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MACHINERY'S DATA SHEETS
REVISED AND RE-ARRANGED IN LIBRARY FORM
Reamers, Sockets, Drills
Milling Cutters
PRICE 25 CENTS
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Shell Reamers and Arbors. $\qquad$
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# MACHINERY'S DATA SHEET SERIES 

COMPILED FROM MACHINERY'S MONTHLY DATA SHEETS AND ARRANGED WITH EXPLANATORY MATTER

## No. 4

# Reamers, Sockets, Drills and 

 Milling Cutters
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In the following pages are compiled a number of concise tables relating to reamers, sockets, drills, and milling cutters, carefully selected from Machinery's monthly Data Sheets, issued as supplements to the Engineering and Railway editions of Machinery since September, 1898. A number of additional tables are also included which are published here for the first time.

In order to enhance the value of the tables, brlef explanatory notes have been provided. In these notes a complete list of references is given to articles which have appeared in Machinery, and to matter published in Machinery's Reference Series, giving additional information on the subject. These references will be of considerable value to readers who wish to make a more thorough study of the subject. In a note at the foot of each table, reference is made to the page on which the explanatory note relating to the table appears.


# REAMERS, SOCKETS, DRILLS AND MILLING CUTTERS 

## Dimensions of Hand Reamers

On pages 4 and 5 are given dimensions for ordinary hand reamers provided with a guide of the length $G$. All hand reamers should be provided with a guide of this type in order to obtain a straight reamed hole. This provision is not generally made in reamers manufactured for the market, but it is of great importance in a tool expected to produce accurate work. The guide portion $G$ at the end of the reamer is not relieved, but is left cylindrical; the flutes, of course, are cut through it in the usual manner. The amount that this pilot should be less in diameter than the reamer itself is determined by the maximum amount of metal that the reamer should be expected to remove.

While not so shown in the engraving on page 4, the diameter of the shank at the end where the square is milled should be turned down slightly below the diameter of the shank proper. The purpose of this is to prevent any burrs that may be raised on the edges of the square by the wrench by which the reamer is turned from projecting outside of the diameter of the shank. These burrs would prevent the reamer from being drawn clear through the hole reamed, or, at least, would scratch the inside of the hole when the reamer is pulled through. As seen from the table, all the reamers are made with an even number of flutes in order to facilitate the measuring of the diameter. The flutes, however, should be "broken up," that is, the cutting edges should not be equally spaced, but a slight difference in spacing of all the cutting edges
around the reamer should be introduced. This ununiformity in spacing need not be greater than two or at most three degrees, which will still permit of measuring the diameter of the reamer over two opposite cutting edges. This measurement will be nearly correct enough for all practical purposes.

The relief of the cutting edges should preferably be eccentric, that is, the land back of the cutting edge should be convex rather than flat. This makes it posstble for the reamer to hold its size longer, but an eccentrically relieved reamer should be used purely for finishing, as it cannot, with advantage, be used to remove any considerable amount of metal; for hand reamers used merely for removing stock or simply for enlarging holes, the flat relief is superior. For straight, smooth and accurate work, again, the eccentric relief is better. [Machinery, January, 1906, Hand Reamers; August and September, 1907, Reamers; May, 1910, Irregular Spacing of the Cutting Edges of Reamers.]

## Shell Reamers and Arbors

Dimensions of shell reamers and arbors are given on page 6. It will be seen that one arbor can be used for a considerable number of sizes of reamers, and the material that would otherwise be used in the shank of each individual reamer is saved. The reamer has a keyway $F$, which fits the key on the arbor with $1 / 64$ inch play. The hole through the reamer tapers $1 / 8$ inch per foot, as shown. The tapered part of the arbor as well as the hole in the reamer must be ground after hardening to in(Continued on page 16.)

| $\begin{gathered} F=\text { size } \\ \text { of Square } \end{gathered}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |
|  |  |  |  | 交 |  |  | $\begin{aligned} & \text { Number } \\ & \text { of } \end{aligned}$ |
|  |  | --b |  |  |  |  |  |
| Diam. | $\begin{aligned} & \text { Total } \\ & \text { Length } \end{aligned}$ | $\begin{aligned} & \text { Length } \\ & \text { of } \\ & \text { Flute } \end{aligned}$ | $\begin{aligned} & \text { length } \\ & \text { of } \\ & \text { Shank } \end{aligned}$ | $\begin{aligned} & \text { Length } \\ & \text { of } \\ & \text { squared } \\ & \text { apart } \end{aligned}$ | $\begin{gathered} \text { size } \\ \text { of } \\ \text { square } \end{gathered}$ | $\begin{aligned} & \text { Length } \\ & \text { of } \\ & \text { Guide } \end{aligned}$ |  |
| A | $B$ | c | D | E | F | G |  |
| $\frac{1}{16}$ | $2{ }^{\frac{3}{16}}$ | $\frac{7}{8}$ | $1 / 5$ | $\frac{7}{32}$ | $\frac{3}{64}$ | $\frac{3}{16}$ | 6 |
| \% | $2{ }^{5}$ | $1 \frac{18}{8}$ | $1 \frac{1}{2}$ | $\frac{1}{4}$ | $\frac{3}{32}$ | $\frac{7}{32}$ | 6 |
| $\frac{3}{16}$ | $3 \frac{18}{16}$ | 13 | 116 | $\frac{9}{32}$ | $\frac{9}{84}$ | \% | 6 |
| $\frac{1}{4}$ | $3 \frac{1}{2}$ | 15 | 178 | $\frac{5}{16}$ | $\frac{3}{16}$ | $\frac{5}{16}$ | 6 |
| $\frac{5}{16}$ | 315 | 18 | $2 \frac{1}{16}$ | $\frac{11}{32}$ | $\frac{15}{64}$ | $\frac{3}{8}$ | 6 |
| 3/8 | $4 \frac{3}{8}$ | $2 \frac{1}{8}$ | $2{ }^{\frac{1}{4}}$ | 3/8 | $\frac{9}{32}$ | ${ }_{32}^{13}$ | 6 |
| $\frac{7}{16}$ | 416 | 28 | $27 \frac{7}{16}$ | $\frac{13}{32}$ | $\frac{21}{54}$ | $\frac{7}{16}$ | 6 |
| $\frac{1}{2}$ | $5 \frac{1}{4}$ | $2{ }^{5}$ | $2{ }^{\frac{5}{8}}$ | $\frac{7}{16}$ | 3 | $\frac{1}{2}$ | 6 |
| $\frac{9}{16}$ | $5 \frac{11}{16}$ | $2 \frac{8}{8}$ | $2 \frac{13}{16}$ | $\frac{15}{32}$ | $\frac{27}{64}$ | $\frac{9}{16}$ | 8 |
| $5 / 8$ | $6 \frac{1}{8}$ | $3 \frac{1}{8}$ | 3 | $\frac{1}{2}$ | $\frac{15}{32}$ | $\frac{19}{32}$ | 8 |
| $\frac{11}{16}$ | $6 \frac{9}{6}$ | $3 \frac{3}{8}$ | $3{ }^{\frac{3}{16}}$ | $\frac{17}{32}$ | $\frac{33}{64}$ | 5/8 | 8 |
| $3 / 4$ | 7 | $3 \frac{5}{8}$ | $3 \frac{3}{8}$ | $\frac{9}{16}$ | $\frac{9}{16}$ | $\frac{11}{16}$ | 8 |
| $\frac{13}{16}$ | 77 | $3 \frac{7}{8}$ | 39 | $\frac{19}{32}$ | 39 | $\frac{3}{4}$ | $\dot{8}$ |
| 78 | $7 \frac{8}{8}$ | $4 \frac{1}{8}$ | $3^{\frac{3}{4}}$ | $5 / 8$ | $\frac{21}{32}$ | $\frac{25}{32}$ | 8 |
| $\frac{15}{16}$ | $8 \frac{5}{16}$ | 48 | $3 \frac{15}{16}$ | $\frac{21}{32}$ | $\frac{45}{64}$ | $\frac{13}{16}$ | 8 |
| 1 | $8^{3}$ | $4 \frac{5}{8}$ | $4 \frac{1}{8}$ | $\frac{11}{16}$ | 3/4 | $\overline{8}$ | 8 |
| $1 \frac{1}{16}$ | $9 \frac{3}{16}$ | $4 \frac{7}{8}$ | $4 \frac{5}{16}$ | ${ }_{3}^{23}$ | $\frac{51}{64}$ | ${ }_{32}^{29}$ | 8 |
| $1 \frac{18}{8}$ | 93 | 415 | $4 \frac{7}{16}$ | $\frac{3}{4}$ | $\frac{27}{32}$ | 15 | 8 |
| $1 \frac{3}{16}$ | 99 | $5 \frac{1}{10}$ | $4 \frac{1}{2}$ | $\frac{25}{32}$ | $\frac{57}{64}$ | $\frac{31}{32}$ | 8 |

DIMENSIONS OF HAND REAMERS-II

| Diam. | Total Length | Length flute | Length of shank | Length of squared Part | size of square | Length of Guide | Number of Flutes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $A$ | $B$ | C | 0 | E | $F$ | G |  |
| $1 \frac{1}{4}$ | $9^{3}$ | $5 \frac{3}{16}$ | $4 \frac{9}{16}$ | $\frac{13}{16}$ | $\frac{15}{16}$ | 1 | 8 |
| 15 | 915. | $5 \frac{5}{16}$ | $4 \frac{5}{8}$ | $\frac{27}{32}$ | ${ }_{6}^{63}$ | $1 \frac{1}{32}$ | 10 |
| 13 | $10 \frac{1}{8}$ | $5 \frac{3}{8}$ | $4 \frac{3}{4}$ | 78 | $1 \frac{1}{32}$ | $1 \frac{1}{16}$ | 10 |
| $1{ }_{16}$ | $10 \frac{5}{16}$ | $5 \frac{1}{2}$ | $4 \frac{13}{16}$ | $\frac{29}{32}$ | $1 \frac{5}{64}$ | $1 / \frac{3}{32}$ | 10 |
| $1 \frac{1}{2}$ | $10 \frac{1}{2}$ | $5 \frac{5}{8}$ | $4 \frac{7}{8}$ | $\frac{15}{16}$ | 1/8 | 1\% | 10 |
| $1 \frac{19}{16}$ | $10 \frac{11}{16}$ | $5 \frac{3}{4}$ | $4 \frac{15}{16}$ | $\frac{31}{32}$ | $1 \frac{11}{64}$ | $1 \frac{5}{32}$ | 10 |
| 15 | 10\% | $5 \frac{13}{16}$ | $5 \frac{1}{16}$ | 1 | $1 \frac{7}{32}$ | $1 \frac{3}{16}$ | 10 |
| 111 | $11 / 16$ | $5 \frac{15}{16}$ | $5 \frac{1}{8}$ | $1 \frac{1}{32}$ | $1 \frac{17}{64}$ | $1 \frac{7}{32}$ | 10 |
| 13 | $11 \frac{1}{4}$ | $6 \frac{1}{16}$ | $5 \frac{3}{16}$ | 116 | 15 | 1/4 | 10 |
| $1{ }^{13}$ | $11 / 15$ | $6 \frac{3}{16}$ | $5 \frac{1}{4}$ | $13 \frac{3}{32}$ | 123 | $1 \frac{9}{32}$ | 12 |
| 18 | 115 | $6 \frac{1}{4}$ | $5 \frac{3}{8}$ | $1 / 8$ | 138 | 15 | 12 |
| $1 \frac{15}{16}$ | 1116 | $6 \frac{3}{8}$ | $5 \frac{7}{16}$ | 138 | 129 | 131 | 12 |
| 2 | 12 | $6 \frac{1}{2}$ | $5 \frac{1}{2}$ | $1 \frac{3}{16}$ | $1 \frac{1}{2}$ | 13 | 12 |
| $2 \frac{1}{8}$ | 1238 | $6 \frac{11}{16}$ | $5 \frac{11}{16}$ | $1 / 4$ | $1 \frac{19}{32}$ | i/16 | 12 |
| $2 \frac{1}{4}$ | $12^{\frac{3}{4}}$ | 615 | $5 \frac{13}{16}$ | 15 | 111 | $1 \frac{1}{2}$ | 12 |
| $2{ }^{3} 8$ | $13 \frac{18}{8}$ | $7 \frac{1}{8}$ | 6 | 18 | $1 \frac{25}{32}$ | 19 | 14 |
| $2 \frac{1}{2}$ | $13 \frac{1}{2}$ | $7 \frac{3}{8}$ | $6 \frac{18}{8}$ | $1 \frac{7}{16}$ | 178 | 15 | 14 |
| 258 | 1378 | 79 | $6 \frac{5}{16}$ | $1 \frac{1}{2}$ | 132 | 116 | 14 |
| $2 \frac{3}{4}$ | $14 \frac{1}{4}$ | $7 \frac{13}{16}$ | $6 \frac{7}{16}$ | $1 \frac{9}{16}$ | $2 \frac{1}{16}$ | 13 | 14 |
| 27 | $14 \frac{5}{8}$ | 8 | 65 | 15 | $2 \frac{5}{32}$ | $1 \frac{13}{16}$ | 16 |
| 3 | 15 | $8 \frac{1}{4}$ | $6 \frac{3}{4}$ | $11 / 1$ | $2 \frac{1}{4}$ | 17 | 16 |
| 318 | $15 \frac{3}{8}$ | $81 / 6$ | $6 \frac{15}{16}$ | 13 | $2 \frac{11}{32}$ | . 115 | 16 |
| $3 \frac{1}{4}$ | $15 \frac{3}{4}$ | 8110 | $7 \frac{1}{16}$ | $1 \frac{13}{16}$ | $2 \frac{7}{16}$ | 2 | 18 |
| $3 \frac{3}{8}$ | $16 \frac{1}{8}$ | $8 \frac{7}{8}$ | $7 \frac{1}{4}$ | 178 | $2 \frac{17}{32}$ | $2 \frac{1}{16}$ | 18 |
| $3 \frac{1}{2}$ | $16 \frac{1}{2}$ | 9\%88 | $7 \frac{3}{8}$ | $1{ }^{15}$ | 258 | 218 | 18 |
| $3 \frac{5}{8}$ | $16 \%$ | $9 \frac{5}{16}$ | $7 \frac{9}{16}$ | 2 | $2{ }^{23}$ | $2 \frac{3}{16}$ | 18 |
| $3 \frac{3}{4}$ | 17\% | $9 \frac{9}{10}$ | 7119 | $2 \frac{1}{16}$ | $2 \frac{13}{16}$ | $2 \frac{1}{4}$ | 18 |
| 378 | $17 \frac{5}{8}$ | $9 \frac{3}{4}$ | $7 \%$ | $2 \frac{1}{8}$ | $2 \frac{29}{32}$ | $2 \frac{5}{16}$ | 20 |
| 4 | 18 | 10 | 8 | $2 \frac{3}{16}$ | 3 | $2 \frac{3}{8}$ | 20 |

SHELL REAMERS AND ARBORS

| Dimensions of Shell Reamers. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |
| Diam. of Reamers | Diam. of Hole, Large End | Total Length | Length of Turneddown Portion | Length of Flutes | width of Keyway | Depth of Keyway | Constant for finding Diam. of Recess | Number of Flutes |
| A | B | C | D | E | F | G | A-H |  |
| 1/4-5/16 | $1 / 8$ | 1/2 | $3 / 8$ | $1 / 8$ | \%/16 | $1 / 8$ | 0.006 | 6 |
| $11 / 32-7 / 6$ | 3/16 | $13 / 4$ | $3 / 8$ | $13 / 8$ | 3/32 | 1/8 | 0.006 | 6 |
| 15/32-9/16 | $1 / 4$ | 2 | $1 / 2$ | $1 / 2$ | 764 | 5/32 | $1 / 64$ | 8 |
| $1932-11 / 6$ | $3 / 8$ | 2/4 | 1/2 | 134 | 964 | 3/16 | $1 / 64$ | 8 |
| $23 / 32-15 / 16$ | $1 / 2$ | 21/2 | 1/2 | 2 | 1164 | $1 / 4$ | 1/32 | 10 |
| $31 / 32-1 / 4$ | $5 / 8$ | $2 \frac{3}{4}$ | $5 / 8$ | 21/8 | $13 / 64$ | 1/4 | 1/6 | 10 |
| $1932-158$ | $3 / 4$ | 3. | $5 / 8$ | $2 \frac{3}{8}$ | $1 / 4$ | 5/6 | $1 / 8$ | 12 |
| $1^{21 / 32-2}$ | 1 | $31 / 2$ | $5 / 8$ | 278 | $1 / 4$ | 5/16 | $1 / 8$ | 12 |
| $2 \frac{132-2 \frac{1}{2}}{}$ | $1 / 4$ | $3 \frac{3}{4}$ | 3/4 | 3 | 5/6 | $3 / 8$ | $1 / 8$ | 14 |
| 2/732-3. | $1 \frac{1}{2}$ | 4 | $3 / 4$ | $3 \frac{1}{4}$ | 5/16 | $3 / 8$ | 1/8 | 14 |
| 31/32-3/2 | 13 | $4 \frac{1}{2}$ | 1 | $31 / 2$ | 5/16 | $3 / 8$ | $1 / 8$ | 16 |
| $3{ }^{1 / 32} 32$ | 2 | 5 | 1 | 4 | 5/16 | $3 / 8$ | 1/8 | 16 |
| $4 \frac{1}{32}-4 / 2$ | 2/4 | $5 \frac{1}{2}$ | 1 | $4 \frac{1}{2}$ | 5/16 | 3/8 | 1/8 | 18 |
| $4^{\prime / 3} 32-5$ | $2 \frac{1 / 2}{}$ | 6 | 1 | 5 | 5/16 | 3/8 | 1/8 | 18 |
| Arbors for Shell Reamers. |  |  |  |  |  |  |  |  |
| $F, G$ and $H$ are given in Table above. |  |  |  |  |  |  |  |  |
| Diam. at size Line | Length from size Line to End of Arbor | Total Length | $\begin{gathered} \text { Diam.at } \\ \text { Size } \\ \text { Line } \end{gathered}$ | Length from size Line to End of Arbor | Total Length | Diam. af size Line | Length from size <br> Line to End of Arbor | Total Length |
| K | $L$ | M | $K$ | L | M | $K$ | L | M |
| 1/8 | 1/2 | 6 | 5/8 | $2 \frac{3}{4}$ | 10 | 13 | 4/2 | 15 |
| 3/16 | 13 | 7 | $3 / 4$ | 3 | $1 /$ | 2 | 5 | 16 |
| 1/4 | 2 | 8 |  | 31/2 | 12 | $2 \frac{1}{4}$ | $5 \frac{1}{2}$ | 17 |
| $3 / 8$ | 2/4 | 9 | $1 \frac{1}{4}$ | $3 \frac{3}{4}$ | 13 | $2 \frac{1}{2}$ | 6 | 18 |
| 1/2 | $21 / 2$ | 91/2 | 1/2 | 4 | 14 |  |  |  |

