# MINING TABLES HATCH AND VALENTINE 




## MINING TABLES



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## MINING TABLES

BEING A COMPARISON OF THE UNITS OF WEIGHT, measure, Currency, mining area, Etc., of DIFFERENT COUNTRIES; TOGETHER WITH TABLES, CONSTANTS \& OTHER DATA USEFUL TO MINING ENGINEERS AND SURVEYORS

BY

## F. H. HATCH, Рн.D., F.G.S.

MEMBER OF THE INSTITUTE OF CIVIL ENGINEERS MEMBER OF THE AMERICAN INSTITUTE OF MINING ENGINEERS MEMBER OF THE INSTITUTION OF MINING AND METALLURGY LATE PRESIDENT OF THE GEOLOGICAL SOCIETY OF SOUTH AFRICA

AND

## E. J. VALLENTINE, F.G.S.

MEMBER OF THE FEDERATED INSTITUTE OF MINING ENGINEERS ASSOCIATE OF THE INSTITUTION OF MINING AND METALLURGY

## PREFACE

Most engineers get together a quantity of formulae, constants and other data useful to them in the exercise of their profession, which are not always to be found in text-books. The authors, having arranged and tabulated a collection of this nature for their own use, decided to print it, believing that its pub lication would be of service to other workers in the same field.

The work thus begun has extended beyond the original plan, especially in regard to the tables of weight and measure, which have been compiled from the latest publications of the "Bureau international des Poids et Mesures" and of the Board of Trade. It appears that most published equivalents of the British Imperial and Metric measures of length are based either on a comparison made in Paris in 1818 by Arago and Kater, or on a comparison made in 1866 by Capt. A. R. Clarke of the Ordnance Survey. Similarly, Professor Miller's determination in 1844 of the avoirdupois pound as equal to 453.59265 grammes forms the usua! basis of comparison for the weights of the British Imperial and Metric systems. The values adopted in this book are derived from determinations since made under the direction of the International Committee of Weights and Measures and of the Board of Trade, and legalised by Order in Council of the 19th May, 1898. In like manner the equivalents of the Russian weights and measures adopted are based on the results of Prof. D. Mendelieff's work in 1897, which were subsequently embodied in the Russian Weights and Measures Law of June, 1899.

The definitions of the electrical units given in Section II. of Part II. are taken chiefly from the Reports made to the Board of Trade in 1892 and 1894 by the Electrical Standards Committee, and the Order in Council made by her late Majesty on the
${ }^{2} 3$ rd August, 1894. They are defined in terms of the fundamental units of length (the centimetre), mass (the gramme), and time (the second), from which this system of units has come to be known as the c.g.s. (centimetre-gramme-second) system.

The compilation of the short section on thermal units disclosed the existence of much confusion in text-books, largely due to the various thermometric scales in use. There is also an absence of any agreement as to the terminology of the units. For instance, as Swinburne points out, there is no name for the unit of difference of temperature, "degree" being almost as primitive as " mark" or "notch." ${ }^{1}$ Again, the British thermal unit or pound-degree (Fahrenheit) has no name; and "calorie" may mean either the gramme-degree (Centigrade) or the kilogram-degree (Centigrade). In regard to specific heat, thermal capacity, calorific power and thermal efficiency, there is a lack of authoritative definition such as has fixed for all time the electrical units.

The mining data collected in Part V. refer rather to the physical properties of ore-bodies than to the mechanical devices for their extraction. Thus, hoisting, pumping and ventilation, to which many special treatises have been devoted, are not dealt with. On the other hand, tables are given by which the calculation and valuation of ore-reserves are assisted and simplified. The latest information regarding the question of underground temperatures is summarised. The various methods in use in different countries for expressing gold ore values and for stating copper prices are compared. Finally, there is a section on mining areas which has been carefully compiled from the laws now in force in the Colonies and in foreign countries where mining is carried on.

The data relating to surveying which comprise Part VI. include a description of the conventional methods in practical use for the coordination of survey points, also a description of the use of the tacheometer, and a table for the calculation of heights and distances from tacheometric readings.

[^0]
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## PART I. WEIGHTS AND MEASURES.

SECTION I. STANDARD UNITS.

## THE METRIC SYSTEM.

Length.-The original intention of the founders of the Metric System was to select from nature itself some permanent and invariable unit of length, which could be measured with a high degree of precision, and might therefore be reproduced at will. The metre, which was the unit selected, was intended to be equal to one ten-millionth of a terrestrial meridian contained between the north pole and the equator.* The geodetic survey from Barcelona to Dunkirk, from which the length of the arc of the meridian was computed, was conducted by Méchain and Delambre between the years 1792 and 1798 .

A platinum standard was then constructed and deposited in the Archives of the French Republic in 1799, being legalised in the same year. This standard is known as the Metre of the Archives. It is a platinum bar 25 millimetres broad, 4 millimetres thick, and, being an 'end' standard, is exactly one metre long at $0^{\circ} \mathrm{C}$.

Subsequent researches showed that the length of the arc differs from that determined by the original triangulation to an extent equivalent to about o.1 millimetre in the standard metre. Nevertheless, the Metre of the Archives is adhered to as the unit of length, although its reference to the earth's quadrant has been abandoned.

In 1875 the International Bureau of Weights and Measures was established at Breteuil, near Paris, under a Metric Convention signed by twenty different High Contracting States $\dagger$ for the

[^1]purpose of constructing, restoring, and verifying new metric standards (now known as the international prototypes) to replace the standards of the Archives. Accurate copies of the new standards were also to be constructed for all the contracting States. Thirty-one standards of iridio-platinum, with a cross-section nearly of the shape of the letter X , known as the 'Tresca' form, were made, and compared with the Metre of the Archives and with one another. These were approved of by the International Committee in 1889, the standard most nearly approximating to the length of the Metre of the Archives being selected as the International Prototype Standard Metre and deposited in the Observatory at Breteuil. The remaining national prototype standards were distributed by lot to the different contracting States.

The British Prototype Standard Metre "is represented by the distance marked by two fine lines on the iridio-platinum standard bar numbered 16 , when at the temperature of $\circ^{\circ}$ Centigrade. This bar is deposited with the Board of Trade." *

An elaborate series of researches carried on at the International Bureau of Weights and Measures has shown that it is possible, after all, to realise the desire of the founders of the Metric System to refer the metre to a natural unit ; for the standard can be expressed in terms of wave-lengths of light. In 1893 Professor A. A. Michelson found that, by the interference method, 1553163.5 wave-lengths of the red ray of cadmium, measured in air at $15^{\circ} \mathrm{C}$., under an atmospheric pressure of 760 millimetres, are equal to the length of the International Prototype Standard Metre. $\dagger$

Weight.-The unit of weight in the Metric System is the Gramme, which was originally defined "as the absolute weight of a volume of pure water equal to a cube of the one-hundredth part of a metre, and at the temperature of melting ice." As this unit, however, is rather small for accurate weighings, a weight of 1000 grammes was adopted as the practical standard. The first step in the preparation of the original standard kilogram (1000

[^2]grammes) was the determination of the weight in vacuo of a cubic decimetre ( 1000 cubic centimetres) of distilled water at its maximum density. This was found to be $18,827.15$ grains of the Pile de Charlemagne. A platinum standard of that weight was then constructed and deposited in the Archives of the French Republic in 1799. It is known as the Kilogram of the Archives. In form it is cylindrical, with height equal to the diameter and with its edges slightly rounded. When the construction of new standards for the metre and the kilogram was authorised under the Metric Convention, it was decided, since the kilogram did not represent the mass of a cubic decimetre of water with scientific accuracy, to adopt the Kilogram of the Archives as the standard unit of weight, and subsequently to determine its true relation to the mass of a cubic decimetre of distilled water at its temperature of maximum density. Accordingly, in 1879, three iridio-platinum standard kilograms were made, cylindrical in form, and of a density of 2 1.55. They were compared with the Kilogram of the Archives and with one another ; and in 1883 the one known as K III. was adopted as the International Prototype Standard Kilogram. It has since been designated by 刑, although it bears no mark. Forty cylindrical iridio-platinum national prototype kilograms were then made, and compared with筑 and with one another. They were approved of by the International Committee in 1889, and distributed by lot to the different contracting States. The British Prototype Standard Kilogram "is represented by the cylindrical iridio-platinum standard kilogram weight numbered 18 , which is deposited with the Board of Trade." *

Capacity.-The unit of capacity in the Metric System is the Litre, which was intended to be the volume of a cubic decimetre, so that a litre of distilled water at $4^{\circ} \mathrm{C}$. should weigh exactly a kilogram. But on further investigation it was found that this was not scientifically accurate, and it was therefore decided by the International Committee to define the Litre as "the volume occupied by the mass one kilogram of pure water at its maximum density and under normal atmospheric pressure," this definition being sanctioned at the General Conference of 1901. Recent determinations of the weight in vacuo of a cubic decimetre of distilled water at its temperature of maximum

[^3]density ( $4^{\circ}$ C.) made independently by Benoît, Chappuis, Macé de Lépinay and Buisson, gave very uniform results, the mean of which was found to be 0.999974 kilogram.* This value has been provisionally adopted by the Bureau international des Poids et Mesures pending the completion of a further elaborate series of experiments now being made at the Bureau, the results of which will be announced at the sexennial General Conference of the delegates representing the contracting States of the Metric Convention, which is to be held at Paris in October, 1907. It is anticipated that any variation between the provisional and the new values will only affect the sixth decimal place. Consequently, for all practical purposes a litre can be regarded as the volume of a cubic decimetre, the error involved being only 26 parts in a million.

The British Standard Litre "is represented by the capacity at $0^{\circ}$ Centigrade of the cylindrical brass measure marked 'Litre, $1897^{\prime}$ (which is deposited with the Board of Trade), and having a diameter equal to one half its height. This Litre at $\circ^{\circ}$ Centigrade when full contains one kilogram of distilled water at the temperature of $4^{\circ}$ Centigrade, under an atmospheric pressure equal to that represented by a column of mercury 760 millimetres high at $0^{\circ}$ Centigrade, at sea level, and at latitude $45^{\circ}$; the weighing being made in air, but reduced by calculation to a vacuum." $\dagger$

The Metric System is in use in the following countries, to the exclusion of the older systems, except where noted :
Argentine. Almost exclusively used.
Austria. Old system still sometimes used.
Belgium.
Brazil. In common use.
Bulgaria. Old system not entirely supplanted.
Chile. In common use.
Colombia. Both old and metric systems used.
Denmark. Used by State Railways ; but not in general use. It has been made compulsory by a law passed in March, 1907.
Ecuador. Old system used in commerce, metric officially.
Egypt. Old system used in commerce, metric officially and by engineers, etc.
Finland.

[^4]
## France.

Germany. In general use, but old measures sometimes encountered.
Great Britain. Optional, but not in general use.
Greece. Very little used.
Guatemala. Used officially but not generally.
Hungary. In general use : old system dying out.
Italy. In general use, but old system still found in the south.
Japan. Not in general use.
Luxemburg. Old system practically obsolete.
Mexico. In general use : old system dying out
Montenegro. In general use.
Netherlands. Almost entirely used, but old system sometimes encountered.
Norway.
Peru. Only used by Government.
Philippine Islands.
Porto Rico.
Portugal.
Russia. Optional, but not in general use.
Servia. In general use.
Siam. Used by railways and public works.
Spain. In general use, but old measures still encountered.
Sweden.
Switzerland.
United States of America. Optional, but not in general use.
Uruguay.
Venezuela. Only used officially.

## THE BRITISH IMPERIAL SYSTEM.

Length. -The British Imperial Standard unit of length is the Yard. The 'line' standard constructed by Bird in 1760 having been lost in the fire which destroyed the Houses of Parliament in 1834 , the present standard yard was made by Messrs. Baily and Sheepshanks in 1843, by reference to the 5 -foot brass Shuckburgh scale of 1796 , the two iron standards made for the Ordnance Survey in $1826-7$, the brass tubular scale of the Royal Astronomical Society, and the Kater scale of 1831 made for the Royal Society.

It is a solid bar of 'Baily's metal' (i6 parts by weight of
copper, $2 \frac{1}{2}$ of tin, and $\mathbf{I}$ of zinc) 38 inches long, with a crosssection I inch square. Near its ends are two circular wells half an inch deep. At the bottom of these wells, and consequently on the 'neutral plane' of the bar, are gold studs, on which the fiducial lines are engraved, the distance between them forming the British Imperial Standard Yard at a temperature of $62^{\circ}$ Fahr. It was legalised by the Standards Act of 1855. It is preserved at the Standards Office, Westminster, and has been in the custody of the Board of Trade since 1866.

Thirty-nine copies of this standard were made of the same material and dimensions. Four of these are specially designated Parliamentary Copies, which, by the Weights and Measures Act of 1878 , must be compared with each other once in every ten years and with the Imperial Standard once in every twenty years, in order to ensure the perpetuation of the standard. These Parliamentary Copies are stamped with the temperature at which they represent the true standard, namely:
P.C. 2 in the custody of the Royal Mint : standard at $61.94^{\circ}$ F.

| P.C. 3 | $"$ | $"$ | Royal Society : standard at $62.10^{\circ} \mathrm{F}$. |
| :--- | :--- | :--- | :--- |
| P.C. 4 |  |  |  |$\quad " \quad$ Royal Observatory, Greenwich : standard

P.C. 5 " New Palace, Westminster: standard at $61.98^{\circ} \mathrm{F}$.

The remaining thirty-five copies were distributed to various nations and scientific institutions.

Weight.-The British Imperial standard unit of weight is the Avoirdupois Pound of 7000 grains. The standard troy pound of 5760 grains having been destroyed in the fire of 1834 , the avoirdupois pound of 7000 grains was substituted as the standard, on the recommendation contained in a report submitted by the Parliamentary Standards Committee, Dec. 21, 1841 ; and the present standard pound was constructed by Prof. W. H. Miller in 1844 by reference to a troy pound belonging to the Royal Society, and a troy pound the property of Prof. Schumacher. It is of platinum, cylindrical in form, 1.35 inches high and 1.15 inches in diameter, with a density of 21.1572 . It has a small groove in its circumference to permit of its being lifted with an ivory fork, and is marked 'P.S. 1844. i lb.' * on its upper surface. It was legalised in 1855, and is preserved at the Standards

[^5]Office, Westminster, in the custody of the Board of Trade. As in the case of the unit of length, there are four Parliamentary Copies. Compared with the standard,
No. I P.C., which is in the custody of the Royal Mint, is $0.0005^{1}$ grain too heavy.
No. 2 P.C., in the custody of the Royal Society, is 0.00089 grain too light.
No. 3 P.C., in the custody of the Royal Observatory, Greenwich, is 0.00178 grain too light.

No. 4 P.C., in the custody of the New Palace, Westminster, is 0.00314 grain too light.
The Weights and Measures Act of 1878 provides that one additional Parliamentary copy of the Standard Yard and of the Pound should be made. These were constructed and approved of by the Board of Trade, and were accordingly legalised by an Order in Council of Aug. 3, 1886.* The Board of Trade secondary standards, by which all other standards are tested, are required by the Act to be re-verified once every five years by comparison with these new Parliamentary copies.

Capacity:-The British Imperial standard unit of capacity is the Gallon, which is the volume of ten Imperial standard pounds of distilled water weighed in air against brass weights, with the water and air at a temperature of $62^{\circ}$ Fahr. and under a barometric pressure of 30 inches. The standard is of brass, with a diameter equal to its depth, and bears the date of 1828 . It is in the custody of the Board of Trade, and is deposited at the Standards Office, Westminster. A standard Bushel (equal to 8 gallons) is also preserved at the Standards Office as the unit of dry measure It is of gun-metal, with a diameter equal to twice its depth. It dates from 1824, and was verified in 1825.

The Weights and Measures Act of 1824 gives the weight of a cubic inch of distilled water under standard conditions as 252.458 grains, a value derived from weighings made ly Sir George Shuckburgh in $1798 \dagger$ and Captain Henry Kater in $182 \mathrm{I} . \ddagger$ On this basis, 277.274 and 2218.192 cubic inches are the volumes of the Imperial gallon and bushel respectively.

[^6][^7]In r889, Mr. H. J. Chaney determined the mass of a cubic inch of distilled water, freed from air, weighed in air against brass weights of a density of 8.143, with the water and air at a temperature of $62^{\circ}$ Fahr. and the barometer at 30 inches, to be $25^{2.286}$ grains $\pm .0002$ grain.* The weight of a cubic foot of such water under similar conditions would therefore be 62.27860 I lbs., and the volume of the Imperial gallon and of the bushel 277.46288 and 2219.70304 cubic inches respectively. Although no direct determination of the weight of a cubic inch of water has since been made, the foregoing values have been superseded. It has been found that I litre $=1.000026$ cubic decimetres (see p. 4), and that 4.5459631 litres $=1$ Imperial gallon (see p. 15) ; therefore, under standard conditions:
The weight of 1 cubic inch of water at $62^{\circ} \mathrm{F} .=252.3253$ grains.

$$
\text { I cubic foot of water at } 62^{\circ} \mathrm{F} .=62.2883 \mathrm{lbs} \text {. }
$$

$\left.\begin{array}{c}\text { and the vol- } \\ \text { ume of }\end{array}\right\}$ I Imperial gallon $\quad\left\{\begin{array}{r}=277.420 \text { cubic } \\ \text { inches. }\end{array}\right.$
These values have been provisionally adopted by the Board of Trade Standards Department.

The Imperial Weights and Measures are now legally in force in the following Colonies, etc.:

| Antigua. | Jamaica. | Sierra Leone. |
| :--- | :--- | :--- |
| Barbadoes. | Malta. | Straits Settlements. |
| Bermuda. | Natal. | South Australia. |
| British Guiana. | Nevis. | St. Christopher. |
| British Honduras. | New Brunswick. | St. Helena. |
| Canada. | New South Wales. | St. Vincent. |
| Cape of Good Hope. | New Zealand. | Transvaal. |
| Cyprus. | Nova Scotia. | Tobago. |
| Dominica. | Orange RiverColony. | Trinidad. |
| Grenada. | Queensiand. | Vancouver's Island. |
| Hong Kong | Rhodesia. | Victoria. |
|  | Western Australia. $\dagger$ |  |

An Act of 1897 permits the use of Metric Weights and Measures in the United Kingdom, and provides that the Board of Trade standards shall include metric standards.

[^8]
## THE UNITED STATES OF AMERICA.

The weights and measures of the United States are practically identical with those of the British Imperial System, with the exception of the measures of capacity which, although defined in units having the same names and sub-divisions, have quite different volumes.

The use of the Metric System is recognised by an Act of 1866. Prototype standard meters, Nos. 21 and 27 , and kilograms, Nos. 4 and 20 , were received from the International Bureau of Weights and Measures in 1889, and Meter No. 27 and Kilogram No. 20 were adopted as the National Prototype Standards in 1890. In Bulletin No. 26 of the 5th April, 1893, issued by the U.S. Coast and Geodetic Survey with the approval of the Secretary of the Treasury, the United States Government recognises "the International Prototype Meter and Kilogram* as fundamental standards," and states that "the customary units, the yard and the pound, will be derived therefrom in accordance with the Act of July 28, 1866." The metric equivalents of the yard and the pound legalised by this Act differ in a slight degree from the British equivalents legalised in 1898 , but the differences are so small that, for all practical purposes, they may be disregarded (see pp. 36 and 40). In 1901 the custody of the national standards was transferred from the Coast and Geodetic Survey to the Bureau of Standards, which was established in that year under the Department of Commerce and Labor.

Liquid Measure.-The standard unit of liquid measure is the U.S. Gallon, which is derived from the Queen Anne wine gallon of 1707. It is defined as having a volume of 231 cubic inches. It is also the standard unit of Apothecaries' Fluid Measure.

Dry Measure.-The standard unit of dry measure is the U.S. Bushel, which is derived from the old Winchester "struck" bushel. It is defined as having a volume of $2150.4^{2}$ cubic inches. The U.S. Bushel measure has the form of an inverted frustum of a right cone of the following dimensions

[^9](inside measurement): top diameter, $19 \frac{1}{2}$ inches; bottom diameter, $18 \frac{1}{2}$ inches; depth, 8 inches.

The dry measures are considerably larger than the liquid measures of the same name; for instance, the $d r y$ U.S. gallon $\left(\frac{1}{8}^{\text {th }}\right.$ bushel $)=268.8025$ cubic inches, while the liquid U.S. gallon $=231$ cubic inches.

## RUSSIA.

Lengtn.-In 1833 the Russian units of length were defined in terms of liritish feet, and a standard Sagene (equal to 7 British feet) was constructed and compared with the British Imperial Standard Yard, and subsequently legalised by an Act of Oct. 1835. A standard Archine, equal to $\frac{1}{3}$ sagene, constructed by Prof. Kupffer, is recognised as the standard unit of length by a law passed in June 1899 . It is an iridio-platinum 'line' standard of Tresca form, standard at $16 \frac{2}{3}^{\circ} \mathrm{C}$. $\left(62^{\circ} \mathrm{F}\right.$.), and is inscribed H ir 1894. It is defined as equal to 28 British inches or $0.711200 \pm 0.000001$ metre.

Weight.-The standard unit of weight is the Funt or Russian pound. The standard Funt is of iridio-platinum of a density of 21.51 at $16 \frac{20}{3} \mathrm{C}$., and is inscribed ${\underset{\text { II }}{ }}_{\mathrm{H}}^{1894}$. It was reproduced from the platinum funt of 1835 , which was derived from a funt of 1747 . It is defined as equal to $0.40951241 \pm 0.00000001$ kilogram.

Capacity.-The standard units of liquid and dry measures are respectively the Vedro and the Tchetverik. The Vedro is defined as the volume of 30 funts, weighed in vacuo, of distilled water at a temperature of $16 \frac{2}{3}^{\circ} \mathrm{C}$. The Tchetverik is defined as the volume of 64 funts of such water under similar conditions.

The national standards are deposited at St. Petersburg.
The law of June 1899 , which became effective on Jan. 1 , 190c, permits the use of the Metric System.

## CHINA.

The Weights and Measures of China have different local names and values.* The only standards legally in use for international

[^10]purposes are those adopted in the foreign treaties for the payment of duties at the Foreign Maritime Customs. By Rule IV. of the Rules of Trade signed at Shanghai on Nov. 8, 1858, the weight of a Pikul (Tam) of 100 Katis (Kan or Chin) is defined as equal to $133 \frac{1}{3} \mathrm{lbs}$. avoirdupois, and the length of a Chang of 10 Ch'ih as equal to 14I British inches. Similar equations were adopted in the Rules of Trade appended to other foreign treaties. The standard Chinese weights verified for Hong Kong by the Board of Trade in 1900-0 were a Tam of $133 \frac{1}{3}$ lbs., a Kan of $1 \frac{1}{3}$ lbs., and a Tael of $1 \frac{1}{3}$ oz. avoirdupois. The Standard Ying-tsao Ch'ih or foot of the Chinese Board of Works, from which all measures connected with the Revenue, whether of length, capacity, or weight, are derived, is approximately equal to $\mathbf{1 2 . 5}$ British inches;* but different local commercial standards obtain throughout the whole of China. A standard Chinese 'Chek' (Ch'ih) of $14 \frac{5}{8}$ inches, divided into 10 'Tsun,' and each Tsun into 10 'Fan,' was verified by the Board of Trade Standards Department in 1896-97 for Hong Kong, where both British and Chinese weights and measures are used. $\dagger$ Measures of capacity are seldom used-grains, liquids, etc., being mostly bought and sold by weight.

## JAPAN.

In March i891, a law was passed, with effect from Jan. i, 1893, permitting the use of the Metric System. The same Act re-organised the national weights and measures, and defined them in terms of the metric units, prototype standards of which had been received in 1889.

Length.-The standard unit of length is the Shaku, which is defined as $\frac{10}{3}$ of the length of the national iridio-platinum prototype metre, standard at $0^{\circ} .15$ Centigrade. The unit of square or land measure is the $B u$ or $T s u b o$, which is equal to a square, each side of which measures 6 shakus.

Weight.-The standard unit of weight is the Krean, which is defined as equal to $\frac{15}{4}$ of the weight of the national iridioplatinum prototype kilogram. The density of a Japanese standard iridio-platinum Kwan weight of 3750 grammes was determined

[^11]as 21.5423 at $0^{\circ} \mathrm{C}$. by the Board of Trade Standards Department in 1896-97.*

Capacity.-The standard unit of capacity is the Shô, which is defined as equal to r.8039r litres.

The national standards are in the custody of the Minister of Agriculture and Commerce at Tokio.

## BRITISH INDIA.

Various weights and measures are in use in India, the local standards being kept by the district and municipal authorities.

Length. - The British Imperial yard, foot, and inch are statutory by the Measures of Length Act of 1889. This Act does not refer to square measures. A brass standard yard was verified by the Board of Trade Standards Department for the Government of India in 1889. It is inscribed: "Accurate copy of Imperial Standard Yard, 1889, Calcutta. Standard Yard at 85 degrees Fahrenheit." At the same time two similar standards were also supplied to the Presidencies of Bombay and Madras. $\dagger$

Weight.-The standard unit of weight is the Tola, which is equal to 180 grains, the weight of the rupee. Primary standard iridio-platinum weights of 30,20 , and 10 Tolas were verified by the Board of Trade Standards Department for the Calcutta and Bombay Mints in $1892 . \ddagger$

Capacity.-Measures of capacity are seldom used by the natives -grain, liquids, etc., being usually bought and sold by weight. Measures are made to contain certain weights of some commodities. They are really 'measures of weight,' and are named by the weights which they represent.

## THE STRAITS SETTLEMENTS.

The Straits Settlements Ordinance No. VII. of 1886 assimilates the weights and measures of the colony to the British Imperial System, with the exception of certain customary native weights, such as the Tahil, Kati, and Pikul, to which are assigned values in terms of British Imperial weights (see p. 30). The Board

[^12]of Trade Standards Department assisted in the drawing up of the Ordinance, and verified a large number of copies of the Imperial standards for the colony.* They have also supplied other standards, such as the Kati $=1 \frac{1}{3}$ lbs. avoirdupois, and a quarterChupah (2 Imperial gills), which contains ten fluid ounces of distilled water at $62^{\circ}$ Fahr. $\dagger$ The standards of the colony are deposited at Singapore.

## SOUTH AFRICA.

In Natal, the British Imperial is the legal system of weights and measures. $\ddagger$ This is also the case in Cape Colony, British Bechuanaland, the Orange River Colony, the Transvaal, and Rhodesia, except that there is a special system of land measure. The unit of land measure is a foot " of such length that 1000 of such feet shall be equal to 1033 English feet as now by law defined and established for lineal measurement in England." § This unit is termed the Cape Foot, and is a survival of the Rhynland foot used during the Dutch occupation of the Cape of Good Hope. Twelve Cape feet make a Rood and 600 square roods a Morgen. This system is used in all land surveys, and standard Roods are deposited with the Surveyor-General of each Colony.

## EGYPT.

The use of the metric system is permitted by a decree issued by the Khedive Ismail in 1873. It has been adopted by the government for all purposes except the measurement of areas of land and the tonnage of ships, and is used by the public works, post office, customs and railway departments. A decree issued by the Khedive Mohamed Tewfik on the 28th April 1891, with effect from the ist of January 1892, recognises the International Prototype Metre and Kilogram || as fundamental

[^13]standards from which the Egyptian units of length, weight, and capacity are derived by means of equivalents stated in the decree (see page ${ }_{17}$ ).

The old weights and measures are still in general use, the units being as follows:

Length.-There are several different units of length, namely: the Dirâ̂ baladi or 'town' diraâ; the Dirâ̂ mimari, which is used in building, etc. ; the Pike Istambuli or Constantinople Pike, used in measuring cloth; and the Kassabah, used in land surveying. The Feddan of $333 \frac{1}{3}$ square kassabahs is the legal unit of land area.

Weight.-The standard unit of weight is the Dirhem (drachm).
Capacity.--The standard unit of capacity is the Ardeb.

## SECTION II. COMPARISON OF STANDARD UNITS.

## THE METRIC AND BRITISH IMPERIAL SYSTEMS COMPARED.

In $1894-95$ a comparison of the Yard with the Metre was made under the directions of the Board of Trade and the International Committee of Weights and Measures. The Parliamentary Copy of the Standard Yard, P.C. VI.. was first carefully compared with the Imperial Standard Yard at the Standards Office, Westminster. It was then taken to the International Bureau of Weights and Measures at Breteuil and compared with the International Prototype Standard Metre,* and the following result was confirmed at a meeting of the Metric Conference in September 1895. $\dagger$ At $16^{\circ} .667$ Centigrade the Imperial Yard is equal to 0.9143992 Metre, the temperature $16^{\circ} .667 \mathrm{C}$. being taken as equal to $62^{\circ}$ Fahrenheit ; or, conversely, at $16^{\circ} .667$ C. $\left(62^{\circ}\right.$ F. $)$ the Metre is equal to $39.370{ }^{1} 3$ inches. $\ddagger$

In 1883 a comparison of the Pound and the Kilogram was made in the same manner. A copy of the pound was compared

[^14]with the Imperial Standard at the Standards Office, and then with the International Prototype Kilogram at the International Bureau, with the following result: the Imperial Avoirdupois Pound weighed in vacuo at $0^{\circ}$ Centigrade is equal to $453 \cdot 5924277$ Grammes; or, conversely, the Kilogram is equal to $\mathbf{1 5 4 3 2}^{\mathbf{5}} \mathbf{2 . 3 5 6 3 9}$ Grains.*

In comparing the units of capacity of the two systems, the weight in vacuo of distilled water at $4^{\circ} \mathrm{C}$. contained in a Litre is compared with the weight in air of distilled water at $16^{\circ} .667 \mathrm{C}$. ( $62^{\circ} \mathrm{F}$.) contained in a Gallon. The Imperial Gallon is equal to 4.5459631 Litres ; or, conversely, the Litre is equal to 1.75980 Pints. The Board of Trade equivalents of Metric and Imperial Weights and Measures, legalised by an Order in Council of May 19 , 1898, are based on the foregoing comparisons, which may be summarised as follows:

$$
\begin{aligned}
& 1 \text { Yard }=0.9143992 \text { Metre. } \\
& \text { 1 Metre }=39.370113 \text { Inches. } \\
& \text { I Pound }=453.5924277 \text { Grammes. } \\
& \text { I Kilogram }=15432.35639 \text { Grains. } \\
& \text { I Gallon } \\
& \text { I Litre } \\
& =4.5459631 \text { Litres. } \\
& =1.75980 \text { Pints. }
\end{aligned}
$$

The French Toise and the Austrian Klafter were the units of length formerly used in most of the European geodetic surveys. They are, however, no longer in use, having been superseded by the Metre. Compared with the Imperial Yard,

$$
\begin{aligned}
& \text { I Toise }=2.13151116 \text { Yards. } \\
& \text { I Klafter }=2.07403483 \text { Yards. } \\
& \text { I Metre }=1.09361426 \text { Yards. } \dagger
\end{aligned}
$$

## THE UNITED STATES, THE METRIC, AND THE BRITISH IMPERIAL SYSTEMS.

Since 1893 the International Prototype Meter and Kilogram (deposited at Breteuil Observatory, near Paris) have been regarded in the United States as fundamental standards, from

[^15]which all units of weight and measure are derived in terms of the equivalents legalised by the Act of July 1866.* The U.S. yard is reproduced from the meter in terms of the equation: I yard $=\frac{3600}{3937}$ meter, while the British equivalent is: I yard $=0.9143992$ metre. Therefore
$$
\text { I U.S. Yard }=1.000002875 \text { Imp. Yards, }
$$
a difference of only 2.875 in a million. U.S. and British measures of length can therefore be regarded as practically' identical.

The British equivalent:
I Avoirdupois Pound $=453.5924277$ Grammes
has been adopted by the U.S. Bureau of Standards. U.S. and British weights are therefore exactly alike.

The Bureau of Standards equivalents of the U.S. units of capacity are:
I U.S. Liquid Gallon of 231 cubic inches $=3.785434497$ Liters. $\dot{\dagger}$
I U.S. Bushel of 2150.42 cubic inches $=0.3523928160$ Hectoliter.
The British equivalents are : 1 Imp. Gallon $=4.545963$ I Litres, and I Imp. Bushel $=0.363677048$ Hectolitre. Therefore

I U.S. Liquid Gallon $=0.83270$ Imp. Gallon.
I Imp. Gallon $\quad=1.20091$ U.S. Gallons.
I U.S. Bushel $\quad=0.96897$ Imp. Bushel.
I Imp. Bushel $=1.03202$ U.S. Bushels.

COMPARISON OF THE RUSSIAN WITH THE METRIC AND THE BRITISH IMPERIAL SYSTEMS.

In 1897 Prof. D. Mendelieff, acting on the authority of the Russian Government, determined the values of the Russian standard units in terms of those of the Metric System by a series of experiments made at the International Bureau of Weights and Measures, which values were subsequently legalised by the Act of June 1899 (see page 10). The units of capacity are derived from the unit of weight by reference to the volume of distilled water at $16 \frac{2}{3}^{\circ} \mathrm{C}$. The equivalents on which the conversion

[^16]tables given on page 42 are based, may be summarised as follows :
\[

$$
\begin{aligned}
& \text { I Archine }=28 \text { British Inches or } 0.711200 \text { Metre.* } \\
& \text { I Funt }=409.51241 \text { Grammes. } \\
& \text { I Vedro }=12.2993285 \text { Litres. } \\
& \text { I Tchetverik }
\end{aligned}
$$
\]

## COMPARISON OF THE EGYPTIAN WITH THE METRIC AND THE BRITISH IMPERIAL SYSTEMS.

A decree issued by the Khedive Mohamed Tewfik on the 28th April, 1891, with effect from the rst of January, 1892, defines the Egyptian units of length, weight, and capacity in terms of the international metric standards (deposited at Breteuil Observatory, near Paris) as follows:
${ }_{1}$ Diraâ baladi $=0.580$ Metre.
I Diraâ mimari $=0.750$ Metre.
I Kassabah $\quad=3.550$ Metres.
I Dirhem $=3.12$ Grammes.
I Ardeb $=1.98$ Hectolitres.
The decree also embodies a table of the legal Metric and British Imperial equivalents of the Egyptian weights and measures (see page $5^{2}$ ).

In 1902 and 1903 the Board of Trade Standards Department verified standard Rotl and Oke weights for the Sudan Customs, I rotl being taken as equal to 0.990492 lb . and I oke as equal to 2.751367 lbs., these being the Egyptian legal equivalents. $\dagger$
*28 British inches $=0.7111995$ metre.

+ Board of Trade Reports, 334 of 1903, p. 7, and 348 of 1904, p. 6.


## SECTION III. TABLES.

THE METRIC SYSTEM.
Weight.


* The abbreviation 'kilo' is frequently used for kilogram.

Lineal Measure.

|  | Unit. |  | Symbol. | Value in Metres. |
| :---: | :---: | :---: | :---: | :---: |
| Micron, - | - - | - - | $\mu$. | . 000 oor m. |
| Millimetre, | - - | - - | mm . | .Ool m. |
| Centimetre, | - - | - - | cm . | . OI m . |
| Decimetre, | - - | - - | dm. | . I m. |
| Metre, - | - - | - - | m . | 1 m . |
| Dekametre, | - - | - - | dam. | 10 m . |
| Hectometre, | - - | - - | hm . | 100 m . |
| Kilometre, | . - | - - | km. | I, 000 m . |
| Myriametre, | - - | - - | Mm . | $10,000 \mathrm{~m}$. |
| Megametre, | - - | - - |  | $\mathrm{I}, 000,000 \mathrm{~m}$. |

Square Measure.

| Unit. | Symbol. | Value in SQuare Metres. |
| :---: | :---: | :---: |
| Square millimetre, - | $\mathrm{mm} .{ }^{2}$ | . $000001 \mathrm{~m} .{ }^{2}$ |
| Square centimetre, - | $\mathrm{cm} .{ }^{2}$ | . $0001 \mathrm{~m} .^{2}$ |
| Square decimetre, - | dm. ${ }^{2}$ | . $\mathrm{OI} \mathrm{m} .{ }^{2}$ |
|  |  | $\mathrm{Im} .{ }^{2}$ |
| Are (square dekametre), | $\mathrm{a} .-\mathrm{dm} .^{2}$ | $100 \mathrm{~m} .{ }^{2}$ |
| Hectare (square hectometre), | ha. -hm. ${ }^{2}$ | $10,000 \mathrm{~m} .{ }^{2}$ |
| Square kilometre, - . | km . ${ }^{2}$ | 1,000,000 m. ${ }^{2}$ |

Cubic Measure.

| Unit. | Symbol. | $\underset{\substack{\text { Malue in } \\ \text { Meres. }}}{\text { cubic }}$ |
| :---: | :---: | :---: |
| Cubic millimetre, | $\mathrm{mm} .^{3}$ | . $000000001 \mathrm{~m} .{ }^{3}$ |
| Cubic centimetre, | $\mathrm{cm} .{ }^{3 *}$ | . $0000001 \mathrm{~m} .{ }^{3}$ |
| Cubic decimetre, - | dm. ${ }^{3}$ | . 001 l m. ${ }^{3}$ |
| Cubic metre or stere, | $\mathrm{m} .{ }^{3}$ or s. | $1 \mathrm{~m} .{ }^{3}$ |

* The symbol c.c. is frequently used for the cubic centimetre.

Measure of Capacity.

| Unir. | Symbol. | Value in Litres. | Volume. |
| :---: | :---: | :---: | :---: |
| Millilitre, | ml . | . 0011. | $1 \mathrm{~cm} .^{3}$ |
| Centilitre, | cl. | .or 1. | $10 \mathrm{cm}.{ }^{3}$ |
| Decilitre, | d1. | .11. | $100 \mathrm{~cm} .^{3}$ |
| Litre, | 1. | 11. | $1 \mathrm{dm} .^{3}$ |
| Dekalitre, | dal. | 101. | $10 \mathrm{dm} .{ }^{3}$ |
| Hectolitre, | hl. | 1001. | $100 \mathrm{dm} .{ }^{3}$ |
| Kilolitre, | kl. | 10001. | $1 \mathrm{~m} .{ }^{3}$ |

Note.-The weight in vacuo of a cubic decimetre of distilled water at $4^{\circ} \mathrm{C}$. is .999974 kilogram (see page 4). Therefore for all practical purposes a litre may be regarded as the volume of a cubic decimetre, the error involved being only 26 parts in a million.
The above metric symbols are those adopted by the Comité international.des Poids et Mesures. $\dagger$

## THE BRITISH IMPERIAL SYSTEM.

Avoirdupois or Commercial Weight.
27.34375 grains $=1$ drachm.

16 drachms $=1$ ounce (oz.) $=437.5$ grains.
16 ounces $=1$ pound (lb. $)=256$ drachms $=7000$ grains.
28 pounds $=1$ quarter (qr.) $=448$ ounces.
4 quarters $=1$ hundredweight (cwt.) $=112$ pounds.
20 hundredweights $=1$ ton $=80$ quarters $=2240$ pounds.
I stone $=14$ pounds : i cental $=100$ pounds:
20 centals $=1$ 'short' ton of 2000 pounds.
The ton of 2240 lbs. is usually termed the 'long' ton, in contradistinction to the 'short' ton of 2000 lbs . To convert long into short tons, multiply by 1.12 ; or from short into long, divide by 1.12.

Ounces (avoir.) in Decimals of a Pound (avoir.).

| Ounces. | Pound. | Ounces. | Pound. | Ounces. | Pound. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{1}{4}$ | . 0156 | 5 | .3125 | $1{ }^{1} \frac{1}{2}$ | . 6562 |
| $\frac{1}{2}$ | . 0312 | $5 \frac{1}{2}$ | . 3437 | 11 | . 6875 |
| $\frac{3}{4}$ | . 0468 | 6 | . 375 | $11 \frac{1}{2}$ | . 7187 |
| 1 | . 0625 | 61 | . 4062 | 12 | . 75 |
| $1 \frac{1}{2}$ | . 0937 | 7 | . 4375 | $12 \frac{1}{2}$ | .7812 |
| 2 | . 1250 | 712 | . 4687 | 13 | . 8125 |
| $2 \frac{1}{2}$ | . 1562 | 8 | . 5 | $13 \frac{1}{2}$ | . 8437 |
| 3 | . 1875 | $8 \frac{1}{2}$ | . 5312 | 14 | . 875 |
| $3{ }^{\frac{1}{2}}$ | . 2187 | 9 | . 5625 | $14^{\frac{1}{2}}$ | . 9062 |
| 4 | . 25 | $9 \frac{1}{2}$ | . 5937 | 15 | . 9375 |
| 412 | .2812 | 10 | . 625 | $15^{\frac{1}{2}}$ | . 9687 |

## Troy Weight.

(Used for the weighing of precious metals.)
24 grains = I pennyweight (dwt.).
20 pennyweights $=I$ ounce (oz. troy) $=480$ grains.
12 ounces $=1$ pound (lb. troy) $=240$ pennyweights $=5760$ grains.
The grain is the same in both troy and avoirdupois weights.
The troy pound is seldom used.
The Diamond Carat and the Pearl Grain, although in general use, are not legal weights. They are thus defined by the Board of Trade: $151 \frac{1}{2}$ diamond carats or 600 pearl grains $=1$ troy ounce; therefore a diamond carat $=3 . \dot{1} 68 \dot{j}$ grains ( 205.30 milligrams) and a pearl grain $=0.8$ grain ( 5 I .84 milligrams).*

* Board of Trade Reports, 330 of 1888, p. 13, and 302 of 1889, p. 2.

Comparison of Avoirdupois and Troy weights.

$$
\begin{aligned}
& \text { I lb. avoir. }=14.58 \dot{3} \quad \text { oz. troy, logarithm }=1.1638568 . \\
& \text { I oz. } \quad==0.911458 \dot{3} \text { oz. }, \quad " \quad=9.9597368 \text {. } \\
& \text { I oz. troy }=1.097143 \text { oz. avoir., } \quad=0.0402632 \text {. }
\end{aligned}
$$

Grains and Dwts. in Decimals of a Troy Oz.

|  | rain | $\begin{aligned} &=.0021 \\ & s=.0042 \end{aligned}$ | Oz. |  |  | $\begin{aligned} & =.05 \\ & =.1 \end{aligned}$ | , |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | " | $=.0063$ | ", | 3 | ," | $=.15$ | ," |
| 4 | , | $=.0083$ | , | 4 | ," | $=.2$ | ", |
| 5 | " | =.0104 | " | 5 | , | $=.25$ | " |
| 6 | " | $=.0125$ | " | 6 | ," | $=.3$ | " |
| 7 | , | $=.0146$ | " | 7 | " | $=.35$ | " |
| 8 | , | $=.0167$ | " | 8 | ,, | $=.4$ | " |
| 9 | , | $=.0188$ | ," | 9 | " | $=.45$ | , |
| 10 | " | $=.0208$ | ", | 10 | " | $=.5$ | " |
| 11 | " | =. 0229 | ", | 11 | , | $=\cdot 55$ | " |
| 12 | " | $=.025$ | ,' | 12 | " | $=.6$ | " |
| 13 | " | $=.027 \mathrm{I}$ | " | 13 | " | $=.65$ | " |
| 14 | " | $=.0292$ | " | 14 | " | $=.7$ | " |
| 15 | " | $=.0313$ | " | 15 | " | $=.75$ | " |
| 16 | , | =.0333 | , | 16 | , | $=.8$ | , |
| 17 | , | $=.0354$ | ", | 17 | ," | $=.85$ | " |
| 18 | " | =. 0375 | " | 18 | ,, | $=.9$ | , |
| 19 | " | $=.0396$ | ," | 19 | " | $=.95$ | ,, |
| 20 | " | $=.0417$ | " | 20 | " | = I .0 | " |
| 21 | , | $=.0438$ | , |  |  |  |  |
| 22 | , | $=.0458$ | , |  |  |  |  |
| 23 | , | $=.0479$ | , |  |  |  |  |
| 24 | " | $=.05$ | , |  |  |  |  |

Grains in Decimals of a Dwt.

| Grain $=.0417$ Dwt.Grains $=.0833$ |  |  |  |
| :---: | :---: | :---: | :---: |
| 3 | " | $=.125$ | ", |
| 4 | " | $=.1667$ | " |
| 5 | " | $=.2083$ | " |
| 6 | , | $=.25$ | " |
| 7 | " | $=.2917$ | " |
| 8 | " | $=.3333$ | " |
| 9 | , | $=.375$ |  |
| 10 | " | $=.4167$ | , |
| 11 | " | $=.4583$ |  |
| 12 | " | $=.5$ |  |

13 Grains $=.5417$ Dwt
14 , $=.5833$,,
15 ,, $=.625$,,
16 ,, $=.6667$,,
17 " $=.7083$,,
18 ,, $=.75$,,
19 ," $=.7917$,,
20 ,, $=.8333$,,
21 " $=.875$,,
22 " $=.9167$,
23 " = .9583 ,,
24 ," = I.O ,,

## Apothecaries' Weight.

$$
\begin{aligned}
20 \text { grains } & =1 \text { scruple }(Э .) \\
3 \text { scruples } & =1 \text { drachm }(5 .)=60 \text { grains. } \\
8 \text { drachms } & =1 \text { ounce }(\widetilde{3} .)=480 \text { grains. } \\
12 \text { ounces } & =1 \text { pound }(\mathrm{bb} .)=5760 \text { grains. }
\end{aligned}
$$

Drugs are now often weighed by avoirdupois weight. The scruple and drachm are not introduced into the British Pharmacopœia, but are still used in prescriptions.
The ounce and pound are the same as in troy weight, while the grain is the same in avoirdupois, troy and apothecaries' weights.

## Lineal Measure.

12 inches $=1$ foot.
3 feet $=1$ yard $=36$ inches.
$5 \frac{1}{2}$ yards $=1$ rod, pole or perch $=16 \frac{1}{2}$ feet $=198$ inches.
40 rods $=1$ furlong $=220$ yards $=660$ feet.
8 furlongs $=1$ statute mile $=1760$ yards $=5280$ feet.
I link $=7.92$ inches $=0.66$ foot ; Ioo links= 1 Gunter's chain $=66$ feet; 80 chains $=1$ statute mile $; 6$ feet $=I$ fathom $; 3$ statute miles $=1$ league; 6075.6 feet $=1$ geographical mile.

Inches expressed in Decimals of a Foot.

| Ins. | Foot. | Ins. | Foot. | Ins. | Foot. | Ins. | Foot. | Ins. | Foot. | Ins. | Foot. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 0000 | 2 | . 1667 | 4 | -3.333 | 6 | . 5000 | 8 | . 6667 | 10 | . 8333 |
| $\frac{1}{4}$ | . 0208 | $\frac{1}{4}$ | . 1875 | $\frac{1}{4}$ | . 3542 | $\frac{1}{4}$ | . 5208 | $\frac{1}{4}$ | . 6875 | $\frac{1}{4}$ | . 8542 |
| $\frac{1}{2}$ | . 0417 | $\frac{1}{2}$ | . 2083 | $\frac{1}{2}$ | . 3750 | $\frac{1}{2}$ | . 5417 | $\frac{1}{2}$ | . 7083 | $\frac{1}{2}$ | . 8750 |
| $\frac{3}{4}$ | . 0625 | $\frac{3}{4}$ | . 2292 | $\frac{3}{4}$ | . 3958 | $\frac{3}{4}$ | . 5625 | $\frac{3}{4}$ | . 7292 | $\frac{3}{4}$ | . 8958 |
| 1 | . 0833 | 3 | . 2500 | 5 | . 4167 | 7 | . 5833 | 9 | . 7500 | II | . 9167 |
| 4 | . 1042 | $\frac{1}{4}$ | . 2708 | $\frac{1}{4}$ | . 4375 | $\frac{1}{4}$ | . 6042 | $\frac{1}{4}$ | . 7708 | $\frac{1}{4}$ | . 9375 |
| $\frac{1}{2}$ | . 1250 | $\frac{1}{2}$ | . 2917 | $\frac{1}{2}$ | . 4583 | $\frac{1}{2}$ | . 6250 | $\frac{1}{2}$ | . 7917 | $\frac{1}{2}$ | . 9583 |
| $\frac{3}{4}$ | . 1458 | $\frac{3}{4}$ | . 3125 | $\frac{3}{4}$ | . 4792 | $\frac{3}{4}$ | . 6458 | $\frac{3}{4}$ | .8125 | $\frac{3}{4}$ | . 9792 |

Fractions of an Inch expressed in Decimals of an Inch．

| ${ }^{\frac{1}{8} 4}=.015625$ | $\frac{17}{\frac{1}{4}}=.265625$ | $\frac{38}{87}=.515625$ | ${ }^{\frac{4}{49}}=.765625$ |
| :---: | :---: | :---: | :---: |
| $\frac{1}{32}=.03125$ | $\frac{9}{32}=.28125$ | ${ }_{\frac{1}{8} \frac{7}{2}}=.53125$ | ${ }_{\frac{2}{3} \frac{5}{2}}=.788125$ |
| ${ }^{\frac{3}{4} 4}=.046875$ | $8^{19} \times=.296875$ | ${ }^{\text {缕 }}=.546875$ | $\frac{51}{84}=.796875$ |
| ${ }_{18}^{18}=.0625$ | $\frac{5}{16}=.3125$ | 웅 $=.5625$ | ${ }_{1}^{13} 5=.8125$ |
| $8^{5}=.078125$ | $\frac{21}{61}=.328125$ | ${ }^{\text {䂆 }}=.578125$ | $\frac{58}{68}=.828125$ |
| ${ }^{\frac{3}{32}}=.09375$ | $\frac{11}{4}=.34375$ | ${ }_{3}^{19} 2=.59375$ | $\frac{27}{32}=.84375$ |
| ${ }^{\frac{7}{4}}=.109375$ | ${ }^{2}$ 鲑 $=.359375$ | $88{ }^{8}=.609375$ | $\frac{85}{85}=.859375$ |
| $\frac{1}{8}=.125$ | $\frac{3}{8}=.375$ | $\frac{5}{8}=.625$ | ${ }^{7} 8=.875$ |
| ${ }_{87}=.140625$ | ${ }^{2}{ }^{25}=.390625$ | ${ }_{61}{ }^{4}=.640625$ | ${ }^{\frac{5}{6} 7}=.890625$ |
| $\frac{5}{3^{5}}=.15625$ | ${ }_{3}{ }^{\frac{3}{2}}=.40625$ | ${ }_{312}^{21}=.65625$ |  |
| ${ }^{11}=.171875$ | $\frac{27}{\%^{\prime}}=.421875$ | ${ }^{48} 4=.671875$ |  |
| $\frac{3}{16}=.1875$ | $\frac{7}{16}=.4375$ | $110=.6875$ | ${ }^{15} 5=.9375$ |
| ${ }^{\frac{13}{4}}=.203125$ |  | ${ }^{\frac{4}{4}} \times=.703125$ | ${ }_{81}^{64}=.953125$ |
| ${ }_{3} \frac{7}{2}=.21875$ | ${ }^{\frac{1}{3}} \mathbf{5}=.46875$ | ${ }^{\frac{2}{3} \frac{3}{2}}=.71875$ | $\frac{31}{31}=.96875$ |
| $\frac{15}{84}=.234375$ | ${ }^{81}=.484375$ | ${ }^{\text {特 }}=.734375$ | ${ }_{63} \frac{63}{4}=984375$ |
| $\underline{1}=.25$ | $\frac{1}{2}=.5$ | ${ }_{4}^{3}=.75$ |  |

## Square Measure．

144 square inches $=1$ square foot．
9 square feet $=1$ square yard $=1296$ square inches．
$30 \frac{1}{4}$ square yards $=1$ square $\operatorname{rod}=272 \frac{1}{4}$ square feet．
40 square rods $=1$ rood＝1210 square yards $=10890$ square feet．
4 roods $\quad=1$ acre $=160$ sq．rods $=4840$ sq．yards $=43560 \mathrm{sq}$ ． feet $=10$ sq．chains．
640 acres $\quad=I$ square mile $=27,878,400$ square feet．
In a square 1 acre in extent，each side measures 208.710 feet．

| $"$ | $"$ | $\frac{1}{2}$ | $"$ | $"$ | $"$ | , | 147.581 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $"$ | $"$ | $\frac{1}{4}$ | $"$ | $"$ | $"$ | $"$ | 104.355 |

## Cubic Measure．

1728 cubic inches $=1$ cubic foot．
27 cubic feet $=1$ cubic yard $=46656$ cubic inches．

## Imperial Measures of Capacity，both Liquid and Dry．＊

$$
\begin{aligned}
& 4 \text { gills }=1 \text { pint (pt.) }=34.6775 \text { cubic inches. } \\
& 2 \text { pints }=1 \text { quart (qt.) }=69.355 \text { " " } \\
& 4 \text { quarts }=1 \text { gallon (gal.) }=277.420 \mathrm{"} \\
& 2 \text { gallons }=1 \text { peck (pk.) }=554.840 \quad \text { " } \\
& 4 \text { pecks =I bushel (bush.) }=2219.360 \text { " ., } \\
& 8 \text { bushels }=1 \text { quarter (qr.) }=10.27 \dot{4} 8 \mathrm{i} \text { cubic feet. } \\
& 36 \text { bushels }=1 \text { chaldron (chal.) }=46.236
\end{aligned}
$$

＊See page 8 for the determinations from which the volumes are derived．

## Apothecaries' Measure.



I minim ( $m$.) is the volume of $0.911458 \dot{3}$ grain of distilled water at $62^{\circ} \mathrm{F}$.

| I fluid drachm (f.3.) | $"$ | 54.6875 | grains | $"$ | $"$ | $"$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| I fluid ounce (f.J.) | $"$ | 437.5 | $"$ | $"$ | $"$ | $"$ |
| I pint (O.) | $"$ | 8,750 | $"$ | $"$ | $"$ | $"$ |
| I gallon (C.) | $"$ | 70,000 | $"$ | $"$ | $"$ | $"$ |

## THE UNITED STATES OF AMERICA.

## Avoirdupois or Commercial Weight.

27.34375 grains $=1$ dram .

16 drams $=1$ ounce (oz.) $=437.5$ grains.
16 ounces $=1$ pound ( lb. ) $=7000$ grains.
14 pounds $=1$ stone.
2 stones $=1$ quarter (qr.) $=28$ pounds.
4 quarters $=1$ hundredweight (cwt.) $=112$ pounds.
20 hundredweights $=1$ 'long' ton $=80$ quarters $=2240$ pounds.
Also: 100 pounds $=1$ quintal ; 20 quintals $=1$ 'short' ton of 2000 pounds.

## Troy Weight.

24 grains $=1$ pennyweight (dwt.).
20 pennyweights $=1$ ounce (oz. troy) $=480$ grains.
12 ounces $=1$ pound (lb. troy) $=240$ dwts $=5760$ grains.

## Apothecaries' Weight.

```
20 grains \(=1\) scruple (Э).
    3 scruples \(=1\) dram (3) \(=60\) grains.
    8 drams \(=1\) ounce ( 3 ) \(=24\) scruples \(=480\) grains.
    12 ounces \(=1\) pound \(=288\) scruples \(=5760\) grains.
```

In avoirdupois, troy, and apothecaries' weights the grain is of the same weight, and in troy and apothecaries' weights the ounce and pound are the same.

## Lineal Measure.

$$
\begin{aligned}
12 \text { inches } & =\text { I foot (ft.). } \\
3 \text { feet } & =\text { I yard (yd.) }=36 \text { inches. } \\
5 \frac{1}{2} \text { yards } & =\text { I rod, pole or perch }=16 \frac{1}{2} \text { feet. } \\
40 \text { rods } & =\text { I furlong }=220 \text { yards }=660 \text { feet. } \\
8 \text { furlongs } & =\text { I statute mile }=1760 \text { yards }=5280 \text { feet. } \\
3 \text { miles } & =\text { I league. }
\end{aligned}
$$

Also: 7.92 inches $=1 /$ link ; 100 links $=1$ Gunter's chain $=66$ feet; 80 chains = I mile.

3 inches $=1$ palm; 4 inches $=1$ hand; 9 inches $=1$ span.
6 feet $=1$ fathom ; I cable's length $=120$ fathoms.

## Square Measure.

144 square inches $=1$ square foot.
9 square feet $=1$ square yard $=1296$ square inches.
$30 \frac{1}{4}$ square yards $=1$ square $\operatorname{rod}=272 \frac{1}{4}$ square feet.
40 square rods $=1$ rood= I210 square yards.
4 roods $\quad=1$ acre $=43560$ square feet $=10$ square chains.
640 acres $\quad=1$ square mile or section.
36 square miles $=1$ township.

## Cubic Measure.

1728 cubic inches $=1$ cubic foot.
27 cubic feet $=1$ cubic yard.
I 6 cubic feet $=$ I cord.
$24 \frac{3}{4}$ cubic feet $=1$ perch of stone or masonry. I 28 cubic feet $=\mathrm{I}$ cord of wood.

## Liquid Measure.



## Apothecaries' Fluid Measure.



## Dry Measure.

$$
\begin{aligned}
2 \text { pints } & =1 \text { quart }=67.2006 \text { cubic inches. } \\
4 \text { quarts } & =\text { I gallon }=268.8025 \\
2 \text { gallons } & =\text { I peck }=537.605 \\
4 \text { pecks } & =\text { I bushel }=2150.42 \\
8 \text { bushels } & \text { I quarter. } \\
2 \text { I } \frac{1}{2} \text { bushels } & \text { I barrel (dry) } \\
36 \text { bushels } & \text { I chaldron. }
\end{aligned}
$$

Note that the dry measures are larger than the liquid measures of the same names.

## RUSSIA.

## Commercial Weight.

$9 f$ dolis $=\mathrm{I}$ zolotnik.
96 zolotniks $=1$ funt.
40 funts $=1$ pood.
Other weights sometimes used are: the loth $=3$ zolotniks; the lana $=8$ zolotniks ; the berkovetz $=10$ poods ; and the packen $=3$ berkovetz. Gold ore values are expressed in zolotniks per ioo poods (see pages 103 and 104).
Apothecaries' Weight.
60 medical grains $=$ I medical drachme.
$8 \quad, \quad$ drachmes $=1 \quad "$ once.
$12 \quad$ onces $=1 \quad "$ funt $=84$ zolotniks.

Drugs are now mostly weighed by metric weights.

## Lineal Measure.

$$
\begin{aligned}
10 \text { totchkas } & =1 \text { l liniia. } \\
17.5 \text { liniias } & =1 \text { vershok. } \\
16 \text { vershoks } & =1 \text { archine } . \\
3 \text { archines } & =1 \text { sagene }=48 \text { vershoks. } \\
500 \text { sagenes } & =1 \text { verst. }
\end{aligned}
$$

The British Imperial foot and inch and the metre are also in use. The archine is used in mining and trade, the sagene in land measurement, and the foot and inch in engineering works.

## Square Measure.

256 square vershoks $=1$ square archine.
9 square archines $=1$ square sagene $=2304$ square vershoks.
2400 square sagenes $=1$ dessiatina.
104.1 $\dot{6}$ dessiatinas $=$ I square verst $=250,000$ square sagenes.

## Cubic Measure.

4096 cubic vershoks $=1$ cubic archine.
27 cubic archines $=1$ cubic sagene $=110,592$ cubic vershoks.

## Liquid Measure.

Io tcharkas $=1$ schtoff.
Io schtoffs $=1$ vedro.
16 boutylkas (bottles of wine) $=1$ vedro.
20 boutylkas (bottles) $\quad=1$ vedro.

## Dry Measure.

8 garnetz = r tchetverik.
4 tchetveriks = I osmina.
2 osminas = I tchetvert. 12 tchetverts $=1$ last.

$$
\text { I cubic sagene }=\left\{\begin{array}{c}
789.67123 \text { vedros. } \\
46.2698 \text { tchetverts. }
\end{array}\right.
$$

## CHINA.

## Commercial Weight.

I6 liang (taels or tahils $)=\mathrm{I}$ chin $($ kan or kati $)=1 \frac{1}{3} \mathrm{lbs}$. avoir. Ioo chin

$$
=\tan (\operatorname{tam} \text { or pikul })=133 \frac{1}{3}
$$

## Silver Weight.

Io ssŭ = I hao (thousandths).
Io hao $=$ I li (hundredths - 'cash').
io li $=$ I fên (tenths - 'candareen').
Io fên $=$ I ch'ien ('mace').
Io ch'ien $=I$ liang (tael or tahil) $=I_{\frac{1}{3}}$ oz. avoir.

## Lineal Measure.

$$
\begin{aligned}
& \text { Io fan }=1 \text { ts'un } \quad=1.41 \text { British inches. } \\
& \text { Io } \mathrm{ts}^{\prime} \mathrm{un}=\mathrm{I} \text { ch'ih }(\text { covid })=14.1 \\
& \text { Io ch'ih }=\mathrm{I} \text { chang }(\text { rod })=14 \mathrm{I} \\
& \text { " } \\
& 10 \text { chin }=1 \text { chang (rod) }=141 \text { " }
\end{aligned}
$$

The foregoing values are those of the British Treaty of 1858 . They are used in the payment of duties at the Foreign Maritime Customs. At Hong Kong, where both British Imperial and Chinese weights and measures are in use, the present standard chek or chith was verified by the Board of Trade. It measures $14 \frac{5}{8}$ inches, and is therefore 0.525 inch longer than the chin of the British Treaty. The standard ying-tsao chith of the Chinese Board of Works is approximately 12.5 inches. The Hong Kong weights are identical with those of the British Treaty.

| Itinerary | Measure. |
| ---: | :--- |
| $5 \mathrm{ch}{ }^{\prime} \mathrm{ih}$ (covids) | $=$ I pu (pace). |
| 360 pu | $=$ I li (about $\frac{1}{3}$ mile). |
| 250 li | $=$ I tu (degree). |

## Land Measure.

5 ch'ih (covids) = I kung (bow).
240 square kung $=1$ mou (rood).

## Cubic Measure.

100 cubic ch'ih = I fang or ma.

## Measures of Capacity.

```
Io ho \(=1\) shêng \(=\) approx. 2 Imp. pints.
Io shêng = I tou.
    5 tou \(=\mathrm{I}\) hu.
```

JAPAN.
Weight.
Io shi $=1$ mô.
10 mô $=1$ rin.
Io rin $=1$ fun.
Io fun $=1$ mommē.
$160 \mathrm{momme}=1 \mathrm{kin}$.
rooo mommē $=\mathbf{I} \mathrm{kwan}$.

## Lineal Measure.

$$
\begin{aligned}
\text { Io shi } & =1 \text { mô. } \\
\text { Io mô } & =1 \text { rin. } \\
\text { io rin } & =1 \text { bu. } \\
\text { Io bu } & =1 \text { sun. } \\
\text { io sun } & =1 \text { shaku. } \\
6 \text { shaku } & =1 \text { ken. } \\
60 \text { ken } & =1 \text { chô }=360 \text { shaku. } \\
36 \text { chô } & =1 \text { ri }=12960 \text { shaku. }
\end{aligned}
$$

For cloth measurement the kujira shaku is used. It is equal to I shaku 2 sun 5 bu.

## Square Measure.

$$
\begin{aligned}
& \text { Io shaku }=\text { I gò. } \\
& \text { Io gô }=\text { I bu or tsubo. } \\
& 30 \text { tsubo }=\text { I sē. } \\
& \text { Io sē }=\text { I tan }=300 \text { tsubo. } \\
& \text { Io tan }=\text { I chô }=3000 \text { tsubo. }
\end{aligned}
$$

A bu or tsubo equals 36 square shaku (i square ken) of lineal measure.

## Measures of Capacity.

```
Io shaku=r gô.
IO gô = I shô.
IO shô = I to.
Io to = I koku= 100 shô.
```

In the above tables the same name is sometimes applied to units having no connection with each other. For instance, the shaku as a lineal measure is quite different from the shaku of square measure, which again has no connection with the shaku of capacity.

## BRITISH INDIA.

The following weights are based on the tola, which is the weight of a rupee (i8o grains). They are officially recognised, and are used on the railways, etc., but numerous local weights of varying value obtain throughout India. The Burmese viss of 100 tikals $=3.65 \mathrm{lbs}$. avoir. exactly.*

[^17]> Weight. $\begin{aligned} \text { I } 80 \text { grains } & \text { I I tola. } \\ 80 \text { tolas } & \text { I seer. } \\ 40 \text { seers } & =\text { I maund. } \\ 20 \text { maunds } & \text { I kandy. }\end{aligned}$

## Lineal Measure.

The Imperial yard, foot and inch are statutory by Act 2 of India, 1889. Various native measures, which are mostly based on the guz or yard, are also used.

## Square Measure.

The biga is the common unit of land measure. It varies in size in almost every village.

The Bengal biga=approximately 1600 sq. yards.

| The N.W. Province | $"=$ | $"$ | 3025 |
| ---: | :--- | :--- | :--- |
| The Bombay | $"=$ | $"$ | 3927 |

In Madras, the unit is the kani=approximately 6400 sq. yards.

## THE STRAITS SETTLEMENTS.

Ordinance No. VII. of 1886 assimilates the weights and measures used in the Straits Settlements to the British Imperial weights and measures, with the exception of the following weights :

$$
\begin{aligned}
& \text { Io hoons }=1 \text { chee. } \\
& \text { Io chee }=\mathrm{I} \text { tahil (tael) }=\quad \mathrm{I} \frac{1}{3} \text { oz. avoir. } \\
& 16 \text { tahils }=1 \text { kati }(\mathrm{kan})=1 \frac{1}{3} \mathrm{lbs} ., \\
& \text { roo katis }=1 \text { pikul (tam) }=133 \frac{1}{3} \mathrm{lbs} \text {. ", } \\
& 40 \text { pikuls }=1 \text { koyan }=5333 \frac{1}{3} \mathrm{lbs} \text {." }
\end{aligned}
$$

## Measures of Capacity.

I pau or quarter chupah $=2$ Imp. gills.
1 half chupah $=1$ " pint.
I chupah $=1$ " quart.
1 gantang $=1$, gallon.

## SOUTH AFRICA.

The British Imperial system of weights and measures is used throughout British South Africa, but in the Cape Colony, British Bechuanaland, the Orange River Colony, the Transvaal and Rhodesia, a special system of land measure known as the Cape System is used :

## Lineal Measure.

12 Cape inches $=1$ Cape foot.
12 Cape feet $=1$ rood.
425.94385 roods $=1$ statute mile ( 1760 yards).

Note.-I Cape foot $=$ I. 033 British feet.

## Square Measure.

144 square Cape inches $=1$ square Cape foot.
144 square Cape feet $=1$ square rood.
600 square roods $=1$ morgen.

## EGYPT.

## Commercial Weight.

I2 dirhems (drachms)=I okieh.

12 okiehs
400 dirhems
36 okes
ioo rotls
60 okes
112 "
200 " = I heml.

Jewellers' Weight.
4 kamhas $=\boldsymbol{r}$ kirat.
16 kirats $=1$ dirhem.
24 " = i mithkal.

## Lineal Measure.

24 kirats $=1$ dirâ baladi.
There are several diraâs (cubits or pikes) of different lengths in use, namely, the diraâ baladi or 'town' diraâ ; the diraâ mimari, used in building, etc. ; and the pike istambuli or Constantinople pike, used in measuring cloth.
The kassabah is the unit used in land surveying.

## Square or Land Measure.

$$
\begin{array}{rlrl}
24 & \text { sohts } & =1 \text { sahm. } \\
4 \text { sahms } & =1 \text { danek. } \\
2 \text { daneks } & =1 \text { habbah. } \\
3 \text { habbahs } & =I \text { kamel kirat. } \\
24 \text { kamel kirats } & =1 \text { feddan (masri). } \\
333 \frac{1}{3} \text { square kassabahs } & =\text { I feddan (masri). }
\end{array}
$$

| Measures of Capacity. |  |
| :---: | :---: |
| 2 kirats | $=1$ karrūbah. |
| 2 karrūbahs | = I tūmnah. |
| 2 tūmnahs | = I rūbaah. |
| 2 rūbaahs | = I nesf kadah. |
| 2 nesf kadah | = i kadah. |
| 2 kadahs | = I malwa. |
| 2 malwas | = I rūb. |
| 2 rūbs | $=\mathrm{I}$ kilah. |
| 2 kilahs | = I webah. |
| 6 webahs | $=\mathrm{I}$ ardeb. |
| 8 ardebs | $=\mathrm{I}$ daribah. |
| 7 rūbs | = I small fard. |
| 14 " | = I large " |

## SECTION IV. CONVERSION TABLES.

In this section the scientific equivalents of the Metric and British Imperial weights and measures, together with the corresponding logarithms, are first given. These are followed by the Board of Trade legal equivalents of the Metric weights and measures, in which, as they are for use in trade, the same degree of accuracy is not required. The scientific equivalents of the United States and Metric weights and measures as published by the U.S. Bureau of Standards at Washington, and the shorter equivalents legalised in the United States by the Act of July 28, 1866, are also given. Then follow in the order named the Metric and British equivalents, together with the corresponding logarithms, of the Russian, Chinese, Japanese, British, Indian, Straits Settlements, Cape (S. Africa), and Egyptian weights and measures.

