15． 4 ？


Cogoor Ontiam sovi2 1907

$$
\begin{aligned}
& \text { nomin Amo } \\
& \text { Crisirs. }
\end{aligned}
$$

## A

## SYSTEM

or

## GEOMETRY AND TRIGONOMETRY:

TOGETHER WITH A
TREATISE ON SURVEYING;
reaching various ways of taking the survey of a fiezd ;
ALSO TO PROTRACT THE SAME AND FIND THE AREA.
LIKEWISE,

## RECTANGULAR SURVEYING;

OR,
an accurate method of calculating the area of ANY FIELD ABITHMETICALLY, WITHOUT THE NECESSITY OF PLOTTING IT.
to the whole are added,
several mathematical tables,
NECESSARY FOR SOLVING QUESTIONS IN
TRIGONOMETRY AND SURVEYING;
WITH A PARTICULAR EXPLANA'TION "F THOSE TABLES, AND THE MANNER OF USING THEM.
compiled from various authors, BY ABEL FLINT, A.M.

GIFTH EDITION, WITH IMPORTANT ADDITIONS,
BY GEORGE GILLET, surveyor general of the state of connecticut.

HARTFORD: :
PUBLISHED BY OLIVER L.' COOKE \& ©R

## District of Connecticut, ss.

BIT REMEMBERED, That on the twenty-fifth day of September, in the forty-third year of the Independence of the United States of America, Oliver D. Cooke \& Co., of the said district, have deposited in this office the title of a book, the right whereof they claim as Proprietors, in the words following, to wit-
" A System of Geometry and Trigonometry: together with a Treatise on Surveying; Teaching various ways of taking the Survey of a Field; Also to Protract the same and find the Area. Likewise, Rectangular Surveying; or, an Accurate Method of calculating the Area of any Field Arithmetically without the necessity of Plotting it. To the whole are added several Mathematical Tables, necessary for solving Questions in Trigonometry and Surveying; with a particular explanation of those Tables, and the Manner of using them. Compiled from various Authors. By Abel Flint, A. M. Fifth Edition, with important Additions, By George Filet, Surveyor General of the State of Connecticut."

- In conformity to the Act of the Congress of the United States, entitled "An Act for the encouragement of Learning, by securing the copies of Maps, Charts, and Books, to the authors and proprietors of such copies, during the times therein mentioned."
R. I. INGERSOLL,

Clerk of the District of Connecticut. A true copy of Record, examined and sealed by me,
R. I. INGERSOLL,

Clerk of the District of Connecticut.


## RECOMMENDATIONS.

HAVING perused, with some attention, the following Treatise on Surveying, in Manuscript, it appears to me to be estimable for its simplicity and perspicuity; and, by excluding all matter but remotely connected with the main subject, and reducing the Tables of Logarithms, of Logarithmic Sines, Tangents, and Secants; and of Difference of Latitude and Departure, without impairing their use, in their application to most cases which occur in common Surveying, and supplying any possible defect by a Table of Natural Sines, to comprise, in the limits of a pocket volume, whatever is most essential and most useful in the Art, including the important modern improvement of Rectangular Surveying; and on the whole, particularly from the size of the volume, to be well adapted to general use.

JOHN TREADWELL.

Garmington, Sept. 20th, 1804.

$$
41: 453
$$

WE the subscribers have carefully perused a Trea. tise on Surveying, prepared for the Press' by the Rev. Abel Flint of Hartford; and find it worthy of the public patronage. Every thing not immediately necessary for the practical Surveyor has been excluded; while it comprises all which is requisite in Field Surveying, both on the old and new plan; elucidated and explained with a degree of conciseness and perspicuity not usually to be found in Treatises on the same subject. The Mathematical Tables are reduced to less than half the size occupied by others; and any inconvenience which might result from such reduction, is obviated by the insertion of a Table of Natural Sines, not usually found in works of this nature. The Surveyor who shall own this will not be under the necessity of purchasing $\mathrm{G}_{\text {Ib- }}$ son, which is a more expensive work.

ASHER MILLER, Surveyor General. GEORGE GILLET, Deputy Surveyor for Tolland County.

## PREFACE.

The following work is chiefly a compilation from other Books; and but very little new is added, except a more full explanation, than has yet been published, of Rectangular Surveying, or the method of calculating the Area of Fields arithmetically, without drawing a plot of them and measuring with a Scale and Dividers, as has been the common practice; and also a more particular $\epsilon x$ planation of the use of Natural Sines than is contained in most Mathematical Books.

The Compiler has endeavoured to render this work so easy and intelligible that a Learner will require but little assistance from an Instructer, except with regard to the construction and use of Mathematical and Surveying Instruments. Before, however, he enters. on the study of this Book he must be well acquainted with common Arithmetic, with Decimal Fractions, and the Square Root; and he must also know the various characters or marks used in Arithmetic.

A Surveyor will doubtless find many questions arise in the course of his practice, for the solution of which, no particular directions are here given; nor is it possible to give directions for every case that may occur. In all practical Sciences much must be left to the judgment of the practitioner, who, if he is well acquainted with the general principles of his Art, will readily learn to apply those principles to particular cases.

The primary design of this treatise is to teach common Field Surveying; at the same time it contains the elements of Surveying upon a larger
scale; ; and the system of Geometry and Trigonometry with which it is introduced, with the Problems for the mensuration of Superficies, as also the Mathematical Tables at the end, will be found useful for many other purposes. It would be well, therefore, for those who do not intend to become practical Surveyors to acquaint themselves with what is here taught; and with this view the following work is very proper to be introduced into Academies, and those higher Schools which are designed to fit young men for active business in life. Indeed every person who frequently buys and sells land should learn to calculate the Contents of a field arithmetically ; a knowledge which may be acquired in a very little time, from the particular explanation here given of that method.

Notwithstanding the many Books already published on the subjects here treated upon, it was thought a work of this kind was really wanted, and that if judiciously executed it would be useful. It is more particularly necessary at the present time in Connecticut, as the Legislature of the State have lately enacted a Law on the subject of Surveying, in consequence of which more attention must be paid to the Theory of that Art than has been common.

These considerations induced the Compiler to select from various publications what appeared to him important; and to arrange the whole in a method best adapted, in his view, for teaching that useful Art. How far he has succeeded in his endeavours to simplify the subject, and render it easy to the Learner, must be submitted to the test of experience.

[^0]A GENERAL VIEW OF THE CONTENTS OF THIS WORK.
The System of Geometry is divided into two parts. The first contains Geometrical Definitions respecting Lines, Angles, Superficies, \&c. The second part contains a number of Geometrical Problems necessary for Trigonometry and Surveying.

The System of Trigonometry is also divided into two parts: and teaches the solution of questions in Right and Oblique angled Trigonometry, by Logarithms and also by Natural Sines.

The Treatise on Surveying is divided into three parts. Part first treats of measuring Land, and is divided into three Sections. The first contains several Problems respecting Mensuration, and for finding the Area of various Right-lined Figures and Circles.

The second Section teaches different methods of taking the Survey of Fields; also to protract them, and find their Area in the manner commonly practised, and likewise by Arithmetical and Trigonometrical calculations, without measuring Diagonals and Perpendiculars with a Scale and Dividers ; interspersed with sundry useful rules and directions.

The third Section is a particular explanation and demonstration of Rectangular Surveying, or the method of computing the Area of Fields from the Field Notes, by Mathematical Tables, without the necessity of plotting the Field. To this Section is added a useful Problem for ascertaining the true Area of a Field which has been measured by a Chain too long or too short.

Part second treats of laying out Land in various shapes.

Part third contains sundry Problems and Rules for dividing Land and determining the true Course and Distance of dividing Lines, or from one part of a Field to another. To this is added an Appendix concerning the Variation of the Compass and Attraction of the Needle; also, a rule to find the difference between the present Variation, and that at a time when a Tract was formerly surveyed, in order to trace or run out the original lines.

The Mathematical Tables, are a Traverse Table, or Table of Difference of Latitude and Departure, calculated for every Degree and quarter of a Degree, and for any distance up to 50 ; a Table of Natural Sines calculated for every Minute; a Table of Logarithms comprised in four pages, yet sufficiently extensive for common use; and a Table of Logarithmic or Artificial Sines, Tangents, and Secants, calculated for every 5 Minutes of a Degree. To these Tables are prefixed particular explanations of the manner of using them.

## GEOMETRY.

GEOMETRY is a Science which treats of the properties of Magnitude.

## PART I.

## Geometrical Definitions. *

1. A Point is a small Dot ; or, Mathematically considered, is that which has no parts, being of itself indivisible.
2. A Line has length but no breadth.
3. A Superficies or Surface, called also Area, has length and breadth, but no thickness.
4. A Solid has length, breadth, and thickness.
5. A Right Line is the shortest that can be drawn between two Poirts.

Fig. 1.
6. The inclination of tiro Lines meeting oue another, or the opening between them, is called an Angle. Thus at B. Fig. 1. is an Angle, formed by the meeting of the Lines $A B$ and $B C$.


Fig. 2.
7. If a right Line CD. Fig. 2. fall upon another Rigbt Line AB, so as to incline to neither side, but make the Angles on each side equal, then those Angles are called Right Angles; and the Line CD is said to be Perperidicular to the other Line.

GEOMETRY.
Fig. 3.
8. An Obtuse Angle is greater than a Right Angle; as ADE. Fig. 3.
9. An Acute Angle is less than a Right Angle ; as EDB. Fig. 3.


Note. When three letters are used to express an Angle, the middle letter denotes the angular Point.
10. A Circle is a round Figure, bounded by a Line equally distant from some Point, which is called the Centre. Fig. 4.
11. The Circumference or Periphery of a Circle is the bounding Line; as ADEB. Fig. 4.
12. The Radius of a Circle is a Line drawn from the Centre to the Circumference; as CB. Fig. 4. Therefore all Radii of the same Circle are equal.
13. The Diameter of a Circle is a Right Line drawn from one side of the Circumference to the other, passing through the Centre; and it divides the Circle into two equal parts, called Semicircles; as AB or DE. Fig. 5.
14. The Circumference of every Circle is snpposed to be divided into 360 equal parts, called Degrees; and each Degree into 60

Fig. 4.


Fig: 5. equal parts, called Minutes; and each Minute into 60 equal parts, called Seconds; and these into Thirds, \&e.

Note. Since all Circles are civided into the same number of Degrees, a Degree is not to be accounted a quantity of any determinate length, as so many inches or feet, \&c. but is always to be reckoned as being the 360th part of the Circumference of any Circle, without regarding the bigness. of the Circle.
15. An Arch or Arc of a Circle is any part of the Circumfereuce; as BF or FD. Fig. 5; and is said to be an Arch of so many Degrees as it contains pacts of 360 into which the whole. Circle is divided.
16. A Chord is a Right Line drawn from one end of an Arch to the other, and is the measure of the Arch; as HG is the Chord of the Arch HIG. Fig. 6.


Note. The Chord of an Arch of 60 degrees is equal in Iength to the Radius of the Circle of which the Arch is a part.
17. The Segment of a Circle is a part of a Circle, cut off by a Chord; thus the space comprehended between the Arch HIG and the Chord HG is called a Segment. Fig. 6.
18. A Quadrant is one quarter of a Circle; as ACB. Fig. 6.
19. A Sector of a Circle is a space contained between two Radii and an Arch less than a Semicircle; as BCD or ACD. Fig. 6.
20. The Sine of an Arch is a Line drawn from one end of the Arch, perpendicular to the Radius or Diameter drawn through the other end: Or, it is half the Chord of double the Arch; thus HL is the Sine of the Arch HB. Fig. 7.
21. The Sines on the same Diameter in- A crease in length till they come to the Centre, and so become the Radius. Hence it is plain that the Radius CD Fig. 7. is the greatest possible Sine, or Sine of 90 Degrees.

22. The Versed Sine of an Arch is that part of the Diameter or Radius which is between the Sine and the Circumference thus LB is the Versed Sine of the Arch HB. Fig. 7.
23. The Tangent of an Arch is a Right Line touching the Circumference, and drawn perpendicular to the Diameter; and is terminated by a Line drawn from the Centre through the other end of the Arch; thus BK is the Tangent of the Arcl BH. Fig. 7.

Note. The Tangent of an Arch of 45 Degrees is equal in length to the Radius of the Circle of which the Arch is a part.

## 24. The Secant of an Arch is a Line drawn from the Centre

through one end of the Arch till it meets the Tangent; thus CK is the Secant of the Arch BH. Fig. 7.
25. The Complement of an Arch is what the Arch wants of 90 Degrees, or a Quadrant ; thus HD is the Complement of the Arch BH. Fig. 7.
26. The Supplement of an Arch is what the Arch wants of 180 Degrees, or a Semicircle; thus ADH is the Supplement of the Arch BH. Fig. 7.
27. The Sine, Tangent or Segant of the Complement of any Arch is called the Co-Sine, Co-Tangent, or Co-Secant of the Arch; thus, FH is the Sine, DI the Tangent, and CI the Secant of the Arch DH; or they are the Co-Sine, Co-Tangent, and CoSecant of the Arch BH. Fig. 7.
28. The measure of an Angle is the Aych of a Circle contained between the two Lines which form the angle, the angular Point being the Centre ; thus, the Angle HCB. Fig. 7. is measured by the Arch BH : and is said to contain so many Degrees as the Arch does.

Note. An Angle is esteemed greater or less according to the opening of the Lines which form it, or as the Arch intercepted by those Lines contains more or fewer Degrees. Hence it may be observed, that the bigness of an Angle does not depend at all upon the length of the including Lines; for all Arches described on the same Point, and intercepted by the same Right Lines, contain exactly the same number of Degrees, whether the Radius be longer o: shorter.
29. The Sine, Tangent, or Secant of an Arch is also the Sine, Tangent, or Secant of the Angle whose measure the Arch is. Fig. 8.
30. Parallel Lines are such as are equally $\mathbf{A}$ _ $\mathbf{H}$ distant from each other ; as AB and CD. Fig. 8.

33. An Isocles Triangle has two of its sides equal, and the other longer or shorter. Fig. 10.

Fig. 10.


Fig. 11.
34. A Scalene Triangle has three unequal sides. Fig. 11.


Fig. 12.
35. A Right Angled Triangle has one Right Angle. Fig. 12.


Fig. 13.
36. An Obtuse Angled Triangle has one Obtuse Angle. Fig. 13.

37. An Acute Angled Triangle has all its Angles Acute, Fig. 9, or 10.
38. Acute and Obtuse Angled Triangles are called Oblique Angled Triangles, or simply Oblique Triangles; in which the bottom Side is generally called the Base and the other two, Legs.
39. In a Right Angled Triangle the longest side is called the Hypothenuse, and the other two, Legs, or Base and Perpendicular.

Note. The three Angles of every Triangle being added together will amount to 180 Degrees; consequently the two Acute Angles of a Right Angled Triangle amount to 90 Degrees, the Right Angle being also 90.

Fig. 14
40. The perpendicular height of a Triangle is a Line drawn from one of the Angles to its opposite side; thus, the dotted Line AD. Fig. 14. is the perpendicular height of the Triangle ABC.


Note. This Perpendicular may be drawn from either of the Angles; and whether it falls within the Triangle, or on one of the Lines continued beyond the Triangle, is immaterial.

Fig. 15.
41. A Square is a Figure bounded by four equal sides, and containing four Right Angles. Fig. 15.


Fig. 16.
42. A Parallelogram, or Oblong Square, is a Figure bounded by four sides, the opposite ones being equal and the Angles Right. Fig. 16.


Fig. 17.
43. A Rhombus is a Figure bounded by four equal sides, but has its Angles Oblique. Fig. 17.


Fig. 18.
44. A Rhomboides is a Figure bounded by four sides, the opposite ones being equal, but the Angles Oblique. Fig. 18.

45. The perpendicular height of a Rhombus or Rhomboides is a Line drawn from one of the Angles to its opposite side; thus, the dotted Lines AB. Fig. 17. and Fig. 18. represent the perpendicular height of the Rhombus and Rhomboides.

Fig. 19.
46. A Trapezoid is a Figure bounded by four sides, two of which are parallel though of unequal lengths. Fig. 19. and Fig. 20.



Fig. 20.

Note. Fig. 19. is sometimes called a Right Angled Trapes zium.

Fig. 21.
47. A Trapezium is a figure bounded by four unequal sides. Fig. 21.
48. A Diagonal is a Lire drawn between two opposite Angles; as the Line AB. Fig. 21.

49. Figures which consist of more than four sides are called Polygons; if the sides are equal to each other they are called regular Polygons, and are sometimes named from the number of their sides, as Pentagon, or Hexagon, a Figure of five or six sides, \&c. ; if the sides are unequal, they are called irregula: Polygons.

## PART II.

## Geometrical Problems.

PROBLEM I. To draw a Line parallel to another Line at any given distance; as at the Point D, to make a Line, parallel to the Line .9B. Fig. 22.


With the Dividers take the nearest distance between the Point $D$ and the given Line $A B$; with that distance set one foot of the Dividers any where on the Line AB , as at E , and draw the Arch $\mathbf{C}$; through the Point $\mathbf{D}$ draw a Line so as just to touch the top of the Arch $\mathbf{C}$.

A more convenient way to draw parallel Lines is with a parallel Rute.


Open the Dividers to any convenient distance, more than half the given Line AB, and with one foot in $A$, describe an Arch above and below the Line, as at $C$ and $D$; with the same distance, and one foot in B, describe Arches to cross the former; lay a Rule from $\mathbf{C}$ to $\mathbf{D}$, and where the Rule crosses the Line, as at E , will be the middle.

Fig. 24.

PROBLEM III. To erect a Perpendicular from the end, or any part of a given Line. Fig. 24.


Open the Dividers to any convenient distance, as from $\mathbf{D}$ to $A$, and with one foot on the Point $\mathbf{D}$, from which the Perpendicular is to be erected, describe an Arch, as AEG; set off the same distance from $\mathbf{A}$ to $\mathbf{E}$, and from $\mathbf{E}$ to $\mathbf{G}$; upon $\mathbf{E}$ and $\mathbf{G}$ describe two Arches to intersect each other at $\mathbf{H}$; draw a Line from $H$ to $D$, and one Line will be perpendicular to the other.

Note. There are other methods of execting a Perpendicular, hut this is the most simple.

Fig. 25.

PROBLEM IV. From a given Point, as at C, to drop a Perpendicular on given Line AB. Fig. 25.

With one foot of the dividers in $\mathbf{C}$ describe an Arch to cut the given Line in two places, as at $\mathbf{F}$ and $\mathbf{G}$; upon $\mathbf{F}$ and $\mathbf{G}$ describe two Arches to intersect each other below the Line as at $\mathbf{D}$; lay a Rule from $\mathbf{C}$ to $\mathbf{D}$ and draw a Line from $\mathbf{C}$ to the given Line.

Perpendiculars may be more readily raised and let fall, by a small Square made of brass, ivory, or wood.

Fig. 26.

PROBLEM V. To make an Angle at E,A
 equal to a given Angle ABC. Fig. 26.


Open the dividers to any convenient distance, and with one foot in B describe the Arch FG; with the same distance and one foot in $\mathbf{E}$, describe an Arch from $\mathbf{H}$; measure the Arch FG, and lay off the same distance on the Arch from H to I ; draw a Line through I to $\mathbf{E}$, and the Angles will be equal.

Fig. 27.
PROBLEM VI. To make an Acute Angle equal to a given nnmber of Degrees, suppose 36. Fig. 27.


Draw the Line AB to any convenient length; from a Scale of Chords take 60 Degrees with the dividers, and with one foot in B describe an Arch from the Line AB; from the same Scale take the given number of Degrees, 36, and lay it on the Arch from $\mathbf{C}$ to D ; draw a line from $\mathbf{B}$ through $\mathbf{D}$, and the Angle at $B$ will be an Angle of 36 Degrees.

D

PROBLEM VII. To make an Obtuse An${ }_{g}$ gle, suppose of 110 Degrces. Fig. 23.


Take a Chord of 60 Degrees as before, and describe an Arch greater than a Quadrant; set off 90 Degrees from $\mathbf{B}$ to $\mathbf{C}$, and from $C$ to $E$ set off the excess above 90 , which is 20 ; draw a Line from $G$ through $E$, and the Angle will contain 110 Degrees.

Note. In a similar manner Angles may be measured; that is, with a Chord of 60 Degrees describe an Arch on the angular Point, and on a Scale of Chords measure the Arch intercepted by the Lines forming the angle.

A more convenient method of making and measuring Angles. is to use a Protractor instead of a Scale and Dividers.

$$
\text { Fig. } 29 .
$$

PROBLEM VIII. To make a Triangle of three given Lines, as BO, BL, LO. Fig. 29.


Draw the Line BL from $\mathbf{B}$ to L ; from $\mathbf{B}$, with the length oi the Line BO, describe an Arch as at $\mathbf{O}$; from L, with the length of the Line LO, describe another Arch to intersect the former; from $\mathbf{O}$ draw the Lines $\mathbf{O B}$ and OL, and BOL will be the Triangle required.

Fig. 30.

PROBLEM IX. To make a Right Angled Triangle, the Hypothenuse and Angles being given. Fig. 30.


Suppose the Hypothenuse CA 25 Rods or Chains, the angle
at C $35^{\circ} 30^{\prime}$ and consequently the Angle at A $54^{\circ} 30^{\prime}$. See Note after the 39th Geometrical Definition.

Note. When degrees and minutes are expressed, they are distinguished from each other by a small cipher at the right hand of the degrees, and a dash at the right hand of the minutes; thus $35^{\circ} 30^{\prime}$ is 35 degrees and 30 minutes.

Draw the Line CB an indefinite length; at $\mathbf{C}$ make an Angle of $35^{\circ} 30^{\prime}$; through where that number of Degrees cuts the Arch draw the Line CA 25 Rods, which must be taken from some Scale of equal parts; drop a Perpendicular from A to B, and the Triangle will be completed.

Note. The length of the two Legs may be found by measuring them upon the same scale of equal parts from which the Hypothenuse was taken.

Fig. 31.

PROBLEM X. To make a Right Angled Triangle, the Angles and one Leg being given. Fig. 31.


Suppose the Angle at C $33^{\circ} 15^{\prime}$, and the Leg AC 285.
Draw the Leg AC making it in length 285 ; at A erect a Perpendicular an indefinite length; at C make an Angle of $33^{\circ}$ 15'; through where that number of Degrees cuts the Arch, draw a Line till it meets the Perpendicular at B.

Noie. If the given Line CA should not be so long as the Chord of $60^{\circ}$, it may be continued beyond $A$, for the purpose of making the Angle.

Fig. 32.

PROBLEM XI. To make a Right Angled Triangle, the Hypothenuse and one Leg being given. Fig. 32.

Suppose the Hypothenuse AC 40, and the Leg AB 28.
Draw the Leg AB in length 28 ; from B erect a Perpendicular an indefinite length; take 40 in the Dividers, and setting.
one foot in A, wherever the other foot strizes the Perpendicular will be the point $\mathbf{C}$.

Note. When the Triangle is constructed, the Angles may be measured by a Protractor, or by a Scale of Chords.

Fig. 33.

PROBLEM XII. To make a Right Angled Triangle, the two Legs being given. Fig. 33.


Suppose the Leg AB 38, and the Leg BC 46.
Draw the Leg AB in length 38 ; from $B$ erect a Perpendicular to $C$ in length 46 ; and draw a Line from $A$ to $C$.

Fig. 34.

PROBLEM XIII. To make an Oblique Angled Triangle, the Angles and one Side being given. Fig. 34.


Suppose the side BC 98; the Angle at B450 15', the Angle at D $108030^{\prime}$, consequently the other Angle $26^{\circ} 15^{\prime}$.

Draw the side BC in length 98; on the Point B make an Angle of $45^{\circ} 15^{\prime}$; on the Point C make an Angle of $26^{\circ} 15^{\prime}$, and draw the Lines BD and CD.

Fig. 35.
PROBLEM XIV. To make an Oblique Angled Triangle, two Sides and an Angle opposite to one of them being given. Fig. 35.


Suppose the side BC 160, the side BD 79, and the Angle at C $290{ }^{9}$.

Draw the side BC in length 160 ; at $\mathbf{C}$ make an Angle of $29^{\circ} 9^{\prime}$, and draw an indefinite Line through where the Degrees cut the Arch; take 79 in the dividers, and with one foot in B lay the other on the Line CD; the point $\mathbf{D}$ will be the other Angle of the Triangle.

Fig. 36.
PROBLEM XV. To make an Oblique Angled Triangle, two Sides and their contained Angle being given. Fig. 36.


Suppose the side BC 109, the side BD 76, and the Angle at B $101030^{\prime}$.

Draw the side BC in length 109; at B make an Angle of $101^{\circ} 30^{\prime}$, and draw the side BD in length 76; draw a line from D to $\mathbf{C}$ and it is done.

PROBLEM XVI. To make a Square. lig. 37.


Draw the Line AB the length of the proposed Square; from $B$ erect a Perpendicular to $\mathbf{C}$ and make it of the same length as AB ; from A and C , with the same distance in the dividers, describe Arches intersecting each other at D , and draw the Lines AD and DC.

PROBLEM XVII. To make a Parallelogram. Fig. 38.

Fig. 38.


Draw the Line AB equal to the longest side of the Parallelogram; on $\mathbf{B}$ erect a Perpendicular the length of the shortest side to $\mathbf{C}$; from $\mathbf{C}$, with the longest side, and from $\mathbf{A}$, with the shortest side, describe Arches intersecting each other at D , and draw the Lines AD and CD.

PROBLEM XVIII. To describe a Circle, which shall pass through any three given Points, not lying in a Right Line, as A, B, D. Fig. 43.


Draw Lines from $\mathbf{A}$ to $\mathbf{B}$ and from $\mathbf{B}$ to $\mathbf{D}$; bisect those Lines by Problem II. and the Point where the bisecting Lines intersect each other, as at $\mathbf{C}$, will be the centre of the Circle.

PROBLEM XIX. To find the centre of a Circle.
By the last Problem it is plain, that if three Points be any where taken in the given Circle's Periphery, the centre of the Circle may be found as there taught.

Directions for constructing irregular Figures of four or more sides may be found in the following Treatise on Surveying

## TRIGONOMETRY.

TRIGONOMETRY is that part of practical Geometry by which the Sides and Angles of Triangles are measured; whereby three things being given, either all sides, or sides and Angles, a fourth may be found; either by measuring with a Scale and Dividers, according to the Problems in Geometry, or more accurately by calculation with Logarithms, or with Natural Sines.

Trigonometry is divided into two Parts, Rectangular and Oblique-angular.

## PART I.

## RECTANGULAR TRIGONOMETRY.

This is founded on the following methods of applying a Triangle to a Circle.

Fig. 44.
PROPOSITION I. In every Right Angled Triangle, as ABC, Fig. 44, it is plain from Fig. 7. compared with the Geometrical definitions to which that Figure refers, that if the Hypothenuse AC be made Radius, and with it an Arch of a Circle be described from each end, BC will be the Sine of the Angle at A, and $A B$ the Sine of the Angle at $C$; that is, the Legs will be Sines of their opposite Angles.


Fig. 45.

PROPOSITION II. If one Leg, AB, Fig. 45, be made Radius, and with it on the Point A an Arch be described, then BC, the other Leg, will be the Tangent and AC the Secant of the Angle at A; and if BC be made Radius, and an Arch be described with it on the Point $C$, then $A B$ will be the Tangent and AC the Se cant of the Angle at C ; that is, if one Leg
 be made Radius the other Leg will be a Tangent of its opposite Angle, and the Hypothenuse a Secant of the same Angle.

Thus, as different sides are made Radius, the other sides acquire different names, which are either Sines, Tangents or Secants.

As the sides and Angles of Triangles bear a certain proportion to each other, two sides and one Angle, or one side and two Angles being given, the other sides or Angles may be found by instituting Proportions, according to the following Rules.

Rule I. To find a side, either of the sides may be made Radius, then institute the following Proportion:

As the name of the side given, which will be either Radius, Sine, Tangent or Secant ;
Is to the length of the side given;
So is the name of the side required, which also will be either Radius, Sine, Tangent or Secant ;
To the length of the side required.
Rule II. To find an Angle one of the given sides must be made Radius, then institute the following Proportion :

As the length of the given side made Radius;
Is to its name, that is Radius;
So is the length of the other given side;
To its name, which will be either Sine, Tangent or Secant.
Having instituted the Proportion, look for the corresponding Logarithms, in the Logarithms for numbers for the length of the sides, and in the Table of Artificial Sines, Tangents and Secants, for the Logarithmic Sine, Tangent or Secant.

Having found the Logarithms of the three given Terms, add together the Log. of the second and third Terms, and from their sum subtract the Log. of the first Term, the Remainder will be the Log. of the fourth Term, which, seek in the Tables and find its corresponding Number or Degrees and Minutes.

See the Introduction to the Table of Logarithms; which should be attentively studied by the Learner before he proceeds any further.

Note. The Logarithm for Radius is always 10, which is the Logarithmic Sine of $90^{\circ}$, and the Logarithmic Tangent of 450.

The preceding Propositions and Rules being duly attended to, the solution of the following Cases of Rectangular Trigono. metry will be easy.

## CASE I.

Fig. 39.

The Angles and Hypothenuse given to find the Legs. Fig.' 39.


In the Triangle ABC, given the Hypothenuse AC 25 Rods or Chains; the Angle at A $35^{\circ} 30^{\prime}$ : and consequently the Angle at C $54 \circ 30$ : to find the Legs.

Making the Hypothenuse Radius, the Proportions will be :
To find the Leg AB.

| As Radius - | 10.00000 | As Radius fo find the | 10.00000 |
| :---: | :---: | :---: | :---: |
| : Hyp. AC, 25. | 1.39794 | : Hyp. AC, 25 | 1.39794 |
| : : Sine ACB, $54^{\circ} 30^{*}$ | 9.91069 | : : Sine CAB, $35^{\circ} 30^{\prime}$ | 9.76395 |
|  | 11.30863 | ; | 11.16189 |
|  | 10.00000 |  | 10.00000 |
| : Leg AB, 20.35 | 1.30863 | : Leg BC, 14.52 | 1.16189 |

Note. When the first.Term is Radius, it may be subtracted by cancelling the first figure of the Sum of the other two Terms.

Making the Leg AB Radius, the Proportions will be :

To find the Leg AB.
As Secant CAB, 350 30
: Hyp. AC, 25
: : Radius
: Leg AB, 20.35

To find the Leg BC. As Secant CAB, $35^{\circ} 30^{\prime}$ : Hyp. AC, 25
: : Tangent, CAB, $35^{\circ} 30^{\prime}$
: Leg BC, 14.52

Making the Leg BC Radius, the Proportions will be:

To find the $\operatorname{Leg} \mathrm{AB}$.
As Secant ABC, $54{ }^{\circ} 30^{\prime}$
: Hyp. AC, 25
: : Tangent ACB, $54^{\circ} 30^{\prime}$
: Leg AB, 20.35

To find the Leg BC. As Secant ACB, $54^{\circ} 30^{\prime}$
: Hyp. AC, 25
:: Radius
: Leg. BC, 14.52

The Logarithms of the four last Proportions being looked out, and added and subtracted according to the Rule, the result will be found to be the same as the two first Proportions.

## By Natural Sines.

This Case may be solved by Natural Sines,* according to the following Proportions:

As Unity or 1, is to the length of the Hypothenuse, so is the Natural Sine of the smallest Angle, to the length of the shortest Leg. Or, so is the Natural Sine of the largest Angle, to the length of the longest Leg.

Or, which is the same thing, multiply the Natural Sines of the two Angles by the Hypothenuse, the Products will be the length of the two Legs.

Example.

Nat. Sine of $35^{\circ} 30^{\prime}$
0.58070

Hyp. 25
$\underline{290350}$

116140
14.51750

Leg BC 14.52

Nat. Sire of $54030^{\prime}$
0.81412

Hyp. 25
407060
162824
20.35300

Leg AB 20.35

Note. The third Decimal figure in the first Product being 7, the preceding figure may be called one more than it is, viz. 2. And whenever in any Product, \&c. there are more places of Decimals than you wish to work with, if the one at the right hand of the last which you wish to retain is more than 5, add a Unit to the last, because a greater number than 5 is more than half.

As the Table of Artificial or Logarithmic Sines, Tangents and Secants, contained in this book, is calculated only for every 5 Minutes of a Degree, whenever any Question is to be solved where the Minutes cannot be found in that Table; or where the length of the Hypothenuse is such a number as cannot be found in the Table of Logarithms for Numbers, the Question may be solved by Natural Sines as above taught.

[^1]
## CASE II.

Fig. 40.


The Angles and one Leg given, to find the Hypothenuse and the other Leg. Fig. 40.

In the Triangle ABC, given the Leg AB 325, the Angle at A $33 \circ 15^{\prime}$ and the Angle at C 560 45' : to find the Hypothenuse and the Leg BC.
Making the given Leg Radius, the Proportions will be:

| To find the Hypothenuse |  | To find the Leg BC. |  |
| :---: | :---: | :---: | :---: |
| As Radius, | 10.00000 | As Radius, | 10.00000 |
| : Leg AB, 325 | 2.51188 | : Leg AB, 325 | 2.51188 |
| $\therefore$ : Sec. CAB, $33^{\circ} \mathbf{1 5}^{\prime}$ | 10.07765 | : : Tan. CAB, $33^{\circ} 15^{\prime}$ | 9.81666 |
| : Hyp. 388.6 | 12.58953 | : Leg BC, 213.1 | 12.32854 |

Note. Reject the first figure, which is the same as subtracting Radius, and seek the numbers corresponding to the other figures.
Making the Leg BC Radius, the Proportions will be;
To find the Hypothenuse To find the Leg BC.

As Tang. ACB, $56{ }^{\circ} 45^{\prime}$
: Leg AB, 325
$:$ : Sect. ACB. $56{ }^{\circ} 45^{\prime}$
: Hyp. 388.6
As Tang. ACB, $56{ }^{\circ} \mathbf{4 5}^{\prime}$
: Leg AB, 325
: : Radius
: Leg BC, 213.1
Making the Hypothenuse Radius, the Proportions will be ;
To find the Hypothenuse. $\quad$ To find the Leg BC.
is Sine BCA, $56^{\circ} 45^{\prime}$
: Leg AB, 325
: : Radius
: Hyp. 388.6

As Sine BCA, $56{ }^{\circ} 45^{\prime}$
: Leg AB, 325
$\mp:$ Sine BAC, $33015^{\prime}$
: Leg BC, 213.

Note. If the Leg BC had been given, instead of the Leg AB, the Proportions would have been the same mutatis mutandis.

## By: Natural Sines.

To solve this Case by Natural Sines, institute the following Proportions:

To find the Hypothenuse. As the Natural Sine of the Angle opposite the given Leg, is to the length of the Leg, so is Unity or 1 , to the length of the Hypothenuse.

Or, which is the same thing, Divide the given Leg by the Natural Sine of its opposite Angle, and the Quotient will be the Hypothenuse.

To find the other Leg. As the Natural Sine of the Angle opposite the given Leg, is to the length of the given Leg, so is the Natural Sine of the Angle opposite the other Leg, to the length of the other Leg.

## Example.

Given Leg 325.' Nat. Sine of $56^{\circ} 45^{\prime}$, the Angle opposite the given Leg 0.83629. Nat. Sine of $33{ }^{\circ} 15^{\prime}$, the Angle opposite the other Leg 0.54829 .

As $0.83629: 325:: 1: 388.6$
A's $0.83629: 325:: 0.54829: 213.07$.

## CASE III.

Fig. 41.

The Hypothenuse and one Leg given, to find the Angles and the other Leg. Fig. 41.


In the Triangle ABC, given the Hypothenuse $\mathbf{A C} 50$ and the Leg AB 40, to find the Angles and Leg BC.

Making the Hypothenuse Radius, the Proportion to find the Angle ACB will be :

| As Hyp. 50 | 1.69897 |
| :---: | :---: |
| : Radius | 10.00000 |
| $:: \mathbf{L e g ~ A B , ~} 40$ | 1.60206 |
|  | 11.60206 |
|  | 1.69897 |
| : Sine ACB, $53010^{\prime}$ | 9.90309 |

The Angle ACB being $53^{\circ} 10^{\prime}$ the other is consequently $36^{\circ} 50^{\prime}$.

Making the Leg AB Radius, the Angle ${ }^{\text {BAC may }}$ be found by the following Proportion;


The Angles, being found, the Leg BC may be found by either of the preceding Cases. It is $\mathbf{3 0}$.

## By $\mathfrak{\mathcal { N }}$ atural Sines.

The Angle opposite the given Leg may be found by the following Proportion;
As the Hypothenuse is to Unity or 1, so is the given leg to the Nat. Sine of its opposite Angle.

Or, which is the same thing, Divide the given Leg by the Hypothenuse, and the Quotient will be the Nat. Sine.

## Example.

The Leg AB 40 divided by the Hypothenuse 50 quotes 0.80000 which looked in the Table of Nat. Sines, the nearest corresponding number of Degrees and Minutes will be found to be $53 \circ 8^{\prime}$, the Angle ACR.

Note. The reason why the Angle as found by Nat. Sines differs 2 Minutes from the Angle as found by Logarithms, is that the Table of Logarithmic Sines, \&c. contained in this book, is calculated only for every 5 minutes. By a Table of Logarithmic Sines, \&c. calculated for every minute, the Angle will be found the same.

## By the Square Root.

In this Case the required Leg may be found by the Square Loot, without finding the Angles; according to the following. Proposition;

In every Right Angled Triangle, the Square of the Hypothenuse is equal to the Sum of the Squares of the two Legs. Hence,

The Square of the given Leg being subtracted from the Square of the Hypothenuse, the Remainder will be the Square of the required Leg.

As in the preceding Example; the Square of the Leg AB 40 is 1600 ; this subtracted from the Square of the Hypothenuse 50 which is 2500 , leaves 900 , the Square of the Leg BC, the Square Root of which is 30, the length of Leg BC as found by Logarithms:

## CASE IV:

The Legs given to find the Angles and $\boldsymbol{H}_{y}$ * pothenuse. Fig. 42.

Fig. 42.


In the Triangle ABC, given the Leg AB 78.7 and the Leg BC 89 ; to find the Angles and Hypothenuse.

Making the Leg AB Radius, the Proportion to find the Angle BAC will be ;

| As Leg AB, 78.7 : Radius <br> $::$ Leg BC, 89 | 1.89597 |
| :---: | :---: |
|  | 10.00000 |
|  | 1.94939 |
|  | 11.94939 |
|  | 1.89597 |
| : Tang. BAC, 480 | 10.05342 |

The Angle ACB is consequently $41030^{\prime}$.
Making the Leg BC Radius, the Proportion to find the Angle BCA will be the same as the above, mutatis mutandis.

The Angles being found, the Hypothenuse may be found lyg. Case II. It is nearest 119.

## By the Square Root.

In this Case the Hypothenuse may be found by the Square Root, without finding the Angles; according to the following Proposition.

In every Right Angled Triangle, the sum of the Squares of the two Legs is equal to the Square of the Hypothenuse.

In the above Example; the Square of AB 78.7 is 6193.69, the Square of BC 89 is 7921 ; these added make 14114.69 the Square Root of which is nearest 119.

## By Natural Sines.

The Hypothenuse being found by the Square Root, the Angles may be found by Nat. Sines, according to the preceding Case.

Hyp. Leg. BC. Nat. Sine.
119) $89.00000(74789$

83 3....

| 570 | The nearest degrees and minutes cor- |
| ---: | ---: |
| 476 | Tesponding to the above Nat. Sine are 480 <br> 24', for the Angle BAC. The difference |
| 940 <br> between this and the Angle as found by <br> Logarithms is occasioned by dividing by |  |
| 1070 | 119, which is not the exact length of the <br> Hypothenuse, it being a Fraction too much |
| 952 |  |

1180
1071
109

## PART II.

Oblique Trigonometry.
The solution of the two first Cases of Oblique Trigonometiry drepends on the following Proposition.

In all Plane Triangles, the Sides are in proportion to each other as the Sines of their opposite Angles. That is, as the

Sine of one Angle is to its opposite Side, so is the Sine of another Angle to its opposite Side. Or, as one Side is to its opposite Angle, so is another Side to the Sine of its opposite Argle...

Note. When an Angle exceeds $90^{\circ}$ make use of its Supplement, which is what it wants of $180^{\circ}$. As the Sine of $90^{\circ}$ is the greatest possible Sine, the Sine of any number of Degrees will be as much less as that number of Degrees. exceeds 90 , and will be the same as the Sine of the Supplement of that number of Degrees; thus, the Sine of $100^{\circ}$ is the same as the Sine of 800 , and the Sine of $130^{\circ}$ the same as the Sine of $500, \& c$.

## CASE I.

The Angles and one Side given, to find the other Sides. Fig. 47.


In the Triangle ABC, given the Angle at B 480, the Angle at $\mathbf{C} 72^{\circ}$, consequently the Angle at $\mathbf{\Lambda} 60^{\circ}$, and the Side AB 200, to find the Sides AC and BC.


## By $\mathcal{N}$ atural Sines.

As the Nat. Sine of the Angle opposite the given Side is to the given Side, so is the Nat. Sine of the Angle opposite either of the required Sides to that required Side.

Given Side 200 ; Nat. Sine of $\mathbf{7 2 0}$, its opposite Angle, 0.95115 ; Nat. Sine of ABC $480,0.74334$; Nat. Sine of BAC $600,0.86617$.

As 0.9511 : 200 : : 0.74334 : 156
As 0.95115 : $200: \mathbf{0 . 8 6 6 1 7}: 182$.

## CASE II.

Fig. 48.

Tivo Sides, and an Angle opposite to one of them given, to find the other angles and Side. Fig. 48.


In the Triangle ABC, given the Side AB 240, the Side BC 200 , and the Angle at A $46^{\circ} 30^{\prime}$; to find the other Angles and the Side AC.

| To find the Angle ACB. |  | Angle at ${ }_{\mathbf{C}}^{\mathbf{A}}$ | $\begin{array}{r} 46^{\circ} 30^{\prime} \\ 6030 \end{array}$ |
| :---: | :---: | :---: | :---: |
| As Side BC, 200 | 2.30103 |  |  |
| : Sine BAC, $46^{\circ} \mathbf{3 0}$ | 9.86056 |  |  |
| : : Side AB, 240 | 2.38021 |  |  |
|  | 12.24077 |  | 107.00 |
|  | 2.30103 | Sum of the three Angles | $180^{\circ}$ |
|  |  | Sum of two | 107 |
| : Sine ACB, $60{ }^{\circ} 30^{\prime}$ | 9.93974 |  |  |
|  |  | Angle at B | 73 |

The Side AC will be found by Case I. to be nearest 253.
Note. If the given Angle be Obtuse, the Angle sought will be Acute; but if the given Angle be Acute, and opposite a given lesser Side, then the Angle found by the operation may be either Obtuse or Acute. It ought therefore to be mentioned which it is, by the conditions of the question.

## By $\mathcal{N}$ atural Sines.

As the Side opposite the given Angle is to the Nat. Sine of that Angle, so is the other given Side to the Nat. Sine of its opposite Angle.

One given Side 200, Nat. Sine of $46^{\circ} 30^{\prime}$, its opposite Angle, 0.72537 , the other given Side 240.

$$
\text { As } 200: 0.72537:: 240: 0.87044=60030^{\prime} \text {. }
$$

H

## CASE III.

Two Sides and their contained Angle given, to find the other Angles and Side. Fig. 49.

Fig. 49


The solution of this Case depends on the following Proposition.

In every Plane Triangle, as the sum of any two Sides is to their difference, so is the Tangent of half the sum of the two opposite Angles to the Tangent of half the difference between them. Add this half difference to half the sum of the Angles and you will have the greater Angle, and subtract the half difference from the half sum and you will have the lesser Angle.

In the Triangle ABC, given the Side AB 240, the Side AC 180, and the Angle at A 36040 to find the other Angles and Side.

| Side $\mathbf{A B}$ | - | 240 | $\mathbf{A B}$ | - | 240 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{A C}$ | - | 180 | $\mathbf{A C}$ | - | 180 |
|  |  |  |  |  |  |
| Sum of the two Sides |  |  | Difference |  |  |

The given Angle BAC $36^{\circ} 40^{\prime}$, subtracted from $180^{\circ}$, leaves $143^{\circ} 20^{\prime}$ the sum of the other two Angles, the half of which is $71040^{\prime}$.

As the sum of two Sides, $420 \quad$ - $\quad$ 2.62326
Their difference 60 - $\quad$ - $\quad 1.77815$
: : Tangent half unknown Ang. $71040^{\prime} \quad$ - 10.47969
12.25784
2.62325
: Tangent half difference, $23020^{\prime}$
9.63459

The half sum of the two unknown Angles,
$71040^{\prime}$
The half difference between them,
2320
Add, gives the greater Angle ACB
9500
Subtract, gives the lesser Angle ABC
4820
The Side BC may be found by Case I or IF.

## CASE IV.

Fig. 50.

The three Sides given to find the Angles. Fig. 50.


The solution of this Case depends on the following Proposition.

In every Plane Triangle, as the longest Side is to the sum of the other two Sides, so is the difference between those two Sides to the difference between the Segments of the longest Side, made by a Perpendicular let fall from the Angle opposite that Side.

Half the difference between these Segments, added to half the sum of the Segments, that is, to half the length of the longest Side, will give the greatest Segment; and this half difference sultracted from the haif sum will be the lesser Segment. The Triangle being thus divided, becomes two Right Angled Triangles, in which the Hypothenuse and one Leg are given to find the Angles.

In the Triangle ABC, given the Side AB 105, the Side AC 85, and the Side BC 50, to find the Angles.

| Side $\begin{array}{r}\text { AC } \\ \text { BC }\end{array}$ | $\begin{aligned} & 85 \\ & 50 \end{aligned}$ | AC | -- | 85 50 |
| :---: | :---: | :---: | :---: | :---: |
| Sum of the two Sides | 135 |  | Differe | 35 |
| As the longest Side AB, 105 : Sum of the other two Sides, 135 : : Difference between those Sides, 35 |  |  |  | 2.02119 |
|  |  |  |  | 2.13033 |
|  |  |  |  | 1.54407 |
|  |  |  |  | 3.67440 |
|  |  |  |  | 2.02119 |
| : Difference between the Segments, 45 |  |  |  | 1.65321 |
| Half the Side AB <br> Half the difference of the Segments |  |  |  | 52.5 |
|  |  |  | - | 22.5 |
| Add, gives the greater Segment AD |  |  |  | 75.0 |
| Subtract, gives the lesser Segment BD |  |  |  | 30.0 |

Thus the Triangle is divided into two Right Angled Triangles, ADC and BDC ; in each of which the Hypothenuse and one Leg are given to find the Angles.


The Angle DCA $61055^{\prime}$ subtracted from $90{ }^{\circ}$ leaves the Angle CAD $2805^{\prime}$.

The Angle DCB $366^{\circ} 50^{\prime}$ subtracted from $90^{\circ}$ leaves the Angle CBD $53{ }^{\circ} \mathbf{1 0}^{\prime}$.

The Angle DCA $61055^{\prime}$ added to the Angle DCB 36050 gives the Angle ACB 980 45'.

This Case may also be soived according to the following Proposition.

In every Plane Triangle, as the Product of any two Sides containing a required Angle is to the Product of half the sum of the three Sides, and the difference between that half sum and the Side opposite the Angle required, so is the Square of Radius to the Square of the Co-Sine of half the Angle required.

Those who make themselves well acquainted with Trigonometry will find its application easy to many useful purposes, particularly to the mensuration of Heights and Distances; called Altimetry and Longimetry. These are here omitted, because, as this work is designed principally to teach the Art of common Field-Surveying, it was thought improper to swell its size, and consequently increase its price, by inserting any thing not particularly connected with that Art.

It is recommended to those who design to be Surveyors to study Trigonometry thoroughly; for though a common field may be measured without an acquaintance with that Science, yet many cases will occur in practice where a knowledge of it will be found very beneficial; particularly in dividing Land, and ascertaining the boundaries of old Surveys. Indeed no one who is ignorant of Trigonometry, can be an accomplished surveyor.

## SURVEYING.

SURYEYING is the Art of measuring, laying out, and dividing Land,

## PART I.

Measuring Land.

The most common measure for Land is the Acre; which contains 160 Square Rods, Poles or Perches; or 4 Square Roods, each containing 40 Square Rods.

The instrument most in use, for measuring the Sides of Fields, is Gunter's Chain, which is in length 4 Rods or 66 Feet; and is divided into 100 equal parts, called Links, each containing 7 Inches and 92 Hundredths. Consequently, 1 Square Chain contains 16 Square Rods, and 10 Square Chains make 1 Acre.

In small Fields, or where the Land is uneven, as is the case with a great part of the Land in New-England, it is better to use a Chain of only two Rods in length; as the Survey can be more accurately taken.

## SECTION I.

## Preliminary Problems.

PROBLEM I. To reduce Two Rod Chains to Four Rod Chains.

Rule. If the number of Two Rod Chains be even, take half the number for Four Rod Chains, and annex the Links if any : thus, 16 Two Rod Chains and 37 Links make 8 Four Rod Chains and 37 Links.

But if the number of Chains be odd, take half the greatest even number for Chains, and for the remaining number add 50 to the Links: Thus, 17 Two Rod Chains and 42 Links make 8 Four Rod Chains and 92 Links.

PROBLEM II. To reduce Tivo Rod Chains to Rods and Decin.al Parts.

Rule. Multiply the Chains by 2, and the Links by 4, which will give Hundredths of a Rod: thus, 17 Two Rod Chains and 21 Links make 34 Rods and 84 Hundredths; expressed thus, 34.84 Rods.

If the Links exceed 25, -add-1 to the number of Rods and multiply the excess by 4 : thus, 15 Two Rod Chains and 38 Links make 31.52 Rods.

PROBLEM III. To reduce Four Rod Chains to Rods and Decimal parts.

Rule. Multiply the Chains, or Chains and Links, by 4 ; the Product will be Rods and Hundredths: thus, 8 Chains and 64 Links make 34.56 Rods.

Note. The reverse of this Rule, that is, dividing by 4, will reduce Rods and Decimals to Chains and Links : thus, 105.12 Rods make 26 Chains and 28 Links.
PROBLEM IV. To reduce Square Rods to Acres.
Rule. Divide the Rods by 160, and the Remainder by 40 , if it exceeds that number, for Roods or Quarters of an Acre: thus, 746 Square Rods make 4 Acres, 2 Roods, and 26 Rods.

PROBLEM V. To reduce Square Chains to Acres.
Rule. Divide by 10 ; or, which is the same thing, cut off the Right hand figure : thus, 1460 Square Chains make 146 Acres; and 846 Square Chains make 84 Acres and 6 Tenths.

PROBLEM VI. To reduce Square Links to Acres.
Rule. Divide by 100000 ; or, which is the same thing, cut off the 5 Right-hand figures : thus, 3845120 Square Linksmake 38 Acres and 45120 Decimals.

Vote. When the Area of a Field, by which is meant its Superficial Contents, is expressed in Square Chains and Links, the whole may be considered as Square Links, and the number of Acres contained in the Field, found as above. Then multiply the figures cut off by 4, and again cut off 5 figures, and you have the Roods; multiply the figures last cut of ${ }^{\circ}$ by 40 , and again cut off 5 figures, and you have the Rods.
Example. How many Acres, Roods, and Rods, are there in 156 Square Chains and 3274 Square Links ?
2) 53096

40
21) 23840

Answer. 15 Acres 2 Roods and 21 Rods.

Problems for finding the Area of Right Lined Figures, and also of Circles.

PROBLEM VIL. To find the Area of a Square or Parallelogram.

Rule. Multiply the length into the breadth; the Product will be the Area.

PROBLEM VIII. To find the Area of a Rhombus or Rhomboides.

Rule. Drop a Perpendicular from one of the Angles to its opposite Side, and multiply that Side into the Perpendicular ; the Product will be the Area.

PROBLEM IX. To find the Area of a Triangle.
Rule 1. Drop a Perpendicular from one of the Angles to its opposite Side, which may be called the Base; then multiply the Base by half the Perpendicular, or the Perpendicular by half the Base; the Product will be the Area. Or, multiply the whole Base by the whole Perpendicular, and half the Product will be the Area.

Rule 2. If it be a Right Angled Triangle, multiply one of the Legs into half the other; the Product will be the Area. Or, multiply the two Legs into each other, and half the Product will be the Area.

Rule 3. When the three Sides of a Triangle are known, the Area may be found Arithmetically, as follows:

Add together the three Sides; from halt their Sum subtract each side, noting down the Remainders; multiply the half Sum by one of those Remainders, and that Product by another Remainder, and that Product by the other Remainder ; the Square Root of the last Product will be the Area.
Example. Suppose a Triangle whose three Sides are 24, 20, and 18 Chains. Demanded the Area.
$24+20+18=62$, the Sum of the three Sides, the half of which is 31 . From 31 subtract 24, 20, and 18; the three Remainders will be 7, 11 , and 13 .
$31 \times 7=217 ; \quad 217 \times 11=2387 ; \quad 2387 \times 13=31031$, the Square Root of which is $\mathbf{1 7 6 . 1}$, or 17 Acres 2 Roods and 17 Rods.

## By Logarithms.

As the Addition of Logarithms is the same as the Multiplication of their corresponding Numbers; and as the Number answering to the one half of a Logarithm will be the Square Root of the Number corresponding to that Logarithm: it follows, That if the Logarithm of the half Sum of the three Sides and the Logarithms of the three Remainders be added together,
the Number corresponding to one half the Sum of those Log. arithms will be the Area of the Triangle.

| The half Sum, 31 |  | - | 1.49136 |
| :--- | :--- | :--- | :--- |
| The first Remainder, 7 | - | - | 0.84510 |
| The second Remainder, 11 | - | - | 1.04139 |
| The third Remainder, 13 |  |  | 1.11394 |
| The Square of the Area, 31000 | - | - | 4.49179 |
| Area 176 Square Chains | - | - | 2.24589 |

Role 4. When two Sides of a Triangle and their contained Angle, that is, the Angle made by those Sides, are given, the Area may be found as follows:

Add together the Logarithms of the two Sides and the Logarithmic Sine of the Angle; from their sum subtract the Logarithm of Radius, the Remainder will be the Logarithm of double the Area.

Example. Suppose a Triangle one of whose Sides is 10.5 Rods and another 85, and the Angle contained between them 280 5'. Demanded the Area.

| One Side, 105 | - | - | - | - |
| :--- | :--- | :--- | :--- | :--- |
| The other Side, 85 | - | - | - | 1.02119 |
| Sine Angle, $2805^{\prime}$ | - | - | - | - |
|  |  |  | 9.672842 |  |
|  |  | - | - | 13.62341 |
| Subtract Radius | - | - | 10.00000 |  |
|  |  |  |  |  |
| Double Area, 4200 Rods | - | - | - | 3.62341 |

.Anstwer. 2100 Rods.
Note. Radius may be subtracted by cancelling the Left-hand figure of the Index, or subtracting 10, without the troable of setting down the $\mathrm{Ci}^{4}$ phers.

## By Natural Sines.

Multiply the two given Sides into each other, and that Product by the Natural Sine of the given Angle; the last Product will be double the Area of the Triangle.

Nat. Sine of the Angle $28^{\circ} 5^{\prime} 0.47076$
$105 \times 85=8925$, and $8925 \times 0.47076=4201$ the double Area of the Triangle.

PROBLEM X. To find the Area of a Trapezoid.

Rule. Multiply half the Sum of the two parallel Sides by the perpendicular distance between them, or the sum of the two parallel Sides by half the perpendicular distance, the product will be the Area.

PROBLEM XI. To find the Area of a Trapezium, or irregular Four Sided Figure.

Rule. Draw a Diagonal between two opposite Angles, which will divide the Trapezium into two Triangles. Find the Area of each Triangle and add them together. Or, multiply the Diagonal by half the Sum of the two perpendiculars let fall upon it, or the Sum of the two perpendiculars by half the Diagonal, the product will be the Area.

Note. Where the length of the four Sides and of the Diagonal is known, the Area of the two Triangles, into which the Trapezium is divided, may be calculated Arithmetically, according to Prob. IX. Rule 3.

PROBLEM XII. To find the Area of a Figure containing more than Four Sides.

Rule. Divide the Figure into Triangles, and Trapezia, by drawing as many Diagonals as are necessary, which Diagonals must be so drawn as not to intersect each other ; then find the Area of each of the several Triangles or Trapezia, and add them together; the sum will be the Area of the whole Figure.

Note. A little practice will suggest the most convenient way of drawing the Diagonals; but whichever way they are drawn, provided they do not intersect each other, the whole Area will be found the same.

## PROBLEM XIII. Respecting Circles.

Rule 1. If the Diameter be given the Circumference may be found by one of the following proportions : as 7 is to 22, or more exactly, as 113 is to 355 , or in Decimals, as 1 is to 3.14159, so is the Diameter to the Circumference.

Rule 2. If the Circumference be given the Diameter may be found by one of the following proportions: as 22 is to 7, or as 355 is to 113 , or as 1 is to 0.31831 , so is the Circumference to the Diameter.

Rule 3. The Diameter and Circumference being known, multiply half the one into half the other, and the product will be the Area.

Rule 4. From the Diameter only, to find the Area: multiply the Square of the Diameter by 0.7854 , and the product will be the Area.

Rule 5. From the Circumference only to find the Area:
multiply the Square of the Circumference by 0.07958 , and the product will be the Area.

Rule 6. The Area being given to find the Diameter : divide the Area by 0.7854, and the Quotient will be the Square of the Diameter; from this extract the Square Root, and you will have the Diameter.

Rule 7. The Area being given to find the Circumference : divide the Area by 0.07958 , and the quotient will be the Square of the Circumference ; from this extract the Square Root, and you will have the Circumference.

## SECTION II.

The following Cases teach the most usual methods of taking the Survey of Fields; alsc, how to protract or draw a Plot of them, and to calculate their Aréa.

Vote. The Field Book is a Register containing the length of the Sides of a Field, as found by measuring them with a Chain; also the Bearings or Courses of the Sides, or the Quantity of the several Angles, as found by a Compass or other instrument for that purpose; together with such Remarks as the Surveyor thinks proper to make in the Field.

## CASE I.

To survey a Triangular Field.
Measure the Sides of the Field with a Chain, and enter their several lengths in a Field Boor, protract the Field on Paper, and then find the Area by Рrob. IX. Rule 1. Or, without plotting the Field, calculate the Area by Prob. IX. Rule 3.

Fig. 46.


> 9600
> 7200
> 16800

## Acres 17)61600

Roods 2) 46400
40
Rods 18) 56000

$$
\begin{gathered}
\text { Acres Roods } \quad \begin{array}{c}
\text { Rods } \\
\text { Area } 17-2
\end{array}-18.56
\end{gathered}
$$

Note. When there are ciphers at the Right Hand of the Links, they may be rejected; remembering to cut off a proper number of figures according to Decimal Rules.

Observe, That in measuring with a Chain, slant or inclined Surfaces, as the Sides of Hills, should be measured horizontally, and not on the Plane or Surface of the Hill; otherwise, a survey cannot be accurately taken. To effect this, the lower end of the Chain must be raised from the ground, so as to have the whole in a horizontal Line; and the end thus raised must be directly over the Point where the Chain begins or ends, according as you are ascending or descending a Hill; which Point may be ascertained by a Plummet and Line.

## CASE II.

To survey a Field in the form of a Trapezium.
Measure the several sides, and a Diagonal between two opposite Angles; protract the Field, and find the Area by Рroblem XI. Or, without protracting the Field, calculate the Area according to the Note at the end of that Problem.

Fig. 51.


To protract this Trapezium.
Draw the Side AB the given length; with the Diagonal AC 28 and the Side BC 11.70 describe cross Arches as at C, from $A$ and $B$ as Centres; and the point of intersection will represent that corner of the Field : then, with the Side CD 21.50 and the Side AD 14.70, describe cross Arches as at D, from A and C as Centres; and the point of intersection will represent that corner of the field.


Note. The Perpendiculars need not be actually drawn; their length may be abtained as follows: From the Angle opposite the Diagonal open the Dividers so as when one Foot is in the angular Point, as at B, the other, being moved backwards and forwards, may just toucli the Diagonal at a, and neither go the least above or below it ; that distance in the Dividers being measured on the Scale will give the length of the Perpendicular.

## CASE III.

To survey a Field which has more than four Sides, by the Chain only.

Measure the several Sides, and from some one of the Angles, from which the others may be seen, measure Diagonals to
them; draw a Plot of the Field, and find the Area by ProbLem XII.

FIELD BOOK. See Fig. $\mathbf{~ 5 2 .}$
Fig. 52.



To protract this Field.
Draw the side $A B$, making it the given length 30.60 ; with the Diagonal AC 45 and the Side BC 20.40, describe cross Arches as at C, from the Poirts A and B as Centres, and the Point of intersection will represent that Corner of the Field : draw the Side BC and the dotted Diagonal AC ; with the Diagonal AD 35 and the Side CD 22.40, describe cross Arches as at D , from the Points A and C , and draw the Side CD and the dotted Diagonal AD. Proceed in this manner till all the Sides, and Diagonals are drawn.

To find the Area.
The Field, being plotted, may be divided into one Trapezium and two Triangles; the Area of which is calculated as follows :-


## REMARKS.

As each of the Sides of the several Triangles, into which the preceding Plot of a Field is divided, is known from the Field Book, the Area of the Field may be calculated Arithmetically, by finding the Area of each Triangle, according to Prob. IX. Rule 3 ; and then adding the whole together. This method, though it may require more time, is preferable to the other, because more accurate. : Indeed it is always better to calculate the Area of a Field Arithmetically than Geometrically; for in the former: no two persons can differ in their calculations; whereas, according to the latter, which is the common method of casting the contents of a Field, it is hardly to be expected that any two persons will perfectly agree. The inaccuracy of Scales, and the difficulty of determining with precision the length of Sides and Perpendiculars with a Scale and Dividers, render it almost if not quite impossible to obtain the exact Area of a Field, in the method commonly practised, even if the Surveyor has measured it accurately in the first place.

Other methods of taking the Survey of a Field by the Chain only are mentioned in some Treatises on this subject, but they
are rather curious than useful; and it is much better to ascertain the Angles by an accurate Compass, or some instrument designed purposely for taking Angles.

## CASE IV.

## To Survey a Field with a Chain and Compass.

Measure the length of the Sides with a Chain, and take their bearing or Course with a Compass;* enter these in a Field Book; plot the Field on paper, and calculate the Area by the directions already given.

To protract or draw a Map of a Field.
Draw a Line to represent a Meridian, or North and South Line, from which lay off a Bearing or Course of the first Side of the Field, with a Protractor or from a Line of Chords; and from a Scale of equal parts, measure the length of the Side and draw a Line to represent it.

At the end of this Line draw a Line parallel to the Meridian Line, and then lay off the second Side of the Field as before taught; proceed in the same manner to draw parallel Lines, and lay off the several Sides till the whole is protracted.

In protracting' a Field, let the top of the paper be considered as North, the bottom. South, the right hand East; and the left hand West; lay the Course to the right or left of the Meridian Line, according as it is East or West, and from the upper or lower part of the Line, according as it is North or South.

In all protractions, if the end of the last distance falls exactly on the point from which you began, the Course also being right, the Field work and protraction are truly taken and performed; if not, an error must have been committed in one of them: in such cases, make a second protraction; if this agrees with the former, it is to be presumed the fault is in the Field work; a re-survey must then be taken.

[^2]

## REMARKS.

The Sides of the several Triangles into which the Plot of a Field is divided may be found by Trigonometry; and then the Area of each Triangle may be calculated according to Рrob. IX. Rule 3. The Sum of the Areas of the several Triangles will be the Area of the whole Field. This method may require more time, but it is perfectly accurate, since no dependence is placed on the uncertain measurement of Scale and Dividers.

In the preceding Example, suppose the Field divided into three Triangles. See Fig. 53. In the Triangle EAB, the Sides EA and AB are known from the Firld Book, and their contained Angle is known from the Bearing of the Sides. The other Angles and the Side EB may be found by Oblique Trigonometry, C $_{\text {ase III. }}$; and then there will be the three Sides to find the Area. In the Triangle EBC, the Side BC is known from the Field Book, and the Side EB is found as above mentioned; the Angle EBA is also found as above; this subtracted from the Angle $A B C$, which may be found from the bearing of the Sides AB and BC, will leave the Angle EBC : there will then be the two Sides and their contained Angle to find the third Side; and this being found, there will be the three Sides to find the Area. In the Triangle EDC, the Sides DE and DC are known from the Field Book, and their contained Angle is known from the bearing of the Sides. The Side EC and the Area may be found as above.

It is recommended to the Learner to make these calculaz
tions, as it will improve him in the knowledge of Trigonometry.
Note. Two Sides and their contained Angle being given, the Area may be found by Prob. IX. Rule 4.

## Another Method of protracting Fields.

Without drawing parallel Lines at the end of each Side, a Field may be protracted by the Angles made by the several Sides; and the Angle made between any two Sides may be found by the follawing Rules.

Rule 1. If the course or bearing of one of the Sides is northerly and the other southerly, one easterly and the other westerly, subtract the less Course from the greater, the remainder will be the Angle between them.

Rule 2. If one is northerly and the other southerly, and both easterly or westerly, add both Courses together ; the sum will be the Angle between them.

Rule 3. If both are northerly or southerly, and one easterly and the other westerly, subtract the sum of both from 1800; the remainder will be the Angle between them.

Rule 4. If both are northerly or southerly, and both easterly or westerly, add $90^{\circ}$, the less Course, and the Complement of the greater together ; the sum will be the Angle between them.

To protract a Field according to the preceding Rules is preferable to the method of doing it by parallel Lines, though it may not be so easy to the Learner at first. It is difficult to draw parallel Lines with perfect accuracy, particularly without a parallel Rule; and a small deviation from a true Line may make considerable difference in the Plot of a Field.

> Example II.


To draw a Plot of this Field, according to the preceding Rules.

Having drawn the Side AB, according to the directions before given for laying off the first Course and Distance, compare the first and second Courses together, and they will be found to be both northerly and both easterly; conséquently, the Angle between them is found by Rule 4, as follows: $90^{\circ}$ added to $16^{\circ} 30^{\prime}$ the less Course, and 80 the Complement of the greater, the sum is $114^{\circ} 30^{\prime}$, for the Angle at B. Compare the second and third Courses, and they will be found to be one northerly and one southerly, and both easterly ; consequently, according to Rtile 2, 820 the second Course added to 170 the third Course, the sum 990 is the Angle at C. The third and fourth Courses are both southeriy, and one easterly and the other westerly. -The Angle between them at D is $126^{\circ}$; for 170 the third Course added to 370 the fourth Course is 540 , which subtracted from $180^{\circ}$ leaves $126^{\circ}$, according to Rule 3. The fourth and fifth Courses are one southerly and the other northerly, and both westerly. According to Rule 2, 370 the fourth Course added to 490 the fifth Course, the sum 860 is the Angle at E.

A little practice will render this mode of protracting a Field familiar and easy, and an attention to the Courses will show in. what direction the Angle is to be made.

> Example III. FIELD BOOK. See Fig. 66.

Fig. 66.


|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | ---: |
| AB. | N. | 560 | $15^{\prime}$ | E. | Ch. L. |
| BC. | N. | 26 | 30 | E. | 13.44 |
| CD. | S. | 71 | 30 | E. | 18.96 |
| DE. | S. | 26 | 30 | E. | 13.44 |
| EF. | S. | 71 | 30 | W. | 18.96 |
| FG. | S. | 45 | 0 | E. | 8.47 |
| GH. | S. | 63 | 30 | E. | 13.44 |
| HI. | N. | 45 | 0 | E. | 8.47 |
| IK. | S. | 26 | 30 | E. | 13.44 |
| KL. | S. | 45 | 0 | W. | 8.47 |
| LM. | S. | 63 | 30 | W. | 13.44 |
| MN. | N. | 76 | 0 | W. | 24.73 |
| NA. | N. | 36 | 45 | W. | 30. |

Acres Rood Rods Area 167 - 1-30

The above Field may be protracted, and its Area calculated according to the directions given in the preceding Examples.

Scveral Field Books to exercise the Learner in plotting Fields and calculating their Area.



| 10. | N. | 52030 | W. | 12.8 | 21. | N. 36 | $0^{\prime}$ | E. | 41.56 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 11 | S. | 450 | W. | 18.24 | 22. | S. 68 | 0 | E. | 80.6 |
| 12. | S. | 690 | W. | 21.4 | 23. | N. 44 | 30 | E. | 20.4 |
| 13. | S. | 1240 | W. | 9.4 | 24. | N. | 30 | W. | 41. |
| 14. | S. | 8420 | W. | 9.5 | 25. | N. 14 | 45 | W. | 62.32 |
| 15. | $N$. | 2215 | W. | 24. | 26. | N. 16 | 0 | W. | 14.8 |
| 16. | Nor |  |  | 9.8 | 27. | N. 1 | 45 | W. | 14.8 |
| 17 | N. | 2915 | W | 30.6 | 28. | N. 82 | 30 | W. | 99. |
| 18. | N. | 4425 | W | 21.8 |  |  |  |  |  |
| 19. | N. | 6130 | W | 23.1 |  |  |  |  |  |
| 20. | N | 410 | W | 10.8 |  | $135$ |  |  |  |

## CASE V.

To survey a field from one station, at any place within the Field, from which the several Angles may be seen.

Take the Bearing of the Angles, and measure their Distance from the Station.

EIELD BOOK. See Fig. 61.
Fig. 61.


From Station to A. N. 200 W. $\quad \begin{gathered}\text { Ch. L. } \\ 8.70\end{gathered}$
B. N. 60 E. 10 .
C. N. 87 E. $\quad 11.40$
D. S. $\quad 15$ E. $\quad 10.50$
E. S. 60 W. 12 .
F. N. 65 W. 8.78

To protract this Field.
Draw a Meridian Line as N. S. From some point in that Line as a Centre lay off the Bearing and Distance to the several Angles, and draw Lines from one Angle to another, as $\mathbf{A B} \mathbf{B C}$, CD, \&c.

## To find the Area.

'The Area may be calculated according to Рrob. XII. by measuring Diagonals and Perpendiculars; or more accurately according to Prob. IX. Rule 4.

As the Bearing and Distance of the Lines from the Station to the several Angles are known, two Sides and their contained Angle are given in each of the Triangles into which the Plot is divided; the Area may, therefore, be readily calculated by the Rule above referred to.

Note. As in the operation, the Logarithm of Radius is to be subtracted from the Sum of the other Logarithms, it may be done by rejecting the Left-hand figure, without the trouble of putting down the Ciphers and subtracting.


| Triangle aAB | - | 85.7 |
| ---: | :---: | :---: |
| aBC | - | 51.8 |
| aCD | - | 117. |
| aDE | - | 122. |
| aEF | - | 86.3 |
| aFA | - | 54. |
| Double Area | - | $\frac{516.8}{}$ |
| Area | - | $25) 84$ |



## CASE VI.

To survey a Field from some one of the Angles, from which the others may be seen.

From the stationary Angle take the Bearing and Distance to each of the other Angles, with a Compass and Chain.

FIELD BOOK. See Fig. 59.


Ch. L.
FG. N. 700 W. 14.60
FA. N. 50 W. 18.20
FB. N. 30 W. 16.80
FC. N. 10 W. 21.20
FD. N. 7 E. 16.95
FE. N. 30 E. 8.50
To draw a Plot of this Field.
Draw a Meridian Line to pass through the stationary Angle as at F. From the Point F, lay off the Bearing and Distance to the several Angles, and connect them by Lines, as FG, FA, FB, \&c.

The Area may be calculated as taught in the preceding Casm:

## CASE VII.

To survey a Field from two Stations within the Field, provided the several Angles can be seen from each Station.

Find the Bearing from each Station to the respective Angles; and also the Bearing and Distance from one Station to the other.

FIELD BOOK. See Fig. 62.

First Station.
AC. N. $38^{\circ} 30^{\prime}$ E.
AD. S. $69 \quad 0 \quad$ E.
AE. S. $59 \quad 0 \quad$ W.
AF. N. 630 W.
AG. N. 210 W.
AH. North.
Stationary Line AB. N. 140


Second Station.
BC. S. $82^{\circ} 0^{\prime}$ E.
BE. $\quad$ S. 28 0 $\quad \mathbf{W}$.
BF. S. $49 \quad 0 \quad W$.
BG. N. $76 \quad 0 \quad W$.

BH. N. $24 \quad 0 \quad W$. E. 20 Chains.

To protract this Field.
At the first Station A, draw a Meridian Line and lay off the Bearings to the respective Angles; draw the Stationary Line AB , according to the Bearing and Distance; at B, draw a Meridian Line parallel to the other, and lay of the Bearings to the Angles, as taken from this Station; from each Station draw Lines through the Degree which shows the Bearing of each Angle, as marked by the Protractor or Line of Chords, and the Points where those Lines intersect each other will be the Angles of the Field. Connect those angular Points together by Lines, and those Lines will represent the several Sides of the Field.

## CASE VIII.

To Survey an inaccessible Field.
Fix upon two Stations, at a convenient distance from the Field, from each of which the several Angles may be seen; from each Station take the Bearing of the Angles; and take the Bearing and Distance from one Station to the other. Fig. 67.

HIELD BOOK. See Fig. 67.

First Station.
AE. N. $9015^{\prime}$ E.
AF. N. 160 E.
AG. N. 1430 E.
AD. N. $39 \quad \mathbf{0}$ E.
AH. N. 40 E.
AC. N. 720 E.


Second Station.
BE. N. $50^{\circ} 0^{\prime} \mathrm{W}$.
BF. N. 2915 W.
BD. N. 240 W.
BG. N. 2130 W.
BH. N. 50 E.
BC. N. 2030 E.
Ch. L.

Stationary Distance AB, S. $88^{\circ} 3^{\prime}$ E. 19.20.
The directions given in the last Case for plotting the Field, will apply in this Case also; and the Area in this and the preceding Case may be calculated in the manner pointed out in Case IV. by dividing the Plot into Triangles and measuring Diagonals and Perpendiculars. Or the Sides may be found by Trigonometry, and the Area calculated Arithmetically, as already taught.

## CASE IX.

To survey a Field where the boundary Lines are very irregular, without noticing with the Compass every small Bend.

Fig. 68.
Begin near one corner of the Field, as at A, Fig. 68. and measure to the next large Corner, as $B$, in a straight Line; noticing also the Bearing of this Line. From the Line take Offsets to the several Bends, at Right Angles from the Line; noticing in the Field Воoк at what part of $\mathbf{N}$ the Line they are taken, as at A 1, H 2, I 3, B 4. Proceed in the same manner round the Field. In the Figure the dotted Lines represent the stationary Lines, and the black
 lines the Boundaries of the Field.

## FIELD BOOK.

| Bearing and Distance, | Offisets | Bearing | ce. | sets |
| :---: | :---: | :---: | :---: | :---: |
| AB. N. $85^{\circ} 0^{\prime}$ E. $\begin{array}{r}11 \\ \\ \\ \\ \\ \text { at } 5 \\ \text { - the }\end{array}$ | Ch. L. | EF. S. $37^{\circ} 50{ }^{\prime} \mathrm{W}$. | at 1.4 <br> 2.96 <br> the end | $\begin{gathered} \text { Ch. L. } \\ 0.40 \\ 0.36 \\ 0.33 \\ 1 . \\ 0.12 \end{gathered}$ |
|  | 1.40 |  |  |  |
|  | 0.36 |  |  |  |
|  | 0.36 |  |  |  |
| BC. N. $7^{\circ}{ }^{2} 0^{\prime}$ E. 7.96 | 0.20 |  |  |  |
| at 2.36 | 0.36 | FG. S. $27^{\circ} 40$ | 7.06 | 1.20 |
| 4.28 | 0.96 |  | at 2. | 0.24 |
| the end | 0.30 |  | the end | 0.16 |
| $\text { CD. N. } 62^{\circ} 0^{\prime} \text { W. } \begin{array}{r} 4.68 \\ \\ \\ \\ \text { at } 4.34 \end{array}$ | 0.30 | $\text { GA. S. } 25^{\circ} 20^{\prime} \mathrm{W} .$ | $\begin{array}{r} 6.48 \\ \text { at } 3.80 \end{array}$ | 0.80 |
| DE. N. $11^{\circ} 10^{\prime}$ W. 4.20 | 0.30 |  |  |  |

## To protract this Field.

Draw the stationary Lines according to the directions in Case IV. From A make an Offset of 56 Links to I; measure from A to H 540 Links and make the Offset H2, 140 Links; measure from A to I 826 Links and make the Offset I 3, 36 Links : at B make the Offset B 4, 36 Links. Proceed in the same manner round the Field, and connect the ends of the Offsets by Lines, which will represent the Boundaries of the Field.

> To find the Area.

Find the Area within the Stationary Lines as before taught ; then of the several small Trapezoids, Parallelograms and Triangles made by the stationary Lines, Offsets and boundary Lines, and add the whole together : thus, add 56 Links the Offset A 1 to 140 Links the Offset H 2 and multiply their sum 196 by half 540 the length of the line AH , and the Product 52920 Square Links will be the Area of the Trapezoid AH 21 : again, add 140 the Offset H 2 to 36 the Offset I 3 and multiply their Sum 176 by half 286 the length of the Line HI, and the product 25168 Square Links will be the Area of the Trapezoid HI 32. Proceed in the same manner to calculate the Area of all the Trapezoids, Triangles, \&c.

## CASE X.

'I'o survey a Field by taking Off sets both to the Right and Left; that is, within and without the Field, as occasion shall require, in consequence of the Stationary Lines crossing the boundary Lines: also, by Intersections, that is, taking the bearing of an inaccessible Corner from two Stations.

The directions given in the preceding Case, together with the following Field Book, will show the Learner how to survey a Field like the following, and also to protract it when sur. veyed.

FIELD BOOK. Fig. 69.


| Uffsets to the Left. | Bearing and Distance. | Offsets to the Rıght. | Remarks. |
| :---: | :---: | :---: | :---: |
| Ch. L. <br> 1.12 3.40 <br> 1.25 | $\text { AB. N. } 88^{\circ} 0^{\prime} \mathrm{W} . \begin{array}{r} \text { Ch. L. } \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ 7.12 .12 \\ \hline 13 . \end{array}$ | Ch. L. | A Tower bears from A. N. $48^{\circ} \mathrm{W}$. |
| 0.45 | $\begin{array}{\|cc\|} \text { BC. N. } 27^{\circ} 45^{\prime} \mathrm{W} . & 21.12 \\ & \text { at } 4.10 \\ & 10.25 \\ 15 . \end{array}$ | 1.20 1.15 | From B the Tower bears N. $38^{\circ} 30^{\prime} \mathrm{E}$. |
|  | $\begin{array}{lllr} \text { C 1. S. } 82^{\circ} & 15^{\prime} \text { E. } & 5.45 \\ \text { 1, 2. N. } 70 & 0 & \text { E. } & 13.25 \\ \text { 2 D. N. } 20 & 0 & \text { E. } & 3.36 \end{array}$ |  | From C go into the Field to 1, on account of some impediment on or near the boundary Line. At $D$, you get into another Corner of the Field. |
|  | $\text { DF. S. } 35^{\circ} 0^{\prime} \text { E. } \quad 15.15$ |  | E, an inaccessible Corner, bears from D. S. $65^{\circ} 30^{\prime}$ E. |
| 2.20 2.32 | $\begin{array}{\|rr\|} \hline \text { FA. S. } 15^{\circ} 15 & 15.10 \\ & \text { at } 1.20 \\ & 7.45 \\ & 12.25 \end{array}$ | 0.36 | E, the inaccessible Corner, bears from $F$ N. $4^{0} \mathrm{~W}$. |

Note. To draw a Tree, House, Tower, or any other remarkable object, in its proper place, in the Plot of a Field-From any two stations, while surveying the Field, take the bearing of the object, and the intersection of the Lines, which represent the bearings, will determine the place of the object, in the same manner that the Tower is drawn in the tigure.

## To find the Area of the above Field.

Find the Area within the stationary Lines, and then of the several small Trapezoids, \&c. remembering to distinguish those without the stationary Lines from those which are within. Subtract the Area of those within the stationary Lines from the Area of those without, and add the Remainder to the Area contained within the stationary Lines; the sum will be the whole Area of the Field.

## -

## SECTION III.

Rectangular Surveying, or an accurate method of calculating the Area of a Ficld Arithmetically, from the Field Boon, without the necessity of protracting it and measuring with a Scale and Dividers, as is commonly practised.
I. Survey the Field in the usual method with an accurate Compass and Chain, and from the Field Book set down, in a Traverse Table, the Course or Bearing of the several Sides, and their length in Chains and Links, or Rods and Decimal parts of a Rod; as in the 2 d and 3 d Columns of the following. Example.

| 6 606.etici |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ...... | 0881.099 | 70.16 | $0{ }^{\circ}$ | $\left\lvert\, \begin{aligned} & 30 \cdot 17 \\ & 60.17\end{aligned}\right.$ |  |  | c9.9\% 02.93 |  |  |  |
| 6¢60.6IIZ | ........ | 62:90 | 70.1\% | $\begin{aligned} & c L \varepsilon Z^{\prime} \\ & 6 L . \varepsilon z \end{aligned}$ |  | $17^{\circ} 78$ <br>  | . | 08 |  |  |
| !.......... |  | 67.62I | LLFO | $\begin{aligned} & 96.6 \varepsilon \\ & 0.06 \end{aligned}$ |  | .... | $\cdots$ | $0 \pm$ | ${ }^{59}{ }^{\text {M }}$ M 9 | 9 |
| $0^{050209916}$ |  | D6.691 | 62•V8 | … |  |  | $\cdots$ | $\checkmark$ | $\mathrm{q}_{3} \mathrm{nos}$ |  |
| 0701-898\% |  | 88.69 | 62.ES |  | $\begin{array}{r} 99^{\circ} 6 \\ \boxed{5} 5^{\circ} 6 \end{array}$ | $\begin{aligned} & \mathrm{GI} .6 \mathrm{~F} \\ & 80.6 \mathrm{t} \end{aligned}$ | . ${ }^{\text {a }}$ | 0 S | $\cdots{ }^{\prime} 0$ II ${ }^{\text {S }}$ | * |
| ........ |  | S3.07I | 91.92 |  | $\begin{aligned} & 70.08 \\ & 0.08 \end{aligned}$ | - | .... | $0 \varepsilon$ | ${ }^{758}$ | $\varepsilon$ |
| ... | 92\% ${ }^{\circ} \mathrm{C} 880{ }^{\text {c }}$ | 98.99 | \%1 96 |  | $\begin{aligned} & 8 \varepsilon^{\circ} 78 \\ & s \varepsilon^{\circ} \hbar 8 \end{aligned}$ |  | $\begin{aligned} & 99^{\circ} 1 \varepsilon \\ & \varepsilon \mathcal{L}^{\prime} \mathrm{E} \end{aligned}$ | 00 | ${ }^{\circ} \mathrm{T}$ OE LE ${ }^{\circ} \mathrm{N}$ | 3 |
|  | 0160.009I | VL0\% | 54,06 |  | $\begin{aligned} & +2 \cdot 0 \sigma \\ & L \cdot 06 \end{aligned}$ |  | $\begin{aligned} & 91 . \angle 2 \\ & \angle Z: \angle 2 \end{aligned}$ | 08 | $\cdots \mathrm{A}, 0 \mathrm{ogl}{ }^{\text {c }}$ | 1 |
| $\begin{aligned} & \text { sea.v } \\ & \text { yinos } \end{aligned}$ | $\begin{aligned} & \text { Seady } \\ & \text { quison } \\ & \hline \end{aligned}$ |  |  | ${ }^{\circ} \mathrm{Al}$ | $\bullet 3$ | 'S | ${ }^{\circ} \mathrm{N}$ | $\begin{aligned} & 40 \\ & \text { syp } \end{aligned}$ | sasanos | $\xrightarrow{\circ}$ |

$\begin{aligned} & \text { 19143.9019 Sum of South Areas } \\ & 4245.4016 \\ & \text { North Do. } \\ & \text { 2) }\end{aligned}$ (4898.5003 Double Area of the Field:

Acres 744)92501
4
Roods 3)70004

Rods 28)00160
Acres Roods Rods
Area 744-3-28
2. Calculate by Right Angled Trigonometry, Case 1, or find by the Table of Difference of Latitude and Departure,* or by the Table of Natural Sines, $\dagger$ the northing or southing, easting or westing, made on each Course, and set them down against their several Courses, in their proper Columns, marked N. S. E. W.

> Note. To determine whether the Latitude and Departure for any partir cular Course and Distance are accurately calculated, square each of them; and if they are right, the Sum of their Squares will equal the Square of the distance, for the following reason : the Latitude and Departure represent the two Legs of a Right Angled Triangle, and the Distance the Hypothenuse; and it is a Mathematical truth, that the Square of the Hypothenuse of any Right Angled Triangle is equal ta the Sum of the Squares of the two Lege.
3. If the Survey has been accurately taken, the sum of the northings will equal the southings, and the eastings will equal the westings. If, upon adding up the respective Columns, these are found to differ very considerably, the Field should be again surveyed; as some error must have been committed, either in taking the Courses or measuring the Sides. It the difference is small, a judicicus, experienced Surveyor will judge from the nature of the ground or shape of the Field surveyed, where the mistake was most probably made, and will correct accordingly. Or, the northings and southings and the eastings and westings may be equalled by balancing them, as follows; subtract one half the difference from that Column which is the largest, and add the other half to that Column which is the smallest ; and let the difference, to be added or subtracted, be divided among the several Courses, according to their length.

In Example I. the upper numbers are the northings, \&c. as found by a Table of Difference of Latitude and Departure. The several Columns being added, the northings are found to exceed the southings 47 Links, and the westings to exceed the eastings 24 Links. They may be balanced by taking 24 Links from the northings, and adding 23 Links to the southings; and taking 12 Links from the westings, and adding 12 Links to the eastings. Take from the first Course of the northings 12 Links, from the second 7, and from the third 5 ; to the first southing add 7 Links, to the second 10 , and to the third 6 : add to the first easting 3 ,Links, to the second 3 , to the third 4 , and to the

[^3]fourth 2 ; take from the first westing 5 Links, from the second 4 , and from the third 3 . The lower numbers will then represent the northings, \&c. as balanced.
4. These Columns being balanced, proceed to furm a Departure Column, or a Column of Meridian Distances; which shows how far the end of each Side of the Field is east or west of the station where the calculation begins. This Column is formed by a continual addition of the eastings and subtraction of the westings; or by adding the westings and subtracting the eastings: See Example I.

