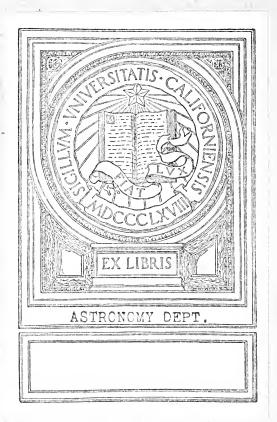
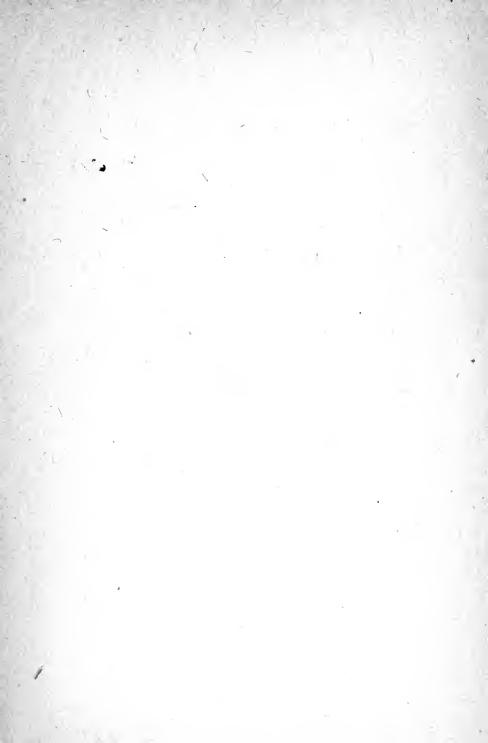
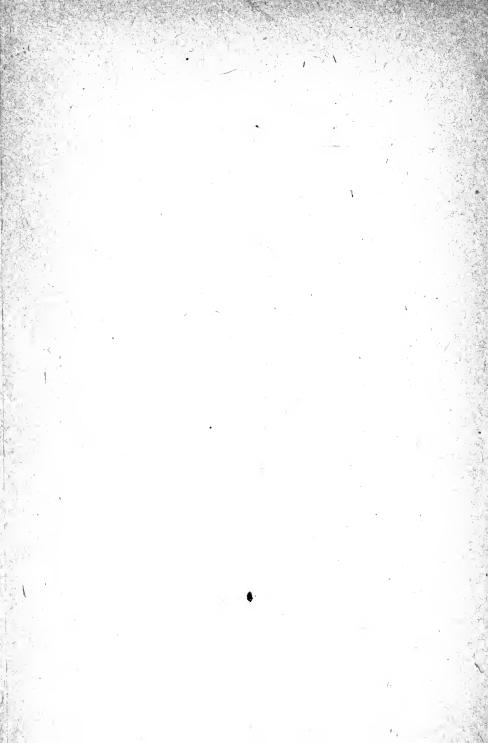


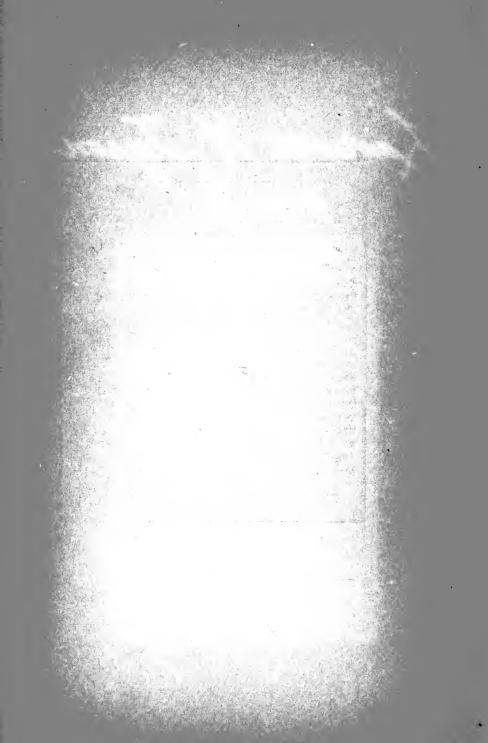
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# LOGARITHMIC AND OTHER MATHEMATICAL TABLES

WITH EXAMPLES OF THEIR USE AND HINTS ON THE ART OF COMPUTATION

BY

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## ASTRONOMY DEPT.

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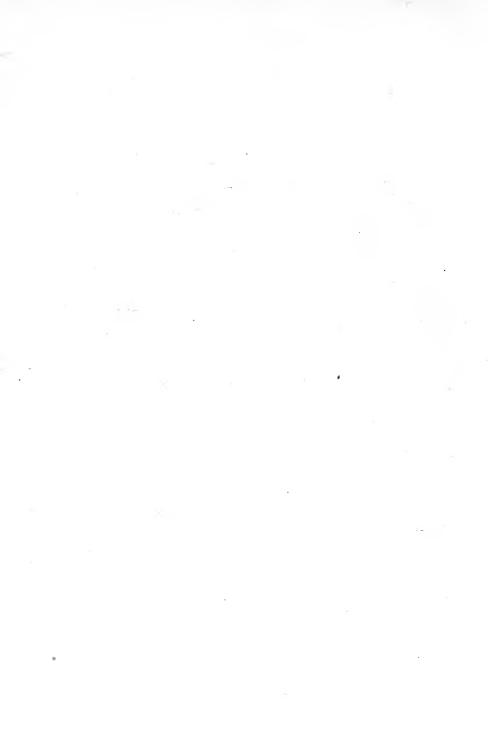
#### PREFACE.

In the present work an attempt is made to present to computers and students a set of logarithmic and trigonometric tables which shall have all the conveniences familiar to those who use German tables. The five-figure tables of F. G. GAUSS, of which fifteen editions have been issued, have, after long experience with them, been taken as the basis of the present ones, but modifications have been introduced wherever any improvement could be made.

Five places of decimals have been adopted as an advantageous mean. The results obtained by them, being nearly always reliable to the 10,000th part, are amply accurate for most computations, while the time of the student who uses them is not wasted in unnecessary calculation.

The Introduction is intended to serve not only as an explanation of the tables, but as a little treatise on the art of computation, and the methods by which the labor of computation may be abridged.

To avoid fostering the growing evil of nearsightedness among students, the author and publishers have spared neither pains nor expense in securing clearness of typography.



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#### TABLE I.

#### LOGARITHMS OF NUMBERS.

#### 1. Introductory Definitions.

Natural numbers are numbers used to represent quantities. The numbers used in arithmetic and in the daily transactions of life are natural numbers.

To every natural number may be assigned a certain other number, called its logarithm.

The **logarithm** of a natural number is the exponent of the power to which some assumed number must be raised to produce the first number. The assumed number is called the **base**. *E.g.*, the logarithm of 100 with the base 10 is 2, because  $10^2 = 100$ ; with the base 2, the logarithm of 64 would be 6, because  $2^6 = 64$ .

A system of logarithms means the logarithms of all positive numbers to a given base.

Although there may be any number of systems of logarithms, only two are used in practice, namely:

- 1. The natural or Napierian system, base = e = 2.718282.
- 2. The common system, base = 10.

The natural system is used for purely algebraic purposes.

The common system is used to facilitate numerical calculations and is the only one employed in this book.

If the natural number is represented by n, its logarithm is called  $\log n$ .

A logarithm usually consists of an integer number and a decimal part.

The integer is called the **characteristic** of the logarithm. The decimal part is called the **mantissa** of the logarithm.

A table of logarithms is a table by which the logarithm of any given number, or the number corresponding to any given logarithm, may be found.

The most simple form of table is that on the first page of Table I., which gives the logarithms of all entire numbers from 1 to 150; each logarithm being found alongside its number. The student may begin his exercises with this table.

Mathematical tables in general enable us, when one of two related quantities is given, to find the other.

In such tables the quantity supposed to be given is called the argument.

The argument is usually printed on the top, bottom, or side of the table.

The quantities to be found are called **functions** of the argument, and are found in the same columns or lines as the argument, but in the body of the table.

In a table of logarithms the natural number is the argument, and the logarithm is the function.

#### 2. The Use of Logarithms.

The following properties of logarithms are demonstrated in treatises on algebra.

I. The logarithm of a product is equal to the sum of the logarithms of its factors.

II. The logarithm of a quotient is found by subtracting the logarithm of the divisor from that of the dividend.

III. The logarithm of any power of a number is equal to the logarithm of the number multiplied by the exponent of the power.

IV. The logarithm of the root of a number is equal to the logarithm of the number divided by the index of the root.

We thus derive the following rules:

To find the product of several factors by logarithms.

Rule. Add the logarithms of the several factors. Enter the table with the sum as a new logarithm, and find the number corresponding to it.

This number is the product required.

Example 1. To multiply  $7 \times 8$ .

We find from the first page of Table I.

 $\log 7 = 0.84510$ 

" 8 = 0.90309

Sum of logs = 1.748 19 = log of product. Having added the logarithms, we look in column log for a number corresponding to 1.788 19 and find it to be 56, which is the product required.

Ex. 2 To find the continued product  $2 \times 6 \times 8$ .

log 2, 0.301 03
 6, 0.778 15
 8, 0.903 09

Sum of logs, 1.982 27 = log product.

The number corresponding to this logarithm is found to be 96, which is the product required.

Ex. 3. To find the quotient of  $147 \div 21$ .

log 147, 2.167 32 " 21, 1.322 22

Difference, 0.845 10

We find this difference to be the logarithm of 7, which is the required quotient.

Ex. 4. To find the quotient arising from dividing the continued roduct  $98 \times 102 \times 148$  by the continued product  $21 \times 37 \times 68$ .

log 21, 1.322 22 log 98, 1.991 23
" 37, 1.568 20 " 102, 2.008 60
" 68, 1.832 51 " 148, 2.170 26

Sum = log divisor, 4.722 93 Sum = log dividend, 6.170 09 log divisor, 4.722 93

Difference = log quotient, 1.447 16

Looking into the table, we find the number corresponding to this logarithm to be 28, which is the required quotient.

Note. The student will notice that we have found this quotient without actually determining either the divisor or dividend, having used only their logarithms. If he will solve the problem arithmetically, he will see how much shorter is the logarithmic process.

Ex. 5. To find the seventh power of 2.

We have  $\log 2 = 0.30103$ 

7

 $2.10721 = \log 128$ 

Hence 128 is the required power.

Ex. 6. To find the cube root of 125.

 $\begin{array}{r}
3 \mid 2.09691 \\
\hline
0.69897
\end{array}$ 

The index of the root being 3, we divide the logarithm of 125 by it. Looking in the tables, we find the number to be 5, which is the root required.

#### EXERCISES.

Compute the following products, quotients, powers, and roots by logarithms.

1. 11.13. Ans. 143. 5. 
$$\frac{22 \cdot 8^3}{\sqrt{121}}$$
. Ans. 128. 2. 12°. Ans. 144. 6.  $\frac{51 \cdot 98 \sqrt{81}}{34 \cdot 63}$ . Ans. 21. 3.  $\frac{12^3}{6^3}$ . Ans. 48. 7.  $\frac{2^7 \cdot 3^4}{6^3}$ . Ans. 144. 4.  $\frac{2 \cdot 9^2 \cdot 91 \cdot 78}{13^2 \cdot 21 \cdot 3}$ . Ans. 108. 8.  $\frac{54 \cdot 48}{8 \cdot 9}$ . Ans. 36.

#### 3. Arrangement of the Table of Logarithms.

A table giving every logarithm alongside its number, as on the first page of Table I., would be of inconvenient bulk. For numbers larger than 150 the succeeding parts of Table I. are therefore used. Here the first three figures of the natural number are given in the left-hand column of the table. The first figure must be understood where it is not printed. The fourth figure is to be sought in the horizontal line at the top or bottom. The mantissa of the logarithm is then found in the same line with the first three digits, and in the column having the fourth digit at the top.

To save space the logarithm is not given in the column, but only its last three figures. The first two figures are found in the first column, and are commonly the same for all the logarithms in any one line.

Example 1. To find the logarithm of 2090.

We find the number 209, the figure 2 being omitted in printing, in the left-hand column of the table, and look in the column having the fourth figure, 0, at its top or bottom. In this column we find 320 15, which is the mantissa of the logarithm required.

Ex. 2. To find the logarithm of 2092.

Entering the table with 209 in the left-hand column, and choosing the column with 2 at the top, we find the figures 056. To these we prefix the figures 32 in column 0, making the total logarithm .320 56. Therefore

Mantissa of  $\log 2092 = .32056$ .

#### EXERCISES.

Find in the same way the mantissæ of the logarithms of the following numbers:

2240;	5133;
2242;	5256;
2249;	5504;
2895;	8925;
3644;	9557;
4688;	9780.

When the first two figures of the mantissa are not found in the same line in which the number is sought, they are to be found in the first line above which contains them.

Example. The first two figures of log 6250 are 79, which belongs to all the logarithms below as far as 6309. Therefore mantissa of log 6250 = .79588.

#### EXERCISES.

Find the mantissæ of the logarithms of

6300;	answer,	.799 34.
6309;	66	.79996
6434;		
6653;		
6755;		
6918;		
7868.		

Exception. There are some cases in which the first two figures change in the course of the line. In this case the first two figures are to be sought in the line above before the change and in the line next below after the change.

Example. The mantissa of log 6760 is .82995. But the mantissa of log 6761 is .83001. In this case the figures 83 are to be found in the next line below. To apprise the computer of these cases, each of the logarithms in which the two first figures are found in the line below is indicated by an asterisk.

#### EXERCISES.

#### Find the mantissa of

log 1022;	answer,	.009 45.
log 1024:	66	.010 30.

1999;
3988;
4675;
4798;
5377;
8512;
1009.

#### 4. Characteristics of Logarithms.

The part of the table here described gives only the *mantissa* of each logarithm. The characteristic must be found by the general theory of logarithms.

The following propositions are explained in treatises on algebra:

$\mathbf{T}$ he	logarithm	of	1	is	0.
"	"	"	10	"	1.
66	"	"	100	66	2.
"	"	"	1000	"	3.
66	"	"	$10^{n}$	"	n.

Since any number of one digit is between 0 and 10, its logarithm is between 0 and 1; that is, it is 0 plus some fraction. In the same way, the logarithm of a number of two digits is 1 + a fraction. And in general,

The characteristic of the logarithm of any number greater than 1 is less by unity than the number of its digits preceding the decimal point.

Example. The characteristic of the logarithm of any number between 1 and 10 is 0; between 10 and 100 it is 1; between 100 and 1000 it is 2, etc.

It is also shown in algebra that if a number be divided by 10 we diminish its logarithm by unity.

Logarithms of numbers less than unity are most conveniently expressed by making the characteristic alone negative.

For example:

log 
$$0.2 = \log 2 - 1 = -1 + .30103$$
;  
"  $0.02 = \log 2 - 2 = -2 + .30103$ .

Hence: The mantissæ of the logarithms of all numbers which differ only in the position of the decimal point are the same.

Hence, also, in seeking a logarithm from the table we find the mantissa without any reference to the decimal point. Afterward we affix the characteristic according to the position of the decimal point.

For convenience, when a negative characteristic is written the minus sign is put above it to indicate that it extends only to the characteristic below it and not to the mantissa. Thus we write

$$\log .02 = \overline{2}.30103.$$

In practice, however, it is more common to avoid the use of negative characteristics by increasing them by 10. We then write  $\log .02 = 8.30103 - 10$ .

If we omitted to write -10 after the logarithm, the latter would, in strictness, be the log of  $2 \times 10^{\rm s}$ . But numbers so great as this product occur so rarely in practice that it is not generally necessary to write -10 after the logarithm. This may be understood.

A convenient rule for remembering what characteristic belongs to the logarithm of a decimal fraction is:

The characteristic is equal to 9, minus the number of zeros after the decimal point and before the first significant figure.

Examples. 
$$\log 34060 = 4.53224$$

"  $340.60 = 2.53224$ 

"  $3.4060 = 0.53224$ 

"  $.03406 = 8.53224 - 10$ 

"  $.0003406 = 6.53224 - 10$ 

It will be seen that we can find the logarithms of numbers from 1 to 150 without using the first page of the table at all, since all the mantissæ on this page are found on the following pages as logarithms of larger numbers.

#### EXERCISES.

Find the logarithms of the following numbers:

1.515	.003 899
.01 702	0.4276
18.62	464 700
.03 735	98.030

Find the numbers corresponding to the following logarithms:

<b>- 10</b> ;

#### 5. Interpolation of Logarithms.

In all that precedes we have used only logarithms of numbers containing not more than 4 significant digits. But in practice numbers of more than four figures have to be used. To find the logarithms of such numbers the process of interpolation is necessary. This process is one of simple proportion, which can be seen from the following example.

To find log. 1167.23.

The table gives the logarithms of 1167 and of 1168, which we find to be as follows:

 $\log 1167 = 3.067 07$ " 1168 = 3.067 44Difference of logarithms = .000 37

Now the number of which we wish to find the logarithm being between these numbers, its logarithm is between these logarithms; that is, it is equal to 3.067 07 plus a fraction less than .000 37.

Since the difference 37 corresponds to the difference of unity in the two numbers, we assume that the quantity to be added to the logarithm bears the same proportion to .23 that 37 does to unity. We therefore state the proportion

1:.23:: 37: increase required.

The solution of this proportion gives  $.23 \times 37 = 8.51$ , which is the quantity to be added to log 1167 to produce the logarithm required.\* The result is 3.0671551.

But our logarithms extend only to five places of decimals, while the result we have written has seven. We therefore take only five places of decimals. If we write the mantissa 3.06715, the result will be too small by .51. If we write 3.06716, it will be too great by .49. Since the last result is nearer than the first, we give it the preference, and write for the required logarithm

 $\log 1167.23 = 3.06716.$ 

We thus have the following rule for interpolating:

Take from the table the logarithm corresponding to the first four significant digits of the number.

Considering the following digits as a decimal fraction, multiply the difference between the logarithm and the next one following by such decimal fraction.

<sup>\*</sup>In this multiplication we have used a decimal point to mark on the fifth order of decimals. This is a convenient process in all such computations.

This product being added to the logarithm of the table will give the logarithm required.

The whole operation by which we have found log 1167.23 would then be as follows:

The products for interpolation, 7.4 and 1.11, may be found by multiplying by the fifth and sixth figures of the number separately.

To facilitate this multiplication, tables of proportional parts are given in the margin. Each difference between two logarithms will be readily found in heavy type not far from that part of the table which is entered, and under it is given its product by .1, .2, etc., . . .9. We therefore enter this little table with the fifth figure, and take out the corresponding number to be added to the logarithm. Then if there is a sixth figure, we enter with that also and move the decimal one place to the left. We then add the two sums to the logarithm.

#### 6. Labor-saving Devices.

In using a table of logarithms, the student should accustom himself to certain devices by which the work may be greatly facilitated.

In the first place it is not necessary to take the whole difference between two consecutive logarithms. He has only to subtract the last figure of the preceding logarithm from the last one of the following, increased by 10 if necessary, and thus find the last figure of the difference.

The nearest difference in the margin of the table having this same last figure will always be the difference required.

Example. If the first four figures of the number are 1494, instead of subtracting 435 from 464 we say 5 from 14 leaves 9, and look for the nearest difference which has 9 for its last figure. This we readily find to be 29, at the top of the next page.

Note. In nearly all cases the difference will be found on the same page with the logarithm. The only exception is at the bottom of the first page, where, owing to the number of differences, they cannot all be printed.

In the preceding examples we have written down the numbers in full, which it is well that the beginner should do for himself. But after a little practice it will be unnecessary to write down anything but the logarithm finally taken out. The student should accustom himself to take the proportional parts mentally, adding them to the logarithm of the table and writing down the sum at sight. The habit of doing this easily and correctly can be readily acquired by practice.

Exercises. Find the logarithms of 792 638; 0.99997; 1000.77; 949.916; 1000.07; 20.8962; 100 007; 660 652; 181 982; 77.642; 281.936; 8.8953.

As a precaution in taking out logarithms, the computer should always, after he has got his result, look into the table and see that it does really fall between two consecutive logarithms in the table.

If the fraction to be interpolated is nearly unity, especially if it is equal to or greater than 9, it will generally be more convenient to multiply the difference of the logarithms by the complement\* of the fraction and subtract the product from the logarithm next succeeding. The following are examples of the two methods, which may always be applied whether the fraction be large or small:

Example 1.  $\log 1004.28 = \log (1005 - .72)$ . log 1004, .001 73  $\log 1005$ , .002 17 pr. pt. for pr. pt. for .7, .2, -30.88.8 66 66 66 66 66 66 .08. 3.5 .02,log, 3.001 85 log, 3.001 85  $Ex. 2. \log 154993 = 155000 - 7.$ .19005log 1549, 1550, .190 33 pr. pt. for -.07, pr. pt. for 25.2-1.96.9, .. .. .. 0.8 .03. log, 5.190 31 log, 5.19031

co. .723 = .277 co. .1796 = .8204 co. .9932 = .0068.

<sup>\*</sup> By the complement or arithmetical complement of a decimal fraction is here meant the remainder found by subtracting it from unity or from a unit of the next order higher than itself. Thus:

#### 7. To find the Number corresponding to a given Logarithm.

The reverse process of finding the number corresponding to a given logarithm will be seen by the following example:

To find the number of which the logarithm is 2.02790.

Entering the table, we find that this logarithm does not exactly occur in the table. We therefore take the next smaller logarithm, which we find to be as follows:

 $\log 1066 = 2.02776.$ 

Subtracting this from the given logarithm we find the latter to be greater by 14, while the difference between the two logarithms of the table is 40. We therefore state the proportion

40:14::1 to the required fraction.

The result is obtained by dividing 14 by 40, giving a quotient .35. The required number is therefore 106.635. It will be remarked that we take no account of the characteristic and position of the decimal until we write down the final result, when we place the decimal in the proper position.

The table of proportional parts is used to find the fifth and sixth

figures of the number by the following rule:

If the given logarithm is not found in the table, note the excess of the given logarithm above the next smaller one in the table, which call \( \Delta \).

Take the difference of the two tabular logarithms, and find it among the large figures which head the proportional parts.

That proportional part next smaller than \( \Delta \) will be the fifth

figure of the required number.

Take the excess of △ above this proportional part; imagine its decimal point removed one place to the right, and find the nearest number of the table.

This number will be the sixth figure of the required number.

Example. To find the number of which the logarithm is 2.193 59.

Entering the table, we find the next smaller logarithm to be .193 40. Therefore  $\Delta = 19$ .

Also its tabular difference = 28.

Entering the table of proportional parts under 28, we find 16.8 opposite 6 to be the number next smaller than 19 the value of  $\Delta$ . Therefore the fifth figure of the number is 6.

The excess of 19 above 16.8 is 2.2. Looking in the same table

for the number 22, we find the nearest to be opposite 8.

Therefore the fifth and sixth figures of the required number are 68. Now looking at the log .193 40 and taking the corresponding number, we find the whole required number to be

156 168.

The characteristic being 2, the number should have three figures before the decimal point. Therefore we insert the decimal point at the proper place, giving as the final result 156.168.

#### 8. Number of Decimals necessary.

In the preceding examples we have shown how with these tables the numbers may be taken out to six figures. In reality, however, it will seldom be worth while to write down more than five figures. That is, we may be satisfied by adding only one figure to the four found from the table. In this case, when we enter the table of proportional parts, we take only the number corresponding to the nearest proportional part.

To return to the last preceding example, where we find the number corresponding to 2.19359. We find under the difference 28 that the number nearest 19 is 19.6, which is opposite 7.

Therefore the number to be written down would be 156.17.

In the following exercises it would be well for the student to write six figures when the number is found on one of the first two pages of the table and only five when on one of the following pages. The reason of this will be shown subsequently.

#### EXAMPLES AND EXERCISES.

1. To find the square root of 3.

We have  $\begin{array}{c}
\log 3, \ 0.477 \ 12 \\
\text{`` 2, } 0.301 \ 03 \\
\log \frac{3}{2}, \ 0.176 \ 09 \\
\div 2, \log \sqrt{\frac{3}{2}}, \ 0.088 \ 04
\end{array}$ 

Here we have a case in which the half of an odd number is required. We might have written the last logarithm 0.088 045, but we should then have had six decimals, whereas, as our tables only give five decimals, we drop the sixth. If we write 4 for the fifth figure it will be too small by half a unit, and if we write 5 it will be too large by half a unit. It is therefore indifferent which figure we write, so far as mere accuracy is concerned.

A good rule to adopt in such a case is to write the nearest EVEN number. For example,

for the half of .261 81 we write .130 90; .261 83 .130 92; " " .26185.130 92; 66 .261 87 .130 94; 66 .261 89 66 .130 94; 66 .261 97 .130 98; " " .261 99 .131 00.

Returning to our example, we find, by taking the number corresponding to 0.08804,

$$\sqrt{\frac{3}{2}} = 1.22472.$$

2. To find the square root of \(\frac{2}{3}\).

$$\log 2, 0.301 03$$
" 3, 0.477 12
$$\log \frac{2}{3}, 9.823 91 - 10$$

$$\frac{1}{2} \log \frac{2}{3}, 4.911 96 - 5 = \log \sqrt{\frac{2}{3}}.$$

The last logarithm is the same as

$$9.91196 - 10,$$

which is the form in which it is to be written in order to apply the rule of characteristics. The corresponding number is 0.816 50.

We have here a case in which, had we neglected considering the surplus -10 as we habitually do, the characteristic of the answer would have been 4 instead of 9 or -1. The easiest way to treat such cases is this:

When we have to divide a logarithm in order to extract a root, instead of increasing the characteristic by 10, increase it by 10 × index of root.

Thus we write  $\log \frac{2}{3} = 19.823 \ 91 - 20$ . Dividing by 2,  $\log \sqrt{\frac{2}{3}} = 9.911 \ 96 - 10$ , which is in the usual form.

3. To find the cube root of  $\frac{1}{2}$ .

$$\log 1, 0.00000$$
" 2, 0.30103
$$\log \frac{1}{2}, 9.69897 - 10,$$

which we write in the form

$$\log \frac{1}{2} = 29.69897 - 30.$$

Dividing this by 3,

$$\frac{1}{3}\log\frac{1}{4} = \log^3\sqrt{\frac{1}{4}} = 9.89966 - 10.$$

This logarithm is in the usual form, and gives

$$\sqrt[3]{\frac{1}{2}} = 0.79370.$$

The affix -30, or  $-10 \times \text{divisor}$ , can be left to be understood in these cases as in others. All that is necessary to attend to is that instead of supposing the characteristic to be one or more units less than 10, as in the usual run of cases, we suppose it to be one or more units less than  $10 \times \text{divisor}$ .

Find:

- 4. The square root of  $\frac{1}{2}$ ;
- 5. The cube root of 2;
- 6. The fourth root of 3;
- 7. The fifth root of 20;
- 8. The tenth root of 10;
- 9. The tenth root of 10.

#### 9. The Arithmetical Complement.

When a logarithm is subtracted from zero, the remainder is called its arithmetical complement.

If L be any logarithm, its arithmetical complement will be -L. Hence if

 $L = \log n$ 

then

arith. comp. = 
$$-L = \log \frac{1}{n}$$
;

that is,

The arithmetical complement of a given logarithm is the logarithm of the reciprocal of the number corresponding to the given logarithm.

Notation. The arithmetical complement of a logarithm is written co-log. It is therefore defined by the form

$$\text{co-log } n = \log \frac{1}{n}.$$

Finding the arithmetical complement. To find the arithmetical complement of  $\log 2 = 0.30103$ , we may proceed thus:

0.00000

log 2, 0.301 03

co-log 2, 
$$9.69897 - 10$$
.

We subtract from zero in the usual way; but when we come to the characteristic, we subtract it from 10. This makes the remainder too large by 10, so we write -10 after it, thus getting a quantity which we see to be  $\log 0.5$ .

We may leave the -10 to be understood, as already explained.

The arithmetical complement may be formed by the following rule:

Subtract each figure of the logarithm from 9, except the last significant one, which subtract from 10. The remainders will form the arithmetical complement.

For example, having, as above, the logarithm 0.301 03, we form, mentally, 9-0=9; 9-3=6; 9-0=9; 9-1=8; 9-0=9; 10-3=7; and so write

9.698 97

as the arithmetical complement.

To form the arithmetical complement of 3.284 00 we have 9-3=6; 9-2=7; 9-8=1; 10-4=6. The complement is therefore

6.716 00.

The computer should be able to form and write down the arithmetical complement without first writing the tabular logarithm, the subtraction of each figure being performed mentally.

Use of the arithmetical complement. The co-log is used to substitute addition for subtraction in certain cases, on the principle: To add the co-logarithm is the same as to subtract the logarithm.

Example. We may form the logarithm of  $\frac{3}{2}$  in this way by addition:

log 3, 0.47712 co-log 2, 9.69897 log 3, 0.17609

Here there is really no advantage in using the co-log. But there is an advantage in the following example:

To find the value of  $P = \frac{2763 \times 419.24}{99}$ . We add to the logarithms of the numerator the co-log of the denominator, thus:

The use of the arithmetical complement is most convenient when the divisor is a little less than some power of 10.

#### EXERCISES.

Form by arithmetical complements the values of:

1. 
$$\frac{109 \times 216.26}{0.99316}$$

2. 
$$\frac{8263 \times 9162.7}{92 \times 99.618}$$

$$3. \quad \frac{4 \times 6 \times 8219}{9 \times 992}$$

#### 10. Practical Hints on the Art of Computation.

The student who desires to be really expert in computation should learn to reduce his written work to the lowest limit, and to perform as many of the operations as possible mentally. We have already described the process of taking a logarithm from the table without written computation, and now present some exercises which will facilitate this process.

1. Adding and subtracting from left to right. If one has but two numbers to add it will be found, after practice, more easy and natural to write the sum from the left than from the right. The method is as follows:

In adding each figure, notice, before writing the sum, whether the sum of the figures following is less or greater than 9, or equal to it.

If the sum is less than 9, write down the sum found, or its last figure without change.

If greater than 9, increase the figure by 1 before writing it down.

If equal to 9, the increase should be made or not made according as the first sum following which differs from 9 is greater or less than 9.

If the first sum which differs from 9 exceeds it, not only must we increase the number by 1, but must write zeros under all the places where the 9's occur. If the first sum different from 9 is less than 9, write down the 9's without change.

The following example illustrates the process:

Here 7 and 8 are 15. 5+2 being less than 9, we write 15 without change. 3+0 being less than 9, we write 7 without change. 9+2 being greater than 9, we increase the sum 3+0 by 1 and write down 4. 7+1 being

less than 9, we write the last figure of 9+2, or 1, without change. 6+7 being greater than 9, we increase 7+1 by 1 and write down 9. Under 6+7 we write down 3 or 4. To find which, 8+1=9; 3+6=9; 5+4=9; 7+5=12. This first sum which is different from 9 being greater than 9, we write 4 under 6+7, and 0's in the three following places where the sums are 9. 7+5=12. Since 8+0<9, we write down 2. Before deciding whether to put 8 or 9 under 8+0, we add 5+4=9; 8+1=9; 8+1=9; 9+0=9; 2+2=4. This being less than 9, we write 8 under 8+0, and 9's in the four following places. Since 5+8=13>9, we write 5 under 2+2. Since 9+3=12>9, we write 4 under 5+8. Since 8+7=15>9, we write 3 under 9+3. Finally, under 8+7 we write 5.

This process cannot be advantageously applied when more than two numbers are to be added.

#### EXERCISES.

Let the student practise adding each consecutive pair of the following lines, which are spaced so that he can place the upper margin of a sheet of paper under the lines he is adding and write the sum upon it.

2	5	0	9	1	7	2	8	5	3	1	6	9	8	1	2	0	8
																6	
																9	
2																	
8	6	8	5	8	8	9	6	4	3	4	2	9	4	4	8	2	5
9	8	7	6	5	4	3	2	1	0	1	2	3	4	5	6	7	4

Subtracting. We subtract each figure of the subtrahend from the corresponding one of the minuend (the latter increased by 10 if necessary), as in arithmetic.

Before writing down the difference, we note whether the following figure of the subtrahend is greater, less, or equal to the corresponding figure of the minuend.

If greater, we diminish the remainder by 1 and write it down.\*

If less, we write the remainder without change.

If equal, we note whether the subtrahend is greater or less than the minuend in the first following figure in which they differ.

If greater, we diminish the remainder by 1, as before, and write 9's under the equal figures.

<sup>\*</sup> If the student is accustomed to carrying 1 to the figures of the minuend when he has increased the figure of his subtrahend by 10, he may find it easier to defer each subtraction until he sees whether the remainder is or is not to be diminished by 1, and, in the latter case, to increase the minuend by 1 before subtracting.

If less, write the remainder unchanged, putting 0's under the equal figures.

Example.

7 2			_	_	_		-		-				
4	8	0	2	4	9	9	8	2	0	0	1	9	6

Here 7-2=5; because 4>2, we write 4. 12-4=8; because 2=2 and 6<9, we write 8; and write 0 in the following place. 9-6=3; because 8>3, we write 2. 13-8=5; 5=5; 1=1; 8>6; so under 13-8 we write 4, with 9's in the two next places. 16-8=8; because 0<2, we write 8. 2-0=2; 1=1; 4=4; 1<3; so under 2-0 we write 2, followed by 0's. 3-1=2; because 9=9, 8>4, we write 1, with 9 in the next place. 14-8=6, which we write as the last figure.

#### EXERCISES.

The preceding exercises in addition will serve as exercises in subtraction by subtracting each line from that above or below it. The student should be able to subtract with equal facility whether the minuend is written above or below the subtrahend.

Mental addition and subtraction. When an expert computer has to add or subtract two logarithms, as in forming a product or quotient of two quantities, he does not necessarily write both of them, but prefers to write the first and, taking the other mentally, add (or subtract) each figure in order from left to right, and write down the sum (or difference). He thus saves the time spent in writing one number, and, sometimes, the inconvenience of writing it where there is not sufficient room for it.

This process of inverted addition is most useful in adding the proportional part in taking a logarithm from the table. It is then absolutely necessary to save the computer the trouble of copying both logarithm and proportional part.

Expert computers can add seven-figure logarithms in this way without trouble. But with those who do not desire to become experts it will be sufficient to learn to add two or three figures, so as to be able to take a five-figure or seven-figure logarithm from the table without writing anything but the result.

#### 11. Imperfections of Logarithmic Calculations.

Nearly all practical computations with logarithms are affected by certain sources of error, arising from the omission of decimals. It is important that these errors should be understood in order not only to avoid them so far as possible, but to avoid spending labor in aiming at a degree of accuracy beyond that of which the numbers admit.

Mathematical results may in general be divided into two classes: (1) those which are absolutely exact, and (2) those which are only to a greater or less degree approximate.

As an example of the former case, we have all operations upon entire numbers which involve only multiplication and division. For example, the equations

$$16^2 = 256$$

$$\frac{8^2}{6^2} = \frac{16}{9}$$

are absolutely exact.

But if we express the fraction  $\frac{1}{4}$  as a decimal fraction, we have  $\frac{1}{4} = .142857...$ , etc., ad infinitum.

Hence the representation of ‡ as a decimal fraction can never be absolutely exact. The amount of the error will depend upon how many decimals we include. If we use only two decimals we shall certainly be within one hundredth; if three, within one thousandth, etc. Hence the degree of accuracy to which we attain depends upon the number of decimals employed. By increasing the number of decimals we can attain to any degree of accuracy. As an example, it is shown in geometry that if the ratio of the circumference of a circle to its diameter be written to 35 places of decimals, the result will give the whole circumference of the visible universe without an error as great as the minutest length visible in the most powerful microscope.

There are no numbers, except the entire powers of 10, of which the logarithms can be exactly expressed in decimals. We must therefore omit all figures of the decimal beyond a certain limit. The number of decimals to be used in any case depends upon the degree of accuracy which is required. The large tables of logarithms contain seven decimal places, and therefore give results correct to the ten-millionth part of the unit. This is sufficiently near the truth in nearly all the applications of logarithms.

With five places of decimals our numbers will be correct to the hundred-thousandth part of a unit. This is sufficiently near for most practical applications.

Accumulation of errors. When a long computation is to be made, the small errors are liable to accumulate so that we cannot rely upon this degree of accuracy in the final result. The manner

in which the tables are arranged so as to reduce the error to a minimum may be shown as follows:

We have to seven places of decimals

 $\log 17 = 1.2304489$ " 18 = 1.2552725

When the tables give only five places of decimals the two last figures must be omitted. If the tables gave log 17=.23044, the logarithm would be too small by 89 units in the seventh place. It is therefore increased by a unit in the fifth place, and given .23045. This quantity is then too large by 11, and is therefore nearer the truth than the other. The nearest number being always given, we have the result:

Every logarithm in the table differs from the truth by not more than one half a unit of the last place of decimals.

Since the error may range anywhere from zero to half a unit, and is as likely to have one value as another between those limits, we conclude:

The average error of the logarithms in the tables is one fourth of a unit of the last place of decimals.

Errors in interpolation. When we interpolate the logarithm we add to the tabular logarithm another quantity, the proportional part, which may also be in error by half a unit, but of which the average error will only be one fourth of a unit.

As most logarithms have to be interpolated, the general result will be:

An interpolated logarithm may possibly be in error by a unit in the last place of decimals.

The sum of the average errors will, however, be only half a unit. But these errors may cancel each other, one being too large and the other too small. The theory of probabilities shows that, in consequence of this probable cancellation of errors, the average error only increases as the square root of the number of erroneous units added.

The square root of 2 is 1.41.

If, therefore, we add two quantities each affected with a probable error  $\pm$  .25, the result will be, for the probable error of the sum,

$$1.41 \times .25 = 0.35$$
.

We therefore conclude:

The average error of a logarithm derived from the table by interpolation is 0.35 of a unit of the last place.

Applying the above rule of the square root to the case in which

several logarithms are added or subtracted to form a quotient, we find the results of the following table:

No. of logs	s added or subtracted.	Average error.
	1	0.35
	2	0.50
	3	0.63
	4	0.72
	5	0.81
-	6	0.88
	7	0.95
	8	1.02
	9	1.08
	10	1.14

From this table we see that if we form the continued product of eight factors, by adding their logarithms the average error of the sum of the logarithms will be more than a unit in the last place.

As an example of the accumulation of errors, let us form the product 11.13.

We have from the table

$$\log 11 = 1.04139$$
" 13 = 1.11394
log product, 2.15533

We see that this is less than the given logarithm of the product.

143 by a unit of the fifth order. But if we use seven decimals we have

log 11, 1.041 392 7

Comparing this with the computation to five places, we see the source of the error.

If the numbers with which we enter the tables are affected by errors, these errors will of course increase the possible errors of the logarithms.

In determining to what degree of accuracy to carry our results, we have the following practical rule:

It is never worth while to carry our decimals beyond the limit of precision given by the tables, which limit may be a considerable fraction of the unit in the last figure of the tables.

Let us have a logarithm to five places of decimals, 1.92949, of which we require the corresponding number. Entering the table, we

perceive that the corresponding number is between 85.01 and 85.02 If this logarithm is the result of adding a number of logarithms, each of which may be in error in the way pointed out, we may suppose it probably affected by an error of half a unit in the last figure and possibly by an error of a whole unit or more. That is, its true value may be anywhere between 92 948 and 92 950.

The number corresponding to the former value is 85.012, and that corresponding to the latter 85.016. Since the numbers may fall anywhere between these limits, we assign to it a mean value of 85.014, which value, however, may be in error by two units in the last place. It is not, therefore, worth while to carry the interpolation

further and to write more than five digits.

Next suppose the logarithm to be 2.02170. Entering the table, we find in the same way that the number probably lies between the limits 105.121 and 105.126. There is therefore an uncertainty of five units in the sixth place, or half a unit in the fifth place. If the greatest precision is desired, we should write 105.124. But our last figure being doubtful by two or three units, the question might arise whether it were worth while to write it at all. As a general rule, if the sixth figure is required to be exact, we must use a six- or seven-place table of logarithms.

Still, near the beginning of the table, the probable error will be diminished by writing the sixth figure.

Now knowing that at the beginning of the table a difference of one unit in the number makes a change ten times as great in the logarithm as at the end of the table, we reach the conclusions:

In taking out a number in the first part of the table, it can never be worth while to write more than six significant figures, and very little is added to the precision by writing more than five.

In the latter part of the table it is never worth while to write more than five significant figures.

Sometimes no greater accuracy is required than can be gained by using four-figure logarithms. There is then no need of writing the last figure. If, however the printed logarithm is used without change, the fourth figure must be increased by unity whenever the fifth figure exceeds 5. When the fifth figure is exactly 5, the increase should or should not be made according as the 5 is too small or too great. To show how the case should be decided, a stroke is printed above the 5 when it is too great. In these cases the fourth figure should be used as it stands, but, when there is no stroke, it should be increased by unity.

# 12. Applications of Logarithms to the Computation of Annuities and Accumulations of Funds at Compound Interest.

One of the most useful applications of logarithms is to fiscal calculations, in which the value of moneys accumulating for long periods at compound interest is required.

Compound interest is gained by any fund on which the interest is collected at stated intervals and put out at interest.

As an example, suppose that \$10000 is put out at 6 per cent interest, and the interest collected semi-annually and put out at the same rate. The principal will then grow as follows:

Principal at starting	
Amount at end of 6 months  Interest on this amount = 3 per cent	
Amount at end of 1 year	
Amount at end of $1\frac{1}{2}$ years	
Amount at end of 2 years	\$11 255.09

Although in business practice interest is commonly payable semiannually, it is in calculations of this kind commonly supposed to be collected and re-invested only at the end of each year. This makes the computation more simple, and gives results nearer to those obtained in practice, because a company cannot generally invest its income immediately. If it had to wait three months to invest each semi-annual instalment of interest collected, the general result would be about the same as if it collected interest only once a year and invested it immediately.

If r be the rate per cent per annum, the annual rate of increase will be  $\frac{r}{100}$ . Let us put

- $\rho$ , the annual rate of increase  $=\frac{r}{100}$ ;
- p, the amount at interest at the beginning of the time, or the principal;
  - a, the amount at the end of one or more years.

 $a = p (1 + \rho)^n. \tag{1}$ 

To compute by logarithms, let us take the logarithms of both members. We then have

 $\log a = \log p + n \log (1+\rho). \tag{2}$ 

Example. Find the amount of \$1250 for 30 years at 6 per cent per annum.

Here ho = .06 1 + 
ho = 1.06  $\log (1 + 
ho) = 0.025\,306$  (end of Table I.)  $n \log (1 + 
ho), \overline{0.759\,18}$   $\log p, \overline{3.096\,91}$   $\log a, \overline{3.856\,09}$ a, \$7179.50 = required amount.

#### EXERCISES.

- 1. Find the amount of \$100 for 100 years at 5 per cent compound interest.
- 2. A man bequeathed the sum of \$500 to accumulate at 4 per cent interest for 80 years after his death. After that time the annual interest was to be applied to the support of a student in Harvard College. What would be the income from the scholarship?
- 3. If the sum of one cent had been put out at 3 per cent per annum at the Christian era, and accumulated until the year 1800, what would then have been the amount, and the annual interest on this amount?

It is only requisite to give three significant figures, followed by the necessary number of zeros.

4. Solve by logarithms the problem of the horseshoeing, in which a man agrees to pay 1 cent for the first nail, 2 for the second, and so on, doubling the amount for every nail for 32 nails in all.

Note. It is only necessary to compute the amount for the 32d nail, because it is easy to see that the amount paid for each nail is 1 cent more than for all the preceding ones.

- 5. A man lays aside \$1000 as a marriage-portion for his new-born daughter, and invests it so as to accumulate at 8 per cent compound interest. The daughter is married at the age of 25. What does the portion amount to?
- 6. A man of 30 pays \$2000 in full for a \$5000 policy of insurance on his life. Dying at the age of 80, his heirs receive \$7000, policy and dividends. If the money was worth 4 per cent to him, how much have the heirs gained or lost by the investment?
- 7. What would have been the answer to the previous question, had the man died at the age of 40, and the amount paid been \$6000?

Other applications of the formulæ. By means of the equations (1) and (2) we may obtain any one of the four quantities  $a, p, \rho$ , and n when the other three are given.

CASE I. Given the principal, rate of interest, and time, to find the amount.

This case is that just solved.

CASE II. Given the amount, time, and rate per cent, to find the principal.

Solution. Equation (1) gives

$$p = \frac{a}{(1+\rho)^n}.$$

Taking the logarithms,

$$\log p = \log a - n \log (1 + \rho),$$

by which the computation may be made.

CASE III. Given the principal, amount, and time, to find the rate. Solution. Equation (2) gives

$$\log (1+\rho) = \frac{\log a - \log p}{n} = \frac{1}{n} \log \frac{a}{p}.$$

Example. A man wants a principal of \$600 to amount to \$1000 in 10 years. At what rate of interest must be invest it?

Solution. 
$$\log a = 3.000\ 00$$

$$\log p = 2.778\ 15$$

$$\log \frac{a}{p} = 0.221\ 85$$

$$\frac{1}{10} \log \frac{a}{p} = 0.022\ 185 = \log (1 + \rho).$$

Hence, from last page of logarithms,

$$1 + \rho = 1.05241;$$
  
rate = 5.241,

and

or 54 per cent, nearly.

#### EXERCISES.

1. At what rate of interest will money double itself every ten years?

Ans. 7.177.

2. At what rate will it treble itself every 15 years? Ans. 7.599.

- 3. A man having invested \$1000, with all the interest it yielded him, for 25 years, finds that it amounts to \$3386. What was the rate of interest?

  Ans. 5 per cent.
- 4. A life company issued to a man of 20 a paid-up policy for \$10,000, the single premium charged being \$3150. If he dies at the age of 60, at what rate must the company invest its money to make itself good?

  Ans. 2.93 per cent.
- 5. A man who can gain 4 per cent interest wants to invest such a sum that it shall amount to \$5000 when his daughter, now 5 years old, attains the age of 20. How much must he invest? Ans. \$2776.62.
- 6. How much must a man leave in order that it may amount to \$1,000,000 in 500 years at  $2\frac{1}{2}$  per cent interest? Ans. \$4.36\frac{1}{2}
- 7. How much if the time is 1000 years, the rate being still  $2\frac{1}{2}$  per cent, and the amount \$1,000,000? Ans. 0.0019 of a cent.
- 8. A man finds that his investment has increased fivefold in 25 years. What is the average rate of interest he has gained?

Ans. 6.65.

9. An endowment of \$7500 is payable to a man when he attains the age of 65. What is its value when he is 45, supposing the rate of interest to be 4 per cent?

Ans. \$3423.

## 13. Accumulation of an Annuity.

It is often necessary to ascertain the present or future value of a series of equal annual payments. Thus it is very common to pay a constant annual premium for a policy of life insurance. The value of such a series of payments at any epoch is found by reducing the value of each one to the epoch, allowing for interest, and taking the sum. Supposing the epoch to be the present time, the problem may be stated as follows:

A man agrees to pay p dollars a year for n years, the first payment being due in one year, and the total number of payments n. What is the present value of all n payments?

Putting, as before,  $\rho = \frac{\text{rate of interest}}{100}$ , the present value of p dollars payable after y years will, by § 12, Case II., be

$$\frac{p}{(1+\rho)^y}$$
.

Putting in succession, y = 1, y = 2, ... y = n, the sum of the present values is

$$\frac{p}{1+\rho} + \frac{p}{(1+\rho)^2} + \frac{p}{(1+\rho)^3} + \cdots + \frac{p}{(1+\rho)^n}.$$

This is a geometrical progression in which

First term = 
$$\frac{p}{1+\rho}$$
;  
Common ratio =  $\frac{1}{1+\rho}$ ;

Number of terms = n.

By College Algebra, § 212, the sum of this progression will be

$$\Sigma_{1} = \frac{p}{1+\rho} \cdot \frac{1 - \left(\frac{1}{1+\rho}\right)^{n}}{1 - \frac{1}{1+\rho}} = p \frac{(1+\rho)^{n} - 1}{(1+\rho)^{n+1} - (1+\rho)^{n}} \\
= \frac{p}{(1+\rho)^{n}} \cdot \frac{(1+\rho)^{n} - 1}{\rho} \tag{1}$$

If the first payment is to be made immediately, instead of at the end of a year, the last or nth payment will be due in n-1 years, and the progression will be

$$p + \frac{p}{1+\rho} + \frac{p}{(1+\rho)^2} + \cdots + \frac{p}{(1+\rho)^{n-1}}$$

We find the sum of the geometric progression to be

$$\Sigma_{\bullet} = p \frac{(1+\rho)^n - 1}{(1+\rho)^n - (1+\rho)^{n-1}}.$$
 (2)

#### EXERCISES.

1. What is the present value of 15 annual payments of \$85 each, of which the first is due in one year, the rate being 5 per cent?

We find by substitution

Present value = 
$$85 \frac{1.05^{15} - 1}{1.05^{15} - 1.05^{15}} = \frac{85}{1.05^{15}} \cdot \frac{1.05^{15} - 1}{.05}$$
  
=  $\frac{1700 (1.05^{15} - 1)}{(1.05)^{15}}$ .  
log 1.05, 0.021 189 1.05<sup>15</sup>, 2.078 95  
15 1.05<sup>15</sup> - 1, 1.078 95  
log 1.05<sup>15</sup>, 0.317 84 log, 0.033 00  
co-log 1.05<sup>15</sup>, 9.682 16  
log 1700, 3.230 45  
Value, \$882.28 log value, 2.945 61

- 2. The same thing being supposed, what would be the present value if the rate of interest were 4 per cent?

  Ans. \$945.80
- 3. What is the present value of 25 annual payments of \$1000 each, the first due immediately, if the rate of interest is 3 per cent?

  Ans. \$17.935
- 4. A debtor owing \$10,000 wishes to pay it in 10 equal annual instalments, the first being payable immediately. If the rate of interest is 6 per cent, how much should each payment be?

Ans. \$1281.76.

Note. This problem is the reverse of the given one, since, in the equation (2), we have given  $\Sigma_2 = 10\,000$ ,  $\rho = 0.06$ , and n = 10, to find p.

5. The same thing being supposed, what should be the annual payment in case the payments should begin in a year?

Ans. \$1358.69.

Perpetual annuities. If the rate of interest were zero, the present value of an infinity of future payments would be infinite. But with any rate of interest, however small, it will be finite. For if, in the first equation (1), we suppose n infinite,  $\left(\frac{1}{1+\rho}\right)^n$  will converge toward zero, and we shall have

$$\Sigma = \frac{p}{(1+\rho)\left(1-\frac{1}{1+\rho}\right)} = \frac{p}{\rho}.$$
 (3)

This result admits of being put into a concise form, thus:

Since  $\Sigma$  is the present value of the perpetual annuity p, the annual interest on this value will be  $\rho\Sigma$ . But the equation (3) gives

 $\rho \Sigma = p$ .

Hence:

The present value of a perpetual annuity is the sum of which the annuity is the annual interest.

Example. If the rate of interest were  $3\frac{1}{2}$  per cent, the present value of a perpetual annuity of \$70 would be \$2000.

#### EXERCISES.

1. A government owing a perpetual annuity of \$1000 wishes to pay it off by 10 equal annual payments. If the rate of interest is 4 per cent, what should be the amount of each payment?

Ans. \$3082.30.

2. A government bond of \$100 is due in 15 years with interest at 6 per cent. The market rate of interest having meanwhile fallen to 3½ per cent, what should be the value of the bond?

Note. We find, separately, the present value of the 15 annual instalments

of interest, and of the principal.

## TABLE II.

## MATHEMATICAL CONSTANTS.

14. In this table is given a collection of constant quantities which frequently occur in computation, with their logarithms.

The logarithms are given to more than five decimals, in order to be useful when greater accuracy is required. When used in five-place computations, the figures following the fifth decimal are to be dropped, and the fifth decimal is to be increased by unity in case the figure next following is 5 or any greater one.

## TABLES III. AND IV.

## LOGARITHMS OF TRIGONOMETRIC FUNCTIONS.

15. By means of these tables the logarithms of the six trigonometric functions of any angle may be found.

The logarithm of the function instead of the function itself is given, because the latter is nearly always used as a factor.

We begin by explaining Table IV., because Table III. is used only in some special cases where Table IV. is not convenient.

I. Angles less than 45°. If the angle of which a function is sought is less than 45°, we seek the number of degrees at the top of the table and the minutes in the left-hand column. Then in the line opposite these minutes we find successively the sine, the tangent, the cotangent, and the cosine of the angle, as given at the heading of the page.

Example.  $\log \sin 31^{\circ} 27' = 9.717 47;$   $\log \tan 31^{\circ} 27' = 9.786 47;$   $\log \cot 31^{\circ} 27' = 0.213 53;$   $\cos 31^{\circ} 27' = 9.931 00.$ 

The sine, tangent, and cosine of this angle being all less than unity, the true mantissæ of the logarithm are negative; they are therefore increased by 10, on the system already explained.

If the secant or cosecant of an angle is required, it can be found by taking the arithmetical complement of the cosine or sine. It is shown in trigonometry that

$$secant = \frac{1}{cosine},$$

and

cosecant = 
$$\frac{1}{\text{sine}}$$
.

Therefore  $\log \operatorname{secant} = 0 - \log \operatorname{cosine} = \operatorname{co-log cosine}$ ;  $\log \operatorname{cosec} = 0 - \log \operatorname{sine} = \operatorname{co-log sine}$ .

We thus find

 $\log \sec 31^{\circ} 27' = 0.06900;$ 

 $\log \csc 31^{\circ} 27' = 0.28253.$ 

After each column, upon intermediate lines, is given the differ-

ence between every two consecutive logarithms, in order to facilitate interpolation.

In the case of tangent and cotangent, only one column of differences is necessary for both functions.

If we use no fractional parts of minutes, no interpolation is . necessary; but if decimals of a minute are employed, we can interpolate precisely as in taking out the logarithms of numbers.

Where the differences are very small they are sometimes omitted. Tables of proportional parts are given in the margin, the use of

which is similar to those given with the logarithms of numbers.

Example 1. To find the log sin of 31° 27'.7.

We have from the tables,  $\log \sin 31^{\circ} 27' = 9.71747$ Under diff. 20, P.P. for 7,

 $\log \sin 31^{\circ} 27'.7 = 9.71761$ 

To find log cot 15° 44'.34. Ex. 2.

> The tables give  $\log \cot 15^{\circ} 44' = 0.55019$ Under diff. 48, opposite 0.3, P.P., - 14.4 " 0.4 ÷ 10, - 1.9

log cot 15° 44′.34, 0.550 03

Since the tabular quantity diminishes as the angle increases, the proportional parts are subtractive.

#### EXERCISES.

Find from the tables:

- 1. log cot 43° 29'.3;
- 2. log tan 43° 29'.3;
- 3. log cos 27° 10'.6;
- 4. log sin 27° 10'.6;
- 5. log tan 12° 9'.43;
- log cot 12° 9'.43. 6.

In the case of sines and tangents of small angles the differences vary so rapidly that in most cases the exact difference will not be found in the table of proportional parts. In this case, if the proportional parts are made use of, a double interpolation will generally be necessary to find the fraction of a minute corresponding to a given sine or tangent. If only tenths of minutes are used, an expert computer will find it as easy to multiply or divide mentally as to refer to the table.

II. Angles between 45° and 90°. It is shown in trigonometry that if we compute the values of the trigonometric functions for the

first 45°, we have those for the whole circle by properly exchanging them in the different parts of the circle. First, if we have

$$\alpha + \beta = 90$$
,

then  $\alpha$  and  $\beta$  are complementary functions, and

 $\sin \beta = \cos \alpha;$  $\tan \beta = \cot \alpha.$ 

Therefore if our angle is between 45° and 90°, we may find its complement. Entering the table with this complement, the complementary function will then be the required function of the angle.

Example. To find the sine of  $67^{\circ}$  23', we may enter the table with  $22^{\circ}$  37' (=  $90^{\circ}$  -  $67^{\circ}$  23') and take out the cosine of  $22^{\circ}$  37', which is the required sine of  $67^{\circ}$  23.

To save the trouble of doing this, the complementary angles and the complementary denominations of the functions are given at the bottom of the page.

The minutes corresponding to the degrees at the bottom are given on the right hand. Therefore:

To find the trigonometric functions corresponding to an angle between 45° and 90°, we take the degrees at the bottom of the page and the minutes in the right-hand column. The values of the four functions log sine, log tangent, log cotangent, and log cosine, as read at the bottom of the page, are then found in the same line as the minutes.

Example 1. For 52° 59' we find

log sin = 9.902 25; log tan = 0.122 62; log cot = 9.877 38; log cos = 9.779 63.

Ex. 2. To find the trigonometric functions of 77° 17'.28.

#### EXERCISES.

Find the logarithms of the six functions of the following angles:

III. When the angle exceeds 90°.

Rule. Subtract from the angle the greatest multiple of 90° which it contains.

If this multiple is 180°, enter the table with the excess of the angle over 180° and take out the functions required, as if this excess were itself the angle.

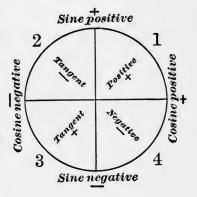
If the multiple is 90° or 270°, take out the complementary function to that required.

By then assigning the proper algebraic sign, as shown in trigonometry, the complete values of the function will be obtained.

The computer should be able to assign the proper algebraic sign according to the quadrant, without burdening his memory with

the special rules necessary in each case. This he can do by carrying in his mind's eye the following scheme. He should have at command the arrangement of the four quadrants as usually represented in trigonometry, so as to know, when an angle is stated, where it will fall relatively to the horizontal and vertical lines through the centre of the circle. Then, in the case of—

Sine or cosecant. If the angle is above the horizontal line (which



it is between 0° and 180°), the sine is positive; if below, negative.

Cosine or secant. If the angle is to the right of the vertical central line (as it is in the first and fourth quadrants), the cosine and secant are positive; if to the left (as in the second and third quadrants), negative.

Tangent or cotangent. Through the opposite first and third quadrants, positive; through the opposite second and fourth quadrants, negative.

Example 1. To find the tangent and cosine of 122° 44'. Subtracting 90°, we enter the table with 32° 44' and find

log cot 
$$32^{\circ} 44' = 0.191 92$$
;  
log sin  $32^{\circ} 44' = 9.732 98$ .

'Inerefore, writing the algebraic sign before the logarithm, we have

$$\log \tan 122^{\circ} 44' = -0.191 92;$$
  
 $\log \cos 122^{\circ} 44' = -9.732 98.$ 

Ex. 2. To find the sine and cotangent of 322° 58'.

Entering the table with  $52^{\circ} 58' = 322^{\circ} 58' - 270^{\circ}$ , and taking out the complementary functions, we find

 $\log \sin 322^{\circ} 58' = -9.779 80;$  $\log \cot 322^{\circ} 58' = -0.122 36.$ 

Ex. 3. To find the sine and tangent of 253° 5'.

Entering with 73° 5', we take out the sine and tangent, finding

 $\log \sin 253^{\circ} 5' = -9.89079;$  $\log \tan 253^{\circ} 5' = +0.51693.$ 

Ex. 4. To find the six trigonometric functions of  $152^{\circ}$  38'. We have

#### EXERCISES.

Find the six trigonometric functions of the following angles:

276° 29'.3; 66° 0'.5; 96° 59'.8; 252° 20'.3; 318° 10'.7; - 25° 22'.2; -155° 30'.7.

## 16. Method of Writing the Algebraic Signs.

As logarithms are used in computation, they may always be considered positive. It is true that the logarithms of numbers less than unity are in reality negative, but, for convenience in calculation, we increase them by 10, so as to make them positive.

The number corresponding to a given logarithm may, in computation, be positive or negative. There are two ways of distinguishing the algebraic sign of the number, between which the computer may choose for himself.

I. Write the algebraic sign of the number before the logarithm. As usually interpreted, the algebraic sign written thus would apply to the logarithm, which it does not. It is therefore necessary for the

computer to bear in mind that the sign belongs, not to the logarithm, as written, but to the number.

II. Write the letter n after the logarithm when the number is negative. This plan is theoretically the best, but, should the computer accidentally omit the letter, the number will be treated as positive, and a mistake will be made. It therefore requires vigilance on his part. An improvement would be to write a letter not likely to be mistaken for n, s for instance, after all positive logarithms.

# 17. To Find the Angle Corresponding to a Given Trigonometric Function.

Disregarding algebraic signs, there will always be four angles corresponding to each function, one in each quadrant. These angles will be:

The smallest angle, as found in the table;

This angle increased by 180°;

The complementary angle increased by 90°;

The complementary angle increased by 270°.

For instance, for the angle of which log tan is 0.611 92, we find 76° 16'. But we should get this same tangent for 103° 44', 256° 16', and 283° 44'.

Of the four functions corresponding to the four angles, two will always be positive and two negative; so that, in reality, there will only be two angles corresponding to a function of which both the sign and the absolute value are given. These values are found by selecting from the four possible ones the two for which the functions have the given algebraic sign. After selecting them, they may be checked by the following theorems, which are easily deduced from the relations between the values of each function as given in trigonometry:

The sum of the two angles corresponding to the same sine is  $180^{\circ}$  or  $540^{\circ}$ .

The sum of the two angles corresponding to the same cosine is  $360^{\circ}$ .

The difference of the two angles corresponding to the same tangent is 180°.

Which of the two possible angles is to be chosen depends upon the conditions of the problem or the nature of the figure to which the angle belongs. If neither the conditions nor the figure decide the question, the problem is essentially ambiguous, and either a both angles are to be taken.

#### EXERCISES.

Find the pairs of values of the angle  $\alpha$  from the following values of the trigonometric functions:

```
1. \log \sin \alpha = +9.90243;
                                     12. \log \sec \alpha = +0.22106;
 2. \log \sin \alpha = -9.90243;
                                     13. \log \sec \alpha = -0.22106;
 3. \log \cos \alpha = +9.90243;
                                     14. \log \sec \alpha = -0.09920;
4. \log \cos \alpha = -9.90243;
                                     15. \log \sec \alpha = +0.12346;
5. \log \tan \alpha = + 0.14316;
                                     16. \log \sin \alpha = + 8.99030;
                                     17. \log \sin \alpha = -8.99030;
6. \log \tan \alpha = -0.14316;
7. \log \cot \alpha = +0.14316;
                                     18. \log \cos \alpha = +9.21867;
8. \log \cot \alpha = -0.14316;
                                     19. \log \cos \alpha = -9.21867;
                                     20. \log \tan \alpha = -9.13690;
 9. \log \tan \alpha = -9.02481;
10. \log \tan \alpha = -0.97519;
                                     21. \log \tan \alpha = +9.13690;
                                     22. \log \cot \alpha = +9.13690.
11. \log \tan \alpha = +0.97519;
```

## 18. Cases when the Function is very Small or Great.

When the angle of which we are to find the functions approaches to zero, the logarithms of the sine, tangent, and cotangent vary so rapidly that their values to five figures cannot be readily interpolated. The same remark applies to the cosine, cotangent, and tangent of angles near 90° or 270°. The mode of proceeding in these cases will depend upon circumstances.

In the use of five-place logarithms, there is little advantage in carrying the computations beyond tenths of minutes, though the hundredths may be found when the tangent or cotangent is given. Where greater accuracy than this is required, six- or seven-place tables must be used.

If the angles are only carried to tenths of minutes, there is no necessity for taking out the sine, tangent, or cotangent to more than four decimals when the angle is less than 3°, and three decimals suffice for angles less than 30′. The reason is that this number of decimals then suffice to distinguish each tenth of minute.

When the decimals are thus curtailed, an expert computer will be able to perform the multiplication and division for the tenths or minutes mentally. If, however, this is inconvenient, the following rule may be applied.

To find the log sine or log tangent of an angle less than 2° to four places of decimals:

Rule. Enter the table of logarithms of numbers with the value

of the angle expressed in minutes and tenths, and take out the logarithm.

To this logarithm add the quantity 6.4637.

The sum will be the log sine, and the log tangent may be assumed to have the same value.

Example 1. To find log sin 1° 22'.6.

1° 22′.6 = 82′.6 log 82′.6 = 1.9170 constant, 6.4637

log sin 1° 22′.6, 8.3807

This rule is founded on the theorem that the sines and tangents of very small arcs may be regarded as equal to the arcs themselves. Since, in using the trigonometric functions, the radius of the circle is taken as unity, an arc must be expressed in terms of the unit radius when it is to be used in place of its sine or tangent. Now, it is shown in trigonometry that the unit radius is equal to 57°.2958 or 3437'.747 or 206 264".8. Hence we must divide the number of angular units in the angle by the corresponding one of these coefficients to obtain the length of the corresponding arcs in unit radius. Now,

 $\log 3437.747 = 3.5363$  $\operatorname{co-log}.....6.4637$ 

which may be added instead of subtracting the logarithm.

To find the cosine of an angle very near 90°, we find the sine of its complement, which will then be a very small angle, positive or negative.

## EXERCISES.

Find to four places of decimals:

1. log sin 22'.73;

2. log sin 1° 1'.12;

3. log cos 90° 0'.78;

4. log tan 88° 59'.35;

5. log cot 90° 28′.76;

6. log cos 89° 22'.23;

7. log sin 0° 0'.25.

If an angle corresponding to a given sine or tangent is required, the rule is:

From the given log sine or tangent subtract 6.4637 or add 3.5363. The result is the logarithm of the number of minutes.

Of course this rule applies only to angles less than 2°, in the value of which only tenths of minutes are required.

#### EXERCISES.

Find  $\alpha$  from:

1.  $\log \sin \alpha = 7.2243$ ; 3.  $\log \tan \alpha = -2.8816$ ;

2.  $\log \cot \alpha = 2.8816$ ; 4.  $\log \cos \alpha = 6.9218$ .

When the small angle is given in seconds. Although the computer may take out his angles to tenths of minutes, cases often arise in which a small angle is given in seconds, or degrees, minutes, and seconds, and in which the trigonometric function is required to five decimals. In this case the preceding method may not always give accurate results, because the arc and its sine or tangent may differ by a greater amount than the error we can admit in the computation.

Table III. is framed to meet this case. The following are the

quantities given:

In the second column: The argument, in degrees and minutes, as already explained for Table IV.

In the first column: This argument reduced to seconds. From this column the number of seconds in an arc of less than 2°, given in degrees, minutes, and seconds, may be found at sight.

Example. How many seconds in 1° 28′ 39″? In the table, before 1° 28′, we find 5280″, which being increased by 39″ gives 5319″, the

number required.

Col. 3. The logarithm of the sine of the angle. This is the same as in Table IV.

Col. 4. The value of log sine minus log arc; that is, the difference between the logarithm of the sine and the logarithm of the number of seconds in the angle.

Col. 5. The same quantity for the tangent.

Cols. 6 and 7. The complements of the preceding logarithms, distinguished by accents.

The use of the tables is as follows.

To find the sine or tangent of an angle less than 2°:

Express the angle in seconds by the first two columns of the table.

Write down the logarithm in column S or column T, according as the sine or a tangent is required.

Find from Table I. the logarithm of the number of seconds.

Adding this logarithm to S or T, the sum will be the log sine or log tangent.

Example. Find log sin 1° 2' 47".9.

S, 4.685 55

 $1^{\circ} 2' 47''.9 = 3767''.9; \log, 3.57610$ 

log sin 1° 2′ 47″.9, 8.261 65

To find the arc corresponding to a given sine or tangent:

Find in the column L. sin. the quantity next greater or next smaller than the given logarithm.

Take the corresponding value of S' or T' according as the given function is a sine or tangent, and add it to the given function.

The sum is the logarithm of the number of seconds in the required angle.

Example. Given log tan x = 8.40125, to find x.

 $\log \tan x$ , 8.401 25

T', 5.314 33

 $\log x$ , 3.71558

 $x = 5194''.9 = 1^{\circ} 26' 34''.9$ , from col. 2.

#### EXERCISES.

Find: 1.  $\log \sin 0^{\circ} 20' 20''.25;$ 

2. log tan 0° 0′ 1″.2273;

3. log sin 1° 59′ 22″.7;

4. log tan 1° 0′ 59″.7.

Find x from:

1.  $\log \tan x = 8.42796$ ;

2.  $\log \tan x = 7.42796$ ;

3.  $\log \tan x = 6.42796$ ;

4.  $\log \sin x = 5.35435$ ;

5.  $\log \sin x = 4.22619$ ;

6.  $\log \sin x = 8.54078$ .

When the cosine or cotangent of an angle near 90° or 270° is required, we take its difference from 90° or 270°, and find the complementary function by the above rules.

Remark. The use of the logarithms of the trigonometric functions is so much more extensive than that of the functions themselves that the prefix "log" is generally omitted before the designation of the logarithmic function, where no ambiguity will result from the omission.

## TABLE V.

## NATURAL SINES AND COSINES.

19. This table gives the actual numerical values of the sine and cosine for each minute of the quadrant.

To find the sine or cosine corresponding to a given angle less than 45°, we find the degrees at the top of a pair of columns and the minutes on the left.

In the two columns under the degrees and in the line of minutes we find first the sine and then the cosine, as shown at the head of the column.

A decimal point precedes the first printed figure in all cases, except where the printed value of the function is unity.

If the given angle is between 45° and 90°, find the degrees at the bottom and the minutes at the right.

Of the two numbers above the degrees, the right-hand one is the sine and the left-hand one the cosine.

For angles greater than 90° the functions are to be found according to the precepts given in the case of the logarithms of the sines and tangents.

## TABLE VI.

## ADDITION AND SUBTRACTION LOGARITHMS.

20. Addition and subtraction logarithms are used to solve the problem: Having given the logarithms of two numbers, to find the logarithm of the sum or difference of the numbers.

The problem can of course be solved by finding the numbers corresponding to the logarithms, adding or subtracting them, and taking out the logarithm of their sum or difference. The table under consideration enables the result to be obtained by an abbreviated process.

I. Use in addition. The principle on which the table is constructed may be seen by the following reasonings. Let us put

$$S = a + b$$
,

a and b being two numbers of which the logarithms are given. We shall have

$$S = a\left(1 + \frac{b}{a}\right) = a\left(1 + x\right);$$

putting, for clearness,  $x = \frac{b}{a}$ .

We then have

 $\log S = \log a + \log (1+x).$ 

Since  $\log a$  and  $\log b$  are both given, we can find  $\log x$  from the equation

 $\log x = \log b - \log a,$ 

which is therefore a known quantity.

Now, for every value of  $\log x$  there will be one definite value of each of the quantities x, 1+x, and  $\log (1+x)$ . Therefore a table may be constructed showing, for every value of  $\log x$ , the corresponding value of  $\log (1+x)$ .

Such a table is Table VI.

The argument, in column A, being  $\log x$ , the quantity B in the table is  $\log (1 + x)$ .

Example.  $\log 0.25 = 9.39794$ .

Entering the table with A = 9.39794, we find

B = 0.09691

which is the logarithm of 1.25.

Therefore, entering the table with  $\log x$  as the argument, we take out  $\log (1+x)$ , which added to  $\log a$  will give  $\log S$ .

We have therefore the following precept for using the table in addition:

Take the difference of the two given logarithms.

Enter the table with this difference as the argument A, and take out the quantity B.

Adding B to the subtracted logarithm, the sum will be the required

logarithm of the sum.

It is indifferent which logarithm is subtracted, but convenience in interpolating will be gained by subtracting the greater logarithm from the lesser increased by 10. The number B will then be added to the greater logarithm.

Example. Given  $\log m = 1.62974$ ,  $\log n = 2.20386$ ; find

 $\log (m+n)$ .

The required logarithm is found in either of the following two ways:

$$A = \log m \div n, \ 9.425 \ 88 \quad (3) \qquad \log n \div m, \ 0.574 \ 12 \quad (3)$$
$$\log (m+n), \ 2.306 \ 50 \quad (5) \qquad \log (m+n), \ 2.306 \ 50 \quad (5)$$

The figures in parentheses show the order in which the numbers are written.

#### EXERCISES.

Log a and log b having the following values, find log (a + b).

1. 
$$\log a = 1.70037$$
;  $\log b = 0.92169$ .

2. 
$$\log a = 0.62460$$
;  $\log b = 9.88126$ .

3. 
$$\log a = 9.79186$$
;  $\log b = 9.32209$ .

4. 
$$\log a = 1.60162$$
;  $\log b = 1.30606$ .

5. 
$$\log a = 0.79290$$
;  $\log b = 9.22127$ .

6. 
$$\log a = 0.60132$$
;  $\log b = 9.00168$ .

7. 
$$\log a = 4.79643$$
;  $\log b = 3.98186$ .

II. Use in subtraction. The problem is, having given  $\log a$  and  $\log b$ , to find the logarithm of

$$D = a - b.$$
We have 
$$D = b \left(\frac{a}{b} - 1\right);$$
whence 
$$\log D = \log b + \log \left(\frac{a}{b} - 1\right).$$

Since  $\log \frac{a}{b}$  is found by subtracting  $\log b$  from  $\log a$ , if we can find  $\log \left(\frac{a}{b}-1\right)$  from  $\log \frac{a}{b}$ , the problem will be solved.

From the construction of the table already explained, if we have

$$B = \log \frac{a}{h},$$

we must have

$$A = \log \left(\frac{a}{h} - 1\right).$$

We now have the following precept for subtraction:

Subtract the lesser of the given logarithms from the greater.

Enter the table so as to find the difference of the logarithms in the numbers B of the table.

Add the corresponding value of A to the lesser of the given logarithms. The sum will be the logarithm of the difference.

Example. Find  $\log (n-m)$  in the example of the preceding section.

$$\log n, 2.20386$$
 (1)

$$\log m$$
, 1.629 74 (2)

$$\log \frac{n}{m} = B, \ 0.574 \ 12 \quad (3)$$

$$\log (n-m), \overline{2.06919}$$
 (5)

#### EXERCISES.

Find the logarithms of the differences of the quantities a and b in the preceding section.

Remark. In the use of addition and subtraction logarithms, the precepts apply to numerical sums and differences, without respect to the algebraic signs of the quantities. For example, the algebraic difference between + 1473 and - 29 462 is to be found by addition, and the algebraic sum of a positive and negative quantity by subtraction.

Case where the quotient is large. Near the end of the table, A and B become nearly equal; the structure of the table is therefore changed so as to simplify its use. It is evident that if b is very small compared with a, the logarithms of a + b and a - b will not differ much from the logarithm of a itself. Hence, in this case, we shall have smaller numbers to use if we can find the quantity which must be added to  $\log a$  to give  $\log (a + b)$ , or subtracted from

 $\log a$  to give  $\log (a - b)$ . Now, the equations already written give, when a > b,  $\log a = \log b + A$ ,

$$\log (a+b) = \log b + B;$$

whence, by subtraction,

$$\log\left(a+b\right)-\log a=B-A,$$

or  $\log (a+b) = \log a + B - A$ . (with Arg. A)

We find in the same way,

$$\log (a - b) = \log a - (B - A)$$
. (with Arg. B)

Now, whenever  $\log a - \log b$  is greater than 1.65, we shall find it more convenient to take out B - A from the table than either A or B. We notice that the last two figures of B in this part of the table vary slowly, and we need only attend to them in interpolating. For instance, in the horizontal line corresponding to A = 1.66 we find:

for 
$$A=1.660\ 00; \quad B=1.669\ 40; \quad B-A=.009\ 40; \\ .661\ 00; \quad .670\ 38; \quad .009\ 38; \\ .662\ 00; \quad .671\ 36; \quad .009\ 36; \\ .663\ 00; \quad .672\ 33; \quad .009\ 33; \\ .664\ 00; \quad .673\ 31; \quad .009\ 31; \\ .665\ 00; \quad .674\ 29; \quad .009\ 29; \\ etc. \quad etc. \quad etc.$$

The interpolation of B-A is now very easy whether the quantity given is A or B. We note that B-A has but three significant figures, of which the first is found in column zero, and the other two are the last two figures of B as printed.

As an example, let us find  $\log (a + b)$  from

$$\log a = 2.791 63 \log b = 1.128 19$$

$$A = \overline{1.66344}$$

Entering the table with this value of A, we find by column 0 that B-A falls between .009 40 and .009 19. Following the horizontal line A=1.66 to column 3 and interpolating the last two figures between 33 and 31 for .44, with the difference -2, we find

$$B - A = .00932$$

Then

$$\log a = 2.791 63$$
$$\log (a + b) = 2.800 95$$

Next, if  $\log (a - b)$  is required, we have to find the difference 1.663 44 in the part B of the table. We find in the table:

for 
$$B = 1.66255$$
;  $B - A = .00955$ ;  
for  $B = 1.66353$ ;  $B - A = .00953$ .

Therefore

for 
$$B = 1.66344$$
;  $B - A = .00953$ .

Subtracting this from  $\log a$ , we have

$$\log (a - b) = 2.782 \, 10.$$

#### EXERCISES.

Find  $\log (a + b)$  and  $\log (a - b)$  from:

8. 
$$\log a = 0.36702$$
;  $\log b = 8.46283$ .

9. 
$$\log a = 0.00126$$
;  $\log b = 8.32907$ .

10. 
$$\log a = 2.06923$$
;  $\log b = 0.11085$ .

11. 
$$\log a = 5.80735$$
;  $\log b = 3.83809$ .

For values of A and B greater than 2.00, the table is so arranged that no interpolation at all is necessary. The computer has only to find what value of A or B given in the table comes *nearest* his value of  $\log a - \log b$  and take the corresponding value of B - A. He must remember that column A is to be entered for addition, and B for subtraction.

In this part of the table A and B are given to fewer than five decimals; because five decimals are not necessary to give B-A with accuracy. The nearer the end of the table is approached, the fewer the decimals necessary in taking the difference.

Example. Find  $\log (a + b)$  and  $\log (a - b)$  from

$$\log a = 1.26532$$

$$\log b = 9.22230$$

$$\log a - \log b, 2.04302$$

Entering column A with this difference, we find the nearest tabular value of A to be 2.0425, to which corresponds  $B-A=.003\,92$ . Hence

$$\log (a + b) = 1.26532 + .00392 = 1.26924.$$

Entering column B with the same difference, we find B - A = .00395; whence

$$\log (a - b) = 1.26532 - .00395 = 1.26137.$$

#### EXERCISES.

Find  $\log (a + b)$  and  $\log (a - b)$  from:

1. 
$$\log a = 4.06905$$
;  $\log b = 2.00132$ .

2. 
$$\log a = 3.92693$$
;  $\log b = 1.20159$ .

3. 
$$\log \alpha = 3.06164$$
;  $\log b = 0.12615$ .

4. 
$$\log a = 1.220$$
 68;  $\log b = 7.321$  56.

5. 
$$\log a = 0.69317$$
;  $\log b = 6.01023$ .

6. 
$$\log a = 2.30620$$
;  $\log b = 7.02301$ .

Case of nearly equal numbers. Near the beginning of the table the reverse is true: it is not possible to find A with accuracy to five places of decimals. But here the value of A taken from the tables, though it be found to only two, three, or four places of decimals, will give as accurate a result as the computation of a and b to five places will admit of. Let us suppose, for example, that we have to find  $\log (a - b)$  from

 $\log a = 9.883 15$   $\log b = 9.882 96$  B = 0.000 19 A = 6.64 - 10;  $\log (a - b) = 6.52 - 10.$ 

We find

whence

We note that the value of A may be 6.63 or 6.65 as well as 6.64, so that the result cannot be carried beyond two decimals. To show that these two are as accurate as the work admits of, we find the natural numbers a and b from Table I.

a = 0.76410 b = 0.76377 a - b = 0.00033

Since a-b has but two significant figures, and the first of these is less than 5, two figures in the logarithm are all that can be accurate.

