 6.6
383	320	331	343	354	365	377	388	399	410	422	7 7·7 8 8.8
384	433	444	456	467	478	490	501	512	524	535	9 9.9
385	546	557	569	580	591	602	614	625	636	647	
386 387	659 771	670	681	692 805	704	715	726	737	749 861	760 872	
388	883	894	794	017	028	939	950	961	973	984	
389	995	*006	*017	*028	+040	*051	*062	*073	*084	*095	
390	59 106	IIS	120	140	151	162	173	184	195	207	10 1 1.0
391	218	229	2.10	251	202	273	284	295	306	318	2 2.0
392	329	340	351	362	373	384	395	406	417	428	3 3.0 4 4.0
393	439	450	461	472	483	494	506	517	528	539	5 5.0
394	550	561	572	583	594	605	616	627	638	649	
395	660	671	682	693	704	715	726	737	748	759	7 7.0 8 8.0
396	770	780	791	802	813	824	835	846	857	868	9 9.0
397 398	879 988	890	901	912 *021	923 *032	934	945	956	966 *076	977 *086	
399	60 097	999 108	*010 110	130	141	*043 152	*054	*065	184		
400	206	217	228	239	249	260	271	282	293	<u>195</u> 304	
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400	60	206	217	228	239	249	260	271	282	293	304		
401		314	325	336	347	358	369	379	390	401	412		
402		423	433	444	455	466	477	487	498	509	520		
403		531	541	552	563	574	584	595	606	617	627		
404		638 746	649 756	660 767	670 778	681 788	692 799	703	713	724 831	735		
406		853	863	874	885	895	906	917	927	938	940		11
407		959	970	981	100	*002	*013	*023	*034	*045	*055	11	1.1
408	61	066	077	087	098	109	119	130	140	151	162	2	2.2
409		172	183	194	204	215	225	236	247	257	268	#	4-4
410		278	289	300	310	321	331	342	352	363	374	56	5.5
411		384	395	405	416	426	437	448	458	469	479	78	7·7 8.8
412 413		490	500	511	521	532	542	553	563	574	584	8	9.9
413		595 700	606 711	616 721	627 731	637	648 752	658 763	669 773	679 784	690 794		
415		805	815	826	836	847	857	868	878	888	899		
416		909	920	930	941	951	962	972	982	993	*003		
417	62	014	024	034	045	055	066	076	086	097	107		
418		118	128	138	149	159	170	180	190	201	211		
419		22I	232	242	252	263	273	284	294	304	315		
420		325	335	346	356	366	377	387	397	408	418		
421		428	439	449	459	469	480	490	500	511	521		10
422 423		531	542	552	562 665	572	583	593	603	613	624	I	1.0
423		634 737	644 747	655 757	767	675	788	696 798	706	716	726	2	2.0
425		839	849	859	870	880	800	000	910	921	931	4	4.0
426		941	951	961	972	982	992	*002	*012	*022	*033	5	5.0
427	63	043	053	063	073	083	094	104	114	124	134	2	7.0 · 8.0
428		144	155	165	175	185	195	205	215	225	236	9	9.0
429		246	256	266	276	286	296	306	317	327	337		
430		347	357	367	377	387	397	407	417	428	438		
431 432		448	458 558	468	478	488	498	508	518	528	538		
433		548 649	659	669	579 679	689	599	709	719	729	639 739		
434		749	759	769	779	789	799	800	819	820	839		
435		849	859	869	879	889	899	909	919	929	939		
436		949	959	969	979	988	998	*008	*018	*028	*038		
437 438	04	048	058	068	078	088	098	108	118	128	137		9
430		147 246	157 256	167 266	177 276	187	197 296	207 306	217	227	237	1 2	0.9
439	-	345	355	365	375	385	395	404	414	424	335	3 4	2.7 3.6
441		444	454	464	473	483	493	503	513	523	532	5	4.5
442		542	552	562	572	582	591	601	611	621	631		5.4 6.3
443		640	650	660	670	680	689	699	709	719	729	7	7.2
444		738	748	758	768	777	787	797	807	816	826	A 1	
445		836	846	856	865	875	885	895	904 *002	914 *011	924 *021		
440	65	933 031	943 040	953 050	963	972	079	992	002	108	118		
448	100	128	137	147	157	167	176	186	196	205	215		
449		225	234	244	254	263	273	283	292	302	312		
450		321	331	341	350	360	369	379	389	398	408		
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450	65 321	331	341	350	360	369	: 379	389	398	408	
451	418	427	437	447	456	466	475	485	495	504	
452	514	523	533	543	552	562	571	581	591	600	
453	610	619	629	639	648	658	667	677	686	696	
454	706	715	725	734	744	753	763	772	782	792	
455	801	SII	820	830	839	849	858	868	877	887	
456	896 992	906 *001	916 *011	925 *020	935 *030	944 *039	954 *049	963 *058	973 *065	982 *077	10 1 1.0
457 458	66 087	006	106	IIS	124	134	143	153	162	172	2 2.0
459	181	191	200	210	219	220	238	247	257	266	3 3.0
460	276	285	295	304	314	323	332	342	351	361	5 5.0
161	370	380	389	398	408	417	427	436	445	455	
462	464	474	483	492	502	511	521	530	539	549	7 7.0 8.0
463	558	567	577	586	596	605	614	624	633	642	9.0
464	652	661	671	680	689	699	708	717	727	736	
465	745	755	764	773	783	792	801	811	820	829	
466	839	848	857	867	876	885	894	904	913	922	
467	932	941	950	960	969	978	987	997	*006	*015	
468	67 025	034	043	052	062	071	080	089	099	IOS	
469	117	127	136	145	154	164	173	182	191	201	
470	210	219	228	237	247	256	265	274	284	293	
471	302	311	321	330	339	348	357	367	376	385	
472	394	403	413	422	431	440	449	459	468	477	1 0.9
473	486	495	504	514	523	532 624	541	550	560	569	
474 475	578 669	587 679	596 688	605 697	614 706	715	633 724	642	651 742	660 752	3 2.7 4 3.6