The first easting 20.74 is set for the first number in the Departure Column ; to this add 24.38 the second easting, and it makes 45.12 , for the second number; to this add 30.04 the third easting, and it makes 75.16, for the third number; to this add 9.56 the fourth easting, and it makes 84.72 , for the fourth number ; the fifth Course being south, it is evident the Meridian Distance will remain the same, therefore, place against it the same easting as for the preceding Course; from this subtract 39.95 , the first westing, and it leaves 44.77 , for the sixth Course; from this subtract 23.75 , the second westing, and it leaves 21.02, for the seventh Course; from this subtract 21.02 the last westing, and it leaves 0.0 , to be set against the last Course, which shows that the additions and subtractions have been accurately made. For as the eastings and westings equal each other, it is evident that one being added and the other subtracted; there will in the end be no remainder.
5. The next step in the process is to form a second Departure Column, the numbers in which show the Sum of the Meridian Distances at the end of the first and second, second and third, third and fourth Courses, \&c.

The first number in this column will be the first in the other Departure Column; to which add the second number in that Column for the second in this; for the third add the second and third; and for the fourth, the third and fourth; and so on till the Column be completed. See Example I.

The first number to be placed in the second Departure Column is 20.74 ; to this add 45.12, and it makes 65.86 , for the second number; to 45.12 add 75.16 , and it makes 120.28 , for the third number; to 75.16 add 84.72, and it makes 159.88 for the fourth number; to 84.72 add 84.72 , and it makes $\mathbf{1 6 9 . 4 4}$ for the fifth number; to 84.72 add 44.77, and it makes 129.49 for the sixth number; to 44.77 add 21.02 , and it makes 65.79 for the seventh number; to 21.02 add 0.0 , and it makes 21.02 for the eighth number.
6. When the work is thus far prepared, multiply the several numbers in the second Departure column by the northings or southings standing against them respectively; place the products of those multiplied by the northings in the column of north areas, and of those multiplied by the southings in the column of south areas; add up these two columns and subtract the less from the greater; the remainder will be double the area of the field in square rods or square chains and links, whichever measure was used in the survey.


The dotted line A 2 represents the northing, and the line 2 B the easting made by the first course; these multiplied together, that is, $77.15 \times 20.74=1600.0910$, which is doulle the area of the triangle A2B, as is evident from the Rule to find the area of a triangle, Prob. IX. Rule 1. This number is to be placed for the first number in the column of north areas. The line 3C represents the sum of the eastings made by the first and second courses, which is 45.12 the second number in the first departure column; if to this you add 20.74 the length of the line 2 B you have 65.86, which is the second number in the second departure column, and which represents the sum of the two lines 3 C and 2B. These two lines with the line 2, 3 which represents the northing made by the second course, and the line BC, one of the sides of the field, form a Right Angled Trapezoid. Now, by the rule to find the area of such a Trapezoid, See Prob. X. $65.86 \times 31.66=2085.1276$, double the area of the Trapezoid 2 BC 3 . Place this product for the second number in the column of north areas.

To the line 3 C add CD 30.04, the easting made by the third course, and you have 75.16. which is the sum of the eastings made by the three first courses, and the third number in the first departure column. To this add 9.56, the easting of the fourth course, and you have 84.72, the length of the line 1 E , which represents the sum of the eastings made by the four first courses, and is the fourth number in the first departure column, These two, viz. the lines 3D 75.16 and 1E 84.72, added together make 159.88, the fourth number in the second departure column; which, being multiplied by 49.15 , the length of the line 3,1 which represents the southing made by the fourth course, will give double the area of the Trapezoid 1 ED 3. The number thus produced is 7858.1020 , which is to be placed. for the first number in the column of south areas.

The fifth course being due south, it is evident the sum of the eastings will remain the same as at the end of the fourth course; that is, the line 4 F equals the line 1 E , which is 84.72 . These added make 169.44, the fifth number in the second departure column. This, being multiplied by 54.10, the length of the line EF, which is the southing of the fifth course as corrected in balancing, and the same as the line 1,4 -will give double the area of the parallelogram 1 EF 4, which is 9166.7040, the second number in the column of south areas.

From the line AF 84.72 subtract 39.95 , which is a west course, and it leaves 4G 44.77, the sum of the eastings, or the Meridian distance, at the end of the sixth course, and the sixth number in the first departure column. From this subtract 23.75 the westing made by the seventh course, and you have 21.02, the length of the line 5II, which is the Meridian distance at the end of the seventh course, and the seventh number in the first departure column. The line 4G 44.77 added to the line 5 H 21.02 make 65.79, the seventh number in the second departure column. This being multiplied by 32.21 , the length of the line 4,5 -which is the southing of the seventh course, will give double the area of the Trapezoid 4GH5, which is 2119. .0959, the third number in the column of south areas.

The line H5, 21.02, is the westing of the last course, and: the last number in the second departure column. This being multiplied by 26.65 , the length of the line 5 A , and the northing of the last course, produces 560.1830, which is double the area of the Triangle A5H, and the last number in the column of north areas.

[^4]other west, there is no northing or southing to be multiplied into them : regard can therefore be had to them only in forming the Departure Cor lumns.

By inspecting the Figure, and attending to the preceding illustrations, it will be seen that the three North Areas represent double the Area of the Triangle A2B, the Trapezoid 2BC3, and the Triangle $\mathbf{A} 5 \mathrm{H}$, all of which are without the boundary lines of the field: also, that the three South Areas represent double the Area of the Trapezoid 3DE1, the Parallelogram 1EF4, and the Trapezoid 4GH5; and that these include not only the field but also what was included in the North Areas. Therefore the North Areas subtracted from the South, the remainder will be double the Area of the field, contained within the black lines.

## Additional Directions and Explanations.

The northings and southings may be added and subtracted instead of the eastings and westings; then there will be two Latitude columns instead of Departure columns, and the numbers in the second Latitude column must be multiplied into the eastings and westings, and you will have east and west Areas.

When the course is directly north or south, the distance must be set in the north or south column; when east or west, in the east or west column. There will therefore sometimes be no number to be added to or subtracted from the number last set in the Latitude or Departure column; then the number last placed in the column must be brought down and set against such Course; as in Example I. at the 5th Course. It may also sometimes be the case that there will be no number to multiply into the number in the second Latitude or Departure column; then that number must be omitted, and against such Course there will be no Area as in Example I. at the 3d and 6th Courses.

When the northings or southings, eastings or westings, beginning at the top, will not admit of a continual addition of the one and subtraction of the other, without running out before you get through the several Courses, you may begin at such a Course as will admit of a continual addition and subtraction; and when you get to the bottom go to the top, and you will end in cipher
at the Course next above that where you began; as in Examplr. II. which begins at the 9th Course to add the eastings and subtract the westings.


Example II.

| xo. Courses. | Dist. ${ }^{\text {Dids }}$ | N. | S. | E. |  | Idep. | 2dep. Col. | North Areas | South Areas |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1 \mathrm{~N} .75^{\circ} 0^{\prime} \mathrm{E}$. | 54. | 14.2 |  | 52.9 |  | 144.1 | 235.3 | 3341 |  |
| 2 N .2030 E . | 41.2 | 38.6 |  | 14 |  | 158.5 | 302.61 | 11680 |  |
| 3 East | 64.8 |  |  | 64.8 |  | 223.3 | 381.8. |  |  |
| 4S. 3330 W . | 141.2 |  | 7. |  | 77.9 | 145.4 | 368.7 |  | 395.99 |
| $5{ }_{6} \mathbf{S} .760 \mathrm{~W}$. | 64 |  | 15.5 |  |  | 83.3 | 228.7. |  | 3544.85 |
| ${ }_{6} 6$ North | 36 | 36 |  |  |  | *83.3 | 166.6 | 599.6 |  |
| ${ }_{8}^{6}$ S. 840 OV. | 46.4 |  | 49 |  | 46.1 | 37.2 | 120.5 |  | 590.45 |
|  | 76.4 | 27.8 |  |  | 37.2 | 0.0 |  | 44. |  |
| 10 N .2230 E . | 56 | 51.7 |  | 21.4 |  |  | 113.4 | 5862.7 |  |
| 11 S. 7645 E . | 48 |  | 11 | 46.7 |  | 114.1 | 181.5 |  | 1996.50 |
| 12 S .150 W. | 43.4 |  | 41.9 |  | 11.2 | 102,9 |  |  | 9092.30 |
| 13 S .1645 W. | 40.5 |  | 38.8 |  | 11.7 | 91.2 | 191.1. |  | 7531.08 |

Area 110 Acres, 2 Roods, 23 Rods.
Note. In the above Example you might begin at the 4th Course to add the westings and subtract the eastings; or at the 6th Course to add the northings and subtract the southings : or at the 11th Course to add the southings and subtract the northings. So in every survey, some place may be found where you may begin to add and subtract, without running out before you get through all the Courses.

When a field is very irregularly shaped, it will often happen that parts of the same Area will be contained in several different products in the columns of Areas; but in the final result, one column being subtracted from the other will leave what is included within the boundary lines of the field.

Demonstration. See Fig. 64, and Example II.

Fig. 64.


The Area standirg against the 9th Course, which is where the calculation begins, is the Triangle I2K, all without the Field.

The Area against the 10th Course is the Trapezoid 2KL3, also without the Field.

The Area against the 11th Course is the Trapezoid 4ML3. This is a South Area, and contains a part of the Field and also part of the preceding North Area.

The Area against the 12th Course is the Trapezoid 5NM4, part within and part without the Field.

The Area against the 13th Course is the Trapezoid 6AN5, part within and part without the Field.

The Area against the 1st Course is the Trapezoid 6AB7, part within and part without the Field. This is a North Area, and to be ultimately subtracted from the South Areas; but this includes a part of the preceding South Area, viz. the space uAso; it will, however, be seen hereafter that this same space is included in another South Area. This North Area contains also a part of the first North Area, viz. the space 6 no 7 ; but the same space is also included in another South Area.

The Area against the 2d Course is also a North Area, and is the Trapezoid 7BC8. This Trapezoid contains the space sBCx, without the Field; the space osxw, within the Field; and the space 7ow8, without the Field. But the space ossw will be contained in the next south Area; and the space 7ow8, which was contained in the two first North Areas, will be contained in the next South Area.

By examining the whole Figure in this manner, it will be seen that the North Areas contain all without the Field that is
taken into the Calculation, and some of it twice over; they also contain part of the Area within the Field. The South Areas contain all within the Field, and all without the Field that is contained in the North Areas. They also contain, twice over, so much of the Field as is included in any of the North Areas; and likewise, twice over, that part without the Field which is contained twice in the North Areas. So that subtracting the North from the South Areas leaves double the Area of the Field.

This method of calculating the Area of a Field by the Northings, Southings, Eastings, and Westings, divides the Field, with a certain quantity of the adjoining ground, into Right Angled Triangles, Right Angled Trapezoids, Parallelograms, or Squares, as may be seen by the Figures. It may therefore with propriety be called Rectangular Surveying.

## A Useful Problem.

To find the true Area of a Field which has been measured by a Chain too long or too short.

Calculate the Area as if the Chain was of a true length, then institute the following Proportion:

As the Square of the length of the true Chain;
Is to the Area, as found by the Chain made use of;
So is the Square of the length of that Chain;
To the true Area of the Field.

## Example.

Suppose a Field, measured by a Two Rod Chain 3 Inches too long, is found to contain 41 Acres 1 Rood and 33 Rods, what is the true Area?

As the Square of 33 Feet, the true length of a Two Rod Chain; Is to 41 Acres 1 Rood and 33 Rods; So is the Square of 33 Feet 3 Inches, the length of the Chain used in the Survey; To 42 Acres and 13 Rods. 33 Feet $=396$ Inches. $396 \times 396=156816$ Square Inches.

41 Acres 1 Rood 33 Rods $=6633$ Rods.
33 Feet 3 Inches $=399$ Inches. $399 \times 399=150201$ square inches.
$159201 \times 6633 \div 156316=6733$ Rods.
$6733 \div 160=42$ Acres 13 Rods, the true Arẹa.

## PART II.

## Laying out Land.

PROBLEM I. To lay out any number of Acres in the form of a Square.

Annex 5 Ciphers to the number of Acres, which will turn them into Square Links, the Square Root of which will be the Side of the Square in Links.

Example. It is required to lay out 810 Acres in the form of a Square.

Answer. Each Side of the Square must be 9000 Links, or 90 Chains.

PROBLEM II. To lay out any number of Acres in the form of a Parallelogram, whereof one Side is given.

Divide the number of Acres, when turned into Square Links, by the given Side; the Quotient will be the Side required.

Example. What must be the longest side of a Parallelogram, which is to contain 25 Acres, when the shortest side is 5 Chains and 50 Links?

Answer. $2500000 \div 550=4545$ Links for the longest Side.
PROBLEM III. To lay out any number of Acres in a Field, 3, 4, 5, 6, \&c. times as long as it is broad.

Divide the Acres, when turned into Square Links, by the proportion between the length and breadth; the Square Rioot of the Quotient will be the shortest Side.

Example. It is required to lay out 100 Acres 5 times as long as it is broad.

Answer. $10000000 \div 5=2000000$ the Square Root of which is 1414 Links for the shortest Side, and the longest will be 7070 Links.

PROBLEM IV. To make a Triangle which shall contain a given number of Acres, being confined to a certain Base.

Double the given number of Acres, to which, annex 5 Ci phers, and divide by the Base; the Quotient will be the Perpendicular in Links.

Example. Upon a Base of 40 Chains to lay out 100 Acres in a Triangular form.

Answer. 5000 Links or 50 Chains will be the length of the Perpendicular.

The Perpendicular may be erected from any part of the Base: Thus, the Triangle ABC. See Fig. 55. is the same as ABE, each containing 100 Acres.


Fig. 56.

When the given Base is so situated that a Perpendicular of sufficient length cannot be erected therefrom, continue the Base as from $B$ to D. Fig. 56. from which erect the Perpendicular DC, and complete the Triangle ABC, which will contain 100 Acres.


## PART III.

## Dividing Land.

As different Fièds are so variously, and many of them irre: gularly shaped, and as they are required to be divided in many different proportions, it is difficult to give Rules which will apply to particular cazes. Thee business of dividing Land must therefore be left, in a great measure, to the skill and judgment of the Surveyor; who, if he is well acquainted with Trigonometry, and with measuring Land, will not find it difficult, after a little practice, to divide a Field in such a manner as shall be desired. If he has before him a plot of the Field, and knows the number of parts into which it is to be divided, and the proportion which each part is to bear to the others, he will readily find out where the dividing Lines are to be drawn.

A few Rules and Examples will be given for the general instruction of the Learner.

PROBLEM I. To cut off any number of Acres from a Squarr or Parallelogram.

Say, as the whole number of Acres in the Field; Is to the length of the Square or length or breadth of the Parallelogram; So is the number of Acres proposed to be cut off; To their proportion of the length or breadth.

PROBLEM II. To cut off any number of Acres by a Line proceeding from any Angle of a Triangle.

Measure the Base, or Side opposite the Angle from which the dividing Line is to be drawn; Then say, As the number of Acres in the whole Triangle; Is to the whole Base; So is the given number of Acres; 'To their part of the Base.

Fig. 5\%.

Example. See Fig. 57.


In the Triangle ABC, which contains 48 Acres, it is required to cut off 18 Acres, by a Line proceeding from $\mathbf{C}$ to the Base AB , which is 40 Chains.

$$
\text { As } 48: 40:: 18: 15
$$

Lay 45 Chains on the Base from B to D , and draw the Line CD. The Triangle will then be divided as was proposed; BCD containing 18 Acres.

PROBLEM III. To take off any given number of Acres from a multangular Ficld.

Fig. 65.

Example I. See Fig. 65.


Let ABCD, \&c. be the Plot of a Field containing 11 Acres, from which it is required to cut off 5 Acres.

Join two opposite Corners of the Field as D and G, with the

Line DG (which you may judge to be near the partition Line) and find the Area of the part DEFG, which, suppose, may want 140 Rods of the quantity proposed to be cut off. Mea-. sure the Line DG, which, suppose to be 70 Rods; divide 140 by 35 the half of DG, and the Quotient 4 wili be the length of a Perpendicular whose Base is 70 and the Area 140. Lay of 4 Rods from $G$ to I, and draw the Line DI, which will be the dividing Line.

Example II. See Fig. 60.

Let $\triangle B C D, \& c$. be a tract of land to be divided into two equal parts, by a line from I to the opposite side CD; to find arithmetically on what part of the line CD the dividing line IN will fall ; or to find the Distance CN.


FIELD BOOK.

Rods.

| AB. | N. | $19^{\circ}$ | $0^{\prime}$ | E. | 103 |
| :--- | :--- | :--- | :--- | ---: | ---: |
| BC. | S. | 77 | 0 | E. | 91 |
| CD. | S. | 27 | 0 | E. | 115 |
| DE. | S. | 52 | 0 | W. | 58 |
| EF. | S. | 15 | 30 | E. | 75 |

GF. West Ros.
GH. N. $36^{\circ} 0^{\prime}$ W. 47
HI. North 64.3
IA. N. 6215 W. 59
Acres Rood Rods
Whole Area $152-1-25$

Find the Area of the part IABCI, according to Section III. Page 57, as follows: set the Latitude and Departure of the three first Sides, $\mathrm{IA}, \mathrm{AB}$, and BC , in their proper columns, in a Traverse Table; and place as much southing, visto109.1, equal to the line CK, and as much westing, viz. 71.7, equal to the line KI, as will balance the columns. This southing and westing wvill be the Latitude and Departure made by the line CI. The Area of IABCI will be found to be 8722 Rods, which is less
than half the Area of the whole Field by 3470 Rods, the quantity to be contained in the Triangle ICN.

Find the bearing and distance of Cl by Right Angled Trigonometry, Case IV. as follows:


Vote. In this way the Course and Distance may be found from one Angle -of a Field to another.

Having found the line CI, divide 3470; the number of Rods to be contained in the Triangle ICN, by one half the line CI, viz. 65, the quotient will be the length of the Perpendicular PN, viz. 53.4.

Now, by the bearings of CI and CD, it appears that they form an Angle of $60^{\circ} 20^{\prime}$; wherefore, in the Triangle CPN are given the side PN 53.4, and the Angle at C $60^{\circ} 20^{\prime}$, to find the Hypothenuse CN.


Thus the dividing line must go from I to a point on the line CD, which is 61.5 Rods from C. The bearing and distance of
this line may be found by the directions given above for finding the bearing and distance of the line CI. Or, they may be found by Oblique Trigonometry, Case III.


## Another Method of finding the Distance CN:

Having ascertained the Latitude and Departure of the line Cl , set them down in a Traverse Table ; find the Latitude and Departure of the line CD, and place them in the Table; the difference between the northing of the line IC, and the southing of the Line CD will be the southing of the line DI, viz. 6.6; and the sum of the eastings of those lines, as they are both easterly, will be the westing of the line DI, viz. 123.9. Proceed to calculate the Area of the Triangle ICD, which will be found to be 6522 Rods, nearest.

Note. As in this Triangle two sides and their contained Angle are given, the Area may be found by Рrob. IX. Rule 4, Page 38.

Having found the Area of this Triangle, proceed to find CN according to Prob. II. Page 73, as follows:

As the Area of the Triangle; Is to CD the Base; So is the quantity to be contained in the Triangle ICN ; To CN its proportion of the Base.

As 65:2: 115: : 3470: 61.2

## A third method of finding the Distance CN.

${ }^{-}$To the Logarithm of double the Area to be contained within the Triangle ICN add Radius; from this Sum subtract the Logarithmic Sine of the angle at C; and from the Remainder subtract the Logarithm of the Side IC ; the last Remainder will be the Logarithm of the Side CN.

The double Area of the Triangle ICN is 6940 ; the Angle at C is $60^{\circ} 20^{\prime}$; the Side IC is 130 .

| Double Area 6940 | - | - | 3.84136 |
| :--- | :--- | :--- | :--- |
| Radius | - | - | - |
|  |  |  | 10.00000 |
| Sine ICN 600 20' |  |  | 13.84136 |
|  |  |  | 9.93898 |
|  |  |  | 3.90238 |


|  |  | 3.90238 <br> Side IC 130 | - |
| :--- | :--- | :--- | :--- |
| Side CN 61.5 | - | - | - |

Note. Radius may be added by placing a Unit before the Index of the Logarithm for the double Area, without the trouble of setting down the Ciphers:
$\rightarrow$
By Natural Sines.
Divide the Double Area by the Natural Sine of the given Angle, and that quotient by the given Side; the last Quotient will be the Side CN.

Nat. Sine of the Angle at C $60020^{\prime} 0.86892$
$6940 \div 0.86892=7986.92$
$7986.92 \div 130=61.43$

From the above the following general Rule may be drawn.
To find the Side of a Triangle when the Area is given, with one of the Sides and the Angle contained between the given Side and the Side required.

To the Logarithm of double the Area add Radius; from this Sum subtract the Logarithmic Sine of the given Angle, and from the Remainder subtract the Logarithm of the given Side; the last Remainder will be the Logarithm of the Side required.

Or, By Natural Sines: Divide the double Area by the Nat. Sine of the given Angle, and that Quotient by the given Side; the last Quotient will be the Side required.

## CONCLUDING REMARKS.

Other methods of surveying Fields are taught by some authors on this subject. The preceding, however, will be found most useful in actual practice. Other instruments besides those mentioned in this Book are also son etimes used; such as the Plain Table, Semicircle, Perambulator, Theodo-
lite, \&c. But of these instruments very little use is made in New-England; and they are not often to be met with. For general practice none will be found more useful than a common Chain, and a Compass upon Rittenhouse's construction. A Surveyor should also provide himself with an Offset Staff, ten Links in length, and accurately divided into Links. This should be made of firm hard wood, and will be found very convenient in taking Offsets, and also in measuring the Chain; which should be often done, as from a variety of causes a Chaia is liable to become inaccurate.

It will be observed that in this Work there are no descriptions of Mathematical and Surveying instruments. The Compiler omitted such descriptions from a belief that nothing which can be written on the subject will enable a person to understrand them without an actual inspection of the instruments themselves, and some instruction from those acquainted with them.

The general principles here taught may be applied to the surveying of Townships, Roads, Rivers, Harbours, \&c.

## APPENDIX.

of the variation of the compass and attraction of the NEEDLE.

The Variation of the Compass is the number of Degrees that the Magnetic Needle points from the true North, either East or West. This differs in different places, and in the same place at different times. It is, at present, in Connecticut, a few degrees to the Westward. That is, the Needle points to the Westward of North, and is gradually approaching the true North.

The following method of ascertaining the Variation, by the North Star, has been adopted by many Surveyors, as the most eligible to be practised on Land. It was communicated to the Compiler by Moses Warren, Jun. Esq. of Lyme, an experienced Surveyor, with permission to publish it.

The Star commonly called the North Star, is not directly North but revolves round the Pole in a small circle, once in 24 hours. It cannot therefore be due North but twice in that period; and that is within a very few minutes of the time when a Star, called Alioth, in the Constellation of Ursa Major, or the Great Bear, is directly over or under it. There is also another Star nearly in an opposite direction from the Pole, called Gamma, in the Constellation of Cassiopeia. When these three Stars are vertical the North Star is very near the Meridian; and whea they are horizontal, it is at its greatest Elongation, that is, at its greatest distance East or West of the Pole, and on the same side as the Star in Cassiopeia. The Variation may be calculated when the Star is on the Meridian, or when at its greatest Elongation; more accurately, however, at the latter period, because its motion being then nearly verti-
cal for some time gives the observer a better opportunity to complete his observation.*

To find the Elongation of this Star in any Latitude, its Decination must be known ; that is, its distance North of the Equator. This being found, institute the following Proportion:

As Co-Sine of the Latitude ; Is to Radius; So is Co-Sine of the Declination; to Sine of the Elongation.

The Declination of the North Star, January 1, 1810, was $88^{\circ} 17^{\prime} 28^{\prime \prime}$, and increasing at the rate of about 19 seconds and one half annually.

The following Table Shows the Elongation, in several different Latitudes, for 5 years successively. It is calculated for the first of January in each year ; and in using it, if the time, when the Elongation is required, be past the middle of the year, take it for the beginning of the next year.
a Table showing the Elongation of the North Star.

| Latitude. | 1820 | 1821 | 1822 | 1823 | 1824 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 380 | $205^{\prime} 34^{\prime \prime}$ | $2^{\circ} 5^{\prime} 7^{\prime \prime}$ | $2^{\circ} 4^{\prime} 39$ | $4^{\prime} 13^{\prime \prime}$ | $2^{\circ} 3^{\prime} 47^{\prime \prime}$ |
| 39 | 2723 | $2 \quad 654$ | 2625 | $2 \bigcirc 59$ | $2 \quad 533$ |
| 40 | 2912 | 2841 | $2 \quad 814$ | 2746 | $2 \quad 720$ |
| 41 | 21111 | 21040 | 21012 |  | $2 \quad 918$ |
| 42 | 21310 | 21239 | 21211 | 21143 | 21116 |
| 43 | 21522 | 21451 | 21422 | 21354 | 21326 |
| 44 | 21733 | 2174 | 21634 | 2165 | 21537 |

[^5]Whe Elongation for the Latitude of the observation being calculated, or taken from the above Table, proceed to find its ranges according to the following directions;

Take a pole 18 or 20 feet in length; to the end of it fasten a small line; raise it to an elevation of $45^{\circ}$ or $50^{\circ}$; and support it by two cratches of suitable height to keep it firm in its place. At the end of the line, near the ground, fasten a weight of half a pound or more, which should swim in water to prevent the air from moving the line. Southward of the line, fix a Compass sight, or other piece of metal or wood, with a narrow, perpendicular aperture at a convenient height from the ground, say about 2 or 2 1-2 feet; and let it be so fixed that it can be moved a small distance East or West at pleasure. Let an assistant hold a light either NE. or NW. of the line, nearly as high as the range from the sight to the North Star, in such a position that the line may be plainly seen; then, (the three Stars above mentioned being parallel or nearly so with the Horizon) move the sight-vane East or West, until through the aperture, the line is seen to cut the Star; and continue to observe, at short intervals, till the Star is seen at its greatest Elongation. Let a lighted candle be placed in an exact range with the sight-vane and line at the distance of 20 Rods or more, which should stand perpendicularly, be made fast, extinguished, and left till morning. Then the sight-vane, the line, and the candle, will be the range of Elongation, which observe accurately with a Compass; and if the Elongation be East and the Variation West, the former must be subtracted from the latter; and if they are both West they must be added, and their difference or sum will be the true Variation.

## OF THE ATTRACTION OF THE NEEDLE.

It is well known that any iron substance has an influence upon the magnetic Needle, attracting it one way or the other from the point where it would settle, were there no such attraction. A surveyor should therefore be careful to see that no iron is near the compass when taking a bearing. But as the Earth ir, certain spots contains, near its surface, iron or other minerals which attract the Needle, it will frequently happen that it will point wrong. To ascertain whether this is the case, the surveyor, at each station, should take a back view of the one last left; and if he finds that the compass does not reverse truly, he
may be sure, provided the compass be accurately graduated and placed horizontally, that he either made a mistake at the last station, or that in one or the other of the stations, the Needle was attracted from the true point. When he finds a place where he suspects there is an attraction, he should go a few rods backward or forward, and see whether the Needle points differently. In this way he may prevent mistakes in his field notes, by putting down a wrong course. To take back sights is particularly necessary in running long lines, and laying out new lands, where the Needle is the only thing to guide the surveyor.

By practice and experience a knowledge will be acquired on this subject, and with regard to many other things in surveying, which cannot be taught by books; and after all the directions which can be written, the practitioner will frequently find occasion for the exercise of his own judgment.

> -opion

1 Rule to find the difference between the present variation of the Compass, and that at a time when a Tract was formerly surveyed, in order to trace or run out the original lines.

Go to any part of the premises where any two adjacent corners are known; and if one can be seen from the other, take their bearing; which, compared with that of the same line in the former survey, shows the difference. But if one corner cannot be seen from the other, run the line according to the given bearing, and observe the nearest distance between the line so run and the corner; then work by the following proportion:

As the length of the whole line,
Is to 57.3 degrees,*
So is the said distance,
To the difference of variation required.

## Example.

Suppose it be required to run a line, which, some years ago, bore N. 450 E., distance 20 chains, and in running this line by the given bearing, the corner is found 20 links to the left hand; what is the present bearing of this line?

[^6]
2000)68760(34 Minutes.

Answer- 34 Minutes to the left hand is the allowance required, and the line in question bears N. $44026^{\prime}$ E.

The compiler of this work acknowledges himself under obligations to George Gillett, Esq. Surveyor General of the state of Connecticut, for the following illustrations, remarks, and miscellaneous questions, considering them calculated to be useful to the learner, and the practical surveyor. They came to hand too late to be inserted in their proper places, in the body of the work, and are here put together in the Appendix.

## Rcinarks on the Irregularitics of the Magnetic Needle.

By a statute of this state, applicants for the appointment of County Surveyor are required to be well skilled in point of science in the theory of the most approved methods of surveying lands. It is also as necessary that they should be as well skilled in practical surveying. A practical knowledge must be acquired by experience, and no one can have a thorough knowledge of correct practice without being made acquainted with the imperfections and irregularities of the Magnetic Needle.

It is supposed, by most people, that this instrument, in all places, points directly to the Poles of the earth, and that it remains as permanont as the Poles themselves-an infallible guide.* This is a mistaken idea. A few remarks on this sub-

[^7]
## ject will here be offered, and some facts respecting it will be

 stated.
## Notwithstanding the great utility derived from the Magnetic

thence nearly a west course untir it struck the continent near Charleston, in South Carolina. This the is not stationary, but is ever varying its position; and, notwithstanding the irregularity of its courses, it never crosses itself. About 1756, another variation chart was made, when it was found that the line had fallen so far to the west that it struck the continent near the coast of Florida:- On the cast side of this line, the Magnetic Negdle points to the west of north, and on the west side it points to the east of north, and a regular increase of either east or west variation is found from it, depending on the course that is taken. The line of no variation now runs through Pennsylvania, and not far from Norfolk, in Virginia. When the Connecticut Western Reserve was surveyed into townshipa, the variation at that-place was easterly from one 'to tho degrees.' In 1813, at New-Orleans, the variation was easterly, about eight or nine degrees. In 1701, at Philadeiphia, the variation was westerly, eight degrees and ajbalf. In 1794, nt the same city, the west variation had diminished to one degree and a half, which proves that the progress of the line of no variation had been from west to east. In 1813, by observations at this city, itl wos found that the west variation had increased to about two or three degrees. By a serics of observations, commenced at Hebron in Connecticut, by the writer of this, in 1805, and continued to 1813 , it was found that the west variation during that period increased more than half a degree. The result of these observations agree with those at Philadelphia, that there had been a retrograde motion of the Necdle. Since 1813, the west variation has diminished, or certainly it has not increased. The west variation at Hebron is now (1825) a few mintes more than five degrees. In 1580, at London, the Magnetic Needle pointed eleven degrees and a half to the east of north, which proves that the line of no variation was east of that place. The east variation diminished until 1657, when the line of no variation arrived there and soon passed by; of course west variation began, and continucd to increase until 1806, when it exceeded twenty-four degrees.

The line of no variation must have had a rapid progress through the Atlantic and through a great part of the United States, to have arrived at Charleston in 1700, and at the coast of Florida in 1756. The present bearing of all old lines in this state prove that there has been a considerable decrease of west variation since the first surveys were made; which also proves that the progress of the line of no variation, in the United States, has, for a long time, been from west to east. How far the line of no variation progressed westward in the interior of this country before it turned, no one can tell. It is unaccountable how the west variation in London should increase, while at Philadelphia it was diminishing, when both places are on the sume side of the line of no variation. The variation of the Needle bas long been a subject of much perplexity. Observations have been made in abundance. Many facts have been ascertained, but the difficulty is, they are not reducible to system. The polarity of the Magnetic Needle, with its variations and irregularities, is a hidden mystery, which is never to be searched out by man. It is sufficient in itself, without any other evidence, to cause the reflecting mind to wonder at, admire, and adore the wisdom, knowledge, and porer of HIM who planned and directs it.

Needle, it cannot be relied on where great accuracy is required, on account of the irregularities to which it is subject, such as its annual motion in variation, its diurnal motion, and, what is attended with greater difficulty, its local attraction. When an old course is given to renew a line, it cannot be depended on, on account of the difference in variation between the time of the first running and the renewal of it.

No annual rate can be fixed on for the variation of the Magnetic Needle, as its motion is much more rapid in some years than in others. By observations made at London during a period of more than two hundred years, it appears that in some. years the motion of the Needle was rapid, in others, but little would be discovered, and, in some years, the motion was retrograde. There is no regularity in its motion in any place.

Another difficulty in retracing a line from an old course or from one recently given is, that it is often found that two compasses do not make the same course. It was well kuown to the celebrated Rittenhouse, that his compasses did not all agree, or: make the same course, and he never was satisfied as to the reason of it. It has also been ascertained that different Needles do not point alike at the same place. French writers, on Magnetism, have lately treated on this subject. Two compasses may differ a quarter of a degree or more or less, when no defect can be discovered in either. A survey may be taken as correctly with one as with the other. 'The question then naturally arises, which of the two is right? The answer is, both are right; neither of them points directly to the Poles of the carth, except on the line of no variation. All that can be said of them is, that onc has a greater variation than the other, and that which has the least cannot have the preference. The diurnal motion of the Magnetic Needle is another defect in it. As the sun rises in the forenoon, and the earth becomes heated, it has an effect on the unknown something which gives polarity to the Needle, and turns the north end of it to the west. In the afternoon and night following, it returns to its position.

For several years, the writer of this made observations with Rittenhouse's compass, to ascertain the diurnal motion; and in the summer season usually found about a sixth part of a degree. In the winter, but little or none could be discovered. The di-urnal motion of the Needle. has been known in Europe about a century.* The local attraction is an irregularity to which the Magnetic Needle is subject. These are found oftener in hilly,

[^8]broken lands, filled with ledges, than in level, feasible land, where there are no ledges. As attractions are out of sight, they must be searched out, as before directed in this work, by locd experiment. They often amount to a quarter, a half, and sometimes to a whole degree or more. The writer of this has known a difference of more than five degrees within a distance of forty rods.

When an old line is to be renewed where the bounds are lost, the circumstances attending the case must govern. These may be various, such as giving the lots on each side of the line and contiguous thereto, their full width or quantity, or by dividing the overplus or the wantage, as the case may happen. It would be difficult to mention all the circumstances which may govern; or which may serve as evidence in such cases.

After all, the Magnetic Needle is the best guide that has yet been discovered, and it cannot be dispensed with in land surveying; but the surveyor who is best acquainted with it, will make as little use of it as he can. In small surveys, where one angle may be seen from another, the quantity of each angle may be taken by an instrument constructed for that purpose, without the use of the Magnetic Needle; and the sides may be measured, and one side, no matter which, may be made a meridian, and from that meridian courses may be calculated for the other sides, and the survey may be calculated by the rules of rectangular surveying. This method has been recommended by theorists, and the ingenuity displayed in the invention, together with the correctness of it, so far as it is practicable, must be acknowledged; but in larger surveys, it cannot be introduced to practice, on account of the obstructions which intervene between the angular point and the termination of two contiguous lines which contain the angle : in such cases, the danger in taking the quantity of an angle will be greater than that of the Magnetic Needle.

If in every town in the state, a meridian line was established by the motion of the heavenly bodies, and such meridians were perpetuated by durable monuments, whenever a survey was to be taken in the vicinity of a meridian, a surveyor might set his compass on it and note the variation found, and that variation should be inserted in the deed or in whatever writing or instrument by which the land is conveyed and made a record; this would assist a surveyor at any future period in retracing those lines, by setting his compass on the same meridian and allowing the same variation that was allowed when the survey was made. This would tend greatly to the security of landed property, and
perhaps would be the best remedy for the variation of the Magnetic Needle, and for the difference between two compasses which differ, that can be invented.

## On Practical Surveying.

It would be no easy matter to describe all the different methods which may be taken in different cases, in taking the fieldwork of a survey. Only one case will be given here, which is represented by the following figure. See Fig. 1.

Fig. 1.
The survey was begun at the corner numbered 1. The corner numbered 2 was in a pond. The course and distance were taken from 1 to $m$, then from $n$ to $n$. The augle at 2 was a right one, of course there was a right angled triangle, wherein the angles and hypothenuse were given, to find the sides. $m 2$ and $2 n$. From $n$ to 3 , the course and distance were taken on the line. The next
 line ran through a thicket in a swamp, where nothing could be done correctly. Courses and distances were taken from 3 to $s$, thence to $z$, thence to 4 , and the course and distance of the line 3-4 were calculated by a traverse from those courses and distances. At the angle 5, a tree stond on a high bluff of ledges, inaccessible on either line terminating at that point. The course from 4 to 5 was taken at 4 . Next, the course and distance were taken from 4 to $a$, and from $a$ the course was taken to 5 . Next, the course and distance were taken from $a$ to 6, and from 6 the course was taken to 5 . Two oblique triangles, with the angles and one side in each, were given to find the sides $4-5$ and 5-6. The closing line ran through thick bushes and water; and the course and distance were taken on the dotted
line to the line 1-2, at a point twenty rods from 1. The course and distance of 6-1 were calculated accordingly.

Whenever a line runs through or over a place where it is difficult to take either course or distance correctly, if, by taking a traverse around at a little distance, the surveyor can have level, clear land, and then calculates his course ahd distance by the traverse, he will be more likely to ascertain the true course and distance than by continuing on the line.

## Directions for running Lines.

Many people suppose that a surveyor at the beginning of a line, by intuition or by some magic art, can set his compass directly to the terminating point, whatever obstructions may intervene, and that he needs no assistants ; but this is a mistaken idea. In running a line of considerable length, a surveyor should have two assistants to carry the chain, and two to carry tlage, in whose ability and correctness he can confide, and a fifth to use un axe. If the surveyor is not furnished with such a set of assistants, his employer need not place too much confidence in his work. The flag staves should be as much as two and a half inches in diameter, or what would be better, two stripes of a board of that width and seven or eight feet in length. If they are not so wide, they cannot be seen through the sights of the compass, at any great distance. On one end of each staff, a red flag of a yard in length should be wound tight, and not left to hang loose and flutter in the wind. Red will be seen quicker through bushes than any other colour, and the brighter the colour the better. Being thus manned and equipped, at the beginning of the line, he must set his compass as near the true line as he can, or, what would be better, he may set up one of the flags at the place of beginning, and go forward as far as he can have a fair view of the back flag, there set his compass on his random line, and send the other assistant as far forward as he can conveniently see the flag. When each flag is clearly seen through the sights of the compass, the back'flag must. be brought up and placed where the compass stood. In this man. ner, he must proceed on his random line, taking care each time he sets his compass to turn the sights to the back flag. Great care must be taken to keep these flags perpendicular; also, the surveyor must keep the staff and the sights of his compass pernendicular. A little leaning of the flags, or turning the sights
of the compass from a perpendicular, will make a crooked line. In looking through the sights of the compass to the flags, the surveyor must look as near the ground as he can, and, when practicable, the flag should be turned down, on account of the danger of being leaned when kept up.

All obstructions, such as bushes, brush, \&cc. must be cleared away. The random line must be measured, and at convenient distances, perhaps at every twenty rods, stakes must be set directly in it. Every stake must be numbered, that no mistake may be made in calculating, to set them in the true line. If, in the course of the random line, the Magnetic Needle does not traverse as at first, or traverse alike at different places, no regard must be paid to it-the two flags must direct the course ; neither shouldthe surveyor be turned aside or terrified by the cry of either of the parties, You are zorong, Yout are zurong,(for he will most certainly hear it,) but he must continue his random line, until turning at right angles either to the right or to the left, as the case may be, he will exactly strike the bound, or the point where a bound is to be erected; there he may stop, and measure the distance from the termination of it to the bound. Then, having the length of the random line and the distance to the true bound, he fas the less of a right angled triangle, the hypothenuse will be the length of the true line; also, the angle contained between the true and the random line must be added to or subtracted from the course of the random line, (as the case may happen,) which will give the course of the true line. Suppose the whole length of the random line is 200 rods, and the distance from the termination of it to the bound is 90 links, the calculation for setting the stakes on the true line may be made thus :-As the whole distance is to 90 links, so is 180 , or any other 20 rods stake, to the distance that such stake is to be moved. The answer is, the first stake is to be moved 9 links, the second 18 links, and so adding 9 links at each stake until the whole are moved at right angles from the random on the true line. Most of the crooked lines and consequent disputes and law-suits between farmers have arisen for the want of this care and attention.

When a long line is to be run over a number of ridges and through intervening valleys, it should first be run and established from one ridge to another, and the intermediate spaces in the valleys may be taken afterward. By taking long sights there will be less danger of turning from a straight line. In all cases, the forward flag should be carried as far as it can be distinctly seen, unless it is at the termination of a line.
commit much error on them; while other lines, on other parts of the same survey, are atterided with so many difficulties, that when they have done their best, it will scarcely be possible for them to avoid some error, and the surveyor whe takes the survey will best judge on what lines the errors were committed, and whether they are in the courses or in the distances. In all cases the corrections should be made on the lines containing the errors. When the errors are in the courses they should be corrected, and when the errors are in the distances, the correction should be in them: or the corrections may be in both courses and distances as the surveyor may judge proper.

When a course is northwesterly and southeasterly, or northeasterly and southwesterly, if the correction of it increases the latitude and diminishes the departure, or if it diminishes the latitude and increases the departure, so as to bring the differences to an even balance, it is good evidence that the course contains some error.

## On Rectangular Surveying.

Rectangular Surveying is a name given to the method here treated of, by the late Governor Treadwell.

A more appropriate name could not have been given; for the whole survey is reduced to right lined figures, such as triangles, trapezia, squares, and parallelograms. It is simply multiplying the latitudes by the longitudes from a meridian from which the survey is calculated.

The calculations are made from a meridian, drawn, either at the eastern or at the western extremity of the map. All the spaces lying between the field and the meridian from which the survey is calculated, and between, the parallels of latitude of the northern and southern extremities of it, are included in the calculation. Parallels of latitude are drawn from each angle to the meridian, which are called meridian distances.

In forming the column of meridian distances, when the meridian is drawn at the eastern extremity, the westings are added and the eastings are subtracted. When the meridian is drawn at the western extremity, the eastings are added, and the westings are subtracted.

The meridian distances proceeding from each end of a line, are added together, to form the column of double mean distances, which the compiler of the foregoing work has called second departure column.

The whole is illastrated by the following fgure. See Fig. 2:

Directions for calculating meridian distances by scveral methods； also，for plotting a survey，from the several latitudes and meridian distances，without the use of the protractor，or the line of chords．
$\underset{-4}{4} \cdot \underset{\sim}{8}$


|  | － |  | $\wedge$ | $\omega$ | N | － | ${ }^{7}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 告 | $\begin{aligned} & \text { in } \\ & \text { or } \\ & 8 \\ & 2 \end{aligned}$ | $7 \Omega$ $\vdots$ $\vdots$ 8 $\sum$ | $\begin{aligned} & n \\ & a \\ & a \\ & 0 \\ & 8 \\ & 0 \end{aligned}$ | 2 <br> $\cdots$ <br> 0 <br> 0 <br> 8 <br> 0 <br> 1 | H｜ | 边 |
|  | $\begin{aligned} & \text { - } \\ & \text { i } \end{aligned}$ | $\begin{aligned} & \text { iे } \\ & 8 \end{aligned}$ | $\begin{aligned} & \infty \\ & 8 \\ & 8 \end{aligned}$ | 8 3 | ¢ <br> 8 <br> 8 | 号 | We |
| 圭 |  |  |  | 第 | 宫 | ¢ ¢ ion | 2 |
|  | \＄8 | ¢ | ¢ |  |  |  | $\square$ |
| $\begin{aligned} & 0 . \\ & 0 \\ & 0 \end{aligned}$ |  |  |  | cid <br> 8 <br> 8 | 0 <br> $i 0$ <br> 0 | 0 <br> 0 <br> 8 <br> 8 | 탕 |
|  |  | 官 | \％ |  |  |  | $\sum$ |
|  | 8 8 8 | － | $\begin{aligned} & \text { 山ै } \\ & \infty \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & \hline 9 \end{aligned}$ | 皆1 | $\begin{array}{\|c\|} \hline 6 \\ 8 \end{array}$ | 気 |
|  | \％ | 苍 | $\begin{aligned} & \text { W} \\ & \substack{0 \\ 0 \\ 0 \\ \hline} \end{aligned}$ | 菖 | $\begin{aligned} & \mathscr{8} \\ & 0 \\ & \varrho \end{aligned}$ | $\begin{aligned} & 6 \\ & 0 \\ & 0.8 \end{aligned}$ | － |
|  | $\begin{aligned} & 80 \\ & 80.1 \\ & 80.0 \end{aligned}$ | $$ |  |  | $\begin{aligned} & \text { 公 } 0_{0}^{0} \\ & 190 \\ & 100 \end{aligned}$ | $\begin{aligned} & 140 \\ & \text { Ho } \\ & 08 \\ & 080 \end{aligned}$ | ｜c岛 |
|  | $\left\|\begin{array}{c} \infty \\ 0 \\ \vdots \end{array}\right\|$ | $\begin{aligned} & 10 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & -1 \\ & 0 \\ & 0 \\ & \hline 8 \end{aligned}$ | $\left\|\begin{array}{l} 0 \\ 0 \\ 8 \end{array}\right\|$ | $\left.\begin{aligned} & 6 \\ & 0 \\ & 0 \end{aligned} \right\rvert\,$ | $\left\lvert\, \begin{aligned} & \infty \\ & A \\ & \Delta \end{aligned}\right.$ | 皆 |
| － | ． |  |  |  | $\begin{aligned} & \text { ー } \\ & \text { 侖 } \\ & \text { CiO } \end{aligned}$ | $\begin{aligned} & \infty \\ & \substack{\circ \\ \hline \\ \hline \\ \hline} \end{aligned}$ | 为 |
| た్త్ర |  | $\begin{aligned} & \text { N } \\ & \text { A } \\ & \stackrel{+}{\infty} \end{aligned}$ |  |  |  |  | \％ |

commit much error on them; while other lines, on other parts of the same survey, are attended with so many difficulties, that when they have done their best, it will scarcely be possible for them to avoid some error, and the surveyor who takes the survey will best judge on what lines the errors were committed, and whether they are in the courses or in the distances. In all cases the corrections should be made on the lines containing the errors. When the errors are in the courses they should be corrected, and when the errors are in the distances, the correction should be in them: or the corrections may be in both courses and distances as the surveyor may judge proper.

When a course is northwesterly and southeasterly, or northeasterly and southwesterly, if the correction of it increases the latitude and diminishes the departure, or if it diminishes the latitude and increases the departure, so as to bring the differences to an even balance, it is good evidence that the course contains some error.

## On Rectangular Surveying.

Rectangular Surveying is a name given to the method here treated of, by the late Governor 'Treadwell.

A more appropriate name could not have been given; for the whole survey is reduced to right lined figures, such as triangles, trapezia, squares, and parallelograms. It is simply multiplying the latitudes by the longitudes from a meridian from which the survey is calculated.

The calculations are made from a meridian, drawn, either at the eastern or at the western extremity of the map. All the spaces lying between the field and the meridian from which the survey is calculated, and between the parallels of latitude of the northern and southern extremities of it, are included in the calculation. Parallels of latitude are drawn from each angle to the meridian, which are called meridian distances.

In forming the column of meridian distances, when the meridian is drawn at the eastern extremity, the westings are added and the eastings are subtracted. When the meridian is drawn at the western extremity, the eastings are added, and the westings are subtracted.

The meridian distances proceeding from each end of a line, are added together, to form the column of double mean distances, which the compiler of the foregoing work has called second departure column.

The whole is illastrated by the following fegure. See Fig. 2:

Directions for calculating meridian distances by scveral methods; also, for plotting a survey, from the several latitudes and meridian distances, without the use of the protractor, or the line of chords.

| 91 | 88'1956 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 88:867 |  | $\overline{91 \cdot 98} 800^{0000}$ | 8804 | $00^{\circ 00} 88^{\circ} 02$ |  | 20'9 |  | $87^{\circ} 02$ | M90 c8s 9 |
| S8'tzLa |  | $20^{\circ} 6299^{90071}$ | 915 | $88^{\circ} 04667^{\circ} 8$ |  | 98.68 |  | 00000 | M00 ¢ 's 9 |
| Oп¢¢9\%9 |  | $56^{\circ .92} 69.2 \mathrm{FI}$ | 68\%891 |  |  | $9 \square^{\circ} 98$ |  | $00 \cdot 98$ | M00 ors |
|  | $98^{\prime 9891}$ | $60^{\circ 19} 8 \mathrm{I}^{\circ} \mathrm{OM1}$ | $81 \% 01$ | 20.08 | $9^{96} \mathrm{LS}$ |  | Ss'si | $00^{\circ} 09$ | \%00 92N ${ }^{\text {c }}$ |
|  | 986911 | $09.61 \begin{aligned} & z 2^{20} 57 \\ & 10.68 \end{aligned}$ | 10'68 | 1178 | $16^{\circ 9}$ |  | 79\% 6 | $00^{\circ}$ | 900 01-N |
|  | 89\%\%19 | $97^{9.8} \begin{aligned} & 080^{\circ} 88 \\ & 06.91 \end{aligned}$ | 0699 | 0691 | 06'91 |  | 97.98 | $00 \cdot 0$ | 400096\% 1 |
| e.rv | ${ }^{\text {seasy }} \cdot \mathrm{N}$ |  | - 'N | $\mathrm{A} \cdot \mathrm{N} \cdot \mathrm{M}$ | 'a | S | - |  | -59sanos ${ }^{\text {os }}$ |

Meridian Distances, and Double Mean Distances, are more proper terms or names for the eighthandninth columns, than first Departure, and second Departure.

The meaning of the term Meridian Distance is the distance made from any Meridian. It is not very essential by what names the columns are called, as names have no effect on the final result.


This survey is calculated from the meridian of the first station.

To form the first column, marked at the top, Merid. Dist., set the easting 16.90 against the first station into the column, which is the meridian distance of 2 , or the distance from 2 to 1 ; to this number add the next easting, and they make 22.11, the meridian distance of 3 ; to this number add the next easting, and they make 80.07, the meridian distance of 4 ; from this number, subtract the first westing, and 73.82 remains, the meridian distance of 5 ; from this number, subtract the next westing, and 70.33 remains, the meridian distance of 6 , or the westing of the closing line. Subtract the last westing, and 00.00 remains. This is on the principle of going around a circle. Next, form the column of double mean distances by adding two opposite sides of the different figures. Set the first Merid. Dist. into the column. To the first meridian distance, add the second, and they make 39.01, the double of the figure $23 n \mathrm{~s}$. To the second, add the ,hird, and they make 102.18, the double of the figure 34 mn . To the third, add the fourth, and they make 153.89, the double of the figure 45 am . To the fourth, add the fifth, and they make 144.15, the double of the figure $56 a z$. To the fifth, add the sixth, and they make 70.33.

The second column, marked at the top, Merid. Dist., is commonly called the Pennsylvania method. Only one column is used in finding the meridian distances, but the operation and final results are the same as that when two columns are used. This method is not so easily explained to the learner, but is preferable in practice only because an error may be committed in forming the column of double mean distances which may not be discovered, but in this method an error cannot be committed without being detected.

To form this column, set the first easting 16.90 in the upper place, and add it to itself and they make 33.80 ; to this number, add the next easting, and they make 39.01 ; add the same easting again, and they make 44.22 ; to this number, add the last easting, and they make 102.18; add the same easting again, and they make 160.14 ; from this number, subtract the first westing, and 153.89 remains; subtract the same westing again, and 147.64 remains; from this number, subtract the second westing, and 144.15 remains; subtract the same westing again, and 140.66 remains; from this number subtract the last westing, and 70.33 remains; subtract the same westing again, and 00.00 remains.

The upper numbers in this column are the same as the double mean distances which stand against them.

For the remainder of the process in finding the areas, proceed as before taught in this work.

The north area against the first station is the double of the triangle $12 s$; that against the second, is the double of the figure $23 n \mathrm{~s}$; that against the third, is the double of the figure 34 mn ; the south area against the fourth station, is the double of the figure 45 am ; that against the fifth, is the double of the figure $56 z a$; that against the sixth, is the double of the triangle $61 z$.

The three north areas all lie without the field, and are bounded north on the line $m 4$. The three south areas contain all within, and all without the field, which is included in the calculation. It is obvious then that when the less is subtracted from the greater, the contents of the field will remain.

Another column may be formed as the eleventh in this example, which, for distinction, is here called half departure. It contains half the sum of the numbers in the double mean column. These numbers when multiplied by their respective northings or southings, give the simple areas of the different figures. This method is preferable in practice, as the multiplications are greatly diminished. When the last decirual in the double mean distance is an odd number, a unit may be taken
off, and take half the remainder rather than annex another decimal. Perhaps this would not make the difference of a rod is a survey of one hundred acres, or the odd numbers in the last place of decimals may be balanced by sometimes adding a unit. If the numbers are diminished a trifle, it may be remarked, that, on account of the uneven surfaces, there is danger of making the distances too much rather than falling short of the true measure.

To plot the foregoing Field from the several Latitudes and Meridian Distances, without the use of the protractor, or the line of Chords.

First, set the northing of the first line from 1 to $s$; set the northing of the second line from $s$ to $n$; set the northing of the third line from $n$ to $m$; set the southing of the fourth line from m to $a$; set the southing of the fifth line from $a$ to $z$; next, from these points, draw parallels of latitude perpendicular to the meridian; then, on these parallels of latitude, set the meridian distances of the several stations from $s$ to $2,16.90$; from $x$ to $3,22.11$; from $m$ to 4, 80.07 ; from $a$ to $5,73.82$; from $\approx$ to 6, 70.33. From one of these last points to another, draw the boundary lines of the field, and if the plan does not perfectiy close, it is because some error was committed in the process, or the scale was incorrect. In practical surveying, it is next to an impossibility in any case, to work so accurately that the survey will exactly close without some correction. The difference between the two columns of latitude, and the two columns of departure, are the legs of a right angled triangle, the hypothenuse of which will be the distance which the survey will fail of closing.

These differences, as before taught in this work, must be balanced, and the column of meridian distances must be formed by the numbers as balanced. When the survey is balanced, and this method of plotting is taken, the parallels of latitude must be laid down according to the balancing, and the map. will perfectly close.

When the courses and distances are corrected according to the balancing, they will form a survey which will contain no error.
N. B. Great care must be taken to keep the latitudes parallel and perpendicular to the meridian. The better to effect this, a meridian line may be laid on each side of a sheet, or a half sheet of paper, as the occasion may require.

The following survey is calculated from a meridian running. through the map: of course, part of the meridian distances are east, and part are west. See Fig. 3.

Fig. 3.


The column of meridian distances in this example is formed by adding twice, and subtracting twice against each station, as in the Pennsylvania method. Set the first easting in the upper place, which is the distance from $a$ to 2, being east meridian distance; add it to itself, and it makes 34.64 ; to this number, add the next easting, and they make 54.64 , east meridian distance from $a$ to $m$; add the same easting again, and they make 74.64 ; from this number, subtract the first westing, and there remains 8.86 east meridian distance from $i$ to $s$. As the first westing cannot be subtracted again, the last east meridian distance, 8.86, must be subtracted from the first westing; this crosses the meridian, and gives 56.92 west meridian distance in the lower place. Having crossed the meridian, the westings must now be added, and the eastings subtracted.

To the 56.92 in the lower place, add the last westing, and they make 76.92 west meridian distance from $r$ to $u$; add the same westing again, and they make 96.92 ; from this number, subtract the easting of the closing line, and there remains 48.46 west meridian distance, from $v$ to 1 , or the easting of the closing line; subtract again, and 00.00 remains. Having completed the column of meridian distances, next multiply the upper number against each station, by its northing or southing, and set the products on the east side of the meridian, in their respective columns of north or south areas; but on the west side of the meridian, the order is reversed; the north products are set in the column of south areas, and the south products are set in the column of north areas. The north area against the tirst station, is the figure $2 z 1 a$; the south area against the second station, is the figure mnia; the south area against the third station, is the figure sxie; the south area against the fourth station, is the figure uwer, made by the northing of the fourth line; the south area against the last station, is the figure $v 5 r 1$.

The foregoing columns of meridian distances might have been commenced, by setting the first easting in the lower place, and the additions and subtractions, made as before directed, and the last subtraction would end in 00.00 at the upper place, against the first station. In this case, as there would be no upper number against the first station, there would be no product in either column of areas against it. The east meridian distance against the second station would extend no further east than the third station, and the meridian distance against the third station, would be on the west side of the meridian; and the meridian distances, against the fourth and fifth stations, would extend as much farther west, as the easting of the first lines

The products against the second, fourth, and fifth stations, would be set in the column of south areas, and that against the third station, on account of its being on the west side of the meridian, would be placed in the column of north areas, and would be subtracted from the footing of the south areas.

When a survey is calculated from a meridian running through the map, it is always best to set the first departure in the lower place, as it saves one multiplication.

## On Distributing Estates.

A farm is to be distributed among a number of heirs. A survey is made, and the difference between the columns of latitude, and between those of departure, are two rods for each. The survey is balanced, and calculated arithmetically, and is found to contain two hundred acres. The surveyor next draws his map, by which the divisions are to be made, according to the courses and distances. The plan does not close by nearly two rods and three-quarters. He next corrects the lines, and makes the map close as well as he can ; and when the divisions are made, they may not agree with the first calculation by two or three acres, or more. Should the map be drawn as before directed, by the meridian distances and the latitudes as balanced, it would close, and would be in exact conformity to the calculation made arithmetically. If the divisions are made arithmetically, without the use of the scale and dividers, the calculations must be made according to the balancing, or the divisions will not agree with the first calculation.

It will he acknowledged by every experienced surveyor, that it is a difficult matter to make the amount of a considerable number of divisions agree with the whole, when calculated by itself.

It is the common practice in distributions, to make the divisions with scale and dividers; this method will answer very well provided the map is drawn on a large scale.

The following is a useful rule in dividing lands, when any quantity is to be added to, or taken from, a division in the form of a triangle.

Having the area, the contained angle, and one side of a triangle given, to find the adjoining side, including the angle.

## Rule.

To the sine of the given angle, or its supplement if obtuse, add the logarithm of the given side; subtract radius from this sum, and subtract the remainder from the logarithm of the double area, the last remainder will be the logarithm of the side required.

In taking a survey, go around with the sun, not that you can work more correctly, or that it will have any effect in calculating, but when you put your courses and distances on your map they will follow around with the lines, from the left to the right.

Wherever you begin, set your compass on the angle and cause a stake or a flag-staff to be erected at the next. When your line runs over a hill, cause a stake to be erected at each end of it, and take your station on the top of the hill, directly between them. If bushes obstruct the sight, make an offset, or set your compass a little distance from the line, from whence you may see the back flag, and cause the forward flag or stake to be set against the bound in a direction with the compass and the back flag. When the line is measured, measure the distance from the flag to the bound, and calculate your true course by Trigonometry. If your next line is of such a distance that you cannot see through the whole length of it, run as near the truc line as you can, and if you do not exactly strike the bound, measure the distance from the termination of your random line, and calculate your course as before directed, or if you can discover a tree standing near the termination of your line, take the course and distance to that, thence to the bound, and calculate your true course and distance.

By practice and experience, a method for taking courses wil! soon become familiar, in all cases. In measuring hills and inclined surfaces, the horizontal distances must be taken. A Flummet should be suspended from the end of the chain, when it is levelled. Where hills are very steep, the surveyor should assist the chainmen, and when the best is done in levelling and plumbing the chain, judgment must frequently be called into exercise. Even when rises and descents are easy, there is danger of making too much measure. In such cases, chainmes often make allowances, but the surveyor would do better to keep them to close measure, and from the shape of the ground judge himself what allowances ought to be made. If he is exgerienced in his business, he will form a more correct judgment
than inexperienced chainmen. Particular care must be taken that the chain is carried on a straight line, and that it is well straightened. When a tally is ended, and the hinder chanman brings up the sticks, they must be counted.

When on counting the sticks it is discovered that one is lost ${ }_{0}$ the chainmen should not leave the chain and go back to find it, but, from the last mark, should measure back to the point where the tally began, to see whether one chain is lost from their measure. Many blunders in this way have been left undetected by not taking this care.

A careful accurate chainman never lost a stick or miscounted a tally. Young surveyors should practice much for their own instruction, and should make correct practice familiar, before they offer their services. It is as necessary that they should spend some time in acquiring a practical knowledge, as it is that they should spend any time in acquiring a knowledge of theory.

A young surveyor should bear in mind that if he is detected in one error in the beginning of his practice, it will be more to his disadvantage than to be detected in two when he shall be well established. If an error is committed in a survey, it is not against the surveyor provided he detects and corrects it, but if he cannot detect and correct his own errors, that is sufficient evidence of his deficiency in point of knowledge and skill.

## Form of a Field Book.

Beginning at a murstone at the southwest corner, Rods Links


When a survey is calculated by chains and links, the numbers are less than when it is calculated by rods and decimal parts. Every method by which the numbers are diminished is an improvement. In a hilly country, the two-pole chain is preferable and is more commonly used, because it can be levelled better.

Hills are often found so steep that even the two-pole chain cannot be levelled.

## APPENDIX.

## MISCELLANEOUS.

When a survey is calculated by chains and links, and the contents stand in acres and decinal parts of an acre, it may be multiplied by the price of an acre, and the product will be the amount.

## Example.

A piece of land, 12 chains and 25 links in length, and 10 chains and 25 links in breadth, is sold for $\$ 2025$, per acre ;what is the price of it?

Length 12.25
Breadth 10.25


The writer of these pages knows not who invented the following rules for finding contained angles. For plainness, none of the kind exceeds them.
N. $62^{\circ} \mathrm{E}$. When the first letters are alike, and the two N. 44 W. last are unlike, add the degrees of both courses together, which gives the contained angle.
S. $72 \circ \mathrm{E} . \quad$ When the two first and the two last letters are S. 25 E. alike, subtract one course from the other, and the remainder will be the contained angle.

When the two first letters are unlike, and the
N. 640 E. two last alike, add both courses together, and sub-
S. 35 E . tract their sum from 180 , the remainder will be the contained angle.
N. When the two first and the two last letters are
N. 570 W . unlike, subtract one course from the other, the
S. 25 F. remainder from 180 , and the remainder will be the contained angle.
Application of the above Rules.
Two courses are given, viz. N. 670 W. and N. 280 E. to find
the angle.-Suppose yourself standing at the point where these courses meet. Reverse the letters of the first course, and they will stand thus,

> S. 670 E. N. 28 E. $\}$ case.

When the quantity of any angle in a survey is wanted, the preceding course must be reversed; then both courses will run from the same point.

## Converging of Meridians.

The breadth of a degree of longitude in any parallel of latitude is to the breadth of a degree upon the equator, as the Co-sine of that Lat. is to Radius.
R. : 60 Miles : : Co-sine of the Lat. : the breadth of a degree on that Lat.

| As Radius | - | 10.00000 |
| :--- | ---: | ---: |
| Is to 60 Miles, | - | 1.77815 |
| So is Co-sine Lat. 600 | 9.69897 |  |
|  |  | 11.47712 <br>  <br> To 30 Miles |
|  | - | 10.00000 |

## MISCELLANEOUS QUESTIONS.

1. At a certain point I took the elevation of a tower $\mathbf{3 0 1 5}$ -then measured toward the tower on an angle of depression 70333 feet to a level with the base of the tower, when I took the elevation again 80 .-Required the height of the tower and the distance from the second place of observation to the base ; also how much higher the land was at the place of the first observation than at the second.

$$
\begin{gathered}
\text { Ans.-Height, - } \quad-\quad 99.6 \text { feet. } \\
\begin{array}{l}
\text { Distance required, } \\
\text { Difference in the height of land, } \\
\text { 40.5 }
\end{array} \text { feet. } \\
\text { feet. }
\end{gathered}
$$

2. Two persons made observations on the altitude of a meteor, both being on the same side of it, and in a vertical plane passing through it. The distance of their stations were 200 rods apart, and at one the angle of elevation was $36{ }^{\circ} 25^{\prime}$, at the other $32^{\circ} 50^{\prime}$, and at the last the outer limb of the meteor
subtended an angle of $2^{\prime}$.-Required the distance from the last place of observation, also the height and diameter of it. $\boldsymbol{M}$. Q. R.

$$
\begin{array}{ccc}
\text { Answer.-The distance, } & 5 . . & \mathbf{3} . . \\
\hline & 60 \\
\text { Height, } & 3 \times 0 \quad . \\
\text { Diameter, } & 18 \text { feet } 2 \text { inches. }
\end{array}
$$

3. From the top of a steeple 165 feet high, the angle of depression of the nearest bank of a river is $11^{\circ} 15^{\prime}$, that of the opposite bank is $6^{\circ} 15^{\prime}$. Required the width of the river.

Answ. 41.13 rods.
4. What length of cart-tire will it take to band a wheel 5 feet in diameter? Answ. 15 feet 8 1-2 inches.
5. A gentleman laid out a garden in a circle, containing one acre, one quarter, and one rod, with a gravelled walk on the outer side of it within the circle which took up twelve rods of ground. What is the diameter of the circle, and what is the width of the walk ?

Answ. The diameter 16 rods-Width of the walk 4 feet.
6. Neptune laid out 1000 square miles of the surface of the sea in a circle, and sold to Aeolus all that part of it which lies without a concentric circle of one third of the diameter. What is the diameter, and how much was sold?

Ansio. The diameter 35.68 miles. The quantity sold 888.92 square miles.
7. A Farmer laid out an elliptical orchard, the longest diameter of which was 30 rods, and the shortest was 20 rods, and surrounded the same with a wall two feet thick, within the figure. What is the quantity within the wall, and how much is covered by it?
A. Q. R.

Answ. Within the wall 2 .. 3 .. 22
Covered by the wall, 9.3 rods.
8. From a point in an equilateral triangle, I measured the distances to each corner, and found them 20, 29, and 30 rods. Required the area and the length of the sides.*
A. Q. $R$.

Answ. The Area 5 .. 1 .. 33
Length of each side 45 rods.
9. Required the dimensions of a parallelogram, containing one acre and a half, bounded by 64 rods of fence.

Answ. 12 by 20 rods.
10. The area of a parallelogram is five acres one quarter and thirty-five rods, and the diagonal is forty-three rods. Required the length of the sides. . Answ. 35 by 25 rods.
11. Required the dimensions of a parallelogram containing twenty-six acres one quarter and twenty-four rods, when the length exceeds the breadth by fifty-two rods. Answ. 44 by 96 rods.
12. Required the dimensions of a parallelogram containing 250 acres, when the sides are in the proportion of 7 to 3 . Answ. 130.93 by 305 1-2.
13. The state of Connecticut contains a little upwards of 4828 square miles, or $3,090,000$ acres, including rivers, harbours, creeks, roads, \&c. if this quantity of land is laid in a square, what will be the length of each side?
M. Q. R.

Answ. 69 .. 1 .. 75.11
Note. In the Preface, it is observed that the Traverse Table in this book is calculated for any distance up to 50. After the Preface was printed, it was thought best to extend that Table to 70. The table of Logarithms is also much more extensive, than is noticed in the Preface.

[^9]
## MATHEMATICAL TABLES.

VIZ :

1. A Table of Logarithms for Numbers.
II. A Table of Logarithmic or Artificial Sines, Tangents, and Secants.
III. A Traverse Table, or Table of Difference of Latitude and Departure.
IV. A Table of Natural Sines.
I. a table of logarithms for numbers.

Logarithms are Numbers in Arithmetical Progression, corresponding to other Numbers in Geometrical Proportion.
As, $0.31 . \quad 2 . \quad 3 . \quad$ 4. Logarithm:.

The Lorarithm for any Number lin 10 is number of Decimals; for any Number between 10 and 100, it is 1 with Decimals; for any Number between 100 and 1000, it is 2 with Decimals, \&c. The whole Number in Logarithms, or the Number which stands at the left hand of the Decimal! point, is called the Index; and is always a unit less than the places of figures in the whole Number for which it is the Logaritlım: Thus,

$$
\text { rnerffin } \quad \text { is } \quad 3.81578
$$

subtended an angle of $2^{\prime}$.-Required the distance from the last place of observation, also the height and diameter of it.

$$
\begin{aligned}
& \boldsymbol{M} \text {. Q. R. } \\
& \text { Answer.-The distance, } 5 \text {.. } 3 \text {.. } 60 \\
& \text { Height, } 3 \text {.. } 0 \text {.. } 70 \\
& \text { Diameter, } 18 \text { feet } 2 \text { inches. }
\end{aligned}
$$

3. From the top of a steeple 165 feet high, the angle of depression of the nearest bank of a river is $11^{\circ} 15^{\prime}$, that of the opposite bank is $6^{\circ} 15^{\prime}$. Required the width of the river. Answ. 41.13 rods.
4. What length of cart-tire will it take to band a wheel 5 feet in diameter? Answ. 15 feet 8 1-2 inches.
5. A gentleman laid out a garden in a circle, containing one acre, one quarter, and one rod, with a gravelled walk on the outer side of it within the circle which took up twelve rods of ground. What is the diameter of the circle, and what is the width of the walk ?

Answ. The diameter 16 rods-Width of the walk 4 feet.
6. Neptune laid out 1000 square miles of the surface of the sea in a circle, and sold to Aeolus all that part of it which lies without a concentric circle of one third of the diameter. What is the diameter, and how much was sold?
Answo. The diameter $\mathbf{3 5 . 6 8}$ miles. The quantity sold 888.92 square miles.
7. A Farmer laid out an elliptical orchard, the longest diameter of which was 30 rods, and the shortest was 20 rods, and surrounded the same with a wall two feet thick, within the figure. What is the quantity within the wall, and how much is covered by it?
A. Q. $\boldsymbol{R}$.

Answ. Within the wall 2 .. 3 .. 22
Covered by the wall, 9.3 rods.
8. From a point in an equilateral triangle, I measured the distances to each corner, and found them 20, 29, and 30 rods. Required the area and the length of the sides.*
A. $Q$. $R$.

$$
\text { Answ. The Area } 5 . .1 \text {.. } 33
$$

Length of each side 45 rods.
9. Required the dimensions of a parallelogram, containing one acre and a half, bounded by 64 rods of fence.

Answ. 12 by 20 rods.
10. The area of a parallelogram is five acres one quarter and thirty-five rods, and the diagonal is forty-three rods. Required the length of the sides.

Insw. 35 by 25 rods.
11. Required the dimensions of a parallelogram containing twenty-six acres one quarter and twenty-four rods, when the length exceeds the breadth by fifty-two rods.

Answ. 44 bu 96 rads.

## ERRATA.

Appendix, page 89 , line 22, for "less," read legs. " " 101 line 25 , for "murstone,"- read meerstone. In site the second angle (near the figures 16, 90) should have been inserted the figure 2; this deficiency can easily: be supplied by the pen or pencil.

## MATHEMATICAL TABLES.

## VIZ :

1. A Table of Logarithms for Numbers.
II. A Table of Logarithmic or Artificial Sines, Tangents, and Secants.
III. A Traverse Table, or Table of Difference of Latitude and Departure.
1V. A Table of Natural Sines.

## I. a table of logarithms for numbers.

Logarithms are Numbers in Arithmetical Progression, corresponding to other Numbers in Geometrical Proportion. As, 0.3 1. 2. $3 . \quad$ 4. Logarithm:. 1. 10. 100.1000 .10000 . Numbers.

The Logarithm for any Number less than 10 is a certain number of Decimals; for any Number between 10 and 100, it is 1 with Decimals; for any Number between 100 and 1000, it is 2 with Decimals, \&c. The whole Number in Logarithms, or the Number which stands at the left hand of the Decimal point, is called the Index; and is always a unit less than the places of figures in the whole Number for which it is the Logarithm : Thus,

| The Log. of 6543 | is | 3.81578 |
| ---: | ---: | ---: |
| 654.3 | - | 2.81578 |
| 65.43 | - | 1.81578 |
| 6.543 | - | 0.81578 |

The Log. of a Decimal Fraction is the same as that of an Integer, only the Index is negative, and is distinguished from a positive one, by placing a Point, or a negative Sign before it : Thus,

The Log. of 0.6543 is $\quad 9.81578$ or -1.81578 .

$$
0.06543-\quad .8 .81578 \text { or }-2.81578 \text {. }
$$

Note.-In the following Table the Index is not prefixed. It may be easily supplied as it is always a unit less than the number. of figures in the corresponding natural whole number.

## To find the Logarithm of any Number.

If the Number is less than 100 , its Log. is found in the first page of the Table, directly opposite thereto: Thus, the Log. of 34 is 1.53148 .

If the Number consists of three figures, find it in the first column of the following part of the Table, opposite to which, and under 0, is the Log. : Thus the Log. of 346 is .53908 to which prefix 2 for the Index, because there are three places of figures in the whole Number.

If the given Number contains four figures, the first three are to be found, as before, in the side column, and under the fourth at the top of the table is the Log. to which the Index 3 is to be prefixed, if the given Number is an Integer: Thus the Log. of 3467 is .53995 to which prefix 3 for the Index.

If the given Number exceeds four figures, find the difference between the Log. of the first four figures, and the next following Log. Multiply this difference by the remaining figure or figures in the given Number; point off as many figures to the right hand as there are in the multiplier; and the remainder, added to the Log. of the first four figures, will be the required Log.

To find the Number corresponding to any given Logarithm.
Find the next less Log. to that given in the column marked 0 at the top, and continue the sight along that horizontal line, and the Log. the same as that gives, or very near it, will be found ; then the first three figures of the corresponding Number will be found opposite, in the first side column, and the fourth figure directly above, at the top of the page. If the Index of the given Log. is 3, the four figures thus found are whole numbers; if the Index is 2, the first three figures are whole numbers, and the fourth is a Decimal, and so on.
'To find the nearest number corresponding to any Log. for more than four figures, find the Log. next less than the given one, and take the difference between that and the given one; also take the difference between the next greater and the next less Log. than the given one ; divide the former difference by the latter, according to the Rule in Division of Decimals for dividing a less number by a greater; add the Quotient to the number answering to the Log. next less than the given one, and you will have the required Number; whether a whole, or a mixed Number will be determined by the Index.

The addition and subtraction of Logarithms answers the same purpose as the multiplication and division of their corres-
ponding Numbers: That is, the Log. of any two Numbers being added, their sum will be the Log. of the Product of those Numbers; and the Log. of one Number being subtracted from the Log. of another Number, the Remainder will be the Log. of the Quotient of one of those Numbers divided by the other. Again, the Log. of any Number being doubled will produce the Log. of the Square of that number; and one half the Log. of any Number is the Log. of the Square Root of that Number.
II. Of the Table of Logarithmic or Artificial Sines, Tangents, and Secants.

To find the Logarithmic Sine, §c. for any number of Degrees and Minutes, zeithin the compuss of the Table.

If the Degrees be less than 45 , look for them at the top of the columns, and under Sine, Tangent or Secant, whichever is wanted, and for the Minutes at the left hand; but if more than 45 , look for the Degrees at the bottom over Sine, \&c. and for the Minutes at the right hand ; under or over the Degrees and against the Minutes will be the required Log. Sine, \&c.

To find the Degrees and Minutes corresponding to a given Logarithmic Sine, \&c.

Look in the proper column for the nearest Log. to the given one; and the Degrees and Minutes standing over or under and against it, are those required.

Note. When the Log. Sine, \&c. for more than $90^{\circ}$ is required, subtract the given number of Degrees from $180^{\circ}$, and make use of the Remainder.
It will be observed that this Table is calculated only for every 5 Minutes. This was thought sufficient for Surveyors, as few Compasses will take a course to greater exactness. If, however, a Question is to be solved where greater accuracy is required, work by natural Sines. Or,

The Log. Sine, \&r. for any Minute may be found as follows:
Look in the Table for the Log. of the nearest number of Minutes greater than the given one, and from this subtract the next less Log. contained in the 'Table: Then say, as 5 Minutes, is to this difference; So is the excess of the given Minutes above $5,10,15,20,25, \& c$. ; To a fourth number, which add to the Log. of the Minutes next less than the given number, and the sum will be the Log. required.

## Example.

Required the Logarithmic Sine of $34^{\circ} 23^{\prime}$
Sine of $34^{\circ} 25^{\prime}$
9.75221

3420
9.75128

Difference
93

| As $5: 93:: 3: 56$ |  |
| :---: | ---: |
| Sine of $34^{\circ} 20^{\prime}$ | 9.75128 |
| Add | $-\quad 56$ |
| Sine of $34^{\circ} 23^{\prime}$ | 9.75184 |

To find the nearest Minutes corresponding to a given Loga sithmic Sine, \&c.

Look in the Table, in the proper column, for the Log. next less than the given one, and take the difference between that and the given one; also take the difference between the next greater and the next less Log. than the given one; Then say, As the latter difference; is to 5 Minutes; so is the former dif ference; to the number of Minutes to be added to the Minutes of the Log. next less than the given one.

Example.
Required the Degrees and Minutes corresponding to the Logarith. ritic Tangent 9.73597 .

| Given Log. | 9.73597 | Next greater Log. | $9.7362 \%$ |
| :---: | :---: | :---: | :---: |
| Yeit less | 9.73476 | Next less | 9.73470 |
| Difference | 121 | Difference | 151 |

As $151: 5:: 121: 4$
The Degrees and Minutes for the Log. next less than the given one are $28^{\circ} 30^{\prime}$ to which add $4^{\prime}$ and it makes $28^{\circ} 34^{\prime}$.

Note. As after the most careful attention of the Printers some figures in the Table may be wrong; and as some may be so blurred as to be illegible, let it be observed that the Sines and Co-Secants, the Co-Sines and Secants, and the Tangents and Co-Tangents, standing against each other respectively, being added together, will amount to 90.00000 , if the Tables are accurate. Thus against $25^{\circ}$ $20^{\prime}$ the Sine 9.67533 added to the Co-Secant $10.3236^{\circ}$
their sum is 20.00000 ; so also is the sum of the Co-Sine 9.94458 and the Secant 10.05542, and likewise the sum of the Tangent 9.73175 and the Co-Tangent 10.26825. An error may consequently be easily detected, or any defaced figure be supplied.

To calculate the Northing or Southing, \&c. for any Course and Disiance by Logarithms.

This is done by the first Case of Right Angled Trigonometry, as follows:

Find the Log. Sine and Co-Sine of the Course ; to each of these add the Log. of the Distance ; subtract Radius or 10.00000 from their sums, and the remainders will be the Log. of the required Latitude and Departure.

Note. When the Angle is very small or very large, and the Distance short, the sum of the Log. Sine or Co-Sine and the Log. of the Distance may be less than 10.00000 or Radius, which cannot therefore be subtracted. In such cases look for the Log. without regard to the Index, and the corresponding number will be a Decimal, the first figure of which will be tenths if the Index be 9 , and hundredths if the Index be 8 .