## SETTING OF TOOTH-REST FOR GRINDING CLEARANCE ON REAMERS

| $\begin{aligned} & x \\ & 0 \\ & 0 \\ & N \\ & \text { N } \\ & \text { b } \\ & 0 \end{aligned}$ | Hand Reamer for: Steel Cutting Cleari ance Land 0.006" wide |  | II <br> Hand Reamer tor Cast Iron and Bronze. Cutfing Clearance tand. $0.025^{\prime \prime}$ wide |  | III <br> Chucking Reamer for Cast Iron and Bronze. Cutting Clearance Land $0.025^{\prime \prime}$ wide |  | IV Rose Chucking Reamers for steel, Clircular Ground |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | For Cutting Clearance | For. Second. Clearance | For Cuifting Clearance | For second Cleararice | For Cutting Clearance | For second Clearance | For Cutting Clearance on Angular Edge at End |
|  | 0.012 | 0.052 | 0.032 | 0.072 | 0.040 | 0.080 | 0.080 |
|  | 0.012 | $0: 062$ | 0.032 | 0.072 | 0.040 | 0.090 | 0.090 |
| $3 / 4$ | 0.012 | 0.072 | 0.035 | 0.095 | 0.040 | 0.100 | 0.100 |
| $7 / 8$ | 0.012 | 0.082 | 0.040 | 0.120 | 0.045 | 0.125 | 0.125 |
| 1 | 0.012 | 0.092 | 0.040 | 0.120 | 0.045 | 0.125 | 0.125 |
| 18 | 0.012 | 0.102 | 0.040 | 0.120 | $0.04,5$ | 0.125 | 0.125 |
| $1 \frac{1}{4}$ | 0.012 | 0.112 | 0.045 | 0.145 | 0.050 | 0.160 | 0.160 |
| 138 | 0.0 .12 | 0.122 | 0.045 | 0.1 .45 | 0.050 | 0.160 | 0.175 |
| $1 / 2$ | 0.012 | . 0.132 | 0.048 | 0.168 | 0.055 | 0.175 | 0.175 |
| $13 / 8$ | 0.012 | 0.142 | $0.05{ }^{\circ}$ | 0.170 | 0.060 | 0200 | 0.200 |
| $13 / 4$ | 0.012 | 0.152 | 0.052 | 0.192 | $: 0.060$. | 0.200 | 0.200 |
| 178 | 0.012 | 0.162 | 0.056 | 0.196 | 0.060 | 0.200 | 0.200 |
| 2 | 0.012 | 0.172 | 0.056 | 0.216 | .0.064 | 0.224 | 0.225 |
| $2 \frac{1}{8}$ | 0.012 | 0.172 | 0.059 | $0.2 / 9$ | 0.064 | 0.224 | 0.225 |
| $2 \frac{1}{4}$ | 0.012 | 0.172 | 0.063 | 0.223 | 0.064 | 0.224 | 0.225 |
| $23 / 8$ | $0.0 \% 2$ | 0.172 | 0.063 | 0.223 | 0.068 | 0.228 | 0.230 |
| $2 \frac{1}{2}$ | 0.012 | $0.172 \ldots$ | 0.065 | 0.225 | 0.072 | 0.232 | 0.230 |
| 25/8 | 0.012 | 0.172 | 0.065 | 0.225 | 0.075 | 0.235 | 0.235 |
| $23 / 4$ | 0.012 | 0.1 .72 | 0.065 | 0.225 | 0.0 .77 | 0.237 | 0.240 |
| $27 / 8$ | 0.012 | 0.172 | 0.070 | 0.230 | 0.08 .0 | 0.240 | 0.240 |
| 3 | 0.012 | 0.172 | 0.072 | 0.232 | 0.0880 | 0.240 | 0.240 |
| $3 \frac{1}{8}$ | 0.012 | 0.172 | 0.075 | 0.235 | 0.083 | 0.240 | 0.240 |
| $31 / 4$ | 0.012 | 0.172 | 0.078 | 0.238 | 0.083 | 0.243 | 0.245 |
| 3.8 | 0.012 | 0.172 | 0.081 | 0.241 | 0.087 | 0.247 | 0.245 |
| $3 \frac{1}{2}$ | 0.012 | 0.172 | 0.084 | 0.244 | 0.090 | 0.250 | 0.250 |
| $3 \frac{5}{8}$ | 0.012 | 0.172 | 0.087 | 0.247 | 0.093 | 0.253 | 0.250 |
| $3 \frac{3}{4}$ | 0.012 | 0.172 | 0.090 | 0.250 | 0.097 | 0.257 | 0.255 |
| 378 | 0.012 | 0.172 | 0.093 | 0.253 | 0.100 | 0.260 | 0.255 |
| 4 | 0.012 | 0.172 | 0.096 | 0.256 | $0.104^{\circ}$ | 0.264 | 0.260 |
| $4 \frac{1}{8}$ | 0.012 | 0.172 | 0.096 | 0.256 | 0.104 | 0.264 | 0.260 |
| 41/4 | 0.012 | 0.172 | 0.096 | 0.256 | 0.106 | 0.266 | 0.265 |
| $43 / 8$ | 0.01 .2 | 0.172 | 0.096 | 0.256 | 0.108 | 0.268 | 0.265 |
| $4 \frac{1}{2}$ | 0.012 | 0.172 | 0.100 | 0.260 | 0.108 | 0.268 | 0.265 |
| $4 \frac{5}{8}$ | 0.012 | 0.172 | 0.100 | 0.260 | 0.110 | 0.270 | 0.270 |
| $43 / 4$ | 0.012 | 0.172 | 0.104 | 0.264 | 0.1 .14 | 0.274 | 0.275 |
| $47 / 8$ | 0.012 | 0.172 | 0.106 | 0.266 | 0.116 | 0.276 | 0.275 |
| 5 | 0.012 | 0.172 | 0.11 .0 | 0.270 | $0.1 / 8$ | 0.278 | 0.275 |

DIMENSIONS OF PIPE REAMERS

| ( $\begin{gathered}\mathrm{H}=\text { Size } \\ \text { of Square }\end{gathered}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  | - | - | - |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  | \% | - |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | --- | -F- |  |  |  |  |
| $\begin{aligned} & \text { Pipe } \\ & \text { Size } \end{aligned}$ | Diam. |  |  | Length | Length | $\begin{aligned} & \text { Total } \\ & \text { Length } \end{aligned}$ | $\begin{aligned} & \text { Length } \\ & \text { Square } \end{aligned}$ | $\begin{gathered} \text { size } \\ \text { sof } \\ \text { square } \end{gathered}$ | $\begin{aligned} & \text { Number } \\ & \text { Filutes } \end{aligned}$ |
|  | Line | Line to small | Shank | Fluted Part | Shank |  |  |  |  |
|  | A | B | c |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| $\frac{1}{8}$ | 0.343 | $\frac{25}{64}$ | $\frac{11}{32}$ | 1 | 18 | $2 \frac{5}{8}$ | $\frac{1}{2}$ | 年 | 6 |
| $\frac{1}{4}$ | 0.447 | $\frac{9}{16}$ | $\frac{7}{16}$ | 1/8 | 138 | $2 \frac{7}{8}$ | $\frac{9}{16}$ | $\frac{5}{16}$ | 6 |
| $\frac{3}{8}$ | 0.582 | $\frac{9}{16}$ | $\frac{9}{16}$ | 去 | 1\% | $3 \frac{18}{8}$ | 5/8 | $\frac{7}{16}$ | $\sigma$ |
| $\frac{1}{2}$ | 0.721 | $\frac{3}{4}$ | $\frac{3}{4}$ | $1 \frac{1}{2}$ | 2 | $3 \frac{1}{2}$ | $\frac{11}{16}$ | $\frac{9}{16}$ | 8 |
| $\frac{3}{4}$ | 0.931 | $3 / 4$ | $\frac{15}{16}$ | 158 | $2 \frac{1}{4}$ | $3 \frac{7}{8}$ | $\frac{3}{4}$ | . 116 | 8 |
| , | 1.170 | $\frac{15}{16}$ | 1/8 | 13 | $2 \frac{1}{2}$ | $4 \frac{1}{4}$ | $\frac{13}{16}$ | $\frac{13}{16}$ | 10 |
| , 4 | 1.515 | $\frac{31}{32}$ | $1 / 5$ | 188 | $2^{\frac{3}{4}}$ | $4 \frac{5}{8}$ | 1 | 1 | 10 |
| $1 \frac{1}{2}$ | 1.755 | 1 | $1 \frac{1}{2}$ | 2 | 3 | 5 | 188 | 1/8 | 12 |
| 2 | 2.230 | 1 | 1\%8 | $2 \frac{1}{4}$ | $3 \frac{1}{2}$ | $5 \frac{3}{4}$ | 138 | 138 | 12 |
| $2 \frac{1}{2}$ | 2.667 | $1 \frac{1}{2}$ | $2{ }^{\frac{1}{4}}$ | $2 \frac{7}{8}$ | 4 | 678 | 116 | 116 | 14 |
| 3 | 3.292 | 19 | $2{ }^{\frac{5}{8}}$ | $3 \frac{1}{4}$ | $4 \frac{1}{2}$ | $7 \frac{3}{4}$ | $1 / 15$ | 170 | 14 |
| $3 \frac{1}{2}$ | 3.792 | 15 | $2 \frac{13}{16}$ | $3 \frac{5}{8}$ | $4 \frac{9}{10}$ | $8 \frac{3}{16}$ | $2 \frac{1}{8}$ | $2 \frac{1}{8}$ | 16 |
| 4 | 4.292 | 116 | 3 | $3 \frac{3}{4}$ | $4 \frac{5}{8}$ | 88 | $2 \frac{1}{4}$ | $2 \frac{1}{4}$ | 18 |

## STANDARD TAPER PINS AND REAMERS



## DIMENSIONS OF BROWN \＆SHARPE STANDARD TAPERS

| BROWN \＆SHARPE STANDARD TAPERS． |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Length of Keyway． | Length of Tongue． |  |  |  |
|  | D | A | P | H | K | L | T | t | w |  |
| 1 | ． 20 | ． 239 | 9 | $1 \frac{1}{16}$ | $\frac{18}{18}$ | 8 | $\frac{8}{16}$ | $\frac{1}{8}$ | .135 | ． 500 |
| 2 | ． 25 | ． 299 | 9 1 $\frac{8}{16}$ | 115 $\frac{5}{16}$ | 111 | $\frac{1}{2}$ | 4 | $\frac{5}{82}$ | ． 166 | ． 500 |
| 3 | ． 312 | ． 385 | 5 1寊 | 17 | $1 \frac{28}{88}$ | $\frac{5}{8}$ | $\frac{5}{16}$ | $\frac{8}{18}$ | ． 197 | ． 500 |
| 3 | ． 312 | ． 395 | 5 | 218 | $1 \frac{21}{\frac{1}{2}}$ | $\frac{5}{8}$ | $\frac{5}{16}$ | $\frac{8}{16}$ | ． 197 | ． 500 |
| 4 | ． 35 | ． 402 | 2 1 | 1 \％ | 1184 | $\frac{11}{18}$ | $\frac{11}{81}$ | $\frac{7}{88}$ | ． 228 | ． 500 |
| 5 | ． 45 | ． 523 | 3 1星 | 17 | $1 \frac{11}{18}$ | 龧 | 8 | $\frac{1}{4}$ | ． 260 | ． 500 |
| 6 | ． 50 | ． 599 | 9 2\％ | $2 \frac{1}{2}$ | $2 \frac{19}{64}$ | $\frac{4}{8}$ | $\frac{7}{16}$ | $\frac{9}{82}$ | ． 291 | ． 500 |
| 6 | ． 50 | ． 635 | 5 3t | － 3 年 | 311 | $\frac{7}{8}$ | $\frac{7}{16}$ | $\frac{9}{88}$ | ． 291 | ． 500 |
| 7 | ． 60 | ． 725 | 53 | $3 \frac{1}{8}$ | $2 \frac{29}{88}$ | $\frac{18}{18}$ | $\frac{18}{18}$ | $\frac{8}{18}$ | ． 322 | ． 500 |
| 7 | ． 60 | ． 766 | 6 4 | $4 \frac{1}{8}$ | 3登 | $\frac{18}{18}$ | $\frac{15}{8}{ }^{5}$ | $\frac{5}{16}$ | ． 322 | ． 500 |
| 8 | ． 75 | ． 898 | 8 39 ${ }^{\frac{9}{16}}$ | $31 \frac{1}{6}$ | $3{ }^{\frac{8}{64}}$ | 1 | $\frac{1}{2}$ | $\frac{11}{8}$ | ． 353 | ． 500 |
| 9 | ． 90 | 1.066 | 6 － | $4 \frac{1}{8}$ | 3 y | $1 \frac{1}{8}$ | $\frac{9}{16}$ | 8 | ． 385 | ． 500 |
| 10 | 1.0446 | 1.260 | 5 | $5 \frac{1}{8}$ | $4 \frac{27}{83}$ | 18 $\frac{8}{16}$ |  | $\frac{7}{16}$ | ． 447 | ． 5161 |
| 10 | 1.0446 | 1.289 | $95 \frac{11}{18}$ | $5 \frac{18}{18}$ | $5 \frac{17}{88}$ |  | $\frac{21}{81}$ | $\frac{7}{16}$ | ． 447 | ． 5161 |
| 10 | 1.0446 | 1.312 | 2 67 | $6 \frac{11}{8} \frac{1}{2}$ | $6 \frac{1}{16}$ | $1{ }^{\frac{5}{8}}$ | $\frac{81}{88}$ | $\frac{7}{18}$ | ． 447 | ． 5161 |
| 11 | 1.25 | 1.531 | 1 6量 | 6 \％ | $6 \frac{1}{8} \frac{8}{2}$ | $1 \frac{5}{16}$ | $\frac{21}{82}$ | $\frac{7}{16}$ | ． 447 | ． 500 |
| 12 | 1.50 | 1.796 | 6 7 7 | 71 | $6 \frac{1}{1} \frac{6}{6}$ | $1 \frac{1}{2}$ | 4 | $\frac{1}{2}$ | ． 510 | ． 500 |

REAMERS FOR BROWN \& SHARPE STANDARD TAPER SOCKETS

|  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |



DIMENSIONS OF MORSE TAPER SOCKETS


| Dimensions of R.Reamers for Morse Standard Tapers. |  |  |  |  |  |  |  | Dimensions of Reamers for Jarno Tapers. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Finish | $--A$ hing Rea |  |  |  | No. of Jarno | Total Length of |  | Length of | Diam. at Small End, | Diam.at Small End, | Number of |
| No. of Morse Standara Taper | Total Length Length of of Cutting Reamer Edges |  | Length of Shank | Diam. at Diam.at <br> Small Small <br> End, End, <br> Finishing Roughing <br> Reamer Reamer |  | Taper per foot | Number of Flutes | Taper | Reamer | Edge | C | Reamer | Roughing Reamer | Flutes |
|  |  |  | 2 |  |  | $2 \frac{5}{8}$ |  | $13 / 8$ | $1 \frac{1}{4}$ | 0.200 | 0.190 | 4 |
|  |  |  | 3 |  |  | 31/2 |  | 2 | $11 / 2$ | 0.300 | 0.290 | 6 |
|  | $A$ | $B$ |  | $C$ | D |  |  | - E |  | 4 | $43 / 5$ | $25 / 8$ | 13 | 0.400 | 0.390 | 6 |
| 0 | 4 | $2 \frac{1}{2}$ |  | $1 \frac{1}{2}$ | 0.252 |  | 0.242 | 0.625 | 6 | 5 | $5 \frac{1}{4}$ | $3 \frac{1}{4}$ | 2 | 0.500 | 0.490 | 8 |
|  |  |  | 6 |  |  | $57 / 8$ |  |  |  | $3 \frac{3}{4}$ | 21/8 | 0.600 | 0.590 | 8 |
| 1 | $4 \frac{5}{8}$ | $2 \frac{3}{4}$ | 178 | 0.369 | 0.359 | 0.600 | 6 | 7 | 61/2 | $4 \frac{1}{4}$ | $2 \frac{1}{4}$ | 0.700 | 0.690 | 8 |
|  |  |  |  |  |  |  |  | 8 | $73 / 8$ | 478 | 21/2 | 0.800 | 0.790 | 8 |
| 2 | $5 \frac{1}{2}$ | $3 \frac{1}{4}$ | $2 \frac{1}{4}$ | 0.572 | 0.562 | 0.602 | 8 | 9 | 81/8 | $5 \frac{3}{8}$ | $23 / 4$ | 0.900 | 0.890 | 8 |
|  |  |  |  |  |  |  |  | 10 | $87 / 8$ | 6 | 278 | 1.000 | 0.990 | 8 |
| 3 | $6 \frac{5}{8}$ | 4 | $25 / 8$ | 0.778 | 0.768 | 0.602 | 8 | 11 | 91/2 | $6 \frac{12}{2}$ | 3 | 1.100 | 1.090 | 10 |
|  |  |  |  |  |  |  |  | 12 | 101/8 | 7 | 3/8 | 1.200 | 1.190 | 10 |
| 4 | 8 | 5 | 3 | 1.020 | 1.010 | 0.623 | 8 | 13 | $10 \frac{3}{4}$ | 71/2 | $3 \frac{1}{4}$ | 1.300 | 1. 290 | 10 |
|  |  |  |  |  |  |  |  | 14 | $113 / 8$ | 8 | 33/8 | 1.400 | 1.390 | 10 |
| 5 | $9 \frac{1}{2}$ | $6 \frac{1}{8}$ | $3 \frac{3}{8}$ | 1.475 | 1.465 | 0.630 | 10 | 15 | 12 | $81 / 2$ | 312 | 1.500 | 1.490 | 10 |
|  |  |  |  |  |  |  |  | 16 | $125 / 8$ | 9 | $35 / 8$ | 1.600 | 1.590 | 12 |
| 6 | 12 | $8 \frac{1}{4}$ | 3年 | 2.116 | 2.106 | 0.626 | 14 | 17 | $13 \frac{3}{8}$ | 95/8 | $3 \frac{3}{4}$ | 1.700 | 1.690 | 12 |
|  |  |  |  |  |  |  |  | 18 | 14 | $10 \frac{1}{8}$ | 378 | 1.800 | 1.790 | 12 |
| 7 | 15 | $1 /$ | 4 | 2.750 | 2.740 | 0.625 | 16 | 19 | $14 \%$ | 105/8 | 4 | 1.900 | 1.890 | 14 |
|  |  |  |  |  |  |  |  | 20 | $15^{\frac{1}{4}}$ | $11 \frac{18}{8}$ | 4/8 | 2.000 | 1.990 | 14 |