475	761	770	779	788	797	806	815	825	834	843	5 4.5
477	852	861	870	879	888	897	906	916	925	934	7 6.3
478	943	952	961	970	979	988	997	*006	*015	*024	7 6.3 7.2 5 8.1
479	68 034	043	052	061	070	079	088	097	106	115	B 1 0.1
480	124	133	142	151	160	169	178	187	196	205	
481	215	224	233	242	251	260	260	278	287	206	
482	305	314	323	332	341	350	359	368	377	386	
483	395	404	413	422	431	440	449	458	467	476	
484	485	494	502	511	520	529	538	547	556	565	
485	574	583	592	601	610	619	628	637	646	655	
486	664	673	681	690	699 780	708	717 806	726	735	744	8
487	753 842	762 851	771 860	780 860	709 878	797 886	895	815 904	824	833	1 0.8
400	931	940	949	958	966	975	984	904	913 *002	*011	1.6 3 2.4
490	60 020	028	037	046	055	064	073	082	000	099	4 3.2
491	108	117	126	135	144	152	161	170	179	188	5 4.0
491	108	205	214	223	232	241	249	258	267	276	7 5.6 U 6.4
493	285	294	302	311	320	329	338	346	355	364	B 0.4
494	373	381	390	399	408	417	425	434	443	452	
495	461	469	478	487	496	504	513	522	531	539	
496	548	557	566	574	583	592	601	600	618	627	
497	636	644	653	602	671	679	688	607	705	714	-
498	723	732	740	749	758	767	775	784	793	801	
499	10	819	827	836	845	854	862	871	880	888	
500	897	906	914	923	932	940	949	958	966	975	
N.	L. o	I	2	3	4	5	6	7	8	9	P. P.

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500	69 897	906	914	923	932	940	949	958	966	975	
501	984	992	*001	*010	*018	*027	#036	++044	*053	*062	
502	70 070	079	088	096	105	114	122	131	140	148	
503	157	165	174	183	191	200	209	217	226	234	
504	243	252	260	269	278	286	295	303	312	321	
505	329	338	346	355	364	372	381	389	398	406	
506	415	424	432	441	449	458	467	475	484	492	
507	501	509	518	526	535	544	552	561	569	578	1 0.0
508	586	595	603	612	621	629	638	646	655	663	1 1.8
509	672	680	689	697	700	714	723	731	740	749	3 2.7
510	757	766	774	783	791	800	808	817	825	834	4 3.6 5 4.5
511	842	851	859	868	876	885	893	902	910	919	6 5.4
512	927	935	944	952	961	969	978	986	995	*003	7 6.3
513	71 012	020	029	037	046	054	063	071	079	088	間 7·2 預 8.1
514	096	105	II3	122	130	139	147	155	164	172	**
515	181	189	198	206	214	223	231	240	248	257	
516	265	273	282	290	299	307	315	324	332	341	
517 518	349	357	366	374	383	391	399	408	410	425 508	
519	433 517	44I 525	533	458	550	475 559	567	492	584	592	
520	600	-	617					659	667	675	
		609		625	634	642	650		1		
521	684	692	700	709	717	725	734	742	750	759	
522	767	775	784 867	792 875	800 883	809 892	817 900	825 908	834	842 925	1 0.8
523 524	850 933	941	950	958	966	975	983	900	999	*008	2 1.6 3 2.4
525	72 016	024	032	041	049	9/5	066	074	082	000	4 3.2
526	000	107	115	123	132	140	148	156	165	173	5 4.0
527	181	189	198	206	214	222	230	239	247	255	6 4.8 7 5.6
528	263	272	280	288	296	304	313	321	329	337	7 5.6
529	346	354	362	370	378	387	395	403	411	419	₩ 7.2
530	428	436	444	452	460	469	477	485	493	501	
531	509	518	526	534	542	550	558	567	575	583	
532	591	599	607	616	624	632	640	648	656	665	
533	673	681	689	697	705	713	722	730	738	746	
534	754	762	770	779	787	795	803	811	819	827	
535	835	843	852	860	868	876	884	892	900	908	
536	916	925	933	941	949	957 *028	905	973 *054	981 *062	989	7
537 538	997 73 078	*006	*014 094	*022 102	*030 111	*038	*046	135	143	*070	1 0.7
530	159	167	175	183	101	119	207	215	223	231	II 1.4
539 540	239	247	255	263	272	280	288	200	304	312	3 2.1 A 2.8
541	320	328	336	344	352	360	368	376	384	392	5 3.5
542	400	408	416	424	432	440	448	456	464	472	7 4.9
543	480	488	496	504	512	520	528	536	544	552	1 5.6 10 6.3
544	560	568	576	584	592	600	608	616	624	632	
545	640	648	656	664	672	679	687	695	703	711	
546	719	727	735	743	751	759	767	775	783	791	
547	799	807	815	823	830	838	846	854	862	870	
548	878	886	894	902	910	918	926	933	941	949	
549	957	965	973	981	989	997	*005	*013	*020	*028	
550	74 036	044	052	000	068	076	084	092	099	107	
N.	L. o	I	2	3	4	.5	6	7	8	9	<u>P. P.</u>

