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## HENDY'S Handy Atlas of the World

Containing New Maps of Each State and Territory in the United States and Each Country in the World

> Also Practical Pointers and Condensed Data for the Machinist, Mechanic, Millman and Miner.


# ALPHABETICAL LIST OF STATES AND COUNTRIES 

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## PROJECTION

EXPLANATORY NOTE
 of a globe, if removed and later, For example, Greenland, whlch, on Mercator's Projection, seems to be larger than South America, here is shown in its relative proportion of size to that continent, having less than one-eighth of the latter's area. In fact, this is the oniy projection in which are shown the equivalent areas, or correct sizes, of all parts of the giobe, in their proper relative position.
 FEATURES
Submarine Cahles, shown in fine black lines.
Colonial possessions of European powers in Africa, Asia and Oceania, shown in colors corresponding with those used for mother countries.
























ATLAS OF THE WORLD

















(ays)


















ATLAS OF THE WORLD








MEXICO


AUSTRALIA


NIGARAGUA


PORTUGAL


IRELAND


HONDURAS


BRAZIL


SALVADOR


CHILE


SPAIN ENSIGN


FLAGS OF ALL NATIONS












Land to bo excerased rulued enue: $\square$






## PRINCIPAL CITIES OF THE WORLD

The following list contains the principal towns of the world in all countries except the United States. In it will be found approximately all places of more than thirty thousand inhabitants and most of those of from twenty to thirty thousand. The date of the latest census enumerations and official estimates of the following countries is given as indicating the respective value of the figures used in the compilation: Algeria, 1901; Australia, 1901; Austria Hungary, 1900; British South African States, 1904; England and Wales, 1901, with government estimates of all towns of over 50,000 for 1905; Germany, 1901, with government estimates of Berlin, Hamburg and Essen for 1905; Japan, 1903; Philippine Islands, 1903; Sweden, 1905.

| hen, Germany | 135,245 |
| :---: | :---: |
| Aalborg. Denm | 31,457 |
| Aarbus, Denma | 51,81 |
| A bbeokuta, Yor | 150,000 |
| Aberdare. Wales | 43,357 |
| Aderdeen, Scot | 167,537 |
| Abo, Russia | 38,235 |
| Accrington, En | 48,890 |
| Acireale, Italy | 35,418 |
| Acton, England | 37,744 |
| Adama. Turkey in | 15,000 |
| Adelalde, Australia. | 170,729 |
| Aden, Arabla | 42,758 |
| Adis Abeba, Abyssinia | 35,000 |
| Adrianople, Turkey in Europe | 81,000 |
| Agra, India. | 180,022 |
| Abmadabad, Ind | 185,888 |
| Addin, Turkey in | 38,000 |
| Aix, France | 24,861 |
| Ajmer, India | 73,839 |
| Akerman, Ru | 32,470 |
| Akita. Japan | 34,350 |
| Alcano. Italy | 51,809 |
| Alcoy, Spain. | 32,053 |
| Aldershot, Engla | 30,974 |
| Aleppo, Turkey in | 127,150 |
| Alessandria, Italy | 71,298 |
| Alexandria, Egypt | 319,766 |
| Alexandropol, Russia | 32,018 |
| Alexandrovsk, Rus | 40,807 |
| Algiers, Algeria | 96,542 |
| Alicante, Spain | 50,142 |
| Allgarh, India | 70,434 |
| Allahabad, Indi | 172,032 |
| Allenstein. Germ | 24,287 |
| Almeria, Spsin. | 47,320 |
| Alost, Belgium. | 31,655 |
| Altenburg, Germany | 37,110 |
| Altendorf, Germany | 63,238 |
| Altona, Germany. | 161,501 |
| Alwar, India. | 56,771 |
| Ambala, Indi | 78,638 |
| Amlens, Fran | 90,758 |
| Amoy, China | 114,000 |
| Amritsar, India | 162,429 |
| Amsterdam, Net | 551,415 |
| Ascona, Italy. | 56,835 |
| Anderlecht. Bel | 51.921 |
| Andijan, Russia in Asis | 16,882 |
| Indria, Italy. | 49,509 |
| Angers. France | 82,308 |
| Angoulema Franca | 87,650 |


| Barquisimeto, Venezuela. | 31,470 |
| :---: | :---: |
| Barranquilla, Colombia. | 65,000 |
| Barrow-In-Furness, England. . | 60,300 |
| Basel, Swltzerland. | 124,392 |
| Basra. Turkey in Asia. | 50,000 |
| Batangas, P. | 33,131 |
| Batavia, Ja | 115,887 |
| Bath, Engiand. | 49,817 |
| Batley, England | 30,321 |
| Batum, Russia. | 28,512 |
| Bauan, P. I. | 39,048 |
| Bautzen, Germany | 28,125 |
| Bayonne, France | 25,075 |
| Bedford, England | 35,144 |
| Beirut, Turkey in Asi | 118,800 |
| Bekes. Hungary. | 37,547 |
| Belfast. Ireland | 349,180 |
| Belfort. Fran | 32,567 |
| Belgrade. Servia | 60,790 |
| Bellary, India. | 58,247 |
| Benares. India | 209,331 |
| Bender, Russi | 35,741 |
| Bendigo. Australia | 42,600 |
| Benevento, Italy. | 24,447 |
| Berbera, Br, Somalilan | 30,000 |
| Berdiansk, Russla. | 29,168 |
| Berditchef, Russis | 63,728 |
| Bergamo, Italy. | 47,772 |
| Bergen, Norway | 72,251 |
| Berlat, Roumani | 24,000 |
| Beriln. Germany | 2,033,000 |
| Bera, Switzerlan | 70,339 |
| Bernburg, Germany | 34,175 |
| Besancon, France | 55,406 |
| Beuthen, Germany | 61,369 |
| Beziers, France | 52,510 |
| Bhagaipur, India | 75,560 |
| Bhaunagar. Indla | 56,442 |
| Bhopal, India. | 77,023 |
| Bialystok, Russia | 63,040 |
| Biel, Swltzerland. | 29,304 |
| Blelefeld, Germany | 63,040 |
| Bikanor, Indla. | 63,078 |
| Bilbao, Spain. | 83,30e |
| Birkenhead, England | 118,035 |
| Birmingham, Engiand | 542,959 |
| Bltis, Turkey In Asia. | 38,800 |
| Blackburn, England. | 133,067 |
| Blackpool, England. | 47,346 |
| Blagoveschensk, Russia in Asis | 37,368 |
| Bloemfontein, Orange R. Col. | 33,890 |
| Blols, France. . . . . . | 20.64 |

## PRINCIPAL CITIES OF THE WORLD-Continued

|  | 40,000 |
| :---: | :---: |
| Bobrinsk, Russia. | 35,177 |
| Bochum, Germany | $6 \mathrm{Ej}, 5 \mathrm{5} 1$ |
| Bogota, Colombia | 130,000 |
| Bologna, Italy . | 152,009 |
| Bolton, Englan | 178,111 |
| Bombay, India | 776,006 |
| Bona, Al | 36,993 |
| Bonn, Cerman | 50,736 |
| Bootle, Engla | 62,758 |
| Bordeaux, Franc | 257,638 |
| Borgerhout, Belgit | 11,075 |
| Botuchany, Rouma | 32,000 |
| Boulogne-sur-Mer, |  |
| Boulogne-sur-Selne |  |
| Bourges, France. | 66,551 |
| Bournemouth, En | 66,168 |
| Bradford, England | 286,799 |
| Braga. Portugal | 24,202 |
| Bralia. Roumanta | 58,392 |
| Brandenburg, Germ | 49,250 |
| Breda, Netherlands. |  |
| Bremen. German | 163,297 |
| Brescia, Italy. | 70,614 |
| Breslau, Germ | 422,709 |
| Brest. France. | 84,284 |
| Brest-Litovsk, Rus | 42,812 |
| Bridgetown, Barb | 35,000 |
| Brleg. Germany. | 24,224 |
| Brighton, Engla | 127,183 |
| Brishane, Australl | 122,815 |
| Bristol, England | 358,515 |
| Broken Hill. Australl | 27,500 |
| Bromberg, Gcrmany | 52,204 |
| Bruges, Belgium | 53,728 |
| Brunn. Austrla | 109,346 |
| Brunswlek, Gcrma | 128,226 |
| Brusa, Turkey in A |  |
| Brussels. Belgium. | 508,509 |
| Budapest, Hungar | 732,322 |
| Budwels, Austria. | 39,328 |
| Buenos Aires, Argen | 979,235 |
| Bukharest. Rou | 282,071 |
| Burgos. Spaln. | 30,167 |
| Burnley, Englan | 101,682 |
| Burslem, Engla |  |
| Burton-upon-Trent, | 52,424 |
| Eury, England. | 58,954 |
| Cadiz, Spa | 69,382 |
| Caen, Fran | 44,794 |
| Cagliarl, Italy | 53.747 |
| Cairo. Egypt | 570,062 |
| Calals, Franc | 59,743 |
| Calcutta, Ind | 028,987 |
| Callcut. India | 76,881 |
| Callao, Per | 31,000 |
| Caltagirone, Ita | 44,879 |
| Caltanisetta, Italy | 43,303 |
| Camaguey, Cuba | 25.102 |
| Cambrldge, Engl | 38,393 |
| Canea, Cre |  |
| Cannes, Fran | 30,420 |
| Cannstadt, German | 28,575 |
| Canterbury, Englan | 24,809 |
| Canton, China | 800,000 |
| Cape Coast Castle, Gol Africa. $\qquad$ | 28,943 |
| Cape Halticn, IIaltl. | 29,000 |
| Cape Town, Cape of |  |
| Hope. | 87,483 |
| Caracas, Venezuela | 72,429 |
| Carcassonne, Fran | 30,720 |
| Cardenas, Cuba | 26,448 |
| Cardiff. Wales | 180,054 |
| Carear, P. I. | 31,805 |
| risisle. E | 45,478 |
| ra, Italy | 4,007 |


| Spa | 99,871 |
| :---: | :---: |
| Caserts, Italy. | 32,709 |
| Cassel, Germany | 106,034 |
| Castellon, Spaln. | 29,904 |
| Castres, Franc | 24,135 |
| Catanla, Italy |  |
| Catanzaro, Ita | 31,824 |
| Cawnpur, India | 197,170 |
| Ceara, Brazil | 40,902 |
| Cebls, P. I. | 31,079 |
| Celaya, Mexico | 25,565 |
| Cette, France. | 33,246 |
| Chalon-sur-SaO | 26,462 |
| Changsha, China |  |
| Charleroj, Belgi | 26,528 |
| Charlottenburg, Ge | 189,305 |
| Chatham, England | 40,753 |
| Chaux de Fonds, Switzerland | 38,784 |
| Chefu. Chlna.. | 75,000 |
| Cheltenham, Englan | 19,439 |
| Chemnitz, Germany | 214,030 |
| Cherbourg. Franc |  |
| Chernigot, Russia | 27,006 |
| Chester, England | 38,309 |
| Chteta, Italy. | 26,368 |
| Chihuahua, M | 30,405 |
| Chllan, Chile | 36,681 |
| Chinandega, Nica | 20,000 |
| Chingtu, China. | ,000,000 |
| ChInklang. | 167,000 |
| Cholan, China | 129,721 |
| Christehurch, New Zea | 57,041 |
| Christlania, Norway | 227,628 |
| Chungking, China | 600,000 |
| Cienfuegos, Cuba. | 59,428 |
| Clermont. France | 52,833 |
| Clichy, France |  |
| Coatbridge, Scot |  |
| Coban, Guatemala. | 30,770 |
| Coblenz, Germany | 47,520 |
| Cochabamba, Bollv | 21,886 |
| Colmbatore, India. | 53,080 |
| Colchesicr. Englan | 38,351 |
| Colmar, Germany |  |
| Cologne, Germany | 372,529 |
| Colombo, Ceylon | 158,228 |
| Combaconum, In | 59,673 |
| Como, Italy | 38,895 |
| Concepcion, Chile | 55,458 |
| Constantlne, Algeri | 48,243 |
| Constantinople. Turkey | ,125,000 |
| Copenhagen, Dermark | 500,479 |
| Cordoba, Argenína. |  |
| Cordova, Spaln | 58,275 |
| Cork, Ireland | 76,123 |
| Coruna, Spaln | 43,971 |
| Courbevole, Fra | 23.796 |
| Coutral, Belgium. | 34,564 |
| Coventry, Englan | 75,134 |
| Crajova, Rouma | 45,438 |
| Crefeld, Germany | 107,968 |
| Cremona, Italy | 37,693 |
| Crewe, Engla | 42,075 |
| Cronstadt, Russ | 59,539 |
| Croydon, England | 147,704 |
| Cuddalore, India | 52,216 |
| Cuenca, Ecua | 30,000 |
| Cuneo, Italy | 27,065 |
| Cuttack, India | 51,364 |
| Czegled, Hungar | 30,106 |
| Czenstochowa. Ru | 53,650 |
| Czernowitz, Austria | 67,623 |
| Dacca, Indla. |  |
| Daman, India. | 41,671 |
| Damanhur, Egypt | 27,263 |
| Damascus, Turkey in As | 225,000 |
| DanzIg, Germany. | 147,301 |


| , | 66,2* |
| :---: | :---: |
| Darlington, England. | 44,400 |
| Darmstadt, Germany | 72,381 |
| Darwen, England | 38,211 |
| Debreczin. Hunga | 75,008 |
| Delift. Netherland | 32,050 |
| Delhi, India | 208,575 |
| Derby, England | 122,207 |
| Dessau. Germany | 50,849 |
| Deventer, Netherl | 27,411 |
| Devonport, England | 78,864 |
| Diarbekr, Turkey | 34,000 |
| Dljon. France. | 71,320 |
| Dordrecht. Ne | 43,482 |
| Dorpat, Russ | 42,421 |
| Dortmund, Ger | 142,733 |
| Doual. France. | 33,649 |
| Dover, Engla | 41,782 |
| Drammen, Norw | 23,003 |
| Dresden, German | 480,658 |
| Dublin, Ireland. | 373,178 |
| Dudley. England | 48,808 |
| Dulsburg. Germany | 94,185 |
| Dumbarton, Scotlan | 115,176 |
| Dunaburg, Russla. | 65,900 |
| Dundee. Scotland | 164,260 |
| Dunedin, New Zea | 62,300 |
| Dunkirk, France | 38,825 |
| Durango, Mexico | 31,092 |
| Durban, Natal. | 79,000 |
| Düren, German | 27,185 |
| Düsseldorf. Germ | 213,711 |
| Dvinsk, Russia. |  |
| Ealling, England. | 85,040 |
| Eastbourne, England | 43,337 |
| East Ham, England | 05,089 |
| East London, C. of Go | 25,220 |
| Eccles, England. | 34,300 |
| Eclja, Spaln | 24,395 |
| Edinburgh, Scotland. | 338,577 |
| Edmonton, Engla | 46,899 |
| Eger, Austrla. | 23,675 |
| Eisenach. Germany. | 31,457 |
| Ekaterinburg, Russi | 55,448 |
| Ekaterinodar, Russla | 65,007 |
| Ekaterinoslat, Russi | 135,552 |
| Elberfeld, Germany | 156,288 |
| Elbing, Germany. | 52,518 |
| Elche, Spain. | 27,380 |
| Elizavetgrad, Russi | 68,188 |
| Elizavetpol, Russi | 33,090 |
| Enfleld, England. | 42,738 |
| Enschede, Nether | 29,510 |
| Erfurt, Germany | 85,202 |
| Erivan, Russla. | 29,033 |
| Erzerum, Turkey | 38,000 |
| Essen, Germany.. | 229,270 |
| Esslingen, Germa | 27,260 |
| Exeter, England | 47,185 |
| Faizabad, Indla. | 75,085 |
| Falkirk, Scotland | 20,271 |
| Farakhabad. India | 67,338 |
| Felegyhaza. Hungar | 83,400 |
| Ferrara. Italy. | 87,648 |
| Ferrol, Spain | 25,281 |
| Fez, Morocco | 140,000 |
| Flume, Hungary | 38,955 |
| Flensburg, German | 48,922 |
| Florence, Italy. | 205,589 |
| Foggla, Italy | 63,151 |
| Folkstone, Eng | 30,024 |
| Forli. Italy. | 43,708 |
| Forst. Germany | 32,150 |
| Fort de France, Marti | 22,104 |
| Frankfort-on-Main, Ger | 288,089 |
| Frankfortoon-Oder. Germ | 61,852 |

## PRINCIPAL CITIES OF THE WORLD-Continued

|  | $34,$ |
| :---: | :---: |
| relberg, Germany | 31, |
| Freiburg, Germany | 61,504 |
| Fremantle, Austral | 23,006 |
| Fuchau, China | 624,000 |
| Fukui, Japan | 50,155 |
| Fukuoka, Japa | 71,047 |
| Funchal, Madeira |  |
| Fünfkirchen, H |  |
| Fifth, Germany. |  |
| Gäfe, Sweden | 30,776 |
| Galatz, Rouman | 62,678 |
| Gailipoil, Turkey. | 30,000 |
| Gateshead, Engla | 120,620 |
| Gaya. India |  |
| Gelsenkirchen, |  |
| Geneva, Swit | 112,736 |
| Genoa, Italy | 234,710 |
| Georgetown, B | 53,176 |
| Gera, Germany | 45,034 |
| Ghent, Belgiu | 162,925 |
| Gibraltar. Spa | 27,460 |
| Giessen, Germ |  |
| Gifu, Japan. | 10,188 |
| Gijon, Spain | 47,544 |
| Gllilingham, Enc | 42,530 |
| Girgenti. Italy | 25,025 |
| Gladbach, Germany | 58,023 |
| Glasgow, Scotland | 809,986 |
| Glauchau, Germany | 25,776 |
| Gleiwitz, Germany |  |
| Gloucester, Engla | 47,955 |
| Gomel, Russia | 45,081 |
| Gorakhpur, India | 64,148 |
| Gorlitz, Germany | 80,931 |
| Gotha, Germany | 34,185 |
| Gottenborg, Swed | 138,030 |
| Gottingen, Germany | 39,359 |
| Govan, Scotland | 76,351 |
| Granada. Nicarag | 25,000 |
| Granada. Spain | 75,900 |
| Gratz. Austria | 138,080 |
| Graudenz, Germany | 32,788 |
| Great Grimsby. Engl | 68,153 |
| Greenock, Scotland | 70,253 |
| Grenoble, France | 68,615 |
| Grodno. Russia | 41,756 |
| Groningen. Netheriands | 71,490 |
| Grosswardeln, Hungar | 50,177 |
| Guadalajara, Mexico | 101,208 |
| Guanajuato, Mexlco | 41,480 |
| Guayaquil, Ecuador | 51,000 |
| Guben, Germany | 33,135 |
| Gwalior, Indis. | 119,433 |
| Haarlem. Netherlan | 68,518 |
| Hagen, Germany | 50,812 |
| Hague, Netherlands | 234,459 |
| Haidarabad, India. | 448,448 |
| Fakodate, Japan. | 83,313 |
| Halberstadt, Germa | 42,810 |
| Halifax, England. | 108,419 |
| Halitax. Nova Sco | 10,832 |
| IIaile, Germsng | 156,609 |
| Hälsingborg, Sweden | 27,253 |
| Hama, Turkey in As | 44,000 |
| Hamadan, Persia. | 40,000 |
| Hamburg, Germany | 872,028 |
| IIamilton, Ontarlo. C | 52,634 |
| Hamilton, Scotland | 32,775 |
| Hamm. Germany | 31,390 |
| Handsworth. Engla | 52,921 |
| Hangchau, China | 300,000 |
| Hankau, China | 870,000 |
| Hanley, England | 64,607 |
| Hanol. Anam. | 103,238 |
| Hanover, Germany | 235,049 |


| Harar, Abyssinla | 40,000 |
| :---: | :---: |
| Harbin, China | 60,000 |
| Harburg, Germany | 49,153 |
| Hastings, England | 66,820 |
| Hav ana. Cuba | 262,395 |
| Havre, France | 130,196 |
| Heidelberg, Germany | 40,121 |
| Heilbronn, Germany | 37,891 |
| Helder, Netheriands | 20,681 |
| Helsingtors, Finland | 93,570 |
| Herat, Afghanistan. | 45,000 |
| Hildesheim, Germany | 42,973 |
| Himeji, Japan. | 36,443 |
| Hirosakl. Japan | 36,509 |
| Hiroshima, Japan | 121,198 |
| Howart, Australia | 34,809 |
| Hodmezo-Vasarbely, Hungary | 60,883 |
| Hof, Germany . | 32,805 |
| Hongkong, China | 136,900 |
| Honolulu, Hawail | 39,300 |
| Hornsey, England | 72,058 |
| Hove, Engiand | 36.542 |
| Howrah, India | 157,594 |
| Hubli, India. | 60,214 |
| Huddersfield, Eng | 96,008 |
| Hue, Anam | 50,000 |
| Huil, England | 258,127 |
| Hyde, England | 32,708 |
| Ibadan, Yoruba | 200,000 |
| Ichang, China. | 45,000 |
| Igtau. Austria | 24,423 |
| Ilford England | 41,240 |
| Imoschi, Austria | 36,789 |
| Indore, India. | 97,804 |
| Innsbruck, Austria | 27,058 |
| Inowraclaw, Germany | 20,152 |
| Insterburg, Germany | 27,288 |
| Ipswich, Engiand. | 20,802 |
| Iquique, Chile. | 43,005 |
| Irkutsk, Russla in Asia | 49,108 |
| Iserlobn. Germany. | 27,275 |
| Ismall, Russia | 33,607 |
| Ispahan, Persia.. | 80,000 |
| I vanovo-Voznesensk. P | 56,628 |
| Ivry-sur-Seine, France | 25,575 |
| Ixelies, Beigium | 62,879 |
| Jabalpur. India. | 00,318 |
| Jalpur, India. | 160,167 |
| Jalandhar, Indla | 67,735 |
| Janina, T-ikey | 25,000 |
| Jaroslaw, Austr | 22,641 |
| Jarrow, England | 34,204 |
| Jassy, Roumania | 78,069 |
| Jerez, Spaln. | 63,473 |
| Jerusalem, Turkey in | 18,000 |
| Jhansl, India.. | 55,724 |
| Jodhpur, India | 60,437 |
| Johannesburg, Transvaal | 158,580 |
| Jokjokarta, Java | 58,229 |
| Jönköping. Swed | 23,240 |
| Jumet, Beigium | 25,950 |
| Kabul. Atghanistan. | 70,000 |
| Kagoshima, Japan. | 59,001 |
| Kaiserleh, Turkey in As | 72,000 |
| Kalserslautern, Germany | 48,310 |
| Kaluga, Russia......... | 49,728 |
| Kamenetz, Russi | 39,113 |
| Kanazawa, Japan | 99,657 |
| Kandahar, Afghanistan | 60,000 |
| Karachi, India. | 110,663 |
| Kariskrona. Sweden | 20,074 |
| Karlsruhe, Germany | 97,185 |
| Kaschau, Hungary. | 40,102 |
| Kashan, Persia | 40,000 |
| Kashgar. Turkestan. | 75,000 |