## TABLE VII.

## SQUARES OF NUMBERS.

21. By means of this table the square of any number less than 1000 may be found at sight, and that of any number less than 10000 by a simple and easy interpolation.

The first page gives the squares of the first 100 numbers, which it is often convenient to have by themselves.

On the second and third pages (98 and 99) the hundreds of the number to be squared are found at the tops of the several columns, and the tens and units in the left-hand column. The first three or four figures of the square are in the column under the hundreds, and opposite the tens and units, and the last two figures on the right of the page after the column 9 +

Examples. The square of 634 is 401 956;

" 329 " 108 241;

" 265 " 70 225;

" 153 " 23 409;

" 999 " 998 001.

The same table may be used for any number of three significant figures by attention to the position of the decimal-point. Thus:

$$51100^{2} = 2611210000;$$

$$511^{2} = 261121;$$

$$51.1^{2} = 2611.21;$$

$$5.11^{2} = 26.1121;$$

$$0.511^{2} = 0.261121.$$

When there are four significant figures, an interpolation may be executed in several ways. If n be the nearest number the square of which is found in the table, and h the excess of the given number over this, so that n + h is the number whose square is required, we shall have

 $(n+h)^2 = n^2 + 2nh + h^2 = n^2 + h(2n+h)$ =  $n^2 + h(N+n)$ ;

where N = n + h, the given number.

We may therefore find the square of 257.4 in the following way:

$$\begin{array}{r}
257^{2} = 66\,049 \\
514.4 \times .4 = 205.76 \\
(257.4)^{2} = 66\,254.76
\end{array}$$

To find the square of 9037 we proceed thus:

$$\begin{array}{rrr} 9037 \\ 9030^{\circ} & = 81\,540\,900 \\ \hline 18067 \times 7 & = 126\,469 \\ \mathbf{9}037^{\circ} & = 81\,667\,369 \end{array}$$

In many cases only one more figure will be required in the square than in the given number. The square can then be interpolated with all required accuracy by the differences, the last two figures of which are found in the last column of the table, while the remaining figures are found by taking the difference between two consecutive numbers in the principal column.

To return to the last example, we find the difference between 257<sup>2</sup> and 258<sup>2</sup> to be 515, the first figure being the difference between 660 and 665, and the last two, 15, in the last column. Then

$$257^{2} = 66\ 049$$

$$515 \times 0.4 = 206$$

$$(257.4)^{2} = 66\ 255$$

-which is correct to the nearest unit.

It will be remarked that the two methods are substantially the same when only five figures are sought in the result. The substantial identity rests upon the general theorem that

The difference of the squares of two consecutive numbers is equal to the sum of the numbers.

We prove this theorem thus:

$$(n+1)^2 - n^2 = 2n + 1 = n + (n+1).$$

When the tabular difference is taken in the way already described, it will often happen that the difference between the numbers in the columns of hundreds is to be diminished by unity. Thus, although 4173-4160=13, the difference between  $645^{\circ}$  and  $646^{\circ}$  is not 1391, but 1291. These cases are noted by the asterisk after the number in the last column.

The squares of numbers of more than four figures may be found in the same way, but in such cases it will generally be easier to use logarithms than the table of squares.

## TABLE VIII.

# TO CONVERT HOURS, MINUTES, AND SECONDS INTO DECIMALS OF A DAY, AND VICE VERSA.

22. The familiar method of solving this problem is to convert the seconds into decimals of a minute, and the minutes into decimals of an hour, by dividing by 60, and then the hours into decimals of a day by dividing by 24. The reverse problem is solved by multiplying by 24, 60, and 60.

Table VIII. enables us to perform these operations without division. Column D gives each hundredth of a day, but its numbers may also be regarded as ten thousandths or millionths of a day, according to which of the following three columns is used. In column H.M.S. are found the hours, minutes, and seconds corresponding to these hundredths. In the next column is one hundredth of column H.M.S., or the minutes and seconds in the number of ten thousandths of a

day in column D. Finally, column  $\frac{H.M.S.}{100^2}$  shows the number of seconds in the number of millionths of a day found in column D.

Example. To convert 0d.532 946 into hours, minutes, and seconds.

It will be seen that we divide the figures of the given decimal of a day into pairs, and enter the three columns of time with these three pairs in succession.

If seven decimals are given, we may interpolate the last number, as in taking out a logarithm.

Example. Convert 
$$0^{d}.050\ 762\ 7$$
.

 $0^{d}.05 = 1^{h}\ 12^{m}\ 0^{s}$ 
 $.000\ 7 = 1^{m}\ 0^{s}.48$ 
 $.000\ 062 = 5^{s}.36$ 
 $.000\ 000\ 7 = .7 \times .08 = 0^{s}.06$ 
 $1^{h}\ 13^{m}\ 5^{s}.90$ 

In practice the computer will perform the interpolation mentally, adding  $.7 \times .08 = .06$  to the number 5.36 of the table in his head, and writing down  $5^{\circ}.42$  as the last quantity to be added.

#### EXERCISES.

Convert into hours, minutes, and seconds:

1. 04.203 079 2;

2. 0d.783 605 8;

3. 0d.010 203 4;

4. 0d, 990 990 9.

To use the table for the reverse operation, we proceed as in the following example:

It is required to convert 17h 29m 30s.93 into decimals of a day. Looking in the table, we find that the required decimal is between 0.72 and 0.73. Hence the first two figures are 0.72, the equivalent of 17h 16m 48s. Subtracting the lat-17h 29m 30s, 93 ter from the given number, we 0.72 = 17h 16m 48s have a remainder 12m 42\*.93, to be 12m 42\*.93 .0088 sought for in column  $\frac{H.M.S.}{100}$ . 12m 40s,32 This .0000302 =gives 88 as the next two figures. Subtracting the equivalent of .0088 or 12m 40\*.32, we have left 2\*.61, which we are to seek in  $\frac{H.M.S.}{100^{2}}$ . We find the corresponding number of column D to be 302. Hence

 $17^{\text{h}} 29^{\text{m}} 30^{\text{s}}.93 = 0^{\text{d}}.7288302.$ 

In solving this problem the computer should be able, after a little practice, to perform the subtractions and carry the remainders mentally, thus saving himself the trouble of writing down the numbers.

#### EXERCISES.

Take the answers obtained from the four preceding exercises, subtract each result from 24<sup>h</sup> 0<sup>m</sup> 0<sup>e</sup>, change the remainder to decimals of a day, and see if when added to the decimals of the preceding exercises the sum is 1<sup>d</sup>.000 000 0, as it should be.

## TABLE IX.

## TO CONVERT TIME INTO ARC, AND VICE VERSA.

23. In astronomy the right ascensions of the heavenly bodies are commonly given in hours, minutes, and seconds, the circumference being divided into 24 hours, each hour into 60 minutes, and each minute into 60 seconds.

Since 360' = one circumference, we have  $1^h = 15^\circ;$   $1^m = 15';$   $1^* = 15';$ 

the signs b, m, and o indicating hours, minutes, and seconds of time.

Hence we may change time into arc by multiplying by 15, and arc into time by dividing by 15, the denominations being changed in each case. Table IX. enables us to do this by simple addition and subtraction by a process similar to that employed in changing hours, minutes, and seconds into decimals of a day.

To turn time into arc, we find in the table the whole number of degrees contained in the time denomination next smaller than the given one, and subtract the former time denomination from the latter.

Next we find the minutes of arc corresponding to the given time next smaller than the remainder, and again subtract.

Lastly we interpolate the seconds corresponding to the second remainder.

Example. Change  $15^{h}$   $29^{m}$   $46^{\circ}.24$  to are.

Given time,  $15^{h}$   $29^{m}$   $46^{\circ}.24$ The table gives  $232^{\circ} = 15^{h}$   $28^{m}$ Remainder,  $1^{m}$   $46^{\circ}.24$ The table gives  $26' = 1^{m}$   $1^{m}$   $44^{\circ}$ Remainder,  $2^{\circ}.24 = 33^{\circ}.6$ 

Hence

 $15^{\text{h}} 29^{\text{m}} 46^{\circ}.24 = 232^{\circ} 26' 33'.6.$ 

The computer should be able to go through this operation without writing down anything but the result.

The operation of changing arc into time is too simple to require description, but it is more necessary to write down the work.

#### EXERCISES.

Change the following times to arc, and then check the results by changing the arcs into time and seeing whether the original times are reproduced:

- 1. 7<sup>h</sup> 29<sup>m</sup> 17<sup>s</sup>.86;
- 2. 0h 4m 0s.25;
- 3. 12h 4m 0s.25;
- 4. 13h 48m 16s.40;
- 5. 19h 7m 59s.92.

## TABLE X.

## TO CONVERT MEAN TIME INTO SIDEREAL TIME, AND SIDEREAL INTO MEAN TIME.

24. Since 365½ solar days = 366½ sidereal days (very nearly), any period expressed in mean time may be changed to sidereal time by increasing it by its  $\frac{1}{365.25}$  part, and an interval of sidereal time may be changed to mean time by diminishing it by its  $\frac{1}{366.25}$  part.

The first part of the table gives, for each 10 minutes of the argument, its  $\frac{1}{365.25}$  part, by which it is to be increased. The second part of the table gives the  $\frac{1}{366.25}$  part of the argument.

The small table in the margin shows the change for periods of less than 10 minutes.

Example 1. To change 17<sup>h</sup> 48<sup>m</sup> 36<sup>s</sup>.7 of mean time to sidereal time.

Given mean time, 17<sup>h</sup> 48<sup>m</sup> 36<sup>s</sup>.70 Corr. for 17<sup>h</sup> 40<sup>m</sup>, 2<sup>m</sup> 54<sup>s</sup>.13 Corr. for 8<sup>m</sup> 37<sup>s</sup>, 1<sup>s</sup>.41 Sidereal time, 17<sup>h</sup> 51<sup>m</sup> 32<sup>s</sup>.24

Ex. 2. To change this interval of sidereal time back to mean time.

Corr. for  $17^h$   $50^m$ ,  $-2^m$   $55^s.29$ Corr. for  $1^m$   $32^s$ ,  $-2^m$   $55^s.54$ Sidereal time,  $17^h$   $51^m$   $32^s.24$ Mean time,  $17^h$   $48^m$   $36^s.70$ 

#### EXERCISES.

Change to sidereal time:

1. 3<sup>h</sup> 42<sup>m</sup> 36<sup>s</sup>.5 m. t.; 3. 22<sup>h</sup> 3<sup>m</sup> 5<sup>s</sup>.61 m. t. 2. 18<sup>h</sup> 46<sup>m</sup> 29<sup>s</sup>.82 " 4. 0<sup>h</sup> 1<sup>m</sup> 12<sup>s</sup>.55 "

Change to mean time:

5. 0h 7m 16s.3 sidereal time; 6. 22h 17m 29s.65

# OF DIFFERENCES AND INTERPOLATION.\*

## 25. General Principles.

We call to mind that the object of a mathematical table is to enable one to find the value of a function corresponding to any value whatever of the variable argument. Since it is impossible to tabulate the function for all values of the argument, we have to construct the table for certain special values only, which values are generally equidistant. For example, in the tables of sines and cosines in the present work the values of the functions are given for values of the argument differing from each other by one minute.

The process of finding the values of functions corresponding to values of the argument intermediate between those given is called interpolation.

We have already had numerous examples of interpolation in its most simple form; we have now to consider the subject in a more general and extended way.

In the first place, we remark that, in strictness, no process of interpolation can be applicable to all cases whatever. From the mere facts that

To the number 2 corresponds the logarithm 0.301 03, "" " 0.477 12,

we are not justified in drawing any conclusion whatever respecting the logarithms of numbers between 2 and 3. Hence some one or more hypotheses are always necessary as the base of any system of interpolation. The hypotheses always adopted are these two:

- 1. That, supposing the argument to vary uniformly, the function varies according to some regular law.
- 2. That this law may be learned from the values of the function given in the table.

These hypotheses are applied in the process of differencing, the

<sup>\*</sup> The study of this subject will be facilitated by first mastering so much of it as is contained in the author's College Algebra, §§ 299-302.

It is also recommended to the beginner in the subject that, before going over the algebraic developments, he practise the methods of computation according to the rules and formulæ, so as to have a clear practical understanding of the notation. He can then more readily work out the developments.

nature of which will be seen by the following example, where it is applied to the logarithms of the numbers from 30 to 37:

	Function.	$\Delta'$	∆''	4'''	⊿i▼
log 30.	1.477 12	1424			
" 31.	1.491 36	1379	- 45	1.0	
<b>~~</b> 32.			- 43	+ 2	+2
<b>"</b> 33.		1336	- 39	+ 4	<del>-</del> 3
" 34.		1297	-38	+1	+1
<b>"</b> 35.	-1 344 07	1259	- 36	+ 2	+1
<b>~~</b> 36.		1223	- 33	+ 3	
··· 37.	1.56820 +	1190			

The column  $\Delta'$  gives each difference between two consecutive values of the function, formed by subtracting each number from that next following. These differences are called *first differences*.

The column  $\Delta''$  gives the difference between each two consecutive first differences. These are called second differences.

In like manner the numbers in the succeeding columns, when written, are called third differences, fourth differences, etc.

Now if, in continuing the successive orders of differences, we find them to continually become smaller and smaller, or to converge toward zero, this fact shows that the values of the functions follow a regular law, and the first hypothesis is therefore applicable.

In order to apply interpolation we must then assume that the intermediate values of the function follow the same law. The truth of this assumption must be established in some way before we can interpolate with mathematical rigor, but in practice we may suppose it true in the absence of any reason to the contrary.

26. Effect of errors in the values of the functions. In the preceding example it will be noticed that if we continue the orders of differences beyond the fourth, they will begin to increase and become irregular. This arises from the imperfections of the logarithms, owing to the omission of decimals beyond the fifth, already described in § 11.

When we find the differences to become thus irregular, we must be able to judge whether this irregularity arises from actual errors in the original numbers, which ought to be corrected, or from the small errors necessarily arising from the omission of decimals.

The great advantage of differencing is that any error, however small, in the quantities differenced, unless it follows a regular law, will be detected by the differences. To show the reason of this, we investigate what effect errors in the given functions will have upon the successive orders of differences. THEOREM. The differences of the sum of two quantities are equal to the sums of their differences.

General proof. Let

 $f_1$ ,  $f_2$ ,  $f_3$ , etc., be one set of functions;  $f_1'$ ,  $f_2'$ ,  $f_3'$ , etc., another set.

 $f_1 + f_1'$ ,  $f_2 + f_2'$ ,  $f_3 + f_3'$ , etc., will then be their sums.

In the first of the following columns we place the first differences of f, in the second those of f', and in the third those of f+f', each formed according to the rule:

It will be seen that the quantities in the third column are the sums of those in the first two.

#### NUMERICAL EXAMPLE.

$f \qquad \Delta'$	$f' = \Delta'$	$f+f'$ $\Delta'$
$\frac{14}{25} + 25$	$\frac{1}{2} + 2$	$\frac{15}{12} + 27$
$\frac{39}{50} + 11$	$\frac{3}{6} + \frac{3}{3}$	$\frac{42}{56} + 14$
$     \begin{array}{r}                                     $	$egin{array}{c} rac{1}{3} + 2 \\ 6 + 3 \\ 10 + 4 \end{array}$	$     \begin{array}{r}       15 \\       42 \\       42 \\       56 \\       9     \end{array}     + 14 $

We see that the third set of values of  $\Delta'$  follow the theorem.

Because the second differences are the differences of the first, the third the differences of the second, etc., it follows that the theorem is true for differences of any order.

Now when we write a series of functions in which the decimals exceeding a certain order are omitted, we may conceive each written number to be composed of the algebraic sum of two quantities, namely:

- 1. The true mathematical value of the function.
- 2. The negative of the omitted decimals.

Example. In the preceding collection of logarithms, since the true value of log 30 is 1.477 121 3..., we may conceive the quantity written to be

$$1.47712 = \log 30 - .0000013...$$

Hence the differences actually written are the differences of the true logarithms minus the differences of the errors. Now suppose the errors to be alternately + 0.5 and - 0.5 = the point marking off the last decimal. Their differences will then be as follows:

It is evident that the *n*th order of differences of the errors are equal to  $\pm 2^{n-1}$ . Hence, in this case, if the *n*th order of differences of the true values of the function were zero, still, in consequence of the omission of decimals, the actual differences of the *n*th order would be  $2^{n-1}$ .

This, however, is a very extreme case, since it is beyond all probability that the errors should alternate in this way. A more probable average example will be obtained by supposing a single number to have an error of 0.5, while the others are correct. We shall then have:

In this case the maximum value of the difference of the nth order is 1.5 in the differences of the third order, 3 in those of the fourth, 5 in those of the fifth, etc. Its general expression is

$$\frac{1}{2}\frac{n(n-1)(n-2)\ldots(n-s+1)}{1\cdot 2\cdot 3\cdot \ldots s},$$

where n is the order of differences, and

$$s = \frac{n}{2} \text{ or } \frac{n-1}{2}$$

according as n is even or odd. Thus:

$$\Delta' = \frac{1}{2};$$

$$\Delta'' = \frac{1}{2} \cdot \frac{2}{1} = 1;$$

$$\Delta''' = \frac{1}{2} \cdot \frac{3}{1} = 1.5;$$

$$\Delta^{1v} = \frac{1}{2} \cdot \frac{4 \cdot 3}{1 \cdot 2} = 3;$$

$$\Delta^{v} = \frac{1}{2} \cdot \frac{5 \cdot 4}{1 \cdot 2} = 5;$$
etc.
etc.

This being about the average case, in actual practice the differences may be two or three times as great without necessarily implying an error greater than 0.5 in the numbers written.

We have now the following general rule for judging whether a series of numbers do really follow a uniform law:

Difference the series until we reach an order of differences in which the + and - signs either alternate or follow each other irregularly.

If none of the differences of this order expressed in units of the last place of decimals exceed the limit

$$\frac{n(n-1)\ldots(n-s+1)}{1\cdot 2\cdot 3\cdot \ldots s}$$

—that is, the value of the largest binomial coefficient of the nth order the given numbers may be assumed to follow a regular law, and therefore to be correct to a unit in the last figure.

If some differences exceed this limit, their quotient by the above binomial coefficient may be considered to show the maximum error with which the number opposite it is probably affected.

We can thus detect an isolated error in a series of numbers with great certainty. Suppose, for example, an error of 2 in some number of the series. Differencing the series 0, 0, 0, 2, 0, 0, 0, we shall find the four largest differences of the fifth order to be -10, +20, -20, +10, which would enable us to hit at once upon the erroneous number and judge of the magnitude of its error.

An error near the beginning and end of the series of numbers of which the differences are taken cannot be detected by the differences unless it is considerable. If, for instance, the first or last number is in error by 1, the error of each order of differences will only be 1, as we may easily see by the following example:

It is only in those differences which are on or near the same line as the numbers which are magnified in the way we have shown. But at the beginning and end of the series we cannot determine these differences.

Examining the various tables of differences, we see that n numbers have n-1 first differences, n-2 second differences, and so on, the number diminishing by 1 with each succeeding order. Hence, unless the number of given functions exceeds the index expressing the order of differences which we have to form, no certain conclusion can be drawn.

What is here said of the correctness of the numbers when the differences run properly must be understood as applicable to isolated errors only. If all the numbers were subject to an error following a regular law, this error would not be detected by the differences because, from the nature of the case, the latter only show deviations from some regular law.

# 27. Fundamental Formulæ of Interpolation.

We suppose a series of numbers to be differenced in the way already shown, and the various differences to be designated as in the following scheme, which is supposed to be a selection from a series preceding and following it.

It will be seen that the lower indices are chosen so as to show on which line a difference of any order falls. Thus all quantities with index 2 are on one horizontal line, those with index  $\frac{5}{2} = 2\frac{1}{2}$  are half a line below, etc. This notation is a little different from that used in algebra, but the change need not cause any confusion.

It is shown in algebra that if n be any index, we have

$$u_{n} = u_{0} + n\Delta'_{1} + \frac{n(n-1)}{1.2}\Delta''_{1} + \frac{n(n-1)(n-2)}{1.2.3}\Delta'''_{2} + \text{etc.}; \qquad (a)$$

the notation being changed as in the preceding scheme.

Now the fundamental hypothesis of interpolation is that this formula, which can be demonstrated only for integral values of n, is true also for fractional values; that is, for values of the function u between those given in the table or in the above scheme. We therefore suppose this formula to express the value of the function u for any value of n between 0 and 1.

For values between +1 and +2 we have only to increase the indices of u and its differences by unity, thus:

$$u_{1+n} = u_1 + n\Delta'_1 + \frac{n(n-1)}{1 \cdot 2}\Delta''_1 + \text{etc,},$$

and by supposing n to increase from 0 to 1 in this formula we shall have values of u from  $u_1$  to  $u_2$ .

Increasing the indices again—that is, applying our general formulæ to a row of quantities one line lower—we shall have

$$u_{2+n} = u_1 + n\Delta'_{\frac{1}{2}} + \frac{n(n-1)}{1 \cdot 2}\Delta''_{\frac{1}{2}} + \text{etc.}$$

The equation (a) is known as Newton's formula of interpolation.

## 28. Transformations of the Formula of Interpolation.

In the equation (a) and those following it, the formula of interpolation is not in its most convenient form. We shall therefore transform it so that the differences employed shall be symmetrical with respect to the functions between which the interpolation is to be made.

In working these transformations we shall suppose the sixth and following orders of differences to be so small as not to affect the result. These differences being supposed zero, any two consecutive fifth differences may be supposed equal.

First transformation. Let us first find what the original formula (a) will become when, instead of using the series of differences

 $\Delta'_{1}$ ,  $\Delta''_{1}$ ,  $\Delta'''_{2}$ ,  $\Delta^{iv}_{2}$ , etc.,

we use

$$\Delta'_1$$
,  $\Delta''_2$ ,  $\Delta'''_1$ ,  $\Delta^{iv}_2$ , etc.

To effect the transformation we must find the values of the first series of differences in terms of the second, and substitute them in the formula (a).

We find, by the mode of forming the differences,

$$\Delta''_{i} = \Delta''_{0} + \Delta'''_{i}; 
\Delta'''_{i} = \Delta'''_{i} + \Delta^{1v}_{i}; 
= \Delta'''_{i} + \Delta^{1v}_{0} + \Delta^{v}_{i}; 
\Delta^{1v}_{0} = \Delta^{1v}_{0} + \Delta^{v}_{i} + \Delta^{v}_{i};$$

for which, because we suppose the values of  $\Delta^{\mathsf{v}}$  to be equal, we may put

$$\Delta^{iv}_{2} = \Delta^{iv}_{0} + 2\Delta^{v}_{1};$$
  
$$\Delta^{v}_{2} = \Delta^{v}_{1}.$$

Making these substitutions in (a), we have

$$u_{n} = u_{0} + n\Delta'_{1} + \frac{n(n-1)}{1 \cdot 2} (\Delta''_{0} + \Delta'''_{1})$$

$$+ \frac{n(n-1)(n-2)}{1 \cdot 2 \cdot 3} (\Delta'''_{1} + \Delta^{iv}_{0} + \Delta^{v}_{1})$$

$$+ \frac{n(n-1)(n-2)(n-3)}{1 \cdot 2 \cdot 3 \cdot 4} (\Delta^{iv}_{0} + 2\Delta^{v}_{1})$$

$$+ \frac{n(n-1) \cdot \dots \cdot (n-4)}{1 \cdot 2 \cdot 3 \cdot 4 \cdot 5} \Delta^{v}_{1}.$$

Reducing by collecting the coefficients of equal differences, we find

$$u_{n} - u_{o} = n\Delta'_{\frac{1}{4}} + \frac{n(n-1)}{1 \cdot 2} \Delta''_{o} + \frac{(n+1)n(n-1)}{1 \cdot 2 \cdot 3} \Delta'''_{\frac{1}{4}} + \frac{(n+1)n(n-1)(n-2)}{1 \cdot 2 \cdot 3 \cdot 4} \Delta^{iv}_{o} + \frac{(n+2)(n+1)n(n-1)(n-2)}{1 \cdot 2 \cdot 3 \cdot 4 \cdot 5} \Delta^{v}_{\frac{1}{4}}.$$
 (b)

Second transformation. Next, instead of the series of this last formula, (b),

$$\Delta'_{t}$$
,  $\Delta''_{o}$ ,  $\Delta'''_{t}$ ,  $\Delta^{iv}_{o}$ , etc.,

let us use

$$\Delta'_{-\frac{1}{2}}$$
,  $\Delta''_{\circ}$ ,  $\Delta'''_{-\frac{1}{2}}$ ,  $\Delta^{iv}_{\circ}$ , etc.

To effect this transformation we substitute in (b) for  $\Delta'_{\frac{1}{2}}$ ,  $\Delta''_{\frac{1}{2}}$ , etc.,

$$\Delta'_{\frac{1}{2}} = \Delta'_{-\frac{1}{2}} + \Delta''_{\circ};$$
  
 $\Delta'''_{\frac{1}{2}} = \Delta'''_{-\frac{1}{2}} + \Delta^{iv}_{\circ};$   
 $\Delta^{v}_{\frac{1}{2}} = \Delta^{v}_{-\frac{1}{2}}.$ 

The series (b) then changes into

$$u_{n} - u_{\bullet} = n\Delta'_{-\frac{1}{2}} + \frac{n(n+1)}{1 \cdot 2} \Delta''_{\bullet} + \frac{(n+1)n(n-1)}{1 \cdot 2 \cdot 3} \Delta'''_{-\frac{1}{2}} + \frac{(n+2)(n+1)n(n-1)}{1 \cdot 2 \cdot 3 \cdot 4} \Delta^{\frac{1}{2}} \cdot + \frac{(n+2)(n+1)n(n-1)(n-2)}{1 \cdot 2 \cdot 3 \cdot 4 \cdot 5} \Delta^{\frac{1}{2}} \cdot \cdot$$

$$(c)$$

Third transformation. Stirling's formula. We effect a third transformation by taking the half sum of the equations (b) and (c), which gives us a formula perfectly symmetrical with respect to the lines of differences, namely,

$$u_{n} - u_{o} = n \frac{\Delta'_{-\frac{1}{4}} + \Delta'_{\frac{1}{4}}}{2} + \frac{n^{2}}{2} \Delta''_{o} + \frac{n(n^{2} - 1)}{1 \cdot 2 \cdot 3} \frac{\Delta'''_{-\frac{1}{4}} + \Delta'''_{\frac{1}{4}}}{2} + \frac{n^{2}(n^{2} - 1)}{1 \cdot 2 \cdot 3 \cdot 4} \Delta^{1}_{o} + \frac{n(n^{2} - 1)(n^{2} - 4)}{1 \cdot 2 \cdot 3 \cdot 4 \cdot 5} \frac{\Delta^{v}_{-\frac{1}{4}} + \Delta^{v}_{\frac{1}{4}}}{2} + \text{etc.}, (d)$$

which is known as Stirling's formula of interpolation.

It will be seen that we have put

$$n^2 - 1$$
 for  $(n + 1)$   $(n - 1)$ ,  $n^3 - 4$  for  $(n + 2)$   $(n - 2)$ , etc.

Fourth transformation. In the equation (b), instead of the series of differences

$$\Delta'_{\frac{1}{2}}$$
,  $\Delta''_{\frac{1}{2}}$ ,  $\Delta'''_{\frac{1}{2}}$ ,  $\Delta^{iv}_{\frac{1}{2}}$ , etc.,

let us use

$$\Delta'_{\frac{1}{2}}$$
,  $\Delta''_{\frac{1}{2}}$ ,  $\Delta'''_{\frac{1}{2}}$ ,  $\Delta^{iv}_{\frac{1}{2}}$ , etc.

To effect this we put

$$\Delta''_{0} = \Delta''_{1} - \Delta'''_{\frac{1}{2}};$$
 $\Delta^{iv}_{0} = \Delta^{iv}_{1} - \Delta^{v}_{\frac{1}{2}}.$ 

Making these substitutions in (b), it becomes

$$u_{n} - u_{0} = n\Delta'_{\frac{1}{2}} + \frac{n(n-1)}{1.2}\Delta''_{1} + \frac{n(n-1)(n-2)}{1.2.3}\Delta'''_{\frac{1}{2}} + \frac{(n+1)n(n-1)(n-2)}{1.2.3.4}\Delta^{iv}_{1} + \frac{(n+1)n(n-1)(n-2)(n-3)}{1.2.3.4.5}\Delta^{v}_{\frac{1}{2}}.$$
 (e)

Fifth transformation. Bessel's formula. Let us take half the sum of the equations (e) and (b). We then have

$$u_{n} - u_{o} = n\Delta'_{\frac{1}{2}} + \frac{n(n-1)}{1 \cdot 2} \frac{\Delta''_{o} + \Delta''_{o}}{2} + \frac{n(n-1)(n-\frac{1}{2})}{1 \cdot 2 \cdot 3} \Delta'''_{\frac{1}{2}} + \frac{(n+1)n(n-1)(n-2)}{1 \cdot 2 \cdot 3 \cdot 4} \frac{\Delta^{iv}_{o} + \Delta^{iv}_{o}}{2} + \frac{(n+1)n(n-1)(n-2)(n-\frac{1}{2})}{1 \cdot 2 \cdot 3 \cdot 4 \cdot 5} \Delta^{v}_{\frac{1}{2}}, \quad (f)$$

which is commonly known as Bessel's formula of interpolation, and which is the one most convenient to use in practice.

In applying this formula to find a value of the function intermediate between two given values, we must always suppose the index 0 to apply to the given value next preceding that to be found, and the index 1 to apply to that next following. The quantity n will then be a positive proper fraction.

29. Example of interpolation to halves. If we increase the logarithms of 30, 31, etc., already given, by unity, we shall have the logarithms of 300, 310, 320, etc. It is required to find, by interpolation, the logarithms of the numbers half way between the given ones (omitting the first and last), namely, the logarithms of 315, 325, 335, etc.

Here, the required quantities depending upon arguments half way between the given ones, we have  $n = \frac{1}{2}$ , and the values of the Besselian coefficient, so far as wanted, are

$$\frac{n(n-1)}{2} = -\frac{1}{8};$$

$$\frac{n(n-1)(n-\frac{1}{2})}{6} = 0.$$

The subsequent terms are neglected, being insensible. So, if we put  $a_0$  and  $a_1$  for any consecutive two of the numbers 300, 310, etc., we have

$$\log (a_0 + 5) = \log a_0 + \left(\frac{1}{2}\Delta'_{\frac{1}{2}} - \frac{1}{8}\frac{\Delta''_0 + \Delta''_1}{2}\right)$$

$$\log (a_1 - 5) = \log a_1 - \left(\frac{1}{2}\Delta'_{\frac{1}{2}} + \frac{1}{8}\frac{\Delta''_0 + \Delta''_1}{2}\right),$$
(h)

where we put  $\Delta_{t}$  for that first difference between  $a_{0}$  and  $a_{1}$ .

and

These two formulæ are two expressions for the same quantity because  $a_0 + 5 = a_1 - 5$ . They are both used in such a way as to provide a check upon the accuracy of the work. For this purpose we compute the two quantities

$$\log (a_o + 5) - \log a_o = \frac{1}{2} \Delta'_{\frac{1}{2}} - \frac{1}{8} \frac{\Delta''_o + \Delta''_o}{2},$$

$$\log a_1 - \log (a_o + 5) = \frac{1}{2} \Delta'_{\frac{1}{2}} + \frac{1}{8} \frac{\Delta''_o + \Delta''_o}{2}.$$
(k)

The most convenient and expeditious way of doing the work is shown in the accompanying table, where we give every figure which it is necessary to write, besides those found on p. 57. The following is the plan of computation:

No. Log. Diff. 
$$\frac{1}{2} \mathcal{L}'_{\frac{1}{4}}$$
.  $\frac{1}{8} \frac{\mathcal{L}''_{\frac{0}{4}} + \mathcal{L}''_{\frac{1}{4}}}{2}$ .  $\frac{\mathcal{L}''_{\frac{0}{4}} + \mathcal{L}''_{\frac{0}{4}}}{2}$ .  $\frac{\mathcal{L}''_{\frac{0}{4}} + \mathcal{L}''_{\frac{0}{4}}}{2}}$ .  $\frac{\mathcal{L}''_{\frac{0$ 

We compute the right-hand column by the formula

$$\frac{\Delta''_{\circ} + \Delta''_{1}}{2} = \Delta''_{\circ} + \frac{1}{2}\Delta'''_{\frac{1}{2}} = \Delta''_{1} - \frac{1}{2}\Delta'''_{\frac{1}{2}},$$

using the values of  $\Delta$  given in the scheme, p. 57.

This mode of computing the half sum of two numbers which are nearly equal is easier than adding and dividing by 2.

In the next two columns to the left, the sixth place of decimals

is added in order that the errors may not accumulate by the addition of several quantities. This precaution should always be taken when the interpolated quantities are required to be as accurate as the given ones.

The fourth column from the right is formed by adding and subtracting the numbers of the second and third columns according to the formula (k). The additional figure is now dropped, because no longer necessary for accuracy. The numbers thus formed are the first differences of the series of logarithms found by inserting the interpolated logarithms between the given ones, as will be seen by equation (k).

We write the first logarithm of the series, namely,

$$\log 310 = 2.49136,$$

and then form the subsequent ones by continual addition of the differences, thus:

$$\log 315 = \log 310 + 695;$$
  
 $\log 320 = \log 315 + 684;$   
 $\log 325 = \log 320 + 673;$   
etc. etc. etc.

If the work is correct, the alternate logarithms will agree with the given ones in the former table.

The continuance of the above process for a few more numbers, say up to 450, is recommended to the student as an exercise.

**30.** Interpolation to thirds. Let us suppose the value of a quantity to be given for every third day, and the value for every day to be required. By putting  $n = \frac{1}{3}$  and applying formula (f) to each successive given quantity, we shall have the value for each day following one of those given, and by putting  $n = \frac{2}{3}$  we shall have values for the second day following, which will complete the series. But the interpolation can be executed by a much more expeditious process, which consists in computing the middle difference of the interpolated quantities and finding the intermediate differences by a secondary interpolation.

Let us put

 $f_0$ ,  $f_1$ ,  $f_2$ , etc., the given series of quantities;

 $f_0$ ,  $f_1$ ,  $f_2$ ,  $f_3$ ,  $f_4$ , etc., the required interpolated series;

 $\Delta'$ ,  $\Delta''$ , etc., the first differences, second differences, etc., of the given series;

6', 6", etc., the first differences, second differences, etc., of the

interpolated series.

We may then put

$$f_{\bullet} - f_{\bullet} = \Delta'_{\bullet}$$
 (in the given series);  
 $f_{\bullet} - f_{\bullet} = \delta'_{\bullet}$  (in the interpolated series).  
 $f_{\bullet} - f_{\bullet} = \delta'_{\bullet}$  (in the interpolated series).

We shall then have

$$\delta'_1 + \delta'_2 + \delta'_4 = \Delta'_4.$$

The value of  $f_1 - f_0 = \delta_1$  is given by putting  $n = \frac{1}{3}$  in the Besselian formula (f). Thus we find

$$\begin{split} \delta'_{i} &= \frac{1}{3} \varDelta'_{i} - \frac{1}{9} \frac{\varDelta''_{o} + \varDelta''_{1}}{2} + \frac{1}{162} \varDelta'''_{i} \\ &+ \frac{5}{243} \frac{\varDelta^{1}_{o} + \varDelta^{1}_{1}}{2} - \frac{1}{1458} \varDelta^{7}_{i}. \end{split}$$

Putting  $n = \frac{2}{3}$ , we have the value of  $f_{\bullet} - f_{\bullet}$ , that is, of  $\delta'_{\bullet} + \delta'_{\bullet}$ . Thus we find

$$\begin{split} \delta'_{1} + \delta'_{1} &= \frac{2}{3} \varDelta'_{1} - \frac{1}{9} \frac{\varDelta''_{0} + \varDelta''_{1}}{2} - \frac{1}{162} \varDelta'''_{1} \\ &+ \frac{5}{243} \frac{\varDelta^{\text{i}\text{v}}_{0} + \varDelta^{\text{i}\text{v}}_{1}}{2} + \frac{1}{1458} \varDelta^{\text{v}}_{1} \end{split}$$

Subtracting these expressions, we have

$$\delta'_{i} = \frac{1}{3} \Delta'_{i} - \frac{1}{81} \Delta'''_{i} + \frac{1}{729} \Delta^{v_{i}}$$

which is most easily computed in the form

$$\delta'_{\frac{1}{2}} = \frac{1}{3} \left\{ \Delta'_{\frac{1}{2}} - \frac{1}{27} \left( \Delta'''_{\frac{1}{2}} - \frac{1}{9} \Delta^{\mathsf{v}}_{\frac{1}{2}} \right) \right\}. \tag{m}$$

We see that the computation of  $\delta'_{i}$ , the middle difference of the interpolated quantities, is much simpler than that of  $\delta'_{i}$ . It will therefore facilitate the work to compute only these middle differences, and to find the others by interpolation.

This process is again facilitated, in case the second differences are considerable, by first computing the second differences of the interpolated series on the same plan. The formulæ for this purpose are derived as follows:

Let us put

$$\delta'_{\bar{i}} = f_{i} - f_{i}.$$

The second difference of which we desire the value is then

$$\delta''_{3} = \delta'_{\frac{1}{2}} - \delta'_{\frac{1}{2}}.$$

The value of &'s is given by the equation

$$\delta'_{i} = \Delta'_{i} - (\delta'_{i} + \delta'_{i}),$$

and the value of  $\delta'_{i}$  is found from that of  $\delta'_{i}$  by simply increasing the indices of the differences by unity, because it belongs to the next lower line.

We thus find

$$\delta'_{\frac{1}{2}} = \frac{1}{3} \Delta'_{\frac{1}{2}} - \frac{1}{9} \frac{\Delta''_{1} + \Delta''_{2}}{2} + \frac{1}{162} \Delta'''_{\frac{1}{2}}$$

$$+ \frac{5}{243} \frac{\Delta^{iv}_{1} + \Delta^{iv}_{2}}{2} - \frac{1}{1458} \Delta^{v}_{\frac{1}{2}};$$

$$\delta'_{\frac{1}{2}} = \frac{1}{3} \Delta'_{\frac{1}{2}} + \frac{1}{9} \frac{\Delta''_{0} + \Delta''_{1}}{2} + \frac{1}{162} \Delta'''_{\frac{1}{2}}$$

$$- \frac{5}{243} \frac{\Delta^{iv}_{0} + \Delta^{iv}_{1}}{2} - \frac{1}{1458} \Delta^{v}_{\frac{1}{2}}.$$

Then by subtraction,

$$\delta^{"}_{\bullet} = \frac{1}{3} (\Delta^{'}_{\bullet} - \Delta^{'}_{\bullet}) - \frac{1}{9} \frac{\Delta^{"}_{\circ} + 2\Delta^{"}_{\bullet} + \Delta^{"}_{2}}{2} + \frac{1}{162} (\Delta^{"'}_{\bullet} - \Delta^{"}_{\bullet}) + \frac{5}{243} \frac{\Delta^{!}_{\circ} + 2\Delta^{!}_{\bullet} + \Delta^{!}_{2}}{2} - \frac{1}{1458} (\Delta^{v}_{\bullet} - \Delta^{v}_{\bullet}).$$

Reducing the first of these terms, we have

$$\Delta'_{\frac{3}{2}} - \Delta'_{\frac{1}{2}} = \Delta''_{1}.$$

For the second term,

$$\Delta''_{0} = \Delta''_{1} - \Delta'''_{1};$$
  
 $\Delta''_{0} = \Delta''_{1} + \Delta'''_{1};$ 

whence

and

$$\Delta''_{0} + \Delta''_{2} = 2\Delta''_{1} + \Delta'''_{2} - \Delta'''_{1} = 2\Delta''_{1} + \Delta^{1}_{1},$$

$$\Delta''_{0} + 2\Delta''_{1} + \Delta''_{2} = 2\Delta''_{1} + \frac{1}{2}\Delta^{1}_{1},$$

For the third term,

$$\Delta^{\prime\prime\prime\prime}_3 - \Delta^{\prime\prime\prime\prime}_4 = \Delta^{1v}$$

For the fourth term, dropping the terms in  $\Delta^{vi}$  as too small in practice, we may put

 $\frac{\Delta^{\mathrm{i}\,\mathrm{v}}_{0} + 2\Delta^{\mathrm{i}\,\mathrm{v}}_{1} + \Delta^{\mathrm{i}\,\mathrm{v}}_{2}}{2} = 2\Delta^{\mathrm{i}\,\mathrm{v}}_{1}.$ 

The difference of the fifth terms may also be dropped, because they contain only sixth differences.

Making these substitutions in the value of  $\delta''$ , we find

$$\delta''_{,} = \frac{1}{3} \Delta''_{,} - \frac{1}{9} \left( 2\Delta''_{,} + \frac{1}{2} \Delta^{iv}_{,} \right) + \frac{1}{162} \Delta^{iv}_{,} + \frac{10}{243} \Delta^{iv}_{,}$$

$$= \frac{1}{9} \Delta''_{,} - \frac{2}{243} \Delta^{iv}_{,}$$

$$= \frac{1}{9} \left( \Delta^{\rho\rho}_{,} - \frac{2}{27} \Delta^{iv}_{,} \right). \qquad (n)$$

By this formula we may compute every third value of  $\delta''$ , and then interpolate the intermediate values. By means of these values we find by addition the intermediate values of  $\delta'$ , of which every third value has been computed by formula (m). Then, by continually adding the values of  $\delta'$ , we find those of the function f.

As an example of the work, we give the following values of the sun's declination for every third day of part of July, 1886, for Greenwich mean noon:

The values of  $\Delta^{iv}$  are too small to have any influence.

The whole work of interpolation is shown in the following table, where, as before, the right-hand column is that first computed, and gives the value of  $\Delta' - \frac{1}{27}\Delta'''$  according to formula (m):

Date.	⊙ 's .	Dec.	$\delta'$	$\delta^{\prime\prime}$	$\Delta' - \frac{1}{27}\Delta'''$
1886.	0 1	11	1 11	11	2 1
July 6			- 6 16.	$_{86} - 23.60$	
0	. 22 34 . 22 28	10.1	- 6 40.	29 - 25.45	- 20 0.87
9	. 22 20 . 22 21	$\frac{12.1}{8.5}$ -	- 7 3.4 - 7 26.1	$egin{array}{l} 56 & -23.27 \\ 66 & -23.10 \\ 59 & -22.93 \\ 37 & -22.78 \\ 98 & -22.61 \\ 40 & -23.42 \\ \hline \end{array}$	
10	. 22 13	41.9	- 7 26.0 - 7 <b>19</b> !	$\frac{66}{59} - 22.93$	- 23 28.77
11	. 22 5	52.3	- 8 12.3	$\frac{22.78}{37}$ - 22.78	- 20 20.11
13	. 21 49	39.9 - 4.9 -	- 8 34.9	$\frac{-22.61}{22.42}$	
14	. 21 40	7.5	- 8 57	$\frac{1}{50}$ - 22.19	-2652.21
15	. 21 30	47.9	- 0 10.0	-21.97	

To make the process in the example clear, the computed differences, etc., are printed in heavier type than the interpolated ones.

It is also to be remarked that the sum of the three consecutive values of  $\delta''$ , formed of one computed value and the interpolated values next above and below it, should be equal to the difference between the corresponding computed first differences. For instance,

$$23''.27 + 23''.10 + 22''.93 = 7' 49''.59 - 6' 40''.29$$
.

But in the first computation this condition will seldom be exactly fulfilled, owing to the errors arising from omitted decimals and other sources. If the given quantities are accurate, the errors should never exceed half a unit of the last decimal in the given quantities, or five units in the additional decimal added on in dividing.

To correct these little imperfections after the interpolation of the second differences, but before that of the first differences, the sum of the last two figures in each triplet of second differences should be formed, and if it does not agree with the difference of the first differences, the last figures of the second difference should each be slightly altered, to make the sum exact.

The first differences can then be formed by addition.

In the same way, the sum of three consecutive first differences should be equal to the difference between the given quantities. If, as is generally the case, this condition is not exactly fulfilled, the differences should be altered accordingly. This alteration may, however, be made mentally while adding to form the required interpolated functions.

As an exercise for the student we give the continuance of the sun's declination for the remainder of the month, to be interpolated for the intermediate dates from July 15th onward:

	0	,	"
July 21	<b>2</b> 0	27	16.5
24	19	<b>5</b> 0	49.1
27	19	11	22.7
<b>3</b> 0	18	29	4.8
Aug. 2	17	44	3.1

As another exercise the logarithms of the intermediate numbers from 998 to 1014 may be interpolated by the following table:

	_
Number.	Logarithm.
994	2.997 386 4
997	2.998 695 2
1000	3.000 000 0
1003	3.001 300 9
1006	3.002 598 0
1009	3.003 891 2
1012	3.005 180 5
1015	3.006 466 0
1018	3.0077478

32. Interpolation to fifths. Let us next investigate the formulæ when every fifth quantity is given and the intermediate ones are to be found by interpolation. By putting  $n = \frac{2}{5}$  in the Besselian formula, we shall have the value of the interpolation function second

following one of the given ones, and by putting  $n = \frac{3}{5}$  that third following. The difference will be the middle interpolated first difference of the interpolated series. Putting  $n = \frac{3}{5}$  in (f), we have

$$u_{1} = u_{c} + \frac{2}{5} \Delta'_{1} - \frac{2.3}{2.5^{2}} \frac{\Delta''_{0} + \Delta''_{1}}{2} + \frac{2.3.1}{2^{2} \cdot 3.5^{2}} \Delta'''_{1} + \frac{2.3.7.8}{2 \cdot 3.4.5^{4}} \frac{\Delta^{1}_{0} + \Delta^{1}_{1}}{2} - \frac{2.3.7.8.1}{2^{2} \cdot 3.4.5.5^{4}} \Delta^{1}_{1},$$

Putting  $n = \frac{3}{5}$ , we have

$$u_{\frac{3}{4}} = u_{0} + \frac{3}{5} \Delta'_{\frac{1}{4}} - \frac{2.3}{2.5^{2}} \frac{\Delta''_{0} + \Delta''_{1}}{2} - \frac{2.3.1}{2^{2}.3.5^{3}} \Delta'''_{\frac{1}{4}} + \frac{2.3.7.8}{2.3.4.5^{4}} \frac{\Delta^{1}_{0} + \Delta^{1}_{1}}{2} + \frac{8.3.2.7.1}{2^{2}.3.4.5.5^{4}} \Delta^{7}_{\frac{1}{4}}.$$

The difference of these expressions, being reduced, gives

$$u_{i} - u_{i} = \frac{1}{5} \Delta'_{i} - \frac{1}{125} \Delta'''_{i} + \frac{14}{15625} \Delta^{v}_{i}$$
$$= \frac{1}{5} \left\{ \Delta'_{i} - \frac{1}{25} \left( \Delta'''_{i} - \frac{14}{125} \Delta^{v}_{i} \right) \right\}.$$

The term in  $\Delta^v$  will not produce any effect unless the fifth differences are considerable, and then we may nearly always, in practice, put  $\frac{1}{4}$  instead of  $\frac{1}{125}$ .

The interpolated second differences opposite the given functions are most readily obtained by Stirling's formula, (d). Putting  $n = \frac{1}{4}$ , we have the following value of the interpolated first differences immediately following a given value of the function:

$$u_{\frac{1}{2}} - u_{0} = \frac{1}{5} \frac{\Delta'_{-\frac{1}{2}} + \Delta'_{\frac{1}{2}}}{2} + \frac{1}{50} \Delta''_{0} - \frac{24}{6.5.25} \frac{\Delta'''_{-\frac{1}{2}} + \Delta'''_{\frac{1}{2}}}{2} - \frac{24}{6.5.20.25} \Delta^{\frac{1}{2}} + \text{etc.}$$

Again, putting  $n = -\frac{1}{5}$ , and changing the signs, we find for the first difference next preceding a given function

$$u_{\bullet} - u_{-\frac{1}{8}} = \frac{1}{5} \frac{\Delta'_{-\frac{1}{8}} + \Delta'_{\frac{1}{8}}}{2} - \frac{1}{50} \Delta''_{\bullet} - \frac{24}{6.5.25} \frac{\Delta'''_{-\frac{1}{8}} + \Delta'''_{\frac{1}{8}}}{2} + \frac{24}{6.5.20.25} \Delta^{1}_{\bullet} - \text{etc.}$$

The difference of these quantities gives the required second difference, which we find to be

$$\delta''_{\bullet} = \frac{1}{25} \Delta''_{\bullet} - \frac{2}{625} \Delta^{iv}_{\bullet} = \frac{1}{25} \left( \Delta''_{\bullet} - \frac{2}{25} \Delta^{iv}_{\bullet} \right).$$

As an example and exercise we show the interpolation of logarithms when every fifth logarithm is given:

Number.	Logarithm.	$\delta'$	δ''	10	1"
1000	3.000 000 0	_	Ū		
1005	3.002 166 1	4319.2	- 4.32	+ 21 661	108
$\begin{array}{c} 1006 \\ 1007 \end{array}$	.0025980 $.0030295$	4314.9	-4.31 $-4.30$		
$\frac{1008}{1009}$	$.003\ 460\ 6$ $.003\ 891\ 2$	<b>4310.6</b> 4306.3	-4.30	+ 21 553	
1010	3.004 321 4	$4302.0 \\ 4297.7$	-4.29 $-4.28$		- 107
$\begin{array}{c} 1011 \\ 1012 \end{array}$	$.004\ 751\ 2$ $.005\ 180\ 5$	4293.5	-4.27 $-4.26$		
$1013 \\ 1014$	$.005\ 609\ 4$ $.006\ 037\ 9$	<b>4289.2</b> 4285.0	-4.23 $-4.20$	+ 21 446	
1015	3.0064660	4280.8	<b>- 4.16</b>	+ 21 342	- 104
1020	3.008 600 2			1 11 010	
$\begin{array}{c} 1025 \\ 1030 \end{array}$	3.0107239 $3.0128372$				
$1035 \\ 1040$	3.014 940 <b>3</b> 3.017 033 <b>3</b>	. 1			
1010	0.011 000 0				

## FORMULÆ

FOR THE SOLUTION OF

PLANE AND SPHERICAL TRIANGLES.

#### REMARKS.

1. It is better to determine an angle by its tangent than by its sine or cosine, because a small angle or an angle near 180° cannot be accurately determined by its cosine, nor one near either 90° or 270° by its sine.

Sometimes, however, the data of the problem are such that the angle can be determined only through its sine or cosine. Any uncertainty which may then arise from the source pointed out is then inherent in the problem; e.g., if the hypothenuse and one side of a right triangle are 0.39808 and 0.39806 respectively (sixth and following decimals being omitted), the value of the included angle may be anywhere between 0° 25′ and 0° 42′, no matter what method of computation be adopted.

2. If the sine and cosine can be independently computed, their agreement as to the angle will generally serve as a check on the accuracy of the computation. If they agree, their quotient will give

the tangent.

3. It is desirable, when possible, to have a check upon the accuracy of the computation; that is, to make a computation which must give a certain result if the work is right. But no check can give a positive assurance of accuracy: all it can do is to make it more or less improbable that a mistake exceeding a certain limit exists.

4. In the following list several formulæ are sometimes given as applicable to the same problem. In such cases, the most convenient

for the special purpose must be chosen.

**Notation.** a, b, and c are the three sides. A, B, and C are the opposite angles.

#### PLANE TRIANGLES.

Given.	Required.	$s = \frac{1}{2}(a+b+c).$
a, b, c,	A,	
the three sides.	one angle.	$\tan \frac{1}{2}A = \sqrt{\frac{(s-b)(s-c)}{s(s-a)}}.$
DIGOS.	A, B, C,	$-\sqrt{(s-a)(s-b)(s-c)}$
	all the	$H = \sqrt{\frac{(s-a)(s-b)(s-c)}{s}};$
	angles.	$\tan \frac{1}{2}A = \frac{H}{s-d}$
		$ \tan \frac{1}{2}B = \frac{H}{s - b}; $
		$\tan \frac{1}{2} C = \frac{H}{s-c}.$
		Checks: $A + B + C = 180^{\circ}$ ;
		$\frac{a}{\sin A} = \frac{b}{\sin B} = \frac{c}{\sin C}$
b, c, A,	B and $C$ ,	h - c
two sides	the other	$\tan \frac{1}{2}(B-C) = \frac{b-c}{b+c} \cot \frac{1}{2}A;$
and the included	angles.	$\frac{1}{2}(B+C) = 90^{\circ} - \frac{1}{2}A;$
angle.		$B = \frac{1}{2}(B+C) + \frac{1}{2}(B-C);$
8		$C = \frac{1}{2}(B+C) - \frac{1}{2}(B-C)$ . Check, as before.
	a, B, C,	$a \sin \frac{1}{2} (B - C) = (b - c) \cos \frac{1}{2} A;$
	the	$a\cos\frac{1}{2}(B-C) = (b+c)\sin\frac{1}{2}A.$
	remaining	Having found $a$ and $\frac{1}{2}(B-C)$ , proceed
	parts.	as in the last case.
a, b, A,	c, B, C,	$\sin B = \frac{b}{a} \sin A$ ; (two values of B.)
two sides and the	the re-	LC .
and the	maining parts.	$C = 180^{\circ} - (A + B);$
site one of	President	$c = \frac{b \sin C}{\sin B} = \frac{a \sin C}{\sin A}.$
them.		NAME OF TAXABLE PARTY.

Given.

a, A, B,
one side
and any
two angles.

Bequired.
b, c, C,
the remaining
parts.

$$c = \frac{a \sin B}{\sin A};$$

$$c = \frac{a \sin C}{\sin A} = \frac{a \sin (A + B)}{\sin A}.$$

#### RIGHT SPHERICAL TRIANGLES.

a, b, the sides containing the right angle.	A, B, or c.	c is the hypothenuse. $\cot A = \cot a \sin b;$ $\cot B = \cot b \sin a;$ $\cos c = \cos a \cos b;$ $\sin c = \frac{\sin a}{\sin A}.$
	A and $c$ .	$\sin c \sin A = \sin a;$ $\sin c \cos A = \cos a \sin b;$ $\cos c = \cos a \cos b.$
	$B \ { m and} \ c$	$\sin c \sin B = \sin b;$ $\sin c \cos B = \sin a \cos b.$
a, c, one side and the hy- pothenuse.		$\sin A = \frac{\sin a}{\sin c};$ $\cos B = \tan a \cot c;$ $\cos b = \frac{\cos c}{\cos a}.$
a, A, one side and the opposite	b, c, or B.	$\sin b = \tan a \cot A;$ $\sin c = \frac{\sin a}{\sin A};$ $\sin B = \frac{\cos A}{\cos a}.$
angle. $a$ , $B$ , one side and the adjacent	b, c, or A.	$\tan b = \sin a \tan B;$ $\tan c = \frac{\tan a}{\cos B};$ $\cos A = \cos a \sin B.$
angle.	c and A.	$\sin A \sin c = \sin a;$ $\sin A \cos c = \cos a \cos B;$ $\cos A = \cos a \sin B.$

Given.	Required.		
a, B.	b and A.	$\sin A \sin b = \sin a \sin B;$	
		$\sin A \cos b = \cos B.$	
c, A,	a, b,  or  B.	$\sin a = \sin \overline{c \sin A};$	
the hypo-	_	$\tan b = \tan c \cos A;$	
thenuse		$\cot B = \cos c  \tan A.$	
and one angle.	a and B.	$\cos a \sin B = \cos A;$ $\cos a \cos B = \sin A \cos c;$ $\sin a = \sin A \sin c.$	
	a and $b$ .	$\cos a \sin b = \cos A \sin c;$ $\cos a \cos b = \cos c.$	*
$\overline{A, B,}$ the two	a, b, or c.	$\cos a = \frac{\cos A}{\sin B};$	
angles.		$\cos b = \frac{\cos B}{\sin A};$	
		$\cos c = \cot A \cot B$ .	

### QUADRANTAL SPHERICAL TRIANGLES.

a, b, the two sides.	A, B, or C, either angle.	c is the omitted side equal to 90°.  C is the angle opposite this side. $\cos A = \frac{\cos a}{\sin b};$ $\cos B = \frac{\cos b}{\sin a};$ $\cos C = -\cot a \cot b.$
	1 D or 1	ain A sin nain C
a, C, one side	$A, D, \text{ or } \theta.$	$\sin A = \sin a \sin C;$ $\tan B = -\cos a \tan C;$
and the angle oppo- site the	A and $b$ .	$\cot b = -\cot a \cos C,$ $\cot b = -\tan a \cos C,$ $\cos A \sin b = \cos a;$
right side.		$\cos A \cos b = -\sin a \cos C$ , $\sin A = \sin a \sin C$ .
	A and B.	$\cos A \sin B = \cos a \sin C;$ $\cos A \cos B = -\cos C.$

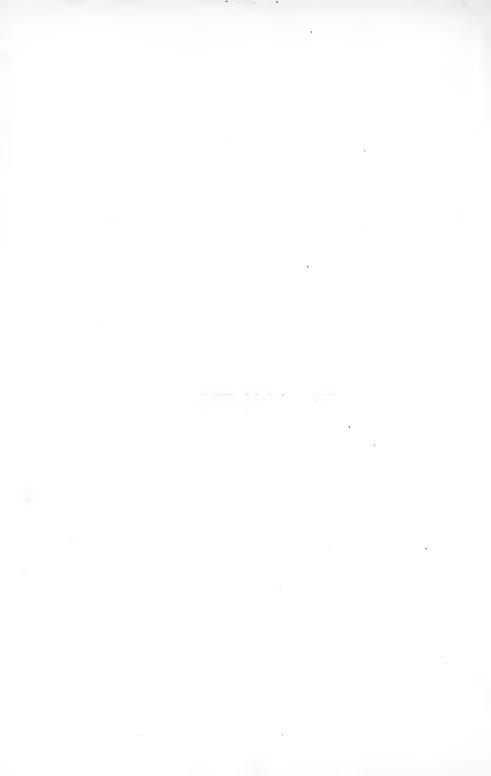
Given.	Required.	
A, b,	a, $B$ , or $C$ .	$\cos a = \cos A \sin b;$
one angle		$\tan B = \sin A \tan b;$
and the		$\cot C = -\cot A \cos b.$
adjacent	1.70	in a sin B - sin A sin he
side.	a and $B$ .	$\sin a \sin B = \sin A \sin b;$ $\sin a \cos B = \cos b;$
		$\cos a = \cos A \sin b.$
		008 4 - 008 11 311 00
	a and C.	$\sin a \sin C = \sin A;$
	a and or	$\sin a \cos C = -\cos A \cos b.$
-		
a, A,	b, B, or C.	$\sin b = \frac{\cos a}{\cos A};$
one side		
and the		$\sin B = \cot a \tan A;$
opposite		$\sin C = \frac{\sin A}{\sin a}.$
angle.		$\sin a$
		ain 4
A, C,	a, b,  or  B.	$\sin a = \frac{\sin A}{\sin C};$
one angle and the		$\cos b = -\tan A \cot C;$
and the		$\cos B = -\frac{\cos C}{\cos A}.$
site the		$\cos B = -\frac{1}{\cos A}$
right side.		
A, B,		$\cot a = \cot A \sin B;$
two angles.	1	$\cot b = \sin A \cot B;$ $\cos C = -\cos A \cos B.$
		$\cos C \equiv -\cos A \cos B$
	a and C.	$\sin C \sin a = \sin A;$
	W unia Oi	$\sin C \cos a = \cos A \sin B;$
		$\cos C = -\cos A \cos B.$
	b and $C$ .	$\sin C \sin b = \sin B;$
		$\sin C \cos b = \sin A \cos B.$

# SPHERICAL TRIANGLES IN GENERAL.

Given.	Required.	$s = \frac{1}{2}(a + b + c)$ :
a, b, c, the three	A, B, C,	, , ,
sides.	the three angles.	$H = \sqrt{\frac{\sin(s-a)\sin(s-b)\sin(s-c)}{\sin s}};$
		$\tan \frac{1}{2}A = \frac{H}{\sin (s-a)};$
		,
		$\tan \frac{1}{2}B = \frac{H}{\sin (s-b)};$
		$\tan \frac{1}{2} C = \frac{H}{\sin (s - c)}.$
		Check: $\frac{\sin a}{\sin A} = \frac{\sin b}{\sin B} = \frac{\sin c}{\sin C}$ .
		Check: $\frac{1}{\sin A} = \frac{1}{\sin B} = \frac{1}{\sin C}$
a, b, C,	A and $c$ ,	$\sin c \sin A = \sin a \sin C;$
two sides	one angle	$\sin c \cos A = \cos a \sin b - \sin a \cos b \cos C;$
and the	and the	$\cos c = \cos a \cos b + \sin a \sin b \cos C.$
included	remaining	
angle.	B  and  c.	sin a sin B - sin h sin C
	Danu c.	$ \sin c \sin B = \sin b \sin C; $ $ \sin c \cos B = \sin a \cos b - \cos a \sin b \cos C. $
		If addition and subtraction logarithms
		are not available for this computation, we
		may compute $k$ and $K$ from
		$k \sin K = \sin a \cos C;$
		$k\cos K = \cos a.$
		Then
		$\sin c \cos A = k \sin (b - K);$ $\cos c = k \cos (b - K).$
		Also,
		$h \sin H = \sin b \cos C;$
		$h \cos H = \cos b$ .
		Then
		$\sin c \cos B = h \sin (a - H);$ $\cos c = h \cos (a - H).$
		000 0 - 10 000 (W 11).
	A, B, c,	$\sin \frac{1}{2} c \sin \frac{1}{2} (A - B) = \cos \frac{1}{2} C \sin \frac{1}{2} (a - b);$
	all the	$\sin \frac{1}{2} c \cos \frac{1}{2} (A - B) = \sin \frac{1}{2} C \sin \frac{1}{2} (a + b);$
	remaining	$\cos \frac{1}{2} c \sin \frac{1}{2} (A + B) = \cos \frac{1}{2} C \cos \frac{1}{2} (a - b);$
	parts.	$\cos \frac{1}{2} c \cos \frac{1}{2} (A + B) = \sin \frac{1}{2} C \cos \frac{1}{2} (a + b).$

Given.	Required.	I
a, b, A, two sides	B, C, c, all the	$\sin B = \frac{\sin A \sin b}{\sin a}$ (two values of B);
and an opposite	remaining parts.	$\tan \frac{1}{2} C = \frac{\cos \frac{1}{2} (a - b) \cot \frac{1}{2} (A + B)}{\cos \frac{1}{2} (a + b)};$
angle.	Į.	$\tan \frac{1}{2}c = \frac{\cos \frac{1}{2}(A+B)\tan \frac{1}{2}(a+b)}{\cos \frac{1}{2}(A-B)}$
A, B, c,	a and $C$ ,	$\sin C \sin a = \sin A \sin c;$
two angles	one side	$\sin C \cos a = \cos A \sin B + \sin A \cos B \cos c;$
and the	and the	$\cos C = -\cos A \cos B + \sin A \sin B \cos c.$
included side.	third angle.	
DIGG.	b and C.	$\sin C \sin b = \sin B \sin c;$
		$\sin C \cos b = \sin A \cos B + \cos A \sin B \cos c.$
		If we compute $k$ and $K$ from
		$k \sin K = \cos A$ ,
		$k\cos K = \sin A \cos c,$
	. 1	then $\sin C \cos a = k \cos (B - K);$
		$\cos C = k \sin (B - K).$
/		If we compute $h$ and $H$ from $h \sin H = \cos B$ ,
		$h \sin H = \cos B,$ $h \cos H = \sin B \cos c,$
		then $\sin C \cos b = h \cos (A - H);$
1 2		$\cos C = h \sin (A - H).$
	a, b, C,	$\sin \frac{1}{2} C \sin \frac{1}{2} (a + b) = \sin \frac{1}{2} c \cos \frac{1}{2} (A - B);$
	all the	$\sin \frac{1}{2} C \cos \frac{1}{2} (a + b) = \cos \frac{1}{2} c \cos \frac{1}{2} (A + B);$
	remaining	$\cos \frac{1}{2} C \sin \frac{1}{2} (a - b) = \sin \frac{1}{2} c \sin \frac{1}{2} (A - B);$
	parts.	$\cos \frac{1}{2} C \cos \frac{1}{2} (a - b) = \cos \frac{1}{2} c \sin \frac{1}{2} (A + B).$
1 D a	$\overline{b, c, C}$	$\sin a \sin B$
A, B, a, two angles	all the	$\sin b = \frac{\sin a \sin B}{\sin A}$ (two values of b);
and an	remaining	5111 11
opposite	parts.	$\tan \frac{1}{2}c = \frac{\cos \frac{1}{2}(A+B)\tan \frac{1}{2}(a+b)}{\cos \frac{1}{2}(A-B)};$
side.	•	
		$\tan \frac{1}{2} C = \frac{\cos \frac{1}{2} (a - b) \cot \frac{1}{2} (A + B)}{\cos \frac{1}{2} (a + b)}.$
$\overline{A, B, C}$	$\overline{a, b, c}$	$S = \frac{1}{2} \left( A + B + C \right);$
the three	the three	$S = \frac{1}{2} (\Pi + D + O),$
angles.	sides.	$P = \sqrt[4]{\frac{-\cos S}{\cos (S-A)\cos (S-B)\cos (S-C)}};$
		$\tan \frac{1}{2}a = P \cos (S - A);$
		$\tan \frac{1}{2} a = I \cos (S - A),$ $\tan \frac{1}{2} b = P \cos (S - B);$
		$\tan \frac{1}{2} c = P \cos (S - C).$
		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

TABLES.



# TABLE I.

# COMMON LOGARITHMS

OF NUMBERS.

N.	Log.	N.	Log.	N.	Log.	N.	Log.	N.	Log.
0	- Infinity.	30	1.47 712	60	1.77 815	90	1.95 424	120	2.07 918
1	0.00 000	31	1.49 136	61	1.78 533	91	1.95 904	121	2.08 279
2	0.30 103	32	1.50 515	62	1.79 239	92	1.96 379	122	2.08 636
3	0.47 712	33	1.51 851	63	1.79 934	93	1.96 848	123	2.08 991
4	o.60 206	34	1.53 148	64	1.80 618	94	1.97 313	124	2.09 342
5	o.69 897	35	1.54 407	65	1.81 291	95	1.97 772	125	2.09 691
6	o.77 815	36	1.55 630	66	1.81 954	96	1.98 227	126	2.10 037
7	0.84 510	37	1.56 820	67	1.82 607	97	1.98 677	127	2.10 380
8	0.90 309	38	1.57 978	68	1.83 251	98	1.99 123	128	2.10 721
9	0.95 424	39	1.59 106	69	1.83 885	99	1.99 564	129	2.11 059
10	1.00 000	40	1.60 206	70	1.84 510	100	2.00 000	130	2.11 394
11	1.04 139	41	1.61 278	71	1.85 126	101	2.00 432	131	2.11 727
12	1.07 918	42	1.62 325	72	1.85 733	102	2.00 860	132	2.12 057
13	1.11 394	43	1.63 347	73	1.86 332	103	2.01 284	133	2.12 385
14	1.14 613	44	1.64 345	74	1.86 923	104	2.01 703	134	2.12 710
15	1.17 609	45	1.65 321	75	1.87 506	105	2.02 119	135	2.13 033
16	1.20 412	46	1.66 276	76	1.88 081	106	2.02 531	136	2.13 354
17	1.23 045	47	1.67 210	77	1.88 649	107	2.02 938	137	2.13 672
18	1.25 527	48	1.68 124	78	1.89 209	108	2.03 342	138	2.13 988
19	1.27 875	49	1.69 020	79	1.89 763	109	2.03 743	139	2.14 301
20	1.30 103	50	1.69 897	80	1.90 309	110	2.04 139	140	2.14613
21	1.32 222	51	1.70 757	81	1.90 849	111	2.04 532	141	2.14 922
22	1.34 242	52	1.71 600	82	1.91 381	112	2.04 922	142	2.15 229
23	1.36 173	53	1.72 428	83	1.91 908	113	2.05 308	143	2.15 534
24	1.38 021	54	1.73 239	84	1.92 428	114	2.05 690	144	2.15 836
25	1.39 794	55	1.74 036	85	1.92 942	115	2.06 070	145	2.16 137
26	1.41 497	56	1.74 819	86	1.93 450	116	2.06 446	146	2.16 435
27	1.43 136	57	1.75 587	87	1.93 952	117	2.06 819	147	2.16 732
28	1.44 716	58	1 76 343	88	1.94 448	118	2.07 188	148	2.17 026
29	1.46 240	59	1.77 085	89	1.94 939	119	2.07 555	149	2.17 319
30	1.47 712	60	1.77 815	90	1.95 424	120	2.07 918	150	2.17 (109

2							BLE I					
N.		0	1	2	3	4	5	6	7	8	9	Prop. Pts.
100	00 0	000	043	087	130	173	217	260	303	346	389	
01	-4	132	475	518	561	604	647	689	732	775	817	
$\begin{bmatrix} 02 \\ 03 \end{bmatrix}$	01 2	860	903	945 368	988	*030	*072	*115	*157	*199 620	*24 <b>2</b> 662	44 43 42
11 1			326		410	452	494	536	578			1 4.4 4.3 4.2 2 8.8 8.6 8.4
04 05		703	745 160	787 202	828 243	870 284	912 325	9 <b>5</b> 3 366	99 <del>5</del> 407	*036 449	*078 490	3 13.2 12.9 12.6
06		531	572	612	653	694	735	776	816	857	898	4 17.6 17.2 16.8
07		938	979	*019	*060	*100	*141	*181	*222	*262	*302	5 22.0 21.5 21.0 6 26.4 25.8 25.2
08		342	383	423	463	503	543	583	623	663	703	7 30.8 30.1 29.4
09	_	743	782	822	862	902	941	981	*021	*060	*100	8 35.2 34.4 33.6 9 39.6 38.7 37.8
110		139	179	218	258	297	336	376	415	454	493	9139.0130.7137.0
11 12		532 922	-571 961	610 999	650 *038	689 *077	727 *115	766 *154	805 *192	844 *231	883 *269	41   40   39
13	05		346	385	423	461	500	538	576	614	652	1 4.1 4.0 3.9
14		590	729	767	803	843	881	918	956	994	*032	2 8.2 8.0 7.8
15	<b>o</b> 6 d	070	108	145	183	221	258	296	333	371	408	3 12.3 12.0 11.7 4 16.4 16.0 15.6
16		446	483	521	558	595	633	670	707	744	781	5 20.5 20.0 19.5
17	3	819	856	893	930	967	*004	*041	*078	*115	*151	6 24.6 24.0 23.4 7 28.7 28.0 27.3
18 19	07	555	225 591	262 628	298 664	335	372 737	408 773	809	482 846	518 882	8 32.8 32.0 31.2
120		918	954	990	*027	*063	*099	*135	*171	*207	*243	9 36.9 36.0 35.1
21	_	279	314	350	386	422	458	493	529	565	600	
22		636	672	707	743	778	814	849	884	920	955	38 37 36
23		991	*026	*061	*096	*132	*167	*202	*237	*272	*307	1 3.8 3.7 3.6 2 7.6 7.4 7.2
24	09	342	377	412	447	482	517	552	587	621	656	3 11.4 11.1 10.8
25 26	10 (	691	726	760 106	795	830	864 209	899	934	968 312	*003	4 15.2 14.8 14.4
27		380			483			585	619	653	687	5 19.0 18.5 18.0 6 22.8 22.2 21.6
28		72I	41 <u>5</u> 755	449 789	823	517 857	551 890	924	958	992	*025	7 26.6 25.9 25.2
29	11		093	126	160	193	227	261	294	327	361	9 34 -2 33 -3 32 -4
130		394	428	461	494	528	561	594	628	661	694	9134133-3134
31		727	760	793	826	860	893	926	959	992	*024	35   34   33
32 33	12		090	123	156	189	222 548	254 581	287	320 646	352 678	2 3.5 3.4 3.3
		385	418	450	483	516			613			2 7.0 6.8 6.6
34 35	13	710	743 o66	775 098	808	162	872 194	905	937 258	969	*001	3 10.5 10.2 9 9 4 14.0 13.6 13.2
36		354	386	418	450	481	513	545	577	609	640	5 17.5 17.0 16.5
37		672	704	735	767	799	830	862	893	925	956	6 21.0 20.4 19.8 7 24.5 23.8 23.1
38		988	*019	*051	*082	*114	*145	*176	*208	*239	*270	8 28.0 27.2 26.4
39	14_		333	364	395	426	768	489	520	551	582	9 31.5 30.6 29.7
140	-	613	644	675	706	737		799 *106	829	*168	*198	
41 42	15	922	953 259	983	*014 320	*045 351	381	412	*137 442	473	503	32 31 30
43		534	564	594	625	653	685	715	746	776	806	1 3.2 3.1 3.0 2 6.4 6.2 6.0
44		836	866	897	927	957	987	*017	*047	*077	*107	3 9.6 9.3 9.0
45	16	137	167	197	227	256	286	316	346	376	406	4 12.8 12.4 12.0
46		435	465	495	524	554	584	613	643	673	702	5 16.0 15.5 15.0 6 19.2 18.6 18.0
47 48	177	732 026	761 056	791 085	820	850	879 173	909	938	967 260	997	7 22.4 21.7 21.0
49		319	348	377	406	143	464	493	522	551	580	9 28.8 27.9 27.0
150		609	638	667	696	725	754	782	811	840	869	,
N.		0	1	2	3	4	5	6	7	8	9	Prop. Pts.