## SCIENTIFIC EQUIVALENTS OF METRIC AND BRITISH IMPERIAL WEIGHTS AND MEASURES.

## METRIC TO BRITISH IMPERIAL.

## Weight.

Metric.
Avoirdupois.
I milligram (mg.) $=.01543$ grain
I centigram (cg.) $=.15432$ ",
I decigram (dg.) $=1.54324$,
$"$
I gramme (g.) $=\left\{\begin{array}{l}.00220462234 \text { pound } \\ 15.43235639 \text { grains }\end{array}\right.$
Logarithm.
8.1884322
9.1884322
0. 1884322
7.3433342
1.1884322

I dekagram(dag.) $=.35274$ ounce 9.5474542
1 hectogram (hg.) $=3.52740$ ounces
I kilogram (kg.) $=\left\{\begin{array}{l}\text { 2.20462234 pounds } \\ \text { I } 5432.35639 \text { grains }\end{array}\right.$
0.5474542
0.3433342
4.1884322

1 myriagram $\quad=22.04622$ pounds

1. 3433342

I quintal (q.) $=1.96841$ hundredweights
0.2941162

I tonne (t.) $\quad=\left\{\begin{array}{l}0.98420640 \text { tons of } 2240 \mathrm{lbs} . \\ \text { I. } 10231 \text { II } 7 \text { tons of } 2000 \mathrm{lbs} .\end{array}\right.$
9.9930862
0.0423042

Troy.
I gramme (g.) $=\left\{\begin{array}{l}0.03215074248 \text { ounce } \\ 0.64301485 \text { pennyweight }\end{array}\right.$
Apothecaries. I gramme (g.) $= \begin{cases}0.2572 \mathrm{I} \text { drachm } & 9.4102809 \\ 0.77162 \text { scruple } & 9.8874022 \\ \mathrm{I} 5.43235639 \text { grains } & 1.1884322\end{cases}$

## Lineal Measure.

| 1 micron ( $\mu$.) | $=.00003937$ inch | 5.5951667 |
| :---: | :---: | :---: |
| 1 millimetre (mm.) | =.039370113 | 8.5951667 |
| I centimetre (cm.) | $=.39370113$ | 9.5951667 |
| 1 decimetre (dm.) | $=3.9370113$ inches | -. 5951667 |
|  | 39.370113 inches | 1.5951667 |
| I metre (m.) | $=\{3.2808427654$ feet | 0.5159855 |
|  | 1.09361425513 yards | 0.0388642 |
| I dekametre (dam.) | $=10.93614255$ yards | 1.0388642 |
| I hectometre (hm.) | $=109.3614255$ | 2.0388642 |
| 1 kilometre (km.) | $=0.62137173$ mile | 9.7933515 |
| I myriametre (Mm.) | $=6.2137173$ miles | 0.7933515 |

5.5951667
8.5951667
9.5951667
0.5951667

1. 5951667
2. 5159855
0.0388642
1.0388642
2.0388642
9.7933515
0.7933515
9.8082210

Square Measure. Logarithm.

| square millimetre ( $\mathrm{mm} .{ }^{2}$ ) | =.oor 550 square inch | 7.1903333 |
| :---: | :---: | :---: |
| I square centimetre (cm. ${ }^{2}$ ) | $=.1550006$ | 9.1903333 |
| I square decimetre (dm. ${ }^{2}$ ) | $=15.50006$ square inches | 1.1903333 |
|  | 1550.005812 sq. inches | 3.1903333 |
| I square metre (m. ${ }^{2}$ ) | 10.76392925 square feet | 1.0319708 |
|  | I.195992139 sq. yards | 0.0777283 |
| e (sq. decametre) (a.- | = 119.5992139 square yards | 2.0777283 |
| ctare (ha.) | $=2.471058 \mathrm{I} 385 \mathrm{acres}$ | 0.3928830 |
| I square kilometre (km. ${ }^{2}$ ) | $=.386102834$ square mile | 9.5867030 |
| I square myriametre (Mm. ${ }^{2}$ ) | $=38.6102834$ ", miles | 1.5867030 |

## Cubic Measure.



## Measures of Capacity.

I mililitre (ml.) $=16.894$ I I minims $\quad 1.2277353$
I centilitre (cl.) $=.07039$ gill 8.847524 I
I decilitre (dl.) $=.17598$ pint 9.245464 I
I litre (1.) $\quad= \begin{cases}\text { I. } 75980 \text { pints } & 0.245464 \mathrm{I}\end{cases}$
I dekalitre (dal.) $=2.19975389$ gallons 0.342374 I
I hectolitre (hl.) $=2.74969236$ bushels $\quad 0.439284$ I
I kilolitre (kl.) $=3.437$ II 545 quarters 0.5361941

BRITISH IMPERIAL TO METRIC.

## Weight.

Avoirdupois.
I grain
I drachm
I ounce
I pound
I stone
I quarter
I cental ( 100 lbs .)
I hundredweight

Metric.
$=64.79891824$ milligrams
$=1.77185$ grammes
$=28.34953 \quad "$
$=\left\{\begin{array}{l}453.5924277 \text { grammes } \\ .4535924277 \text { kilogram }\end{array}\right.$
$=6.35029$ kilograms
$=12.70059$ "
$=45.35924277$ "
$=50.802352$ "

Logarithm.
1.81 15678
0.5897191
I. 4525458
2.6566658
9.6566658
0.8027938
1.1038238

1. 6566658
2. 7058838
9.9576958
0.0069138

| Troy. Metric. | Logarithm. |
| :---: | :---: |
| 1 grain $\quad=64.79891824$ milligrams | 1.8115678 |
| I pennyweight $=1.555174$ grammes | 0.1917790 |
| 1 ounce $\quad=31.1034807566$ grammes | I. 4928090 |
| Apothecaries. Metric. | Logarithm. |
| 1 grain $=64.7989 \mathrm{I} 824$ milligrams | 1.8115678 |
| I scruple $=1.29598$ grammes | 0.1125978 |
| I drachm $=3.88794$ grammes | 0.5897191 |
| 1 ounce $=3$ I.1034807566 grammes | I. 4928090 |

## Lineal Measure.

| I inch | $=25.3999 \dot{7}$ millimetres | 1.4048333 |
| :--- | :--- | :--- |
| I foot | $=.3047997$ 3ं metre | 9.4840145 |
| I yard | $=.9143992$ metre | 9.9611358 |
| I pole | $=5.0291956$ metres | 0.7014985 |
| I chain | $=20.116782 \quad "$ | 1.3035585 |
| I furlong | $=201.16782 \quad$ " | 2.3035585 |
| I statute mile $=1.60934259$ kilometres | 0.2066485 |  |

## Square Measure.

I square inch $=6.45158871$ square centimetres
0.8096667

I square foot $=.092902877$ square metre $\quad 8.9680292$
I square yard $=.8361259$ ",
9.9222717

I square perch $=25.2928084$ square metres $\quad 1.4029970$
1 rood $=$ IOI 1.712335 "
$I$ acre $\quad=.404684934$ hectare
I square mile $=2.5899835784$ square kilometres
3.0050570
9.6071170
0.4132970

## Cubic Measure.

| I cubic inch $=16.38702$ I cubic centimetres | I.2145000 |
| :--- | :--- | :--- |
| I cubic foot $=.02831677$ cubic metre | 8.4520437 |
| I cubic yard $=.76455285 \quad \Longrightarrow$ | 9.8834075 |

## Measures of Capacity.

| Imperial. Metric. | Logarithm. |
| :---: | :---: |
| 1 gill $=1.42061$ decilitres | 0.1524759 |
| 1 pint $=.56825$ litre | 9.7545359 |
| I quart $=$ I. 13649 litres | 0.0555659 |
| I gallon $=4.545963 \mathrm{x}$ litres | 0.6576259 |
| I peck $=9.091926$, | 0.9586559 |
| I bushel $=3.63677$ dekalitres | 0.5607159 |
| I quarter $=2.9094164$ hectolitres | 0.4638059 |


| Apothecaries. | Metric. | Logarithm. |
| :--- | :--- | :---: |
| I minim | $=.059192$ millilitre | 8.7722647 |
| I fluid drachm | $=3.55153$ millilitres | 0.5504159 |
| I fluid ounce | $=2.84123$ centilitres | 0.4535059 |
| I pint | $=.56825$ litre. | 9.7545359 |
| I gallon | $=4.545963$ I litres | 0.6576259 |

## THE BOARD OF TRADE LEGAL EQUIVALENTS OF THE METRIC AND IMPERIAL WEIGHTS AND MEASURES FOR USE IN TRADE.*

## METRIC TO BRITISH IMPERIAL.

## Linear Measure.

I millimetre (mm.) $\left.\frac{1}{1000} \mathrm{~m}.\right)=0.03937$ inch.
I centimetre $\left(\frac{1}{100} \mathrm{~m}\right.$.) $\quad=0.3937$ ",
1 decimetre ( $\frac{1}{10} \mathrm{~m}$. ) $\quad=3.937$ inches.

| I metre (m.) | $=\left\{\begin{array}{l} 3.310843 \text { feet. } \\ 3.2806 \mathrm{I} .0936143 \text { yards. } \end{array}\right.$ |
| :---: | :---: |
| 1 dekametre ( I ( m.) | $=10.936$ yards |
| I hectometre ( 100 m. ) | $=109.36$ |
| I kilometre ( 1000 m. ) | $=0.62137 \mathrm{mile}$. |

## Square Measure.

I square centimetre $\quad=0.15500$ square inch.
I square decimetre ( 100 square centimetres) $=15.500$ square inches.
I square metre (ioo square decimetres) $\quad=\left\{\begin{array}{l}\text { I0.7639 square feet. } \\ \text { I. } 1960 \text { square yards. }\end{array}\right.$
I are (ioo square metres)
$=119.60$
I hectare ( 100 ares or 10,000 square metres) $=2.4711$ acres.

## Cubic Measure.

I cubic centimetre
$=0.06$ IO cubic inch.
I cubic decimetre ( 1000 cubic centimetres) $=6$ 1.024 cubic inches.
I cubic metre (Iooo cubic decimetres) $\quad=\left\{\begin{array}{l}35.3148 \text { cubic feet. } \\ \text { I. } 307954 \text { cubic yards. }\end{array}\right.$

## Measures of Capacity.

I centilitre ( $\frac{1}{100}$ litre) $=0.070$ gill.
I decilitre ( $\frac{1}{10}$ litre) $=0.176$ pint.
I litre $\quad=1.75980$ pints.
I dekalitre ( ro litres) $=2.200$ gallons.
I hectolitre ( I 00 litres) $=2.75$ bushels.
${ }^{*}$ These equivalents were legalised by Order in Council of May 19, 1898 (For the Scientific Equivalents see page 33.)

## Weight.

Metric. Avoirdupois.
1 milligram $\left(\frac{1}{1000}\right.$ grm. $)=0.015$ grain.
I centigram ( $\frac{1}{100}$ grm.) $=0.154$ "
1 decigram ( $\frac{1}{10}$ grm.) $=1.543$ grains.
I gramme ( I grm.) $=15.432$ "
I dekagram ( 10 grm .) $=5.644$ drams.
I hectogram ( I 0 og grm .) $=3.527$ ounces.
I kilogram ( 1000 grm.$)=\left\{\begin{array}{l}2.2046223 \text { pounds or } \\ 15432.3564 \text { grains. }\end{array}\right.$
1 myriagram ( 10 kilog.) $=22.046$ pounds.
I quintal ( 100 kilog.) $=1.968$ hundredweights.
I tonne (1000 kilog.) $=0.9842$ ton.
Metric.
Troy.
1 gramme ( 1 grm.) $\quad=\left\{\begin{array}{l}0.03215 \text { ounce } . \\ 15.432 \text { grains. }\end{array}\right.$
Metric.
Apothecaries.
I gramme ( I grm.) $\quad=\left\{\begin{array}{l}0.2572 \text { drachm. } \\ 0.7716 \text { scruple. } \\ 15.432 \text { grains. }\end{array}\right.$

BRITISH IMPERIAL TO METRIC.

## Linear Measure.

$I$ inch $\quad=25.400$ millimetres.
I foot ( I 2 in. ) $\quad=0.30480$ metre.
I yard ( 3 ft .) $\quad=0.914399$ metre.
I fathom ( 6 ft .) $=1.8288$ metres.
I pole ( $5 \frac{1}{2}$ yds.) $=5.0292$ "
1 chain ( 22 yds.) $=20.1168$ "
I furlong ( 220 yds. ) $=201.168$,
I mile (8 furlongs) $=1.6093$ kilometres.

## Square Measure.

I square inch
I square foot ( I 44 sq . ins.) $=9.2903$ square decimetres.
I square yard ( 9 sq . ft.) $=0.836126$ square metre.
${ }^{1}$ perch ( $30 \frac{1}{4}$ sq. $y$ ds.) $\quad=25.293$ square metres.
I rood ( 40 perches) $=10.117$ ares.
I acre ( 4840 sq. yds.) $\quad=0.40468$ hectare.
I square mile ( 640 acres) $=259.00$ hectares.

## Cubic Measure.

$I$ cubic inch $\quad=16.387$ cubic centimetres.
I cubic foot ( 1728 cub. ins.) $=0.028317$ cubic metre.
I cubic yard ( 27 cub . ft.) $=0.764553$
Measures of Capacity.
Imperial. Metric.
1 gill $=1.42$ decilitres.
I pint ( 4 gills) $\quad=0.568$ litre.
I quart ( 2 pints) $=1.136$ litres.
I gallon (4 quarts) $=4.545963$ I litres.
I peck ( 2 gallons) $=9.092$ litres.
I bushel ( 8 gallons) $=3.637$ dekalitres.
I quarter ( 8 bushels $)=2.909$ hectolitres.
Apothecaries. Metric.
1 minim $\quad=0.059$ millilitre.
1 fluid scruple $\quad=1.184$ millilitres.
1 fluid drachm ( 60 minims) $=3.552$ ",
I fluid ounce ( 8 drachms) $\quad=2.84 \mathrm{I} 23$ centilitres.
I pint $=0.568$ litre.
I gallon (8 pints or 160 fluid oz.) $=4.545963$ litres.

Weight.
Avoirdupois. Metric.
1 grain
$=0.0648$ gramme .
$I$ dram $\quad=1.772$ grammes.
I ounce ( 16 drams) $=28.350$ "
I pound ( 16 oz. or 7000 grains) $=0.45359243$ kilogram.
1 stone ( I 4 lbs.$) \quad=6.350$ kilograms.
I quarter ( 28 lbs .)
$=12.70$ "
I hundredweight (cwt.) (112 lb.) $=\left\{\begin{array}{l}50.80 \\ 0.5080 \text { quintal. }\end{array}\right.$
I ton ( 20 cwt .)
$=\left\{\begin{array}{l}\text { I.O160 tonnes or } \\ \text { IoI6 kilograms. }\end{array}\right.$

## Troy.

Metric.
I grain $\quad=0.0648$ gramme.
I pennyweight ( 24 grains) $\quad=1.5552$ grammes.
I troy ounce ( 20 pennyweights) $=3$ I.1035
Apothecaries.
Metric.
1 grain $\quad=0.0648$ gramme .
I scruple ( 20 grains) $=1.296$ grammes.
I drachm ( 3 scruples) $=3.888$
I ounce ( 8 drachms) $=31.1035$ "

## COMPARISON OF UNITED STATES AND BRITISH IMPERIAL WEIGHTS AND MEASURES.

## Lineal Measure.

United States and British Imperial Measures of length are practically the same, as I U.S. unit $=1.000002875$ Imp. units of the same denomination, a difference of 2.875 in a million.

## Square Measure.

I U.S. unit $=1.00000575$ Imp. units, a difference of 5.75 in a million.

## Cubic Measure.

I U.S. unit $=1.000008625$ Imp. units, a difference of 8.625 in a million.

## Measures of Capacity.

Liquid.
I U.S. liquid gallon $=0.83270$ Imp. gallon. $\quad \log =9.9204898$
1 Imp. gallon $\quad=1.20091$ U.S. liquid gallons. $\quad \log =0.0795102$
Dry.
I U.S. bushel $=0.96897$ Imp. bushel. $\quad \log =9.98631$ II
I Imp . bushel $=1.0 \mathrm{j}_{2} 202$ U.S. bushels. $\quad \log =0.0136889$
Weights.
No difference.

## EQUIVALENTS OF UNITED STATES AND METRIC WEIGHTS AND MEASURES AS PUBLISHED BY THE U.S. BUREAU OF STANDARDS, WASHINGTON.*

## Measures of Length.

Basis : 1 meter $=39.37$ inches.
I U.S. inch $=25.4000508$ millimeter. $\quad \log =1.4048346$
I U.S. foot $=0.3048006096$ meter. $\quad \log =9.4840158$
I U.S. yard $=0.9144018288$ meter. $\quad \log =9.9611371$
I U.S. mile $=1.609347219$ kilometers. $\quad \log =0.2066497$
I millimeter $=0.03937$ U.S inch. $\quad \log =8.5951654$
I meter $=3.2808 \dot{3}$ U.S. feet. $\log =0.5159842$
I kilometer $=0.6213699495$ U.S. mile. $\log =9.7933503$

[^18]
## Measures of Area.

I U.S. acre $=0.40468726$ ro hectare. $\quad \log =9.6071196$
I hectare $=2.471043930$ U.S. acres. $\quad \log =0.3928804$

## Measures of Volume.

I U.S. cubic yard $=0.7645594453$ cubic meter.
$\log =9.8834113$
I cubic meter $=1.307942772$ U.S. cubic yards.
$\log =0.1165887$

## Measures of Capacity.

## Liquid.

Basis: x U.S. liquid gallon $=23 \mathrm{I}$ cubic inches, and I cubic decimeter $=\mathrm{x}$ liter.
I U.S. liquid gallon $=3.785434497$ liters.
$\log =0.5781157$
I liter $\quad=0.2641704673$ U.S. liquid gall. $\quad \log =9.4218843$
Dry.
Basis: $x$ U.S. bushel $=2150.42$ cubic inches, and I cubic decimeter $=\mathrm{I}$ liter.

$$
\begin{array}{lll}
\text { I U.S. bushel }=0.3523928160 \text { hectoliter. } & & \log =9.5470270 \\
\text { I hectoliter } & =2.837742299 \text { U.S. bushels. } & \\
l o g=0.4529730
\end{array}
$$

## Weights.

Basis : r avoirdupois pound $=453.5924277$ grams.
The equivalents are therefore the same as those given for British Imperial Weights on pages 33 and 34 .

## THE EQUIVALENTS OF THE METRIC WEIGHTS AND MEASURES LEGALISED IN THE UNITED STATES BY THE ACT OF JULY 28th, 1866.*

Measures of Length.

| Metric denominations and values. | Equivalents in denominations in use. |
| :---: | :---: |
| Myriameter - - 10,000 meters. | 6.2137 miles. |
| Kilometer - - 1,000 meters. | 0.62137 miles or 3280 feet and 10 inches. |
| Hectometer - - 100 meters. | 328 feet and I inch. |
| Dekameter - - 10 meters. | 393.7 inches. |
| Meter - - - . I meter. | 39.37 inches. |
| Decimeter - - $\frac{1}{10}$ of a meter. | 3.937 inches. |
| Centimeter - - $\frac{1}{180}$ of a meter. | 0.3937 inch. |
| Millimeter - $\frac{1}{1000}$ of a meter. | 0.0394 inch. |

[^19]Measures of Surface.

| Metric denominations and values. | Equivalents in denominations in use. |
| :---: | :---: |
| Hectare - - 10,000 square meters. | 2.471 acres. |
| Are - - - - 100 square meters. | 119.6 square yards. |
| Centiare - - - I square meter. | 1,550 square inches. |

## Measures of Capacity.

| Metric denominations and values. |  |  | Equivalents in denominations in use. |  |
| :---: | :---: | :---: | :---: | :---: |
| Names. | Number of liters. | Cubic Measure. | Dry Measure. | Liquid or Wine Measure. |
| Kiloliter or stere Hectoliter | $\begin{array}{r} 1,000 \\ 100 \end{array}$ | I cubic metre $\frac{1}{10}$ of a cubic meter | 1. 308 cubic yards <br> 2 bushels and 3.35 pecks | 264.17 gallons. 26.417 gallons. |
| Dekaliter <br> Liter |  | Io cubic decimeters I cubic decimeter | 9.08 quarts <br> 0.908 quart | 2.6417 gallons. 1.0567 quarts. |
| Deciliter | 1 | $\frac{1}{10}$ of a cubic decimeter | 6. 1022 cub. inches | 0.845 gill. |
| Centiliter | $\frac{1}{100}$ | Io cubic centimeters | 0.6102 cubic inch | 0. 338 fluid ounce. |
| Milliliter | $\frac{1000}{100}$ | I cubic centimeter | 0.061 cubic inch | 0.27 fluid dram. |

Weights.

| Metric denominations and values. |  |  | Equivalents in denominations in use. |
| :---: | :---: | :---: | :---: |
| Names. | Number of grams. | Weight of what quantity of water at maximum density. | Avoirdupois Weight. |
| Millier or tonneau | 1,000,000 | 1 cubic meter | 2204.6 pounds. |
| Quintal - | 100,000 | I hectoliter | 220.46 pounds. |
| Myriagram - | 10,000 | Io liters | 22.046 pounds. |
| Kilogram or kilo- | 1,000 | 1 liter | 2.2046 pounds. |
| Hectogram- | 100 | I deciliter | 3. 5274 ounces. |
| Dekagram - | 10 | Io cubic centimeters | 0.3527 ounce. |
| Gram | 1 | 1 cubic centimeter | 15.432 grains. |
| Decigram - | $\frac{1}{10}$ | $\frac{1}{10}$ of a cub. centimeter | 1.5432 grains. |
| Centigram - | $\frac{10}{100}$ | Io cubic millimeters | 0. 1543 grain. |
| Milligram - | \%000 | I cubic millimeter | 0.0154 grain. |

## EQUIVALENTS OF THE RUSSIAN WEIGHTS AND MEASURES.

## Commercial Weight.

Russian. Metric. British.
1 doli $=44.43494$ milligrams $=.6857358$ grain.
I zolotnik $=4.26575427$ grammes $=65.83064$ grains.
I funt $=\left\{\begin{array}{l}.40951241 \text { kilogram } \\ 409.5124 \text { grammes } \\ 409512.4 \text { I milligrams }\end{array}\right\}=\left\{\begin{array}{l}.902820208 \mathrm{lbs} . \text { avoir. } \\ \text { I3.166I280 oz. troy. } \\ 6319.741457 \text { grains. }\end{array}\right.$ $I$ pood $=\left\{\begin{array}{l}.0163804964 \text { tonne } \\ 16.3804964 \text { kilograms }\end{array}\right\}=\left\{\begin{array}{l}.01612178943 \text { tons of } 2240 \mathrm{lbs} . \\ .01805640416 \text { tons of } 2000 \mathrm{lbs} . \\ 36.112808327 \mathrm{lbs} . \text { avoir. } \\ 526.6451214 \mathrm{oz} . \text { troy. }\end{array}\right.$

## Apothecaries' Weight.

Russian. Metric. British. 1 medical grain $=62.20892$ milligrams $=.96003017$ grain .
1 medical drachme $=3.732535$ grammes $=57.60181$ grains .
I medical once $=29.860280 \quad=\quad=.96003017 \mathrm{oz}$. apoth.
I medical funt $=358.323359 \quad, \quad=11.5203620 \quad "$

Meţric. Russian.
I milligram $=.0225048$ doli
I gramme $=\left\{\begin{array}{l}.234425 \text { I } 3 \text { zolotnik } \\ 16.074866 \text { medical grains }\end{array}\right.$
I kilogram $=\left\{\begin{array}{l}.06104821 \text { I pood } \\ 2.44192844 \text { funts } \\ 234.42513 \text { zolotniks } \\ 22504.8125 \text { dolis }\end{array}\right.$
$\left.\begin{array}{l}\text { I metric } \\ \text { quintal }\end{array}\right\}=244.192844$ funts
I tonne $=61.04821097$ poods
British. Russian.
I grain $=1.4582875$ dolis
1 ounce troy $\quad=7.2914375$ zolotniks
I pound avoir. $=\left\{\begin{array}{l}.027691006 \text { pood } \\ \text { r.10764025 funts } \\ 106.333464 \text { zolotniks }\end{array}\right.$
I hundredweight $=124.055708$ funts
I 'short' ton $\left.\begin{array}{c}(2000 \mathrm{lbs} .)\end{array}\right\}=55.38201244$ poods
A 'long' ton $(2240$ lbs. $)\}=62.02785393$ poods

Logarithm.
8.3522754
9.3700042
1.2061474
8.7856729
0.3877330
2.3700042
4.3522754
2.3877330
1.7856729

Logarithm.
0.1638432
0.8628132
8.4423387
0.0443987
2.0266700
2.0936168
I. 7433687
1.7925868

## Lineal Measure.

Russian. Metric. British.
I totchka $=254$ microns $\quad=.01$ inch.
I liniia $=2540$ microns $=. I$ inch.
I vershok $=44.45$ millimetres $=1.75$ inches.
1 archine $=.71120$ metre $\quad=2$ feet 4 inches.
I sagene $=2,13360$ metres $=7$ feet.
$I_{\text {I }}$ verst $=1.06680$ kilometres $=.662 \dot{8} \dot{7}$ mile.
Metric. Russian Logarithm.
I metre $=\left\{\begin{array}{l}\text { I. } 40607424 \text { archines } \quad 1.1480082\end{array}\right.$
I kilometre $=9378$

British. Russian. Logarithm.
1 inch $=10$ liniias.
1 foot $=6 . \dot{8} 5714 \dot{2}$ or $6 \frac{6}{7}$ vershoks $\quad 0.8361432$
I yard $= \begin{cases}.00 \dot{8} 5714 \dot{2} \text { or } \frac{6}{700} \text { verst } & 7.9330532\end{cases}$
I chain $=9 . \dot{4} 2857 \mathrm{i}$ or $9_{7}^{3}$ sagenes 0.9744459
1 mile $=1.50 \dot{8} 5714 \dot{2}$ versts
0. 1785659

## Square Measure.

Russian. Metric. British.
I square sagene $=4.55224896$ square metres $=49$ square feet. 1 dessiatina $=1.09253975$ hectares $\quad=2.6997245$ acres.
I square verst $=1.13806224$ square kilometres $=.43940829 \mathrm{sq}$. mile.

| Metric. | Russian. |
| :---: | :---: |$\quad$| Logarithm. |
| :---: |,

## Cubic Measure.

Russian.
Metric.
British.
I cubic vershok $=87.8244$ cubic centimetres $=5.359375$ cubic inches.
I cubic archine $=.3597288$ cubic metre $=12 . \dot{7} \circ \mathfrak{j}$ cubic feet.
$I_{1}$ cubic sagene $=9.7126784$ cubic metres $=12 . \dot{7} 0 \dot{3}$ cubic yards.

| Metric. | Russian. | Logarithm. |
| ---: | :---: | :---: |
| I cubic centimetre | $=.0113864$ cubic vershok | 8.0563848 |
| I cubic decimetre | $=.00277987$ cubic archine | 7.4440248 |
| I cubic metre $($ stere $)$ | $=.1029582$ I cubic sagene | 9.0126610 |
| British. | Russian. | Logarithm. |
| I cubic inch $=1000$ cubic liniias. |  |  |
| I cubic foot | $=.0787172$ cubic archine | 8.8960696 |
| I cubic yard | $=.0787172$ cubic sagene | 8.8960696 |

## Liquid Measure.

Russian. Metric. British.

I tcharka
I schtoff
I vedro
$=.1229933$ litre $=.216444$ pint.
$=\mathrm{I} .22993285$ litres $=2.16444$ pints.
$=\mathbf{1 2 . 2 9 9 3 2 8 5}$ litres $=2.70555$ gallons.
1 boutylka (bottle of wine) $=.76870803$ litre $=1.352775$ pints.
I boutylka (bottle)
$=.6149664$ "
$=1.08222$

## Dry Measure.

Russian.
Metric.
British.
I garnetz $\quad=3.27982093$ litres $\quad=.721480$ gallon .
I tchetyerik $=26.2385674$ litres $=.721480$ bushel.
I tchetvert $=2.09908539$ hectolitres $=5.77184$ bushels.
I last $\quad=25.18902473 \quad, \quad=8.65776$ quarters.
I cubic sagene $=97.1242585 \quad " \quad=\left\{\begin{array}{l}267.061832 \text { bushels } . \\ 2136.49465 \text { gallons. }\end{array}\right.$

Metric.
I litre

$$
=\left\{\begin{array}{l}
0.8 \mathrm{I} 30525 \text { schtoff } \\
\mathrm{I} .300884 \text { boutylkas of wine }
\end{array}\right.
$$

Russian.

I hectolitre $=\left\{\begin{array}{l}3.81118368 \text { tchetveriks } \\ 8.130525184 \text { vedros }\end{array}\right.$
$\left.\begin{array}{r}\text { I cubic metre } \\ (\text { stere })\end{array}\right\}=\left\{\begin{array}{l}38.110846 \text { tchetveriks } \\ 8 \mathrm{I} .303 \mathrm{I} 38 \text { vedros }\end{array}\right.$

> British. Russian.

I gallon $=\left\{\begin{array}{l}0.3696107 \text { vedro } \\ \text { I.386040 garnetz }\end{array}\right.$
I bushel $=\left\{\begin{array}{l}\mathrm{I} .386040 \text { tchetveriks } \\ \mathrm{II} .08832 \text { garnetz }\end{array}\right.$
$I$ cubic foot $=\left\{\begin{array}{l}1.0791790 \text { tchetveriks } \\ 2.3022485 \text { vedros } \\ 8.6334318 \text { garnetz }\end{array}\right.$

Logarithm.
9.9101186
0. 1142386
0.5810599
0.9101186
I. 5810486
1.9101073

Logarithm.
9.5677445
o. 1417757
o. 1417757
1.0448657
0.0330935
0.3621522
0.9361835

Table for the conversion of Russian Vershoks into British Feet.

|  | Feet. | 安 | Feet. |  | Feet. |  | Feet. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $0.1458 \dot{3}$ | 5 | 0.72916 | 9 | 1.3125 | 13 | 1.8958 ${ }^{\text {3 }}$ |
| 2 | 0.2916 | 6 | 0.875 | 10 | $1.458{ }^{\text {j }}$ | 14 | $2.041{ }^{6}$ |
| 3 | 0.4375 | 7 | 1.02083 | 11 | 1.60416 | 15 | 2.1875 |
| 4 | $0.58 \dot{3}$ | 8 | 1.10 | 12 | 1.75 | 16 | 2.3 |

Table for the conversion of Russian Archines into British Feet.

|  | Feet. |  | Feet. |  | Feet. |  | Feet. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2.3 | 31 | 72.3 | 61 | 142.3 | 91 | 212.3 |
| 2 | 4.6 | 32 | 74.6 | 62 | 144.6 | 92 | 214.6 |
| 3 | 7.0 | 33 | 77.0 | 63 | 147.0 | 93 | 217.0 |
| 4 | 9.3 | 34 | 79.3 | 64 | 149.3 | 94 | 219.3 |
| 5 | 11.6 | 35 | 81.6 | 65 | 151.6 | 95 | 221.6 |
| 6 | 14.0 | 36 | 84.0 | 66 | 154.0 | 96 | 224.0 |
| 7 | 16.3 | 37 | 86.3 | 67 | ${ }^{156.3}$ | 97 | 226.3 |
| 8 | 18.6 | 38 | 88.6 | 68 | 158.6 | 98 | 228.6 |
| 9 | 21.0 | 39 | 91.0 | 69 | 161.0 | 99 | 231.0 |
| 10 | 23.3 | 40 | 93.3 | 70 | 163.3 | 100 | 233.3 |
| 11 | 25.6 | 41 | 95.6 | 71 | 165.6 | 200 | 466.6 |
| 12 | 28.0 | 42 | 98.0 | 72 | 168.0 | 300 | 700.0 |
| 13 | 30.3 | 43 | 100.3 | 73 | 170.3 | 400 | 933.3 |
| 14 | 32.6 | 44 | 102.6 | 74 | 172.6 | 500 | 1166.6 |
| 15 | 35.0 | 45 | 105.0 | 75 | 175.0 | 600 | 1400.0 |
| 16 | 37.3 | 46 | 107.3 | 76 | 177.3 | 700 | 1633.3 |
| 17 | 39.6 | 47 | 109.6 | 77 | 179.6 | 800 | 1866.6 |
| 18 | 42.0 | 48 | 112.0 | 78 | 182.0 | 900 | 2100.0 |
| 19 | 44.3 | 49 | 114.3 | 79 | 184.3 | 1000 | 2333.3 |
| 20 | 46.6 | 50 | 116.6 | 80 | 186.6 | 1100 | 2566.6 |
| 21 | 49.0 | 51 | 119.0 | 81 | 189.0 | 1200 | 2800.0 |
| 22 | 51.3 | 52 | 121.3 | 82 | 191.3 | 1300 | 3033.3 |
| 23 | 53.6 | 53 | 123.6 | 83 | 193.6 | 1400 | 3266.6 |
| 24 | 56.0 | 54 | 126.0 | 84 | 196.0 | 1500 | 3500.0 |
| 25 | 58.3 | 55 | 128.3 | 85 | 198.3 | 1600 | $3733 \cdot 3$ |
| 26 | 60.6 | 56 | 130.6 | 86 | 200.6 | 1700 | 3966.6 |
| 27 | 63.0 | 57 | 133.0 | 87 | 203.0 | 1800 | 4200.0 |
| 28 | 65.3 | 58 | 135.3 | 88 | 205.3 | 1900 | $4433 \cdot 3$ |
| 29 | 67.6 | 59 | 137.6 | 89 | 207.6 | 2000 | 4666.6 |
| 30 | 70.0 | 60 | 140.0 | 90 | 210.0 |  |  |

Table for converting Russian Poods into avoirdupois pounds, 'short tons of 2000 lbs ., 'long' tons of 2240 lbs ., or tonnes of 1000 kilograms.

| Poods. | Avoirdupois Pounds. | 'Short' Tons of 2000 lbs. | $\begin{aligned} & \text { 'Long' Tons of } \\ & 2240 \text { lbs. } \end{aligned}$ | Tonnes of 1000 kilograms. |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 36.112808327 | 0.018056404 | 0.016121789 | 0.0163804964 |
| 2 | 72.225616654 | 0.036112808 | 0.032243579 | 0.0327609928 |
| 3 | 108.338424980 | 0.054169212 | 0.048365368 | 0.0491414892 |
| 4 | 144.451233307 | 0.072225617 | 0.064487158 | 0.0655219856 |
| 5 | 180.564041634 | 0.090282021 | 0.080608947 | 0.0819024820 |
| 6 | 216.67684996 I | 0. 108338425 | 0.096730737 | 0.0982829784 |
| 7 | 252.789658287 | 0.126394829 | 0. 112852526 | 0. 1146634748 |
| 8 | 288.902466614 | 0.144451233 | 0.128974315 | 0.1310439712 |
| 9 | 325.015274941 | 0.162507637 | 0.145096105 | 0. 1474244676 |

A table for converting Russian weight into troy ounces is given on page 102.

## EQUIVALENTS OF THE CHINESE WEIGHTS AND MEASURES.

## Commercial Weight.

Chinese.
Metric.
British.

I liang $($ tael or tahil $)=37.799368975$ grammes $=\mathrm{I} . \dot{3}$ or $\mathrm{I}_{\frac{1}{3}}$ oz. avoir.
I chin (kan or kati) $=.6047899036$ kilogram $=1.3$ or $1 \frac{1}{3} \mathrm{lbs}$. avoir.
I $\tan (\operatorname{tam}$ or pikul $)=60.47899036$ kilograms $=133 . \dot{3}$

## Silver Weight.

Chinese. Metric. British.

Metric. Chinese. Logarithm.

$$
\begin{array}{lll}
\text { I milligram } & =2.6455468 \mathrm{ssŭ} & 0.4225155 \\
\text { I gramme } & =.026455468 \text { liang } & 8.4225155 \\
\text { I kilogram } & =1.653466757 \mathrm{chin} & 0.2183955 \\
\text { I tonne } & =16.53466757 \mathrm{tan} & 1.2183955
\end{array}
$$

| British. | Chinese. | Logarithm. |
| :--- | :--- | :--- |
| I grain | $=1 . \dot{7} 1428 \dot{5}$ or $\mathrm{I} \frac{5}{7} \mathrm{li}$ | 0.2340832 |
| I pound avoir. | $=.75$ or $\frac{3}{4}$ chin | 9.8750613 |
| I short ton $(2000$ lbs. $)=15$ tan | I. 1760913 |  |
| I long ton $(2240$ lbs. $)$ | $=16.8$ tan | 1.2253093 |

Note--Similar weights to the above, but bearing different names, are used in the Straits Settlements (see page 50).

## Lineal Measure (a).

Basis: 1 ch'ih $=14$. I inches.
(As adopted in the British Treaty of 1858, and used in the assessment of duties at the Foreign Maritime Customs.)


Lineal Measure (b).
Basis: I chek or ch'ih $=14 \frac{5}{8}$ inches.
(This is the Hong Kong standard chek or ch'ih, as verified by the Board of Trade.)
Chinese Metric. British.
I fan $\quad=3.71474675$ millimetres $=.14625$ inch.
I ts'un $\quad=37.1474675 \quad, \quad=1.4625$ inches.
I chek or ch'ih $=.371474675$ metre $\quad=1.21875$ feet.

| Metric. | Chinese. | Logarithm. |
| ---: | :---: | :---: |
| I millimetre | $=.269197355$ fan | 9.4300708 |
| I metre | $=2.69197355$ chek or ch'ih | 0.4300708 |

British. Chinese. Logarithm.
I inch $=. \dot{6} 8376 \dot{0}^{\text {on'un }} \quad 9.834904 \mathrm{I}$
I foot $=. \dot{8} 2051 \dot{2}$ chek or ch'ih $\quad 9.9140853$
$I$ yard $=2 . \dot{4} 6153 \dot{8} \quad, \quad 0.3912066$

## EQUIVALENTS OF THE JAPANESE WEIGHTS AND MEASURES.

## Weight.

| Japanese. | Metric. | British. |
| :---: | :---: | :---: |
| $1 \mathrm{mô}$ | $=3.75$ milligrams | $=.05787$ grain. |
| 1 rin | =. 0375 gramme | $=.5787$ grain. |
| 1 fun | $=.375$ gramme | $=5.787$ grains. |
| I mommē | $=3.75$ grammes | $=57.8713365$ grains |
| 1 kin | $=600$ grammes | $=1.3227734 \mathrm{lbs}$. avoir. |
| I kwan | $=3.75$ kilograms | $=8.26733378$ lbs. avoir. |


| Metric. Japanese. | Logarithm. |
| :---: | :---: |
| 1 milligram $=.26$ mô | 9.4259687 |
| I gramme $=.26$ mommē | 9.4259687 |
| kilogram $=\left\{\begin{array}{l}\text { I } . \dot{6} \text { or } \mathrm{I} \frac{2}{3} \mathrm{kin} \\ .6\end{array}\right.$ | 0.2218487 |
| $\left\{\begin{array}{l}.26 \mathrm{kwan}\end{array}\right.$ | 9.4259687 |
| British. Japanese. | Logarithm. |
| I grain $=17.27971153 \mathrm{mo}$ | 1. 2375365 |
| Ib. avoir $=\int .75598738 \mathrm{kin}$ | 9.8785145 |
| avoir. $=\left\{\begin{array}{l}\text {.r } 2095798 \text { kwan }\end{array}\right.$ | 9.0826345 |

## Lineal Measure.

Japanese. Metric. British.
I mô $=\frac{1}{33}$ or $.0 \dot{3}$ millimetre $=.001193$ inch.
I rin $=\frac{100}{33}$ or .30 millimetre $=.01193$ inch.
I bu $=\frac{1}{3} \frac{3}{3}$ or $.0 \dot{3}$ centimetre $=.11930337$ inch.
1 sun $=\frac{1}{33}$ or .03 metre $\quad=1.19303 .37$ inches.
I shaku $=\frac{10}{33}$ or.$\dot{3}$ ó metre $\quad=.9941948$ foot.
1 ken $=\frac{20}{11}$ or $1 . \dot{8} \mathrm{i}$ metres $\quad=1.98839$ yards.
I chô $=\frac{1200}{11}$ or $109.0 \circ 9$ metres $=119.30337$ yards.
I ri $\quad=\frac{432}{110}$ or $3.9 \dot{2} 7$ kilometres $=2.440296$ statute miles.
I kujira shaku $=\frac{25}{88}$ or $\cdot 3 \dot{7} \dot{8}$ metre $\quad=1.24274$ feet.
(cloth measure)

| Metric. $\quad$ Japanese. | Logarithm. |  |
| ---: | :---: | :---: |
| I millimetre $=$ | 33 mô | 1.5185139 |
| I metre | $=3.3$ shaku | 0.5185139 |
| I kilometre | $=.2546 \dot{2} 96$ ri | 9.4059090 |
| British $\quad$ Japanese. | Logarithm. |  |
| I inch $=.838199$ sun | 9.9233473 |  |
| I foot | $=1.005839$ shaku | 0.0025285 |
| I yard | $=3.017517$ shaku | 0.4796498 |
| I mile | $=.4097863$ ri | 9.6125575 |

## Square Measure.

| Japanese. | Metric. | British. |
| :--- | :--- | :--- |
| I shaku | $=.03306$ square metre | $=.3558$ square foot. |
| I gô | $=.3305785$ square metre | $=3.558324$ square feet. |
| I bu or tsubo | $=3.305785$ I square metres | $=3.953693$ square yards. |
| I sē | $=.99173554$ are | $=39.53693$ square yards. |
| I tan | $=.099173554$ hectare | $=.245064$ acre. |
| I chồ | $=.991735537$ hectare | $=2.45064$ acres. |


| Metric. Japanese. | Logarithm. |
| :---: | :---: |
| I square metre $=.3025$ tsubo | 9.4807254 |
| 1 are $\quad=30.25$ tsubo | 1.4807254 |
| I hectare $\quad=\mathrm{I} .008 \dot{3}$ chô | 0.0036041 |
| British. Japanese. | Logarithm. |
| I square foot $=.28 \mathrm{IO} 31 \mathrm{~g}$ gô | 9.4487545 |
| I square yard $=.2529277$ tsubo | 9.4029971 |
| 1 acre $\quad=.40805667$ chô | 9.6107205 |

## Measures of Capacity.

| Japanese. $\quad$ Metric. | British. |
| :--- | :--- |
| I shaku $=.01804$ litre | $=.12698$ gill. |
| I gô $=.18039$ litre | $=.3174515$ pint. |
| I shô $=1.8039068$ litres | $=3.174515$ pints. |
| I to $=18.039068$ litres | $=3.968144$ gallons. |
| I koku $=1.8039068$ hectolitres | $=4.96018$ bushels. |


| Metric. | Japanese. | Logarithm . |
| :--- | :--- | :---: |
| I centilitre $=$ | $=.5543524$ shaku | 9.7437859 |
| I litre $=$ | .5543524 shô | 9.7437859 |
| I hectolitre $=$ | .5543524 koku | 9.7437859 |


| British. $\quad$ Japanese. | Logarithm. |
| :--- | :---: |
| I pint $=3.15008$ gô | 0.4983218 |
| I gallon $=2.5200654$ shô | 0.4014118 |
| I bushel $=.2016052$ koku | 9.3045018 |

## EQUIVALENTS OF THE INDIAN WEIGHTS.

| Indian. | Metri. | British. |
| :---: | :---: | :---: |
| I tola | $=11.66380528$ grammes $=$ | 180 grains. |
| 1 seer | $=.933104423$ kilogram $=$ | 2.0571428 lbs. avoir. |
| 1 maund | $=37.3241769$ kilograms | $82.28571 \dot{4}$ |
|  |  | $\left(\begin{array}{l} 1645 . \dot{j} 1428 \dot{j} \\ 8228571 \dot{4} \\ 8 h o r t \end{array}\right.$ |
| I kandy | $=.746483538$ tonne | (2000 lbs.). |
|  |  | $\begin{aligned} & .7346939 \text { long ton } \\ & (2240 \text { lbs.). } \end{aligned}$ |

I Burmese tikal $=16.55612361$ grammes $=255.5$ grains.
I $\quad, \quad$ viss $=1.65561236 \mathrm{I}$ kilograms $=3.65$ lbs. avoir.

Metric. Indian. Logarithm.

$$
\begin{aligned}
& \text { I kilogram }= \begin{cases}\text { I.071691416 seers } \\
.604006121 \text { Burmese viss } & 0.0300697 \\
\text { I tonne } & =1.7810413 \\
1.33961427 \text { kandy } & 0.1269797\end{cases}
\end{aligned}
$$

British. Indian. Logarithm.

## EQUIVALENTS OF THE STRAITS SETTLEMENTS WEIGHTS.

## Straits Settlements.

Metric.
British.


Metric. Straits Settlements. Logarithm.
I milligram $=.002645547$ hoon $\quad 7.4225155$

1 gramme $=.026455+68$ tahil $\quad 8.4225155$
I kilogram $=1.653466757$ kati $\quad 0.2183955$
I tonne $=.413366689$ koyan 9.6163355
British. Straits Settlements. Logarithm.

| I grain | $=.1 \dot{1} 1428 \dot{5}$ or $\frac{12}{6}$ hoon | 9.2340832 |
| :--- | :--- | :--- |
| I pound avoir. | $=.75$ or $\frac{3}{4}$ kati | 9.8750613 |
| I short ton $(2000$ lbs. $)=.375$ or $\frac{3}{8}$ koyan | 9.5740313 |  |
| I long ton $(2240 \mathrm{lbs})=$..42 koyan | 9.6232493 |  |

Note.-Similar weights to the above, but bearing different names, are used in China (see page 46.)

## EQUIVALENTS OF THE CAPE (S. AFRICA) MEASURES.

## Lineal Measure.

|  | Logarithm. <br> I Cape foot | $=1.033$ British feet |
| ---: | :--- | ---: |$\quad=0.0141003$.

## Square Measure.



## LEGAL EQUIVALENTS* OF THE EGYPTIAN WEIGHTS AND MEASURES.

(Legalised by a decree issued by the Khedive on the 28th April, 1891, with effect from the ist of January, 1892.)

## Commercial Weight.

| Egyptian. | Metric. | British. |
| :---: | :---: | :---: |
| I dirhem | $=3.12 \mathrm{grms}$. | $=48.148928$ grains. |
| I okieh | $=37.44 \mathrm{grms}$. | $=1.320656$ oz. avoir. |
| I rotl or rottolo | $=449.28$ grms. | $=.990492 \mathrm{lb}$. avoir. |
| I oke | $=1.248 \mathrm{kilog}$. | $=2.751367 \mathrm{lbs}$. avoir. (99.049223 lbs. avoir. |
| I kantar | $=44.928$ kilog. | $=\left\{\begin{array}{l} .0495246 \text { short ton (2000 lbs.) } \\ .0442184 \text { long ton }(2240 \mathrm{lbs} .) \end{array}\right.$ <br> 165.082039 lbs. avoir. |
| I hamlah | $=74.880$ kilog. | $=\left\{\begin{array}{l} .08254102 \text { short ton }(2000 \mathrm{lbs} .) \\ .07369734 \text { long ton }(2240 \mathrm{lbs}) . \end{array}\right.$ <br> (308.1531 39 lbs. avoir. |
| I Alexandria ka | $=139.776$ kilog | $\begin{aligned} &=\left\{\begin{array}{l} .15477657 \text { short ton ( } 2000 \mathrm{lbs} .) . \\ .1375684 \text { long ton }(2240 \mathrm{lbs} .) . \end{array}\right. \\ & 550.273463 \text { lbs. avoir. } \end{aligned}$ |
| I heml | $=249.60 \mathrm{kilog}$. | $=\left\{\begin{array}{l} 550.273463 \text { lbs. avoir. } \\ .27513673 \text { short ton (2000 lbs.). } \\ .2456578 \text { long ton }(2240 \mathrm{lbs} .) . \end{array}\right.$ |

Jewellers' Weight.
Egyptian. Metric. British.
I kamha $=48.75$ milligrams $=.752327$ grain .
1 kirat $=.195$ gramme $=3.009308$ grains.
1 dirhem $=3.12$ grammes $=48.148928$ grains.
1 mithkal $=4.68$ grammes $=72.223392$ grains .

| tric. | Egyptian. | Log |
| :---: | :---: | :---: |
| 1 gram | 5.1282 kirats | 0.7099654 |
|  | $=.32051282$ dirhem | 9.5058454 |
| I kilogra | $=2.2257835$ rotls | 0.3474829 |
|  | =.801282 oke | 9.9037854 |
|  | $=.022257835 \mathrm{kantar}$ | 8.3474829 |
| tonne | $=4.0064103 \mathrm{hemls}$ | 0.6027554 |

British. Egyptian. Logarithm.
1 grain

$$
\begin{array}{ll}
=.3323023 \text { kirat } & 9.5215333 \\
=.0207689 \text { dirhem } & 8.3174133 \\
=9.969067 \text { dirhems } & 0.9986545 \\
=1.00960 \text { rotls } & 0.0041489 \\
=20.1920 \text { kantars } & 1.3051789 \\
=22.6150 \text { kantars } & 1.3543969 \\
=4.0707 \text { hemls } & 0.6096695
\end{array}
$$

$$
\text { I oz. troy } \quad=9.969067 \text { dirhems } \quad 0.9986545
$$

$$
\text { I lb. avoir. } \quad=1.00960 \text { rotls } \quad 0.0041489
$$

$$
\text { I short ton }(2000 \text { lbs. })=20.1920 \text { kantars } \quad 1.3051789
$$

$$
\text { I long ton }(2240 \mathrm{lbs} .)=22.6 \mathrm{I} 50 \text { kantars } \quad \text { I. } 3543969
$$

[^20]
## Lineal Measure.

| Egyptian. Metric. British. |  |
| :---: | :---: |
| I diraâ baladi $=0.580$ metre $=\left\{\begin{array}{l}22.835058 \text { inch }\end{array}\right.$ |  |
| diraâ mimari $=0.750$ metre $=\left\{\begin{array}{l}\text { a } \\ 2.460675 \text { feet }\end{array}\right.$ |  |
| I pike istambuli $=0.665$ metre $=2.18176$ feet. |  |
| $=3.550 \text { metres }=\left\{\begin{array}{l} 139.766304 \text { incl } \\ 1 \text { I } .647192 \text { feet } . \end{array}\right.$ |  |
| Metric. Egyptian. | Logarithm. |
| 1 metre $=1.724138$ diraâs baladi | 0.2365720 |
| $=1.3$ or $1 \frac{1}{3}$ diraâs mimari | 0.1249387 |
| $=1.50376$ pikes istambuli | o.1771784 |
| $=.28 \mathrm{I} 69 \mathrm{kassabah}$ | 9.4497716 |
| British. Egyptian. | Logarithm. |
| 1 foot $=.525508$ diraâ baladi | 9.7205791 |
| $=.4063926$ diraâ mimari | 9.6089458 |
| $=.4583455$ pike istambuli | 9.6611930 |
| =.0858576 kassabah | 8.9337787 |
| 1 yard $=.2575728$ kassabah | 9.4109000 |

## Square Measure.

Egyptian.
I square diraâ baladi $=.3364$ square metre $=3.62$ II square feet. I square diraâ mimari $=.5625$ square metre $=6.05492$ square feet. I square kassabah $\quad=12.6025$ square metres $=15.073009$ sq. yards. I feddan

$$
=.42008 \dot{3} \text { hectare } \quad=1.038086 \text { acres } . *
$$

Egyptian.
I square metre $=2.97265$ square diraâs baladi
$=1 . \overline{7}$ or $\mathrm{I} \frac{7}{9}$ square diraâs mimari
$=.079349$ square kassabah
$=2.380480$ feddans
Egyptian.
I square foot $=.27615845$ square diraâ baladi
$=.165155$ square diraâ mimari
I square yard $=.06634374$ square kassabah
1 acre $\quad=.9633113$ feddan.

Logarithm.
0.4731440
0.2498775
8.8995433
0.3766646

Logarithm.
9.4411582
9.2178916
8.8218000
9.9837667

[^21]
## Measures of Capacity.

| Egyptian. | Metric. | British. |
| :--- | :--- | :--- |
| I kirat | $=.06445$ litre | $=.453949$ gill. |
| I karrūbah | $=.1289$ litre | $=.9079$ gill. |
| I tūmnah | $=.2578$ litre | $=1.815797$ gills. |
| I rūbaah | $=.515625$ litre | $=.9079$ pint. |
| I nesf kadah | $=1.03125$ litres | $=1.815797$ pints. |
| I kadah | $=2.0625$ litres | $=3.631595$ pints. |
| I malwa | $=4.125$ litres | $=3.631595$ quarts. |
| I rūb | $=8.25$ litres | $=1.815797$ gallons. |
| I kilah | $=16.5$ litres | $=3.631595$ gallons. |
| I webah | $=33.0$ litres | $=7.26319$ gallons. |
| I ardeb | $=1.98$ hectolitres | $= \begin{cases}43.579136 \text { gallons.* } \\ 5.447392 \text { bushels. }\end{cases}$ |


| Metric. | Egyptian. | Logarithm. |
| :---: | :---: | :---: |
| I hectolitre | $=.500$ ardeb | 9.7033348 |
| I litre | $=.30 \dot{\text { webah }}$ | 8.4814861 |
|  | $=.60$ kilah | 8.7825161 |
|  | $=.12$ rūb | 9.0835461 |
|  | $=. \dot{2} \dot{4}$ malwa | 9.3845761 |
|  | $=.48$ kadah | 9.685606 I |
|  | $=.9 \dot{6}$ nesf kadah | 9.9866361 |
|  | = $\mathrm{I} . \dot{9} \dot{3}$ rübaahs | 0.287666 I |
|  | $=3.8 \dot{7}$ tūmnahs. | 0.588696I |
|  | $=7.75$ karrūbahs | 0.8897261 |
|  | $=15.5 \mathrm{i}$ kirats | I.190756I |


| British. | $\quad$ Egyptian. | Logarithm. |
| ---: | :--- | ---: |
| I bushel | $=.18357409$ ardeb | 9.26381 I 4 |
| I gallon | $=.02294676$ ardeb | 8.3607214 |
|  | $=.13768$ webah | 9.1388727 |
|  | $=.275361$ kilah | 9.4399027 |
|  | $=.550722$ rūb | 9.7409327 |
| I quart | $=.27536 \mathrm{I}$ malwa | 9.4399027 |
| I pint | $=.275361$ kadah | 9.4399027 |
|  | $=.550722$ nesf kadah | 9.7409327 |
|  | $=1.1014445$ rūbaahs | 0.0419627 |
|  | $=2.202889$ tūmnahs | 0.3429927 |
| I gill | $=1.1014445$ karrūbahs | 0.0419627 |
|  | $=2.202889$ kirats | 0.3429927 |

[^22]
## SECTION V. COMPARISON OF PRICES AND RATES OF EXCHANGE.

## COMPARISON OF FRENCH AND GERMAN PRICES FOR METRIC UNITS, BRITISH PRICES FOR IMPERIAL UNITS, AND UNITED STATES PRICES FOR UNITED STATES UNITS.

| $\begin{gathered} \text { Francs } \\ \text { phillings } \\ \text { per } \\ \text { per } \\ \text { kilogram. } \\ \text { avound. } \\ \text { pound. } \end{gathered}$ | $\begin{gathered} \text { Francs } \\ \text { Shillings } \\ \text { per } \\ \text { metre. } \\ \text { per } \\ \text { yard. } \end{gathered}$ | $\begin{array}{cc} \text { Francs } & \text { Shillings } \\ \text { per } \\ \text { per } \\ \text { litre. } & \text { British } \\ \text { Imp. gal. } \end{array}$ | $\begin{gathered} \text { Francs } \\ \text { per } \\ \text { hectolitre. } \end{gathered} \begin{gathered} \text { Sillings } \\ \text { prer } \\ \text { bushelish } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: |
| $=.360$ | $=.725$ | 3.605 | $=.288$ | $=4.110$ |
| $2=.719$ | $2=1.450$ | $2=7.210$ | $=.577$ | $2=8.219$ |
| = 1.079 | $3=2.175$ | $3=10.815$ | $=.865$ | $3=12.329$ |
| $=1.439$ | $4=2.901$ | $4=14.420$ | $=1.154$ | $4=16.439$ |
| = 1.799 | $=3.626$ | $5=18.025$ | $=1.442$ | $=20.549$ |
| $6=2.158$ | $6=4.351$ | $6=21.630$ | $=1.730$ | $6=24.658$ |
| $7 \quad=2.518$ | $7 \quad=5.076$ | $7=25.235$ | $=2.019$ | $7=28.768$ |
| $8=2.878$ | 8 - 5.801 | $8=28.840$ | $=2.307$ | $8=32.878$ |
| $9=3.237$ | $9=6.526$ | $9=32.445$ | $=2.596$ | $9=36.988$ |
| $\begin{array}{r} 2.780=1 \\ 5.560=2 \\ 8.340=3 \\ 11.120=4 \end{array}$ | 1. $379=1$ | . $277=1$ | $3.467=1$ | . $243=1$ |
|  | $2.758=2$ | $\begin{aligned} .555 & =2 \\ .832 & =3\end{aligned}$ | $6.935=2$$10.402=3$ | $\begin{aligned} .487 & =2 \\ .730 & =3\end{aligned}$ |
|  |  |  |  |  |
|  | $5 \cdot 516=4$ | 1. $110=4$ | $13.869=4$ | . $973=4$ |
| $\begin{aligned} & 13.900=5 \\ & 16.680=6 \\ & 19.460=7 \\ & 22.240=8 \\ & 25.020=9 \end{aligned}$ | $\begin{array}{r} 6.895=5 \\ 8.274=6 \\ 9.653=7 \\ 11.032=8 \\ 12.411=9 \end{array}$ | I. $387=5$ <br> 1. $664=6$ <br> 1. $942=7$ <br> $2.219=8$ <br> $2.497=9$ | $\begin{aligned} & 17.337=5 \\ & 20.804=6 \\ & 24.272=7 \\ & 27.739=8 \\ & 31.206=9 \end{aligned}$ | $1.217=5$ <br> $1.460=6$ <br> $1.703=7$ <br> $1.947=8$ <br> 2. $190=9$ |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
| $\begin{gathered} \text { Marks } \\ \text { per } \\ \text { phillings } \\ \text { per } \\ \text { kilogram. } \\ \text { avoir. } \\ \text { pound. } \end{gathered}$ |  | Marks Shillings <br> per <br> per <br> litre. <br> Imp. gal.  |  |  |
|  | Marks Shilling $\underset{\text { per }}{ }$ metre. yard. |  |  | Cents Pence <br> per U.S. per <br> unit of <br> British  <br> weight unit of <br> or lineal weight <br> or lineal  <br> measure. or lineal <br> measure.  |
| $\begin{array}{ll}1 & = \\ 2 & =.444 \\ 3 & =1888 \\ 4 & =1.332 \\ \mathbf{5} & =1.776 \\ 6 & =2.220 \\ 7 & =2.664 \\ 7 & =3.108 \\ 8 & =3.552 \\ 9 & =3.996\end{array}$ | $1=.895$ | $1=4.450$ |  | $1=.493$ |
|  | $2=1.790$ | $2=8.901$ | $1=.356$ $2=.712$ | $2=.986$ |
|  | $3 \quad=2.685$ | 3 = 13.351 | $3=1.068$ | = 1.480 |
|  | $4=3.58 \mathrm{I}$ | $4=17.801$ | $4=1.424$ | $4=1.973$ |
|  | $5 \quad=4.476$ | $5=22.251$ | $5=1.780$ | $5=2.466$ |
|  | $6=5.371$ | $6=26.702$ | $6=2.136$ | $6=2.959$ |
|  | $7 \quad=6.266$ | $7=31.152$ | $7 \quad=2.492$ | $7=3.452$ |
|  | $8=7.16 \mathrm{y}$ | $8=35.602$ | 8 9 | $8=3.945$ |
|  | $9=8.056$ | $9=40.053$ | $9=3.204$ | $9=4.439$ |
| $\begin{aligned} & 2.252=1 \\ & 4.504=2 \\ & 6.756=3 \\ & 9.008=4 \end{aligned}$ | $\begin{aligned} & \text { I. } 117=1 \\ & 2.234=2 \\ & 3 \cdot 35 \mathrm{I}=3 \\ & 4 \cdot 469=4 \end{aligned}$ | . $225=1$ | $2.809=1$ | $2.028=1$ |
|  |  | $\begin{aligned} .449 & =2 \\ .674 & =3\end{aligned}$ | $5.618=2$$8.426=3$ | $4.055=2$ <br> $6.083=3$ |
|  |  |  |  |  |
|  |  | . $899=4$ | 1 $1.235=4$ | 8. $1111=4$ |
| $\begin{aligned} & 11.260=5 \\ & 13.512=6 \\ & 15.764=7 \\ & 18.016=8 \\ & 20.268=9 \end{aligned}$ | $\begin{array}{r} 5.586=5 \\ 6.703=6 \\ 7.820=7 \\ 8.937=8 \\ 10.054=9 \end{array}$ | $\begin{aligned} & \mathrm{I} .124=5 \\ & \mathrm{I} .348=6 \\ & \mathrm{I} .573=7 \\ & \mathrm{I} .798=8 \\ & 2.022=9 \end{aligned}$ | $\begin{aligned} & 14.044=5 \\ & 16.853=6 \\ & 19.662=7 \\ & 22.470=8 \\ & 25.279=9 \end{aligned}$ | $\begin{aligned} & 10.139=5 \\ & 12.166=6 \\ & 14.194=7 \\ & 16.222=8 \\ & 18.249=9 \end{aligned}$ |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |

Comparison of French and German Prices for Metric Units, British Prices for Imperial Units, and United States Prices for United States Units (Continued).

| $\begin{gathered} \text { Francs } \\ \text { per } \begin{array}{c} \text { Dollars } \\ \text { per } \\ \text { perogram. } \\ \text { avoir. } \\ \text { pound. } \end{array} \end{gathered}$ | Francs per metre. | $\begin{gathered} \text { Dollars } \\ \text { per } \\ \text { yard. } \end{gathered}$ | Franc per litre. | Dollars per liquid gal. | $\begin{gathered} \text { Francs Dollars } \\ \text { per } \\ \text { per U.S. } \\ \text { hectititre. bushel. } \end{gathered}$ | $\begin{aligned} & \text { Shillings } \\ & \text { per } \\ & \text { British } \\ & \text { Imp.gal. } \end{aligned}$ | Dollars U.S. liquid gal. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $=.088$ |  | $=.176$ | 1 | = .731 | =. 068 | 1 | $=.203$ |
| =. 175 | 2 | $=.353$ | 2 | = 1.461 | =. 136 | 2 | = . 405 |
| $3=.263$ |  | $=.529$ | 3 | = 2.192 | $=.204$ | 3 | $=.608$ |
| $4=.350$ | 4 | $=.705$ | 4 | $=2.922$ | $=.272$ | 4 | . 810 |
| $=.438$ 。 | 5 | $=.882$ | 5 | $=3.653$ | $=.340$ |  | = 1.013 |
| $6=.525$ |  | $=1.058$ |  | $=4.384$ | $6=.408$ | 6 | $=1.216$ |
| $7=.613$ | 7 | $=1.234$ | 7 | = 5. 114 | $=.476$ | 7 | $=1.418$ |
| $8=.700$ | 8 | $=1.411$ | 8 | $=5.844$ | $=.544$ | 8 | $=1.621$ |
| $9=.788$ |  | $=1.587$ |  | $=6.575$ | $9=.612$ | 9 | $=\mathrm{I} .824$ |
| $11.423=1$ | 5.66 | $7=1$ |  | $69=1$ | $14.703=1$ |  | $5=1$ |
| $22.846=2$ | II. 33 | $4=2$ | 2.73 | 88=2 | $29.407=2$ |  | $1=2$ |
| $34.269=3$ | 17.00 | $0=3$ |  | 6 $=3$ | $44.110=3$ | 14.80 | $6=3$ |
| $45.69 \mathrm{I}=4$ | 22.66 | $7=4$ | 5.47 | $75=4$ | $58.813=4$ | 19.74 | $2=4$ |
| $57.115=5$ | 28.33 | $4=5$ | 6.8 | 44 $=5$ | $73.517=5$ | 24.67 | $7=5$ |
| $68.537=6$ | 34.00 | $1=6$ | 8.21 | $13=6$ | $88.220=6$ | 29.61 | $2=6$ |
| $79.960=7$ | 39.668 | $8=7$ | 9.58 | $8 \mathrm{I}=7$ | $102.923=7$ | 34.54 | $8=7$ |
| $91.383=8$ | 45.33 | $4=8$ | 10.95 | $50=8$ | $117.627=8$ | 39.48 | $3=8$ |
| $102.806=9$ | 51.00 | $\mathrm{I}=9$ | 12.31 | $19=9$ | $132.330=9$ | 44.41 | $9=9$ |



TABLE OF RATES OF EXCHANGE FOR MONEY.

| Country. | Gold Import Point. | Mint Parity. | $\underset{\text { Point. }}{\text { Gold Export }}$ |
| :---: | :---: | :---: | :---: |
| $\left.\begin{array}{l} \text { France, Belgium, } \\ \text { Italy, Switzerland, } \end{array}\right\}$ | Francs 25.35 | Fr. 25.22 | Fr. 25.09 |
| Holland, - - | Florins 12.15 | Fl. 12.1093 | Fl. 12.04 |
| Germany, | Marks 20.51 | M. 20.43 | M. 20.35 |
| Austria-Hungary, | Kronen 24.20 | Kr. 24.02 | Kr. 23.90 |
| Scandinavia, | Kroner 18.30 | Kr. 18.16 | Kr. 18.02 |
| Russia, | Roubles 9.6 <br> (I Rr. $=25 \mathrm{~d}$.) | $\begin{gathered} \text { Rs. } 9.459 \\ \text { (I Rs. } \left.=255_{8}^{3} \mathrm{~d} .\right) \end{gathered}$ | $\begin{gathered} \text { Rs. } 9.366 \\ \left(\mathrm{IRs.}=25 \frac{5}{8} \mathrm{~d} .\right) \end{gathered}$ |
| $\left.\begin{array}{l} \text { United States of } \\ \text { America, } \end{array}\right\}$ | Dollars 4.90 | \$ 4.8665 | \$4.84 |
| British India, - \{ |  | $\begin{aligned} & \text { Rupees } 15 \\ & (1 \mathrm{R}=1 \mathrm{s.} \text { 4d. }) \end{aligned}$ |  |
| Egypt, | Piastres 978 | Piastres $97 \frac{1}{2}$ | Piastres $97 \frac{1}{8}$ |

The above table* gives the value of $£ \mathrm{r}$ sterling in the currencies of the following countries: France, Belgium, Italy, Switzerland, Holland, Germany, Austria-Hungary, Scandinavia, Russia, United States of America, British India and Egypt.

The middle column gives the exchange at mint parity, i.e. the actual gold value of the foreign currency in comparison with the pound sterling, while the other columns show the extremes of fluctuation in the rate of exchange in normal times. In the left-hand column are the rates of exchange at which in sending remittances to London it would be more profitable to send gold than to purchase drafts; while in the right-hand column are the rates at which in remitting from London it would be more profitable to buy gold and send it abroad than to purchase drafts.

[^23]
## PART II. DATA RELATING TO FORCE AND ENERGY.

## SECTION 1. MECHANICAL UNITS.

Force.-The British unit of force is termed the poundal; it is that force which, acting on a mass of 1 lb . for one second, gives it a velocity of one foot per second. On the c.g.s. (centi-metre-gramme-second) system the unit of force is the dyne, which may be defined as that force which, acting on a mass of I gramme, gives it a velocity of a centimetre per second.

$$
1 \text { poundal }=13825 \text { dynes. }
$$

Gravity.-The apparent acceleration (or increase of velocity per unit of time) of a body falling freely under the influence of gravity in vacuo ( $g$ ) varies according to locality. The value of $g$ in C.g.S. units is 981.17 centimetres per second at Greenwich, 980.94 at Paris, 98 I .25 at Berlin, 978.10 at the equator and 983 .II at the poles. The mean value adopted by the International Bureau of Weights and Measures for latitude $45^{\circ}$ at.sealevel is 980.665 .* In British measure the value of $g$ for London at sea-level is about 32.19 feet per second. $\dagger$ The length of the seconds pendulum for the same places is as follows:

Greenwich, 99.413 cm. ; Paris, 99.390 cm. ; Berlin, 9.422 cm. ; equator, 99.103 cm. ; and the poles, 99.6 ro cm .

Work.-The British unit of work is the foot-poundal. It is the work done by a force of I poundal acting over a distance of I foot. Work is also expressed in foot-pounds, the unit in this case being the work done when a body moves through I foot against a resistance of gravity equal to I lb .
r foot-pound $=g$ poundals.

[^24]On the c.g.s. system the unit of work is the erg. It is the work done by a force of I dyne acting over a distance of $I$ centimetre.

I foot poundal $=421401$ ergs.
I foot-pound $=1.356 \times 10^{7}$ ergs ( $g$ being taken as 981 ).
Power.-The British unit of power or rate of doing work is the horse-power. It is equivalent to 33,000 foot-pounds per minute or 550 foot-pounds per second. The French unit-the force de cheval-is defined as 75 kilogram-metres per second. One "force de cheval" equals 0.9863 horse power or 542.48 foot-pounds per second, and conversely i horse-power $=1.01385$ "force de cheval."

On the C.G.S. system the unit of power is I erg per second.
Taking $g$ as equal to $98 \mathbf{r}$, we have
I horse-power $=7.46 \times 10^{9}$ ergs per second.
I force de cheval $=7.36 \times 10^{9}$ ergs per second.

## SECTION II. ELECTRICAL UNITS.

Resistance.-The unit of electrical resistance is the ohm.* It is defined by the Board of Trade $\dagger$ as "the resistance offered to an unvarying electric currrent by a column of mercury, at the temperature of melting ice, 14.452 I grammes in mass of a constant cross sectional area and of a length of 106.3 centimetres." For practical purposes, however, the Board of Trade use as the standard of electrical resistance the resistance between the copper terminals of a coil of insulated wire of platinum alloy to the passage of an unvarying electrical current, at a temperature of 15.4 C . This standard is marked "Board of Trade Ohm Standard, verified $1894, " \ddagger$ and is deposited at the Board of Trade Standardising Laboratory. 'The ohm has the value of $10^{9}$ absolute units on the c.g.s. system.

Current.-The unit of current is the ampere. It is defined by

[^25]the Board of Trade as the electric current, which, when passed through a neutral solution containing 15 per cent. of nitrate of silver, deposits silver at the rate of 0.001118 of a gramme per second.* For practical purposes the standard used by the Board of Trade is the current "which is passing in and through the coils of wire forming part of the instrument marked 'Board of Trade Ampere Standard, verified 1894' when in reversing the current in the fixed coils the change in the forces acting upon the suspended coil in its righted position is exactly balanced by the force exerted by gravity in Westminster upon the iridio platinum weight marked $A$ and forming part of the said instrument." $\dagger$ The ampere has the value of $\frac{1}{10}$ or $10^{-1}$ c.g.s. units.
$$
\text { I milli-ampere }=\frac{1}{100 \delta} \text { ampere. }
$$

I kilo-ampere $=1000$ amperes .
Pressure.-The unit of electrical pressure is the volt. It is " the pressure which, if steadily applied to a conductor whose resistance is one ohm, will produce a current of one ampere, and is represented by 0.6974 of the electrical pressure at a temperature of $15^{\circ} \mathrm{C}$. between the poles of the voltaic cell, known as Clark's cell." $\ddagger$ For practical purposes the unit is measured by a particular instrument marked "Board of Trade Volt Standard, verified 1894," deposited at the Board of Trade Standardising Laboratory. On the c.g.s. system the volt has the value of $10^{8}$.