N.	1. 0	I	2	3	4	5	6	7	8	9	P. P.
550	74 036	044	052	060	065	076	084	092	099	107	
55I	115	123	131	139	147	155	162	170	178	186	
552	194	202	210	218	225	233	241	249	257	265	
553	273	280	288	296	304	312	320	327	335	343	
554	351	359	367	374	382	390	398	406	414	421	-
555	429	437	445	453	461	468	476	484	492	500	
556	507	515	523	531	539	547	554	562	570	578	
557	586	593	601	609	617	624	632	640	648	656	
558	663	671	679	687	695	702	710	718	726	733	
559	741	749	757	764	772	780	788	796	803	811	
560	819	827	834	842	850	858	865	873	881	889	8
561	896	904	912	920	927	.935	_943	950	958	966	I 0.8 2 I.6
562	974	981	989	997	*005	°012	*020	*028	*035	*043	
563	75 051	059	066	074	082	089	097	105	II3	120	4 3.2
564	128	136	143	151	159	166	174	182	189	197	5 4.0
565	205	213	220	228	236	243	251	259	266	274	7 5.6 8 6.4
566 567	282	289 366	297	305	312	320	328	335	343	351	8 6.4
568	358 435	300	374 450	381 458	465	397 473	404 481	412	420	427	417.0
569	435 511	519	526	534	542	549	557	565	572	580	
570	587	595	603	610	618	626	633	641	648	656	
571	664	671	679	686	694		700	717			
572		747	755	762	770	702 778	785		724 800	732 808	
573	740	823	831	838	846	853	861	793 868	876	884	
574	801	899	906	914	921	929	937	944	952	959	
575	967	974	982	989	997	*005	*012	*020	*027	*035	
576	76 042	050	057	065	072	080	087	095	103	IIO	
577	118	125	133	140	148	155	163	170	178	185	
578	193	200	208	215	223	230	238	245	253	260	
579.	268	275	283	290	298	305	313	320	328	335	
580	343	350	358	365	373	380	388	395	403	410	
581	418	425	433	440	448	455	462	470	477	485	
582	492	500	507	515	522	530	537	545	552	559	
583	567	574	582	589	597	604	612	619	626	634	
584	641	649	656	664	671	678	686	693	701	708	1 0.7
585	716	723	730	738	745	753	760	768	775	782	2 1.4
586 587	790	797	805	812	819	827	834	842	849	856	3 2.1 4 2.8
507	864	871	879	886	893	901	908	916	923	930	5 3.5
589	938 77 012	945 019	953 026	960 034	967 041	975 048	982 056	989 063	997 070	*004	
590	085	093	100	107	115	122	120	137	144	151	7 4.9 8 5.6 9 6.3
591	159	166	173	181	188	195	203	210	217	225	910.3
592	232	240	247	254	262	269	276	283	201	298	
593	305	313	320	327	335	342	349	357	364	371	
594	379	386	393	401	408	415	422	430	437	444	
595	452	459	466	474	481	488	495	503	510	517	
596	525	532	539	546	554	561	568	576	583	590	
597	597	605	612	619	627	634	641	648	656	663	
598	670	677	685	692	699	706	714	721	728	735	
599	743	750	757	764	772	779	786	793	801	808	
600	815	822	830	837	844	851	859	866	873	880	
N.	L. o	T	2	3	4	5	6	7	8	9	P. P.

601 602	77 815 887 960 78 032 104 176 247 319	822 895 967 039 111 183	830 902 974 046	837 909 981	844 916	851	859	866			
602 603 604 605 606 607	960 78 032 104 176 247	967 039 111	974 046		And the second s			000	873	880	
603 604 605 606 607	78 032 104 176 247	967 039 111	974 046			924	931	938	945	952	
604 605 606 607	104 176 247	III			988	996	*003	*010	*017	*025	
605 606 607	176 247		- · · ·	053	001	068	075	082	089	097	
606 607	247	183	118	125	132	140	147	154	161	168	
607			190	197	204	211	219	226	233	240	
	310	254	262	269	276	283	290	297	305	312	н
008		326	333	340	347	355	362	369	376	383	1 0.8
600	390	398	405	412	419	426	433	440	447	455	2 1.6 3 2.4
	462	469	476	483	490	497	504	512	519	526	H 3.2
610	533	540	547	554	561	569	576	583	590	597	5 4.0 6 4.8
611	604	611	618	625	633	640	647	654	661	668	7 5.6
612	675	682	689	696	704	711	718	725	732	739	8 6.4
613	746	753	760	767	774	781	789	796	803	810	
615	817 888	824	831	838	845	852	859	866	873	880	
616	958	965	902 972	9 09 9 79	916 986	923 993	930	937 *007	944 *014	951 *021	
617	79 029	036	043	050	057	064	071	078	085	0021	
618	000	106	II3	120	127	134	141	148	155	162	
619	169	176	183	190	107	204	211	218	225	232	
620	239	240	253	200	267	274	281	288	295	302	
621	300	310	323	330	337	344	351	358	365	372	
622	379	386	393	400	407	414	421	428	435	442	7
623	449	456	463	470	477	484	491	408	505	511	I 0.7 I 1.4
624	518	525	532	539	546	553	560	567	574	581	3 2.1
625	588	595	602	609	616	623	630	637	644	650	4 2.8 5 3.5 6 4.2
626	657	664	671	678	685	692	699	706	713	720	
627	727	734	741	748	754	761	768	775	782	789	7 4.9 .
