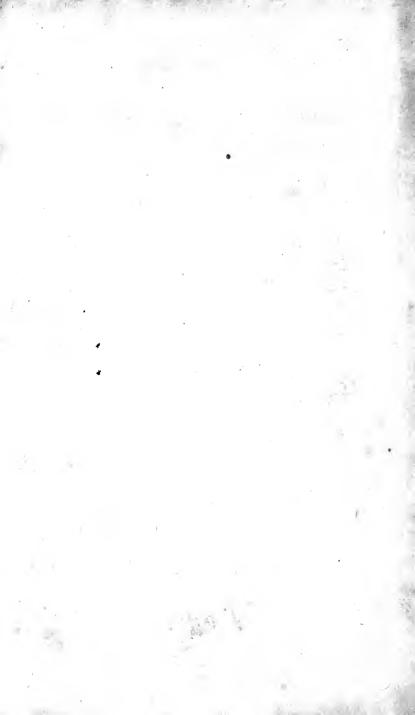




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GEOMETRY AND TRIGONOMETRY:

TOGETHER WITH A

TREATISE ON SURVEYING;

TEACHING VARIOUS WAYS OF TAKING THE SURVEY OF A FIELD ; ALSO TO PROTRACT THE SAME AND FIND THE AREA.

LIKEWISE,

RECTANGULAR SURVEYING;

OR,

AN ACCURATE METHOD OF CALCULATING THE AREA OF ANY FIELD ARITHMETICALLY, WITHOUT THE NECESSITY OF PLOTTING IT.

TO THE WHOLE ARE ADDED,

SEVERAL MATHEMATICAL TABLES,

NECESSARY FOR SOLVING QUESTIONS IN

TRIGONOMETRY AND SURVEYING;

WITH A PARTICULAR EXPLANATION OF THOSE TABLES, AND THE MANNER OF USING THEM.

COMPILED FROM VARIOUS AUTHORS,

BY ABEL FLINT, A.M.

FIFTH EDITION, WITH IMPORTANT ADDITIONS,

BY GEORGE GILLET,

SURVEYOR GENERAL OF THE STATE OF CONNECTICUT.

HARTFORD :

PUBLISHED BY OLIVER D. COOKE &, CO.

1825.

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District of Connecticut, ss. BE IT REMEMBERED, That on the twenty-fifth day of September, in the forty-third year of the Independence of the United States of America, Oliver D. Cooke & Co., of the said district, have deposited in this office the title of a book, the right whereof they claim as Proprietors, in the words following, to wit-

THEYS

"A System of Geometry and Trigonometry : together with a Treatise on Surveying; Teaching various ways of taking the Survey of a Field; Also to Protract the same and find the Area. Likewise, Rectangular Surveying; riouract the same and find the Area. Likewise, Rectangular Surveying; or, an Accurate Method of calculating the Area of any Field Arithmetically without the necessity of Plotting it. To the whole are added several Mathematical Tables, necessary for solving Questions in Trigonometry and Surveying; with a particular explanation of those Tables, and the Manner of using them. Compiled from various Authors. By Abel Flint, A. M. Fifth Edition, with important Additions, By George Gillet, Surveyer General of the State of Connecticut."

In conformity to the Act of the Congress of the United States, entitled "An Act for the encouragement of Learning, hy securing the copies of Maps, Charts, and Books, to the authors and proprietors of such copies, during the times therein mentioned."

R. I. INGERSOLL, Clerk of the District of Connecticut. A true copy of Record, examined and sealed by me, R. I. INGERSOLL, Clerk of the District of Connecticut.

RECOMMENDATIONS.

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HAVING perused, with some attention, the following Treatise on Surveying, in Manuscript, it appears to me to be estimable for its simplicity and perspicuity; and, by excluding all matter but remotely connected with the main subject, and reducing the Tables of Logarithms, of Logarithmic Sines, Tangents, and Secants, and of Difference of Latitude and Departure, without impairing their use, in their application to most cases which occur in common Surveying, and supplying any possible defect by a Table of Natural Sines, to comprise, in the limits of a pocket volume, whatever is most essential and most useful in the Art, including the important modern improvement of RECTANGULAR SUR-VEYING; and on the whole, particularly from the size of the volume, to be well adapted to general use.

JOHN TREADWELL.

FARMINGTON, Sept. 20th, 1804.

411458

RECOMMENDATIONS.

WE the subscribers have carefully perused a Treatise on Surveying, prepared for the Press by the Rev. Abel Flint of Hartford; and find it worthy of the public patronage. Every thing not immediately necessary for the practical Surveyor has been excluded ; while it comprises all which is requisite in Field Surveying, both on the old and new plan; elucidated and explained with a degree of conciseness and perspicuity not usually to be found in Treatises on the same subject. The Mathematical Tables are reduced to less than half the size occupied by others; and any inconvenience which might result from such reduction, is obviated by the insertion of a Table of Natural Sines, not usually found in works of this nature. The Surveyor who shall own this will not be under the necessity of purchasing GIBson, which is a more expensive work.

> ASHER MILLER, Surveyor General. GEORGE GILLET, Deputy Surveyor for Tolland County.

MIDDLETOWN, Oct. 3, 1804.

THE following work is chiefly a compilation from other Books; and but very little new is added, except a more full explanation, than has yet been published, of RECTANGULAR SURVEYING, or the method of calculating the Area of Fields arithmetically, without drawing a plot of them and measuring with a Scale and Dividers, as has been the common practice; and also a more particular explanation of the use of Natural Sines than is contained in most Mathematical Books.