Quantity.-The unit of quantity is the coulomb. It is the quantity of electricity which in one second of time passes any part of a circuit in which the current has the strength of one ampere. Therefore I coulomb equals i ampere-second.

On the c.g.s. system the coulomb has the value of $10^{-1}$.

$$
\text { I micro coulomb }=\frac{1}{1,000,000} \text { or } 10^{-6} \text { coulomb. }
$$

Capacity.-The unit of capacity is the farad. It is the capacity of a condenser charged to the potential of I volt by i coulomb of electricity. On the c.g.s. system the farad has the value of $10^{-9}$.

$$
\text { I micro-farad }=\frac{1}{1,000,000} \text { or } 10^{-6} \text { farad. }
$$

[^26]Work.-The unit of work is the joule. It is equivalent to the energy disengaged as heat in one second by a current of 1 ampere flowing through a resistance of 1 ohm, or in other words, under an electro-motive force of $I$ volt.

$$
\mathrm{I} \text { joule }=1 \mathrm{o}^{7} \text { ergs or absolute units of work. }
$$

Power.-The unit of power or rate of doing work is the watt. It is the work done at the rate of I joule per second. In other words, the watt represents the energy contained in a current of one ampere flowing under an electro-motive force of 1 volt. On the c.g.s. system the watt represents $10^{7}$ ergs per second. The practical unit of work is the kilowatt.

$$
\begin{aligned}
\text { I kilowatt } & =1000 \text { watts } \\
& =1.34 \text { horse-power. } \\
\text { I horse-power } & =746 \text { watts or } .746 \text { kilowatt. }
\end{aligned}
$$

The commercial or Board of Trade unit is the kilowatt-hour. It is defined by the Board of Trade as "the energy contained in a current of one thousand amperes flowing under an electro-motive force of one volt during one hour."

Induction.-The unit of induction is the henry. It is the induction in a circuit when the electro-motive force induced in this circuit is one volt, while the inducing current varies at the rate of one ampere per second.

On the c.g.s. system the henry has the value of $10^{9}$.


## SECTION III. THERMAL UNITS.

The British thermal unit is the amount of heat required to raise 1 pound of water through I degree Fahrenheit. The thermal capacity of water varies slightly with the temperature; but the standard temperature of the water at which the unit should be defined has not yet been fixed by convention.

The French thermal unit is the therm or gramme-degree. It has also been termed the minor calorie. It is the quantity of heat required to raise I gramme of water through I degree Centigrade. It is sometimes defined as the amount of heat required to raise I gramme of water from $0^{\circ} \mathrm{C}$. to $\mathrm{I}^{\circ} \mathrm{C}$., or as the one-hundredth part of the heat required to raise one gramme of water from $0^{\circ}$ to $100^{\circ} \mathrm{C}$.

The major calorie is the quantity of heat required to raise I kilogramme of water through I degree Centigrade.

I major calorie $\quad=1000$ therms.
I therm or minor calorie $=0.0039683^{2}$ British thermal unit ( $\log =7.5986067$ ).
I British thermal unit $=25 \mathrm{r} .99579$ therms

$$
(\log =2.40 \mathrm{I} 3933) .
$$

The capacity for heat (or thermal capacity) of a substance is the quantity of heat required to raise the temperature of that substance I degree (Centigrade or Fahrenheit, according to the units in use).

The capacity for heat of water can be expressed thus:
I calorie (therm) $=4.180$ joules at $20^{\circ} \mathrm{C}$.*
The specific heat of a substance is the ratio of the quantity of heat required to raise the temperature of a given mass of any substance one degree to the quantity of heat required to raise the temperature of an equal mass of water one degree (Glazebrook).

The latent heat of fusion is the quantity of heat required to change I gramme (or I lb .) of a substance from the solid to its liquid form without raising its temperature. The latent

[^27]heat of fusion of ice is 80 therms (Bunsen) or 144 British thermal units.

The latent heat of vaporization of a liquid is the amount of heat required to change I gramme (or I lb.) of the liquid into vapour without raising its temperature. The latent heat of vaporization of water is 537 therms, or 967 British thermal units.

The evaporative power or calorific value of a fuel is the number of pounds of water evaporated at $212^{\circ} \mathrm{F}$. by the combustion of I lb. of that fuel. It may be expressed in British thermal units by multiplying the number of pounds of water evaporated at $212^{\circ} \mathrm{F}$. by 967 (the latent heat of vaporization of water).

The mechanical equivalent of heat. The symbol $J$ is used to designate the number of units of work necessary to generate one unit of heat when the unit is all spent in generating heat. Prof. Rowland's experiments show that at $20^{\circ}$ C.*

$$
\begin{aligned}
J & =427.5 \text { gramme-metres } \\
& =779 \text { foot-pounds, }
\end{aligned}
$$

i.e. the work done in raising $\left\{\begin{array}{l}\mathrm{I} \text { gramme } \\ \mathrm{I} \text { pound }\end{array}\right\}$ through $\left\{\begin{array}{l}427.5 \text { metres } \\ 779.0 \text { feet }\end{array}\right\}$ will, if spent in friction, raise the temperature of $\left\{\begin{array}{l}\text { I gramme } \\ \text { I pound }\end{array}\right\}$ of water I degree $\left\{\begin{array}{l}\text { Centigrade } \\ \text { Fahrenheit }\end{array}\right\}$.

[^28]Thermometric Scales.
Comparative Table of Fahrenheit, Réaumur and Centigrade Degrees.

| Degrees. |  |  | Degrees. |  |  | Degrees. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fahr. | Réaum. | Cent. | Fahr. | Réaum. | Cent. | Fahr. | Réaum. | Cent. |
| 212 | 80.0 | 100.0 | 171 | 61.8 | 77.2 | 130 | 43.6 | 54.4 |
| 211 | 79.6 | 99.4 | 170 | 61.3 | 76.7 | 129 | 43.1 | 53.9 |
| 210 | 79.1 | 98.9 | 169 | 60.9 | 76.1 | 128 | 42.7 | 53.3 |
| 209 | 78.7 | 98.3 | 168 | 60.4 | 75.6 | 127 | 42.2 | 52.8 |
| 208 | 78.2 | 97.8 | 167 | 60.0 | 75.0 | 126 | 41.8 | 52.2 |
| 207 | 77.8 | 97.2 | 166 | 59.6 | 74.4 | 125 | 4 I .3 | 51.7 |
| 206 | 77.3 | 96.7 | 165 | 59.1 | 73.9 | 124 | 40.9 | 51.1 |
| 205 | 76.9 | 96. I | 164 | 58.7 | 73.3 | 123 | 40.4 | 50.6 |
| 204 | 76.4 | 95.6 | 163 | 58.2 | 72.8 | 122 | 40.0 | 50.0 |
| 203 | 76.0 | 95.0 | 162 | 57.8 | 72.2 | 12 I | 39.6 | 49.4 |
| 202 | 75.6 | 94.4 | 161 | 57.3 | 71.7 | 120 | 39.1 | 48.9 |
| 201 | 75.1 | 93.9 | 160 | 56.9 | 71.1 | 119 | 38.7 | 48.3 |
| 200 | 74.7 | 93.3 | 159 | 56.4 | 70.6 | 118 | 38.2 | 47.8 |
| 199 | 74.2 | 92.8 | 158 | 56.0 | 70.0 | 117 | 37.8 | 47.2 |
| 198 | 73.8 | 92.2 | 157 | 55.6 | 69.4 | 116 | 37.3 | 46.7 |
| 197 | 73.3 | 91.7 | 156 | 55.1 | 68.9 | 115 | 36.9 | 46.1 |
| 196 | 72.9 | 91.1 . | 155 | 54.7 | 68.3 | 114 | 36.4 | 45.6 |
| 195 | 72.4 | 90.6 | 154 | 54.2 | 67.8 | 113 | 36.0 | 45.0 |
| 194 | 72.0 | 90.0 | 153 | 53.8 | 67.2 | 112 | 35.6 | 44.4 |
| 193 | 71.6 | 89.4 | 152 | 53.3 | 66.7 | III | 35.1 | 43.9 |
| 192 | 7 I .1 | 88.9 | 151 | 52.9 | 66.1 | 110 | 34.7 | 43.3 |
| 191 | 70.7 | 88.3 | 150 | 52.4 | 65.6 | 109 | 34.2 | 42.8 |
| 190 | 70.2 | 87.8 | 149 | 52.0 | 65.0 | 108 | 33.8 | 42.2 |
| 189 | 69.8 | 87.2 | 148 | 5 S .6 | 64.4 | 107 | 33.3 | 41.7 |
| 188 | 69.3 | 86.7 | 147 | 5 I .1 | 63.9 | 106 | 32.9 | 4 I .1 |
| 187 | 68.9 | 86.1 | 146 | 50.7 | 63.3 | 105 | 32.4 | 40.6 |
| 186 | 68.4 | 85.6 | 145 | 50.2 | 62.8 | 104 | 32.0 | 40.0 |
| 185 | 68.0 | 85.0 | 144 | 49.8 | 62.2 | 103 | 31.6 | 39.4 |
| 184 | 67.6 | 84.4 | 143 | 49.3 | 61.7 | 102 | 31.1 | 38.9 |
| 183 | 67.1 | 83.9 | 142 | 48.9 | 6 I .1 | 101 | 30.7 | 38.3 |
| 182 | 66.7 | 83.3 | 141 | 48.4 | 60.6 | 100 | 30.2 | 37.8 |
| 181 | 66.2 | 82.8 | 140 | 48.0 | 60.0 | 99 | 29.8 | 37.2 |
| 180 | 65.8 | 82.2 | 139 | 47.6 | 59.4 | 98 | 29.3 | 36.7 |
| 179 | 65.3 | 8 I .7 | 138 | 47.1 | 58.9 | 97 | 28.9 | 36.1 |
| 178 | 64.9 | 81.1 | 137 | 46.7 | 58.3 | 96 | 28.4 | 35.6 |
| 177 | 64.4 | 80.6 | 136 | 46.2 | 57.8 | 95 | 28.0 | 35.0 |
| 176 | 64.0 | 80.0 | 135 | 45.8 | 57.2 | 94 | 27.6 | 34.4 |
| 175 | 63.6 | 79.4 | 134 | 45.3 | 56.7 | 93 | 27.1 | 33.9 |
| 174 | 63.1 | 78.9 | 133 | 44.9 | 56.1 | 92 | 26.7 | 33.3 |
| 173 | 62.7 | 78.3 | 132 | 44.4 | 55.6 | 91 | 26.2 | 32.8 |
| 172 | 62.2 | 77.8 | 131 | 44.0 | 55.0 | 90 | 25.8 | 32.2 |

Comparative Table of Fahrenheit, Réaumur and Centigrade Degrees (Continued).

| Degrees. |  |  | Degrees. |  |  | Degrees. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fahr. | Réaum. | Cent. | Fahr. | Réaum. | Cent. | Fabr. | Réaum. | Cent. |
| 89 | 25.3 | 31.7 | 48 | 7.1 | 8.9 | 7 | - 11.1 | - 13.9 |
| 88 | 24.9 | 3 I I | 47 | 6.7 | 8.3 | 6 | - II. 6 | - 14.4 |
| 87 | 24.4 | 30.6 | 46 | 6.2 | 7.8 | 5 | -12.0 | - 15.0 |
| 86 | 24.0 | 30.0 | 45 | 5.8 | 7.2 | 4 | - 12.4 | - 15.6 |
| 85 | 23.6 | 29.4 | 44 | $5 \cdot 3$ | 6.7 | 3 | -12.9 | -16.1 |
| 84 | 23.1 | 28.9 | 43 | 4.9 | 6.1 | 2 | - 13.3 | -16.7 |
| 83 | 22.7 | 28.3 | 42 | $4 \cdot 4$ | 5.6 | 1 | - 13.8 | - 17.2 |
| 82 | 22.2 | 27.8 | 41 | 4.0 | 5.0 | - | -14.2 | - 17.8 |
| 81 | 21.8 | 27.2 | 40 | 3.6 | $4 \cdot 4$ | - I | - 14.7 | $-18.3$ |
| 80 | 21.3 | 26.7 | 39 | 3.1 | 3.9 | -2 | -15.I | - 18.9 |
| 79 | 20.9 | 26.1 | 38 | 2.7 | 3.3 | -3 | - 15.6 | - 19.4 |
| 78 | 20.4 | 25.6 | 37 | 2.2 | 2.8 | -4 | - 16.0 | -20.0 |
| 77 | 20.0 | 25.0 | 36 | 1.8 | 2.2 | - 5 | - 16.4 | - 20.6 |
| 76 | 19.6 | 24.4 | 35 | 1.3 | 1.7 | -6 | -16.9 | -21.1 |
| 75 | 19.1 | 23.9 | 34 | 0.9 | I.I | -7 | -17.3 | -21.7 |
| 74 | 18.7 | 23.3 | 33 | 0.4 | 0.6 | -8 | - 17.8 | - 22.2 |
| 73 | 18.2 | 22.8 | 32 | 0.0 | 0.0 | -9 | - 18.2 | - 22.8 |
| 72 | 17.8 | 22.2 | 31 | -0.4 | -0.6 | - 10 | - 18.7 | - 23.3 |
| 71 | 17.3 | 21.7 | 30 | -0.9 | - I. 1 | - II | - 19.1 | -23.9 |
| 70 | 16.9 | 21.1 | 29 | - I. 3 | - 1.7 | - 12 | - 19.6 | - 24.4 |
| 69 | 16.4 | 20.6 | 28 | - 1.8 | -2.2 | - 13 | -20.0 | - 25.0 |
| 68 | 16.0 | 20.0 | 27 | -2.2 | -2.8 | -14 | - 20.4 | -25.6 |
| 67 | 15.6 | 19.4 | 26 | -2.7 | -3.3 | - 15 | -20.9 | - 26.1 |
| 66 | 15.1 | 18.9 | 25 | -3.1 | -3.9 | -16 | -21.3 | -26.7 |
| 65 | 14.7 | 18.3 | 24 | -3.6 | -4.4 | -17 | -21.8 | - 27.2 |
| 64 | 14.2 | 17.8 | 23 | -4.0 | - 5.0 | -18 | - 22.2 | -27.8 |
| 63 | 13.8 | 17.2 | 22 | -4.4 | -5.6 | - 19 | -22.7 | $-28.3$ |
| 62 | 13.3 | 16.7 | 21 | -4.9 | -6.1 | -20 | -23.1 | - 28.9 |
| 61 | 12.9 | 16.1 | 20 | - 5.3 | -6.7 | -21 | - 23.6 | - 29.4 |
| 60 | 12.4 | 15.6 | 19 | - 5.8 | -7.2 | -22 | -24.0 | - 30.0 |
| 59 | 12.0 | 15.0 | 18 | -6.2 | -7.8 | -23 | -24.4 | -30.6 |
| 58 | 11.6 | 14.4 | 17 | -6.7 | -8.3 | -24 | -24.9 | -31.1 |
| 57 | 1 I .1 | 13.9 | 16 | -7.1 | -8.9 | -25 | -25.3 | -31.7 |
| 56 | 10.7 | 13.3 | 15 | - 7.6 | -9.5 | -26 | -25.8 | -32.2 |
| 55 | 10.2 | 12.8 | 14 | -8.0 | - 10.0 | -27 | -26.2 | - 32.8 |
| 54 | 9.8 | 12.2 | 13 | -8.4 | - 10.6 | -28 | -26.7 | -33.3 |
| 53 | 9.3 | 11.7 | 12 | -8.9 | - II.1 | -29 | -27.1 | - 33.9 |
| 52 | 8.9 | 11.1 | 11 | -9.3 | - 11.7 | -30 | -27.6 | - 34.4 |
| 51 | 8.4 | 10.6 | 10 | -9.8 | $-12.2$ | -31 | -28.0 | - 35.0 |
| 50 | 8.0 | 10.0 | 9 | -10.2 | - 12.8 | -32 | -28.4 | -35.6 |
| 49 | 7.6 | 9.4 | 8 | - 10.7 | - 13.3 | -33 | -28.9 | -36.1 |

To convert Fahrenheit degrees to Centigrade or Réaumur, subtract 32 and multiply the difference by $\frac{5}{9}$ or $\frac{4}{9}$ respectively. To convert Centigrade or Réaumur to Fahrenheit, multiply by $\frac{9}{5}$ or $\frac{9}{4}$, as the case may be, and add 32 to the product. To convert Centigrade to Réaumur, multiply Centigrade degrees by $\frac{4}{5}$; and to convert to Centigrade, multiply Réaumur degrees by $\frac{5}{4}$. To obtain absolute temperature, add $273^{\circ}$ to the Centigrade scale.

## Photometric Standards.

The British unit of light, the candle pozver, as originally defined,* is the illuminating power of a sperm candle $\frac{7}{8}$ inch in diameter ( 6 to the pound) burning 120 grains per hour. The Harcourt ro-candle power pentane lamp, however, is accepted by the Gas Referees as representing ten British candles.

The French unit, the Carcel, is the illuminating power of a lamp burning 42 grammes of pure colza oil per hour.

The German unit, the Hefner, is the illuminating power of the Hefner-Alteneck lamp, burning amyl-acetate with a cylindrical wick 8 mm . in diameter and a flame-height of 40 mm .

The International Congress, held at Paris in April, 1884, proposed the illuminating power of a square centimetre of molten platinum at the temperature of solidification as a unit ; but at the Congress held in 1890 the 20 th part of this unit was adopted as the international standard unit, under the name of the decimal candle.

The following relations between these lamps have been established by tests made in the German Reichsanstalt, at the instance of the International Committee on Photometry. The tests were made in air containing 8.8 litres of aqueous vapour per cubic metre of dry air, and under a barometric pressure of $760 \mathrm{~mm} . \dagger$


I Decimal candle $=$. . 02 Harcourt units.
$=1.02$ British candles.
$=.104$ Carcels.
$=\mathbf{1 . 1 2 2 ~ H e f n e r s . ~}$

[^29]
## PART III. DATA RELATING TO WATER.

## SECTION I. CONSTANTS.

## Relation of Weight and Volume.

The Imperial Gallon is the volume of 10 avoir. lbs. of distilled water weighed in air against brass weights, with the water and air at a temperature of $62^{\circ}$ Fahr., under a barometric pressure of 30 inches. The following constants apply to water under these conditions:*

Weight of $x$ cubic inch of water at $62^{\circ} \mathrm{F}$.

$$
\begin{array}{ll}
=252.3253 \text { grains. } & \log =2.4019608 \\
=.0360465 \text { lb. } & \\
=.00360465 \text { Imp. gallon. } & \log =7.5568628 \\
=7.556628
\end{array}
$$

Weight of 1 cubic foot of water at $62^{\circ} \mathrm{F}$.
$=62.2883$ lbs. $\quad \log =1.7944065$
$=6.22883$ Imp. gallons. $\quad \log =0.7944065$
Volume of 1 short ton ( 2000 lbs .) of water at $62^{\circ} \mathrm{F}$.
$=32.1088$ cub. feet. $\log =1.5066235$
Volume of 1 long ton ( 2240 lbs .) of water at $62^{\circ} \mathrm{F}$.
$=35.9618 \mathrm{cub}$. feet.
I Imperial gallon

$$
\begin{array}{lll}
=277.420 \text { cub. inches. } & & \log =2.4431372 \\
=.160544 \text { cub. foot. } & & \log =9.2055935
\end{array}
$$

A column of water I foot high at $62^{\circ} \mathrm{F}$. exerts a pressure of $.4325^{\circ} \mathrm{lb}$. per sq. inch : $\log =9.6360419$.
A pressure of I lb . per sq. in. is exerted by a column of water at $62^{\circ}$ F., 2.31184 feet high: $\log =0.363958$ r.

The Litre is the volume of a kilogram of distilled water weighed in vacuo at its temperature of maximum density * See page 7 .
( $4^{\circ} \mathrm{C}$. or $39^{\circ} .2 \mathrm{~F}$.). By means of the equivalents given on page 33, and the weight of a cubic decimetre of water on page 4 , we find that

I gramme per cubic centimetre $=62.4278 \mathrm{lbs}$. per cubic foot ; and the weight in vacuo of 1 cubic decimetre of distilled water at $4^{\circ} \mathrm{C}=.999974$ kilogram.

Therefore the weight in vacuo of I cubic foot of distilled water at $4^{\circ} \mathrm{C} .=62.4278 \times .999974=62.4262 \mathrm{lbs}$.

## Constants used in the measurement of flow.

1 cusec* of water at $62^{\circ} \mathrm{F}$.
$=60$ cubic feet per minute $\quad \log =1.778{ }^{5} 513$
$=3600$ cubic feet per hour $\quad \log =3.5563025$
$=86400$ cubic feet per day of 24 hours $\log =4.9365137$
$=6.22883$ Imp. gallons per second $\quad \log =0.7944065$
$=373.73$ Imp. gallons per minute $\quad \log =2.572557^{8}$
$=22423.8$ Imp. gallons per hour $\quad \log =4.3507090$
$\left.\begin{array}{c}538170.9 \text { Imp. gallons per day of } \\ 24 \text { hours }\end{array}\right\} \log =5.7309202$
$=7.48026$ U.S. gallons per second $\quad \log =0.8739167$
$=448.8$ I6 U.S. gallons per minute $\quad \log =2.6520680$
$=26928.94$ U.S. gallons per hour $\quad \log =4.4302192$
$=646294 \cdot 4$ U.S. gallons per day of $\} \log =5.8104304$
24 hours.
r cubic foot per minute of water at $62^{\circ} \mathrm{F}$.
$=60$ cubic feet per hour $\quad \log =1.7781513$
$=1440$ cubic feet per day of 24 hours $\log =3.1583625$
$=6.22883$ Imp. gallons per minute $\quad \log =0.7944065$
$=373.73$ Imp. gallons per hour $\quad \log =2.5725578$
$\left.\begin{array}{l}=8969.54 \text { Imp. gallons per day of } \\ 24 \text { hours }\end{array}\right\} \log =3.5927700$
$=7.48026$ U.S. gallons per minute $\quad \log =0.8739167$
$=448.816$ U.S. gallons per hour $\quad \log =2.6520680$
$\left.=\begin{array}{r}10771.58 \text { U.S. gallons per day of } \\ 24 \text { hours. }\end{array}\right\} \log =4.0322792$
The miner's inch is usually taken to be a flow of I .5 cubic feet per minute.

* 'Cusec' is the abbreviation of 'cubic foot per second,' commonly used in referring to the flow of water.

The volume in cubic centimetres at various temperatures from $0^{\circ}$ to $35^{\circ}$ Centigrade of a cubic centimetre of distilled water at $4^{\circ}$ C.*

| Temp. C. | - 0 | $\cdot 1$ | -2 | 3 | $\cdot 4$ | $\cdot 5$ | $\cdot 6$ | $\cdot 7$ | - 8 | $\cdot 9$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0{ }^{\circ}$ | 1.000127 | 120 | 114 | 108 | 102 | 096 | 091 | 086 | 080 | 075 |
| 1 | 070 | 066 | 061 | 057 | 052 | 048 | 044 | 040 | 037 | 033 |
| 2 | 030 | 027 | 024 | 021 | 019 | 017 | OI4 | 012 | oro | 009 |
| 3 | 007 | 006 | 004 | 003 | 002 | 002 | OOI | 001 | 000 | 000 |
| 4 | 000 | 000 | 001 | 001 | 001 | 002 | 003 | 004 | 005 | 007 |
| 5 | 1.000008 | 010 | 012 | 014 | or6 | or8 | 020 | 023 | 026 | 029 |
| 6 | 032 | 035 | 038 | 041 | 045 | 049 | 053 | 057 | 061 | 065 |
| 7 | 069 | 074 | 079 | 084 | 089 | 094 | 099 | 105 | 110 | 116 |
| 8 | 122 | 128 | 134 | 141 | 147 | 154 | 160 | 167 | 174 | 181 |
| 9 | 189 | 196 | 204 | 211 | 219 | 227 | 235 | 244 | 252 | 260 |
| 10 | 1.000269 | 278 | 287 | 296 | 305 | 314 | 324 | 334 | 343 | 353 |
| 11 | 363 | 373 | 383 | 394 | 405 | 415 | 426 | 437 | 448 | 459 |
| 12 | 471 | 482 | 494 | 505 | 517 | 529 | 541 | 553 | 566 | 578 |
| 13 | 591 | 603 | 616 | 629 | 642 | 655 | 668 | 681 | 695 | 709 |
| 14 | 722 | 736 | 750 | 765 | 779 | 794 | 809 | 823 | 838 | 853 |
| 15 | 1.000868 | 884 | 899 | 914 | 930 | 945 | 961 | 977 | 993 | $\overline{009}$ |
| 16 | 1025 | 042 | 058 | 075 | 091 | 108 | 125 | 142 | 159 | 177 |
| 17 | 194 | 211 | 229 | 247 | 265 | 283 | 301 | 319 | 338 | 356 |
| 18 | 374 | 393 | 412 | 431 | 450 | 469 | 488 | 507 | 527 | 546 |
| 19 | 566 | 585 | 605 | 625 | 645 | 666 | 686 | 707 | 727 | 748 |
| 20 | 1.001768 | 789 | 810 | 831 | 852 | 874 | 895 | 916 | 938 | 960 |
| 21 | 981 | 003 | 025 | $\overline{047}$ | 069 | $\overline{092}$ | 114 | 137 | 159 | 182 |
| 22 | 2205 | 228 | 251 | 274 | 297 | 320 | 343 | 367 | 391 | 414 |
| 23 | 438 | 462 | 486 | 510 | 534 | 559 | 583 | 607 858 | 632 | 657 |
| 24 | 682 | 707 | 732 | 757 | 782 | 807 | 833 | 858 | 884 | 910 |
| 25 | 1.002935 | 961 | 987 | 014 | 040 | 066 | 092 | 119 | 146 | 172 |
| 26 | 3199 | 226 | 253 | 280 | 307 | 335 | 362 | 389 | 417 | 445 |
| 27 | 472 | 500 | 528 | 556 | 584 | 612 | 641 | 669 | 697 | 726 |
| 28 | 754 | 783 | 812 | 841 | 870 | 899 | 928 | 957 | 987 | $\overline{\mathrm{O} 6}$ |
| 29 | 4045 | 075 | 105 | 134 | 164 | 194 | 224 | 254 | 284 | 315 |
| 30 | 1.004.345 |  |  | 436 | 467 | 498 | 529 | 560 | 591 | 622 |
| 31 | 653 | 684 | 716 | 748 | 780 | 81 I | 843 | 875 | $\underline{907}$ | 939 |
| 32 | 971 | 003 | 036 | 068 | 101 | 133 | 166 | 199 | 231 | 264 |
| 33 | 5297 | 330 | 363 | 396 | 430 | 463 | 497 | 530 | 564 | 597 |
| 34 | 631 | 665 | 699 | 733 | 767 | 801 | 835 | 870 | 904 | 939 |
| 35 | 1.005973 | 008 | 042 | 077 | III | $\overline{146}$ | 181 | 217 | 252 | 287 |

For $162_{3}^{\circ} \mathrm{C} .\left(62^{\circ} \mathrm{F}\right.$.) the volume is $\mathrm{r} .00113^{3} 6$.

[^30]
## SECTION II. MEASUREMENT OF THE FLOW OF WATER.

In measuring the flow of a stream by means of a rectangularnotched weir (Fig. 1), the length of the notch should be at least three times the depth of water on the sill. Air should have free access to the space behind the falling sheet of water, and the sill should be carefully levelled.


Fig. i.
End contraction, which occurs when the weir at each end of the notch projects into the approach channel, diminishes the discharge. The contraction is complete, that is as great as it can be, when the distance from the end of the notch to the side of the approach channel is equal to the depth of water on the sill. If the width of the notch be not less than three times the depth of water on the sill, a complete end contraction diminishes the effective width of the notch by an amount equal to one-tenth of the depth of the water on the sill. If contraction occurs at both ends of the notch, the effective width will of course be diminished by twice the above amount.

The notches of weirs should be made preferably in thin sheet iron; if in wood, the downstream side should be bevelled off so as to present a smooth sharp edge to the water on the upstream side. In a wooden weir two inches thick, a notch cut with square edges (without bevel) gives a discharge $15 \frac{1}{2}$ per cent. less than that of a similar notch in thin sheet iron. The weir can be made of deal boards with the notch cut in the wood, or a thin sheet iron plate with the notch can be attached to the topmost board. The weir site should be chosen at a point where the stream will be dammed back for at least six feet. The weir should be let into the banks and should be firmly fixed into
position and made water-tight by means of clay. Unless a proper approach channel is provided, the ends of the notch should be far enough from the banks to ensure complete end contraction, which must then be allowed for. No measurements should be made until the normal flow of the stream is passing through the notch. The depth of the water must not be measured on the notch itself, but from the sill to the surface of the still water at a point some six feet above the weir, a level being employed.

For gauging a small flow, a right-angled triangular notch (Fig. 2) will be found more convenient. It is the only form of notch in which the periphery always bears the same ratio to the cross-sectional area of the stream flowing through it.


Fig. 2.
On pages 72 and 73 are tables giving the discharges through each form of notch for a varying depth of water. In the first table, which is for a rectangular-notched weir in thin sheet iron,
$Q=$ Discharge in 'cusecs' (cubic feet per second).
$H=$ Depth in feet of water, measured from sill of notch to surface of still water above the weir.
$L=$ Width in feet of notch.
$Q=3.33 L H \sqrt{\prime} \bar{H}$ (Francis' formula).
The table is calculated for a notch 1 foot in width, and no deduction has been made for end contraction which is hardly appreciable when $H$ is less than $\frac{L}{10}$. In using the table, multiply $Q$ by the effective width of the notch in feet.

Table for Estimating Discharge of Water through a Rectangularnotched Weir, without end contraction.

| $H$ | $Q$ | $H$ | $Q$ | H | $Q$ | $H$ | $Q$ | $H$ | $Q$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . OI | 0.003 | . 51 | 1.213 | I. O | 3.380 | 1.51 | 6. 179 | 2.01 | 9.489 |
| . 02 | 0.009 | . 52 | 1. 249 | 1.02 | 3.430 | I. 52 | 6.240 | 2.02 | 9.560 |
| . 03 | 0.017 | . 53 | I. 285 | 1.03 | $3 \cdot 481$ | I. 53 | 6.302 | 2.03 | 9.631 |
| . 04 | 0.027 | . 54 | I. 321 | I. 04 | 3.532 | I. 54 | 6.364 | 2.04 | 9.703 |
| . 05 | 0.037 | . 55 | 1.358 | 1.05 | 3.583 | I. 55 | 6.426 | 2.05 | 9.774 |
| . 06 | 0.049 | . 56 | 1.395 | 1.06 | 3.634 | I. 56 | 6.488 | 2.06 | 9.846 |
| . 07 | 0.062 | . 57 | 1.433 | 1.07 | 3.686 | I. 57 | 6.551 | 2.07 | 9.917 |
| . 08 | 0.075 | . 58 | 1.471 | 1.08 | 3.737 | I. 58 | 6.613 | 2.08 | 9.989 |
| . 09 | 0.090 | . 59 | I. 509 | 1.09 | 3.790 | I. 59 | 6.676 | 2.09 | 10.062 |
| . 10 | -. 105 | . 60 | I. 548 | I. 10 | 3.842 | I.60 | 6.739 | 2.10 | Io. 134 |
| . 11 | 0.121 | .61 | I. 586 | I. 11 | 3.894 | 1.61 | 6.803 | 2.11 | 10.206 |
| . 12 | 0.138 | . 62 | 1.626 | 1.12 | 3.947 | 1.62 | 6.866 | 2.12 | Io. 279 |
| . 13 | -. I 56 | . 63 | I. 665 | I. 13 | 4.000 | 1. 63 | 6.930 | 2.13 | 10.352 |
| . 14 | o. 174 | . 64 | 1.705 | I. 14 | 4.053 | 1. 64 | 6.994 | 2. 14 | 10.425 |
| . 15 | o. 193 | . 65 | I. 745 | I. 15 | 4.107 | 1. 65 | 7.058 | 2.15 | 10.498 |
| . 16 | 0.213 | . 66 | 1.786 | 1.16 | 4.160 | 1. 66 | 7.122 | 2.16 | 10.571 |
| . 17 | 0.233 | . 67 | 1.826 | 1.17 | 4.214 | 1. 67 | 7.187 | 2.17 | 10.645 |
| . 18 | 0.254 | . 68 | I. 867 | I. 18 | 4.268 | 1.68 | 7.251 | 2.18 | 10.718 |
| . 19 | 0.276 | . 69 | 1.909 | I. 19 | 4.323 | I. 69 | $7 \cdot 316$ | 2.19 | 10.792 |
| . 20 | 0.298 | . 70 | 1.950 | 1.20 | $4 \cdot 377$ | 1.70 | 7.38I | 2.20 | 10.866 |
| .21 | 0. 320 | . 71 | 1.992 | I. 21 | 4.432 | 1.71 | 7.446 | 2.21 | 10.940 |
| . 22 | 0.344 | . 72 | 2.034 | 1.22 | 4.487 | 1.72 | 7.512 | 2.22 | 11.015 |
| . 23 | 0. 367 | . 73 | 2.077 | 1. 23 | 4.543 | 1.73 | 7.577 | 2.23 | 11.089 |
| . 24 | 0. 392 | . 74 | 2.120 | I. 24 | 4.598 | I. 74 | 7.643 | 2.24 | II. 164 |
| . 25 | 0.416 | . 75 | 2.163 | I. 25 | 4.654 | 1.75 | 7.709 | 2.25 | II. 239 |
| . 26 | 0.441 | . 76 | 2.206 | I. 26 | 4.710 | I. 76 | 7.775 | 26 | II. 314 |
| . 27 | 0:467 | . 77 | 2.250 | 1.27 | 4.766 | I. 77 | 7.842 | 2.27 | II. 389 |
| . 28 | - 0.493 | . 78 | 2.294 | 1. 28 | 4.822 | 1. 78 | 7.908 | 2.28 | II. 464 |
| . 29 | 0. 520 | . 79 | 2.338 | I. 29 | 4.879 | I. 79 | 7.975 | 2.29 | II. 540 |
| . 30 | 0. 547 | . 80 | 2.383 | I. 30 | 4.936 | I. 80 | 8.042 | 2.30 | 11.615 |
| . 31 | 0. 575 | . 81 | 2.428 | I.3I | 4.993 | 1.81 | 8. 109 | 2.31 | 11.691 |
| . 32 | 0.603 | . 82 | 2.473 | I. 32 | 5.050 | 1.82 | 8.176 | 2.32 | II. 767 |
| . 33 | 0.63 I | . 83 | 2.518 | I. 33 | 5.108 | I. 83 | 8.244 | 2.33 | 11.843 |
| . 34 | 0.660 | . 84 | 2.564 | I. 34 | 5.165 | 1.84 | 8.311 | 2.34 | II. 920 |
| . 35 | 0.690 | . 85 | 2.610 | I. 35 | 5.223 | 1. 85 | 8.379 | 2.35 | 11.996 |
| . 36 | - 0.719 | . 86 | 2.656 | I. 36 | 5.28 I | I. 86 | 8.447 | 2.36 | 12.073 |
| . 37 | 0.749 | . 87 | 2.702 | 1. 37 | $5 \cdot 340$ | I. 87 | 8.515 | 2.37 | 12.150 |
| . 38 | 0.780 | . 88 | 2.749 | I. 38 | $5 \cdot 398$ | I. 88 | 8. 584 | 2.38 | 12.227 |
| . 39 | 0.811 | . 89 | 2.796 | I. 39 | $5 \cdot 457$ | I. 89 | 8.652 | 2.39 | 12.304 |
| . 40 | 0.842 | . 90 | 2.843 | I. 40 | 5.516 | I. 90 | 8.721 | 2.40 | 12.381 |
| -4I | 0.874 | .91 | 2.891 | I.4I | 5.575 | 1.91 | 8.790 | 2.41 | 12.459 |
| . 42 | 0.906 | . 92 | 2.939 | I. 42 | 5.635 | 1.92 | 8.859 | 2.42 | 12.536 |
| . 43 | 0.939 | . 93 | 2.987 | I. 43 | 5.694 | I. 93 | 8.929 | 2.43 | 12.614 |
| . 44 | 0.972 | . 94 | 3.035 | I. 44 | 5.754 | I. 94 | 8.998 | 2.44 | 12.692 |
| . 45 | 1.005 | . 95 | 3.083 | I. 45 | 5.814 | 1.95 | 9.068 | 2.45 | 12.770 |
| . 46 | 1.039 | . 96 | 3.132 | I. 46 | 5.875 | 1.96 | 9.138 | 2.46 | 12.848 |
| . 47 | I. 073 | . 97 | 3.18I | I. 47 | 5.935 | I. 97 | 9.208 | 2.47 | 12.927 |
| . 48 | I. 107 | . 98 | 3.231 | I. 48 | 5.996 | I. 98 | 9.278 | 2.48 | 13.005 |
| . 49 | I. 142 | . 99 | 3.280 | I. 49 | 6.057 | 1.99 | 9.348 | 2.49 | 13.084 |
| $\cdot 50$ | I. 177 | 1.00 | 3.330 | I. 50 | 6.118 | 2.00 | 9.419 | 2.50 | I3. 163 |

Table for Estimating Discharge of Water through a Right-angled
Triangular Notch in Thin Sheet Iron.
$Q=$ Discharge in cubic feet per minute.
$n=$ Head in inches measured from bottom of notch to surface of still water above weir.
$Q=.306 \sqrt{n^{5}}$ (Thomson's formula).
The Table is calculated for heads from I to 15 inches, increasing by decimal parts of an inch. No deduction has to be made for end contraction.

| $n$ | $Q$ | $n$ | $Q$ | $n$ | $Q$ | $n$ | $Q$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | . 306 | 4.6 | 13.886 | 8.2 | 58.935 | I 1.8 | 146.329 |
| I. I | . 388 | $4 \cdot 7$ | 14.654 | 8.3 | 60.701 | 11.9 | 148.838 |
| 1.2 | . 480 | 4.8 | I 5.446 | 8.4 | 62.577 | 12 | 151.032 |
| 1.3 | . 589 | 4.9 | 16.263 | 8.5 | 64.574 | I2. I | I55.813 |
| 1.4 | . 709 | 5 | 17.105 | 8.6 | 66.371 | 12.2 | 159.058 |
| 1.5 | . 843 | 5.1 | 17.974 | 8.7 | 68.329 | 12.3 | 163.333 |
| 1.6 | . 990 | 5.2 | 18.867 | 8.8 | 70.288 | 12.4 | 165.168 |
| 1.7 | I. I 53 | $5 \cdot 3$ | 19.789 | 8.9 | 72.338 | 12.5 | 169.034 |
| 1.8 | 1.330 | $5 \cdot 4$ | 20.734 | 9 | 74.358 | 12.6 | 172.431 |
| 1.9 | 1.523 | 5.5 | 21.707 | 9.1 | 77.662 | 12.7 | 175.858 |
| 2 | 1.73 I | 5.6 | 22.708 | 9.2 | 78.550 | 12.8 | 179.346 |
| 2.1 | 1.954 | 5.7 | 23.736 | 9.3 | 80.722 | 12.9 | 182.865 |
| 2.2 | 2. 197 | 5.8 | 24.792 | 9.4 | 82.895 | 13 | 186.463 |
| 2.3 | 2.454 | $5 \cdot 9$ | 25.875 | 9.5 | 85.129 | 13.1 | 190.056 |
| 2.4 | 2.730 | 6 | 26.983 | 9.6 | 87.393 | 13.2 | 193.698 |
| 2.5 | 3.023 | 6.1 | 28. 12 I | 9.7 | 89.688 | 13.3 | 197.400 |
| 2.6 | 3.338 | 6.2 | 29.290 | 9.8 | 92.014 | 13.4 | 201. 103 |
| 2.7 | 3.665 | 6.3 | 30.483 | 9.9 | 94.370 | 13.5 | 204.897 |
| 2.8 | 4.014 | 6.4 | 31.701 | 10 | 96.787 | 13.6 | 208.692 |
| 2.9 | 4.384 | 6.5 | 32.956 | IO. I | 99.174 | 13.7 | 212.578 |
| 3 | 4.767 | 6.6 | 34.24 I | 10.2 | 101.653 | 13.8 | 216.464 |
| 3.1 | 5.177 | 6.7 | 35.557 | 10.3 | 104.162 | 13.9 | 220.411 |
| 3.2 | 5.605 | 6.8 | 36.903 | 10.4 | 106.702 | 14 | 224.389 |
| $3 \cdot 3$ | 6.055 | 6.9 | 38.280 | 10.5 | 109.303 | 14. I | 228.429 |
| $3 \cdot 4$ | 6.523 | 7 | 39.688 | 10.6 | 111.934 | 14.2 | 232.498 |
| $3 \cdot 5$ | 7.013 | 7.1 | 41.095 | 10.7 | I 14.570 | 14.3 | 236.599 |
| 3.6 | $7 \cdot 525$ | 7.2 | 42.564 | 10.8 | 117.289 | 14.4 | 240.760 |
| 3.7 | 8.069 | $7 \cdot 3$ | 44.064 | 10.9 | 120.013 | 14.5 | 244.983 |
| 3.8 | 8.673 | $7 \cdot 4$ | 45.594 | 11 | 122.797 | 14.6 | 249.206 |
| 3.9 | 9. 192 | 7.5 | 47. I 54 | II. I | 125.582 | 14.7 | 253.521 |
| 4 | 9.792 | 7.6 | 48.745 | 11.2 | 128.458 | 14.8 | 257.835 |
| 4.1 | 10.400 | 7.7 | 50.337 | 11.3 | 131.352 | 14.9 | 262.211 |
| 4.2 | 11.061 | 7.8 | 51.989 | 11.4 | 134.272 | 15 | 266.709 |
| $4 \cdot 3$ | 11.735 | 7.9 | 53.672 | 11.5 | 137.332 |  |  |
| $4 \cdot 4$ | 12.426 | 8 | 55.386 | 11.6 | 138.220 |  |  |
| $4 \cdot 5$ | 13.151 | 8. I | 57.160 | 11.7 | 143.269 |  |  |

SECTION III. STORAGE OF WATER BY SMALL DAMS FOR MINING AND IRRIGATION PURPOSES.

## Dimensions for Small Earthen Dams.

Mr. A. M. Strange* recommends the following dimensions for small earthen dams:

| Maximum height of Dam above Ground Level. | Height of top of Dam above <br> High Flood Level. | $\xrightarrow[\text { Width. }]{\text { Top }}$ | Upstream (or Reservoir side) Slope. | Downstream Slope. |
| :---: | :---: | :---: | :---: | :---: |
|  | Feet. | Feet. | Ratio of Horizontal Width to Vertical Height. |  |
| 1. Under 8 feet, - | 3 | 6 | $\mathrm{I}_{\frac{1}{2}}$ to I | I to I |
| 2. From 8 to 15 feet, | 4 | 8 | 2 to I | I $\frac{1}{2}$ to I |

The above dimensions only apply when the soil is of a suitable nature and the wall is well and compactly made on a site from which all vegetation has first been removed. A clay core is usually effective in preventing leakage. The by-wash or waste weir channel and the upstream face of the wall should be "pitched" with stone. The high flood level is the level of the maximum discharge over the waste weir in time of flood.

## Flood Discharge Allowances for Waste Weir Channels.

The following table gives what should prove quite safe allowances for the widths of waste weirs required for ordinary small catchment or drainage areas.

Table of Waste Weir Channels.

| $\begin{gathered} \begin{array}{c} \text { For } \\ \text { catchment } \\ \text { up to } \end{array} \\ 1 \\ 1 \end{gathered}$ | Discharge per 250 acres of catchment <br> 2 | Width of Waste Weir Channels required per 250 acres of catchment. |  |
| :---: | :---: | :---: | :---: |
|  |  | I ft. deep. $3$ | $\begin{gathered} 2 \mathrm{ft.} \text { deep. } \\ 4 \end{gathered}$ |
| Acres. | Cubic feet per second. | Feet. | Feet. |
| 640 | $75$ | 31.5 | $10.3$ |
| 1280 | 70 | $29.5$ | $9.6$ |
| 1920 | $66$ | 27.7 | 9.06 |
| 2560 | 62 | 26.0 | 8.5 |
| 3200 | 59 | 24.8 | 8.0 |

Note. In regard to the catchment area, take the figure entered in column I, which is the nearest greater than the one under consideration, and use the corresponding figures in columns 2-4. For * Bulletin No. I, Irrigation Dept., Transvaal, Pretoria, 1905.
catchments above 3200 acres ( 5 square miles), the discharges (vide column 2 ) should be reduced gradually.

Example. A catchment area of 1000 acres may be expected to produce a high-flood discharge of $(4 \times 70=) 280$ cubic feet per sec., which would require a waste weir channel flowing I foot deep to be ( $4 \times 29.5=)_{\mathrm{I}} 18$ feet wide; or a channel flowing 2 feet deep to be ( $4 \times 9.6=$ ) 38.4 feet wide.

The tables on pp. 76,77 will be found of use in calculating the amount of earthwork contained in the wall. The height of the wall should be taken at each change of slope in the contour of the site, also the distance between each height measurement. Then half the sum of the areas of two adjoining cross-sections multiplied by the distance in feet between them gives the contents in cubic feet of that portion of the wall.

## The Relation of Rainfall to Irrigation.

I inch rainfall over I acre $=3630$ cubic feet of water.

| 2 | " | ., | " | $=7260$ | " | " | , |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2.5 | " | " | " | $=9075$ | " | " | " |
| 3 | " | " | " | = 10890 | " | " |  |
| 4 | " | " | " | $=14520$ | " | " |  |
| 7.13 |  |  | " | $=25882$ |  |  |  |

Therefore, water flowing at the rate of 1 cubic foot per second for 30 days ( 1 month) is equivalent to
a rainfall of r inch per month on 713 acres.

| $"$, | $"$, | 2 | $"$ | $"$, | $"$ | 356 | $"$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $"$, | $"$ | 2.5 | $"$ | $"$ | $"$ | 285 | $"$ |
| $"$ | $"$, | 3 | $"$ | $"$ | $"$ | 237 | $"$ |
| $"$, | $"$ | 4 | $"$ | $"$ | $"$ | 178 | $"$ |
| $"$ | $"$, | 7.13 | $"$ | $"$ | $"$ | 100 | $"$ |

It will be seen from the above table that a rainfall of $2 \frac{1}{2}$ inches per month corresponds to the flow of I cubic foot per second (r cusec) over 285 acres.

This is termed an 'irrigating duty' of 285 acres per cusec, which means that one cubic foot of water per second has to irrigate 285 acres.

The irrigating duty of water varies according to the climate, the nature of the soil, the class of crop and the method of cultivation.

An irrigating duty of
285 acres per cusec $=9075$ cub. ft. per acre per month.
250
,, $=10345$
200 ", $\quad, 12931$
$150, \quad, \quad=17242$
100 , , $=25863$,
Tables for Calculation of Cubic Contents of Earthen Dam Embankments.*

| $\begin{aligned} & \text { Height } \\ & \text { in Feet. } \end{aligned}$ | Cross Sectional Area in Square Feet. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| o | 0.00 | 0.61 | 1.25 | I.91 | 2.60 | 3.31 | 4.05 | 4.81 | 5.60 | 6.41 |
| 1 | 7.25 | 8.11 | 9.00 | 9.91 | 10.85 | 11.81 | 12.80 | 13.81 | 14.85 | 15.91 |
| 2 | 17.00 | 18.11 | 19.25 | 20.41 | 21.60 | 22.81 | 24.05 | 25.31 | 26.60 | 27.91 |
| 3 | 29.25 | 30.61 | 32.00 | 33.41 | 34.85 | 36.31 | 37.80 | 39.31 | 40.85 | 42.41 |
| 4 | 44.00 | 45.61 | 47.25 | 48.91 | 50.60 | 52.31 | 54.05 | 55.81 | 57.60 | 59.41 |
| 5 | 61.25 | 63.11 | 65.00 | 66.91 | 68.85 | 70.81 | 72.80 | 74.81 | 76.85 | 78.91 |
| 6 | 81.00 | 83.11 | 85.25 | 87.41 | 89.60 | 9 I .8 I | 94.05 | 96.31 | 98.60 | 100.91 |
| 7 | 103.25 | 105.61 | 108.00 | 110.41 | 112.85 | 115.31 | 117.80 | 120.31 | 122.85 | 125.41 |
| 8 | 128.00 | 130.61 | 133.25 | 135.91 | 138.60 | 141.31 | 144.05 | 146.81 | 149.60 | 152.41 |
| Decimals of a Foot. | 0.0 | $0 \cdot 1$ | 0.2 | $0 \cdot 3$ | $0 \cdot 4$ | 0.5 | 0.6 | 0.7 | 0.8 | $0 \cdot 9$ |

* Bulletin No. 1, Irrigation Dept., Transvaal, Pretoria, 1905.
Table 2.

| Height in Feet. | Cross Sectional Area in Square Feet. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0.00 | 0.82 | 1.67 | 2.56 | 3.48 | 4.44 | 5.43 | 6.46 | $7 \cdot 52$ | 8.62 |
| I | 9.75 | 10.92 | * 12.12 | I 3.36 | 14.63 | I 5.94 | 17.28 | $18.66$ | 20.07 | $21.52$ |
| 2 | 23.00 | 24.52 | 26.07 | 27.66 | 29.28 | 30.94 | 32.63 | $34 \cdot 36$ | 36. I2 | 37.92 |
| 3 | 39.75 | 41.62 | $43 \cdot 52$ | 45.46 | 47.43 | 49.44 | 5 I .48 | $53 \cdot 56$ | 55.67 | 57.82 |
| 4 | 60.00 | 62.22 | 64.47 | 66.76 | 69.08 | 7 I .44 | 73.83 | 76.26 | 78.72 | 81.22 |
| 5 | 83.75 | 86.32 | 88.92 | 91.56 | 94.23 | 96.94 | 99.68 | 102.46 | 105.27 | 108.12 |
| 6 | III.OO | 113.92 | 116.87 | I 19.86 | 122.88 | 125.94 | 129.03 | 132.16 | 135.32 | 138.52 |
| 7 | 141.75 | 145.02 | 148.32 | 151.66 | 155.03 | 158.44 | 161.88 | 165.36 | 168.87 | 172.42 |
| 8 | 176.00 | 179.62 | 183.27 | I86.96 | 190.68 | 194.44 | 198.23 | 202.06 | 205. 92 | 209.82 |
| 9 | 213.75 | 217.72 | 221.72 | 225.76 | 229.83 | 233.94 | 238.08 | 242.26 | 246.47 | 250.72 |
| 10 | 255.00 | 259.32 | 263.67 | 268.06 | 272.48 | 276.94 | 281.43 | 285.96 | 290. 52 | 295.12 |
| 11 | 299.75 | 304.42 | 309. 12 | 313.86 | 318.63 | 323.44 | 328.28 | 333.16 | 338.07 | 343.02 |
| 12 | 348.00 | 353.02 | 358.07 | 363.16 | 368.28 | 373.44 | 378.63 | 383.86 | 389.12 | 394.42 |
| 13 | 399.75 | 405.12 | 410.52 | 415.96 | 421.43 | 426.94 | 432.48 | 438.06 | 443.67 | $449 \cdot 32$ |
| 14 | 455.00 | 460.72 | 466.47 | 472.26 | 478.08 | $483.94$ | 489.93 550.68 | 495.76 556.96 | 501.72 563.27 | $\begin{aligned} & 507.72 \\ & 560.62 \end{aligned}$ |
| 15 | 513.75 | 519.82 | 525.92 | 532.06 | 538.23 | 544.44 | 550.68 | 556.96 | 563.27 | 569.62 |
| Decimals of a Foot. | 0.0 | $0 \cdot 1$ | $0 \cdot 2$ | $0 \cdot 3$ | 0.4 | 0.5 | 0.6 | $0 \cdot 7$ | 0.8 | 0.9 |

A general rule for dimensions of dams over 16 feet high is :


## SECTION IV. FLOW OF WATER IN PIPES.

General Laws.-I. When the diameter and length are constant, the discharge varies directly as the square root of the head. Conversely, the head is directly as the square of the discharge.
2. When the head and length are constant, the discharge is directly as the 2.5 th power of the diameter. Conversely, the diameter will vary as the 2.5 th root of the discharge.
3. When the discharge and length are constant, the head will be inversely as the 5 th power of the diameter. Conversely, the diameter will be inversely as the 5th root of the head.
4. When the head and diameter are constant, the discharge will be inversely as the square root of the length. Conversely, the length varies as the square of the discharge.
5. When the discharge and diameter are constant, the head is directly and simply as the length.

The hydraulic mean gradient corresponds to a straight line drawn between the points of intake and delivery of a pipe. No loss of effect will arise from the pipe following the contour of the ground as long as it keeps below the hydraulic mean gradient. If the pipe be carried over a hill which is above the hydraulic mean gradient but below the level of the intake, the first section, having a low head, must be of a greater diameter than the subsequent section, which has a greater head.

The sine of slope of the hydraulic mean gradient is the head divided by the length of the pipe.

The hydraulic mean depth, or mean radius, is the crosssectional area of the water divided by the length of the wetted perimeter of the pipe or channel ; in a circular pipe running full it is equal to one-fourth the diameter ( $\left(\frac{d}{4}\right)$.

Except under considerable pressure, flowing water does not entirely fill the pipe, and yet if it be more than three-quarters full, the discharge is but slightly less than if it were full. This is due to the fact that the full circle does not give the maximum discharging velocity, which is attained when the pipe is filled to the level of the chord of an arc of $78 \frac{1}{2}^{\circ}$. This gives an increase over the full circle of $9 \frac{1}{2}$ per cent. in velocity, and
over $2 \frac{1}{2}$ per cent. in discharge. The mean radius can therefore be safely taken as equal to $\frac{d}{4}$ when the pipe is more than three-quarters full.

Discharge in cubic feet per second $=$ cross-sectional area of water in square feet $\times$ mean velocity in feet per second.

Cross-Sectional Areas and Capacities of Cylindrical Pipes of Various Diameters.
$D=$ the diameter of the pipe in inches.
$A=$ the cross-sectional area of the pipe in square feet; or the number of cubic feet in a length of 1 foot.

| D | $A$ | D | A | D | A |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{1}{2}$ | . 0014 | 10, $\frac{1}{2}$ | . 6013 | 2012 | 2.292 |
| 1 | . 0055 | 11 | . 6600 | 21 | 2.405 |
| $1 \frac{1}{2}$ | . 0123 | $11 \frac{1}{2}$ | . 7213 | $21 \frac{1}{2}$ | 2.52 I |
| 2 | . 0218 | 12 | .7854 | 22 | 2.640 |
| $2 \frac{1}{2}$ | . 0341 | 123 ${ }^{\frac{1}{2}}$ | . 8522 | $22 \frac{1}{2}$ | 2.761 |
| 3 | .0491 | 13 | . 9218 | 23 | 2.885 |
| $3 \frac{1}{2}$ | . 0668 | $13 \frac{1}{2}$ | . 9940 | $23 \frac{1}{2}$ | 3.012 |
| 4 | . 0873 | 14 | 1. 069 | 24 | 3.142 |
| 42 | . 1104 | 14 ${ }^{\frac{1}{2}}$ | 1. 147 | 25 | 3.409 |
| 5 | . 1363 | 15 | 1.227 | 26 | 3.687 |
| $5 \frac{1}{2}$ | . 1650 | 159 | 1.310 | 27 | 3.976 |
| 6 | . 1964 | 16 | I. 396 | 28 | 4.276 |
| $6 \frac{1}{2}$ | . 2304 | $16 \frac{1}{2}$ | I. 485 | 29 | 4.587 |
| 7 | . 2673 | 17 | 1. 576 | 30 | 4.909 |
| 73 | . 3068 | $17 \frac{1}{2}$ | 1. 670 | 31 | 5.24 I |
| 8 | .3491 | 18 | 1.767 | 32 | 5.585 |
| $8 \frac{1}{2}$ | .394I | $18 \frac{1}{2}$ | 1. 867 | 33 | 5.940 |
| 9 | . 4418 | 19 | 1. 969 | 34 | 6.305 |
| $9{ }^{\frac{1}{2}}$ | . 4922 | $19 \frac{1}{2}$ | 2.074 | 35 | 6.681 |
| 10 | . 5454 | 20 | 2. 182 | 36 | 7.069 |

Velocity.-Let $v=$ the mean velocity in feet per second.
$r=$ the hydraulic mean depth.
$s=$ the sine of slope.
Then $v=C r^{\frac{2}{3}} s^{\frac{1}{2}}$.
Or $z^{\prime}=$ the cube root of the square of $r \times$ the square root of $s \times$ the value of $C$ in the table. $C$ is a coefficient which varies according to the smoothness of the interior surface of the pipe or conduit ; but which is not appreciably affected by differences in slope or diameter.

Values of $C$.
Asphalted wrought-iron pipe $=170$. Plain " ", $\quad=160$.
Cast-iron pipe, new, $\quad=130$.
" ", in service, $=104$.
Lap-riveted pipe, $\quad=115$.
Brick conduits, $\quad=110$.

## Loss of Head in Friction

(1) is proportional to the length of the pipe,
(2) is increased by roughness of the interior surface of the pipe,
(3) decreases as the diameter of the pipe is increased,
(4) increases nearly as the square of the velocity,
(5) is independent of the pressure of the water.

These five laws may be expressed by the formula:

$$
h^{\prime}=f \frac{l}{d} \frac{v^{2}}{2 g}
$$

where $h^{\prime}=$ loss of head in friction in feet
$l=$ length of pipe in feet.
$d=$ diameter of pipe in feet.
$v=$ mean velocity in feet per second.
$g=$ acceleration due to gravity $=32.19$ feet per second.
$f=\mathrm{a}$ variable constant (see table).
$\frac{v^{2}}{2 g}=$ velocity head due to mean velocity of flow.
Values of $f$. (Mansfield Merriman.*)

| Diameter of Pipe in feet. | Velocity in feet per second. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | I | 2 | 3 | 4 | 6 | 10 | 15 |
| . 05 | . 047 | .04I | . 037 | . 034 | . 031 | . 029 | . 028 |
| . 1 | . 038 | .032 | . 030 | . 028 | . 026 | . 024 | . 023 |
| . 25 | . 032 | . 028 | . 026 | . 025 | . 024 | . 022 | .02I |
| . 5 | . 028 | . 026 | . 025 | . 023 | . 022 | . 020 | . 019 |
| . 75 | . 026 | . 025 | . 024 | . 022 | . 021 | . 019 | . 018 |
| I. 0 | . 025 | . 024 | . 023 | . 022 | . 020 | . 018 | . 017 |
| 1. 25 | . 024 | . 023 | . 022 | .02I | .OI9 | . 017 | . 016 |
| I. 5 | . 023 | . 022 | . 02 I | . 020 | . 018 | . 016 | . 015 |
| 1. 75 | . 022 | . 021 | . 020 | . 018 | . 017 | . 015 | . 014 |
| 2.0 | . 021 | . 020 | . 019 | . 017 | . 016 | . 014 | . 013 |

[^31]
## Loss of Head in Curvature.

Let $h^{\prime \prime}=$ loss of head in curvature in feet.
$R=$ radius of curve in feet.
$f_{1}=$ a variable coefficient.
Then $h^{\prime \prime}=f_{1} \frac{l}{d} \frac{v^{2}}{2 g}$
Values of $f_{1}$.

| $\frac{R}{d}$ | 20 | 10 | 5 | 3 | 2 | 1.5 | 1.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f_{1}$ | .004 | .008 | .016 | .030 | .047 | .072 | .184 |

In laying down a permanent pipe-line, allowance should be made for incrustation, which reduces the effective diameter of a pipe by from $\frac{1}{2}$ to $\mathrm{I}_{2}$ inches. A small reduction in the size of a pipe makes a large reduction in the discharge. $\frac{1}{10}$ th increase in the diameter gives an increase of about $25 \%$, and $\frac{1}{6}$ th about $50 \%$ in the discharge.

## PART IV. DATA RELATING TO AIR AND STEAM.

SECTION I. AIR.
The coefficient of expansion of air at constant pressure per I degree Centigrade $=\frac{1}{2} \frac{1}{7}$ or .00366957 (Jolly).

The standard height of a mercury barometer is 29.922 inches or 760 millimetres.

The standard atmospheric pressure at sea-level and standard barometric pressure

$$
\begin{aligned}
& =14.706 \mathrm{lbs} . \text { per square inch }=1 \text { atmosphere } \\
& =1033.3 \text { grammes per square centimetre. }
\end{aligned}
$$

The average atmospheric pressure at $\frac{1}{4}$ mile above sea-level $=14.02 \mathrm{lbs}$. per sq. in.

| $"$, | $"$ | at $\frac{1}{2}$ mile above sea-level $=13.33$ | $"$ | $"$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $"$, | $"$ | $\frac{3}{4}$ | $"$ | , | $"$ | $=12.66$ | $"$ |
| $"$ | $"$ | 1 | $"$ | $"$ | $"$ | $=12.02$ | $"$ |
| $"$, | $"$ | $1 \frac{1}{4}$ | $"$ | $"$ | $"$ | $=11.42$ | $"$ |
| $"$ | $"$ | $1 \frac{1}{2}$ | $"$ | $"$ | $"$ | $=1088$ | $"$ |
| $"$, | $"$ | 2 | $"$ | $"$ | $"$ | $=9.80$ | $"$ |
| $"$ | $"$ |  |  |  |  |  |  |

The pressure of one atmosphere (or 14.706 lbs. to the square inch $)=$ that of a column of water at $62^{\circ} \mathrm{F} .34$ feet in height. This is therefore the maximum theoretical lift of a pump at sea-level.

One lb. of dry air at $0^{\circ} \mathrm{C}$. $\left(32^{\circ} \mathrm{F}\right.$.) has a volume of 12.39 cub . ft.

$$
" \quad \# \quad, \quad 15^{\circ} \mathrm{C} .\left(60^{\circ} \mathrm{F} .\right)
$$

One cubic foot of dry air at $0^{\circ} \mathrm{C}$. $\left(32^{\circ} \mathrm{F}\right.$. $)$ weighs .0807 lb .

$$
\text { " } \quad, \quad, \quad " \quad 15^{\circ} \mathrm{C} .\left(60^{\circ} \mathrm{F} .\right) \quad, \quad .0765,
$$

One gramme of dry air at $0^{\circ} \mathrm{C}$. has a volume of $773.3 \mathrm{~cm} .^{3}$
One cubic centimetre of dry air at $0^{\circ} \mathrm{C}$. weighs .001293 gramme.