40,367 Kattowitz, Germany.......... 31,74Kazvin, Persia40,000
34,454
82,000La Paz. Bollvia

## PRINCIPAL CITIES OF THE WORLD-Continued

| Le Mans, France | 63,272 |
| :---: | :---: |
| Lemberg, Aust | 159,877 |
| Lens, France | 24,353 |
| Lenz, Austria. | 58,791 |
| Leon, Mexico | 63,263 |
| Leon, Nicarag | 45,000 |
| Leyton, Englan | 88,899 |
| Libau. Russia. | 64,505 |
| Lichtenberg, Ge | 43,371 |
| Lleben, Austria | 21,375 |
| Lege, Belgium | 168,532 |
| Legnltz, Germ | 54,882 |
| Lima. Peru. | 130,000 |
| Limerlck, | 45,809 |
| Limoges, Franc | 84,121 |
| Linares, Chlle. | 33,000 |
| Linares, Spain | 38,245 |
| Lincoln, Engla | 48,784 |
| Linden, Germa | 50,628 |
| Lipa, P. I | 37,924 |
| Llsbon, Portug | 356,009 |
| Lisle, France | 210,696 |
| Liverpool, Engla | 730,143 |
| Lodz, Russla | 351,570 |
| London, England | ,580,016 |
| Zondon, Ont., Cana | 37,083 |
| Londonderry. Irelan | 39,892 |
| Longton. England. | 35,825 |
| Lorca, Spain. | 69,836 |
| Lorlent. Fran | 44,640 |
| Louvain. Belgium | 42,194 |
| Lübeck, Germa | 82,098 |
| Lublin, Russla. | 50,152 |
| Lucca, Italy. | 74,971 |
| Lucerne, Swltzer | 32,801 |
| Lucknow, India. | 264,049 |
| Ludwlgshaten, Germ | 61,814 |
| Lüneburg, Germany | 24,715 |
| Luton, England. | 36,404 |
| Luxemburg, Lu | 20,928 |
| Lyon, France. | 159,099 |
| Maastricht. Netherlands. | 36,140 |
| Macao, China. | 63,991 |
| Macclesfleld, England. | 34,635 |
| Madras, Ind ${ }^{\text {a }}$. | 509,346 |
| Madrid, Spaln | 533,835 |
| Madura, Indla | 105,984 |
| Magdeburg, Germany | 229,667 |
| Maldstone, England | 33,510 |
| Malkop. Russla In | 34,191 |
| Mainz. Germany | 84,251 |
| Mako, Hungary | 33,722 |
| Malaga, Spaln | 130,109 |
| Malines, Belgiu | 58,101 |
| Malmo. Sweden | 70,797 |
| Managua, Nicaragua | 30,000 |
| Manchester, England | 631,185 |
| Mandalay, India | 183,816 |
| Manlla, P. I | 219,928 |
| Manipur, Indla | 67,093 |
| Manlssa. Turkey in | 50,000 |
| Mannheim, Germany | 141,131 |
| Mantua, Italy... | 29,142 |
| Maracaibo. Venezue | 34,284 |
| Maranhao, Brazll. | 29,308 |
| Marla Thereslopol, Hung | 82,122 |
| Mariapol. Russia. | 52,770 |
| Marsala, Italy | 57,567 |
| Marsellie. France | 491,161 |
| Maskat, Arabia | 60,000 |
| Massa, Italy. | 26,413 |
| Matanzas, Cuba. | 45,282 |
| Matsuyama, Japan | 37,841 |
| Matsuye, Japan. | 35.081 |
| Maulman. Ind | 58,446 |
| Mayebeshi, Japan | 41,724 |
| Mecca, Turkey in A | 00,000 |


| Mechlin, Belglum... . . . . . . . . . |  |
| :---: | :---: |
| Medellin, Colombla | 10,000 |
| Medina, Turkey in | 48,000 |
| Medinet-el-Fayoum, | 40,350 |
| Meerut. India. | 118,129 |
| Mehallet-el Kebir, | 31,535 |
| Mckinez, Morocco |  |
| Melbourne, Aus | 508,450 |
| Mendoza, Arge |  |
| Merlda, Mexico | 43. |
| Merthyr Tydil | 69,227 |
| Meshed, Persia. | 60,000 |
| Messina. Italy | 149,778 |
| Metz, Germany | 58,462 |
| Mexico, Mexi | 368,777 |
| Middlesborough |  |
| Mllan, Italy . | 491, |
| Minsk, Russl | 91,494 |
| Mirzapur, India | 79,862 |
| Miskolcz, Hung | 43,036 |
| Mitau, Russia. | 35,011 |
| Mito, Japa | 36,928 |
| Modena, Italy |  |
| Modica. Italy |  |
| Mobllet, Russ |  |
| Molenbeek, Belg | 61,122 |
| Molfetta, Italy. | 40,135 |
| Mombasa, Br. E. | 27,000 |
| Monastir, Turkey | 45,000 |
| Mons, Belglum. | 27,072 |
| Monterey, Mexlco |  |
| Montevideo, Urug | 276,000 |
| Montlucon, France | 35,062 |
| Montpeller, France | 75,950 |
| Montreal. Canada | 267,730 |
| Montreull, Fran | 31,773 |
| Monza, Itaiy.. |  |
| Morade bad, In |  |
| Morella. Mex |  |
| Morocco, Moroce |  |
| Morshansk, Russ | 25,913 |
| Moscow, Russia. | 092,360 |
| Mosul, Turkey | 61,000 |
| Motherwell, Scotla | 30,423 |
| Mountaln Ash, Wa | 31,093 |
| Mukden, China.. | 180,000 |
| Mülhausen, Germany |  |
| M ulheim-on-Rhlne, Germany. |  |
| Mülhelm-on-Ruhr, Germany. . | 80,609 |
| Multan. Indla. | 87,394 |
| Munlch, Germany | 199,959 |
| Münster, Germany | 63,776 |
| Murcla, Spaln. | 111,538 |
| Mustapha, Alge |  |
| Muttra, Indla |  |
| Mysore. India. | 68,111 |
| Nata, Japan | 43,133 |
| Nagano. Japan | 37,202 |
| NagasakI, Japan | 153,293 |
| Nagoya, Japan. | 288,639 |
| Nagpur, Indla | 127,734 |
| Nagy-Koros, Hungar |  |
| Nakichevan. Rus | 40,384 |
| Namangan, Russia | 61,900 |
| Namur, Belgium | 31,940 |
| Nanchang, China | 300,000 |
| Nancy, Franee. | 102,559 |
| Nankln. Chlna | 270,000 |
| Nantes, Fran | 132,990 |
| Naples, Italy | 563,540 |
| Nara. Japan. | 33,735 |
| Narbonne, France | 24,670 |
| Nawangar. India. | 53,844 |
| Negapatam, India | 57,190 |
| Nelsset, Germany | 24,307 |
| Nelson, Englan | 32,810 |
| Neully, France | 37,03 |


| Neumünster, Germany |  |
| :---: | :---: |
| Neustadt. Austria. | 28,700 |
| Nevers, France. | 27,673 |
| Newcastle, Australl | 58,620 |
| Newcastle, England | 284,511 |
| New Guatemala. Gu | 98,560 |
| Newport, Engla | 72,880 |
| Nice, France. | 105,100 |
| Nilgata, Japan | 59,570 |
| Nijmegen, Nethe | 19,342 |
| Nikolatet. Russia | 92,060 |
| Nimes. France | 80,605 |
| Ningpo, China | 260,000 |
| Nissa, Servi | 24:000 |
| Nluchwang, China |  |
| Nizhn! Novgorod, Ru |  |
| Nordhausen. Germany |  |
| Norköping, Sweden. | 44,378 |
| Northampton. Engl | 92,441 |
| Norwich. England | 110,741 |
| Nottingham, Engla | 251,671 |
| Novara, Italy. | 45,248 |
| Novgorod, Russ | 20,972 |
| Novo Cherkask |  |
| Nuka, Russla | 24,811 |
| Nuremberg, Germany | 281,081 |
| Nyrreghybaza, Hungar | 33,088 |
| Oaxaca Mexico |  |
| Oberhausen, German | 12,148 |
| Odenburg. Hungary | 33,478 |
| Odense, Denmark | 40,138 |
| Odessa, Russia. | 449,673 |
| Offenbach, German | 50,468 |
| Okayama, Japan. | 81,025 |
| Oldenburg. German | 26,850 |
| Oldham, England | 140,225 |
| Olmütz, Austria |  |
| Omdurman. Egypt | 60,000 |
| Omsk, Russia in As | 53,050 |
| Oporto, Portugal | 172,421 |
| Oppeln, Germany | 30,175 |
| Oran, Algerla | 88,235 |
| Orebro. Swed |  |
| Orel. Russla | 70,075 |
| Orizaba, Mex |  |
| Orleans, Franc | 67,311 |
| Osaka, Japan | 095,045 |
| Osh, Russia | 37,307 |
| Osnabrück. Germa | 51,573 |
| Ostend, Belgium | 41,181 |
| Otaru, Japan |  |
| Otsu, Japan |  |
| Ottawa. Ca | 59,828 |
| Oulgaret. India | 54,965 |
| Ouro Preto, Bra | 59,249 |
| Oviedo. Spain | 48,103 |
| Oxiord, Englan | 40,336 |
| achuca, Mex | 37,487 |
| adua. Italy | 82,281 |
| Paisley, Scotla | 85,804 |
| Pakhol, China. | 30,000 |
| Palembang. Sum | 53,789 |
| Palermo. Italy | 300,004 |
| Paima. Spain | 63,937 |
| Palmas, Canary Istand | 44,517 |
| Panama, Panam | 30,000 |
| Para, Brazill | 100,000 |
| Paramaribo, Du | 32,585 |
| Parana. Argentina | 25,000 |
| Paris. France | 2,714,088 |
| Parma, Italy | 40,340 |
| Partick, Scotla | 64,274 |
| Patlala, India | 53,545 |
| Patna. India | 134,785 |
| Patras, Greec | 50,158 44,208 |

## PRINCIPAL CITIES OF THE WORLD-CONTINUED




## PRINCIPAL CITIES OF THE WORLD-Continued

| Bwindon, England | 45,900 |
| :---: | :---: |
| Bydney, Australia | 508,501 |
| Syracuse, Italy.. | 32,887 |
| Byzran, Russia. | 33,046 |
| Szegedin, Hungary | 102,901 |
| Szekestejervar, Hu | 32,107 |
| Szentes, Hungary. | 31,308 |
| Tabriz, Persi | 200,000 |
| Taganrog, Russ | 58,298 |
| Talwan, Formos | 18,097 |
| Takamatsu. Japa | 37,430 |
| Takasaki, Japan | 35,228 |
| Taica, Chile | 43,331 |
| Tambof, Russla | 49,203 |
| Tammerfors | 36,344 |
| Tsmsui. Formosa. | 100,000 |
| Tananarivo, Madag | 55,579 |
| Tangier, Morocco. | 30,056 |
| Tanjore, India. | 57,870 |
| 'ranta. Egypt | 57,289 |
| Taranto, Italy | 60,733 |
| Tarbes, France | 20,845 |
| Tarnopol, Austria | 30,415 |
| Tarragona. Spain | 26,285 |
| Tashkend, Turkestan | 156,414 |
| Tegucigalpa, Hondu | 34,682 |
| Teheran, Persia | 280,000 |
| Temesvar. Hung | 53,033 |
| Teplitz, Austria | 24,560 |
| Terama, Italy. | 24,563 |
| Theodosia, Russ | 27,236 |
| Thorn, Germany | 29,470 |
| Tlentsin, China | 750,000 |
| Tifis, Russia. | 160,645 |
| Tuburg, Netherla | 45,625 |
| Tilsit. Germany | 34,539 |
| Tipton, England | 30,543 |
| Tiraspol, Russi | 29,323 |
| Tiumen, Russia in | 35,000 |
| Tlemcen, Algeria. | 35,468 |
| Tobolsk. Russia in | 21,401 |
| Tojama, Japan. | 56,275 |
| Tokat, Turkey in A | 60,000 |
| Tokyo, Japan | ,818,655 |
| Tokushima, Jap | 63,710 |
| Toledo, Spain. | 23,303 |
| Toluca. Mexico | 29,004 |
| Comsk, Russia in Asl | 65,530 |
| Toronto. Canada | 208,040 |
| Torquay, England. | 33,025 |
| Tortosa. Spain. | 25,368 |
| Totonicapam, Guatem | 28,310 |
| Tottenham, England. | 102,519 |
| Toulon, France. | 101,602 |
| Toulouse. Franc | 149,841 |
| Tour, France | 64,095 |
| Tourcolng, France | 79,243 |
| Ournay, Belgium | 30,940 |


volgoda, Russia. 27,88
Volsk, Russia ..... 27,572
Voronezh, Russla. ..... 84,148
Wakayama, Japan 68,527
Wakefleld, England ..... 41,554
Wallasey, England ..... 53,58
Walsall, England. ..... 92,908
Walthamstow, England ..... 95,125
Warrington, England ..... 68,301
Warsaw, Russia ..... 756,42t
Waterford. Ireland ..... 27,941
Weimar, Germany ..... 28,498
Weissenfels. Germany ..... 28,206
Wellington, New Zealand. .... ..... 52,500
Wenchau, China ..... 80,009
West Bromwich, England ..... 67,823
West Ham, England ..... 294.097
West Hartlepool, England. ..... 62,61
Wlesbaden, Germany ..... 86,111
Wigan, England. ..... 88,581
Willesden, England.
41,604
Wimbledon, England
90,204
90,204
Winnipeg, Manitoba.
Winnipeg, Manitoba.
25,088
25,088
Withington, England ..... 38,201
Witten, Germany ..... 33,535
Wolverhampton, England ..... 99,456
Wood Green, England ..... 34,183
Worcester, England40,705
Wuchang Ching ..... 800,000
Wuchau, China ..... 53,000
Wuhu, China ..... 122,000
Würzburg, Germany ..... 75,409
Yamagata, Japan ..... 40,240
Yarkand, China. ..... 100,000
Yarmouth, England ..... 52,353
Yarosial. Russka ..... 70,610
Yelsk, Russia in Asia ..... 35,448
Yekaterinburg, Russia ..... 55,488
Yekaterinosial. Russia ..... 135,552
Yelets, Russia
66,182
66,182
Yelizavethgrad, Russia
Yelizavethgrad, Russia ..... 45,000
Yochau, China ..... 20,000
Yokohama, Japan 326,035
York, Engiand
42,812
Yurief, Russla
23,517
zaandam, Netherlands.
35,715
35,715
Zanzibar, Zanziba ..... 50,000
Zhitomer, Russia ..... 80,787
Zlttau, Germany ..... 30, 875
Zurich. Switzeriand
62,507
Zwickau. Germany ..... 83,280

## PRINCIPAL CITIES OF THE UNITED STATES <br> Latest Official Estimates of Population

This alphabetical list of cities of the United States having 10,000 inhabitants or more gives population of cities in States of Florida, Iowa, Kansas, Massachusetts, Minnesota, New Jersey, New York, North Dakota, Rhode Island, South Dakota and Wisconsin in accordance with the State enumerations of 1905, cities of Michigan in accordance with the State enumeration of 1904 and the other cities are estimated as of 1909, under the method adopted by the United States Census Bureau and known as the "arithmetical method." This method rests on the assumption that the annual increase of each year since the last census would be one-tenth of the decennial increase between the last two censuses. The country as a whole and most of the states and cities are growing with a stcadily decreasing per cent. of increase. As this condition has obtained in the United States for the last twenty years it is likely to hold good in the immediate future. Under such conditions the "arithmetical method" has been proved moreaccurate than any alternative method available. Population of places marked thus * are estimated from reliable local sources.


## PRINCIPAL CITIES OF THE UNITED STATES

| City and State. | Pop. | City and State. | Pop. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| annibal | 13,000 | Malden, | 38,037 |  |  |  |  |
| arrisbur | 59,870 | Manches |  |  |  |  |  |
| Harrison, | 12. |  |  |  | 10,203 |  |  |
| Hartford, Con | 103. | Manistee |  |  | 22,572 | Sherman | 12,5 |
| Haverhill. M | 37,83 | Manitow |  | O |  | Shrevepo | 30 |
| azelton | 16.352 | Mankato, |  |  | 20, | Sioux | 40,9 |
| Helena, Mo | $15,000$ | Mansfield, | $21,380$ | $0 \mathrm{O}$ |  | Sioux Fa | 12, |
|  | $11,565$ | Marietta, Ohio | $17,916$ |  |  | Somervil | 69 |
|  | $65,468$ | Marinette, Wis | 15,354 |  |  |  |  |
| lyoke, | 49,934 | Marion | 25,045 |  | 12,034 | 4 S. Bethlehe |  |
| mest |  | Marion, Ohi |  |  | 37,837 | Southbridge, N |  |
| rnell | 13,259 | Marlboro, |  |  | 111,529 | South Oma | 38 |
| uston, | $80,000$ |  |  |  | 49,669 | Spartanbur | 16,0 |
| udson, N. Y | 10,290 |  |  |  | 13,098 | Spokane, | 15,0 |
| Huntington, W | 15,220 | Massillon, | 13,611 |  |  | Springfie | $46$ |
| utchinson, K | 11,214 | Meadville, | 10,830 |  | 15,9 | Springfield, |  |
| yde Park | 14,510 |  | 19,686 |  | 69,6 | Springfi |  |
| dependence, |  |  |  |  | 25,8 |  |  |
| dianapolis, |  |  |  |  |  |  |  |
| onton, Oh | 12,800 | Menomin |  |  | 567,8 | Steelton, |  |
| nw |  | Meriden, C | 20,636 |  | 13,352 | Steuben | 15 |
| hpet |  | Meridian, M |  | Pin |  | Stillwater, | 12,435 |
| Ithaca, N. Y | 14,615 | MichiganCit | 18,517 |  |  |  | $25,00$ |
|  | 25,300 | Middletown | 14.516 |  |  |  |  |
| kson, T | 18.536 |  | 12,105 |  | 500,0 | Superi |  |
| ksonvil | 35. |  | 11.884 |  | 25,0 |  |  |
| cksonvil |  | Milwaukee, | 312,948 |  |  |  | 00 |
| mesto | 26, | Minneapolis |  |  | 18,468 | Tamp | 22,8 |
|  |  | $\mathrm{Mis}$ | 20,000 |  | 10,184 | Taunto | 30,9 |
| , |  | Mobile, Al |  | Plymou | 11,1 | Terre Ilaute, |  |
|  | 232,699 | Moline | 21,971 | Plymou | 17,5 | Tiff |  |
|  | 9,845 | ) | 16,370 |  |  | Toled |  |
| nst | 48,65 |  | 37,963 |  | 20.0 |  |  |
| et, | 50,00 |  | 12,146 | Portl | 62,493 | Topeka | 37,817 |
|  |  | MIt. | 16,623 | Portl | 175,000 | Travers | 11,237 |
| 右 |  | Mt. | 25,006 | Portsm | 11,204 | r | 84,180 |
| ankakee, III |  |  |  | Portsmo |  |  | 76 |
| ansas City, I | 67.613 | Muscati | 15,087 |  |  |  | $17.005$ |
| ansas City, | 250,000 |  | 20,897 |  | 14,100 |  |  |
|  | 13,601 | Nanti | 13,981 | Pottsv | 17,150 | Vicksburg, |  |
|  | 16, | Nashau, | 28,028 | Po | 25,379 | $V$ incennes, | 11,509 |
|  |  | Nashvi | 95,000 | Pr | $214,703$ | Waco, | 26,303 |
|  |  |  | 14,108 | P |  | W | 10,268 |
|  |  |  | $13,565$ | $\mathrm{Ou}$ | $\begin{aligned} & 01,534 \\ & 40,534 \end{aligned}$ | Walla W | 15,450 |
| Knoxville | 52,000 | New Albany, In | $2 \mathrm{I}, 000$ | Ouinc |  | W | 26,282 |
| Kokomo, | 12,8:2 | New Bedford, Mas | 74,362 | Racine | 32,290 | Warwick | $73$ |
| La Crosse, | 2,078 | New Britain, Con | 34,529 | Raleigh | 14,315 | Washington |  |
| Lafayette, | 19,802 | New Brunswick, | 23,133 |  | 97,231 | Waterbury, | 62,351 |
| Lancaster, |  | New Haven, Co | 131,083 | Re | 10,715 |  | 18,071 |
| Lansing, |  | New London, |  | Re | 12,650 | Water tow | 11,258 |
|  | 15,328 | New Orl |  | Richmon | $\begin{aligned} & 12,682 \\ & 19,682 \end{aligned}$ | Waterto | 25,447 |
| La Salle, It | 10,859 | New Roc | 20,480 | Richmo | $88,345$ | $\underset{W}{W}$ | 14,600 |
| Lawrence, | 11,597 |  | 283,289 |  | 25,226 | Wausau, | $58$ |
| Lawrence, | 70,050 | Newark, | 21,745 |  | 181, 266 | Webster, |  |
| Leadville, Col. | 14,345 | Newburg, | 26,498 |  | 36,2'3 |  |  |
| Leavenwort | 20,924 | Newburyport, | 14,675 |  | 24,766 | W. | 13,611 |
|  |  | Newcastle, Pa. | 43,404 |  | 15,562 | W. Hoboken | 29,082 |
| Leor |  | Vew |  | Rutland, | $12,038$ |  | 11,585 |
| Lewiston, | 25,615 | Newp |  | Sacramento, | 50,000 | Wheeling, | 42,798 |
| Lexington, K | 30,591 | Newport, R. I | 25,039 | Saginaw, M | $\begin{aligned} & 46,610 \\ & 46,610 \end{aligned}$ | White Plai | 31,078 |
| Lima, Ohio | 26,981 | Newton, Ma | 36,827 | St. Jose | 148,569 | Wichita, | 11,579 |
| Lincol | 53,656 | New York, | 13,781 | Louis | 712,425 | Wichita Falls | 8.000 |
| Little Fall | 11,122 | Niagara Falls | 26,560 | , | 197,023 | Wilkes-Barre, | 64,324 |
| Little Roc | 49,497 | Norfolk, Va. | 56,902 | Salem | 36,627 | Wilkinsburg | 16,588 |
|  | 17,55.3 | Norristown, $\overline{\text { I }}$ | 24,582 | Salt Lake, Utah | 90,000 | Williamsport, P | 30.220 |
| Logansport, I | 18,765 | North Adams, Mas | 22,150 | San Antonio, T | 93,000 | Wilmington, D | 90,077 |
| Long Branch, | 12,183 | Northampton, Ma | 19,957 | San Diego, Calif | 45,000 | Wilmington. N. | 22,000 |
| Lorain, Ohio. | 26,076 | N. Tonawan | 10,157 | Sandusky | 20,738 | Winona, Minn. | 20,334 |
| Los Angeles, | 225,000 | North Yakima, Was | 12,000 | San Francis | 25,000 | Winston-Salem | 18,000 |
| Louisville, Ky | 24.3,973 | Norwich | 18,014 | San José, Ca | 30,000 | Woburn, Mass. | 14,402 |
| Lowell, Mass | 94.889 | Oakland, C | 190,000 | Saratoga Spgs., N. | 12,909 | Woonsocket, R. | 34,841 |
| Lynchbur | 18,891 77,042 | Ogdensbu | 13,179 | Sault Ste. Marie, Mich | 11,442 | Worcester, Mass. | 48,710 |
| Lenn, Mass. ${ }_{\text {Le }}$ |  |  |  |  |  | Yonkers, N. Y. | 61,716 |
| Macon, Ga | 50,000 | Oklahoma, Ok | 30.000 |  | 126,156 | York, Pa. | 45,332 |
| Madison, W | 24,301 |  | , |  | 250,000 | Youngstown, Ohi | 55,385 |
| noy City, Pa |  |  |  |  |  | Younstil, | 25,302 |