628	796	803	810	817	824	831	837	844	851	858	1 5.6 9 6.3
629	865	872	879	886	893	900	906	913	920	927	
630	934	94I	948	955	962	969	975	982	989	996	
631	80 003	010	017	024	030	037	044	051	058	065	
632	072	079	085	092	099	106	113	120	127	134	
633 634	140	147	154	101	165	175	182	188	195	202	
635	209	216	223	229	236	243	250	257	264	271	
636	277 346	353	291 359	298 366	305	380	387	325 393	332	339	
637	414	421	428	434	373 441	448	455	462	468	407	
638	482	480	496	502	500	516	523	530	536	543	1 0.5
639	550	557	564	570	577	584	591	598	604	611	2 1.2
640	618	625	632	638	645	652	659	665	672	679	3 1.8
641	686	693	600	706	713	720	726	733	740	747	5 3.0
642	754	760	767	774	781	787	794	801	808	814	7 4.2
643	821	828	835	841	848	855	862	868	875	882	8 4.8
644	889	895	902	909	916	922	929	936	.943	.949	10 5-4
645	956	963	969	976	983	990	996	*003	*010	*017	
646	81 023	030	037	043	050	057	064	070	077	084	
647 648	000	097	104	III	117	124	131	137	144	151	
649	158 224	164	171	178	184	191	198	204	211	218 285	
650	224	231	238	245	251 318	258 325	331	27I 338	278	351	
	L. 0	I	305	3	4	5	6	7	8	9	P. P.

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650	SI 291	298	305	311	318	325	331	338	345	351	
651	358	365	371	378	385	391	398	405	411	418	
652	425	431	438	445	451	458	465	471	478	485	
653	491	498	505	511	518	525	53I	538	544	551	
654	558	564	571	578	584	591	598	604	611	617	
655	624	631	637	644	651	657	664	671	677	684	
656	690	697	704	710	717	723	730	737	743	750	
657 658	757	763	770	776	783	790 856	796 862	803 869	809 875	882	
659	823 880	895	836	842	849	921	928	935	941	948	
660	954	961	068	974	915	987	920	*000	*007	*014	
661							060	066			7
662	82 020 086	027	033	040	046	053	125	132	073	079 145	2 1.4
663	151	158	164	105	178	184	125	197	204	210	3 2.I 4 2.8
664	217	223	230	236	243	249	256	263	269	276	
665	282	289	295	302	308	315	321	328	334	341	6 4.2
666	347	354	360	367	373	380	387	393	400	406	7 4·9 8 5.6 9 6.3
667	413	419	426	432	439	445	452	458	465	471	9 6.3
668	478	484	491	497	504	510	517	523	530	536	
669	543	549	556	562	569	575	582	588	595	601	
670	607	614	620	627	633	640	646	653	659	666	
671	672	679	685	692	698	705	711	718	724	730	
672	737	743	750	756	763	769	776	782	789	795	
673	802	808	814	821	827	834	840	847	853	860	
674	866	872	879	885	892	898	905	911	918	924	
675 676	930	937	943	950	956	963	969	975	982	988	
677	995 83 059	*001	*003	*014 078	*020	*027	*033	*040 104	*046 110	*052 117	
678	123	129	136	142	149	155	161	165	174	181	
679	187	193	200	206	213	219	225	232	238	245	
680	251	257	264	270	276	283	280	206	302	308	
681	315	321	327	334	340	347	353	359	366	372	2
682	378	385	391	398	404	410	417	423	429	436	
683	442	448	455	461	467	474	480	487	493	499	
684	506	512	518	525	531	537	544	550	556	563	6 1 0.6
685	569	575	582	588	594	601	607	613	620	626	2 1.2
686	632	639	645	651	658	664	670	677	683	689	3 1.8
687	696	702	708	715	721	727	734	740	746	753	4 2.4 5 3.0
688 689	759 822	765	771	778	784	790	797	803	809	816	6 3.6
690	885	891	835	841	847	853	860	866	872	879 942	7 4-2 8 4.8
601	948	954	060	904 967	<u>910</u> 973	979	923	929 992	<u>935</u> 998	*004	9 5-4
692	84 011	017	023	020	036	042	048	055	061	067	
693	073	080	086	002	008	105	III	117	123	130	
694	136	142	148	155	161	167	173	180	186	192	
695	198	205	211	217	223	230	236	242	248	255	
696	261	267	273	280	286	292	298	305	311	317	
697	323	330	336	342	348	354	361	367	373	379	
698	386	392	398	404	410	417	423	429	435	442	
699	448	454	460	466	473	479	485	491	497	504	
700	510	516	522	528	535	541	547	553	559	566	
N.	L. 0	I	2	3	4	5	6	7	8	9	P. P.

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N.	L. 0	I	2	3	4	5	6	7	8	9	P. P.
700	84 510	516	522	528	535	541	5.47	553	559	566	
701	572	578	584	590	597	603	600	615	621	628	
702	634	640	646	652	658	665	671	677	683	689	
703	696	702	708	714	720	726	733	739	745	751	
704	757	763	770 831	776	782	788	794 856	800	807	813	
706	880	887	803	800	905	911	917	924	930	936	
707	942	948	954	960	967	973	979	985	991	997	7
708	85 003	009	016	022	028	034	040	046	052	058	1 0.7
709		071	077	083	089	095	101	107	114	120	2.1 1 2.8
710	120	132	138	144	150	156	163	169	175	181	3.5
711	187	193	199	205	211	217	224	230	236	242	7 4.9
712	248 300	254 315	260 321	266 327	272	278	285	29I 352	297 358	303	7 4.9 8 5.6 0 6.3
714	370	376	382	388	394	400	406	412	418	425	010.3
715	431	437	443	449	455	461	467	473	479	485	
716	491	497	503	509	516	522	528	534	540	546	
717 718	552 612	558 618	564	570 631	576	582 643	588	594 655	600 661	606	
719	673	679	685	691	697	703	709	715	721	727	
720	733	739	745	751	757	763	769	775	781	788	
721	794	800	806	.812	818	824	830	836	842	848	
722	854	860	866	872	878	884	800	896	902	008	6
723	914	920	926	932	938	944	950	956	962	968	1 0.6
724	974	980	986	992	998	*004	*010	*016	*022	*028	3 1.8
725 726	86 034	040 100	046 106	052 112	058	064	070	076	082	088	5 3.0
727	094 153	159	165	171	177	124	130	195	141 201	147	
728	213	219	225	231	237	243	249	255	261	267	E 4.8
729	273	279	285	291	297	303	308	314	320	326	10 5-4
730	332	338	344	350	356	362	368	374	380	386	
73I	392	398	404	410	415	421	427	433	439	445	