## Pressure of Columns of Mercury and Water.*

Metric and British measures. Correct at $\circ^{\circ} \mathrm{C}$. for mercury and $4^{\circ} \mathrm{C}$. for water.

| METRIC MEASURE. |  |  | BRITISH MEASURE. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Cms. of Mercury. | Pressure in grammes per sq. cm. | Pressure in pounds per sq. inch. | Inches of Mercury. | Pressure in grammes per sq. cm. | Pressure in pounds per sq. inch. |
| 1 | 13.5956 | 0.193376 | 1 | 34.533 | 0.491174 |
| 2 | 27.1912 | 0.386752 | 2 | 69.066 | 0.982348 |
| 3 | 40.7868 | 0.580128 | 3 | 103.598 | 1. 473522 |
| 4 | 54.3824 | 0.773504 | 4 | I 38.131 | 1.964696 |
| 5 | 67.9780 | 0.966880 | 5 | 172.664 | 2.455870 |
| 6 | 81. 5736 | I. 160256 | 6 | 207.197 | 2.947044 |
| 7 | 95.1692 | 1. 353632 | 7 | 241.730 | 3.438218 |
| 8 | 108.7648 | 1.547008 | 8 | 276.262 | 3.929392 |
| 9 | 122.3604 | 1.740384 | 9 | 310.795 | 4.420566 |
| 10 | I 35.9560 | 1.933760 | 10 | 345.328 | 4.911740 |
| Cms. of Water. | in grammes sq. cm. | Pressure in pounds per sq. inch. | Inches of Water. | $\begin{array}{\|c\|} \text { Pressure } \\ \text { in grammes per } \\ \text { sq. } \mathrm{cm} . \end{array}$ | Pressure in pounds per sq. inch. |
| I | I | 0.0142234 | 1 | 2.54 | 0.036227 |
| 2 | 2 | 0.0284468 | 2 | 5.08 | 0.072255 |
| 3 | 3 | 0.0426702 | 3 | 7.62 | 0.108382 |
| 4 | 4 | 0.0568936 | $4 \times$ | 10.16 | 0.144510 |
| 5 | 5 | 0.0711170 | 5 | 12.70 | 0.180637 |
| 6 | 6 | 0.0853404 | 6 | 15.24 | 0.216764 |
| 7 | 7 | 0.0995658 | 7 | 17.78 | 0.252892 |
| 8 | 8 | 0.1137872 | 8 | 20.32 | 0.289019 |
| 9 | 9 | 0.1280106 | 9 | 22.86 | 0.325147 |
| 10 | 10 | 0.1422340 | 10 | 25.40 | 0.361274 |

## SECTION II. STEAM.

The following table (from the Smithsonian Physical Tables) summarises the chief properties of steam for pressures ranging from 1 to 219 lbs . per square inch:

[^32]PROPERTIES OF STEAM．＊

|  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 144 | 0.068 | 102.0 | 334.23 | 0.0030 | 70.1 | 980.6 | 62.34 | 1043. | 1113．0 |
| 2 | 288 | ． 136 | 126.3 | 173.23 | ． 0058 | 94.4 | 961.4 | 64.62 | 1026. | 1120.4 |
| 3 | 432 | ． 204 | 141.6 | 117.98 | ． 0085 | 109.9 | 949.2 | 66.58 | IOII． | 1127.0 |
| 4 | 576 | ． 272 | 153.1 | 89.80 | ． OHI | 121.4 | 940.2 | 67.06 | $100 \%$ ． | I 128.6 |
| 5 | 720 | ． 340 | 162.3 | 72.50 | ． 0137 | 130.7 | 932.8 | 67.89 | 1001. | 1131.4 |
| 6 | 864 | 0.408 | 170.1 | 61．10 | 0.0163 | 138.6 | 926.7 | 68.58 | 995.2 | I 133.8 |
| 7 | 1008 | ． 476 | 176.9 | 53.00 | ． 0189 | 145.4 | 92 I .3 | 69.18 | 990.5 | II 35.9 |
| 8 | 1152 | ． 544 | 182．9 | 46.60 | ． 0214 | 15 I .5 | 916.5 | 69.71 | 986.2 | 1137.7 |
| 9 | 1296 | ． 612 | 188.3 | 4 I .82 | ． 0239 | 156.9 | 912.2 | 70.18 | 982.4 | 1139.4 |
| 10 | 1440 | ． 680 | 193.2 | 37.80 | ． 0264 | 161.9 | 908.3 | 70.61 | 979.0 | 1140.9 |
| 11 | 1584 | 0.748 | 197.8 | 34.61 | 0.0289 | 166.5 | 904.8 | 70.99 | 975.8 | 1142.3 |
| 12 | 1728 | ． 816 | 202.0 | 31.90 | ． 0314 | 170.7 | 901.5 | 71.34 | 972.8 | 1143.5 |
| 13 | 1872 | ． 884 | 205.9 | 29.58 | ．0338 | 174.7 | 898.4 | 71.68 | 970.0 | 1144.7 |
| 14 | 2016 | ． 952 | 209.5 | 27.59 | ． 0362 | 178.4 | 895.4 | 72.00 | 967.4 | 1145.9 |
| 15 | 2160 | 1.020 | 213.0 | 25.87 | ． 0387 | 181.9 | 892.7 | 72.29 | 965.0 | I 146.9 |
| 16 | 2304 | 1.088 | 216.3 | 24.33 | 0.0411 | 185.2 | 890.1 | 72.57 | 962.7 | 1147.9 |
| 17 | 2448 | ． 156 | 219.4 | 22.98 | ． 0435 | 188.4 | 887.6 | 72.82 | 960.4 | 1148.9 |
| 18 | 2592 | ． 224 | 222.4 | 21.78 | ． 0459 | 191.4 | 885.3 | 73.07 | 958.3 | 1149.8 |
| 19 | 2736 | ． 292 | 225.2 | 20.70 | ． 0483 | 194.3 | 883.1 | 73.30 | 956.3 | 1150.6 |
| 20 | 2880 | $\cdot 360$ | 227.9 | 19.72 | ． 0507 | 197.0 | 880.9 | 73.53 | 954.4 | II 51．4 |
| 21 | 3024 | I． 429 | 230.5 | 18.84 | 0.0531 | 199.7 | 878.8 | 73.74 | 952.6 | II52．2 |
| 22 | 3168 | ． 497 | 233.0 | 18.03 | ． 0554 | 202.2 | 876.8 | 73.94 | 950.8 | 1153.0 |
| 23 | 3312 | ． 565 | 235.4 | 17.30 | ． 0578 | 204.7 | 874.9 | 74．13 | 949．I | 1153.7 |
| 24 | 3456 | ． 633 | 237.7 | 16.62 | ． 0602 | 207.0 | 873.1 | 74.32 | 947.4 | II 54.4 |
| 25 | 3600 | ． 701 | 240.0 | 15.99 | ． 0625 | 209.3 | 871.3 | 74.51 | 945.8 | 1155.1 |
| 26 |  | 1． 769 | 242.2 | 15.42 | 0.0649 | 211.5 | 869.6 | 74.69 | 944.3 | 1155.8 |
| 27 | 3888 | ． 837 | 244.3 | 14.88 | ． 0672 | 213.7 | 867.9 | 74.85 | 942.8 | II 56.4 |
| 28 | 4032 | ． 905 | 246.3 | 14.38 | ． 0695 | 215.7 | 866.3 | 75.01 | 941.3 | 1157.1 |
| 29 | 4176 | ． 973 | 248.3 | 13.91 | ．0619 | 217.8 | 864.7 | 75.17 | 939.9 | 1157.7 |
| 30 | 4320 | 2.041 | 250.2 | 13.48 | ． 0742 | 219.7 | 863.2 | 75.33 | 938.5 | 1158.3 |
| 31 | 4464 | 2． 109 | 252.1 | 13.07 |  | 221.6 |  |  |  | II 58.8 |
| 32 | 4608 | ． 177 | 253.9 | 12.68 | ． 0788 | 223.5 | 860.3 | 75.61 | 935.9 | II59．4 |
| 33 | 4752 | ． 245 | 255.7 | 12.32 | ．0811 | 225.3 | 858.9 | 75.76 | 934.6 | I 159.9 |
| 34 | 4896 | ． 313 | 257.5 | 11.98 | ． 0835 | 227.1 | 857.5 | 75.89 | 933.4 | If60．5 |
| 35 | 5040 | ． 381 | 259.2 | 11.66 | ． 0858 | 228.8 | 856.1 | 76.02 | 932.1 | 1161．0 |
| 36 | 5184 | 2.449 | 260.8 | I 1.36 | 0．088I | 230.5 | 854.8 | 76.16 | 931.0 | 1161．5 |
| 37 | 5328 | ． 517 | 262.5 | 11.07 | ． 0903 | 232.2 | 853.5 | 76.28 | 929.8 | 1162.0 |
| 38 | 5472 | ． 585 | 264.0 | 10.79 | ． 0926 | 233.8 | 852.3 | 76.40 | 928.7 | 1162.5 |
| 39 | 5616 | ． 653 | 265.6 | 10． 53 | ． 0949 | 235.4 | 85 I． 0 | 76.52 | 927.6 | 1162.9 |
| 40 | 5760 | ． 722 | 267． 1 | 10.29 | ． 0972 | 236.9 | 849.8 | 76.63 | 926.5 | I 163.4 |
| 41 | 5904 | 2.789 | 268.6 | 10.05 | 0.0995 | 238.5 | 848.7 | 76.75 | 925.4 | 1163.9 |
| 42 | 6048 | ． 857 | 270.1 | 9.83 | ． 1018 | 239.9 | 847.5 | 76.86 | 924.4 | 1164.3 |
| 43 | 6192 | ． 925 | 271.5 | 9.61 | ． 1040 | 24 I .4 | 846.4 | 76.97 | 923.3 | 1164.7 |
| 44 | 6336 | ． 993 | 272.9 | 9.41 | ． 1063 | 242.9 | 845.2 | 77.07 | 922.3 | 1165.2 |
| 45 | 6480 | 3.061 | 274.3 | 9.21 | ． 1086 | 244.3 | 844．I | 77.18 | 921.3 | I165．6 |
| 46 | 6624 | 3．129 | 275.6 | 9.02 | 0． 1108 | 245.6 | 843． 1 | 77.29 | 920.4 | 1166.0 |
| 47 | 6768 | ． 197 | 277.0 | 8.84 | ． 1131 | 247.0 | 842.0 | 77.39 | 919.4 | 1166.4 |
| 48 | 6912 | ． 265 | 278.3 | 8.67 | ． 1153 | 248.3 | 841.0 | 77.49 | 918.5 | 1166.8 |
| 49 | 7056 | ． 333 | 279.6 | 8.50 | ． 1176 | 249.7 | 840.0 | 77.58 | 917.5 | 1167.2 |

[^33]|  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 7200 | 3.401 | 280.8 | 8.34 | 0． 1198 | 251.0 | 839.0 | 77.67 | 916.6 | 1167.6 |
| 51 | 7344 | ． 469 | 282.1 | 8.19 | ． 1221 | 252.2 | 838.0 | 77.76 | 915.7 | I 168.0 |
| 52 | 7488 | ． 537 | 283.3 | 8.04 | ． 1243 | 253.5 | 837.0 | 77.85 | 914.9 | 1168.3 |
| 53 | 7632 | ． 605 | 284.5 | 7.90 | ． 1266 | 254.7 | 836.0 | $7 \% .94$ | 914.0 | 1168.7 |
| 54 | 7776 | ． 673 | 285.7 | 7.76 | ． 1288 | 256.0 | 835.1 | 78.03 | 913.1 | 1169.1 |
| 55 | 7920 | 3.741 | 286.9 | 7.63 | 0．1310 | 257.1 | 834.2 | 78.12 | 912.3 | 1169.4 |
| 56 | 8064 | ． 801 | 288.1 | 7.50 | ． 1333 | 258.3 | 833.2 | 78.21 | 911.5 | 1169.8 |
| 57 | 8208 | ． 878 | 289.2 | 7.38 | ． 1355 | 259.5 | 832.3 | 78.29 | 910.6 | 1170.1 |
| 58 | 8352 | ． 946 | 290.3 | 7.26 | ． 1377 | 260.7 | 831.5 | 78.37 | 909.8 | 1170.5 |
| 59 | 8496 | 4.014 | 291.4 | 7.14 | ． 1400 | 261.8 | 830.6 | 78.45 | 909.0 | 1170.8 |
| 60 | 8640 | 4.082 | 292.5 | 7.03 | 0． 1422 | 262.9 | 829.7 | 78.53 | 908.2 | 1171.2 |
| 61 | 8784 | ． 150 | 293.6 | 6.92 | ． 1444 | 264.0 | 828.9 | 78.61 | 907.5 | 1171.5 |
| 62 | 8928 | ． 218 | 294.7 | 6.82 | ． 1466 | 265.1 | 828.0 | 78.68 | 906.7 | 1171.8 |
| 63 | 9072 | ． 286 | 295.7 | 6.72 | ． 1488 | 266.1 | 827.2 | 78.76 | 905.9 | 1172.1 |
| 64 | 9216 | ． 354 | 296.7 | 6.62 | ． 1511 | 267.2 | 826.4 | 78.83 | 905.2 | 1172.4 |
| 65 | 9360 | 4.422 | 297.8 | 6.52 | 0．1533 | 268.3 | 825.6 | 78.90 | 904.5 | 1172.8 |
| 66 | 9504 | ． 490 | 293.8 | 6.43 | ． 1555 | 269.3 | 824.8 | 78.97 | 903.7 | 1173.1 |
| 67 | 9648 | ． 558 | 299.8 | 6.34 | ． 1577 | 270.4 | 824.0 | 79.04 | 903．1 | 1173.4 |
| 68 | 9792 | ． 626 | 300.1 | 6.25 | ． 1599 | 271.4 | 823.2 | 79．11 | 902.3 | 1173.7 |
| 69 | 9936 | ． 694 | 301.8 | 6.17 | ．162I | 272.4 | 822.4 | 79.18 | 901.6 | 1174.0 |
| 70 | 10080 | 4.762 | 302.7 | 6.09 | 0． 1643 | 273.4 | 821.6 | 79.25 | 900.9 | 1174.3 |
| 71 | 10224 | ． 830 | 303.7 | 6.00 | ． 1665 | 274.3 | 820.9 | 79.32 | 900.2 | 1174.6 |
| 72 | 10368 | ． 898 | 304.6 | 5.93 | ． 1687 | 275.3 | 820.1 | 79.39 | 899.5 | 1174.9 |
| 73 | 10512 | ． 966 | 305.5 | 5.85 | ． 1709 | 276.3 | 819.4 | 79.46 | 898.8 | 1175． 1 |
| 74 | 10656 | 5.034 | 306.5 | 5.78 | ．1731 | 277.2 | 818.7 | 79.53 | 898.1 | 1175.4 |
| 75 | 10800 | 5．102 | 307.4 | 5.70 | 0． 1753 | 278.2 | 817.9 | 79.59 | 897.5 | 1175.7 |
| 76 | 10944 | ． 170 | 308.3 | 5.63 | ． 1775 | 279.1 | 817.2 | 79.65 | 896.9 | 1176.0 |
| 77 | 11088 | ． 238 | 309.2 | 5.57 | ． 1797 | 280.0 | 816.5 | 79．71 | 896.2 | 1176.2 |
| 78 | 11232 | ． 306 | 310.1 | 5.50 | ． 1818 | 280.9 | 815.8 | 79.77 | 895.6 | 1176.5 |
| 79 | 11376 | ． 374 | 310.9 | 5．43 | ． 1840 | 281.8 | 815．1 | 79.83 | 895.0 | 1176.8 |
| 80 | 11520 | $5 \cdot 442$ | 311.8 | $5 \cdot 37$ | 0． 1862 | 282.7 | 814. | 79.89 | 894.3 | 1177.0 |
| 81 | 11664 | ． 510 | 312.7 | 5.31 | ． 1884 | 283.6 | 813.8 | 79.95 | 893.7 | 1177.3 |
| 82 | 11808 | ． 578 | 313.5 | 525 | ． 1906 | 284.5 | 813.0 | 80.01 | 893.1 | 1177.6 |
| 83 | 11952 | ． 646 | 314.4 | 5．19 | ． 1928 | 285.3 | 812.4 | 80.07 | 892.5 | 1177.8 |
| 84 | 12096 | ． 714 | 315.2 | 5．13 | ． 1949 | 286.2 | 811．7 | 80.13 | 891.9 | 1178.0 |
| 85 | 12240 | 5.782 | 316.0 | 5.07 | 0．1971 | 287.0 | 8iI．I | 80.19 | 891.3 | 1178.3 |
| 86 | 12384 | ． 850 | 316.8 | 5.02 | ． 1993 | 287.9 | 810.4 | 80.25 | 890.7 | 1178.6 |
| 87 | 12528 | ． 918 | 317.6 | 4.96 | ． 2015 | 288.7 | 809.8 | 80.30 | 890.1 | 1178.9 |
| 88 | 12672 | ． 986 | 318.4 | 4.91 | ． 2036 | 289.5 | 809.2 | 80.35 | 889.5 | 1179.0 |
| 89 | 12816 | 6.054 | 319．2 | 4.86 | ． 2058 | 290.4 | 808.5 | 80.40 | 888.9 | 1179.3 |
| 90 | 12960 | 6.122 | 320.0 | 4.81 | 0.2080 | 291.2 | 807.9 | 80.45 | 888.4 | 1179.5 |
| 91 | 13104 | ． 190 | 320.8 | 4.76 | ． 2102 | 292.0 | 807.3 | 80.50 | 887.8 | 1179.8 |
| 92 | 13248 | ． 258 | 321.6 | 4.71 | ． 2123 | 292.8 | 806.7 | 80.56 | 887.2 | 1180.0 |
| 93 | 13392 | ． 327 | 322.4 | 4.66 | ． 2145 | 293.6 | 806．1 | 80.61 | 886.7 | 1180.3 |
| 94 | 13536 | －396 | 323.1 | 4.62 | ． 2166 | 294.3 | 805.5 | 80.66 | 886． 1 | 1180.5 |
| 95 | 13680 | 6.463 | 323.9 | 4.57 | 0.2188 | 295.1 | 804.9 | 80.71 | 885.6 | 1180.7 |
| 96 | 13824 | ． 53 I | 324.6 | 4.53 | ． 2209 | 295.9 | 804.3 | 80.76 | 885.0 | 1180.9 |
| 97 | 13968 | ． 599 | 325.4 | 4.48 | ．2231 | 296.7 | 803.7 | 80.81 | 884.5 | 1181.2 |
| 98 | 14112 | ． 667 | 326.1 | 4.44 | ． 2252 | 297.4 | 803.1 | 80.86 | 884.0 | 1181.4 |
| 99 | 14256 | ． 735 | 326.8 | 4.40 | ． 2274 | 298.2 | 802.5 | 80.91 | 883.4 | 1181． 6 |

DATA RELATING TO AIR AND STEAM［part iv．

|  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 14400 | 6.803 | 327.6 | 4.356 | 0.2295 | 298.9 | 802.0 | 80.95 | 882.9 | II81．8 |
| 101 | 14544 | ． 871 | 328.3 | ． 316 | ． 2317 | 299.7 | 801.4 | 81.00 | 882.4 | 1182.1 |
| 102 | 14688 | ． 939 | 329.0 | ． 276 | ． 2338 | 300.4 | 8008 | 81.05 | 881.9 | 1182.3 |
| 103 | 14832 | 7.007 | 329.7 | ． 237 | ． 2360 | 301.1 | 800.3 | 81.10 | 88 I .4 | 1182.5 |
| 104 | 14976 | ． 075 | 330.4 | ． 199 | ．2381 | 301：9 | 799.7 | 8 I .14 | 880.8 | I182．7 |
| 105 | 15120 | 7．143 | 331．I | 4．16I | 0.2403 | 302.6 | 799.2 | 8 I .18 | 880.3 | 1182.9 |
| 106 | 15264 | ． 211 | 331.8 | ． 125 | ． 2424 | 303.3 | 798.6 | 8 I .23 | 879.8 | II83． 1 |
| 107 | 15408 | ． 279 | 332.5 | ． 088 | ． 2446 | 304.0 | 798.1 | 81.27 | 879.3 | 1183.4 |
| 108 | 15552 | ． 347 | 333.2 | ． 053 | ． 2467 | 304.7 | 797.5 | 81.31 | 878.8 | 1183.6 |
| 109 | 15696 | ． 415 | 333.8 | ． 18 | ． 2489 | 305.4 | 797.0 | 81．36 | 878.3 | 1183.8 |
| 110 | 15840 | 7.483 | 334.5 | 3.984 | 0.2510 | 306． 1 | 796.5 | 81.41 | 877.9 | 1184.0 |
| 111 | 15984 | ． 551 | 335.2 | ． 950 | ． 2531 | 306.8 | 795.9 | 81.45 | 877.4 | 1184.2 |
| 112 | 16128 | ． 619 | 335.8 | ． 917 | ． 2553 | 307.5 | 795.4 | 8 I .50 | 876.9 | 1184.4 |
| 113 | 16272 | ． 687 | 336.5 | ． 885 | ． 2574 | 308.2 | 794.9 | 81.54 | 876.4 | 1184.6 |
| 114 | 16416 | ． 757 | 337.2 | ． 853 | ． 2596 | 308.8 | 794.4 | 81． 58 | 875.9 | 1184.8 |
| 115 | 16560 | 7.823 | 337.8 | 3.821 | 0.2617 | 309.5 | 793.8 | 81.62 | 875.5 | 1185.0 |
| 116 | 16704 | ． 891 | 338.5 | ． 790 | ． 2638 | 310.2 | 793.3 | 81.66 | 875.0 | 1185.2 |
| 117 | 16848 | ． 959 | 339． 1 | ． 760 | ． 2660 | 310.8 | 792.8 | 81.70 | 874.5 | 1185.4 |
| 118 | 16992 | 8.027 | 339.7 | ． 730 | ． 2681 | 311.5 | 792.3 | 8 8 .74 | 874.1 | 1185.6 |
| 119 | 17136 | ． 095 | 340.4 | ． 700 | ． 2702 | 312.1 | 791.8 | 81.78 | 873.6 | 1185.7 |
| 120 | 17280 | 8.163 | 341.0 | 3.671 | 0.2724 | 312.8 | 791.3 | 81． 82 | 873.2 | 1185.9 |
| 121 | 17424 | ．231 | 341.6 | ． 643 | ． 2745 | 313.4 | 790.8 | ${ }^{81} 1.86$ | 872.7 | 1186.1 |
| 122 | 17568 | ． 299 | 342.2 | ． 615 | ． 2766 | 314.1 | 790.3 | 81.90 | 872.2 | 1186.3 |
| 123 | 17712 | ． 367 | 342.8 | ． 587 | ． 2787 | 314.7 | 789.9 | 81.94 | 871.8 | 11865 |
| 124 | 17856 | ． 435 | 343.5 | ． 560 | ． 2809 | 315.3 | 789.4 | 81.98 | 871.4 | 1186.7 |
| 125 | 18000 | 8.503 | 344 | 3.534 | 0.2830 | 316.0 | 788.9 | 82.02 | 870.9 | 1186.9 |
| 126 | 18144 | ． 57 I | 344.7 | ． 507 | ． 2851 | 316.6 | 788.4 | 82.06 | 870.5 | 1187.1 |
| 127 | 18288 | ． 639 | 3453 | ．481 | ． 2872 | 317.2 | 787.9 | 82.09 | 870.0 | 1187.2 |
| 128 | 18432 | ． 708 | 345.9 | ． 456 | ． 2893 | 317.8 | 787.5 | 82.13 | 869.6 | 1187.4 |
| 129 | 18576 | ． 776 | 346.5 | ． 431 | ． 2915 | 318.4 | 787.0 | 82.17 | 869.2 | 1187.6 |
| 130 | 18720 | 8.844 | 347．I | 3.406 | 0.2936 | 319.0 | 786.5 | 82.21 | 868.7 | 1187.8 |
| 131 | 18864 | ． 912 | 347.6 | ． 382 | ． 2957 | 319.7 | 786.1 | 82.25 | 868.3 | 1188.0 |
| 132 | 19008 | ． 980 | 348.2 | －358 | ． 2978 | 320.3 | 785.6 | 82.28 | 867.9 | 1188.1 |
| 133 | 19152 | 9.048 | 348.8 | ． 334 | ． 2999 | 320.9 | 785.1 | 82.32 | 867.5 | 1188.3 |
| 134 | 19296 | ． 116 | 349.4 | ． 310 | ． 3021 | 321.5 | 784.7 | 82.35 | 867.0 | I 188.5 |
| 135 | 19440 | 9．184 | 349.9 | 3.287 | 0． 3042 | 322.1 | 784.2 | 82.38 | 866.6 |  |
| 136 | 19584 | ． 252 | 350.5 | ． 265 | ． 3063 | 322.6 | 783.8 | 82.42 | 866.2 | I 188.8 |
| 137 | 19728 | ． 320 | 351.1 | ． 424 | ． 3084 | 323.2 | 783.3 | 82.45 | 865.8 | 1189.0 |
| 138 | 19872 | －388 | 351.6 | ． 220 | ． 3105 | 323.8 | 782.9 | 82.49 | 865.4 | 1189.2 |
| 139 | 20016 | －456 | 352.2 | ． 199 | －3126 | 324.4 | 782.4 | 82.52 | 865.0 | I 189.4 |
| 140 | 20160 | 9． 524 | 352.8 | 3．177 | 0.3147 | 325.0 | 782.0 | 82.56 | 864.6 | 1189.5 |
| 141 | 20304 | ． 592 | $353 \cdot 3$ | ． 156 | ． 3168 | 325.5 | 78 I .6 | 82.59 | 864.2 | 1189.7 |
| 142 | 20448 | ． 660 | 353.9 | ． 135 | ． 3190 | 326.1 | 781.1 | 82.63 | 863.8 | 1189.9 |
| 143 | 20592 | ． 728 | 354.4 | ． 115 | ． 3211 | 326.7 | 780.7 | 82.66 | 863.4 | 1190.0 |
| 144 | 20736 | ． 796 | 355．0 | ． 094 | ． 3232 | 327.2 | 780.3 | 82.69 | 863.0 | 1190.2 |
| 145 | 20880 | 9.864 | 355.5 | 3.074 | 0.3253 | 327.8 | 779.8 | 82.72 | 862.6 | 1190.4 |
| 146 | 21024 | ． 932 | 356.0 | ． 054 | ． 3274 | 328.4 | 779.4 | 82.75 | 862.2 | 1190.5 |
| 147 | 21168 | 10.000 | 356.6 | ． 035 | ． 3295 | 328.9 | 779.0 | 82.79 | 861.8 | 1190.7 |
| 148 | 21312 | ． 068 | 357.1 | ． 016 | －3316 | 329.5 | 778.6 | 82.82 | 861.4 | 1190.9 |
| 149 | 21456 | ． 136 | 357.6 | ． 997 | ． 3337 | 330.0 | 778.1 | 82.86 | 861．0 | I 191.0 |


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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 150 | 21600 | 10.204 | 358.2 | 2.978 | 0. 3358 | 330.6 | 777.7 | 82.89 | 860.6 | 1191.2 |
| 151 | 217 | . 272 | 358.7 | . 960 | . 3379 | 331.1 | 777.3 | 82.92 | 860.2 | 1191.3 |
| 152 | 21888 | . 340 | 359.2 | . 941 | - 3400 | 331.6 | 776.9 | 82.95 | 859.9 | I 191.5 |
| 153 | 22032 | . 408 | 359.7 | . 923 | - 342 I | 332.2 | 776.5 | 82.98 | 859.5 | 1191.7 |
| 154 | 22176 | . 476 | 360.2 | . 906 | - 3442 | 332.7 | 776. I | 83.01 | 859.1 | I 191.8 |
| 155 | 22320 | 10.544 | 360.7 | 2.888 | 0.3462 | 333.2 | 775.7 | 83.04 | 858.7 | I 192.0 |
| 156 | 22464 | . 612 | 361.3 | . 871 | . 3483 | 333.8 | 775.3 | 83.07 | 858.3 | 1192.1 |
| 157 | 22608 | . 680 | 36 I .8 | . 854 | . 3504 | 334.3 | 774.9 | 83.10 | 858.0 | I 192.3 |
| 158 | 22752 | . 748 | 362.3 | . 837 | . 3525 | 334.8 | $774 \cdot 5$ | 83.13 | 857.6 | I 192.4 |
| 159 | 22896 | .816 | 362.8 | . 820 | . 3546 | $335 \cdot 3$ | 774.1 | 83.16 | 857.2 | I 192.6 |
| 160 | 23040 | 10.884 | 363.3 | 2.803 | 0.356 | 335.9 | 773.7 | 83.19 | 856.9 | I 192.7 |
| 161 | 23184 | . 952 | 363.8 | . 787 | . 3588 | 336.4 | $773 \cdot 3$ | 83.22 | 856.5 | I 192.9 |
| 162 | 23328 | 11.020 | 364.3 | . 771 | . 3609 | 336.9 | 772.9 | 83.25 | 856.1 | 1193.0 |
| 163 | 23472 | . 088 | 364.8 | . 755 | . 3630 | 337.4 | 772.5 | 83.28 | 855.8 | 1193.2 |
| 164 | 23616 | . 157 | $365 \cdot 3$ | . 739 | . 3650 | 337.9 | 772.1 | 83.31 | 855.4 | 1193.3 |
| 165 | 23760 | 11.225 | 365.7 | 2.724 | 0.3671 | 338.4 | 771.7 | 83.34 | 855. I | 1193.5 |
| 166 | 23904 | . 293 | 366.2 | . 708 | . 3692 | 338.9 | 771.3 | 83.37 | 854.7 | 1193.6 |
| 167 | 24048 | . 361 | 366.7 | . 693 | . 3713 | 339.4 | 771.0 | 83.39 | 854.3 | 1193.8 |
| 168 | 24192 | . 429 | 367.2 | . 678 | . 3734 | 339.9 | 770.6 | 83.42 | 854.0 | 1193.9 |
| 169 | 24336 | . 497 | 367.7 | . 663 | . 3754 | 340.4 | 770.2 | 83.45 | 853.6 | I 194.I |
| 170 | 24480 | II. 565 | 368.2 | 2.649 | 0. 377 | 340.9 | 769.8 | 83.48 | 853.3 | I 194.2 |
| 171 | 24624 | . 633 | 368.6 | . 634 | . 3796 | 341.4 | 769.4 | 83.51 | 852.9 | I 194.4 |
| 172 | 24768 | . 701 | 369. I | . 620 | . 3817 | 341.9 | 769.1 | 83.54 | 852.6 | I 194.5 |
| 173 | 24912 | . 769 | 369.6 | . 606 | . 3838 | 342.4 | 768.7 | 83.56 | 852.2 | 1194.7 |
| 174 | 25056 | . 837 | 370.0 | . 592 | . 3858 | 342.9 | 768.3 | 83.59 | 851.9 | I 194.8 |
| 175 | 25200 | II. 905 | 370.5 | 2. 578 | 0.3879 | 343 | 767.9 | 83.62 | 851.6 | 1194.9 |
| 176 | 25344 | . 973 | 371.0 | . 564 | . 3900 | 343.9 | 767.6 | 83.64 | 851.2 | I 195. I |
| 177 | 25488 | 12.041 | 371.4 | . 550 | . 3921 | 344.3 | 767.2 | 83.67 | 850.9 | 1195.2 |
| 178 | 25632 | . 109 | 371.9 | . 537 | . 3942 | 344.8 | 766.8 | 83.70 | 850.5 | 1195.4 |
| 179 | 25776 | . 177 | 372.4 | . 524 | . 3962 | 345.3 | 766.5 | 83.73 | 850.2 | I 195.5 |
| 180 | 25920 | I2.245 | 372.8 | 2.510 | 0.3983 | 345.8 | 766.1 | 83.75 | 8499 | 1195.6 |
| 181 | 26064 | . 313 | 373.3 | . 497 | . 4004 | 346.3 | 765.8 | 83.77 | 849.5 | 1195.8 |
| 182 | 26208 | .381 | 373.7 | . 485 | . 4025 | 346.7 | 765.4 | 83.80 | 849.2 | I 195.9 |
| 183 | 26352 | . 449 | 374.2 | . 472 | . 4046 | 347.2 | 765.0 | 83.83 | 848.9 | I 196. I |
| 184 | 26496 | . 517 | 374.6 | . 459 | . 4066 | 347.7 | 764.7 | 83.86 | 848.5 | I I96.2 |
| 185 | 26640 | 12.585 | 375. I | 2.447 | 0.4087 | 348.1 | 764.3 | 83.88 | 848.2 | 1196.3 |
| 186 | 26784 | . 653 | 375.5 | . 434 | . 4108 | 348.6 | 764.0 | 83.90 | 847.9 | 1196.5 |
| 187 | 26928 | . 721 | 376.0 | . 422 | . 4129 | 349.1 | 763.6 | 83.92 | 8.47 .5 | 1196.6 |
| 188 | 27072 | . 789 | 376.4 | . 410 | . 4150 | 349.5 | 763.3 | 83.95 | 847.2 | I 196.7 |
| 189 | 27216 | . 857 | 376.8 | . 398 | . 4170 | 350.0 | 762.9 | 83.97 | 846.9 | I 196.9 |
| 190 | 27360 | 12.925 | $377 \cdot 3$ | 2.386 | 0.4191 | 350.4 | 762.6 | 83.99 | 846.6 | 1197.0 |
| 191 | 27504 | . 993 | 377.7 | . 374 | . 4212 | 350.9 | 762.2 | 84.02 | 846.3 | 1197.1 |
| 192 | 27648 | 13.061 | 378.2 | . 362 | . 4233 | 351.3 | 761.9 | 84.04 | 845.9 | 1197.3 |
| 193 | 27792 | . 129 | 378.6 | .351 | . 4254 | 351.8 | 761.6 | 84.06 | 845.6 | 1197.4 |
| 194 | 27936 | . 197 | 379.0 | . 339 | . 4275 | 352.2 | 761.2 | 84.08 | 845.3 | I 197.5 |
| 195 | 28080 | 13.265 | 379.4 | 2.328 | 0.4296 | 352.7 | 760.9 | 84.10 | 845.0 | 1197.7 |
| 196 | 28224 | . 333 | 379.9 | . 317 | . 4316 | 353. I | 760.5 | 84.13 | 844.7 | 1197.8 |
| 197 | 28368 | . 401 | 380.3 | . 306 | . 4337 | 353.6 | 760.2 | 84.16 | 844.4 | 1197.9 |
| 198 | 28512 | . 469 | 380.7 | . 295 | . 4358 | 354.0 | 759.9 | 84.19 | 844.0 | I 198.1 |
| 199 | 28656 | . 537 | 38 I . I | . 284 | . 4379 | 354.4 | 759.5 | 84.2I | 843.7 | 1198.2 |

88 DATA RELATING TO AIR AND STEAM [pART. iv.

|  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 200 | 28800 | 13.605 | 381.6 | 2.273 | 0.4399 | 354.9 | 759.2 | 84.23 | 843.4 | I 198.3 |
| 201 | 28944 | 13.673 | 382.0 | . 262 | . 4420 | 355.3 | 758.9 | 84.26 | 843.1 | I 198.4 |
| 202 | 29088 | 13.742 | 382.4 | . 252 | . 4441 | 355.8 | 758.5 | 84.28 | 842.8 | 1198.6 |
| 203 | 29232 | 13.810 | 382.8 | . 241 | . 4461 | 356.2 | 758.2 | 84.30 | 842.5 | 1198.7 |
| 204 | 29376 | I 3.878 | 383.2 | . 231 | . 4482 | 356.6 | 757.9 | 84.33 | 842.2 | I 198.8 |
| 205 | 29520 | 13.946 | 383.7 | 2.22 I | 0.4503 | 357. I | 757.5 | 84.35 | 841.9 | 1199.0 |
| 206 | 29664 | 14.014 | 384. I | . 211 | . 4523 | 357.5 | 757.2 | 84.37 | 841.6 | II99. I |
| 207 | 29808 | 14.082 | 384.5 | . 201 | . 4544 | 357.9 | 756.9 | 84.40 | 841.3 | 1199.2 |
| 208 | 29952 | 14.150 | 384.9 | . 191 | . 4564 | 358.3 | 756.6 | 84.42 | 841.0 | 1199.3 |
| 209 | 30096 | 14.218 | 385.3 | .181 | .4585 | 358.8 | 756.2 | 84.44 | 840.7 | I 199.4 |
| 210 | 30240 | 14.386 | 385.7 | 2. 171 | 0.4605 | 359.2 | 755.9 | 84.46 | 840.4 | 1199.6 |
| 211 | 30384 | 14.454 | 386.I | . 162 | . 4626 | 359.6 | 755.6 | 84.48 | 840.1 | 1199.7 |
| 212 | 30528 | 14.522 | 386.5 | . 152 | .4646 | 360.0 | 755.3 | 84.51 | 839.8 | II99.8 |
| 213 | 30672 | 14.590 | 386.9 | . 143 | . 4666 | 360.4 | 755.0 | 84.53 | 839.5 | I I99.9 |
| 214 | 30816 | 14.658 | 387.3 | . 134 | . 4687 | 360.9 | 754.7 | 84.55 | 839.2 | 1200. 1 |
| 215 | 30960 | 14.726 | 387.7 | 2. 124 | 0.4707 | 36 I .3 | 754.3 | 84.57 | 838.9 | 1200.2 |
| 216 | 31104 | 14.794 | 388. 1 | . 115 | . 4727 | 361.7 | 754.0 | 84.60 | 838.6 | 1200.3 |
| 217 | 31248 | 14.862 | 388.5 | . 106 | . 4748 | 362.1 | 753.7 | 84.62 | 838.3 | 1200.4 |
| 218 | 31392 | 14.930 | 388.9 | . 097 | . 4768 | 362.5 | 753.4 | 84.64 | 838.0 | I200. 5 |
| 219 | 31536 | 14.998 | 389.3 | . 088 | .4788 | 362.9 | 753. 1 | 84.66 | 837.7 | 1200.7 |

## PART V. DATA SPECIALLY RELATING TO MINING.

SECTION I. DENSITY AND OTHER PHYSICAL PROPERTIES OF VARIOUS MINERAL SUBSTANCES, ORES, METALS, ETC.

## DENSITY AND SPECIFIC GRAVITY.

Density is the weight in vacuo of unit volume. On the c.g.s. system it is expressed in grammes per cubic centimetre.

The Specific Gravity of a substance is the ratio of its density to that of water at $4^{\circ} \mathrm{C}$. (this being the temperature at which water has its maximum density).

The density of water at $4^{\circ} \mathrm{C}$. ( $39^{\circ} .2 \mathrm{~F}$.) is very little less than unity. According to the latest determination, the weight in vacuo of a cubic centimetre of water at $4^{\circ} \mathrm{C}$. is 0.999974 gramme (see page 4).

For practical purposes, therefore, 'specific gravity,' as above defined, is identical with 'density.'

The first table ( p .90 ) gives the weight in pounds per cubic foot and the number of cubic feet per ton corresponding to a given density. The density of a given substance being known, this table gives either its weight per cubic foot or its volume per ton, as may be required. The densities of the principal ores are given on p. 93, those of the rock-forming minerals and gemstones on pp. 94 and 95 . The remaining tables give the density and pounds per cubic foot of various mineral substances in common use, of the metals and their alloys and of different kinds of wood.

Table giving the weight in pounds per cubic foot and the number of cubic feet per short ton of 2000 lbs . and per long ton of 2240 lbs. corresponding to a given density.

A density of $\mathrm{r} .0=1$ gramme per cubic centimetre $=62.4278 \mathrm{lbs}$. per cubic foot.

| $\begin{gathered} \text { Density } \\ = \\ \text { grammes } \\ \text { per } \\ \text { cubic } \\ \text { centi- } \\ \text { metre. } \end{gathered}$ | Pounds per cubic foot. | Cubic feet per ton 2000 lbs. | Cubic feet per ton of 2240 lbs. | $\left\|\begin{array}{c}\text { Density } \\ = \\ \text { grammes } \\ \text { per } \\ \text { cubic } \\ \text { centi- } \\ \text { metre. }\end{array}\right\|$ | Pounds per cubic foot. | Cubic feet per ton 2000 lbs. | Cubic feet per ton of 2240 lbs . |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.5 | 31.2 | 64.1 | 71.8 | 2.55 | 159.2 | 12.6 | 14.1 |
| 0.55 | 34.3 | 58.3 | 65.3 | 2.6 | 162.3 | 12.3 | 13.8 |
| 0.6 | 37.5 | 53.3 | 59.7 | 2.65 | 165.4 | 12.1 | I 3.5 |
| 0.65 | 40.6 | 49.3 | 55.2 | 2.7 | 168.6 | 11.9 | 13.3 |
| 0.7 | 43.7 | 45.8 | 5 I .3 | 2.75 | 171.7 | 11.6 | 13.0 |
| 0.75 | 46.8 | 42.7 | 47.9 | 2.8 | 174.8 | 11.4 | 12.8 |
| 0.8 | 49.9 | 40.1 | 44.9 | 2.85 | 177.9 | 11.2 | 12.6 |
| 0.85 | 53.1 | 37.7 | 42.2 | 2.9 | 181.0 | 11.0 | 12.4 |
| 0.9 | 56.2 | 35.6 | 39.9 | 2.95 | 184.2 | 10.9 | 12.2 |
| 0.95 | 59.3 | 33.7 | 37.8 | 3.0 | 187.3 | 10.7 | 12.0 |
| 1.0 | 62.4 | 32.1 | 35.9 | 3.05 | 190.4 | 10.5 | 11.8 |
| 1.05 | 65.5 | 30.5 | 34.2 | 3.1 | 193.5 | 10.3 | 11.6 |
| I.I | 68.7 | 29.1 | 32.6 | 3.2 | 199.8 | 10.0 | 11.2 |
| I. 15 | 71.8 | 27.9 | 31.2 | $3 \cdot 3$ | 206.0 | 9.7 | 10.9 |
| 1.2 | 74.9 | 26.7 | 29.9 | 3.4 | 212.3 | 9.4 | 10.5 |
| 1.25 | 78.0 | 25.6 | 28.7 | 3.5 | 218.5 | 9.2 | 10.3 |
| I. 3 | 81.2 | 24.6 | 27.6 | 3.6 | 224.7 | 8.9 | 10.0 |
| 1.35 | 84.3 | 23.7 | 26.6 | 3.7 | 231.0 | 8.7 | . 9.7 |
| I. 4 | 87.4 | 22.9 | 25.6 | 3.8 | 237.2 | 8.4 | 9.4 |
| 1. 45 | 90.5 | 22.1 | 24.8 | 3.9 | 243.5 | 8.2 | 9.2 |
| 1.5 | 93.6 | 21.4 | 23.9 | 4.0 | 249.7 | 8.0 | 9.0 |
| 1. 55 | 96.8 | 20.7 | 23.1 | 4.1 | 256.0 | 7.8 | 8.8 |
| 1.6 | 99.9 | 20.0 | 22.4 | 4.2 | 262.2 | 7.6 | 8.5 |
| 1.65 | 103.0 | 19.4 | 21.7 | 4.3 | 268.4 | 7.5 | 8.3 |
| 1.7 | 106. 1 | 18.9 | 21.1 | 4.4 | 274.7 | $7 \cdot 3$ | 8.2 |
| 1.75 | 109.2 | 18.3 | 20.5 | 4.5 | 280.9 | 7.1 | 8.0 |
| 1.8 | 112.4 | 17.8 | 19.9 | 4.6 | 287.2 | 7.0 | 7.8 |
| 1. 85 | 115.5 | 17.3 | 19.4 | 4.7 | 293.4 | 6.8 | 7.6 |
| 1.9 | 118.6 | 16.9 | 18.9 | 4.8 | 299.7 | 6.7 | 7.5 |
| 1.95 | 121.7 | 16.4 | 18.4 | 4.9 | 305.9 | 6.5 | 7.3 |
| 2.0 | 124.9 | 16.0 | 17.9 | 5.0 | 312.1 | 6.4 | 7.2 |
| 2.05 | 128.0 | 15.6 | 17.5 | 5.1 | 318.4 | 6.3 | 7.0 |
| 2.1 | 131.1 | 15.3 | 17.1 | 5.2 | 324.6 | 6.2 | 6.9 |
| 2.15 | 134.2 | 14.9 | 16.7 | $5 \cdot 3$ | 330.9 | 6.0 | 6.8 |
| 2.2 | 137.3 | 14.6 | 16.3 | $5 \cdot 4$ | 337.1 | 5.9 | 6.6 |
| 2.25 | 140.5 | 14.2 | 15.9 | 5.5 | 343.4 | 5.8 | 6.5 |
| 2.3 | 143.6 | 13.9 | 15.6 | 5.6 | 349.6 | 5.7 | 6.4 |
| 2.35 | 146.7 | 13.6 | 15.3 | 5.7 | 355.8 | 5.6 | 6.3 |
| 2.4 | 149.8 | 13.4 | 15.0 | 5.8 | 362.1 | $5 \cdot 5$ | 6.2 |
| 2.45 | 152.9 | 13.1 | 14.7 | 5.9 | 368.3 | 5.4 | 6.1 |
| 2.5 | 156.1 | I 2.8 | 14.3 | 6.0 | 374.6 | $5 \cdot 3$ | 6.0 |

Density or grammes per cubic centimetre, also pounds per cubic foot and cubic feet per short ton of 2000 lbs. and per long ton of 2240 lbs. of various mineral substances.
A density of $\mathrm{x} . \mathrm{O}=\mathrm{I}$ gramme per cubic centimetre $=62.4278 \mathrm{lbs}$. per cubic foot.

| Substance. | $\begin{gathered} \text { Density } \\ =\text { grammes per } \\ \text { centicictre. } \end{gathered}$ | Pounds per cubic foot. | Cubic feet per ton of 2000 lbs . | Cubic feet per ton of 2240 lbs . |
| :---: | :---: | :---: | :---: | :---: |
| Anthracite (solid), | 1.4-1.8 | 87.4-112.4 | 22.9-17.8 | 25.6-19.9 |
| Asbestos, | 2.0-2.8 | 124.9-174.8 | 16.0-1 1.4 | 17.9-12.8 |
| Asphaltum, | 1.1-1.2 | 68-7-74.9 | 29.1-26.7 | 32.6-29.9. |
| Basalt, - | 2.8-3.0 | 174.8-187.3 | 11.4-10.7 | 12.8-12.0 |
| Bricks (see end of table). <br> Brickwork |  |  |  |  |
| Cement- |  |  |  |  |
| Pulverized, loose, | 1.15-1.7 | 71.8-106.1 | 27.9-18.9 | 31.2-21.1 |
| Set, - | 2.7-3.0 | 168.6-187.3 | 11.9-10.7 | 13.3-12.0 |
| Chalk, - | 1.9-2.8 | 118.6-174.8 | 16.9-11.4 | 18.9-12.8 |
| Clay, | 1.8-2.6 | 112.4-162.3 | 17.8-12.3 | 19.9-13.8 |
| Clay Slate, | 2.8-2.9 | 174.8-181.0 | 11.4-11.0 | 12.8-12.4 |
| Coal- |  |  |  |  |
| 'Soft' or bituminous, in situ, | 1.2-1.5 | 74.9-93.6 | 26.7-21.4 | 29.9-23.9 |
| ' Round,' in trucks, | 0.88-0.9 | 54.9-56.2 | 36.4-35.6 | 40.8-39.9 |
| Coke, | - | 23.0-28.0 | 87.0-71.4 | 97.4-80.0 |
| Diorite, | 2.8-3.0 | 174.8-187.3 | 11.4-10.7 | 12.8-12.0 |
| Dolomite, | 2.8-2.9 | 174.8-181.0 | 11.4-11.0 | 12.8-12-4 |
| Earth (dry), - | 1.3-1.9 | 81.2-1 18.6 | 24.6-16.9 | 27.6-18.9 |
| Gneiss, | 2. 59-2.7 | 161.7-168.6 | 12.4-11.9 | 13.9-13.3 |
| Granite, | 2.59-2.75 | 161.7-171.7 | 12.4-11.6 | 13.9-13.0 |
| Graphite, | 1.9-2.3 | 118.6-143.6 | 16.9-13.9 | 18.9-15.6 |
| Gravel, | 1.2-1.8 | 74.9-112.4 | 26.7-17.8 | 29.9-19.9 |
| Greenstone, - | 2.9-3.0 | 181.0-187.3 | 11.0-10.7 | 12.4-12.0 |
| Ice, | 0.88-0.91 | 54.9-56.8 | 36.4-35.2 | 40.8-39.4 |
| Kaolin, | 2.2 | 137.3 | 14.6 | 163 |
| Lime- |  |  |  |  |
| Quick, | 0.9-1. 2 | 56.2-74.9 | 35.6-26.7 | 39.9-29.9 |
| Slaked, | 1.3-I.4 | 81.2-87.4 | 24.6-22.9 | 27.6-25.6 |
| Mortar, | 1.65-1.78 | 103.0-111.1 | 19.4-18.0 | 21.7-20.2 |
| Limestone, | 2.46-2.86 | 153.6-178.5 | 13.0-11.2 | 14.6-12.5 |
| Marble, | 2.5-2.8 | 156.1-174.8 | 12.8-11.4 | 14.3-12.8 |
| Marl, - | 1.6-2.5 | 99.9-156. 1 | 20.0-12.8 | 22.4-14.3 |
| Masonry(seeend of table). |  |  |  |  |


| Substance. | $\begin{gathered} \text { Density } \\ \text { grammes per } \\ \text { centinietre. } \end{gathered}$ | Pounds per cubic foot. | Cubic feet per ton of 2000 lbs . | Cubic feet per ton of 2240 lb . |
| :---: | :---: | :---: | :---: | :---: |
| Oolite, - | 2.0-2.4 | 124.9-149-8 | 16.0-13.4 | 17.9-1 5.0 |
| Peat, | 0. 84 | 52.4 | 38.2 | 42.7 |
| Peridotite, | 3.0-3.3 | 187.3-206.0 | 10.7-9.7 | 12.0-10.9 |
| Quartz- |  |  |  |  |
| Solid, as in lodes, | 2.67 | 166.7 | 12.0 | 13.4 |
| Broken, ready for milling, | 1. 6 | 99.9 | 20.0 | 22.4 |
| Tailings, i.e. the sands from the mill pulp, wet, as collected in settling vats, - | 1.42 | 88.7 | 22.5 | 25.3 |
| Do., dry, - - | 1. 23 | 76.8 | 26.0 | 29.2 |
| Slimes, i.e. the slowly settled portion of the mill pulp, wet, in collecting dam, - | 1.92 | 119.9 | 16.7 | 18.7 |
| Sand- |  |  |  |  |
| Dry, - | 1.3-1.65 | 81.2-103.0 | 24.6-19.4 | 27.6-21.7 |
| Damp, | I.9-2.05 | 118.6-128.0 | 16.9-15.6 | 18.9-17.5 |
| Sandstone, | 2.2-2.5 | 137.3-156. 1 | 14.6-I2.8 | 16.3-14.3 |
| Serpentine, - | 2.43-2.66 | 151.7-166.0 | 13.2-12.0 | 14.8-I 3.5 |
| Shale, - | 2.4-2.8 | 149.8-174.8 | 13.4-1 1.4 | 15.0-12.8 |
| Slate, - | 2.6-2.7 | 162.3-168.6 | 12.3-11.9 | 13.8-13.3 |
| Slimes (see under Quartz). |  |  |  |  |
| Syenite, - - | 2.75-2.9 | 171.7-181.0 | 11.6-11.0 | 13.0-12.4 |
| Tailings (see under Quartz). |  |  |  |  |
| Trachyte, - - | 2.7-2.8 | 168.6-1 74.8 | 11.9-11.4 | 13.3-12.8 |

## Bricks-

Best, pressed, weigh from 145 to 155 lbs . per cubic foot.
Common, hard,
, 120 to 130 , ,
Inferior, soft,
" 90 to ilo ", "
Masonry -
Of granite or limestone-
Best ashlar, weighs from 155 to 180 lbs . per cubic foot.
Best mortar rubble, ," 150 to 160 .,, "
Best dry rubble, , 130 to 145 ,, ,"
Rough mortar rubble, , 140 to 150 ,, ,"
Rough dry rubble, , I20 to 130 ,, ,"
Of sandstone, deduct $\frac{1}{8}$ th from the above weights.
Of brickwork-
Best pressed brick, fine joints, weighs from $\mathbf{1} 35$ to 145 lbs . per cubic ft .
Common hard brick,
, 120 to 130 ," ,"
Inferior soft brick, coarse work, ,, 90 to 110 ,, ,
Cement concrete weighs from $\mathbf{1 2 5}$ to $\mathbf{1} 45 \mathrm{lbs}$. per cubic foot.

Density and pounds per cubic foot of various metals and alloys.

| Metal or Alloy. |  |  | $\begin{array}{\|c} \text { Density } \\ =\text { grammes per cubic } \\ \text { centimetre. } \end{array}$ | Pounds per cubic foot. |
| :---: | :---: | :---: | :---: | :---: |
| Aluminium, | - - - | - - | 2.6-2.8 | 162.3-174.8 |
| Antimony, | - - - | - - | 6.7-6.72 | 418.3-419.5 |
| Bismuth, | - - - | - - | 9.7-9.9 | 605.5-618.0 |
| Brass, - | - - - | - - | 8.44-8.7 | 526.9-543.1 |
| Bronze, | - - - | - - | 8.74-8.89 | 545.6-555.0 |
| Cobalt, - | - - - | - - | 8.5-9.1 | 530.6-568.1 |
| Copper,- | - - - | - - | 8.8-8.95 | 549.4-558.7 |
| Gold, - | - - - | - - | 19.26-19.34 | 1202.4-1 207.4 |
| Iridium, | - - - | - - | 21.78-22.42 | 1359.7-1 399.6 |
| Iron- |  |  |  |  |
| Gray cast, - | - | - - | 7.03-7.13 | 438.9-445.1 |
| White cast, | , | - - | 7.58-7.73 | 473.2-482.6 |
| Wrought, | - - | - - | 7.8-7.9 | 486.9-493.2 |
| Lead, - |  | - - | II.34-1 I. 36 | 707.9-709.2 |
| Mercury at $o^{\circ}$ | C., - | - - | 13.596 | 848.8 |
| Nickel, - | - - | - - | 8.3-8.9 | 518.2-555.6 |
| Platinum, - | - | - - | 21.2-21.7 | 1323.5-I354.7 |
| Platinum and | Iridium, | - - | 21.62-22.38 | I 349.7-1 397.1 |
| Silver, - | - - - | - - | 10.4-10.57 | 649.2-659.9 |
| Steel, | - - - | - - | 7.8-7.9 | 486.9-493.2 |
| Tin, | - - - | - - | 7.29-7.3 | 455.1-455.7 |
| Tungsten, | - - - | - - | 19.12 | 1193.6 |
| Zinc, | - - - | - - | 7.04-7.19 | 439.5-448.9 |

## Density of the principal ores of the metals.

| Antimonite, | 4.6-4.7 | Hemimorphite, | 3.4-3.5 |
| :---: | :---: | :---: | :---: |
| Argentite, - | 7.0-7.4 | Kerargyrite, | 5.58-5.6 |
| Blende, | 3.9-4.2 | Limonite, | 3.4-3.9 |
| Bornite, | 4.9-5.2 | Magnetite, - | 4.9-5.2 |
| Calamine, | 4.1-4.5 | Malachite, - | 3.7-4.1 |
| Cassiterite, - | 6.8-7.0 | Manganese-spar, | 3.3-3.6 |
| Cerussite, | 6.4-6.6 | Nagyagite, - | 6.85-7.2 |
| Chalcopyrite, | 4. $\mathrm{I}-4.3$ | Platinum, | 12-18 |
| Chessylite, - | 3.7-3.8 | Proustite, | 5.5-5.6 |
| Chromite, - | 4.4-4.6 | Psilomelane, | 314-3.36 |
| Cinnabar, | 8.0-8.2 | Pyrargyrite, | 5.75-5.85 |
| Copper (Native), | 8.5-8.9 | Pyrolusite, - | 4.7-5.0 |
| Copper Glance, | 5.5-5.8 | Siderite, | 3.7-3.9 |
| Covellite | 4.6 | Silver (Native), | 10.5-1 1.0 |
| Cryolite, | 2.95-2.99 | Stephanite, | 6.2-6.3 |
| Cuprite, | 5.7-6.0 | Sylvanite, | 7.99-8.33 |
| Galena, | 7.3-7.6 | Wad, - | 2.3-3.7 |
| Gold (Native), | 15.6-19.4 | Willemite, - | 3.9-4.2 |

## Density and pounds per cubic foot of different kinds of wood.*

The wood is supposed to be seasoned and of average dryness.

| Wood. | Density $=$ grammes per cubic cm. | Pounds per cubic foot. | Wood. | Density $=$ gramnies per cubic cn. | Pounds per cubic foot. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Alder | 0.42-0.68 | 26-42 | Greenheart | 0.93-I. 04 | 58-65 |
| Apple | 0.66-0.84 | 41-52 | Hazel - | 0.60-0.80 | 37-49 |
| Ash - | 0.65-0.85 | 40-53 | Hickory | 0.60-0.93 | 37-58 |
| Basswood. See Linden. |  |  | Iron-bark - | 1.03 | 64 |
| Beech | 0.70-0.90 | 43-56 | Laburnum - | 0.92 | 57 |
| Blue gum | 0. 84 | 52 | Lancewood | 0.68-1.00 | 42-62 |
| Birch- | 0.51-0.77 | 32-48 | Lignum vitæ - | 1.17-1. 33 | 73-83 |
| Box | 0.95-1. 16 | 59-72 | Linden or Lime-tree | o. $32-0.59$ | 20-37 |
| Bullet-tree | 1.05 | 65 | Locust - - | 0.67-0.71 | 42-44 |
| Butternut | 0.38 | 24 | Mahogany, Honduras | -. 56 | 35 |
| Cedar | 0.49-0.57 | 30-35 | Spanish - | 0.85 | 53 |
| Cherry | 0.70-0.90 | 43-56 | Maple - | 0.62-0.75 | 39-47 |
| Cork - | 0.22-0.26 | 14-16 | Oak- | 0.60-0.90 | 37-56 |
| Ebony | I. 11 I-I. 33 | 69-83 | Pear-tree | 0.61-0.73 | 38-45 |
| Elm - | 0.54-0.60 | 34-37 | Plum-tree - | 0.66-0.78 | 41-49 |
| Fir or Pine, American |  |  | Poplar - - | 0.35-0. 5 | 22-31 |
| White | 0.35-0.50 | 22-31 | Satinwood | 0.95 | 59 |
| Larch | 0.50-0.56 | 31-35 | Sycamore - - | 0.40-0.60 | 24-37 |
| ", Pitch - | 0.83-0.85 | 52-53 | Teak, Indian - | 0.66-0.88 | 4I-55 |
| ," Red - | 0.48-0.70 | 30-44 | African | 0.98 | 61 |
| ," Scotch | $0.43-0.53$ | 27-33 | Walnut - | 0.64-0.70 | 40-43 |
| ", Spruce | 0.48-0.70 | 30-44 | Water gum | 1.00 | 62 |
| " Yellow | 0.37-0.60 | 23-37 | Willow - | 0.40-0.60 | 24-37 |

## Density of the rock-forming minerals and of gem-stones.

Agate, ..... 2.6
Apatite, - ..... 3.2
Aragonite, ..... 2.9
Augite, ..... 3.3-3.49
Barytes (heavy spar), ..... 4.5
Beryl (aquamarine, emerald), ..... 2.7
Calcite (calcspar, Icelàndspar), ..... 2.72
Chlorite, ..... 2.6-3.0
Chrysoberyl (Alexandrite), ..... 3.7
Corundum (ruby, sapphire), ..... 4.0
Diamond, ..... 3.52
Diopside, ..... 3.3
Dolomite, ..... 2.85
Felspar, - ..... 2.56-2.75
Fluorspar, ..... 3.2
Garnet (almandine, carbuncle, pyrope, etc.), ..... 3.1 5-4.3
Gypsum, ..... 2.3
Hornblende, - ..... 3.18-3.22

[^34]DENSITY95
Ilmenite, ..... 4.8
Magnetite, ..... 5.2
Mica, ..... 2.84-2.93
Olivine (peridote, chrysolite), ..... 3.4
Opal, ..... 2.6
Phenakite, ..... 3.0
Quartz, - ..... 2.65
Serpentine, ..... 2.6
Spinel (balas-ruby), ..... 3.5
Talc, ..... 2.7
Topaz, ..... 3.5
Tourmaline, ..... 3.1
Turquoise, ..... 2.7
Zircon (jargoon, hyacinth), ..... 4.7

## HARDNESS OF MINERALS.

The hardness of a mineral is measured by the force required to scratch (i.e. to separate) the superficial particles of the mineral with a steel point or the sharp-pointed fragment of some harder mineral. In Moh's scale, the hardness of 10 minerals is taken to represent 10 successive degrees of hardness. The degrees of hardness are, however, arbitrarily fixed, and there is no constant ratio between them :

## Moh's Scale of hardness.

I. Talc.
2. Gypsum or rock salt.
3. Calcite.
4. Fluorspar.
5. Apatite.
6. Felspar (orthoclase).
7. Quartz.
8. Topaz.
9. Corundum (sapphire).
10. Diamond.

Each of the minerals forming this scale can be scratched by those which follow, and will itself scratch those that precede it in the list; consequently the hardness of a mineral is estimated by its capability of scratching or being scratched by any mineral in this list:

## Hardness of gem-stones (on Moh's scale).

| Agate, |  |
| :---: | :---: |
| Beryl (aquamarine, emerald), |  |
| Chrysoberyl (Alexandrite), - | 82 |
| Corundum (ruby, sapphire). | 9 |
| Diamond, | 10 |
| Diopside, - | $5 \frac{1}{2}$ |
| Felspar (moonstone), - | 5 |
| Fluorspar, - | 4 |
| Garnet (almandine, carbuncle, pyrope, etc.), | 7 |
| Olivine (peridote, chrysolite), | 7 |

Opal, - - - 7
Phenakite, - - - 8
Quartz (rock-crystal, cairngorm, prase), - - 7
Serpentine, - - 3
Spinel (balas-ruby), - - 8
Topaz, - - . 8
Tourmaline, - - 7
Turquoise, - - - 6
Zircon (jargoon, hyacinth), - $7 \frac{1}{2}$

Linear expansion of the principal metals, in microns per metre (or millionths per unit length).*

Name of Metal. $\quad$. \begin{tabular}{c}
Expansion <br>
per degree C.

 

Expansion <br>
per degree F.
\end{tabular}

## SECTION II. ORE-TONNAGE PER UNIT AREA.

By means of the table on p. 97 the number of tons of an ore or mineral contained in an acre of surface can be calculated if we know the density of the ore or mineral and the average thickness and dip of the vein or bed in which it occurs : for the tonnage given in the table for the angle of dip $\times$ the thickness of the vein or bed in feet $x$ the density of the ore or mineral $=$ the number of tons per acre of surface. For example, supposing it is required to know the number of long tons of coal contained in an area of 300 acres, the seam being of an average thickness of 5 feet, having a dip of $6^{\circ}$, and the density of the coal having been determined to be r.4. For a dip of $6^{\circ}$ the table gives the constant $\mathbf{1 2 2 0 . 6}$. Therefore the required tonnage is: $1220.6 \times 5$ $\times$ I. $4 \times 300=2,563,260$ long tons. From this figure a considerable deduction has to be made in order to obtain the amount of marketable coal, the percentage to be deducted depending on the local conditions.

The table on p. 98 gives the tons of quartz per Transvaal claim.

* Smithsonian Geographical Tables, 1906, p. 170.
†Or Iridio-platinum; $90 \%$ platinum and $10 \%$ iridium. It is the alloy of which the International Prototype Metric Standards are made.

Table giving the number of short tons ( 2000 lbs .) and of long tons ( 2240 lbs .) per acre of surface contained in a vein or bed one foot thick and of a density $=\mathrm{r}$, for each degree of dip from $0^{\circ}$ to $85^{\circ}$.*

| Degrees of dip. | Short tons of 2000 lbs. per acre for a density $=1$. | Long tons of 2240 lbs. per acre for a density $=1$. | Degrees of dip. | Short tons of 2000 lbs. per acre for a density $=1$. | Long tons of 2240 lbs. per acre for a density $=1$. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | 1359.6 | 1213.9 | $45^{\circ}$ | 1922.7 | 1716.7 |
| 1 | 1359.8 | 1214.1 | 46 | 1957. I | 1747.4 |
| 2 | 1360.4 | 1214.6 | 47 | 1993.4 | 1779.9 |
| 3 | 1361.4 | 1215.6 | 48 | 2031.8 | 1814.1 |
| 4 | I 362.9 | 1216.8 | 49 | 2072.3 | 1850.3 |
| 5 | 1364.7 | 1218.5 | 50 | 2115.1 | 1888.5 |
| 6 | 1367.0 | 1220.6 | 51 | 2160.3 | 1928.9 |
| 7 | 1369.8 | 1223.0 | 52 | 2208.3 | 1971.7 |
| 8 | I 372.9 | 1225.8 | 53 | 2259. I | 2017.1 |
| 9 | 1376.5 | 1229.0 | 54 | 2313.0 | 2065.2 |
| 10 | 1380.5 | 1232.6 | 55 | 2370.3 | 2116.3 |
| 11 | 1385.0 | 1236.6 | 56 | 2431.3 | 2170.8 |
| 12 | 1389.9 | 1241.0 | 57 | 2496.2 | 2228.8 |
| 13 | 1395.3 | 1245.8 | 58 | 2565.6 | 2290.7 |
| 14 | 1401.2 | 1251.0 | 59 | 2639.7 | 2356.9 |
| 15 | 1407.5 | 1256.7 | 60 | 2719.1 | 2427.8 |
| 16 | 1414.3 | 1262.8 | 61 | 2804.3 | 2503.8 |
| 17 | 1421.7 | I 269.3 | 62 | 2895.9 | 2585.6 |
| 18 | 1429.5 | 1276.4 | 63 | 2994.7 | 2673.8 |
| 19 | 1437.9 | 1283.8 | 64 | 3101.4 | 2769. I |
| 20 | 1446.8 | I 291.8 | 65 | 3217.0 | 2872.3 |
| 21 | 1456.3 | 1300.2 | 66 | 3342.6 | 2984.5 |
| 22 | 1466.3 | 1309.2 | 67 | 3479.5 | 3106.7 |
| 23 | 1477.0 | 1318.7 | 68 | 3629.3 | 3240.4 |
| 24 | 1488.2 | I 328.8 | 69 | 3793.7 | 3387.3 |
| 25 | 1500.1 | 1339.7 | 70 | 3975. I | 3549.2 |
| 26 | 1512.6 | 1 350.6 | 71 | 4175.9 | 3728.5 |
| 27 | 1525.9 | I 362.4 | 72 | 4399.6 | 3928.2 |
| 28 | 1539.8 | 1374.8 | 73 | 4650.1 | 4151.9 |
| 29 | 1554.4 | 1387.9 | 74 | 4932.4 | 4403.9 |
| 30 | 1569.9 | 1401.7 | 75 | 5252.9 | 4690. I |
| 31 | 1586.1 | 1416.2 | 76 | 5619.8 | 5017.7 |
| 32 | 1603.2 | 1431.4 | 77 | 6043.8 | 5396.2 |
| 33 | 1621.1 | 1447.4 | 78 | 6539.1 | 5838.4 |
| 34 | 1639.9 | 1464.2 | 79 | 7125.2 | 6361.8 |
| 35 | 1659.7 | 1481.9 | 80 | 7829.3 | 6990.5 |
| 36 | 1680.5 | 1500.4 | 81 | 8690.9 |  |
| 37 | 1702.3 | I519.9 | 82 | 9768.8 | 8722.1 |
| 38 | 1725.3 | I 540.4 | 83 | I I 155.8 | 9960.5 |
| 39 | 1749.4 | 1562.0 | 84 | 13006.5 | 11613.0 |
| 40 | I 774.8 | I 584.6 | 85 | I 5599. I | 13927.8 |
| 41 | 1801. 4 | 1608.4 |  |  |  |
| 42 | 1829.5 | 1633.4 |  |  |  |
| 43 | 1859.0 | 1659.8 |  |  |  |
| 44 | 1890.0 | 1687.5 |  |  |  |
| 45. | 1922.7 | 1716.7 |  |  |  |

[^35]Table giving the number of short tons ( 2000 lbs .) of Quartz contained in a Transvaal claim of 60,000 square Cape feet per one British foot thickness of Reef, for each degree of dip from $0^{\circ}$ to $85^{\circ}$, calculated on a basis of 12 cubic feet to the ton.*

Rule: Multiply the tonnage given by the thickness of the reef in feet.

| Degrees of dip. | Tons of 2000 lbs . per claim. | Degrees of dip. | Tons of 2000 lbs . per claim. | Degrees of dip. | Tons of 2000 lbs . per claim. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | 5335 |  |  |  |  |
| 1 | 5336 | $31^{\circ}$ | 6225 | $61^{\circ}$ | 11005 |
| 2 | 5339 | 32 | 6291 | 62 | 11365 |
| 3 | 5343 | 33 | 6362 | 63 | 11752 |
| 4 | 5348 | 34 | 6436 | 64 | 12171 |
| 5 | 5356 | 35 | 6513 | 65 | 12625 |
| 6 | 5365 | 36 | 6595 | 66 | 13118 |
| 7 | 5376 | 37 | 6681 | 67 | I 3655 |
| 8 | 5388 | 38 | 6771 | 68 | 14243 |
| 9 | 5402 | 39 | 6865 | 69 | 14888 |
| 10 | 5418 | 40 | 6965 | 70 | 15600 |
| I I | 5435 | 41 | 7070 | 71 | 16388 |
| 12 | 5455 | 42 | 7180 | 72 | 17266 |
| 13 | 5476 | 43 | 7295 | 73 | 18249 |
| 14 | 5499 | 44 | 7417 | 74 | 19357 |
| 15 | 5524 | 45 | 7545 | 75 | 20615 |
| 16 | 5550 | 46 | 7681 | 76 | 22054 |
| 17 | 5579 | 47 | 7823 | 77 | 23718 |
| 18 | 5610 | 48 | 7974 | 78 | 25662 |
| 19 | 5643 | 49 | 8133 | 79 | 27962 |
| 20 | 5678 | 50 | 8300 | 80 | 30726 |
| 21 | 5715 | 51 | 8478 | 81 | 34107 |
| 22 | 5754 - | 52 | 8666 | 82 | 38337 |
| 23 | 5796 | 53 | 8866 | 83 | 43780 |
| 24 | 5840 | 54 | 9077 | 84 | 51043 |
| 25 | 5887 | 55 | 9302 | 85 | 61217 |
| 26 | 5936 | 56 | 9541 |  |  |
| 27 | 5988 | 57 | 9796 |  |  |
| 28 | 6043 | 58 | 10068 |  |  |
| 29 | 6100 | 59 | 10359 |  |  |
| 30 | 6161 | 60 | 1067 I |  |  |

*The tonnage is not affected by the shape of the claim. No deduction has been made for dykes and faults.

## SECTION 1II. UNDERGROUND TEMPERA TURES.

The rise in temperature with increasing depth is a factor of great importance in deep-level mining. The rate of increase of temperature in boreholes and deep shafts has therefore to be carefully determined. The method of observing the temperature in deep boreholes by the use of clinical thermometers is described in detail by H. F. Marriott (Trans. Inst. Min. Met., vol. xv., p. 405). Since in deep boring there is a considerable deviation from the vertical, the correct depth at the point of observation can only be obtained by a survey. Several instruments for this purpose have been invented. The simplest and most practical is that invented by Mr. Oehmen of Johannesburg, Transvaal. By this ingenious instrument the deviation from the vertical and the direction of the deviation are recorded by taking photographs of the position of a plumb-bob and a magnetic needle at any desired point in the borehole. The photographs are taken after the instrument has been lowered to the desired point, by means of two small incandescent lamps, which are illuminated by a dry battery by means of a time-contact regulated by a watch. The amount of deviation and its direction are calculated from the photograph after the sensitised paper has been developed at the surface. The amount of deviation is calculated by measuring the distance between the centre of the photograph of the plumbbob and the centre of the disc, the length of the plumb-bob being a known factor. The direction of the deviation is obtained from the photograph of the magnetic needle, the correct orientation being fixed by two pin-pricks, which have the same relative position both in the photograph of the needle and in that of the plumb-bob.*

[^36]Table of Underground Temperatures in Mines and Vertical Boreholes. (J. D. Everett, Royal Commission on Coal Supplies, 1904, vol. ii., p. 293.)


From a number of observations made in deep boreholes and mines in the Witwatersrand, Transvaal, Mr. Marriott has deduced a mean rate of increase of temperature for that district of $\mathrm{I}^{\circ}$ Fahrenheit for each 208 feet of depth, or $.48^{\circ}$ Fahr. increase per 100 feet of depth. He finds the mean temperature at 1000 feet depth to be $68.75^{\circ}$ Fahr. (Trans. Inst. Min. and Met., vol. xv., 1905-6.)

## SECTION IV. DATA RELATING TO GOLD AND COPPER RETURNS.

## The Valuation of Gold Bullion.

The value of pure gold (iooo fine) is $£ 44$ s. II.4545d. per troy ounce.* The following table for the valuation of gold bullion is calculated on this basis, namely one troy ounce of gold (iooo fine) equals $£ 4.24773$.

| Weight in <br> Grains. | Value in pounds sterling. | Weight in Dwts. | Value in pounds sterling. | $\begin{aligned} & \text { Weight } \\ & \text { in } \\ & \text { Oz. Troy. } \end{aligned}$ | Value in pounds sterling. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| I | 0.00885 | I | 0.21239 | 1 | 4.24773 |
| 2 | 0.01770 | 2 | 0.42477 | 2 | 8.49546 |
| 3 | 0.02655 | 3 | 0.63716 | 3 | 12.74319 |
| 4 | 0.03540 | 4 | 0.84955 | 4 | 16.99092 |
| 5 | 0.04425 | 5 | 1.06193 | 5 | 21.23865 |
| 6 | 0.05310 | 6 | 1.27432 | 6 | 25.48638 |
| 7 | 0.06195 | 7 | I. 48671 | 7 | 29.73411 |
| 8 | 0.07080 | 8 | 1.69909 | 8 | 33.98184 |
| 9 | 0.07964 | 9 | I.91148 | 9 | 38.22957 |
| 10 | 0.08849 | 10 | 2. 12386 |  |  |
| II | 0.09734 | II | 2.33625 |  |  |
| 12 | 0.10619 | 12 | 2. 54864 |  |  |
| 13 | O. II 504 | 13 | 2.76102 |  |  |
| 14 | 0.12389 | 14 | 2.97341 |  |  |
| I5 | 0. 13274 | 15 | 3.18580 |  |  |
| 16 | 0.14159 | 16 | 3.39818 |  |  |
| 17 | 0. 15044 | 17 | 3.61057 |  |  |
| 18 | -. 15929 | 18 | 3.82296 |  |  |
| 19 | 0.168I4 | 19 | 4.03534 |  |  |
| 20 | 0.17699 |  |  |  |  |
| 21 | o. 18584 |  |  |  |  |
| 22 | 0. 19469 |  |  |  |  |
| 23 | 0. 20354 |  |  |  |  |

Example of Application of Table.
Find value of 464 oz . I3 dwts. 3 grns. of gold bullion having a fineness of 850.5 .


[^37]Table for the conversion of Metric weight into Troy ounces.

| Grammes. | Troy ounce. |
| :---: | :---: |
| I | .03215074248 |
| 2 | .06430148496 |
| 3 | .09645222744 |
| 4 | .12860296992 |
| 5 | .16075371239 |
| 6 | .19290445487 |
| 7 | .22505519735 |
| 8 | .25720593983 |
| 9 | .28935668231 |

Table for the conversion of Russian weight into Troy ounces.
I Pood $=40$ Funts $=526.64512$ I 4319 oz. troy .
I Funt $=96$ Zolotniks $=13.1661280358 \mathrm{oz}$. troy.
I Zolotnik $=96$ Dolis $=0.1371471670$ oz. troy.
I Doli $=0.00$ I 4286163 oz. troy.

| Troy ounces. <br> 1 Pood $=526.6451214$ 2 Poods $=1053.2902429$ | Troy ounces. <br> I Zolotnik $=0.137147$ <br> 2 Zolotniks $=0.274294$ |  |
| :---: | :---: | :---: |
|  |  |  |
|  |  |  |
| $3 \quad \% \quad=1579.9353643$ | 3 | " $=0.411442$ |
| $4 \quad$ " $=2106.5804857$ | 4 | " $=0.548589$ |
| $5 \quad \#=2633.2256072$ | 5 | " $=0.685736$ |
| 6 " 6159.8707286 | 6 | " $=0.822883$ |
| $7 \quad=3686.5158500$ | 7 | $"=0.960030$ |
| $8 \quad \#=4213.1609715$ | 8 | = 1.097177 |
| $9 \quad$ ¢ 9739.8060929 | 9 | $=1.234324$ |
| 1 Funt $=13.166128$ |  | 1 Doli $=0.001429$ |
| 2 Funts $=26.332256$ |  | 2 Dolis $=0.002857$ |
| $3 \gg 39.498384$ |  | $3>=0.004286$ |
| $4 \gg 52.664512$ |  | $4>=0.005714$ |
| $5 "=65.830640$ |  | $5 "=0.007143$ |
| $6 "=78.996768$ |  | 6 " $=0.008572$ |
| $7>=92.162896$ |  | 7 " = 0.010000 |
| 8 " $=105.329024$ |  | 8 " = 0.01 1429 |
| $9 \%=118.495152$ |  | $9.10=0.012858$ |

Example of use of Table.
Convert 28 poods 39 funts 76 zolotniks 24 dolis into troy ounces.
$20 \mathrm{p} .=10532.902429 \mathrm{oz}$. troy.
$8 \mathrm{p} .=4213.160972$ "
$30 \mathrm{f} .=394.98384 \quad$ "
$9 \mathrm{f} .=118.495152 \quad$ "
$70 \mathrm{z} .=9.60030 \quad$ "
$6 \mathrm{z}=0.822883$,
$20 \mathrm{~d} .=0.02857 \quad$,
$4 \mathrm{~d} .=0.005714$ "
15269.999860 or say 15270 oz. troy.