#### LOGARITHMS OF NUMBERS.

N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
150	17 609	638	667	696	725	754	782	811	840	869	
51	898	926	955	984	*013	*041	*070	*099	*127	*156	29   28
52 53	18 184 469	498	241 526	270 554	298 583	327 611	355	3 <sup>8</sup> 4 667	696	724	1 2.9 2.8
54	752	780	808	837	863	893	921	949	977	*005	2 5.8 5.6 3 8.7 8.4
55	19 033	061	089	117	145	173	201	229	257	285	4 11.6 11.2
56	312	340	368	396	424	451	479	507 783	535	562	$\begin{bmatrix} 5 & 14.5 & 14.0 \\ 6 & 17.4 & 16.8 \end{bmatrix}$
57 58	590 866	893	921	673 948	976	728 *003	756 *030	*058	811 *085	838 *112	7 20.3 19.6
59	20 140	167	194	222	249	276	303	330	358	385	$\begin{vmatrix} 8 & 23 & 2 & 22 & 4 \\ 9 & 26 & 1 & 25 & 2 \end{vmatrix}$
160	412	439	466	493	520	548	573	602	629	656	
61 62	683 952	978	737 *005	763 *032	790 *059	817 *085	844 *112	871 *139	898 *165	92 <u>5</u> *192	27   26
63	21 219	245	272	299	325	352	378	405	431	458	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
64	484	511	537 801	564	590	617	643	669	696	722	3 8.1 7.8
65 66	748 22 OII	775	063	827 089	854	880 141	906	932	958	98 <del>5</del> 246	4 10.8 10.4 5 13.5 13.0
67	272	298	324	350	376	401	427	453	479	505	6 16.2 15.6
68	531	557	583	608	634	660	686	712	737	763	7 18.9 18.2 8 21.6 20.8
69	789	814	840	866	891	917	943	968	994	*019	9 24.3 23.4
170	23 045	070	096	121	147	172	198	223	249 502	274 528	25
71 72	300 553	3 <sup>2</sup> 5 578	350 603	376 629	654	426 679	452 704	477 729	754	779	1 2.5
73	805	830	855	880	905	930	955	980	*005	*030	2 5.0
74	24 055	080	105	130	155	180	204	229	254	279	3 7.5 4 10.0
75 76	304 551	329 576	353 601	378 625	403 650	428 674	452 699	477 724	502 748	527 773	5 12.5
77	797	822	846	871	895	920	944	969	993	*018	6 15.0 7 17.5
78	25 042	<b>o</b> 66	091	115	139	164	188	212	237	261	8 20.0
79	285	310	334	358 600	382 624	406 648	672	455 696	720	744	9 22.5
180 81	768	551 792	575 816	840	864	888	912	935	959	983	24   23
82	26 007	031	055	079	102	126	150	174	198	221	1 2.4 2.3
83	245	269	293	316	340	364	387	411	435	458	$\begin{bmatrix} 2 & 4.8 & 4.6 \\ 3 & 7.2 & 6.9 \end{bmatrix}$
84 85	482 717	741	529 764	553 788	576 811	834	623 858	647 881	670 905	928	4 9.6 9.2
86	951	975	998	*021	*045	*068	*091	*114	*138	*161	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
87	27 184	207	231	254	277	300	323	346	370	393	7 16.8 16.1
88	416 646	439	692	485	508 738	53I 76I	784	807	830	852	$   \begin{array}{c cccccccccccccccccccccccccccccccccc$
190	875	898	921	944	967	989	*012	*035	*058	*081	, ,
91	28 103		149	171	194	217	240	262	285	307	22 21
92	330	353	375	398	421	443 668	466 691	488 713	735	533 758	$egin{array}{ c c c c c c c c c c c c c c c c c c c$
93	556 780		825	847	870	892	914	937	959	981	3 6.6 6.3
94 95	29 003	026	048	070	092	115	137	159	181	203	4 8.8 8.4 5 11.0 10.5
96	226	1	270	292	314	336	358	380	403	425	6 13.2 12.6
97	447 667	469 688	491	513 732	535 754	557 776	579 798	601 820	623 842	863	7 15.4 14.7 8 17.6 16.8
98 99	885	907	929	951	973	994	*016	*038		*08I	9 19.8 18.9
200	30 103	-	146	168	190	211	233	255	276	298	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

Í	N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
												Arop. 1 ts.
ı	200	30 103	125 341	146 363	168 384	190 406	428	233 449	25 <del>5</del> 471	276 492	298 514	1 00 1 01
I	02	535	557	578	600	621	643	664	685	707	728	22   21   1   2.2   2.1
I	03 04	750 963	77 I 984	792 *006	814 *027	835 *048	856 *069	878 * <b>0</b> 91	899 *112	920 *133	942 *154	2 4.4 4.2
	05 06	31 175 387	197	218 429	2 <u>3</u> 9 4 <u>5</u> 0	260 47 I	281 492	302 513	3 <sup>2</sup> 3 534	345 555	366 576	3 6.6 6.3 4 8.8 8.4 5 11.0 10.5
	07 08 09	597 806 32 015	618 827 035	639 848 <b>05</b> 6	660 869 977	890 098	702 911 118	723 931 139	744 952 160	76 <del>5</del> 973 181	785 994 201	6 13.2 12.6 7 15.4 14.7 8 17.6 16.8
ı	210	222	243	263	284	305	325	346	366	387	408	9 19.8 18.9
	11 12 13	428 634 838	449 654 858	46 <u>9</u> 67 <u>5</u> 879	490 695 899	510 715 919	531 736 940	552 756 960	572 777 980	593 797 *001	613 818 *021	$\begin{bmatrix} 20 \\ 1 \\ 2.0 \\ 4.0 \end{bmatrix}$
	14 15 16	33 041 244 445	062 264 465	082 284 486	102 304 506	122 325 526	14 <u>3</u> 34 <u>5</u> 546	16 <u>3</u> 36 <u>5</u> 566	183 385 586	203 405 606	224 425 626	3 6.0 4 8.0 5 10.0
	17 18 19	646 846 34 044	666 866 <b>o</b> 64	686 885 084	706 905 104	726 925 124	746 945 143	766 965 163	786 98 <del>5</del> 183	806 *005 203	826 *025 223	6 12.0 7 14.0 8 16.0
ı	220	242	262	282	301	321	341	361	380	400	420	9 18.0
l	21 22 23	439 635 830	459 655 850	479 674 869	498 694 889	518 713 908	537 733 928	557 753 947	577 772 967	596 792 986	616 811 *005	1 1.9 2 3.8
	24 25 26	35 02 <del>5</del> 218 411	044 238 430	064 257 449	083 276 468	102 295 488	122 315 507	141 334 526	160 353 545	180 372 564	199 392 583	3 5.7 4 7.6 5 9.5
	27 28 29	603 793 984	622 813 *003	641 832 *021	660 851 *040	679 870 *059	698 889 *078	717 908 *097	736 927 *116	755 946 *135	77 <u>4</u> 96 <u>5</u> *154	6 11.4 7 13.3 8 15.2 9 17.1
ı	230	36 173	192	211	229	248	267	286	305	324	342	
	31 32 33	361 549 736	380 568 754	399 586 773	418 605 791	436 624 810	455 642 829	474 661 847	493 680 866	511 698 884	530 717 903	18 1 1.8 2 3.6
	34 35 36	922 37 107 291	940 125 310	959 144 328	977 162 346	996 181 36 <del>5</del>	*014 199 383	*033 218 401	*051 236 420	*070 254 438	*088 273 457	3 5.4 4 7.2 5 9.0 6 10.8
	37 38 39	47 <u>5</u> 658 840	493 676 858	511 694 876	530 712 894	548 731 912	566 749 931	583 767 949	603 785 967	621 803 985	639 822 *003	7 12.6 8 14.4 9 16.2
ı	240	38 021	039	057	075	093	112	130	148	166	184	1 17
	41 42 43	202 382 561	399 578	238 417 596	256 435 614	274 453 632	292 47 I 650	310 489 668	328 507 686	346 525 703	364 543 721	1 1.7 2 3.4
	44 45 46	739 917 <b>39 09</b> 4	757 934 111	775 952 129	792 970 146	810 987 164	828 *005 182	846 *023 199	863 *041 217	881 *058 235	899 *076 252	3 5.1 4 6.8 5 8.5 6 10.2
-	47 48 49	270 445 620	287 463 637	30 <u>5</u> 480 65 <u>5</u>	322 498 672	340 515 690	358 533 707	375 550 724	393 568 742	410 585 759	428 602 777	7 11.9 8 13.6 9 15.3
	250	794	811	829	846	863	881	898	915	933	950	•
	N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

N.		0	1	2	3	4	5	6	7	8	9	Prop. Pts.
250	39 7	94	811	829	846	863	881	898	915	933	950	
51		67	985	*002	*019	*037	*054	*071	*088	*106	*123	18
52 53	40 1	12	157	175 346	192 364	209 381	398	415	261	278 449	<b>2</b> 95 <b>4</b> 96	1 1.8
			329						432	620		2 3.6
54 55		83	500 671	518 688	535 705	552 722	569 739	586 756	603 773	790	637 837	3 5.4 4 7.2
56		24	841	858	875	892	909	926	943	960	976	5 9.0
57	9	93	*010	*027	*044	*061	*078	*095	*111	*128	*145	6 10.8
58	41 I	62	179	196	212	229	246	263	280	296	313	7 12.6 8 14.4
59 260		30	347	363	380	397	414	430	614	631	481	9 16.2
61		97 64	514 681	53I 697	547	564	581	597 764	780		814	1 17
62	8	30	847	863	714 880	731 896	747 913	929	946	797	979	
63	9	96	*012	*029	*045	*062	*078	*095	*111	*127	*144	1 1.7 2 3.4
64		60	177	193	210	226	243	259	275	292	308	3 5.1
65 66		25	341	357	374	390	406	423 586	439 602	455	472	4 6.8 5 8.5
67		88	504	521	537	553	570			781	635	5 8.5 6 10.2
68	8	51 13	667 830	684 846	700 862	716 878	732 894	749	765	943	<b>7</b> 97	7 11.9
69		75	991	*008	*034	*040	*056	*072	*ó88	*104	*120	8 13.6 9 15.3
270	43 I	36	152	169	185	201	217	233	249	265	281	0(10.0
71		97	313	329	345	361	377	393	409	425	441	16
72 73		57	473 632	489 648	50 <del>5</del>	521 680	537 696	553 712	569 727	584 743	759	1 1.6
74				807	823	838	854	870	886	902	917	2 3.2 3 4.8
75		775	791 949	965	981	996	*012	*028	*044	*059	*075	4 6.4
76	44 0		107	122	138	154	170	185	201	217	232	5 8.0 6 9.6
77	2	248	264	279	295	311	326	342	358	373	389	7 11.2
78 79	4	60	420	436	607	623	483 638	654	669	529 68 <b>5</b>	545	8 12.8
280	_	716	731	592 747	762	778	793	809	824	840	855	9 14.4
81		371	886	902	917	932	948	963	979	994	*010	15
82	45 0		040	056	071	086	102	117	133	148	163	1 1.5
83		79	194	209	225	240	255	271	286	301	317	2 3.0 3 4.5
84 85	3	332	347	362	378	393	408 561	423	439	454 606	469 621	4 6.0
86		184 537	652	515	530	545 697	712	576 728	743	758	773	5 7.5
87		788	803	818	834	849	864	879	894	909	924	6 9.0 7 10.5
88	9	939	954	969	984	*000	*015	*030	*045	*060	*075	8 12.0
89	46 0		105	120	135	150	165	180	195	210	225	9 13.5
290		240	255	270	285	300	315	330	345	359	374	14
91 92	3	389 538	553	568	434 583	598	464 613	479 627	494 642	509	523 672	1 1.4
93	ě	587	702	716	731	746	761	776	790	805	820	2 2.8
94		835	850	864	879	894	909	923	938	953	967	3 4.2 4 5.6
95	9	982	997	*012	*026	*041	*056	*070	*085	*100	*114	5 7.0
96	47		144	159	173	188	202	217	232	246		6 8.4 7 9.8
97 98		276 422	290 436	305	319 465	334 480	349 494	363 509	378	392 538	553	8 11.2
99	1	567	582	596	611	625	640	654	669	683	698	9 12.6
300	_	712	727	741	756	770	784	799	813	828	842	
N.		0	1	2	3	4	5	6	7	8	9	Prop. Pts.

log TT = 0.497/5 = 0.497/499

6 J	TABLE I.											
N.		0	1	2	3	4	5	6	7	8	9	Prop. Pts.
300	47	712	727	741	756	770	784	799	813	828	842	
01	40	857	871	885	900	914	929	943	958	972	986	
02 03	40	00I I44	159	173	187	202	973 216	230	244	259	130 273	15
04		287	302	316	330	344	359	373	387	401	416	1 1.5
05 06		430 572	444 586	458 601	473	487	501 643	515 657	530 671	544 686	558	2 3.0
07		714	728	742	756	770	785	799	813	827	841	3 4.5 4 6.0
08		855	869	883	897	911	926	940	954	968	982	5 7.5
09		996	*010	*024	*038	*052	*066 206	*080	*094	*108 248	*122	6 9.0 7 10.5
310 11	49	136 276	150 290	304	318	332	346	360	374	388	402	8 12.0 9 13.5
12		415	429	443	457	471	485	499 638	513	527	541	0,10.0
13		554	568	582	596	610	624		651	665	679	
14 15		693 831	707 843	859	734 872	748 886	762 900	776	790	803 941	817 955	14
16		969	982	996	*010	*024	*037	*051	*66 <del>5</del>	*079	*092	1 1.4
17 18	50	106 243	120 256	133	147	161 297	174 311	188	202 338	215 352	229 365	2 2.8 3 4.2
19		379	393	406	420	433	447	461	474	488	501	4 5.6
320		513	529	542	556	569	583	596	610	623	637	5 7.0 6 8.4
21 22		651 786	664 799	678 813	691	70 <u>5</u> 840	718 853	732 866	745 880	759 893	772 907	7 9.8 8 11.2
23		920	934	947	961	974	987	*001	*014	*028	*041	9 12.6
24	51	055	068	180	095	108	121	13 <del>5</del> 268	148	162	175	
25 26		188 322	202 335	215 348	228 362	242 375	255 388	402	282 415	295 428	308 441	
27		455	468	481	495	508	521	534	548	561	574	18
28 29		587 720	601 733	614 746	627 759	640 772	654 786	667 799	680 812	693 825	706 838	1 1.3
330	•	851	865	878	891	904	917	930	943	957	970	2 2.6 3 3.9
31	•	983	996	*009	*022	*035	*048	*061	*075	*088	*101	4 5.2 5 6.5
32 33	52	114 244	127 257	140 270	153 284	166 297	310	192 323	205 336	218 349	23I 362	6 7.8
34		375	388	401	414	427	440	453	466	479	493	7 9.1 8 10.4
35		504	517	530 660	543	556 686	569	582	595	608	621	9 11.7
36		634	647	789	673 802	813	699 827	711 840	724 853	737	750 879	
37 38		763 892	776 903	917	930	943	956	969	982	994	*007	
39	53	020	033	046	058	071	084	097	110	122	135	12
340 41		148 275	161 288	30I	314	199 326	212	352	237 364	2 <u>5</u> 0	<b>2</b> 63	$\begin{array}{c c} 1 & 1.2 \\ 2 & 2.4 \end{array}$
42		403	415	428	441	453	339 466	479	491	504	517	3 3.6
43		529	542	553	567	580	593	605	618	631	643	4 4.8 5 6.0
44 45		656 782	668 794	681 807	694 820	706 832	719 845	732 857	744 870	757 882	769 895	6 7.2 7 8.4
46		908	920	933	945	958	970	983	995	*008	*020	8 9.6
47	54	033	045	058	070	083 208	095	108	120	133 258	145	9 10.8
48 49		158 283	295	183 307	195 320	332	34 <del>5</del>	233 357	245 370	382	270 394	
850		407	419	432	444	456	469	481	494	506	518	
N.		0	1	2	3	4	5	6	7	8	9	Prop. Pts.

N.		. 0	1	2	3	4	5	6	7	8	9	Prop. Pts.
350	54	497	419	432	444	456	469	481	494	506	518	
51 52		531 654	543	555 679	568	580 704	593 716	60 <del>5</del> 728	617	630	642	
53		777	790	802	814	827	839	851	864	753 876	765 888	13
54		900	913	925	937	949	962	974	986	998	*011	1 1.3
55 56	55	145	035	169	182	194	084 206	096	108	242	13 <u>3</u> 25 <u>5</u>	2 2.6 3 3.9
57		267	279	291	303	315	328	340	352	364	376	4 5.2
58 59		388 509	400 522	534	425   546	437 558	449 570	461 582	473 594	485	497	5 6.5 6 7.8
360		630	642	654	666	678	691	703	715	727	739	7 9.1 8 10.4
61 62		751 871	763 883	77 <u>5</u> 895	787 907	799	811	823	835	847	859	9 11.7
63		991	*003	*015	*027	919 *038	931 *050	943 *062	955 *074	967 *086	979 *098	
64	56	110	122	134	146	158	170	182	194	205	217	1 12
65 66		229 348	241 360	253 372	26 <del>5</del> 384	396	289 407	301 419	312 431	324 443	336 45 <del>5</del>	1 1.2
67		467	478	490	502	514	526	538	549	561	573	2 2.4
68 69		58 <del>5</del>	597 714	608 726	738	750	761	656	785	797	808	4 4.8
370		820	832	844	855	867	879	891	902	914	926	5 6.0 6 7.2
71 72	57	937 054	949 066	961 078	972 089	984	996 113	*008	*019	*031 148	*043 159	7 8.4 8 9.6
73	"	171	183	194	206	217	229	241	252	264	276	9 10.8
74 75		287 403	299 415	310 426	322 438	334	345 461	357	368 484	380 496	392	
76		519	530	542	553	44 <u>9</u> 56 <u>5</u>	576	473 588	600	61.1	507 623	
77 78		634	646 761	657	669 784	680	692 807	703	715	726 841	738	11
79		749 864	875	772 887	898	795 910	921	933	830 944	955	852 967	$egin{array}{c c} 1 & 1.1 \\ 2 & 2.2 \end{array}$
880	_	978	990	100*	*013	*024	*035	*047	*058	*070	*081	3 3.3 4 4.4
81 82	58	092 206	218	229	127	138 252	149 263	161 274	172 286	184	309	5 5.5 6 6.6
83		320	331	343	354	365	377	388	<b>3</b> 99	410	422	7 7.7
84 85		433 546	444 557	456 569	467 580	478 591	490 602	501 614	625	524 636	53 <del>5</del> 647	8 8.8 9 9.9
86		659	670	681	692	704	715	726	737	749	760	
87 88		77 I 883	782 894	794 906	80 <del>3</del>	928	827 939	838 950	8 <u>5</u> 0	861 973	872 984	
89		995	*006	*017	*028	*040	*051	*062	*073	*084	*095	10
390 91	<b>5</b> 9	106	229	129	140 251	262	273	173 284	184	306	318	$ \begin{array}{c c} 1 & 1 & 0 \\ 2 & 2 & 0 \end{array} $
92		329	340	240 351	362	373	384	395	295 406	417	428	3 3.0 4 4.0
93		439	450	461	472	483	494 603	506	517 627	528	539	5 5.0
94 95		5 <u>5</u> 0 660	561 671	572 682	583 693	594 704	715	726	737	638 748	649 759	6 6.0 7 7.0
96		770	780	791	802	813	824	835	846	857	868	8 8.0 9 9.0
97 98	•	879 988	890 999	100	912 *021	923 *032	934 *043	94 <del>5</del> *054	956 *06 <del>5</del>	966 *076	977 *o86	0,0.0
99	60	097	108	119	130	141	152	163	173	184	195	
400		206	217	228	239	249	260	271	282	293	304	
N.		0	1	2	3	4	5	6	7	8	9	Prop. Pts.

8					IA.	BLE I	•				
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
400	60 206	217	228	239	249	260	271	282	293	304	
01	314	325	336	347	358 466	369	379 487	390	401	412	
02 03	423 531	433 541	444 552	455 563	574	477 584	595	498 606	509 617	520 627	
04	638	649	660	670	681	692	703	713	724	735	
05 06	746 853	756 863	767 874	778 88 <u>5</u>	788 895	799 9 <b>0</b> 6	810 917	821 927	831 938	842 949	11
07	959	970	981	991	*002	*013	*023	*034	*045	*055	$   \begin{array}{ccccccccccccccccccccccccccccccccccc$
08 09	61 o66 172	077	087	098 204	215	119 225	130 236	140 247	151 257	162 268	3 3.3
410	278	289	300	310	321	331	342	352	363	374	4 4.4 5 5.5
11	384	395	405	416	426	437	448	458	469	479	6 6.6
12 13	490 <b>5</b> 95	500 606	511 616	521 627	532 637	542 648	553 658	563 669	574 679	584 690	7 7. <b>7</b> 8 8.8
14	700	711	721	731	742	752	763	773	784 888	794	9 9.9
15 16	80 <u>3</u> 909	815 920	826 930	836 941	847 951	857 962	868 972	878 982	993	899 * <b>003</b>	
17	62 014	024	034	045	055	<b>o</b> 66	076	086	097	107	
18 19	118	128	138	149 252	159 263	170 273	180	190	201 304	315	
420	325	335	346	356	366	377	387	397	408	418	
21	428	439	449	459	469	480	490	500	511	521	10
22 23	531 634	54 <b>2</b> 644	552 655	562 66 <del>5</del>	572 675	583 685	593 696	603 706	613	624 726	$ \begin{array}{c c} 1 & 1 & 0 \\ 2 & 2 & 0 \end{array} $
24	737	747	757	767	778	788	798	808	818	829	3 3.0
25 26	839 941	849 951	859 961	87 <b>0</b> 972	982	890 992	900 *002	910 *012	92I *022	931 *033	4 4.0 5 5.0
27	63 043	053	<b>o</b> 63	073	083	094	104	114	124	134	6 6.0 7 7.0
28 29	144 246	155 256	16 <u>5</u> 266	17 <del>5</del> 276	185	195 296	205 306	215 317	225 327	236 337	8 8.0 9 9.0
430	347	357	367	377	387	397	407	417	428	438	0,0,0
31	448	458	468	478	488	498	508	518	528	538	
32 33	548 649	558	568	579 679	589 689	599 699	609 709	619 719	629	639 739	
34	749	259	769	779	789	799	809	819	829	839	
35	849	859	869	879	889	899	909	919	929	939	
36	949	959	969	979	988	998	*008	*018	*028	*038	9
37 38	64 048 147	058	167	078	088	098 197	108	118	128	237	$ \begin{array}{c c} 1 & 0.9 \\ 2 & 1.8 \end{array} $
39	246	256	266	276	286	296	306	316	326	335	$\begin{array}{c c} 3 & 2.7 \\ 4 & 3.6 \end{array}$
440	345	355	365	375	38 <del>5</del> 483	395	404	414	424	434	5 4.5
41 42	444 542	454 552	464 562	473 572	582	493 591	503	513	523 621	532 631	6 5.4 7 6.3
43	640	650	660	670	680	591 689	699	709	719	729	8 7.2
44 45	738 836	748 846	758 856	768 865	777	787 885	797 895	807 904	816	826 924	9 8.1
46	933	943	953	963	972	982	992	*002	*011	*021	
47	65 031	040	050	060	070	079	089 186	099	108	118	
48 49	128 225	137 234	147 244	1 57 254	167	176 273	283	196	302	312	~ 1
450	321	331	341	350	360	369	379	389	398	408	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
450	65 321	331	341	350	360	369	379	389	398	408	
51 52	418 514	427 523	437 533	447 543	456 552	466 562	475 571	485 581	495 591	504	
53	610	619	629	639	648	658	667	677	686	696	
54 55	706 801	715	72 <del>5</del> 820	734 830	744 839	753 849	763 858	772 868	782 877	792 887	
56 57	896 992	*001	*011	925 *020	935	944	954	963	973	982	1 1.0
58	66 087	096	106	115	*030 124	*039 134	*049 143	*058	*068 162	*077 172	2 2.0
59 460	276	285	200	304	314	323	332	342	257 351	266 361	4 4.0
61	370	380	389	398	408	417	427	436	445	455	5 5.0 6 6.0
62 63	464 558	474 567	483 577	492 586	502 596	511 60 <del>5</del>	52I 614	530 624	539 633	549 642	7 7.0 8 8.0
64 65	652 745	661 755	671 764	680	689 783	699	708 801	717	727 820	736	9 9.0
66	839	848	857	773 867	876	792 885	894	904	913	829 922	
67 68	932 67 025	941 034	950 043	960 052	969 062	978 071	987 080	997 089	*006	*015	
69	117	127	136	145	154	164	173	182	191	201	
470 71	302	311	321	330	339	256 348	265 357	367	376	293 38 <del>5</del>	9
72 73	394 486	403	413	422 514	431	440	449	459	468	477	1 0.9 2 1.8
74	578	587	596	605	523 614	532 624	633	550 642	560	569 660	3 2.7 4 3.6
75 76	669 761	679 770	688	697 788	706 797	715	724 815	73 <u>3</u> 82 <u>5</u>	742 834	752 843	5 4.5
77	852	861	870	879	888	897	906	916	925	934	65.4 76.3
78 79	68 o <sub>34</sub>	952	961	970	979 070	988 979	997 088	*006	*015	115	8 7.2 9 8.1
480	124	133	142	151	160	169	178	187	196	205	
81 82	21 <u>5</u> 30 <u>5</u>	224 314	233 323	242 332	251 341	260 3 <u>5</u> 0	269	278 368	287	296 386	
83	39 <del>5</del> 48 <del>5</del>	404	413	422	431	440	449	458	467	476	-
84 85	574	494 583	502 592	601	520	529 619	538 628	547 637	556 646	56 <u>5</u>	
86 87	664 753	762	681	780	699 789	708	806	726	735 824	833	8 10.8
88 89	842	851	860	869	878 966	797 886	895 984	904	913	922	2 1.6 3 2.4
490	93I 69 020	940	949	958	055	975 064	073	993	090	099	4 3.2
91 92	108	117	126 214	135 223	144 232	152 241	161 249	170 258	179 267	188 276	5 4.0 6 4.8
93	285	294	302	311	320	329	338	346	355	364	7 5.6 8 6.4
94 95	373 461	381 469	390 478	399 487	408 496	417 504	425 513	434 522	443 531	452 539	9 7.2
96	548	557	566	574	583	592	601	609	53I 618	539 627	
97 98	636 723	732	653 740	662 749	671 758	679 767	688 775	697 784	705 793 880	714 801	
99	810 897	906	827	836	845	854	862	958	966	975	
500			914	923	932	940	949				Drop Die
N.	Ó	1	2	3	4	5	6	7	8	9	Prop. Pts.

10					10	RLE 1					
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
500	69 897	906	914	923	932	940	949	958	966	975	1
01	984	992	*001	*010	*018	*027	*036	*044	*053	*062	
02	70 070	079	088	096	105	114	122	131	140	148	
03	157	165	174	183	191	200	.209	217	226	234	
04 05	243	252 338	260 346	269	278 364	286	29 <u>5</u> 381	303	312	321	
05	329 415	424	432	355 441	449	372 458	467	475	398 484	406 492	19
07	501	509	518	526	535	544	552	561	569	578	10.9
08	586	595	603	612	621	629	638	646	655	663	2 1.8
09	672	680	689	697	706	714	723	731	740	749	3 2.7 4 3.6
510	757	766	774	783	791	800	808	817	825	834	54.5
11	842	851	859	868		885	893	902	910	919	6 5.4
12 13	927 71 012	935	944	952 037	961 046	969 054	978 063	986 071	995	*003 088	$\begin{array}{c} 7 & 6.3 \\ 8 & 7.2 \end{array}$
14	096	105	113	122			_		164		98.1
15	181	189	198	206	130	139 223	147 231	155	248	172 257	
16	265	273	282	290	299	307	315	324	332	341	
17	349	357	366	374	383	391	399	408	416	425	
18	433	441	450	458	466	475	483	492	500	508	
19	517	525	533	542	550	559	567	575	584	592	
520	600	609	617	625	634	642	650	659	667	675	18
21 22	684 767	692	700	709 792	800	725 809	734 817	742 825	750 834	759 842	10.8
23	850	775 858	867	875	883	892	900	908	917	925	2 1.6
24	933	941	950	958	966	975	983	991	999	*008	3 2.4
25	72 016	024	032	041	049	057	066	074	082	090	43.2 54.0
26	099	107	115	123	132	140	148	156	165	173	64.8
27	181	189	198	206	214	222	230	239	247	255	75.6
28	263	272	280 362	288	296	304 387	313	321	329	337	8 6.4 9 7.2
29 <b>530</b>	346 428	354	444	370 452	378 460	469	395	485	411	419 501	011.2
31		436 518	526		542	550	477 558	567	493 575	583	
32	509 591	599	607	534 616	624	632	640	648	656	665	
33	673	681	689	697	705	713	722	730	738	746	
34	754	762	770	779	787	795	803	118	819	827	
35	835	843	852	860	868	876	884	892	900	908	17
36	916	925	933	941	949	957	965	973	981	989	
37 38	997 73 078	*006	*014	*022 102	*030	*038	*046 127	*054 135	*062	*070 151	1 0.7 2 1.4
39	159	167	175	183	191	199	207	215	223	231	3 2.1
540	239	247	255	263	272	280	288	296	304	312	42.8
41	320	328	336	344	352	360	368	376	384	392	5 3.5 6 4.2
42	400	408	416	424	432	440	448	456	464	472	74.9
43	480	488	496	504	512	520	528	536	544	552	8 5.6 9 6 3
44	560	568	576	584	592 672	600 679	608 687	616	703	632	810 2
45 46	640 719	648 727	656 735	743	751	759	767	775	783	791	
47	799	807	813	823	830	838	846	854	862	870	
48	878	886	894	902	910	918	926	933	941	949	
49	957	965	973	981	989	997	*005	*013	*020	*028	
550	74 036	044	052	060	068	076	084	092	099	107	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
550	74 036	044	052	060	o68	076	084	092	099	107	
51 52	115 194	123	131	139 218	147 225	15 <del>5</del> 233	162	170	178	186 26 <del>5</del>	
53	273	280	288	296	304	312	24I 320	249 327	257 335	343	
54	351	359	367	374	382	390	398	406	414	421	
55 56	429 507	437 515	445 523	453 531	461 539	468 547	476 554	484 562	492 570	500 578	
57	586	593	601	609	617	624	632	640	648	656	
58 59	663 741	671 749	679 757	687 764	69 <del>5</del>	702 780	710	718	726 803	733 811	
560	819	827	834	842	850	858	865	873	881	889	
61 62	896 974	904 981	912 989	920 997	927 *005	93 <del>5</del>	943 *020	950 *028	958 *035	966 *043	1 0.8
63	75 051	059	066	074	082	089	097	105	113	120	2 1.6
64 65	128 205	136	143	151	159	166	174	182	189 266	197	3 2.4 4 3.2
66	282	289	220 297	228 30 <del>5</del>	236 312	243 320	251 328	259 335	343	274 351	5 4.0 6 4.8
67	358	366	374	381	389	397	404	412	420	427	7 5.6
68 69	435 511	519	450 526	458 534	465 542	473 549	481 557	488 56 <del>5</del>	496 572	504 580	8 6.4 9 7.2
570	587	595	603	610	618	626	633	641	648	656	
71 72	664 740	671 747	67 <u>9</u> 755	686 762	694 770	702 778	709 785	717	724 800	732 808	`
73	815	823	831	-838	846	853	861	793 868	876	884	
74 75	891 967	899 974	906 982	914 989	921	92 <u>9</u> *00 <u>5</u>	937 *012	944 *020	952 *027	95 <u>9</u> *03 <u>5</u>	
76	76 042	050	057	065	997 072	080	087	095	103	110	
77 78	118	125	133	140 215	148	155 230	163 238	170 245	178 253	185 260	
79	268	275	283	290	298	305	313	320	328	335	
580	343	350	358	365	373	380	388	395	403	410	17
81 82	418 492	425 500	433	440 515	448 522	45 <del>5</del> 530	462 537	545	477 552	48 <u>5</u> 559	10.7
83	567	574	582	589	597	604	612	619	626	634	2 1.4 3 2.1
84 85	641 716	649 723	656 730	664 738	745	678 753	686 760	693 768	701	708 782	4 2.8
86	790	797	805	812	819	827	834	842	849	856	5 3.5 6 4.2
87 88	864 938	871 945	879 953	886 960	893 967	90 <u>1</u> 97 <u>5</u>	908 982	916	923 997	930 *004	7 4.9 8 5.6
89	77 012	019	026	034	041	048	056	063	070	078	9 6.3
590	085	093	100	107	115	122	129	137	144	151	
91 92	6 159. 232	166	173 247	181 254	188 262	195 269	203	283	217	225	
93	305	313	320	327	335	342	349	357	364	371	
94 95	379 452	386 459	393 466	40I 474	408 481	415	422 495	503	437	444 517	
96	525	532	539	546	554	561	568	576	583	590	
97 98	597 670	605	612	619	627	634 706	641 714	648 721	656 728	735	
99	743	750	757	764	772	779	786	793	108	735 808	
600	815	822	830	837	844	851	859	866	873	880	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

12					IA	BLE :	l.				
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
600	77 815	822	830	837	844	851	859	866	873	880	
01	887	893	902	909	916	924	931	938	945	952.	
02	960 78 032	967 039	974 <b>o</b> 46	981 053	988 061	996 068	*003 075	*010	*017 089	*025	
04	104	III	118	125	132	140	147	154	161	168	* -
05	176	183	190	197	204	211	219	226	233	240	18
06	247	254	262	269	276	283	290 362	297	305	312	10.8
07 08	319 390	326 398	33 <u>3</u> 40 <u>5</u>	340 412	347 419	35 <del>5</del> 426	433	369 440	376 447	38 <u>3</u> 455	2 1.6
09	462	469	476	483	490	497	504	512	519	526	3 2.4 4 3.2
610	533	540	547	554	561	569	576	583	590	597	5 4.0
11 12	604 675	611	689	625 696	633 704	640 711	647	65 <u>4</u> 72 <u>5</u>	661 732	668 739	64.8 75.6
13	746	753	760	767	774	781	789	796	803	810	8 6.4
14	817	824	831	838	845	852	859	866	873	880	9 7.2
15 16	888 958	89 <del>5</del> 965	902 972	909 979	916 986	923 993	930 * <b>0</b> 00	937 * <b>0</b> 07	944	951 *021	
17	79 029	036	043	050	057	064	071	078	085	092	
18	099	106	113	120	127	134	141	148	155	162	
19 <b>620</b>	169	246	253	190 260	267	204	211	218	225	302	
21	309	316	323	330	337	344	351	358	365	372	7
22	379	386	393	400	407	414	421	428	435	442	1 0.7
23	449	456	463	470	477	484	491	498	505	511	$   \begin{array}{c c}     2 & 1.4 \\     3 & 2.1   \end{array} $
24 25	518 588	52 <u>5</u> 59 <u>5</u>	532 602	539 609	546 616	553 623	560 630	567 637	574 644	581 650	42.8
26	657	664	671	678	685	692	699	706	713	720	5 3.5 6 4.2
27	727	734	741	748	754	761	768	775	782	789	7 4.9
28 29	796 865	803 872	810 879	817 886	824	831 900	837 906	844 913	851 92 <b>0</b>	858 927	8 5.6 9 6.3
630	934	941	948	955	962	969	975	982	989	996	
31	80 003	010	017	024	030	037	044	051	058	063	
32 33	072 140	079	085 154	092 161	168	106	113	120	127	134	
34	209	216	223	229	236	243	250	257	264	271	
1 35	277	284	291	298	305	312	318	325	332	339	
36 37	346	353	359 428	366 434	373 441	380 448	3 <sup>8</sup> 7 45 <del>5</del>	393 462	400 468	407	6
38	414 482	489	496	502	509	516	523	530	536	475 543	$ \begin{array}{c c} 1 & 0.6 \\ 2 & 1.2 \end{array} $
39	550	557	564	570	577	584	591	598	604	611	3 1.8
640	618	625	632	706	645	652	726	665	672	679	$\begin{array}{c c} 4 & 2.4 \\ 5 & 3.0 \end{array}$
41 42	754	693 760	767	774	713 781	720 787	794	733 801	740 808	747 814	6 3.6
43	821	828	835	841	848	855	862	868	875	882	$   \begin{array}{c}     7 & 4.2 \\     8 & 4.8   \end{array} $
44	889.	895 963	902 969	909 976	916 983	922	929 996	936 *003	943	949	9 5.4
45 46	956 81 023	030	037	043	050	990 057	064	070	077	*017 084	
47	090	097	104	111	117	124	131	137	144	151	
48 49	158 224	164 231	171 238	178 245	184 251	191 258	198 26 <del>5</del>	204 271	211 278	218 28 <del>5</del>	
650	291	298	305	311	318	325	331	338	$\frac{2}{34\overline{5}}$	351	
N.	0	1	2	3	4	5	6	7	8	9	Prop Pts.

\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		-	0 1	g	. 1		-		_	_ 1	-
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
650	81 291	298	305	311	318	325	331	338	345	351	
51 52	358 425	36 <del>5</del> 431	371 438	378 445	38 <del>5</del> 451	391 458	398 46 <del>5</del>	40 <u>5</u> 47 I	411	418 48 <del>5</del>	
53	491	498	505	511	518	525	531	538	544	551	
54	558	564	571	578	584	591	598	604	611	617	
55 56	624	631 697	704	710	651 717	657 723	664	671	677	684 7 <u>5</u> 0	
57	757	763	770	776	783	790	730	737 803	743   809	816	
58	823	829	836	842	849	856	862	869	875	882	
59	889	895	902	908	913	921	928	935	941	948	
660	954	961	968	974	046	987 053	994	*000	*007	*014	7
62	086	027	033	105	112	119	125	132	073 138	07 <u>9</u>	1 0.7
63	151	158	164	171	178	184	191	197	204	210	$   \begin{array}{c c}     2 & 1.4 \\     3 & 2.1   \end{array} $
64 65	217 282	223 289	230	236	243 308	24 <u>9</u> 31 <u>5</u>	256	263	269	276	4 2.8
66	347	354	295 360	302 367	373	380	321 387	328	334 400	34I 406	5 3.5 6 4.2
67	413	419	426	432	439	445	452	458	465	471	7 4.9
68 69	478 543	484	491 556	497 562	504 569	510	517 582	523 588	530 595	536 601	8 5.6 9 6.3
670	607	549 614	620	627	633	640	646	653	659	666	0,0.0
71	672	679	685	692	698	703	711	718	724	730	
72 73	737 802	743 808	750 814	756 821	763 827	769 834	776 840	782 847	789	795 86 <b>o</b>	
74	866	872	879	885	892	898	905	911	918	924	
75	930	937	943	950	956	963	969	975	982	988	
76	995	*001	*008	*014	*020	*027	*033	*040	*046	*052	
77 78	83 059	065	072 136	078	08 <del>5</del>	155	097	168	174	181	
79	187	193	200	206	213	219	225	232	238	245	
680	251	257	264	270	276	283	289	296	302	308	1.0
81	31 <u>5</u> 378	321	327	334 398	340 404	347 410	353	359 423	366 429	372 436	10.6
82 83	442	448	39 <sup>1</sup> 45 <sup>5</sup>	461	467	474	480	487	493	499	2 1.2
84	506	512	518	525	531	537	544	550	556	563	$   \begin{array}{c c}     3 & 1.8 \\     4 & 2.4   \end{array} $
85 86	569 632	575 639	582	588	594 658	664	670	613	620	626.	5 3.0
87	696	702	708	713	721	727	734	740	746		6 3.6 7 4.2
88	759	765	771	778	784	790	797 860	803	809	753 816	84.8
89	822	828	835	841	847	853 916		866	872	879 942	9 5.4
690 91	948	891 954	897 960	904	910	979	923 985	929	935	*004	
92	84 011	017	023	029	036	042	048	055	061	067	
93	973	080	086	092	098	105	111	117	123	130	
94 95	136 198	142	148	155	161	167 230	173 236	180	186	192 255	
96	261	267	273	280	286	292	298	305	311	317	
97	323 386	330	336	342	348	354	361	367	373	379	
98 99	386 448	392 454	398 460	464	410	417	42 <u>3</u> 48 <u>5</u>	429 491	435	504	
700	510	516	522	528	535	541	547	553	559	566	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

4 TABLE 1.										
0	1	2	3	4	5	6	7	8	9	Prop. Pts.
84 510	516	522	528	533	541	547	553	559	566	
572	578	584	590	597	603	609	615	621	628	
634 606				-						-
819	825	831	837	844	850	856	862	868	874	
				905	911	917	1			7
									997	1 0.7 2 1.4
065	071	077	083	089	095	101	107	114	120	3 2.1
126	132		144	150	156	163	169	175	181	4 2.8 5 3.5
	193		205	211	217	224	230	236	242	64.2
									364	7 4.9 8 5.6
		_			400	406	412	418	425	96.3
431	437	443	449	455			473	479	485	
				-		-		_		
612	618	625	631	637			655	661		
673	679	685	691	697	703	709	715	721	727	
733	739	745	751	757			775	<u> </u>		
794 854					824		806			6
914	920	926	932	938	944	950	956	962	968	$ \begin{array}{c c} 1 & 0.6 \\ 2 & 1.2 \end{array} $
974	980	986	992	998	*004	*010	*016	*022	*028	3 1.8
										4 2.4 5 3.0
						1 -				63.6
213	219	225	231	237	243	249	255	261	267	7 4.2 8 4.8
			291							95.4
			469		481				504	;
510	516	522	528	534	540	546	552	558	564	
570	576	581		593	599	605		617	623	
688	694	700	705	711	717	723	729		741	15
747	753	759	764	770	776	782	788	794	800	1 0.5
806	812	817	823	829	835	841	847	853		21.0
										3 1.5 4 2.0
					-					5 2 5
87 040	046	052	058	064	070	975	180	087	093	63.0 73.5
	- 1									84.0
216								262		9 4.5
274	280	286	291	297	303	309	315	320	326	
332	338	344	349	355	361	367	373	379	384	
390 448										
	512	518				541	547	552	558	
0	1	2	3	4	5	6	7	8	9	Prop. Pts.
	84 510 572 634 696 757 819 880 942 85 003 126 187 248 309 370 431 491 552 673 733 794 854 914 86 034 094 153 213 273 392 451 570 688 747 866 864 923 982 87 040 099 157 216 274 339 854 974 856 864 974 866 864 974 866 864 974 866 864 974 866 864 974 866 864 974 876 876 876 876 876 876 876 876	84         510         516           572         578         634         640         702           757         763         819         825         887         948         825         887         948         965         971         126         132         187         193         248         254         399         315         370         376         431         437         491         497         552         558         612         618         679         733         739         794         800         854         860         914         920         980         854         860         914         920         980         866         034         040         094         100         153         219         273         279         332         338         390         451         5516         576         635         688         694         747         753         806         812         860         94         747         753         806         812         860         923         929         988         87         940         946         929         929         988         87         940         946         940         940	84         510         516         522           572         578         584         640         646         646         646         702         788         798         798         783         770         819         825         831         880         887         893         948         944         260         309         315         321         337         376         382         431         437         443         443         443         443         443         443         443         443         443         497         503         552         558         564         665         673         679         685         733         739         745         794         800         806         854         866         914         920         926         926         926         926         926         926	84 510         516         522         528           572         578         584         590           634         640         646         652           757         763         770         776           819         825         831         839           880         887         893         899           942         948         954         960           942         948         954         960           942         948         954         960           942         948         954         960           942         948         954         960           948         254         260         326           309         315         321         327           370         376         382         388           431         437         443         449           491         497         503         509           552         558         564         570           612         618         625         691           733         739         745         751           794         800         806	84         510         516         522         528         535           572         578         584         590         597           634         640         646         652         658           696         702         708         714         720           757         763         770         776         782           819         825         831         837         844           800         309         016         022         028           965         063         071         077         083         089           954         948         954         960         905           942         948         954         960         922         028           85         033         099         016         022         028           85         033         099         016         022         028           85         033         399         205         926         272         333           370         376         382         388         394         431         437         443         449         455         691         697         733	84 510         516         522         528         533         541           572         578         584         590         597         603           634         640         646         652         658         665           696         702         708         714         720         726           757         763         770         776         782         788           819         825         831         837         844         850           850         303         009         016         022         027         973           85         033         009         016         022         208         095           126         132         138         144         150         156           187         193         199         205         211         217           248         254         260         266         272         278           309         315         321         327         333         339           376         382         388         394         400           431         437         443         449         455         461	84         510         516         522         528         535         541         547           572         578         584         590         597         603         609           696         640         646         652         658         665         671           757         763         770         776         782         788         794           819         825         831         837         844         850         856           8003         099         016         022         028         034         040           065         071         077         083         089         095         101           126         132         138         144         150         156         163           187         193         199         205         211         217         224           248         254         260         266         272         278         285           309         315         321         327         333         339         345           370         376         382         388         394         400         406           431	84         510         516         522         528         535         541         547         553           572         578         584         590         597         603         609         615           696         702         708         714         720         726         733         739           757         763         770         776         782         788         794         800           819         825         831         837         844         850         856         862           85         003         009         016         022         028         034         040         046           065         071         077         083         089         995         101         107           126         132         138         144         150         156         163         169           187         193         199         205         211         217         224         230           248         254         260         266         272         278         285         291           379         376         382         388         394         400	84         510         516         522         528         533         541         547         553         559           634         640         646         652         658         665         667         677         683           696         702         708         714         720         726         733         739         743           757         763         770         766         782         788         794         800         808           880         887         893         899         905         911         917         924         930           85         033         009         016         022         028         034         040         046         052           126         132         138         144         150         156         163         169         173           187         193         199         205         211         212         224         230         236           248         254         260         266         272         278         285         291         297           309         315         321         327         333         339 <th>84         510         516         522         528         533         541         547         553         559         566           572         578         584         590         597         603         609         615         621         628           696         702         708         714         720         726         733         739         743         751           757         763         770         776         782         788         794         800         807         813           819         825         831         837         844         850         865         862         868         874           85         063         070         016         022         028         034         040         046         052         053           065         071         077         083         089         095         101         107         114         120         066         202         028         034         040         046         052         058         058         091         107         114         120         052         115         1107         114         120         065         <td< th=""></td<></th>	84         510         516         522         528         533         541         547         553         559         566           572         578         584         590         597         603         609         615         621         628           696         702         708         714         720         726         733         739         743         751           757         763         770         776         782         788         794         800         807         813           819         825         831         837         844         850         865         862         868         874           85         063         070         016         022         028         034         040         046         052         053           065         071         077         083         089         095         101         107         114         120         066         202         028         034         040         046         052         058         058         091         107         114         120         052         115         1107         114         120         065 <td< th=""></td<>

N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
750	87 506	512	518	523	529	535	541	547	552	558	
51 52	564 622	570 628	576	581	587	593	599	604	610	616	
53	679	685	633	639	703	651 708	656	720	726	674 731	
54	737	743	749 806	754 812	760	766	772	777	783	789	
55 56	795 852	800 858	864	869	818	823 881	829 887	835	841	904	
57	910	915	921	927	933	938	944	950	955	961	
58 59	967 88 024	973	978	984	990	996	*001 058	*007	*013 070	*018	
760	180	087	093	098	104	110	116	121	127	133	
61 62	138	144 201	150	156	161	167	173	173	184	190	6
63	195 252	258	264	213	275	224 281	230	235	241	304	$\begin{array}{c c} & 1 & 0.6 \\ & 2 & 1.2 \end{array}$
64 65	309	315	321	326	332	338	343	349	355	360	3 1.8 4 2.4
66	366 423	372 429	377 434	383 440	389 446	395 451	457	406 463	412	417	53.0
67 68	480	485	491	497	502	508	513	519	525	530	7 4.2
69	536 593	542 598	547 604	553 610	559 615	564 621	570 627	576	581	587 643	8 4.8 9 5.4
770	649	655	660	666	672	677	683	689	694	700	
71 72	705 762	711	717 773	722 779	728 784	734 790	739 795	745 801	750 807	756 812	
73	818	824	829	835	840	846	852	857	863	868	
74 75	874 930	880 936	885 941	891 947	897 953	902 958	908 964	913 969	919	92 <u>5</u> 981	
76	986	992	997	*003	*009	*014	*020	*025	*031	*037	
77 78	89 042 098	048 104	053	059	064 120	070 126	076	081	087	092 148	
79	154	159	165	170	176	182	131	137	143	204	
780	209	215	221	226	232	237	243	248	254	260	15
81 82	265 321	271 326	276 332	282 337	287 343	293 348	298 354	304	365	315	10.5
83	376	382	387	393	398	404	409	415	421	426	2 1.0
84 85	432 487	437 492	443 498	448 504	454 509	459	46 <del>5</del> 520	470 526	476 531	481 537	$ \begin{array}{c c} 3 & 1.5 \\ 4 & 2.0 \end{array} $
86	542	548	553	559	564	570	575	581	586	592	5 2.5 6 3.0
87 88	597 653	603 658	609 664	669	620 675	625 680	631 686	636	642 697	647 702	7 3.5 8 4.0
89	708	713	719	724	730	735	741	746	752	757	9 4.5
790 91	763	768	774	779	785	790	796	801	807 862	812	
92	873	823 878	829 883	834 889	840 894	845 900	905	856 911	916	922	
93	927	933	938	944	949	955	960	966	971	977	
94 95	982 90 037	988 042	993 048	998 053 108	*004 059	*009 064	*015 069	*020 075	*026 080	*031 086	
96	160	097	102		113	119	124	129	135	140	
97 98	146	151 206	157 211	162 217	168	173 227	179 233	184	189 244	19 <del>5</del> 249	
99	255	260	266	271	276	282	287	293	298	304	
800	309	314	320	325	331	336	342	347	352	358	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

-	IADLE I.											
	N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
	800	90_309	314	320	325	331	336	342	347	352	358	•
	01 02 03	363 417 472	369 423 477	374 428 482	380 434 488	38 <del>5</del> 439 493	390 445 499	396 450 504	401 455 509	407 461 51 <del>5</del>	412 466 <b>520</b>	
	04 05 06	526 580 634	531 585 639	536 590 644	542 596 650	547 601 655	553 607 660	558 612 666	563 617 671	569 623 677	574 628 682	
	07 08 <b>0</b> 9	687 741 795	693 747 800	698 752 806	703 757 811	709 763 816	714 768 822	720 773 827	725 779 832	730 784 838	736 789 843	
ı	810	849	854	859	865	870	875	188	886	891	897	1.0
	11 12 13	902 956 91 009	907 961 014	913 966 020	918 972 025	924 977 030	929 982 <b>0</b> 36	934 988 <b>041</b>	940 993 <b>0</b> 46	945 998 <b>052</b>	950 *004 057	1 0.6 2 1.2
	14 15 16	062 116 169	068 121 174	073 126 180	078 132 185	084 137 190	089 142 196	094 148 201	100 153 206	105 158 212	110 164 217	3 1.8 4 2.4 5 3.0 6 3.6
	17 18 19	222 275 328	228 281 334	233 286 339	238 291 344	243 297 350	249 302 355	254 307 360	259 312 365	26 <del>5</del> 318 371	270 323 376	7 4.2 8 4.8 9 5.4
	820	381	387	392	397	403	408	413	418	424	429	
	21 22 23	434 487 540	440 492 <b>5</b> 45	44 <del>5</del> 498 551	450 503 556	455 508 561	461 514 566	466 519 572	47 I 524 577	477 529 582	482 535 587	
	24 25 26	593 645 698	598 651 703	603 656 709	609 661 714	614 666 719	619 672 724	624 677 730	630 682 73 <del>5</del>	63 <u>5</u> 687 740	640 693 745	
	27 28 29	751 803 855	756 808 861	761 814 866	766 819 871	772 824 876	777 829 882	782 834 887	787 840 892	79 <u>3</u> 845 897	798 850 903	
	830	908	913	918	924	929	934	939	944	950	955	
	31 32 33	960 92 012 065	965 018 070	971 02 <u>3</u> 075	976 028 080	981 033 085	986 038 091	991 044 096	997 049 101	*002 054 106	*007 059	1 0.5 2 1.0
	34 35 36	117 169 221	122 174 226	127 179 231	132 184 236	137 189 241	14 <u>3</u> 19 <u>5</u> 247	148 200 252	153 205 257	158 210 262	163 215 267	3 1.5 4 2.0 5 2.5 6 3.0
	37 38 39	273 324 376	278 330 381	28 <u>3</u> 335 387	288 340 392	293 345 397	298 350 402	304 355 407	309 361 412	314 366 418	319 371 423	73.5 84.0 94.5
ı	840	428	433	438	443	449	454	459	464	469	474	
	41 42 43	480 531 583	48 <del>5</del> 536 <b>5</b> 88	490 542 593	495 547 598	500 552 603	505 557 609	511 562 614	516 567 619	521 572 624	526 578 629	
	44 45 46	634 686 <b>7</b> 37	639 691 742	64 <u>5</u> 696 747	650 701 752	65 <del>5</del> 706 758	660 711 763	665 716 768	670 722 773	675 727 778	681 732 783	
	47 48 49	788 840 891	79 <u>3</u> 84 <u>5</u> 896	799 850 901	804 853 906	869 860 911	814 865 916	819 870 921	824 875 927	829 881 932	834 886 937	
1	850	942	947	952	957	962	967	973	978	983	988	
	N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
850	92 942	947	952	957	962	967	973	978	983	988	
51	993	998	*003	*008	*013	*018	*024	*029	*034	*039	
52 53	93 04 <u>4</u> 09 <u>5</u>	100	105	110	064	069 120	075	080	085	090	
54	146	151	156	161	166	171	176	181	186	192	
55 56	197 247	202	207 258	263	217	222 273	227 278	232 283	237 288	242 293	16
57 58	298 349	303 354	308 359	313 364	318	323	328	334	339 389	344	$ \begin{array}{c c} 1 & 0.6 \\ 2 & 1.2 \end{array} $
59	399	404	409	414	420	37 <u>4</u> 42 <u>5</u>	379 430	38 <u>4</u> 435	440	39 <u>4</u> 445	3 1.8 4 2.4
860	450	455	460	465	470	475	480	485	490	495	5 3.0
61 62	500 551	505 556	510 561	515	520 571	526 576	531	536 586	54I 59I	546 596	$\begin{array}{c} 6 & 3.6 \\ 7 & 4.2 \end{array}$
63	601	606	611	616	621	626	631	636	641	646	8 4.8 9 5.4
64 65	651 702	656 707	661 712	666	671 722	676 727	682 732	687 737	692 742	697 747	80.4
66	752	757	762	767	772	777	782	787	792	797	
67 68	802 852	807 857	812	817	822 872	827 877	832 882	837 887	842 892	847 897	
69	902	907	912	917	922	927	932	937	942	947	
870	952	957	962	967	972	977	982	987	992	997	15
71 72	94 002 052	007 057	012	067	022	027	032	037	042	047	10.5
73	101	106	III	116	121	126	131	136	141	146	2 1.0 3 1.5
74 75	151 201	156 206	161	166 216	171 221	176 226	181	186 236	191	196 245	4 2.0
76	250	255	260	265	270	275	280	285	290	295	5 2.5 6 3.0
77 78	300	303	310	31 <del>5</del> 364	320 369	325	330	335	340	345	7 3.5 8 4.0
79	349 399	354 404	<b>359</b> 409	414	419	374 424	379 429	384 433	389 438	394 443	9 4.5
880	448	453	458	463	468	473	478	483	488	493	1
81 82	498 547	503	507	512 562	517 567	522 571	527 576	532 581	537 586	542 591	
83	596	552 601	557 606	611	616	621	626	630	635	640	
84 85	645 694	650 699	655 704	660 709	66 <del>5</del>	670 719	67 <del>5</del> 724	680 729	685	689 738	
86	743	748	753	758	763	768	773	778	734 783	787	4
87 88	792 841	797 846	802	807	812 861	817 866	822	827	832 880	836	10.4
89	890	895	900	856 905	910	915	919	876 924	929	885 934	2 0.8 3 1.2
890	939	944	949	954	959	963	968	973	978	983	$ \begin{array}{c c} 4 & 1.6 \\ 5 & 2.0 \end{array} $
91 92	988 95 036	993	998 046	*002 051	*007 056	*012 061	*017 066	*022 071	*027 <b>0</b> 75	*032 080	6 2.4 7 2.8
93	085	090	095	100	103	109	114	119	124	129	8 3.2
94 95	134 182	139	143 192	148	153	158	163	168 216	173 221	177 226	9 3.6
96	231	236	240	245	250	255	260	265	270	274	
97 98	279 328	284	289	294	299	303	308	313 361	318 366	323	
99	376	332 381	337 386	342 390	347 395	352 400	35 <u>7</u> 40 <u>5</u>	410	415	371 419	
900	424	429	434	439	444	448	453	458	463	468	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

8					IA	BLE I	•				
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
900	95 424	429	434	439	444	448	453	458	463	468	*
01	472	477	482	487	492	497	501	506	511	516	
02 03	521 569	525 574	530 578	535 583	540 588	545 593	5 <u>5</u> 0 598	554 602	559 607	564 612	
04	617	622	626	631	636	641	646	650	655	660	
05	663	670	674	679	684	689	694	698	703	708	
06	713	718	722	727	732	737	742	746	751	756	
07	761 809	766	818	775 823	780 828	785	789	794	799	804 852	
08 09	856	813	866	871	875	832 880	837 885	842 890	847 895	899	
910	904	909	914	918	923	928	933	938	942	947	
11	952	957	961	966	971	976	980	985	990	995	5
12 13	999 96 047	*004 052	*009	*014 061	*019 066	*023 071	*028 076	*033	*038	*042 090	$   \begin{array}{c c}     1 & 0.5 \\     2 & 1.0   \end{array} $
	90 047		104	109		118	123	128		137	3 1.5
14 15	142	147	152	156	114	166	171	175	133	185	42.0
16	190	194	199	204	209	213	218	223	227	232	5 2.5 6 3.0
17	237	242	246	251	256	261	265	270	275	280	7 3.5
18 19	284 332	289 336	294 341	298 346	303	308 355	313	317 365	369	327 374	8 4.0 9 4.5
920	379	384	388	393	398	402	407	412	417	421	0,570
21	426	431	435	440	445	450	454	459	464	468	
22	473 <b>52</b> 0	478	483	487	492	497	501	506	511	515 562	
23	567	525	530	534 581	539 586	544	548	553 600	558 60 <del>3</del>	609	
24 25	614	572	577 624	628	633	591 638	595 642	647	652	656	
26	66 i	666	670	675	680	683	689	694	699	703	
27	708	713	717	722	727	731	736	741	745	750	
28 29	755 802	759 806	764	769	774 820	778 825	783 830	788 834	792 839	797 844	
930	848	853	858	862	867	872	876	188	886	890	
31	895	900	904	909	914	918	923	928	932	937	4
32	942	946	951	956	960	963	970	974	979	984	10.4
33	988	993	997	*002	*007	*011	*016	*021	*025	*030	2 0.8 3 1.2
34 35	97 035 081	039	044	049	100	058 104	063	067	072	077	4 1.6
36	128	132	137	142	146	151	155	160	165	169	$\begin{array}{c} 5 & 2.0 \\ 6 & 2.4 \end{array}$
37	174	179	183	188	192	197	202	206	211	216	7 2.8
38 39	220 267	225	230	234	239	243 290	248	253 299	257 304	308	83.2 93.6
940	313	317	322	327	331	336	340	345	350	354	0,0.0
41	359	364	368	373	377	382	387	391	396	400	
42	405	410	414	419	424	428	433	437	442	447	
43	451	456	460	465	470	474	479	483	488	493	
44	497 543	502	506	511	516	520 566	523 571	529 575	534 580	53 <u>9</u> 58 <u>5</u>	
46	589	594	598	603	607	612	617	621	626	630	
47	633	640	644	649	653	658	663	667	672	676	-
48	681 727	685	690 736	695	745	704 749	708 754	713	717	722 768	
950	772	777	782	786	791	795	800	804	809	813	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
74.		-	1		-	1	1	_			Pe - 400

N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
			782	786							Trop. 1 ts.
950 51	97 772	777 823	827	832	791 836	795 841	800	804	809 85 <del>5</del>	813	
52	864	868	873	877	882	886	891	896	900	905	
53	909	914	918	923	928	932	937	941	946	950	
54 55	955	959	964	968	973	978 023	982 028	987 032	991 937	996 041	
56	046	050	055	059	064	<b>o</b> 68	073	078	082	087	,
57	100	096	100	105	109	114	118	123	127	132	
58 59	137	141	146	150	155	159 204	164 209	168 214	173 218	223	
960	227	232	236	241	245	250	254	259	263	268	
61	272	277	281	286	290	295	299	304	308	313	5
62 63	318 363	322 367	327 372	331 376	336	340 385	345	349 394	354 399	358 403	1 0.5 2 1.0
64	408	412	417	421	426	430	435	439	444	448	3 1.5
65	453	457	462	466	471	475	480	484	489	493	4 2.0 5 2.5
66	498	502	507	511	516	520	525	529	534	538	63.0
67 68	543 588	547 592	552 597	556 601	605	565 610	570 614	574 619	579 623	583 628	73.5 84.0
69	632	637	641	646	650	655	659	664	668	673	94.5
970	677	726	686	691	695	700	704	709	713	717	
71 72	722 767	771	731 776	735 780	740 784	744 789	749 793	753 798	802	762 807	
73	811	816	820	823	829	834	838	843	847	851	- 3
74 75	856 900	860 903	86 <del>5</del> 909	869 914	874 918	878 923	883 927	887	892 936	896	
76	945	949	954	958	963	967	972	932 976	981	941 98 <b>5</b>	
77	989	994	998	*003	*007	*012	*016	*021	*025	*029	
73 79	99 °34 °078	038	043	047 092	052	100	105	109	069	074	
980	123	127	131	136	140	145	149	154	158	162	-5
81	167	171	176	180	185	.189	193	198	202	207	4
82 83	211 255	216 260	220 264	269	229 273	233 277	238 282	242 286	247 291	251 295	1 0.4 2 0.8
84	300	304	308	313	317	322	326	330	335	339	3 1.2
85	344	348	352	357	361	366	370	374	379	383	4 1.6 5 2.0
86	388	392 436	396 441	401	405	410	414	463	4 <sup>2</sup> 3	427	62.4
87 88	432 476	480	484	489	449 493	<b>454</b> 498	502	506	511	47I 515	7 2.8 8 3.2
89	520	524	528	533	537	542	546	550	555	559	9 3.6
990	564 607	568 612	572 616	577 621	581 62 <del>5</del>	585 629	590 634	594 638	599 642	603	
92	651	656	660	664	669	673	677	-682	686	691	
93	695	699	704	708	712	717	721	726	730	734	
94 95	739 782	<b>74</b> 3 787	747 791	752 795	756 800	760 804	76 <del>5</del> 808	769 813	774 817	778 822	1 - 1
96	826	830	835	839	843	848	852	856	861	865	
97	870	874	878	883	887	891	896	000	904 948	909	
98	913 957	917 961	922 965	926 970	930 974	935 978	939 983	944 987	991	952 996	
1000	00 000	004	009	013	017	022	026	030	035	039	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

20				-							
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
1000	000 000	043	087	130	174	217	260	304	347	391	
1001 1002	<b>434</b> 868	477	521	564 998	608 * <b>0</b> 41	651 *084	694 *128	738 *171	781 *214	824 *258	
1002	001 301	344	954 388	431	474	517	561	604	647	690	1 44
1004	734	777	820	863	907	950	993	*036	*o8o	*123	1 4.4
1005 1006	002 166 598	209 641	252 684	296 727	339 771	382 814	425 857	900	943	555 986	2 8.8 3 13.2
1007	003 029	073	116	159	202	245	288	331	374	417	4 17.6 5 22.0
1008	461 891	934	547 977	*020	633 *063	676 *106	719 *149	762 *192	805 *235	848 *278	6 26.4
1010	004 321	364	407	450	493	536	579	622	665	708	7 30.8 8 35.2
1011	751	794	837	880	923	966	*009	*052	*095	*138	9 39.6
1012 1013	005 180 609	223 652	266 <b>6</b> 95	309 738	352 781	395 824	438 867	481 909	524 952	5 <sup>6</sup> 7 995	
1014	006 038	081	124	166	209	252	295	338	380	423	43
1015 1016	466 894	509 936	552 979	*022	637 *o65	680 *107	723 *150	765 *193	808 *236	851 *278	1 4.3
1017	007 321	364	406	449	492	534	577	620	.662	705	2 8.6 3 12.9
1018 1019	008 174	790	833	876	918	961 387	*004 430	*046 472	*089 515	*132 558	4 17.2
1020	600	643	685	728	770	813	856	898	941	983	5 21.5 6 25.8
1021	009 026	068	III	153	196	238	281	323	366	408	7 30.1
1022 1023	451 876	493 918	536 961	578 *003	*045	663 *088	706 *130	748 *173	791 *215	833 *258	8 34.4 9 38.7
1024	010 300	342	385	427	470	512	554	597	639	681	
1025 1026	724 011 147	766	809	851 274	893	936 359	978 401	*020 444	*063 486	*105 528	
1027	570	613	655	697	740	782	824	866	909	951	42
1028 1029	993	*035 458	*078 500	*120 542	*162 584	*204 626	*247 669	*289	*331 753	*373 795	1 4,2 2 8,4
1030	837	879	922	964	*006	*048	*090	*132	*174	*217	3 12.6
1031	013 259	301	343	385	427	469	511	553	596	638	4 16.8 5 21.0
1032	680	722	764 184	806	268	310	932 352	395	*016 437	*058 479	6 25.2
1034	521	563	605	647	689	730	772	814	856	898	7 29.4 8 33.6
1035 1036	940 015 360	982 402	*024	*066 485	*108	*150 569	*192 611	*234 653	*276	*318	9 37.8
1037	779	821	863	904	5 <sup>2</sup> 7 946	988	*030	*072	*114	737 *156	
1038	016 197	239	281	323	365	407	448	490	532	574	1.44
1039 1040	017 033	657 075	699	741	783	824 242	284	908 326	950 367	409	1 4.1
1041	451	492	534	576	618	659	701	743	784	826	2 8.2
1042	868 018 284	909	951	993	*034	*076	*118	*159	*201	*243	3 12.3 4 16.4
1043 1044	700	326 742	368 784	825	451 867	492 908	534 950	576	*033	659 * <b>075</b>	5 20.5
1044	019 116	158	199	241	282	324	366	992 407	449	490	6 24.6 7 28.7
1046	532	573	615	656	698	739	781	822	864	905	8 32.8 9 36.9
1047 1048	947 020 361	988	*030 444	*071 486	*113 527	*154 568	*195 610	*237 651	*278 693	*320 734	مامونو
1049	775	817	858	900	941	982	*024	*065	*107	*148	
1050	021 189	231	272	313	355	396	437	479	520	561	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

N.		0	1	2	3	4	5	6	7	8	9	Prop. Pts.
1050	021		231	272	313	355	396	437	479	520	561	
1051 1052 1053		603 016 428	644 057 470	685 098 511	727 140 552	768 181 593	809 222 635	851 263 676	892 305 717	933 346 <b>75</b> 8	974 <b>3<sup>8</sup>7</b> 799	42
1054 1055 1056	023	841 252 664	882 294 705	923 335 746	964 376 787	*005 417 828	*047 458 870	*088 499 911	*129 541 952	*170 582 993	*211 623 *034	1 4.2 2 8.4 3 12.6
1057 1058 1059	024	075 486 896	116 527 937	157 568 978	198 609 *019	239 650 * <b>o</b> 60	280 691 *101	321 732 *142	363 773 *183	404 814 *224	445 855 *265	$ \begin{array}{c c} 4 & 16.8 \\ 5 & 21.0 \\ 6 & 25.2 \end{array} $
1060	025	306	347	388	429	470	511	552	593	634	674	7 29.4 8 33.6
1061 1062 1063	026	715 125 533	756 165 574	797 206 615	838 247 656	879 288 697	920 329 737	961 370 778	*002 411 819	*043 452 860	*084 492 901	9 37.8
1064 1065 1066		942 350 <b>75</b> 7	982 390 798	*023 431 839	*064 472 879	*105 513 920	*146 553 961	*186 594 *002	*22 <u>7</u> 63 <u>5</u> *042	*268 676 *083	*309 716 *124	41 1 4.1
1067 1068 1069		57 I 978	205 612 *018	246 653 *059	287 693 *100	327 734 *140	368 775 *181	409 815 *221	449 856 *262	490 896 *303	531 937 *343	2 8.2 3 12.3 4 16.4
1070	029		424	465	506	546	587	627	668	708	749	$ \begin{array}{c c} 5 & 20.5 \\ 6 & 24.6 \end{array} $
1071 1072 1073	030	7 <sup>8</sup> 9 195 600	830 235 640	871 276 681	911 316 721	952 357 762	992 397 802	*033 438 843	*073 478 883	*114 519 923	*154 559 964	7 28.7 8 32.8 9 36.9
1074 1075 1076	031	004 408 812	045 449 853	085 489 893	126 530 933	166 570 974	206 610 *014	247 651 *054	287 691 *095	328 732 *135	368 772 *175	
1077 1078 1079	032 033	216 619 021	256 659 062	296 699 102	337 740 142	377 780 182	417 820 223	458 860 263	498 901 303	538 941 343	•578 981 384	1 4.0 2 8.0
1080		424	464	504	544	585	625	663	705	745	785	3 12.0
1081 1082 1083	034	826 227 628	866 267 669	906 308 709	946 348 749	986 388 789	*027 428 829	*067 468 869	*107 508 909	*147 548 949	*187 588 989	$\begin{array}{c} 4 & 16.0 \\ 5 & 20.0 \\ 6 & 24.0 \\ 7 & 28.0 \end{array}$
1084 1085 1086	035	029 430 830	069 470 870	109 510 910	149 550 950	190 590 990	230 630 *030	270 670 *070	310 710 *110	350 750 *150	390 790 *190	8 32.0 9 36.0
1087 1088 1089	036 037	629	269 669 068	309 709 108	349 749 148	389 789 187	429 828 227	469 868 267	509 908 307	549 948 347	589 988 387	89
1090		426	466	506	546	586	626	665	705	745	785	1 3.9
1091 1092 1093	038	825 223 620	865 262 660	904 302 700	914 342 739	984 382 779	*024 421 819	*064 461 859	*103 501 898	*143 541 938	*183 580 978	2 7.8 3 11.7 4 15.6 5 19.5
1094 1095 1096	039	017 414 811	057 454 8 <b>5</b> 0	097 493 890	136 533 929	176 573 969	216 612 *009	255 652 *048	295 692 *088	335 731 *127	374 771 *167	6 23.4 7 27.3 8 31.2
1097 1098 1099	040	207 602 998	246 642 *037	286 681 *077	325 721 *116	36 <u>5</u> 761 *156	405 800 *195	444 840 *235	484 879 *274	523 919 *314	563 958 *353	9 35.1
1100	041		432	472	511	551	590	630	669	708	748	
N.		0	1	2	3	4	5	6	7	8	9	Prop. Pts.



## TABLE II.

## CONSTANTS WITH THEIR LOGARITHMS.

	Number.	Logarithm.
Ratio of circumference to diameter, $\pi$ ,	3.14159265	0-49714 99
π <sup>3</sup> ,	9.86960440	0.99429 97
2π,	6.28318531	0.79817 99
$\sqrt{\pi}$ ,	1.77245385	0.24857 49
Number of degrees in circumference,	360°	2.55630 25
minutes	21600'	4-33445 38
seconds	1296000"	6.11260 50
Degrees in arc equal to radius,	570-2957795	1.75812 26
Minutes	3437 - 74677	3-53627 39
Seconds	206264".806	5-31442 51
Length of arc of 1 degree,	.01745329	8.24187 74-10
ı minute,	.00029089	6.46372 61-10
r second,	.000004848	4.68557 49-10
Number of hours in 1 day,	24	1.38021 12
minutes	1440	3.15836 25
seconds .	86400	4.93651 37
Number of days in Julian year,	365.25	2.56259 02
Naperian base,	2.718281828	0.43429 45
Modulus of common logarithms,	0.434294482	9.63778 43-10
Hours in which earth revolves through		
arc equal to radius,	3.8197186	0.58203 14
Minutes of time	229.18312	2.36018 26
Seconds of time	13750.987	4.13833 39



### TABLE III.

FOR

# SINES AND TANGENTS OF SMALL ANGLES.

#### TO FIND THE SINE OR TANGENT:

Log sin  $\alpha = \log \alpha$  (in seconds) + S.

Log tan  $\alpha = \log \alpha$  (in seconds) + T.

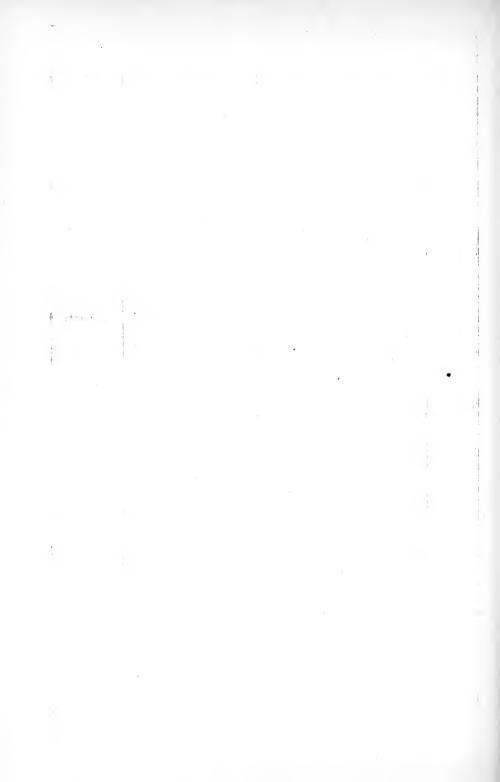
### TO FIND A SMALL ANGLE FROM ITS SINE OR TANGENT:

Log  $\alpha$  (in seconds) = log sin  $\alpha + S'$ .

Log  $\alpha$  (in seconds) = log tan  $\alpha + T$ .

			0°			
"	,	L. Sin.	S	T	S'	T'
0 60 120 180	0 I 2	6.46373	4.68557 .68557 .68557	4.68557 .68557 .68557	5.31443 .31443 .31443	5.31443 .31443 .31443
240	3 4	.94085 7.06579	.68557	.68557	.31443	.31443
300 360 420 480	56 78	7.16270 .24188 .30882 .36682	4.68557 .68557 .68557 .68557	4.68558 .68558 .68558 .68558	5.31443 31443 .31443 .31443	5.31442 .31442 .31442 .31442
540 600 660 720	9 10 11 12	7.46373 .50512 .54291	.68557 4.68557 .68557 .68557	.68558 4.68558 .68558 .68558	5.31443 5.31443 .31443	5.31442 5.31442 .31442 .31442
780 840	13	.57767	.68557 .68557	.68558 .68558	.31443	.31442
900 960 1020 1080 1140	15 16 17 18 19	7.63982 .66784 .69417 .71900 .74248	4.68557 .68557 .68557 .68557 .68557	4.68558 .68558 .68558 .68558	5.31443 .31443 .31443 .31443 .31443	5.31442 .31442 .31442 .31442 .31442
1200 1260 1320 1380 1440	20 2I 22 23 24	7.76475 .78594 .80615	4.68557 .68557 .68557 .68557 .68557	4.68558 .68558 .68558 .68558 .68558	5.31443 .31443 .31443 .31443	5.31442 .31442 .31442 .31442
1500 1560 1620 1680	25 26 27 28	7.86166 .87870 .89509 .91088	4.68557 .68557 .68557 .68557	4.68558 .68558 .68558	31443 5.31443 .31443 .31443 .31443	31442 5.31442 .31442 .31442 .31442
1800 1860 1920 1980	30 31 32 33	.92612 7.94084 .95508 .96887 .98223	.68557 4.68557 .68557 .68557 .68557	.68559 4.68559 .68559 .68559 .68559	5.31443 5.31443 .31443 .31443	31441 5.31441 .31441 .31441
2040 2100 2160 2220 2280	34 35 36 37 38	.99520 8.00779 .02002 .03192 .04350	.68557 4.68557 .68557 .68557 .68557	.68559 4.68559 .68559 .68559	5.31443 .31443 .31443 .31443	.31441 5.31441 .31441 .31441
2340 2400 2460 2520 2580 2640	39 40 41 42 43 44	.05478 8.06578 .07650 .08696 .09718	.68557 4.68557 68556 .68556 .68556	.68559 4.68559 .68560 68560 .68560	31443 5.31443 .31444 .31444 .31444	.31441 5.31441 .31440 .31440 .31440
2700 2760 2820 2880 2940	45 46 47 48 49	8.11693 .12647 .13581 .14495 .15391	4.68556 .68556 .68556 .68556 .68556	4.68560 .68560 .68560 .68560 .68560	5.31444 .31444 .31444 .31444 .31444	5.31440 .31440 .31440 .31440 .31440
3000 3060 3120 3180 3240	50 51 52 53 54	8.16268 .17128 .17971 .18798 .19610	4.68556 .68556 .68556 .68556 .68556	4.68561 .68561 .68561 .68561 .68561	5.31444 .31444 .31444 .31444 .31444	5.31439 .31439 .31439 .31439 .31439
3300 3360 3420 3480	55 56 57 58	8.20407 .21189 .21958 .22713	4.68556 .68556 .68555 .68555	4.68561 .68561 .68561 .68562	5.31444 .31444 .31445 .31445	5.31439 .31439 .31439 .31438
3540 3600	60	8.24186	4.68555	4.68562 4.68562	5.31445	5.31438

"	'	L. Sin.	8	T	S'	T
3600	0	8.24186	4.68555	4.68562	5.31445	5.31438
3660	1	.24903	.68555	.68562	.31445	.31438
3720 3780	3	.25609 .26304	.68555 .68555	.68562 .68562	31445	.31438
3840	3 4	.26988	.68555	.68563	.31445 .31445	.31438
3900	5	8.27661	4.68555	4.68563	5.31445	5.31437
3960		.28324	.68555	.68563	.31445	.31437
4020	8	.28977	.68555 .68555	.68563 .68563	.31445	.31437
4140	9	.30255	.68555	.68563	.31445	.31437
4200	10	8.30879	4.68554	4.68563	5.31446	5.31437
4260	11	.31495	.68554	.68564	.31446	.31436
4320 4380	12	.32103	.68554 .68554	.68564	.31446	.31436
4440	13 14	.32702 .33292	.68554	.68564 .68564	.31446 .31446	.31436 .31436
4500		8.33875	4.68554	4.68564	5.31446	5.31436
4560	15 16	.34450	.68554	.68565	.31446	.31435
4620 4680	17	.35018	.68554	.68565	.31446	.31435
4740	19	.35578 .36131	.68554 .68554	.68565 .68565	.31446 .31446	.31435 .31435
4800	20	8.36678	4.68554	4.68565	5.31446	5.31435
4860	21	.37217	.68553	.68566	.31447	.31434
4920 4980	22	·37750 38276	.68553 .68553	.68566 68566	.31447	.31434
5040	23	.38796	.68553	.68566 .68566	.31447 .31447	.31434
5100	25	8.39310	4.68553	4.68566	5.31447	5.31434
5160	26	.39818	.68553	.68567	.31447	•31433
5220 5280	27 28	.40320 .40816	.68553 .68553	.68567	.31447	.31433
5340	29	.41307	.68553	.68567 .68567	.31447 .31447	.31433
5400	30	8 41792	4.68553	4.68567	5.31447	5.31433
5460	31	.42272	.68552	.68568	.31448	.31432
5520	32	.42746	.68552 .68552	.68568 .68568	.31448	.31432
5580 5640	33 34	.43216 .43680	.68552	.68568	.31448 .31448	.31432
5700		8.44139	4.68552	4.68569	5.31448	5.31431
5760	35 36	•44594	.68552	.68569	.31448	.31431
5820 5880	37 38	.45044	.68552 .68552	.68569 .68569	.31448 .31448	.31431
5940	39	.45489	.68551	.68569	.31449	.31431
6000	40	8.46366	4.68551	4.68570	5.31449	5.31430
6060	41	.46799	.68551	.68570	.31449	.31430
6120 6180	42	.47226 .47650	.68551 .68551	.68570 .68570	.31449	.31430
6240	43	.48069	.68551	.68571	.31449 .31449	.31430
6300	45	8.48485	4.68551	4.68571	5.31449	5.31429
6360	46	.48896	.68551	.68571	.31449	.31429
6420 6480	47 48	.49304	.68550 .68550	.68572 .68572	.31450	.31428
6540	49	.50108	.68550	.68572	.31450	.31428
6600	50	8.50504	4.68550	4.68572	5.31450	5.31428
6660	51	.50097	.68550 .68550	.68573 .68573	.31450	.31427 .31427
6720 6780	52 53	.51287 .51673	.68550	.68573	.31450 .31450	.31427
6840	54_	. 52055	.68550	.68573	.31450	.31427
6900	55 56	8.52434	4.68549	4.68574	5.31451	5.31426
6960 7020	50	.52810 .53183	.68549 .68549	.68574 .68574	.31451	.31426 .31426
7080	57 58	.53552	.68549	.68575	.31451	.31425
7140	_59_	.53919	.68549	.68575	.31451	.31425
7200	60	8.54282	4.68549	4.68575	5.31451	5.31425



### TABLE IV.

# LOGARITHMS

OF THE

SINE, COSINE, TANGENT AND COTANGENT

FOR

EACH MINUTE OF THE QUADRANT.

- 7					<b>0</b> °						
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.		]	Prop	. Pt	s.
0	6 -6		6 .6			0.00 000	60			01	
1 2	6.46 373 6.76 476	30103	6.46 373 6.76 476	30103	3.53 627 3.23 524	0.00 000	59 58	.1	3470	3218	2997 300
3	6.94 083	17609	6.94 083	17609	3.05 915	0.00 000	57	.2	695	644	599
4	7.06 579	9691	7.06 579	9691	2.93 421	0.00 000	56	·3	1390	965 1287	899
5	7.10 270	7918	7.16 270 7.24 188	7918	2.83 730 2.75 812	0.00 000	55 54	-5	1738		1199
7 8	7.30 882	6694 5800	7.30 882	5800	2.69 118	0.00 000	53		2802	ofool	0.00
8	7.36 682 7.41 797	5115	7.36 682 7.41 797	5115	2.63 318 2.58 203	0.00 000	52 51	.1	280	2633 263	2483 248
10	7.46 373	4576	7.46 373	4576	2.53 627	0.00 000	50	.2	560	527	497
11	7.50 512	4139 3779	7.50 512	4139 3779	2.49 488	0.00 000	49 48	·3	1121	790	745 993
12	7.54 291 7.57 767	3476	7.54 291 7.57 767	3476	2.45 709	0.00 000	48 47	.5	1401		
14	7.60 985	3218	7.60 986	3219	2.39 014	0.00 000	46		2227	2021	1848
15	7.63 982	2997 2802	7.63 982	2996 2803	2.36 018	0.00 000	45	.2	223	202	185
16	7.66 784 7.69 417	2633	7.66 783 7.69 418	2633	2.33 215	9.99 999	44 43	.2	445	404	370
18	7.71 900	2483	7.71 900	2482	2.28 100	9.99 999	42	·3	668 891	606 808	554 739
19	7.74 248	2348	7.74 248	2348	2.25 752	9.99 999	41	.5	1113	1010	924
20	7.76 475 7.78 <b>594</b>	2119	7.76 476 7.78 595	2119	2.23 524	9.99 999 9.99 999	40	,	1704	<b>1579</b>	1472
22	7.80 613	2021	7.80 615	2020	2.19 385	9.99 999	39 38	.1	170	158	147
23	7.82 545	1930	7.82 546	1931	2.17 454	9.99 999	37	.2	341	316	294
24	7.84 393 7.86 166	1773	7.84 394	1773	2.15 606	9.99 999	36	·3	511 682	474 632	442 589
26	7.87 870	1704	7.87 871	1704	2.12 129	9.99 999	35 34	.5	852	789	736
27	7.89 509	1579	7.89 510	1579	2.10 490	9 99 999	33		1379	7007	1223
28 29	7.92 612	1524	7.91 089 7.92 613	1524	2.08 911	9.99 999	32 31	.1	138	1297	122
30	7.94 084	1472	7.94 086	1473	2.05 914	9.99 998	30	.2	276	259	245
31	7.95 508	1424	7.95 510 7.96 889	1424	2.04 490	9.99 998	29	·3	414 552	389 519	367 489
32 33	7.96 887 7.98 223	1336	7.98 225	1336	2.03 111	9.99 998	28 27	•5	690	649	612
34	7.99 520	1297	7.99 522	1297	2.00 478	9.99 998	26		1158	1100	1046
35 36	8.00 779	1259	8.00 781	1223	1.99 219	9.99 998	25	. 1	116	110	105
30	8.02 002	1190	8.02 004 8.03 194	1190	1.97 996	9.99 998	24	.2	232	220	209
37 38	8.04 350	1158	8.04 353	1159	1.95 647	9.99 997	22	·3	347 463	330 440	314 418
39	8.05 478	1128	8.05 481	1100	1.94 519	9.99 997	21	.5	579	550	523
40 41	8.06 578 8.07 650	1072	8.06 581 8.07 653	1072	1.93 419	9.99 997 9.99 997	20 19		0001	oral	
42	8.08 696	1046	8.08 700	1047	1.91 300	9.99 997	18	.1	999	954 95	914
43	8.09 718 8.10 717	999	8.09 722 8.10 720	998	1.90 278 1.89 280	9.99 997	17 16	.2	200	191	183
44 45	8.11 693	976	8.11 696	976	1.88 304	9.99 996	15	·3	300	286 382	274 366
46	8.12 647	954	8.12 651	955	1.87 349	9.99 996	14	-5	500	477	457
47	8.13 581	934	8.13 585 8.14 500	934 915	1.86 415	9.99 996	13	,	877	843	812
48 49	8.14 495 8.15 391	896	8.15 395	895	1.84 605	9.99 996 9.99 996	11	.1	88	84	81
50	8.16 268	877	8.16 273	878	1.83 727	9.99 995	10	.2	175	169	162
51	8.17 128	86o 843	8.17 133 8.17 976	860 843	1.82 867	9.99 995	9	·3	263 351	253 337	244 325
52 53	8.17 97 <b>1</b> 8.18 798	827	8.18 804	828	1.81 196	9.99 99 <u>5</u> 9.99 99 <u>5</u>		-5	438		
54	8 19 610	812	8.19616	812 797	1.80 384	9.99 995	6	,	782	755	730
55 56 57 58	8.20 407	782	8.20 413	782	1.79 587	9.99 994	5	.1	78	75	73
57	8.21 958	769	8.21 195 8.21 964	769	1.78 036	9.99 994 9.99 994	4 3	.2	156	151	146
58	8.22 713	755	8.22 720	756	1.77 280	9.99 994	3 2	·3	235 313	302	219
59 60	8.23 456	.730	8.23 462	742	1.76 538	9.99 994	1 0	.5	391	377	
00						9 99 993 T Sim		_	D	The	-
-	L. Cos.	d.	L. Cotg.		L. Tang. 89°	L. Sin.	,	<u> </u>	rrol	Pt	S.

