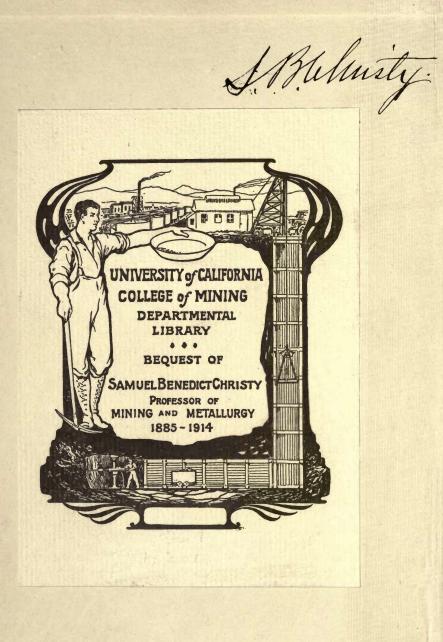
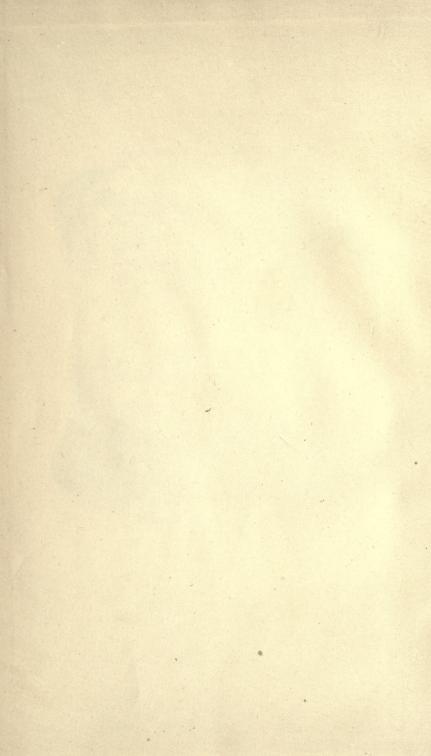
MINING TABLES

HATCH AND VALLENTINE







MINING TABLES

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MINING TABLES

BEING A COMPARISON OF THE UNITS OF WEIGHT, MEASURE, CURRENCY, MINING AREA, ETC., OF DIFFERENT COUNTRIES; TOGETHER WITH TABLES, CONSTANTS & OTHER DATA USEFUL TO MINING ENGINEERS AND SURVEYORS

BY

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PREFACE

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Most engineers get together a quantity of formulae, constants and other data useful to them in the exercise of their profession, which are not always to be found in text-books. The authors, having arranged and tabulated a collection of this nature for their own use, decided to print it, believing that its publication would be of service to other workers in the same field.

The work thus begun has extended beyond the original plan, especially in regard to the tables of weight and measure, which have been compiled from the latest publications of the "Bureau international des Poids et Mesures" and of the Board of Trade. It appears that most published equivalents of the British Imperial and Metric measures of length are based either on a comparison made in Paris in 1818 by Arago and Kater, or on a comparison made in 1866 by Capt. A. R. Clarke of the Ordnance Survey. Similarly, Professor Miller's determination in 1844 of the avoirdupois pound as equal to 453.59265 grammes forms the usual basis of comparison for the weights of the British Imperial and Metric systems. The values adopted in this book are derived from determinations since made under the direction of the International Committee of Weights and Measures and of the Board of Trade, and legalised by Order in Council of the 19th May, 1898. In like manner the equivalents of the Russian weights and measures adopted are based on the results of Prof. D. Mendelieff's work in 1897, which were subsequently embodied in the Russian Weights and Measures Law of June, 1899.

The definitions of the electrical units given in Section II. of Part II. are taken chiefly from the Reports made to the Board of Trade in 1892 and 1894 by the Electrical Standards Committee, and the Order in Council made by her late Majesty on the

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PREFACE

23rd August, 1894. They are defined in terms of the fundamental units of length (the centimetre), mass (the gramme), and time (the second), from which this system of units has come to be known as the c.g.s. (centimetre-gramme-second) system.

The compilation of the short section on thermal units disclosed the existence of much confusion in text-books, largely due to the various thermometric scales in use. There is also an absence of any agreement as to the terminology of the units. For instance, as Swinburne points out, there is no name for the unit of difference of temperature, "degree" being almost as primitive as "mark" or "notch."¹ Again, the British thermal unit or pound-degree (Fahrenheit) has no name; and "calorie" may mean either the gramme-degree (Centigrade) or the kilogram-degree (Centigrade). In regard to specific heat, thermal capacity, calorific power and thermal efficiency, there is a lack of authoritative definition such as has fixed for all time the electrical units.

The mining data collected in Part V. refer rather to the physical properties of ore-bodies than to the mechanical devices for their extraction. Thus, hoisting, pumping and ventilation, to which many special treatises have been devoted, are not dealt with. On the other hand, tables are given by which the calculation and valuation of ore-reserves are assisted and simplified. The latest information regarding the question of underground temperatures is summarised. The various methods in use in different countries for expressing gold ore values and for stating copper prices are compared. Finally, there is a section on mining areas which has been carefully compiled from the laws now in force in the Colonies and in foreign countries where mining is carried on.

The data relating to surveying which comprise Part VI. include a description of the conventional methods in practical use for the coordination of survey points, also a description of the use of the tacheometer, and a table for the calculation of heights and distances from tacheometric readings.

¹ Entropy, by James Swinburne, Westminster, 1904.

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PART I. WEIGHTS AND MEASURES.

SECTION I. STANDARD UNITS.

THE METRIC SYSTEM.

Length.—The original intention of the founders of the Metric System was to select from nature itself some permanent and invariable unit of length, which could be measured with a high degree of precision, and might therefore be reproduced at will. The metre, which was the unit selected, was intended to be equal to one ten-millionth of a terrestrial meridian contained between the north pole and the equator.* The geodetic survey from Barcelona to Dunkirk, from which the length of the arc of the meridian was computed, was conducted by Méchain and Delambre between the years 1792 and 1798.

A platinum standard was then constructed and deposited in the Archives of the French Republic in 1799, being legalised in the same year. This standard is known as the *Metre of the Archives*. It is a platinum bar 25 millimetres broad, 4 millimetres thick, and, being an 'end' standard, is exactly one metre long at \circ° C.

Subsequent researches showed that the length of the arc differs from that determined by the original triangulation to an extent equivalent to about o. I millimetre in the standard metre. Nevertheless, the Metre of the Archives is adhered to as the unit of length, although its reference to the earth's quadrant has been abandoned.

In 1875 the International Bureau of Weights and Measures was established at Breteuil, near Paris, under a Metric Convention signed by twenty different High Contracting States[†] for the

+ Great Britain did not join the Convention until 1884.

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^{*} See Art. 5, Law of April 7, 1795, French Republic.

purpose of constructing, restoring, and verifying new metric standards (now known as the international prototypes) to replace the standards of the Archives. Accurate copies of the new standards were also to be constructed for all the contracting States. Thirty-one standards of iridio-platinum, with a cross-section nearly of the shape of the letter X, known as the 'Tresca' form, were made, and compared with the Metre of the Archives and with one another. These were approved of by the International Committee in 1889, the standard most nearly approximating to the length of the Metre of the Archives being selected as the International Prototype Standard Metre and deposited in the Observatory at Breteuil. The remaining national prototype standards were distributed by lot to the different contracting States.

The British Prototype Standard Metre "is represented by the distance marked by two fine lines on the iridio-platinum standard bar numbered 16, when at the temperature of \circ° Centigrade. This bar is deposited with the Board of Trade." *

An elaborate series of researches carried on at the International Bureau of Weights and Measures has shown that it is possible, after all, to realise the desire of the founders of the Metric System to refer the metre to a natural unit; for the standard can be expressed in terms of wave-lengths of light. In 1893 Professor A. A. Michelson found that, by the interference method, 1553163.5 wave-lengths of the red ray of cadmium, measured in air at 15° C., under an atmospheric pressure of 760 millimetres, are equal to the length of the International Prototype Standard Metre.[†]

Weight.—The unit of weight in the Metric System is the *Gramme*, which was originally defined "as the absolute weight of a volume of pure water equal to a cube of the one-hundredth part of a metre, and at the temperature of melting ice." As this unit, however, is rather small for accurate weighings, a weight of 1000 grammes was adopted as the practical standard. The first step in the preparation of the original standard kilogram (1000

* Board of Trade Report, 367 of 1898, page 9.

† See "Détermination expérimentale de la valeur du mètre en longueurs d'ondes lumineuses," A. A. Michelson, vol. xi., *Travaux et Mémoires, Bureau International des Poids et Mesures*; also, *Board of Trade Report*, 373 of 1896, page 37.

SECT. I.

grammes) was the determination of the weight in vacuo of a cubic decimetre (1000 cubic centimetres) of distilled water at its maximum density. This was found to be 18,827.15 grains of the Pile de Charlemagne. A platinum standard of that weight was then constructed and deposited in the Archives of the French Republic in 1799. It is known as the Kilogram of the Archives. In form it is cylindrical, with height equal to the diameter and with its edges slightly rounded. When the construction of new standards for the metre and the kilogram was authorised under the Metric Convention, it was decided, since the kilogram did not represent the mass of a cubic decimetre of water with scientific accuracy, to adopt the Kilogram of the Archives as the standard unit of weight, and subsequently to determine its true relation to the mass of a cubic decimetre of distilled water at its temperature of maximum density. Accordingly, in 1879, three iridio-platinum standard kilograms were made, cylindrical in form, and of a density of 21.55. They were compared with the Kilogram of the Archives and with one another; and in 1883 the one known as K III. was adopted as the International Prototype Standard Kilogram. It has since been designated by R. although it bears no mark. Forty cylindrical iridio-platinum national prototype kilograms were then made, and compared with It and with one another. They were approved of by the International Committee in 1889, and distributed by lot to the different contracting States. The British Prototype Standard Kilogram "is represented by the cylindrical iridio-platinum standard kilogram weight numbered 18, which is deposited with the Board of Trade." *

Capacity.-The unit of capacity in the Metric System is the Litre, which was intended to be the volume of a cubic decimetre, so that a litre of distilled water at 4° C. should weigh exactly a kilogram. But on further investigation it was found that this was not scientifically accurate, and it was therefore decided by the International Committee to define the Litre as "the volume occupied by the mass one kilogram of pure water at its maximum density and under normal atmospheric pressure," this definition being sanctioned at the General Conference of 1901. Recent determinations of the weight in vacuo of a cubic decimetre of distilled water at its temperature of maximum * Board of Trade Report, 367 of 1898, page 9.

density (4° C.) made independently by Benoît, Chappuis, Macé de Lépinay and Buisson, gave very uniform results, the mean of which was found to be 0.999974 kilogram.* This value has been provisionally adopted by the Bureau international des Poids et Mesures pending the completion of a further elaborate series of experiments now being made at the Bureau, the results of which will be announced at the sexennial General Conference of the delegates representing the contracting States of the Metric Convention, which is to be held at Paris in October, 1907. It is anticipated that any variation between the provisional and the new values will only affect the sixth decimal place. Consequently, for all practical purposes a litre can be regarded as the volume of a cubic decimetre, the error involved being only 26 parts in a million.

The British Standard Litre "is represented by the capacity at o° Centigrade of the cylindrical brass measure marked 'Litre, 1897' (which is deposited with the Board of Trade), and having a diameter equal to one half its height. This Litre at o° Centigrade when full contains one kilogram of distilled water at the temperature of 4° Centigrade, under an atmospheric pressure equal to that represented by a column of mercury 760 millimetres high at o° Centigrade, at sea level, and at latitude 45°; the weighing being made in air, but reduced by calculation to a vacuum." †

The Metric System is in use in the following countries, to the exclusion of the older systems, except where noted :

Argentine. Almost exclusively used.

Austria. Old system still sometimes used.

Belgium.

4

Brazil. In common use.

Bulgaria. Old system not entirely supplanted.

Chile. In common use.

Colombia. Both old and metric systems used.

Denmark. Used by State Railways; but not in general use. It has been made compulsory by a law passed in March, 1907.

Ecuador. Old system used in commerce, metric officially.

Egypt. Old system used in commerce, metric officially and by engineers, etc.

Finland.

* See Procès-verbaux du Comité international des Poids et Mesures, Session 1905, p. 55.

+ Board of Trade Report, 367 of 1898, page 9.

STANDARD UNITS

SECT. I.]

France. Germany. In general use, but old measures sometimes encountered. Great Britain. Optional, but not in general use. Greece. Very little used. Guatemala. Used officially but not generally. Hungary. In general use : old system dying out. Italy. In general use, but old system still found in the south. Japan. Not in general use. Luxemburg. Old system practically obsolete. Mexico. In general use : old system dying out Montenegro. In general use. Netherlands. Almost entirely used, but old system sometimes encountered. Norway. Peru. Only used by Government. Philippine Islands. Porto Rico. Portugal. Russia. Optional, but not in general use. Servia. In general use. Siam. Used by railways and public works. Spain. In general use, but old measures still encountered. Sweden. Switzerland. United States of America. Optional, but not in general use. Uruguay. Venezuela. Only used officially.

THE BRITISH IMPERIAL SYSTEM.

Length.—The British Imperial Standard unit of length is the *Yard*. The 'line' standard constructed by Bird in 1760 having been lost in the fire which destroyed the Houses of Parliament in 1834, the present standard yard was made by Messrs. Baily and Sheepshanks in 1843, by reference to the 5-foot brass Shuckburgh scale of 1796, the two iron standards made for the Ordnance Survey in 1826-7, the brass tubular scale of the Royal Astronomical Society, and the Kater scale of 1831 made for the Royal Society.

It is a solid bar of 'Baily's metal' (16 parts by weight of

copper, $2\frac{1}{2}$ of tin, and 1 of zinc) 38 inches long, with a crosssection 1 inch square. Near its ends are two circular wells half an inch deep. At the bottom of these wells, and consequently on the 'neutral plane' of the bar, are gold studs, on which the fiducial lines are engraved, the distance between them forming the British Imperial Standard Yard at a temperature of 62° Fahr. It was legalised by the Standards Act of 1855. It is preserved at the Standards Office, Westminster, and has been in the custody of the Board of Trade since 1866.

Thirty-nine copies of this standard were made of the same material and dimensions. Four of these are specially designated Parliamentary Copies, which, by the Weights and Measures Act of 1878, must be compared with each other once in every ten years and with the Imperial Standard once in every twenty years, in order to ensure the perpetuation of the standard. These Parliamentary Copies are stamped with the temperature at which they represent the true standard, namely:

| P.C. 2 in | the custod | y of the | Royal Mint : standard at 61.94° F. |
|-----------|------------|----------|---|
| P.C. 3 | >> | " | Royal Society : standard at 62.10° F. |
| P.C. 4 | >> | " | Royal Observatory, Greenwich : standard |
| | | | at 62.16° F. |
| P.C. 5 | " | >> | New Palace, Westminster: standard at |
| 1.1 | | | 61.98° F. |

The remaining thirty-five copies were distributed to various nations and scientific institutions.

Weight.—The British Imperial standard unit of weight is the Avoirdupois Pound of 7000 grains. The standard troy pound of 5760 grains having been destroyed in the fire of 1834, the avoirdupois pound of 7000 grains was substituted as the standard, on the recommendation contained in a report submitted by the Parliamentary Standards Committee, Dec. 21, 1841; and the present standard pound was constructed by Prof. W. H. Miller in 1844 by reference to a troy pound belonging to the Royal Society, and a troy pound the property of Prof. Schumacher. It is of platinum, cylindrical in form, 1.35 inches high and 1.15 inches in diameter, with a density of 21.1572. It has a small groove in its circumference to permit of its being lifted with an ivory fork, and is marked 'P.S. 1844. I lb.'* on its upper surface. It was legalised in 1855, and is preserved at the Standards

* P.S. signifies Parliamentary Standard.

PART I.

STANDARD UNITS

SECT. I.]

Office, Westminster, in the custody of the Board of Trade. As in the case of the unit of length, there are four Parliamentary Copies. Compared with the standard,

No. I P.C., which is in the custody of the Royal Mint, is 0.00051 grain too heavy.

No. 2 P.C., in the custody of the Royal Society, is 0.00089 grain too light.

No. 3 P.C., in the custody of the Royal Observatory, Greenwich, is 0.00178 grain too light.

No. 4 P.C., in the custody of the New Palace, Westminster, is 0.00314 grain too light.

The Weights and Measures Act of 1878 provides that one additional Parliamentary copy of the Standard Vard and of the Pound should be made. These were constructed and approved of by the Board of Trade, and were accordingly legalised by an Order in Council of Aug. 3, 1886.* The Board of Trade secondary standards, by which all other standards are tested, are required by the Act to be re-verified once every five years by comparison with these new Parliamentary copies.

Capacity.—The British Imperial standard unit of capacity is the *Gallon*, which is the volume of ten Imperial standard pounds of distilled water weighed in air against brass weights, with the water and air at a temperature of 62° Fahr. and under a barometric pressure of 30 inches. The standard is of brass, with a diameter equal to its depth, and bears the date of 1828. It is in the custody of the Board of Trade, and is deposited at the Standards Office, Westminster. A standard Bushel (equal to 8 gallons) is also preserved at the Standards Office as the unit of dry measure It is of gun-metal, with a diameter equal to twice its depth. It dates from 1824, and was verified in 1825.

The Weights and Measures Act of 1824 gives the weight of a cubic inch of distilled water under standard conditions as 252.458 grains, a value derived from weighings made by Sir George Shuckburgh in 1798 † and Captain Henry Kater in 1821.‡ On this basis, 277.274 and 2218.192 cubic inches are the volumes of the Imperial gallon and bushel respectively.

* Board of Trade Report 9, Sess. 2 of 1886, p. 1. This Parliamentary Copy of the pound is referred to as No. 5 P.C., and is deposited at the Standards Office.

Philosophical Transactions, Royal Society, 1798, p. 133.
Phil. Trans., Roy. Soc., 1821, pp. 316, 326.

In 1889, Mr. H. J. Chaney determined the mass of a cubic inch of distilled water, freed from air, weighed in air against brass weights of a density of 8.143, with the water and air at a temperature of 62° Fahr. and the barometer at 30 inches, to be 252.286 grains $\pm .0002$ grain.* The weight of a cubic foot of such water under similar conditions would therefore be 62.278601 lbs., and the volume of the Imperial gallon and of the bushel 277.46288 and 2219.70304 cubic inches respectively. Although no direct determination of the weight of a cubic inch of water has since been made, the foregoing values have been superseded. It has been found that I litre = 1.000026 cubic decimetres (see p. 4), and that 4.5459631 litres = I Imperial gallon (see p. 15); therefore, under standard conditions:

The weight of 1 cubic inch of water at 62° F. = 252.3253 grains. ,, 1 cubic foot of water at 62° F. = 62.2883 lbs.

and the volume of r Imperial gallon $\begin{cases} = 277.420 \text{ cubic} \\ \text{inches.} \end{cases}$

These values have been provisionally adopted by the Board of Trade Standards Department.

The Imperial Weights and Measures are now legally in force in the following Colonies, etc.:

| Antigua. | Jamaica. | Sierra Leone. |
|--------------------|---------------------|----------------------|
| Barbadoes. | Malta. | Straits Settlements. |
| Bermuda. | Natal. | South Australia. |
| British Guiana. | Nevis. | St. Christopher. |
| British Honduras. | New Brunswick. | St. Helena. |
| Canada. | New South Wales. | St. Vincent. |
| Cape of Good Hope. | New Zealand. | Transvaal. |
| Cyprus. | Nova Scotia. | Tobago. |
| Dominica. | Orange RiverColony. | Trinidad. |
| Grenada. | Queensland. | Vancouver's Island. |
| Hong Kong | Rhodesia. | Victoria. |
| | Wastown Australia 4 | |

Western Australia.[†]

An Act of 1897 permits the use of Metric Weights and Measures in the United Kingdom, and provides that the Board of Trade standards shall include metric standards.

* Trans. Royal Society, 1892, pp. 331-354; also Board of Trade Report, 302 of 1889, p. 10.

+ See Board of Trade Report 9, Sess. 2, 1886. The Orange River Colony, the Transvaal, and Rhodesia have since been included.

THE UNITED STATES OF AMERICA.

The weights and measures of the United States are practically identical with those of the British Imperial System, with the exception of the measures of capacity which, although defined in units having the same names and sub-divisions, have quite different volumes.

The use of the Metric System is recognised by an Act of 1866. Prototype standard meters, Nos. 21 and 27, and kilograms, Nos. 4 and 20, were received from the International Bureau of Weights and Measures in 1889, and Meter No. 27 and Kilogram No. 20 were adopted as the National Prototype Standards in 1890. In Bulletin No. 26 of the 5th April, 1893, issued by the U.S. Coast and Geodetic Survey with the approval of the Secretary of the Treasury, the United States Government recognises "the International Prototype Meter and Kilogram* as fundamental standards," and states that "the customary units, the yard and the pound, will be derived therefrom in accordance with the Act of July 28, 1866." The metric equivalents of the yard and the pound legalised by this Act differ in a slight degree from the British equivalents legalised in 1898, but the differences are so small that, for all practical purposes, they may be disregarded (see pp. 36 and 40). In 1901 the custody of the national standards was transferred from the Coast and Geodetic Survey to the Bureau of Standards, which was established in that year under the Department of Commerce and Labor.

Liquid Measure.—The standard unit of liquid measure is the U.S. Gallon, which is derived from the Queen Anne wine gallon of 1707. It is defined as having a volume of 231 cubic inches. It is also the standard unit of Apothecaries' Fluid Measure.

Dry Measure.—The standard unit of dry measure is the U.S. Bushel, which is derived from the old Winchester "struck" bushel. It is defined as having a volume of 2150.42 cubic inches. The U.S. Bushel measure has the form of an inverted frustum of a right cone of the following dimensions

* *i.e.* the international metric standards deposited at Breteuil Observatory, near Paris.

(inside measurement): top diameter, $19\frac{1}{2}$ inches; bottom diameter, $18\frac{1}{2}$ inches; depth, 8 inches.

The dry measures are considerably larger than the *liquid* measures of the same name; for instance, the dry U.S. gallon $(\frac{1}{8}^{th} \text{ bushel}) = 268.8025$ cubic inches, while the *liquid* U.S. gallon = 231 cubic inches.

RUSSIA.

Length.—In 1833 the Russian units of length were defined in terms of British feet, and a standard *Sagene* (equal to 7 British feet) was constructed and compared with the British Imperial Standard Yard, and subsequently legalised by an Act of Oct 1835. A standard *Archine*, equal to $\frac{1}{3}$ sagene, constructed by Prof. Kupffer, is recognised as the standard unit of length by a law passed in June 1899. It is an iridio-platinum 'line' standard of Tresca form, standard at $16\frac{2}{3}^{\circ}$ C. (62° F.), and is inscribed H 1894. It is defined as equal to 28 British inches or 0.711200±0.000001 metre.

Weight.—The standard unit of weight is the *Funt* or Russian pound. The standard Funt is of iridio-platinum of a density of 21.51 at $16\frac{2}{3}$ ° C., and is inscribed $\frac{H}{11}$ 1894. It was reproduced from the platinum funt of 1835, which was derived from a funt of 1747. It is defined as equal to 0.40951241±0.0000001 kilogram.

Capacity.—The standard units of liquid and dry measures are respectively the *Vedro* and the *Tchetverik*. The Vedro is defined as the volume of 30 funts, weighed *in vacuo*, of distilled water at a temperature of $16\frac{2}{3}^{\circ}$ C. The Tchetverik is defined as the volume of 64 funts of such water under similar conditions.

The national standards are deposited at St. Petersburg.

The law of June 1899, which became effective on Jan. 1, 1900, permits the use of the Metric System.

CHINA.

The Weights and Measures of China have different local names and values.* The only standards legally in use for international * See Dr. Williams' Chinese Commercial Guide.

SECT. I.]

purposes are those adopted in the foreign treaties for the payment of duties at the Foreign Maritime Customs. By Rule IV. of the Rules of Trade signed at Shanghai on Nov. 8, 1858, the weight of a Pikul (Tam) of 100 Katis (Kan or Chin) is defined as equal to 1331 lbs. avoirdupois, and the length of a Chang of 10 Ch'ih as equal to 141 British inches. Similar equations were adopted in the Rules of Trade appended to other foreign treaties. The standard Chinese weights verified for Hong Kong by the Board of Trade in 1900-01 were a Tam of 1331 lbs., a Kan of 11 lbs., and a Tael of 11 oz. avoirdupois. The Standard Ying-tsao Ch'ih or foot of the Chinese Board of Works, from which all measures connected with the Revenue, whether of length, capacity, or weight, are derived, is approximately equal to 12.5 British inches;* but different local commercial standards obtain throughout the whole of China. A standard Chinese ' Chek' (Ch'ih) of $14\frac{5}{8}$ inches, divided into 10 'Tsun,' and each Tsun into 10 'Fan,' was verified by the Board of Trade Standards Department in 1896-97 for Hong Kong, where both British and Chinese weights and measures are used.† Measures of capacity are seldom used-grains, liquids, etc., being mostly bought and sold by weight.

JAPAN.

In March 1891, a law was passed, with effect from Jan. 1, 1893, permitting the use of the Metric System. The same Act re-organised the national weights and measures, and defined them in terms of the metric units, prototype standards of which had been received in 1889.

Length.—The standard unit of length is the *Shaku*, which is defined as $\frac{10}{33}$ of the length of the national iridio-platinum prototype metre, standard at 0°.15 Centigrade. The unit of square or land measure is the *Bu* or *Tsubo*, which is equal to a square, each side of which measures 6 shakus.

Weight.—The standard unit of weight is the *Kwan*, which is defined as equal to $\frac{15}{4}$ of the weight of the national iridio-platinum prototype kilogram. The density of a Japanese standard iridio-platinum Kwan weight of 3750 grammes was determined

* Board of Trade Report 9, Sess. 2, 1886, pp. 46 and 49. + Board of Trade Report, 392 of 1897, p. 6. as 21.5423 at 0° C. by the Board of Trade Standards Department in 1896-97.*

Capacity.—The standard unit of capacity is the *Shô*, which is defined as equal to 1.80391 litres.

The national standards are in the custody of the Minister of Agriculture and Commerce at Tokio.

BRITISH INDIA.

Various weights and measures are in use in India, the local standards being kept by the district and municipal authorities.

Length.—The British Imperial yard, foot, and inch are statutory by the Measures of Length Act of 1889. This Act does not refer to square measures. A brass standard yard was verified by the Board of Trade Standards Department for the Government of India in 1889. It is inscribed: "Accurate copy of Imperial Standard Yard, 1889, Calcutta. Standard Yard at 85 degrees Fahrenheit." At the same time two similar standards were also supplied to the Presidencies of Bombay and Madras.[†]

Weight.—The standard unit of weight is the *Tola*, which is equal to 180 grains, the weight of the rupee. Primary standard iridio-platinum weights of 30, 20, and 10 Tolas were verified by the Board of Trade Standards Department for the Calcutta and Bombay Mints in 1892.[‡]

Capacity.—Measures of capacity are seldom used by the natives —grain, liquids, etc., being usually bought and sold by weight. Measures are made to contain certain weights of some commodities. They are really 'measures of weight,' and are named by the weights which they represent.

THE STRAITS SETTLEMENTS.

The Straits Settlements Ordinance No. VII. of 1886 assimilates the weights and measures of the colony to the British Imperial System, with the exception of certain customary native weights, such as the Tahil, Kati, and Pikul, to which are assigned values in terms of British Imperial weights (see p. 30). The Board

> * Board of Trade Report, 392 of 1897, p. 6. + Board of Trade Report, 302 of 1889, p. 6. + Board of Trade Report, 364 of 1893, p. 13.

PART I.

STANDARD UNITS

SECT. I.]

of Trade Standards Department assisted in the drawing up of the Ordinance, and verified a large number of copies of the Imperial standards for the colony.* They have also supplied other standards, such as the Kati = $1\frac{1}{3}$ lbs. avoirdupois, and a quarter-Chupah (2 Imperial gills), which contains ten fluid ounces of distilled water at 62° Fahr.[†] The standards of the colony are deposited at Singapore.

SOUTH AFRICA.

In Natal, the British Imperial is the legal system of weights and measures.[‡] This is also the case in Cape Colony, British Bechuanaland, the Orange River Colony, the Transvaal, and Rhodesia, except that there is a special system of land measure. The unit of land measure is a foot "of such length that 1000 of such feet shall be equal to 1033 English feet as now by law defined and established for lineal measurement in England."§ This unit is termed the *Cape Foot*, and is a survival of the Rhynland foot used during the Dutch occupation of the Cape of Good Hope. Twelve Cape feet make a *Rood* and 600 square roods a *Morgen*. This system is used in all land surveys, and standard Roods are deposited with the Surveyor-General of each Colony.

EGYPT.

The use of the metric system is permitted by a decree issued by the Khedive Ismail in 1873. It has been adopted by the government for all purposes except the measurement of areas of land and the tonnage of ships, and is used by the public works, post office, customs and railway departments. A decree issued by the Khedive Mohamed Tewfik on the 28th April 1891, with effect from the 1st of January 1892, recognises the International Prototype Metre and Kilogram || as fundamental

* Board of Trade Reports, 262 of 1887, p. 3, and 330 of 1888, p. 1.

+ Board of Trade Report, 302 of 1889, pp. 2 and 7.

‡ See Natal Laws, No. 11 of 1852, No. 19 of 1872, and No. 39 of 1884.

§ Cape Colony Law, No. 9 of 1859.

 $\| \dot{i} \cdot \epsilon$, the international metric standards deposited at Breteuil Observatory, near Paris.

standards from which the Egyptian units of length, weight, and capacity are derived by means of equivalents stated in the decree (see page 17).

The old weights and measures are still in general use, the units being as follows :

Length.—There are several different units of length, namely: the *Diraâ baladi* or 'town' diraâ; the *Diraâ mimari*, which is used in building, etc.; the *Pike Istambuli* or Constantinople Pike, used in measuring cloth; and the *Kassabah*, used in land surveying. The *Feddan* of $333\frac{1}{3}$ square kassabahs is the legal unit of land area.

Weight.—The standard unit of weight is the *Dirhem* (drachm). Capacity.—The standard unit of capacity is the *Ardeb*.

SECTION II. COMPARISON OF STANDARD UNITS.

THE METRIC AND BRITISH IMPERIAL SYSTEMS COMPARED.

In 1894-95 a comparison of the Yard with the Metre was made under the directions of the Board of Trade and the International Committee of Weights and Measures. The Parliamentary Copy of the Standard Yard, P.C. VI.. was first carefully compared with the Imperial Standard Yard at the Standards Office, Westminster. It was then taken to the International Bureau of Weights and Measures at Breteuil and compared with the International Prototype Standard Metre,* and the following result was confirmed at a meeting of the Metric Conference in September 1895.† At 16°.667 Centigrade the Imperial Yard is equal to 0.9143992Metre, the temperature 16°.667 C. being taken as equal to 62° Fahrenheit; or, conversely, at 16°.667 C. (62° F.) the Metre is equal to 39.370113 inches.‡

In 1883 a comparison of the Pound and the Kilogram was made in the same manner. A copy of the pound was compared

* Board of Trade Report, 432 of 1895, pp. 3 and 23.

+ Board of Trade Report, 373 of 1896, p. 37.

‡ Détermination du Rapport du Yard au Métre, by Dr. Benoît (Director of the International Bureau of Weights and Measures), Paris, 1896.

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SECT. II.] COMPARISON OF STANDARD UNITS

with the Imperial Standard at the Standards Office, and then with the International Prototype Kilogram at the International Bureau, with the following result: the Imperial Avoirdupois Pound weighed *in vacuo* at o° Centigrade is equal to 453.5924277 Grammes; or, conversely, the Kilogram is equal to 15432.35639 Grains.*

In comparing the units of capacity of the two systems, the weight *in vacuo* of distilled water at 4° C. contained in a Litre is compared with the weight *in air* of distilled water at $16^{\circ}.667$ C. (62° F.) contained in a Gallon. The Imperial Gallon is equal to 4.5459631 Litres; or, conversely, the Litre is equal to 1.75980 Pints. The Board of Trade equivalents of Metric and Imperial Weights and Measures, legalised by an Order in Council of May 19, 1898, are based on the foregoing comparisons, which may be summarised as follows:

| 1 | Yard | = 0.9143992 Metre. |
|---|----------|------------------------|
| 1 | Metre | = 39.370113 Inches. |
| 1 | Pound | = 453.5924277 Grammes. |
| I | Kilogram | = 15432.35639 Grains. |
| I | Gallon | = 4.5459631 Litres. |
| I | Litre | = 1.75080 Pints. |

The French Toise and the Austrian Klafter were the units of length formerly used in most of the European geodetic surveys. They are, however, no longer in use, having been superseded by the Metre. Compared with the Imperial Yard,

> 1 Toise = 2.13151116 Yards. 1 Klafter = 2.07403483 Yards. 1 Metre = 1.09361426 Yards.†

THE UNITED STATES, THE METRIC, AND THE BRITISH IMPERIAL SYSTEMS.

Since 1893 the International Prototype Meter and Kilogram (deposited at Breteuil Observatory, near Paris) have been regarded in the United States as fundamental standards, from

* Travaux et Mémoires, Comité international des Poids et Mesures, Tome IV., 1885; also Board of Trade Annual Weights and Measures Report, 1884.

+ H. J. Chaney, Our Weights and Measures, London, 1897, p. 67.

which all units of weight and measure are derived in terms of the equivalents legalised by the Act of July 1866.* The U.S. yard is reproduced from the meter in terms of the equation: $1 \text{ yard} = \frac{3600}{3937}$ meter, while the British equivalent is: 1 yard = 0.9143992 metre. Therefore

1 U.S. Yard = 1.000002875 Imp. Yards,

a difference of only 2.875 in a million. U.S. and British measures of length can therefore be regarded as practically identical.

The British equivalent :

I Avoirdupois Pound = 453.5924277 Grammes

has been adopted by the U.S. Bureau of Standards. U.S. and British weights are therefore exactly alike.

The Bureau of Standards equivalents of the U.S. units of capacity are:

I U.S. Liquid Gallon of 231 cubic inches = 3.785434497 Liters.†

I U.S. Bushel of 2150.42 cubic inches = 0.3523928160 Hectoliter.

The British equivalents are: 1 Imp. Gallon = 4.5459631 Litres, and 1 Imp. Bushel = 0.363677048 Hectolitre. Therefore

| I | U.S. | Liquid | Gallon = 0.83270 | Imp. | Gallon. |
|---|------|--------|------------------|------|----------|
| I | Imp. | Gallon | = 1.20091 | U.S. | Gallons. |
| I | U.S. | Bushel | = 0.96897 | Imp. | Bushel. |
| I | Imp. | Bushel | = 1.03202 | U.S. | Bushels. |

COMPARISON OF THE RUSSIAN WITH THE METRIC AND THE BRITISH IMPERIAL SYSTEMS.

In 1897 Prof. D. Mendelieff, acting on the authority of the Russian Government, determined the values of the Russian standard units in terms of those of the Metric System by a series of experiments made at the International Bureau of Weights and Measures, which values were subsequently legalised by the Act of June 1899 (see page 10). The units of capacity are derived from the unit of weight by reference to the volume of distilled water at $16\frac{2}{3}^{\circ}$ C. The equivalents on which the conversion

* Bulletin No. 26, U.S. Coast and Geodetic Survey, 5th April, 1893.

⁺In the United States a liter is regarded as the volume of a cubic decimeter, which, according to the most recent determination (see p. 4), involves an error of only 26 parts in a million.

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PART I.

SECT. II.] COMPARISON OF STANDARD UNITS

tables given on page 42 are based, may be summarised as follows:

- 1 Archine = 28 British Inches or 0.711200 Metre.*
- I Funt = 409.51241 Grammes.
- 1 Vedro = 12.2993285 Litres.
- I Tchetverik = 26.2385674 ,,

COMPARISON OF THE EGYPTIAN WITH THE METRIC AND THE BRITISH IMPERIAL SYSTEMS.

A decree issued by the Khedive Mohamed Tewfik on the 28th April, 1891, with effect from the 1st of January, 1892, defines the Egyptian units of length, weight, and capacity in terms of the international metric standards (deposited at Breteuil Observatory, near Paris) as follows:

I Diraâ baladi = 0.580 Metre.
I Diraâ mimari = 0.750 Metre.
I Kassabah = 3.550 Metres.
I Dirhem = 3.12 Grammes.
I Ardeb = 1.98 Hectolitres.

The decree also embodies a table of the legal Metric and British Imperial equivalents of the Egyptian weights and measures (see page 52).

In 1902 and 1903 the Board of Trade Standards Department verified standard Rotl and Oke weights for the Sudan Customs, I rotl being taken as equal to 0.990492 lb. and I oke as equal to 2.751367 lbs., these being the Egyptian legal equivalents.[†]

*28 British inches=0.7111995 metre.

+ Board of Trade Reports, 334 of 1903, p. 7, and 348 of 1904, p. 6.

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SECTION III. TABLES.

THE METRIC SYSTEM.

Weight.

| | UNI | r . | | | Symbol. | VALUE IN GRAMMES. |
|--------------|-------|------------|--------|------|-----------|---------------------|
| Millionam | | | | | ma | 001.0 |
| Milligram, | - | - | - | - | mg. | .001 g. |
| Centigram, | - | - | - | | cg. | .oi g. |
| Decigram, | - | - | 1 | - | dg. | .1 g. |
| Gramme, | - | - | - | - | g. | I g. |
| Dekagram, | - | - | - | | dag. | IO g. |
| Hectogram, | | - | - | | hg. | 100 g. |
| Kilogram, | - | - | - | - | kg.* | 1,000 g. |
| Myriagram, | - | - | - | - | Spar Land | 10,000 g. |
| Quintal, - | - | - | - | - | q. | 100,000 g. |
| Tonne, Milli | er or | Met | ric To | on,- | t. | I,000,000 g. |

* The abbreviation 'kilo' is frequently used for kilogram.

| | UNI | т. | | | SYMBOL. | VALUE IN METRES. |
|-------------|-----|----|---|----|---------|------------------|
| Micron, - | - | - | | - | μ. | .000 001 m. |
| Millimetre, | - | - | - | - | mm. | .001 m. |
| Centimetre, | - | - | - | - | cm. | .OI m. |
| Decimetre, | - | - | - | - | dm. | .I m. |
| Metre, - | - | - | | - | m. | i m. |
| Dekametre, | - | - | - | | dam. | IO m. |
| Hectometre, | - | - | | | hm. | 100 m. |
| Kilometre, | - | - | - | 4. | km. | I,000 m. |
| Myriametre, | - | - | | - | Mm. | 10,000 m. |
| Megametre, | - | - | - | - | a | I,000,000 m. |

Lineal Measure.

Square Measure.

| Unit. | Symbol. | VALUE IN SQUARE METRES. |
|------------------------------|------------------------|----------------------------|
| Square millimetre, | mm. ² | .000 001 m. ² |
| Square centimetre, | cm. ² | .0 001 m. ² |
| Square decimetre, | dm. ² | .01 m. ² |
| Square metre or centiare, - | m. ² or ca. | I m. ² |
| Are (square dekametre), | adm. ² | 100 m. ² |
| Hectare (square hectometre), | ha.—hm.2 | 10,000 m. ² |
| Square kilometre, | km.2 | 1,000,000 m. ² |

Cubic Measure.

| Unit. | Symbol. | VALUE IN CUBIC METRES. |
|-----------------------|-----------------------|------------------------------|
| Cubic millimetre, | mm. ³ | .000 000 001 m. ³ |
| Cubic centimetre, | cm.3* | .000 001 m.3 |
| Cubic decimetre, | dm. ³ | .001 m. ³ |
| Cubic metre or stere, | m. ³ or s. | I m. ³ |

* The symbol c.c. is frequently used for the cubic centimetre.

| Unit | • | | SYMBOL. | VALUE IN LITRES. | VOLUME. |
|-------------|---|----|---------|------------------|----------------------|
| Millilitre, | | 2. | ml. | .001 l. | I cm. ³ |
| Centilitre, | | | cl. | .or l. | IO cm. ³ |
| Decilitre, | | - | dl. | .1 1. | 100 cm. ³ |
| Litre, - | | | 1. | I l. | I dm. ³ |
| Dekalitre, | | - | dal. | IO l. | IO dm.3 |
| Hectolitre, | | | hl. | 100 l. | 100 dm.3 |
| Kilolitre, | | - | kl. | 1000 l. | I m. ³ |

Measure of Capacity.

NOTE.—The weight *in vacuo* of a cubic decimetre of distilled water at 4°C. is .999974 kilogram (see page 4). Therefore for all practical purposes a litre may be regarded as the volume of a cubic decimetre, the error involved being only 26 parts in a million.

The above metric symbols are those adopted by the *Comité inter*national des Poids et Mesures.[†]

+ Proces-verbaux, Session 1905, p. 175.

WEIGHTS AND MEASURES

THE BRITISH IMPERIAL SYSTEM.

Avoirdupois or Commercial Weight.

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27.34375 grains = I drachm.
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16 drachms=1 ounce (oz.)=437.5 grains.

16 ounces=1 pound (lb.)=256 drachms=7000 grains.

28 pounds = I quarter (qr.) = 448 ounces.

4 quarters = I hundredweight (cwt.)= II2 pounds.

20 hundredweights=1 ton=80 quarters=2240 pounds.

I stone = 14 pounds : I cental = 100 pounds :

20 centals = I 'short' ton of 2000 pounds.

The ton of 2240 lbs. is usually termed the 'long' ton, in contradistinction to the 'short' ton of 2000 lbs. To convert long into short tons, multiply by 1.12; or from short into long, divide by 1.12.

| Ounces. | Pound. | Ounces. | POUND. | Ounces. | Pound. |
|----------------|--------|---------|--------|---------|--------|
| · 1 | .0156 | 5 | .3125 | 101/2 | .6562 |
| 1/2 | .0312 | 51/2 | ·3437 | II | .6875 |
| 12 34 | .0468 | 6 | ·375 | 1112 | .7187 |
| I | .0625 | 61/2 | .4062 | 12 | •75 |
| 112 | .0937 | 7 | •4375 | 121 | .7812 |
| 2 | .1250 | 71/2 | .4687 | 13 | .8125 |
| $2\frac{1}{2}$ | .1562 | 8 | .5 | I 3½ | .8437 |
| 3 | . 1875 | 81/2 | . 5312 | 14 | .875 |
| 31/2 | .2187 | 9 | . 5625 | 141 | .9062 |
| 4 | .25 | 91 | · 5937 | 15 | ·9375 |
| 41 | .2812 | 10 | .625 | 151 | .9687 |

Ounces (avoir.) in Decimals of a Pound (avoir.).

Troy Weight.

(Used for the weighing of precious metals.)

24 grains = I pennyweight (dwt.).

20 pennyweights = I ounce (oz. troy) = 480 grains.

12 ounces = I pound (lb. troy) = 240 pennyweights = 5760 grains. The grain is the same in both troy and avoirdupois weights.

The troy pound is seldom used.

The Diamond Carat and the Pearl Grain, although in general use, are not legal weights. They are thus defined by the Board of Trade: $151\frac{1}{2}$ diamond carats or 600 pearl grains = 1 troy ounce; therefore a diamond carat = 3.1683 grains (205.30 milligrams) and a pearl grain =0.8 grain (51.84 milligrams).*

* Board of Trade Reports, 330 of 1888, p. 13, and 302 of 1889, p.2.

SECT. III.]

BRITISH TABLES

Comparison of Avoirdupois and Troy weights.

| I lb. avoir | r. = 14.583 | oz. | troy, lo | ogarithm | n = 1.1638568. |
|-------------|-------------|-----|----------|----------|----------------|
| I OZ. ,, | =0.9114583 | oz. | " | " | =9.9597368. |
| I oz. troy | = 1.097143 | oz. | avoir., | " | =0.0402632. |

Grains and Dwts. in Decimals of a Troy Oz.

| I | Grain | =.0021 | Oz. | 1.1.7.4 | I | Dwt. | = | .05 | Oz. |
|----|--------|--------|-----|----------|----|-------|-----|-----|-----|
| 2 | Grains | =.0042 | ,, | C. Check | 2 | Dwts. | = | .1 | ,, |
| 3 | ,, | =.0063 | ,, | 10000 | 3 | ,, | = | .15 | ,, |
| 4 | " | =.0083 | ,, | 12 North | 4 | ,, | = | .2 | ,, |
| 5 | ,, | =.0104 | " | 10.2 | 5 | ,, | = | .25 | ,, |
| 6 | ,, | =.0125 | " | | 6 | ,, | = | .3 | ,, |
| 7 | ,, | =.0146 | " | | 7 | " | = | .35 | ,, |
| 8 | ,, | =.0167 | " | | 8 | ,, | = | •4 | " |
| -9 | ,, | =.0188 | " | | 9 | ,, | = | •45 | ,, |
| 10 | ,, | =.0208 | " | 1 | 10 | " | = | .5 | " |
| II | ,, | =.0229 | ,, | | II | ,, | = | .55 | " |
| 12 | ,, | =.025 | " | 1 | 12 | ,, | = | | " |
| 13 | ,, | =.0271 | " | | 13 | ,, | = | .65 | ,, |
| 14 | " | =.0292 | " | | 14 | ,, | = | .7 | ,, |
| 15 | ,, | =.0313 | " | 5 | 15 | " | = | .75 | ,, |
| 16 | ,, | =.0333 | " | 1. | 16 | " | | .8 | ,, |
| 17 | •: | =.0354 | " | | 17 | ,, | = | .85 | ,, |
| 18 | ,, | =.0375 | ,, | - | 18 | ,, | = | .9 | ,, |
| 19 | ,, | =.0396 | " | _ | 19 | ,, | = | .95 | ,, |
| 20 | ,, | =.0417 | ,, | | 20 | ,, | = 1 | .0 | ,, |
| 21 | ,, | =.0438 | " | - | | | | | |
| 22 | ,, | =.0458 | " | | | | | | |
| 23 | ,, | =.0479 | " | | | | | | |
| 24 | " | =.05 | " | | | | | | |

Grains in Decimals of a Dwt.

| I | Grain | n =.0417 | Dwt. | | | 13 | Grains | s= | .5417 | Dwt |
|----|-------|------------|------|-------------|---|----|--------|----|--------|-----|
| 2 | Grain | ns = .0833 | ,, | Le a La Sta | | 14 | ,, | = | . 5833 | ,, |
| 3 | ,, | =.125 | ,, | | | 15 | ,, | = | .625 | ,, |
| 4 | ,, | =.1667 | ,, | | | 16 | ,, | = | .6667 | ,, |
| 5 | ,, | =.2083 | ,, | 1.3 - 1 | | 17 | ,, | = | .7083 | " |
| 6 | ,, | =.25 | ,, | - | | 18 | ,, | = | .75 | ,, |
| 7 | ,, | =.2917 | ,, | 36.44 | | 19 | ,, | = | .7917 | ,, |
| 8 | ,, | =.3333 | ,, | | | 20 | ,, | = | .8333 | " |
| 9 | ,, | =.375 | ,, | | e | 21 | ,, | = | .875 | ,, |
| 10 | ,, | =.4167 | ,, | | | 22 | ,, | = | .9167 | " |
| II | ,, | =.4583 | " | 1 | | 23 | ,, | = | .9583 | ,, |
| 12 | ,, | =.5 | ,, | | | 24 | ,, | | 1.0 | " |

PART I.

Apothecaries' Weight.

20 grains = I scruple (\Im .) 3 scruples = I drachm (\Im .)=60 grains. 8 drachms=I ounce (\Im .)=480 grains. 12 ounces = I pound (lb.)=5760 grains.

Drugs are now often weighed by avoirdupois weight. The scruple and drachm are not introduced into the British Pharmacopœia, but are still used in prescriptions.

The ounce and pound are the same as in troy weight, while the grain is the same in avoirdupois, troy and apothecaries' weights.

Lineal Measure.

```
12 inches = I foot.

3 feet = I yard=36 inches.

5\frac{1}{2} yards = I rod, pole or perch=16\frac{1}{2} feet=198 inches.

40 rods = I furlong=220 yards=660 feet.

8 furlongs=I statute mile=1760 yards=5280 feet.
```

I link=7.92 inches=0.66 foot; Ioo links=I Gunter's chain=66 feet; 80 chains=I statute mile; 6 feet=I fathom; 3 statute miles=I league; 6075.6 feet=I geographical mile.

| Ins. | Foot. | Ins. | Foot. | Ins. | Foot. | Ins. | Foot. | Ins. | Foot. | Ins. | Foot. |
|------|-------|---------------|-------|------|-------|---------------|--------|------------|-------|---------------|-------|
| 0 | .0000 | 2 | .1667 | 4 | ·3333 | 6 | . 5000 | 8 | .6667 | ю | .8333 |
| 4 | .0208 | 1/4 | .1875 | 4 | .3542 | 1 | .5208 | 4 | .6875 | 4 | .8542 |
| 1/2 | .0417 | 1/2 | .2083 | 12 | .3750 | $\frac{1}{2}$ | .5417 | 12 | .7083 | $\frac{1}{2}$ | .8750 |
| 34 | .0625 | <u>3</u> 4 | .2292 | 34 | .3958 | 34 | . 5625 | 34 | .7292 | <u>3</u> 4 | .8958 |
| I | .0833 | 3 | .2500 | 5 | .4167 | 7 | .5833 | 9 | .7500 | II | .9167 |
| 4 | .1042 | 1 | .2708 | 1 | •4375 | 1 | .6042 | 1 | .7708 | 1 | .9375 |
| 12 | .1250 | 12 | .2917 | 12 | .4583 | 12 | .6250 | 12 | .7917 | 12 | .9583 |
| 34 | .1458 | <u>3</u> 4 | .3125 | 34 | .4792 | <u>3</u> 4 | .6458 | 3 <u>4</u> | .8125 | 34 | .9792 |

Inches expressed in Decimals of a Foot.

SECT. III.

Fractions of an Inch expressed in Decimals of an Inch.

| $\frac{1}{64} = .015625$ | $\frac{17}{64} = .265625$ | $\frac{33}{64} = .515625$ | $\frac{49}{64} = .765625$ |
|---------------------------|---------------------------|---|----------------------------|
| $\frac{1}{32} = .03125$ | $\frac{9}{32} = .28125$ | $\frac{17}{32} = .53125$ | $\frac{25}{32} = .78125$ |
| $\frac{3}{64} = .046875$ | $\frac{19}{64} = .296875$ | $\frac{35}{64} = .546875$ | $\frac{51}{64} = .796875$ |
| $\frac{1}{16} = .0625$ | $\frac{5}{16} = .3125$ | $\frac{9}{16} = .5625$ | $\frac{13}{16} = .8125$ |
| $\frac{5}{64} = .078125$ | $\frac{21}{64} = .328125$ | $\frac{37}{64} = .578125$ | $\frac{53}{64} = .828125$ |
| $\frac{3}{32} = .09375$ | $\frac{11}{32} = .34375$ | $\frac{19}{32} = .59375$ | $\frac{27}{32} = .84375$ |
| $\frac{7}{64} = .109375$ | $\frac{23}{64} = .359375$ | ₹ ⁹ / ₄ = .609375 | $\frac{55}{64} = .859375$ |
| $\frac{1}{8} = .125$ | $\frac{3}{8} = .375$ | $\frac{5}{8} = .625$ | $\frac{7}{8} = .875$ |
| $\frac{9}{64} = .140625$ | $\frac{25}{64} = .390625$ | $\frac{41}{64} = .640625$ | $\frac{5.7}{64} = .890625$ |
| $\frac{5}{32} = .15625$ | $\frac{13}{32} = .40625$ | $\frac{21}{32} = .65625$ | $\frac{29}{32} = .90625$ |
| $\frac{11}{64} = .171875$ | $\frac{27}{64} = .421875$ | $\frac{43}{64} = .671875$ | $\frac{59}{64} = .921875$ |
| $r_{16}^{3} = .1875$ | $\frac{7}{16} = .4375$ | 11 = .6875 | $\frac{15}{16} = .9375$ |
| $\frac{13}{64} = .203125$ | $\frac{29}{64} = .453125$ | $\frac{45}{64} = .703125$ | $\frac{61}{64} = .953125$ |
| $\frac{7}{32} = .21875$ | $\frac{15}{32} = .46875$ | $\frac{23}{32} = .71875$ | $\frac{31}{32} = .96875$ |
| $\frac{15}{64} = .234375$ | $\frac{31}{64} = .484375$ | $\frac{47}{4} = .734375$ | $\frac{63}{64} = .984375$ |
| $\frac{1}{4} = .25$ | $\frac{1}{2} = .5$ | $\frac{3}{4} = .75$ | I = I |

Square Measure.

144 square inches = I square foot.
9 square feet = I square yard=1296 square inches.
30¼ square yards = I square rod=272¼ square feet.
40 square rods = I rood=1210 square yards=10890 square feet.
4 roods = I acre=160 sq. rods=4840 sq. yards=43560 sq. feet=10 sq. chains.
640 acres = I square mile=27,878,400 square feet.

In a square I acre in extent, each side measures 208.710 feet. 147.581 15 " ,, 22 ,, ٠, >> 1 ,, 104.355 " • • " ., " 22

Cubic Measure.

1728 cubic inches=1 cubic foot.
27 cubic feet =1 cubic yard=46656 cubic inches.

Imperial Measures of Capacity, both Liquid and Dry.*

4 gills = I pint (pt.)= 34.6775 cubic inches. 2 pints = I quart (qt.)= 69.355 " 4 quarts = I gallon (gal.) = 277.420 " " 2 gallons = 1 peck (pk.)= 554.840 99 4 pecks = I bushel (bush.) = 2219.360 22 ., 8 bushels = 1 quarter (qr.) = 10.2748i cubic feet. $_{36}$ bushels = 1 chaldron (chal.) = $_{46.236}$ 22 "

* See page 8 for the determinations from which the volumes are derived.

23

WEIGHTS AND MEASURES

Apothecaries' Measure,

| I fluid drachm (fl. dr.) | =60 minims (min. |)= 0.216734 | cubic inch. |
|--------------------------|---------------------|------------------|-----------------------|
| I fluid ounce (fl. oz.) | = 8 fluid drachms | = 1.733875 | ,, inches. |
| 1 pint (O.) | =20 fluid ounces | = 34.6775 | >> >> |
| I gallon (C.) | = 8 pints | =277.420 | ? ? ? ? |
| | | | |
| 1 minim (m.) is the vo | lume of 0.9114583 g | rain of distille | d water at 62°F. |

| 1 mmm (1. C.) 10 mm . | | | 58 | | | |
|-------------------------|----|---------|--------|----|----|----|
| 1 fluid drachm (f.3.) | "" | 54.6875 | grains | " | " | " |
| I fluid ounce (f.3.) | " | 437.5 | " | " | ,, | >> |
| 1 pint (O.) | ,, | 8,750 | " | ., | " | •? |
| I gallon (C.) | >> | 70,000 | " | " | " | " |

THE UNITED STATES OF AMERICA.

Avoirdupois or Commercial Weight.

```
27.34375 grains = 1 dram.
```

16 drams = 1 ounce (oz.) = 437.5 grains.

16 ounces = I pound (lb.) = 7000 grains.

14 pounds = 1 stone.

2 stones=I quarter (qr.)=28 pounds.

4 quarters = I hundredweight (cwt.)=112 pounds.

20 hundredweights=1 'long' ton=80 quarters=2240 pounds.

Also: 100 pounds = 1 quintal; 20 quintals = 1 'short' ton of 2000 pounds.

Troy Weight.

24 grains=1 pennyweight (dwt.). 20 pennyweights=1 ounce (oz. troy)=480 grains. 12 ounces=1 pound (lb. troy)=240 dwts.=5760 grains.

Apothecaries' Weight.

20 grains = I scruple (9).
3 scruples=I dram (3)=60 grains.
8 drams = I ounce (3)=24 scruples=480 grains.
12 ounces = I pound=288 scruples=5760 grains.

In avoirdupois, troy, and apothecaries' weights the grain is of the same weight, and in troy and apothecaries' weights the ounce and pound are the same.

A

Lineal Measure.

12 inches = I foot (ft.).

3 feet = i yard (yd.) = 36 inches.

 $5\frac{1}{2}$ yards = 1 rod, pole or perch = $16\frac{1}{2}$ feet.

40 rods = I furlong = 220 yards = 660 feet.

8 furlongs = 1 statute mile = 1760 yards = 5280 feet.

3 miles = 1 league.

Also: 7.92 inches=1 link; 100 links=1 Gunter's chain=66 feet; 80 chains=1 mile.

3 inches=I palm; 4 inches=I hand; 9 inches=I span.

6 feet = 1 fathom; I cable's length = 120 fathoms.

Square Measure.

| 144 square inche | s = I | square foot. |
|------------------------------|-------|--|
| 9 square feet | =I | square yard = 1296 square inches. |
| $30\frac{1}{4}$ square yards | 5 = I | square rod $= 272\frac{1}{4}$ square feet. |
| 40 square rods | = I | rood = 1210 square yards. |
| 4 roods | = I | acre = 43560 square feet = 10 square chains. |
| 640 acres | = I | square mile or section. |
| 36 square miles | = I | township. |

Cubic Measure.

| 1728 | cubic | inches | =I | cubic foot. |
|-----------------|-------|--------|-----|----------------------------|
| 27 | cubic | feet | = I | cubic yard. |
| 16 | cubic | feet | = I | cord. |
| $24\frac{3}{4}$ | cubic | feet | = I | perch of stone or masonry. |
| 128 | cubic | feet | - I | cord of wood. |

Liquid Measure.

| 4 | gills | = I | pint (pt.) | = 28.875 cubi | c inches. |
|-----------------|-----------|-----|-------------------|------------------|--------------|
| 2 | pints | = I | quart (qt.) | = 57.75 | " |
| | quarts | = I | gallon (gal.) | =231.0 | >> |
| $3I\frac{1}{2}$ | gallons | = I | barrel. | | |
| 2 | barrels | = I | hogshead | =63 gallons. | |
| 2 | hogsheads | = I | pipe or butt | = 126 gallons. | |
| 2 | pipes | = I | tun | =252 gallons. | |
| Also: 42 | gallons | = I | tierce; 2 tierces | s = t puncheon = | =84 gallons. |

Apothecaries' Fluid Measure.

| 60 minims $(\mathbf{m}) = \mathbf{I}$ fluid drachm (f.3) |)= | 0.2256 | cubic | inch. |
|--|----|--------|-------|---------|
| 8 fluid drachms = I fluid ounce $(f.\overline{3})$ | = | 1.8047 | ,, | inches. |
| 16 fluid ounces $= I \text{ pint } (O.)$ | = | 28.875 | " | " |
| 8 pints = I gallon | =2 | 231.0 | " | " |

Dry Measure.

| | 2 | pints | =I | quart = | 67.2006 | cubic | inches. | |
|----|----|---------|-------|------------|-----------|-------|---------|--|
| | 4 | quarts | =I | gallon = | .268.8025 | | " | |
| | 2 | gallons | =I | peck = | 537.605 | | " | |
| | 4 | pecks | =I | bushel =: | 2150.42 | | " | |
| | 8 | bushels | I = I | quarter. | | | | |
| 21 | 12 | bushels | I = I | barrel (di | ry). | | | |
| 3 | 6 | bushels | I = i | chaldron | | | | |

Note that the dry measures are larger than the liquid measures of the same names.

RUSSIA.

Commercial Weight.

96 dolis = I zolotnik. 96 zolotniks=I funt. 40 funts = I pood.

Other weights sometimes used are: the loth = 3 zolotniks; the lana = 8 zolotniks; the berkovetz = 10 poods; and the packen = 3 berkovetz. Gold ore values are expressed in zolotniks per 100 poods (see pages 103 and 104).

Apothecaries' Weight.

60 medical grains = I medical drachme. 8 ,, drachmes = I ,, once. 12 ,, onces = I ,, funt = 84 zolotniks.

Drugs are now mostly weighed by metric weights.

Lineal Measure.

10 totchkas = 1 liniia.
17.5 liniias = 1 vershok.
16 vershoks = 1 archine.
3 archines = 1 sagene=48 vershoks.
500 sagenes = 1 verst.

The British Imperial foot and inch and the metre are also in use. The archine is used in mining and trade, the sagene in land measurement, and the foot and inch in engineering works.

2

RUSSIAN TABLES

SECT. III.]

Square Measure.

256 square vershoks=1 square archine.
9 square archines =1 square sagene=2304 square vershoks.
2400 square sagenes =1 dessiatina.
104.16 dessiatinas =1 square verst=250,000 square sagenes.

Cubic Measure.

4096 cubic vershoks = 1 cubic archine.
27 cubic archines = 1 cubic sagene = 110,592 cubic vershoks.

Liquid Measure.

Io tcharkas=I schtoff. Io schtoffs = I vedro. I6 boutylkas (bottles of wine)=I vedro. 20 boutylkas (bottles) = I vedro.

Dry Measure.

8 garnetz = I tchetverik. 4 tchetveriks=I osmina. 2 osminas = I tchetvert. 12 tchetverts = I last.

1 cubic sagene = $\begin{cases} 789.67123 \text{ vedros.} \\ 46.2698 \text{ tchetverts.} \end{cases}$

CHINA.

Commercial Weight.

16 liang (taels or tahils) = 1 chin (kan or kati) = I_3^1 lbs. avoir. 100 chin = tan (tam or pikul) = $I_33_3^1$...

Silver Weight.

| IO SSŬ | = I | hao (thousandths). |
|-----------|-----|--|
| 10 hao | = I | li (hundredths-'cash'). |
| 10 li | = I | fên (tenths-' candareen '). |
| 10 fên | = I | ch'ien (' mace '). |
| 10 ch'ien | 1=1 | liang (tael or tahil) = $I^{\frac{1}{2}}$ oz. avoir. |

PART I.

Lineal Measure.

Io fan = I ts'un = I.4I British inches. Io ts'un = I ch'ih (covid) = I4.1 ", Io ch'ih = I chang (rod) = I4I ",

The foregoing values are those of the British Treaty of 1858. They are used in the payment of duties at the Foreign Maritime Customs. At Hong Kong, where both British Imperial and Chinese weights and measures are in use, the present standard *chek* or *chih* was verified by the Board of Trade. It measures $14\frac{5}{8}$ inches, and is therefore 0.525 inch longer than the *chih* of the British Treaty. The standard *ying-tsao chih* of the Chinese Board of Works is approximately 12.5 inches. The Hong Kong weights are identical with those of the British Treaty.

Itinerary Measure.

5 ch'ih (covids)=I pu (pace). 360 pu =I li (about $\frac{1}{3}$ mile). 250 li =I tu (degree).

Land Measure.

5 ch'ih (covids)=1 kung (bow). 240 square kung =1 mou (rood).

Cubic Measure.

100 cubic ch'ih = I fang or ma.

Measures of Capacity.

Io ho = I shêng=approx. 2 Imp. pints.
Io shêng=I tou.
5 tou = I hu.

JAPAN.

Weight.

| IO | shi = I | mô. |
|------|-------------------|--------|
| IO | mô = I | rin. |
| IO | rin = I | fun. |
| IO | fun = I | mommē. |
| 160 | $momm\bar{e} = I$ | kin. |
| 0001 | $momm\bar{e} = I$ | kwan. |

Lineal Measure.

| 10 | shi | = I | mô. |
|----|--------------|-----|--------|
| 10 | mô | =1 | rin. |
| 10 | rin | =I | bu. |
| IO | bu | =I | sun. |
| | | | |
| 10 | sun | =1 | shaku. |
| | sun shaku | | |
| 9 | shaku | = I | |

For cloth measurement the kujira shaku is used. It is equal to I shaku 2 sun 5 bu.

Square Measure.

Io shaku=I gô. Io gô =I bu or tsubo. 30 tsubo =I sē. Io sē =I tan = 300 tsubo. Io tan =I chô=3000 tsubo.

A bu or tsubo equals 36 square shaku (I square ken) of lineal measure.

Measures of Capacity.

Io shaku=I gô. Io gô = I shô. Io shô = I to. Io to = I koku=100 shô.

In the above tables the same name is sometimes applied to units having no connection with each other. For instance, the *shaku* as a lineal measure is quite different from the *shaku* of square measure, which again has no connection with the *shaku* of capacity.

BRITISH INDIA.

The following weights are based on the *tola*, which is the weight of a rupee (180 grains). They are officially recognised, and are used on the railways, etc., but numerous local weights of varying value obtain throughout India. The Burmese *viss* of 100 *tikals*=3.65 lbs. avoir. exactly.*

* See Board of Trade Report, 326 of 1901, p. 5.

WEIGHTS AND MEASURES

PART I.

Weight.

180 grains = I tola.
80 tolas = I seer.
40 seers = I maund.
20 maunds= I kandy.

Lineal Measure.

The Imperial yard, foot and inch are statutory by Act 2 of India, 1889. Various native measures, which are mostly based on the guz or yard, are also used.

Square Measure.

The *biga* is the common unit of land measure. It varies in size in almost every village

| The Bengal | biga=approximately | 1600 sq. yards. |
|-------------------|--------------------|-----------------|
| The N.W. Province | ,, = " | 3025 " |
| The Bombay | " = " | 3927 " |

In Madras, the unit is the kani = approximately 6400 sq. yards.

THE STRAITS SETTLEMENTS.

Ordinance No. VII. of 1886 assimilates the weights and measures used in the Straits Settlements to the British Imperial weights and measures, with the exception of the following weights :

| IO | hoons | =I | chee. | | | | |
|-----|--------|-----|--------------|------|--------------------------------|------|--------|
| IO | chee | =I | tahil (tael) | = | $I\frac{1}{3}$ | oz. | avoir. |
| 16 | tahils | =I | kati (kan) | = | 113 | lbs. | " |
| 100 | katis | = I | pikul (tam) | = 1 | 333 | lbs. | " |
| 40 | pikuls | = I | koyan | = 53 | 33 ¹ / ₃ | lbs. | " |

Measures of Capacity.

| I pau or quarter | chupah = 2 | Imp. | gills. |
|------------------|------------|------|---------|
| I half chupah | . = I | " | pint. |
| I chupah | = I | " | quart. |
| 1 gantang | = I | " | gallon. |

SOUTH AFRICA.

The British Imperial system of weights and measures is used throughout British South Africa, but in the Cape Colony, British Bechuanaland, the Orange River Colony, the Transvaal and Rhodesia, a special system of land measure known as the *Cape System* is used :

Lineal Measure.

12 Cape inches = I Cape foot. 12 Cape feet = I rood. 425.94385 roods = I statute mile (1760 yards). NOTE.—I Cape foot = I.033 British feet.

Square Measure.

144 square Cape inches = I square Cape foot.
144 square Cape feet = I square rood.
600 square roods = I morgen.

EGYPT.

Commercial Weight.

| 12 | dirhems (drachms) | = I | okieh. |
|-----|-------------------|-----|------------------------------|
| 12 | okiehs | =I | rotl or rottolo=144 dirhems. |
| 400 | dirhems | = I | oke. |
| 36 | okes) | | kantar. |
| 100 | rotls | =1 | Kantai. |
| 60 | okes | = I | hamlah. |
| 112 | " | = I | Alexandria kantar. |
| 200 | ,, | = I | heml. |
| | | | |

Jewellers' Weight.

4 kamhas = 1 kirat. 16 kirats = 1 dirhem. 24 , = 1 mithkal.

Lineal Measure.

24 kirats = I diraâ baladi.

There are several diraâs (cubits or pikes) of different lengths in use, namely, the diraâ baladi or 'town' diraâ; the diraâ mimari, used in building, etc.; and the pike istambuli or Constantinople pike, used in measuring cloth.

The kassabah is the unit used in land surveying.

Square or Land Measure.

| 24 | sohts | = I | sahm. | |
|------|---------------|---------|--------|----------|
| 4 | sahms | = I | danek. | |
| 2 | daneks | = 1 | habbah | |
| 3 | habbahs | = I | kamel | kirat. |
| 24 | kamel kirats | 1 == | feddan | (masri). |
| 3333 | square kassab | ahs = 1 | feddan | (masri). |

Measures of Capacity.

| 2 | kirats | = | I | karrūbah. |
|----|-------------|-----|---|-------------|
| 2 | karrūbahs | = | I | tūmnah. |
| 2 | tūmnahs | = | I | rūbaah. |
| 2 | rūbaahs | = | I | nesf kadah. |
| 2 | nesf kadahs | = | I | kadah. |
| 2 | kadahs | == | I | malwa. |
| 2 | malwas | = | I | rūb. |
| 2 | rūbs | = | I | kilah. |
| 2 | kilahs | = | I | webah. |
| 6 | webahs | = | I | ardeb. |
| 8 | ardebs | | I | daribah. |
| | | | | |
| 7 | rūbs | | T | small fard. |
| / | 1405 | | | sman laiu. |
| 14 | " | === | I | large " |
| | | | | |

SECTION IV. CONVERSION TABLES.

In this section the scientific equivalents of the Metric and British Imperial weights and measures, together with the corresponding logarithms, are first given. These are followed by the Board of Trade legal equivalents of the Metric weights and measures, in which, as they are for use in trade, the same degree of accuracy is not required. The scientific equivalents of the United States and Metric weights and measures as published by the U.S. Bureau of Standards at Washington, and the shorter equivalents legalised in the United States by the Act of July 28, 1866, are also given. Then follow in the order named the Metric and British equivalents, together with the corresponding logarithms, of the Russian, Chinese, Japanese, British, Indian, Straits Settlements, Cape (S. Africa), and Egyptian weights and measures.

SCIENTIFIC EQUIVALENTS OF METRIC AND BRITISH IMPERIAL WEIGHTS AND MEASURES.

METRIC TO BRITISH IMPERIAL.