Comparison of the various methods of expressing gold ore values in use in different countries.
Dwts. per short ton to dwts. per long ton and to Metric and Russian values.

| Dwts. per short ton (2000 lbs.). | Dwts. per long ton ( 2240 lbs .). | Grammes per tonne(toookgs.). | Zolotniks per 100 poods. |
| :---: | :---: | :---: | :---: |
| I | 1.1200 | I. 7143 | 0.6583 |
| 2 | 2.2400 | 3.4286 | 1.3166 |
| 3 | 3.3600 | 5.1429 | I. 9749 |
| 4 | 4.4800 | 6.857 I | 2.6331 |
| 5 | 5.6000 | 8.5714 | 3.2914 |
| 6 | 6.7200 | 10.2857 | 3.9497 |
| 7 | 7.8400 | 12.0000 | 4.6080 |
| 8 | 8.9600 | 13.7143 | 5.2663 |
| 9 | 10.0800 | 15.4286 | 5.9246 |

Dwts. per long ton to dwets. per short ton and to Metric and Russiąn values.

| Dwts. per long <br> ton (2240 lbs.). | Dwts. per short <br> ton (2000 lbs.). | Grammes per <br> tonne(1000kg.). | Zolotniks per <br> 1oo poods. |
| :---: | :---: | :---: | :---: |
|  | 0.8929 | 1.5306 | 0.5878 |
|  | 1.7857 | 3.0612 | 1.1755 |
| 3 | 2.6786 | 4.5918 | 1.7633 |
| 4 | 3.5714 | 6.1224 | 2.3510 |
| 5 | 4.4643 | 7.6531 | 2.9388 |
| 6 | 5.3571 | 9.1837 | 3.5265 |
| 7 | 6.2500 | 10.7143 | 4.1143 |
| 7 | 7.1429 | 12.2449 | 4.7020 |
| 8 | 8.0357 | 13.7755 | 5.2898 |
| 9 |  |  |  |

Grammes per tonne to British and Russsian values.

| Grammes per <br> tonne(foookgs.) | Dwts. per short <br> ton (2000 lbs.). | Dwts. per long <br> ton (2240 lbs.). | Zolotniks per <br> Ioo poods. |
| :---: | :---: | :---: | :---: |
|  | 0.5833 | 0.6533 | 0.3840 |
| 2 | 1.1667 | 1.3067 | 0.7680 |
| 3 | 1.7500 | 1.9600 | 1.1520 |
| 4 | 2.3333 | 2.6133 | 1.5360 |
| 5 | 2.9167 | 3.2667 | 1.9200 |
| 6 | 3.5000 | 3.9200 | 2.3040 |
| 7 | 4.0833 | 4.5733 | 2.6880 |
| 8 | 4.6667 | 5.2267 | 3.0720 |
| 9 | 5.2500 | 5.8800 | 3.4560 |

Zolotniks per 100 poods to British and Metric values.

| Zolotniks per <br> Ioo poods. | Dwts. per short <br> ton (2000 lbs.). | Dwts. per long <br> ton (2240 lbs.). | Grammes per <br> tonne(Ioookgs.). |
| :---: | :---: | :---: | :---: |
|  | 1.5191 | 1.7014 | 2.6042 |
| 2 | 3.0382 | 3.4028 | 5.2083 |
| 3 | 4.5573 | 5.1042 | 7.8125 |
| 4 | 6.0764 | 6.8056 | 10.4167 |
| 5 | 7.5955 | 8.5069 | 13.0208 |
| 6 | 9.1146 | 10.2083 | 15.6250 |
| 7 | 10.6337 | 11.9097 | 18.2292 |
| 8 | 12.1528 | 13.6111 | 20.8333 |
| 9 | 13.6719 | 15.3125 | 23.4375 |

Dolis per 100 poods to British and Metric values.

| Dolis per ioo <br> poods. | Dwts. per short <br> ton (2000 lbs.). | Dwts. per long <br> ton (2240 lbs.). | Grammes per <br> tonne(roookgs.). |
| :---: | :---: | :---: | :---: |
|  | 0.0158 | 0.0177 | 0.0271 |
| 2 | 0.0316 | 0.0354 | 0.0543 |
| 3 | 0.0475 | 0.0532 | 0.0814 |
| 4 | 0.0633 | 0.0709 | 0.1085 |
| 5 | 0.0791 | 0.0886 | 0.1356 |
| 6 | 0.0949 | 0.1063 | 0.1628 |
| 7 | 0.1108 | 0.1241 | 0.1899 |
| 8 | 0.1266 | 0.1418 | 0.2170 |
| 9 | 0.1424 | 0.1595 | 0.2441 |

Grammes per cubic Metre to Grains and Dwts. per cubic Yard.

| Grammes per <br> cubic metre. | Grains per <br> cubic yard. | Grammes per <br> cubic metre. | Dwts. per <br> cubic yard. |
| :---: | :---: | :---: | :---: |
| $\mathbf{0 . 1}$ | $\mathbf{I . 1 7 9 9}$ | $\mathbf{I . 0}$ | 0.4916 |
| 0.2 | 2.3598 | 2.0 | 0.9832 |
| 0.3 | 3.5397 | 3.0 | 1.4749 |
| 0.4 | 4.7195 | 4.0 | 1.9665 |
| 0.5 | 5.8994 | 5.0 | 2.458 I |
| 0.6 | 7.0793 | 6.0 | 2.9497 |
| 0.7 | 8.2592 | 7.0 | 3.4413 |
| 0.8 | 9.4391 | 8.0 | 3.9330 |
| 0.9 | 10.6190 | 9.0 | 4.4246 |

Grains and Dwts. per cubic Yard to Grammes per cubic Metre.

| Grains per <br> cubic yard. | Grammes per <br> cubic metre. | Dwts. per <br> cubic yard. | Grammes per <br> cubic metre. |
| :---: | :---: | :---: | :---: |
| I | 0.0848 | 1 | 2.0341 |
| 2 | 0.1695 | 2 | 4.0682 |
| 3 | 0.2543 | 3 | 6.1023 |
| 4 | 0.3390 | 4 | 8.1364 |
| 5 | 0.4238 | 5 | 10.1705 |
| 6 | 0.5085 | 6 | 12.2046 |
| 7 | 0.5933 | 7 | 14.2387 |
| 8 | 0.6780 | 8 | 16.2728 |
| 9 | 0.7628 | 9 | 18.3069 |

## Comparison of the British and American Methods of stating Copper Prices.

Based on I British pound sterling $=\$ 4.8665$, the legal equivalent given in the circular issued by the Secretary of the U.S. Treasury in October 1906.
$£_{\mathrm{I}}$ per long ton of $2240 \mathrm{lbs} .=.217254464$ cent per lb.

| Price per long ton of 2240 lbs. in British pounds sterling. | Price per lb. avoir. in U.S.A. cents. | Price per long ton of 2240 lbs. it pounds sterling. | Price per lb . avoir. in U.S.A. cents. | Price per long ton of 2240 lbs. in British sterling. | Price per lb. avoir. in U.S.A. cents. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $£ 50$ | 10.863 c. | $£ 80$ | 17.380 c . | £ıIo | 23.898 c. |
| 51 | 11.080 | 81 | 17.598 | III | 24.115 |
| 52 | 11.297 | 82 | 17.815 | 112 | 24.331 |
| 53 | 11.513 | 83 | 18.032 | 113 | 24.550 |
| 54 | 11.732 | 84 | 18.249 | 114 | 24.767 |
| 55 | 11.949 | 85 | 18.467 | 115 | 24.984 |
| 56 | 12.166 | 86 | 18.684 | 116 | 25.202 |
| 57 | 12.384 | 87 | 18.901 | 117 | 25.419 |
| 58 | 12.601 | 88 | 19.118 | 118 | 25.636 |
| 59 | 12.818 | 89 | 19.336 | 119 | 25.853 |
| 60 | 13.035 | 90 | 19.553 | 120 | 26.071 |
| 61 | 13.253 | 91 | 19.770 | 121 | 26.288 |
| 62 | 13.470 | 92 | 19.987 | 122 | 26.505 |
| 63 | 13.687 | 93 | 20.205 | 123 | 26.722 |
| 64 | 13.904 | 94 | 20.422 | 124 | 26.940 |
| 65 | 14.122 | 95 | 20.639 | 125 | 27.157 |
| 66 | 14.339 | 96 | 20.856 | 126 | 27.374 |
| 67 | 14.556 | 97 | 21.074 | 127 | 27.591 |
| 68 | 14.773 | 98 | 21.291 | 128 | 27.809 |
| 69 | 14.991 | 99 | 21.508 | 129 | 28.026 |
| 70 | 15.208 | 100 | 21.725 | 130 | 28.243 |
| 71 | 15.425 | IOI | 21.943 | 131 | 28.460 |
| 72 | 15.642 | 102 | 22.160 | 132 | 28.678 |
| 73 | 15.860 | 103 | 22.377 | 133 | 28.895 |
| 74 | 16.077 | 104 | 22.594 | 134 | 29.112 |
| 75 | 16.294 | 105 | 22.812 | 135 | 29.329 |
| 76 | 16.51 I | 106 | 23.029 | 136 | 29.547 |
| 77 | 16.729 | 107 | 23.246 | 137 | 29.764 |
| 78 | 16.964 | 108 | 23.463 | 138 | 29.981 |
| 79 | 17.163 | 109 | 23.681 | 139 | 30.198 |
| 80 | 17.380 | 110 | 23.898 | 140 | 30.416 |

## Comparison of the British and Russian Methods of stating Copper Prices.

Based on the equivalent : I rouble $=25.1 \frac{3}{8} d$. (see page 57 ). $£ \mathrm{I}$ per long ton of 2240 lbs. $=0.15248195$ rouble per pood.

| Price per long ton of 2240 lbs. in British pounds sterling. | Price in roubles per pood. | Price per long ton of 2240 lbs. in British pounds sterling. | Price in roubles per pood. | Price per long ton of 2240 lbs. in British pounds sterling. | Price in roubles per pood. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $£ 60$ | 9.149 r . | $£ 90$ | 13.723 r . | £120 | 18.298 r. |
| 61 | 9.301 | 91 | 13.876 | 12 I | 18.450 |
| 62 | 9.453 | 92 | 14.028 | 122 | 18.603 |
| 63 | 9.606 | 93 | 14.181 | 123 | 18.755 |
| 64 | 9.759 | 94 | 14.333 | 124 | 18.908 |
| 65 | 9.911 | 95 | 14.486 | 125 | 19.060 |
| 66 | 10.064 | 96 | 14.638 | 126 | 19.213 |
| 67 | 10.216 | 97 | 14.791 | 127 | 19.365 |
| 68 | 10.369 | 98 | 14.943 | 128 | 19.518 |
| 69 | 10.52 I | 99 | 15.096 | 129 | 19.670 |
| 70 | 10.674 | 100 | 15.248 | 130 | 19.823 |
| 71 | 10.826 | 101 | 15.401 | 131 | 19.975 |
| 72 | 10.979 | 102 | 15.553 | 132 | 20.128 |
| 73 | 11.131 | 103 | 15.706 | 133 | 20.280 |
| 74 | 11.284 | 104 | 15.858 | 134 | 20.433 |
| 75 | I 1.436 | 105 | 16.01 I | 135 | 20.585 |
| 76 | 11.589 | 106 | 16.163 | 136 | 20.738 |
| 77 | 11.741 | 107 | 16.316 | 137 | 20.890 |
| 78 | 11.894 | 108 | 16.467 | 138 | 21.043 |
| 79 | 12.046 | 109 | 16.62 I | 139 | 21.195 |
| 80 | 12.199 | 110 | 16.773 | 140 | 21.347 |
| 81 | 12.351 | III | 16.925 | 141 | 21.500 |
| 82 | 12.504 | II2 | 17.078 | 142 | 21.652 |
| 83 | 12.656 | 113 | 17.230 | 143 | 21.805 |
| 84 | 12.808 | 114 | 17.383 | 144 | 21.957 |
| 85 | 12.961 | 115 | 17.535 | 145 | 22.110 |
| 86 | 13.113 | 116 | 17.688 | 146 | 22.262 |
| 87 | 13.266 | 117 | 17.840 | 147 | 22.415 |
| 88 | 13.418 | 118 | 17.993 | 148 | 22.567 |
| 89 | 13.571 | 119 | 18.145 | 149 | 22.720 |
| 90 | 13.723 | 120 | 18.298 | 150 | 22.872 |

## SECTION V. MINING AREAS OF DIFFERENT COUNTRIES.

## AFRICA.

Transvaal.-The unit area for mining on proclaimed ground in the Transvaal is the Claim.

For vein and reef mining, the claim has an area of 60,000 square Cape feet. Where practicable it is rectangular in form, measuring 150 Cape feet along the strike by 400 Cape feet in a direction at right angles to the strike.

For alluvial gold mining the claim has an area of 22,500 square Cape feet. Where practicable it is square in form, measuring 150 by 150 Cape feet.

For diamond ('pipe') mining the claim has an area of 900 square Cape feet. Where practicable it is a square of 30 by 30 Cape feet.

For alluvial diamond mining the claim has an area of 1800 square Cape feet. Where practicable it is a rectangle measuring 60 by 30 Cape feet.
A vein or reef claim $=64025.34$ sq. British feet $\quad \log =4.8063519$

$$
=\mathrm{I} .4698 \mathrm{I} 95592 \text { acres } \quad \log =0.1672640
$$

$$
=0.694 \text { morgen } . \quad \log =9.8416375
$$

I acre $\quad=0.6803556217$ reef claim. $\quad \log =9.8327360$
I morgen $\quad=1.44$ reef claims. $\quad \log =0.1583625$
An alluvial gold claim $=24009.5025$ sq. British feet $\quad \log =4.3803832$

$$
=0.5511823347 \text { acre } \quad \log =9.74 \mathrm{I} 2953
$$

$=0.26041 \dot{6}$ morgen $\quad \quad \log =9.4156688$
I acre $=1.814281658$ alluvial gold claims.
$\log =0.2587047$
1 morgen $=3.84$ alluvial gold claims.
$\log =0.5843312$
A diamond (' pipe') claim $=960.380$ I sq. British feet
$\log =2.9824432$
$=0.0220472934$ acres $\quad \log =8.3433553$
$=0.010416$ morgen. $\quad \log =8.0177288$
1 acre $=45.35704155$ diamond ('pipe') claims. $\log =1.6566447$
I morgen $=96$ diamond ('pipe') claims. $\quad \log =1.9822712$
An alluvial diamond claim $=1920.7602$ sq. British feet $\log =3.2834732$

$$
\begin{array}{ll}
=0.044094587 \text { acre } & \log =8.6443853 \\
=0.02083 \text { morgen. } & \log =8.3187588
\end{array}
$$

1 acre $=22.6785208$ alluvial diamond claims. $\log =1.3556147$
I morgen $=48$ alluvial diamond claims. $\quad \log =1.6812412$

Orange River Colony.-For precious metal mining a reef claim on a public diggings has an area of 60,000 square Cape feet, and where practicable is rectangular in form, measuring 150 Cape feet along the strike by 400 Cape feet in a direction at right angles to the strike. An alluvial gold claim measures 150 by 150 Cape feet, and is either square or as nearly as possible the equivalent thereof.* A diamond ('pipe') claim is 30 by 30 , and an alluvial diamond claim 90 by 90 Cape feet. $\uparrow$ Concessions for the mining of base metals (including coal, oil, salt, etc.) can be granted by the Government or the private owner as the case may be.
An alluvial diamond claim $=8643.4209$ sq. British feet $\log =3.9366857$

$$
\begin{array}{ll}
=0.19842564 \mathrm{acre} & \log =9.2975978 \\
=0.09375 \text { morgen. } & \log =8.9719713
\end{array}
$$

I acre $=5.03967128$ alluvial diamond claims. $\log =0.7024022$
i morgen $=10.6$ alluvial diamond claims. $\quad \log =1.0230287$
For equivalents of reef, alluvial gold and diamond ('pipe') claims, see under Transvaal.

Cape Colony and British Bechuanaland.-A claim on a reef digging is a rectangle measuring $\mathrm{I}_{50}$ Cape feet in the direction of the strike by 800 Cape feet either across or on one side of the reef. On any Government land not proclaimed as a public diggings or on any abandoned public diggings a mining lease of an area not exceeding 100 morgen (211. 654 acres) may be granted by the Governor. An alluvial gold claim is a square of 150 by 150 Cape feet. A diamond ('pipe') claim is usually 30 Cape feet square, and an alluvial diamond claim is usually 60 by 30 Cape feet, but the size of the claim to be pegged is stated by the Government on the proclamation of a diamond diggings. Mining concessions for coal, copper or any mineral except gold, silver and platinum are granted by the Government or the private owner, as the case may be. $\ddagger$

$$
\begin{aligned}
& \text { A reef claim }=128050.68 \text { square British feet } \quad l o g=5.1073819 \\
& =2.939639118 \text { acres } \quad \log =0.4682940 \\
& =\mathrm{I} .38 \text { morgen. } \quad \log =0.1426675 \\
& 1 \text { acre }=0.340177811 \text { reef claim. } \quad \log =9.5317060 \\
& 1 \text { morgen }=0.72 \text { reef claim. } \quad \log =9.8573325
\end{aligned}
$$

For equivalents of alluvial gold, 'pipe' and alluvial diamond claims, see under Transvaal.

[^38]Natal.-The claim for the mining of gold and other minerals, including coal, but excepting precious stones and alluvial minerals, must not exceed 300 by 300 yards ( I 8.595 acres). A mineral claim for the mining of coal, limestone, stratified ironstone, slate, soapstone, and such minerals as may from time to time be included by order of the Governor in Council, must not exceed 700 by 700 yards (iol. 239 acres).* An alluvial claim for the mining of alluvial deposits of precious stones or minerals must not exceed 100 by 100 British feet (0.229 acre).

Rhodesia.-A reef claim is a rectangle of 150 by 600 Cape feet, the shorter sides of which are parallel to the strike of the reef. It carries the so-called 'extra-lateral right,' that is, the reef can be followed underground beyond the vertical planes in which the surface boundaries lie. Reef claims are pegged in blocks of rо, a block being under ordinary circumstances a parallelogram of 1500 by 600 Cape feet, and in no case of a greater area than 900,000 square Cape feet. An alluvial gold claim must, where possible, be a square of 200 by 200 Cape feet, and must in no case contain more than 40,000 square Cape feet. Coal mining locations of either 50 , 100 or 150 morgen (105.827, 211.654 or 327.48 r acres) are granted. A copper-mining location may be pegged of an area equivalent to not more than 30 reef claims of 90,000 square Cape feet each. No extra lateral rights exist in the mining of coal or copper locations. $\dagger$

| A reef claim | $=96038.01$ sq. British feet | $\log =4.9824432$ |
| :---: | :---: | :---: |
|  | $=2.20472934$ acres | $\log =0.3433553$ |
|  | $=1.041 \dot{6}$ morgen. | $\log =0.0177288$ |
| 1 acre | $=0.4535704155$ reef claim. | $\log =9.6566447$ |
| 1 morgen | $=0.96$ reef claim. | $\log =9.9822712$ |
| A block of io reef claims $=\mathbf{2 2 . 0 4 7 2 9 3 4}$ acres |  | $\log =1.3433553$ |
|  | $=10.41 \dot{6}$ morgen. | $\log =1.0177288$ |
| An alluvial gold claim | $=42683.56$ sq. British feet | $\log =4.6302606$ |
|  | $=0.9798797 \mathrm{acre}$ | $\log =9.9911727$ |
|  | $=0.4 \dot{6} 2 \dot{9}$ morgen. | $\log =9.6655462$ |
| 1 acre $=1.02$ | 53343 alluvial gold claims. | $\log =0.0088273$ |
| 1 morgen $=2.16$ | alluvial gold claims. | $\log =0.3344538$ |

* Natal Mines Act of 1899 .
†The British South Africa Company's Mining Ordinance of 1903.

The Gold Coast Colony and Ashanti.-Mining concessions obtained from natives must not exceed five square miles in area. This does not apply to concessions obtained and registered previous to October 1895.*

Egypt.-There is no definite limit as to the size of a mining lease, which may be granted by the Government at a price per feddan ( .42008 j hectare or 1.038086 acres), which varies according to the nature of the mineral to be mined. There is in addition a tax of $10 \%$ on all net profits accruing from the working of the lease.

Sudan.-The maximum areas of mining leases are:

| For non-alluvial gold, | 64 | hectares | or | 160 | acres. |
| :--- | ---: | :--- | :--- | :--- | :--- |
| $"$ silver, | 64 | $"$ | $"$ | 160 | $"$ |
| $"$ any other metal, | 128 | $"$ | $"$ | 320 | $"$ |
| $"$ oil, | 256 | $"$ | $"$ | 640 | $"$ |
| $"$ coal, | 512 | $"$ | $"$ | 1280 | $"$ |

Each lease must be rectangular in shape, and of a length not exceeding four times its breadth. $\dagger$

## AUSTRALASIA.

New South Wales.-A gold-mining lease must not exceed an area of 25 acres, except when the Secretary for Mines is "satisfied that special difficulties exist in working the ground either by way of great depth or wetness, or on account of the cost by appliances required." In such case a special lease is granted, the tenure, form and area of which is prescribed by the Governor. If an ordinary gold-mining lease not exceeding 25 acres be located on a quartz vein or lode, the maximum length (measured in the direction of the strike) is 600 yards and the maximum width (measured across the lode) 200 yards. "In no case shall the area be marked out so that the lode will be distant from either extremity of the boundaries defining the width of the said area less than one-tenth of such width, nor shall the length along the lode in any such area be

[^39]greater than three times the width of such area." * All other gold-mining leases must be, where practicable, in the form of a parallelogram, the maximum length of which must not be more than twice the maximum breadth. "The area of a mining lease for any mineral shall not exceed 640 acres and (unless specially authorised by the Secretary for Mines) shall not be less than 40 acres for coal-mining lots, and shall not exceed 80 acres nor be less than 20 acres for other mineral lots." . . . "Mineral lots shall be measured in the form of a square, except in any case where the Minister shall authorise a departure from that form." $\dagger$

Queensland.-The area of a gold-mining lease is limited to 12 acres until seven years from the date of the proclamation of the gold-field, or to 25 acres until fourteen years from the date of proclamation. After the expiration of this latter period the area of the lease may be extended to 50 acres if the ground in question has previously been worked and abandoned, or if, in the opinion of the Warden of the gold-field, the undue wetness or great depth of the workings and the consequent high working costs warrant the extension. A mining lease for silver, antimony or tin within the limits of any gold-field or mineral-field specially notified by proclamation shall not exceed 80 acres, and beyond such limits shall not exceed 120 acres. The maximum area of a mining lease for any other mineral except coal is 160 acres. A coal-mining lease may not be larger than 320 acres, except in the case of the discovery of a new seam of coal at least 15 miles from any known payable coal-field, or of a hitherto unknown coal seam at a depth of at least 600 feet. The discoverer in such case is entitled to a lease of 640 acres. $\ddagger$ Wherever practicable, a mining lease must be rectangular in form, with the length not exceeding twice the breadth, but in special cases leases of irregularly shaped areas may be granted.

South Australia.-The maximum areas of mining leases are: for gold, 20 acres; for other minerals except coal, oil, salt and gypsum, 40 acres; for coal, oil, salt or gypsum, 640 acres.

[^40]Any number of leases may be held by one person, but not more than four adjoining gold or mineral leases may be amalgamated.*

Victoria.-The maximum area of a gold-mining lease is 100 acres, while a mining lease for any other mineral (including coal) must not exceed 640 acres. There are no regulations as to the form of a mining lease. $\dagger$

West Australia.-The maximum area of an ordinary goldmining lease is 24 acres; but where the ground has previously been worked for alluvial gold and afterwards abandoned, or where, in the opinion of the Warden, the working will be costly by reason of excessive wetness or great depth, a lease not exceeding 48 acres may be granted. The maximum area of a mining lease for all minerals, except gold and coal, is 48 acres. A coal-mining lease must not exceed 320 acres, except in the case of the discovery of a new seam of coal at least 15 miles from any known payable coal. The discoverer in such case is granted a lease of $6 \not+0$ acres free of royalty for ten years. $\ddagger$

Tasmania.-The maximum area of a gold-mining lease is 20 acres. A mining lease for coal, shale, slate, freestone or limestone must not exceed 320 acres, while the maximum area of a mining lease for any mineral except those already mentioned is 80 acres. If gold be found associated or combined with other minerals in such proportion that the amount recovered is of less value than that of the minerals with which it is associated or combined, the lease may have a maximum area of 80 acres. All mining leases must, where practicable, be square in form with the bearings of the boundary lines corresponding to the cardinal points of the compass. Two or more leases may be amalgamated.s

New Zealand.-The unit of mining area in New Zealand is the Claim. Claims may be either ordinary, extended or special. The maximum areas are: for an ordinary claim, $\mathbf{I}$ acre if under license, or 10,000 square feet if not under license; for an extended claim, 5 acres; and for a special claim, 100 acres.

[^41]The maximum lengths in the direction of the strike of the reef are: for an ordinary quartz claim 200 feet, and for an extended quartz claim 500 feet. The maximum lengths along the watercourse are: for an ordinary dredging or river claim, 3 chains ( 198 feet); for an extended dredging claim, 15 chains ( 990 feet): and for a special dredging claim, i mile. The maximum lengths of shore frontage are: for an ordinary seabeach claim, 200 feet; for an extended sea-beach claim, 500 feet ; and for a special sea-beach claim, I mile. A special sea-beach claim may be extended beyond 100 acres* in the seawards direction.

## NORTH AMERICA.

British Columbia.-From 1884 to 1892 the vein-mining claim of British Columbia was the same as that of the United States, namely, an area of 1500 by 600 feet, carrying the 'extra-lateral right.' The Mineral Act, however, was revised in 1891, and further augmented in 1896 and 1897. It now defines the unit of mining area as a rectangular claim not exceeding 1500 feet in either length or width (measured horizontally), with no extralateral right. The underground rights are therefore confined to the vertical planes in which the surface boundaries lie.

$$
\begin{array}{cccc}
\text { A vein-mining claim } & =51.65289 \text { acres } & & \log =1.7130946 \\
& =20.90315 \text { hectares. } & & \log =1.3202116 \\
\text { I acre } & & =.01936 \text { claim. } & \\
\text { I hectare } & & =.0478397 \text { claim. } & \\
l o g=8.2869054 \\
& \log =8.6797884
\end{array}
$$

In 'creek diggings' a placer claim is 250 feet square, the side lines of which must run in the general direction of the watercourse or stream. In 'bar diggings' a placer claim may be either 250 feet square on any bar which is covered at high water, or 250 in length, and of the width contained between the highwater and the extreme low-water marks. In 'dry diggings' a claim is 250 feet square.

A placer claim must be as nearly as possible rectangular in form. The maximum length of a dredging lease is 5 miles. The maximum areas of leases for hydraulicing and precious stone diggings are 80 acres and io acres respectively. A coal or petroleum lease is a square block of a maximum area of 640 acres.

[^42]Nova Scotia.-For gold and silver mining the unit area is a rectangle measuring 250 feet by 150 feet, laid off with the shorter sides running east and west. Any number of these areas, not exceeding 100, can be taken up. For the mining of other minerals an area of 5 square miles, not exceeding $2 \frac{1}{2}$ miles in length, may be granted.

Quebec.-The total area of the mining concessions which can be acquired by one person is 400 acres, but under special circumstances the Lieutenant-Governor in Council may grant an area not exceeding 1000 acres.

Ontario.-A mining claim may be either 15 chains square ( $22 \frac{1}{2}$ acres) or 20 chains square ( 40 acres).

New Brunswick.-From 10 to 100 rectangular areas of 250 by 150 feet may be acquired for gold and silver mining. The boundaries must be laid off in the direction of the cardinal points of the compass. Mining leases of a maximum area of one square mile are granted for oil, natural gas or any mineral excepting gold and silver, but the Surveyor-General may, under special circumstances, sanction a larger lease.

Manitoba and the North-West Territories.-A gold quartz claim is a square of 1500 by 1500 feet without the extra-lateral right (see British Columbia).

Placer mining claims generally are 100 feet square. On the North Saskatchewan River, placer claims "are either bar or bench, the former being 100 feet long and extending between high and low-water mark. The latter includes bar diggings, but extends back to the base of the hill or bank, but not exceeding 1000 feet. Where steam power is used, claims 200 feet wide may be obtained."

Two dredging leases of five miles each may be obtained. "The lessee's right is confined to the submerged bed or bars of the river below low-water mark, and subject to the rights of all persons who have, or who may receive entries for bar diggings or bench claims, except on the Saskatchewan River, where the lessee may dredge to high-water mark on each alternate leasehold."

For iron and mica the maximum area of a location is 160 acres ; a coal-mining location may not exceed 320 acres; and the
area of a petroleum location may not be larger than 1920 acres.

Yukon Territory.-A gold quartz claim is a square 1500 by 1500 feet, without the extra-lateral right (see British Columbia). Creek, gulch, river and hill claims may not exceed 250 feet in length, measured in the general direction of the creek or gulch, with a width of from 1000 to 2000 feet. All other placer claims are 250 feet square. For dredging, six leases, each five miles long, may be acquired. "The lessee's right is confined to the submerged bed or bars in the river below low-water mark, that boundary to be fixed by its position on the ist day of August in the year of the date of the lease."

For iron, mica or copper mining, the Minister of the Interior may grant an area of 160 acres. The size of coal-mining areas is not defined, but applications for the purchase of such lands may be made to the Crown Timber and Land Agent. Petroleum leases of an area not exceeding 1920 acres ( 3 square miles) can also be acquired.

The United States.-The unit area for vein mining in the United States is the claim of 1500 feet along the strike of the vein by 600 feet in width. The 'law of the apex' gives the extra-lateral right, i.e. the vein may be followed beyond the vertical planes in which the surface boundaries lie, to an indefinite depth on all its 'dips, spurs and angles.'

$$
\begin{aligned}
\text { I vein-mining claim } & =20.661157 \text { acres } & & \log =1.3151546 \\
& =8.3613 \text { hectares. } & & \log =0.9222742 \\
& \text { I acre } & & =.0484 \text { vein-mining claim. }
\end{aligned} \begin{array}{ll}
\log =8.6848454 \\
\text { I hectare } & \\
& =.119585 \text { vein-mining claimı. }
\end{array}
$$

The maximum area of a placer claim is: for one person 20 acres, or for an association or company of eight or more persons, 160 acres.

The maximum area of a coal-mining location is: for one person 160 acres, or for an association or company of not less than four persons, 640 acres.

Mexico.-The unit area for the mining of all metals, also precious stones, rock-salt and sulphur, is the Pertenencia, which by a decree of President Diaz issued on June 4, 1892, with effect from July 1, 1892, is "a solid block of unlimited depth, defined above ground by that part of the surface which in
horizontal projection gives a square, each side of which measures 100 metres; and bounded underground by the four vertical planes corresponding to the sides of the said square."

$$
\begin{aligned}
\text { I pertenencia } & =1 \text { hectare } & & \\
& =2.471058 \text { acres. } & & \log =0.3928830 \\
\text { I acre } & =0.404685 \text { pertenencia. } & & \log =9.6071170
\end{aligned}
$$

## SOUTH AMERICA.

British Guiana.-A gold-mining claim must not exceed 1500 feet in length by 800 feet in width. A claim located for the purpose of searching for precious stones must not exceed 1500 feet in length by 800 feet in width, nor contain a greater area than 500 acres. A claim must, where practicable, be rectangular in form and it is limited underground by the vertical planes in which the surface boundaries lie.*

Colombia.-The unit area for vein mining is 600 by 240 metres, and for alluvial mining 5 by 2 kilometres. $\dagger$

$$
\begin{aligned}
& \text { I vein-mining area } \quad=14.4 \text { hectares } \quad \log =1.1583625 \\
& =35.583235 \text { acres. } \quad \log =\mathbf{1 . 5 5 1 2 4 5 5} \\
& 1 \text { hectare } \quad=.069 \dot{4} \text { vein-mining claim. } \quad \log =8.8416375 \\
& 1 \text { acre } \quad=.028103 \text { vein-mining claim. } \quad \log =8.4487545 \\
& \text { I alluvial-mining area }=10 \text { sq. kilometres } \\
& =1000 \text { hectares } \\
& =2471.05814 \text { acres } \quad \log =3.3928830 \\
& =3.86103 \text { square miles. } \quad \log =0.5867030
\end{aligned}
$$

Chile.-For coal the mining area or pertenencia is 50 hectares ( 123.5529 acres); while for any other mineral it may be from I to 5 hectares ( 2.47106 to $\mathbf{1 2 . 3 5 5 3}$ acres). There is no 'extralateral right.' $\ddagger$

Peru.-The mining area or pertenencia for gold, silver, platinum, lead, tin, copper, antimony, zinc, coal or petroleum is a square of 200 by 200 metres ( 4 hectares or 9.88423 acres), while a pertenencia located on a deposit of borax, sulphur or any other non-metallic mineral is half that size

[^43](2 hectares or 4.942116 acres). The maximum holding is limited to 240 hectares (593.05395 acres, 60 large or 120 small pertenencias). There is no 'extra-lateral right.'

## ASIA.

British India.-The Collector of any district in British India can grant a prospecting license carrying with it the right to a lease for 30 years on a block of ground of any size not exceeding I square mile, provided the ratio of the length (in the direction of strike of the vein) to the breadth does not exceed 4 to i. Applications for more than 1 square mile are dealt with by the Board of Revenue.

In the Native State of Mysore, the size of the mining area granted to one applicant is limited to 2 square miles.

Ceylon.-On Crown lands, mining leases for one or more blocks, each of which must be over 10 and not more than 100 acres in extent, may be granted by the Governor, but the total area held by the lessee or by those joined in interest with him must not exceed 500 acres. Except when specially sanctioned, the length of a block must not exceed four times its breadth.*

Malay Peninsula.-Mining leases for large areas are granted by the Sultan of Pahang on the recommendation of the British Resident; but mining permits giving the holder the right to dig for gold and tin within an area of 5 acres are also granted. $\dagger$

Russian Empire.-For vein-mining the maximum area of an Otreod or concession is a square verst (r.138062 square kilometres or .439408 square mile). The ratio of the length (in the direction of the strike of the vein) to the breadth must not exceed 3 to I .

For alluvial mining in Siberia, the length of the concession is limited to 5 versts ( 5.3340 kilometres or 3.314394 miles), while the breadth may extend to the full width of the valley in which the auriferous gravels lie. In the Urals the size of

[^44]an alluvial concession is limited to 1 square verst (1.138062 square kilometres or .439408 square mile), the maximum length being 5 versts ( 5.3340 kilometres or 3.314394 miles) and the minimum breadth 100 sagenes ( 213.36 metres or 700 feet).*

Japan. - The right to exploit alluvial gold, iron-sand or stream tin deposits is restricted to Japanese subjects, but foreign companies registered under, and conforming to, the laws of the country are permitted to mine all minerals occurring otherwise than as alluvial deposits.

The area of a mining concession for any mineral except coal must not be less than 3000 tsubo ( 2.45064 acres or .99173553 hectare) or more than 600,000 tsubo (490.128 acres or 198.347106 hectares). A coal concession must not be less than 10,000 tsubo (8.1688 acres or 3.3057851 hectares) or more than 600,000 tsubo. If two or more concessions be amalgamated, the combined areas may exceed 600,000 tsubo. $\dagger$

* Code Minière Russe, St. Petersburg, J893, p. 105.
$\dagger$ From Sketch of the Mining Industry of Japan, published by the Japanese Bureau of Mines in 1904.


## PART VI. DATA RELATING TO SURVEYING.

## SECTION I. TRIGONOMETRICAL AND MISCELLANEOUS FORMULA AND CONSTANTS.

Let $A$ be any acute angle, and let a perpendicular $B C$ be drawn from any point in one side to the other side. Then, if the sides

of the right triangle thus formed are denoted by letters, as in the figure, we have these six formulæ:

1. $\sin A=\frac{a}{c}$.
2. $\cos A=\frac{b}{c}$.
3. $\tan A=\frac{a}{b}$.
4. $\operatorname{cosec} A=\frac{c}{a}$.
5. $\sec A=\frac{c}{b}$.
6. $\cot A=\frac{b}{a}$.

Solution of Right Angles. (Fig. i.)

|  | Given. | Sought. | Formule. |  |
| :--- | :---: | :---: | :---: | :---: |
| 7. | $a, c$ | $A, B ; b$ | $\sin A=\frac{a}{c}$, | $\cos B=\frac{a}{c}$, |
| 8. | $a, b$ | $A, B, c$ | $\tan A=\frac{a}{b}, \quad \cot B=\frac{a}{b}$, | $c=\sqrt{(c+a)(c-a)}$. |
| 9. | $A, a$ | $B, b, c$ | $B=90^{\circ}-A, \quad b=a \cot A$, | $c=\frac{a}{\sin A}$. |
| 10. | $A, b$ | $B, a, c$ | $B=90^{\circ}-A, a=b \tan A$, | $c=\frac{b}{c \sin }$. |
| 11. | $A, c$ | $B, a, b$ | $B=90^{\circ}-A, a=c \sin A$, | $b=c \cos A$. |

Solution of Oblique Triangles. (Fig. 2.)


Fig. 2.

|  | Given. | Sought. | Formule. |
| :---: | :---: | :---: | :---: |
| 12. | $A, B, a$ | $b$ | $b=\frac{a \sin B}{\sin A}=a \sin B \operatorname{cosec} A .$ |
| 13. | $A, a, b$ | $B$ | $\sin B=\frac{b \sin A}{a} .$ |
| 14. | $a, b, C$ | $A, B$ | $\begin{array}{rlrl} \tan \frac{1}{2}(A-B) & =\frac{a-b}{a+b} \cot \frac{1}{2} C, \\ \text { then } & A & =\left(90^{\circ}-\frac{1}{2} C\right)+\frac{1}{2}(A-B) \\ \text { and } & B & =\left(90^{\circ}-\frac{1}{2} C\right)-\frac{1}{2}(A-B), \end{array}$ $a \text { being the longer side. }$ |
| 15. | $a, b, c$ | A | $\left\{\begin{array}{l} \text { Let } s=\frac{1}{2}(a+b+c): \quad \sin \frac{1}{2} A=\sqrt{\frac{(s-b)(s-c)}{b c}} ; \\ \cos \frac{1}{2} A=\sqrt{\frac{s(s-a)}{b c}}, \tan \frac{1}{2} A=\sqrt{\frac{(s-b)(s-c)}{s(s-a)}} ; \\ \sin A=\frac{2 \sqrt{[s(s-a)(s-b)(s-c)]}}{b c} . \end{array}\right.$ |
| 16. | $A, B, C, a$ | Area | $\text { Area }=\frac{a^{2} \sin B \sin C}{2 \sin A}$ |
| 17. | $A, b, c$ | Area | Area $=\frac{1}{2} b c \sin A$. |
| 18. | $a, b, c$ | Area | Let $s=\frac{1}{2}(a+b+c):$ area $=\sqrt{s(s-a)(s-b)(s-c)}$. |

## General Trigonometrical Formulæ.

19. 
```
\mp@subsup{\operatorname{sin}}{}{2}A+\mp@subsup{\operatorname{cos}}{}{2}A=1.
    sin}(A\pmB)=\operatorname{sin}A\operatorname{cos}B\pm\operatorname{sin}B\operatorname{cos}A
    cos(A\pmB)=cos A cos B\mp\operatorname{sin}A\operatorname{sin}B.
                    sin}2A=2\operatorname{sin}A\operatorname{cos}A
    cos 2A= 㓣2}A-\mp@subsup{\operatorname{sin}}{}{2}A=\mathbf{I}-2\mp@subsup{\operatorname{sin}}{}{2}A=2\mp@subsup{\operatorname{cos}}{}{2}A-\textrm{I}
    \mp@subsup{\operatorname{sin}}{}{2}A=\frac{1}{2}-\frac{1}{2}\operatorname{cos}2A.
    \mp@subsup{\operatorname{cos}}{}{2}A=\frac{1}{2}+\frac{1}{2}\operatorname{cos}2A.
```



General Trigonometrical Formulæ-continued.
26.
27.
28.
29.
30.
31.
32.
33.
34.
35.
36.
37.
38.
39.
40.
$\frac{\sin A-\sin B}{\cos A+\cos B}=\tan \frac{1}{2}(A-B)$.
$\frac{\sin A-\sin B}{\cos B-\cos A}=\cot \frac{1}{2}(A+B)$.
$\tan \frac{1}{2} A=\frac{\sin A}{1+\cos A}$.
$\cot \frac{1}{2} A=\frac{\sin A}{\mathrm{I}-\cos A}$.

Miscellaneous Formulæ.

|  | Sought. | Given. | Formules. |
| :---: | :---: | :---: | :---: |
| 44. | Area of Circle, | Radius $=r$, | $\pi r^{2}$. |
| 45. | Ellipse, | Semi-axes $=a$ and $b$, | $\pi a b$. |
| 46. | Parabola, | Chord $=c$, height $=h$, | ${ }_{3}^{2} c h$.* |
| 47. | Regular Polygon, | $\left\{\begin{array}{c} \text { Side }=a, \\ \text { number of sides }=n, \end{array}\right\}$ | $\frac{1}{4} a^{2} n \cot \frac{180^{\circ}}{n} .$ |
| 48. | Surface of Sphere, | Radius $=r$, | $4 \pi r^{2}$. |
| 49. | Zone, | Radius $=r$, height $=h$, | $2 \pi r h$. |
| 50. | Spherical Polygon, | $\left\{\begin{aligned} \text { Radius of sphere } & =r, \\ \text { sum of angles } & =S, \\ \text { number of sides } & =n, \end{aligned}\right\}$ | $\pi r^{2} \times \frac{S-(n-2) 180^{\circ}}{180^{\circ}}$ |
| 51. | Solidity of Prism or Cylinder, | Base $=b$, height $=h$, | bh. |
| 52. | Pyramid or cone, | Base $=b$, height $=h$, | $\frac{1}{3} b h$ |
| 53. | $\left\{\begin{array}{c} \text { Frustum of Pyra- } \\ \text { mid or Cone, } \end{array}\right\}$ | $\left\{\begin{array}{c} \text { Bases }=b \text { and } b_{1}, \\ \text { height }=h, \end{array}\right\}$ | $\frac{1}{3} h\left(b+b_{1}+\sqrt{6 b_{1}}\right)$. |
| 54. | Sphere, | Radius $=r$, | $\frac{4}{3} \pi r^{3}$. |
| 55. | Spherical Segment, | $\left\{\begin{array}{c} \text { Radii of bases }=r \text { and } r_{1}, \\ \text { height }=h, \end{array}\right\}$ | $\frac{1}{2} \pi h\left(r^{2}+r_{1}^{2}+\frac{1}{3} h^{2}\right)$. |
| 56. | Prolate Spheroid, | $\left\{\begin{array}{l} \text { Semi-transverse axis of } \\ \text { ellipse }=a \end{array}\right\}$ | ${ }_{3}^{4} \pi a b^{2}$. |
| 57. | Oblate Spheroid, | $\left\{\begin{array}{c} \text { Semi-conjugate axis of } \\ \text { ellipse }=b, \end{array}\right.$ | $\frac{4}{3} \pi a^{2} b$ |
| 58. | Paraboloid, | $\left\{\begin{array}{c} \text { Radius of base }=r, \\ \text { height }=h, \end{array}\right\}$ | $\frac{1}{2} \pi r^{2} h$. |
| $\begin{array}{rlrl} \pi=3.1415926536 ; & \text { logarithm } & =0.4971498727 . \\ \pi^{2} & =9.8696044011 ; & ,, & \\ \sqrt{\pi} & =1.7724538509 ; & ,, & \\ =0.248529974546 . \end{array}$ |  |  |  |
|  |  |  |  |
|  |  |  |  |

[^45]
## Physical Constants.

Velocity of light (Harkness)
$=186,337$ miles per second
$=299,878$ kilometres per second.
Velocity of sound through dry air
$=1090 \sqrt{1+0.00367 t}$ feet per second,
where $t \quad=$ temperature in degrees Centigrade.
The general mean deduced by Rowland (Proc. Am. Acad., vol. xv., p. 144) for dry air at $0^{\circ} \mathrm{C}$.

$$
\begin{aligned}
& =331.75 \text { metres per second } \\
& =1088.42 \text { feet per second }
\end{aligned}
$$



From the Smithsonian Physical Tables, p. ıоо.

## Astronomical Constants (Harkness).

Sidereal year $=365.2563578$ mean solar days.
Sidereal day $=23$ hours 56 min . 4.100 seconds mean solar time. Mean solar day $=24$ hours 3 min . 56.546 seconds sidereal time. Mean distance of the earth from the sun $=92,800,000$ miles.

## Geodetic Constants.

Dimensions of the earth (Clarke's spheroid) :
Equatorial semi-axis 3963.3 miles.
Polar ", 3949.8 ,,
Perimeter of meridian ellipse $24,854.76$ miles.
Circumference of equator $24,901.96$ "
Area of earth's surface $196,940,400 \mathrm{sq}$. miles.
Mean density of the earth (Harkness) $5.576 \pm 0.016$.
Surface density of the earth (Harkness) $2.56 \pm 0.16$.

Acceleration of gravity at sea-level (Harkness)
$=980.60(\mathrm{r}-0.002662 \cos 2 \phi)$ centimetres per second,
where $\phi=$ the latitude.
Length of seconds pendulum (Harkness)
$=0.990910+0.005290 \sin ^{2} \phi$ metres,
where $\phi=$ the latitude.

## SECTION II. THE COORDINATION OF

 SURVEY POINTS.The permanent stations of a modern survey are usually plotted by means of rectangular coordinates, the use of the protractor being restricted to the draughting of the temporary points and


Fig. I.
detail. The customary method of coordinating a survey is as follows :

The most prominent and central station of the survey, from which the direction of the true meridian has been determined, is selected as the 'point of origin' o. At this point two fixed axes, $y$ and $x$, are assumed to intersect at right angles, the direction of the $y$ axis being made to coincide with the true meridian. From the starting point $o$, the latitude (distance north or south) and the departure (distance east or west) of each station of the survey are calculated, the latitudes being the $y$ and the departures the $x$ coordinates.

The $y$ coordinates to the north of, and the $x$ coordinates to the east of $o$ are positive and carry a plus sign, while those to the south of and to the west of $o$ are negative and carry a minus sign. They are stated with the $y$ s before (to the left of) the $x \mathrm{~s}$; thus $+950.13-726.48$ may represent the coordinates of a point 950.13 units north of, and 726.48 units west of 0 . From 0 , the bearing of the true north (along the $y$ axis) is taken as $360^{\circ}$ or $0^{\circ}$, the east (along the $x$ axis) as $90^{\circ}$, the south as $180^{\circ}$ and the west as $270^{\circ}$. Therefore, if the coordinates of a point carry the signs :
++ , its bearing from $o$ is in the ist quadrant between $0^{\circ}$ and $90^{\circ}$

| ,-+ | $"$ | $\#$ | $"$ | 2nd | $"$ | $\#$ | $90^{\circ}$ | $180^{\circ}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ,-- | $"$ | $"$ | $"$ | 3 3rd | $"$ | $"$ | $180^{\circ}$ | $"$ | $270^{\circ}$ |
| ,+- | $"$ | $"$ | $"$ | 4 th | $"$ | $"$ | $270^{\circ}$ | $"$ | $360^{\circ}$ |

Coordinates are usually calculated by means of logarithms and checked by natural sines and cosines, using 'short' multiplication.*

Example. Given the measured lengths

$$
o A=377.92, A B=1015.74 \text { and } B C=284.63,
$$

and the observed angles $y 0 A=47^{\circ} 19^{\prime} \quad 20^{\prime \prime}$ (the bearing of the line $O A$ ), $O A B=83^{\circ} 47^{\prime} 40^{\prime \prime}$ and $A B C=321^{\circ} 33^{\prime} 50^{\prime \prime}$. The coordinates of the points $A, B$ and $C$ are calculated as follows :

To Determine $A$.
Check.

| Length o $A=377.92$Bearing $o A=47^{\circ} 19^{\prime}$ | (By logarithms.) |  | (By nat. sines and cosines.) |  |
| :---: | :---: | :---: | :---: | :---: |
|  | =2.5773999 | =2.5773999 | 37792 | 37792 |
|  | S=9.8311493 | $\sin =9.8663922$ | 78776 | 81537 |
|  |  |  | 22675 | 26454 |
|  | 2.4085492 | 2.4437921 | 2645 | II34 |
|  | +256.18 | +277.84 | 265 | 189 |
|  | $0= \pm 0.00$ | $\pm \quad 0.00$ | 33 | 7 |
|  | $A=+256.18$ | +277.84 | 256.18 | 277.84 |

[^46]| Length $A B=1015.74=3.0067826=3.0067826$ | Check. |  |
| :---: | :---: | :---: |
| Bearing $A 0=227^{\circ} 19^{\prime} 20^{\prime \prime}$ | 101574 | 101574 |
| Angle oAB $=83^{\circ} 47^{\prime} 40^{\prime \prime}$ | 495756 | 75337 |
| Bearing $A B=\overline{311^{\circ} 7^{\prime} 00^{\prime \prime}} \sin =9.817958 \mathrm{I} \cos =9.8770096$ | 60944 | 71102 |
| $2.8247407 \quad 2.8837922$ | 5079 | 5079 |
|  | 711 | 305 |
| $+667.95 \quad-765.23$ | 61 | 37 |
| $A=+256.18 \quad+277.84$ | +667.95 | 765.23 |
| $B=+924.13 \quad-487.39$ | +924.13 | 487.39 |

To Determine $C$.


The bearing of a line $=$ that of the backsight + its angle with reference to the backsight (measured clockwise, from left to right); and the bearing of the line used as a backsight differs by $180^{\circ}$ from its bearing when a foresight. For example, in the above calculations the bearing of the line $o A$ is $47^{\circ} 19^{\prime} 20^{\prime \prime}$; therefore, when used as a backsight from the station $A$, its bearing is $47^{\circ} 19^{\prime} 20^{\prime \prime}+180^{\circ}=227^{\circ} 19^{\prime} 20^{\prime \prime}$, which, added to the observed angle $o A B$ which $A o$ makes with $A B$, gives the bearing of the line $A B$.

Similarly the bearing $B C=\left(\right.$ the bearing $\left.A B-180^{\circ}\right)+$ the angle $A B C$, which sum, being greater than $360^{\circ}$, has that amount deducted from it. A bearing is denoted by the prefix $y$. For example, $y A B$ signifies the bearing of the line $A B$, or its direction with reference to $y$ (the true north, $\circ^{\circ}$ ).

If the bearing of a line be in the ist quadrant, its length $\times$ the cosine of the bearing is the $y$ distance or latitude, ., $\times$ the sine " " $x$, departure ;
if in the 2 nd quadrant, its length $\times$ the sine of the (bearing $-90^{\circ}$ ) is the $y$ distance or lat., " $\times$ the cosine , ,. $x$., departure ;
if in the 3 rd quadrant,
its length $\times$ the cosine of the (bearing $-180^{\circ}$ ) is the $y$ distance or lat.,
" $\times$ the sine ", $\quad x$, departure; and if in the 4th quadrant, its length $x$ the sine of the (bearing $-270^{\circ}$ ) is the $y$ distance or lat., " $\times$ the cosine ", $\quad$, departure.
To coordinate any point $B$ which has been fixed from a coordinated point $A$, the $y$ and the $x$ distances of $B$ from $A$ are added algebraically to the coordinates of $A$. For example, in the foregoing calculations the $y$ distance $A B=+667.95$, and the $x$ distance $A B=-765.23$, which, when added alge braically to the coordinates of $A$, give the coordinates of $B$ with reference to the point of origin $o$.

Method used in calculating the length and bearing of a line connecting two coordinated points:

|  | Check. |  |
| :---: | :---: | :---: |
| $A=+256.18+277.84$ | 101574 | 101574 |
| $B=+924.13-487.39$ | 495756 | 73357 |
| Diff. $=+667.95-765.23$ | 60944 | 71102 |
|  | 5079 | 5079 |
|  | 711 | 305 |
|  | 61 | 37 |
| $667.95=2.8247440$ | $\underline{+667.95}$ | -765.23 |
| $765.23=2.8837920$ |  |  |
| $\begin{array}{r} 9 \cdot \overline{9409320}=\tan 41^{\circ} 7^{\prime} 00^{\prime \prime} \\ 270^{\circ} 0^{\prime} 00^{\prime \prime} \end{array}$ |  |  |
|  |  |  |
| cosine $41^{\circ} 7^{\prime} 00^{\prime \prime}=9.8770096$ | $311^{\circ} 7^{\prime} 00^{\prime \prime}=$ |  |
| (Subtracted from $\log 765.23) \frac{1}{3.0067824}=1015.74=$ length $A B$. |  |  |

The signs before the $y$ and $x$ differences of the coordinates of the two points indicate the quadrant in which the bearing of the connecting line lies. Divide the $y$ difference by the $x$ difference. Then:

$$
y \text { difference }=\left\{\begin{array}{llll}
\text { the cotangent of the bearing } & \text { if in the ist quadrant. } \\
\text { the tangent of (the bearing } \left.-90^{\circ}\right) & , & \text { 2nd } \\
\text { the cotangent of ( } & " \\
\text { the tangent of } & \left(180^{\circ}\right) & " & 3 \text { rd }
\end{array}\right.
$$

For example, in the foregoing calculation, as the differences carry the signs +- , the bearing is in the 4 th quadrant. Consequently $\frac{667.95}{765.23}=$ the tangent of $4 \mathrm{I}^{\circ} 7^{\prime} \circ 0^{\prime \prime}$, which, $+270^{\circ},=311^{\circ} 7^{\prime} \circ 0^{\prime \prime}=y \mathrm{AB}$.

The distance between the two points $=$
$\frac{y \text { difference }}{\text { cosine of the bearing }}$
or $\frac{x \text { difference }}{\text { sine of the bearing }}$
if the bearing be in the ist quadrant.

$$
\frac{y \text { difference }}{\text { the sine of (the bearing } \left.-90^{\circ}\right)} \text { or } \frac{x \text { difference }}{\text { cosine of (the bearing } \left.-90^{\circ}\right)}
$$

if the bearing be in the $2 n d$ quadrant.

$$
\frac{y \text { difference }}{\text { cosine of }\left(\text { the bearing }-180^{\circ}\right)} \text { or } \frac{x \text { difference }}{\text { sine of (the bearing } \left.-180^{\circ}\right)}
$$

if the bearing be in the 3 rd quadrant.

$$
\frac{y \text { difference }}{\text { sine of (the bearing }-270^{\circ} \text { ) }} \quad \text { or } \frac{x \text { difference }}{\operatorname{cosine} \text { of (the bearing }-270^{\circ} \text { ) }}
$$

if the bearing be in the 4 th quadrant.
For example, in the foregoing calculation the bearing is in
 length of the line $A B$.

## Method used in calculating the coordinates of a triangulation.



Fig. 2.
Given the coordinates of the points $A$ and $C$, and by observation the interior angles of the triangle $A B C$. Required the coordinates of the point $B$.

$$
\begin{array}{lc}
\text { Angles. } & \text { Coordinates. } \\
A=72^{\circ} 15^{\prime} 30^{\prime \prime} & y \\
B=51^{\circ} 55^{\prime} 40^{\prime \prime} & A=+7230.91+538.64 \\
C=55^{\circ} 48^{\prime} 50^{\prime \prime} & C=+8522.77+9367.05
\end{array}
$$

The first step is to determine the length and bearing of the line $A C$ :

| $A=+7230.91+538.64$ | Check. |  |
| :---: | :---: | :---: |
| $C=+8522.77+9367.05$ | 892243 | 892243 |
| +1291.86+8828.41 | 887441 | 364989 |
|  | 89224 | 803019 |
| 3.1112155 | 35690 | 71379 |
| 3.9458825 | 3569 | 8030 |
| 9.1653330 $=8 \mathrm{I}^{\circ} \cdot 40^{\prime} 30^{\prime \prime}=y A C$ | 625 | 357 |
| 9.9953994 | 78 | 56 |
| $3.950483 \mathrm{I}=8922.43=A C$. | +1291.86 | 8828.41 |

The coordinates of $B$ are then determined from the two sides $A B$ and $C B$, each calculation acting as a check on the other. The lengths of these sides are:
$A B=A C$ sine $C$ cosecant $B$, and $B C=A C$ sine $A$ cosecant $B$; and their bearings are derived from the known bearing $y A C$, and the observed angles of the triangle. The logarithm of the cosecant of $B$ is got by subtracting the logarithm of the sine from 10.0000000 . This is most easily done by subtracting each figure from 9, except the right-hand one, which is subtracted from 10.


The method of calculating the lengths of the sides $A B$ and $C B$ is not clear in the finished calculation. It is as follows: First, to determine the length $A B$,

$$
\begin{aligned}
\log 8922.43 & =3.9504832 \\
\operatorname{cosec} B & =0.1038961 \\
\sin A & = \\
\sin C & =9.9176193 \\
\log A B & =3.9719986
\end{aligned}
$$

the space for the $\log \sin A$ being left blank. Then, to determine the length $C B, \log \sin A$ is filled in, and the sum of the three top $\operatorname{lines}=\log C B$, which is placed to the right of the repeated $\log A B$.

Then, as already described, $A B \times$ the $\cos$ and $\sin$ of $y A B$ (ist quadrant) $=$ the latitude and departure of $B$ from $A$; and $C B \times$ the $\sin$ and $\cos$ of $y C B-270^{\circ}$ (4th quadrant) $=$ the latitude and departure of $B$ from $C$.

## Calculation of the area of a figure from its coordinates.

$$
\text { Area }=\frac{\text { sums of the } y \mathrm{~s} \times \text { diffs. of the } x \mathrm{~s}}{2} \text { or } \frac{\text { sums of the } x \mathrm{~s} \times \text { diffs. of the } y \mathrm{~s}}{2}
$$

The sum and difference of the coordinates of each two adjoining points is taken separately, and the sum of the products is divided by 2 , care being taken to distinguish between the positive and the negative signs when making the addition. The computation is checked by calculating by each way separately, using either 'sho:t' multiplication or logarithms as preferred, the former method being the more accurate for dealing with large amounts.

For example, in the triangle $A B C$ we have the coordinates :

$$
\begin{array}{cc}
y & x \\
A=+7230.91+538.64 \\
B=+16480.16+2072.61 \\
C=+8522.77+9367.05
\end{array}
$$

$$
\begin{aligned}
& \text { Sums of the } y \mathrm{~s} \text {. Diffs. of the } x \text { s. } \\
& A B+23711.07 \times+1533.97=+36,372,070.04 \\
& B C+25002.93 \times+7294.44=+182,382,372.71 \\
& C A+15753.68 x-8828.4 \mathrm{I}=-139,079,946.05 \\
& +79,674,496.70 \\
& \div 2=39,837,248.35
\end{aligned}
$$

## Check.

$$
\begin{aligned}
& \text { Sums of the } x \text { s. Diffs. of the } y \text { ys. } \\
& A B+26 \text { II.25x+9249.25 }=+24,152,104.06 \\
& B C+11439.66 \times-7957.39=-91,029,836.09 \\
& C A+9905.69 x-1291.86=\frac{-12,796,764.68}{-79,674,496.69} \\
& \div 2=39,837,248.35
\end{aligned}
$$

Area $A B C=39,837,248.35$ square units.
The calculation of an area may often be simplified by deducting either a positive or a negative constant from each of the $y \mathrm{~s}$, and similarly, another positive or negative constant from each of the $x \mathrm{~s}$.

For example, in the foregoing calculation $+7000 y$ and $+500 x$ may be deducted from the coordinates of $A, B$ and $C$, giving:

|  | $\begin{gathered} y \\ A=+230.91+c \\ B \end{gathered}=+9480.16+1572.61$ |
| :---: | :---: |
|  | Sums of the $y \mathrm{y}$. Diffs. of the $x$ s. |
| $A B$ | + $9711.07 \times+1533.97=+14,896,490.05$ |
| $B C$ | + $111002.93 \times+7294.44=+80,260,212.71$ |
| $C A$ | $+1753.68 \times-8828.41=-15,482,206.05$ |
|  | +79,674,496.71 |
|  | $\div 2=39,837,248.35$ |

## Check.

Sums of the $x$ s. Diffs. of the $y$ s.
$A B+1611.25 \times+9249.25=+14,902,854.06$
$B C+10439.66 x-7957.39=-83,072,446.08$
$C A+8905.69 x-1291.86=-11,504,904.68$
$-79,674,496.70$
$\div 2=39,837,248.35$
Area $A B C=39,837,248.35$ square units.

Calculation of the coordinates of a point, the angles which it makes with three coordinated points having been observed.

Given the coordinates of the points $A, C$ and $B$, and the observed angles $A R C$ and $B R C$ which subtend these points at $R$. Required the coordinates of the point $R$ (Fig. 3).

Describe a circle cutting $A, B$ and $R$. Join $R A, R B, R C$
and $A B$. Produce $R C$ to the circumference of the circle at $D$, and join $A D$ and $B D$. Then :
the observed angle $A R D=$ the angle $A B D$ and the observed angle $B R D=$ the angle $B A D$,
as they subtend the same chords $A D$ and $B D$. Determine the length and bearing of $A B$ and coordinate $D$ from the triangle $A B D$. Then calculate the bearing $y C D$ which $=$ the bearing $y R D$. Determine $y R A$ and $y R B$ from $y R C$ and the angles $A R D$ and $B R D$, and coordinate $R$ from the triangle $A B R$.

It is apparent that the calculation will not be accurate when the middle point $C$ is close to the circumference of the circle,


Fig. 3.
and quite impossible when $C$ is cut by the circle. It is therefore advisable to first add the observed angles $A R C$ and $B R C$ to the known angle $A C B$; if their sum be $180^{\circ}$, all four points will be cut by the circle, as the opposite angles of a quadrilateral inscribed within a circle are together equal to $180^{\circ}$. Therefore, when the sum of the angles $A R C, B R C$ and $A C B$ is more than $180^{\circ}, C$ is inside the circle and $y C D=y R D$; and when it is less than $180^{\circ}, C$ is outside the circle and $y C D=y D R$.
$R$ may also be calculated by the following formula:
Let $T=(\angle R B C+\angle R A C)=360^{\circ}-(\angle A C B+\angle A R C+\angle B R C)$.
When $T$ is $90^{\circ}$ or under,

$$
\operatorname{cotan} R B C=\operatorname{cotan} T\left(\frac{B C \sin A R C}{A C \sin B R C \cos T}+\mathrm{I}\right)
$$

When $T$ is between $90^{\circ}$ and $180^{\circ}$, the I in the formula is negative instead of positive, thus:

$$
\operatorname{cotan} R B C=\operatorname{cotan} T\left(\frac{B C \sin A R C}{A C \sin B R C \cos T}-\mathrm{I}\right)
$$

$R$ is then coordinated from the triangle $C B R$.

## The Cape System.

In South Africa, a method of coordination which is known as the Cape System is in general use. It differs from the conventional method in that the $x$ axis is positive to the west, which is taken as $360^{\circ}$ or $0^{\circ}$, and the bearings are therefore stated with reference to the west instead of to the north, the bearing of a line being consequently denoted by the prefix $x$ instead of $y$. It is best explained by the following diagram :


The methods of calculation are similar to those already described, but the arrangement of the quadrants is of course quite different. Therefore, if the bearing of a line be :
In the Ist quadrant, $\left\{\begin{array}{c}\text { its length } \times \text { the sin of the bearing is the } y \text { distance. } \\ \# \times, \ldots \cos , \#, ~\end{array}\right.$


In determining the length and bearing of a line between two coordinated points :

$$
\begin{aligned}
& \text { Length }=\frac{y \text { difference }}{\sin \text { of bearing }} \quad \text { or } \quad \frac{x \text { difference }}{\cos \text { of bearing }} \text { if in the ist quadrant. } \\
& ,=\frac{y \text { difference }}{\left.\cos \text { of (bearing }-90^{\circ}\right)} \text { or } \frac{x \text { difference }}{\left.\sin \text { of (bearing }-90^{\circ}\right)} \quad, \quad \text { 2nd } \quad, \\
& ,,=\frac{y \text { difference }}{\sin \text { of }\left(\text { bearing }-180^{\circ}\right)} \text { or } \frac{x \text { difference }}{\left.\cos \text { of (bearing }-180^{\circ}\right)} \quad, \quad 3 \text { rd } \quad, \\
& ,=\frac{y \text { difference }}{\cos \text { of }\left(\text { bearing }-270^{\circ}\right)} \text { or } \frac{x \text { difference }}{\left.\sin \text { of (bearing }-270^{\circ}\right)} \quad \text {, 4th },
\end{aligned}
$$

# SECTION III. THE COMPARISON AND VERIFICATION OF STANDARD MEASURES OF LENGTH. 

r. The following measures of length can be tested by the Board of Trade Standards Department, Westminster :

Metal measures in the form of 'ribands' or 'tapes':

$$
\begin{aligned}
& 100 \text { links or } 66 \text { feet. } \\
& 50 \text { links or } 33 \text { feet. } \\
& \text { 100 feet. } \\
& 50 \text { feet. } \\
& 25 \text { feet. } \\
& 20 \text { metres. } \\
& 10 \text { metres. }
\end{aligned}
$$

2. The whole or total length only of each of the above measures will be tested, except in the case of a standard measure required for survey purposes, when the corrected values of each part or interval of the measure will be given, $e g$. every 5 metres on 20 metres, or every 10 feet on 100 feet.
3. Unless otherwise required, each measure will be tested under the following condition as to normal tension, 'pull,' or
stretching-weight, when the measure under test is supported throughout its whole length on a plane and even base:

|  | Metal Measures. |
| :---: | :---: |
| $\left.\begin{array}{l}\left.\begin{array}{l}100 \text { link riband } \\ 100 \text { feet to } 50 \text { feet - } \\ 20 \text { metres }- \\ 10 \text { metres }- \\ 10- \\ \hline\end{array}\right\}\end{array}\right\}$ | io lb. avoir. <br> 5 kilograms. |

Linked chains, or round-wire chains composed of links and rings and tapes made of linen or other fabric are only verified for certain official purposes.
4. All results are reduced to $62^{\circ} \mathrm{F}$. for links and feet and to $0^{\circ} \mathrm{C}$. for metres.

The coefficient of linear expansion of a metal measure is taken to be as follows, unless otherwise stated:

|  | For $\mathrm{x}^{\circ} \mathrm{F}$ | For $\mathrm{I}^{\circ} \mathrm{C}$ |
| :--- | :--- | :--- |
| Steel - <br> 'Invar' or Nickel Steel <br> (35.7 Nickel, 64.3 Steel.) | 0.00000689 | 0.00001240 |

5. The following design of stamp or mark of verification (including the year) is placed on a verified measure:


Metal measures should have a brass disc ( $\frac{1}{2}$-inch diameter) affixed upon which to place the official stamp.
6. In certain cases Treasury fees are required, particulars of which can be obtained at the Standards Office. Fees are not payable on measures for Government Departments or for Local Authorities.

A certificate of verification is given with each measure, in which its error or difference from Standard is stated, and also, in some instances, the modulus of elasticity and 'sag' of a chain.

In standard steel tapes for the use of local Inspectors of Weights and Measures an error in manufacture of 0.1 inch is allowed in excess or deficiency. In other steel standards 0.25 inch is allowed, and in linen tapes 0.5 inch is permitted.

Metric measures should be accurate to about 5 millimetres in 20 metres or to one four-thousandth of the whole length. The verification of measures can be carried out to nearly one four-thousandth part of the whole length.

The above regulations were issued by the Board of Trade Standards Department on the ist of August, 1904.

## SECTION IV. TACHEOMETRY.

## The Use of the Tacheometer in Contouring.

For accurate contouring, a sufficient number of stations should be flagged so that any part of the ground is not more than about 1200 feet distant from at least one station, this being about the limit for accurate reading with the usual 5 -inch instrument. The levels of the stations should then be determined, and their positions fixed by triangulation in the following manner. When the instrument is levelled up over a station, set it so that the clamped bottom plate has always the same position relative to the true or to the magnetic meridian. This is done by clamping the top plate at the known bearing which the instrument station makes with the back-sight, and then directing the telescope on the back sight with the bottom plate unclamped. The bearing of each sight can thus be booked direct, which saves time in plotting. The angles to all the fixed stations to be located by triangulation should be carefully read and booked before any staff readings are taken. With one man observing and another booking, two or even three staff men can be kept going. Great care should be insisted on in the holding of the staffs perpendicularly, more especially at a point above or below the level of the instrument station, where the sight has to be taken with an inclined telescope. The form of field book given on the following page is recommended.