SQUARES ON SHANKS OF REAMERS AND TAPS
Sizes of Squares of Tools Corresponding to certain Shank Diameters



| $\begin{aligned} & \text { Diam.of } \\ & \text { Shank } \end{aligned}$ | square | biam of Shank | square | $\begin{aligned} & \text { Piam.of } \\ & \text { Shank } \end{aligned}$ | square | $\begin{aligned} & \text { Diam. of } \\ & \text { shank } \end{aligned}$ | square | $\begin{aligned} & \text { Diam.of } \\ & \text { shank } \end{aligned}$ | Square | $\begin{aligned} & \text { Diam.of } \\ & \text { shank } \end{aligned}$ | square | $\begin{aligned} & \text { Diam. of } \\ & \text { Shank } \end{aligned}$ | square |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D | 5 | D | 5 | 0 | 5 | D | 5 | D | 5 | D | 5 | D | 5 |
| $\frac{1}{16}$ | $\frac{3}{64}$ | $\frac{27}{64}$ | $\frac{5}{16}$ | $\frac{25}{32}$ | $\frac{19}{32}$ | 194 | $\frac{55}{64}$ | $1 \frac{1}{2}$ | 1/8 | $2 \frac{7}{32}$ | 143 | $2 \frac{15}{16}$ | $2 \frac{13}{64}$ |
| $\frac{5}{64}$ | $\frac{1}{16}$ | $\frac{7}{16}$ | $\frac{21}{64}$ | $\frac{51}{64}$ | $\frac{19}{32}$ | $1 \frac{5}{32}$ | 78 | $1 \frac{17}{32}$ | $1 \frac{5}{32}$ | $2 \frac{1}{4}$ | 1116 | $2 \frac{31}{52}$ | $2 \frac{15}{64}$ |
| $\frac{3}{32}$ | $\frac{5}{64}$ | $\frac{29}{64}$ | $\frac{11}{32}$ | $\frac{13}{16}$ | $\begin{aligned} & 39 \\ & 64 \end{aligned}$ | $11 /$ | $\frac{7}{8}$ | 19 | $1 \frac{11}{64}$ | $2 \frac{9}{32}$ | $1 \frac{23}{32}$ | 3 | $2 \frac{1}{4}$ |
| $\frac{7}{64}$ | $\frac{5}{64}$ | $\frac{15}{32}$ | $\frac{23}{64}$ | $\frac{53}{64}$ | 5 | $1 \frac{3}{16}$ | $\frac{57}{64}$ | 1900 | $1 \frac{13}{64}$ | $2 \frac{5}{16}$ | 147 | $3 \frac{1}{32}$ | $2 \frac{9}{32}$ |
| $\frac{1}{8}$ | $\frac{3}{32}$ | $\frac{31}{64}$ | $\frac{23}{64}$ | $\frac{27}{32}$ | $\frac{41}{64}$ | $1 \frac{13}{64}$ | $\frac{29}{32}$ | 15 | $1 \frac{7}{32}$ | $2 \frac{11}{32}$ | 149 | $3 \frac{1}{16}$ | $2 \frac{19}{64}$ |
| 9 | $\frac{7}{64}$ | $\frac{1}{2}$ | 3 | $\frac{55}{64}$ | $\frac{41}{64}$ | $1 \frac{7}{32}$ | $\frac{59}{64}$ | $1 \frac{21}{32}$ | 1年 | $2 \frac{3}{8}$ | $1{ }^{\frac{25}{32}}$ | $3 \frac{3}{32}$ | $2 \frac{21}{64}$ |
| $\frac{5}{32}$ | $\frac{1}{8}$ | $\frac{33}{64}$ | $\frac{25}{64}$ | 78 | $\frac{21}{32}$ | $1 \frac{15}{64}$ | $\frac{59}{64}$ | 1116 | $1 \frac{17}{64}$ | $2 \frac{13}{32}$ | $1 \frac{13}{16}$ | 3\% | $2 \frac{11}{32}$ |
| $\frac{11}{64}$ | $\frac{18}{8}$ | $\frac{17}{32}$ | $\frac{13}{32}$ | $\frac{57}{64}$ | 43 | $1 \frac{1}{4}$ | $\frac{15}{16}$ | $1{ }^{\frac{25}{32}}$ | $1 \frac{19}{64}$ | 276 | 153 | $3 \frac{5}{32}$ | $2 \frac{3}{8}$ |
| $\frac{3}{16}$ | $\frac{9}{64}$ | $\frac{35}{64}$ | $\frac{13}{32}$ | $\frac{29}{32}$ | $\frac{11}{16}$ | $1 \frac{17}{64}$ | $\frac{61}{64}$ | $1 \frac{3}{4}$ | $1 \frac{5}{16}$ | $2 \frac{15}{32}$ | 155 | $3 \frac{3}{16}$ | 225 |
| $\frac{13}{64}$ | $\frac{5}{32}$ | $\frac{9}{16}$ | $\frac{27}{64}$ | $\frac{59}{64}$ | $\frac{11}{16}$ | 19 | $\frac{31}{32}$ | 125 | $1 \frac{11}{32}$ | $2 \frac{1}{2}$ | $1 \frac{7}{8}$ | $3 \frac{7}{32}$ | $2 \frac{27}{64}$ |
| $\frac{7}{32}$ | $\frac{11}{64}$ | $\frac{37}{64}$ | $\frac{7}{16}$ | $\frac{15}{16}$ | $\frac{45}{64}$ | $1 \frac{19}{64}$ | $\frac{31}{52}$ | $1 \frac{13}{16}$ | $1 \frac{23}{64}$ | $2 \frac{17}{32}$ | $1 \frac{29}{32}$ | 3 年 | $2 \frac{7}{16}$ |
| $\frac{15}{64}$ | $\frac{11}{64}$ | $\frac{19}{32}$ | $\frac{29}{64}$ | $\frac{61}{64}$ | $\frac{23}{52}$ | 15 | $\frac{63}{64}$ | $1 \frac{27}{32}$ | 125 | $2 \frac{9}{16}$ | 159 | $3 \frac{5}{16}$ | $23 \frac{31}{64}$ |
| $\frac{1}{4}$ | $\frac{3}{16}$ | $\frac{39}{64}$ | $-\frac{29}{64}$ | $\frac{31}{32}$ | $\frac{47}{64}$ | $1 \frac{21}{64}$ | 1 | 1\% | $1 \frac{13}{32}$ | $2 \frac{19}{32}$ | $1 \frac{61}{64}$ | 33 | $2 \frac{17}{32}$ |
| $\frac{17}{64}$ | $\frac{13}{64}$ | 5 | $\frac{15}{32}$ | $\frac{63}{64}$ | $\frac{47}{64}$ | 111 | $1 \frac{1}{64}$ | 129 | $1 \frac{7}{16}$ | 25 | $1 \frac{31}{32}$ | $3 \frac{7}{16}$ | $2 \frac{37}{64}$ |
| $\frac{9}{32}$ | $\frac{7}{32}$ | $\frac{41}{64}$ | $\frac{31}{64}$ | 1 | 3 | $1 \frac{23}{64}$ | $1 \frac{1}{64}$ | $1 \frac{15}{16}$ | $1 \frac{29}{64}$ | $2 \frac{21}{32}$ | 2 | $3 \frac{1}{2}$ | 25 |
| $\frac{19}{64}$ | $\frac{7}{32}$ | $\frac{21}{32}$ | $\frac{1}{2}$ | $1 \frac{1}{64}$ | $\frac{49}{64}$ | $1 \frac{3}{8}$ | $1 \frac{1}{32}$ | 131 | $1 \frac{31}{6.4}$ | $2 \frac{11}{16}$ | $2 \frac{1}{64}$ | $3 \frac{1}{16}$ | 285 |
| $\frac{5}{16}$ | $\frac{15}{64}$ | 43 | $\frac{1}{2}$ | $1 \frac{1}{32}$ | $\frac{25}{32}$ | $1 \frac{25}{64}$ | $1 \frac{3}{64}$ | 2 | $1 \frac{1}{2}$ | $22^{\frac{23}{35}}$ | $2 \frac{3}{64}$ | 35 | $2 \frac{23}{32}$ |
| $\frac{21}{64}$ | $\frac{1}{4}$ | $\frac{11}{16}$ | $\frac{33}{64}$ | $1 \frac{3}{64}$ | $\frac{25}{52}$ | $1 \frac{13}{52}$ | $1 \frac{1}{16}$ | $2 \frac{1}{32}$ | $1 \frac{17}{32}$ | $2 \frac{3}{4}$ | $2 \frac{1}{16}$ | 3118 | 249 |
| $\frac{11}{32}$ | $\frac{17}{64}$ | $\frac{45}{64}$ | $\frac{17}{32}$ | $1 / 16$ | $\frac{51}{64}$ | $1 \frac{27}{64}$ | $1 \frac{1}{16}$ | $2 \frac{1}{16}$ | $1, \frac{35}{64}$ | $2 \frac{25}{32}$ | $2 \frac{3}{32}$ | $3 \frac{3}{4}$ | $2 \frac{13}{16}$ |
| $\frac{23}{64}$ | $\frac{17}{64}$ | $\frac{23}{32}$ | $\frac{35}{64}$ | $1 \frac{5}{64}$ | $\frac{13}{16}$ | $1 \frac{7}{16}$ | $1 \frac{5}{64}$ | $2 \frac{3}{32}$ | $1 \frac{37}{64}$ | $2 \frac{13}{16}$ | $2 \frac{7}{64}$ | $3 \frac{13}{16}$ | 25.5 |
| 38 | $\frac{9}{32}$ | $\frac{47}{64}$ | $\frac{35}{64}$ | $1 \frac{3}{32}$ | $\frac{53}{64}$ | $1 \frac{29}{64}$ | $13 \frac{3}{32}$ | 2\% | $1 \frac{19}{32}$ | $2 \frac{27}{32}$ | 298 | $3 \frac{7}{8}$ | $2 \frac{29}{32}$ |
| $\frac{25}{64}$ | $\frac{19}{64}$ | 3 | $\frac{9}{16}$ | $1 \frac{7}{64}$ | $\frac{53}{64}$ | $1 \frac{15}{32}$ | $1 \frac{7}{64}$ | $2 \frac{5}{32}$ | $1 \frac{5}{8}$ | $2 \frac{7}{8}$ | $2^{25}$ | $3 \frac{15}{16}$ | $2 \frac{61}{64}$ |
| $\frac{13}{32}$ | $\frac{5}{16}$ | $\frac{49}{64}$ | $\frac{37}{64}$ | 1/8 | $\frac{27}{52}$ | $1 \frac{31}{64}$ | $1 \frac{7}{64}$ | $2 \frac{3}{16}$ | 141 | $2 \frac{29}{32}$ | $2 \frac{3}{16}$ | 4 | 3 |

sure that the reamer will run true. Referring to the use of the table, it will be seen that in the second column from the right a heading "Constant for finding diameter of recess" is given, the recess being the portion $D$ at the end of the reamer which is turned down below the diameter over the cutting edges. The diameter $H$ is a certain amount less than the diameter $A$ of the reamer, according to the size, and the amount which $H$ is less than $A$ is given in the column referred to. For example, if $A$ is 1 inch, then, according to the table, $A-H$ is $1 / 16$ inch, and hence $H$ is 15/16 inch. In other words, the constant given in this table is subtracted from the diameter of the reamer in order to obtain the diameter of the turned down portion.

The arbor used for driving shell reamers consists of a stem or arbor provided with a collar which is fastened to the arbor by means of a taper pin, as shown. The collar is provided with a key, as already mentioned, which engages into the keyway of the reamer. Precaution must be taken in milling this key or tongue so that it will be exactly in the center of the collar. The same care must, of course, be used when milling the keyway in the mill, which must be exactly in the center in order that the key and keyway may fit properly together. When grinding the outside of the reamer to size it should preferably be ground on an arbor similar to that on which it is to be used. At the front end the corners are slightly rounded as shown. The arbors and driving collars should preferably be made of tool steel and the collars should be hardened. The end of the arbor is provided with a small fiat milled on the shank for the set-screws by which it is clamped in a tool-holder. [MACHINERY, October, 1907, Reamers.]

## Clearance for Reamers

The table on page 7 will be found useful when grinding the clearance on
hand and chucking reamers of various sizes. These clearances were decided upon as giving the best results by experiments extending over a period of over a year, undertaken by the Cincinnati Milling Machine Co., Cincinnati, Ohio. The clearance is ground with a cup wheel three inches in diameter. The figures in the body of the table give the amount in inches which the work-holding centers should be above the toothrest.

In the cases marked I, II, and III the tooth-rest is mounted on the emery wheel head and should be set centrally with the emery wheel spindle. In the case marked IV the tooth-rest is mounted on the table of the machine. By setting the tooth-rest and the work-holding centers as called for by this table the reamers will be provided with clearance of such an amount as to ream the greatest number of smooth holes with the minimum amount of wear. It will be seen that in the table two columns of dimensions for setting the work-holding centers above the tooth-rest, are given for each class of reamer specified, except for the rose chucking reamers. The first of these columns is headed "For cutting clearance," and the second, "For second clearance." The first clearance is that on the actual land of the reamer, while the second clearance is that back of the cutting land. The chucking reamers for cast iron or bronze have 23 -degree beveled ends, and are provided with two clearances along the blades, the same as the hand reamers, but the beveled ends have only one clearance, which is ground by setting the work-holding centers to the figures in the second column under III. Chucking reamers for reaming steel are ground circular to the exact size of the hole to be reamed, and the 45 -degree beveled ends only have clearance, the setting for the grinding of which is given in the table under IV. [MAchinery, June, 1904, Reamer Clearances.]

DIMENSIONS OF CENTERS FOR REAMERS AND ARBORS

## CENTERS FOR REAMERS AND ARBORS.



Formulas:

$$
\text { Arbors to } 1^{\prime \prime} \text { diam. : } B=\frac{1}{2} A ; C=\frac{1}{5} A ; D=\frac{8}{5} A ;
$$

Arbors from $11 / 8^{\prime \prime}$ diam. to $5^{\prime \prime}$ diam. $: B=\frac{1}{2}+\frac{A-1}{8} ; C=.2+\frac{A-1}{20} ; D=.6+\frac{A-1}{6}$.
APPROXIMATE VALUES FOR PRACTICAL USE.

| $\stackrel{A}{\text { Dlam. of }}$ Arbor. | B <br> Largest Dlam. of Center. | C <br> No. of Drill. | Depth of Hole. | A Dlam. of Arbor. | B Largest Dlam. of Center. | C Letter of Drill. | D Depth of Hole. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\pm$ | $\frac{1}{8}$ | 55 | $\frac{8}{82}$ | 27 | $\frac{21}{82}$ | G | $\frac{18}{18}$ |
| - $\frac{5}{16}$ | $\frac{5}{38}$ | 52 | ${ }^{8} 8$ | $2 \frac{8}{8}$ | $\frac{4}{8} \frac{8}{4}$ | H | $\frac{87}{87}$ |
| $\frac{8}{8}$ | $\frac{8}{16}$ | 48 | $\frac{9}{32}$ | $2 \frac{1}{2}$ | $\frac{11}{16}$ | J | $\frac{87}{82}$ |
| ${ }^{3} 8$ | $\frac{7}{88}$ | 43 | $\pm$ | 2 咸 | $\frac{45}{4}$ | K | $\frac{1}{8}$ |
| $\frac{1}{8}$ | $\frac{1}{4}$ | 39 | $\frac{5}{16}$ | 28 | $\frac{98}{88}$ | L | $\frac{88}{88}$ |
| $\frac{2}{16}$ | ${ }^{\frac{8}{88}}$ | 33 | $\frac{11}{32}$ | 27 | $\frac{47}{84}$ | M | $\frac{89}{38}$ |
| 5 | $\frac{8}{16}$ | 30 | $\frac{8}{8}$ | 3 | 8 | N | ${ }_{1}^{15}$ |
| $\frac{11}{18}$ | $\frac{11}{81}$ | 29 | $\frac{18}{88}$ | 31 | $4 \frac{4}{4}$ | N | $\frac{81}{88}$ |
| 4 | ${ }_{8}^{8}$ | 25 | $\frac{7}{16}$ | $3 \frac{1}{4}$ | $\frac{85}{38}$ | 0 | $\frac{8}{81}$ |
| $\frac{1}{1} \frac{8}{8}$ | $\frac{18}{3} \frac{3}{8}$ | 20 | 1 | $3 \frac{3}{8}$ | $\frac{51}{64}$ | O | 1 |
| ${ }_{8}$ | $\frac{7}{16}$ | 17 | $\frac{17}{82}$ | $3 \frac{1}{8}$ | $\frac{1}{18}$ | P | 1 |
| $\frac{1}{15}$ | $\frac{18}{8 \frac{1}{2}}$ | 12 | ${ }^{9} 8$ | 3 3 | 88 84 88 | Q | $1{ }_{16}^{16}$ |
| 1 | $\frac{1}{2}$ | 8 | $\frac{1}{8} \frac{1}{2}$ | $3 \frac{8}{4}$ | $\frac{87}{82}$ | R | $1 \frac{1}{16}$ |
| $1 \frac{1}{8}$ | $\frac{88}{64}$ | 5 | - | $3 \frac{7}{8}$ | ${ }^{\frac{85}{65}}$ | R | 11/6 |
| $1 \frac{1}{4}$ | $\frac{17}{82}$ | 3 | $\frac{21}{82}$ | 4 | $\frac{9}{8}$ | S | $1 \frac{1}{8}$ |
| $1 \frac{8}{8}$ | $\frac{88}{68}$ | 2 | $\frac{21}{8 \frac{1}{2}}$ | $4 \frac{1}{8}$ | $\frac{8}{67}$ | T | 118 |
| $1 \frac{1}{8}$ | $\frac{9}{18}$ | 1 | $\frac{11}{18}$ | $4 \frac{1}{4}$ | $\frac{99}{88}$ | T | $1 \frac{18}{8}$ |
|  |  | Letter. |  | 4 용 | $\frac{59}{64}$ | U | $1 \frac{8}{16}$ |
| 15 | $\frac{87}{64}$ | A | $\frac{28}{88}$ | $4 \frac{1}{2}$ | $\frac{18}{16}$ | V | $1 \frac{8}{18}$ |
| $1{ }^{\frac{8}{4}}$ | $\frac{1}{8} \frac{19}{2}$ | B |  | $4 \frac{5}{8}$ | 81 | V | 118 |
| $1 \frac{7}{3}$ | $\frac{8}{69}$ | C | $\frac{8}{4}$ | $4 \frac{8}{4}$ | $\frac{81}{88}$ | W | 1. |
| 2 | \% | E | 4 | $4 \frac{7}{8}$ |  | X | 11 |
| $2 \frac{1}{8}$ | 84 | F | $\frac{88}{88}$ | 5 | 1 | X | 14 |