Weight.

| Metric. Avoi | rdupois. Logarithm. |
|---|--|
| 1 milligram (mg.)=.01543 grain | 8.1884322 |
| 1 centigram (cg.) =.15432 " | 9.1884322 |
| I decigram (dg.) = 1.54324 ,, | 0.1884322 |
| $I \text{ gramme (g.)} = \begin{cases} .0022046223 \\ I5.43235639 \end{cases}$ | 34 pound 7.3433342 |
| | |
| 1 dekagram(dag.)=.35274 ounce | 9.5474542 |
| 1 hectogram (hg.)=3.52740 ound | es 0.5474542 |
| $I kilogram (kg.) = \begin{cases} 2.20462234 \\ 15432.35639 \end{cases}$ | pounds 0.3433342 |
| 1 knogrum (kg.) - (15432.35639 | grains 4.1884322 |
| 1 myriagram = 22.04622 pou | inds 1.3433342 |
| 1 quintal (q.) = 1.96841 hunch | |
| I tonne (t.) $= \begin{cases} 0.98420640 \\ 0.000000 \\ 0.000000 \\ 0.000000 \\ 0.000000 \\ 0.000000 \\ 0.00000 \\ 0.00000 \\ 0.00000 \\ 0.000000 \\ 0.00000 $ | tons of 2240 lbs.9.9930862tons of 2000 lbs.0.0423042 |
| 1 toline (t.) - {1.10231117 | tons of 2000 lbs. 0.0423042 |
| | |
| T | roy. |

| 1 gramme (g.) | $= \begin{cases} 0.03215074248 \text{ ounce} \\ 0.64301485 \text{ pennyweight} \end{cases}$ | 8.5071910 9.8082210 |
|---------------|---|------------------------|
| | Abothecaries. | |

| | (0.25721 drachm | 9.4102809 |
|---------------|---|-----------|
| I gramme (g.) | $= \begin{cases} 0.25721 \text{ drachm} \\ 0.77162 \text{ scruple} \end{cases}$ | 9.8874022 |
| | (15.43235639 grains | 1.1884322 |

Lineal Measure.

| 1 micron $(\mu.)$ | =.00003937 inch | 5.5951667 |
|--------------------|--|-----------|
| 1 millimetre (mm.) | =.039370113 " | 8.5951667 |
| I centimetre (cm.) | =.39370113 " | 9.5951667 |
| I decimetre (dm.) | = 3.9370113 inches | 0.5951667 |
| | (39.370113 inches | 1.5951667 |
| I metre (m.) | = { 3.2808427654 feet | 0.5159855 |
| | $= \begin{cases} 3.2808427654 \text{ feet} \\ 1.09361425513 \text{ yards} \end{cases}$ | 0.0388642 |
| I dekametre (dam.) | =10.93614255 yards | 1.0388642 |
| I hectometre (hm.) | = 109.3614255 ,, | 2.0388642 |
| 1 kilometre (km.) | =0.62137173 mile | 9.7933515 |
| I myriametre (Mm. | | 0.7933515 |
| Н.М. | С | |

WEIGHTS AND MEASURES [PART I.

| I square millimetre (mm.2) $=.001550$ square inch 7.190333 I square centimetre (cm.2) $=.1550006$ $,,$ 9.190333 | 3 |
|---|---|
| | - |
| | 3 |
| I square decimetre (dm. ²) = $I5.50006$ square inches $I.190333$ | 5 |
| 1550.005812 sq. inches 3.190333 | 3 |
| I square metre (m. ²) = { 10.76392925 square feet 1.031970 | 8 |
| • [1.195992139 sq. yards 0.077728 | 3 |
| 1 are (sq. decametre) (adm. ²)=119.5992139 square yards 2.077728 | 3 |
| i hectare (ha.) =2.4710581385 acres 0.392883 | 0 |
| 1 square kilometre (km. ²) = $.386102834$ square mile 9.586703 | 0 |
| I square myriametre $(Mm.^2) = 38.6102834$, miles 1.586703 | 0 |

Cubic Measure.

| 1 cubic millimetre (mm. ³) | =.000061 cubic inch | 5.7855000 |
|---|---------------------------|-----------|
| I cubic centimetre (cm. ³) | =.0610239 " | 8.7855000 |
| I cubic decimetre (dm. ³) | =61.0239 cubic inches | 1.7855000 |
| | (61023.90426 cubic ins. | 4.7855000 |
| I cubic metre or stere (m. ³ or s. | = 35.314759411 cubic feet | 1.5479563 |
| | (1.30795405226 cub. yds. | 0.1165925 |

Measures of Capacity.

| I millilitre (ml.) = 16.89411 minims | 1.2277353 |
|---|-----------|
| 1 centilitre (cl.) =.07039 gill | 8.8475241 |
| I decilitre (dl.) $=.17598$ pint | 9.2454641 |
| I litre (l.) $= \begin{cases} 1.75980 \text{ pints} \\ .219975389 \text{ gallon} \end{cases}$ | 0.2454641 |
| 1 Inte (1.) = 1.219975389 gallon | 9.3423741 |
| 1 dekalitre (dal.)=2.19975389 gallons | 0.3423741 |
| 1 hectolitre (hl.) $= 2.74969236$ bushels | 0.4392841 |
| I kilolitre (kl.) = 3.43711545 quarters | 0.5361941 |

BRITISH IMPERIAL TO METRIC.

Weight.

| Avoirdupois. | Metric. | Logarithm. |
|--------------------------|--|------------|
| 1 grain | =64.79891824 milligrams | 1.8115678 |
| I drachm | = 1.77185 grammes | 0.5897191 |
| I ounce | = 28.34953 " | 1.4525458 |
| I pound | = {453.5924277 grammes .4535924277 kilogram | 2.6566658 |
| 1 pound | -1.4535924277 kilogram | 9.6566658 |
| I stone | =6.35029 kilograms | 0.8027938 |
| I quarter | = 12.70059 ,, | 1.1038238 |
| I cental (100 lbs.) | =45.35924277 " | 1.6566658 |
| 1 hundredweight | = 50.802352 ,, | 1.7058838 |
| I 'short' ton of 2000 lb | | 9.9576958 |
| I 'long' ton of 2240 lbs | 5. = 1.01604704 tonnes | 0.0069138 |
| | | |

SECT. IV.] CÓNVERSION TABLES

| | Troy. | Metric. | Logarithm. |
|---|------------|-------------------------|------------|
| I | grain | =64.79891824 milligrams | 1.8115678 |
| I | pennyweigh | t = 1.555174 grammes | 0.1917790 |
| I | ounce | =31.1034807566 grammes | 1.4928090 |
| | Apothecari | es. Metric. | Logarithm. |
| | I grain | =64.79891824 milligrams | 1.8115678 |
| | I scruple | = 1.29598 grammes | 0.1125978 |
| | I drachm | n = 3.88794 grammes | 0.5897191 |
| | I ounce | = 31.1034807566 grammes | 1.4928090 |

Lineal Measure.

| I inch | =25.39997 millimetres | 1.4048333 |
|-------------|---------------------------|-----------|
| I foot | =.30479973 metre | 9.4840145 |
| I yard | =.9143992 metre | 9.9611358 |
| I pole | = 5.0291956 metres | 0.7014985 |
| 1 chain | =20.116782 " | 1.3035585 |
| I furlong | =201.16782 ,, | 2.3035585 |
| I statute m | ile=1.60934259 kilometres | 0.2066485 |

Square Measure.

| I | square inch | =6.45158871 square centimetres | 0.8096667 |
|---|--------------|----------------------------------|-----------|
| I | square foot | =.092902877 square metre | 8.9680292 |
| I | square yard | =.8361259 ,, | 9.9222717 |
| I | square perch | 1=25.2928084 square metres | 1.4029970 |
| I | rood | = IOI I.712335 " | 3.0050570 |
| I | acre | =.404684934 hectare | 9.6071170 |
| I | square mile | = 2.5899835784 square kilometres | 0.4132970 |

Cubic Measure.

| 1 cubic inch = 16.387021 | cubic centimetres | 1.2145000 |
|---------------------------|-------------------|-----------|
| I cubic foot =.02831677 | cubic metre | 8.4520437 |
| I cubic yard = .76455285 | " | 9.8834075 |

Measures of Capacity.

| Imp | erial. Metric. | Logarithm. |
|------|-----------------------------|------------|
| I gi | l = 1.42061 decilitres | 0.1524759 |
| I pi | =.56825 litre | 9.7545359 |
| I qu | art $= 1.13649$ litres | 0.0555659 |
| I ga | llon =4.5459631 litres | 0.6576259 |
| I ре | ck = 9.091926 ,, | 0.9586559 |
| I bu | shel $= 3.63677$ dekalitres | 0.5607159 |
| Iqu | arter=2.9094164 hectolitres | 0.4638059 |

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WEIGHTS AND MEASURES

PART I.

| Apothecaries. | Metric. | Logarithm. |
|----------------|-----------------------|------------|
| I minim | =.059192 millilitre | 8.7722647 |
| I fluid drachn | n=3.55153 millilitres | 0.5504159 |
| I fluid ounce | =2.84123 centilitres | 0.4535059 |
| 1 pint | =.56825 litre. | 9.7545359 |
| 1 gallon | =4.5459631 litres | 0.6576259 |

THE BOARD OF TRADE LEGAL EQUIVALENTS OF THE METRIC AND IMPERIAL WEIGHTS AND MEASURES FOR USE IN TRADE.*

METRIC TO BRITISH IMPERIAL.

Linear Measure.

1 millimetre (mm.) $(\frac{1}{1000} \text{ m.}) = 0.03937$ inch. I centimetre $\left(\frac{1}{100} \text{ m.}\right)$ =0.3937 " I decimetre $(\frac{1}{10} \text{ m.})$ = 3.937 inches. 39.370113 inches. = 3.280843 feet. I metre (m.) 1.0036143 yards. = 10.936 yards I dekametre (10 m.) I hectometre (100 m.) = 109.36 I kilometre (1000 m.) =0.62137 mile.

Square Measure.

| I square centimetre | =0.15500 square inch. |
|---|--|
| I square decimetre (100 square centimetr | |
| 1 square metre (100 square decimetres) | $= \begin{cases} 10.7639 \text{ square feet.} \\ 1.1960 \text{ square yards.} \end{cases}$ |
| I are (100 square metres) | = 119.60 ,, |
| I hectare (100 ares or 10,000 square metr | (es) = 2.4711 acres. |

Cubic Measure.

| I cubic centimetre | = 0.0610 cubic inch. |
|--|--|
| I cubic decimetre (1000 cubic centimetre | es)=61.024 cubic inches. |
| I cubic metre (1000 cubic decimetres) | $= \begin{cases} 35.3148 \text{ cubic feet.} \\ 1.307954 \text{ cubic yards.} \end{cases}$ |

Measures of Capacity.

- I centilitre $\left(\frac{1}{100} \text{ litre}\right) = 0.070 \text{ gill.}$
- I decilitre $(\frac{1}{10}$ litre) = 0.176 pint.
- 1 litre = 1.75980 pints.
 - 1 dekalitre (10 litres) = 2.200 gallons.
 - I hectolitre (100 litres)=2.75 bushels.

* These equivalents were legalised by Order in Council of May 19, 1898 (For the Scientific Equivalents see page 33.)

CONVERSION TABLES

Weight.

| | Metric. Avoirdupois. |
|---|--|
| I | milligram $(\frac{1}{1000} \text{ grm.}) = 0.015 \text{ grain.}$ |
| I | centigram $(\frac{1}{100} \text{ grm.}) = 0.154$ " |
| I | decigram $(\frac{1}{10} \text{ grm.}) = 1.543 \text{ grains.}$ |
| I | gramme (I grm.) $=$ 15.432 " |
| I | dekagram (10 grm.) $=$ 5.644 drams. |
| I | hectogram (100 grm.)=3.527 ounces. |
| I | kilogram (1000 grm.) = $\begin{cases} 2.2046223 \text{ pounds or} \\ 15432.3564 \text{ grains.} \end{cases}$ |
| I | myriagram (10 kilog.)=22.046 pounds. |
| I | quintal (100 kilog.) = 1.968 hundredweights. |
| I | tonne (1000 kilog.) $= 0.9842$ ton. |

Metric.

1 gramme (1 grm.)

 $Troy. = \begin{cases} 0.03215 \text{ ounce.} \\ 15.432 \text{ grains.} \end{cases}$

Metric.

I gramme (I grm.)

 $= \begin{cases} 0.2572 \text{ drachm.} \\ 0.7716 \text{ scruple.} \\ 15.432 \text{ grains.} \end{cases}$

BRITISH IMPERIAL TO METRIC.

Linear Measure.

| I | inch | =25.400 millimetres. |
|---|----------------------------|----------------------|
| I | foot (12 in.) | =0.30480 metre. |
| I | yard (3 ft.) | =0.914399 metre. |
| I | fathom (6 ft.) | = 1.8288 metres. |
| I | pole $(5\frac{1}{2}$ yds.) | = 5.0292 " |
| I | chain (22 yds.) | =20.1168 " |
| I | furlong (220 yds.) |)=201.168 " |
| I | mile (8 furlongs) | = 1.6093 kilometres. |

Square Measure.

| I | square inch | =6.4516 square centimetres. |
|---|----------------------------------|-----------------------------|
| I | square foot (144 sq. ins.) |)=9.2903 square decimetres. |
| I | square yard (9 sq. ft.) | = 0.836126 square metre. |
| I | perch $(30\frac{1}{4}$ sq. yds.) | =25.293 square metres. |
| I | rood (40 perches) | = 10.117 ares. |
| I | acre (4840 sq. yds.) | =0.40468 hectare. |
| I | square mile (640 acres) | =259.00 hectares. |

PART I.

Cubic Measure.

I cubic inch = 16.387 cubic centimetres. I cubic foot (1728 cub. ins.)=0.028317 cubic metre. I cubic yard (27 cub. ft.) = 0.764553"

Measures of Capacity.

| res. |
|---------|
| |
| |
| itres. |
| |
| litres. |
| litres. |
| |

Apothecaries.

I minim =0.059 millilitre. I fluid scruple = 1.184 millilitres. 1 fluid drachm (60 minims) = 3.552 , I fluid ounce (8 drachms) =2.84123 centilitres. I pint =0.568 litre. I gallon (8 pints or 160 fluid oz.)=4.5459631 litres.

Metric.

Weight.

| | Avoirdupois. | Metric. |
|---|--------------------------------|---|
| I | grain | =0.0648 gramme. |
| I | dram | = 1.772 grammes. |
| I | ounce (16 drams) | =28.350 " |
| I | pound (16 oz. or 7000 grains) | =0.45359243 kilogram. |
| 1 | stone (14 lbs.) | =6.350 kilograms. |
| I | quarter (28 lbs.) | =12.70 " |
| I | hundredweight (cwt.) (112 lb.) | $=\begin{cases} 50.80 & ,, \\ 0.5080 & \text{quintal.} \end{cases}$ |
| | ton (20 cwt.) | $= \begin{cases} 1.0160 \text{ tonnes or} \\ 1016 \text{ kilograms.} \end{cases}$ |
| | Troy. | Metric. |
| | - | 10 |

I grain

=0.0648 gramme. I pennyweight (24 grains) = 1.5552 grammes.

I troy ounce (20 pennyweights)=31.1035 "

Apothecaries. Metric. I grain =0.0648 gramme. 1 scruple (20 grains) = 1.296 grammes. I drachm (3 scruples) = 3.8881 ounce (8 drachms) = 31.1035 ,,

SECT. IV:

COMPARISON OF UNITED STATES AND BRITISH IMPERIAL WEIGHTS AND MEASURES.

Lineal Measure.

United States and British Imperial Measures of length are practically the same, as I U.S. unit=1.000002875 Imp. units of the same denomination, a difference of 2.875 in a million.

Square Measure.

I U.S. unit = 1.00000575 Imp. units, a difference of 5.75 in a million.

Cubic Measure.

I U.S. unit=1.000008625 Imp. units, a difference of 8.625 in a million.

Measures of Capacity.

Liquid.

| 1 U.S. liquid galle | on=0.83270 Imp. gallon. | $\log = 9.9204898$ |
|---------------------|-------------------------------|--------------------|
| I Imp. gallon | = 1.20091 U.S. liquid gallons | $\log = 0.0795102$ |

Dry.I U.S. bushel = 0.96897 Imp. bushel. $\log = 9.9863111$ I Imp. bushel = 1.03202 U.S. bushels. $\log = 0.0136889$

Weights.

No difference.

EQUIVALENTS OF UNITED STATES AND METRIC WEIGHTS AND MEASURES AS PUBLISHED BY THE U.S. BUREAU OF STANDARDS, WASHINGTON.*

Measures of Length.

Basis: I meter=39.37 inches.

| I U.S. inch = 25.4000508 millimeter. | log = 1.4048346 |
|---|---|
| I U.S. foot = 0.3048006096 meter. | log=9.4840158 |
| I U.S. yard =0.9144018288 meter. | log=9.9611371 |
| I U.S. mile = 1.609347219 kilometers. | log=0.2066497 |
| 1 millimeter = 0.03937 U.S inch. 1 meter = 3.28083 U.S. feet. 1 kilometer = 0.6213699495 U.S. mile. | log = 8.5951654 log = 0.5159842 log = 9.7933503 |

* Tables of Equivalents, Washington, Nov. 1906. The U.S. legal equivalents are given on page 40.

WEIGHTS AND MEASURES

Measures of Area.

| I U.S. acre | e=0.4046872610 hectare. | log=9.6071196 |
|-------------|--------------------------|--------------------|
| 1 hectare | =2.471043930 U.S. acres. | $\log = 0.3928804$ |

Measures of Volume.

| I | U.S. cubic yard | l=0.7645594453 cubic meter. | $\log = 9.8834113$ |
|---|-----------------|---------------------------------|--------------------|
| I | cubic meter | = 1.307942772 U.S. cubic yards. | $\log = 0.1165887$ |

Measures of Capacity.

Liquid.

Basis: I U.S. liquid gallon=23I cubic inches, and I cubic decimeter=I liter.I U.S. liquid gallon=3.785434497 liters.log=0.5781157I liter=0.2641704673 U.S. liquid gall.log=9.4218843

Dry.

Basis: I U.S. bushel=2150.42 cubic inches, and I cubic decimeter=I liter.

| I U.S. bushe | l=0.3523928160 hectoliter. | $\log = 9.5470270$ |
|--------------|----------------------------|--------------------|
| I hectoliter | =2.837742299 U.S. bushels. | $\log = 0.4529730$ |

Weights.

Basis: 1 avoirdupois pound=453.5924277 grams.

The equivalents are therefore the same as those given for British Imperial Weights on pages 33 and 34.

THE EQUIVALENTS OF THE METRIC WEIGHTS AND MEASURES LEGALISED IN THE UNITED STATES BY THE ACT OF JULY 28th, 1866.*

| Metric denominations and values. | Equivalents in denominations in use. |
|---|---|
| Myriameter - 10,000 meters. Kilometer - 1,000 meters. Hectometer - 100 meters. Dekameter - 100 meters. Meter 10 meters. Meter 1 meter. Decimeter - $\frac{1}{10}$ of a meter. Centimeter - $\frac{1}{1000}$ of a meter. Millimeter - $\frac{1}{1000}$ of a meter. | 6.2137 miles. 0.62137 miles or 3280 feet and 10 inches. 328 feet and 1 inch. 393.7 inches. 39.37 inches. 3.937 inches. 0.3937 inch. 0.0394 inch. |

Measures of Length.

*(The scientific equivalents published by the Bureau of Standards, Washington, are given on page 39.)

SECT. IV.]

2

Measures of Surface.

| Metric denominations and values. | | | Equivalents in denominations in use. |
|----------------------------------|--|--|---|
| Are | | 10,000 square meters. - 100 square meters. - 1 square meter. | 2.471 acres. 119.6 square yards. 1,550 square inches. |

Measures of Capacity.

| Metric denominations and values. | | | Equivalents in denominations in use. | |
|----------------------------------|----------------------|-------------------------------------|--------------------------------------|----------------------------|
| Names. | Number of liters. | Cubic Measure. | Dry Measure. | Liquid or Wine Measure. |
| Kiloliter | | | | |
| or stere | 1,000 | I cubic metre | 1.308 cubic yards | 264.17 gallons. |
| Hectoliter | 100 | $\frac{1}{10}$ of a cubic meter | 2 bushels and 3.35 | 26.417 gallons. |
| | | | pecks | |
| Dekaliter | IO | 10 cubic decimeters | 9.08 quarts | 2.6417 gallons. |
| Liter | I | I cubic decimeter | 0.908 quart | 1.0567 quarts. |
| Deciliter | 10 | $\frac{1}{10}$ of a cubic decimeter | 6. 1022 cub. inches | 0.845 gill. |
| Centiliter | 1100 | 10 cubic centimeters | 0.6102 cubic inch | 0. 338 fluid ounce. |
| Milliliter | 1 1000 | I cubic centimeter | 0.061 cubic inch | 0.27 fluid dram. |

Weights.

| Metric o | Equivalents in denominations in use. | | |
|-------------------------|--------------------------------------|--|---------------------|
| Names. Number of grams. | | Weight of what quantity of water at maximum density. | Avoirdupois Weight. |
| Millier or tonneau | 1,000,000 | I cubic meter | 2204.6 pounds. |
| Quintal | 100,000 | I hectoliter | 220.46 pounds. |
| Myriagram | 10,000 | IO liters | 22.046 pounds. |
| Kilogram or kilo - | 1,000 | I liter | 2.2046 pounds. |
| Hectogram | 100 | I deciliter | 3.5274 ounces. |
| Dekagram - · - | IO | 10 cubic centimeters | 0.3527 ounce. |
| Gram · · · · | I | I cubic centimeter | 15.432 grains. |
| Decigram | 110 | 1 of a cub. centimeter | 1.5432 grains. |
| Centigram | 1 100 | 10 cubic millimeters | 0.1543 grain. |
| Milligram | 1000 | I cubic millimeter | 0.0154 grain. |

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42 WEIGHTS AND MEASURES [PART I.

EQUIVALENTS OF THE RUSSIAN WEIGHTS AND MEASURES.

| | Commercial Weight. | | | | | |
|---|--------------------|--------------------------|-----------|---|-----|---|
| | Russian. | | | Metric. | | British. |
| I | doli | =4 | 4.43494 | milligrams | =. | 6857358 grain. |
| I | zolotnik | = 4 | 1.2657542 | 27 grammes | =(| 55.83064 grains. |
| | | | .409512 | 41 kilogram 41 grammes 41 milligram |) | .902820208 lbs. avoir. |
| 1 | funt | = - | 409.512 | 41 grammes | }=- | 13.1661280 oz. troy. 6319.741457 grains. |
| | | | 409512. | 41 milligram | s) | 6319.741457 grains. |
| | | | | | | .01612178943 tons of 2240 lbs. .01805640416 tons of 2000 lbs. 36.112808327 lbs. avoir. 526.6451214 oz. troy. |
| т | nood | _] | .016380 | 4964 tonne | 1- | .01805640416 tons of 2000 lbs. |
| 1 | pood | _ 16.3804964 kilograms ∫ | 55 | 36.112808327 lbs. avoir. | | |
| | | | | | | 526.6451214 oz. troy. |

Apothecaries' Weight.

| | Russian. | Metric. | British. |
|---|----------------|-------------------|-----------------------|
| I | medical grain | =62.20892 milligr | ams=.96003017 grain. |
| I | medical drachm | e=3.732535 gramm | = 57.60181 grains. |
| I | medical once | =29.860280 " | =.96003017 oz. apoth. |
| I | medical funt | = 358.323359 " | =11.5203620 " |

| Metric. | Russian. | Logarithm. | | |
|--|--|--|--|--|
| | milligram=.0225048 doli | | | |
| | | 8.3522754 9.3700042 | | |
| I gramme = | .23442513 zolotnik 16.074866 medical grains | 1.2061474 | | |
| | (10.0/4000 methear grains | 8.7856729 | | |
| | 2 44102844 funts | 0.3877330 | | |
| 1 kilogram =- | 0.061048211 pood 2.44192844 funts 234.42513 zolotniks 22504.8125 dolis | 2.3700042 | | |
| | 22504 8125 dolis | 4.3522754 | | |
| I metric | 22304.0125 0013 | | | |
| quintal}=: | 244.192844 funts | 2.3877330 | | |
| I tonne =0 | 61.04821097 poods | 1.7856729 | | |
| | | | | |
| D 7 | D 1 | 77 | | |
| British. | Russian. | Logarithm. | | |
| <i>British.</i> I grain | <i>Russian.</i> = 1.4582875 dolis | <i>Logarithm.</i> 0.1638432 | | |
| | = 1.4582875 dolis =7.2914375 zolotniks | ., | | |
| 1 grain | = 1.4582875 dolis = 7.2914375 zolotniks (.027691006 pood | 0.1638432 | | |
| 1 grain | = 1.4582875 dolis = 7.2914375 zolotniks (.027691006 pood | 0.1638432 0.8628132 | | |
| f grain 1 ounce troy | = 1.4582875 dolis =7.2914375 zolotniks (.027691006 pood | 0.1638432 0.8628132 8.4423387 | | |
| f grain 1 ounce troy 1 pound avoir. | = 1.4582875 dolis = 7.2914375 zolotniks $= \begin{cases} .027691006 \text{ pood} \\ 1.10764025 \text{ funts} \\ 106.333464 \text{ zolotniks} \end{cases}$ | 0.1638432 0.8628132 8.4423387 0.0443987 | | |
| f grain 1 ounce troy 1 pound avoir. 1 hundredweig | = 1.4582875 dolis = 7.2914375 zolotniks (.027691006 pood | 0.1638432 0.8628132 8.4423387 0.0443987 2.0266700 | | |
| f grain 1 ounce troy 1 pound avoir. 1 hundredweig 1 'short' ton (2000 lbs | = 1.4582875 dolis = 7.2914375 zolotniks $= \begin{cases} .027691006 \text{ pood} \\ 1.10764025 \text{ funts} \\ 106.333464 \text{ zolotniks} \end{cases}$ ght = 124.055708 funts | 0.1638432 0.8628132 8.4423387 0.0443987 2.0266700 2.0936168 | | |

Lineal Measure.

| | Russian. | Metric. | British. |
|---|----------|--------------------|-------------------|
| I | totchka | =254 microns | =.01 inch. |
| I | liniia | =2540 microns | =.1 inch. |
| I | vershok | =44.45 millimetres | = 1.75 inches. |
| I | archine | =.71120 metre | =2 feet 4 inches. |
| | | =2,13360 metres | =7 feet. |
| I | verst | =1.06680 kilometre | s=.66287 mile. |

| Metric. | | Logarithm. |
|-------------|---|------------|
| 1 metre | $= \begin{cases} 1.40607424 \text{ archines} \\ 22.49718785 \text{ vershoks} \end{cases}$ | 1.1480082 |
| 1 metre | 22.49718785 vershoks | 1.3521282 |
| I kilometre | =.9373828 verst | 9.9719170 |
| British. | Russian. | Logarithm. |

| I inch = IO liniias. | |
|--|-----------|
| 1 foot = 6.857142 or 6^6_7 vershoks | 0.8361432 |
| I yard = $\begin{cases} .00857142 \text{ or } \frac{6}{7000} \text{ verst} \\ 1.285714 \text{ or } 1\frac{2}{7} \text{ archines} \end{cases}$ | 7.9330532 |
| (1.285714 or 17 archines | 0.1091444 |
| $1 \text{ chain} = 9.42857 \text{ i} \text{ or } 9\frac{3}{7} \text{ sagenes}$ | 0.9744459 |
| I mile = 1.50857142 versts | 0.1785659 |

Square Measure.

| | Russian. | Metric. | British. |
|---|--------------|------------------------------|-------------------------|
| I | square sagen | e = 4.55224896 square metres | =49 square feet. |
| I | dessiatina | = 1.09253975 hectares | =2.6997245 acres. |
| I | square verst | = I.I 3806224 square kilomet | res=.43940829 sq. mile. |

| | Metric. | Russian. | Logarithm. |
|------------|----------------------------|---|--------------------------------|
| I | square metr | e=1.97704477 square archines | 0.2960165 |
| I | hectare | =.9152985 dessiatina | 9.961 5628 |
| I : | sq. kilometr | e = .87868656 square verst | 9.9438340 |
| | | | |
| | 73 1.1 7 | | |
| | British. | Russian. | Logarithm. |
| | | <i>Russian.</i> =47.0204 square vershoks | <i>Logarithm.</i> 1.6722864 |
| I : | square foot | | 0 |
| I : I : | square foot square yard | =47.0204 square vershoks | 1.6722864 |

1 square mile=2.2757878 square versts 0.3571318

Cubic Measure.

| Russian. | Metric. | British. |
|------------------------|------------------------|----------------------------|
| I cubic vershok = 87. | .8244 cubic centimetre | s = 5.359375 cubic inches. |
| I cubic archine $=.35$ | 97288 cubic metre | =12.703 cubic feet. |
| I cubic sagene = 9.7 | 126784 cubic metres | = 12.703 cubic yards. |

WEIGHTS AND MEASURES

[PART I.

| | Metric. | Russian. | Logarithm. |
|---|--------------------|--------------------------|------------|
| I | cubic centimetre | =.0113864 cubic vershok | 8.0563848 |
| I | cubic decimetre | =.00277987 cubic archine | 7.4440248 |
| I | cubic metre (stere |)=.10295821 cubic sagene | 9.0126610 |
| | | | 1 1 K |

| British. | Russian. | Logarithm. |
|--------------------|-----------------------|------------|
| I cubic inch $=$ | 1000 cubic liniias. | |
| I cubic foot $=$. | 0787172 cubic archine | 8.8960696 |
| I cubic yard =. | 0787172 cubic sagene | 8.8960696 |

Liquid Measure.

| | Russian. | Metric. | British. |
|---|---------------------|-----------------------|----------------------|
| 1 | tcharka | =.1229933 litre | =.216444 pint. |
| I | schtoff | = 1.22993285 litre | s = 2.16444 pints. |
| I | vedro | =12.2993285 litre | s = 2.70555 gallons. |
| I | boutylka (bottle of | wine)=.76870803 litre | = 1.352775 pints. |
| I | boutylka (bottle) | =.6149664 " | = 1.08222 ,, |

Dry Measure.

| Russian. | Metric. | British. |
|---------------|------------------------|--|
| 1 garnetz | = 3.27982093 litres | =.721480 gallon. |
| I tchetverik | =26.2385674 litres | =.721480 bushel. |
| 1 tchetvert | =2.09908539 hectolitre | s = 5.77184 bushels. |
| 1 last | =25.18902473 " | =8.65776 quarters. |
| 1 cubic sagen | e=97.1242585 " | $= \begin{cases} 267.061832 \text{ bushels.} \\ 2136.49465 \text{ gallons.} \end{cases}$ |

| Metric. | Russian. | Logarithm. |
|--|---|------------|
| I litre $= \begin{cases} 0 \\ 0 \\ 0 \\ 0 \end{cases}$ | .8130525 schtoff .300884 boutylkas of wine | 9.9101186 |
| | .300884 boutylkas of wine | 0.1142386 |
| (3 | .81118368 tchetveriks | 0.5810599 |
| I hectolitre $=\begin{cases} 3\\ 8 \end{cases}$ | .81118368 tchetveriks .130525184 vedros | 0.9101186 |
| | 8.110846 tchetveriks | 1.5810486 |
| (stere) \int_{-18}^{-18} | 1.303138 vedros | 1.9101073 |
| | | |
| British. | Russian. | Logarithm. |
| I gallon = | ∫0.3696107 vedro 1.386040 garnetz | 9.5677445 |
| A Senton - | 1.386040 garnetz | 0.1417757 |
| I bushel = | 1.386040 tchetveriks 11.08832 garnetz | 0.1417757 |
| I busher = | 111.08832 garnetz | 1.0448657 |
| | (1.0791790 tchetveriks | 0.0330935 |
| I cubic foot = | 2.3022485 vedros | 0.3621522 |
| | {1.0791790 tchetveriks 2.3022485 vedros 8.6334318 garnetz | 0.9361835 |

Table for the conversion of Russian Vershoks into British Feet.

| Vershoks. | Feet. | Vershoks. | Feet. | Vershoks. | Feet. | Vershoks. | Feet. |
|-----------|---------|-----------|---------|-----------|---------|-----------|---------|
| I | 0.14583 | 5 | 0.72916 | 9 | 1.3125 | 13 | 1.89583 |
| 2 | 0.2916 | 6 | 0.875 | 10 | 1.4583 | 14 | 2.0416 |
| 3 | 0.4375 | 7 / | 1.02083 | II | 1.60416 | 15 | 2.1875 |
| 4 | 0.583 | 8 | 1.1Ġ | 12 | 1.75 | 16 | 2.3 |

Table for the conversion of Russian Archines into British Feet.

| | | | | | 1 m 1 m 1 m 1 m 1 m 1 m 1 m 1 m 1 m 1 m | | |
|-----------|-------|-----------|-------|-----------|---|-----------|--------|
| Archines. | Feet. | Archines. | Feet. | Archines. | Feet. | Archines. | Feet. |
| I | 2.3 | 31 | 72.3 | 61 | 142.3 | 91 | 212.3 |
| 2 | . 4.6 | 32 | 74.6 | 62 | 144.6 | 92 | 214.6 |
| 3 | 7.0 | 33 | 77.0 | 63 | 147.0 | 93 | 217.0 |
| 4 | 9.3 | 34 | 79.3 | 64 | 149.3 | 94 | 219.3 |
| 5 | 11.6 | 35 | 81.6 | 65 | 151.6 | 95 | 221.6 |
| 6 | 14.0 | 36 | 84.0 | 66 | 154.0 | .96 | 224.0 |
| 7 | 16.3 | 37 | 86.3 | 67 | 156.3 | 97 | 226.3 |
| 8 | 18.6 | 38 | 88.6 | 68 | 158.6 | 98 | 228.6 |
| 9 | 21.0 | 39 | 91.0 | 69 | 161.0 | 99 | 231.0 |
| 10 | 23.3 | 40 | 93.3 | 70 | 163.3 | 100 | 233.3 |
| II | 25.6 | 41 | 95.6 | 71 | 165.6 | 200 | 466.6 |
| 12 | 28.0 | 42 | 98.0 | 72 | 168.0 | 300 | 700.0 |
| 13 | 30.3 | 43 | 100.3 | 73 | 170.3 | 400 | 933.3 |
| 14 | 32.6 | 44 | 102.6 | 74 | 172.6 | 500 | 1166.6 |
| 15 | 35.0 | 45 | 105.0 | 75 | 175.0 | 600 | 1400.0 |
| 16 | 37.3 | 46 | 107.3 | 76 | 177.3 | 700 | 1633.3 |
| 17 | 39.6 | 47 | 109.6 | 77 | 179.6 | 800 | 1866.6 |
| 18 | 42.0 | 48 | 112.0 | 78 | 182.0 | 900 | 2100.0 |
| 19 | 44.3 | 49 | 114.3 | 79 | 184.3 | 1000 | 2333.3 |
| 20 | 46.6 | 50 | 116.6 | 80 | 186.6 | 1100 | 2566.6 |
| 21 | 49.0 | 51 | 119.0 | 81 | 189.0 | 1200 | 2800.0 |
| 22 | 51.3 | 52 | 121.3 | 82 | 191.3 | 1300 | 3033.3 |
| 23 | 53.6 | 53 | 123.6 | 83 | 193.6 | 1400 | 3266.6 |
| 24 | 56.0 | 54 | 126.0 | 84 | 196.0 | 1 500 | 3500.0 |
| 25 | 58.3 | 55 | 128.3 | 85 | 198.3 | 1600 | 3733.3 |
| 26 | 60.6 | 56 | 130.6 | 86 | 200.6 | 1700 | 3966.6 |
| 27 | 63.0 | 57 | 133.0 | 87 | 203.0 | 1800 | 4200.0 |
| 28 | 65.3 | 58 | 135.3 | 88 | 205.3 | 1900 | 4433.3 |
| 29 | 67.6 | 59 | 137.6 | 89 | 207.6 | 2000 | 4666.6 |
| 30 | 70.0 | 60 | 140.0 | 90 | 210.0 | | |
| | | | | | | | |

PART I.

| Poods. | Avoirdupois | 'Short' Tons of | 'Long' Tons of | Tonnes of |
|--------|---------------|-----------------|----------------|-----------------|
| | Pounds. | 2000 lbs. | 2240 lbs. | 1000 kilograms. |
| I | 36.112808327 | 0.018056404 | 0.016121789 | 0.0163804964 |
| 2 | 72.225616654 | 0.036112808 | 0.032243579 | 0.0327609928 |
| 3 | 108.338424980 | 0.054169212 | 0.048365368 | 0.0491414892 |
| 4 | 144.451233307 | 0.072225617 | 0.064487158 | 0.0655219856 |
| 5 | 180.564041634 | 0.090282021 | 0.080608947 | 0.0819024820 |
| 6 | 216.676849961 | 0.108338425 | 0.096730737 | 0.0982829784 |
| 7 | 252.789658287 | 0.126394829 | 0.112852526 | 0.1146634748 |
| 8 | 288.902466614 | 0.144451233 | 0.128974315 | 0.1310439712 |
| 9 | 325.015274941 | 0.162507637 | 0.145096105 | 0.1474244676 |

Table for converting Russian Poods into avoirdupois pounds, 'short tons of 2000 lbs., 'long' tons of 2240 lbs., or tonnes of 1000 kilograms.

A table for converting Russian weight into troy ounces is given on page 102.

EQUIVALENTS OF THE CHINESE WEIGHTS AND MEASURES.

Commercial Weight.

| | Chinese. | Metric. | British | h. |
|---|----------------------|------------------------|----------------------------------|-------------|
| I | liang (tael or tahil | = 37.799368975 grammes | $= 1.3 \text{ or } 1\frac{1}{3}$ | oz. avoir. |
| I | chin (kan or kati) | =.6047899036 kilogram | $= 1.3 \text{ or } 1\frac{1}{3}$ | lbs. avoir. |
| I | tan (tam or pikul) | =60.47899036 kilograms | =133.3 | ,, |

Silver Weight.

| Chinese. | | Metric. | British. | |
|----------|----------------|------------------------|----------------|--|
| I | ssŭ | =.37799369 milligram | =.00583 grain. | |
| I | hao | = 3.7799369 milligrams | s=.0583 " | |
| I | li (cash) | = 37.799369 ,, | =.583 " | |
| I | fên (candareen |)=377.99369 ,, | = 5.83 grains. | |
| I | ch'ien (mace) | = 3.7799369 grammes | = 58.3 ,, | |
| I | liang (tael) | = 37.799368975 ,, | = 583.3 ,, | |
| | Metric | Chinese | Logarithm | |

| | Metric. | Chinese. | Logarithm. |
|---|-----------|-------------------|------------|
| I | milligram | =2.6455468 ssŭ | 0.4225155 |
| I | gramme | =.026455468 liang | 8.4225155 |
| I | kilogram | =1.653466757 chin | 0.2183955 |
| I | tonne | =16.53466757 tan | 1.2183955 |

| British. | Chinese. | Logarithm. |
|-----------------------|---|------------|
| 1 grain | =1.714285 or 15 li | 0.2340832 |
| 1 pound avoir. | $=.75 \text{ or } \frac{3}{4} \text{ chin}$ | 9.8750613 |
| I short ton (2000 lbs | $(s.) = 15 \tan \theta$ | 1.1760913 |
| I long ton (2240 lbs | $= 16.8 \tan(100)$ | 1.2253093 |

Note.—Similar weights to the above, but bearing different names, are used in the Straits Settlements (see page 50).

Lineal Measure (a).

Basis: I ch'ih=14.I inches. (As adopted in the British Treaty of 1858, and used in the assessment of duties at the Foreign Maritime Customs.)

| | Chinese. | Metric. | British. |
|---|--------------|------------------------|------------------|
|] | fan | = 3.581 39686 millimet | res = .141 inch. |
|] | ts'un | = 35.8139686 " | = 1.41 inches. |
| 1 | ch'ih (covid | l)=.358139686 metre | = 1.175 feet. |
| 1 | chang (rod) | = 3.58139686 metres | =11.75 " |
| | Metric. | Chinese. | Logarithm. |
| I | millimetre = | .27922066 fan | 9.4459475 |
| I | metre = | 2.792206609 ch'ih | 0.4459475 |
| | British. | -Chinese. | Logarithm. |
| | I inch = | .709219858 ts'un | 9.8507809 |
| | I foot = | .85106383 ch'ih | 9.9299621 |
| | I yard = | .25531915 chang | 9.4070834 |

Lineal Measure (b).

Basis: I chek or ch'ih= $14\frac{5}{8}$ inches. (This is the Hong Kong standard chek or ch'ih, as verified by the Board of Trade.)

| Chinese. | Metric. | British. |
|-----------------|--------------------------|------------------|
| I fan | = 3.71474675 millimetres | s=.14625 inch. |
| I ts'un | = 37.1474675 " | = 1.4625 inches. |
| I chek or ch'il | n=.371474675 metre | =1.21875 feet. |
| Metric. | Chinese. | Logarithm. |
| I millimetre = | .269197355 fan | 9.4300708 |
| I metre = | 2.69197355 chek or ch'ih | 0.4300708 |
| British. | Chinese. | Logarithm. |
| | .683760 ts'un | 9.8349041 |
| | .820512 chek or ch'ih | 9.9140853 |
| I yard = | = 2.461538 ,, | 0.3912066 |

EQUIVALENTS OF THE JAPANESE WEIGHTS AND MEASURES.

Weight.

| J | apanese. | | | Metric. | B | ritish. |
|--------|--------------|-----|-------------|--------------------|--------------------|-----------------------------------|
| I | mô | = | 3.75 | milligrams | s=.0578 | 7 grain. |
| I | rin | =. | .0375 | gramme | =.5787 | grain. |
| I | fun | = | .375 | gramme | = 5.787 | |
| I | mommē | ;== | 3.75 | grammes | = 57.87 | 13365 grains. |
| I | kin | = | 600 | grammes | =1.322 | 7734 lbs. avoir. |
| I | kwan | = | 3.75 | kilograms | = 8.267 | 33378 lbs. avoir. |
| I I | mommē kin | | 3.75 600 | grammes grammes | = 57.87 = 1.322 | 13365 grains. 7734 lbs. avoir. |

| Metric. Japanese. | Logarithm. |
|--|------------|
| 1 milligram=.26 mô | 9.4259687 |
| 1 gramme =.26 mommē | 9.4259687 |
| $I \text{ kilogram} = \begin{cases} 1.6 \text{ or } I_3^2 \text{ kin} \\ .26 \text{ kwan} \end{cases}$ | 0.2218487 |
| 1 knogram – 1.26 kwan | 9.4259687 |
| British. Japanese. | Logarithm. |
| 1 grain = 17.27971153 mô | 1.2375365 |
| 1 lb. avoir. = $\begin{cases} .75598738 \text{ kin} \\ .12095798 \text{ kwan} \end{cases}$ | 9.8785145 |
| 1 1b. avon. – (.12095798 kwan | 9.0826345 |

Lineal Measure.

| Japane | se. | Metric. | British. |
|--------------|---------------------------------|------------------|-----------------------------|
| ı mâ | $=\frac{1}{33}$ or | .o3 millimetre | =.001193 inch. |
| ı rin | $=\frac{10}{33}$ or | .30 millimetre | =.01193 inch. |
| ı bu | $=\frac{10}{33}$ or | .oż centimetre | =.11930337 inch. |
| I SUI | $n = \frac{1}{33}$ or | .oż metre | = 1.1930337 inches. |
| | $aku = \frac{10}{33}$ or | | =.9941948 foot. |
| ı ker | $n = \frac{20}{11} \text{ or }$ | 1.81 metres | = 1.98839 yards. |
| I che | $\hat{0} = \frac{1200}{11}$ | or 109.09 metres | =119.30337 yards. |
| | | | s = 2.440296 statute miles. |
| I kujira sha | aku=25 or | .378 metre | = 1.24274 feet. |
| (cloth meas | sure) | | |

| Metric. Japanese. | Logarithm. |
|----------------------------|------------|
| 1 millimetre=33 mô | 1.5185139 |
| I metre $= 3.3$ shaku | 0.5185139 |
| I kilometre =.2546296 ri | 9.4059090 |
| British. Japanese. | Logarithm. |
| 1 inch =.838199 sun | 9.9233473 |
| I foot = 1.005839 shaku | 0.0025285 |
| 1 yard=3.017517 shaku | 0.4796498 |
| 1 mile = .4097863 ri | 9.6125575 |

PART I.

SECT. IV.]

CONVERSION TABLES

Square Measure.

| Japanese. | Metric. | British. |
|--------------|----------------------------------|----------------------------|
| 1 shaku | =.03306 square metre | =.3558 square foot. |
| I gô | =.3305785 square metre | = 3.558324 square feet. |
| I bu or tsub | o =3.3057851 square metre | s = 3.953693 square yards. |
| ı sē | =.99173554 are | = 39.53693 square yards. |
| I tan | =.099173554 hectare | =.245064 acre. |
| 1 chô | =.991735537 hectare | = 2.45064 acres. |

| | Logarithm. |
|----------------------------|------------|
| 1 square metre=.3025 tsubo | 9.4807254 |
| I are $= 30.25$ tsubo | 1.4807254 |
| I hectare $= 1.008$ ġ chô | 0.0036041 |

| British. | Japanese. | Logarithm. |
|---------------|------------------|------------|
| I square foot | =.281031 gô | 9.4487545 |
| I square yard | d=.2529277 tsubo | 9.4029971 |
| I acre | =.40805667 chô | 9.6107205 |

Measures of Capacity.

| Japanes | se. Metric. | British. |
|---------|----------------------|------------------------|
| I shaku | u=.01804 litre | =.12698 gill. |
| ı gô | =.18039 litre | =.3174515 pint. |
| I shô | = 1.8039068 litres | = 3.174515 pints. |
| I to | =18.039068 litres | = 3.968144 gallons. |
| I koku | = 1.8039068 hectolit | res = 4.96018 bushels. |

| Metric. | Japanese. | Logarithm. |
|--------------|-----------------|------------|
| I centilitre | =.5543524 shaku | 9.7437859 |
| 1 litre | =.5543524 shô | 9.7437859 |
| I hectolitre | =.5543524 koku | 9.7437859 |
| | | |

| Logarithm. |
|------------|
| 0.4983218 |
| 0.4014118 |
| 9.3045018 |
| |

EQUIVALENTS OF THE INDIAN WEIGHTS.

| Indian. | Metric. | British. |
|---------------|--|---|
| I tola | =11.66380528 grammes = | 180 grains. |
| ı seer | =.933104423 kilogram = | 2.0571428 lbs. avoir. |
| 1 maund | = 37.3241769 kilograms = | 82.285714 " |
| | (| 1645.714285 " |
| | | .82285714 short ton |
| 1 kandy | =.746483538 tonne $=$ | 1645.714285 " .82285714 short ton (2000 lbs.). .7346939 long ton (2240 lbs.). |
| | | .7346939 long ton |
| | | (2240 lbs.). |
| I Burmese tik | al=16.55612361 grammes = | |
| | s =1.655612361 kilograms = | |
| | | 55 |
| Metric. | Indian. | Logarithm. |
| | (.0857353133 tola | 8.9331598 |
| 1 gramme | = {.0857353133 tola .0604006121 Burmese tikal | 8.7810413 |
| I bilogram | $= \begin{cases} 1.071691416 \text{ seers} \\ .604006121 \text{ Burmese viss} \end{cases}$ | 0.0300697 |
| | _ \.604006121 Burmese viss | 9.7810413 |
| I tonne | = 1.33961427 kandy | 0.1269797 |
| | | |
| British. | Indian. | Logarithm. |
| | (38.8 tolas | 1.5898256 |
| pound avoir. | ={38.8 tolas .486i seer .2739726 Burmese viss | 9.6867356 |
| | L.2739726 Burmese viss | 9.4377071 |

| | (.2/ 39/20 Durmese 105 | 9.43//0/1 |
|----------------------------|------------------------|-----------|
| I short ton(2000lbs.)= | 1.21527 kandy | 0.0846756 |
| $I \log ton (2240 lbs.) =$ | 1.36i kandy | 0.1338936 |

EQUIVALENTS OF THE STRAITS SETTLEMENTS WEIGHTS.

| Straits Settlements | . Metric. | | British. |
|---------------------|------------------------|----|---|
| 1 hoon (candareen) | = 377.99369 milligrams | = | 5.83 grains. |
| I chee (mace) | = 3.7799369 grammes | | 58.3 " |
| I tahil (tael) | = 37.799368975 " | = | 583.3 " or 13 oz. avoir. |
| 1 kati (kan) | =.6047899036 kilogram | = | 1.3 or $1\frac{1}{3}$ lbs. avoir. |
| 1 pikul (tam) | =60.47899036 kilograms | = | 133.3 " |
| | | 1 | 5333.3 " 2.6 or 2 ³ / ₃ short tons (2000 lbs.). |
| | | | 2.6 or 2 ³ / ₃ short tons |
| 1 koyan | =2.4191596144 tonnes | ={ | (2000 lbs.). |
| | | | 2.380952 long tons (2240 lbs.). |
| | | | (2240 lbs.). |

I

SECT. IV.

| Metric. | Straits Settlements. | Logarithm. |
|-------------------------|---------------------------------|------------|
| 1 milligram | n=.002645547 hoon | 7.4225155 |
| 1 gramme | =.026455+68 tahil | 8.4225155 |
| ı kilogram | =1.653466757 kati | 0.2183955 |
| I tonne | =.413366689 koyan | 9.6163355 |
| | | |
| British. | Straits Settlements. | Logarithm. |
| 1 grain | ∉.1714285 or 12 hoon | 9.2340832 |
| 1 pound avoir. | $=.75$ or $\frac{3}{4}$ kati | 9.8750613 |
| I short ton (2000 lbs.) | | 9.5740313 |
| I long ton (2240 lbs.) |)=.42 koyan | 9.6232493 |

Note.-Similar weights to the above, but bearing different names, are used in China (see page 46.)

EQUIVALENTS OF THE CAPE (S. AFRICA) MEASURES.

Lineal Measure.

| | | Logarithm. |
|----------------|----------------------------|----------------|
| I Cape foot | = 1.033 British feet | =0.0141003 |
| | =0.31485812453 metre | =9.4981149. |
| I Cape rood | = 12.396 British feet | =1.0932816 |
| | = 3.77829749440 metres | =0.5772961. |
| I metre | = 3.1760336548 Cape feet | =0.5018851 |
| | =0.26466947123 Cape rood | =9.4227039. |
| I British foot | t=0.968054211036 Cape foot | =9.9858997 |
| | =0.080671184253 Cape rood | |
| I statute mile | =425.9438528557 Cape roods | s = 2.6293523. |

Square Measure.

| | | Logarithm. |
|-------------------|----------------------------------|----------------|
| I square Cape roo | d=0.0035275669 acre | = 7.5474752. |
| I morgen | =0.85653191734 hectare | =9.9327435 |
| | =2.1165401652 acres | =0.3256265. |
| I hectare | =1.1674988166 morgen | =0.0672565. |
| I acre | = 40821.337301762 square Cape fe | et = 4.6108872 |
| | =283.48150904 square Cape rood | s = 2.4525247 |
| | =0.4724691817 morgen | =9.6743734. |
| I square mile | = 302.3802763093 morgen | =2.4805535 |

WEIGHTS AND MEASURES

PART I.

LEGAL EQUIVALENTS* OF THE EGYPTIAN WEIGHTS AND MEASURES.

(Legalised by a decree issued by the Khedive on the 28th April, 1891, with effect from the 1st of January, 1892.)

Commercial Weight.

| Egyptian. | Metric. | British. |
|--------------------|--------------------|--|
| I dirhem | = 3.12 grms. | =48.148928 grains. |
| I okieh | = 37.44 grms. | = 1.320656 oz. avoir. |
| I rotl or rottolo | =449.28 grms. | =.990492 lb. avoir. |
| ı oke | = 1.248 kilog. | = 2.751367 lbs. avoir. |
| | | = {99.049223 lbs. avoir. .0495246 short ton (2000 lbs.). .0442184 long ton (2240 lbs.). |
| 1 kantar | =44.928 kilog. | $=$ {.0495246 short ton (2000 lbs.). |
| | | .0442184 long ton (2240 lbs.). |
| | | $=\begin{cases} 165.082039 \text{ lbs. avoir.} \\ .08254102 \text{ short ton } (2000 \text{ lbs.}). \\ .07369734 \text{ long ton } (2240 \text{ lbs.}). \end{cases}$ |
| I hamlah | =74.880 kilog. | $=$ $\frac{1}{2000}$ lbs.). |
| | | .07369734 long ton (2240 lbs.). |
| | | (308.153139 lbs. avoir. |
| I Alexandria kanta | r = 139.776 kilog. | $= \begin{cases} 308.153139 \text{ lbs. avoir.} \\ .15407657 \text{ short ton } (2000 \text{ lbs.}). \\ .1375684 \text{ long ton } (2240 \text{ lbs.}). \end{cases}$ |
| | | .1375684 long ton (2240 lbs.). |
| | | $= \begin{cases} 550.273463 \text{ lbs. avoir.} \\ .27513673 \text{ short ton } (2000 \text{ lbs.}). \\ .2456578 \text{ long ton } (2240 \text{ lbs.}). \end{cases}$ |
| 1 heml | =249.60 kilog. | $=$ {.27513673 short ton (2000 lbs.). |
| | | .2456578 long ton (2240 lbs.). |

Jewellers' Weight.

| | Egyptian | <i>n</i> . | Metric. | В | ritish. | |
|---|---------------|------------|-------------|-----------|------------|-----|
| | I kamha | =48.75 | milligrams | =.752327 | grain. | |
| | 1 kirat | =.195 § | gramme | = 3.00930 | 8 grains. | |
| | 1 dirhem | = 3.12 | grammes | =48.1489 | 28 grains. | |
| | I mithkal | =4.68 | grammes | =72.2233 | 92 grains. | |
| | Metric. | E | gyptian. | Le | garithm. | |
| | I gramme | e = 5.12 | 82 kirats | 0 | .7099654 | |
| | | =.320 | 51282 dirh | em 9 | .5058454 | |
| | ı kilograr | n = 2.22 | 57835 rotls | 0 | .3474829 | |
| | | =.801 | 282 oke | 9 | .9037854 | |
| | | =.022 | 257835 kar | ntar 8 | .3474829 | |
| | I tonne | =4.00 | 64103 hem | ls o | .6027554 | |
| | British. | | Egypt | ian. | Logarit | hm. |
| I | grain | | =.3323023 | kirat | 9.52153 | 33 |
| | | | =.0207689 | dirhem | 8.31741 | 33 |
| I | oz. troy | | =9.969067 | | 0.99865 | 45 |
| I | lb. avoir. | | = 1.00960 | rotls | 0.00414 | .89 |
| | short ton (20 | | | | 1.30517 | |
| I | long ton (22 | 40 lbs.) | - | | 1.35439 | |
| | | | =4.0707 h | emls | 0.60966 | 95 |

* The relation of the British Imperial to the Metric equivalents given in these tables is not quite accurate, as will be seen by reference to page 14.

SECT. IV.]

CONVERSION TABLES

Lineal Measure.

| Egyptian. | Metric. | British. |
|------------------|----------------|--|
| ı diraâ baladi | =0.580 metre | $= \begin{cases} 22.835058 \text{ inches.} \\ 1.9029215 \text{ feet.} \end{cases}$ |
| 1 diraâ mimari | =0.750 metre | $= \begin{cases} 29.5281 \text{ inches.} \\ 2.460675 \text{ feet.} \\ = 2.18176 \text{ feet.} \end{cases}$ |
| 1 pike istambuli | =0.665 metre | =2.18176 feet. |
| 1 kassabah | = 3.550 metres | $S = \begin{cases} 139.766304 \text{ inches.} \\ 11.647192 \text{ feet.} \end{cases}$ |

| Metric. | Egyptian. | Logarithm. |
|--------------|-----------------------|------------|
| I metre = I. | 724138 diraâs baladi | 0.2365720 |
| = 1. | 3 or 13 diraâs mimari | 0.1249387 |
| = I. | 50376 pikes istambuli | 0.1771784 |
| =.28 | 8169 kassabah | 9.4497716 |
| British | Fountian | Locarithan |

| British. Egyptian. | Logarithm. |
|------------------------------|------------|
| 1 foot =.525508 diraâ baladi | 9.7205791 |
| =.4063926 diraâ mimari | 9.6089458 |
| =.4583455 pike istambuli | 9.6611930 |
| =.0858576 kassabah | 8.9337787 |
| I yard=.2575728 kassabah | 9.4109000 |

Square Measure.

Egyptian.

Metric.

British.

| | square diraâ baladi =.3364 square metre =3.62111 square feet. |
|---|--|
| I | square diraâ mimari=.5625 square metre =6.05492 square feet. |
| I | square kassabah $=$ 12.6025 square metres = 15.073009 sq. yards. |
| I | feddan $=.420083$ hectare $=1.038086$ acres.* |

| Metric. | Egyptian. | Logarithm. |
|---------------|--|---------------------------------|
| I square metr | e=2.97265 square diraâs baladi | 0.4731440 |
| | $=1.7$ or $1\frac{7}{9}$ square diraâs mimari | 0.2498775 |
| | =.079349 square kassabah | 8.8995433 |
| I hectare | =2.380480 feddans | 0.3766646 |
| | | |
| 70 141 7 | 73 / / * | * 1.7 |
| British. | Egyptian. | Logarithm. |
| | <i>Egyptian.</i> =.27615845 square diraâ baladi | <i>Logarithm</i> . 9.4411582 |
| | 07* | 0 |
| I square foot | =.27615845 square diraâ baladi | 9.4411582 |
| I square foot | =.27615845 square diraâ baladi =.165155 square diraâ mimari | 9.4411582 9.2178916 |

* From the equivalent given on page 34, .420083 hectare=1.03805 acres.

WEIGHTS AND MEASURES

Measures of Capacity.

| Egyptian. | Metric. | . British. |
|--------------|--------------------|--|
| 1 kirat | =.06445 litre | =.453949 gill. |
| 1 karrūbah | =.1289 litre | =.9079 gill. |
| I tūmnah | =.2578 litre | = 1.815797 gills. |
| I rūbaah | =.515625 litre | =.9079 pint. |
| I nesf kadah | 1=1.03125 litres | =1.815797 pints. |
| 1 kadah | =2.0625 litres | = 3.631595 pints. |
| 1 malwa | =4.125 litres | = 3.631595 quarts. |
| ı rūb | =8.25 litres | = 1.815797 gallons. |
| 1 kilah | = 16.5 litres | = 3.631595 gallons. |
| 1 webah | = 33.0 litres | =7.26319 gallons. |
| 1 ardeb | = 1.98 hectolitres | $= \begin{cases} 43.579136 \text{ gallons.*} \\ 5.447392 \text{ bushels.} \end{cases}$ |

| Metric. | Egyptian. | Logarithm. |
|--------------|------------------|------------|
| 1 hectolitre | e=.50 ardeb | 9.7033348 |
| 1 litre | =.jo webah | 8.4814861 |
| | =.60 kilah | 8.7825161 |
| | =.iż rūb | 9.0835461 |
| | =.24 malwa | 9.3845761 |
| | =.48 kadah | 9.6856061 |
| | =.96 nesf kadah | 9.9866361 |
| | = 1.93 rūbaahs | 0.2876661 |
| | = 3.87 tūmnahs. | 0.5886961 |
| | =7.75 karrūbahs | 0.8897261 |
| | =15.5i kirats | 1.1907561 |
| | | |
| British. | Egyptian. | Logarithm. |
| I bushel | =.18357409 ardeb | 9.2638114 |
| 'I gallon | =.02294676 ardeb | 8.3607214 |
| | =.13768 webah | 9.1388727 |

| =.13768 webah | 9.1388727 |
|-----------------------|--|
| =.275361 kilah | 9.4399027 |
| =.550722 rūb | 9.7409327 |
| =.275361 malwa | 9.4399027 |
| =.275361 kadah | 9.4399027 |
| =.550722 nesf kadah | 9.7409327 |
| =1.1014445 rūbaahs | 0.0419627 |
| =2.202889 tūmnahs | 0.3429927 |
| = 1.1014445 karrūbahs | 0.0419627 |
| =2.202889 kirats | 0.3429927 |
| | =.275361 kilah =.550722 rūb =.275361 malwa =.275361 kadah =.550722 nesf kadah =1.1014445 rūbaahs =2.202889 tūmnahs =1.1014445 karrūbahs |

* The British legal equivalent of 198 litres is 43.55505 gallons.

SECT. V.] COMPARISON OF PRICES

SECTION V. COMPARISON OF PRICES AND RATES OF EXCHANGE.

COMPARISON OF FRENCH AND GERMAN PRICES FOR METRIC UNITS, BRITISH PRICES FOR IMPERIAL UNITS, AND UNITED STATES PRICES FOR UNITED STATES UNITS.

| Francs Shillings per per kilogram. pound. | Francs Shillings per per metre. yard. | Francs Shillings per British litre. Imp. gal. | Francs Shillings per per hectolitre. British bushel. | Dollars per U.S. weight or lineal measure. Shillings per British weight or lineal measure. |
|--|---|--|---|--|
| $\begin{array}{rrrr} 1 & = .360 \\ 2 & = .719 \\ 3 & = 1.079 \\ 4 & = 1.439 \end{array}$ | $\begin{array}{rrrr} 1 & = .725 \\ 2 & = 1.450 \\ 3 & = 2.175 \\ 4 & = 2.901 \end{array}$ | $\begin{array}{rrrr} 1 &= 3.605 \\ 2 &= 7.210 \\ 3 &= 10.815 \\ 4 &= 14.420 \end{array}$ | $\begin{array}{rrrr} 1 & = .288 \\ 2 & = .577 \\ 3 & = .865 \\ 4 & = 1.154 \end{array}$ | $ \begin{array}{rcl} 1 &= 4.110 \\ 2 &= 8.219 \\ 3 &= 12.329 \\ 4 &= 16.439 \end{array} $ |
| 5 = 1.799 6 = 2.158 7 = 2.518 8 = 2.878 9 = 3.237 | $5 = 3.626 \\ 6 = 4.351 \\ 7 = 5.076 \\ 8 = 5.801 \\ 9 = 6.526$ | 5 = 18.025 6 = 21.630 7 = 25.235 8 = 28.840 9 = 32.445 | 5 = 1.442 6 = 1.730 7 = 2.019 8 = 2.307 9 = 2.596 | 5 = 20.5496 = 24.6587 = 28.7688 = 32.8789 = 36.988 |
| 2.780 = 1 5.560 = 2 8.340 = 3 11.120 = 4 | 1.379 = 1 2.758 = 2 4.137 = 3 5.516 = 4 | .277=1 .555=2 .832=3 I.110=4 | 3.467 = 1 6.935 = 2 10.402 = 3 13.869 = 4 | .243=1 .487=2 .730=3 .973=4 |
| 13.900 = 5 16.680 = 6 19.460 = 7 22.240 = 8 25.020 = 9 | 6.895=5 8.274=6 9.653=7 11.032=8 12.411=9 | 1.387 = 5 1.664 = 6 1.942 = 7 2.219 = 8 2.497 = 9 | 17.337 = 5 20.804 = 6 24.272 = 7 27.739 = 8 31.206 = 9 | $ \begin{array}{r} 1.217 = 5\\ 1.460 = 6\\ 1.703 = 7\\ 1.947 = 8\\ 2.190 = 9 \end{array} $ |
| Marks Shillings per avoir, kilogram. pound. | Marks Shillings per per metre, yard. | Marks Shillings per per litre. Imp. gal. | Marks Shillings per British hectolitre. bushel. | Cents per per U.S. British unit of unit of weight unit of or lineal weight measure. |
| 1 = .444 | 1 = .895 | 1 = 4.450 | 1 = .356 | 1 = .493 |

| $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ | $\begin{array}{rrrr} 1 & = .895\\ 2 & = 1.790\\ 3 & = 2.685\\ 4 & = 3.581\\ 5 & = 4.476\\ 6 & = 5.371\\ 7 & = 6.266\\ 8 & = 7.161\\ 9 & = 8.056 \end{array}$ | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ |
|--|--|---|---|--|
| 2.252 = 1 $4.504 = 2$ $6.756 = 3$ $9.008 = 4$ $11.260 = 5$ $13.512 = 6$ $15.764 = 7$ $18.016 = 8$ $20.268 = 9$ | I. 117 = 1 2. 234 = 2 3. 351 = 3 4.469 = 4 5.586 = 5 6. 703 = 6 7.820 = 7 8.937 = 8 10.054 = 9 | .225=1 .449=2 .674=3 .899=4 I.124=5 I.348=6 I.573=7 I.798=8 2.022=9 | 2.809 = 1 5.618 = 2 8.426 = 3 11.235 = 4 14.044 = 5 16.853 = 6 19.662 = 7 22.470 = 8 25.279 = 9 | 2.028=1 4.055=2 6.083=3 8.111=4 10.139=5 12.166=6 14.194=7 16.222=8 18.249=9 |

WEIGHTS AND MEASURES [PART I.

Comparison of French and German Prices for Metric Units, British Prices for Imperial Units, and United States Prices for United States Units (Continued).

| Francs Dollars per avoir. kilogram. pound. | Francs Dollars per per metre. yard. | Francs Dollars per U.S. litre. liquid gal. | Francs Dollars per per U.S. hectolitre. bushel. | Shillings Dollars per per British U.S. Imp. gal. liquid gal. |
|---|--|---|--|--|
| $ \begin{array}{rcrr} 1 & =.088 \\ 2 & =.175 \\ 3 & =.263 \\ 4 & =.350 \end{array} $ | $ \begin{array}{rcl} 1 & = .176 \\ 2 & = .353 \\ 3 & = .529 \\ 4 & = .705 \end{array} $ | $ \begin{array}{rcl} 1 & = .731 \\ 2 & = 1.461 \\ 3 & = 2.192 \\ 4 & = 2.922 \end{array} $ | $\begin{array}{rrrr} 1 & =.068 \\ 2 & =.136 \\ 3 & =.204 \\ 4 & =.272 \end{array}$ | $ \begin{array}{rcrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ |
| 5 =.438 6 =.525 7 =.613 8 =.700 9 =.788 | 5 = .8826 = I.0587 = I.2348 = I.4119 = I.587 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ | 5 =.340 6 =.408 7 =.476 8 =.544 9 =.612 | 5 = 1.013 6 = 1.216 7 = 1.418 8 = 1.621 9 = 1.824 |
| 11.423 = 1 $22.846 = 2$ $34.269 = 3$ $45.691 = 4$ $57.115 = 5$ $68.537 = 6$ $79.960 = 7$ $91.383 = 8$ $102.806 = 9$ | 5.667 = 1 II. 334 = 2 I7.000 = 3 22.667 = 4 28.334 = 5 34.001 = 6 39.668 = 7 45.334 = 8 51.001 = 9 | 1.369 = 1 $2.738 = 2$ $4.106 = 3$ $5.475 = 4$ $6.844 = 5$ $8.213 = 6$ $9.581 = 7$ $10.950 = 8$ $12.319 = 9$ | 14.703 = 1 $29.407 = 2$ $44.110 = 3$ $58.813 = 4$ $73.517 = 5$ $88.220 = 6$ $102.923 = 7$ $17.627 = 8$ $132.330 = 9$ | $\begin{array}{c} 4.935 = 1\\ 9.871 = 2\\ 14.806 = 3\\ 19.742 = 4\\ 24.677 = 5\\ 29.612 = 6\\ 34.548 = 7\\ 39.483 = 8\\ 44.419 = 9\end{array}$ |

| Marks per kilogram. Dollars per avoir. pound. | Marks Dollars per per metre. yard. | Marks Dollars per U.S. litre. liquid gal. | Marks Dollars per per U.S. hectolitre. bushel. | Shillings Dollars per per U.S. British bus. bushel. |
|--|--|--|--|---|
| $\begin{array}{rrrr} 1 & =.108 \\ 2 & =.216 \\ 3 & =.324 \\ 4 & =.432 \end{array}$ | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ | $ \begin{array}{rcl} 1 & = .901 \\ 2 & = 1.802 \\ 3 & = 2.703 \\ 4 & = 3.604 \end{array} $ | $ \begin{array}{rcrr} 1 & =.084 \\ 2 & =.168 \\ 3 & =.252 \\ 4 & =.335 \end{array} $ | $ \begin{array}{rcl} 1 & = .236 \\ 2 & = .472 \\ 3 & = .707 \\ 4 & = .943 \end{array} $ |
| 5 =.540 6 =.648 7 =.756 8 =.864 9 =.972 | | | 5 = .419 6 = .503 7 = .587 8 = .671 9 = .755 | 5 = 1.179 6 = 1.415 7 = 1.650 8 = 1.886 9 = 2.122 |
| 9.263=1 18.526=2 27.789=3 37.052=4 | 4.595= 1 9.190= 2 13.785= 3 18.380= 4 | 1.110=1 2.220=2 3.330=3 4.440=4 | 11.923=1 23.847=2 35.770=3 47.693=4 | 4.24I = 1 8.483 = 2 12.724 = 3 16.965 = 4 |
| 46.316=5 55.579=6 64.842=7 74.105=8 83.368=9 | 22.975=5 27.570=6 32.165=7 36.760=8 41.355=9 | 5.550=5 6.660=6 7.770=7 8.880=8 9.990=9 | 59.616=5 71.540=6 83.463=7 95.386=8 107.310=9 | 21.207 = 5 25.448 = 6 29.689 = 7 33.931 = 8 38.172 = 9 |

SECT. V.]

Gold Export Country. Gold Import Point. Mint Parity. Point. France, Belgium, Francs 25.35 Fr. 25.22 Fr. 25.09 Italy, Switzerland, Holland, -Florins 12.15 Fl. 12.103 Fl. 12.04 Germany, Marks 20.51 M. 20.43 M. 20.35 Austria-Hungary, Kronen 24.20 Kr. 24.02 Kr. 23.90 Scandinavia, Kroner 18.30 Kr. 18.16 Kr. 18.02 Russia. Roubles 9.6 Rs. 9.366 Rs. 9.459 $(1 \text{Rs.} = 25\frac{3}{8} \text{d.})(1 \text{Rs.} = 25\frac{5}{8} \text{d.})$ (1 Rr. = 25 d.)United States of Dollars 4.90 \$ 4.8665 \$ 4.84 America, Rupees 15 R 14.657 British India, - $(I \mathbf{R} = Is. 4d.) (I \mathbf{R} = Is.4\frac{3}{8}d.)$ Piastres 971 Egypt, Piastres 97% Piastres 975

TABLE OF RATES OF EXCHANGE FOR MONEY.

The above table * gives the value of \pounds_I sterling in the currencies of the following countries: France, Belgium, Italy, Switzerland, Holland, Germany, Austria-Hungary, Scandinavia, Russia, United States of America, British India and Egypt.

The middle column gives the exchange at mint parity, *i.e.* the actual gold value of the foreign currency in comparison with the pound sterling, while the other columns show the extremes of fluctuation in the rate of exchange *in normal times*. In the left-hand column are the rates of exchange at which in sending remittances *to* London it would be more profitable to send gold than to purchase drafts; while in the right-hand column are the rates at which in remitting *from* London it would be more profitable to buy gold and send it abroad than to purchase drafts.