## A TABLE OF LOGARITHMS.



| No. 100-1600. |  |  |  |  |  |  | Log. 00c00-20413. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. |  |  |  |  |  |  | 6 | 7 | 8 | 9 |
| 10000 | 00000 | $\overline{00043}$ | 000870 | $\overline{00130}$ | $\overline{00173}$ | 0217 | 00260 | 00303 | 00346 | $\overline{00389}$ |
| 101 | 0432 | 0475 | 0518 | 0561 | 0604 | 0647 | 0689 | 0732 | 0775 | 0817 |
| 102 | 0860 | 0903 | 0945 | 0988 | 1030 | 1072 | 1115 | 1157 | 1199 | 1242 |
| 103 | 1284 | 1326 | 1368 | 1410 | 1452 | 1494 | 1536 | 1578 | 16 |  |
| 104 | 1703 | 1745 | 1787 | 1828 | 1870 | 1912 | 1953 | 1995 | 203 | 2078 |
| 105 | 2119 | 2160 | 2202 | 2243 | 2284 | 2325 | 2366 | 2407 | 24 | 2490 |
| 106 | 2531 | 2572 | 2612 | 2653 | 2694 | 2735 | 2776 | 2816 | 2857 | 28 |
| 107 | 2938 | 2979 | 3019 | 3060 | 3100 | 3141 | 3181 | 3222 | 3262 | 3302 |
| 108 | 3342 | 3383 | 3423 | 3463 | 3503 | 3543 | 3583 | 3623 | 3663 | 3703 |
| 109 | 3743 | 3782 | 3822 | 3862 | 3902 | 3941 | 3981 | 4021 | 4060 | 4100 |
| 110 | 41 | 4179 | 4218 | 4258 | 4297 | 4336 | 4376 | 4415 | 445 | 4493 |
| 111 | 4532 | 4571 | 4610 | 4650 | 4683 | 4727 | 476 | 4805 | 4844 | 3 |
| 112 | 4932 | 4961 | 4999 | 5038 | 5077 | 5115 | 5154 | 5192 | 523 |  |
| 113 | 5308 | 5346 | 5385 | 5423 | 5461 | 5500 | 5538 | 5576 | 561 | 5652 |
| 114 | 5690 | 5729 | 5767 | 5805 | 5843 | 5881 | 5918 | 5956 | 599 | 60 |
| 115 | 6070 | 6108 | 6145 | 6183 | 6221 | 6258 | 6296 | 6333 | 6371 |  |
| 116 | 6446 | 6483 | 6521 | 6558 | 6595 | 6633 | 6670 | 6707 | 6744 |  |
| 117 | 6819 | 6856 | 6893 | 6930 | 6967 | 7004 | 7041 | 7078 | 711 | 7151 |
| 118 | 7188 | 7225 | 7262 | 7298 | 7335 | 7372 | 7408 | 7445 |  | 7518 |
| 119 | 7555 | 7591 | 7628 | 7664 | 7700 | 7737 | 777 | 7809 |  |  |
| 120 | 7918 | 7954 | 7990 | 802 | 806 | 8099 | 8135 | 81 | 820 |  |
| 121 | 8279 | 8314 | 8350 | 8356 | 8422 | 8458 | 849 | 8599 | 856 |  |
| 122 | 8636 | 8672 | 8707 | 8743 | 8778 | 8814 | 8849 | 8884 | 892 |  |
| 123 | 8991 | 9026 | 9061 | 9096 | 9132 | 916 | 9202 | 9237 | 927 | 9307 |
| 124 | 9342 | ${ }_{9}^{9376}$ | 9412 | 9447 | 9482 | 9517 | 955 | 9587 | 962 | 9650 |
| 125 | 9691 | 9726 | 9760 | 9795 | 9830 | 9864 | 989 | 993 | 996 | 1000 |
| 126 | 10037 | 10072 | 10106 | 10140 | 10175 | 10209 | 10243 | 10278 | 1031 | 0346 |
| 127 | 0380 | 0415 | 0449 | 0483 | 0517 | 0551 | 058 | 0619 | 06 | 碞 |
|  | 0721 | 0755 | 0789 | 0823 | 0857 | C890 | 0924 | 0958 | 099 | 1025 |
| 129 | 1059 | 10 | 112 | 1160 | 1193 | 1227 | 1261 | 129 | 132 | 1361 |
| 13 | 1394 | 1428 | 1461 | 1494 | 152 | 1561 | 159 | 162 | 16 | 1694 |
| 131 | 1727 | 1760 | 1793 | 1826 | 1860 | 1893 | 1926 | 1959 | 199 | 202 |
| 132 | 2057 | 2090 | 2123 | 2156 | 2189 | 2222 | 2254 | 2287 | 232 | 235 |
|  | 2385 | 2418 | 2450 | 2483 | 2516 | 2548 | 2581 | 2613 | 264 | 2678 |
|  | 2710 | 2743 | 2775 | 2808 | 2840 | 2872 | 2905 | 2937 | 29 | 3001 |
| 135 | 3033 | 3066 | 3098 | 3130 | 3162 | 3194 | 3226 | 3258 | 3290 | 3322 |
|  | 3354 | 3386 | 3418 | 3450 | 3481 | 3513 | 3545 | $357 \%$ | 3609 | 9640 |
|  | 3672 | 3704 | 3735 | 3767 | 3799 | 3530 | 3862 | 3893 | 3925 | 3956 |
|  | 3988 | 4019 | 4051 | 4082 | 4114 | 4145 | 4176 | 4908 | 4238 | 4270 |
| 13 | 4301 | 4333 | 4364 | 4395 | 4426 | 4457 | 7489 | 4520 | 4551 |  |
| 140 | 4613 | 4644 | 4675 | 4706 | 4737 | 4768 | 4799 | 482 | 4860 | 48 |
|  | 4922 | 4953 | 4983 | 5014 | 5045 | 5076 | 5106 | 5137 | 516 |  |
| 142 | 5229 | 5259 | 5290 | 5320 | 5351 | 15381 | 15412 | 5442 | 5473 | 55 |
| 143 | 5534 | 5564 | 5594 | 5625 | 5655 | 5685 | 5715 | 5744 | 5776 | 65806 |
| 14 | 5836 | 5866 | 5897 | 5927 | 5957 | 5987 | 6017 | 6047 | 6077 | 7610 |
| 14 | 6137 | 6167 | 6197 | 6227 | 6256 | 6286 | 6316 | 6346 | 6376 |  |
| 146 | 6435 | 6465 | 6495 | 6524 | 6554 | 6584 | 6613 | 6643 | 6673 | 36702 |
| 14 | 6732 | 6761 | 6791 | 6820 | 6850 | 06879 | 6509 | $693 \varepsilon$ | 696 | 6997 |
| 148 | 7026 | 7056 | 87085 | 7114 | 7143 | 37173 | 7202 | 7231 | 726 | C 7289 |
| 149 | 7319 | 763 | 737 | 7406 | 7435 | 746 | 748 | 75 | 755 | 7580 |
| 150 | 7609 | 7638 | 7667 | 7696 | 7725 | 5 7754 | 4782 | 7811 | 7846 | 78 |
| 5 | 7898 | 7926 | 7955 | 57984 | 8013 | 38041 | 18070 | 8095 | 812 |  |
|  | 818 | 8213 | 3824 | 18270 | 8298 | 8327 | 78355 | 58384 | 4812 | 2844 |
| 153 | 8469 | 8498 | 8526 | 8554 | 8583 | 8611 | 18639 | 8667 | 869 | 872 |
| 154 | 8752 | 8780 | - 8808 | 8837 | 8865 | 88893 | 8921 | 8945 | 8977 | 900 |
|  | 9033 | 9061 | $1{ }^{1} 968{ }^{6}$ | 9117 | $7{ }^{9145}$ | $5{ }^{5173}$ | 39201 | 1 9229 | 9825 | 79285 |
|  | 9312 | 29340 | 19368 | 9396 | 9424 | 49451 | 1 9479 | 9 9507 | 795 | 956 |
|  | 9590 | 9618 | $8{ }^{9645}$ | 59673 | 89700 | 09728 | 89756 | 69783 | 9811 | 9838 |
| 158 | 9866 0140 |  | 7 9921 <br> 194  | 19948 <br> 0222 |  | ${ }^{7} 20003$ | 320030 |  | 820085 | 5520112 |
|  | $\frac{0}{0}$ | - | 0194 | 022 |  | 22, | , | 03 | $\left\|\frac{0358}{8}\right\|$ | - |


| No. 1600-2200. |  |  |  |  |  | Log. 20412-34242. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 |  | 2 : |  | 4 |  |  |  |  | 9 |
| 160 | 20439 | 20 | 20493 | 20 |  |  |  |  | 20656 |
| 1610683 | 0710 | 0737 | 0763 | 0790 | 081 | 084 | 0871 | 0898 | 0995 |
| 162 0952 | 0978 | 1005 | 1032 | 1059 | 1085 | 1112 | 1139 | 1165 | , |
| 1631219 | 1245 | 1272: | 1299 | 1325 | 1352 | 1378 | 1405 | 1431 | 1158 |
| 1641484 | 1511 | 1537 | 1564 | 1590 | 1617 | 1643 | 1669 | 1696 | 1792 |
| 1651748 | 1775 | 1801 | 1827 | 1854 | 1880 | 1906 | 1932 | 1958 |  |
| 1662011 | 2037 | 2063 | 2059 | 2115 | 2141 | 2167 | 2194 | 2220 | 2246 |
| 1672272 | 2298 | 2324 | 2350 | 2376 | 2401 | 2427 | 2453 | 2479 | 5 |
| 1682531 | 2557 | 2583 | 2608 | 2634 | 2660 | 2686 | 2712 | 2737 |  |
| 1692789 | 2814 | 2840 | 2866 | 2891 | 2017 | 29 | 29 | 299 | 3019 |
| 170 | 307 |  | 3121 | 31 | 317 | 3198 | 32 | 3249 |  |
| 3300 | 3325 | 3350 | 3376 | 3401 | 3426 | 3452 | 3477 | 3502 | 3528 |
| 172 3553 | 3578 | 3603 | 3629 | 3654 | 3679 | 3 | 3729 | 37 | 3779 |
| 3805 | 3830 | 3855 | 3880 | 3905 | 3930 | 3955 | 3980 | 4005 | 30 |
| 4055, | 4080 | 4105 | 4130 | 4155 | 4180 | 4204 | 4229 | 4254 | 4279 |
| 4304 | 4329 | 4353 | 4378 | 4403 | 4428 | 44 | 4477 | 4502 | 4527 |
| 4551 | 4576 | 4601. | 4625 | 4650 | 4674 | 4699 | 4724 | 4748 | 47 |
| 1774797 | 4822 | 4846 | 4871 | 4895 | 4920 | 494 | 4969 | 4993 | 5018 |
| 1785042 | 5066 | 5091 | 5115 | 5139 | 5164 | 5188 | 5212 | 5237 |  |
| 1795285 | 5310 | 5334 | 5358 | 5382 | 5406 | 5431 | 5455 | 547 | 03 |
| 5527 | 5551 | 5575 | 5600 | 56 | 5648 | 5672 |  |  |  |
| 1815768 | 5792 | 5816. | 5840 | 5864 | 5888 | 5912 | 5935 | 59 |  |
| 1826007 | 6031 | 6055 | 6079 | 6102 | 6126 | 6150 | 617 | 619 | 62 |
| 6245 | 6269 | 6293 | 6316 | 6340 | 6364 | 6357 | 6411 | 8435 | 625 |
| 6482. | 6505 | 6529 | 6553 | 6576 | 6000 | 6683 | 6647 | 6670 | 6694 |
| 6717 | 6741 | 6764, | 6788 | 6811 | 6834 | 6858 | 6881 | 690 |  |
| 6951 | 6975 | 6998 | 7021 | 7045 | 7068 | 7091 | 71 | 713 | 71 |
| 1877184 | 7207 | 7231 | 7254 | 7277 | 7300 | 7323 | 734 | 737 | 7393 |
| 1887416 | 7439 | 7462 | 748 | 750 | 7531 | 75 | 7577 | 76 |  |
| 1897646 | 7669 | 76921 | 771 | 77 | 7761 | 77 | 780 | 78 |  |
| 7875 | 7898 | 1 | 794 | 7967 |  |  |  |  |  |
| 1918103 | 8126 | 8149 | 817 | 8194 | 8217 | 824 | 836 | 828 | 83 |
| 1928330 | 8353 | 8375 | 8398 | 8421 | 8443 | 846 | 8 | 85 |  |
| 8556 | 8578 | 8601 | 36\% | 8646 | 8668 | 8691 | 8713 | 873 | 87 |
| 194.8780 | 8803 | 8825 | 8847 | 8870 | 889 | 891 | 893 | 8959 | 1- |
| 1959003 | 9026 | 9048 | 9070 | 9092 | 9115 |  | 9159 | 918 | 9203 |
| 196,9226 | 9248 | 9970 | 929 | 9314 | 9336 |  | 9330 | 9403 |  |
| 197 9447 <br> 198  | 9469 | 9491 | 951 | 9535 | 9557 | 957 | 9601 | 96 | 9645 |
|  | 9688 | 9710 | 973 | 9754 | 9776 | 979 | 982 | 98 | 98 |
| 199 988 | 9907 | 9929 | 9951 | 99 | 9994 | 300 |  |  |  |
| $\overline{200} \overline{30103}$ | 30125 | 30146 |  | , | 3021 |  |  |  |  |
| 2010320 | 0341 | 0364 | 0381 | 0406 | 0428 | 0449 | 047 | 0.4 | 0514 |
| 2090535 | 0557 | 0578 | 0 0 00 | 0621 | 0643 | 0664 | 068 | 070 | 072 |
| 2030750 | 0771 | 0792 | 0814 | 0835 | 0856 | 0878 | 089 | 0920 | 09 |
| 2040963 | 0984 | 1006 | 1027 | 1048 | 1069 | $1091{ }^{\text {i }}$ | 111 | 1133 |  |
| 2051175 | 1197 | 1218 | 1239 | 1260 | 1281 | 1302 | 1393 | 134 | 13 |
|  | 1408 | 1429 | 1450 | 1471 | 1492 | 1513 | 153 | 1555 | 1576 |
| 207 1597 | 1618 | 1639 | 1660 | 1681 | 1702 | 1793' | 174 | 176 | 178 |
| 2081806 | 1827 | 1848 | 1869 | 1890 | 1911 | 1931 ${ }^{\text {¹ }}$ | 195 | 197 |  |
| 2092015 | 2035 | 2056 | 2077 | 209 | 2118 | 2139 | 21 | 218 | 220 |
| 2929 | 22 | 2263 | 2284 | 2305 | 2325 | 2346 | 236 | 23 |  |
| 2112428 | 2449 | 9469 | 2490 | 2510 | 2531 | 255 | 257 | 259 |  |
| 112.2634 | 2654 | 2675 | 2695 | 2715 | 2736 | 2756 | 2777 | 279 | 281 |
| 2838 | 285 | 2879 | 2899 | 2919 | 2940 | 2960 | 2980 | 5001 | 302 |
| 2143041 | 3062 | 3082 | 3102 | 3192 | 3143 | 3163 | 318 | 320 |  |
| 3244 | 3264 | 3284 | 3304 | 3325 | 3345 | 3365 | 338 | 340 | 34 |
| 1163445 | 3465 | 3486 | 3506 | 3526 | 3546 | 3566 | 3586 | 3606 | 362 |
| 2173646 | 3666 | 3686 | 3706 | 3726 | 3746 | 3766 | 378 | 3800 | 3826 |
| 218,3846 | 3866 | 3885 | 3905 | 3925 | 3945 | 3965 | 3985 | 400 | 4025 |
| 219 4044 | 4064 | $4^{\prime} 84$ | 4104 | 4124 | 4143 | 4168 | 4183 | 420 | 4223 |
| No. 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |


| No. 2200-2800. |  |  |  |  |  | Log. 34242-44716. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.1 | 0 |  |  |  |  |  | 6 |  |  | 9 |
| 220 | 34242 | 34262 | 34282 | 34301 | 343 | 34341 | 34361 | 34380 | 3400 |  |
| 221 | 4439 | 4453 | 4479 | 4498 | 4518 | 4537 | 4557 | 4577 | 4596 | 4616 |
| 22 | 4635 | 4655 | 4674 | 4694 | 4713 | 4733 | 4753 | 4772 | 4792 | 4811 |
| 223 | 4830 | 4850 | 4869 | 4889 | 4908 | 4928 | 4947 | 4967 | 4986 | 5005 |
| 224 | 5025 | 5044 | 5064 | 5083 | 5102 | 5122 | 5141 | 5160 | 5180 | 5199 |
| 225 | 5218 | 5338 | 5257 | 5276 | 5295 | 5315 | 5334 | 5353 | 5372 | 5392 |
| 226 | 5411 | 5430 | 5449 | 5468 | 5488 | 5507 | 5526 | 5545 | 5564 | 5583 |
| 227 | 5603 | 5622 | 5641 | 5660 | 5679 | 5698 | 5717 | 5736 | 5755 | 5774 |
| 228 | 5793 | 5813 | 5832 | 5851 | 5870 | 5889 | 5908 | 5927 | 5946 | 5965 |
| 229 | 5984 | 6003 | 6021 | 6040 | 6059 | 6078 | 6097 | 6116 | 6135 | 6154 |
| 23 | 6173 | 6192 | 6211 | 6229 | 6248 | 6267 | 6286 | 6305 | 6324 | 6342 |
| 331 | 6361 | 6380 | 6399 | 6418 | 6436 | 6455 | 6474 | 6493 | 6511 | 6530 |
| 232 | 6549 | 6568 | 6586 | 6605 | 6624 | 6642 | 6661 | 6680 | 6698 | 6717 |
| 32 | 6736 | 6754 | 6773 | 6791 | 6810 | 6829 | 6847 | 6866 | 6884 | 6903 |
| 23 | 6922 | 6940 | 6959 | 6977 | 6996 | 7014 | 7033 | 7051 | 7070 | 7088 |
| 23 | 7107 | 7125 | 7144 | 7162 | 7181 | 7199 | 7218 | 7236 | 7254 | 7278 |
| 23 | 7291 | 7310 | 7328 | 7346 | 7365 | 7383 | 7401 | 7420 | 7438 | 7457 |
| 237 | 7475 | 7493 | 7511 | 7530 | 7548 | 7566 | 7585 | 7603 | 7621 | 7638 |
| 23 | 7658 | 7676 | 7694 | 7712 | 7731 | 7749 | 7767 | 7785 | 7803 | 7822 |
| 239 | 7840 | 7858 | 7876 | 7894 | 7912 | 7931 | 7949 | 7967 | 7985 | 8003 |
| 24 | 80\%1 | 8039 | 8057 | 8075 | 8093 | 8112 | 8130 | 8148 | 816 | 8184 |
| 241 | 8202 | 8220 | 8238 | 8256 | 8274 | 8292 | 8310 | 8328 | 8346 | 8364 |
| 242 | 8382 | 8399 | 8417 | 8435 | 8453 | 8471 | 8489 | 8507 | 8525 | 8543 |
| 24 | 8561 | 8578 | 8596 | 8614 | 8632 | 8650 | 8668 | 8686 | 8703 | 8721 |
| 244 | 8739 | 8757 | 8775 | 8792 | 8810 | 5828 | 8846 | 8863 | 8881 | 8899 |
| 345 | 8917 | 8934 | 8952 | 8970 | 8987 | 9005 | 9023 | 9041 | 9058 | 9076 |
| 246 | 9094 | 9111 | 9129 | 9146 | 916 | 9182 | 9199 | 9217 | 9235 | 9252 |
| 24 | 9270 | 9287 | 9305 | 9322 | 9340 | 9358 | 9375 | 9393 | 9410 | 9428 |
| 24 | 9445 | 9463 | 9420 | 9498 | 9515 | 9533 | 9550 | 9568 | 9585 | 9602 |
| 24 | 9620 | 9637 | 9655 | 9672 | 9690 | 9707 | 9724 | 974 | 97 | 77 |
| 25 | 9794 | 9811 | 9829 | 9846 | 9863 | 9881 | 9898 |  | 99 |  |
| 25 | 9967 | 9985 | 40002 | $4 \mathrm{C019}$ | 40037 | 40054 | 40071 | 4008 | 401 | 40123 |
| 95 | 40140 | 40157 | 0175 | 0192 | 0209 | 0226 | 0243 | 0261 | 0278 | 0295 |
| 253 | 0312 | 0329 | 0346 | 0364 | 0381 | 0398 | 0415 | 0432 | 0449 | 0466 |
| 25 | 0483 | 0500 | 0518 | 0535 | 0552 | 0569 | 0586 | 0603 | 0620 | 0637 |
|  | 0654 | 0671 | 0688 | 0705 | 0722 | 0739 | 0756 | 0773 | 0790 | 0807 |
|  | 0824 | 0841 | 0858 | 0875 | 0892 | 0909 | 0926 | 0943 | 0960 | 0976 |
| 25 | 0993 | 1010 | 1027 | 1044 | 1061 | 1078 | 1095 | 1111 | 1128 | 1145 |
| 25 | 1162 | 1179 | 1196 | 1212 | 1229 | 1246 | 1263 | 1280 | 1296 | 13 |
| 25 | 1330 | 1347 | 1363 | 1380 | 1397 | 141 | 1430 | 1447 | 146 | 81 |
| $\overline{260}$ | 1497 | 1514 | 1531 | 1547 | 1564 | 1581 | 1597 | 1614 | 1631 | 1647 |
| 261 | 1664 | 1681 | 1697 | 1714 | 1731 | 1747 | 1764 | 1780 | 1797 | 1814 |
| 262 | 1830 | 1847 | 1863 | 1880 | 1896 | 1913 | 1939 | 1946 | 1963 | 1979 |
| 26 | 1996 | 2012 | 2029 | 2045 | 2069 | 2078 | 2095 | 2111 | 2127 | 2141 |
| 26 | 2160 | 2177 | 2193 | 2210 | 2226 | 2243 | 2259 | 2275 | 2299 | 2308 |
| 26 | 2335 | 2341 | 2357 | 2375 | 2390 | 2406 | 2423 | 2439 | 2455 | 2472 |
| 266 | 2488 | 2504 | 2521 | 2537 | 2553 | 2570 | 2586 | 2602 | 2619 | 2635 |
| 26 | 2651 | 2667 | 2684 | 2700 | 2716 | 2732 | 2749 | 2765 | 2781 | 2797 |
| 26 | 2813 | 2830 | 2846 | 2862 | 2878 | 2894 | 2911 | 2927 | 2943 | 2959 |
| 269 | 2975 | 2991 | 3008 | 3024 | 3040 | 3056 | 3072 | 3088 | 3104 | 3120 |
| 27 | 3136 | 3152 | 3169 | $\overline{3185}$ | 3 201 | 3217 | 3933 | $\overline{3249}$ | 3265 | 3281 |
| 271 | 3297 | 3313 | 3329 | 3345 | 3361 | 3377 | 3393 | 3409 | 3435 | 3441 |
| 272 | 3457 | 3473 | 3489 | 3505 | 3521 | 3537 | 3553 | 3569 | 3584 | 3600 |
| 27 | 3516 | 3639 | 3648 | 3664 | \| 3680 | 3696 | 3712 | 3727 | / 3743 | 3759 |
| 274 | - 3775 | 3791 | 3807\| | - 3893 | 3838 | 3854 | 3870 | 3886 | 3902 | 3917 |
| 275 | 3933 | 3949 | 3965 | . 3981 | 3996 | 4012 | 4028 | 4044 | 4059 | 4075 |
| 276 | 4091 | 4107 | 4129 | - 4138 | 4154 | 4170 | 4185 | 4201 | 4217 | 4232 |
| 277 | 4248 | 4264 | 4279 | . 4295 | 4311 | 4326 | 4342 | 4358 | 4373 | 4389 |
| 278 | 4404 | 4420 | - 4136 | - 4451 | 4467 | 4483 | 4498 | 4514 | 4529 | 4545 |
| 279 | 4560 | 4576 | 4592 | 4607 | 4693 | 4638 | 4654 | 4669 | 4685 | 4700 |
| vo. | . 0 |  |  | , 3 | 2 | 5 | 6 | 7 | 18 | 9 |

## A TABLE OF LOGARITHMS.

| No. 2800-3400. |  |  |  |  |  |  | Log. 44716-53148. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 |  |  |  |  |  |  | 17 | 8 | 9 |
| 280 | 44716 | $\overline{44731}$ | $\overline{44747}$ | 44762 | $\overline{44778}$ | 84793 | 44809 | 44824 | 4840 | $\frac{}{44855}$ |
| 281 | 4871 | 4886 | 4902 | 4917 | 4932 | 4948 | 4963 | 4979 | 499 | 5010 |
| 28 | 5025 | 5040 | 5056 | 5071 | 5086 | 5102 | 5117 | 5133 | 514 | 5163 |
| 283 | 5179 | 5194 | 5209 | 5225 | 5240 | 5255 | 5271 | 528 | 5301 | 5317 |
| 284 | 5332 | 5347 | 5362 | 5378 | 5393 | 5408 | 5423 | 5439 | 5454 | 5469 |
| 285 | 5484 | 5500 | 5515 | 5530 | 5545 | 5561 | 5576 | 5591 | 560 | 5621 |
| 286 | 5637 | 5652 | 5667 | 5682 | 5697 | 5712 | 5728 | 5743 | 575 | 5773 |
| 287 | 5788 | 5803 | 5318 | 5834 | 5849 | 5864 | 5879 | 5894 | 5909 | 5924 |
| 988 | 5939 | 5954 | 5969 | 5934 | 6000 | 6015 | 6030 | 6045 | 606 | 6075 |
| 289 | 6090 | 6105 | 6120 | 6135 | 6150 | 6165 | 6180 | 619 | 621 | 6225 |
| $\overline{290}$ | 6240 | 6255 | 6270 | 6285 | 6300 | 6315 | 6330 | 63 | 6359 | 4 |
| 291 | 6389 | 6404 | 6419 | 6434 | 6449 | 6464 | 6479 | 649 | 650 | 6523 |
| 292 | 6538 | 6553 | 6568 | 6583 | 6598 | 6613 | 6627 | 6642 | 665 | 66 |
| 293 | 6687 | 6702 | 6716 | 6731 | 6746 | 6761 | 6776 | 6790 | 680 | 6820 |
| 294 | 6835 | 6850 | 6864 | 6879 | 6894 | 6909 | 6923 | 693 | 695 | 67 |
| 295 | 6982 | 6997 | 7012 | 7026 | 7041 | 7056 | 7070 | 708 | 710 | 7114 |
| 29 | 7129 | 7144 | 7159 | 7173 | 7188 | 7202 | 7217 | 72 | 724 | 7261 |
| 29 | 7276 | 7290 | 7305 | 7319 | 7334 | 7349 | 7363 | 7378 | 739 | 7407 |
| 298 | 7422 | 7436 | 7451 | 7465 | 7480 | 7494 | 7509 | 752 | 753 | 7553 |
| 299 | 7567 | 7582 | 7596 | 7611 | 7625 | 7640 | 765 | 760 | 768 | 69 |
| 300 | 7712 | 7727 | 7741 | 7756 | 7770 | 7784 | 7799 | 781 | 782 | 2 |
| 301 | 7857 | 7871 | 7885 | 7900 | 7914 | 7929 | 7943 | 795 | 797 | 7986 |
| 302 | 8001 | 8015 | 8029 | 804 | 8058 | 8073 | 8087 | 810 | 8116 | 0 |
| 303 | 8144 | 8159 | 8173 | 8187 | 8202 | 8216 | 3230 | 824 | 825 | 8273 |
| 304 | 8287 | 8302 | 8316 | 8330 | 8344 | 8359 | 8373 | 838 | 8401 | 8416 |
| 305 | 8430 | 8444 | 8458 | 8473 | 8487 | 8501 | 8515 | 8530 | 8544 | 8558 |
| 306 | 8572 | 8586 | 8601 | 8615 | 8629 | 8643 | $865{ }^{7}$ | 867 | 868 | 870 |
| 307 | 8714 | 8728 | 8742 | 8756 | 8770 | 8785 | 879 | 8813 | 882 | 88 |
| 308 | 8855 | 8869 | 8883 | 8897 | 8911 | 8926 | 8940 | 895 | 8968 |  |
| 309 | 8996 | 9010 | 9024 | 9038 | 9052 | 9066 | 90 | 909 | 910 | 9122 |
| $\overline{310}$ | 9136 | 9150 | 9164 | 9178 | 9192 | 9206 | 9220 | 223 | 924 |  |
| 311 | 9276 | 9290 | 9304 | 9318 | 9332 | 9346 | 9360 | 9374 | 938 | 940 |
| 312 | 9415 | 9429 | 9443 | 945 | 9471 | 9485 | 9499 | 9513 | 952 | 9541 |
| 313 | 9554 | 9568 | 9582 | 9596 | 9610 | 9624 | 9638 | 9651 | 966 | 9679 |
| 314 | 9693 | 9707 | 9721 | 9734 | 9748 | 9762 | 9776 | 9790 | 980 | 9817 |
| 315 | 9831 | 9845 | 9859 | 9872 | 9886 | 9900 | 9914 | 9927 | 9941 | 9955 |
| 316 | 9969 | 9982 | 9996 | 50010 | 50024 | 50037 | 50051 | 50065 | 50079 | 0092 |
| 317 | 50106 | 50120 | 50133 | 0147 | 0161 | 0174 | 018 | 0202 | 0215 | 0229 |
| 318 | 0243 | 0256 | 0270 | 0284 | 0297 | 0311 | 032 | 033 | 0352 | 0365 |
| 319 | 0379 | 0393 | 040 | 042 | 043 | 04 | 046 | 04 | 0488 | 0501 |
| 320 | 0515 | 0529 | 0542 | 0556 | 0569 | 058 | 0596 | 0610 | 032 | 0637 |
| 321 | 0651 | 0664 | 0678 | 0691 | 0705 | 0718 | 0732 | 0745 | 075 | 0772 |
| 322 | 0786 | 0799 | 0813 | 0826 | 0840 | 0853 | 0866 | 0880 | 089 | 090 |
| 323 | 0920 | 0934 | 0947 | 0961 | 0974 | 0987 | 1001 | 1014 | 102 | 1041 |
| 324 | 1055 | 1068 | 1081 | 1095 | 1108 | 1121 | 1135 | 114 | 116 | 1175 |
| 325 | 1188 | 1202 | 1215 | 1228 | 1242 | 1255 | 1268 | 128 | 129 | 1308 |
| 326 | 1322 | 1335 | 1348 | 1362 | 1375 | 1388 | 1402 | 1415 | 142 | 1441 |
| 327 | 1455 | 1468 | 1481 | 1495 | 1508 | 1521 | 153 | 1548 | 156 | 1574 |
| 328 | 1587 | 1601 | 1614 | 1627 | 1640 | 1654 | 1667 | 168 | 169 | 1706 |
| 329 | 1720 | 1733 | 1746 | 1759 | 1772 | 178 | 179 | 18 | 1825 | 1838 |
| 33 | 1851 | 1865 | 1878 | 1891 | 1904 | 1917 | 1930 | 1948 | 1957 | 1970 |
| 331 | 1983 | 1996 | 2009 | 2022 | 2035 | 2048 | 2061 | 2075 | 208 | 210 |
| 332 | 2114 | 2127 | 2140 | 2153 | 2166 | 2179 | 2192 | 2205 | 221 | 2231 |
| 333 | 2244 | 2257 | 2270 | 2284 | 2297 | 2310 | 2323 | 2336 | 2349 | 2362 |
| 334 | 2375 | 2388 | 2401 | 2414 | 2427 | 2440 | 2453 | 2466 | 2479 | 2492 |
| 335 | 2504 | 2517 | 2530 | 2543 | 2556 | 256 | 258 | 2595 | 260 | 2621 |
| 336 | 2634 | 2647 | 2660 | 2673 | 2686 | 2699 | 2711 | 2724 | 2737 | 2750 |
| 337 | 2763 | 2776 | 2789 | 2802 | 2815 | 2827 | 2840 | 2853 | 2866 | 2879 |
| 338 339 | 2892 | 2905 | 2917 | 2930 | 2943 | 2956 | 2969 | 2982 | 2991 | 300 |
| 339 | 3020 | 3033 | 3046 | 3058 | 3071 | 3084 | 3097 | 3110 | 31 | 31 |
| No. | 0 | 1 | 2 | 3 | 4 | 5 | -6 | 7 | 8 | 9 |


| No. $3400-4000$. |  |  |  |  |  | Log. 53148-60206. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 1 |  |  | 4 | 5 | 6 | 7 | 8 | 9 |
| 340 | 33148 | 53161 | $\overline{53173}$ | $\overline{53186}$ | $\overline{53199}$ | $\overline{53212}$ | 53224 | $\overline{53237}$ | $\stackrel{5}{5350}$ |  |
| 341 | 3275 | 3288 | 3301 | 3314 | 3326 | 3339 | 3352 | 3364 | 3377 | 3390 |
| 342 | 3403 | 3415 | 3428 | 3441 | 3453 | 3466 | 3479 | 3491 | 3504 | 3517 |
| 343 | 3529 | 3542 | 3555 | 3567 | 3580 | 3593 | 3605 | 3618 | 3631 | 3643 |
| 34 | 3656 | 3668 | 3681 | 3694 | 3706 | 3719 | 3732 | 3744 | 3757 | 3769 |
| 345 | 3782 | 3794 | 3807 | 3820 | 3832 | 3845 | 3857 | 3870 | 3882 | 3895 |
| 346 | 3908 | 3920 | 3933 | 3945 | 3958 | 3970 | 3983 | 3995 | 4008 | 4020 |
| 347 | 4033 | 4045 | 4058 | 4070 | 4083 | 4095 | 4108 | 4120 | 4133 | 4145 |
| 348 | 4158 | 4170 | 4183 | 4195 | 4208 | 4220 | 4233 | 4245 | 4258 | 4270 |
| 349 | 4283 | 4295 | 4307 | 4320 | 4332 | 4345 | 4357 | 4370 | 4382 | 4394 |
| 35 | 4407 | 4419 | 443 | 4444 | 445 | 4469 | 4481 | 4494 | 4506 | 4518 |
| 951 | 4531 | 4543 | 4555 | 4568 | 4580 | 4593 | 4605 | 4617 | 4630 | 4642 |
| 352 | 4654 | 4667 | 4679 | 4691 | 4704 | 4716 | 4728 | 4741 | 4753 | 4765 |
| 353 | 4777 | 4790 | 4802 | 4814 | 4827 | 4839 | 4851 | 4864 | 4876 | 4888 |
| 354 | 4900 | 4913 | 4925 | 4937 | 4949 | 4962 | 4974 | 4986 | 4998 | 5011 |
| 355 | 5023 | 5035 | 5047 | 5060 | 5072 | 5084 | 5096 | 5108 | 5121 | 5133 |
| 356 | 5145 | 5157 | 5169 | 5182 | 5194 | 5206 | 5218 | 5230 | 5242 | 5255 |
| 357 | 5267 | 5279 | 5291 | 5303 | 5315 | 5328 | 5340 | 5352 | 5364 | 5376 |
| 358 | 5388 | 5400 | 5413 | 5425 | 5437 | 5449 | 5461 | 5473 | 5485 | 5497 |
| 359 | 5509 | 5522 | 5534 | 5546 | 5558 | 5570 | 5582 | 5594 | 5606 | 5618 |
| $\overline{360}$ | 5630 | 5642 | 5654 | 5666 | 5678 | 5691 | 5703 | 5715 | 5727 | 5739 |
| 361 | 5751 | 5763 | 5775 | 5787 | 5799 | 5811 | 5823 | 5835 | 5847 | 5859 |
| 362 | 5871 | 5883 | 5895 | 5907 | 5919 | 5931 | 5943 | 5955 | 5967 | 5979 |
| 363 | 5991 | 6003 | 6015 | 6027 | 6038 | 6050 | 6062 | 6074 | 6086 | 6098 |
| 364 | 6110 | 6122 | 6134 | 6146 | 6158 | 6170 | 6182 | 6194 | 6205 | 6217 |
| 365 | 6229 | 6241 | 6253 | 6265 | 6277 | 6289 | 6301 | 6312 | 6324 | 6336 |
| 366 | 6348 | 6360 | 6372 | 6384 | 6396 | 6407 | 6419 | 6431 | 6443 | 6455 |
| 367 | 6467 | 6478 | 6490 | 6502 | 6514 | 6526 | 6538 | 6549 | 6561 | 6573 |
| 368 | 6585 | 6597 | 6608 | 6620 | 6632 | 6644 | 6656 | 6667 | 6679 | 6691 |
| 369 | 6703 | 6714 | 6726 | 6738 | 6750 | 6761 | 6773 | 6785 | 6797 | 6808 |
| [370 | 6820 | $\overline{6832}$ | 6844 | 6855 | 6867 | 6879 | 6891 | 6902 | 6914 | 6926 |
| 371 | 6937 | 6949 | 6961 | 6972 | 6984 | 6996 | 7008 | 7019 | 7031 | 7043 |
| 372 | 7054 | 7066 | 7078 | 7089 | 7101 | 7113 | 7124 | 7136 | 7148 | 7159 |
| 373 | 7171 | 7183 | 7194 | 7206 | 7217 | 7229 | 7241 | 7252 | 7264 | 7276 |
| 374 | 7287 | 7299 | 7310 | 7322 | 7334 | 7345 | 7357 | 7368 | 7380 | 7392 |
| 375 | 7403 | 7415 | 7426 | 7438 | 7449 | 7461 | 7473 | 7484 | 7496 | 7507 |
| 376 | 7519 | 7530 | 7542 | 7553 | 7565 | 7576 | 7588 | 7600 | 7611 | 7623 |
| 377 | 7634 | 7646 | 7657 | 7669 | 7680 | 7692 | 7703 | 7715 | 7726 | 7738 |
| 378 | 7749 | 7761 | 7772 | 7784 | 7795 | 7807 | 7818 | 7830 | 7841 | 7852 |
| 379 | 786 | 7875 | 7857 | 7898 | 7910 | 7921 | 7933 | 7944 | 7955 | 7967 |
| 380 | 7978 | 7990 | 8001 | 8013 | 8024 | 8035 | 8047 | 8058 | 8070 | 8081 |
| 381 | 8092 | 8104 | 8115 | 8127 | 8138 | 8149 | 8161 | 8172 | 8184 | 8195 |
| 382 | 8206 | 8218 | 8229 | 8240 | 8252 | 8263 | 8274 | 8286 | 8297 | 8309 |
| 383 | 8320 | 8331 | 8343 | 8354 | 8365 | 8377 | 8388 | 8399 | 8410 | 8422 |
| 384 | 8433 | 8444 | 8456 | 8467 | 8473 | 8490 | 8501 | 8512 | 8524 | 8535 |
| 385 | 8546 | 8557 | 8569 | 8580 | 8591 | 8602 | 8614 | 8625 | 8636 | 8647 |
| 386 | 8659 | 8670 | 8681 | 8692 | 8704 | 8715 | 8726 | 8737 | 8749 | 8760 |
| 387 | 5771 | 8782 | 8794 | 8805 | 8816 | 8827 | 8838 | 8850 | 8861 | 8872 |
| 388 | 8883 | 8894 | 8906 | 8917 | 8928 | 8939 | 8950 | 8961 | 8973 | 8984 |
| 38 | 8995 | 9006 | 9017 | 9028 | 9040 | 9051 | 9062 | 9073 | 9084 | 9095 |
| 390 | 9106 | 9118 | 9129 | 9140 | 9151 | 9162 | 9173 | 9184 | 9195 | 9207 |
| 391 | 9218 | 9229 | 9240 | 9251 | 9262 | 9273 | 9284 | 9295 | 9306 | 9318 |
| 392 | 9329 | 9340 | 9351 | 9362 | 9373 | 9384 | 9395 | 9406 | 9417 | 79488 |
| 393 | 9439 | 9450 | 9461 | 9472 | - 9483 | 9494 | 9506 | 9517 | 9528 | 9539 |
| 394 | 9550 | 9561 | 9572 | 9583 | 9594 | 9605 | 9616 | 9627 | 9638 | 9649 |
| 395 | 9660 | 9671 | 9682 | 9693 | 9704 | 9715 | 9726 | 9737 | 9748 | 9759 |
| 396 | 9770 | 9780 | 9791 | 9802 | 9813 | 9824 | 9835 | 9846 | 9857 | 9868 |
| 397 | 9879 | 9890 | 9901 | 9912 | 9923 | 9934 | 9945 | 9956 | 996 | 9977 |
| 398 <br> 398 | 9988 <br> 60097 | 9999 60108 | 60010 0119 | 60021 | 60032 0141 | 60043 | 60054 | 60065 0173 | 60076 | 60086 <br> 0195 |
| 398 | 60097 | 60108 | 0119 | 0130 | 0141 | 0152 | 016 | 0173 | 01 | 0195 |
| No | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |


| No. 4000-4600. |  |  |  |  |  |  | Log. 60206-66276. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 |  |  |  |  |  |  |  | 8 | 9 |
| $\stackrel{\square}{400}$ | 60206 | 60217 | $\overline{60228}$ | $\overline{60239}$ | 60249 | 60260 | 602 | 0282 | $\overline{60293}$ | 4 |
| 401 | 0314 | 0325 | 0336 | 0347 | 0358 | 0369 | 0379 | 0390 | 0401 | 0412 |
| 402 | 0423 | 0433 | 0444 | 0455 | 0466 | 0477 | 0487 | 0498 | 0509 | 0520 |
| 403 | 0531 | 0541 | $0 \cdot 52$ | 0563 | 0574 | 0584 | 0595 | 0606 | 0617 | 0627 |
| 404 | 0638 | 0649 | 0660 | 0670 | 068I | 0692 | 0703 | 0713 | 0724 | 0735 |
| 405 | 0746 | 0756 | 0767 | 0778 | 0788 | 0799 | 0810 | 0821 | 0831 | 0842 |
| 406 | 0853 | 0863 | 0874 | 0885 | 0895 | 0906 | 0917 | 0927 | 0938 | 0949 |
| 407 | 0959 | 0970 | 0981 | 0991 | 1002 | 1013 | 1023 | 1034 | 1045 | 1055 |
| 408 | 1066 | 1077 | 1087 | 1098 | 1109 | 1119 | 1130 | 1140 | 1151 | 1162 |
| 409 | 1172 | 1188 | 1194 | 1204 | 1215 | 1225 | 1236 | 1247 | 1257 | 1268 |
| 410 | 1278 | 1289 | 1300 | 1310 | 1321 | 1331 | 1342 | 1352 | 1363 | 1374 |
| 411 | 138 | 1395 | 1405 | 1416 | 1426 | 1437 | 1448 | 1458 | 1469 | 1479 |
| 412 | 1490 | 1500 | 1511 | 1521 | 1532 | 1542 | 1553 | 1563 | 157 | 1584 |
| 413 | 1595 | 1606 | 1616 | 1627 | 1637 | 1648 | 1658 | 1669 | 1679 | 1690 |
| 414 | 1700 | 1711 | 1721 | 1731 | 1742 | 1752 | 1763 | 1773 | 1784 | 1794 |
| 415 | 1805 | 1815 | 1826 | 1836 | 1847 | 1857 | 1868 | 1878 | 1888 | 1899 |
| 416 | 1909 | 1920 | 1930 | 1941 | 1951 | 1962 | 1972 | 1982 | 1993 | 2003 |
| 417 | 2014 | 2024 | 2034 | 2045 | 2055 | 2066 | 2076 | 2086 | 2097 | 2107 |
| 418 | 2118 | 2128 | 2138 | 2149 | 2159 | 2170 | 2180 | 2190 | 2201 | 2211 |
| 419 | 2221 | 2232 | 2242 | 2252 | 2263 | 2273 | 2284 | 2294 | 2304 | 2315 |
| 42 | 2325 | 2335 | 2346 | 2356 | 2366 | 2377 | $\overline{2387}$ | 2397 | 2408 | 2418 |
| 421 | 2428 | 2439 | 2449 | 2459 | 2469 | 2480 | 2490 | 2500 | 2511 | 2521 |
| 422 | 2531 | 2542 | 2552 | 2562 | 2572 | 2583 | 2593 | 2603 | 2613 | 2624 |
| 423 | 2634 | 2644 | 2655 | 2665 | 2675 | 2685 | 2696 | 2706 | 2716 | 2726 |
| 424 | 2737 | 2747 | 2757 | 2767 | 2778 | 2788 | 2798 | 2808 | 2818 | 2829 |
| 425 | 2839 | 2849 | 2859 | 2870 | 2880 | 2890 | 2300 | 2910 | 2921 | 2931 |
| 426 | 2941 | 2951 | 2961 | 2972 | 2982 | 2992 | 3002 | 3012 | 3022 | 3033 |
| 427 | 3043. | 3053 | 3063 | 3073 | 3083 | 3094 | 3104 | 3114 | 312 | 3134 |
| 428 | 3144 | 3155 | 3165 | 3175 | 3185 | 3195 | 3205 | 3215 | 3225 | 3236 |
| 429 | 3246 | 3256 | 3266 | 3276 | 3286 | 3296 | 3306 | 3317 | 3327 | 3337 |
| 43 | 3347 | 3357 | 3367 | 3377 | 3387 | 3397 | 3407 | 3417 | 3428 | 3438 |
| 431 | 3448 | 3458 | 3468 | 3478 | 3488 | 3498 | 3508 | 3518 | 3528 | 3538 |
| 432 | 3548 | 3558 | 3568 | 3579 | 3589 | 3599 | 3609 | 3619 | 3629 | 3639 |
| 433 | 3649 | 3659 | 3669 | 3679 | 3689 | 3699 | 3709 | 3719 | 372 | 3739 |
| 434 | 3749 | 3759 | 3769 | 3779 | 3789 | 3799 | 3809 | 3819 | 3829 | 3839 |
| 435 | 3849 | 3859 | 3869 | 3879 | 3889 | 3899 | 3909 | 3919 | 3929 | 3939 |
| 43 | 3949 | 3959 | 3969 | 3979 | 3988 | 3998 | 4008 | 4018 | 4028 | 4038 |
| 43 | 4048 | 4058 | 4068 | 4078 | 4088 | 4098 | 4108 | 4118 | 4128 | 4137 |
| 438 | 4147 | 4157 | 4167 | 4177 | 4187 | 4197 | 4207 | 4217 | 4227 | 4237 |
| 43 | 4246 | 4256 | 4266 | 4276 | 4286 | 4296 | 4306 | 4316 | 4326 | 4335 |
| $\overline{440}$ | 4345 | 4355 | 4365 | 4375 | 4385 | 4395 | 4404 | 4414 | 4424 | 4434 |
| 441 | 4444 | 4454 | 4464 | 4473 | 4483 | 4493 | 4503 | 4513 | 4523 | 4532 |
| 442 | 4542 | 4552 | 4562 | 4572 | 4582 | 4591 | 4601 | 4611 | 4621 | 4631 |
| 443 | 4640 | 4650 | 4660 | 4670 | 4680 | 4689 | 4699 | 4709 | 4719 | 4729 |
| 444 | 4738 | 4748 | 4758 | 4768 | 4777 | 4787 | 4797 | 4807 | 4816 | 4826 |
| 445 | 4836 | 4846 | 4856 | 4865 | 4875 | 4885 | 4895 | 4904 | 4914 | 4924 |
| 446 | 4933 | 4943 | 4953 | 4963 | 4972 | 4982 | 4992 | 5002 | 5011 | 5021 |
| 447 | 5031 | 5040 | 5050 | 5060 | 5070 | 5079 | 5089 | 5099 | 5108 | 5118 |
| 148 | 5128 | 5137 | 5147 | 5157 | 5167 | 5176 | 5186 | 5196 | 5205 | 5215 |
| 449 | 5225 | 5234 | 5244 | 5254 | 5263 | 5273 | 5283 | 5292 | 5302 | 5312 |
| 45 | 5321 | 5331 | 5341 | 5350 | 5360 | 5369 | 5379 | 5389 | 5398 | 5408 |
| 45 | 5418 | 5427 | 5437 | 5447 | 5456 | 5466 | 5475 | 5485 | 5495 | 5504 |
| 452 | 5514 | 5523 | 5533 | 5543 | 5552 | 5562 | 5571 | 5581 | 5591 | 5600 |
| 40 | 5610 | 5619 | 5629 | 5639 | 5648 | 5658 | 5667 | 5677 | 5686 | 5696 |
| 45 | 5706 | 5715 | 5725 | 5734 | 5744 | 5753 | 5763 | 5772 | 5782 | 5792 |
| 45 | 5801 | 5811 | 5820 | 5830 | 5839 | 5849 | 5858 | 5868 | 5877 | 5887 |
| 456 | 5896 | 5906 | 5916 | 5925 | 5935 | 5944 | 5954 | 5963 | 5973 | 5982 |
| 457 | 5992 | 6001 | 6011 | 6020 | 6030 | 6039 | 6049 | 6058 | 6068 | 6077 |
| 458 | 6087 | 6096 | 6106 | 6115 | 6124 | 6134 | 6143 | 6153 | 6162 | 6172 |
| 459 | 618 | 6191 | 6200 | 6210 | 6219 | 6229 | 6238 | 6247 | 6257 | 6266 |
|  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |


| No. 4600-5020. |  |  |  |  |  |  | Log. 66276-71600. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 |  |  |  |  |  |  |  |  |  |
| 460 | 66276 | 66285 | $\overline{66295}$ | 6630 | 66314 | 66323 |  |  |  |  |
| 461 | 6370 | 6330 | 6389 | 6398 | 6408 | 6417 | 6427 | 6436 | 6445 |  |
| 46 | 6464 | 6474 | 6483 | 6492 | 6502 | 6511 |  | 6530 | 6539 | 65 |
| 46 | 6558 | 6567 | 6577 | 6586 | 6596 | 6605 | 6614 | 6624 | 6633 |  |
| 46 | 6652 | 6661 | 6671 | 6680 | 6689 | 6699 | 6708 | 6717 | 6727 |  |
| 46 | 6745 | 6755 | 6764 | 6773 | 6783 | 6792 | 6801 | 6811 | 6820 | 68 |
| 46 | 6839 | 6848 | 6857 | 6867 | 6876 | 6385 | 6894 | 6904 | 6913 | 6992 |
| 467 | 6932 | 6941 | 6950 | 6960 | 6969 | 6978 | 6987 | 6997 | 7006 |  |
| 46 | 7025 | 7034 | 7043 | 7052 | 7062 | 70 | 7080 | 7089 | 7099 | 7108 |
| 46 | 7117 | 7127 | 7136 | 714 | 71 | 716 | 7173 | 718 | 719 |  |
| 47 | 7210 | , | 228 | 723 | 7247 | 7256 | 72 | 727 |  |  |
|  | 730 | 7311 | 7321 | 733 | 7339 |  | 73 | 736 |  | 7385 |
| 47 | 7394 | 7403 | 7413 | 7422 | 7431 | 7440 | 7449 | 745 | 7468 | 7 |
| 47 | 7486 | 7495 | 7504 | 7514 | 7523 | 7532 | 7541 | 755 | 7560 | 7569 |
| 47 | 7578 | 7587 | 7596 | 7605 | 7614 | 762 | 7633 | 764 | 7651 | 7660 |
| 47 | 7669 | 7679 | 7688 | 7697 | 7706 | 7715 | 7724 | 773 | 7742 | 7752 |
| 47 | 7761 | 7770 | 7779 | 7788 | 7797 | 7806 | 7815 | 782 | 783 | 78 |
| 4 | 7852 | 7861 | 7870 | 7879 | 7888 | 78 | 7906 | 7916 | 79 | 7934 |
| 47 | 7943 | 7952 | 7961 | 7970 | 79 | 79 | 7997 | 8006 | 80 | 1024 |
| 47 | 803 |  | 8052 | 8061 | 807 | 80 | 8088 | 8097 | 8106 | 15 |
| 48 | 8 | 8133 | 8142 | 81 | 8160 | 816 | 8178 | 8187 | 8196 | - |
| 48 | 8215 | 8224 | 8233 | 8242 | 8251 | 826 | 8269 | 8278 | 8287 | 8296 |
| 48 | 8305 | 8314 | 8323 | 8332 | 8341 | 8350 | 8359 | 8368 | 8377 | 83 |
| 48 | 8395 | 8404 | 8413 | 8422 | 8431 | 8440 | 8449 | 845 |  |  |
| 48 | 8485 | 8494 | 8502 | 8511 | 8520 | 8529 | 8538 | 8547 | 8556 | 8565 |
| 48 | 8574 | 8583 | 8592 | 8601 | 8610 | 8618 | 8628 | 8637 | 8646 | 8655 |
| 48 | 8664 | 8673 | 8681 | 8690 | 8699 | 87 | 8717 | 87 | 87 |  |
| 48 | 875 | 8762 | 8771 | 8780 | 8789 | 879 | 8806 | 881 | 8824 |  |
| 48 | 8842 | 8851 | 8860 | 8869 | 8878 | 888 | 8895 | 890 | 8913 | 8922 |
| 48 | 8931 | 8940 | 8949 | 89 | 89 | 89 | 89 | 899 | 90 |  |
| 490 | 9020 | 9028 |  | 9046 |  | 906 | 90 | 918 |  |  |
| 49 | 9108 | 9117 | 9126 | 9135 | 9144 | 91 | 9161 | 917 | 91 |  |
| 49 | 9197 | 9205 | 9214 | 9295 | 23 | 9241 | 9249 | 925 | 926 |  |
| 19 | 9285 | 9294 | 9302 | 9311 | 932 | 9329 | 9338 | 934 | 9 |  |
| 49 | 9373 | 9381 | 9390 | 9399 | 9408 | 9417 | 9425 | 94 | 9 |  |
| 49 | 9461 | 9469 | 9478 | 9487 | 9496 | 9504 | 9513 | 9522 |  | 9539 |
| 49 | 9548 | 9557 | 9566 | 9574 | 958 | 9592 | 9601 | 9609 | 9618 |  |
| 49 | 9636 | 9644 | 9653 | 9662 | 9671 | 9679 | 9688 | 9697 | 9705 |  |
| 49 | 9723 | 9732 | 9740 | 9749 | 9758 | 976 | 9775 | 978 | 9793 |  |
| 49 | 9810 | 9819 | 9827 | - |  |  | 98 |  |  | 9888 |
| 50 |  |  | 991 | , | 9332 |  | 9949 | , |  |  |
| 501 | 9984 | 9992 | 70001 | 70010 | 70018 | 700 | 70036 | 7004 |  |  |
| 50 | 7007 | 70079 | 008 | 0096 | 0105 | 011 | 0122 | 0131 | 0140 |  |
| 50 | 015 | 0165 | 0174 | 0183 | 0191 | 020 | 0209 | 0217 | 0226 |  |
| 50 | 0243 | 0252 | 0260 | 0269 | 0278 | 028 | 0295 | 0303 | 0312 | 0321 |
| 50 | 0329 | 0338 | 034 | 035 | 03 | 03 | 0381 | 0389 | 0398 | 04 |
| 50 | 0415 | 0424 | 0432 | 044] | 0449 | 0458 | 0467 | 0475 | 048 | 0492 |
| 50 | 0501 | 0509 | 0518 | 0526 | 0535 | 0544 | 0552 | 0561 | 0563 | 057 |
| 50 | 0586 | 0595 | 060 | 0612 | 0621 | 062 | 06 | 0646 | 0655 | 0663 |
| 50 | 0672 | 0680 | 06 | 0697 | 07 | 07 | 0723 | 0 | 07 | 07 |
|  | 0 | 076 |  | 0783 | 0791 | 0800 |  | 081 | 0825 | 0834 |
| 51 | 0842 | 0851 | 08 | 086 | 08 | 088 | 08 | 0902 | 0910 | 0919 |
| 51 | 0927 | 0935 | 0944 | 0952 | 0961 | 0969 | 0978 | 0986 | 0995 | 1003 |
| 51 | 1012 | 1020 | 1029 | 1037 | 1046 | 105 | 1063 | 107 | 1079 | 1088 |
|  | 1096 | 1105 | 1113 | 1122 | 1130 | 113 | 1147 | 115 | 1164 | 1172 |
| 51 | 1181 | 1189 | 1198 | 1206 | 1214 | 1223 | 1231 | 1240 | 1248 | 1257 |
| 51 | 1265 | 1273 | 1282 | 1290 | 1299 | 1307 | 1315 | 1324 | 1332 | 1341 |
| 517 | 1349 | 1357 | 1366 | 1374 | 1383 | 1391 | 1399 | 1408 | 1416 | 1425 |
| 51 | 1433 | 1441 | 1450 | 1458 | 1466 | 1475 | 1483 | 1492 | 1500 | 1509 |
| 51 | 1517 | 1525 | 1533 | 1542 | 155 | 15 | 156 | 1575 | 158 | 1592 |
| vo | 0 |  | 2 |  |  | 5 | 6 | 7 | 8 | 9 |




| No. 6400-7000. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 640 | 806 | 8062 | 80632 | 80638 | $\overline{80645}$ | 80652 | $\overline{80659}$ | 80665 | $\overline{80672}$ | 80679 |
| 641 | 0686 | 0693 | 0699 | 0766 | 0713 | 0720 | 0726 | 0733 | 0740 | 0747 |
| 642 | 0754 | 0760 | 0767 | 0774 | 0781 | 0787 | 0794 | 0801 | 0808 | 0814 |
| 643 | 0821 | 0828 | 0835 | 0841 | 0848 | 0855 | 0862 | 0869 | 0875 | 0882 |
| 644 | 0889 | 0895 | 0902 | 0909 | 0916 | 0922 | 0929 | 0936 | 0943 | 0949 |
| 645 | 0956 | 0963 | 0969 | 0976 | 0983 | 0990 | 0996 | 1003 | 1010 | 1017 |
| 646 | 1023 | 1030 | 1037 | 1043 | 1050 | 1057 | 1064 | 1070 | 1077 | 1084 |
| 647 | 1090 | 1097 | 1104 | 1111 | 1117 | 1124 | 1131 | 1137 | 1144 | 1151 |
| 648 | 1158 | 1164 | 1171 | 1178 | 1184 | 1191 | 1198 | 1204 | 1211 | 1218 |
| 649 | 1224 | 1231 | 1238 | 1245 | 1251 | 1258 | 1265 | 1271 | 1278 | 1285 |
| 650 | 1291 | 1298 | 1305 | 13 | 13 | 1325 | 1331 | 1338 | 1345 | 1 |
| 651 | 1358 | 1365 | 1371 | 1378 | 1385 | 1391 | 1398 | 1405 | 1411 | 1418 |
| 652 | 1425 | 1431 | 1438 | 1445 | 1451 | 1458 | 1465 | 1471 | 1478 | 1485 |
| 653 | 1491 | 1498 | 1505 | 1511 | 1518 | 1525 | 1531 | 1538 | 1544 | 1551 |
| 654 | 1558 | 1564 | 1571 | 1578 | 1581 | 1591 | 1598 | 1604 | 1611 | 1617 |
| 655 | 1624 | 1631 | 1637 | 1644 | 1651 | 1657 | 1664 | 1671 | 1677 | 1694 |
| 656 | 1690 | 1697 | 1704 | 1710 | 1717 | 1723 | 1730 | 1737 | 1743 | 1750 |
| 657 | 1757 | 1763 | 1770 | 1776 | 1783 | 1790 | 1796 | 1803 | 1809 | 1816 |
| 658 | 1823 | 1829 | 1836 | 1842 | 1849 | 1856 | 1862 | 1869 | 1875 | 1882 |
| 659 | 1889 | 1895 | 1902 | 1908 | 1915 | 1921 | 1928 | 1935 | 1941 | 1948 |
| 660 | 1954 | 1961 | 1968 | 1974 | 1981 | 1987 | 1994 | 2000 | 2007 | 2014 |
| 661 | 2020 | 2027 | 2033 | 2040 | 2046 | 2053 | 2060 | 2066 | 2073 | 2079 |
| 662 | 2086 | 2092 | 2099 | 2105 | 2112 | 2119 | 2125 | 2132 | 2138 | 2145 |
| 663 | 2151 | 2158 | 2164 | 2171 | 2178 | 2184 | 2191 | 2197 | 2204 | 2210 |
| 664 | 2217 | 2223 | 2230 | 2236 | 2243 | 2249 | 2256 | 2263 | 2269 | 2276 |
| 665 | 2282 | 2289 | 2295 | 2302 | 2308 | 2315 | 2321 | 2328 | 2334 | 2341 |
| 666 | 2347 | 2354 | 2360 | 2367 | 2373 | 2380 | 2387 | 2393 | 2400 | 2406 |
| 667 | 2413 | 2419 | 2426 | 2432 | 2439 | 2445 | 2452 | 2458 | 2465 | 2471 |
| 668 | 2478 | 2484 | 2491 | 2497 | 2504 | 2510 | 2517 | 2523 | 2530 | 2536 |
| 669 | 2543 | 2549 | 2556 | 2562 | 2569 | 2575 | 2582 | 2588 | 2595 | 2601 |
| 67 | 2607 | 2614 | 2620 | 2627 | 2633 | 2640 | 2646 | 2653 | 2659 | 2666 |
| 671 | 2672 | 2679 | 2685 | 2692 | 2698 | 2705 | 2711 | 2718 | 2724 | 2730 |
| 672 | 2737 | 2743 | 2750 | 2756 | 2763 | 2769 | 2776 | 2782 | 2789 | 2795 |
| 673 | 2802 | 2808 | 2814 | 2821 | 2827 | 2834 | 2840 | 2847 | 2853 | 2860 |
| 67 | 2866 | 2872 | 2879 | 2885 | 2892 | 2898 | 2905 | 2911 | 2918 | 2924 |
| 675 | 2930 | 2937 | 2943 | 2950 | 2956 | 2963 | 2969 | 2975 | 2982 | 2988 |
| 676 | 2995 | 3001 | 3008 | 3014 | 3020 | 3027 | 3033 | 3040 | 3046 | $305 \%$ |
| 677 | 3059 | 3065 | 3072 | 3078 | 3085 | 3091 | 3097 | 3104 | 3110 | 3117 |
| 678 | 3123 | 3129 | 3136 | 3142 | 3149 | 3155 | 3161 | 3168 | 3174 | 3181 |
| 679 | 3187 | 3193 | 3200 | 3206 | 3213 | 3219 | 3225 | 3232 | 3238 | 3245 |
| 680 | 3251 | 3257 | 3264 | 3270 | 3276 | 3283 | 3289 | 3296 | 3302 | 3308 |
| 681 | 3315 | 3321 | 3327 | 3334 | 3340 | 3347 | 3353 | 3359 | 3366 | 3372 |
| 682 | 3378 | 3385 | 3391 | 3398 | 3404 | 3410 | 3417 | 3423 | 3429 | 3436 |
| 683 | 3442 | 3448 | 3455 | 3461 | 3467 | 3474 | 3480 | 3487 | 3493 | 3499 |
| 684 | 3506 | 3512 | 3518 | 3525 | 3581 | 3537 | 3544 | 3550 | 3556 | 3563 |
| 685 | 3569 | 3575 | 3582 | 3588 | 3594 | 3601 | 3607 | 3613 | 3620 | 3626 |
| 686 | 3632 | 3639 | 3645 | 3651 | 3658 | 3664 | 3670 | 3677 | 3683 | 3689 |
| 687 | 3696 | 3702 | 3708 | 3715 | 3721 | 3727 | 3734 | 3740 | 3746 | 3753 |
| 688 | 3759 | 3765 | 3771 | 3778 | 3784 | 3790 | 3797 | 3803 | 3809 | 3816 |
| 689 | 3822 | 3828 | 3835 | 3841 | 3847 | 3853 | 3860 | 3866 | 3872 | 3879 |
| 690 | 3885 | 3891 | 3897 | 3904 | 3910 | 3916 | 3923 | 3929 | 3935 | 3942 |
| 691 | 3948 | 3954 | 3960 | 3967 | 3973 | 3979 | 3985 | 3992 | 3998 | 4004 |
| 692 | 4011 | 4017 | 4023 | 4029 | 4036 | 4042 | 4048 | 4055 | 4061 | 4067 |
| 693 | 4073 | 4080 | 4086 | 4092 | 4098 | 4105 | 4111 | 4117 | 4123 | 4130 |
| 694 | 4136 | 4142 | 4148 | 4155 | 4161 | 4167 | 4173 | 4180 | 4186 | 4192 |
| 695 | 4198 | 4205 | 4211 | 4217 | 4223 | 4230 | 4236 | 4242 | 4248 | 4255 |
| 696 | 4261 | 4267 | 4273 | 4280 | 4286 | 4292 | 4298 | 4305 | 4311 | 4317 |
| 697 | 4323 | 4330 | 4336 | 4342 | 4348 | 4354 | 4361 | 4367 | 4373 | 4379 |
| 698 | 4386 | 4392 | 4398 | 4404 | 4410 | 4417 | 4423 | 4429 | 4435 | 4442 |
| 699 | 4448 | 4454 | 4460 | 4466 | 4473 | 4479 | 4485 | 4491 | 4497 | 4504 |
| No. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |


| No. $7000-7600$. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 11 | 2 |  | 4 | 5 | 6 | 7 | 8 | 9 |
| 700 | 84510 | 451 | 4522 | 8459 | 84535 | 909 | 450 | 4553 | 4559 | 84566 |
| 701 | 4572 | 4578 | 4584 | 4590 | 4597 | 4603 | 4609 | 4615' | 4621 |  |
| 702 | 4634 | 4640 | 4646 | 4652 | 4658 | 4665 | 4671 | 4677 | 4683 |  |
| 703. | 4696 | 4702 | 4708 | 4714 | 4720 | 4726 | 4733 | 4739 | 4745 |  |
| 704 | 4757 | 4763 | 4770 | 4776 | 4782 | 4788 | 4794 | 4800 | 4807 | 3 |
| 705 | 4819 | 4825 | 4831 | 4837 | 4844 | 4850 | 4856 | 4862 | 4868 | 4874 |
| 706 | 4880 | 4887 | 4893 | 4899 | 4905 | 4911 | 4917 | 4924 | 4930 |  |
| 707 | 4942 | 4948 | 4954 | 4960 | 4967 | 4973 | 4979 | 4985 | 4991 |  |
| 708 | 5003 | 5009 | 5016 | 5022 | 5028 | 5034 | 5040 | 5046 | 5052 |  |
| 709 | 5065 | 5071 | 5077 | 5083 | 5089 | 5095 | 5101 | 5107 | 5114 | 20 |
| 710 | 5126 | 5132 | 5138 | 5144 | 5150 | 5156 | 5163 | 5169 | 523 |  |
| 711 | 5187 | 5193 | 5199 | 5205 | 5211 | 5217 | 5224 | 5230 | 52 |  |
| 712 | 5248 | 5254 | 5260 | 5266 | 5272 | 5278 | 5285 | 5291 | 5297 |  |
| 713 | 5309 | 5315 | 5321 | 5327 | 5333 | 5339 | 5345 | 5352 | 5358 |  |
| 714 | 5370 | 5376 | 5382 | 5388 | 539 | 5400 | 5406 | 5412 | 5418 |  |
| 1715 | 5431 | 5437 | 5443 | 5449 | 5455 | 5461 | 5467 | 5473 | 5479 |  |
| 1716 | 5491 | 5497 | 5503 | 5509 | 5516 | 5522 | 5528 | 5534 | 5540 | 5546 |
| 717 | 5552 | 5558 | 5564 | 5570 | 5576 | 5582 | 5588 | 5594 | 5600 |  |
| 718 | 5612 | 5618 | 5625 | 5631 | 5637. | 5643 | 5649 | 5655 | 5661 |  |
| 719 | 5673 | 5679 | 5685 | 5691 | 5697 | 5703 | 5709 | 5715 | 5721 | 57 |
| 720 | 5733 | 5739 | 5745 | 5751 | 5757 | 5763 | 5769 | 5775 | 5781 |  |
| 721 | 5794 | 5800 | 5806 | 5812 | 5818 | 5824 | 5830 | 5836 | 5842 |  |
| 722 | 5854 | 5860 | 5866 | 5872 | 5878 | 5884 | 5890 | 5896 | 5902: |  |
| 723 | 5914 | 5920 | 5926 | 5932 | 5938 | 5944 | 5950 | 5956 | 5962 |  |
| 724 | 5974 | 5980 | 5986 | 5992 | 5998 | 6004 | 6010 | 6016 | 6022. |  |
| 725 | 6034 | 6040 | 6046 | 6052 | 6058 | 6064 | 6070 | 6076 | 6082 |  |
| 726 | 6094 | 6100 | 6106 | 6112 | 6118 | 6124 | 6130 | 6136 | 6141 |  |
| 727 | 6153 | 6159 | 6165 | 6171 | 6177 | 6183 | 6189 | 6195 | 6201 |  |
| 728 | 6213 | 6219 | 6225 | 6231 | 6237 | 6243 | 6249 | 6255 | 6261 | 62 |
| 729 | 6273 | 6279 | 6285 | 6291 | 6297 | 6303 | 6308 | 631 | 6320 |  |
| 730 | 6332 | 6338 | 6344 | 6350 | 6356 | 6362 | 6368 | 6374 | 6380 | 63 |
| 731 | 6392 | 6398 | 6404 | 6410 | 6415 | 6421 | 6427 | 6433 | 6439 |  |
| 732 | 6451 | 6457 | 6463 | 6469 | 6475 | 6481 | 6487 | 6493 | 6499 |  |
| 733 | 6510 | 6516 | 6522 | 6528 | 6534 | 6540 | 6546 | 6552 | 6558. | 6564 |
| 734 | 6570 | 6576 | 6581 | 6587 | 6593 | 6599 | 6605 | 6611 | 6617 |  |
| 735 | 6629 | 6635 | 6641 | 6646 | 6652 | 6658 | 6664 | 6670 | 6676 | 66 |
| 736 | 6688 | 6694 | 6700 | 6705 | 6711 | 6717 | 6723 | 6729 | 6735 |  |
| 737 | 6747 | 6753 | 6759 | 6764 | 6770 | 6776 | 6782 | 6788 | 6794 | 880 |
| 738 | 6806 | 6812 | 6817 | 6823 | 6829 | 6835 | 6841 | 6847 | 6853 | 68 |
| 739 | 6864 | 6870 | 6876 | 6882 | 6888 | 6894 | 6900 | 69 | 6911 | 6917 |
| 740 | 6923 | 6929 | 6935 | 6941 | 6947 | 6953 | ${ }^{6958}$ | 696 | 6970 | 69 |
| 741 | 6982 | 6988 | 6994 | 6999 | 7005 | 7011 | 7017 | 7023 | 7029 | 7035 |
| 742 | 7040 | 7046 | 7052 | 7058 | 7064 | 7070 | 7075 | 708 | 7087 | 7093 |
| 743 | 7099 | 7105 | 7111 | 7116 | 7122 | 7128 | 7134 | 7140 | 714 | 7151 |
| 744 | 7157 | 7163 | 7169 | 7175 | 7181 | 7186 | 7192 | 7198 | 7204 | 7210 |
| 745 | 7216 | 7221 | 7227 | 7233 | 7239 | 7245 | 7251 | 725 | 726 | 7263 |
| 746 | 7274 | 7280 | 7286 | 7291 | 7297 | 7303 | 7309 | 7315 | 7320 | 7326 |
| 747 | 7332 | 7338 | 7344 | 7349 | 7355 | 7361 | 736 | 7373 | 7379 | 7384 |
| 748 | 7390 | 7396 | 7402 | 7408 | 7413 | 7419 | 742 | 7431 | 743 | 5 |
| 749 | 7448 | 7454 | 7460 | 7466 | 7471 | 7477 | 7483 | 7489 | 7495 | 7500 |
| 750 | 7506 | 7512 | 7518 | 7523 | 7529 | 7535 | 7541 | 7547 | 750 | 7558 |
| 751 | 7564 | 7570 | 7576 | 7581 | 7587 | 7593 | 7599 | 7604 | 7610 | 761 |
| 752 | 7622 | 7628 | 7633 | 7639 | 7645 | 7651 | 7656 | 7662 | 766 | 7674 |
| 753 | 7679 | 7685 | 7691 | 7697 | 7703 | 7708 | 7714 | 7720 | 772 | 773 |
| 754 | 7737 | 7743 | 7749 | 7754 | 7760 | 7766 | 7772 | 7777 | 7783 | 7789 |
| ${ }_{755}{ }^{1}$ | 7795 | 7800 | 7806 | 7812 | 7818 | 7823 | 7829 | 7835 | 7841 | 784 |
| 756 | 7852 | 7858 | 7864 | 7869 | 7875 | 7881 | 7887 | 7892 | 7898 | 790 |
| 757 | 7910 | 7915 | 7921 | 7927 | 7933 | 7938 | 7944 | 7950 | 7955 | 7961 |
| 758 | 7967 | 7973 | 7978 | 7984 | 7990 | 7996 | 8001 | 8007 | 8013 | 8018 |
| 759 | 8024 | 8030 | 8036 | 8041 | 8047 | 805 | 805 | 8064 | 8070 | 807 |
| No. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |


| No. 7600-8200. |  |  |  |  | Log. $88081-91381$. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NO. 0 | 1 | 2 | 3 | 41 | 5 | 6 | 7 | 8 | 9 |
| $\overline{760} 88081$ | $\overline{88087}$ | 8098 | 8098 | 881 | 1 | 881608 | 88121 | 88127 | 88133 |
| 7618138 | 8144. | 8150 | 8156 | 8161 | 8167 | 8173 | 8178 | 8184 | 8190 |
| 7628195 | 8201 | 8207 | 8213 | 8218 | 8224 | 8230 | 8235 | 8241 | 8247 |
| 7638252 | 8258 | 8264 | 8270 | 8275 | 8281 | 8287 | 8292 | 8298 | 8304 |
| 7648309 | 8315 | 8321 | 8326 | 8332 | 8338 | 8343 | 8349 | 8355 | 8360 |
| 7658366 | 8372 | 8377 | 8383 | 8389 | 8395 | 8400 | 8406 | 8412 | 8417 |
| 7668423 | 8429 | 8434 | 8440 | 8446 | 8451 | 8457 | 8463 | 8468 | 8474 |
| 7678480 | 8485 | 8491 | 8497 | 8502 | 8508 | 8513 | 8519 | 8525 | 8530 |
| 7688536 | 8542 | 8547 | 8553 | 8559 | 8564 | 8570 | 8576 | 8581 | 8587 |
| 7698593 | 85.98 | 8604 | 8610 | 8615 | 8621 | 8627 | 8632: | 8638 | 8643 |
| 7708649 | 8655 | 8660 | 8666 | 8672 | 8677 | 8683 | 8689 | 8694 | 8700 |
| 7718705 | 8711 | 8717 | 8722 | 8728 | 8734 | 8739 | 8745 | 8750 | 8756 |
| 772.8762 | 8767 | 8773 | 8779 | 8784 | 8790 | 8795 | 8801 | 8807 | 8812 |
| 7738818 | 8824 | 8829 | 8835 | 8840 | 8846 | 8852 | 8857 | 8863 | 8868 |
| 7748874 | 8880 | 8885 | 8891 | 8897 | 8902 | 8908 | 8913. | 8919 | 8925 |
| 7758930 | 8936 | 8941 | 8947 | 8953 | 8958. | 8964 | 8969 | 8975 | 8981 |
| 7768986 | 8992 | 8997 | 9003 | 9009 | 9014 | 9020 | 9025 | 9031 | 9037 |
| 7779042 | 9048 | 9053 | 9059 | 9064 | 9070 | 9076 | 081 | 087 | 092 |
| 7789098 | 9104 | 9109 | 9115 | 9120 | 9126 | 9131 | 137 | 143 | 148 |
| 7799154 | 9159 | 9165 | 9170 | 9176 | 9182 | 9187 | 193 | 198 | 仡 |
| 780 | 9215 | 9221 | 9226 | 9232 | 9237 | 9243 | 248 | 254 |  |
| 7819265 | 9271 | 9276 | 9282 | 9287 | 9293 | 9298 | 304 | 310 | 315 |
| 7829321 | 9326. | 9332 | 9337 | 9343 | 9348 | 9354 | 360 | 365 | 3 |
| 7839376 | 9382. | 9387 | 9393 | 9398 | 9404 | 9409 | 415 | 421 | 42 |
| 7849432 | 9437 | 9443 | 9448 | 9454 | 9459 | 9465 | 470 | 476 | 88 |
| 785, 9487 | 9492 | 9498 | 9504 | 9509 | 9515 | 9520 | 526 | 531 | 537 |
| 786.9542 | 9548 | 9553 | 9559 | 9564 | 9570 | 9575 | 581 | 586 | 592 |
| 7879597 | 9603 | 9609 | 9614 | 9620 | 9625 | 9631 | 636 | 642 | 6 |
| 788.9653 | 9658 | 9664 | 9669 | 9675 | 9680 | 9686 | 691 | 697 | 70 |
| 789 9708 | 9713 | 9719 | 9794 | 9730 | 9735 | 9741 | 746 | 752 |  |
| 7909763 | 9768 | 9774 | 9779 | 9785 | 9790 | 9796 | 801 | 807 |  |
| 7919818 | 9823 | 9829 | 9834 | 9840 | 9845 | 9851 | 856 | 862 |  |
| 792. 9873 | 9878 | 9883 | 9889 | 9894 | 9900 | 9905 | 911 | 916 |  |
| 7939927 | 9933 | 9938 | 9944 | 9949 | 9955 | 9960 | 966 | 971. | 977 |
| 7949982 | 9988 | 9993 | 9998 | 90004 | 9000 | 000159 | 00020 | 0026 | 003 |
| 79590037 | 90042 | 90048 | 90053 | 0059 | 0064 | 0069 | 0075 | 0080 | 0086 |
| 7960091 | 0097 | 0102 | 0108 | 0113 | 0119 | 0124 | 0129 | 0135 | 0140 |
| 7970146 | 0151 | 0157 | 0162 | 0168 | 0173 | 0179 | 0184 | 0189 | 0195 |
| 77980200 | 0206 | 0211 | 0217 | 0222 | 0227 | 0233 | 0238 | 0244 | 0249 |
| 7990255 | 0260 | 0266 | 0271 | 0276 | 0282 | 0287 | 0293 | 0298 | 0304 |
| $\overline{800} 0309$ | 0314 | 0320 | 0325 | 0391 | 0336 | 0342 | 0347 | 0352 | 0358 |
| 8010363 | 0369 | 0374 | 0380 | 0385 | 0390 | 0396 | 0401 | 0407 | 0412 |
| [802 0417 | 0423. | 0428 | 0434 | 0439 | 0445 | 0450 | 0455 | 0461 | 0466 |
| 8030472 | 0477 | 0482 | 0488 | 0493 | 0499 | 0504 | 0509 | 0515 | 0520 |
| 8040526 | 0531 | 0536 | 0542 | 0547 | 0553 | 0558 | 0563 | 0569 | 0574 |
| 8050580 | 0585 | 0590 | 0596 | 0601 | 0607 | 0612 | 0617 | 0623 | 0628 |
| 806 807 80634 | 0639 0693 | 0644 | 0650 0703 | 0655 0709 | 0660 | 0666 | 0671 | 0677 | 0682 |
| $[80780687$ | 0693 0747 | 0698 | 0703 | 0709 | 0714 | 0720 | 0725 | 6730 | 0736 |
| -809 0795 | 0800 | 0806 | 0811 | 0816 | 0822 | 0827 | 0832 | 0838 | 0843 |
| 810 0849 | 0854 | 0859 | 0865 | 0870 | 0875 | 0881 | 0886 | 0891 | 0897 |
| 8110902 | 0907 | 0913. | 0918 | 0924 | 0929 | 0934 | 0940 | 0945 | 0950 |
| 812. 0956 | 0961 | 0966 | 0972 | 0977 | 0982 | 0988 | 0993 | 0998 | 1004 |
| 8131009 | 1014 | 1020. | 1025 | 1030 | 1036 | 1041 | 1046 | 1052 | 1057 |
| 814.1062 | 1068 | 1073 | 1078 | 1084 | 1089 | 1094 | 1100 | 1105 | 1110 |
| 8151116 | 1121 | 1126 | 1132 | 1137 | 1142 | 1148 | 1153 | 1158 | 116 |
| 8161169 | , 1174 | 1180 | 1185 | 1190 | 1196 | 1201 | 1206 | 1212 | 1217 |
| 817.1222 | 1228 | 1233 | 1238 | 1243. | 1249 | 1254 | 1259 | 1265 | 1270 |
| 8181275 | 1281 | 1286 | 1291 | 1297 | 1302 | 1307 | 1312 | 1318 | 1323 |
| 8191328 | 1334 | 1339 | 1344 | 1350 | 1355 | 1360 | 1365 | 1371 | 1376 |
| No. 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |


| No．8200－8800． |  |  |  |  |  |  | og |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 13 | 913 |  |  |  |  | 9142 |  |
|  | 143 | 141 | 144 | 145 | 145 |  |  |  |  |  |
|  | 1487 | 1492 | 149 | 150 | 1508 | 151 | 151 | 1524 |  |  |
|  |  |  | 155 |  | 156 | 156 |  | 157 |  |  |
|  | 1593 | 1598 | 1603 | 160 | 161 | 161 |  |  |  |  |
|  | 16 |  |  | 16 | 166 | 167 | 167 | 16 | 168 |  |
|  | 1691 | 1703 | 170 |  | 171 |  |  |  |  |  |
| 827 | 1751 | 1756 | 1761 | 176 | 1772 | 1777 | 178 | 178 | 179 |  |
|  | 18 | 1808 | 1814 | 181 | 182 | 1829 | 183 | 184 | 1845 |  |
|  | 1855 | 1861 | 1866 | 1871 | 1876 |  | 188 | 189 | 189 |  |
| 830 | 1908 | 191 | 1918 | 192 | 192 | 193 | 193 | 194 | 1950 |  |
|  |  | 1965 | 197 | 197 | 198 | 198 | 199 | 199 | 200 |  |
|  | 2012 | 210 | 27 |  |  |  | 204 | 204 | 205 |  |
|  | 2065 | 2070 | 2975 | 208 | 208 | 209 | 209 | 210 | 210 |  |
|  | 2117 | 2122 | 212 | 131 | 213 | 214 | 214 | 215 | 215 |  |
|  | 216 | 2174 | 2179 | 218 | 28 | 219 | 220 | 220 | 221 |  |
| 33 | 2221 | 2226 | 2231 | 223 | 2241 | 224 | 225 | 225 | 226 |  |
|  | 2273 | 2278 | 2283 | 228 | 2293 | 229 | 230 | 230 | 231 |  |
|  | 232 |  | 2335 | 2 | 234 | 235 | 235 | 236 |  |  |
| 83 | 2376 | 2381 | 2387 | 2392 | 239 | 2402 | 240 | 241 | 241 |  |
|  | 242 | 243 |  |  | 24 |  |  |  |  |  |
|  |  | 248 | 249 | 24 | 250 | 250 | 5 | － | 25 |  |
|  | 2531 | 2536 | 2542 | 254 | 255 | 255 | 256 | 256 | 25 |  |
|  | 2583 | 25 | 2593 | 2598 | 260 | 260 | 261 | 261 | 26 |  |
|  | 263 | 2639 | 2645 | 265 | 265 | 260 | 66 | 26 | 72 |  |
|  | 268 | 2891 | 2696 | 270 | 270 | 271 | 271 | 272 | 272 |  |
|  | 273 | 2742 | 2747 | 275 | 275 | 276 | 276 | 277 | 27 |  |
|  | 278 | 2793 | 2799 | 280 | 28 | 281 | 81 | 282 | 2829 |  |
|  | 2840 | 2845 | 2850 | 2355 | 286 | 286 | 287 | 287 | 288 |  |
| 849 | 2891 | 2896 | 2901 | 2906 | 291 | 291 | 292 | 292 |  |  |
| 850 | 2942 | 2947 | 295 | 295 | 296 | 296 | 2973 | 29 |  |  |
|  | 2993 | 299 | 300 | 300 | 301 | 301 | 302 | 302 | 303 |  |
|  | 204 | 3049 | 305 | 305 | 306 | 306 | 307 | 308 |  |  |
| 853 | 3095 | 00 | 3105 | 3110 | 31 | 312 | 312 | 31 | 313 |  |
| 854 | 3146 | 3151 | 315 | 3161 | 316 | 317 | 3176 | 318 | 3186 |  |
|  | 319 |  |  | 321 | 321 | 322 | 322 | 323 |  |  |
|  | ， | 3252 |  | 326 |  | 327 | 327 | 328 |  |  |
| 85 | 3298 | 330 | 330 | 331 | 331 | 332 | 3328 | 383 | 333 |  |
| 85 | 3349 | 3354 |  | 336 |  | 337 | 337 | 33 |  |  |
| 859 |  |  |  | 341 | 位 | 342 |  |  |  |  |
|  | 345 | 3455 |  | 346 | 34 | 34 | 483 |  |  |  |
|  |  |  | 3510 | 3515 |  |  |  |  |  |  |
| 86 | 3551 | 3556 | 3561 | 356 | 357 | 357 | 358 | 358 | 509 |  |
|  | 3601 | 3606 | 3611 | 361 | 362 | 36 | 363 | 36 | 364 |  |
| 86 | 3651 |  | S | 366 | 367 | 367 |  | 368 | 369 |  |
| 86 | 3702 | 3707 | 371 | 3717 | 372 | 372 | 373 | 379 |  |  |
|  | 3752 | 3757 | 376 | 3767 | 377 | 377 | 378 | 378 | 379 |  |
| 86 | 3802 | 3807 | 381 | 3817 |  | 38 | 383 | 383 | 促 |  |
| 868 | 3852 | 3857 | 3862 | 3867 | 387 | 387 | 388 | 388 | 389 |  |
| 869 | 3902 | 3907 | 3912 | 3917 | 392 | 392 | 393 | 893 | 89 |  |
| 870 | 395 | 957 | 3962 | 3967 |  | 析 | 988 |  | ， |  |
| 871 | 4002 | 4007 | 4012 | 401 | 402 | 402 | 403 | 408 | 4042 |  |
| 872 | 405 | 4057 | 4062 | 406 | 40 | 407 | 408 | 408 | 4091 |  |
| 873 | 4101 | 4106 | 4111 | 4116 | 412 | 412 | 413 | 413 | 414 |  |
| 874 | 4151 | 4156 | 4161 | 416 | 417 | 417 | 418 | 418 | 419 |  |
| 875 | 4201 | 4206 | 4211 | 421 | 422 | 422 | 423 | 42 | 4240 |  |
| （876 | 4250 | 4255 | 426 | 226 | 427 |  | 28 | 28 | 4290 |  |
| 877 | 4300 | 4305 | 4310 | 4315 | 432 | 432 | 433 | 433 | 4340 |  |
| 878 | 4349 | 4354 | 4359 | 436 | 43 | 437 | 437 | 438 | 438 |  |
| 879 | 439 | 440 | 4409 | 44 | 4419 | 442 | 442 | 44 | 443 | 444 |
|  | 0 |  |  |  |  | 5 |  |  | 8 |  |

A TABLE OF LOGARITHMS.