	10											
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.			Prop	. Pts.		
0	8.24 186	717	8.24 192	718	1.75 808	9.99 993	60					
I 2	8.24 903 8.25 609	706	8.24 91C 8.25 616	706	I.75 090 I.74 384	9.99 993 9.99 993	59 58	.1	717	69.5	67.3	
3	8.26 304	695 684	8.26 312	696 684	1.73 688	9 99 993	57	.2	143.4	139.0	134.6	
4	8.26 988	673	8.26 996	673	1.73 004	9.99 992	56	.3	215.1	208.5	201.9	
5 6	8.27 661	663	8.27 669	663	1.72 331	9.99 992	55	·4 ·5	286.8	278.0	269.2 336.5	
	8.28 324 8.28 977	653	8.28 332 8.28 986	654	1.71 668	9.99 992 9.99 992	54 53	.5	330.31	34/-31	330.3	
7 8	8.29 621	644	8.29 629	643	1.70 371	9.99 992	52		653	634	616	
9	8.30 255	634	8.30 263	625	1.69 737	9.99 991	51	.1	65.3	63.4	61.6	
10	8.30 879	616	8.30 888	617	1.69 112	9.99 991	50	.3	195.9	190.2	184.8	
11	8.31 495 8.32 103	608	8.31 50 <del>5</del> 8.32 112	607	1.67 888	9.99 991	49 48	-4	261.2	253.6	246.4	
13	8.32 702	599	8.32 711	599	1.67 289	9.99 990	47	-5	326.5	317.0	308.0	
14	8.33 292	590 583	8.33 302	591 584	1.66 698	9.99 990	46	c 1	599	583	568	
15	8.33 875	575	8.33 886	575	1.66 114	9.99 990	45	.1	59.9	58.3	56.8	
16	8.34 450 8.35 018	568	8.34 461 8.35 029	568	1.65 539	9.99 989	44	.2	119.8	116.6	113.6	
17	8.35 578	560	8.35 590	56 <b>1</b>	1.64 410	9.99 989	43 42	.3	179.7 239.6	174.9	170.4	
19	8.30 131	553 547	8.30 143	553 546	1.63 857	9.99 989	4I	·4 ·5	299.5	233.2	-	
20	8.36 678	539	8.36 689	540	1.63 311	9.99 988	40	,	,,, 0	, ,,		
21	8.37 217 8.37 750	533	8.37 229 8.37 762	533	1.62 771	9.99 988	39 38		553	539	526	
22	8.38 276	526	8.38 289	527	1.61 711	9.99 988	37	.1	55·3 110.6	53.9	52.6	
24	8.38 796	520	8.38 809	520	1.61 191	9.99 987	36	.3	165.9	161.7	157.8	
25	8.39 310	514	8.39 323	514	1.60 677	9.99 987	35	-4	221.2		210.4	
26	8.39 818	508	8.39 323 8.39 832	509	1.60 168	9.99 986	34	-5	276.5	269.5	263.0	
27	8.40 320	496	8.40 334 8.40 830	496	1.59 666	9.99 986	33 32		514	502	490	
29	8.41 307	491	8.41 321	491	1.58 679	9.99 985	31	.1	51.4	50.2	49	
30	8.41 792	485	8.41 807	486	1.58 193	9.99 985	30	.2	102.8	100.4	98	
31	8.42 272	480	8.42 287	480	1.57 713	9.99 985	29	-3	154.2	200.8	147	
32	8.42 746	474	8.42 762	475	1.57 238	9.99 984	28	·4 ·5	205.6		245	
33	8.43 216 8.43 680	464	8.43 232 8.43 696	464	1.56 768	9.99 984 9.99 984	27 26					
35	8.44 139	459	8.44 156	460	1.55 844	9.99 983	25		480	470	450	
36	8.44 594	455	8.44 611	455	1.55 389	9.99 983	24	.I	48 96	47 94	46 92	
37 38	8.45 044	450	8.45 061	450	1.54 939	9.99 983	23	.3	144	141	138	
38	8.45 489 8.45 930	441	8.45 507 8.45 948	441	1.54 493	9.99 982	22 21	-4	192	188	184	
39 40		436	8.46 385	437	1.53 615	9.99 982	20	•5	240	235	230	
41	8.46 366 8.46 799	433	8.46 817	432	1.53 183	9.99 981	19		450	440	430	
42	8.47 226	427	8.47 245	428	1.52 755	9.99 981	18	.1	45	44	43	
43.	8.47 650	424	8.47 669	424	1.52 331	9.99 981 9.99 980	17	.2	90	88	86	
44	8.48 o69 8.48 485	416	8.48 089	416	1.51 911	9.99 980	15	·3	135	132	172	
45 46	8.48 896	411	8.48 917	412	1.51 083	9.99 979	14	.5	225			
47	8.49 304	408	8.49 325	408	1.50 675	9.99 979	13				455	
48	8.49 708	404	8.49 729	404	1.50 271	9.99 979	12 11		420	410	400	
49	8.50 108	396	8.50 130	397	1.49 870	9.99 978	10	.1	84	41 82	40 80	
50	8.50 504 8.50 897	393	8.50 527 8.50 920	393	1.49 473	9.99 977	9	.3	126	123	120	
52	8.51 287	390	8.51 310	390	1.40 090	9.99 977		-4	168	164	160	
53	8.51 673	386	8.51 696	386	1.48 304	9.99 977	7 6	.5	210	205	200	
54	8.52 055	379	8.52 079	- 380	1.47 921	9.99 976			390	380	370	
55	8.52 434 8.52 810	376	8.52 45 <u>9</u> 8.52 83 <u>5</u>	376	1.47 541	9.99 976 9.99 97 <u>5</u>	5 4	·x.	39	38	37	
. 57	8.53 183	373	8.53 208	373	1.46 792	9.99 975	3 2	.2	78	76	74	
57 58 59	8.53 552	369	8.53 578	370	1.46 422	9.99 974	2	-3	117		148	
59	8.53 919	367	8.53 945	367	1.46 055	9.99 974	0	-5	1			
60	8.54 282		8.54 308		1.45 692	9.99 974	-	-	-			
1	L. Cos.	d.	L. Cotg.	c. d	L. Tang.	L. Sin.	,	1	Pro	p. Pts	8.	
					88°							

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F	$2^{\circ}$										
1	L. Sin	. d.	L. Tang.	c.d.	L. Cotg.	L. Cos.		Prop. Pts.			
	8.54 28	360	8.54 308	361	1.45 692	9.99 974	60				
	8.54 64 2 8.54 99	2	8.54 669 8.55 <b>0</b> 27	358	1.45 331	9.99 973	59 58		360	350	340
	3 8.55 35	4   333	8.55 382	355	I.44 973 I.44 618	9.99 973 9.99 972	57	.1	36 72	35 70	34 68
_	4 8.55 70	5 332	8.55 734	352 349	I.44 266	9.99 972	56	•3	108	105	102
	8.55 70 8.56 05 8.56 40	4	8.56 o83 8.56 429	346	1.43 917	9.99 971	55	·4 ·5	144 180	140	136
	7 8.56 74 8 8.57 08	3 343	8.56 773	344	I.43 57I I.43 227	9.99 971 <b>9.9</b> 9 970	54	.6	216	210	204
	8 8.5708	4	8.57 114	34I 338	1.42 886	9.99 970	52	·7	252	245	238
1	$\begin{array}{c c} 9 & 8.57 & 42 \\ \hline 0 & 8.57 & 75 \\ \end{array}$	336	8.57 452 8.57 788	336	1.42 548	9.99 969	$\frac{51}{50}$	.9	288 324	280 315	272 306
ī	1 8.58 08	9 332	8.58 121	333	1.41 879	9.99 969			330	320	310
I	2   8.5841	9 330	8 58 451	330	1.41 549	9.99 968	49 48	.1	33	32	31
I.		2   3-3	8.58 779 8.59 105	3:6	1.41 221	9.99 967 9.99 967	47 46	.2	66 99	64 96	62 93
I	5 8.59 39	323	8.59 428	323	1.40 572	9.99 967	45	.4	132	128	124
I	6 8.59 71	5   320	8.59 749 8.60 068	321 319	1.40 251	9.99 966	44	.6	165 198	160 192	155
1	8 8.60 34	316	8.60 384	316	1.39 932 1.39 616	9.99 965	43 42	.7	231	224	217
I	9 8.60 66	2 3-3	8.60 698	314	1.39 302	9.99 964	41	.8	264	256	248
20		3	8.61 009 8.61 319	310	1.38 991 1.38 681	9.99 964	40	.9	297 300	288	275 285
2		9 307	8.61 626	307	1.38 374	9.99 963	39 38	.1	30	29	28.
2	3 8.61 89		8.61 931	303	1.38 069	9.99 962	37	.2	60	58	57.0
2.		207	8.62 234 8.62 535	301	1.37 766	9.99 962	36	•3	90 120	87 116	85.5
2	6 8.62 79	5   29°	8.62 834	299	1.37 465	9.99 961 9.99 961	35 34	•5	150	145	142.5
2	7 8.63 09	I 290	8.63 131	297	1 36 869	9.99 960	33	.6	180	203	171.0
2 2		8 293	8.63 426 8.63 718	292	1.36 574 1.36 282	9.99 960	32 31	.8	240	232	228.0
30		200	8.64 009	291	1.35 991	9.99 959	30	٠9	270	261	256.5
3	8.64.25	0	8.64 298	289	1.35 702	9.99 958	29	л.	280 28.0	275 27·5	270 27.0
3		7 204	8.64 585 8.64 870	¥85	1.35 415	9.99 958	28 27	.2	56.0	55.0	54.0
3	4 8.65 11	0 203	8.65 154	284	1.34 846	9.99 956	26	•3	84.0	82.5	81.0 108.0
3 3	5 8.65 39 6 8.65 67	I	8.65 43 <u>5</u> 8.65 71 <u>5</u>	280	1.34 565	9.99 956	25	•4	112.0	110.0	135.0
3	7 8.65 94	7 277	8.65 993	278	1.34 285	9.99 95 <u>5</u> 9.99 95 <u>5</u>	24 23	.6	168.0	165.0	162.0
3	8 8.66 22	3 270	8.66 269	276	1.33 731	9.99 954	22	.7	196.0	192.5	216 0
3		272	8.66 543 8.66 816	273	1.33 457	9.99 954	$\frac{21}{20}$	.9	252.0		
4	1 8.67 03	9 270	8.67 087	271	1.33 184	9.99 953 9.99 952	19		265	260	255
4	2 8.67 30	8 209	8.67 356	269 268	1.32 644	9.99 952	18	.1	.26.5	.26.0	.25.5
	3   8.67 57 4   8.67 82	266	8.67 624 8.67 890	266	1.32 376	9.99 951 9.99 951	17 16	.3	· <b>7</b> 9·5	.78.0	.76.5
4	5 8.68 10	203	8.68 154	264	1.31 846	9.99 950	15	-4	106.0	104.0	102.0
4	6 8.68 36	7 263	8.68 417 8.68 678	263 261	1.31 583	9.99 949	14	·5 .6	132.5	130.0	127.5
4	7   8.68 62 8   8.68 88	36   <sup>259</sup>	8.68 938	260	1.31 322	9.99 949 9.99 948	13	.7	185.5	182.0	178.5
4	9 8.69 14	4 258	8.69 196	258	1.30 804	9.99 948	11	.8	212.0	208.0	204.0
5	8.69 40	00	8.69 453	255	1.30 547	9.99 947	10	.,	250		
5	8.69 65 2 8.69 90	253	8.69 708 8.69 962	254	1.30 292	9.99 946	8	.z	.25.0	.24.5	.24.0
1 5	3 8.70 15	9 252	8.70 214	252 251	1.29 786	9.99 945	7 6	.2	.50.0	.49.0	
	8.70 40	240	8.70 465	249	1.29 535	9.99 944		.4	.75.0 100.0	·73·5	.96.0
5	8.70 6 8.70 9 7 8.71 1 8 8.71 3 9 8.71 6	247	8.70 714 8.70 962	248	1.29 286	9·99 944 9·99 943	5 4	٠5	125.0	122.5	120.0
5	7 8.71 1	1 240	8.71 208	246	1.28 792	9.99 942	3	.6 .7	150.0	147.0	
5	8 8.71 3	13	8.71 453 8.71 697	244	1.28 547	9.99 942 9.99 943	2 I	.8	200.0	196.0	192.0
6	0 8.71 8	1 040	8.71 940	243	1.28 060	9.99 940	10	.9	225.0	220.5	216.0
	L. Cos		L. Cotg.	c. d.			1		Pro	p. Pts	
-	1 20 (100		50-8	,00 02	87°		•	·			

	30											
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.			Prop	. Pts		
0	8.71 880	240	8.71 940 8.72 181	241	1.28 060	9.99 940	60		228 1			
1 2	8.72 120 8.72 359	239	8.72 420	239	1.27 819	9.99 940	59 58	.1	235	234	22.9	
3	8.72 597	238	8.72 659	239	1.27 341	9.99 938	57	.2	47.6	46.8	45.8	
4	8.72 834	235	8.72 896 8.73 132	236	1.26 868	9.99 938	56	·3	95.21	93.6	68.7 gr.6	
5 6	8.73 303	234	8.73 366	234	1.26 634	9.99 937 9.99 936	55 54	.5	119.0	117.0		
7 8	8.73 535	232	8.73 600	234	1.26 400	9.97936	53	.6	142.8	163.8	137.4	
9	8.73 767 8.73 997	230	8.73 832 8.74 063	231	1.26 168	9 · 99 935 9 · 99 934	52 51	.8	190.4	187.2		
10	8.74 226	229	8.74 292	229	1.25 708	9.99 934	50	•9	214.2	210.5	206.1	
II	8.74 454	226	8.74 521	229	1.25 479	9 99 933	49 48		225	220	216	
12	8.74 680 8.74 906	226	8.74 748 8.74 974	226	1.25 252 1.25 026	9.99 932 9.99 932	47	.1	22.5 45.0	22.0	43.2	
14	8.75 130	224	8.75 199	225	1.24 801	9.99 931	46	-3	67.5	66.0	64.8	
15	8.75 353	222	8.75 423 8.75 645	222	1.24 577	9.99 930	45	•4	90.0	88.0	86.4 108.0	
	8.75 575 8.75 795	220	8.75 867	222	1.24 355	9 99 929	44 43	.6	135.0	132.0	129.6	
17	8.70 015	219	8.76 087	220	1.23 913	9.99 928	42	.7	157.5 180.0	154.0 176.0	151.2	
20	8.76 234	217	8.76 306 8.76 525	219	1.23 694	9.99 927	$\frac{4^{\mathrm{I}}}{40}$	.9	202.5			
21	8.76 667	216	8.76 742	217	1.23 475	9.99 926			212	208	204	
22	8.76 883	216	8.76 958	216	1.23 042	9.99 925	39 38	.1	21.2 42.4	20.8	40.8	
23	8.77 097 8.77 310	213	8.77 173 8.77 387	214	1.22 827	9.99 924 9.99 923	37 36	.2	63.6	62.4	61.2	
25	8.77 522	212	8.77 600	213	1.22 400	9.99 923	35	-4	84.8	83.2	81.6	
26	8.77 733	211	8.77 811	211	1.22 189	9.99 922	34	.6	127.2	104.0	102.0	
27	8.77 943 8.78 152	209	8.78 022 8.78 232	210	1.21 978	9.99 921	33	.7	148.4	145.6	142.8	
29	8.78 360	208	8.78 441	209	1.21 559	9.99 920	31	.8	169.6	166.4	163.2	
30	8.78 508 8.78 774	206	8.78 649 8.78 855	206	1.21 351	9.99 919	30	.,	201	197	193	
31 32	8.78 979	205	8.79 061	205	1 21 145	9.99 918	29 28	.ı	20.1	19.7	19.3	
33	8.79 183	204	8.79 266	205	1.20 734	9 99 917	27	.2	40.2 60.3	39·4 59.1	38.6 57·9	
34	8.79 386 8.79 588	202	8.79 470 8.79 673	203	1.20 530	9.99 916	25	·3	80.4	78.8	77.2	
35 36	8.79 789	201	8.79 875	202	1.20 327	9.99 915	24	.5	100.5	98.5	96.5	
37 38	8.79 990 8.80 189	199	8 80 076	201	1.19 924	9.99 913	23	.7	140.7	137.9	135.1	
39	8.80 388	199	8.80 277 8.80 476	199	1.19 723	9.99 913	22 2I	.8	160.8	157.6		
40	8.80 585	197	8 80 674	198	1.19 326	9.99 911	20	.9	180.9	177.3	173.7	
41	8.80 782 8.80 978	197	8.80 872 8.81 068	198	1.19 128	9.99 910	19	.1	18.9	18.5	1	
42	8.81 173	195	8.81 264	196	1.18 736	9.99 909	17	.2	37.8	37.0	4	
44	8.81 367	194	8.81 459	195	1.18 541	9.99 908	16	·3	56.7 75.6	55·5 74·0		
45 46	8.81 560 8.81 752	192	8.81 653 8 81 846	193	1.18 347	9.99 907	15	.5	94-5	92.5	90.5	
47		192	8.82 038	192	1.17 962	9.99 905	13	.6	113.4	111.0		
47	8.82 134 8.82 324	190	8.82 230 8.82 420	192	1.17 770	9.99 904	I2 II	.8	151.2	148.0	144.8	
49 50	8.82 513	189	8.82 610	190	1.17 390	9.99 903	10	.9	170.1		162.9	
51	8.82 701	188	8.82 799	189	1.17 201	9.99 902	9	.,	0.4	0.3 0	2 0.1	
52		187	8.82 987 8.83 175	188	1.17 013	9.99 901		.2	0.8	0.6 0	.4 0.2	
53 54	8.83 261	186	8.83 361	186	1.16 639	9.99 899	6	·3	1.6		.6 0.3	
55	8.83 446	184	8.83 547	185	1.16 453 1.16 268	9.99 898	5	-5	2.0	1.5 1	.0 0.5	
55 56 57 58 59	8.83 630 8.83 813	183	8.83 732 8.83 916	184	1.16 208	9.99 898	4 3	.6	2.4		.4 0.7	
58	8.83 996	181	8.84 100	184	1.15 900	9.39 896	3 2	.8	3.2	2.4 1	.6 o 8	
59 60		181	8.84 282	182	1.15 718	9.99 895	1	. 9	3.6	2.7 1	.8 09	
-00	L. Cos.	d.	L. Cotg.	0. 1	L. Tang.		1	-	Pro	p. Pt	S.	
-	1 11. COS.	ı u.	L. Corg.	to u	86°	I II. SIII.	. /		110	p. xt		

	4°										
,	L. Sin.	d.	L. Tang.	c.d.	L. Cotg.	L. Cos.			Prop	• Pts	•
0	8.84 358	181	8.84 464	182	1.15 536	9.99 894	60				
1 2	8.84 539 8.84 718	179	8.84 646 8.84 826	180	1.15 354	9.99 893	59 58		181	779	177
3	8.84 897	179	8.85 006	180	1.14 994	9.99.891	57	.1	36.2	17.9 35.8	35.
4	8.85 075	178	8.85 183	179	1.14 815	9.99 891	56	•3	54.3	53.7	53.
5	8.85 252		8.85 363		1.14 637	9.99 890	55	•4	72.4	71.6	70.
	8.85 429	177	8.85 540	177	1.14 460	9.99 889	54	•5	90.5	89.5	88.
7 8	8.85 603 8.85 780	175	8.85 717 8.85 893	176	1.14 283	9.99 888	53	.6 ·7	108.6	107.4	106.
9	8.85 955	175	8.86 069	176	1.14 107	9.99 887 9.99 886	52 51	.8	144.8	143.2	141.
10	8.86 128	173	8.86 243	174	1.13 757	9.99 885	$\frac{51}{50}$	٠9	162.9		
11	8.86 301	173	8.86 417	174	1.13 583	9.99 884	49		175	173	171
12	8.86 474	173	8.86 591	174	1.13 409	9.99 883	48	.1	17.5	17.3	17.
13	8.86 645	171	8.86 763	172	1.13 237	9.99882	47	.2	35.0	34.6	34.
14	8.86 816	171	8.86 935	171	1.13 065	9.99 881	46	-3	52.5	51.9	51.
15 16	8.86 987	169	8.87 106	171	1.12 894	9.99 880	45	·4 ·5	70.0 87.5	69.2 86.5	68. 85.
17	8.87 156 8.87 325	169	8.8 <b>7 277</b> 8.87 447	170	1.12 723	9.99 8 <b>79</b> 9.99 879	44.	.6	105.0	103.8	102.
18	8.87 494	169	8.87 616	169	1.12 384	9.99 878	43 42	.7	122.5	121.1	119.
19	8.87 661	167	8.87 783	169	1.12 215	9.99 877	41	.8	140.0	138.4	136.
20	8.87 829		8.87 953	168	1.12 047	9.99 876	40	.9	157.5		
21	8.87 995	166	8.88 120	167	1.11880	9.99875	39 38		168	166	164
22	8.88 161	165	8.88 287	166	1.11 713	9.99 874	38	. 1	.16.8	16.6	16.
23 24	8.88 326 8.88 490	164	8.88 453 8.88 618	165	1.11 547 1.11 382	9.99 873	37	.2	33.6 50.4	33.2 49.8	32. 49.
25	8.88 654	164	8.88 783	165		9.99 872	36	·3	67.2	66.4	65.
26	8.88 817	163	8.88 948	165	1.11 217	9.99 871	35	•5	84.0	83.0	82
27	8.88 980	163	8.89 111	163	1.10 889	9.99 869	34 33	.6	100.8	99.6	98.
28	8.89 142	162	8.89 274	163	1.10 726	9.99 868	32	.7	117.6	116.2	114.
29	8.89 304	160	8.89 437	163 161	1.10 563	9.99867	31	.8	134.4	132.8	131.
80	8.89 464	161	8.89 598	162	1.10 402	9.99 866	30	٠,٠	151.2		
31	8.89 623	159	8.89 760	160	1.10 240	9.99 865	29	,	16.2	159	157
32 33	8.89 784 8.89 943	159	8.89 920 8.90 080	160	1.10 080	9.99 864 9.99 863	28 27	.1	32.4	15.9 31.8	31.
34	8.90 102	159	8.90 240	160	1.09 760	9.99 862	26	•3	48.6	47.7	47.
35	8.90 260	158	8.90 399	159	1.09 601	9.99 861	25	•4	64.8	63.6	62.
36	8.90 417	157	8.90 557	158	1.09 443	9.99 860	24	-5	81.0	79.5	78.
37	8.90 574	157	8.90 715	158	1.09 285	9.99 859	23	.6	97.2	95.4	.94
38	8.90 730	155	8.90 872	157	1.09 128	9.99 858	22	.8	113.4	111.3	
39 40	8.90 885	155	8.91 029	156	1.08 971	.9 99 857	21	.9	145.8		-
41	8.91 040 8.91 19 <del>3</del>	155	8.91 185	155	1.08 815	9.99 856	20		155	153	151
12	8.91 349	154	8.91 340 8.91 495	155	1.08 503	9.99 855	19 18	.1	15.5	15.3	15.
43	8.91 502	153	8.91 650	155	1.08 350	9.99 853	17	.2	31.0	30.6	30.
44	8.91 655	153	8.91 803	153	1.08 197	9.99 852	16	٠3	46.5	45.9	45.
45	8.91 807	152	8.91 957	154	1.08 043	9.99 851	15	-4	62.0	61.2	60.
46	8.91 959	152	8.92 110	153	1.07 890	9.99 850	14	.6	77·5 93.0	76.5 91.8	75· 90.
47	8.92 110	151	8.92 262	152	1.07 738	9.99 848	13	.7	108.5	107.1	105.
48 49	8.92 261 8.92 411	150	8 92 414 8.92 56 <del>5</del>	151	1.07 586	9.99 847 9.99 846	12 11	.8	124.0		120.
$\frac{7}{50}$	8.92 561	150	8.92 716	151	1.07 284	9.99 845	10	٠9	139.5	137.7	135.
51	8.92 710	149	.8.92 866	150	1.07 134	9.99 844	10		149	147	1
52	8.92 859	149	8.93 016	150	1.06 984	9.99 843	8	, I	14.9	14.7	0.
53	8.93 007	148	8.93 165	149	1.06 835	9.99 842	7 6	.2	29.8	29.4	0.
54	8.93 154	147	8.93 313	148	1.06 687	9.99 841		•3	44·7 59.6	44.I 58.8	o. o.
55	8.93 301	147	8.93 462	1	1.06 538	9.99 840	5	-5	74.5	73.5	0.
50	8.93 448	146	8 93 609	147	1.06 391	9.99 839	4	.6	89.4	88.2	0.
58	8.93 594	146	8.93 756 8.93 903	147	1.06 244	9.99 838 9.99 837	3 2	.7	104.3	102.9	0.
55 56 57 58 59	8.93 740 8.93 88 <del>5</del>	145	8.94 049	146	1.05 951	9.99 836	I	.8	119.2	117.6	0.
60	8.94 030	145	8.94 195	146	1.05 805	9.99 834	0	.9	134.1	132.3	0.
_											
	L. Cos.	d.	(104 m		L. Tang.	L. Sin.	,		D	p. Pts	

	5°										
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.			Pro	p. Pts	3.
0	8.94 030	144	8.94 195	145	1.05 805	9.99 834	60				
1 2	8.94 174 8.94 317	143	8.94 340 8.94 485	145	1.05 660	9.99 833 9.99 832	59 58		145	143	141
3	8.94 461	144	8.94 630	145	1.05 370	9.99 831	57	.I	14.5	14.3 28.6	28.2
4	8.94 603	143	8.94 773	144	1.05 227	9.99 830	56	•3	43.5	42.9	42.3
5 6	8.94 746 8.94 887	141	8.94 917 8.95 060	143	1.05 083	9.99 829 9.99 828	55	-4	58.0 72.5	57.2 71.5	70.5
7 8	8.95 029	142	8.95 202	142	1.04 798	9.99 827	54 53	.6	87.0	85.8	84.6
	8.95 170	141	8.95 344	142	1.04 656	9.99 825	52	.7	101.5	100.1	98.7
9 10	8.95 310 8.95 450	140	8.95 486	141	1.04 514	9.99 824	51	.8	116.0	114.4	112.8
II	8.95 589	139	8.95 767	140	I.04 373 I.04 233	9.99 823	<b>50</b>		139	138	136
12	8.95 728	139	8.95 908	139	1.04 092	9.99 821	49 48	.1	13.9	13.8	13.6
13 14	8.95 867 8.96 005	138	8.96 047 8.96 187	140	1.03 953	9.99 820 9.99 819	47 46	.2	27.8	27.6	27.2
15	8.96 143	138	8.96 325	138	1.03 675	9.99 817	45	-3	41.7 55.6	41.4 55.2	40.8 54·4
16	8.96 280	137	8.96 464	139	1.03 536	9.99 816	44	-5	69.5	69.0	68.0
17	8.96 417 8.96 553	136	8.96 602 8.96 739	138	1.03 398	9.99 815	43	.6	83.4 97.3	82.8 96.6	81.6 95.2
19	8.96 689	136	8.96 877	138	1.03 261	9.99 814 9.99 813	42 41	.8	111.2	110.4	108.8
20	8.96 825	136	8.97 013	136	1.02 987	9.99 812	40	.9	125.1	:24.2	- 1
2I 22	8.96 960 8.97 09 <del>5</del>	135	8.97 150	137	1.02 850	9.99 810	39 38		135	133	131
23	8.97 229	134	8.97 285 8.97 421	136	1.02 715	9.99 809 9.99 808	38 37	.1	27.0	26.6	26.2
24	8.97 363	134	8.97 556	135	I.02 444	9.99 807	36	•3	40.5	39.9	39.3
25	8.97 496	133	8.97 691	135	1.02 309	9.99 806	35	•4	54.0	53.2	52.4
26 27	8.97 629 8.97 762	133	8.97 82 <del>5</del> 8.97 959	134	1.02 175	9.99 804 9.99 803	34	.6	67.5 81.0	79.8	65.5 78.6
28	8.97 894	132	8.98 092	133	1.01 908	9.99 802	33	.7	94.5	93.1	91.7
29	8.98 026	132	8.98 225	133	1.01 775	9.99 80 <b>1</b>	31	.8	108.0	106.4	104.8
30 31	8.98 157 8.98 288	131	8.98 358 8.98 490	132	1.01 642	9.99 800	30	6	129	128	126
32	8.98 419	131	8.98 622	132	1.01 510	9.99 798	29 28	.1	12.9	12.8	12.6
33	8.98 549	130	8.98 753	131	1.01 247	9.99 796	27	.2	25.8	25.6	25.2
34	8.98 679	129	8.98 884 8.99 01 <del>5</del>	131	1.01 116	9.99 795	26	·3	38.7 51.6	38.4	37.8
35 36	8.98 937	129	8.99 145	130	1.∞ 98 <u>5</u> 1.∞ 8 <u>55</u>	9.99 793 9.99 792	25 24	-5	64.5	64.0	63.0
37 38	8.99 066	129	8.99 275	130	1.00 725	9.99 791	23	.6	77·4 90·3	76.8 89.6	75.6 88.2
38 39	8.99 <b>194</b> 8.99 <b>322</b>	128	8.99 40 <del>5</del> 8.99 534	130	1.∞ 595 1.∞ 466	9.99 790	22 2I	.8	103.2	:02.4	8.001
40	8.99 450	128	8.99 662	128	1.00 338	9.99 788	20	.9	116.1	:15.2	113.4
41	8.99 577	127	8.99 791	129	1.00 209	9.99 786	19		125	123	122
42	8.99 704 8.99 830	126	8.99 919 9.00 046	128	1.00 081	9.99 785	18	.1	25.0	12.3	12.2
43	8.99 956	126	9.00 040	128	0.99 954 0.99 826	9.99 783 9.99 782	17 16	.3	37.5	36.9	36.6
45	9.00 082	126	9.00 301	127	0.99 699	9.99 781	15	-4	50.0	49.2 61.5	48.8 61.0
46	9.00 207	125	9.00 427	126	0.99 573	9.99 780	14	·5 .6	75.0	73.8	73.2
47 48	9.00 332	124	9.00 553	126	0.99 447 0.99 32I	9.99 778 9.99 777	13	.7	87.5	86.1	85.4
49	9.00 581	125	9.00 805	126	0.99 195	9.99 776	II	.8	100.0	98.4	97.6
50	9.00 704	124	9.00 930	125	0.99 070	9.99 775	10	7	121	120	1
51 52	9.00 828 9.00 951	123	9.01 055 9.01 179	124	0.98 945 0.98 821	9.99 773 9.99 772	9	л.	12.1	12.0	0.1
52 53	9.01 274	123	9.01 303	124	0.98 697	9.99 771	7	.2	24.2	24.0	0.2
54	9.01 196	122	9.01 427	123	0.98 573	9.99 769		·3	36.3 48.4	36.0	0.4
55	9.01 318 9.01 440	122	9.01 550 9.01 673	123	0.98 450	9.99 768 9.99 767	5	-5	60.5	60.0	0.5
57	9.01 561	121	9.01 796	123	0.98 327 0.98 204	9.99 765	3	.6	72.6	72.0 84.0	0.6
55 56 57 58 59	9.01 682 9.01 803	121	9.01 918 9.02 040	122	0 98 082	9.99 764	2 I	.8	96.8	96.0	v 8
60	9.01 923	120	9.02 040	122	0.97 960	9.99 763 9.99 761	0	.9	108.9	108.0	0.9
٣	L. Cos.	d.	L. Cotg.	e d		L. Sin.	<u>,</u>		Pron	. Pts.	
l	Li. Cus.	u.	Te Ouige	0. u.		n. Sin.			LIUP	LUS	
			,		84°						

I						6°						60
1	,	L. Sin.	d.	L. Tang.	c.d.	L. Cotg.	L. Cos.			Prop	. Pts	
1	0	9.01 923	120	9.02 162	121	0.97 838	9.99 761	60				
1	I 2	9.02 043	120	9.02 283	121	0.97 717	9.99 760	59 58	.1	121	120	11.9
1	3	9.02 283	110	9.02 525	121	0.97 475	9.99 757	57	.2	24.2	24.0	23.8
1	-4-	9.02 402	118	9.02 645	121	0.97 355	9.99 756	<u>56</u> 55	·3	36.3 48.4	3t o	35 7 47.6
ı	5	9.02 639	119	9.02 885	119	0.97 115	9·99 755 9·99 753	54	.5	60.5	60.0	59 5
1	7 8	9.02 757	117	9.03 003	119	0.96 995	9.99 752	53	.6	72.6 84.7	72.0 84.0	71.4 83.3
1	9	9.02 874	118	9.03 124 9.03 242	118	0.96 876 0.96 758	9.99 751 9.99 749	52 51	.8	96.8	96.0	95.2
1	10	9.03 109	117	9.03 361	119	0.96 639	9.99 748	50	.9	108.9	108.0	107.1
1	11	9.03 226	116	9.03 479	118	0.96 521	9.99 747	49 48	.1	118	117	116 11.6
1	13	9.03 458	116	9.03 597 9.03 714	117	0.96 286	9·99 745 9·99 744	47	.2	23.6	23.4	23.2
ı	14	9.03 574	110	9.03 832	116	0.96 168	9.99 742	46	•3	35.4	35.1	34.8
	15 16	9.03 690 9.03 80 <del>3</del>	115	9.03 948 9.04 06 <b>5</b>	117	0.96 052	9.99 741 9.99 740	45	·4 ·5	47.2 59.0	46.8	58.0
1	17	9.03 920	115	9.04 181	116	0.95 819	9.99 738	44 43	.6	70.8	70.2	69.6
1	18	9.04.034	114	9.04 297	116	0.95 703	9.99 737	42	.8	94.4	93.6	81.2 92.8
	20	9.04 149	113	9.04 413	115	0.95 587	9.99 736	41	.9	106.2	105.3	104.4
ı	21	9.04 376	114	9.04 643	115	0.95 357	9.99 733			115	114	113
1	22 23	9.04.490	114	9.04 <b>75</b> 8 9.04 873	115	0.95 242 0.95 127	9.99 731 9.99 730	39 38	.1	23.0	22.8	11.3
ı	24	9.04 715	112	9.04 987	114	0.95 013	9.99 728	37 36	.3	34.5	34.2	33 9
١	25	9.04 828	113	9.05 101	114	0.94 899	9.99 727	35	-4	46.0	45.6	45.2
ı	26	9.04 940	112	9.05 214 9.05 328	114	0.94 786	9.99 726 9.99 724	34	·5	57·5 69.0	57.0 68.4	56.5
1	27 28	9.05 164	112	9.05 441	113	0.94 559	9.99 723	33 32	-7	80.5	79.8	79.1
I	29	9.05 275	111	9.05 553	112	0.94 447	9.99 721	31	.8 .9	92.0	91.2	90.4
1	30 31	9.05 386 9.05 497	III	9.05 666	112	0.94 334	9.99 <b>72</b> 0 9.99 <b>7</b> 18	30 29		113	III	110
ı	32	9.05 607	110	9.05 890	112	0.94 110	9.99 717	28	.x	11.2	11.1	11.0
	33	9.05 717	110	9.06 002 9.06 113	112	0.93 998 0.93 887	9.99 716	27 26	.2	33.6	33.3	33.0
1	35	9.05 827	110	9.06 224	111	0.93 776	9.99 714	25	-4	44.8	44.4	44.0
ı	36	9.06 046	109	9.06 335	111	0.93 665	9.99 711	24	·5	56.0 67.2	55·5 66.6	55.0 66.0
١	37 38	9.06 155	109	9.06 445 9.06 556	111	0.93 555	9.99 710	23	.7	78.4	77.7	77.0
١	39	9.06 372	108	9.06 666	110	0.93 444	9.99 708	21	.8	89.6	88.8	88.0
ı	40	9.06 481	109	9.06 775	110	0.93 225	9 99 705	20	.9	100.8	99·9	99.0
	41 42	9.06 589	107	9.06 88 <del>3</del> 9.06 994	109	0.93 115	9.99 704 9.99 702	19	т.	10.9	10.8	107
	43	9.06 804	108	9.00 994	109	0.92 897	9.99 701	17	.2	21.8	21.6	21.4
I	44	9.06 911	107	9.07 211	108	0.92 789	9.99 699	16	·3	32.7 43.6	32.4 43.2	32.I 42.8
	45 46	9.07 018 9.07 124	106	9.07 320 9.07 428	108	0.92 680	9.99 698	15 14	•5	54 5	54.0	53.5
1	47 48	9.07 231	107	9.07 536	108	0.92 464	9.99 695	13	.6	65.4 76.3	64.8 75.6	64.2 74.9
	48	9.07 337	105	9.07 643 9.07 751	107	0.92 357	9.99 693	12 11	٠7 ٤.	87.2	86.4	85.6
I	<del>49</del> <b>50</b>	9.07 548	106	9.07 858	107	0.92 249	9.99 692	$\frac{11}{10}$	۰۶	98.1		
1	51		105	9.07 964	106	0.92 036	9.99 689	0		106	_	
	52 53	9.07 653 9.07 758 9.07 863	105	9.08 071 9.08 177	107	0.91 929	9.99 687 9.99 686	8	.1	21.2	21.0	20.8
١	54	9.07 968	105	9.08 283	106	0.91 717	9.99 684	7 6	.3	31.8	31.5	31.2
1	55 56	9.08 072	104	9.08 389	106	0.91 611	9.99 683	5	-4	53.0	42.0 52.5	
1	56	9.08 176	104	9.08 495	105	0 91 505	9.99 681	4	.6	63.6	63.0	62.4
	57 58	9.08 383	103	9.08 705	105	0.91 295	9.99 678	3 2	.7	74.2 84.8		
	59	9.08 486	103	9.08 810	105	0 91 190	9 99 677	1	.9	95.4		
	60	9.08 589		9.08 914		0 91 086	9.99 675	0	-			
		L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	1,		Pro	p. Pts	3.
		,				83°						

						7°			
	1	L. Sin.	d.		c. d.	L. Cotg.	L. Cos.		Prop. Pts.
	0	9.08 589 9.08 692	103	9.08 914	105	0.91 086	9.99 675 9.99 674	60	105 104 103
	1 2	9.08 795	103	9.09 123	104	0.90 877	9.99 672	59 58	.1 10.5 10.4 10.3
	3	9.08 897 9.08 999	103	9.09 227	103	0.90 773	9 99 670	57	.2 21.0 20.8 20.6
-	5	9.00 999	102	9.09 330	104	0.90 566	9.99 667	55	.3 31.5 31.2 30.9 .4 42.0 41.6 41.2
	6	9.09 202	101	9.09 537	103	0.90 463	9.99 666	54	.5 52.5 52.0 51.5
	8	9.09 304 9.09 405	101	9.09 640	102	0.90 360	9.99 664	53 52	
	9	9.09 506	101	9.09 845	103	0.90 155	9.99 661	51	.8 84.0 83.2 82 4
	10	9.09 606	101	9.09 947	102	0.99 053 0.89 951	9.99 659	50	9 94.5 93.6 92.7
	11	9.09 707	100	9.10 049	101	0.89 850	9.99 656	49 48	.1 10.2 10.1 10.0
	13	9.09 907	.99	9.10 252	102	0.89 748	9 99 653	47	.2 20.4 20.2 20.0 .3 30.6 30.3 30.0
	14	9.10 006	100	9.10 353	101	0.89 647	9.99.651	46	.3 30.6 30.3 30.0 .4 40.8 40.4 40.0
	16	9.10 203	99	9.10 555	101	0.89 445	9 99 650	44	.5 51.0 50.5 50.0
	17 18	9.10 304 9.10 402	98	9.10 656 9.10 756	100	0.89 344	9.99 648	43	
	19	9.10 501	99 98	9.10 856	100	0.89 144	9.99 645	41	.8 81.6 80.8 80.0
	20	9.10 599	98	9.10 956	100	0 89 044	9.99 643	40	.9  91.8  90.9  90.0
	2I 22	9.10 697	98	9.11 056	99	0.88 944	9.99.642	39 38	.1 9.9 9.8
	23	9.10 893	98 97	9.11 254	99	0.88 746	9.99 638	37	.2 19.8 19.6
-	24 25	9.10 990	97	9.11 353	99	0.88 647	9 99 637	36	.3 29.7 29.4 .4 39.6 39.2
	26	9.11 184	97 97	9.11 551	99	0.88 449	9.99 633	34	.5 49.5 49.0
	27 28	9.11 281	96	9.11 649	98	0.88 351	9.99 632 9.99 630	33 32	.6 59.4 58.8 .7 69.3 68.6
	29	9.11 474	97 96	9.11 747 9.11 845	98	0.88 155	9.99 629	31	.7 69.3 68.6 .8 79.2 78.4 .9 89.1 88.2
	30	9.11 570	96	9.11 943	98	0.88 057	9 99 627	30	97   96   95
	31	9.11 666	95	9.12 040 9.12 138	98	0.87 960	9.99 625 9.99 624	29 28	.1 9.7 9.6 9.5
	33	9.11 857	96	9.12 235	97	0 87 765	9.99 622	27	.2 19.4 19.2 19.0 .3 29.1 28.8 28.5
1	34	9.11 952	95	9.12 332	96	0 87 668	9.99 620	26	.4 38.8 38.4 38.0
	35 36	9.12 142	95	9.12 425	97	0.87 475	9.99 617	25 24	.5 48.5 48.0 47.5 .6 58.2 57.6 57.0
	37 38	9.12 236	94	9.12 621	96	0.87 379	9.99 613	23	.7 67.9 67.2 66.5
	39	9.12 331	94	9.12 717 9.12 813	96	0.87 187	9.99 612	21	.8 77.6 76.8 76.0
	40	9.12 519	94	9.12 909	96	0.87 091	9.99 610	20	94   93   93
1	41	9.12 612	94	9.13 004 9.13 099	95	0.86 996	9.59 608	18	.1 9.4 9.3 9.2
;	43	9.12 799	93 93	9.13 194	95 95	0 86 806	9 99 603	17	
	44	9.12 892	93	9.13 289	95	0.86 711	9.99 603	16	.4 37.6 37.2 36.8
	45 46	9.12.905	93	9.13 384 9 13 478	94	0 86 522	9 99 600	14	.5 47.0 46.5 46.0
	47 48	9 13 171	93	9 13 573 9 13 667	95	0 86 427	9 99 598	13	1 .7 05 .0 05 .1 04 .4
	49	9 13 263 9 13 355	92	9.13 761	94	0 86 239	9 99 596	11	.8 75.2 74.4 73.6 .9 84.6 83.7 82.8
	50	9 13 447	92	9.13 854	93	0.86 146	9.99 593	10	91 90 3
	51 52	9.13 539 9.13 630	91	9.13 948	93	0.86 052	9.99 591	9	.1 9 1 9.0 0.2
	52 53 54	9.13 722	92	9.14 134	93	0.85 866	9.99 589 9.99 588	7 6	.2 18.2 18.0 0.4 .3 27.3 27.0 0.6
-	54	9.13 813	91	9.14 227	93	0.85 773	9.99 586		.4 36.4 36.0 0.8
	56	9.13 904 9.13 994	90	9.14 320 9.14 412	92	0.85 588	9.99 584 9.99 582	5 4	.5 45.5 45.0 I.0 .6 54.6 54.0 I.2
	57	9.14 085	91	9.14 504	92	0.85 496	9.99 581	3 2	.7 63.7 63.0 1.4 .8 72.8 72.0 1.6
	55 56 57 58 59	9.14 175 9.14 266	91	9.14 597 9.14 688	91	0.85 403	9.99 579 9.99 577	I	.7 63.7 63.0 1.4 .8 72.8 72.0 1.6 .9 81.9 81.0 1.8
	60	9.14 356	90	9.14 780	92	0.85 220	9.99 575	0	
		L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	,	Prop. Pts.
						82°			

					8°	a: -				
,	L. Sin.	d.	L. Tang.	c.d.	L. Cotg.	L. Cos.		Prop. Pts.		
0	9.14 356 9.14 44 <u>5</u>	89	9.14 780 9.14 872	92	0.85 220 0.85 128	9.99 575 9.99 574	60	92   91   90		
2	9.14 535	90 89	9.14 963	91 91	0.85 037	9.99 572	<b>5</b> 9 58	.1 9.2 9.1 9.0		
3 4	9.14 624 9.14 714	90	9.15 054 9.15 145	91	0.84 946	9.99 570 9.99 568	57 56	.2 18.4 18.2 18.0 .3 27.6 27 3 27.0		
	9.14 803	89 88	9.15 236	91	0.84 764	9.99 566	55	.4 30.8 30.4 30.0		
5	9.14.891	89	9.15 327	91	0.84 673	9.99 563	54	.5 46.0 45.5 45.0		
8	9.14 980 9.15 069	89 88	9.15 417 9.15 508	91 90	0.84 492	9.99 563 9.99 561	53 52	.7 64.4 63.7 63.0		
9	9.15 157	88	9.15 598	90	0.84 402	9.99 559	51	.8 73.6 72.8 72.0 9 82.8 81.9 81.0		
10	9.15 245 9.15 333	88 88	9.15 688 9.15 777	89	0.84 312 0.84 223	9.99 557 9.99 556	50 49	89   88		
12	9.15 421	87	9.15 867	90 89	0.84 133	9.99 554	49 48	.1 8.9 8.8		
13	9.15 508	88	9.15 956 9.16 046	90	0.84 044 0.83 954	9:99 552 9.99 550	47 46	.2 17.8 17.6 .3 26 7 26.4		
15 16	9.15 683	8 <sub>7</sub>	9.16 135	89	0.83 865	9.99 548	45	.4  35.0  35.2		
17	9.15 770	87	9.16 224 9.16 312	88	0.83 776	9.99 546	44	6 53.4 52.8		
17	9.15 944	87 86	9.16401	89 88	0.83 599	9.99 543	42	6 53.4 52.8 .7 62.3 61.6 .8 71.2 70.4		
19 20	9.16 030	86	9.16 489	88	0.83 511	9-99 541	41	.9 80.1 79.2		
21	9 16 203	8 <sub>7</sub>	9.16 665	88	0.83 335	9-99 537	39 38	87   86		
22	9.16 289 9.16 374	. 85	9.16 753 9.16 841	88	0.83 247 0.83 159	9 99 535	38	.1 8.7 8.6 .2 17.4 17.2		
24	9 16 460	86 85	9.16 928	87 88	0.83 072	9.99 532	36	.3 26.1 25.8		
25 26	9.16 545 9.16 631	86	9.17 016 9.17 103	87	0.82 984	9.99 530 9.99 528	35	.4 34.8 34.4 .5 43.5 43.0		
27 28	9.16 716	8 <sub>5</sub> 8 <sub>5</sub>	9.17 190	8 <sub>7</sub>	0.82 810	9.99 526	34	.6 52.2 51.6		
28	9.16 801	85	9.17 277 9.17 363	86	0.82 723	9.99 524 9.99 522	32 31	.7 60.9 60. <b>2</b> .8 69.6 68. <b>8</b>		
80	9.16 970	84	9.17 450	87	0.82 550	9.99 520	30	.9 78.3 77.4		
31	9.17 053	8 <sub>5</sub>	9.17 536	86 86	0.82 464	9.99 518	29 28	.1 85 84 8.5 8.4		
3 <sup>2</sup> 33	9.17 139	84	9.17 622	86	0.82 378	9.99 517	27	.1 8.5 8.4 .2 17.0 16.8		
34	9.17 307	8 <sub>4</sub>	9.17 794	86 86	0.82 206	9.99 513	26	.3 25.5 25.2 .4 34.0 33.6		
35 36	9.17 391 9.17 474	83	9.17 880 9.17 965	85	0.82 120 0.82 035	9.99 511	25 24	.4 34.0 33.0 .5 42.5 42.0 .6 51.0 50.4		
37 38	9.17 558	8 <sub>4</sub> 8 <sub>3</sub>	9.18 051	86 85	0.81 949	9.99 507	23	.6 51.0 50.4 .7 59.5 58.8		
39	9.17 641 9.17 724	83	9.18 136 9.18 221	85	0.81 864	9 99 505	22 21	.8 68.0 67.2		
40	9.17 807	8 <sub>3</sub>	9.18 306	8 <sub>5</sub>	0.81 694	9.99 501	20	.9 76.5 75.6		
4I 42	9.17 890 9.17 973	83	9.18 391 9.18 475	84	0.81 609	9.99 499 9.99 497	19	.1 8.3 82 8.3 8.2		
43	9.18 055	82 82	9.18 560	8 <sub>5</sub>	0.81 440	9.99 495	17	.2 16.6 16.4		
44	9.18 137	83	9.18 644	84	0.81 356	9.99 494	16	.3 24.9 24.6 .4 33.2 32.8		
45 46	9.18 302	82 81	9.18 812	84	0.81 188	9.99 490	15	.5 41.5 41.0		
47 48	9.18 383 9.18 465	82	9.18 896 9.18 979	84 83	0.81 104	9.99 488 9.99 486	13 12	.7 58.1 57.4		
49	9.18 547	82 81	9.19 063	84	0.80 937	9.99 484	II	.8 66 4 65.6 .9 74 7 73.8		
50	9.18 628	81	9.19 146	8 <sub>3</sub>	0.80 854	9.99 482	10	8x   80   s		
5 <u>1</u> 5 <u>2</u>	9.18 709 9.18 790	81	9.19 229 9.19 312	83	0.80 771	9.99 480 9.99 478	9	.1 8.1 8.0 0.2		
52 53 54	9.18 871	81 81	9.19 395	83 83	0.80 60 <del>5</del> 0.80 522	9.99 476	7	.2 16.2 16.0 0.4 .3 24.3 24.0 0.6		
	9.18 952	81	9.19478	83	0.80 439	9.99 474		.4 32.4 32.0 0.8		
55 56 57 58 59	9.19 113	80 80	9.19 643	82 82	0.80 357	9.99 470	5	.5 40.5 40.0 I.O .6 48.6 48.0 I.2		
57	9.19 193 9.19 273	80	9.19 725 9 19 807	82	o.80 275 o.80 193	9.99 468 9.99 466	3 2	.7 56.7 56.0 I.4		
59	9.19 353	80 80	9.19 889	82 82	0.80 111	9.99 464	I	.8 64.8 64.0 1.6 .9 72.9 72.0 1.8		
60	9 19 433		9.19971		0.80 029	9.99 462	0			
	L. Cos.	d.	L. Cotg.	c. d.		L. Sin.	- /'	Prop. Pts.		
1	81°									

9°										
,	L. Sin.	d.	L. Tang.	c.d.	L. Cotg.	L. Cos.		Prop. Pts.		
0	9.19 433	80	9.19971	82	0.80 029	9.99 462	60			
1	9.19513	79	9.20 053	8r	0.79 947	9.99 460	59 58	82 81 80		
2	9.19 592	80	9.20 134	82	0.79 866	9.99 458 9.99 456	50	.1 8.2 8.1 8.0		
3	9.19 751	79	9.20 297	81	0.79 703	9.99 454	57 56	2 16.4 16.2 16.0 .3 24.6 24.3 24.0		
	9.19 830	79	9.20 378	8r	0.79 622	9.99 452	55	.3 24.6 24.3 24.6 .4 32.8 32.4 32.6		
5	9.19 909	79	9.20 459	8z	0.79 541	9.99 450	54	.5 41.0 40.5 40.0		
7 8	9.19 988	79	9.20 540	81	0.79 460	9.99 448	53	.5 41.0 40.5 40.6 .6 49.2 48.6 48.6		
	9.20 067	79 78	9.20 621	8r 8o	0.79 379	9.99 446	52	.7 57.4 56.7 56.6 .8 65.6 64.8 64.6		
9	9.20 145	78	9.20 701	81	0.79 299	9.99 444	51	.8 65.6 64.8 64.0		
10	9.20 223	79	9.20 782	80	0.79 218	9.99 442	50	.9 73.8 72.9 72.0		
11	9.20 302 9.20 380	78	9.20 862	80	0.79 138	9.99 440	49 48	79 78		
13	9.20 458	78	9.20 942	80	0.79 058	9.99 438 9.99 436		.1 7.9 7.8 .2 15.8 15.6		
14	9.20 535	77	9.21 102	80	0.78 898	9.99 434	47 46	.3 23.7 23.4		
15	9.20 613	78	9.21 182	80	0.78818	9.99 432	45	.4 31.6 31.2		
16	9.20 691	78	9.21 261	79	0.78 739	9.99 429	44	5 39.5 39.0		
17	9.20 768	77	9.21 341	80	<b>o</b> . 78 659	9.99 427	43	6 47.4 46.8		
18	9.20 845	77	9.21 420	79	0.78 580	9.99.425	42	.7 55.3 54.6 8 63.2 62.4		
19	9.20 922	77 77	9.21 499	79 79	0.78 501	9.99 423	41			
20	9.20 999	77	9 21 578		0.78 422	9,99 421	40			
21	9 21 076	77	9.21 657	<b>79</b>	0.78 343	9 99 419	39 38	77 76		
22 23	9 21 153	76	9 21 736	78	0.78 264	9.99 417	37	.I 7.7 7.6 .2 15.4 15.2		
24	9 21 306	77	9.21 893	79	0.78 107	9.99 413	36	.3 23.1 22.8		
25	9 21 382	76	9.21 971	78	0.78 029	9.99411	35	.4 30.8 30.4		
26	9.21 458	76	9.22 049	78	0.77 951	9.99 409	34	.5 38.5 38.0		
27 28	9 21 534	76	9.22 127	78	0.77 873	9.99 407	33	.6 46.2 45.6		
	9 21 610	76	9 22 205	78	0.77 793	9 99 404	32	.7 53.9 53.2 .8 61.6 60.8		
29	9.21 685	75 76	9.22 283	78 78	0.77 717	9 99 402	31	.9 69.3 68.4		
30	9.21 761		9.22 361		0 77 639	9 99 400	30			
31	9 21 836	75 76	9.22 438	77 78	0.77 552	9,99 398	29 28	75 74 . I 7.5 7.4		
32 33	9.21 912 9.21 987	75	9.22 516	77	0.77 484	9 99 396	27	.2 15.0 14.8		
34	9.22 062	75	9.22 670	- 77	0.77 330	9.99 394	26	.3 22.5 22.2		
	9.22 137	75	9.22 747	77	0.77 253	9 99 390	25	.4 30.0 29.6		
35 36	9.22 211	74	9.22 824	77	0.77 176	9.99 388	24	.5 37.5 37.0 .6 45.0 44.4		
37 38	9.22 286	75	9.22 901	77	0.77 099	9 99 385	23			
38	9.22 361	75 74	9.22 977	76	0.77 023	9 99 383	22	.7 52.5 51.8 .8 60.0 59.2		
39	9.22 435	74	9.23 054	77 76	0.76 946	9 99 381	21	.9 67.5 66.6		
40	9.22 509	74	9.23 130	76	0.76870	9 99 379	20	73   72		
41 42	9.22 583	74	9.23 206	77	0.76 717	9·99 37 <u>7</u> 9 99 37 <u>5</u>	18	.1 7.3 7.2		
43	9 22 731	74	9 23 359	76	0.76 641	9 99 372	17	.2 14.6 14.4		
44	9.22 803	74	9.23 435	76	0.76 565	9 99 370	16	.3 21.9 21.6		
45	9.22 878	73	9.23 510	75	0 76 490	9 99 368	15	4 29.2 28.8 5 36.5 36.0		
46	9.22 952	74	9.23 586	76	0.76 414	9.99 366	14	5 36.5 36.0 6 43.8 43.2		
47 48	9.23 025	73	9.23 661	75 76	0.76 339	9 99 364	13	.7 51.1 50.4		
40	9.23 098	73 73	9.23 737	75	0.76 263	9 99 362	12 11	.8 58.4 57.6		
49 <b>50</b>	9.23 171	73	9.23 812	75	0.76 113	9 99 359	10	.9 65.7 64.8		
51	9.23 244 9.23 317	73	9.23 887 9.23 962	75	0.76 038	9 · 99 357 9 · 99 355		72 3 3		
	9.23 390	73	9.24 037	75	0.75 063	9 99 353	9	.1 7.1 0.3 0.2		
52 53 54	9.23 462	72	9.24 112	75	0.75 888	9.99 351	7 6	.2 14.2 0.6 0.4 .3 21.3 0.9 0.6		
54	9.23 535	73	9.24 186	74	0.75 814	9.99 348		.3 21.3 0.9 0.6 .4 28.4 1.2 0.8		
55	9.23 607	72	9.24 261	75	0.75 739	9.99 346	5	.4 28.4 1.2 0.8 .5 35.5 1.5 1.6		
56	9.23 679	72	9.24 335	74	0.75 665	9.99 344	4	.5 35.5 I.5 I.6 .6 42.6 I 8 I.2		
57	9.23 752	73 71	9.24 410	75 74	0.75 590	9.99 342	3	.7 49.7 2 1 1.4		
55 56 57 58 59	9.23 823	72	9.24 484	74	0.75 516	9.99 34C	5 4 3 2 1	8 56.8 24 1.0		
27	9.23 895	72	9.24 558	74	0.75 442	9·99 337 9·99 33 <b>5</b>	0	.9 63 9 2 7 1.8		
4:11			U.ZA U(2		0.75 300	9.99 335	v			
60	L. Cos.	d.		c. d.	L. Tang.	L. Sin.	<b>—</b>	Prop. Pts.		

					10°			
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.		Prop. Pts.
0	9.23 967	72	9.24 632	74	0.75 368	9.99 335	60	
1 2	9.24 039 9.24 110	71	9.24 706	73	0.75 294 0.75 221	9.99 333 9.99 331	59 58	.I 7.4 7.3
3	9.24 181	71 72	9.24 853	74 73	0.75 147	9.99 328	57	.2 14.8 14.6
4	9.24 253	71	9.24 926	74	0.75 074	9.99 326	56	.3 22.2 21.9
5	9.24 32 <u>4</u> 9.24 39 <u>5</u>	71	$9.2\overline{5} \infty$ $9.25 073$	73	0.75 000 0.74 927	9.99 324 9.99 322	55 54	.4 29.6 29.2 .5 37.0 36.5
7 8	9.24 466	71 70	9.25 146	73	0.74 854	9.99 319	53	.6 44 4 43.8
	9.24 536 9.24 607	71	9.25 219	73 73	0.74 781	9.99 317	52	.7 51.8 51.1 .8 59.2 58.4
9 10	9.24 677	70	9.25 292	73	0.74 708	9.99 315	$\frac{51}{50}$	.9 66.6 65.7
11	9.24 748	7I 70	9.25 437	72 73	0.74 563	9.99 310	49 48	72 71
12	9.24 818 9.24 888	70	9.25 510 9.25 582	73	0.74 490	9.99 308		.I 7.2 7.I
13 14	9.24 958	70	$9.2565\overline{5}$	73	0.74 418	9.99 306	47 46	.2 14.4 14.2 .3 21.6 21.3
15 16	9.25 028	70	9.25 727	72.	0.74 273	9.99.301	45	.4 28.8 28.4
	9.25 098	70	9.25 799	72 72	0.74 201	9.99 299	44	.5 36.0 35.5 .6 43.2 42.6
17	9.25 168	69	9.25 871	72	0.74 129	9.99 297 9.99 294	43 42	
19	9.25 307	7° 69	9.26 015	72 71	0.73 985	9.99 292	41	.7 50.4 49.7 .8 57.6 56.8
20	9.25 376	69	9.26 086	72	0.73 914	9.99 290	40	.9 64.8 63.9
2I 22	9.25 445 9.25 514	69	9.26 158	71	0.73 842	9.99 288 9.99 285	39 38	.1 7.0 6.9
23	9.25 583	69	9.26 301	72	c 73 699	9.99 283	1 37 1	.2 14.0 13.8
24	9.25 652	69	9.26 372	71	0.73 628	9.99 281	36	.3 21.0 20.7 .4 28.0 27.6
25 26	9.25 721	69	9.26 443 9.26 514	71	0.73 557	9.99 278	35 34	
27	9.25 858	68	9.26 583	71	0.73 415	9.99 274	33	.6 42.0 41.4
28	9.25 927	69	9.26 655	70	0.73 345	9.99 271	32	.7 49.0 48.3 .8 56.0 55.2
30	9.25 995	68	9.26 797	71	0.73 274	9.99 269	$\frac{31}{30}$	.9 63.0 62.1
31	9.26 131	68	9.26 867	70	0.73 133	9.99 264	29	68 67
32	9.26 199	68	9.26 937	70	0.73 063	9.99 262	28	.1 6.8 6.7 1 .2 13.6 13.4
33 34	9.26 267 9.26 335	68	9.27 008 9.27 078	70	0.72 992	9.99 260	27 26	.3 20.4 20.1
35	9.26 403	68	9.27 148	70	0.72 852	9.99 255	25	.4 27.2 26.8
36	9.26 470	67	9.27 218	70	0.72 782	9.99 252	24	.5 34.0 33.5 .6 40.8 40.2
37 38	9.26 538	67	9.27 288 9.27 357	69	0.72 712	9.99 250 9.99 248	23	.7 47.6 46.9
39	9.26 672	67	9.27 427	- 69	0.72 573	9 99 245	21	.8 54.4 53.6 .9 61.2 60.3
40	9.26 739	67	9.27 496	70	0.72 504	9.99 243	20	66   65
41	9.26 806 9.26 873	67	9.27 566 9.27 635	69	0.72 434	9.99 241 9.99 238	18	.1 6.6 6.5
43	9.26 940	67	9.27 704	69	0.72 296	9.99 236	17	.2 13.2 13.0
44	9.27 007	66	9.27 773	- 69	0.72 227	9.99 233	16	.3 19.8 19.5 .4 26.4 26.6
45 46	9.27 073 9.27 140	67	9.27 842 9.27 911	69	0.72 158	9.99 231 9.99 229	15	.5 33.0 32.5
47 48	9.27 206	66	9.27 980	69	0.72 020	9.99 226	13	
	9.27 273	66	9.28 049 9.28 117	68	0.71 951	9 99 224	12 11	.8 52.8 52.0
49 <b>50</b>	$\frac{9.27\ 339}{9.27\ 40\overline{5}}$	66	9.28 186	- 69	0.71 814	9.99 219	10	.9 59.4 58.5
51	9.27 471	66	9.28 254	68	0.71 746	9.99 217	0	3 2
52	9.27 537 9.27 602	66	0.28 323	68	0.71 677	9.99 214	8	.I 0.3 0.2 .2 0.6 0.4
53 51	9.27 668	66	9.28 391 9.28 459	68	0.71 609	9.99 212 9.99 209	7 6	.3 0.9 0.6
55	9.27 734	66	9.28 527	- 68	0.71 473	9.99 207	5	.4 I.2 C.8
56	9.27 799	65	9.28 595	68	0.71 405	9.99 204	4	.5 1.5 1.0 .6 1.8 1.2
57	9.27 864 9.27 930	66	9.28 730	68	0.71 338	9.99 202	3 2	.7 2.1 1.4
55 56 57 58 59 <b>60</b>	9.27 995	65	9.28 798	68	0.71 202	9.99 197	1	.8 2.4 1.6 .9 2.7 1.8
60	9 38 060	65	9.28 865		0.71 135	9.99 195	0	
-	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	,	Prop. Pts.

					11°			
,	L. Sin.	d.	L. Tang.	c.d.	L. Cotg.	L. Cos.	1	Prop. Pts.
7 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 31 31 31 31 31 31 31 31 31 31 31 31	9.28 060 9.28 125 9.28 190 9.28 254 9.28 319 9.28 348 9.28 448 9.28 517 9.28 705 9.28 769 9.28 833 9.28 896 9.28 960 9.29 024 9.29 087 9.29 140 9.29 277 9.29 340 9.29 277 9.29 340 9.29 591 9.29 591 9.29 654 9.29 779 9.29 347 9.29 591 9.29 591 9.29 666 9.30 028	65 64 65 65 64 64 65 64 64 63 64 63 64 63 63 63 63 63 63 63 63 63 63 63 63 63	L. Tang.  9.28 865 9.28 933 9.29 ∞∞ 9.29 657 9.29 134 9.29 235 9.29 402 9.29 468 9.29 535 9.29 661 9.29 668 9.29 734 9.29 8∞ 9.29 866 9.29 932 9.29 938 9.30 654 9.30 130  9.30 195 9.30 525 9.30 527 9.30 522 9.30 587 9.30 552 9.30 717 9.30 782 9.30 846	68 67 67 67 67 67 66 66 66 66 66 66 65 65 65 65 65 65 65		L. Cos.  9.99 195 9.99 190 9.99 180 9.99 180 9.99 172 9.99 173 9.99 172 9.99 160 9.99 160 9.99 160 9.99 157 9.99 152 9.99 152 9.99 152 9.99 154 9.99 154 9.99 154 9.99 154 9.99 154 9.99 154 9.99 154 9.99 124 9.99 124 9.99 129 9.99 119	60 59 57 55 55 55 55 55 55 55 49 47 44 43 44 44 44 44 44 44 45 44 47 46 47 46 47 48 48 48 48 48 48 48 48 48 48	68   67 .1   6.8   6.7 .2   13.6   13.4 .3   20.4   20.1 .4   27.2   26.8 .5   34.0   33.5 .6   40.8   40.2 .7   47.6   46.9 .8   54.4   53.6 .9   61.2   60.3 66   6.5 .1   6.6   6.5 .2   13.2   13.0 .3   19.8   19.5 .4   26.4   26.0 .5   33.0   32.5 .6   39.6   39.0 .7   46.2   45.5 .8   52.8   52.0 .9   59.4   58.5 64   63 .1   6.4   6.3 .2   12.8   12.6 .3   19.2   18.9 .4   25.6   25.2 .5   32.0   31.5 .6   38.4   37.8 .7   44.8   44.1   .8   57.6   56.7 62   61
32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 55 57 58 59 60	9.30 090 9.30 151 9.30 213 9.30 275 9.30 336 9.30 336 9.30 352 9.30 521 9.30 582 9.30 643 9.30 765 9.30 887 9.30 947 9.31 068 9.31 129 9.31 189 9.31 250 9.31 370 9.31 430 9.31 490 9.31 549 9.31 669 9.31 728 9.31 788	62 62 61 62 61 62 61 61 61 61 61 60 60 60 60 60 60 60 60 60 60 60 60 60	9.30 975 9.31 040 9.31 104 9.31 168 9.31 233 9.31 297 9.31 361 9.31 425 9.31 489 9.31 552 9.31 616 9.31 670 9.31 743 9.31 806 9.31 870 9.31 933 9.31 996 9.32 248 9.32 248 9.32 311 9.32 373 9.32 498 9.32 591 9.32 623 9.32 685 9.32 747	64 64 65 64 64 64 63 64 63 63 63 63 63 63 63 63 62 63 62 63 62 63 62 63	o. 69 o25 o. 68 960 o. 68 896 o. 68 896 o. 68 767 o. 68 703 o. 68 575 o. 68 575 o. 68 571 o. 68 321 o. 68 321 o. 68 321 o. 68 027 o. 68 007 o. 67 941 o. 67 875 o. 67 689 o. 67 669 o. 67 650 o. 67 439 o. 67 377 o. 67 315 o. 67 253	9.99 114 9.99 109 9.99 106 9.99 104 9.99 101 9.99 099 9.99 093 9.99 086 9.99 083 9.99 086 9.99 072 9.99 072 9.99 072 9.99 064 9.99 065 9.99 059 9.99 059 9.99 059 9.99 059 9.99 059 9.99 054 9.99 048 9.99 048 9.99 048 9.99 049	28 27 26 25 24 23 22 21 20 19 18 17 16 15 14 13 12 11 10 9 8 7 6 4 3 2 1	.1 6.2 6.1 .2 12.4 12.2 .3 18.6 18.3 .4 24.8 24.4 .5 31.0 30.5 .6 37.2 36.6 .7 43.4 42.7 .8 49.6 48.8 .9 55.8 54.9 .1 6.0 5.9 .1 6.0 5.9 .2 12.0 11.8 .3 18.0 17.7 .4 24.0 23.6 .5 30.0 29.5 .6 36.0 35.4 .7 42.0 41.3 .8 48.0 47.2 .9 54.0 53.1 .1 0.3 0.2 .2 0.6 0.4 .3 0.9 0.6 .4 1.2 0.8 .5 1.5 1.0 .6 1.8 1.2 .7 2.1 1.4 .9 2.7 1.8
1-	L. Cos.	d.	I L. Cotg.	C. d.	L. Tang. 78°	L. Sin.	,	Prop. Pts.
1					10			

	12°										
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.		Prop. Pts.			
0	9.31 788	59	9.32 747	63	0.67 253	9.99 040	60	-			
I	9.31 847	60	9.32 810 9.32 872	62	0.67 190	9.99 038	59 58	63   62			
3	9.31 907	59	9.32 972	61	0.67 128	9.99 035 9.99 032	50	.1 6.3 6.2 .2 12.6 12 4			
4	9.32 023	59 59	9.32 995	62 62	0.67 ∞5	9.99 030	56	.3 18.9 18.6			
5	9.32 084	59	9.33 057	62	0.66 943	9.99 027	55	.4 25.2 24.8			
	9.32 I43 9.32 202	59	9.33 119 9.33 180	61	0.66 881 0.66 820	9.99 024	54	.5 31.5 31.0 .6 37.8 37.2			
7 8	9.32 261	59	9.33 242	62	0.66 758	9.99 022 9.99 019	53 52	.7 44.1 43.4			
9	9.32 319	58 <b>5</b> 9	9.33 303	61 62	0.66 697	9.99 016	51	8 50.4 49.6			
10	9.32 378	59	9.33 365	61	0.66 635	9.99 013	50	.9 56.7 55.8			
II I2	9.32 437 9.32 49 <b>5</b>	58	9.33 426 9.33 487	61	0.66 574 0.66 513	9.99 011	49 48	. I 6. I 6.0			
13	9.32 553	58	9.33 548	61	0.66 452	9.99 005	47	.2 12.2 12.0			
14	9.32 612	59 58	9.33 609	61 61	0.66 391	9.99 002	46	.3 18.3 18.0			
15	9.32 670	58	9.33 670	61	0.66 330	9.99 000	45	.4 24.4 24.0			
16	9.32 728 9.32 786	58	9.33 731	61	0.66 269	9.98 997	44	.5 30.5 30.0 .6 36.6 36.0			
17 18	9.32 844	58	9.33 792 9.33 853	61	0.66 147	9.98 991	43 42	.7 42.7 42.0			
19	9.32 902	<b>58</b>	9.33 913	60 61	0.66 087	9.98 989	4I	.7 42.7 42.0 .8 48.8 48.0			
20	9.32 960	58	9.33 974	60	0.66 026	9.98 986	40	.9  54.9  54.0			
21	9.33 018	57	9.34 034	61	0.65 966	9.98 983	39 38	.1 5.9			
22 23	9.33 075 9.33 <b>1</b> 33	58	9.34 095	60	0.65 90 <u>5</u> 0.65 845	9.98 980 9.98 978	30	.1 5.9 .2 11.8			
24	9.33 190	57	9.34 215	60 61	0.65 785	9.98 975	37 36	.3 17.7			
25	9.33 248	58	9.34 276	60	0.65 724	9.98 972	35	.4 23.6			
26	9.33 305	57 57	9.34 336	60	0.65 664	9.98 969	34	.5 29.5 .6 35.4			
27 28	9.33 362	58	9.34 396	60	0.65 604	9.98 967 9.98 964	33				
29	9.33 477	57	9.34 456 9.34 516	60	0.65 484	9.98 961	32 31	.7 41.3 .8 47.2			
30	9.33 534	57	9.34 576	60	0.65 424	9.98 958	30	.9  53.1			
31	9.33 591	57 56	9.34 635	59 60	0.65 365	9.98 955	29	.I 5.8 5.7			
32	9.33 647 9.33 704	57	9.34 695	60	0.65 305	9.98 9 <u>5</u> 3 9.98 9 <u>5</u> 0	28 27	2 11.6 11.4			
34	9.33 761	57	9·34 755 9·34 814	59	0.65 186	9.98 947	26	.3 17.4 17.1			
35	9.33 818	57	9.34 874	60	0.65 126	9.98 944	25	.4 23.2 22.8 .5 29.0 28.5			
36	9.33 874	56 57	9.34 933	59 59	0.65 067	9.98 941	24	.5 29.0 28.5 .6 34.8 34.2			
37 38	9.33 931	56	9.34 992	59	0.65 008	9.98 938	23 22	7 40.6 39.9			
39	9.33 987 9.34 043	56	9.35 051	60	0.64 889	9.98 933	21				
40	9.34 100	57	9.35 170	59	0.64 830	9.98 930	20	.9  52.2  51.3			
41	9.34 156	56 56	9.35 229	59	0.64 771	9.98 927	19	.1 56 55 .1 5.6 5.5			
42	9.34 212 9.34 268	56	9.35 288	59	0.64 712	9.98 924 9.98 921	18	.2 11.2 11.0			
43 44	9.34 208	56	9·35 347 9·35 405	58	0.64 595	9.98 921	16	.3 16.8 16.5			
45	9.34 380	56	9.35 464	59	0.64 536	9.98 916	15	.4 22.4 22.0 .5 28.0 27.5			
46	9.34 436	56	9.35 523	59 58	0.64 477	9.98 913	14	6 33.6 33.0			
47 48	9.34 491	55 56	9.35 581	59	0.64 419	9.98 910	13	.7 39.2 38.5			
49	9·34 547 9·34 602	55	9.35 640 9.35 698	58	0.64 302	9.98 904	II				
50	9.34 658	56		59	0.64 243	9.98 901	10				
51	9.34 713	55	9·35 757 9·35 815	58	0.64 185	9.98 898	9				
52 53	9.34 769	56 55	9.35 873	58	0.64 127	9.98 896 9.98 893	8	.2 0.6 0.4			
53 54	9.34 824 9.34 879	55	9.35 931 9.35 989	58	0.64 011	9.98 890	7 6				
55	9.34 934	55	9.36 047	58	0.63 953	9.98 887	5	.3 0.9 0.6 4 1.2 0.8 5 1.5 1.0 6 1.8 1.2			
56	9.34 989	55	9.36 105	58	0.63 893	9.98 884	4	5 1.5 1.0 6 1.8 1.2			
57	9.35 044	55 55	9.36 163	58 58	0.63 837	9.98 881	3 2	7 2.1 1.4			
58	9.35 099	55	9.36 221 9.36 279	58	0.63 779	9.98 878 9.98 875	1				
55 56 57 58 59 <b>60</b>	9.35 154	55	9.36 336	57	0.63 664	9.98 872	0	.9  2.7  1.8			
-00		-		-				Prop. Pts.			
	L. Cos.	d.	1104		L. Tang.	L. Sin.	,	Pron. Pre.			