* Kindly compiled by Mr. F. Moshack of the Deutsche Bank.

PART II. DATA RELATING TO FORCE AND ENERGY.

SECTION I. MECHANICAL UNITS.

Force.—The British unit of force is termed the *poundal*; it is that force which, acting on a mass of I lb. for one second, gives it a velocity of one foot per second. On the c.g.s. (centimetre-gramme-second) system the unit of force is the *dyne*, which may be defined as that force which, acting on a mass of I gramme, gives it a velocity of I centimetre per second.

1 poundal = 13825 dynes.

Gravity.—The apparent acceleration (or increase of velocity per unit of time) of a body falling freely under the influence of gravity in vacuo (g) varies according to locality. The value of g in c.g.s. units is 981.17 centimetres per second at Greenwich, 980.94 at Paris, 981.25 at Berlin, 978.10 at the equator and 983.11 at the poles. The mean value adopted by the International Bureau of Weights and Measures for latitude 45° at sealevel is 980.665.* In British measure the value of g for London at sea-level is about 32.19 feet per second.† The length of the seconds pendulum for the same places is as follows:

Greenwich, 99.413 cm.; Paris, 99.390 cm.; Berlin, 9.422 cm.; equator, 99.103 cm.; and the poles, 99.610 cm.

Work.— The British unit of work is the *foot-poundal*. It is the work done by a force of I poundal acting over a distance of I foot. Work is also expressed in *foot-pounds*, the unit in this case being the work done when a body moves through I foot against a resistance of gravity equal to I lb.

I foot-pound = g poundals.

* Comptes Rendus des séances de la Troisième Conférence générale des Poids et Mesures à Paris, 1901, p. 70.

† This is the value adopted by the Board of Trade Standards Department.

SECT. I.

On the c.g.s. system the unit of work is the erg. It is the work done by a force of I dyne acting over a distance of I centimetre.

1 foot poundal = 421401 ergs.

1 foot-pound = 1.356×10^7 ergs (g being taken as 981).

Power.—The British unit of power or rate of doing work is the *horse-power*. It is equivalent to 33,000 foot-pounds per minute or 550 foot-pounds per second. The French unit—the *force de cheval*—is defined as 75 kilogram-metres per second. One "force de cheval" equals 0.9863 horse-power or 542.48 foot-pounds per second, and conversely 1 horse-power = 1.01385 "force de cheval."

On the c.g.s. system the unit of power is 1 erg per second.

Taking g as equal to 981, we have

1 horse-power = 7.46×10^9 ergs per second.

I force de cheval = 7.36×10^9 ergs per second.

SECTION II. ELECTRICAL UNITS.

Resistance.—The unit of electrical resistance is the *ohm*.* It is defined by the Board of Trade \dagger as "the resistance offered to an unvarying electric current by a column of mercury, at the temperature of melting ice, 14.4521 grammes in mass of a constant cross sectional area and of a length of 106.3 centimetres." For practical purposes, however, the Board of Trade use as the standard of electrical resistance the resistance between the copper terminals of a coil of insulated wire of platinum alloy to the passage of an unvarying electrical current, at a temperature of 15.4 C. This standard is marked "Board of Trade Ohm Standard, verified 1894,"‡ and is deposited at the Board of Trade Standardising Laboratory. The ohm has the value of 10⁹ absolute units on the c.g.s. system.

Current.-The unit of current is the ampere. It is defined by

* The terms *ohm* and *volt* were first suggested by Sir C. Bright and Mr. Latimer Cross: together with *ampere*, *coulomb* and *farad*, they were adopted by an International Congress which met in 1881. The use of the terms *joule*, *watt* and *henry* was recommended by the Chamber of Delegates at the Chicago Exhibition in 1893.

+ Final Report of the Electrical Standards Committee, 1894, p. 10.

[‡]This Standard was legalised by Order in Council of her late Majesty Queen Victoria of Aug. 23, 1894. the Board of Trade as the electric current, which, when passed through a neutral solution containing 15 per cent. of nitrate of silver, deposits silver at the rate of 0.001118 of a gramme per second.* For practical purposes the standard used by the Board of Trade is the current "which is passing in and through the coils of wire forming part of the instrument marked 'Board of Trade Ampere Standard, verified 1894' when in reversing the current in the fixed coils the change in the forces acting upon the suspended coil in its righted position is exactly balanced by the force exerted by gravity in Westminster upon the iridio platinum weight marked A and forming part of the said instrument."[†] The ampere has the value of $\frac{1}{10}$ or 10⁻¹ C.G.S. units.

1 milli-ampere = $\frac{1}{1000}$ ampere.

1 kilo-ampere = 1000 amperes.

Pressure.—The unit of electrical pressure is the *volt*. It is "the pressure which, if steadily applied to a conductor whose resistance is one ohm, will produce a current of one ampere, and is represented by 0.6974 of the electrical pressure at a temperature of 15° C. between the poles of the voltaic cell, known as Clark's cell."‡ For practical purposes the unit is measured by a particular instrument marked "Board of Trade Volt Standard, verified 1894," deposited at the Board of Trade Standardising Laboratory. On the c.g.s. system the volt has the value of 10^{8} .

Quantity.—The unit of quantity is the *coulomb*. It is the quantity of electricity which in one second of time passes any part of a circuit in which the current has the strength of one ampere. Therefore I coulomb equals I ampere-second.

On the c.g.s. system the coulomb has the value of 10^{-1} .

1 micro coulomb = $\frac{1}{1,000,000}$ or 10^{-6} coulomb.

Capacity.—The unit of capacity is the *farad*. It is the capacity of a condenser charged to the potential of I volt by I coulomb of electricity. On the c.g.s. system the farad has the value of Io^{-9} .

I micro-farad =
$$\frac{I}{I,000,000}$$
 or $I0^{-6}$ farad.

* Final Rep. of the Elect. Stand. Comm., 1894, p. 10.

+ Loc. cit., p. 11.

 \ddagger Loc. cit. Clark's cell consists of zinc or an amalgam of zinc with mercury and of mercury in a neutral saturated solution of zinc sulphate and mercurous sulphate in water, prepared with mercurous sulphate in excess.

ELECTRICAL UNITS

Work.—The unit of work is the *joule*. It is equivalent to the energy disengaged as heat in one second by a current of I ampere flowing through a resistance of I ohm, or in other words, under an electro-motive force of I volt.

I joule = 10^7 ergs or absolute units of work.

Power.—The unit of power or rate of doing work is the *watt*. It is the work done at the rate of I joule per second. In other words, the watt represents the energy contained in a current of one ampere flowing under an electro-motive force of I volt. On the c.g.s. system the watt represents 10^7 ergs per second. The practical unit of work is the *kilowatt*.

1 kilowatt = 1000 watts

= 1.34 horse-power.

1 horse-power = 746 watts or .746 kilowatt.

The commercial or Board of Trade unit is the *kilowatt-hour*. It is defined by the Board of Trade as "the energy contained in a current of one thousand amperes flowing under an electro-motive force of one volt during one hour."

Induction.—The unit of induction is the *henry*. It is the induction in a circuit when the electro-motive force induced in this circuit is one volt, while the inducing current varies at the rate of one ampere per second.

On the c.g.s. system the henry has the value of 109.

Table of Horse Power and Kilowatts in terms of one another.

| I | Horse-powe | r = 0.746 | Kilowatt. | IK | Cilowat | tt = | 1.340 | Horse power |
|---|------------|-----------|------------|-----|---------|------|-----------------|-------------|
| 2 | " | = 1.492 | Kilowatts. | 2 K | Cilowat | tts= | 2.681 | >> |
| 3 | >> | =2.238 | ,, | 3 | ,, | = | 4.02 I | 37 |
| 4 | >> | = 2.984 | " | 4 | " | = | 5.362 | " |
| 5 | >> | = 3.730 | " | 5 | ,, | | 6.702 | " |
| 6 | >> | =4.476 | " | 6 | ,, | = | 8.043 | >> |
| 7 | >> | = 5.222 | " | 7 | • • • • | = | 9.383 | " |
| 8 | >> | = 5.968 | " | 8 | " | | 0.724 | >> |
| 9 | >> | =6.714 | ,, | 9 | >> | = 1 | 1 2.06 4 | " |
| | | | | | | | | |

SECTION III. THERMAL UNITS.

The British thermal unit is the amount of heat required to raise 1 pound of water through 1 degree Fahrenheit. The thermal capacity of water varies slightly with the temperature; but the standard temperature of the water at which the unit should be defined has not yet been fixed by convention.

The French thermal unit is the *therm* or gramme-degree. It has also been termed the *minor calorie*. It is the quantity of heat required to raise I gramme of water through I degree Centigrade. It is sometimes defined as the amount of heat required to raise I gramme of water from 0° C. to 1° C., or as the one-hundredth part of the heat required to raise one gramme of water from 0° to 100° C.

The *major calorie* is the quantity of heat required to raise I kilogramme of water through I degree Centigrade.

- 1 major calorie = 1000 therms.
- 1 therm or minor calorie = 0.00396832 British thermal unit

 $(\log = 7.5986067).$

I British thermal unit = 251.99579 therms

 $(\log = 2.4013933).$

The capacity for heat (or thermal capacity) of a substance is the quantity of heat required to raise the temperature of that substance I degree (Centigrade or Fahrenheit, according to the units in use).

The capacity for heat of water can be expressed thus:

1 calorie (therm) = 4.180 joules at 20°C.*

The specific heat of a substance is the ratio of the quantity of heat required to raise the temperature of a given mass of any substance one degree to the quantity of heat required to raise the temperature of an equal mass of water one degree (Glazebrook).

The latent heat of fusion is the quantity of heat required to change I gramme (or I lb.) of a substance from the solid to its liquid form without raising its temperature. The latent

* Preston's Theory of Heat, 2nd edition, London, 1904, p. 322.

SECT. III.

heat of fusion of ice is 80 therms (Bunsen) or 144 British thermal units.

The latent heat of vaporization of a liquid is the amount of heat required to change I gramme (or I lb.) of the liquid into vapour without raising its temperature. The latent heat of vaporization of water is 537 therms, or 967 British thermal units.

The evaporative power or calorific value of a fuel is the number of pounds of water evaporated at 212° F. by the combustion of 1 lb. of that fuel. It may be expressed in British thermal units by multiplying the number of pounds of water evaporated at 212° F. by 967 (the latent heat of vaporization of water).

The mechanical equivalent of heat. The symbol J is used to designate the number of units of work necessary to generate one unit of heat when the unit is all spent in generating heat. Prof. Rowland's experiments show that at 20° C.*

> J = 427.5 gramme-metres = 779 foot-pounds,

i.e. the work done in raising $\begin{bmatrix} I & gramme \\ I & pound \end{bmatrix}$ through $\begin{cases} 427.5 & metres \\ 779.0 & feet \end{cases}$ will, if spent in friction, raise the temperature of $\begin{bmatrix} I & gramme \\ I & pound \end{bmatrix}$ of water I degree $\begin{cases} Centigrade \\ Fahrenheit \end{cases}$.

* Preston's Theory of Heat, London, 1904, p. 45.

FORCE AND ENERGY [PART 11.

| Compa | rative T | Table of | Fahren | iheit, Ré | aumur a | and Cer | ntigrade | Degrees. |
|------------|--------------|--------------|------------|--------------|--------------|------------|--------------|--------------|
| | Degrees. | | | Degrees. | | | Degrees. | |
| Fahr. | Réaum. | Cent. | Fahr. | Réaum. | Cent. | Fahr. | Réaum. | Cent. |
| 212 | 80.0 | 100.0 | 171 | 61.8 | 77.2 | 1 30 | 43.6 | 54·4 |
| 211 | 79.6 | 99.4 | 170 | 61.3 | 76.7 | 1 29 | 43.1 | 53·9 |
| 210 209 | 79.I 78.7 | 98.9 98.3 | 169 168 | 60.9 60.4 | 76.1 75.6 | 128 | 42.7 | 53.3 |
| 208 | 78.2 | 97.8 | 167 | 60.0 | 75.0 | 127 126 | 42.2 41.8 | 52.8 52.2 |
| 207 | 77.8 | 97.2 | 166 | 59.6 | 74·4 | 125 | 41 .3 | 51.7 |
| 206 | 77.3 | 96.7 | 165 | 59.1 | 73·9 | 124 | 40.9 | 51.1 |
| 205 | 76.9 | 96.1 | 164 | 58.7 | 73·3 | 123 | 40.4 | 50.6 |
| 204 | 76.4 | 95.6 | 163 | 58.2 | 72.8 | 122 | 40.0 | 50.0 |
| 203 | 76.0 | 95.0 | 162 | 57.8 | 72.2 | 121 | 39.6 | 49.4 |
| 202 | 75.6 | 94.4 | 161 | 57.3 | 71.7 | 120 | 39.1 | 48.9 |
| 20I 200 | 75.1 | 93.9 93.3 | 160 159 | 56.9 | 71.I 70.6 | 119 | 38.7 38.2 | 48.3 |
| 199 | 74.2 | 92.8 | 158 | 56.0 | 70.0 | 117 | 37.8 | 47.2 |
| 198 | 73.8 | 92.2 | 157 | 55.6 | 69.4 | 116 | 37·3 | 46.7 |
| 197 | 73.3 | 91.7 | 156 | 55.1 | 68.9 | 115 | 36.9 | 46.1 |
| 196 | 72.9 | 91.1 | 155 | 54.7 | 68.3 | 114 | 36.4 | 45.6 |
| 195 | 72.4 | 90.6 | 154 | 54.2 | 67.8 | 113 | 36.0 | 45.0 |
| 194 | 72.0 | 90.0 | 153 | 53.8 | 67.2 | II2 | 35.6 | 44.4 |
| 193 | 71.6 | 89.4 | 152 | 53.3 | 66.7 | III | 35.1 | 43.9 |
| 192 | 71.1 | 88.9 | 151 | 52.9 | 66.1 | 110 | 34.7 | 43·3 |
| 191 | 70.7 | 88.3 | 150 | 52.4 | 65.6 | 109 | 34.2 | 42.8 |
| 190 | 70.2 | 87.8 | 149 | 52.0 | 65.0 | 108 | 33.8 | 42.2 |
| 189 | 69.8 | 87.2 | 148 | 51.6 | 64.4 | 107 | 33.3 | 41.7 |
| 188 | 69.3 | 86.7 | 147 | - 51.I | 63.9 | 106 | 32.9 | 41.1 |
| 187 | 68.9 | 86.1 | 146 | 50.7 | 63.3 | 105 | | 40.6 |
| 186 185 | 68.4 68.0 | 85.6 | 145 | 50.2 | 62.8 | 104 | 32.4 32.0 | 40.0 |
| 184 | 67.6 | 85.0 84.4 | 144 143 | 49.8 49.3 | 62.2 61.7 | 103 102 | 31.6 31.1 | 39.4 38.9 |
| 183 | 67. I | 83.9 | 142 | 48.9 | 61.1 | 101 | 30.7 | 38.3 |
| 182 | 66.7 | 83.3 | 141 | 48.4 | 60.6 | 100 | 30.2 | 37.8 |
| 181 | 66.2 | 82.8 | 140 | 48.0 | 60.0 | 99 | 29.8 | 37.2 |
| 180 | 65.8 | 82.2 | 139 | 47.6 | 59.4 | 98 | 29.3 | 36.7 |
| 179 | 65.3 | 81.7 | 138 | 47.I | 58.9 | 97 | 28.9 | 36.1 |
| 178 | 64.9 | 81.1 | 137 | 46.7 | 58.3 | 96 | 28.4 | 35.6 |
| 177 | 64.4 | 80.6 | 136 | 46.2 | 57.8 | 95 | 28.0 | 35.0 |
| 176 | 64.0 | 80.0 | 135 | 45.8 | 57.2 | 94 | 27.6 | 34.4 |
| 175 174 | 63.6 63.1 | 79.4 78.9 | 134 | 45.3 | 56.7 56.1 | 93 | 27.1 26.7 | 33.9 |
| 173 | 62.7 | 78.3 | 133 132 | 44.9 44.4 | 55.6 | 92 91 | 26.2 | 33.3 32.8 |
| 172 | 62.2 | 77.8 | 131 | 44.0 | 55.0 | 90 | 25.8 | 32.2 |

Thermometric Scales.

SECT. III.] THERMOMETRIC SCALES

| | Degrees. | | | Degrees. | | | Degrees. | | | | | |
|---|---|---|---|--|---|--|--|---|--|--|--|--|
| Fahr. | Réaum. | Cent. | Fahr. | Réaum. | Cent. | Fahr. | Réaum. | Cent. | | | | |
| Fahr. 89 88 87 86 85 84 83 82 81 80 79 78 77 76 75 74 73 72 71 70 69 68 67 66 65 64 63 62 61 60 59 58 57 55 55 54 55 55 55 52 51 | Réaum. 25.3 24.9 24.4 24.0 23.6 23.1 22.7 22.2 21.8 21.3 20.9 20.4 20.0 19.6 19.1 18.7 18.2 17.8 17.3 16.9 16.4 15.6 15.1 14.7 14.2 13.8 13.3 12.9 12.4 12.0 11.1 10.7 10.2 9.8 9.3 8.4 | Cent. 31.7 31.1 30.6 30.0 29.4 28.9 28.3 27.8 27.2 26.7 26.1 25.6 25.0 24.4 23.9 23.3 22.8 22.2 21.7 21.1 20.6 20.4 23.9 23.3 22.8 22.2 21.7 21.1 20.6 25.0 24.4 23.9 23.3 22.8 22.2 21.7 21.1 20.6 25.0 24.4 23.9 23.3 22.8 22.2 21.7 21.1 20.6 20.4 23.9 24.3 27.8 27.2 26.7 26.1 25.0 24.4 23.9 20.3 22.8 22.2 21.7 21.1 20.6 20.0 19.4 18.9 19.4 20.7 20.7 21.1 15.6 20.0 19.4 18.9 18.3 17.2 16.7 15.6 15.0 19.4 18.9 18.3 17.2 16.7 15.6 15.0 19.4 18.9 18.3 17.2 16.7 15.6 15.0 20.0 19.4 18.9 18.3 17.2 16.7 15.6 19.4 18.9 18.3 17.2 16.7 15.6 15.0 19.4 18.9 18.3 17.2 16.7 15.6 15.0 14.4 13.9 15.6 15.0 14.4 13.9 15.6 15.0 14.4 13.9 12.8 12.8 12.8 12.8 12.8 12.8 12.8 17.2 16.7 16.1 15.6 15.0 14.4 13.9 12.8 12.7 12.7 13.7 14.1 15.6 15.0 14.4 15.6 15.0 14.4 15.6 15.0 14.4 15.6 15.0 14.4 15.6 15.7 | Fahr. 48 47 46 45 44 43 42 41 40 39 38 37 36 35 34 33 32 31 30 29 28 27 26 25 24 23 22 21 20 19 18 17 16 15 14 13 12 11 10 | Réaum. 7.1 6.7 5.8 5.3 4.9 4.4 4.0 3.6 3.1 2.7 2.2 1.8 1.3 0.9 -0.4 -0.9 -1.3 -1.8 -2.2 -2.7 -3.1 -3.6 -4.0 -4.0 -5.3 -5.8 -6.2 -5.8 -6.2 -5.8 -5.8 -5.8 -5.3 -5.8 -5.3 -5.8 -5.3 -5.8 -5.3 -5.8 -5.3 -5.8 -5.3 -5.8 -5.3 -5.8 -5.3 -5.8 -5.3 -5.8 -5.3 -5.3 -5.3 -5.3 -5.3 -5.3 -5.3 -5.3 | Cent. 8.9 8.3 7.8 7.2 6.7 6.1 5.6 5.0 4.4 3.9 3.3 2.8 2.2 1.7 1.1 - 1.7 - 2.2 - 2.8 - 3.3 - 3.9 - 4.4 - 5.0 - 0.6 - 1.1 - 1.7 - 2.2 - 2.8 - 3.3 - 3.9 - 4.4 - 5.0 - 0.6 - 1.1 - 1.7 - 7.2 - 7.8 - 8.3 - 3.9 - 4.4 - 5.0 - 5.6 - 6.1 - 1.1 - 1.7 - 7.2 - 7.8 - 8.3 - 8.9 - 9.5 - 10.0 - 10.0 - 11.7 - 1.2 - 2.8 - 3.3 - 3.9 - 5.6 - 6.1 - 1.1 - 6.7 - 7.2 - 7.8 - 8.3 - 8.9 - 9.5 - 10.0 - 10.1 - 11.7 - 1.2 - 7.2 - 7.8 - 8.3 - 8.9 - 9.5 - 10.0 - 10.1 - 11.7 - 12.2 | Fahr. 7 6 5 4 3 2 1 0 -1 1 -2 -3 -4 -5 -6 -7 -8 -9 -10 -11 -12 -3 -4 -5 -6 -7 -8 -9 -10 -11 -12 -13 -4 -5 -6 -7 -8 -9 -10 -11 -12 -13 -14 -5 -6 -7 -8 -9 -10 -11 -12 -13 -14 -5 -6 -7 -8 -9 -10 -11 -12 -13 -14 -15 -16 -17 -17 -22 -23 -24 -25 -26 -27 -28 -20 -21 -22 -22 -23 -24 -25 -26 -27 -28 -29 -20 -21 -22 -22 -22 -22 -26 -27 -28 -26 -27 -28 -26 -27 -28 -26 -27 -28 -26 -27 -28 -27 -28 -27 -28 -27 -28 -27 -28 -27 -27 -28 -27 -27 -28 -27 -27 -28 -27 -27 -28 -27 -27 -28 -27 -27 -28 -27 -27 -28 -27 -20 -27 -27 -28 -27 -20 -27 -27 -28 -27 -27 -28 -27 -27 -28 -27 -27 -28 -27 -27 -28 -27 -27 -28 -27 -27 -28 -27 -27 -28 -27 -27 -28 -27 -30 -31 -31 -31 -31 -27 -28 -37 -37 -37 -37 -37 -37 -37 -37 | Réaum. - 11.1 - 11.6 - 12.0 - 12.4 - 12.9 - 13.3 - 13.8 - 14.2 - 14.7 - 15.1 - 15.6 - 16.0 - 16.4 - 16.9 - 17.3 - 17.8 - 18.2 - 18.7 - 19.1 - 19.6 - 20.0 - 20.4 - 20.9 - 21.3 - 21.8 - 22.2 - 22.7 - 23.1 - 23.6 - 24.0 - 24.4 - 24.9 - 25.3 - 25.8 - 26.2 - 26.7 - 27.6 - 28.0 | Cent. - 13.9 - 14.4 - 15.0 - 15.6 - 16.1 - 16.7 - 17.2 - 17.8 - 18.3 - 18.9 - 19.4 - 20.0 - 20.6 - 21.1 - 21.7 - 22.2 - 22.8 - 23.3 - 23.9 - 24.4 - 25.0 - 25.6 - 26.1 - 26.7 - 27.2 - 27.8 - 28.3 - 28.9 - 29.4 - 30.0 - 30.6 - 31.1 - 31.7 - 32.2 - 32.8 - 33.3 - 33.9 - 34.4 - 35.0 | | | | |

Comparative Table of Fahrenheit, Réaumur and Centigrade Degrees (Continued).

H.M.

To convert Fahrenheit degrees to Centigrade or Réaumur, subtract 32 and multiply the difference by $\frac{5}{9}$ or $\frac{4}{9}$ respectively. To convert Centigrade or Réaumur to Fahrenheit, multiply by $\frac{9}{5}$ or $\frac{9}{4}$, as the case may be, and add 32 to the product. To convert Centigrade to Réaumur, multiply Centigrade degrees by $\frac{4}{5}$; and to convert to Centigrade, multiply Réaumur degrees by $\frac{5}{4}$. To obtain absolute temperature, add 273° to the Centigrade scale.

Photometric Standards.

The British unit of light, the *candle power*, as originally defined,* is the illuminating power of a sperm candle $\frac{1}{8}$ inch in diameter (6 to the pound) burning 120 grains per hour. The Harcourt 10-candle power pentane lamp, however, is accepted by the Gas Referees as representing ten British candles.

The French unit, the *Carcel*, is the illuminating power of a lamp burning 42 grammes of pure colza oil per hour.

The German unit, the *Hefner*, is the illuminating power of the Hefner-Alteneck lamp, burning amyl-acetate with a cylindrical wick 8 mm. in diameter and a flame-height of 40 mm.

The International Congress, held at Paris in April, 1884, proposed the illuminating power of a square centimetre of molten platinum at the temperature of solidification as a unit; but at the Congress held in 1890 the 20th part of this unit was adopted as the international standard unit, under the name of the *decimal candle*.

The following relations between these lamps have been established by tests made in the German Reichsanstalt, at the instance of the International Committee on Photometry. The tests were made in air containing 8.8 litres of aqueous vapour per cubic metre of dry air, and under a barometric pressure of 760 mm. †

| Name of Lamp. | Harcourt Units (=10 British Candles). | Carcel Units. | Hefner Units. | Decimal Candles. | |
|---------------|--|------------------|------------------|---------------------|--|
| Harcourt, | I | I 02 | II | 9.8 | |
| Carcel, | .98 | I | 10.8 | 9.61 | |
| Hefner, | .091 | .093 | I | .891 | |

1 Decimal candle = .102 Harcourt units. = 1.02 British candles. = .104 Carcels.

= .104 Carcers.

= 1.122 Hefners.

* Metropolis Gas Act of 1860.

+ Journal für Gasbeleuchtung, Munich, 30 June, 1906, pp. 559-561.

PART III. DATA RELATING TO WATER.

SECTION I. CONSTANTS.

Relation of Weight and Volume.

THE Imperial Gallon is the volume of 10 avoir. lbs. of distilled water weighed *in air* against brass weights, with the water and air at a temperature of 62° Fahr., under a barometric pressure of 30 inches. The following constants apply to water under these conditions:*

| Weight of I cubic inch of water at (| 52° F. |
|--------------------------------------|--------------------|
| = 252.3253 grains. | log = 2.4019608 |
| =.0360465 lb. | $\log = 8.5568628$ |
| =.00360465 Imp. gallon. | $\log = 7.5568628$ |
| Weight of 1 cubic foot of water at 6 | 52° F. |
| = 62.2883 lbs. | log = 1.7944065 |
| = 6.22883 Imp. gallons. | $\log = 0.7944065$ |
| Volume of 1 short ton (2000 lbs.) c | of water at 62° F. |
| = 32.1088 cub. feet. | $\log = 1.5066235$ |
| Volume of 1 long ton (2240 lbs.) of | water at 62° F. |
| = 35.9618 cub. feet. | $\log = 1.5558415$ |
| I Imperial gallon | |
| = 277.420 cub. inches. | $\log = 2.4431372$ |
| =.160544 cub. foot. | log = 9.2055935 |

A column of water 1 foot high at 62° F. exerts a pressure of .4325 lb. per sq. inch: $\log = 9.6360419$.

A pressure of 1 lb. per sq. in. is exerted by a column of water at 62° F., 2.31184 feet high : $\log = 0.3639581$.

The Litre is the volume of a kilogram of distilled water weighed *in vacuo* at its temperature of maximum density * See page 7. $(4^{\circ}C. \text{ or } 39^{\circ}.2 \text{ F.})$. By means of the equivalents given on page 33, and the weight of a cubic decimetre of water on page 4, we find that

I gramme per cubic centimetre = 62.4278 lbs. per cubic foot; and the weight *in vacuo* of I cubic decimetre of distilled water at 4° C. = .999974 kilogram.

Therefore the weight *in vacuo* of 1 cubic foot of distilled water at 4° C. = $62.4278 \times .999974 = 62.4262$ lbs.

Constants used in the measurement of flow.

= 60 cubic feet per minute $\log = 1.7781513$ = 3600 cubic feet per hour $\log = 3.5563025$ = 86400 cubic feet per day of 24 hours $\log = 4.9365137$ = 6.22883 Imp. gallons per second $\log = 0.7944065$ = 373.73 Imp. gallons per minute $\log = 2.5725578$ = 22423.8 Imp. gallons per hour $\log = 4.3507090$ = 538170.9 Imp. gallons per day of $\log = 5.7309202$ = 7.48026 U.S. gallons per second $\log = 0.8739167$ = 448.816 U.S. gallons per minute log = 2.6520680= 26928.94 U.S. gallons per hour $\log = 4.4302192$ = 646294.4 U.S. gallons per day of $\log = 5.8104304$ 24 hours. I cubic foot per minute of water at 62°F. = 60 cubic feet per hour $\log = 1.7781513$ = 1440 cubic feet per day of 24 hours log = 3.1583625= 6.22883 Imp. gallons per minute $\log = 0.7944065$ = 373.73 Imp. gallons per hour $\log = 2.5725578$ = 8969.54 Imp. gallons per day $\log = 3.5927700$ 24 hours = 7.48026 U.S. gallons per minute $\log = 0.8739167$ $\log = 2.6520680$ =448.816 U.S. gallons per hour = $_{440.010}$ c.c. gallons per day of $\log = 4.0322792$

The *miner's inch* is usually taken to be a flow of 1.5 cubic feet per minute.

* 'Cusec' is the abbreviation of 'cubic foot per second,' commonly used in referring to the flow of water.

CONSTANTS

SECT. I.]

| | | 1 | 1 | | | | | | 1 | |
|----------|-------------|------------|------------|------------|------------|------------|------------|------------|-------------------|------------|
| Temp, C. | ·0 | •1 | •2 | •3 | •4 | •5 | •6 | •7 | ·8 | ·9 |
| 0° | 1.000127 | 120 066 | 114 061 | 108 | 102 | 096 | 091 | 086 | 080 | 075 |
| I 2 | 070 030 | 000 | 001 | 057 021 | 052 019 | 048 | 044 014 | 040 012 | 037 010 | 033 |
| 3 | 007 | 006 | 004 | 003 | 002 | 002 | 001 | 001 | 000 | 000 |
| 4 | 000 | 000 | 001 | 100 | 001 | 002 | 003 | 004 | 005 | 007 |
| 5 | 1.000008 | 010 | 012 | 014 | 016 | 018 | 020 | 023 | 026 | 029 |
| 6 | 032 | 035 | 038 | 041 | 045 | 049 | 053 | 057 | 061 | 065 |
| 78 | 069 | 074 128 | 079 | 084 | 089 | 094 | 099 160 | 105 | IIO | 116 181 |
| 9 | 122 189 | 128 | 134 204 | 141 211 | 147 219 | 154 227 | 235 | 167 244 | 174 252 | 181 260 |
| 10 | 1.000269 | 278 | 287 | 296 | - | | | | | |
| II | 363 | 373 | 383 | 394 | 305 405 | 314 415 | 324 426 | 334 437 | 343 448 | 353 459 |
| 12 | 471 | 482 | 494 | 505 | 517 | 529 | 541 | 553 681 | 566 | 578 |
| 13 | 591 | 603 | 616 | 629 | 642 | 655 | 668 | | 695 | 709 |
| 14 | 722 | 736 | 750 | 765 | 779 | 794 | 809 | 823 | 838 | 853 |
| 15 | 1.000868 | 884 | 899 | 914 | 930 | 945 | 961 | 977 | 993 | 009 |
| 16 | 1025 | 042 | 058 | 075 | 091 | 108 | 125 | 142 | 159 | 177 |
| 17 18 | 194 | 211 | 229 | 247 | 265 | 283 469 | 301 488 | 319 | 338 | 356 |
| 10 | 374 566 | 393 585 | 412 605 | 431 625 | 450 645 | 666 | 400 686 | 507 707 | 527 727 | 546 748 |
| 20 | 1.001768 | 789 | 810 | 831 | 852 | 874 | 895 | 916 | | 960 |
| 21 | 981 | 003 | 025 | 031 | 069 | 092 | 114 | 137 | <u>938</u> 159 | 182 |
| 22 | 2205 | 228 | 251 | 274 | 297 | 320 | 343 | 367 | 391 | 414 |
| 23 | 438 | 462 | 486 | 510 | 534 | 559 | 583 | 607 | 632 | 657 |
| 24 | 682 | 707 | 732 | 757 | 782 | 807 | 833 | 858 | 884 | 910 |
| 25 | 1.002935 | 961 | 987 | 014 | 040 | 066 | 092 | 119 | 146 | 172 |
| 26 | 3199 | 226 | 253 | 280 | 307 | 335 | 362 | 389 | 417 | 445 |
| 27 | .472 | 500 | 528 | 556 | 584 | 612 | 641 | 669 | 697 | 726 |
| 28 | 754 | 783 | 812 | 841 | 870 | 899 | 928 | 957 | 987 | 016 |
| 29 | 4045 | 075 | 105 | 134 | 164 | 194 | 224 | 254 | 284 | 315 |
| 30 | 1.004345 | 375 | 406 | 436 | 467 | 498 | 529 | 560 | 591 | 622 |
| 31 | 653 | 684 | 716 | 748 | 780 | 811 | 843 | 875 | 907 | <u>939</u> |
| 32 33 | 971 5297 | 003 330 | 036 363 | 068 396 | 101 430 | 133 463 | 166 497 | 199 520 | 231 564 | 264 597 |
| 33 | 631 | 665 | 699 | 733 | 767 | 403 801 | 835 | 530 870 | 904 | 939 |
| 35 | 1.005973 | 008 | 042 | 077 | 111 | 146 | 181 | 217 | 252 | 287 |

The volume in cubic centimetres at various temperatures from 0° to 35° Centigrade of a cubic centimetre of distilled water at 4° C.*

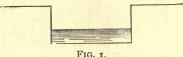
For 163° C. (62° F.) the volume is 1.001136.

* This table was compiled by Landolt and Börnstein from determinations made by Thiesen, Scheel and Marek. It is taken from the *Smithsonian Physical Tables*, Washington, 1906.

PART III.

SECTION II. MEASUREMENT OF THE FLOW OF WATER.

In measuring the flow of a stream by means of a rectangularnotched weir (Fig. 1), the length of the notch should be at least three times the depth of water on the sill. Air should have free access to the space behind the falling sheet of water, and the sill should be carefully levelled.



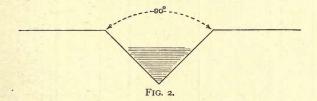
End contraction, which occurs when the weir at each end of the notch projects into the approach channel, diminishes the discharge. The contraction is complete, that is as great as it can be, when the distance from the end of the notch to the side of the approach channel is equal to the depth of water on the sill. If the width of the notch be not less than three times the depth of water on the sill, a complete end contraction diminishes the *effective width* of the notch by an amount equal to one-tenth of the depth of the water on the sill. If contraction occurs at both ends of the notch, the effective width will of course be diminished by twice the above amount.

The notches of weirs should be made preferably in thin sheet iron; if in wood, the *downstream* side should be bevelled off so as to present a smooth sharp edge to the water on the upstream side. In a wooden weir two inches thick, a notch cut with square edges (without bevel) gives a discharge $15\frac{1}{2}$ per cent. less than that of a similar notch in thin sheet iron. The weir can be made of deal boards with the notch cut in the wood, or a thin sheet iron plate with the notch can be attached to the topmost board. The weir site should be chosen at a point where the stream will be dammed back for at least six feet. The weir should be let into the banks and should be firmly fixed into

SECT. 11.] MEASUREMENT OF FLOW OF WATER 71

position and made water-tight by means of clay. Unless a proper approach channel is provided, the ends of the notch should be far enough from the banks to ensure complete end contraction, which must then be allowed for. No measurements should be made until the normal flow of the stream is passing through the notch. The depth of the water must not be measured on the notch itself, but from the sill to the surface of the still water at a point some six feet above the weir, a level being employed.

For gauging a small flow, a right-angled triangular notch (Fig. 2) will be found more convenient. It is the only form of notch in which the periphery always bears the same ratio to the cross-sectional area of the stream flowing through it.



On pages 72 and 73 are tables giving the discharges through each form of notch for a varying depth of water. In the first table, which is for a rectangular-notched weir in thin sheet iron,

Q = Discharge in 'cusecs' (cubic feet per second).

H= Depth in feet of water, measured from sill of notch to surface of still water above the weir.

L = Width in feet of notch.

 $Q=3.33 LH\sqrt{H}$ (Francis' formula).

The table is calculated for a notch I foot in width, and no deduction has been made for end contraction which is hardly appreciable when H is less than $\frac{L}{10}$. In using the table, multiply Q by the *effective* width of the notch in feet.

Table

| H | Q | H | 6 | H | Q | H | 6 | H | Q | | |
|------------|----------------|------------|----------------|--------------|----------------|--------------|----------------|--------------|------------------|--|--|
| .01 | 0.003 | .51 | 1.213 | 1.01 | 3.380 | 1.51 | 6.179 | 2.01 | 9.489 | | |
| .02 | 0.009 | .52 | 1.249 | I.02 | 3.430 | 1.52 | 6.240 | 2.02 | 9.560 | | |
| .03 | 0.017 | .53 | 1.285 | 1.03 | 3.481 | 1.53 | 6.302 | 2.03 | 9.631 | | |
| .04 | 0.027 | •54 | 1.321 | 1.04 | 3.532 | 1.54 | 6.364 | 2.04 | 9.703 | | |
| .05 | 0.037 | •55 | 1.358 | 1.05 | 3.583 | 1.55 | 6.426 | 2.05 | 9.774 | | |
| .06 | 0.049 | .56 | 1.395 | 1.06 | 3.634 | 1.56 | 6.488 | 2.06 | 9.846 | | |
| .07 | 0.062 | · 57 | 1.433 | 1.07 | 3.686 | 1.57 | 6.551 | 2.07 | 9.917 | | |
| .08 | 0.075 | .58 | 1.471 | 1.08 | 3.737 | 1.58 | 6.613 | 2.08 | 9.989 | | |
| .09 | 0.090 | .59 | 1.509 | 1.09 | 3.790 | 1.59 1.60 | 6.676 | 2.09 2.10 | 10.062 10.134 | | |
| .10 | 0.105 | .60 .61 | 1.548 | I.IO I.II | 3.842 | 1.61 | 6.739 6.803 | 2.10 | 10.134 | | |
| .11 | 0.121 0.138 | .62 | 1.586 1.626 | I.I2 | 3.894 3.947 | 1.62 | - 6.866 | 2.12 | 10.279 | | |
| .12 | 0.130 | .63 | 1.665 | 1.13 | 3.947 | 1.63 | 6.930 | 2.13 | 10.352 | | |
| .14 | 0.174 | .64 | 1.705 | I.14 | 4.053 | 1.64 | 6.994 | 2.14 | 10.425 | | |
| .15 | 0.193 | .65 | 1.745 | 1.15 | 4.107 | 1.65 | 7.058 | 2.15 | 10.498 | | |
| .16 | 0.213 | .66 | 1.786 | 1.16 | 4.160 | 1.66 | 7.122 | 2.16 | 10.571 | | |
| .17 | 0.233 | .67 | 1.826 | 1.17 | 4.214 | 1.67 | 7.187 | 2.17 | 10.645 | | |
| .18 | 0.254 | .68 | 1.867 | 1.18 | 4.268 | 1.68 | 7.251 | 2.18 | 10.718 | | |
| .19 | 0.276 | .69 | 1.909 | 1.19 | 4.323 | 1.69 | 7.316 | 2.19 | 10.792 | | |
| .20 | 0.298 | .70 | 1.950 | I.20 | 4.377 | 1.70 | 7.381 | 2.20 | 10.866 | | |
| .21 | 0.320 | .71 | 1.992 | 1.21 | 4.432 | 1.71 | 7.446 | 2.2I | 10.940 | | |
| .22 | 0.344 | .72 | 2.034 | 1.22 | 4.487 | I.72 | 7.512 | 2.22 | 11.015 | | |
| .23 | 0.367 | .73 | 2.077 | 1.23 | 4.543 | 1.73 | 7.577 | 2.23 | 11.089 | | |
| .24 | 0.392 | •74 | 2.120 | I.24 | 4.598 | 1.74 | 7.643 | 2.24 | 11.164 | | |
| .25 | 0.416 | .75 | 2.163 | 1.25 | 4.654 | 1.75 | 7.709 | 2.25 | 11.239 | | |
| .26 | 0.441 | .76 | 2.206 | 1.26 | 4.710 | 1.76 | 7.775 | 2.26 | 11.314 11.389 | | |
| .27 | 0:467 | ·77 .78 | 2,250 2,294 | I.27 I.28 | 4.766 | 1.77 1.78 | 7.842 7.908 | 2.28 | 11.369 | | |
| .20 | 0.493 | .79 | 2.294 | I.20 I.29 | 4.879 | 1.79 | 7.975 | 2.20 | 11.540 | | |
| .30 | 0.520 0.547 | .80 | 2.383 | I.30 | 4.936 | 1.80 | 8.042 | 2.30 | 11.615 | | |
| .31 | 0.575 | .81 | 2.428 | 1.31 | 4.993 | 1.81 | 8.109 | 2.31 | 11.691 | | |
| .32 | 0.603 | .82 | 2.473 | I.32 | 5.050 | 1.82 | 8.176 | 2.32 | 11.767 | | |
| .33 | 0.631 | .83 | 2.518 | 1.33 | 5.108 | 1.83 | 8.244 | 2.33 | 11.843 | | |
| •34 | 0.660 | .84 | 2.564 | 1.34 | 5.165 | 1.84 | 8.311 | 2.34 | 11.920 | | |
| .35 | 0.690 | .85 | 2.610 | 1.35 | 5.223 | 1.85 | 8.379 | 2.35 | 11.996 | | |
| .36 | 0.719 | .86 | 2.656 | 1.36 | 5.281 | 1.86 | 8.447 | 2.36 | 12.073 | | |
| .37 | 0.749 | .87 | 2.702 | 1.37 | 5.340 | 1.87 | 8.515 | 2.37 | 12.150 | | |
| .38 | 0.780 | .88 | 2.749 | 1.38 | 5.398 | 1.88 | 8.584 | 2.38 | 12.227 | | |
| •39 | 0.811 | .89 | 2.796 | 1.39 | 5.457 | 1.89 | 8.652 | 2.39 | 12.304 | | |
| •40 | 0.842 | .90 | 2.843 | 1.40 | 5.516 | 1.90 | 8.721 | 2.40 | 12.381 | | |
| •4I | 0.874 | .91 | 2.891 | I.4I | 5.575 | 1.91 | 8.790 8.859 | 2.4I 2.42 | 12.459 12.536 | | |
| •42 | 0.906 | .92 | 2.939 | I.42 | 5.635 | 1.92 1.93 | 8.929 | 2.42 | 12.530 | | |
| •43 | 0.939 | ·93 ·94 | 2.987 3.035 | I.43 | 5.694 5.754 | 1.93 1.94 | 8.998 | 2.43 | 12.692 | | |
| •44 •45 | 1.005 | .94 | 3.035 | I.44 I.45 | 5.814 | 1.94 | 9.068 | 2.44 | 12.770 | | |
| .46 | 1.039 | .95 | 3.132 | 1.45 | 5.875 | 1.95 | 9.138 | 2.46 | 12.848 | | |
| .47 | I.073 | .97 | 3.181 | 1.47 | 5.935 | 1.97 | 9.208 | 2.47 | 12.927 | | |
| .48 | 1.107 | .98 | 3.231 | 1.48 | 5.996 | 1.98 | 9.278 | 2.48 | 13.005 | | |
| .49 | I.I42 | .99 | 3.280 | 1.49 | 6.057 | 1.99 | 9.348 | 2.49 | 13.084 | | |
| .50 | 1.177 | 1.00 | 3.330 | 1.50 | 6.118 | 2.00 | 9.419 | 2.50 | 13.163 | | |
| | | | | | | | | 11 | | | |

Table for Estimating Discharge of Water through a Rectangularnotched Weir, without end contraction.

Table for Estimating Discharge of Water through a Right-angled Triangular Notch in Thin Sheet Iron.

Q = Discharge in cubic feet per minute.

- n = Head in inches measured from bottom of notch to surface of still water above weir.
- $Q = .306 \sqrt{n^5}$ (Thomson's formula).

The Table is calculated for heads from 1 to 15 inches, increasing by decimal parts of an inch. No deduction has to be made for end contraction.

| n | Q | n | Q | 12 | Q | n | 6 |
|------------|----------------|------------|------------------|--------------|--------------------|--------------|--------------------|
| I | .306 | 4.6 | 13.886 | 8.2 | 58.935 | 11.8 | 146.329 |
| I.I | .388 | 4.7 | 14.654 | 8.3 | 60.701 | 11.9 | 148.838 |
| I.2 | .480 | 4.8 | 15.446 | 8.4 | 62.577 | 12 | 151.032 |
| 1.3 | .589 | 4.9 | 16.263 | 8.5 | 64.574 | I2.I | 155.813 |
| 1.4 | .709 | 5 | 17.105 | 8.6 | 66.371 | 12.2 | 159.058 |
| 1.5 | .843 | 5.1 | 17.974 | 8.7 | 68.329 | 12.3 | 163.333 |
| 1.6 | .990 | 5.2 | 18.867 | 8.8 | 70.288 | 12.4 | 165.168 |
| 1.7 | 1.153 | 5.3 | 19.789 | 8.9 | 72.338 | 12.5 | 169.034 |
| 1.8 | 1.330 | 5.4 | 20.734 | 9 | 74.358 | 12.6 | 172.431 |
| 1.9 | 1.523 | 5.5 | 21.707 | 9.I | 77.662 | 12.7 | 175.858 |
| 2 | 1.731 | 5.6 | 22.708 | 9.2 | 78.550 | 12.8 | 179.346 |
| 2. I | 1.954 | 5.7 5.8 | 23.736 | 9.3 | 80.722 | 12.9 | 182.865 |
| 2.2 | 2.197 | 5.8 | 24.792 | 9.4 | 82.895 | 13 | 186.463 |
| 2.3 | 2.454 | 5.9 | 25.875 | 9.5 | 85.129 | 13.1 | 190.056 |
| 2.4 | 2.730 | 6 | 26.983 | 9.6 | 87.393 | 13.2 | 193.698 |
| 2.5 | 3.023 | 6. I | 28.121 | 9.7 | 89.688 | 13.3 | 197.400 |
| 2.6 | 3.338 | 6.2 | 29.290 | 9.8 | 92.014 | 13.4 | 201.103 |
| 2.7 | 3.665 | 6.3 | 30.483 | 9.9 | 94.370 | 13.5 | 204.897 |
| 2.8 | 4.014 | 6.4 | 31.701 | 10 | 96.787 | 13.6 | 208.692 |
| 2.9 | 4.384 | 6.5 | 32.956 | IO.I | 99.174 | 13.7 | 212.578 |
| 3 | 4.767 | 6.6 | 34.241 | 10.2 | 101.653 | 13.8 | 216.464 |
| 3.1 | 5.177 | 6.7 6.8 | 35.557 | 10.3 | 104.162 | 13.9 | 220.411 224.389 |
| 3.2 | 5.605 | | 36.903 | 10.4 | 106.702 | 14 | 224.309 |
| 3.3 | 6.055 | 6.9 | 38.280 39.688 | 10.5 10.6 | 109.303 | 14.1 | 232.498 |
| 3.4 | 6.523 | 7 | 41.095 | | 111.934 114.570 | 14.2 14.3 | 236.599 |
| 3.5 3.6 | 7.013 7.525 | 7.I 7.2 | 41.095 | 10.7 10.8 | 114.5/0 | 14.3 14.4 | 240.760 |
| 3.7 | 8.069 | 7.3 | 44.064 | 10.0 | 120.013 | 14.5 | 244.983 |
| 3.8 | 8.673 | 7.4 | 45.594 | 10.9 II | 122.797 | 14.5 | 249.206 |
| 3.9 | 9.192 | 7.5 | 45.594 | 11.1 | 125.582 | 14.7 | 253.521 |
| 4 | 9.192 | 7.6 | 48.745 | 11.2 | 128.458 | 14.8 | 257.835 |
| 4.I | 10.400 | 7.7 | 50.337 | 11.3 | 131.352 | 14.9 | 262.211 |
| 4.2 | 11.061 | 7.8 | 51.989 | 11.4 | 134.272 | 15 | 266.709 |
| 4.3 | 11.735 | 7.9 | 53.672 | 11.5 | 137.332 | | |
| 4.4 | 12.426 | 8 | 55.386 | 11.6 | 138.220 | | |
| 4.5 | 13.151 | 8.1 | 57.160 | 11.7 | 143.269 | 1.1.2.2 | |
| | | | | 1 | | | |

SECTION III. STORAGE OF WATER BY SMALL DAMS FOR MINING AND IRRIGATION PURPOSES.

Dimensions for Small Earthen Dams.

Mr. A. M. Strange* recommends the following dimensions for small earthen dams :

| Maximum height of Dam above Ground Level. | Height of top of Dam above High Flood Level. | | Upstream (or Reservoir side) Slope. | Downstream Slope. |
|--|--|-------|--|------------------------------------|
| | Feet. | Feet. | Ratio of Horizontal Wid to Vertical Height. | |
| 1. Under 8 feet, | 3 | 6 | $I\frac{1}{2}$ to I | I to I |
| 2. From 8 to 15 feet, - | 4 | 8 | 2 to I | I ¹ / ₂ to I |

The above dimensions only apply when the soil is of a suitable nature and the wall is well and compactly made on a site from which all vegetation has first been removed. A clay core is usually effective in preventing leakage. The by-wash or waste weir channel and the upstream face of the wall should be "pitched" with stone. The high flood level is the level of the maximum discharge over the waste weir in time of flood.

Flood Discharge Allowances for Waste Weir Channels.

The following table gives what should prove quite safe allowances for the widths of waste weirs required for ordinary small catchment or drainage areas.

| For catchment areas | Discharge per 250 acres of | Width of Waste Weir Channels required per 250 acres of catchment. | | | | |
|---------------------|-------------------------------|--|-------------|--|--|--|
| up to | catchment | ı ft. deep. | 2 ft. deep. | | | |
| 1 | 2 | 3 | 4 | | | |
| Acres. | Cubic feet per second. | Feet. | Feet. | | | |
| 640 | 75 | 31.5 | 10.3 | | | |
| 1280 | 70 | 29.5 | 9.6 | | | |
| 1920 | 66 | 27.7 | 9.06 | | | |
| 2560 | 62 | 26.0 | 8.5 | | | |
| 3200 | 59 | 24.8 | 8.0 | | | |

TABLE OF WASTE WEIR CHANNELS.

Note. In regard to the catchment area, take the figure entered in column I, which is the nearest greater than the one under consideration, and use the corresponding figures in columns 2-4. For

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catchments above 3200 acres (5 square miles), the discharges (*vide* column 2) should be reduced gradually.

Example. A catchment area of 1000 acres may be expected to produce a high-flood discharge of $(4 \times 70 =)280$ cubic feet per sec., which would require a waste weir channel flowing I foot deep to be $(4 \times 29.5 =)118$ feet wide; or a channel flowing 2 feet deep to be $(4 \times 9.6 =)38.4$ feet wide.

The tables on pp. 76, 77 will be found of use in calculating the amount of earthwork contained in the wall. The height of the wall should be taken at each change of slope in the contour of the site, also the distance between each height measurement. Then half the sum of the areas of two adjoining cross-sections multiplied by the distance *in feet* between them gives the contents in cubic feet of that portion of the wall.

The Relation of Rainfall to Irrigation.

| I inch | n rair | fall ov | eria | cre = 3630 c | ubic | feet of | water. |
|--------|--------|---------|------|--------------|------|-----------------|--------|
| 2 | " | •• | " | =7260 | " | " | ,, |
| 2.5 | ,, | • • | " | = 9075 | ,, | >> | " |
| 3 | • 7 | ,, | " | = 10890 | " | > 9 * | " |
| 4 | " | " | " | = 14520 | " | " | " |
| 7.13 | " | " | " | = 25882 | •• | >> | >> |

Therefore, water flowing at the rate of 1 cubic foot per second for 30 days (1 month) is equivalent to

a rainfall of I inch per month on 713 acres.

| ,, | ; ; | 2 | " | ,, | ,, | 356 | 37 |
|------|------|------|-----|----|----|-----|----|
| " | " | 2.5 | " | ,, | 37 | 285 | " |
| " | ,, | 3 | ,, | ,, | | 237 | |
| ,, . | , ,, | 4 | " | ,, | | 178 | ,, |
| " | " | 7.13 | ,,, | ,, | ,, | 100 | " |

It will be seen from the above table that a rainfall of $2\frac{1}{2}$ inches per month corresponds to the flow of 1 cubic foot per second (1 cusec) over 285 acres.

This is termed an 'irrigating duty' of 285 acres per cusec, which means that one cubic foot of water per second has to irrigate 285 acres.

The irrigating duty of water varies according to the climate, the nature of the soil, the class of crop and the method of cultivation.

An irrigating duty of

| 285 | acres | per | cusec | = | 9075 | cub. | ft. | per | acre | per | month | 1, |
|-----|-------|-----|-------|-----|-------|------|-----|-----|------|-----|-------|----|
| 250 | ,. | | ,, | = | 10345 | , | , | | ,, | | •, | |
| 200 | " | | ,, | = | 12931 | , | , | | ,, | | ,, | |
| 150 | " | | ,. | | 17242 | , | , | | ,, | | " | |
| 100 | ,, | | ,, | = : | 25863 | , | , | | ., | | ,, | |

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TABLE I.

Top width, 6 ft.; upstream slope, $1\frac{1}{2}$ to 1; downstream slope, 1 to 1.

| Height in Feet. | | | | CROSS SE | SECTIONAL AREA IN SQUARE FEET | ea in Squa | RE FEET. | | | |
|------------------------|--------|--------|--------|----------|-------------------------------|------------|----------|--------|--------|--------|
| 0 | 0.00 | 0.61 | 1.25 | 19.1 | 2.60 | 3.31 | 4.05 | 4.81 | 5.60 | 6.41 |
| I | 7.25 | 8.11 | 00.6 | 16.6 | 10.85 | 11.81 | 12.80 | 13.81 | 14.85 | 16.91 |
| 0 | 17.00 | 18.11 | 19.25 | 20.41 | 21.60 | 22.81 | 24.05 | 25.31 | 26.60 | 27.01 |
| 3 | 29.25 | 30.61 | 32.00 | 33.41 | 34.85 | 36.31 | 37.80 | 39.31 | 40.85 | 42.41 |
| 4 | 44.00 | 45.61 | 47.25 | 48.91 | 50.60 | 52.3I | 54.05 | 55.81 | 57.60 | 50.41 |
| 5 | 61.25 | 63.11 | 65.00 | 16.99 | 68.85 | 70.81 | 72.80 | 74.81 | 76.85 | 18.01 |
| 9 | 81.00 | 83.11 | 85.25 | 87.41 | 89.60 | 91.81 | 04.05 | 06.21 | 08.60 | TOO.01 |
| . 2 | 103.25 | 105.61 | 108.00 | 110.41 | 112.85 | 115.31 | 117.80 | 120.31 | 122.85 | 125.41 |
| 8 | 128.00 | 130.61 | 133.25 | 135.91 | 138.60 | 141.31 | 144.05 | 146.81 | 149.60 | 152.41 |
| Decimals of a Foot. | 0.0 | I.0 | 0.2 | 6.0 | 0.4 | 9.0 | 9.0 | 2.0 | 8.0 | 6.0 |

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[PART III.

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|---|----|
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| | BL |
| | < |
| 1 | E |

Top width, 8 ft. ; upstream slope, 2 to 1 ; downstream slope, $1\frac{1}{2}$

21.52 37.92 57.82 81.22 108.12 138.52 172.42 209.82 250.72 295.12 343.02 394.42 449.32 507.72 569.62 8.62 6.0 **7.52** 20.07 36.12 78.72 77.72 78.72 78.72 78.72 77.77 563.27 8.0 6.46 18.66 34.36 53.56 76.26 102.46 132.16 165.36 202.06 242.26 285.96 333.16 383.86 438.06 495.76 4.0 $\begin{array}{c} 1129.03\\ 1161.88\\ 161.88\\ 238.08\\ 2281.43\\ 3281.28\\ 3281.28\\ 3378.63\\ 3378.63\\ 3378.63\\ 550.68\\$ 5.43 17.28 32.63 51.48 99.68 CROSS SECTIONAL AREA IN SQUARE FEET. 9.0 4.44 15.94 30.94 49.44 71.44 96.94 158.44 194.44 194.44 194.44 276.94 323.44373.44426.94483.94544.44 2.0 $\begin{array}{c} 155.03\\ 190.68\\ 229.83\\ 272.48\\ 318.63\\ 368.28\\ 368.28\end{array}$ 3.48 14.63 29.28 47.43 69.08 94.23 122.88 421.43 478.08 538.23 0.4 2.56 13.36 27.66 45.46 66.76 91.56 119.86 151.66 186.96 225.76 268.06 313.86 363.16 363.16 415.96 472.26 532.06 0.3 26.07 43.52 64.47 88.92 88.92 116.87 148.32 183.27 221.72 263.67 309.12 358.07 410.52 466.47 525.92 12.12 1.67 0.2 405.12 460.72 519.82 145.02 179.62 217.72 259.32 304.42 24.52 41.62 62.22 86.32 113.92 353.02 0.82 IO.92 0.1 9.75 39.75 60.00 83.75 141.75 176.00 213.75 255.00 299.75 348.00 399.75 23.00 0.00 00'II 513.75 0.0 Decimals of a Foot. Height in Feet. 104000000 13 13 OH II

SECT. III.

to I.

77

The level of the waste weir should be from 5 to 6 feet below the level of the top of the wall.

Downstream slope = 2 to I.

 $=\frac{1}{2}$ the maximum height.

= 3 to I.

Upstream slope

Top width

general rule for dimensions of dams over 16 feet high is:

A

SECTION IV. FLOW OF WATER IN PIPES.

General Laws.—1. When the diameter and length are constant, the discharge varies directly as the square root of the head. Conversely, the head is directly as the square of the discharge.

2. When the head and length are constant, the discharge is directly as the 2.5th power of the diameter. Conversely, the diameter will vary as the 2.5th root of the discharge.

3. When the discharge and length are constant, the head will be inversely as the 5th power of the diameter. Conversely, the diameter will be inversely as the 5th root of the head.

4. When the head and diameter are constant, the discharge will be inversely as the square root of the length. Conversely, the length varies as the square of the discharge.

5. When the discharge and diameter are constant, the head is directly and simply as the length.

The hydraulic mean gradient corresponds to a straight line drawn between the points of intake and delivery of a pipe. No loss of effect will arise from the pipe following the contour of the ground as long as it keeps below the hydraulic mean gradient. If the pipe be carried over a hill which is above the hydraulic mean gradient but below the level of the intake, the first section, having a low head, must be of a greater diameter than the subsequent section, which has a greater head.

The sine of slope of the hydraulic mean gradient is the head divided by the length of the pipe.

The hydraulic mean depth, or mean radius, is the crosssectional area of the water divided by the length of the wetted perimeter of the pipe or channel; in a circular pipe running full it is equal to one-fourth the diameter $\binom{d}{4}$.

Except under considerable pressure, flowing water does not entirely fill the pipe, and yet if it be more than three-quarters full, the discharge is but slightly less than if it were full. This is due to the fact that the full circle does not give the maximum discharging velocity, which is attained when the pipe is filled to the level of the chord of an arc of $78\frac{1}{2}^{\circ}$. This gives an increase over the full circle of $9\frac{1}{2}$ per cent. in velocity, and

SECT. IV.] FLOW OF WATER IN PIPES

over $2\frac{1}{2}$ per cent. in discharge. The mean radius can therefore be safely taken as equal to $\frac{d}{4}$ when the pipe is more than three-quarters full.

Discharge in cubic feet per second = cross-sectional area of water in square feet × mean velocity in feet per second.

Cross-Sectional Areas and Capacities of Cylindrical Pipes of Various Diameters.

D = the diameter of the pipe in inches.

A = the cross-sectional area of the pipe in square feet; or the number of cubic feet in a length of 1 foot.

| Ď | A | D | A | D | А |
|-------------------------------|-------|---------------------------------|-------|--------------------------------|-------|
| 1/2 | .0014 | 10 <u>1</u> | .6013 | 2012 | 2.292 |
| I | .0055 | 11 | .6600 | 21 | 2.405 |
| 11 | .0123 | $II\frac{1}{2}$ | .7213 | 211 | 2.521 |
| 2 | .0218 | 12 | .7854 | 22 | 2.640 |
| 21/2 | .0341 | I2 ¹ / ₂ | .8522 | 22 ¹ / ₂ | 2.761 |
| 3 | .0491 | 13 | .9218 | 23 | 2.885 |
| 31 | .0668 | I 3 ¹ / ₂ | .9940 | 23 ¹ / ₂ | 3.012 |
| 4 | .0873 | 14 | 1.069 | 24 | 3.142 |
| 41 | .1104 | I41/2 | I.147 | 25 | 3.409 |
| 5 | .1363 | 15 | 1.227 | 26 | 3.687 |
| 51 | .1650 | 151 | 1.310 | 27 | 3.976 |
| 6 | .1964 | 16 | 1.396 | 28 | 4.276 |
| $6\frac{1}{2}$ | .2304 | 161/2 | 1.485 | 29 | 4.587 |
| 7 | .2673 | 17 | 1.576 | 30 | 4.909 |
| 71/2 | .3068 | 17 ¹ / ₂ | 1.670 | 31 | 5.241 |
| 8 | .3491 | 18 | 1.767 | 32 | 5.585 |
| 81 | .3941 | 181 | 1.867 | 33 | 5.940 |
| 9 | .4418 | 19 | 1.969 | 34 | 6.305 |
| 9 ¹ / ₂ | .4922 | 19 <u>1</u> | 2.074 | 35 | 6.681 |
| IO | •5454 | 20 | 2.182 | 36 | 7.069 |

Velocity.—Let v = the mean velocity in feet per second.

r = the hydraulic mean depth.

s =the sine of slope.

Then $v = C r^{\frac{2}{3}} s^{\frac{1}{2}}$.

Or v = the cube root of the square of $r \times$ the square root of $s \times$ the value of C in the table. C is a coefficient which varies according to the smoothness of the interior surface of the pipe or conduit; but which is not appreciably affected by differences in slope or diameter.

DATA RELATING TO WATER

PART III.

| Values of C. | |
|-----------------------------|---------|
| Asphalted wrought-iron pipe | = 170. |
| Plain " " " | = 160. |
| Cast-iron pipe, new, | = 1 30. |
| ", " in service, | = 104. |
| Lap-riveted pipe, | = 115. |
| Brick conduits, | = 110. |

Loss of Head in Friction

(1) is proportional to the length of the pipe,

(2) is increased by roughness of the interior surface of the pipe,

(3) decreases as the diameter of the pipe is increased,

(4) increases nearly as the square of the velocity,

(5) is independent of the pressure of the water.

These five laws may be expressed by the formula:

$$h' = f \frac{l}{d} \frac{v^2}{2g}$$

where h' = loss of head in friction in feet.

l =length of pipe in feet.

d = diameter of pipe in feet.

v = mean velocity in feet per second.

g = acceleration due to gravity = 32.19 feet per second.

f = a variable constant (see table).

 $\frac{v^2}{2g}$ = velocity head due to mean velocity of flow.

Values of f. (Mansfield Merriman.*)

| Diameter of Pipe | | V | elocity | in feet p | er secon | d | |
|------------------|------|------|---------|-----------|----------|------|------|
| in feet. | I | 2 | 3 | 4 | 6 | 10 | 15 |
| .05 | .047 | .041 | .037 | .034 | .031 | .029 | .028 |
| . I | .038 | .032 | .030 | .028 | .026 | .024 | .023 |
| .25 | .032 | .028 | .026 | .025 | .024 | .022 | .021 |
| .5 | .028 | .026 | .025 | .023 | .022 | .020 | .019 |
| .75 | .026 | .025 | .024 | .022 | .021 | .019 | .018 |
| I.0 | .025 | .024 | .023 | .022 | .020 | .018 | .017 |
| 1.25 | .024 | .023 | .022 | .021 | .019 | .017 | .016 |
| 1.5 | .023 | .022 | .021 | .020 | .018 | .016 | .015 |
| 1.75 | .022 | .021 | .020 | .018 | .017 | .015 | .014 |
| 2.0 | .021 | .020 | .019 | .017 | .016 | .014 | .013 |

* Treatise on Hydraulics, New York, 1904, p. 559.

Loss of Head in Curvature.

Let h'' = loss of head in curvature in feet. R = radius of curve in feet. $f_1 = a$ variable coefficient. Then $h'' = f_1 \frac{l}{d} \frac{v^2}{2\sigma}$

| 1/ | n | 111 | 20 | 01 | * | f_1 . |
|----|---|-----|----|----|---|---------|
| | | | | | | |
| | | | | | | |

| $\frac{R}{d}$ | 20 | IO | 5 | 3 | 2 | 1.5 | 1.0 |
|---------------|------|------|------|------|------|------|------|
| f_1 | .004 | .008 | .016 | .030 | .047 | .072 | .184 |

In laying down a permanent pipe-line, allowance should be made for incrustation, which reduces the effective diameter of a pipe by from $\frac{1}{2}$ to $1\frac{1}{2}$ inches. A small reduction in the size of a pipe makes a large reduction in the discharge. $\frac{1}{10}$ th increase in the diameter gives an increase of about 25%, and $\frac{1}{2}$ th about 50% in the discharge.

PART IV. DATA RELATING TO AIR AND STEAM.

SECTION I. AIR.

THE coefficient of expansion of air at constant pressure per 1 degree Centigrade = $\frac{1}{273}$ or .00366957 (Jolly).

The standard height of a mercury barometer is 29.922 inches or 760 millimetres.

The standard atmospheric pressure at sea-level and standard barometric pressure

= 14.706 lbs. per square inch = 1 atmosphere

= 1033.3 grammes per square centimetre.

The average atmospheric pressure at $\frac{1}{4}$ mile above sea-level

= 14.02 lbs. per sq. in.

| | | | | | | | | - |
|----|----|----------------|-------|---------|--------|------------|----|----|
| ,, | ,, | | ile a | bove se | ea-lev | el = 13.33 | >> | " |
| ,, | ,, | $\frac{3}{4}$ | ;, | •, | " | = 12.66 | ,, | ,, |
| " | ,, | Ι. | ,, | ,, | ,, | = I 2.02 | " | •, |
| ,, | " | 14 | | | ,, | = 11.42 | ,, | " |
| " | ,. | $I\frac{1}{2}$ | ,, | ,, | ,, | = 10 88 | ,, | ,, |
| ,, | | 2 | ,, | ., | "" | = 9.80 | ,, | ,, |

The pressure of one atmosphere (or 14.706 lbs. to the square inch) = that of a column of water at 62° F. 34 feet in height. This is therefore the maximum theoretical lift of a pump at sea-level.

One lb. of dry air at 0° C. (32° F.) has a volume of 12.39 cub. ft.

SECT, I.]

Pressure of Columns of Mercury and Water.*

Metric and British measures. Correct at o° C. for mercury and 4° C. for water.

| M | IETRIC MEAS | URE. | B | RITISH MEAS | URE. |
|---------------------|---------------------------------------|--|-----------------------|---------------------------------------|--|
| Cms. of Mercury. | Pressure in grammes per sq. cm. | Pressure in pounds per sq. inch. | Inches of Mercury. | Pressure in grammes per sq. cm. | Pressure in pounds per sq. inch. |
| I | 13.5956 | 0.193376 | I | 34.533 | 0.491174 |
| 2 | 27.1912 | 0.386752 | 2 | 69.066 | 0.982348 |
| 3 | 40.7868 | 0.580128 | 3 | 103.598 | 1.473522 |
| 4 | 54.3824 | 0.773504 | 4 | 138.131 | 1.964696 |
| 5 | 67.9780 | 0.966880 | 5 | 172.664 | 2.455870 |
| 6 | 81.5736 | 1.160256 | 6 | 207.197 | 2.947044 |
| 7 | 95.1692 | 1.353632 | 7 | 241.730 | 3.438218 |
| 8 | 108.7648 | 1.547008 | 8 | 276.262 | 3.929392 |
| 9 | 122.3604 | 1.740384 | 9 | 310.795 | 4.420566 |
| IO | 135.9560 | 1.933760 | ю | 345.328 | 4.911740 |
| Cms. of Water. | Pressure in grammes per sq. cm. | Pressure in pounds per sq. inch. | Inches of Water. | Pressure in grammes per sq. cm. | Pressure in pounds per sq. inch. |
| I | I | 0.0142234 | I | 2.54 | 0.036227 |
| 2 | 2 | 0.0284468 | 2 | 5.08 | 0.072255 |
| 3 | 3 | 0.0426702 | 3 | 7.62 | 0.108382 |
| 4 | 4 | 0.0568936 | 4° | 10.16 | 0.144510 |
| 5 | 5 - | 0.0711170 | 5 | 12.70 | 0.180637 |
| 6 | 6 | 0.0853404 | 6 | 15.24 | 0.216764 |
| 7 | 7 | 0.0995658 | 7 | 17.78 | 0.252892 |
| 8 | 8 | 0.1137872 | 8 | 20.32 | 0.289019 |
| 9 | 9 | 0.1280106 | 9 | 22.86 | 0.325147 |
| IO | ІО | 0.1422340 | 10 | 25.40 | 0.361274 |

SECTION II. STEAM.

The following table (from the *Smithsonian Physical Tables*) summarises the chief properties of steam for pressures ranging from 1 to 219 lbs. per square inch:

* Smithsonian Physical Tables, Washington, 1906, p. 119.

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84 DATA RELATING TO AIR AND STEAM [PART IV.