## A TABLE OF LOGARITHAS.

| N0.9400-10000. |  |  |  |  |  |  | Log. $97313-99996$. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | 0 | I | 9 | 3 | 4 | 5 |  |  | - | - |
| $\overline{940} 9$ |  |  |  |  |  |  |  |  |  |  |
| 941 | 735 | 7364 | 7368 | 7373 | 7377 | 7382 | 7387 | 7391 | 7396 | 7400 |
| 942 | 7405 | 7410 | 7414 | 7419 | 7424 | 7428 | 7433 | 7437 | 7442 | 7447 |
| 943 | 7451 | 7456 | 7460 | 7465 | 7470 | 7474 | 7479 | 7483 | 7488 | 7493 |
| 944 | 7497 | 7502 | 7506 | 7511 | 7516 | 7520 | 7525 | 7529 | 7534 | 7539 |
| 945 | 7543 | 7548 | 7552 | 7557 | 7562 | 7566 | 7571 | 7575 | 7580 | 7585 |
| 946 | 7589 | 7594 | 7598 | 7603 | 7607 | 7612 | 7617 | 7621 | 7626 | 7630 |
| 947 | 7635 | 7640 | 7644 | 7649 | 7653 | 7658 | 7663 | 7667 | 7672 | 7676 |
| 948 | 7681 | 7685 | 7690 | 7695 | 7699 | 7704 | 7708 | 7713 | 7717 | 7722 |
| 949 | 7727 | 7731 | 7736 | 7740 | 7745 | 7749 | 7754 | 7759 | 7763 | 7768 |
| 950 | 7772 | 7777 | 7782 | 7786 | 7791 | 7795 | 7800 | 7804 | 7809 | 7813 |
| 951 | 7818 | 7823 | 7827 | 7832 | 7836 | 7841 | 7845 | 7850 | 7855 | 7859 |
| 952 | 7864 | 7868 | 7873 | 7877 | 7882 | 7886 | 7891 | 7896 | 7900 | 7905 |
| 953 | 7909 | 7914 | 7918 | 7923 | 7928 | 7932 | 7937 | 7941 | 7946 | 7950 |
| 954 | 7955 | 7950 | 7964 | 7968 | 7973 | 7978 | 7982 | 7987 | 7991 | 7996 |
| 955 | 8000 | 8 CO 5 | 8009 | 8014 | 8019 | 8023 | 8028 | 8032 | 8037 | 8041 |
| 956 | 8046 | 8050 | 8055 | 8059 | 8064 | 8068 | 8073 | 8078 | 8082. | 8087 |
| 957 | 8091 | 8096 | 8100 | 8105 | 8109 | 8114 | 8118 | 8123 | 8127 | 8132 |
|  | 8137 | 8141 | 8146 | 8150 | 8155 | 8159 | 8164 | 8168 | 8173 | 8177 |
| 959 | 8182 | 8186 | 8191 | 8195 | 8200 | 8204 | 8209 | 8214 | 821 |  |
| 960 | 8227 | 8232 | 8236 | 8241 | 8245 | 825 | 8254 | 8259 | 82 | 8268 |
| 961 | 8272 | 8277 | 8281 | 8286 | 8290 | 8295 | 8299 | 8304 | 830 |  |
| 962 | 8318 | 8322 | 8327 | 8331 | 8336 | 8340 | 8345 | 8349 | 8354 | 83 |
| 963 | 8363 | 8367 | 8372 | 8376 | 8381 | 8385 | 8390 | 8394 | 8399 | 84 |
| 964 | 8408 | 8412 | 8417 | 8421 | 8426 | 8430 | 8435 | 8439 | 8444 | 84 |
| 965 | 8453 | 8457 | 8462 | 8466 | 8471 | 8475 | 8480 | 8484 | 8489 | 84 |
| 966 | 8498 | 8502 | 8507 | 8511 | 8516 | 8520 | 8525 | 8529 | 8534 | 85 |
| 967 | 8543 | 8547 | 8552 | 8556 | 8561 | 8565 | 8570 | 8574 | 8579 | 85 |
| 968 | 8588 | 8592 | 8597 | 8601 | 8605 | 8610 | 8614 | 8619 | 8623 | 8628 |
| 969 | 8632 | 3637 | 8641 | 8646 | 8650 | 8655 | 8659 | 8664 | 8668 | 8673 |
| 970 | 8677 | 8682 | 8686 | 8691 | 8695 | 8700 | 8704 | 8709 | 8713 | 8717 |
| 971 | 8722 | 8726 | 8731 | 8735 | 8740 | 8744 | 8749 | 8753 | 8753. | 8762 |
| 972 | 8767 | 8771 | 8776 | 8780 | 8784 | 8789 | 8793 | 8798 | 8802 | 88 |
| 973 | 8811 | 8816 | 8820 | 8825 | 8829 | 8834 | 8838 | 8843 | 8847 |  |
| 974 | 8856 | 8860 | 8865 | 8869 | 8874 | 8878 | 8883 | 8887 | 8892 | 8896 |
| 975 | 8900 | 8905 | 8909 | 8914 | 8918 | 8923 | 8927 | 8932 | 8936 |  |
| 976 | 8945 | 8949 | 8954 | 8958 | 8963 | 8967 | 8972 | 8976 | 8981 |  |
| 977 | 8989 | 8994 | 8998 | 9003 | 9007 | 9012 | 9016 | 9021 | 9025 | 9029 |
| 978 | 9034 | 9038 | 9043 | 047 | 052 | 056 | 061 | 065 | 069. | 074 |
| 979 | 9078 | 9083 | 9087 | 032 | 096 | 100 | 105 | 109 | 114 | 18 |
| 980 | 9123 | 9127 | 9131 | 136 | 140 | 145 | 149 | 154 | 158 | 162 |
| 981 | 9167 | 9171 | 9176 | 180 | 185 | 189 | 193 | 198 | 202 | 207 |
| 982 | 9211 | $9216^{\circ}$ | 9220 | 224 | 229 | 233 | 238 | 242 | 247 | 251 |
| 1983 | 9255 | 9260 | 9264 | 269 | 273 | 277 | 282 | 286 | 291 | 295 |
| 984 | 9300 | 9304 | 9308 | 313 | 317 | 322 | 326 | 330 | 335 | 339 |
| 985 | 9344 | 9348 | 9352 | 357 | 361 | 366 | 370 | 374 | 379 | 383 |
| 986 | 9388 | 9392 | 9396 | 401 | 405 | 410 | 414 | 419 | 423. | 427 |
| 987 | 9432 | 9436 | 9441 | 445 | 449 | 454 | 458 | 463 | 467 | 471 |
| 988 | 9476 | 9480 | 9484 | 499 | 493 | 498 | 502 | 506 | 511 | 515 |
| 989 | 9520 | 9524 | 9528 | 533 | 537 | 542 | 546 | 550 | 555 | 559 |
| $\stackrel{990}{ }$ | 9564 | 9568 | 9572 | 577 | 581 | 585 | 590 | 59 | 599 | 603 |
| 991 | 9607 | 9612 | 9616 | 621 | 625 | 629 | 634 | 638 | 642 | 647 |
| 992 | 9651 | 9656: | 9660 | 664 | ${ }^{669}$ | 673 | 677 | 682 | 686 | 691 |
| 993 | 9695 | 9699 | 9704 | 708 | 712 | 717 | 721 | 72 | 730 | 734 |
| 994 | 9739 | 9743 | 9747 | 752 | 756 | 760 | 765 | 760 | 774 | 778 |
| 1995 | 9782 | 9787 | ${ }^{9791}$ | 795 | 800 | 804 | 808 | 813 | 817 | 822 |
| 996 | 9826 | 9830 | 9835 | 839 | 843 | 848 | 852 | 856 | 861 | 865 |
| ${ }_{998}^{997}$ | ${ }_{9}^{9870}$ | 9874 | 9878 | 883 | 887 | 891 | 896 | 900 | 904 | 909 |
| 998 | ${ }_{9}^{9913}$ | 9917 | ${ }^{9922}$ | 926 | 930 | 935 | 939 | 94 | 948 | 952 |
| 999 | 9957 | 996 | 9965 | 970 | 974 | 978 | 983 | 987 | 991 | 996 |
| No. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |



## 22 Artificial Sines, Tangents, and Secants.

| 3 Degrees. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | C. Sine | Tang. C.Tang. Secant C. Sec. 11 |  |  |  |  |
| 0 | 8.71880 | 9.99940 | 8.71940 | 11.28060 | 10.00060 | 11.28120 | 60 |
| 5 | 73069 | 37 | 73132 | 26868 | 63 | 26931 | 55 |
| 10 | 74226 | 34 | 74292 | 25708 | 66 | 25774 | 50 |
| 15 | 75353 | 30 | 75423 | 24577 | 70 | 24647 | 45 |
| 20 | 76451 | 26 | 76525 | 23475 | 74 | 23549 | 40 |
| 25 | 77522 | 23 | 77600 | 22400 | 77 | 22478 | 35 |
| 30 | 78567 | 19 | 78649 | 21351 | 81 | 21433 | 30 |
| 35 | 8.79588 | 9.99915 | 8.79673 | 1.20327 | 10.00085 | 1.20412 | 25 |
| 40 | 80585 | 11 | 80674 | 19326 | 89 | 19415 | 20 |
| 45 | 81560 | 07 | 81653 | 18347 | 93 | 18440 | 15 |
| 50 | 82513 | 03 | 82610 | 17390 | 97 | 17487 | 10 |
| 55 | 83446 | 99898 | 83547 | 16453 | 102 | 16554 | 5 |
| 60 | 84358 | 894 | 84464 | 15536 | 106 | 15642 | 0 |
| $M$ C. Sine. Sine C.Tang. Tang. C. Sec. Secant IM <br> 86 Degrees. <br> 4 Degrees. |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  | Sine | C. Sine | Tang. | C.Tang. | Secant | C. Sec. | II |
| 0 | 8.84358 | 9.99894 | 8.84464 | 11.15536 | 10.00106 | 11.15642 | 60 |
| 5 | 85252 | 890 | 85363 | 14637 | 110 | 14748 | 55 |
| 10 | 86128 | 885 | 86243 | 13757 | 115 | 13872 | 50 |
| 15 | 86987 | 880 | 87106 | 12894 | 120 | 13013 | 45 |
| 20 | 87829 | 876 | 87953 | 12047 | 124 | 12171 | 40 |
| 25 | 88654 | ع71 | 88783 | 11217 | 129 | 11846 | 35 |
| 30 | 89464 | 866 | 85598 | 10402 | 134 | 10536 | 30 |
| 35 | 8.90260 | 9.99861 | 8.90399 | 11.09601 | 10.00139 | 11.09740 | 25 |
| 40 | 91040 | 856 | 91185 | 08815 | 144 | 08960 | 20 |
| 45 | 91807 | 851 | 91957 | 08043 | 149 | 08193 | 15 |
| 50 | 92561 | 845 | 92716 | 07284 | 155 | 07439 | 10 |
| 55 | 93302 | 840 | 93462 | 06538 | 160 | 06698 | 5 |
| 60 | 94030 | 834 | 94195 | 05805 | 166 | 05970 | 0 |
| $\overline{\mathrm{M}}$ C. Sine Sine C.Tang. Tang. C. Sec. Secant M |  |  |  |  |  |  |  |
| 85 Degrees |  |  |  |  |  |  |  |
| Degrees. |  |  |  |  |  |  |  |
| $M$ Sine C. Sine Ting. C.Tang. Secant C. Sec. M1 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| $\begin{array}{lllllllllllllllllll}10 & 95450 & 823 & 95627 & 04373 & 177 & 04550 & 50\end{array}$ |  |  |  |  |  |  |  |
| J5 | 96143 | 817 | 96325 | 03675 | 183 | 03857 | 45 |
|  |  |  |  |  |  |  |  |
| $\begin{array}{lllllllllll}25 & 97496 & 806 & 97691 & 02309 & 194 & 02504 & 35\end{array}$ |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| $\overline{35} 8.98808 \overline{9.99794} \overline{8.99015} \overline{11.00985} \overline{10.00206} \overline{11.01192}$-25 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| 45 | 9.00082 | 781 | 9.00301 | 10.99699 | 2191 | 10.99918 | 15 |
| $\begin{array}{lllllllllll}50 & 00704 & 775 & 00930 & 99070 & 225 & 99296 & 10\end{array}$ |  |  |  |  |  |  |  |
| 55 01318 768 01550 98450 232 98682 5 <br> 60 01923 761 02162 97838 239 98077 0 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| $\bar{M}$ C. Sine Sine C.Tang. Tang. $\bar{C}$. Sec. $\overline{\text { Secant }} \overline{\mathrm{Ml}}$ |  |  |  |  |  |  |  |
|  |  |  | 84 Deg | grees. |  |  |  |



24 Artificial Sines, Tangen ts, and Secants.

| 9 Degrees. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Sine | C. Sine | Tang. | C.Tang. | Secant | C. Sec. 1 M |  |
| 0 | 9.19433 | 9.99462 | 9.19971 | 10.80029 | 10.00538 | 10.80567 | 60 |
| 5 | 19830 | 452 | 20378 | 79622 | 548 | 80170 | 55 |
| 10 | 20223 | 442 | 20782 | 79218 | 558 | 79777 | 50 |
| 15 | 20613 | 432 | 21182 | 78818 | 568 | 79387 | 45 |
| 20 | 20999 | 421 | 21578 | 78422 | 579 | 79001 | 40 |
| 25 | 21382 | 411 | 21971 | 78029 | 589 | 78618 | 35 |
| 30 | 21761 | 400 | 22361 | 77639 | 600 | 78239 | 30 |
| 35 | 9.22137 | 9.99390 | 9.22747 | $\overline{10.77253}$ | 10.00610 | $\overline{10.77863}$ | 25 |
| 40 | 22509 | 379 | 23130 | 76870 | 621 | 77491 | 20 |
| 45 | 22878 | 368 | 23510 | 76490 | 632 | 77122 | 15 |
| 50 | 23244 | 357 | 23887 | 76113 | 643 | 76756 | 10 |
| 55 | 23607 | 346 | 24261 | 75739 | 654 | 76393 | 5 |
| 60 | 23967 | 335 | 24632 | 75368 | 665 | 76033 | 0 |
| M | C. Sine | ine | C.Tang. | Tang. | Se | Secant | M |
|  |  |  | 80 De | grees. |  |  |  |
|  |  |  | 10 Deg | rees. |  |  |  |
| M | ne | C. Sine | Tang. | C.Tang. | cant | . sec. | I |
| 0 | 9.23967 | 9.99335 | 9.24632 | 0.75368 | 10.00665 | 10.76033 | 60 |
| 5 | 24324 | 324 | 25000 | 75000 | 676 | 75676 | 55 |
| 10 | 24677 | 313 | 25365 | 74635 | 687 | 75323 | 50 |
| 15 | 25028 | 301 | 25727 | 74273 | 699 | 74972 | 45 |
| 20 | 25376 | 290 | 26086 | 73914 | 710 | 74624 | 40 |
| 25 | 25721 | 278 | 26443 | 73557 | 722 | 74279 | 35 |
| 30 | 26063 | 267 | 26797 | 73203 | 733 | 73937 | 30 |
| 35 | $\overline{9.26403}$ | 9.99255 | 9.27148 | $\overline{10.72852}$ | 0.00745 | $\overline{10.73597}$ | 25 |
| 40 | 26739 | 243 | 27496 | 72504 | 757 | 73261 | 20 |
| 45 | 27073 | 231 | 27842 | 72158 | 769 | 72927 | 15 |
| 50 | 27405 | 219 | 28186 | 71814 | 781 | 72595 | 10 |
| 55 | 27734 | 207 | 28527 | 71473 | 793 | 72266 |  |
| 60 | 28060 | 195 | 28865 | 71135 | 805 | 71940 | 0 |
| M C. Sine Sine C.Tang. Tang. C. Sec. Secant M |  |  |  |  |  |  |  |
| 79 Degrees. |  |  |  |  |  |  |  |
| 11 Degrees. |  |  |  |  |  |  |  |
| M | S | ne | Tang. | C.Tang. | - | Sec. | M |
| 0 | 9.28060 | 9.99195 | 9.28865 | 10.71135 | 10.00805 | 10.71940 | 60 |
| 5 | 28384 | 182 | 29201 | 70799 | 818 | 71616 | 55 |
| 10 | 28705 | 170 | 29535 | 70465 | 830 | 71295 | 50 |
| 15 | 29024 | 157 | 29866 | 70134 | 843 | 70976 | 45 |
| 20 | 29340 | 145 | 30195 | 69805 | 855 | 70660 | 40 |
| 25 | 29654 | 132 | 30522 | 69478 | 868 | 70346 | 35 |
| 30 | 29966 | 119 | 30846 | 69154 | 881 | 70034 | 30 |
| 35 | 9.30275 | 9.99106 | 9.31168 | 10.68832 | 10.00894 | 10.69725 | 25 |
| 40 | 30582 | 093 | 31489 | 68511 | 907 | 69418 | 20 |
| 45 | 30887 | 080 | 31806 | 68194 | 920 | 69113 | 15 |
| 50 | 31189 | 067 | 32122 | 67878 | 933 | 68811 | 10 |
| 55 | 31490 | 054 | 32436 | 67564 | 946 | 68510 |  |
| 60 | 31788 | 040 | 32748 | 67252 | 960 | 68212 | 0 |
| $\overline{\text { M }}$ C. Sine |  | Sine | C.Tang. | Tang. | Sec. | Secan | M |
| 78 Degrees. |  |  |  |  |  |  |  |



| 15 Degrees. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M | Sine 1 C. Sine |  | Tang. C.Tang. Secant C. Sec. $\mathbf{N}$ |  |  |  |  |
| 0 | 9.41300 | 9.98494 | 9.42805 | 0.57195 | 10.01506 | 0.58700 | 60 |
| 5 | 41535 | 98477 | 43057 | 56943 | 01523 | 58465 | 55 |
| 10 | 41768 | 98460 | 43308 | 56692 | 01540 | 58232 | 5 |
| 15 | 42001 | 98443 | 43558 | 56442 | 01557 | 57999 | 5 |
| 20 | 42232 | 98426 | 43806 | 56194 | 01574 | 57768 | 0 |
| 25 | 42462 | 98409 | 44053 | 55947 | 01591 | 57538 | 35 |
| 30 | 42690 | 98391 | 44299 | 55701 | 01609 | 57310 | 30 |
| 35 | 9.42917 | 9.98374 | 9.4454 | 0.5545 | 0.0162 | 0.57083 | 5 |
| 40 | 43143 | 98356 | 44787 | 55213 | 01644 | 56857 | 20 |
| 45 | 43368 | 98338 | 45029 | 54971 | 01662 | 56632 | 5 |
| 50 | 43591 | 98320 | 45271 | 54729 | 01680 | 56409 | 0 |
| 55 | 43813 | 98302 | 45511 | 54489 | 01698 | 56187 |  |
| 60 | 44034 | 98284 | 45750 | 54250 | 01716 | 55966 |  |
| M C. Sine |  | ne | $\overline{\text { C.Tang. Tang. }} \overline{\text { C. Sec. Secant }}$ |  |  |  |  |
| 74 Degrees |  |  |  |  |  |  |  |
| 16 Degrees. |  |  |  |  |  |  |  |
| $\overline{\text { M }}$ | Sine | C. Sine | Tang. C.Tang. Secant C. Sec. 11 |  |  |  |  |
| 0 | 9.44034 | 9.98284 | 9.45750 | 10.54250 | $\overline{10.01716}$ | 10.55966 | 60 |
| 5 | 44253 | 98266 | 45987 | 54013 | 01734 | 55747 | 5 |
| 10 | 44472 | 98248 | 46224 | 53776 | 01752 | 55528 | 50 |
| 15 | 44689 | 98229 | 46460 | 53540 | 01771 | 55311 | 45 |
| 20 | 44905 | 98211 | 46694 | 53306 | 01789 | 55095 |  |
| 25 | 45120 | 98192 | 46928 | 53072 | 01808 | 54880 | 35 |
| 30 | 45334 | 98174 | 47160 | 52840 | 01828 | 54666 | 0 |
| 35 | 9.45547 | 9.98155 | 9.47392 | 1.52608 | 0.01845 | 0.5445 |  |
| 40 | 45758 | 98136 | 47622 | 52378 | 01864 | 54242 | 20 |
| 45 | 45969 | 98117 | 47852 | 52148 | 01883 | 54031 | 15 |
| 50 | 46178 | 98098 | 48080 | 51920 | 01902 | 53822 | 0 |
| 55 | 46386 | 98079 | 48307 | 51693 | 01921 | 53614 |  |
| 60 | 46594 | 98060 | 48534 | 51466 | 01940 | 53406 |  |
| M | C. Sine | e | C.Tang. | Tang. | C. Sec |  |  |
|  |  |  | 73 D | - |  |  |  |
|  |  |  | 17 D | rees. |  |  |  |
| M Sine C. Sine Tang. C.Tang. Secant C. Sec, M |  |  |  |  |  |  |  |
| 0 | 9.46594 | 9.98060 | $9 . 4 8 5 3 4 \longdiv { 1 0 . 5 1 4 6 6 1 0 . 0 1 9 4 0 } \overline { 1 0 . 5 3 4 0 6 } \overline { 6 0 }$ |  |  |  |  |
| 5 | 46800 | 98040 | 48759 | 51241. | 01960 | 53200 | 5. |
| 10 | 47005 | 98021 | 48984 | 51016 | 01979 | 52995 | 50 |
| 15 | 47209 | 98001 | 49207 | 50793 | 01999 | 52791 | 45 |
| 20 | 47412 | 97982 | 49430 | 50570 | 02018 | 52588 | 40 |
| 25 | 47613 | 97962 | 49652 | 50348 | 02038 | 52387 | 35 |
| 30 | 47814 | 97942 | 49872 | 50128 | 02058 | 52186 | 30 |
| 35 | 9.48014 | 9.97922 | 9.50092 | 0.49908 | $\overline{10.02078}$ | 0.51986 | 25 |
| 40 | 48213 | 97902 | 50311 | 49689 | 02098 | 51787 | 20 |
| 45 | 48411 | 97882 | 50529 | 49471 | 02118 | 51589 | 15 |
| 50 | 48608 | 97861 | 50746 | 49254 | 02189 | 51392 | 0 |
| 55 | 48803 | 97841 | 50962 | 49038 | 02159 | 51197 | 5 |
| 60 | 48998 | 97821 | 51178 | 48822 | 02179 | 51002 | $\theta$ |
| M C. Sine Sine C.Tang. Tang. C. Sec. Secant M1 |  |  |  |  |  |  |  |
| 72 Degrees. |  |  |  |  |  |  |  |


| M Sine |  | $\frac{\text { C. Sine }}{9.97821}$ |  | C.Tang. Secant |  | C. Sec. M |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 9.48998 |  | 9.5117810 | 0.4882210 | 0.02179 | $0.51002$ |  |
| 5 | 49192 | 97800 | 51392 | 48608 | 02200 | 50808 | 55 |
| 10 | 49885 | 97779 | 51606 | 48394 | 02221 | 50615 | 50 |
| $\begin{aligned} & 10 \\ & 15 \end{aligned}$ | 49577 | 97759 | 51819 | 48181 | 02241 | 50423 | 5 |
| 20 | 49768 | 97738 | 52031 | 47969 | 02262 | 50232 |  |
| 25 | 49958 | 97717 | 52242 | 47758 | 02283 | 50042 |  |
| 30 | 50148 | 97696 | 52452 | 47548 | 02304 | 49852 |  |
| 35 | 9.50336 | 9.97674 | 9.52661 | 10.4733910 | 10.02326 | 10.49664 |  |
| 40 | 50523 | 97653 | 52870 | 47130 | 02347 | 49477 |  |
| $45$ | 50710 | 97632 | 53078 | 46922 | 02368 | 49290 | 15 |
| 50 | 50896 | 97610 | 53285 | 46715 | 02390 | 49104 | 0 |
| 55 | 51080 | 97589 | 53492 | 46508 | 02411 | 48920 |  |
| 60 | 51264 | 97567 | 53697 | 46303 | 02433 | 48736 |  |
|  | C. Sine | Sine | C.Tang. | Tang. | C. Sec. | ecant |  |
|  |  |  | 71 Deg | rees. |  |  |  |
|  |  |  | 19 Deg | grees. |  |  |  |
| M | Sine | C. Sine | Tang. C | C.Tang. | Secant | S | M |
| $\bigcirc$ | 9.51264 | 9.97567 | 9.536971 | 10.463031 | 10.02433 | 10.4873 | 0 |
|  | 51447 | 97545 | 53902 | 46098 | 02455 | 48553 | 55 |
| $\begin{array}{r} 5 \\ 10 \end{array}$ | 51629 | 97523 | 54106 | 45894 | 02477 | 48371 | 0 |
| 1520 | 51811 | 97501 | 54309 | 45691 | 02499 | 48189 | 45 |
|  | 51991 | 97479 | 54512 | 45488 | 02521 | 48009 | 0 |
| $\begin{aligned} & 20 \\ & 25 \end{aligned}$ | 52171 | 97457 | 54714 | 45286 | 02543 | 47829 | 35 |
| $\begin{aligned} & 25 \\ & 30 \\ & \hline \end{aligned}$ | 52350 | 97435 | 54915 | 45085 | 02565 | 47650 | 30 |
|  | 9.52527 | 9.97412 | 9.551151 | 10.44885 | $\underline{10.02588}$ | 10.4747 | 5 |
| $\begin{aligned} & 35 \\ & 40 \end{aligned}$ | 52705 | 97390 | 55315 | 44685 | 02610 | 4729 |  |
| 45 | 52881 | 97367 | 55514 | 44486 | 02633 | 47119 | 15 |
|  | 53056 | 97344 | 55712 | 44288 | 02656 | 46944 | 0 |
| $\begin{aligned} & 50 \\ & 55 \end{aligned}$ | 53231 53405 | 97322 | 55910 | 44090 | 02678 | 4676 |  |
| $\overline{\mathrm{M}} \overline{\mathrm{C} . \text { Sint }}$ |  | Sine | C.Tang. | Tang. | C. Sec. | Secant |  |
| 70 Degrees. |  |  |  |  |  |  |  |
|  |  | 20 Degrees. |  |  |  |  |  |
|  |  | C. Sine | Tang. | C.Tang. | Secant | C. Sec | I |
| - 9.53405 |  | 9.97299 | $9 . 5 6 1 0 7 \longdiv { 1 0 . 4 3 8 9 3 } \overline { 1 0 . 0 2 7 0 1 } \overline { 1 0 . 4 6 5 9 5 }$ |  |  |  |  |
| $5 \quad 53578$ |  | 97275 | 56303 | 43697 | 02725 | 46422 |  |
| $10 \quad 53751$ |  | 97252 | 56498 | 43502 | 02748 | 46249 | 50 |
| 1553922 |  | 97229 | 56693 | 43307 | 02771 | 46078 |  |
| 20.54093 |  | 97206 | 56887 | 43113 | 02794 | 45907 |  |
| $25 \quad 54263$ |  | 97182 | 57081 | 42919 | 02818 | 45737 |  |
| 30 | 54433 | 97158 | 57274 | 42726 | 02841 | 45567 |  |
| 359.5460 |  | 9.97135 | 9.57466 | 10.42534 | 10.02865 | $\overline{10.45399}$ | 25 |
| $\begin{aligned} & 30 \\ & 40 \\ & 45 \\ & 50 \\ & 56 \\ & 60 \end{aligned}$ | 54769 | 97111 | 57658 | 42342 | 02889 | 45231 |  |
|  | 54936 | 97087 | 57849 | 42151 | 02913 | 45064 |  |
|  | 55102 | 97063 | 58039 | 41961 | 02937 | 44898 |  |
|  | 55268 | 97039 | 58229 | 41771 | 02961 | 44732 |  |
|  | 55433 | 97015 | 58418 | 41582 | 02985 | 44567 |  |
|  | C. Sine | Sine | C.Tang. | Tang. | C. Sec. | Secant |  |
|  |  |  | 69 De | egrees. |  |  |  |

98 Artificial Sines, Tangents, and Secants.

| 21 Degrees. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Tang. |  | C.Tang. ${ }^{\text {Secant }}$ (C. Sec. ${ }^{\text {M }}$ |  |  |  |
| 0 | 9.55433 | 9.97015 | 9.58418 | 10.41582 | 10.02985 | $\overline{10.44567}$ | -60 |
| 5 | 55597 | 96991 | 58606 | 41394 | 03009 | 44403 | 55 |
| 10 | 55761 | 96966 | 58794 | 41206 | 03034 | 44239 | 50 |
| 15 | 55923 | 96942 | 58981 | 41019 | 03058 | 44077 | 45 |
| 20 | 56085 | 96917 | 59168 | 40832 | 03083 | 43915 | 40 |
| 25 | 56247 | 96893 | 59354 | 40646 | 03107 | 43753 | 35 |
| 30 | 56408 | 96868 | 59540 | 40460 | 03132 | 43592 | 30 |
| 35 | 9.56568 | 9.96843 | 9.59725 | 10.40275 | 10.03157 | 10.43432 | 25 |
| 40 | 56727 | $96818{ }^{\text {i }}$ | 59909 | 40091 | 03182 | 43273 | 20 |
| 45 | 56886 | 96793 | 60093 | 39907 | 03207 | 43114 | 15 |
| 50 | 57044 | 95767 | 60276 | 39724 | 03233 | 42956 | 10 |
| 55 | 57201 | 96742 | 60459 | 39541 | 03258 | 42799 |  |
| 60 | 57358 | 96717 | 60641 | 39359 | 03283 | 42642 | 0 |
| M\| C. Sine Sine C.Tang. Tang. C. Sec. ${ }^{\text {Secant }}$ / $M$ |  |  |  |  |  |  |  |
| 68 Degrees. |  |  |  |  |  |  |  |
| 22 Degrees. |  |  |  |  |  |  |  |
|  |  | C. Sine Tang. C.Tang. Secant C. Sec. M |  |  |  |  |  |
| 0 | 9.57358 | 9.96717 | 9.60641 | 10.39359 | 10.03283 | 10.42642 | 60 |
| 5 | 57514 | 36691 | 60823 | 39177 | 03309 | 42486 | 55 |
| 10 | 57669 | 96665 | 61004 | 38996 | 03335 | 42331 |  |
| 15 | 57824 | 96640 | 61184 | 38816 | 03360 | 42176 | 45 |
| 20 | 57978 | 96614 | 61364 | 38636 | 03386 | 42022 | 40 |
| 25 | 58131 | 96588 | 61544 | 38456 | 03412 | 41869 | 3 |
| 30 | 58284 | 96562 | 61722 | 38278 | 03438 | 41716 | 30 |
| 35 | 9.58436 | 9.96535 | 9.61901 | 10.38099 | 0.03465 | 10.41564 | 25 |
| 40 | 58588 | 96509 | 62079 | 37921 | 03491 | 41412 | 20 |
| 45 | 58739 | 96483 | 62256 | 37744 | 03517 | 41261 | 15 |
| 50 | 58889 | 96456 | 62433 | 37567 | 03544 | 41111 | 10 |
| 55 | 59039 | 96429 | 62609 | 37391 | 03571 | 40961 |  |
| 60 | 59188 | 96403 | 62785 | 37215 | 03597 | 40812 |  |
| M | S | Sine | Tang. | Tang. | Sec |  | 1 |
| 67 Degrees. |  |  |  |  |  |  |  |
| 23 Degrees. |  |  |  |  |  |  |  |
| M | Si |  | Tang. C.Tang. Secant C. Sec. M |  |  |  |  |
| 0 | 9.59188 | $\overline{9.96403}$ | 9.62785 | 10.37215 | 10.03597 | 10.40812 | 60 |
| 5 | 59336 | 96376 |  | 37039 | 03624 | 40664 | 5 |
| 10 | 59484 | 96349 | 63135 | 36865 | 03651 | 40516 | 50 |
| 15 | 59632 | 96322 | 63310 | 36690 | 03678 | 4036 | 40 |
| 20 | 59778 | 96294 | 63484 | 36516 | 03706 | 40222 | 40 |
| 25 | 59924 | 96267 | 63657 | 36343 | 03733 | 40076 | 35 |
| 30 | 60070 | 96240 | 63830 | 36170 | 03760 | 39930 | 30 |
| 35 | 9.60215 | 9.96212 | 9.64003 | $\overline{10.35997}$ | 10.03788 | 10.39785 | 25 |
| 40 | 60359 | 96185 | 64175 | 35825 | 03815 | 3964 | 20 |
| 45 | 60503 | 96157 | 64346 | 35654 | 03843 | 39497 | 15 |
| 50 | 60646 | 96129 | 64517 | 35483 | 03871 | 39354 | 10 |
| 55 | 60789 | 96101 | 64688 | 35312 | 03899 | 39211 | 5 |
| 60 | 60931 | 96073 | 64858 | 35142 | 03927 | 39069 | 9 |
| $\bar{M} \bar{C}$ |  | Sine | C.Tang. Tang. C. Sec. |  |  |  | M |
|  |  |  | 66 Deg | grees. |  |  |  |

Avtificial Sines, Tangents, and Secants. 29


## 30 Artificial Sines, Tangents, and Secants,



Artificial Sines, Tangents, and Secants. 31


32 Artificial Sines, Tangents, and Secants.

| 33 Degrees. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M | Sine | C. Sine | Tang. | C.Tang. | Secant | C. Sec. 1 M |  |
| 0 | $\overline{9.73611}$ | 9.92359 | 9.81252 | 10.18748 | $\overline{10.07641}$ | 10.26389 | 60 |
| 5 | 73708 | 92318 | 81390 | 18610 | 07682 | 26292 | 55 |
| 10 | 73805 | 92277 | 81528 | 18472 | 07723 | 26195 | 50 |
| 15 | 73901 | 92235 | 81666 | 18334 | 07765 | 26099 | 45 |
| 20 | 73997 | 92194 | 81803 | 18197 | 07806 | 26003 | 40 |
| 25 | 74093 | 92152 | 81941 | 18059 | 07848 | 25907 | 35 |
| 30 | 74189 | 92111 | 82078 | 17922 | 07889 | 25811 | 30 |
| 35 | 9.74284 | $\overline{9.92069}$ | 9.82215 | $\underline{10.17785}$ | 10.07931 | $\overline{10.25716}$ | 25 |
| 40 | 74379 | 92027 | 82352 | 17648 | 07973 | 25621 | 20 |
| 45 | 74474 | 91985 | 82489 | 17511 | 08015 | 25526 | 15 |
| 50 | 74568 | 91942 | 82626 | 17374 | 08058 | 25432 | 10 |
| 55 | 74662 | 91900 | 82762 | 17238 | 08100 | 25338 | 5 |
| 60 | 74756 | 91857 | 82899 | 17101 | 08143 | 25244 | 0 |
| M | C. Sin | Sine | Tang. | Tang | C. Sec. |  | M |
| 56 Degrees. |  |  |  |  |  |  |  |
| 34 Degrees. |  |  |  |  |  |  |  |
| M |  |  | Tang. | C.Tang | Secant | Se | M |
| 0 | 9.74756 | .91857 | 9.82899 | 0.17101 | 10.08143 | 10.25244 | 60 |
| 5 | 74850 | 91815 | 83035 | 16965 | 08185 | 25150 | 55 |
| 10 | 74943 | 91772 | 83171 | 16829 | 08228 | 25057 | 50 |
| 15 | 75036 | 91729 | 83307 | 16693 | 08271 | 24964 | 45 |
| 20 | 75128 | 91686 | 83442 | 16558 | 08314 | 24872 | 40 |
| 25 | 75221 | 91643 | 83578 | 16422 | 08357 | 24779 | 35 |
| 30 | 75313 | 91599 | 83713 | 16287 | 08401 | 24687 | 30 |
| 35 | 9.75405 | 9.91556 | 9.83849 | 10.16151 | 10.08444 | 10.24595 | 25 |
| 40 | 75496 | 91512 | 83984 | 16016 | 08488 | 24504 | 20 |
| 45 | 75587 | 91469 | 84119 | 15881 | 08531 | 24413 | 15 |
| 50 | 75678 | 91425 | 84254 | 15746 | 08575 | 24322 | 10 |
| 55 | 75769 | 91381 | 84388 | 15612 | 08619 | 24231 |  |
| 60 | 75859 | 91336 | 84523 | 15477 | 08664 | 24141 | 0 |
| M | C. Sin | Sine | T Tang. | Tang. | . Sec | Secan | M |
|  |  |  |  |  |  |  |  |
|  |  |  | 35 Deg |  |  |  |  |
| M | Sine | C. Sine | Tang. | C.Tan | Secan | C. Sec. |  |
| 0 | 9.75859 | 9.91336 | 9.84523 | 10.15477 | 10.08664 | 10.24141 | 60 |
| 5 | 75949 | 91292 | 84657 | 15343 | 08708 | 24051 | 55 |
| 10 | 76039 | 91248 | 84791 | 15209 | 08752 | 23961 | 50 |
| 15 | 76129 | 91203 | 84925 | 15075 | 08797 | 23871 | 45 |
| 20 | 76218 | 91158 | 85059 | 14941 | 08842 | 23782 | 40 |
| 25 | 76307 | 91114 | 85193 | 14807 | 08886 | 23693 | 35 |
| 30 | 76395 | 91069 | 85327 | 14673 | 08931 | 23605 | 30 |
| 35 | 9.76484 | $\overline{9.91023}$ | 9.85460 | 10.14540 | $\overline{10.08977}$ | $\overline{10.23516}$ | 25 |
| 40 | 76572 | 90978 | 85594 | 14406 | 09022 | 23428 | 20 |
| 45 | 76660 | 90933 | 85727 | 14273 | 09067 | 23340 | 15 |
| 50 | 76747 | 90887 | 85860 | 14140 | 09113 | 23253 | 10 |
| 55 | 76835 | 90842 | 85993 | 14007 | 09158 | 23165 | 5 |
| 60 | 76922 | 9079 | 86128 | 13874 | 09204 | 23078 | 0 |
|  | $\overline{\text { C. Sine }}$ | Sine | $\overline{\text { C.Tang. }}$ | Tang. | C. Se\%. | $\overline{\text { Secant }}$ | M1 |
| 54 Degrees. |  |  |  |  |  |  |  |

Artificial Sines, Tangents, and Secants. 33

| 36 Degrees. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Sine | C. Sine | Tang. C.Tang. Secant C. Sec. +M |  |  |  |  |
| 0 | 9.76922 | 9.90796 | 9.8612610 | 10.13874 | 0.092041 | 0.23078 |  |
| 5 | 77009 | 90750 | 86259 | 13741 | 09250 | 22991 | 55 |
| 10 | 77095 | 90704 | 86392 | 13608 | 09296 | 22905 | 50 |
| 15 | 77181 | 90657 | 86524 | 13476 | 09343 | 22819 | 45 |
| 20 | 77268 | 90611 | 86656 | 13344 | 09389 | 22732 | 40 |
| 25 | 77353 | 90565 | 86789 | 13211 | 09435 | 22647 | 35 |
| 30 | 77439 | 90518 | 86921 | 13079 | 09482 | 22561 | 30 |
| 35 | $\overline{9.77524}$ | 9.90471 | 9.87053 | $\overline{10.12947}$ | 0.0953910 | 0.22476 | 25 |
| 40 | 77609 | 90424 | 87185 | 12815 | 09576 | 22391 | 20 |
| 45 | 77694 | 90377 | 87317 | 12683 | 09623 | 22306 |  |
| 50 | 77778 | 90330 | 87443 | 12552 | 09670 | 22222 |  |
| 55 | 77862 | 90282 | 87580 | 12420 | 09718 | 22138 |  |
| 60 | 77946 | 90235 | 87711 | 12289 | 09765 | 22054 |  |
| $\bar{M}$ C.Sine Sine $\overline{\text { C.Tang. Tang. }} \overline{\text { C. Sec. }}$ Secant $+\mathbf{M}$ |  |  |  |  |  |  |  |
| 53 Degrees. |  |  |  |  |  |  |  |
| 37 Degrees. |  |  |  |  |  |  |  |
| M Sine C. Sine Tang. C.Tang. Secant C. Sec. M |  |  |  |  |  |  |  |
| 0 | $\overline{9.77946}$ | 9.90235 | 9.87711 | 10.12289 | 0.09765 | 10.22054 |  |
| 5 | 78030 | 90187 | 87843 | 12157 | 09813 | 21970 | 55 |
| 10 | 78113 | 90139 | 87974 | 12026 | 09861 | 21887 |  |
| 15 | 78197 | 90091 | 88105 | 11895 | 09909 | 21803 | 45 |
| 20 | 78280 | 90043 | 88236 | 11764 | 09957 | 21720 | 40 |
| 25 | 78362 | 89995 | 88367 | 11633 | 10005 | 21638 | 35 |
| 30 | 78445 | 89947 | 88498 | 11502 | 10053 | 21555 | 30 |
| 35 | 9.78527 | 9.89898 | 9.88629 | $\underline{10.11371}$ | $\overline{10.10102}$ | $\overline{10.21473}$ | 25 |
| 40 | 78609 | 89849 | 88759 | 11241 | 10151 | 21391 | 20 |
| 45 | 77691 | 89801 | 88890 | 11110 | 10199 | 21309 | 15 |
| 50. | 78772 | 89752 | 89020 | 10380 | 10248 | 21228 |  |
| 55 | 78853 | 89702 | 89151 | 10849 | 10298 | 21147 | 5 |
| 60 | 78934 | 89653 | 89281 | 110719 | 10347 | 21066 |  |
| $\overline{\mathrm{I}}$ C. Sine $\overline{\text { Sine }}$ C.Tang. Tang. $\overline{\text { C. Sec. }} \overline{\text { Secant }} \mathrm{M}$ |  |  |  |  |  |  |  |
| 52 Degrees. |  |  |  |  |  |  |  |
| 38 Degrees. |  |  |  |  |  |  |  |
| $\mathbf{M}$ Sine C. Sine Tang. C.Tang. Secant C. Sec. M |  |  |  |  |  |  |  |
| 0 | 9.78934 | 9.89653 | 9.89281 | 10.10719 | 10.10347 | 10.21066 | 60 |
| 5 | 579015 | 89604 | 89411 | 110589 | 10396 | 20985 | 55 |
| 10 | 79095 | 89554 | 89541 | 110459 | 10446 | 20905 | 50 |
| 15 | 59176 | -89504 | - 89671 | 110329 | 10496 | 20824 |  |
| 20 | -79256 | - 89455 | 89801 | 110199 | 10545 | 20744 |  |
| 25 | 579335 | 58405 | 89931 | 10069 | 10595 | 20655 | 5.35 |
| 30 | $0 \quad 79415$ | 5 89354 | 490061 | 109939 | 10646 | 20585 |  |
| 35 | $5 \overline{9.79494}$ | 9.89304 | 9.90190 | 010.09810 | 10.10696 | 10.20506 | 6 |
|  | 079573 | 38954 | 490320 | - 09680 | 10746 | 20427 | 720 |
| 45 | 573652 | 289203 | 390449 | 909551 | 10797 | 20348 |  |
|  | - 79731 | 189152 | 290578 | 809422 | 10848 | 20269 | 910 |
|  | 5) 79809 | 989101 | 190708 | 8 09292 | 10899 | 20191 | 15 |
|  | $60 \quad 79887$ | $7 \quad 89050$ | $0 \quad 90837$ | $7 \quad 09163$ | 10950 | 20113 |  |
| $\bar{M}$ C. Sine Sine C.Tang. Tang. $\overline{\text { C. Sec. }}$ Secant $\bar{M}$ |  |  |  |  |  |  |  |
| 51 Degrees. |  |  |  |  |  |  |  |

34 Artificial Sines, Tangents, and Secants.

| 39 Degrees. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M Sine |  | C. Sine | Tang | C.Tang. Secant |  | C. Sec. ${ }^{\text {N1 }}$ |  |
| 0 | 9.79887 | 9.89050 | 9.90837 | 10.09163 | 10.10950 | 10.20113 | 60 |
| 5 | 79965 | 88999 | 90966 | 09034 | 11001 | 20035 | 55 |
| 10 | 80043 | 88948 | 91095 | 08905 | 11052 | 19957 | 50 |
| 15 | 80120 | 88896 | 91224 | 08776 | 11104 | 19880 | 45 |
| 20 | 80197 | 88844 | 91353 | 08647 | 11156 | 19803 | 40 |
| 25 | 80274 | 88793 | 91482 | 08518 | 11207 | 19726 | 35 |
| 30 | 80351 | 88741 | 91610 | 08990 | 11259 | 19649 | 30 |
| 35 | 9.80428 | 9.88688 | 9.91739 | 10.08261 | 10.11312 | 10.19572 | 25 |
| 40 | 80504 | 88636 | 91868 | 08132 | 11364 | 19496 | 20 |
| 45 | 80580 | 88584 | 91996 | 08004 | 11416 | 19420 | 15 |
| 50 | 80656 | 88531 | 92125 | 07875 | 11469 | 19344 | 10 |
| 55 | 80731 | 88478 | 92253 | 07747 | 11522 | 19269 | 5 |
| 60 | 80807 | 88425 | 92381 | 07619 | 11575 | 19193 | 0 |
| M | C. Sine | C.Tang. |  | Tang. | C. Sec | Secant |  |
|  | 50 Degrees. |  |  |  |  |  |  |
|  | 40 Degrees. |  |  |  |  |  |  |
| $\overline{\mathrm{M}}$ Sine $\mid$ C. Sine Tang. C.Tang. Secant $\mid$ C. Sec. $\mathbf{M}$ |  |  |  |  |  |  |  |
| $\square_{0} 9.80807$ |  | 9.88425 | 9.92381 | 10.07619 | 10.11575 | 10.19193 |  |
| 5 | 80882 | 88372 | 92510 | 07490 | 11628 | 19118 | 55 |
| 10 | 80957 | 88319 | 92638 | 07362 | 11681 | 19043 | 50 |
| 15 | 81032 | 88266 | 92766 | 07234 | 11734 | 18968 | 45 |
| 20 | 81106 | 88212 | 92894 | 07106 | 11788 | 18594 | 40 |
| 25 | 81180 | 88158 | 93022 | 06978 | 11842 | 18820 | 35 |
| 30 | 81254 | 88105 | 93150 | 06850 | 11845 | 18746 | 30 |
| 35 | 9.81328 | 9.88050 | 9.93278 | 10.06722 | 0.11950 | $\overline{10.18672}$ | 25 |
| 40 | 81402 | 81996 | 93406 | 06594 | 12004 | 18598 | 30 |
| 45 | 81475 | 87942 | 93533 | 06467 | 12058 | 18535 | 15 |
| 50 | 81549 | 87887 | 93661 | 06339 | 72113 | 18451 | 10 |
| 55 | 81682 | 87833 | 93789 | 06211 | 12167 | 18378 | 5 |
| 60 | 81694 | 87778 | 93916 | 06084 | 12222 | 18306 | 0 |
| $\overline{\text { M C. Sine }}$ |  | Sin |  | Tang. | . | Se | I |
| 49 Degrees. |  |  |  |  |  |  |  |
| 417 Degrees. |  |  |  |  |  |  |  |
| M | Sine | C. Sine | Tang. | C.Tang. Secant |  | C. Sec. ${ }^{1}$ |  |
| 0 | 9.81694 | 9.87778 | 9.9391694044 | 10.0608405956 | 10.12222 | 10.18306 | 60 |
| 5 | 81767 | 87723 |  |  | 12277 | 18233 | 65 |
| 10 | 81839 | 87668 |  94044 <br>  94171 | 05829 | 12332 | 18161 | 50 |
| 15 | 81911 | 87613 | 94299 | 05701 | 12387 | 18089 | 45 |
| 20 | 81983 | 87557 | 94426 | 05574 | 12443 | 18017 | 40 |
| 25 | 82055 | 87501 | 94554 | 05446 | 12499 | 17945 | 35 |
| 30 | 82126 | 87446 | 94681 | 05319 | 12554 | 178 | 0 |
| 35 | 9.82198 | 9.87390 | 9.94808 | $\overline{10.05192}$ | 10.12610 | $\overline{10.17802}$ | 25 |
| 40 | 82269 | 87334 | $\begin{aligned} & 94935 \\ & 95062 \end{aligned}$ | 05065 | 12666 | 17731 | $2 \theta$ |
| 45 | 82340 | 87277 |  | 04938 | 12723 | 17660 | 15 |
| 50 | 82410 | 87221 | 95190 | 04810 | 12779 | 17590 | 10 |
| 55 | 82481 | 87164 | 95317 | 04683 | 12836 | 17519 | 5 |
| 60 | 82551 | 87107 | 95444 | 04556 | 12893 | 17449 | 0 |
|  | C. | Sine | C.Tang. Tang. |  |  | $\overline{\text { Secant }}$ | 1 |
| 48 Degrees. |  |  |  |  |  |  |  |

Artificial Sines, Tangents, and Secants. 35

| 42 Degrees. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M. Sine |  | C. Sine | Tang. C.Tang. |  | Secant. C. Sec. 1 I |  |  |
| 0 | 9.82551 | 9.87107 | 9.95444 | 10.04556 | 10.12893 | 10.17449 | 60 |
| 5 | 82621 | 87050 | 95571 | 04429 | 12950 | 17379 | 5 |
| 10 | 82691 | 86993 | 95698 | 04302 | 13007 | 17309 | 50 |
| 15 | 82761 | 86936 | 95825 | 04175 | 13063 | 17239 | 45 |
| 20 | 82830 | 86879 | 95952 | 04048 | 13121 | 17170 | 40 |
| 25 | 82899 | 86821 | 96078 | 03922 | 13179 | 17101 | 85 |
| 30 | 82968 | 86763 | 96205 | 03795 | 13237 | 17032 | 30 |
| 35 | 9.83037 | 9.86705 | 9.96332 | $\overline{10.03668}$ | 10.13295 | 10.16963 | 25 |
| 40 | 83106 | 86647 | 96459 | 03541 | 13353 | 16894 | 20 |
| 45 | 83174 | 86589 | 96586 | 03414 | 13411 | 16826 | 15 |
| 50 | 83242 | 86530 | 96712 | 03288 | 13470 | 16758 | 10 |
| 55 | 83310 | 86472 | 96839 | 03161 | 13528 | 16690 | 5 |
| 60 | 83378 | 86413 | 96966 | 03034 | 13587 | 16622 | 0 |
|  | C. Sin | Sine | .Tang. | Tang. | . Sec. | Secant | M |
| 47 Degrees. <br> 43 Degrees. |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| $\overline{\mathbf{M}}$ Sine C. Sine Tang. C.Tang. Secant. C. Sec. M |  |  |  |  |  |  |  |
| 0 | $\overline{\text { S.83378 }}$ | 9.86413 | 9.96966 | . 03034 |  | 10.16622 |  |
| 5 | 83446 | 86354 | 97092 | 02908 | 13646 | 16554 |  |
| 10 | 83513 | 86295 | 97219 | 02781 | 13705 | 16487 | 50 |
| 15 | 83581. | $8623{ }^{\prime}$ | 97345 | 02655 | 13765 | 16419 |  |
| 20 | 83648 | 86176 | 97472 | 02528 | 13824 | 16352 |  |
| 25 | 83715 | 86116 | 97598 | 02402 | 13884 | 16285 | 35 |
| 30 | 83781 | 86056 | 97725 | 02275 | 13944 | 16219 | 30 |
| 35 | 9.83848 | 9.85996 | 9.97851 | 10.02149 | 10.14004 | 10.16152 | 25 |
| 40 | 83914 | 85936 | 97978 | 02022 | 14064 | 16086 |  |
| 45 | 83980 | 85876 | 98104 | 01896 | 14124 | 16020 |  |
| 50 | 84046 | 85815 | 98931 | 01769 | 14185 | 15954 | 10 |
| 55 | 84112 | 85754 | 98357 | 01643 | 14246 | 15888 | 5 |
| 60 | 84177 | 85693 | 98484 | 01516 | 14307 | 15823 |  |
| $\bar{M} \overline{\text { C. Sine }}$ Sine C.Tang. Tang. $\overline{\text { C. Sec. }}$ Secant. $\bar{M}$ |  |  |  |  |  |  |  |
| 46 Degrees. |  |  |  |  |  |  |  |
| 44 Degrees. |  |  |  |  |  |  |  |
| M | Sine | C. Sine Tang. C.Tang. Secant C. Sec. M |  |  |  |  |  |
| 0 | 9.84177 | $\overline{9.85693} \overline{9.98484} \overline{10.01516} \overline{10.14307} \overline{10.15823}$ - $-\overline{60}$ |  |  |  |  |  |
| 5 | 84242 | $\begin{array}{llll}85632 & 98610 & 01390 \\ 85571 & 98737 & 01263\end{array}$ |  |  | 14368 | 15758 | 55 |
| 10 | 84308 |  |  |  | 14429 | 15692 | 50 |
| 15 | 84373 | 8551098863 |  | 01137 | 14490 | 15627 | 45 |
| 20 | 84437 | 8544898989 |  | 01011 | 14552 | 15563 | 40 |
| 25 | 84502 | 8538699116 |  | 00884 | 14614 | 15498 | 35 |
| 30 | 84566 | $85324 \quad 99242$ |  | 00758 | 14676 | 15434 | , |
| 35 | 9.84630 | $\overline{9.85262} 9.99368$ | 9.99368 10.00632 10.1473810 .15370 |  |  |  |  |
| 40 | 84694 | 85200 99495  <br>  85137 99621 |  | 00505 | 14800 | 15306 | 20 |
| 45 | 84758 |  |  | 00379 | 14863 | 15242 | 15 |
| 50 | 84822 | $85074 \quad 99747$ |  | 00253 | 14926 | 15178 | 10 |
| 55 | 84885 | $85012 \quad 99874$ |  | 00126 | 14988 | 15115 | 5 |
| (M) | C. Sine | Sine C.Tang. Tang. C. Sec. Seca |  |  |  |  | 0 |
| 45 Degrees. |  |  |  |  |  |  |  |

III. A Traverse Table, or Table of Difference of Latitude and Departure, calculated for degrees and quarters of degrees, and for any distance up to 100 Rods, Chains, \&c. ; by which the northings and southings, eastings and westings made in a Survey may be found.

Vote. Northings and southings are called Difference of Latitude, or simply Latitude ; eastings and westings are called Departure, Meridian Distance, or Longitude.

## Explanation of the Table.

To find the Latitude and Departure, or Northing, \&ic. for any Course and Distance.

If the Course be less than $45^{\circ}$, look for it at the top, but if more than 450 at the bottom of the page, and look for the Distance in the right or left hand column; against the Distance, and directly under or over the Course, stand the northing, \&c. in whole numbers and decimals.

If the Course be less than $45^{\circ}$, the northing or southing will be greater than the easting or westing; but if more than 450 . the easting or westing will be the greatest.

When the Distance exceeds 100 , take any two or more numbers, which, added together, will equal the Distance, and find the Latitude and Departure for each of those numbers; add the several Latitudes together and the sum will be the whole Latitude; and so for the Departure. And when the Distance is in Chains and Links, or whole numbers and decimals, find the Latitude, \&c. for the Chains or whole numbers, and then for the Links or decimals, remembering to remove the decimal point in the Table further to the left, according to the given decimal.

## Examples.

1. Required the Latitude and Departure for 45 Rods, on a Course N. $15^{\circ} 15^{\prime} W$.

Under $15^{\circ} 15^{\prime}$ and against 45 is 43.42 for the nortbing, and 11.84 for the westing.
2. Required the Latitude and Departure for 120 Rods, on a Course S. $58 \circ 30^{\prime}$ E.

Sake one third of 120 which is 40 ; against this number, over $58^{\circ} 30^{\prime}$ is 29.90 for the Latitude and 34.11 for the Departure. These multiplied by 3 give 62.70 for the Southing and 102.33 for the Easting.
3. Required the Latitude and Departure for 37.36 Rods or 37 Chains and 36 Links, on a Course $\mathcal{N} .26^{\circ} 45^{\prime} E$.


Northing 33.36 Easting 16.81
Yote. When the Minutes are not 15, 30, or 45, the Northings, \&c. must be calculated by Natural Sines, or by Trigonometry.

|  | $\frac{1}{4} \mathrm{De}$ | eg: | $\frac{1}{2}$ Deg. |  | $\frac{3}{4}$ Deg. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. ${ }^{\text {D }}$ | Dep. | Lat. | Dep. | Lat. | Dep. |  |
| 1 | 1.00 | 0.00 | 1.00 | 0.01 | 1.00 | 0.01 |  |
| 2 | 2.00 | 0.01 | 2.00 | 0.02 | 2.00 | 0.08 | 2 |
| 3 | 3.00 | 0.01 | 3.00 | 0.03 | 3.00 | 0.04 | 3 |
| 4 | 4.00 | 0.02 | 4.00 | 0.03 | 4.00 | 0.05 | 4 |
| 5 | 5.00 | 0.02 | 5.00 | 0.04 | 5.00 | 0.07 | 5 |
| 6 | 6.00 | 0.03 | 6.00 | 0.05 | 6.00 | 0.08 | 6 |
|  | 7.00 | 0.03 | 7.00 | 0.06 | 7.00 | 0.09 | 8 |
| 8 | 8.00 9.00 | 0.03 0.04 | 8.00 9.00 | 0.07 0.08 | 8.00 9.00 | 0.10 0.12 | 8 |
| 10 | 10.00 | 0.04 | 10.00 | 0.09 | 10.00 | 0.13 | 10 |
| 11 | 11.00 | 0.05 | 11.00 | 0.10 | 11.00 | 0. | 11 |
| 12 | 12.00 | 0.05 | 12.00 | 0.10 | 12.00 | 0.16 | 12 |
| 13 | 13.00 | 0.06 | 13.00 | 0.11 | 13.00 | 0.17 | 13 |
|  | 14.00 | 0.06 | 14.00 | 0.12 | 14.00 | 0.18 | 14 |
| 15 | 15.00 | 0.07 | 15.00 | 0.13 | 15.00 | 0.20 | 15 |
|  | 16.00 | 0.07 | 16.00 | 0.14 | 16.00 | 0.21 | 6 |
|  | 17.00 | 0.07 | 17.00 | 0.15 | 17.00 | 0.22 | 7 |
|  | 18.00 | 0.08 | 18.00 | 0.16 | 18.00 | 0.24 | 8 |
|  | 19.00 | 0.08 | 19.09 | 0.17 | 19.00 | 0.25 | 19 |
| 20 | 20.00 | 0.09 | 20.00 | 0.17 | 20.00 | 0.26 | 20 |
|  | 21.00 | 0.09 | 21.00 | 0.18 | 21.00 | 0.27 | 21 |
|  | 22.00 | 0.10 | 22.00 | 0.19 | 22.00 | 0:29 | 2 |
|  | 23.00 | 0.10 | 23.00 | 0.20 | 23.00 | 0.30 | 23 |
|  | 424.00 | 0.10 | 24.00 | 0.21 | 24.00 | 0.31 | 24 |
|  | 25.00 | 0.11 | 25.00 | 0.22 | 25.00 | 0.33 | 25 |
|  | 26.00 | 0.11 | 26.00 | 0.23 | 26.00 | 0.34 | 26 |
|  | 27.00 | 0.12 | 27.00 | 0.24 | 27.00 | 0.35 | 77 |
|  | 28.00 | 0.12 | 28.00 | 0.24 | 28.00 | 0.37 | 28 |
|  | 929.00 | 0.13 | 29.00 | 0.25 | 29.00 | 0.38 | 29 |
|  | 30.00 | 0.13 | 30.00 | 0.26 | 30.00 | 0.39 | - |
|  | 131.00 | 0.14 | 31.00 | 0.27 | 31.00 | 0.41 | 31 |
|  | 232.00 | 0.14 | 32.00 | 0.28 | 32.00 | 0.42 | 32 |
|  | 33.00 | 0.14 | 33.00 | 0.29 | 33.00 | 0.43 | 33 |
|  | 434.00 | 0.15 | 34.00 | 0.30 | 34.00 | 0.45 | 34 |
|  | 5.35.00 | 0.15 | 35.00 | 0.31 | 35.00 | 0.46 | 35 |
|  | 636.00 | 0.16 | 36.00 | 0.31 | 36.00 | 0.47 | 36 |
|  | 737.00 | 0.16 | 37.00 | 0.32 | 37.00 | 0.48 | 37 |
|  | 888.00 | 0.17 | 38.00 | 0.33 | 38.00 | 0.50 | 38 |
|  | 9.39.00 | 0.17 | 39.00 | 0.34 | 39.00 | 0.51 | 39 |
|  | 0:40.00 | 0.17 | 40.00 | 0.35 | 40.00 | 0.52 | 40 |
|  | 141.00 | 0.18 | 41.00 | 0.36 | 41.00 | 0.54 | 41 |
|  | 242.00 | 0.18 | 42.00 | 0.37 | 42.00 | 0.55 | 42 |
|  | 343.00 | 0.19 | 43.00 | 0.38 | 43.00 | 0.56 | 43 |
|  | 44.00 | 0.19 | 44.00 | 0.38 | 44.00 | 0.58 | 4 |
|  | 545.00 | 0.20 | 45.00 | 0.39 | 45.00 | 0.59 | 45 |
|  | 646.00 | 0.20 | 46.00 | 0.40 | 46.00 | 0.60 | 46 |
|  | 747.00 | 0.21 | 47.00 | 0.41 | 47.00 | 0.62 | 47 |
| 48 | 84.00 | 0.21 | 48.00 | 0.42 | 48.00 | 0.63 | 48 |
| 49 | 949.00 | + 0.21 | 49.00 | 0.43 | 49.00 | 0.64 | 49 |
| 50 | 050.00 | 0.22 | 50.00 | 0.44 | 50.00 | 0.65 | 50 |
|  | Dep. | Lat. | Dep. Lat. |  | Dep. |  |  |
|  | $89 \frac{3}{4}$ | Deg. | 8912 | Deg. | 891 | Deg. |  |


| $\stackrel{\square}{\square}$ | $\frac{\frac{1}{4} \mathrm{D}}{\text { Lat. }}$ | Deg. | $\frac{1}{2}$ Deg. |  | $\frac{3}{4}$ Deg. |  | $\begin{aligned} & Y \\ & 5 \\ & 5 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 51 |  |  |  |  |  |  | 51 |
| 52 | 52.00 | 0.23 | 52.00 | 0. | 52.00 | 68 | 52 |
| 53 | 53.00 | 0.23 | 53.00 | 0.46 | 53.00 | 0.69 | 53 |
| 54 | 54.00 | 0.24 | 54.00 | 0.47 | 54.00 | 0.71 | 54 |
| 55 | 55.00 | 0.24 | 55.00 | 0.48 | 55. | 0.72 | 55 |
| 56 | 56.00 | 0.24 | 56.00 | 0.49 | 56.0 |  | 56 |
| 57 | 57.00 | 0.25 | 57.00 | 0.50 | 57.00 | 0.75 | 57 |
| 58 | 58.00 | 0.25 | 58.00 | 0.5 | 57.99 | 0.76 | 58 |
| 59 | 59.0 | 0.26 | 59.00 | 0.51 | 58.99 | 0.77 | 59 |
| 60 | 60. | 0.26 | 60.00 | 0.52 |  | 0.79 | 60 |
| 61 |  |  |  |  |  |  | 1 |
| 62 | 62.0 | 0.27 | 62.00 | 0.5 | 61 |  | 62 |
| 63 | 63.0 | 0.27 | 63.00 | 0.55 | 62.9 | 0.82 | 68 |
| 64 | 64.00 | 0.28 | 64.00 | 0.56 | 63.9 | 0. | 64 |
| 65 | 65.00 | 0.28 | 65.00 | 0.57 | 64.9 |  | 65 |
| 66 | 66.0 | 0.29 | 66.00 | 0.58 | 65.99 | 86 | 66 |
| 67 | 67.0 | 0.29 | 67.00 | 0.58 | 66.9 | . 8 | 67 |
| 68 | 68.4 | 0.30 | 68.00 | 0.59 | 67.9 | 0. | 68 |
| 69 | 69.00 | 0.30 | 69.0 | 0.60 | 68.99 | 0.90 | 69 |
| 70 | 70. | 0.31 | 70.0 | 0.61 | 69.99 | 0.92 | 70 |
| 7 |  |  |  |  | \% |  |  |
| 72 | 72.00 | 0.31 | 72.00 | 0.6 | 71.9 | 0. | 72 |
| 73 | 73.00 | 0.32 | 73.00 | 0.64 | 72.9 | 0.96 | 73 |
| 74 | 74.00 | 0.32 | 74.00 | 0.65 | 73.9 | 0.97 |  |
| 75 | 75.00 | 0.33 | 75.00 | 0.65 | 74.9 | 0. | 75 |
| 76 | 76.00 | 0.33 | 76.0 | 0.66 | 75.9 | 0. |  |
| 77 | 77.0 | 0.34 | 77.00 | 0.67 | 76.9 | 1.01 |  |
| 78 | 78.0 | 0.34 | 78.00 | 0.68 | 77. | 1.02 | 78 |
| 79 | 79.0 | 0.34 |  | 0.69 | 78 | 1.0 |  |
| 80 | 80.0 | 0.35 | 80.0 | 0.7 |  |  |  |
| 81 |  | , 3 |  | 71 |  |  |  |
| 82 | 82.0 | 0.36 | 2.0 | 0.72 | 81. | 1.07 | 82 |
| 83 | 83.0 | 0.36 | 83.0 | 0.72 | 82. | 1.09 | 83 |
| 84 | 84. | 0.37 | 84.00 | 0.73 | 83.9 |  | 8 |
| 85 | 85.0 | 0.37 | 85.00 | 0.74 | 84.9 | 1.11 | 85 |
| 86 | 86.6 | 0.38 | 86.0 | 0.75 |  | 1.13 | 86 |
| 8 | 87. | 0.38 | 87.00 | 0.76 | 86.9 | 1.14 | 87 |
| 88 | 88.0 | 0.38 | 88.00 | 0.77 | 87.9 | 1.15 | 88 |
| 89 | 89.0 | 0.39 | 89.0 | 0.78 | 88. | 1. | 8 |
| 90 | 90.0 | 0.3 |  | 0.79 |  |  |  |
| 91 | 91. | 0.40 | 91. | 0.79 | 90 | 1.10 | 91 |
| 92 | 92.0 | 0.40 | 92.09 | 0.80 | 91.9 | $1 . \sim 0$ |  |
| 93 | 93.0 | . 0.41 | 93.00 | 0.81 | 92. | 1.2 | 93 |
| 94 | 94. | 0.41 | 94.00 | 0.82 | 33. | 1.23 |  |
| 95 | 95.6 | 0.41 | 95.00 | 0.83 | 94.9 | 1.2 |  |
| 96 | 96.0 | 0.4 | 96.00 | 0.84 | 95. | 1.26 | 96 |
| 9 | 97. | 0.4 | 97.0 | 0.85 | 96.9 | 1.27 | 97 |
| 98 | 98.0 | 0.43 | 98.00 | 0.86 | - | 1.28 |  |
| 99 | 99.00 | 0.43 | 99.0 | 0.86 |  | 1.30 | 99 |
| 100 | 100.0 | 0. | 100.0 | 0.8 | 99. |  |  |
|  |  | Lat. | Dep | Lat. |  |  |  |
|  | $89 \frac{3}{4}$ Deg. |  | 89 $\frac{1}{2}$ Deg. $89 \frac{1}{4} \mathrm{Deg}$. |  |  |  |  |

TRAVERSE TABLE.

| $\underset{\substack{\circ\\}}{\sim}$ | 1 D | e | 14 |  | $1 \frac{1}{2}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. |  |  | Lat. | Dep. | Lat. | Dep. |  |
| 1 | 1.00 | 0.02 | 1.00 | 0.02 | 1.00 | 0.03 | 1.00 |  |  |
| 2 | 2.00 | 0.03 | 2.00 | 0.04 | 2.00 | 0.05 | 2.00 | 0.0 |  |
| 3 | 3.00 | 0.05 | 3.00 | 0.07 | 3.00 | 0.08 | 3.00 | 0.09 |  |
| 4 | 4.00 | 0.07 | 4.00 | 0.09 | 4.00 | 0.10 | 4.00 | 0.12 |  |
| 5 | 5.00 | 0.09 | 5.00 | 0.11 | 5.00 | 0.13 | 5.00 | 0.15 |  |
| 6 | 6.00 | 0.10 | 6.00 | 0.13 | 6.00 | 0.16 | 6.00 | 0.18 |  |
| 7 | 7.00 | 0.12 | 7.00 | 0.15 | 7.00 | 0.18 | 7.00 | 0.21 |  |
|  | 8.00 | 0.14 | 8.00 | 0.17 | 8.00 | 0.21 | 8.00 | 0.25 |  |
| 9 | 9.00 | 0.16 | 9.00 | 0.20 | 9.00 | 0.24 | 9.00 | 0.2 |  |
| 10 | 10.00 | 0.17 | 10.00 | 0.22 | 10.00 | 0.26 | 10.00 | 0.31 | 10 |
| 11 | 11.00 | 0.19 | 11.00 | 0.24 | 11.00 | 0.28 | 10.99 |  | 11 |
| $\begin{aligned} & 12 \\ & 13 \end{aligned}$ | 12.00 | 0.21 | 12.00 | 0.26 | 12.00 | 0.31 | 11.99 | 0, | 2 |
|  | 13.00 | 0.23 | 13.00 | 0.28 | 13.00 | 0.34 | 12.99 | 0 | 3 |
| $\left.\begin{aligned} & 13 \\ & 14 \\ & 15 \end{aligned} \right\rvert\,$ | 14.00 | 0.24 | 14.00 | 0.31 | 14.00 | 0.37 | 13.99 | 0. | 4 |
|  | 15.00 | 0.26 | 15.00 | 0.33 | 14.99 | 0.39 | 14.99 | 0.46 | 5 |
| $\left\|\begin{array}{l} 15 \\ 16 \\ 17 \end{array}\right\|$ | 16.00 | 0.28 | 16.00 | 0.35 | 15.99 | 0.42 | 15.99 | 0.49 |  |
|  | 17.00 | 0.30 | 17.00 | 0.37 | 16.99 | 0.45 | 16.99 |  | 7 |
| 17 | 18.00 | 0.31 | 18.00 | 0.39 | 17.99 | 0.47 | 17.99 | 0. | 8 |
| $\begin{aligned} & 19 \\ & 20 \end{aligned}$ | 19.00 | 0.33 | 19.00 | 0.41 | 18.99 | 0.50 | 18.99 | 0.5 | 9 |
|  | 20.00 | 0.35 | 20.00 | 0.44 | 19.99 | 0.52 | 19.99 | 0. | 0 |
|  |  | 0.37 | 21.00 | 0.46 | 20.99 | 0.55 | 20.99 |  | 1 |
|  | 22.00 | 0.38 | 21.99 | 0.48 | 21.99 | 0.58 | 21.99 | 0.67 | 2 |
|  | 23.00 | 0.40 | 22.99 | 0.50 | 23.99 | 0.60 | 22.99 | 0.70 | 3 |
| 24 | 24.00 | 0.42 | 23.99 | 0.52 | 23.99 | 0.63 | 23.99 | 0.7 | 4 |
|  | 25.00 | 0.44 | 24.99 | 0.55 | 24.99 | 0.65 | 24.99 | 0.76 | 5 |
|  | 26.00 | 0.45 | 25.99 | 0.57 | 25.99 | 0.68 | 25.99 |  | 6 |
| 278 28 | 27.00 | 0.47 | 26.99 | 0.59 | 26.99 | 0.71 | 26.99 | 0.8 | 7 |
|  | 28.00 | 0.49 | 27.99 | 0.61 | 27.99 | 0.73 | 27.99 | 0.8 | 8 |
| 29 | 29.00 | 0.51 | 28.99 | 0.63 | 28.99 | 0.76 | 28.99 |  | 9 |
|  | 30.00 | 0.52 | 29.99 | 0.65 | 29.99 | 0.79 | 29.99 |  | 0 |
|  | 31.00 | 0.54 | 30.99 | 0.68 | 30.99 | 0.81 | 30.99 | 0.9 | 31 |
|  | 32.00 | 0.56 | 31.99 | 0.70 | 31.99 | 0.84 | 31.99 | 0.9 | 32 |
|  | 32.99 | 0.58 | 32.99 | 0.72 | 32.99 | 0.86 | 32.98 | 1.01 | 3 |
|  | 33.99 | 0.59 | 33.99 | 0.74 | 33.99 | 0.89 | 33.98 | 1.04 | 34 |
|  | 34.99 | 0.61 | 34.99 | 0.76 | 34.99 | 0.92 | 34.98 | 1.07 | 5 |
|  | 35.99 | 0.63 | 35.99 | 0.79 | 35.99 | 0.94 | 35.98 | 1.10 | 36 |
|  | 36.99 | 0.65 | 36.99 | 0.81 | 36.99 | 0.97 | 36.9 | 1.13 | 37 |
|  | 37.99 | 0.66 | 37.99 | 0.83 | 37.99 | 0.99 | 37.98 | 1.16 | 38 |
| 3940 | 38.99 | 0.68 | 38.99 | 0.85 | 38.99 | 1.02 | 38.98 | 1.19 | 9 |
|  | 39.99 | 0.70 | 39.99 | 0.87 | 39.99 | 1.05 | 39.98 | 1.22 | 0 |
|  | 40.99 | 0.72 | 40.99 | 0.89 | 40.99 | 1.07 | 40.9 | 1.2 | 1 |
|  | 41.99 | 0.73 | 41.99 | 0.92 | 41.99 | 1.10 | 41.9 | 1.28 |  |
|  | 42.99 | 0.75 | 42.99 | 0.94 | 42.99 | 1.13 | 2. | 1.31 | 43 |
|  | 43.99 | 0.77 | 43.99 | 0.96 | 13.98 | 1.15 | 43.9 | 1.34 | 4 |
|  | 44.99 | 0.79 | 44.99 | 0.98 | 44.99 | 1.18 | 44.9 | 1.37 | 45 |
|  | 45.99 | 0.80 | 45.99 | 1.00 | 45.99 | 1.2 | 45.9 | 1.40 | 46 |
|  | 46.99 | 0.82 | 46.99 | 1.03 | 46.49 | 1.23 | 46.98 | 1.44 | 7 |
|  | 47.99 | 0.84 | 47.99 | 105 | 47.98 | 1.26 | 47.9 | 1.47 | 8 |
|  | 48.99 | 0.86 | 48.99 | 1.07 | 48.98 | 1.28 | 48.98 | 1.50 | 49 |
|  | 49.99 | 0.87 | 49.99 | 1.09 | 49.98 | 1.31 | 49.98 | 1.53 | 50 |
|  | Dep | Lat. | D | Lat. | Dep | Lat. | Dep |  |  |
|  |  |  |  |  | $8 \frac{1}{2}$ |  |  |  |  |


| $\left\lvert\, \begin{gathered} - \\ \underset{\sim}{6} \end{gathered}\right.$ |  | Dep. | $1 \frac{1}{4}$ Deg. |  | 112 Deg. ${ }^{\frac{1}{2}} 1 \frac{3}{4}$ Deg. |  |  |  | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. |  | La | Dep. |  | ep. | Lat. | Dep. |  |
| 51 | 50.98 | 0.89 | 50.99 | 1.11 | 50.98 | 1.34 | 50.98 | 1.56 | 1. |
| 52 | 51.99 | 0.91 | 51.99 | 1.13 | 51.98 | 1.36 | 51.98 | 1.59 | 52 |
| 53 | 52.98 | 0.92 | 52.99 | 1.16 | 52.98 | 1.39 | 52.98 | 1.62 | 53 |
| 54 | 53.99 | 0.94 | 53.99 | 1.18 | 53.98 | 1.41 | 53.97 | 1.65 | 5 |
| 55 | 54.99 | 0.96 | 54.99 | 1.20 | 54.98 | 1.44 | 54.97 | 1.68 | 55 |
| 56 | 55.98 | 0.98 | 55.99 | 1.22 | 55.98 | 1.47 | 55.97 | 1.71 | 56 |
| 57 | 56.99 | 0.99 | 56.99 | 1.24 | 56.98 | 1.49 | 56.97 | 1.74 | 57 |
| 58 | 57.99 | 1.01 | 57.99 | 1.27 | 57.98 | 1.52 | 57.97 | 1.77 | 58 |
| 59 | 53.99 | 1.03 | 58.99 | 1.29 | 58.98 | 1.54 | 58.97 | 1.80 | 59 |
| 60 | 59.98 | 1.05 | 59.99 | 1.31 | 59.98 | 1.57 | 59.97 | 1.83 | 60 |
| 61 | 60.99 | 1.06 | 60.99 | 1.33 | 60.98 | 1.60 | 60.97 | 1.86 | , |
| 62 | 61.95 | 1.08 | 61.99 | 1.35 | 61.98 | 1.62 | 61.97 | 1.89 | 62 |
| 63 | 62.99 | 1.10 | 62.99 | 1.37 | 62.98 | 1.65 | 62.97 | 1.92 | 63 |
| 64 | 63.99 | 1.12 | 63.98 | 1.40 | 63.98 | 1.68 | 63.97 | 1.95 | 64 |
| 65 | 64.95 | 1.13 | 64.98 | 1.42 | 64.98 | 1.70 | 64.97 | 1.99 | 65 |
| 66 | 65.98 | 1.15 | 65.98 | 1.44 | 65.98 | 1.73 | 65.97 | 2.02 | 66 |
| 67 | 66.99 | 1.17 | 66.98 | 1.46 | 66.98 | 1.75 | 66.97 | 2.05 | 67 |
| 68 | 67.99 | 1.19 | 67.98 | 1.48 | 67.98 | 1.78 | 67.97 | 2.08 | 68 |
| 69 | 68.99 | 1.20 | 68.98 | 1.51 | 68.98 | 1.81 | 68.97 | 2.11 | 69 |
| 70 | 69.95 | 1.22 | 69.98 | 1.53 | 69.98 | 1.83 | 69.97 | 2.14 | 70 |
| 71 | 70.93 | 1.24 | 70.9 | 1. | 70.9 | 1.86 | 70 | 2.17 | 71 |
| 72 | 71.98 | 1.26 | 71.98 | 1.57 | 71.98 | 1.88 | 71.97 | 2.20 | 72 |
| 73 | 72.99 | 1.27 | 72.98 | 1.59 | 72.97 | 1.91 | 72.97 | 2.23 | 73 |
| 74 | 73.99 | 1.29 | 73.98 | 1.61 | 73.97 | 1.94 | 73.97 | 2.26 | 74 |
| 75 | 74.99 | 1.31 | 74.98 | 1.64 | 74.97 | 1.96 | 74.97 | 2.29 | 75 |
| 76 | 75.99 | 1.33 | 75.98 | 1.66 | 75.97 | 1.99 | 75.96 | 2.32 | 76 |
| 77 | 76.95 | 1.34 | 76.98 | 1.68 | 76.97 | 2.02 | 76.9 | 2.35 | 77 |
| 78 | 77.99 | 1.36 | 77.98 | 1.70 | 77.97 | 2.04 | 77.9 | 2.38 | 78 |
| 79 | 78.94 | 1.38 | 78.98 | 1.72 | 78.97 | 2.07 | 78.96 | 2.41 | 79 |
| S0 | 79.9 | 1.40 | 79.98 | 1.75 | 79.97 | 2.09 | 79.96 | 2.44 | 80 |
| 81 | 80.95 | 1.41 | 80.98 | 1.77 | 80.97 | 2.12 | 90.96 | 2.47 | 81 |
| 82 | 81.9¢ | 1.43 | 81.98 | 1.79 | 81.97 | 2.15 | 81.96 | 2.50 | 82 |
| 83 | 82.98 | 1.45 | 82.98 | 1.81 | 82.97 | 2.17 | 82.96 | 2.53 | 83 |
| 84 | 83.99 | 1.47 | 83.98 | 1.83 | 83.97 | 2.20 | 83.96 | 2.57 |  |
| 83 | 84.95 | 1.48 | 84.98 | 1.85 | 84.97 | 2.23 | 84.96 | 2.60 | 85 |
| 86 | 85.9¢ | 1.50 | 85.98 | 1.88 | 85.97 | 2.25 | 85.96 | 2.6 | 86 |
| 87 | 86.9 c | 1.52 | 86.98 | 1.90 | 86.97 | 2.28 | 86.96 | 2.66 | 8 |
| 88 | 87.94 | 1.54 | 87.98 | 1.92 | 87.97 | 2.30 | 87.96 | 2.69 | 88 |
| 89 | 88.95 | 1.55 | 88.98 | 1.94 | 88.97 | 2.33 | 88.96 | 2.72 | 89 |
| 90 | 89.98 | 1.57 | 89.98 | 1.96 | 80.97 | 2.36 | 89.96 | 2.75 | 90 |
| 91 | 90.95 | 1.59 | 90.98 | 1.99 | ¢0.97 | 2.38 | 90.96 | 2.78 | 91 |
| 92 | 91.9¢ | 1.61 | 91.98 | 2.01 | 91.97 | 2.41 | 91.96 | 2.81 | 92 |
| 93 | c2.9 | 1.62 | 92.98 | 2.03 | 92.97 | 2.43 | 92.96 | 2.84 | 93 |
| 94 | 93.95 | 1.64 | 93.98 | 2.05 | 93.97 | 2.46 | 93.96 | 2.87 | 4 |
| 95 | 94.99 | 1.66 | 94.98 | 2.07 | 94.97 | 2.49 | 94.96 | 2.90 | 95 |
| 96 | 95.99 | 1.68 | 95.98 | 2.09 | 95.97 | 2.51 | 95.96 | 2.94 | 96 |
| 97 | 96.98 | 1.69 | 96.98 | 2.12 | 96.97 | 2.54 | 96.95 | 2.96 | 97 |
| 98 | 97.95 | 1.71 | 97.98 | 2.14 | :7.97 | 2.57 | 97.95 | 2.99 | 98 |
| 99 | 98.98 | 1.73 | 98.98 | 2.16 | 98.97 | 2.59 | 98.95 | 3.02 | 99 |
| 100 | 99.95 | 1.75 | 99.98 | 2.18 | 99.97 | 2.62 | 99.95 | 3.05 | 100 |
| $\because$ | Dep | Lat. | Dep. | Lat. | Dep. | Lat. | Dep | , |  |
|  | 89 Deg. |  | $88 \frac{3}{4}$ Deg. |  | $88 \frac{1}{2}$ Deg. |  |  |  |  |
|  |  |  |  |  | 0 |  |  |  |  |

TRAVERSE TABLE.

|  |  |  |  |  |  | g. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat | Dep. | Lat. | Dep. |  | Dep. | Lat. | Dep. |  |
|  | 1.00 | 0.03 | 1.00 | 0.0 | 1.00 | 0.04 | 1.00 | 0.05 |  |
|  | 2.00 | 0.07 | Q. 00 | 0.08 | 2.00 | 0.09 | 2.00 | 0.10 |  |
|  | 3.00 | 0.10 | 3.00 | 0.12 | 3.00 | 0.13 | 3.00 | 0.1 |  |
|  | 4.00 | 0.14 | 4.00 | 0.16 | 4.00 | 0.17 | 4.0 | 0.19 |  |
|  | 5.00 | 0.17 | 5.06 | 0.20 | 5.00 | 0.22 | 4.98 | 0.2 |  |
|  | 6.00 | 0.21 | 6.00 | 0.24 | 5.99 | 0.26 | 5.99 | 0.29 |  |
|  | 7.00 | 0.24 | 6.99 | 0.27 | 6.99 | 0.31 | 6.99 | 0.3 |  |
|  | 7.99 | 0.28 | 7.99 | 0.31 | 7.99 | 0.35 | 7.99 | 0.3 |  |
|  | 8.99 | 0.31 | 8.99 | 0.35 | 8.99 | 0.39 | 8.99 | 0.43 |  |
| 10 | 9.99 | 0.35 | 9.99 | 0.39 | 9.99 | 0.44 | 9.99 | 0.48 | 10 |
| 11 | 10.99 | 0.38 | 10.99 | 0.43 | 10.99 | 0.48 | 10.99 | 0.5 | , |
| 12 | 11.99 | 0.42 | 11.99 | 0.47 | 11.99 | 0.52 | 11.99 | 0.58 | 12 |
| 13 | 12.99 | 0.45 | 12.99 | 0.51 | 12.99 | 0.57 | 12.99 | 0.6 | 3 |
| 14 | 13.99 | 0.49 | 13.99 | 0.55 | 13.99 | 0.61 | 13.98 | 0.6 | 14 |
| 15 | 14.99 | 0.52 | 14.99 | 0.59 | 14.99 | 0.6 | 14.9 | 0.7 |  |
| 16 | 15.99 | 0.56 | 15.99 | 0.63 | 15.99 | 0.70 | 15.9 | 0.77 | 6 |
| 17 | 16.99 | 0.59 | 16.99 | 0.67 | 16.98 | 0.74 | 16.98 | 0.8 | 7 |
| 18 | 17.99 | 0.63 | 17.99 | 0.71 | 17.98 | 0.79 | 17.9 | 0 | 8 |
| 19 | 18.99 | 0.66 | 18.99 | 0.75 | 18.98 | 0.83 | 18.9 | 0.9 | 9 |
| 20 | 19.99 | 0.70 | 19.98 | 79 | 19.98 | 0.87 | 19.98 | 0.96 | 0 |
|  | 20.99 | 0.73 | 20.98 | 0.82 | 20.98 | 0.92 | 20.98 | 1.01 | 2, |
| 22 | 1.99 | 0.77 | 21.98 | 0.86 | 21.98 | 0.96 | 21.97 | 1.0 | , |
| 23 | 22.99 | 0.80 | 22.98 | 0.90 | 22.98 | 1.00 | 22.97 | 1.10 | 23 |
| 24 | 23.99 | 0.84 | 23.98 | 0.94 | 23.98 | 1.05 | 23.97 | 1.15 | 4 |
| 25 | 4.98 | 0.87 | 24.98 | 0.98 | 24.98 | 1.09 | 24.97 | 1.20 | 5 |
| 26 | 5.98 | 0.91 | 25.98 | 1.02 | 25.98 | 1.13 | 25.97 | 1.25 | 6 |
| $\stackrel{5}{2}$ | 26.98 | 0.94 | 26.98 | 1.06 | 26.97 | 1.18 | 26.97 | 1.30 | 7 |
| 28 | 27.98 | 0.98 | 27.98 | 1.10 | 27.97 | 1.22 | 27.97 | 1.34 | 8 |
| 2 | 28.98 | 1.01 | 28.98 | 1.14 | 28.97 | 1.26 | 28.97 | 1.39 | 29 |
| 30 | 29.98 | 1.05 | 29.98 | 1.18 | 29.97 | 1.31 | 29.97 | 1.44 | 0 |
|  | 30.98 | 1.08 | 30.98 | 1.22 | 30.97 | 1.35 | 30.9 | 1.49 | 31 |
| 32 | 31.98 | 1.12 | 31.98 | 1.26 | 31.97 | 1.40 | 31.96 | 1.5 | 32 |
|  | 32.98 | 1.15 | 32.97 | 1.30 | 32.97 | 1.44 | 32.9 | . 58 | 3 |
|  | 33.98 | 1.19 | 33.97 | 1.39 | 33.97 | 1.48 | 33.96 | 1.63 | 34 |
| 35 | 34.98 | 1.22 | 34.97 | 1.37 | 34.97 | 1.53 | 34.9 | 1.6 | 35 |
|  | 35.98 | 1.26 | 35.97 | 1.41 | 35.97 | 1.57 | 35.9 | 1.73 |  |
| 37 | 6.98 | 1.29 | 36.97 | 1.45 | 36.96 | 1.61 | 36.96 | 1.8 | \% |
| 38 | 37.98 | 1.33 | 37.97 | 1.49 | 37.96 | 1.66 | 37.9 | 1.8 | 3 |
| 39 | 38.98 | 1.36 | 38.97 | 1.53 | 38.96 | 1.70 | 38.96 | 1.87 | 9 |
| 40 | 39.98 | 1.40 | 39.97 | 1.57 | 39.96 | 1.75 | 39.95 | 1.92 |  |
| 41 | 40.98 | 1.43 | 40.97 | 1.61 | 40.96 | 1.77 | 40.95 | 1.97 | 41 |
| 4 | 41.97 | 1.47 | 41.97 | 1.65 | 41.96 | 1.83 | 41.95 | 2.62 | 42 |
| 43 | 42.97 | 1.50 | 42.97 | 1.69 | 42.96 | 1.88 | 42.95 | 2.06 | 33 |
| 44 | 43.97 | 1.54 | 43.97 | 1.73 | 43.96 | 1.92 | 43.95 | 2.11 | 44 |
| 45 | 44.97 | 1.57 | 44.97 | 1.77 | 44.96 | 1.96 | 44.95 | 2.16 | 45 |
| 46 | 45.93 | 1.61 | 45.96 | 1.81 | 45.96 | 2.01 | 45.9 | 2.2 | 46 |
| 47 | 46.97 | 1.64 | 46.96 | 1.85 | 46.96 | 2.05 | 46.9 | 2.25 | 47 |
| 48 | 47.97 | 1.68 | 47.96 | 1.88 | 47.95 | 2.09 | 47.95 | 2.30 | 48 |
| 49 | 48.97 | 1.71 | 48.96 | 1.92 | 48.95 | 2.14 | 48.94 | 2.35 | , |
| 50 | 49.97 | 1.74 | 49.96 | 1.96 | 49.95 | 2.18 | 49.9 | 2.40 | 50 |
|  | Dep. | Lat. | Dep. | Lat | Dep. | La | Dep. |  |  |
|  | 88 |  | $7 \frac{3}{4}$ |  | 87 | eg. |  | eg. |  |

TRAVERSE TABLE.