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## Useful Information

## Useful Numbers in Calculating Weights, Measures, Etc.

Feet multiplied by .00019 equals miles.
Yards multiplied by . 0006 equals miles.
Links multiplied by .22 equals yards.
Links multiplied by . 66 equals fect.
Feet multiplied by 1.515 equals links.
Square inches multiplied by .00695 equals square fcet.
Circular inches multiplied by .00546 equals square fect.
Square feet multiplied by . 111 equals square yards.
Acres multiplied by . 4840 equals square yards.
Square yards multiplied by .0002066 equals acres.
Width in chains multiplied by .8 equals acres per mile.
Cubic feet multiplied by . 03704 equals cubic yards.
Cubic inches multiplied by .00058 equals cubic feet.
U. S. bushels multiplied by .0461 equals cubic yards.
U. S. bushels multiplied by 1.2444 equals cubic feet.
U. S. bushels multiplied by 2150.42 equals cubic inches.
Cubic feet multiplied by .8036 equals U. S. bushels.
Cubic inches multiplied by .000465 equals U. S. bushels.
U. S. gallons multiplied by . 13367 equals cubic fect.
U. S. gallons multiplied by . 231 equals cubic inches.
Cubic feet multiplied by 7.48 equals U. S. gallons.
Cylindrical feet multiplied by .0034 equals U. S. gallons.

Pounds multiplied by 009 cquals cwt.
Pounds multiplied by . 00045 equals long tons.
Cubic foot of water multiplied by 62.5 equals libs. avoird.
Cubic inch of water multiplied by .03608 equals llos. a voird.
Cylindracal inch of water multiplied by .02842 equals lhs. avoird.
Cylindrical foot of water multiplied by 49.1 equals lbs. avoird.
Cubic inches multiplied by .004329 equals U. S. gallons.

Cylindrical feet multiplied by 5.874 equals U. S. gallons.
U. S. gallons of water multiplied by 13.44 equals one cwt.
U. S. gallons of water multiplied by 268.8 equals one ton.

Cubic feet of water multiplied by 1.8 equals one cwt.
Cubic feet of water multiplied by 35.88 equals one ton.
Cylindrical foot of water multiplied by 5.875 equals U. S. gallons.

Diameter of a circle multiplied by 3.14159265 equals circumference.
Diameter of a circle multiplied by .8862 equals side of an equal square.
Diameter of a circie multiplied by .7071 equals side of an inscribed square.
Square of a cliameter multiplied by .7854 cquals area of circle.
Circumference of a circle multiplied by .31831 equals diameter.
Side of a square multiplied by 1.128 equals diameter of equal circle.
Square foot of an area multiplied by 1.12837 equals diameter of equal circle.
Square of the diameter of a sphere multiplied by 3.1416 equals convex surface.
Cube of the diameter of a sphere multiplied by . 5236 equals solidity.
Diameter of a sphere multiplied by .806 equals dimensions of equal cube.
Diameter of a sphere multiplied by .6667 equals length of equal cylinder.
Cylindrical inches multiplied by . 0004546 equals cubic feet.
Cylindrical feet multiplied by .02909 equals cubic yards.
Cubic inches multiplied by .003607 equals imperial gallons.
Cubic feet multiplied by . 6232 equals imperial gallons.
Cylindrical inches multiplied by .002832 equals imperial gallons.
Cylindrical feet multiplied by 4.595 equals imperial gallons.
Lineal feet multiplied by . 00019 equals statute miles.
Lineal yards multiplied by .000568 equals statute miles.
Column of water 12 inches high, 1 inch in diameter, equals 341 lbs .
183.346 circular inches equals 1 square foot.

2200 cylindrical inches equals 1 cubic foot.
French metres multiplied by 3.28 equals feet.
Kilogrammes multiplied by 2.205 equals avoird. lbs.
Grammes multiplied by . 002205 equals a voird. lbs.
Square of diameter of cylinder in feet multiplied by depth in feet and by 14 equals barrels of 42 gallons.

## Table of Weights and Measures



## TIM1 MEASURE.

|  |  |
| :---: | :---: |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |

CUBIC measure.
172S cubic inches. ..................... . . . . 1 cubic foot
27 cubic feet . . . . . . . . . . . . . . . . . . . . . . . . 1 cubic yard
16 cubic feet. . . . . . . . . . . . . . . . . . . . . . . . 1 cord foot
8 cord feet. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . .
128 cubic feet. . . ( 1 cord
LAND MEASURE.
7.92 inches . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1 link

25 links. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1 rod
4 rods . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1 chain
80 chains. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1 nile
GIRCULAR MEASURE.
60 seconds.. . . . . . . . . . . . . . . . . . . . . . . . . . . . 1 minute
60 minutes... . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1 degree
30 degrees. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1 sign

- 60 degrees . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1 sextant
-90 degrees . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1 quadrant
360 degrees. . . . . . . . . . . . . . . . . . . . . . . . . . . . 1 circle
TABLE OF QUANTITIES.

| 2 units |  | dozen |
| :---: | :---: | :---: |
| 12 dozen. |  | 1 gross |
| 20 units |  | 1 score |
| 24 sheets. |  | 1 quire |
| 20 quires. |  | 1 ream |
|  | GENERAL MEASURE. |  |
| A mile |  | 5280 feet |
| A knot |  | 6080.26 feet |
| A cubit |  | 2 feet |
| A pace. |  | 3 feet |
| A palin. |  | 3 inches |
| A hand. |  | 4 inches |
| Aspan. . |  | . 9 inches |

## Metric System

MEASURES OF WEIGITT.
(Unit Gramme.)

|  | Grains. | $\underset{\text { Troy }}{\mathrm{Oz}}$ | Lobs. Avoir. | Cwt. |
| :---: | :---: | :---: | :---: | :---: |
| Centigramme . | 0.15432 |  |  |  |
| Decigramm | 1.54323 | 0.003 |  |  |
| Gramme.. | 15.43235 | 0.032 | 0.002 |  |
| Decagramme | 154.32349 | 0.321 | 0.022 |  |
| Hectogramme | 1543.23488 | 3.215 | 0.220 | 0.001 |
| Kilogramme. . | 15432.34880 | 32.150 | 2.204 | 0.019 |

## MEASURES OF LENGTH. <br> (Unit Metre.)

|  | Inches. | Feet | Yards | Miles |
| :--- | ---: | ---: | ---: | ---: |
| Millimetre.... | 0.03937 | 0.003 | 0.001 | $\ldots$ |
| Centimetre... | 0.39371 | 0.032 | 0.010 | $\ldots$ |
| Decimetre.... | 3.93708 | 0.328 | 0.109 | $\ldots$ |
| Metre....... | 39.37079 | 3.280 | 1.093 | $\ldots$ |
| Decametre.... | 393.70790 | 32.808 | 10.936 | 0.006 |
| Ifectometre... | 3937.07900 | 328.089 | 109.363 | 0.062 |
| Kilometre. . 39370.79000 | 3280.899 | 1093.633 | 0.621 |  |



## Weights of Flat Iron

Per lineal foot in pounds.
íhickness in inches.

| Width in Inch. | 1/4 | $\frac{5}{16}$ | 3/8 | 1/2 | 5/8 | $3 / 4$ | 7/8 | 1 | 11/4 | 11/2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/2 | . 422 | . 52 | . 634 |  |  |  |  |  |  |  |
| $3 / 4$ | . 6333 | .79 1.05 | .950 1.25 | 1.26 1.67 | 1.58 2.08 | 2.50 | 2.92 | 3.33 | 4.17 | 5.00 |
| 11/8 | . 930 | 1.18 | 1.40 | 1.87 | 2.34 | 2.81 | 3.38 | 3.75 | 4.75 | 5.70 |
| $11 / 4$ | 1.04 | 1.32 | 1.56 | 2.08 | 2.60 | 3.12 | 3.64 | 4.17 | 5.21 | 6.25 |
| $13 / 8$ | 1.14 | 1.45 | 1.71 | 2.29 | 2.86 | 3.40 | 4.01 | 4.58 | 5.77 | 6.97 |
| 1112 | 1.25 | 1.58 | 1.88 | 2.50 | 3.13 | 3.75 | 4.38 | 5.00 | 6.25 | 7.50 |
| $13 / 1$ | 1.46 | 1.84 | 2.19 | 2.92 | 3.65 | 4.37 | 5.10 | 5.83 | 7.29 | 8.75 |
| 2. | 1.67 | 2.11 | 2.50 | 3.33 | 4.17 | 5.00 | 5.83 | 6.67 | 8.33 | 10.00 |
| $21 / 4$ | 1.88 | 2.37 | 2.81 | 3.75 | 4.69 | 5.63 | 6.56 | 7.50 | 9.37 | 11.25 |
| $21 / 2$ | 2.08 | 2.63 | 3.12 | 4.17 | 5.21 | 6.25 | 7.29 | 8.33 | 10.42 | 12.50 |
| $23 / 4$ | 2.29 | 2.89 | 3.44 | 4.59 | 5.73 | 6.87 | 8.02 | 9.17 10.00 | 11.46 | 13.75 |
| 3 | 2.50 | 3.16 | 3.75 | 5.00 | 6.25 | 7.50 8.12 | 8.75 9.47 | 10.00 10.83 | 12.50 | 15.00 |
| 314 | $\stackrel{2.70}{2 .}$ | 3.42 3.68 | 4.06 4.38 | 5.41 5.83 | 6.77 7.29 | 8.12 8.75 | 9.47 10.21 | 10.83 11.67 | 13.65 14.58 | 16.47 17.50 |
| 31/2. | 2.92 3.11 | 3.68 3.95 | 4.38 4.58 | 5.83 6.25 | 7.29 7.80 | 8.75 9.37 | 10.21 10.93 | 11.67 | 15.58 | 17.50 |
| $4{ }^{3 / 4}$ | 3.33 | 4.21 | 5.00 | 6.67 | 8.33 | 10.00 | 11.67 | 13.33 | 16.67 | 20.00 |
| $41 / 2$ | 3.75 | 4.74 | 5.63 | 7.50 | 9.38 | 11.25 | 13.13 | 15.00 | 18.75 | 22.50 |
| 5 | 4.17 | 5.26 | 6.25 | 8.34 | 10.42 | 12.50 | 14.59 | 16.67 | 20.84 | 25.00 |
| 6 | 5.00 | 6.32 | 7.50 | 10.00 | 12.50 | 15.00 | 17.50 | 20.00 | 25.01 | 30.00 |
| 7 | 5.83 | 7.29 | 8.75 | 11.67 | 14.58 | 17.50 | 20.42 | 23.33 | 29.18 | 35.00 |
| 8 | 6.67 | 8.33 | 10.00 | 13.33 | 16.67 | 20.00 | 23.33 | 26.67 | 33.35 | 40.00 |
| 10 | 8.33 | 10.41 | 12.50 | 16.67 | 20.83 | 25.00 | 29.17 | 33.33 40.00 | 41.68 | 50.00 |
| 12 | 10.00 | 12.50 | 15.00 | 20.00 | 25.00 | 30.00 | 35.00 | 40.00 | 50.01 | 60.00 |

## Weights of Iron and Steel

U. S. STANDARD GUAGE

Adopted by the U. S. Government July 1, 1893.

| No. of Gauge. | Thickness in Inches. |  | Weight Square Foot. | No. of Gauge. | Thickness in Inches. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Fraction. | Decimals. |  |  | Fraction. | Decimals. |  |
| 0000000 | 1/2 | . 5 | 20.00 | 12 | ${ }^{7} 8$ | . 109 | 4.375 |
| 000000 | $\frac{15}{15}$ | . 468 | 18.75 | 13 | ${ }^{3}$ | . 093 | 3.75 |
| 00000 | ${ }^{7}$ | . 437 | 17.50 | 14 | $\frac{5}{68}$ | . 078 | 3.125 |
| 0000 |  | . 406 | 16.25 | 15 | ${ }^{198}$ | . 070 | 2. 8125 |
| 000 | 3/8 | . 375 | 15. | 16 | 16 | . 062 | 2.5 |
| 00 | $\frac{11}{3}$ | . 343 | 13.75 | 17 | $1{ }^{\circ} \mathrm{O}$ | .056 | 2.25 |
| 0 | $\frac{5}{16}$ | . 312 | 12.50 | 18 | 2\% | . 05 |  |
| 1 | ${ }^{18}$ | . 281 | 11.25 | 19 | $1{ }^{7}$ | . 043 | 1.75 |
| 2 | ${ }^{17}$ | . 265 | 10.625 | 20 | \% | . 037 | 1.50 |
| 3 | $1 / 1$ | . 23 | 10. | 21 | - ${ }^{\frac{1}{3} 16}$ | . 034 | 1.375 |
| 4 | ${ }_{7}^{15}$ | . 234 | 9.375 | 22 | ${ }^{12}$ | . 031 | 1.25 |
| 5 | 37 | . $2 \cdot 8$ | 8.75 | 23 | ${ }^{19} 8$ | . 028 | 1.125 |
| 6 | $\frac{13}{13}$ | . 20.3 | 8.125 | 24 | 10 | . 025 | 1. |
| 7 | ${ }^{3}$ | . 187 | 7.5 | 25 | 320 | . 021 | . 875 |
| 8 | 11 | . 171 | 6.875 | 26 | I ${ }^{\text {b/ }}$ | . 018 | . 75 |
| 9 | ${ }^{6}$ | . 156 | 6.25 | 27 | - ${ }^{1 / 1}$ | . 017 | . 6875 |
| 10 | ${ }^{8}$ | . 140 | 5625 | 28 | ${ }^{1 / 4}$ | . 015 | . 625 |
| 11 | 1/8 | . 125 | 5. | 30 | AO | .012 | . 5 |

The U.S. Standard Gauge is the one commonly used in the United States.

| BIRMINGHAM GUAGE |  |  |  |
| :---: | :---: | :---: | :---: |
| No. of Gauge. | Thickness in Inches | Weight Square Foot |  |
|  |  | Iron. | Steel. |
| 0000 | . 454 | 18.22 | 18.46 |
| 000 | . 425 | 17.05 | 17.28 |
| 00 | . 38 | 15.25 | 15.45 |
| 0 | . 34 | 13.64 | 13.82 |
| 1 | . 3 | 12.04 | 12.20 |
| 2 | . 284 | 11.40 | 11.55 |
| 3 | 259 | 10.39 | 10.53 |
| 4 | 238 | 9.55 | 9.68 |
| 5 | . 22 | 8.83 | 8.95 |
| 6 | . 203 | 8.15 | 8.25 |
| 7 | . 18 | 7.22 | 7.32 |
| 8 | . 165 | 6.62 | 6.71 |
| 9 | . 118 | 5.94 | 6.02 |
| 10 | . 134 | 5.38 | 5.45 |
| 11 | . 12 | 4.82 | 4.88 |
| 12 | . 109 | 4.37 | 4.43 |
| 13 | . 095 | 3.81 | 3.86 |
| 14 | . 083 | 3.33 | 3.37 |
| 15 | . 072 | 2.89 | 2.93 |
| 16 | . 065 | 2.61 | 2.64 |
| 17 | . 0.58 | 2.33 | 2.36 |
| 18 | . 049 | 1.97 | 1.99 |
| 19 | . 012 | 1.69 | 1.71 |
| 20 | . 035 | 1.40 | 1.42 |
| 21 | . 032 | 1.28 | 1.30 |
| 22 | .029 | 1.12 | 1.14 |
| 23 | . 02.5 | 1.00 | 1.02 |
| 24 | 022 | . 883 | . 895 |
| 2.5 | . 02 | . 803 | . 813 |
| 26 | . 018 | . 722 | . 732 |
| 27 | . 016 | . 642 | . 651 |
| 28 | . 014 | . 562 | . 569 |
| 29 | .013 |  |  |
| 30 | . 012 |  |  |
| 31 | . 01 | . . . |  |