-					13°			
1	L. Sin.	d.	L. Tang.	c.d.	L. Cotg.	L. Cos.		Prop. Pts.
0	9.35 209 9.35 263	54	9.36 336 9.36 394	58	0.63 664	9.98 872	60	
2	9.35 318	55	9.36 452	58	0.63 548	9.98 869	59 58	.I 5.8 5.7
3	9.35 373	55 54	9.36 509	57 57	0.63 491	9.98 864	57	.2 11.6 11.4
4	9.35 427	54	9.36 566	58	0.63 434	9.98 861	56	-3 17.4 17.1
5	9.35 536	55	9.36 681	57	0.63 319	9.98 858 9.98 85 <del>3</del>	55 54	4 23.2 22.8 .5 29.0 28.5
8	9.35 590	54 54	9.36 738	57 57	0.63 262	9.98 852	53	.6 34.8 34.2
9	9.35 644 9.35 698	54	9.36 795 9.36 852	57	0.63 203	9.98 849 9.98 846	52 51	.7 40.6 39.9 .8 46.4 45.6
10	9.35 752	54	9.36 909	57	0.63 091	9.98 843	$\frac{3}{50}$	.9 52.2 51.3
II	9.35 806	54 54	9.36 966	57 57	0.63 034	9.98 840	40	56 55
12	9.35 860 9.35 914	54	9.37 023 9.37 080	57	0.62 977	9.98 837 9.98 834	48 47	.1 5.6 5.5 .2 11.2 11.0
14	9.35 968	54 54	9.37 137	57 56	0.62 863	9.98 831	46	.3 16.8 16.5
15 16	9.36 022	53	9.37 193	57	0.62 807	9.98 828	45	.4 22.4 22.0
	9.36 075 9 36 129	54	9.37 250 9.37 306	56	0.62 750	9.98 825 9.98 822	44 43	.6 33.6 33.6
17 18	9.36 182	53 54	9.37 363	57 56	0.62 637	9.98 819	42	.7 39.2 38.5
20	9.36 236	53	9.37 419	57	0.62 581	9.98 816	$\frac{41}{40}$	.8 44.8 44.0 .9 50.4 49.5
21	9.36 342	53	9.37 476 9.37 532	56	0.62 524 0.62 468	9.98 813		54
22	9.36 395	53 54	9.37 588	56 56	0.62 412	9.93 807	39 38	.1 5.4
23 24	9.36 449 9.36 502	53	9.37 644 9.37 700	56	0.62 356 0.62 300	9.98 804 9.98 801	37 36	.2 10.8 .3 16.2
25	9.36 555	53	9.37 756	56	0.62 244	9.98 798	35	.4 21.6
26	9.36 608	53 53	9.37 812	56 56	0.62 188	9.98 795	34	.5 27.0 .6 32.4
27 28	9.36 660 9.36 713	53	9.37 868	56	0.62 132	9.98 792 9.98 789	33 32	.7 37.8
29	9.36 766	53 53	9.37 980	56	0.62 020	9.98 786	31	.7 37.8 .8 43.2 .9 48.6
30	9.36 819	52	9.38 035	55 56	0.61 963	9.98 783	30	1 53   52
31 32	9.36 871 9.36 924	53	9.38 091	56	0.61 909 0.61 853	9.58 780 9.98 777	29 28	.1 5.3 5.2
33	9.36 976	52 52	9.38 202	55 55	0.61 853 0.61 798	9.98 774	27	.2 10.6 10.4
34	9.37 028 9.37 081	53	9.38 257	56	0.61 743	9.98 771 9.98 768	26	.3 15.9 15.6
35 36	9.37 133	52	9.38 368	55	0.61 632	9.98 765	25 24	.5 26.5 26.0
37 38	9.37 185	52 52	9.38 423	55 56	0.61 577	9.98 762	23	.6 31.8 31.7 .7 37.1 36.4
39	9.37 237 9.37 289	52	9.38 479 9.38 534	55	0.61 521	9.98 759 9.98 756	22 2I	.8 42.4 41.6
40	9.37 34I	52	9.38 589	55	0.61 411	9.98 753	20	.9 47.7 46.8
41	9.37 393	52 52	9.38 644 9.38 699	<b>55</b> <b>5</b> 5	0.61 356	9.98 750 9.98 746	19 18	.1 5.1 0.4
42	9·37 445 9·37 497	52	0.38 754	55	0.61 246	9.98 743	17	.2 10.2 0.8
44	9-37 549	52 51	9.38 808	54 55	0.61 192	9.98 740	16	.3 15.3 1.2 .4 20.4 1.6
45 46	9.37 600 9.37 652	52	9.38 863 9.38 918	55	0.61 137 0.61 082	9.98 737 9.98 734	15 14	.5 25.5 2.0
47 48	9.37 703	51	9.38 972	54	0.61 028	9.98 731	13	.6 30.6 2.4 C
48 49	$9.3775\overline{5}$ $9.37806$	52 51	9.39 027 9.39 082	55 55	o.60 973 o.60 918	9.98 728 9.98 72 <del>5</del>	12 11	.8 40.8 3.2
50	9.37 858	52	9.39 136	54	0.60 864	9.98 722	10	.9 45.9 3.6
51	9.37 909	51 51	9.39 190	54	0.60 810	9.98 719	9	.1 0.3 0.2
52	9.37 960 9.38 011	51	9.39 24 <del>5</del> 9.39 299	55 54	0.60 755 <b>0</b> .60 701	9.98 715 9.98 712		.2 0.6 0.4 .3 0.9 0.6
52 53 54	9.38 002	51	9.39 353	54	0.60 647	9.98 709	7	.2 0.6 0.4 .3 0.9 0.6 .4 1.2 0.8
55 56	9.38 113	51 51	9.39 407	54 54	0.60 593	9.98 706	5	.5 1.5 1.0
57	9.38 164 9.38 215	51	9.39 461 9.39 515	54	o.60 539 o.60 485	9.98 703 9.98 700	4	.6 I.8 I.2 .7 2.1 I.4
57 58 59	9.38 266	51 51	9.39 569	54	0.60 431	9.98 697	3 2	.8 2.4 1.6
<u>59</u>	9.38 317	51	9.39 623 9.39 677	54 54	0.60 377	9.98 694	- <u>I</u>	.9 2.7 1.8
00							_	Drop Die
	L. Cos.	d.	L. Cotg.	c. u.	76°	L. Sin.	,	Prop. Pts.

					14°				
,	L. Sin.	d.	L. Tang.	c.d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.38 368	50	9.39 677	54	0.60 323	9.98 690	3	60	
I 2	9.38 418 9.38 469	51	9.39 731	54	0.60 269	9.98 68 <b>7</b> 9.98 684	3	59 58	
3	9.38 519	50 51	9.39 78 <del>5</del> 9.39 838	53 54	0.60 162	9.98 681	3	57	54 53 .1 5.4 5.3
4	9.38 570	50	9.39 892	53	0.60 108	9.98 678	3	57 56	.1 5.4 5.3 .2 10 8 10.6
5	9.38 620 9.38 670	50	9·39 945 9·39 999	54	0.60 05 <u>5</u> 0.60 001	9.98 67 <del>5</del> 9.98 671	4	55	.3 16.2 15.9
	9.38 721	51	9.40 052	53	0.59 948	9.98 668	3	54 53	.4 21.6 21.2 .5 27.0 26.5
8	9.38 771 9.38 821	50	9.40 106	54 53	0.59 894	9.98 665	3	53 52	.5 27.0 26.5 .6 32.4 31 8
9	9.38 821	50	9:40 159	53	0.59 841	9.98 662	3	51	.7 37.8 37.1
10 11	9.38 921	50	9.40 212	54	0.59 788 0.59 734	9.98 659 9.98 656	3	50	.8 43.2 42.4 .9 48.6 47.7
12	9.38 971	50	9.40 319	53 53	0.59 681	9.98 652	4	49 48	.9140.0147.7
13	9.39 021	50	9.40 372	53	0.59 628	9.98 649 9.98 646	3	47 46	1 50 1 50
14	9.39 071	50	9.40 425	53	0.59 575	9.98 643	3	45	.1 5.2 5.1
16	9.39 170	49	9.40 531	53	0.59 469	9.98 640	3	44	.2 10.4 10.2
17 18	9.39 220	50	9.40 584	53 52	0.59 416	9.98 636	4	43	.3 15.6 15.3 .4 20.8 20.4
19	9.39 270 9.39 319	49	9.40 636 9.40 689	53	0.59 364	9.98 633 9.98 630	3	42 41	
20	9.39 369	50	9.40 742	53	0.59 258	9.98 627	3	40	.6 31.2 30.6
21	9.39 418	49 49	9.40 795	53 52	0.59 205	9.98 623	4	39 38	.7 36.4 35. <b>7</b> .8 41.6 40. <b>8</b>
22 23	9.39 467 9.39 517	50	9.40 847 9.40 900	53	0.59 153	9 98 620 9.98 617	3	38 37	.9 46.8 45.9
24	9.39 566	49	9.40 952	52	0.59 048	9.98 614	3	36	
25	9.39 615	49	9.41 005	53 52	0.58 995	9.98 610	4	35	1 50 1 49
26	9.39 664	49 49	9.41 057	52	0.58 943	9.98 607	3	34	
27 28	9.39 713 9.39 762	49	9.41 161	52	0.58 891	9.98 604 9.98 601	3	33 32	2 10.0 9.8
29	9.39 811	49	9.41 214	53 52	0.58 786	9.98 597	4	31	.3 15.0 14.7 .4 20.0 19.6
80	9.39 860	49 49	9.41 266	52	0.58 734	9.98 594	3	30	
3I 32	9.39 909 9.39 958	49	9.41 318	52	0.58 682	9.98 591 9.98 588	3	29 28	.5 25.0 24.5 .6 30.0 29.4
33	9.40 006	48	9.41 422	. 52	0.58 578	9.98 584	4	27	.7 35.0 34.3 .8 40.0 39.2
34	9.40 053	49 48	9.41 474	52 52	0.58 526	9.98 581	3	26	.9 45.0 44.1
35	9.40 103	49	9.41 526	52	0.58 474	9.98 578 9.98 574	4	25 24	
36	9.40 152 9.40 200	48	9.41 578	51	0.58 371	9.98 571	3	23	48   47
37 38	9.40 249	49 48	9.41 681	52 52	0.58 319	9.98 568	3	22	.1 48 47
39	9.40 297	49	9.41 733	51	0.58 267	9.98 56 <del>5</del> 9.98 561	4	$\frac{21}{20}$	.2 9.6 9.4
40 41	9.40 346	48	9.41 784 9.41 836	52	0.58 164	9.98 558	3	19	.3 I4.4 I4.I .4 19.2 18.8
42	9.40 442	48	9.41 887	51 52	0.58 113	9.98 555	3	18	
43	9.40 490 9.40 538	48	9.41 939	51	0.58 061	9.98 551 9.98 548	3	17	6 28.8 28.2
44 45	9.40 586	48	9.41 990	51	0.57 959	9.98 545	3	15	.7 33.6 32.9 .8 38.4 37.6
46	9.40 634	48	9.42 041	52	0.57 907	9.98 541	4	14	.9 43.2 42.3
47	9.40 682	48	9.42 144	51	0.57 856	9.98 538	3	13	
48 49	9.40 <b>7</b> 30 9.40 778	48	9.42 195 9.42 246	51	0.57 803	9.98 53 <del>5</del> 9.98 531	4	12 11	1 4 1 3
50	9.40 825	47	9.42 297	51	0.57 703	9.98 528	3	10	.1 0.4 0.3
51	9.40 873	48 48	9.42 348	51	0.57 652	9.98 525	3 4	9 8	.2 0.8 0.6
52	9.40 921 9 4c 968	47	9.42 399	51	0.57 601	9 98 521 9.98 518	3	7	.3 I.2 0.9 .4 I.6 I.2
54	9.41 016	48	9.42 501	51	0.57 499	9.98 515	3	7 6	.5 2.0 1.5
55 56	9.41 063	47	9.42 552	51	0.57 448	9.98 511	4	5	.6 2.4 1.8 .7 2.8 2.1
56	9.41 111	47	9.42 603 9.42 653	50	0.57 397 0.57 347	9.98 508	3	5 4 3 2	.8 3.2 2.4
58	9.41 205	47	9.42 704	51	0.57 296	9.98 501	4		.9 3.6 2.7
59	9.41 252	47	9.42 753	51	0.57 245	9.98 498	3 4	1	
60	9.41 300		9.42 805		0.57 193	9.98 494		0	
	L. Cos.	d.	L. Cotg.	c.d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.

					15°						
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		P	rop. P	ts.
0	9.41 300	47	9.42 805	51	0.57 195	9.98 494	3	60			
1 2	9.41 347 9.41 394	47	9.42 856 9.42 906	50	0.57 144	9.98 491 9.98 488	3 .	59 58			
3	9.41 441	47	9.42 957	51 50	0.57 043	9.98 484	4	57	.1	5. I	5.0
4	9.41 488	47	9.43 007	50	0.56 993	9.98 481	3 4	_56_	.2		10.0
5	9.41 53 <del>5</del> 9.41 582	47	9.43 057 9.43 108	51	0.56 943	9.98 477 9.98 474	3	55	.3	15.3	15.0
7 8	9.41 628	46	9.43 158	50	0.56 842	9.98 471	3	54 53	.4		20.0
	9.41 675	47	9.43 208	50 50	0.56 792	9.98 467	4	52	.5	30.6	30.0
10	9.41 722	46	9.43 258	50	0.56 742	9.98 464	14	51	.7	35.7	35.0
11	9.41 815	47	9.43 308 9.43 358	50	0.56 642	9.98 460 9.98 457	3	50 40	.9	40.8	40.0
12	9.41 861	46	9.43 408	50	0.56 592	9.98 453	4 3.	49 48	7	73.71	13
13	9.41 908	46	9.43 458 9.43 508	50	0.56 542	9.98 450 9.98 447	3.	47 46		49	48
	9.41 934	47	9.43 558	50	0.56 442	9.98 447	4	45	.1		4.8
15 16	9.42 047	46 46	9.43 607	49	0.56 393	9.98 440	3	45	.2	9.8	9.6
17	9.42 093	47	9.43 657	50	0.56 343	9.98 436	4	43	.4		14.4 19.2
19	9.42 140	46	9.43 707 9.43 756	49	0.56 293	9.98 433 9.98 429	4	42 4I		24.5	24.0
20	9.42 232	46	9.43 806	50	0.56 194	9.98 426	3	40	.6		28.8
21	9.42 278	46 46	9.43 855	49 50	0.56 143	9.98 422	4	39 38	·7	34.3	33.6 38.4
22 23	9.42 324 9.42 370	46	9.43 905 9.43 954	49	0.56 095	9.98 419	4	38	.9	44.1	43.2
24	9.42 416	46	9.44 004	50	0.55 996	9.98 412	3	36	6		
25	9.42 461	45 46	9.44 053	49	0.55 947	9.98 409	3	35	,	47	46
26	9.42 507	46	9.44 IO2 9.44 ISI	49	0.55 898	9.98 405	4	34	. 1	4.7	4.6
27 28	9.42 553	46	9.44 201	50	0.55 799	9.98 398	4	33 32	.2	9.4	9.2
29	9.42 644	45 46	9.44 250	49	0.55 750	9.98 395	3	31	·3	14.1	13.8
80	9.42 690	45	9.44 299	49	0.55 701	9.98 391	3	30	.5	23.5	23.0
31 32	9.42 735 9.42 781	46	9.44 348	49	0.55 652	9.98 388 9.98 384	4	29	.6		27.6 32.2
33	9.42 826	45 46	9.44 446	49	0.55 554	9.98 381	3	27	.7	37.6	36.8
34	9.42 872	45	9.44 495	49	0.55 505	9.98 377	4	26	.9		41.4
35 36	9.42 917 9.42 962	45	9·44 544 9·44 592	48	0.55 456	9.98 373 9.98 370	3	25 24			i
37 38	9.43 008	46	9.44 641	49	0.55 359	9.98 366	4	23	١,	45	44
38	9.43 053 9.43 098	45	9.44 690	49	0.55 310	9.98 363 9.98 359	3	22 21	1.	4.5	4.4
40		45	9.44 738	49	0.55 213	9.98 356	3	20	.2	9.0	
41	9.43 I43 9.43 I88	45	9.44 836	49	0.55 164	9.98 352	4	19	•3		13.2 17.6
42	9.43 233	45 45	9.44 884	48	0.55 116	9.98 349	3 4	18	.5	22.5	22.0
43	9.43 278	45	9.44 933 9.44 981	48	0.55 067	9.98 345 9.98 342	3	17 16	.0	27.0	26.4 30.8
45	9.43 367	44	9.45 029	48	0.54 971	9.98 338	4	15	.7 .8	36.0	35.2
46	9.43 412	45	9.45 078	49	0.54 922	9.98 334	3	14	.9	40.5	39.6
47 48	9.43 457 9.43 502	45	9.45 I26 9.45 I74	48	0.54 874	9.98 331 9.98 327	4	13			
49	9.43 546	44	9.45 222	48	0.54 778	9.98 324	3	II		4 1	3
50		45	9.45 271	49	0.54 729	9.98 320	3	10	.I	0.8	0.6
51	9.43 635	45	9.45 319	48	0.54 681	9.98 317 9.98 313	4	8	.2	1.2	
52 53 54	9.43 724	44	9.45 307	48	0.54 585	9.98 309	4	7 6	.4	1.6	0.9
54	9.43 769	45	9.45 463	48	0.54 537	9.98 306	3		.4 .5 .6	2.0	I.5 I.8
55 57 58 59	9.43 813 9.43 857	44	9.45 511 9.45 559	48	0.54 489	9.98 302 9.98 299	3	5 4	.7	2.4	2.I
57	9.43 901	44	9.45 606	47	0.54 394	9.98 295	4	3 2	.7 .8	3.2	2.4
58	9.43 946	45	9.45 654	48	0.54 346	9.98 291 9.98 288	3	2 I	.9	3.0	2.7
60		44	9.45 750	48	0.54 298	9.98 284	4	0			
00	_	-1		0.4			d.	_	D	rep. P	fq.
	L. Cos.	d.	L. Cotg.	ic. d.	L. Tang.	L. SIII.	u.	,	, ,	repo I	``-

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					16°				
, :	L. Sin.	d.		c.d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.44 034 9.44 078	44	9.45 750	47	0.54 250	9.98 284 9.98 281	3	60	
2	9.44 122	44 44	9.45 79 <u>7</u> 9.45 845	48 47	0.54 155	9.98 277	4	59 58	48   47
3	9.44 166 9.44 210	44	9.45 892 9.45 940	48	0.54 108	9.98 273 9.98 270	4	57 56	.1 4.8 4.7
4	9.44 253	43	9.45 987	47	0.54 013	9.98 266	4	55	.2 9.6 9.4
5	9.44 297	44	9.46 035	48 47	0.53 965	9.98 262	4	54	.3 I4.4 I4.I .4 I9.2 I8.8
7 8	9.44 341 9.44 38 <del>5</del>	44	9.46 082 9.46 130	48	0.53 918	9.98 259 9.98 255	4	53 52	.5 24.0 23.5 .6 28.8 28.2
9	9.44 428	43 44	9.46 177	47 47	0.53 823	9.98 251	4	51	.7 33.6 32.9
10	9.44 472	44	9.46 224 9.46 271	47	0.53 776 0.53 729	9.98 248	4	50	8 38.4 37.6 .9 43.2 42.3
12	9.44 559	43 43	9.46 319	48 47	0.53 681	9.98 240	4	49 48	.9   43.2   42.3
13 14	9.44 602 9.44 646	44	9.46 366 9.46 413	47	0.53 634 0.53 587	9.98 <b>237</b> 9.98 <b>233</b>	3	47 46	46   45
15	9.44 689	43	9.46 460	47	0.53 540	9.98 229	4	45	.1 4.6 4.5
16	9.44 733	44	9.46 507	47	0.53 493	9.98 226	3	44	.2 9.2 9.0 .3 13.8 13.5
17	9.44 776 9.44 819	43	9.46 554 9.46 601	47	0.53 446	9.98 222 9.98 218	4	43 42	.4 18.4 18.0
19	9.44 862	43 43	9.46 648	47	0.53 352	9.98 213	3	41	.5 23.0 22.5
20 21	9.44 905 9.44 948	43	9.46 694 9.46 741	47	0.53 306	9.98 211	4	40	.7 32.2 31.5
22	9.44 992	44	9.46 788	47	0.53 212	9.98 204	3	39 38	36.8 36.0
23	9.45 035	43 42	9.46 83 <del>5</del> 9.46 881	47 46	0.53 165	9.98 200 9.98 196	4	37	.9 41.4 40.5
24	9.45 077	43	9.46 928	47	0.53 119	9.98 192	4	36	
26	9.45 163	43 43	9.46 975	47 46	0.53 025	9.98 189	3	34	.1 4.4 4.3
27 28	9.45 206 9.45 249	43	9.47 021	47	0.52 979	9.98 185	4	33 32	.2 8.8 8.6
29	9.45 292	43 42	9.47 114	- 46 46	0.52 886	9.98 177	4	31	.3 13.2 12.9 .4 17.6 17.2
30	9.45 334	43	9.47 160	47	0.52 840	9.98 174	4	30	.5 22.0 21.5
31 32	9.45 377 9.45 419	42	9.47 253	46	0.52 747	9.98 166	4	29 28	.6 26.4 25.8 7 30.8 30.1
33	9.45 462	43 42	9.47 299	46 47	0.52 701	9.98 162 9.98 159	3	27 26	.8 35.2 34.4
34	9.45 504	43	9.47 346	46	0.52 608	9.98 155	4	25	.9 39.6 38.7
35 36	9.45 589	42 43	9.47 438	46 46	0.52 562	9.98 151	4	24	1
37 38	9.45 632 9.45 674	42	9.47 484 9.47 530	46	0.52 516	9.98 147 9.98 144	4	23	42 41
39	9.45 716	42 42	9.47 576	46 46	0.52 424	9.98 140	4	21	.I 4.2 4.I .2 8.4 8.2
40	9.45 758	43	9.47 622	46	0.52 378	9.98 136	4	20	.3 12.6 12.3
4I 42	9.45 801 9.45 843	42	9.47 668	46	0.52 332 0.52 286	9.98 132 9.98 129	3	19	.4 16.8 16.4 .5 21.0 20.5
43	$9.4588\overline{5}$	42 42	0.47 760	46 46	0.52 240	9.98 12 <del>5</del> 9.98 121	4	17 16	.6 25.2 24.6
44 45	9.45 927	42	9.47 806	46	0.52 194	9.98 117	4	15	.7 29.4 28.7 .8 33.6 32.8
46	9.46 011	42 42	9.47 897	45 46	0.52 103	9.98 113	4	14	.9 37.8 36.9
47 43	9.46 05 <u>3</u> 9.46 09 <u>5</u>	42	9·47 943 9·47 989	46	0.52 057	9.98 110	3 4	13	
49	9.46 136	41 42	9.48 035	46	0.51 965	9.98 102	4	11	1413
50	9 46 178	42	9.48 080 9.48 126	46	0.51 920	9.98 098 9.98 094	4	10	.I 0.4 0.3 .2 0.8 0.6
51 52	9.46 262	42	9.48 171	45	0.51 829	9.98 090	4	8	
52 53 54	9.46 303	41 42	9.48 217	46 45	0.51 783	9.98 087	3 4	8 7 6	.4 1.6 1.2
55	9.46 <u>345</u> 9.46 <u>386</u>	41	9.48 262	45	0.51 738	9.98 083	4		.3 I.2 0.9 .4 I.6 I.2 .5 2.0 I.5 .6 2.4 I.8
55 56 57 58 59	9.46 428	42	9.48 353	46	0.51 647	9.98 075	4	5 4 3 2	7 2.8 2.1
57	9.46 469 9.46 511	41 42	9.48 398 9.48 443	45 45	0.51 602	9.98 071 9.98 067	4	3 2	.8 3.2 2.4 .9 3.6 2.7
	9.46 552	41	9.48 489	46	0.51 511	9.98 063	4	1	
60	9.46 594	42	9.48 534	45	0.51 466	9.98 060	3	0	
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.
					73°				

						17°						
ı	1	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		P	rop. Pt	S.
١	0	9.46 594	41	9.48 534	45	0.51 466	9.98 060	4	60			
1	I 2	9.46 63 <del>5</del> 9.46 676	41	9.48 579 9.48 624	45	0.51 421	9.98 056	4	59 58			
ı	3	9 46 717	41 41	9.48 669	45	0.51 331	9.98 048	4	57			44
ı	4	9.46 758	42	9.48 714	45 45	0.51 286	9.98 044	4	56	. I	4.5 9.0	8.8
ı	5	9.46 800	41	9.48 759 9.48 804	45	0.51 241	9.98 040	4	55	-3	13.5 1	3.2
ı	7	9.46 882	41	9.48 849	45	0.51 196	9.98 036	4	54	.4		76
1	7 8	9.46 923	41 41	9.48 894	45	0.51 106	9.98 029	3	53 52	· 5	22.5 2 27.0 2	6.4
ı	9	9.46 964	41	9.48 939	45	0.51 061	9.98 025	4	51	·7	31.5 3	0.8
ı	10	9.47 00 <del>5</del> 9.47 045	40	9.48 984 9.49 029	45	0.51 016	9.98 021	4	50		36.0 3	5.2
ı	12	9.47 045	41	9.49 029	44	0.50 971	9.98 017	4	49 48	.9	40.5 3	9.0
ı	13	9.47 127	41 41	9.49 118	45	0.50 802	9 98 00 1	4	47			
ı	14	9.47 168	41	9.49 163	45 44	0.50 837	9.98 005	4	46			42
ı	15 16	9.47 209	40	9.49 207	45	0.50 793	9.98 001	4	45	.1	4.3	4.2 8.4
1	17	9.47 249 9.47 290	41	9.49 252 9.49 296	44	0.50 748	9·97 997 9·97 993	4	44	.3		2.6
ı	18	9.47 330	40	9.49 341	45	0.50 659	9.97 989	4	43	.4	17.2 1	6.8
	19	9.47 371	41 40	9.49 385	44	0.50615	9.97 986	3	41	·5		1.0
	20	9.47 411	41	9.49 430	44	0.50 570	9.97 982	4	40	.0		5.2 9.4
	2I 22	9.47 452	40	9.49 474 9.49 519	45	0.50 526	9.97 978	4	39 38	·.7	34.4 3	3.6
ı	23	9.47 533	41	9.49 563	44	0.50 437	9.97 979	4	37	.9	38.7 3	7.8
ı	24	9.47 573	40	9.49 607	44	0.50 393	9.97 966	4	36			
ı	25	9.47 613	41	9.49 652	45 44	0.50 348	9.97 962	4	35		41	40
ı	26 27	9.47 654	40	9.49 696	44	0.50 304	9.97 958	4	34	1		4.0
ı	28	9.47 694 9.47 734	40	9.49 740 9.49 784	44	0.50 260	9.97 9 <u>5</u> 4 9.97 9 <u>5</u> 0	4	33 32	.2	8.2	8.0
1	29	9.47 774	40	9.49 828	44	0.50 172	9.97 946	4	31	.3		6.0
I	30	9.47 814	40	9.49 872	44	0.50 128	9.97 942	4	30	.4		0.0
ı	31	9.47 854	40	9.49 916	44	0.50 084	9.97 938	4	29	.6		4.0
П	32	9.47 894 9.47 934	40	9.49 960 9.50 004	44	0.50 040	9.97 934 9.97 930	4	28 27	.7		8.0
ı	34	9.47 974	40	9.50 048	44	0.49 952	9.97 926	4	26	.8		6.0
I	35	9.48 014	40	9.50 092	44	0.49 908	9.97 922	4	25	.91	30.913	0.0
ı	36	9.48 054	40 40	9.50 136	44	0.49 864	9.97 918	4	24			
I	37 38	9.48 094   9.48 133	39	9.50 180	43	0.49 820	9.97 914 9.97 910	4	23		39	5
1	39	9.48 173	40	9.50 267	44	0.49 777	9.97 906	4	21	.1	3.9	0.5
1	40	9.48 213	40	9.50 311	44	0.49 689	9.97 902	4	20	.2	, ,	1.0
ı	4 I	9.48 252	39 40	9.50 355	44	0.49 645	9.97 898	4	19	.4		2.0
ı	42	9.48 292	40	9.50 398	43	0.49 602	9.97 894	4	18	.5	19.5	2.5
	43	9.48 332 9.48 371	39	9.50 442 9.50 485	43	0.49 558	9.97 886	4	17 16	.6		3.0
	45	9.48 411	40	9.50 529	44	0.49 471	9.97 882	4	15	·7		3·5 4.0
	46	9.48 450	39 40	9.50 572	43	0.49 428	9.97 878	4	14	.9		4.5
	47	9.48 490	39	9.50 616	44	0.49 384	9.97 874	4	13			
1	48 49	9.48 529	39	9.50 659	44	0.49 341	9.97 870	4	12		4 1	2
1	50	9.48 607	39	9.50 746	43	0.49 254	9.97 861	5	10	. 1	0.4	3
	51	0.48 647	40 39	9.50 789	43	0.49 211	9.97 857	4	9	.2		0.6
1	52	9.48 686	39	9.50 833 9.50 876	44	0.49 167	9.97 853	4	0	.3	1.2	0.9
	53 54	9.48 725 9.48 764	39	9.50 919	43	0.49 124	9.97 849 9.97 845	4	7 6	.4	1.6	1.5
I	55	0.48.802	39	9.50 962	43	0.49 038	9.97 841	4	5	·4 ·5	2.4	1.5
	55 56	9.48 842 9.48 881	39	9.51 005	43	0.48 995	9.97 837	4	4	·7 .8	2.8	2.I
,	57	9.48 881	39 39	9.51 048	43 44	0 48 952	9.97 833	4	3 2	.8		2.4
ı	58 59	9.48 9 <b>20</b> 9.48 959	39	9.51 092	43	0.48 908	9.97 82 <u>9</u> 9.97 82 <u>5</u>	4	2 I	.91	3.01	/
	$\frac{39}{60}$	9.48 998	39	9.51 178	43	0.48 822	9.97 821	4	0			
-			d.	L. Cotg.	a d		L. Sin.	d.	<del>,</del>	- D	rop. Pts	_
1		L. Cos.	u.	Tr. Corg.	c. u.		Lie Bille	u.		r	rop. Fu	340
I						$72^{\circ}$						

					18°				
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.48 998	39	9.51 178	43	0.48 822	9.97 821		60	
1	9.49 037	39	9.51 221 9.51 264	43	0.48 779	9.97 817 9.97 812	5	59 58	
3	9.49 076	39	9.51 306	42	0.48 694	9.97 808	4	57	43 42
4	9.49 153	38 39	9.51 349	43 43	0.48 651	9.97 804	4	56	.I 4.3 4.2 .2 8.6 8.4
5 6	9.49 192	39	9.51 392	43	0.48 608	9 97 800	4	55	.3 12.9 12.6
	9.49 231 9.49 269	38	9.51 435 9.51 478	43	0.48 565	9.97 796 9.97 792	4	54	.4 17.2 16.8
7 8	9.49 308	39	9.51 520	42	2.48 480	9.97 788	4	53 52	.5 21.5 21.0 .6 25.8 25.2
9	9.49 347	39 33	9.51 563	43	2 48 437	9.97 784	5	51	.7 30.1 29.4
10	9.49 385	39	9.51 606	42	0.48 394	9.97 779	4	50	.8 34.4 33.6
11	9.49 424	38	9.51 648 9.51 691	43	0.48 352	9.97 775 9.97 771	4	49 48	.9   38.7   37.8
13	9.49 500	28 39	9.51 734	43 42	0.48 266	9.97 767	4	47	
14	9 49 539	38	9.51 776	43	0.48 224	9.97 763	4	46	41.
15	9.49 577	38	9.51 819 9.51 861	42	0.48 18 <b>1</b> 0.48 139	9.97 759	5	45	.I 4.I .2 8 2
16	9.49 615	39	9.51 903	42	0.48 097	9·97 754 9·97 750	4	44 43	.3 12 3
17 18	9.49 692	38 38	9.51 946	43	0.48 054	9.97 746	4	42	.4 16.4
19	9.49 730	38	9.51 988	43	0.48 012	9.97 742	4	41	.5 20.5 .6 24.6
20	9.49 768	38	9.52 031	42	0.47 969	9.97 738	4	40	.6 24.6 .7 28.7
2I 22	9.49 806 9.49 844	. 38	9.52 073 9.52 115	42	0.47 92 <u>7</u> 0.47 88 <u>5</u>	9.97 <b>734</b> 9.97 <b>729</b>	5	39 38	.7 28.7 .8 32.8
23	9.49 882	38	9.52 157	42	0.47 843	9.97 725	4	37	.9 36.9
24	9.49 920	38 38	9.52 200	43	0.47 800	9.97 721	4	37 36	
25	9.49 958	38	9.52 242	42	0.47 758	9.97717	4	35	1 39   38
26	9.49 996	38	9.52 284 9.52 326	42	0.47 716	9.97 713 9.97 708	5	34	.1 3.0 3.8
27 28	9.50 072	38	9.52 368	42	0.47 632	9.97 704	4	33 32	7.8 7.6
29	9.50 110	38 38	9.52 410	42	0.47 590	9.97 700	4	31	.3 11.7 11.4 .4 15.6 15.2
80	9.50 148	37	9.52 452	42	0.47 548	9.97 696	4	30	
31	9.50 185	38	9.52 494	42	0.47 506	9.97 691	5	29 28	.6 23.4 22.8
32 33	9.50 223	38	9.52 536 9.52 578	42	0.47 464 0.47 422	9.97 687 9.97 683	4	27	.7 27.3 26.6 .8 31.2 30.4
34	9.50 298	37 38	9.52 620	42 41	0.47 380	9.97 679	4	26	.9 35.1 34.2
35	9.50 336	38	9.52 661	42	0.47 339	9.97 674	5	25	7.00 .01
30	9.50 374	37	9.52 703	42	0.47 297	9.97 670 9.97 666	4	24	
37 38	9.50 411	38	9.52 745 9.52 787	42	0.47 255	9.97 662	4	23	37 36
39	9.50 486	37 37	9.52 829	42	0.47 171	9.97657	5	21	.I 3 7 3.6 .2 7.4 7.2
40	9.50 523	38	9.52 870	42	0.47 130	9.97 653	4	20	.3 11.1 10.8
41	9 50 561	37	9 52 912	4 <sup>I</sup>	0 47 088	9.97 649	4	19	.4 14.8 14 4
42	9 50 598 9 50 635	37	9 52 953 9 52 995	42	0 47 047	9.97 645	5	17	.5 18.5 18 0 .6 22.2 21 6
44	9.50 673	38 37	9.53 037	42 41	0.46 963	9.97 636	4	16	.7 25.9 25.2
45	9.50 710	37	9.53 078	42	0.46 922	9.97 632	1	15	.8 29.6 28.8
46	9.50 747	37	9.53 120	41	0.46 880	9.97 628 9.97 623	5	14	.9   33.3   32.4
47 48	9.50 784	37-	9.53 161 9.53 202	41	0.46 798	9.97 619	4	13	
49	9.50 858	37 38	9.53 244	42	0.46 756	9.97615	4	11	5 4
50	9.50 896	30	9.53 285	4 <sup>1</sup>	0.46 715	9.97 610	5	10	.I 0.t; 3.4
51	9.50 933	37	9.53 327	41	0.46 673	9.97 606	4	9 8	
52 53	9.50 970 9.51 007	37	9.53 368 9.53 409	41	0.46 591	9.97 602 9.97 597	5	7	.3 1.5 1.2 .4 2.0 1.6
54		36	9.53 450	41	0.46 550	9.97 593	4	7 6	5 2.5 2.0
		37	9.53 492	42	0.46 508	9.97 589	4	5	.6 3.6 2.4 .7 3.5 2.8
56	9.51 117	37	9.53 533	41	0.46 467	9.97 584	5	5 4 3 2	.7 3.5 2.8 .8 4.0 3.2
57	9.51 154 9.51 191	37	9.53 574 9.53 615	41	0.46 426	9.97 580 9.97 576	4	2	.9 4.5 3.6
55 56 57 58 59	9.51 227	36	9.53 656	41	0.46 344	9.97 571	5	1	
60	9.51 264	37	9.53 697	41	0.46 303	9.97 567	4	0	
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.
					710				

					19°	100			
,	L. Sin.	d.		c.d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.51 264	37	9.53 697 9.53 738	41	0.46 303	9.97 567	4	60	
I 2	9.51 301 9.51 338	37	9.53 738	41	0.46 262	9.97 563	5	59 58	
3	9.51 374	36	9.53 779 9.53 820	41 41	0.46 180	9.97 554	4	57	41 40
4	9.51 411	36	9.53 861	4I	0.46 139	9.97 550	5	56	.I 4.I 4.0 .2 8.2 8.0
5 6	9.51 447 9.51 484	37	9.53 902 9.53 943	41	0.46 098	9.97 545	4	55	.3 12.3 12.0
7 8	9.51 520	36	9.53 984	41	0 46 016	9.97 541 9.97 536	5	54 53	.4 16.4 16.0 .5 20.5 20.0
	9.51 557	37 36	9.54 023	41 40	0.45 975	9.97 532	4	52	.6 24.6 24.0
9	9.51 593	36	9.54 065	41	0.45 935	9.97 528	5	$\frac{51}{50}$	.7 28.7 28.0 .8 32.8 32.0
11	9.51 666	37 36	9.54 147	41	0.45 853	9.97 523 9.97 519	4		.8 32.8 32.0 .9 36.9 36.0
:2	9.51 702	36	9.54 187	40 41	0.45 813	9.97 515	4 5	49 48	
13	9.51 738 9.51 774	36	9.54 228 9.54 269	41	0.45 772 0.45 731	9.97 510 9.97 506	4	47 46	39
	9.51 811	37	9.54 309	40	0.45 691	9.97 501	5	45	
15 16	9.51 847	36 36	9.54 350	41 40	0.45 650	9.97 497	4	44	.I 3.9 .2 7.8
17	9.51 883	36	9.54 390 9.54 431	41	0.45 610	9.97 492 9.97 488	5 4	43	.3 11.7
19	9.51 955	36 36	9.54 471	40 41	0.45 529	9.97 484	4	41	.5 19.5
20	9.51 991	36	9.54 512	40	0.45 488	9.97 479	5	40	.6 23.4 .7 27.3
2I 22	9.52 027	36	9.54 552	41	0.45 448	9.97 475	- 4 5	39 38	.7 27.3 .8 31.2
23	9.52 003	36	9 · 54 · 593 9 · 54 · 633	40	0.45 367	9.97 470 9.97 466	4	37	.9  35.1
24	9.52 135	36 36	9.54 673	40 41	0.45 327	9.97 461	5 4	37 36	
25 26	9.52 171	36	9.54 714	40	0.45 286	9.97 457	4	35	1 37   36
27	9.52 207	35	9·54 754 9·54 794	40	0.45 246	9.97 453 9.97 448	5	34 33	.1 3.7 3.6
28	9.52 278	36 36	9.54 835	41	0.45 165	9.97 444	4	32	.2 7.4 7.2 .3 11.1 10.8
30	9.52 314	36	9.54 875	40	0.45 125	9.97 439	5	$\frac{31}{30}$	.4 14.8 14.4
31	9.52 350 9.52 385	35	9.54 91 <del>5</del> 9.54 955	40	0.45 085	9.97 435	5	29	.5 18.5 18.0 .6 22.2 21.6
32	9.52 421	36 35	9.54 995	40	0.45 005	9.97 426	4	28	.7 25.9 25.2
33	9.52 456	36	9.55 035	40	0.44 965	9.97 421	5	27 26	.8 29.6 28.8
34	9.52 527	35	9.55 075	40	0.44 885	9.97 417	5	25	.9   33.3   32.4
35 36	9.52 563	35	9.55 155	40	0.44 845	9.97 408	4	24	
37 38	9.52 598 9.52 634	36	9.55 195	40	0.44 805	9.97 403	5	23 22	35 34
39	9.52 669	35	9.55 235 9.55 275	40	0.44 725	9.97 399 9.97 394	5	21	.I 3.5 3.4 .2 7.0 6.8
40	9 52 705	36	9 55 315	40	0.44 685	9.97 390	4	20	.2 7.0 6.8 .3 10.5 10.2
41	9.52 740	35 35	$9.5535\overline{5}$	40	0.44 645	9 97 385	5 4	19 18	.4 14.0 13.6
42	9.52 775 9.52 811	36	9·55 395 9·55 434	39	0.44 605	9.97 381 9.97 376	5	17	.5 17.5 17.0 .6 21.0 20.4
44	9.52 846	35 35	9.55 474	40	0.44 526	9.97 372	5	16	.7 24.5 23.8
45 46	9.52 881	35	9.55 514	40	0.44 486	9.97 367	4	15	
47	9.52 916	35	9·55 554 9·55 593	39	0.44 446	9.97 363 9.97 358	5	14	.9  31.5  30.6
47 48	9.52 986	35 35	9.55 633	40	0.44 367	9.97 353	5	12	
49	9.53 021	35	9.55 673	39	0.44 327	9.97 349	5	10	.1 0.5 0.4
50	9.53 056 9.53 092	36	9.55 712 9.55 752	40	0.44 288	9.97 344 9.97 340	4		.I 0.5 0.4 .2 I.0 0.8
52	9.53 126	34 35	9.55 791	39	0.44 209	9.97 335	5	8	.3 1.5 1.2
52 53 54	9.53 161 9.53 196	35	9.55 791 9.55 831 9.55 870	39	0.44 169	9.97 331 9.97 326	5	7 6	.4 2.0 I.6 .5 2.5 2.0
55	9.53 231	35	9.55 910	40	0.44 090	9.97 322	4		.6 3.0 2.4
56	9.53 266	35 35	9.55 949	39	0.44 051	9.97317	5	5 4	.7 3.5 2.8 .8 4.0 3.2
57	9.53 301 9.53 336	35	9.55 989 9.56 028	39	0.44 011	9.97 312 9.97 308	5	3 2 1	.8 4.0 3.2 .9 4.5 3.6
55 56 57 58 59	9.53 330	34	9.56 067	39	0.43 933	9.97 303	5		
60	9.53 405	35	9.56 107	40	0.43 893	9.97 299	4	0	
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	1,	Prop. Pts.
					70°				

					20°				
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
Ō	9.53 405	35	9.56 107	39	0.43 893	9.97 299	5	60	
I 2	9·53 440 9·53 475	35	9.56 146 9.56 185	39	0.43 854	9.97 294 9.97 289	5	59 58	1.0
3	9.53 509	34 35	9.56 224	39 40	0.43 776	9.97 283	4	57	.I 4.0 3.9
4	9·53 544 9·53 578	34	9.56 264	39	0.43 736	9.97 280	4	56	.2 8.0 7.8
5	9.53 576	35	9.56 342	39	0.43 697 0.43 658	9.97 276 9.97 271	5	55 54	.3  12.0   11.7 .4   16.0   15.6
7 8	9.53 047	34 35	9.56 381	39 39	0.43 619	9.97 266	5	53	
9	9.53 682 9.53 716	34	9.56 420 9.56 459	39	0.43 580 0.43 54 <b>1</b>	9.97 262 9.97 257	5	52 51	.6 24.0 23 4
10	9.53 751	35	9.56 498	39	0.43 502	9.97 252	5	$\frac{51}{50}$	.7   28.0   27.3   .8   32.0   31.2
11	9.53 785	34 34	9.56 537	39 39	0.43 463	9.97 248	5	49 48	.9  36.0   35.1
12 13	9.53 819 9.53 854	35	9.56 576	39	0.43 424	9.97 243 9.97 238	5	48 47	
14	9.53 888	34 34	9.56 654	39 39	0.43 346	9.97 234	4	46	38   37
15	9.53 922	35	9.56 693	39	0.43 307	9.97 229	5	45	.I 3.8 3.7 .2 7.6 7.4
16 17	9·53 957 9·53 991	34	9.56 732 9.56 771	39	0.43 268	9.9 <b>7 224</b> 9.9 <b>7 22</b> 0	4	44 43	.2 7.6 7.4 .3 II.4 II.I
18	9.54 025	34 34	9.56810	39 39	0.43 190	9.97 215	5	42	.4 15.2 14.8
19	9 54 059	34	9.56 849	38	0.43 151	9.97 210	5	41	.5 19.0 18.5 .6 22.8 22.2
20	9.54 093 9.54 127	34	9.56 887 9.56 926	39	0.43 113	9.97 206 9.97 201	5	40	.7 26.6 25.9
22	9.54 161	34 34	9.56 963	39 39	0.43 035	9.97 196	5	39 38	
23	9.54 195 9.54 229	34	9.57 004	38	0.42 996	9.97 192	5	37 36	.9  34.2  33.3
24	9.54 263	34	9.57 042	39	0.42 919	9.97 187	5	35	
25 26	9.54 297	34 34	9.57 120	39 38	0.42 880	9.97 178	4	34	.1 3.5
27 28	9.54 331	34	9.57 158	39	0.42 842	9.97 173	5	33	.1 3.5 .2 7.0
29	9.54 365 9.54 399	34	9.57 197 9.57 235	38	0.42 765	9.97 168 9.97 163	5	32 31	.3 10.5
30	9.54 433	34 33	9.57 274	39 38	0.42 726	9.97 159	5	30	.4 14.0 .5 17.5
31	9.54 466 9.54 500	34	9.57 312 9.57 351	39	0.42 688	9.97 I54 9.97 I49	5	29 28	.6 21.0
32 33	9.54 534	34	9.57 389	38	0.42 611	9.97 145	4	27	.7 24.5 .8 28.0
34	9.54 567	33 34	9.57 428	39	0.42 572	9.97 140	5	26	.9 31.5
35 36	9.54 601 9.54 635	34	9.57 466	38	0.42 534	9.97 135 9.97 130	5	25 24	
37	9.54 668	33	9.57 504 9.57 543	39	0.42 457	9.97 126	4	23	34   33
37 38	9.54 702	34 33	9.57 581	38 38	0.42 419	9.97 121	5	22	
39 <b>40</b>	9·54 735 9·54 769	34	9.57 658	39	0.42 381	9.97 116	5	$\frac{21}{20}$	.2 6.8 6.6
41	9.54 802	33	9.57 696	38	0.42 342	9.97 111	4	10	.3 IO.2 9.9 .4 I3.6 I3.2
42	9.54 836	34 33	9.57 734	38	0.42 266	9.97 102	5	18	.5 17.0 16.5
43	9.54 869 9.54 903	34	9.57 772 9.57 810	38	0.42 228	9.97 097 9.97 092	5	17 16	.6 20.4 19.8 .7 23.8 23.1
45	9.54 936	33	9.57 849	39 38	0.42 151	9.97 087	5	15	.8 27.2 26.4
46	9.54.969	33 34	9 57 887	38	0.42 113	9.97 083	5	14	.9 30.6 29.7
47 48	9.55 ∞3 9.55 o36	33	9.57 925 9.57 963	38	0.42 075	9.97 078 9.97 073	5	13	
49	9.55 069	33 33	9.58 001	38 38	0.41 999	9.97 068	5 5	11	5   4
50	9.55 102	34	9.58 039	38	0.41 961	9.97 063	4	10	.I 0.5 0.4
51 52	9.55 136 9.55 169	33	9.58 115	38	0.41 923	9.97 059	5	9 8	.3 1.5 1.2
53	9.55 202	33 33	9.58 11 <del>5</del> 9.58 153	38 38	0.41 847	9.97 049	5	7	.4 2.0 1.6
54	9.55 235	33	9.58 191	38	0.41 809	9.97 044	5		.4 2.0 1.6 .5 2.5 2.0 .6 3.0 2.4
55 56	9.55 268 9.55 301	33	9.58 229 9.58 267	38	0.41 733	9.97 03 <u>9</u> 9.97 03 <u>5</u>	4	5 4 3 2	7 3.5 2.0
57	9.55 334	33 33	0.58 204	37 38	0.41 696	9.97 030	5	3	.8 4.0 3 2 .9 4.5 3.6
57 58 59	9.55 367 9.55 400	33	9.58 342 9.58 380	38	0.41 658	9.97 02 <del>5</del> 9.97 <b>0</b> 20	5	2 I	.91 4.51 3.0
60	9.55 433	33	9.58 418	38	0.41 582	9.97 015	5	0	
	L. Cos.	d.		c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.
			33-		69°				
					00				

 $\overline{68^{\circ}}$ 

						22°.				
١		L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
	0	9.57 358 9.57 389	31	9.60 641 9.60 677	36	0.39 359	9.96 717	6	60	
	2	9.57 420	31	9.60 714	37 36	0.39 323 0.39 286	9.96 711 9.96 706	5	59 58	37   36
ı	3	9.57 451 9.57 482	31	9.60 750 9.60 786	36	0.39 250 0.39 214	9.96 701 9.96 696	5	57	.1 3.7 3.6
ı	5 6	9.57 514	32	9.60 823	37	0.39 177	9.96 691	5	56	.2 7.4 7.2 .3 11.1 10.8
ı		9.57 545	31	9.60 859 9.60 895	36 36	0.39 141	9.96 686	5	54	.4 14.8 14.4
ı	7 8	9.57 576	31	9.60 931	36 36	0.39 105	9.96 681 9.96 676	5	53 52	.5 18.5 18.0 6 22.2 21.6
ı	9	9.57 638	31	9.60 967	37	0.39 033	9.96 670	5	51	.7 25.9 25.2
ı	10	9.57 669 9.57 700	31	9.61 004 9.61 040	36	0.38 996 0.38 960	9.96 665 9.96 660	5	50 49	.8 29.6 28.8 .9 33.3 32.4
ı	12	9.57 731	31	9.61 076	36 36	0.38 924	9.96 655	5	49 48	7.000,000
1	13 14	9.57 762 9.57 793	31	9.61 148	36 36	0.38 888 0.38 852	9.96 650 9.96 643	5	47 46	1 35
1	15	9.57 824	31	9.61 184	36	0.38816	9.96 640	5	45	1 3.5
1	16 17	9.57 85 <del>3</del> 9.57 885	30	9.61 220	36	0.38 780	9.96 634	5	44 43	.2 7.0 .3 10.5
ı	17	9.57 916	31	9.61 292	36 36	0.38 708	9.96 624	5	42	.4 14.0
	19 20	9.57 947	31	9.61 328	36	0.38 672	9.96 619	5	41 40	.6 21.0
	21	9.57 978 9.58 008	30	9.61 400	36 36	0.38 600	9.96 608	5	39 38	.7 24.5 .8 28.0
	22	9.58 039 9.58 070	31	9.61 436 9.61 472	36	0.38 564 0.38 528	9.96 603	5	38 37	9 31.5
ı	24	9.58 101	31 30	9.61 508	36 36	0.38 492	9.96 593	5	36	
ı	25 26	9.58 131 9.58 162	31	9.61 544 9.61 579	35	0.38 456	9.96 588 9.96 582	6	35	32   31
1	27	9.58 192	30 31	9.61 615	36 36	0.38 385	9.96 577	5	34 33	.I 3.2 3.I .2 6.4 6.2
ł	28 29	9.58 223 9.58 253	30	9.61 651 9.61 687	36	0.38 349	9.96 572	5	32 31	.3 9.6 9.3
	30	9.58 284	31	9.61 722	35	0.38 278	9.96 562	5	30	.4 12.8 12.4
	31	9.58 314	30 31	9.61 758	36 36	0.38 242 0.38 206	9.96 556	6	29 28	.6 19.2 18.6
I	32	9.58 375	30	9.61 794 9.61 830	36	0.38 170	9.96 551	5	27	.7 22.4 21.7 .8 25.6 24.8
	34	9.58 406	30	9.61 865	35 36	0.38 135	9.96 541	6	26	.9 28.8 27.9
-	35 36	9.58 436 9.58 467	31	9.61 901 9.61 936	35	0.38 099	9.96 535 9.96 530	5	25 24	
1	37 38	9.58 497 9.58 527	30	9.61 972	36 36	0.38 028	9.96 523	5	23	30   29
and the	39	9.58 527	30	9.62 008 9.62 043	35	0.37 992	9.96 520 9.96 514	6	22 21	.I 3.0 2.9 .2 6.0 5.8
ı	10	9.58 588	31	9.62 079	36 35	0.37 921	9.96 509	5	20	.3 9.0 8.7
ı	41	9.58 618	30	9.62 114	36	0.37 886	9.96 504 9.96 498	6	19	.4 12.0 11.6
1	43	9.58 678	30	9.62 185	35 36	0.37 813	9.96 493	5 5	17	.6 18.0 17.4
1	44	9.58 709	30	9.62 221	35	0.37 779	9.96 488	5	16	.7 21.0 20.3 .8 24.0 23.2
١	:46	9.58 769	30	9.62 292	36 35	0.37 708	9.96 477	6 5	14	.9 27.0 26.1
ı	47 48	9.58 799 9.58 829	30	9.62 327	35	0.37 673	9.96 472	5	13	
	49	9.58 859	30	9.62 398	36 35	0.37 602	9 96 461	6 5	11	6 5
	50	9.58 889	30	9.62 433 9.62 468	35	0.37 567	9.96 456	5	10	.1 0.6 0.5
	51 52	9.58 919	30	9.62 504	36	0.37 532	9.96 451	6	8	3 1.8 1.5
	53 54	9.58 979 9.59 ∞9	30	9.62 539 9.62 574	35 35	0.37 461	9.96 440 9.96 433	5 5	7 6	.4 2.4 20
	55	9.59 039	30	9.62 609	35	0.37 420	9.96 435	6		1 .6 3.6 3.0
	55 56 57 58 59	9.59 069	30 29	9.62 645	36 35	0.37 355	9.96 424	5	5 4	.7 4.2 3.5 .8 4.8 4.0 .9 5.4 4.5
1	58	9.59 098 9.59 128	30	9.62 680	35	0.37 320	9.96 419	6	3 2	9 5.4 4.5
1	59	9.59 158	30	9.62 750	35 35	0.37 250	9.96 408	5	I	
	60	9.59 188		9.62 785		0.37 215	9.96 403		0	
		L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.
						67°				

					23°				
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.59 188	30 -	9.62 785	35	0.37 215	9.96 403	6	60	
I 2	9.59 218	29	9.62 855	35	0.37 180	9.96 397 9.96 392	5	59 58	1 26 1 25
3	9.59 277	30	9.62 890	35 36	0.37 110	9.96 387	5	57	.1 3.6 3.5
<u>-4</u> 5	9.59 307	29	9.62 926	35	0.37 074	9.96 381	5	56	.2 72 7.0
6	9.59 336 9.59 366	30	9.62 901	35	0.37 039 0.37 <b>0</b> 04	9.96 370	6	55 54	.3 10.8 10.5 .4 14.4 14.0
7 8	9.59 396	30 29	9.63 031	35 35	0.36 969	9.96 365	5	53	.5 18 0 17.5
8 9	9·59 42 <u>5</u> 9·59 455	30	9.63 066	35	0.36 934 0.36 899	9.96 360 9.96 354	6	52 51	6 21.6 21.0
$\frac{10}{10}$	9.59 484	29	9.63 135	34	0.36 865	9.96 349	5	50	.8 28.8 28.0
II	9.59 514	30	9.63 170	35 35	0.36 830	9.96 343	5	49 48	.9 32.4 31.5
12	9·59 543 9·59 573	30	9.63 205	35	0.36 795	9.96 338	5	40	
14	9.59 602	30	9.63 275	35 35	0.36 725	9.96 327	6	46	34
15 16	9.59 632	29	9.63 310	35	0.36 690	9.96 322	6	45	.I 3.4 .2 6.8
	9.59 661 9.59 690	29	$9.6334\overline{5}$ $9.63379$	34	0.36 655	9.96 316	5	44 43	.3 10.2
17	9.59 720	30	9.63 414	35 35	0.36 586	9.96 305	6	42	.4 13.6
19	9.59 749	29	9.63 449	35	0.36 551	9.96 300	6	$\frac{41}{40}$	.5 17.0 .6 20.4
20	9.59 778 9.59 808	30	9.63 484 9.63 519	35	0.36 516	9.96 294 9.96 289	5	39	7 23.8
22	9.59 037	29	9.63 553 9.63 588	34 35	0.36 447	9.96 284	5	39 38	.8 27.2 .9 30.6
23	9.59 866 9.59 895	29	9.63 588	35	0.36 412	9.96 278 9.96 273	5	37 36	.,,,,,,,,
25	9.59 924	29	9.63 657	34	0.36 343	9.96 267	6	35	1 00 1 00
26	9.59 954	30	9.63 692	35 34	0.36 308	9.96 262	5	34	.1 3.0 2.9
27	9.59 983 9.60 012	29	9.63 726 9.63 761	35	0.36 274	9.96 256	5	33	.2 6.0 5.8
29	9.60 041	29	9.63 796	35 34	0.36 204	9.96 245	6	31	.3 9.0 8.7 .4 12.0 11.6
30	9.60 070	29	9.63 830	35	0.36 170	9.96 240	5	80	.5 15.0 14.5
31 32	9.60 099	29	9.63 865 9.63 899	34	0.36 135	9.96 234	5	29 28	.6 18.6 17.4
33	9.60 157	29	9.63 934	35 34	0.36 066	9.96 223	6	27	.7 21.0 20.3 .8 24.0 23.2
34	9.60 186	29	9.63 968	35	0.36 032	9.96 218	6	26	.9 27.0 26.1
35 36	9.60 215	29	9.64 037 9.64 037	34	0.35 997 0.35 963	9.96 212	5	25 24	
37 38	9.60 273	29	9.64 072	35 34	0.35 028	9.96 201	6 5	23	1 28
38	9.60 302 9.60 331	29	9.64 106	34	0.35 894	9.96 196	6	22 21	.1 2.8
40	9.60 359	28	9.64 175	35	0.35 825	9.96 185	5	20	.2 5.6 .3 8.4
41	9.60 388	29	9.64 209	34	0.35 791	9.96 179	5	19	.4 11.2
42	9.60 417	29	9.64 243 9.64 278	35	0.35 757	9.96 174	6	18	.5 14.0 .6 16.8
44	9.60 474	28	9.64 312	34	0.35 688	9.96 162	5	16	7 19.6
45	9.60 503	29	9 64 346	35	0.35 654	9.96 157	6	15	.8 22.4
1 47	9.60 532 9.60 561	29	9.64 381	34	0.35 619	9.96 151	5	14	.9  25.2
48	9.60 589	28	9.64 449	34	0.35 551	9.96 140	5	12	
49	9.60 618	28	9.64 483	34	0.35 517	9.96 135	6	10	.1 0.6 0.5
50 51	9.60 646	29	9.64 517	35	0.35 483 0.35 448	9.96 123	6	9	.1 0.6 0.5 .2 1.2 1.0
52	9.60 704	28	4.64 586	34	0.35 414	9.96 118	5	0	
53 54	9.60 732	29	9.64 620 9.64 654	34	0.35 380 0.35 346	9.96 112	5	7 6	.4 2.4 2.0 .5 3.0 2.5
55	9.60 789	28	9.64 688	34	0.35 312	9.96 101	6		1.6 3.6 3.0
55 56 57 58 59	9.60 789	29	9.64 722	34	0.35 278	9 96 095	5	5 4 3 2	.7 4.2 3.5 .8 4.8 4.0 .9 5.4 4.5
57	9.60 846 9.60 873	29	9.64 756	34	0.35 244	9.96 090	6		.9 5.4 4.5
59	9.60 903	28	9.64 790 9.64 824	34	0.35 176	9.96 079	5	1	
60	9.60 931	20	9.64 858		0.35 142	9.96 073		0	
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.
					66°	•			

					24°					
1	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Pı	rop. Pts.
0	9.60 931	29	9.64 858	34	0.35 142	9.96 073	6	60		
1 2	9.60 960 9.60 988	28	9.64 892	34	0.35 108 0.35 074	9.96 067 9.96 062	5	59 58		
3	9.61 016	28	9.64 960	34 34	0.35 040	9.96 056	6	57 56	. 1	34 33
4	9.61 045	28	9.64 994	34	0.35 006	9.96 050	5	56	.2	3·4 3·3 6.8 6.6
5 6	9.61 073 9.61 101	28	9.65 062	34	0.34 972	9.96 04 <del>5</del> 9.96 039	6	55 54	·3	10.2 9.9   13.6 13.2
7 8	9.61 129	28 29	9.65 096	34 34	0.34 904	9.96 034	5	53	.5	17.0 16.5
9	9.61 158 9.61 186	28	9.65 130	34	0.34 870 0.34 836	9.96 028 9.96 022	6	52 51	.6	
10	9.61 214	28 28	9.65 197	33	0.34 803	9.96 017	5	50	.8	27.2 26.4
11	9.61 242	28	9.65 231	34 34	0.34 769	9.96 011	6	49 48	.9	30.6 29.7
12 13	9.61 270 9.61 298	28	9.65 265 9.65 299	34	0.34 735	9.96 005	5	48 47		
14	9.61 326	28 28	9.65 333	34 33	0.34 667	9.95 994	6	46		29
15 16	9.61 354 9.61 382	28	9.65 366	34	0.34 634	9.95 988	6	45		2 5.8
	9.61 411	29	9.65 400	34	0.34 600	9.95 982 9.95 977	5	44 43		3 8.7
17 18	9.61 438	27 28	9.65 467	33 34	0.34 533	9.95 971	6	42		4 11.6 5 14.5
19 20	9.61 466	28	9.65 501	34	0.34 499	9.95 965	5	$\frac{41}{40}$		6 17.4
21	9.61 522	28 28	9.65 568	33	0.34 432	9.95 954	6			7 20.3 8 23.2
22	9.61 550	28	9.65 602	34 34	0.34 398	9.95 948	6	39 38		.8 23.2 .9 26.1
23 24	9.61 578 9.61 606	28	9.65 636 9.65 669	33	0.34 364 0.34 331	9.95 942 9.95 937	5	37 36		
25	9.61 634	28 28	9.65 703	34	0.34 297	9.95 931	6	35		1 28
26	9.61 662 9.61 689	27	9.65 736	33 34	0.34 264	9.95 925	5	34		1 2.8
27 28	9.61 717	28	9.65 770 9.65 803	33	0.34 230	9.95 920 9.95 914	6	33 32		.2 5.6 .3 8.4
29	9.61 743	28 28	9.65 837	34 33	0.34 163	9.95 908	6	31		.3 8.4
30 31	9.61 773 9.61 800	27	9.65 870 9.65 904	34	0.34 130	9.95 902 9.95 897	5	30 29		.5 14.0
32	9.61 828	28 28	9.65 937	33	0.34 063	9.95 891	6	28		6 16.8
33	9.61 856	27	9.65 971	34	0.34 029	9.95 88 <del>5</del> 9.95 879	6	27 26		.8 22.4
35	9.61 911	28	9.66 038	34	0.33 962	9.95 873	6	25		.9 25.2
36	9.61 939	28 27	9.66 071	33	0.33 929	9.95 868	5 6	24		
37 38	9.61 966	28	9.66 104	34	0.33 896	9.95 862 9.95 856	6	23 22		27
39	9.62 021	27 28	9.66 171	33	0.33 829	9.95 850	6	21		.1 2.7
40	9.62 049	27	9.66 204	34	0.33 796	9.95 844	1	20		.3 8.1
4I 42	9.62 076	28	9.66 238	33	0.33 762	9.95 839 9.95 833	5	18		.4 10.8
43	9.62 131	27 28	9.66 304	33	0.33 696	9.95 827	6	17		.6 16.2
44 45	9.62 159	27	9.66 337 9.66 371	34	0.33 663	9.95 821	6	16		.7 18.9 .8 21.6
46	9.62 214	28	9.66 404	33	0.33 596	9.95 810	5	14		.9 24 3
47 48	9.62 241	27 27	9.66 437	33 33	0.33 563	9.95 804	6	13		
49	9.62 296	28	9.66 503	33	0.33 530	9.95 798 9.95 792	6	11		6   5
50	9.62 323	27	9.66 537	34	0.33 463	9.95 786	6	10	.1	0.6 0.5
51 52	9.62 350 9.62 377	27	9.66 570 9.66 603	33	0.33 430	9.95 780	5	8	.2	1.8 1.5
53 54	9.62 405	28	9.66 636	33	0.33 364	9.95 775 9.95 769	6	7 6	.4	2.4 2.0
54	9.62 432	27	9.66 669	33	0.33 331	9.95 703	6		.5	3 0 2.5
55	9. <b>62</b> 459 9. <b>62</b> 486	27	9.66 702 9.66 735	33	0.33 298	9.95 757 9.95 751	6	5 4	.4 .5 6 .7 .8	3.6 3.0 4.2 3.5
57	9.62 513	27	9.66 768	33 33	0.33 232	9.95 745	6	3 2	.8	4.2 3.5 4.8 4.0 5 4 4.5
55 56 57 58 59 <b>60</b>	9.62 541 9.62 568	27	9.66 801 9.66 834	33	0.33 199	9 95 739 9 95 733	6	1	91	3 41 4.3
60	9.6 2595	27	9.66 867	33	0.33 133	9 95 728	5	0		
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.		d.	, T	P	rop. Pts.
					65°					

					25°				
1	L. Sin.	d.	L. Tang.	c. d.		L. Cos.	d.	1	Prop. Pts.
0	$9.6259\overline{5}$ $9.62622$	27	9.66 867 9.66 900	33	0.33 133	9.95 728	6	60	
2	9.62 649	27	9.66 933	33	0.33 100	9.95 722 9.95 716	6	59 58	
3	9.62 676	27	9.66 966	33	0.33 034	9.95 710	6	57	.1 3.3 3.2
4.	9.62 703	27	9.66 999	33	0.33 001	9.95 704	6	56	.I 3.3 3.2 .2 6.6 6.4
5	9.62 757	27	9.67 032 9.67 06 <del>5</del>	33	0.32 968	9.95 698	6	55	.3 9.9 9.6
7 8	9.62 784	27	9.67 098	33	0.32 902	9.95 686	6	54 53	.4 13.2 12.8 .5 16.5 16.0
9	9.62 811	27	9.67 131 9.67 163	32	0.32 869	9.95 680	6	52	.6 19.8 19.2
10	9.62 865	27	9.67 196	33	0.32 804	9.95 674	6	$\frac{51}{50}$	.7 23.1 22.4 .8 26.4 25.6
11	9.62 892	27 26	9.67 229	33	0.32 771	9.95 663	5		.9 29.7 28.8
12	9.62 918	27	9.67 262 9.67 293	33	0.32 738	9.95 657	6	49 48	
14	9.62 972	27	9.67 327	32	0.32 705	9.95 651 9.95 64 <del>5</del>	6	47 46	27
15	9.62 999	27	9.67 360	33	0.32 640	9.95 639	6	45	.1 2.7
16	9.63 026	26	9.67 393	33	0.32 607	9.95 633	6	44	.2 5.4 3 8.1
17	9.63 052	27	9.67 426 9.67 458	32	0.32 574	9.95 627 9.95 621	6	43	3 8.1 .4 10.8
19	9.63 106	27	9.67 491	33	0.32 509	9.95 613	6	42 41	.5 13.5
20	9.63 133	26	9.67 524	33	0.32 476	9.95 609	6	40	.6 16.2 .7 18.9
21 22	9.63 159 9.63 186	27	9.67 556 9.67 589	33	0.32 444	9.95 603 9.95 <b>5</b> 97	6	39 38	.8 21.6
23	9.63 213	27	9.67 622	33	0.32 378	9.95 591	6	37	.9 24.3
24	9.63 239	27	9.67 654	33	0.32 346	9.95 585	6	36	
25 26	9.63 266 9.63 292	26	9.67 687 9.67 719	32	0.32 313	9.95 579 9.95 573	6	35	26
27 28	9.63 319	27 26	9.67 752	33	0.32 248	9.95 567	6	34	.1 2.6
28	9.63 345	27	9.67 785	33 32	0.32 215	9.95 561	6	32	.2 5.2
30	9.63 372	26	9.67 850	33	0.32 183	9 95 555	6	$\frac{31}{30}$	.4 10.4
31	9.63 425	27 26	9.67 882	32	0.32 118	9 · 95 · 549 9 · 95 · 543	6		.5 13.0 .6 15.6
32	9.63 451	27	9.67 915	33	0.32 085	9.95 537	6	29 28	.7 18.2
33 34	9.63 478 9.63 504	26	9.67 947 9.67 980	33	0.32 053	9.95 531	6	27 26	.8 20.8
	9.63 531	27 26	9.68 012	32	0.31 988	9.95 519	6	25	.9 23.4
35 36	9.63 557	26	9.68 044	32 33	0.31 956	9.95 513	6	24	
37 38	9.63 583 9.63 610	27	9.68 077	32	0.31 923	9.95 507	7	23	7
39	9.63 636	26	9.68 142	33 32	0.31 858	9.95 494	6	21	.I 0.7 .2 I.4
40	9.63 662	27	9.68 174	32	0.31 826	9.95 488	6	20	.3 2.1
4I 42	9.63 689	26	9.68 206 9.68 239	33	0.31 794	9.95 482	6	19 18	.4 2.8
43	9.63 741	26 26	9.68 271	32	0.31 729	9.95 476	6	17	.5 3.5 .6 4.2
44	9.63 767	27	9.68 303	32 33	0.31 697	9.95 464	6	16	.7 4.9 .8 5.6
45 46	9.63 794 9.63 820	26	9.68 336 9.68 368	32	0.31 664 0.31 632	9.95 458 9.95 452	6	15 14	.7 4.9 .8 5.6 .9 6 3
47 48	9.63 846	26 26	9.68 400	32	0.31 600	9.95 446	6	13	.91 0 3
48	9.63 872	26	9.68 432	32 33	0.31 568	9.95 440	6	12	
<u>49</u> 50	9.63 898	26	9.68 465	32	0.31 535	9.95 434	7	10	.1 0.6 0.5
51	9.63 950	26 26	9.68 529	32	0.31 471	9.95 421	6	9	.2 1.2 1.0
51 52	9.63 976	26	9.68 561	32	0.31 439	9.95 415	6	0	.3 1.8 1.5
53 54	9.64 002 9.64 028	26	9.68 593 9.68 626	33	0.31 407	9.95 409	6	7	.3 1.8 1.5 .4 2.4 2.0 .5 3.0 2.5 .6 3.6 3.0
55	9.64 054	26 26	9.68 658	32	0.31 342	9.95 397	6		3.0 2.5 3.6 3.0 7 4.2 3.5 .8 4.8 4.0 .9 5.4 4.5
56	9.64 080	26	9.68 690	32 32	0.31 310	9.95 391	6	5 4 3 2	.7 4.2 3.5 .8 4.8 4.0
56 57 58 <b>5</b> 9	9.64 106 9.64 132	26	9.68 722 9.68 754	32	0.31 278 0.31 246	9.95 384 9.95 378	6	3 2	9 5.4 4.5
	9.64 158	26	9.68 786	32 32	0.31 214	9.95 372	6	1	
60	9.64 184		9.68 818		0.31 182	9.95 366		0	
	L. Cos.	d.	L. Cotg.	c. d.		L. Sin.	d.	,	Prop. Pts.
					610				

4   184   26				26°										
4 210         26         9.68 850         32         0.31 150         9.95 360         6         59           4 236         26         9.68 882         32         0.31 118         9.95 354         6         58           4 236         26         9.68 946         32         0.31 054         9.95 348         7         56         13 .2         3.1           4 339         26         9.68 978         32         0.31 054         9.95 335         6         55         3 .9         9         9.95 329         6         55         3 .9         9         9         9.95 329         6         55         3 .9         9         9         9.95 323         6         55         3 .9         9         9         9.95 323         6         55         3 .9         9         9         9.95 323         6         55         3 .5         16         12.8         12.2				L. Cos.	L. Corg.	c. a.		d.	L. Sin.	,				
44 216         26         9.68 882         32         0.31 130         9.95 354         6         58         32         31 32         33 118         9.95 348         6         58         7         57         1         3.2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	59	6	5	9.95 366		32		26	9.64 184	0				
44 288	- 2		2	9.95 300		- 1			9.64 210 9.64 236	1 2				
44 288   25   9.68 946   32   0.31 054   9.95 341   6   56   1.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	57					- 1			9.64 262	3				
44 339							9.68 946		9.64 288	4				
44 339	55								9.64 313	5				
44 391         26         9.69 074         32         0.30 926         9.95 317         7         52         6         19.2         18.6         18.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         19.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         18.2         <	54	6				32			9.64 339 9.64 365					
44 477 (4 442)         25 (9.69 138)         32 (0.30 864)         9.95 310 (6 6 7)         6 (50 8)         25.6 (24.8)         24.468         26 (9.69 170)         32 (0.30 830)         9.95 298 (6 48)         6 (48)         48 (25.6)         24.519         25 (9.69 202)         32 (9.69 266)         32 (9.69 367)         32 (9.69 266)         32 (9.69 367)         32 (9.69 367)         32 (9.69 367)         32 (9.69 367)         32 (9.69 367)         32 (9.69 367)         32 (9.69 367)         32 (9.69 367)         32 (9.69 367)         32 (9.69 367)         32 (9.69 367)         32 (9.69 367)         33 (9.99 5 242)         34 (9.69 367)         32 (9.69 367)         33 (9.99 5 242)         33 (9.99 5 242)         33 (9.99 5 242)         33 (9.99 5 242)         33 (9.99 5 242)         33 (9.99 5 242)         34 (9.69 367)         34 (9.69 367)         34 (9.69 367)	52				0.30 926				9.64 391	7 8				
44 468         26         9.69 170         32         0.30 830         9.95 298         6         49         .9   28.8   27:6           44 519         26         9.69 202         32         0.30 708         9.95 298         6         48           45 515         26         9.69 234         32         0.30 706         9.95 286         7         46         47           45 571         26         9.69 329         32         0.30 671         9.95 267         6         44         47         46         46         47         46         48         42         45         5.2         5.2         6         44         47         46         48         42         44         44         44         46         47         46         42         44         44         44         44         46         47         46         43         47         48         44         44         46         43         43         78         44         44         46         43         43         78         44         44         46         43         43         43         78         44         43         43         43         78         44         44         43	51		2	9.95 310		- 1			9.64 417	9				
44 494         25         9.69 202         32         0.30 768         9.95 202         6         48         47         46         47         47         46         48         47         44         47         46         48         47         46         48         47         47         46         48         47		6	ţ	9.95 304				26	9.64 442	10				
44 519	49								9.64 494	11 12				
44 545       26       9.09 260       32       0.30 734       9.95 279       6       46       45       2.6       46 506       2.6       45 506       26       9.69 329       32       0.30 702       9.95 273       6       445       .1       2.6       2.5       2.6       2.6       45 50       .2       5.2       2.6       2.6       45 70       .2       5.2       3.2       7.8       .3       7.8       .4       2.6       44 673       2.6       9.69 425       32       0.30 607       9.95 248       6       41       .4       10.4       .4       10.4       .4       10.4       .4       .4       .4       10.4       .5       13.0       .0       .9.95 248       6       41       .5       13.0       .0       .9.95 242       6       41       .5       13.0       .0       .9.95 242       6       41       .6       15.6       .7       18.2       .9       .9.95 242       6       .9       .9.95 236       7       .38       .9       .9.95 242       6       .39       .8       20.8       .8       20.8       .9.95 223       6       .37       .3       .8       20.8       .9       .9.95 223       6       <	47		5	9 95 286	0.30 766		9.69 234		9.64 519	13				
24         596         25         9.69 329         31         0.30 671         9.95 267         6         44         32         5.2           24         25         9.69 361         32         0.30 671         9.95 261         6         43         31         0.30 679         9.95 261         6         44         32         7.8         32         7.8         32         0.30 677         9.95 254         6         42         42         44         42         44         42         44         42         44         42         44         42         44         42         44         42         44         42         44         42         44         42         44         42         44         42         44         42         44         42         44         42         44         42         44         42         44         44         44         9.95 248         6         41         51         13.0         6         42         42         44         44         44         9.96 96         48         31         0.30 575         9.95 242         6         41         40         .96         52         32         0.30 448         9.95 229         6			2	9.95 279					9.64 545	14				
34 622       30       9.69 361       32       0.30 639       9.95 261       6       43       .3       7.8         44 647       25       9.69 393       32       0.30 607       9.95 254       6       42       .4       10.4       .5       13.0         44 673       25       9.69 488       32       0.30 575       9.95 242       6       41       .5       13.0         44 724       25       9.69 488       32       0.30 512       9.95 236       7       39       .8       20.8         44 775       26       9.69 520       32       0.30 448       9.95 223       6       37       39       .8       20.8         44 850       25       9.69 552       32       0.30 448       9.95 223       6       37       36       9       23.4         44 851       26       9.69 584       31       0.30 385       9.95 211       6       36       37       36         44 857       25       9.69 615       32       0.30 385       9.95 204       6       34       34       1       2.5       35         44 897       25       9.69 677       32       0.30 358       9.95 102       32 <td></td> <td>6</td> <td></td> <td></td> <td></td> <td>31</td> <td></td> <td>25</td> <td>9.64 571</td> <td>15 16</td>		6				31		25	9.64 571	15 16				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						-			9.64 622					
44 673       25       9.69 425       32       0.30 575       9.95 248       6       41       3 13.6         44 724       26       9.69 488       32       0.30 543       9.95 242       6       39       7 18.2         44 749       26       9.69 520       32       0.30 543       9.95 229       7 38       20.8         44 775       26       9.69 552       32       0.30 448       9.95 223       6       37         44 850       25       9.69 584       31       0.30 448       9.95 221       6       36         44 851       26       9.69 647       32       0.30 385       9.95 204       6       36         44 877-       26       9.69 647       32       0.30 323       9.95 102       33       25         44 877-       25       9.69 679       32       0.30 321       9.95 102       33       .2       25         44 902       25       9.69 702       32       0.30 290       9.95 102       32       .3       .2       5.0         44 978       25       9.69 774       32       0.30 296       9.95 179       6       31       .3       7.5         49 953       25			1	9.95 254	0.30 607		9.69 393		9.64 647	17 18				
24 090 24 724       25 9.69 488       31 0.30 512 9.95 236 6 7 38 25 9.69 522 9 0.30 480 9.95 229 6 38 29 23.4       6 9.69 552 32 9.69 552 32 9.69 582 32 9.69 582 32 9.69 582 32 9.69 582 32 9.69 582 32 9.69 582 32 9.69 582 32 9.69 582 32 9.69 582 32 9.69 615 32 9.69 647 32 9.69 679 32 9.69 679 32 9.69 679 32 9.69 679 32 9.69 679 32 9.69 679 32 9.69 679 32 9.69 679 32 9.69 679 32 9.69 772 36 9.69 774 32 9.69 679 32 9.69 772 36 9.69 774 32 9.69 679 32 9.69 772 36 9.69 774 32 9.69 679 32 9.69 772 36 9.69 774 32 9.69 679 32 9.69 774 32 9.69 679 32 9.69 774 32 9.69 679 32 9.69 774 32 9.69 679 32 9.69 774 32 9.69 679 32 9.69 774 32 9.69 679 31 9.69 679 32 9.69 670 32 9.69 670 32 9.69 670 32 9.69 670 32 9.69 670 32 9.69 670 32 9.69 670									9.64 673	19				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		6				31	9.69 457	26	9.64 698	20 21				
14 4 800	38						9.69 520		9.64 749	22				
14 826	37		3	9.95 223	0.30 448		9.69 552		9.64 775	23				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	36					-			9.64 800	24				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		7				32			9.64 851	25 26				
14 902   25   9.69 710   32   0.30 290   9.95 192   7   31   32   32   32   34   37   32   32   32   32   32   32   32	33								9.64 877.					
14 953   25   9.69 774   32   0.30 226   9.95 179   6   30   12.5   15.00   26   9.69 805   32   0.30 163   9.95 167   6   28   77   17.5   17	32					1 -			9.64 902	27 28				
04 978   55   9.69 805   32   0.30 195   9.95 173   6   29   .6   15.0   05 003   25   9.69 837   32   0.30 163   9.95 167   6   28   .7   17.5   05 029   26   9.69 868   31   0.30 132   9.95 160   7   27   8   20 0			_					-	9.64 927	29				
05 029 26 9.69 868 31 0.30 132 9.95 160 7 27 17.5 05 029 26 9.69 868 31 0.30 132 9.95 160 7 27 8 20 0					0.30 220	31		25	9.64 953	<b>30</b> 31				
55 029 25 9.69 868 32 0.30 132 9.95 160 7 27 8 20.0	28					-	9.69 837		9.65 003	32				
		6			0.30 132	32		25	9.65 029	33				
25   32   37   37   37   37   37   37   37		6				32		25	9.65 054	34				
$\frac{1}{100}$									9.65 104	35 36				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	23		3	9.95 135	0.30 005		9.69 995		9.65 130	37 38				
55 155 25 9.70 020 32 0.29 974 9.95 129 7 22 1 2.4						1 -		1	9.65 155 9.65 180	38				
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		6	_			1		25	9.65 205	39 40				
$0.5 \times 230$ $0.70 \times 121$ $0.29 \times 121$ $0.29 \times 121$ $0.60 \times 121$	10								9.65 230	41				
05 255   26   9.70 152   32   0.29 848   9.95 103   7   18   .5   12.0			3	9.95 103					9.65 255	42				
55 281 25 9.70 184 32 0.29 816 9.95 097 7 17 .6 14.4 65 306 25 9.70 215 31 0.29 785 9.95 090 7 16 .7 16.8								25	9.65 281 9.65 306	43 44				
0.70 247 0.20 753 0.05 084 15 .8 19.2									9.65 331	45				
$65,356 \mid {}^{25}\mid 9.70,278 \mid {}^{31}\mid 0.29,722 \mid 9.95,078 \mid {}^{6}\mid 14 \mid {}^{6}\mid .9 \mid 21.6$			8	9.95 078	0.29 722	1		1	9.65 356	46				
05 301   0.70 309   0.29 091   9.95 071   2 13								1	9.65 381	47 48				
$65.431$ $^{25}$ $0.70.372$ $^{31}$ $0.29.628$ $0.05.050$ $^{6}$ $11$ $1.7.1.6$		6				1			9.65 431	49				
$\frac{65}{456}$ $\frac{25}{9.70404}$ $\frac{32}{0.29596}$ $\frac{9.95}{9.95052}$ $\frac{7}{10}$ .1 0.7 0.									9.65 456	50				
$65481 \mid {}^{25} \mid 9.7043\overline{5} \mid {}^{31} \mid 0.29565 \mid 9.95046 \mid {}^{6} \mid 9 \mid .2 \mid 1.4 \mid 1.$			6	9.95 046	0.29 565		9.70 435		9.65 481	51				
65 521   25   0 70 408   32   0 20 502   0 05 022   0 7   4   2 8   2	8	6							9.65 506	52				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	6						9.70 529		9.65 556	53 54				
	5		0	9.95 020	0.29 440	1	9.70 560		9.65 580	55				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4		4	9.95 014	0.29 408		9.70 592		9 65 605	55 56 57 58				
65 605   25   9.70 592   32   0.29 408   9.95 014   0   4   7   4.9   4.65 630   25   9.70 623   31   0.29 377   9.95 007   7   3   .8   5.6   4.65 655   25   9.70 654   31   0.29 346   9.95 001   6   2   .9   6.3   5.		6				31		25	9 65 630	57				
65 680 25 9.70 685 31 0.29 315 9 94 995 1	3	6							9.65 680	59				
65 705 25 9.70 717 32 0.29 283 9.94 988 <b>7 0</b>	1							1 25		40				
	1	7		9.94 988	0.29 283	3-	9.70 717		9.65 705	60				
63°	0	7	8	-			-		9.65 705 L. Cos.	60				