TRAVERSE TABLE.

| $\stackrel{\substack{0 \\ \multirow{2}{*}{\hline}\\ \hline}}{ }$ | 3 Deg. |  | $3 \frac{1}{4}$ Deg. |  | $3 \frac{1}{2}$ Deg. |  | $3 \frac{3}{4}$ Deg. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L |  | Lat. \|D | ep. |  | Dep. |  | Dep. |  |
|  | 1.00 | 0.0 | 1.00 | 0.06 | 1.00 | 0.0 | 1.00 | . 6 |  |
| 2 | 2.00 | 0.10 | 2.00 | 0.11 | 2.00 | 0.12 | 2.00 | 0.13 |  |
| 3 | 3.00 | 0.16 | 3.00 | 0.17 | 2.99 | 0.18 | 2.99 | 0. |  |
|  | 3.99 | 0.21 | 3.99 | 0.23 | 3.99 | 0.24 | 3.99 | 0.2 |  |
| 5 | 4.99 | 0.26 | 4.99 | 0.28 | 4.99 | 0.31 | 4.99 | 0.3 |  |
| 6 | 5.99 | 0.31 | 5.99 | 0.34 | 5.99 | 0.37 | 5.99 | 0.3 |  |
|  | 6.99 | 0.37 | 6.99 | 0.40 | 6.99 | 0.43 | 6.99 | 0. |  |
|  | 7.99 | 0.42 | 7.99 | 0.45 | 7.99 | 0.49 | 7.98 | 0.5 |  |
| 9 | 8.99 | 0.47 | 8.98 | 0.51 | 8.98 | 0.55 | 8.98 | 0.5 |  |
| 10 | 9.99 | 0.52 | 9.98 | 0.57 | 9.98 | 0.61 | 9.98 | 0.65 | 10 |
| 11 | 10. | 0.58 | 10.9 | 0.6 | 10.98 | 0.67 | 10.9 | 0.72 |  |
| 12 | 11.98 | 0.63 | 11.98 | 0.68 | 11.98 | 0.73 | 11.97 | 0.7 |  |
| 13 | 12.98 | 0.68 | 12.98 | 0.73 | 12.98 | 0.79 | 12.97 | 0.85 | 13 |
| 14 | 13.98 | 0.73 | 13.9 | 0.79 | 13.97 | 0.8 | 13.97 | 0. |  |
| 15 | 14.98 | 0.79 | 14.98 | 0.85 | 14.97 | 0.9 | 14.97 | 0.9 | 5 |
| 16 | 15.98 | 0.84 | 15.97 | 0.91 | 15.97 | 0.98 | 15.97 | 1.0 |  |
| 17 | 16.98 | 0.89 | 16.97 | 0.96 | 16.97 | 1.0 | 16.96 | 1.11 | 1 |
| 18 | 17.98 | 0.94 | 17.97 | 1.02 | 17.9 | 1.10 | 17.9 | 181 |  |
| 19 | 18.98 | 0.99 | 18.97 | 1.08 | 18.96 | 1.16 | 18.96 | 1 |  |
| 20 | 19.97 | 1.05 | 19.97 | 1.13 | 19.96 | 1.22 | 19.96 | 1.31 | 0 |
| 21 | 20. | 1.10 | 20.9 | 1. | 20 | 1.28 | 20 |  |  |
| 22 | 21.97 | 1.15 | 21.96 | 1.25 | 21.96 | 1.34 | 21.9 | , |  |
| 23 | 22.97 | 1.20 | 22.96 | 1.30 | 22:96 | 1.40 | 22.9 | 5 | 23 |
| 24 | 23.97 | 1.26 | 23.96 | 1.36 | 23.9 | 1.47 | 23.95 | 1.57 |  |
| 25 | 24.97 | 1.31 | 24.96 | 1.42 | 24.95 | 1.53 | 24.9 | 1.64 | 25 |
| 26 | 25.96 | 1.36 | 25.96 | 1.47 | 25.9 | 1.59 | 25.9 | 1.7 |  |
| 27 | 26.96 | 1.41 | 26.36 | 1.53 | 26.9 | 1.65 | 26.9 | 1.77 | 27 |
| 28 | 27.96 | 1.47 | 27.95 | 1.59 | 27.9 | 1.71 | 27.9 |  |  |
| 29 | 28.96 | 1.52 | 28.95 | 1.64 | 28.9 | 1.77 | 28.9 | 1.90 | 29 |
| 30 | 29.96 | 1.57 | 29.95 | 1.70 | 29.9 | 1.8 | 29.9 | 1.9 | 30 |
|  | . 96 | 1.62 | 30.95 | 1.76 | 30.9 | 1.89 | 30.9 | , | , |
| 32 | 31.96 | 1.67 | 31.95 | 1.81 | 31.9 | 1.95 | 31.9 | 2.0 |  |
|  | 32.95 | 1.73 | 32.95 | 1.87 | 32.9 | 2.01 | 32.9 | 2.1 |  |
|  | 33.95 | 1.78 | 33.95 | 1.93 | 33.9 | 2.08 | 33.93 | 2.2 |  |
|  | 34.95 | 1.83 | 34.94 | 1.98 | 34.9 | 2.1 | 34.9 | 2. |  |
|  | 35.95 | 1.88 | 35.94 | 2.04 | 35.9 | 2.20 | 35.92 |  |  |
|  | 36.95 | 1.94 | 36.94 | 2.10 | 36.9 | 2.26 | 36.92 | 2.4 | 3 |
| 38 | 37.95 | 1.99 | 37.94 | 2.15 | 37.9 | 2.3 | 37.9 | 2. | 38 |
|  | 38.95 | 2.04 | 38.94 | 2.21 | 38.93 | 2.38 | 38.92 | . |  |
| 40 | 39.95 | 2.09 | 39.94 | 2.27 | 39.93 | 2.4 | 39.91 | . |  |
|  | 40.94 | 2.15 | 40.93 | 2.32 | 40.92 | 2.50 | 40.91 |  |  |
|  | 41.94 | 2.20 | 41.93 | 2.38 | 41.9 | 2.56 | 41.91 | 2.75 |  |
|  | 42.94 | 2.25 | 42.93 | 2.44 | 42.9 | 2.6 | 42.91 | 2.81 |  |
|  | 43.94 | 2.30 | 43.93 | 2.49 | 43.92 | 2.6 | 43.91 | 2.88 |  |
| 45 | 44.94 | 2.36 | '44.93 | 2.55 | 44.92 | 2.75 | 44.90 | 2.94 | 45 |
| 46 | 45.94 | 2.41 | 45.93 | 2.61 | 45.91 | 2.81 | 45.90 | 3.01 |  |
| 47 | 46.94 | 2.46 | 46.92 | 2.66 | 46.91 | 2.87 | 46.90 | 3.07 | 47 |
|  | 47.93 | 2.51 | 47.92 | 2.72 | 47.91 | 2.93 | 47.9 | 3.14 | 48 |
| 49 | 48.93 | 2.56 | 48.92 | 2.78 | 48.91 | 2.9 | 48.9 | 3.20 | 49 |
| 50 | 49.9 | 2. | 49.92 | 2.83 | 49.9 | 3.05 | 49 | 3.27 | 50 |
|  | De | Lat | Dep | Lat. | Dep. Lat. |  | Dep. Lat. |  |  |
|  | 87 |  |  |  |  |  |  |  |  |

TRAVERSE TABLE.


TRAVERSE TABLE.



| $\rightarrow$ | L | Dep. | Lat | Dep. | Lat. | Dep. |  | Dep. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.09 | 1.00 | 0.09 | 1.00 | C. 10 | 0.99 |  |  |
| 2 | 1.99 | 0.17 | 1.99 | 0.18 | 1.99 | 0.19 | 1.99 |  |  |
| 3 | 2.99 | 0.26 | 2.99 | 0.27 | 2.99 | 0.29 | 2.98 | 0.30 |  |
| 4 | 3.98 | 0.35 | 3.98 | 0.37 | 3.98 | 0.38 | 3.98 |  |  |
| 5 | 4.98 | 0.44 | 4.98 | 0.46 | 4.98 | 0.48 | 4.97 | 0. |  |
| 6 | 5.98 | 0.52 | 5.97 | 0.55 | 5.97 | 0.58 | 5.97 | 0.60 |  |
| 7 | 6.97 | 0.61 | 6.97 | 0.64 | 6.97 | 0.67 | 6.96 | 0. |  |
|  | 7.97 | 0.70, | 7.97 | 0.73 | 7.96 | 0.76 | 7.96 | 0.80 |  |
| 9 | 8.97 | 0.78 | 8.96 | 0.82 | 8.96 | 0.86 | 8.95 | 0.90 |  |
| 10 | 9.96 | 0.87 | 9.96 | 0.92 | 9.95 | 0.96 | 9.95 | 1.00 | 0 |
| 11 | 10.96 | 0.96 | 10.95 | 1.01 | 10.95 | 1.05 | 10.94 | 1.10 |  |
| 12 | 11.95 | 1.05 | 11.95 | 1.10 | 11.94 | 1.15 | 11.94 | 1.20 |  |
| 13 | 12.95 | 1.13 | 12.95 | 1.19 | 12.94 | 1.25 | 12.93 | 1.30 | 3 |
|  | 13.95 | 1.22 | 13.94 | 1.28 | 13.94 | 1.34 | 13.93 | 1.40 | 4 |
|  | 14.94 | 1.31 | 14.94 | 1.37 | 14.93 | 1.44 | 14.92 | 1.50 | 5 |
| 16 | 15.94 | 1.39 | 15.93 | 1.46 | 15.93 | 1.53 | 15.92 | 1.60 | 6 |
| 17 | 16.94 | 1.48 | 16.93 | 1.56 | 16.92 | 1.63 | 16.91 | 1.70 | 7 |
|  | 17.93 | 1.57 | 17.92 | 1.65 | 17.92 | 1.73 | 17.91 | 1.80 |  |
|  | 18.93 | 1.66 | 18.92 | 1.74 | 18.91 | 1.82 | 18.90 | 1.90 | 19 |
| 20 | 19.92 | 1.74 | 19.92 | 1.83 | 19.91 | 1.92 | 19.90 | 2.00 |  |
| 21 | 20.92 | 1.83 | 20.91 | 1.92 | 20.9 | 2.01 | 20.89 | 2.10 | 1 |
|  | 21.92 | 1.92 | 21.91 | 2.01 | 21.90 | 2.11 | 21.89 | 2.20 | 2 |
|  | 22.91 | 2.00 | 22.90 | 2.10 | 22.89 | 2.20 | 22.88 | 2.30 |  |
|  | 23.91 | 2.09 | 23.90 | 2.20 | 23.89 | 2.30 | 23.88 | 2.40 | 2 |
|  | 24.90 | 2.18 | 24.90 | 2.29 | 24.88 | . 2.40 | 24.87 | 2.50 | 2 |
|  | 25.90 | 2.27 | 25.89 | 2.38 | 25.88 | 2.49 | 25.87 | 2.60 | 26 |
| 27 | 26.90 | 2.35 | 26.89 | 2.47 | 26.88 | 2.59 | 26.86 | 2.71 | 27 |
|  | 27.89 | 2.44 | 27.88 | 2.56 | 27.87 | 2.68 | 27.86 | 2.81 | 2 |
|  | 28.89 | 2.53 | 28.88 | 2.65 | 28.87 | 2.78 | 28.85 | 2.91 | 29 |
| 30 | 29.89 | 2.61 | 29.87 | 2.75 | 29.86 | 2.88 | 29.85 | 3.01 | 30 |
|  | 30.88 | 2.70 | 30.87 | 2.84 | 30.86 | 2.97 | 30.84 | 3.11 | 31 |
|  | 31.88 | 2.79 | 31.87 | 2.93 | 31.85 | 3.07 | 31.84 | 3.21 | 32 |
| 33 | 32.87 | 2.88 | 32.86 | 3.02 | 32.85 | 3.16 | 32.83 | 3.31 | 33 |
|  | 33.87 | 2.96 | 33.86 | 3.11 | 33.84 | 3.26 | 33.83 | 3.41 | 34 |
|  | 34.87 | 3.05 | 34.85 | 3.20 | 34.84 | 3.35 | 34.82 | 3.51 | 35 |
| 36 | 35.86 | 3.14 | 35.85 | 3.29 | 35.83 | 3.45 | 35.82 | 3.61 | 36 |
|  | 36.86 | 3.22 | 36.84 | 3.39 | 36.83 | 3.55 | 36.81 | 3.71 | 37 |
| 38 | 37.86 | 3.31 | 37.84 | 3.48 | 37.83 | 3.64 | 37.81 | 3.81 | 38 |
| 39 | 38.85 | 3.40 | 38.84 | 3.57 | 38.82 | 3.74 | 38.80 | 3.91 | 39 |
| 40 | 39.85 | 3.49 | 39.83 | 3.66 | 39.82 | 3.83 | 39.80 | 4.01 | - |
|  | 40.8 | 3.57 | 40.83 | 3.75 | 40.81 | 3.93 | 40.79 | 4.11 | 4 |
|  | 41.84 | 3.66 | 41.82 | 3.84 | 41.81 | 4.03 | 41.79 | 4.21 | 42 |
|  | 42.84 | 3.75 | 42.82 | 3.93 | 42.80 | 4.12 | 42.78 | 4.31 | 4 |
| 44 | 43.83 | 3.83 | 43.82 | 4.03 | 43.80 | 4.22 | 43.78 | 4.41 | 4 |
| 45 | 44.83 | 3.92 | 44.81 | 4.12 | 44.79 | 4.31 | 44.77 | 4.51 | 45 |
| 46 | 45.82 | 4.01 | 45.81 | 4.21 | 45.79 | 4.41 | 45.77 | 4.61 | 46 |
| 47 | 46.82 | 4.10 | 46.80 | 4.30 | 46.78 | 4.50 | 46.76 | 4.71 | 47 |
| 48 | 47.82 | 4.18 | 47.80 | 4.39 | 47.78 | 4.60 | 47.76 | 4.81 | 48 |
|  | 48.81 | 4.27 | 48.79 | 4.48 | 48.77 | 4.70 | 48.75 | 4.91 | 49 |
| 50 | 49.81 | 4.36 | 49.79 | 4.58 | 49.77 | 4.79 | 49.75 | 5.01 | 50 |
|  | Dep. | Lat. | Dep. | Lat. | Dep | Lat. | Dep. | Lat. |  |
|  |  |  |  |  |  |  |  |  |  |

TRAVERSE TABLE.

| + | 5 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. |  |
| 51 | 50.81 | 4.4 | 50.79 | 4.67 | 50.77 | 4.89 | 50.74 |  |  |
| 52 | 51.80 | 4.53 | 51.78 | 4.76 | 51.76 | 4.98 | 51.74 | 5.21 | 52 |
| 53 | 52.80 | 4.62 | 52.78 | 4.85 | 52.76 | 5.08 | 52.73 | 5.31 | 53 |
| 54 | 53.79 | 4.71 | 53.77 | 4.94 | 53.75 | 5.18 | 53.73 | 5.41 | 5 |
| 55 | 54.79 | 4.79 | 54.77 | 5.03 | 54.75 | 5.27 | 54.72 | 5.51 | 55 |
| 56 | 55.79 | 4.88 | 55.77 | 5.12 | 55.74 | 5.37 | 55.72 | 5.61 | 56 |
| 57 | 56.78 | 4.97 | 56.76 | 5.22 | 56.74 | 5.46 | 56.71 | 5.71 | 57 |
| 58 | 57.78 | 5.06 | 57.76 | 5.31 | 57.73 | 5.56 | 57.71 | 5.81 | 58 |
| 59 | 58.78 | 5.14 | 58.75 | 5.40 | 58.73 | 5.65 | 58.70 | 5.91 | 59 |
|  | 59.77 | 5.23 | 59.75 | 5.49 | 59.72 | 5.75 | 59.70 | 6.01 | a |
| 61 | 60.77 | 5.32 | 60.74 | 5.58 | 60.72 | 5.85 | 60. |  | 1 |
| 62 | 61.76 | 5.40 | 61.74 | 5.67 | 61.71 | 5.94 | 61.69 | 6.21 |  |
|  | 62.76 | 5.49 | 62.74 | 5.76 | 62.71 | 6.04 | 62.68 | 6.31 | 63 |
|  | 63.76 | 5.58 | 63.73 | 5.86 | 63.71 | 6.13 | 63.68 | 6.41 | 4 |
| 65 | 64.75 | 5.67 | 64.73 | 5.95 | 64.70 | 6.23 | 64.67 | 6.51 | 5 |
| 66 | 65.75 | 5.75 | 65.72 | 6.04 | 65.70 | 6.33 | 65.67 | 6.61 | 6 |
|  | 66.75 | 5.84 | 66.72 | 6.13 | 66.69 | 6.42 | 66.66 | 6.71 | 67 |
| 68 | 67.74 | 5.93 | 67.71 | 6.22 | 67.69 | 6.52 | 67. | 6.81 | 68 |
|  | 68.74 | 6.01 | 68.71 | 6.31 | 68.68 | 6.61 | 68.6 | 6.91 | 68 |
| 70 | 69.73 | 6.10 | 69.71 | 6.41 | 69.68 | 6.71 | 69.6 | 7.0 | 70 |
|  | 70.73 | 6.19 | 70 | 6.50 | 70 | 6.81 | 70. | 11 | 1 |
| 72 | 71.73 | 6.28 | 71.70 | 6.59 | 71.67 | 6.90 | 71.6 | 7.21 | 2 |
| $\begin{aligned} & 72 \\ & 73 \end{aligned}$ | 72.72 | 6.36 | 72.69 | 6.68 | 72.66 | 7.00 | 72.6 | 7.31 | 73 |
| $74$ | 73.72 | 6.45 | 73.69 | 6.77 | 73.6 | 7.09 | 73.6 | 7.41 | 74 |
|  | 74.71 | 6.54 | 74.69 | 6.86 | 74. | 7.19 | 74.62 | 7.51 | 75 |
| 75 | 75.71 | 6.62 | 75.68 | 6.95 | 75.6 | 7.2 | 75.6 | 7.61 | 76 |
| 77 | 76.71 | 6.71 | 76.68 | 7.05 | 76.6 | 7.38 | 76.6 | 7.71 | 77 |
|  | 77.70 | 6.80 | 77.67 | 7.14 | 77.6 | 7.48 | 77.6 | 7.81 | 78 |
|  | 78.70 | 6.89 | 78.67 | 7.23 | 78.64 | 7.57 | 78.60 | 7.91 | 79 |
|  | 79.70 | 6.97 | 79.66 | 7.32 | 79.63 | 7.67 | 79.60 | 8.0 | s0 |
|  | 80.69 | 7.06 | 80.66 | 7.41 | 80.63 | 7.76 | 80.59 | 8.12 | 8 |
| $\begin{gathered} 81 \\ 82 \end{gathered}$ | 81.69 | 7.15 | 81.66 | 7.50 | 81.62 | 7.86 | 81.59 | 8.22 |  |
| 83 84 | \$2.68 | 7.23 | 82.65 | 7.59 | 82.62 | 7.96 | 82.5 | 8.3 | 83 |
|  | 83.68 | 7.32 | 83.65 | 7.69 | 83.61 | 8.05 | 83.5 | 8.4 |  |
| 85 | 84.68 | 7.41 | 84.64 | 7.78 | 84.6 | 8.15 | 84.57 | 8.5 |  |
|  | 85.67 | 7.50 | 85.64 | 7.87 | 35.60 | 8.24 | 85.5 | 8.62 | 86 |
| 87 | 86.67 | 7.58 | 86.64 | 7.96 | 86.60 | 8.34 | 86.56 | 8.7 | 87 |
|  | 87.67 | 7.67 | 87.63 | 8.05 | 87.5 | 8.43 | 87.5 | 8.8 | 88 |
| $\begin{aligned} & 89 \\ & 90 \end{aligned}$ | 88.66 | 7.76 | 88.63 | 8.14 | 88.5 | 8.53 | 88.55 | 8.92 | 89 |
|  | 89.66 | 7.84 | 89.62 | 8. | 89 | 8. | 89.55 | 9.02 | 90 |
|  | 90.65 | 7.93 | 90.62 | 8.33 | 90.58 | 8.72 | 90.5 | 9. | 91 |
| $\begin{aligned} & 91 \\ & 92 \end{aligned}$ | 91.65 | 8.02 | 91.61 | 8.42 | 91.5 | 8.82 | 91.54 | 9.22 | 92 |
| 9394 | 92.65 | 8.11 | 92.61 | 8.51 | 92.5 | 8.91 | 92.53 | 9.3 | 93 |
|  | 93.64 | 8.19 | 93.61 | 8.60 | 93.5 | 9.01 | 93.5 | 9.42 | 94 |
| 9596 | 94.6 | 8.28 | 94.60 | 8.69 | 94.5 | 9.11 | 94.5 | 9.52 |  |
|  | 95.63 | 8.37 | 95.60 | 8.78 | 95.56 | 9.20 | 95.5 | 9.62 | 96 |
|  | 96.63 | 8.45 | 96.59 | 8.88 | 96.5 | 9.30 | 96.5 | 9.72 | 97 |
|  | 97.63 | 8.54 | 97.59 | 8.97 | 97.5 | 9.39 | 97.5 | 9.8 | 98 |
| 9899100 | 98.6 | 8.63 | 98.59 | 9.06 | 98. | 9.49 | 98.50 | 9.92 | 99 |
|  | 99. | 8.72 | 99.58 | 9.15 | 99 | 9.5 | 99.50 |  |  |
| $\stackrel{\ddot{2}}{\stackrel{2}{2}}$ | Dep | Lat | Dep | Lat. | Dep | Lat. |  |  |  |
|  |  |  |  |  |  |  |  |  |  |

TRAVERSE TABLE.

| E | 6 Deg. |  | $6 \frac{1}{4}$ Deg. |  | $6 \frac{1}{2}$ Deg. |  | $6 \frac{3}{4}$ Deg. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. | Lat. | Dep. | $L$ | Dep. |  | ep. |  |
| 1 | 0.99 | 0.10 | 0.99 | 0.11 | 0.99 | 0.11 | 0.99 | 0.12 |  |
| 2 | 1.99 | 0.21 | 1.99 | 0.22 | 1.99 | 0.23 | 1.99 | 0.24 | 2 |
|  | 2.98 | 0.31 | 2.98 | 0.33 | 2.98 | 0.34 | 2.98 | 0.35 |  |
| 4 | 3.98 | 0.41 | 3.98 | 0.44 | 3.97 | 0.45 | 3.97 | 0.47 |  |
| 5 | 4.97 | 0.52 | 4.97 | 0.54 | 4.97 | 0.57 | 4.97 | 0.59 |  |
| 6 | 5.97 | 0.63 | 5.96 | 0.65 | 5.96 | 0.68 | 5.96 | 0.71 |  |
| 7 | 6.96 | 0.73 | 6.96 | 0.76 | 6.96 | 0.79 | 6.95 | 0.82 |  |
| 8 | 7.96 | 0.84 | 7.95 | 0.87 | 7.95 | 0.91 | 7.94 | 0.94 | 8 |
| 9 | 8.95 | 0.94 | 8.95 | 0.98 | 8.94 | 1.02 | 8.94 | 1.06 |  |
| 10 | 9.95 | 1.05 | 9.94 | 1.09 | 9.94 | 1.13 | 9.93 | 1.18 | 10 |
| 11 | 10.94 | 1.15 | 10.93 | 1.20 | 10.93 | 1.25 | 10.92 | 1.29 | 11 |
| 12 | 11.93 | 1.25 | 11.93 | 1.31 | 11.92 | 1.36 | 11.92 | 1.41 | 12 |
| 13 | 12.93 | 1.36 | 12.92 | 1.42 | 12.92 | 1.47 | 12.91 | 1.53 | 13 |
| 14 | 13.92 | 1.46 | 13.92 | 1.52 | 13.91 | 1.59 | 13.90 | 1.65 | 14 |
| 15 | 14.92 | 1.57 | 14.91 | 1.63 | 14.90 | 1.70 | 14.90 | 1.76 | 15 |
| 16 | 15.91 | 1.67 | 15.90 | 1.74 | 15.90 | 1.81 | 15.89 | 1.88 | 16 |
| 17 | 16.91 | 1.78 | 16.90 | 1.85 | 16.89 | 1.92 | 16.88 | 2.00 | 17 |
| 18 | 17.90 | 1.88 | 17.89 | 1.96 | 17.88 | 2.04 | 17.88 | 2.12 | 18 |
| 19 | 18.90 | 1.99 | 18.89 | 2.07 | 18.88 | 2.15 | 18.87 | 2.23 | 19 |
| 20 | 19.89 | 2.09 | 19.88 | 2.18 | 19.87 | ,2.26 | 19.86 | 2.35 | 20 |
| 21 | 20 | 2.20 | 20.88 | 2.29 | 20 | 2.38 | 20.85 |  | 21 |
| 22 | 21.88 | 2.30 | 21.87 | 2.40 | 21.86 | 2.49 | 21.85 | 2.59 | 2 |
| 23 | 22.87 | 2.40 | 22.86 | 2.50 | 22.85 | 2.60 | 22.84 | 2.70 | 23 |
| 24 | 23.87 | 2.51 | 23.86 | 2.61 | 23.85 | 2.72 | 23.83 | 2.82 | 2 |
| 25 | 24.86 | 2.61 | 24.85 | 2.72 | 24.84 | 2.83 | 24.83 | 2.94 | 2 |
| 26 | 25.86 | 2.72 | 25.85 | 2.83 | 25.83 | 2.94 | 25.82 | 3.06 | 26 |
| 27 | 26.85 | 2.82 | 26.84 | 2.94 | 26.83 | 3.06 | 26.81 | 3.17 | 27 |
| 28 | 27.85 | 2.93 | 27.83 | 3.05 | 27.82 | 3.17 | 27.81 | 3.29 | 26 |
| 29 | 28.84 | 3.03 | 28.83 | 3.16 | 28.81 | 3.28 | 28.80 | 3.41 | 29 |
| 30 | 29.84 | 3.14 | 29.82 | 3.27 | 29.81 | 3.40 | 29.79 | 3.53 | 0 |
| 31 |  | 3.24 | 30.82 | 3.37 | 30.80 | 3.51 | 30.79 |  |  |
| 32 | 31.82 | 3.34 | 31.81 | 3.48 | 31.79 | 3.62 | 31.78 | 3.76 | 32 |
| 33 | 32.82 | 3.45 | 32.80 | 3.59 | 32.79 | 3.74 | 32.77 | 3.88 |  |
| 34 | 33.81 | 3.55 | 33.80 | 3.70 | 33.78 | 3.85 | 33.76 | 4.00 | 3 |
| 35 | 34.81 | 3.66 | 34.79 | 3.81 | 34.78 | 3.96 | 34.76 | 4.11 | 35 |
| 36 | 35.80 | 3.76 | 35.79 | 3.92 | 35.77 | 4.08 | 35.75 | 4.23 | 36 |
| 37 | 36.80 | 3.87 | 36.78 | 4.03 | 36.76 | 4.19 | 36.75 | 4.35 |  |
| 38 | 37.79 | 3.97 | 37.77 | 4.14 | 37.76 | 4.30 | 37.74 | 4.47 | 38 |
| 39 | 38.79 | 4.08 | 38.77 | 4.25 | 38.75 | 4.41 | 38.73 | 4.58 | 30 |
| 40 | 39.78 | 4.18 | 39.76 | 4.35 | 39.74 | 4.53 | 39.72 | 4.70 | 40 |
| 41 | 40.78 | 4.29 | 40.76 | 4.46 | 40.74 | 4.64 | 40.72 | 4.82 | 41 |
| 42 | 41.77 | 4.39 | 41.75 | 4.57 | 41.73 | 4.76 | 41.71 | 4.94 | 49 |
| 43 | 42.76 | 4.49 | 42.74 | 4.68 | 42.72 | 4.87 | 42.70 | 5.05 | 42 |
| 44 | 43.76 | 4.60 | 43.74 | 4.79 | 43.72 | 4.98 | 43.70 | 5.17 | 41 |
| 45 | 44.75 | 4.70 | 44.73 | 4.90 | 44.71 | 5.09 | 44.69 | 5.29 | 45 |
| 46 | 45.75 | 4.81 | 45.73 | 5.01 | 45.70 | 5.21 | 45.68 | 5.41 | 46 |
| 47 | 46.74 | 4.91 | 46.72 | 5.12 | 46.70 | 5.32 | 46.67 | 5.52 | 42 |
| 48 | 47.74 | 5.02 | 47.71 | 5.23 | 47.69 | 5.43 | 47.67 | 5.64 | 48 |
| 49 | 48.73 | 5.12 | 48.71 | 5.34 | 48.69 | 5.55 | 48.66 | 5.76 | 49 |
| 50 | 49.73 | 5.23 | 49.70 | 5.44 | 49.68 | 5.66 | 49.65 | 5.88 | 50 |
|  | Dep. | Lat. | Dep | Lat. | Dep. | Lat. | Dep. | Lat. |  |
|  |  |  |  |  |  |  |  |  |  |

TRAVERSE TABLE. 51

| $\frac{8}{5}$ | 6 Deg . |  | 6 $\frac{1}{4}$ Deg. $6 \frac{1}{2} \mathrm{Deg}$. |  |  |  | $6 \frac{3}{4}$ Deg. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep | Lat. | Dep. | L | Dep. |  |  |  |
| 51 |  |  |  |  | 50.6 | 5.77 |  |  |  |
| 52 | 51.72 | 5.44 | 51.69 | 5.66 | 51.67 | 5.89 | 51.64 |  | 52 |
| 53 | 52.71 | 5.54 | 52.68 | 5.77 | 52.66 | 6.00 | 52.63 |  | 3 |
| 54 | 53.70 | 5.64 | 53.68 | 5.88 | 53.65 | 6.11 | 53.63 | 6. |  |
| 55 | 54.70 | 5.75 | 54.67 | 5.99 | 54.65 | 6.23 | 54.62 |  | 55 |
| 56 | 55.69 | 5.85 | 55.67 | 6.10 | 55.64 | 6.34 | 55.61 | 6. |  |
| 57 | 56.69 | 5.96 | 56.6 | 6.21 | 56.63 | 6.45 | 56.60 | 6. | 57 |
| 58 | 57.68 | 6.06 | 57.66 | 6.31 | 57.63 | 6.57 | 57.60 |  | 5 |
| 59 | 58.68 | 6.17 | 58.65 | 6.42 | 58.62 | 6.68 | 58.59 |  |  |
| 60 | 59.67 | 6.27 | 59.64 | 6.53 | 59.61 | 6.79 | 59.58 | 7 | 60 |
| 61 |  |  |  |  | 60.61 |  |  |  |  |
| 62 | 61.66 | 6.48 | 61.63 | 6.75 | 61.60 | 7.02 | 61.57 | 7. |  |
| 63 | 62.65 | 6.59 | 62.63 | 6.86 | 62.60 | 7.13 | 62.56 | 7. |  |
| 64 | 63.65 | 6.69 | 63.62 | 6.97 | 63.59 | 7.25 | 63.56 | 7. |  |
| 65 | 64.64 | 6.79 | 64.61 | 7.08 | 64.58 | 7.36 | 64.55 | 7.6 | 65 |
| 66 | 65.64 | 6.90 | 65.61 | 7.19 | 65.58 | 7.47 | 65.54 | 7. |  |
| 67 | 66.63 | 7.00 | 66.60 | 7.29 | 66.57 | 7.58 | 66.54 | 7.8 |  |
| 68 | 67.63 | 7.11 | 67.60 | 7.40 | 67.56 | 7.70 | 67.53 | 7. |  |
| 69 | 68.62 | 7.21 | 68.59 | 7.51 | 68.56 | 7.81 | 68.52 |  |  |
| 70 | 69.62 | 7.32 | 69.58 | 7.62 | 69.55 | 7.92 | 69.51 | 8. |  |
| 7 |  | . |  | 7.73 |  |  |  |  |  |
| 72 |  | 7.53 | 71.57 | 7.84 | 71. | 8.15 | 71.50 |  |  |
| 73 | 72.60 | 7.63 | 72.57 | 7.95 | 72.53 | 8.26 | 72. | 8.5 |  |
| 74 | 73.59 | 7.74 | 73.56 | 8.06 | 73.52 | 8.38 | 73.49 | 8. |  |
| 75 | 74.59 | 7.84 | 74.55 | 8.17 | 74.52 | 8.49 | 74.48 | 8. | - |
| 76 | 75.58 | 7.94 | 75.55 | 8.27 | 75.51 | 8.60 | 75. | 8.9 | 76 |
| 77 | 76.58 | 8.05 | 76.54 | 8.38 | 76.51 | 8.72 | 76 | 9. | 77 |
| 7 | 77.57 | 8.15 | 77.54 | 8.49 | 77.50 | 8. | 77 | 9.1 | 778 |
| 79 | 78.57 | 8.26 | 78.53 | 8.60 | 78.49 | 8. |  | 9. | 79 |
| 80 | 79.56 | 8.36 | 79.53 | 8.71 | 79.49 | 9.06 |  |  |  |
| 81 |  |  |  | 8.82 |  | 9.17 |  |  | 1 |
| 8 | 81.55 | 8.57 | 81.51 | 8.93 | 81. | 9.28 | 81. |  |  |
| 83 | 82.55 | 8.68 | 82.51 | 9.04 | 82.47 | 9.40 | 82.42 | 9. | 83 |
| 84 | 83.54 | 8.78 | 83.50 | 9.14 | 83.46 | 9.51 | 83. | 9. |  |
| 8 | 84.53 | 8.88 | 84.50 | 9.25 |  | 9.62 | 4.41 |  |  |
| 86 | 85.53 | 8.99 | 85.49 | 9.36 | 85.45 | 9.74 | 85.40 | 10. |  |
| 87 | 86.52 | 9.09 | 86.48 | 9.47 | 86 | 9.85 | 86.40 | 10. |  |
| 88 | 87.52 | 9.20 | 87.48 | 9.58 | 87 | 9.96 | 87.39 | 10. |  |
| 89 | 88.51 | 9.30 | 88.47 | 9.69 | 88.43 | 10.08 | 88.38 |  | 相 |
| 90 | 89.51 | 9.41 | 89. | 9.8 |  |  | 89.38 |  | 890 |
| 9 |  | 9.51 | 90.4 | 9.91 | 90 | 10.30 | 90.37 |  |  |
| 92 | 91.50 | 9.62 | 91.45 | 0.02 | 91.41 | 10.41 | 91.36 | 10. |  |
| 93 | 92.49 | 9.72 | 92.4 | 10.12 | 92.40 | 10.53 | 92.36 | 10. |  |
| 9 | 93.49 | 9.83 | 93 | 0.23 | 93.40 | 10.64 | 93.35 |  |  |
| 95 | 94.48 | 9.93 | 94.44 | 10.34 | 94.39 | 10.75 | 94.34 | 11. | 795 |
| 96 | 95.47 | 10.03 | 95.43 | 10.45 | 95.38 | 10.87 | 95.33 | 11. | 8.96 |
| 9 | 96.47 | 10.14 | 96.42 | 10.56 | 96.38 | 10.98 | 96.33 |  |  |
| 98 | 97.46 | 10.24 | 97.42 | 10.67 | 97.37 | 11.09 | 97.32 |  |  |
| 99 |  | 10.35 | 98 | 10.78 | 98.36 | 11.21 | 98:31 |  |  |
| 100 |  | 10.45 |  | 10.89 | 99.36 | 11.32 | 99.31 | 11.75 | 00 |
|  |  | L |  | Lat. |  |  |  |  |  |

TRAVERSE TABLE.

| $\underset{\substack{e \\ \square}}{ }$ |  |  |  |  |  |  |  | eg. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep | Lat | Dep. | Lat | Dep. | Lat. | Dep. |  |
|  | 0.99 | 0.12 | 0.99 | 0.13 | 0.99 | 0.13 | 0.99 | 0.13 |  |
|  | 1.99 | 0.24 | 1.98 | 0.25 | 1.98 | 0.26 | 1.98 | 0. |  |
| 3 | 2.98 | 0.37 | 2.98 | 0.38 | 2.97 | 0.39 | 2.97 | 0.40 |  |
|  | 3.97 | 0.49 | 3.97 | 0.50 | 3.97 | 0.52 | 3.96 | 0.5 |  |
|  | 4.96 | 0.61 | 4.96 | 0.63 | 4.96 | 0.65 | 4.95 | 0.67 |  |
| 6 | 5.96 | 0.73 | 5.95 | 0.76 | 5.95 | 0.78 | 5.95 | 0.81 |  |
| 7 | 6.95 | 0.85 | 6.94 | 0.88 | 6.94 | 0.91 | 6.94 | 0.94 |  |
| 8 | 7.94 8.93 | 0.97 | 7.94 8.93 | 1.01 | 7.93 | 1.04 | 7.93 8.92 | , |  |
| 10 | 9.93 | 1.22 | 9.92 | 1.26 | 8.92 9.91 | 1.171 | 8.92 9.91 | 1.21 | 10 |
| 11 | 10.92 | 1.34 | 10.91 | 1.39 | 10.91 | 1.44 | 10.90 |  | 11 |
| 12 | 11.91 | 1.46 | 11.90 | 1.51 | 11.90 | 1.57 | 11.8 | 1.62 | 2 |
|  | 12.90 | 1.58 | 12.90 | 1.64 | 12.89 | 1.70 | 12.8 | 1.75 | 仡 |
| $\left.\begin{array}{l} 13 \\ 14 \end{array}\right]$ | 13.90 | 1.71 | 13.89 | 1.77 | 13.88 | 1.83 | 13.87 | . 5 |  |
| 15 | 14.89 | 1.83 | 14.88 | 1.89 | 14.87 | 1.9 | 14.86 | 2.02 | 5 |
|  | 15.88 | 1.95 | 15.87 | 2.02 | 15.86 | 2.09 | 15.85 | 2.16 | 16 |
| 17 | 16.87 | 2.07 | 16.86 | 2.15 | 16.85 | 2.22 | 16.84 |  | 7 |
| 18 | 17.87 | 2.19 | 17.86 | 2.27 | 17.85 | 2.35 | 17.84 | 2.43 | 18 |
|  | 18.86 | 2.32 | 18.85 | 2.40 | 18.84 | 2.48 | 18.83 | 2.56 | 19 |
| 20 | 19.85 | 2.44 | 19.84 | 2.52 | 19.83 | 2.61 | 19.82 | 2.70 |  |
| 21 | 20.84 | 2.56 | 20.83 | 2.65 | 20.82 | 2.74 | 20.81 | 83 | 21 |
| 2223 | 21.84 | 2.68 | 21.82 | 2.78 | 21.81 | 2.87 | 21.80 | 2.97 | 2 |
|  | 22.83 | 2.80 | 22.82 | 2.90 | 22.80 | 3.00 | 22.79 | 3.10 | 23 |
| 23 | 23.82 | 2.92 | 23.81 | 3.03 | 23.79 | 3.13 | 23.7 | 3.24 | 24 |
| 25 | 24.81 | 3.05 | 24.80 | 3.15 | 24.79 | 3.26 | 24.77 | 3.37 |  |
| $\begin{aligned} & 25 \\ & 26 \end{aligned}$ | 25.81 | 3.17 | 25.79 | 3.28 | 25.78 | 3.39 | 25.76 | 3.51 | 26 |
| $\begin{aligned} & 26 \\ & .27 \end{aligned}$ | 26.80 | 3.29 | 26.78 | 3.41 | 26.77 | 3.52 | 26.75 | 3.64 | 27 |
| 27 | 27.79 | 3.41 | 27.78 | 3.53 | 27.76 | 3.6 | 27.74 | 3.78 | 28 |
| $\begin{aligned} & 29 \\ & 30 \end{aligned}$ | 28.78 | 3.53 | 28.77 | 3.66 | 28.75 | 3.79 | 28.74 | 3.91 |  |
|  | 29.78 | 3.66 | 29.76 | 3.79 | 29.74 | 3.92 | 29.73 | 4.0 |  |
|  | 30.77 | 3.78 | 30.75 | 3.91 | 30.73 | 4.05 | 30. |  | 1 |
| $\begin{aligned} & 31 \\ & 32 \end{aligned}$ | 31.76 | 3.90 | 31.74 | 4.04 | 31.73 | 4.18 | 31.71 | 4.32 |  |
| $\begin{aligned} & 32 \\ & 33 \end{aligned}$ | 32.75 | 4.02 | 32.74 | 4.16 | 32.72 | 4.31 | 32.70 | 4.45 |  |
| $\begin{aligned} & 33 \\ & 34 \end{aligned}$ | 33.75 | 4.14 | 33.73 | 4.29 | 33.71 | 4.44 | 33.6 | 4.58 | 34 |
| $\begin{aligned} & 34 \\ & 35 \\ & 25 \end{aligned}$ | 34.74 | 4.27 | 34.72 | 4.42 | 34.70 | 4.57 | 34.6 | 4.72 | 35 |
|  | 35.73 | 4.39 | 35.71 | 4.54 | 35.69 | 4.70 | 35.67 | 4.85 | 36 |
| $37$ | 36.72 | 4.51 | 36.70 | 4.67 | 36.68 | 4.8 | 36.66 | 4.99 |  |
| $\begin{aligned} & 38 \\ & 39 \end{aligned}$ | 37.72 | 4.63 | 37.70 | 4.80 | 37.67 | 4.96 | 37.65 | 5.12 | 38 |
|  | 38.71 | 4.75 | 38.69 | 4.92 | 38.67 | 5.09 | 38.64 | 5.26 | 9 |
| 40 | 39.70 | 4.87 | 39.68 | 5.0 | 39.6 | 5.22 | 39.63 | 5.3 | - |
| $41$ |  | 5.00 | 40.67 | 5.17 | 40.65 | 5.35 | 40. | 5 5 | 41 |
|  | 41.69 | 5.12 | 41.66 | 5.30 | 41.64 | 5.48 | 41.6 | 5.6 | 42 |
|  | 42.68 | 5.24 | 42.66 | 5.43 | 42.63 | 5.61 | 42.61 | 5.80 | 43 |
| $\begin{aligned} & 43 \\ & 44 \end{aligned}$ | 43.67 | 5.36 | 43.65 | 5.55 | 43.62 | 5.74 | 43.60 | 5.93 | 44 |
| 444546 | 44.67 | 5.48 | 44.64 | 5.68 | 44.62 | 5.87 | 44.59 | 6.07 |  |
|  | 45.66 | 5.61 | 45.63 | 5.81 | 45.61 | 6.00 | 45.58 | 6.20 | 析 |
| 46 47 | 46.65 | 5.73 | 46.62 | 5.93 | 46.60 | 6.13 | 46.57 | 6.34 | 47 |
| $\begin{aligned} & 47 \\ & 48 \\ & 49 \end{aligned}$ | 47.64 | 5.85 | 47.62 | 6.06 | 47.59 | 6.27 | 47.5 | 6.47 |  |
|  | 48.63 | 5.97 | 48.61 | 6.18 | 48.58 | 6.40 | 48.5 | 6.61 | 49 |
| 49 50 | 49.63 | 6.09 | 49.60 | 6.31 | 49.57 | 6.53 | 49.54 | 6.74 | 50 |
|  |  |  | Dep | Lat. |  | t. |  |  |  |
|  | 83 | Deg. | 82 | eg. | 82 | Deg. |  |  |  |



TRAVERSE TABLE.


|  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | p. | Lat. | ep. | La | Dep. | Lat. |  |  |
|  | 50.50 | 7.10 | 50.47 | 7.32 | 50.44 | 7.54 | 50.41 | , | 1 |
|  | 51.49 | 7.24 | 51.46 | 7.46 | 51.43 | 7.69 | 1. | 7.91 |  |
|  | 52.48 | 7.38 | 52.45 | 7.61 | 52.4 | 7.83 | 52.38 | 8.06 | 53 |
|  | 53.47 | 7.52 | 53.44 | 7.75 | 53.41 | 7.98 | 53.37 | 8.21 | 4 |
|  | 54.46 | 7.65 | 54.43 | 7.89 | 54.40 | 8.13 | 54.36 | 8.37 | 55 |
|  | 55.46 | 7.79 | 55.42 | 8.04 | 55.38 | 8.28 | 55.35 | 8.5 | 56 |
|  | 56.45 | 7.93 | 56.41 | 8.18 | 56.37 | 8.43 | 56.34 | 8.6 | 57 |
|  | 57.44 | 8.07 | 57.40 | 8.32 | 57.36 | 8.57 | 57.32 | 8.8 | 8 |
|  | 58.43 | 8.21 | 58.39 | 8.47 | 58.35 | 8.72 | 58.31 | 8.9 | 9 |
|  | 59.42 | 8.35 | 59.38 | 8.61 | 59.34 | 8.87 | 59.30 | 9.13 | 0 |
|  | 60.41 | 8.49 | 60.37 | 8.7 | 60.3 | 9.02 | 60 |  | 1 |
|  | 61.40 | 8.63 | 61.36 | 8.90 | 61.3 | 9.16 | 61. |  |  |
|  | 62.39 | 8.77 | 62.35 | 9.04 | 62.31 | 9.31 | 62.27 | 9.5 | 63 |
|  | 63.38 | 8.91 | 63.34 | 9.18 | 63.30 | 9.46 | 63.26 | 9.7 | 64 |
|  | 64.37 | 9.05 | 64.33 | 9.33 | 64.2 | 9.61 | 64.24 | 9.8 | 5 |
|  | 65.36 | 9.19 | 65.32 | 9.47 | 65.2 | 9.76 | 65.23 | 0.04 | 6 |
|  | 66.35 | 9.32 | 66.31 | 9.61 | 66.26 | 9.90 | 66.2 | 10.19 | 7 |
|  | 67.34 | 9.46 | 67.30 | 9.76 | 67.25 | 10.05 | 67.2 | 0.34 |  |
|  | 68.33 | 9.60 | 68.29 | 9.90 | 68.24 | 0.20 | 68 |  |  |
| 70 | 69.32 | 9.74 | 69.28 | 10.04 | 69.23 | 10.35 | 69 |  | 0 |
|  | 70.31 | 9.88 | 70. | 10. | 70.22 | 10.49 | 70.17 |  |  |
|  | 71.30 | 10.02 | 71.25 | 10.33 | 71.21 | 10.64 | 71.1 |  | 2 |
|  | 72.29 | 10.16 | 72.24 | 10.47 | 72.20 | 10.79 | 72.1 |  |  |
|  | 73.28 | 10.30 | 73.23 | 10.62 | 73.19 | 10.94 |  |  | 74 |
|  | 74.27 | 10.44 | 74.22 | 10.76 | 74.18 | 11.09 | 74.1 |  | 5 |
|  | 75.2 | 10.58 | 75.21 | 10.91 | 75.17 | 11.23 | 75.12 |  |  |
|  | 76.2 | 10.72 | 76.20 | 11.05 | 76.15 | 11.38 | 76.10 | 1.71 |  |
|  | 77.24 | 0.86 | 77.19 | 11.19 | 77.14 | 11.53 | 77.09 |  |  |
|  | 78.23 | 0.99 | 78.18 | 11.34 | 78.13 | 11.68 | 78.08 |  | 9 |
| 80 | 79.22 | 11.13 | 79.17 | 11.48 | 79.12 | 11.82 | 79. |  |  |
|  | 80 | 11.27 | 80.16 | 11.62 | 80.11 | 11.97 | 80.0 | 12 | 81 |
|  |  | 1.41 | 81.15 | 1.77 | 81.10 | 12.12 | 81.05 |  | 2 |
|  | 82.19 | 11.55 | 82.1 | 1.91 | 82.09 | 12.27 | 82.03 |  | 3 |
|  | 83.18 | 1.69 | 83.13 | 12.05 | 83.08 | 12.42 | 83.02 | 12.78 | 84 |
|  | 84.17 | 1.83 | 84.12 | 12.20 | 84.07 | 12.56 | 84.01 |  | 85 |
|  | 85.16 | 1.97 | 85.11 | 2.34 | 85.06 | 12.71 | 85.00 | . |  |
|  | 86,15 | 12.11 | 86.10 | 12.48 | 86.04 | 12.86 | 85.99 | 13.23 | 7 |
| 888990 | 87.14 | 12.25 | 87.09 | 12.63 | 87.03 | 13.01 | 86.98 | 13.39 |  |
|  | 88.13 | 12.39 | 88.08 | 12.77 | 88.02 | 13.16 | 87.96 | 13.54 |  |
|  | 89.12 | 12.53 | 89,07 | 12.9 | 89.01 | 13.3 |  |  |  |
|  | 90.11 | 12.66 | 90.06 | 13.06 | 90.00 | 13.45 | 89.9 |  | 1 |
|  | 91.10 | 12.80 | 91.05 | 13.20 | 90.99 | 13.60 | 90. |  |  |
|  | 2.09 | 12.94 | 92.0 | 13.34 | 91.98 | 13.75 | 91.92 | 1 |  |
|  | 93.09 | 13.08 | 93.03 | 13.49 | 92.97 | 13.89 | 92.91 | 4.30 |  |
|  | 94.08 | 13.29 | 94.02 | 13.63 | 93.96 | 14.04 | 93.89 | 4.45 |  |
|  | 95.07 | 13.36 | 95.01 | 33.78 | 94.95 | 14.19 | 94.88 | 4.60 | 96 |
|  | 96.06 | 13.50 | 96.00 | 13.92 | 95.93 | 14.34 | 95.8 | 4.7 | 97 |
|  | 97.05 | 13.64 | 96.99 | 14.06 | 96.92 | 14.49 | 96.8 | 14.91 |  |
| 9899100 | 98.04 | 13.78 | 97.98 | 4.21 | 97.91 | 14.6 |  |  | 99 |
|  | 99 | 13.92 | 98 | 4. | 98.90 | 14. |  |  |  |
| 4 |  |  | D |  | D | Lat: |  |  |  |
|  |  |  |  |  |  |  |  |  |  |

TRAVERSE TABLE.


| $\begin{aligned} & ? \\ & ? . \\ & ? \\ & \hline \end{aligned}$ | 9 D | Deg. |  | eg. |  |  |  | eg. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. | Lat. | Dep. | La | Dep. | La | p. | $\stackrel{+}{4}$ |
|  | . 37 | 7.98 | 50.34 | 8.20 | 50.30 | 8.42 | 50.26 | 8.6 | 51 |
|  | 51.36 | 8.13 | 51.32 | 8.36 | 51.29 | 8.58 | 51.25 | 8.81 | 52 |
|  | 52.35 | 8.29 | 52.31 | 8.52 | 52.27 | 8.75 | 52.23 | 8.98 | 53 |
|  | 53.34 | 8.45 | 53.30 | 8.68 | 53.26 | 8.91 | 53.22 | 9.14 | 54 |
|  | 54.32 | 8.60 | 54.28 | 8.84 | 54.25 | 9.08 | 54.21 | 9.31 | 55 |
|  | 55.31 | 8.76 | 55.27 | 9.00 | 55.23 | 9.24 | 55.19 | 9.48 | 56 |
|  | 56.30 | 8.92 | 56.26 | 9.16 | 56.22 | 9.41 | 56.18 | 9.65 | 57 |
| 58 | 57.29 | 9.07 | 57.25 | 9.32 | 57.20 | 9.57 | 57.16 | 9.82 | 58 |
|  | 58.27 | 9.23 | 58.23 | 9.48 | 58.19 | 9.74 | 58.15 | 9.99 | - |
| 60 | 59.26 | 9.39 | 59.22 | 9.64 | 59.18 | 9.90 | 59.13 | 10.16 | 0 |
|  | 25 | 9.5 | 60.21 | 9.81 |  | 0.07 |  |  | 61 |
|  | 61.24 | 9.70 | 61.19 | 9.97 | 61.15 | 10.23 | 61.10 | 10.50 | 62 |
|  | 62.22 | 9.86 | 62.18 | 10.13 | 62.14 | 10.40 | 62.09 | 10.67 | 63 |
|  | 63.21 | 10.01 | 63.17 | 10.29 | 63.12 | 10.56 | 63.08 | 10.84 | 4 |
|  | 64.201 | 10.17 | 64.15 | 10.45 | 64.11 | 10.73 | 64.0 | 11.01 | 65 |
|  | 65.191 | 10.32 | 65.14 | 10.61 | 65.09 | 10.89 | 65.05 | 11.18 | 66 |
|  | 66.18 | 10.48 | 66.13 | 10.77 | 66.08 | 11.06 | 66.03 | 11.35 | 67 |
|  | 67.16 | 10.64 | 67.12 | 10.93 | 67.07 | 11.22 | 67.02 | 11.52 | 88 |
|  | 68.15 | 10.79 | 68.10 | 11.09 | 68.05 | 11.39 | 68.00 | 11.69 | 69 |
|  | 69.14 | 10.95 | 69.09 | 11.25 | 69.04 | 11.55 | 68.99 |  | 70 |
|  | 70.13 | 11.11 | 70. | 11.41 | 70.0 | 11.72 | 69.9 |  | 71 |
|  | 71.11 | 11.26 | 71.06 | 11.57 | 71.01 | 11.88 | 70.96 | 12.19 | 72 |
|  | 72.101 | 11.42 | 72.05 | 11.73 | 72.00 | 12.05 | 71.95 |  | 73 |
|  | 73.091 | 11.58 | 73,04 | 11.89 | 72.99 | 12.21 | 72.93 | 12.53 | 74 |
|  | 74.08 I | 11.73 | 74.02 | 12.06 | 73.97 | 12.38 | 73.92 | 12.70 | 75 |
|  | 75.061 | 11.89 | 75.01 | 12.22 | 74.96 | 12.54 | 74.90 |  | 76 |
|  | 76.05 | 12.05 | 76.00 | 12.38 | 75.94 | 12.71 | 75.8 |  | 77 |
|  | 77.04 | 12.20 | 76.99 | 12.54 | 76.93 | 12.87 | 76.87 | 13.21 | 8 |
|  | 78.031 | 12.36 | 77.97 | 12.70 | 77.32 | 13.04 | 77.86 | 13.38 | 79 |
|  | 79.02 | 12.51 | 73.96 | 12.86 | 78.9 | 13.20 |  | 13.55 |  |
|  | 80.001 | 12.67 | 79.95 | 13.02 | 79.8 | 13.37 |  |  | 1 |
| 81 <br> 82 <br> 83 <br> 84 <br> 85 <br> 86 <br> 87 <br> 88 <br> 89 <br> 90 | 80.99 | 12.83 | 80.93 | 13.18 | 80.88 | 13.53 | 80.82 | 13.89 | 2 |
|  | 81.981 | 12.98 | 81.92 | 13.34 | 81.86 | 13.70 | 81.80 | 14.06 | 83 |
|  | 82.97 | 13.14 | 82.91 | 13.50 | 82.85 | 13.86 | 82.7 | 14.23 | 84 |
|  | 83.95 | 13.30 | 83.89 | 13.66 | 33.83 | 14.03 | 83.7 | 14.39 | 85 |
|  | 84.94 | 13.45 | 84.88 | 13.82 | 84. S 2 | 14.19 | 84.76 | 14.56 | 86 |
|  | 85.931 | 13.61 | 85.87 | 13.98 | -85.81 | 14.36 | 85.74 | 14.73 | 87 |
|  | ,86.92 | 13.77 | 86.86 | 14.15 | 86.79 | 14.52 | 86.73 | 14.90 | 88 |
|  | 87.901 | 13.92 | 87.84 | 14.31 | 87.78 | 14.69 | 87.71 | 15.07 | 89 |
|  | 38.89 | 14.08 | 88 | 14.47 | 88.77 | 14.85 | 88.70 |  | - |
|  | 59.88 | 14.24 | 89.82 | 4.63 | 89.75 | 15.02 | 39. |  | 91 |
|  | 90.871 | 14.39 | 90.80 | 14.79 | 90.74 | 15.18 | 90.67 | 15.58 | 92 |
|  | 91.86 | 14.55 | 91.79 | 14.95 | 91.72 | 15.35 | 91.66 | 15.75 | 93 |
|  | 92.841 | 14.70 | 32.78 | 15.11 | 92.71 | 15.51 | 92.64 | 15.92 | - |
|  | 93.831 | 14.86 | 93.76 | 15.27 | 93.70 | 15.68 | 93.63 | 16.09 | 95 |
|  | 94.821 | 15.02 | 94.75 | 15.43 | 94.68 | 15.84 | 94.61 | 16.26 | 96 |
|  | 95.811 | 15.17 | 95.74 | 15.59 | 95.67 | 16.01 | 95.60 | 16.4 | 97 |
|  | 96.79 1 | 15.33 | 96.73 | 15.75 | 96.66 | 16.17 | 96.58 | 6. 6 | 98 |
|  | 97:781 | 15.49 | 97:71 | 15.91 | 97.64 | 16.34 | 97.57 | 16.77 | 99 |
| 199 | 98.77 | 15.64 | 98 | 6.07 | 98.63 | 16.50 | 98.56 | 16.9 | 100 |
|  | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep | Lat. |  |
|  | 81 | D |  | eg. |  |  |  |  |  |


| $\underset{\sim}{0}$ |  |  | 4 |  |  | eg. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat | Dep. |  | ep. | Lat | Dep. |  | Dep. |  |
| - | 0.98 | 0.17 | 0.98 | 0.18 | 0.98 | 0.18 | 0.98 | 0.19 |  |
| 2 | 1.97 | 0.35 | 1,97 | 0.36 | 1.97 | 0.36 | 1.96 | 0.37 |  |
| 3 | 2.95 | 0.52 | 2.95 | 0.53 | 2.95 | 0.55 | 2.95 | 0.56 |  |
| , | 3.94 | 0.69 | 3,94 | 0.71 | 3.93 | 0.73 | 3.93 | 0.75 |  |
| 5 | 4.92 | 0.87 | 4.92 | 0.89 | 4.92 | 0.91 | 4.91 | 0.93 |  |
| 6 | 5.91 | 1.04 | 5.90 | 1.07 | 5.90 | 1.09 | 5.89 | 1.12 |  |
| 7 | 6.89 | 1.22 | 6.89 | 1.25 | 6.88 | 1.28 | 6.8 | 1.31 |  |
| 8 | 7.88 | 1.39 | 7.87 | 1.42 | 7.87 | 1.46 | 7.86 | 1.49 |  |
|  | 8.86 | 1.56 | 8.86 | 160 | 8.85 | 1.64 | 8.84 | 1.68 |  |
| 10 | 9.85 | 1.74 | 9.84 | 1.78 | 9.83 | 1.82 | 9.82 | 1.87 | 10 |
| 11 | 10.83 | 1.91 | 10.82 | 1.96 | 10.82 | 2.00 | 10.81 | 2.05 |  |
|  | 11.82 | 2.08 | 11.81 | 2.14 | 11.80 | 2.19 | 11.79 |  | 12 |
|  | 12.80 | 2.26 | 12.79 | 2.31 | 12.78 | 2.37 | 12.77 | 2. | 3 |
|  | 13.79 | 2.43 | 13.78 | 2.49 | 13.77 | 2.55 | 13.75 | 2.61 | 4 |
|  | 14.77 | 2.60 | 14.76 | 2.67 | 14.75 | 2.73 | 14.74 | 2.8 | 5 |
|  | 15.76 | 2.78 | 15.74 | 2.85 | 15.73 | 2.92 | 15.72 |  | 6 |
|  | 16.74 | 2.95 | 16.73 | 3.03 | 16.72 | 3.10 | 16.70 | 3. | 7 |
|  | 17.73 | 3.13 | 17.71 | 3.20 | 17.70 | 3.28 | 17.68 | 3.3 | 8 |
|  | 18.71 | 3.30 | 18.70 | 3.38 | 18.68 | 3.46 | 18.67 | 3.5 | 19 |
|  | 19.70 | 3.47 | 19.68 | 3.56 | 19.67 | 3.64 | 19.65 | 3.7 | 20 |
|  | 20.6 | 3.65 | 20.66 | 3.74 | 20.65 | 3.83 | 20.63 |  |  |
|  | 21.67 | 3.82 | 21.65 | 3.91 | 21.63 | 4.01 | 21.61 | 4.10 |  |
|  | 22.65 | 3.99 | 22.63 | 4.09 | 22.61 | 4.19 | 22.6 |  | 3 |
|  | 23.64 | 4.17 | 23.62 | 4.27 | 23.60 | 4.37 | 23.58 | 4. | 4 |
|  | 24.62 | 4.34 | 24.60 | 4.45 | 24.58 | 4.56 | 24.56 | 4.6 | 25 |
|  | 25.61 | 4.51 | 25.59 | 4.63 | 25.56 | 4.74 | 25.5 |  | 2 |
|  | 26.59 | 4.69 | 26.57 | 4.80 | 26.55 | 4.92 | 26.53 | 5.0 | 27 |
|  | 27.0゙' | 4.86 | 2? 35 | 4.98 | 27.53 | 5.10 | 97. 51 |  | 28 |
| 2930 | 28.56 | 5.04 | 28.54 | 5.16 | 28.51 | 5.28 | 28.49 | 5.4 | - |
|  | 29.54 | 5.21 | 29.52 | 5.34 | 29.50 | 5.47 | 29,47 | 5 |  |
|  | 30.53 | 5.38 | 30.51 | 5.52 | 30.48 | 5.65 | 30.46 | 5.78 | 31 |
|  | 31.51 | 5.56 | 31.49 | 5.69 | 31.46 | 5.83 | 31.44 | 5.97 | 32 |
|  | 32.50 | 5.73 | 32.47 | 5.87 | 32.45 | 6.01 | 32.42 | 6.1 | 33 |
|  | 33.48 | 5.90 | 33.46 | 6.05 | 33.43 | 6.20 | 33.40 | 6.34 | 31 |
|  | 34.47 | 6.08 | 34.44 | 6.23 | 34.41 | 6.38 | 34.39 | 6.5 | 35 |
|  | 35.45 | 6.25 | 35.43 | 6.41 | 35.40 | 6.56 | 35.37 | 6.71 | 36 |
|  | 36.44 | 6.42 | 36.41 | 6.58 | 36.38 | 6.74 | 36.35 | 6. | 37 |
|  | 37.42 | 6.60 | 37.39 | 6.76 | 37.36 | 6.92 | 37.33 | 7.0 | 38 |
| 39 <br> 40 | 38.41 | 6.77 | 38.38 | 6.94 | 38.35 | 7.11 | 38.32 | 7.27 | 39 |
|  | 39.39 | 6.95 | 39.36 | 7.12 | 39.33 | 7.29 | 39.30 | 7.4 | 40 |
|  | 40.38 | 7.12 | 40.35 | 7.30 | 40.31 | 7.47 | 40.28 | 7.65 | 41 |
|  | 41.36 | 7.29 | 41.33 | 7.47 | 41.50 | 7.65 | 41.26 | 7.83 | 4 |
|  | 49.35 | 7.47 | 42.31 | 7.65 | 42.28 | 7.84 | 42.25 | 8.02 |  |
|  | 43.33 | 7.64 | 43.30 | 7.83 | 43.26 | 8.02 | 43.23 | 8.21 | 44 |
|  | 44.32 | 7.81 | 44.28 | 8.01 | 44.25 | 8.20 | 44.21. | 8.39 | 45 |
|  | 45.30 | 7.99 | 45.27 | 8.19 | 45.23 | 8.38 | 45.19 | 8.58 | 46 |
|  | 46.29 | 8.16 | 46.25 | 8.36 | 46.21 | 8.57 | 46.18 | 8.77 | 47 |
|  | 47.27 | 8.34 | 47.23 | 8.54 | 47.20 | 8.75 | 47.16 | 8.95 | 48 |
|  | 43.26 | 8.51 | 48.22 | 8.72 | 48.18 | 8.93 | 48.14 | 9.1 | 49 |
| 50 | 49.24 | 8. | 49.20 | 8.90 | 49.16 | 9.11 | 49.12 | 9. | 50 |
|  | Dep | Lat. | Dep | Lat. | Dep. | Lat. | Dep. | Lat. |  |
|  | 80 |  |  |  |  | eg. |  |  |  |



TRAVERSE TABLE.




TRAVERSE TABLE.

| $\begin{aligned} & 8 \\ & 6 \\ & 6 \end{aligned}$ | 12 Deg . |  | $12 \frac{1}{4}$ Deg. |  | $12 \frac{1}{2} \mathrm{Deg}$ |  | $\frac{12 \frac{3}{4} \mathrm{Deg}}{\text { Lat. Dep. }}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. |  |  |  |
| 51 | 49.89 | 10.60 | 49.84 | 10.82 | 49.79 | 11.04 | 49.74 | 26 |  |
| 52 | 50.86 | 10.81 | 50.8\% | 11.03 | 50.77 | 11.25 | 50.72 |  | 52 |
| 53 | 51.84 | 11.02 | 51.79 | 11.25 | 51.74 | 11.47 |  |  | 53 |
| 54 | 52.82 | 11.23 | 52.77 | 11.46 | 52.72 | 11.69 | 52.6 |  | 54 |
| 55 | 53.80 | 11.44 | 53.75 | 11.67 | 53.70 | 11.90 | 53.6 | 2.14 | 55 |
| 56 | 54.78 | 11.64 | 54.72 | 11.88 | 54.67 | 12.12 | 54.6 | 36 | 56 |
| 57 | 55.75 | 11.85 | 55.70 | 12.09 | 55.65 | 12.34 | 55.59 | 12.58 | 57 |
| 58 | 56.73 | 12.06 | 56.68 | 12.31 | 56.63 | 12.55 | 56.57 | 12.80 | 58 |
| 59 | 57.71 | 12.27 | 57.66 | 12.52 | 57.60 | 12.77 | 57.55 | 13,02 | 59 |
| 60 | 58.69 | 12.47 | 58.63 | 12.73 | 58.58 | 12.99 | 58.52 | 13.24 | 60 |
| 61 |  | 1268 | 59.61 | 12.94 | 59.55 | 13.20 |  |  | 1 |
| 62 | 60.65 | 12.89 | 60.59 | 13.16 | 60.53 | 13.42 |  |  | 62 |
| 63 | 61.62 | 13.10 | 61.57 | 13.37 | 61.51 | 13.64 | 61.4 | 3.90 | 63 |
| 64 | 62.601 | 13.31 | 62.54 | 13.58 | 62.48 | 13.85 | 62. | 4.12 | 64 |
| 65 | 63.58 | 13.51 | 63.52 | 13.79 | 63.46 | 14.07 |  | 4.35 | 65 |
| 66 | 64.56 | 13.72 | 64.50 | 14.00 | 64.44 | 14.29 | 64.37 | 14.57 | 66 |
| 67 | 65.54 | 13.93 | 65.47 | 14.22 | 65.41 | 14.50 | 65.35 | 14.79 | 67 |
| 68 | 66.51 | 14.14 | 66.45 | 14.43 | 66.39 | 14.72 | 66.32 |  | 68 |
| 69 | 67.49 | 14.35 | 67.43 | 14.64 | 67.36 | 14.93 | 67.30 | 15.23 | 69 |
| 70 | 68.47 | 14.55 | 68.41 | 14.85 | 68.34 | 15.15 | 68.27 | 15.45 | 70 |
| 71 | 69.45 | 14.76 | 69.38 | 15.06 | 69.32 | 15.37 | 69.35 |  | 1 |
| 72 | 70 | 14.97 | 70.36 | 15.28 | 70.29 | 15.58 | 70.22 | 15.89 | 72 |
| 73 | 71.40 | 15.18 | 71.34 | 15.49 | 71.27 | 15.80 | 71.20 | 16.11 | 3 |
| 74 | 72.38 | 15.39 | 72.32 | 15.70 | 72.25 | 16.02 | 72.18 | 16.33 | 74 |
| 75 | 73.36 | 15.59 | 73.29 | 15.91 | 73.22 | 16.23 | 73.15 | 6.55 | 75 |
| 76 | 74.34 | 15.80 | 74.27 | 16.13 | 74.20 | 16.45 | 74.13 | 16.77 | 76 |
| 77 | 75.32 | 16.01 | 75.25 | 16.34 | 75.17 | 16.67 | 75.10 | 16.99 | 77 |
| 78 | 76.30 | 16.22 | 76.22 | 16.55 | 76.1 | 16.88 | 76.08 | 17.21 | 8 |
| 79 | 77.27 | 16.43 | 77.20 | 16.76 | 77.13 | 17.10 | 77.05 | 17.44 | 9 |
| 80 | 78.25 | 16.63 | 78.18 | 16.97 | 78.10 | 17.32 | 78.03 | 17.66 | 8 |
| 81 | 79.23 | 16.84 | 79.16 | 17.19 | 79.08 | 17.53 | 79.00 | 17.88 | 81 |
| 82 | 80.21 | 17.05 | 80.13 | 17.40 | 80.06 | 17.75 | 79.98 | 18.10 | 8 |
| 83 | 81.19 | 17.26 | 81.11 | 17.61 | 81.03 | 17.96 | 80.95 | 18.32 | 83 |
| 84 | 82.16 | 17.46 | 82.09 | 17.82 | 82.01 | 18.18 | 81.93 |  | 84 |
| 85 | 83.14 | 17.67 | 83.06 | 18.04 | 82.99 | 18.40 | 82.90 | 18.76 | 85 |
| 86 | 84.121 | 17.88 | 84.04 | 18.25 | 83.96 | 18.61 | 83.88 | 18.98 | 86 |
| 87 | 85.10 | 18.09 | 85.02 | 18.46 | 84.94 | 18.83 | 84.85 | 19.20 | 8 |
| 88 | 86.08 | 18.30 | 86.00 | 18.67 | 85.91 | 19.05 | 85.83 | 19.42 | 88 |
| 89 | 87.06 | 18.50 | 86.97 | 18.88 | 86.89 | 19.26 | 86.81 |  | 89 |
| 90 | 88.03 | 18.71 | 87.95 | 19.10 | 87.87 | 19.48 | 87.78 | 19.86 | 90 |
| 91 | 89.01 | 18.92 | 88.93 | 19.31 | 88.84 | 19,70 |  | 20.08 | 91 |
| 92 | 89.99 | 19.13 | 89.91 | 19.52 | 89.82 |  |  | 20.30 | 32 |
| 93 | 90.97 | 19.34 | 90.83 | 19.73 | 90.80 | 20.13 | 90.71 | 20.52 | 93 |
| 94 | 91.95 | 19.54 | 91.86 | 19.94 | 91.77 | 20.35 | 91.68 | 20.75 | 94 |
| 95 | 92.92 | 19.75 | 92.84 | 20.16 | 92.75 | 20.56 | 92.66 | 20.9 | 95 |
| 96 | 93.90 | 19.96 | 93.81 | 20.37 | 93.72 | 20.78 | 93.6 | 21.19 | 96 |
| 97 | 94.88 | 20.17 | 94.79 | 20.58 | 94.70 | 20.99 | 94.6 | 21.4 | 97 |
| 98 | 95.86 | 20.38 | 95.77 | 20.79 | 95.68 | 21.21 | 95.58 | 21.6 | 8 |
| 99 | 96.84 | 20.58 | 96.75 | 21.01 | 96.65 | 21.43 | 96.56 | 21.85 | 99 |
| 100 | 97.81 | 20.79 | 97.72 | 21.22 | 97.63 | 21.64 | 97.53 | 22.07 | 100 |
|  | Dep. | Lat. | Dep | Lat. | Dep | Lat. | Dep. | Lat. |  |
|  | 78 Deg. $1777 \frac{3}{4} \mathrm{Deg}$ |  |  |  |  |  |  |  |  |

TRAVERSE TABLE.

| $\begin{aligned} & 0 \\ & \stackrel{5}{4} \end{aligned}$ | 113 Deg . |  | $13 \times \mathrm{Deg}$. | 131 Deg. | $13_{4}^{3}$ Deg. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. | Lat. Dep. | Lat. Dep. | Lat. | Dep |  |
|  | 0.97 | 0.23 | 0.970 .23 | $0.97 \quad 0.2$ | 0.97 |  |  |
| 2 | 1.95 | 0.45 | $\begin{array}{ll}1.95 & 0.46\end{array}$ | 1.95 | 1.94 | 0. |  |
| 3 | 2.92 | 0.67 | 2.920 .69 | 2.920 .70 | 2.91 |  |  |
|  | 3.90 | 0.90 | 3.890 .92 | 3.890 .93 | 3.89 | 0.95 |  |
| 5 | 4.87 | 1.12 | 4.871 .15 | 4.86 | 4.86 |  |  |
| 6 | 5.85 | 1.35 | 5.841 .38 | 5.831 .40 | 5.83 |  |  |
| 7 | 6.82 | 1.57 | 6.81 1.60 | 6.811 .63 | 6.80 | 1.66 |  |
| 8 | 7.80 | 1.80 | 7.791 .83 | 7.781 .87 | 7.77 | 1. |  |
| 9 | 8.77 | 2.02 | 8.762 .06 | 8.752 .10 | 8.74 | 2. |  |
| 10 | 9.74 | 2.25 | 9.732 .29 | 9.722 .33 | 9.71 | 2. | 10 |
| 11 | 10.72 | 2.47 | 10.712 .52 | $70 \quad 2.57$ | 10.68 | 2. | 1 |
| 12 | 11.69 | 2.70 | $11.68 \quad 2.75$ | 11.672 .80 | 11.66 | 2. | 12 |
| 13 | 12.67 | 2.92 | $12.65 \quad 2.98$ | 12.64 3.03 | 12.63 | 3. | 13 |
| 14 | 13.64 | 3.15 | 13.63 3.21 | 13.613 .27 | 13.60 | 3. |  |
| 15 | 14.62 | 3.37 | 14.603 .44 | 14.593 .50 | 14.57 | 3.5 | 15 |
| 16 | 15.59 | 3.60 | 15.573 .67 | 15.56 | 15.54 | 3. | 16 |
| 17 | 16.57 | 3.82 | $16.55 \quad 3.90$ | $16.53 \quad 3.97$ | 16.51 | 4.0 | 17 |
| 18 | 17.54 | 4.05 | 17.524 .13 | 17.504 .20 | 17.48 | 4.2 | 18 |
| 19 | 18.51 | 4.27 | 18.494 .35 | 18.484 .44 | 18.46 | 4.5 | 19 |
| 20 | 19.49 | 4.50 | 19.474 .58 | 19.454 .67 | 19.43 | 4.7 | 20 |
| 21 | 20.46 | 4.72 | 20.444 .81 | ${ }^{2} 0.424 .90$ | 20.40 |  | 21 |
| 22 | 21.44 | 4.95 | 21.415 .04 | $21.39 \quad 5.14$ | 21.37 | 5. | 22 |
| 23 | 22.41 | 5.17 | 22395.27 | 22.36 | 22.34 |  | 23 |
| 24 | 23.38 | 5.40 | 23.365 .50 | 23.345 .60 | 23.31 | 5.7 | 24 |
| 25 | 24.36 | 5.62 | 24.33 5.73 | 24.31 | 24.28 | 5. | 20 |
| 26 | 25.33 | 5.85 | 25.315 .96 | 25.286 .07 | 25.25 | 6.1 | 26 |
| 27 | 26.31 | 6.07 | 26.286 .19 | $26.25 \quad 6.30$ | 26.23 | 6.4 | 27 |
| 28 | 27.28 | 6.30 | 27.256 .42 | 27.236 .54 | 27.20 | 6.6 | 28 |
| 29 | 28.26 | 6.52 | 28.236 .65 | 28.206 .77 | 28.17 | 6.8 | 9 |
| 30 | 29.23 | 6.75 | 29.206 .88 | 29.177 .00 | 29.14 | 7. | 30 |
|  |  | 97 | $30.17 \quad 7.11$ | $30.14 \quad 7.24$ | 30.11 | 7. | 31 |
| 32 | 31.18 | 7.20 | $31.15 \quad 7.33$ | $31.12 \quad 7.47$ | 31.08 | 7.6 | 32 |
| 33 | 32.15 | 7.42 | 32.127 .56 | 32.0978 .70 | 32.05 | 7.8 | 33 |
| 34 | 33.13 | 7.65 | 33.097 .79 | 33.067 .94 | 33.03 | 8.0 | 34 |
| 35 | 34.10 | 7.87 | 34.078 .02 | 34.038 .17 | 34.00 | 8.3 | 35 |
| 36 | 35.08 | 8.10 | 35.048 .25 | 35.0188 .40 | 34.97 | 8.5 | 36 |
| 37 | 36.05 | 8.32 | 36.028 .48 | 35.98 8.64 | 35.94 | 8.7 | 37 |
| 38 | 37.03 | 8.55 | 36.998 .71 | 36.9588 .87 | 36.91 | 9.0 | 38 |
| 39 | 38.00 | 8.77 | 37.968 .94 | 37.929 .10 | 37.88 | 9.27 | 39 |
| 40 | 38.97 | 9.00 | 38.94 9.17 | 38.89 9.34 | 38.85 | 9.51 | 40 |
| 41 | 39.95 | 9.22 | 39.919 .40 | $\begin{array}{lll}39.87 & 9.57\end{array}$ | 39.83 | 9.75 | 41 |
| 42 | 40.92 | 9.45 | 40.889 .63 | $40.84 \quad 9.80$ | 40.80 | 9.98 | 42 |
| 43 | 41.90 | 9.67 | 41.86 .9 .86 | 41.8110 .04 | 41.77 | 0.22 | 43 |
| 44 | 42.87 | 9.90 | 42.8310 .08 | 49.7810 .27 | 42.74 | 10.4 | 44 |
| 45 | 43.85 | 10.12 | 43.8010 .31 | 43.7610 .51 | 43.71 | 10.70 | 45 |
| 46 | 44.82 | 10.35 | 44.7810 .54 | 44.7310 .74 | 44.68 | 10.93 | 46 |
| 47 | 45.80 | 10.57 | 45.7510 .77 | 45.7010 .97 | 45.6 | 11.17 | 47 |
| 48 | 46.77 | 10.80 | 46.7211 .00 | 46.6711 .21 | 46.62 | 11.41 | 48 |
| 49 | 47.74 | 11.02 | 47.7011 .23 | 47.6511 .44 | 47.60 | 11.65 | 49 |
| 50 | 48:72 | 11.25 | 48.6711 .46 | 48.6211 .67 | 48.57 | 11.8 | 50 |
|  | Dep. Lat. |  | Dep. Lat. | Dep. Lat. | Dep. Lat. |  |  |
|  |  |  | $76{ }_{4}^{3} \mathrm{Deg}$. | eg |  | g. |  |



| $\underset{\substack{0 \\ ?}}{0}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.97 | 0.24 | 0.97 | 0.25 | 0.97 | 0.25 | 0.97 |  |  |
| 2 | 1.94 | 0.48 | 1.94 | 0.49 | 1.94 | 0.50 | 1.93 | 0.51 | 2 |
| 3 | 2.91 | 0.73 | 2.91 | 0.74 | 2.90 | 0.75 | 2.90 | 0.76 |  |
| 4 | 3.88 | 0.97 | 3.88 | 0.98 | 3.87 | 1.00 | 3.87 | 1.02 |  |
| 5 | 4.85 | 1.21 | 4.85 | 1.23 | 4.84 | 1.25 | 4.84 | 1.2 | 5 |
| 6 | 5.82 | 1.45 | 5.82 | 1.48 | 5.81 | 1.50 | 5.80 | 1.5 |  |
| 7 | 6.79 | 1.69 | 6.78 | 1.72 | 6.78 | 1.75 | 6.77 | 1.78 |  |
| 8 | 7.76 | 1.94 | 7.75 | 1.97 | 7.75 | 2.00 | 7.74 | 2.04 |  |
| 9 | 8.73 | 2.18 | 8.72 | 2.22 | 8.71 | 2.25 | 8.70 | 2.29 |  |
| 10 | 9.70 | 2.42 | 9.69 | 2.46 | 9.68 | 2.50 | 9.67 | 2.55 | 0 |
| 111 | 110.67 | 2.66 | 10.66 | 2.71 | 10.65 | 2.75 | 10.64 | 2.80 |  |
| 1211.64 |  | 2.90 | 11.63 | 2.95 | 11.62 | 3.00 | 11.60 | 3.06 | 2 |
|  | 12.61 | 3.15 | 12.60 | 3.20 | 12.59 | 3.25 | 12.57 | 1 |  |
|  | 13.58 | 3.39 | 13.57 | 3.45 | 13.55 | 3.51 | 13.54 | 3.56 | 14 |
|  | 4.55 | 3.63 | 14.54 | 3.69 | 14.52 | 3.76 | 14.51 | 3.82 | 5 |
|  | 15.52 | 3.87 | 15.51 | 3.94 | 15.49 | 4.01 | 15.47 | 4.07 | 6 |
| 17 | 16.50 | 4.11 | 16.48 | 4.18 | 16.46 | 4.26 | 16.44 | 4.33 | 17 |
|  | 17.47 | 4.35 | 17.45 | 4.43 | 17.43 | 4.51 | 17.41 | 4.58 | 18 |
|  | 18.44 | 4.60 | 18.42 | 4.68 | 18.39 | 4.76 | 18.37 | 4.84 | 9 |
| 20 | 19.41 | 4.84 | 19.38 | 4.92 | 19.36 | 5.01 | 19.3 | 5.09 | 0 |
|  | 20.38 | 5.08 | 20.35 | 5.17 | 20.33 | 5.26 | 20.31 | 5.35 | 1 |
|  | 21.35 | 5.32 | 21.32 | 5.42 | 21.30 | 5.51 | 21.28 | 5.60 | 2 |
|  | 22.32 | 5.56 | 22.29 | 5.66 | 2.27 | 5.76 | 22.2 | 5.8 |  |
|  | 23.29 | 5.81 | 23.26 | 5.91 | 23.24 | 6.01 | 23.21 | 6.11 | 4 |
|  | 24.26 | 6.05 | 24.23 | 6.15 | 24.20 | 6.26 | 24.18 | 6.37 | 5 |
|  | 25.23 | 6.29 | 25.20 | 6.40 | 2.17 | 6.51 | 25.14 | 6.62 | 6 |
|  | 26.20 | 6.53 | 26.17 | 6.65 | 26.14 | 6,76 | 26.11 | 6.87 | 7 |
|  | 27.17 | 6.77 | 27.14 | 6.89 | 27.11 | 7.01 | 27.08 | 7.1 | 8 |
|  | 28.14 | 7.02 | 28.11 | 7.14 | 28.08 | 7.26 | 28.04 | 7.3 | 9 |
|  | 29.11 | 7.26 | 29.08 | 7.38 | 29.04 | 7.51 | 29.0 | 7.64 |  |
|  | 30.08 | 7.50 | 30.05 | 7.63 | 30.01 | 7.76 | 29.98 | 7.8 | 31 |
|  | 31.05 | 7.74 | 31.02 | 7.88 | 30.98 | 8.01 | 30.95 | 8.1 | 2 |
|  | 32.02 | 7.98 | 31.98 | 8.12 | 31.95 | 8.26 | 31.91 |  | 3 |
|  | 32.99 | 8.23 | 32.95 | 8.37 | 32.92 | 8.51 | 32.88 | 8.6 | 4 |
|  | 33.96 | 8.47 | 33.92 | 8.62 | 33.89 | 8.76 | 33.85 | 8.91 | 55 |
|  | 34.93 | 8.71 | 34.89 | 8.86 | 34.85 | 9.01 | 34.81 | 9.1 | 6 |
|  | 35.90 | 8.95 | 35.86 | 9.11 | 35.82 | 9.2 | 35.7 |  | 37 |
|  | 36.87 | 9.19 | 36.83 | 9.35 | ${ }^{36.79}$ | 9.51 | 36.75 | 9.67 | 38 |
| 34 | 37.84 | 9.44 | 37.80 | 9:60 | 37.76 | 9.76 | 37.71 | 9. | 9 |
|  | 38.81 | 9.68 | 38.77 | 9. |  | 10. | 38 | 10. |  |
|  |  | 9.92 | 39.74 | 10.09 | 39.69 | 10.27 | 39.6 |  | 41 |
|  | 40.75 | 10.16 | 40.71 | 110.34 | 40.66 | 10.52 | ${ }^{4} 40.6$ | 10.69 | 42 |
|  | 41.72 | 10.40 | 41.68 | 10.58 | 41.63 | 10.77 | 41.58 | 10.9 | 43 |
|  | 42.69 | 10.64 | 42.65 | 10.83 | 42.60 | 11.02 | 42.55 | 11.20 | 4 |
|  | 43.66 | 10.89 | 43.62 | 11.08 | 43.57 | 11.27 | 43.52 | 11.46 | 5 |
|  | 44.63 | 11.13 | 44.58 | 11.32 | 44.53 | 11.52 | 44.48 | 11.71 | 46 |
|  | 45.60 | 11.37 | 45.55 | 11.57 | 45.50 | 11.77 | 45.45 | 11.97 | 47 |
|  | 46.57 | 11.61 | 46.52 | 11.82 | 46.47 | 12.02 | 46.42 | 12.22 | 48 |
|  | 47.54 | 11.85 | 47.49 | 912.06 | 47.44 | 12.27 | 47.39 | 12.48 | 49 |
| 50 | 48.51 | 12.10 | 48.4 | 12.31 | 48.41 | 12.52 | 48.3 | 12.73 | 50 |
| $\stackrel{+}{2}$ | Dep | Lat. | De | Lat. | Dep. | Lat. | Dep |  |  |
|  | 10 |  |  |  |  |  |  |  |  |

TRAVERSE TABLE.