A pocket steel tape 6 feet long, in a circular metal case and winding up by means of a spring, will be found very convenient for measuring the height of the instrument. In setting up at a
Specimen Page of Field Book.

| $\begin{aligned} & \text { Inst. } \\ & \text { Stn. } \end{aligned}$ | $\begin{gathered} \text { Hght. } \\ \text { Inst. } \end{gathered}$ | Sighted <br> Stn. <br> S. | Bearing. | Vert. Angle | Wires. | Distances. |  |  | Rise. | Fall. | Axis Level | Red. <br> Level. | Remaris. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Slope. | Hor. | Vert. |  |  |  |  |  |
| $\triangle B$ | 4.54 |  |  |  |  |  |  |  |  |  | +91.89 | $+87.35$ |  |
|  |  | 1 | $73^{\circ} 15^{\prime}$ | $83^{\circ} 40^{\prime}$ | $\begin{array}{r} 10.87 \\ 9.00 \\ 7.13 \end{array}$ | 374 | 369.45 | +41.01 | 32.01 |  |  | +123.90 |  |
|  |  | 2 | $129^{\circ} 43^{\prime}$ | level. | 8.95 7.21 5.47 |  | 348 |  |  | 7.21 |  | $+84.68$ |  |
|  |  | 3 | $4^{\circ} 18^{\prime}$ | $94^{\circ} 21^{\prime}$ | 10.48 9.00 7.52 | 296 | 294.06 | $-23.92$ |  | 32.92 |  | $+58.97$ |  |

station, first level up, then take height of instrument (from centre of telescope axis to top of peg), then set bottom plate to correct bearing as already described. Take sights with a level telescope where possible, so as to save calculation in the office. Book the readings of the top, middle and bottom wires in the same column. When sighting to the rise or dip, bring the middle wire on to the same even number on the staff whenever possible, as an error in the reading of the top or bottom wire can then be easily detected when booking, and there is less liability to error in working out reduced levels. For instance, on sighting an ordinary 16 feet level staff, keep cutting the 9 foot mark with the middle wire, then the sum of the top and bottom wire readings should always be $9 \times 2=18$, and the 'Rise' or 'Fall' is more easily calculated. In the office first get the slope distance from the wire readings, then work out the horizontal and vertical readings by multiplying by the constants given in the table on pages 141-171. Enter them up, putting a + sign before the vertical distance for a rise, and a - sign for a fall. Then fill in the Axis Level, which is the Reduced Level + the height of the instrument. In case of a rise (see Sighted Station I in field book) subtract the middle wire reading from the Vertical Distance and book the result in the 'Rise' column. With a level telescope (see Sighted Station 2 in field book) enter the middle wire reading in the 'Fall' column. In case of a fall (see Sighted Station 3 in field book) add the middle wire reading to the Vertical Distance and book result in the 'Fall' column. Although in the specimen page everything is worked out to two decimal places, it is usual to work the Horizontal Distance to the nearest foot, which is sufficiently accurate for plotting.

Corrections for Curvature and Refraction.

| Distance. | Correction. | Distance. | Correction. | Distance. | Correction. |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| 300 | .002 | 800 | .013 | 1300 | .035 |
| 400 | .003 | 900 | .017 | 1400 | .040 |
| 500 | .005 | 1000 | .020 | 1500 | .046 |
| 600 | .007 | 1100 | .025 | 1600 | .052 |
| 700 | .010 | 1200 | .030 | 1700 | .059 |

In + or rise angles, add the correction to the amount of rise in ' Rise' column. In level distances, book the correction in the 'Rise' column. In - or dip angles, deduct correction from amount of fall in 'Fall' column.

The stadia wires of a tacheometer are usually set to a 'measuring angle' twice the tangent of the half of which is 0.01 , i.e., the distance between the wires as read on the staff is 0.01 of the actual distance between the staff and the instrument, and consequently the difference between the top and bottom wire readings $\times 100=$ the slope distance. Tacheometer telescopes are now made with an 'anallatic lens,' by which the stadia readings are referred to the centre of the instrument. If a telescope which is not 'anallatic' be used, a correction for 'focal length' has to be applied to all the readings.

The vertical circles of most tacheometers are graduated so that with a level telescope the right hand vernier is at $90^{\circ}$ and the left hand vernier at $270^{\circ}$, with $360^{\circ}$ at the tangent screw. Therefore a rise angle reads less, and a dip angle more than $90^{\circ}$ on the right hand vernier, which is the one usually read. The following table is arranged for instruments of this type, but with an instrument where the actual rise or dip angle is read direct, add $90^{\circ}$ when looking up the constants for the angle.

The horizontal distance and the difference in height are calculated from the slope distance and the vertical angle as follows :

Let $G=$ the slope distance, or 'generating number.'
$V=$ the vertical angle, or inclination of $G$ from the horizontal.
$D=$ the horizontal distance.
$H=$ the vertical distance, or difference in height.
Then $D=G \cos ^{2} V$
and $H=G \sin V \cos V$.*
The following table gives the values of $\cos ^{2} V$ and $\sin V \cos V$ for each minute of arc from $0^{\circ}$ to an inclination of $30^{\circ}$ from the horizontal.

Rule: Multiply the slope distance by the constants given in the table for the vertical angle.

$$
{ }^{*} H=D \tan V
$$

Table for the Calculation of Heights and Distances from Tacheometer Readings.

90 Degrees.

| Minutes. | Constant for <br> Distance. | Constant for Difference in Height. |  | Minutes. | Constant for Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1.0000 | . 0000 | 60 | 30 | . 9999 | . 0087 | 30 |
| 1 | 1.0000 | . 0003 | 59 | 31 | . 9999 | . 0090 | 29 |
| 2 | 1.0000 | . 0006 | 58 | 32 | . 9999 | . 0093 | 28 |
| 3 | 1.0000 | . 0009 | 57 | 33 | . 9999 | . 0096 | 27 |
| 4 | 1.0000 | . 0012 | 56 | 34 | . 9999 | . 0099 | 26 |
| 5 | 1.0000 | . 0015 | 55 | 35 | . 9999 | . 0102 | 25 |
| 6 | 1.0000 | . 0018 | 54 | 36 | . 9999 | . 0105 | 24 |
| 7 | 1.0000 | . 0020 | 53 | 37 | . 9999 | . 0108 | 23 |
| 8 | 1.0000 | . 0023 | 52 | 38 | . 9999 | . 0111 | 22 |
| 9 | 1.0000 | . 0026 | 51 | 39 | . 9999 | .OII3 | 21 |
| 10 | 1.0000 | . 0029 | 50 | 40 | . 9999 | . 0116 | 20 |
| II | 1.0000 | . 0032 | 49 | 41 | . 9999 | . 0119 | 1.9 |
| 12 | 1.0000 | . 0035 | 48 | 42 | . 9999 | . 0122 | 18 |
| 13 | 1.0000 | . 0038 | 47 | 43 | . 9998 | . 0125 | 17 |
| 14 | 1.0000 | . 0041 | 46 | 44 | . 9998 | . 0128 | 16 |
| 15 | 1.0000 | . 0044 | 45 | 45 | . 9998 | . 0131 | 15 |
| 16 | 1.0000 | . 0047 | 44 | 46 | . 9998 | . 0134 | 14 |
| 17 | 1.0000 | . 0050 | 43 | 47 | . 9998 | . 0137 | 13 |
| 18 | 1.0000 | . 0052 | 42 | 48 | . 9998 | . 0140 | 12 |
| 19 | 1.0000 | . 0055 | 4 I | 49 | . 9998 | . 0143 | 11 |
| 20 | 1.0500 | . 0058 | 40 | 50 | . 9998 | . 0145 | 10 |
| 21 | 1.0000 | . 0061 | 39 | 51 | . 9998 | . 0148 | 9 |
| 22 | 1.0000 | . 0064 | 38 | 52 | . 9998 | . 0151 | 8 |
| 23 | 1.0000 | . 0067 | 37 | 53 | . 9998 | .OI 54 | 7 |
| 24 | 1.0000 | .0070 | 36 | 54 | . 9998 | . OI 57 | 6 |
| 25 | 1.0000 | . 0073 | 35 | 55 | . 9997 | . 0160 | 5 |
| 26 | . 9999 | . 0076 | 34 | 56 |  | . 0163 | 4 |
| 27 | . 9999 | . 0079 | 33 | 57 | . 9997 | . 0166 | 3 |
| 28 | . 9999 | .008I | 32 | 58 | . 9997 | . 0169 | 2 |
| 29 | . 9999 | . 0084 | 3 I | 59 | . 9997 | . 0172 | 1 |
| 30 | . 9999 | .0087 | 30 | 60 | . 9997 | . 0175 | 0 |
|  | Constant for Distance. | Constant for Difference in Height. | Minutes. |  | Constant for <br> Distance. | Constant for Difference in Height. | Minutes. |

89 Degrees.

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Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

91 Degrees.

| Minutes. | Constant for <br> Distance. | Constant for Difference in Height. |  | Minutes. | Constant for <br> Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 9997 | . 0175 | 60 | 30 | -9993 | -0262 | 30 |
| 1 | . 9997 | .or 77 | 59 | 31 | . 9993 | . 0265 | 29 |
| 2 | . 9997 | . 0180 | 58 | 32 | . 9993 | . 0268 | 28 |
| 3 | . 9997 | . 0183 | 57 | 33 | -9993 | . 0270 | 27 |
| 4 | . 9997 | . 0186 | 56 | 34 | -9993 | . 0273 | 26 |
| 5 | . 9996 | . 0189 | 55 | 35 | . 9992 | . 0276 | 25 |
| 6 | . 9996 | . 0192 | 54 | 36 | . 9992 | . 0279 | 24 |
| 7 | . 9996 | . 0195 | 53 | 37 | . 9992 | . 0282 | 23 |
| 8 | . 9996 | . 19198 | 52 | 38 | . 9992 | . 0285 | 22 |
| 9 | . 9996 | . 0201 | 51 | 39 | . 9992 | . 0288 | 21 |
| 10 | . 9796 | . 0204 | 50 | 40 | . 9992 | . 0291 | 20 |
| 11 | . 9996 | . 0207 | 49 | 41 | . 9991 | . 0294 | 19 |
| 12 | . 9996 | . 0209 | 48 | 42 | .9991 | . 0297 | 18 |
| 13 | . 9995 | . 0212 | 47 | 43 | .9991 | . 0300 | 17 |
| 14 | . 9995 | . 0215 | 46 | 44 | . 9991 | . 0302 | 16 |
| 15 | . 9995 | . 0218 | 45 | 45 | .9991 | . 0305 | 15 |
| 16 | -9995 | . 0221 | 44 | 46 | . 9991 | . 0308 | 14 |
| 17 | . 9995 | . 0224 | 43 | 47 | . 9990 | . 0311 | 13 |
| 18 | . 9995 | . 0227 | 42 | 48 | . 9990 | . 0314 | 12 |
| 19 | . 9995 | . 0230 | 41 | 49 | . 9990 | . 0317 | 11 |
| 20 | . 9995 | . 0233 | 40 | 50 | . 9990 | . 0320 | 10 |
| 21 | . 9994 | . 0236 | 39 | 51 | . 9990 | . 0323 | 9 |
| 22 | . 9994 | . 0238 | 38 | 52 | . 9989 | . 0326 | 8 |
| 23 | . 9994 | . 0241 | 37 | 53 | . 9989 | . 0328 | 7 |
| 24 | . 9994 | . 0244 | 36 | 54 | . 9989 | . 0331 | 6 |
| 25 | . 9994 | . 0247 | 35 | 55 | . 9989 | . 0334 | 5 |
| 26 | . 9994 | . 0250 | 34 | 56 | . 9989 | . 0337 | 4 |
| 27 | . 9994 | . 0253 | 33 | 57 | . 9988 | . 0340 | 3 |
| 28 | . 9994 | . 0256 | 32 | 58 | . 9988 | . 0343 | 2 |
| 29 | . 9993 | . 0259 | 31 | 59 | . 9988 | . 0346 | 1 |
| 30 | . 9993 | . 0262 | 30 | 60 | . 9988 | . 0349 | 0 |
|  | Constant for fistance <br> Distance. | $\begin{gathered} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{gathered}$ | Minutes. |  | Constant <br> Distan <br> Distance. | Constant for Difference in Height. | Minutes. |

88 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

92 Degrees.

| Minutes. | Constant Distar <br> Distance. | Constant for Difference in Height. |  | Minutes. | $\begin{gathered} \text { Constant } \\ \text { for } \\ \text { Distance. } \end{gathered}$ | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 9988 | . 0349 | 60 | 30 | . 998 r | . 0436 | 30 |
| 1 | . 9988 | . 0352 | 59 | 31 | .9981 | . 0439 | 29 |
| 2 | . 9987 | . 0355 | 58 | 32 | . 9981 | . 0442 | 28 |
| 3 | . 9987 | . 0358 | 57 | 33 | . 9980 | . 0445 | 27 |
| 4 | . 9987 | . 0360 | 56 | 34 | . 9980 | . 0447 | 26 |
| 5 | . 9987 | . 0363 | 55 | 35 | . 9980 | . 0450 | 25 |
| 6 | . 9987 | . 0366 | 54 | 36 | . 9980 | . 0453 | 24 |
| 7 | . 9986 | . 0369 | 53 | 37 | . 9979 | . 0456 | 23 |
| 8 | . 9986 | . 0372 | 52 | 38 | . 9979 | . 0459 | 22 |
| 9 | . 9986 | . 0375 | 51 | 39 | . 9979 | . 0462 | 21 |
| 10 | . 9986 | . 0378 | 50 | 40 | . 9978 | . 0465 | 20 |
| 11 | . 9986 | .038r | 49 | 41 | . 9978 | . 0468 | 19 |
| 12 | . 9985 | . 0384 | 48 | 42 | . 9978 | . 0471 | 18 |
| 13 | . 9985 | . 0387 | 47 | 43 | . 9978 | . 0474 | 17 |
| 14 | . 9985 | . 0389 | 46 | 44 | . 9977 | . 0476 | 16 |
| 15 | . 9985 | . 0392 | 45 | 45 | . 9977 | . 0479 | 15 |
| 16 |  |  |  | 46 |  |  | 14 |
| 17 | . 9984 | . 0398 | 43 | 47 | . 9976 | . 0485 | 13 |
| 18 | . 9984 | . 0401 | 42 | 48 | . 9976 | . 0487 | 12 |
| 19 | . 9984 | . 0404 | 41 | 49 | . 9976 | . 0491 | 11 |
| 20 | . 9983 | . 0407 | 40 | 50 | . 9976 | . 0494 | 10 |
| 21 | . 9983 | . 0410 | 39 | 51 | -9975 | . 0497 | 9 |
| 22 | . 9983 | .04:3 | 38 | 52 | . 9975 | . 0500 | 8 |
| 23 | . 9983 | . 0416 | 37 | 53 | . 9975 | . 0502 | 7 |
| 24 | . 9983 | . 0418 | 36 | 54 | . 9974 | . 0505 | 6 |
| 25 | . 9982 | . 0421 | 35 | 55 | . 9974 | . 0508 | 5 |
| 26 | . 9982 | . 0424 | 34 | 56 | . 9974 | . 0511 | 4 |
| 27 | . 9982 | . 0427 | 33 | 57 | . 9974 | . 0514 | 3 |
| 28 | . 9982 | . 0430 | 32 | 58 | . 9973 | . 0517 | 2 |
| 29 | . 9988 | . 0433 | 31 | 59 | . 9973 | . 0520 | I |
| 30 | .9981 | . 0436 | 30 | 60 | . 9973 | . 0523 | $\bigcirc$ |
|  | Constant for <br> Distance. | $\begin{gathered} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{gathered}$ | Minutes |  | Constant for <br> Distance. | Constant for Difference in Height. | Minutes |

87 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

93 Degrees.

| Minutes. | $\begin{aligned} & \text { Constant } \\ & \text { fir } \\ & \text { Distance. } \end{aligned}$ | Constant for Difference in Height. |  | Minutes. | Constant Distanc Distance. | $\left\|\begin{array}{c} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{array}\right\|$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcirc$ | . 9973 | . 0523 | 60 | 30 | . 9963 | . 0609 | 30 |
| 1 | . 9972 | . 0526 | 59 | 31 | . 9962 | . 0612 | 29 |
| 2 | . 9972 | . 0529 | 58 | 32 | . 9962 | . 0615 | 28 |
| 3 | . 9972 | .053I | 57 | 33 | . 9962 | . 0618 | 27 |
| 4 | . 9971 | . 0534 | 56 | 34 | . 9961 | . 0621 | 26 |
| 5 | . 9971 | . 0537 | 55 | 35 | .9961 | . 0624 | 25 |
| 6 | -9971 | . 0540 | 54 | 36 | .9961 | . 0627 | 24 |
| 7 | .9971 | . 0543 | 53 | 37 | . 9960 | . 0629 | 23 |
| 8 | .9970 | . 0546 | 52 | 38 | . 9960 | . 0632 | 22 |
| 9 | . 9970 | . 0549 | 51 | 39 | . 9960 | . 0635 | 21 |
| 10 | . 9970 | . 0552 | 50 | 40 | . 9959 | . 0638 | 20 |
| 11 | . 9969 | . 0554 | 49 | 41 | . 9959 | . 0641 | 19 |
| 12 | . 9969 | . 0557 | 48 | 42 | . 9958 | . 0644 | 18 |
| 13 | . 9969 | . 0560 | 47 | 43 | -9958 | . 0647 | 17 |
| 14 | . 9968 | . 0563 | 46 | 44 | . 9958 | . 0650 | 16 |
| 15 | . 9968 | . 0566 | 45 | 45 | . 9957 | . 0653 | 15 |
| 16 | . 9968 | . 0569 | 44 | 46 | . 9957 | . 0656 | 14 |
| 17 | . 9967 | . 0572 | 43 | 47 | . 9956 | . 0658 | 13 |
| 18 | . 9967 | . 0575 | 42 | 48 | . 9956 | . 0661 | 12 |
| 19 | . 9967 | . 0578 | 41 | 49 | . 9956 | . 0664 | 11 |
| 20 | . 9966 | . 0580 | 40 | 50 | . 9955 | . 0667 | 10 |
| 21 | . 9966 | . 0583 | 39 | 51 | . 9955 | . 0670 | 9 |
| 22 | . 9966 | . 0586 | 38 | 52 | . 9955 | . 0673 | 8 |
| 23 | . 9965 | . 0589 | 37 | 53 | . 9954 | . 0676 | 7 |
| 24 | . 9965 | . 0592 | 36 | 54 | . 9954 | . 0679 | 6 |
| 25 | . 9965 | . 0595 | 35 | 55 | . 9953 | . 0682 | 5 |
| 26 | . 9964 | . 0598 | 34 | 56 | . 9953 | . 0684 | 4 |
| 27 | . 9964 | . 0601 | 33 | 57 | . 9953 | . 0687 | 3 |
| 28 | . 9964 | . 0604 | 32 | 58 | . 9952 | . 0690 |  |
| 29 | . 9963 | . 0607 | 31 | 59 | . 9952 | . 0693 | - |
| 30 | . 9963 | . 0609 | 30 | 60 | .9951 | . 0696 | - |
|  | Constant for Distance. | $\begin{gathered} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{gathered}$ | Minutes |  | Constant Distar <br> Distance. | Constant for Difference in Height. | Minutes |

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

## 94 Degrees.

| Minutes. | Constant for Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: |
| $\bigcirc$ | .9951 | . 0696 | 60 |
| 1 | .9951 | . 0699 | 59 |
| 2 | .9951 | . 0702 | 58 |
| 3 | . 9950 | . 0705 | 57 |
| 4 | . 9950 | . 0707 | 56 |
| 5 | . 9949 | . 0710 | 55 |
| 6 | . 9949 | . 0713 | 54 |
| 7 | . 9949 | . 0716 | 53 |
| 8 | . 9948 | . 0719 | 52 |
| 9 | . 9948 | . 0722 | 51 |
| 10 | . 9947 | . 0725 | 50 |
| 11 | . 9947 | . 0728 | 49 |
| 12 | . 9946 | .0731 | 48 |
| 13 | . 9946 | . 0733 | 47 |
| 14 | . 9946 | . 0736 | 46 |
| 15 | . 9945 | . 0739 | 45 |
| 16 | . 9945 | . 0742 | 44 |
| 17 | . 9944 | . 0745 | 43 |
| 18 | . 9944 | . 0748 | 42 |
| 19 | . 9943 | . 0751 | 41 |
| 20 | . 9943 | . 0753 | 40 |
| 21 | . 9943 | . 0756 | 39 |
| 22 | . 9942 | . 0759 | 38 |
| 23 | . 9942 | . 0762 | 37 |
| 24 | -994I | . 0765 | 36 |
| 25 | .994I | . 0768 | 35 |
| 26 | . 9940 | . 0771 | 34 |
| 27 | . 9940 | . 0774 | 33 |
| 28 | . 9939 | . 0776 | 32 |
| 29 | . 9939 | . 0779 | 31 |
| 30 | . 9938 | . 0782 | 30 |
|  | Constant for <br> Distance. | Constant for Difference in Height. | Minutes. |


| Minutes. | Constant Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: |
| 30 | . 9938 | . 0782 | 30 |
| 31 | . 9938 | . 0785 | 29 |
| 32 | . 9938 | . 0788 | 28 |
| 33 | . 9937 | . 0791 | 27 |
| 34 | . 9937 | . 0794 | 26 |
| 35 | . 9936 | . 0797 | 25 |
| 36 | . 9936 | . 0799 | 24 |
| 37 | . 9935 | . 0802 | 23 |
| 38 | . 9935 | . 0805 | 22 |
| 39 | . 9934 | . 0808 | 21 |
| 40 | . 9934 | .0811 | 20 |
| 41 | . 9933 | .0814 | 19 |
| 42 | . 9933 | . 0817 | 18 |
| 43 | . 9932 | . 0820 | 17 |
| 44 | . 9932 | . 0822 | 16 |
| 45 | .993I | . 0825 | 15 |
| 46 | .9931 | . 0828 | 14 |
| 47 | . 9930 | .0831 | 13 |
| 48 | . 9930 | . 0834 | 12 |
| 49 | . 9929 | . 0837 | 11 |
| 50 | . 9929 | . 0840 | 10 |
| 51 | . 9929 | . 0843 |  |
| 52 | . 9928 | . 0845 | 8 |
| 53 | . 9928 | . 0848 | 7 |
| 54 | . 9927 | .0851 | 6 |
| 55 | . 9927 | . 0854 | 5 |
| 56 | . 9926 | . 0857 | 4 |
| 57 | . 9926 | . 0860 | 3 |
| 58 | . 9925 | . 0863 | 2 |
| 59 | . 9925 | . 0865 | 1 |
| 60 | . 9924 | . 0868 | o |
|  | Constant fistan Distance. | Constant for Difference in Heigh | Minutes. |

85 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

95 Degrees.

| Minutes. | Constant Distar Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: |
| o | . 9924 | . 0868 | 60 |
| 1 | . 9924 | .0871 | 59 |
| 2 | . 9923 | . 0874 | 58 |
| 3 | . 9923 | . 0877 | 57 |
| 4 | . 9922 | . 0880 | 56 |
| 5 | . 9922 | . 0883 | 55 |
| 6 | . 9921 | . 0885 | 54 |
| 7 | .9921 | . 0888 | 53 |
| 8 | . 9920 | .0891 | 52 |
| 9 | . 9920 | . 0894 | 51 |
| 10 | . 9919 | . 0897 | 50 |
| 11 | .9918 | . 0900 | 49 |
| 12 | . 9918 | . 0903 | 48 |
| 13 | . 9917 | . 0905 | 47 |
| 14 | . 9917 | . 0908 | 46 |
| 15 | .9916 | . 0911 | 45 |
| 16 | . 9916 | . 0914 | 44 |
| 17 | . 9915 | . 0917 | 43 |
| 18 | . 9915 | . 0920 | 42 |
| 19 | . 9914 | . 0923 | 41 |
| 20 | . 9914 | . 0926 | 40 |
| 21 | . 9913 | . 0928 | 39 |
| 22 | .9913 | .093I | 38 |
| 23 | .9912 | . 0934 | 37 |
| 24 | .9912 | . 0937 | 36 |
| 25 | .991I | . 0940 | 35 |
| 26 | .9910 | . 0943 | 34 |
| 27 | .9910 | . 0946 | 33 |
| 28 | . 9909 | . 0948 | 32 |
| 29 | . 9909 | . 0951 | 31 |
| 30 | . 9908 | . 0954 | 30 |
|  | Constant for Distance | $\begin{gathered} \text { Constant } \\ \text { for } \\ \text { fiference } \\ \text { in Height. } \end{gathered}$ | Minutes. |


| Minutes. | Constant for <br> Distance | $\left\lvert\, \begin{gathered} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{gathered}\right.$ |  |
| :---: | :---: | :---: | :---: |
| 30 | . 9908 | . 0954 | 30 |
| 31 | . 9908 | . 0957 | 29 |
| 32 | . 9907 | . 0960 | 28 |
| 33 | . 9907 | . 0963 | 27 |
| 34 | . 9906 | . 0965 | 26 |
| 35 | . 9905 | . 0968 | 25 |
| 36 | . 9905 | . 0971 | 24 |
| 37 | . 9904 | . 0974 | 23 |
| 38 | . 9904 | . 0977 | 22 |
| 39 | . 9903 | . 0980 | 21 |
| 40 | . 9903 | . 0983 | 20 |
| 41 | . 9902 | . 0985 | 19 |
| 42 | .9901 | . 0988 | 18 |
| 43 | .9901 | . 0991 | 17 |
| 44 | . 9900 | . 0994 | 16 |
| 45 | . 9900 | . 0997 | 15 |
| 46 | . 9899 | . 1000 | 14 |
| 47 | . 9898 | . 1003 | 13 |
| 48 | . 9898 | . 1005 | 12 |
| 49 | . 9897 | . 1008 | 11 |
| 50 | . 9897 | . 101 I | 10 |
| 51 | . 9896 | . 1014 | 9 |
| 52 | . 9896 | . 1017 | 8 |
| 53 | . 9895 | . 1020 |  |
| 54 | . 9894 | . 1023 | 6 |
| 55 | . 9894 | . 1025 | 5 |
| 56 | . 9893 | . 1028 | 4 |
| 57 | . 9893 | . 1031 | 3 |
| 58 | . 9892 | . 1034 | 2 |
| 59 | .9891 | . 1037 | I |
| 60 | .9891 | . 1040 | $\bigcirc$ |
|  | Constant <br> Distance <br> Distance. | Constant for Difference in Height. | Minutes. |

84 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

## 96 Degrees.

| Minutes. | Constant for Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: |
| 0 | .9891 | . 1040 | 60 |
| I | . 9890 | . 1042 | 59 |
| 2 | . 9890 | . 1045 | 58 |
| 3 | . 9889 | . 1048 | 57 |
| 4 | . 9888 | . 1051 | 56 |
| 5 | . 9888 | . 1054 | 55 |
| 6 | . 9887 | . 1057 | 54 |
| 7 | . 9887 | . 1059 | 53 |
| 8 | . 9886 | . 1062 | 52 |
| 9 | . 9885 | . 1065 | 51 |
| 10 | . 9885 | . 1068 | 50 |
| 11 | . 9884 | . 1071 | 49 |
| 12 | . 9883 | . 1074 | 48 |
| 13 | . 9883 | . 1077 | 47 |
| 14 | . 9888 | . 1079 | 46 |
| 15 | .9882 | . 1082 | 45 |
| 16 | . 9881 | . 1085 | 44 |
| 17 | . 9880 | . 1088 | 43 |
| 18 | . 9880 | . 1091 | 42 |
| 19 | . 9879 | . 1094 | 41 |
| 20 | . 9878 | . 1096 | 40 |
| 21 | . 9878 | . 1099 | 39 |
| 22 | . 9877 | . 1102 | 38 |
| 23 | . 9876 | . 1105 | 37 |
| 24 | . 9876 | . 1108 | 36 |
| 25 | . 9875 | . II II | 35 |
| 26 | .9875 | . 1113 | 34 |
| 27 | . 9874 | . II 16 | 33 |
| 28 | . 9873 | . 1119 | 32 |
| 29 | . 9873 | . 1122 | 31 |
| 30 | .9872 | . 1125 | 30 |
|  | Constant for Distance. | Constant for Difference in Height. | Minutes. |


| Minutes. | Constant for Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: |
| 30 | .9872 | . 1125 | 30 |
| 31 | . 9871 | . 1128 | 29 |
| 32 | . 9871 | . 1130 | 28 |
| 33 | . 9870 | . 1133 | 27 |
| 34 | . 9869 | . I 136 | 26 |
| 35 | . 9869 | . 1139 | 25 |
| 36 | . 9868 | . I I42 | 24 |
| 37 | . 9867 | . 1145 | 23 |
| 38 | . 9867 | . 1148 | 22 |
| 39 | . 9866 | . 1150 | 21 |
| 40 | . 9865 | . I I 53 | 20 |
| 41 | . 9865 | . I I 56 | 19 |
| 42 | . 9864 | . II 59 | 18 |
| 43 | . 9863 | . 1162 | 17 |
| 44 | . 9863 | . 1164 | 16 |
| 45 | . 9862 | . 1167 | 15 |
| 46 | .986I | . 1170 | 14 |
| 47 | . 9860 | . I I 73 | 13 |
| 48 | . 9860 | . 1176 | 12 |
| 49 | . 9859 | . 1179 | II |
| 50 | . 9858 | . 1181 | 10 |
| 51 | . 9858 | . 1184 | 9 |
| 52 | . 9857 | .1187 | 8 |
| 53 | . 9856 | . 1190 |  |
| 54 | . 9856 | . 1193 | 6 |
| 55 | . 9855 | . 1196 | 5 |
| 56 | . 9854 | . 1198 | 4 |
| 57 | . 9854 | . I201 | 3 |
| 58 | . 9853 | . 1204 | 2 |
| 59 | . 9852 | . 1207 | I |
| 60 | . 9852 | . 1210 | 0 |
|  | Constant for Distance. | Constant for Difference in Height. | Minutes. |

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DATA RELATING TO SURVEYING [part vi.

Table for the Calculation of Heights and Distances from Tacheometer
Readings-continued.

97 Degrees.

| Minutes. | Constant for Distance. | Constant for Difference in Height. |  | Minutes. | Constant <br> Distar <br> Distance. | Constant Diff Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 9852 | . 1210 | 60 | 30 | . 9830 | . 1294 | 30 |
| 1 | . 9851 | . 1213 | 59 | 31 | . 9829 | . 1297 | 29 |
| 2 | . 9850 | . 1215 | 58 | 32 | . 9828 | . 1300 | 28 |
| 3 | . 9849 | . 1218 | 57 | 33 | . 9827 | . 1303 | 27 |
| 4 | . 9849 | .1221 | 56 | 34 | . 9827 | . 1305 | 26 |
| 5 | . 9848 | . 1224 | 55 | 35 | . 9826 | . 1308 | 25 |
| 6 | . 9847 | . 1227 | 54 | 36 | . 9825 | . 1311 | 24 |
| 7 | . 9847 | . 1229 | 53 | 37 | . 9824 | .1314 | 23 |
| 8 | . 9846 | . 1232 | 52 | 38 | . 9824 | . 1317 | 22 |
| 9 | . 9845 | . 1235 | 51 | 39 | . 9823 | .1319 | 21 |
| 10 | . 9844 | . 1238 | 50 | 40 | . 9822 | . 1322 | 20 |
| 11 | . 9844 | . 1241 | 49 | 41 | . 9821 | . 1325 | 19 |
| 12 | . 9843 | . 1243 | 48 | 42 | . 9821 | . 1328 | 18 |
| 13 | . 9842 | . 1246 | 47 | 43 | . 9820 | . 1331 | 17 |
| 14 | . 9842 | . 1249 | 46 | 44 | . 9819 | . 1333 | 16 |
| 15 | .9841 | . 1252 | 45 | 45 | .9818 | . 1336 | 15 |
| 16 | . 9840 | . 1255 | 44 | 46 | . 9817 | . 1339 | 14 |
| 17 | . 9839 | . 1258 | 43 | 47 | . 9817 | . 1342 | 13 |
| 18 | . 9839 | . 1260 | 42 | 48 | . 9816 | . 1345 | 12 |
| 19 | . 9838 | . 1263 | 41 | 49 | .9815 | . 1347 | 11 |
| 20 | . 9837 | . 1266 | 40 | 50 | .9814 | . 1350 | 10 |
| 21 | . 9836 | . 1269 | 39 | 51 | .9814 | . 1353 |  |
| 22 | . 9836 | . 1272 | 38 | 52 | .9813 | . 1356 | 8 |
| 23 | . 9835 | . 1274 | 37 | 53 | . 9812 | .1359 | 7 |
| 24 | . 9834 | . 1277 | 36 | 54 | .98II | .1361 | 6 |
| 25 | . 9833 | . 1280 | 35 | 55 | .9810 | . 1364 | 5 |
| 26 | . 9833 | . 1283 | 34 | 56 | .9810 | . 1367 | 4 |
| 27 | . 9832 | . 1286 | 33 | 57 | . 9809 | . 1370 | 3 |
| 28 | . 9831 | . 1289 | 32 | 58 | . 9808 | . 1373 | 2 |
| 29 | . 9830 | . 1291 | 31 | 59 | . 9807 | . 1375 | 1 |
| 30 | . 9830 | . 1294 | 30 | 60 | . 9806 | . 1378 | - |
|  | Constant for <br> Distance. | Constant for Difference in Height. | Minutes. |  | Constant Distance. | $\begin{gathered} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{gathered}$ | Minutes. |

82 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

98 Degrees.

| Minutes. | Constant for Distance. | $\begin{gathered} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{gathered}$ |  | Minutes. | Constant for <br> Distance. | $\begin{aligned} & \text { Constant } \\ & \text { for } \\ & \text { Difference } \\ & \text { in Height. } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 9806 | . 1378 | 60 | 30 | . 9782 | . 1462 | 30 |
| 1 | . 9806 | .1381 | 59 | 31 | .9781 | . 1465 | 29 |
| 2 | . 9805 | . 1384 | 58 | 32 | . 9780 | . 1467 | 28 |
| 3 | . 9804 | . 1387 | 57 | 33 | . 9779 | . 1470 | 27 |
| 4 | -9803 | . 1390 | 56 | 34 | . 9778 | . 1473 | 26 |
| 5 | . 9802 | . 1392 | 55 | 35 | . 9777 | . 1476 | 25 |
| 6 | . 9802 | . 1395 | 54 | 36 | 9776 | . 1479 | 24 |
| 7 | .9801 | . 1398 | 53 | 37 | 9776 | .1481 | 23 |
| 8 | . 9800 | .1401 | 52 | 38 | . 9775 | . 1484 | 22 |
| 9 | . 9799 | . 1403 | 51 | 39 | . 9774 | . 1487 | 21 |
| 10 | . 9798 | . 1406 | 50 | 40 | . 9773 | . 1490 | 20 |
| 11 | . 9797 | . 1409 | 49 | 41 | . 9772 | . 1492 | 19 |
| 12 | . 9797 | . 1412 | 48 | 42 | . 9771 | . 1495 | 18 |
| 13 | . 9796 | . 1415 | 47 | 43 | . 9770 | . 1498 | 17 |
| 14 | . 9795 | . 1417 | 46 | 44 | . 9770 | . 1501 | 16 |
| 15 | . 9794 | . 1420 | 45 | 45 | . 9769 | . 1504 | 15 |
| 16 | . 9793 | . 1423 | 44 | 46 | . 9768 | . 1506 | 14 |
| 17 | . 9792 | . 1426 | 43 | 47 | . 9767 | . 1509 | 13 |
| 18 | . 9792 | . 1429 | 42 | 48 | . 9766 | . 1512 | 12 |
| 19 | .9791 | .143I | 41 | 49 | . 9765 | . 1515 | 11 |
| 20 | . 9790 | . 1434 | 40 | 50 | . 9764 | . 515 | 10 |
| 21 | . 9789 | . 1437 | 39 | 51 | . 9763 | . 1520 | 9 |
| 22 | . 9788 | . 1440 | 38 | 52 | . 9763 | . 1523 | 8 |
| 23 | . 9788 | . 1442 | 37 | 53 | . 9762 | . 1526 | 7 |
| 24 | . 9787 | . 1445 | 36 | 54 | . 9761 | . 1529 | 6 |
| 25 | . 9786 | . 1448 | 35 | 55 | . 9760 | . 1531 | 5 |
| 26 | . 9785 | . 1451 | 34 | 56 | . 9759 | . 1534 | 4 |
| 27 | . 9784 | . 1454 | 33 | 57 | . 9758 | . 1537 | 3 |
| 28 | . 9783 | . 1456 | 32 | 58 | . 9757 | . 1540 | 2 |
| 29 | . 9782 | . 1459 | 31 | 59 | . 9756 | . 1542 | 1 |
| 30 | . 9782 | . 1462 | 30 | 60 | . 9755 | . 1545 | $\bigcirc$ |
|  | Constant for <br> Distance. | Constant for Difference in Height. | Minutes. |  | Constant Distance. |  | Minutes. |

8I Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings - continued.

99 Degrees.

| Minutes. | Constant for Distance. | Constant for Difference in Height. |  | Minutes. | Constant for Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 9755 | . 1545 | 60 | 30 | . 9728 | . 1628 | 30 |
| 1 | . 9754 | . 1548 | 59 | 31 | . 9727 | . 1631 | 29 |
| 2 | . 9754 | . 1551 | 58 | 32 | . 9726 | . 1633 | 28 |
| 3 | . 9753 | . 1553 | 57 | 33 | . 9725 | . 1636 | 27 |
| 4 | . 9752 | . 1556 | 56 | 34 | . 9724 | . 1639 | 26 |
| 5 | .975I | . 1559 | 55 | 35 | . 9723 | . 1642 | 25 |
| 6 | . 9750 | . 1562 | 54 | 36 | -9722 | . 1644 | 24 |
| 7 | - 9749 | . 1565 | 53 | 37 | . 9721 | . 1647 | 23 |
| 8 | . 9748 | . I567 | 52 | 38 | . 9720 | . 1650 | 22 |
| 9 | . 9747 | . 1570 | 5 I | 39 | . 9719 | . 1653 | 21 |
| 10 | . 9746 | . 1573 | 50 | 40 | . 9718 | . 1655 | 20 |
| II | . 9745 | . I 575 | 49 | 41 | . 9717 | . 1658 | 19 |
| 12 | . 9744 | . 1578 | 48 | 42 | . 9716 | . 1661 | 18 |
| 13 | . 9744 | . 158 I | 47 | 43 | . 9715 | . 1664 | 17 |
| 14 | . 9743 | . 1584 | 46 | 44 | . 9714 | . 1666 | 16 |
| 15 | . 9742 | . 1587 | 45 | 45 | . 9713 | . 1669 | 15 |
| 16 | .974I | . 1589 | 44 | 46 | . 9712 | . 1672 | 14 |
| 17 | . 9740 | . 1592 | 43 | 47 | . 97 II | . 1675 | 13 |
| 18 | . 9739 | . I 595 | 42 | 48 | . 9710 | . 1677 | 12 |
| 19 | . 9738 | . 1598 | 4 I | 49 | . 9709 | . 1680 | 11 |
| 20 | . 9737 | . 1600 | 40 | 50 | . 9708 | . 1683 | 10 |
| 21 | . 9736 | . 1603 | 39 | 51 | . 9707 | . 1686 | 9 |
| 22 | . 9735 | . 1606 | 38 | 52 | . 9706 | . 1688 | 8 |
| 23 | . 9734 | . 1609 | 37 | 53 | . 9705 | . 1691 | 7 |
| 24 | . 9733 | . I6II | 36 | 54 | . 9704 | . 1694 | 6 |
| 25 | . 9733 | . 1614 | 35 | 55 | . 9703 | . 1697 | 5 |
| 26 | . 9732 | .1617 | 34 | 56 | . 9702 | . 1700 | 4 |
| 27 | . 9731 | . 1620 | 33 | 57 | . 9701 | . 1703 | 3 |
| 28 | . 9730 | . 1622 | 32 | 58 | . 9701 | . 1705 | 2 |
| 29 | . 9729 | . 1625 | 3 I | 59 | . 9700 | . 1707 | I |
| 30 | . 9728 | . 1628 | 30 | 60 | . 9699 | . 1710 | 0 |
|  | Constant for Distance. | Constant for Difference in Height. | Minutes. |  | Constant for Distance. | Constant for Difference in Height. | Minutes. |

8o Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

Ioo Degrees.

| Minutes. | Constant for <br> Distance. | Constant for Difference in Height. |  | Minutes. | Constant for <br> Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcirc$ | . 9699 | . 1710 | 60 | 30 | . 9668 | . 1792 | 30 |
| 1 | . 9698 | . 1713 | 59 | 31 | . 9667 | . 1795 | 29 |
| 2 | . 9697 | . 1716 | 58 | 32 | . 9666 | . 1797 | 28 |
| 3 | . 9696 | . 1718 | 57 | 33 | . 9665 | . 1800 | 27 |
| 4 | . 9695 | . 1721 | 56 | 34 | . 9664 | . 1803 | 26 |
| 5 | . 9694 | . 1724 | 55 | 35 | . 9663 | . 1806 | 25 |
| 6 | . 9693 | . 1727 | 54 | 36 | . 9662 | . 1808 | 24 |
| 7 | . 9692 | . 1729 | 53 | 37 | . 9661 | . 1811 | 23 |
| 8 | . 9691 | . 1732 | 52 | 38 | . 9660 | .1814 | 22 |
| 9 | . 9689 | . 1735 | 51 | 39 | . 9659 | . 1816 | 21 |
| 10 | . 9688 | . 1737 | 50 | 40 | . 9657 | .1819 | 20 |
| 11 | . 9687 | . 1740 | 49 | 41 | . 9656 | . 1822 | 19 |
| 12 | . 9686 | . 1743 | 48 | 42 | . 9655 | . 1824 | 18 |
| 13 | . 9685 | . 1746 | 47 | 43 | . 9654 | . 1827 | 17 |
| 14 | . 9684 | . 1748 | 46 | 44 | . 9653 | . 1830 | 16 |
| 15 | . 9683 | .1751 | 45 | 45 | . 9652 | . 1833 | 15 |
| 16 | . 9682 | . 1754 | 44 | 46 | .9651 | . 1835 | 14 |
| 17 | . 9681 | . 1757 | 43 | 47 | . 9650 | . 1838 | 13 |
| 18 | . 9680 | . 1759 | 42 | 48 | . 9649 | . 1841 | 12 |
| 19 | . 9679 | . 1762 | 41 | 49 | . 9648 | . 1843 | 11 |
| 20 | . 9678 | . 1765 | 40 | 50 | . 9647 | . 1846 | 10 |
| 21 | . 9677 | $\because 767$ | 39 | 51 | . 9646 | . 1849 |  |
| 22 | . 9676 | . 1770 | 38 | 52 | . 9645 | . 1851 | 8 |
| 23 | . 9675 | . 1773 | 37 | 53 | . 9643 | . 1854 | 7 |
| 24 | . 9674 | . 1776 | 36 | 54 | . 9642 | . 1857 | 6 |
| 25 | . 9673 | . 1778 | 35 | 55 | .964t | . 1860 | 5 |
| 26 | . 9672 | . 1781 | 34 | 56 | . 9640 | . 1862 | 4 |
| 27 | . 9671 | . 1784 | 33 | 57 | . 9639 | . 1865 | 3 |
| 28 | . 9670 | . 1786 | 32 | 58 | . 9638 | . 1868 | 2 |
| 29 | . 9669 | . 1789 | 31 | 59 | . 9637 | . 1870 | 1 |
| 30 | . 9668 | . 1792 | 30 | 60 | . 9636 | . 1873 | - |
|  | Constant for Distance. | Constant Difference in Height. | Minutes. |  | Constant for Distance. | $\begin{aligned} & \text { Constant } \\ & \text { for } \\ & \text { Difference } \\ & \text { in Height. } \end{aligned}$ | Minutes |

79 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer
Readings-continued.
iol Degrees.

| Minutes. | Constant Distan Distance. | $\begin{array}{\|c\|} \hline \begin{array}{c} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{array} \end{array}$ |  | Minutes. | Constant Distar <br> Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| O | . 9636 | . 1873 | 60 | 30 | . 9603 | . 1954 | 30 |
| 1 | . 9635 | . 1876 | 59 | 31 | . 9601 | . 1956 | 29 |
| 2 | . 9634 | . 1878 | 58 | 32 | . 9600 | . 1959 | 28 |
| 3 | . 9633 | . 1881 | 57 | 33 | . 9599 | . 1962 | 27 |
| 4 | . 9632 | . 1884 | 56 | 34 | . 9598 | . 1964 | 26 |
| 5 | . 9630 | . 1887 | 55 | 35 | . 9597 | . 1967 | 25 |
| 6 | . 9629 | . 1889 | 54 | 36 | . 9596 | . 1970 | 24 |
| 7 | . 9628 | . 1892 | 53 | 37 | . 9595 | . 1972 | 23 |
| 8 | . 9627 | . 1895 | 52 | 38 | . 9593 | . 1975 | 22 |
| 9 | . 9626 | . 1897 | 51 | 39 | . 9592 | . 1977 | 21 |
| 10 | . 9625 | . 1900 | 50 | 40 | .959I | . 1980 | 20 |
| II | . 9624 | . 1903 | 49 | 41 | . 9590 | . 1983 | 19 |
| 12 | . 9623 | . 1905 | 48 | 42 | . 9589 | . 1986 | 18 |
| 13 | . 9622 | . 1908 | 47 | 43 | . 9588 | . 1988 | 17 |
| 14 | . 9621 | . 1911 | 46 | 44 | . 9587 | . 1991 | 16 |
| 15 | .9619 | . 1913 | 45 | 45 | . 9585 | . 1994 | 15 |
| 16 | . 9618 | . 1916 | 44 | 46 | . 9584 | . 1997 | 14 |
| 17 | . 9617 | . 1919 | 43 | 47 | . 9583 | . 1999 | 13 |
| 18 | . 9616 | . 1922 | 42 | 48 | . 9582 | . 2002 | 12 |
| 19 | .9615 | . 1924 | 41 | 49 | . $95^{81}$ | . 2004 | II |
| 20 | . 9614 | . 1927 | 40 | 50 | . 9580 | . 2007 | 10 |
| 21 | . 9613 | -1930 | 39 | 51 | . 9578 | . 2010 |  |
| 22 | .9612 | . 1932 | 38 | 52 | . 9577 | . 2012 | 8 |
| 23 | . 9610 | . 1935 | 37 | 53 | . 9576 | . 2015 | 7 |
| 24 | . 9609 | . 1938 | 36 | 54 | . 9575 | . 2018 | 6 |
| 25 | . 9608 | . 1940 | 35 | 55 | . 9574 | . 2020 | 5 |
| 26 | . 9607 | . 1943 | 34 | 56 | . 9573 | . 2023 | 4 |
| 27 | . 9606 | . 1946 | 33 | 57 | . 9571 | . 2026 | 3 |
| 28 | . 9605 | . 1948 | 32 | 58 | . 9570 | . 2028 | 2 |
| 29 | . 9604 | . 1951 | 31 | 59 | . 9569 | . 2031 | 1 |
| 30 | . 9603 | . 1954 | 30 | 60 | . 9568 | . 2034 | $\bigcirc$ |
|  | Constant for <br> Distance. |  | Minutes. |  | Constant Distance. | Constant <br> for <br> Difference <br> in Height. | Minutes. |

78 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

102 Degrees.

| Minutes. | Constant Distance. | Constant Difference in Height. |  |
| :---: | :---: | :---: | :---: |
| 0 | . 9568 | . 2034 | 60 |
| 1 | . 9567 | . 2036 | 59 |
| 2 | . 9565 | . 2039 | 58 |
| 3 | . 9564 | . 2042 | 57 |
| 4 | -9563 | . 2044 | 56 |
| 5 | . 9562 | . 2047 | 55 |
| 6 | .9561 | . 2050 | 54 |
| 7 | . 9559 | . 2052 | 53 |
| 8 | . 9558 | . 2055 | 52 |
| 9 | . 9557 | . 2058 | 51 |
| 10 | . 9556 | . 2060 | 50 |
| 11 | . 9555 | . 2063 | 49 |
| 12 | . 9553 | . 2066 | 48 |
| 13 | . 9552 | . 2068 | 47 |
| 14 | .9551 | . 2071 | 46 |
| 15 | . 9550 | . 2074 | 45 |
| 16 | . 9549 | . 2076 | 44 |
| 17 | . 9547 | . 2079 | 43 |
| 18 | . 9546 | . 2081 | 42 |
| 19 | . 9545 | . 2084 | 41 |
| 20 | . 9544 | . 2087 | 40 |
| 21 | . 9543 | . 2089 | 39 |
| 22 | .954I | . 2092 | 38 |
| 23 | . 9540 | . 2095 | 37 |
| 24 | . 9539 | . 2097 | 36 |
| 25 | . 9538 | .2100 | 35 |
| 26 | . 9537 | . 2103 | 34 |
| 27 | . 9535 | . 2105 | 33 |
| 28 | . 9534 | . 2108 | 32 |
| 29 | . 9533 | . 2111 | 31 |
| 30 | . 9532 | .2113 | 30 |
|  | Constant for <br> Distance. | Constant <br> Difference <br> in Height. | Minutes. |


| Minutes. | Constant Distanc <br> Distance. | $\left\lvert\, \begin{gathered} \text { Constant } \\ \text { for } \\ \text { Diference } \\ \text { in Height. } \end{gathered}\right.$ |  |
| :---: | :---: | :---: | :---: |
| 30 | . 9532 | . 2113 | 30 |
| 31 | . 9530 | . 2116 | 29 |
| 32 | . 9529 | .2118 | 28 |
| 33 | . 9528 | . 2121 | 27 |
| 34 | . 9527 | . 2124 | 26 |
| 35 | . 9525 | . 2126 | 25 |
| 36 | . 9524 | . 2129 | 24 |
| 37 | . 9523 | . 2132 | 23 |
| 38 | . 9522 | . 2134 | 22 |
| 39 | . 9520 | .2137 | 21 |
| 40 | . 9519 | . 2139 | 20 |
| 41 | . 9518 | . 2142 | 19 |
| 42 | . 9517 | . 2145 | 18 |
| 43 | . 9515 | . 2147 | 17 |
| 44 | . 9514 | . 2150 | 16 |
| 45 | .9513 | . 2153 | 15 |
| 46 | . 9512 | . 2155 | 14 |
| 47 | .9510 | . 2158 | 13 |
| 48 | . 9509 | . 2160 | 12 |
| 49 | . 9508 | . 2163 | 11 |
| 50 | . 9507 | . 2166 | 10 |
| 51 | . 9505 | . 2168 | 9 |
| 52 | . 9504 | . 2171 | 8 |
| 53 | . 9503 | . 2174 | 7 |
| 54 | . 9502 | . 2176 | 6 |
| 55 | . 9500 | . 2179 | 5 |
| 56 | . 9499 | .2181 | 4 |
| 57 | . 9498 | .2184 | 3 |
| 58 | . 9497 | . 2187 | 2 |
| 59 | . 9495 | .2189 | 1 |
| 60 | . 9494 | . 2192 | $\bigcirc$ |
|  | Constant for <br> Distance. | $\begin{aligned} & \text { Constant } \\ & \text { for } \\ & \text { Difference } \\ & \text { in Height. } \end{aligned}$ | Minutes |

77 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

## 103 Degrees.

| Minutes. | $\begin{aligned} & \text { Constant } \\ & \text { for } \\ & \text { Distance. } \end{aligned}$ | Constant Difference in Height. |  |
| :---: | :---: | :---: | :---: |
| $\bigcirc$ | . 9494 | . 2192 | 60 |
| 1 | . 9493 | .2194 | 59 |
| 2 | . 9492 | . 2197 | 58 |
| 3 | . 9490 | . 2200 | 57 |
| 4 | . 9489 | . 2202 | 56 |
| 5 | . 9488 | . 2205 | 55 |
| 6 | . 9486 | . 2208 | 54 |
| 7 | . 9485 | .2210 | 53 |
| 8 | . 9484 | .2213 | 52 |
| 9 | . 9482 | . 2215 | 51 |
| 10 | .948I | .2218 | 50 |
| 11 | . 9480 | . 2221 | 49 |
| 12 | . 9479 | . 2223 | 48 |
| 13 | . 9477 | . 2226 | 47 |
| 14 | . 9476 | . 2228 | 46 |
| 15 | . 9475 | .223I | 45 |
| 16 | . 9473 | . 2234 | 44 |
| 17 | . 9472 | . 2236 | 43 |
| 18 | .9471 | . 2239 | 42 |
| 19 | . 9470 | . 2241 | 41 |
| 20 | . 9468 | . 2244 | 40 |
| 21 | . 9467 | . 2247 | 39 |
| 22 | . 9466 | . 2249 | 38 |
| 23 | . 9464 | . 2252 | 37 |
| 24 | . 9463 | . 2254 | 36 |
| 25 | . $9462^{\circ}$ | . 2257 | 35 |
| 26 | . 9460 | . 2260 | 34 |
| 27 | . 9459 | . 2262 | 33 |
| 28 | . 9458 | . 2265 | 32 |
| 29 | . 9456 | . 2267 | 31 |
| 30 | . 9455 | . 2270 | 30 |
|  | Constant Distare <br> Distance. | Constant Differ Difference in Height. | Minutes. |


| Minutes. | Constant for Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: |
| 30 | . 9455 | . 2270 | 30 |
| 31 | - 9454 | . 2273 | 29 |
| 32 | . 9452 | . 2275 | 28 |
| 33 | .945I | . 2278 | 27 |
| 34 | . 9450 | . 2280 | 26 |
| 35 | . 9448 | .2283 | 25 |
| 36 | . 9447 | . 2286 | 24 |
| 37 | . 9446 | . 2288 | 23 |
| 38 | . 9444 | . 2291 | 22 |
| 39 | . 9443 | . 2293 | 21 |
| 40 | . 9442 | . 2296 | 20 |
| 41 | . 9440 | . 2299 | 19 |
| 42 | . 9439 | . 2301 | 18 |
| 43 | . 9438 | . 2304 | 17 |
| 44 | . 9436 | . 2306 | 16 |
| 45 | . 9435 | . 2309 | 15 |
| 46 | . 9434 | . 23 II | 14 |
| 47 | - 9433 | . 2314 | 13 |
| 48 | .943I | . 2316 | 12 |
| 49 | . 9430 | .2319 | II |
| 50 | . 9428 | . 2322 | 10 |
| 51 | . 9427 | . 2324 | 9 |
| 52 | . 9426 | . 2327 | 8 |
| 53 | . 9424 | . 2329 | 7 |
| 54 | . 9423 | . 2332 | 6 |
| 55 | . 9422 | . 2335 | 5 |
| 56 | . 9420 | . 2337 | 4 |
| 57 | . 9419 | . 2340 | 3 |
| 58 | .9418 | . 2342 | 2 |
| 59 | . 9416 | . 2345 | 1 |
| 60 | . 9415 | . 2347 | 0 |
|  | Constant for Distance. | Constant for Difference in Height. | Minutes |

76 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

IO4 Degrees.

| Minutes. | Constant for Distance. | Constant for Difference in Height. |  | Minutes. | Constant . for <br> Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 9415 | . 2347 | 60 | 30 | . 9373 | . 2424 | 30 |
| 1 | . 9413 | . 2350 | 59 | 31 | . 9372 | . 2427 | 29 |
| 2 | .9412 | . 2353 | 58 | 32 | . 9370 | . 2429 | 28 |
| 3 | .94II | . 2355 | 57 | 33 | . 9369 | . 2432 | 27 |
| 4 | . 9409 | . 2358 | 56 | 34 | . 9367 | . 2434 | 26 |
| 5 | . 9408 | . 2360 | 55 | 35 | . 9366 | . 2437 | 25 |
| 6 | . 9407 | . 2363 | 54 | 36 | . 9365 | . 2439 | 24 |
| 7 | . 9405 | . 2365 | 53 | 37 | . 9363 | . 2442 | 23 |
| 8 | . 9404 | . 2368 | 52 | 38 | . 9362 | . 2444 | 22 |
| 9 | . 9402 | . 2370 | 51 | 39 | . 9360 | . 2447 | 21 |
| 10 | . 9401 | . 2373 | 50 | 40 | . 9359 | . 2450 | 20 |
| 11 | . 9400 | . 2376 | 49 | 41 | . 9358 | . 2452 | 19 |
| 12 | . 9398 | . 2378 | 48 | 42 | . 9356 | . 2455 | 18 |
| 13 | . 9397 | .238I | 47 | 43 | . 9355 | . 2457 | 17 |
| 14 | . 9396 | .2383 | 46 | 44 | . 9353 | . 2460 | 16 |
| 15 | . 9394 | . 2386 | 45 | 45 | . 9352 | . 2462 | 15 |
| 16 | . 9393 | . 2388 | 44 | 46 | . 9350 | . 2465 | 14 |
| 17 | . 9391 | . 2391 | 43 | 47 | . 9349 | . 2467 | 13 |
| 18 | . 9390 | . 2394 | 42 | 48 | . 9348 | . 2470 | 12 |
| 19 | . 9389 | . 2396 | 4 I | 49 | . 9346 | . 2472 | 11 |
| 20 | .9387 | . 2399 | 40 | 50 | . 9345 | . 2475 | 10 |
| 21 | . 9386 | -.2401 | 39 | 51 | - 9343 | . 2477 |  |
| 22 | . 9384 | . 2404 | 38 | 52 | . 9342 | . 2480 | 8 |
| 23 | . 9383 | . 2406 | 37 | 53 | . 9340 | . 2482 | 7 |
| 24 | . 9382 | .2409 | 36 | 54 | . 9339 | . 2485 | 6 |
| 25 | . 9380 | . 2411 | 35 | 55 | . 9337 | . 2487 | 5 |
| 26 | . 9379 | . 2414 | 34 | 56 | . 9336 | . 2490 | 4 |
| 27 | . 9377 | .2417 | 33 | 57 | . 9335 | . 2493 | 3 |
| 28 | . 9376 | . 2419 | 32 | 58 | . 9333 | . 2495 | 2 |
| 29 | . 9375 | . 2422 | 3 I | 59 | . 9332 | . 2498 | 1 |
| 30 | . 9373 | . 2424 | 30 | 60 | . 9330 | . 2500 | 0 |
|  | Constant for Distance. | Constant for Difference in Height. | Minutes. |  | Constant for Distance. | Constant for Difference in Height. | Minutes. |

Table for the Calculation of Heights and Distances from Tacheometer Readings--continued.

105 Degrees.

| Minutes. | Constant Distan <br> Distance. | $\begin{array}{\|c\|c} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{array}$ |  | Minutes. | Constant Distance. | $\begin{array}{\|c\|c} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{array}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcirc$ | . 9330 | . 2500 | 60 | 30 | . 9286 | . 2575 | 30 |
| 1 | . 9329 | . 2503 | 59 | 3 I | . 9284 | . 2578 | 29 |
| 2 | . 9327 | . 2505 | 58 | 32 | . 9283 | . 2580 | 28 |
| 3 | . 9326 | . 2508 | 57 | 33 | .928I | . 2583 | 27 |
| 4 | . 9324 | . 2510 | 56 | 34 | . 9280 | . 2585 | 26 |
| 5 | . 9323 | . 2513 | 55 | 35 | . 9278 | . 2588 | 25 |
| 6 | .9321 | .2515 | 54 | 36 | . 9277 | . 2590 | 24 |
| 7 | . 9320 | . 2518 | 53 | 37 | . 9275 | . 2593 | 23 |
| 8 | . 9319 | . 2520 | 52 | 38 | . 9274 | . 2595 | 22 |
| 9 | . 9317 | . 2523 | 51 | 39 | . 9272 | . 2598 | 21 |
| 10 | . 9316 | . 2525 | 50 | 40 | . 9271 | . 2600 | 20 |
| 1 I | . 9314 | . 2528 | 49 | 41 | . 9269 | . 2603 | 19 |
| 12 | .9313 | . 2530 | 48 | 42 | . 9268 | . 2605 | 18 |
| 13 | .9311 | . 2533 | 47 | 43 | . 9266 | . 2608 | 17 |
| 14 | .9310 | . 2535 | 46 | 44 | . 9265 | . 2610 | 16 |
| 15 | . 9308 | . 2538 | 45 | 45 | . 9263 | .2613 | 15 |
| 16 | . 9307 | . 2540 | 44 | 46 | . 9262 | . 2615 | 14 |
| 17 | . 9305 | . 2543 | 43 | 47 | . 9260 | .2618 | 13 |
| 18 | . 9304 | . 2545 | 42 | 48 | . 9259 | . 2620 | 12 |
| 19 | . 9302 | . 2548 | 41 | 49 | . 9257 | . 2622 | 11 |
| 20 | .9301 | . 2550 | 40 | 50 | . 9256 | . 2625 | 10 |
| 21 | . 9299 | . 2553 | 39 | 51 | . 9254 |  |  |
| 22 | . 9298 | . 2555 | 38 | 52 | . 9253 | . 2630 | 8 |
| 23 | . 9296 | . 2558 | 37 | 53 | . 9251 | . 2632 | 7 |
| 24 | . 9295 | . 2560 | 36 | 54 | . 9249 | . 2635 | 6 |
| 25 | . 9293 | . 2563 | 35 | 55 | . 9248 | . 2637 | 5 |
| 26 | . 9292 | . 2565 | 34 | 56 | . 9246 | . 2640 | 4 |
| 27 | . 9290 | . 2568 | 33 | 57 | . 9245 | . 2642 | 3 |
| 28 | . 9289 | . 2570 | 32 | 58 | . 9243 | . 2645 |  |
| 29 | . 9287 | . 2573 | 31 | 59 | . 9242 | . 2647 | 1 |
| 30 | . 9286 | . 2575 | 30 | 60 | . 9240 | . 2650 | - |
|  | Constant .for <br> Distance. | Constant for Difference in Height. | Minutes. |  | $\begin{aligned} & \text { Constant } \\ & \text { for } \\ & \text { Distance. } \end{aligned}$ | Constant for Difference in Height. | Minutes. |

74 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

106 Degrees.

| Minutes. | Constant Distance. | $\begin{gathered}\text { Constant } \\ \text { for }\end{gathered}$ $\begin{gathered}\text { Difference } \\ \text { in Height. }\end{gathered}$ |  |
| :---: | :---: | :---: | :---: |
| $\bigcirc$ | . 9240 | . 2650 | 60 |
| 1 | . 9239 | . 2652 | 59 |
| 2 | . 9237 | . 2655 | 58 |
| 3 | . 9236 | . 2657 | 57 |
| 4 | . 9234 | . 2660 | 56 |
| 5 | . 9233 | . 2662 | 55 |
| 6 | .9231 | . 2664 | 54 |
| 7 | . 9230 | . 2667 | 53 |
| 8 | . 9228 | . 2669 | 52 |
| 9 | . 9226 | . 2672 | 51 |
| 10 | . 9225 | . 2674 | 50 |
| 11 | . 9223 | . 2677 | 49 |
| 12 | . 9222 | . 2679 | 48 |
| 13 | . 9220 | . 2682 | 47 |
| 14 | . 9219 | . 2684 | 46 |
| 15 | . 9217 | . 2687 | 45 |
| 16 | . 9215 | . 2689 | 44 |
| 17 | . 9214 | . 2691 | 43 |
| 18 | . 9212 | . 2694 | 42 |
| 19 | .92II | . 2696 | 41 |
| 20 | . 9209 | . 2699 | 40 |
| 21 | . 9208 | . 2701 | 39 |
| 22 | . 9206 | : 2704 | 38 |
| 23 | . 9204 | . 2706 | 37 |
| 24 | . 9203 | . 2709 | 36 |
| 25 | . 9201 | .27II | 35 |
| 26 | . 9200 | . 2713 | 34 |
| 27 | . 9198 | . 2716 | 33 |
| 28 | .9197 | . 2718 | 32 |
| 29 | . 9195 | . 2721 | 31 |
| 30 | . 9193 | . 2723 | 30 |
|  |  | Constant <br> Difference <br> in Height. | Minutes. |


| Minutes. | Constant for <br> Distance. | $\begin{array}{\|c} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{array}$ |  |
| :---: | :---: | :---: | :---: |
| 30 | . 9193 | . 2723 | 30 |
| 31 | . 9192 | . 2726 | 29 |
| 32 | . 9190 | . 2728 | 28 |
| 33 | . 9189 | . 2731 | 27 |
| 34 | . 9187 | . 2733 | 26 |
| 35 | .9185 | . 2735 | 25 |
| 36 | . 9184 | . 2738 | 24 |
| 37 | . 9182 | . 2740 | 23 |
| 38 | .9181 | . 2743 | 22 |
| 39 | .9179 | . 2745 | 21 |
| 40 | .9177 | . 2748 | 20 |
| 41 | . 9176 | . 2750 | 19 |
| 42 | .9174 | . 2752 | 18 |
| 43 | .9173 | . 2755 | 17 |
| 44 | .9171 | . 2757 | 16 |
| 45 | . 9169 | . 2760 | 15 |
| 46 | . 9168 | . 2762 | 14 |
| 47 | .9166 | . 2765 | 13 |
| 48 | . 9165 | . 2767 | 12 |
| 49 | . 9163 | . 2769 | 11 |
| 50 | .916I | . 2772 | 10 |
| 51 | . 9160 | . 2774 | 9 |
| 52 | .9158 | . 2777 | 8 |
| 53 | .9157 | . 2779 | 7 |
| 54 | .9155 | . 2781 | 6 |
| 55 | .9153 | . 2784 | 5 |
| 56 | .9152 | . 2786 | 4 |
| 57 | .9150 | . 2789 | 3 |
| 58 | .9148 | .2791 | 2 |
| 59 | .9147 | . 2794 | 1 |
| 60 | . 9145 | . 2796 | $\bigcirc$ |
|  | Constant fistan <br> Distance. | Constant for Difference in Height. | Minutes. |

73 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer
Readings-continued.
107 Degrees.

| Minutes. | Constant Distar Distance. | $\left\lvert\, \begin{gathered} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{gathered}\right.$ |  | Minutes. | Constant for <br> Distance. | $\left\lvert\, \begin{gathered} \text { Constant } \\ \text { for } \\ \text { fifference } \\ \text { in Height. } \end{gathered}\right.$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - | . 9145 | . 2796 | 60 | 30 | . 9096 | . 2868 | 30 |
| 1 | . 9144 | . 2798 | 59 | 31 | . 9094 | . 2870 | 29 |
| 2 | . 9142 | . 2801 | 58 | 32 | . 9092 | . 2873 | 28 |
| 3 | . 9140 | . 2803 | 57 | 33 | .9091 | . 2875 | 27 |
| 4 | .9139 | . 2806 | 56 | 34 | . 9089 | . 2878 | 26 |
| 5 | .9137 | . 2808 | 55 | 35 | . 9087 | . 2880 | 25 |
| 6 | .9135 | .2810 | 54 | 36 | . 9086 | . 2882 | 24 |
| 7 | .9134 | .2813 | 53 | 37 | . 9084 | . 2885 | 23 |
| 8 | . 9132 | . 2815 | 52 | 38 | . 9082 | . 2887 | 22 |
| 9 | . 9130 | . 2818 | 51 | 39 | .9081 | . 2889 | 21 |
| 10 | . 9129 | . 2820 | 50 | 40 | . 9079 | . 2892 | 20 |
| 11 | . 9127 | . 2822 | 49 | 41 | . 9077 | . 2894 | 19 |
| 12 | .9126 | . 2825 | 48 | 42 | . 9076 | . 2896 | 18 |
| 13 | .9124 | . 2827 | 47 | 43 | . 9074 | . 2899 | 17 |
| 14 | . 9122 | . 2830 . | 46 | 44 | . 9072 | .2901 | 16 |
| 15 | .912I | . 2832 | 45 | 45 | .907 I | . 2904 | 15 |
| 16 | .9119 | . 2834 | 44 | 46 | . 9069 | . 2906 | 14 |
| 17 | .9117 | . 2837 | 43 | 47 | . 9067 | . 2908 | 13 |
| 18 | .9116 | . 2839 | 42 | 48 | . 9066 | . 2911 | 12 |
| 19 | .9114 | . 2842 | 41 | 49 | . 9064 | . 2913 | 11 |
| 20 | .9112 | . 2844 | 40 | 50 | . 9062 | . 2915 | 10 |
| 21 | .9111 | . 2846 | 39 | 51 | . 9060 | . 2918 |  |
| 22 | .9109 | . 2849 | 38 | 52 | . 9059 | . 2920 | 8 |
| 23 | . 9107 | . 2851 | 37 | 53 | . 9057 | . 2922 | 7 |
| 24 | .9106 | . 2854 | 36 | 54 | . 9055 | . 2925 | 6 |
| 25 | . 9104 | . 2856 | 35 | 55 | . 9054 | . 2927 | 5 |
| 26 | . 9102 | . 2858 | 34 | 56 | . 9052 | . 2930 | 4 |
| 27 | .9101 | . 2861 | 33 | 57 | . 9050 | . 2932 | 3 |
| 28 | . 9099 | . 2863 | 32 | 58 | . 9049 | . 2934 | 2 |
| 29 | . 9098 | . 2866 | 31 | 59 | . 9047 | . 2937 | 1 |
| 30 | . 9096 | . 2868 | 30 | 60 | . 9045 | . 2939 | o |
|  | Constant Distan <br> Distance. | $\begin{aligned} & \text { Constant } \\ & \text { for } \\ & \text { Difference } \\ & \text { in Height. } \end{aligned}$ | Minutes. |  | Constant for Distance. | Constant for Difference in Height. | Minutes. |

72 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer
Readings-continued.
108 Degrees.

| Minutes. | Constant for Distance. | Constant for Difference in Height. |  | Minutes. | Constant for Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 9045 | . 2939 | 60 | 30 | . 8993 | - 3009 | 30 |
| 1 | . 9043 | . 2941 | 59 | 31 | . 8991 | . 3011 | 29 |
| 2 | . 9042 | . 2944 | 58 | 32 | . 8990 | . 3014 | 28 |
| 3 | . 9040 | . 2946 | 57 | 33 | . 8988 | . 3016 | 27 |
| 4 | . 9038 | . 2948 | 56 | 34 | . 8986 | . 3018 | 26 |
| 5 | . 9037 | . 2951 | 55 | 35 | . 8984 | . 3021 | 25 |
| 6 | . 9035 | . 2953 | 54 | 36 | .8983 | - 3023 | 24 |
| 7 | . 9033 | . 2955 | 53 | 37 | .898I | . 3025 | 23 |
| 8 | .903I | . 2958 | 52 | 38 | . 8979 | - 3028 | 22 |
| 9 | . 9030 | . 2960 | 51 | 39 | . 8977 | . 3030 | 21 |
| 10 | . 9028 | .2962 | 50 | 40 | . 8976 | . 3032 | 20 |
| 11 | . 9026 | . 2965 | 49 | 41 | . 8974 | . 3035 | 19 |
| 12 | . 9024 | . 2967 | 48 | 42 | . 8972 | . 3037 | 18 |
| 13 | . 9023 | . 2969 | 47 | 43 | . 8970 | . 3039 | 17 |
| 14 | . 9021 | . 2972 | 46 | 44 | . 8969 | . 3041 | 16 |
| 15 | . 9019 | . 2974 | 45 | 45 | . 8967 | . 3044 | 15 |
| 16 | . 9018 | . 2977 | 44 | 46 | . 8965 | . 3046 | 14 |
| 17 | . 9016 | . 2979 | 43 | 47 | . 8963 | . 3048 | 13 |
| 18 | . 9014 | . 2981 | 42 | 48 | . 8962 | . 3051 | 12 |
| 19 | . 9012 | . 2984 | 4 I | 49 | . 8960 | . 3053 | 11 |
| 20 | . 901 I | . 2986 | 40 | 50 | . 8958 | . 3055 | 10 |
| 21 | . 9009 | . 2988 | 39 | 51 | . 8956 | . 3058 | 9 |
| 22 | . 9007 | . 29891 | 38 | 52 | . 8954 | - 3060 | 8 |
| 23 | . 9005 | . 2993 | 37 | 53 | . 8953 | - 3062 | 7 |
| 24 | . 9004 | . 2995 | 36 | 54 | . 8951 | - 3065 | 6 |
| 25 | . 9002 | . 2998 | 35 | 55 | . 8949 | . 3067 | 5 |
| 26 | . 9000 | - 3000 | 34 | 56 | . 8947 | . 3069 | 4 |
| 27 | . 8998 | - 3002 | 33 | 57 | . 8946 | -3071 | 3 |
| 28 | . 8997 | . 3004 | 32 | 58 | . 8944 | . 3074 | 2 |
| 29 | . 8995 | - 3007 | 3 I | 59 | . 8942 | - 3076 | I |
| 30 | . 8993 | . 3009 | 30 | 60 | . 8940 | . 3078 | O |
|  | Constant for Distance. | Constant for Difference in Height. | Minutes. |  | Constant for Distance. | Constant for Difference in Height. | Minutes. |

71 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued

IO9 Degrees.

| Minutes. | Constant for <br> Distance. | $\left\lvert\, \begin{gathered} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{gathered}\right.$ |  | Minutes. | $\begin{gathered} \text { Constant } \\ \text { for } \\ \text { Distance. } \end{gathered}$ | $\begin{array}{\|l\|l} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{array}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 8940 | . 3078 | 60 | 30 | . 8886 | . 3147 | 30 |
| 1 | . 8938 | . 3081 | 59 | 31 | . 8884 | . 3149 | 29 |
| 2 | . 8937 | . 3083 | 58 | 32 | . 8882 | .3151 | 25 |
| 3 | . 8935 | . 3085 | 57 | 33 | . 8880 | . 3153 | 27 |
| 4 | . 8933 | . 3088 | 56 | 34 | . 8878 | . 3156 | 26 |
| 5 | . 8931 | . 3090 | 55 | 35 | . 8877 | . 3158 | 25 |
| 6 | . 8929 | . 3092 | 54 | 36 | . 8875 | . 3160 | 24 |
| 7 | . 8928 | . 3094 | 53 | 37 | . 8873 | . 3162 | 23 |
| 8 | . 8926 | . 3097 | 52 | 38 | . 887 I | . 3165 | 22 |
| 9 | . 8924 | . 3099 | 51 | 39 | . 8869 | . 3167 | 21 |
| 10 | . 8922 | . 3101 | 50 | 40 | . 8867 | . 3169 | 20 |
| 11 | . 8920 | . 3103 | 49 | 41 | . 8866 | . 3171 | 19 |
| 12 | . 8918 | - 3106 | 48 | 42 | . 8864 | . 3174 | 18 |
| 13 | . 8917 | . 3108 | 47 | 43 | . 8862 | . 3176 | 17 |
| 14 | . 8915 | . 31110 | 46 | 44 | . 8860 | . 3178 | 16 |
| 15 | . 8913 | .3113 | 45 | 45 | . 8858 | . 3180 | 15 |
| 16 | .8911 | . 3115 | 44 | 46 | . 8856 | . 3183 | 14 |
| 17 | . 8909 | -3117 | 43 | 47 | . 8854 | . 3185 | 13 |
| 18 | . 8908 | -3119 | 42 | 48 | . 8853 | . 3187 | 12 |
| 19 | . 8906 | -3122 | 41 | 49 | . 8851 | . 3189 | 11 |
| 20 | . 8904 | . 3124 | 40 | 50 | . 8849 | -3192 | 10 |
| 21 | . 8902 | . 3126 | 39 | 51 | . 8847 | . 3194 | 9 |
| 22 | . 8900 | -3129 | 38 | 52 | . 8845 | -3196 | 8 |
| 23 | . 8899 | -3131 | 37 | 53 | . 8843 | -3198 | 7 |
| 24 | . 8897 | -3133 | 36 | 54 | . 8842 | . 3201 | 6 |
| 25 | . 8895 | . 3136 | 35 | 55 | . 8840 | . 3203 | 5 |
| 26 | . 8893 | . 3138 | 34 | 56 | . 8838 | . 3205 | 4 |
| 27 | . 8891 | . 3140 | 33 | 57 | . 8836 | . 3207 | 3 |
| 28 | . 8889 | . 3142 | 32 | 58 | . 8834 | . 3209 | 2 |
| 29 | . 8888 | . 3144 | 31 | 59 | . 8832 | . 3212 | 1 |
| 30 | . 8886 | -3147 | 30 | 60 | . 8830 | . 3214 | - |
|  | $\begin{aligned} & \text { Constant } \\ & \text { for } \\ & \text { Distance. } \end{aligned}$ | $\begin{aligned} & \text { Constant } \\ & \text { for } \\ & \text { Difference } \\ & \text { in Height. } \end{aligned}$ | Minutes. |  | Constant for <br> Distance. | $\begin{aligned} & \text { Constant } \\ & \text { for } \\ & \text { Difference } \\ & \text { in Height. } \end{aligned}$ | Minutes. |

70 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

1 Io Degrees.

| Minutes. | Constant for <br> Distance. | Constant for Difference in Height. |  | Minutes. | Constant Distan Distance. | Constant for Difference in Height |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 8830 | . 3214 | 60 | 30 | . 8774 | . 3280 | 30 |
| 1 | . 8828 | . 3216 | 59 | 31 | . 8772 | . 3283 | 29 |
| 2 | . 8826 | -3218 | 58 | 32 | . 8770 | . 3285 | 28 |
| 3 | . 8825 | . 3221 | 57 | 33 | . 8768 | . 3287 | 27 |
| 4 | . 8823 | . 3223 | 56 | 34 | . 8766 | . 3289 | 26 |
| 5 | . 8821 | . 3225 | 55 | 35 | . 8764 | . 3291 | 25 |
| 6 | .8819 | . 3227 | 54 | 36 | . 8762 | . 3293 | 24 |
| 7 | .8817 | . 3230 | 53 | 37 | . 8760 | . 3296 | 23 |
| 8 | . 8815 | . 3232 | 52 | 38 | . 8758 | . 3298 | 22 |
| 9 | .8813 | . 3234 | 51 | 39 | . 8756 | . 3300 | 21 |
| 10 | .8811 | . 3236 | 50 | 40 | . 8754 | . 3302 | 20 |
| 11 | .8810 | . 3238 | 49 | 41 | . 8753 | . 3304 | 19 |
| 12 | . 8808 | . 3241 | 48 | 42 | .875I | . 3307 | 18 |
| 13 | . 8806 | . 3243 | 47 | 43 | . 8749 | . 3309 | 17 |
| 14 | . 8804 | . 3245 | 46 | 44 | . 8747 | -3311 | 16 |
| 15 | . 8802 | . 3247 | 45 | 45 | . 8745 | . 3313 | 15 |
| 16 | . 8800 | - 3249 | 44 | 46 | . 8743 | . 3315 | 14 |
| 17 | . 8798 | - 3252 | 43 | 47 | . 8741 | -3318 | 13 |
| 18 | . 8796 | . 3254 | 42 | 48 | . 8739 | . 3320 | 12 |
| 19 | . 8794 | - 3256 | 41 | 49 | . 8737 | - 3322 | 11 |
| 20 | . 8793 | . 3258 | 40 | 50 | . 8735 | - 3324 | 10 |
| 21 | . 8791 | -3261 | 39 | 51 | . 8733 | . 3326 |  |
| 22 | . 8789 | . 3263 | 38 | 52 | . 8731 | . 3328 | 8 |
| 23 | . 8787 | . 3265 | 37 | 53 | . 8729 | . 3331 | 7 |
| 24 | . 8785 | . 3267 | 36 | 54 | . 8727 | . 3333 | 6 |
| 25 | . 8783 | . 3269 | 35 | 55 | . 8725 | . 3335 | 5 |
| 26 | .8781 | . 3272 | 34 | 56 | . 8723 | . 3337 | 4 |
| 27 | . 8779 | . 3274 | 33 | 57 | . 8722 | - 3339 | 3 |
| 28 | . 8777 | . 3276 | 32 | 58 | . 8720 | . 3341 | 2 |
| 29 | . 8776 | . 3278 | 31 | 59 | . 8718 | . 3344 | 1 |
| 30 | . 8774 | . 3280 | 30 | 60 | . 8716 | . 3346 | - |
|  | $\begin{gathered} \text { Constant } \\ \text { for } \\ \text { Distance. } \end{gathered}$ | $\begin{gathered} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{gathered}$ | Minutes. |  | Constant for <br> Distance. | Constant for Difference in Height. | Minutes. |

69 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer
Readings-continued.