27°    L. Sin.   d.   L. Tang.   e. d.   L. Cotg.   L. Cos.   d.   Prop. Pts.   Pro										
,		d.	L. Tang.	c. d.			d.		Prop. Pts.	
0	9.65 70 <del>5</del> 9.65 729	24	9.70 717 9.70 748	31	0.29 283 0.29 252	9.94 988	6	60		
2	9.65 754	25	9.70 779	31	0.29 252	9.94 982 9.94 975	7	59 58	1 00 1 00	
3	9.65 779	25 25	9.70 779	31	0.29 190	9.94 969	6 7	57 56	.I 3.2 3.1	
4	9.65 804	24	9.70 841	32	0.29 159	9.94 962	6		.2 6.4 6.2	
5 6	9.65 853	25 25	9.70 904	31	0.29 096	9.94 956 9.94 949	7	55 54	.3 9.6 9.3 .4 12.8 12.4	
7 8	9.65 878	24	9.70 935	31	0.29 065	9.94 943	7	53	.5 16.0 15.5	
9	9.65 902	25	9.70 966 9.70 997	31	0.29 034	9.94 936 9.94 930	6	52 51		
10	9.65 952	25 24	9.71 028	31	0.28 972	9.94 923	7	50	.8 25.6 24.8	
11	9.65 976 9.66 001	25	9.71 059	31	0.28 941	9.94 917	6	49 48	.9 28.8 27.9	
13	9.66 025	24	9.71 090 9.71 121	31	0.28 879	9.94 911	7	48		
14	9.66 050	25 25	9.71 153	32 31	0.28 847	9.94 898	6	46	30	
15 16	9.66 075	24	9.71 184	31	0.28 816	9.94 891	6	45	.1 3.0 .2 6.0	
17	9.66 099	25	9.71 215	31	0.28 754	9.94 88 <del>5</del> 9.94 878	7	44 43	.3 9.0	
18	9.66 148	24 25	9.71 277	31	0.28 723	9.94 871	7 6	42	.4 12.0	
19 20	9.66 173	24	9.71 308	31	0.28 661	9.94 865	7	41	.5 15.0 .6 18.0	
21	9.66 197	24	9.71 339 9.71 370	31	0.28 630	9.94 858 9.94 852	6	<b>40</b>	.7 21.0	
22	9.66 246	25	9.71 401	30	0.28 500	9.94 845	7 6	39 38	.8 24.0 .9 27.0	
23 24	9.66 270	25	9.71 431 9.71 462	31	o 28 569 o.28 538	9.94 839 9.94 832	7	37 36		
25	9.66 319	24	9.71 493	31	0.28 507	9.94 826	6	35	1 00 1 01	
26	9.66 343	24 25	9.71 524	31	0.28 476	9.94 819	7	34	.1 2.5 2.4	
27	9.66 368 9.66 392	24	9.71 555 9.71 586	31	0.28 445	9.94 813 9.94 806	7	33 32	.2 5.0 4.8	
29	9.66 416	24 25	9.71 617	31	0.28 383	9.94 799	7	31	.3 7.5 7.2 .4 10.0 9.6	
30	9.66 441	24	9.71 648	31	0.28 352 0.28 32I	9.94 793	7	30		
31 32	9.66 465	24	9.71 679	30	0.28 321	9.94 786 9.94 780	6	29 28	.5 12.5 12.0 .6 15.0 14.4 .7 17.5 16.8	
33	9.66 513	24	9.71 740	31	0.28 260	9.94 773	7	27	.7 17.5 16.8 .8 20.0 19.2	
34	9.66 537	25	9.71 771	31	0.28 229	9.94 767	7	26	.9 22.5 21.6	
35 36	9.66 562 9.66 586	24	9.71 802 9.71 833	31	0.28 198	9.94 760 9.94 753	7	25 24		
37	9.66 610	24	9.71 863	30	0.28 137	9.94 747	6	23	1 23	
37 38	9.66 634 9.66 658	24	9.71 894	31	0.28 106	9.94 740	6	22	.1 2.3	
39 <b>40</b>	9.66 682	24	9.71 925	30	0.28 045	9·94 734 9·94 727	7	20	.2 4.6	
41	9.66 706	24	9.71 986	31	0.28 014	9.94 720	7 6	19	.4 9.2	
42	9.66 731 9.66 755	24	9.72 017 9.72 048	31	0.27 983	9.94 714 9.94 707	7	18	.5 II.5 .6 I3.8	
43	9.66 779	24	9.72 078	30	0.27 922	9.94 700	7 6	16	.7 16.1	
45	9.66 803	24	9.72 109	31	0 27 891	9.94 694	7	15	.7 16.1 .8 18.4	
46	9.66 827	24	9.72 140	30	0.27 860	9.94 687 9.94 680	7	14	.9 20.7	
47 48	9.66 873	• 24 24	9.72 201	31	0.27 799	9.94 674	6	12		
49	9.66 899	23	9.72 231	30	0.27 769	9.94 667	7	11	.1 0.7 0.6	
50	9.66 922	24	9.72 262 9.72 293	31	0.27 738	9.94 660 9.94 654	6	10	.2 1.4 1.2	
52	9.66 970	24	9.72 323	30	0.27 677	9.94 647	7	8	.3 2.1 1.8	
53 54	9.66 994 9.67 018	24	9.72 354 9.72 384	30	0.27 646	9.94 640 9.94 634	6	7 6	.4 2.8 2.4	
55	9.67 042	24	9.72 415	31	0.27 585	9.94 627	7		.4 2.8 2.4 .5 3.5 3.0 .6 4.2 3.6 .7 4.9 4.2 .8 5.6 4.8 .9 6.3 5.4	
56	9.67 066	24	9.72 445	30	0.27 555	9.94 620	7 6	4	.7 4.9 4.2 .8 5.6 4.8	
57	9 67 090 9 67 113	23	9.72 476 9.72 506	30	0.27 524	9.94 614	7	5 4 3 2	.9 6.3 5.4	
55 56 57 58 59	9.67 137	24	9.72 537	31	0.27 463	9.94 600	7	1		
60	9.67 161	24	9.72 567	30	0.27 433	9.94 593	7	0		
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	1	Prop. Pts.	
					62°					

28°    L. Sin.   d.   L. Tang.   c. d.   L. Cotg.   L. Cos.   d.   Prop. Pts.     O 0 0 72 167   0 0 27 422   0 04 102   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0											
,	L. Sin.	d.		c.d.	L. Cotg.	L. Cos.	d.		Pr	op. Pt	s.
7 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	9.67 161 9.67 185 9.67 282 9.67 256 9.67 280 9.67 303 9.67 373 9.67 350 9.67 374 9.67 398 9.67 442 9.67 468 9.67 492 9.67 515 9.67 539 9.67 562 9.67 562	24 23 24 24 24 23 24 23 24 23 24 23 24 23 24 23 24 23 24 23 24 23 24 23 24 23 24 24 24 23 24 24 24 24 24 24 24 24 24 24 24 24 24	L. Tang. 9.72 567 9.72 598 9.72 628 9.72 689 9.72 689 9.72 750 9.72 780 9.72 781 9.72 841 9.72 842 9.72 902 9.72 902 9.72 903 9.73 054 9.73 054 9.73 114 9.73 114	31 30 31 30 31 30 31 30 31 30 31 30 31 30 31 30 31 30 31 30 31 30 31 30 31 30 31 30 31 30 31 30 31 30 31 30 30 31 30 30 30 30 30 30 30 30 30 30 30 30 30	0.27 433 0.27 402 0.27 372 0.27 341 0.27 280 0.27 250 0.27 250 0.27 189 0.27 189 0.27 189 0.27 068 0.27 068 0.27 069 0.26 977 0.26 946 0.26 886 0.26 886	9.94 593 9.94 587 9.94 580 9.94 567 9.94 567 9.94 563 9.94 546 9.94 546 9.94 546 9.94 546 9.94 546 9.94 546 9.94 546 9.94 547 9.94 548 9.94 548 9.94 548 9.94 548 9.94 499 9.94 499 9.94 472 9.94 472 9.94 472 9.94 475	6 7 7 6 7 7 6 7 7 7 6 7 7 7 6 7 7 7 6 7 7 7 7 6 7 7 7 7 6 7	60 59 58 57 56 55 55 54 48 47 46 44 43 44 44	.1 .2 .3 .4 .5 .6 .7 .8	31 3.1 6.2 9.3 12.4 15.5 188.6 121.7 224.8 227 9 29 20 21 22 23 3.1 3.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4	30 3.0 6.0 9.0 5.0 5.0 24.0 27.0
20 21 22 23 24 25 26 27 28 29	9.67 633 9.67 656 9.67 680 9.67 703 9.67 726 9.67 730 9.67 773 9.67 796 9.67 843 9.67 843	24 23 24 23 24 23 24 23 24 23 24 23 24	9.73 175 9.73 205 9.73 235 9.73 265 9.73 295 9.73 326 9.73 356 9.73 386 9.73 416 9.73 446	31 30 30 30 30 31 30 30 30 30 30	0.26 825 0.26 795 0.26 795 0.26 705 0.26 705 0.26 674 0.26 644 0.26 684 0.26 584 0.26 554	9.94 458 9.94 451 9.94 445 9.94 431 9.94 424 9.94 417 9.94 410 9.94 404 9.94 397	7 7 6 7 7 7 7 6 7	40 39 38 37 36 35 34 33 32 31	.1 .2 .3 .4	7 20. 8 23. 9 26 24 2.4 4.8 7.2	4 3 2 1 23 2.3 4.6 9.2
31 32 33 34 35 36 37 38 39	9.67 890 9.67 890 9.67 936 9.67 959 9.67 982 9.68 006 9.68 029 9.68 052 9.68 075 9.68 098	24 23 23 23 24 23 23 23 23 23	9.73 476 9.73 507 9.73 537 9.73 567 9.73 567 9.73 627 9.73 657 9.73 687 9.73 717 9.73 747	31 30 30 30 30 30 30 30	0.26 493 0.26 463 0.26 403 0.26 403 0.26 373 0.26 343 0.26 383 0.26 283 0.26 253	9.94 390 9.94 383 9.94 376 9.94 369 9.94 362 9.94 349 9.94 349 9.94 328 9.94 328	7 7 7 7 7 6 7 7	29 28 27 26 25 24 23 22 21 20	.6 .7 .8 .9	16.8 19.2 21.6	. 2
41 42 43 44 45 46 47 48 49	9 68 121 9 68 144 9 68 167 9 68 190 9 68 237 9 68 260 9 68 283 9 68 305	23 23 23 23 23 24 23 22 23 22 23	9.73 77 9.73 807 9.73 837 9.73 867 9.73 897 9.73 927 9.73 957 9.73 987 9.74 017 9.74 047	30 30 30 30 30 30 30 30 30	0.26 193 0.26 163 0.26 133 0.26 103 0.26 073 0.26 043 0.26 013 0.25 983 0.25 953	9.94 321 9.94 307 9.94 300 9.94 293 9.94 286 9.94 273 9.94 266 9.94 259	7 7 7 7 7 7 6 7	19 18 17 16 15 14 13 12		4 8 5 11 6 13 7 15 8 17 9 19	.8 .0 .2 .4 .6 .8
50 51 52 53 54 55 56 57 58 59 <b>60</b>	9.68 328 9.68 351 9.68 374 9.68 397 9.68 443 9.68 446 9.68 469 9.68 512 9.68 534	23 23 23 23 23 23 23 23 23 23 22 23	9.74 077 9.74 107 9.74 137 9.74 166 9.74 196 9.74 226 9.74 256 9.74 286 9.74 316 9.74 345	30 30 30 29 30 30 30 30 30	0.25 923 0.25 893 0.25 863 0.25 804 0.25 804 0.25 774 0.25 714 0.25 684 0.25 655	9.94 252 9.94 245 9.94 238 9.94 231 9.94 224 9.94 217 9.94 210 9.94 203 9.94 196 9.94 189	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	10 9 8 7 6 5 4 3 2 1	.1 .2 .3 .4 .5 .6 .7 .8 .9	0.7 1.4 2.1 2.8 3.5 4.2 4.9 5.6 6.3	0.6 1.2 1.8 2.4 3.0 3.6 4.2 4.8 5.4
60	9.68 557 <b>L. Cos.</b>	d.	9.74 375 L. Cotg.		0.25 625 L. Tang.	9.94 182 L. Sin.	đ.	,	Pı	rop. I	rts.

	29°    L. Sin.   d.   L. Tang.   c. d.   L. Cotg.   L. Cos.   d.   Prop. Pts.     9.68 557   23   9.74 375   30   0.25 625   9.94 182   60											
		d.		c.d.			d.		Prop. Pts.			
0	9.68 557 9.68 580	23	9·74 37 <u>5</u> 9·74 40 <u>5</u>	30	0.25 625	9.94 182 9.94 17 <del>5</del>	7	60				
2	9 58 603	23	9.74 435	30	0.25 565	9.94 168	7	59 58	1 30			
3 4	9.68 625 9.68 648	23	9.74 465 9.74 494	29	0.25 535 0.25 506	9.94 161 9.94 154	7	57 56	.1 3.0			
5 6	9.68 671	23	9.74 524	30	0.25 476	9.94 147	7	55	.2 6.0			
	9.68 694 9.68 716	23	9.74 554	30 29	0.25 446	9.94 140	7	54	.4 12.0			
7 8	9.68 739	23	9.74 583 9.74 613	30	0.25 417	9.94 133 9.94 126	7	53 52	.5 15.0 .6 18.0			
9	9.68 762	23	9:74 643	30	0.25 357	9.94 119	7	51	.7 21.0			
10	9.68 784 9.68 807	23	9.74 673 9.74 702	29	0.25 327 0.25 298	9.94 II2 9.94 IO5	7	50	.8 24.0 .9 27.0			
12	9.68 829	22	9.74 732	30	0.25 268	9.94 098	7	49 48	.9(2).0			
13	9.68 852 9.68 873	23	9.74 762 9.74 791	29	0.25 238	9.94 090	7	47 46	1 29			
15	9.68 897	22	9.74 821	30	0.25 179	9.94 076	7	45	1 20			
16	9.68 920 9.68 942	23	9.74 851 9.74 880	30 29	0.25 149	9.94 069	7	44	.2 5.8 .3 8.7			
17	9.68 963	23	9.74 910	30	0.25 120	9.94 062 9.94 055	7	43 42	.4 11.6			
19.	9.68 987	23	9.74 939	29 30	0.25 061	9.94 048	7	41	.5 14.5 .6 17.4			
20	9.69 010	22	9.74 969 9.74 998	29	0.25 031	9.94 041 9.94 034	7	40	.7 20.3			
22	9.69 055	23	9.75 028	30 30	0.24 972	9.94 027	7	39 38	.8 23.2 .9 26.1			
23	9.69 077	23	9.75 058	29	0.24 942	9.94 020 9.94 012	7 8	37 36	.91 55.1			
25	9.69 122	22	9.75 117	30	0.24 883	9.94 005	7	35	1 00			
26	9.69 144	22	9.75 146	30	0.24 854	9.93 998	7	34	.1 2.3			
27	9.69 167 9.69 189	22	9.75 176	29	0.24 824	9.93 99 <b>1</b> 9.93 984	7	33 32	.2 4.6			
29	9.69 212	23	9.75 235	29	0.24 765	9.93 977	7	31	.4 9.2			
30 31	9.69 234 9.69 256	22	9.75 264 9.75 294	30	0.24 736	9.93 970 9.93 963	7	30 29				
32	9.69 279	23	9.75 323	29	0.24 677	9.93 955	8	28	.5 11.5 .6 13.8 .7 16.1 .8 18.4			
33 34	9.69 301 9.69 323	22	9.75 353 9.75 382	30	0.24 647	9.93 948 9.93 94 <b>1</b>	7	27 26				
35	9.69 345	22	9.75 411	29	0.24 589	9.93 934	7	25	.9 20.7			
35 36	9.69 368	23	9.75 441	30 29	0.24 559	9.93 927	7	24				
37 38	9.69 390	22	9.75 <u>4</u> 70 9.75 <u>5</u> 00	30	0.24 530	9.93 920 9.93 912	8	23	,I 2.2			
1 39	9.69 434	22	9.75 529	29	0.24 471	9.93 905	7	21				
40 41	9.69 456 9.69 479	23	9.75 558 9.75 588	30	0.24 442 0.24 412	9.93 898 9.93 891	7	20	.2 4.4 .3 6.6 .4 8.8			
42	9.69 501	22	9.75 617	29	0.24 383	9.93 884	7 8	18	.4 8.8 .5 11.0 .6 13.2			
43	9.69 523 9.69 545	22	9.75 647 9.75 676	30	0.24 353	9.93 876 9.93 869	7	17 16	.6 13.2			
45	9.69 567	22	9.75 705	29	0.24 295	9.93 862	7	15	.7 15.4 .8 17.6			
46	9.69 589	22	9.75 735	30	0.24 265	9.93 855	7 8	14	.9  19.8			
47 48	9.69 611	22	9.75 7 <sup>6</sup> 4 9.75 793	29	0.24 230	9.93 847 9.93 840	7	13 12				
49	9.69 655	22	9.75 822	29 30	0.24 178	9.93 833	7	11	8 7			
50 51	9.69 677 9.69 699	22	9.75 852 9.75 881	29	0.24 148	9.93 826 9.93 819	7	10 9	.I 0.8 0.7 .2 1.6 1.4			
52	9.69 721	22	9.75 910	29	0.24 090	0.03 811	8	0				
53 54	9.69 743 9 69 765	22	9.75 939 9.75 969	29 30	0.24 061	9.93 804 9.93 797	7	7 6	.4 3.2 2.8 .5 4.0 3.5			
55 56	9 69 787 9 69 809	22	9.75 998 9.76 027	29	0.24 002	9.93 789	8		.3 2.4 2.1 .4 3.2 2.8 .5 4.0 3.5 .6 4.8 4.2 .7 5.6 4.9 .8 6.4 5.6 .9 7.2 6.3			
56	9.69.809 9.69.831	22	9.76 <b>027</b> 9.76 <b>0</b> 56	29 29	C 23 973 O.23 944	9.93 782 9.93 775	7	5 4 3 2	.8 6.4 5.6			
58	9.69853	22	9.76 086	30	0.23 914	9.93 768	7 8		.9 7.2 6.3			
57 58 59 60	9 69 875	22	9.76 115	29 29	0.23 885	9.93 700	7	1				
60												
-	L. Cos.	d.	L. Cotg.	c. d.		L. Sin.	d.	,	Prop. Pts.			
1					60°							

					30°				
,	L. Sin.	d.		c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.69 897 9.69 919	22	9.76 144 9.76 173	29	0.23 856	9.93 753	7	60	
I 2	9.69 941	22	9.76 202	29	0.23 827 0.23 798	9 93 746 9 93 738	8	59 58	
3	9.69 963	22	9.76 231	30	0.23 769	9 93 731	7	57 56	.I 3.0 2.0
4	9.69 984	22	9.76 261	29	0.23 739	9 93 724	7		.2 6.0 5.8
5 6	9.70 000	33	9.76 319	29	0.23 710 0.23 681	9.93 717 9.93 7 <b>09</b>	8	55 54	.3 9.0 8.7
7 8	9.70 050	22 1	9.76 348	29 29	0 23 652	9.93 702	7	53	.4 12.0 11.6 .5 15.0 14.5
8 9	9.70 072	21	9.76 377 9.76 406	29	0.23 623	9.93 69 <del>5</del> 9.93 687	7	52	.6 18.0 17.4
10	9.70 115	22	9.76 435	29	0.23 565	9.93 680	7	50	.7 21.0 20.3 .8 24.0 23.2
11	9.70 137	22	9.76 464	29 29	0.23 536	9.93 673	7 8	49 48	.9 27.0 26.1
12	9.70 159 9.70 180	21	9.76 493 9.76 522	29	0.23 507 0.23 478	9 93 665 9 93 658	7	48	
14	9.70 202	22	9.76 551	29	0.23 449	9 93 650	8	47 46	28
15	9.70 224	21	9.76 580	29 29	0.23 420	9.93 643	7.	45	.1 2.8
16	9.70 245	22	9.76 609 9.76 639	30	0.23 391	9.93 636 9.93 628	8	44	.2 5.6 .3 8.4
17 18	9.70 288	21	9.76 668	29	0.23 332	9.93 621	7	43 42	.4 11.2
19	9.70 310	22	9.76 697	29 28	0.23 303	9.93 614	7	41	.5 14.0 .6 16.8
20 21	9.70 332 9.70 353	21	9.76 725 9.76 754	29	0.23 275	9.93 606	7	40	
22	9.70 375	22	9.76 783	29	0.23 217	9.93 599 9.93 591	8	39 38	.7 19.6 .8 22.4
23	9.70 396	22	9.76812	29 29	0.23 188	9.93 584	7	37 36	.9 25.2
24	9.70 418	31	9.76 841	29	0.23 159	9.93 577 9.93 569	8	36	·
26	9.70 461	22	9.76 899	29	0.23 101	9.93 562	7	35 34	22
27 28	9.70 482	22	9.76 928	29 29	0.23 072	9.93 554	8	33	.1 2.2
29	9.70 504	31	9.76 957 9.76 986	29	0.23 043	9·93 547 9·93 539	8	32 31	.3 6.6
30	9.70 547	22	9.77 015	29	0.22 985	9.93 532	7	30	.4 8.8
31	9.70 568	22	9.77 044	29 29	0.22 956	9.93 523	7	29 28	.6 13.2
32 33	9.70 590 9.70 611	31	9.77 073 9.77 101	28	0.22 927	9.93 517 9.93 510	7	28	.7 15.4
34	9.70 633	22	9.77 130	29	0.22 870	9.93 502	8	26	.8 17.6 .9 19.8
35	9.70 654	21	9.77 159	29	0.22 841	9.93 493	7 8	25	
36	9.70 675	22	9.77 188 9.77 217	29	0.22 812	9.93 487 9.93 480	7	24 23	1
37 38	9.70 718	2I 2I	9.77 246	29 28	0.22 754	9.93 472	8	22	.I 2.I
39	9.70 739	22	9.77 274	29	0.22 726	9.93 465	7 8	21	.2 42
40 41	9.70 761 9.70 782	21	9.77 3°3 9.77 33 <sup>2</sup>	29	0.22 697	9.93 4 <u>5</u> 7 9.93 4 <u>5</u> 0	7	20	
42	9.70 803	2I 2I	9.77 361	29	0.22 639	9.93 442	8	18	.4 8.4 .5 10.5 .6 12.6
43	9.70 824 9.70 846	22	9.77 390 9.77 418	28	0.22 610	9 93 435 9 93 427	8	17 16	
	9.70 867	21	9.77410	29	0.22 553	9.93 427	7	15	.7 14.7 .8 16.8
45 46	9.70 888	21 21	9.77 476	29 29	0.22 524	9 93 412	8	14	.9 18.9
47 48	9.70 909	22	9.77 505 9.77 533	28	0.22 495	9.93 405 9.93 397	7 8	13 12	
49	9.70 952	21 21	9.77 562	29	0.22 438	9.93 390	7	11	1817
50	9.70 973	21	9.77 591	29 28	0.22 409	9.93 382	8	10	.1 0.8 0.
51 52	9.70 994	21	9.77 619 9.77 648	29	0.22 381	9 93 37 <del>5</del> 9 93 367	8	9	.2 I.6 I.4 .3 2.4 2.1
53	9.71 036	21	9.77 677	29	0.22 323	9.93 360	7	9 7 6	.3 2.4 2.1 .4 3.2 2.8
54	9.71 058	31	9.77 706	29 28	0.22 294	9 93 352	8		.5 4.0 3.5
55 56	9.71 079	21	9·77 734 9·77 763	29	0.22 266 0.22 237	9.93 344	7	5 4 3 2	.6 4.8 4.2 .7 5.6 4.9 .8 6.4 5.6
57	9.71 121	21		28	0.22 209	9.93 337 9.93 329	8	3	.7 5.6 4.9 .8 6.4 5.6 .9 7.2 6.3
57 58	9.71 142	21	9.77 791 9.77 820	29	0.22 180	9.93 322	7 8		.9 7.2 6.3
59 <b>60</b>	9.71 163	21	9.77 849	28	0.22 151	9.93 314	7	1	1
1		- 1		- 1		9 93 307 T Sin			Duon Die
-	L. Cos.	d.	L. Cotg.	c. u.	L. Tang.	L. Sin.	d.	,	Prop. Pts.

I

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78

9

19

21

22

29

4 I

	32°  / L. Sin. d. L. Tang. c. d. L. Cotg. L. Cos. d. Prop. Pts.  0 9.72 421 9.79 570 2.29 421 9.92 842 60										
	,	L. Sin.	d.	L. Tang.	c. d.		L. Cos.	d.		Pre	op. Pts.
	0	9.72 42I 9.72 44I	20	9.79 579 9.79 607	28	0.20 421	9.92 842 9.92 834	8	60 59		-
	2	9.72 461 9.72 482	21	9.79 635 9.79 663	28	0.20 365	9.92 826 9.92 818	8	59 58	1	29   28
ı	3 4	9.72 502	20	9.79 691	28 28	0.20 309	9.92 810	8 7	57 56	. I .2	2.9 2.8 5.8 5.6
	5	9.72 522 9.72 542	20	9.79 719 9.79 747	28	0.20 281 0.20 253	9.92 80 <u>3</u> 9.92 795	8	55	.3	8.7 8.4
ı	7 8	9.72 562	20	9.79 776	29 28	0.20 224	9.92 787	8	54 53		11.6 11.2 14.5 14.0
ı	8	9.72 582 9.72 602	20	9.79 804 9.79 832	28	0.20 196 0.20 168	9.92 779 9.92 771	8	53 52 51	.6 1	17.4 16.8
	10	9.72 622	20	9.79 860	28 28	0.20 140	9.92 763	8	$\frac{32}{50}$	.8 2	20.3 19.6
ı	II 12	9.72 643	20	9.79 888 9.79 916	28	0.20 112	9.92 755 9.92 747	8	49 48	.9 2	26.1 25.2
ı	13	9.72 683	20	9.79 944	28 28	0.20 056	9.92 739	8	47 46		1
ı	14	9.72 703	20	9.79 972	28	0.20 028	9.92 731	8	45	.1	27
ı	15 16	9.72 743	20	9.80 028	28 28	0.19 972	9.92 715	8	44		
ı	17 18	9.72 763 9.72 783	20	9.80 056 9.80 084	28	0.19 944 0.19 916	9.92 707 9.92 699	8	43 42	:	4 10.8
	19	9.72 803	20	9.80 112	28 28	0.19 888	9.92 691	8	4I		5 13.5 6 16.2
	20	9.72 823 9.72 843	20	9.80 140 9.80 168	28	o. 19 860 o. 19 832	9.92 683	8	<b>40</b>		7 18.9
	22	9.72 863	20	9.80 195	27 28	0.19803	9.92 667	8	39 38		8 21.6 9 24.3
	23 24	9.72 883 9.72 902	19	9.80 223 9.80 251	28 28	0.19 777 <b>0</b> .19 749	9.92 659 9.92 651	8	37 36		
	25	9.72 922	20	9.80 279	28	0.19 721	9.92 643	8	35		21   20
ı	26 27	9.72 942 9.7 <b>2 9</b> 62	20	9.80 307 9.80 335	28	0.19 69 <u>3</u> 0.19 66 <u>5</u>	9.92 635 9.92 627	8	34 33	.1	2.1 2.0
I	28	0.72 982	20	9.80 363	28 28	0.19 637	9.92 619	8	32	.2	4.2 4.0 6.3 6.0
	29 30	9.73 002	20	9.80 391	28	0.19 581	9.92 611	8	$\frac{31}{30}$	.4	8.4 8.0
ı	31	9.73 041	20	9.80 447	28	0.19 553	9.92 595	8	29	·5 .6	12.6 12.0
I	32 33	9.73 061 9.73 081	20	9.80 474 9.80 502	28	0.19 526	9.92 587 9.92 579	8	28 27	·7	14.7 14.0 16.8 16.0
ı	34	9.73 101	20	9.80 530	28 28	0.19 470	9.92 571	8	26	.9	18.9 18.0
;	35 36	9.73 121 9.73 140	19	9.80 558 9.80 586	28	0.19 442	9.92 56 <u>3</u> 9.92 55 <u>5</u>	8	25 24		
١	37 38	9.73 160	20	9.80 614	28	0.19 386	9.92 546	8	23		19 9
۱	39	9.73 180 9.73 200	20	9.80 642 9.80 669	27	0.19 358	9.92 538 9.92 530	8	22 2I	. I . 2	1.9 0.9 3.8 1.8
ł	40	9.73 219	19	9.80 697	28	0.19 303	9.92 522	8	20	.3	5.7 2.7
	41	9.73 239 9.73 259	20	9.80 72 <del>5</del> 9.80 753	28	0.19 275	9.92 514 9.92 506	8	19 18	.4	7.6 3.6 9.5 4.5
	43	9.73 278 9.73 298	19 20	9.80 781 9.80 808	28 27	0.19 219	9.92 498	8	17 16		11.4 5.4
	44	9.73 318	20	9.80 836	28	0.19 164	9.92 482	8	15	.81	15.2 7.2
1	46	9 · 73 337	20	9.80 864	28 28	0.19 136	9 92 473 9 92 465	8	14	.91	17.1 8.1
	47 48	9·73 357 9·73 377	20 19	9.80 919	27 28	0.19081	9.92 457	8	12		
	$\frac{49}{50}$	9.73 396	20	9.80 947	28	0.19 053	9.92 449	8	$\frac{11}{10}$	1.1	0.8 0.7
	51	9.73 416 9.73 43 <u>5</u>	19	9.81 003	28	0.18 997	9.92 433	8	9 8	.2	1.6 1.4
1	52	9 · 73 · 455 9 · 73 · 474	19	9.81 030	27 28	0.18 970	9.92 425 9.92 416	9	8	.3	2.4 2.I 3.2 2.8
	54	9.73 474	20 19	9.81 086	28	0.18 914	9.92 408	8	7 6	.4 .5 .6	4.0 3.5 4.8 4.2
1	55	9 73 513	20	9.81 113 9.81 141	28	o. 18 887 o. 18 859	9.92 400 9.92 392	8	5 4	.7	3.2 2.8 4.0 3.5 4.8 4.2 5.6 4.9 6.4 5.6
	57	9·73 533 9·73 552	19	9.81 169	28 27	0.18831	9.92 384	8	3 2	.7 .8 .9	5.6 4.9 6.4 5.6 7.2 6.3
	52 53 54 55 56 57 58 59	9 73 572 9 73 591	19	9.81 196	28	0.18 804	9.92 376	9	2 I	.91	71 0.3
	60	9 73 611	20	9.81 252	28	0.18 748	9.92 359	8	0		
		L. Cos.	d.	L. Cotg.	c. d.		L. Sin.	d.	,	Pr	op. Pts.
-						$57^{\circ}$					

					33°				
		d.	L. Tang.	c. d.		L. Cos.	d.		Prop. Pts.
	9.73 611 9.73 630	19	9.81 252 9.81 279	27	0.18 748 0.18 721	9.92 359	8	60	
	9.73 650	19	9.81 307	28	0.18 693	9.92 351	8	59 58	28   27
1	3 9.73 669	20	9.81 335	27	0.18 665	9.92 335	9	57 56	.1 2.8 2.7
-	9.73 689 9.73 708	19	9.81 362	28	0.18 610	9.92 326	8		.2 5.6 5.4
	6 9.73 727	20	9.81 418	28	0.18 582	9.92 310	8	55 54	.3 8.4 8.1 .4 II.2 10.8
	7 9·73 747 8 9·73 766	19	9.81 445 9.81 473	28	0.18 555	9.92 302	9	53	.5 14.0 13.5
	9 9.73 766 9 9.73 785	19	9.81 500	27 28	0.18 500	9.92 293	8	52 51	
1	9.73 805	19	9.81 528	28	0.18 472	9.92 277	8	50	.8 22.4 21.6
I	1 9.73 824	19	9.81 556	27	0.18 444 0.18 417	9.92 269	9	49	.9 25.2 24.3
I	3 9.73 863	20	9.81 611	28	0.18 389	9.92 260	8	48 47	
I.	4 9.73 882	19	9.81 638	27 28	0.18 362	9.92 244	9	46	20
I	9.73 901	20	9.81 666 9.81 693	27	0.18 334 0.18 307	9.92 235	. 8	45	.I 2.0 .2 4.0
I		19	9.81 721	28	0.18 279	9.92 227 9.92 219	8	44 43	.3 6.0
1	8 9.73 959	19	9.81 748	27 28	0.18 252	9.92 211	9	42	.4 8.0 .5 10.0
$\frac{1}{2}$		19	9.81 776	27	0.18 224	9.92 202	8	$\frac{41}{40}$	.6 12.0
2		20	9.81 831	28	0.18 169	9.92 186	8	30	.7 14.0 .8 16.0
2	2 9.74 036	19	9.81858	27	0.18 142	9.92 177	9	38	.0 18.0
2 2		19	9.81 886	27	0.18 114	9.92 169 9.92 161	8	37 36	1
2		19	9.81 941	28	0.18 059	9.92 152	9	35	1 19
2	, , , ,	19	9.81 968	27	0.18 032	9.92 144	8	34	.1 1.0
2	7 9.74 I32 8 9.74 I5I	19	9.82 023	27	0.18 004	9.92 I36 9.92 I27	9	33	.2 3.8
	9 9.74 170	19	9.82 051	28	0.17 949	9.92 119	8	31	·3 5·7 ·4 7.6
3		19	9.82 078 9.82 106	28	0.17 922	9.92 111	9	<b>30</b> 29	-5 9.5
	1 9.74 208 2 9.74 227	19	9.82 133	27	0.17 867	9.92 102	8	28	.6 11.4 .7 13.3
3	3 9.74 246	19	9.82 161	28	0.17 839	9.92 086	9	27	.8 15.2
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	19	9.82 188	27	0.17 812	9.92 077	8	25	.9 17.1
3	6 9.74 303	19	9.82 243	28	0.17 757	9.92 060	9	24	
3	7 9.74 322	19	9.82 270 9.82 298	27 28	0.17 730	9.92 052	8	23 22	18
3	8 9.74 34 <b>1</b> 9 9.74 360	19	9.82 325	27	0.17 702	9.92 044	9	21	.1 1.8 2 3.6
4	9.74 379	19	9.82 352	27	0.17 648	9.92 027	9	20	-3 5-4
4	9.74 398	19	9.82 380 9.82 407	27	0.17 620	9.92 018	8	18	.4 7.2
	9.74 417	19	9.82 435	28	0.17 565	9.92 002	8	17	.5 9.0 .6 10.8
4	$9.7445\overline{5}$	19	9.82 462	27	0.17 538	9.91 993	8	16	.7 12.6
1 4	5 9.74 474 6 9.74 493	19	9.82 489 9.82 517	28	0.17 511	9.91 98 <del>5</del> 9.91 976	9	15	.8 14.4 .9 16.2
1	9.74 493 7 9.74 512 8 9.74 531	19	9.82 544	27	0.17 456	9.91 968	8	13	
4		18	9.82 571 9.82 599	27	0.17 429	9.91 959	8	12 11	1918
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	19	9.82 599	27	0.17 374	9.91 942	9	10	.1 0.0 0.8
1 5	9.74 587	19	9.82 653	27	0.17 347	9.91 934	8	9	1.8 1.6
1	9.74 606	19	9.82 681	27	0.17 319	9.91 925	8	0	.3 2.7 2.4 .4 3.6 3.2
	9.74 644	19	9.82 735	27	0.17 265	9.91 908	9	7 6	.5 4.5 4.0
1	5 9.74 662	19	9.82 762	27	0.17 238	9.91 900 9.91 891	9	5 4 3 2	2.7 2.4 .4 3.6 3.2 .5 4.5 4.0 .6 5.4 4.8 .7 6.3 5.6 .8 7.2 6.4 .9 8.1 7.2
1	6 9.74 681 7 9.74 700	19	9.82 790 9.82 817	27	0.17 210	9.91 883	8	3	.8 7.2 6.4
1	8 9.74 719	19	9.82 844	27	0.17 156	9.91 874	9	2	.9 8.1 7.2
-	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	. 19	9.82 871	28	0.17 129	9.91 866	9	0	
-				0 4			d.	<del>  ,</del>	Prop. Pts.
-	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	I L. SIII.	· u.	,	1 1 top- 1 ts-
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					34°				
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.74 756	19	9.82 899	27	0.17 101	9.91 857	8	60	
1 2	9·74 775 9·74 794	19	9.82 926 9.82 953	27	0.17 074	9.91 849   9.91 840	9	59 58	1 40 1
3	9.74 812	18	9.82 980	27	0.17 020	9.91 832	8	57	.1 2.8 2.7
4	9.74 831	19	9.83 008	27	0.16 992	9.91 823	8	56	.2 5.6 5.4
5	9.74 868	18	9.83 03 <del>5</del> 9.83 062	27	0.16 965 0.16 938	9.91 81 <del>5</del> 9.91 806	9	55 54	
7 8	9.74 887	19	9.83 089	27 28	0.16 911	9.91 798	8	53	
8	9.74 906	18	9.83 117 9.83 144	27	o. 16 883 o. 16 856	9.91 789 9.91 781	8	52 51	.6 16.8 16.2
10	9.74 943	19	9.83 171	27	0.16 829	9.91 772	9	$\frac{51}{50}$	.7 19.6 18.9 .8 22.4 21.6
11	9.74 961	18	9.83 198	27 27	0.16 802	9.91 763	9	49 48	.9 25.2 24.3
12 13	9.74 980 9.74 999	19	9.83 225 9.83 252	27	0.16 77 <del>5</del> 0.16 748	9.91 755	9	48 47	
14	9.75 017	18	9.83 280	28 27	0.16 720	9.91 738	8	46	26
15	9.75 036	18	9.83 307	27	0.16 693	9.91 729	9	45	.I 2.6 .2 5.2
16	9 · 75 ° 54   9 · 75 ° 73	19	9.83 334 9.83 361	27	0.16 666 0.16 639	9.91 720	8	44 43	3 7.8
17 18	9.75 091	18	9.83 388	27	0.16 612	9.91 703	9	43	.4 10.4
19	9.75 110	18	9.83 415	27	0.16 585	9.91 695	9	41	.5 13.0 .6 15.6
20	9.75 128 9.75 147	19	9.83 442 9.83 470	28	0.16 558	9.91 686	9	40	.7 18.2
22	9.75 165	18	9.83 497	27	0.16 503	9.91 669	8	39 38	.8 20.8 .9 23.4
23	9.75 184 9.75 202	18	9.83 524 9.83 551	27	0.16476 0.16449	9.91 660 9.91 651	9	37 36	.91-3.4
24 25	9.75 221	19	9.83 578	27	0.16 422	9.91 643	8	35	
26	9.75 239	18	9.83 605	27	0.16 395	9.91 634	9	34	.1 1.9
27 28	9.75 258 9.75 276	18	9.83 632	27	0.16 368	9.91 625 9.91 617	9 8	33	.2 3.8
29	9.75 294	18	9.83 686	27	0.16 314	9.91 608	9	32 31	.3 5.7
30	9.75 313	19	9.83 713	27	0.16 287	9.91 599	9	30	.4 7.6 .5 9.5
31	9.75.331 9.75.350	19	9.83 740 9.83 768	28	0.16 260	9.91 591	9	29 28	.6 11.4
33	9.75 368	18	$9.8379\overline{5}$	27 27	0.16 205	9.91 573	9	27	.7 13.3 .8 15.2
34	9.75 386	19	9.83 822	27	0.16 178	9.91 563	9	26	.9 17.1
35 36	9.75 40 <del>5</del> 9.75 423	18	9.83 849 9.83 876	27	0.16 151	9.91 556 9 91 547	9	25 24	
37	9.75 44I	18	9.83 903	27	0.16 097	9.91 538	9	23	18
38	9 75 459 9 75 478	19	9.83 930 9.83 957	27	0.16 070	9.91 530	9	22	.1 1.8
$\frac{39}{40}$	9.75 496	18	9.83 984	27	0.16 016	9.91 521	9	20	.2 3.6 .3 5.4
41	9.75 514	18	9.84 011	27	0.15 989	9.91 504	8	19	.4 7.2
42 43	9·75 533 9·75 551	18	9.84 038 9.84 06 <del>5</del>	27	0.15 962	9.91 49 <del>5</del> 9.91 486	9	18	.5 9.0 .6 10.8
43	9.75 569	18	9.84 092	27	0.15 908	9.91 488	9	16	
45 46	9.75 587	18	9.84 119	27	0.15 881	9.91 469	9	15	.7 12.6 .8 14.4 .9 16.2
40	9.75 605 9 75 624	19	9.84 146 9.84 173	27	0.15 854	9.91 460 9.91 451	9	14	.9  16.2
47 48	9.75 642	18 18	9.84 200	27	0.15 800	9.91 442	9	12	
49	9.75 660	18	9.84 227	27	0.15 773	9.91 433	9	$\frac{11}{10}$	.1 0.9 0.8
50 51	9.75 678 9.75 696	18	9.84 254 9.84 280	26	0.15 746	9.91 42 <del>5</del> 9.91 416	9		1 2 7 8 7 6
52	9.75 714	18	9.84 307	27	0.15 720 0.15 693 0.15 666	9.91 407	9	8	.3 2.7 2.4 .4 3.6 3.2
53	9.75 714 9.75 733 9.75 751	18	9.84 334 9.84 361	27	0.15 666	9.91 398	9	9 8 7 6	5 4.5 4.6
55	9.75 769	18	9.84 388	- 27	0.15 6T2	9.91 381	8		.3 2.7 3.4 .4 3.6 3.2 .5 4.5 4.6 .6 5.4 4.6 .7 6.3 5.6 .8 7.2 6.4 .9 8.1 7.2
56	9.75 769 9.75 787 9.75 805 9.75 823	18	9.84 415	27	0.15 583	9.91 372	9	5 4 3 2	8 7.2 6.4
57	9.75 805	18	9.84 442 9.84 469	27	0.15 558	9.91 363	9	3 2	.9 8.1 7.2
52 53 54 55 56 57 58 59 <b>60</b>	9.75 041	18	9.84 496	27	0.15 504	9.91 345	9		
60	9.75 859	15	9.84 523		0.15 477	9.91 336		0	
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.
					55°				

					35°						
,	L. Sin.	d.	L. Tang.	c.d.	L. Cotg.	L. Cos.	d.		Pr	op. Pt	ts.
0	9.75 859 9.75 877	18	9.84 523 9.84 550	27	0.15 477	9.91 336 9.91 328	8	60			
2	9.75 895	18	9.84 576	26	0.15 424	9.91 319	9	59 58		27	26
3	9.75 913	18	9.84 603	27	0.15 397	9.91 310	9	57 56	.1	2.7	2.6
4	9.75 931 9.75 949	18	9.84 657	27	0.15 370	9.91 301	9	55	.2	5.4 8.1	5.2 7.8
5	9.75 967	18	9.84 684	27 27	0.15 316	9.91 283	9	54		10.8	10.4
7 8	9.75 985 9.76 003	18	9.84 711 9.84 738	27	0.15 289	9.91 274 9.91 266	9	53 52	.5		13.0
9	9.76 021	18	9.84 764	26 27	0.15 236	9.91 257	9	51	.7		15.6
10	9.76 039	18	9.84 791 9.84 818	27	0.15 209	9.91 248	9	50	.8	21.6 2	20.8
11	9.76 057	18	9.84 845	27	0.15 182	9.91 239 9.91 230	9	49 48	.9	24.3 2	3.4
13	9.76 093	18	9.84 872	27 27	0.15 128	9.91 221	9	47		1 18	
14	9.76 111	18	9.84 899	26	0.15 101	9.91 212	9	46	١.	1 1.	
15 16	9.76 146	17	9.84 952	27 27	0.15 048	9.91 194	9	45 44		2 3.	
17	9.76 164 9.76 182	18	9.84 979 9.85 006	27	0.15 021	9.91 185	9	43		3 5.	
19	9.76 200	18	9.85 033	27 26	0.14 967	9.91 167	9	42 41		5 9.	0
20	9.76 218	18	9.85 059	27	0.14 941	9.91 158	9	40			
2I 22	9.76 236 9.76 253	17	9.85 086	27	0.14 914	9.91 149 9.91 141	8	39 38		8 14.	4
23	9.76 271	18	9.85 140	27	0.14 860	9.91 132	9	37 36		9   16.	2
24	9.76 289	18	9.85 166	27	0.14 834	9.91 123	9	36			
25 26	9.76 307 9.76 324	17	9.85 193 9.85 220	27	0.14 807	9.91 114	9	35 34		17	
27 28	9.76 342	18	9.85 247	27	0.14 753	9 91 096	9	33		1 1.	
28	9.76 360 9.76 378	18	9.85 273 9.85 300	27	0.14 727	9.91 087 9.91 078	. 9	32 31		3 5	
30	9.76 395	17	9.85 327	27	0.14 673	9.91 069	9	30			5
31	9.76 413	18	9.85 354 9.85 380	27 26	0.14 646	9.91 060	9	29 28		6 10.	2
32 33	9.76 448	17	9.85 407	27	0.14 593	9.91 051	9	27		7 11.	
34	9.76 466	18	9.85 434	27	0.14 566	9.91 033	10	26		9 15	
35 36	9.76 484 9.76 501	17	9.85 460 9.85 487	27	0.14 540	9.91 023	9	25 24			
37 38	9 76 519	18	9.85 514	27 26	0.14 486	9.91 005	9	23		1 10	,
38	9.76 537 9.76 554	17	9.85 540 9.85 567	27	0.14 460	9.90 996	9	22 21			.0
40	9.76 572	18	9.85 594	27	0.14 406	9.90 978	9	20		3 3	0
41	9.76 590	18	9.85 620	26	0.14 380	9.90 969	9	19		4 4	.0
42	9.76 607 9.76 625	18	9.85 647 9.85 674	27	0.14 353	9.90 960	9	18		5 5	.0
44	9.76 642	17	9.85 700	26	0.14 300	9.90 942	9	16			.0
45 46	9.76 660 9.76 677	17	9.85 727 9.85 754	27	0.14 273 0.14 246	9.90 933 9.90 924	9	15		8 8	
47	9.76 695	18	9.85 754 9.85 780	26	0.14 240	9.90 915	9	14		) ( )	
47 48 49	9.76 712	17	9.85 807 9.85 834	27	0.14 193	9.90 906	10	12 11		0 1	8
50	9.76 730	17	9.85 860	26	0.14 166	9.90 887	9	10	1.	0.9	0.8
51	9.76 763	18	9.85 887	27	0.14 113	9.90 878	9	9	.2	1.8	1.6
52	9.76 782 9.76 800	18	9.85 913 9.85 940	27	0.14 087	9.90 869	9	7	.4	3.6	3.2
54	9.76 817	17	9.85 967	27 26	0.14 033	9.90 851	9	7 6	.5	4.5	4.0
52 53 54 55 56 57 58 59	9.76 835	17	9.85 993	27	0.14 007	9.90 842 9.90 832	10	5 4 3 2	·3 ·4 ·5 ·6 ·7 ·8	4.5 5.4 6.3 7.2 8.1	4.0 4.8 5.6 6.4
57	9.76 852 9.76 870	18	9.86 020 9.86 046	26	0.13 980	9.90 823	9	3	.8	7.2	6.4
58	9.76 887	17	9.86 073 9.86 100	27	0.13 927	9.90 814 9 90 805	9	2 I	.91	0.1	12
60	9.76 904	18	9.86 126	26	o 13 900 o 13 874	9 90 796	9	0			
1	L. Cos.	d.		c. d.	L. Tang.		d.	<b>-</b>	P	rop. P	ts.
-	12000	. 40	. 2. 0018	-CJ tt	54°			-			

F						36°						
	,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		P	rop.	Pts.
	0	9.76 922	17	9.86 126 9.86 153	27	0.13 874 0.13 847	9.90 796	9	60			
T	I 2	9.76 939 9.76 957	18	9.86 179	26 27	0.13 821	9.90 787 9.90 777	10	59 58	,	27	26
	3	9.76 974 9.76 991	17	9.86 206	26	0.13 794	9.90 768	9	57 56	. 1	2.7	2.6
1	4	9.77 009	18	9.86 259	27	0.13 741	9.90 759 9.90 750	9	55	.2	5.4 8.1	5.2 7.8
	5	9.77 026	17	9.86 285	26 27	0.13 715	9.90 741	30	54	.4	10.8	10.4
	7 8	9.77 043 9.77 061	18	9.86 312 9.86 338	26	0.13 688	9.90 731 9.90 722	9	53 52	.5	13.5 16.2	13.0
	9	9.77 078	17	9.86 365	27	0.13 635	9.90 713	9	51	.7 .8	18.9	18.2
	10 11	9.77 095 9.77 112	17	9.86 392 9.86 418	26	0.13 608 0.13 582	9.90 704 9.90 694	10	50	.8	21.6 24.3	20.8
	12	9.77 130	18	9.86 445	27 26	0.13 555	9.90 685	9	49 48	.91	-4.31	~3.4
	13	9.77 147 9.77 164	17	9.86 471 9.86 498	27	0.13 529 0.13 502	9.90 676 9.90 667	9	47		1	18
-	15	9.77 181	17	9.86 524	26	0.13 476	9.90 657	10	46 45		.1 1	.8
	16	9.77 199	17	9.86 551	27 26	0.13 449	9.90 648	9	44			.6
l	17 18	9.77 216 9.77 233	17	9.86 577	26	0.13 423 0.13 397	9.90 639	9	43		.4 7	.2
	19	9.77 250	17	9.86 630	27 26	0.13 370	9.90 620	9	41			0.0
	20 21	9.77 268 9.77 285	17	9.86 656 9.86 683	27	0.13 344 0.13 317	9.90 611 9.90 602	9	40		.7 12	2.6
	22	9.77 302	17	9.86 700	26 27	0.13 291	9.90 592	10	39 38			.4
	23 24	9.77 319 9.77 336	17	9.86 736 9.86 762	26	0.13 264	9.90 583	9	37 36		.91 4	
-	25	9.77353	17	9.86 789	27	0.13 211	9.90 565	9	35			
	26	9.77 370	17	9.86 815	26 27	0.13 185	9.90 555	10	34			7 1 . 7
	27 28	9.77 387 9.77 405	18	9.86 842 9.86 868	26	0.13 158 0.13 132	9.90 546 9.90 537	9	33 32		.2 3	3.4
	29	9.77 422	17	9.86 894	26 27	0.13 106	9.90 527	9	31		.3	. i . 8
	30 31	9·77 439 9·77 456	17	9.86 921 9.86 947	26	0.13 079	9.90 518	9	30		.5	3.5
ı	32	9.77 473	17	9.86 974	27 26	0.13 026	9.90 499	10	28		.7 I	0.2
I	33 34	9.77 490 9.77 507	17	9.87 000 9.87 027	27	0.13 000 0.12 973	9.90 490	9	27 26		.8 1	3.6
	35	9.77 524	17	9.87 053	26	0.12 947	9.90 471	9	25		.9  1	5.3
	35 36	9.77 541	17	9.87 079	26 27	0.12 921	9.90 462	9	24			
	37 38	9.77 558 9.77 575	17	9.87 106	26	0.12 894	9.90 452 9.90 443	9	23			<b>16</b> 1.6
	39	9.77 592	17	9.87 158	26 27	0.12 842	9.90 434	9	21		.2	2.2
1	40 41	9.77 609 9.77 626	17	9.87 185	26	0.12 815	9.90 424	9	20		.3 4	1.8
	42	9.77 643	17	9.87 238	27 26	0.12 762	9.90 405	10	18		.5	3.0
	43 44	9 77 660 9.77 677	17	9.87 264 9.87 290	26	0.12 730	9.90 396 9.90 386	9 10	17 16			).6 1.2
1	45	9.77 694	17	9.87 317	27	0.12 683	9.90 377	9	15		.8 1:	2.8
	46	9.77 711	17	9.87 343 9.87 369	26	0.12 657	9.90 368 9.90 358	10	14		9 1	1.4
	47 48	9.77 744	16 17	9.87 396	27 26	0.12 604	9.90 349	9	12			
	49 <b>50</b>	9.77 761	17	9.87 422	26	0.12 578	9.90 339	10	11 10	п.	10 1.0	0.9
	51	9.77 778 9.77 79 <b>5</b>	17	9.87 448 9.87 475	27	0.12 552 0.12 525	9.90 330	10		.2	2.0	1.8
	52	9.77 795 9.77 812	17	9.87 501	26 26	0.12 499	9.90 311	9	8	.3	3.0	2.7 3.6
	53	9.77 829 9.77 846	17	9.87 527 9.87 554	27	0.12 473	9.90 301 9.90 292	9	7 6	.4 .5 .6	4.0 5.0 6.0	4.5
	55	9.77 862	16	9.87 580	26 26	0.12 420	9.90 282	10		.6	6.0	5.4. 6.3
	56	9.77 879 9.77 896	17	9.87 606 9.87 633	27	0.12 394	9.90 273 9.90 263	9 10	5 4 3 2	.7 .8	7.0 8.0	7.2
	58	9.77 913	17	9.87 659	26 26	0.12 341	9.90 254	9		.9		8.1
	53 54 55 56 57 58 59 <b>60</b>	9.77 930	16	9.87 685	26	0.12 315	9.90 244	9	1			
	30	9.77 946	-		0 1	L. Tang.	9.90 235 T. Sin		, ,	<u></u>	rop.	Pte
		L. Cos.	d.	L. Cotg.	ic. u.		L. Sin.	d.	1 /		rop.	1 (3)
						53°						

					37°					
1	1. Sin.	d.	L. Tang.	c. d.		L. Cos.	d.		Prop. Pts.	
0	9.77 946	17	9.87 711 9.87 738	27	0.12 289	9.90 235	10	60		
1 2	9.77 963 9.77 980	17	9.87 764	26	0.12 236	9.90 225 9.90 216	9	59 58	1	
3	9.77 997 9.78 013	17	9.87 790	27	0.12 210	9.90 206	9	57	.1 2.7	
4	9.78 030	17	9.87 817	26	0.12 183	9.90 197	10	56	.2 5.4	
5 6	9.78 047	17	9.87869	26 26	0.12 131	9.90 178	9	55 54	.3 8.1 .4 10.8	
7 8	9.78 o63 9.78 o80	17	9.87 895 9.87 922	27	0.12 103	9.90 168	9	53	.5 13.5	
9	9.78 097	17	9.87 948	26	0.12 0/8	9.90 <b>15</b> 9 9.90 <b>1</b> 49	10	52 51	.6 16.2 .7 18.9	
10	9.78 113	16	9.87 974	26 26	0.12 026	9.90 139	10	50	.7 18.9 .8 21.6	
II	9.78 130 9.78 147	17	9.88 000	27	0.12 000	9.90 130	9	49 48	.9 24.3	
13	9.78 163	16	9.88 053	26	0.11 973	9.90 120	9	48	į.	
14	9.78 180	17	9.88 079	26 26	0.11 921	9.90 101	10	46	26	
15 16	9.78 197 9.78 213	16	9.88 105 9.88 131	26	0.11 893	9.90 091	9	45	.1 2.6 .2 5.2	
17	9.78 230	17	9.88 158	27	0.11 842	9.90 082	10	44	.3  7.8	
18	9.78 246	16	9.88 184	26 26	0.11 816	9.90 063	9	42	.4 10.4	
19 20	9.78 263	17	9.88 210	26	0.11 790	9.90 053	10	41	.5 13.0 .6 15.6	
21	9.78 296	16	9.88 262	26	0.11 738	9.90 043	9	40	.7 18.2	
22	9.78 313	17	9.88 289	27 26	0.11 711	9.90 024	10	39 38	.8 20.8	
$\begin{bmatrix} 23 & 9.76 & 329 & 17 \\ 24 & 9.78 & 346 & 16 \end{bmatrix} \xrightarrow{17} \begin{bmatrix} 9.88 & 341 & 26 \\ 9.88 & 341 & 26 \\ 26 & 6.11 & 659 & 9.90 & 65 \end{bmatrix} \xrightarrow{9} \begin{bmatrix} 37 \\ 36 \end{bmatrix}$										
	9.78 362		9.88 367		0.11 633	9.89 995	10	35		
25 26	9.78 379	17	9.88 393	26 27	0.11 607	9.89 985	9	34	.1 1.7	
27 28	9.78 395 9.78 412	17	9.88 420	26	0.11 580	9.89 976 9.89 966	10	33	.2 3.4	
29	9.78 428	16	9.88 472	26 26	0.11 528	9.89 956	9	31	.3 5.1 .4 6.8	
30	9.78 445	16	9.88 498	26	0.11 502	9.89 947	10	30	.5 8.5	
31 32	9.78 461 9.78 478	17	9.88 524 9.88 550	26	0.11 476	9.89 937 9.89 927	10	29 28	.6 10.2	
33	9.78 494	16 16	9.88 577	27 26	0.11 423	9.89 918	9	27	.7 11.9 .8 13.6	
34	9.78 510	17	9.88 603	26	0.11 397	9.89 908	10	26	.9 15.3	
35 36	9.78 527 9.78 543	16	9.88 655	26	0.11 371	9.89 898 9.89 888	10	25 24		
37 38	9.78 560	17	9.88 681	26 26	0.11 319	9.89879	·9	23	16	
38	9.78 576 9.78 592	16	9.88 707 9.88 733	26	0.11 293	9.89 869 9.89 859	10	22 21	.1 1.6	
40	9.78 609	17	9.88 759	26	0.11 241	9.89 849	10	20	.2 3.2 .3 4.8 .4 6.4	
41	9.78 625	16	9.88 786	27 26	0.11 214	9.89 840	9	19	.4 6.4	
42	9.78 642 9.78 658	16	9.88 812 9.88 838	26	0.11 188	9.89 830 9.89 820	10	18	.5 8.0 .6 9.6	
44	9.78 674	16	9.88 864	26 26	0.11 136	9.89 810	10	16	.7 11.2	
45	9.78 691	16	9.88.890	26	0.11 110	9.89 801	10	15		
46	9.78 707 9.78 723	16	9.88 916	26	0.11 084	9.89 <b>791</b> 9.89 781	10	14	.9  14.4	
48	9.78 739	16	9.88 968	26 26	0.11 032	9.89 771	10	12		
49 <b>50</b>	9.78 756	16	9.88 994	26	0.11 006	9.89 761	9	$\frac{11}{10}$	.1 1.0 0.9	
51	9.78 <b>772</b> 9.78 788	16	9.89 046	26	0.10 954	9.89 752 9.89 742	10		.2 2.0 1.8	
52	9.78 805	17	9.89 073	27 26	0.10 927	9.89 732	10	9	.3 3.0 2.7	
53 54	9.78 821 9.78 837	16	9.89 099 9.89 123	26	0.10 901	9.89 722 9.89 712	10	7	.3 3.0 2.7 .4 4.0 3.6 .5 5.0 4.5 .6 6.0 5.4	
55	9.78 853	16	9.89 151	26	0.10 849	9.89 702	10		3 3.0 2.7 .4 4.0 3.6 .5 5.0 4.5 .6 6.0 5.4 7.0 6.3 .8 3.0 7.2 .9 9.0 8.1	
55 56 57 58	9.78 853 9.78 869	16	9.89 177	26 26	0.10 823	9.89 693	9	5 4 3 2	.7 7.0 6.3 .8 8.0, 7.2	
57	9.78 886 9.78 902	16	9.89 203	26	0.10 797	9.89 683 9.89 673	10	3 2	.9 4.0 8.1	
59	9.78 918	16	9.89 255	26 26	0.10745	9.89 663	10	I		
60	9.78 934	·	9.89 281		0.10719	9.89 653		0		
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.	
					52°					

9.78 934 9.78 950 9.78 967	38°  / L. Sin. d. L. Tang. c. d. L. Cotg. L. Cos. d. Prop. Pts.  0 9.78 934 16 9.89 281 26 0.10 719 9.89 653 10 60													
9.78 950			c. a.			d.		_P	rop. I	ets.				
9.78 967	16	9.89 281 9.89 307	26	0.10 719 0.10 693	9.89 653	10								
10 0 1	17	9.89 333	26	0.10 667	9.89 643 9.89 633	10	59 58							
9.78 983	16 16	9.89 359	26 26	0.10641	9.89 624	10	57	1.	26	25 2.5				
9.78 999	16	9.89 385	26	0.10613	9.89 614	10	57 56	.2	5.2	50				
9.79 OI 5 9.79 O31	16	9.89 411 9.89 437	26	0.10 589 0.10 563	9.89 604 9.89 594	10	55	.3	7.8	7 3				
9.79 047	≱6 16	9.89 463	26 26	0.10 537	9.89 584	10	54 53	•4		10.0 12.5				
9.79 063	16	9.89 489	26	0.10 511	9.89 574	10	52	·5	15.6	15.0				
9.79 079	16	9.89 515	26	0.10483	9.89 564	10	51	.7 .8		17.5				
9.79 095   9.79 111	16	9.89 567	26	0.10459	9.89 554 9.89 544	10	<b>50</b> 49	.9	23.4	20.0				
9.79 128	17	9.89 593	26 26	0.10 407	9.89 534	10	48	,,,,	-5-11					
9.79 144	16	9.89 619	26	0.10 381	9.89 524	10	47		1 27	,				
9.79 160 9.79 176	16	9.89 645	26	0.10 355	9.89 514	10	46			.7				
9.79 192	16 16	9.89 697	26	0.10 303	9.89 495	9	45 44		.2 3	.4				
9.79 208	16	9.89 723	26 26	0.10 277	9.89 485	10	43		.3 5	. I . 8				
9.79 224 9.79 240	16	9.89 749 9.89 775	26	0.10 251 0.10 225	9.89 475	10	42	1		.5				
9.79 256	16	9.89 801	26	0.10 199	9.89 455	10	$\frac{41}{40}$		.6 10	.2				
9.79 272	16	9.89827	26 26	0.10 173	9.89 445	10	39		.7 II .8 I3					
9.79 288	16	9.89 853	26	0.10147	9.89 435	10	39 38		.9 15					
9.79 304   9.79 319	15	9.89 879	26	0.10 121	9.89 425	10	37 36			•				
9.79 335	16	9.89 931	26	0.10 069	9.89 405	10	35	Ι.	-6.1					
9.79 351	16 16	9.89 957	26 26	0.10043	9.89 395	10	34	.1	1.6	1.5				
9.79 367	16	9.89 983	26	0.10017	9.89 385	10	33	.2	3.2	3.0				
9 · 79 383   9 · 79 399	16	9.90 009	26	0.09 991	9.89 37 <b>5</b> 9.89 364	11	32 31	.3	4.8	4.5				
9.79 415	16	9.90 061	26	0.09 939	9.89 354	10	80	.4	8.0	6.0 7.5				
9.79 431	16	9.90 086	25 26	0.09 914	9.89 344	10	29	.5 .6	9.6	9.0				
9·79 447   0·70 463	16	9.90 112	26	0.09 888	9.89 334 9.89 324	10	28 27	·7	11.2	10.5				
9.79 463 9.79 478	15 16	9.90 164	26	0.09 836	9.89 314	10	26	.9	14.4					
9.79 494	16	9.90 190	26	0.09 810	9.89 304	10	25			5 5				
9.79 510	16	9.90 216	26	0.09 784	9.89 294 9.89 284	10	24	1						
9.79 526	16		26			10	23			1 . I				
9.79 558		9.90 294		0.09 706	9.89 264	10	21			.2				
9.79 573		9.90 320		0.09 680	9.89 254	1			.3 3	.3				
9.79 589	16		25			11				.4				
9.79 621	16	9.90 397	26	0.09 603	9.89 223	10	17	l	.6 6.	.6				
9.79 636		9.90 423	1	0.09 577			I		.7 7	·7 .8				
9.79 652	16		26	0.09 551		10				.9				
	16		26			10		1	.21 2	.,				
9.79 699		9.90 527		0.09 473	9.89 173	10	12	١.						
9.79 715	16		25			10	1	١.		9 0.9				
	15		26		0.	10		.2		1.8				
9.79 762	16	9.90 630	26	0.09 370	9.89 132	10	8	.3	3.0	2.7 3.6				
9.79 778		9.90 656		0.09 344	9.89 122		7	.4	4.0	3.6				
9 79 793	16		26			11		6.	6.0	4·5 5·4 6·3 7·2 8·1				
9.79 825	16		26			10	4	.7	7.0	6 3				
9.79 840	15		25	0.09 241	9.89 081	10	3		0.0	7.2 8.1				
9.79 856	16	9.90 785	26			11		الو.	۶۰۰۱					
	15		26			10								
	-		a 4			<u>a</u>		D	ron. E	rts-				
L. U08.	u.	L. Cotg.	ic. a.		п. эш.	u.	<u>'                                    </u>		rope r					
	9. 79 542 9. 79 558 9. 79 578 9. 79 589 9. 79 685 9. 79 621 9. 79 636 9. 79 652 9. 79 684 9. 79 684 9. 79 684 9. 79 775 9. 79 746 9. 79 778 9. 79 778 9. 79 778 9. 79 793 9. 79 798 9. 79 798 9. 79 798 9. 79 798 9. 79 798 9. 79 809 9. 79 809	2. 79 542 16 2. 79 558 15 2. 79 573 16 2. 79 605 16 2. 79 605 16 2. 79 636 16 2. 79 636 16 2. 79 668 16 2. 79 668 16 2. 79 668 16 2. 79 699 15 2. 79 775 16 2. 79 775 16 2. 79 776 16 2. 79 776 16 2. 79 7778 16 2. 79 778 16 2. 79 778 16 2. 79 780 16 2. 79 79 80 16 2. 79 80 16 2. 79 80 16 2. 79 88 16 2. 79 8 16 2. 79 8 16 2. 79 8 16 2. 79 7 7 8 16 2. 79 7 8 16 2. 70	0.79 542	0.79 542       16       9.90 268       26         9.79 573       16       9.90 320       26         9.79 589       16       9.90 346       26         9.79 605       16       9.90 371       25         9.79 636       16       9.90 397       26         9.79 636       16       9.90 423       26         9.79 668       16       9.90 442       26         9.79 668       16       9.90 475       26         9.79 679       15       9.90 551       26         9.79 7715       16       9.90 553       25         9.79 776       16       9.90 553       25         9.79 776       16       9.90 578       26         9.79 776       16       9.90 604       26         9.79 778       16       9.90 634       26         9.79 778       16       9.90 634       26         9.79 780       16       9.90 634       26         9.79 781       15       9.90 632       26         9.79 809       16       9.90 682       26         9.79 856       16       9.90 734       25         9.79 872       16       9.90 785	0.79 542         16         9.90 268         26         0.09 732           2.79 558         16         9.90 294         26         0.09 766           2.79 573         16         9.90 320         26         0.09 680           9.79 605         16         9.90 371         25         0.09 629           9.79 636         16         9.90 423         26         0.09 603           9.79 668         16         9.90 475         26         0.09 571           9.79 668         16         9.90 475         26         0.09 551           9.79 699         16         9.90 571         26         0.09 551           9.79 715         16         9.90 557         26         0.09 473           9.79 7715         16         9.90 557         26         0.09 473           9.79 7761         15         9.90 557         26         0.09 499           9.79 776         16         9.90 557         26         0.09 473           9.79 778         15         9.90 557         26         0.09 370           9.79 779         16         9.90 650         26         0.09 370           9.79 79762         16         9.90 656         26         0.09 384<	0.79 542         16         9.90 268         26         0.09 732         9.89 274           0.79 573         16         9.90 320         26         0.09 766         9.89 264           0.79 589         16         9.90 346         26         0.09 680         9.89 254           0.79 605         16         9.90 371         25         0.09 629         9.89 233           0.79 636         16         9.90 423         26         0.09 603         9.89 223           0.79 652         16         9.90 447         26         0.09 557         9.89 223           0.79 668         16         9.90 475         26         0.09 557         9.89 203           0.79 699         16         9.90 557         26         0.09 473         9.89 173           0.79 79 699         16         9.90 557         26         0.09 473         9.89 173           0.79 7715         16         9.90 5573         26         0.09 473         9.89 162           0.79 776         15         9.90 5578         26         0.09 473         9.89 152           0.79 776         16         9.90 565         26         0.09 370         9.89 152           0.79 762         16         9.90 656	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.79 542         16         9.90 268         26         0.09 732         9.89 274         10         22           0.79 573         16         9.90 294         26         0.09 766         9.89 264         10         21           0.79 573         16         9.90 320         26         0.09 680         9.89 234         10         12           0.79 605         16         9.90 371         26         0.09 629         9.89 233         11         18           0.79 636         16         9.90 397         26         0.09 677         9.89 213         10         17           0.79 636         16         9.90 442         26         0.09 577         9.89 213         10         17           0.79 668         16         9.90 449         26         0.09 577         9.89 213         10         17           0.79 668         16         9.90 449         26         0.09 577         9.89 103         10         15           0.79 699         16         9.90 557         26         0.09 473         9.89 173         11         13           0.79 775         16         9.90 578         25         0.09 447         9.89 152         10           0.79 762	9.79 542 16 9.90 268 26 0.09 706 9.89 274 10 22 1	0.79 542				

					39°				
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.79 887	16	9.90 837 9.90 863	26	0.09 163	9.89 050	10	60	
1 2	9.79 903 9.79 918	15	9.90 889	26	0.09 137	9.89 040 9.89 030	10	59 58	
3	9.79 934	16	9.90 914	25 26	0.09 086	9.89 020	10	57	.1 2.6
4	9.79 950	15	9.90 940	26	0.09 060	9.89 009	10	56	.2 5.2
5	9.79 981	16	9.90 992	26	0.09 008	9.88 989	10	55 54	
7 8	9.79 996	16	9.91 018	26	0.08 982	9.88 978	11	53	.5 13.0
9	9.80 012 9.80 027	15	9.91 043 9.91 069	26	0.08 957 0.08 931	9.88 968 9.88 958	10	52 51	.6 15.6 .7 18.2
10	9.80 043	16	9.91 095	26 26	0.08 003	9.88 948	10	50	.7 18.2 .8 20.8
11	9.80 058	16	9.91 121	26	0.08 879	9.88 937	11	49 48	.9 23.4
12	9.80 074 9.80 089	15	9.91 147 9.91 172	25	o.o8 853 o.o8 828	9.88 927	10	47	
14	9.80 105	15	9.91 198	26 26	0.08 802	9.88 906	11	46	25
15 16	9.80 120 9.80 136	16	9.91 224 9.91 230	26	0.08 776 0.08 750	9.88 896 9.88 886	10	45	.1 2.5
	9.80 151	15	9.91 276	26	0.08 724	9.88 875	11	44 43	-3 7-5
17	9.80 166	16	9.91 301	25 26	0.08 699	9.88 865	10	42	.4 10.0 .5 12.5
19 20	9.80 182	15	9.91 327	26	0.08 673	9.88 855	11	$\frac{41}{40}$	.6 15.0
21	9.80 213	16	9.91 379	26	0.08 621	9.88 834	10		.7 17.5
22	9.80 228	16	9.91 404 9.91 430	25 26	0.08 596	9.88 824 9.88 813	10	39 38	.8 20.0 9 22.5
23 24	9.80 244	15	9.91 456	26	0.08 544	9.88 803	10	37 36	
25	9.80 274	15	9.91 482	26	0.08 518	9.88 793	10	35	1 16
26	9.80 290 9.80 305	15	9.91 507 9.91 533	25 26	0.08 493	9.88 782	11	34	.1 1.6
27 28	9.80 320	15	9.91 559	26	0.08 441	9.88 761	11	33 32	.2 3.2
29	9.86 336	15	9.91 585	26 25	0.08 415	9.88 751	10	31	.3 4.8
30	9.80 351 9.80 366	15	9.91 610 9.91 636	26	0.08 390	9.88 741 9.88 730	11	30	.5 8.0
31 32	9.80 382	16	9.91 662	26 26	0.08 338	9.88 720	10	29 28	6 9.6
33	9.80 397	15	9.91 688	25	0.08 312	9.88 709	11	27	8 12.8
34	9.80 412	16	9.91 713	26	0.08 261	9.88 699	11	25	.9 14.4
35 36	9.80 443	15	9.91 763	26 26	0.08 235	9.88 678	10	24	
37 38	9.80 458	15	9 91 791	25	0.08 209	9.88 668 9.88 657	10	23	15
39	9.80 4/3	16	9 91 842	26	0.08 158	9.88 647	10	21	.1 1.5
40	9.80 504	15	9 91 868	26 25	0.08 132	9.88 636	11	20	3 4.5
4I 42	9.80 519   9.80 534	15	9 91 893	26	0.08 107	9.88 626 9 88 615	11	18	.4 60
43	9 80 550	16 15	9.91 945	26 26	0.08 055	9.88 605	10	17	.5 7.5 .6 9.0
44	9.80 565	15	9.91 971	25	0.08 029	9.88 594	11	16	7 10.5
45 46	9.80 580 9 80 595	15	9.91 996 9.92 022	26	0.08 004	9 88 584 9 88 573	11	15 14	.8 12.0 .9 13.5
47	9 80 610	15 15	9.92 048	26 25	0 07 952	9.88 563	10	13	
48	9 80 625 9 80 641	16	9.92 073	26	0.07 927	9.88 552 9.88 542	10	12 11	1 11 1 10
50	9.80 656	15	9.92 125	26	0.07 875	9.88 531	11	10	.1 1.1 1.0
51	9.80 671	15	9.92 150	25 26	0.07 850	9.88 521	10	9	.2 2.2 2.0
52 53	9.80 686 9.80 701	15	9.92 176	26	0.07 824	9.88 510	11	8	.3 3.3 3.0 .4 4.4 4.0
54	9.80 716	15	9.92 227	25 26	0.07 773	9.88 489	10	76	.3 3.3 3.0 .4 4.4 4.0 .5 5.5 5.0 .6 6.6 6.0
55 56	9.80 731	15	9.92 253	26	0.07 747	9 88 478 9 88 468	10	5	7 7.7 7.0
50	9 80 746 9 80 762	16	9.92 279 9.92 304	25	0.07 721	9.88 457	11	5 4 3 2	.7 7.7 7.0 .8 8.8 8.0
57 58	9.80 777	15	9.92 330	26 26	0.07 670	9.88 447	10		.9 9.9 9.0
<u>59</u> 60	9.80 792	15	9.92 356 9.92 3SI	25	0.07 644	9.88 436	11	<u> </u>	
-00				0 4				-	Drop Dto
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.		Prop. Pts.

					40°						
1	L. Sin.	d.		c. d.	L. Cotg.	L. Cos.	d.		Pr	op. P	ts.
0	9.80 807 9.80 822	15	9.92 381	26	0.07 619	9.88 42 <u>5</u> 9.88 41 <u>5</u>	10	60			
1 2	9.80 837	15	9.92 407 9.92 433	26	0.07 593	9.88 404	11	59 58		1 26	
3	9.80 852	15	9.92 433 9.92 458	25 26	0.07 542	9.88 394	11	57 56		1	
4	9.80 867	15	9.92 484	26	0.07 516	9.88 383	11	50			2
5 6	9.80 897	15	9.92 535	25	0.07 465	9.88 362	10	55 54			
8	9.80 912	15	9.92 561	26 26	0.07 439	9.88 351	11	53		5 13.	o
9	9.80 927	15	9.92 587 9.92 612	25	0.07 413 0.07 388	9.88 340 9.88 330	10	52 51		6 15. 7 18.	6
10	9.80 957	15	9.92 638	26	0.07 362	9.88 319	11	$\overline{50}$	:	8 20.	.8
II		15 15	9.92 663	25 26	0.07 337	9.88 308 9.88 298	10	49 48	• 9	9   23	4
12	9.80 987 9.81 002	15	9.92 689	26	0.07 311	9.88 287	11	40			
14	9.81 017	15	9.92 740	25 26	0.07 260	9.88 276	11	46		25	
15 16	9.81 032	15	9.92 766	26	0.07 234	9.88 266 9.88 253	11	45	:	2 5	.5
17	9.81 047 9.81 061	14	9.92 792 9.92 817	25	0.07 208	9.88 244	11	44 43		3 7	.5
17 18	9.81 076	15	9.92 843	26 25	0.07 157	9.88 234	10	42		4 IO.	
19	9.81 091	15	9.92 868	26	0.07 132	9.88 223	11	$\frac{41}{40}$		6 15	
20	9.81 100	15	9.92 894	26	0.07 106	9.88 201	11			7 17 20	
22	9.81 136	15	9.92 945	25 26	0.07 055	9.88 191	10	39 38		9 22	
23 24	9.81 151	15	9.92 971 9.92 996	25	0.07 029	9.88 180 9.88 169	11	37 36			
		14	9.93 022	26	0.06 978	9.88 158	11	35		[ 25	
25 26	9.81 195	15	9.93 048	26	0.06 952	9.88 148	10	34			.5
27	9.81 210	15	9.93 073 9.93 099	26	0.06 927	9.88 137 9.88 126	11	33 32		2 3	.0
29	9.81 240	15	9.93 124	25 26	0.06 876	9.88 115	11	31		3 4	·5 .o
30	9.81 254	15	9.93 150	25	0.06 850	9.88 105	11	30		5 7	.5
31	9.81 269	15	9.93 175 9.93 201	26	0.06 825	9.88 o94 9.88 o83	11	29 28		6 9 7 10	.0
33	9.81 299	15	9.93 227	26	0.06 773	9.88 072	11	27		7 10 8 12	
34	9.81 314	14	9.93 252	25	0.06 748	9.88 061	10	26		9 13	.5
35 36	9.81 328 9.81 343	15	9.93 278 9.93 303	25	0.06 722	9.88 051 9.88 040	11	25 24			
37	9.81 358	15	9.93 329	26	0.06 671	9.88 029	11	23		1 2	4
38	9.81 372 9.81 387	15	9.93 354	25 26	0.06 646	9.88 018	11	22 21		1 1	.4
40	9.81 402	15	9.93 380	26	0.06 594	9.87 996	11	$\frac{20}{20}$			.8 .2
41	9.81 417	15	9.93 431	25 26	0.06 569	9.87 985	11	19		4 5	.6
42	9.81 <b>431</b> 9.81 <b>44</b> 6	15	9.93 457 9.93 482	25	0.06 543	9.87 975	11	18		5 7	.4
44	9.81 461	15	9.93 508	26	0.06 492	9.87 953	11	16		7 9	.8
45	0.81 475	15	9.93 533	25	0.06 467	9.87 942	111	15		8 11 9 12	
46	9.81 490	15	9.93 559	25	0.06 441	9.87 931 9.87 920	11	14 13		9  12	.0
47	9.81 519	14	9.93 584 9.93 610	26	0.06 390	9.87 909	11	12			
49 50	9 81 534	15	9.93 636	26	0.06 364	9.87 898	11	10		I.I	10 1.0
51	9.81 549	14	9.93 661 9.93 687	26	0.06 339	9.87 877	10		. I . 2	2.2	2.0
52	9.81 578	15	9.93 712	25 26	0.06 288	9.87 877	11	8	.3	3.3	3.0
53 54	9.81 592	15	9.93.738 9.93.763	25	0.06 262	9.87 85 <del>5</del> 9.87 844	11	7 6	.4	4·4 5·5 6.6	4.0 5.0 6.0
		15	9.93 789	26	0.06 211	9.87 833	11		.4	6.6	6.0
56	9.81 636	14	9.93 814	25 26	0.06 186	9.87 822	11	5 4 3 2	·7	7.7 8.8 9.9	7.0 8.0
57	9.81 651	14	9.93 840 9.93 865	25	0.06 160	9.87811	11	3 2	.9	9.9	9.0
55 56 57 58 59	9.81 680	15	9.93 891	26	0.06 109	9.87 789	11	ı			
60	9.81 694		9.93 916	25	0.06 084	9.87 778		0			
-	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Pı	op. I	ets.