732	451	457	463	469	475	481	487	493	499	504	
733 734	510 570	516 576	522 581	528 587	534	540	546	552	558	564	
735	629	635	641	646	593 652	599 658	664	670	676	682	
736	688	694	700	705	711	717	723	729	735	741	
737	747	753	759	764	770	776	782	788	794	800	8
738	806	812	817 876	823 882	829 888	835	841	847	853	859	1 0.5 2 1.0
739	864	870				894	900	900	911	917	3 1.5
740	923	929	935	941	947	953	958	964	970	976	5 2.5
741 742	982 87 040	988 046	994 052	999 058	*005	*011 070	*017	*023 081	*029	*035	7 3.5
742	000	105	III	116	122	128	134	140	146	151	1 4.0 9 4.5
744	157	163	169	175	181	186	192	198	204	210	914.5
745	216	221	227	233	239	245	251	256	262	268	
746	274	280	286	291	297	303	309	315	320	326	
747 748	332 390	338 396	344 402	349 408	355 413	361 419	367	373 431	379 437	384 442	
749	448	454	460	466	413	477	483	489	495	500	
750	506	512	518	523	529	535	541	547	552	558	
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N.L.cI23456789P. 750 87 564 570 576 581 557 593 599 604 616 616 752 622 628 601 607 703 708 714 720 726 731 753 679 685 601 607 703 708 714 720 726 731 753 7743 740 754 760 766 714 720 726 731 755 795 806 812 818 823 820 835 841 846 755 997 978 984 990 996^{4011} 4070 7613^{4010} 7813^{4018} 760 681 687 093 059 104 110 116 121 127 133 766 824 930 996^{1011} 807 8070^{101} 8070^{101} 8070^{101} 764 3030^{101} 321^{102} 328^{102} 323^{103} 333^{103} 395^{150} 304 764 83^{101} 81^{101} 81^{102} 772^{102} 777^{102} 777^{102} 777^{102} 777^{102} 776^{102} 81^{102} 81^{102} 766 423^{1102} 434^{1140} 445^{11457} 453^{1163} 457^{116} 859^{116} 766^{116} 857^{116} 857^{116} 766 <												
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755 705 830 830 837 837 837 836 836 846 847 837 836 836 836 836 837 837 836 836 836 837 837 836 836 836 837 836 837 836 837 836 837 836 837 836 837 836 837 836 837 836 936 990 955 961 757 916 915 921 927 933 938 944 950 955 961 976 953 951 915 917 133 818 110 116 1121 1127 1133 113 113 114 150 111 1127 1133 114 124 127 133 114 124 127 133 114 124 147 14 124 147 14 124 14 124 147 124 124 127 133 113 133 113 133 113 133 <td< th=""><th></th><th></th><th></th><th>-</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></td<>				-								
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760 081 057 003 006 104 110 116 121 127 133 761 138 144 150 156 161 167 173 178 184 190 763 252 258 264 270 275 281 287 229 293 304 764 309 315 321 326 332 338 343 349 355 360 764 423 429 434 440 446 451 457 465 468 474 7 766 423 423 440 446 451 457 456 587 87 766 536 512 547 553 550 564 570 576 881 887 9 5.4 770 649 655 660 666 672 677 683 689 694 700 771 705 711 717 773 779 784 790 795 870 795 870 795 776 996 902 907 700 797 <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>-</th> <th></th> <th></th>										-		
76113814415015616116717317818419076219520120721321822423023524124724776325225826427027528128729229830436764309315321326332338334349355300317653663723773833893954004064124174766433429440446451457463468474476653654254457057658158753078769593598604610615615621627632638643770649655660666726776836896947007717057117177227287347397457507567759309369419079539589649699759817977767847808553505447907958618876937927768904204805305906407007608187709277689042048953059054793198204<												
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766423429434440446451457463468474 δ δ 76653653654254755355956457057657658158776959359860461061562162763263864377064965566066667267768368960470077170571171772272873473974575075677276276777377978473974575075677381882482083584084685285786386877487488088580189790290897598177593093694194795395896496997598177698699297797670678114314877905415910511701761821311311431487780981041091151201261311311311431487802092152212262322372432482542607812652712762822872932983043103153784437433				-								4 2.4
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769593598604610615621627632638643770649655660666672677683689604700771705711717722728734739745750772818824829835840846852857863868774874880885891897902908913919925775930936941947953958964960975981776986992997*6038000*6046020*025*031*837777890420480530590640700760810870927780981041091151201261311371431487791541591051701761821871931982047802002152212262322372432482542607812652712762822872932983043103151783376382387393398404409415421426311.578443243744344845445946547047648142.5 <t< td=""><th>768</th><td>536</td><td>542</td><td>,547</td><td></td><td>559</td><td>564</td><td>570</td><td>576</td><td>581</td><td>587</td><td></td></t<>	768	536	542	,547		559	564	570	576	581	587	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	769	593	598	604	610	615	621	627	632	638	643	31.5.4
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773 818 824 820 835 640 846 852 857 863 868 774 874 880 885 891 897 902 908 913 919 925 775 930 936 941 947 953 958 964 969 975 981 776 986 992 997 *003*009*014*020*025*031*037 777 89 042 048 053 059 064 070 766 81 087 092 778 098 104 109 115 120 126 131 137 143 148 779 154 159 165 170 176 182 187 193 198 204 780 209 215 221 226 232 237 243 248 254 260 781 265 271 276 282 287 293 298 304 310 315 315 783 376 332 337 343 348 354 360 355 371 31 31 784 432 437 443 448 454 459 465 470 476 481 420 787 597 603 609 614 620 625 631 636 642 647 84 205	77I			717	722		734	739				