PROPERTIES OF STEAM.*

| Pressure in pounds per square inch. | Pressure in pounds per square foot. | Pressure in atmospheres. | Temp. in degrees Fahr. | Volume per pound in cubic feet. | Weight per cubic foot in pounds. | Heat of water per pound in B.T.U. | Internal latent heat per pound of steam in B.T.U. | External latent heat per pound of steam in B.T.U. | Total latent heat per pound of steam in B.T.U. | Total heat per pound of steam in B.T.U. |
|---|---|-----------------------------|---------------------------|---------------------------------------|--|---|--|--|---|---|
| 1 | 144 | 0.068 | 102.0 | 334.23 | 0.0030 | 70.1 | 980.6 | 62.34 | 1043. | 1113.0 |
| 2 | 288 | .136 | 126.3 | 173.23 | .0058 | 94.4 | 961.4 | 64.62 | 1026. | 1120.4 |
| 3 | 432 | .204 | 141.6 | 117.98 | .0085 | 109.9 | 949.2 | 66.58 | 1011. | 1127.0 |
| 4 | 576 | .272 | 153.1 | 89.80 | .0111 | 121.4 | 940.2 | 67.06 | 1007. | 1128.6 |
| 5 | 720 | .340 | 162.3 | 72.50 | .0137 | 130.7 | 932.8 | 67.89 | 1001. | 1131.4 |
| 6 | 864 | 0.408 | 170.1 | 61.10 | 0.0163 | 138.6 | 926.7 | 68.58 | 995.2 | 1133.8 |
| 7 | 1008 | .476 | 176.9 | 53.00 | .0189 | 145.4 | 921.3 | 69.18 | 990.5 | 1135.9 |
| 8 | 1152 | .544 | 182.9 | 46.60 | .0214 | 151.5 | 916.5 | 69.71 | 986.2 | 1137.7 |
| 9 | 1296 | .612 | 188.3 | 41.82 | .0239 | 156.9 | 912.2 | 70.18 | 982.4 | 1139.4 |
| 10 | 1440 | .680 | 193.2 | 37.80 | .0264 | 161.9 | 908.3 | 70.61 | 979.0 | 1140.9 |
| 11 | 1584 | 0.748 | 197.8 | 34.61 | 0.0289 | 166.5 | 904.8 | 70.99 | 975.8 | 1142.3 |
| 12 | 1728 | .816 | 202.0 | 31.90 | .0314 | 170.7 | 901.5 | 71.34 | 972.8 | 1143.5 |
| 13 | 1872 | .884 | 205.9 | 29.58 | .0338 | 174.7 | 898.4 | 71.68 | 970.0 | 1144.7 |
| 14 | 2016 | .952 | 209.5 | 27.59 | .0362 | 178.4 | 895.4 | 72.00 | 967.4 | 1145.9 |
| 15 | 2160 | 1.020 | 213.0 | 25.87 | .0387 | 181.9 | 892.7 | 72.29 | 965.0 | 1146.9 |
| 16 | 2304 | 1.088 | 216.3 | 24.33 | 0.0411 | 185.2 | 890.1 | 72.57 | 962.7 | 1147.9 |
| 17 | 2448 | .156 | 219.4 | 22.98 | .0435 | 188.4 | 887.6 | 72.82 | 960.4 | 1148.9 |
| 18 | 2592 | .224 | 222.4 | 21.78 | .0459 | 191.4 | 885.3 | 73.07 | 958.3 | 1149.8 |
| 19 | 2736 | .292 | 225.2 | 20.70 | .0483 | 194.3 | 883.1 | 73.30 | 956.3 | 1150.6 |
| 20 | 2880 | .360 | 227.9 | 19.72 | .0507 | 197.0 | 880.9 | 73.53 | 954.4 | 1151.4 |
| 21 | 3024 | 1.429 | 230.5 | 18.84 | 0.0531 | 199.7 | 878.8 | 73.74 | 952.6 | 1152.2 |
| 22 | 3168 | .497 | 233.0 | 18.03 | .0554 | 202.2 | 876.8 | 73.94 | 950.8 | 1153.0 |
| 23 | 3312 | .565 | 235.4 | 17.30 | .0578 | 204.7 | 874.9 | 74.13 | 949.1 | 1153.7 |
| 24 | 3456 | .633 | 237.7 | 16.62 | .0602 | 207.0 | 873.1 | 74.32 | 947.4 | 1154.4 |
| 25 | 3600 | .701 | 240.0 | 15.99 | .0625 | 209.3 | 871.3 | 74.51 | 945.8 | 1155.1 |
| 26 | 3744 | 1.769 | 242.2 | 15.42 | 0.0649 | 211.5 | 869.6 | 74.69 | 944.3 | 1155.8 |
| 27 | 3888 | .837 | 244.3 | 14.88 | .0672 | 213.7 | 867.9 | 74.85 | 942.8 | 1156.4 |
| 28 | 4032 | .905 | 246.3 | 14.38 | .0695 | 215.7 | 866.3 | 75.01 | 941.3 | 1157.1 |
| 29 | 4176 | .973 | 248.3 | 13.91 | .0619 | 217.8 | 864.7 | 75.17 | 939.9 | 1157.7 |
| 30 | 4320 | 2.041 | 250.2 | 13.48 | .0742 | 219.7 | 863.2 | 75.33 | 938.5 | 1158.3 |
| 31 | 4464 | 2.109 | 252. I | 13.07 | 0.0765 | 221.6 | 861.7 | 75.47 | 937.2 | 1158.8 |
| 32 | 4608 | .177 | 253.9 | 12.68 | .0788 | 223.5 | 860.3 | 75.61 | 935.9 | 1159.4 |
| 33 | 4752 | .245 | 255.7 | 12.32 | .0811 | 225.3 | 858.9 | 75.76 | 934.6 | 1159.9 |
| 34 | 4896 | .313 | 257.5 | 11.98 | .0835 | 227.1 | 857.5 | 75.89 | 933.4 | 1160.5 |
| 35 | 5040 | .381 | 259.2 | 11.66 | .0858 | 228.8 | 856.1 | 76.02 | 932.1 | 1161.0 |
| 36 | 5184 | 2.449 | 260.8 | 11.36 | 0.0881 | 230.5 | 854.8 | 76.16 | 931.0 | 1161.5 |
| 37 | 5328 | .517 | 262.5 | 11.07 | .0903 | 232.2 | 853.5 | 76.28 | 929.8 | 1162.0 |
| 38 | 5472 | .585 | 264.0 | 10.79 | .0926 | 233.8 | 852.3 | 76.40 | 928.7 | 1162.5 |
| 39 | 5616 | .653 | 265.6 | 10.53 | .0949 | 235.4 | 851.0 | 76.52 | 927.6 | 1162.9 |
| 40 | 5760 | .722 | 267.1 | 10.29 | .0972 | 236.9 | 849.8 | 76.63 | 926.5 | 1163.4 |
| 41 | 5904 | 2.789 | 268.6 | 10.05 | 0.0995 | 238.5 | 848.7 | 76.75 | 925.4 | 1163.9 |
| 42 | 6048 | .857 | 270.1 | 9.83 | .1018 | 239.9 | 847.5 | 76.86 | 924.4 | 1164.3 |
| 43 | 6192 | .925 | 271.5 | 9.61 | .1040 | 241.4 | 846.4 | 76.97 | 923.3 | 1164.7 |
| 44 | 6336 | .993 | 272.9 | 9.41 | .1063 | 242.9 | 845.2 | 77.07 | 922.3 | 1165.2 |
| 45 | 6480 | 3.061 | 274.3 | 9.21 | .1086 | 244.3 | 844.1 | 77.18 | 921.3 | 1165.6 |
| 46 | 6624 | 3.129 | 275.6 | 9.02 | 0.1108 | 245.6 | 843.1 | 77.29 | 920.4 | 1166.0 |
| 47 | 6768 | .197 | 277.0 | 8.84 | .1131 | 247.0 | 842.0 | 77.39 | 919.4 | 1166.4 |
| 48 | 6912 | .265 | 278.3 | 8.67 | .1153 | 248.3 | 841.0 | 77.49 | 918.5 | 1166.8 |
| 49 | 7056 | .333 | 279.6 | 8.50 | .1176 | 249.7 | 840.0 | 77.58 | 917.5 | 1167.2 |

* From the Smithsonian Physical Tables, Washington, 1904 : based on a Table by Dwelshauvers-Dery (Trans. Am. Soc. Mech. Eng., vol. xi.).

| S | ECT. 11. | | | | STEAN | M | | | | 85 |
|---|---|-----------------------------|---------------------------|---------------------------------------|--|---|--|--|---|---|
| Pressure in pounds per square inch. | Pressure in pounds per square foot. | Pressure in atmospheres. | Temp. in degrees Fahr. | Volume per pound in cubic feet. | Weight per cubic foot in pounds. | Heat of water per pound in B.T.U. | Internal latent heat per pound of steam in B.T.U. | External latent heat per pound of steam in B.T.U. | Total latent heat per pound of steam in B.T.U. | Total heat per pound of steam in B.T.U. |
| 50 | 7200 | 3.401 | 280.8 | 8.34 | 0.1198 | 251.0 | 839.0 | 77.67 | 916.6 | 1167.6 |
| 51 | 7344 | .469 | 282.1 | 8.19 | .1221 | 252.2 | 838.0 | 77.76 | 915.7 | 1168.0 |
| 52 | 7488 | .537 | 283.3 | 8.04 | .1243 | 253.5 | 837.0 | 77.85 | 914.9 | 1168.3 |
| 53 | 7632 | .605 | 284.5 | 7.90 | .1266 | 254.7 | 836.0 | 77.94 | 914.0 | 1168.7 |
| 54 | 7776 | .673 | 285.7 | 7.76 | .1288 | 256.0 | 835.1 | 78.03 | 913.1 | 1169.1 |
| 55 | 7920 | 3.741 | 286.9 | 7.63 | 0.1310 | 257.1 | 834.2 | 78.12 | 912.3 | 1169.4 |
| 56 | 8064 | .801 | 288.1 | 7.50 | .1333 | 258.3 | 833.2 | 78.21 | 911.5 | 1169.8 |
| 57 | 8208 | .878 | 289.2 | 7.38 | .1355 | 259.5 | 832.3 | 78.29 | 910.6 | 1170.1 |
| 58 | 8352 | .946 | 290.3 | 7.26 | .1377 | 260.7 | 831.5 | 78.37 | 909.8 | 1170.5 |
| 59 | 8496 | 4.014 | 291.4 | 7.14 | .1400 | 261.8 | 830.6 | 78.45 | 909.0 | 1170.8 |
| 60 | 8640 | 4.082 | 292.5 | 7.03 | 0.1422 | 262.9 | 829.7 | 78.53 | 908.2 | 1171.2 |
| 61 | 8784 | .150 | 293.6 | 6.92 | .1444 | 264.0 | 828.9 | 78.61 | 907.5 | 1171.5 |
| 62 | 8928 | .218 | 294.7 | 6.82 | .1466 | 265.1 | 828.0 | 78.68 | 906.7 | 1171.8 |
| 63 | 9072 | .286 | 295.7 | 6.72 | .1488 | 266.1 | 827.2 | 78.76 | 905.9 | 1172.1 |
| 64 | 9216 | .354 | 296.7 | 6.62 | .1511 | 267.2 | 826.4 | 78.83 | 905.2 | 1172.4 |
| 65 | 9360 | 4.422 | 297.8 | 6.52 | 0.1533 | 268.3 | 825.6 | 78.90 | 904.5 | 1172.8 |
| 66 | 9504 | .490 | 298.8 | 6.43 | .1555 | 269.3 | 824.8 | 78.97 | 903.7 | 1173.1 |
| 67 | 9648 | .558 | 299.8 | 6.34 | .1577 | 270.4 | 824.0 | 79.04 | 903.1 | 1173.4 |
| 68 | 9792 | .626 | 300.1 | 6.25 | .1599 | 271.4 | 823.2 | 79.11 | 902.3 | 1173.7 |
| 69 | 9936 | .694 | 301.8 | 6.17 | .1621 | 272.4 | 822.4 | 79.18 | 901.6 | 1174.0 |
| 70 | 10080 | 4.762 | 302.7 | 6.09 | 0.1643 | 273.4 | 821.6 | 79.25 | 900.9 | 1174.3 |
| 71 | 10224 | .830 | 303.7 | 6.00 | .1665 | 274.3 | 820.9 | 79.32 | 900.2 | 1174.6 |
| 72 | 10368 | .898 | 304.6 | 5.93 | .1687 | 275.3 | 820.1 | 79.39 | 899.5 | 1174.9 |
| 73 | 10512 | .966 | 305.5 | 5.85 | .1709 | 276.3 | 819.4 | 79.46 | 898.8 | 1175.1 |
| 74 | 10656 | 5.034 | 306.5 | 5.78 | .1731 | 277.2 | 818.7 | 79.53 | 898.1 | 1175.4 |
| 75 | 10800 | 5.102 | 307.4 | 5.70 | 0.1753 | 278.2 | 817.9 | 79.59 | 897.5 | 1175.7 |
| 76 | 10944 | .170 | 308.3 | 5.63 | .1775 | 279.1 | 817.2 | 79.65 | 896.9 | 1176.0 |
| 77 | 11088 | .238 | 309.2 | 5.57 | .1797 | 280.0 | 816.5 | 79.71 | 896.2 | 1176.2 |
| 78 | 11232 | .306 | 310.1 | 5.50 | .1818 | 280.9 | 815.8 | 79.77 | 895.6 | 1176.5 |
| 79 | 11376 | .374 | 310.9 | 5.43 | .1840 | 281.8 | 815.1 | 79.83 | 895.0 | 1176.8 |
| 80 | 11520 | 5.442 | 311.8 | 5.37 | 0.1862 | 282.7 | 814.4 | 79.89 | 894.3 | 1177.0 |
| 81 | 11664 | .510 | 312.7 | 5.31 | .1884 | 283.6 | 813.8 | 79.95 | 893.7 | 1177.3 |
| 82 | 11808 | .578 | 313.5 | 5 25 | .1906 | 284.5 | 813.0 | 80.01 | 893.1 | 1177.6 |
| 83 | 11952 | .646 | 314.4 | 5.19 | .1928 | 285.3 | 812.4 | 80.07 | 892.5 | 1177.8 |
| 84 | 12096 | .714 | 315.2 | 5.13 | .1949 | 286.2 | 811.7 | 80.13 | 891.9 | 1178.0 |
| 85 | 12240 | 5.782 | 316.0 | 5.07 | 0.1971 | 287.0 | 811.1 | 80.19 | 891.3 | 1178.3 |
| 86 | 12384 | .850 | 316.8 | 5.02 | .1993 | 287.9 | 810.4 | 80.25 | 890.7 | 1178.6 |
| 87 | 12528 | .918 | 317.6 | 4.96 | .2015 | 288.7 | 809.8 | 80.30 | 890.1 | 1178.9 |
| 88 | 12672 | .986 | 318.4 | 4.91 | .2036 | 289.5 | 809.2 | 80.35 | 889.5 | 1179.0 |
| 89 | 12816 | 6.054 | 319.2 | 4.86 | .2058 | 290.4 | 808.5 | 80.40 | 888.9 | 1179.3 |
| 90 | 12960 | 6.122 | 320.0 | 4.81 | 0.2080 | 291.2 | 807.9 | 80.45 | 888.4 | 1179.5 |
| 91 | 13104 | .190 | 320.8 | 4.76 | .2102 | 292.0 | 807.3 | 80.50 | 887.8 | 1179.8 |
| 92 | 13248 | .258 | 321.6 | 4.71 | .2123 | 292.8 | 806.7 | 80.56 | 887.2 | 1180.0 |
| 93 | 13392 | .327 | 322.4 | 4.66 | .2145 | 293.6 | 806.1 | 80.61 | 886.7 | 1180.3 |
| 94 | 13536 | .396 | 323.1 | 4.62 | .2166 | 294.3 | 805.5 | 80.66 | 886.1 | 1180.5 |
| 95 | 13680 | 6.463 | 323.9 | 4.57 | 0.2188 | 295.1 | 804.9 | 80.71 | 885.6 | 1180.7 |
| 96 | 13824 | .531 | 324.6 | 4.53 | .2209 | 295.9 | 804.3 | 80.76 | 885.0 | 1180.9 |
| 97 | 13968 | .599 | 325.4 | 4.48 | .2231 | 296.7 | 803.7 | 80.81 | 884.5 | 1181.2 |
| 98 | 14112 | .667 | 326.1 | 4.44 | .2252 | 297.4 | 803.1 | 80.86 | 884.0 | 1181.4 |
| 99 | 14256 | .735 | 326.8 | 4.40 | .2274 | 298.2 | 802.5 | 80.91 | 883.4 | 1181.6 |

| 0 | 6 |
|---|---|
| 0 | 0 |

DATA RELATING TO AIR AND STEAM [PART IV.

| | | | | | | | | | - | |
|---|---|-----------------------------|---------------------------|---------------------------------------|--|---|--|--|---|---|
| Pressure in pounds per square inch. | Pressure in pounds per square foot. | Pressure in atmospheres. | Temp. in degrees Fahr. | Volume per pound in cubic feet. | Weight per cubic foot in pounds. | Heat of water per pound in B.T.U. | Internal latent heat per pound of steam in B.T.U. | External latent heat per pound of steam in B.T.U. | Total latent heat per pound of steam in B.T.U. | Total heat per pound of steam in B.T.U. |
| 100 | 14400 | 6.803 | 327.6 | 4.356 | 0.2295 | 298.9 | 802.0 | 80.95 | 882.9 | 1181.8 |
| 101 | 14544 | .871 | 328.3 | .316 | .2317 | 299.7 | 801.4 | 81.00 | 882.4 | 1182.1 |
| 102 | 14688 | .939 | 329.0 | .276 | .2338 | 300.4 | 800 8 | 81.05 | 881.9 | 1182.3 |
| 103 | 14832 | 7.007 | 329.7 | .237 | .2360 | 301.1 | 800.3 | 81.10 | 881.4 | 1182.5 |
| 104 | 14976 | .075 | 330.4 | .199 | .2381 | 301.9 | 799.7 | 81.14 | 880.8 | 1182.7 |
| 105 | 15120 | 7.143 | 331.1 | 4.161 | 0.2403 | 302.6 | 799.2 | 81.18 | 880.3 | 1182.9 |
| 106 | 15264 | .211 | 331.8 | .125 | .2424 | 303.3 | 798.6 | 81.23 | 879.8 | 1183.1 |
| 10 7 | 15408 | .279 | 332.5 | .088 | .2446 | 304.0 | 798.1 | 81.27 | 879.3 | 1183.4 |
| 108 | 15552 | .347 | 333.2 | .053 | .2467 | 304.7 | 797.5 | 81.31 | 878.8 | 1183.6 |
| 109 | 15696 | .415 | 333.8 | .018 | .2489 | 305.4 | 797.0 | 81.36 | 878.3 | 1183.8 |
| 110 | 15840 | 7.483 | 334.5 | 3.984 | 0.2510 | 306.1 | 796.5 | 81.41 | 877.9 | 1184.0 |
| 111 | 15984 | .551 | 335.2 | .950 | .2531 | 306.8 | 795.9 | 81.45 | 877.4 | 1184.2 |
| 112 | 16128 | .619 | 335.8 | .917 | .2553 | 307.5 | 795.4 | 81.50 | 876.9 | 1184.4 |
| 113 | 16272 | .687 | 336.5 | .885 | .2574 | 308.2 | 794.9 | 81.54 | 876.4 | 1184.6 |
| 114 | 16416 | .757 | 337.2 | .853 | .2596 | 308.8 | 794.4 | 81.58 | 875.9 | 1184.8 |
| 115 | 16560 | 7.823 | 337.8 | 3.821 | 0.2617 | 309.5 | 793.8 | 81.62 | 875.5 | 1185.0 |
| 116 | 16704 | .891 | 338.5 | .790 | .2638 | 310.2 | 793.3 | 81.66 | 875.0 | 1185.2 |
| 117 | 16848 | .959 | 339.1 | .760 | .2660 | 310.8 | 792.8 | 81.70 | 874.5 | 1185.4 |
| 118 | 16992 | 8.027 | 339.7 | .730 | .2681 | 311.5 | 792.3 | 81.74 | 874.1 | 1185.6 |
| 119 | 17136 | .095 | 340.4 | .700 | .2702 | 312.1 | 791.8 | 81.78 | 873.6 | 1185.7 |
| 120 | 17280 | 8.163 | 341.0 | 3.671 | 0.2724 | 312.8 | 791.3 | 81.82 | 873.2 | 1185.9 |
| 121 | 17424 | .231 | 341.6 | .643 | .2745 | 313.4 | 790.8 | 81.86 | 872.7 | 1186.1 |
| 122 | 17568 | .299 | 342.2 | .615 | .2766 | 314.1 | 790.3 | 81.90 | 872.2 | 1186.3 |
| 123 | 17712 | .367 | 342.8 | .587 | .2787 | 314.7 | 789.9 | 81.94 | 871.8 | 1186.5 |
| 124 | 17856 | .435 | 343.5 | .560 | .2809 | 315.3 | 789.4 | 81.98 | 871.4 | 1186.7 |
| 125 | 18000 | 8.503 | 344.1 | 3.534 | 0.2830 | 316.0 | 788.9 | 82.02 | 870.9 | 1186.9 |
| 126 | 18144 | .571 | 344.7 | .507 | .2851 | 316.6 | 788.4 | 82.06 | 870.5 | 1187.1 |
| 127 | 18288 | .639 | 345 3 | .481 | .2872 | 317.2 | 787.9 | 82.09 | 870.0 | 1187.2 |
| 128 | 18432 | .708 | 345.9 | .456 | .2893 | 317.8 | 787.5 | 82.13 | 869.6 | 1187.4 |
| 129 | 18576 | .776 | 346.5 | .431 | .2915 | 318.4 | 787.0 | 82.17 | 869.2 | 1187.6 |
| 130 | 18720 | 8.844 | 347.1 | 3.406 | 0.2936 | 319.0 | 786.5 | 82.21 | 868.7 | 1187.8 |
| 131 | 18864 | .912 | 347.6 | .382 | .2957 | 319.7 | 786.1 | 82.25 | 868.3 | 1188.0 |
| 132 | 19008 | .980 | 348.2 | .358 | .2978 | 320.3 | 785.6 | 82.28 | 867.9 | 1188.1 |
| 133 | 19152 | 9.048 | 348.8 | .334 | .2999 | 320.9 | 785.1 | 82.32 | 867.5 | 1188.3 |
| 134 | 19296 | .116 | 349.4 | .310 | .3021 | 321.5 | 784.7 | 82.35 | 867.0 | 1188.3 |
| 135 | 19440 | 9.184 | 349.9 | 3.287 | 0.3042 | 322. I | 784.2 | 82.38 | 866.6 | 1188.7 |
| 136 | 19584 | .252 | 350.5 | .265 | .3063 | 322.6 | 783.8 | 82.42 | 866.2 | 1188.8 |
| 137 | 19728 | .320 | 351.1 | .424 | .3084 | 323.2 | 783.3 | 82.45 | 865.8 | 1189.0 |
| 138 | 19872 | .388 | 351.6 | .220 | .3105 | 323.8 | 782.9 | 82.49 | 865.4 | 1189.2 |
| 139 | 20016 | .456 | 352.2 | .199 | .3126 | 324.4 | 782.4 | 82.52 | 865.0 | 1189.4 |
| 140 | 20160 | 9.524 | 352.8 | 3.177 | 0.3147 | 325.0 | 782.0 | 82.56 | 864.6 | 1189.5 |
| 141 | 20304 | .592 | 353·3 | .156 | .3168 | 325.5 | 781.6 | 82.59 | 864.2 | 1189.7 |
| 142 | 20448 | .660 | 353·9 | .135 | .3190 | 326.1 | 781.1 | 82.63 | 863.8 | 1189.9 |
| 143 | 20592 | .728 | 354·4 | .115 | .3211 | 326.7 | 780.7 | 82.66 | 863.4 | 1190.0 |
| 144 | 20736 | .796 | 355·0 | .094 | .3232 | 327.2 | 780.3 | 82.69 | 863.0 | 1190.2 |
| 145 | 20880 | 9.864 | 355.5 | 3.074 | 0.3253 | 327.8 | 779.8 | 82.72 | 862.6 | 1190.4 |
| 146 | 21024 | .932 | 356.0 | .054 | .3274 | 328.4 | 779.4 | 82.75 | 862.2 | 1190.5 |
| 147 | 21168 | 10.000 | 356.6 | .035 | .3295 | 328.9 | 779.0 | 82.79 | 861.8 | 1190.7 |
| 148 | 21312 | .068 | 357.1 | .016 | .3316 | 329.5 | 778.6 | 82.82 | 861.4 | 1190.9 |
| 149 | 21456 | .136 | 357.6 | .997 | .3337 | 330.0 | 778.1 | 82.86 | 861.0 | 1191.0 |

| and the second | | | | | | | | | | |
|---|---|----------------------------|----------------------------|---------------------------------------|--|---|--|--|--|---|
| er . | . er | ý | i | Volume per pound in cubic feet. | c | in | latent pound in | External latent heat per pound of steam in B.T.U. | tent pound t in | Total heat per pound of steam in B.T.U. |
| Pressure in pounds per square inch. | Pressure in pounds per square foot. | Pressure in atmospheres | l'emp. in degrees Fahr. | Volume per pound in cu feet. | Weight per cubic foot in pounds. | Heat of water per pound in B.T.U. | r pc | r po | Total latent heat per pour of steam in B.T.U. | Total heat pound of sto in B.T.U. |
| oun | oun | ssur | np. | um . | ght ic fo | pour U. | Internal heat per of steam B.T.U. | erne t pe | u.U. | nd bu |
| Pres | Pres in p | Pre | deg | Volu pour feet. | Wei cubi | Hea B.T | Inte beat of st B. T | Ext heat of st B.T | Tot: heat of si B. T | Tot: pour |
| | | | | | | | | | | |
| 150 | 21600 | 10.204 | 358.2 | 2.978 | 0.3358 | 330.6 | 777.7 | 82.89 | 860.6 | 1191.2 |
| 151 | 21744 | .272 | 358.7 | .960 | .3379 | 331.1 | 777.3 | 82.92 | 860.2 | 1191.3 |
| 152 | 21888 | .340 | 359.2 | ·941 | .3400 | 331.6 | 776.9 | 82.95 | 859.9 | 1191.5 |
| 153 154 | 22032 22176 | .408 .476 | 359.7 | .923 | .3421 .3442 | 332.2 332.7 | 776.5 776.1 | 82.98 83.01 | 859.5 859.1 | 1191.7 1191.8 |
| 155 | | | 1 | 2.888 | | | | | | |
| 156 | 22320 22464 | 10.544 .612 | 360.7 | .871 | 0.3462 .3483 | 333.2 333.8 | 775.7 775.3 | 83.04 | 858.7 858.3 | 1192.0 1192.1 |
| 157 | 22608 | .680 | 361.3 361.8 | .854 | .3504 | 334.3 | 774.9 | 83.10 | 858.0 | 1192.3 |
| 158 | 22752 | .748 .816 | 362.3 | .837 | .3525 | 334·3 334·8 | 774.5 | 83.13 | 857.6 | 1192.4 |
| 159 | 22896 | | 362.8 | .820 | .3546 | 335.3 | 774.1 | 83.16 | 857.2 | 1192.6 |
| 160 | 23040 | 10.884 | 363.3 363.8 | 2.803 | 0.3567 | 335.9 | 773.7 | 83.19 | 856.9 | 1192.7 |
| 161 162 | 23184 23328 | .952 11.020 | 303.8 | .787 .771 | .3588 .3609 | 336.4 336.9 | 773.3 | 83.22 83.25 | 856.5 856.1 | 1192.9 1193.0 |
| 163 | 23472 | .088 | 364.3 364.8 | .755 | .3630 | 337.4 | 772.5 | 83.28 | 855.8 | 1193.2 |
| 164 | 23616 | .157 | 365.3 | .739 | .3650 | 337.9 | 772.1 | 83.31 | 855.4 | 1193.3 |
| 165 | 23760 | 11.225 | 365.7 | 2.724 | 0.3671 | 338.4 | 771.7 | 83.34 | 855.1 | 1193.5 |
| 166 | 23904 | .293 | 366.2 | .708 | .3692 | 338.9 | 771.3 | 83.37 | 854.7 | 1193.6 |
| 167 168 | 24048 24192 | .361 | 366.7 367.2 | .693 .678 | .3713 | 339.4 | 771.0 | 83.39 | 854.3 | 1193.8 |
| 169 | 24192 | ·429 ·497 | 367.7 | .663 | ·3734 ·3754 | 339.9 340.4 | 770.6 | 83.42 83.45 | 854.0 853.6 | 1193.9 1194.1 |
| 170 | 24480 | 11.565 | 368.2 | 2.649 | 0.3775 | 340.9 | 769.8 | 83.48 | 853.3 | 1194.2 |
| 171 | 24624 | .633 | 368.6 | .634 | .3796 | 341.4 | 769.4 | 83.51 | 852.9 | 1194.2 |
| 172 | 24768 | .701 | 369.1 | .620 | .3796 .3817 .3838 | 341.9 | 769.1 | 83.54 | 852.6 | 1194.5 |
| 173 | 24912 | .769 | 369.6 | .606 | .3838 | 342.4 | 768.7 | 83.56 | 852.2 | 1194.7 |
| 174 175 | 25056 | .837 | 370.0 | .592 | .3858 | 342.9 | 768.3 | 83.59 | 851.9 | 1194.8 |
| 175 | 25200 25344 | 11.905 •973 | 370.5 371.0 | 2.578 .564 | 0.3879 | 343·4 343·9 | 767.9 | 83.62 83.64 | 851.6 851.2 | 1194.9 1195.1 |
| 177 | 25488 | 12.041 | 371.4 | .550 | .3921 | | 767.2 | 83.67 | 850.9 | 1195.2 |
| 178 | 25632 | .109 | 371.9 | ·537 | .3942 | 344·3 344·8 | 766.8 | 83.70 | 850.5 | 1195.4 |
| 179 | 25776 | .177 | 372.4 | .524 | .3962 | 345.3 | 766.5 | 83.73 | 850.2 | 1195.5 |
| 180 | 25920 | 12.245 | 372.8 | 2.510 | 0.3983 | 345.8 | 766.1 | 83.75 | 849 9 | 1195.6 |
| 181 182 | 26064 26208 | ·313 ·381 | 373.3 | ·497 .485 | .4004 | 346.3 | 765.8 | 83.77 83.80 | 849.5 | 1195.8 |
| 183 | 26352 | .301 | 373.7 | .405 | .4025 | 340.7 | 765.0 | 83.83 | 849.2 848.9 | 1195.9 1196.1 |
| 184 | 26496 | .517 | 374.6 | .459 | .4066 | 347.7 | 764.7 | 83.86 | 848.5 | 1196.2 |
| 185 | 26640 | 12.585 | 375.1 | 2.447 | 0.4087 | 348.1 | 764.3 | 83.88 | 848.2 | 1196.3 |
| 186 | 26784 | .653 | 375.5 376.0 | •434 | .4108 | 348.6 | 764.0 | 83.90 | 847.9 | 1196.5 |
| 187 188 | 26928 | .721 .789 | 376.0 | .422 | .4129 | 349.1 | 763.6 | 83.92 | 847.5 | 1196.6 |
| 189 | 27216 | .857 | 376.8 | .410 .398 | .4150 | 349.5 350.0 | 763.3 | 83.95 83.97 | 847.2 846.9 | 1196.7 |
| 190 | 27360 | 12.925 | 377.3 | 2.386 | 0.4191 | 350.4 | 762.6 | 83.99 | 846.6 | 1197.0 |
| 191 | 27504 | .993 | 377.7 | .374 | .4212 | 350.9 | 762.2 | 84.02 | 846.3 | 1197.1 |
| 192 | 27648 | 13.061 | 377.7 378.2 | .362 | .4233 | 351.3 | 761.9 | 84.04 | 845.9 | 1197.3 |
| 193 194 | 27792 27936 | .129 | 378.6 | .351 | .4254 | 351.8 | 761.6 | 84.06 | 845.6 | 1197.4 |
| 194 | 27930 | | 379.0 | •339 | .4275 | 352.2 | 1 | 84.08 | 845.3 | 1197.5 |
| 196 | 28080 | 13.265 | 379.4 | 2.328 | 0.4296 | 352.7 353.1 | 760.9 | 84.10 | 845.0 844.7 | 1197.7 1197.8 |
| 197 | 28368 | .401 | 380.3 | .306 | .4310 | 353.6 | 760.2 | 84.16 | 844.4 | 1197.9 |
| 198 | 28512 | .469 | 380.7 | .295 | .4358 | 354.0 | 759.9 | 84.19 | 844.0 | 1198.1 |
| 199 | 28656 | •537 | 381.1 | .284 | •4379 | 354.4 | 759.5 | 84.21 | 843.7 | 1198.2 |
| | | 1 | 1 | 1 | | | 1 | 1 | 1 | |

-

STEAM

87

SECT. II.]

| 0 | 0 | |
|---|---|--|
| ο | 0 | |

212

213

214

215

216

217 218

219

30528

30672

30816

30960

31104

31248

31392

31536

14.522

14.590 14.658

14.726

14.794 14.862

14.930

14.998

386.5

386.9

387.3

387.7 388.1

388.5

388.9

389.3

DATA RELATING TO AIR AND STEAM [PART. IV.

| - | | | | | | | | | | | |
|----------|---------------------------------|---|--|---|---------------------------------------|--|---|--|--|---|--|
| Pressure | in pounds per square inch. | Pressure in pounds per square foot. | Pressure in atmospheres. | Temp. in degrees Fahr. | Volume per pound in cubic feet. | Weight per cubic foot in pounds. | Heat of water per pound in B.T.U. | Internal latent heat per pound of steam in B.T.U. | External latent heat per pound of steam in ' B.T.U. | Total latent heat per pound of steam in B.T.U. | Total heat per pound of steam in B.T.U. |
| | 200 201 202 203 204 | 28800 28944 29088 29232 29376 | 13.605 13.673 13.742 13.810 13.878 | 381.6 382.0 382.4 382.8 383.2 | 2.273 .262 .252 .241 .231 | 0.4399 .4420 .4441 .4461 .4482 | 354.9 355.3 355.8 356.2 356.6 | 759.2 758.9 758.5 758.2 757.9 | 84.23 84.26 84.28 84.30 84.33 | 843.4 843.1 842.8 842.5 842.2 | 1198.3 1198.4 1198.6 1198.7 1198.8 |
| 4 44 44 | 205 206 207 208 209 | 29520 29664 29808 29952 30096 | 13.946 14.014 14.082 14.150 14.218 | 383.7 384.1 384.5 384.9 385.3 | 2.221 .211 .201 .191 .181 | 0.4503 .4523 .4544 .4564 .4585 | 357.1 357.5 357.9 358.3 358.8 | 757.5 757.2 756.9 756.6 756.2 | 84.35 84.37 84.40 84.42 84.44 | 841.9 841.6 841.3 841.0 840.7 | 1199.0 1199.1 1199.2 1199.3 1199.4 |
| | 210 | 30240 30384 | 14.386 14.454 | 385.7 386.1 | 2.171 .162 | 0.4605 .4626 | 359.2 359.6 | 755.9 755.6 | 84.46 84.48 | 840.4 840.1 | 1199.6 1199.7 |

755.3

755.0

754.7

754.3

754.0

753.7

753.4

753.1

360.0

360.4

360.9

361.3

361.7

362.1

362.5

362.9

84.51

84.53

84.55

84.57

84.60

84.62

84.64

84.66

839.8

839.5

839.2

838.9

838.6

838.3

838.0

837.7

1199.8

1199.9

1200. I

1200.2

1200.3

1200.4

1200.5

1200.7

.152

.143

.134

2.124

.115

.106

.097 .088

.4646

.4666

.4687

0.4707

.4727

.4748

.4768

.4788

PART V. DATA SPECIALLY RELATING TO MINING.

SECTION I. DENSITY AND OTHER PHYSICAL PROPERTIES OF VARIOUS MINERAL SUBSTANCES, ORES, METALS, ETC.

DENSITY AND SPECIFIC GRAVITY.

Density is the weight *in vacuo* of unit volume. On the c.g.s. system it is expressed in grammes per cubic centimetre.

The Specific Gravity of a substance is the ratio of its density to that of water at 4° C. (this being the temperature at which water has its maximum density).

The density of water at 4° C. $(39^{\circ}.2$ F.) is very little less than unity. According to the latest determination, the weight *in* vacuo of a cubic centimetre of water at 4° C. is 0.999974 gramme (see page 4).

For practical purposes, therefore, 'specific gravity,' as above defined, is identical with 'density.'

The first table (p. 90) gives the weight in pounds per cubic foot and the number of cubic feet per ton corresponding to a given density. The density of a given substance being known, this table gives either its weight per cubic foot or its volume per ton, as may be required. The densities of the principal ores are given on p. 93, those of the rock forming minerals and gemstones on pp. 94 and 95. The remaining tables give the density and pounds per cubic foot of various mineral substances in common use, of the metals and their alloys and of different kinds of wood.

Table giving the weight in pounds per cubic foot and the number of cubic feet per short ton of 2000 lbs. and per long ton of 2240 lbs. corresponding to a given density.

| Density = grammes per cubic centi- metre. | Pounds per cubic foot. | Cubic feet per ton of 2000 lbs. | Cubic feet per ton ot 2240 lbs. | Density = grammes per cubic centi- metre. | Pounds per cubic foot, | Cubic feet per ton of 2000 lbs. | Cubic feet per ton of 2240 lbs. |
|--|--|--|--|--|---|---|--|
| metre. 0.5 0.55 0.6 0.655 0.7 0.755 0.8 0.855 0.9 0.955 1.0 1.05 1.1 1.15 1.2 1.25 1.3 1.4 1.455 1.55 1.55 1.6 1.655 1.7 1.755 1.8 1.855 1.9 1.955 2.0 2.055 2.15 2.22 2.255 2.45 2.455 | 31.2 34.3 37.5 40.6 43.7 46.8 49.9 53.1 56.2 59.3 62.4 65.5 68.7 71.8 74.9 78.0 81.2 84.3 87.4 90.5 93.6 96.9 93.0 103.0 106.1 109.2 112.4 115.5 118.6 121.7 124.9 131.1 134.2 137.3 140.5 143.6 146.7 149.8 152.9 | 64.1 58.3 53.3 49.3 45.8 42.7 40.1 37.7 35.6 33.7 32.1 30.5 29.1 27.9 26.7 25.6 24.6 23.7 22.9 22.1 21.4 20.7 20.7 20.7 20.7 20.0 19.4 18.9 18.3 17.8 17.8 17.8 17.8 17.8 17.8 17.3 16.9 16.4 16.0 15.6 15.3 14.9 13.6 13.4 13.1 | 71.8 65.3 59.7 55.2 51.3 47.9 44.9 42.2 39.9 37.8 35.9 34.2 32.6 31.2 29.9 28.7 27.6 26.6 25.6 24.8 23.9 23.1 22.4 21.7 21.1 20.5 19.9 19.4 18.9 18.4 17.9 19.4 18.9 17.5 17.1 16.3 15.9 15.6 15.3 15.0 14.7 | metre. 2.55 2.6 2.65 2.7 2.75 2.8 2.99 2.95 3.0 3.2 3.3 3.4 3.5 3.6 3.7 3.8 3.9 4.0 4.1 4.2 4.3 4.4 4.5 4.6 4.7 5.3 5.4 5.5 5.7 5.8 5.9 | 159.2 162.3 165.4 168.6 171.7 174.8 177.9 181.0 184.2 187.3 190.4 193.5 199.8 206.0 212.3 218.5 224.7 231.0 237.2 243.5 224.7 231.0 237.2 243.5 224.7 231.0 237.2 243.5 224.7 236.0 262.2 268.4 274.7 280.9 287.2 299.7 305.9 312.1 318.4 324.6 330.9 337.1 343.4 349.6 355.8 362.1 368.3 | 12.6 12.3 12.1 11.9 11.6 11.4 11.2 10.7 10.5 10.0 9.7 9.4 9.2 8.9 8.7 8.4 8.0 7.8 7.5 7.3 7.1 7.0 6.8 6.7 6.5 6.4 6.2 6.0 5.9 5.7 5.6 5.7 5.6 5.7 5.6 | 14.1 13.8 13.5 13.3 13.0 12.8 12.6 12.4 12.2 12.0 11.8 11.6 11.2 10.9 10.5 10.0 .9.7 9.4 9.2 9.0 8.8 8.5 8.3 8.2 8.0 7.8 7.6 7.5 7.3 7.2 7.0 6.9 6.6 6.5 6.4 6.3 6.2 6.1 |
| 2.5 | 156.1 | 12.8 | 14.3 | 6.0 | 374.6 | 5.3 | 6.0 |

A density of 1.0=1 gramme per cubic centimetre=62.4278 lbs. per cubic foot.

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SECT. I.]

DENSITY

Density or grammes per cubic centimetre, also pounds per cubic foot and cubic feet per short ton of 2000 lbs. and per long ton of 2240 lbs. of various mineral substances.

A density of 1.0=1 gramme per cubic centimetre=62.4278 lbs. per cubic foot.

| SUBSTANCE. | Density =grammes per cubic centimetre. | Pounds per cubic foot. | Cubic feet per ton of 2000 lbs. | Cubic feet per ton of 2240 lbs. |
|-----------------------------|---|------------------------------|---------------------------------------|---------------------------------------|
| | Centrinetre. | | | |
| Anthracite (solid), - | 1.4-1.8 | 87.4-112.4 | 22.9-17.8 | 25.6-19.9 |
| Asbestos, | 2.0-2.8 | 124.9-174.8 | 16.0-11.4 | 17.9-12.8 |
| Asphaltum, | I.I-I.2 | 68-7-74.9 | 29.1-26.7 | 32.6-29.9 |
| Basalt, | 2.8-3.0 | 174.8-187.3 | 11.4-10.7 | 12.8-12.0 |
| Bricks (see end of table). | | | | |
| Brickwork " | | | 190.6 19 | |
| Cement- | | | | |
| Pulverized, loose, - | 1.15-1.7 | 71.8-106.1 | 27.9-18.9 | 31.2-21.1 |
| Set, | 2.7-3.0 | 168.6-187.3 | 11.9-10.7 | 13.3-12.0 |
| Chalk, | 1.9-2.8 | 118.6-174.8 | 16.9-11.4 | 18.9-12.8 |
| Clay, | 1.8-2.6 | 112.4-162.3 | 17.8-12.3 | 19.9-13.8 |
| Clay Slate, | 2.8-2.9 | 174.8-181.0 | 11.4-11.0 | 12.8-12.4 |
| Coal- | 3525 S. R. | | | |
| 'Soft' or bituminous, | 22166 | 1.1.1.17 | | 1999 |
| in situ, | 1.2-1.5 | 74.9-93.6 | 26.7-21.4 | 29.9-23.9 |
| 'Round,' in trucks, - | 0.88-0.9 | 54.9-56.2 | 36.4-35.6 | 40.8-39.9 |
| Coke, | · | 23.0-28.0 | 87.0-71.4 | 97.4-80.0 |
| Diorite, | 2.8-3.0 | 174.8-187.3 | 11.4-10.7 | 12.8-12.0 |
| Dolomite, | 2.8-2.9 | 174.8-181.0 | 11.4-11.0 | 12.8-12-4 |
| Earth (dry), | 1.3-1.9 | 81.2-118.6 | 24.6-16.9 | 27.6-18.9 |
| Gneiss, - · · | 2.59-2.7 | 161.7-168.6 | 12.4-11.9 | 13.9-13.3 |
| Granite, | 2.59-2.75 | 161.7-171.7 | 12.4-11.6 | 13.9-13.0 |
| Graphite, | 1.9-2.3 | 118.6-143.6 | 16.9-13.9 | 18.9-15.6 |
| Gravel, - · · | 1.2-1.8 | 74.9-112.4 | 26.7-17.8 | 29.9-19.9 |
| Greenstone, | 2.9-3.0 | 181.0-187.3 | 11.0-10.7 | 12.4-12.0 |
| Ice, | 0.88-0.91 | 54.9-56.8 | 36.4-35.2 | 40.8-39.4 |
| Kaolin, | 2.2 | 137.3 | 14.6 | 163 |
| Lime- | | | 1.1.1.1.1.1.1 | Contraction of |
| Quick, | 0.9-1.2 | 56.2-74.9 | 35.6-26.7 | 39.9-29.9 |
| Slaked, | I.3-I.4 | 81.2-87.4 | 24.6-22.9 | 27.6-25.6 |
| Mortar, | 1.65-1.78 | 103.0-111.1 | 19.4-18.0 | 21.7-20.2 |
| Limestone, | 2.46-2.86 | 153.6-178.5 | 13.0-11.2 | 14.6-12.5 |
| Marble, | 2.5-2.8 | 156.1-174.8 | 12.8-11.4 | 14.3-12.8 |
| Marl, | 1.6-2.5 | 99.9-156.1 | 20.0-12.8 | 22.4-14.3 |
| Masonry (see end of table). | 1.11 | 1000 | | |

92 DATA RELATING TO MINING [PART V.

| | Density | Pounds | Cubic feet | Cubic feet |
|---|--|-----------------|-------------------------|---|
| SUBSTANCE. | =grammes pe | | | |
| | cubic centimetre. | cubic foot. | per ton of 2000 lbs. | per ton of 2240 lbs. |
| | | | | |
| Oolite, | 2.0-2.4 | 124.9-149-8 | 16.0-13.4 | 17.9-15.0 |
| Peat, | 0.84 | 52.4 | 38.2 | 42.7 |
| Peridotite, | | 187.3-206.0 | 10.7-9.7 | |
| | 3.0-3.3 | 107.3-200.0 | 10.7-9.7 | 12.0-10.9 |
| Quartz- | | | 2 | |
| Solid, as in lodes, - | 2.67 | 166.7 | 12.0 | 13.4 |
| Broken, ready for mill- | | | | |
| ing, | 1.6 | 99.9 | 20.0 | 22.4 |
| Tailings, <i>i.e.</i> the sands | | | | - |
| from the mill pulp, | | | | 1 1 N. S. |
| wet, as collected in | | | | |
| settling vats, | I.42 | 88.7 | 22.5 | 25.3 |
| Do., dry, | 1.23 | 76.8 | 26.0 | 29.2 |
| Slimes, <i>i.e.</i> the slowly | | | | |
| settled portion of | | | | |
| settled portion of the mill pulp, wet, | | | | |
| in collecting dam, - | 1.92 | 119.9 | 16.7 | 18.7 |
| Sand- | | | | |
| Dry, | 1.3-1.65 | 81.2-103.0 | 24.6-19.4 | 27.6-21.7 |
| Damp, | 1.9-2.05 | 118.6-128.0 | 16.9-15.6 | 18.9-17.5 |
| | | | | |
| Sandstone, | 2.2-2.5 | 137.3-156.1 | 14.6-12.8 | 16.3-14.3 |
| Serpentine, | 2.43-2.66 | 151.7-166.0 | 13.2-12.0 | 14.8-13.5 |
| Shale, | 2.4-2.8 | 149.8-174.8 | 13.4-11.4 | 15.0-12.8 |
| Slate, | 2.6-2.7 | 162.3-168.6 | 12.3-11.9 | 13.8-13.3 |
| Slimes (see under Quartz). | | | | |
| Syenite, | 2.75-2.9 | 171.7-181.0 | 11.6-11.0 | 13.0-12.4 |
| Tailings (see under | | | | |
| Quartz). | | | | |
| Trachyte, | 2.7-2.8 | 168.6-174.8 | 11.9-11.4 | 13.3-12.8 |
| Bricks- | | | | |
| Bricks-Best, pressed, | weigh from | 145 to 155 lbs. | per cubic for | |
| Common, hard, | - | | | |
| Inferior, soft, | | | | |
| | 3.9 | 90 to 110 , | , ,, | |
| Masonry— | and the second | | | |
| Of granite or limestor | | | . 11. 6 | |
| | 0 | 155 to 180 lbs. | | ν. |
| Best mortar rubble, | | 150 to 160 , | , ,, | |
| Best dry rubble, | | 130 to 145 , | , ,, | |
| Rough mortar rubb | | 140 to 150 , | , ,, | |
| Rough dry rubble, | | 120 to 130 , | , ,, | |
| Of sandstone, deduct | h from the | above weights. | | |
| Of brickwork— | | | | |
| Best pressed brick, | fine joints, v | weighs from 135 | to 145 lbs. | per cubic ft. |
| Common hard brick | | | | , ,, |
| Inferior soft brick, | | | | ., ,, |
| Cement concrete weighs fr | | | | |
| 3.0 | | S Por subio | | |

SECT. I.]

Density and pounds per cubic foot of various metals and alloys.

| Metal or Alloy. | Density =grammes per cubic centimetre. | Pounds per cubic foot. |
|---|--|--|
| Aluminium, Antimony, Bismuth, Brass, Bronze, Cobalt, Gold, Iridium, | 2.6-2.8 6.7-6.72 9.7-9.9 8.44-8.7 8.74-8.89 8.5-9.1 8.8-8.95 19.26-19.34 21.78-22.42 | 162.3-174.8 418.3-419.5 605.5-618.0 526.9-543.1 545.6-555.0 530.6-568.1 549.4-558.7 1202.4-1207.4 1359.7-1399.6 |
| Gray cast, $ -$ White cast, $ -$ Wrought, $ -$ Mercury at o° C., $ -$ Nickel, $ -$ Platinum, $ -$ Platinum, $ -$ Silver, $ -$ Tin, $ -$ Tungsten, $ -$ Zinc, $ -$ | $\begin{array}{c} 7.03-7.13\\ 7.58-7.73\\ 7.8-7.9\\ 11.34-11.36\\ 13.596\\ 8.3-8.9\\ 21.2-21.7\\ 21.62-22.38\\ 10.4-10.57\\ 7.8-7.9\\ 7.29-7.3\\ 19.12\\ 7.04-7.19\end{array}$ | 438.9-445.1 473.2-482.6 486.9-493.2 707.9-709.2 848.8 518.2-555.6 1323.5-1354.7 1349.7-1397.1 649.2-659.9 486.9-493.2 455.1-455.7 1193.6 439.5-448.9 |

Density of the principal ores of the metals.

| | or one brough | | |
|------------------|---------------|--------------------|-----------|
| Antimonite, - | 4.6-4.7 | Hemimorphite, - | 3.4-3.5 |
| Argentite, | 7.0-7.4 | Kerargyrite, - | 5.58-5.6 |
| Blende, | 3.9-4.2 | Limonite, | 3.4-3.9 |
| Bornite, | 4.9-5.2 | Magnetite, | 4.9-5.2 |
| Calamine, | 4.1-4.5 | Malachite, | 3.7-4.I |
| Cassiterite, | 6.8-7.0 | Manganese-spar, | 3.3-3.6 |
| Cerussite, | 6.4-6.6 | Nagyagite, | 6.85-7.2 |
| Chalcopyrite, - | 4.1-4.3 | Platinum, | 12-18 |
| Chessylite, | 3.7-3.8 | Proustite, | 5.5-5.6 |
| Chromite, | 4.4-4.6 | Psilomelane, - | 3 14-3.36 |
| Cinnabar, | 8.0-8.2 | Pyrargyrite, - | 5.75-5.85 |
| Copper (Native), | 8.5-8.9 | Pyrolusite, | 4.7-5.0 |
| Copper Glance, - | 5.5-5.8 | Siderite, | 3.7-3.9 |
| Covellite | 4.6 | Silver (Native), - | 10.5-11.0 |
| Cryolite, | 2.95-2.99 | Stephanite, - | 6.2-6.3 |
| Cuprite, | 5.7-6.0 | Sylvanite, | 7.99-8.33 |
| Galena, | 7.3-7.6 | Wad, | 2.3-3.7 |
| Gold (Native), - | 15.6-19.4 | Willemite, | 3.9-4.2 |
| Hæmatite, | 5.19-5.28 | | |

Density and pounds per cubic foot of different kinds of wood.*

The wood is supposed to be seasoned and of average dryness.

| · · · · · · · · · · · · · · · · · · · | | | | | | | | |
|---------------------------------------|--------------------------------------|------------------------------|---------------------|---------------------------------------|------------------------------|--|--|--|
| Wood. | Density= grammes per cubic cm. | Pounds per cubic foot. | Wood. | Density= gramnies per cubic cm. | Pounds per cubic foot. | | | |
| Alder | 0.42-0.68 | 26-42 | Greenheart | 0.93-1.04 | 58-65 | | | |
| Apple | 0.66-0.84 | 41-52 | Hazel | 0.60-0.80 | 37-49 | | | |
| Ash | 0.65-0.85 | 40-53 | Hickory | 0.60-0.93 | 37-58 | | | |
| Basswood. See Linden. | | | Iron-bark | 1.03 | 64 | | | |
| Beech | 0.70-0.90 | 43-56 | Laburnum | 0.92 | 57 | | | |
| Blue gum | 0.84 | 52 | Lancewood | 0.68-1.00 | 42-62 | | | |
| Birch | 0.51-0.77 | 32-48 | Lignum vitæ | 1.17-1.33 | 73-83 | | | |
| Box | 0.95-1.16 | 59-72 | Linden or Lime-tree | 0.32-0.59 | 20-37 | | | |
| Bullet-tree | 1.05 | 65 | Locust | 0.67-0.71 | 42-44 | | | |
| Butternut | 0.38 | 24 | Mahogany, Honduras | | 35 | | | |
| Cedar | 0.49-0.57 | 30-35 | ,, Spanish - | 0.85 | 53 | | | |
| Cherry | 0.70-0.90 | 43-56 | Maple | 0.62-0.75 | 39-47 | | | |
| Cork | 0.22-0.26 | 14-16 | Oak- | 0.60-0.90 | 37-56 | | | |
| Ebony | I.II-I.33 | 69-83 | Pear-tree | 0.61-0.73 | 38-45 | | | |
| Elm | 0.54-0.60 | 34-37 | Plum-tree | 0.66-0.78 | 41-49 | | | |
| Fir or Pine, American | | | Poplar | 0.35-0.5 | 22-3I | | | |
| White | 0.35-0.50 | 22-31 | Satinwood | 0.95 | 59 | | | |
| " Larch - | 0.50-0.56 | 31-35 | Sycamore | 0.40-0.60 | 24-37 | | | |
| ,, Pitch | 0.83-0.85 | 52-53 | Teak, Indian | 0.66-0.88 | 41-55 | | | |
| ,, Red | 0.48-0.70 | 30-44 | ", African | 0.98 | 61 | | | |
| ,, Scotch - | 0.43-0.53 | 27-33 | Walnut | 0.64-0.70 | 40-43 | | | |
| " Spruce - | | 30-44 | Water gum | 1.00 | 62 | | | |
| " Yellow - | 0.37-0.60 | 23-37 | Willow | 0.40-0.60 | 24-37 | | | |

Density of the rock-forming minerals and of gem-stones.

| Agate, - | • | - | - | - | - | - | | - | - | 2.6 |
|----------------|-------|---------|-------|--------|-------|--------|---|-----|--------|-----------|
| Apatite, - | - | - | - 11 | - | - | * | - | - | - II., | 3.2 |
| Aragonite, | - | - | - | - 1 | - | - | - | - | - | 2.9 |
| Augite, - | - | - 21 | - 2 | - | - | - | - | - | - | 3.3-3.49 |
| Barytes (heav | vy sp | ar), | - | - | - | - | - | - | - | 4.5 |
| Beryl (aquam | | , | ' | , | - | - | - | | - | 2.7 |
| Calcite (calcs | par, | Icelan | ldspa | ur), | - | - | - | - | - | 2.72 |
| Chlorite, | - | | - | - | | | - | - | - | 2.6-3.0 |
| Chrysoberyl | (Alex | andri | te), | - | - | - | - | - | - | 3.7 |
| Corundum (r | uby, | sapph | ire), | - | - | - 11 | - | - | - | 4.0 |
| Diamond, | - | - | - | • | | - | - | - | - | 3.52 |
| Diopside, | • | - | • | | - | - 10 | - | - | - | 3.3 |
| Dolomite, | - | - | - | | - | • | - | - | - | 2.85 |
| Felspar, - | - | | - | | - | | - | - | - | 2.56-2.75 |
| Fluorspar, | - | - | • | - | - | - | - | - | - | 3.2 |
| Garnet (alma | ndin | e, carl | buncl | le, py | rope, | etc.), | • | - 1 | - | 3.15-4.3 |
| Gypsum, | - | - | - | - | - | - 1 | - | - | - | 2.3 |
| Hornblende, | - | • | - | • | • | • | - | - | - | 3.18-3.22 |
| | | | | | | | | | | |

* Smithsonian Physical Tables, Washington, 1906.

SECT. I.]

DENSITY

| Ilmenite, | - | - | - | | - | - | - | - | - | 4.8 | |
|---------------|--------|-------|--------|-----|---|---|---|---|---|-----------|---|
| Magnetite, | - | - | - | - | - | 2 | - | - | - | 5.2 | |
| Mica, - | - | | | - | - | - | - | - | - | 2.84-2.93 | 3 |
| Olivine (peri | dote, | chry | solite | e), | | - | • | - | - | 3.4 | |
| Opal, - | - | - | - | - | - | - | - | - | | 2.6 | |
| Phenakite, | - | | - | | - | - | - | - | - | 3.0 | |
| Quartz, - | - | - ' | 1.8 | - | - | - | - | - | - | 2.65 | |
| Serpentine, | - | | 1 - | - | - | - | - | - | - | 2.6 | |
| Spinel (balas | s-ruby | y), | - | - | - | | - | - | - | 3.5 | |
| Talc, - | - | - | - | - | - | - | - | - | - | 2.7 | |
| Topaz, - | - 11 | - | - | - | | | - | - | - | 3.5 | |
| Tourmaline, | - | - | - | | - | - | - | - | - | 3.I | |
| Turquoise, | - | - 5 | - | - | - | - | | - | - | 2.7 | |
| Zircon (jargo | oon, l | hyaci | nth), | - | - | - | - | - | - | 4.7 | |
| | | | | | | | | | | | |

HARDNESS OF MINERALS.

The hardness of a mineral is measured by the force required to scratch (*i.e.* to separate) the superficial particles of the mineral with a steel point or the sharp-pointed fragment of some harder mineral. In Moh's scale, the hardness of 10 minerals is taken to represent 10 successive degrees of hardness. The degrees of hardness are, however, arbitrarily fixed, and there is no constant ratio between them :

Moh's Scale of hardness.

Each of the minerals forming this scale can be scratched by those which follow, and will itself scratch those that precede it in the list; consequently the hardness of a mineral is estimated by its capability of scratching or being scratched by any mineral in this list:

Hardness of gem-stones (on Moh's scale).

| Agate, | 7 1 | Opal, 7 |
|---------------------------------|------|--|
| Beryl (aquamarine, emerald), | 71 | Phenakite, 8 |
| Chrysoberyl (Alexandrite), - | 81 | Quartz (rock-crystal, cairn- |
| Corundum (ruby, sapphire), | 9 | gorm, prase), 7 |
| Diamond, | IO | Serpentine, 3 |
| Diopside, | 51 | Spinel (balas-ruby), 8 |
| Felspar (moonstone), | 6 | Topaz, · · 8 |
| Fluorspar, | 4 | Tourmaline, 7 |
| Garnet (almandine, car- | 1990 | Turquoise, 6 |
| buncle, pyrope, etc.), - | 7 | Zircon (jargoon, hyacinth), - $\cdot 7\frac{1}{2}$ |
| Olivine (peridote, chrysolite), | 7 | |

| Name of Metal. | Expansion per degree C. | Expansion per degree F. |
|----------------------|----------------------------|----------------------------|
| Aluminium, - | - 20 | 11.1 |
| Brass, | - 19 | 10.5 |
| Copper, | - 17 | 9.4 |
| Glass, | - 9 | 5.0 |
| Gold, | - 15 | 8.3 |
| Iron, cast, - | - II | 6.1 |
| Iron, wrought, - | · I2 | 6.7 |
| Lead, | - 28 | 15.5 |
| Platinum, | . 9 | 5.0 |
| Platinum-iridium,† - | 8.7 | 4.8 |
| Silver, | · 19 | 10.5 |
| Steel, hard, - | · I2 | 6.7 |
| Steel, soft, - | 11 | 6.1 |
| Tin, | . 19 | 10.5 |
| Zinc, | - 29 | 16.1 |

Linear expansion of the principal metals, in microns per metre (or millionths per unit length).*

SECTION II. ORE-TONNAGE PER UNIT AREA.

By means of the table on p. 97 the number of tons of an ore or mineral contained in an acre of surface can be calculated if we know the density of the ore or mineral and the average thickness and dip of the vein or bed in which it occurs : for the tonnage given in the table for the angle of dip x the thickness of the vein or bed in feet x the density of the ore or mineral = the number of tons per acre of surface. For example, supposing it is required to know the number of long tons of coal contained in an area of 300 acres, the seam being of an average thickness of 5 feet, having a dip of 6°, and the density of the coal having been determined to be 1.4. For a dip of 6° the table gives the constant 1220.6. Therefore the required tonnage is: 1220.6 × 5 $\times 1.4 \times 300 = 2,563,260$ long tons. From this figure a considerable deduction has to be made in order to obtain the amount of marketable coal, the percentage to be deducted depending on the local conditions.

The table on p. 98 gives the tons of quartz per Transvaal claim.

* Smithsonian Geographical Tables, 1906, p. 170.

+Or Iridio-platinum ; 90°/, platinum and 10°/, iridium. It is the alloy of which the International Prototype Metric Standards are made.

SECT. II.] ORE-TONNAGE PER UNIT AREA

Table giving the number of short tons (2000 lbs.) and of long tons (2240 lbs.) per acre of surface contained in a vein or bed one foot thick and of a density=I, for each degree of dip from o° to 85°.*

| Degrees of dip. | Short tons of 2000 lbs. per acre for a density=1. | Long tons of 2240 lbs. per acre for a density=1. | Degrees of dip. | Short tons of 2000 lbs. per acre for a density=1. | Long tons of 2240 lbs. per acre for a density=1. |
|-----------------------------------|--|---|--------------------|--|---|
| 0° | 1359.6 | 1213.9 | 45° | 1922.7 | 1716.7 |
| 1 | 1359.8 | 1214.1 | 46 | 1957.1 | 1747.4 |
| 2 | 1360.4 | 1214.6 | 47 | 1993.4 | 1779.9 |
| 3 4 5 | 1361.4 1362.9 1364.7 | 1214.0 1215.6 1216.8 1218.5 | 48 49 50 | 2031.8 2072.3 2115.1 | 1814.1 1850.3 1888.5 |
| 6 | 1367.0 | 1220.6 | 51 | 2160.3 | 1928.9 |
| 7 | 1369.8 | 1223.0 | 52 | 2208.3 | 1971.7 |
| 8 | 1372.9 | 1225.8 | 53 | 2259.1 | 2017.1 |
| 9 | 1376.5 | 1229.0 | 54 | 2313.0 | 206 <u>5</u> .2 |
| 10 | 1380.5 | 1232.6 | 55 | 2370.3 | 2116.3 |
| 11 | 1385.0 | 1236.6 | 56 | 2431.3 | 2170.8 |
| 12 | 1389.9 | 1241.0 | 57 | 2496.2 | 2228.8 |
| 13 | 1395.3 | 1245.8 | 58 | 2565.6 | 2290.7 |
| 14 | 1401.2 | 1251.0 | 59 | 2639.7 | 2356.9 |
| 15 | 1407.5 | 1256.7 | 60 | 2719.1 | 2427.8 |
| 16 | 1414.3 | 1262.8 | 61 | 2804.3 | 2503.8 |
| 17 | 1421.7 | 1269.3 | 62 | 2895.9 | 2585.6 |
| 18 | 1429.5 | 1276.4 | 63 | 2994.7 | 2673.8 |
| 19 | 1437.9 | 1283.8 | 64 | 3101.4 | 2769.1 |
| 20 | 1446.8 | 1291.8 | 65 | 3217.0 | 2872.3 |
| 21 | 1456.3 | 1300.2 | 66 | 3342.6 | 2984.5 |
| 22 | 1466.3 | 1309.2 | 67 | 3479.5 | 3106.7 |
| 23 | 1477.0 | 1318.7 | 68 | 3629.3 | 3240.4 |
| 24 | 1488.2 | 1328.8 | 69 | 3793.7 | 33 ⁸ 7.3 |
| 25 | 1500.1 | 1339.7 | 70 | 3975.1 | 3549.2 |
| 26 | 1512.6 | 1350.6 | 71 | 4175.9 | 3728.5 |
| 27 | 1525.9 | 1362.4 | 72 | 4399.6 | 3928.2 |
| 28 | 1539.8 | 1374.8 | 73 | 4650.1 | 4151.9 |
| 29 | 1554.4 | 1387.9 | 74 | 4932.4 | 4403.9 |
| 30 | 1569.9 | 1401.7 | 75 | 5252.9 | 4690.1 |
| 31 | 1586.1 | 1416.2 | 76 | 5619.8 | 5017.7 |
| 32 | 1603.2 | 1431.4 | 77 | 6043.8 | 5396.2 |
| 33 | 1621.1 | 1447.4 | 78 | 6539.1 | 5838.4 |
| 34 | 1639.9 | 1464.2 | 79 | 7125.2 | 6361.8 |
| 35 | 1659.7 | 1481.9 | 80 | 7829.3 | 6990.5 |
| 36 | 1680.5 | 1500.4 | 81 | 8690.9 | 7759.7 |
| 37 | 1702.3 | 1519.9 | 82 | 9768.8 | 8722.1 |
| 38 | 1725.3 | 1540.4 | 83 | 11155.8 | 9960.5 |
| 39 | 1749.4 | 1562.0 | 84 | 13006.5 | 11613.0 |
| 40 | 1774.8 | 1584.6 | 85 | 15599.1 | 13927.8 |
| 41 42 43 44 45 | 1801.4 1829.5 1859.0 1890.0 1922.7 | 1608.4 1633.4 1659.8 1687.5 1716.7 | | | |

* The tonnage is not affected by the shape of the area. No deduction has been made for dykes or faults.

H.M.

G

PART V.

Table giving the number of short tons (2000 lbs.) of Quartz contained in a Transvaal claim of 60,000 square Cape feet per one British foot thickness of Reef, for each degree of dip from 0° to 85°, calculated on a basis of 12 cubic feet to the ton.*

| Degrees of dip. | Tons of 2000 lbs. per claim. | Degrees of dip. | Tons of 2000 lbs. per claim. | Degrees of dip. | Tons of 2000 lbs. per claim. |
|-----------------------------|--|-----------------------------|---|-----------------------------|---|
| 0° 1 2 3 4 5 | 5335 5336 5339 5343 5348 5356 | 31° 32 33 34 35 | 6225 6291 6362 6436 6513 | 61° 62 63 64 65 | 11005 11365 11752 12171 12625 |
| 6 | 5365 | 36 | 6595 | 66 | 13118 |
| 7 | 5376 | 37 | 6681 | 67 | 13655 |
| 8 | 5388 | 38 | 6771 | 68 | 14243 |
| 9 | 5402 | 39 | 6865 | 69 | 14888 |
| 10 | 5418 | 40 | 6965 | 70 | 15600 |
| 11 | 5435 | 41 | 7070 | 71 | 16388 |
| 12 | 5455 | 42 | 7180 | 72 | 17266 |
| 13 | 5476 | 43 | 7295 | 73 | 18249 |
| 14 | 5499 | 44 | 7417 | 74 | 19357 |
| 15 | 5524 | 45 | 7545 | 75 | 20615 |
| 16 | 5550 | 46 | 7681 | 76 | 22054 |
| 17 | 5579 | 47 | 7823 | 77 | 23718 |
| 18 | 5610 | 48 | 7974 | 78 | 25662 |
| 19 | 5643 | 49 | 8133 | 79 | 27962 |
| 20 | 5678 | 50 | 8300 | 80 | 30726 |
| 21 | 5715 | 51 | 8478 | 81 | 34107 |
| 22 | 5754 | 52 | 8666 | 82 | 38337 |
| 23 | 5796 | 53 | 8866 | 83 | 43780 |
| 24 | 5840 | 54 | 9077 | 84 | 51043 |
| 25 | 5887 | 55 | 9302 | 85 | 61217 |
| 26 27 28 29 30 | 5936 5988 6043 6100 6161 | 56 57 58 59 60 | 9541 9796 10068 10359 10671 | | |

Rule: Multiply the tonnage given by the thickness of the reef in feet.

*The tonnage is not affected by the shape of the claim. No deduction has been made for dykes and faults.

SECT. III.] UNDERGROUND TEMPERATURES

SECTION III. UNDERGROUND TEMPERATURES.

The rise in temperature with increasing depth is a factor of great importance in deep-level mining. The rate of increase of temperature in boreholes and deep shafts has therefore to be carefully determined. The method of observing the temperature in deep boreholes by the use of clinical thermometers is described in detail by H. F. Marriott (Trans. Inst. Min. Met., vol. xv., p. 405). Since in deep boring there is a considerable deviation from the vertical, the correct depth at the point of observation can only be obtained by a survey. Several instruments for this purpose have been invented. The simplest and most practical is that invented by Mr. Oehmen of Johannesburg, Transvaal. By this ingenious instrument the deviation from the vertical and the direction of the deviation are recorded by taking photographs of the position of a plumb-bob and a magnetic needle at any desired point in the borehole. The photographs are taken after the instrument has been lowered to the desired point, by means of two small incandescent lamps, which are illuminated by a dry battery by means of a time-contact regulated by a watch. The amount of deviation and its direction are calculated from the photograph after the sensitised paper has been developed at the surface. The amount of deviation is calculated by measuring the distance between the centre of the photograph of the plumbbob and the centre of the disc, the length of the plumb-bob being a known factor. The direction of the deviation is obtained from the photograph of the magnetic needle, the correct orientation being fixed by two pin-pricks, which have the same relative position both in the photograph of the needle and in that of the plumb-bob.*

* Brit. Assoc. Rep. for 1905, p. 404.

Table of Underground Temperatures in Mines and Vertical Boreholes. (J. D. Everett, Royal Commission on Coal Supplies, 1904, vol. ii., p. 293.)

| Place. | | Temp. (Fahr.) | Depth (Feet). | Feet per Degree of Increase of Temp. | Recorded in Brit. Association Report for |
|---|---|---|---|---|--|
| Sperenberg (near Berlin), Rosebridge (near Wigan), Paruschowitz (Silesia), Pendleton (near Manchester), - Schladebach (near Leipzig), - Kingswood (near Bristol), Searle (Lincolnshire), Dukinfield (Manchester), - Wheeling (W. Virginia), | | 116 94 157 100.6 134 75 79 86.5 110 | 3,492 2,445 6,445 3,480 5,630 1,769 2,000 2,700 4,462 | 511 54 60 66 67 68 69 72 74 | 1876 1870 1901 |
| Port Jackson (N.S.W.), Ashton Moss (near Manchester), Tamerack (Lake Superior), - | • | 97 84 84 | 2,733 2,880 4,450 | 80 82 100 | 1895 1881 1901 |

From a number of observations made in deep boreholes and mines in the Witwatersrand, Transvaal, Mr. Marriott has deduced a mean rate of increase of temperature for that district of 1° Fahrenheit for each 208 feet of depth, or .48° Fahr. increase per 100 feet of depth. He finds the mean temperature at 1000 feet depth to be 68.75° Fahr. (*Trans. Inst. Min. and Met.*, vol. xv., 1905-6.)