| - |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. | Lat. | Dep. | Lat. | Dpe. | Lat. | p. | + |
|  |  | 12.34 | 49.43 | 12.55 | 49.38 | 12.77 | 49.32 | 12. | 1 |
|  | 50.46 | 12.58 | 50.40 | 12.80 | 50.34 | 13.02 | 50.29 | 13.2 | 52 |
|  | 51.43 | 12.82 | 51.37 | 13.05 | 51.31 | 13.27 | 51.25 | 13.4 | 3 |
|  | 52.40 | 13.06 | 52.34 | 13.29 | 52.28 | 13.52 | 52.22 | 13.75 |  |
|  | 53.37 | 13.31 | 53.31 | 13.54 | 53.25 | 13.77 | 53.19 | 14.00 | 55 |
|  | 54.34 | 13.55 | 54.28 | 13.78 | 54.22 | 14.02 | 54.15 | 14.2 | 6 |
|  | 55.31 | 13.79 | 55.25 | 14.03 | 55.18 | 14.27 | 55.12 | 14.51 | 7 |
|  | 56.28 | 14.03 | 56.22 | 14.28 | 56.15 | 14.52 | 56.0 | 14.77 | 8 |
|  | 57.25 | 14.27 | 57.18 | 14.52 | 57.12 | 14.77 | 57.0 | 15.0 | 59 |
| 60 | 58.22 | 14.5\% | 58.15 | 14.77 | 58.09 |  | 58.02 | 15.2 | 60 |
|  |  |  |  | 15.02 | 59. | 27 | 58.9 |  | 61 |
|  | 60.16 | 15.00 | 60.09 | 15.25 | 60.03 | 15.52 | 59.96 | 15.79 | 62 |
|  | 61.13 | 15.24 | 61.06 | 15.51 | 60.99 | 15.77 | 60.92 | 16.04 | 63 |
|  | 62.10 | 15.48 | 62.03 | 15.75 | 61.96 | 16.02 | 61.89 | 16.29 |  |
|  | 63.07 | 15.72 | 63.00 | 16.00 | 62.93 | 16.27 | 62.86 | 16.55 | 65 |
|  | 64.04 | 15.97 | 63.97 | 16.25 | 63.90 | 16.53 | 63.83 | 16.80 | 66 |
|  | 65.01 | 16.21 | 64.94 | 16.49 | 64.87 | 16.78 | 64.79 | 17.06 | 67 |
| 686970 | 65.98 | 16.45 | 65.91 | 16.74 | 65.83 | 17.03 | 65.76 | 17.31 | 8 |
|  | 66.95 | 16.69 | 66.88 | 16.98 | 66.80 | 17.2 | 66.73 | 17.57 | 69 |
|  | 67.92 | 16.93 | 67.85 | 17.23 | 67.77 | 7.53 | 67.69 |  | 70 |
|  | 68.89 | 17.18 | 68.82 | 17.48 | 68. | 78 | 68.66 | 18 | 8 |
|  | 69.86 | 17.42 | 69.78 | 17.72 | 69.71 | 18.03 | 69.6 | 18. | 2 |
|  | 70.83 | 17.66 | 70.75 | 17.97 | 70.67 | 18.28 | 70.59 | 18.59 | 73 |
|  | 71.80 | 17.90 | 71.72 | 18.22 | 71.64 | 18.53 | 71.56 | 18.84 | 44 |
|  | 72.77 | 18.14 | 72.69 | 18.46 | 72.61 | 18.78 | 72.53 | 19.10 | 75 |
|  | 73.74 | 18.39 | 73.66 | 18.71 | 73.58 | 19.03 | 73.50 | 19.3 | 76 |
|  | 74.71 | 18.63 | 74.63 | 18.95 | 74.55 | 19.28 | 74.46 | 19.60 | - |
|  | 75.68 | 18.87 | 75.60 | 19.20 | 75.52 | 19.53 | 75.43 |  | 78 |
|  | 76.65 | 19.11 | 76.57 | 19.45 | 76.48 | 19.78 | 76.40 | 20.11 | 1 |
|  | 77.62 | 19.35 | 77.54 | 19.69 | 77.45 | 0.03 | 77.36 | 20 | 80 |
|  | 78.59 | 19.60 | 78.51 | 19.94 | 78.4 | 2.28 | 78.33 | 20. | 81 |
| 82 | 79.56 | 19.84 | 79.48 | 20.18 | 79.35 | 20.53 | 79.30 |  | 2 |
|  | 80.53 | 20.08 | 80.45 | 20.43 | 80.3 | 20.78 | 80.2 | 21.1 | 83 |
| 84 | 81.50 | 20.32 | 81.42 | 20.68 | 81.32 | 21.03 | 81.2 | 21.3 | 84 |
|  | 2.48 | 20.56 | 82.38 | 20.92 | 82.29 | 21.28 | 82.20 | 21.64 | 85 |
| 85 | 83.45 | 20.81 | 83.35 | 21.17 | 83.26 | 21.55 | 83.17 | . 1 | 86 |
| 8788 | 34.42 | 21.05 | 84.32 | 21,42 | 84.23 | 21.78 | 84.13 | 22.15 | 87 |
|  | 85.39 | 21.29 | 85.29 | 21.66 | 85.20 | 22.03 | 85.10 | 22.41 | 88 |
| $\begin{aligned} & 89 \\ & 90 \end{aligned}$ | 86.36 | 21.53 | 86.26 | 21.91 | ${ }^{36.17}$ | 22.28 | 86.07 | 22.6 | 9 |
|  | 87 | 21.77 | 87 | 22. |  | 22.53 | 87 | 22 |  |
|  | 88.30 | 22.01 | 88.20 | 22.40 | 88.10 | 22.78 | 88.00 | 23.1 | 1 |
| 91 | 89.27 | 22.26 | 89.17 | 22.65 | 89.07 | 23.04 | 88.97 | 23.4 | 92 |
|  | 90.24 | 22.50 | 90.14 | 22.89 | 90.64 | 23.29 | 89.94 | 3.68 | 3 |
|  | 91.21 | 22.74 | 91.11 | 23.14 | 91.01 | 23.54 | 90.90 | 23.9 | 析 |
|  | 92.18 | 22.98 | 92.08 | 23.38 | 91.97 | 23.79 | 91.87 | 24.19 | 95 |
| 95 | 93.15 | 23.22 | 93.05 | 23.63 | 92.94 | 24.04 | 92.84 | 24.44 | 96 |
| 97 | 94.12 | 23.47 | 94.02 | 23.88 | 93.9 | 24.29 | 93.80 | 24.70 | 97 |
| $\begin{aligned} & 98 \\ & 99 \end{aligned}$ | 95.09 | 23.71 | 94.98 | 24.12 | 94.88 | 24.54 | 94.77 | 24.95 | 8 |
|  | 96.06 | 23.95 | 95.95 | 24.37 | 95.8 | 24.79 | 95.74 | 25.21 | 99 |
| 100 | 97.03 | 24.19 | 96.92 | 24.62 | 96. | . 04 | 96.70 | 25 | 00 |
|  | Dep | Lat. | Dep | Lat. |  | Lat. | De |  |  |
|  |  |  |  |  |  |  |  |  |  |


|  |  | Deg. |  |  | $15 \frac{1}{8}$ | - | 159 Deg. |  | $\left\lvert\, \begin{aligned} & 0 \\ & \frac{5}{4} \\ & \frac{1}{4} \end{aligned}\right.$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. |  |
|  | 0.97 | 0.26 | 0.96 | 0.26 | 0.96 | 0.27 | 0.96 | 0.27 |  |
| 2 | 1.93 | 0.52 | 1.93 | 0.53 | 1.93 | 0.53 | 1.92 | 0.54 |  |
| 3 | 2.90 | 0.78 | 2.89 | 0.79 | 2.89 | 0.80 | 2.89 | 0.81 |  |
| 4 | 3.86 | 1.04 | 3.86 | 1.05 | 3.85 | 1.07 | 3.85 | 1.09 |  |
| 5 | 4.83 | 1.29 | 4.82 | 1.32 | 4.82 | 1.34 | 4.81 | 1.36 |  |
| 6 | 5.80 | 1.55 | 5.79 | 1.58 | 5.78 | 1.60 | 5.77 | 1.63 |  |
| 7 | 6.76 | 1.81 | 6.75 | 1.84 | 6.75 | 1.87 | 6.74 | 1.90 |  |
| 8 | 7.73 | 2.07 | 7.72 | 2.10 | 7.71 | 2.14 | 7.70 | 2.17 |  |
| 9 | 8.69 | 2.33 | 8.68 | 2.37 | 8.67 | 2.41 | 8.66 | 2.44 | 9 |
| 10 | 9.66 | 2.59 | 9.65 | 2.63 | 9.64 | 2.67 | 9.62 | 2.71 | 10 |
| 11 | 10.63 | 2.85 | 10.61 | 2.89 | 10.60 | 2.94 | 10.59 | 2.99 | 11 |
| 12 | 11.59 | 3.11 | 11.58 | 3.16 | 11.56 | 3.21 | 11.55 | 3.26 | 12 |
| 13 | 12.56 | 3.36 | 12.54 | 3.42 | 12.53 | 3.47 | 12.51 | 3.53 | 13 |
| 14 | 13.52 | 3.62 | 13.51 | 3.68 | 13.49 | 3.74 | 13.47 | 3.80 | 14 |
| 15 | 14.49 | 3.88 | 14.47 | 3.95 | 14.45 | 4.01 | 14.44 | 4.07 | 15 |
| 16 | 15.45 | 4.14 | 15.44 | 4.21 | 15.42 | 4.28 | 15.40 | 4.34 | 16 |
| 17 | 16.42 | 4.40 | 16.40 | 4.47 | 16.38 | 4.54 | 16.36 | 4.61 | 17 |
| 18 | 17.39 | 4.66 | 17.37 | 4.73 | 17.35 | 4.81 | 17.32 | 4.89 | 18 |
| 19 | 18.35 | 4.92 | 18.33 | 5.00 | 18.31 | 5.08 | 18.29 | 5.16 | 19 |
| 20 | 19.32 | 5.18 | 19.30 | 5.26 | 19.27 | 5.34 | 19.25 | 5.43 | 20 |
| 21 | 20.28 | 5.44 | 20.26 | 5.52 | 20.24 | 5.61 | 2 C .21 | 5.70 | 21 |
| 22 | 21.25 | 5.69 | 21.23 | 5.79 | 21.20 | 5.88 | 21.17 | 5.97 | 22 |
| 23 | 22.22 | 5.95 | 22.19 | 6.05 | 22.16 | 6.15 | 22.14 | 6.24 | 23 |
| 24 | 23.18 | 6.21 | 23.15 | 6.31 | 23.13 | 6.41 | 23.10 | 6.51 | 24 |
| 25 | 24.15 | 6.47 | 24.12 | 6.58 | 24.09 | 6.68 | 24.06 | 6.79 | 25 |
| 26 | 25.11 | 6.73 | 25.08 | 6.84 | 25.05 | 6.95 | 25.02 | 7.06 | 26 |
| 27 | 26.08 | 6.99 | 26.05 | 7.10 | 26.02 | 7.22 | 25.99 | 7.33 | 27 |
| 28 | 27.05 | 7.25 | 27.01 | 7.36 | 26.98 | 7.48 | 26.95 | 7.60 | 28 |
| 29 | 28.01 | 7.51 | 27.98 | 7.63 | 27.95 | 7.75 | 27.91 | 7.87 | 29 |
| 30 | 28.98 | 7.76 | 28.94 | 7.89 | 28.91 | 8.02 | 28.87 | 8.14 | 30 |
| 31 | 29.94 | 8.02 | 29.91 | 8.15 | 29.87 | 8.28 | 29.84 | 8.41 | 31 |
| 32 | 30.91 | 8.28 | 30.87 | 8.42 | 30.84 | 8.55 | 30.80 | 8.69 | 32 |
| 33 | 31.88 | 8.54 | 31.84 | 8.68 | 31.80 | 8.82 | 31.76 | 8.96 | 33 |
| 34 | 32.84 | 8.80 | 32.80 | 8.94 | 32.76 | 9.09 | 32.72 | 9.23 | 34 |
| 35 | 33.81 | 9.06 | \|33.77 | 9.21 | 33.73 | 8.35 | 33.69 | 9.50 | 35 |
| 36 | 34.77 | 9.32 | 34.73 | 9.47 | 34.69 | 9.62 | 34.65 | 9.77 | 36 |
| 37 | 35.74 | 9.58 | 35.70 | 9.73 | 35.65 | 9.89 | 35.61 | 10.04 | 37 |
| 38 | 36.71 | 9.84 | 36.66 | 10.00 | 36.62 | 10.16 | 36.57 | 10.31 | 38 |
| 39 | 37.67 | 10.09 | 37.63 | 10.26 | 37.58 | 10.42 | 37.54 | 10.58 | 39 |
| 40 | 38:64 | 10.35 | 38.59 | 10.52 | 38.55 | 10.69 | 38.50 | 10.86 | 40 |
| 41 | 39.60 | 10.61 | 39.56 | 10.78 | 39.51 | 10.96 | 39.46 | 11.13 | 41 |
| . 42 | $40.5{ }^{\circ}$ | 10.87 | 40.52 | 11.05 | 40.47 | 11.22 | 40.42 | 11.40 | 42 |
| 43 | 41.53 | 11.13 | 41.49 | 11.31 | 41.44 | 11.49 | 41.39 | 11.67 | 43 |
| - 44 | 42.50 | 11.39 | 42.45 | 11.57 | 42.40 | 11.76 | 42.35 | 11.94 | 44 |
| 45 | 43.47 | 11.65 | 43.42 | 11.84 | 43.36 | 12.03 | 43.31 | 12.21 | 45 |
| 46 | 44.43 | 11.91 | 44.38 | 12.10 | 44.33 | 12.29 | 44.27 | 12.49 | 46 |
| -47 | 45.40 | 12.16 | 45.35 | 12.36 | 45.29 | 12.56 | 45.24 | 12.76 | 47 |
| 48 | 46.36 | 12.42 | :46.31 | 12.63 | 46.25 | 12.83 | 46.20 | 13.03 | 48 |
| - 49 | 47.33 | 12.68 | 47.27 | 12.89 | 47.22 | 13.09 | 47.16 | 13.30 | 49 |
| 50 | 48.30 | 12.94 | 48.24 | 13.15 | 48.18 | 13.36 | 48.12 | 13.57 | 50 |
|  | Dep | Lat. | Dep | Lat. | Dep | Lat. | Dep. | Lat. |  |
| 75 Deg. 743 Deg. $74 \frac{1}{2}$ Deg. $74_{4}$ Deg |  |  |  |  |  |  |  |  |  |


| $5$ |  |  |  |  | $15 \frac{1}{2} \mathrm{Deg} \\|^{153 \mathrm{Deg}}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. | Lat. D | Dep. |  | ep. | Lat. | Dep. |  |
| 51 | 4, | 13.20 | 49.2013 | 13.41 | 49.15 | 13.63 |  |  | 51 |
| 52 | 50.23 | 13.46 | 50.1713 | 13.68 | 50.11 | 13.90 | 50.05 |  | 52 |
| 53 | 51.19 | 13.72 | 51.1313 | 13.94 | 51.07 | 14.16 | 51.01 | 14.39 | 53 |
|  | 52.16 | 13.98 | 52.10 | 14.20 | 52.04 | 14.43 | 51.97 |  | 54 |
| 55 | 53.13 | 14.24 | 53.06 1 | 14.47 | 53.00 | 14.70 | 52.94 | 4.93 | 55 |
| 56 | 54.09 | 14.49 | 54.03 1 | 14.73 | 53.96 | 14.97 | 53.90 | 15.20 | 56 |
| 57 | 55.06 | 14.75 | 54.991 | 14.99 | 54.93 | 15.23 | 54.86 | 15.47 | 7 |
| 58 | 56.02 | 15.01 | 55.96 | 15.26 | 55.89 | 15.50 | 55.82 | 15.74 | 8 |
| 59 | 56.99 | 15.27 | 56.92 | 15.52 | 56,85 | 15.77 | 56.78 | 16.01 | 59 |
| 60 | 57.96 | 15.53 | 57.89 | 15.78 | 57.82 | 16.03 | 57.75 |  | 60 |
| 61 | 58.92 | 15.79 | 58.85 | 16.04 | 58.7 | 16.30 | 58. |  | 61 |
|  | 59.89 | 16.05 | 59.821 | 16.31 | 59.75 | 16.57 | 59.6 |  |  |
|  | 60.85 | 16.31 | 60.781 | 16.57 | 60.71 | 16.8 | 60. | 17.10 | 3 |
|  | 61.82 | 16.56 | 61.751 | 16.83 | 61.67 | 17.10 | 61.6 | 17.37 | 64 |
| 65 | 62.79 | 16.82 | '62.71 | 17.10 | 62.64 | 17.37 | 62.5 | 17.64 | 65 |
|  | 63.75 | 17.08 | 63.681 | 17.36 | 63.60 | 17.64 | 63.5 | 17.92 | 66 |
| 67 | 64.72 | 17.34 | 64.641 | 17.62 | 64.56 | 17.90 | 64.48 | 18.19 | 7 |
| 68 | 65.68 | 17.60 | 65.611 | 17.89 | 65.53 | 18.17 | 65.45 | 18.4 | 8 |
| 69 | 66.65 | 17.86 | 66.571 | 18.15 | 66.49 | 18.44 | 66.41 | 18.73 | 69 |
| 70 | 67.61 | 18.12 | 67.541 | 18.41 | 67.45 | 18.7 | 67.37 |  | 0 |
|  | 68. | 18.38 | 68.50 | 析 | 68.42 | 18.97 |  |  | 71 |
| 72 | 69.55 | 18.63 | 69.46 | 18.94 | 69.38 | 19.24 | 69. |  | 72 |
| 73 | 70.51 | 18.89 | 70.431 | 19.20 | 70.35 | 19.51 | 70.26 | 19 | 3 |
|  | 71.48 | 19.15 | 71.391 | 19.46 | 71.31 | 19.78 | 71.22 | 20 | - |
|  | 72.44 | 19.41 | 72.36 | 19.73 | 72.27 | 20.04 | 72.18 | 20.3 | 5 |
|  | 73.41 | 19.67 | 73.32 | 19.99 | 73.24 | 20.31 | 73.15 | 20. | 6 |
|  | 74.38 | 19.93 | 74.29 | 20.25 | 74.20 | 20.58 | 74.11 | 20. | 77 |
| 78 | 75.34 | 20.19 | 75.25 | 20.52 | 75.16 | 20.84 | 75.0 | 21.1 | 78 |
|  | 76.31 | 20.45 | 76.22 | 20.78 | 76.13 | 21.11 | 76.0 | 21 | 79 |
| 80 | 77.27 | 20.71 | 77.1 | 1 | 77.0 | 1 | 77. |  |  |
|  | 78.2 | 20.96 | 78.15 | 21.31 | 78.0 | 21.65 |  |  | 81 |
|  | 79.21 | 21.22 | 79.112 | 21.57 | 79.02 | 21.91 | 78.9 | 22.26 |  |
|  | 80.17 | 21.48 | 80.082 | 21.83 | 79.98 | 22.18 | 79.88 | 22.53 |  |
|  | 81.14 | 21.74 | 81.042 | 22.09 | 80.94 | 22.45 | 80.85 |  |  |
| 85 | 82.10 | 22.00 | 82.01 | 22.36 | 81.91 | 22.72 | 81.81 | 23.07 | 85 |
| 86 | 3.07 | 22.26 | 82.97 | 22.62 | 82.87 | 22.98 | 82.77 | 23.3 | 86 |
| 87 | 84.04 | 22.52 | 83.94 | 22.88 | 83.84 | 23.25 | 83:73 | 23.62 |  |
| 88 | 85.00 | 22.78 | 84.90 | 23.15 | 84.80 | 23.52 | 84.70 | 23.89 |  |
|  | 85.97 | 23.03 | 85.87 | 23.41 | 85.76 | 23.78 | 85.66 | 24.1 |  |
| 90 | 86.9 | 29 | 86.83 | . 67 | 86. | 24.05 | 86.62 |  |  |
|  | 87. | 23.55 | 87.8 | 23.94 | 87.6 | 24.32 |  |  | 91 |
| 92 | 88.87 | 23.81 | 88.76 | 24.20 | 88.65 | 24.59 | 88.55 | 24.97 | 92 |
|  | 89.83 | 24.07 | 89.73 | 24.46 | 89.62 | 24.85 | 89.51 | 25.2 |  |
|  | 90.80 | 24.33 | 90.69 | 24.72 | 90.58 | 25.12 | 90.47 | 25.52 |  |
|  | 91.76 | 24.59 | 91.65 | 24.99 | 91.54 | 25.39 | 91.43 | 25.79 | 95 |
| 96 | 92.73 | 24.85 | 92.62 | 25.25 | 92.51 | 25.65 | 92.40 | 26.0 | 96 |
| 51 | 93.69 | 25.11 | 93.58 | 25.51 | 93.47 | 25.92 | 93.36 | 26.33 |  |
|  | 94.66 | 25.36 | 94.55 | 25.78 | 94.44 | 26.19 | 94. | 26.6 |  |
|  | 95.63 | 25.62 | 95.51 | 26.04 | 95.40 | 26.46 | 95.23 | 26.87 | 99 |
| 100 | 96. | 5.88 | 96.48 | 26.30 | 96.3 | 26.72 | 96.25 | 27. | 100 |
|  |  |  | De |  |  |  | Dep | Lat. |  |
|  | 75 |  |  |  |  |  |  |  |  |



TRAVERSE TABLE.

| $\begin{gathered} \square \\ \square \\ \rightarrow \end{gathered}$ | 16 Deg. |  | $16 \frac{1}{4}$ Deg. |  | $16 \frac{1}{2}$ Deg. |  | $16_{4}^{3} \mathrm{Deg}$. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep |  |  |  |  | t. | p. |  |
|  |  |  |  |  |  |  |  |  | 1 |
| 52 | 49.9 | 14.33 | 49.9 | 14.55 | 49.86 | 14.77 | 49.79 | 14.99 | 52 |
| 53 | 50.95 | 14.61 | 50.88 | 4.83 | 50.82 |  | 50.75 |  | 53 |
| 54 | 51.91 | 14.88 | 51.8 | 5.11 | 51.78 |  | 51.71 | 15.56 |  |
| 55 | 52.87 | 15.16 | 52.8 | 15.39 | 52.74 | 15.62 | 52.67 | 15.85 | 5 |
| 56 | 53.83 | 15.44 | 53.76 | 15.67 | 53.69 | 15.90 | 53.62 |  | 6 |
| 5 | 54.79 | 15.71 | 54.72 | 15.95 | 54.65 | 16.19 | 54.58 | 16.43 | 5 |
| 58 | 55.75 | 15.99 | 55.6 | 6.23 | 55.61 | 16.47 | 55.54 | 16.72 | 58 |
| 59 | 56.71 | 16.26 | 56.6 | 16.51 | 56.57 | 16.76 | 56.50 | 17.00 | 59 |
| 60 | 57.68 | 16.54 | 57.60 | 16.79 | 57.53 | 17.04 | 57.45 | 17.29 | 60 |
| 61 |  |  |  |  |  |  |  |  | 1 |
| 62 | 59. | 17.09 |  | 7.35 | 59.45 | 17.61 | 59.37 | 17.87 | 62 |
| 63 | 60.5 | 17.37 |  | 17.63 | 60.41 | 17.89 | 60.33 | 18.16 | 63 |
| 64 | 61.5 | 17.64 | 61.4 | 17.91 | 61.36 | 18.18 | 61.28 | 18.44 | 64 |
| 65 | 62.48 | 17.92 |  | 8.19 | 62.32 | 18.46 | 62.2 | 18.73 | 65 |
| 66 | 63.44 | 18.19 | 63.36 | 18.47 | 63.28 | 18.74 | 63.20 | 19 | 66 |
| 67 | 64.40 | 18.47 | 64.32 | 18.75 | 64.24 | 19.03 | 64.16 | 19.31 | 67 |
| 68 | 65.37 | 18.74 |  | 19.03 | 65.20 | 19.31 | 65.11 | 19.60 | 68 |
| 69 | 66.33 | 19.02 | 66.24 | 19.31 | 66.16 | 19.30 | 66.07 | 19 | 69 |
| 70 | 67.29 | 19.29 | 67.20 | 19.59 | 67.12 | 19.88 | 67.03 | 20.17 | - |
| 71 |  |  |  |  |  |  |  |  | 71 |
| 72 | 69.2 | 19.85 | 69.1 | 0.15 | 69.03 |  | 68.95 | 75 | 72 |
| 73 | 70.17 | 20.12 |  | 0.43 | 69.99 | 20.73 | 69. |  | 73 |
| 74 | 71. | 20.40 |  | 0.71 | 70.95 | 21.02 | 70. | 21.33 | 74 |
| 75 | 72.09 | 20.67 | 72.00 | 2.99 | 71.91 | 21.30 | 71.82 | 21.61 | 75 |
| 76 | 73.0 | 20.95 | 72.9 | 2.27 | 72.87 | 21.59 | 72.7 |  | 76 |
| 77 | 74.02 | 21.22 | 73.92 | 21.55 |  | 21.87 | 73.73 |  | 77 |
| 78 | 74.98 | 21.50 | 74.88 | 21.83 | 74.79 | 22.15 | 74.69 | 22.48 | 78 |
| 79 | 75. | 21.78 |  | 22.11 | 75.75 | 22.44 | 75. | 22.77 | 9 |
| 80 | 76.90 | 22.05 |  | 22.39 |  | 22 |  | 23.06 | 80 |
| 8 |  | 22.33 |  |  | 77.66 | 23.01 | 77.56 |  | 1 |
| 8 | 78.82 | 22.60 | 73.72 | 22.95 | 78.62 | 22.29 | 78.52 | 23.63 | 82 |
| 83 | 79.78 | 22.88 | 79.68 | 23.23 | 79. | 23.57 | 79. | 23.92 | 3 |
| 8 | 80.75 | 23.15 | 80.64 | 23.51 | 80. | 23.86 | 80.44 | 24.21 | 84 |
| 85 | 81.71 | 23.43 | 81.60 | 23.79 | 81.5 | 24.14 | 81.39 | 34.50 | 85 |
| 86 | 82.67 | 23.70 | 82.56 | 24.07 | 82.46 | 24.43 | 82.35 | 24.78 | 86 |
| 87 | 63.63 | 23.98 | 83.52 | 24.35 | 83.42 | 24.71 | 83.31 | . 07 |  |
| 85 | 84.59 | 24.26 | 84.4 | 24.62 | 84.38 | 24.99 | 84.27 | 25.36 | 88 |
| 89 | 85.55 | 24.53 | 85.44 | 24.90 | 85.33 | 25.28 | 85.22 | . 65 | 89 |
| 90 | 86.51 | 24.8 |  | 25.18 | 86.29 | 25.56 | 86.18 |  | 90 |
| 91 |  | 25.08 | 87.36 | 25.46 | 87.25 | 25.85 |  | 23 | 91 |
| 9 | 88.44 | 25.36 | 88.32 | 25.74 | 88. | 26.13 | 88. | 6.51 | 92 |
| 93 | 89.40 | 25.63 | 89,28 | 26.02 | 89.1 | 26.41 | 89.0 | 6.80 | 93 |
| 94 | 90.36 | 25.9 | 90.2 | 26.30 | 90. | 26.70 | 90.0 | 09 | 94 |
|  | 91.32 | 26.19 | 91.20 | 26.58 | 91 | 26.98 | 90.9 | 7.38 | 95 |
| 96 | 92.28 | 26.46 | 92.16 | 26.86 |  | 27.27 | 91.93 | 27.67 | 96 |
| 97 | 93,2 | 26.74 | 93.1 | 27.14 | 93. | 55 | 92.8 | 5 | 97 |
|  | 94.20 | 27.01 | 94.08 | 27.42 | 93.9 | 27.83 | 93. | 28.24 |  |
|  | 95.16 | 27.29 | 95.04 | 27.70 | 94.92 | 28.12 |  | 28.53 | 99 |
| 100 | 96.13 | 27.56 | 96.00 | 27.98 | 95.88 | ,28.40 | 95.76 | 28 | 00 |
|  | Dep | Lat. | D | Lat. |  | Lat. | Dep. | . |  |
|  | $74 \text { Deg. } 73 \frac{3}{4} \text { Deg. } 73 \frac{1}{2} \text { Deg. } 73 \frac{1}{4} \text { Deg. }$ |  |  |  |  |  |  |  |  |



| $1 \begin{gathered} \square \\ \stackrel{6}{?} \\ \hline \end{gathered}$ | 17 D | g. | $17 \frac{1}{4} \mathrm{D}$ | eg. | 171 ${ }^{2}$ | Deg. | $17 \frac{3}{4}$ D | eg. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. D | Dep. | Lat. ${ }^{\text {D }}$ | Dep. | Lat. ${ }^{\text {D }}$ | Dep. | Lat. | Dep. |  |
| 514 | 48.771 | 14.91 | 48.711 | 15.12 | 48.641 | 15.34 | 48.57 | 15 | 51 |
| 524 | 49.7315 | 15.20 | 49.66 | 15.42 | 49.59 | 15.64 | 49.52 | 15.85 | 52 |
| 535 | 50.681 | 15.50 | 50.62 | 15.72 | 50.55 | 15.94 | 50.48 | 16.16 | 53 |
| 545 | 51.641 | 15.79 | 51.57 | 16.01 | 51.50 - | 16.24 | 51.43 | 16.46 | 54 |
| 55 | 52.6016 | 16.08 | 52.53 | 16.31 | 52.45 | 16.54 | 52.38 | 16.77 | 55 |
| 56 | 53.5516 | 16.37 | 53.48 | 16.61 | 53.41 | 16.84 | 53.33 | 17.07 | 56 |
| 575 | 54.5116 | 16.67 | 54.44 | 16.90 | 54.36 | 17.14 | 54.29 | 17.38 | 57 |
| 585 | 55.4716 | 16.96 | 55.39 | 17.20 | 55.32 | 17.44 | 55.2 | 17.68 | 58 |
| 595 | 56.4217 | 17.25 | 56.35 | 17.50 | 56.27 | 17.74 | 56.19 | 17.99 | 58 |
| 60 | 57.38 | 17.54 | 57.30 | 17.78 | 57.22 | 18.04 | 57.14 |  | 60 |
| 615 | 58.331 | 17.83 | 58.26 | 18.09 | 58.18 | 18.34 | 58.10 | 18.60 | 61 |
| 625 | 59.29 181 | 18.13 | 59.21 | 18.39 | 59.13 | 18.64 | 59.05 | 18.90 | 62 |
| 636 | 60.2518 | 18.42 | 60.17 | 18.68 | 60.08 | 18.94 | 60.00 | 19.21 | 63 |
| 646 | 61.20 | 18.71 | 61.12 | 18.98 | 61.04 | 19.25 | 60.95 | 19.51 | 64 |
| 65 | 62.161 | 19.40 | 62.08 | 19.28 | 61.99 | 19.55 | 61.91 | 19.82 | 65 |
| 66 | 63.12 | 19.30 | 63.03 | 19.57 | 62.95 | 19.85 | 62.86 | 20.12 | 66 |
| 676 | 64.07 | 19.59 | 63.99 | 19.87 | 63.90 | 20.15 | 63.81 | 20.43 | 67 |
| 68 | 65.031 | 19.88 | 64.94 | 20.16 | 64.85 | 20.45 | 64.76 | 20.73 | 68 |
| 69 | 65.992 | 20.17 | 65.90 | 20.46 | 65.81 | 20.75 | 65.72 | 21.04 | 69 |
| 70 | 66.94 | 2.47 | 66.85 | 20.76 | 66.76 | 21.05 | 66.67 |  | 0 |
| 71 | 67.90 | 20.76 | 67.81 | 21.05 | 67.71 | 21.35 | 67.62 | 21.65 | 7 |
| $\begin{gathered} 7236 \\ 7316 \end{gathered}$ | 63.85 | 21.05 | 68.76 | 21.35 | 68.67 | 21.65 | 68.57 | 21.95 | 72 |
|  | 69.812 | 21.34 | 69.72 | 21.65 | 69.62 | 21.95 | 69.58 | 22.26 | 3 |
| 74 | 70.772 | 21.64 | 70.67 | 21.94 | 70.58 | 22.25 | 70.48 | 22.56 | 74 |
|  | 71.72 | 21.93 | 71.63 | 22.24 | 71.53 | 22.55 | 71.43 | 22.86 | 75 |
|  | 72.68 | 22.22 | 72.58 | 22.54 | 72.48 | 22.85 | 72.38 | 23.17 | 76 |
| 77 | 73.64 | 22.51 | 73.54 | 22.83 | 73.44 | 23.15 | 73.3 | 3.4 | 77 |
| $\begin{aligned} & 78 \\ & 79 \end{aligned}$ | 74.59 | 22.80 | 74.49 | 23.13 | 74.39 | 23.46 | 74.29 | 23.78 | 78 |
|  | 75.55 | 23.10 | 75.45 | 23.43 | 75.34 | 23.76 | 75.24 | 24.0 | 79 |
| 80 | 76.50 | 23.39 | 76.40 | 23.72 | 76.30 | 24.06 | 76.19 | 24.38 | 80 |
| 81 | 77.46 | 23.68 | 77.36 | 24.02 | 77.25 | 24.36 | 77.14 | 24.69 | 81 |
| 8 | 78.42 | 23.97 | 78.31 | 24.32 | 78.20 | 24.66 | 78.10 | 25.00 | 82 |
|  | 79.37 | 24.27 | 79.27 | 24.61 | 79.16 | 24.96 | 79.05 | 525.30 | 83 |
| 8384858 | 80.33 | 24.56 | 80.22 | 24.91 | 80.11 | 25.26 | 80.00 | 25.61 | 84 |
|  | 81.29 | 24.85 | 81.18 | 25.21 | 81.07 | 25.56 | 80.95 | 25.91 | 85 |
| 86 | 82.24 | 25.14 | 82.13 | 25.50 | 82.02 | 25.86 | 81.91 | 26.22 | 86 |
| 8788 | 83.20 | 25.44 | 83.09 | 25.80 | 82.97 | 26.16 | 82.86 | 26.52 | 87 |
|  | 84.15 | 25.73 | 84.04 | 26.10 | 83.93 | 26.46 | 83.81 | 26.83 | 88 |
| 8990 | 85.11 | 26.02 | 85.00 | 26.39 | 84.88 | 26.76 | 134.76 | 627.13 | 89 |
|  | 86.07 | 26.31 | 85.95 | 26.69 | 85.83 | 27.06 | 85.7 | 27 | 90 |
| 91 | 87.02 | 26.61 | 86.91 | 26.99 | 86.79 | 27.36 | 86. | 27. | 91 |
| 92 | 87.98 | 26.90 | 87.86 | 27.28 | 87.74 | 27.66 | 87.62 | 28.05 | 92 |
|  | 88.94 | 27.19 | 88.82 | 27.58 | 88.70 | 27.97 | 88.57 | 728.35 | 93 |
| 93 94 | 89.89 | 27.48 | 89.77 | 27.87 | 89.65 | 28.27 | 89.53 | 328.66 | 94 |
| 9596 | 90.85 | 27.78 | 90.73 | 328.17 | 90.60 | 28.57 | 90.48 | 828.96 | 95 |
|  | 91.81 | 28.07 | 91.68 | 28.47 | 91.56 | 28.87 | 91.43 | 329.27 | 96 |
| 97 | 92.76 | 28.36 | 92.64 | 28.76 | 92.51 | 29.17 | 92.38 | 829.57 | 97 |
|  | 93.72 | 28.65 | 93.59 | 29.06 | 93.46 | 29.47 | 93.33 | 329.88 | 88 |
| $\left.\begin{gathered} 98 \\ 99 \\ 100 \end{gathered} \right\rvert\,$ | 94.67 | 28.94 | 94.55 | 529.36 | 94.42 | 29.77 | 94.29 | 930.18 | 99 |
|  | 95.6 | 29.24 | 95.50 | 029.65 | 95.37 | 30.07 | 95.24 | 430.49 | 100 |
| $\stackrel{\dot{0}}{\dot{0}}$ | Dep | Lat. | Dep | Lat. | Dep | Lat. | De | Lat. |  |
|  |  |  | 72 | Deg. | 72 | eg | 72 | Deg. |  |
|  |  |  |  |  | 15 |  |  |  |  |



|  |  |  |  |  |  | Dep. |  | Dep. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 48 | 15.76 | 48.4 | 15.9 | 48.3 | 16.18 | 48.29 | 39 | 1 |
|  | 49.45 | 16.07 | 49.3 | 16.28 | 49.3 | 16.50 | 49.24 | 16.71 | 52 |
|  | 50.41 | 16.38 | 50.33 | 16.60 | 50.26 | 16.82 | 50.19 | 7.04 | 3 |
|  | 1. | 16.69 | 51.28 | 16.91 | 51.21 | 17.13 | 51.13 | 7.86 | 4 |
|  | 52.3 | 17.00 | 52.23 | 17.22 | 52.16 | 17.45 | 52.08 | 88 | 5 |
|  | 53.26 | 17.30 | 53.18 | 17.54 | 53.11 | 17.77 | 53.03 | 00 | 6 |
|  | 54.21 | 17.61 | 54.13 | 17.85 | 54.05 | 18.09 | 53.98 | 32 | 7 |
|  | 55.16 | 17.92 |  |  | 55.00 | 18.40 | 54,9 | 18.64 | $58$ |
| 59 69 | 56.11 | 8.2 | 56.0 | 8. | 55.95 | 18.72 | 55.8 | 18.96 19.29 | - |
| 60 |  |  |  |  | .90 |  |  |  |  |
| 61 |  |  |  |  |  |  |  |  |  |
|  | 58 | 9.1 |  | 9.42 |  | 19.6 | 58.7 | 3 |  |
|  | 59.92 | 19.47 | 59.83 | 19.73 | 59.74 | 19.99 | 59.66 | 0.25 |  |
|  | 60.87 | 19.78 | 60.78 | 20.04 | 60.69 | 20.31 | 60.6 | 0.57 |  |
|  | 61.82 | 20.09 | 61.73 | 20.36 | 61.6 | 20.6 | 61.55 | 20.89 | 65 |
|  | 62.77 | 20.40 | 62.68 | 20.67 | 62.5 | 20.9 | 62.5 | 21.22 | 66 |
|  | 63.72 | 20.70 | 63.63 | 20.98 | 63.5 | 21.26 | 63. | 21.54 |  |
|  | 64.6 | 21.01 | 64.58 | 21.30 | 64.4 | 21.5 | 64. | 21.86 | 68 |
|  | 65.62 | 21.32 | 65.53 | 21.61 | 65.43 | 21.8 | 65.3 |  | 69 |
| 70 | 66.5 | 21.63 | 66.48 | 21.92 | 66.38 | 22.21 | 66. |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  | 68.4 | 22.25 | 68.38 | 22.55 | 68.28 | 22.85 | 68.18 | 14 | 72 |
|  | 69.4 | 22.56 | 69.33 | - | 69.23 | 23.16 | 69.13 |  | 位 |
|  | 70.38 | 22.87 | 70.28 | 23.17 | 70.18 | 23.48 | 70.07 | 79 |  |
|  | 71.3 | . 18 | 71.23 | 23.49 | 71.1 | . | 71.0 | 4.11 |  |
|  | 72.28 | 23.49 | 72.18 | 23.80 | 72.07 | 24.12 | 71.97 | 43 |  |
|  | 73.23 | 23.79 | 73.13 | 24.11 | 73.02 | 24.43 | 72.91 | 4.75 | 7 |
|  | 74.18 | 24.10 | 74.08 | 24.43 | 73.97 | 24.75 | 73. | 25.07 |  |
|  | 75.1 | 24.41 | 75.03 | 24.74 | 74.92 | 25.07 | 74.81 | 25.39 | 79 |
| 80 |  | 24.72 | 75.98 | 25.05 | 75.87 | 25.38 | 75.7 |  |  |
|  |  |  |  | 5.37 |  |  |  |  |  |
|  |  | $25 .$ |  | 25.68 | $\begin{array}{r} 0.01 \\ 77.76 \end{array}$ | $26.02$ |  |  |  |
|  | 78.9 | 25.65 | 78.33 | 25.99 | 78.71 | 26.34 | 78.6 | 26.68 | 3 |
|  | 79.89 | 25.96 | 79.77. | 26.31 | 79.66 | 26.65 | 79.5 | 7.0 |  |
|  | 80.8 | 6.27 | . 72 | 28.62 | 80.61 | 26.97 |  |  | 85 |
|  | 81.79 | 26.58 | 81.67 | 26.93 | 81.56 | 27.29 | 81. | 27.64 | 86 |
|  | 82.74 | 26.88 | 82.62 | 27.25 | 82.50 | 27.61 | 82.3 | 7.97 | 7 |
|  |  | 27.19 | 83.57 | 27.56 | 83.45 | 27.32 | 83.3 | 88.29 | 8 |
|  | 84 | 27.50 | 84.52 | 27.87 | 84.40 | 28.24 | 84.28 | 28.61 | 89 |
| 90 | 85.60 | 27.81 | 85.47 | 28.18 | 85.35 | 28.56 | 85.22 |  | 0 |
|  |  |  |  |  |  | 28.87 |  |  | 91 |
|  | 87.5 | 28.43 | 87.37: | 28.81 | 87.25 | 29.19 | 87.1 | 2.57 | 92 |
|  | 88.45 | 28.74 | 88.32 | 29.12 | 88.19 | 29.51 | 88.06 | 29.89 | 3 |
|  | 89.40 | 29.05 | 89.27 | 29.44 | 89.14 | 29.83 | 89.01 | 30.22 | - |
|  | 90.35 | 9.36 | 90.22 | 29.75 | 90.0 | 3.14 | 9, | 0.54 | 95 |
|  | 91.30 | 29.67 | 91.17 | 30.06 | 91.04 | 30.46 | 90.9 | 30.86 | 96 |
|  | 92.25 | 29.97 | 92.12 | 30.38 | 91.99 | 30.78 | 91.8 | 31.18 | 7 |
|  | 93.20 | 0.28 | 93.07 | 30.69 | 92.9 | 31.10 | 92. | 31.5 | 98 |
|  | 94.15 | 30.59 | 94.02 | 31.00 | 93.88 | 31.41 |  |  | 9 |
| 100 | 95.11 | 30.90 | 94.97 | 31.32 | 94.83 | 31.73 | 94 |  |  |
|  | Dep. | Lat. | D | t. | De | Lat. | Dep |  |  |
|  |  |  |  |  |  |  |  |  |  |




|  | 20 Deg. |  | 2019 Deg. |  | $20 \frac{1}{2}$ Deg. ${ }^{20}{ }_{4}^{3} \mathrm{Deg}$. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. |  |  | Dep. | Lat. | Dep. |  | Dep: |  |
|  | 0.94 | 0.34 | 0.94 |  | 0.94 | 0.35 | 0.94 | 0.35 |  |
| 2 | 1.88 | 0.68 | 1.88 | 0.69 | 1.87 | 0.70 | 1.87 | 0.71 |  |
| 3 | 2.82 | 1.03 | 2.81 | 1.04 | 2.81 | 1.05 | 2.81 | 1.06 |  |
|  | 3.76 | 1.37 | 3.75 | 1.38 | 3.75 | 1.40 | 3.7 | 1.42 |  |
| 5 | 4.70 | 1.71 | 4.69 | 1.73 | 4.68 | 1.75 | 4.6 | 1.77 |  |
| 6 | 5.64 | 2.05 | 5.63 | 2.08 | 5.62 | 2.10 | 5.6 | 2.13 |  |
| 7. | 6.58 | 2.39 | 6.57 | 2.4 | 6.5 | 2.45 | 6.55 | 2.48 |  |
| 8 | 7.52 | 2.74 | 7.51 | 2.77 | 7.49 | 2.80 | 7.48 | 2.83 |  |
| 9 | 8.46 | 3.08 | 8.44 | 3.12 | 8.43 | 3.15 | 8.42 | 3.19 |  |
| 10 | 9.40 | 3.42 | 9.38 | 3.46 | 9.37 | 3.50 | 9.35 | 3.54 |  |
|  | 10.34 | 3.76 | 10.32 | 3.81 | 10.30 | 3.85 | 10.29 | 3.90 | 1 |
|  | 11.28 | 4.10 | 11.26 | 4.15 | 11.24 | 4.20 | 11.22 | 4.25 | 2 |
|  | 12.22 | 4.45 | 12.20 | 4.50 | 12.18 | 4.55 | 12.16 | 4.61 | 3 |
|  | 13.16 | 4.79 | 13.13 | 4.85 | 13.11 | 4.9 | 13.09 | 4.96 | 4 |
|  | 14.10 | 5.13 | 14.07 | 5.19 | 14.05 | 5.25 | 14.03 | 5.31 | 5 |
| 1615 | 15.04 | 5.47 | 15.01 | 5.54 | 14.99 | 5.60 | 14.96 | 5.67 |  |
| 1715 | 15.97 | 5.81 | 15.95 | 5.88 | 15.92 | 5.95 | 15.90 | 6.02 | 7 |
|  | 16.91 | 6.16 | 16.89 | 6.23 | 16.86 | 6.30 | 16.83 | 6.38 | 8 |
|  | 17.85 | 6.50 | 17.83 | 6.58 | 17.80 | 6.65 | 17.77 | 6.73 | - |
|  | 18.79 | 6.84 | 18.76 | 6.92 | 18.73 | 7.00 | 18.70 | 7.09 |  |
|  | 19.73 | 18 | 19.70 | 7.27 | 19. | 35 | 19. |  | 1 |
|  | 20.67 | 7.52 | 20.64 | 7.61 | 20.61 | 7.70 | 20.5 | 7.79 | 2 |
| 232 | 21.61 | 7.87 | 21.58 | 7.96 | 21.54 | 8.05 | 21.51 | 8.15 |  |
|  | 22.55 | 8.21 | 22.52 | 8.31 | 22.48 | 8.40 | 22.44 | 8.50 |  |
| 25 | 23.49 | 8.55 | 23.45 | 8.65 | 23.42 | 8.76 | 23.3 | 8.86 | 5 |
| 26 | 24.43 | 8.89 | 24.39 | 9.00 | 24.35 | 9.11 | 24.3 | 9.21 | 6 |
| 2725 | 25.37 | 9.23 | 25.33 | 9.35 | 25.25 | 9.46 | 25.25 | 9.57 |  |
| 2826 | 26.31 | 9.58 | 26.27 | 9.69 | 26.23 | 9.81 | 26.18 | 9.92 |  |
|  | 27.25 | 9.92 | 27.21 | 10.04 | 27.16 | 10.16 | 27.12 | 10.27 | 9 |
| 30 | 28.10 | 10.26 | 28.1 | 10.38 | 28.10 | 10.51 | 28.05 | 10.63 | 30 |
| 3129 | 29.13 | . 60 | 9,08 | 10.73 | 29.0 | 10.86 | 28.99 | 10.98 | 1 |
| 3230 | 30.071 | 10.94 | 30.02 | 11.08 | 29.97 | 11.21 | 29.92 | 11.34 |  |
| 333 | 31.011 | 11.29 | 30.96 | 11.42 | 30.91 | 11.56 | 30.86 | 11.69 | 33 |
| 343 | 31.951 | 11.63 | 31.901 | 11.77 | 31.85 | 11.91 | 31.79 | 12.05 | 4 |
| 3532 | 32.891 | 11.97 | 32.84 | 12.11 | 32.78 | 12.26 | 32.73 | 12.40 | 35 |
|  | 33.831 | 12.31 | 33.771 | 12.46 | 33.72 | 12.61 | 33.66 | 12.75 | 36 |
| 373 | 34.771 | 12.65 | 34.71 | 12.81 | 34.66 | 12.96 | 34.60 | 13.11 | 37 |
| 3835 | 35.711 | 13.00 | 35,651 | 13.15 | 35.59 | 13.31 | 35.54 | 13.46 | 38 |
| 3936 | 36.65 | 13.34 | 36.59 | 13.50 | 36.53 | 13.66 | 36.47 | 13.82 | - |
| 4037 | 37.5918 | 13.68 | 37.531 | 13.84 | $37.4{ }^{\text {? }}$ | 14.01 | 37.41 | 14. | 0 |
| 418 | 38.53 | 14.02 | 38.47 | 14.19 | 38.40 | 14.36 | 38.34 | 14.53 | 41 |
| 4239 | 39.471 | 14.36 | 39.40 | 14.54 | 39.34 | 14.71 | 39.28 | 14.88 | 析 |
|  | 40.41 | 14.71 | 40.341 | 14.8 r | 40.28 | 15.06 | 40.21 | 15.23 | 3 |
| 44 | 41.351 | 15.05 | 41.281 | 15.23 | 41.21 | 15.41 | 41.15 | 15.59 | 44 |
| 45 | 42.291 | 15.39 | 42.22 | 15.58 | 42.15 | 15.76 | 42.08 | 15.94 | 45 |
| 46 | 43.231 | 15.73 | 42.161 | 15.92 | 43.09 | 16.11 | 43.02 | 16.30 | 46 |
|  | 44.171 | 16.07 | 44.091 | 16.27 | 44.02 | 16.46 | 43.95 | 6.65 | 47 |
| 48 | 45.111 | 16.42 | 45.031 | 16.61 | 44.96 |  | 44.89 | 17.01 | 48 |
| 49 | 46.041 | 16.76 | 45.971 | 16.96 | 45.90 | 17.16 | 45.82 | 7.36 | 49 |
| 504 | 46.981 | 17.10 | 46 | 17.31 | 46.83 | 17. | 46. | 7.71 | 0 |
|  | Dep. | Lat. | De | Lat. | Dep | Lat. | Dep |  |  |

TRAVERSE TABLE.

| $0$ | 20 Deg . |  | 201 Deg. |  | $20 \frac{1}{2}$ Deg. |  | $20 \frac{3}{4}$ Deg. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. |  |  | Lat. ${ }^{\text {d }}$ | D | L |  |  |
| 51 | 47.92 |  |  |  |  |  | 47. |  |  |
|  | 48.8 | 17.79 |  |  | 48.71 | 18.21 |  | 18.42 | 52 |
|  | 49.80 | 18.13 | 49.72 | 18.34 | 49.64 | 18.56 |  |  | 53 |
|  | 50.74 | 18.47 | 50.6 | 18.69 | 50.58 | 18.91 |  | 19.13 |  |
|  | 51.68 | 18.81 |  |  | 51.52 | 19.26 |  | 19.4 |  |
|  | 52 | 19.15 | 52.54 | , | 52.45 | 19.61 |  |  | 6 |
|  | 53.56 | 19.50 | 53.48 | 19.73 | 53.39 | 19.9 | 53 | 2.19 | 57 |
|  | 54.50 | 19.84 | 54.42 | 20.07 | 54.3 | 20.3 | 54. | 2.55 | 58 |
|  | 55.4 | 20.18 | 55.35 | 20.42 | 55.2 | 20.66 |  | 2.90 | 59 |
| 60 |  | 20.52 | 56.29 | 0.77 | 56.2 | 1 |  |  | 60 |
|  |  |  |  |  |  |  |  |  | 61 |
| 62 |  |  | 58.1 | . | 58.0 | 21.71 |  |  |  |
| 63 | 59.20 |  | 59.1 | 21.81 | 59.0 | 22.0 |  | 23 | 3 |
|  | 60.14 | 21. | 60.0 | 22.15 | 59.9 | 22. | 59. | 2.67 | 64 |
| 65 | 61. | 22.23 | 60.98 | 22.50 | 60.8 | 22. | 60. | . 03 | 65 |
|  | 62.02 | 22.57 | 61.92 | 22.84 | 61.8 | 23.11 | 61. |  |  |
|  |  | 22.92 | 62.8 | 33.19 | 62.7 | 23.4 |  |  | 7 |
| 68 | 63.90 | 23.26 | 63.8 | 23.54 | 63.6 | 23.81 | 63. | 4.0 | 8 |
| 69 | 64. | 23.60 | 64.7 | , | 64.6 | 4.16 |  |  | 69 |
| 70 |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  | 24.8 |  |  |  |
| 72 |  | 24.63 | 67.5 | 24.92 | 67.4 | 25.21 |  | 25.51 | 2 |
|  | 68.60 | 24.97 | 68.49 | 25.27 | 68.38 | 25.57 |  |  | 73 |
|  |  | 25.31 | 69.4 | 25.61 | 69.31 | 25.92 |  |  | 4 |
|  | 0.48 | 25.65 | 70.36 | 25.96 | 70.25 | 26.27 | 70. | 6. | 75 |
| 76 | 71.4 | 25.99 | 71.3 | 6.30 | 71.1 | 6.6 |  |  | 36 |
|  | 72. | 26.34 | 72.2 | 26.65 | 72.1 | 26.9 |  |  | 7 |
|  | 73. | 26.68 | 73.18 | 27.00 | 73.06 | 27.32 |  | 7. | 8 |
|  | 74. | 27.02 | 74.12 | 27.34 | 74.0 | 27.67 | 73.8 | '27.99 | 9 |
| 80 | 75. |  | 75 |  |  | 28.02 |  |  |  |
|  |  |  |  |  |  |  |  |  | 1 |
|  |  | 28.05 | 76.93 | 28.38 | 76.81 | 28.72 |  |  | 2 |
|  | 77.9 | 8.39 | 77.87 | 28.73 | 77.74 | 29.07 |  |  | 3 |
|  | 78.93 | 8.73 | 78.81 | 29.07 | 78.6 | 29. |  |  | 84 |
|  |  | 29.07 | 79.75 | 29.42 | 79.62 | 29.7 |  |  |  |
| 86 | 30.8 | 29.41 | 80.68 | 29.77 | 80.55 | 30.1 |  |  |  |
|  | 81.7 | 29. | 81.6 | 30.11 | 81.4 | 30. |  |  | 87 |
| 88 | 82.69 | 30.10 | 82.5 | . 4 | 82. | 30.8 |  |  |  |
| 0 | 83.6 | 30.44 | 83.50 | 30.80 | 83.36 | 31.17 |  |  | 89 |
| 00 | 84.5 | 30.78 | 84.44 |  |  | 31.52 |  |  | 90 |
| 91 |  | 31.12 |  |  |  |  |  |  | 1 |
|  | 86.45 | 31.47 | 86.313 | 31.8 | 86.1 | 32.2 |  |  | 2 |
|  | 7.39 | 31.81 | 87.25 | 32.19 | 87.11 | 32.57 | 86.9 | 22.9 | 3 |
| 94 | 88.33 | 32.15 | 88.19 | 32.54 | 88.05 | 32.92 | 87.9 | 33.3 |  |
| 95 | 89.2 | 32.49 | 89.13 | 32.88 | 88.9 | 33.27 |  | 33.6 |  |
|  | 90.21 | 32.83 | 90.073 | 33.23 | 89.92 | 33.62 |  |  | 6 |
| 97 | 91.15 | 33.18 | 91.00 | 33.57 | 90.8 | 33.97 | 90. | 4.3 | 9 |
| 98 | 92.09 | 33.52 | 91.9 | 33.92 | 91.7 | 34.3 |  | 34.72 |  |
| 100 | 93.03 | 33.86 | 92.88 | 34.27 | 92.7 | 4.6 |  |  | 99 |
| 100 | 93.97 | 34.20 | 93. |  | 93.6 | - |  |  |  |
|  |  |  | Dep | Lat. |  | Lat. | Dep |  |  |
|  |  |  |  |  |  |  |  |  |  |


|  |  |  |  |  |  | Dep. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.93 | 0.36 | 0.93 | 0.3 | 0.93 | 0.3 | 0. 3 |  |  |
| 2 | 1.87 | 0.72 | 1.86 | 0.72 | 1.8 | 0.73 | 1.86 | 0.74 |  |
| 3 | 2.80 | 1.08 | 2.80 | 1.09 | 2.79 | 1.10 | 2.79 | 1.11 |  |
|  | 3.73 | 1.43 | 3.73 | 1.45 | 3.72 | 1.47 | 3.72 | 1.48 |  |
|  | 4.67 | 1.79 | 4.66 | 1.81 | 4.65 | 1.83 | 4.64 | 1.85 |  |
| 6 | 5.60 | 2.15 | 5.59 | 2.17 | 5.58 | 2.20 | 5.5 | . 2 |  |
| 7 | 6.54 | 2.51 | 6.52 | 2.54 | 6.51 | 2.57 | 6.5 | 2.59 |  |
| 8 | 7.47 | 2.87 | 7.46 | 2.90 | 7.44 | 2.93 | 7.43 |  |  |
| 9 | 8.40 | 3.23 | 8.39 | 3.26 | 8.37 | 3.30 | 8.36 | 3.34 |  |
| 10 | 9.34 | 3.58 | 9.32 | 3.62 | 9.30 | 3.67 | 9.29 |  |  |
|  | 10.27 | 3.94 | 10.25 | 3.99 | 10.23 | 4.0 | 10. |  |  |
|  | 11.20 | 4.30 | 11.18 | 4.35 | 11.17 | 4.40 | 11.15 |  |  |
|  | 12.14 | 4.66 | 12.12 | 4.71 | 12.10 | . 7 | 12.07 | , |  |
|  | 13.07 | 5.02 | 13.05 | 5.07 | 13.03 | 5.1 | 13.00 | 19 |  |
|  | 14.00 | 5.38 | 13.98 | 5.4 | 13.96 | 5.50 | 13. | 5.56 |  |
|  | 14.84 | 5.73 | 14.91 | 5.80 | 14.89 | 5.8 | 14. |  |  |
|  | 15.87 | 6.09 | 15.84 | 6.16 | 15.82 | 6.23 | 15.79 | 6.30 | 17 |
|  | 16.80 | 6.45 | 16.78 | 6.52 | 16.75 | 6.6 | 16.72 | 6.67 | 18 |
|  | 17.74 | 6.81 | 17.71 | 6.89 | 17.68 | 6.96 | 17.65 | 7.0 | 9 |
| 20 | 18.67 | 7.17 | 18,64 | 7.25 | 18.61 | 7.3 | 18.58 |  | 0 |
|  | 19.61 | 7.53 | 19.57 | 7.61 | 19.54 | 7.70 | 19. |  | 21 |
|  | 20.54 | 7.88 | 20.50 | 7.97 | 20.47 | 8.0 | 20.43 | 8.15 | 22 |
|  | 21.47 | 8.2 | 21.44 | 8.3 | 21.40 | 8.4 | 21.3 |  |  |
|  | 22.41 | 8.60 | 22.37 | 8.70 | 22.33 | 8.80 | 22.29 | 8.89 | 2 |
|  | 23.34 | 8.96 | 23.30 | 9.06 | 23.26 | 9.1 | 23.22 |  |  |
|  | 24.27 | 9.32 | 24.23 | 9.4 | 24.19 | 9.5 | 24.1 |  | 6 |
|  | 25.21 | 9.68 | 25,16 | 9.79 | 25.12 | 9.90 | 25.0 | , | 27 |
|  | 26.14 | 10.03 | 26.10 | 10.15 | 26.05 | 10.26 | 26.0 |  |  |
|  | 27.0 | 10.39 | 27.03 | 10.51 | 26.98 | 10.6 | 26.9 | 10.75 | 29 |
| 30 | 28.0 | 10.75 | 27 | 0.87 | 27.9 | 11.0 |  |  |  |
|  | 28.9 | . 11 | 28.8 | 1.24 | 28. | 1.36 |  |  | 31 |
|  | 29.8 | 1.47 | 29.82 | 11. | 29.7 | 1. | 29.7 |  |  |
|  | 30.8 | 11.83 | 30.7 | 1.96 | 30.7 | 2.0 | 30.6 |  |  |
|  | 31.7 | 12.18 | 31.69 | 12.32 | 31.6 | 12.4 | 31.5 | 12.6 |  |
|  | . 68 | 12.54 | 32.62 | 12.69 | 32.5 | 12.8 | 32.5 |  | 3 |
|  | 33.61 | 2.90 | 33.5 | 13.05 | 33.50 | 13.1 | 33.4 | 13.34 | 36 |
|  | 34.54 | 13.26 | 34.4 | 13.41 | 34.4 | 3.5 | 34.3 |  |  |
|  | 35.48 | 13.62 | 35.42 | 13.77 | 35.36 | 13.9 | 35.2 | 14.08 | 38 |
|  | 36.41 | 13.98 | 36.35 | 14.14 | 36.29 | 14.2 | 36.2 |  | 39 |
| 40 | 37.3 | 14.3 | 37.28 | 14.5 | 37.22 |  | 37.15 |  |  |
|  | 38.2 | 69 | 38.2 | 4.86 | 38.15 | 15. | 38.0 |  | 析 |
|  | 1 | 15.05 | 39.1 | 15.22 | 39.0 | 15.3 | 39.0 |  |  |
|  | 40.14 | 15.41 | 40.0 | 15.58 | 40.0 | . 76 | 39.9 | . |  |
|  | 41.08 | 15.77 | 41.01 | 15.95 | 40.94 | 16.13 | 40.8 | , | 4 |
|  | 42.01 | 16.13 | 41.94 | 16.31 | 41.8 | 16.48 | 41.8 | 16.68 | 45 |
| 46 | 42.94 | 16.48 | 42.87 | 16.67 | 42.80 | 16.8 | 42.73 | 7.05 |  |
| 47 | 43.8 | 6.84 | 43.8 | 17.03 | 43.73 | 17.2 | 43.6 | 17.42 | 47 |
| 48 | 44.81 | 17.20 | 44.7 | 17.40 | 44.66 | 17.5 | 44.5 | 17.79 | 48 |
|  | 45.75 | 17.56 | 45.6 | 17.76 | 45.5 | 17.9 | 45.5 | 18.16 | 49 |
| 50 | 46. | 92 | 46. | 18. | 46.52 | 18.33 |  |  | 50 |
|  |  | Lat. | De | Lat. | De | Lat |  |  |  |
|  |  |  |  |  |  |  |  |  |  |




| \% |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | De |  |  |  | Dep. | Lat. |  |  |
|  |  | 19.10 | 47.20 | 19.31 |  | 19.52 | \% |  |  |
|  | 48.2 | 19.48 | 48.13 | 19.69 | 48.0 |  | 47.95 |  | 52 |
|  | 49.14 | 19.85 | 49.05 | 20.07 | 48.97 | 20.28 | 48.88 |  |  |
|  | 50.07 | 20.23 | 49.98 | 20.45 | 49.89 | 20.66 | 49.80 |  |  |
|  | 51.00 | 20.60 | 50.9 | 2.83 | 50.81 | 21.05 | 50.72 | 21.2 |  |
|  | 51.92 | 20.98 | 51.83 | 21.20 | 51.7 | 21.43 | 51.64 |  |  |
|  | 52.8 | 21.35 | 52.76 | 21.58 | 52.6 | 21.81 | 52.5 |  |  |
|  | 53.78 | 21.73 | 53.6 | 21.96 | 53.5 | 22.20 | 53.4 | 22. |  |
|  | 54.76 | 22.10 | 54.61 | 22.34 | 54. |  | 54.4 |  |  |
|  | 55. | 22.48 | 55.53 | 22.72 | 55.43 | 22 | 55.33 |  |  |
|  |  | 22.85 |  | 23.10 |  | 23.34 |  |  |  |
| $\begin{aligned} & 6256.56 \\ & 6257.49 \\ & \hline \end{aligned}$ |  | 23.23 | 57.38 | 23.48 | 57. |  | 57. |  |  |
| 63 58.41 |  | 23.60 | 58.31 | 23.85 | 58.2 | 24.11 | 58.1 |  |  |
| 6459.34 |  | 23.97 | 59.23 | 24.23 | 59.1 | 4. | 59.0 | 4.75 |  |
| 6560.27 |  | 24.35 | 60.16 | 24.61 | 60.0 | 4. | 59.9 |  |  |
| 6661.19 |  | 24.72 | 61.09 | 24.99 | 60. | 25.26 | 60.8 |  |  |
| 6762.12 |  | 25.10 | 62.01 | 25.37 | 61. | 25.6 | 61.79 |  |  |
| $\begin{aligned} & 6863.05 \\ & 6963.98 \end{aligned}$ |  | 25.47 | 62.9 | 25.75 | 62. | 仡 | 62.71 |  |  |
|  |  | 25.85 | 63.86 | 26.13 | 63.7 | 26.41 | 63.63 |  |  |
| 70 | 64.90 | 26.22 | 64.78 | 26.51 |  |  | 64 |  |  |
|  | 65.83 | 26. |  | 26 |  |  | 65 |  |  |
|  | 66 | 26.97 |  | 27.2 | 66.5 |  |  |  |  |
|  | 67. | 27.35 | 67.56 | 27.64 | 67. |  | 67. |  |  |
|  | 68.6 | 27.72 | 68.49 | 28.02 | 68.3 | 8. | 68. |  |  |
|  | 69.5 | 28.10 | 69.42 | 28.40 | 69.2 |  |  |  |  |
|  | 7.47 | 28.47 | 70.3 | 28.78 | 70.2 | 9. | 70.09 |  |  |
|  | 71.3 | 28.84 | 71.27 | 29.16 | 71.1 | 29.4 | 71.0 |  |  |
| $\begin{gathered} 78 \\ 79 \\ 80 \end{gathered}$ | 72.32 | 29.22 | 72.19 | 29.53 |  |  | 71.93 |  |  |
|  | 73.25 | 29.59 | 73.12 | 9.91 |  |  | 72.85 |  |  |
|  | 74.17 | 29.97 |  | 30.29 |  |  |  |  |  |
|  | \% | 30.3 | 74. | 30.67 |  | . 0 |  |  |  |
|  | 6. | 30 |  |  |  |  |  |  |  |
|  | 7. |  |  |  |  |  |  |  |  |
| -84 | 77.8 | 31.47 | 77. | 31.81 | 77.6 | 32.1 | 77. |  |  |
|  | 8.8 | 31.8 | 78 | 32.19 | 78.5 |  | 78 |  |  |
| 88 |  | 32.2 |  | . 6 |  |  |  |  |  |
| $\begin{aligned} & 86 \\ & 87 \end{aligned}$ | 80. | 32.59 | 80.5 | 32.94 | 80.3 | 33.2 | 80.2 |  |  |
| $\begin{aligned} & 88 \\ & 89 \end{aligned}$ | 81.5 | 32. | 81 | 33.32 | 81.3 |  |  |  |  |
|  | 82.52 | 3.34 | 82.3 | 3.7 | 82.23 | 34 |  |  |  |
| 90 | 83.45 | 33.71 | 83 |  | 83.1 |  |  |  |  |
| 91 |  | 34.09 |  |  |  |  |  |  |  |
| 91 | 5 | 34.4 | 85.1 | 4.84 | 85.0 | 35.2 | 8. | . |  |
|  | 86.23 | 34.84 | 86.0 | 5.21 | 85.9 | 35.5 | 85. |  |  |
|  | 87.1 | 35,21 | 87.0 | 35.59 | 86.8 | 35.9 | 86.69 | 36.3 |  |
|  | 88.0 | 35.53 | 87.9 | 5.97 | 87.7 | 36.3 | 87.6 | 6.7 |  |
| $96$ | 89.0 | 35.96 | 88.8 | 5.3 | 88.6 | 仡 | 88.3 | 37.1 |  |
| $97$ | 89.9 | 36.34 | 89.7 | 6.73 | 89.6 | 37.12 | 89.45 | 37.51 |  |
|  | 90.8 | 36.71 | 90.7 | 7.11 | 90.5 | 37.50 | 90.3 | 37.90 |  |
| $\begin{gathered} 98 \\ 99 \\ 10 \end{gathered}$ | 91.7 | 37.09 | -1 | 37.49 | 91. | 887 | - | 38.28 | 9 |
|  | 92.7 | 37.46 | 92 |  | 92.3 | 88.27 |  |  |  |
|  |  |  |  |  | Dep |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |




| ¢ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Dep. | Lat. | Dep. |  | Dep. | La | Dep. | 4 |
|  | 1 | 0.41 | 0.91 | 0.41 | 0. |  | 1 |  |  |
|  | 1.83 | 0.81 | 1.82 | 0.82 | 1.82 | 0.83 | 1.82 | 0.84 | 2 |
|  | 2.74 | 1.22 | 2.74 | 1.23 | 2.73 | 1.24 | 2.72 | 1.26 |  |
|  | 3.65 | 1.63 | 3.65 | 1.64 | 3.64 | 1.66 | 3.63 | 1.67 |  |
| 5 | 4.57 | 2.03 | 4.56 | 2.05 | 4.55 | 2.07 | 4.5 | 2.09 |  |
|  | 5.48 | 2.44 | 5.47 | 2.46 | 5.46 | 2.49 | 5.4 | 2.51 |  |
|  | 6.39 | 2.85 | 6.38 | 2.87 | 6.37 | 2.90 | 6.3 | 2.93 |  |
| 8 | 7.31 | 3.25 | 7.29 | 3.29 | 7.2 | 3.32 | 7.27 | 3.55 |  |
|  | 8.22 | 3.66 | 8.21 | 3.70 | 8.19 | 3.73 | 8.1 | 3.77 |  |
| 10 | 9.14 | 4.07 | 9.12 | 4.11 | 9.10 | 4.15 | 9.0 | 4.19 | 10 |
| 11 | 10.05 | 4.47 | 10.03 | 4.52 | 10.0 | 4.56 | 9.9 | 4.61 | 11 |
| 12 | 10.96 | 4.88 | 10.94 | 4.93 | 10.92 | 4.98 | 10.90 | 5.02 | 12 |
| 13 | 11.88 | 5.29 | 11.85 | 5.34 | 11.83 | 5.39 | 11.8 | 5.4 | 13 |
| 1 | 12.79 | 5.69 | 12.76 | 5.75 | 12.74 | 5.81 | 12.71 | 5.86 | 4 |
| 15 | 13.70 | 6.10 | 13.68 | 6.16 | 13.65 | 6.22 | 13.6 | 6.2 | 15 |
| 16 | 14.62 | 6.51 | 14.59 | 6.57 | 14.56 | 6.64 | 14.5 | 6.70 | 16 |
|  | 15.53 | 6.92 | 15.50 | 6.98 | 15.47 | 7.05 | 15.4 | 7.12 | 17 |
| 18 | 16.44 | 7.32 | 16.41 | 7.39 | 16.38 | 7.46 | 16.3 | 7.54 | 8 |
| 19 | 17.36 | 7.73 | 17.32 | 7.80 | 17.29 | 7.88 | 17.2 | 7.95 | 19 |
| 20 | 18.27 | 8.13 | 18.24 | 8.21 | 18.20 | 8.29 | 18.16 | 8.37 | 20 |
|  | 19.18 | 8.54 | 19.15 | 8.63 | 19.11 | 8.71 | 19.0 | 8.79 | 1 |
| 23 | 20.10 | 8.95 | 20.06 | 9.04 | 20.02 | 9.12 | 19.9 | 9.2 | 22 |
|  | 21.01 | 9.35 | 20.97 | 9.45 | 20.93 | 9.54 | 2 C .89 | 9.6 | 23 |
| 23 | 21.93 | 9.76 | 21.88 | 9.86 | 21.84 | 9.95 | 21.80 | 10.0 | 24 |
| 22 | 22.84 | 10.17 | 22.79 | 10.27 | 22.75 | 10.37 | 22.70 | 10.4 | , |
|  | 23.75 | 10.58 | 23.71 | 10.68 | 23.66 | 10.78 | 23.61 | 10.8 | 26 |
| 27 | 24.67 | 10.98 | 24.62 | 11.09 | 24.57 | 11.20 | 24.5 | 11.3 | 27 |
| $\begin{aligned} & 28 \\ & 29 \end{aligned}$ | 25.58 | 11.39 | 25.53 | 11.50 | 25.48 | 11.61 | 25.43 | 11.72 | 28 |
|  | 26.49 | $11.80^{\circ}$ | 26.44 | 11.91 | 26.39 | 12.03 | 26.34 | 12.14 | 9 |
| 30 | 27.41 | 12.20 | 27.35 | 12.3 | 27.3 | 12.44 | 27.24 | 12 | 30 |
| 31 | 28.32 | 12.61 | 28 | 12.73 | 28.21 | 86 | 28.1 |  | 31 |
| $33$ | 29.23 | 13.02 | 29.18 | 13.14 | 29.12 | 13.27 | 29.06 | 13.4 | 32 |
|  | 30.15 | 13.42 | 30.09 | 13.55 | 30.03 | 13.68 | 29.97 | 13.8 |  |
| $\begin{aligned} & 33 \\ & 34 \end{aligned}$ | 31.06 | 13.83 | 31.00 | 13.96 | 30.94 | 14.10 | 30.88 | 14.2 | 34 |
| 35 | 31.97 | 14.24 | 31.91 | 14.38 | 31.85 | 14.51 | 31.78 | 14.6 | 35 |
|  | 32.89 | 14.64 | 32.82 | 14.79 | 32.76 | 14.93 | 32.69 | 15.07 | 36 |
| 36 | 33.80 | 15.05 | 33.74 | 15.20 | 33.67 | 15.34 | 33.60 | 15.49 | 37 |
| S | 4.71 | 15.46 | 34.65 | 15.61 | 34.58 | 15.76 | 34.51 | 15.9 | 38 |
|  | 35.63 | 15.86 | 35.56 | 16.02 | 35.49 | 16.17 | 35.42 | 16.3 | 9 |
| 40 | 6.54 | 16.27 | 36.47 | 16.43 | 36.40 | 16.59 | 36.33 | 16.7 | 40 |
|  | 37.46 | 16.68 | 37.38 | 16.84 | 37.31 | 17.00 | 37.23 | 17.16 | 4 |
| $42$ | 8.37 | 17.08 | 38.20 | 17.25 | 38.22 | 17.42 | 38.14 | 17.5 | 42 |
|  | 39.28 | 17.49 | 39.21 | 17.66 | 39.13 | 17.83 | 39.05 | 18.00 | 43 |
| $\begin{aligned} & 43 \\ & 43 \end{aligned}$ | 40.20 | 17.90 | 40.12 | 18.07 | 40.04 | 18.25 | 39.96 | 18.42 |  |
| $\begin{aligned} & 49 \\ & 45 \\ & 46 \\ & 4 \end{aligned}$ | 41.11 | 18.30 | 41.03 | 18.48 | 40.95 | 18.66 | 40.87 | 18.84 | 5 |
| $\begin{aligned} & 45 \\ & 46 \end{aligned}$ | 42.02 | 18.71 | 41.94 | 18.89 | 41.86 | 19.08 | 41.77 | 19.2 |  |
| $\begin{aligned} & 46 \\ & 47 \end{aligned}$ | 42.94 | 19.12 | 42.85 | 19.30 | 42.77 | 19.49 | 42.68 | 19.68 | 7 |
| 4849 | 43.85 | 19.52 | 43.76 | 19.71 | 43.68 | 19.81 | 43.59 | 20.10 |  |
|  | 44.76 | 19.93 | 44.68 | 20.13 | 44.55 | 20.32 | 44.50 | 20.51 | 49 |
| 49 50 | 45.6 | 20.3 | 45.5 | 20.5 | 45.50 | 20. | 45.4 | 20.93 | 50 |
|  | Dep | Lat | Dep | Lat. | Dep | Lat. | Dep |  |  |
|  |  |  |  |  |  |  |  |  |  |

TKAVERSE TABLE.

| E |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Dep. |  | Dep. |  | Dep. | La | Dep. |  |
| 51 | 46.59 | 20.74 |  | 20.95 |  | 21.15 | 46.32 |  | 1 |
| 52 | 47.50 | 21.15 | 47.41 | 21.36 | 47.3 | 1.56 | 47.22 | 21.77 | 52 |
| 53 | 48.42 | 21.56 | 48.32 | 21.77 | 48.23 | 21.98 | 48.13 | 22.19 | 58 |
| 54 | 49.33 | 21.96 | 49.2 | 22.18 | 49.14 | 22.39 | 49.04 |  |  |
| 5 | 50.24 | 22.37 | 50.1 | 22.59 | 50.05 | 22.81 | 49.95 |  |  |
| 56 | 51.16 | 22.78 | 51.06 | 23.00 | 50.96 | 23.22 | 50.86 | 23. | 56 |
| 57 | 52.07 | 23.18 | 51.9 | 23.41 | 51.87 |  | 51.76 | 23 | 57 |
| 58 | 52.99 | 23.59 | 52.8 | 23.82 | 52.78 | 24 | 52.67 | 2 | 58 |
| 5 | 53.90 | 24.00 | 53.79 | 24.23 | 53.69 | 24.47 | 53.58 | 24.7 | 59 |
| 60 | 54.81 | 24.40 | 54.71 | 24.64 | 54.60 |  | 54.49 |  | 60 |
| 61 |  |  |  |  |  |  |  |  | 61 |
|  |  | 25.22 | 56.5 |  | 56.42 | 25.71 | 56.30 |  |  |
|  | 57.55 | 25.62 | 57.4 | 5.8 | 57.33 | 26.13 | 57.21 | 26.38 | 3 |
| $\begin{aligned} & 03 \\ & \mathbf{6 4} \end{aligned}$ | 58.47 | 26.03 | 58.3 | 26.29 | 58.2 | 26.54 | 58.12 | 26 |  |
| 65 | 59.38 | 26.44 | 59.26 | 6.70 | 59.15 | 26.96 | 59.03 | 27.21 | 65 |
| 66 | 60.29 | 26.84 | 60.18 | 7.11 | 60.06 | 27.3 | 59.9 |  |  |
|  | 61.21 | 27.25 | 61.09 | 7.52 | 60.97 | 27.78 | 60.8 |  | 67 |
| $\begin{aligned} & 67 \\ & 68 \\ & 69 \end{aligned}$ | 62.12 | 27.66 | 62.00 | 27.9 | 61.88 | 28.20 | 61.75 | 28 |  |
|  | 63.03 | 28.06 | 62.91 | 28.34 | 62.79 | 28.61 | 62.6 | 28. | 9 |
| 69 70 | 63.95 | 28.47 | 63.82 | 8.75 | 63.70 | 29.03 | 63.57 |  | 70 |
|  | 64.8 | 28.88 | 64.7 | 9.16 | 64.61 | 29.44 | 64.48 | 29.72 |  |
|  | 65.78 | 29.28 | 65.6 | 29.57 | 65.52 |  | 65.39 |  | 72 |
| $\left.\begin{array}{\|l\|} 72 \\ 73 \end{array} \right\rvert\,$ | 66.69 | 29.69 | 66.56 | 29.98 | 66.43 | 30.27 | 66.29 | 30 | 73 |
| 74 | 67.60 | 30.10 | 67.47 | 30.39 | 67.34 | 30.69 | 67.20 | 30. |  |
| $\left\|\begin{array}{\|c} 74 \\ 75 \end{array}\right\|$ | 68.52 | 30.51 | 68.38 | 0.80 | 68.25 | 31.10 | 68.11 | 31.4 | 75 |
| 76 | 69.43 | 30.91 | 69.29 | 1.21 | 69.16 |  | 69.02 |  | 76 |
| 76 | 70.34 | 31.32 | 70.21 | 31.63 | 70.07 | 31.93 | 69.93 | 32.2 | 77 |
| $\left\|\begin{array}{l} 77 \\ 78 \\ 79 \end{array}\right\|$ | 71.26 | 31.73 | 71.12 | 32.04 | 70.98 | 32.35 | 70.8 | 32.66 | 78 |
|  | 72.17 | 32.13 | 72.03 | 32.45 | 71.89 | 32.76 | 71.74 | 33.07 | 79 |
| $\begin{aligned} & 79 \\ & 80 \end{aligned}$ | 73 | 32 | 72.9 | 32 | 72 |  | 72. |  |  |
|  |  |  | 73. | 33.27 | 73 | 33.59 |  |  | 81 |
| $\begin{aligned} & 81 \\ & 82 \\ & 83 \end{aligned}$ | 74.91 | 33.35 | 74.76 | 33.68 | 74.62 | 34.00 | 74.47 | 34 | 82 |
|  | 75.82 | 33.76 | 75.68 | 34.09 | 75.53 | 34.42 | 75.38 | 34.75 |  |
| $\left[\left.\begin{array}{l} 83 \\ 84 \end{array} \right\rvert\,\right.$ | 76.74 | 34.17 | 76.59 | 34.50 | 76.44 | 34.83 | 76.28 | 35.17 |  |
| 85 | 77.65 | 34.57 | 77.50 | 34.91 | 77.35 | 35.25 | 77.19 | 35.59 |  |
| $\left\|\begin{array}{l} 86 \\ 87 \end{array}\right\|$ | 78.56 | 34.98 | 78.41 | 35.32 | 78.26 | 35.66 | 78.10 | 36.0 | 86 |
|  | 79.48 | 35.39 | 79.32 | 35.73 | 79.17 | 36.08 | 79.01 | 36.42 |  |
| $\begin{array}{\|l\|} 87 \\ 88 \end{array}$ | 80.39 | 35.79 | 80.24 | 36.14 | 80.08 | 36.49 | 79.9 | 36.84 |  |
| $\left\|\begin{array}{l} 89 \\ 90 \end{array}\right\|$ | 81.31 | 36.20 | 81.15 | 36.55 | 80.99 | 36.91 | 8 | 31.26 | 89 |
|  | 82.22 | 36.61 | 82.06 | 6, | 81.90 | 37.32 | 81.73 |  |  |
|  |  | 37.01 |  | 7.38 | 82.81 | 37.74 | 82. |  |  |
| 92 | 84.0 | 37. | 83.88 | 37.79 | 83.72 | 38.15 | 83.5 | 38.52 |  |
|  | 84.96 | 37.83 | 84.79 | 38.20 | 84.63 | 38.57 | 84.4 | 38.94 | 4 |
|  | 85.87 | 38. | 85.71 | 38.61 | 85.54 | 438.98 | 85.3 | 39.35 | 5 |
| 95 | 86.79 | 38.64 | 86.62 | 39.02 | 86.45 | 39.40 | 86.2 | 39.77 |  |
|  | 87.70 | 39.05 | 87.53 | 39.43 | 87.36 | 39.81 |  |  |  |
|  | 88.61 | 39.45 | 88.44 | 39.84 | 88.27 | 40.23 | 88.09 | 40.61 | 1 |
|  | 89.53 | 39.86 | 89.35 | 40.25 | 89.18 | 80.64 | 89.0 |  |  |
| $\begin{array}{r} 98 \\ 99 \\ 100 \end{array}$ | 90.44 | 40.27 | 90.26 | 40.66 | 90.09 | 41.05 | 89.9 | 41. |  |
|  | 91 | 40.67 | 91.18 | 41.07 | 91.00 | 41.4 | 90.8 |  |  |
|  | D | Lat. | De | Lat. | De | Lat | Dep |  |  |
|  |  |  |  |  |  |  |  |  |  |





TRAVERSE TABLE.


|  | Lat |  |  |  |  | Dep. |  | p. | $\xrightarrow{+}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.89 | 0.45 | 0.89 | 0.46 | 0.89 | 0.46 | 0.88 | 0.47 |  |
| 2 | 1.78 | 0.91 | 1.78 | 0.92 | 1.77 | 0.92 | 1.77 | 0.93 |  |
| 3 | 2.67 | 1.36 | 2.67 | 1.37 | 2.66 | 1.39 | 2.65 | 1.40 |  |
| 4 | 3.56 | 1.82 | 3.56 | 1.83 | 3.55 | 1.85 | 3.54 | 1.86 |  |
| 5 | 4.45 | 2.27 | 4.45 | 2.29 | 4.44 | 2.31 | 4.42 | 2.33 |  |
| 6 | 5.35 | 2.72 | 5.33 | 2.75 | 5.32 | 2.77 | 5.31 | 2.79 | 6 |
| 7 | 6.24 | 3.18 | 6.22 | 3.21 | 6.21 | 3.23 | 6.19 | 3.26 |  |
| 8 | 7.13 | 3.63 | 7.11 | 3.66 | 7.10 | 3.69 | 7.08 | 3.72 |  |
| 10 | 8.02 | 4.09 4.54 | 8.00 | 4.12 | 7.98 | 4.16 | 7.96 | 4.19 | 0 |
|  |  |  | 8.89 | 4.5 | 8.87 | 4.62 | 8.8 |  | 0 |
| 11 | 9.80 | 4.99 | 9.78 | 5.04 | 9.76 | 5.08 | 9. |  | 11 |
|  | 10.69 | 5.45 | 10.67 | 5.49 | 10.64 | 5.54 | 10.62 | 5.59 | 12 |
|  | 11.58 | 5.90 | 11.56 | 5.95 | 11.53 | 6.00 | 11.50 | 6.05 | 13 |
|  | 12.47 | 6.36 | 12.45 | 6.41 | 12.42 | 6.46 | 12.39 | 6.52 | 14 |
|  | 13.37 | 6.81 | 13.34 | 6.87 | 13.31 | 6.93 | 13.27 | 6.98 | 15 |
|  | 14.26 | 7.26 | 14.22 | 7.33 | 14.19 | 7.39 | 14.16 | 7.45 | 16 |
|  | 15.15 | 7.72 | 15.11 | 7.78 | 15.08 | 7.85 | 15.04 | 7.92 | 17 |
|  | 16.04 | 8.17 | 16.00 | 8.24 | 15.97 | 8.31 | 15.93 | 8.38 | 18 |
|  | 16.93 | 8.63 | 16.89 | 8.70 | 16.85 | 8.77 | 16.81 | 8.85 | 9 |
| 20 | 17.82 | 9.08 | 17.78 | 9.16 | 17.74 | 9.23 | 17.70 | 9.31 | 0 |
|  | 18 | 9.53 | 18.67 | 9.62 | 18.63 | 9.70 | 18.58 | 9.78 | 1 |
|  | 19.60 | 9.99 | 19.56 | 0.07 | 19.51 | 0.16 | 19.47 | 0.24 | 2 |
|  | 20.49 | 10.44 | 20.45 | 10.53 | 20.40 | 10.62 | 20.3 | 10.71 | 23 |
|  | 21.38 | 10.90 | 21.34 | 10.99 | 21.29 | 11.08 | 21.24 | 11.17 | 4 |
|  | 22.28 | 11.35 | 22.23 | 11.45 | 22.18 | 11.54 | 22.12 | 11.64 | 5 |
|  | 23.17 | 11.80 | 23.11 | 11.90 | 23.06 | 12.01 | 23.01 | 12.11 | 26 |
|  | 24.06 | 12.26 | 24.00 | 12.36 | 23.95 | 12.47 | 23.89 | 12.57 | 7 |
|  | 24.95 | 12.71 | 24.89 | 12.82 | 24.84 | 12.93 | 24.78 | 13.04 | 8 |
|  | 25.84 | 13.17 | 25.78 | 13.28 | 25.72 | 13.39 | 25.66 | 13.50 | 9 |
| 30 | 26.73 | 13.62 | 26.67 | 13.74 | 26.61 | 13.85 | 26.55 |  | 0 |
|  | 27.62 | 14.07 | 27.56 | 4.19 | 27.50 | 14.31 | 27.4 | 14.43 | 1 |
|  | 28.51 | 14.53 | 28.45 | 14.65 | 28.38 | 14.78 | 28.32 | 14.90 | 32 |
|  | 40 | 14.98 | 29.34 | 15.11 | 29.27 | 15.24 | 29.20 | 15.37 | 3 |
|  | 30.29 | 15.44 | 30.23 | 15.57 | 30.16 | 15.70 | 30.09 | 15.83 | 4 |
|  | 31.19 | 15.89 | 31.12 | 16.63 | 31.65 | 16.16 | 30.97 | 16.30 | 35 |
|  | 3.08 | 16.34 | 32.00 | 16.48 | 31.93 | 16.62 | 31.86 | 16.76 | 36 |
|  | 32.97 | 16.80 | 32.89 | 16.94 | 32.82 | 17.08 | 32.74 | 17.23 | 37 |
|  | 33.86 | 17.25 | 33.78 | 17.40 | 33.71 | 17.55 | 33.63 | 17.69 | 8 |
|  | 34.75 | 17.71 | 34.67 | 17.86 | 34.59 | 18.01 | 34.51 | 18.16 | 39 |
| 40 | 35.6 | 18.16 | 35.56 | 18.31 | 35.4 | 18.47 | 35.40 | 18.62 | 40 |
|  |  | 8.61 |  | 18.77 |  | 8.93 | 36.28 | 19.09 | 11 |
|  | 37.42 | 19.07 | 37.34 | 19.23 | 37.25 | 19.39 | \|37.17 | 19.56 | 42 |
|  | 38.31 | 19.52 | 38.23 | 19.69 | 38.14 | 19.86 | 38.05 | 20.02 | 43 |
|  | 39.20 | 19.98 | 39.12 | 20.15 | 39.03 | 20.32 | 38.94 | 0.49 | 44 |
|  | 40.10 | 20.43 | 40.01 | 20.60 | 39.92 | 20.78 | 39.82 | 20.95 | 45 |
|  | 40.99 | 20.88 | 40.89 | 21.06 | 40.80 | 21.24 | 40.712 | 21.42 | 46 |
|  | 1.88 | 21.34 | 41.78 | 21.52 | 41.69 | 21.70 | 41.59 | 21.88 | 47 |
| 43 | 42.77 | 21.79 | 42.67 | 21.98 | 42.58 | 22.16 | 42.48, | 22.35 | 48 |
| 49 50 | 43.66 | 22.25 | 43.56 | 22.44 | 43.46 | 22.63 | 43.36 | 22.82 | 49 |
| 50 | 44.55 | 22.70 | 44.45 | 22.89 | 44.35 | 23.09 | 44.25 | 23.28 | 50 |
|  | Dep. | Lat. | Dep. | Lat. | Dep | Lat. | Dep. | La |  |
| Q |  |  | 62 |  | 62 |  |  |  |  |

TRAVERSE TABLE:


TRAVERSE TABLE.