## DIMENSIONS OF TWIST DRILLS－I

| $\begin{aligned} & \text { L } \\ & \text { x } \\ & \text { E } \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { rè } \\ & \text { oे } \\ & \text { oे } \\ & \text { م̀ } \\ & A \end{aligned}$ |  | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 8 \\ & 8 \\ & 8 \end{aligned}$ | $\begin{aligned} & x y \\ & x \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 1 \\ & \text { o } \\ & \text { ह } \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { co } \\ & \text { ob } \\ & 0 \\ & \text { o } \\ & \text { A } \\ & A \end{aligned}$ |  | $\begin{aligned} & 0 . \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | x 0 0 0 0 0 0 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{1}{4}$ | $6 \frac{1}{2}$ | 4\％ | 1 | 13 | $1 \frac{11}{16}$ | $15 \frac{1}{8}$ | 105 | 4 | $11 \frac{13}{16}$ |
| $\frac{5}{16}$ | 67 | 43 | 1 | $2 \frac{3}{16}$ | $1 \frac{3}{4}$ | 15 $\frac{1}{2}$ | 10\％ | 4 | 12年 |
| 3. | $7 \frac{1}{4}$ | $4 \frac{11}{16}$ | 1 | $2 \frac{5}{8}$ | $1 \frac{13}{16}$ | 15\％ | $11 \frac{3}{16}$ | 4 | $12 \frac{11}{16}$ |
| $\frac{7}{16}$ | 758 | $4 \frac{15}{16}$ | 1 | $3 \frac{1}{16}$ | 178 | 164 | $11 \frac{7}{16}$ | 4 | $13 \frac{1}{8}$ |
| $\frac{1}{2}$ | 8 | $5 \frac{1}{4}$ | 1. | $3 \frac{1}{2}$ | $1 \frac{15}{16}$ | 165 | $11 \frac{3}{4}$ | 4 | $13 \frac{9}{16}$ |
| $\frac{9}{16}$ | $8 \frac{3}{8}$ | $5 \frac{1}{2}$ | 1 | $3 \frac{15}{16}$ | 2 | 17. | 12 | 4 | 14 |
| $5 / 8$ | － $8 \frac{3}{4}$ | 513 | 2 | $4 \frac{3}{8}$ | $2 \frac{1}{16}$ | 174 | $12 \frac{3}{16}$ | 5 | $14 \frac{7}{16}$ |
| $\frac{11}{16}$ | 918 | $6 \frac{1}{16}$ | 2 | $4 \frac{13}{16}$ | 218 | $17 \frac{1}{2}$ | $12 \frac{3}{8}$ | 5 | $14 \%$ |
| 3 | $9 \frac{1}{2}$ | $6 \frac{3}{8}$ | 2 | $5 \frac{1}{4}$ | $2 \frac{3}{16}$ | $17 \frac{3}{4}$ | 12.9 | 5 | $15^{\frac{5}{16}}$ |
| $\frac{13}{16}$ | 97 | 65／8 | 2 | $5 \frac{11}{16}$ | $2 \frac{1}{4}$ | 18 | $12 \frac{3}{4}$ | 5 | $15 \frac{3}{4}$ |
| 78 | 1014 | $6 \frac{15}{16}$ | 2 | 6\％ | $2 \frac{5}{16}$ | $18 \frac{1}{4}$ | $12 \frac{15}{16}$ | 5 | $16 \frac{3}{16}$ |
| $\frac{15}{16}$ | 1058 | $7 \frac{3}{16}$ | 3 | $6 \frac{9}{16}$ | $2 \frac{3}{8}$ | $18 \frac{1}{2}$ | 131／8 | 5 | $16 \frac{5}{8}$ |
| 1 | 11. | $7 \frac{1}{2}$ | 3 | 7 | $2 \frac{7}{16}$ | $18 \frac{3}{4}$ | $13 \frac{5}{16}$ | 5 | $17 \frac{1}{16}$ |
| $1 \frac{1}{16}$ | 1138 | $7 \frac{3}{4}$ | 3 | $7 \frac{7}{16}$ | $2 \frac{1}{2}$ | 19 | $13 \frac{1}{2}$ | 5 | $17 \frac{1}{2}$ |
| 1／8 | 113 | $8 \frac{1}{16}$ | 3 | $7 \frac{7}{8}$ | $2 \frac{9}{16}$ | 194 | $13 \frac{11}{16}$ | 5 | $17 \frac{15}{16}$ |
| $1 \frac{3}{16}$ | 12\％ | $8 \frac{3}{8}$ | 3 | $8 \frac{5}{16}$ | 25 | 19\％ | $13 \%$ | 5 | $18 \frac{3}{8}$ |
| 1／4 | 12 $\frac{1}{2}$ | 85 | 3 | 83 | $2 \frac{11}{16}$ | $19 \frac{3}{4}$ | $14 \frac{1}{16}$ | 5 | $18 \frac{13}{16}$ |
| $1 \frac{5}{16}$ | 12\％ | $8 \frac{15}{16}$ | 4 | 916 | $2 \frac{3}{4}$ | 20 | 14年 | 5 | 19年 |
| $13 / 8$ | $13 \frac{1}{4}$ | $9 \frac{3}{16}$ | 4 | 95 | $2 \frac{13}{16}$ | $2.0 \frac{1}{4}$ | $14 \frac{7}{16}$ | 5 | $19 \frac{11}{16}$ |
| $1 \frac{7}{16}$ | $13 \frac{5}{8}$ | $9 \frac{1}{2}$ | 4 | $10 \frac{1}{16}$ | 2\％ | 20\％$\frac{1}{2}$ | 145／8 | 5 | 20\％ |
| $1 \frac{1}{2}$ | 14 | $9 \frac{3}{4}$ | 4 | $10 \frac{1}{2}$ | $2 \frac{15}{16}$ | $20 \frac{3}{4}$ | $14 \frac{13}{16}$ | 5 | 20916 |
| $1 \frac{9}{16}$ | $1.4 \frac{3}{8}$ | 1016 | 4 | $10 \frac{15}{16}$ | 3 | 21 | 15 | 5 | 21 |
| 15 | $14 \frac{3}{4}$ | $10 \frac{5}{16}$ | 4 | $11 \frac{3}{8}$ |  |  |  |  |  |


| $\begin{array}{ll}  & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 \end{array}$ | $\left\lvert\, \begin{gathered} -100 \\ M \end{gathered}\right.$ | $\left\lvert\, \begin{gathered} m i o \\ \infty \end{gathered}\right.$ | $\left\lvert\, \begin{gathered} -v \\ -w \end{gathered}\right.$ | $\begin{aligned} & \text { hio } \\ & 0 \end{aligned}$ | $\underset{\sim}{m i c}$ | Nos | －10y | 910 | $\left\lvert\, \begin{gathered} 600 \\ 0 \end{gathered}\right.$ | $\underset{\sim}{2}$ | miv | $\underset{2}{20}$ | Nó $\sim$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\left\|\begin{array}{cc} 5 & 0 \\ 0 & x \\ 0 & 0 \\ 5 & 0 \\ 0 & 0 \\ v & 0 \end{array}\right\| \infty$ | $\stackrel{\text { Mio }}{\nabla}$ | $\stackrel{M 10}{\gamma}$ | $\stackrel{N}{\gamma}$ | $\underset{\sim}{x}$ | $\underset{i n}{x}$ | $\underset{\nabla}{910}$ | $\stackrel{610}{8}$ | $\left\|\begin{array}{c} 4,0 \\ \nabla \end{array}\right\|$ | $\geq 10$ | $\|\stackrel{\text { miv }}{\forall}\|$ | $\underset{\gamma}{90}$ | $\frac{910}{7}$ | $\stackrel{N 0}{*}$ |
|  | $\frac{910}{6}$ | $\begin{gathered} n \\ 0 \\ 0 \end{gathered}$ | $\frac{20}{6}$ | $\checkmark$ | $\stackrel{-10}{1}$ | -10 | $-10$ | mio | $-N$ | hie | $\underset{i}{m 00}$ | $\xrightarrow{\text { N }}$ | ${ }^{104}$ |
|  | $\begin{aligned} & N \\ & 0 \\ & \text { m } \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0^{\circ} \end{aligned}$ | $\begin{aligned} & m \\ & N \\ & m \\ & 0 \end{aligned}$ | $\begin{gathered} \text { N } \\ m \\ m \\ 0 \end{gathered}$ | $\begin{aligned} & 9 \\ & m \\ & m \\ & 0 \end{aligned}$ | $\begin{aligned} & \infty \\ & \alpha \\ & m \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \infty \\ & b^{2} \\ & m \\ & 0 \end{aligned}$ | $\begin{aligned} & \infty \\ & 0 \\ & m \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & \infty \\ & m \\ & 0 \end{aligned}$ | $\begin{aligned} & n \\ & 0 \\ & m \\ & 0 \end{aligned}$ | $\begin{aligned} & \nabla \\ & 8 \\ & \nabla \\ & 0 \end{aligned}$ | 3 $\vdots$ 0 |
|  | ＜ | 0 | $Q$ | $\sigma$ | 0 | $\emptyset$ | N | ১ | $>$ | $\pm$ | $x$ | $\lambda$ | N |
| $\begin{array}{rr} 2 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{array}$ | 610 | 三－10 | 三19 | が | Miv | 9 | N10 | N0 | $1 \times$ | 20 | $20$ | N | －10 |
| $\left\|\begin{array}{cc} x & 0 \\ 0 & 0 \\ 5 & 0 \\ j & 0 \\ v & 0 \end{array}\right\| \infty$ | $\left\lvert\, \frac{10}{\gamma}\right.$ | $-\frac{10}{8}$ | $\frac{-10}{8}$ | $\stackrel{-10}{\nabla}$ | $\underset{\nabla}{-10}$ | $\stackrel{m, 10}{\gamma}$ | $\frac{m i o}{\gamma}$ | $\left\|\frac{m i g}{\nabla}\right\|$ | $\underset{~}{-1}$ | $\underset{\sim}{\alpha}$ | $\stackrel{-1 \nabla}{\nabla}$ | $\frac{610}{\sigma}$ | $\frac{b 10}{x}$ |
|  | $9$ | $10$ | $\left\lvert\, \begin{gathered} \mathrm{M} \\ 10 \end{gathered}\right.$ | $\left\|\begin{array}{c} -10 \\ 6 \end{array}\right\|$ | $\left\lvert\, \begin{gathered} -104 \\ 0 \end{gathered}\right.$ | $0$ | $0$ | $\begin{gathered} 600 \\ 6 \end{gathered}$ | $\begin{gathered} 600 \\ 6 \end{gathered}$ | $\left\lvert\, \begin{gathered} -10 \\ 6 \end{gathered}\right.$ | $=10$ | $\underset{0}{m i t}$ | $\mathrm{mit}_{0}$ |
| $\left\|\begin{array}{ll} \frac{0}{0} & 9 \\ \frac{0}{0} & 2 \\ 5 & 5 \\ 0 & 5 \\ 0 & 5 \end{array}\right\| 0$ | $\begin{aligned} & 7 \\ & m \\ & N \\ & 0 \end{aligned}$ | $\begin{aligned} & \infty \\ & \underset{\sim}{N} \\ & \underset{\sim}{1} \end{aligned}$ | $\begin{aligned} & N \\ & \underset{\sim}{N} \\ & 0 \end{aligned}$ | $\begin{aligned} & \bullet \\ & \underset{\sim}{\sim} \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0 \\ & i \\ & \sim \\ & 0 \end{aligned}$ | $\begin{aligned} & \hat{N} \\ & \underset{\sim}{n} \\ & 0 \end{aligned}$ | $\begin{aligned} & \overline{0} \\ & \underset{N}{2} \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & \sim \\ & 0 \end{aligned}$ | $\begin{aligned} & N \\ & N \\ & \\ & 0 \end{aligned}$ | $\begin{aligned} & N \\ & N \\ & \text { N } \\ & \hline \end{aligned}$ | $\begin{gathered} \infty \\ \underset{\sim}{n} \\ 0 \end{gathered}$ | $\begin{aligned} & 0 \\ & 0 \\ & \mathrm{~N} \\ & 0 \end{aligned}$ | 6 0 $N$ 0 |
|  | V | $\infty$ | $\cup$ | 0 | 4 | 4 | $\checkmark$ | さ | $\cdots$ | ＞ | $t$ | $V$ | $₹$ |

DIMENSIONS OF TWIST DRILLS—III

| $\begin{array}{c\|} \hline \text { No. of } \\ \text { Stee/Wire } \\ \text { Gage } \end{array}$ | Diam. in Inches D | $\begin{array}{\|c\|} \hline \text { Total } \\ \text { Length } \\ \hline \end{array}$ | $\begin{gathered} \begin{array}{c} \text { Length of } \\ \text { Groove } \end{array} \\ \hline B \\ \hline \end{gathered}$ | $\begin{gathered} \text { Lead } \\ \text { of } \\ \text { Grooves } \end{gathered}$ | No. of SteelWire Gage | $\begin{gathered} \text { Diam. in } \\ \text { Inches } \\ \hline D \\ \hline \end{gathered}$ | $\begin{gathered} \text { Total } \\ \text { Length } \\ A \end{gathered}$ | $\begin{gathered} \begin{array}{c} \text { Length of } \\ \text { Groove } \end{array} \\ \hline B \end{gathered}$ | $\begin{gathered} \text { Lead } \\ \text { of } \\ \text { of } \\ \text { Grooves } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.2280 | 4 | $2 \frac{3}{4}$ | 15 | 31 | 0.1200 | $2 \frac{13}{16}$ | $1 \frac{9}{16}$ | $\frac{13}{16}$ |
| 2 | . 2210 | 315 | 2116 | 19 | 32 | .1160 | $2 \frac{3}{4}$ | $1 \frac{1}{2}$ | $\frac{13}{16}$ |
| 3 | . 2130 | 37 | $2 \frac{5}{8}$ | $1 \frac{1}{2}$ | 33 | .1130 | 23 | $1 \frac{1}{2}$ | $\frac{13}{16}$ |
| 4 | . 2090 | $3 \frac{13}{16}$ | $2 \frac{9}{16}$ | 17 | 34 | .1110 | $2 \frac{3}{4}$ | $1 \frac{1}{2}$ | $3 / 4$ |
| 5 | . 2055 | $3 \frac{3}{4}$ | $2 \frac{1}{2}$ | 176 | 35 | .1100 | $2 \frac{11}{16}$ | 17 | $3 / 4$ |
| 6 | . 2040 | $3 \frac{3}{4}$ | $2 \frac{1}{2}$ | $1 \frac{7}{16}$ | 36 | . 11065 | $2 \frac{11}{16}$ | 17 | $\frac{3}{4}$ |
| 7 | .20,10 | $3 \frac{3}{4}$. | $2 \frac{1}{2}$ | 1.76 | 37 | . 1040 | $2 \frac{5}{8}$ | 138 | $\frac{3}{4}$ |
| 8 | . 1990 | 3117 | 27 | 138 | 38 | . 1015 | 2588 | 138 | $\frac{11}{16}$ |
| 9 | . 1960 | 3118 | $27 \frac{7}{16}$ | 138 | 39 | . 0995 | $2 \frac{9}{16}$ | $1{ }^{5}$ | $\frac{11}{16}$ |
| 10 | . 1935 | 3 5/8 | $2 \frac{3}{8}$ | 138 | 40 | . 0980 | $2 \frac{16}{16}$ | 15 | $\frac{11}{16}$ |
| 11 | . 1910 | $35 / 8$ | $2 \frac{3}{8}$ | $1 \frac{5}{16}$ | 41 | . 0960 | $2 \frac{3}{8}$ | $1{ }^{3}$ | $\frac{11}{16}$ |
| 12 | 1.890 | $3 \frac{9}{16}$ | $2 \frac{5}{15}$ | $1 \frac{5}{16}$ | 42 | . 0935 | $2 \frac{5}{16}$ | $1 \frac{3}{16}$ | 58 |
| 13 | . 1850 | 39 16 | $2 \frac{5}{16}$ | $1{ }^{5}$ | 43 | . 0890 | $2 \frac{1}{4}$ | 1/8 | 5/8 |
| 14 | . 1820 | $3 \frac{1}{2}$ | $2 \frac{1}{4}$ | 1/4 | 44 | . 0860 | $2 \frac{1}{4}$ | $1 \%$ | $5 / 8$ |
| 15 | . 1800 | $3 \frac{1}{2}$ | 2年 | 1年 | 45 | . 0820 | $2 \frac{3}{16}$ | $1 \frac{1}{16}$ | $\frac{9}{16}$ |
| 16 | . 1770 | $3 \frac{7}{16}$ | $2 \frac{3}{16}$ | 1/4 | 46 | . 0810 | $2 \frac{3}{16}$ | $1 \frac{1}{16}$ | $\frac{9}{16}$ |
| 17 | . 1730 | $3 \frac{3}{8}$ | 218 | $1 \frac{3}{16}$ | 47. | . 0.785 | 218 | $1 \frac{1}{16}$ | $\frac{9}{16}$ |
| 18 | . 1695 | 33/8 | 218 | $1 \frac{3}{16}$ | 48 | . 0760 | 218 | 1 | . 16 |
| 19 | . 1660 | $3 \frac{5}{16}$ | $2 \frac{1}{16}$ | $1 \frac{3}{16}$ | 49 | . 0730 | $2 \frac{1}{16}$ | 1 | $\frac{1}{2}$ |
| 20 | . 1610 | 314 | 2 | 1/8 | 50 | . 0700 | 2 | $\frac{15}{16}$ | $\frac{1}{2}$ |
| 21 | . 1590 | $3 \frac{1}{4}$ | 2 | 1/8 | 51 | . 0670 | 2 | $\frac{15}{16}$ | $\frac{1}{2}$ |
| 22 | . 1570 | $3 \frac{1}{4}$ | 2 | 1/8 | 52 | . 0635 | $1 \frac{15}{16}$ | 78 | $\frac{7}{16}$ |
| 23 | . 1540 | $3 \frac{3}{16}$ | $1 \frac{15}{15}$ | $1 \frac{1}{16}$ | 53 | . 0595 | 18 | 78 | $\frac{7}{16}$ |
| 24 | . 1520 | $3 \frac{3}{16}$ | $1 \frac{15}{16}$ | $1 \frac{1}{16}$ | 54 | . 0550 | $1 \%$ | $\frac{13}{16}$ | 3/8 |
| 25 | . 1495 | 31/8 | 178 | $1 \frac{1}{16}$ | 55 | . 0520 | $1 \frac{13}{16}$ | $3 / 4$ | 3/8 |
| 26 | . 1470 | 3/8 | 178 | 1 | 56 | . 0465 | $13 / 4$ | $\frac{11}{16}$ | $\frac{5}{16}$ |
| 27 | . 1440 | 316 | $1 \frac{13}{16}$ | 1 | 57 | . 0430 | 111 | $\frac{11}{16}$ | $\frac{5}{16}$ |
| 28 | . 1405 | $3 \frac{1}{16}$ | $1 \frac{13}{16}$ | 1 | 58 | . 0420 | $1 \frac{11}{16}$ | $\frac{11}{16}$ | $\frac{5}{16}$ |
| 29. | . 1360 | 3 | 13 | $\frac{15}{16}$ | 59 | . 0410 | 111 | $\frac{11}{16}$ | $\frac{5}{16}$ |
| 30 | . 1285 | $2 \frac{15}{16}$ | 116 | $7 / 8$ | 60 | . 0400 | 1110 | $5 / 8$ | $\frac{5}{16}$ |