## Weights of Round and Square Steel per Lineal Foot

（Based on 489.6 lbs．per cubic foot）．

| SIZE． <br> Inches． | VIt．of Round $1 \mathrm{ft} . \mathrm{lg}$ ． | Wt．of Square $1 \mathrm{ft} . \mathrm{lg}$ ． | SIZE． Inches． | Wt．of Round $1 \mathrm{ft} . \mathrm{lg}$ ． | Wt．of Square $1 \mathrm{ft} . \mathrm{lg}$ ． | SIZE． Inches． | Wt．of Round $1 \mathrm{ft} . \mathrm{lg}$ ． | Wt．of Square $1 \mathrm{ft} . \mathrm{lg}$ ． | SIZE． <br> Inches． | Wt．of Round $1 \mathrm{ft} . \mathrm{lg}$ | Wt．of Square $1 \mathrm{ft} . \mathrm{lg}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| O $\frac{1}{812}$ | ． 0026 | ． 0033 | 2 | 10.68 | 13.60 | 4 | 42.73 | 54.40 | 6 | 96.14 | 122.4 |
| ＂ $1 / 16$ | ． 0104 | ． 0133 | ＂1／16 | 11.36 | 14.46 | ＂ $1 / 16$ | 44.07 | 56.11 | ＂ 116 | 98.14 | 125.0 |
| ＂1／8 | ． 0417 | ． 0531 | ＂1／8 | 12.06 | 15.35 | ＂ $1 / 8$ | 45.44 | 57.85 | ＂1／8 | 100.2 | 127.6 |
| ＂3／16 | ． 0938 | ． 1195 | ＂3／16 | 12.78 | 16.27 | ＂3／16 | 4683 | 59.62 | ＂3／16 | 102.2 | 130.2 |
| ＂1／4 | ． 1669 | ． 2123 | ＂ $1 / 4$ | 13.52 | 17.22 | ＂ $1 / 4$ | 48.24 | 61.41 | ＂ $1 / 4$ | 104.3 | 132.8 |
| ＂ 516 | ． 2608 | ． 3333 | ＂ 516 | 14.28 | 18.19 | ＂ 5 偱 | 49.66 | 63.23 | ＂沰 | 106.4 | 135.5 |
| ＂ $3 / 8$ | ． 3756 | ． 4782 | ＂ $3 / 8$ | 15.07 | 19.18 | ＂ $3 / 8$ | 51.11 | 65.08 | ＂ $3 / 8$ | 108.5 | 138.2 |
| ＂ 7 ， 6 | ． 5111 | ． 6508 | ＂7／16 | 15.86 | 20.20 | ＂7／5 | 52.58 | 66.95 | ＂7／16 | 110.7 | 140.9 |
| ＂1／2 | ． 6676 | ． 8500 | ＂ $1 / 2$ | 16.69 | 21.25 | ＂1／2 | 54.97 | 68.85 | ＂ $1 / 2$ | 112.8 | 143.6 |
| ＂ $9 / 6$ | ． 8449 | 1.076 | ＂ 916 | 17.53 | 22.33 | ＂ 916 | 55.59 | 70.78 | ＂ 96 | 114.9 | 146.5 |
| ، 6118 | 1.043 | 1.328 | ＂ 68 | 18.40 | 23.43 | ＂＇518 | 57.12 | 72.73 | ＂${ }^{\text {c／8 }}$ | 117.2 | 149.2 |
| ＂ 1116 | 1.262 | 1.608 | ＂ 116 | 19.29 | 24.56 | ＂ 116 | 58.67 | 74.70 | ＂ $11 / 16$ | 119.4 | 152.1 |
| ＂3／4 | 1.502 | 1.913 | ＂ $3 / 4$ | 20.20 | 25.00 | ＂3／4 | 60.25 | 76.71 | ＂3／4 | 121.7 | 154.9 |
| ＂4，${ }^{1 / 16}$ | 1.763 | 2.245 | ＂ 1316 | 21.12 | 26.90 | ＂4 13.16 | 61.84 | 78.74 | ＂13816 | 123.9 | 157.8 |
| ＂7／8 | 2.044 | 2.603 | ＂7／8 | 22.07 | 28.10 | ＂ $7 / 8$ | 63.46 | 80.81 | ＂7／8 | 126.2 | 160.8 |
| ＂${ }^{15}$ | 2.317 | 2.989 | ＂ 15 | 23.04 | 29.34 | ＂． 516 | 65.10 | 82.89 | ＂ 1516 | 128.5 | 163.6 |
| 1 | 2.670 | 3.400 | 3 | 24.03 | 30.60 | 5 | 66.76 | 85.00 | 7 | 130.9 | 166.6 |
| ＂1／6 | 3.014 | 3.838 | ＂1／16 | 25.04 | 31.89 | ＂1／16 | 68.44 | 87.14 | ＂1／8 | 135.6 | 172.6 |
| ＂ $1 / 8$ | 3.379 | 4.303 | ＂1／8 | 26.08 | 33.20 | ＂1／8 | 70.14 | 89.30 | ＂${ }^{1 / 4}$ | 140.4 | 178.7 |
| ＂3／16 | 3.766 | 4.795 | ＂ 316 | 27.13 | 34.55 | ＂3／16 | 71.86 | 91.49 | ＇ $3 / 8$ | 145.3 | 184.9 |
| ＂1／4 | 4.173 | 5.312 | ＂1／4 | 28.20 | 35.92 | ＂1／4 | 73.60 | 93.72 | ＂ $1 / 2$ | 150.2 | 191.3 |
| ＂ 416 | 4.600 | 5.857 | ＂ 516 | 29.30 | 37.31 | ＂ 516 | 75.37 | 95.96 | ＂ $5 / 8$ | 155.2 | 197.7 |
| ＂ $3 / 8$ | 5.019 | 6.428 | ＂ $3 / 8$ | 30.42 | 38.73 | ＂ $3 / 8$ | 77.15 | 98.23 | ＂ $3 / 4$ | 160.3 | 204.2 |
| ＂7／16 | 5.518 | 7.026 | ＂7／16 | 31.56 | 40.18 | ＂7／6 | 78.95 | 100.5 | ＂7／8 | 165.6 | 210：8 |
|  | 6.008 | 7.650 | ＂1／2 | 32.71 | 41.65 | ＂1／2 | 80.77 | 102.8 | 8 | 171.0 | 217.6 |
| ＂ 9 价 | 6.520 | 8.301 | ＂916 | 33.90 | 43.14 | ＂916 | 82.62 | 10．5．2 | ＂1／8 | 176.3 | 224.5 |
| ＂5／8 | 7.051 | 8.978 | ＂ $5 / 8$ | 35.09 | 44.68 | ＂5／8 | 84.49 | 107.6 | ＂ $1 / 4$ | 181.8 | 231.4 |
| ＂11／6 | 7.604 | 9.682 | ＂1116 | 36.31 | 46.24 | ＂11／16 | 86.38 | 110.0 | ＂38 | 187.3 | 238.5 |
|  | 8.178 | 10.41 | ＂3／4 | 37.56 | 47.82 | ＇ $3 / 4$ | 88.29 | 112.4 | ＂ $1 / 2$ | 193.0 | 245.6 |
| ＂ $11 / 16$ | 8.773 | 11.17 | ＂ 19 | 38.81 | 49.42 | ＂ 1316 | 90.22 | 114.0 | ＂ $5 / 8$ | 198.7 | 252.9 |
| ＂7／8 | 9.388 | 11.95 | ＂7／8 | 40.10 | 51.05 | ＂ $7 / 8$ | 92.17 | 117.4 | ＂ $3 / 4$ | 204.4 | 260.3 |
| ＂ $19 / 16$ | 10.02 | 12.76 | ＂ 1515 | 41.40 | 52.71 | ＂ 1516 | 94.14 | 119.9 | ＂ $7 / 8$ | 210.3 | 267.9 |

These figures represent the theoretical weights of steel．Iron will run about 2 per cent lighter．

## GENERAL RULE．

For round iron，the weight per foot may be found by taking the diameter in quarter inches， squaring it，and dividing by 6 ．

## Example．

What is the weight of $2^{\prime \prime}$ round iron？

$$
2^{\prime \prime}=8 \text { quarter inches. } \quad 8^{2}=64
$$

$\frac{64}{6}=10 \frac{3}{3}$ lbs．per foot of $2^{\prime \prime}$ round．

## Example．

What is the weight of $3 / 4^{\prime \prime}$ round iron？
$34^{\prime \prime}=3$ quarter inches．$\quad 3^{2}=9$ ．
$\frac{9}{6}=11 / 2 \mathrm{lbs}$ ．per foot of $3 / 4^{\prime \prime}$ round．
The above rule is highly convenient，and cnables mental calculations of weight to be made quickly and accurately．

Circumferences and Areas of Circles.

| Diam. | Circumference. | Area. | Diam. | Circumference. | Area. | Diam. | Circumference. | Area. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{1}{82}$ | . 098 | .0007 | 9 | 28.27 | 63.61 | 47 | 147.65 | 1734.94 |
| ${ }^{1}$ | . 196 | . 0030 | 1/4 | 29.05 | 67.20 | 48 | 150.80 | 1809.56 |
| 1/8 | . 392 | . 0122 | 1/2 | 29.84 | 70.88 | 49 | 153.94 | 1885.74 |
| $\frac{8}{16}$ | . 589 | . 0276 | $3 / 4$ | 30.63 | 74.66 | 50 | 157.08 | 1963.50 |
| $1 / 4$ | . 785 | . 0490 | 10 | 31.41 | 78.53 | 51 | 160.22 | 2042.82 |
| ${ }^{6}$ | . 981 | . 0766 | $1 / 4$ | 32.20 | 82.51 | 52 | 163.36 | 2123.72 |
| 3/8 | 1.178 | . 1104 | $1 / 2$ | 32.98 | 86.59 | 53 | 166.50 | 2206.18 |
| ${ }^{7} 16$ | 1.374 | . 1503 | 3, | 33.77 | 90.76 | 54 | 169.65 | 2290.22 |
| $1 / 2$ | 1.570 | . 1963 | 11 | 31.55 | 95.03 | 55 | 172.79 | 2375.83 |
| $\frac{9}{16}$ | 1.767 | . 2485 | $1 / 4$ | 35.34 | 99.40 | 56 | 175.93 | 2463.01 |
| $5 / 8$ | 1.963 | . 3067 | 1/2 | 36.12 | 103.86 | 57 | 179.07 | 25.51 .76 |
| $1 \frac{18}{8}$ | 2.159 | . 3712 | $3 / 4$ | 36.91 | 108.43 | 58 | 182.21 | 2642.08 |
| $3 / 4$ | 2.356 | . 4417 | 12 | 37.69 | 113.09 | 59 | 185.35 | 2733.97 |
| 118 | 2.552 | . 5184 | $1 /$ | 38.48 | 117.85 | 60 | 188.50 | 2827.43 |
| 7/8 | 2.748 | . 6013 | 1/2 | 39.27 | 12271 | 61 | 191.64 | 2922.47 |
| $\frac{1}{15}$ | 2.945 | . 6902 | $3 / 4$ | 40.05 | 127.67 | 62 | 194.78 | 3019.07 |
| 1 | 3.141 | . 7854 | 13 | 40.84 | 132.73 | 63 | 197.92 | 3117.25 |
| 1/8 | 3534 | . 9940 | 1/4 | 41.62 | 137.88 | 61 | 201.06 | 3216.99 |
| $1 / 4$ | 3.927 | 1.227 | $1 / 2$ | 42.41 | 143.13 | 65 | 204.20 | 3318.31 |
| 3/8 | 4.319 | 1.484 | $3 / 4$ | 43.19 | 148.48 | 66 | 207.34 | 3421.19 |
| $1 / 2$ | 4.712 | 1. 767 | 14 | 43.98 | 153.93 | 67 | 210.49 | 3525.65 |
| $5 \%$ | 5.105 | 2.073 | 1/4 | 44.76 | 159.48 | 68 | 213.63 | 3631.68 |
| $3 / 4$ | 5.497 | 2.405 | 1/2 | 45.55 | 165.13 | 69 | 216.73 | 3739.28 |
| 7/8 | 5.890 | 2. 761 | $3 / 4$ | 46.33 | 170.87 | 70 | 219.91 | 3548.25 |
| 2 | 6.283 | 3.141 | 15 | 47.12 | 176.78 | 71 | 223.05 | 3959.19 |
| 1/8 | 6.675 | 3.546 | 16 | 50.26 | 201.06 | 72 | 226.19 | 4071.50 |
| 1 | 7.068 | 3.976 | 17 | 53.40 | 226.98 | 73 | 229.34 | 4185.39 |
| 3/8 | 7.461 | 4.130 | 18 | 56.54 | 25.5.47 | 74 | 232.48 | 4300.84 |
| $1 / 2$ | 7.854 | 4.908 | 19 | 59.69 | 283.53 | 75 | 235.62 | 4417.86 |
| 5/3, | 8.246 | 5.411 | 20 | 62.83 | 314.16 | 76 | 238.76 | 4536.46 |
| 3 | 8.639 | 5.939 | 21 | 65.97 | 346.36 | 77 | 241.90 | 4656.63 |
| 7/8 | 9.032 | 6.491 | 22 | 69.11 | 380.13 | 78 | 245.04 | 4778.36 |
| 3 | 9.424 | 7.068 | 23 | 72.25 | 415.48 | 79 | 248.19 | 4901.67 |
| 1/4 | 10.21 | 8.295 | 24 | 75.39 | 452.39 | 80 | 251.33 | 5026.55 |
| 1/2 | 10.99 | 9.621 | 25 | 78.54 | 490.87 | 81 | 254.07 | 5153.00 |
| $3 / 4$ | 11.78 | 11.044 | 26 | 81.68 | 530.93 | 82 | 257.61 | 5281.02 |
| 4 | 12.56 | 12.566 | 27 | 84.82 | 572.56 | 83 | 260.75 | 5410.61 |
| $1 / 4$ | 13.35 | 14.186 | 28 | 87.96 | 615.75 | 84 | 263.89 | 5541.77 |
| $1 / 2$ | 14.13 | 15. 904 | 29 | 91.10 | 660.52 | 85 | 267.04 | 5674.50 |
| $3 / 4$ | 14.92 | 17.720 | 30 | 94.24 | 706.86 | 86 | 270.18 | 5808.80 |
| 5 | 15.70 | 19.635 | 31 | 97.38 | 7.54 .77 | 87 | 273.32 | 5944.68 |
| $1 / 1$ | 16.49 | 21. 647 | 32 | 100.53 | 804.25 | 88 | 276.46 | 6082.12 |
| 1/2 | 17.27 | 23.758 | 33 | 10367 | 8.55 .30 | 89 | 279.60 | 6221.14 |
| $3 / 4$ | 18.06 | 25.967 | 31 | 106.81 | 907.92 | 90 | 282.74 | 6361.73 |
| $6^{6}$ | 18.94 | 28.274 | 35 | 109.96 | 962.11 | 91 | 285.88 | 6503.88 |
| 1/1 | 19.63 | 30.679 | 36 | 113.10 | 1017.88 | 92 | 289.03 | 6647.61 |
| 1/2 | 20.42 | 33.183 | 37 | 116.24 | 1075.21 | 93 | 292.17 | 6792.91 |
| $3 / 4$ | 21.20 | 35.781 | 38 | 119.38 | 1134. 11 | 9.4 | 295.31 | 6939.78 |
| 7 | 21.99 | 38.484 | 39 | 122.52 | 1194.59 | 95 | 298.45 | 7088.22 |
| 14 | 22.77 | 41.282 | 40 | 125.66 | 1256.64 | 96 | 301.59 | 7238.23 |
| $1 / 2$ | 23.56 | 44.178 | 41 | 128.81 | 1320.25 | 97 | 304.73 | 7389.81 |
| 3 | 24.31 | 47.173 | 42 | 131.95 | 1355.44 | 98 | 307.88 | 7542.96 |
| 8 | 25.13 | 50.265 | 43 | 135.09 | 1452.20 | 99 | 311.02 | 7697.69 |
| $1 / 4$ | 25.91 | 53.456 | 44 | 138.23 | 1520.53 | 100 | 314.16 | 7853.98 |
| 12 | 26.70 | 56.745 | 45 | 141.37 | 1590.43 | 101 | 317.30 | 8011.95 |
| $3 / 4$ | 27.48 | 60.132 | 46 | 144.51 | 1661.90 | 102 | 320.44 | 8171.28 |

## Workshop Recipes

BRAZING.-The edges filed or scraped clean and bright, covered with spelter and powdered borax, and exposed in a clear fire to a heat sufficient to melt the solder.

CASE HARDENING WITII PRUSSIATE OF POTASH.-Heat the articles, after polishing, to a bright red, rub the surface over with prussiate of potash, allow it to cool to a dull red, and immerse it in water.
CASE HARDENING MIXTURES.-Three parts of prussiate of potash to one part of sal ammoniac, mixed; or two parts of sal ammoniac, two parts of bone dust, and one part of prussiate of potash.

MIXTURE FOR WELDING STEEL.-One part of sal ammoniac and ten parts of horax pounded together and fused until clear, when it is poured out, and when cool redised to powder.

TEMPERING STEEL.-Stecl in its hardest state being too brittle for most purposes, the requisite strength and elasticity are o! tained by tempering-or letting down the temper, as it is termed-which is performed by heating the hardened steel to a certain degree and cooling it quickly. The requisite heat is usually ascertained by the color which the surface of the steel assumes from the film of oxide thus formed. The degrees of heat to which these several colors correspond are as follows:

At 430, a very faint yellow. At 450, a pale straw color.
Suitable for hard instruments; as hammer faces, drills, etc.
At 470, a full ycllow. At 490, a brown color.
For instruments requiring hard edges without elasticity; as shears, scissors, turning tools, etc.

At 510 , brown, with purple spots. At 538 , purple.
For tools, for cutting wood and soft metals; such as plane-irons, knives, etc.
At 550, dark blue. At 560, full blue.
For tools requiring strong edges without extreme hardness; as cold chisels, axes, cutlery, etc.

At 600 , grayish blue, verging on black.
For spring temper, which will bend before breaking; as saws, sword blades, etc.
If the steel is heated higher than this, the effect of the hardening process is destroyed.
ANNEALING STEEL.-For small pieces of steel, take a piece of gas-pipe two or three inches in diameter, and put the pieces in it, first heating one end of the pipe, and drawing it together, leaving the other end open to look into. When the pieces are of a cherry red, cover the fire with sawdust, use a charcoal fire, and leave the steel in over night.

TO RENEW WORN FILES.-Thoroughly cleanse them from grease or oil with alkali, then dip them in a solution made with one part nitric arid, three parts sulphuric acid, seven parts water by weight; time, five seconds to five minutes, according to fineness of cut. Wash in hot water, dip in lime water, dry and oil them.

- Specially Useful to Engineers in the Mining Districts.

CEMENT FOR CAST IRON.-Two ounces sal ammoniac, one ounce sulphur and sixteen ounces of borings or filings of cast iron, to be mixed well in a mortar and kept diy. When required for use, take one part of this powder to twenty parts of clear iron borings or filings, mix

## Workshop Recipes

(Continued)
theroughly in a mortar; make the mixture into a stiff paste with a little water, and then it is ready for use. A little fine grindstone sand improves the cement.
RED LEAD GEMENT FOR FACE JOINTS.-Equal parts of white and red lead mixed with linseed oil to the consistency.
CEMENT-STEAM BOILER.-Litharge in fine powder two parts, very fine sand and quicklime (that has been allowed to slack spontaneously in a damp place), of each one part; mix, and keep it from the air.

Used to mend cracks in boilers and to secure steam joints.
It is made into a paste with boiled oil before application.
CEMENT-STEAM PIPE.-Good linseed-oil varnish is ground with equal weights of white lead, oxide of manganese and pipe clay.

CEMENT-HYDRAULIG.-Made by slaking lime with water containing about two per cent. of gypsum and adding a little sand to the product.

The presence of the gypsum tends to delay the slaking of the lime, and also to harden the substance formed after the slaking.

CEMENT-CUTLERS'.-Black resin four parts, beeswax one part, finely powdered brickdust one part; mix well. Used to fix tools into their handles.

CEMENT-LEATHER.-Cutta-percha one pound, caoutchouc four ounces, pitch two ounces, shellac one ounce, linseed oil two ounces, melted together; must be melted before being applied.

Used for uniting leather or rubber.
SOLDERS.-For Lead, one of tin and one and one-half of lead.
For Tin, one of tin, and two of lead.
For Pewter, two of tin and one of lead.
For Brazing (hardest), three of copper and one of zinc.
For Brazing (hard), one of copper and one of zinc.
For Brazing (soft), one of tin, four of copper and three of zinc; or two of tin and one of antimony.
FLUXES FOR SOLDERING OR WELDING.-For Iron or Steel, borax or sal ammoniac.
For Tinned Iron, resin or chloride of zinc.
For Copper and Brass, sal ammoniac or chloride of zinc.
For Zinc, chloride of zinc.
For Lead, tallow or resin.
For Lead and Tin Pipes, resin and sweet oil.
TO HARDEN CAST IRON.-Many times it is very convenient to make an article of cast iron that needs to be finished, and which should be very hard. Cast iron can be hardened as easily as steel, and to such a degree of hardness that a file will not touch it. Take one-half pint of vitriol, one peck of common salt, one-half pound of saltpeter, two pounds of alum, one-quarter pound prussic potash, one-quarter pound cyanide of potash, all to be dissolved in ten gallons of soft water. Be sure that all the articles are dissolved. Heat the iron to a cherry red and dip it in the solution. If the article needs to be very hard, heat and dip the scond time, and even the third time.

## Workshop Recipes

(Continued)
TO INSCRIBE METAL.-Cover the part with melted beeswax; when cold, write what you desire plainly in the wax clean to the metal with scriber, then apply a mixture of $1 / 20$. nitric acid, 1 oz . muriatic acid, with a feather, carefully fill each letter; let it remain from one to ten minuses, according to appearance desired, then throw on water to stop the process of cutting, heat wax to remove it, and you have your inscription.

TO KEEP MACHINERY FROM RUSTING.-Take one ounce of camphor and dissolve it in one pound of melted lard; take off the scum, amd mix in as much fine black as will give it iron color. Clean the machinery and smear it with the mixture. After twenty-four hours rub clean with a soft linen cloth. It will keep clean for months under ordinary circumstances.

TO REMOVE RUST FROM STEEL.-Steel which has been rusted can be cleaned by brushing with a paste compound of $1 / 2$ oz. cyanide potassium, $1 / 2 \mathrm{oz}$. castile soap, 1 oz . whiting, and water sufficient to form a paste. The steel should be washed with a solution of $1 / 2 \mathrm{oz}$. cyanirle potassium in 2 oz. water.

RUST JOINT, QUICK SETTING.-Take flour of sulphur, two pounds, powdered sal ammoniac one pound, iron filings eighty pounds; mix to a paste with water.

RUST JOINT, SLOW SETTING.-Take flour of sulphur one pound, powdered sal ammoniac two pounds, iron filings or borings, two hundred pounds. This is much the better joint, if time can be given to set.