|  | 28 Deg. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. | Lat. Dep. |  | Lat. Dep. |  | Lat. | Dep. |  |
| 1 | 0.88 | 0.47 | 0.88 | 0.47 | 0.88 | 0.48 | 0.88 |  |  |
| 2 | 1.77 | 0.94 | 1.76 | 0.95 | 1.76 | 0.95 | 1.75 | 0.96 | 2 |
| 3 | 2.65 | 1.41 | 2.64 | 1.42 | 2.64 | 1.43 | 2.63 | 1.44 |  |
| 4 | 3.53 | 1.88 | 3.52 | 1.89 | 3.52 | 1.91 | 3.51 | 1.92 |  |
| 5 | 4.41 | 2.35 | 4.40 | 2.37 | 4.39 | 2.39 | 4.38 | 2.40 |  |
| 6 | 5.30 | 2.82 | 5.29 | 2.84 | 5.27 | 2.86 | 5.26 | 2.89 |  |
| 7 | 6.18 | 3.29 | 6.17 | 3.31 | 6.15 | 3.34 | 6.14 | 3.37 |  |
| 8 | 78.3 | 3.76 | 7.05 | 3.79 | 7.03 | 3.82 | 7.01 | 3.85 |  |
| 9 | 7.95 | 4.23 | 7.93 | 4.26 | 7.91 | 4.29 | 7.89 | 4.33 |  |
| 10 | 8.83 | 4.69 | 8.81 | 4.73 | 8.79 | 4.77 | 8.77 | 4.81 |  |
| 11 | 0.7 | 5.16 | 9.69 | 5.21 | 9.65 | 5.25 |  | 5.29 | 1 |
| 12 | 10.60 | 5.63 | 10.57 | 5.68 | 10.55 | 5.73 | 10.52 | 5.77 | 12 |
| 13 | 11.48 | 6.10 | 11.45 | 6.15 | 11.42 | 6.20 | 11.40 | 6.25 | 13 |
| 14 | 12.36 | 6.57 | 12.33 | 6.63 | 12.30 | 6.68 | 12.27 | 6.7 | 14 |
| 15 | 13.24 | 7.04 | 13.21 | 7.10 | 13.18 | 7.16 | 13.15 | 7. | 15 |
| 16 | 14.13 | 7.51 | 14.09 | 7.57 | 14.06 | 7.63 | 14.03 | 7.70 | 16 |
| 17 | 15.01 | 7.98 | 14.98 | 8.05 | 14.94 | 8.11 | 14.90 | 8.18 | 1 |
| 18 | 15.89 | 8.45 | 15.86 | 8.52 | 15.82 | 8.59 | 15.78 | 8.66 | 18 |
| 19 | 16.78 | 8.92 | 16.74 | 8.99 | 16.70 | 9.07 | 16.66 | 9.14 | 19 |
| 20 | 17.66 | 9.39 | 17.62 | 9.47 | 17.58 | 9.54 | 17.53 | 9.62 | 20 |
| 21 | 18.54 | 9.86 | 18.50 | 9.94 | 18.46 | . 02 |  |  | 21 |
| 22 | 19.42 | 10.33 | 19.381 | 10.41 | 19.3 | 0.50 | 19. | 0 | 99 |
| 23 | 20.31 | 10.80 | 20.261 | 10.89 | 20.21 | 10.97 | 20.1 | 1.06 | 3 |
| 24 | 21.19 | 11.27 | 21.14 | 11.36 | 21.09 | 1.45 | 21.0 | 11.5 | 24 |
| 25 | 22.07 | 11.74 | 22.021 | 11.83 | 21.97 | 11.93 | 21.92 | 12.02 | 25 |
| 26 | 22.96 | 12.21 | 22.90 | 12.31 | 22.85 | 2.41 | 22.7 | 12.51 | 2 |
| 27 | 23.84 | 12.68 | 23.781 | 12.78 | 23.73 | 12.88 | 23.6 | 12.99 | 27 |
| 28 | 24.72 | 13.15 | 24.661 | 13.25 | 24.61 | 13.36 | 24.5 | 13.47 |  |
| 29 | 25.61 | 13.61 | 25.55 | 13.73 | 25.49 | 13.84 | 25. | 13.95 | 23 |
| 30 | 26.49 | 14.08 | 26.43 | 14.20 | 26.36 | 4.31 | 26.3 |  | 39 |
| 31 | 27.37 | 14.55 | 27.3 | 4.67 | 27.2 |  | 27.1 |  | 31 |
| 32 | 28.25 | 15.02 | 28.19 | 15.15 | 28.1 | .27 | 28.0 | 5.39 | 32 |
| 33 | 29.14 | 15.49 | 29.071 | 15.62 | 29.00 | 15.75 | 28.93 | 5.87 | 33 |
| 34 | 30.02 | 15.96 | 29.951 | 16.09 | 29.88 | 16.22 | 29.8 | 6.35 | 34 |
| 35 | 30.90 | 16.43 | 30.831 | 16.57 | 30.76 | 16.70 | 30.6 | 6.8 | 3 |
| 36 | 31.79 | 16.90 | 31.711 | 17.04 | 31.64 | 17.18 | 31.561 | 17.32 | 36 |
| 37 | 32.67 | 17.37 | 32.591 | 17.51 | 32.52 | 17.65 | 32.441 | 17.80 | 37 |
| 38 | 33.55 | 17.84 | 33.471 | 17.99 | 33.39 | 18.13 | 33.321 | 18.28 | 38 |
| 39 | 34.43 | 18.51 | 34.351 | 18.46 | 34.27 | 18.61 | 34.19 | 8.76 | 9 |
| 40 | 35.32 | 18.78 | 35.241 | 18.93 | 35.15 | . 09 | 35.07 | 19.24 | 4 |
| 41 | 36.20 | 19.25 | 36.12 | 9.41 | 36.0 |  |  |  | 41 |
| 42 | 37.08 | 19.72 | 37.001 | 19.88 | 36.91 | 2.04 | 36.82 | 20.20 | 42 |
| 43 | 37.97 | 20.19 | 37.88 | 20.35 | 37.792 | 20.52 | 37.7 | 20.68 | 43 |
| 44 | 38.85 | 20.66 | 38.76 | 20.83 | 38.672 | 20.95 | 38.58 | 21.16 | 44 |
| 45 | 39.73 | 21.13 | 39.642 | 21.30 | 39.55 | 21.47 | 39.45 | 21.64 | 45 |
| 46 | 40.62 | 21.60 | 40.522 | 21.77 | 40.43 | 21.95 | 40.332 | 22.13 | 46 |
| 47 | 41.50 | 22.07 | 41.402 | 22.25 | 41.302 | 22.43 | 41.212 | 22.61 | 47 |
| 48 | 42.38 | 22.53 | 42.28 | 22.72 | 42.18 | 22.90 | 42.08 | 23.09 | 48 |
| 49 | 43.26 | 23.00 | 43.16 | 23.19 | 43.062 | 23.38 | 42.962 | 23.57 | 49 |
| 50 | 44.15 | 23.47 | 44.04 | 23.67 | 43.94 | 23.86 | 43.84 | 24.05 | 50 |
| $\stackrel{\square}{\circ}$ | Dep. Lat. |  | D | Lat. | Dep | Lat. | Dep | Luat. |  |
|  | 62. Deg. |  |  |  | 61. |  |  |  |  |


|  |  |  |  |  |  | De |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | 51 |
|  |  |  |  |  |  | 81 | 45. |  | 52 |
|  | 46 | 24.88 | 46.69 | 25.09 | 46.58 | 25.29 | 46.47 | 25.49 | 53 |
|  | 47.6 | 25.35 | 47.57 | 25.56 | 47.46 | 25.77 | 47.34 | 5.97 | 54 |
|  | 48 | 25.82 | 48.45 | 26.03 | 48.3 | 26.24 | 48.22 | 26.45 |  |
|  | 49.45 | 26.29 | 49.33 | 28.51 | 49.21 | 26.72 | 49.10 | 6. | 56 |
|  | 50.33 | 26.76 | 50.212 | 26.98 | 50.09 | 27.20 | 49.9 | 7.42 | 57 |
|  | 51.2 | 27.2 | 51.092 | 27.45 | 50.97 | 27.68 | 50.8 | 7.90 |  |
|  | 52.09 | 27:70 | 51.9712 | 27.93 | 51.85 | 28.15 | 51.7 | . 38 | 59 |
| 60 | 52. | 28.17 | 52.85 | 28.40 | 52.73 | 28.63 | 52. |  | 60 |
|  |  |  |  | 28.87 |  |  |  |  |  |
|  | 54.74 | 29.1 | 54.62 | 29.35 | 54.49 | 29.58 | 54 | 29.82 | 2 |
|  | 55.63 | 29.58 | 55.50 | 29.8 | 55.37 | 30.06 |  | 30.30 | 63 |
|  | 56.51 | 30.05 | 56.383 | 30.29 | 56.24 | 30.54 | 56.11 |  |  |
|  | 57.39 | 30.52 | 57.2 | 30.77 | 57.12 | 31.02 | 56. | 1.26 | 65 |
|  | 58.27 | 30.99 | 58.14 | 31.24 | 58.00 | 31.49 | 57. | 1.75 | 66 |
|  | 59.16.3 | 31.45 | 59.02:3 | 31.71 | 58.88 | 31.97 | 58.7 | 32.23 | 67 |
|  | 60.04 | 31.92 | 59.90, | 32.19 | 59.7 | 2.45 |  | 2.71 | 68 |
|  | 60.92 | 32.39 | 60.783 | 32.66 | 60.6 | 32.92 | 60 | 33.19 | 69 |
|  | 61.81 | 32.86 | 61.66 | 33.13 | 61.5 |  | 61 |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  | $63: 57$ | 33.80 | 63.4 | 34.08 | 63.2 | 34.36 | 63. |  | 7 |
|  | 64.46 | 34.27 | 64.303 | 34.55 | 64.1 | 34.83 |  |  | 析 |
|  | 65.3 | 34.74 | 65.193 | 35.03 | 65. | 35.31 |  |  | 74 |
|  | 66.22 | 35.21 | 66.0 | 35.50 | 65.9 | 35.79 | 65. | 6. | 75 |
|  | 67.10 | 35.6 | 66.9 | 35.97 | 66.79 | 36.26 |  |  | 6 |
|  | 67.99 | 36.1 | 67.8 | 36.45 | 67.6 | 36.74 | 67. |  | 77 |
|  | 68.87 | 36.62 | 68.71 | 36.92 | 68.5 | 37.2 |  |  |  |
|  | 69.75 | 37.09 | 69.59 | 37.39 | 69.43 | 37.70 |  |  | 79 |
| 80 |  | 5 | 70.4 | 7. | 70.3 | 38.1 |  |  |  |
|  |  |  |  | 38.3 |  |  |  |  | 81 |
|  | 72.40 | 38.5 | 72.23 | 38.81 | 72.0 | 39.1 |  |  |  |
|  | 73.28 | 38.9 | 73.11 | 39.29 | 72.94 | 39.60 | 72.7 |  |  |
|  | 14 | 9,44 | 73.99 | 39.76 | 73.82 | 40.08 | 73.6 |  |  |
|  | 75.0 | 39.9 | 74.8 | 40.23 | 74.70 | 40.56 |  | 8 | 85 |
|  | 75:93 | 40.37 | 75.76 | 40.71 | 75.58 | 41.04 | 75. |  |  |
|  | 76.82 | . 84 | 76.64 | 41.18 | 76.4 | 41.5 | 76.2 | . 85 |  |
|  | 77.70 | 41.3 | 77.52 | 41.6 | 77.3 | 41.9 |  | 42.33 |  |
|  | 78.58 | 41.7 | 78.40 | 42.13 | 78.21 | 42.4 | 78.03 | 42.81 |  |
|  |  | - | 79.2 | 42.6 | 79.0 | 42. | 78. |  |  |
|  | 80.35 |  |  |  |  |  |  |  |  |
|  | 81.23 | 43.19 | 81.04 | 43.55 | 80.85 | 43.90 | 8. | 44.25 |  |
|  | 82.11 | . 66 | 81.92 | 44.02 | 81.73 | 44.38 | 81.5 | 44.73 |  |
|  | 83.0 | 4.13 | 82.80 | '44.49 | 82.61 | 44.85 | 82.4 | 5.21 |  |
|  | 83.88 | 44.60 | 83.68 | 44.97 | 83.49 | 45.33 | 83.2 | 5.69 |  |
|  | 84 |  | 84.57 | 45.44 | 84.37 | 45.81 |  | 6.17 |  |
|  | 85.65 | 45.54 | 85.4 | 45.91 | 85.25 | 46.2 |  | . 6. |  |
|  | 86.53 |  | 8. | 46 |  | 46. |  | 47.14 |  |
|  | 87.41 | 46. | 87.21 | 46. | 87.00 | 47.24 |  |  |  |
|  | 88.29 | 46.95 | 83.09 | 47.33 | 87.88 | 47.7 |  |  |  |
|  |  |  | De | at. | Dep | La |  |  |  |
|  |  |  |  |  |  |  |  |  |  |

TRAVERSE TABLE.

|  | 29 | g. | $29 \frac{1}{4}$ |  | $29 \frac{1}{3}$ Deg. |  | 2934 Deg. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. | Lat. | Dep. |  | Dep: | Lat. | Dep. |  |
|  | 0.87 | 0.48 | 0.87 | 0.49 | 0.87 | 0.49 | 0.87 | 0.50 |  |
| 2 | 1.75 | 0.97 | 1.74 | 0.98 | 1.74 | 0.98 | 1.74 | 0.99 |  |
| 3 | 2.62 | 1.45 | 2.62 | 1.47 | 2.61 | 1.48 | 2.60 | 1.49 |  |
| 4 | 3.50 | 1.94 | 3.49 | 1.95 | 3.48 | 1.97 | 3.47 | 1.98 |  |
| 5 | 4.37 | 2.42 | 4.36 | 2.44 | 4.35 | 2.46 | 4.34 | 2.48 |  |
| 6 | 5.25 | 2.91 | 5.23 | 2.93 | 5.2 | 2.95 | 5.21 | 2.98 |  |
| 7 | 6.12 | 3.39 | 6.11 | 3.42 | 6.09 | 3.45 | 6.08 | 3.47 |  |
| 8 | 7.00 | 3.88 | 6.98 | 3.91 | 6.96 | 3.94 | 6.95 | 3.97 |  |
| 9 | 7.87 | 4.36 | 7.85 | 4.40 | 7.83 | 4.43 | 7.8 | 4.47 | 9 |
| 10 | 8.75 | 4.85 | 8.72 | 4.89 | 8.70 | 4.92 | 8.68 | 4.96 | 0 |
| 11 | 9.62 | 5.33 | 9.60 | 5.37 | 9.5 | 5.42 | 9.55 |  | 1 |
|  | 10.50 | 5.82 | 10.47 | 5.86 | 10.44 | 5.91 | 10.42 | 5.95 | 2 |
|  | 11.37 | 6.30 | 11.54 | 6.35 | 11.31 | 6.40 | 11.29 | 6.45 | 3 |
|  | 12.24 | 6.79 | 12.21 | 6.84 | 12.18 | 6.89 | 12.15 | 6.95 | 14 |
|  | 13.12 | 7.27 | 13.09 | 7.33 | 13.06 | 7.39 | 13.02 | 7.44 | 15 |
|  | 13.99 | 7.76 | 13.96 | 7.82 | 13.93 | 7.88 | 13.89 | 7.94 | 16 |
|  | 14.87 | 8.24 | 14.83 | 8.31 | 14.80 | 8.57 | 14.76 | 8.44 | 7 |
|  | 15.74 | 8.73 | 15.70 | 8.80 | 15.67 | 8.86 | 15.63 | 8.93 | 8 |
|  | 16.62 | 9.21 | 16.58 | 9.28 | 16.54 | 9.36 | 16.50 | 9.43 | - |
| 20 | 17.49 | 9.70 | 17.45 | 9.77 | 17.41 | 9.85 | 17.36 |  | 0 |
|  | 18.37 | . 18 | 18.32 | 10.26 | 18.2 | 10.34 | 18.23 | 10.42 | 1 |
|  | 19.24 | 10.67 | 19.19 | 10.75 | 19.15 | 10.83 | 19.10 | 10.92 | 2 |
|  | 20.121 | 11.15 | 20.07 | 11.24 | 20.02 | 11.33 | 19.97 | 11.41 | 3 |
|  | 20.99 | 11.64 | 20.94 | 11.73 | 20.89 | 11.82 | 20.84 | 11.91 | 4 |
|  | 21.87 | 12.12 | 21.81 | 12.22 | 21.76 | 12.31 | 21.70 | 12.41 | 25 |
|  | 22.74 | 12.60 | 22.68 | 12.70 | 22.63 | 12.80 | 22.57 | 12.90 | 2 |
|  | 23.61 | 13.09 | 23.56 | 13.19 | 23.50 | 13.30 | 23.44 | 13.40 | 7 |
|  | 24.49 | 13.57 | 24.43 | 13.68 | 24.37 | 13.79 | 24.31 | 13.89 | 8 |
|  | 25.361 | 14.06 | 25.30 | 14.17 | 25.24 | 14.28 | 25.18 | 14.39 | 29 |
| 30 | , | 4.54 | 26.17 | 4.6 | 26.11 | 14.77 | 26.05 |  |  |
|  |  | . 03 | 27 | 5.15 | 26.98 | 15.27 | 6.91 | 5.38 | 31 |
|  | 27.99 | 15.51 | 27.92 | 15.64 | 27.85 | 15.76 | 27.78 | 15.88 | 32 |
|  | 28.86 | 16.00 | 28.79 | 16.12 | 28.72 | 16.25 | 28.65 | 16.38 | 3 |
|  | 29.74 | 16.48 | 29.66 | 16.61 | 29.59 | 16.74 | 29.52 | 16.87 | 4 |
|  | 30.61 | 16.97 | 30.54 | 17.10 | 30.46 | 17.23 | 30.39 | 17.37 | 35 |
|  | 31.49 | 17.45 | 31.41 | 17.59 | 31.33 | 17.73 | 31.26 | 17.86 | 3 |
|  | 32.36 | 17.94 | 32.28 | 18,08 | 32.20 | 18.22 | 32.12 | 18.36 |  |
|  | 33.24 | 18.42 | 33.15 | 18.57 | 33.07 | 18.71 | 32.99 | 18.86 | 38 |
|  | 34.11 | 18.91 | 34.03 | 19.66 | 33.94 | 19.20 | 33.86 | 19.35 | 39 |
| 40 | 34.98 | 19.39 | 34.90 | 19.54 | 34.81 | 19.70 | 34. | 19.85 |  |
|  | . | 88 |  | 03 |  | 0.19 |  | 29.34 | 41 |
|  | 36.73 | 20.36 | 36.64 | 20.52 | 36.55 | 20.68 | 35.46 | 20.84 | 42 |
|  | 37.612 | 20.85 | 37.52 | 21.01 | 37.43 | 21.17 | 37.3:3 | 21.34 | 3 |
|  | 38.48 | 21.33 | 38.39 | 21.50 | 38.30 | 21.67 | 38.20 | 21.83 | 44 |
|  | 39.36 | 21.82 | 39.26 | 21.99 | 39.17 | 22.16 | 39.07 | 22.33 | 45 |
|  | 40.23 | 22.30 | 40.13 | 22.48 | 40.04 | 22.65 | 39.94 | 22.83 | 46 |
|  | 41.11 | 22.79 | 41.01 | 22.97 | 40.91 | 23.14 | 40.81 | 23.32 | 7 |
|  | 41.98 | 23.27 | 41.88 | 23.45 | 41.78 | 23.63 | 41.67 | . 8 | 48 |
|  | 42.86 | 23.76 | 42.75 | 23.94 | 42.65 | 24.13 | 42.54 | 24.31 | 49 |
| 50 | 43.73 | 24.24 | 43.62 | 4.43 | 43.52 | 24.62 | 43.41 | . 81 | 5 |
|  | Dep | Lat. | Dep | Lat. | De | Lat |  |  |  |
|  |  |  |  |  |  |  |  |  |  |



|  |  |  |  |  |  | eg. |  | eg. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | La | Dep. |  | Dep. | Lat. | Dep. | Lat. | D |  |
| 1 | 0.87 | 0.50 | 0.86 | 0.50 | 0.86 | 0.51 | 0.86 | 0.51 |  |
|  | 1.73 | 1.00 | 1.73 | 1.01 | 1.72 | 1.02 | 1.72 | 1.02 | 2 |
| 3 | 2.60 | 1.50 | 2.59 | 1.51 | 2.58 | 1.52 | 2.58 | 1.53 | 3 |
| 4 | 3.46 | 2.00 | 3.46 | 2.02 | 3.45 | 2.03 | 3.44 | 2.05 |  |
| 5 | 4.33 | 2.50 | 4.32 | 2.52 | 4.31 | 2.54 | 4.30 | 2.56 | 5 |
| 6 | 5.20 | 3.00 | 5.18 | 3.02 | 5.17 | 3.05 | 5.16 | 3.07 |  |
| 7 | 6.06 | 3.50 | 6.05 | 3.53 | 6.03 | 3.55 | 6.02 | 3.58 |  |
| 8 | 6.93 | 4.00 | 6.91 | 4.03 | 6.89 | 4.06 | 6.88 | 4.09 | 8 |
| 9 | 7.79 | 4.50 | 7.77 | 4.53 | 7.75 | 4.57 | 7.73 | 4.60 |  |
| 10 | 8.66 | 5.00 | 8.64 | 5.04 | 8.62 | 5.08 | 8.59 | 5.11 | 0 |
| 11 | 9.53 | 5.50 | 9.50 | 5.54 | 48 | 5.58 | 9.45 | 5.62 | 1 |
|  | 10.39 | 6.00 | 10.37 | 6.05 | 10.34 | 6.09 | 10.31 | 6.14 | 2 |
|  | 11.26 | 6.50 | 11.23 | 6.55 | 11.20 | 6.60 | 11.17 | 6.65 | 3 |
|  | 12.12 | 7.00 | 12.09 | 7.05 | 12.06 | 7.11 | 12.03 | 7.1 |  |
|  | 12.99 | 7.50 | 12.96 | 7.56 | 12.92 | 7.61 | 12.89 | 7.67 | 15 |
|  | 13.86 | 8.00 | 13.82 | 8.06 | 13.79 | 8.12 | 13.75 | 8.18 | 6 |
|  | 14.72 | 8.50 | 14.69 | 8.56 | 14.65 | 8.63 | 14.61 | 8.69 | 7 |
|  | 15.59 | 9.00 | 15.55 | 9.07 | 15.51 | 9.14 | 15.47 | 9.20 | 8 |
|  | 16.45 | 9.50 | 16.41 | 9.57 | 16.37 | 9.64 | 16.33 | 9.71 | 19 |
| 19 | 17.321 | 10.00 | 17.28 | 10.08 | 17.23 | 10.15 | 17.19 | 10.23 | 0 |
|  | 18.191 | 10.50 | 18.14 | 10.58 | 18.09 | 10.66 | 18.05 | 74 | 1 |
|  | 19.051 | 11.00 | 19.00 | 11.08 | 18.96 | 11.17 | 18.91 | 1.25 | 22 |
|  | 19.92 | 11.50 | 19.87 | 11.59 | 19.82 | 11.67 | 19.77 | 11.76 | 23 |
|  | 20.78 | 12.00 | 20.73 | 12.09 | 20.68 | 12.18 | 20.63 | 12.27 | 24 |
|  | 21.651 | 12.50 | 21.60 | 12.59 | 21.54 | 12.69 | 21.49 | 12.78 | 25 |
|  | 22.52 | 13.00 | 22.46 | 13.10 | 22.40 | 13.20 | 22.3 | 13.29 | 2 |
|  | 23.381 | 13.50 | 23.32 | 13.60 | 23.26 | 13.70 | 23.20 | 13.80 | 27 |
|  | 24.251 | 14.00 | 24.19 | 14.11 | 24.13 | 14.21 | 24.06 | 14.32 | 28 |
|  | 25.11 | 14.50 | 25.05 | 14.61 | 24.99 | 14.72 | 24.92 | 14.83 | 29 |
| 30 | 25.98 | 5.00 | 25.92 | 15.11 | 25.85 | 15.23 | 25.78 | 15.34 | O |
|  |  | 50 |  | . 62 | 26.7 | 5.73 |  |  | 1 |
|  | 27.71 | 16.00 | 27.64 | 16.12 | 27.57 | 16.24 | 27.50 | 16.36 | 32 |
|  | 28.58 | 16.50 | 28.51 | 16.62 | 28.43 | 16.75 | 28.36 | 16.87 | 33 |
|  | 9.44 | 17.00 | 29.37 | 17.13 | 29.30 | 17.26 | 29.22 | 17.38 | 34 |
|  | 30.31 | 17.50 | 30.23 | 17.63 | 30.16 | 17.76 | 30.08 | 7.90 | 5 |
|  | 31.18 | 18.00 | 31.10 | 18.14 | 31.02 | 18.27 | 30.94 | 18.41 | 3 |
|  | 32.04 | 18.50 | 31.96 | 18.64 | 31.88 | 18.78 | 31.80 | 18.92 | 37 |
|  | 32.911 | 19.00 | 32.83 | 19.14 | 32.74 | 19.29 | 32.6 | 19.43 | 38 |
|  | 33.771 | 19.50 | 33.69 | 19.65 | 33.60 | 19.79 | 33,52 | 19.94 | 39 |
|  | 34.64 | 20.00 | 34.55 | 20.15 | 34.47 | 20.30 | 34.3 | 20. | 40 |
|  |  |  |  | 20.65 | 35.33 | 20.81 |  |  | 41 |
|  | 36.372 | 21.00 | 36.28 | 21.16 | 36.19 | 21.32 | 36.10 | 21.47 | 42 |
|  | 37.24 | 21.50 | 37.14 | 21.66 | 37.05 | 21.82 | 36.95 | 21.99 | 43 |
|  | 8.11 | 22.00 | 38.01 | 2.17 | 37.91 | 22.33 | 37.81 | 22.50 | 44 |
|  | . 97 | 2.50 | 38.87 | 22.67 | 38.77 | 22.84 | 38.67 | 23.01 | 45 |
|  | 39.84 | 23.00 | 39.74 | 23.17 | 39.63 | 23.35 | 39.53 | 23.52 | 46 |
|  | 40.70 | 23.50 | 40.60 | 23.68 | 40.50 | 23.85 | 40.39 | 24.03 | 47 |
| 484950 | 41.572 | 24.00 | 41.46 | 24.18 | 41.36 | 24.36 | 41.25 | 24.54 | 48 |
|  | 22.42210 | 24.50 | 42.33 | 24.68 | 42.22 | 24.87 | 42.11 | 25.05 | - |
|  | 43.30 | 25.00 | 43.19 | 2.19 | 43.08 | 25.38 | 42.97 |  | 0 |
|  | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep | at. |  |
|  |  |  |  | Deg |  |  |  |  |  |


|  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Dep. |  | p. | Lat. | Dep. | Lat. | p. |  |
|  | 44.1 | 2. | 44.0 | 25.69 | 4. | 88 | 43.83 | 26.08 | 51 |
|  | 45.03 | 26.0 | 44.92 | 26.20 | 44.80 | 26.39 | 44.69 | 26. | 52 |
|  | 45.90 | 26.50 | 45.78 | 26.70 | 45.67 | 26.90 | 45.55 | 27 | 53 |
|  | 46.77 | 27.00 | 46.6 | 27.20 | 46.53 | 27.41 | 46.41 | 27.61 | 54 |
|  | 47.63 | 27.50 | 47.51 | 27.71 | 47.3 | 27.91 | 47.27 | 28.12 | 55 |
|  | 48.50 | 28.00 | 48.37 | 28.21 | 48.25 | 28.42 | 48.13 |  | 6 |
|  | 49.36 | 28.50 | 49.2 | 28.72 | 49.11 | 28.93 | 48.99 | 29.14 | 7 |
|  | 50.23 | 29.00 | 50.1 | 29.22 | 49.97 | 29.44 | 49.85 | 29.65 | 58 |
|  | 51.10 | 29.50 | 50.97 | 29.72 | 50.84 | 29.94 | 50.70 | 30.17 | 59 |
|  | 51.96 | 30.00 | 51.83 | 0.23 | 51.70 |  | 51.56 |  | 0 |
|  | 52.83 | 30.50 |  |  | 52.5 | 30.96 | 52 |  |  |
|  | 53.69 | 31.00 | 53.56 | 31.23 | 53.42 | 31.47 | 53.2 | 31.70 | 62 |
|  | 54.56 | 31.50 | 54.42 | 31.74 | 54.28 | 31.97 | 54.1 | 32.21 | 仡 |
|  | 55.43 | 32.00 | 55.29 | 32.24 | 55.14 | 32.48 | 55. | 32.72 | 64 |
|  | 56.29 | 32.50 | 56.15 | 32.75 | 56.01 | 32.99 | 55. | - | 65 |
|  | 57.16 | 33.00 | 57.01 | 33.25 | 56.87 | 33.50 | 56. |  | 66 |
|  | 58.02 | 33.50 | 57.88 | 33.75 | 57.73 | 34.01 | 57.5 | 34.2 | 67 |
|  | 58.89 | 34.00 | 58.74 | 34.26 | 58.59 | 34.51 | 58.4 | 34.7 | 68 |
|  | 59.76 | 34.50 | 59.60 | 34.76 | 59.45 | 135.02 | 59.30 | 35.2 |  |
|  | 60.62 | 35. | 60.47 | 35.26 |  | 35. | 60.16 |  |  |
|  | 1.49 | 35.50 |  |  |  |  |  |  | 71 |
|  | 62. | 36.00 | 62.20 | 36.27 | 62.04 | 36. |  |  | 2 |
|  | 63.22 | 36.50 | 63.06 | 36.78 | 62.90 | 37. | 62.74 |  | 8 |
|  | 64.09 | 37.00 | 63.92 | 37.28 | 63.76 | 37.56 |  | 37 | 4 |
| 75 | 64.95 | 37.50 | 64.79 | 7.78 | 64.62 | 38.0' | 64.46 | 38.3 |  |
|  | 65. | 38.00 | 65.65 | 38.29 | 65.48 | 38.57 | 65.31 |  | 76 |
| 77 | 66.6 | 38.50 | 66.52 | 38.79 | 66.35 | 39.08 | 66.17 |  | 7 |
|  | 67.5 | 39.00 | 67.38 | 39.29 | 67.21 | 39.5 | 67.03 | 39.8 | 8 |
| $\begin{aligned} & 79 \\ & 80 \end{aligned}$ | 68.42 | 39.50 | 68.24 | 39.80 | 68.07 | 40.10 | 67.8 | 40.3 | 9 |
|  | 69.28 | 40.00 | 69.11 | i0.30 |  |  | 68.75 |  | 30 |
| 81 | 70.15 | 40.50 | 69.97 | 40.81 | 69.79 | 41.11 | 69.61 |  |  |
|  | 71.01 | 41.00 | 70.83 | 41.31 | 70.65 | 41. | 70.47 | 41. |  |
|  | 71.88 | 41.50 | 71.70 | 41.81 | 71.52 | 42. | 71.33 |  | 3 |
| 88 | 72.75 | 42.00 | 72.56 | 42.32 | 72.38 | 42. | 72.19 | 42. | 34 |
|  | 73.61 | 42.50 | 73.43 | 42.82 | 73.24 | 43.1 | 73.05 | 43.4 | 5 |
| 85 | 74.48 | 13.00 | 74.29 | 43.32 | 74.10 | 43.6 | 73.91 | 3. |  |
|  | 75.34 | 43.50 | 75.15 | 43.83 | 74.96 | 44.16 | 74.77 |  | 7 |
|  | 76.21 | 44.00 | 76.02 | 44.33 | 75.82 | 44.66 | 75.6 | 44. | 88 |
| 8990 | 77.08 | 44.50 | 76.88 | 44.84 | 76.68 | 45. | 76.49 |  | 59 |
|  | 77.94 | 45. | 77 | 4. | 77 |  |  |  |  |
|  | 78.81 | 45.50 | 78.61 | 45.84 | 78.41 | 46.19 | 78.21 |  | 91 |
| 92 | 79.67 | 46.00 | 79.4 | 46.3 | 79.27 | 46.69 | 79.07 | 47.04 | 92 |
|  | 80.54 | 46.50 | 80.34 | 46.85 | 80.13 | 47.20 | 79.92 | . |  |
|  | 81.41 | 47.00 | 81.20 | 47.35 | 80.99 | 47.71 | 30.78 | 8. | 94 |
|  | 82.27 | 47.50 | 82.06 | 47.86 | 31.85 | 48.22 | 81.64 | 48.5 |  |
| 9697 | 83.14 | 48.00 | 82.93 | 48.36 | 82.72 | 48.72 | 82.50 | 49.0 |  |
|  | 84.00 | 48.50 | 83.79 | 48.87 | 83.58 | 49.23 | 83.36 | 49.6 |  |
| $\begin{aligned} & 97 \\ & 98 \\ & 99 \end{aligned}$ | 34.87 | 49.00 | 84.66 | 49.37 | 84.44 | 4.74 | 84.22 | 50.1 |  |
|  | 85.7 | 49.50 | 85.52 | 49.87 | 85.30 | 50.25 | 85 | 50.6 | 99 |
| 100 |  | 50.00 | 86. | 50.38 | 86. | 50 |  | 51.1 | 100 |
| $\stackrel{\rightharpoonup}{\underline{\omega}}$ | Dep | at | De | Lat. | De | Lat. |  |  |  |
|  | 60 |  |  |  |  |  |  |  |  |

TRAVERSE TABLE.


|  | 31 Deg. |  | $31 \frac{1}{4}$ Deg. |  | $31 \frac{1}{2}$ Deg. |  | 313Deg. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. | Lat. | Dep. | Lat: | Dep. | Lat. | Dep. |  |
| 51 | \%.72 | 26.27 | 43.60 | 26. | 43.48 | 26.65 | 43.37 | 26.84 | 51 |
| 52 | 44.57 | 26.78 | 44.46 | 26.98 | 44.34 | 27.17 | 44.22 | 27.36 | 52 |
| 53 | 45.43 | 27.30 | 45.31 | 27.49 | 45.19 | 27.69 | 45.07 | 27.89 | 53 |
| 54 | 46.29 | 27.81 | 46.17 | 28.01 | 46.04 | 28.21 | 45.92 | 28.42 | 54 |
| 55 | 47.14 | 28.33 | 47.02 | 28.53 | 46.90 | 28.74 | 46.77 | 28.94 | 55 |
| 56 | 48.00 | 28.84 | 47.88 | 29.05 | 47.75 | 29.26 | 47.62 | 29.47 | 56 |
| 57 | 48.86 | 29.36 | 48.73 | 29.57 | 48.60 | 29.78 | 48.47 | 29.99 | 57 |
| 58 | 49.72 | 29.87 | 49.58 | 30.09 | 49.45 | 30.30 | 49.32 | 30.52 | 58 |
| 59 | 50.57 | 30.39 | 50.44 | 30.61 | 50.31 | 30.83 | 50.17 | 31.05 | 59 |
| 60 | 51.43 | 30.90 | 51.29 | 31.13 | 51.16 | 31.35 | 51.02 | 31.57 | 60 |
| 61 | 52.29 | 31.42 | 52.15 | 31.65 | 52.01 | 31.87 | 51.87 | 32.10 | 61 |
| 62 | 53.14 | 31.93 | 53.00 | 32.16 | 52.86 | 32.39 | 52.72 | 32.63 | 62 |
| 63 | 54.00 | 32.45 | 53.86 | 32.68 | 53.72 | 32.92 | 53.57 | 33.15 | 63 |
| 64 | 54.86 | 32.96 | 54.71 | 33.20 | 54.57 | 33.44 | 54.42 | 33.68 | 64 |
| 65 | 55.72 | 33.48 | 55.57 | 33.72 | 55.42 | 33.96 | 55.27 | 34.20 | 65 |
| 66 | 56.57 | 33.99 | 56.42 | 34.24 | 56.27 | 34.48 | 56.12 | 34.73 | 66 |
| 67 | 57.43 | 34.51 | 57.28 | 34.76 | 57.13 | 35.01 | 56.98 | 35.26 | 67 |
| 68 | 58.29 | 35.02 | 58.13 | 35.28 | 57.98 | 35.53 | 57.82 | 35.78 | 68 |
| 69 | 59.14 | 35.54 | 58.99 | 35.80 | 58.83 | 36.05 | 58.67 | 36.31 | 69 |
| 70 | 60.00 | 36.05 | 59.84 | 36.31 | 59.68 | 36.57 | 59.52 | 36.83 | 70 |
| 71 | 60.86 | 36.57 | 60.70 | 36.83 |  | 37.10 | 60.37 | 37.36 | 71 |
| 72 | 61.72 | 37.08 | 61.55 | 37.35 | 61.39 | 37.62 | 61.23 | 37.89 | 72 |
| 73 | 62.57 | 37.60 | 62.41 | 37.87 | 62.24 | 38.14 | 62.08 | 38.41 | 73 |
| 74 | 63.43 | 38.11 | 63.26 | 38.39 | 63.10 | 38.66 | 62.93 | 38.94 | 74 |
| 75 | 64.29 | 38.63 | 64.12 | 38.91 | 63.95 | 39.19 | 63.78 | 39.47 | 75 |
| 76 | 65.14 | 39.14 | 64.97 | 39.43 | 64.80 | 39.71 | 64.63 | 39.99 | 76 |
| 77 | 66.00 | 39.66 | 65.83 | 39.95 | 65.65 | 40.23 | 65.48 | 40.52 | 77 |
| 78 | 66.86 | 40.17 | 66.68 | 40.46 | 66.51 | 40.75 | 66.33 | 41.04 | 78 |
| 79 | 67.72 | 40.69 | 67.54 | 40.98 | 67.36 | 41.28 | 67.18 | 41.57 | 79 |
| 80 | 68.57 | 41.20 | 68.39 | 41.50 | 68.21 | 41.80 | 68.03 | 42.10 | 80 |
| 81 | 69.43 | 41.72 | 69.25 | 42.02 | 69.06 | 42.32 | 68.88 | 42.62 | 81 |
| 82 | 70.29 | 42.23 | 70.10 | 42.54 | 69.92 | 42.84 | 69.73 | 43.15 | 82 |
| 83 | 71.14 | 42.75 | 70.96 | 43.06 | 70.77 | 43.37 | 70.58 | 43.68 | 83 |
| 84 | 72.00 | 43.26 | 71.81 | 43.58 | 71.62 | 43.89 | 71.43 | 44.20 | 84 |
| 85 | 72.86 | 43.78 | 72.67 | 44.10 | 72.47 | 44.41 | 72.28 | 44.73 | 85 |
| 86 | 73.72 | 44.29 | 73.52 | 44.61 | 73.33 | 44.93 | 73.13 | 45.25 | 86 |
| 87 | 74.57 | 44.81 | 74.38 | 45.13 | 74.18 | 45.46 | 73.98 | 45.78 | 87 |
| 88 | 75.43 | 45.32 | 75.23 | 45.65 | 75.03 | 45.98 | 74.83 | 46.31 | 88 |
| 89 | 76.99 | 45.84 | 76.09 | 46.17 | 75.88 | 46.50 | 75.68 | 46.83 | 89 |
| 90 | 77.15 | 46.35 | 76.94 | 46.69 | 76.74 | 47.02 | 76.53 | 47.36 | 90 |
| 91 | 78.00 | 46.87 | 77.80 | 47.21 | 77.59 | 47.55 | 77.38 | 47.89 | 91 |
| 92 | 78.86 | 47.38 | 78.65 | 47.73 | 78.44 | 48.07 | 78.23 | 48.41 | 92 |
| 93 | 79.72 | 47.90 | 79.51 | 48.25 | 79.30 | 48.59 | 79.08 | 48.94 | 93 |
| 94 | 80.57 | 48.41 | 80.36 | 48.76 | 80.15 | 49.11 | 79.93 | 49.47 | 94 |
| 95 | 81.43 | 48.93 | 81.22 | 49.28 | 81.00 | 49.64 | 80.78 | 49.99 | 95 |
| 96 | 82.29 | 49.44 | 82.07 | 49.80 | $81 \cdot 85$ | 50.16 | 81.63 | 50.52 | 96 |
| 97 | 83.15 | 49.96 | 82.93 | 50.32 | 82.71 | 50.68 | 82.48 | 51.04 | 97 |
| 98 | 84.00 | 50.47 | 83.78 | 50.84 | 83.56 | 51.20 | 83.33 | 51.57 | 98 |
| 99 | 84.86 | 50.99 | 84.64 | 51.36 | 84.41 | 51.73 | 84.18 | 52.10 | 99 |
| 100 | 85.72 | 51.50 | 85.49 | 51.88 | 85.26 | 52.25 | 85.04 | 52.62 | 100 |
| $\stackrel{\square}{*}$ | Dep | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. |  |
|  | 59 Deg. |  | $58 \frac{3}{4}$ Deq. |  | $58 \frac{1}{2} \mathrm{Deg}$. |  | $58 \frac{1}{4} \text { Des. }$ |  |  |

TRAVERSE TABLE:

| 苞 | 32 D | Deg. | 32 ${ }_{4}^{1}$ D | Deg. | $32 \frac{1}{2}$ | eg. | 32 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. D | Dep. | Lat. D | Dep. | Lat. | Dep. | Lat |  |  |
|  | 0.85 | 0.53 |  | 0.53 | 0.84 | 0.54 | , |  |  |
|  | 1.70 | 1.06 | 169 | 1.07 | 1.6 | , ${ }^{5}$ | 88 |  |  |
|  | 2.54 | 1.59 | 2.54 | 1.60 | 2 |  | 2.52 |  |  |
|  | 3.39 | 2.12 | 3.38 | 2.13 | 3.37 | 2.15 | 3.36 |  |  |
|  | 5.09 | 3.18 | 4.23 | ${ }^{2.67}$ | 4.22 5.06 |  | ${ }_{5}^{4.21}$ | 3.25 |  |
|  | 5.94 | 3.71 | 5.92 | 3.74 | 5.90 | 3.7 | 5.89 | 3.79 |  |
|  | 6.78 | 4.24 | 6.77 | 4.27 | 6.75 | 4.3 | 6.73 | 4.33 |  |
| 10 | 8.4 | 4.75 | 7.6 | 4.80 | 7.59 | 4.84 | 7.57 |  |  |
|  | 8.48 | 5.30 | 8.46 | 5.34 | 8.43 | 5.37 | 8.41 |  |  |
| 11 | 9.38 | 5.8 | . 30 | 5.87 | 9.28 | 5.91 | 9.25 |  |  |
|  | 10.18 | ${ }_{6}^{6.36}$ | 10.15 | 6.40 | 10.12 | 6.45 | 10.09 | 49 |  |
|  | 1311.02 | ${ }_{7}^{6.89}$ | ${ }^{10.95}$ | 6.94 | ${ }_{11}^{10.96}$ | 6.98 | 10.9 |  |  |
|  | 11.87 | ${ }^{7.95}$ | [12.69 | 7.47 8.00 | 11.81 | ${ }_{8.06}^{7.52}$ | 11.7 |  | 14 |
|  | 13.57 | 8.48 | 13.53 | 8.54 | 13.49 | 8.60 | 13. |  | 6 |
|  | 14.42 | 9.01 | 14.38 | 9.07 | 14.34 | 9.13 | 14.5 | 9.2 | 17 |
|  | 15.26 | 9.54 | 15.22 | 9.61 | 15.18 | 9.67 | 15.14 | 4.74 | 18 |
| 19 | 16.11 | 10.07 |  | 10.14 | 16. | 10.21 |  |  | 19 |
| 20 | 16.96 | 10.6 | 16.91 | 10.67 | 16.87 | 10.75 | 16. |  | 20 |
| $\left\|\begin{array}{l\|} 21 \\ 22 \\ 23 \\ 24 \\ 24 \\ 25 \\ 26 \\ 27 \\ 28 \\ 28 \\ 29 \end{array}\right\|$ | 17.81 | 11.13 | 17.7 | 11.21 | 17.71 | 1.28 |  |  | 21 |
|  | 218.66 | 11.66 | 18.61 | 11.74 | 18.55 | 11.82 | 18.50 |  |  |
|  | 319.51 | 12.19 | 19.45 | 2.27 | 19.40 | 12.36 | 19.3 |  |  |
|  | 420.35 | 12.72 | 20. | 12.81 | 0.24 | 2.90 | 2 L .1 |  | 24 |
|  | 550.21.2 | ${ }^{13.25}$ | 21.14 | 13.34 | ${ }^{21.08}$ | ${ }^{13.43}$ | 21.83 |  | 25 |
|  | 722.90 | 14.31 | 22.83 | 14.41 | 22.77 | 714.51 | 22.71 |  |  |
|  | 823.75 | 14.34 | 23.68 | 14.94 | 23.61 | 15.04 | 23.55 |  |  |
|  | 924.5 | 5.37 | 24.5 | 15.47 | 24.46 | 15.58 | 24.3 |  |  |
|  | 25.44 | 15.90 | 25.3 | . 0 | 25.30 | 16.12 | 25.2 |  |  |
|  |  | 8.43 |  | 16.54 | 26.15 | 16.66 |  |  | 31 |
|  |  | 1.9 | 27.06 | 17.08 | 26.99 | 917.19 | 26.9 |  |  |
|  | $3{ }^{27.99}$ | 17.49 | 27.91 | 17.61 | 27.83 | 317.73 | 27.7 |  |  |
|  | 54 28.88 | 18.02 | 28.75 | 18.14 | 28.68 | 818.27 | 8. |  |  |
|  | 29.68 | 8.55 | 29.60 | 18.68 | 29.52 | ${ }^{18.81}$ | 29.4 |  |  |
|  | 13.38 | 19.61 | ${ }^{31.29}$ | 19.74 | ${ }_{31.21}^{30.36}$ | 19.88 |  |  | 37 |
|  | 析 | 20.14 | 32.14 | 20.28 | 32.0 | 20.42 | 31.96 |  |  |
|  | 9 | 0.67 | 32.9 | 0.8 | 32. | 20. |  |  |  |
|  | 033.92 | 21.20 | 33.83 | 1.34 | 33.74 | 71.49 | 33. |  |  |
|  | 4134.77 | 21.78 | 34. | 21.88 | 34.58 | 22.03 |  |  | 41 |
| 432.35.62 |  | 22. |  | 2.4 | 35.42 | 22.57 | 35.32 | 72 |  |
|  |  | ${ }^{22.79}$ | ${ }^{36.37}$ | 222.95 |  |  |  |  |  |
|  | 4437.31 | 23.92 | 37.21 | 123.48 | 37.11 | 123.64 | 37.01 | 123.8 |  |
|  | $5{ }^{3} / 8.16$ | 23.85 | 38.06 | 624.01 | 37.95 | 24.18 | 37.85 | 5.24.3 |  |
|  | 4639.0 | 24.38 | 38.90 | 24.55 | 38.50 | 24.72 | 38.6 | 24.88 |  |
|  | 4739.8 | 24.91 | 39.7 | 25.08 |  |  | 39.5 | 325.43 |  |
|  | 4840.71 | 2.44 | 40.59 | 25.61 | 40. | 25.79 | 40.37 |  |  |
|  | 41.55 | 25.97 | 41.44 | 26.15 | 41. | 26.33 |  |  |  |
|  | ${ }^{50} 42.40$ | 26.5 | 42.29 | 26.68 | 42.17 | 26.86 | 42.05 |  | 50 |
|  | Dep | Lat. | Dep |  | Dep. | Lat. | Dep. |  |  |
|  | 58 |  |  |  |  |  |  |  |  |




TRAVERSE TABLE.


|  | Lat. | $\frac{\text { Deg. }}{\text { Dep. }}$ | $34 \frac{1}{4}$ Deg. |  | $34 \frac{1}{3} \mathrm{Deg}$. |  | $34_{4}^{3}$ Deg. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. |  |
| , | 0.83 | 0.56 | 0.83 | 0.56 | 0.32 | 0.57 | 0.82 | 0.57 | 1 |
| 2 | 1.66 | 1.12 | 1.65 | 1.13 | 1.65 | 1.13 | 1.64 | 1.14 | 2 |
| 3 | 2.49 | 1.68 | 2.48 | 1.69 | 2.47 | 1.70 | 2.46 | 1.71 | 3 |
| 4 | 3.82 | 2.24 | 3.31 | 2.25 | 3.30 | 2.27 | 3.29 | 2.28 |  |
| 5 | 4.15 | 2.80 | 4.13 | 2.81 | 4.12 | 2.83 | 4.11 | 2.85 | 5 |
| 6 | 4.97 | 3.36 | 4.96 | 3.38 | 4.94 | 3.40 | 4.93 | 3.42 | 6 |
| 7 | 5.80 | 3.91 | 5.79 | 3.94 | 5.77 | 3.96 | 5.75 | 3.99 | 7 |
| 8 | 6.63 | 4.47 | 6.61 | 4.50 | 6.59 | 4.53 | 6.57 | 4.56 | 8 |
| 9 | 7.46 | 5.03 | 7.44 | 5.07 | 7.42 | 5.10 | 7.39 | 5.13 | 9 |
| 10 | 8.29 | 5.59 | 8.27 | 5.63 | 8.24 | 5.66 | 8.22 | 5.70 | 10 |
| 11 | 9.12 | 6.15 | 9.09 | 6.19 | 9.07 | 6.23 | 9.04 | 6.27 | 11 |
| 12 | 9.95 | 6.71 | 9.92 | 6.75 | 9.89 | 6.80 | 9.86 | 6.84 | 12 |
| 13 | 10.78 | 7.27 | 10.75 | 7.32 | 10.71 | 7.36 | 10.68 | 7.41 | 13 |
| 14 | 11.61 | 7.83 | 11.57 | 7.88 | 11.54 | 7.93 | 11.50 | 7.98 | 14 |
| 15 | 12.44 | 8.39 | 12.40 | 8.44 | 12.36 | 8.50 | 12.32 | 8.55 | 15 |
| 16 | 13.26 | 8.95 | 13.23 | 9.00 | 13.19 | 9.06 | 13.15 | 9.12 | 16 |
| 17 | 14.09 | 9.51 | 14.05 | 9.57 | 14.01 | 9.63 | 13.97 | 9.69 | 17 |
| 18 | 14.92 | 10.07 | 14.88 | 10.13 | 14.83 | 10.20 | 14.79 | 10.26 | 18 |
| 19 | 15.75 | 10.62 | 15.71 | 10.69 | 15.66 | 10.76 | 15.61 | 10.83 | 19 |
| 20 | 16.58 | 11.18 | 16.53 | 11.26 | 16.48 | 11.33 | 16.43 | 11.40 | 20 |
| 21 | 17.41 | 11.74 | 17.36 | 11.82 | 17.31 | 11.69 | 17.25 | 1.97 | 21 |
| 22 | 18.24 | 12.30 | 18.18 | 12.38 | 18.13 | 12.46 | 18.08 | 12.54 | 22 |
| 23 | 19.07 | 12.86 | 19.01 | 12.94 | 18.95 | 13.03 | 18.90 | 13.11 | 23 |
| 24 | 19.90 | 13.42 | 19.84 | 13.51 | 19.78 | 13.59 | 19.72 | 13.68 | 24 |
| 25 | 20.73 | 13.98 | 20.66 | 14.07 | 20.60 | 14.16 | 20.54 | 14.25 | 25 |
| 26 | 21.55 | 14.54 | 21.49 | 14.63 | 21.43 | 14.73 | 21.36 | 14.82 | 26 |
| 27 | 22.38 | 15.10 | 22.32 | 15.20 | 22.25 | 15.29 | 22.18 | 15.39 | 27 |
| 28 | 23.21 | 15.66 | 23.14 | 15.76 | 23.08 | 15.86 | 23.01 | 15.96 | 28 |
| 29 | 24.04 | 16.22 | 23.97 | 16.32 | 23.90 | 16.43 | 23.83 | 16.53 | 29 |
| 30 | 24.87 | 16.78 | 24.80 | 16.88 | 24.72 | 16.99 | 24.65 | 17.10 | 30 |
| 31 | 25.70 | 17.33 | 25.62 | 17.45 | 25.55 | 17.56 | 25.4 | 17.67 | 31 |
| 32 | 26.53 | 17.89 | 26.45 | 18.01 | 26.37 | 18.12 | 26.29 | 18.24 | 32 |
| 33 | 27.36 | 18.45 | 27.28 | 18.57 | 27.20 | 18.69 | 27.11 | 18.81 | 33 |
| 34 | 28.19 | 19.01 | 28.10 | 19.14 | 28.02 | 19.26 | 27.94 | 19.38 | 34 |
| 35 | 29.02 | 19.57 | 28.93 | 19.70 | 28.84 | 19.82 | 28.76 | 19.95 | 35 |
| 36 | 29.85 | 20.13 | 29.76 | 20.26 | 29.67 | 20.39 | 29.58 | 20.52 | 36 |
| 37 | 30.67 | 20.69 | 30.58 | 20.82 | 30.49 | 20.96 | 30.40 | 21.09 | 37 |
| 38 | 31.50 | 21.25 | 31.41 | 21.39 | 31.32 | 21.52 | 31.22 | 21.66 | 38 |
| 39 | 32.33 | 21.81 | 32.24 | 21.95 | 32.14 | 22.09 | 32.04 | 22.23 | 39 |
| 40 | 33.16 | 22.37 | 33.06 | 22.51 | 32.97 | 22.66 | 32.87 | 22.80 | 40 |
| 41 | 33.99 | 22.93 | 33.89 | 23.07 | 33.79 | 23.22 | 33.69 | 23.37 | 41 |
| 42 | 34.82 | 23.49 | 34.72 | 23.64 | 34.61 | 23.79 | 34.51 | 23.94 | 42 |
|  | 35.65 | 24.05 | 35.54 | 24.20 | 35.44 | 24.36 | 35.33 | 24.51 | 43 |
|  | 36.48 | 2.4.60 | 36.37 | 24.76 | 36.26 | 24.92 | 36.15 | 25.08 | 44 |
| 45 | 37.81 | 25.16 | 37.20 | 25.33 | 37.09 | 25.49 | 36.97 | 25.65 | 45 |
| 46 | 38.14 | 25.72 | 38.02 | 25.89 | 37.91 | 26.05 | 37.80 | 26.22 | 46 |
| 47 | 38.96 | 26.28 | '38.85' | '26.45 | 38.73 | 26.62 | 38.62 | 26.79 | 47 |
| 48 | 39.79 | 26.84 | 39.68 | 27.01 | 39.56 | 27.19 | 39.44 | 27.36 | 48 |
| 49 | 40.62 | 27.40 | 40.50 | 27.58 | 40.38 | 27.75 | 40.26 | 27.93 | 49 |
| 50 | 41.45 | 27.96 | 41.33 | 28.14 | 41.21 | 28.32 | 41.08 | 28.50 | 50 |
|  | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | - |
|  | 56 Deg. $55{ }_{4}^{3} \mathrm{Deg} .{ }_{55 \frac{1}{2} \mathrm{Deg} .} 55 \frac{1}{4} \mathrm{Deg} . \mathrm{A}$ |  |  |  |  |  |  |  |  |



| $35 \mathrm{Deg} .35{ }_{4}^{1} \mathrm{Deg} .35 \frac{1}{2} \mathrm{Deg} .35{ }_{4}^{3} \mathrm{Deg}$. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L |  |  |  |  |  | Lat. | De |  |
|  | 10.82 |  | 0.82 | 0.58 | 0.81 | 0.58 | 0.81 | 0 |  |
|  | $2{ }^{2} 1.64$ | 1.15 | 1.63 | 1.15 |  | ${ }^{1} 1.16$ | 1.62 | 1.17 |  |
|  | 3 2.46 <br> 4 2.48 | 1.72 | ${ }_{3}^{2.45}$ | 1.73 | 2.44 | [4 | 2.43 | [ 1.75 | 3 |
|  | 54.10 | ${ }_{2.87}$ | 3.28 | 2.89 | 4.07 | ${ }^{2}$ | ${ }^{3.06}$ | ${ }_{2}^{2.92}$ |  |
|  | 64.91 | 3.44 | 4.90 | 3.46 | 4.88 | 3.48 | 4.87 | 3.5 |  |
|  | 75.73 | 4.01 | 5.72 | 4.04 | 5.7 | 4.06 | 5.6 | 4.09 |  |
|  | $8{ }^{8} 6.55$ | 4.59 | 6.53 | 4.62 | 6.51 | 14.6 |  | 4.6 |  |
|  | 9 7.37 <br> 0 8.19 | 5.16 | 7.17 8.17 | 5.19 5.77 | 7.33 8.14 | $14{ }^{5} 5.81$ | 8.12 | [ 5.84 | 10 |
|  | 19.01 | 6.31 | 8.98 | 6.35 |  | 6.39 | 8.93 | 6.43 |  |
|  | 2.9 .83 | 6.88 | 9.80 | 6.93 | 9.77 | 76.97 | 9.74 | 7.01 |  |
|  | 310.65 | 7.46 | 10.62 | 7.50 | 10.5 | 7.55 | 10.5 |  |  |
|  | 411.47 | 8.03 | 11.43 | 8.08 | 11.4 | 8.17 |  | 8.18 |  |
|  | 1-21 | 8.60 | 12.25 | 8.66 | 12.21 | 8.71 | 12.17 | 18.76 |  |
|  | 613.11 | 9.18 | 13.07 | 9.23 | 13.03 | 9.29 | 12.99 | ${ }^{9.35}$ |  |
|  | 713.93 | 9.75 | 13.88 | 9.81 | 13.84 | 9.87 |  | 9.93 |  |
|  | 814.74 | 10.32 | 14.70 | 10.39 | 14.65 | 10.45 | 14.61 |  |  |
|  |  | 10.90 | 15.52 | 10.97 | 15.4 | 11.0 | 15.42 | 11. | 19 |
|  | 016.38 | 11.47 | 16.3 | 1.54 | 16. | 1.61 | 16.23 |  | 20 |
|  | 17.20 | 12.05 |  | 12.12 |  | 2.19 | 17. | 12.27 | 1 |
|  |  |  | 17.9 |  | 17.9 | 28 | 17.85 |  |  |
|  | 18.84 | 13.19 | 18.78 |  | 18.72 | 13.36 | 18.67 |  |  |
|  | 419.6 | 13. | 19.60 | 13.85 | 19.54 | 413.94 | 19.48 |  |  |
|  | 520.48 | 14.34 | 20.42 | 14.43 | 20.35 | 14.52 | 20.29 | 14.61 |  |
|  | 1.30 | 14.91 | 21.23 | 15.01 | 21.17 | 715.10 | 21.10 | 15.19 |  |
|  | 7.22.12 | 15.49 | 22.05 | 15.58 | 21.98 | 815.68 | 21.91 |  |  |
|  | 22.94 | 16.06 | 22.87 | 16.16 | 22.8 | 16.26 | 22.72 | , |  |
|  | 293.76 | 16.63 | 23.68 | 16.74 | 23.61 | 16.84 | 23.54 |  |  |
|  | 024.57 | 17.21 | 24.50 | 17.31 | 24. | 7.4 | 24.35 |  |  |
| 25.3917 |  |  |  | 89 |  | 418.00 |  |  |  |
| 35 |  |  | 26. | 8.47 | 26.05 | 518.58 | 25.97 |  |  |
|  |  |  | 26.95 | 19.05 | 26,87 | 719.16 | 26.78 |  |  |
|  |  |  |  |  |  |  |  |  |  |
| 29.4920 .65 29.40 20.78 29.31 20.91 29.22 21.03 |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  | 1.95 | 22.37 | 31.85 | 22.51 | 31.75 | 522.65 | 31.65 | 22.79 |  |
|  | 032.772 | 22.94 | 32.6 | . 09 | 32.5 | 62.2 |  |  |  |
| 33.59: 23.52 33.48 23.66 33.3883.81 |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| 42 34.4024.09 34.30 24.24 34.19 24.39 34.09 24.54 4335.2224 .6635 .1224 .8235 .01 24.97 34.90 25.12 |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  | 28.11 |  | . 28 |  |  |  |  |  |
|  | 68 |  | 40.83 | 28.8 | 40.71 | 129.04 | 40.58 | 29.2 |  |
|  | Dep | Lat. | Dep. | Lat | Dep | Lat. | Dep. |  |  |
|  | 55 | eg |  |  |  |  |  |  |  |



|  | 36 |  |  |  |  | eg. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\stackrel{\square}{+}$ | Lat. | Dep. | Lat | Dep. |  | Dep. | Lat. | Dep. |  |
| 1 | 0.81 | 0.59 | 0.81 | 0.59 | 0.80 | 0.59 | 0.80 | 0.60 |  |
| 2 | 1.62 | 1.18 | 1.61 | 1.18 | 1.61 | 1.19 | 1.60 | 1.20 |  |
| 3 | 2.43 | 1.76 | 2.42 | 1.77 | 2.41 | 1.78 | 2.40 | 1.78 |  |
| 4 | 3.24 | 2.35 | 3.23 | 2.37 | 3.2 | 2.38 | 3.20 | 2.39 |  |
| 5 | 4.05 | 2.94 | 4.03 | 2.96 | 4.02 | 2.97 | 4.01 | 2.99 |  |
| 6 | 4.85 | 3.53 | 4.84 | 3.55 | 4.82 | 3.57 | 4.81 | 3.59 |  |
| 7 | 5.66 | 4.11 | 5.65 | 4.14 | 5.6 | 4.16 | 5.61 | 4.19 |  |
| 8 | 6.47 | 4.70 | 6.45 | 4.73 | 6.4 | 4.76 | 6.41 | 1.73 |  |
| 9 | 7.28 | 5.29 | 7.26 | 5.32 | 7.23 | 5.35 | 7.21 | 5.38 |  |
| 10 | 8.09 | 5.88 | 8.06 | 5.91 | 8.04 | 5.95 | 8.01 | 5.88 | 10 |
| 11 | 8.90 | 6.47 | 8.87 | 6.50 | 8.8 | 6.54 | 8.81 | 6.58 | 11 |
| 12 | 9.71 | 7.05 | 9.68 | 7.10 | 9.6 | 7.14 | 9.61 | 7.18 | 12 |
|  | 10.52 | 7.64 | 10.48 | 7.69 | 10.45 | 7.73 | 10.42 | 7.78 | 3 |
|  | 11.33 | 8.23 | 11.29 | 8.28 | 11.25 | 8.33 | 11.22 | 8.3 | 4 |
|  | 12.14 | 8.82 | 12.10 | 8.87 | 12.0 | 8.92 | 12.0 | 8.97 |  |
|  | 12.94 | 9.40 | 12.90 | 9.46 | 12.86 | 9.52 | 12.82 | 9.57 | 16 |
|  | 13.75 | 9.99 | 13.71 | 10.05 | 13.67 | 0.11 | 13.62 | 0.17 | 17 |
|  | 14.56 | 10.58 | 14.52 | 10.64 | 14.47 | 10.71 | 14.42 | 0.77 | 8 |
|  | 15.37 | 11.17 | 15.32 | 11.23 | 15.27 | 11.30 | 15.22 | 11.37 | 19 |
|  | 16.18 | 11.76 | 16.13 | 11.83 | 16.08 | 11.90 | 16.03 | 11.97 | 8 |
|  | 16.99 | 12.34 | 16.94 | 12.42 | 16.88 | 12.49 | 16.83 | 12.56 | 1 |
|  | 17.80 | 12.93 | 17.74 | 13.01 | 17.68 | 13.09 | 17.63 |  | 22 |
|  | 18.61 | 13.52 | 18.55 | 13.60 | 18.49 | 13.68 | 18.43 | 13.76 | 23 |
|  | 19.42 | 14.11 | 19.35 | 14.19 | 19.29 | 14.28 | 19.23 | 14.36 | 2 |
|  | 20.23 | 14.69 | 20.16 | 14.78 | 20.10 | 14.8 | 20.03 | 4. | 25 |
|  | 21.03 | 15.28 | 20.97 | 15.37 | 20.90 | 5.47 | 20.83 | 5.56 | 26 |
|  | 21.8 | 15.87 | 21.77 | 15.97 | 21.70 | 16.06 | 21.63 | 16.15 | 27 |
|  | 22.65 | 16.46 | 22.58 | 16.56 | 22.51 | 16.65 | 22.44 | 16.75 | 28 |
| $\begin{aligned} & 29 \\ & 30 \end{aligned}$ | 23.46 | 17.05 | 23.39 | 7.15 | 23.31 | 17.25 | 23.24 | 17.35 | 9 |
|  | 24.27 | 17.63 | 24.19 | 17.74 | 24.12 | 17.84 | 24.04 | 17.95 | 0 |
|  | 25.081 | 18.22 | 25.00 | 18.33 | 24.92 | 18.44 | 24.84 | 18. | 1 |
|  | 25.891 | 18.81 | 25.81 | 18.92 | 25.72 | 19.03 | 25.64 | 1.15 | 2 |
|  | 26.70 | 19.40 | 26.61 | 19.51 | 26.53 | 19.63 | 26.44 | 9.74 | 33 |
|  | 27.51 | 19.98 | 27.42 | 20.10 | 27.33 | 20.22 | 27.24 | 20.34 | 34 |
|  | 28.32 | 20.57 | 28.23 | 20.70 | 28.13 | 20.82 | 28.04 | 20.94 | 35 |
|  | 29.12 | 21.16 | 29.03 | 21.29 | 28.94 | 21.41 | 28.85 | 21.54 | 36 |
| 37 <br> 38 | 29.93 | 21.75 | 29.84 | 21.88 | 29.74 | 22.01 | 29.65 | 22.14 |  |
|  | 30.74 | 22.34 | 30.64 | 22.47 | 30.55 | 22.60 | 30.45 | 22.74 |  |
| $\left\lvert\, \begin{aligned} & 30 \\ & 39 \\ & 40 \end{aligned}\right.$ | 31.55 | 22.92 | 31.45 | 23.06 | 31.35 | 23.20 | 31.25 | 23.33 | 39 |
|  | 32.36 | 23.51 | 32.26 | 3.65 | 32.15 | 23.79 | 32.05 | 23.93 | , |
| 41 | 53.17 | 24.10 | 33.06 | 24.24 | 32.96 | 24.39 | 32.85 | 24.53 | 41 |
| 4 | 33.98 | 24.69 | 33.87 | 24.83 | 33.76 | 24.98 | 33.65 | 25.13 | 42 |
|  | 34.792 | 25.27 | 34.68 | 25.43 | 34.57 | 25.58 | 34.45 | 25.73 | 43 |
|  | 35.602 | 25.86 | 35.48 | 26.02 | 35.37 | 26.17 | 35.26 | 26.83 | 44 |
|  | 36.41 2 | 26.45 | 36.29 | 26.61 | 36.17 | 26.77 | 36.06 | 26.92 | 45 |
|  | 37.212 | 27.04 | 37.10 | 27.20 | 36.98 | 27.36 | 36.86 | 27.52 | 46 |
|  | 38.02 2 | 27.63 | 37.90 | 27.79 | 37.78 | 27.96 | 37.66 | 38.12 | 47 |
|  | 38.832 | 28.21 | 38.71 | 28.38 | 36.59 | 28.55 | 38.46 | 28.78 | 48 |
|  | 39.64 | 28.80 | 39.52 | 28.97 | 39.39 | 29.15 | 39.26 | 29.32 | 4 |
| 49 | 40.4 | 29.39 | 40.32 | 9.57 | 40.19 | 29.74 | 40.06 | 29.92 | 50 |
|  | Dep. | Lat. | Dep | Lat. | Dep | Lat. | Dep |  |  |
|  | 54 |  |  |  |  |  |  |  |  |

TRAVERSE TABLE.

|  | Lat |  |  | ep. |  | De | Lat. |  | $\stackrel{\square}{\square}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 29.98 | 41.18 | 30.16 | 41.00 | 30.34 | 40.8 |  |  |
|  | 42.07 | 30.56 | 41.94 | 30.75 | 41.8 | 30.93 | 41.6 |  | 52 |
|  | . 8 | 31.15 |  | 1. | 42.6 | 31.53 | 42. |  | 53 |
|  | 13.69 | 31.74 | 43.55 | 31. | 43.41 | 32.12 | 43.2 | 2.31 | 54 |
|  | 44.50 | 32.33 | 44.35 | 32. | 44.21 | 32.72 | 44.0 |  |  |
|  | 45.30 | 32.92 | 45.16 | 33.11 | 45.02 | 33.31 | 44.8 |  | 56 |
|  | 46.11 | 33.50 |  |  | 45.8 | 33.90 | 45.6 |  | 7 |
|  | 46.92 | 34.09 | 46.77 | 34.30 | 46.62 | 34.50 | 46.4 | 34.70 | 58 |
|  | 47.73 | 34.68 | 47.58 | 34.89 | 47.43 | 35.09 | 47.2 |  | 59 |
| 60 | 485 | 35.27 | 48.39 | 35.48 | 48.23 | 35. | 48.08 |  |  |
|  |  | 35.8 |  |  |  |  | 48 |  |  |
|  | 0.16 | 5. |  |  |  |  | 49. |  | 2 |
|  | 0.97 | 37.0 |  |  |  | . |  |  |  |
|  | 51.78 | 37.62 | 51.6 |  | 51.4 | 38. | 51. | 8.29 | 64 |
|  | 52.59 | 38.21 | 52.4 | 38. | 52. | 88 | 52. | 38.8 | 5 |
|  | 53.40 | 38.79 | 53.23 | 39.03 |  | 39.26 | 52.8 | 3.4 | 66 |
|  | 54.20 | 39.38 | 54.0 | 39.62 | 53.8 | 39. | 53. | 40.0 | 67 |
|  | 5.01 | 39.97 | 54.8 | 40.21 | 54.6 | 40.4 | 54. | 40.69 | 68 |
|  | 55.82 | 40.56 | 55.6 | 40.80 | 55.47 | 41.0 | 55.2 |  | ${ }^{69}$ |
| 70 |  |  | 56.45 | 41.39 | 56.27 | 41.64 |  |  |  |
|  | 57.44 | . 7 |  | 41.98 | 57.0 | 42. |  |  |  |
|  | 88.25 | , | 58.06 |  | 57.8 |  | 57.6 |  | 72 |
|  | 69.06 | 42.91 | 58.87 | 43.17 | 58.6 | 43.4 | 58. |  | 73 |
|  | 59.87 | 43.50 | 59.68 | 43.76 | 59.4 | 4.0 | 59. |  | 74 |
|  | 60.68 | 44.0 | 60.48 | 44.35 | 60.2 | 44.6 | 60.0 |  | 75 |
|  | 61.49 | 44.67 | 61.2 | 44.94 | 61. | 45.2 | 60.9 |  | 76 |
|  | 2.29 | 45.26 | 62.10 | 45.53 | 61.9 | 45.8 | 61. |  |  |
|  | 63.10 | 45.85 | 62.90 | 46.12 | 62.7 | 46.4 | 62. |  | 78 |
|  | 63.9 | 46.43 | 63.71 | 46.71 | 63.50 | 46.99 |  |  | 9 |
| 80 | 64 | 47, | 64.52 | 47.3 | 64.31 | 47.5 |  |  |  |
|  | 65 |  |  |  |  |  |  |  | 81 |
|  | 66.3 | 48.2 | 66.13 | 48.49 | 65.92 | 48.78 | 65.70 |  |  |
|  | 67.1 | 48.7 | 66.93 | 49.08 | 66.72 | 49.37 | 66.5 |  | 83 |
|  | 67. | 49.3 | 67.7 | 49.67 | 67.5 | 49.97 | 67.31 |  | 4 |
|  | 68.77 | 49.96 | 68.55 | 50.28 | 68.33 | 50.56 | 68.11 | 50. | 85 |
|  | 69.58 | 50.55 | 69.35 | 50.85 | 69.13 | 51.15 | 68.91 |  | 86 |
|  | 70.38 | 51.14 | 70.16 | 51.44 | 69.9 | 1.75 | 69.71 |  | 87 |
|  | 71.19 | 51.73 | 70.97 | 52.04 | 70.74 | 52.34 | 70.51 | 52.65 | 88 |
|  | 72.00 | 52.31 | 71.77 | 52.63 | 71.54 | 52.94 | 71.31 | 53 |  |
| 90 | 72.81 | 52.90 | 72.5 | 53.22 | 72.3 | 53.53 | 72. |  |  |
|  |  | 53.49 | 73.39 | 53. | 73. | 54.13 | 72.91 |  | 1 |
|  | 74.4 | 54.08 | 74.19 | 54.40 | 73.95 | 54.72 | 73.72 | 55.05 |  |
|  | 75.2 | 54.66 | 75.0 | 54.99 | 74.7 | 55.32 | 74.5 | . 64 |  |
|  | 76.0 | 55.25 | 75.81 | 55.58 | 75.5 | 55.91 | 5. | . 24 | 5 |
|  | 76.86 | 55.84 | 76.61 | 56.17 | 76.37 | 56.51 | 76.12 | 6.84 | 95 |
|  | 77.67 | 56.43 | 77.42 | 56.77 | 77.17 | 57.10 | 76.92 | 57.44 | 96 |
|  | 78.47 | 57.02 | 78.23 | 57.36 | 7.97 | 7.70 | 77.72 | 8.04 |  |
|  | 79.28 | 57.60 | 79.03 | 57.95 | 78.78 | 58.23 | 78.52 | 8.64 | 8 |
|  | 80. | 58.19 | 79 | 58. | 79.5 | 58.89 |  |  |  |
| 100 | 80.90 | 58. |  | 59.13 | 80.3 | 59.48 | 80 |  |  |
|  | Dep | Lat. | De | Lat. | D | La |  |  |  |
|  |  |  |  |  |  |  |  |  |  |


| $\stackrel{\square}{2}$ | $4 \text { Lat. }$ | Dep. |  | Dep | Lat | Dep. | Lat. | Deg. | + |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10.80 | 0.60 | 0.80 | 0.61 | 0.79 | 9.61 | 0.79 | 90.61 |  |
|  | 21.60 | 1.20 | 1.59 | 1.21 | 1.59 | 91.22 | 1.58 | 81.22 | 2 |
|  | 32.40 | 1.81 | 2.39 | 1.82 | 2.38 | 1.83 | 2.37 | 71.84 | 3 |
|  | 4 3.19 | 2.41 | 3.18 | 2.42 | 3.17 | 2.43 | 3.16 | 62.45 | 4 |
|  | 53.99 | 3.01 | 3.98 | 3.03 | 3.97 | 3.04 | 3.95 | 53.06 | 5 |
|  | 64.79 | 3.61 | 4.78 | 3.63 | 4.76 | 3.65 | 4.74 | 43.67 | 6 |
|  | 75.59 | 4.21 | 5.57 | 4.24 | 5.55 | 4.26 | 5.53 | 4.29 | 7 |
|  | 8.6 .39 | 4.81 | 6.37 | 4.84 | 6.35 | 4.87 | 6.33 | 4.90 | 8 |
|  | 97.19 | 5.42 | 7.16 | 5.45 | 7.14 | 5.48 | 7.12 | 5.51 | 9 |
| 10 | ) 7.99 | 6.02 | 7.96 | 6.05 | 7.93 | 6.09 | 7.91 | 16.12 | 10 |
| 11 | 1.8 .78 | 6.62 | 8.76 | 6.66 | 8.73 | 6.70 | 8.70 | 6.73 | 1 |
| 12 | 9.58 | 7.22 | 9.55 | 7.86 | 9.52 | 7.31 | 9.49 | 7.35 | 12 |
| 13 | 10.38 | 7.82 | 10.35 | 7.87 | 10.31 | 7.91 | 10.28 | 7.96 | 13 |
| 14 | 411.18 | 8.43 | 11.14 | 8.47 | 11.11 | 8.52 | 11.07 | 8.57 | 14 |
| 15 | 511.98 | 9.03 | 11.94 | 9.08 | 11.90 | 9.13 | 11.86 | 9.18 | 15 |
| 16 | 12.78 | 9.63 | 12.74 | 9.68 | 12.69 | 9.74 | 12.65 | 9.80 | 16 |
| 17 | 713.58 | 10.23 | 13.53 | 10.29 | 13.49 | 10.35 | 13.44 | 10.41 | 17 |
| 18 | 14.38 | 10.83 | 14.33 | 10.90 | 14.2 | 10.96 | 14.23 | 11.02 | 18 |
| 19 | 15.17 | 11.43 | 15.12 | 11.50 | 15.07 | 11.57 | 15.02 | 11.63 | 19 |
| 20 | 15.97 | 12.04 | 15.92 | 12.11 | 15.87 | 12.18 | 15.81 | 12.24 | 20 |
| 21 | 16.77 | 12.64 | 16.72 | 12.71 | 16.6 | 12.78 | 16.60 | 12.86 | 21 |
| 22 | 17.57 | 13.24 | 17.51 | 13.32 | 17.4 | 13.39 | 17.40 | 13.47 | 22 |
| 23 | 18.37 | 13.84 | 18.31 | 13.92 | 18.2 | 14.00 | 18.19 | 14.08 | 23 |
| 24 | 19.17 | 14.44 | 19.10 | 14.53 | 19.0 | 14.61 | 18.98 | 4.69 | 24 |
| 25 | 19.97 | 15.05 | 19:30 | 15.13 | 19.83 | 15.22 | 19.77 | 5.37 | 25 |
| 26 | 20.76 | 15.65 | 20.70 | 15.74 | 20.65 | 15.83 | 20.56 | 15.92 | 26 |
| 27 | 21.56 | 16.25 | 21.49 | 16.34 | 21.42 | 16.44 | 21.35 | 16.53 | 27 |
| \% 28 | [22.36 | 16.85 | 22.29' | 16.95 | 212.21 | 17.05 | 22.1 | 7.14 | 28 |
| 29 | 23.16 | 17.45 | 23.08 | 17.55 | 23.01 | 17.65 | 22.93 | 7.75 | 29 |
| 30 | 23.96 | 18.05 | 23.88 | 18.16 | 23.80 | 18.26 | 23.72 | 18.37 | 30 |
| 31 | 24.76 | 18.66 | 24.68 | 8.76 | 24.59 | 8.87 | 24.51 | 18.98 | 31 |
| 32 | 25.56 | 19.26 | 25.47 | 19.37 | 25.39 | 19.48 | 25.30 | 19.59 | 32 |
| 33 | 26.35 | 19.86 | 26.27 | 19.97 | 26.18 | 20.09 | 26.09 | 20.20 | 33 |
| 34 | 27.15 | 20.46 | 27.06 | 20.58 | 26.97 | 20.70 | 26.88. | 20.82 | 34 |
| 35 | 27.95 | 21.06 | 27.86 | 21.19 | 27.77 | 21.31 | 27.672 | 21.43 | 35 |
| 36 | 28.75 | 21.67 | 28.66 | 21.79 | 28.56 | 21.92 | 28.46 | 22.04 | 36 |
| 37 | 29.55 | 22.27 | 29.45 | 22.40 | 29.35 | 22.52 | 29.262 | 22.65 | 37 |
| 38 | 30.35 | 22.87 | 30.25 | 23.00 | 30.15 | 23.13 | $30.05{ }^{\prime}$ | 23.26 | 38 |
| 39 | 31.15 | 23.47 | 31.04 | 23.61 | 30.94 | 23.74 | $30.84 ' 2$ | 23.88 | 39 |
| 40 | 31.95 | 24.07 | 31.84 | 24.21 | 31.73 | 24.35 | 31.63 | 24.49 | 40 |
| 41 | 32.74 | 24.67 | 32.64 | 24.82 | 32.53 | 24.96 | 32.422 | 25.10 | 41 |
| 42 | 33.54 | 25.28 | 33.43 | 25.42 | 33.32 | 25.57 | 33.212 | 25.71 | 42 |
| 43 | 34.342 | 25.88 | 34.23 | 26.08 | 34.11 | 26.18 | 34.002 | 26.33 | 43 |
| 44 | 35.14 | 26.48 | $35.02{ }^{2}$ | 26.63 | 34.91 | 26.79 | 34.79 | 26.94 | 44 |
| 45 | 35.942 | 27.08 | 35.82 | 27.24 | 35.70 | 27.39 | 35.58 2 | 27.55 | 45 |
| 46 | 36.74 | 27.68 | 36.62 | 27.84 | 36.49 | 28.00 | 36.372 | 28.16 | 46 |
| 47 | 37.54 | 28.29 | 37.41 | 28.45 | 37.29 | 28.61 | 37.162 | 28.77 | 47 |
| 48 | 38.33 | 28.89 | 38.21 | 29.05 | 38.08 | 29.22 | 37.95 2 | 29.39 | 48 |
| 49 | 39.13 | 29.49 | 39.00 | 29:66 | 38.87 | 29.83 | 38.743 | 30.00 | 49 |
| 50 | 39.98 | 30.09 | 39.80 | 30.26 | 39.67 | 30.44 | 39.53 | 30.61 | 50 |
|  | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. |  |
|  |  | g. | $52_{4}^{3}$ | Deg. | $52 \frac{1}{2}$ | eg. | 22 ${ }_{4}$ | eg. |  |



|  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\rightarrow$ | Lat. | Dep. | Lat. D | Dep | Lat. | Dep. | Lat. | Dep. | + |
|  | 0 | , |  |  |  |  | 0.78 | 0.63 |  |
| 2 | 1.58 | 1.23 | 1.57 | 1.24 | 1.57 | 1.24 | 1.56 | 1.25 | 2 |
| 3 | 2.36 | 1.85 | 2.36 | 1.86 | 2.35 | 1.87 | 2.34 | 1.88 | 3 |
| 4 | 3.15 | 2.46 | 3.14 | 2.48 | 3.13 | 2.49 | 3.12 | 2.50 |  |
| 5 | 3.94 | 3.08 | 3.93 | 3.10 | 3.91 | 3.11 | 3.90 | 3.13 | 5 |
| 6 | 4.73 | 3.69 | 4.71 | 3.71 | 4.70 | 3.74 | 4.68 | 3.76 |  |
| 7 | 5.52 | 4.31 | 5.50 | 4.33 | 5.48 | 4.36 | 5.46 | 4.38 |  |
| 8 | 6.30 | 4.93 | 6.28 | 4.95 | 6.26 | 4.98 | 6.24 | 5. | 8 |
| 9 | 7.09 | 5.54 | 7.07 | 5.57 | 7.04 | 5.60 | 7.02 | 5.63 | 9 |
| 10 | 7.88 | 6.16 | 7.85 | 6.19 | 7.83 | 6.23 | 7.80 | 6.26 | 10 |
| 11 |  | 6.7 |  | 6.81 |  | 5 |  |  | 1 |
| 12 | 9.46 | 7.39 | 9.42 | 7.43 | 9.39 | 7.47 | 9.36 |  | 12 |
| 13 | 10.24 | 8.00 | 10.21 | 8.05 | 10.17 | 8.09 | 10.14 | 8. | 13 |
| 14 | 11.0 | 8.62 | 10.99 | 8.67 | 10.96 | 8.72 | 10.92 | 8.76 | 14 |
| 15 | 11.82 | 9.23 | 11.78 | 9.29 | 11.74 | 9.34 | 11.70 | 9.39 | 15 |
| 16 | 12.61 | 9.85 | 12.57 | 9.91 | 12.52 | 9.96 | 12.48 | 10.01 | 16 |
| 17 | 13.4 | 10.47 | 13.35 | 10.52 | 13.30 | 10.58 | 13.26 | 10.64 | 17 |
| 18 | 14.18 | 11.08 | 14.14 | 11.14 | 14.09 | 11.21 | 14.04 | 11.27 | 18 |
| 19 | 14.97 | 11.70 | 14.92 | 11.76 | 14.87 | 11.83 | 14.8 | 11.89 | 19 |
| 20 | 15.76 | 12.31 | 15.71 | 12.38 | 15.65 | 12.45 | 15.60 | 12.52 | 20 |
| 21 | 16.55 | 12.93 | 16.49 | 13.00 | 16.43 | 13.07 | 16.38 | 13.1 | 21 |
| 22 | 17.3 | 13.54 | 17.28 | 13.62 | 17.22 | 13.7 | 17.16 | 13. | 22 |
| 23 | 18.12 | 14.16 | 18.06 | 14.24 | 18.00 | 14.32 | 17.94 |  | 23 |
| 24 | 18.9 | 14.78 | 18.85 | 14.86 | 18.78 | 14.94 | 18.72 |  | 24 |
| 25 | 19.70 | 15.39 | 19.63 | 15.48 | 19.57 | 15.56 | 19. | 1 | 25 |
| 26 | 20.49 | 16.01 | 20.42 | 16.10 | 20.35 | 16.19 | 26. | 16 | 26 |
| 27 | 21.28 | 16.62 | 21.20 | 16.72 | 21.15 | 16.81 | 21. |  | 27 |
| 28 | 22.06 | 17.24 | 21.99 | 17.33 | 21.91 | 17.43 | 21.84 |  | 28 |
| 29 | 22.85 | 17.85 | 22.77 | 17.95 | 22.7 C | 18.05 | 22.62 |  |  |
| 30 | 23.64 | 18.47 | 23.56 | 18.57 | 23.48 | 18.68 | 23.40 | 18.7 | 0 |
| 31 |  |  |  | 19.19 | 24.2 t | 19.30 | 24.18 |  | I |
| 3 | 25.2 | 19.70 | 25.13 | 19.81 | 25.64 | 19.92 | 94 |  | 32 |
| 33 | 26.0 | 20.32 | 25.92 | 20.43 | 25.83 | 20.54 |  |  | 33 |
| 34 | 26.79 | 20.93 | 26.70 | 21.05 | 26.6 | 21.17 | 26. |  | 34 |
| 35 | 27.58 | 21.55 | 27.49 | 21.67 | 27.35 | 21.79 |  |  |  |
| 36 | 28.37 | 22.16 | 28.27 | 22.29 | 28.17 | 22.41 | 28. | 22.53 | 36 |
| 37 | 29.16 | 22.78 | 29.06 | 22.91 | 28.96 | 23.03 | 28. | 23. | 37 |
| 38 | 29.94 | 23.40 | 29.84 | 23.53 | 29.74 | 23.66 |  | 23.7 | 38 |
| 39 | 30.73 | 24.01 | 30.63 | 24.14 | 30.52 | 24.28 |  |  | 39 |
| 40 | 31.52 | 24.63 | 31.41 | 24.76 | 31.30 | 24.90 | 31.20 |  | 40 |
|  | 32.3] | 25.24 | 32.20 | 25.38 | 32.01 | 25.52 | 31.98 |  | 1 |
| 42 | 33.10 | 25.86 | 32.98 | 26.00 | 32.87 | 26.15 | 32.76 | 26.29 | 42 |
| 43 | 33.88 | 26.47 | 33.77 | 26.62 | 33.6 | 26.77 | 33.53 | . 31 | 43 |
| 4 | 34.67 | 27.09 | 34.55 | 27.24 | 34.45 | 27.39 | 34.31 | . | 44 |
| 45 | 35.46 | 27.70 | 35.34 | 27.86 | 35.22 | 28.01 | 35.09 | 8.17 | 45 |
| 46 | 36.25 | 28.32 | 36.12 | 28.48 | 36.06 | 28.64 | 35.8 | 28.79 | 46 |
| 4 | 37.04 | 28.94 | 36.91 | 29.10 | 36.78 | 29.26 | 36.65 | 29.42 | 47 |
| 48 | 37.82 | 29.55 | 37.70 | 29.72 | 37.57 | 29.88 | 37.43 | 30.04 | 48 |
| 49 | 38.61 | 30.17 | 38.48 | 30.34 | 38.35 | 30.50 | 38.21 | 30.67 | 49 |
| 50 | 39.4 | 30.78 | 39.27 | 30.95 | 39.13 | 31.13 | 38.99 | 31.30 | 50 |
|  | Dep | Lat. | Dep | Lat. | d | Lat. | Dep. | Lat. |  |
| 52 Deg. $51 \frac{3}{4} \mathrm{Deg} .51 \frac{1}{2} \mathrm{Deg} .51 \frac{1}{4} \mathrm{Deg}$. |  |  |  |  |  |  |  |  |  |

TRAVERSE TABLE.