WIRE GAGES

| $\begin{aligned} & x \\ & 0 \\ & 0 \\ & 0 \\ & 10 \\ & 0 \\ & 0 \\ & 0 \\ & 5 \\ & 8 \\ & 8 \end{aligned}$ |  |  |  |  | $\begin{aligned} & 5 \\ & 5 \\ & 5 \\ & 50 \\ & \text { 20 } \\ & 5 \\ & 5 \end{aligned}$ | $\begin{aligned} & 0 \\ & i \\ & 5 \\ & i \\ & 6 \\ & 5 \\ & 5 \end{aligned}$ | $\begin{aligned} & 0 \\ & 1 \\ & 0 \\ & 0 \\ & 50 \\ & 50 \\ & 0 \\ & 40 \\ & 40 \\ & 0 \end{aligned}$ |  |  |  | $\begin{array}{ll} 0 & 0 \\ 5 & 0 \\ 5 & 0 \\ 5 & 5 \\ 0 & 5 \\ 5 & 0 \\ 5 & 8 \end{array}$ |  | $\begin{aligned} & 5 \\ & 5 \\ & 50^{\circ} \\ & \text { so } \\ & \text { s } \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & i n \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 5 \end{aligned}$ | $\begin{aligned} & \text { U.S. Standard } \\ & \text { for Plate } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 000000 | - | - | - | - | - | 0.464 | 0.4688 | 18 | 0.0403 | 0.049 | 0.0475 | 0.168 | 0.0450 | 0.0480 | 0.0500 |
| 00000 | - | - | - | - | 0.450 | . 432 | . 4375 | 19 | . 0359 | . 042 | . 0410 | . 164 | . 0400 | . 0400 | . 0438 |
| 0000 | 0.4600 | 0.454 | 0.3938 | - | . 400 | . 400 | . 4063 | 20 | . 0320 | . 035 | . 0348 | . 161 | . 0350 | . 0360 | . 0375 |
| 000 | . 4096 | . 425 | . 3625 | - | .360 | . 372 | . 3750 | 21 | . 0285 | . 032 | .0318 | . 157 | . 0310 | . 0320 | . 0344 |
| 00 | . 3648 | . 380 | . 3310 | - | . 330 | . 348 | . 3438 | 22 | . 0253 | . 028 | . 0286 | . 155 | . 0280 | . 0280 | .0313 |
| 0 | . 3249 | . 340 | . 3065 | - | . 305 | . 324 | . 3125 | 23 | . 0226 | . 025 | . 0258 | . 153 | . 0250 | . 0240 | . 0281 |
| 1 | . 2893 | . 300 | . 2830 | 0.227 | 285 | . 300 | .2813 | 24 | . 0201 | . 022 | . 0230 | . 151 | . 0222 | . 0222 | . 0250 |
| 2 | . 2576 | . 284 | . 2625 | . 219 | . 265 | . 276 | . 2656 | 25 | . 0179 | . 020 | . 0204 | . 148 | . 0200 | . 0200 | . 0219 |
| 3 | . 2294 | . 259 | . 2437 | . 212 | . 245 | . 252 | . 2500 | 26 | . 0159 | . 018 | . 0181 | . 146 | :0180 | . 0180 | . 0188 |
| 4 | . 2043 | . 238 | . 2253 | . 207 | 225 | . 232 | . 2344 | 27 | . 0142 | . 016 | . 0173 | . 143 | . 0170 | . 0164 | . 0172 |
| 5 | . 1819 | . 220 | . 2070 | . 204 | . 205 | . 212 | . 2188 | 28 | . 0126 | . 014 | . 0162 | . 139 | . 0160 | . 0149 | . 0156 |
| 6 | 1620 | . 203 | . 1920 | . 201 | . 190 | . 192 | .2031. | 29. | .0113 | . 013 | . 0150 | . 134 | . 0150 | . 0136 | . 0141 |
| 7 | . 1443 | . 180 | . 1770 | . 199 | . 175 | . 176 | . 1875 | 30 | . 0100 | . 012 | . 0140 | . 127 | . 0140 | . 0124 | . 0125 |
| 8 | . 1285 | . 165 | . 1620 | . 197 | . 160 | . 160 | . 1719 | 31. | . 0089 | . 010 | .0132 | . 120 | . 0130 | . 0116 | . 0109 |
| 9 | . 1144 | . 148 | . 1483 | . 194 | . 145 | . 144 | . 1563 | 32 | . 0080 | . 009 | . 0128 | .115 | . 0120 | . 0108 | . 0102 |
| 10 | . 1019 | .134 | . 1350 | . 191 | . 130 | .128 | . 1406 | 33. | . 0071 | . 008 | . 0118 | .112 | . 0110 | 0100 | . 0094 |
| 11 | . 0907 | . 120 | . 1205 | . 188 | . 1175 | . 116 | . 1250 | 34 | . 0063 | . 007 | . 0104 | :110 | . 0100 | . 0092 | . 0086 |
| 12 | . 0808 | . 109 | . 1055 | . 185 | . 105 | . 104 | . 1094 | 35 | . 0056 | . 005 | . 0095 | . 108 | . 0095 | . 0084 | . 0078 |
| 13 | . 0720 | . 095 | .0915 | . 182 | . 0925 | . 092 | . 0938 | 36 | . 0050 | . 004 | . 0090 | . 106 | . 0090 | . 0076 | . 0070 |
| 14 | . 0641 | . 083 | . 0800 | . 180 | . 080 | . 080 | . 0781 | 37 | . 0045 | - | - | . 103 | . 0085 | . 0068 | . 0066 |
| 15 | . 0571 | . 072 | . 0720 | . 178 | . 070 | . 072 | . 0703 | 38 | . 0040 | - | - | .101 | . 0080 | . 0060 | . 0063 |
| 16 | . 0508 | . 065 | . 0625 | . 175 | . 061 | . 064 | .0,625 | 39 | . 0035 | - | - | . 099 | . 0075 | . 0052 | - |
| 17 | . 0453 | . 058 | . 0540 | . 172 | . 0525 | . 056 | . 0563 | 40 | . 0031 | - | - | . 097 | . 0070 | . 0048 |  |

American Gage: Standard for sheet brass, copper or German silver, and for wire of the some material. Birmingham Gage: For soft iron wire or rods.
Washburn \& Moen Gage: Used for iron or copper telegraph and telephone wire.
Stubs'Steel Wire Gage: For Stubs'drill rads. Not same as Stubs'Iron Wire Gage.
U.S.Standard Gage: Recognized as standard for sheet iron and steel.

## Pipe Reamers

Dimensions of pipe reamers are given on page 8. These reamers are used to precede pipe taps. They are made of the same sizes as pipe taps, except that the dimensions of the pipe reamer correspond to the root diameter of the thread of the pipe taps, the taper being, of course, the same, or $3 / 4$ inch per foot. The small end of pipe reamers is slightly chamfered in order to facilitate the entering of the reamer in holes which are of about the same size as the small diameter of the reamer. [Machinery, December, 1907, Reamers.]

## Dimensions of Taper Pin Reamers

Dimensions of taper pin reamers are given on page 9. These reamers are intended for reaming holes for standard taper pins, the dimensions of which are given on the same page. These pins are made of various lengths, and the length specified in the table is the maximum length of each size. The pins and reamers taper one-fourth inch per foot. The diameter at the small end of the reamer should be made to such a dimension that the reamer will project at least $1 / 16$ inch, or on the larger sizes * $1 / 8$ inch, through the hole reamed for the longest standard taper pin of the size to which it corresponds. The length of the cutting edges should also be enough longer than the longest pin to permit the reamer to be ground a number of times without it becoming too small in diameter at the upper end of the flutes for the size of pin for which it is intended. The length of the square on the end of the shank should be about $11 / 2$ times the diameter of the shank, and the size of the square should be $3 / 4$ the diameter of the shank. The exact diameter of the shank portion, of course, is of little importance, it being usually turned down a slight amount below the diameter at the large end of the fluted portion of the reamer. [MAchinery, November, 1907, Reamers;

December, 1909, Errors in Grinding Taper Reamers.]

Sockets and Taper Reamers for Brown \& Sharpe Standard Tapers
On page 10 are given the dimensions of the various Brown \& Sharpe standard tapers. As will be seen from the table, the taper is $1 / 2$ inch per foot in all cases, except for taper No. 10, which has a taper of 0.5161 inch per foot. It will be observed that in certain cases there are several different lengths corresponding to the same number of taper, all the tapers of the same number, however, being of the same diameter at the small end. While the lengths of the taper shanks thus are different, the reamers, the dimensions for which are specified on page 11, can all be made the same for the same number of taper, inasmuch as the diameter at the small end is the same. The only thing necessary to consider is to make the length of the cutting edges of the reamers long enough for the longest or deepest taper socket of a given size, in which case they, of course, will be sufficient for the shorter lengths. The Brown \& Sharpe taper shanks are used mostly on shank end mills and T-slot cutters, as well as on several other tools for the machines manufactured by the Brown \& Sharpe Mfg. Co. The sizes of the taper sockets have been carried up to No. 12 only, larger sizes being seldom used. As will be seen on page 11, dimensions are given for the diameters at the small end both for roughing and finishing reamers, the roughing reamer being in all cases 0.010 inch smaller in diameter than the finishing reamer. [Machinery, November, 1907, Reamers; December, 1909, Errors in Grinding Taper Reamers.]

## Sockets and Taper Reamers for Morse Standard Tapers

On page 12 dimensions are given for Morse standard tapers, and on page 14 dimensions for the reamers for reaming these taper sockets. As shown on page
(Continued on page 26.)

Diameter Thickness
American or B. \& S.
Birmingham or Stubbs
American Screw Gage
Steel Music Wire
Wire Gage
Drills
Letter Drill
Gage
Diameter
 Thickness
American or B. \& S.
N:
Birmingham
or Stubbs
American
Screw Gage

Steel Music
Wire


Wire Gage Drills

Letter Drill
Gage

| 0000000000000000000000000000000000000000 <br>  <br>  <br> ê： <br> ャ <br> $\underset{\sim}{\sim}$ <br> $\stackrel{\infty}{\infty}$ <br> $\omega$ ： <br> is <br>  | Diameter Thickness <br> American or B．\＆S． <br> Birmingham or Stubbs <br> American Screw Gage <br> Steel Music Wire <br> Wire Gage Drills <br> Letter Drill Gage |
| :---: | :---: |
|  <br>  $\qquad$ <br> cr： <br> $\rightarrow$ <br> $\infty$ ： <br> co <br> ๒： <br> 占：上 <br> ©： <br> $\infty$ <br> a： <br> os： <br> cr <br>  | Diameter or Thickness <br> American or B．\＆S． <br> Birmingham or Stubbs <br> American Screw Gage <br> Steel Music Wire <br> Wire Gage Drills <br> Letter Drill Gage |



|  <br>  <br>  <br> N $\square$ co is: <br> er <br> os <br> $\stackrel{\omega}{\infty}$ : <br> ッ <br> ↔. | Diameter or Thickness <br> American or B. \& S. <br> Birminghar or Stubbs <br> American Screw Gag <br> Steel Musi Wire <br> Wire Gage Drills <br> Letter Dril Gage |
| :---: | :---: |
|  | Diameter or Thickness <br> American or B. \& S. <br> Birminghar or Stubbs <br> American Screw Gag <br> Steel Musi Wire <br> Wire Gage Drills <br> Letter Dril Gage |

14, both a finishing reamer and roughing reamer are used, the latter being provided with a spiral groove cut like a thread all around the cutting edges, as shown in the top view. This thread or groove breaks up the chips in the same manner as the nicks in the cutting edges of plain "nicked" milling cutters. The thread is cut left-hand with a tool similar to a square threading tool, but having the corners slightly rounded. The width of the tool should vary from about $1 / 32$ inch for the smallest size reamer for Morse taper sockets to $3 / 32$ inch for the largest sizes, the depth of the groove being a little more than half the width of the tool. The pitch of the thread should be about $1 / 5$ inch for the smallest size, increasing up to $1 / 3$ inch for the largest sizes. On page 13 are given dimensions of Morse standard taper sockots with a Morse taper both on the inside and outside. [Machinery, November, 1907, Reamers.]

## Taper Reamers for Jarno Standard Tapers

On page 14 are given dimensions for the reamers for Jarno tapers. The Jarno taper was originally proposed by Mr. Oscar J. Beale of the Brown \& Sharpe Mfg. Co. The taper per foot of all the Jarno tapers is 0.600 inch on the diameter. All the dimensions necessary for Jarno tapers are determined by the number of the taper. The diameter at the large end of the taper is as many eighths, the diameter at the small end of the taper as many tenths, and the length of the taper between the large and small diameter as many half inches as is expressed by the number of the taper. For example, the No. 7 Jarno taper is $7 / 8$ inch in diameter at the large end, $7 / 10$ or 0.7 inch in diameter at the small end, and the length is $7 / 2$ inches or $31 / 2$ inches. [Machinery, November, 1907, Reamers.]
Squares on Shanks of Reamers and Taps
On page 15 a table is given by means of which the proper size of square cor-
responding to a given diameter of shank can be seen at a glance. If the diameter of the shank $D$, for example, is $19 / 64$ inch, then we find directly from the table that the square $S$ should be $55 / 64$ inch across flats. The table, extending from $1 / 16$ inch up to 4 inches, covers the whole range ordinarily met with in the machine shop. The size of the square is, on an average, $3 / 4$ times the diameter of the shank.

## Centers for Reamers and Arbors

On page 17 a table of well proportioned reamer and arbor centers is given, together with the general formulas by means of which the dimensions are determined. These centers are laid out so as to be large enough for heavy duty. Care should be exercised in drilling the hole $C$ so that it is of the full depth $D$, and when countersinking care should be taken not to exceed the diameter $B$.

## Dimensions of Twist Drills

On pages 18,19 and 20 are given dimensions for twist drills. The first table gives the dimensions for drills from $1 / 4$ inch up to 3 inches in diameter, the second for the so-called letter-size drills, and the third for steel wire gage drills, from No. 1 down to No. 60 steel wire gage. Referring first to the table for drills from $1 / 4$ - to 3 -inch size, the dimensions provided give the total length and the length of the fluted portion on straight shank drills, the size of shank of Morse taper shank drills, and the lead of spiral of the grooves or flutes. In order to establish uniformity in regard to the total lengths, taper shank and straight shank drills ought to be made of the same total lengths. As the length of the taper shank always must be its regular standard length, dimensions are not given for the lengths of the grooved parts on taper shank drills, as these lengths will, when the total length is given, depend entirely upon
(Continued on page 29.)

NUMBER OF TEETH AND KEYWAYS IN MILLING CUTTERS

| Number of Teeth and Lead of Spiral of Plain Milling Cutters.$\begin{aligned} \text { No. of Teeth } & =\frac{5 \times \text { Diam. }+24}{2} \\ \text { Lead of Spiral } & =9 \times \text { Diam. }+4 \end{aligned}$ |  |  |  |  |  | Number of Teeth in Side Milling Cutters. <br> No. of teeth $=3.1$ Diam. +11 . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diam. of Cutter | Number of Teeth | Lead of Spiral of Teeth, Inches | Diam. of Cutter | Number Lead of <br> of <br> Spiral <br> Teeth <br> of Teeth, <br> Inches |  | Diam. of Cutter <br> 2 | Number of Teeth$18$ |  | Diam. ofCutter | Number of Teeth |
|  |  |  |  |  |  | 28 |  |  |  |
| 2 | 16 | 22 | $5 \frac{1}{2}$ | 26 | $53 \frac{1}{2}$ |  | $2 \frac{1}{4}$ | 18 |  | 6 | 30 |
| $2 \frac{1}{4}$ | 18 | 24年 | 6 | 26 | 58 | $2 \frac{1}{2}$ | 18 |  | $6 \frac{1}{2}$ | 32 |
| $2 \frac{1}{2}$ | 18 | $2.6 \frac{1}{2}$ | $6 \frac{1}{2}$ | 28 | $62 \frac{1}{2}$ | 23 | 20 |  | 7 | 32 |
| 23 | 1.8 | $28 \frac{3}{4}$ | 7 | 30 | - 67 | 3 | 20 |  | $7 \frac{1}{2}$ | 34 |
| 3 | 20 | 31 | $7 \frac{1}{2}$ | 30 | $71 \frac{1}{2}$ |  |  |  |  |  |
| $3 \frac{1}{2}$ | 20 | $35 \frac{1}{2}$ | 8 | 32 | 76 | $3 \frac{1}{2}$ | 22 |  | 8 | 36 |
| 4 | 22 | 40. | 9 | 34 | 45 | 4 | 24 |  | 9 | 38 |
| $4 \frac{1}{2}$ | 24. | $44 \frac{1}{2} 1$ | 10 | 36 | 94 | $4 \frac{1}{2}$ | 24 |  | 10 | 42 |
| 5 | 24 | 49 |  |  |  | 5 | 26 |  |  |  |
| Standard Keyways for Milling Cutfers.-Square. |  |  |  |  |  | Standard Keyways for Milling Cutters.-Halfround. |  |  |  |  |
| $\begin{array}{r} D=\operatorname{Dia} \\ \text { Hols } \end{array}$ | am. of le | A = Width of Keyway | $\begin{array}{l\|l\|l\|} \hline h & B=D e p t h & C=\text { Radius } \\ \text { ay of Keyway of Coiners } \\ \hline \end{array}$ |  |  | $\begin{aligned} & D= \text { Diami. of } \\ & \text { Hole } \end{aligned}$ |  | $A=$ width of  <br> Keyway $B=$ Depth of <br> Keyway  |  |  |
| $\frac{3}{8}$ to | $\frac{9}{16}$ inch | $\frac{3}{32}$ |  | $\frac{3}{4}$ | 0.020 | $\frac{3}{8}$ to $\frac{5}{8}$ inch |  | 1/8 |  | $\frac{1}{16}$ |
| 5 s to | 7 \% inch | 1/8 |  | $\frac{1}{16}$ | 0.030 | $\frac{11}{16}$ to. $\frac{13}{16}$ inch |  |  | $\frac{3}{16}$ | $\frac{3}{32}$ |
| $\frac{15}{16}$ to | $1 \frac{1}{8}$ inch | $\frac{5}{32}$ |  | 5 | 0.035 | $\frac{78}{8}$ tol $\frac{3}{16}$ inch |  |  | $1 / 4$ | $1 / 8$ |
| $1 \frac{3}{16}$ to. 1 | $1 \frac{3}{8}$ inch | $\frac{3}{16}$ |  | $\frac{3}{32}$ | 0.040 | $1 \frac{1}{4}$ to $1 \frac{7}{16}$ inch |  |  | $\frac{5}{16}$ | $\frac{5}{32}$ |
| $1 \frac{7}{16}$ to | $1 \frac{3}{4}$ inch | $1 / 4$ |  | $1 / 8$ | 0.050 | $1 \frac{1}{2}$ to 2 inch |  |  | $3 / 8$ | $\frac{3}{16}$ |
| $1 \frac{13}{16}$ to | 2 inch | $\frac{5}{16}$ |  | $\frac{5}{32}$ | 0.060 | $2 \frac{1}{16}$ to $2 \frac{7}{16}$ inch |  |  | $\frac{7}{16}$ | $\frac{7}{32}$ |
| $2 \frac{1}{16}$ to | $2 \frac{1}{2}$ inch | $3 / 8$ |  | $\frac{3}{16}$ | 0.060 | $2 \frac{1}{2}$ to 3 inch |  |  | $\frac{1}{2}$ | $1 / 4$ |
| $2 \frac{9}{16}$ to 3 inch |  | $\frac{7}{16}$ |  | $\frac{3}{16}$ | 0.060 | 22 - |  |  |  |  |

DIMENSIONS OF END MILLS

|  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diam. | Length of Cut | Length of Neck | $\begin{aligned} & \text { Diam. of } \\ & \text { End Reces } \end{aligned}$ | Morse Tap End | er Shank Mills | Brown \& Shank | arpe Taper d. Mills | Number |
| A | $B$ | C | D | No. of Morse Taper | $\begin{gathered} \text { Total } \\ \text { Lengoth } \\ \hline \end{gathered}$ | $\begin{aligned} & \text { No. of } \\ & \text { B. \& S. } \\ & \text { Toper } \end{aligned}$ | $\begin{aligned} & \text { Total } \\ & \text { Length } \end{aligned}$ | of Flutes |
| $\frac{1}{4}$ | $3 / 4$ | $1 / 4$ | $5 / 64$ | 1 | 39/16 | 4 | $23 / 8$ | 5 |
| $1 / 4$ | $3 / 4$ | 5/16 | $5 / 64$ | - | - | 5 | $2^{15 / 6}$ | 5 |
| 5/6 | 7/8 | $1 / 4$ | 3/32 | 1 | 311/6 | 4 | $21 / 2$ | 5 |
| 5/16 | 7/8 | 5/16 | 3/32 | - | - | 5 | 31/6 | 5 |
| 3/8 | $7 / 8$ | $1 / 4$ | 1/8 | 1 | $3^{11} / 6$ | 4 | 21/2 | 6 |
| 3/8 | $7 / 8$ | 5/16 | 1/8 | - | - | 5 | $3!16$ | 6. |
| $7 / 16$ | 1 | $1 / 4$ | 3/16 | 1 | $3^{13 / 16}$ | 4 | $25 / 8$ | 6 |
| $7 / 16$ | 1 | 5/16 | 3/16 | 2 | $43 / 8$ | 5 | $3 \frac{3}{16}$ | 6 |
| 1/2 | 118 | 5/6 | $1 / 4$ | 1 | 4 | 5 | 35/16 | 6 |
| $1 / 2$ | 118 | 3/8 | $1 / 4$ | 2 | 49/16 | 7 | $5^{1 / 8}$ | 6 |
| 9/16 | $1 \frac{1}{4}$ | 5/16 | $1 / 4$ | 1 | $41 / 8$ | 5 | 37/16 | 6 |
| $9 / 16$ | $1 \frac{1}{4}$ | 3/8 | $1 / 4$ | 2 | $4^{1 / 16}$. | 7 | $5^{\frac{1}{4}}$ | 6 |
| 5/8 | 138 | 5/16 | $1 / 4$ | - | - | 5 | 39/16 | 7 |
| 5/8 | $13 / 8$ | 3/8 | $1 / 4$ | 2 | $4^{13 / 16}$ | 7 | $53 / 8$ | 7 |
| $11 / 6$ | $1 / 2$ | 3/8 | $1 / 4$ | 2 | $4^{15 / 16}$ | 7 | $5^{1 / 2}$ | 7 |
| 11/6 | $1 / 2$ | 1/2. | $1 / 4$ | - | - | 9 | $63 / 4$ | 7. |
| $3 / 4$ | $15 / 8$ | 3/8 | 5/16 | 2 | 51/6 | 7 | $5 \frac{5}{8}$ | 7 |
| 3/4 | $15 / 8$ | $1 / 2$ | $5 / 16$ | 3 | 57/8 | 9 | 67/8 | 7 |
| 7/8 | $13 / 4$ | 3/8 | $3 / 8$ | 2 | 53/15 | 7. | $5^{3 / 4}$ | 8 |
| 718 | $13 / 4$ | $1 / 2$ | 3/8 | 3 | 6 | 9 | 7 | 8 |
| 1 | $17 / 8$ | 3/8 | 3/8 | 2 | 5//6 | . 7 | 5\%/8 | 8 |
| 1 | 178 | 1/2 | 3/8 | 3 | 618 | 9 | 7\% | 8 |
| 118 | 2 | 3/8 | 7/16 | - | - | 7 | 6 | 9 |
| $1 \frac{18}{}$ | 2 | $1 / 2$ | 7/16 | 3 | $6 \frac{1}{4}$ | 9 | 714 | 9 |
| 1/4 | 2 | 1/2 | 1/2 | 3 | 614. | 7 | 618 | 9 |
| $1 / 4$ | 2 | 1/2 | $1 / 2$ | 4 | $71 /$ | 9 | $7 \frac{1}{4}$ | 9 |
| $13 / 8$ | 21/8 | 1/2 | 5/8 | 3 | 63/8 | 9 | $73 / 8$ | 10 |
| $13 / 8$ | 21/8 | $1 / 2$ | 5/8 | 4 | $73 / 8$ | - | - | 10 |
| $11 / 2$ | 214 | 1/2 | 3/4 | 3 | $6 \frac{1}{2}$ | 9 | $71 / 2$ | 10 |
| $11 / 2$ | 21/4 | 1/2 | 3/4 | 4 | $71 / 2$ | - | - | 10 |
| $15 / 8$ | $2^{1 / 4}$ | $1 / 2$ | 13,16 | 4 | $71 / 2$ | 9 | 71/2 | 10 |
| $13 / 4$ | 23/8 | 1/2 | $7 / 8$ | 4 | $75 / 8$ | 9 | $75 / 8$ | 11 |
| 178 | $2^{1 / 2}$ | $1 / 2$ | 15/16 | 4 | $73 / 4$ | 11 | $93 / 4$ | 11 |
| 2 | $2^{1 / 2}$ | 1/2 | 1 | 4 | $73 / 4$ | 11 | $93 / 4$ | 11 |