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777 89 0.42 0.48 0.53 0.59 0.64 0.70 0.76 0.81 0.87 0.92 778 0.98 10.4 10.9 11.5 12.0 126 131 137 143 148 779 1.54 159 165 170 176 182 187 103 198 204 780 209 215 221 226 232 237 243 248 254 260 781 265 271 276 282 287 293 298 304 310 315 782 321 326 332 337 343 348 354 360 355 371 1 0.5 783 376 382 387 393 398 404 409 415 421 426 3 1.5 784 432 437 443 448 454 459 465 470 476 481 4 2.05 786 542 248 553 559 564 570 575 581 586 592 7 786 653 658 664 669 675 680 686 697 702 7 3.5 786 763 768 774 779 785 790 796 801 807 812 790 763 768 774 779 785 790 966 <					947	953	958			975	981	
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784 432 437 443 448 454 459 465 470 476 481 481 785 487 492 498 504 509 515 520 526 531 537 527 786 542 548 553 559 564 570 575 581 586 592 7 787 597 603 609 614 620 625 631 636 642 647 84.0 788 653 658 664 669 675 680 686 691 697 702 9 789 708 713 719 724 730 735 741 746 752 757 790 763 768 774 779 785 790 796 801 807 812 701 818 823 829 834 840 845 851 856 862 867 792 873 878 883 889 894 900 905 911 916 922 793 927 933 938 944 949 955 960 966 971 977 794 982 988 993 998 $*004$ $*009$ $*015$ $*020$ $*026$ $*051$ 796 091 097 102 108 113 119 124 129 135 140												2 1.0
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788 653 658 664 669 675 686 686 691 697 702 914-5 789 708 713 719 724 730 735 741 746 752 757 790 763 768 774 779 785 790 796 801 807 812 701 818 823 829 834 840 845 851 856 867 792 873 878 883 899 944 949 955 960 966 971 977 794 982 988 993 998 *044 949 955 960 966 971 977 794 982 988 993 998 *044 *009 *015 *020 *026 *031 795 90 037 042 048 053 059 064 069 75 080 086 796 091 097 102 113 119 124					1				1		647	8 4.0
7'90 763 768 774 779 785 790 796 801 807 812 791 818 823 829 834 840 845 851 856 862 867 792 873 878 883 889 894 900 905 911 916 922 793 927 933 938 944 949 955 960 966 971 977 794 982 988 993 998 *004 *009 *015 *020 *026 *051 795 90 037 042 048 053 059 064 069 075 080 086 796 097 1097 102 108 113 119 124 129 135 140 797 146 151 157 162 168 173 179 184 189 195					-		1			1 .		9 4-5
818 823 829 834 840 845 851 856 862 867 792 873 878 883 889 894 900 905 911 916 922 793 927 933 938 944 949 955 960 966 971 977 794 982 988 993 998 *004 *009 *015 *020 *026 *051 795 90 037 042 048 053 059 064 069 075 080 086 796 097 1097 102 108 113 119 124 129 135 140 797 146 151 157 162 106 173 179 184 189 195 798 200 206 211 217 222 227 233 238 244 249 799						-						
792 873 878 883 889 894 900 905 911 916 922 793 927 933 938 944 949 955 960 966 971 977 794 982 988 993 998 *004 *009 *015 *020 *026 *051 795 90 037 042 048 053 059 064 069 075 080 086 796 097 102 108 113 119 124 129 135 140 797 146 151 157 162 106 173 179 184 189 195 798 200 206 211 217 222 227 233 238 244 249 799 255 260 266 271 276 282 287 203 298 304 800 <				-								
793 927 933 938 944 949 955 960 966 971 977 794 982 988 993 998 *004 *009 *015 *020 *026 *051 795 90 937 042 048 053 059 064 069 075 980 086 796 097 102 108 113 119 124 129 135 140 797 146 151 157 162 106 173 179 184 189 195 798 200 206 211 217 222 227 233 238 244 249 799 255 260 266 271 276 282 287 203 298 304 800 309 314 320 325 331 336 342 347 352 358 <th></th> <th>-</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>1</th> <th>1 .</th> <th></th>		-								1	1 .	
794 982 988 993 998 *004 *009 *015 *020 *026 *031 795 90 037 042 048 053 059 064 069 075 080 086 796 091 097 102 108 113 119 124 129 135 140 797 146 151 157 162 168 173 179 184 189 195 798 200 206 211 217 222 227 233 238 244 249 799 255 260 266 271 276 282 287 203 298 304 800 309 314 320 325 331 336 342 347 352 358					-					1 -		
795 90 037 042 048 053 059 064 069 075 080 086 796 091 097 102 108 113 119 124 129 135 140 797 146 151 157 162 168 173 179 184 189 195 798 200 206 211 217 222 227 233 238 244 249 799 255 260 266 271 276 282 287 203 298 304 800 309 314 320 325 331 336 342 347 352 358							\$955			971		
796 091 097 102 108 113 119 124 129 135 140 797 146 151 157 162 168 173 179 184 189 195 798 200 206 211 217 222 227 233 238 244 249 799 255 260 266 271 276 282 287 293 298 304 800 309 314 320 325 331 336 342 347 352 358			-									
797 146 151 157 162 168 173 179 184 189 195 798 200 206 211 217 222 227 233 238 244 249 799 255 260 266 271 276 282 287 293 298 304 800 309 314 320 325 331 336 342 347 352 358												
798 200 206 211 217 222 227 233 238 244 249 799 255 260 266 271 276 282 287 293 298 304 800 309 314 320 325 331 336 342 347 352 358												
799 255 260 266 271 276 282 287 293 298 304 800 309 314 320 325 331 336 342 347 352 358										· · ·		
800 309 314 320 325 331 336 342 347 352 358												
		309	314	320	325	331	336	342	347	352	358	
1. 1. 0 1 2 0 T 0 0 7 0 7 F. F.	N.	L. 0	I	2	3	4	5	6	7	8	9	P. P.