SECT. IV.] GOLD AND COPPER RETURNS

SECTION IV. DATA RELATING TO GOLD AND COPPER RETURNS.

The Valuation of Gold Bullion.

The value of pure gold (1000 fine) is $\pounds 4$ 4s. 11.4545d. per troy ounce.* The following table for the valuation of gold bullion is calculated on this basis, namely one troy ounce of gold (1000 fine) equals $\pounds 4.24773$.

| Weight in Grains. | Value in pounds sterling. | Weight in Dwts. | Value in pounds sterling. | Weight in Oz. Troy. | Value in pounds sterling. |
|---|--|---|---|---|--|
| 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 | 0.00885 0.01770 0.02655 0.03540 0.04425 0.05310 0.06195 0.07080 0.07080 0.07084 0.08849 0.09734 0.10619 0.11504 0.12389 0.13274 0.14159 0.13274 0.14159 0.15044 0.15929 0.16814 0.17699 0.18584 0.19469 0.20354 | 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 | 0.21239 0.42477 0.63716 0.84955 1.06193 1.27432 1.48671 1.69909 1.91148 2.12386 2.33625 2.54864 2.76102 2.97341 3.18580 3.39818 3.61057 3.82296 4.03534 | 1 2 3 4 5 6 7 8 9 | 4.24773 8.49546 12.74319 16.99092 21.23865 25.48638 29.73411 33.98184 38.22957 |

Example of Application of Table.

Find value of 464 oz. 13 dwts. 3 grns. of gold bullion having a fineness of 850.5.

| 400 OZ. = | = 1699.092 | | |
|------------|----------------------------|----------|------------|
| 60 ,, = | = 254.8638 | | |
| 4 ,, = | | | |
| 13 dwts. = | = 2.76102 | | |
| 3 grns. = | = 0.02655 | | |
| | 1973.73429 x 5 058 | k 0.8505 | |
| | 15789874 986867 9869 | | |
| Ī | 1678.6610 or | £1678. 1 | 3s. 2.64d. |
| | | | |

* The British sovereign, which is 916.6 (22 carats) fine, weighs 123.27447 grains. The gold of which it is coined is termed "standard gold," and has a value of \pounds_3 175. 10¹/₂d. per oz.

| Grammes. | Troy ounce. |
|----------|--------------|
| I | .03215074248 |
| 2 | .06430148496 |
| 3 | .09645222744 |
| 4 | .12860296992 |
| 5 | .16075371239 |
| 6 | .19290445487 |
| 7 | .22505519735 |
| 8 | .25720593983 |
| 9 | .28935668231 |

Table for the conversion of Metric weight into Troy ounces.

Table for the conversion of Russian weight into Troy ounces.

- I Pood=40 Funts=526.6451214319 oz. troy.
- I Funt=96 Zolotniks=13.1661280358 oz. troy.
- I Zolotnik=96 Dolis=0.1371471670 oz. troy.
- I Doli=0.0014286163 oz. troy.

| Troy ounces. | Troy ounces. |
|----------------------|--|
| I Pood = 526.6451214 | I Zolotnik =0.137147 |
| 2 Poods=1053.2902429 | 2 Zolotniks=0.274294 |
| 3 " = 1579.9353643 | 3 " =0.411442 |
| 4 ,, =2106.5804857 | 4 " =0.548589 |
| 5 " = 2633.2256072 | 5 " =0.685736 |
| 6 " = 31 59.8707286 | 6 " =0.822883 |
| 7 " = 3686.5158500 | 7 " =0.960030 |
| 8 ,, =4213.1609715 | 8 " =1.097177 |
| 9 " =4739.8060929 | 9 " =1.234324 |
| | |
| I Funt = 13.166128 | 1 Doli =0.001429 |
| 2 Funts= 26.332256 | 2 Dolis=0.002857 |
| 3 " = 39.498384 | 3 " =0.004286 |
| 4 " = 52.664512 * | 4 " =0.005714 |
| 5 " = 65.830640 | 5 " =0.007143 |
| 6 " = 78.996768 | 6 " =0.008572 |
| 7 " = 92.162896 | 7 " =0.010000 |
| 8 " = 105.329024 | 8 " =0.011429 |
| 9 " = 118.495152 | 9 ,, =0.012858 |
| | and the second s |

SECT. IV.] GOLD RETURNS

Example of use of Table.

Convert 28 poods 39 funts 76 zolotniks 24 dolis into troy ounces.

| 57 | | States and an | |
|------------|-------------|---------------|--------|
| 20 p. = 10 | 0532.902429 | oz. troy. | |
| 8 p.= . | 4213.160972 | " | |
| 30 f. = | 394.98384 | " | |
| 9 f. = | 118.495152 | " | |
| 70 z. = | 9.60030 | " | |
| 6 z. = | 0.822883 | " | |
| 20 d.= | 0.02857 | " | |
| 4 d.= | 0.005714 | " | |
| | | | 1999 B |

15269.999860 or say 15270 oz. troy.

Comparison of the various methods of expressing gold ore values . in use in different countries.

Duts. per short ton to duts. per long ton and to Metric and Russian values.

| Dwts. per short ton (2000 lbs.). | Dwts. per long ton (2240 lbs.). | Grammes per tonne(1000 kgs.). | Zolotniks per 100 poods. |
|-------------------------------------|------------------------------------|----------------------------------|-----------------------------|
| I | 1.1200 | 1.7143 | 0.6583 |
| 2 | 2.2400 | 3.4286 | 1.3166 |
| 3 | 3.3600 | 5.1429 | 1.9749 |
| 4 | 4 4800 | 6.8571 | 2.6331 |
| 5 | 5.6000 | 8.5714 | 3.2914 |
| 6 | 6.7200 | 10.2857 | 3.9497 |
| 7 | 7.8400 | 12.0000 | 4.6080 |
| 8 | 8.9600 | 13.7143 | 5.2663 |
| 9 | 10.0800 | 15.4286 | 5.9246 |

Dwts. per long ton to dwts. per short ton and to Metric and Russian values.

| Dwts. per long ton (2240 lbs.). | Dwts. per short ton (2000 lbs.). | Grammes per tonne(1000 kgs.). | Zolotniks per 100 poods. |
|------------------------------------|-------------------------------------|----------------------------------|-----------------------------|
| I | 0.8929 | 1.5306 | 0.5878 |
| 2 | 1.7857 | 3.0612 | 1.1755 |
| 3 | 2.6786 | 4.5918 | 1.7633 |
| 4 | 3.5714 | 6.1224 | 2.3510 |
| 5 | 4.4643 | 7.6531 | 2.9388 |
| 6 | 5.3571 | 9.1837 | 3.5265 |
| 7 | 6.2500 | 10.7143 | 4.1143 |
| 8 | 7.1429 | 12.2449 | 4.7020 |
| 9 | 8.0357 | 13.7755 | 5.2898 |

| Grammes per tonne(1000 kgs.). | Dwts. per short ton (2000 lbs.). | Dwts. per long ton (2240 lbs.). | Zolotniks per 100 poods. |
|----------------------------------|-------------------------------------|------------------------------------|-----------------------------|
| · I | 0.5833 | 0.6533 | 0.3840 |
| 2 | 1.1667 | 1.3067 | 0.7680 |
| 3 | 1.7500 | 1.9600 | 1.1520 |
| 4 | 2.3333 | 2.6133 | 1.5360 |
| 5 | 2.9167 | 3.2667 | 1.9200 |
| 6 | 3.5000 | 3.9200 | 2.3040 |
| 7 | 4.0833 | 4.5733 | 2.6880 |
| 8 | 4.6667 | 5.2267 | 3.0720 |
| 9 | 5.2500 | 5.8800 | 3.4560 |
| | | | |

Grammes per tonne to British and Russsian values.

Zolotniks per 100 poods to British and Metric values.

| Zolotniks per 100 poods. | Dwts. per short ton (2000 lbs.). | Dwts. per long ton (2240 lbs.). | Grammes per tonne(1000 kgs.). |
|-----------------------------|-------------------------------------|------------------------------------|----------------------------------|
| I | 1.5191 | 1.7014 | 2.6042 |
| 2 | 3.0382 | 3.4028 | 5.2083 |
| 3 | 4.5573 | 5.1042 | 7.8125 |
| 4 | 6.0764 | 6.8056 | 10.4167 |
| 5 | 7.5955 | 8.5069 | 13.0208 |
| 6 | 9.1146 | 10.2083 | 15.6250 |
| 7 | 10.6337 | 11.9097 | 18.2292 |
| 8 | 12.1528 | 13.6111 | 20.8333 |
| 9 | 13.6719 | 15.3125 | 23.4375 |

| Dolis per 100 poods to British and Metric value | Dolis | per | 100 | poods | to | British | and | Metric | value. |
|---|-------|-----|-----|-------|----|---------|-----|--------|--------|
|---|-------|-----|-----|-------|----|---------|-----|--------|--------|

| Dolis per 100 poods. | Dwts. per short ton (2000 lbs.). | Dwts. per long ton (2240 lbs.). | Grammes per tonne(1000 kgs.) |
|-------------------------|-------------------------------------|------------------------------------|---------------------------------|
| I | 0.0158 | 0.0177 | 0.0271 |
| 2 | 0.0316 | 0.0354 | 0.0543 |
| 3 | 0.0475 | 0.0532 | 0.0814 |
| 4 | 0.0633 | 0.0709 | 0.1085 |
| 5 | 0.0791 | 0.0886 | 0.1356 |
| 6 | 0.0949 | 0.1063 | 0.1628 |
| 7 | 0.1108 | 0.1241 | 0.1899 |
| 8 | 0.1266 | 0.1418 | 0.2170 |
| 9 | 0.1424 | 0.1595 | 0.2441 |

| GOLD | RETURNS |
|------|---------|
|------|---------|

SECT. IV.]

| Grammes per cubic metre. | Grains per cubic yard. | Grammes per cubic metre. | Dwts. per cubic yard. |
|-----------------------------|---------------------------|-----------------------------|--------------------------|
| 0.1 | 1.1799 | I.0 | 0.4916 |
| 0.2 | 2.3598 | 2.0 | 0.9832 |
| 0.3 | 3.5397 | 3.0 | I.4749 |
| 0.4 | 4.7195 | 4.0 | 1.9665 |
| 0.5 | 5.8994 | 5.0 | 2.4581 |
| 0.6 | 7.0793 | 6.0 | 2.9497 |
| 0.7 | 8.2592 | 7.0 | 3.4413 |
| 0.8 | 9.4391 | 8.0 | 3.9330 |
| 0.9 | 10.6190 | 9.0 | 4.4246 |

Grammes per cubic Metre to Grains and Dwts. per cubic Yard.

Grains and Dwts. per cubic Yard to Grammes per cubic Metre.

| Grains per cubic yard. | Grammes per cubic metre. | Dwts. per cubic yard. | Grammes per cubic metre. |
|---------------------------|-----------------------------|--------------------------|-----------------------------|
| I | 0.0848 | I | 2.0341 |
| 2 | 0.1695 | 2 | 4.0682 |
| 3 | 0.2543 | 3 | 6.1023 |
| 4 | 0.3390 | 4 | 8.1364 |
| 5 | 0.4238 | 5 | 10.1705 |
| 6 | 0.5085 | 6 | 12.2046 |
| 7 | 0.5933 | 7 | 14.2387 |
| 8 | 0.6780 | 8 | 16.2728 |
| 9 | 0.7628 | 9 | 18.3069 |

PART V.

Comparison of the British and American Methods of stating Copper Prices.

Based on 1 British pound sterling=\$4.8665, the legal equivalent given in the circular issued by the Secretary of the U.S. Treasury in October 1906. £1 per long ton of 2240 lbs.=.217254464 cent per lb.

| Price per long ton of 2240 lbs. in British pounds sterling. | Price per lb. avoir. in U.S.A. cents. | Price per long ton of 2240 lbs. in British pounds sterling. | Price per lb. avoir. in U.S.A. cents. | Price per long ton of 2240 lbs. in British pounds sterling. | Price per lb. avoir. in U.S.A. cents. |
|--|---|--|---|--|---|
| £50 | 10.863 c. | £,80 | 17.380 c. | £110 | 23.898 c. |
| 51 | 11.080 | 81 | 17.598 | III | 24.115 |
| 52 | 11.297 | 82 | 17.815 | II2 | 24.331 |
| 53 | 11.513 | 83 | 18.032 | 113 | 24.550 |
| .54 | 11.732 | 84 | 18.249 | 114 | 24.767 |
| 55 | 11.949 | 85 | 18.467 | 115 | 24.984 |
| 56 | 12.166 | 86 | 18.684 | 116 | 25.202 |
| 57 | 12.384 | 87 | 18.901 | 117 | 25.419 |
| 58 | 12.601 | 88 | 19.118 | ·118 | 25.636 |
| 59 | 12.818 | 89 | 19.336 | 119 | 25.853 |
| 60 | 13.035 | 90 | 19.553 | I 20 | 26.071 |
| 61 | 13.253 | 91 | 19.770 | 121 | 26.288 |
| 62 | 13.470 | 92 | 19.987 | I 22 | 26.505 |
| 63 | 13.687 | 93 | 20.205 | 123 | 26.722 |
| 64 | 13.904 | 94 | 20.422 | 124 | 26.940 |
| 65 | 14.122 | 95 | 20.639 | 125 | 27.157 |
| -66 | 14.339 | 96 | 20.856 | 126 | 27.374 |
| -67 | 14.556 | 97 | 21.074 | 127 | 27.591 |
| 68 | 14.773 | 98 | 21.291 | 128 | 27.809 |
| 69 | 14.991 | 99 | 21.508 | 129 | 28.026 |
| 70 | 15.208 | 100 | 21.725 | 130 | 28.243 |
| 71 | 15.425 | IOI | 21.943 | 131 | 28.460 |
| 72 | 15.642 | 102 | 22.160 | 132 | 28.678 |
| 73 | 15.860 | 103 | 22.377 | 133 | 28.895 |
| 74 | 16.077 | 104 | 22.594 | I 34 | 29.112 |
| 75 | 16.294 | 105 | 22.812 | 135 | 29.329 |
| 76 | 16.511 | 106 | 23.029 | 136 | 29.547 |
| 77 | 16.729 | 107 | 23.246 | 137 | 29.764 |
| 78 | 16.964 | 108 | 23.463 | 138 | 29.981 |
| 79 | 17.163 | 109 | 23.681 | 139 | 30.198 |
| 80 | 17.380 | 110 | 23.898 | 140 | 30.416 |

Comparison of the British and Russian Methods of stating Copper Prices.

Based on the equivalent: I rouble=2s. $1\frac{3}{5}d$. (see page 57). \pounds I per long ton of 2240 lbs.=0.15248195 rouble per pood.

| Price per long ton of 2240 lbs. in British pounds sterling. | Price in roubles per pood. | Price per long ton of 2240 lbs. in British pounds sterling. | Price in roubles per pood. | Price per long ton of 2240 lbs. in British pounds sterling. | Price in roubles per pood. |
|--|----------------------------------|--|----------------------------------|--|----------------------------------|
| £60 | 9.149 r. | £90 | 13.723 r. | £120 | 18.298 r. |
| 61 | 9.301 | 91 | 13.876 | 121 | 18.450 |
| 62 | 9.453 | 92 | 14.028 | 122 | 18.603 |
| 63 | 9.606 | 93 | 14.181 | 123 | 18.755 |
| 64 | 9.759 | 94 | 14.333 | 124 | 18.908 |
| 65 | 9.911 | 95 | 14.486 | 125 | 19.060 |
| 66 | 10.064 | 96 | 14.638 | 126 | 19.213 |
| 67 | 10.216 | 97 | 14.791 | 127 | 19.365 |
| 68 | 10.369 | 98 | 14.943 | 128 | 19.518 |
| 69 | 10.521 | 99 | 15.096 | 129 | 19.670 |
| 70 | 10.674 | 100 | 15.248 | 130 | 19.823 |
| 71 | 10.826 | IOI | 15.401 | 131 | 19.975 |
| 72 | 10.979 | 102 | 15.553 | 132 | 20.128 |
| 73 | 11.131 | 103 | 15.706 | 133 | 20.280 |
| 74 | 11.284 | 104 | 15.858 | 134 | 20.433 |
| 75 | 11.436 | 105 | 16.011 | 135 | 20.585 |
| 76 | 11.589 | 106 | 16.163 | 1 36 | 20.738 |
| 77 | 11.741 | 107 | 16.316 | 137 | 20.890 |
| 78 | 11.894 | 108 | 16.467 | 138 | 21.043 |
| 79 | 12.046 | 109 | 16.621 | 139 | 21.195 |
| 80 | 12.199 | 110 | 16.773 | 140 | 21.347 |
| 18 | 12.351 | III | 16.925 | 141 | 21.500 |
| 82 | 12.504 | II2 | 17.078 | 142 | 21.652 |
| 83 | 12.656 | 113 | 17.230 | 143 | 21.805 |
| 84 | 12.808 | 114 | 17.383 | I44 | 21.957 |
| 85 | 12.961 | 115 | 17.535 | 145 | 22.110 |
| 86 | 13.113 | 116 | 17.688 | 146 | 22.262 |
| 87 | 13.266 | 117 | 17.840 | 147 | 22.415 |
| 88 | 13.418 | 118 | 17.993 | 148 | 22.567 |
| 89 | 13.571 | 119 | 18.145 | 149 | 22.720 |
| 90 | 13.723 | 120 | 18.298 | 150 | 22.872 |

SECTION V. MINING AREAS OF DIFFERENT COUNTRIES.

AFRICA.

Transvaal.-The unit area for mining on proclaimed ground in the Transvaal is the Claim.

For vein and reef mining, the claim has an area of 60,000 square Cape feet. Where practicable it is rectangular in form, measuring 150 Cape feet along the strike by 400 Cape feet in a direction at right angles to the strike.

For alluvial gold mining the claim has an area of 22,500 square Cape feet. Where practicable it is square in form, measuring 150 by 150 Cape feet.

For diamond ('pipe') mining the claim has an area of 900 square Cape feet. Where practicable it is a square of 30 by 30 Cape feet.

For alluvial diamond mining the claim has an area of 1800 square Cape feet. Where practicable it is a rectangle measuring 60 by 30 Cape feet.

| A vein or reef claim | =64025.34 sq. British feet | $\log = 4.8063519$ |
|------------------------|----------------------------------|--------------------|
| | = 1.4698195592 acres | log=0.1672640 |
| | =0.694 morgen. | log=9.8416375 |
| I acre | =0.6803556217 reef claim. | $\log = 9.8327360$ |
| I morgen | = 1.44 reef claims. | log=0.1583625 |
| An alluvial gold claim | = 24009.5025 sq. British feet | log=4.3803832 |
| | =0.5511823347 acre | log=9.7412953 |
| | =0.260416 morgen. | $\log = 9.4156688$ |
| 1 acre = 1.81 | 4281658 alluvial gold claims. | log=0.2587047 |
| 1 morgen = 3.84 | alluvial gold claims. | log=0.5843312 |
| A diamond ('pipe') cl | aim=960.3801 sq. British feet | $\log = 2.9824432$ |
| | =0.0220472934 acres | log=8.3433553 |
| | =0.010416 morgen. | log=8.0177288 |
| 1 acre =45.3 | 5704155 diamond ('pipe') claims. | $\log = 1.6566447$ |
| I morgen $= 96 c$ | liamond ('pipe') claims. | log=1.9822712 |
| An alluvial diamond cl | aim = 1920.7602 sq. British feet | $\log = 3.2834732$ |
| | =0.044094587 acre | $\log = 8.6443853$ |
| | =0.02083 inorgen. | $\log = 8.3187588$ |
| | 785208 alluvial diamond claims. | $\log = 1.3556147$ |
| I morgen $=$ 48 a | alluvial diamond claims. | log=1.6812412 |

SECT. V.]

Orange River Colony.—For precious metal mining a reef claim on a public diggings has an area of 60,000 square Cape feet, and where practicable is rectangular in form, measuring 150 Cape feet along the strike by 400 Cape feet in a direction at right angles to the strike. An alluvial gold claim measures 150 by 150 Cape feet, and is either square or as nearly as possible the equivalent thereof.* A diamond ('pipe') claim is 30 by 30, and an alluvial diamond claim 90 by 90 Cape feet.† Concessions for the mining of base metals (including coal, oil, salt, etc.) can be granted by the Government or the private owner as the case may be.

| An alluvial dian | mond claim | =8643.4209 sq. British feet | $\log = 3.9366857$ |
|------------------|--------------|---------------------------------|--------------------|
| | | =0.19842564 acre | $\log = 9.2975978$ |
| | | =0.09375 morgen. | log=8.9719713 |
| I acre | = 5.03967 | 128 alluvial diamond claims. | log=0.7024022 |
| I morge: | n = 10.6 all | uvial diamond claims. | log=1.0280287 |
| For equivalents | of reef, all | uvial gold and diamond ('pipe') | claims, see under |
| Transvaal. | | | |

Cape Colony and British Bechuanaland.—A claim on a reef digging is a rectangle measuring 150 Cape feet in the direction of the strike by 800 Cape feet either across or on one side of the reef. On any Government land not proclaimed as a public diggings or on any abandoned public diggings a mining lease of an area not exceeding 100 morgen (211.654 acres) may be granted by the Governor. An alluvial gold claim is a square of 150 by 150 Cape feet. A diamond ('pipe') claim is usually 30 Cape feet square, and an alluvial diamond claim is usually 60 by 30 Cape feet, but the size of the claim to be pegged is stated by the Government on the proclamation of a diamond diggings. Mining concessions for coal, copper or any mineral except gold, silver and platinum are granted by the Government or the private owner, as the case may be.[‡]

| A reef claim | n=128050.68 square British feet | log=5.1073819 |
|--------------|---------------------------------|---------------|
| | =2.939639118 acres | log=0.4682940 |
| | = 1.38 morgen. | log=0.1426675 |
| I acre | =0.340177811 reef claim. | log=9.5317060 |
| I morger | n=0.72 reef claim. | log=9.8573325 |

For equivalents of alluvial gold, ' pipe' and alluvial diamond claims, see under Transvaal.

* The O.R.C. Precious Metals Ordinance of 1904.

+ The O.R.C. Precious Stones Ordinance of 1904.

[‡]Cape of Good Hope Colony, Precious Minerals Act of 1898 and Precious Stones Act of 1899.

Natal.—The claim for the mining of gold and other minerals, including coal, but excepting precious stones and alluvial minerals, must not exceed 300 by 300 yards (18.595 acres). A mineral claim for the mining of coal, limestone, stratified ironstone, slate, soapstone, and such minerals as may from time to time be included by order of the Governor in Council, must not exceed 700 by 700 yards (101.239 acres).* An alluvial claim for the mining of alluvial deposits of precious stones or minerals must not exceed 100 by 100 British feet (0.229 acre).

Rhodesia.—A reef claim is a rectangle of 150 by 600 Cape feet, the shorter sides of which are parallel to the strike of the reef. It carries the so-called 'extra-lateral right,' that is, the reef can be followed underground beyond the vertical planes in which the surface boundaries lie. Reef claims are pegged in blocks of 10, a block being under ordinary circumstances a parallelogram of 1500 by 600 Cape feet, and in no case of a greater area than 900,000 square Cape feet. An alluvial gold claim must, where possible, be a square of 200 by 200 Cape feet, and must in no case contain more than 40,000 square Cape feet. Coal mining locations of either 50, 100 or 150 morgen (105.827, 211.654 or 327.481 acres) are granted. A copper-mining location may be pegged of an area equivalent to not more than 30 reef claims of 90,000 square Cape feet each. No extra lateral rights exist in the mining of coal or copper locations.†

| A reef claim | =96038.01 sq. British feet | $\log = 4.9824432$ |
|--------------------------|-----------------------------|--------------------|
| | =2.20472934 acres | log=0.3433553 |
| | = 1.0416 morgen. | log=0.0177288 |
| I acre | =0.4535704155 reef claim. | $\log = 9.6566447$ |
| I morgen | =0.96 reef claim. | $\log = 9.9822712$ |
| A block of 10 reef claim | s=22.0472934 acres | $\log = 1.3433553$ |
| | = 10.416 morgen. | $\log = 1.0177288$ |
| An alluvial gold claim | =42683.56 sq. British feet | log=4.6302606 |
| | =0.9798797 acre | log=9.9911727 |
| | =0.4629 morgen. | $\log = 9.6655462$ |
| | 53343 alluvial gold claims. | $\log = 0.0088273$ |
| I morgen $= 2.16$ a | alluvial gold claims. | $\log = 0.3344538$ |
| | | |

* Natal Mines Act of 1899.

+ The British South Africa Company's Mining Ordinance of 1903.

IIO

MINING AREAS

SECT. V.]

The Gold Coast Colony and Ashanti.—Mining concessions obtained from natives must not exceed five square miles in area. This does not apply to concessions obtained and registered previous to October 1895.*

Egypt.—There is no definite limit as to the size of a mining lease, which may be granted by the Government at a price per *feddam* (.420083 hectare or 1.038086 acres), which varies according to the nature of the mineral to be mined. There is in addition a tax of 10% on all net profits accruing from the working of the lease.

Sudan.-The maximum areas of mining leases are :

| For | non-alluvial gold, | 64 | hectares | or | 160 | acres. |
|-----|--------------------|-----|----------|----|------|--------|
| " | silver, | 64 | " | ,, | 160 | " |
| ,, | any other metal, | 128 | ,, | ,, | 320 | " |
| " | oil, | 256 | " | ,, | 640 | " |
| " | coal, | 512 | " | ,, | 1280 | " |

Each lease must be rectangular in shape, and of a length not exceeding four times its breadth.[†]

AUSTRALASIA.

New South Wales.—A gold-mining lease must not exceed an area of 25 acres, except when the Secretary for Mines is "satisfied that special difficulties exist in working the ground either by way of great depth or wetness, or on account of the cost by appliances required." In such case a special lease is granted, the tenure, form and area of which is prescribed by the Governor. If an ordinary gold-mining lease not exceeding 25 acres be located on a quartz vein or lode, the maximum length (measured in the direction of the strike) is 600 yards and the maximum width (measured across the lode) 200 yards. "In no case shall the area be marked out so that the lode will be distant from either extremity of the boundaries defining the width of the said area less than one-tenth of such width, nor shall the length along the lode in any such area be

* The Gold Coast Colony and Ashanti Concessions Ordinance of 1900.

+Mining Laws of the British Empire, C. J. Alford, London, 1906, p. 35 et seq.

PART V.

greater than three times the width of such area."* All other gold-mining leases must be, where practicable, in the form of a parallelogram, the maximum length of which must not be more than twice the maximum breadth. "The area of a mining lease for any mineral shall not exceed 640 acres and (unless specially authorised by the Secretary for Mines) shall not be less than 40 acres for coal-mining lots, and shall not exceed 80 acres nor be less than 20 acres for other mineral lots."... "Mineral lots shall be measured in the form of a square, except in any case where the Minister shall authorise a departure from that form."[†]

Queensland.-The area of a gold-mining lease is limited to 12 acres until seven years from the date of the proclamation of the gold-field, or to 25 acres until fourteen years from the date of proclamation. After the expiration of this latter period the area of the lease may be extended to 50 acres if the ground in question has previously been worked and abandoned, or if, in the opinion of the Warden of the gold-field, the undue wetness or great depth of the workings and the consequent high working costs warrant the extension. A mining lease for silver, antimony or tin within the limits of any gold-field or mineral-field specially notified by proclamation shall not exceed 80 acres, and beyond such limits shall not exceed 120 acres. The maximum area of a mining lease for any other mineral except coal is 160 acres. A coal-mining lease may not be larger than 320 acres, except in the case of the discovery of a new seam of coal at least 15 miles from any known payable coal-field, or of a hitherto unknown coal seam at a depth of at least 600 feet. The discoverer in such case is entitled to a lease of 640 acres ‡ Wherever practicable, a mining lease must be rectangular in form, with the length not exceeding twice the breadth, but in special cases leases of irregularly shaped areas may be granted.

South Australia.—The maximum areas of mining leases are: for gold, 20 acres; for other minerals except coal, oil, salt and gypsum, 40 acres; for coal, oil, salt or gypsum, 640 acres.

* The New South Wales Mining Act of 1874, Section 36.

+ Regulations relating to Mineral Leases on Crown Lands, February 1885. [†] The Mining Act of Queensland, 1898.

II2

SECT. V.]

Any number of leases may be held by one person, but not more than four adjoining gold or mineral leases may be amalgamated.*

Victoria .- The maximum area of a gold-mining lease is 100 acres, while a mining lease for any other mineral (including coal) must not exceed 640 acres. There are no regulations as to the form of a mining lease.[†]

West Australia.- The maximum area of an ordinary goldmining lease is 24 acres; but where the ground has previously been worked for alluvial gold and afterwards abandoned, or where, in the opinion of the Warden, the working will be costly by reason of excessive wetness or great depth, a lease not exceeding 48 acres may be granted. The maximum area of a mining lease for all minerals, except gold and coal, is 48 acres. A coal-mining lease must not exceed 320 acres, except in the case of the discovery of a new seam of coal at least 15 miles from any known payable coal. The discoverer in such case is granted a lease of 640 acres free of royalty for ten years. ‡

Tasmania.-The maximum area of a gold-mining lease is 20 acres. A mining lease for coal, shale, slate, freestone or limestone must not exceed 320 acres, while the maximum area of a mining lease for any mineral except those already mentioned is 80 acres. If gold be found associated or combined with other minerals in such proportion that the amount recovered is of less value than that of the minerals with which it is associated or combined, the lease may have a maximum area of 80 acres. All mining leases must, where practicable, be square in form with the bearings of the boundary lines corresponding to the cardinal points of the compass. Two or more leases may be amalgamated.§

New Zealand .- The unit of mining area in New Zealand is the Claim. Claims may be either ordinary, extended or special. The maximum areas are: for an ordinary claim, I acre if under license, or 10,000 square feet if not under license; for an extended claim, 5 acres; and for a special claim, 100 acres.

H

The Mining Act of West Australia, 1904.

§ Tasmanian Mining Acts of 1900 and 1905.

H.M.

^{*} From the South Australian Mining Act of 1893.

⁺ The Victorian Mines Acts of 1890 and 1897.

The maximum lengths in the direction of the strike of the reef are: for an ordinary *quartz* claim 200 feet, and for an extended quartz claim 500 feet. The maximum lengths along the watercourse are: for an ordinary *dredging* or river claim, 3 chains (198 feet); for an extended dredging claim, 15 chains (990 feet): and for a special dredging claim, 1 mile. The maximum lengths of shore frontage are: for an ordinary *seabeach* claim, 200 feet; for an extended sea-beach claim, 500 feet; and for a special sea-beach claim, 1 mile. A special sea-beach claim may be extended beyond 100 acres * in the seawards direction.

NORTH AMERICA.

British Columbia.—From 1884 to 1892 the vein-mining claim of British Columbia was the same as that of the United States, namely, an area of 1500 by 600 feet, carrying the 'extra-lateral right.' The Mineral Act, however, was revised in 1891, and further augmented in 1896 and 1897. It now defines the unit of mining area as a rectangular claim not exceeding 1500 feet in either length or width (measured horizontally), with no extralateral right. The underground rights are therefore confined to the vertical planes in which the surface boundaries lie.

| A vein-mining | claim = 51.65289 acres | $\log = 1.7130946$ |
|---------------|------------------------|--------------------|
| | = 20.90315 hectares. | $\log = 1.3202116$ |
| I acre | =.01936 claim. | $\log = 8.2869054$ |
| 1 hectare | =.0478397 claim. | $\log = 8.6797884$ |

In 'creek diggings' a placer claim is 250 feet square, the side lines of which must run in the general direction of the watercourse or stream. In 'bar diggings' a placer claim may be either 250 feet square on any bar which is covered at high water, or 250 in length, and of the width contained between the highwater and the extreme low-water marks. In 'dry diggings' a claim is 250 feet square.

A placer claim must be as nearly as possible rectangular in form. The maximum length of a dredging lease is 5 miles. The maximum areas of leases for hydraulicing and precious stone diggings are 80 acres and 10 acres respectively. A coal or petroleum lease is a square block of a maximum area of 640 acres.

* New Zealand Mining Act, No. 38 of 1898.

SECT. V.]

Nova Scotia.—For gold and silver mining the unit area is a rectangle measuring 250 feet by 150 feet, laid off with the shorter sides running east and west. Any number of these areas, not exceeding 100, can be taken up. For the mining of other minerals an area of 5 square miles, not exceeding $2\frac{1}{2}$ miles in length, may be granted.

Quebec.—The total area of the mining concessions which can be acquired by one person is 400 acres, but under special circumstances the Lieutenant-Governor in Council may grant an area not exceeding 1000 acres.

Ontario.—A mining claim may be either 15 chains square $(22\frac{1}{2} \text{ acres})$ or 20 chains square (40 acres).

New Brunswick.—From 10 to 100 rectangular areas of 250 by 150 feet may be acquired for gold and silver mining. The boundaries must be laid off in the direction of the cardinal points of the compass. Mining leases of a maximum area of one square mile are granted for oil, natural gas or any mineral excepting gold and silver, but the Surveyor-General may, under special circumstances, sanction a larger lease.

Manitoba and the North-West Territories.—A gold quartz claim is a square of 1500 by 1500 feet without the extra-lateral right (see British Columbia).

Placer mining claims generally are 100 feet square. On the North Saskatchewan River, placer claims "are either bar or bench, the former being 100 feet long and extending between high and low-water mark. The latter includes bar diggings, but extends back to the base of the hill or bank, but not exceeding 1000 feet. Where steam power is used, claims 200 feet wide may be obtained."

Two dredging leases of five miles each may be obtained. "The lessee's right is confined to the submerged bed or bars of the river below low-water mark, and subject to the rights of all persons who have, or who may receive entries for bar diggings or bench claims, except on the Saskatchewan River, where the lessee may dredge to high-water mark on each alternate leasehold."

For iron and mica the maximum area of a location is 160 acres; a coal-mining location may not exceed 320 acres; and the

area of a petroleum location may not be larger than 1920 acres.

Yukon Territory.—A gold quartz claim is a square 1500 by 1500 feet, without the extra-lateral right (see British Columbia). Creek, gulch, river and hill claims may not exceed 250 feet in length, measured in the general direction of the creek or gulch, with a width of from 1000 to 2000 feet. All other placer claims are 250 feet square. For dredging, six leases, each five miles long, may be acquired. "The lessee's right is confined to the submerged bed or bars in the river below low-water mark, that boundary to be fixed by its position on the 1st day of August in the year of the date of the lease."

For iron, mica or copper mining, the Minister of the Interior may grant an area of 160 acres. The size of coal-mining areas is not defined, but applications for the purchase of such lands may be made to the Crown Timber and Land Agent. Petroleum leases of an area not exceeding 1920 acres (3 square miles) can also be acquired.

The United States.—The unit area for vein mining in the United States is the claim of 1500 feet along the strike of the vein by 600 feet in width. The 'law of the apex' gives the extra-lateral right, *i.e.* the vein may be followed beyond the vertical planes in which the surface boundaries lie, to an indefinite depth on all its 'dips, spurs and angles.'

| 1 vein-mining clai | m=20.661157 acres | $\log = 1.3151546$ |
|--------------------|-----------------------------|--------------------|
| | =8.3613 hectares. | log=0.9222742 |
| 1 acre | =.0484 vein-mining claim. | $\log = 8.6848454$ |
| I hectare | =.119585 vein-mining claim. | log=9.0777258 |

The maximum area of a *placer* claim is: for one person 20 acres, or for an association or company of eight or more persons, 160 acres.

The maximum area of a coal-mining location is: for one person 160 acres, or for an association or company of not less than four persons, 640 acres.

Mexico.—The unit area for the mining of all metals, also precious stones, rock-salt and sulphur, is the *Pertenencia*, which by a decree of President Diaz issued on June 4, 1892, with effect from July 1, 1892, is "a solid block of unlimited depth, defined above ground by that part of the surface which in

MINING AREAS

SECT. V.]

horizontal projection gives a square, each side of which measures 100 metres; and bounded underground by the four vertical planes corresponding to the sides of the said square."

| ı pertenenci | a=1 hectare | |
|--------------|------------------------|---------------|
| | =2.471058 acres. | log=0.3928830 |
| I acre | =0.404685 pertenencia. | log=9.6071170 |

SOUTH AMERICA.

British Guiana.—A gold-mining claim must not exceed 1500 feet in length by 800 feet in width. A claim located for the purpose of searching for precious stones must not exceed 1500 feet in length by 800 feet in width, nor contain a greater area than 500 acres. A claim must, where practicable, be rectangular in form and it is limited underground by the vertical planes in which the surface boundaries lie.*

Colombia.—The unit area for vein mining is 600 by 240 metres, and for alluvial mining 5 by 2 kilometres.†

| I vein-mining area | = 14.4 hectares | $\log = 1.1583625$ | |
|--|-----------------------------|--------------------|--|
| | = 35.583235 acres. | log=1.5512455 | |
| I hectare | =.0694 vein-mining claim. | $\log = 8.8416375$ | |
| I acre | =.028103 vein-mining claim. | $\log = 8.4487545$ | |
| I alluvial-mining area = 10 sq. kilometres | | | |
| | = 1000 hectares | | |
| | =2471.05814 acres | $\log = 3.3928830$ | |
| | = 3.86103 square miles. | log=0.5867030 | |

Chile.—For coal the mining area or pertenencia is 50 hectares (123.5529 acres); while for any other mineral it may be from 1 to 5 hectares (2.47106 to 12.3553 acres). There is no 'extralateral right.' ‡

Peru.—The mining area or pertenencia for gold, silver, platinum, lead, tin, copper, antimony, zinc, coal or petroleum is a square of 200 by 200 metres (4 hectares or 9.88423 acres), while a pertenencia located on a deposit of borax, sulphur or any other non-metallic mineral is half that size

* British Guiana Mining Regulations, 1903.

⁺H. G. Granger and E. B. Treville, p. 85, *Trans. Am. Inst. M.E.*, vol. 28, 1899.

‡ Chilian Mining Law of 1888.

(2 hectares or 4.942116 acres). The maximum holding is limited to 240 hectares (593.05395 acres, 60 large or 120 small pertenencias). There is no 'extra-lateral right.'

ASIA.

British India.—The Collector of any district in British India can grant a prospecting license carrying with it the right to a lease for 30 years on a block of ground of any size not exceeding I square mile, provided the ratio of the length (in the direction of strike of the vein) to the breadth does not exceed 4 to I. Applications for more than I square mile are dealt with by the Board of Revenue.

In the Native State of Mysore, the size of the mining area granted to one applicant is limited to 2 square miles.

Ceylon.—On Crown lands, mining leases for one or more blocks, each of which must be over 10 and not more than 100 acres in extent, may be granted by the Governor, but the total area held by the lessee or by those joined in interest with him must not exceed 500 acres. Except when specially sanctioned, the length of a block must not exceed four times its breadth.*

Malay Peninsula.—Mining leases for large areas are granted by the Sultan of Pahang on the recommendation of the British Resident; but mining permits giving the holder the right to dig for gold and tin within an area of 5 acres are also granted.[†]

Russian Empire.—For vein-mining the maximum area of an *Otwod* or concession is 1 square verst (1.138062 square kilometres or .439408 square mile). The ratio of the length (in the direction of the strike of the vein) to the breadth must not exceed 3 to 1.

For alluvial mining in Siberia, the length of the concession is limited to 5 versts (5.3340 kilometres or 3.314394 miles), while the breadth may extend to the full width of the valley in which the auriferous gravels lie. In the Urals the size of

* From Mining Laws of the British Empire, by C. J. Alford, London, 1906, p. 64.

+ The States of Pahang Mining Enactment of 1904.

MINING AREAS

an alluvial concession is limited to 1 square verst (1.138062 square kilometres or .439408 square mile), the maximum length being 5 versts (5.3340 kilometres or 3.314394 miles) and the minimum breadth 100 sagenes (213.36 metres or 700 feet).*

Japan.—The right to exploit alluvial gold, iron-sand or stream tin deposits is restricted to Japanese subjects, but foreign companies registered under, and conforming to, the laws of the country are permitted to mine all minerals occurring otherwise than as alluvial deposits.

The area of a mining concession for any mineral except coal must not be less than 3000 tsubo (2.45064 acres or .99173553 hectare) or more than 600,000 tsubo (490.128 acres or 198.347106 hectares). A coal concession must not be less than 10,000 tsubo (8.1688 acres or 3.3057851 hectares) or more than 600,000 tsubo. If two or more concessions be amalgamated, the combined areas may exceed 600,000 tsubo.†

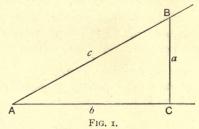
* Code Minière Russe, St. Petersburg, 1893, p. 105.

+ From Sketch of the Mining Industry of Japan, published by the Japanese Bureau of Mines in 1904.

PART VI. DATA RELATING TO SURVEYING.

SECTION I. TRIGONOMETRICAL AND MISCELLANEOUS FORMULÆ AND CONSTANTS.

LET A be any acute angle, and let a perpendicular BC be drawn from any point in one side to the other side. Then, if the sides

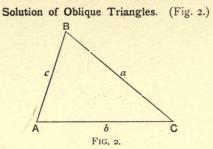


of the right triangle thus formed are denoted by letters, as in the figure, we have these six formulæ:

| 1 . sin | $A = \frac{a}{c}$. | 4. | $\operatorname{cosec} A = \frac{c}{a}.$ |
|----------------|---------------------|----|---|
| 2. cos | $A = \frac{b}{c}$ | 5. | $\sec A = \frac{c}{b}.$ |
| 3. tan | $A = \frac{a}{b}$. | 6. | $\cot A = \frac{b}{a}.$ |

Solution of Right Angles. (Fig. 1.)

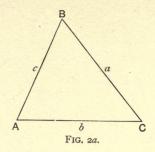
| | GIVEN. | Sought. | Formulæ. | | |
|-----|--------|--------------------|--|---------------------------|--|
| 7. | а, с | A, B; b | $\sin A = \frac{a}{c}, \qquad \cos B = \frac{a}{c},$ | $b = \sqrt{(c+a)(c-a)}.$ | |
| 8. | a, b | A, B, c | $\tan A = \frac{a}{b}, \cot B = \frac{a}{b},$ | $c = \sqrt{a^2 + b^2}.$ | |
| 9. | A, a | B, b, c | $B=90^\circ-A, b=a\cot A,$ | $c = \frac{a}{\sin A}$. | |
| 10. | A, b | B, a, c | $B=90^\circ-A, \ a=b\tan A,$ | $c = \frac{b}{c \ s \ A}$ | |
| 11. | A, c | B, a, c B, a, b | $B=90^\circ-A, a=c\sin A,$ | | |



| $\frac{(b)(s-c)}{bc};$ |
|-----------------------------|
| $\frac{(-b)(s-c)}{s(s-a)};$ |
| |
| |
| |
| (-b)(s-c). |
| |

General Trigonometrical Formulæ.

| 19. | $\sin^2 A + \cos^2 A = \mathbf{I}.$ |
|-----|--|
| 20. | $\sin (A \pm B) = \sin A \cos B \pm \sin B \cos A.$ |
| 21. | $\cos (A \pm B) = \cos A \cos B \mp \sin A \sin B.$ |
| 22. | $\sin 2A = 2\sin A\cos A.$ |
| 23. | $\cos 2A = \cos^2 A - \sin^2 A = I - 2\sin^2 A = 2\cos^2 A - I.$ |
| 24. | $\sin^2 A = \frac{1}{2} - \frac{1}{2} \cos 2A.$ |
| 25. | $\cos^2 A = \frac{1}{2} + \frac{1}{2} \cos 2A.$ |



General Trigonometrical Formulæ-continued.

| 26. | $\sin A + \sin B = 2 \sin \frac{1}{2}(A + B) \cos \frac{1}{2}(A - B).$ |
|-----|--|
| 27. | $\sin A - \sin B = 2\cos \frac{1}{2}(A+B)\sin \frac{1}{2}(A-B).$ |
| 28. | $\cos A + \cos B = 2 \cos \frac{1}{2}(A + B) \cos \frac{1}{2}(A - B).$ |
| 29. | $\cos B - \cos A = 2 \sin \frac{1}{2}(A+B) \sin \frac{1}{2}(A-B).$ |
| 30. | $\sin^2 A - \sin^2 B = \cos^2 B - \cos^2 A = \sin(A+B)\sin(A-B),$ |
| 31. | $\cos^2 A - \sin^2 B = \cos \left(A + B\right) \cos \left(A - B\right).$ |
| 32. | $\tan A = \frac{\sin A}{\cos A}.$ |
| 33. | $\cot A = \frac{\cos A}{\sin A}.$ |
| 34. | $\tan(A \pm B) = \frac{\tan A \pm \tan B}{\mathbf{I} \mp \tan A \tan B}.$ |
| 35. | $\tan A \pm \tan B = \frac{\sin (A \pm B)}{\cos A \cos B}.$ |
| 36. | $\cot A \pm \cot B = \pm \frac{\sin (A \pm B)}{\sin A \sin B}.$ |
| 37. | $\frac{\sin A + \sin B}{\sin A - \sin B} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}.$ |
| 38. | $\frac{\sin A + \sin B}{\cos A + \cos B} = \tan \frac{1}{2}(A + B).$ |
| 39. | $\frac{\sin A + \sin B}{\cos B - \cos A} = \cot \frac{1}{2}(A - B).$ |
| 40. | $\frac{\sin A - \sin B}{\cos A + \cos B} = \tan \frac{1}{2}(A - B).$ |
| 41. | $\frac{\sin A - \sin B}{\cos B - \cos A} = \cot \frac{1}{2}(A+B).$ |
| 42. | $\tan \frac{1}{2}A = \frac{\sin A}{1 + \cos A}.$ |
| 43. | $\cot \frac{1}{2}A = \frac{\sin A}{\mathbf{I} - \cos A}.$ |
| | |

SECT. 1.] FORMULÆ AND CONSTANTS

Miscellaneous Formulæ.

| | Sought. | GIVEN. | Formulæ. | |
|-----|---|--|---|--|
| | Area of | | | |
| 44. | Circle, | Radius= r , | πr^2 . | |
| 45. | Ellipse, | Semi-axes $= a$ and b , | πab. | |
| 46. | Parabola, | Chord $= c$, height $= h$, | 23ch.* | |
| 47. | Regular Polygon, | $\left\{ \begin{array}{l} \text{Side} = a, \\ \text{number of sides} = n, \end{array} \right\}$ | $\frac{1}{4}a^2n\cot\frac{180^\circ}{n}.$ | |
| | Surface of | | | |
| 48. | Sphere, | Radius= r , | $4\pi r^{2}$. | |
| 49. | Zone, | Radius= r , height= h , | 2 <i>πrh</i> . | |
| 50. | Spherical Polygon, | $ \left\{ \begin{array}{l} \text{Radius of sphere } = r, \\ \text{sum of angles } = S, \\ \text{number of sides} = n, \end{array} \right\} $ | $\pi r^2 \times \frac{S - (n-2) \mathrm{I80^\circ}}{180^\circ}$ | |
| | Solidity of | | | |
| 51. | Prism or Cylinder, | Base = b , height = h , | bh. | |
| 52. | Pyramid or cone, | Base = b , height = h , | 13bh | |
| 53. | {Frustum of Pyra- mid or Cone, } | $ \left\{ \begin{array}{l} \text{Bases} = b \text{ and } b_1, \\ \text{height} = h, \end{array} \right\} $ | $\frac{1}{3}h(b+b_1+\sqrt{bb_1}).$ | |
| 54. | Sphere, | Radius = r , | $\frac{4}{3}\pi\gamma^{3}$. | |
| 55. | Spherical Segment, | $ \left\{ \begin{array}{l} \text{Radii of bases} = r \text{ and } r_1, \\ \text{height} = h, \end{array} \right\} $ | $\frac{1}{2}\pi h (r^2 + r_1^2 + \frac{1}{3}h^2).$ | |
| 56. | Prolate Spheroid, | (Semi-transverse axis of) | - | |
| | | $\int ellipse = a,$ | $\frac{4}{3}\pi ab^{2}$. | |
| 57. | Oblate Spheroid, | $\begin{cases} \text{Semi-conjugate axis of} \\ \text{ellipse} = b, \end{cases}$ | 4-24 | |
| 58. | Paraboloid, | $\begin{cases} \text{Radius of base} = r, \\ \text{height} = h, \end{cases} $ | $\frac{1}{2}\pi r^2h.$ | |
| | $\pi = 3.1415926536 ; \text{ logarithm} = 0.4971498727.$ $\pi^{2} = 9.8696044011 ; ,, = 0.9942997454.$ $\sqrt{\pi} = 1.7724538509 ; ,, = 0.2485749363.$ | | | |

* The area of a circular segment on railroad curves, where the chord is very long in proportion to the height, may be found with great accuracy by this formula.

DATA RELATING TO SURVEYING [PART VI.

Physical Constants.

Velocity of light (Harkness)

= 186,337 miles per second = 299,878 kilometres per second.

Velocity of sound through dry air

= $1090\sqrt{1+0.00367t}$ feet per second, = temperature in degrees Centigrade.

The general mean deduced by Rowland (*Proc. Am. Acad.*, vol. xv., p. 144) for dry air at 0° C.

= 331.75 metres per second = 1088.42 feet per second.

| Velocity in metres per sec. | Velocity in feet per sec. | Authority. | | | |
|--|---|---|--|--|--|
| 3950 | 12,960 | Gray and Milne. | | | |
| 3810 | 12,500 | 3 7 3 7 | | | |
| 4510 | 14,800 | »» »» | | | |
| 3652 | 11,980 | Chladni. | | | |
| | | | | | |
| Pine, along the fibre, - 3320 10,900 Wertheim. | | | | | |
| - 3850 | 12,620 | " | | | |
| - 4670 | 15,310 | >> | | | |
| - 1437 | 4714 | Martini. | | | |
| | metres per sec. 3950 3810 4510 3652 , - 3320 - 3850 - 4670 | metres per sec. feet per sec. 3950 12,960 3810 12,500 4510 14,800 3652 11,980 , - 3320 10,900 - 3850 12,620 - 4670 15,310 | | | |

From the Smithsonian Physical Tables, p. 100.

Astronomical Constants (Harkness).

Sidereal year = 365.2563578 mean solar days. Sidereal day = 23 hours 56 min. 4.100 seconds mean solar time. Mean solar day = 24 hours 3 min. 56.546 seconds sidereal time. Mean distance of the earth from the sun = 92,800,000 miles.

Geodetic Constants.

Dimensions of the earth (Clarke's spheroid): Equatorial semi-axis 3963.3 miles. Polar ,, 3949.8 ,, Perimeter of meridian ellipse 24,854.76 miles. Circumference of equator 24,901.96 ,, Area of earth's surface 196,940,400 sq. miles. Mean density of the earth (Harkness) 5.576±0.016. Surface density of the earth (Harkness) 2.56±0.16.

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where t

SECT. I.] FORMULÆ AND CONSTANTS

Acceleration of gravity at sea-level (Harkness)

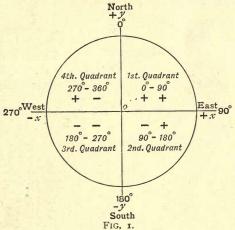
= 980.60 ($r - 0.002662 \cos 2\phi$) centimetres per second, where ϕ = the latitude. Length of seconds pendulum (Harkness)

= 0.990910 + 0.005290 $\sin^2 \phi$ metres,

where $\phi =$ the latitude.

SECTION II. THE COORDINATION OF SURVEY POINTS.

The permanent stations of a modern survey are usually plotted by means of rectangular coordinates, the use of the protractor being restricted to the draughting of the temporary points and



detail. The customary method of coordinating a survey is as follows:

The most prominent and central station of the survey, from which the direction of the true meridian has been determined, is selected as the 'point of origin' o. At this point two fixed *axes*, y and x, are assumed to intersect at right angles, the direction of the y axis being made to coincide with the true meridian. From the starting point o, the *latitude* (distance north or south) and the *departure* (distance east or west) of each station of the survey are calculated, the latitudes being the y and the departures the x coordinates.

DATA RELATING TO SURVEYING PART VI.

The γ coordinates to the north of, and the x coordinates to the east of o are positive and carry a plus sign, while those to the south of and to the west of o are negative and carry a minus sign. They are stated with the ys before (to the left of) the xs; thus +950.13-726.48 may represent the coordinates of a point 950.13 units north of, and 726.48 units west of o. From o, the bearing of the true north (along the y axis) is taken as 360° or 0° , the east (along the x axis) as 90° , the south as 180° and the west as 270°. Therefore, if the coordinates of a point carry the signs : + +, its bearing from o is in the 1st quadrant between o° and 90° - +. 2nd " ,, 90° •• 180° " ,, ,, 180° 270° - -, 3rd ,, ,, ,, ,, ,, 270° 4th 360° + -, 27 ,, ,, " 22

Coordinates are usually calculated by means of logarithms and checked by natural sines and cosines, using 'short' multiplication.*

EXAMPLE. Given the measured lengths

oA = 377.92, AB = 1015.74 and BC = 284.63,

and the observed angles $y_0A = 47^{\circ} 19' 20''$ (the bearing of the line oA), $oAB = 83^{\circ} 47' 40''$ and $ABC = 321^{\circ} 33' 50''$. The coordinates of the points A, B and C are calculated as follows :

To Determine A.

Check.

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| | (By logarithms.) | | (By nat. sines and cosines.) | |
|---|------------------|-------------------------------|------------------------------|----------------|
| Length $oA = 377.92$ Bearing $oA = 47^{\circ} 19' 20''$ co | = 2.5773999 | =2.5773999 sin = 0.8662022 | 37792 78776 | 37792 81537 |
| Dearing 011-47 19 20 C | 2.4085492 | 2.4437921 | 22675 2645 | 26454 1134 |
| | + 256.18 | + 277.84 | 265 | 189 |
| | $o = \pm 0.00$ | ± 0.00 | 33 | 7 |
| | A = +256.18 | + 277.84 | +256.18 | + 277.84 |

* Rule for 'short' multiplication: Reverse the multiplier and place it below the multiplicand so that its unit figure (the one preceding the 10375 decimal point) is directly under that decimal place of the 54493 multiplicand to which the product is required. For example, 311250 to multiply 103.75 by 39.445, the product being required 93375 to two decimal places, the unit figure 9 is placed under the 5. 4150

Therefore in checking by natural sines and cosines, in order to get the product to two decimal places reverse the function and place its initial figure under the first decimal place of the multiplicand. (See the above calculation, where .67787=the 4092.42 nat. cos of 47° 19' 20").

SECT. II.] COORDINATION OF SURVEY POINTS

| | To Determi | ine B. | | |
|----------------------------------|--------------------|--------------------|----------|----------|
| Length $AB = 1015.74$ | = 3.0067826 | = 3.0067826 | Ch | eck. |
| Bearing A0=227° 19' 20" | | | 101574 | 101574 |
| Angle $oAB = 83^{\circ}47'40''$ | | | 495756 | 75337 |
| Bearing $AB = 311^\circ 7' 00''$ | $\sin = 9.8179581$ | $\cos = 9.8770096$ | 60944 | 71102 |
| | 2.8247407 | 2.8837922 | 5079 | 5079 |
| | | | 711 | 305 |
| 4 | +667.95 | - 765.23 | 61 | 37 |
| | A = +256.18 | +277.84 | + 667.95 | - 765.23 |
| and the second | <i>B</i> = +924.13 | - 487.39 | +924.13 | |
| | | | | |

To Determine C.

| Length $BC = 284.63 = 2.4542807$ | =2.4542807 | Checi | k. |
|---|-------------|-----------|--------|
| Bearing $BA = 131^{\circ} 7' 00''$ | 151 | 28463 | 28463 |
| Angle $ABC = 321^{\circ} 33' 50''$ | | 77640 | 19899 |
| Bearing $BC = 92^{\circ} 40' 50'' \sin = 8.6699437 \cos^{10}{10}$ | 5=9.9995245 | 1138 | 25617 |
| I.1242244 | 2.4538052 | 171 | 2562 |
| 1.1242244 | 2.4530052 | 20 | 228 |
| - 13.31 | + 284.32 | 2 | 25 |
| B = +924.13 | - 487.39 | - 13.31 + | 284.32 |
| C = +910.82 | - 203.07 | +910.82 - | 203.07 |

The bearing of a line = that of the backsight + its angle with reference to the backsight (measured clockwise, from left to right); and the bearing of the line used as a backsight differs by 180° from its bearing when a foresight. For example, in the above calculations the bearing of the line oA is 47° 19' 20"; therefore, when used as a backsight from the station A, its bearing is 47° 19' 20" + $180^{\circ} = 227^{\circ}$ 19' 20", which, added to the observed angle oAB which Ao makes with AB, gives the bearing of the line AB.

Similarly the bearing $BC = (\text{the bearing } AB - 180^\circ) + \text{the angle } ABC$, which sum, being greater than 360°, has that amount deducted from it. A bearing is denoted by the prefix y. For example, yAB signifies the bearing of the line AB, or its direction with reference to y (the true north, 0°).

If the bearing of a line be in the 1st quadrant, its length \times the cosine of the bearing is the y distance or latitude,

., \times the sine ,, ,, x ,, departure ; if in the 2nd quadrant,

its length × the sine of the (bearing -90°) is the y distance or lat., ,, × the cosine ,, x , departure ;

if in the 3rd quadrant,

its length × the cosine of the (bearing - 180°) is the y distance or lat., ,, × the sine ,, ,, x, departure; and if in the 4th quadrant,

its length \times the sine of the (bearing -270°) is the y distance or lat., ,, \times the cosine ,, ,, ,, y, departure. To coordinate any point B which has been fixed from a coordinated point A, the y and the x distances of B from A are added algebraically to the coordinates of A. For example, in the foregoing calculations the y distance AB = +667.95, and the x distance AB = -765.23, which, when added algebraically to the coordinates of A, give the coordinates of B with reference to the point of origin o.

Method used in calculating the length and bearing of a line connecting two coordinated points :

| | C, | heck. |
|--------------------------|-------------|----------|
| A = +256.18 + 277.84 | 101574 | 101574 |
| B = +924.13 - 487.39 | 495756 | 73357 |
| Diff. = +667.95 - 765.23 | 60944 | 71102 |
| | 5079 | 5079 |
| | 711 | 305 |
| | 61 | 37 |
| 667.95 = 2.8247440 | +667.95 | - 765.23 |
| 765.23=2.8837920 | 1 | |
| . 9.9409320=tan | 41° 7′ 00″ | |
| | 270° 0' 00″ | |

 $\begin{array}{c} \text{cosine } 41^{\circ} 7' \circ 0'' = 9.8770096 \\ \text{(Subtracted from } \log 765.23) \\ 3.0067824 = 1015.74 = \text{length } AB. \end{array}$

The signs before the y and x differences of the coordinates of the two points indicate the quadrant in which the bearing of the connecting line lies. Divide the y difference by the x difference. Then:

| | the cotangent of | the l | bearing | | if in th | e Ist o | quadrant. |
|-----------------|------------------|-------|---------|---------|----------|---------|-----------|
| y difference | the tangent of | (the | bearing | - 90°) | ••• | 2nd | ,, |
| x difference | the cotangent of | (- | ,, | - 180°) | ,, | 3rd | " |
| 1- 10 - 10 - 10 | the tangent of | (| ** | - 270°) | ,, | 4th | ,, |

For example, in the foregoing calculation, as the differences carry the signs + -, the bearing is in the 4th quadrant. Consequently $\frac{667.95}{765.23}$ = the tangent of 41° 7′ 00″, which, $+ 270^\circ$, $= 311^\circ 7' 00″ = yAB$.

SECT. II.] COORDINATION OF SURVEY POINTS

The distance between the two points =

 $\frac{y \text{ difference}}{\text{cosine of the bearing}} \text{ or } \frac{x \text{ difference}}{\text{sine of the bearing}}$ if the bearing be in the 1st quadrant.

 $\frac{y \text{ difference}}{\text{the sine of (the bearing - 90°)}} \text{ or } \frac{x \text{ difference}}{\text{cosine of (the bearing - 90°)}}$ if the bearing be in the 2nd quadrant.

 $\frac{y \text{ difference}}{\text{cosine of (the bearing - 180°)}} \text{ or } \frac{x \text{ difference}}{\text{sine of (the bearing - 180°)}}$ if the bearing be in the 3rd quadrant.

 $\frac{y \text{ difference}}{\text{sine of (the bearing - 270°)}} \text{ or } \frac{x \text{ difference}}{\text{cosine of (the bearing - 270°)}}$ if the bearing be in the 4th quadrant.

For example, in the foregoing calculation the bearing is in the 4th quadrant. Consequently $\frac{765.23}{\text{cosine } 41^\circ 7' \circ 0''} = 1015.74$, the length of the line *AB*.

Method used, in calculating the coordinates of a triangulation.

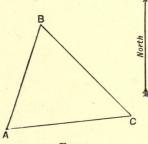


FIG. 2.

Given the coordinates of the points A and C, and by observation the interior angles of the triangle ABC. Required the coordinates of the point B.

| Angles. | Coordinates. | |
|---------------------------|------------------------|--|
| $A = 72^{\circ} 15' 30''$ | y x | |
| $B = 51^{\circ} 55' 40''$ | A = +7230.91 + 538.64 | |
| $C = 55^{\circ} 48' 50''$ | C = +8522.77 + 9367.05 | |

The first step is to determine the length and bearing of the line AC:

| A = +7230.91 + 538.64 | Check. | | | |
|--|-----------|----------|--|--|
| C = +8522.77 + 9367.05 | 892243 | 892243 | | |
| + 1291.86 + 8828.41 | 887441 | 364989 | | |
| The second second second second | 89224 | 803019 | | |
| 3.1112155 | 35690 | 71379 | | |
| 3.9458825 | 3569 | 8030 | | |
| 8x° 10' 00'' 11' | 625 | 357 | | |
| 9.1653330=81° 40′ 30″= <i>yAC</i> 9.9953994 | 78 | 56 | | |
| 3.9504831=8922.43= <i>AC</i> . | + 1291.86 | +8828.41 | | |

The coordinates of B are then determined from the two sides AB and CB, each calculation acting as a check on the other. The lengths of these sides are:

AB = AC sine C cosecant B, and BC = AC sine A cosecant B; and their bearings are derived from the known bearing yAC, and the observed angles of the triangle. The logarithm of the cosecant of B is got by subtracting the logarithm of the sine from 10.0000000. This is most easily done by subtracting each figure from 9, except the right-hand one, which is subtracted from 10.

| $yAC = 81^{\circ} 40' 30''$ $A = 72^{\circ} 15' 30''$ | | | $yCA = 261^{\circ}$ $C = 55^{\circ}$ | 40' 30" 48' 50" |
|--|-----------|--------|--------------------------------------|--------------------|
| $yAB = 9^{\circ} 25' 00''$ | | | $\gamma CB = 317^{\circ}$ | 29' 20" |
| | | | $B = 51^{\circ}$ | |
| log 8922.43 = 3.9504832 | (| Check) | $yAB = 9^{\circ}$ | 25' 00" |
| cosec B = 0.1038961 | | | | |
| $\sin A = 9.9788377$ | | | | |
| $\sin C = 9.9176193$ | | | | |
| 1 47 | | 1 00 | | |
| $\log AB = 3.9719986$ | 3.9719986 | | = 4.0332170 | 4.0332170 |
| <i>yAB</i> =9.9941079 | 9.2138176 | yCB | =9.8675537 | 9.8297752 |
| 3.9661065 | 3.1858162 | | 3.9007707 | 3.8629922 |
| + 9249.25 | +1533.97 | | + 7957.39 | - 7294.44 |
| A = + 7230.91 | + 538.64 | C | = + 8522.77 | +9367.05 |
| B = +16480.16 | + 2072.61 | B | + 16480.16 | +2072.61 |

SECT. II.] COORDINATION OF SURVEY POINTS

The method of calculating the lengths of the sides AB and CB is not clear in the finished calculation. It is as follows: First, to determine the length AB,

> $\log 8922.43 = 3.9504832$ cosec B = 0.1038961 $\sin A =$ $\sin C = 9.9176193$ $\log AB = 3.9719986$

the space for the log sin A being left blank. Then, to determine

the length CB, $\log \sin A$ is filled in, and the sum of the three top lines = $\log CB$, which is placed to the right of the repeated log AB.

Then, as already described, $AB \times$ the cos and sin of γAB (1st quadrant) = the latitude and departure of B from A; and $CB \times$ the sin and cos of $\gamma CB - 270^{\circ}$ (4th quadrant) = the latitude and departure of B from C.

Calculation of the area of a figure from its coordinates.

Area =
$$\frac{\text{sums of the } y \text{s} \times \text{diffs. of the } x\text{s}}{2}$$
 or $\frac{\text{sums of the } x \text{s} \times \text{diffs. of the } y\text{s}}{2}$

The sum and difference of the coordinates of each two adjoining points is taken separately, and the sum of the products is divided by 2, care being taken to distinguish between the positive and the negative signs when making the addition. The computation is checked by calculating by each way separately, using either 'short' multiplication or logarithms as preferred, the former method being the more accurate for dealing with large amounts.

For example, in the triangle ABC we have the coordinates :

A = + 7230.91 + 538.64 B = +16480.16 + 2072.61C = + 8522.77 + 9367.05

| | Sums of the ys. Diffs. of the xs. |
|----|---|
| AB | $+23711.07 \times +1533.97 = +36,372,070.04$ |
| BC | $+25002.93 \times +7294.44 = +182,382,372.71$ |
| CA | $+15753.68 \times -8828.41 = -139,079,946.05$ |
| | + 79,674,496.70 |
| | $\div 2 = 39,837,248.35$ |

Check.

Sums of the xs. Diffs. of the ys. $AB + 2611.25 \times +9249.25 = +24,152,104.06$ $BC + 11439.66 \times -7957.39 = -91,029,836.09$ $CA + 9905.69 \times -1291.86 = -12,796,764.68$ -79,674,496.69 $\div 2 = 39,837,248.35$ Area ABC = 39,837,248.35 square units.

The calculation of an area may often be simplified by deducting either a positive or a negative constant from each of the ys, and similarly, another positive or negative constant from each of the xs.

For example, in the foregoing calculation +7000y and +500x may be deducted from the coordinates of A, B and C, giving :

y xA = + 230.91 + 38.64B = +9480.16 + 1572.61C = + 1522.77 + 8867.05

Sums of the ys. Diffs. of the xs.

 $\begin{array}{rcl} AB &+ & 9711.07 \times + 1533.97 = + 14,896,490.05 \\ BC &+ & 11002.93 \times + 7294.44 = + 80,260,212.71 \\ CA &+ & 1753.68 \times - 8828.41 = - & 15,482,206.05 \end{array}$

+79,674,496.71 $\div 2 = 39,837,248.35$

Check.

Sums of the xs. Diffs. of the ys.

 $\begin{array}{rcl} AB &+ & 1611.25 \times +9249.25 = + & 14,902,854.06 \\ BC &+ & 10439.66 \times - & 7957.39 = - & 83,072,446.08 \\ CA &+ & 8905.69 \times - & 1291.86 = - & 11,504,904.68 \end{array}$

-79,674,496.70 $\div 2 = 39,837,248.35$ Area *ABC*=39,837,248.35 square units.

Calculation of the coordinates of a point, the angles which it makes with three coordinated points having been observed.

Given the coordinates of the points A, C and B, and the observed angles ARC and BRC which subtend these points at R. Required the coordinates of the point R (Fig. 3).

Describe a circle cutting A, B and R. Join RA, RB, RC

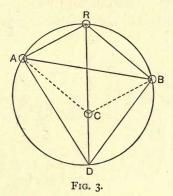
SECT. II.] COORDINATION OF SURVEY POINTS 133

and AB. Produce RC to the circumference of the circle at D, and join AD and BD. Then:

the observed angle ARD = the angle ABDand the observed angle BRD = the angle BAD,

as they subtend the same chords AD and BD. Determine the length and bearing of AB and coordinate D from the triangle ABD. Then calculate the bearing yCD which = the bearing yRD. Determine yRA and yRB from yRC and the angles ARD and BRD, and coordinate R from the triangle ABR.

It is apparent that the calculation will not be accurate when the middle point C is close to the circumference of the circle,



and quite impossible when C is cut by the circle. It is therefore advisable to first add the observed angles ARC and BRC to the known angle ACB; if their sum be 180°, all four points will be cut by the circle, as the opposite angles of a quadrilateral inscribed within a circle are together equal to 180°. Therefore, when the sum of the angles ARC, BRC and ACB is more than 180°, C is inside the circle and yCD=yRD; and when it is less than 180°, C is outside the circle and yCD=yDR.

R may also be calculated by the following formula:

Let $T = (\angle RBC + \angle RAC) = 360^{\circ} - (\angle ACB + \angle ARC + \angle BRC)$. When T is 90° or under,

 $\cot an RBC = \cot an T \left(\frac{BC \sin ARC}{AC \sin BRC \cos T} + \mathbf{I} \right).$

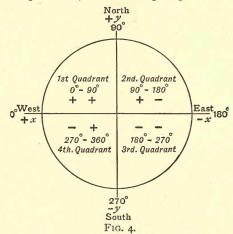
DATA RELATING TO SURVEYING [PART VI.

When T is between 90° and 180°, the 1 in the formula is negative instead of positive, thus:

 $\cot an RBC = \cot an T \left(\frac{BC \sin ARC}{AC \sin BRC \cos T} - \mathbf{I} \right).$ R is then coordinated from the triangle CBR.

The Cape System.