the length of the standard taper used. It is obvious that after the length of the taper shank is deducted from the total length and provision has been made for a short "neck" between the taper shank and the grooved part, the remaining portion will be the fluted length. The lead of the flutes or grooves is 7 times the diameter of the drill. In the case of the letter-size and steel wire gage drills no taper shanks are specified, as drills of these sizes are almost exclusively provided with straight shanks. The letter-size drills over $1 / 4$ inch in diameter, however, may be provided with a No. 1 Morse taper shank if required. [Machinery, August, 1905, Proportions of Twist Drills.]

## Wire Gages

On page 21 is given a table by means of which the dimensions in inches may be found for given wire and plate gage numbers. The table includes all the commonly used gages. On pages 23,24 and 25 a set of tables is given by means of which the corresponding number of any wire gage may be easily found when the dimension in inches is known. These tables are, in a measure, a reversal of the table on page 21, and all the tables may profitably be used in conjunction with each other. The explanatory note on page 25 illustrates more fully the use of these tables.

## Plain and Side Milling Cutters

On page 27 are given the number of teeth and the lead of spiral for plain milling cutters of diameters from 2 to 10 inches. Cutters with the width of face greater than 4 inches should preferably be made in two or more interlocking sections. Cutters larger than 5 inches in diameter should preferably be made with inserted teeth, in which case, of course, the number of teeth cannot be as large as that given in the table. A 6 -inch inserted blade cutter should not have more than about 12 teeth; an 8 inch, 16 teeth; and a 10 -inch, 18 teeth.

The number of teeth to be used in side milling cutters is somewhat greater than that used in plain milling cutters, as shown in the table to the right on page 27. On the same page tables of standard keyways to be used in milling cutters, and as adopted by leading milling cutter manufacturers, are given. In case of the square keyway shown to the left, care should be taken to have the corners at $C$ well rounded to the radius specified. The half-round keyway is preferable, as there is less likelihood of a crack starting, as is often the case at the corner of the square keyway. [MAchinery, April, 1906, Milling Cutters.]

## Dimensions of End Mills

Dimensions of end mills provided with a solid taper shank are given on page 28. The teeth on the cylindrical surface are usually cut straight, but may also be cut on a spiral. The amount of the spiral should not exceed 20 degrees. The direction of spiral should be left-hand for right-hand end mills, and vice versa, especially if the mill is to be used for cutting both with its end and with its side. If the mill is to be used exclusively as an end mill, cutting only with the teeth on its extreme end, then the spiral on a righthand end mill should preferably be right-hand, because in that case it is possible to give the teeth a positive front rake. Solid shank end mills are commonly provided with either Brown \& Sharpe or Morse taper shank. In the table of these mills, columns are given for both, and in some cases two numbers of shanks are specified for the same size of mill, indicating that in usual practice the mills in question may be provided with either of the two shanks. The numbers of shanks given, and the dimensions in general correspond to the practice of prominent end mill manufacturers. The total length, of course, differs according to the number of taper shank used, as indicated.

## DIMENSIONS OF SHELL END MILLS

|  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

DIMENSIONS OF ARBORS FOR SHELL END MILLS


SETTING ANGLES FOR MILLING ANGULAR CUTTERS-I
In Fig. 1, the line $O A$ is the axis of a cone which would
result from prolonging the blank down to a point. The line
$O C$ is the intersection of the two planes which form the sides
of the tooth space, and hence the cutter must run parallel
to this line while cutting a space. The head must then be
elevated so that the line $O C$ is parallel with the table, and
in doing so we will have turned it through an angle equal to
$A O C$ or $a$. Line $E F$ is drawn perpendicular to oc.
From the figure,

SETTING ANGLES FOR MILLING ANGULAR CUTTERS－II

ANOLNB OF ELEVATION FOR END MILLE．

| ¢¢ ${ }^{\text {¢ }}$ | Angle of Cutter． |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 穴安 | 85 | 80 | 75 | 70 | 65 | 60 | 53 | 50 |
| 5 | $74^{\circ} 23^{\prime}$ | $57^{\circ} 8^{\prime}$ | $84^{\circ} 27^{\prime}$ |  |  |  |  |  |
| 6 | 8117 | 7213 | 6221 | $\bigcirc$ | $36^{\circ} 8^{\circ}$ |  |  |  |
| 7 | 8342 | 7713 | 7022 | 6250 | 5412 | $43^{\circ} 36^{\prime}$ |  |  |
| 8 | 8459 | $79 \quad 51$ | 7427 | 6839 | 6212 | 5444 | 44 ${ }^{\circ}{ }^{\circ} 7^{\prime}$ | $32^{\circ} \mathrm{J} 7^{\prime}$ |
| 9 | 8547 | 8129 | 770 | 7213 | 6658 | 611 | 541 | 4515 |
| 10 | 8621 | 8288 | 7846 | 7440 | 7012 | 6512 | 5925 | 5226 |
| 11 | 8647 | 8329 | 80 5 | ${ }^{7} 768$ | 72 84， | 6813 | 6315 | 5722 |
| ． 12 | 876 | 849 | 816 | 7752 | 7423 | 70 32 | 66 | $61 \sim$ |
| 18 | 8722 | 8144 | 8154 | 7859 | 7548 | 7221 | 6826 | 6352 |
| 14 | 8785 | 858 | 8285 | 7954 | 771 | 7351 | 7017 | 6610 |
| 15 | 8746 | 8530 | 839 | 8040 | 781 | 756 | 7150 | 684 |
| 16 | 8755 | 8549 | 8338 | 8120 | 7852 | 7610 | 738 | 69 40， |
| 17 | $88 \quad 3$ | 865 | 848 | 8153 | 7986 | 77： 4 | 7415 | $\mathrm{T}_{7} 11^{\prime}$ |
| 18 | 8811 | 8619 | 8424 | 8223 | 8014 | 7752 | 7514 | 7213 |
| 19 | 8817 | 8632 | 8443 | 8249 | 8047 | 7884 | 766 | 7815 |
| 20 | 8822 | 8643 | 850 | $8318{ }^{\text {² }}$ | 8117 | 7911 | 7651 | 7411 |
| 21 | 8827 | 8653 | 8515 | 8383 | 8144 | 7944 | 7781 | 7459 |
| 22 | 8832 | 872 | 8529 | $83 \quad 52$ | 828 | 8014 | 788 | 7544 |
| 23 | 8836 | 8710 | 8542 | 849 | 8880 | 8042 | 7841 | 7624 |
| 24 | 8839 | 8718 | 8553 | 8424 | 8249 | 81.6 | 7911 | 770 |

ANGLES OF RLTVATION FOR 5 DEGREE BLANK．

| ¢ | Angle of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| そ\％ | 90 | 85 | 80 | 75 | 70 | 65 | 60 | 65 | 80 |
| 5 | $74^{\circ} 12$ | $89^{\circ} 11^{\prime}$ | $42^{\circ} 48^{\prime}$ | $21^{\circ} 41^{\prime}$ |  |  |  |  |  |
| 6 | 804 | 7129 | 62． 34 | 5858 | $41^{\circ} 41^{\prime}$ | $27^{\circ} 22^{\prime}$ |  |  |  |
| 7 | 821 | 7547 | 6922 | 6235 | 55 | 4683 | $36^{\circ} 12^{\prime}$ | $21^{\circ} 86^{\prime}$ |  |
| 8 | 8257 | 7758 | 7252 | 6732 | 6147 | 5523 | $48 \quad 0$ | 3856 | $25^{\circ} 40^{\prime}$ |
| 9 | 8329 | 7918 | $75 \quad 2$ | 7035 | 6549 | 6086 | 5443 | 4746 | 3880 |
| 10 | $83 \quad 50$ | 8013 | 7631 | 7241 | 68 35 | 649 | 5911 | 5327 | 464 |
| 11 | $84 \quad 4$ | 8052 | 7786 | 7412 | 7037 | 6643 | 6224 | 5728 | 5115 |
| 12 | 8414 | 8121 | $78 \quad 25$ | 7523 | $72 \quad 10$ | 6842 | 6452 | 0031 | $55 \quad 5$ |
| 13 | 8421 | 8144 | 79 | 7618 | 7823 | 7015 | 6648 | 6： 54 | 58 |
| 14 | 8427 | 828 | 7936 | 774 | 7424 | 7132 | 6823 | 6450 | 6028 |
| 15. | 8482 | 8219 | 80 | 7643 | 7515 | 7280 | 6942 | 6627 | 6228 |
| 16 | 8435 | 8231 | 8025 | 7814 | $75 \quad 57$ | 7330 | 7049 | 6748 | $64 \quad 7$ |
| 17 | 8438 | 8242 | 8044 | 7842 | 7684 | 7416 | 7146 | 6858 | 6538 |
| 18 | 8441 | 8252 | 81.1 | $79 \quad 7$ | 77 | 7457 | 7236 | 6959 | 6647 |
| 19 | 8448 | 830 | 81.16 | 7928 | 7734 | 7533 | 7320 | 7052 | 6742 |
| 20 | 8445 | 838 | 8129 | 7947 | 7759 | 76 | 7859 | $71 \quad 39$ | 0850 |
| 21 | 8446 | 8314 | 8140 | $80 \quad 3$ | 7721 | 7632 | 7433 | 72． 20 | 6940 |
| 22 | 8447 | 8319 | 8150 | $80 \quad 17$ | 7840 | 7657 | 75 | 7258 | 7026 |
| 23 | 8448 | 8324 | 8159 | 8030 | 7858 | 7720 | 7532 | 7882 | 717 |
| 24 | 8449 | 8329 | 827 | 8043 | 7915 | 7740 | 7557 | $74 \quad 3$ | 7144 |

ANGLES OF ELEVATION FOR IO DEGREE BLANK．

|  | Angle of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \％ | 90 | 85 | 80 | 75 | \％0 | 65 | － 60 | 55 | 50 |
| 5 | $60^{\circ} 16$ | $46^{\circ} 45^{\prime}$ | $32^{\circ} 9$ | $14^{\circ} 81$ |  |  |  |  |  |
| $f$ | 7034 | 6211 | 5350 | 4437 | $34^{\circ}{ }^{\prime}$ | $20^{\circ} 57^{\prime}$ |  |  |  |
| 7 | 7412 | 68 | 6155 | 5520 | 48 | 3957 | $30^{\circ} 2^{\prime}$ | $16^{\circ} 82$ |  |
| 8 |  | 718 | $6^{611} 9$ | 6056 | 5519 | 49 | 4156 | ${ }^{33} 12$ | ${ }_{33}^{20^{\circ} 39^{\prime}}$ |
| 10 | $\begin{array}{ll}77 & 2 \\ 72\end{array}$ | 7256 | 6845 | ［6463 <br> 68 <br> 64 | 5921 |  | 48 58 58 82 | 426 | $338$ |
| 10 11 | 77 78 78 18 | 748 | $\begin{array}{ll}70 & 81 \\ 71 & 48\end{array}$ | 6644 63.28 | 62 64 48 | ［ 5722 | 53 $\begin{aligned} & 58 \\ & 56 \\ & 58\end{aligned}$ | ${ }^{47} 54$ | 4042 4556 |
| 12 | 7880 | 7540 | 7248 | 6947 | 6637 | 6312 | 5926 | 5510 | 4950 |
| 18 | 7844 | 769 | 7831 | 7048 | 6756 | 6451 | 6126 | 5736 | 5251 |
| 14 | 78 56 | 7684 | 749 | 7139 | 692 | 6812 | 63 | 5936 | 5518 |
| 15 | 795 | 7654 | 7440 | 7221 | 6956 | 6719 | 6428 | 6115 | 5720 |
| 16 | 7912 | 7710 | 755 | 7257 | 7041 | 6816 | 6537 | 6238 |  |
| 17 | 7918 | 7723 | 7527 | 7327 | 7120 | 69． 4 | 6636 | 6351 | 6028 |
| 18 | 7922 | 7784 | 7545 | 7352 | 7153 | 6946 | 6727 | 6458 | 6148 |
| 19 | 7926 | 7744 | 761 | 7415 | 7228 | 7023 | 6812 | 6546 | 6248 |
| 20 | 7980 | 7754 | 7616 | 7435 | 7244 | 7056 | 6852 | 6634 | 6347 |
| 21 | 7938 | 78 | 7629 | 7453 | 7312 | 7125 | 6928 | 6717 | 6488 |
| 22 | 7985 | 788 | 7640 | 75 | 7333 | 7151 | 6959 | 6755 | 6525 |
| 23. | 7937 | ¢8 18 | 7650 | 7523 | 7852 | 7214 | 7028 | 6829 |  |
| 24 | 7989 | 7820 | 7659 | 7580 | 74 | 7235 | 7054 |  | 66 |

ANOLES＇OF ELEVATION FOR 15 DEGRER BLANE．

|  | Angle of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| z\％ | 90 | 85 | 80 | 75 | \％ 0 | 65 | 60 | 85 | 50 |
| 5 | $49^{\circ} 4^{\circ}$ | $37^{\circ} 8^{\prime}$ | $24^{\text {c }} 52$ | $10^{\circ} 38^{\prime}$ |  |  |  |  |  |
| 6 | 61.49 | $54 \quad 9$ | 4612 | 3740 | $28^{\circ} 4$ | 16.96 |  |  |  |
| 7 | 6644 | $60 \quad 57$ | 551 | 4845 | 4157 | 3414 | $25^{\circ} 2^{\prime}$ | $12{ }^{\circ} 57$ |  |
| 8 | 6915 | 6483 | 5946 | \＄4 44 | 4921 | 4324 | 8634 | 2821 | $17^{\circ} 34^{\prime}$ |
| 9 | 7043 | 6645 | 6241 | 5828 | 5358 | 498 | 4330 | 372 | 294 |
| 10 | 7140 | 6812 | 6441 | 61， 1 | 578 | 5255 | 4812 | 4247 | 3618 |
| 11 | 7220 | 6916 | 668 | 6254 | $59 \quad 27$ | 5544 | 5137 | 4686 | 4124 |
| 12 | 72.48 | 70． 2 | $6{ }^{7} 13$ | 6418 | 6113 | 5754 | 5414 | 50 | 4513 |
| 13 | 7310 | $70 \quad 39$ | $68 \quad 5$ | $65 \quad 26$ | 6238 | 5937 | 56 18 | 5284 | 4814 |
| 14 | 7326 | 717 | 6846 | 6620 | 6346 | 610 | 5759 | 5435 | 5038 |
| 15 | 7839 | 7130 | 6920 | 675 | 6442 | 6210 | 592 ？ | 5615 | $52 \cdot 39$ |
| 16 | 73． 50 | 7150 | 6949 | 6743 | 6530 | 63 | 6033 | 5740 | 5420 |
| 17 | 7388 | 720 | 7012 | 6814 | 6611 | 6358 | 61.33 | 5851 | 5546 |
| 18 | 74 | 7220 | 7088 | ． 6842 | 6646 | 6441 | $62 \quad 26$ | 5954 | 570 |
| 19 | 7411 | 7232 | 7051 | 696 | 6717 | $65 \quad 19$ | 6311 | 6049 |  |
| 20 | 7416 | 7242 | 716 | 6928 | 6744 | 6553 | 6852 | 6187 | 59 |
| 21 | 7420 | 7251 | 7120 | 6946 | $68 \quad 7$ | 6622 | 6427 | ． 6220 | 5954 |
| 22 | 7424 | 7259 | 7132 | $70 \cdot 3$ | 6829 | 6649 | 650 | 6259 | 6040 |
| 23 | $74 \quad 27$ | 736 | 7143 | 70 18 | $6849^{\prime}$ | 6713 | 6529 | 63.83 | 6122 |
| 24 | 7430 | 7312 | 7153 | 7032 | 69 6 | 6735 | 6556 | $64 \quad 5$ | 6159 |