## HOW TO MIX PAINTS FOR TINTS.

Mixing Red and Black makes Brown
Mixing Lake and White makes. ..... Rose
Mixing White and Brown makes Chestnut
Mixing White, Blue and Lake makes ..... Purple
Mixing Blue and Lead Color makes ..... Pearl
Mixing White and Carmine makes ..... Pink
Mixing lndigo and Lamp-Black makes ..... Silver Gray
Mixing White and Lamp-Black makes ..... Lead Color
Mixing Black and Venctian Red makes. Chocolate
Mixing White and Green makes Bright Green
Mixing Purple and White makes. French White
Mixing Light Green and Black makes ..... Dark Green
Mixing White and Greer makes Pea Green
Mixing White and Emerald Green makes Brilliant Green
Mixing Red and Yellow makes. Orange
Mixing White and Yellow makes Straw Color
Mixing White, Blue and Black makes. ..... Pearl Gray
Mixing White, Lake and Vermilion makes ..... Flesh Color
Mixing Umber, White and Venetian Red makes ..... Drab
Mixing White, Yellow and Venetian Red makes ..... Cream
Mixing Red, Blue, Black and Red makes. ..... Olive
Mixing Yellow, White and a little Venetian Red makes ..... Buff

# Approximate Cost of Erecting Mill Buildings Exclusive of Power House 

| Free milling | 5 STAMPS WITH CONCENT |  |  |
| :---: | :---: | :---: | :---: |
| Lumber, 32 M. ft. at $\$ 25.00$. | \$800.00 | Lumber, 38 M. ft. at \$25.00 | \$950.00 |
| Labor, at $\$ 25.00$ per M. ft | 800.00 | Labor, at \$25.00 per M. ft. | 950.00 |
| Labor, setting machinery. | 156.00 | Labor, setting machinery. | 187.00 |
| Shingle roof* | 105.00 | Shingle roor* | 204.00 |
| Hardware | 45.00 | Hardware. | 60.00 |
| Windows, 12 | 53.00 | Windows, 18 | 80.00 |
|  | 1,959.00 |  | 2,431.00 |

## 10 STAMPS

| Lumber, $52 \mathrm{M} . \mathrm{ft}$. at \$25.00 | \$1,300.00 | Lumber, $60 \mathrm{M} . \mathrm{ft}$. at \$ 25.00 | \$1,500.00 |
| :---: | :---: | :---: | :---: |
| Lahor, ar \$25.00 per M. ft. | 1,300.00 | Labor, at \$25.00 per M. ft. | 1,500.00 |
| Labor, setting machinery. | 315.00 | Labor, setting machinery | 375.00 |
| Shingle roof*. | 145.00 | Shingle roof*. | 250.00 |
| Hardware. | 62.00 | Hardware. | 95.00 |
| Windows, 16. | 71.00 | Windows, 20. | 88.00 |
|  | \$3,193.00 |  | \$3,808.00 |

## 20 STAMPS

| Lumber, $63 \mathrm{M} . \mathrm{ft}$. at $\$ 25.00$ | \$1,575.00 | Lumber, $85 \mathrm{M} . \mathrm{ft}$ at $\$ 25.00$ | \$2,125.00 |
| :---: | :---: | :---: | :---: |
| Labor, at \$25.00 per M. ft. . | 1,575.00 | Labor, at \$25.00 per M. ft. | 2,125.00 |
| Labor, setting machinery. | 470.00 | Labor, setting machinery.. | 562.00 |
| Shingle roof*. | 250.00 | Shingle roof*. | 440.00 |
| Harduare . | 77.00 | Hardware. . | 25.5 .00 |
| Windows, 20. | 88.00 | Windows, 26. | 115.00 |
|  | \$4,035.00 |  | \$5,622.00 |

30 STAMPS

| Lumber, 90 M . ft . at $\$ 25.00$ | \$2,250.00 | Lumber, $106 \mathrm{M} . \mathrm{ft}$. at \$25.00. | \$2,650.00 |
| :---: | :---: | :---: | :---: |
| I abor, at \$25.00 per M. ft. . | 2,250.00 | Labor, at $\$ 25.00$ per M. ft. | 2,650.00 |
| Labor, setting machinery. | 550.00 | Labor, setting machinery. | 750.00 |
| Shingle roof*. | 330.00 | Shingle roof** | 605.00 |
| Hardware | 220.00 | Hardware. | 320.00 |
| Windows, 24. | 106.00 | Windows, 30. | 132.00 |
|  | \$5̃,706.00 |  | \$7,107.00 |

## 40 STAMPS

| Lumber, 108 M. ft. at \$ 25.00 . | \$2,700.00 | Lumber, 130 M . ft. at $\$ 25.00$. | \$3,250.00 |
| :---: | :---: | :---: | :---: |
| Labor, at $\$ 25.00$ per M. ft. . | 2,700.00 | Labor, at $\$ 25.00$ per M. it.. . | \$3,250.00 |
| labor, setting machinery. | 715.00 | Labor, setting machinery | 875.00 |
| Shingle roof*. | 430.00 | Sningle roof*. | 770.00 |
| Hardware. | 319.00 | Hardware. | 390.00 |
| Windows, 28. | 125.00 | Windows, 34. | 150.00 |
|  | \$6,989.00 |  | \$8,685.00 |

[^0]
## Amount of Material Required for Buildings

SHINGL.ES. -250 to 1 bundle. 4 bundles $=1,000$ shingles, will cover 100 sq . ft. of surface, laid $4^{\prime \prime}$ to the weather.

1 bundle of $16^{\prime \prime}$ shingles will cover 30 sq. ft ., while the same number of $18^{\prime \prime}$ shingles will cover 33 sq. ft. when laid $51 / 2^{\prime \prime}$ to the weather.

LATH. $-1,000$ laths will cover $70 \mathrm{sq} . \mathrm{yd}$. of surface.
SHAKES. $-1,000$ shakes, $6^{\prime \prime} \times 36^{\prime \prime}$, laid $16^{\prime \prime}$ to the weather, will cover 650 sq . ft. of surface; add for doubling top and bottom courses one extra shake for each ft . in the length of roof.

CORRUGATED GALVANIZED ROOFING.-Size of sheets, 26 inches by from 6 to 10 ft . flat steel, made corrugated with corrugations about $1^{\prime \prime}$ in depth and $5^{\prime \prime}$ between centers of corrugations, laying $24^{\prime \prime}$ wide, with from $3^{\prime \prime}$ to $6^{\prime \prime}$ lap, according to pitch of roof, weigh about one-third more than flat shects of same area.

For roofing, No. 24 is more generally used, while No. 26 is used for siding. Tack with wire nails on ends only and lap one corrugation on sides and from one to two inches on ends. The nail heads are sometimes soldered to assure absolute impermeability. The usual method, however, is to place lead washers under the heads.

LUMBER.-When computing the amount of material required to cover a specified area, arld to the area:


NAILS.-For 1,000 shingles allow 4 lbs of 4 d nails or $31 / 2 \mathrm{lbs}$. of 3 d nails.
For 1,000 lath allow 6 lbs. 3 d fine nails.
", $1,000 \mathrm{ft}$. of clapboarding allow 18 lbs . of 6 d box nails.
" $1,000 \mathrm{ft}$. of board siding allow 20 lbs .8 d or 25 lbs .10 d common nails.
" 10 ft . of partition studding allow 1 lb . of 10 d common nails.
" $1,000 \mathrm{ft}$. of $1^{\prime \prime} \mathrm{x} 3^{\prime \prime}$ flooring allow 45 lbs .10 d common nails.
" $1,000 \mathrm{ft}$. of $1^{\prime \prime} \times 2^{\prime \prime}$ flooring allow 65 lbs .10 d common nails.
", $1,000 \mathrm{ft}$. of pine finish allow 30 lbs . of 8 d wire nails.
BRICK.-A

| $13^{\prime \prime}$ | " | " | 20 | " | " | " | " |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $18^{\prime \prime}$ | " | " | 261/2 | " | " | " |  |
| $21^{\prime \prime}$ | " | " | 33 "" | " | " | " |  |
| $27^{\prime \prime}$ | " | " |  | " | " | " |  |

The weight of brickwork is 112 pounds per $\mathrm{cu} . \mathrm{ft}$.
Laid brick will crush at 500 lbs . per sq. in. or at $72,000 \mathrm{lbs}$. per sq. ft .
Fire brick weighs 150 lbs. per cu. ft.
Cement concrete weighs 140 lbs . per cu. ft.
A bricklayer should average 1,500 bricks in 8 hours, and 2,000 to 2,400 when starting wall before staging or ladder is used. Staging is used above 4 ft .

Brick at $\$ 10.00$ and labor at $\$ 7.50$ per 1,000 should be considered good work.
CONCRETE.

## Formula No. 1.

For retaining walls and machinery foundations.
$60 \mathrm{cu} . \mathrm{ft}$. of rock that will pass a 3 -inch mesh screen.
$20 \mathrm{cu} . \mathrm{ft}$. of clean, sharp, coarse sand.
$10 \mathrm{cu} . \mathrm{ft}$. of Portland cement.
Formula No. 2.
For concrete mortar blocks for stamp batteries.
$52 \mathrm{cu} . \mathrm{ft}$. of rock.
$32 \mathrm{cu} . \mathrm{ft}$. of sand.
$16 \mathrm{cu} . \mathrm{ft}$. of cement.
If broken rock is not available, clean creck gravel of the same size may be substituted, but in no case use clay, loam or very fine sand.

Mix all together dry. When required for use, mix small quantities with sufficient water to make a thick mortar, use immediately and tamp with a tamping bar.

Concrete will set sufficiently in 24 hours to sustain a load, and in from three to four days in medium dry weather machinery may be run on the foundations.

## Water and Pumping

A United States gallon of fresh water weighs 8.33 pounds and contains 231 cubic inches.
A cubic foot of water weighs 62.4 pounds and contains 1728 cubic inches, or 7.5 gallons.
A British Imperial gallon contains 277.27 cubic inches, which is equivalent to 1.20 United States gallons, or 10 pounds in weight.

The normal pressure of the atmosphere is 14.7 pounds per square inch; it is equal to a column of water 34 feet high, though 20 feet is the greatest suction lift it is advisable to use.

To find the pressure in pounds per square inch of a column of water, multiply the height of the column in feet by .434. To find the head in feet, multiply the pressure in pounds by 2.31 .

The term "head" in connection with pumps is understood to be the sum of the actual elevation and the friction head. The elevation, or lift, is the vertical distance from the surface of the suction water to the center of the discharge outlet.

Friction is that due to the passage of water through the suction and discharge pipes.
In practice, the size of the suction and discharge pipes is usually larger than the openings in the pump. This is especially desirable when the pipe is of any length. The friction head may be greater than the actual elevation, and the cost of the increased pipe size will be saved in a short time by the difference in horse-power. The friction increases with the velocity, and users are reminded that rather than to run the pump considerably above its capacity, it is better to install a larger pump and pipe line.

Doubling the diameter of a pipe increases its capacity four times. Friction of liquids in pipes increases as the square of the velocity.

To find the diameter of a pump cylinder to move a given quantity of water per minute ( 100 feet of piston being the standard of speed), divide the number of gallons by 4 , then extract the square root, and the product will be the diameter in inches of the pump cylinder.

To find quantity of water elevated in one minute, running at 100 feet of piston speed per minute. Square the diameter of the water cylinder in inches and multiply by 4.

Example-Capacity of a 5 inch cylinder is desired. The square of the diameter (5 inches) is 25 , which, multiplied by 4 , gives 100 , the number of gallons per minute (approximately).

To find the horsepower necessary to elevate water to a given height, multiply the weight of the water elevated per minute in pounds by the height in feet, and divide the product by 33,000 , (an allowance should be added for water friction, and a further allowance for loss in steam cylinder, say from 20 to 30 per cent).

The area of the steam piston, multiplied by the steam pressure, gives the total amount of pressure that can be exerted. The area of the water piston, multiplied by the pressure of water per square inch, gives the resistance. A margin must be made between the power and the resistance to move the pistons at the required speed, say from 20 to 40 per cent., according to specd and other conditions.

Quantity of water in gallons per minute and velocity of flow in feet per second being given to find area of pipe in square inches, multiply quantity by 231 and divide by velocity multiplied by 720. Area of pipe and velocity being given, to find quantity delivered, multiply area of pipe by velocity and by 720 , and divide product by 231 .

A "miners inch" of water in California is regulated by law and is equal to a flow of one and one-half cubic feet of water per minute through any opening and under any pressure.

# Standard Dimensions of Wrought-Iron Pipe for Water, Gas or Steam 

| $\begin{aligned} & \text { Nominal } \\ & \text { Size. } \end{aligned}$ | $\begin{gathered} \text { Actual } \\ \text { Inside } \\ \text { Diameter. } \end{gathered}$ | $\begin{gathered} \text { Actual } \\ \text { Outside } \\ \text { Diameter. } \end{gathered}$ | Diameter at Bottom of Thread at End of Pipe | Diameter at Top of Thread at End of Pipe | Number of Threads per Inch. | $\begin{aligned} & \text { Length } \\ & \text { of Perfect } \\ & \text { Screw. } \end{aligned}$ | Weight ner Foot of Length. | Contents in <br> U.S. Gallons per Foot. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inch. | Inch. | Inch. | Inch. | Inch. |  | Inch. | Lus. |  |
| 1/8 | . 270 | . 405 | . 334 | . 393 | 27 | . 19 | . 241 | . 0006 |
| 1/4 | . 364 | . 540 | . 433 | . 522 | 18 | . 29 | . 420 | . 0026 |
| $3 / 8$ | . 494 | . 675 | . 567 | . 656 | 18 | . 30 | . 559 | . 0057 |
| 1/2 | . 623 | . 840 | . 701 | 815 | 14 | . 39 | . 837 | . 0102 |
| 34 | . 824 | 1.050 | . 911 | 1.025 | 14 | . 40 | 1.115 | . 0230 |
| 1 | 1.0.18 | 1.315 | 1.144 | 1.283 | 111/2 | . 51 | 1.668 | . 0408 |
| 1114 | 1.380 | 1.660 | 1.488 | 1.627 | $111 / 2$ | . 54 | 2.244 | . 0638 |
| 11/2 | 1.610 | 1.900 | 1.727 | 1.866 | $111 / 2$ | . 55 | 2.678 | . 0918 |
| 2 | 2.067 | 2.375 | 2.200 | 2.339 | $111 / 2$ | . 58 | 3.609 | . 1632 |
| 21/2 | 2.468 | 2.875 | 2.620 | 2.820 | 8 | . 89 | 5.739 | . 2550 |
| 3 | 3.067 | 3.500 | 3.241 | 3.441 | 8 | . 95 | 7.536 | . 3673 |
| $31 / 2$ | 3.548 | 4.000 | 3.738 | 3.938 | 8 | 1.00 | 9.001 | . 4998 |
| 4 | 4.026 | 4.500 | 4.235 | 4.435 | 8 | 1.05 | 10.665 | . 6528 |
| 41/2 | 4.508 | 5.000 | 4.732 | 4.932 | 8 | 1.10 | 12.490 | . 8263 |
| 5 | 5.045 | 5.563 | 5.291 | 5.491 | 8 | 1.16 | 14.502 | 1.020 |
| 6 | 6.065 | 6.625 | 6.346 | 6.546 | 8 | 1.26 | 18.762 | 1.469 |
| 7 | 7.023 | 7.625 | 7.340 | 7.540 | 8 | 1.36 | 23.271 | 1.999 |
| 8 | 7.982 | 8.625 | 8.334 | 8.534 | 8 | 1.46 | 28.177 | 2.611 |
| 9 | 9.000 | 9.625 | 9.327 | 9.527 | 8 | 1.57 | 33.701 | 3.300 |
| 10 | 10.019 | 10.750 | 10.445 | 10.645 | 8 | 1.68 | 40.065 | 4.081 |
| 12 | 12.000 | 12.750 | 12.431 | 12.631 | 8 | 1.87 | 48.985 | 5.875 |

$11 / 4$ inch and below are butt-welded and tested to 300 lbs . per sq. in. $11 / 2$ inch and above are lap-welded and tested to 500 lbs . per sq.in.

Light Wrought-Iron Artesian, Salt, Oil and Gas Well Casing

| Nominal Inside Diameter Inches. | Actual Outside Diameter. Inches. | $\begin{aligned} & \text { Nominal } \\ & \text { Weight per } \\ & \text { Foot. } \\ & \text { Pounds. } \end{aligned}$ | No. Threads per Inch of Screw. | $\begin{aligned} & \text { Nominal } \\ & \text { Inside } \\ & \text { Diameter. } \\ & \text { Inches. } \end{aligned}$ | $\begin{aligned} & \text { Actual } \\ & \text { Outside } \\ & \text { Diameter. } \\ & \text { Inches. } \end{aligned}$ | $\begin{gathered} \text { Nominal } \\ \text { Welght per } \\ \text { Foot. } \\ \text { Pounds. } \end{gathered}$ | No. Threads per Inch of Screw. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 21/4 | 2.22 | 14 | 55/8 | 6 | 10.46 | 14 |
| $21 / 4$ | $21 / 2$ | 2.82 | 14 | 55/8 | 6 | 12.04 | 111/2 |
| $21 / 2$ | $23 / 4$ | 3.13 | 14 | 55/8 | 6 | 14.20 | 111/2 |
| $23 / 4$ | 3 | 3.45 | 14 | $55 / 3$ | 6 | 16.70 | 111/2 |
| 3 | 31/1 | 4.10 | 14 | $61 / 4$ | 65/8 | 11.58 | 14 |
| 31/4 | $31 / 2$ | 4.45 | 14 | $61 / 4$ | 65/8 | 13.32 | 14 and 111/2 |
| $31 / 2$ | $33 / 4$ | 4.78 | 14 | $61 / 4$ | $65 / 8$ | 17.02 | 111/2 |
| $33 / 4$ | 4 | 5.56 | 14 | $65 / 8$ | 7 | 12.34 | 14 |
| 4 | 41/4 | 6.00 | 14 | 65/8 | 7 | 17.51 | $111 / 2$ and 10 |
| $41 / 4$ | $41 / 2$ | 6.36 | 14 | $71 / 4$ | 75/8 | 13.55 | 14 |
| 411/4 | $41 / 2$ | 9.38 | 14 | $75 / 8$ | 8 | 15.41 | 111/2 |
| $41 / 2$ | $43 / 4$ | 6.73 | 14 | $75 / 8$ | 8 | 20.17 | 111/2 |
| $41 / 2$ | $43 / 4$ | 9.39 | 14 | $81 / 4$ | 85/3 | 16.07 | 111/2 |
| $43 / 4$ | 5 | 7.80 | 14 | $81 / 4$ | 85/8 | 20.10 | 111\% |
| 5 | 51/4 | 8.20 | 14 | $81 / 4$ | $85 / 8$ | 24.38 | $111 / 2$ and 8 |
| 5 | $51 / 4$ | 9.86 | 14 | $85 / 3$ | 9 | 17.60 | $111 / 2$ |
| 5 | $51 / 4$ | 12.80 | $111 / 2$ | 95/8 | 10 | 21.90 | 111/2 |
| 5 | $51 / 4$ | 15.88 | 111/2 | 105\% | 11 | 26.72 | 111\% |
| $53 / 6$ | $51 / 2$ | 8.62 | 14 | 115/8 | 12 | 30.35 | 111/3 |
| 53/6 | $51 / 2$ | 12.49 | $111 / 2$ | 121/2 | 13 | 33.78 | 111/2 |

## Horse Power or Capacity of Boilers

Steam Boilers are nearly always rated and sold on the basis of a certain number of square feet of heating surface. The basis of the rating heating surface varies, however, so much by different builders, that it is a very unsatisfactory method of rating. For instance Boilers are rated:

Return Tabular at from 12 to 15 square feet for each horse power.
Portable Locomotive and Vertical Boilers on from 9 to 11 square feet.
Water Tube and Scotch Marine Boilers on from $7 \frac{1}{2}$ to 10 square feet.
The Centennial Rating of boiler capacity is the most practical and satisfactory. It provides for the evaporation or turning into steam of 30 pounds of water for each horse power per hour. This is a moderate rating, and any boiler that is not capable of evaporating that amount of water for each horse-power of its rated capacity and without forcing the firing or draft, must be in bad condition or over-rated. The safest method for all purchasers, will be to first ascertain the number of horse-power of work required from the engines for which the boiler is to be provided and then calculate the amount of steam the engine or engines will consume in developing that amount of power. By dividing by 30 they will arrive at the horse-power of boiler required to supply the engines.

## Amount of Steam Required by Various Engines

The following allowance of pounds of water or steam for each indicated horse-power for engines of different kinds, will be found a safe calculation:
Triple Expansion (Condensing) Engines. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 15 pounds
Triple Expansion (Non-Condensing) Engines. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 20
Compound Condensing Corliss Engines . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 18
Compounđ̃ Non-Condensing Corliss Engines . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 22
Simple or Single Corliss Engine (Condensing) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 23
Simple or Single Corliss Engine (Non-Condensing) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 25
Automatic Compound Condensing Engines. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 23
Automatic Compound Engine (Non-Condensing) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 30
High-Speed Automatic Engines. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 33
Side Valve Engines with Adjustable Cut-off. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 35
Plain Slide Valve Engines . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 40
Steam Pumps (Compound Condensing) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 40
Steam Pumps (Compound Non-Condensirg)......................................... . . . . . . 0
Steam Pumps, Single or Duplex. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 75

## Water Consumption of Boilers

From the foregoing, it is evident that to arrive at the amount of water required by a boiler, it is only a matter of multiplying its horse-power by 30 pounds of water per hour. In some cases, an allowance of as much as 60 pounds or $71 / 2$ gallons of water per horse-power of boilers is allowed, but this is excessive, and a boiler should not be expected to evaporate more than 30 to 40 pounds of water per horse-power per hour, except under stress.

## Fuel Consumption of Boilers

Provided that feed water is delivered to a boiler as hot as it can be made with exhaust steam, that is at $200^{\circ} \mathrm{F}$., a good boiler with ample draft and grate surface and carefully fired should be capable of evaporating from 8 to 10 pounds of water for each pound of good coal.

In practice, however, the question of water evaporated for each pound of coal varies between 6 and 8 pounds of water and in many larger plants where mine slack is used, the evaporation of water, is between 6 and 7 pounds.

The average consumption of coal for steam boilers is 12 lls . per hour for each square foot of grate surface.

To evaporate one cubic foot of water requires the consumption of $71 / 2 \mathrm{lbs}$. of ordinary coal, or about 1 lb . of coal to 1 gallon of water.

One pound of crude petroleum will evaporate 12 to 16 lbs . of water.
One pound of natural gas ( 25 cubic feet) will evaporate about 20 lbs of water. One ton of coal is equal to about 22,450 cubic feet natural gas. (Atmospheric pressure).

One ton of coal is' equal to $31 / 2$ to 4 barrels of petroleum.
One ton of coal is equal to one cord of hickory.
One ton of coal is equal to $1 \frac{1}{4}$ cords of white oak.
One ton of coal is equal to $11 / 3$ cords of. black oak.
One ton of coal is equal to 2 cords of pine.
One cubic foot of anthracite coal weighs about 53 pounds.
One cubic foot of bituminous coal weighs from 47 to 50 pounds.