In South Africa, a method of coordination which is known as the *Cape System* is in general use. It differs from the conventional method in that the x axis is positive to the *west*, which is taken as 360° or 0° , and the bearings are therefore stated with reference to the west instead of to the north, the bearing of a line being consequently denoted by the prefix x instead of y. It is best explained by the following diagram :



The methods of calculation are similar to those already described, but the arrangement of the quadrants is of course quite different. Therefore, if the bearing of a line be:

In the set quart (its length \times the sin of the bearing is the y distance.

| In the 1st quadrant, J | >> | x ,, cos | ,, | ,, ,, x ,, | |
|------------------------|----|-----------------|----|--|--|
| | | | | | |
| », 2nd », l | ,, | × ,, sin | ,, | (bearing -90°) is the y distance. (,, ,,) ,, x ,, | |
| ard f | ,, | \times ,, sin | ,, | (bearing $- 180^{\circ}$) ,, y ,, (,, ,,) ,, x ,, | |
| | | | | | |
| , ath | ,, | × ,, cos | ,, | (bearing -270°) ,, y ,, (,, ,,) ,, x ,, | |
| » 4 ¹¹ » (| ,, | \times ,, sin | ,, | (,, ,,),, <i>x</i> ,, | |

SECT. II.] COORDINATION OF SURVEY POINTS

In determining the length and bearing of a line between two coordinated points :

| $\frac{y \text{ difference}}{x \text{ difference}} = \begin{cases} \text{the tan of the bearing if in the 1st quadrant.} \\ ,, \text{ cotan of (the bearing - 90°) if in the 2nd quadrant.} \\ ,, \text{ tan },, (,, -180°), , 3rd ,, \\ ,, \text{ cotan },, (,, -270°), , 4th ,, \end{cases}$ | |
|--|----|
| $\overline{x \text{ difference}} = \left\{ \begin{array}{ccc} ,, & \tan & ,, & (& ,, & -180^{\circ}) & ,, & 3rd & ,, \\ ,, & \cot an ,, & (& ,, & -270^{\circ}) & ,, & 4th & ,, \end{array} \right.$ | |
| Length = $\frac{y \text{ difference}}{\sin \text{ of bearing}}$ or $\frac{x \text{ difference}}{\cos \text{ of bearing}}$ if in the 1st quadrant | t. |
| $y = \frac{y \text{ difference}}{\cos \text{ of (bearing - 90^\circ)}} \text{ or } \frac{x \text{ difference}}{\sin \text{ of (bearing - 90^\circ)}} y = 2nd y$ | |
| $y \text{ difference} = \frac{y \text{ difference}}{\sin \text{ of (bearing} - 180^\circ)} \text{ or } \frac{x \text{ difference}}{\cos \text{ of (bearing} - 180^\circ)} y \text{ or } x \text{ difference} = 180^\circ \text{ or } y \text{ difference}$ | |
| $y = \frac{y \text{ difference}}{\cos \text{ of (bearing - 270°)}} \text{ or } \frac{x \text{ difference}}{\sin \text{ of (bearing - 270°)}} y = 4 \text{ th} y = 10^{-1} \text{ shown of } y = 10^{-1} shown of$ | |

SECTION III. THE COMPARISON AND VERI-FICATION OF STANDARD MEASURES OF LENGTH.

1. The following measures of length can be tested by the Board of Trade Standards Department, Westminster:

Metal measures in the form of 'ribands' or 'tapes':

100 links or 66 feet.
50 links or 33 feet.
100 feet.
50 feet.
25 feet.
20 metres.
10 metres.

2. The whole or total length only of each of the above measures will be tested, except in the case of a standard measure required for survey purposes, when the corrected values of each part or interval of the measure will be given, eg. every 5 metres on 20 metres, or every 10 feet on 100 feet.

3. Unless otherwise required, each measure will be tested under the following condition as to normal tension, 'pull,' or

stretching-weight, when the measure under test is supported throughout its whole length on a plane and even base:

| | Metal Measures. |
|---|-------------------------------|
| 100 link riband-100 feet to 50 feet20 metres-10 metres- | 10 lb. avoir. 5 kilograms. |

Linked chains, or round-wire chains composed of links and rings and tapes made of linen or other fabric are only verified for certain official purposes.

4. All results are reduced to 62° F. for links and feet and to 0° C. for metres.

The coefficient of linear expansion of a metal measure is taken to be as follows, unless otherwise stated :

| | For 1° F. | For 1° C. |
|---|---------------------------|--------------------------|
| Steel - ' Invar' or Nickel Steel - (35.7 Nickel, 64.3 Steel.) | 0.00000689 0.000000487 | 0.00001240 0.00000877 |

5. The following design of stamp or mark of verification (including the year) is placed on a verified measure:



Metal measures should have a brass disc ($\frac{1}{2}$ -inch diameter) affixed upon which to place the official stamp.

6. In certain cases Treasury fees are required, particulars of which can be obtained at the Standards Office. Fees are not payable on measures for Government Departments or for Local Authorities.

A certificate of verification is given with each measure, in which its error or difference from Standard is stated, and also, in some instances, the modulus of elasticity and 'sag' of a chain.

SECT. III.] STANDARD MEASURES OF LENGTH

In standard steel tapes for the use of local Inspectors of Weights and Measures an error in manufacture of 0.1 inch is allowed in excess or deficiency. In other steel standards 0.25 inch is allowed, and in linen tapes 0.5 inch is permitted.

Metric measures should be accurate to about 5 millimetres in 20 metres or to one four-thousandth of the whole length. The verification of measures can be carried out to nearly one four-thousandth part of the whole length.

The above regulations were issued by the Board of Trade Standards Department on the 1st of August, 1904.

SECTION IV. TACHEOMETRY.

The Use of the Tacheometer in Contouring.

For accurate contouring, a sufficient number of stations should be flagged so that any part of the ground is not more than about 1200 feet distant from at least one station, this being about the limit for accurate reading with the usual 5-inch instrument. The levels of the stations should then be determined, and their positions fixed by triangulation in the following manner. When the instrument is levelled up over a station, set it so that the clamped bottom plate has always the same position relative to the true or to the magnetic meridian. This is done by clamping the top plate at the known bearing which the instrument station makes with the back-sight, and then directing the telescope on the back sight with the bottom plate unclamped. The bearing of each sight can thus be booked direct, which saves time in plotting. The angles to all the fixed stations to be located by triangulation should be carefully read and booked before any staff readings are taken. With one man observing and another booking, two or even three staff men can be kept going. Great care should be insisted on in the holding of the staffs perpendicularly, more especially at a point above or below the level of the instrument station, where the sight has to be taken with an inclined telescope. The form of field book given on the following page is recommended.

A pocket steel tape 6 feet long, in a circular metal case and winding up by means of a spring, will be found very convenient for measuring the height of the instrument. In setting up at a

Specimen Page of Field Book.

Field

Office.

| REMARKS | | | | | |
|------------------------|----------|----------------|-----------------------|----------------------|-----------------------|
| Red. | Level. | +91.89 + 87.35 | + 123.90 | + 84.68 | + 58.97 |
| Axis | Level. | +91.89 | · . | | |
| Fall | r all. | | | 7.21 | 32.92 |
| Dice | NISC. | | 32.01 | | |
| Ś | Vert. | | 369.45 +41.01 32.01 | | - 23.92 |
| DISTANCES. | Hor. | | 369.45 | 348 | 294.06 |
| | Slope. | | 374 | | 296 |
| W. | w ires. | | 10.87 9.00 7.13 | 8.95 7.21 5.47 | 10.48 9.00 7.52 |
| Vert. | Angle. | | 73° 15′ 83° 40′ | 129° 43' level • | 4° 18′ 94° 21′ |
| | Bearing. | | 73° 15′ | 129° 43′ | 4° 18′ |
| Sighted | Stn. | | H | 63 | က |
| Hght. Sighted Bearing. | | 4.54 | | | |
| Inst. | Stn. | $\triangle B$ | | | |

station, first level up, then take height of instrument (from centre of telescope axis to top of peg), then set bottom plate to correct bearing as already described. Take sights with a level telescope where possible, so as to save calculation in the office. Book the readings of the top, middle and bottom wires in the same column. When sighting to the rise or dip, bring the middle wire on to the same even number on the staff whenever possible, as an error in the reading of the top or bottom wire can then be easily detected when booking, and there is less liability to error in working out reduced levels. For instance, on sighting an ordinary 16 feet level staff, keep cutting the 9 foot mark with the middle wire, then the sum of the top and bottom wire readings should always be $9 \times 2 = 18$, and the 'Rise' or 'Fall' is more easily calculated. In the office first get the slope distance from the wire readings, then work out the horizontal and vertical readings by multiplying by the constants given in the table on pages 141-171. Enter them up, putting a + sign before the vertical distance for a rise, and a - sign for a fall. Then fill in the Axis Level, which is the Reduced Level + the height of the instrument. In case of a rise (see Sighted Station 1 in field book) subtract the middle wire reading from the Vertical Distance and book the result in the 'Rise' column. With a level telescope (see Sighted Station 2 in field book) enter the middle wire reading in the 'Fall' column. In case of a fall (see Sighted Station 3 in field book) add the middle wire reading to the Vertical Distance and book result in the 'Fall' column. Although in the specimen page everything is worked out to two decimal places, it is usual to work the Horizontal Distance to the nearest foot, which is sufficiently accurate for plotting.

| Distance. | Correction. | Distance. | Correction. | Distance. | Correction. |
|-----------|-------------|-----------|-------------|-----------|-------------|
| 300 | .002 | 800 | .013 | 1300 | .035 |
| 400 | .003 | 900 | .017 | 1400 | .040 |
| 500 | .005 | 1000 | .020 | 1500 | .046 |
| 600 | .007 | 1100 | .025 | 1600 | .052 |
| 700 | .010 | I 200 | .030 | 1700 | .059 |

Corrections for Curvature and Refraction.

In + or rise angles, add the correction to the amount of rise in 'Rise' column. In level distances, book the correction in the 'Rise' column. In - or dip angles, deduct correction from amount of fall in 'Fall' column. The stadia wires of a tacheometer are usually set to a 'measuring angle' twice the tangent of the half of which is 0.01, *i.e.*, the distance between the wires as read on the staff is 0.01 of the actual distance between the staff and the instrument, and consequently the difference between the top and bottom wire readings $\times 100 =$ the slope distance. Tacheometer telescopes are now made with an 'anallatic lens,' by which the stadia readings are referred to the centre of the instrument. If a telescope which is not 'anallatic' be used, a correction for 'focal length' has to be applied to all the readings.

The vertical circles of most tacheometers are graduated so that with a level telescope the right hand vernier is at 90° and the left hand vernier at 270° , with 360° at the tangent screw. Therefore a rise angle reads less, and a dip angle more than 90° on the right hand vernier, which is the one usually read. The following table is arranged for instruments of this type, but with an instrument where the actual rise or dip angle is read direct, add 90° when looking up the constants for the angle.

The horizontal distance and the difference in height are calculated from the slope distance and the vertical angle as follows :

Let G = the slope distance, or 'generating number.'

V= the vertical angle, or inclination of G from the horizontal.

D = the horizontal distance.

H= the vertical distance, or difference in height.

Then $D = G \cos^2 V$

and $H = G \sin V \cos V$.*

The following table gives the values of $\cos^2 V$ and $\sin V \cos V$ for each minute of arc from \circ° to an inclination of $3\circ^\circ$ from the horizontal.

Rule: Multiply the slope distance by the constants given in the table for the vertical angle.

* $H = D \tan V$.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------------|--|---|----------------------------------|---|----------------------------------|--|--|----------------------------------|
| 0 I 2 3 | I.0000 I.0000 I.0000 I.0000 | .0000 .0003 .0006 .0009 | 60 59 58 57 | | 30 31 32 33 | .99999 .9999 .9999 .9999 | .0087 .0090 .0093 .0096 | 30 29 28 27 |
| 4 5 | I.0000 I.0000 | .0012 | 56 55 | | 34 35 | ·9999 ·9999 | .0099 .0102 | 26 25 |
| 6 7 8 9 10 | I.0000 I.0000 I.0000 I.0000 I.0000 | .0018 .0020 .0023 .0026 .0029 | 54 53 52 51 50 | X | 36 37 38 39 40 | .9999 .9999 .9999 .9999 .9999 | .0105 .0108 .0111 .0113 .0116 | 24 23 22 21 20 |
| 11 12 13 14 15 | I.0000 I.0000 I.0000 I.0000 I.0000 I.0000 | .0032 .0035 .0038 .0041 .0044 | 49 48 47 46 45 | | 41 42 43 44 45 | .99999 .9999 .9998 .9998 .9998 | .0119 .0122 .0125 .0128 .0131 | 1.9 18 17 16 15 |
| 15 16 17 18 19 20 | I.0000 I.0000 I.0000 I.0000 I.0000 I.0000 | .0047 .0050 .0052 .0055 .0058 | 43 44 43 42 41 40 | | 45 46 47 48 49 50 | .99998 .9998 .9998 .9998 .9998 | .0131 .0134 .0137 .0140 .0143 .0145 | 15 14 13 12 11 10 |
| 21 22 23 24 25 | I.0000 I.0000 I.0000 I.0000 I.0000 I.0000 | .0061 .0064 .0067 .0070 .0073 | 39 38 37 36 35 | | 51 52 53 54 55 | .9998 .9998 .9998 .9998 .9998 .9997 | .0148 .0151 .0154 .0157 .0160 | 9 8 7 6 5 |
| 26 27 28 29 30 | •9999 •9999 •9999 •9999 •9999 | .0076 .0079 .0081 .0084 .0087 | 34 33 32 31 30 | | 56 57 58 59 60 | •9997 •9997 •9997 •9997 •9997 | .0163 .0166 .0169 .0172 .0175 | 4 3 2 1 0 |
| - | Constant for Distance. | Constant for Difference in Height. | Minutes. | | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

90 DEGREES.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------|---|--|----------------------------------|----------------------------------|--|--|----------------------------------|
| 0 1 2 3 4 5 | •9997 •9997 •9997 •9997 •9997 •9997 •9996 | .0175 .0177 .0180 .0183 .0186 .0189 | 60 59 58 57 56 55 | 30 31 32 33 34 35 | .9993 .9993 .9993 .9993 .9993 .9992 | •0262 .0265 .0268 .0270 .0273 .0276 | 30 29 28 27 26 25 |
| 6 7 8 9 10 | .9996 .9996 .9996 .9996 .9996 .9796 | .0192 .0195 .0198 .0201 .0204 | 54 53 52 51 50 | 36 37 38 39 40 | .9992 .9992 .9992 .9992 .9992 .9992 | .0279 .0282 .0285 .0288 .0291 | 24 23 22 21 20 |
| 11 12 13 14 15 | .9996 .9996 .9995 .9995 .9995 | .0207 .0209 .0212 .0215 .0218 | 49 48 47 46 45 | 41 42 43 44 45 | .9991 .9991 .9991 .9991 .9991 | .0294 .0297 .0300 .0302 .0305 | 19 18 17 16 15 |
| 16 17 18 19 20 | •9995 •9995 •9995 •9995 •9995 | .0221 .0224 .0227 .0230 .0233 | 44 43 42 41 40 | 46 47 48 49 50 | .9991 .9990 .9990 .9990 .9990 | .0308 .0311 .0314 .0317 .0320 | 14 13 12 11 10 |
| 21 22 23 24 25 | .9994 .9994 .9994 .9994 .9994 .9994 | .0236 .0238 .0241 .0244 .0247 | 39 38 37 36 35 | 51 52 53 54 55 | .9990 .9989 .9989 .9989 .9989 | .0323 .0326 .0328 .0331 .0334 | 9 8 7 6 5 |
| 26 27 28 29 30 | ·9994 ·9994 ·9994 ·9993 ·9993 | .0250 .0253 .0256 .0259 .0262 | 34 33 32 31 30 | 56 57 58 59 60 | .9989 .9988 .9988 .9988 .9988 .9988 | .0337 .0340 .0343 .0346 .0349 | 4 3 2 1 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

91 DEGREES.

| | | 11.6 | reading | ,5-00 | пиписи. | | | |
|----------------------------|--|--|----------------------------------|-------|----------------------------------|--|--|----------------------------------|
| | | | 92 I | DEGR | EES. | | | |
| Minutes. | Constant for Distance. | Constant for Difference in Height. | | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
| 0 1 2 3 4 5 | .9988 .9988 .9987 .9987 .9987 .9987 | .0349 .0352 .0355 .0358 .0360 .0363 | 60 59 58 57 56 55 | | 30 31 32 33 34 35 | .9981 .9981 .9981 .9980 .9980 .9980 | .0436 .0439 .0442 .0445 .0447 .0450 | 30 29 28 27 26 25 |
| 6 7 8 9 10 | .9987 .9986 .9986 .9986 .9986 .9986 | .0366 .0369 .0372 .0375 .0378 | 54 53 52 51 50 | | 36 37 38 39 40 | .9980 .9979 .9979 .9979 .9979 .9978 | .0453 .0456 .0459 .0462 .0465 | 24 23 22 21 20 |
| 11 12 13 14 15 | .9986 .9985 .9985 .9985 .9985 | .0381 .0384 .0387 .0389 .0392 | 49 48 47 46 45 | | 41 42 43 44 45 | .9978 .9978 .9978 .9978 .9977 .9977 | .0468 .0471 .0474 .0476 .0479 | 19 18 17 16 15 |
| 16 17 18 19 20 | .9984 .9984 .9984 .9984 .9983 | .0395 .0398 .0401 .0404 .0407 | 44 43 42 41 40 | | 46 47 48 49 50 | •9977 •9976 •9976 •9976 •9976 •9976 | .0482 .0485 .0487 .0491 .0494 | 14 13 12 11 10 |
| 21 22 23 24 25 | .9983 .9983 .9983 .9983 .9983 .9982 | .0410 .0413 .0416 .0418 .0421 | 39 38 37 36 35 | | 51 52 53 54 55 | ·9975 ·9975 ·9975 ·9974 ·9974 | .0497 .0500 .0502 .0505 .0508 | 9 8 7 6 5 |
| 26 27 28 29 30 | .9982 .9982 .9982 .9981 .9981 | .0424 .0427 .0430 .0433 .0436 | 34 33 32 31 30 | | 56 57 58 59 60 | ·9974 ·9974 ·9973 ·9973 ·9973 | .0511 .0514 .0517 .0520 .0523 | 4 3 2 1 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes | | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

87 DEGREES.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------|---|---|----------------------------|----------------------------|--|---|----------------------------|
| 0 | .9973 | .0523 | 60 | 30 | .9963 | .0609 | 30 |
| 1 | .9972 | .0526 | 59 | 31 | .9962 | .0612 | 29 |
| 2 | .9972 | .0529 | 58 | 32 | .9962 | .0615 | 28 |
| 3 | .9972 | .0531 | 57 | 33 | .9962 | .0618 | 27 |
| 4 | .9971 | .0534 | 56 | 34 | .9961 | .0621 | 26 |
| 5 | .9971 | .0537 | 55 | 35 | .9961 | .0624 | 25 |
| 6 | •9971 | .0540 | 54 | 36 | .9961 | .0627 | 24 |
| 7 | •9971 | .0543 | 53 | 37 | .9960 | .0629 | 23 |
| 8 | •9970 | .0546 | 52 | 38 | .9960 | .0632 | 22 |
| 9 | •9970 | .0549 | 51 | 39 | .9960 | .0635 | 21 |
| 10 | •9970 | .0552 | 50 | 40 | .9959 | .0638 | 20 |
| 11 12 13 14 15 | .9969 .9969 .9969 .9968 .9968 | .0554 .0557 .0560 .0563 .0566 | 49 48 47 46 45 | 41 42 43 44 45 | .9959 .9958 .9958 .9958 .9958 .9957 | .0641 .0644 .0647 .0650 .0653 | 19 18 17 16 15 |
| 16 | .9968 | .0569 | 44 | 46 | •9957 | .0656 | I4 |
| 17 | .9967 | .0572 | 43 | 47 | •9956 | .0658 | I3 |
| 18 | .9967 | .0575 | 42 | 48 | •9956 | .0661 | I2 |
| 19 | .9967 | .0578 | 41 | 49 | •9956 | .0664 | II |
| 20 | .9966 | .0580 | 40 | 50 | •9955 | .0667 | I0 |
| 2I | .9966 | .0583 | 39 | 51 | ·9955 | .0670 | 9 |
| 22 | .9966 | .0586 | 38 | 52 | ·9955 | .0673 | 8 |
| 23 | .9965 | .0589 | 37 | 53 | ·9954 | .0676 | 7 |
| 24 | .9965 | .0592 | 36 | 54 | ·9954 | .0679 | 6 |
| 25 | .9965 | .0595 | 35 | 55 | ·9953 | .0682 | 5 |
| 26 | .9964 | .0598 | 34 | 56 | ·9953 | .0684 | 4 |
| 27 | .9964 | .0601 | 33 | 57 | ·9953 | .0687 | 3 |
| 28 | .9964 | .0604 | 32 | 58 | ·9952 | .0690 | 2 |
| 29 | .9963 | .0607 | 31 | 59 | ·9952 | .0693 | I |
| 30 | .9963 | .0609 | 30 | 60 | ·9951 | .0696 | 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes |

93 DEGREES.

| | 94 DEGREES. | | | | | | | | | | |
|----------------------------|--|--|----------------------------------|--|----------------------------------|---|--|----------------------------------|--|--|--|
| Minutes. | Constant for Distance. | Constant for Difference in Height. | | | Minutes. | Constant for Distance. | Constant for Difference in Height. | | | | |
| 0 1 2 3 4 5 | .9951 .9951 .9950 .9950 .9950 .9949 | .0696 .0699 .0702 .0705 .0707 .0710 | 60 59 58 57 56 55 | | 30 31 32 33 34 35 | .9938 .9938 .9938 .9937 .9937 .9937 .9936 | .0782 .0785 .0788 .0791 .0794 .0797 | 30 29 28 27 26 25 | | | |
| 6 | ·9949 | .0713 | 54 | | 36 | .9936 | .0799 | 24 | | | |
| 7 | ·9949 | .0716 | 53 | | 37 | .9935 | .0802 | 23 | | | |
| 8 | ·9948 | .0719 | 52 | | 38 | .9935 | .0805 | 22 | | | |
| 9 | ·9948 | .0722 | 51 | | 39 | .9934 | .0808 | 21 | | | |
| 10 | ·9948 | .0725 | 50 | | 40 | .9934 | .0811 | 20 | | | |
| 11 | ·9947 | .0728 | 49 | | 41 | .9933 | .0814 | 19 | | | |
| 12 | ·9946 | .0731 | 48 | | 42 | .9933 | .0817 | 18 | | | |
| 13 | ·9946 | .0733 | 47 | | 43 | .9932 | .0820 | 17 | | | |
| 14 | ·9946 | .0736 | 46 | | 44 | .9932 | .0822 | 16 | | | |
| 15 | ·9945 | .0739 | 45 | | 45 | .9931 | .0825 | 15 | | | |
| 16 | ·9945 | .0742 | 44 | | 46 | .9931 | .0828 | 14 | | | |
| 17 | ·9944 | .0745 | 43 | | 47 | .9930 | .0831 | 13 | | | |
| 18 | ·9944 | .0748 | 42 | | 48 | .9930 | .0834 | 12 | | | |
| 19 | ·9943 | .0751 | 41 | | 49 | .9929 | .0837 | 11 | | | |
| 20 | ·9943 | .0753 | 40 | | 50 | .9929 | .0840 | 10 | | | |
| 21 | ·9943 | .0756 | 39 | | 51 | .9929 | .0843 | 9 | | | |
| 22 | ·9942 | .0759 | 38 | | 52 | .9928 | .0845 | 8 | | | |
| 23 | ·9942 | .0762 | 37 | | 53 | .9928 | .0848 | 7 | | | |
| 24 | ·9941 | .0765 | 36 | | 54 | .9927 | .0851 | 6 | | | |
| 25 | ·9941 | .0768 | 35 | | 55 | .9927 | .0854 | 5 | | | |
| 26 | .9940 | .0771 | 34 | | 56 | .9926 | .0857 | 4 | | | |
| 27 | .9940 | .0774 | 33 | | 57 | .9926 | .0860 | 3 | | | |
| 28 | .9939 | .0776 | 32 | | 58 | .9925 | .0863 | 2 | | | |
| 29 | .9939 | .0779 | 31 | | 59 | .9925 | .0865 | 1 | | | |
| 30 | .9938 | .0782 | 30 | | 60 | .9924 | .0868 | 0 | | | |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | | Constant for Distance. | Constant for Difference in Height. | Minutes. | | | |

85 DEGREES.

K

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------|------------------------------|---|----------|----------|------------------------------|---|----------|
| 0 | .9924 | .0868 | 60 | 30 | .9908 | .0954 | 30 |
| I | .9924 | .0871 | 59 | 31 | .9908 | .0957 | 29 |
| 2 | .9923 | .0874 | 58 | 32 | .9907 | .0960 | 28 |
| 3 | .9923 | .0877 | 57 | 33 | .9907 | .0963 | 27 |
| 4 | .9922 | .0880 | 56 | 34 | .9906 | .0965 | 26 |
| 5 | .9922 | .0883 | 55 | 35 | .9905 | .0968 | 25 |
| 6 | .9921 | .0885 | 54 | 36 | .9905 | .0971 | 24 |
| 7 | .9921 | .0888 | 53 | 37 | .9904 | .0974 | 23 |
| 8 | .9920 | .0891 | 52 | 38 | .9904 | .0977 | 22 |
| 9 | .9920 | .0894 | 51 | 39 | .9903 | .0980 | 21 |
| 10 | .9919 | .0897 | 50 | 40 | .9903 | .0983 | 20 |
| 11 | .9918 | .0900 | 49 | 41 | .9902 | .0985 | 19 |
| 12 | .9918 | .0903 | 48 | 42 | .9901 | .0988 | 18 |
| 13 | .9917 | .0905 | 47 | 43 | .9901 | .0991 | 17 |
| 14 | .9917 | .0908 | 46 | 44 | .9900 | .0994 | 16 |
| 15 | .9916 | .0911 | 45 | 45 | .9900 | .0997 | 15 |
| 16 | .9916 | .0914 | 44 | 46 | .9899 | .1000 | I4 |
| 17 | .9915 | .0917 | 43 | 47 | .9898 | .1003 | I3 |
| 18 | .9915 | .0920 | 42 | 48 | .9898 | .1005 | I2 |
| 19 | .9914 | .0923 | 41 | 49 | .9897 | .1008 | II |
| 20 | .9914 | .0926 | 40 | 50 | .9897 | .1011 | I0 |
| 21 | .9913 | .0928 | 39 | 51 | .9896 | .1014 | 9 |
| 22 | .9913 | .0931 | 38 | 52 | .9896 | .1017 | 8 |
| 23 | .9912 | .0934 | 37 | 53 | .9895 | .1020 | 7 |
| 24 | .9912 | .0937 | 36 | 54 | .9894 | .1023 | 6 |
| 25 | .9912 | .0940 | 35 | 55 | .9894 | .1025 | 5 |
| 26 | .9910 | .0943 | 34 | 56 | .9893 | .1028 | 4 |
| 27 | .9910 | .0946 | 33 | 57 | .9893 | .1031 | 3 |
| 28 | .9909 | .0948 | 32 | 58 | .9892 | .1034 | 2 |
| 29 | .9909 | .0951 | 31 | 59 | .9891 | .1037 | 1 |
| 30 | .9908 | .0954 | 30 | 60 | .9891 | .1040 | 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

95 DEGREES.

| | 96 Degrees. | | | | | | | | | | | |
|----------------------------|--|--|----------------------------------|--|----------------------------------|--|--|----------------------------------|--|--|--|--|
| Minutes. | Constant for Distance. | Constant for Difference in Height. | | | Minutes. | Constant for Distance. | Constant for Difference in Height. | | | | | |
| 0 I 2 3 4 5 | .9891 .9890 .9890 .9889 .9888 .9888 | .1040 .1042 .1045 .1048 .1051 .1054 | 60 59 58 57 56 55 | | 30 31 32 33 34 35 | .9872 .9871 .9871 .9870 .9869 .9869 | .1125 .1128 .1130 .1133 .1136 .1139 | 30 29 28 27 26 25 | | | | |
| 6 7 8 9 10 | .9887 .9887 .9886 .9885 .9885 | .1057 .1059 .1062 .1065 .1068 | 54 53 52 51 50 | | 36 37 38 39 40 | .9868 .9867 .9867 .9866 .9865 | .1142 .1145 .1148 .1150 .1153 | 24 23 22 21 20 | | | | |
| 11 12 13 14 15 | .9884 .9883 .9883 .9882 .9882 | .1071 .1074 .1077 .1079 .1082 | 49 48 47 46 45 | | 41 42 43 44 45 | .9865 .9864 .9863 .9863 .9862 | .1156 .1159 .1162 .1164 .1167 | 19 18 17 16 15 | | | | |
| 16 17 18 19 20 | .9881 .9880 .9880 .9879 .9879 | .1085 .1088 .1091 .1094 .1096 | 44 43 42 41 40 | | 46 47 48 49 50 | .9861 .9860 .9860 .9859 .9859 .9858 | .1170 .1173 .1176 .1179 .1181 | 14 13 12 11 10 | | | | |
| 21 22 23 24 25 | .9878 .9877 .9876 .9876 .9876 .9875 | .1099 .1102 .1105 .1108 .1111 | 39 38 37 36 35 | | 51 52 53 54 55 | .9858 .9857 .9856 .9856 .9855 | .1184 .1187 .1190 .1193 .1196 | 9 8 7 6 5 | | | | |
| 26 27 28 29 30 | .9875 .9874 .9873 .9873 .9873 .9872 | .1113 .1116 .1119 .1122 .1125 | 34 33 32 31 30 | | 56 57 58 59 60 | .9854 .9854 .9853 .9852 .9852 | .1198 .1201 .1204 .1207 .1210 | 4 3 2 1 0 | | | | |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | | Constant for Distance. | Constant for Difference in Height. | Minutes. | | | | |

| Table for | the | Calculation | of | Heights | and | Distances | from | Tacheometer |
|-----------|-----|-------------|-----|---------|-------|-----------|------|-------------|
| | | F | Rea | dings-c | ontin | ued. | | |

•

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------|--|--|----------------------------------|----------------------------------|--|--|----------------------------------|
| 0 1 2 3 4 5 | .9852 .9851 .9850 .9849 .9849 .9848 | .1210 .1213 .1215 .1218 .1221 .1224 | 60 59 58 57 56 55 | 30 31 32 33 34 35 | .9830 .9829 .9828 .9827 .9827 .9827 | .1294 .1297 .1300 .1303 .1305 .1308 | 30 29 28 27 26 25 |
| 6 7 8 9 10 | .9847 .9847 .9846 .9845 .9844 | .1227 .1229 .1232 .1235 .1238 | 54 53 52 51 50 | 36 37 38 39 40 | .9825 .9824 .9824 .9824 .9823 .9822 | .1311 .1314 .1317 .1319 .1322 | 24 23 22 21 20 |
| 11 12 13 14 15 | .9844 .9843 .9842 .9842 .9841 | .1241 .1243 .1246 .1249 .1252 | 49 48 47 46 45 | 41 42 43 44 45 | .9821 .9821 .9820 .9819 .9818 | .1325 .1328 .1331 .1333 .1336 | 19 18 17 16 15 |
| 16 17 18 19 20 | .9840 .9839 .9839 .9838 .9837 | .1255 .1258 .1260 .1263 .1266 | 44 43 42 41 40 | 46 47 48 49 50 | .9817 .9817 .9816 .9816 .9815 .9814 | .1339 .1342 .1345 .1347 .1350 | I4 I3 I2 II I0 |
| 21 22 23 24 25 | .9836 .9836 .9835 .9835 .9834 .9833 | .1269 .1272 .1274 .1274 .1277 .1280 | 39 38 37 36 35 | 51 52 53 54 55 | .9814 .9813 .9812 .9811 .9810 | .1353 .1356 .1359 .1361 .1364 | 9 8 7 6 5 |
| 26 27 28 29 30 | .9833 .9832 .9831 .9830 .9830 | .1283 .1286 .1289 .1291 .1294 | 34 33 32 31 30 | 56 57 58 59 60 | .9810 .9809 .9808 .9807 .9806 | .1367 .1370 .1373 .1375 .1378 | 4 3 2 1 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

97 DEGREES.

SECT. IV.]

TACHEOMETRIC TABLE

Table for the Calculation of Heights and Distances from Tacheometer Readings—continued.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------|--|--|----------------------------|----------------------------|--|---|-----------------------------|
| 0 | .9806 | .1378 | 60 | 30 | .9782 | .1462 | 30 |
| 1 | .9806 | .1381 | 59 | 31 | .9781 | .1465 | 29 |
| 2 | .980 5 | .1384 | 58 | 32 | .9780 | .1467 | 28 |
| 3 | .9804 | .1387 | 57 | 33 | .9779 | .1470 | 27 |
| 4 | -9803 | .1390 | 56 | 34 | .9778 | .1473 | 26 |
| 5 | .9802 | .1392 | 55 | 35 | .9777 | .1476 | 25 |
| 6 | .9802 | .1395 | 54 | 36 | 9776 | .1479 | 24 |
| 7 | .9801 | .1398 | 53 | 37 | 9776 | .1481 | 23 |
| 8 | .9800 | .1401 | 52 | 38 | •9775 | .1484 | 22 |
| 9 | .9799 | .1403 | 51 | 39 | •9774 | .1487 | 21 |
| 10 | .9798 | .1406 | 50 | 40 | •9773 | .1490 | 20 |
| 11 12 13 14 15 | ·9797 ·9797 ·9796 ·9795 ·9794 | .1409 .1412 .1415 .1415 .1417 .1420 | 49 48 47 46 45 | 41 42 43 44 45 | .9772 .9771 .9770 .9770 .9770 .9769 | .1492 .1495 .1498 .1501 .1504 | 19 18. 17 16 15 |
| 16 | .9793 | .1423 | 44 | 46 | .9768 | .1506 | I4 |
| 17 | .9792 | .1426 | 43 | 47 | .9767 | .1509 | 13 |
| 18 | .9792 | .1429 | 42 | 48 | .9766 | .1512 | 12 |
| 19 | .9791 | .1431 | 41 | 49 | .9765 | .1515 | 11 |
| 20 | .9790 | .1434 | 40 | 50 | .9764 | .1517 | 10 |
| 21 22 23 24 25 | .9789 .9788 .9788 .9788 .9787 .9786 | .1437 .1440 .1442 .1445 .1448 | 39 38 37 36 35 | 51 52 53 54 55 | .9763 .9763 .9762 .9761 .9760 | .1520 .1523 .1526 .1529 .1531 | 9 8 7 6 5 |
| 26 | .9785 | .1451 | 34 | 56 | •9759 | .1534 | 4 |
| 27 | .9784 | .1454 | 33 | 57 | •9758 | .1537 | 3 |
| 28 | .9783 | .1456 | 32 | 58 | •9757 | .1540 | 2 |
| 29 | .9782 | .1459 | 31 | 59 | •9756 | .1542 | 1 |
| 30 | .9782 | .1462 | 30 | 60 | •9755 | .1545 | 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

98 DEGREES.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------|------------------------------|---|----------|----------|------------------------------|---|----------|
| 0 | .9755 | .1545 | 60 | 30 | .9728 | .1628 | 30 |
| 1 | .9754 | .1548 | 59 | 31 | .9727 | .1631 | 29 |
| 2 | .9754 | .1551 | 58 | 32 | .9726 | .1633 | 28 |
| 3 | .9753 | .1553 | 57 | 33 | .9725 | .1636 | 27 |
| 4 | .9752 | .1556 | 56 | 34 | .9724 | .1639 | 26 |
| 5 | .9751 | .1559 | 55 | 35 | .9723 | .1642 | 25 |
| 6 | .9750 | .1562 | 54 | 36 | .9722 | .1644 | 24 |
| 7 | .9749 | .1565 | 53 | 37 | .9721 | .1647 | 23 |
| 8 | .9748 | .1567 | 52 | 38 | .9720 | .1650 | 22 |
| 9 | .9747 | .1570 | 51 | 39 | .9719 | .1653 | 21 |
| 10 | .9746 | .1573 | 50 | 40 | .9718 | .1655 | 20 |
| 11 | •9745 | .1575 | 49 | 41 | .9717 | .1658 | 19 |
| 12 | •9744 | .1578 | 48 | 42 | .9716 | .1661 | 18 |
| 13 | •9744 | .1581 | 47 | 43 | .9715 | .1664 | 17 |
| 14 | •9743 | .1584 | 46 | 44 | .9714 | .1666 | 16 |
| 15 | •9742 | .1587 | 45 | 45 | .9713 | .1669 | 15 |
| 16 | .9741 | .1589 | 44 | 46 | .9712 | .1672 | 14 |
| 17 | .9740 | .1592 | 43 | 47 | .9711 | .1675 | 13 |
| 18 | .9739 | .1595 | 42 | 48 | .9710 | .1677 | 12 |
| 19 | .9738 | .1598 | 41 | 49 | .9709 | .1680 | 11 |
| 20 | .9737 | .1600 | 40 | 50 | .9708 | .1683 | 10 |
| 21 | .9736 | .1603 | 39 | 51 | .9707 | .1686 | 9 |
| 22 | .9735 | .1606 | 38 | 52 | .9706 | .1688 | 8 |
| 23 | .9734 | .1609 | 37 | 53 | .9705 | .1691 | 7 |
| 24 | .9733 | .1611 | 36 | 54 | .9704 | .1694 | 6 |
| 25 | .9733 | .1614 | 35 | 55 | .9703 | .1697 | 5 |
| 26 | .9732 | .1617 | 34 | 56 | .9702 | .1700 | 4 |
| 27 | .9731 | .1620 | 33 | 57 | .9701 | .1703 | 3 |
| 28 | .9730 | .1622 | 32 | 58 | .9701 | .1705 | 2 |
| 29 | .9729 | .1625 | 31 | 59 | .9700 | .1707 | I |
| 30 | .9728 | .1628 | 30 | 60 | .9699 | .1710 | 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

99 DEGREES.

80 DEGREES.

SECT. IV.]

TACHEOMETRIC TABLE

.....

Table for the Calculation of Heights and Distances from Tacheometer Readings—continued.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------|------------------------------|---|----------|----------|------------------------------|---|----------|
| 0 | .9699 | .1710 | 60 | 30 | .9668 | .1792 | 30 |
| I | .9698 | .1713 | 59 | 31 | .9667 | .1795 | 29 |
| 2 | .9697 | .1716 | 58 | 32 | .9666 | .1797 | 28 |
| 3 | .9696 | .1718 | 57 | 33 | .9665 | .1800 | 27 |
| 4 | .9695 | .1721 | 56 | 34 | .9664 | .1803 | 26 |
| 5 | .9694 | .1724 | 55 | 35 | .9663 | .1806 | 25 |
| 6 | .9693 | .1727 | 54 | 36 | .9662 | .1808 | 24 |
| 7 | .9692 | .1729 | 53 | 37 | .9661 | .1811 | 23 |
| 8 | .9691 | .1732 | 52 | 38 | .9660 | .1814 | 22 |
| 9 | .9689 | .1735 | 51 | 39 | .9659 | .1816 | 21 |
| 10 | .9688 | .1737 | 50 | 40 | .9657 | .1819 | 20 |
| 11 | .9687 | .1740 | 49 | 41 | .9656 | .1822 | 19 |
| 12 | .9686 | .1743 | 48 | 42 | .9655 | .1824 | 18 |
| 13 | .9685 | .1746 | 47 | 43 | .9654 | .1827 | 17 |
| 14 | .9684 | .1748 | 46 | 44 | .9653 | .1830 | 16 |
| 15 | .9683 | .1751 | 45 | 45 | .9652 | .1833 | 15 |
| 16 | .9682 | .1754 | 44 | 46 | .9651 | .1835 | I4 |
| 17 | .9681 | .1757 | 43 | 47 | .9650 | .1838 | I3 |
| 18 | .9680 | .1759 | 42 | 48 | .9649 | .1841 | I2 |
| 19 | .9679 | .1762 | 41 | 49 | .9648 | .1843 | I1 |
| 20 | .9678 | .1765 | 40 | 50 | .9647 | .1846 | I0 |
| 21 | .9677 | .1767 | 39 | 51 | .9646 | .1849 | 9 |
| 22 | .9676 | .1770 | 38 | 52 | .9645 | .1851 | 8 |
| 23 | .9675 | .1773 | 37 | 53 | .9643 | .1854 | 7 |
| 24 | .9674 | .1776 | 36 | 54 | .9642 | .1857 | 6 |
| 25 | .9673 | .1778 | 35 | 55 | .9641 | .1860 | 5 |
| 26 | .9672 | .1781 | 34 | 56 | .9640 | .1862 | 4 |
| 27 | .9671 | .1784 | 33 | 57 | .9639 | .1865 | 3 |
| 28 | .9670 | .1786 | 32 | 58 | .9638 | .1868 | 2 |
| 29 | .9669 | .1789 | 31 | 59 | .9637 | .1870 | 1 |
| 30 | .9668 | .1789 | 30 | 60 | .9636 | .1873 | 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

100 DEGREES.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------|---|---|----------------------------|----------------------------|--|---|----------------------------|
| 0 | .9636 | .1873 | 60 | 30 | .9603 | .1954 | 30 |
| 1 | .9635 | .1876 | 59 | 31 | .9601 | .1956 | 29 |
| 2 | .9634 | .1878 | 58 | 32 | .9600 | .1959 | 28 |
| 3 | .9633 | .1881 | 57 | 33 | .9599 | .1962 | 27 |
| 4 | .9632 | .1884 | 56 | 34 | .9598 | .1964 | 26 |
| 5 | .9630 | .1884 | 55 | 35 | .9597 | .1967 | 25 |
| 6 | .9629 | .1889 | 54 | 36 | .9596 | .1970 | 24 |
| 7 | .9628 | .1892 | 53 | 37 | .9595 | .1972 | 23 |
| 8 | .9627 | .1895 | 52 | 38 | .9593 | .1975 | 22 |
| 9 | .9626 | .1897 | 51 | 39 | .9592 | .1977 | 21 |
| 10 | .9625 | .1900 | 50 | 40 | .9591 | .1980 | 20 |
| 11 12 13 14 15 | .9624 .9623 .9622 .9621 .9619 | .1903 .1905 .1908 .1911 .1913 | 49 48 47 46 45 | 41 42 43 44 45 | .9590 .9589 .9588 .9587 .9587 .9585 | .1983 .1986 .1988 .1991 .1994 | 19 18 17 16 15 |
| 16 | .9618 | .1916 | 44 | 46 | .9584 | .1997 | 14 |
| 17 | .9617 | .1919 | 43 | 47 | .9583 | .1999 | 13 |
| 18 | .9616 | .1922 | 42 | 48 | .9582 | .2002 | 12 |
| 19 | .9615 | .1924 | 41 | 49 | .9581 | .2004 | 11 |
| 20 | .9614 | .1927 | 40 | 50 | .9580 | .2007 | 10 |
| 21 | .9613 | .1930 | 39 | 51 | .9578 | .2010 | 9 |
| 22 | .9612 | .1932 | 38 | 52 | .9577 | .2012 | 8 |
| 23 | .9610 | .1935 | 37 | 53 | .9576 | .2015 | 7 |
| 24 | .9609 | .1938 | 36 | 54 | .9575 | .2018 | 6 |
| 25 | .9608 | .1940 | 35 | 55 | .9575 | .2020 | 5 |
| 26 | .9607 | .1943 | 34 | 56 | .9573 | .2023 | 4 |
| 27 | .9606 | .1946 | 33 | 57 | .9571 | .2026 | 3 |
| 28 | .9605 | .1948 | 32 | 58 | .9570 | .2028 | 2 |
| 29 | .9604 | .1951 | 31 | 59 | .9569 | .2031 | 1 |
| 30 | .9603 | .1954 | 30 | 60 | .9568 | .2034 | 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

IOI DEGREES.

SECT. IV.]

TACHEOMETRIC TABLE

Table for the Calculation of Heights and Distances from Tacheometer Readings—continued.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. |
|----------------------------|---|--|----------------------------|----------------------------|---|--|
| 0 | .9568 | .2034 | 60 | 30 | .9532 | .2113 |
| 1 | .9567 | .2036 | 59 | 31 | .9530 | .2116 |
| 2 | .9565 | .2039 | 58 | 32 | .9529 | .2118 |
| 3 | .9564 | .2042 | 57 | 33 | .9528 | .2121 |
| 4 | .9563 | .2044 | 56 | 34 | .9527 | .2124 |
| 5 | .9562 | .2047 | 55 | 35 | .9525 | .2126 |
| 6 7 8 9 10 | .9561 .9559 .9558 .9557 .9556 | .2050 .2052 .2055 .2058 .2058 .2060 | 54 53 52 51 50 | 36 37 38 39 40 | .9524 .9523 .9522 .9520 .9519 | .2129 .2132 .2134 .2137 .2139 |
| 11 | .9555 | .2063 | 49 | 41 | .9518 | .2142 |
| 12 | .9553 | .2066 | 48 | 42 | .9517 | .2145 |
| 13 | .9552 | .2068 | 47 | 43 | .9515 | .2147 |
| 14 | .9551 | .2071 | 46 | 44 | .9514 | .2150 |
| 15 | .9550 | .2074 | 45 | 45 | .9513 | .2153 |
| 16 | ·9549 | .2076 | 44 | 46 | .9512 | .2155 |
| 17 | ·9547 | .2079 | 43 | 47 | .9510 | .2158 |
| 18 | ·9546 | .2081 | 42 | 48 | .9509 | .2160 |
| 19 | ·9545 | .2084 | 41 | 49 | .9508 | .2163 |
| 20 | ·9544 | .2087 | 40 | 50 | .9507 | .2166 |
| 21 | .9543 | .2089 | 39 | 51 | .9505 | .2168 |
| 22 | .9541 | .2092 | 38 | 52 | .9504 | .2171 |
| 23 | .9540 | .2095 | 37 | 53 | .9503 | .2174 |
| 24 | .9539 | .2097 | 36 | 54 | .9502 | .2176 |
| 25 | .9538 | .2100 | 35 | 55 | .9500 | .2179 |
| 26 27 28 29 30 | .9537 .9535 .9534 .9533 .9532 | .2103 .2105 .2108 .2111 .2113 | 34 33 32 31 30 | 56 57 58 59 60 | •9499 •9498 •9497 •9495 •9494 | .2181 .2184 .2187 .2187 .2189 .2192 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. |

102 DEGREES.

77 DEGREES.

Minutes

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------|---|--|----------------------------|----------------------------|---|--|-----------------------|
| 0 | .9494 | .2192 | 60 | 30 | .9455 | .2270 | 30 |
| 1 | .9493 | .2194 | 59 | 31 | .9454 | .2273 | 29 |
| 2 | .9492 | .2197 | 58 | 32 | .9452 | .2275 | 28 |
| 3 | .9490 | .2200 | 57 | 33 | .9451 | .2278 | 27 |
| 4 | .9489 | .2202 | 56 | 34 | .9450 | .2280 | 26 |
| 5 | .9488 | .2205 | 55 | 35 | .9448 | .2283 | 25 |
| 6 | .9486 | .2208 | 54 | 36 | ·9447 | .2286 | 24 |
| 7 | .9485 | .2210 | 53 | 37 | ·9446 | .2288 | 23 |
| 8 | .9484 | .2213 | 52 | 38 | ·9444 | .2291 | 22 |
| 9 | .9482 | .2215 | 51 | 39 | ·9443 | .2293 | 21 |
| 10 | .9481 | .2218 | 50 | 40 | ·9442 | .2296 | 20 |
| 11 | .9480 | .2221 | 49 | 41 | .9440 | .2299 | 19 |
| 12 | .9479 | .2223 | 48 | 42 | .9439 | .2301 | 18 |
| 13 | .9477 | .2226 | 47 | 43 | .9438 | .2304 | 17 |
| 14 | .9476 | .2228 | 46 | 44 | .9436 | .2306 | 16 |
| 15 | .9475 | .2231 | 45 | 45 | .9435 | .2309 | 15 |
| 16 | •9473 | .2234 | 44 | 46 | ·9434 | .2311 | 14 |
| 17 | •9472 | .2236 | 43 | 47 | ·9433 | .2314 | 13 |
| 18 | •9471 | .2239 | 42 | 48 | ·9431 | .2316 | 12 |
| 19 | •9470 | .2241 | 41 | 49 | ·9430 | .2319 | 11 |
| 20 | •9468 | .2244 | 40 | 50 | ·9428 | .2322 | 10 |
| 21 | .9467 | .2247 | 39 | 51 | .9427 | .2324 | 9 |
| 22 | .9466 | .2249 | 38 | 52 | .9426 | .2327 | 8 |
| 23 | .9464 | .2252 | 37 | 53 | .9424 | .2329 | 7 |
| 24 | .9463 | .2254 | 36 | 54 | .9423 | .2332 | 6 |
| 25 | .9462 | .2254 | 35 | 55 | .9422 | .2335 | 5 |
| 26 27 28 29 30 | .9460 .9459 .9458 .9456 .9455 | .2260 .2262 .2265 .2265 .2267 .2270 | 34 33 32 31 30 | 56 57 58 59 60 | .9420 .9419 .9418 .9416 .9415 | .2337 .2340 .2342 .2345 .2345 .2347 | 4 3 2 1 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes |

103 DEGREES.

TACHEOMETRIC TABLE

Table for the Calculation of Heights and Distances from Tacheometer Readings—continued.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | | Minutes. | Constant • for Distance. | Constant for Difference in Height. | |
|----------------------------|---|---|----------------------------|---|----------------------------|---|--|----------------------------|
| 0 | .9415 | .2347 | 60 | - | 30 | .9373 | .2424 | 30 |
| 1 | .9413 | .2350 | 59 | | 31 | .9372 | .2427 | 29 |
| 2 | .9412 | .2353 | 58 | | 32 | .9370 | .2429 | 28 |
| 3 | .9411 | .2355 | 57 | | 33 | .9369 | .2432 | 27 |
| 4 | .9409 | .2358 | 56 | | 34 | .9367 | .2434 | 26 |
| 5 | .9408 | .2360 | 55 | | 35 | .9366 | .2437 | 25 |
| 6 | .9407 | .2363 | 54 | | 36 | .9365 | .2439 | 24 |
| 7 | .9405 | .2365 | 53 | | 37 | .9363 | .2442 | 23 |
| 8 | .9404 | .2368 | 52 | | 38 | .9362 | .2444 | 22 |
| 9 | .9402 | .2370 | 51 | | 39 | .9360 | .2447 | 21 |
| 10 | .9401 | .2373 | 50 | | 40 | .9359 | .2450 | 20 |
| 11 | .9400 | .2376 | 49 | | 41 | .9358 | .2452 | 19 |
| 12 | .9398 | .2378 | 48 | | 42 | .9356 | .2455 | 18 |
| 13 | .9397 | .2381 | 47 | | 43 | .9355 | .2457 | 17 |
| 14 | .9396 | .2383 | 46 | | 44 | .9353 | .2460 | 16 |
| 15 | .9394 | .2386 | 45 | | 45 | .9352 | .2462 | 15 |
| 16 17 18 19 20 | .9393 .9391 .9390 .9389 .9387 | .2388 .2391 .2394 .2396 .2399 | 44 43 42 41 40 | | 46 47 48 49 50 | .9350 .9349 .9348 .9346 .9345 | .2465 .2467 .2470 .2472 .2472 .2475 | I4 I3 I2 I1 I0 |
| 21 22 23 24 25 | .9386 .9384 .9383 .9382 .9380 | .2401 .2404 .2406 .2409 .2411 | 39 38 37 36 35 | | 51 52 53 54 55 | •9343 •9342 •9340 •9339 •9337 | .2477 .2480 .2482 .2485 .2485 .2487 | 9 8 7 6 5 |
| 26 | ·9379 | .2414 | 34 | | 56 | .9336 | .2490 | 4 |
| 27 | ·9377 | .2417 | 33 | | 57 | .9335 | .2493 | 3 |
| 28 | ·9376 | .2419 | 32 | | 58 | .9333 | .2495 | 2 |
| 29 | ·9375 | .2422 | 31 | | 59 | .9332 | .2498 | 1 |
| 30 | ·9373 | .2424 | 30 | | 60 | .9330 | .2500 | 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

104 DEGREES.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------|---|--|----------------------------|----------------------------|---|---|----------------------------|
| 0 | .9330 | .2500 | 60 | 30 | .9286 | .2575 | 30 |
| 1 | .9329 | .2503 | 59 | 31 | .9284 | .2578 | 29 |
| 2 | .9327 | .2505 | 58 | 32 | .9283 | .2580 | 28 |
| 3 | .9326 | .2508 | 57 | 33 | .9281 | .2583 | 27 |
| 4 | .9324 | .2510 | 56 | 34 | .9280 | .2585 | 26 |
| 5 | .9323 | .2513 | 55 | 35 | .9278 | .2588 | 25 |
| 6 7 8 9 10 | .9321 .9320 .9319 .9317 .9316 | .2515 .2518 .2520 .2523 .2523 .2525 | 54 53 52 51 50 | 36 37 38 39 40 | .9277 .9275 .9274 .9272 .9271 | .2590 .2593 .2595 .2598 .2600 | 24 23 22 21 20 |
| 11 | .9314 | .2528 | 49 | 41 | .9269 | .2603 | 19 |
| 12 | .9313 | .2530 | 48 | 42 | .9268 | .2605 | 18 |
| 13 | .9311 | .2533 | 47 | 43 | .9266 | .2608 | 17 |
| 14 | .9310 | .2535 | 46 | 44 | .9265 | .2610 | 16 |
| 15 | .9308 | .2538 | 45 | 45 | .9263 | .2613 | 15 |
| 16 | .9307 | .2540 | 44 | 46 | .9262 | .2615 | 14 |
| 17 | .9305 | .2543 | 43 | 47 | .9260 | .2618 | 13 |
| 18 | .9304 | .2545 | 42 | 48 | .9259 | .2620 | 12 |
| 19 | .9302 | .2548 | 41 | 49 | .9257 | .2622 | 11 |
| 20 | .9301 | .2550 | 40 | 50 | .9256 | .2625 | 10 |
| 2I | .9299 | .2553 | 39 | 51 | .9254 | .2627 | 9 |
| 22 | .9298 | .2555 | 38 | 52 | .9253 | .2630 | 8 |
| 23 | .9296 | .2558 | 37 | 53 | .9251 | .2632 | 7 |
| 24 | .9295 | .2560 | 36 | 54 | .9249 | .2635 | 6 |
| 25 | .9293 | .2563 | 35 | 55 | .9248 | .2637 | 5 |
| 26 27 28 29 30 | .9292 .9290 .9289 .9287 .9286 | .2565 .2568 .2570 .2573 .2573 .2575 | 34 33 32 31 30 | 56 57 58 59 60 | .9246 .9245 .9243 .9242 .9240 | .2640 .2642 .2645 .2647 .2650 | 4 3 2 1 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

105 DEGREES.

74 DEGREES.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|-------------|------------------------------|---|----------|------|----------|------------------------------|---|----------|
| 0 | .9240 | .2650 | 60 | | 30 31 | .9193 | .2723 | 30 |
| I | .9239 | | 59 58 | - 12 | | .9192 | .2726 | 29 |
| 2 | .9237 | .2655 | 50 | | 32 | .9190 | .2728 | 28 |
| 3 4 5 | .9236 | .2657 | 57 | 14 | 33 | .9189 | .2731 | 27 |
| 4 | .9234 | .2660 | 56 | 1.1 | 34 | .9187 | .2733 | 26 |
| 5 | .9233 | .2662 | 55 | | 35 | .9185 | .2735 | 25 |
| 6 | .9231 | .2664 | 54 | | 36 | .9184 | .2738 | 24 |
| 78 | .9230 | .2667 | 53 | | 37 | .9182 | .2740 | 23 |
| 8 | .9228 | .2669 | 52 | | 37 38 | .9181 | .2743 | 22 |
| 9 | .9226 | .2672 | 51 | | 39 | .9179 | .2745 | 21 |
| IO | .9225 | .2674 | 50 | 1 | 40 | .9177 | .2748 | 20 |
| II | .9223 | .2677 | 49 | | 41 | .9176 | .2750 | 19 |
| 12 | .9222 | .2679 | 48 | | 42 | .9174 | .2752 | 18 |
| 13 | .9220 | .2682 | 47 | | 43 | .9173 | .2755 | 17 |
| 14 | .9219 | .2684 | 46 | | 44 | .9171 | .2757 | 16 |
| 15 | .9217 | .2687 | 45 | | 45 | .9169 | .2760 | 15 |
| 16 | | .2689 | | | | 0.40 | | |
| | .9215 | .2009 | 44 | | 46 | .9168 | .2762 | 14 |
| 17 18 | .9214 | | 43 | | 47 | | .2765 | 13 |
| | .9212 | .2694 | 42 | | 48 | .9165 | .2767 | 12 |
| 19 | .9211 | .2696 | 41 | | 49 | .9163 | .2769 | II |
| 20 | .9209 | . 2699 | 40 | | 50 | .9161 | .2772 | IO |
| 21 | .9208 | .2701 | 39 38 | | 51 | .9160 | .2774 | 9 |
| 22 | .9206 | .2704 | | | 52 | .9158 | .2777 | 8 |
| 23 | .9204 | .2706 | 37 | _ | 53 - | .9157 | .2779 | 76 |
| 24 | .9203 | .2709 | 36 | | 54 | .9155 | .2781 | 6 |
| 25 | .9201 | .2711 | 35 | | 55 | .9153 | .2784 | 5 |
| 26 | .9200 | .2713 | 34 | | 56 | .9152 | .2786 | 4 |
| | .9198 | .2716 | 33 | | 57 | .9150 | .2789 | 3 |
| 27 28 | .9197 | .2718 | 32 | | 57 58 | .9148 | .2791 | 2 |
| 29 | .9195 | .2721 | 31 | | 50 | .9147 | .2794 | I |
| 30 | .9193 | .2723 | 30 | | 59 60 | .9145 | .2796 | 0 |
| | Constant | Constant | Minutes. | | | Constant | Constant | Minutes. |
| - | Distance. | Difference in Height. | minutes. | | | Distance. | Difference in Height. | manuces. |

106 DEGREES.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------|--|--|----------------------------------|----------------------------------|--|---|----------------------------------|
| 0 I 2 3 4 5 | .9145 .9144 .9142 .9140 .9139 .9137 | .2796 .2798 .2801 .2803 .2806 .2808 | 60 59 58 57 56 55 | 30 31 32 33 34 35 | .9096 .9094 .9092 .9091 .9089 .9087 | .2868 .2870 .2873 .2875 .2875 .2878 .2880 | 30 29 28 27 26 25 |
| 6 7 8 9 10 | .9135 .9134 .9132 .9130 .9129 | .2810 .2813 .2815 .2818 .2820 | 54 53 52 51 50 | 36 37 38 39 40 | .9086 .9084 .9082 .9081 .9079 | .2882 .2885 .2887 .2887 .2889 .2892 | 24 23 22 21 20 |
| 11 12 13 14 15 | .9127 .9126 .9124 .9122 .9121 | .2822 .2825 .2827 .2830 .2832 | 49 48 47 46 45 | 41 42 43 44 45 | .9077 .9076 .9074 .9072 .9071 | .2894 .2896 .2899 .2901 .2904 | 19 18 17 16 15 |
| 16 17 18 19 20 | .9119 .9117 .9116 .9114 .9112 | .2834 .2837 .2839 .2842 .2844 | 44 43 42 41 40 | 46 47 48 49 50 | .9069 .9067 .9066 .9064 .9062 | .2906 .2908 .2911 .2913 .2915 | 14 13 12 11 10 |
| 21 22 23 24 25 | .9111 .9109 .9107 .9106 .9104 | .2846 .2849 .2851 .2854 .2856 | 39 38 37 36 35 | 51 52 53 54 55 | .9060 .9059 .9057 .9055 .9054 | .2918 .2920 .2922 .2925 .2925 .2927 | 9 8 7 6 5 |
| 26 27 28 29 30 | .9102 .9101 .9099 .9098 .9096 | .2858 .2861 .2863 .2866 .2868 | 34 33 32 31 30 | 56 57 58 59 60 | .9052 .9050 .9049 .9047 .9045 | .2930 .2932 .2934 .2937 .2939 | 4 3 2 1 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

107 DEGREES.

| Table for th | e Calculation | of Heights and | Distances | from | Tacheometer |
|--------------|---------------|-----------------|-----------|------|-------------|
| | R | Readings-contin | ued. | | |

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. |
|----------|------------------------------|---|----------|----------|------------------------------|
| 0 | .9045 | .2939 | 60 | 30 | .8993 |
| I | .9043 | .2941 | 59 | 31 | .8991 |
| 2 | .9042 | .2944 | 58 | 32 | .8990 |
| 3 | .9040 | .2946 | 57 | 33 | .8988 |
| 4 | .9038 | .2948 | 56 | 34 | .8986 |
| 5 | .9037 | .2951 | 55 | 35 | .8986 |
| 6 | .9035 | .2953 | 54 | 36 | .8983 |
| 7 | .9033 | .2955 | 53 | 37 | .8981 |
| 8 | .9031 | .2958 | 52 | 38 | .8979 |
| 9 | .9030 | .2960 | 51 | 39 | .8977 |
| 10 | .9028 | .2962 | 50 | 40 | .8976 |
| 11 | .9026 | .2965 | 49 | 41 | .8974 |
| 12 | .9024 | .2967 | 48 | 42 | .8972 |
| 13 | .9023 | .2969 | 47 | 43 | .8970 |
| 14 | .9021 | .2972 | 46 | 44 | .8969 |
| 15 | .9019 | .2974 | 45 | 45 | .8967 |
| 16 | .9018 | .2977 | 44 | 46 | .8965 |
| 17 | .9016 | .2979 | 43 | 47 | .8963 |
| 18 | .9014 | .2981 | 42 | 48 | .8962 |
| 19 | .9012 | .2984 | 41 | 49 | .8960 |
| 20 | .9011 | .2986 | 40 | 50 | .8958 |
| 21 | .9009 | .2988 | 39 | 51 | .8956 |
| 22 | .9007 | .2591 | 38 | 52 | .8954 |
| 23 | .9005 | .2993 | 37 | 53 | .8953 |
| 24 | .9004 | .2995 | 36 | 54 | .8951 |
| 25 | .9002 | .2998 | 35 | 55 | .8949 |
| 26 | .9000 | .3000 | 34 | 56 | .8947 |
| 27 | .8998 | .3002 | 33 | 57 | .8946 |
| 28 | .8997 | .3004 | 32 | 58 | .8944 |
| 29 | .8995 | .3007 | 31 | 59 | .8942 |
| 30 | .8993 | .3009 | 30 | 60 | .8940 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. |

108 DEGREES.

71 DEGREES.

30

29

28

27

26

25

24

23

22

21

20

19

18

17

16

15

14

13

12

II

10

9 8

76

5

4

32

I

0

Minutes.

Constant

for Difference

in Height. . 3009

.3011

.3014

.3016

.3018

.3021

.3023

.3025

.3030

.3032 .3035

.3037

.3039

.3041

.3044

.3046

.3048

.3051

.3053

.3055

.3058

.3060

.3062

.3065

.3069

.3071

.3074

.3076 .3078

Constant

for Difference

in Height.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------|--|--|----------------------------------|----------------------------------|--|--|----------------------------------|
| 0 1 2 3 4 5 | .8940 .8938 .8937 .8935 .8933 .8931 | .3078 .3081 .3083 .3085 .3088 .3090 | 60 59 58 57 56 55 | 30 31 32 33 34 35 | .8886 .8884 .8882 .8880 .8878 .8877 | .3147 .3149 .3151 .3153 .3156 .3158 | 30 29 28 27 26 25 |
| 6 7 8 9 10 | .8929 .8928 .8926 .8924 .8922 | .3092 .3094 .3097 .3099 .3101 | 54 53 52 51 50 | 36 37 38 39 40 | .8875 .8873 .8871 .8869 .8867 | .3160 .3162 .3165 .3165 .3169 | 24 23 22 21 20 |
| 11 12 13 14 15 | .8920 .8918 .8917 .8915 .8913 | .3103 .3106 .3108 .3110 .3113 | 49 48 47 46 45 | 41 42 43 44 45 | .8866 .8864 .8862 .8860 .8858 | .3171 .3174 .3176 .3176 .3178 .3180 | 19 18 17 16 15 |
| 16 17 18 19 20 | .8911 .8909 .8908 .8906 .8906 | .3115 .3117 .3119 .3122 .3124 | 44 43 42 41 40 | 46 47 48 49 50 | .8856 .8854 .8853 .8851 .8851 .8849 | .3183 .3185 .3185 .3187 .3189 .3192 | 14 13 12 11 10 |
| 21 22 23 24 25 | .8902 .8900 .8899 .8897 .8895 | .3126 .3129 .3131 .3133 .3136 | 39 38 37 36 35 | 51 52 53 54 55 | .8847 .8845 .8843 .8842 .8840 | .3194 .3196 .3198 .3201 .3203 | 9 8 7 6 5 |
| 26 27 28 29 30 | .8893 .8891 .8889 .8888 .8888 .8886 | .3138 .3140 .3142 .3142 .3144 .3147 | 34 33 32 31 30 | 56 57 58 59 60 | .8838 .8836 .8834 .8832 .8830 | .3205 .3207 .3209 .3212 .3214 | 4 3 2 I 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

109 DEGREES.

| Table for | the | Calculation | of | Heights | and | Distances | from | Tacheometer |
|-----------|-----|-------------|-----|----------|-------|-----------|------|-------------|
| | | J | Rea | dings-co | ontin | ued. | | |

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------|--|--|----------------------------------|----------------------------------|--|---|----------------------------------|
| 0 1 2 3 4 5 | .8830 .8828 .8826 .8825 .8823 .8823 | .3214 .3216 .3218 .3221 .3223 .3225 | 60 59 58 57 56 55 | 30 31 32 33 34 35 | .8774 .8772 .8770 .8768 .8766 .8766 | .3280 .3283 .3285 .3287 .3287 .3289 .3291 | 30 29 28 27 26 25 |
| 6 7 8 9 10 | .8819 .8817 .8815 .8813 .8811 | .3227 .3230 .3232 .3234 .3236 | 54 53 52 51 50 | 36 37 38 39 40 | .8762 .8760 .8758 .8756 .8754 | .3293 .3296 .3298 .3300 .3300 .3302 | 24 23 22 21 20 |
| 11 12 13 14 15 | .8810 .8808 .8806 .8804 .8802 | .3238 .3241 .3243 .3245 .3247 | 49 48 47 46 45 | 41 42 43 44 45 | .8753 .8751 .8749 .8747 .8745 | .3304 .3307 .3309 .3311 .3313 | 19 18 17 16 15 |
| 16 17 18 19 20 | .8800 .8798 .8796 .8794 .8793 | .3249 .3252 .3254 .3256 .3258 | 44 43 42 41 40 | 46 47 48 49 50 | .8743 .8741 .8739 .8737 .8735 | .3315 .3318 .3320 .3322 .3324 | 14 13 12 11 10 |
| 21 22 23 24 25 | .8791 .8789 .8787 .8785 .8785 .8783 | .3261 .3263 .3265 .3267 .3269 | 39 38 37 36 35 | 51 52 53 54 55 | .8733 .8731 .8729 .8727 .8725 | .3326 .3328 .3331 .3333 .3335 | 9 8 7 6 5 |
| 26 27 28 29 30 | .8781 .8779 .8777 .8776 .8776 | .3272 .3274 .3276 .3276 .3278 .3280 | 34 33 32 31 30 | 56 57 58 59 60 | .8723 .8722 .8720 .8718 .8716 | •3337 •3339 •3341 •3344 •3346 | 4 3 2 1 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

110 DEGREES. - -

69 DEGREES.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|--------------------------------|---|--|----------------------------|----------------------------|---|--|----------------------------|
| 0 | .8716 | .3346 | 60 | 30 | .8657 | .3410 | 30 |
| 1 | .8714 | .3348 | 59 | 31 | .8655 | .3412 | 29 |
| 2 | .8712 | .3350 | 58 | 32 | .8653 | .3414 | 28 |
| 3 | .8710 | .3352 | 57 | 33 | .8651 | .3416 | 27 |
| 4 | .8708 | .3354 | 56 | 34 | .8649 | .3419 | 26 |
| 5 | .8706 | .3356 | 55 | 35 | .8647 | .3421 | 25 |
| 6 · 7 · 8 · 9 · 10 | .8704 .8702 .8700 .8698 .8696 | ·3359 ·3361 ·3363 ·3365 ·3367 | 54 53 52 51 50 | 36 37 38 39 40 | .8645 .8643 .8641 .8639 .8637 | ·3423 ·3425 ·3427 ·3427 ·3429 ·3431 | 24 23 22 21 20 |
| 11 | .8694 | .3369 | 49 | 41 | .8635 | ·3433 | 19 |
| 1·2 | .8692 | .3372 | 48 | 42 | .8633 | ·3436 | 18 |
| 13 | .8690 | .3374 | 47 | 43 | .8631 | ·3438 | 17 |
| 14 | .8688 | .3376 | 46 | 44 | .8629 | ·3440 | 16 |
| 15 | .8686 | .3378 | 45 | 45 | .8627 | ·3442 | 15 |
| 16 17 18 19 20 | .8684 .8682 .8680 .8678 .8677 | .3380 .3382 .3384 .3384 .3387 .3389 | 44 43 42 41 40 | 46 47 48 49 50 | .8625 .8623 .8621 .8619 .8617 | · 3444 · 3446 · 3448 · 3450 · 3452 | I4 I3 I2 II I0 |
| 2I | .8675 | •3391 | 39 | 51 | .8615 | · 3454 | 9 |
| 22 | .8673 | •3393 | 38 | 52 | .8613 | · 3457 | 8 |
| 23 | .8671 | •3395 | 37 | 53 | .8611 | · 3459 | 7 |
| 24 | .8669 | •3397 | 36 | 54 | .8609 | · 3461 | 6 |
| 25 | .8667 | •3399 | 35 | 55 | .8607 | · 3463 | 5 |
| 26 | .8665 | .3402 | 34 | 56 | .8605 | .3465 | 4 |
| 27 | .8663 | .3404 | 33 | 57 | .8603 | .3467 | 3 |
| 28 | .8661 | .3406 | 32 | 58 | .8601 | .3469 | 2 |
| 29 | .8659 | .3408 | 31 | 59 | .8599 | .3471 | I |
| 30 | .8657 | .3410 | 30 | 60 | .8597 | .3473 | 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

III DEGREES.

SECT. IV.]