ANGLES OF ELEVATION FOR 20 DEGREE BLANK．

| ¢5 | Angle of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $2{ }^{2}$ | 90 | 85 | 80 | 75 | 70 | 65 | 60 | 65 | 80 |
| 5 | $40^{\circ} 20^{\prime}$ | $30^{\circ} 4$ | $19^{\circ} 46^{\prime}$ | $8^{\circ} 4^{\prime}$ |  |  |  |  |  |
| 6 | 5357 | 4655 | 3939 | 3155 | $23^{\circ} 18^{\prime}$ | $13^{\circ} 11$ |  |  |  |
| 7 | 5943 | 5417 | 4842 | 4251 | 3630 | 2923 | $21^{\circ} 1^{\prime}$ | $10^{\circ} 23^{\prime}$ |  |
| 8 | 62.46 | 5818 | 5345 | 4859 | 4353 | 3816 | 3158 | 2416 | $14^{\circ} 31$ |
| 9 | 6435 | 6047 | 5654 | 5252 | 4834 | 4383 | 8838 | 8282 | 255 |
| 10 | 6547 | 6228 | 59 | 5538 | 51.50 | 4747 | 4318 | ＇88 9 | 321 |
| 11 | 6686 | 6389 | 60.38 | 5730 | 5412 | 5038 | 4611 | 4212 | $36 \quad 56$ |
| 12 | 6712 | 6432 | 6149 | $59 \quad 0$ | $56 \quad 2$ | 52.50 | 4918 | 4.519 | 4040 |
| 18 | 6739 | $65 \quad 13$ | 6244 | 6011 | 5728 | 5484 | 5122 | 4747 | 4336 |
| 14 | 68． 0 | 6546 | 6329 | 618 | 58.89 | 5559 | 53 4 | 4947 | 46 |
| 15 | 6817 | 6613 | $64 \quad 3$ | 6155 | 5938 | 5710 | 5428 | 5127 | 4758 |
| 16 | 6830 | 6684 | 6436 | 6234 | 60． 26 | 58 | 5589 | L2 51 | 4938 |
| 17 | 6841 | 6653 | 65 | 63 8 8 | 618 | $\begin{array}{ll}59 & 0\end{array}$ | 5640 | 548 | 514 |
| 18 | $68 \quad 50$ | 678 | $65 \quad 24$ | 6387 | 6144 | 5944 | 5732 | 55 | 5217 |
| 19 | 9857 | 6721 | 6543 | $64 \quad 2$ | 6215 | 6022 | 5818 | 5559 | 3321 |
| 20 | 698 | 67.32 | 6559 | 6423 | 6243 | 6055 | 5858 | 5647 | 54 18 |
| 21 | 60.9 | 67.42 | 6614 | 6442 | 638 | 6125 | 5934 | 5780 | 559 |
| 22 | 69.14 | 6751 | 66.28 | 6459 | 6380 | 61.52 | 607 | 589 | 55 55 |
| 23 | 6918 | 6759 | $\begin{array}{lll}66 & 39\end{array}$ | 6.515 | 6350 | 62 16 | 6086 | 5844 | 5636 |
| 24 | 6021 | $68 \quad 5$ | 6649 | 65.30 | $64 \quad 7$ | 6288 | 612 | 5914 | 5712 |

ANOLES OF ELEVATION FOR 25 DEOREE BLANK．

| \％${ }^{\text {¢ }}$ | Angle of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Z ${ }^{\text {\％}}$ | 90 | 85 | 80 | 75 | 70 | 65 | 60 | 55 | 50 |
| 5 | $33^{\circ} 32^{\prime}$ | $25^{\circ} 0$ | $16^{\circ} 5^{\prime}$ | $6^{\circ} 27^{\prime}$ |  |  |  |  |  |
| 6 | $47 \quad 0$ | 4088 | $34 \quad 0$ | 2710 | $19^{\circ} 38$ | $10^{\circ}{ }^{\circ} 8^{\prime}$ |  |  |  |
| 7 | 5312 | 4910 | 430 | 3785 | 3143 | 2517 | $17^{\circ} 44^{\prime}$ | $8^{p} 31$ |  |
| 8 | 5636 | 5225 | 488 | 4340 | 3855 | 3341 | 2747 | $20^{\circ} 50$ | $11^{\circ} 33^{\prime}$ |
| 9 | 5840 | 55 | 5124 | 4786 | 4338 | 398 | 8418 | 2838 | 2115 |
| 10 | 602 | 5653 | 5340 | 5021 | 4647 | $42: 8$ | 3843 | 8253 | 2747. |
| 11 | $61 \quad 0$ | 5811 | 5518 | 5220 | 4912 | ． 4548 | 424 | 8749 | 5282 |
| 12 | 61 42 | 59 9 | 5638 | 5352 | 512 | 4759 | 4438 | 40 है। | 3610 |
| 18 | 6214 | 5954 | 5732 | $\begin{array}{ll}55 & 5\end{array}$ | 5230 | 4944 | 46． 41 | 4815 | 892 |
| 14 | 6288 | 6029 | 5819 | $\begin{array}{ll}56 & 3\end{array}$ | 5841 | 518 | 4820 | 4512 | 4122 |
| 15 | 6257 | 610 | 5857 | 5652 | 5489 | 5218 | 4948 | 4650 | 4818 |
| 10 | 68.13 | 6122 | 5929 | 5782 | 5529 | ${ }_{58}^{517}$ | 5058 | 4818 | 4457 |
| 17 | 6326 | 6142 | 5954 | 58 | 5611 | 54 8 | 5154 | 4923 | 4621 |
| 18 | 6387 | 8159 | 6019 | 5836 | 5648 | 5452 | 5246 | 5025 | 4734 |
| 19 | 6346 | 6213 | 6038 | 511 | 5720 | 5580 | 5381 | 5119 | 4838 |
| 20 | 6383 | 6225 | 6056 | 5923 | 5747 | 56 5 | 5411 | 526 | 4983 |
| 21 | 6359 | 6236 | 6111 | 5943 | 5811 | 5634 | 5447 | 5248 | 5023 |
| 23 | $64 \quad 5$ | 6246 | 6125 | 60） 1 | 5834 | 57.1 | 5519 | 5326 | 519 |
| 23 | 6410 | 625.5 | 6137 | 60.17 | 5854 | 5725 | 5548 | 54 | 5150 |
| 24 | 6414 | 63 3 | 6147 | 6081 | 5912 | 5746 | 5613 | 54.80 | 5226 |

ANGLDI OF HLEVATION FOR BO DEGRE1 BLANRE．

|  | Angle of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 言 | 90 | 85 | 80 | 75 | 70 | 65 | 60 | BS | so |
| 5 | $28^{\circ} 9$ | $20^{\circ} 51$ | $18^{\circ} 17$ |  |  |  |  |  |  |
| 6 | 4054 |  |  |  |  |  |  |  |  |
| 7 | 4712 50 46 | 4835 46 48 | 87 42 42 58 | 82.56 <br> 88 <br> 17 | $\begin{aligned} & 17 \\ & 27 \\ & 88 \end{aligned}$ | 21 <br> 29 <br> 48 <br> 8 | $15^{\circ}$ 24 12 |  |  |
| $\begin{aligned} & 8 \\ & 9 \end{aligned}$ | ［1046 | 4658 4988 | $\begin{array}{ll}42 & 55 \\ 4618\end{array}$ | 88 42 40 | 34 24 | 2986 84 48 | 2412 80 14 | 1755 | $10^{\circ} 14^{\prime}$ 18 |
| 10 | 5429 | 5131 | 4830 | 45.22 | 428 | 38.29 | 3481 | 30 | 2444 |
| 11 | 5582 | 5258 | 5010 | 4722 | 4425 | 4118 | 3743 | 8845 | 298 |
| 12 | 5618 | 5358 | 5128 | 4854 | 4614 | 4821 | 4012 | 3688 | 8238 |
| 13 | 5654 | 5442 | 5227 | 50 | 4741 | 454 | 4212 | 8858 | 8515. |
| 14 | 57.21 | 5519 | 5315 | 51 | 4852 | 4627 | 4849 | 4051 | 3727 |
| 15 | 5742 | 5549 | 5854 | 5155 | 4950 | 4735 | 459 | 4225 | 8917 |
| 16 | 58 | 5614 | 54.27 | 5236 | 5039 | 4834 | $46: 9$ | 48.47 | 40 ค2 |
| 17 | 5814 | 5635 | 5454 | 53.10 | 5121 | 4924 | 4717 |  | $42 \cdot 13$ |
| 18 | 5826 | 5653 | 5518 | 53.40 | 5157 | ${ }^{50} 7$ | 487 | 4583 | 4320 |
| 19 | 5836 | 578 | 5588 | 54 | 5.329 | 5045 | 4851 | 4648 | 4422 |
| 20 | 5844 | 5721 | 55.55 | 5428 | 5256 | 5118 | 4930 | 4781 | 4515 |
| 31 | 5851 | 5732 | 3610 | 5447 | 5320 | 5147 | 305 | 4812 | 468 |
| 22 | 6857 | 5742 | 5624 | 55 | 5342 | 5218 | 5036 | 4448 | 4646 |
| 28 | 59 | 5751 | 5637 | 5521 |  | 5237 | 51.4 | 4921 | 4725 |
| 24 | 598 | 5759 | 5648 | 5536 | 5420 | 5259 | 5130 | 4952 | 48 \％ |

ANGLES OF ELEVATION FOR 96 DEGREX BLANK．


ANGLEE OF ELEVATION FOR 40 DEGREE BLANK．

| 号够 | Angle of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \％ | 90 | 8 | 80 | 75 | 70 | ${ }_{6}$ | 60 | 65 | so． |
| 5 | $20^{\circ} 13$ | $14^{\circ} 58{ }^{\prime}$ | $9^{\circ} 24$ | $8^{\circ} 39$ |  |  |  |  |  |
| 6 | 3048 | 2621 | 2148 | 173 | 11 ${ }^{\circ} 58^{\prime}$ | $6^{\circ} 22^{\prime}$ |  |  |  |
| 7 | 8637 | 8252 | 292 | 25 | 2049 | 1612 | $11^{\circ} 1^{\prime}$ | $5^{\circ} 2$ |  |
| 8 | 407 | 365 | 3336 | 3010 | 2683 | 2238 | 1816 | 1820 | $7{ }^{\circ} 23^{\prime}$ |
| 9 | 4224 | 3934 | 8641 | 3341 | 3031 | 2726 | 2320 | 194 |  |
| 10 | 4357 | 4126 | 3851 | 3611 | 8332 | 30.21 | 278 | 2316 | 1885 |
| 11 | 45.4 | 4248 | 4028 | 38 | 8582 | 3249 | 2950 | 2629 | 2888 |
| 12 | 4554 | 4350 | 4148 | 8932 | 87.14 | 3445 | 32.3 | 292 | 2533 |
| 18 | 4683 | 4488 | 4242 | 4041 | 88.35 | 3619 | 3350 | 81 | 2754 |
| 14. | 47 | 4517 | 4329 | 4138 | 3941 | 8736 | 8519 | 3248 | 2951 |
| 15 | 4726 | 4547 | 447 | 4224 | 4035 | 3839 | 3682 | 8410 | 3128 |
| 16 | 4745 | 4618 | 4439 | 433 | 4121 | 3982 | 3783 | 3521 | 3250 |
| 17 | 481 | 46.84 | 456 | 4330 | 420 | 4018 | 3827 | 3623 |  |
| 18 | 48.14 | 4652 | 4529 | 44 | 4334 | 4058 | 3913 | 3717 | 355 |
| 19 | 4825 | 478 | 4549 | 4428 | 438 | 4183 | 39.54 | 384 | $85 \quad 59$ |
| 20 | 4885 | 4722 | 467 | 4450 | 4330 | 424 | 4030 | 8846 | 3647 |
| 21 | 4848 | 4783 | 4628 | 459 | 4353 | 4231 | 412 | 39＇23 | 3780 |
| ＇22 | 4850 | 4743 | 4636 | 4526 | 4413 | 4253 | 4130 | 3956 | 388 |
| 23 | 4856 | 4752 | 4648 | 4541 | 4431 | 4817 | 4155 | 4025 | 3842 |
| 34 | 49 |  | 4658 | 4555 | 4448 | 43.36 | 4219 | 4052 | 8915 |

ANGLEA OF LISVATION TOR 46 DEGREE BLANE，

| 농 | Angle，of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 边 | 90 | ＊ | 80 | 75 | 50 | 65 | 60 | B5 | 50 |
| 5 | $17^{\circ} 10^{\circ}$ | 12＇86＇ | $7{ }^{\circ} 57^{\prime}$ | $8^{\circ} 5$ |  |  |  |  |  |
| 6 | 2684 | 2241 | 1843 | 1435 | $10^{\circ} 11^{\prime}$ | 5＇23＇ |  |  |  |
| 7 | 8156 | 2886 | 2513 | 2142 | 1756 | 1855 | $9^{\circ} 24^{\prime}$ | $4^{\circ} 15^{\prime}$ |  |
| 8 | 8516 | 82.3 | 2925 | 2622 | 288 | 19.89 | 1548 | 1125 | $5^{\circ} 58^{\prime}$ |
| 9 | 8727 | 8454 | 3217 | 2986 | 2645 | 2341 | $20 \cdot 19$ | 1631 | 1149 |
| 10 | 3858 | 8641 | 3421 | $81 \cdot 57$ | 2924 | 2640 | $23 \quad 40$ | 2018 | 1610 |
| 11. | 40 | 880 | 8553 | 3342 | 8124 | 28.57 | 2615 | 2314 | 1932 |
| 12 | 4064 | 39 0 | 375 | $85 \quad 5$ | 880 | 8045 | 2818 | 2583 | 2218 |
| 13 | 4182 | $39 \quad 47$ | 881 | 36111 | 8415 | 8212 | 2957 | 2786 | 2423 |
| 14 | $42 \quad 1$ | 4024 | 8846 | 874 | 3517 | 8322 | 81.18 | $28 \quad 58$ | 269 |
| 15 | 4225 | 40.55 | 3923 | 3748 | 869 | 3422 | 3226 | 3017 | 2740 |
| 16 | 4244 | 4120 | 3954 | － 8825 | $36 \quad 52$ | 3512 | 3824 | 81.23 | 2857 |
| 17 | 480 | 4141 | 4020 | 88.57 | 8729 | 8555 | 34 14 | $82 \quad 20$ | 804 |
| 18 | 4318 | 4158 | 4042 | 8924 | $88 \quad 1$ | 3683 | 8456 | 3310 | 31 |
| 19. | 4321 | 4218 | 411 | 8947 | 8828 | 875 | 8584 | $83 \quad 54$ | 3151 |
| 20 | 4384 | 4226 | 4118 | 408 | $38 \quad 53$ | 87 784 | $\begin{array}{ll}36 & 8\end{array}$ | 3433 | 3237 |
| 21 | 4842 | 4737 | 4183 | 4026 | 8915 | $38 \quad 0$ | $\begin{array}{lll}36 & 38\end{array}$ | 357 | 3317 |
| 22 | 4349 | 4247 | 4146 | 4042 | 8984 | 8823 | 87.5 | 8588 | 3453 |
| 23 | 435.5 | 4256 | 4157 | 4056 | 8952 | 3843 | 8729 | 366 | 3526 |
| 24 | 440 | $43 \quad 4$ | 427 | 415 | 407 | 89 1． | 3750 | 8681 | 8555 |

ANOLES OF HLSVATION FOR 60 DEGREE BLANE．

| ¢ | Angle of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \％${ }^{3}$ | 90 | 65 | 80 | 75 | 70 | 65 | CO | 85 | 80 |
| 5 | $14^{\circ} 92{ }^{\prime}$ | $10^{\circ} 89^{\prime}$ | $6^{\circ} 42^{\prime}$ | $2{ }^{\circ} 33^{\prime}$ |  |  |  |  |  |
| 6 | 2245 | 1923 | 1538 | 1224 | $8^{\circ} 38^{\prime}$ | $4^{\circ} 82^{\prime}$ |  |  |  |
| 7 | 2787 | 2442 | 2144 | 1889 | 1524 | 1184 | $8^{\circ} 1^{\prime}$ | $8^{\circ} 86^{\prime}$ |  |
| 8 | 3041 | 288 | 2581 | 2350 | $19 \quad 69$ | 1655 | 1883 | 945 | $5^{\circ} 20^{\prime}$ |
| 9 | 8244 | 8028 | $28 \quad 9$ | 2545 | 2314 | 2031 | 1782 | 1418 | 1022 |
| 10 | 8410 | 387 | $30 \quad 2$ | 2754 | 2589 | 2312 | 2032 | 1734 | 149 |
| 11 | 8518 | 3822 | 3128 | 2931 | 2728 | $25 \quad 16$ | 2252 | 2011 | 176 |
| 18 | 360 | 3418 | 3284 | 3047 | 2853 | $26 \quad 54$ | 2442 | 2215 | 1927 |
| 13 | 3636 | $85 \quad 2$ | 8326 | 3148 | $\begin{array}{ll}30 & 3\end{array}$ | $28 \quad 18$ | 2611 | 2356 | 2122 |
| 14 | 375 | 3588 | 349 | 3247 | 311 | $29 \quad 18$ | 2726 | 2521 | 2258 |
| 15 | 8728 | 367 | 3444 | 8818 | 3149 | 8018 | 2828 | 2632 | 2420 |
| 16 | 3747 | 8681 | 8518 | $33 \quad 53$ | 82.29 | 810 | 2922 | 2733 | 2580 |
| 17 | 882 | 3650 | 8587 | 3422 | 838 | 3138 | 307 | 2824 | 2629 |
| 18 | 3815 | 377 | 35.58 | 3447 | $83 \quad 33$ | 8213 | ． 3046 | 2910 | 2721 |
| 19 | 3826 | 3722 | 3617 | 359 | $\begin{array}{ll}33 & 59\end{array}$ | 3243 | 8121 | 2950 | 287 |
| 20 | 3835 | 3784 | 8682 | 3528 | 3421 | 33 C | 8153 | 3025 | 2847 |
| 21 | 3843 | 3745 | 8646 | 3545 | 3441 | 3333 | 3219 | 3057 | 2924 |
| 22 | 3850 | 8755 | 8658 | 360 | 3459 | 8355 | 3244 | 3126 | $29 \quad 57$ |
| 23 | 88． 56 | 38 3 | 879 | 3614 | 3515 | 3414 | 336 | 8151 | 8026 |
| 24 | 391. | 3810 | 3719 | 3625 | 3530 | 3480 | 8325 | 3214 | 3052 |

ANGLES OF ELEVATION FOR B6．DMGREE BLANE．

| 형 | Argle of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7\％ | 00 | 85 | 80 | 75 | 70 | 65 | 60 | 55 | 80 |
| 5 | $12^{\circ} 18{ }^{\prime}$ | $8^{\circ} 57^{\prime}$ | $6^{\circ} 37^{\prime}$ | $2^{\circ} 10^{\prime}$ |  |  |  |  |  |
| 6 | 1917 | 1625 | 1380 | 1028 | $7^{\circ} 15^{\prime}$ | $3^{\circ} 48^{\prime}$ |  |  |  |
| 7 | 2385 | 214 | 1881 | 1551 | 134 | 108 | $6^{\circ} 44^{\prime}$ | $8^{\circ} 1^{\prime}$ |  |
| 8 | 2621 | 248 | 2152 | 19 81 | 17 | 1425 | 11．80 | 817 | $4^{\circ} 17$ |
| 9 | 2813 | 2614 | $24 \quad 18$ | 227 | 1955 | 17.34 | 1459 | 126 | 834 |
| 10 | 2932 | 2745 | 2555 | 24． 2 | $22 \quad 3$ | $19 \quad 35$ | 1736 | 151 | 1152 |
| 11 | 3030 | 2852 | 2712 | $25 \quad 29$ | 2341 | 2145 | 1939 | 1718 | 1427 |
| 12. | 3114 | 2944 | $28 \cdot 12$ | 2888 | 2459 | 2313 | 21.17 | 19 19 | 1682 |
| 13. | 3148 | 8025 | $29 \quad 0$ | 2733 | $26 \quad 2$ | 2424 | 2237 | 20.38 | 1815 |
| 14 | 8215 | $30 \quad 58$ | 2989 | 2818 | $26 \quad 53$ | $25 \quad 25$ | 2343 | 2153 | 1940 |
| 15 | 3286 | 3124 | 3011 | $28 \quad 55$ | 2735 | 26111 | $2 \pm 38$ | 2256 | 2052 |
| 16 | 3254 | 8147 | 8088 | 2927 | $28 \quad 12$ | $26 \quad 53$ | 2526 | $23 \quad 51$ | 2154 |
| 17 | 839 | 326 | 311 | $29 \quad 54$ | 2844 | 2729 | $\begin{array}{ll}26 & 7\end{array}$ | 2438 | 2249 |
| 18 | 8321 | 3221 | 3120 | $\begin{array}{lll}80 & 17\end{array}$ | 29.10 | $28 \quad 0$ | 2643 | 2518 | 2335 |
| 19 | 3381 | 8284 | 31． 36 | 3036 | 2933 | 2827 | 2714 | $25 \quad 54$ | 2417 |
| 20 | 3340 | 3246 | 8151 | 3054 | 2954 | 2851 | 2742 | 2625 | 2453 |
| 21 | 3347 | 8256 | $\begin{array}{ll}32 & 8\end{array}$ | 818 | 3012 | 2912 | $28 \quad 6$ | 2653 | 2520 |
| 22 | 3354 | 835 | 3215 | 8128 | $80 \quad 29$ | 2931 | 2828 | 2719 | 2555 |
| 23 | 340 | 3318 | $32 \quad 25$ | 3136 | 3044 | 2948 | 2848 | 2742 | 2622 |
| 24 | 345 | 3320 | 3234 | 3147 | $30 \quad 57$ | $30 \quad 4$ | 297 | $28 \quad 8$ | 2646 |