III DEGREES.

| Minutes. | Constant for <br> Distance. | $\begin{array}{\|c\|} \hline \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{array}$ |  | Minutes. | Constant for <br> Distance. | $\begin{array}{c}\text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. }\end{array}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 8716 | . 3346 | 60 | 30 | . 8657 | . 3410 | 30 |
| 1 | . 8714 | . 3348 | 59 | 31 | . 8655 | . 3412 | 29 |
| 2 | . 8712 | . 3350 | 58 | 32 | . 8653 | -3414 | 28 |
| 3 | . 8710 | . 3352 | 57 | 33 | . 8651 | . 3416 | 27 |
| 4 | . 8708 | - 3354 | 56 | 34 | . 8649 | -3419 | 26 |
| 5 | . 8706 | . 3356 | 55 | 35 | . 8647 | -3421 | 25 |
| 6 | . 8704 | . 3359 | 54 | 36 | . 8645 | . 3423 | 24 |
| 7 | . 8702 | . 3361 | 53 | 37 | . 8643 | . 3425 | 23 |
| 8 | . 8700 | . 3363 | 52 | 38 | . 8641 | . 3427 | 22 |
| 9 | . 8698 | . 3365 | 51 | 39 | . 8639 | . 3429 | 21 |
| 10 | . 8696 | . 3367 | 50 | 40 | . 8637 | . 3431 | 20 |
| 11 | . 8694 | . 3369 |  | 41 | . 8635 | . 3433 |  |
| 1.2 | . 8692 | . 3372 | 48 | 42 | . 8633 | . 3436 | 18 |
| 13 | . 8690 | . 3374 | 47 | 43 | . 8631 | . 3438 | 17 |
| 14 | . 8688 | . 3376 | 46 | 44 | . 8629 | . 3440 | 16 |
| 15 | . 8686 | . 3378 | 45 | 45 | . 8627 | . 3442 | 15 |
| 16 | . 8684 | . 3380 | 44 | 46 | . 8625 | . 3444 | 14 |
| 17 | . 8682 | .3382 | 43 | 47 | . 8623 | . 3446 | 13 |
| 18 | . 8680 | . 3384 | 42 | 48 | . 8621 | . 3448 | 12 |
| 19 | . 8678 | . 3387 | 41 | 49 | .8619 | . 3450 | 11 |
| 20 | . 8677 | . 3389 | 40 | 50 | .8617 | - 3452 | 10 |
| 21 | . 8675 | . 3391 | 39 | 51 | .8615 | . 3454 | 9 |
| 22 | . 8673 | . 3393 | 38 | 52 | .8613 | - 3457 | 8 |
| 23 | . 867 I | . 3395 | 37 | 53 | .86II | - 3459 | 7 |
| 24 | . 8669 | - 3397 | 36 | 54 | . 8609 | -3461 | 6 |
| 25 | . 8667 | . 3399 | 35 | 55 | . 8607 | - 3463 | 5 |
| 26 | . 8665 | -3402 | 34 | 56 | . 8605 | . 3465 | 4 |
| 27 | . 8663 | . 3404 | 33 | 57 | . 8603 | - 3467 | 3 |
| 28 | .866I | . 3406 | 32 | 58 | . 8601 | . 3469 | 2 |
| 29 | . 8659 | . 3408 | 31 | 59 | . 8599 | -3471 | 1 |
| 30 | . 8657 | . 3410 | 30 | 60 | . 8597 | - 3473 | - |
|  | Constant Distan <br> Distance. | $\begin{aligned} & \text { Constant } \\ & \text { for } \\ & \text { Difference } \\ & \text { in Height. } \end{aligned}$ | Minutes. |  | $\begin{gathered} \text { Constant } \\ \text { fistance. } \end{gathered}$ | $\begin{gathered} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{gathered}$ | Minutes. |

## Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

112 Degrees.

| Minutes. | Constant for Distance. | Constant for Difference in Height. |  | Minutes. | Constant for Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 8597 | - 3473 | 60 | 30 | . 8536 | . 3536 | 30 |
| 1 | . 8595 | . 3475 | 59 | 31 | . 8534 | . 3538 | 29 |
| 2 | . 8593 | - 3478 | 58 | 32 | . 8531 | - 3540 | 28 |
| 3 | . 8591 | . 3480 | 57 | 33 | . 8529 | . 3542 | 27 |
| 4 | . 8589 | . 3482 | 56 | 34 | . 8527 | . 3544 | 26 |
| 5 | . 8587 | . 3484 | 55 | 35 | . 8525 | \&3546 | 25 |
| 6 | .8585 | . 3486 | 54 | 36 | .8523 | . 3548 | 24 |
| 7 | . 8583 | . 3488 | 53 | - 37 | . 8521 | - 3550 | 23 |
| 8 | . 8581 | . 3490 | 52 | - 38 | . 8519 | . 3552 | 22 |
| 9 | . 8579 | . 3492 | 51 | 39 | .8517 | - 3554 | 2 I |
| 10 | .8576 | - 3494 | 50 | 40 | .8515 | -3556 | 20 |
| 11 | . 8574 | . 3496 | 49 | 41 | . 8513 | . 3558 | 19 |
| 12 | . 8572 | - 3498 | 48 | 42 | . 8511 | - 3560 | 18 |
| 13 | . 8570 | . 3500 | 47 | 43 | . 8509 | - 3562 | 17 |
| 14 | . 8568 | - 3503 | 46 | 44 | . 8507 | . 3564 | 16 |
| 15 | . 8566 | . 3505 | 45 | 45 | . 8505 | . 3566 | 15 |
| 16 | . 8564 | . 3507 | 44 | 46 | .8503 | - 3568 | 14 |
| 17 | . 8562 | . 3509 | 43 | 47 | . 8500 | - 3570 | 13 |
| 18 | . 8560 | .3511 | 42 | 48 | . 8498 | - 3572 | 12 |
| 19 | . 8558 | -3513 | 41 | 49 | . 8496 | . 3574 | II |
| 20 | . 8556 | . 3515 | 40 | 50 | . 8494 | . 3576 | 10 |
| 21 | . 8554 | . 3.517 | 39 |  | . 8492 | . 3578 |  |
| 22 | . 8552 | . 3519 | 38 | 52 | . 8490 | . 3581 | 8 |
| 23 | . 8550 | . 3521 | 37 | 53 | . 8488 | . 3583 | 7 |
| 24 | . 8548 | - 3523 | 36 | 54 | . 8486 | - 3585 | 6 |
| 25 | . 8546 | . 3525 | 35 | 55 | . 8484 | -3587 | 5 |
| 26 | .8544 | - 3527 | 34 | 56 | . 8482 | . 3589 | 4 |
| 27 | . 8542 | - 3529 | 33 | 57 | . 8480 | -3591 | 3 |
| 28 | . 8540 | - 3531 | 32 | 58 | . 8478 | - 3593 | 2 |
| 29 | . 8538 | - 3534 | 31 | 59 | . 8475 | - 3595 | I |
| 30 | . 8536 | - 3536 | 30 | 60 | . 8473 | - 3597 | 0 |
|  | Constant for Distance. | Constant for Difference in Height. | Minutes. |  | Constant for Distance. | Constant for Difference in Height. | Minutes. |

67 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

II3 Degrees.

| Minutes. | Constant Distan Distance. | Constant for Difference in Height. |  | Minutes. | Constant for <br> Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcirc$ | . 8473 | . 3597 | 60 | 30 | .8410 | . 3657 | 30 |
| 1 | . 8470 | . 3599 | 59 | 31 | . 8408 | . 3659 | 29 |
| 2 | . 8468 | . 3601 | 58 | 32 | . 8406 | . 3661 | 28 |
| 3 | . 8466 | . 3603 | 57 | 33 | . 8404 | . 3663 | 27 |
| 4 | . 8464 | -3605 | 56 | 34 | . 8401 | . 3665 | 26 |
| 5 | . 8463 | . 3607 | 55 | 35 | . 8399 | . 3667 | 25 |
| 6 | .846r | . 3609 | 54 | 36 | . 8397 | . 3669 | 24 |
| 7 | . 8459 | -36II | 53 | 37 | . 8395 | . 3671 | 23 |
| 8 | . 8457 | . 3613 | 52 | 38 | . 8393 | . 3673 | 22 |
| 9 | . 8454 | . 3615 | 51 | 39 | . 8391 | . 3675 | 21 |
| 10 | . 8452 | - 3617 | 50 | 40 | . 8389 | -3677 | 20 |
| 11 | . 8450 | . 3619 | 49 | 41 | . 8387 | . 3679 | 19 |
| 12 | . 8448 | . 3621 | 48 | 42 | . 8384 | . 3681 | 18 |
| 13 | . 8446 | . 3623 | 47 | 43 | . 8382 | - 3682 | 17 |
| 14 | . 8444 | . 3625 | 46 | 44 | . 8380 | . 3684 | 16 |
| 15 | . 8442 | . 3627 | 45 | 45 | . 8378 | . 3686 | 15 |
| 16 | . 8440 | . 3629 | 44 | 46 | . 8376 | . 3688 | 14 |
| 17 | . 8438 | . 3631 | 43 | 47 | . 8374 | . 3690 | 13 |
| 18 | . 8436 | . 3633 | 42 | 48 | . 8372 | . 3692 | 12 |
| 19 | . 8433 | . 3635 | 41 | 49 | . 8369 | . 3694 | 11 |
| 20 | . 843 I | . 3637 | 40 | 50 | . 8367 | . 3696 | 10 |
| 21 | . 8429 | . 3639 | 39 | 51 | . 8365 | . 3698 |  |
| 22 | . 8427 | . 3641 | 38 | 52 | . 8363 | . 3700 | 8 |
| 23 | . 8425 | . 3643 | 37 | 53 | . 8361 | . 3702 | 7 |
| 24 | . 8423 | . 3645 | 36 | 54 | . 8359 | . 3704 | 6 |
| 25 | . 842 I | . 3647 | 35 | 55 | . 8356 | . 3706 | 5 |
| 26 | . 8419 | . 3649 | 34 | 56 | . 8354 | . 3708 | 4 |
| 27 | . 8416 | . 3651 | 33 | 57 | . 8352 | . 3710 | 3 |
| 28 | . 8414 | . 3653 | 32 | 58 | . 8350 | . 3712 | 2 |
| 29 | . 8412 | . 3655 | 31 | 59 | . 8348 | . 3714 | 1 |
| 30 | . 8410 | . 3657 | 30 | 60 | . 8346 | . 3716 | - |
|  | Constant for Distance. | $\begin{aligned} & \text { Constant } \\ & \text { for } \\ & \text { Difference } \\ & \text { in Height. } \end{aligned}$ | Minutes. |  | Constant Distar <br> Distance. | Constant for Difference in Height. | Minutes. |

66 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

114 Degrees.

| Minutes. | Constant $\underset{\text { Distan }}{ }$ <br> Distance. | $\begin{aligned} & \text { Constant } \\ & \text { for } \\ & \text { Difference } \\ & \text { in Height. } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: |
| 0 | . 8346 | . 3716 | 60 |
| 1 | . 8344 | . 3718 | 59 |
| 2 | .8341 | . 3720 | 58 |
| 3 | . 8339 | - 3722 | 57 |
| 4 | . 8337 | . 3724 | 56 |
| 5 | . 8335 | . 3725 | 55 |
| 6 | . 8333 | . 3727 | 54 |
| 7 | . 8331 | . 3729 | 53 |
| 8 | . 8328 | . 3731 | 52 |
| 9 | . 8326 | . 3733 | 51 |
| 10 | . 8324 | $\bullet .3735$ | 50 |
| 11 | . 8322 | . 3737 | 49 |
| 12 | . 8320 | . 3739 | 48 |
| 13 | . 8318 | . 3741 | 47 |
| 14 | . 8315 | - 3743 | 46 |
| 15 | .8313 | - 3745 | 45 |
| 16 | . 8311 | . 3747 | 44 |
| 17 | . 8309 | . 3749 | 43 |
| 18 | . 8307 | . 3751 | 42 |
| 19 | . 8304 | - 3753 | 41 |
| 20 | . 8302 | - 3754 | 40 |
| 21 | . 8300 | . 3756 | 39 |
| 22 | . 8298 | - 3758 | 38 |
| 23 | . 8296 | . 3760 | 37 |
| 24 | . 8294 | - 3762 | 36 |
| 25 | . 8291 | . 3764 | 35 |
| 26 | . 8289 | . 3766 | 34 |
| 27 | . 8287 | . 3768 | 33 |
| 28 | . 8285 | - 3770 | 32 |
| 29 | . 8283 | - 3772 | 31 |
| 30 | . 8280 | - 3774 | 30 |
|  | Constant Dis Distance. | Constant for Difference in Height. | Minutes |


| Minutes. | Constant Distar Distance. | $\begin{array}{\|c\|} \begin{array}{c} \text { Constant } \\ \text { for } \\ \text { Diference } \\ \text { in Height. } \end{array} \\ \hline \end{array}$ |  |
| :---: | :---: | :---: | :---: |
| 30 | .8280 | . 3774 | 30 |
| 31 | . 8278 | . 3776 | 29 |
| 32 | . 8276 | . 3777 | 28 |
| 33 | . 8274 | - 3779 | 27 |
| 34 | . 8272 | . 3781 | 26 |
| 35 | . 8269 | . 3783 | 25 |
| 36 | . 8267 | . 3785 | 24 |
| 37 | . 8265 | . 3787 | 23 |
| 38 | . 8263 | . 3789 | 22 |
| 39 | . 8261 | . 3791 | 21 |
| 40 | . 8258 | - 3793 | 20 |
| 41 | . 8256 | -3794 | 19 |
| 42 | . 8254 | . 3796 | 18 |
| 43 | . 8252 | . 3798 | 17 |
| 44 | . 8249 | . 3800 | 16 |
| 45 | . 8247 | . 3802 | 15 |
| 46 | . 8245 | .3804 | 14 |
| 47 | . 8243 | . 3806 | 13 |
| 48 | . 8241 | . 3808 | 12 |
| 49 | . 8238 | . 3810 | II |
| 50 | . 8236 | . 3811 | 10 |
| 51 | . 8234 | .3813 | 9 |
| 52 | . 8232 | . 3815 | 8 |
| 53 | . 8230 | . 3817 |  |
| 54 | . 8227 | . 3819 | 6 |
| 55 | . 8225 | . 3821 | 5 |
| 56 | . 8223 | . 3823 | 4 |
| 57 | . 8221 | -3825 | 3 |
| 58 | . 8218 | . 3827 | 2 |
| 59 | . 8216 | -3828 | 1 |
| 60 | . 8214 | . 3830 | 0 |
|  | Constant for <br> Distance. | $\begin{aligned} & \text { Constant } \\ & \text { for } \\ & \text { Difference } \\ & \text { in Height. } \end{aligned}$ | Minutes. |

65 DEgREES.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

II5 DEGREES.

| Minutes. | Constant Dis <br> Distance. | $\begin{gathered} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{gathered}$ |  | Minutes. | Constant Distar <br> Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 8214 | . 3830 | 60 | 30 | .8147 | . 3886 | 30 |
| 1 | . 8212 | . 3832 | 59 | 31 | .8144 | . 3888 | 29 |
| 2 | . 8210 | . 3834 | 58 | 32 | . 8142 | . 3889 | 28 |
| 3 | . 8207 | . 3836 | 57 | 33 | .8140 | .3891 | 27 |
| 4 | . 8205 | . 3838 | 56 | 34 | .8138 | . 3893 | 26 |
| 5 | . 8203 | . 3840 | 55 | 35 | .8135 | . 3895 | 25 |
| 6 | .8201 | . 3841 | 54 | 36 | .8133 | . 3897 | 24 |
| 7 | .8198 | - 3843 | 53 | 37 | .813I | . 3899 | 23 |
| 8 | .8196 | . 3845 | 52 | 38 | .8128 | . 3900 | 22 |
| 9 | .8194 | . 3847 | 51 | 39 | . 8126 | . 3902 | 21 |
| 10 | .8192 | . 3849 | 50 | 40 | .8124 | . 3904 | 20 |
| 11 | . 8189 | . 3851 | 49 | 41 | .8122 | . 3906 |  |
| 12 | . 8187 | . 3853 | 48 | 42 | .8119 | . 3908 | 18 |
| 13 | .8185 | . 3854 | 47 | 43 | . 8117 | . 3909 | 17 |
| 14 | . 8182 | . 3856 | 46 | 44 | .8115 | -3911 | 16 |
| 15 | .8180 | . 3858 | 45 | 45 | .8r13 | . 3913 | 15 |
| 16 | . 8178 | . 3860 | 44 | 46 | .8110 | . 3915 | 14 |
| 17 | . 8176 | . 3862 | 43 | 47 | .8108 | . 3917 | 13 |
| 18 | .8174 | . 3864 | 42 | 48 | . 8106 | . 3919 | 12 |
| 19 | .8171 | . 3866 | 41 | 49 | . 8103 | . 3920 | 11 |
| 20 | .8169 | . 3867 | 40 | 50 | .8101 | - 3922 | 10 |
| 21 | . 8167 | . 3869 | 39 | 51 | . 8099 | . 3924 |  |
| 22 | .8165 | . 387 I | 38 | 52 | . 8097 | . 3926 | 8 |
| 23 | .8163 | - 3873 | 37 | 53 | . 8094 | . 3928 | 7 |
| 24 | .8160 | - 3875 | 36 | 54 | . 8092 | - 3929 | 6 |
| 25 | .8158 | -3877 | 35 | 55 | . 8090 | -393I | 5 |
| 26 | .8156 | . 3878 | 34 | 56 | . 8088 | - 3933 |  |
| 27 | .8154 | . 3880 | 33 | 57 | . 8085 | - 3935 | 3 |
| 28 | . 8151 | . 3882 | 32 | 58 | . 8083 | . 3937 | 2 |
| 29 | . 8149 | . 3884 | 31 | 59 | . 808 I | . 3938 | 1 |
| 30 | .8147 | - 3886 | 30 | 60 | . 8078 | . 3940 | - |
|  | Constant for <br> Distance. | $\begin{aligned} & \text { Constant } \\ & \text { for } \\ & \text { Difference } \\ & \text { in Height. } \end{aligned}$ | Minutes. |  | Constant for Distance. | Constant for Difference in Height. | Minutes. |

64 Degrees.

## Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

II6 Degrees.

| Minutes. | Constant for Distance. | Constant for Difference in Height. |  | Minutes. | Constant for Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 8078 | . 3940 | 60 | 30 | . 8009 | - 3993 | 30 |
| I | . 8076 | - 3942 | 59 | 3 I | . 8007 | . 3995 | 29 |
| 2 | . 8074 | . 3944 | 58 | 32 | . 8004 | - 3997 | 28 |
| 3 | . 8071 | - 3946 | 57 | 33 | . 8002 | . 3998 | 27 |
| 4 | . 8069 | - 3947 | 56 | 34 | . 8000 | . 4000 | 26 |
| 5 | . 8067 | . 3949 | 55 | 35 | . 7998 | . 4002 | 25 |
| 6 | . 8065 | -395I | 54 | 36 | . 7995 | . 4004 | 24 |
| 7 | . 8062 | . 3953 | 53 | 37 | . 7993 | . 4005 | 23 |
| 8 | . 8060 | . 3954 | 52 | 38 | . 7991 | . 4007 | 22 |
| 9 | . 8058 | - 3956 | 51 | 39 | . 7988 | .4009 | 2 I |
| 10 | . 8055 | - 3958 | 50 | 40 | . 7986 | . 401 I | 20 |
| I I | . 8053 | . 3960 | 49 | 41 | . 7984 | . 4012 | 19 |
| 12 | .8051 | . 3962 | 48 | 42 | . 7981 | . 4014 | 18 |
| 13 | . 8048 | - 3963 | 47 | 43 | . 7979 | . 4016 | 17 |
| 14 | . 8046 | - 3965 | 46 | 44 | . 7976 | . 4018 | 16 |
| I 5 | . 8044 | - 3967 | 45 | 45 | . 7974 | . 4019 | I 5 |
| 16 | . 8042 | . 3969 | 44 | 46 | . 7972 | . 402 I | 14 |
| 17 | . 8039 | - 3970 | 43 | 47 | . 7970 | .4023 | 13 |
| 18 | . 8037 | . 3972 | 42 | 48 | . 7967 | . 4025 | 12 |
| 19 | . 8035 | - 3974 | 41 | 49 | . 7965 | . 4026 | 11 |
| 20 | . 8032 | . 3976 | 40 | 50 | . 7962 | . 4028 | 10 |
| 21 | . 8030 | . 3977 | 39 | 51 | . 7960 | . 4030 |  |
| 22 | . 8028 | -. 3979 | 38 | 52 | . 7958 | . 4031 | 8 |
| 23 | . 8025 | . 3981 | 37 | 53 | . 7955 | . 4033 | 7 |
| 24 | . 8023 | - 3983 | 36 | 54 | . 7953 | . 4035 | 6 |
| 25 | . 8021 | - 3984 | 35 | 55 | . 795 I | . 4037 | 5 |
| 26 | . 8018 | . 3986 | 34 | 56 | . 7948 | . 4038 | 4 |
| 27 | . 8016 | . 3988 | 33 | 57 | . 7946 | . 4040 | 3 |
| 28 | . 8014 | - 3990 | 32 | 58 | . 7944 | . 4042 | 2 |
| 29 | . 8011 | . 3991 | 31 | 59 | . 7941 | . 4043 | 1 |
| 30 | . 8009 | - 3993 | 30 | 60 | . 7939 | . 4045 | 0 |
|  | Constant for Distance. | Constant for Difference in Height. | Minutes. |  | Constant for Distance. | Constant for Difference in Height. | Minutes. |

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

II7 DEGREES.

| Minutes. | Constant for Distance. | Constant for Difference in Height. |  | Minutes. | Constant for Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 7939 | . 4045 | 60 | 30 | .7868 | . 4096 | 30 |
| 1 | . 7937 | . 4047 | 59 | 31 | . 7866 | . 4098 | 29 |
| 2 | . 7934 | . 4049 | 58 | 32 | . 7863 | . 4099 | 28 |
| 3 | . 7932 | . 4050 | 57 | 33 | .786I | . 4101 | 27 |
| 4 | . 7930 | . 4052 | 56 | 34 | .7858 | .4102 | 26 |
| 5 | . 7927 | . 4054 | 55 | 35 | .7857 | .4104 | 25 |
| 6 | . 7925 | . 4055 | 54 | 36 | .7854 | .4106 | 24 |
| 7 | . 7922 | . 4057 | 53 | 37 | .7851 | . 4107 | 23 |
| 8 | . 7920 | . 4059 | 52 | 38 | . 7849 | .4109 | 22 |
| 9 | .7918 | . 4060 | 51 | 39 | . 7846 | .4III | 2 I |
| 10 | .7915 | . 4062 | 50 | 40 | .7844 | .4112 | 20 |
| II | . 7913 | .4064 | 49 | 41 | .7842 | .4114 | 19 |
| 12 | .7911 | . 4066 | 48 | 42 | . 7839 | .4116 | 18 |
| 13 | . 7908 | . 4067 | 47 | 43 | . 7837 | .4117 | 17 |
| 14 | . 7906 | . 4069 | 46 | 44 | . 7835 | . 4119 | 16 |
| 15 | . 7904 | . 407 I | 45 | 45 | .7832 | .412I | 15 |
| 16 | . 7901 | . 4072 | 44 | 46 | .7830 | . 4122 | 14 |
| 17 | . 7899 | . 4074 | 43 | 47 | .7827 | . 4124 | 13 |
| 18 | . 7896 | . 4076 | 42 | 48 | . 7825 | .4126 | 12 |
| 19 | . 7894 | . 4077 | 41 | 49 | . 7822 | .4127 | 11 |
| 20 | . 7892 | .4079 | 40 | 50 | . 7820 | .4129 | 10 |
| 21 | .7889 | . 4081 | 39 | 51 | . 7818 |  |  |
| 22 | .7887 | .4082 | 38 | 52 | . 7815 | .4132 | 8 |
| 23 | .7885 | . 4084 | 37 | 53 | .7813 | . 4134 | 7 |
| 24 | . 7882 | . 4086 | 36 | 54 | .7810 | .4135 | 6 |
| 25 | . 7880 | .4087 | 35 | 55 | . 7808 | .4137 | 5 |
| 26 | .7877 | .4089 | 34 | 56 | .7806 | . 4139 |  |
| 27 | . 7875 | . 4091 | 33 | 57 | .7803 | . 4140 | 3 |
| 28 | . 7873 | . 4092 | 32 | 58 | . 7801 | .4142 | 2 |
| 29 | . 7870 | . 4094 | 31 | 59 | . 7798 | . 4144 | 1 |
| 30 | .7868 | . 4096 | 30 | 60 | . 7796 | . 4145 | 0 |
|  | Constant for Distance. | Constant for Difference in Height. | Minutes. |  | Constant for Distance. | Constant for Difference in Height. | Minutes. |

62 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

II8 Degrees.

| Minutes. | Constant for Distance. | Constant for Difference in Height. |  | Minutes. | Constant for Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 7796 | . 4145 | 60 | 30 | .7723 | .4193 | 30 |
| 1 | . 7794 | .4147 | 59 | 3 I | . 7721 | . 4195 | 29 |
| 2 | . 7791 | . 4149 | 58 | 32 | . 7718 | . 4197 | 28 |
| 3 | . 7789 | . 4150 | 57 | 33 | . 7716 | .4198 | 27 |
| 4 | . 7786 | . 4152 | 56 | 34 | .7713 | . 4200 | 26 |
| 5 | . 7784 | . 4153 | 55 | 35 | .7711 | . 4201 | 25 |
| 6 | .7782 | .4155 | 54 | 36 | .7709 | . 4203 | 24 |
| 7 | . 7779 | . 4157 | 53 | 37 | . 7706 | . 4204 | 23 |
| 8 | . 7777 | . 4158 | 52 | 38 | . 7704 | . 4206 | 22 |
| 9 | . 7774 | . 4160 | 5 I | 39 | . 7701 | . 4208 | 21 |
| 10 | . 7772 | . 4162 | 50 | 40 | .7699 | . 4209 | 20 |
| II | .7769 | .4163 | 49 | 41 | .7696 | .42II | 19 |
| 12 | .7767 | .4165 | 48 | 42 | . 7694 | . 4212 | 18 |
| 13 | .7765 | . 4166 | 47 | 43 | . 7692 | . 4214 | 17 |
| 14 | .7762 | . 4168 | 46 | 44 | . 7689 | . 4215 | 16 |
| 15 | .7760 | .4169 | 45 | 45 | .7687 | . 4217 | 15 |
| 16 | . 7757 | .4171 | 44 | 46 | .7684 | . 4219 | 14 |
| 17 | . 7755 | . 4173 | 43 | 47 | . 7682 | . 4220 | 13 |
| 18 | . 7752 | . 4174 | 42 | 48 | . 7679 | . 4222 | 12 |
| 19 | . 7750 | . 4176 | 41 | 49 | . 7677 | . 4223 | 11 |
| 20 | . 7748 | . 4177 | 40 | 50 | .7674 | .4225 | 10 |
| 21 | . 7745 | . 4179 | 39 | 51 | .7672 | . 4226 | 9 |
| 22 | . 7743 | -.418I | 38 | 52 | .7669 | . 4228 | 8 |
| 23 | . 7740 | . 4182 | 37 | 53 | . 7667 | . 4230 | 7 |
| 24 | . 7738 | .4184 | 36 | 54 | . 7664 | . 4231 | 6 |
| 25 | . 7735 | .4185 | 35 | 55 | . 7662 | . 4233 | 5 |
| 26 | . 7733 | .4187 | 34 | 56 | . 7659 |  |  |
| 27 | . 7731 | . 4189 | 3.3 | 57 | . 7657 | .4236 | 3 |
| 28 | . 7728 | . 4190 | 32 | 58 | . 7655 | . 4237 | 2 |
| 29 | - 7726 | . 4192 | 3 I | 59 | . 7652 | . 4239 | 1 |
| 30 | .7723 | .4193 | 30 | 60 | .7650 | . 4240 | $\bigcirc$ |
| , | Constant for Distance. | Constant for Difference in Height. | Minutes. |  | Constant for Distance. | Constant for Difference in Height. | Minutes. |

6I Degrees.

Table for the Calculation of Heights and Distances from Tacheometer
Readings-continued.

## 119 Degrees.

| Minutes. | Constant for <br> Distance. | $\begin{array}{\|c} \text { Constant } \\ \text { for } \\ \text { Difference } \\ \text { in Height. } \end{array}$ |  |
| :---: | :---: | :---: | :---: |
| $\bigcirc$ | . 7650 | . 4240 | 60 |
| 1 | . 7647 | . 4242 | 59 |
| 2 | .7645 | . 4243 | 58 |
| 3 | . 7642 | . 4245 | 57 |
| 4 | . 7640 | . 4246 | 56 |
| 5 | .7637 | . 4248 | 55 |
| 6 | . 7635 | . 4250 | 54 |
| 7 | .7632 | . 4251 | 53 |
| 8 | . 7630 | . 4253 | 52 |
| 9 | . 7627 | . 4255 | 51 |
| 10 | . 7625 | . 4256 | 50 |
| 11 | .7622 | . 4257 | 49 |
| 12 | . 7620 | . 4259 | 48 |
| 13 | .7617 | . 4260 | 47 |
| 14 | .7615 | . 4262 | 46 |
| 15 | .76I3 | . 4263 | 45 |
| 16 | .7610 | . 4265 | 44 |
| 17 | . 7608 | . 4266 | 43 |
| 18 | .7605 | . 4268 | 42 |
| 19 | . 7603 | . 4269 | 41 |
| 20 | .7600 | .4271 | 40 |
| 21 | . 7598 | . 4272 | 39 |
| 22 | . 7595 | . 4274 | 38 |
| 23 | . 7593 | . 4275 | 37 |
| 24 | . 7590 | . 4277 | 36 |
| 25 | . 7588 | . 4278 | 35 |
| 26 | .7585 | . 4280 | 34 |
| 27 | .7583 | . 4281 | 33 |
| 28 | . 7580 | . 4283 | 32 |
| 29 | . 7578 | . 4284 | 31 |
| 30 | . 7575 | . 4286 | 30 |
|  | Constant <br> Distance. | Constant <br> Difference <br> in Height. | Minutes. |


| Minutes. | Constant for <br> Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: |
| 30 | . 7575 | . 4286 | 30 |
| 31 | . 7573 | . 4287 | 29 |
| 32 | . 7570 | . 4289 | 28 |
| 33 | . 7568 | . 4290 | 27 |
| 34 | . 7565 | . 4292 | 26 |
| 35 | . 7563 | . 4293 | 25 |
| 36 | . 7560 | . 4295 | 24 |
| 37 | . 7558 | . 4296 | 23 |
| 38 | . 7555 | . 4298 | 22 |
| 39 | . 7553 | . 4299 | 21 |
| 40 | . 7550 | -4301 | 20 |
| 41 | . 7548 | . 4302 | 19 |
| 42 | . 7545 | . 4304 | 18 |
| 43 | . 7543 | -4305 | 17 |
| 44 | . 7540 | . 4307 | 16 |
| 45 | .7538 | . 4308 | 15 |
| 46 | . 7535 | . 4310 | 14 |
| 47 | . 7533 | .431I | 13 |
| 48 | . 7530 | . 4313 | 12 |
| 49 | . 7528 | . 4314 | 11 |
| 50 | . 7525 | . 4316 | 10 |
| 51 | .7523 | . 4317 | 9 |
| 52 | . 7520 | .4318 | 8 |
| 53 | .7518 | . 4320 |  |
| 54 | .7515 | .4321 | 6 |
| 55 | .7513 | . 4323 | 5 |
| 56 | .7510 | . 4324 | 4 |
| 57 | . 7508 | . 4326 | 3 |
| 58 | . 7505 | -4327 | 2 |
| 59 | . 7503 | . 4329 | 1 |
| 60 | . 7500 | . 4330 | - |
|  | Constant <br> Distance. | Constant for Difference in Height. | Minutes. |

60 Degrees.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

120 DEGREES.

| Minutes. | Constant for <br> Distance. | Constant for Difference in Height. |  | Minutes. | Constant for Distance. | Constant for Difference in Height. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 7500 | . 4330 | 60 | 30 | .7424 | . 4373 | 30 |
| 1 | . 7498 | . 4332 | 59 | 31 | . 7422 | . 4375 | 29 |
| 2 | . 7495 | . 4333 | 58 | 32 | . 7419 | . 4376 | 28 |
| 3 | . 7492 | . 4335 | 57 | 33 | . 7416 | . 4377 | 27 |
| 4 | . 7490 | . 4336 | 56 | 34 | .7414 | . 4379 | 26 |
| 5 | . 7487 | . 4337 | 55 | 35 | .74II | . 4380 | 25 |
| 6 | . 7485 | . 4339 | 54 | 36 | . 7409 | . 4382 | 24 |
| 7 | . 7482 | . 4340 | 53 | 37 | . 7406 | . 4383 | 23 |
| 8 | . 7480 | . 4342 | 52 | 38 | . 7404 | . 4384 | 22 |
| 9 | - 7477 | . 4343 | 51 | 39 | . 7401 | . 4386 | 2 I |
| 10 | . 7475 | . 4345 | 50 | 40 | . 7399 | . 4387 | 20 |
| 11 | . 7472 | . 4346 | 49 | 4I | .7396 | . 4389 | 19 |
| 12 | . 7470 | . 4348 | 48 | 42 | . 7394 | . 4390 | 18 |
| 13 | . 7467 | . 4349 | 47 | 43 | .7391 | . 4391 | 17 |
| 14 | . 7466 | . 4350 | 46 | 44 | . 7388 | . 4393 | 16 |
| 15 | . 7462 | . 4352 | 45 | 45 | . 7386 | . 4394 | I 5 |
| 16 | . 7460 | . 4353 | 44 | 46 | . 7383 | . 4396 | 14 |
| 17 | . 7457 | . 4355 | 43 | 47 | .7381 | . 4397 | 13 |
| 18 | . 7455 | . 4356 | 42 | 48 | . 7378 | . 4398 | 12 |
| 19 | . 7452 | . 4358 | 41 | 49 | . 7376 | . 4400 | II |
| 20 | . 7449 | . 4359 | 40 | 50 | . 7373 | . 4401 | 10 |
| 21 | . 7447 | . 4360 | 39 | 51 | . 7370 | . 4402 | 9 |
| 22 | . 7444 | . 4362 | 38 | 52 | . 7368 | . 4404 | 8 |
| 23 | . 7442 | . 4363 | 37 | 53 | . 7365 | . 4405 | 7 |
| 24 | . 7439 | . 4365 | 36 | 54 | . 7363 | . 4407 | 6 |
| 25 | . 7437 | . 4366 | 35 | 55 | . 7360 | . 4408 | 5 |
| 26 | . 7434 | . 4368 | 34 | 56 | . 7358 | . 4409 | 4 |
| 27 | . 7432 | . 4369 | 33 | 57 | . 7355 | . 44 I I | 3 |
| 28 | . 7429 | . 4370 | 32 | 58 | . 7353 | . 4412 | 2 |
| 29 | .7427 | . 4372 | 3 I | 59 | . 7350 | . 4413 | I |
| 30 | . 7424 | . 4373 | 30 | 60 | . 7347 | . 4415 | 0 |
|  | Constant for Distance. | Constant for Difference in Height. | Minutes. |  | Constant for Distance. | Constant for Difference in Height. | Minutes. |

59 Degrees.

## SECTION V. TABLE OF CHORDS.

## The Accurate Plotting of Angles on Large Scale Plans by means of Chords.

The Table of Chords furnishes a means of laying down angles on paper more accurately than by an ordinary protractor. The procedure is as follows: after having drawn and measured the first side (say $a c$ ) of the figure to be plotted, describe from its end $c$ as a centre, an arc $n y$ of sufficient length to subtend the angle at that point. The radius $c n$ with which the arc is described should be as great as convenience will permit. It must be decimally sub-divided, to be used as a scale for laying down the


Fig. 3.
chords taken from the table, in which their lengths are given in terms of the radius taken as 1. Having described the arc, find in the table the length of the chord $n t$ corresponding to the angle act. Suppose this angle to be $45^{\circ}$, the corresponding chord is .7654 . Therefore from $n$ lay off the chord $n t$, equal to .7654 of the radius-scale; and the line cs drawn through the point $t$ will form the required angle act of $45^{\circ}$. The degree of accuracy attained will evidently depend on the length of the radius, and the care taken in drafting. The dividers in boxes of instruments are rarely fit for accurate arcs of more than about 6 inches diameter. For larger radii the beam compass is the best instrument to use, or if not obtainable, a straight strip of paper with the length of the radius marked on one edge ; by laying it from $c$ toward $s$, and at the same time placing another strip (with one edge divided to a radius-scale) from $n$ toward $t$, we can by trial find their exact point of intersection at the required point $t$. The fastest method of plotting the chords is by the use of a beam-compass and $a \frac{1}{1000}$ scale, the compass being set to the length of the scale.

Table of Chords，in parts of a radius I；for protracting．

| 棠 | $\bigcirc$－$+\cdots \infty 0$ |  | Ṅন | N్ల్ల్ల్ల口 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 악 |  |  $\stackrel{\wedge}{\square} \hat{\sim}$ |  |  | ㄴNㅇNㅇ $\underset{\sim}{\infty} \rightarrow \infty$ |  |
| ¢ | 운둥 싱ㅇ <br>  |  | Noల్ల゚윤 은ํํํํ | Nơ to toin | 정성얀 은욱숙 | iN N |
| $\infty$ |  |  |  | m | Amoyo $\because ำ ํ$ | 넝№ ㄴ․ッ․ |
| ： |  | 엉్ㅓㅇㅓN N్N్N | 뚜ㄴㅒㅒ․ |  | Nowno | Nopmon ッッッット |
| $\bigcirc$ |  |  |  |  |  |  |
| is |  |  |  |  |  | Nowno 웅 |
| ¢ |  | M 성으응 |  |  |  |  |
| $\bigcirc$ |  <br>  | かす웅 웅으응 | $\begin{aligned} & \text { moun Mo } \\ & \text { minhiob } \\ & \text { OMo } \end{aligned}$ |  |  |  |
| ® |  |  |  |  |  |  |
| $\bigcirc$ | no N Nós す <br>  |  | 억운Nㅜㅇ <br>  |  | Noop |  |
| $\bigcirc$ |  |  |  | $\begin{aligned} & \text { たơ으을 } \\ & \text { Bo } \end{aligned}$ | Now ơo io |  |
| 品 | －N $+\infty \infty$ |  |  | N్ల్ల్ల¢ | ブサ¢ |  |

Table of Chords，in parts of a radius 1 ；for protracting． （Continued．）

| 㦴 | $\bigcirc \times+\infty \infty$ | $\underset{\sim}{\text { Now }}$ | Nત弋్N®্N O | N్ల్ల్ల్ల్ర |  | N4．400 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ¢\％ |  |  |  | 꿍ㅇㅇ లొల్ల゙ల |  |  |
| $\stackrel{\circ}{\circ}$ | $\begin{array}{ll} \text { D్ల్లN్ల్లN్ల్ల్ల్ల } \end{array}$ |  | $\begin{aligned} & \text { पipow } \\ & \text { స్ల్ల్ల్ల్ల్ల్ల్ల } \end{aligned}$ |  |  |  |
| $\stackrel{\infty}{\sim}$ |  <br>  | $\begin{aligned} & \text { ouno ino } \\ & \text { mencen } \end{aligned}$ |  | N్N్N్ల్ల్ల్ల్ల్ల్లు |  |  |
| $\stackrel{i}{\text { in }}$ |  |  | 잉N్ల －్ల్ల్ల్ | क 낭ㅇㅇㅇㅇㅇ －M్ల్ల్ల్ల | 성ㅇㅇㅇ －్ల్ల్లM |  |
| $\stackrel{\square}{\square}$ |  |  |  |  |  |  |
| $\stackrel{10}{10}$ |  |  |  |  |  |  |
| $\stackrel{\circ}{\text { H }}$ |  |  |  |  | 엉ㅇㅇㅇ웅 <br>  |  |
| $\stackrel{\sim}{\sim}$ | すo 우웅 <br> స్ ત્ત્તૅస్ તે | 운ㅇํㄴN สัヘึพฺ๙ึ |  |  |  |  |
| ๙ิ |  |  |  |  |  |  |
| $\stackrel{\circ}{-1}$ |  かo ooogo | Niñon |  |  | － |  |
| 告 | $\bigcirc{ }^{\circ}+\cdots \infty$ O | N ホーツoio | NָN0 ${ }_{\text {Now }}$ | N్ల్ల్ల¢ |  | N゙W゙い |

Table of Chords，in parts of a radius 1 ；for protracting． （Continued．）

| $\begin{aligned} & \hline{ }_{0}^{3} \\ & \text { B } \\ & \\ & \hline \end{aligned}$ | －N $+\cdots \infty$ |  |  |  | ボササ¢ | N14000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ®－8 | 웅 <br>  | $\begin{aligned} & \text { 얼 NㅓN } \\ & \text { Nun } \end{aligned}$ |  |  | 아으를 <br>  | N్ల్ల్ల్ల్ల్ <br>  |
| $\stackrel{\text { as }}{ }$ | oma甘o 유 o 응응ㅇㅇ | F fon 느는은 |  | $\begin{aligned} & \text { ono no } \\ & \text { on on } \\ & \text { Binctin } \end{aligned}$ | No |  느느ํํํํำ |
| $\stackrel{\sim}{\sim}$ |  $\stackrel{\infty}{+\infty}+\underbrace{\infty}_{+}+\square$ |  |  |  |  | 뜽웅子 $\ddagger 寸{ }^{\circ}$ |
| 는 |  |  |  |  |  |  |
| ¢ |  |  | － チケ寸サ |  |  |  |
| 옹 |  デサザデヂチ |  |  | ouñoño |  |  |
| H |  |  |  |  |  |  |
| ® | がのダす은 |  | ¢ |  |  |  |
| สู |  | 안숭ㅇㅇN N్లాల్లా్లా |  | $\begin{aligned} & \text { onaino } \\ & \text { ద్ల్ల్ల్ల్ల్ల } \end{aligned}$ |  | 능사웅웅 శ్ల్ల్ల్ల్ల్ల |
| － | ヱ유눙웅 ర్ల్ల్ల్రా్లర్ల్ల్ల | $\begin{aligned} & \text { ounoిo N } \\ & \text { O్ల్ల్ల్ల్ల్ల్ల్ల } \end{aligned}$ | 웅NNN ल్ల్లోल | m No, Mni ल్లিल్య | 둥ㅇํㅅNㅒ స్ల్ల్స్ల్ | $\begin{aligned} & \text { nowou } \\ & \text { Nopen ow } \end{aligned}$ |
| $\begin{aligned} & \text { y } \\ & \text { y } \\ & \text { B } \end{aligned}$ | $\bigcirc \times+\infty \times$ | N 寸 | Nָ | N్ల్ల్లై¢ |  |  |



Table of Chords，in parts of a radius I；for protracting． （Continued．）

| 年 |  | 머네N | N సָ ${ }^{\circ} \times$ |  | ボずが品 | Nuticin |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\therefore$ |  |  $\infty \infty$ |  | pend fix | గ్రే న్రి $\infty \infty \infty \infty$ |  |
| \％ | 흥ㅇㅇㄴ దీ o © |  |  <br>  |  |  |  |
| \％ |  |  |  |  |  |  |
| \％ |  |  |  |  |  |  |
| \％ | にo 뉴융 <br>  |  |  <br> 옷웃ํ | $\begin{aligned} & 8 \\ & 8 \\ & 8 \end{aligned}$ | $1$ | Hotitiontion |
| \％ 7 |  사운융웅 | out iod | Nox cicim <br> 솟NN송 | 子と운が 소솟소 | ®NN 소소소․ | ๙ơさoun 소숫ํํ |
| \％ |  ＋순산 |  <br> 손ㄴํㄴํㄴ | 낸ㄴㅇㅇㅇㅇㅇN 수ํํํㅅํ | ～が |  |  |
| \％ | ㅇ్లోల్లు คกำกำ |  |  | KN N్ No | 寺过过 |  |
| \％ | 氝 ํํํํํํํ |  |  |  |  กำกำ |  |
| $\stackrel{7}{7}$ |  | 人户⿱丶万卜 No | すioni ioioio |  |  |  |
| . |  | 저우ㅇㅜㅜ |  |  |  | 바낭inc |


| Table of Chords，in parts of a radius I ；for protracting． （Continued．） |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 崖 | －atomo | ロ ป ¢ ¢ |  | －\＃¢ ¢ ¢ ¢ |  | 넊ํํํ 8 |
| \％ |  |  |  | Bog oig ob |  | \| |
| \％ |  |  |  |  | Hig iosp iot | \％åo ehe |
| \％ |  |  |  | Nơo moig | Ong mox ex ex ex |  |
| \％ |  <br>  | Aotiodot | ిigeteng ig |  |  |  |
| \％ |  |  |  |  |  |  |
| \％ | － |  |  |  |  |  |
| \％ |  | E® |  |  |  |  |
| \％ |  | Mise iso |  |  |  | \％ |
| \％ |  Co． | ®ita | ※゙ロ |  |  |  |
| $\stackrel{\square}{5}$ |  |  |  |  |  | Finin |
|  | $\bigcirc 0+7000$ | ホ オ ¢ ¢ O |  | ¢ $\ddagger$ ¢ |  | 난ํํ 8 |

Table of Chords，in parts of a radius I ；for protracting． （Continued．）

| 戒 | $\bigcirc$ N $+\infty \times 0$ |  |  | N్ల్ల్లెల |  | N゙以 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcirc$ |  |  |  |  ざぎぎき | 산웅 ジぎき ガューュ゙ |  |
| 8 |  <br>  | N్ల్లిం్ల్ల్ల్MN نـ |  |  |  |  |
| $\stackrel{\infty}{\infty}$ |  |  |  |  |  |  |
| $\stackrel{\square}{\circ}$ |  |  |  |  |  |  |
| ® | ooso Hix |  |  |  |  |  |
| 요 |  | 승뭉웅웅 |  | OO |  |  |
| \＃̇ |  |  |  |  |  |  |
| ¢ \％ |  |  |  | oón ion |  | 성어앵웅 <br>  |
| ¢ |  |  |  |  |  | ƠO Ơ Ơ Ơ Ơ Ơ |
| $\stackrel{\circ}{6}$ |  |  |  |  |  |  |
| $\frac{\pi}{E}$ | $\bigcirc \mathrm{N}+\mathrm{O}_{0}$ O | Nサー№ㅇ |  | N్ల్ల్ల¢ |  |  |


| 聝 | $\bigcirc \mathrm{O}+6 \infty$ O | Nポ心め |  | N్ల్ల్ల్ల | ソ寸¢＋ | N－4tiois |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\stackrel{\circ}{\circ}$ |  |  |  |  |  |  |
| $\stackrel{\circ}{\circ}$ | N゚्N ming <br>  |  <br>  |  |  |  | がッチ゚ か్No ベッ～～～～ |
| $\stackrel{\circ}{\circ}$ |  |  |  |  |  |  |
| $\stackrel{\circ}{\circ}$ |  |  |  |  |  |  |
| \％ | $\cdots{ }^{2} \times{ }^{-1}$ <br>  ガッジゥ |  |  |  |  |  |
| 은 |  |  |  |  |  |  |
| 过 |  |  |  |  |  |  |
| 운 |  |  |  |  |  |  |
| ำ |  |  |  |  |  |  |
| $\stackrel{\sim}{-}$ |  |  |  |  |  |  |
|  | 0 －$+\cdots \infty$ O | N サー |  | N్ల్లాగ్ర | ソ寸 |  |

Table of Chords，in parts of a radius 1 ；for protracting． （Continued．）

| 坒 | ON＋600 |  |  | N్ల్ల్ల్ర |  | N゙W00008 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ® |  |  |  |  |  |  |
| $\pm$ |  |  |  |  |  | No ơo |
| $\stackrel{\circ}{\infty}$ | 솟ㅇㅇ ${ }^{+\infty}$ <br>  <br>  |  |  |  |  |  |
| $\stackrel{\circ}{\circ}$ |  |  |  |  |  | 넌№̂ స్లిल్లో ガュージュ |
| $\stackrel{\circ}{\circ}$ |  |  | ㅇํ응ํ n은NN －～～～～～ |  |  |  |
| ＋ |  |  |  | N్రియి i్రి |  |  |
| ¢ ¢ |  |  |  |  |  |  |
| ® |  |  |  |  |  |  |
| $\stackrel{\circ}{\infty}$ |  |  |  |  |  |  |
|  | $\bigcirc$ O $+\cdots \infty$ O | Nポロ～～～ |  | N్ల్ర్ల్ల口 |  |  |

## APPENDIX.

Table giving the circumference and area of a circle corresponding to a given diameter.*

| Diameter. | Circum. ference. | Area. | Diameter. | Circumference. | Area. | Diameter. | Circum. ference. | Area. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 31.416 | 78.5398 | 40 | 125.66 | 1256.64 | 70 | 219.91 | 3848.45 |
| I I | 34.558 | 95.0332 | 41 | 128.81 | I320.25 | 71 | 223.05 | 3959.19 |
| 12 | 37.699 | 113.097 | 42 | 131.95 | I 385.44 | 72 | 226.19 | 4071.50 |
| 13 | 40.84 I | 132.732 | 43 | 135.09 | 1452.20 | 73 | 229.34 | 4185.39 |
| 14 | 43.982 | 153.938 | 44 | 138.23 | I 520.53 | 74 | 232.48 | 4300.84 |
| 15 | 47.124 | 176.715 | 45 | 141.37 | I 590.43 | 75 | 235.62 | 4417.86 |
| 16 | 50.265 | 201.062 | 46 | 144.51 | 1661.90 | 76 | 238.76 | 4536.46 |
| 17 | 53.407 | 226.980 | 47 | 147.65 | I734.94 | 77 | 241.90 | 4656.63 |
| 18 | 56.549 | 254.469 | 48 | 150.80 | 1809.56 | 78 | 245.04 | 4778.36 |
| 19 | 59.690 | 283.529 | 49 | 153.94 | 1885.74 | 79 | 248.19 | 4901.67 |
| 20 | 62.832 | 314.159 | 50 | I 57.08 | 1963.50 | 80 | 251.33 | 5026.55 |
| 21 | 65.973 | 346.361 | 51 | 160.22 | 2042.82 | 81 | 254.47 | 5153.00 |
| 22 | 69.115 | 380.133 | 52 | 163.36 | 2123.72 | 82 | 257.6I | 5281.02 |
| 23 | 72.257 | 415.476 | 53 | 166.50 | 2206.18 | 83 | 260.75 | 5410.61 |
| 24 | 75.398 | 452.389 | 54 | 169.65 | 2290.22 | 84 | 263.89 | 5541.77 |
| 25 | 78.540 | 490.874 | 55 | 172.79 | 2375.83 | 85 | 267.04 |  |
| 26 | $8 \mathrm{8r} .68 \mathrm{I}$ | 530.929 | 56 | 175.93 | 2463.01 | 86 | 270.18 | 5808.80 |
| 27 | 84.823 | 572.555 | 57 | I79.07 | 2551.76 | 87 | 273.32 | 5944.68 |
| 28 | 87.965 | 615.752 | 58 | 182.2I | 2642.08 | 88 | 276.46 | 6082. 12 |
| 29 | 91.106 | 660.520 | 59 | I85.35 | 2733.97 | 89 | 279.60 | 6221.14 |
| 30 | 94.248 | 706.858 | 60 | 188.50 | 2827.43 | 90 | 282.74 | 6361.73 |
| 31 | 97.389 | 754.768 | 61 | 191.64 | 2922.47 | 91 | 285.88 | 6503.88 |
| 32 | 100. 53 | 804.248 | 62 | 194.78 | 3019.07 | 92 | 289.03 | 6647.61 |
| 33 | 103.67 | 855.299 | 63 | 197.92 | 3II7.25 | 93 | 292. 17 | 6792.91 |
| 34 | 106.8I | 907.920 | 64 | 201.06 | 3216.99 | 94 | 295.3I | 6939.78 |
| 35 | 109.96 | 962. I 1 3 | 65 | 204.20 | 3318.31 | 95 | 298.45 | 7088.22 |
| 36 | II 3. 10 | 1017.88 | 66 | 207.35 | 3421.19 | 96 | 301.59 | 7238.23 |
| 37 | I16.24 | 1075.2 I | 67 | 210.49 | 3525.65 | 97 | 304.73 | 7389.81 |
| 38 | I 19.38 | I I 34. I I | 68 | 213.63 | 3631. 68 | 98 | 307.88 | 7542.96 |
| 39 | 122.52 | I194.59 | 69 | 216.77 | 3739.28 | 99 | 311.02 | 7697.69 |

[^47]
## APPENDIX

## Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to 1000.*

In the roots, wherever the effect of a fifth decimal would be to add I to the fourth and final decimal, the addition has been made.

| No. | Square. | Cube. | Sq. Rt. | Cu. Rt. | No. | Square. | Cube. | Sq. Rt. | Cu. Rt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 1 | I. | 1. | 51 | 2601 | 132651 | 7.1414 | 3.7084 |
| 2 | 4 | 8 | I. 4142 | I. 2599 | 52 | 2704 | 140608 | 7.2111 | 3.7325 |
| 3 | 9 | 27 | 1.7321 | 1.4422 | 53 | 2809 | 148877 | 7.2801 | 3.7563 |
| 4 | 16 | 64 | 2. | I. 5874 | 54 | 2916 | 157464 | 7.3485 | 3.7798 |
| 5 | 25 | 125 | 2.2361 | 1.7100 | 55 | 3025 | 166375 | 7.4162 | 3.8030 |
| 6 | 36 | 216 | 2.4495 | 1.8171 | 56 | 3136 | 175616 | 7.4833 | 3.8259 |
| 7 | 49 | 343 | 2.6458 | 1.9129 | 57 | 3249 | 185193 | 7.5498 | 3.8485 |
| 8 | 64 | 512 | 2.8284 | 2. | 58 | 3364 | 195112 | 7.6158 | 3.8709 |
| 9 | 8 I | 729 | 3. | 2.0801 | 59 | 348 I | 205379 | 7.68 II | 3.8930 |
| 10 | 100 | 1000 | 3.1623 | 2. 1544 | 60 | 3600 | 216000 | 7.7460 | 3.9149 |
| 11 | 121 | 1331 | 3.3166 | 2.2240 | 61 | 3721 | 226981 | 7.8102 | 3.9365 |
| 12 | 144 | 1728 | 3.4641 | 2.2894 | 62 | 3844 | 238328 | 7.8740 | 3.9579 |
| 13 | 169 | 2197 | 3.6056 | 2.3513 | 63 | 3969 | 250047 | 7.9373 | 3.9791 |
| 14 | 196 | 2744 | 3.7417 | 2.4101 | 64 | 4096 | 262144 |  | 4. |
| 15 | 225 | 3375 | 3.8730 | 2.4662 | 65 | 4225 | 274625 | 8.0623 | 4.0207 |
| 16 | 256 | 4096 | 4. | 2.5198 | 66 | 4356 | 287496 | 8.1240 | 4.0412 |
| 17 | 289 | 4913 | 4.1231 | 2.5713 | 67 | 4489 | 300763 | 8. 1854 | 4.0615 |
| 18 | 324 | 5832 | 4.2426 | 2.6207 | 68 | 4624 | 314432 | 8.2462 | 4.0817 |
| 19 | 36 I | 6859 | 4.3589 | 2.6684 | 69 | 4761 | 328509 | 8.3066 | 4. 1016 |
| 20 | 400 | 8000 | 4.4721 | 2.7144 | 70 | 4900 | 343000 | 8.3666 | 4. 1213 |
| 21 | 441 | 9261 | 4.5826 | 2.7589 | 71 | 5041 | 3579 I | 8.4261 | 4. 1408 |
| 22 | 484 | 10648 | 4.6904 | 2.8020 | 72 | 5184 | 373248 | 8.4853 | 4. 1602 |
| 23 | 529 | 12167 | $4.795^{8}$ | 2.8439 | 73 | 5329 | 389017 | 8.5440 | 4. I793 |
| 24 | 576 | I 3824 | 4.8990 | 2.8845 | 74 | 5476 | 405224 | 8.6023 | 4. 1983 |
| 25 | 625. | 15625 | 5. | 2.9240 | 75 | 5625 | 421875 | 8.6603 | 4.2172 |
| 26 | 676 | 17576 | 5.0990 | 2.9625 | 76 | 5776 | 438976 | 8.7178 | 4.2358 |
| 27 | 729 | 19683 | 5.1962 | 3. | 77 | 5929 | 456533 | 8.7750 | 4.2543 |
| 28 | 784 | 21952 | 5.2915 | 3.0366 | 78 | 6084 | 474552 | 8.8318 | 4.2727 |
| 29 | 841 | 24389 | $5 \cdot 385^{2}$ | 3.0723 | 79 | 6241 | 493039 | 8.8882 | 4.2908 |
| 30 | 900 | 27000 | 5.4772 | 3.1072 | 80 | 6400 | 512000 | 8.9443 | 4.3089 |
| 31 | 961 | 29791 | 5.5678 | 3.1414 | 81 | 6561 | 531441 | 9. | 4.3267 |
| 32 | 1024 | 32768 | 5.6569 | 3.1748 | 82 | 6724 | 551368 | 9.0554 | $4 \cdot 3445$ |
| 33 | 1089 | 35937 | 5.7446 | 3.2075 | 83 | 6889 | 571787 | 9.1104 | 4.3621 |
| 34 | I I 56 | 39304 | 5.8310 | 3.2396 | 84 | 7056 | 592704 | 9.1652 | $4 \cdot 3795$ |
| 35 | 1225 | 42875 | 5.9161 | 3.27 II | 85 | 7225 | 614125 | 9.2195 | $4 \cdot 3968$ |
| 36 | 1296 | 46656 | 6. | 3.3019 | 86 | 7396 | 636056 | 9.2736 | 4.4140 |
| 37 | 1369 | 50653 | 6.0828 | 3.3322 | 87 | 7569 | 658503 | 9.3274 | 4.4310 |
| 38 | 1444 | 54872 | 6.1644 | 3.3620 | 88 | 7744 | 681472 | 9.3808 | 4.4480 |
| 39 | 1521 | 59319 | 6.2450 | 3.3912 | 89 | 7921 | 704969 | 9.4340 | 4.4647 |
| 40 | 1600 | 64000 | 6.3246 | 3.4200 | 90 | 8100 | 729000 | 9.4868 | $4 \cdot 4814$ |
| 41 | 1681 | 68921 | 6.4031 | 3.4482 | 91 | 8281 | 75357 I | 9.5394 | 4.4979 |
| 42 | 1764 | 74088 | 6.4807 | 3.4760 | 92 | 8464 | 778688 | 9.5917 | 4.5144 |
| 43 | 1849 | 79507 | 6.5574 | 3. 5034 | 93 | 8649 | 804357 | 9.6437 | 4.5307 |
| 44 | 1936 | 85184 | 6.6332 | 3.5303 | 94 | 8836 | 830584 | 9.6954 | 4.5468 |
| 45 | 2025 | 91125 | 6.7082 | $3 \cdot 5569$ | 95 | 9025 | 857375 | 9.7468 | 4.5629 |
| 46 | 2116 | 97336 | 6.7823 | 3.5830 | 96 | 9216 | 884736 | 9.7980 | 4.5789 |
| 47 | 2209 | 103823 | 6.8557 | 3.6088 | 97 | 9409 | 912673 | 9.8489 | 4.5947 |
| 48 | 2304 | I10592 | 6.9282 | 3.6342 | 98 | 9604 | 941192 | 9.8995 | 4.6104 |
| 49 | 2401 | 117649 | 7. | 3.6593 | 99 | 9801 | 970299 | 9.9499 | 4.6261 |
| 50 | 2500 | 125000 | 7.0711 | 3.6840 | 100 | 10000 | 1000000 | 10. | 4.6416 |

* From Smithsonian Geographical Tables, Washington, 1906, checked by comparison with a similar


## APPENDIX

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to rooo-continued.