## Safety Valve Rules

To find the distance, ball should be placed on lever when the weight is known, or to find weight when distance is known:

Multiply the pressure required by area of valve, then multiply this answer by the fulcrum, subtract the weight of the lever, valve and stem, and divide by the weight of the ball for distance; or divide by distance for the weight of the ball with the same example.

To find the pressure when the area of the valve; the weight of lever valve and stem, the fulcrum and the weight of ball is known:

Divide fulcrum into length of lever, multiply the answer by weight of ball, add weight of lever, valve and stem, and divide by area of valve; the answer will be the steam pressure.

The mean effective weight of valve lever and stem is found by connecting the lever at fulcrum, tie the valve stem to leve:, attach a spring scale to lever immediately over the valve, and raise until the value is clear of its seat.

By the fulcrum is meant the distance the valve stem is, from where the lever is connected.
Safety valves should be allowed to blow straight out into the room and not hitched on to a leading pipe which may allow water to stand on the valve, increasing its weight, or to freeze up if the boiler is laid up. When the valve blows into the room it will be known when steam is escaping, whether from leakage or over pressure.

Don't depend too much upon the glass gauge, but try the cocks often enough to keep your hand in, in telling the height of water by them. If a gauge cock has a tendency to leak, fix it thoroughly; if you do not, you will neglect to use it for fear of the work which you may have, to stop the leak after using.

To determine the heating surface in the Tubes of any Boiler multiply the number of feet of Tubes by . 523 for 2 inch; by . 654 for $2 \frac{1}{2}$ inch; by .785 for 3 inch; $b^{\cdot י} .916$ for $31 / 2$ inch, and by 1.047 for 4 inch.

## Horse Power

A Standard Engine Horse Power is 33,000 foot-pounds per minute-that is 33,000 pounds raised one foot in one minute, or 3,300 pounds raised ten feet, or 330 pounds raised one hundred feet, and so on.

To calculate the horse power of an engine, multiply together the area of the steam piston in square inches, the piston speed in feet per minute and the mean effective pressure of the steam in pounds per square inch and divide the result by 33,000 . This will give the horse power in the cylinder, or Indicated Horse Power. From this must be taken the horse power consumed by the engine in friction, etc., to obtain the Net or Actıal Horse Power.

## Table of Mean Effective Pressure

The M. E. P. in the table are for non-coudensing Engines. One pound is allowed for back pressure of Exhaust. Ten pounds added to any of the M. E. P. given will give the M. E. P. for Condensing Engines.

| Jnitial Pressure in | Points of Cut-Off. |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Square <br> Inch. | 1/4 | $\frac{2}{7}$ |  | 1/3 | 3/8 | $\frac{2}{6}$ | ${ }_{7}^{3}$ | ${ }_{9}^{4}$ | 1/2 | ${ }_{9}^{5}$ | ${ }_{5}^{8}$ | 5/8 | 2/3 | $3 / 4$ |
| 30 | 10.75 | 12.7 | 13.75 | 15.50 | 1. | 18.50 | 19.50 | 0.00 | 22.00 | 23.50 | 24.75 | 25.25 | 26.00 | 27.25 |
| 35 | 13.75 | 16.00 | 17.00 | 19.00 | 21.00 | 22.25 | 23.50 | 24.25 | 26.25 | 28.00 | 29.25 | 29.50 | 30.75 | 32.35 |
| 40 | 16.75 | 19.25 | 20.25 | 22.50 | 24.75 | 26.00 | 27.00 | 28.25 | 30.50 | 32.50 | 33.75 | 34.50 | 35.50 | 37.00 |
| 45 | 19.75 | 22.50 | 23.75 | 26.00 | 28.50 | 30.00 | 31.50 | 32.25 | 34.75 | 36.75 | 38.25 | 39.25 | 40.25 | 41.75 |
| 50 | 22.75 | 25.75 | 27.00 | 29.50 | 32.25 | 33.75 | 35.50 | 36.25 | 39.00 | 40.50 | 42.75 | 43.75 | 45.00 | 46.50 |
| 55 | 25.75 | 29.00 | 39.25 | 3300 | 36.00 | 37.50 | 39.25 | 40.25 | 43.25 | 45.75 | 47.25 | 48.25 | 49.50 | 51.50 |
| 60 | $2 \times .75$ | 32.25 | 33.75 | 36.50 | 39.75 | 41.50 | 43.25 | 44.25 | 47.50 | 50.00 | 51.75 | 52.75 | 54.25 | 56.25 |
| 65 | 31.75 | 35.50 | 37.00 | 40.00 | 43.50 | 45.25 | 47.25 | 48.25 | 51.75 | 54.50 | 56.50 | 57.50 | 59.90 | 61.25 |
| 70 | 34.75 | 38.50 | 40.00 | 43.50 | 47.00 | 49.00 | . 51.25 | 52.25 | 56.00 | 58.75 | 61.00 | 62.00 | 63.50 | 66.00 |
| 75 | 37.75 | 11.75 | 43.00 | 47.00 | 50.75 | 53.00 | 55.25 | 56.25 | 60.25 | 63.25 | 65.50 | 66.50 | 68.50 | 71.00 |
| 80 | 40.75 | 45.00 | 46.75 | 50.50 | 54.50 | 56.75 | 59.25 | 60.25 | 64.50 | 67.75 | 70.00 | 71.25 | 73.00 | 75.75 |
| 85 | 43.75 | 48.25 | 50.25 | 54.00 | 58.25 | 60.50 | 63.00 | 64.50 | 68.75 | 72.00 | 74.50 | 75.75 | 77.75 | 80.50 |
| 90 | 46.75 | 51.50 | 53.25 | 57.00 | 62.00 | 64.25 | 67.00 | 68.50 | 73.00 | 76.50 | 79.25 | 80.50 | 82.25 | 85.25 |
| 95 | 49.75 | 54.75 | 57.00 | 61.50 | 65.75 | 68.25 | 71.00 | '72.50 | 77.25 | 81.00 | 83.50 | 85.00 | 87.00 | 90.25 |
| 100 | 52.50 | 58.00 | 60.25 | 64.50 | 69.50 | 72.00 | 75.00 | 76.50 | 81.25 | 85.25 | 88.25 | 89.50 | 91.75 | 95.00 |
| 105 | 55.50 | 61.25 | 63.50 | 68.00 | 73.00 | 75.75 | 78.75 | 80.50 | 85.50 | 89.75 | 92.75 | 94.25 | 96.50 | 99.75 |
| 110 | 58.50 | 64.50 | 66.75 | 71.50 | 76.75 | 79.75 | 82.75 | 84.50 | 89.75 | 94.25 | 97.25 | 98.75 | 101.00 | 104.75 |
| 115 | 61.50 | 67.50 | 70.00 | 75.00 | S0.50 | 83.50 | 86.25 | 88.50 | 94.00 | 98.50 | 101.75 | 103.50 | 105.75 | 109.50 |
| 120 | 64.50 | 70.75 | 73.25 | 78.50 | 84.25 | 87.50 | 90.25 | 92.50 | 98.25 | 102.75 | 106.25 | 108.00 | 110.00 | 114.25 |
| 125 | 67.50 | 73.75 | 76.50 | 81.00 | 88.00 | 91.25 | 91.25 | .96.50 | 02.25 | 107.00 | 110.75 | 112.50 | 114.50 | 119.25 |

## How to Center an Engine

The "dead center" is the point in the stroke where the crank and piston rod are in the same right line. To find dead center, turn engine in the direction it runs until cross-head is within a short distance of its limit of motion. Mark guide at end of cross-head shoe. Mark some revolving circular part of engine, as disk crank or fly wheel, and place one point of a fixed tram in this mark and the other on some fixed object in line. Now turn engine past the center in the direction she runs until end of cross-head shoe passes mark on guide. Turn back till shoe reaches mark. Holding tram still on the fixed object, place other point on selected revolving part and mark as before. Bisect distance between marks on revolving part and turn engine till point of tram rests on central mark, and the engine is on "dead center."

Horizontal engines, when practicable, should be run over rather than under, as the thrust will then come downward upon the foundation rather than upon the caps of the boxes and the upper guides.

# Power Required for Different Parts of Gold and Silver Mills 

Each Stamp, Dropping 100 Times per Minute, Requires:

| Weight per stamp in $\mathrm{lbs} \ldots . . .$. | 750 | 800 | 850 | 900 | 950 | 1000 | 1050 | 1100 | 1200 | 1300 | 1350 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Horse Power each Stamp . . .... | 1.5 | 1.6 | 1.8 | 1.9 | 2.0 | 2.1 | 2.2 | 2.3 | 2.4 | 2.6 | 2.7 |

Each Dodge Crusher, Requires:
Each Blake Type Crusher, Requires:

| Size of crusher . . ...... | $6 \times 6$ | $7 \times 8$ | $8 \times 12$ | $11 \times 15$ | Size of crusher . . ... | $6 \times 71 / 2$ | $7 \times 9$ | $8 \times 12$ | $10 \times 16$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Horse power. ......... | 4 | 6 | 8 | 12 | Horse power...... | 4 | 5 | 8 | 12 |
| Revolutions per minute. | 350 | 300 | 250 | 225 | Rev. per minute.... | 275 | 275 | 250 | 225 |

Each Standard Crushing Rolls, Requires:

| Size of rolls. . . . . . . . . . . . . . . . . . . . . | $20 \times 8$ | $20 \times 12$ | $27 \times 14$ | $30 \times 14$ | $36 \times 16$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Horse power. . . . . . . . . . . . . . . . . . . . | $3-6$ | $4-8$ | $5-10$ | $8-15$ | $10-20$ |
| Revolutions per minute. . . . . . . . . . . . . . | $100-150$ | $100-150$ | $75-125$ | $65-85$ | $50-75$ |

Each 6-foot Belt Concentrator, requires about $1 / 2$ horse-power.
Each 18 -inch Amalgam Barrel, requires from 1 to 2 horse-power.
Each 24 -inch Amalgam Barrel, requires from 2 to 3 horse-power.
Each 36 -inch Clean-up Pan, requires from 1 to $1 \frac{1}{2}$ horse-power.
Each 48 -inch Clean-up Pan requires from $11 / 2$ to 2 horse-power.
Each 4-foot Combination Pan, 65 revolutions per-minute, requires from 3 to 6 horse-power.
Each 5 -foot Combination Pan, 65 revolutions per minute, requires from 5 to 10 horse-power.
Each 8 -foot Settler, 14 revolutions per minute, requires 2.5 horse-power.
Each 8 -foot Agitator, 16 revolutions per minute, requires 3 horse-power.
Each Quicksilver Elevator requires from .25 to 2 horse-power.
Each Revolving Dryer requires 5 horse-power.
Each Howell-White Roasting Furnace requires from 4 to 6 horse-power.
Each Bruckner Furnace, $8 \times 18$ feet, requires from 5 to 8 horse-power.
Above estimates include the friction of the parts named, but not that of the power transmitting machinery, for which an additional allowance should be made.

## Water Required for Various Parts of Gold and Silver Mills

Boiler feed for each horse-power, per hour, 5 gallons.
For each stamp, per hour, from 60 to 80 gallons.
For each 5-foot Pan, per hour, 100 gallons.
For each 8 -foot Settler, per hour, 80 gallons.
For each Corcentrator, per hour, from 200 to 300 gallons.
For each Graupner or Huntington 5 -foot mill, per hour, 1000 to 1200 gallons.
When water is settled and returned to the mill for re-use, a reduction of 50 per cent. may be safely estimated for all except the boiler, which must have clear water.

## Horse-Power Shafting Will Transmit

| $\begin{gathered} \text { Diameter } \\ \text { of } \\ \text { Shaft. } \end{gathered}$ | Weight per Foot. | Revolutions per Minute. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 125 | 150 | 175 | 200 | 225 | 2.50 | 300 | 350 | 400 |
|  | 2.05 | 1.2 | 1.4 | 1.7 | 2.1 | 2.4 | 2.6 | 3.1 | 3.6 | 4.3 | 5.0 |
| $1_{18}^{18}$ | 3.77 | 2.4 | 3.1 | 3.7 | 4.3 | 4.9 | 5.5 | 6.1 | 7.3 | 8.5 | 9.7 |
| 17. | 5.52 | 4.3 | 5.3 | 6.4 | 7.4 | S. 5 | 9.5 | 10.5 | 12.7 | 14.8 | 16.9 |
| 11. | 7.61 | 6.7 | 8.1 | 10.1 | 11.7 | 13.4 | 15.1 | 16.7 | 20.1 | 23.4 | 26.8 |
| $1 \frac{1}{1} \frac{1}{6}$ | 10.03 | 10.0 | 12.5 | 15.0 | 17.5 | 20.0 | 22.5 | 25.0 | 30.0 | 35.0 | 40.0 |
| $2{ }_{16}^{3}$ | 12.80 | 14.3 | 17.8 | 21.4 | 24.9 | 28.5 | 32.1 | 35.6 | 42.7 | 49.8 | 57.0 |
| $2_{17}{ }^{16}$ | 15.89 | 19.5 | 24.4 | 29.3 | 34.1 | 39.0 | 44.1 | 48.7 | 58.5 | 68.2 | 78.0 |
| $2 \frac{11}{16}$ | 19.31 | ${ }^{26.0}$ | 32.5 | 39.0 | 43.5 | 52.0 | 58.5 | 65.0 | 78.0 | 87.0 | 104.0 |
| 215 | 23.06 | 33.8 | 42.2 | 50.6 | 59.1 | 67.5 | 75.9 | 84.4 | 101.3 | 118.2 | 135.0 |
| $3{ }^{186}$ | 27.16 | 43.0 | 53.6 | 64.4 | 75.1 | 85.8 | 96.6 | 107.3 | 128.7 | 150.3 | 171.6 |
|  | 31.58 | 53.6 | 67.0 | 79.4 | 93.8 | 107.2 | 120.1 | 134.0 | 155.8 | 187.6 | 214.4 |
| 311 | 36.40 | 65.9 | 82.4 | 97.9 | 115.4 | 121.8 | 148.3 | 164.8 | 195.7 | 230.7 | 243.6 |
| $31{ }_{16}{ }^{5}$ | 41.40 | 80.0 | 100.0 | 120.0 | 140.0 | 160.0 | 180.0 | 2000 | 240.0 | 280.0 | 320.0 |
| $4{ }^{7}$ | 52.58 | 113.9 | 142.4 | 170.8 | 199.3 | 227.8 | 256.2 | ${ }_{2} 284.7$ | 341.7 | 399.6 | 455.6 |
| $4 \frac{15}{15}$ | 65.10 | 156.3 | 195.3 | 234.4 | 273.4 | 312.5 | 351.5 | 390.6 | 468.7 | 516.8 | 605.0 |

## To Obtain the Size and Speed of Pulleys, Gears, or Sprocket Wheels

Diameter of Dtiver-Diameter of driven multiplied by revolutions of driven, and the product obtained divided by the revolutions of driver.

Diameter of Driven-Diameter of driver multiplied by revolutions of driver, and the product obtained divided by revolutions of driven.

Revolutions of Driven.-Diameter of driver multiplied by revolutions of driver, and the product obtained divided by the revolutions of driven.

Revolutions of Driver.-Diameter of driven multiplied by the revolutions of driven, and the pooduct obtained divided by the diameter of the driver.

The driving pulley is called the driver, and the driven pulley the driven.
It the number of teeth in gears or sprocket wheels are insed instead of diameter in thesecalculations, number of teeth must be substituted whenever diameter occurs.

## Horse-Power of Gearing

The following table is for cast-iron gears, and is based unon a factor of safety of eight, with an ultimate tensile strength of 30,000 pounds.

Speed of gear, 100 feet per minute at pitcón line.

| Spur Gears, Horse Power. | Pitch. | loace. | Bevel Cears, Horse Power. |
| :---: | :---: | :---: | :---: |
| $1.41)$ | 1 | 21/2 | 1.01 |
| 2.52 | 11/4 | $31 / 4$ | 1.78 |
| 3.84 | 11\% | 4 | 2.61 |
| 5. 48 | 13 | 5 | 3.73 |
| 6.83 | 2 | 6 | 4.68 |
| 8.99 | 214 | $6{ }^{1 / 2}$ | 6.39 |
| 10.70 | 21/2 | 7 | 7.52 |
| 15.39 | 3 | 9 | 10.54 |

The horse-power of gears increases and recreases directly with the speed.

## Belting

SINGLE LEATHER

| Speed in Feet per Minute. | Wimth of Belt in Inches. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 | 3 | 4 | 5 | 6 | 8 | 10 | 12 | 14 | 16 |
|  | H.-P. | H.-P. | H.-P. | H.-P. | H.- - | H.-P. | $\mathrm{H}_{\boldsymbol{\sigma}}-\mathrm{P}$. | 11.-1. | H.-P. | 18.-P. |
| 400 |  | 11/2 | 2 | 21/2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 600 | 11/2 | $21 / 4$ | 3 | $33 / 4$ | 41.2 | 6 | $71 / 2$ | 9 | 101/2 | 12 |
| 800 | 2 | 3 | 4 | 5 | 6 | 8 | 10 | 12 | 14 | 16 |
| 1000 | 21/2 | $33 / 4$ | 5 | 61/4 | 71/2 | 10 | 121/2 | 15 | 171/2 | 20 |
| 1200 | 3 | $41 / 2$ | 6 | $71 / 2$ | 9 | 12 | 15 | 15 | 21 | 24 |
| 1500 | $33 / 4$ | $53 / 4$ | 71/2 | 9112 | 111/2 | 15 | $183 / 4$ | 221/2 | 261/2 | 30 |
| 1800 | 41/2 | $63 / 4$ | 9 | 111/4 | 131/2 | 18 | 221\% | 27 | 311/2 | 36 |
| 2000 | 5 . | $71 / 2$ | 10 | 121/2 | 15 | 20 | 25 | 30 | 35 | 40 |
| 2400 | 6 | 9 | 12 | 15 | 18 | 24 | 30 | 36 | 42 | 48 |
| 2800 | 7 | 101/2 | 14 | 171/2 | 21 | 28 | 35 | 42 | 49 | 56 |
| 3000 | $71 / 2$ | 111/4 | 15 | 183/4 | 221/2 | 30 | $371 / 2$ | 45 | 521/2 | 60 |
| 3500 | 834 | 13 | 171/2 | 22 | 26 | 35 | 44 | $521 / 2$ | 61 | 70 |
| 4000 | 10 | 15 | 20 | 25 | 30 | 40 | 50 | 60 | 70 | 80 |
| 4500 | 111/4 | 17 | $22^{1 / 2}$ | 28 | 34 | 45 | 57 | 69 | 78 | 90 |
| 5000 | 121/2 | 19 | 2.5 | 31 | $371 / 2$ | 50 | 621\% | 75 | 87\% | 100 |

## DOUBLE LEATHER

| Speed in <br> Feet per <br> Minute. | Width of Belt in Inches. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 | 20 |
|  | $11-\mathrm{P}$. | H.-P. | 11.-1. | H.-P. | H.-P. | H.-P. | 11.-P. | H.-P. | II. P P |
| 400 | 23, 4 | 414 | $53 / 4$ | 71/4 | $81 / 2$ | 10 | 11112 |  | $14 \frac{1}{2}$ |
| 600 | $41 / 4$ | $61 / 2$ | $83 / 4$ | 11 | 13 | 15 | 171/2 | 191/2 | 22 |
| 800 | $53 / 4$ | 81/2 | 111/2 | 141/2 | 171/2 | 201/2 | 23 | 26 | 29 |
| 1000 | $71 / 4$ | 11 | 141/2 | 181/4 | 211/2 | $251 / 2$ | 29 | 321/2 | 36 |
| 1200 | 81/3 | 13 | 171/2 | 22 | 26 | 301/2 | $341 / 2$ | 39 | 44 |
| 1500 | 103/4 | 161/4 | $213 / 4$ | $271 /$ | 321/2 | 38 | $431 / 2$ | 49 | $541 / 2$ |
| 1800 | 13 | 191/2 | 26 | 323 | 39 | $451 / 2$ | 52 | 59 | $651 / 2$ |
| 2000 | 141/2 | 213/4 | 29 | $361 / 2$ | 431/2 | $501 /$ | 58 | $651 / 2$ | $72 \%$ |
| 2400 | 171/4 | 26 | 3434 | 44 | 521/2 | $601 / 2$ | $691 / 2$ | 781/2 | 88 |
| 2800 | 201/4 | $301 /$ | 401/2 | 51 | 61 | 71 | 81 | 911/2 | 102 |
| 3000 | $211 / 2$ | $321 / 2$ | 431/2 | 541/2 | 651/2 | 76 | 871/2 | 98 | 108 |
| 3500 | $251 / 2$ | 38 | $503 / 4$ | $631 / 2$ | 76 | 89 | 101 | 114 | 127 |
| 4000 | 29 | $431 / 2$ | 581/4 | 723 | 87 | 101 | 116 | 131 | 145 |
| 4500 | $321 / 2$ | 49 | 65 | 82 | 98 | 114 | 131 | 147 | 163 |
| 5000 | $361 / 2$ | $511 / 2$ | 723/4 | 91 | 109 | 127 | 145 | 163 | 182 |

The above tables are based on the following equivalents:
Single Belting, one inch wide, 800 feet per minute $=$ one horse-power, equal to four ply rubber $=$ working tension of 42 pounds.

Double Belting, one inch wide, 550 feet per minute $=$ one horse-power, equal to six ply rubber $=$ Working tension of 60 pounds.