N.	L. 0	I	2	3	4	5	6	7	8	9	P. P.
800	90 309	314	320	325	331	336	342	347	352	358	
801	363	369	374	380	385	390	396	401	407	412	
802	417	423	428	434	439	445	450	455	461	466	
803	472	477	482	488	493	499	504	509	515	520	
804 805	526	531	536	542	547	553	558	563	569	574	
806	580 634	585	590 644	596 650	601 655	607 660	612 666	617 671	623 677	628 682	
807	687	693	698	703	700	714	720	725	730	736	
808	741	747	752	757	763	768	773	779	784	789	
809	795	800	806	811	816	822	827	832	838	843	
810	849	854	859	865	870	875	881	886	891	897	
811	902	907	913	918	924	929	934	940	945	950	
812	956	961	966	972	977	982	988	993	998	+004	6
813	9I 009	014	020	025	030	036	041	046	052	057	1 0.6 2 1.2
814 815	062	068	073	078	084	089	094	100	105	IIO IGA	3 1.8
816	160	121	126 180	132 185	137 190	142	148 201	153	158	164	4 2.4 5 3.0 6 3.6
817	222	228	233	238	243	249	254	259	265	270	
818	275	281	286	291	297	302	307	312	318	323	8 4.8
819	328	334	339	344	350	355	360	365	371	376	9 5.4
820	381	387	392	397	403	408	413	418	424	429	
821	434	440	445	450	455	461	466	471	477	482	
822	487	492	498	503	508	514	519	524	529	535	
823	540	545	551	556	561	566	572	577	582	587	
824 825	593	598	603	609	614	619	624	630	635	640	
826	645 698	651 703	656 700	661 714	666	672	677 730	682	687 740	693 745	
827	751	756	761	766	772	777	782	787	793	798	
828	803	808	814	819	824	829	834	840	845	850	
829	855	861	866	871	876	882	887	892	897	903	
830	908	913	918	924	929	934	939	944	950	955	
831	960	965	971	976	981	986	991	997	*002	*007	5
832	92 012	018	023	028	033	038	044	049	054	059	I 0.5 2 I.0
833	065	070	075	080	085	091	096	IOI	106	III	3 1.5
834 835	117 169	122 174	127 179	132 184	137 189	143 195	148	153	158	163	4 2.0 5 2.5
836	221	226	231	236	241	247	252	257	262	267	6 3.0
837	273	278	283	288	293	298	304	300	314	319	7 3.5 8 4.0
838	324	330	335	340	345	350	355	361	366	371	9 4.5
839	376	381	387	392	397	402	407	412	418	423	
840	428	433	438	443	449	454	459	464	469	474	
841	480	485	490	495	500	505	511	516	521	526	
842	531	536	542	547	552	557	562	567	572	578	
843 844	583 634	588	593	598	603	609 660	614	619 670	624 675	629 681	
845	686	639 691	645 696	650 701	655 706	711	716	722	075 727	732	
846	737	742	747	752	758	763	768	773	778	783	
847	788	793	799	804	809	814	819	824	829	834	
848	840	845	850	855	860	865	870	875	881	886	
849	891	896	901	906	911	916	921	927	932	937	
850	942	947	952	957	962	967	973	978	983	985	
N.	L. 0	I		3	4	=5	6	7	8	9	P. P.

N.	L. 0	I	2	3	4	5	6	7	8	9	P. P.
850	92 942	947	952	957	962	967	973	978	983	988	
851	993	998	*003	*008	*013	*018	*024	*029	*034	*039	
852	93 044	049	054	059	064	060	075	080	085	000	
853	095	100	105	110	115	120	125	131	136	141	
854	146	ISI	150	161	166	171	176	181	186	192	
855	197	202	207	212	217	222	227	232	237	242	
856	247	252	258	263	268	273	278	283	288	293	6
857	298	303	308	313	318	323	328	334	339	344	1 0.6
858 859	349	354 404	359	364	369 420	374	379	384	389	394	2 1.2 J 1.8
	399		460			425	430	435		445	I I.8 A 2.4
860	450	455		465	470	475	480	485	490	495	5 3.0
861 862	500	505	510	515 566	520	526	531	536 586	541	546	7 4.2
863	551 601	556 606	561 611	616	57I 62I	576	581 631	636	59I 64I	596 646	8 4.8
864	651	656	661	666	671	676	682	687	692	697	9 5-4
865	702	707	712	717	722	727	732	737	742	747	
866	752	757	762	767	772	777	782	787	792	797	
867	802	807	812	817	822	827	832	837	842	847	
868	852	857	862	867	872	877	882	887	892	897	
869	902	907	912	917	922	927	932	937	942	947	
870	952	957	962	967	972	977	982	987	992	997	
871	94 002	007	OI2	017	022	027	032	037	042	047	
872	052	057	062	067	072	077	082	086	100	096	1 0.5
873	IOI	106	III	116	121	126	131	136	141	146	2 1.0
874	151	156	161	166	I7I	176	181	186	191	196	3 I.5 4 2.0
875 876	201	206	211	216	221	226	231	236	240	245	5 2.5
877	250 300	255 305	260 310	265 315	270 320	275	280	285	290 340	295	
878	349	354	359	364	369	325 374	330	335	389	345 394	8 4.0
879	399	404	409	414	419	424	429	433	438	443	<u>9</u> 4+5
880	448	453	458	463	468	473	478	483	488	493	
881	498	503	507	512	517	522	527	532	537	542	
882	547	552	557	562	567	571	576	581	586	591	
883	596	601	606	611	616	621	626	630	635	640	
884	645	650	655	660	665	670	675	680	685	689	
885	694	699	704	709	714	719	724	729	734	738	
886	743	748	753	758	763	768	773	778	783	787	
887	792	797	802	807	812	817	822	827	832	836	I 0.4
888 889	841	846	851	856	861	866	871	876	880	885	∎ 0.8
-	890	895	900	905	910	915	919	924	929	934	U 1.2 4 1.6
890	939	944	949	954	959	963	968	973	978	983	8 2.0
891	988	993	998	*002	*007	*012	*017	*022	*027	*032	
892 893	95 036	041	046	051	056	061	066	071	075	080	8 3.2
893	085 I 34	090	095	100 148	105	109 158	II4 I63	119	124	129 177	9 3.6
895	134	139	I43 I92	140	202	207	211	216	221	226	
896	231	236	240	245	250	255	260	265	270	274	
897	279	284	289	294	299	303	308	313	318	323	
898	328	332	337	342	347	352	357	361	366	371	
899	376	381	386	390	395	400	405	410	415	419	
900	424	429	434	439	444	448	453	458	463	468	
N.	L. 0	r	2	3	4	5	6	7	8	9	P. P.