| No. | Square. | Cube. | Sq. Rt. | Cu. Rt. | No. | Square. | Cube. | Sq. Rt. | $\mathrm{Cu} . \mathrm{Rt}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 101 | 10201 | 1030301 | 10.0499 | 4.6570 | 151 | 22801 | 3442951 | 12.2882 | $5 \cdot 3251$ |
| 10 | 10404 | 1061208 | 10.0995 | 4.6723 | 152 | 23104 | 3511808 | 12.3288 | 5.3368 |
| 103 | 10609 | 1092727 | 10.1489 | 4.6875 | 153 | 23409 | 3581577 | 12.3693 | $5 \cdot 3485$ |
| 104 | 10816 | 1124864 | 10. 1980 | 4.7027 | 154 | 23716 | 3652264 | 12.4097 | $5 \cdot 3601$ |
| 105 | 11025 | 1157625 | 10.2470 | 4.7177 | 155 | 24025 | 3723875 | 12.4499 | $5 \cdot 3717$ |
| 106 | 11236 | 1191016 | 10.2956 | 4.7326 | 156 | 24336 | 3796416 | 12.4900 | $5 \cdot 3832$ |
| 107 | 11449 | 1225043 | 10.3441 | 4.7475 | 157 | 24649 | 3869893 | 12.5300 | $5 \cdot 3947$ |
| 108 | 11664 | 1259712 | 10.3923 | 4.7622 | 158 | 24964 | 3944312 | 12.5698 | 5.406I |
| 109 | 11881 | 1295029 | 10.4403 | 4.7769 | 159 | 2528I | 4019679 | 12.6095 | $5 \cdot 4175$ |
| 110 | 12100 | 1331000 | 10.488 I | 4.7914 | 160 | 25600 | 4096000 | 12.6491 | $5 \cdot 4288$ |
| 111 | 12321 | 1367631 | 10. 5357 | 4.8059 | 161 | 25921 | 4173281 | 12.6886 | 5.4401 |
| 112 | 12544 | 1404928 | 10.5830 | 4.8203 | 162 | 26244 | 4251528 | 12.7279 | 5.4514 |
| 113 | 12769 | 1442897 | 10.6301 | 4.8346 | 163 | 26569 | 4330747 | 12.7671 | 5.4626 |
| 114 | 12996 | 1481544 | 10.6771 | 4.8488 | 164 | 26896 | 4410944 | 12.8062 | 5.4737 |
| 115 | 13225 | 1520875 | 10.7238 | 4.8629 | 165 | 27225 | 4492125 | 12.8452 | 5.4848 |
| 116 | 13456 | 1560896 | 10.7703 | 4.8770 | 166 | 27556 | 4574296 | 12.8841 | 5.4959 |
| 117 | I 3689 | 1601613 | 10.8167 | 4.8910 | 167 | 27889 | 4657463 | 12.9228 | 5.5069 |
| II | I 3924 | 1643032 | 10.8628 | 4.9049 | 168 | 28224 | 4741632 | 12.9615 | 5.5178 |
| 119 | 14161 | 1685159 | 10.9087 | 4.9187 | 169 | 28561 | 4826809 | 13. | 5. 5288 |
| 120 | 14400 | 1728000 | 10.9545 | 4.9324 | 170 | 28900 | 4913000 | 13.0384 | 5.5397 |
| 121 | 14641 | 1771561 | 1 I . | 4.9461 | 171 | 29241 | 5000211 | 13.0767 | $5 \cdot 5505$ |
| 122 | 14884 | 1815848 | 11.0454 | 4.9597 | 172 | 29584 | 5088448 | 13.1149 | 5.5613 |
| 123 | 15129 | 1860867 | 11.0905 | 4.9732 | 173 | 29929 | 5177717 | 13.1529 | $5 \cdot 5721$ |
| 124 | 15376 | 1906624 | 11.1355 | 4.9866 | 174 | 30276 | 5268024 | 13.1909 | 5.5828 |
| 125 | 15625 | 1953125 | 11.1803 | 5. | 175 | 30625 | 5359375 | 13.2288 | 5.5934 |
| 126 | 15876 | 2000376 | 11.2250 | 5.01 33 | 176 | 30976 | 5451776 | 13.2665 | 5.6041 |
| 127 | 16129 | 2048383 | II. 2694 | 5.0265 | 177 | 31329 | 5545233 | 13.3041 | 5.6147 |
| 128 | 16384 | 2097152 | 11.3137 | 5.0397 | 178 | 31684 | 5639752 | 13.3417 | 5.6252 |
| 129 | 16641 | 2146689 | 11.3578 | 5.0528 | 179 | 32041 | 5735339 | 13.3791 | 5.6357 |
| 130 | 16900 | 2197000 | 11.4018 | 5.0658 | 180 | 32400 | 5832000 | 13.4164 | 5.6462 |
| 131 | 17161 | 2248091 | 11.4455 | 5.0788 | 181 | 32761 | 5929741 | 13.4536 | 5.6567 |
| 132 | 17424 | 2299968 | II.4891 | 5.0916 | 182 | 33124 | 6028568 | 13.4907 | 5.6671 |
| 133 | 17689 | 2352637 | II. 5.326 | 5. 1045 | 183 | 33489 | 6128487 | 13.5277 | 5.6774 |
| 134 | 17956 | 2406104 | II. 5758 | 5.1172 | 184 | 33856 | 6229504 | 13.5647 | 5.6877 |
| 135 | 18225 | 2460375 | 11.6190 | 5.1299 | 185 | 34225 | 6331625 | 13.6015 | 5.6980 |
| 136 | 18496 | 2515456 | 11.6619 | 5.1426 | 186 | 34596 | 6434856 | 13.6382 | 5.7083 |
| 137 | 18769 | 2571353 | 11.7047 | 5.155I | 187 | 34969 | 6539203 | 13.6748 | 5.7185 |
| 138 | 19044 | 2628072 | 11.7473 | 5.1676 | 188 | 35344 | 6644672 | 13.7113 | 5.7287 |
| 139 | 19321 | 2685619 | 11.7898 | 5.1801 | 189 | 35721 | 6751269 | 13.7477 | 5.7388 |
| 140 | 19600 | 2744000 | 11.8322 | 5.1925 | 190 | 36100 | 6859000 | 13.7840 | 5.7489 |
| 141 | 1988I | 2803221 | 11.8743 | 5.2048 | 191 | 36481 | 6967871 | 13.8203 | 5.7590 |
| 142 | 20164 | 2863288 | 11.9164 | 5.217 I | 192 | 36864 | 7077888 | 13.8564 | 5.7690 |
| 143 | 20449 | 2924207 | 11.9583 | 5.2293 | 193 | 37249 | 7189057 | 13.8924 | 5.7790 |
| 144 | 20736 | 2985984 | 12. | 5.2415 | 194 | 37636 | 7301384 | 13.9284 | 5.7890 |
| 145 | 21025 | 3048625 | 12.0416 | 5.2536 | 195 | 38025 | 7414875 | 13.9642 | 5.7989 |
| 146 | 21316 | 3112136 | 12.0830 | 5.2656 | 196 | 38416 | 7529536 | 14. | 5.8088 |
| 147 | 21609 | 3176523 | I2. 1244 | 5.2776 | 197 | 38809 | 7645373 | 14.0357 | 5.8186 |
| 148 | 21904 | 3241792 | 12.1655 | 5.2896 | 198 | 39204 | 7762392 | 14.0712 | 5.8285 |
| J 49 | 22201 | 3307949 | 12.2066 | 5.3015 | 199 | 39601 | 7880599 | 14. 1067 | 5.8383 |
| 150 | 22500 | 3375000 | 12.2474 | $5 \cdot 3133$ | 200 | 40000 | 8000000 | 14. 1421 | 5.8480 |

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers
from I to 1000-continued.

| No. | Square. | Cube. | Sq. Rt. | $\mathrm{Cu} . \mathrm{Rt}$. | No. | Square. | Cube. | Sq. Rt. | $\mathrm{Cu} . \mathrm{Rt}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 201 | 40401 | 8120601 | 14.1774 | 5.8578 | 251 | 63001 | 15813251 | 15.8430 | 6.3080 |
| 20 | 40804 | 8242408 | 14.2127 | 5.8675 | 252 | 63504 | 16003008 | 15.8745 | 6.3164 |
| 203 | 41209 | 8365427 | 14.2478 | 5.8771 | 253 | 64009 | 16194277 | 15.9060 | 6.3247 |
| 204 | 41616 | 8489664 | 14.2829 | 5.8868 | 254 | 64516 | 16387064 | 15.9374 | 6.3330 |
| 205 | 42025 | 8615125 | 14.3178 | 5.8964 | 255 | 65025 | 16581375 | 15.9687 | 6.3413 |
| 206 | 42436 | 8741816 | 14.3527 | 5.9059 | 256 | 65536 | 16777216 | 16. | 6.3496 |
| 207 | 42849 | 8869743 | 14.3875 | 5.9155 | 257 | 66049 | 16974593 | 16.0312 | 6. 3579 |
| 208 | 43264 | 8998912 | 14.4222 | 5.9250 | 258 | 66564 | 17173512 | 16.0624 | 6. 3661 |
| 209 | 43681 | 9129329 | 14.4568 | 5.9345 | 259 | 67081 | 17373979 | 16.0935 | 6. 3743 |
| 210 | 44100 | 9261000 | 14.4914 | 5.9439 | 260 | 67600 | 17576000 | 16.1245 | 6.3825 |
| 211 | 44521 | 9393931 | 14.5258 | 5.9533 | 261 | 68121 | 17779581 | 16. 1555 | 6.3907 |
| 212 | 44944 | 9528128 | 14.5602 | 5.9627 | 262 | 68644 | 17984728 | 16. 1864 | 6.3988 |
| 213 | 45369 | 9663597 | 14.5945 | 5.9721 | 263 | 69169 | 18191447 | 16.2173 | 6.4070 |
| 214 | 45796 | 9800344 | 14.6287 | 5.9814 | 264 | 69696 | 18399744 | 16.2481 | 6.4151 |
| 215 | 46225 | 9938375 | 14.6629 | 5.9907 | 265 | 70225 | 18609625 | 16.2788 | 6.4232 |
| 216 | 46656 | 10077696 | 14.6969 | 6. | 266 | 70756 | 18821096 | 16.3095 | 6.4312 |
| 217 | 47089 | 10218313 | 14.7309 | 6.0092 | 267 | 71289 | 19034163 | 16.3401 | 6.4393 |
| 218 | 47524 | 10360232 | 14.7648 | 6.0185 | 268 | 71824 | 19248832 | 16.3707 | 6.4473 |
| 219 | 47961 | 10503459 | 14.7986 | 6.0277 | 269 | 72361 | 19465109 | 16.4012 | 6.4553 |
| 220 | 48400 | 10648000 | 14.8324 | 6.0368 | 270 | 72900 | 19683000 | 16.4317 | 6.4633 |
| 221 | 48841 | 10793861 | 14.8661 | 6.0459 | 271 | 73441 | 19902511 | 16.4621 | 6.4713 |
| 222 | 49284 | 10941048 | 14.8997 | 6.0550 | 272 | 73984 | 20123648 | 16.4924 | 6.4792 |
| 223 | 49729 | 11089567 | 14.9332 | 6.0641 | 273 | 74529 | 20346417 | 16.5227 | 6.4872 |
| 224 | 50176 | 11239424 | 14.9666 | 6.0732 | 274 | 75076 | 20570824 | 16.5529 | 6.4951 |
| 225 | 50625 | 11390625 | 15. | 6.0822 | 275 | 75625 | 20796875 | 16.5831 | 6.5030 |
| 226 | 51076 | 11543176 | 15.0333 | 6.0912 | 276 | 76176 | 21024576 | 16.6132 | 6.5108 |
| 227 | 51529 | 11697083 | 15.0665 | 6.1002 | 277 | 76729 | 21253933 | 16.6433 | 6.5187 |
| 22 | 51984 | 11852352 | 15.0997 | 6.1091 | 278 | 77284 | 21484952 | 16.6733 | 6.5265 |
| 229 | 52441 | 12008989 | 15.1327 | 6.1180 | 279 | 77841 | 21717639 | 16.7033 | 6.5343 |
| 230 | 52900 | 12167000 | 15.1658 | 6.1269 | 280 | 78400 | 21952000 | 16.7332 | 6.5421 |
| 231 | 53361 | 12326391 | 15.1987 | 6. 1358 | 281 | 78961 | 22188041 | 16.7631 | 6.5499 |
| 232 | 53824 | 12487168 | 15.2315 | 6. 1446 | 282 | 79524 | 22425768 | 16.7929 | 6.5577 |
| 233 | 54289 | 12649337 | 15.2643 | 6. 1534 | 283 | 80089 | 22665187 | 16.8226 | 6.5654 |
| 234 | 54756 | 12812904 | 15.2971 | 6. 1622 | 28. | 80656 | 22906304 | 16.8523 | 6. 5731 |
| 235 | 55225 | 12977875 | 15.3297 | 6.1710 | 285 | 81225 | 23149125 | 16.8819 | 6.5808 |
| 236 | 55696 | 13144256 | 15.3623 | 6. 1797 | 286 | 81796 | 23393656 | 16.9115 | 6.5885 |
| 237 | 56169 | 13312053 | 15.3948 | 6.1885 | 287 | 82369 | 23639903 | 16.9411 | 6.5962 |
| 238 | 56644 | 13481272 | 15.4272 | 6.1972 | 288 | 82944 | 23887872 | 16.9706 | 6.6039 |
| 239 | 57121 | I3651919 | 15.4596 | 6.2058 | 289 | 83521 | 24137569 |  | 6.6115 |
| 240 | 57600 | 13824000 | 15.4919 | 6.2145 | 290 | 84100 | 24389000 | 17.0294 | 6.6191 |
| 241 | 58081 | 13997521 | 15.5242 | 6.2231 | 291 | 84681 | 24642171 | 17.0587 | 6.6267 |
| 242 | 58564 | 14172488 | 15.5563 | 6.2317 | 292 | 85264 | 24897088 | 17.0880 | 6.6343 |
| 243 | 59049 | 14348907 | 15.5885 | 6.2403 | 293 | 85849 | 25153757 | 17.1172 | 6.6419 |
| 244 | 59536 | 14526784 | 15.6205 | 6.2488 | 294 | 86436 | 25412184 | 17.1464 | 6.6494 |
| 245 | 60025 | 14706125 | 15.6525 | 6.2573 | 295 | 87025 | 25672375 | 17.1756 | 6.6569 |
| 246 | 60516 | 14886936 | 15.6844 | 6.2658 | 296 | 87616 | 25934336 | 17.2047 | 6.6644 |
| 247 | 61009 | 15069223 | 15.7162 | 6.2743 | 297 | 88209 | 26198073 | 17.2337 | 6.6719 |
| 248 | 61504 | 15252992 | 15.7480 | 6.2828 | 298 | 88804 | 26463592 | 17.2627 | 6.6794 |
| 249 | 62001 | 15438249 | 15.7797 | 6.2912 | 299 | 89401 | 26730899 | 17.2916 | 6.6869 |
| 250 | 62500 | 15625000 | 15.8114 | 6.2996 | 300 | 90000 | 27000000 | 17.3205 | 6.6943 |

## APPENDIX

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to 1000-continued.

| No. | Square. | Cube | Sq. Rt. | Cu. Rt. | No. | Square. | Cube. | Sq. Rt. | Cu. Rt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 301 | 90601 | 2727 | 17.3494 | 6.7018 | 351 | 123201 | 4324355 | 18.7350 | 540 |
| 302 | 91204 | 27543608 | 17.3781 | 6.7092 | 352 | 123904 | 43614208 | 18.7617 | 7.0607 |
| 303 | 91809 | 27818127 | 17.4069 | 6.7166 | 353 | 124609 | 43986977 | 18.7883 | 7.0674 |
| 304 | 92416 | 28094464 | 17.4356 | 6.7240 | 354 | 125316 | 44361864 | 18.8149 | 7.0740 |
| 305 | 93025 | 28372625 | 17.4642 | 6.7313 | 355 | 126025 | 44738875 | 18.8414 | 7.0807 |
| 306 | 93636 | 28652616 | 17.4929 | 6.7387 | 356 | 126736 | 45118016 | 18.8680 | 7.0873 |
| 307 | 94249 | 28934443 | 17.5214 | 6.7460 | 357 | 127449 | 45499293 | 18.8944 | 7.0940 |
| 308 | 94864 | 29218112 | 17.5499 | 6.7533 | 358 | 128164 | 45882712 | 18.9209 | 7.1006 |
| 309 | 9548 I | 29503629 | 17.5784 | 6.7606 | 359 | 128881 | 46268279 | 18.9473 | 7.1072 |
| 310 | 96100 | 29791000 | 17.6068 | 6.7679 | 00 | 129600 | 46656000 | 18.9737 | 7.1138 |
| 311 | 96721 | 30080231 | 17.6352 | 6.7752 | 361 | 130321 | 47045881 | 19. | 1204 |
| 312 | 97344 | 30371328 | 17.6635 | 6.7824 | 362 | 131044 | 47437928 | 19.0263 | 7.1269 |
| 313 | 97969 | 30664297 | 17.6918 | 6.7897 | 363 | 131769 | 47832147 | 19.0526 | 7.1335 |
| 314 | 98596 | 30959144 | 17.7200 | 6.7969 | 364 | I 32496 | 48228544 | 19.0788 | 7. 1400 |
| 3'5 | 99225 | 31255875 | 17.7482 | 6.8041 | 365 | I 33225 | 48627125 | 19.1050 | 7. 1466 |
| 316 | 99856 | 31554496 | 17.7764 | 6.8113 | 366 | 133956 | 49027896 | 19.1311 | 7.1531 |
| 317 | 100489 | 31855013 | 17.8045 | 6.8185 | 367 | 1 34689 | 49430863 | 19.1572 | 7.1596 |
| 318 | 101124 | 32157432 | 17.8326 | 6.8256 | 368 | 135424 | 49836032 | 19.1833 | 7•1661 |
| 319 | 101761 | 32461759 | 17.8606 | 6.8328 | 369 | 136161 | 50243409 | 19.2094 | 7.1726 |
| 320 | 102400 | 32768000 | 17.8885 | 6.8399 | 370 | I 36900 | 50653000 | 19.2354 | . 1791 |
| 321 | 10304 | 33076161 | 17.9165 | 6.8470 | 371 | 137641 | 510648 II | 19.2614 | 7.1855 |
| 322 | 10368 | 33386248 | 17.9444 | 6.8541 | 372 | 138384 | 51478848 | 19.2873 | 7.1920 |
| 3 | 104329 | 33698267 | 17.9722 | 6.8612 | 373 | 139129 | 51895117 | 19.3132 | 7. 1984 |
| 324 | 104976 | 34012224 | 18. | 6.8683 | 374 | I 39876 | 52313624 | 19.3391 | 7.2048 |
| 325 | 105625 | 34328125 | 18.027 | 6.8753 | 375 | 140625 | 52734375 | 19.3649 |  |
| 326 | 106276 | 34645976 | 18.0555 | 6.8824 | 376 | 141376 | 53157376 | 19.3907 | 7.2177 |
| 327 | 106929 | 34965783 | 18.0831 | 6.8894 | 377 | 142129 | 53582633 | 19.4165 | 7.2240 |
| 328 | 107584 | 35287552 | 18.1 108 | 6.8964 | 378 | 142884 | 54010152 | 19.4422 | 7.2304 |
| 329 | 10824I | 35611289 | 18.1384 | 6.9034 | 379 | 143641 | 54439939 | 19.4679 |  |
| 330 | 108900 | 35937000 | 9 | 6.9104 | 380 | 14 | 54872000 | 19.4936 |  |
| 331 | 10956I | 36264691 | 18.1934 | 6.9174 | 381 | 145161 | 55306341 | 19.5192 | 7.2495 |
| 332 | 110224 | 36594368 | 18.2209 | 6.9244 | 382 | 145924 | 55742968 | 19.5448 | 7.2558 |
| 333 | 110889 | 36926037 | 18.2483 | 6.9313 | 383 | 146689 | 56181887 | 19.5704 | 7.2622 |
| 334 | III556 | 37259704 | 18.2757 | 6.9382 | 384 | 147456 | 56623104 | 19.5959 | 7. |
| 335 | 112225 | 37595375 | 18.3030 | 6.945 ${ }^{\text {I }}$ | 385 | 148225 | 57066625 | 19.6214 |  |
| 336 | I 12896 | 37933056 | 18.3303 | 6.952 I | 386 | 148996 | 57512456 | 19.6469 | . 281 |
| 337 | 1 13569 | 38272753 | 18.3576 | 6.9589 | 387 | 149769 | 57960603 | 19.6723 | 7.2874 |
| 338 | 114244 | 38614472 | 18.3848 | 6.9658 | 388 | 150544 | 58411072 | 19.6977 | 7.2936 |
| 339 | 114921 | 38958219 | 18.4120 | 6.9727 | 389 | 151321 | 58863869 | 19.7231 | 7.2999 |
| 340 | 115600 | 39304000 | 18.4391 | 6.9795 | 390 | 152100 | 59319000 | 19.74 | 7-3061 |
| 341 | 11628I | 39651821 | 18.4662 | 6.9864 | 391 | 152881 | 5977647 I | 19.7737 | . 3124 |
| 342 | 116964 | 40001688 | .18.4932 | 6.9932 | 392 | 153664 | 60236288 | 19.7990 | $7 \cdot 3186$ |
| 343 | 117649 | 40353607 | 18.5203 | 7. | 393 | 154449 | 60698457 | 19.8242 | 7.3248 |
| 344 | 118336 | 40707584 | 18.5472 | 7.0068 | 394 | 155236 | 61162984 | 19.8494 | 7.3310 |
| 345 | 119025 | 41063625 | 18.5742 | 7.0136 | 395 | 156025 | 61629875 | 19.8746 | $7 \cdot 3372$ |
| 346 | 119716 | 41421736 | 18.6011 | 7.0203 | 396 | 156816 | 62099136 | 19.8997 | 7.3434 |
| 34 | 120409 | 41781923 | 18.6279 | 7.0271 | 397 | 157609 | 62570773 | 19.9249 | 7.3496 |
| 348 | 121104 | 42144192 | 18.6548 | 7.0338 | 398 | 158404 | 63044792 | 19.9499 | $7 \cdot 3558$ |
| 349 | 121801 | 42508549 | 18.6815 | 7.0406 | 399 | 159201 | 63521199 | 19.9750 | $7 \cdot 3619$ |
| 350 | 122500 | 42875000 | 18.7083 | 7.0473 | 400 | 160000 | 64000000 | 20. | $7 \cdot 3681$ |

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to 1000-continued.

| No. | Square. | Cube. | Sq. Rt. | Cu. Rt. | No. | Square. | Cube. | Sq. Rt. | $\mathrm{Cu} . \mathrm{Rt}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 401 | 160801 | 64481201 | 20.02 | $7 \cdot 374$ | 451 | 203401 | 91733851 | 21.2368 | 7.6688 |
| 402 | 161604 | 64964808 | 20.0499 | 7.3803 | 452 | 204304 | 92345408 | 21.2603 | 7.6744 |
| 403 | 162409 | 65450827 | 20.0749 | 7.3864 | 453 | 205209 | 92959677 | 21.2838 | 7.6801 |
| 404 | 163216 | 65939264 | 20.0998 | 7.3925 | 454 | 206116 | 93576664 | 21.3073 | 7.6857 |
| 405 | 164025 | 66430125 | 20.1246 | $7 \cdot 3986$ | 455 | 207025 | 94196375 | 21.3307 | 7.6914 |
| 406 | 164836 | 66923416 | 20.1494 | $7 \cdot 4047$ | 456 | 207936 | 94818816 | 21.3542 | 7.6970 |
| 407 | 165649 | 67419143 | 20.1742 | 7.4108 | 457 | 208849 | 95443993 | 21.3776 | 7.7026 |
| 408 | 166464 | 67917312 | 20.1990 | 7.4169 | 458 | 209764 | 96071912 | 21.4009 | 7.7082 |
| 409 | 167281 | 68417929 | 20.2237 | 7.4229 | 459 | 210681 | 96702579 | 21.4243 | 7.7138 |
| 410 | 168100 | 68921000 | 20.2485 | 7.4290 | 460 | 2116 | 97336000 | 21.4476 | 7.7194 |
| 411 | 168921 | 69426531 | 20.2731 | 7.4350 | 461 | 212521 | 9797218 I | 21. 4709 | 7.7250 |
| 412 | 169744 | 69934528 | 20.2978 | 7.4410 | 462 | 213444 | 98611128 | 21.4942 | 7.7306 |
| 413 | 170569 | 70444997 | 20.3224 | 7.4470 | 463 | 214369 | 99252847 | 21.5174 | 7.7362 |
| 414 | 171396 | 70957944 | 20.3470 | 7.4530 | 464 | 215296 | 99897344 | 21.5407 | 7.7418 |
| 415 | 172225 | 71473375 | 20.3715 | $7 \cdot 45$ | 465 | 216225 | 100544625 | 21.5639 | 7.7473 |
| 416 | 173056 | 71991296 | 20.3961 | 7.4650 | 466 | 217156 | IOII 194696 | 21.5870 | 7.7529 |
| 417 | 173889 | 72511713 | 20.4206 | 7.4710 | 467 | 218089 | 101847563 | 21.6102 | 7.7584 |
| 18 | 174724 | 73034632 | 20.4450 | 7-4770 | 468 | 219024 | 102503232 | 21.6333 | 7.7639 |
| 419 | 175561 | 73560059 | 20.4695 | 7.4829 | 469 | 21996I | 103161709 | 21.6564 | 7.7695 |
| 420 | 176400 | 74088000 | 20.4939 | 7. | 470 | 220900 | 103823000 | 21.6795 | 7.7750 |
| 421 | 177241 | 74618461 | 20.5183 | 7.4948 | 471 | 221841 | 104487111 | 21.7025 | 7.7805 |
| 42 | 178084 | 75151448 | 20.5426 | 7.5007 | 472 | 222784 | 105154048 | 21.7256 | 7.7860 |
| 423 | 178929 | 75686967 | 20.5670 | 7.5067 | 473 | 223729 | 105823817 | 21.7486 | 7.7915 |
| 424 | 179776 | 76225024 | 20.5913 | 7.5126 | 474 | 224676 | 106496424 | 21.7715 | 7.7970 |
| 425 | 180625 | 76765625 | 20.6155 | $7 \cdot 5185$ | 475 | 225625 | 107171875 | 21.7945 | 25 |
| 426 | 181476 | 77308776 | 20.6398 | 7.5244 | 476 | 226576 | 107850176 | 21.8174 | 7.8079 |
| 427 | 182329 | 77854483 | 20.6640 | 7.5302 | 477 | 227529 | 108531333 | 21.8403 | 7.8134 |
| 428 | 183184 | 78402752 | 20.6882 | 7.5361 | 478 | 228484 | 109215352 | 21.8632 | 7.8188 |
| 429 | 184041 | 78953589 | 20.7123 | 7.5420 | 479 | 229441 | 109902239 | 21.8861 | 7.8243 |
| 430 | i84900 | 79507000 | 20.7364 | 7.54 | 480 | 230400 | 110592000 | 21.9089 | 97 |
| 431 | 185761 | 80062991 | 20.760 | 7.553 | 481 | 231361 | 111284641 | 21.9317 | 7.8352 |
| 432 | 186624 | 80621568 | 20.7846 | 7.5595 | 482 | 232324 | 111980168 | 21.9545 | 7.8406 |
| 433 | 187489 | 81182737 | 20.8087 | 7.5654 | 483 | 233289 | 112678587 | 21.9773 | 7.8460 |
| 434 | 188356 | ${ }^{81746504}$ | 20.8327 | 7.5712 | 484 | 234256 | 113379904 | 22. | 7.8514 |
| 435 | 189225 | 82312875 | 20.8567 | 7.577 | 485 | 235225 | 114084125 | 22.0227 |  |
| 436 | 190096 | 82881856 | 20.8806 | 7.5828 | 486 | 236196 | 114791256 | 22.0454 | 7.8622 |
| 437 | 190969 | 83453453 | 20.9045 | 7.5886 | 487 | 237169 | 115501303 | 22.0681 | 7.8676 |
| 438 | 191844 | 84027672 | 20.9284 | 7. 5944 | 488 | 238144 | 116214272 | 22.0907 | 7.8730 |
| 439 | 192721 | 84604519 | 20.9523 | 7.6001 | 489 | 239121 | 116930169 | 22.1133 | 7.8784 |
| 440 | 193600 | 85184000 | 20.9762 | 7.6059 | 490 | 240100 | 117649000 | 22.1359 | 7.8837 |
| 441 | 194481 | 85766121 | 21. | 7.6117 | 491 | 241081 | 118370771 | 22.1585 | 7.8891 |
| 442 | 195364 | 86350888 | 21.0238 | 7.6174 | 492 | 242064 | 119095488 | 22.1811 | 7.8944 |
| 443 | 196249 | 86938307 | 21.0476 | 7.6232 | 493 | 243049 | 119823157 | 22.2036 | 7.8998 |
| 444 | 197136 | 87528384 | 21.0713 | 7.6289 | 494 | 244036 | 120553784 | 22.2261 | 7.9051 |
| 445 | 198025 | 88121125 | 21.0950 | 7.6346 | 495 | 245025 | 121287375 | 22.2486 | 7.9105 |
| 446 | 198916 | 88716536 | 21.1187 | 7.6403 | 496 | 246016 | 122023936 | 22.2711 | 7.9158 |
| 447 | 199809 | 89314623 | 21.1424 | 7.6460 | 497 | 247009 | 122763473 | 22.2935 | 7.9211 |
| 448 | 200704 | 89915392 | 21.1660 | 7.6517 | 498 | 248004 | 123505992 | 22.3159 | 7.9264 |
| 449 | 201601 | 90518849 | 21.1896 | 7.6574 | 499 | 249001 | 124251499 | 22.3383 | 7.9317 |
| 450 | 202500 | 91125000 | 21.2132 | 7.6631 | 500 | 250000 | 125000000 | 22.3607 | $7 \cdot 9370$ |

## APPENDIX

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to 1000-continued.

| No. | Square. | Cube. | Sq. Rt. | $\mathrm{Cu} . \mathrm{Rt}$. | No. | Square. | Cube. | Sq. Rt. | $\mathrm{Cu} . \mathrm{Rt}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 501 | 251001 | 125751 | 22.3830 | 7.942 | 51 | 303601 | 167284151 | 23.4734 | 8. 1982 |
| 2 | 252004 | 126506008 | 22.4054 | 7.9476 | 552 | 304704 | 168196608 | 23.4947 | 8.2031 |
| 3 | 253009 | 127263527 | 22.4277 | 7.9528 | 553 | 305809 | 169112377 | 23.5160 | 8.2081 |
| 504 | 254016 | 128024064 | 22.4499 | 7.9581 | 554 | 306916 | 170031464 | 23.5372 | 8.2130 |
| 505 | 255025 | 128787625 | 22.4722 | 7.9634 | 555 | 308025 | 170953875 | 23.5584 | 8.2180 |
| 506 | 256036 | 129554216 | 22.4944 | 7.9686 | 556 | 309136 | 171879616 | 23.5797 | 8. |
| 507 | 257049 | 130323843 | 22.5167 | 7.9739 | 557 | 310249 | 172808693 | 23.6008 | 8.2278 |
| 508 | 258064 | 131096512 | 22.5389 | 7.9791 | 558 | 311364 | 173741112 | 23.6220 | 8.2327 |
| 509 | 259081 | 131872229 | 22.5610 | 7.9843 | 559 | 312481 | 174676879 | 23.6432 | 8.2377 |
| 510 | 260100 | 132651000 | 22.5832 | 7.9896 | - | 31 3600 | 175616000 | 23.6643 | 8.2426 |
| 511 | 261121 | 133432831 | 22.6053 | 7.9948 | 561 | 314721 | 176558481 | 23.6854 | 8.2475 |
| 51 | 262144 | 134217728 | 22.6274 | 8. | 562 | 315844 | 177504328 | 23.7065 | 8.2524 |
| 513 | 263169 | 135005697 | 22.6495 | 8.0052 | 563 | 316969 | 178453547 | 23.7276 | 8.2573 |
| 514 | 264196 | 135796744 | 22.6716 | 8.0104 | 564 | 318096 | 179406144 | 23.7487 | 8.2621 |
| 515 | 265225 | 136590875 | 22.6936 | 8.01 56 | 565 | 319225 | 180362125 | 23.7697 |  |
| 516 | 266256 | 137388096 | 22.7156 | 8.0208 | 566 | 320356 | 181321496 | 23.7908 | 8.2719 |
| 517 | 267289 | 138188413 | 22.7376 | 8.0260 | 567 | 321489 | 182284263 | 23.8118 | 8.2768 |
| 518 | 268324 | 138991832 | 22.7596 | 8.0311 | 568 | 322624 | 183250432 | 23.8328 | 8.2816 |
| 519 | 269361 | 139798359 | 22.7816 | 8.0363 | 569 | 323761 | 184220009 | 23.8537 | 8.2863 |
| 520 | 270400 | 140608000 | 22.8035 | 8.0415 | 570 | 324900 | 185193000 | 23.8747 | 8.2913 |
| 621 | 271 | 141420761 | 22.8254 | 8.0466 | 571 | 326041 | 186169411 | 23.8956 | 8.2962 |
| 522 | 272484 | 142236648 | 22.8473 | 8.0517 | 572 | 32718 | 187149248 | 23.9165 | 8.3010 |
| 523 | 273529 | 143055667 | 22.8692 | 8.0569 | 573 | 32832 | 188132517 | 23.937 | 8.3059 |
| 524 | 274576 | 143877824 | 22.8910 | 8.0620 | 574 | 3294 | 189119224 | 23.958 | 8.3107 |
| 525 | 275625 | 144703125 | 22.9129 | 8.0671 | 575 | 330625 | 190109375 | 23.9792 | 8.3155 |
| 526 | 276676 | 145531576 | 22.9347 | 8.0723 | 576 | 331776 | 191102976 | 24. | 8.3203 |
| 527 | 277729 | 146363183 | 22.9565 | 8.0774 | 577 | 332929 | 192100033 | 24.0208 | 8.325 I |
| 5 | 278784 | 147197952 | 22.9783 | 8.0825 | 578 | 334084 | 193100552 | 24.0416 | 8.3300 |
| 529 | 279841 | 148035889 | 23. | 8.0876 | 579 | 335241 | 194104539 | 24.0624 | 8.3348 |
| 530 | 280900 | 148877000 | 23.0217 | 8.0927 | 580 | 33 | 195112000 | 24.0832 | 8.3396 |
| 531 | 281961 | 149721291 | 23.0434 | 8.0978 | 581 | 337561 | 196122941 | 24. 1039 | 8.3443 |
| 532 | 283024 | 150568768 | 230651 | 8. 102 | 582 | 338724 | 197137368 | 24.1247 | 8.3491 |
| 533 | 284089 | 151419437 | 23.0868 | 8. 1079 | 583 | 339889 | 198155287 | 24. 1454 | 8.3539 |
| 53 | 285156 | 152273304 | 23.1084 | 8.1130 | 584 | 341056 | 199176704 | 24.1661 | 87 |
| 5 | 28 | 153130375 | 23 | 8. | 585 | 342225 | 200201625 | 24. 1868 | 634 |
| 536 | 287296 | 153990656 | 23.1517 | 8.1231 | 586 | 343396 | 201230056 | 24.2074 | 8.3682 |
| 537 | 288369 | 154854153 | 23.1733 | 8.128I | 587 | 344569 | 202262003 | 24.2281 | 8.3730 |
| 538 | 289444 | 155720872 | 23.1948 | 8.1332 | 588 | 345744 | 203297472 | 24.2487 | 8.3777 |
| 539 | 290521 | I56590819 | 23.2164 | 8.1382 | 589 | 346921 | 204336469 | 24.2693 | 8.3825 |
| 540 | 291600 | I 57464000 | 23.2379 | 8.1433 | 590 | 348100 | 205379000 | 24.2899 | 8.3872 |
| 541 | 292681 | 158340421 | 23.2594 | 8.1483 | 591 | 349281 | 206425071 | 24.3105 | 8.3919 |
| 542 | 293764 | 159220088 | 23.2809 | 8. 1533 | 592 | 350464 | 207474688 | 24.3311 | 8.3967 |
| 543 | 294849 | 160103007 | 23.3024 | 8.1583 | 593 | 351649 | 208527857 | 24.3516 | 8.4014 |
| 544 | 295936 | 160989184 | 23.3238 | 8.16.33 | 594 | 352836 | 209584584 | 24.3721 | 8.4061 |
| 545 | 297025 | 161878625 | 23.3452 | 8.1683 | 595 | 354025 | 210644875 | 24.3926 | 8.4108 |
| 546 | 298116 | 162771336 | 23.3666 | 8. 1733 | 596 | 355216 | 211708736 | 24.4131 | 8.4155 |
| 547 | 299209 | 163667323 | 23.3880 | 8.1783 | 597 | 356409 | 212776173 | 24.4336 | 8.4202 |
| 548 | 300304 | 164566592 | 23.4094 | 8.1833 | 598 | 357604 | 213847192 | 24.4540 | 8.4249 |
| 549 | 301401 | 165469149 | 23.4307 | 8.1882 | 599 | 358801 | 214921799 | 24.4745 | 8.4296 |
| 550 | 302500 | 166375000 | $23 \cdot 4521$ | 8. 1932 | 600 | 360000 | 216000000 | 24.4949 | 8.4343 |

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to 1000-continued.

| No. | Square. | Cube. | Sq. Rt. | Cu. Rt. | No. | Square. | Cube | Sq. Rt. | $\mathrm{Cu} . \mathrm{Rt}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 601 | 361201 | 217081801 |  | 8.4390 | 651 | 423801 |  |  | 8.6668 |
| 602 | 362404 | 218167208 | 24.5357 | 8.4437 | 652 | 425104 | 277167808 | 25.5343 | 8.6713 |
| 603 | 363609 | 219256227 | 24.5561 | 8.4484 | 653 | 426409 | 278445077 | 25.5539 | 8.6757 |
| 604 | 364816 | 220348864 | 24.5764 | 8.4530 | 654 | 427716 | 279726264 | 25.5734 | 8.6801 |
| 605 | 366025 | 221445125 | 24.5967 | 8.4577 | 655 | 429025 | 281011375 | 25.5930 | 8.6845 |
| 606 | 367236 | 222545016 | 24.6171 | 8.4623 | 656 | 430336 | 282300416 | 25.6125 | 8.6890 |
| 60 | 368449 | 223648543 | 24.6374 | 8.4670 | 657 | 431649 | 283593393 | 25.6320 | 8.6934 |
| 60 | 369664 | 224755712 | 24.6577 | 8.4716 | 658 | 432964 | 284890312 | 25.6515 | 8.6978 |
| 609 | 370881 | 225866529 | 24.6779 | 8.4763 | 659 | 434281 | 286191179 | 25.6710 | 8.7022 |
| 610 | 372100 | 226981000 | 24.6982 | 8.4809 | 660 | 435600 | 287496000 | 25.6905 | 8.7066 |
| 611 | 373321 | 228099131 | 24.7184 | 8.4856 | 661 | 436921 | 288804781 | 25.7099 | 8.7110 |
| 612 | 3745 | 229220928 | 24.7386 | 8.4902 | 662 | 438244 | 290117528 | 25.7294 | 8.7154 |
| 613 | 375769 | 230346397 | 24.7588 | 8. 4948 | 663 | 439569 | 291434247 | 25.7488 | 8.7198 |
| 614 | 376996 | 231475544 | 24.7790 | 8.4994 | 664 | 440896 | 292754944 | 25.7682 | 8.724 I |
| 615 | 378225 | 232608375 | 24.7992 | 8.5040 | 665 | 442225 | 294079625 | 25.7876 | 8.7285 |
| 616 | 379456 | 233744896 | 24.8193 | 8.5086 | 666 | 443556 | 295408296 | 25.8070 | 8.7329 |
| 617 | 380689 | 234885113 | 24.8395 | 8.5132 | 667 | 444889 | 296740963 | 25.8263 | 8.7373 |
| 618 | 381924 | 236029032 | 24.8596 | 8.5178 | 668 | 446224 | 298077632 | 25.8457 | 8.7416 |
| 619 | 383161 | 237176659 | 24.8797 | 8.5224 | 669 | 447561 | 299418309 | 25.8650 | 8.7460 |
| 62 | 384400 | 238328000 | 24.8998 | 8.5270 | 670 | 448900 | 300763000 | 25.8844 | 8.7503 |
| 621 | 385641 | 239483061 | 24.9199 | 8.5316 | 671 | 450241 | 302111711 | 25.9037 | 8.7547 |
| 622 | 386884 | 240641848 | 24.9399 | 8.5362 | 672 | 451584 | 303464448 | 25.9230 | 8.7590 |
| 623 | 388129 | 241804367 | 24.9600 | 8. 5408 | 673 | 452929 | 304821217 | 25.9422 | 8.7634 |
| 624 | 389376 | 242970624 | 24.9800 | 8. 5453 | 674 | 454276 | 306182024 | 25.9615 | 8.7677 |
| 625 | 390625 | 244140625 | 25. | 8.54 | 675 | 455625 | 307546875 | 25.9808 | 8.7721 |
| 626 | 391876 | 245314376 | 25.0200 | 8. 5544 | 676 | 456976 | 308915776 | 26. | 64 |
| 627 | 393129 | 246491883 | 25.0400 | 8. 5590 | 677 | 458329 | 310288733 | 26.0192 | 8.7807 |
| 62 | 394.384 | 247673152 | 25.0599 | 8. 5635 | 678 | 459684 | 311665752 | 26.0384 | 8.7850 |
| 629 | 395641 | 248858189 | 25.0799 | 8.5681 | 679 | 461041 | 313046839 | 26.0576 | 8.7893 |
| 630 | 3969 | 250047000 | 25.0998 | 8. 5726 | 680 | 46240 | 314432000 | 26.0768 | 8.7937 |
| 631 | 398161 | 251239 | 25.1197 | 8.5772 | 681 | 463761 | 315821241 | 26.0960 | 980 |
| 632 | 399424 | 25243596 | 25.1396 | 8.5817 | 682 | 465124 | 317214568 | 26.1151 | 8.8023 |
| 633 | 400689 | 253636137 | 25.1595 | 8.5862 | 683 | 466489 | 318611987 | 26.1343 | 8.8066 |
| 634 | 401956 | 254840104 | 25.1794 | 8. 5907 | 684 | 467856 | 320013504 | 26.1534 | 8.8109 |
| 635 | 403225 | 256047875 | 25.1992 | 8. 5952 | 685 | 469225 | 321419125 | 26.1725 | 8.8152 |
| 636 | 40 | 25725 | 25.2190 | 8.5997 | 686 | 470596 | 322828856 | 26.1916 | 8.8194 |
| 637 | 405769 | 258474853 | 25.2389 | 8.6043 | 687 | 471969 | 324242703 | 26.2107 | 8.8237 |
| 638 | 407044 | 259694072 | 25.2587 | 8.6088 | 688 | 473344 | 325660672 | 26.2298 | 8.8280 |
| 639 | 408321 | 260917119 | 25.2784 | 8.6132 | 689 | 474721 | 327082769 | 26.2488 | 8.8323 |
| 640 | 409600 | 262144000 | 25.2982 | 8.6177 | 690 | 476100 | 328509000 | 26.2679 | 8.8366 |
| 41 | 410881 | 26 | 25.3180 | 8.6222 | 691 | 477481 | 29939 | 26.2869 | 8.8408 |
| 642 | 412164 | 264609288 | 25.3377 | 8.6267 | 692 | 478864 | 331373888 | 26.3059 | 8.8451 |
| 643 | 413449 | 265847707 | 25.3574 | 8.6312 | 693 | 480249 | 332812557 | 26.3249 | 8.8493 |
| 644 | 414736 | 267089984 | 25.3772 | 8.6357 | 694 | 481636 | 334255384 | 26.3439 | 8.8536 |
| 645 | 416025 | 268336125 | 25.3969 | 8.6401 | 695 | 483025 | 335702375 | 26.3629 | 8.8578 |
| 646 |  | 2695861 |  | 8.6 | 696 | 484416 | 337153536 | 26.3818 | 8.8621 |
| 64 | 418609 | 270840023 | 25.4362 | 8.649 | 697 | 485809 | 338608873 | 26.4008 | 8.8663 |
| 648 | 419904 | 272097792 | 25.4558 | 8.6535 | 698 | 487204 | 340068392 | 26.4197 | 8.8706 |
| 649 | 421201 | 273359449 | 25.4755 | 8.6579 | 699 | 488601 | 341532099 | 26.4386 | 8.8748 |
| 650 | 422500 | 274625000 | 25.4951 | 8.6624 | 700 | 490000 | 34300000 | 26.4575 | 8.8790 |

## APPENDIX

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to 1000-continued.

| No. | Squar | Cube. | Sq. Rt. | Cu. Rt. | No. | Squar | Cube. | Sq. Rt. | $\mathrm{Cu} . \mathrm{Rt}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 701 | 491 | 344 | 26.4764 | 8.8833 | 751 | 564001 | 42 | 27 | 9.0896 |
| 702 | 492804 | 345948408 | 26.4953 | 8.8875 | 752 | 565504 | 425259008 | 27.4226 | 9.0937 |
| 703 | 494209 | 347428927 | 26.5141 | 8.8917 | 753 | 567009 | 426957777 | 27.4408 | 9.0977 |
| 704 | 495616 | 348913664 | 26.5330 | 8.8959 | 754 | 568516 | 428661064 | 27.4591 | 9. 1017 |
| 705 | 497025 | 350402625 | 26.5518 | 8.9001 | 755 | 570025 | 430368875 | 27.4773 | 9. 1057 |
| 706 | 498436 | 351895816 | 26.5707 | 8.9043 | 756 | 571536 | 432081216 | 27.49 | 9. 1098 |
| 70 | 499849 | 353393243 | 26.5895 | 8.9085 | 757 | 573049 | 433798093 | 27.5136 | 9. II 38 |
| 70 | 501264 | 354894912 | 26.6083 | 8.9127 | 758 | 574564 | 435519512 | 27.5318 | 9.1178 |
| 709 | 502681 | 356400829 | 26.6271 | 8.9169 | 759 | 576081 | 437245479 | 27.5500 | 9.1218 |
| 710 | 504100 | 357911000 | 26.6458 | 8.92 II | 760 | 577600 | 438976000 | 27.5681 | 9.1258 |
| 711 | 50552 I | 359425431 | 26.6646 | 8.9253 | 761 | 579121 | 440711081 | 27.5862 | 9. 1298 |
| 71 | 506944 | 360944128 | 26.6833 | 8.9295 | 762 | 580644 | 442450728 | 27.6043 | 9.1338 |
| 71 | 508369 | 362467097 | 26.7021 | 8.9337 | 763 | 582169 | 444194947 | 27.6225 | 9.1378 |
| 714 | 509796 | 363994344 | 26.7208 | 8.9378 | 764 | 583696 | 445943744 | 27.6405 | 9.1418 |
| 715 | 511225 | 365525875 | 26.7395 | 8.9420 | 765 | 585225 | 447697125 | 27.6586 | 9.1458 |
| 716 | 512656 | 367061696 | 26.7582 | 8.9462 | 766 | 586756 | 449455096 | 27.6767 | 9. 1498 |
| 717 | 514089 | 368601813 | 26.7769 | 8.9503 | 767 | 588289 | 451217663 | 27.6948 | 9. 1537 |
| 718 |  | 370146232 | 26.7955 |  | 768 | 589824 | 452984832 | 27.7128 | 9. 1577 |
| 9 | 516961 | 371694959 | 26.8142 | 8.958 | 769 | 591361 | 454756609 | 27.7308 | 9.1617 |
| 720 | 518400 | 373248000 | 26.8328 | 8.9628 | 770 | 592900 | 456533000 | 27.7489 | 9.1657 |
| 721 | 519841 | 374805361 | 26.8514 | 8.9670 | 771 | 59444 | 458314011 | 27.7669 | 9. 1696 |
| 722 | 521284 | 376367048 | 26.8701 | 8.9711 | 772 | 595984 | 460099648 | 27.7849 | 9. 1736 |
| 723 | 522729 | 377933067 | 26.8887 | 8.9752 | 773 | 597529 | 461889917 | 27.8029 | 9. 1775 |
| 724 | 524176 | 379503424 | 26.9072 | 8.9794 | 774 | 599076 | 463684824 | 27.8209 | 9.1815 |
| 725 | 525625 | 381078125 | 26.9258 | 8.9835 | 775 | 600625 | 465484375 | 27.8388 | 9.1855 |
| 726 | 527076 | 382657176 | 26.9444 | 8.9876 | 776 | 602176 | 467288576 | 27.8568 | 9.1894 |
| 727 | 528529 | 384240583 | 26.9629 | 8.9918 | 777 | 603729 | 469097433 | 27.8747 | 9. 1933 |
| 728. | 529984 | 385828352 | 26.9815 | 8.9959 | 778 | 605284 | 470910952 | 27.8927 | 9.1973 |
| 729 | 531441 | 387420489 | 27. | 9. | 779 | 606841 | 472729139 | 27.9106 | 9.2012 |
| 730 | 532900 | 389017000 | 27.0185 | 9.004 1 | - | 6084 | 474552000 | 27.9285 | 9.2052 |
| 731 | 53436 | 390617891 | 27.0370 | 9.0082 | 781 | 609961 | 476379541 | 27.9464 | 9.2091 |
| 732 | 535824 | 392223168 | 27.0555 | 9.0123 | 782 | 611524 | 478211768 | 27.9643 | 9.2130 |
| 733 | 537289 | 393832837 | 27.0740 | 9.0164 | 783 | 613089 | 480048687 | 27.9821 | 9.2170 |
| 734 | 538756 | 395446904 | 27.0924 | 9.0205 | 784 | 614656 | 481890304 | 28. | 9.2209 |
| 735 | 540225 | 397065375 | 37.1109 | 9.0246 | 785 | 616225 | 483736625 | 28.0179 | 9.2248 |
| 736 | 541696 | 398688256 | 27.1293 | 9.028 | 786 |  |  | 28.0357 | 9.2287 |
| 73 | 543169 | 400315553 | 27.1477 | 9.0328 | 787 | 619369 | 487443403 | 28.0535 | 9.2326 |
| 738 | 544644 | 401947272 | 27.1662 | 9.0369 | 788 | 620944 | 489303872 | 28.0713 | 9.2365 |
| 739 | 546121 | 403583419 | 27.1846 | 9.0410 | 789 | 622521 | 491169069 | 28.0891 | 9.2404 |
| 740 | 547600 | 405224000 | 27.2029 | 9.0450 | 790 | 624100 | 493039000 | 28. 1069 | 9.2443 |
| 741 | 549081 | 406869021 | 27.2213 | 9.0491 | 791 | 625 | 494913671 |  | 9.2482 |
| 742 | 550564 | 408518488 | 27.2397 | 9.0532 | 792 | 627264 | 496793088 | 28.1425 | 9.2521 |
| 743 | 552049 | 410172407 | 27.2580 | 9.0572 | 793 | 628849 | 498677257 | 28.1603 | 9.2560 |
| 744 | 553536 | 411830784 | 27.2764 | 9.0613 | 794 | 630436 | 500566184 | 28.1780 | 9.2599 |
| 745 | 555025 | 413493625 | 27.2947 | 9.0654 | 795 | 632025 | 502459875 | 28.1957 | 9.2638 |
| 746 | 556516 | 415160936 | 27.3130 | 9.0694 | 796 | 633616 | 544358336 | 8.2135 | 9.2677 |
| 747 | 558009 | 416832723 | 27.3313 | 9.0735 | 797 | 635209 | 506261573 | 28.2312 | 9.2716 |
| 748 | 559504 | 418508992 | 27.3496 | 9.0775 | 798 | 636804 | 508169592 | 28.2489 | 9.2754 |
| 749 | 56100I | 420189749 | 27.3679 | 9.0816 | 799 | 638401 | 510082399 | 28.2666 | 9.2793 |
| 750 | 562500 | 421875000 | 27.386I | 9.0856 | 800 | 640000 | 512000000 | 28.2843 | 9.2832 |

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to 1000-continued.

| No. | Squar | ube | Sq. Rt. | $\mathrm{Cu} . \mathrm{Rt}$. | No. | Square. | Cub | Sq. Rt. | Cu. Rt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 80 | 6416 | 51 | 28. | 9.28 | 851 | 724201 | 616295051 | 29.1719 |  |
| 802 | 6432 | 515849608 | 28.3196 | 9.2909 | 852 | 725904 | 618470208 | 29.1890 | I |
| 803 | 6448 | 517781627 | 28.3373 | 9.2948 | 853 | 727609 | 620650477 | 29.2062 | 9.4838 |
| 804 | 646416 | 519718464 | 28.3549 | 9.298 | 854 | 729316 | 622835864 | 29.2233 | 9.4875 |
| 805 | 648025 | 521660125 | 28.3725 | 9.3025 | 855 | 731025 | 625026375 | 29.2404 | 9.4912 |
| 806 | 649636 | 523606616 | 28.3901 | 9.3063 | 856 | 732736 | 627222016 | 29.2575 |  |
| 80 | 651249 | 525557943 | 28.4077 | 9.3102 | 857 | 734449 | 629422793 | 29.2746 |  |
| 808 | 652864 | 527514112 | 28.4253 | 9.3140 | 858 | 736164 | 631628712 | 29.2916 | 9.5023 |
| 80 | 654481 | 529475129 | 28.4429 | 9.3179 | 859 | 73788 I | 633839779 | 29.3087 | 9. 5060 |
| 81 |  | 531441000 | 28.4605 | 9.3217 | 860 |  | 636056000 | 29.3258 | 9. 5097 |
| 811 | 657721 | 533411731 | 28. | 9.3255 | 861 | 741321 | 638277381 | 29.3428 | 34 |
| 812 | 659344 | 535387328 | 28.4956 | 9.3294 | 862 | 743044 | 640503928 | 29.3598 | 9.5171 |
| 813 | 660969 | 537367797 | 28.5132 | 9.3332 | 863 | 744769 | 642735647 | 29.3769 | 9.5207 |
| 814 | 662596 | 539353144 | 28.5307 | 9.3370 | 864 | 746496 | 644972544 | 29.3939 | 9. 5244 |
| 815 | 664225 | 541343375 | 28.5482 | 9.3 | 865 | 748225 | 647214625 | 29.4109 | 9.5281 |
| 816 | 665856 | 543338496 | 28.5657 | 9.3447 | 866 | 749956 | 649461896 | 29.4279 | 5317 |
| 817 | 667489 | 545338513 | 28.5832 | 9.3485 | 867 | 751689 | 651714363 | 29.4449 | 354 |
| 818 | 669124 | 547343432 | 28.6007 | 9.3523 | 868 | 753424 | 653972032 | 29.4618 | 391 |
| 819 | 670761 | 549353259 | 28.6182 | 9.3561 | 869 | 755161 | 656234909 | 29.4788 | 427 |
| 820 | 672400 | 551368000 | 28.6356 | 9.3599 | 870 | 756900 | 658503000 | 29.4958 |  |
| 821 | 674 | 553387661 | 28.6531 | 9.3637 | 871 | 758 | 66 | 29. | 9.550I |
| ع22 | 67568 | 555412248 | 28.6705 | 9.3675 | 872 | 760384 | 663054848 | 29. | 9.5537 |
| 823 | 67732 | 557441767 | 28.6880 | 9.3713 | 873 | 762129 | 665338617 | 29.5466 | 9. 5574 |
| 824 | 678976 | 559476224 | 28.7054 | 9.3751 | 874 | 763876 | 667627624 |  | 9.5610 |
| 825 | 680625 | 561515625 | 28.7228 | 9.3789 | 875 | 765625 | 669921875 |  | 647 |
| 826 | 682276 | 563559976 | 28.7 | 9.3 | 876 | 767376 | 672221376 | 29.5973 | 9. 5683 |
| 8 | 683929 | 565609283 | 28.7576 | 9.3865 | 877 | 769129 | 674526133 | 29.6142 | 9.5719 |
| 828 | 685584 | 567663552 | 28.7750 | 9.3902 | 878 | 770884 | 676836152 | 29.6311 | 9.5756 |
| 829 | 687241 | 569722789 | 28.7924 | 9.3940 | 879 | 772641 | 679151439 | 29.6479 | 9.5792 |
| 830 | 688900 | 571787000 | 28.8097 |  |  | 774400 | 681472000 |  |  |
| 831 | 690561 | 573856191 | 28.8271 | 9.4016 | 881 | 776161 | 6837 | 29.6816 | 9.5865 |
| 832 | 692224 | 575930368 | 28.8444 | 9.4053 | 882 | 777924 | 68612896 | 29.6985 | 9.590I |
| 833 |  | 578009537 | 28.8617 | 9.4091 | 883 | 77968 | 688465387 | 29.7153 | 9.5937 |
| 834 | 695556 | 580093704 | 28.8791 | 9.4129 | 884 | 781456 | 690807104 | 29.7321 | 9.5973 |
| 835 | 697225 | 582182875 | 28.8964 |  | 885 | 783225 | 3154125 | 29.7489 |  |
| 336 | 698896 | 584277056 | 28.9137 | 9.4204 | 886 | 78 | 95506456 | 29.7658 | 9.6046 |
| 837 | 700569 | 586376253 | 28.93 IO | 9.4241 | 888 | 786769 | 697864103 | 29.7825 | 9.6082 |
| 835 | 702244 | 588480472 | 28.948 | 9.4279 | 888 | 788544 | 700227072 | 29.7993 | 9.6118 |
| 5 | 70392 | 590589719 | 28.9655 | 9.4316 | 889 | 790321 | 702595369 | 29.8161 | 9.6154 |
| 340 | 7056 | 592704000 | 28.9828 | 9.4354 | 8 | 7921 | 704969000 | 29.8329 | 619 |
| 841 | 707281 | 594823321 | 29. | 9.4391 | 891 | 793881 | 707347971 | 29.8496 | 9.6226 |
| 842 | 708964 | 596947688 | 29.0172 | 9.4429 | 892 | 795664 | 709732288 | 29.8664 | 9.6262 |
| 843 | 710649 | 599077107 | 29.0345 | 9.4466 | 893 | 797449 | 712121957 | 29.8831 | 9.6298 |
| 844 | 712336 | 601211584 | 29.0517 | 9.4503 | 894 | 799236 | 714516984 | 29.8998 | 9.6334 |
| 845 | 714025 | 603351125 | 29.0689 | I.454I | 895 | 801025 | 716917375 | 29.9166 | 9.6370 |
| 846 | 715716 | 605495736 | 29.0861 | 9.4578 | 896 | 802816 | 719323136 | 9.9333 | 9.6406 |
| 847 | 717409 | 607645423 | 29.1033 | 9.4615 | 897 | 804609 | 721734273 | 29.9500 | 9.6442 |
| 848 | 719104 | 609800192 | 29.1204 | 9.4652 | 898 | 806404 | 724150792 | 29.9666 | 9.6477 |
| 849 | 720801 | 611960049 | 29.1376 | 9.4690 | 899 | 808201 | 726572699 | 29.9833 | 9.6513 |
| 850 | 722500 | 614125000 | 29.1548 | 9.4727 | 900 | 810000 | 729000000 | 30. | 9.6549 |

## APPENDIX

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers
from I to 1000-continued.

| No. | Squar | Cub | Sq. R | Cu . | No. | Squa | Cub | Sq. Rt. | $\mathrm{Cu} . \mathrm{Rt}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 901 | 811801 |  | 30.01 |  | 95 |  | 860085351 | 30.8383 |  |
| 902 | 81360 | 7338708 | 30.0333 |  | 952 | 90630 |  | 30.8545 | 9.8374 |
| 903 | 81540 | 736314327 | 30.05 | 9.6656 | 953 | 9082 | 865523177 | 30.8707 | 9.840 |
|  | 817216 | 738763264 | 30.0 | 9.6692 | 954 | 9101 | 868250664 | 30.8869 |  |
| 905 | 819025 | 741217625 | 30.0832 | 9.6727 | 955 | 912 | 870983875 | 30.9031 |  |
| 906 | 8208 | 74.3 | 30.0998 | 9.6763 | 55 | 9139 | 873722816 | 30.9192 |  |
| 907 | 822649 | 746142643 | 30. 1164 | 9.6799 | 957 | 915849 | 876467493 | 30.9354 |  |
| 908 | 824464 | 748613312 | 30.1330 | 9.6834 | 95 | 917764 | 879217912 | 30.9516 |  |
| 909 | 82 | 751089429 | 30. 1496 | 9.6870 | 959 | 91968 I | 881974079 | 30.9677 |  |
| 910 | 828100 | 753571000 | 30.1 | 9.6905 |  | 921600 | 884736000 | 30.9839 |  |
| 911 | 829921 | 756058 | 30.1828 | 9.6 | 961 | 92352 I | 887503681 | 3 I . |  |
| 912 | 831744 | 758550528 | 30. 1993 | 9.6976 | 962 | 9254 | 890277128 | 31.0161 |  |
| 913 | 83356 | 761048497 | 30.2159 | 9.7012 | 963 | 9273 | 893056347 | 31.0322 | 51 |
| 914 | 83539 | 763551944 | 30.2324 | 9.704 | 964 | 929296 | 895841344 | 31.0483 |  |
| 915 | 837225 | 766060 | 30.2490 |  | 965 | 931225 | 898632125 | 31.0644 |  |
| 916 | 839056 | 768575296 | 30.2655 | 9.7118 | 966 | 933 | 901428696 | 31.0805 |  |
| 917 | 840889 | 771095213 | 30.2820 | 9.715 | 967 | 9350 | 9042310 | 31.0966 |  |
| 918 | 842724 | 773620632 | 30.2985 | 9.7188 | 968 | 937024 | O7039232 | 31.1127 | 8922 |
| 919 | 844561 | 776151559 | 30.3150 | 9.7224 | 969 | 9389 | 909853209 | 31.1288 |  |
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[^0]:    ${ }^{1}$ Entropy, by James Swinburne, Westminster, 1904.

[^1]:    * See Art. 5, Law of April 7, 1795, French Republic.
    $\dagger$ Great Britain did not join the Convention until 1884.

[^2]:    * Board of Trade Report, 367 of 1898, page 9.
    $\dagger$ See "Détermination expérimentale de la valeur du mètre en longueurs d'ondes lumineuses," A. A. Michelson, vol. xi., Travaux et Mémoires, Bureau International des Poids et Mesures ; also, Board of Trade Report, 373 of 1896, page 37.

[^3]:    * Board of Trade Report, 367 of 1898, page 9.

[^4]:    * See Proces-verbaux du Comité international des Poids et Mesures, Session 1905, p. 55.
    $\dagger$ Board of Trade Report, 367 of 1898, page 9.

[^5]:    * P.S. signifies Parliamentary Standard.

[^6]:    * Board of Trade Report 9, Sess. 2 of 1886, p. 1. This Parliamentary Copy of the pound is referred to as No. 5 P.C., and is deposited at the Standards Office.

[^7]:    $\dagger$ Philosophical Transactions, Royal Society, 1798, p. 133.
    $\ddagger$ Phil. Trans., Roy. Soc., 1821, pp. 316, 326.

[^8]:    *Trans. Royal Society, 1892, pp. 331-354; also Board of Trade Retort, 302 of 1889, p. 10.
    $\dagger$ See Board of Trade Report 9, Sess. 2, 1886. The Orange River Colony, the Transvaal, and Rhodesia have since been included.

[^9]:    * i.e. the international metric standards deposited at Breteuil Observatory, near Paris.

[^10]:    * See Dr. Williams' Chinese Commercial Cuide.

[^11]:    * Board of Trade Report 9, Sess. 2, 1886, pp. 46 and 49.
    $\dagger$ Board of Trade Report, 392 of 1897, p. 6.

[^12]:    * Board of Trade Report, 392 of 1897, p. 6.
    $\dagger$ Board of Trade Report, 302 of 1889, p. 6.
    $\ddagger$ Board of Trade Report, 364 of 1893, p. 13 .

[^13]:    * Board of Trade Reports, 262 of 1887, p. 3, and 330 of 1888, p. i.
    + Board of Trade Report, 302 of 1889, pp. 2 and 7.
    $\ddagger$ See Natal Laws, No. 11 of 1852, No. 19 of 1872, and No. 39 of 1884.
    § Cape Colony Law, No. 9 of 1859.
    $\| i . e$. the international metric standards deposited at Breteuil Observatory, near Paris.

[^14]:    * Board of Trade Report, 432 of 1895, pp. 3 and 23.
    $\dagger$ Board of Trade Report, 373 of 1896, p. 37.
    $\ddagger$ Dêtermination du Rapport du Yard au Mêtre, by Dr. Benoît (Director of the International Bureau of Weights and Measures), Paris, 1896.

[^15]:    * Travaux et Mémoires, Comité international des Poids et Mesures, Tome IV., 1885 ; also Board of Trade Annual Weights and Measures Report, 1884.
    $\dagger$ H. J. Chaney, Our Weights and Measures, London, 1897, p. 67.

[^16]:    * Bulletin No. 26, U.S. Coast and Geodetic Survey, 5th April, 1893.
    $\dagger$ In the United States a liter is regarded as the volume of a cubic decimeter, which, according to the most recent determination (see p. 4), involves an error of only 26 parts in a million.

[^17]:    * See Board of Trade Report, 326 of 1901, p. 5 .

[^18]:    * Tables of Equivalents, Washington, Nov. 1906. The U.S. legal equivalents are given on page 40 .

[^19]:    *(The scientific equivalents published by the Bureau of Standards, Washington, are given on page 39.)

[^20]:    * The relation of the British Imperial to the Metric equivalents given in these tables is not quite accurate, as will be seen by reference to page 14.

[^21]:    * From the equivalent given on page 34, . $42008 \dot{3}$ hectare $=1.03805$ acres.

[^22]:    * The British legal equivalent of 198 litres is 43.55505 gallons.

[^23]:    * Kindly compiled by Mr. F. Moshack of the Deutsche Bank.

[^24]:    * Comptes Rendus des séances de la Troisième Conférence générale des Poids et Mesures à Paris, igor, p. 70.
    $\dagger$ This is the value adopted by the Board of Trade Standards Department.

[^25]:    *The terms ohm and volt were first suggested by Sir C. Bright and Mr. Latimer Cross: together with ampere, coulomb and farad, they were adopted by an International Congress which met in 1881. The use of the terms joule, watt and henry was recommended by the Chamber of Delegates at the Chicago Exhibition in 1893.
    $\dagger$ Final Report of the Electrical Standards Committee, 1894, p. 10.
    $\ddagger$ This Standard was legalised by Order in Council of her late Majesty Queen Victoria of Aug. 23, 1894.

[^26]:    * Final Rep. of the Elect. Stand. Comm., 1894, p. ro. $\dagger$ Loc. cit., p. II.
    $\ddagger$ Loc. cit. Clark's cell consists of zinc or an amalgam of zinc with mercury and of mercury in a neutral saturated solution of zinc sulphate and mercurous sulphate in water, prepared with mercurous sulphate in excess.

[^27]:    * Preston's Theory of Heat, 2nd edition, London, 1904, p. 322.

[^28]:    * Preston's Theory of Heat, London, 1904, p. 45.

[^29]:    * Metropolis Gas Act of 1860.
    †Journal für Gasbeleuchtung, Munich, 30 June, 1906, pp. 559-56r.

[^30]:    * This table was compiled by Landolt and Börnstein from determinations made by Thiesen, Scheel and Marek. It is taken from the Smithsonian Physical Tables, Washington, 1906.

[^31]:    * Treatise on Hydraulics, New York, 1904, p. 559.

[^32]:    *Smithsonian Physical Tables, Washington, 1906, p. 119.

[^33]:    ＊From the Smithsonian Physical Tables，Washington，1904：based on a Table by Dwelshauvers－Dery（Trans．Am．Soc．Mech．Eng．，vol．xi．）．

[^34]:    * Smithsonian Physical Tables, Washington, 1906.

[^35]:    * The tonnage is not affected by the shape of the area. No deduction has been made for dykes or faults.

[^36]:    * Brit. Assoc. Rep. for 1905, p. 404.

[^37]:    * The British sovereign, which is 916.6 ( 22 carats) fine, weighs 123.27447 grains. The gold of which it is coined is termed "standard gold," and has a value of $£ 317 \mathrm{~s}$. ro $\frac{1}{2}$ d. per oz.

[^38]:    * The O.R.C. Precious Metals Ordinance of 1904.
    $\dagger$ The O.R.C. Precious Stones Ordinance of 1904.
    $\ddagger$ Cape of Good Hope Colony, Precious Minerals Act of 1898 and Precious Stones Act of 1899.

[^39]:    * The Gold Coast Colony and Ashanti Concessions Ordinance of 1900.
    $\dagger$ Mining Lawes of the British Empire, C. J. Alford, London, 1906, p. 35 et seq.

[^40]:    * The New South Wales Mining Act of 1874, Section 36.
    $\dagger$ Regulations relating to Mineral Leases on Crown Lands, February 1885.
    $\ddagger$ The Mining Act of Queensland, 1898.

[^41]:    * From the South Australian Mining Act of 1803 .
    $\dagger$ The Victorian Mines Acts of 1890 and 1897.
    $\ddagger$ The Mining Act of West Australia, 1904.
    § Tasmanian Mining Acts of 1900 and 1905.

[^42]:    * New Zealand Mining Act, No. 38 of 1898.

[^43]:    * British Guiana Mining Regulations, 1903.
    $\dagger$ H. G. Granger and E. B. Treville, p. 85, Trans. Am. Inst. M.E., vol. 28, 1899.
    $\ddagger$ Chilian Mining Law of 1888 .

[^44]:    * From Mining. Lazus of the British Empire, by C. J. Alford, London, 1906, p. 64.
    $\dagger$ The States of Pahang Mining Enactment of 1904.

[^45]:    * The area of a circular segment on railroad curves, where the chord is very long in proportion to the height, may be found with great accuracy by this formula.

[^46]:    * Rule for 'short' multiplication: Reverse the multiplier and place it below the multiplicand so that its unit figure (the one preceding the
    decimal point) is directly under that decimal place of the

    Therefore in checking by natural sines and cosines, in order to get the product to two decimal places reverse the function 4150 and place its initial figure under the first decimal place of the 415 multiplicand. (See the above calculation, where $.67787=$ the nat. $\cos$ of $\left.47^{\circ} 19^{\prime} 20^{\prime \prime}\right)$.

[^47]:    * From The Smithsonian Geographical Tables, Washington, 1906, p. 23.