TACHEOMETRIC TABLE

Table for the Calculation of Heights and Distances from Tacheometer Readings—continued.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | N |
|----------------------------|---|--|----------------------------------|------|
| 0 I 2 3 4 5 | .8597 .8595 .8593 .8591 .8589 .8589 .8587 | ·3473 ·3475 ·3478 ·3480 ·3482 ·3484 | 60 59 58 57 56 55 | |
| 6 7 8 9 10 | .8585 .8583 .8581 .8579 .8576 | .3486 .3488 .3490 .3492 .3494 | 54 53 52 51 50 | 1. T |
| 11 12 13 14 15 | .8574 .8572 .8570 .8568 .8566 | •3496 •3498 •3500 •3503 •3505 | 49 48 47 46 45 | |
| 16 17 18 19 20 | .8564 .8562 .8560 .8558 .8556 | .3507 .3509 .3511 .3513 .3515 | 44 43 42 41 40 | |
| 21 22 23 24 25 | .8554 .8552 .8550 .8548 .8546 | •3517 •3519 •3521 •3523 •3525 | 39 38 37 36 35 | |
| 26 27 28 29 30 | .8544 .8542 .8540 .8538 .8536 | •3527 •3529 •3531 •3534 •3536 | 34 33 32 31 30 | |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | |

112 DEGREES.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------------|--|--|----------------------------------|
| 30 31 32 33 34 35 | .8536 .8534 .8531 .8529 .8527 .8525 | .3536 .3538 .3540 .3542 .3544 .3544 | 30 29 28 27 26 25 |
| 36 37 38 39 40 | .8523 .8521 .8519 .8517 .8515 | •3548 •3550 •3552 •3554 •3556 | 24 23 22 21 20 |
| 41 42 43 44 45 | .8513 .8511 .8509 .8507 .8505 | .3558 .3560 .3562 .3564 .3566 | 19 18 17 16 15 |
| 46 47 48 49 50 | .8503 .8500 .8498 .8496 .8494 | .3568 .3570 .3572 .3574 .3576 | 14 13 12 11 10 |
| 51 52 53 54 55 | .8492 .8490 .8488 .8486 .8486 .8484 | -3578 -3581 -3583 -3585 -3585 -3587 | 9 8 7 6 5 |
| 56 57 58 59 60 | .8482 .8480 .8478 .8475 .8473 | .3589 .3591 .3593 .3595 .3595 .3597 | 4 3 2 1 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. |

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------|---|--|----------------------------------|----------------------------------|--|--|----------------------------------|
| 0 I 2 3 4 5 | .8473 .8470 .8468 .8466 .8466 .8464 .8463 | .3597 .3599 .3601 .3603 .3605 .3607 | 60 59 58 57 56 55 | 30 31 32 33 34 35 | .8410 .8408 .8406 .8404 .8401 .8399 | .3657 .3659 .3661 .3663 .3665 .3667 | 30 29 28 27 26 25 |
| 6 | .8461 | .3609 | 54 | 36 | .8397 | .3669 | 24 |
| 7 | .8459 | .3611 | 53 | 37 | .8395 | .3671 | 23 |
| 8 | .8457 | .3613 | 52 | 38 | .8393 | .3673 | 22 |
| 9 | .8454 | .3615 | 51 | 39 | .8391 | .3675 | 21 |
| 10 | .8452 | .3617 | 50 | 40 | .8389 | .3677 | 20 |
| 11 | .8450 | .3619 | 49 | 41 | .8387 | .3679 | 19 |
| 12 | .8448 | .3621 | 48 | 42 | .8384 | .3681 | 18 |
| 13 | .8446 | .3623 | 47 | 43 | .8382 | .3682 | 17 |
| 14 | .8444 | .3625 | 46 | 44 | .8380 | .3684 | 16 |
| 15 | .8442 | .3627 | 45 | 45 | .8378 | .3686 | 15 |
| 16 | .8440 | .3629 | 44 | 46 | .8376 | .3688 | 14 |
| 17 | .8438 | .3631 | 43 | 47 | .8374 | .3690 | 13 |
| 18 | .8436 | .3633 | 42 | 48 | .8372 | .3692 | 12 |
| 19 | .8433 | .3635 | 41 | 49 | .8369 | .3694 | 11 |
| 20 | .8431 | .3637 | 40 | 50 | .8367 | .3696 | 10 |
| 21 | .8429 | .3639 | 39 | 51 | .8365 | .3698 | 9 |
| 22 | .8427 | .3641 | 38 | 52 | .8363 | .3700 | 8 |
| 23 | .8425 | .3643 | 37 | 53 | .8361 | .3702 | 7 |
| 24 | .8423 | .3645 | 36 | 54 | .8359 | .3704 | 6 |
| 25 | .8421 | .3647 | 35 | 55 | .8356 | .3706 | 5 |
| 26 27 28 29 30 | .8419 .8416 .8414 .8412 .8410 | .3649 .3651 .3653 .3655 .3655 .3657 | 34 33 32 31 30 | 56 57 58 59 60 | .8354 .8352 .8350 .8348 .8346 | .3708 .3710 .3712 .3714 .3716 | 4 3 2 1 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

113 DEGREES.

.8326

.8324

.8322

.8320

.8318

.8315

.8313

.8311

.8309

.8307

.8304

.8302

.8300

.8298

.8296

.8294

.8291

.8289

.8287

.8285

.8283

.8280

Constant

for

Distance.

9

IO

II

12

13

14

15

16

17 18

19

20

21

22

23

24

25

26

27

28

29

30

.3733

.3735

·3737

.3739

·3741

.3743

·3745

.3747

·3749

·3751

·3753

·3754

.3756

·3758 ·3760

.3762

.3764

.3766

.3768

.3770

.3772

· 3774

Constant

for

Difference

in Height.

51

50

49 48

47

46

45

44

43

42

41

40

39 38

37 36

35

34

33

32

31

30

Minutes.

| | Readings—continued. | | | | | | | | | | |
|----------------------------|--|--|----------------------------------|--|----------------------------------|--|--|----------------------------------|--|--|--|
| 114 DEGREES. | | | | | | | | | | | |
| Minutes. | Constant for Distance. | Constant for Difference in Height. | | | Minutes. | Constant for Distance. | Constant for Difference in Height. | | | | |
| 0 I 2 3 4 5 | .8346 .8344 .8341 .8339 .8337 .8335 | .3716 .3718 .3720 .3722 .3724 .3725 | 60 59 58 57 56 55 | | 30 31 32 33 34 35 | .8280 .8278 .8276 .8274 .8272 .8269 | · 3774 · 3776 · 3777 · 3779 · 3781 · 3783 | 30 29 28 27 26 25 | | | |
| 6 7 8 | .8333 .8331 .8328 | · 3727 · 3729 · 3731 | 54 53 52 | | 36 37 38 | .8267 .8265 .8263 | .3785 .3787 .3789 | 24 23 22 | | | |

.8261

.8258

.8256

.8254

.8252

.8249

.8247

.8245

.8243

.8241

.8238

.8236

.8234

.8232

.8230

.8227

.8225

.8223

.8221

.8218

.8216

.8214

Constant

for

Distance.

.3791

·3793

·3794

.3796

.3798

.3800

.3802

.3804

.3806

.3808

.3810

.3811

.3813

.3815

.3817

.3819

.3821

.3823

.3825

.3827

.3828

.3830

Constant

for

Difference

in Height.

21

20

19

18

17

16

15

14

13

12

II

10

9 8

76

5

4

3

2

I

0

Minutes.

39

40

41

42

43

44

45

46

47 48

49

50

51

52

53

54

55

56

57 58

59 60

Table for the Calculation of Heights and Distances from Tacheometer

6

| 5 | DEGREES. | |
|---|------------|--|
| | D DOLUDDO! | |

| | | | | | | | |
|----------------------------|--|--|----------------------------------|----------------------------------|--|--|----------------------------------|
| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
| 0 1 2 3 4 5 | .8214 .8212 .8210 .8207 .8205 .8203 | .3830 .3832 .3834 .3836 .3838 .3840 | 60 59 58 57 56 55 | 30 31 32 33 34 35 | .8147 .8144 .8142 .8140 .8138 .8135 | .3886 .3888 .3889 .3891 .3893 .3895 | 30 29 28 27 26 25 |
| 6 7 8 9 10 | .8201 .8198 .8196 .8194 .8192 | .3841 .3843 .3845 .3845 .3847 .3849 | 54 53 52 51 50 | 36 37 38 39 40 | .8133 .8131 .8128 .8126 .8126 .8124 | .3897 .3899 .3900 .3902 .3904 | 24 23 22 21 20 |
| 11 12 13 14 15 | .8189 .8187 .8185 .8182 .8180 | .3851 .3853 .3854 .3856 .3858 | 49 48 47 46 45 | 41 42 43 44 45 | .8122 .8119 .8117 .8115 .8113 | .3906 .3908 .3909 .3911 .3913 | 19 18 17 16 15 |
| 16 17 18 19 20 | .8178 .8176 .8174 .8174 .8171 .8169 | .3860 .3862 .3864 .3866 .3867 | 44 43 42 41 40 | 46 47 48 49 50 | .8110 .8108 .8106 .8103 .8103 .8101 | .3915 .3917 .3919 .3920 .3922 | I4 I3 I2 II I0 |
| 21 22 23 24 25 | .8167 .8165 .8163 .8160 .8158 | .3869 .3871 .3873 .3875 .3875 | 39 38 37 36 35 | 51 52 53 54 55 | .8099 .8097 .8094 .8092 .8090 | .3924 .3926 .3928 .3929 .3931 | 9 8 7 6 5 |
| 26 27 28 29 30 | .8156 .8154 .8151 .8149 .8147 | .3878 .3880 .3882 .3884 .3884 .3886 | 34 33 32 31 30 | 56 57 58 59 60 | .8088 .8085 .8083 .8081 .8078 | •3933 •3935 •3937 •3937 •3938 •3940 | 4 3 2 1 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

115 DEGREES.

78

9

10

TT

12

13

14

15

16

17

18

19

20

21

22

23

24

25

26

27 28

29

30

.8062

.8060

.8058

.8055

.8053

.8051

.8048

.8046

.8044

.8042

.8039

.8037

.8035

.8032

.8030

.8028

.8025

.8023

.8021

.8018

.8016

.8014

.8011

.8009

Constant

for

Distance.

·3953

·3954

.3956

.3958

.3960

.3962

.3963

.3965

.3967

.3969

.3970

.3972

·3974

.3976

·3977

.3979

.3981

.3983

.3984

.3986

.3988

.3990

.3991

.3993 Constant

for

Difference

in Height.

53

52

51

50

49

48

47

46

45

44

43

42

41

40

39

38

37

36

35

34

33

32

31

30

Minutes.

| | | | Reading | s | ntinuea. | | | | |
|----------------------------|--|--|----------------------------------|---|----------------------------------|--|--|----------------------------------|--|
| 116 Degrees. | | | | | | | | | |
| Minutes. | Constant for Distance. | Constant for Difference in Height. | | | Minutes. | Constant for Distance. | Constant for Difference in Height. | | |
| 0 I 2 3 4 5 | .8078 .8076 .8074 .8071 .8069 .8067 | .3940 .3942 .3944 .3946 .3947 .3949 | 60 59 58 57 56 55 | | 30 31 32 33 34 35 | .8009 .8007 .8004 .8002 .8000 .7998 | ·3993 ·3995 ·3997 ·3998 ·4000 ·4002 | 30 29 28 27 26 25 | |
| 6 | .8065 | .3951 | 54 | | 36 | .7995 | .4004 | 24 | |

37 38

39

40

4I

42

43

44

45

46

47 48

49

50

51

52

53

54

55

56

57

58

59

60

·7993

•7991 •7988

.7986

.7984

.7981

.7979

.7976

.7974

.7972

.7970

.7967

.7965

.7962

.7960

.7958

·7955

·7953

.7951

.7948

.7946

·7944

.7941

.7939

Constant

for

Distance.

.4005

.4007

.4009

.4011

.4012

.4014

.4016

.4018

.4019

.4021

.4023

.4025

.4026

.4028

.4030

.4031

.4033

.4035

.4037

.4038

.4040

.4042

.4043

.4045

Constant

for

Difference

in Height.

23

22

21

20

19

18

17

16

15

14

13

12

II

10

98

76

5

4

3

2

I

0

Minutes.

Table for the Calculation of Heights and Distances from Tacheometer

| 63 | DEGREES. |
|----|----------|
|----|----------|

II

98 76

I

Minutes.

Table for the Calculation of Heights and Distances from Tacheometer Readings—continued.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. |
|----------|------------------------------|---|----------|----------|------------------------------|---|
| 0 | .7939 | .4045 | 60 | 30 | .7868 | .4096 |
| 1 | .7937 | .4047 | 59 | 31 | .7866 | .4098 |
| 2 | .7934 | .4049 | 58 | 32 | .7863 | .4099 |
| 3 | .7932 | .4050 | 57 | 33 | .7861 | .4101 |
| 4 | .7930 | .4052 | 56 | 34 | .7858 | .4102 |
| 5 | .7927 | .4054 | 55 | 35 | .7857 | .4104 |
| 6 | .7925 | •4055 | 54 | 36 | .7854 | .4106 |
| 7 | .7922 | •4057 | 53 | 37 | .7851 | .4107 |
| 8 | .7920 | •4059 | 52 | 38 | .7849 | .4109 |
| 9 | .7918 | •4060 | 51 | 39 | .7846 | .4111 |
| 10 | .7915 | •4062 | 50 | 40 | .7844 | .4112 |
| 11 | .7913 | .4064 | 49 | 41 | .7842 | .4114 |
| 12 | .7911 | .4066 | 48 | 42 | .7839 | .4116 |
| 13 | .7908 | .4067 | 47 | 43 | .7837 | .4117 |
| 14 | .7906 | .4069 | 46 | 44 | .7835 | .4119 |
| 15 | .7904 | .4071 | 45 | 45 | .7832 | .4121 |
| 16 | .7901 | .4072 | 44 | 46 | .7830 | .4122 |
| 17 | .7899 | .4074 | 43 | 47 | .7827 | .4124 |
| 18 | .7896 | .4076 | 42 | 48 | .7825 | .4126 |
| 19 | .7894 | .4077 | 41 | 49 | .7822 | .4127 |
| 20 | .7892 | .4079 | 40 | 50 | .7820 | .4129 |
| 21 | .7889 | .4081 | 39 | 51 | .7818 | .4131 |
| 22 | .7887 | .4082 | 38 | 52 | .7815 | .4132 |
| 23 | .7885 | .4084 | 37 | 53 | .7813 | .4134 |
| 24 | .7882 | .4086 | 36 | 54 | .7810 | .4135 |
| 25 | .7880 | .4087 | 35 | 55 | .7808 | .4137 |
| 26 | .7877 | .4089 | 34 | 56 | .78c6 | .4139 |
| 27 | .7875 | .4091 | 33 | 57 | .7803 | .4140 |
| 28 | .7873 | .4092 | 32 | 58 | .7801 | .4142 |
| 29 | .7870 | .4094 | 31 | 59 | .7798 | .4144 |
| 30 | .7868 | .4096 | 30 | 60 | .7796 | .4145 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. |

117 DEGREES.

62 DEGREES.

SECT. IV.] TACHEOMETRIC TABLE

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

| | and state in the second second | and the second second second | and the second second | | | | |
|------------------------|--|---|----------------------------|----------------------------|---|---|----------------------------|
| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
| 0 | .7796 | .4145 | 60 | 30 | .7723 | .4193 | 30 |
| I | .7794 | .4147 | 59 | 31 | .7721 | .4195 | 29 |
| 2 | .7791 | .4149 | 58 | 32 | .7718 | .4197 | 28 |
| 3 | .7789 | .4150 | 57 | 33 | .7716 | .4198 | 27 |
| 4 | .7786 | .4152 | 56 | 34 | .7713 | .4200 | 26 |
| 5 | .7786 | .4153 | 55 | 35 | .7711 | .4201 | 25 |
| 6 7 8 9 10 | .7782 .7779 .7777 .7777 .7774 .7772 | .4155 .4157 .4158 .4160 .4162 | 54 53 52 51 50 | 36 37 38 39 40 | .7709 .7706 .7704 .7701 .7699 | .4203 .4204 .4206 .4208 .4209 | 24 23 22 21 20 |
| 11 | .7769 | .4163 | 49 | 41 | .7696 | .4211 | 19 |
| 12 | .7767 | .4165 | 48 | 42 | .7694 | .4212 | 18 |
| 13 | .7765 | .4166 | 47 | 43 | .7692 | .4214 | 17 |
| 14 | .7762 | .4168 | 46 | 44 | .7689 | .4215 | 16 |
| 15 | .7760 | .4169 | 45 | 45 | .7687 | .4217 | 15 |
| 16 | •7757 | .4171 | 44 | 46 | .7684 | .4219 | I4 |
| 17 | •7755 | .4173 | 43 | 47 | .7682 | .4220 | I3 |
| 18 | •7752 | .4174 | 42 | 48 | .7679 | .4222 | I2 |
| 19 | •7750 | .4176 | 41 | 49 | .7677 | .4223 | I1 |
| 20 | •7748 | .4177 | 40 | 50 | .7674 | .4225 | I0 |
| 21 | •7745 | .4179 | 39 | 51 | .7672 | .4226 | 9 |
| 22 | •7743 | .4181 | 38 | 52 | .7669 | .4228 | 8 |
| 23 | •7740 | .4182 | 37 | 53 | .7667 | .4230 | 7 |
| 24 | •7738 | .4184 | 36 | 54 | .7664 | .4231 | 6 |
| 25 | •7735 | .4185 | 35 | 55 | .7662 | .4233 | 5 |
| 26 | •7733 | .4187 | 34 | 56 | .7659 | .4234 | 4 |
| 27 | •7731 | .4189 | 33 | 57 | .7657 | .4236 | 3 |
| 28 | •7728 | .4190 | 32 | 58 | .7655 | .4237 | 2 |
| 29 | •7726 | .4192 | 31 | 59 | .7652 | .4239 | 1 |
| 30 | •7723 | .4193 | 30 | 60 | .7650 | .4240 | 0 |
| • | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

118 DEGREES.

61 DEGREES.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------|--|--|----------------------------------|----------------------------------|--|--|----------------------------------|
| 0 I 2 3 4 5 | .7650 .7647 .7645 .7642 .7640 .7637 | .4240 .4242 .4243 .4245 .4246 .4248 | 60 59 58 57 56 55 | 30 31 32 33 34 35 | -7575 -7573 -7570 -7568 -7565 -7563 | .4286 .4287 .4289 .4290 .4292 .4293 | 30 29 28 27 26 25 |
| 6 7 8 9 10 | .7635 .7632 .7630 .7627 .7625 | .4250 .4251 .4253 .4255 .4255 .4256 | 54 53 52 51 50 | 36 37 38 39 40 | .7560 .7558 .7555 .7553 .7553 .7550 | .4295 .4296 .4298 .4299 .4299 .4301 | 24 23 22 21 20 |
| 11 12 13 14 15 | .7622 .7620 .7617 .7615 .7613 | .4257 .4259 .4260 .4262 .4263 | 49 48 47 46 45 | 41 42 43 44 45 | .7548 .7545 .7543 .7540 .7538 | .4302 .4304 .4305 .4307 .4308 | 19 18 17 16 15 |
| 16 17 18 19 20 | .7610 .7608 .7605 .7603 .7600 | .4265 .4266 .4268 .4269 .4271 | 44 43 42 41 40 | 46 47 48 49 50 | ·7535 ·7533 ·7530 ·7528 ·7525 | .4310 .4311 .4313 .4314 .4316 | 14 13 12 11 10 |
| 21 22 23 24 25 | .7598 .7595 .7593 .7590 .7588 | .4272 .4274 .4275 .4275 .4277 .4278 | 39 38 37 36 35 | 51 52 53 54 55 | .7523 .7520 .7518 .7515 .7513 | .4317 .4318 .4320 .4321 .4323 | 9 8 7 6 5 |
| 26 27 28 29 30 | •7585 •7583 •7580 •7578 •7578 •7575 | .4280 .4281 .4283 .4284 .4286 | 34 33 32 31 30 | 56 57 58 59 60 | .7510 .7508 .7505 .7503 .7500 | •4324 •4326 •4327 •4329 •4330 | 4 3 2 1 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | | Constant for Distance. | Constant for Difference in Height. | Minutes. |

119 DEGREES.

60 DEGREES.

Table for the Calculation of Heights and Distances from Tacheometer Readings-continued.

| Minutes. | Constant for Distance. | Constant for Difference in Height. | | |
|----------------------------|--|---|----------------------------------|--|
| 0 1 2 3 4 5 | .7500 .7498 .7495 .7492 .7490 .7487 | .4330 .4332 .4333 .4335 .4335 .4336 .4337 | 60 59 58 57 56 55 | |
| 6 | .7485 | •4339 | 54 | |
| 7 | .7482 | •4340 | 53 | |
| 8 | .7480 | •4342 | 52 | |
| 9 | .7477 | •4343 | 51 | |
| 10 | .7475 | •4345 | 50 | |
| 11 | •7472 | •4346 | 49 | |
| 12 | •7470 | •4348 | 48 | |
| 13 | •7467 | •4349 | 47 | |
| 14 | •7466 | •4350 | 46 | |
| 15 | •7462 | •4352 | 45 | |
| 16 | .7460 | ·4353 | 44 | |
| 17 | .7457 | ·4355 | 43 | |
| 18 | .7455 | ·4356 | 42 | |
| 19 | .7452 | ·4358 | 41 | |
| 20 | .7452 | ·4359 | 40 | |
| 21 | •7447 | .4360 | 39 | |
| 22 | •7444 | .4362 | 38 | |
| 23 | •7442 | .4363 | 37 | |
| 24 | •7439 | .4365 | 36 | |
| 25 | •7437 | .4366 | 35 | |
| 26 | •7434 | .4368 | 34 | |
| 27 | •7432 | .4369 | 33 | |
| 28 | •7429 | .4370 | 32 | |
| 29 | •7427 | .4372 | 31 | |
| 30 | •7424 | .4373 | 30 | |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. | |

120 DEGREES.

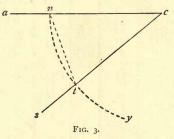
| Minutes. | Constant for Distance. | Constant for Difference in Height. | |
|----------------------------|--|---|----------------------------|
| 30 | .7424 | •4373 | 30 |
| 31 | .7422 | •4375 | 29 |
| 32 | .7419 | •4376 | 28 |
| 33 | .7416 | •4377 | 27 |
| 34 | .7414 | •4379 | 26 |
| 35 | .7411 | •4380 | 25 |
| 36 | .7409 | .4382 | 24 |
| 37 | .7406 | .4383 | 23 |
| 38 | .7404 | .4384 | 22 |
| 39 | .7401 | .4386 | 21 |
| 40 | .7399 | .4387 | 20 |
| 41 | .7396 | .4389 | 19 |
| 42 | .7394 | .4390 | 18 |
| 43 | .7391 | .4391 | 17 |
| 44 | .7388 | .4393 | 16 |
| 45 | .7386 | .4394 | 15 |
| 46 47 48 49 50 | .7383 .7381 .7378 .7376 .7376 .7373 | .4396 .4397 .4398 .4400 .4401 | I4 I3 I2 II I0 |
| 51 | .7370 | .4402 | 9 |
| 52 | .7368 | .4404 | 8 |
| 53 | .7365 | .4405 | 7 |
| 54 | .7363 | .4407 | 6 |
| 55 | .7360 | .4408 | 5 |
| 56 | •7358 | .4409 | 4 |
| 57 | •7355 | .4411 | 3 |
| 58 | •7353 | .4412 | 2 |
| 59 | •7350 | .4413 | 1 |
| 60 | •7347 | .4415 | 0 |
| | Constant for Distance. | Constant for Difference in Height. | Minutes. |

59 DEGREES.

SECTION V. TABLE OF CHORDS.

The Accurate Plotting of Angles on Large Scale Plans by means of Chords.

The TABLE OF CHORDS furnishes a means of laying down angles on paper more accurately than by an ordinary protractor. The procedure is as follows: after having drawn and measured the first side (say ac) of the figure to be plotted, describe from its end c as a centre, an arc ny of sufficient length to subtend the angle at that point. The radius cn with which the arc is described should be as great as convenience will permit. It must be decimally sub-divided, to be used as a scale for laying down the



chords taken from the table, in which their lengths are given in terms of the radius taken as I. Having described the arc, find in the table the length of the chord *nt* corresponding to the angle act. Suppose this angle to be 45°, the corresponding chord is .7654. Therefore from n lay off the chord nt, equal to .7654 of the radius-scale; and the line cs drawn through the point t will form the required angle act of 45°. The degree of accuracy attained will evidently depend on the length of the radius, and the care taken in drafting. The dividers in boxes of instruments are rarely fit for accurate arcs of more than about 6 inches diameter. For larger radii the beam compass is the best instrument to use, or if not obtainable, a straight strip of paper with the length of the radius marked on one edge; by laying it from c toward s, and at the same time placing another strip (with one edge divided to a radius-scale) from n toward t, we can by trial find their exact point of intersection at the required point t. The fastest method of plotting the chords is by the use of a beam-compass and a $\frac{1}{1000}$ scale, the compass being set to the length of the scale.

SECT. V.]

| | Table o | of Chords, in parts of a radius I; for protracting. | |
|---------|--|---|--------|
| Minutes | 0 4 4 0 0 0 | 2 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | 8 |
| 10° | .1743 .1749 .1755 .1761 .1766 | | 1161. |
| °6 | .1569 .1575 .1581 .1581 .1582 .1592 | | .1743 |
| 8° | .1395 .1401 .1407 .1407 .1413 .1418 | | .1509 |
| ۲° | .1221 .1227 .1233 .1238 .1238 .1244 | | .1395 |
| °9 | .1047 .1053 .1058 .1058 .1054 .1070 | .1082 .1087 .1087 .1093 .1093 .1105 .1105 .11140 .11140 .11140 .11145 .11151 .11151 .11151 .11151 .11169 .11169 .11192 .11192 .11192 .11192 | .1221 |
| D.º | .0872 .0878 .0884 .0884 .0890 .0890 | | .1047 |
| 4° | .0698 .0704 .0710 .0715 .0721 | | .0072 |
| 30 | .0524 .0529 .0535 .0535 .0541 | | \$600. |
| 2° | .0349 .0355 .0361 .0366 .0372 .0372 | 0.0390 0.0396 0.0396 0.0396 0.0407 0.0407 0.0413 0.0413 0.0413 0.0436 0.0436 0.0436 0.0454 0.0465 0.04555 0.04555 0.055555 0.055555 0.055555 0.055555 0.055555 0.055555 0.055555 0.055555 0.055555 0.055555 0.0555555 0.055555 0.055555 0.055555 0.0555555 0.0555555 0.055555555 0.05555555555 | .0524 |
| 1° | .0175 .0180 .0186 .0192 .0198 | | .0349 |
| 0° | .0000 .0006 .0012 .0012 .0013 .0023 | | .0175 |
| Minutes | 0 4 4 0 8 0 | 2222 222 222 222 222 222 222 222 222 2 | 8 |

174 DATA RELATING TO SURVEYING [PART V]

| | Table of Chords, in parts of a radius 1; for protracting. (Continued.) | | | | | |
|---------|--|---|---|---|--|--|
| 1 | | Comm | | | | |
| Minutes | 0 4 4 0 2 0 | 11 16 16 16 16 12 22 22 22 22 22 22 22 22 22 22 22 22 | 44 40 33 32 32 33 32 32 32 32 32 32 32 32 32 | 6444 2 2 4 4 9 4 9 4 9 4 9 4 9 9 9 9 9 9 | | |
| 20°. | .3473 .3479 .3484 .3484 .3490 .3496 .3502 | .3507 .3513 .3513 .3519 .3525 .3530 .3536 .3542 .3542 .3542 .3553 | .3585 .3576 .3576 .3576 .3576 .3582 .3582 .3583 .3583 | | | |
| 19° | .3301 .3307 .3312 .3318 .3318 .3318 | | .3393 .3393 .3398 .3404 .3404 .3416 .3416 .3421 | | | |
| 18° | .3129 .3134 .3134 .3140 .3146 .3152 .3152 | .3163 .3169 .3169 .3180 .3180 .3186 .3186 .3192 .3192 .3203 | · 3221 · 3226 · 3226 · 3238 · 3238 · 3238 · 3244 · 3249 | .3261 .3267 .3272 .3272 .3278 .3289 .3289 .3289 | | |
| 17° | .2956 .2962 .2968 .2973 .2973 | -2991 -2996 -2996 -2996 -3002 -3019 -3019 -3031 -3031 -3037 -3037 -3037 -3037 -3037 -3037 -3037 -3037 -3037 -3037 -3037 -3037 -3037 -3037 -3037 -3047 | .3048 .3054 .3056 .3065 .3065 .3071 .3071 | | | |
| 16° | .2783 .2789 .27895 .2801 .2807 .2812 | .2818 .2818 .2824 .2833 .2833 .2847 .2847 .2858 .2858 .2858 .2858 | .2876 .2881 .2887 .2887 .2893 .2899 .2899 | .2916 .2922 .2927 .2933 .2933 .2933 .2945 .2945 | | |
| 15° | .2611 .2616 .2622 .2628 .2638 | .2645 .2655 .2657 .2668 .2668 .2668 .2688 .2685 .2685 | .2703 .2703 .2714 .2714 .2726 .2726 .2732 | .2712 .2755 .2755 .2756 .2756 .2772 .2772 .2772 .2773 .2773 | | |
| 14° | .2437 .2443 .2449 .2449 .2455 .2466 | .2472 .2478 .2478 .2484 .2489 .2495 .2495 .2501 .2501 .2512 .2518 | -2530 -2536 -2536 -2536 -2536 -2553 -2553 -2559 | .2576 .2576 .2582 .25887 .25887 .2593 .2593 .2599 .25095 .2605 | | |
| 13° | .2264 .2270 .2276 .2281 .2287 .2287 | .2299 .2305 .2310 .2310 .2310 .2328 .2328 .2333 .2339 .2345 | .2357 .2357 .2362 .2368 .2368 .2368 .2385 .2385 | -2397 -2397 -2397 -2409 -2414 -2420 -2426 -2432 -2432 | | |
| 12° | .2091 .2096 .2102 .2108 .2114 .2119 | .2125 .2131 .2137 .2137 .2143 .2143 .2143 .2148 .2148 .2166 .2172 | .2183 .2183 .2195 .2195 .2200 .2206 .2218 | -2224 -2225 -2225 -2225 -2255 -2255 -2255 -2255 -2256 | | |
| 11° | .1917 .1923 .1928 .1928 .1934 .1940 | .1952 .1957 .1963 .1963 .1963 .1975 .1975 | .2010 .2010 .2015 .2021 .2023 .2033 .2038 | .2050 .2056 .2056 .2067 .2067 .2073 .2073 .2073 .2073 | | |
| Minutes | 0 4 4 0 0 1 | 112 116 116 116 112 122 222 222 222 226 226 | 4 40 336 32 30 30 30 30 30 30 30 30 30 30 30 30 30 | 65855 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | | |

TABLE OF CHORDS

ECT. V.

176 DATA RELATING TO SURVEYING [PART .V

| | Table of Chords, in parts of a radius I; for protracting. (<i>Continued</i> .) | | | | | |
|---------|--|---|--|--|--|--|
| Minutes | 0 2 4 0 8 0 I | 11 16 16 18 18 20 22 24 26 28 28 28 30 | 2 7 7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | | | |
| 40° | .6840 .6846 .6851 .6857 .6857 .6862 | .6873 .6879 .68879 .6884 .6895 .6895 .6895 .6901 .6911 .6917 .6917 | .6928 .6939 .6939 .6955 .6956 .6956 .6956 .6957 .6957 .6958 .6993 .6993 .6993 | | | |
| 39° | .6676 .6682 .6687 .6693 .6693 .6698 | .6709 .6715 .6715 .6720 .6731 .6736 .6742 .6742 .6753 .6753 | .6764 .6769 .6775 .6786 .6786 .6786 .6786 .6803 .6813 .6819 .6819 .6829 .6829 .6829 .6829 | | | |
| 38° | .6511 .6517 .6522 .6528 .6533 | .6544 .6550 .6555 .6566 .6566 .6572 .6583 .6588 .6594 | .6599 .6605 .6605 .6616 .6616 .6621 .6623 .6633 .6649 .6654 .6655 .6655 .6671 | | | |
| 37° | .6346 .6352 .6357 .6363 .6368 .6368 | .6379 .6385 .6396 .6396 .6396 .6401 .6412 .6412 .6412 .6412 .6423 | .6434 .6446 .6445 .6445 .6451 .6456 .6467 .6467 .6467 .6467 .6467 .6467 .6489 .6489 .6495 .6495 .6495 .6500 | | | |
| 36° | .6180 .6186 .6191 .6197 .6202 .6208 | .6214 .6219 .6225 .6225 .6233 .6236 .6236 .6236 .6247 .6258 .6258 | .6269 .6274 .6285 .6285 .6285 .6291 .6291 .6307 .6313 .6313 .6313 .6313 .6333 .6334 .6334 | | | |
| 35° | .6014 .6020 .6025 .6031 .6036 | .6047 .6053 .6058 .6054 .6075 .6075 .6081 .6092 .6092 | .6103 .6108 .6118 .6119 .6119 .6136 .6136 .6136 .6142 .6153 .6158 .6158 .6158 .6158 .6158 | | | |
| 34° | .5847 .5853 .5853 .5859 .5864 .5870 | .5881 .5886 .5892 .5892 .5892 .5903 .5903 .5914 .5914 .5926 .5926 .5926 .5926 | -5936 -5947 -5947 -5947 -5953 -5959 -5976 -5976 -5976 -5976 -5975 -5997 -5997 -5997 -5003 -6004 -6014 | | | |
| 33° | .5680 .5686 .5691 .5697 .5703 | | | | | |
| 32° | .5513 .5518 .5524 .5530 .5535 .5535 | | | | | |
| 31° | .5345 .5356 .5356 .5356 .5367 .5367 | .5378 .5384 .5384 .5395 .5395 .5406 .5406 .5412 .5418 .5423 | | | | |
| Minutes | 0 4 4 0 0 | 112 114 116 116 128 22 22 22 23 26 23 30 30 | 00000000000000000000000000000000000000 | | | |

.

| | Table of Chords, in parts of a radius 1; for protracting. (Continued.) | | | | | |
|-------------|---|---|--|--|--|--|
| | | (- | sommacu.) | | | |
| Minutes | 0 4 4 0 0 | 12 14 16 18 20 22 | 24 26 30 36 36 40 38 36 40 38 36 40 | 44 46 50 57 50 57 50 50 50 50 50 50 50 50 50 50 50 50 50 | | |
| 50° | .8452 .8458 .8463 .8463 .8463 .8468 .8473 | .8484 .8489 .8495 .8500 .8505 .8505 .8510 | | 8563 8573 8579 8579 8579 8579 8579 8579 85589 85589 85594 85605 8605 8605 8605 | | |
| 49° | .8294 .8299 .8304 .8310 .8310 .8315 | .8326 .8331 .8331 .8336 .8331 .8352 .8352 | | .8405 .8410 .8415 .8421 .8421 .8431 .8437 .8447 .8447 .8447 | | |
| 48° | .8135 .8140 .8145 .8145 .8151 .8151 .8161 | .8167 .8172 .8177 .8183 .8183 .8193 .8193 | .0190 .8204 .8209 .8220 .8220 .8225 .8230 .8235 .8236 .8236 .8231 | .8246 .8251 .8257 .8257 .8267 .8267 .8273 .8273 .8273 .8273 .8289 .8289 | | |
| 47° | .7975 .7980 .7986 .7991 .7996 .7996 | .8007 .8012 .8018 .8023 .8023 .8034 | .8039 .8050 .8050 .8050 .8050 .8071 .8071 .8071 .8071 .8075 | .8087 .8092 .8098 .8103 .8103 .8113 .8113 .8113 .8124 .8124 .8135 | | |
| 46° | .7815 .7820 .7825 .7831 .7831 .7831 | .7847 .7852 .7857 .7853 .7863 .7863 .7873 | .7879 .7884 .7895 .7895 .7906 .7911 .7911 .7916 .7922 | .7927 .7938 .7938 .7943 .7948 .7959 .7959 .7959 .7970 | | |
| 45° | .7654 .7659 .7664 .7670 .7670 .7675 | .7686 .7697 .7702 .7770 .7713 | .7710 .7729 .7729 .7734 .7740 .7746 .7745 .7750 .7755 | .77772 .77772 .77772 .7782 .7783 .7793 .7793 .7793 .7793 .7793 .7793 .7793 .7793 .77809 .7809 | | |
| 44° | .7492 .7498 .7503 .7508 .7514 | .7524 .7530 .7535 .7535 .7546 .7546 | .7557 .7562 .7568 .7578 .7578 .7584 .7589 .7589 .7589 .7589 | .7605 .7611 .7616 .7621 .7627 .7632 .7633 .7643 .7648 | | |
| 43° | -7330 -7335 -7335 -7346 -7346 -7356 -7352 | .7362 .7368 .7373 .7373 .7373 .7379 .7384 | .7395 .7400 .7411 .7417 .7417 .7427 .7427 .7423 .7433 .7438 | .7443 .7449 .7454 .7460 .7465 .7465 .7481 .7481 .7487 .7487 | | |
| 42° | .7167 .7173 .7173 .7178 .7184 .7189 | .7200 .7205 .7211 .7216 .7222 .7222 | .7232 .7238 .7243 .7249 .7249 .7249 .7249 .7260 .7265 .7265 .7270 .7276 | .7281 .7287 .7292 .7298 .7303 .7308 .7314 .7319 .7319 .7325 .7330 | | |
| 41 ° | .7004 .7010 .7015 .7015 .7020 .7020 | .7037 .7042 .7048 .7053 .7053 .7054 | .7009 .7075 .7086 .7086 .7087 .7097 .7102 .7108 .71108 .71108 | .7118 .7124 .7129 .7135 .7140 .7146 .7151 .7156 .7156 .7156 | | |
| Minutes | 0 4 4 0 0 0 | 12 16 16 18 20 20 22 22 | 24 26 32 36 33 32 33 32 33 32 33 32 32 32 32 32 32 | 44 46 50 57 56 56 56 56 56 56 57 50 50 57 50 50 50 50 50 50 50 50 50 50 50 50 50 | | |

DATA RELATING TO SURVEYING [PART VI.

| | Table of Chords, in parts of a radius 1; for protracting. (Continued.) | | | | |
|------------|---|--|------------------|--|--|
| Minutes | 0 4 4 0 % O | 11 14 14 14 15 14 16 14 17 14 18 14 19 14 10 14 11 14 11 14 14 14 15 14 16 14 17 14 18 14 19 14 10 14 10 14 10 14 10 14 10 14 10 14 10 14 10 14 10 14 10 14 10 14 10 14 10 14 10 14 10 14 10 14 10 14 10 14 10 < | 828 Q | | |
| 60° | 1.0000 1.0005 1.0010 1.0015 1.0020 1.0020 | L.0030 L.0035 L.0040 L.0050 L.0055 L. | 1.0146 1.0151 | | |
| 59° | .9848 .9854 .9859 .9864 .9869 | -9889 -9889 -9889 -9889 -9989 -9914 -9914 -9914 -9914 -9936 -9955 -9955 -9955 -9955 -9955 -9956 -90566 -9056 -9056 -9056 -9056 -9056 -9056 -9056 -9056 -9056 -9056 | 00000.1 | | |
| 58° | .9696 .9701 .1720 .9716 .9716 .9717 | .9727 .9732 .9737 .9742 .9747 .9747 .9757 .9757 .9757 .9755 .9755 .9755 .9758 .9778 .9778 .9778 .9778 .9778 .9778 .9778 .97888 .97888 .97888 .97888 .97888 .97888 .97888 .97888 .97888 .97888 .97888 .97888 .97888 .97888 .97888 .978888 .97888 .97888 .97888 .978888 .978888 .97888 .978888 .978888 .978888 .97888888 .978888 .97888888 .978888 .978888888 .9788888888 .9788888888 .978888888888 | .9843 .9848 | | |
| 57° | .9543 .9548 .9553 .9559 .9564 | 9574 9589 9589 9589 9594 9604 9605 9615 9625 9625 9635 9640 9640 9655 9655 9655 9655 9651 9651 | 1696. | | |
| 56° | .9389 .9395 .9400 .9405 .9405 | .9425 .9425 .9425 .9436 .9446 .9446 .9446 .9446 .9447 .9466 .9447 .9482 .9482 .9487 .9487 .9487 .9487 .9487 .9487 .9512 .9518 | .9538 .9538 | | |
| 55° | .9235 .9240 .9245 .9250 .9256 | .9266 .9276 .9281 .9287 .9287 .9287 .9297 .9397 .9317 .9317 .9328 .9328 .9328 .9333 .9359 .9359 .9359 | .9384 .9389 | | |
| 54° | 0800. 0085 0090 0000. 0005 0010. | 91111 9121 9121 9121 9132 9132 9137 9157 9157 9157 9153 9153 9153 9173 9173 9173 9173 9173 9173 9173 917 | .9230 | | |
| 53° | .8924 .8929 .8934 .8940 .8945 .8950 | | .9075 .9080 | | |
| 52° | .8767 .8773 .8773 .8778 .8778 .8783 .8783 .8794 | | .8919 .8924 | | |
| 51° | .8610 .8615 .8621 .8621 .8621 .8631 | | .8762 | | |
| Minutes | 0 % 0 4 9 0 | 1 | 80.00 | | |

SECT. V.]

| | Table of Chords, in parts of a radius 1; for protracting. (Continued.) | | | | |
|---------|---|---|--|--|--|
| Minutes | 0 % 4 % 0 | 12 14 16 18 18 20 22 24 26 28 28 30 30 | 0 2 2 2 2 2 2 4 4 4 4 4 5 2 2 4 5 2 4 5 2 4 5 2 4 5 2 4 5 2 5 5 5 5 5 5 5 5 5 5 5 5 5 | | |
| °07 | 1.1472 1.1476 1.1481 1.1481 1.1486 1.1491 1.1491 | 1.1500 1.1505 1.1505 1.1519 1.1519 1.1529 1.1533 1.1533 1.1533 | 1.1548 1.1557 1.1557 1.1557 1.1567 1.1571 1.1576 1.1586 1.1586 1.1586 1.1586 1.1590 1.1590 1.1590 1.1590 1.1590 1.1600 1.1600 1.1600 1.1600 | | |
| .69° | 1.1328 1.1333 1.1338 1.1338 1.1342 1.1342 1.1352 | 1.1357 1.1362 1.1362 1.1366 1.1371 1.1376 1.1376 1.1381 1.1386 1.1386 1.1385 1.1385 1.1400 | 1.1405 1.1409 1.14409 1.1424 1.1424 1.1423 1.1433 1.1443 1.1443 1.1445 1.1457 1.1457 1.1457 1.1457 1.1467 1.1467 1.1467 1.1467 1.1462 | | |
| , 68° | 1.1184 1.1189 1.1194 1.1198 1.1203 1.1203 | 1.1213 1.1218 1.1222 1.1227 1.1227 1.1237 1.1237 1.1237 1.1246 1.1251 1.1256 | 1.1261 1.1266 1.1275 1.1275 1.1280 1.1280 1.1280 1.1280 1.1280 1.1280 1.1309 1.1309 1.1329 1.1323 1.1328 1.1328 | | |
| 67° | 1.1039 1.1044 1.1048 1.1053 1.1053 1.1053 | 1.1068 1.1073 1.1073 1.1082 1.1082 1.1087 1.1097 1.1102 1.1107 1.1107 | 1.1116 1.1121 1.1126 1.1126 1.1136 1.1136 1.1146 1.1150 1.1155 1.1156 1.1166 1.1174 1.1174 1.1174 1.1174 | | |
| 66° | 1.0893 1.0898 1.0903 1.0903 1.0912 1.0912 | 1.0922 1.0927 1.0932 1.0937 1.0945 1.0946 1.0956 1.0956 1.0961 | 1.0971 1.0976 1.0986 1.0985 1.0990 1.0995 1.0995 1.1000 1.1000 1.1014 1.1014 1.1014 1.1024 1.1024 1.1024 1.1023 1.1023 1.1023 | | |
| 65° | 1.0746 1.0751 1.0756 1.0756 1.0761 1.0766 1.0771 | 1.0775 1.0785 1.0785 1.0795 1.0795 1.0800 1.0800 1.0810 1.0815 1.0820 | 1.0824 1.0824 1.0834 1.0834 1.0849 1.0854 1.0853 1.0853 1.0853 1.0884 1.0884 1.0884 1.0884 1.0884 1.0885454 1.0885454 1.0885454 1.0885454 1.08854545454545454545454545454545455455455 | | |
| 64° | 1.0598 1.0603 1.0608 1.0613 1.0613 1.0613 1.0623 | 1.0628 1.0633 1.0643 1.0643 1.0648 1.0653 1.0658 1.0667 1.0667 | 1.0657 1.0682 1.0687 1.0692 1.0697 1.0697 1.0697 1.0702 1.0712 1.0712 1.0712 1.0713 1.0736 1.0736 1.0736 1.0736 1.0736 | | |
| 63° | 1.0450 1.0455 1.0460 1.0465 1.0475 1.0475 | 1.0480 1.0485 1.0495 1.0495 1.0500 1.0504 1.0504 1.0514 1.0514 1.0524 | $\begin{array}{c} 1.0529\\ 1.0539\\ 1.0539\\ 1.0539\\ 1.0554\\ 1.0556\\ 1.0556\\ 1.0569\\ 1.0569\\ 1.0569\\ 1.0588\\ 1.0588\\ 1.0588\\ 1.0588\\ 1.0593\\ 1.0598\end{array}$ | | |
| 62° | 1.0301 1.0306 1.0311 1.0316 1.0321 1.0325 | 1.0331 1.0336 1.0346 1.0346 1.0351 1.0356 1.0356 1.0356 1.0370 1.0375 | 1.0380 1.0385 1.0395 1.0395 1.0410 1.0410 1.0410 1.0410 1.0420 1.0430 1.0430 1.0440 1.0440 1.0440 1.0440 1.0440 | | |
| 61° | 1.0151 1.0156 1.0161 1.0161 1.0171 1.0171 | 1.0181 1.0186 1.0196 1.0196 1.0201 1.0201 1.0216 1.0216 1.0216 1.0226 | 1.0231 1.0236 1.0246 1.0246 1.0256 1. | | |
| Minutes | 0 % 4 % 0 | 112 116 116 116 116 112 128 222 222 226 226 228 226 228 200 200 200 200 200 200 200 200 200 | 22 25 25 25 25 25 25 25 25 25 25 25 25 2 | | |

180 DATA RELATING TO SURVEYING [PART VI.

| | Table of Chords, in parts of a radius I; for protracting. (Continued.) | | | | | |
|---------|--|--|---------|--|--|--|
| Minutes | 0 4 4 0 8 0 | 2 4 4 4 7 3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 | | | | |
| 80° | 1.2856 1.2860 1.2865 1.2869 1.2874 1.2878 | 1.2882 1.2885 1.2896 1.2896 1.2900 1.2905 1.2905 1.2905 1.2918 1.2916 1.2936 1.2936 1.2936 1.2936 1.2936 1.2936 1.2936 1.29566 1.29566 1.29566 1.29566 1.29566 1.29566 1.29566 1.29566 1.29566 | 6067.1 | | | |
| -61 | 1.2722 1.2726 1.2731 1.2735 1.2740 1.2740 1.2744 | 1.2748 1.2757 1.2756 1.2756 1.2756 1.2775 1.2789 1.2789 1.2789 1.2789 1.2789 1.2789 1.2789 1.2789 1.2789 1.2802 1.2802 1.2811 1.2825 1.28333 1.28333 1.283333 1.28333 1.28333 1.28333 1.2833333 1.2833333 1.2833333333 1.28333333333333333333333333333333333333 | nC07.1 | | | |
| 78° | 1.2586 1.2591 1.2595 1.2600 1.2600 1.2604 1.2609 | L:2614 1.2618 1.2627 1.2627 1.2636 1.2641 1.2641 1.2641 1.2641 1.2641 1.2656 1.2656 1.2656 1.2656 1.2668 1.2677 1.2681 1.2695 1.26555 1.26555 1.26555 1.26555 1.25555 1.25555 1.25555 1.25555555555 | 1.2/24 | | | |
| 77° | 1.2450 1.2455 1.2459 1.2464 1.2468 1.2468 1.2473 | 1.2478 1.2487 1.2487 1.2487 1.2487 1.2496 1.2500 1.2500 1.2500 1.2532 1.2532 1.2553 1.2555 1.2556 1.25556 1.2555 | 1.2300 | | | |
| 76° | 1.2313 1.2318 1.2328 1.2322 1.2322 1.2336 1.2336 | 1.2341 1.2345 1.2355 1.2355 1.23564 1.23564 1.2375 1.2375 1.2375 1.2375 1.2375 1.2375 1.2375 1.2375 1.2405 1.2405 1.2405 1.2405 1.2418 1.2428 1.2418 1.2428 1.2428 1.2418 1.2428 1.2448 | 0642.1 | | | |
| 75° | 1.2175 1.2180 1.2184 1.2184 1.2189 1.2189 1.2194 1.2194 | 1.2203 1.2203 1.2217 1.2217 1.2215 1.2221 1.2235 1.2249 1.2249 1.2249 1.22555 1.22555 1.22555 1.22555 1.22555 1.22555 1.22555 1.225555 1.225555 1.225555 1.225555555555 | 1.2315 | | | |
| 74° | 1.2036 1.2041 1.2046 1.2050 1.2050 1.2050 | 1.2064 1.2064 1.2073 1.2073 1.2083 1.2087 1.2087 1.2097 1.2097 1.2097 1.2097 1.2106 1.2106 1.2129 1.2124 1.2124 1.2124 1.2124 1.2124 1.2124 1.2124 1.2124 1.2124 1.2157 1.2157 1.2166 1.2157 1.2166 1.2157 1.2166 1.2157 1.2166 1.2157 1.2166 1.2157 1.2166 1.2157 1.2166 1.2157 1.2166 1. | \$/12.1 | | | |
| 73° | 1.1896 1.1901 1.1906 1.1910 1.1910 1.1915 1.1920 | 1.1924 1.1923 1.1933 1.1938 1.1948 1.1948 1.1957 1.1957 1.1957 1.1956 1.1956 1.1956 1.1956 1.1956 1.1996 1.1996 1.1996 1.1996 1.1996 1.1996 1.1996 1.1996 1.1996 1.2018 1.2018 1.2018 1.2018 | 1.2030 | | | |
| 72° | 1.1756 1.1760 1.1765 1.1775 1.1775 1.1775 | 1.1793 1.1793 1.1793 1.1793 1.1793 1.1803 1.1803 1.1805 1.1812 1.1825 1.1835 1.1835 1.1835 1.1856 1.1856 1.1856 1.1856 1.1856 1.1856 1.1856 1.1857 1.1857 1.1873 1.18833 1.18833 1.18833 1.18833 1.18833 1.18833 1.18833 1.18833 1 | I. Ioyo | | | |
| °17 | 1.1614 1.1619 1.1624 1.1628 1.1633 1.1633 | 1.1642 1.1647 1.1657 1.1657 1.1666 1.1666 1.1666 1.1666 1.1686 1.1686 1.1686 1.1689 1.1699 1.1709 1.1709 1.1727 1.1723 1.1723 1.1723 1.1723 1.1732 1.17732 1.17752 1.17752 1.17752 1.17752 1.17752 1.17752 1.17752 1.17752 1.1 | 1.1750 | | | |
| Minutes | 0 % 4 % % 0 | 1 | 00 | | | |

Г

SECT. V.] TABLE OF CHORDS

| | Table of Chords, in parts of a radius 1; for protracting. (Continued.) | | | | | |
|---------|---|--|---|--|--|--|
| Minutes | 0 4 4 9 0 0 | 20 20 20 20 20 20 20 20 20 20 20 20 20 2 | 50 50 50 50 50 50 50 50 50 50 50 50 50 5 | 55 55 52 60 58 65 5 52 | | |
| 89° | 1.4018 1.4022 1.4026 1.4031 1.4035 1.4035 | 1.4043 1.4047 1.4051 1.4055 1.4055 1.4056 1.4068 1.4068 1.4072 1.4072 | 1.4084 1.4089 1.4097 1.4101 1.4101 1.4105 1.4105 1.4113 1.4113 1.4113 1.4113 1.4113 | 1.4126 1.4130 1.4134 1.4134 1.4138 1.4142 | | |
| 88° | 1.3893 1.3897 1.3902 1.3906 1.3910 1.3910 | 1.3918 1.3922 1.3927 1.3931 1.3933 1.3933 1.3933 1.3943 1.3943 1.3943 1.3952 | 1.3960 1.3968 1.3968 1.3972 1.3972 1.3985 1.39755 1.39755 1.39755 1.39755 1.397555 1.397555 1.3975555555555 | 1.4002 1.4006 1.4010 1.4010 1.4018 | | |
| 87° | 1.3767 1.3771 1.3776 1.3786 1.3780 1.3784 1.3788 | 1.3792 1.3797 1.3801 1.3805 1.3805 1.3805 1.3809 1.3825 1.3813 1.3813 1.3813 1.3813 1.3813 1.3822 1.3822 | 1.3834 1.3839 1.3839 1.3843 1.3847 1.3855 1.3855 1.3864 1.3868 1.3868 1.3872 | 1.3876 1.3881 1.3885 1.3885 1.3893 1.3893 | | |
| 86° | 1.3640 1.3644 1.3644 1.36548 1.3657 1.3657 1.3661 | 1.3665 1.3670 1.3674 1.3674 1.3682 1.3687 1.3687 1.3687 1.3695 1.3695 1.3695 | 1.3708 1.3712 1.3716 1.3716 1.3721 1.3729 1.3729 1.3733 1.3746 1.3746 | 1.3750 1.3754 1.3759 1.3759 1.3763 1.3767 | | |
| 85° | 1.3512 1.3516 1.3526 1.3520 1.3529 1.3529 1.3533 | 1.3538 1.3542 1.3546 1.3556 1.3555 1.3555 1.3555 1.3553 1.3553 1.3553 | 1.3580 1.3585 1.3585 1.3589 1.3593 1.3597 1.3602 1.3602 1.3610 1.3610 1.3619 | 1.3623 1.3627 1.3631 1.3631 1.3640 | | |
| 84° | 1.3383 1.3387 1.3387 1.3391 1.3396 1.3400 1.3400 | 1.3409 1.3413 1.3417 1.3417 1.3426 1.3426 1.3426 1.3430 1.3430 1.3439 1.3439 | 1.3452 1.3456 1.3466 1.3465 1.3465 1.3473 1.3473 1.3473 1.3486 1.3486 1.3490 | 1.3495 1.3499 1.3503 1.3503 1.3508 1.3512 | | |
| 83° | 1.3252 1.3257 1.3251 1.3261 1.3265 1.3270 1.3270 | 1.3279 1.3283 1.3287 1.3295 1.3296 1.3296 1.3309 1.3309 1.3309 1.3309 1.3313 | 1.3322 1.3326 1.3335 1.3335 1.3335 1.3344 1.3348 1.3348 1.3357 1.3357 1.3357 | 1.3365 1.3370 1.3374 1.3378 1.3378 1.3383 | | |
| 82° | 1.3121 1.3126 1.3130 1.3134 1.3134 1.3139 1.3143 | 1.3147 1.3152 1.3156 1.3156 1.3165 1.3169 1.3169 1.3174 1.3178 1.3178 1.3178 | 323203320 | I.3235 I.3239 I.3244 I.3248 I.3248 I.3252 | | |
| 81° | 1.2989 1.2993 1.2998 1.2998 1.3002 1.3007 1.3011 | 1.3015 1.3020 1.3024 1.3029 1.3033 1.3038 1.3038 1.3042 1.3042 1.3051 | 1.3060 1.3068 1.3068 1.3073 1.3077 1.3082 1.3082 1.3095 1.3095 1.3095 | 1.3104 1.3108 1.3112 1.3112 1.3117 1.3121 | | |
| Minutes | 044000 | 12 16 16 16 16 16 12 26 26 26 26 26 26 26 26 26 26 26 26 26 | 332 336 336 336 338 336 338 338 338 338 338 | 52525 65864 80 80 80 80 80 80 80 80 80 80 80 80 80 | | |

| Table | giving | the | circumference | and | area | of | a | circle | corresponding |
|-------|--------|-----|---------------|-------|-------|------|---|--------|---------------|
| | | | to a give | en di | amete | er.* | | | |

| | | | 1 | | | 1 | | |
|----------------|---------------------|--------------------|----------------|---------------------|--------------------|----------------|---------------------|---------|
| Dia- meter. | Circum- ference. | Area. | Dia- meter. | Circum- ference. | Area. | Dia- meter. | Circum- ference. | Area. |
| | | | | | | | | |
| 10 | 31.416 | 78.5398 | 40 | 125.66 | 1256.64 | 70 | 219.91 | 3848.45 |
| II | 34.558 | 95.0332 | 41 | 128.81 | 1320.25 | 71 | 223.05 | 3959.19 |
| 12 | 37.699 | 113.097 | 42 | 131.95 | 1385.44 | 72 | 226.19 | 4071.50 |
| | 40.841 | | | 135.09 | | | 200.24 | 4185.39 |
| 13 | | 132.732 153.938 | 43 44 | 135.09 | 1452.20 1520.53 | 73 | 229.34 232.48 | 4300.84 |
| 14 15 | 43.982 | 176.715 | 44 | 141.37 | 1520.53 | 74 | 235.62 | 4417.86 |
| | | | | | | | | |
| 16 | 50.265 | 201.062 | 46 | 144.51 | 1661.90 | 76 | 238.76 | 4536.46 |
| 17 | 53.407 | 226.980 | 47 | 147.65 | 1734.94 | 77 | 241.90 | 4656.63 |
| 18 | 56.549 | 254.469 | 48 | 150.80 | 1809.56 | 78 | 245.04 | 4778.36 |
| 19 | 59.690 | 283.529 | 49 | 153.94 | 1885.74 | 79 | 248.19 | 4901.67 |
| 20 | 62.832 | 314.159 | 50 | 157.08 | 1963.50 | 80 | 251.33 | 5026.55 |
| 21 | 65.973 | 346.361 | 51 | 160.22 | 2042.82 | 81 | 254.47 | 5153.00 |
| 22 | 69.115 | 380.133 | 52 | 163.36 | 2123.72 | 82 | 257.61 | 5281.02 |
| 23 | 72.257 | 415.476 | 53 | 166.50 | 2206.18 | 83 | 260.75 | 5410.61 |
| 24 | 75.398 | 452.389 | 54 | 169.65 | 2290.22 | 84 | 263.89 | 5541.77 |
| | 78.540 | 490.874 | 55 | 172.79 | 2375.83 | 85 | 267.04 | 5674.50 |
| 25 26 | 81.681 | 530.929 | 50 | 175.93 | 2463.01 | 86 | 270.18 | 5808.80 |
| 27 | 84.823 | 572.555 | 57 | 179.07 | 2551.76 | 87 | 273.32 | 5944.68 |
| | | | - | | 00. | 88 | | 6082.12 |
| 28 | 87.965 | 615.752 | 58 | 182.21 | 2642.08 | | 276.46 | |
| 29 | 91.106 | 660.520 706.858 | 59 60 | 185.35 | 2733.97 | 89 | 279.60 | 6221.14 |
| 30 | 94.248 | | 1000 | 188.50 | 2827.43 | 90 | 282.74 | |
| 31 | 97.389 | 754.768 | 61 | 191.64 | 2922.47 | 91 | 285.88 | 6503.88 |
| 32 | 100.53 | 804.248 | 62 | 194.78 | 3019.07 | 92 | 289.03 | 6647.61 |
| 33 | 103.67 | 855.299 | 63 | 197.92 | 3117.25 | 93 | 292.17 | 6792.91 |
| 34 | 106.81 | 907.920 | 64 | 201.06 | 3216.99 | 94 | 295.31 | 6939.78 |
| | 109.96 | 962.113 | 65 | 204.20 | 3318.31 | 95 | 298.45 | 7088.22 |
| 35 36 | 113.10 | 1017.88 | 66 | 207.35 | 3421.19 | 96 | 301.59 | 7238.23 |
| 37 | 116.24 | 1075.21 | 67 | 210.49 | 3525.65 | 97 | 304.73 | 7389.81 |
| 38 | 119.38 | 1134.11 | 68 | 213.63 | 3631.68 | 98 | 307.88 | 7542.96 |
| 39 | 122.52 | 1194.59 | 69 | 216.77 | 3739.28 | 99 | 311.02 | 7697.69 |
| | 1 | | 1 | | | 11 | - | |

* From The Smithsonian Geographical Tables, Washington, 1906, p. 23.

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from 1 to 1000.*

In the roots, wherever the effect of a fifth decimal would be to add I to the fourth and final decimal, the addition has been made.

| | | | | , | | | | | |
|-----|-----------------------|--------|---------|---------|-----|---------|---------|---------|-----------|
| No. | Square. | Cube. | Sq. Rt. | Cu. Rt. | No. | Square. | Cube. | Sq. Rt. | Cu. Rt. |
| 1 | I | I | I. | 1 | 51 | -6 | | (a) (a) | |
| | and the second second | | | I. | | 2601 | 132651 | 7.1414 | 3.7084 |
| 2 | / 4 | 8 | 1.4142 | 1.2599 | 52 | 2704 | 140608 | 7.2111 | 3.7325 |
| 3 | 9 | 27 | 1.7321 | I.4422 | 53 | 2809 | 148877 | 7.2801 | 3.7563 |
| 4/ | 16 | 64 | 2. | 1.5874 | 54 | 2916 | 157464 | 7.3485 | 3.7798 |
| 5 | 25 | 125 | 2.2361 | 1.7100 | 55 | 3025 | 166375 | 7.4162 | 3.8030 |
| | | | | | | 5025 | | 1.4102 | |
| 6 | 36 | 216 | 2.4495 | 1.8171 | 56 | 3136 | 175616 | 7.4833 | 3.8259 |
| 78 | 49 | 343 | 2.6458 | 1.9129 | 57 | 3249 | 185193 | 7.5498 | 3.8485 |
| 8 | 64 | 512 | 2.8284 | 2. | 58 | 3364 | 195112 | 7.6158 | 3.8709 |
| 9 | 81 | 729 | 3. | 2.0801 | | 3481 | | | |
| IO | 100 | 1000 | | | 59 | | 205379 | 7.6811 | 3.8930 |
| 10 | 100 | 1000 | 3.1623 | 2.1544 | 60 | 3600 | 216000 | 7.7460 | 3.9149 |
| 11 | 121 | 1331 | 3.3166 | 2.2240 | 61 | 3721 | 226981 | 7.8102 | 3.9365 |
| 12 | I44 | 1728 | 3.4641 | 2.2894 | 62 | 3844 | 238328 | 7.8740 | |
| 13 | 169 | 2197 | 3.6056 | | | | | | 3.9579 |
| | | | | 2.3513 | 63 | 3969 | 250047 | 7.9373 | 3.9791 |
| 14 | 196 | 2744 | 3.7417 | 2.4101 | 64 | 4096 | 262144 | 8. | 4. |
| 15 | 225 | 3375 | 3.8730 | 2.4662 | 65 | 4225 | 274625 | 8.0623 | 4.0207 |
| 16 | 256 | 4096 | 4. | 2.5198 | 66 | 4356 | 287496 | 8.1240 | 4.0412 |
| 17 | 289 | 4090 | 4.1231 | 2.5713 | 67 | 4350 | 300763 | 8.1854 | 4.0412 |
| 18 | | 4913 | | | | | | 0.1054 | |
| | 324 | 5832 | 4.2426 | 2.6207 | 68 | 4624 | 314432 | 8.2462 | 4.0817 |
| 19 | 361 | 6859 | 4.3589 | 2.6684 | 69 | 4761 | 328509 | 8.3066 | 4.1016 |
| 20 | 400 | 8000 | 4.4721 | 2.7144 | 70 | 4900 | 343000 | 8.3666 | 4.1213 |
| 21 | 441 | 9261 | 4.5826 | 2.7589 | 71 | 5041 | 257011 | 8.4261 | 4 7 408 |
| 22 | 441 | 10648 | | 2.7509 | | | 357911 | | 4.1408 |
| | | | 4.6904 | 2.8020 | 72 | 5184 | 373248 | 8.4853 | 4.1602 |
| 23 | 529 | 12167 | 4.7958 | 2.8439 | 73 | 5329 | 389017 | 8.5440 | 4.1793 |
| 24 | 576 | 13824 | 4.8990 | 2.8845 | 74 | 5476 | 405224 | 8.6023 | 4.1983 |
| 25 | 625. | 15625 | 5. | 2.9240 | 75 | 5625 | 421875 | 8.6603 | 4.2172 |
| 26 | 676 | 10006 | 5 0000 | 2.9625 | 76 | | 108056 | 0 | 1 0 0 = 0 |
| | | 17576 | 5.0990 | | | 5776 | 438976 | 8.7178 | 4.2358 |
| 27 | 729 | 19683 | 5.1962 | 3. | 77 | 5929 | 456533 | 8.7750 | 4.2543 |
| 28 | 784 | 21952 | 5.2915 | 3.0366 | 78 | 6084 | 474552 | 8.8318 | 4.2727 |
| 29 | 841 | 24389 | 5.3852 | 3.0723 | 79 | 6241 | 493039 | 8.8882 | 4.2908 |
| 30 | 900 | 27000 | 5.4772 | 3.1072 | 80 | 6400 | 512000 | 8.9443 | 4.3089 |
| 31 | 961 | | 6-0 | | 81 | 6-6- | | 1 | |
| | - | 29791 | 5.5678 | 3.1414 | | 6561 | 531441 | 9. | 4.3267 |
| 32 | 1024 | 32768 | 5.6569 | 3.1748 | 82 | 6724 | 551368 | 9.0554 | 4.3445 |
| 33 | 1089 | 35937 | 5.7446 | 3.2075 | 83 | 6889 | 571787 | 9.1104 | 4.3621 |
| 34 | 1156 | 39304 | 5.8310 | 3.2396 | 84 | 7056 | 592704 | 9.1652 | 4.3795 |
| 35 | 1225 | 42875 | 5.9161 | 3.2711 | 85 | 7225 | 614125 | 9.2195 | 4.3968 |
| 36 | 1296 | 46656 | 6. | 2 2010 | 86 | 1206 | 636056 | 0.0005 | |
| | - | | | 3.3019 | | 7396 | | 9.2736 | 4.4140 |
| 37 | 1369 | 50653 | 6.0828 | 3.3322 | 87 | 7569 | 658503 | 9.3274 | 4.4310 |
| 38 | 1444 | 54872 | 6.1644 | 3.3620 | 88 | 7744 | 681472 | 9.3808 | 4.4480 |
| 39 | 1521 | 59319 | 6.2450 | 3.3912 | 89. | 7921 | 704969 | 9.4340 | 4.4647 |
| 40 | 1600 | 64000 | 6.3246 | 3.4200 | 90 | 8100 | 729000 | 9.4868 | 4.4814 |
| 41 | 1681 | 68921 | 6 1021 | 24.80 | 91 | 8281 | HEATHY | 0 5204 | 1 1070 |
| | | | 6.4031 | 3.4482 | | | 753571 | 9.5394 | 4.4979 |
| 42 | 1764 | 74088 | 6.4807 | 3.4760 | 92 | 8464 | 778688 | 9.5917 | 4.5144 |
| 43 | 1849 | 79507 | 6.5574 | 3.5034 | 93 | 8649 | 804357 | 9.6437 | 4.5307 |
| 44 | 1936 | 85184 | 6.6332 | 3.5303 | 94 | 8836 | 830584 | 9.6954 | 4.5468 |
| 45 | 2025 | 91125 | 6.7082 | 3.5569 | 95 | 9025 | 857375 | 9.7468 | 4.5629 |
| 46 | 2116 | 97336 | 6.7823 | 3.5830 | 96 | 9216 | 884736 | 9.7980 | 4.5789 |
| 47 | 2209 | 103823 | 6.8557 | 3.6088 | 97 | 9409 | 912673 | 9.8489 | 4.5709 |
| 47 | - | | 6.9282 | 3.6342 | 98 | 9604 | 941192 | 9.8409 | 4.5947 |
| | 2304 | 110592 | | | | | | | |
| 49 | 2401 | 117649 | 7. | 3.6593 | 99 | 9801 | 970299 | 9.9499 | 4.6261 |
| 50 | 2500 | 125000 | 7.0711 | 3.6840 | 100 | 10000 | 1000000 | IO. | 4.6416 |
| - | | | | | | 1 | | | |

* From Smithsonian Geographical Tables, Washington, 1906, checked by comparison with a similar table in The Civil Engineer's Pocket-book, Trautwine, New York, 1900.