## SETTING ANGLES FOR MILLING ANGULAR CUTTERS－IV

ANGLES OF ELEVATION FOR GO DEGREE BLANK．

|  | Angie of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| z＇0 | 90 | 85 | 80 | 75 | \％ 0 | 65 | 60 | 55 | 50 |
| 5 | $10^{\circ} 7$ | $7^{\circ} 25^{\prime}$ | $4^{\circ} 39 \cdot$ | $1^{\circ} 47^{\prime}$ |  |  |  |  |  |
| 6 | 166 | 1341 | 1112 | 842 | $6^{\circ} 2^{\prime}$ | $3^{\circ} 9^{\prime}$ |  |  |  |
| 7 | 1848 | 1740 | 1530 | 1316 | 1055 | 822 | $5^{\circ} 36$ | $2^{\circ} 30^{\prime}$ |  |
| 8 | 2213 | 2019 | 1824 | 1624 | 1419 | 124 | 937 | 653 | $3 \cdot 44$ |
| 9 | 2352 | 2210 | 2026 | 1839 | 1646 | 1446 | 1234 | 107 | 719 |
| 10 | $25 \quad 2$ | 2330 | 2156 | 2019 | 1837 | 1648 | 1449 | 1236 | 105 |
| 11 | 2554 | 2430 | 234 | 2135 | $20 \quad 2$ | 1823 | 1634 | 1434 | 1216 |
| 12 | 2634 | 2516 | 2357 | 2236 | 2110 | 1939 | 1759 | 16 | 1413 |
| 13 | 275 | 2553 | 2440 | 2325 | 22.6 | 2041 | 198 | 1727 | 1531 |
| 14 | 2729 | 2622 | 2514 | $24 \quad 4$ | 2251 | 2132 | 206 | 1832 | 1644 |
| 15 | 2749 | 2646 | 2543 | 2437 | $23 \quad 29$ | 2215 | 2055 | 1927 | 1747 |
| 16 | 285 | 27.6 | 26.7 | 25.5 | 241 | 2252 | 2137 | 2014 | 1840 |
| 17 | 2818 | 2723 | $26 \quad 27$ | 2529 | 24：28 | 2323 | 2213 | 2055 | 1926 |
| 18 | $28 \quad 29$ | 2737 | 2644 | 2549 | 2452 | 2350 | 2244 | 2130 | 206 |
| 19 | 2838 | 2749 | 2658 | 26 | 2512 | 2414 | 2311 | $22 \cdot 1$ | 2042 |
| 20 | 2846 | 2759 | $27 \cdot 11$ | 2622 | 2530 | 2435 | 2335 | $22 \quad 29$ | 2114 |
| 21 | 2853 | 288 | 2723 | 2636 | 2546 | 2454 | $23 \quad 57$ | 2254 | 2142 |
| 22 | 290 | $28 \quad 17$ | 2734 | 2649 | $26 \quad 2$ | 2512 | $24 \cdot 17$ | 2317 | 228 |
| 23 | 295 | 2824 | 2743 | 270 | 2615 | $25 \quad 27$ | 3435 | 2337 | 2232 |
| 24 | 298 | 2830 | 2750 | 27 | 2626 | 2540 | 2450 | 2355 | 2252 |

ANGLES OF ELEVATION FOR 65 DEGREE BLANE．

| 동 | Angle of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 之萓 | 90 | 85 | 80 | 75 | 70 | 65 | 60 | 55 | 50 |
| 5 | $8^{\circ} 12^{\prime}$ | $6^{\circ} 0^{\prime}$ | $3^{\circ} 46^{\prime}$ | $1^{\circ} 27^{\prime}$ |  |  |  |  |  |
| 6 | 137 | 1110 | 98 | 74 | $4^{\circ} 53^{\prime}$ | $2^{\circ} 33^{\prime}$ |  |  |  |
| 7 | 1613 | 1428 | 1241 | 1050 | 854 | 649 | $4^{\circ} 83{ }^{\prime}$ | $2^{\circ} 1$ |  |
| 8 | 1815 | 1640 | 156 | 1326 | 1142 | 951 | 750 | 530 | $8^{\circ} 1$ |
| 9 | 1939 | 1814 | 1648 | 1519 | 1345 | 125 | 1016 | 814 | 557 |
| 10 | 2040 | 1923 | $18 \quad 4$ | 1644 | 1519 | 1348 | 129 | 10.19 | 815 |
| 11 | 2125 | 2014 | 19 3 | 1749 | 1631 | $15 \quad 9$ | 1338 | 1158 | 104 |
| 12 | 2159 | 2054 | 1948 | 1840 | 1728 | 1612 | 1449 | 1317 | 1132 |
| 13 | 2226 | 2126 | 2035 | 1922 | 1815 | 17 | 1548 | 1423 | 1246 |
| 14 | 2248 | 2152 | $20 \quad 55$ | 1956 | 1854 | 1748 | 1687 | 1517 | 1848 |
| 15 | $23 \quad 5$ | 2213 | 2119 | 2024 | 1926 | 1824 | 1718 | 164 | 1440 |
| 16 | 2318 | 2229 | 2139 | 2047 | 1953 | 1855 | 1753 | 1643 | 1524 |
| 17 | 2380 | 2243 | 2156 | 218 | 2017 | 1922 | 1823 | 1717 | 168 |
| 18 | 2340 | 2255 | 2211 | 2125 | 2087 | 1946 | 1850 | $17 \cdot 47$ | 1637 |
| 19 | 2348 | 235 | 22.24 | 2140 | 2055 | 206 | 1918 | 1814 | $17 \quad 7$ |
| 20 | 2355 | 2314 | 2285 | 8154 | 2110 | 2024 | 1983 | 1838 | 1734 |
| 21 | 211 | 2323 | 2245 | 226 | 2124 | 2039 | 1951 | 1858 | 1758 |
| 22 | 246 | $23 \quad 29$ | 2253 | 2216 | 2136 | 2053 | 208 | 1917 | 1820 |
| 23 | 2411 | 2336 | 231 | 2226 | 2147 | 217 | 2023 | 1984 | 1889 |
| 24 | 2415 | 2348 | $28 \quad 8$ | 2284 | 2157 | 2118 | 2086 | 1950 | 18 57 |

ANGLES OF ELEVATION FOR TO DRGREE BLANK．

| $\begin{aligned} & \text { 怣: } \\ & \text { 謁 } \\ & \text { zo } \end{aligned}$ | Angle of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 90 | 88 | 80 | 75 | 70 | 65 | 60 | 55 | 50 |
| 5 | $6^{\circ} 25^{\prime}$ | $4^{\circ} 42^{\prime}$ | $2^{\circ} 57^{\prime}$ |  |  |  |  |  |  |
| 6 | 1018 | 844 | 79 | $5^{\circ} 82^{\prime}$ | $3^{\circ} 48$ |  |  |  |  |
| 7 | 1247 | 1123 | 959 | 831 | ${ }^{6} 58$ | $5^{\circ} 21^{\prime}$ | $3^{\circ}{ }^{\circ} 3^{\prime}$ |  |  |
| 8 | 1426 | 1311 | 1155 | 1036 | 914 | 745 | ${ }^{6} 9$ | $4^{\circ} 23{ }^{\prime}$ | $2^{\circ} 21$ |
| 9 | 1535 | 1427 | 1818 | 127 | 1053 | 983 | 86 | 630 | 441 |
| 10 | 1625 | 1523 | 1421 | 1815 | 128 | 1055 | 937 | 8 | 630 |
| 11 | 172 | 165 | 158 | 148 | 187 | 12． 0 | 1048 | 928 | 757 |
| 12 | 1730 | 1688 | 1545 | 1450 | 1358 | 1251 | 1145 | 1081 |  |
| 13 | 1752 | 174 | 1615 | 1524 | 1480 | 1333 | 1232 | 1123 | $10{ }^{10} 6$ |
| 14 | 189 | 1724 | 1688 | 1551 | 151 | 148 | 1311 |  |  |
| 15 | 1823 1835 | 1741 | 1658 | 1614 1683 |  | 14 <br> 15 <br> 15 <br> 8 | 13 14 14 13 | 1244 | 1138 |
| $1 \begin{aligned} & 16 \\ & 17\end{aligned}$ | 1835 1845 | 1755 | $\begin{array}{ll}1715 \\ 17 & 80\end{array}$ | 1683 1650 | 15 <br> 16 <br> 16 | 15 15 | 14138 | 1817 18 46 | 1218 |
| 18 | 1858 | 1817 | 1742 | 175 | 1626 | 1544 | 1459 | 1410 | 1313 |
| 19 |  | 1826 | 1752 | 1717 | 1640 | 161 | 1518 | 1482 | 1838 |
| 20 | 196 | 1835 | 181 | 1728 | 1653 | 1616 | 1535 | 1451 | 1359 |
| 21 | 1911 | 1841 | 189 | 1788 | 175 | 1629 | 1550 | 158 | 1418 |
| 22 | 1915 | 1846 | 1818 | 1746 | 1715 | 1640 | 16 | 15.22 | 1435 |
| 23 | 1919 | 1851 | 1828 | 1754 | 1725 | 1650 | 1615 | 1536 | 1451 |
| 24 | 1922 | 1855 | 1829 | 180 | 1783 | 1659 | 1625 | 1548 | 15. |

ANGLES OF RERVATION FOR 75 DEGREE BLANZ．

| ¢¢ | Angle of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 乙 | 90 | 85 | 80 | 3 | \％ | 65 | 60 | 55 | 50 |
| 5 | $4^{\circ} 44^{\prime}$ | $3^{\circ} 28^{\prime}$ | $2^{\circ} 10$ |  |  |  |  |  |  |
| 6 | 788 | 629 | 519 | $4^{\circ} 6^{\prime}$ | ${ }^{\circ} 50$ | $1^{\circ} 29$ |  |  |  |
| 7 | 929 | 827 | 724 | 617 | 510 | 357 | $2^{\circ} 38^{\prime}$ | $1{ }^{\circ} 10$ |  |
| 8 | 1044 | 948 | 851 | 750 | 651 | 545 | 434 | 314 | $10 \% 5$ |
| 9 | 1186 | 1046 | 954 | 90 | 85 | 75 | 00 | 449 | 827 |
| 10 | 1214 | 1128 | 1040 | 952 |  | 87 | 78 | 63 | 449 |
| 11 | 1242 | 120 | 1116 | 1032 | 945 | 856 | $8 \quad 2$ | 7． 1 | 554 |
| 12 | 184 | 1225 | 1145 | 11.4 | 1021 | 935 | 845 | 749 | 647 |
| 13 | 1821 | 1245 | 128 | 1129 | 1050 | 107 | 921 | 829 | 781 |
| 14 | 1334 | 130 | 1226 | 1150 | 1113 | 1033 | 950 | 92 | 87 |
| 15 | 1345 | 1313 | 1241 | 127 | 1133 | $10 \quad 55$ | 1015 | 930 | 839 |
| 16 | 1354 | 1324 | 1254 | 1222 | 1150 | 1114 | 1037 | 954 | 97 |
| 17 | $14 \quad 2$ | 1333 | $13 \quad 5$ | 1235 | 125 | 1131 | 1056 | 1016 | 931 |
| 18 | 148 | 1341 | 1314 | 1246 | 1217 | 1145 | 1112 | 1034 | 951 |
| 19 | 1413 | 1348 | 1322 | 1255 | 1228 | 1158 | 1126 | 1050 | 1010 |
| 20 | 1418 | 1354 | 1329 | 13 13 | 1238 | 129 | 11.39 | 115 | 1087 |
| 21 | 1422 | 1859 | 1336 | $13 \quad 12$ | 1246 | 1219 | 1150 | 1117 | 1041 |
| 22 | 1425 | 14 | 1341 | 1318 | 1253 | 1228 | 120 | 1129 | 1054 |
| 23 | 14.28 | $14 \quad 7$ | 1346 | 1324 | 13 － | 1236 | 129 | 1140 | 116 |
| 24 | 1431 | 1411 | 1350 | 1329 | 137 | 1244 | 1218 | 1150 | 1118 |

ANGLES OF ELEVATION FOR 80 DEOREE BLANK

|  | Anglo of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 云＂ | 80 | 85 | 80 | 75 | 70 | 65 | 60 | 55 | 50 |
| 5 | $8^{\circ} 7{ }^{\prime}$ | $2^{\circ} 17^{\prime}$ | $1^{\circ} 26^{\prime}$ | $0^{\circ} 43^{\prime}$ |  |  |  |  |  |
| 6 | 52 | 416 | 380 | 242 | $1^{\circ} 52^{\prime}$ | $0^{\circ} 58^{\prime}$ |  |  |  |
| 7 | ${ }^{6} 16$ | 535 | 453 | 410 | 325 | 236 | $1^{\circ} 45^{\prime}$ | $0^{\circ} 46^{\prime}$ |  |
| 8 | 76 | 629 | 551 | 512 | 431 | 348 | 32 | 28 | $1^{\circ} 8^{\prime}$ |
| 9 | 742 | 78 | 634 | 558 | 521 | 442 | 359 | 311 | 217 |
| 10 | 87 | 736 | 75 | 633 | 559 | 528 | 444 | 40 | 311 |
| 11 | 826 | 758 | 729 | 70 | 628 | 555 | 519 | 439 | 354 |
| 12 | 841 | 815 | 748 | 721 | 652 | 622 | 548 | 511 | 429 |
| 13 | 853 | 829 | 84 | 738 | 712 | 643 | 612 | 538 | 459 |
| 14. | 92 | 840 | 816 | 752 | 788 | 71 | 632 | 6 | 524 |
| 15 | $9 \quad 9$ | 848 | 826 | 84 | 740 | 716 | 648 | 619 | 545 |
| 16 | 915 | 855 | 835 | 814 | 751 | 728 | 73 | 633 | 63 |
| 17 | 920 | 91 | 842 | 822 | 81 | 739 | 715 | 649 | 619 |
| 18 | 924 | 96 | 848 | 829 | 810 | 749 | 726 | 71 | 633 |
| 18 | 928 | 911 | 858 | 836 | 817 | 758 | 736 | 712 | 645 |
| 20 | 9.31 | 915 | 858 | 842 | 824 | 85 | 744 | 721 | 656 |
| 21 | 934 | 919 | 93 | 847 | $8 \cdot 80$ | 812 | 752 | 7：30 | 76 |
| 22 | 936 | 922 | 96 | 851 | 835 | 818 | 759 | 738 | 715 |
| 23 | 938 | 924 | 99 | 855 | 839 | 823 | 85 | 745 | 723 |
| 24. | 940 | 926 | 9.13 | 859 | 843 | 828 | 811 | 751 | 7.30 |

ANGLES OF HELSVATION FOR BS DEGRER BLANK．

| ¢ ${ }^{\text {d }}$ | Angle of Cutter． |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 乙\％ | 90 | 85 | 80 | 73 | 70 | 65 | 60 | 55 | 50 |
| 5 | $1^{\circ} 33^{\prime}$ | $1^{\circ} 8^{\prime}$ |  |  |  |  |  |  |  |
| 0 | 280 | 27 | $1^{\circ} 44^{\prime}$ | $1^{\prime} 20^{\prime}$ | $0^{\circ} 55^{\prime}$ |  |  |  |  |
| 7 | 37 | 246 | 226 | 24 | 142 | $1^{\circ} 18^{\prime}$ | $0^{\circ} 50{ }^{\prime}$ |  |  |
| 8 | 382 | 318 | 255 | 235 | 215 | 1.53 | 129 | $1^{\circ} 8^{\prime}$ | $0^{\circ} 84^{\prime}$ |
| 9 | 850 | 333 | 316 | 28 | 240 | 220 | 159 | 135 | 18 |
| 10 | 48 | 348 | 882 | 816 | 259 | 241 | 221 | 159 | 185 |
| 11 | 413 | 359 | 844 | 830 | 314 | 257 | 889 | 219 | 157 |
| 12 | 420 | 47 | 853 | 840 | 325 | 310 | 253 | 235 | 215 |
| 18 | 426 | 414 | 41 | 848 | 835 | 821 | 86 | 248 | 280 |
| 14 | 436 | 419 | 47 | 355 | 343 | 329 | 315 | 259 | 242 |
| 15 | 434 | 423 | 412 | 41 | 850 | 8 87 | 394 | 8 8 9 | 252 |
| 16 | 487 | 427 | 417 | 46 | 856 | 344 | 880 | 817 | 31 |
| 17 | 440 | 430 | 421 | 411 | 41 | 850 | 887 | 824 | 89 |
| 18. | 442 | 433 | 4.24 | 415 | 45 | 355 | 348 | 830 | 316 |
| 19 | 444 | 485 | 427 | 418 | 49 | 359 | 348 | 886 | 822 |
| 20 | 446 | 487 | 429 | 421 | 412 | 48 | 852 | 841 | 328 |
| 21 | 447 | 439 | 481 | 423 | 415 | 46 | 356 | 845 | 883 |
| 22 | 448 | 441 | 433 | 425 | 418 | 49 | 859 | 349. | 387 |
| 23 | 449 | 442 | 435 | 427 | 420 | 412 | 42 | 853 | 341 |
| 24 | 450 | 443 | 436 | 429 | 422 | 414 | 45 | 356 | 345 |



Dimenslops of Shell End Minls
Dimensions for sheli end mills are given on page 30, and for the arbors on which these mills are mounted when in use, on page 31. The head of the screw on the end of the arbor enters into the recess in the end of the mill. The keys in the arbor enter into the keyway $F$ at the upper end of the mill and constitute the drive. It will be seen that the number of teeth in these mills is greater for the same diameters than the number in solid end mills. This is because the coarser teeth of the latter would require a deeper flute than would be possible in the thin shell of the shell end mill.

## Milling the Teeth in End Mills and Angular Cutters

On page 32 is given a table of angles for setting the dividing head of the milling machine when cutting teeth in the end of end mills. The angle to which the dividing head must be set depends on two factors, the number of the teeth in the mill to be cut, and the angle of the cutter with which the teeth are to be cut. When the number of teeth in the cutter and the angle of the cutter used for milling the teeth are given, the setting angle of the dividing head is
found in the body of the table. For example, assume that 12 teeth are to be cut in the end of an end mill with a 60 degree cutter. Then by following the horizontal line from 12 teeth we read in the column under 60 degrees that the dividing head should be set to an angle of 70 degrees 32 minutes for this job. On pages 34 to 36 are given similar tables for milling angular cutters, an explanation of the formulas by which these angles are obtained being given on page 33. [Machinery, April, 1904, To Calculate the Setting of the Dividing Head when Cutting the Teeth of End Mills; November, 1908, Setting Angles for Milling Angular Cutters and Taper Reamers.]

## Dimensions of Plug and Ring Gages

On page 37 are given dimensions of plain plug and ring gages for ordinary use. These dimensions are based upon the dimensions used for these gages by one of the most prominent gage makers in the country. The proportions will be found suitable for every-day use, although for special requirements some of the dimensions may have to be modified.

## 14 DAY USE

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