N.	L. o	1	2	3	4	5	6	7	8	9	P. I	2.	
900	95 424	429	434	439	444	448	453	458	463	468	 		
901	472	477	482	487	492	497	501	506	511	516			
902	521	525	530	535	540	545	550	554	559	564			
903	569	574	578	583	588	593	598	602	607	612			
904	617	622	626	631	636	641	646	650	655	660			
905	665	670	674	679	684	689	694	698	703	708			
906	713	718	722	727	732	737	742	746	751	756			
907	761	766	770	775	780	785	789	794	799	804			
908	809	813	818	823	828	832	837	842	847	852			
909	856	861	866	871	875	880	885	890	895	899			
910	904	909	914	918	923	928	933	938	942	947		5	
911	952	957	961	966	971	976	980	985	990	995	1 10	.5	
912	999	+004	*009	*014	*019	*023	*028	*033	*038	*042	2 1	0.1	
913	96 047	052	057	061	066	071	076	080	085	000			
914	095	099	104	109	114	118	123	128	133	137		2.5	
915	142	147	152	156	161	166	171	175	180	185	6 3	3.0	
916	190	194	199	204	200	213	218	223	227	232	7 3	3.5	
917	237	242	246	251	256	261	265	270	275	280		-5	
918	284	289	294	298	303	308	313	317	322	327			
919	332	336	341	346	350	355	360	365	369	374			
920	379	384	388	393	398	402	407	412	417	421			
921	426	431	435	440	445	450	454	459	464	468			
922	473	478	483	487	492	497	501	506	511	515			
923	520	525	530	534	539	544	548	553	558	562			
924	567	572	577	581	586	591	595	600	605	609			
925	614	619	624	628	633	638	642	647	652	656			
926	661	666	670	675	680	685	689	694	699	703			
927	708	713	717	722	727	731	736	741	745	750			
928	755	759	764	769	774	778	783	788	792	797			
929	802	806	811	816	820	825	830	834	839	844			
930	848	853	858	862	867	872	876	881	886	890			
931	895	900	904	909	914	918	923	928	932	937			
932	942	946	951	956	960	965	970	974	979	984			
933	988	993	997	*002	*007	*011	*016	*021	*025	*030			
934	97 035	039	044	049	053	058	063	067	072	077	- 1	4	
935	081	086	000	095	100	104	109	114	118	123	1 0	0.4 0.8	
936	128	132	137	142	146	151	155	160	165	169	3 1	1.2	
937	174	179	183	188	192	197	202	206	211	216	4 1	1.6	
938	220	225	230	234	239	243	248	253	257	262		2.0	
939	267	271	276	280	285	290	294	299	304	308	7 2	2.8	
940	313	317	322	327	331	336	340	345	350	354		3.2 3.6	
941	359	364	368	373	377	382	387	391	396	400			
942	405	410	414	419	424	428	433	437	442	447			
943	451	456	460	465	470	474	479	483	488	493			
944	497	502	506	511	516	520	525	529	534	539			
945	543	548	552	557	562	566	571	575	580	585			
946	589	594	598	603	607	612	617	621	626	630			
947	635	640	644	649	653	658	663	667	672	676			
948	681	685	690	695	699	704	708	713	717	722			
949	727	731	736	740	745	749	754	759	763	768			
950	772	777	782	786	791	795	800	804	809	813	 		-
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N.	L. o	I	2	3	4	5	6	7	8	9	P. P.
950	97 772	777	782	786	791	795	800	804	800	813	
951	818	823	827	832	836	841	845	850	855	859	
952	864	868	873	877	882	886	SQI	896	000	905	
953	909	410	918	923	928	932	937	941	946	950	
954	955	959	964	968	973	978	982	987	991	996	
955	98 000	005	009	014	019	023	028	032	037	041	
956	046	050	055	059	064	068	073	078	082	087	
957	100	096	100	105	109	II4	118	123	127	132	
958	137	141 186	146	150	155	159	164	168	173	177	
959	182		191	195	200	204	209	214		223	
960	227	232	236	241	245	250	254	259	263	268	
961	272	277	281	286	290	295	299	304	308	313	. 5
962	318	322	327	331	336	340	345	349	354	358	1 0.5
963	363	367	372	376	381	385	390	394	399	403	2 1.0 3 1.5
964 965	408 453	412	417 462	421 466	426	430	435 480	439	444 489	448 493	4 2.0
905	453	45/	507	511	516	520	525	529	534	538	5 2.5 6 3.0
967	543	547	552	556	561	565	570	574	579	583	7 3.5
968	588	592	597	601	605	610	614	619	623	628	8 4.0
969	632	637	641	646	650	655	659	664	668	673	9 4-5
970	677	682	686	691	695	700	704	709	713	717	
971	722	726	731	735	740	744	749	753	758	762	
972	767	771 816	776	780	784	789	793	798	802	807	
973	811		820	825	829	834	838	843	847	851	
974	856	860	865	869	874	878	883	887	892	896	
975	900	905	909	914	918	923	927	932	936	941	
976	945 989	949 994	954 998	958 *003	963 *007	967 *012	972 *016	976 *021	981 *025	985 *029	
977 978	99 034	038	043	047	052	056	061	065	060	074	
979	078	083	087	092	096	100	105	100	114	118	
980	123	127	131	136	140	145	149	154	158	162	
981	167	171	176	180	185	189	193	198	202	207	4
982	211	216	220	224	229	233	238	242	247	251	1 0.4
983	255	260	264	269	273	277	282	286	291	295	2 0.8 3 1.2
984	300	304	308	313	317	322	326	330	335	339	4 1.6
985	344	348	352	357	361	366	370	374	379	383	5 2.0 6 2.4
986	388	392	396	401	405	410	414	419	423	427	7 2.8
987	432	436	441	445	449	454 498	458	463	467	471 515	8 3.2 9 3.6
989	520	524	528	533	537	542	546	550	555	559	1000
990	564	568	572	577	581	585	590	594	599	603	
100	607	612	616	621	625	620	634	638	642	647	
992	651	656	660	664	669	673	677	682	686	691	
993	695	699	704	708	712	717	721	726	730	734	
994	739	743	747	752	756	760	765	769	774	778	
995	782	787	791	795	800	804	808	813	817	822	
996	826	830	835	839	843	848	852	856	861	865	
997	870	874	878	883	887	168	896	900	904	909	
998	913	917	922	926	930	935	939	944	948	952	
999	957	961	965	970	974	978	983	987	100	996	-
		004	009	013	017	022	026	030	035	039	
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2.5400 0.40483 10.764 1.03198 0.092901 2.96802 2.78551 0.061025 16.387 1.21449 1.42190 0.26418 3.7853 0.57810 2.2046 0.34333 1.65667 0.45359



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