## Board Measure

Length in Feet.

| SIZE. | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1x8 | 8 | $91 / 3$ | 102/3 | 12 | 131/3 | 142/3 | 16 | 171/3 | 182/3 | 20 | 211/3 | 222/3 | 24 | 251/3 |  |
| 1×10 | 10 | $112 / 3$ | 131/3 | 15 | 162/3 | 181/3 | 20 | 212/3 | $231 / 3$ | 25 | 262/3 | 281/3 | 30 | 312/3 | 331 |
| 1x12 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 |
| 1x14 | 14 | 161/3 | 182/3 | 21 | 231/3 | 252/3 | 28 | $301 / 3$ | 322/3 | 35 | 371/3 | 392/3 | 42 | 441/3 | 462 |
| $1 \times 16$ | 16 | 182/3 | $211 / 3$ | 21 | $262 / 3$ | 291/3 | 32 | 342/3 | 371/3 | 40 | 422/3 | $45 \%$ | 48 | 502/3 | $531 / 3$ |
| 2x3 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 |
| 2 x 4 | 8 | $91 / 3$ | 102/3 | 12 | 131/3 | 142/3 | 16 | 171/3 | 182/3 | 20 | 211/3 | 222/3 | 24 | 251/3 | $26 \% / 3$ |
| $2 \times 6$ | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 |
| $2 \times 8$ | 16 | 182/3 | 211/3 | 24 | $262 / 3$ | 291/3 | 32 | $342 / 3$ | 371/3 | 40 | 422/3 | 451/3 | 48 | 502/3 | $531 / 3$ |
| $2 \times 10$ | 20 | 231/3 | 26\% 3 | 30 | $331 / 3$ | 362/3 | 40 | $431 / 3$ | 462/3 | 50 | $531 / 3$ | $562 / 3$ | 60 | 631\% | $662 / 3$ |
| 2x12 | 24 | 28 | 32 | 36 | 40 | 41 | 48 | 52 | 56 | 60 | 64 | 68 | 72 | 76 | 80 |
| 2×14 | 28 | 32\% | 371/3 | 42 | $462 / 3$ | 5113 | 56 | 602/3 | 651/3 | 70 | 742/3 | 791/3 | 84 | S82 | $931 / 3$ |
| $2 \times 16$ | 32 | 371\% | 422/3 | 48 | 531/3 | . $582 / 3$ | 64 | 691/3 | 742\% | 80 | 851/3 | 902/3 | 96 | 1011/3 | $1062 / 3$ |
| 3x4 | 12 | 14 | 16 | 15 | 20 | 22 | 21 | 26 | 28 | 30 | 32 | 31 | 30 | 38 | 40 |
| $3 \times 6$ | 18 | 21 | 24 | 27 | 30 | 33 | 36 | 39 | 42 | 45 | 48 | 51 | 54 | 57 | 60 |
| $3 \times 8$ | 24 | 28 | 32 | 36 | 40 | 44 | 48 | 52 | 56 | 60 | 64 | 68 | 72 | 76 | $\bigcirc 0$ |
| $3 \times 10$ | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 6.5 | 70 | 75 | 80 | 85 | 90 | 95 | 100 |
| $3 \times 12$ | 36 | 42 | 48 | 54 | 60 | 66 | 72 | 78 | 84 | 90 | 96 | 102 | 108 | 114 | 120 |
| $3 \times 14$ | 42 | 49 | 56 | 63 | 70 | 77 | 84 | 91 | 98 | 105 | 112 | 119 | 126 | 133 | 140 |
| $3 \times 16$ | 48 | 56 | 64 | 72 | 80 | SS | 96 | 104 | 112 | 120 | 128 | 136 | 144 | 52 | 160 |
| 4 x 4 | 16 | 182/3 | 211/3 | 24 | $262 / 3$ | 291/3 | 32 | 342/3 | 371\% | 40 | 42\%/3 | 451/3 | 48 | 502/3 | $531 / 3$ |
| $4 \times 6$ | 24 | 28 | 32 | 36 | 40 | 44 | 48 | 52 | 56 | 60 | 64 | 68 | 72 | 76 | 80 |
| 4x8 | 32 | $371 / 3$ | 122/3 | 48 | $531 / 3$ | 582/3 | 64 | 691/3 | 742 | 80 | 851/3 | 902/3 | 96 | 101 | 1062 |
| $4 \times 10$ | 40 | 462/3 | $531 / 3$ | 60 | $66 \%$ | $731 / 3$ | 80 | 86\% ${ }^{\frac{3}{3}}$ | $931 / 3$ | 100 | 1062/3 | 1131/3 | 120 | 126 | 1331/3 |
| $4 \times 12$ | 48 | 56 | 64 | 72 | 80 | 88 | 96 | 104 | 112 | 120 | 128 | 136 | 144 | 152 | 160 |
| $4 \times 14$ | 56 | 651/3 | 742 /3 | 84 | 931 | 1022 | 112 | 1211/3 | 1302/3 | 140 | 1491/ | 1582/3 | 168 | 1771 | 1862/3 |
| 4×16 | 64 | $742 / 3$ | 851/3 | 96 | 1062/3 | 1171/3. | 128 | 1382/3 | 1491/3 | 160 | 1702/3 | $1811 / 3$ | 192 | 2022/3 | $2131 / 3$ |
| 6x6 | 36 | 42 | 48 | 54 | 60 | 66 | 72 | 7S | S4 | 90 | 96 | 102 | 108 | 114 | 120 |
| $6 \times 8$ | 48 | 56 | 64 | 72 | 80 | 88 | 96 | 104 | 112 | 120 | 128 | 136 | 144 | 152 | 160 |
| $6 \times 10$ | 60 | 70 | 80 | 90 | 100 | 110 | 120 | 130 | 140 | 150 | 160 | 170 | 180 | 190 | 200 |
| $6 \times 12$ | 72 | 84 | 96 | 109 | 120 | 132 | 144 | 156 | 168 | 180 | 192 | 20.4 | 216 | 228 | 240 |
| $6 \times 14$ | S4 | 98 | 112 | 126 | 140 | 154 | 168 | 182 | 196 | 210 | 224 | 238 | 252 | 256 | 280 |
| x16 | 96 | 112 | 128 | 144 | 160 | 176 | 192 | 208 | 224 | 240 | 256 | 272 | 288 | 304 | 320 |
| 8 x 8 | 64 | 742/3 | 85, $1 / 3$ | 96 | 1062/3 | 1171/3 | 128 | 1382/3 | 1491\% | 160 | 1702 | 1811\% | 192 | 202 | 2131 |
| $8 \times 10$ | S0 | 931/3 | 1062/3 | 120 | 1331/3 | $1462 / 3$ | 160 | $1731 / 3$ | 1862 | 200 | 2131 | $2263 / 3$ | 240 | 2531 | 260 |
| $8 \times 12$ | 96 | 112 | 128 | 144 | 160 | 176 | 192 | 208 | 224 | 240 | 256 | $\stackrel{272}{ }$ | 298 | 304 | 320 |
| $8 \times 14$ | 112 | 1302/3 | 14913 | 168 | 1862/3 | 2051/3 | 22.4 | $2422 / 3$ | $2611 / 3$ | 280 | 2982 | 31713 | 336 | 3542 | 3731 |
| $8 \mathrm{8x} 16$ | 128 | $1491 /$ | 170\% | 192 | 2131/3 | 2342/3 | 256 | '2771/3 | 2982/3 | 320 | 3411 | 3622\% | 384 | -1051/3 | 1262/3 |
| $10 \times 10$ | 100 | 1162/3 | 1331/3 | 1.50 | 1662/3 | 1831/3 | 200 | 2162/3 | 2331/3 | 250 | 2662 | 2831/3 | 300 | $3162 / 3$ | $3331 / 3$ |
| $10 \times 12$ | 120 | 140 | 160 | 180 | 200 | 220 | 240 | 260 | 280 | 300 | 320 | 340 | 360 | 380 | 400 |
| 10×14 | 140 | 1631/3 | 1862/3 | 210 | $2331 / 2$ | 2562/3 | 280 | 30311 | $3262 / 3$ | 350 | 3731 | $3962 / 3$ | 410 | 4431/3 | 4662 |
| $10 \times 16$ | 160 | 1862/3 | 2131/3 | 240 | 2662/3 | 2931\% | 320 | 3462 | 3731 | 400 | 4262/3 | $4531 / 3$ | 480 | 5062 | 5331 |
| $12 \times 12$ | 144 | 168 | 192 | 216 | 240 | 264 | 285 | 312 | 336 | 369 | 384 | 408 | 432 | 456 | 480 |
| $12 \times 14$ | 168 | 196 | 224 | 252 | 280 | 308 | 336 | 364 | 392 | 420 | 448 | 476 | 504 | 532 | 560 |
| $12 \times 16$ | 192 | 224 | 256 | 288 | 320 | 352 | 384 | 416 | 448 | 480 | 512 | 544 | 576 | 608 | 640 |
| $14 \times 14$ | 196 | 22S2/3 | $2611 / 3$ | 294 | $3262 / 3$ | 3591\% | 392 | 4242/3 | 4571/3 | 490 | 5222/3 | $55.51 / 3$ | 588 | 6202 | 6531 |
| $14 \times 16$ | 224 | $2611 / 3$ | 298\% | 336 | $3731 / 3$ | 4102\% | 448 | 4851/3 | $5221 \frac{1}{3}$ | 560 | 5971 | 6312/3 | 672 | 7091/3 | 7462/3 |
| $16 \times 16$ | 256 | 2982/3 | $3411 / 3$ | 384 | 4262/3 | 4691/3 | 512 | 5542/3 | 5971/3 | 640 | 6822/3 | $7251 / 3$ | 768 | 8102/3 | 8531/3 |

Note-By simply multiplying or dividing the above amounts, the number of feet contained in other dimensions can be obtained.

# Board and Timber Measure 

## BOARD MEASURE

In board measure boards are assumed to be one inch in thickness.
To compute the measure or surface in square feet-
When all dimensions are in feet:
Rule-Multiply the length by the breadth, and the product will give the surface required.
When either of the dimensions are in inches:
Rule-Multiply as above and divide the product by 12 .
When all dimensions are in inches:
Rule-Multiply as before and clivide product by 144.

## TIMBER MEASURE

To compute the volume of round timber-
When all dimensions are in feet:
Rule-Multiply the length by the square of one-quarter of the main girt, and the product will give the measurement in cubic feet.

When length is given in feet and girt in inches:
Rule-Multiply as before and divide by 144 .
When a!l the dimensions are in inches:
Rule-Multiply as before and divide by $1,72 \mathrm{~s}$.
Sawed or hewed timber is measured by the cubic foot.

To compute the volume of square timber-
When all dimensions are in feet:
Rule-Multiply the product of the brearth by the depth by the length, and the product will give the volume in cubic feet.

When either of the dimensions are in inches:
Rule-Multiply as above and divide the product by 12 .
When any two of the dimensions are in inches:
Rule-Multiply as before and divide the product by 144 .

# Simple Problems in Air Compression 

## Extracts from an address delivered before the Mining Association of the University of California, By Edward A. Rix.

Allow 20 hp . for every 100 cu . ft. of cylinder-displacement, to compress air to 90 or 95 lb . recciver gauge-pressure at sea-level.

It would be well in small plants, up to 400 cu . ft . capacity to make no distinction between single and two-stage machines.

In using compressed air at 90 lb . pressure cold, it will take $24 \mathrm{cu} . \mathrm{ft}$. free air per minute to give one horse-power in plain slide-valve engines and $15 \mathrm{cu} . \mathrm{ft}$. with good expansion-valve gearing; between these two limits will lie all the various types of engines. If the air be re-heated to about $300^{\circ} \mathrm{F}$, it will reduce the above quantities about one-third.

For operating ordinary station and sinking pumps of the direct-acting type, which is the ordinary stock pump used in mining operations, it will be safe to calculate that one cubic foot of free air compressed to 90 lb . gange-pressure will do 135 foot-gallons of pumping.

Ordinary mining hoists have a mechanical efficiency of about 75 per cent.
For the determination of sizes of pipes, losses of pressure, and terminal pressures for com-pressed-air transmission, we the formula:

$$
\mathrm{P}_{1} 2^{2}-\mathrm{P}_{2} 2=\frac{0.0006 \mathrm{~V}^{2} \mathrm{~L}}{\mathrm{~A}^{5}} \quad \begin{aligned}
& \mathrm{P}_{1}=\text { absolute initial air-pressure. } \\
& \mathrm{P}_{2}=\text { absolute terminal air-pressure. } \\
& \mathrm{V}=\text { free ais equivalent passing through the pipe. } \\
& \mathrm{L}=\text { length of pipe in feet. } \\
& \mathrm{A}=\text { diameter in inches. }
\end{aligned}
$$

Problem.-Given a water-power distant 5000 ft . from a mine, it is desired to generate compressed air and transmit it to the collar of the shaft to perform work as follows:

One hundred tons of ore and waste to be hoisted in 20 hours.
Thirty gallons of water per minute to be pumped.
Five $21 / 4$-in standard piston rock-drills to be operated.
Three air-hammer drills to be operated.

## General Conditions:

Depth of shaft, 600 f .
Weight of skip and rope, $1,000 \mathrm{lb}$.
Weight of ore hoisted, 1 ton.
Initial air-pressure, 95 lb .
Final air-pressure, 90 lb .
Altitude, sea-level.
Geared hoist and unbalanced hoisting.

## Required:

Size of compressor.
Diameter of air-pipe.
Brake horse-power.
Altitude factors.
Re-heating coefficients.
Note: Reduce all requirements to cubic feet of free air, because free air is the basis for all power calculations.

## To determine the free air required for hoisting:

100 tons of ore and waste lioisted in 20 hours $=5$ tons per hour, each load contains one ton $=a$ load hoisted every 12 minutes. 2000 lb . material and 1000 lb . rope and skip $=$ a total of 3000 lb . 3000 lb . lifted $600 \mathrm{ft} .=1,800,000$ foot-pounds, or 54 hp . theoretical, at $75 \%$ efficiency, the 51 hp . becomes 72 brake-power actually required. Using cold air, it requires, 24 cu . ft. free air per horse power. Then the hoist will consume to make a lift, $24 \times 72=1728 \mathrm{cu} . \mathrm{ft}$. of free air. This gives us direct results without taking into consideration the element of time or the dimensions of the hoist.

# Simple Problems in Air Compression 

(Continued)

If $1728 \mathrm{cu} . \mathrm{ft}$. are required to make a hoist every 12 minutes the compressor must furnish $144 \mathrm{cu} . \mathrm{ft}$. free air per minute continuously, and we assume that we hoist at the rate of 300 ft . per min.; it will take 2 minutes to make the lift, and the hoist will be lowering and idle cluring the next 10 minutes, the compressor delivering $10 \times 144=1440 \mathrm{cu}$. ft. free air which must be stored. Sufficient storage capacity is the vital point of hoisting economica!ly with compressed air.

While we have allowed 4 hours in 24 , or 1 hr .20 min . on each shift, for hoisting and lowering men, timbers, supplies, etc., it is probable that at least once every hour someone will be going up and down the shaft, and it would be practical therefore to say that the hoist would handle 6 loads per hour, instead of 5 , and we must therefore add $20 \%$ to the $144 \mathrm{cu} . \mathrm{ft}$. making the hoisting requirement say, $175 \mathrm{cu} . \mathrm{ft}$. per min .

## To determine the amount of compressed air required for pumping:

For pumping 30 gallons per min. 600 ft ., requires 30 x 600 , or $18,00 \mathrm{o}$ foot gallons of work. If one cu. ft . of free air at 90 lb . gauge-pressure will give 135 ft -gal., we shall require $133 \mathrm{cu} . \mathrm{ft}$. free air for the pumping. This requirement is constant.

## To determine the amount of compressed air required for drilling:

Five $21 / 4$-in. rock-drills will require 50 ft . frec air each, or $250 \mathrm{cu} . \mathrm{ft}$.
Three air-hammer drills will require $25 \mathrm{cu} . \mathrm{ft}$. each, or $75 \mathrm{cu} . \mathrm{ft}$.
To get these amounts, take about $80 \%$ of the requirements as stated in rock-drill catalogues, which always give quantities in compressor-cylinder displacement, which do not deliver on an average within $20 \%$ of their displacement, except in large machines.

## Total requirements will therefore be:

| Work. |  | Cubic Feet. |
| :---: | :---: | :---: |
| Hoisting. |  | 175 |
| Pumping. |  | 133 |
| Drilling. |  | 325 |

Allow for a $5 \%$ pipe-leakage on the entire system. This would bring requirement up to 665 .
Allow for a volumetric efficiency of at least $\$ 0 \%$, this will require a total cylinder displacement of 830 ctu . ft. per minute, and with the power factor of 20 hp . per $100 \mathrm{cu} . \mathrm{ft} ., 166 \mathrm{hp}$. delivered on the water-wheel shaft is required to drive compressor.

To determine the size of the pipe: Allow 5 lb . drop in pressure for friction loss.

$$
\text { Formula: } \quad \mathrm{P}_{1}{ }^{2}-\mathrm{P}_{2} 2=\frac{0.0006 \mathrm{~V}_{2} \mathrm{~L}}{\mathrm{~A}^{5}}
$$

$P_{1}$, initial pressure absolute $=95+14.7$, or 109.7 , and its square is 12034 .
$\mathrm{P}_{2}$, the terminal pressure, 5 lb . less than the initial, or 901 ll ., or 104.7 absolute, and, its square is 10962 .

The difference between these two or $\mathrm{P}_{1} 2-\mathrm{P}_{2}{ }^{2}=1072$.

# Simple Problems in Air Compression 

(Continued)

Substituting this in our equation, and also the values for $\mathbf{L}$. and V , we have
reducing, we have

$$
1072=\frac{6 \times 5000 \times 633 \times 633}{10,000 \times \mathrm{A}^{5} .}
$$

$$
\begin{aligned}
1072 \mathrm{xA}^{5} & =3 \times 633^{2}, \text { or } \mathrm{A}^{5}=1121 \\
\mathrm{~A} & =4-\mathrm{in} . \text { pipe } .
\end{aligned}
$$

## In General:

Refer to trade catalogues and tables and look up a satisfactory compressor, having a displacement of $830 \mathrm{cu} . \mathrm{ft}$. For this capacity it is advisable to select a two-stage compressor, because it has a higher volumetric efficiency, requires less power to operate, is easier to lubricate on account of lower temperatures and has less strain on mechanism.

The first thing to consider is the speed at which the compressor will operate. If a limited sum is to be expended, as high a working speed as possible will be selected, because, the higher the speed, the smaller the compressor. If the future is to be taken into consideration, more air will be wanted as shaft goes deeper and more water encountered. It would then be wise to select a machine which at say two-thirds of its rated speed would produce the present requirements and give a 50 per cent. margin for the future.

## Altitude:

As the altitude increases, the initial absolute pressure diminishes and as the final pressure remains the same, the pressure ratio grows larger as the altitude increases. For example, at $10,000 \mathrm{ft}$. elevation the atmospheric pressure is 10 lbs . instead of 14.7 lbs at sea level. In the problem, the ratio of compression at sea level is 7.5 while at 10,000 feet elevation it would be 10.5 . The sea-level compressor must be increased, therefore, $10.5 \div 7.5$, or 1.4 times, to give the same weight of compressed air at $10,000 \mathrm{ft}$. altitude. In other words the altitude compressor must be about 40 per cent. larger to do the same work.

TABLE OF EFFICIENCIES AND CAPACITIES AT VARIOUS ALTITUDES.

| Altitude above Sea-level Fect. | Absolute Pressure per sq. in. Lbs. | Barometric Pressure Inches. | Cubic Feet of Free Air Remaining Constant. |  | Cubic Feet of Compressed Air Remaining Constant. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Volumetric Efficiency | Power Required. | Increased Capacity of Compressor | Increased Horse Power Required. |
| 0 | 14.79 | 30.0 | 100\% | 100\% | 0\% | 0\% |
| 1000 | 14.15 | 28.8 | $97 \%$ | 98.2\% | $3.3 \%$ | 2.2\% |
| 2000 | 13.61 | 27.8 | 93\% | $96.5 \%$ | 7.6\% | $3.9 \%$ |
| 3000 | 13.10 | 26.7 | 90\% | $94.8 \%$ | $10.3 \%$ | $5.6 \%$ |
| 4000 5000 | 12.61 | 25.7 24.8 | $87 \%$ $84 \%$ | $93.1 \%$ $91.5 \%$ | $14 \%$ $18 \%$ | $7.3 \%$ $8.9 \%$ |
| 6000 | 11.68 | 23.8 | 81\% | $89.9 \%$ | $22 \%$ | 10.6\% |
| 7000 | 11.24 | 22.9 | 78\% | 88.4\% | 26\% | 12.3\% |
| 8000 | 10.82 | 22.1 | $76 \%$ | $86.9 \%$ | $31 \%$ | 14.2\% |
| 9000 | 10.42 | 21.3 | $73 \%$ | $85.4 \%$ | $36 \%$ | 16.2\% |
| 10000 | 10.03 | 20.5 | $70 \%$ | $83.9 \%$ | $40 \%$ | 18.2\% |
| 11000 | 9.66 | 19.7 | 68\% | $82.4 \%$ | 45\% | 20.3\% |
| 12000 | 9.30 | 19.0 | 65\% | 80.9\% | 50\% | 22.4\% |

# Simple Problems in Air Compression 

(Continued)

To determine the amount of compressed air required by re-heating:
It is practical to re-heat air to from 300 to $400^{\circ} \mathrm{F}$ in various ways, and great economy is realized especially for pumping and hoisting, and if it is possible you may reduce the quantities of cold air figured for this character of work by the ratio of the atmospheric to the compressed-air temperatures absolute. Thus, if the atmosphere is at $60^{\circ} \mathrm{F}$ or $520^{\circ}$ absolute, and the compressed air is used at $300^{\circ} \mathrm{F}$ or $760^{\circ}$ absolute, then the volume of cold air for your work may be taken at the ratio of $520 \div 760$, or about $70 \%$, thus making a saving of 30 per cent.