## 116

TRAVERSE TABLE.


| $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. | Lat. | ep. | Lat. | Dep. | Lat. | Dep. |  |
| 51 |  | 32.10 | 39.49 | 32.27 | 39.35 | 32.44 | 39.21 |  |  |
|  | 40.41 | 32.72 | 40.27 | 32.90 | 40.12 | 33.08 | 39.98 |  |  |
|  | 41.19 | 33.35 | 41.0 | 33.53 | 40.90 | 33.71 | 40.7 | 33.88 |  |
|  | 41.97 | 33.98 | 41.82 | 34.17 | 41.67 | 34.35 | 41.5 | 34.53 |  |
|  | 42.74 | 34.61 | 42.59 | 34.80 | 42.44 | 4.98 | 42.29 | 35.17 | 55 |
|  | 43.523 | 35.24 | 43.37 | 35.43 | 43.21 | 35.62 | 43.06 | 35.81 |  |
| 57 | 44.30 | 35.87 | 44.1 | 36.06 | 43.98 | 36.2 | 43.8 | 36.45 | 57 |
| E8 | 45.07 | 36.50 | 44.91 | 36.70 | 44.75 | 36.89 | 44.59 | 37.09 | 58 |
| 59 | 45.85 | 37.13 | 45.68 | 37.33 | 45.53 | . 53 | 45.3 | 37.73 | 59 |
| 60 | 46.63 | 37.76 | 46.46 | 37.96 | 46.30 | 38.16 | 46.13 |  | 0 |
| 61 |  | 38 | 47. | 38.60 | 47 | 0 | 46.9 |  |  |
| 62 | 48.18 | 39.02 | 48.0 | 39.23 | 47.8 | 4 | 47,6 |  | 62 |
| 63 | 48.96 | 39.65 | 48.7 | 39.86 | 48.61 | 40.07 | 48.44 |  | 3 |
| 64 | 9.74 | 40.28 | 49.56 | 40.49 | 49.38 | 40.71 | 49.2 | 22 | 64 |
| 65 | 50.51 | 40.91 | 50.3 | 1.13 | 50.16 | 41.35 | 49.9 |  | 65 |
| 66 | 51.29 | 41.64 | 51.1 | 41.76 | 50.93 | 41.98 | 50.7 | 2.20 | 66 |
|  | 52.07 | 42.16 | 51.88 | 42.39 | 51.70 | 42.62 | 51.5 |  | 7 |
| 68 | 52.85 | 42.79 | 52.6 | 43.02 | 52.47 | 43.25 | 52.2 | 3.48 | 68 |
| 69 | 53.52 | 43.42 | 53.4 | 43.66 | 53.24 | 43.89 | 53.0 |  | 69 |
| 70 | 54. | 44.05 | 54.21 | 44.29 | 54.01 | 44.53 | 53.8 |  | 70 |
|  |  | 44.68 | 54 | 44.92 |  | 5.16 |  |  | 71 |
| 72 | 55.95' | 45.31 | 55.7 | 45.55 | 55.5 |  | 55.3 |  | 72 |
| 73 | 6.78 | 45.94 | 56.53 | 46.19 | 56.33 | 46.43 | 56.1 |  | - 73 |
|  | 57.51 | 46.57 | 57.31 | 46.82 | 57.1 | 47.07 | 56. | . 32 | 74 |
| 74 75 76 | 58.29 | 47.20 | 58.08 | 47.45 | 57.8 | 47.71 | 57. |  | 75 |
|  | 59.06 | 47.83 | 58.85 | 48.09 | 58.64 | 48.3 | 58.4 |  | 76 |
|  | 59.84 | 48.46 | 59.6 | 48.72 | 59.42 | 48.98 | 59.2 | . 2 | 7 |
|  | 60.62 | 49.09 | 60.40 | 49.35 | 60.19 | 49.61 | 59.9 | 49.88 | 78 |
|  | 61.39, | 49.72 | 61.18 | 49.98 | 60.96 | 50.25 | 60.7 | 50.52 | 79 |
| 80 | 62.1 | . 35 | 61.9 | 0. | 61.73 | 50.89 | 61.51 |  | 80 |
|  | 62. |  |  | 1.2 | 62. | 51.52 |  |  | 81 |
|  | 63.73 | 51.60 | 63.50 | 51.88 | 63.27 | 52.16 | 63.0 | 52.43 | 89 |
|  | , | 5.23 | 64.2 | 2.51 | 64.04 | 52.79 | 63.8 | 3.07 | 83 |
|  | 65.28 | 52.86 | 65 | 53.15 | 64.82 | 53.43 | 64.5 | 3.71 | 84 |
|  | 66.06 | 53.49 | 65.8 | 53.78 | 65.5 | 54.07 | 65. |  | 85 |
|  | 66.83 | 54.12 | 66.6 | 54.41 | 66.36 | 54.70 | 66.1 | 54.99 | 86 |
|  | 7.61 | 54.75 | 67.3 | 55.05 | 67.13 | 55.34 | 66.8 | 55.6 | 87 |
|  | 68.39 | 55.38 | 68.15 | 55.68 | 67.90 | 55.97 | 67.6 |  | 88 |
|  | 69.17 | 56.01 | 68.92 | 56.32 | 68.67 | 56.61 | 68.4 | .91 | 89 |
| 90 | 69.9 | 56.6 | 69.7 | 6.94 |  | 57.25 | 69.2 |  | 90 |
|  |  |  |  | 7.58 | 70.2 |  |  |  | , |
|  | 71.5 | 57.90 | 71.2 | 53.21 | 70.99 | 58.52 | 70.7 | . | 92 |
|  | 72.27 | 58.53 | 72.02 | 58.84 | 71.76 | 59.16 | 71.50 | 59.47 | 93 |
|  | 730 | 59.16 | 72.79 | 59.47 | 72.53 | 59.79 | 72.27 | 60.1 | 94 |
|  | 73.83 | 59.79 | 73.5 | 60.11 | 73:30 | 60.43 | 73.0 | 60.7 | 0 |
|  | 74.616 | 60.41 | 74.3 | 60.74 | 74.08 | 61.06 | 73.8 | 1.39 | 96 |
|  | 75.38 | 61.04 | 75.12 | 61.37 | 74.85 | 61.70 | 74.5 | 62.03 | 9 |
| 9899100 | 76.16 | 61.67 | 75.8 | 62.01 | 75.62 | 62.34 | 75.3 | 62.6 | 98 |
|  | 76.94 | 62.30 | 76.66 | 62.64 | 76.39 | 62.97 | 76.1 | 63.30 | 99 |
|  | 77.71 | 2.93 | 77.4 | 3.27 | 77.16 | 63.61 | 76.8 |  |  |
| 劳 | Dep. Lat. |  | Dep. Lat. |  | Dep. Lat. |  | Dep. Lat. |  |  |
|  | 51 Deg. $50{ }_{4}^{3} \mathrm{Deg}$. |  |  |  |  |  |  |  |  |

TRAVERSE TABLE.

|  |  |  |  | eg |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. |  | Dep. |  | Dep. | Lat. |  |  |
|  | 0.77 | 0.64 | 0.76 | 0.65 | 0.76 | 0.65 | 0.76 |  |  |
|  | 1.53 | 1.29 | 1.53 | 1.29 | 1.52 | 1.30 | 1.52 | 1.31 |  |
|  | ${ }^{2.06}$ | ${ }_{2.57}^{1.93}$ | 3.05 | ${ }_{2.58}$ | 3.04 | 1.60 | 2.03 | ${ }_{2.61}^{1.96}$ |  |
|  | 3.83 | 3.21 | 3.82 | 3.23 | 3.8 | 3.25 | 3.7 | 3.2 |  |
|  | 4.60 | 3.86 | 4.58 |  | 4.56 | 3.90 | 4.55 | 3.9 |  |
|  | 5.86 6.13 | 4.50 <br> 5.14 | 5.34 | 4.52 5.17 | 5.32 | 4.55 5.20 | 5.30 | 4.2 |  |
|  | 6.89 | 5.79 | 6.87 | 5.82 | 6.84 | 5.84 | 6.82 | 5.8 |  |
| 1 | 7.66 | 6.43 | 7.68 | 6.46 | 7.60 | 6.49 | 7.58 | 6.5 | 10 |
|  | 8.43 | 7.07 | 8.40 | 7.11 | 8.36 | 712 |  |  |  |
|  | 9.19 | 7.71 | 9.16 | 7.75 | 9.12 | 7.79 | 9 |  |  |
|  | 9.96 | 8.36 | 9.92 | 8.40 | 9.89 | 8.44 |  | 8.4 |  |
|  | 10.72 | 9.00 | 0.69 | ${ }_{9}^{9.05}$ | 10.6 | 9.09 | 10.6 | 9. |  |
|  | 11.4 | 9.64 | 12.21 | 10.34 | 11.41 | - $\begin{gathered}9.74 \\ 10.39\end{gathered}$ | 12.12 | ${ }^{9} 10.44$ | 5 |
|  | 13.02 | , | 1297 | 10.98 | 12.93 | 11.04 | 12. |  |  |
|  | 13.79 | 11.57 | 13.74 | 11.63 | 13.69 | 11.69 | 13.64 |  |  |
|  | 14.55 | 12.21 | 14.5 | 12.28 | 14.45 | 12.34 | 14.3 | 12. |  |
|  | 15.32 | 12.86 | 15.26 | 2.92 | 15.21 | 12.99 | 15.15 |  |  |
|  | 16.09 | 13.50 | 16.03 | 3.57 | 15.97 | 13.64 | 15.91 |  |  |
|  | 16. | 4.14 | 16.79 | 4.21 | 16.78 | 14.2 | 16. |  |  |
|  | 17.6 | 4.78 | 17.55 | 14.8 | 17.49 | 14.9 | 17. | 15.01 |  |
|  | 18.39 | 15.43 | 18.32 | 15.51 | 18.25 | 15.59 | 18.18 | 15.67 | 25 |
|  | 19.15 | 16.07 | 19.08 | 16.15 | 19.01 | 16.24 | 18. |  | 25 |
|  | 19.92 | 16.71 | 19.84 | 16.80 | 19.77 | ${ }^{16.89}$ | 19.78 | 17 | 26 |
|  | 21.45 | 8.00 | 21.57 | 18.09 | 21.29 | 18.18 | 21.21 |  | 88 |
|  | 22.22 | 18.64 | 22.13 | 18.74 | 22.05 | 18.8 | 21.97 | 18. |  |
|  | 22.98 | 19.28 | 22.90 | 9,38 | 22.81 | 19.48 | 22.73 | 19.58 |  |
|  |  | 19.93 |  | 0.0s | 23.5 | 2.13 |  |  | 31 |
|  |  |  |  |  | 4.3 |  |  |  |  |
|  | 25.28 | 21.21 | 25.19 | 21.32 | 25.09 | 21.43 | 25.00 | 21.5 |  |
|  | 26.05 | 21.85 | 25.95 | 21.97 | 25.85 | 22.08 | 25.76 | 2. |  |
|  | 26.81 | 2 | 26.7 | 2.61 | 26.61 | 22.73 | 26.51 | 122.85 |  |
|  | 27.5 | 23.14 | 27.48 | 23.26 | '27.37 | 23.38 | 27.27 | 23.50 |  |
|  | 728.3 | 23.78 | 28.24 | 23.91 | 28.13 | 24.03 | 28.03 | 24. |  |
|  | 29.11 | 24. | 29.00 | 24.55 | 28.90 | 24.68 | 28.79 | 94.80 |  |
|  | 29.88 | 25.07 | 29.77 | 25.20 | 29.66 | 25.33 | 29 |  |  |
|  | 30.64 |  | 30.53 | 25.84 | 30 | 25 | 30 |  |  |
|  | 1.4 |  |  | 26.4 | 31.1 | 26. |  |  | 4 |
|  | 32.17 | 27.00 | 32.0 | 27.1 | 31.94 | 27. | 31.8 |  |  |
|  | 32.94 | 27.64 | 32.82 | 27.78 | 32.76 | 27.93 | 32.58 | 28.07 | 4, |
|  | 33.71 | 28.28 | 33.58 | 28.43 | 33.46 | 28.5 | 33.33 | 8. |  |
|  | 34.47, | 28.93 | 34.3 | 9.08 | 34.22 | 29.23 | 34.09 |  |  |
|  | 635.2 | 29.57 | 35.11 | 29.72 | 34.98 | 29.87 | 34.8 |  |  |
|  | 36.00 | 30.21 |  | 30.37 | 35.74 |  | 35.6 |  |  |
|  | 36.77 |  | 36 | 1.0 | S6.50 | 31.17 |  |  |  |
|  | 937.54 | 31.50 | 37. |  | 37.22 | 31.82 | 37.12 | 83 |  |
|  | 038.30 |  |  | 32.31 | 38. | 32.47 |  | 32.64 |  |
| $\mid \stackrel{\rightharpoonup}{2 x}$ | Dep | at. | Dep | Lat. |  | Lat. |  |  |  |
|  | 50 | De |  | cg |  | Deg. | $4912$ |  |  |



TRAVERSE TABLE.


TRAVERSE TABLE.


| $\stackrel{2}{+}$ |  | Deg. $42 \frac{1}{4} \mathrm{Deg}$. |  |  | $42 \frac{1}{3}$ Deg. $\\|^{423}$ Deg. |  |  |  | $\underset{\sim}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | ep. |  |
| 1 | 0.7 | 0.67 | 0.74 | 0.67 | 0.74 | 0.68 | 0.73 |  |  |
| 2 | 1.49 | 1.34 | 1.48 | 1.34 | 1.47 | 1.35 | 1.47 | 1.36 | 2 |
| 3 | 2.23 | 2.01 | 2.22 | 2.02 | 2.21 | 2.03 | 2.20 | 2.04 | 3 |
| 4 | 2.97 | 2.68 | 2.96 | 2.69 | 2.95 | 2.70 | 2.94 | 2.72 | 4 |
| 5 | 3.72 | 3.35 | 3.70 | 3.36 | 3.69 | 3.38 | 3.67 | 3.39 | , |
| 6 | 4.46 | 4.01 | 4.44 | 4.03 | 4.42 | 4.05 | 4.41 | 4.07 | , |
| 7 | 5.20 | 4.68 | 5.18 | 4.71 | 5.16 | 4.73 | 5.14 | 4.75 | 析 |
| 8 | 5.95 | 5.35 | 5.92 | 5.38 | 5.90 | 5.40 | 5.87 | 5.43 | , |
| 9 | 6.69 | 6.02 | 6.66 | 6.05 | 6.64 | 6.08 | 6.61 | 6.11 |  |
| 10 | 7.43 | 6.69 | 7.40 | 6.72 | 7.37 | 6.76 | 7.34 | 6.79 | 10 |
| 11 | 8.17 | 36 |  |  |  |  | 8.08 |  |  |
| 12 | 8.92 | 8.03 | 8.88 | 8.67 | 8.85 | 8.11 | 8.81 | 8.15 | 12 |
| 13 | 9.66 | 8.70 | 9.62 | 8.74 | 9.58 | 8.78 | 9.55 | 8.82 | 13 |
|  | 0.10 | 9.37 | 10.36 | 9.41 | 10.32 | 9.46 | 10.28 | 9.50 | 14 |
|  | 15 | 10.04 | 11.10 | 10.09 | 11.06 | 10.13 | 11.01 | 10.18 | 15 |
| 16 | 1.89 | 10.71 | 11.81 | 10.76 | 11.8 | 10.81 | 11.75 | . 86 | 16 |
| 17 | 2.63 | 11.38 | 12.58 | 11.43 | 12.5 | 11.48 | 12.48 | 11.54 | 17 |
|  | 3.38 | 12.04 | 13.32 | 12.10 | 13.2 | 12.16 | 13.2 | 12.22 | 18 |
| 19 | 4.12 | 12.71 | 14.06 | 12.77 | 14.0 | 12.84 | 13.9 | 90 | 19 |
| 20 | 4.86 | 13.38 | 14.80 | 13.45 | 14.75 | 13.51 | 14.69 | 88 | 20 |
| 2 |  |  |  |  | 15.4 |  |  |  | 21 |
| 22 | 6.35 | 14.72 | 16.28 | 14.79 | 16. | 4.86 | 16. | 3 | 22 |
| 23 | 7.0 | 15.39 | 17.02 | 15.46 | 16.9 | 15.54 | 16.8 | . 61 | 23 |
|  | 7.8 | 16.06 | 17.77 | 16.14 | 17. | 16.21 | 17.6 | 6.29 | 24 |
|  | 8.58 | 16.73 | 18.51 | 16.81 | 18.4 | 16.89 | 18.3 | 6.97 | 25 |
| 26 | 9.32 | 17.40 | 19.25 | 17.48 | 19.1 | 17.57 | 19.0 | 7.65 | 26 |
|  | 0.06 | 18.07 | 19.99 | 18.15 | 19.9 | 18.24 | 19.8 | 8.33 | 27 |
|  | 20.81 | 18.74 | 20.73 | 18.83 | 20.6 | 18.92 | 20.5 | 9.01 | 8 |
| 29 | 21.55 | 19.40 | 21.47 | 19.50 | 21.38 | 19.59 | 21.3 | 9.69 | 29 |
| 30 | 22.29 | 20.07 | 22.21 | 20.17 | 29.12 | 20.27 | 22.0 | 0.36 | 30 |
|  |  | 74 |  |  | 22.8 |  | 22. |  | 31 |
|  | 3.78 | 21.41 | 23.69 | 21.52 | 23.5 | 21.62 | 23.5 | 1.72 | 32 |
|  | 4.52 | 22.08 | 24.43 | 22.19 | 24.3 | 22.29 | 24.2 | 2.40 | 33 |
|  | 25.27 | 22.75 | 25.17 | 22.86 | 25.0 | 22.97 | 24.9 | 3.08 | 34 |
|  | 23.01 | 23.42 | 25.91 | 23.53 | 25.80 | 23.65 | 25.7 | 3.76 | 35 |
|  | 26.75 | 24.09 | 26.65 | 24.21 | 26.54 | 24.32 | 26.4 | 24.44 | 36 |
|  |  | の | 27.39 | 24.88 | 27. | 25.00 | 27.1 | . 12 | 37 |
|  | 28.24 | 25.43 | 28.13 | 25.55 | 28.02 | 25.67 | 27.90 | 25.79 | 38 |
|  | 28.98 | 26.10 | 28.87 | 26.22 | 28.75 | 26.35 | 28.6 | 26.47 | 39 |
| 40 | 29.73 | 26.77 | 29.61 | 26.89 | 29.4 | 27.02 | 2937 | 7.15 | 40 |
|  | 30.4 | . | 30.35 | 27.57 | 30.2 | 27.70 | 30.1 | . 83 | 41 |
|  | 31.21 | 28.10 | 31.09 | 28.24 | 34.9 | 28.37 | 30.84 | 8.51 | 42 |
|  | 31.96 | 28.77 | 31.83 | 28.91 | 31.7 | 29.05 | 31.58 | 29.19 | 43 |
|  | 32.70 | 29.44 | 32.57 | 29.58 | 32.44 | 29.73 | 32.31 | 29.87 | 44 |
|  | 33.44 | 30.11 | 33.31 | 30.26 | 33.18 | 30.40 | 33.04 | 30.55 | 45 |
|  | 34. 18 | 30.78 | 34.05 | 30.93 | 33.9 | 31.08 | 33.78 | 1.22 | 46 |
|  | 34.93 | 31.45 | 34.79 | 31.60 | 34.65 | 31.75 | 34.51 | 1.90 | 47 |
|  | 35.67 | 32.12 | 35.53 | 32.27 | 35.39 | 32.43 | 35.25 | 2.58 | 48 |
| 49 | 36.41 | 32.79 | 36.27 | 32.98 | 36.1 | 33.10 | 35.98 | 33.26 | 49 |
| 50 | 37.16 | 33.46 | 37.01 | 33.62 | 36.8 | 33.78 | 36.72 | 3.94 | 50 |
|  | Dep | Lat. | Dep. | at. | Dep. | Lat. | Dep. |  |  |
|  | 48 Deg. $473 \mathrm{Deg} .47!$ Deg. ${ }^{1} 47 \frac{1}{4} \mathrm{Deg}$, ? |  |  |  |  |  |  |  |  |


|  | Lat. |  | Lat. | Dep. |  | Dep. | Lat. | Dep. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 37.75 | 31 | 37.60 | 34.46 | 37.4 |  | 5 |
|  | 38.64 | 34.79 | 38.49 | 34.96 | 38.34 | 35.13 | 38.18 | 35.30 | 52 |
|  | 39.39 | 35.46 | 39.23 | 35.64 | 39.08 | 35.81 | 38.92 | 35.98 | 53 |
|  | 40.13 | 35.13 | 39.97 | 36.31 | 39.81 | 36.48, | 39.65 | 36.66 | 4 |
|  | 40.87 | 36.80 | 40.71 | 36.98 | 40.55 | 37.16 | 40.39 | 37.33 | 5 |
|  | 41.62 | 37.47 | 41.45 | 37.65 | 41.29 | 37.83 | 41.12 | 38.01 | 56 |
|  | , | 38.14 | 42.19 | 38.32 | 42.02 | 38.51 | 41.86 | 38.69 | 57 |
|  | 43.1 | 38.81 | 93 | 39.00 | 42.76 | 39.18 | 42.59 | 9.37 | 9 |
|  | 43.8 | 39.48 | 43.6 | 39.67 | 43.50 | 39.86 | 43.32 | 0.05 | - |
| 60 | 44.59 | 40.15 | 44.41 | 40.34 | 44.24 | 40.54 | 44.06 |  | 60 |
|  |  | 40 | 45 | 1 | 44.97 |  |  |  | 61 |
|  | 46.0 | 41.49 | 45.89 | 41.69 | 45.71 | 41.89 | 45.53 | 09 | 62 |
|  | 46.8 | 42.16 | 46.63 | 42.36 | 46.45 | 42.56 | 46.26 | 42.76 |  |
|  | 47.56 | 42.82 | 47.37 | 43.03 | 47.19 | 43.24 | 47.0 | 3.44 | 64 |
|  | 48.30 | 43.49 | 48.11 | 43.70 | 47.92 | 43.91 | 47.73 | 44.12 | 65 |
|  | 49.05 | 44.16 | 48.85 | 44.38 | 48.66 | 44.59 | 48.47 | 44.80 | 6 |
|  | 49.79 | 44.83 | 49.59 | 45.05 | 49.40 | 45.26 | 49.20 | 4 | 67 |
|  | 50.53 | 45.50 | 50.33 | 45.72 | 50.13 | 45.94 | 49.93 | S | 68 |
|  | 51.28 | 46.17 | 51.07 | 46.39 | 50.87 | 46.62 | 50.67 | 46.84 | 69 |
| 70 | 52.02 | 46.84 | 51.82 | 47.07 | 51.61 | 47.29 | 51.40 | 47.52 | 0 |
|  | 52.76 |  |  |  | 52.35 |  |  |  | 7 |
|  | 53.51 | 48.18 | 53.30 | 48.41 | 53.08 | 48.64 | 52.87 | 48.87 | 72 |
|  | 54.25 | 48.85 | 54.04 | 49.08 | 53.82 | 49.32 | 53.61 | 49.55 | 73 |
|  | 54.99 | 49.52 | 54.78 | 49.76 | 54.56 | 49.99 | 54.34 | 50.23 | 4 |
|  | 55.7 | 50.18 | 55.52 | 50.43 | 55.30 | 50.67 | 55.0 | 0.91 | 5 |
|  | 56.48 | 50.85 | 56.26 | 51. 10 | 56.03 | 51.34 | 55.81 | 51.59 | 76 |
|  | 57.22 | 51.52 | 57.00 | 51.77 | 56.77 |  | 56.54 | 52.27 | 77 |
|  | 57.97 | 52.19 | 57.74 | 52.44 | 57.51 | 52.70 | 57.28 |  | 78 |
|  | 58.71 | 52.86 | 58.48 | 53.12 | 58.24 | 53.37 | 58.01 | 53 | 9 |
| 80 | 59.45 | 33.53 | 59.22 | 53.79 | 58.98 | 54.0 | 58.75 |  | 80 |
|  |  |  |  | 54.46 | 59.72 |  |  |  | 1 |
|  | 60.9 | 54.87 | 60.70 | 55.13 | 60.46 | 55.40 | 60.21 | 55.66 | 82 |
|  | 61.68 | 55.54 | 61.44 | 55.81 | 61.19 | 56.07 | 60.95 | 56.34 | 83 |
|  | 62.42 | 56.21 | 62.18 | 56.48 | 61.93 | 56.75 | 61.68 | 57.02 | 仡 |
|  | 63.17 | 56.88 | 62.92 | 57.15 | 62.67 | 57.43 | 62.42 | 57.70 | 85 |
|  | 63.91 | 57.55 | 63.66 | 57.82 | 63.41 | 58.10 | 63.15 | 58.38 | 86 |
|  | 64.65 | 58.21 | 64.40 | 58.50 | 64.14 | 58.78 | 63.89 | 59.06 | 87 |
|  | 65 | 58.88 | 65.14 | 59.17 | 64.88 | 59.45 | 64.62 | 59.73 | 8 |
|  |  | 59.55 |  | 59.84 | 65.62 | 60.13 | 65.35 | , | 39 |
| 90 |  | 60.22 | 66.62 | 60.51 | 66.35 | 60.80 | 66.09 |  |  |
|  |  |  |  | 61.19 |  |  |  |  | 91 |
|  | 68.3 | 61.56 | 68.10 | 61.86 | 67.8 | 62.15 | 67.56 | 62.45 | 92 |
|  | 69.1 | 62.23 | 68.84 | 62.53 | 68.57 | 62.83 | 68.29 | 63.13 | 98 |
|  | 69.86 | 62.90 | 69.58 | 63.20 | 69.30 | 63.51 | 69.03 | 63.81 | 9 |
|  | (0) | 63.57 | 70.32 | 63.87 | 70.04 | 64.18 | 69.76 | 4.49 | 95 |
|  | 1.3 | 64.24 | 71.06 | 64.55 | 70.78 | 64.86 | 70.49 | 65.16 | 96 |
|  | 72.0 | 64.91 | 71.80 | 65.22 | 71.52 | 65.53 | 71.23 | 65.84 | 97 |
|  | 72. | 65.57 | 72.54 | 65.89 | 72.25 | 66.21 | 71.96 | 66.52 | 98 |
|  | 1.5 | 66.24 | 73.28 | 66.56 | 72.99 | 66.88 | 72.70 | 67.20 | 99 |
| 100 |  | 101 | 74.02 | 67.2 | 73.73 | 67.56 | 73.43 | 67.88 | 100 |
|  | Vep. | Lat. | Dep | Lat. | Dep. | Lat. | Dep. | Lat. | $\stackrel{\circ}{\circ}$ |
|  | 48 |  |  |  |  |  |  |  |  |


|  | $\frac{43 \text { Lat. }}{\frac{1}{2}}$ | $\overline{\mathrm{De}}$ |  |  |  | Dep. | Lat. | D | 2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.73 | 0.68 | 0.73 | 0.69 | 0.73 | 0.69 | 0.72 | 0.69 |  |
| 2 | 1.46 | 1.36 | 1.46 | 1.37 | 1.45 | 1.38 | 1.44 | 0.69 | 2 |
| 3 | 2.19 | 2.05 | 2.19 | 2.06 | 2.18 | 2.07 | 2.17 | 2.07 | 3 |
| 4 | 2.93 | 2.73 | 2.91 | 2.74 | 2.90 | 2.75 | 2.89 | 2.77 |  |
| 5 | 3.66 | 3.41 | 3.64 | 3.43 | 3.63 | 3.44 | 3.61 | 3.46 | 5 |
| 6 | 4.39 | 4.09 | 4.37 | 4.11 | 4.35 | 4.13 | 4.33 | 4.15 | 6 |
| 7 | 5.12 | 4.77 | 5.10 | 4.80 | 5.08 | 4.82 | 5.06 | 4.84 | 7 |
| 8 | 5.85 | 5.46 | 5.83 | 5.48 | 5.80 | 5.51 | 5.78 | 5.53 | 8 |
| 10 | 6.58 7.31 | 6.14 6.82 | 6.56 7.28 | $6.17$ | $\begin{aligned} & 6.53 \\ & 7.25 \end{aligned}$ | 6.20 6.88 | 6.50 7.22 | 6.22 | 9 |
|  |  |  |  |  |  |  |  |  |  |
| 11 | 8.04 | 7.50 | 01 | 7.54 | 7.98 | 7.57 | , |  | 1 |
| 12 | 8.78 | 8.18 | 8.74 | 8.22 | 8.70 | 8.26 | 8.67 | 8.30 | 12 |
| 13 | 8.51 | 8.87 | 9.47 | 8.91 | 9.43 | 8.95 | 9.39 | 8.99 | 3 |
|  | 10.24 | 9.55 | 10.20 | 9.59 | 10.16 | 9.64 | 10.11 | 9.68 | 4 |
|  | 10.971 | 10.23 | 10.93 | 10.28 | 10.88 | 10.33 | 10.84 | 10.37 | 5 |
|  | 11.70 | 10.91 | 11.65 | 10.96 | 11.61 | 11.01 | 11.56 | 11.06 | 16 |
|  | 12.431 | 11.59 | 12.38 | 11.65 | 12.33 | 11.70 | 12.28 | 11.76 | 17 |
|  | 13.16 | 12.28 | 13.11 | 12.33 | 13.06 | 12.39 | 13.0 | 12.45 | 18 |
|  | 13.90 | 12.96 | 13.84 | 13.02 | 13.78 | 13.08 | 13.7 | 13.14 | 19 |
| 20 | 14.63 | 13.64 | 14.57 | 13.70 | 14.5 | 3.77 |  |  | 0 |
| 21 |  | 14.32 | 15.3 | 4.39 |  |  |  |  | 1 |
|  | 16.091 | 15.00 | 16.021 | 15.07 | 15.96 | 15.14 |  | 5.21 | 22 |
| 23 | 16.82 | 15.69 | 16.75 | 15.76 | 16.68 | 15.83 | 16.61 | 15.90 | 23 |
|  | 17.55 | 16.37 | 17.48 | 16.44 | 17.41 | 16.52 | 17.3 | 416.60 | 4 |
|  | 18.28 | 17.05 | 18.21 | 17.13 | 18.13 | 17.21 | 18.06 | 17.29 | 25 |
|  | 19.02 | 17.73 | 18.94 | 17.81 | 18.86 | 17.90 | 18.78 | 17.98 | 26 |
|  | 19.75 | 18.41 | 19.67 | 18.50 | 19.69 | 18.59 | 19.50 | 18.67 | 7 |
|  | 2.48 | 19.10 | 20.39 | 19.19 | 20.31 | 19.27 | 20.2 | 19.36 | 28 |
|  | 21.21 | 19.78 | 21.12 | 19.87 | 21.04 | 19.96 | 20.9 | 20.05 | 29 |
| 30 | 21.94 | 20.46 | 21.8 | 2.56 | 21. | 0.65 |  |  | 30 |
|  |  |  |  |  |  | . 3 |  |  | 31 |
|  | 23.40 | 21.82 | 23.3 | . 93 | 23.2 | 2.03 |  | 22. | 32 |
|  | 4.13 | 22.51 | 24.0 | 22.61 | 23.9 | 22.72 | 23.8 | 22.82 | 33 |
|  | 24.87 | 23.19 | 24.76 | 23.30 | 24.66 | 23.40 | 24.56 | 23.51 | 34 |
|  | 25.60 | 23.87 | 25.49 | 23.98 | , | 24.09 | 2.2 | 24.20 | 35 |
|  | 26.33 | 24.55 | 26.22 | 24.67 | 26.1 | 24.78 | . 0 | 24.89 | 6 |
|  | 27.06 | 25.23 | 26.95 | 25.35 | 26.84 | 25.47 | 26.73 | 25.59 | 37 |
|  | 27.79 | 25.92 | 27.68 | 26.04 | 27.56 | 26.16 | 27.45 | 26.28 |  |
|  | 28.52 | 26.60 | 28.41 | 26.72 | 28.2 | 2.85 | 28.17 | 26.97 | 39 |
| 40 | 29.25 | 27.28 | 29.13 | 27.41 | 29.01 | 27.53 | 28.89 |  | 0 |
|  | 29.99 | 27.96 | 29.8 | 28.09 | 29.7 | 28.22 |  |  | 41 |
|  | 30.72 | 28.64 | 30.59 | 28.78 | 30.47 | 28.91 | 30.3 | 29.04 | 析 |
|  | 31.45 | 29.33 | 31.32 | 29.46 | 31.19 | 29.60 | 31.06 | 29.74 | 43 |
|  | 32.1813 | 30.01 | 32.05 | 30.15 | 31.92 | 30.29 | 31.78 | 30.43 | 44 |
|  | 32.913 | 30.69 | 32.78 | 30.83 | 32.64 | 30.98 | 32.51 | 31.12 | 45 |
|  | 33.643 | 31.37 | 33.51 | 31.52 | 33.37 | 31.66 | 33.23 | 31.81 | 46 |
|  | 34.37 | 32.05 | 34.23 | 32.20 | [34.09 | 32.35 | 33.95 | 32.50 | 47 |
|  | 35.10 | 32.74 | 34.96 | 32.89 | 34.82 | 33.04 | 34.67 | 38.19 | 48 |
|  | 35.84 | 33.42 | 35.6 | 33.57 | 35.54 | 33.73 | 35.40 | 33.88 | 49 |
| 50 | 36 | 10 | 36 | . 26 | 36.27 | 34.42 | 36.12 | 8 | 50 |
|  | Dep | Lat. | Dep. | Lat. | Dep. | Lat. | Dep | Lat. |  |
|  |  |  |  |  |  |  |  |  |  |




IV. A Table of Natural. Sines, calculated to five places of figures, for every Minute.

Natural Sines are Decimals bearing the same proportion to Usity or 1 that the Sine of the corresponding number of Degrees and Minutes bears to Radius or Sine of $90^{\circ}$. That is, 1 is assumed as the Nat. Sine of 900 , and the Table calculated accordingly.

## Explanation of the Table.

To find the Natural Sine of any number of Degrees and Minutes.
If the degrees be less than 45, look for them at the Top of the Columns, and for the Minutes at the left-hand; but if more than 45 , look for them at the Bottom, and for the Minutes at the right-hand; under or over the Degrees and against the Minutes will be the Natural Sine required.

The reverse of this will give the Degrees and Minutes corresponding to any Natural Sine.

To calculate the Northing or Southing, \&c. for any Course and Distance, by Nat. Sines.

Find the Nat. Sine and Co-Sine of the Course, and into each of these multiply the Distance; the Products will be the Latitude and Departure required.

## Example.

Required the Latitude and Departure for 6 Chains and 22 Links, on a Course N. $38027^{\prime} W$.

| Nat. | Sine of 380 | 27, 0.62183 | Nat. Co-Sine | 0.78315 |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 6.22 |  | 6.22 |
|  |  | 124366 |  | 156630 |
|  |  | 124366 | \% | 156630 |
|  |  | 373098 |  | 469890 |
|  |  | 3.8677826 |  | 8711930 |
|  | Answer: | Northing 4.87 | Westing | g 3.87 |


|  | 0 Deg. | 1 Deg. 2 Deg. |  |  |  | 3 Deg. |  | 4 Deg . |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Nat. N.C- | Nat. ${ }^{\text {N }}$ | N.C- | Nat. ${ }^{\text {N }}$ |  | Nat. | N.C- | Nat. ${ }^{\text {N }}$ | N.C- |  |
|  | Sine Sine | Sine | Sine | Sine | Sine | Sine | Sine | Sine | Sine |  |
| 0 | 00000 Unit. | $\underline{01745}$ | $99985 \cdot 03490$ |  | 99939 | $\begin{array}{r} 05234 \\ 263 \end{array}$ | 99863 06976 |  | $\overline{99756}$ | 7059 |
| 1 | 2900 | 774 | 84 | 519 |  |  |  | 07005 | 54 |  |
| 2 | 5800 | 803 | 84 | 548 | 37 | 292 | 60 | 034 | 52. | 58 |
| 3 | $87 \quad 00$ | 832 | 83 | 577 | 36 | 321 | 58 | 063 | 50 | 57 |
| 4 | 11600 | 862 | 83 | 606 | 35 | 350 | 57 | 092 | 48 | 56 |
| 5 | 14500 | 891 | 82 | 635 | 34 | 379 | 55 | 121 | 46 | 55 |
| 6 | 17500 | 920 | 82 | 664 | 33 | 408 | 54 | 150 | 44 | 54 |
| 7 | $204 \quad 00$ | 949 | 81 | 693 | 32 | 437 | 52 | 179 | 42 | 53 |
| 8 | 23300 | 978 | 80 | 723 | 31 | 1466 | 51 | 208 | 40 | 52 |
| 9 | 262 00, | 02007 | 80 | 752 | 30 | ) | 49 | 237 | 38 | 51 |
| 10 | 29100 | 036 | 79 | 731 | 29 | 9 | 47 | 266 | 36 | 50 |
| 11 | 32099999 | 065 | 79 | 810 | 27 | 7553 | 46 | 295 | 34 | 49 |
| 12 | 349 991 | 094 | 78 | 839 | 26 | 685 | 44 | 324 | 31 | 48 |
| 13 | $378 \quad 99$ | 123 | 77 | 868 | 25 | 5611 | 42 | 353 | 29 | 47 |
| 14 | 407 - 99 | 152 | 77 | 897 | $24$ | 640 | 41 | 382 | 27 | 46 |
| 15 | 436 99 | 181 | 76 | 926 | 23 | 669 | 39 | 411 | 25 | 45 |
| 16 | 00465 99999 | 02211 | 9976, | 3955 | 99922 | [ $\begin{array}{r}05698 \\ 727\end{array}$ | 9983836 | $\overline{07440} \overline{99723}$ |  | 44 |
| 17 | 495 99 | 240 | 75 | 984 | 21 |  |  | 469 | 21 | 43 |
| 18 | $524 \quad 99$ | 269 | 740 | 04013 | 19 | 756 | 34 | 498 | 19 | 49 |
| 19 | 55398 | 298 | 74 | 042 | 18 | 785 | 33 | 527 | 16 | 41 |
| 20 | 58298 | 327 | 73 | 071 | 17 | 814 | 31 | 556 | 14 | 40 |
| 21 | 61198 | 356 | 72 | 100 | 16 | 844 | 29 | 585 | 12 | 39 |
| 22 | 64098 | 385 | 72 | 129 | 15 | 873 | 27 | 614 | 10 | 38 |
| 23 | $669 \quad 98$ | 414. | 71 | 159 | 13 | 902 | 26 | 643 | 08 | 37 |
| 24 | 69898 | 443 | 70 | 188 | 12 | 931 | 24 | 672 | 05 | 36 |
| 25 | 787 97 | 472 | 69 | 217 | 11 | 960 | 22 | 701 | 03 | 35 |
| 26 | 756 97 | 501 | 69 | 246 | 10 | 98.9 | 21 | 730 | 01 | 34 |
| 27 | 78597 | 530 | 68 | 275 | 09 | 06018 | 19 | 759 | 99699 | 33 |
| 28 | 814 97 | 560 | 67 | 304 | 07 | 047 | 17 | 788 | 96 | 32 |
| 29 | $844 \quad 96$ | 589 | 66 | 333 | 06 | 076 | 15 | 817 | 94 | 31 |
| 30 | $873 \quad 96$ | 618 | 66 | 362 | 05 | 105 | 13 | 846 | 92 | 30 |
| 31 | 00902 99996 | 02647 | 99965 | 043919 | 99904 | 06134 | $\overline{99812}$ | $\overline{07875}$ | $\overline{99689}$ | 99 |
| 32 | 93196 | 676 | 64 | 420 | 02 | 163 | 10 | 904 | 87 | 28 |
| 33 | 96095 | 705 | 63 | 449 | 01 | 192 | 08 | 933 | 85 | 27 |
| 34 | $989 \quad 95$ | 734 | 63 | 478 | 00 | 221 | 06 | 963 | 83 | 26 |
| 35 | 01018 95 | 763 | 62 | 5079 | 99898 | 250 | 04 | 991 | 80 | 25 |
| 36 | 047 95 | 792 | 61 | 536 | 97 | 279 |  | 08020 | 78 | 24 |
| 37 | $076 \quad 94$ | 821 | 60 | 565 | 96 | 308 | 01 | 049 | 76 | 23 |
| 38 | 10594 | 850 | 59 | 594 | 94 | 337 | 99799 | 078 | 73 | 2 |
| 39 | $134 \quad 94$ | 879 | 59 | 623 | 93 | 366 | 97 | 107 | 71 | 21 |
| 40 | $164 \quad 93$ | 908 | 58 | 653 | 92 | 395 | 95 | 136 | 68 | 20 |
| 41 | 193 93 | 938 | 57 | 682 | 90 | 424 | 93 | 165 | 66 | 19 |
| 42 | 22293 | 967 | 56 | 711 | 89 | 453 | 92 | 194 | 64 | 18 |
| 43 | $251 \quad 92$ | 996 | 55 | 740 | 88 | 482 | 90 | 223 | 61 | 17 |
| 44 | 28092 | 03025 | 54 | 769 | 86 | 511 | 88 | 252 | 59 | 16 |
| 45 | $309 \quad 91$ | 054 | 53 | 798 | 85 | 540 | 86 | 281 | 57 | 15 |
| 46 | 01338 $\overline{99991}$ | $\overline{03083}$ | 99952 | 04827 | 99883 | 06569 | 99784 | 0831 | 9654 |  |
| 47 | 36791 | 112 | 52 | 856 | 82 | 598 | 82 | 339 | 52 |  |
| 48 | $396 \quad 90$ | 141 | 51 | 885 | 81 | 627 |  | 368 | 49 | 12 |
| 49 | $425 \quad 90$ | 170 | 50 | 914 | 79 | 656 | 78 | 397 | 47 | 110 |
| 50 | $454 \quad 89$ | 199 | 49 | 943 | 78 | 685 | 76 | 426 | 44 | 110 |
| 51 | $483 \quad 89$ | 228 | 48 | 972 | 76 | 714 | 74 | 455 | 42 |  |
| 52 | 51389 | 257 | 47 | 05001 | 75 | 743 | 72 | 434 | 39 |  |
| 53 | 54288 | 286 | 46 | 030 | 73 | 773 | 70 | 513 | 37 |  |
| 54 | 57188 | 316 | 45 | 059 | 72 | 802 | 68 | 542 | 35 |  |
| 55 | 60087 | 345 | 44 | 088 | 70 | 831 | 66 | 571 | 32 |  |
| 56 | 62987 | - 374 | 4.3 | 117 | 69 | 860 | 6 | 600 | 30 |  |
| 57 | $658 \quad 86$ | - 403 | 42 | 146 | 67 | 889 | 62 | 629 | 27 |  |
| 58 | 687 86 | , 432 | 41 | 175 | 66 | 918 | 60 | 658 | 25 |  |
| 59 | $716 \quad 85$ | 461 | 40 | 205 | 64 | 947 | 58 | 687 | 22 |  |
| M | $\frac{7}{\text { N.C- }} \overline{\text { Nat. }}$ | $\begin{array}{\|l} \hline \text { N.C- } \\ \text { Sine } \end{array}$ | Nat. Sine | N.C- | at. | $\overline{\mathbf{N} . \mathbf{C}}$ | Nat | N.C. | Nat. | $\overline{1}$ |
|  | Sine Sine |  |  | Sine | Sine |  | Sine | Sine | Sine |  |
|  | 89 Deg . | 881 | Deg. | 871 | Deg. | 86 | Deg | 85 | Deg. |  |




| 15 Deg. 16 Deg. 117 Deg. 18 Deg.\|19 Deg. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 25882 | 96593 | 27564 | 96126 | 29237 | 95630 | 3090 | 95106 | 32557 | 94552 | 60 |
| 1 | 910 | 585 | 592 | 118 | 265 | 622 | 929 | 097 | 584 | 542 | 59 |
| 2 | 938 | 578 | 620 | 110 | 293 | 613 | 957 | 088 | 612 | 533 | 58 |
| 3 | 966 | 570 | 648 | 102 | 321 | 605 | 985 | 079 | 639 | 523 | 57 |
| 4 | 994 | 562 | 676 | 094 | 348 | 596 | 31012 | 070 | 667 | 514 | 56 |
|  | 26022 | 555 | 704 | 086 | 376 | 588 | 040 | 061 | 694 | 504 | 55 |
| 6 | 050 | 547 | 731 | 078 | 404 | 579 | 068 | 052 | 722 | 495 | 54 |
| 7 | 079 | 540 | 759 | 070 | 432 | 571 | 095 | 043 | 749 | 485 | 53 |
| 8 | 107 | 532 | 787 | 062 | 460 | 562 | 123 | 033 | 777 | 476 | 52 |
| 9 | 135 | 524 | 815 | 054 | 487 | 554 | 151 | 024 | 804 | 466 | 51 |
| 10 | 163 | 517 | 843 | 046 | 515 | 545 | 178 | 015 | 832 | 457 | 50 |
| 11 | 191 | 509 | 871 | 037 | 543 | 536 | 206 | 006 | 859 | 447 | 49 |
| 12 | 219 | 502 | 899 | 029 | 571 | 528 | 233 | 94997 | 887 | 438 | 48 |
| 13 | 247 | 494 | 927 | 021 | 599 | 519 | 261 | 1988 | 914 | 428 | 47 |
| 14 | 275 | 486 | 955 | 013 | 626 | 511 | 289 | 97.9 | 942 | 418 | 46 |
| 15 | 303 | 479 | 983 | 005 | 654 | 502 | 316 | 6 970 | 969 | 409 | 45 |
| 16 | 6331 | 471 | 2801 | $\overline{95997}$ | 9682 | $\overline{95493}$ | 31344 | 94961 | $\widehat{32997}$ | 4899 | 4 |
| 17 | 359 | 463 | 039 | 989 | 710 | 485 | 372 | 952 | 33024 | 390 | 43 |
| 18 | 387 | 456 | 067 | 981 | 737 | 476 | 399 | 943 | 051 | 380 | 42 |
| 19 | 415 | 448 | 095 | 972 | 765 | 467 | 427 | 7933 | 079 | 370 | 41 |
| 20 | 443 | 440 | 123 | 964 | 793 | 459 | 454 | 924 | 106 | 361 | 40 |
| 21 | 471 | 433 | 150 | 956 | 821 | 450 | 482 | 915 | 134 | 351 | 39 |
| 22 | 500 | 425 | 178 | 948 | 849 | 441 | 510 | 906 | 161 | 342 | 38 |
| 23 | 528 | 417 | 206 | 940 | 876 | 433 | 537 | 897 | 189 | 332 | 37 |
| 24 | 556 | 410 | 234 | 931 | 904 | 424 | 565 | 888 | 216 | 322 | 36 |
| 25 | 584 | 402 | 262 | 923 | 932 | 415 | 593 | 878 | 244 | 313 | 35 |
| 26 | 612 | 394 | 290 | 915 | 960 | 407 | 620 | 869 | 271 | 303 | 94 |
| 27 | 640 | 386 | 318 | 907 | 987 | 398 | 648 | 860 | 298 | 293 | 33 |
| 28 | 668 | 379 | 346 | 898 | 30015 | 389 | 675 | 851 | 326 | 284 | 32 |
| 29 | 696 | 371 | 374 | 890 | 043 | 380 | 703 | -842 | 353 | 274 | 31 |
| 30 | 794 | 363 | 402 | 882 | 071 | 372 | 730 | 832 | 381 | 264 | 30 |
| 31 | 2675 | 6355 | $\overline{28429}$ | $\overline{95874}$ | 30098 | 9536 | 1758 | $\overline{94823}$ | 33408 | $\overline{94254}$ | 29 |
| 32 | 780 | 347 | 457 | 865 | 126 | 354 | 786 | - 814 | 436 | 245 | 28 |
| 33 | 808 | 340 | 485 | 857 | 154 | 345 | 813 | 805 | 463 | 235 | 27 |
| 34 | 836 | 332 | 513 | 849 | 182 | 337 | 841 | 795 | 490 | 225 | 26 |
| 35 | 864 | 324 | 541 | 841 | 209 | 328 | 868 | 786 | 518 | 215 | 25 |
| 36 | 892 | 316 | 569 | 832 | 237 | 319 | 896 | 777 | 545 | 206 | 24 |
| 37 | 920 | 308 | 597 | 824 | 265 | 310 | 923 | 768 | 573 | 196 | 23 |
| 38 | 948 | 301 | 625 | 816 | 292 | 301 | 951 | 758 | 600 | 186 | 22 |
| 39 | 976 | 293 | 652 | 807 | 320 | 293 | 979 | 749 | 627 | 176 | 21 |
| 402 | 27004 | 285 | 680 | 795 | 348 | 284 | 32006 | 740 | 655 | 167 | 20 |
| 41 | 032 | 277 | 708 | 791 | 376 | 275 | 034 | 730 | 688 | 157 | 19 |
| 42 | 060 | 269 | 736 | 782 | 403 | 266 | 061 | 721 | 710 | 147 | 18 |
| 43 | 088 | 261 | 764 | 774 | 431 | 257 | 089 | 712 | 737 | 137 | 17 |
| 44 | 116 | 253 | 792 | 766 | 459 | 248 | 116 | 702 | 764 | 127 | 16 |
| 45 | 144 | 246 | 820 | 757 | 486 | 240 | 144 | - 693 | 792 | 118 | 15 |
| 46 | 27172 | 96238 | $\underline{28847}$ | 95749 | 30514 | 95231 | 32171 | 194684 | 33819 | 94108 | 14 |
| 47 | 200 | 230 | 875 | 740 | 542 | 222 | 199 | 674 | 846 | 098 | 13 |
| 48 | 228 | 222 | 903 | 732 | 570 | 213 | 227 | 7663 | 874 | 088 | 12. |
| 49 | 256 | 214 | 931 | 724 | 597 | 204 | 254 | 656 | 901 | 078 | 11 |
| 50 | 284 | 206 | 959 | 715 | 625 | 195 | 282 | 646 | 929 | 068 | 10 |
| 51 | 312 | 198 | 987 | 707 | 653 | 186 | 309 | 637 | 956 | 058 | 9 |
| 52 | 340 | 190 | 29015 | 698 | 680 | 177 | 337 | 627 | 983 | 049 | 8 |
| 53 | 368 | 182 | 042 | 690 | 708 | 168 | 364 | 618 | 34011 | 039 | 7 |
| 54 | 396 | 174 | 070 | 681 | 736 | 159 | 392 | 609 | 038 | 029 | 6 |
| 55 | 424 | 166 | 098 | 673 | 763 | 150 | 419 | 599 | 065 | 019 | 5 |
| 56 | 452 | 158 | 128 | 664 | 791 | 142 | 447 | 590 | 093 | 009 | 4 |
| . 57 | 480 | 150 | 154 | 656 | 819 | 133 | 474 | 580 | 120 | 93999 | 3 |
| 58 | 508 | 142 | 182 | 647 | 846 | 124 | 502 | 571 | 147 | 989 | 2 |
| 59 | 536 | 134 | 209 | 639 | 874 | 115 | 529 | 561 | 175 | 979 | 1 |
|  | N.CS | N. S. | N.CS | D. S. | $\frac{\text { N.CS }}{172 T}$ | D. S. | $\frac{\mathrm{N} . \mathrm{CS}}{71}$ | Deg. | $\frac{\overline{\mathrm{N} . \mathrm{CS}}}{70}$ | $\frac{\overline{N . S}}{\mathrm{Deg} .}$ |  |


|  | $\left\|\begin{array}{l} 20 \text { Deg. } 21 \text { Deg. } \\ \frac{22}{2} \text { Deg. } 23 \text { Deg. } 24 \text { Deg. } \\ \text { N. S.N.CS } \\ \text { N. S. N.CE } \end{array}\right\|$ |  |  |  |  |  |  |  |  |  | M |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 03420293 | 3969 | 83793 | 3358 | 374619 | 92718 | 9073 9 | 9205 |  | 55s | 60 |
| 1 | 12229 | 959 | 864 | 348 | 488 | 707 | 100 | 039 | 700 | 343 | 59 |
| 2 | 2257 | 949 | 891 | 337 | 515 | 697 | 127 | 028 | 727 | 331 | 58 |
|  | 3284 | 939 | 918 | 327 | 542 . | 686 | 153 | 016 | 753 | 319 | 57 |
|  | 4311 | 949 | 945 | 310 | 569 | 675 | 180 | 005 | 780 | 307 | 56 |
|  | 5339 | 919 | 973 | 306 | 595 | 664 | 2079 | 91994 | 806 | 295 | 55 |
|  | $6{ }^{6} 366$ | 90936 | 000 | 295 | 622 | 653 | 234 | 982 | 833 | 283 | 54 |
|  | 7393 | 899 | 027 | 285 | 649 | 642 | 260 | 971 | 860 | 272 | 53 |
|  | 8421 | 889 | 054 | 274 | 676 | 631 | 287 | 959 | 835 | 260 | 52 |
|  | 9448 | 879 | 081 | 264 | 703 | 620 | 314 | 948 | 913 | 248 | 51 |
| 10 | 0475 | 869 | 108 | 253 | 730 | 609 | 341 | 936 | 939 | 236 | 50 |
| 11 | 1.503 | 859 | 135 | 243 | 757 | 598 | 367 | 925 | 966 | 224 | 49 |
| 12 | 2530 | 849 | 162 | 232 | 784 | 587 | 394 | 914 | 992 | 212 | 48 |
| 13 | $3{ }^{557}$ | 839 | 190 | 222 | 811 | 576, | 421 | 9024 | 41019 | 200 | 47 |
| 14 | 4584 | 829 | 217 | 211 | 838 | 565 | 448 | 891 | 045 | 188 | 46 |
| 15 | 5612 | 819 | 244 | 201 | 865 | 554 | 474 | 879 | 072 | 176 | 45 |
| 16 | 634639 | $\bigcirc 809$ | 7 | 3190 | 378929 | 2543 | 501 | 1868 | 1098 | 164 | 44 |
| 17 | 7666 | 799 | 298 | 180 | 919 | 532 | 528 | 856 | 125 | 152 | 43 |
| 18 | $8 \quad 694$ | 739 | 325 | 169 | 946 | 521. | 555 | 845 : | 151 | 140 | 42 |
| 19 | 9721 | 779 | 352 | 159 | 973 | 510 | 581 | 833 | 178 | 128 | 41 |
| 20 | 0 748 | 769 | 379 | 148 | 999 | 499. | 608 | 822 | 204 | 116 | 40 |
| 21 | 1775 | 759 | 406 | 137 | 38096 | 488 | 635 | 810 | 231 | 104 | 39 |
| 22 | 2283 | 748 | 434 | 127 | 053 | 477 | 661 | 799 | 257 | 082 | 38 |
| 23 | 3380 | 738 | 461 | 116 | 080 | 466 | 688 | 787 | 284 | 080 | 37 |
| 24 | 485 | 728 | 488 | 106 | 107 | 435 | 715 | 775 | 310 | 068 | 36 |
| 25 | 5884 | 718 | 515 | 095 | 134 | 444 | 741 | 764 | 337 | 056 | 35 |
|  | 26. 912 | 708 | 542 | 084 | 161 | 432 | 768 | 752 | 363 | 044 |  |
|  | 77939 | 698 | 569 | 074 | 188 | 421 | 795 | 741 | 390 | 032 | 33 |
|  | 88966 | 688 | 596 | 063 | 215 | 410 | 822 | 729 | 416 | 020 | 32 |
|  | 29993 | 677 | 623 | 052 | 241 | 399 | 848 | 718 | 443 | 008 | 31 |
|  | 3035021. | 667 | 650 | 042 | 268 | 388 | 875 | 706 | 469 | 0996 | 30 |
|  | $3 1 \longdiv { 3 5 0 4 8 }$ | 9365 | 6677 | 93031 | 38295 | 23 | 990 | 163 | 149 | 0984 | 29 |
|  | 32075 | 647 | 704 | 020 | 322 | 366 | 928 | 683 | 522 | 972 | 28 |
|  | 33102 | 637 | ; 31 | 010 | 349 | 355 | 955 | 671 | 549 | 960 | 27 |
|  | $34 \quad 130$ | 626. | 7589 | 92999 | 376 | 343 | 982 | 660 | 575 | 945 |  |
|  | 35157 | 616 | 785 | 988 | 403 | 3324 | 40008 | 648 | 602 | 936 | 25 |
|  | 36183 | 606 | 812 | 978 | 430 | 321 | 035 | 636 | 628 | 924 |  |
|  | $37 \quad 211$ | 596 | 839 | 967 | 456 | 310 | 062 | 625 | 655 | 911 |  |
|  | $38 \quad 239$ | 585 | 867 | 956 | 483 | 299 | 038 | 613 | 681 | 899 | 1 |
|  | 39 266 | 575 | 894 | 945 | 510 | 287 | 115 | 601 | 707 | 887 | 21 |
|  | $40 \quad 293$ | 565 | 921 | 935 | 537 | 276 | 141 | 590 | 734 | 875 |  |
|  | $41 \quad 320$ | 555 | 948 | 924 | 564 | 265 | 168 | 5781 | 760 | 863 | 18 |
|  | $42 \quad 347$ | 544 | 975 | 913 | 591 | 254 | 195 | 566 | 787. | 851 |  |
|  | $43 \quad 375$ | 5343 | 7002 | 902 | 617 | 243 | 221 | 555 | 813 | 839 | 1 |
|  | $44 \quad 402$ | 524 | 029 | 892 | 644 | 231 | 248 | 5431 | ${ }^{840}$ | 826 |  |
|  | $45 \quad 429$ | 514 | 056 | 881 | 671 | 220 | 275 | 531 | 866 | 814 |  |
|  | 46 $\overline{35456}$ | 93503 3 | 37083 | 92870 | 3369 | 92209 | 40301 | $\overline{91519}$ | 41892 | 90802 |  |
|  | $47 \quad 484$ | 493 | 110 | 859 | 725 | 198 | 328 | - 508 | 919 | 790 |  |
|  | $48 \quad 511$ | 483 | 137 | 849 | 752 | 186 | 355 | 496 | 945 | 778 | 12 |
|  | 49538 | 472 | 164 | 838 | 778 | 175 | 381 | 434 | 972 | 766 | 11 |
|  | 50565 | 462 | 191. | 827 | - 805 | 164 | 408 | 472 | 993 | 753 | 10 |
|  | 51592 | 452 | 218 | 816 | 832 | 2. 152 | + 434 | 4 46̄1 | 42034 | 741 |  |
|  | 52.619 | 441 | 245 | 805 | 859 | 4 141 | : 461 | $1{ }^{4} 49$ | 051 | 729 |  |
|  | $53 \quad 647$ | 431 | 272 | 794 | 836 | 130 | 488 | 437\% | 077 | 717 |  |
|  | 54 674 | 420. | 299 | 784 | 4 912 | \| 119 | , 514 | 425 | 104 | 704 |  |
|  | $55 \quad 701$ | 410 | 326 | 773 | - 939 | 107 | 541 | 1414 | 130 | 692 |  |
|  | $\begin{array}{lll}56 & 728\end{array}$ | 400 | 353 | 762 | $2 \quad 966$ | - 096 | . 567 | 7 402 | 156 | 680 |  |
|  | $57 \quad 755$ | 389 | 380 | 751 | 1993 | 085 | - 594 | $4 \quad 390$ | 183 | 668 |  |
|  | $58 \quad 782$ | 379 | 407 |  | 0.39020 | 073 | - 621 | 1378 | 209 | 655 |  |
|  | $59 \quad 810$ | 368 | 434 | 729 | $9 \quad 046$ | 062 | - 647 | 7366 | 235 | 643 |  |
| $\bar{M}$ N.CS $/$ N. S. N.CS N. S. |  |  |  |  |  |  |  |  |  |  |  |
| 69 Deg. 68 Deg.67 Deg. 66 Deg. 65 Deg. |  |  |  |  |  |  |  |  |  |  |  |

A TABLE OF NATURAL SINES.

|  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 42262 | 9063 |  | .89879 | 55399 |  | 46947 | 88295 | 8481 |  | 0 |
|  | 128* | 618 | 863 | 867 | 425 | 5087 |  | 281 | 506 |  | 59 |
| 2 | 315 | 606 | 889 | 854 | 451 | 1074 | 999 | 267 | 532 | 434 | 58 |
|  | 341 | 59 | 916 | 841 | 477 | 7061 | 470 | 25 | 557 | 420 | 57 |
|  | 367 |  | 942 | 828 | 503 | 048 | 050 | 240 | 583 | 40 | 56 |
| 5 | 394 | 569 | 968 | 816 | 529 | 035 | 076 | 2226 | 608 | 391 | 5 |
| 6 | 420 | 557 | 994 | 80 | 504 | -021, | 101 | 213 | 634 | 377 | 4 |
|  | 446 |  | 4020 | - 790 | 580 |  | 127 |  | 65 | 363 | 3 |
| 8 | 473 | 532 | 046 | 777 | 606 | 88995 | 153 | 18 | 684 | 34 | 5 |
|  | 59 | 520 | 072 | 764 | 632 | \$81 | 178 | 172 | 710 | 39 | 51 |
|  | 525 | 507 | 098 | 75 | 658 |  | 204 | 158 | 735 | 32 | 50 |
| 11 | 552 | 495 | 124 | 739 | 684 | 455 | 229 | 144 | 761 | 30 | 49 |
| 12 | 578 604 | 488 | 151 | 729 | 710 | -942 | 255 | 130 117 | 786 | 278 | 48 |
| 14 | 631 | 458 | 203 | 700 | 762 | 915 | 306 | 103 | 837 | 26 | 6 |
| 15 | 657 | 446 | 229 | 687 | 787 | 9021 | 33 | 089 | 86 | 250 | 5 |
|  | 42683 | 90433 | 4255 |  | 13 |  | 47358 | 88075 | 8888 | 723 | 4 |
| 17 | 709 | 421 | 281 | 662 | 839 | 875 | 383 | 06 | 913 | 221 | 3 |
| 18 | 736 | 408 | 307 | 649 | 865 | 862 | 409 | 048 | 93 | 207 | 2 |
| 19 | 762 | 396 | 333 | 636 | 891 | 848 | 434 |  | 96 | 19 | 1 |
| 20 | 788 | 383 | 359 | 23 | 917 | 835 | 460 | 020 | 98 | 17 | 0 |
| 21 | 815 | 371 | 385 | 610 | 942 | 822 | 456 | 006 | 901 | 16 | 39 |
| 22 | 841 | 358 | 411 | 597 | 968 | 808 | 5118 | 87993 | 04 | 15 | 38 |
| 23 | 867 | 346 | 437 | 584 | 994 | Tsら | 537. | 97 | 06 | 120 |  |
| 24 | 894 | 334 | 464 | 571 | 6020 | 782 | 562 | 965 | 09 | 121 | 6 |
| 25 | 920 | 321 | 490 | $558!$ | 046 | 768. | 588 | 95 | 116 | 107 | 35 |
| 26 | 946 | 309 | 516 | 545 | 072 | 755 | 61 | 93 | 141 | 093 | 4 |
| 27 | 972 | 296 | 542 | 532 | 097 | $741{ }^{2}$ | 639 | 92 | 16 | 07 | 析 |
| 28 | 999 | 281 | 568 | 519 | 123 | 728 | 665 |  | 192 | 06 | 32 |
|  | 43025 | 271 | 594 | 506 | 149 | 715 | 690 |  | 21 | 05 | 31 |
| 30 | 051 | 259 | 620 | 493 | 175 | 701 | 716 | 882 | 242 | 03 | 30 |
| $\overline{31} \overline{43077} \overline{90246} \overline{44646} \overline{59480} \overline{46201} \overline{88689} \cdot 47741 \overline{87868}$ |  |  |  |  |  |  |  |  |  |  |  |
| 32 | 104 | 2331 | 672 | 467 | 226 | 674 | 767 | 85 | 293 | 007 | 28 |
| 33 | 130 | 221 | 698 | 454 | 252 | 661 | 793 | 84 | 318.8 | 8699 | 7 |
| 34 | 156 | 208 | 724 | 441 | 278 | 647 ' | 818 |  | 344 | 97 | 26 |
| 35 | 182 | 196 | 750 | 428 | 304 | 634 | 844 | 81 | 369 | 96 | 25 |
| 36 | 209 | 183 | 776 | 415 | 330 | 620 | 869 | 79 | 39 | 94 | 4 |
| 37 | 235 | 171 | 802 | 402 | 355 | 607 | 895 | 78 | 419 | 93 | 3 |
| 38 | 261 | 158 | 828 | 389 | 381 | 593. | 920 | 770 | 445 | 92 | 22 |
| 39 | 287 | 146 | 54 | 376 | 407 | 58 | 946 | 75 | 470 | 906 | 21 |
| 40 | 313 | 133 | 880 | 363 | 433 | 566 | 971 | 74 | 49 | 89 | 0 |
| 41 | 340 | 120 | 906 | 350 | 458 | $503:$ | 997 | 72 | 521 | 87 | 19 |
| 42 | 36 | 103 | 302 | 337 | 434. | 5394 | 48022 | 71 | 5 | 86 | 18 |
| 43 | 392 | 095 | 958 | 394 | 510 | 526 | 048 | 701 | 571 | 84 | - |
| 44 | 418 | 082 | 984 | 311 | 536 | 512 | 073 | 687 | 596 | 83 | 16 |
| 45 | 445 | 070,4 | 45010 | 8 | 581 | 499 | 099 | 673 | 622 | 820 | 15 |
|  | 43471 | 9005 | 45036 | 89285 | 6587 | 88485 | $48124 ;$ | 87659 | 647 | 880 | 4 |
| 47 | 497 | 045 | 062 | 272 | 613 | 472. | 150 | 645 | 672 | 791 | 13 |
| 48 | 523 | 032 | 088 | 259 | 63 | 458 | 175 | 631. | 697 | 777 | 12 |
| 49 | 549 | 019 | 114 | 245. | 664 | 445 | 20 | 617 | 723 | 762 | , |
| 50 | 575 | 007 | 140 | 252 | 690 | 431. | 226 | 603 | 748 | 74 | 10 |
| 51 | 6028 | 69994 | 166 | 219 | 716 | 417 | 252 | 589 | 773 | 73 | 9 |
| 5 | 628 | 981 | 192 | 206 | 4 | 404 | 277 | 575 | 798 |  | 8 |
|  | 654 | 968 | 218 | 193 | 767 | 390 | 30 | 561 | 824 | 70 |  |
| 54 | 680 | 956 | 243 | 180. | 793 | 377 | 328 | 546. | 849 | 69 | 6 |
|  | 706 | 943 | 269 | 167 | 819 | 363: | 954 | 532 | 874 | 675 | 5 |
|  | 733 | 930 | 295 | 153 | 844 | 349 | 378 | 518 | 599 | 661 |  |
| 57 | 759 | 918 | 321 | 140 | 870 | 336. | 405 | 504 | 924 | 646 | 3 |
| 58 | 785 | 905 | 347 | 127 | 896 | 322. | 430 | 490 | 950 | 63 |  |
| 59 | 11 | 892 | 373 | 114. | 921 | 308 | 456 | 476 | 975 | 617 | 1 |
| $\bar{M}\left\|\begin{array}{ll} \text { N.CS } \\ 64 \text { Deg. } & \left.\begin{array}{ll} \overline{N . C S} \\ 63 & \text { Deg. } 62 \\ \text { Deg. } 61 & \text { Deg. } 60 \text { Deg. } \end{array} \right\rvert\, \end{array}\right\|$ |  |  |  |  |  |  |  |  |  |  |  |


|  |  | 330 Deg. 31 Deg. 32 Deg. 33 Deg. 34 Deg.\| |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5000 | 86603 | 51504 | 85717 | 52992 | 84805 | 54464 | 83867 | 5591 | 2904 | 60 |
| 1 | 025 | 588 | 529 | 702 | 53017 | 789 | 488 | 851. | 943 | 887 | 58 |
| 2 | 050 | 573 | 554 | 687 | 041 | 774 | 513 | - 835 | 968 | 871 | 58 |
| 3 | 076 | 559: | 579 | 672 | 066 | 759 | 537 | 819 | 992 | 855 | 57 |
| 4 | 101 | 544 | 604 | 657 | 091 | 743 | 561 | 804 | 56016 | 839 | 56 |
| 5 | 126 | 530 | 628 | 642. | 115 | 728 | 586 | 788 | 040 | 822 | 55 |
| 6 | 151 | 515 | 653 | 627 | 140 | 712 | 610 | 772 | 064 | 806 | 54 |
| 7 | 176 | 501 | 678 | 612 | 164 | 697 | 635 | 756 | 088. | 750 | 53 |
| 8 | 201 | 486 | 703 | 597 | 189 | 681 | 659 | 740 | 112. | 773 | 52 |
| 9 | 227 | 471 | 728 | 582 | 214 | 666 | 683 | 724 | 136 | 757 | 51 |
| 10 | 252 | 457 | 753 | 567 | 233 | 650 | 708 | 708 | 160 | 741 | 50 |
| 11 | 977 | 442 | 778 | 551 | 263 | 635 | 732 | 692. | 184 | 724 | 49 |
| 12 | 302 | 427 | $80 \%$ | 536 | 288 | 619 | 756 | 676 | 208 | 708 | 48 |
| 13 | 327 | 413 | 828 | 521 | 312 | 604 | 781 | 660 | 232 | 692 | 47 |
| 14 | 352 | 398 | 852 | 506 | 337 | 588 | 805 | \| 645 | 256 | 675 | 46 |
| 15 | 377 | 384 | 877 | 491 | 361 | 573 | 829 | 629 | 280 | 659 | 45 |
| 16 | 50403 | 86369 | 5190\% | 85476 | 53388 | 84557 | 54854 | 83613 | 305 | 2643 | 44 |
| 17 | 428 | 354 | 927 | 461 | 411 | 542 | 878 | 597 | 329 | 626 | 43 |
| 18 | 453 | 340 | 954 | 446 | 435 | 526 | 902 | 581 | 353 | 610 | 42 |
| 19 | 478 | 325 | 977 | 431 ? | 460 | 511 | 927 | 565 | 377 | 593 | 41 |
| 20 | 503 | 3105 | 52002 | 416 | 484 | 495 | 951. | 549 | 401 | 577 | 40 |
| 21 | 528 | 295 | 026 | 401; | 509 | 486 | 975 | 533. | 425 | 561 | 39 |
| 22 | 553 | 281 | 051 | 385 | 534 | 464 | 999 | 517 | 449 | 544 | 38 |
| 23 | 578 | 266 | 076 | 370 | 558 | 448 | 55024 | 501) | 473 | 528 | 37 |
| 24 | 603 | $\because 51$ | 101 | 355 | 583 | 433 | 048 | 485 | 497 | 511 | 36 |
| 25 | 628 | 237 | 126 | 340 | 607 | 417 | 072 | 469 ! | 521 | 495 | 35 |
| 26 | 654 | $2 \div 2$ | 151 | 325 | 632 | 402 | 097 | 453 | 545 | 478 | 34 |
| 27 | 679 | 207 | 175 | 310 | 656 | 386 | 121 | 437 | 569 | 462 | 33 |
| 28 | 704 | 192 | 200 | 294. | 681 | 370 | 145 | 421: | 593 | 446 | 32 |
| 29 | 729 | 178 | 225 | 279 | 705 | 355 | 169 | 405 | 617 | 429 | 31 |
| 30 | 754 | 163 | 250 | 264 | 730 | 339 | 194 | 389 | 641 | 413 | 30 |
| 31 | 50779 | 8614 ${ }^{\text {a }}$ | 52275 | 85249 | 754 | 84324 | $\overline{55218}$ | 83373 | 685 | 2396 | 29 |
| 32 | 804 | 133 | 299 | 234 | 779 | 308 | 24: | 356. | 689 | 380 | 28 |
| 33 | 829 | 119 | 324 | 218 | 804 | 292 | 266 | 340, | 713 | 363 | 27 |
| 34 | 854 | 104' | 349 | 203. | 898 | 277 | 281 | 324 | 736 | 347 | 26 |
| 35 | 879 | 089 | 374 | 188. | 853 | 261 | 315 | 308 | 760 | 330 | 25 |
| 36 | 904 | 074 | 399 | 1.43 | 877 | 245 | 339 | 292 | 784 | 314 | 24 |
| 37 | y29 | 059 | 423 | 157 | 902 | 230 | 363 | 276 | 808 | 297 | 23 |
| 38 | 954 | 045 | 448 | 142 | 926 | 214 | 388 | 260 | 832 | 281 | 22 |
| 39 | 979 | 030 | 473 | 127 | 951 | 198 | 412 | 244 | 856 | 264 | 21 |
| 40 | 51(104 | 015 | 498 | 119 | 975 | 182 | 436 | 228 | 880 | 248 | 20 |
| 41 | 029 | 000 | 522 | 0965 | 5400 | 167 | 460 | 212 | 904 | 231 | 19 |
| 42 | 054 | 85985 | 547 | 081 | 024 | 151 | 484 | 195 | 928 | 214 | 18 |
| 43 | 079 | 970 | 572 | 066 | 049 | 135 | 509 | 179 | 952 | 198 | 17 |
| 44 | 104 | 956 | 597 | 051 | 073 | 120 | 533 | 163 | 976 | 181 | 16 |
| 45 | 129 | 941 | 621 | 635. | 097 | 104 | 557 | 1475 | 7000 | 165 | 15 |
| 46 | 1154 | 803926 | 52646 | 25021 | 4122 | 4088 | 558 | 13 | 202 | 148 | 14 |
| 47 | 179 | 911 | 671 | 005 | 146 | 072 | 605 | 115 | 047 | 132 | 13 |
| 45 | 204 | 896 | 6968 | 84989 | 171 | 057 | 630 | 098 | 071 | 115 | 12 |
| 48 | 229 | 881 | 790 | 974 | 195 | 041 | 654 | 082 | 095 | 098 | 11 |
| 50 | 254 | 866 | 745 | 959 | 220 | 025 | 678 | 066 | 119 | 082 | 10 |
| 51 | 279 | 851 | 770 | 943 | 244 | 009 | 702 | 050 | 143 | 065 | $\theta$ |
| 52 | 304 | 836 | 794 | 928 | 2698 | 83994 | 726 | 034 | 167 | 048 | 8 |
| 53 | 329 | 821 | 819 | 913 | 243 | 978. | 750 | 017 | 191 | 032 | 7 |
| 54 | 354 | 806 | 844 | 897 | 317 | 962. | 775 | 001 | 215 | 015 | 6 |
| 55 | 379 | 792 | 869 | 883 | 342 | 946 | 7998 | 82985 | 2388 | 1999 | 5 |
| 56 | 404 | 777 | 893 | 866 | 366 | 930 | 823 | 969 | 262 | 982 | 4 |
| 57 | 429 | 762 | 918 | 851 | 391 | 915 | 847 | 953 | 286 | 965 | 3 |
| 58 | 454 | 747 | 943 | 836 | 415 | 899. | 871 | 936 | 310. | 949 | , |
| 59 | 479 | 732 | 967 | 820 | 440 | 883 | 895 | 920 | 334 | 932 |  |
|  |  | $\overline{\mathrm{N} . \mathrm{s}}$ | $\begin{aligned} & \overline{N C 5} \\ & 58 \mathrm{I} \end{aligned}$ | $\begin{aligned} & \text { N.s } \\ & \text { Deg } \end{aligned}$ | $\frac{\overline{\mathrm{N} . \mathrm{CE}}}{57}$ | $\frac{\overline{\mathrm{N} \cdot \mathrm{~S}}}{\mathrm{Deg} \cdot \underline{i}}$ | $\frac{\overline{\text { N.CE }}}{56} \frac{\mathrm{~N}}{\mathrm{D}}$ | D. S. | $\frac{\mathrm{CS}}{5 \mathrm{I}}$ | eg. |  |



A TABLE OF NATURAL SINES.
$13 \%$

|  | $\begin{aligned} & 40 \mathrm{De} \\ & \mathrm{~N} . \mathrm{s} \cdot \mathrm{~N} \end{aligned}$ |  | 41 D |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 64279 | 76604 |  | 75471 |  | 7431468200 |  | 78135 $69466{ }^{116.487} 7$ |  | 71934 |  |
|  | 301 | 586 | 62 | 452 | 935 | 295 | 221 |  |  |  |  |
|  | 323 | 567 | 650 | 433 | 956 | 276 | 242 | 096 | 508 | 894 |  |
|  | 346 | 5480 | 672 | 414 | 978 | 256 | 264 | 076 | 529 | 87 | 57 |
| 4 | 368 | 530 | 694 | 395 | 99 | 287 | 285 | 056 | 549 | 85 |  |
| 5 | 390 | 511 | 16 | 375 | 02 | 217 | 306 | 036 | 570 |  | 5 |
| 6 | 412 | 492 | 738 | 356 |  | 198 | 327 | 016 | 591 | 81 | 5 |
|  | 435 | 473 | 759 | 337 | 0 | 178 | 349 | 72996 | 612 | 79 | 5 |
| 8 | 457 | 455 | 781 | 318 | 086 | 159 | 370 | 976 | 633 | 77 | 2 |
|  | 479 | 436 | 803 | 29 | 10 | 139 | 391 | 957 | 65 |  | 1 |
| 10 | 501 | 417 | 825 | 280 | 129 | 120 | 412 | 937 | 675 | 79 | 5 |
| 11 | 524 | 398 | 847 | 261 | 151 | 100 | 433 | 917 | 696 | 71 | 49 |
| 12 | 546 | 380 | 869 | 241 | 172 | 080 | 455 | 897 | 717 | 691 | 48 |
| 13 | 558 | 361 | 891 | 222 | 194 | 061 | 476 | 877 | 737 | 67 | 47 |
| 14 | 590 | 34 | 913 | 203 | 215 | 041 | 497 | 857 | 758 |  | 6 |
| 15 | 612 | 323 | 935 | 184 | 237 | 022 | 518 | 837 | 779 | 630 | 45 |
|  | 64635 | $\begin{array}{rr} 76304 & 65956 \\ 286 & 978 \end{array}$ |  | 75165.67258 |  | $\overline{74002} \overline{685839}$ |  | $\overline{72817} \overline{69800} \overline{71610}$ |  |  | 44 |
| 17 | 657 |  |  |  |  |  |  |  |  |  |  |
| 18 | 679 | 26766 | 66000 |  |  | 126 | 301 | 963 | 582 | 777 | 842 |  | 42 |
| 19 | 701 | 248 | 022 | 107 | 323 | 94 | 603 | 757 | 86 |  | 41 |
| 20 | 723 | 229 | 044 | 088 | 344 | 92 | 624 | 737 | 883 | 52 | 40 |
| 21 | 746 | 210 | 066 | 069 | 568 | 90 | 645 | 717 | 904 |  | 39 |
| 22 | 768 | 192 | 088 | 050 | 387 | 88 | 666 | 697 | 92 |  |  |
| 23 | 790 | 173 | 109 | 030 | 409 | 86 | 688 | 677 | 946 | 46 | 7 |
| 24 | 812 | 154 | 131 | 011 | 430 | 846 | 709 | 657 | 966 |  | 3 |
| 25 | 834 | 135. | 153 | 74992 | 452 | 826 | 730 | 63 | 987 |  | 5 |
| 26 | 856 | 116 | 175 | 973 | 473 | 806 | 751 |  | 0008 | 40 |  |
| 27 | 878 | 097 | 197 | 953 | 495 | 78 | 772 | 597 | 029 | 38 |  |
|  | 901 | 078 | 218 | 934 | 516 | 76 | 793 | 57 | 049 | 36 | 32 |
| 29 | 923 | 059 | 240 | 915 | 538 | 747 | 814 | 55 | 070 |  | 1 |
| 30 | 915 | 041 | 262 | 896 | 559 | 72 S | 835 | 537 | 091 | 325 | 30 |
|  | 64967 |  |  | $\overline{74876.67580}$ |  |  |  |  |  |  |  |
| 32 | 989 | 003 | 306 | 857 | 602 |  |  |  |  |  |  |  |  |  |  |  |
|  | 650117 | 75984 | 327 | 838 | 623 | 669 | 899 | 477 | 153 |  | 27 |
| 34 | 033 | 965 | 349 | 818 | 645 | 649 | 920 | 45 | 174 |  | 6 |
| 35 | 055 | 946 | 371 | 799 | 666 | 629 | 941 | 43 | 195 |  |  |
| 36 | 077 | 927 | 393 | 780 | 688 | 610 | 962 | 417 | 215 |  |  |
| 37 | 099 | 08 | 41 | 760 | 709 | 590 | 98 | 397 | 236 |  |  |
|  | 122 | 889 | 436 | 41 | 730 |  | 6900 | 87 | 257 |  |  |
| 39 | 144 | 870 | 458 | 722 | 752 | 551 | 025 | 35 | 277 | 14 | 21 |
| 40 | 166 | 851 | 480 | 703 | 773 | 531 | 046 | 33 | 298 |  | 0 |
| 41 | 188 | 832 | 501 | 683 | 79 | 511 | 067 | 31 | 319 |  | 9 |
| 42 | 210 | 813 | 523 | 664 | 816 | 491 | 088 | 297 | 339 |  | 8 |
| 43 | 232 | 794 | . 545 | 644 | 83 | 472 | 109 | 277 | 360 |  |  |
| 44 | -254 | 775 | * 566 | 625 | 㖪 | 452 |  | 257 | 381 |  | 16 |
| 45 | 276 | 756 | 588 | 606 | 880 | 432 | 151 | 236 | 401 | 019 | 15 |
|  | 65298 | 75738 <br> 719 <br> 66610 <br> 632 |  | $\overline{74586} \overline{67901}$ |  |  |  | $\overline{72216} \overline{70422} \overline{70998}$ |  |  |  |
| 47 | 320 |  |  | 567 | 923 |  |  |  |  |  |  |  |  |
| 48 | 342 | 699 | 653 | 548 | 94 | 373 | 21 | 176 | 463 |  | 1 |
| 49 | 364 | 680 | 675 | 528. | 965 | 353 | 235 | 156 | 484 | 937 |  |
| 50 | 386 | 661 | 697 |  | 98 | 333 | 256 | 136 | 505 | 16 | 0 |
| 51 | 408 | 64. | 78 | 489 | 68008 | 314 | 27 | 116 | 25 |  |  |
| 52 | 430 | 623 | 740 | 470 | 029 | 294 | 298 | 095 | 546 | 87 |  |
| 53 | 452 | 604 | 762 | 451 | 05 | 274 | 319 | 075 | 567 |  |  |
| 54 | 474 | 585 | 83 | 431 | 072 | 254 | 340 | 05 | 587 |  |  |
|  | 496 | 566 | 805 | 412 | 093 | 234 | 361 | 035 | 608 |  |  |
| 57 | 518 | 547 | 827 | 392. | 115 | 215 | 382 | 015 | 628 |  |  |
| 57 | 540 | 528 | 848 | 373 | 136 | 195 |  | 71995 | 649 |  |  |
| 58 | 562 | 509 | ( 870 | 353. | 157 | 175 |  | 974 | 690 |  |  |
| 58 60 | $584$ |  | + 891 | 334 314 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## RETURN CIRCULATION DEPARTMENT

TO $\longrightarrow 202$ Main Library

| LOAN PERIOD 1 <br> HOME USE | 2 | 3 |
| :--- | :--- | :--- |
| 4 | 5 | 6 |

ALL BOOKS MAY BE RECALLED AFTER 7 DAYS
Renewals and Recharges may be made 4 days prior to the due date.
Books may be Renewed by calling 642-3405.
DUE AS STAMPED BELOW

| AUTODISCCIRC | Str 21,93 |  |
| :--- | :--- | :--- |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |

UNIVERSITY OF CALIFORNIA, BERKELEY
FORM NO. DD6

## Y̌e 11017


$42$


[^0]:    Hartford, Conn. October, 1804.

[^1]:    3. See the Introdaction to the Table of Natural Sines.
[^2]:    * A Compass may be so constructed with two Indexes, one moveable and the other fixed, as to ascertain the Angle made by two Sides, without reference to the Bearing of those Sides. Such a Compass would be particularly useful in surveying Land where there are mineral substances which have an influence upon the Compass Needle, attracting it one way or the other, ant thus rendering it impossible to take a Course by it with precision.

[^3]:    * For an explanation of this Table, and the manner of using it, scee the remarks preceding the Table.
    $\dagger$ See the Remarks preceding the Table of Natural Sines.

[^4]:    Note. It will be observed that against the third and sixth Courses there are no Areas; the reason is, that these Courses being one east and the-

[^5]:    * The following Figure exhibits a view of the relative situation of these Stars as they appear, when in a borizontal position : or when the North Star is in its greatest Eastern Elongation.

    The Great Bear.
    ${ }^{*}$ *Alioth
    ${ }^{*}{ }^{*}$

    Cassiopeia.
    Gamma******

[^6]:    * 57.3 degrees is the Radius of a circle (nearly) in suc̣h parts as the circamference contains 360 .

[^7]:    * There is one line around the globe on which there is no variation. The general course of this line, on this side of the globe, is from northwest to southeast, but is crooked and irregular in its course. According to Dr. Holly's chart, made in 1700, the line of no variation crossed the meridian of London in $55^{\circ}$ South latitude-cressed the equatur in $17^{\circ} \mathrm{W}$. longi-tude-from thence, by various windings, to the island of Bermuda, from

[^8]:    * Tlie diurnal motion is mentioned in Dr. Williams' History of Vermont.

[^9]:    * This may be solved geometrically.