					41°				
,	L. Sin.	d.	L. Tang.	c.d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.81 694	15	9.93 916	26	0.06 084	9.87 778	11	60	
1 2	9.81 709 9.81 723	14	9.93 942 9.93 967	25	0.06 058	9.87 767 9.87 756	11	59 58	
2 4	9.81 738	15	9.93 993	25	0.06 007	9.87 745	11	57	.I 2.6
4	9.81 752	15	9.94 018	26	0.05 982	9.87 734	11	56	.2 5.2
5	9.81 781	14	9.94 044 9.94 069	25 26	0.05 955	9.87 723 9 87 712	11	55 54	.3 7.8
7 8	9 81 796	14	9.94 095	25	0.05 905	9.87 701	11	53	.4 IO.4 .5 I3.0
8 9	9.81 810	15	9.94 120	26	0.05 880	9.87 690 9.87 679	11	52	.6 15.6
10	9.81 839	14	9.94 171	25	0.05 829	9.87 668	11	$\frac{51}{50}$	.7 18.2 .8 20.8
11	9.81 854	14	9.94 197	25	0.05 803	9.87657	11	49 48	.9 23.4
12 13	9.81 868 9.81 882	14	9.94 222 9.94 248	26	0.05 778	9.87 646 9.87 63 <b>3</b>	11	48	
14	9.81 897	15	9.94 273	25 26	0.05 727	9.87 624	11	46	25
15	9.81-911	15	9.94 299	25	0.05 701	9.87 613	12	45.	.1 2.5 .2 5.0
17	9.81 920	14	9.94 324 9.94 350	26	0.05 676	9.87 601 9.87 590	11	44 43.	3 7.5
18	9.81 955	15	9.94 375	25 26	0.05 625	9.87 579	11	42	.4 10.0
20	9.81 969	14	9.94 401	25	0.05 599	9.87 568	38	41	.5 12.5 .6 15.0
21	9.81 998	15	9.94 426	26	0.05 574	9.87 557 9.87 546	11	40	.7 17.5
22	9 82 012	,14 14	9.94 477	25 26	0.05 523	9.87 535	11	39 38	.8 20.0 .9 22.5
23	9.82 026 9.82 041	15	9.94 503 9.94 528	25	0.05 497	9.87 524 9.87 513	11	37 36	31
25	9.82 055	14	9.94 554	26	0.05 446	9.87 501	12	35	
26	9.82 069	14	9.94 579	25 25	0.05 421	9.87 490	11	34 -	1 1.5
27	9 82 084 9 82 098	14	9.94 604	26	0.05 396	9.87 479 9.87 468	11	33	.2 3.0
29	9.82 112	14 14	9.94 655	25 26	0.05 345	9 87 457	11	31	·3 4·5 ·4 6.0
30	9.82 126	15	9.94 681	25	0.05 319	9.87 446	12	30	-5 7.5
31 32	9.82 141 9.82 155	14	9.94 706	26	0.05 294	9.87 434 9.87 423	11	29 28	
33	9.82 169	14	9.94 757	25 26	0.05 243	9.87 412	11	27	.8 12.0
34	9.82 184	14	9.94 783	25	0.05 217	9.87 401	11	26	.9 13.5
35 36	9.82 198	<b>24</b>	9.94 808	26	0.05 192	9.87 390 9.87 378	12	25 24	1-
37 38	9.82 226	14 14	9.94 859	25 25	0.05 141	9 87 367	11	23.	1 24
38	9.82 240 9.82 255	15	9.94 884	26	0.05 116	9 87 356 9 87 345	11	22	.I I.4 .2 2.8
40	9.82 269	14	9.94 935	25	0.05 065	9 87 334	11	20	.2 2.8
41	9.82 283	14 14	9.94 961	26 25	0.05 039	9.87 322	11	19	.4 5.6
42 43	9.82 297 9.82 311	14	9.94 986 9.95 012	26	0.05 014	9 87 311	11	18	.5 7.0 .6 8.4
44	9.82 326	15 14	9.95 037	25 25	0.04 963	9.87 288	12	16	.7 9.8
45 46	9.82 340	14	9 95 062	26	0.04 938	9 87 277	11	15	.8 11.2 .9 12.6
40	9.82 354 9.82 368	14	9.95 088	25	0.04 912	9.87.266. 9.87.25 <del>5</del>	11	14	.9  12.0
47 48	9 82 382	14 14	9.95 139	26 25	0.04 861	9 87 243	11	12	
50	9.82 396	14	9.95 164	26	0.04 836	9.87 232	11	10	.1 1.2 1.1
51	9 82 424	14	9.95 190	25	0.04 810	9.87 209	13	9	.2 2.4 2.2
52	9.82 439	15	9.95 240	25 26	0.04 760	9.87 198	11	8	
53 54	9.82 453 9.82 467	14	9.95 266 9.95 291	25	0.04 734	9.87 187	12	7 6	.3 3 6 3.3 .4 4 8 4.4 .5 6 0 5 5
55	9.82 481	14	9.95 317	26	0.04 683	9.87 164	11	5 4	3 3 6 3 3 4 8 4 4 4 5 6 0 5 5 6 7 2 6 6 6 7 8 4 7 7 7 8 9 6 8 8 8 9 9 10 8 9 9
55 56 57 58 59	9.82 495	24 24	9.95 342	25 26	0.04 658	9.87 153	11	4	8 9 6 8.8
58	9.82 509 9.82 523	24	9.95 368 9.95 393	25	0.04 632	9.87 141	11	3 2	.9 10.8 9.9
59	9.82 537	14 14	9.95 418	25 26	0.04 582	9.87 119	11	1	
60	9.82 551		9.95 444		0.04 556	9.87 107		0	
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.
					48°				

					42°				
,	L. Sin.	d.	L. Tang.	c.d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.82 551	14	9.95 444	25	0.04 556	9.87 107	11	60	
I 2	9.82 565 9.82 579	14	9 95 46 <u>9</u> 9 95 495	26	0.04 531 0.04 505	9.87 096 9.87 083	11	59 58	
3	9.82 593	14	9.95 520	25 25	0.04 480	9.87 073	12	57	.1 2.6
4	9.82 607	24	9.95 545	26	0.04 455	9.87 062	12	_56	.2 5.2
5 6	9.82 621 9.82 635	14	9.95 571 9.95 596	25	0.04 429	9.87 050 9.87 039	11	55 54	.3 7.8
7 8	9.82 649	14 14	9.95 622	26 25	0.04 378	9.87 528	11	53 52	.4 10.4 .5 13.0
8 9	9.82 663 9.82 677	14	9.95 647 9.95 672	25	0.04 353 0.04 328	9.87 016 9.87 00 <del>5</del>	11	52 51	.6 15.6
10	9.82 691	24	9.95 698	26	0.04 302	9.86 993	12	50	.7 18.2 .8 20.8
II	9.82 703	14	9.95 723	25 25	0.04 277	9.86 982	11	49 48	.9 23.4
12	9.82 719 9.82 733	14	9.95 748 9.95 774	26	0.04 252	9.86 970 9.86 959	11	48	
14	9.82 747	14 14	9.95 799	25 26	0.04 201	9.86 947	12	47 46	25
15 16	9.82 761	14	9.95 825	25	0.04 175	9.86 936	12	45	.1 2.5
	9.82 77 <del>5</del> 9.82 788	13	9.95 850 9.95 875	25	0.04 150	9.86 924 9.86 913	11	44	.2 5.0 .3 7.5
17	9.82 802	14	9.95 901	26	0.04 099	9.86 902	11	43 42	.4 10.0
19	9.82 816	14	9.95 926	25 26	0.04 074	9.86 890	11	41	.5 12.5 .6 15.0
20	9.82 830 9.82 844	14	9.95 952 9.95 977	25	0.04 048	9.86 879 9.86 867	13	40	·7 17.5
22	9.82 858	14 14	9.96 002	25	0.03 998	9.86 855	12	39 38	.8 20 0 .9 22.5
.23	9.82 872 9.82 885	13	9.96 028	96 25	0.03 972	9.86 844 9.86 832	13	37	.91 22.3
24	9.82 899	14	9.96 053	25	0.03 947	9.86 821	11	36 35	
26	9.82 913	14	9.96 104	26	0.03 896	9.86 809	12	34	.I I.4
27 28	9.82 927	14	9.96 129	25 26	0.03 871	9.86 798	12	33	.I I.4 .2 2.8
28 29	9.82 941 9.82 95 <del>5</del>	14	9.96 15 <del>5</del> 9:96 180	25	0.03 845	9.86 786 9.86 775	11	32 31	.3 4.2
30	9.82 968	13	9.96 205	25 26	0.03 795	9.86 763	12	30	.4 5.6 .5 7.0
31	9.82 982 9.82 996	14	9.96 231 9.96 256	25	0.03 769	9.86 752 9.86 740	12	29 28	.5 7.0 .6 8.4 .7 9.8
32 33	9.83 010	14	9.96 281	25	0.03 744	9.86 728	12	20 27	.7 9.8 .8 11.2
34	9.83 023	13	9.96 307	26 25	0.03 693	9.86 717	11	26	.9 12.6
35 36	9.83 037	14	9.96 332	25	0.03 668	9 86 705 9 86 694	11	`25	
30	9.83 o51 9.83 o63	14	9.96 357 9.96 383	26	0.03 643	9.86 682	12	24 23	13
37 38	9.83 078	13	9.96 408	25 25	0.03 592	9.86 670	12	22	
$\frac{39}{40}$	9.83 092	14	9.96 433	26	c 03 567	9.86 659	12	$\frac{21}{20}$	.2 2.6
41	9.83 120	14	9.96 484	25	0.03 541	9.86 635	12	19	•3 3 9 •4 5.2 •5 6.5 .6 7.8
42	9.83 133	13	9.96 510	26 25	0.03 490	9 86 624	11	18	.5 6.5 .6 7.8
43	9.83 147 9.83 161	14	9.96 53 <del>5</del> 9.96 560	25	0.03 465	9.86 600	12	17 16	.6 7.8 .7 9.1
45	9.83 174	13	9.96 586	26	0.03 414	9.86 589	11	15	.8 10.4
40	9.83 188	14	9.96 611	25 25	0.03 389	9.86 577	12	14	.9 11.7
47 48	9.83 202 9.83 215	13	9.96 636 9.96 662	26	0.03 364	9.86 565 9.86 554	11	13 12	
49	9.83 229	14	9.96 687	25 25	0.03 313	9.86 542	12	11	12 11
50	9.83 242	14	9.96 712	26	0.03 288	9.86 530	12	10	.1 1.2 1.1
51	9.83 250 9.83 270	14	9.96 738	25	0.03 262	9.86 518 9.86 507	11	9 8	3 3.6 3.3
52 53 54	9.83 283	13	9.96 788	25 26	0.03 212	9.86 495	12	7 6	.2 2.4 2.2 .3 3.6 3.3 .4 4.8 4.4 .5 6.0 5.5
54	9.83 297	13	9.96 814	25	0.03 186	9.86 483	11		3.6 3.3 .4 4.8 4.4 .5 6.0 5.5 .6 7.2 6.6
55 56 57 58 59	9.83 310	14	9.96 839 9.96 864	25	0.03 161	9.86 472 9.86 460	12	5 4 3 2	.6 7.2 6.6 .7 8.4 7.7 .8 9.6 8.8 .9 10.8 9.9
57	9.83 324 9.83 338	14	9.96 890	26	0.03 110	9.86 448	12	3	.8 9.6 8.8 .9 10.8 9.9
58	9.83 351 9.83 36 <del>5</del>	14	9.96 913	25 25	0.03 085	9.86 436 9.86 42 <del>5</del>	11	2 I	.9  10.0  9.9
60	9.83 378	13	9.96 966	26	0.03 034	9.86 413	12	0	
	L. Cos.	d.		c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.
1	20031	1 410	Lat Corg.	los de	47°	1 are witte			

					43°				73
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.83 378	14	9.96 966	25	0.03 034	9.86 413	12	60	
I 2	9.83 392 9.83 405	13	9.96 991 9.97 016	25	0.03 009	9.86 401 9.86 389	12	59 58	
3 4	9.83 419	14	9.97 042	26 25	0.02 958	9.86 377	12	57	.I 2.6
4	9.83 432	14	9.97 067	25	0.02 933	9.86 366	12	56	.2 5.2
5	9.83 446 9.83 459	13	9.97 092 9.97 118	26	0.02 882	9.86 354 9.86 342	12	55 54	.3 7.8
7 8	9.83 473	14	9.97 143	25	0.02 857	9.86 330	12	53	4 10.4 5 13.0 .6 15.6
9	9.83 486 9.83 500	14	9.97 168 9.97 193	25	0.02 832	9.86 318 9.86 306	12	52	.6 15.6
10	9.83 513	13	9.97 219	26	0.02 781	9.86 295	11	51 50	.7 18.2 .8 20.8
11	9.83 527	14	9.97 244	25 25	0.02 756	9.86 283	12	49 48	.9 23.4
13	9.83 540 9.83 554	14	9.97 269	26	0.02 73I 0.02 705	9.86 271 9.86 259	12	48	
14	9.83 567	13	9.97 320	25 25	0.02 680	9.86 247	12	47 46	25
15 16	9.83 581	13	9.97 345	26	0.02 655	9.86 235	12	45	.1 2.5
	9.83 594 9.83 608	14	9.97 371 9.97 396	25	0.02 629	9.86 223 9.86 211	12	44	.2 5.0 .3 7.5
17	9.83 621	13	9.97 421	25 26	0.02 579	9.86 200	11	43 42	.4 10.0
19	9.83 634	14	9.97 447	25	0.02 553	9.86 188	12	41	.5 12.5 .6 15.0
20	9.83 648 9.83 661	13	9.97 472 9.97 497	25	0.02 528	9.86 176 9.86 164	12	40	.7 17.5
22	9.83 674	13	9.97 523	26 25	0.02 477	9.86 152	12	39 38	.8 20.0 .9 22.5
23	9.83 688	13	9.97 548	25	0.02 452	9.86 140	12	37 36	.91 22.3
24	9.83 701	14	9.97 573 9.97 598	25	0.02 427	9.86 128	12	30	•
26	9.83 728	13	9.97 624	26	0.02 376	9.86 104	12	35 34	.1 1.4
27 28	9.83 741	13	9.97 649	25 25	0.02 351	9.86 092	12	33	.2 2.8
29	9.83 75 <del>5</del> 9.83 768	13	9.97 674 9.97 700	26	0.02 326	9.86 o8o 9.86 o68	12	32 31	.3 4.2
30	9.83 781	13	9.97 725	25	0.02 275	9.86 056	12	30	.4 5.6
31	9.83 795	14	9:97 750	25 26	0.02 250	9.86 044	12	29 28	.5 7.0 .6 8.4 .7 9.8
32	9.83 808 9.83 821	13	9.97 776 9.97 801	25	0.02 224	9.86 032	12	20	.7 9.8 .8 11.2
34	9.83 834	13	9.97 826	25	0.02 174	9.86 008	12	26	.9 12.6
35 36	9.83 848	13	9.97 851	26	0.02 149	9.85 996	12	25	
37	9.83 861 9.83 874	13	9.97 877 9.97 902	25	0.02 098	9.85 984 9.85 972	12	24 23	1 13
37 38	9.83 887	13	9.97 927	25	0.02 073	9.85 960	12	22	.1 1.3
39	9.83 901	13	9.97 953	25	0.02 047	9.85 948	12	$\frac{21}{20}$	
41	9.83 914 9.83 927	13	9.97 978 9.98 ∞3	25	0.02 022	9.85 930	12	19	.3 3.9 .4 5.2
42	9.83 940	13	9.98 029	26 25	0.01 971	9.85 912	12	18	.4 5.2 .5 6.5 .6 7.8
43	9.83 954 9.83 967	13	9.98 054 9.98 079	25	0.01 946	9.85 900	12	17	.6 7.8 .7 9.1
	9.83 980	13	9.98 104	25	0.01 896	9.85 876	12	15	.8 10.4
45 46	9.83 993	13	0.08 130	26 25	0.01 870	9.85 864	12	14	.9 11.7
47	9.84 006	14	9.98 155 9.98 180	25	0.01 845	9.85 851	12	13	
49	9 84 033	13	9.98 206	26	0.01 794	9.85 827	12	11	12 11
50	9 84 046	13	9.98 231	25	0.01 769	9.85 815	12	10	.I I.2 I.I .2 2.4 2.2
51	9 84 059 9 84 072	13	9.98 256 9.98 281	25	0.01 744	9.85 803 9.85 791	12	8	3 3.6 3.3
51 52 53 54	9.84 085	13	0.08 307	26 25	0.01 693	9.85 791 9.85 779 9.85 766	12	8 7 6	.4 4.8 4.4
54	9.84 098	14	9.98 332	25	0.01 668	9.85 766	12		2 2.4 2.2 3 3.6 3.3 4 4.8 4.4 5 6.0 5.5 .6 7.2 6.6 .7 8.4 7.7 .8 9.6 8.8 .9 10.8 9.9
55 56 57 58 59	9.84 112 9.84 125	13	9.98 357 9.98 383 9.98 408	26	0.01 043	9.85 754 9.85 742 9.85 730 9.85 718	12	5 4 3 2	.7 8.4 7.7
57	9.84 138	13	9.98 408	25 25	0.01 592	9.85 730	12	3	.9 10.8 9.9
58	9.84 151	13	9.98 433 9.98 458	25	0.01 567	9.85 718	12	1	.9120.01 9.9
60	9.84 177	13	9.98 484	26	0.01 516	9.85 693	13	0	
-	L. Cos.	d.		c. d.	L. Tang.		d.	,	Prop. Pts.
-	, 134 00.18		, an outer		46°		-		

					44°				
1	L. Sin.	d.	L. Tang.	c. d.		L. Cos.	d.		Prop. Pts.
0	9.84 177 9.84 190	13	9.98 484 9.98 509	25	0.01 516	9.85 693 9.85 681	12	60	
2	9.84 203	13	9.98 534	25	0.01 466	9.85 669	12	59 58	
3	9.84 216	13	9.98 560	26	0.01 440	9.85 657	12	57	.1 2.6
4	9.84 229	13	9.98 585	25	0.01 415	9.85 645	13	56	.2 5.2
5 6	9.84 255	13	9.98 635	25	0.01 390	9.85 632 9.85 620	12	55	.3 7.8
7 8	9.84 269	14	9.98 661	26	0.01 339	9.85 608	12	54 53	.4 10.4
9	9.84 282 9.84 295	13	9.98 686 9.98 711	25	0.01 314	9.85 596	13	52	.6 15.6
10	9.84 308	13	9.98 737	26	0.01 263	9.85 583	12	51	.7 18.2 .8 20.8
11	9.84 321	13	9.98 762	25	0.01 238	9.85 559	12	<b>50</b> 49	.9 23.4
12	9.84 334 9.84 347	13	9.98 787	25 25	O.CI 213	9.85 547	12	48	1 71 311
14	9.84 360	13	9.98 812	26	0.01 188	9.85 534 9.85 522	12	47	1 25
15	9.84 373	13	9.98 863	25	O.OI 137	9.85 510	12	46	.1 2.5
16	9.84 385	13	9.98 888	25 25	0.01 112	9.85 497	13	44	.2 5.0
17	9.84 398	13	9.98 913	26	0.01 001	9.85 485	12	43	·3 7·5
19	9.84 424	13	9.98 964	25	0.01 036	9.85 460	13	42 41	.5 12,5
20	9.84 437	13	9.98 989	25 26	0.01 011	9.85 448	12	40	.6 15.0
2I 22	9.84 450 9.84 463	13	9.99 015	25	0.00 985	9.85 436 9.85 423	13	39 38	.7 17.5 .8 20.0
23	9.84 476	13	9.99 065	25	0.00 935	9.85 411	12	37	.9 22.5
24	9.84 489	13	9.99 090	25 26	0.00 910	9.85 399	12	36	
25 26	9.84 502 9.84 515	13	9.99 116	25	0.00 884	9.85 386	12	35	† 14
27	9.84 528	13	9.99 141	25	0.00 834	9.85 374 9.85 361	13	34 33	.1 1.4
28	9.84 540	12	9.99 191	25 26	0.00 809	9.85 349	12	32	.2 2.8
30	9.84 553	13	9.99 217	25	0.00 783	9.85 337	13	31	.4 5.6
31	9.84 579	13	9.99 242 9.99 267	25	0.00 758	9.85 324 9.85 312	12	30 29	.5  7.0
32	9 84 592	13	9.99 293	26 25	0.00 707	9.85 299	13	28	.6 8.4 .7 9.8
33 34	9.84 605 9.84 618	13	9.99 318	25	0.00 682	9.85 287	13	27 26	.8 11.2
35	9.84 630	12	9.99 343	25	0.00 632	9.85 274	12	25	.9 12.6
36	9.84 643	13	9.99 394	26 25	0.00 606	9.85 250	12	24	7 6
37 38	9.84 656	13	9.99 419	25	0.00 581	9.85 237	13	23	13
39	9.84 082	13	9.99 444 9.99 469	25	0.00 556	9.85 225	₽3	22 2I	.I I.3 .2 2.6
0.45	9.84 694	13	9.99 495	26	0.00 505	9.85 200	12	20	.2 2.6
40 41 42	9.84 707	13	9.99 520	25 25	0.00 480	9.85 187	13	19	.4 5.2
42	9.84 720	13	9.99 545 9.99 570	25	0.00 455	9.85 175	13	18 17	.4 5.2 .5 6.5 .6 7.8
44	9.84 745	12	9.99 596	26 25	0.00 404	9.85 150	12	16	.7 9.1
45	9.84 758	13	9.99 621	25 25	0.00 379	9.85 137	13	15	
46	9.84 77 <b>I</b>   9.84 784	13	9.99 646 9.99 672	26	0.00 354 0.00 328	9.85 125	13	14	.9  11.7
47 48	0.84 706	12	9.99 697	25	0.00 303	9.85 100	12	12	
49	9.84 809	13	9.99 722	25 25	0.00 278	9.85 087	13	11	12
50 51	9.84 822	13	9.99 747	26	0.00 253	9.85 074 9.85 062	12	10	.I I.2 .2 2.4
52	9.84 847	12	9.99 798	25	0.00 202	9.85 049	13	9 8	.3 3.6
52 53 54	9.84 860	13	9.99 773 9.99 798 9.99 823 9.99 848	25 25	0.00 177	9.85 037	12	7	.2 2.4 .3 3.6 .4 4.8 .5 6.0
55	9.84 885	12	9.99 874	26	0.00 152	9.85 024	12		.0 7.2
55 56 57 58 59	9.84 898	13	9.99 899	25	0.00 101	9.84 999	13	5	.7 8.4
57	9.84 911	13	9.99 924	25 25	0.00 076	9.84 986	13	3 2	.8 9.6 .9 10.8
50	9.84 923 9.84 936	13	9·99 949 9·99 975	26	0.00 051	9.84 974 9.84 961	13	2	.91 .0.0
60	9.84 949	13	0.00 000	25	0.00 000	9.84 949	12	0	
	L. Cos.	d.	L. Cotg.	c. d.		L. Sin.	d.	<del>,</del>	Prop. Pts.
	5000				45°			'	

TABLE V.

NATURAL

SINES AND COSINES.

ŕ			)°	1	•	<b>"</b> 2	0	3	0	4	0	
1												
ı	<u>'</u>	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine		N. sine		
I	0	.00000	1.00000	.01745	.99985	.03490	.99939	.25234	.99863	.06976	.99756	60
ı	1 2	.00029	I.00000	.01774	.99984 .99984	.03519	.99938	.05263	.99861 .99860	.07005	·99754	59 58
ı	3	.00087	1.00000	.01832	.99983	.03577	.99936	.05321	.99858	.07063	·99752 ·99750	57
ı		.00116	1.00000	.01862	.99983	.03606	.99935	.05350	.99857	.07092	.99748	57 56
1	4 5 6	.00145	1.00000	.01891	.99982	.03635	.99934	.05379	.99855	.07121	.99746	55
ı		.00175	1.00000	.01920	.99982	.03664	·99933	.05408	-99854	.07150	·99744	54
ı	8	.00204	1.00000	.01949	.99981	.03693	.99932	.05437	.99852	.07179	.99742	53
ı	9	.00233	1.00000	.01978	.99980	.03723 .037 <u>5</u> 2	.99931	.05466	.99851 .99849	.07208	.99740 .99738	52 51
ı	ıc	.00291	1.00000	.02036	.99979	.03781	.99929	.05524	.99847	.07266	.99736	50
ı	11	.00320	.99999	.02065	.99979	.03810	.99927	.05553	.99846	.07295	.99734	49
ı	12	.00349	•99999	.02094	.99978	.03839	.99926	.05582	-99844	.07324	.99731	49 48
ı	13	.00378	.99999	.02123	.99977	.03868	.99925	.05611	.99842	.07353	.99729	47
ı	14	.00407	•99999	.02152	·99977	.03897	.99924	.05640	.99841	.07382	.99727	46
ı	15 16	.00436	•99999 •99999	.02181	.99976 .99976	.03926	.99923	.05698	.99839 .99838	.07411	.99725 .99723	45 44
ı	17	.00495	.99999	.02240	.99975	.03984		.05727	.99836	.07469	.99721	43
	18	.00524	.99999	.02269	.99974	.04013	.99919	.05756	.99834	.07498	.99719	42
	19	.00553	.99998	.02298	.99974	.04042	.99918	.05785	.99833	.07527	.99716	41
ı	20	.00582	.99998	.02327	.99973	.04071	.99917	.05814	.99831	.07556	.99714	40
ı	2I 22	.00611	.99998	.02356	.99972	.04100	.99916	.05844	.99829	.07585	.99712	39 38
	23	.00669	.99998	.02303	.99971	.04129	.99913	.05902	.99827	.07614	.99710 . <b>9</b> 9708	27
ı	24	.00698	.99998	.02443	.99970	.04188	.99912	.05931	.99824	.07672	.99705	37 36
ı	25	.00727	-99997	.02472	.99969	.04217	.99911	.05960	.99822	.07701	.99703	35
1	26	.00756	.99997	.02501	.99969	.04246	.99910	.05989	.99821	.07730	.99701	34
ı	27 28	.00785	•99997	.02530	.99968	.04275	.99909	.06018	.99819	.07759	.99699	33
I		.00814	•99997	.02560	.99967	.04304	.99907	.06047	.99817	.07788	.99696	32
ı	29 30	.00873	.99996 .99996	.02589	.99966 .99966	.04333	.99906	.06105	.99813	.07817 .07846	.99694 .99692	31 30
ı	31	.00902	.99996	.02647	.99965	.04391	.99904	.06134	.99812	.07875	.99689	29
ı	32	.00931	.99996	.02676	.99964	.04420	.99902	.06163	.99810	.07904	.99687	28
1	33	.00960	.99995	.02705	.99963	.04449	.99901	.06192	.99808	.07933	.99685	27
ı	34	.00989	.99995	.02734	.99963	.04478	.99900	.06221	.99806	.07962	.99683	26
ı	35 36	.01018	•99995	.02763	.99962	.04507	.99898		.99804	.07991	.99680	25
1	30	.01047	-99995	.02792	.99961	.04536	.99897 .99896	.06279	.99803 .99801	.08020	.99678	24
ı	37 38	.01076	·99994 ·99994	.02821	.99960	.04565 .04594	.99894		.99799	.08049	.99676	23
ı	39	.01134	.99994	.02879	.99959	.04623	.99893		.99797	.08107	.99671	21
ı	40	.01164	.99993	.02908	.99958	.04653		.06395	-99795	.08136	.99668	20
ł	41	.01193	-99993	.02938	·99957	.04682	.99890	.06424	.99793	.08165	.99666	19
ı	42	.01222	-99993	.02967	.99956	.04711	.99889	.06453	.99792	.08194	.99664	18
J	43	.01251	.99992	.02996	-99955	.04740	.99888 .99886	.06482	.99790 .99788	.08223	.99661	17
	44 45	.01280	.99991	.03025	·99954 ·99953	.04769 .04798		.06540	.99786		.99659 .99657	15
	46	.01338		.03083	.99952	.04827			.99784	.08310	.99654	14
	47	.01367		.03112	.99952	.04856	.99882	.06598	.99782	.08339	.99652	13
I	48	.01396			-99951	.04885	.99881	.06627	.99780		.99649	12
	49	.01425			.99950			.06656	.99778	.08397	.99647	II
	50	.01454 .01483			.99949   . <b>9</b> 9948				.99776 .99774		.99644 .99642	10
	52	.01403		.03257	.99948		.99875	.06743	.99774		.99639	9
	53	.01542	.99988	.03286	.99946		.99873	.06773	.99770	.08513	.99637	7
	53 54	.01571	.99988	.03316	.99945	.05059	.99872	.06802	.99768	.08542	.99635	
	55 56	.01600	.99987	.03345	•99944		.99870		.99766		.99632	5
	56	.01629			.99943				.99764		.99630	4
	57 58	.01658 .01687			.99942 .99941				.99762	.08629 .08658	.99627 .99625	3 2
	59	.01037			.99941				.99758		.99622	ī
	60	.01745				.05234			.99756	.08716	.99619	0
	-							N cos		N. cos.	N cina	
1			N. sine			·				i		
	1	8	99°.	8	8°	8	7°	8	6°	8	5°	

	5	0	G	0	7	0	8	0	9	9° N. sine N. cos.	
,	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	-
0	.08716	.99619	.10453	.99452	.12187	.99255	.13917	.99027	.15643	.98769	60
1	.08745	.99617	.10482	.99449	.12216	.99251	.13946	.99023	.15672	.98764	59 58
2	.08774	.99614	.10511	.99446	.12245	.99248	.13975	.99019	.15701	.98760	58
3	.08831	.99612	.10540	·99443 ·99440	.12274	.99244	.14004	.99015	.15730	.98755	57
4 5	.08860	.99607	.10597	•99437	.12331	.99237		.99006	.15758	.9875 <b>1</b> .98746	56 55
5 6	.08889	.99604	.10626	.99434	.12360	.99233	.14090	.99002	.15816	.98741	54
	.08918	.99602	.10655	-99431	.12389	.99230	.14119	.98998	.15845	.98737	53
7 8	.08947	.99599	.10684	.99428	.12418	.99226		.98994	.15873	.98732	52
9	.08976	.99596	.10713	-99424	.12447	.99222	.14177	.98990	.15902	.98728	51
10	.09005	· <b>9</b> 9594	.10742	.99421	.12476		.14205	.98986	.15931	.98723	50
II	.09034	.99591	.10771	.99418	.12504	.99215	.14234	.98982	.15959	.98718	49 48
12	.09063	.99588	.10800	-99415	.12533	.99211	.14263	.98978	.15988	.98714	
13	.09092	.99586	.10829	.99412	.12562	.99208	.14292	.98973	.16017	.98709	47
14	.09121	.99583 .99580	.10887	.99409 .99406	.12591	.99204		.98969 .98965	.16046 .16074	.98704	46
15 16	.09179	.99578	.10016	.99402	.12649	.99197	.14349 .14378	.98961	.16103	.98700 .98695	45 44
17	.09208	.99575	.10945	.99399	.12678	.99193	.14407	.98957	.16132	.98690	43
18	.09237	.99572	.10973	.99396		. <b>9</b> 9189	.14436	.98953	16160	.98686	42
19	.09266	-99570	.11002	-99393	.12735	.99186	-14464	.98948	.16189	.98681	41
20	.09295	.99567	.11031	.99390	.12764	.99182	.14493	.98944		.98676	40
21	.09324	.99564		.99386	.12793	.99178	.14522	.98940	.16246	.98671	39
22	.09353	.99562	.11089	-99383	-12822	.99175	.14551	.98936	.16275	.98667	38
23	.09382	.99559	81111.	.99380	.12851	.99171	.14580	.98931		.98662	37
24	.09411	-99556	.11147	·99377	.12880	.99167	.14608	.98927		.98657	36
25	.09440	.99553	.11176	.99374	.12908	.99163	.14637	.98923	.16361	.98652	35
26	.09469	-99551	.11205	.99370	.12937	.99160	.14666 .14695	.98919		.98648	34
27	.09498	.99548	.11234	.99367 .99364	.12966	.99150	.14723	.98910		.98643 .98638	33
29	.09556	·99545 ·99542	.11203	.99360	.13024	.99148		.98906		.98633	32 31
30	.09585	.99540		-99357	.13053	.99144		.98902		.98629	30
31	.09614	-99537	.11349	-99354	.13081	-99141	.14810	.98897	.16533	.98624	29
32	.09642			.99351	.13110			.98893	.16562		28
33	.09671	.99531	.11407	.99347	.13139	.99133	.14867	.98889	.16591	.98614	27
34	.09700	.99528			.13168					.98609	26
34 35 36	.09729	.99526		.99341	.13197		.14925	.98880		.98604	25
30	.09758				.13226					.98600	24
37 38	.09787	.99520		.99334	.13254	.99118		.98871	.16706	.98595	23
38	.09816	1		.99331	.13283			98867	.16734 .16763	.98590	22 21
39	.09874		.11609		.13312				.16792		20
40 41	.09903		.11638					.98854			19
42	.09932				.13399	: 0				2000	18
43	.09961	.99503	.11696			.99094	.15155	.98845	.16878	.98565	17
44	.09990			.99310		.99091	.15184	.98841	.16906	.98561	16
45	.10019	.99497	.11754		.13485	.99087				.98556	15
46	.10048			.99303						.98551	14
47	.10077		.11812							.98546	
	.10106				.13572		.15299				12
49	.10135		.11869								11
50	.10164	.99482	.11898	.99286	.13629	.99063		.98809	.17107		
51 52	.10192	.99479	.11927	.99283	.13687	.99059					
53	.10250	.99473	.11985			.99055			.17164		7
53 54	.10279						.15471	.98796			7 6
55	.10308						.15500	.98791	.17222		5
56	.10337				.13802	.99043	.15529	.98787	.17250	.98501	5 4 3 2
57	.10366	.99461	.12100	.99265	.13831	.99039		.98782	.17279	.98496	3
58	.10395							.98778	.17308	.98491	
55 56 57 58 59 60	.10424		.12158						.17336		I
00	.10453				.13917						_
								1°	N. cos.	0°	
1	8	4°	8	3°	1 8	2°		1	8	U	

	1	0°	1	1° >	1	2°	1	3°	1	<b>4°</b>	
,	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	
0	.17365	.98481	.19081	.98163	.20791	.97815	.22495	-97437	.24192	.97030	60
1 2	.17393	.98476 .98471	.19109	.98157 .98152	.20820	.97809	.22523	.97430	.24220	.97023	59 58
3	.17451	.98466	.19167	.98146	.20877	.97797	.22580	·97424 ·97417	.24249 .24277	.97015 .97008	50
4	.17479	.98461	.19195	.98140	.20905	.97791	.22608	.97411	.24305	.97001	56
5	.17508	.98455	.19224	.98135	.20933	.97784	.22637	.97404	.24333	.96994	55
B	.17537	.98450	.19252	.98129	.20962	·97778	.22665	·97398	.24362	· <b>9</b> 6987	54
7 8	.17565	.98445 .98440	.19281	.98124 .98118	.20990	.97772 .97766	.22693	.97391	.24390	-96980	53
9	.17594 .17623	.98435	.19309	.98112	.21019	.97760	.22722	.97384 .97378	.24418 .24446	.96973 . <b>9</b> 6966	52 51
IÓ	.17651	.98430	.19366	.98107	.21076	.97754	.22778	.97371	.24474	.96959	50
II	.17680	.98425	.19395	.98101	.21104	.97748	.22807	.97365	.24503	.96952	49
12	.17708	.98420	.19423	.98096	.21132	.97742	.22835	97358	.24531	.96945	48
13	.17737 .17766	.98414 .98409	.19452 .19481	.98090 .98084	.21161	•97735	.22863	.97351	.24559	.96937	47
14	.17794	.98404	.19509	.98079	.21109	·97729 ·97723	.22920	·97345 ·97338	.24587	.96930	46 45
16	.17823	.98399	.19538	,98073	.21246	.97717	.22948	.97331	.24644	.96916	44
17 18	.17852	.98394	.19566	.98067	.21275	.97711	.22977	.97325	.24672	.96909	43
	.17880	.98389	.19595	.98061	.21303	.97705	.23005	.97318	.24700	.96902	42
19 20	.17909 .17937	.98383 .98378	.19623 .19652	.98056 .98050	.21331	.97698 .97692	.23033	.97311	.24728	.96894	4I
21	.17966	.98373	.19680	.98044	.21360	.97686	.23090	.97304 .97298	.24756 .24784	.96887 .96880	40
22	.17995	.98368	.19709	.98039	.21417	.97680	.23118	.97291	.24813	.96873	39 38
23	.18023	.98362	.19737	.98033	.21445	.97673	.23146	.97284	.24841	.96866	37
24	.18052	.98357	19766	.98027	.21474	.97667	.23175	.97278	.24869	.96858	36
25 26	.18081	.98352	.19794	.98021 .98016	.21502	.97661 .97655	.23203	.97271	.24897	.96851	35
	.18138	.98347 .98341	.19823	.98010	.21530	.97648	.23231	.97264 .97257	.24925	.96844 .96837	34 33
27 28	.18166	.98336	.19880	.98004	.21587	.97642	.23288	.97251	.24982	.96829	32
29	.18195	.98331	.19908	.97998	.21616	.97636	.23316	.97244	.25010	.96822	31
30	.18224	.98325	.19937	.97992	.21644	.97630	.23345	·97237	.25038	.96815	30
31	.18252 .18281	.98320	.19965	.97987	.21672	.97623 .97617	.23373	.97230	.25066	.96807	29 28
32 33	.18309	.98315 .98310	.19994	.97981 ·97975	.21701	.97611	.23401	.97223	.25094	.96800 .96793	27
34	.18338	.98304	.20051	.97969	.21758	.97604	.23458	.97210	.25151	.96786	26
35	.18367	.98299	.20079	.97963	.21786	.97598	.23486	.97203	.25179	.96778	25
36	.18395	.98294	.20108	.97958	.21814	.97592	.23514	.97196	.25207	.96771	24
37 38	.18424 .18452	.98288	.20136	.97952	.21843	.97585	.23542	.97189 .97182	.25235	.96764	23
39	18481	.98283 .98277	.20165	.97946 .97940	.21871	·97579 ·97573	.23571	.97176	.25263 .25291	.96 <u>7.5</u> 6 .96749	22 2I
40	.18509	.98272	.20222	.97934	.21928	.97566	.23627	.97169	.25320	.96742	20
41	.18538	.98267	.20250	.97928	,21956		.23656	.97162	.25348	.96734	19
42	.18567	.98261	.20279	.97922	.21985	·97553	.23684	.97155	.25376	.96727	18
43	.18595 .18624	.98256 .98250	.20307	.97916	.22013	·97547 ·97541	.23712	.97148 .97141	.25404	.95719	17
44	.18652	.98245	.20336 20364	.97910	.22041	.97534	.23769	.97134	.25432 .25460	.96712	15
45	.18681	.98240	.20393	.97899	.22098	.97528	.23797	.97127	.25488	.96697	14
47 48	.18710	.98234	.20421	.97893	.22126	.97521	.23825	.97120	.25516	.95690	13
	18738	.98229	.20450	.97887	.22155	.97515	.23853	.97113	.25545	.96682	12
49 50	. 18767 . 18795	.98223	.20478 .20507	.97881	.22183	.97508	.23882	.97106	.25573 .25601	.9667 .96667	11
51		.98212		.97869			.23938		.25629	1 ///	
52	.18852	.98207	.20563	.97863	.22268	.97489	.23966	.97086	.25657	.96653	8
53 54	.18881										7 6
54	.18910				.22325	.97476	.24023	.97072	.25713 -90038		
55 56 57 58	.18938 .18967			.97845 .97839				.97065 .970 <b>5</b> 8	.25741	.96630 .96623	5 4 3 2
57	.18995	.98179	.20706					.97051	.25798	.96615	3
58	.19024	.98174	.20734	.97827	.22438	-97450	.24136	.97044	.25826	.96608	2
59 60	.19052										0
-00	.19081				-		.24192				
		N. sine	I	1		1					,
	7	9°	7	8°	7	7°	7	6°	7	5°	

	1	5°	1	6°	1	7°	1	s°	1	9°	
,	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	
0	.25882	.96593	.27564	.96126	29237	.95630	.30902	.95106	.32557	-94552	60
1 2	.25910	.96585 .96578	.27592	.96118	.29265	.95622	.30929	.95097 .95088	.32584	·94542 ·94533	59 58
3	.25966	.96570	.27648	.96102	.29321	.95605	.30985	.95079	.32639	.94523	57
4 5 6	.25994	.96562 .96555	.27676	.96094 .96086	.29348	.95566 .95588	.31012	.950 <i>7</i> 0 .95061	.32667	.94514	56
6	.26050	.96547	.27731	.96078	.29404	.95579	.31068	.95052	.32694	·94504 ·94495	55 54
7 8	.26079	.96540	.27759	.96070	.29432	.95571	.31095	.95043	.32749	.94485	53
8 9	.26107 .26135	.96532	.27787	.96062	.29460	.95562 ·95554	.31123	.95033	·32777 ·32804	·94476 ·94466	52
10	.26163	.96517	.27843	.96046	.29515	.95545	.31178	.95015	.32832	.94457	51 50
11	.26191	.96509	.27871	.96037 .96029	.29543	.95536 .95528	.31206	.95006	.32859	.94447	49
13	.26247	.96494	.27927	.96021	.29571	.95519	.31233	<u>-94997</u> -94988	.32887	·94438 ·94428	48
14	.26275	.96486	.27955	.96013	.29626	.95511	.31289	.94979	.32942	.94418	46
15 16	.26303	.96479	.27983	.96005	.29654	.95502	.31316	.94970	.32969	.94409	45
	.26331	.96471	.28039	·95997 ·95989	.29682	·95493 ·95485	.31344	.94961 .94952	.32997 .33024	·94399 ·94390	44
17	.26387	.96456	.28067	.95981	.29737	.95476	.31399	.94943	.33051	.94380	42
19	.26415	.96448 .96440	.28095	.95972 .95964	.29765	.95467	.31427	.94933	.33079	.94370	41
2I	.26471	.96433	.28150	.95956	.29793	· <b>9</b> 5459 ·95450	.31454	·94924 ·94915	.33134	.94361 .94351	40 39
22	.26500	.96425	.28178	.95948	.29849	.95441	.31510	.94906	.33161	·943 <b>42</b>	38
24	.26528	.96417	.28206	.95940 .95931	.29876	·95433 ·95424	.31537	.94897 .94888	.33189 .33216	.94332	37 36
25	.26584	.96402	.28262	.95923	.29932	.95415	.31593	.94878	·332-14	.94313	35
26	.26012	.96394	.28290	.95915	.29960	.95407	.31620	.94859	.33271	.94303	34
27	.26640 .26668	.96386	.28318 .28346	.95907 .95898	.29987	.95398	.31648	.94860 .94851	.33298 .33326	.94 <b>2</b> 93 .94284	33 32
29	.26696	.96371	.28374	.95890	.30043	.95380	.31703	.94842	.33353	.94274	31
30	.26724	.96363	.28402	.95882	.30071	.95372	.31730	94832	.33381	.94264	30
3I 32	.26752 .26780	.96355	.23429	.95874 .95865	.30098 .30126	.95363 ·95354	.31758 .31786	.94823	.33408	94254	29 28
33	.26808	.96340	.28485	.95857	.30154	.95345	.31813	.94805	-33463		27
34	.26836 .26864		.28513	.95849 .95841	.30182	·95337 ·95328	.31841 .31868	·94795	.33490	.94225	26
35 36	.26892	.96324 .96316	.28569	.95832	.30209	.95319	.31896	.94786 -94777	.33518	.94215 .94206	25 24
	.26920	.96308	.28597	.95824	.30265	.95310	.31923	.94768	-33573	.94196	23
37 38	. <b>2</b> 6948 .26976	.96301	.28625	.95816	.30292	.95301	.31951	.94758 .94749	.33600	.94186 .94176	22 2I
39 40	.27004	.96285	.28680	.95799	.30348	.95284	.31979 .32006	.94749	.33655	.94167	20
41	.27032	.96277	.28708	.95791	.30376	.95275	.32034	.94730	.33682	.94157	19
$-\frac{42}{42}$	.27060	.96269	.28736	.95782 ·95774	.30403	.95266 ·95257	.32061	.94721	-33710 -33737	·94147	17
43	.27116	.96253	.28704	.95766	.30459	.95248	.32116	.94702	.33764	.94127	16
45	.27144	.96246	28820	.95757	.30486	.95240	.32144	.94693	.33792	.94118	15
46	.27172	.96238 .96230		·95749 ·95740	.30514	.95231	.32171	.94654 .94674	.33819 .33846	.94108	14
48	.27228	.96222	.28903	-95732	.30570	.95213	.32227	.94605	·33 <sup>8</sup> 74	.94088	12
49	.27256	.96214	.28931	.95724	.30597	.95204 .95195	.32254	.94656 .94646	.33901	.94078	II
50	.27284	.96206 .961 <b>9</b> 8		.95715	.30625	.95186	.32202		.33929 .33956		9
52 53	.27340	.96190	.29015	.95698	.30680	.95177	.32337	.94627	.33983	.94049	8
53	.27368 .27396	.96182 .96174		.95690	.30708 .30736	.95168	.32364			.94039	7 6
54 55 56 57 58 59 60	.27424			.95673	.30763	.95150			.34065		5
56	.27452	.96158	.29126	.95664	.30791	.95142	.32447	.94590	.34093	.94009	4
57	.27480 .27508			.95656	.30819 .30846		·32474 ·32502		.34120 .34147		3 2
59	.27536	.96134	.29209	.95639	.30874	.95115	.32529	.94561	.34175	.93979	I
60		.96126					·3 <sup>2</sup> 557	-94552	.34202	.93969	0
					N. cos.			1	N. cos.	!	,
	7	<b>4°</b>	7	3°	7	2°	7	1°	7	0°	

ð	0	1 20°				TAB	LE V.					
I		2	0°	2	1°	2	2°	2	3°	2	4°	
I	,	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	
1	-	.34202	.93969	·35 <sup>8</sup> 37	.93358	.37461	.92718	-39073	.92050	.40674	Orace	60
ı	1	.34229	.93959	.35864	.93348	.37488	.92707		.92039	.40700	.91355 .91343	
ı	2	.34257	.93949	.35891	.93337	.37515	.92697	.39127		.40727	.91331	<b>5</b> 9
ı	3	.34284	.93939	.35918	.93327	.37542	.92686	.39153	.92016	.40753	.91319	57
	4	.34311	.93929	•35945	.93316		.92675	.39180	.92005	.40780	.91307	56
П	5	·34339 ·34366	.93919	·35973 ·36000	.93306	·37595 ·37622	.92653	·39207 ·39234	.91994. .91982	.40806 .40833	.91295	55
1		34393	.93899	.36027	.93285	.37649	.92642	.39260	.91971	.40860	.91283	54
	7 8	.34421	.93889	.36054	.93274	.37676	.92631	.39287	.91959	.40886	.91272 .91260	53 52
ı	9	.34448	.93879	.36081	.93264	.37703	.92620	.39314	.91948	.40913	.91248	51
ı	10	·34475	.93869	36108	.93253	.37730	.92609	.39341	.91936	.40939	.91236	50
ı	11	.34503	.93859	.36135	.93243	.37757	.92598	.39367	.91925	.40966	.91224	49 48
ı	12	·3453°	.93849	.36162	.93232	·37784	.92587	·39394	.91914	.40992	.91212	-
ı	13 14	·34557 ·34584	.93839 .93829	.36190 .36217	.93222	.37811 .37838	.92576 . <b>92565</b>	.39421 .39448	.91902	.41019 .41045	.91200	47 46
H		.34612	.93819	.36244	.93201	.37865	.92554	.39474	.91879	.41043	.91188 .91176	45
H	15 16	.34639	.93809	.36271	.93190		.92543	.39501	.91868	.41098	.91164	44
I	17	.34666	.93799	.36298	.93180	.37919	.92532	.39528	.91856	.41125	.91152	43
1	18	.34694	.93789	.36325	.93169	-37946	.92521	·39555	.91845	.41151	.91140	42
I	19	.34721	.93779	.36352	.93159	.37973	.92510	.39581	.91833	.41178	.91128	41
H	20 21	·34748 ·34775	·93769 ·93759	.36379 .36406	.93148	·37999 ·38026	.92499 .92488	.39608 .3963 <b>5</b>	.91822	41204	.91116	40
ı	22	.34803	.93748	.36434	.93127	.38053	.92477	.39661	.91799	.41231 .41257	.91104 .91092	39 38
ı	23	.34830	.93738	.36461	.93116	.38080	.92466	.39688	.91787	.41284	.91080	37
H	24	.34857	.93728	.36488	.93106	.38107	.92455	.39715	.91775	.41310	.91068	36
ı	25	.34884	.93718	.36515	.93095	.38134	.92444	·39741	.91764	.41337	.91056	35
ı	26	.34912	.93708	.36542	.93084	.38161	.92432	39768	.91752	.41363	.91044	34
I	27 28	·34939 ·34966	.93698 .93688	.36569 .36596	.93074	.38188 .38215	.92421	39795 39822	.91741 .91729	.41390 .41416	.91032	33
Ш	29	•34993	.93677	.36623	.93052	.38241	.92399	.39848	.91718	.41443	.91020 .91008	32 31
I	30	.35021	.93667	.36650	.93042	.38268	.92388	.39875	.91706	.41469	.90996	30
ı	31	.35048	.93657	.36677	.93031	.38295	.92377	.39902	.91694	.41496	.90984	29
	32	.35075	.93647	.36704	.93020	.38322	.92366	.39928	.91683	.41522	.90972	28
Н	<b>3</b> 3	.35102	.93637	.36731	.93010	.38349	.92355	·39955	.91671	.41549	.90960	27
Ш	34 35	.35130	.93626 .93616	.36758 .36785	.92999 .92988	.38376 .38403	.92343 .92332	.39982 .40008	.91660 .91648	.41575 .41602	.90948	26
I	36	.35184	.93606	.36812	.92978	.38430	.92321	.40035	91636	.41628	.90924	24
I	37	.35211	.93596	.36839	.92967	.38456	.92310	.40062	.91625	.41655	.90911	23
ı	38	.35239	.93585	.36867	.92956	.38483	.92299	.40088	.91613	.41681	.90899	22
I	39	.35266	.93575	.36894	.92945	.38510	.92287	.40115	.91601	.41707	.90887	21
ı	40	.35293	.93565	.36921	.92935	.38537 .38564	.92276	.40141 .40168	.91590	.41734	.90875	20
ı	4I 42	·35320 ·35347	·93555 ·93544	.36948 .36975	.92924	.38591	.92265	.40105	.91578 .91566	.41760 .41787	.90863	19
	43	·35347	·93534	.37002	.92902	.38617	.92243	.40221	.91555	.41813	.90839	17
	43	.35402	.93524	.37029	.92892	.38644	.92231	.40248	.91543	.41840	.90826	16
	45	.35429	.93514	37056	.92881	.38671	.92220	.40275	.91531	.41866	.90814	15
ľ	46	.35456	.93503	.37083	.92870	.38698	.92209	.40301	.91519	.41892	.90802	14
	47 48	.35484	·93493	.37110	.92859	.38725 .38752	.92198 .92186	.40328 .40355	.91508 .91496	.41919	.90790	13
١		.35511	·93483 ·93472	·37137 ·37164	.92838	$\frac{.38752}{.38778}$	.92175	.40381	.91484	·41945 ·41972	.90776	II
ı	<b>4</b> 9 <b>5</b> 0	.35565	.93462		.92827	.38805	.92164	.40408			.90753	10
	51	.35592	.93452		.92816	.38832	.92152	.40434	- 12		.90741	9
	52	.35619	.93441	.37245	.92805	.38850	.92141	.40461	.91449	.42051	.90729	8
1	53	.35647	.93431	.37272	.92794	.38886	.92130			.42077	.90717	7 6
	54	35674	.93420	·37299	.92784			.40514		.42104	.90704	
ı	55 56 57 58	.35701 .35728	.93410	.37326 ·37353	.92773	.38939 .38966	.92107 .92096	.40541	.91414 .91402	.42136	.90680	5 4 3 2
I	57	.35755	.03389	.37380	.92751	.38993	.92085	.40594	.91390		.90668	3
ı	58	.35782	.93379	.37497	.92740	.39020		.40621	.91378	.42209	.90655	2
1	59 60	-35810	.93368	·37434	.92729	.39046		.40647	.91366		.90643	0
ı	-00	·35 <sup>8</sup> 37			.92718					.42262	.90631	
1		N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	,
I		G	9°	6	8°°	6	7°	6	6°	6	5°	
							-	, ,,	- '			

	2	5°	2	6°	2	7°	2	8°	2	9°	81
,	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	
-	.42262	.90631	.43837	.89879	45399	.89101	.46947	.88295	.48481	.87462	60
1	.42288	.90618	.43863	.89867	.45425	.89087	.46973	.88281	.48506	.87448	59
2	.42315	.90606	.43889	.89854	.45451	.89074		.88267	.48532	.87434	59 58
3	.42341	.90594	.43916	.89841 .89828	·45477	.89061 .89048	47024	.88254 .88240	.48557	.87420	57
4	.42367 .42394	.90582	.43942 .43968	.89816	·45503 ·45529	.89035	.47050 .47076	.88226	.48583 .48608	.87406	50
5 6	.42420	.90557	.43994	.89803	.45554	.89021	.47101	.88213	.48634	.87391 .87377	55 54
	.42446	.90545	.44020	.89790	-45580	.89008	.47127	.88199	.48659	.87363	
7 8	.42473	.90532	.44046	.89777	.45606	.88995		.88185	.48684	.87349	53 52
9	.42499	.90520	.44072	.89764	.45632	.88981	.47153 .47178	.88172	.48710	.87335	51
10	.42525	.90507	.44098	.89752	.45658	.88968	.47204	.88158	.48735	.87321	50
II	.42552	.90495	.44124	.89739	.45684	.88955	.47229	.88144	.48761	.87306	
12	.42578	.90483	.44151	.89726	.45710	.88942	.47255	.88130	.48786	.87292	49 48
13	.42604	.90470	.44177	.89713	.45736	.88928	.47281	.88117	.48811	.87278	47
14	.42631	.90458	.44203	.89700	.45762	.88915	.47306	.88103	.48837	.87264	46
15 16	.42657	.90446	.44229 .44255	.89687 .89674	.45787 .45813	.88902 .88888	·47332 ·47358	.88089 .88075	.48862 .48888	.87250	45
	.42709	.90433	.44281	.89662	.45839	.88875	.47383	.88062	.48913	.87235. .87221	44
17	.42736	.90408	.44307	.89649	.45865	.88862	.47409	.88048	.48938	.87207	43
19	.42762	.90396	•44333	.89636	.45891	.88848	47434	.88034	.48964	.87193	41
20	.42788	.90383	.44359	.89623	.45917	.88835	.47460	.88020	.48989	.87178	40
21	.42815	.90371	.44385	.89610	-45942	.88822	.47486	.88006	.49014	.87164	
22	.42841	.90358	.44411	.895 <b>9</b> 7	.45968	.88808	.47511	.87993	.49040	.87150	39 38
23	.42867	.90346	·44437	.89584	·45994	.88795	·47537	.87979	.49065	.87136	37 36
24	.42894	.90334	.44464	.89571	.46020	.88782	·47562	.87965	.49090	.87121	
25	.42920	.90321	.44490	.89558	46046	.88768	-47588	.87951	.49116	.87107	35
26	.42946	.90309	.44516	.89545	.46072	.88755 .88741	.47614	.87937	.49141	.87093	34
27 28	.42972 .42999	.90296 .90284	.44542	.89532	.46097	.88728	.47639 .47665	.87923	.49166	.87079	33
29	.43025	.90284	.44568 .44594	.89519 .89506	.46149	.88715	.47690	.87909 .87896	.49192	.87064 .87050	32 31
30	.43051	.90259	.44620	.89493	.46175	.88701	.47716	.87882	.49242	.87036	30
31	·43º77	.90246	.44646	.89480	46201	.88688	·4774I	.87868	.49268	.87021	29
32	.43104	.90233	.44672	.89467	.46226	.88674	.47767	.87854	.49293	.87007	28
33	.43130	.90221	.44698	.89454	.46252	.88661		.87840	.49318	.86993	27
34	.43156	.90208	-44724	.89441	.46278	.88647	·47793 ·47818	.87826	·49344	.86978	26
35 36	-43182	.90196	.44750	.89428	.46304	.88634	.47844	.87812	.49369	.86964	25
	.43209	.90183	•44776	.89415	.46330	.88620	.47869	.87798	·49394	.86949	24
37 38	·43235	.90171	.44802	.89402	.46355	.88607	.47895	.87784	.49419	.86935	23
38	.43261	.90158	.44828	.89389	.46381	.88593		.87770	·49445	.86921	22
39	.43287	.90146	.44854 .44880	.89376 .89363	46407	.8858 <b>o</b> .88566		.87756	49470	.86906	2I 20
40 41	.43313 .43340	.90133	.44906	.89350	.46433 .46458	.88553	·47971 ·47997	.87743 .87729	·49495 ·49521	.86878	19
42	.43366	.90108	.44932	89337	.46484	.88539	.48022	.87715	.49546	.86863	18
43	-43392	.90095	.44958	.89324	-40510	.88526	.48048	.87701	·4957I	.86849	17
43	.43418	.90082	.44984	.89311	.46536	.88512	.48073		.49596	.86834	16
	.43445	.90070	45010	.89298	46561	.88499	.48099	.87673	.49622	.86820	15
45 46	·43471	.90057	.45036	.89285	.46587	.88485	.48124	.87659	.49647	.86805	14
47	-43497	.90045	.45062	.89272	.46613	88472	.48150		.49672	.86791	13
48	·43523	.90032	.45088	.89259	.46639	.88458	.48175	.87631	.49697	.86777	12
49	•43549	.90019	.45114	.89245	.46664	.88445	.48201 .48226	.87617	.49723	.86762	II
50	43575	.90007	.45140 .45166	.89232	.46690 .46716	.88431 .88417	.48220 .48252	.87603 .87589	.49748	.86748 .86733	10
51 52	.43628	.89991	.45100	.89219				.87575	.49773	.86719	8.
53	43654	.89968					.48303		.49798 .49824	.86704	7
54	.43680	.89956	.45243	.89180			.48328			.86690	7 6
	.43706		.45269	.89167	.46819	.88363	-48354		.49874		5
55 56	.43733	.89930	.45295	.89153	.46844	.88349	.48379	.87518	.49899	.8666 I	4
57	·43759	.89918	.45321	.89140	.46870	.88336	.48405	.87504	-49924		3 2
57 58	.43785 .43811	.89905		.89127			.48430	.87490	-49950		
59 60	.43811	.89892		.89114							1 0
00		.89879	-								
			N. cos.					,		•	,
	6	4°	6	3°	6	2°	6	1°	6	0°	

	3	o°	3	1°	3	2°	3	3°	3	<b>4</b> °	
,	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	
0	.50000	.86603	.51504	.85717	.52992	.84805	.54464	.83867	.55919	.82904	60
1	.50025	.86588	.51529	.85702 .85687	.53017	84789	.54488	.83851	.55943	.82887	59 58
3	.50076	.86573 .86559	.51554 .51579	.85672	.53041 .53066	.84774 .84759	·54513 ·54537	.83835 .83819	.55968 .55992	.82871 .82855	
4	.50101	.86544	.51604	.85657	.53091	.84743 .84728	.54561	.83804	.56016	.82839	57 56
5 6	.50126	.86530	.51628	.85642	53115	.84728	.54586	.83788	.56040	.82822	55
-	.50151	.86515	.51653	.85627	.53140		.54610	.83772	.56064	.82806	_54_
7 8	.50176	.86501 .86486	.51678 .51703	.85612 .85597	.53164 .53189	.84697 .84681	.54635 .54659	.83756	.56088	.82790	53
1 9	.50201	.86471	.51728	.85582	.53214	.84666	.54683	.83740 .83724	.56112 .56136	.82773 .82757	52 51
10	.50252	.86457	.51753	.85567	.53238	.84650	.54708	.83708	.56160	.82741	50
11	.50277	.86442	.51778	.85551	.53263	.84635	·54732	.83692	.56184	.82724	40
12	.50302	.86427	.51803	.85536	.53288		·54756	.83676	.56208	.82708	48
13	.50327	.86413 .86398	.51828 .51852	.85521 .85506	.53312	.84604 .84588	.54781 .54805	.83660 .83645	.56232	.82692	47
14 15	.50352	.86384	.51877	.85491	·53337 ·53361	.84573	.54829	.83629	.56256 .56280	.82675 .82659	46 45
16	.50403	.86369	.51902	.85476	.53386	.84557	.54854	.83613	.56305	.82643	44
17	.50428	.86354	.51927	.85461	.53411	.84542	.54878	.83597	.56329	.82626	43
18	.50453	.86340	.51952	.85446	·53435	.84526	.54902	.83581	$\frac{.56353}{.}$	.82610	42
19	.50478	.86325	.51977	.85431 .85416	.53460 .53484	.84511	.54927	.83565	.56377	.82593	41
20 2I	.50503	.86310 .86295	.52002 .52026	.85401	.53404	.84480	·54951 ·54975	.83549 .83533	.56401 .56425	.82577 .82561	40
22	.50553	.86281	.52051	.85385	.53534	.84464	.54999	.83517	.56449	.82544	39 38
23	.50578	.86266	.52076	.85370	.53558	.84448	.55024	.83501	.56473	.82528	37
24	.50603	.86251	.52101	.85355	·53583	.84433	.55048	.83485	.56497	.82511	36
25	.50628	86237	.52126	.85340	.53607	.84417	.55072	.83469	.56521	.82495	35
26	.50654	.86222 .86207	.52151 .52175	.85325 .85310	.53632 .53656	.84402 .84386	.55097 .55121	.83453 .83437	.56545	.82478 .82462	34
27 28	.50704	.86192	.52200	.85294	.53681	.84370	.55145	.83421	.56569 .56593	.82446	33 32
29	.50729		.52225	.85279	.53705	.84355	.55169	.83405	.56617	.82429	31
30	.50754	.86163	.52250	.85264	.53730	.84339	.55194	.83389	.56641	.82413	30
31	.50779	.86148	.52275	.85249	.53754	.84324	.55218	.83373	.56665	.82396	29 28
32	.50804		.52299	.85234 .85218	.53779	.84308 .84292	.55242	.83356	.56689	.82380	
33	.50829		.52324 .52349	.85203	.53804 .53828	.84277	.55266 .55291	.83340 .83324	.56713 .56736	.82363 .82347	27 26
35	.50879			.85188	.53853	.84261	.55315	.83308	.56760	.82330	25
36	.50904	.86074	.52399	.85173	.53877	.84245	.55339	.83292	.56784	.82314	24
37 38	.50929	.86059	.52423	.85157	.53902	.84230	.55363	.83276	.56808	.82297	23.
38	.50954		.52448	.85142	.53926	.84214	.55388	.83260	.56832	.82281	22
39 40	.50979	.86030 .86015	·52473 ·52498	.85127 .85112	·53951 ·53975	.84182	.55412 .55436	.83244 .83228	.56856 .56880	.82264 .82248	2I 20
41	.51029	.86000		.85096	.54000	.84167	.55460		.56904	.82231	19
42	.51054	.85985	.52547	.85081	.54024		.55484	.83195	.56928	.82214	18
43	.51079	.85970		.85066	.54049	.84135	-55509	.83179	.56952	.82198	17
44	.51104			.85051	.54073		.55533	.83163	.56976	.82181	16
45 46	.51129	.85941 .85926	52621 .52646	.85035 .85020	·54097 ·54122		·55557 ·55581	.83147 .83131	.57000 .57024	.82165 .82148	15
47	.51179	.85911	.52671	.85005	.54146	.84072	.55605	.83115	.57047	.82132	13
47 48	.51204	.85896		.84989	.54171	.84057	.55630	.83098	.57071	.82115	12
49	.51229	.85881	.52720	.84974	.54195	.84041	.55654	.83082	.57095	.82098	H
50	.51254	0-0		.84959		.84025		83066	1	.82082	10
51	.51279	.85851 .85836	.52770 .52794		·54244 ·54269	.84009 .83994	.55702 .55726	.83050 .83034	.57143 .57167		8
52 53	.51329			.84913			.55750				7
54	.51354	0 0 0	.52844	.84897	.54317	.83962	.55775		.57215	.82015	7
	.51379		.52869	.84882	.54342	.83946	.55799	.82985	.57238	.81999	5
56	.51404	.85777	.52893	.84866	.54366	.83930	.55823	82969		.81982	5 4 3 2
57	.51429	85762 .85747	.52918 .52943		.54391 .54415	.83915 .83899	.55847 .55871	.82953   .82936			3
55 56 57 58 59 60	.51454		.52943		.54440		.55895				I
66	.51504		.52992		.54464		.55919				0
	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	<del>,</del>
		9°		8° .		70		<b>6°</b>		5°	
<b>1</b>	•		•				•				

	35° N. sine N. cos.		3	6°	3	7°	3	S°	3	9°	1
,	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	
0	.57358						.61566			.77715	60
I	.57381	.81899		.8088 <u>5</u> .80867					.62955	.77696	59
3	·57405 ·57429		.58849						1 1		58
4	.57453	.81848	.58873	.80833	.60274	.79793					57 56
5	.57477	.81832	.58896	.80816	.60298	.79776	.61681	.78711	.63045	.77623	55
-	-57501	.81815	.58920						.63068	.77605	54
7 8	.57524	.81798 .81782	.58943 .58967	.80782 .80765	.60344		.61726			.77586	53
9	·57548 ·57572	.81765			.60367 .60390			.78658		1	52
IC	.57596	.81748	.59014	.80730	.60414		.61795	.78622			51 50
11	.57619		.59037	.80713	.60437	79671	.61818	.78604	.63180	.77513	49
12	-57643	.81714	.59061	.80696	.60460				.63203	·77494	48
13	.57667 .57691	.81698 .81681	.59084	.80679 .80662	.60483	.79635 .79618	.61864	.78568	.63225	-77476	47
14	.57715	.81664	.59108 .59131	.80644	.60506 .60529			.78550 .78532	.63248 .63271	-77458	46
15 16	.57738	.81647	.59154	.80627	.60553	.79583		.78514	.63293	·77439	45
17	.57762	.81631	.59178	.80610	.60576	.79565	.61955	.78496	.63316	.77402	43
_	.57786	.81614	.59201	.80593	.60599	·79547		.78478	.63338	-77384	42
19	.57810	.81597 .81580	.59225	.80576 .80558	.60622 .60645	.79530	.62001 .62024	.78460		.77366	41
21	.57857	.81563	.59240	.80541	.60668	·79512 ·79494		.78442 .78424	.63383 .63406	•77347	40
22	.57881	.81546	.59295	.80524	.60691	.79477	.62069	.78405	.63428	·77329 ·77310	39 38
23	.57904	.81530	.59318	.80507	.60714	·79459	.62092	.78387	.63451	.77292	37
24	-57928	.81513	·59342	.80489	.60738	·79441	.62115	.78369	.63473	.77273	3 <b>7</b> 36
25 26	.57952	.81496	.59365	.80472 .80455	.60761	.79424	.62138	.78351	.63496	.77255	35
27	.57976 .57999	.81479 .81462	.59389 .59412	.80438	.60784 .60807	·79406 ·79388		.78333 .78315	.63518 .63540	.77236	34
28	.58023	.81445	.59436	.80420	.60830	.79371	.62206	.78297	.63563	.77218	33
29	.58047	.81428	.59459	.80403	.60853	.79353	.62229	.78279	.63585	.77181	31
30	.58070	.81412	-59482	.80386	.60876	·79335	.62251	.78261	.63608	.77162	30
31	.58094	.81395	.59506	.80368	.60899	.79318	.62274	.78243	.63630	.77144	29 28
32	.58118	.81378 .81361	.59529 .595 <b>5</b> 2	.80351	.60922	.79300	.62297 .62320	.78225 .78206	.63653 .63675	.77125 .77107	28 27
34	.58165	.81344	.59576	.80316	.60968	.79264	.62342	.78188	.63698	.77088	26
35 36	.58189	.81327	-59599	.80299	.60991	.79247	.62365	.78170	.63720		25
	.58212	.81310	.59622	.80282	.61015	.79229	.62388	.78152	.63742	.77051	24
37 38	.58236	.81293	.59646	.80264	.61038	.79211	.62411	.78134	.63765	-77033	23
39	.58260	.81276	.59669	.80247 .80230	.61061 .61084	.79193 .79176	.62433 .62456	.78116 .78098	.63787	.77014 .76996	22 21
40	.58307	.81242	.59716	.80212	.61107	.79158		.78079	.63832	.76977	20
41	.58330	.81225	-59739	.80195	.61130		.62502	.78061	.63854	.76959	19
42	·58354	.81208	.59763	.80178	.61153	.79122	.62524	.78043	.63877	.76940	18
43	.58378 .58401	.81191 .81174	-59786	.80160 .80143	.61176	.79105 .79087	.62547	.78025	.63899	76921	17
44 45	.58425	.81157	59832	.80143	.61222	.79069			.63944	.76903 .76884	15
46	.58449		.59856	.80108	.61245	-79051	.62615	.77970	.63966	.76866	14
47	.58472	.81123	.59879	.80091	.61268	.79033	.62638	.77952	.63989		13
48	-58496	.81106	.59902	.80073	.61291	-79016	.62660		.64011	.76828	12
49 50	.58519 .58543	.81089 .81072	.59926 ·59949	.80056 .80038	.61314 .61337	.78998 .78980	.62683	.77916 .77897	.64033 .64056	.76810 .76791	10
51	.58567	.81072	.59972	.80021	.61360	.78962	.62728	.77879	.64078	.76772	9 1
52	.58590	.81038	-59995	.80003	.61383	.78944	.62751	.77861	.64100	-76754	8
52 53	.58614	.81021	.60019	.79986	.61406	78926	.62774				8 7 6
54		.81004		-79968	.61451	.78908			.64145		
55	.58684		.60065	·79951 ·79934		.78873	.62842	.77788	.64190		\$ \$ 3 2
57	.58708	.80953	.60112	.79916	.61497	.78855	.62864		64212	.76661	3
58	.58731	.80936	.60135	.79899		.78837	.62887	.77751	.64234	.76642	2
55 56 57 58 59 60	-58755	.80919	.60158	.79881		.78819 .78801	.62909		.64256 .64279		0
-00		.80902		.79864		-		.77715			
			N. cos.								,
	5	1°	5	3°	5	2°	5	1°	5	0°	

04	1				IAD		1				
	<u> </u>	10°		1°		2°		3°		4°	
'	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	
0	.64279		.65606		66913	.74314		1 .0 02	.69466		60
I	.64301				.66935		.68221	1	.69487		<b>59</b> 58
3	.64323 .64346				.66956 .66978					. ~ .	50 57
4	.64368		.65694	.75395	.66999		.68285	.73056		.71873	56
5	.64390		.65716	.75375	.67021	.74217	.68306	.73036	.69570	.71833	55
1	.64412		.65738		.67043		.68327		.69591	.71813	_54_
7	.64435 .64457		.65759 .65781		.67064 .67086		.68349 .68370	.72996	.69612	.71792	53
9	.64479	.76436	.65803		.67107		.68391	·72976 ·72957	.69633 .69654	.71772 .71752	52 51
ΙÓ	.64501	.76417	.65825	.75280			.68412	.72937	.69675	.71732	50
11	.64524				.67151	.74100	.68434		.69696	.71711	49 48
12	.64546				.67172		.68455		.69717	.71691	
13 14	.64568 .64590			.75222	.67194 .67215	.74061	.68476 .68497	.72877 .72857	.69737 .69758	.71671	47 46
15	.64612			.75184	.67237	.74022	.68518	.72837	.69779	.71650 .71630	45
16	.64635	.76304	.65956	.75165	.67258	.74002	.68539	.72817	.69800	.71610	44
17	.64657		.65978		.67280		.68561	.72797	.69821	.71590	43
	.64679	.76267	.66000		.67301 .67323	·73963	.68582		.69842	.71569	42
19	.64723				.67344	·73944 ·73924	.68624		.69862 .69883	.71549 .71529	4 <b>I</b> 40
21	.64746	.76210	.66066	.75069	.67366	.73904	.68645	.72717	.69904	.71508	
22	.64768			.75050	.67387	.73885	.68666	.72697	.69925	.71488	39 38
23	.64790 .64812	.76173 .76154	.66109 .66131		.67409		.68688 .68 <b>70</b> 9		.69946	.71468	37 36
24	.64834	.76135	.66153	·75011	.67430 .67452	.73826	.68730		.69966	-71447	
25 26	.64856	.76116	.66175	.74973	.67473	.73806	.68751	.72617	.70008	.71427 .71407	35 34
27	.64878	.76097	.66197	·74953	.67495	.73787	.68772	.72597	.70029	.71386	33
28	.64901	.76078	.66218		.67516	.73767	.68793		.70049	.71366	32
30	.64923 .64945	.76059 .76041	.66240 .66262		.67538 .67559	·73747 ·73728	.68814 .68835	·72557 ·72537	.70070 .70091	.71345	30
31	.64967	.76022	.66284	.74876	.67580	.73708	.68857	.72517	.70112	.71325	29
32	.64989		.66306	.74857	.67602		.68878	.72497	.70132	.71284	28
33	.65011	.75984	.66327	.74838	.67623	.73669	.68899	.72477	.70153	.71264	27
34	.65033 .65055	.75965	.66349 .66371		.67645 .67666	.73649 .73629	.68920 .68941		.70174	.71243	26
35 36	.65077	.75946	.66393	·74799 ·74780	.67688		.68962	.72437	.70195 .70215	.71223	25 24
	.65100	.75908	.66414	.74760	.67709	·73590	.68983		.70236	.71182	23
37 38	.65122	.75889	.66436	.74741	.67730	.73570	69004	.72377	.70257	.71162	22
39	.65144	.75870	.66458		.67752	.73551	.69025	-72357	.70277	.71141	21
40 41	.65166 .65188	.75851 .75832	.66480 .66501	·74703 ·74683	.67773 .67795	·73531 ·73511	.69046 .69067	.72337	.70298 .70319	.71121	20 19
42	.65210	.75813	.66523	.74664	.67816	.73491	.69088		.70339	.71080	18
43	.65232	·75794	.66545	.74644	.67837	.73472	.69109	.72277	.70360	.71059	17
44	.65254		.66566		.67859	.73452	.69130	.72257	.70381	.71039	16
45	.65276 .65298		66588 .66610	.74606 .74586	.67880 .67901	·73432 ·73413	.69151 .69172	.72236	.70401	.71019 .70998	15
47	.65320	.75719	.66632	.74567	.67923	.73393	.69193		.70422	.70978	13.
48	.65342	.75700	.66653	.74548	.67944	·73373	.69214		70463	.70957	12
49	.65364	.75680	.66675	.74528	.67965	·73353	.69235	.72156	. 70484	.70937	II
50	.65386		.66697 .66718	.74509	.67987 .68008	·73333		.72136 .72116	.70505 .70525		10
51 52	.65408 .65430		.66740		.68029	·73314 ·73294		.72095	.70525	.70896 .70875	98 7 6
53	.65452	.75604	.66762	.74451	.68051	.73274	.69319	.72075	.70567	.70855	7
54	.65474		.66783	·74431	.68072	·73254	.69340		.70587	.70834	
55 56 57 58	.65496	.75566	.66805	.74412	.68093	.73234	.69361 .69382		.70608	.70813	5 4 3 2
50	.65518 .65540	·75547	.66827 .66848		.68115 .68136	.73215 .73195	.69382		.70628 .70649	.70793 .70772	3
58	.65562	.75509	.66870	.74353	.68157	.73175	.69424		.70670	.70752	2
59 60	.65584	.75490	.66891	·74334	.68179	.73155	.69445	.71954	.70690	.70731	I
00	.65606	·75471	.66913	.74314	.68200	.73135	.69466	.71934	.70711	.70711	0
	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	,
	A	9°	4	8°	4	7°	4	6°	4	5°	
-		-									

## TABLE VI.

## ADDITION AND SUBTRACTION LOGARITHMS.

## PRECEPTS.

I. When difference of given logarithms is less than 2.00.

ADDITION.—Enter table with difference between logarithms as Arg. A, and take out B.

Add B to subtracted logarithm.

SUBTRACTION.—Subtract lesser from greater logarithm; enter with the difference as B, and take out A.

Add A to the subtracted logarithm.

II. When difference of given logarithms exceeds 2.00.

Subtract lesser from greater.

ADDITION.—Enter table with difference as Arg. A, take out B-A and add it to the greater logarithm.

SUBTRACTION.—Enter column B with difference of logarithms; take out B-A, and subtract it from greater logarithm.