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from 1 to 1000—continued.

| | | | | | | | | | - 1 |
|-----|---------|-----------------|---------|---------|-----|---------|---------|---------|--|
| No. | Square. | Cube. | Sq. Rt. | Cu. Rt. | No. | Square. | Cube. | Sq. Rt. | Cu. Rt. |
| 101 | 10201 | 1030301 | 10.0499 | 4.6570 | 151 | 22801 | 3442951 | 12.2882 | 5.3251 |
| 102 | 10404 | 1061208 | 10.0995 | 4.6723 | 152 | 23104 | 3511808 | 12.3288 | 5.3368 |
| 103 | 10609 | 1092727 | 10.1489 | 4.6875 | 153 | 23409 | 3581577 | 12.3693 | 5.3485 |
| 104 | 10816 | 1124864 | 10.1980 | 4.7027 | 154 | 23716 | 3652264 | 12.4097 | 5.3601 |
| | 11025 | 1157625 | 10.2470 | 4.7177 | 155 | 24025 | 3723875 | 12.4499 | 5.3717 |
| 105 | 11023 | 113/023 | 10.24/0 | 4.1.11 | | 24023 | 3123013 | 12.4499 | |
| 106 | 11236 | 1191016 | 10.2956 | 4.7326 | 156 | 24336 | 3796416 | 12.4900 | 5.3832 |
| 107 | 11449 | 1225043 | 10.3441 | 4.7475 | 157 | 24649 | 3869893 | 12.5300 | 5.3947 |
| 108 | 11664 | 1259712 | 10.3923 | 4.7622 | 158 | 24964 | 3944312 | 12.5698 | 5.4061 |
| 100 | 11881 | 1295029 | 10.4403 | 4.7769 | 159 | 25281 | 4019679 | 12.6095 | 5.4175 |
| | 12100 | 1331000 | 10.4881 | 4.7914 | 160 | 25600 | 4096000 | 12.6491 | 5.4288 |
| 110 | 12100 | 1331000 | 10.4001 | 4.1914 | 100 | 23000 | 4090000 | 12.0491 | 3.4200 |
| 111 | 12321 | 1367631 | 10.5357 | 4.8059 | 161 | 25921 | 4173281 | 12.6886 | 5.4401 |
| 112 | 12544 | 1404928 | 10.5830 | 4.8203 | 162 | 26244 | 4251528 | 12.7279 | 5.4514 |
| 113 | 12769 | 1442897 | 10.6301 | 4.8346 | 163 | 26569 | 4330747 | 12.7671 | 5.4626 |
| 0 | 12996 | 1481544 | 10.6771 | 4.8488 | 164 | 26896 | 4410944 | 12.8062 | 5.4737 |
| 114 | | | | 4.8629 | 165 | 27225 | | 12.8452 | |
| 115 | 13225 | 1520875 | 10.7238 | 4.0029 | 105 | 2/225 | 4492125 | 12.0452 | 5.4848 |
| 116 | 13456 | 1 560896 | 10.7703 | 4.8770 | 166 | 27556 | 4574296 | 12.8841 | 5.4959 |
| 117 | 13689 | 1601613 | 10.8167 | 4.8910 | 167 | 27889 | 4657463 | 12.9228 | 5.5069 |
| 118 | 13924 | 1643032 | 10.8628 | 4.9049 | 168 | 28224 | 4741632 | 12.9615 | 5.5178 |
| | | | 10.9087 | | 169 | 28561 | 4826809 | 13. | 5.5288 |
| 119 | 14161 | 1685159 | | 4.9187 | | | | | |
| 120 | I4400 | 1728000 | 10.9545 | 4.9324 | 170 | 28900 | 4913000 | 13.0384 | 5.5397 |
| 121 | 14641 | 1771561 | II. | 4.9461 | 171 | 29241 | 5000211 | 13.0767 | 5.5505 |
| 122 | 14884 | 1815848 | 11.0454 | 4.9597 | 172 | 29584 | 5088448 | 13.1149 | 5.5613 |
| | | 1860867 | 11.0905 | 4.9732 | 173 | 29929 | 5177717 | 13.1529 | 5.5721 |
| 123 | 15129 | | | | | | | | |
| 124 | 15376 | 1906624 | 11.1355 | 4.9866 | 174 | 30276 | 5268024 | 13.1909 | 5.5828 |
| 125 | 15625 | 1953125 | 11.1803 | 5. | 175 | 30625 | 5359375 | 13.2288 | 5.5934 |
| 126 | 15876 | 2000376 | 11.2250 | 5.0133 | 176 | 30976 | 5451776 | 13.2665 | 5.6041 |
| 127 | 16129 | 2048383 | 11.2694 | 5.0265 | 177 | 31329 | 5545233 | 13.3041 | 5.6147 |
| 128 | 16384 | 2040303 | | | 178 | 31684 | | | 5.6252 |
| - | | | 11.3137 | 5.0397 | | | 5639752 | 13.3417 | |
| 129 | 16641 | 2146689 | 11.3578 | 5.0528 | 179 | 32041 | 5735339 | 13.3791 | 5.6357 |
| 130 | 16900 | 2197000 | 11.4018 | 5.0658 | 180 | 32400 | 5832000 | 13.4164 | 5.6462 |
| 131 | 17161 | 2248091 | 11.4455 | 5.0788 | 181 | 32761 | 5929741 | 13.4536 | 5.6567 |
| 132 | 17424 | 2299968 | 11.4891 | 5.0916 | 182 | 33124 | 6028568 | 13.4907 | 5.6671 |
| | 17689 | 2352637 | 11.5326 | 5.1045 | 183 | 33489 | 6128487 | 13.5277 | 5.6774 |
| 133 | | 2352037 2406104 | | | 184 | | 6229504 | 13.5647 | 5.6877 |
| 134 | 17956 | | 11.5758 | 5.1172 | | 33856 | | | |
| 135 | 18225 | 2460375 | 11.6190 | 5.1299 | 185 | 34225 | 6331625 | 13.6015 | 5.6980 |
| 136 | 18496 | 2515456 | 11.6619 | 5.1426 | 186 | 34596 | 6434856 | 13.6382 | 5.7083 |
| 137 | 18769 | 2571353 | 11.7047 | 5.1551 | 187 | 34969 | 6539203 | 13.6748 | 5.7185 |
| 138 | 19044 | 2628072 | 11.7473 | 5. 1676 | 188 | 35344 | 6644672 | 13.7113 | 5.7287 |
| | | 2685619 | 11.7898 | 5.1801 | 189 | | 6751269 | 13.7477 | 5.7388 |
| 139 | 19321 | | | | - | 35721 | | | |
| 140 | 19600 | 2744000 | 11.8322 | 5.1925 | 190 | 36100 | 6859000 | 13.7840 | 5.7489 |
| 141 | 19881 | 2803221 | 11.8743 | 5.2048 | 191 | 36481 | 6967871 | 13.8203 | 5.7590 |
| 142 | 20164 | 2863288 | 11.9164 | 5.2171 | 192 | 36864 | 7077888 | 13.8564 | 5.7690 |
| 143 | 20449 | 2924207 | 11.9583 | 5.2293 | 193 | 37249 | 7189057 | 13.8924 | 5.7790 |
| | 20736 | 2985984 | 12. | 5.2415 | 193 | 37636 | 7301384 | 13.9284 | 5.7890 |
| 144 | | | | | | | | | 5.7989 |
| 145 | 21025 | 3048625 | 12.0416 | 5.2536 | 195 | 38025 | 7414875 | 13.9642 | 1. |
| 146 | 21316 | 3112136 | 12.0830 | 5.2656 | 196 | 38416 | 7529536 | I4. | 5.8088 |
| 147 | 21609 | 3176523 | 12.1244 | 5.2776 | 197 | 38809 | 7645373 | 14.0357 | 5.8186 |
| 148 | 21904 | 3241792 | 12.1655 | 5.2896 | 198 | 39204 | 7762392 | 14.0712 | 5.8285 |
| | 22201 | | 12.2066 | 5.3015 | 190 | 39601 | 7880599 | 14.1067 | 5.8383 |
| J49 | | 3307949 | | | | 0. | 8000000 | 14.1007 | 5.8480 |
| 150 | 22500 | 3375000 | 12.2474 | 5.3133 | 200 | 40000 | 000000 | 14.1421 | 3.0400 |
| | | 1 | | [] | 1 | | | 1 | |

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Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to 1000-continued.

| - | | | | | | | | | |
|-------|---------|-----------|----------|---------|-----|---------|------------|---------|---------|
| No. | Square. | Cube. | Sq. Rt. | Cu. Rt. | No. | Square. | Cube. | Sq. Rt. | Cu. Rt. |
| 201 | 40401 | 8120601 | 14.1774 | 5.8578 | 251 | 63001 | 15813251 | 15.8430 | 6.3080 |
| 202 | 40804 | 8242408 | 14.2127 | 5.8675 | 252 | 63504 | 16003008 | 15.8745 | 6.3164 |
| 203 | 41209 | 8365427 | 14.2478 | 5.8771 | 253 | 64009 | 16194277 | 15.9060 | 6.3247 |
| 204 | 41616 | 8489664 | 14.2829 | 5.8868 | 254 | 64516 | 16387064 | 15.9374 | 6.3330 |
| 205 | 42025 | 8615125 | 14.3178 | 5.8964 | 255 | 65025 | 16581375 | 15.9687 | 6.3413 |
| 10000 | | | | | | | | | |
| 206 | 42436 | 8741816 | 14.3527 | 5.9059 | 256 | 65536 | 16777216 | 16. | 6.3496 |
| 207 | 42849 | 8869743 | 14.3875 | 5.9155 | 257 | 66049 | 16974593 | 16.0312 | 6.3579 |
| 208 | 43264 | 8998912 | 14.4222 | 5.9250 | 258 | 66564 | . 17173512 | 16.0624 | 6.3661 |
| 209 | 43681 | 9129329 | 14.4568 | 5.9345 | 259 | 67081 | 17373979 | 16.0935 | 6.3743 |
| 210 | 44100 | 9261000 | 14.4914 | 5.9439 | 260 | 67600 | 17576000 | 16.1245 | 6.3825 |
| 211 | 44521 | 9393931 | 14. 5258 | 5.9533 | 261 | 68121 | THEROTES | -6 | |
| 212 | | 9528128 | 14.5602 | 5.9627 | 262 | 68644 | 17779581 | 16.1555 | 6.3907 |
| | 44944 | | | | 263 | 69169 | 17984728 | 16.1864 | 6.3988 |
| 213 | 45369 | 9663597 | 14.5945 | 5.9721 | | | 18191447 | 16.2173 | 6.4070 |
| 214 | 45796 | 9800344 | 14.6287 | 5.9814 | 264 | 69696 | 18399744 | 16.2481 | 6.4151 |
| 215 | 46225 | 9938375 | 14.6629 | 5.9907 | 265 | 70225 | 18609625 | 16.2788 | 6.4232 |
| 216 | 46656 | 10077696 | 14.6969 | 6. | 266 | 70756 | 18821096 | 16.3095 | 6.4312 |
| 217 | 47089 | 10218313 | 14.7309 | 6.0092 | 267 | 71289 | 19034163 | 16.3401 | 6.4393 |
| 218 | 47524 | 10360232 | 14.7648 | 6.0185 | 268 | 71824 | 19248832 | 16.3707 | 6.4473 |
| 219 | 47961 | 10503459 | 14.7986 | 6.0277 | 269 | 72361 | 19465109 | 16.4012 | 6.4553 |
| 220 | 48400 | 10648000 | 14.8324 | 6.0368 | 270 | 72900 | 19683000 | 16.4317 | 6.4633 |
| | | | | | | 12900 | 19003000 | | 0.4033 |
| 221 | 48841 | 10793861 | 14.8661 | 6.0459 | 271 | 73441 | 19902511 | 16.4621 | 6.4713 |
| 222 | 49284 | 10941048 | 14.8997 | 6.0550 | 272 | 73984 | 20123648 | 16.4924 | 6.4792 |
| 223 | 49729 | 11089567 | 14.9332 | 6.0641 | 273 | 74529 | 20346417 | 16.5227 | 6.4872 |
| 224 | 50176 | 11239424 | 14.9666 | 6.0732 | 274 | 75076 | 20570824 | 16.5529 | 6.4951 |
| 225 | 50625 | 11390625 | 15. | 6.0822 | 275 | 75625 | 20796875 | 16.5831 | 6.5030 |
| 226 | 0 0 | | | 6 0010 | 276 | 76176 | | | |
| | 51076 | 11543176 | 15.0333 | 6.0912 | | | 21024576 | 16.6132 | 6.5108 |
| 227 | 51529 | 11697083 | 15.0665 | 6.1002 | 277 | 76729 | 21253933 | 16.6433 | 6.5187 |
| 228 | 51984 | 11852352 | 15.0997 | 6.1091 | 278 | 77284 | 21484952 | 16.6733 | 6.5265 |
| 229 | 5244I | 12008989 | 15.1327 | 6.1180 | 279 | 77841 | 21717639 | 16.7033 | 6.5343 |
| 230 | 52900 | 12167000 | 15.1658 | 6.1269 | 280 | 78400 | 21952000 | 16.7332 | 6.5421 |
| 231 | 53361 | 12326391 | 15.1987 | 6.1358 | 281 | 78961 | 22188041 | 16.7631 | 6.5499 |
| 232 | 53824 | 12487168 | 15.2315 | 6.1446 | 282 | 79524 | 22425768 | 16.7929 | 6.5577 |
| 233 | 54289 | 12649337 | 15.2643 | 6.1534 | 283 | 80089 | 22665187 | 16.8226 | 6.5654 |
| | 547.56 | 12812904 | 15.2971 | 6. 1622 | 284 | 80656 | 22906304 | 16.8523 | 6.5731 |
| 234 | | 12977875 | 15.3297 | 6.1710 | 285 | 81225 | 23149125 | 16.8819 | 6.5808 |
| 235 | 55225 | 129/10/5 | 13.3291 | 0.1/10 | | | 23149123 | 10.0019 | ~ |
| 236 | 55696 | 13144256 | 15.3623 | 6.1797 | 286 | 81796 | 23393656 | 16.9115 | 6.5885 |
| 237 | 56169 | 13312053 | 15.3948 | 6.1885 | 287 | 82369 | 23639903 | 16.9411 | 6.5962 |
| 238 | 56644 | 13481272 | 15.4272 | 6.1972 | 288 | 82944 | 23887872 | 16.9706 | 6.6039 |
| 239 | 57121 | 13651919 | 15.4596 | 6.2058 | 289 | 83521 | 24137569 | 17. | 6.6115 |
| 240 | 57600 | 13824000 | 15.4919 | 6.2145 | 290 | 84100 | 24389000 | 17.0294 | 6.6191 |
| 241 | | TACONTAL | 15 5010 | 6.2231 | 291 | 84681 | 24642171 | 17.0587 | 6.6267 |
| | 58081 | 13997521 | 15.5242 | | | | | | |
| 242 | 58564 | 14172488 | 15.5563 | 6.2317 | 292 | 85264 | 24897088 | 17.0880 | 6.6343 |
| 243 | 59049 | 14348907 | 15.5885 | 6.2403 | 293 | 85849 | 25153757 | 17.1172 | 6.6419 |
| 244 | 59536 | 14526784 | 15.6205 | 6.2488 | 294 | 86436 | 25412184 | 17.1464 | 6.6494 |
| 245 | 60025 | 14706125 | 15.6525 | 6.2573 | 295 | 87025 | 25672375 | 17.1756 | 6.6569 |
| 246 | 60516 | 14886936 | 15.6844 | 6.2658 | 296 | 87616 | 25934336 | 17.2047 | 6.6644 |
| 247 | 61009 | 1 5069223 | 15.7162 | 6.2743 | 297 | 88209 | 26198073 | 17.2337 | 6.6719 |
| 248 | 61504 | 15252992 | 15.7480 | 6.2828 | 298 | 88804 | 26463592 | 17.2627 | 6.6794 |
| 249 | 62001 | 15438249 | 15.7797 | 6.2912 | 299 | 89401 | 26730899 | 17.2916 | 6.6869 |
| 250 | 62500 | 15625000 | 15.8114 | 6.2996 | 300 | 90000 | 27000000 | 17.3205 | 6.6943 |
| -30 | 02300 | - 30-3000 | 5 | | 5 | | | | 5.5 |
| | | | | | | | | | |

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to 1000-continued.

| _ | | | | | | | | | |
|-----|---------|-----------|---------|---------|-------|---------|------------|---------|---------|
| No. | Square. | Cube. | Sq. Rt. | Cu. Rt. | No. | Square. | Cube. | Sq. Rt. | Cu. Rt. |
| 301 | 90601 | 27270901 | 17.3494 | 6.7018 | 351 | 123201 | 43243551 | 18.7350 | 7.0540 |
| 302 | 91204 | 27543608 | 17.3781 | 6.7092 | 352 | 123904 | 43614208 | 18.7617 | 7.0607 |
| 303 | 91809 | 27818127 | 17.4069 | 6.7166 | 353 | 124609 | 43986977 | 18.7883 | 7.0674 |
| 304 | 92416 | 28094464 | 17.4356 | 6.7240 | 354 | 125316 | 44361864 | 18.8149 | 7.0740 |
| 305 | 93025 | 28372625 | 17.4642 | 6.7313 | 355 | 126025 | 44738875 | 18.8414 | 7.0807 |
| - | | | | | | - | | | |
| 306 | 93636 | 28652616 | 17.4929 | 6.7387 | 356 | 126736 | 45118016 | 18.8680 | 7.0873 |
| 307 | 94249 | 28934443 | 17.5214 | 6.7460 | 357 | 127449 | 45499293 | 18.8944 | 7.0940 |
| 308 | 94864 | 29218112 | 17.5499 | 6.7533 | 358 | 128164 | 45882712 | 18.9209 | 7.1006 |
| 309 | 95481 | 29503629 | 17.5784 | 6.7606 | 359 | 128881 | 46268279 | 18.9473 | 7.1072 |
| | | 29791000 | 17.6068 | 6.7679 | 360 | 129600 | 46656000 | 18.9737 | 7.1138 |
| 310 | 96100 | 29/91000 | 17.0000 | 0.7079 | 300 | 129000 | 40030000 | 10.9/3/ | 1.1130 |
| 311 | 96721 | 30080231 | 17.6352 | 6.7752 | 361 | 130321 | 47045881 | 19. | 7.1204 |
| 312 | 97344 | 30371328 | 17.6635 | 6.7824 | 362 | 131044 | 47437928 | 19.0263 | 7.1269 |
| | | 30664297 | 17.6918 | 6.7897 | 363 | 131769 | 47832147 | 19.0526 | |
| 313 | 97969 | | | | | | | | 7.1335 |
| 314 | 98596 | 30959144 | 17.7200 | 6.7969 | 364 | 132496 | 48228544 | 19.0788 | 7.1400 |
| 315 | 99225 | 31255875 | 17.7482 | 6.8041 | 365 | 133225 | 48627125 | 19.1050 | 7.1466 |
| 316 | 99856 | 31554496 | 17.7764 | 6.8113 | 366 | 133956 | 49027896 | 19.1311 | 7.1531 |
| | | | 17.8045 | 6.8185 | 367 | 133950 | 49430863 | | |
| 317 | 100489 | 31855013 | | | | 134009 | | 19.1572 | 7.1596 |
| 318 | 101124 | 32157432 | 17.8326 | 6.8256 | 368 | 135424 | 49836032 | 19.1833 | 7.1661 |
| 319 | 101761 | 32461759 | 17.8606 | 6.8328 | 369 | 136161 | 50243409 | 19.2094 | 7.1726 |
| 320 | 102400 | 32768000 | 17.8885 | 6.8399 | 370 | 136900 | 50653000 | 19.2354 | 7.1791 |
| 321 | 100041 | 00076161 | 18 016 | 6.8470 | 371 | 100611 | F1064811 | 19.2614 | H .Q |
| | 103041 | 33076161 | 17.9165 | 0.04/0 | | 137641 | 51064811 | 1 | 7.1855 |
| 322 | 103684 | 33386248 | 17.9444 | 6.8541 | 372 | 138384 | 51478848 | 19.2873 | 7.1920 |
| 323 | 104329 | 33698267 | 17.9722 | 6.8612 | 373 | 139129 | 51895117 | 19.3132 | 7.1984 |
| 324 | 104976 | 34012224 | 18. | 6.8683 | 374 | 139876 | 52313624 | 19.3391 | 7.2048 |
| 325 | 105625 | 34328125 | 18.0278 | 6.8753 | 375 | 140625 | 52734375 | 19.3649 | 7.2112 |
| | 5 0 | | | | | | | | - 10.0 |
| 326 | 106276 | 34645976 | 18.0555 | 6.8824 | 376 | 141376 | 531 57 376 | 19.3907 | 7.2177 |
| 327 | 106929 | 34965783 | 18.0831 | 6.8894 | - 377 | 142129 | 53582633 | 19.4165 | 7.2240 |
| 328 | 107584 | 35287552 | 18.1108 | 6.8964 | 378 | 142884 | 54010152 | 19.4422 | 7.2304 |
| 329 | 108241 | 35611289 | 18.1384 | 6.9034 | 379 | 143641 | 54439939 | 19.4679 | 7.2368 |
| 330 | 108900 | 35937000 | 18.1659 | 6.9104 | 380 | 144400 | 54872000 | 19.4936 | 7.2432 |
| | | | | | | | | | |
| 331 | 109561 | 36264691 | 18.1934 | 6.9174 | 381 | 145161 | 55306341 | 19.5192 | 7.2495 |
| 332 | 110224 | 36594368 | 18.2209 | 6.9244 | 382 | 145924 | 55742968 | 19.5448 | 7.2558 |
| 333 | 110889 | 36926037 | 18.2483 | 6.9313 | 383 | 146689 | 56181887 | 19.5704 | 7.2622 |
| 334 | 111556 | 37259704 | 18.2757 | 6.9382 | 384 | 147456 | 56623104 | 19.5959 | 7.2685 |
| 335 | 112225 | 37595375 | 18.3030 | 6.9451 | 385 | 148225 | 57066625 | 19.6214 | 7.2748 |
| | | | | | | | | | |
| 336 | 112896 | 37933056 | 18.3303 | 6.9521 | 386 | 148996 | 57512456 | 19.6469 | 7.2811 |
| 337 | 113569 | 38272753 | 18.3576 | 6.9589 | 387 | 149769 | 57960603 | 19.6723 | 7.2874 |
| 338 | 114244 | 38614472 | 18.3848 | 6.9658 | 388 | 150544 | 58411072 | 19.6977 | 7.2936 |
| 339 | 114921 | 38958219 | 18.4120 | 6.9727 | 389. | 151321 | 58863869 | 19.7231 | 7.2999 |
| 340 | 115600 | 39304000 | 18.4391 | 6.9795 | 390 | 152100 | 59319000 | 19.7484 | 7.3061 |
| - | | 39304000 | | | | 132100 | 39319000 | 19.7404 | 7.3001 |
| 341 | 116281 | 39651821 | 18.4662 | 6.9864 | 391 | 152881 | 59776471 | 19.7737 | 7.3124 |
| 342 | 116964 | 40001688 | 18.4932 | 6.9932 | 392 | 153664 | 60236288 | 19.7990 | 7.3186 |
| 343 | 117649 | 40353607 | 18.5203 | 7. | 393 | 154449 | 60698457 | 19.8242 | 7.3248 |
| 344 | 118336 | 40707 584 | 18.5472 | 7.0068 | 394 | 155236 | 61162984 | 19.8494 | 7.3310 |
| | 119025 | 41063625 | 18.5742 | 7.0136 | | 156025 | 61629875 | 19.8746 | 7.3372 |
| 345 | | | | | 395 | | | | 1.3314 |
| 346 | 119716 | 41421736 | 18.6011 | 7.0203 | 396 | 156816 | 62099136 | 19.8997 | 7.3434 |
| 347 | 120409 | 41781923 | 18.6279 | 7.0271 | 397 | 157609 | 62570773 | 19.9249 | 7.3496 |
| 348 | 121104 | 42144192 | 18.6548 | 7.0338 | 398 | 158404 | 63044792 | 19.9499 | 7.3558 |
| 349 | 121801 | 42508549 | 18.6815 | 7.0406 | 399 | 159201 | 63521199 | 19.9750 | 7.3619 |
| 350 | 122500 | 42875000 | 18.7083 | 7.0473 | 400 | 160000 | 64000000 | 20. | 7.3681 |
| 555 | | 4.07 5000 | 10.7003 | 1.0413 | 400 | | | | 1.3001 |
| | | | | | | | | | |

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Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to 1000—continued.

| | | | | | | | | | - |
|-----|---------|-----------|---------|---------|-------|---------|-----------|---------|---------|
| No. | Square. | Cube. | Sq. Rt. | Cu. Rt. | No. | Square. | Cube. | Sq. Rt. | Cu. Rt. |
| 401 | 160801 | 64481201 | 20.0250 | 7.3742 | 451 | 203401 | 91733851 | 21.2368 | 7.6688 |
| 402 | 161604 | 64964808 | 20.0499 | 7.3803 | 452 | 204304 | 92345408 | 21.2603 | 7.6744 |
| 403 | 162409 | 65450827 | 20.0749 | 7.3864 | - 453 | 205209 | 92959677 | 21.2838 | 7.6801 |
| 404 | 163216 | 65939264 | 20.0998 | 7.3925 | | 206116 | 93576664 | | |
| | | | | | 454 | | | 21.3073 | 7.6857 |
| 405 | 164025 | 66430125 | 20.1246 | 7.3986 | 455 | 207025 | 94196375 | 21.3307 | 7.6914 |
| 406 | 164836 | 66923416 | 20.1494 | 7.4047 | 456 | 207936 | 94818816 | 21.3542 | 7.6970 |
| 407 | 165649 | 67419143 | 20.1742 | 7.4108 | 457 | 208849 | 95443993 | 21.3776 | 7.7026 |
| 408 | 166464 | 67917312 | 20.1990 | 7.4169 | 458 | 209764 | 96071912 | 21.4009 | 7.7082 |
| 409 | 167281 | 68417929 | 20.2237 | 7.4229 | | 210681 | | | |
| | 168100 | 68921000 | | | 459 | 211600 | 96702579 | 21.4243 | 7.7138 |
| 410 | 100100 | 00921000 | 20.2485 | 7.4290 | 460 | 211000 | 97336000 | 21.4476 | 7.7194 |
| 411 | 168921 | 69426531 | 20.2731 | 7.4350 | 461 | 212521 | 97972181 | 21.4709 | 7.7250 |
| 412 | 169744 | 69934528 | 20.2978 | 7.4410 | 462 | 213444 | 98611128 | 21.4942 | 7.7306 |
| 413 | 170569 | 70444997 | 20.3224 | 7.4470 | 463 | 214369 | 99252847 | 21.5174 | 7.7362 |
| 414 | 171396 | 70957944 | 20.3470 | 7.4530 | 464 | 215296 | 99897344 | 21.5407 | |
| 415 | 172225 | | | | 465 | 216225 | | | 7.7418 |
| | 1/2223 | 71473375 | 20.3715 | 7.4590 | | 210225 | 100544625 | 21.5639 | 7.7473 |
| 416 | 173056 | 71991296 | 20.3961 | 7.4650 | 466 | 217156 | 101194696 | 21.5870 | 7.7529 |
| 417 | 173889 | 72511713 | 20.4206 | 7.4710 | 467 | 218089 | 101847563 | 21.6102 | 7.7584 |
| 418 | 174724 | 73034632 | 20.4450 | 7.4770 | 468 | 219024 | 102503232 | 21.6333 | 7.7639 |
| 419 | 175561 | 73560059 | 20.4695 | 7.4829 | 469 | 219961 | 103161709 | 21.6564 | 7.7695 |
| 420 | 176400 | 74088000 | 20.4939 | 7.4889 | 470 | 220900 | 103823000 | 21.6795 | |
| 1 | 170400 | 7400000 | 20.4939 | 7.4009 | | 220900 | 103023000 | 21.0795 | 7.7750 |
| 421 | 177241 | 74618461 | 20.5183 | 7.4948 | 471 | 221841 | 104487111 | 21.7025 | 7.7805 |
| 422 | 178084 | 75151448 | 20.5426 | 7.5007 | 472 | 222784 | 105154048 | 21.7256 | 7.7860 |
| 423 | 178929 | 7 5686967 | 20.5670 | 7.5067 | 473 | 223729 | 105823817 | 21.7486 | 7.7915 |
| 424 | 179776 | 76225024 | 20.5913 | 7.5126 | 474 | 224676 | 106496424 | 21.7715 | 7.7970 |
| 425 | 180625 | 76765625 | 20.6155 | 7.5185 | 475 | 225625 | 107171875 | 21.7945 | 7.8025 |
| - | | | | | - | | | | |
| 426 | 181476 | 77308776 | 20.6398 | 7.5244 | 476 | 226576 | 107850176 | 21.8174 | 7.8079 |
| 427 | 182329 | 77854483 | 20.6640 | 7.5302 | 477 | 227529 | 108531333 | 21.8403 | 7.8134 |
| 428 | 183184 | 78402752 | 20.6882 | 7.5361 | 478 | 228484 | 109215352 | 21.8632 | 7.8188 |
| 429 | 184041 | 78953589 | 20.7123 | 7.5420 | 479 | 229441 | 109902239 | 21.8861 | 7.8243 |
| 430 | 184900 | 79507000 | 20.7364 | 7.5478 | 480 | 230400 | 110592000 | 21.9089 | 7.8297 |
| | | | | | | | | | |
| 431 | 185761 | 80062991 | 20.7605 | 7.5537 | 481 | 231361 | 111284641 | 21.9317 | 7.8352 |
| 432 | 186624 | 80621568 | 20.7846 | 7.5595 | 482 | 232324 | 111980168 | 21.9545 | 7.8406 |
| 433 | 187489 | 81182737 | 20.8087 | 7.5654 | 483 | 233289 | 112678587 | 21.9773 | 7.8460 |
| 434 | 188356 | 81746504 | 20.8327 | 7.5712 | 484 | 234256 | 113379904 | 22. | 7.8514 |
| 435 | 189225 | 82312875 | 20.8567 | 7.5770 | 485 | 235225 | 114084125 | 22.0227 | 7.8568 |
| | | | | | | | | | |
| 436 | 190096 | 82881856 | 20.8806 | 7.5828 | 486 | 236196 | 114791256 | 22.0454 | 7.8622 |
| 437 | 190969 | 83453453 | 20.9045 | 7.5886 | 487 | 237169 | 115501303 | 22.0681 | 7.8676 |
| 438 | 191844 | 84027672 | 20.9284 | 7.5944 | 488 | 238144 | 116214272 | 22.0907 | 7.8730 |
| 439 | 192721 | 84604519 | 20.9523 | 7.6001 | 489 | 239121 | 116930169 | 22.1133 | 7.8784 |
| 440 | 193600 | 85184000 | 20.9762 | 7.6059 | 490 | 240100 | 117649000 | 22.1359 | 7.8837 |
| 441 | 701.97 | 9==66+0+ | | - 6+++ | 491 | 180110 | 118220221 | 22.1585 | 7.8891 |
| | 194481 | 85766121 | 21. | 7.6117 | | 241081 | 118370771 | 22.1505 | |
| 442 | 195364 | 86350888 | 21.0238 | 7.6174 | 492 | 242064 | 119095488 | | 7.8944 |
| 443 | 196249 | 86938307 | 21.0476 | 7.6232 | 493 | 243049 | 119823157 | 22.2036 | 7.8998 |
| 444 | 197136 | 87528384 | 21.0713 | 7.6289 | 494 | 244036 | 120553784 | 22.2261 | 7.9051 |
| 445 | 198025 | 88121125 | 21.0950 | 7.6346 | 495 | 245025 | 121287375 | 22.2486 | 7.9105 |
| 446 | 198916 | 88716536 | 21.1187 | 7.6403 | 496 | 246016 | 122023936 | 22.2711 | 7.9158 |
| | | 89314623 | 21.110/ | 7.6460 | 497 | 247009 | 122763473 | 22.2935 | 7.9211 |
| 447 | 199809 | | | | | 24/009 | 123505992 | 22.3159 | 7.9264 |
| 448 | 200704 | 89915392 | 21.1660 | 7.6517 | 498 | | 00 000 | | |
| 449 | 201601 | 90518849 | 21.1896 | 7.6574 | 499 | 24900I | 124251499 | 22.3383 | 7.9317 |
| 450 | 202500 | 91125000 | 21.2132 | 7.6631 | 500 | 250000 | 125000000 | 22.3607 | 7.9370 |
| | | | | | 1 | | | | |

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to 1000-continued.

| | | | | | | | | 1.1.1.1.5 | |
|-----|---------|-----------|---------|---------|-----|------------|-----------|-----------|---------|
| No. | Square. | Cube. | Sq. Rt. | Cu. Rt. | No. | Square. | Cube. | Sq. Rt. | Cu. Rt. |
| 501 | 251001 | 125751501 | 22.3830 | 7.9423 | 551 | 303601 | 167284151 | 23.4734 | 8.1982 |
| 502 | 252004 | 126506008 | 22.4054 | 7.9476 | 552 | 304704 | 168196608 | 23.4947 | 8.2031 |
| 503 | 253009 | 127263527 | 22.4277 | 7.9528 | 553 | 305809 | 169112377 | 23.5160 | 8.2081 |
| 504 | 254016 | 128024064 | 22.4499 | 7.9581 | 554 | 306916 | 170031464 | 23.5372 | 8.2130 |
| 505 | 255025 | 128787625 | 22.4722 | 7.9634 | 555 | 308025 | 170953875 | | 8.2180 |
| | 233023 | 120/0/023 | 22.4/22 | | | 300023 | 110953015 | 23.5584 | 0.2100 |
| 506 | 256036 | 129554216 | 22.4944 | 7.9686 | 556 | 309136 | 171879616 | 23.5797 | 8.2229 |
| 507 | 257049 | 130323843 | 22.5167 | 7.9739 | 557 | 310249 | 172808693 | 23.6008 | 8.2278 |
| 508 | 258064 | 131096512 | 22.5389 | 7.9791 | 558 | 311364 | 173741112 | 23.6220 | 8.2327 |
| 509 | 259081 | 131872229 | 22.5610 | 7.9843 | 559 | 312481 | 174676879 | | |
| | 260100 | | 22.5832 | 7.9896 | | | | 23.6432 | 8.2377 |
| 510 | 200100 | 132651000 | 22.5032 | 7.9090 | 560 | 313600 | 175616000 | 23.6643 | 8.2426 |
| 511 | 261121 | 133432831 | 22.6053 | 7.9948 | 561 | 314721 | 176558481 | 23.6854 | 8.2475 |
| 512 | 262144 | 134217728 | 22.6274 | 8. | 562 | 315844 | 177504328 | 23.7065 | 8.2524 |
| 513 | 263169 | 135005697 | 22.6495 | 8.0052 | 563 | 316969 | 178453547 | 23.7276 | 8.2573 |
| | | | | | | | | | 0.23/3 |
| 514 | 264196 | 135796744 | 22.6716 | 8.0104 | 564 | 318096 | 179406144 | 23.7487 | 8.2621 |
| 515 | 265225 | 136590875 | 22.6936 | 8.0156 | 565 | 319225 | 180362125 | 23.7697 | 8.2670 |
| 516 | 266256 | 137388096 | 22.7156 | 8.0208 | 566 | 320356 | 181321496 | 23.7908 | 8.2719 |
| 517 | 267289 | 138188413 | 22.7376 | 8.0260 | 567 | 321489 | 182284263 | 23.8118 | 8.2768 |
| 518 | | 138991832 | | | 507 | | | | |
| | 268324 | | 22.7596 | 8.0311 | 568 | 322624 | 183250432 | 23.8328 | 8.2816 |
| 519 | 269361 | 139798359 | 22.7816 | 8.0363 | 569 | 323761 | 184220009 | 23.8537 | 8.2865 |
| 520 | 270400 | 140608000 | 22.8035 | 8.0415 | 570 | 324900 | 185193000 | 23.8747 | 8.2913 |
| 521 | 271441 | 141420761 | 22.8254 | 8.0466 | 571 | 326041 | 186169411 | 23.8956 | 8.2962 |
| | | | | | | | | | |
| 522 | 272484 | 142236648 | 22.8473 | 8.0517 | 572 | 327184 | 187149248 | 23.9165 | 8.3010 |
| 523 | 273529 | 143055667 | 22.8692 | 8.0569 | 573 | 328329 | 188132517 | 23.9374 | 8.3059 |
| 524 | 274576 | 143877824 | 22.8910 | 8.0620 | 574 | 329476 | 189119224 | 23.9583 | 8.3107 |
| 525 | 275625 | 144703125 | 22.9129 | 8.0671 | 575 | 330625 | 190109375 | 23.9792 | 8.3155 |
| 526 | 276676 | | | 8 | 576 | | | | |
| | | 145531576 | 22.9347 | 8.0723 | | 331776 | 191102976 | 24. | 8.3203 |
| 527 | 277729 | 146363183 | 22.9565 | 8.0774 | 577 | 332929 | 192100033 | 24.0208 | 8.3251 |
| 528 | 278784 | 147197952 | 22.9783 | 8.0825 | 578 | 334084 | 193100552 | 24.0416 | 8.3300 |
| 529 | 279841 | 148035889 | 23. | 8.0876 | 579 | 335241 | 194104539 | 24.0624 | 8.3348 |
| 530 | 280900 | 148877000 | 23.0217 | 8.0927 | 580 | 336400 | 195112000 | 24.0832 | 8.3396 |
| 531 | -9-06- | | | | - | | | | |
| | 281961 | 149721291 | 23.0434 | 8.0978 | 581 | 337561 | 196122941 | 24.1039 | 8.3443 |
| 532 | 283024 | 150568768 | 23 0651 | 8.1028 | 582 | 338724 | 197137368 | 24.1247 | 8.3491 |
| 533 | 284089 | 151419437 | 23.0868 | 8.1079 | 583 | 339889 | 198155287 | 24.1454 | 8.3539 |
| 534 | 285156 | 152273304 | 23.1084 | 8.1130 | 584 | 341056 | 199176704 | 24.1661 | 8.3587 |
| 535 | 286225 | 153130375 | 23.1301 | 8.1180 | 585 | 342225 | 200201625 | 24.1868 | 8.3634 |
| 536 | | | 00 | | | | | | 0 - 1 |
| | 287296 | 153990656 | 23.1517 | 8.1231 | 586 | 343396 | 201230056 | 24.2074 | 8.3682 |
| 537 | 288369 | 154854153 | 23.1733 | 8.1281 | 587 | 344569 | 202262003 | 24.2281 | 8.3730 |
| 538 | 289444 | 155720872 | 23.1948 | 8.1332 | 588 | 345744 | 203297472 | 24.2487 | 8.3777 |
| 539 | 290521 | 156590819 | 23.2164 | 8.1382 | 589 | 346921 | 204336469 | 24.2693 | 8.3825 |
| 540 | 291600 | 157464000 | 23.2379 | 8.1433 | 590 | 348100 | 205379000 | 24.2899 | 8.3872 |
| 541 | 000681 | TEQUIDIDE | | 0 0 . | 591 | a 10 a 9 a | | A. 0107 | 8 2010 |
| | 292681 | 158340421 | 23.2594 | 8.1483 | | 349281 | 206425071 | 24.3105 | 8.3919 |
| 542 | 293764 | 159220088 | 23.2809 | 8.1533 | 592 | 350464 | 207474688 | 24.3311 | 8.3967 |
| 543 | 294849 | 160103007 | 23.3024 | 8.1583 | 593 | 351649 | 208527857 | 24.3516 | 8.4014 |
| 544 | 295936 | 160989184 | 23.3238 | 8.1633 | 594 | 352836 | 209584584 | 24.3721 | 8.4061 |
| 545 | 297025 | 161878625 | 23.3452 | 8.1683 | 595 | 354025 | 210644875 | 24.3926 | 8.4108 |
| 546 | 298116 | 162771336 | 23.3666 | 8.1733 | 596 | 355216 | 211708736 | 24.4131 | 8.4155 |
| 547 | 299209 | 163667323 | 23.3880 | 8.1783 | 597 | 356409 | 212776173 | 24.4336 | 8.4202 |
| 548 | 300304 | 164566592 | 23.4094 | 8.1833 | 597 | | 213847192 | 24.4540 | 8.4249 |
| | | | 0.01 | 8.1882 | | 357604 | | | 8.4296 |
| 549 | 301401 | 165469149 | 23.4307 | | 599 | 358801 | 214921799 | 24.4745 | |
| 550 | 302500 | 166375000 | 23.4521 | 8.1932 | 600 | 360000 | 216000000 | 24.4949 | 8.4343 |
| | | | | | 1 | | | | |

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7

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to 1000—continued.

| 125 | 1 | | | | | | | | |
|---------------------------------|--|---|---|--|---------------------------------|--|---|---|--|
| No. | Square. | Cube. | Sq. Rt. | Cu. Rt. | No. | Square. | Cube. | Sq. Rt. | Cu. Rt. |
| 601 | 361201 | 217081801 | 24.5153 | 8.4390 | 651 | 423801 | 275894451 | 25.5147 | 8.6668 |
| 602 | 362404 | 218167208 | 24.5357 | 8.4437 | 652 | 425104 | 277167808 | 25.5343 | 8.6713 |
| 603 | 363609 | 219256227 | 24.5561 | 8.4484 | 653 | 426409 | 278445077 | 25.5539 | 8.6757 |
| 604 | 364816 | 220348864 | 24.5764 | 8.4530 | 654 | 427716 | 279726264 | 25.5734 | 8.6801 |
| 605 | 366025 | 221445125 | 24.5967 | 8.4577 | 655 | 429025 | 281011375 | 25.5930 | 8.6845 |
| 606 | 367236 | 222545016 | 24.6171 | 8.4623 | 656 | 430336 | 282300416 | 25.6125 | 8.6890 |
| 607 | 368449 | 223648543 | 24.6374 | 8.4670 | 657 | 431649 | 283593393 | 25.6320 | 8.6934 |
| 608 | 369664 | 224755712 | 24.6577 | 8.4716 | 658 | 432964 | 284890312 | 25.6515 | 8.6978 |
| 609 | 370881 | 225866529 | 24.6779 | 8.4763 | 659 | 434281 | 286191179 | 25.6710 | 8.7022 |
| 610 | 372100 | 226981000 | 24.6982 | 8.4809 | 660 | 435600 | 287496000 | 25.6905 | 8.7066 |
| 611 | 373321 | 228099131 | 24.7184 | 8.4856 | 661 | 436921 | 288804781 | 25.7099 | 8.7110 |
| 612 | 374544 | 229220928 | 24.7386 | 8.4902 | 662 | 438244 | 290117528 | 25.7294 | 8.7154 |
| 613 | 375769 | 230346397 | 24.7588 | 8.4948 | 663 | 439569 | 291434247 | 25.7488 | 8.7198 |
| 614 | 376996 | 231475544 | 24.7590 | 8.4994 | 664 | 440896 | 292754944 | 25.7682 | 8.7241 |
| 615 | 378225 | 232608375 | 24.7992 | 8.5040 | 665 | 442225 | 294079625 | 25.7876 | 8.7285 |
| 616 | 379456 | 233744896 | 24.8193 | 8.5086 | 666 | 443556 | 295408296 | 25.8070 | 8.7329 |
| 617 | 380689 | 234885113 | 24.8395 | 8.5132 | 667 | 444889 | 296740963 | 25.8263 | 8.7373 |
| 618 | 381924 | 236029032 | 24.8596 | 8.5178 | 668 | 446224 | 298077632 | 25.8457 | 8.7416 |
| 619 | 383161 | 237176659 | 24.8797 | 8.5224 | 669 | 447561 | 299418309 | 25.8650 | 8.7460 |
| 620 | 384400 | 238328000 | 24.8998 | 8.5270 | 670 | 448900 | 300763000 | 25.8844 | 8.7503 |
| 621 622 623 624 625 | 385641 386884 388129 389376 390625 | 239483061 240641848 241804367 242970624 244140625 | 24.9199 24.9399 24.9600 24.9800 25. | 8.5316 8.5362 8.5408 8.5453 8.5453 8.5499 | 671 672 673 674 675 | 450241 451584 452929 454276 455625 | 302111711 303464448 304821217 306182024 307546875 | 25.9037 25.9230 25.9422 25.9615 25.9808 | 8.7547 8.7590 8.7634 8.7677 8.7721 |
| 626 | 391876 | 245314376 | 25.0200 | 8.5544 | 676 | 456976 | 308915776 | 26. | 8.7764 |
| 627 | 393129 | 246491883 | 25.0400 | 8.5590 | 677 | 458329 | 310288733 | 26.0192 | 8.7807 |
| 628 | 394384 | 247673152 | 25.0599 | 8.5635 | 678 | 459684 | 311665752 | 26.0384 | 8.7850 |
| 629 | 395641 | 248858189 | 25.0799 | 8.5681 | 679 | 461041 | 313046839 | 26.0576 | 8.7893 |
| 630 | 396900 | 250047000 | 25.0998 | 8.5726 | 680 | 462400 | 314432000 | 26.0768 | 8.7937 |
| 631 | 398161 | 251239591 | 25.1197 | 8.5772 | 681 | 463761 | 315821241 | 26.0960 | 8.7980 |
| 632 | 399424 | 252435968 | 25.1396 | 8.5817 | 682 | 465124 | 317214568 | 26.1151 | 8.8023 |
| 633 | 400689 | 253636137 | 25.1595 | 8.5862 | 683 | 466489 | 318611987 | 26.1343 | 8.8066 |
| 634 | 401956 | 254840104 | 25.1794 | 8.5907 | 684 | 467856 | 320013504 | 26.1534 | 8.8109 |
| 635 | 403225 | 256047875 | 25.1992 | 8.5952 | - 685 | 469225 | 321419125 | 26.1725 | 8.8152 |
| 636 | 404496 | 257259456 | 25.2190 | 8.5997 | 686 | 470596 | 322828856 | 26.1916 | 8.8194 |
| 637 | 405769 | 258474853 | 25.2389 | 8.6043 | 687 | 471969 | 324242703 | 26.2107 | 8.8237 |
| 638 | 407044 | 259694072 | 25.2587 | 8.6088 | 688 | 473344 | 325660672 | 26.2298 | 8.8280 |
| 639 | 408321 | 260917119 | 25.2784 | 8.6132 | 689 | 474721 | 327082769 | 26.2488 | 8.8323 |
| 640 | 409600 | 262144000 | 25.2982 | 8.6177 | 690 | 476100 | 328509000 | 26.2679 | 8.8326 |
| 641 | 410881 | 263374721 | 25.3180 | 8.6222 | 691 | 477481 | 329939371 | 26.2869 | 8.8408 |
| 642 | 412164 | 264609288 | 25.3377 | 8.6267 | 692 | 478864 | 331373888 | 26.3059 | 8.8451 |
| 643 | 413449 | 265847707 | 25.3574 | 8.6312 | 693 | 480249 | 332812557 | 26.3249 | 8.8493 |
| 644 | 414736 | 267089984 | 25.3772 | 8.6357 | 694 | 481636 | 334255384 | 26.3439 | 8.8536 |
| 645 | 416025 | 268336125 | 25.3969 | 8.6401 | 695 | 483025 | 335702375 | 26.3629 | 8.8578 |
| 646 | 417316 | 269586136 | 25.4165 | 8.6446 | 696 | 484416 | 337153536 | 26.3818 | 8.8621 |
| 647 | 418609 | 270840023 | 25.4362 | 8.6490 | 697 | 485809 | 338608873 | 26.4008 | 8.8663 |
| 648 | 419904 | 272097792 | 25.4558 | 8.6535 | 698 | 487204 | 340068392 | 26.4197 | 8.8706 |
| 649 | 421201 | 273359449 | 25.4755 | 8.6579 | 699 | 488601 | 341532099 | 26.4386 | 8.8748 |
| 650 | 422500 | 274625000 | 25.4951 | 8.6624 | 7 00 | 490000 | 343000000 | 26.4575 | 8.8790 |

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from 1 to 1000-continued.

| _ | | | | | 1.0.0 | | | | 114.31 |
|-----|---------|-----------|---------|---------|--------------------------------------|---------|-----------|---------|---------|
| No. | Square. | Cube. | Sq. Rt. | Cu. Rt. | No. | Square. | Cube. | Sq. Rt. | Cu. Rt. |
| 701 | 491401 | 344472101 | 26.4764 | 8.8833 | 751 | 564001 | 423564751 | 27.4044 | 9.0896 |
| 702 | 492804 | 345948408 | 26.4953 | 8.8875 | 752 | 565504 | 425259008 | 27.4226 | 9.0937 |
| 703 | 494209 | 347428927 | 26.5141 | 8.8917 | 753 | 567009 | 426957777 | 27.4408 | 9.0977 |
| 704 | 495616 | 348913664 | 26.5330 | 8.8959 | 754 | 568516 | 428661064 | 27.4591 | 9.1017 |
| | | 350402625 | 26.5518 | 8.9001 | | 0 0 | | | |
| 705 | 497025 | 330402023 | 20.3310 | 0.9001 | 755 | 570025 | 430368875 | 27.4773 | 9.1057 |
| 706 | 498436 | 351895816 | 26.5707 | 8.9043 | 756 | 571536 | 432081216 | 27.4955 | 9.1098 |
| 707 | 499849 | 353393243 | 26.5895 | 8.9085 | 757 | 573049 | 433798093 | 27.5136 | 9.1138 |
| | 501264 | | 26.6083 | 8.9127 | | | | | |
| 708 | | 354894912 | | | 758 | 574564 | 435519512 | 27.5318 | 9.1178 |
| 709 | 502681 | 356400829 | 26.6271 | 8.9169 | 759 | 576081 | 437245479 | 27.5500 | 9.1218 |
| 710 | 504100 | 357911000 | 26.6458 | 8.9211 | 760 | 577600 | 438976000 | 27.5681 | 9.1258 |
| 711 | FOFFOT | 250425427 | 26.6646 | 8.9253 | 761 | 579121 | 440711081 | 27.5862 | 9.1298 |
| | 505521 | 359425431 | | | | | | | |
| 712 | 506944 | 360944128 | 26.6833 | 8.9295 | 762 | 580644 | 442450728 | 27.6043 | 9.1338 |
| 713 | 508369 | 362467097 | 26.7021 | 8.9337 | 763 | 582169 | 444194947 | 27.6225 | 9.1378 |
| 714 | 509796 | 363994344 | 26.7208 | 8.9378 | 764 | 583696 | 445943744 | 27.6405 | 9.1418 |
| 715 | 511225 | 365525875 | 26.7395 | 8.9420 | 765 | 585225 | 447697125 | 27.6586 | 9.1458 |
| | | | | | | 000 | | | - 10 |
| 716 | 512656 | 367061696 | 26.7582 | 8.9462 | 766 | 586756 | 449455096 | 27.6767 | 9.1498 |
| 717 | 514089 | 368601813 | 26.7769 | 8.9503 | 767 | | 451217663 | 27.6948 | 9.1537 |
| 718 | 515524 | 370146232 | 26.7955 | 8.9545 | 768 | 589824 | 452984832 | 27.7128 | 9.1577 |
| 719 | 516961 | 371694959 | 26.8142 | 8.9587 | 769 | 591361 | 454756609 | 27.7308 | 9.1617 |
| 720 | 518400 | 373248000 | 26.8328 | 8.9628 | 770 | 592900 | 456533000 | 27.7489 | 9.1657 |
| - | | | | - | | 39-900 | | | |
| 721 | 519841 | 374805361 | 26.8514 | 8.9670 | 771 | 59444I | 458314011 | 27.7669 | 9.1696 |
| 722 | 521284 | 376367048 | 26.8701 | 8.9711 | 772 | 595984 | 460099648 | 27.7849 | 9.1736 |
| 723 | 522729 | 377933067 | 26.8887 | 8.9752 | 773 | 597529 | 461889917 | 27.8029 | 9.1775 |
| 724 | 524176 | 379503424 | 26.9072 | 8.9794 | 774 | 599076 | 463684824 | 27.8209 | 9.1815 |
| | 525625 | 381078125 | 26.9258 | 8.9835 | | 600625 | 465484375 | 27.8388 | 9.1855 |
| 725 | | | 20.9230 | | 775 | 000025 | | | - |
| 726 | 527076 | 382657176 | 26.9444 | 8.9876 | 776 | 602176 | 467288576 | 27.8568 | 9.1894 |
| 727 | 528529 | 384240583 | 26.9629 | 8.9918 | 777 | 603729 | 469097433 | 27.8747 | 9.1933 |
| 728 | 529984 | 385828352 | 26.9815 | 8.9959 | 778 | 605284 | 470910952 | 27.8927 | 9.1973 |
| 729 | 531441 | 387420489 | 27. | 9. | 779 | 606841 | 472729139 | 27.9106 | 9.2012 |
| | | | | - | 780 | | | | - |
| 730 | 532900 | 389017000 | 27.0185 | 9.0041 | 100 | 608400 | 474552000 | 27.9285 | 9.2052 |
| 731 | 534361 | 390617891 | 27.0370 | 9.0082 | 781 | 609961 | 476379541 | 27.9464 | 9.2091 |
| 732 | 535824 | 392223168 | 27.0555 | 9.0123 | 782 | 611524 | 478211768 | 27.9643 | 9.2130 |
| 733 | 537289 | 393832837 | 27.0740 | 9.0164 | 783 | 613089 | 480048687 | 27.9821 | 9.2170 |
| | 538756 | 395446904 | | | 784 | 614656 | 481890304 | 28. | 9.2209 |
| 734 | | | 27.0924 | 9.0205 | | | | | |
| 735 | 540225 | 397065375 | 37.1109 | 9.0246 | 785 | 616225 | 483736625 | 28.0179 | 9.2248 |
| 736 | 541696 | 398688256 | 27.1293 | 9.0287 | 786 | 617796 | 485587656 | 28.0357 | 9.2287 |
| 737 | 543169 | 400315553 | 27.1477 | 9.0328 | 787 | 619369 | 487443403 | 28.0535 | 9.2326 |
| 738 | 544644 | 401947272 | 27.1662 | 9.0369 | 788 | 620944 | 489303872 | 28.0713 | 9.2365 |
| | | | | | | | | 28.0891 | 9.2404 |
| 739 | 546121 | 403583419 | 27.1846 | 9.0410 | 789 | 622521 | 491169069 | | |
| 740 | 547600 | 405224000 | 27.2029 | 9.0450 | 790 | 624100 | 493039000 | 28.1069 | 9.2443 |
| 741 | 549081 | 406869021 | 27.2213 | 9.0491 | 791 | 625681 | 494913671 | 28.1247 | 9.2482 |
| 742 | 550564 | 408518488 | 27.2397 | 9.0532 | 792 | 627264 | 496793088 | 28.1425 | 9.2521 |
| 743 | 552049 | 410172407 | 27.2580 | 9.0572 | 793 | 628849 | 498677257 | 28.1603 | 9.2560 |
| 744 | 553536 | 411830784 | 27.2764 | 9.0613 | 794 | 630436 | 500566184 | 28.1780 | 9.2599 |
| 745 | 555025 | 413493625 | 27.2947 | 9.0654 | 795 | 632025 | 502459875 | 28.1957 | 9.2638 |
| - | | | | | | | | | |
| 746 | 556516 | 415160936 | 27.3130 | 9.0694 | 796 | 633616 | 504358336 | 28.2135 | 9.2677 |
| 747 | 558009 | 416832723 | 27.3313 | 9.0735 | 797 | 635209 | 506261573 | 28.2312 | 9.2716 |
| 748 | 559504 | 418508992 | 27.3496 | 9.0775 | 798 | 636804 | 508169592 | 28.2489 | 9.2754 |
| 749 | 561001 | 420189749 | 27.3679 | 9.0816 | 799 | 638401 | 510082399 | 28.2666 | 9.2793 |
| 750 | 562500 | 421875000 | 27.3861 | 9.0856 | 800 | 640000 | 512000000 | 28.2843 | 9.2832 |
| | | | | | | | | 10 | |
| | | | | | and the second day of the second day | | | | |

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Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to 1000-continued.

| - | | | and the second | | - | | | | |
|-------|---------|-----------|--------------------|---------|-----|---------|-----------|---------|---------|
| No. | Square. | Cube. | Sq. Rt. | Cu. Rt. | No. | Square. | Cube: | Sq. Rt. | Cu. Rt. |
| 801 | 641601 | 513922401 | 28.3019 | 9.2870 | 851 | 724201 | 616295051 | 29.1719 | 9.4764 |
| 802 | 643204 | 515849608 | 28.3196 | 9.2909 | 852 | 725904 | 618470208 | 29.1890 | 9.4801 |
| 803 | 644809 | 517781627 | 28.3373 | 9.2948 | 853 | 727609 | 620650477 | 29.2062 | 9.4838 |
| 804 | 646416 | 519718464 | 28.3549 | 9.2986 | 854 | 729316 | 622835864 | 29.2233 | |
| · · · | 648025 | 521660125 | | | | | | | 9.4875 |
| 805 | | | 28.3725 | 9.3025 | 855 | 731025 | 625026375 | 29.2404 | 9.4912 |
| 806 | 649636 | 523606616 | 28.3901 | 9.3063 | 856 | 732736 | 627222016 | 29.2575 | 9.4949 |
| 807 | 651249 | 525557943 | 28.4077 | 9.3102 | 857 | 734449 | 629422793 | 29.2746 | 9.4986 |
| 808 | 652864 | 527514112 | 28.4253 | 9.3140 | 858 | 736164 | 631628712 | 29.2916 | 9.5023 |
| 809 | 654481 | 529475129 | 28.4429 | 9.3179 | 859 | 737881 | 633839779 | 29.3087 | 9.5060 |
| 810 | 656100 | 531441000 | 28.4605 | 9.3217 | 860 | 739600 | 636056000 | 29.3258 | 9.5097 |
| 811 | 657721 | 533411731 | 28.4781 | 9.3255 | 861 | 741321 | 638277381 | 29.3428 | |
| 812 | 659344 | 535387328 | 28.4956 | 9.3294 | 862 | 743044 | 640503928 | | 9.5134 |
| | | | | | | | | 29.3598 | 9.5171 |
| 813 | 660969 | 537367797 | 28.5132 | 9.3332 | 863 | 744769 | 642735647 | 29.3769 | 9.5207 |
| 814 | 662596 | 539353144 | 28.5307 | 9.3370 | 864 | 746496 | 644972544 | 29.3939 | 9.5244 |
| 815 | 664225 | 541343375 | 28.5482 | 9.3408 | 865 | 748225 | 647214625 | 29.4109 | 9.5281 |
| 816 | 665856 | 543338496 | 28.5657 | 9.3447 | 866 | 749956 | 649461896 | 29.4279 | 9.5317 |
| 817 | 667489 | 545338513 | 28.5832 | 9.3485 | 867 | 751689 | 651714363 | 29.4449 | 9.5354 |
| 818 | 669124 | 547343432 | 28.6007 | 9.3523 | 868 | 753424 | 653972032 | 29.4618 | 9.5391 |
| 819 | 670761 | 549353259 | 28.6182 | 9.3561 | 869 | 755161 | 656234909 | 29.4788 | 9.5427 |
| 820 | 672400 | 551368000 | 28.6356 | 9.3599 | 870 | 756900 | 658503000 | 29.4958 | |
| 1.1.1 | | | | | | | | | 9.5464 |
| 821 | 674041 | 553387661 | 28.6531 | 9.3637 | 871 | 758641 | 660776311 | 29.5127 | 9.5501 |
| 822 | 675684 | 555412248 | 28.6705 | 9.3675 | 872 | 760384 | 663054848 | 29.5296 | 9.5537 |
| 823 | 677329 | 557441767 | 28.6880 | 9.3713 | 873 | 762129 | 665338617 | 29.5466 | 9.5574 |
| 824 | 678976 | 559476224 | 28.7054 | 9.3751 | 874 | 763876 | 667627624 | 29.5635 | 9.5610 |
| 825 | 680625 | 561515625 | 28.7228 | 9.3789 | 875 | 765625 | 669921875 | 29.5804 | 9.5647 |
| 826 | 682276 | 563559976 | 28.7402 | 9.3827 | 876 | 767376 | 672221376 | 29.5973 | 9.5683 |
| 827 | 683929 | 565609283 | 28.7576 | 9.3865 | 877 | 769129 | 674526133 | 29.6142 | 9.5719 |
| 828 | 685584 | 567663552 | 28.7750 | 9.3902 | 878 | 770884 | 676836152 | 29.6311 | |
| 829 | 687241 | | 28.7924 | | 879 | | | | 9.5756 |
| | 688000 | 569722789 | | 9.3940 | | 772641 | 679151439 | 29.6479 | 9.5792 |
| 830 | 688900 | 571787000 | 28.8097 | 9.3978 | 880 | 774400 | 681472000 | 29.6648 | 9.5828 |
| 831 | 690561 | 573856191 | 28.8271 | 9.4016 | 881 | 776161 | 683797841 | 29.6816 | 9.5865 |
| 832 | 692224 | 575930368 | 28.8444 | 9.4053 | 882 | 777924 | 686128968 | 29.6985 | 9.5901 |
| 833 | 693889 | 578009537 | 28.8617 | 9.4091 | 883 | 779689 | 688465387 | 29.7153 | 9.5937 |
| 834 | 695556 | 580093704 | 28.8791 | 9.4129 | 884 | 781456 | 690807104 | 29.7321 | 9.5973 |
| 835 | 697225 | 582182875 | 28.8964 | 9.4166 | 885 | 783225 | 693154125 | 29.7489 | 9.6010 |
| 836 | 698896 | 584277056 | 28.9137 | 9.4204 | 886 | 784996 | 695506456 | 29.7658 | 9.6046 |
| 837 | 700569 | 586376253 | 28.9310 | 9.4204 | 887 | 786769 | 697864103 | | 9.6040 |
| 820 | | | | | 888 | | | 29.7825 | |
| 838 | 702244 | 588480472 | 28.9482 | 9.4279 | | 788544 | 700227072 | 29.7993 | 9.6118 |
| 839 | 703921 | 590589719 | 28.9655 | 9.4316 | 889 | 790321 | 702595369 | 29.8161 | 9.6154 |
| 840 | 705600 | 592704000 | 28.9828 | 9.4354 | 890 | 792100 | 704969000 | 29.8329 | 9.6190 |
| 841 | 707281 | 594823321 | 29. | 9.4391 | 891 | 793881 | 707347971 | 29.8496 | 9.6226 |
| 842 | 708964 | 596947688 | 29.0172 | 9.4429 | 892 | 795664 | 709732288 | 29.8664 | 9.6262 |
| 843 | 710649 | 599077107 | 29.0345 | 9.4466 | 893 | 797449 | 712121957 | 29.8831 | 9.6298 |
| 844 | 712336 | 601211584 | 29.0517 | 9.4503 | 894 | 799236 | 714516984 | 29.8998 | 9.6334 |
| 845 | 714025 | 603351125 | 29.0689 | 1.4541 | 895 | 801025 | 716917375 | 29.9166 | 9.6370 |
| 846 | 715716 | 605495736 | 29.0861 | 9.4578 | 896 | 802816 | 719323136 | | 9.6406 |
| 847 | 717409 | | - | | 897 | 802810 | | 29.9333 | |
| 848 | 719104 | 607645423 | 29.1033 29.1204 | 9.4615 | 898 | 804009 | 721734273 | 29.9500 | 9.6442 |
| 849 | 720801 | 611960049 | | | 899 | 808201 | 724150792 | | 9.6477 |
| | | | 29.1376 | 9.4690 | | | 726572699 | 29.9833 | 9.6513 |
| 850 | 722500 | 614125000 | 29.1548 | 9.4727 | 900 | 810000 | 729000000 | 30. | 9.6549 |
| - | - | | 1 | | 11 | 1 | 1 | 1 | - |

Table of Squares, Cubes, Square Roots, and Cube Roots of Numbers from I to 1000—continued.

| No. | Square. | Cube, | Sq. Rt. | Cu. Rt. | No. | Square. | Cube. | Sq. Rt. | Cu. Rt. |
|---------|------------------|------------|---------|---------|------------|---------|------------|---------|------------------|
| 901 | 811801 | 731432701 | 30.0167 | 9.6585 | 951 | 904401 | 860085351 | 30.8383 | 0 8000 |
| | | | | 9.6620 | | | 860003351 | | 9.8339 |
| 902 | 813604 | 733870808 | 30.0333 | | 952 | 906304 | 862801408 | 30.8545 | 9.8374 9.8408 |
| 903 | 815409 | 736314327 | 30.0500 | 9.6656 | 953 | 908209 | 865523177 | 30.8707 | 9.8408 |
| 904 | 817216 | 738763264 | 30.0666 | 9.6692 | 954 | 910116 | 868250664 | 30.8869 | 9.8443 |
| 905 | 819025 | 741217625 | 30.0832 | 9.6727 | 955 | 912025 | 870983875 | 30.9031 | 9.8477 |
| 906 | 820836 | 743677416 | 30.0998 | 9.6763 | 956 | 913936 | 873722816 | 30.9192 | 9.8511 |
| 907 | 822649 | 746142643 | 30.1164 | 9.6799 | 957 | 915849 | 876467493 | 30.9354 | 9.8546 |
| 908 | 824464 | 748613312 | 30.1330 | 9.6834 | 958 | 917764 | 879217912 | 30.9516 | 9.8580 |
| 909 | 826281 | 751089429 | 30.1496 | 9.6870 | 959 | 919681 | 881974079 | 30.9677 | 9.8614 |
| 910 | 828100 | 753571000 | 30.1662 | 9.6905 | 960 | 921600 | 884736000 | 30.9839 | 9.8648 |
| 911 | 829921 | 756058031 | 30.1828 | 9.6941 | 961 | 923521 | 887 503681 | 31. | 9.8683 |
| 912 | 831744 | 758550528 | 30.1993 | 9.6976 | 962 | | | 31.0161 | |
| | | | | | | 925444 | 890277128 | | 9.8717 |
| 913 | 833569 | 761048497 | 30.2159 | 9.7012 | 963 | 927369 | 893056347 | 31.0322 | 9.8751 |
| 914 | 835396 | 763551944 | 30.2324 | 9.7047 | 964 | 929296 | 895841344 | 31.0483 | 9.8785 |
| 915 | 837225 | 766060875 | 30.2490 | 9.7082 | 965 | 931225 | 898632125 | 31.0644 | 9.8819 |
| 916 | 839056 | 768575296 | 30.2655 | 9.7118 | 966 | 933156 | 901428696 | 31.0805 | 9.8854 |
| 917 | 840889 | 771095213 | 30.2820 | 9.7153 | 967 | 935089 | 904231063 | 31.0966 | 9.8888 |
| 918 | 842724 | 773620632 | 30.2985 | 9.7188 | 968 | 937024 | 907039232 | 31.1127 | 9.8922 |
| 919 | 844561 | 776151559 | 30.3150 | 9.7224 | 969 | 938961 | 909853209 | 31.1288 | 9.8956 |
| 920 | 846400 | 778688000 | 30.3315 | 9.7259 | 970 | 940900 | 912673000 | 31.1448 | 9.8990 |
| 921 | 848241 | 781229961 | 30.3480 | 9.7294 | 971 | 942841 | 915498611 | 31.1609 | 9.9024 |
| 922 | 850084 | 783777448 | | | | | | | |
| - | | | 30.3645 | 9.7329 | 972 | 944784 | 918330048 | 31.1769 | 9.9058 |
| 923 | 851929 | 786330467 | 30.3809 | 9.7364 | 973 | 946729 | 921167317 | 31.1929 | 9.9092 |
| 924 | 853776 | 788889024 | 30.3974 | 9.7400 | 974 | 948676 | 924010424 | 31.2090 | 9.9126 |
| 925 | 855625 | 791453125 | 30.4138 | 9.7435 | 975 | 950625 | 926859375 | 31.2250 | 9.9160 |
| 926 | 857476 | 794022776 | 30.4302 | 9.7470 | 976 | 952576 | 929714176 | 31.2410 | 9.9191 |
| 927 | 859329 | 796597983 | 30.4467 | 9.7505 | 977 | 954529 | 932574833 | 31.2570 | 9.9227 |
| 928 | 861184 | 799178752 | 30.4631 | 9.7540 | 978 | 956484 | 935441352 | 31.2730 | 9.9261 |
| 929 | 863041 | 801765089 | 30.4795 | 9.7575 | 979 | 958441 | 938313739 | 31.2890 | 9.9295 |
| 930 | 864900 | 804357000 | 30.4959 | 9.7610 | 980 | 960400 | 941192000 | 31.3050 | 9.9329 |
| 931 | 866761 | 806954491 | 30.5123 | 9.7645 | 981 | 962361 | 944076141 | 31.3209 | 9.9363 |
| 932 | 868624 | 809557568 | 30.5287 | 9.7680 | 982 | | | | |
| | | 00955/500 | | | | 964324 | 946966168 | 31.3369 | 9.9396 |
| 933 | 870489 | 812166237 | 30.5450 | 9.7715 | 983 | 966289 | 949862087 | 31.3528 | 9.9430 |
| 934 | 872356 | 814780504 | 30.5614 | 9.7750 | 984 | 968256 | 952763904 | 31.3688 | 9.9464 |
| 935 | 874225 | 817400375 | 30.5778 | 9.7785 | 985 | 970225 | 955671625 | 31.3847 | 9.9497 |
| 936 | 876096 | 82002 5856 | 30.5941 | 9.7819 | 986 | 972196 | 958585256 | 31.4006 | 9.9531 |
| 937 | 877969 | 822656953 | 30.6105 | 9.7854 | 987 | 974169 | 961504803 | 31.4166 | 9.9565 |
| 938 | 879844 | 825293672 | 30.6268 | 9.7889 | 988 | 976144 | 964430272 | 31.4325 | 9.9598 |
| 939 | 881721 | 827936019 | 30.6431 | 9.7924 | 989 | 978121 | 967361669 | 31.4484 | 9.9632 |
| 940 | 883600 | 830584000 | 30.6594 | 9.7959 | 990 | 980100 | 970299000 | 31.4643 | 9.9666 |
| 941 | 885481 | 833237621 | 30.6757 | 9.7993 | 991 | 982081 | 973242271 | 31.4802 | 9.9699 |
| 942 | 887364 | 835896888 | 30.6920 | 9.8028 | 992 | 984064 | 976191488 | 31.4960 | 9.9099 |
| 943 | 889249 | 838561807 | 30.7083 | 9.8063 | 992 | 986049 | 979146657 | 31.5119 | 9.9766 |
| 943 | 891136 | 841232384 | 30.7246 | 9.8097 | | 988036 | 982107784 | 31.5278 | 9.9800 |
| 944 945 | 893025 | 843908625 | 30.7240 | 9.8097 | 994 995 | 990025 | 985074875 | 31.5278 | 9.9833 |
| 946 | | | | | 995 | | | | |
| | 894916 896809 | 846590536 | 30.7571 | 9.8167 | | 992016 | 988047936 | 31.5595 | 9.9866 |
| 947 | | 849278123 | 30.7734 | 9.8201 | 997 | 994009 | 991026973 | 31.5753 | 9.9900 |
| 948 | 898704 | 851971392 | 30.7896 | 9.8236 | 998 | 996004 | 994011992 | 31.5911 | 9.9933 |
| 949 | 900601 | 854670349 | 30.8058 | 9.8270 | 999 | 998001 | 997002999 | 31.6070 | 9.9967 |
| 950 | 902500 | 857375000 | 30.8221 | 9.8305 | 1000 | 1000000 | 1000000000 | 31.6228 | 10. |
| | | | | | | | | | |

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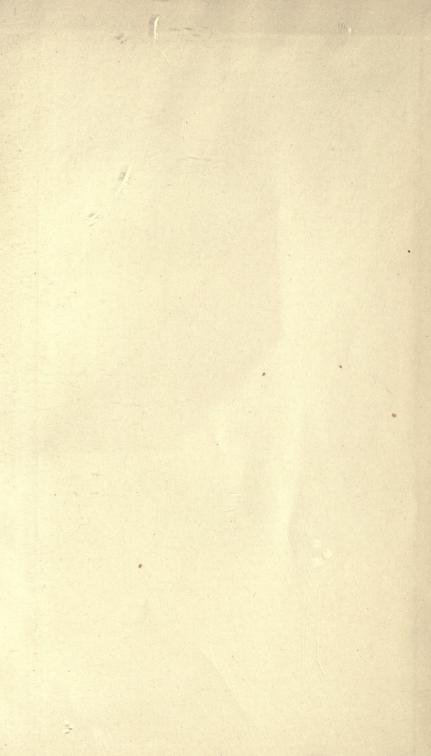
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