TABLE 1.--CUBIC FEET OF FREE AIR REQUIRED TO RUN ONE DRILL OF THE SIZE AND AT THE PRESSURE STATED BELOW.

| Guage Pressure | Cylinder Diameter of Drill. |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $2^{\prime \prime}$ | 21/4" | $21 / 2^{\prime \prime}$ | 23/4" | $3^{\prime \prime}$ | $31 / 8^{\prime \prime}$ | $3_{\frac{3}{3}{ }^{\frac{18}{\prime \prime}}}$ | $31 /{ }^{\prime \prime}$ | $31 /{ }^{\prime \prime}$ | $35 / 8^{\prime \prime}$ | 43/4' ${ }^{\prime \prime}$ | $5^{\prime \prime}$ | $51 / 2^{\prime \prime}$ |
| 60 | 50 | 60 | 68 | 82 | 90 | 95 | 97 | 100 | 108 | 113 | 130 | 150 | 164 |
| 70 | 56 | 68 | 77 | 93 | 102 | 108 | 110 | 113 | 124 | 129 | 147 | 170 | 181 |
| 80 | 63 | 76 | 86 | 104 | 114 | 120 | 123 | 127 | 131 | 143 | 164 | 190 | 207 |
| 90 | 70 | 84 | 95 | 115 | 126 | 133 | 136 | 141 | 152 | 159 | 182 | 210 | 230 |
| 100 | 77 | 92 | 104 | 126 | 138 | 146 | 149 | 154 | 166 | 174 | 199 | 240 | 252 |

TABLE II.-MULTIPLIERS TO DETERMINE COMPRESSOR CAPACITY REQUIRED TO OPERATE FROM 1 TO 70 ROCK DRILLS AT ALTITUDES COMPARED WITH SEA LEVEL.

|  | NUMBER OF DRILLS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 12 | 15 | 20 | 25 | 30 | 40 | 50 | 60 | 70 |
|  | MULTIPLIERS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0 |  | $1.8$ | 2.7 |  | 4.1 | 4.8 | 5.4 | 6.0 | 6.5 | 7.1 | 8.1 | 9.5 | 11.7 | 13.7 | 15.8 | 21.4 | 25.5 | 29.4 | 33.2 |
| 1000 | 1.03 | 1.85 | 2.78 |  | 4.22 | 4.94 | 5.56 | 6.18 | 6.69 | 7.3 | 8.34 | 9.78 | 12.05 | 14.1 | 16.3 | 22.0 | 26.26 | 30.3 | 34.2 |
| 2000 | 1.07 | 1.92 | 2.89 | 3.61 | 4.39 | 5.14 | 5.78 | 6.42 | 6.95 | 7.60 | 8.67 | 10.17 | 12.52 | 14.66 | 16.9 | 22.9 | 27.28 | 31.46 | 35.52 |
| 3000 | 1.10 | 1.93 | 2.97 | 3.74 | 4.51 | 5.28 | 5.94 | 6.6 | 7.15 | 7.81 | 8.91 | 10.45 | 12.87 | 15.07 | 17.38 | 23.54 | 28.05 | 32,34 | 36.52 |
| 4000 | 1.14 | 2.05 | 3.08 | 3.88 | 4.67 | 5.47 | 6.15 | 6.84 | 7.41 | 8.09 | 9.23 | 10.83 | 13.34 | 15.62 | 18.01 | 24.4 | 29.07 | 33.52 | 37.8 |
| 5000 | 1.17 | 2.10 | 3.16 | 3.98 | 4.8 | 5.62 | 6.32 | 7.02 | 7.61 | 8.31 | 9.48 | 11.12 | 13.69 | 16.03 | 18.49 | 25.04 | 29.84 | 34.4 | 38.84 |
| 6000 | 1.20 | 2.16 | 3.24 | 4.08 | 4.9 | 5.76 | 6.48 | 7.2 | 7.8 | 8.52 | 9.72 | 11.7 | 14.04 | 16.44 | 18.96 | 25.68 | 30.6 | 35.4 | 39.84 |
| 7000 | 1.23 | 2.21 | 3.32 | 4.18 | 5.04 | 5.9 | 6.64 | 7.38 | 7.99 | 8.73 | 9.96 | 11.68 | 14.39 | 16.85 | 19.43 | 26.32 | 31.36 | 36.16 | 40.84 |
| 8000 | 1.26 | 2.27 | 3.40 | 4.28 | 5.17 | 6.05 | 6.8 | 7.56 | 8.19 | 8.95 | 10.21 | 11.97 | 14.74 | 17.26 | 19.9 | 26.96 | 32.13 | 37.04 | 41.83 |
| 9000 | 1.29 | 2.32 | 3.48 | 4.39 | 5.29 | 6.19 | 6.96 | 7.74 | 8.38 | 9.16 | 10.45 | 12.26 | 15.09 | 17.67 | 20.38 | 27.6 | 32.9 | 37.92 | 42.83 |
| 10000 | 1.32 | 2.38 | 3.56 | 4.49 | 5.41 | 6.34 | 7.13 | 7.92 | 8.58 | 9.37 | 10.69 | 12.54 | 15,44 | 18.08 | 20.86 | 28.25 | 33.66 | 38.8 | 43.92 |
| 12000 | 1.37 | 2.47 | 3.7 | 4.66 | 5.62 | 6.57 | 7.4 | 8.22 | 8.9 | 9.73 | 11.1 | 13.02 | 16.03 | 18.77 | 21.64 | 29.32 | 34.94 | 10.28 | 45.48 |

Example.-Required the amount of free air necessary to operate thirty 5 inch drills at 9,000 feet altitude, using to operate these drills air at a guage pressure of 80 pounds per square inch.

From Table I we find, when operating the drills at $\$ 0$ pounds guage pressure at sea level, that one 5 -inch drill requires 190 cubic feet of free air per minute.

From Table II we also find that the factor for 30 drills at 9,000 feet altitude is 20.38 ; multiplying 190 cubic feet by 20.38 gives 3,872 cubic feet free air per minute, which is the displacement of a compressor for the above outfit under average conditions, to which must be added pipe line losses, such as friction and leakage.

## Table for Computing Effective Strains and Loads on Inclines

| 1. <br> Degree. | $\begin{aligned} & \text { II. } \\ & \text { Sine. } \end{aligned}$ | III. <br> Cosecant. | I. <br> Degree. | $\begin{gathered} \text { II. } \\ \text { Sine. } \end{gathered}$ | III. <br> Cosecant. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 90 | 1.000 | 1.000 | 45 | 707 | 1.414 |
| 89 | 1.000 | 1.000 | 44 | 605 | 1.440 |
| 88 | . 999 | 1.001 | 43 | . 682 | 1.466 |
| 87 | . 999 | 1.001 | 42 | . 669 | 1.494 |
| 86 | . 99.8 | 1.002 | 41 | . 656 | 1.524 |
| 85 | . 990 | 1.004 | 40 | . 643 | 1.556 |
| 81 | . 995 | 1.009 | 39 | . 629 | 1.589 |
| 83 | . 993 | 1.008 | 38 | . 616 | 1.624 |
| 82 | . 990 | 1.010 | 37 | . 602 | 1.662 |
| S1 | . 988 | 1.012 | 36 | . 588 | 1.701 |
| 80 | .985 | 1.015 | 35 | . 574 | 1.743 |
| 79 | . 982 | 1.019 | 34 | . 559 | 1.788 |
| 78 | . 978 | 1.022 | 33 | . 545 | 1. 536 |
| 77 | . 974 | 1.026 | 32 | . 530 | 1.887 |
| 76 | . 970 | 1.031 | 31 | . 515 | 1.942 |
| 7.5 | . 966 | 1.035 | 30 | . 500 | 2.000 |
| 74 | . 961 | 1.040 | 29 | . 485 | 2.063 |
| 73 | 956 | 1.046 | 28 | . 469 | 2.130 |
| 72 | 951 | 1.051 | 27 | 454 | 2.203 |
| 71 | . 946 | 1.058 | 26 | . 438 | 2.281 |
| 70 | . 940 | 1.064 | 25 | . 423 | 2.366 |
| 69 | . 934 | 1.071 | 24 | . 407 | 2.459 |
| 68 | .927 | 1.079 | 23 | . 391 | 2.559 |
| 67 | . 921 | 1.086 | 22 | . 375 | 2.669 |
| 66 | . 914 | 1.095 | 21 | . 358 | 2.790 |
| 65 | . 906 | 1.103 | 20 | . 342 | 2.924 |
| 64 | . 899 | 1.113 | 19 | . 326 | 3.071 |
| 63 | . 891 | 1.122 | 18 | . 309 | 3.236 |
| 62 | . 883 | 1.133 | 17 | . 292 | 3.420 |
| 61 | . 875 | 1.143 | 16 | . 276 | 3.628 |
| 60 | . 866 | 1.155 | 15 | . 259 | 3.864 |
| 59 | . 857 | 1.167 | 14 | . 242 | 4.134 |
| 58 | . 848 | 1.179 | 13 | .225 | 4.445 |
| 57 | . 839 | 1.192 | 12 | 208 | 4.810 |
| 56 | . 829 | 1.206 | 11 | . 191 | 5.241 |
| 55 | . 819 | 1.221 | 10 | . 174 | 5.759 |
| 54 | . 809 | 1.236 | 9 | . 156 | 6.392 |
| 53 | . 799 | 1.252 | 8 | . 139 | 7.185 |
| 52 | . 788 | 1.269 | 7 | . 122 | 8.206 |
| 51 | . 777 | 1.287 | 6 | . 105 | 9.567 |
| 50 | 766 | 1305 | 5 | . 087 | 11.474 |
| 49 | 755 | 1.325 | 4 | . 070 | 14.336 |
| 48 | 743 | 1.346 | 3 | . 052 | 19.107 |
| 47 | . 7331 | 1.367 | 2 | . 035 | 28.654 |
| 46 | . 719 | 1.390 | 1 | . 017 | 57.299 |

The table will be found useful where hoisting is done in inclined shafts. It may also be applied to "gravity tramways" or "inclined planes."

The following examples will show its uses: Suppose the weight of ore is $10,000 \mathrm{lbs}$; skip, $6,000 \mathrm{lbs}$. ; rope, $7,500 \mathrm{lbs}$.; and that the shaft has an inclination of 55 degrees from the horizontal. What is the strain of the rope? Total load, $10,000+6,000+7,500=23,500$.

Rule:-For each pound weight, the effective load on rope for the angle of incline from the horizontal given in column I will be found opposite in column II.

Therefore, find 55 degrees in column I and opposite in column 1 is .819 , which multiplied by $23,500=19,246.5 \mathrm{lbs}$., the total effective strain on rope.

Suppose an engine can raise $5,000 \mathrm{lbs}$. in a vertical shaft, what can it pull up an incline 30 degrees from the horizontal?

Rule:-For each pound which an engine can lift vertically, it can raise the amount given in column III up an incline of the angle given in column I. Therefore, find 30 degrees in column 1, and opposite in column 1 II is 2 , which multiplied by $5,000=10,000 \mathrm{lbs}$, the amount engine can pull up a 30 degree incline.

If the proper working strain of the rope were $5,000 \mathrm{lbs}$., on a vertical lift, it would be 10,000 lbs. on a 30 degree incline; the process is the same.

Note:-In using the table, it must not be overlooked that the friction of drawing the car, skip or cage on the rails or guides is to be added to the effertive weight in order to obtain the total amount of strain borne by the . rope. This friction is termed "traction" or "tractile effort" and varies between thirty and one hundred pounds per ton, according to circumstances and is of more importance on inclines of small angle.

## Standard Hoisting Ropes

Composed of 6 Strands of 19 wires each, with Hemp Center.


# Practical Hints Regarding Saw Mills and the Care of Saws 

A Right Hand Mill has the saw at the sawyer's right and runs toward him.
A Left Hand Mill has the saw at the sawyer's left and runs toward him.
SIZE OF SAWS.-With the Variable Feed Mill, any size saw can be used according to the
 used on the mandrel to reduce the specd to correspond with the size of the saw and the power. The diameter of the saw should be about one and a half times the diameter of the $\log$ to be cut-a 36 -inch $\log$ requires a 54 -inch saw-a 40 -inch $\log$ requires a 60 -inch saw, and so on.

SPEED OF SAWS.-Speeding saws too high is a very common mistake-usually a serious and a foolish error of judgment. Manufacturers, in their catalogues, give the maximum speeds at which their saws may be operated with safety on the basis of the highest power the saws are calculated to withstand. These speeds cannot properly be used for portable mills for the reason that often the power used is not sufficient-they are put there for selling purposes of the sawmakers and to show what the saw will stand, not what it is supposed to do in practical work. While speed is power-it's easy to consume all the power in speed without doing any work. A 48 -inch saw run by a 10 H . P. engine should have a speed of 300 revolutions a minute-slower if the saw has the usual number of teeth. About twenty-four tecth are necessary to give the best results at 300 revolutions-the usual number is 30 -and usually works satisfactorily.

PORTABLE MILLS running with 20 H . P. and undet should run the rim of the saw at a speed not exceeding 360 ft . per minute to each horse power. For example, multiply 360 by 10 H. P., and divide this by 12 ft . (circumference of the 48 -inch saw), and you get 300 revolutions per minute. For smaller power the speed should be some higher in proportion, but the saw should have fewer teeth to make up for the higher speed. 20 H . P. and above should have more speed in proportion to the larger number of teeth. With this power the teeth should be 5 inches apart, which will give 30 teeth to the 48 -inch saw. For a larger power, the teeth should be closer together until they reach the limit of 3 inches apart, and then as the power is increased the speed of the saw is increased to correspond. A saw must be speeded right to give the best results.

To aid in the selection of a saw and to determine its proper speed; we give the following table, based on a saw 48 inches in diameter:

| Power | Distance from Point to Point of Teeth | Number of Teeth | Speed of Saw |
| :---: | :---: | :---: | :---: |
| $6 \mathrm{t} . \mathrm{P}$. | 7 inches | 22 | 300 |
| 8 " | 7 " | 22 | 300 |
| 10 " | 6 " | 2.1 | 300 |
| 12 " | 6 " | 24 | 350 |
| 15 " | 5 " | 30 | 400 |
| 20 " | 5 " | 30 | 450 |

To find the proper speed of larger or smaller saws, multiply the speed given of a 48 -inch saw by 48 and divide the product by the size of the saw selected. A larger saw should have a greater number of teeth, and a smaller saw a lesser number, the distance apart remaining approximately the same.

Saws for cutting hardwood or frozen timber are usually run at higher speed and have a greater number of teeth.

# Practical Hints Regarding Saw Mills and the Care of Saws 

## (Continued)

In ordering a saw mill or saw, the amount of power used, size and speed of driving pulley should always be given so that a pulley of the proper size may be sent with the mill and a suitable saw sclected.

PROPER GAUGE OF SAWS.-For portable mills as a general rule we recommend $8^{\prime \prime} \mathrm{x} 9^{\prime \prime}$ gauge saws. For larger power where saws are run at high speed, or for cutting valuable hard woods we recommend $9^{\prime \prime} \times 10^{\prime \prime}$ gauge.

HOW TO HANG AND LINE SAWS.-It does not follow that because one saw will work well that another will do so on the same mandrel, or that two saws will hang alike on the same mandrel.

In hanging a new saw, after screwing it up between the collars examine carefully on the front or $\log$ side, and see if the front of the saw is flat. If it is found to be rounding on the log side, cut a ring of paper about half an inch wide, the size of the collar on the outside, oil it and stick iton the face of the fast collar around the outer edge. Then tut another ring of paper the same width, making the hole the same size as the hole in the loose collar; put this small ring between the loose collar and the saw, and screw up the collar. If the two rings are not enough, put in more unti ${ }^{1}$ the saw comes flat and true. If the saw hangs dishing on the log side, reverse the rings of paper; that is, put the small rings between the saw and the fast collar, and the large ring against the loose collar. To do proper work, the saw must be perfectly flat and straight on the side next to the log.

DIRECTIONS FOR RUNNING CHISEL TOOTII SAWS.-First the saw should be placed on the mandrel where it is to be run, observing directions for hanging circular saws.

Should the saw run a little out of true on the rim, it may be made to run true by packing with writing paper between the saw and fast collar. It is necessary that the saw mandrel should be perfectly level so that the saw will hang exactly plumb.

Never attempt to run a saw that is dishing on the log side as it will be sure to draw towards the log. The carriage track must be straight and level, so that the carriage can run true.

HOW TO FILE AND KEEP IN ORDER GIRCULAR SAWS.-It is not well to file all of the teeth of circular saws from the same side of the saw, especially if each alternate tooth is bent for the set, but file one-half of the teeth from each side of the saw, and of the treth that are bent from you, so as to leave them on a slight bevel-leave the outer corners a little the longest.

Never filc any saw to sharp or acute angles at the throats or roots of the teeth, but on circular lines, as all saws are liable to crack from sharp corners.

Keep your saw round, so that each tooth will do its proportional part of the work.
Saw tceth wear narrow at the extreme points; consequently they must be kept spread so that they will be widest at the very points of the teeth; otherwise saws will not work successfully.

Teeth should be kept as near a uniform shape and distance apart as possible, in order to keep a circular saw in balance and condition for business.

Frosted steel is always brittle. No intelligent woodsman will use a good chopping axe on hard frozen timber until after he has taken the frost out of it, and no intelligent sawyer will attempt to set teeth of any saw without taking out the frost.

# Practical Hints Regarding Saw Mills and the Care of Saws 

(Continued)

The greatest wear on the saw is on the under edges of the teeth. File nearly to an edge (but not quite), leaving a short bevel of $\frac{1}{32}$ of an inch wide on the under side of the point. But in no instance file to a fine point and thin wire edge.

Be sure that the saw hangs properly on the mandrel.
The saw must be in proper line with the carriage and the carriage run true.
The mandrel must be level and run freely in the boxes.
Do nearly all the filing on the under sides of the teeth, and see that they are well spread at the points; file square and have them project alike on both sides of the saw.

If the saw heats in the center when the mandrel runs cool in the boxes, cool it off and line it into the log a little.

If the saw heats on the rim and not in the center, cool it off and line it out of the log a littleand vice versa if it heats in the centre. Every sawyer should have a side file to keep the teeth the same width.

Before commencing to insert the teeth, provide a cup of oil, which, together with the tecth, place conveniently near where you will stand, at the back of the saw. Take the wrench, place the pins in the holes in the shank, and turn it so that the hook projects sufficiently to receive the bit, pick up a tooth with the other hand and dip its grooved segment into the oil; then place in position and hold it firmly and even with the sides of the blade, while at the same time press the wrench downward until the shank fits into its place.

The chisel teeth are exact in width, and the spread uniformly good, and make smoother lumber than is made by the solid saw, even when not in the hands of first-class sawyers; but if extra nice work is desired, try a gauge on the side of each tooth, and if any are found to project a trifle too far, reduce them with a side file, being careful to preserve the same relief of the corncr. No flat surface should be allowed on the sides of the teeth; they must be relieved from the very edge; then the saw will run straight, and with the least possible expenditure of power, and make smooth lumber. Practical use of the chisel bits has proven conclusively that in order to get the most and best use of them, when a set has been inserted and properly adjusted, they should remain until they are wern out, and as often as may be required edge them up by applying a file to their face or under side; after being sharpened several times they should be relieved on the side, so as to keep their corners sharp. Should a shank become straight or compressed, by reason of the saw having been run on iron, so that it will not hold the bit firmly, lay it on an anvil and strike it with a hammer on the inner edge until expended sufficiently to hold the bit.

Do not try the experiment of bending ear!s alternate tooth for the set when using Inseried Tooth Saws.

Vse a light lammer in swedging, about 3 to 1 pound weight, holding the swedge so that the teeth will be spread at the points.

IN FILING SOLID-TOOTH CIRCULAR SAWS keep the throats or roots of the tecth round, or as the saws are when new. Angles or square corners filed at the roots of the teeth will almost invariably cause a saw to crack. The filing of such angles or square corners will cancel the warranty on any saw. The back or top of the tooth leads or guides the saw and should be filed square across. The under sides of the teeth may be filed a little beveled when they are bent alternately for the set, so as to leave the outer corner of the cutting edge longest.

## LIST of BULLETINS

Issued to date by the

## Joshua Hendy Iron Works

## Iron Founders, Engineers and Machinery Merchants

## 75 Fremont St., San Francisco, Cal.

| No. | Subject | Date | Condition |
| :---: | :---: | :---: | :---: |
| 100 | Pinder Concentrator | Nov. 1906, | Issued |
| 101 | Hendy Two and Three-stamp Mills, | Nov. 1906, | Exhausted <br> (See No.113) |
| 102 | Davis Horse Whim | Oct. 1906, | Issued |
| 103 | Ore and Water Buckets | Jan. 1907, | Issued |
| 104 | Hendy Standard Ore Cars | Mar. 1907, | Issued |
| 105 | Hydraulic Water Gates, etc. | Feb. 1907, | Issued |
| 106 | Hendy Hydraulic Giants | A pril 1907, | Issued |
| 107 | Ore Crushers | May 1907, | Exhausted (See No.117) |
| 108 | Winches, Derricks, etc. | Nov. 1907, | Issued |
| 110 | Hendy Fire Monitors | Nov. 1907, | Issued |
| 111 | Hendy Gravel Elevators | Aug. 1908, | Issued |
| 113 | Hendy Two and Three-stamp Mills, | June 1908, | Issued |
| 114 | Tangential Water Wheels, etc. | Dec. 1908, | Issued |
| 115 | Matteson Ore Cars | Dec. 1908, | Issued |
| 116 | Graupner Centrifugal Roller Mill | Dec. 1908, | Issued |
| 117 | Crushers and Crushing Rolls | Dec. 1908, | Exhausted (See No. 121) |
| 118 | Challenge Ore Feeders | Dec. 1908, | Issued |
| 119 | Stamp Mills, Standard | Jan. 1910, | In Press |
| 120 | Stamp Mill Accessories | Jan. 1910, | Issued |
| 121 | Crushers and Crushing Rolls | Jan. 1910, | Issued |

January 15th, 1910

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