A.	В.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
5.	0.00	000	100	100	100	100	100	002	002	003	003	
6.0		004	004	005	005	003	005	005	005	005	005	
6.1 6.2 6.3		005 007 009	006 007 009	006 007 009	006 007 009	006 008 010	006	006	006	007 008 010	007 008 011	3 4 5 6 1 0.3 0.4 0.5 0.6 2 0.6 0.8 1.0 1.2
6.4 6.5 6.6		011 014 017	011 014 018	011 014 018	012 015 019	012 015 019	012 015 019	013 016 020	013 016 020	013 017 021	013 017 021	3 0.9 1.2 1.5 1.8 4 1.2 1.6 2.0 2.4 5 1.5 2.0 2.5 3.0 6 1.8 2.4 3.0 3.6
6.7 6.8 6.9		022 027 034	022 028 035	023 029 036	023 029 037	024 030 038	024 031 039	025 031 040	026 032 041	026 033 041	027 034 042	7 2.I 2.8 3.5 4.2 8 2.4 3.2 4.0 4.8 9 2.7 3.6 4.5 5.4
7.0		043	044	045	047	048	049	050	051	052	053	7   8   9   10
7.1 7.2 7.3		055 069 087	056 070 089	057 072 091	059 074 093	060 075 095	061 077 097	063 079 <b>0</b> 99	064 081 102	066 083 104	067 08 <del>5</del> 106	1 0.7 0.8 0.9 1.0 2 1.4 1.6 1.8 2.0 3 2.1 2.4 2.7 3.0
7·4 7·5 7.6		109 137 173	140	114 144 181	117 147 185	119 150 189	122 154 194	125 157 198	128 161 203	131 16 <del>5</del> 207	134 169 212	4 2.8 3.2 3.6 4.0 5 3.5 4.0 4.5 5.0 6 4.2 4.8 5.4 6.0 7 4.9 5.6 6.3 7.0
7.7 7.8 7.9		217 273 344	352	360	368	377	244 306 385 485	394	32I 403	261 328 413	422	8 5.6 6.4 7.2 8.0 9 6.3 7.2 8.1 9.0
8.0 A.	В.	43 <sup>2</sup>	1	45 <sup>2</sup>	463 <b>3</b>	474 • <b>4</b>	5	496 6	507 7	519 8	9	Prop. Pts.

Ī	$\int_{A_{-a}} (\log b - \log a = A) \qquad \qquad \int_{A_{-a}} (\log a - \log b = B)$													
	ADD. $\begin{cases} \log b - \log a = A. \\ \log (a + b) = \log a + B. \end{cases}$ Sub. $\begin{cases} \log a - \log b = B. \\ \log (a - b) = \log b + A. \end{cases}$													
	Α.	В.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.	
	8.00	0.00	432	433	434	435	436	437	438	439	440	441		
	8.01 8.02		442	443	444	445 456	446 457	447 458	448 459	449 460	450	451 462		
	8.03		463	464	465	466	467	468	469	470	471	473	•	
	8.04		474	475	476	477	478	479	480	481	482	483		
	8.05 8.06		485	486	487	488	489 500	490 502	49I 503	492 504	494 505	49 <del>5</del> 506		
I	8.07		507	508	510	511	512	513	514	515	517	518		
	8.08		519	520	521	523	524	525	526	527	529	530	1 0.2	
	8.09 8.10	-	531	532	533	535	536	537	538	540	541	542	2 0.4	
	8.11	-	543 556	545	546 558	547	548 561	550	551 564	552 565	553 566	55 <u>5</u> 567	3 0.6	
	8.12		569	570	571	573	574	575	577	578	579	581	5 1.0	
	8.13		582	583	583	586	587	589	590	591	593	594	7 1.4	
1	8.14		595	597	598	599 613	601 615	602	604	605	606	608 622	8 1.6 9 1.8	
I	8.16		623	625	626	628	629	630	632	633	635	636	91 -10	
	8.17		638	639	641	642	644	645	646	648	649	651		
ı	8.18		652 667	654	655 671	657	658 674	660 675	661	663 678	664 680	666 681		
ı	8.20	-	683	684	686	688	689	691	692	694	696	697		
ı	8.21	-	699	700	702	703	705	707	708	710	712	713		
	8.22		715	716	718	720	721	723	725	726	728	730	I 0.3 2 0.6	
	8.23 8.24		73 <sup>1</sup> 74 <sup>8</sup>	733 750	735 752	736 753	73 <sup>8</sup>   755	740 757	741 759	743 760	745 762	747 764		
	8.25		766	767	769	771	773	774	776	778	780	78 i	4 1.2	
ı	8.26		783	785	787	789	790	792	794	796	798	799	5 I.5 6 I.8	
ı	8.27 8.28		801 820	803 822	80 <u>5</u> 823	807 825	809 827	810 829	812 831	814 833	816 83 <del>5</del>	818 837	7 2.I 8 2.4	
	8.29		839	841	842	844	846	848	850	852	854	856	9 2.7	
	8.30		858	860	862	864	866	868	870	872	874	876		
ı	8.31		878 898	880 900	882 902	884 904	886 906	888 9 <b>0</b> 8	910	892 912	89 <u>4</u> 91 <u>5</u>	896 917		
	8.32 8.33		919	921	923	925	927	929	931	933	936	938		
	8.34		940	942	944	946	948	951	953	955	957	959		
I	8.35 8.36		962 984	964 986	966 <b>9</b> 88	968 990	970	97 <u>3</u> 995	975 997	977 999	979 *002	981 *004	4	
	8.37	0.01	-	009	011	013	016	018	020	022	025	027	I 0.4 2 0.8	
	8.38		030	032	034 058	037 060	039 063	041 065	044 068	046	048 073	051	3 1.2	
	8.39 8.40		053 077	<b>0</b> 56		085	087	090	092	095	097	100	5 2.0	
	8.41		102	105		110		115					7 2.8	
1	8.42		128	130	133	135	138	140	143	146	148	151	7 2.8 8 3.2 9 3.6	
١	8.43		153 180					167		.1	1		913.0	
	8.44		207	210	213		<b>ا</b> م	193 221			1	232		
ラン学	8.46		235	238	240	243	246	249		1				
3	8.47		263					278						
	8.49		292 322			331		307	340			349		
·&	8.50		352	-	-		-		371					
	Δ.	B.	0	1	2	3	4	5	-	7	8	9	Prop. Pts.	

ADD. $\begin{cases} \log b - \log a = A. \\ \log (a + b) = \log a + B. \end{cases}$ SUB. $\begin{cases} \log a - \log b = B. \\ \log (a - b) = \log b + A. \end{cases}$ A.   B. 0   1   2   3   4   5   6   7   8   9   Prop. Pts.														
	В.	0	1					6	7	8		P	rop.	Pts.
8.50	0.01	352	355	358	361	364	368	371	374	377	380			
8.51 8.52		38 <u>3</u>	386 418	389 421	393 424	396 428	399 431	402	405 437	408	412			
8.53		447	450	454	457	460	464	467	470	474	477			
8.54		480	484	487	490	494	497	501	504	507	511		3 1	4
8.55 8.56		514 549	518 552	521 556	525 559	528 563	531 566	535 570	538 574	542 577	545 581	1	0.3	0.4
8.57		584	588	591	595	599	602	606	610	613	617	3	0.9	1.2
8.58 8.59		621 658	624 661	628 665	632 669	635	639 676	643 680	646 684	650 688	654	4	1.5	1.6
8.60		695	699	703	707	673	715	719	722	726	730	5 6 7	1.5 1.8 2.1	2.4
8.61		734	738	742	746	750	754	758	762	766	770	7 8	2.4	3.2
8.62		774	778	782	786	790	794	798	802	806	810	9	2.7	3.6
8.6 <sub>3</sub> 8.6 <sub>4</sub>		814 856	818	822	827 868	831 872	835 877	881	843 885	847 889	851 894			
8.65		898	902	906	911	915	919	924	928	932	937			
8.66		941	945	950	954	959	963	967	972	976	981		5	6
8.67	0,02	985 030	990	994 040	999 044	*003	*008 053	*012 058	*017 063	*021 067	*026 072	1 2	0.5	0.6
8.69		077	081	086	091	095	100	105	110	114	119	3	1.5	1.8
8.70		124	129	133	138	143	148	153	158	162	167	5 6	2.5	3.0
8.71		172 221	177 226	182	187 236	192 241	197 246	202 252	207 257	211	216	7 8	3.0	3.6
8.73		272	277	282	287	292	297	303	308	313	318	8	4.0	4.8
8.74		323	329	334	339	344	350	355	360	365	371			•
8.75		376 430	381 435	387 441	392 446	397 452	403 457	408 463	414	419	424 479			
8.77		485	490	496	502	507	513	518	524	530	535			
8.78		541 599	547 604	552 610	558 616	564 622	570 628	575 634	581 639	587 645	593 651	1	0.7	0.8
8.80		657	663	669	675	681	687	693	699	705	711	3	1.4 2.1	1.6
8.81		717	723	729	735	742	748	754	760	766	772	4	2.8 3·5	3.2
8.82		779 841	78 <u>5</u> 848	791 854	797 860	803 867	810	816	822	829 892	83 <del>5</del> 899	5	4.2	4.8
8.84		905	912	918	925	931	938	944	951	957	964	8	4.9 5.6 6.3	5.6 6.4
8.85 8.86		971	977	984	991 058	997 065	*004	*011 078	*017 085	*024	*031	9	6.3	7.2
8.87	0.03	106	044	120	126	133	071 140	147	154	092 161	168			
8.88		175	183	190	197	204	211	218	225	232	240			
8.89		247 320	254	261	268	276	283	290 364	298	305	386		9	10
8.91		394	327 401	334 409	342 417	349	357 432	439	371 447	379 455	462	1 2	0.9	2.0
8.92		470	478	485	493	501	509	516	524	532	540	3 4	3.6	3.0
8.93		548	555 60F	563	571	579	587 667		683	611	619	4 5 6	4.5	5.0
8.94 8.95		627 <b>70</b> 8	63 <u>5</u> 716	643 724	651 732	659 741	749	675 757	765	691 774	700 782	7 8	5.4	7.0
8.96		790	799	807	816	824	832	841	849	858	866	9	7.2 8.1	8.0 9.0
8.97		875 961	883 970	892 979	901 987	909 996	918 *005	926 *014	935 *023	944 *032	953 *040			
8.99	0.04	-	058	067	076	085	094	103	112	121	130			
9.00		139	148	157	167	176	185	194	203	213	222			
A.	В.	0	1	2	3	4	5	6	7	8	9	P	rop.	Pts.

-														
AD	ADD. $\begin{cases} \log b - \log a = A. \\ \log (a + b) = \log a + B. \end{cases}$ SUB. $\begin{cases} \log a - \log b = B. \\ \log (a - b) = \log b + A. \end{cases}$ A. B. $0 + 1 + 2 + 3 + 4 + 5 + 6 + 7 + 8 + 9 + \text{Prop. Pts.}$													
A.	В.	0	1	2	3			6	7	8	9	Prop. Pts.		
9.00	0.04	139	148	157	167	176	185	194	203	213	222	i a lealer		
9.01		231	240	250	259	268	278	287	297	306	315	1 0.9 1.0 1.1		
9.02		325 421	334 430	344 440	3 <u>5</u> 3 4 <u>5</u> 0	363 460	373 469	382 479	<b>392</b> 489	499	411 509	2 1.8 2.0 2.2		
9.04	1	519	528	538	548	558	568	578	588	598	608	3 2.7 3.0 3.3 4 3.6 4.0 4.4		
9.05		618	628	639	649	659	669	679	689	700	710	5 4.5 5.0 5.5		
9.06		720	731	741	751	762	772	782	793	803	814	6 5.4 6.0 6.6 7 6.3 7.0 7.7		
9.07		824 931	83 <del>5</del> 941	845 952	856 963	867 974	877 985	888 995	898 *006	909 *017	920 *028	8 7.2 8.0 8.8 9 8.1 9.0 9.9		
9.09		039	050	061	072	083	094	105	116	127	139	12   13   14		
9.10		150	161	172	183	195	206	217	229	240	251	1 1.2 1.3 1.4		
9.11	1	263	274	286	297	308	320	332	343	355	366	2 2.4 2.6 2.8 3 3.6 3.9 4.2		
9.12		378	390	401	413	425	436	448	460	472	484	4 4.8 5.2 5.6		
9.13		496 616	508 628	640	531 652	543 664	555 677	567 689	579 701	59I 714	604	5 6.0 6.5 7.0 6 7.2 7.8 8.4		
9.14		738	751	763	775	788	800	813	825	838	726 851	7 8.4 9.1 9.8		
9.16		863	876	889	901	914	927	939	952	965	978	9 10.8 11.7 12.6		
9.17		991	1			*043	*o56	*069	1	77	*108	15   16   17		
9.18 9.19	0.06	121 254	134 267	147 281	161 294	308	187 321	335	214 348	227 362	240 376	1 1.5 1.6 1.7		
9.20		389	403	417	430	444	458	472	486	500	513	3 4.5 4.8 5.1		
9.21	1 .	527	541	555	569	583	597	612	626	640	654	4 6.0 6.4 6.8 5 7.5 8.0 8.5		
9.22		668	683	697	711	725	740	754	769	783	798	6 9.0 9.6 10.2		
9.23	1	812	827	841	856	870	885	900	914	929	944	7 10.5 11.2 11.9 8 12.0 12.8 13.6		
9.24		959 108	973 123	988 138	*003 154	*018	*033	*048	*063	*078 230	*093 245	9 13.5 14.4 15.3		
9.26		261	276	291	307	322	338	354	369	385	400	18 19 20		
9.27		416	432	448	463	479	495	511	527	543	559	1 1.8 1.9 2.0 2 3.6 3.8 4.0		
9.28		575	591	607	623 785	639 802	655 818	671	687 851	704 868	720	3 5.4 5.7 6.0 4 7.2 7.6 8.0		
9.29	1	736	753 918	769	951	968	985	83 <del>5</del>	*018	*035	*052	5 9.0 9.5 10.0		
9.31			086	934	120	137	154		188	206	223	7 12.6 13.3 14.0		
9.32	1	240		275	292	309	327	344	1 .		397	8 14.4 15.2 16.0.		
9.33		415	432	450	468	485	503	521		557	574	9  16.2  17.1  18.0		
9.34		592	610		646		683	701 884	719		755	21 22 23 1 2.1 2.2 2.3		
9.3		774 958	977	996	829 *014		865 *052				940 *127	2 4.2 4.4 4.6		
9.37				1	1	1	242	1		1		3 6.3 6.6 6.9 4 8.4 8.8 9.2		
9.38	3	338	357	377	396	416	435	455		494	514	5 10.5 11.0 11.5 6 12.6 13.2 13.8		
9.39		533			593		632				<u> </u>	7 14.7 15.4 16.1		
9.40	1	732			793		833				914 *120	8 16.8 17.6 18.4 9 18.9 19.8 20.7		
9.4		935 141			204	*017 225	246			309		24   25   26		
9.4		351	1				458					1 2.4 2.5 2.6		
9.4		565	587	609	630		674	696	718	739		2 4.8 5.0 5.2 3 7.2 7.5 7.8		
9.4		783 1 003					894					4 9.6 10.0 10.4		
9.4	1	231		1		1	345	1	-			5 12.0 12.5 13.0 6 14.4 15.0 15.6		
9.4	8	461					577	601	624	648	671	7 16.8 17.5 18.2		
9.4	9	69		742	766	790	814	837		885	909	8 19.2 20.0 20.8 9 21.6 22.5 23.4		
9.5	_	933			-				-		-			
A.	В.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.		

AD	o. { lo	g b - g (a	- log + b)	a = 1	$A$ . $\log a$	+ <i>B</i> .		Su	в. {	log a	$-\log z - \delta$	$g b = B.$ $0 = \log b + A.$
A.	В.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
9.50	0.11	933	957	981	*005	*030	*054	*078	*102	*127	*151	27   28   29   30
9.51	0.12	175	200	224	249	274	298	323	348	372	397	27 28 29 30 1 2.7 2.8 2.9 3.0
9.52 9.53		422 673	447 698	472 724	497 749	522 775	547 800	572 826	597 851	622 877	648 903	2 5.4 5.6 5.8 6.0
9.54		928	954	980	*006	*032	*058	*084	*110	*136	*162	3 8.1 8.4 8.7 9 3 4 10.8 11.2 11.6 12 3
9.55	0.13	188	214	240	267	293	319	346	372	399	425	5 13.5 14.0 14.5 15 a 6 16.2 16.8 17.4 18.0
9.56		452	479	505	532	559	586	613	640	667	694	7 18.9 19.6 20.3 21.0
9.57		721	748 *021	775 *049	802 *077	829 *104	857 *132	884 *160	911 *188	939 *216	966 *244	8 21.6 22.4 23.2 24.0 9 24.3 25.2 26.1 27.0
9.58	0.14	994 272	300	328	356	384	412	441	469	497	526	31   32   33   34
9.60		554	583	611	640	668	697	726	755	783	812	1 3.1 3.2 3.3 3.4
9.61	-	841	870	899	928	957	986	*016	*045	*074	*104	2 6.2 6.4 6.6 6.8 3 9.3 9.6 9.9 10.2
9.62	0.15	133	162	192	221	251	281	310	340	370	400	4 12.4 12.8 13.2 13.6
9.63		430	460	489	520	550	580	610	640	670	701	5 15.5 16.0 16.5 17.0 6 18.6 19.2 19.8 20.4
9.64	0.16	73 <sup>I</sup>	761 068	792 099	822 130	853	884 192	914	94 <u>5</u> 255	976 286	*007 317	7 21.7 22.4 23.1 23.8
9.66	0.10	349	380	411	443	474	506	538	569	601	633	8 24.8 25.6 26.4 27.2 9 27.9 28.8 29.7 30.6
9.67		665	697	729	761	793	825	857	889	921	954	35   36   37   38
9.68		986	810*	*051	*083	*116	*148	*181	*214	*247	*279	1 3.5 3.6 3.7 3.8
9.69	0.17	312	345	378	411	444	477	510	544	577	610	2 7.0 7.2 7.4 7.6 3 10.5 10.8 11.1 11.4
		643	677	710	744 *082	777	811	84 <del>5</del> *184	878 *218	912	946 *287	4 14.0 14.4 14.8 15.2
9.71	0.18	980 322	*014 356	*048 390	425	*116	*150 494	529	564	*253 599	633	5 17.5 18.0 18.5 19.0 6 21.0 21.6 22.2 22.3
9.73		668	703	738	773	808	844	879	914		985	7 24.5 25.2 25.9 26.6
9.74	0.19		056	091	127	163	198	234	270	306	342	8 28.0 28.8 29.6 30.4 9 31.5 32.4 33.3 34.2
9.75		378	414	813	486		558	595 960	631	667 *034	704 *071	39 40 41 42
9.76	0.20	740 108	777	182	220		923 294	331	997 369	1	444	1 3.9 4.0 4.1 4.2 2 7.8 8.0 8.2 8.4
9.78	0.20	481	145 519	557	594	1	670	708		784	822	3 11.7 12.0 12.3 12.6
9.79		860	898	937	975	ala .	*052	*090	*128	*167	*206	4 15.6 16.0 16.4 16.8 5 19.5 20.0 20.5 21.0
9.80	0.21	244	283	322	361	399	438	477	516	556	595	6 23.4 24.0 24.6 25.2
9.81		634	673	712	752		831	870		1	989	7 27.3 28 0 28.7 29.4 8 31.2 32.0 32.8 33.6
9.82 9.83	0.22	<b>0</b> 29	069 470	510		189	632	269 673			-	9 35.1 36.0 36.9 37.8
9.84		836	877	918	1		*041	*082	1	1		43 44 45 46
9.85	0.23	247	289	330	372	414	455	497	539	581	623	1 4.3 4.4 4.5 4.6 2 8.6 8.8 9.0 9.2
9.86		665	707	749	1		875	918	-	1		3 12.9 13.2 13.5 13.8
9.87 9.88	0.24	088 516	130 559	173 603		1 -2 -	733	- /				4 17.2 17.6 18.0 18.4 5 21.5 22.0 22.5 23.0
9.89		950	994	*038			*170	*214				6 25.8 26.4 27.0 27.6 7 30.1 30.8 31.5 32.2
9.90			434	479	-	568	612		701	746		8 34.4 35.2 36.0 36.8
9.91		836	188	926	970	*016	*061	*106	*151	*196	*242	9 38.7 39.6 40.5 41.4
9.92	0.26			378	423	469	515		1 606	652	*160	47 48 49 50 1 4.7 4.8 4.9 5.0
9.93	1	744		1	1	-	974		1	1 -		2 9.4 9.6 9.8 10.0
9.94		$67\overline{5}$	253 722			393 864	911	959	534 *006	*054	*101	3 14.1 14.4 14.7 15.0 4 18.8 19.2 19.6 20.0
9.96		149	197	1 -			388	436	484	532	581	5 23.5 24.0 24.5 25.0
9.97		629	677				871		968	*017	*066	6 28.2 28.8 29.4 30.0 7 32.9 33.6 34.3 35.0
9.98	0.29	606			-1	1 2	359 854	409			556	8 37.6 38.4 39.2 40.0
9.99	1				-	-	354					9 42.3 43.2 44.1 45.0
A.	0.30 B.	0	1	203	3	4	5	6	7	8	9	Prop. Pts.

AD	o. { lo	g a - g (a	- log + b)	b = lo	A. og b -	+ <i>B</i> .		Su	в. { 1	$og a \cdot og (a$	— log — b)	b = B. = $\log b + A$ .
A.	В.	0	1	2	3	4	5	6	7	8.	9	Prop. Pts.
0.00	0.30	103	153	203	253	303	354	404	454	505	555	50   51   52   53
0.01	0.31	606	656	707	758 268	809 320	859 371	910 422	961 474	*012 526	*063   577	1 5.0 5.1 5.2 5.3
0.03	0.31	629	681	732	784	836	888	940			*097	2 10.0 10.2 10.4 10.6 3 15.0 15.3 15.6 15.9
0.04	0.32		201	254	306	359	411	464	517	569	622	4 20.0 20.4 20.8 21.2 5 25.0 25.5 26.0 26.5
0.05	0.33	675 207	728 260	781 314	834 367	887 421	940 474	993 528	*046 582	*100 636	*153 690	6 30.0 30.6 31.2 31.8
0.07		744	798	852	906	960		- 1	- 1	*178	*232	7 35.0 35.7 36.4 37.1 8 40.0 40.8 41.6 42.4
0.08		287 836	342 891	396 946	451 *001	506 *057	561 *112	616 861*	670	726 *279	781 *334	9 45.0 45.9 46.8 47.7
0.10	1 .		446	502	558	614	670	726	782	838	894	54 55 56 57 1 5.4 5.5 5.6 5.7
0.11	", ",	950				*176	*233	*289			*459	2 10.8 11.0 11.2 11.4 3 16.2 16.5 16.8 17.1
0.12		516	573	630	687 260	744 318	801	858	916	973	*030	4 21.6 22.0 22.4 22.8
0.13	0.37	088 663	723	203 781	839	897	375 955	433 *014	491 *072	549 *130	607 *189	5 27.0 27.5 28.0 28.5 6 32.4 33.0 33.6 34.2
0.15		247	306	365	423	482	541	600	659	718	777	7 37.8 38.5 39.2 39.9 8 43.2 44.0 44.8 45.6
0.16		836	895		*013	*073	*132		*251		*370	9 48.6 49.5 50.4 51.3
0.17	0.39		489 089	549 149	609 210	669 270	729 331	789 391	849 452	909 512	969 573	58 59 60 61 1 5.8 5.9 6.0 6.1
0.19		634	695	756	816	877	938		*061	*122	*183	2 11.6 11.8 12.0 12.2
0.20			306	367	428	490	552	613	675	737	798	3 17.4 17.7 18.0 18.3 4 23.2 23.6 24.0 24.4
0.21		860 481	922 544	984 606	*046 669	*108	*170 794	*232 857	*294 920	*357 982	*419 *045	5 29.0 29.5 30.0 30.5 6 34.8 35.4 36.0 36.6
0.23		٠. ^	171	234	297	360	423	487	550	613	677	7 40.6 41.3 42.0 42.7
0.24		740	804	867	931	995	*058	*122	*186	*250	*314	8 46.4 47.2 48.0 48.8 9 52.2 53.1 54.0 54.9
0.25			442 085	506 149	570 214	634 279	698 <b>3</b> 44	763 408	827 473	891 <b>53</b> 8	956 603	62 63 64 65
0.27		668	733	799	864	929	994		*125	*190	*256	1 6.2 6.3 6.4 6.5 2 12.4 12.6 12.8 13.0
0.28		322 980	387 *046	453 *112	518 *178	58 <u>4</u> *245	650 *311	716 *377	782 *444		914 *577	3 18.6 18.9 19.2 19.5 4 24.8 25.2 25.6 26.0
0.30	E .		710	777	844	910	977	*044	*111		*245	5 31.0 31.5 32.0 32.5
0.31			379	447	514	581	648	716	783	851	918	6 37.2 37.8 38.4 39.0 7 43.4 44.1 44.8 45.5
0.32	2	986	*054	*121 801	*189 869		*325 *006	*393	*461		*597 *280	8 49.6 50.4 51.2 52.0 9 55.8 56.7 57.6 58.5
0.33			1	486	555	938 624	692	*074 761	*143 830		968	66 67 68 69
0.35	0.51	037	107	176	245	314	384	453	522	592	661	1 6.6 6.7 6.8 6.9 2 13.2 13.4 13.6 13.8
0.36		731	_	870	940		*080 781	*150 851	*220	*289 992	*360 *062	3 19.8 20.1 20.4 20.7 4 26.4 26.8 27.2 27.6
0.37		133	204		640 345	710 416	486	557	921 628	699	770	5 33.0 33.5 34.0 34.5
0.39		841	912	983	*055		*197	*268	J-		*483	6 39.6 40.2 40.8 41.4 7 46.2 46.9 47.6 48.3
0.40		554			769	1	912	-	*056		*200	8 52.8 53.6 54.4 55.2 9 59.4 60.3 61.2 62.1
0.4		272 994	344 *o66	416 *139	400 *211	*284	632 *357	704 *429	777 *502	849 *575	921 *648	70 71 72 73
0.4		721	794	867	940	*013	* <b>o</b> 86	*159	*232	*305	*379	1 7.0 7.1 7.2 7.3 2 14.0 14.2 14.4 14.6
0.4	0.57	7 452 3 188	525				819 <b>5</b> 58			ا م	*114 854	3 21.0 21.3 21.6 21.9
0.4		928	262 *003		410 *151	484 *226	*300	*375	706 *449	780 *524	*598	4 28.0 28.4 28.8 29.2 5 35.0 35.5 36.0 36.5
0.4	0.59	673	748	822	1 - 0		*047	*122	*197	*272	*347	6 42.0 42.6 43.2 43.8 7 49.0 49.7 50.4 51.1
0.4		) 422 I 175		1		1 0	798 554				*100 857	8 56.0 56.8 57.6 58.4
0.5		933	-		-		*314	_			*619	9 63.0 63.9 64.8 65.7
A.	В.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

ADI	o. { lo	g a - g (a	- log + b)	b = 1	A. og <b>b</b>	+ <i>B</i> .		Su	в. { ]	log a log (a	$-\log(-b)$	$gb = B.$ $0 = \log b + A.$
A.	В.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
0.50	0.61	933	*009	*o85	*161	*237		*390	*466	*542	*619	1 74   75   76
0.51	0.62		771	848 615	924	*001 768	*077	*154	*231	*307	*384	74 75 76 1 7.4 7.5 7.6
0.52	0.63		538 308	386	692 463	540	845 618	923 695	*000 773	*077 850	*154 928	2 14.8 15.0 15.2 3 22.2 22.5 22.8
0.54	0.65	-	083	160	238	316	394	472	549	627	705	3 22.2 22.5 22.8 4 29.6 30.0 30.4
0.55		783	861	939	*018	*096	*174	*252	*330	*409	*487	5 37.0 37.5 38.0 6 44.4 45.0 45.6
0.56		565	644	722	108	879					*273	7 51.8 52.5 53.2
0.57	0.68	351	430 220	300	588 379	667 458	746 538	82 <del>5</del> 617	904 696	983 776	*062   855	8 59.2 60.0 60.8 9 66.6 67.5 68.4
0.59	0.00	935	*014	*094	*174	*253	*333	*413	*493	*573	*652	77   78   79
0.60	0.69		812	892	972	*052	*132	*212	*293	*373	*453	1 7.7 7.8 7.9
0.61	0.70	533	614	694	774	855	935		*096	*177	*257	2 15.4 15.6 15.8 3 23.1 23.4 23.7
0.62	0.71	338	419	499	580	661	742	823	904	984	*065	4 30.8 31.2 31.6
o.63	0.72	- 1	*040	308	390	47 I *284	552 *26°	633	714	796	*602	5 38.5 39.0 39.5 6 46.2 46.8 47.4
0.65	0.73	958 774	*040 855	*121 937	*202 *019	*10I		*447 *264		*610 *428		7 53-9 54-6 55-3
0.66	0.74		674	757	839	921		*085	*168	*250	*332	8 61.6 62.4 63.2 9 69.3 70.2 71.1
0.67	0.75		497	579	662	744	827	909		*075		80   81   82
0.68	0.76		323	406	488 318	571	654 485	737 568	820	903	986 818	1 8.0 8.1 8.2
0.69	0.77	901	984	235 *o68	*151	401 *23 <u>5</u>	*318	*402	651 *485	734	*653	2 16.0 16.2 16.4 3 24.0 24.3 24.6
0.71	0.78		820	904	987	*071	*155	*239	*323	*569 *407	*491	4 32.0 32.4 32.8
0.71	0.79		659	743	827	911	995	*079	*163	*248	*332	5 40.0 40.5 41.0 6 48.0 48.6 49.2
0.73	0.80		500	585	669	754	838	922	*007	*091	*176	7 56.0 56.7 57.4
0.74	0.81	261	345	430	515	599	684	769	854		*023	8 64.0 64.8 65.6 9 72.0 72.9 73.8
0.75	0.82	959	193 *044	278 *129	363 *214	*300	533 *385	618 *470	703	788 *641	873 *727	83   84   85
0.77	0.83		898	983		*154				*497	*583	1 8.3 8.4 8.5 2 16.6 16.8 17.0
0.78	0.84		754	840		*012	*097	*183	*269	*355	*441	3 24.9 25.2 25.5
0.79	0.85		613	700				*044	*130	*217	*303	4 33.2 33.6 34.0 5 41.5 42.0 42.5
0.80		389	476	562	648	735	821	908	994	*081	*167	6 49.8 50.4 51.0
0.81			340	427	514	600	687	774	861	947	*034	7 58.1 58.8 59.5 8 66.4 67.2 68.0
0.82		991	208 *078		382 *252		556 *427	643 *514	730 *601		904 *776	9 74.7 75.6 76.5
0.84	1				*125		*300	*388		*563		86 87 88
0.85	0.90	738	826	914	*001	*089	*177	*264	*352	*440	*528	1 8.6 8.7 8.8 2 17.2 17.4 17.6
0.86	1	_			879		*055			3	*408	3 25.8 26.1 26.4
o.87 o.88				672 555		1	936			*201 *086	*290	4 34.4 34.8 35.2 5 43.0 43.5 44.0
0.89				440		1 -	706		1 33"			6 51.6 52.2 52.8
0.90				-	-		594		772	861	950	7 60.2 60.9 61.6 8 68.8 69.6 70.4
0.91		039	128	217	306	395	485	574	663		841	9 77-4 78-3 79-4
0.92		931	*020	*109	*198	*288	*377	*467	*556	*645	*735	1 8 9 9 9 9 1 1 1 8 9 9 9 9 1 1
0.93				*003		*182		1		*541	1	2 17.8 18.0 18.2
0.94		618	708		888	*079 978	*068	*158	*248	*439 *338	*428	3 26.7 27.0 27.3
0.96						879	969	*060	*150	*240	*330	4 35.6 36.0 36.4 5 44-5 45-0 45-5
0.97	1.01	_	511	601	692		873	963	*053	*144	*234	6 53.4 54.0 54.6 7 62.3 63.0 63.7
0.98							778 685	868		*050	*140 *048	8 71.2 72.0 72.8
0.99					-	-	1					0  80.1 81.0 81.9
1.00 A.	B.	0	230	321	3	4	594 <b>5</b>	6	7/0	8	950	Prop. Pts.
1 A.	i D.	U	' -	-	, 0		1 0	, ,	• •	, ,		Trope rese

ADI	ADD. $\begin{cases} \log a - \log b = A. \\ \log (a + b) = \log b + B. \end{cases}$ SUB. $\begin{cases} \log a - \log b = B. \\ \log (a - b) = \log b + A. \end{cases}$ A. B. 0 1 2 8 4 5 6 7 8 9 Prop. Pts.												
-	В.	0	1	2	8	4	5		7	8	9	Prop. Pts.	
1.00	1.04		230	321	412	503	594	685	776	867	958		
I.01	1.05	049 961	140 *053	232 *144	323 *235	414 *326	505 *418	596 *509	687 *601	779 *692	870 *783	91   92	
1.03	1.06			*058	*149	*241				*607	*699	1 9.1 9.2	
1.04	1.07		882	974	*065	*157	*249	*341	*432	*524	*616	2 18.2 18.4 3 27.3 27.6	
1.05	1.08		800	118	983 903	*07 <u>5</u>	*167	*259 *179	*351	*443	*535	4 36.4 36.8	
1.07	1.10		640	732	824	916	*000	*101	*103	*285	*278	5 45.5 46.0 6 54.6 55.2	
1.08	I.II	470	562	655	747	839	932	*024	*117	*209	*301	7 63.7 64.4 8 72.8 73.6	
1.09	1.12		486	579	671	764	857			*134		9 81.9 82.8	
1.11	1.13		412	505	598	619	783	876 804			*154		
1.12	1.14	175	340 268	432 361	525 454	547	711 640	733	897 826		*083 *013	93	
I 13	1.16		199	292	385	478	571	665	758	851	944	1 9.3 2 18.6	
1.14	1.17	037 971	131 *064	224 *157	317	411 *344	504 *408	597 *531	691	784	877	3 27.9	
1.16	1.18		999	*092	*186	*279		*467	*560	*718 *654	*748	4 137.2 5 46.5 6 55.8	
1.17	1.19	841	935	*029	*122	*216	*310	*403	*497	*591	*683		
1.18	I.20 I.21		872 811			*154	*248 *187	*342 *281	*435	*529	*623	8 74.4	
1.20	1.22		751	905 845	999	*093 *034		*222		*469 *410	*504	9 83.7	
1.21	1.23		693	787	188	975		*164			*447		
1.22	1.24	541	635	730	824	918	*013	*107	*202	*296	*390	1 94 1 9.4	
1.23	1.25	485	579	674	768	863	957	-	*146		*335	2 18.8	
I.24 I.25	I.26		524 471	619 565	714 660	808 755	903 8 <u>5</u> 0	997	*092  *039	*187 *134	*281	3 28.2 4 37.6	
1.26	1.28		418	513	608	703	797	892	987	*082		5 47.0 6 56.4	
1.27	1.29		367	462	557	652	746	841		*031		7 65.8	
1.28	1.30		316 267	411 362	507 458	553	697 648	792 743	887 838	933	*077 *029	8 75.2 9 84.6	
1.30	1.32		219	314	410	505	600	695	791	886	981		
1.31	1.33	077	172	267	363	458	553	649	744	840		95   96	
1.32	1.34	030 985	126 *081		317	*367	508 *463	*550	699 *654	794	890 *845	1 9.5 9.6	
1.33	1.35		*037		*228			*515				2 19.0 19.2 3 28.5 28.8	
1.35	1.36	898	994	*089	*185	*281	*377	*472	*568	*664	*760	4 38.0 38.4	
1.36	1.37		951	*047		*239	*335		*527		*718	6 57.0 57.6	
1.37	1.38 1.39	814 774	910 870		*062	*198 *158	*294 *254	*350	*440	*582	*678 *638	7  66.5   67.2 8   76.0   76.8	
1.39	1.40	734	830	926	*022	*119	*215	*311	*407	*503	*599	9 85.5 86.4	
1.40	1 41		792			*080	*176	*273	*369	*465	*561	-10.5	
1.41	1.42	658	754	850	946	*043	*139	*235	*332	*428	*524 *488	97	
I.42	I.43 I.44	584	717 681			*006 970	*066	*163	*259	*356	*452	1 9.7 2 19.4	
1.44	1.45	<b>5</b> 49	645	742			*031	*128	*225	*321	*418	3 29 I 4 38.8	
1.45	1.46	514	611		804	901	997	*094	*190	*287	*384 *350	4   38.8 5   48.5 6   58.2	
1.46	1.47 1.48		577 544			834	931				*318	7 67.9 8 77.6	
1.48	1.40		512		705	802	899	996	*093	*189	*286	8   77.6 9   87.3	
1.49	1.50		480	577	674		<b>8</b> 68	964	*061	*158	*255	9 107.3	
1.50	1.51	_	_	CONTRACTOR OF THE PARTY NAMED IN		740	837	Charles and the latest and the lates		-	*225	- D 134-	
A.	В.	0	1	2	3	4	5	6	7	8	1 9	Prop. Pts.	

ADI	o. { lo	g a - g (a	- log	b = 0	A. og $b$	+ <i>B</i> .		Su	в. {	log a log (a	$-\log z - \delta$	$gb = B.$ $= \log b + A.$
A.	B.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
1.50	1.51	352	449	546	643	740	837	934	*031		*225	
1.51	1.52	322 292	419	516 486	613 583	710 680	807 778	904 875	*001 972	*098 *069		
1.52	I.53 I.54	-	389 360	457	555	652	749	846	9/2	*040		
1.54	1.55	235	332	429	526	624	721	818	915	*013	*110	
1.55	1.56	207 180	304 277	402 375	499 472	596 569	693 667	791 764	888 861	985	*083 *056	
1.57		153	251	348	446	543	640	738	835		*030	97
1.58	1.59	128	225	322	420	517	6i 5	712	810	907	*005	1 9.7
1.59	1.60		175	297 273	395 370	492	590 565	687 663	78 <u>5</u> 760	882	98 <b>0</b> 956	3  29.1 4  38.8
1.61	1.62		151	248	346	444	541	639	737	834	932	5 48.5 6 58.2
1.62	1.63	030	127	225	322	420	518	616	713	811	909	7 67.9
1 63 1.64	1 64		104	202	299	397	495 *473	593 *570	690 *669	788 *766	886 *864	8   77.6 9   87.3
1.65	1.05	984. 962	*059	*179 *157	*255	*375 *353		*548			*842	,,,,
1.66	1.66	940	<b>*0</b> 38	*136	*233	*331	*429	*527	*625	*723	*821	
1.67 1.68	1.67 1.68			*115 *094			*408	*506 *486	*604	*702 *682	*800 *780	
1.69	1.69			*074						*662		
1.70	1.70		956	*054		*250	*348		*544		*741	
1.71	I.7I I.72	839	937		*133			*427	*525	*623 *605	*722	98
1.72	1.72		899	*016	*096	*194				*587		1 9.8 2 19.6
1.74	1.74		881	980	*078	*176	*274	*373	*471	*569	*667	3 29.4 4 39.2
1.75	.1.75 1.76	766	864 847	962	*050 *043	*159	*257	*355 *338	*453 *436	*552 *535	*633	5 49.0
1.77	1.77	731	830			*125					*616	7 68.6
1.78	1.78	715	813	912	*010	*108	*207	*305	*403	*502	*600	8 78.4 9 88.2
1.79	1.79		797	896		*092 *077	*175			*486 *471	*569	
1.81	1.81		766					*258				
1.82	1.82	652	751	849	948	*046	*145	*244	*342	*441	*539	
1.83	1.83		1			*032 *018				*426 *412	1	
1.84	1.84				905	*004	*102	*201	*299	*398	*497	
1.86	1.86	595	694	1	891	990			1		*483	99
1.87				1 '''			*075	*174	*273 *260	*371	*470 *457	1 9.9 2 19.8
1.89	1.89		655	753	852	951	*050	*148	*247	*346	*445	3 29.7 4 39.6
1.90	•	543								*333		5 49.5
1.91	1.91	531	630		1 - 1	926	*025	*124	*223	*321	*420	7 60.3
1.92							*002	*100	*199	*298	*397	8 79.2 9 89.1
1.94	1.94	496	59	694	792	891					*386	7 103.
1.95					1 '	1 0/					*37 <del>5</del> *364	
1.97				661	760	859	958	*057	*156	*254	*353	
1.98	1.98	45	551	650		848					*343	
2.00			-				937				*333 *323	
A.	B.	0	1	2	3	4	5	6	7		9	Prop. Pts.

 $\log a - \log b = A.$  $\log a - \log b = B.$  $\log\left(a+b\right) = \log a + (B-A).$  $\log(a-b) = \log a - (B-A)$ A. B. B-A. A. B. B-A. A. B. B-A. 1.9868 .00450 2.0955 1.9823 2.0337 2.0377 .00400 2,0920 .00350 .9878 .9833 .0348 .0388 .0932 .0967 449 448 399 349 .9842 .9887 398 348 .0359 0300. .0399 .0945 .9852 .9897 447 .0370 .0410 397 .0957 .0992 347 .9862 .9907 446 .0381 .0421 396 .0970 . 1005 346 1.9872 .00445 2.0392 2.0982 1.9917 2.0432 .00395 2,1017 .00345 .9882 .9926 444 .0403 .0443 394 .0995 .1029 344 .9891 .0414 .1008 .9935 443 .0454 393 .1042 343 .9901 442 .0425 .0465 .1020 .9945 392 .1054 342 .9911 .9955 441 .0437 .0476 391 . 1033 .1067 341 2.0487 .00440 2.0448 .00390 2,1080 1.9921 1.9965 2.1046 .00340 389 .9931 .9975 439 .0459 .0498 .1059 .1093 339 388 338 .9941 .9985 438 .0470 .0509 .1072 .1106 387 .0481 .1085 .9951 .9995 437 .0520 .1119 337 436 386 2.0005 .0493 .0532 . 1098 .1132 .9961 336 .00385 2.1144 2.0015 .00435 2.0504 2.0543 2.1111 1.9971 .00335 .0553 384 .0024 .0515 .1124 .9981 434 .1157 334 .9991 .0034 433 .0527 .0565 383 .1137 .1170 333 382 .1183 .0538 .0576 .1150 2.0001 .0044 432 332 381 .0011 .0588 .1196 .0054 431 .0550 .1163 331 .00380 2.0065 .00430 2.0561 2,0600 2.1176 2.1200 2.0021 00330 .0611 .1223 .0075 429 .0573 379 .1190 .0032 329 378 328 .0085 428 .0584 .0622 . 1203 .0042 .1236 .0052 427 .0596 .0634 .1216 .0095 377 .1249 327 .0062 426 .0607 .0645 376 . 1262 326 .0105 .1229 .00425 2.0619 2.0656 .00375 2.1275 2.0115 2.1243 .00325 2.0073 .0630 .0667 .1288 324 .0125 424 374 . 1256 .0083 .0642 .1270 .0135 423 .0679 373 . 1302 323 .0093 .0654 .0146 422 .0691 372 . 1283 .1315 322 .0104 .0666 .0156 42 I .0703 37 I . 1297 .1329 321 .0114 2.0677 2.0166 .00420 2.0714 .00370 2.1310 2.1342 .00320 2.0124 .0689 .0135 .0177 .0726 369 .1324 . 1356 419 319 368 418 318 .0187 .0701 .0738 .1338 .1370 .0145 367 .1383 317 .0156 .0198 417 .0713 .0750 .1351 416 .0762 366 316 .**0**166 .0208 .0725 .1365 .1397 .00365 2.0177 2.0218 .00415 2.0737 2.0773 2.1379 2.1410 .00315 .0228 .0785 364 .1424 414 .0749 .1393 314 .0187 363 . 1438 .0761 .0198 .0239 413 .0797 .1407 313 412 .0809 362 .1421 .1452 312 ,0208 .0249 .0773 361 .0785 . 1466 .0260 41 I .0821 .1435 311 .0219 .00360 2.1449 | 2.1480 2.0833 .00310 2.0229 2.0270 .00410 2.0797 .0281 409 .0809 .0845 359 .1463 ! .1494 309 .0240 .0857 358 308 408 .0821 .1477 . 1508 .0292 .0251 .0833 .0869 357 .1491 .1522 307 .0261 .0302 407 406 .0845 .0881 . 1505 . 1536 306 .0272 .0313 356 .00405 2.0858 2.0893 .00355 2.1520 2.1550 .00305 2.0283 2.0324 .0870 . 1564 .0294 .0334 404 .0905 354 . 1534 304 403 .0882 . 1 548 . 1578 .0917 353 303 .0345 .0305 302 402 .0895 .0930 352 . 1563 .1593 .0355 .0315 .0366 401 .0907 .0942 351 . 1577 . 1607 301 .0326

2.0955

B.

.00350

B-A.

2.0920

A.

.00400

B-A.

2.0337

В.

2.0337 A. 2.1592

A.

2 1622

В.

.00300

B-A.

$$\log a - \log b = A.$$

$$\log a - \log b = B.$$

$$\log (a + b) = \log a + (B - A).$$

$$\log (a - b) = \log a - (B - A).$$

A.	В.	B-A.	A.	В.	В-А.	Λ.	В.	В-А.
2.1592	2.1622	.00300	2.2386	2.2411	.00250	2.3358	2.3378	.00200
.1606	.1636	299	.2403	.2428	249	•3379	•3399	199
.1621	.1651	298	.2421	.2446	248	.3401	.3421	198
.1635	.1665	297	.2439	.2464	247	.3423	•3443	197
.1650	. 1680	296	.2456	.2481	246	.3446	. 3466	196
2.1665	2.1694	.00295	2.2474	2.2498	.00245	2.3468	2.3487	.00195
.1680	.1709	294	.2492	.2516	244	.3490	.3509	194
.1694	.1723	293 292	.2510	.2534	243	.3513	.3532	193
.1710	. 1739 . 1753	293	.2528	.2552	242 241	•3535	.3554	192
2.1739	2.1768	,00290	2.2564	2.2588	.00240	.3558	-3577	191
.1754	.1783	289	.2582	.2606	239	2.3581	2.3600	.00190
1770	.1799	288	.2600	.2624	238	.3627	.3646	188
.1770	.1814	287	.2618	.2642	237	.3650	.3669	187
.1800	.1829	286	.2637	.2661	236	.3673	.3692	186
2.1815	2.1844	.00285	2,2656	2.2679	.00235	2.3697	2.3715	.00185
.1830	. 1858	284	.2674	.2697	234	.3720	.3738	184
. 1846	. 1874	283	.2693	.2716	233	.3744	.3762	183
.1861	. 1889	282	.2711	.2734	232	. 3768	. 3786	182
.1877	. 1905	281	.2730	.2753	231	•3792	.3810	181
2.1892	2.1920	.00280	2.2749	2.2772	.00230	2.3816	2.3834	.00180
.1908	.1936	279	.2768	.2791	229	.3840	.3858	179
.1923	. 1951	278	.2787	.2810	228	.3865	.3883	178
.1939	.1967	277	.2806	.2829	227	.3889	.3907	177
.1955	. 1983	276	.2825	.2848	226	.3914	.3932	176
2.1971	2.1998	.00275	2.2845	2.2867	.00225	2.3939	2.3956	.00175
.1987	.2014	274	.2864	.2886	224	.3964	.3981	174
.2002	.2029	273 272	.2004	.2906	223	.3989	.4006	173
.2035	.2062	271	.2923	.2925	221	.4039	.4056	171
2.2051	2,2078	.00270	2.2943	2.2965	,00220	2,4065	2.4082	.00170
.2067	.2094	269	.2962	.2984	219	.4090	.4107	169
2083	.2110	268	.2982	.3004	218	.4116	.4133	168
.2099	.2126	267	.3002	3024	217	.4142	.4159	167
.2116	.2143	266	.3022	.3044	216	.4168	.4185	166
2,2132	2.2159	00265	2.3043	2.3064	.00215	2.4195	2.4211	.00165
.2149	.2175	264	.3063	.3084	214	.4221	.4237	164
.2165	.2191	263	.3083	.3104	213	.4248	.4264	163
.2182	.2208	262	.3104	.3125	212	.4275	.4291	162
.2198	.2224	261	.3124	.3145	211	.4302	.4318	161
2.2215	2.2241	.00260	2.3145	2.3166	.00210	2.4329	2.4345	.00160
.2232	.2258	259	.3166	.3187	209	.4356	.4372	159
.2249	.2275	258	.3187	.3208	208	.4383	•4399	158
.2266	.2292	257 256	.3208	.3229	207	.4411	.4427	157
	.2309		.3229	.3250	.00205	·4439 2.4467	·4455 2.4482	
2.2300	2.2325	254	2.3250 .327I	2.3271	204	.4495	.4510	154
.2317	.2342	253	.3293	.3313	203	.4523	.4538	153
.2351	.2376	252	.3314	3334	202	.4552	.4567	152
.2369	.2394	251	.3336	.3356	201	.4581	.4596	151
2.2386	2.2411	.00250	2.3358	2.3378	.00200	2.4609	2 4624	.00150
Α.	В.	В-А.	Α.	В.	В-А.	Α.	В.	В-А.

 $\log a - \log b = A.$  $\log (a + b) = \log a + (B - A).$   $\log a - \log b = B.$ 

 $\log(a-b) = \log a - (B-A).$ 

Α.	В.	B-A.	Α.	В.	В-А.	A.	В.	B-A.
2.4609	2.4624	.00150	2.6373	2.6383	.00100	2.9385	2.9390	.00050
.4638	.4653	149	.6416	.6426	.00099	.9474	.9479	49
.4668	.4683	148	.6461	.6471	98	.9563	.9568	48
.4697	.4712	147	.6505	.6515	97	.9655	.9660	47
.4727	.4742	146	.6550	.6560	96	.9748	·9753	46
2.4757	2.4772	،00145	2.6596	2.6606	.00095	2.9844	2.9848	.00045
.4787	.4801	144	.6642	.6651	94	2.9941	2.9945	44
.4817	.4831	143	.6688	.6697	93	3.0041	3.0045	43
.4848	.4892	142 141	.673 <b>5</b> .6783	.6744	92 91	.0143	.0147	42
			2.6831	2.6840			.0252	41
2.4910	2.4924	.00140 139	.6880	.6889	.00090 89	3.0356	3.0360	.00040
.4941	·4955 ·4986	139	.6928	.6937	88	.0578	.0582	39 38
.5004	.5018	137	.6978	.6987	87	.0694	.0698	37
.5036	. 5050	136	.7028	.7037	86	.0813	.0817	36
2.5068	2.5081		2.7079	2.7088	.00085	3.0935	3.0939	.00035
.5100	.5113	.00135 134	.7131	.7139	84	.1061	.1064	34
.5133	.5146	133	.7183	.7191	83	.1191	.1194	33
.5165	.5178	132	.7236	.7244	82	.1324	.1327	33
.5199	.5212	131	.7289	.7297	81	.1463	.1466	31
2.5232	2.5245	.00130	2.7343	2.7351	.00080	3.1606	3.1609	.00030
.5266	.5279	129	.7398	.7406		.1753	.1756	20
.5299	.5312	128	.7453	.7461	79 78	.1905	.1908	28
•5333	.5346	127	.7509	.7517	77	.2063	.2066	27
.5368	. 5381	126	.7566	.7574	76	.2226	.2229	26
2.5402	2.5415	.00125	2.7623	2.7631	.00075	3.2396	3.2399	.00025
•5437	•5449	124	.7682	.7689	74	.2575	.2577	24
.5472	.5484	123	.7741	.7748	73	.2760	.2762	23
.5508	.5520	122	.7741 .7801	.7808	72	.2952	.2954	22
•5544	.5556	121	.7862	.7869	71	.3154	.3156	21
2.5580	2.5592	.00120	2.7923	2.7930	.00070	3.3366	3.3368	.00020
.5616	.5628	119	.7985	.7992	69	.3590	.3592	19
.5653	.5665	118	.8050	.8057	68	.3825	.3827	18
.5690	. 5702	117	.8114	.8121	67	.4072	.4074	17
.5727	•5739	116	.8180	.8187	66	•4335	•4337	16
2.5765	2.5776	.00115	2.8245	2.8252	.00065	3.4617	3.4619	.00015
.5803	.5814	114	.8313	.8319	64	•4917	.4918	14
.5841	.5852	113	.8381	.8387	63	•5237	.5238	13
.5880	.5891	112	.8451	.8457	62	•5587	.5588	11
.5919	.5930	III	.8521	.8527	1	. 5964	.5965	
2.5958	2.5969	.00110	2.8593	2.8599	.00060	3.6377	3.6378	.00010
.5998	.6009	109	.8666	.8672	59 58	.6835	.6836	09
.6038	.6049		.8741 .8816	.8822		•7345	7926	07
.6079	.6090	107	.8893	.8899	57	.7925 .8595	.8596	06
	.6131	.00105	2,8971	2.8977	.00055	3.9390	3.9391	.00005
2.6161	2.6172	104	.9051	.9056	54	4.0355	4.0355	04
.6202 .6244	.6212	103	.9031	.9137	53	4.1600	4.1600	03
.6244	.6297	103	.9215	.9220	52	4.3375	4.3375	02
.6329	.6339		.9300	.9305	51	4.6367	4.6367	10
2.6373	2.6383	.00100	2.9385	2.9390	.00050	∞ .	.00	.00000
A.	В.	В-А.	A.	В.	B-A.	A.	В.	В-Л.
	1		1	1	<u> </u>	<u>'</u>	<del>'</del>	

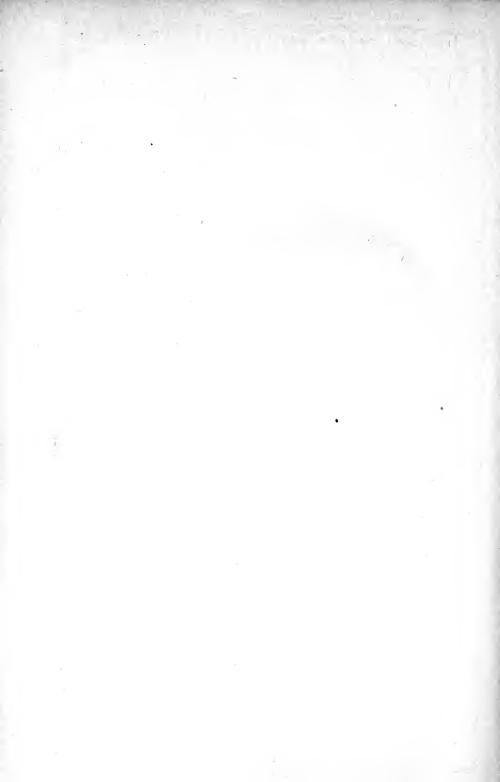
## TABLE VIL

## SQUARES OF NUMBERS.

No.	Square.								
0	0	20	400	40	1600	60	3600	80	6400
1	1	21	441	41	1681	61	3721	8 r	6561
2	4	22	484	42	1764	62	3844	82	6724
3	9	23	529	43	1849	63	3969	83	6889
4	16	24	576	44	1936	64	4096	84	7056
5	25	25	625	45	2025	65	4225	85	7225
6	36	26	676	46	2116	66	4356	86	7396
7	49	27	729	47	2209	67	4489	87	7569
8	64	28	784	48	2304	68	4624	88	7744
9	18	29	841	49	2401	69	4761	89	7921
10	100	30	900	50	2500	70	4900	90	8100
11	121	31	961	51	2601	71	5041	91	8281
12	144	32	1024	52	2704	72	5184	92	8464
13	169	33	1089	53	2809	73	5329	93	8649
14	196	34	1156	54	2916	74	5476	94	8836
15	225	35	1225	55	3025	75	5625	95	9025
16	256	36	1296	56	3136	76	5776	96	9216
17	289	37	1369	57	3249	77	5929	97	9409
18	324	38	1444	58	3364	78	6084	98	9604
19	361	39	1521	59	3481	79	6241	99	9801
20	400	40	1600	60	3600	80	6400	100	10000

	100	200	300	400	5 🍑	6	700	844	900		Diff.
00	100	400	900	1600	2500	3600	4900	6400	8100	00	1
01	102	404	906	1608	2510	3612	4914	6416	8118	01	3
02	104	408	912	1616	2520	3624	4928	6432	8136	04	5
03	106	412	918	1624	2530	3636	4942	6448	8154	09	7
04	108	416	924	1632	2540	3648	4956	6464	8172	16	9 11 13
05	110	420	930	1640	2550	3660	4970	6480	8190	25	
06	112	424	936	1648	2560	3672	4984	6496	8208	36	
07	114	428	942	1656	2570	3684	4998	6512	8226	49	15
08	116	432	948	1664	2580	3696	5012	6528	8244	64	17
09	118	436	954	1672	2590	3708	5026	6544	8262	81	19*
10	121	441	96 <b>1</b>	1681	2601	3721	5041	6561	8281	00	21
11	123	445	967	1689	2611	3733	5055	6577	8299	21	23
12	125	449	973	1697	2621	3745	5069	6593	8317	44	25
13	127	453	979	1705	2631	375 <b>7</b>	5083	6609	8335	69	27
14	129	457	985	1713	2641	3769	5097	6625	8353	96	29*
15	132	462	992	1722	2652	3782	5112	6642	8372	25	31
16	134	466	998	1730	2662	3794	5126	6658	8390	56	33
17	136	470	1004	1738	2672	3806	5140	6674	8408	89	35*
18	139	475	1011	1747	2683	3819	5155	6691	8427	24	37
19	141	479	1017	1755	2693	3831	5169	6707	8445	61	39*
20	144	484	1024	1764	2704	3844	5184	6724	8464	00	41
2I	146	488	1030	1772	2714	3856	5198	6740	8482	4I	43
22	148	492	1036	1780	2724	3868	5212	6756	8500	84	45*
23	151	497	1043	1789	2735	3881	5227	6773	8519	29	47
24	153	501	1049	1797	2745	3893	5241	6789	8537	76	49*
25	156	506	1056	1806	2756	3906	5256	6806	8556	25	51
26	158	510	1062	1814	<b>27</b> 66	3918	5270	6822	8574	76	53*
27	161	515	1069	1823	2777	3931	5285	6839	8593	29	55
28	163	519	1075	1831	2787	3943	5299	6855	8611	84	57*
29	166	524	1082	1840	2798	3956	5314	6872	8630	41	59*
80	169	529	1089	1849	2809	3969	5329	6889	8649	00	61
31	171	533	1095	1857	2819	3981	5343	6905	8667	61	63*
32	174	538	1102	1866	2830	3994	5358	6922	8686	24	65
33	176	542	1108	1874	2840	4006	5372	6938	8704	89	67*
34	179	547	1115	1883	2851	4019	53 <sup>8</sup> 7	6955	8723	56	69*
35	182	552	1122	1892	2862	4032	5402	6972	8742	25	71
36	184	556	1128	1900	2872	4044	5416	6988	8760	96	73*
37	187	561	1135	1909	2883	4057	5431	7005	8779	69	75*
38	190	566	1142	1918	2894	4070	5446	7022	8798	44	77*
39	193	571	1149	1927	2905	4083	5461	7039	8817	21	79*
40	196	576	1156	1936	2916	4096	5476	7056	8836	00	82
41	198	580	1162	1944	2926	4108	5490	7072	8854	81	83*
42	201	585	1169	1953	2937	4121	5505	7089	8873	64	85*
43	204	590	1176	1962	2948	4134	5520	7106	8892	49	87*
44	207	595	1183	1971	2959	4147	5535	7123	8911	36	89*
45	210	600	1190	1980	2970	4160	5550	7140	8930	25	91*
46	213	605	1197	1989	2981	4173	5565	7157	8949	16	93*
47	216	610	1204	1998	2992	4186	5580	7174	8968	09	95*
48	219	615	1211	2007	3003	4199	5595	7191	8987	04	97*
49	222	620	1218	2016	3014	4212	5610	7208	9006	01	99*
50	225	625	1225	2025	3025	4225	5625	7225	9025	00	

	144	200	3	400	5 🍑	644	700	800	940		Diff.
50	225	625	1225	2025	3025	4225	5625	7225	9025	20	1
51	228	630	1232	2034	3036	4238	5640	7242	9044	01	3
52	231	635	1239	2043	3047	4251	5655	7259	9063	04	5
53	234	640	1246	2052	3058	4264	5670	7276	9082	09	7
54	237	645	1253	2061	3069	4277	5685	7293	9101	16	9
55	240	650	1260	2070	3080	4290	5700	7310	9120	25	11
56	243	655	1267	2079	3091	4303	5715	7327	9139	36	13
57	246	660	1274	2088	3102	4316	5730	7344	9158	49	15
58	249	665	1281	2097	3113	4329	5745	7361	9177	64	17
59	252	670	1288	2106	3124	4342	5760	7378	91 <b>96</b>	81	19*
60	256	676	1296	2116	3136	4356	5776	7396	9216	00	91
61	259	681	1303	2125	3147	4369	5791	7413	9235	21	23
62	262	686	1310	2134	3158	4382	5806	7430	9254	44	25
63	265	691	1317	2143	3169	4395	5821	7447	9273	69	27
64	268	696	1324	2152	3180	4408	5836	7464	9292	96	29*
65	272	702	1332	2162	3192	4422	5852	7482	9312	25	31
66	275	707	1339	2171	3203	4435	5867	7499	9331	56	33
67	278	712	1346	2180	3214	4448	5882	7516	93 <b>50</b>	89	35*
68	282	718	1354	2190	3226	4462	5898	7534	9370	24	37
69	285	723	1361	2199	3237	4475	5913	7551	9389	61	39*
70	289	729	1369	2209	3249	4489	5929	7569	9409	00	41
71	292	734	1376	2218	3260	4502	5944	7586	9428	41	43
72	295	739	1383	2227	3271	4515	5959	7603	9447	84	45**
73	299	745	1391	2237	3283	4529	<b>5</b> 975	7621	9467	29	47
74	302	750	1398	2246	3294	4542	5990	7638	9486	76	49*
75	306	756	1406	2256	3306	4556	6006	7656	9506	25	51
76	309	761	1413	2265	3317	4569	6021	7673	<b>9</b> 525	76	53*
77	313	767	1421	2275	33 <sup>29</sup>	4583	6037	7691	9545	29	55
78	316	772	1428	2284	334 <sup>0</sup>	4596	6052	7708	9564	84	57*
79	320	778	1436	2294	335 <sup>2</sup>	4610	6068	7726	9584	41	59*
80	324	784	1444	2304	3364	4624	6084	7744	9604	00	61
81	3 <sup>2</sup> 7	789	1451	2313	3375	4637	6099	7761	9623	61	63*
82	33 <sup>1</sup>	795	1459	2323	3387	4651	6115	7779	9643	24	63
83	334	800	1466	2332	3398	4664	6130	7796	9662	89	67*
84	338	806	1474	2342	3410	4678	6146	7814	9682	56	69*
85	342	812	1482	2352	3422	4692	6162	7832	9702	25	71
86	345	817	1489	2361	3433	4705	6177	7849	9721	96	73*
87	349	823	1497	237I	3445	4719	6193	7867	9741	69	75*
88	353	829	1505	238I	3457	4733	6209	7885	9761	44	77*
89	357	835	1513	239I	3469	4747	6225	7903	9781	21	79*
90	361	841	1521	2401	3481	4761	6241	7921	9801	00	81
91	364	846	1528	2410	3492	4774	6256	7938	9820	81	83*
92	368	852	1536	2420	3504	4788	6272	7956	9840	64	85*
93	372	858	1544	2430	3516	4802	6288	4074	9860	49	87*
94	376	864	1552	2440	3528	4816	6304	7992	9880	36	89*
95	380	870	1560	2450	3540	4830	6320	8010	9900	25	91*
96	384	876	1568	2460	3552	4844	6336	8028	9920	16	93*
97	388	882	1576	2470	3564	4858	6352	8046	9940	09	95*
98	392	888	1584	2480	3576	4872	6363	8064	9960	04	97*
99	396	894	1592	2490	3588	4886	6384	8082	9980	01	99*
100	400	900	1600	2500	3600	4900	6400	8100	10000	∞	1

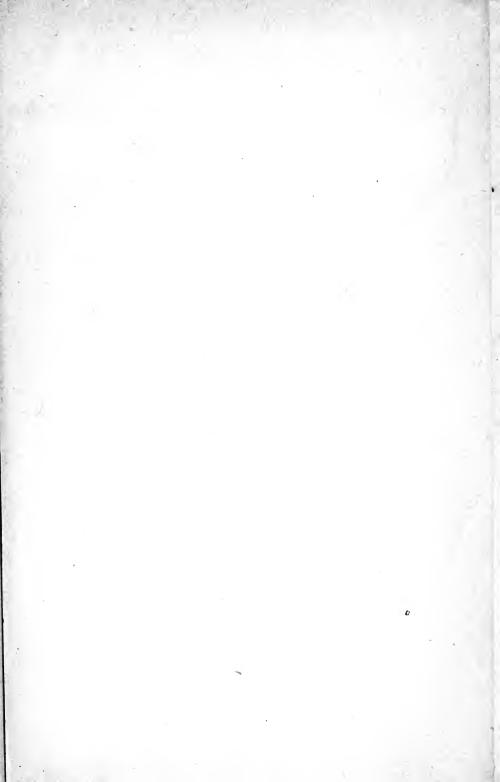


D.	н. м. s.	H. M. S.	H.M.S. 100 <sup>2</sup>	D.	H. M. S.	H. M. S.	H.M.S. 100°
d.	h. m. s.	m. s.	s.	d.	h. m. s.	m, s.	s.
0.01	0 14 24	o \$.64	0.09	0.51		7 20.64	4.41
0.02	0 28 48	o 17.28	0.17	0.52		7 29.28	4.49
0.03	0 43 12	o 25.92	0.26	0.53		7 37.92	4.58
0.04	0 57 36	o 34.56	0.35	0.54		7 46.56	4.67
0.05	1 12 0	o 43.20	0.43	0.55		7 55.20	4.75
0.06	1 26 24	o 51.84	0.52	0.56	13 26 24	8 3.84	4.84
0.07	1 40 48	1 0.48	0.60	0.57	13 40 48	8 12.48	4.92
0.08	1 55 12	1 9.12	0.69	0.58	13 55 12	8 21.12	5.01
0.09	2 9 36	1 17.76	0.78	0.59	14 9 36	8 29.76	5.10
0.10	2 24 0	1 26.40	0.86	0.60	14 24 0	8 38.40	5.18
0.11	2 38 24	1 35.04	0.95	0.61	14 38 24	8 47.04	5.27
0.12	2 52 48	1 43.68	1.04	0.62	14 52 48	8 55.68	5.36
0.13	3 7 12	1 52.32	1.12	0.63	15 7 12	9 4.32	5.44
0.14	3 21 36	2 0.96	1.21	0.64	15 21 36	9 12.96	5.53
0.15	3 36 0	2 9.60	1.30	0.65	15 36 0	9 21.60	5.62
0.16	3 50 24	2 18.24	1.38	o.66	15 50 24	9 30.24	5.70
0.17	4 4 48	2 26.88	1.47	o.67	16 4 48	9 38.88	5.79
0.18	4 19 12	2 35.52	1.56	o.68	16 19 12	9 47.52	5.88
0.19	4 33 36	2 44.16	1.64	o.69	16 33 36	9 56.16	5.96
0.20	4 48 0	2 52.80	1.73	o.70	16 48 0	10 4.80	6.05
0.21	5 2 24	3 1.44	1.81	0.71	17 2 24	10 13.44	
0.22	5 16 48	3 10.08	1.90	0.72	17 16 48	10 22.08	
0.23	5 31 12	3 18.72	1.99	0.73	17 31 12	10 30.72	
0.24	5 45 36	3 27.36	2.07	0.74	17 45 36	10 39.36	
0.25	6 0 0	3 36.00	2.16	0.75	18 0 0	10 48.00	
0.26	6 14 24	3 44.64	2.25	0.76	18 14 24	10 56.64	
0.27	6 28 48	3 53.28	2.33	0.77	18 28 48	11 5.28	
0.28	6 43 12	4 1.92	2.42	0.78	18 43 12	11 13.92	
0.29	6 57 36	4 10.56	2.51	0.79	18 57 36	11 22.56	
0.30	7 12 0	4 19.20	2.59	0.80	19 12 0	11 31.20	
0.31	7 26 24	4 27.84		0.81	19 26 24	11 39.84	7.00
0.32	7 40 48	4 36.48		0.82	19 40 48	11 48.48	7.08
0.33	7 55 12	4 45.12		0.83	19 55 12	11 57.12	7.17
0.34	8 9 36	4 53.76		0.84	20 9 36	12 5.76	7.26
0.35	8 24 0	5 2.40		0.85	20 24 0	12 14.40	7.34
0.36 0.37 0.38 0.39 0.40	8 38 24 8 52 48 9 7 12 9 21 36 9 36 0	5 11.04 5 19.68 5 28.32 5 36.96 5 45.60		o.86 o.87 o.88 o.89 o.90		12 23.04 12 31.68 12 40.32 12 48.96 12 57.60	
0.41	9 50 24	5 54.24	3.54	0.91	21 50 24	13 6.2a	7.86
0.42	10 4 48	6 2.88	3.63	0.92	22 4 48	13 24.88	7.95
0.43	10 19 12	6 11.52	3.72	0.93	22 19 12	13 23.52	8.04
0.44	10 33 36	6 20.16	3.80	0.94	22 33 36	12 2.16	8.12
0.45	10 48 0	6 28.80	3.89	0.95	22 48 0	15 40.80	8.21
0.46 0.47 0.48 0.49 0.50	11 45 36	6 37.44 6 46.08 6 54.72 7 3.36 7 12.00	4.15	0.96 0.97 0.98 0.99 1.00	23 2 24 23 16 48 23 31 12 23 45 36 24 0 0	13 49.44 13 58.08 14 6.72 14 15.36 14 24.00	8.38 8.47 8.55

O	h. m.	0	h. 1n.	0	h. m.	,	m.s.	"	s.						
0 1 2 3 4	0 0 0 4 0 8 0 12 0 16	60 61 62 63 64	4 0 4 4 4 8 4 12 4 16	120 121 122 123 124	8 0 8 4 8 8 8 12 8 16	180 181 182 183 184	12 0 12 4 12 8 12 12 12 16	240 241 242 243 244	16 0 16 4 16 8 16 12 16 16	300 301 302 303 304	20 0 20 4 20 8 20 12 20 16	0 1 2 3 4	0 0 0 4 0 8 0 12 0 16	0 1 2 3 4	0.000 0.066 0.133 0.200 0.266
5 6 7 8 9	0 28	65 66 67 68 69		125 126 127 128 129	8 20 8 24 8 28 8 32 8 36	185 186 187 188 189	12 20 12 24 12 28 12 32 12 36	245 246 247 248 249	16 20 16 24 16 28 16 32 16 36	305 306 307 308 309	20 20 20 24 20 28 20 32 20 36	5 7 8 9	0 20 0 24 0 28 0 32 0 36	56 78 9	0.333 0.400 0.466 0.533 0.600
10 11 12 13 14	0 44 0 48 0 52	70 71 72 73 74	4 44	130 131 132 133 134	8 40 8 44 8 48 8 52 8 56	190 191 192 193 194	12 40 12 44 12 48 12 52 12 56	250 251 252 253 254	16 40 16 44 16 48 16 52 16 56	310 311 312 313 314	20 40 20 44 20 48 20 52 20 56	10 11 12 13 14	0 40 0 44 0 48 0 52 0 56	10 11 12 13 14	o.666 o.733 o.800 o.866 o.933
15 16 17 18 19	I 8	75 76 77 78 79	5 12	135 136 137 138 139	9 0 9 4 9 8 9 12 9 16	195 196 197 198 199	13 0 13 4 13 8 13 12 13 16	255 256 257 258 259	17 0 17 4 17 8 17 12 17 16	315 316 317 318 319	21 0 21 4 21 8 21 12 21 16	15 16 17 18	I 0 I 4 I 8 I 12 I 16	15 16 17 18	I.000 I.066 I.133 I.200 I.266
20 21 22 23 24	I 24 I 28	80 81 82 83 84	5 20 5 24 5 28 5 32 5 36	140 141 142 143 144	9 20 9 24 9 28 9 32 9 36	200 201 202 203 204	13 20 13 24 13 28 13 32 13 36	260 261 262 263 264	17 20 17 24 17 28 17 32 17 36	320 321 322 323 324	21 20 21 24 21 28 21 32 21 36	20 21 22 23 24	I 20 I 24 I 28 I 32 I 36	20 21 22 23 24	I.333 I.400 I.466 I.533 I.600
25 26 27 28 29	I 48	85 86 87 88 89	5 44 5 48 5 52	145 146 147 148 149	9 40 9 44 9 48 9 52 9 56	205 206 207 208 209	13 40 13 44 13 48 13 52 13 56	265 266 267 268 269	17 40 17 44 17 48 17 52 17 56	325 326 327 328 329	21 40 21 44 21 48 21 52 21 56	25 26 27 28 29	1 40 1 44 1 48 1 52 1 56	25 26 27 28 29	1.666 1.733 1.800 1.866 1.933
30 31 32 33 34	2 4 2 8	90 91 92 93 94	6 8	150 151 152 153 154	IC 0 IO 4 IC 8 IO 12 IC I6	210 211 212 213 214	14 0 14 4 14 8 14 12 14 16	270 271 272 273 274	18 0 18 4 18 8 18 12 18 16	330 331 332 333 334	22 0 22 4 22 8 22 12 22 16	30 31 32 33 34	2 0 2 4 2 8 2 12 2 16	30 31 32 33 34	2.000 2.066 2.133 2.200 2.266
35 36 37 38 39	2 28	95 96 97 98 99	6 28	155 156 157 158 159	10 20 10 24 10 28 10 32 10 36	215 216 217 218 219	14 20 14 24 14 28 14 32 14 36	275 276 277 278 279	18 20 18 24 18 28 18 32 18 36	335 336 337 338 339	22 20 22 24 22 28 22 32 22 36	35 36 37 38 39	2 20 2 24 2 28 2 32 2 36	35 36 37 38 39	2.333 2.400 2.466 2.533 2.600
42 43 44	2 44 2 48	100 101 102 103 104	6 44 6 48 6 52 6 56	160 161 162 163 164	10 40 10 44 10 48 10 52 10 56	220 221 222 223 224	14 40 14 44 14 48 14 52 14 56	280 281 282 283 284	18 40 18 44 18 48 18 52 18 56	340 341 342 343 344	22 40 22 44 22 48 22 52 22 56	40 41 42 43 44	2 40 2 44 2 48 2 52 2 56	40 41 42 43 44	2.666 2.733 2.800 2.866 2.933
45 46 47 48 49	3 12		7 4 7 8 7 12		11 8 11 12		15 0 15 4 15 8 15 12 15 16		19 0 19 4 19 8 19 12 19 16		23 8 23 12			45 46 47 48 49	3.000 3.066 3.133 3.200 3.266
50 51 52 53 54	3 24 3 28 3 32	110 111 112 113 114	7 24 7 28 7 32	1	11 24 11 28 11 32	230 231 232 233 234	15 24 15 28 15 32	290 291 292 293 294	19 32	350 351 352 353 354	23 24 23 28 23 32	50 51 52 53 54	3 24 3 28 3 32	50 51 52 53 54	3.400 3.466 3.533 3.500
55 56 57 58 59	3 48	115 116 117 118 119	7 44 7 48 7 52	175 176 177 178 179	11 52	238	15 52	295 296 297 298 299	19 48 19 52	355 356 357 358 359	23 48 23 52	55 56 57 58 59	3 48	55 56 57 58 59	3.800 3.866

Mean T. Co		Cor	orrection. Mean T.		+				Correction.		Corr. for min. and sec.			
h.	m.	m.	s.	h.	m.	m.	s.	h.	m.	m.	s.	m.	s.	s.
0	0 10 20 30 40 50	0	0.00 1.64 3.29 4.93 6.57 8.21	8	0 10 20 30 40 50	I	18.85 20.50 22.14 23.78 25.42 27.07	16	0 10 20 30 40 50	2	37.70 39.35 40.99 42.63 44.28 45.92	0	10 20 30 40 50	0.03 0.05 0.08 0.11 0.14 0.16 0.19
1	0 10 20 30 40 50	0	9.86 11.50 13.14 14.78 16.43 18.07	9	0 10 20 30 40 50	I	28.71 30.35 31.99 33.64 35.28 36.92	17	0 10 20 30 40 50	2	47.56 49.20 50.85 52.49 54.13 55.77	2	20 30 40 50 0 10 20 30	0.22 0.25 0.27 0.30 0.33 0.36 0.38
6	0 10 20 30 40 50	0	19.71 21.36 23.00 24.64 26.28 27.93	10	0 10 20 30 40 50	1	38.56 40.21 41.85 43.49 45.14 46.78	18	0 10 20 30 40 50	3	57.42 59.06 0.70 2.34 3.99 5.63	3	40 50 0 10 20 30 40 50	0.44 0.47 0.49 0.52 0.55 0.57 0.60 0.63
3	0 10 20 30 40 50	0	29.57 31.21 32.86 34.50 36.14 37.78	11	0 10 20 30 40 50	I	48.42 50.06 51.71 53.35 54.99 56.64	19	0 10 20 30 40 50	3	7.27 8.92 10.56 12.20 13.84 15.49	4	0 10 20 30 40 50	0.66 0.68 0.71 0.74 0.77 0.79
4	0 10 20 30 40 50	0	39.43 41.07 42.71 44.35 46.00 47.64	12	0 10 20 30 40 50	1 2	58.28 59.92 1.56 3.21 4.85 6.49	20	0 10 20 30 40 50	3	17.13 18.77 20.42 22.06 23.70 25.34	6	10 20 30 40 50	0.85 0.88 0.90 0.93 0.96 0.99 1.01
5	0 10 20 30 40 50	0	49.28 50.92 52 57 54.21 55.85 57.50	13	0 10 20 30 40 50	2	8.13 9.78 11.42 13.06 14.70 16.35	21	0 10 20 30 40 50	3	26.99 28.63 30.27 31.91 33.56 35.20	7	20 30 40 50 0 10 20 30	I 04 I.07 I.10 I.12 I.15 I.18 I.21 I 23
6	0 10 20 30 40 50	0	59.14 0.78 2.42 4.07 5.71 7.35	14	0 10 20 30 40 50	2	17.99 19.63 21.28 22.92 24.56 26.20	22	0 10 20 30 40 50	3	36.84 38.48 40.13 41.77 43.41 45.06	8	40 50 0 10 20 30 40 50	1.26 1.29 1.31 1.34 1.37 1.40 1.42 1.45
7	0 10 20 30 40 50	1	9.00 10.64 12.28 13.92 15.57 17.21	15	0 10 20 30 40 50	2	27.85 29.49 31.13 32.77 34.42 36.06	23	0 10 20 30 40 50	3	46.70 48.34 49.98 51.63 53.27 54.91	9	0 10 20 30 40 50	1.48 1.50 1.53 1.56 1.59 1.62

Sid.	T.	Correction.		Sid. T.		Correction.		1		Correction.		Corr. for min. and sec.		
h.	m.	m.	s.	h.	m.	m.	s.	h.	m.	m.	s.	m.	s.	s.
O	0 10 20 30 40 30	O	0.00 1.64 3.28 4.92 6.55 8.19	8	0 10 20 30 40 50	1	18.64 20.28 21.91 23.55 25.19 26.83	16	0 10 20 30 40 50	2	37.27 38.91 40.55 42.19 43.83 45.46	0	10 20 30 40 50	0.03 0.05 0.08 0.11 0.14 0.16 0.19
1	0 10 20 30 40 50	0	9.83 11.47 13.11 14.74 16.38 18.02	9	0 10 20 30 40 50	1	28.47 30.10 31.74 33.38 35.02 36.66	17	0 10 20 30 40 50	2	47.10 48.74 50.38 52.02 53.66 55.29	2	20 30 40 50 0 10 20 30	0.22 0.25 0.27 0.30 0.33 0.35 0.38
2	0 10 20 30 40 50	0	19.66 21.30 22.94 24.57 26.21 27.85	10	0 10 20 30 40 50	1	38.30 39.93 41.57 43.21 44.85 46.49	18	0 10 20 30 40 50	3	56.93 58.57 0.21 1.85 3.48 5.12	3	40 50 0 10 20 30 40 50	0.44 0.47 0.49 0.52 0.55 0.57 0.60 0.63
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