The Compiler has endeavoured to render this work so easy and intelligible that a Learner will require but little assistance from an Instructer, except with regard to the construction and use of Mathematical and Surveying Instruments. Before, however, he enters on the study of this Book he must be well acquainted with common Arithmetic, with Decimal Fractions, and the Square Root; and he must also know the various characters or marks used in Arithmetic.

A Surveyor will doubtless find many questions arise in the course of his practice, for the solution of which, no particular directions are here given; nor is it possible to give directions for every case that may occur. In all practical Sciences much must be left to the judgment of the practitioner, who, if he is well acquainted with the general principles of his Art, will readily learn to apply those principles to particular cases.

The primary design of this treatise is to teach common Field Surveying; at the same time it contains the elements of Surveying upon a larger

scale ; and the system of Geometry and Trigonometry with which it is introduced, with the Problems for the mensuration of Superficies, as also the Mathematical Tables at the end, will be found useful for many other purposes. It would be well, therefore, for those who do not intend to become practical Surveyors to acquaint themselves with what is here taught; and with this view the following work is very proper to be introduced into Academies, and those higher Schools which are designed to fit young men for active business in life. Indeed every person who frequently buys and sells land should learn to calculate the Contents of a field arithmetically; a knowledge which may be acquired in a very little time, from the particular explanation here given of that method.

Notwithstanding the many Books already published on the subjects here treated upon, it was thought a work of this kind was really wanted, and that if judiciously executed it would be useful. It is more particularly necessary at the present time in Connecticut, as the Legislature of the State have lately enacted a Law on the subject of Surveying, in consequence of which more attention must be paid to the Theory of that Art than has been common.

These considerations induced the Compiler to select from various publications what appeared to him important; and to arrange the whole in a method best adapted, in his view, for teaching that useful Art. How far he has succeeded in his endeavours to simplify the subject, and render it easy to the Learner, must be submitted to the test of experience.

HARTFORD, Conn. October, 1804.

A GENERAL VIEW OF THE CONTENTS OF THIS WORK.

THE System of Geometry is divided into two parts. The first contains Geometrical Definitions respecting Lines, Angles, Superficies, &c. The second part contains a number of Geometrical Problems necessary for Trigonometry and Surveying.

The System of Trigonometry is also divided into two parts: and teaches the solution of questions in Right and Oblique angled Trigonometry, by Logarithms and also by Natural Sines.

The Treatise on Surveying is divided into three parts. Part first treats of measuring Land, and is divided into three Sections. The first contains several Problems respecting Mensuration, and for finding the Area of various Right-lined Figures and Circles.

The second Section teaches different methods of taking the Survey of Fields; also to protract them, and find their Area in the manner commonly practised, and likewise by Arithmetical and Trigonometrical calculations, without measuring Diagonals and Perpendiculars with a Scale and Dividers; interspersed with sundry useful rules and directions.

The third Section is a particular explanation and demonstration of *Rectangular Surveying*, or the method of computing the Area of Fields from the Field Notes, by Mathematical Tables, without the necessity of plotting the Field. To this Section is added a useful Problem for ascertaining the true Area of a Field which has been measured by a Chain too long or too short.

Part second treats of laying out Land in various shapes.

Part third contains sundry Problems and Rules for dividing Land and determining the true Course and Distance of dividing Lines, or from one part of a Field to another. To this is added an Appendix concerning the Variation of the Compass and Attraction of the Needle; also, a rule to find the difference between the present Variation, and that at a time when a Tract was formerly surveyed, in order to trace or run out the original lines.

The Mathematical Tables, are a Traverse Table, or Table of Difference of Latitude and Departure, calculated for every Degree and quarter of a Degree, and for any distance up to 50; a Table of Natural Sines calculated for every Minute; a Table of Logarithms comprised in four pages, yet sufficiently extensive for common use; and a Table of Logarithmic or Artificial Sines, Tangents, and Secants, calculated for every 5 Minutes of a Degree. To these Tables are prefixed particular explanations of the manner of using them.

GEOMETRY is a Science which treats of the properties of Magnitude.

PART I.

Geometrical Definitions.

1. A Point is a small Dot; or, Mathematically considered, is that which has no parts, being of itself indivisible.

2. A Line has length but no breadth.

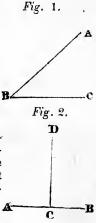
3. A Superficies or Surface, called also Area, has length and breadth, but no thickness.

4. A Solid has length, breadth, and thickness.

5. A Right Line is the shortest that can be drawn between two Points.

6. The inclination of two Lines meeting one another, or the opening between them, is called an Angle. Thus at B. Fig. 1. is an Angle, formed by the meeting of the Lines AB and BC.

7. If a right Line CD. Fig. 2. fall upon another Right Line AB, so as to incline to neither side, but make the Angles on each side equal, then those Angles are called Right Angles; and the Line CD is said to be Perpendicular to the other Line.



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8. An Obtuse Angle is greater than a Right Angle; as ADE. Fig. 3.

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9. An Acute Angle is less than a Right Angle; as EDB. Fig. 3.

Note. When three letters are used to express an Angle, the middle letter denotes the angular Point.

10. A Circle is a round Figure, bounded by a Line equally distant from some Point, which is called the Centre. Fig. 4.

11. The Circumference or Periphery of a Circle is the bounding Line; as ADEB. Fig. 4.

12. The Radius of a Circle is a Line drawn from the Centre to the Circumference; as CB. Fig. 4. Therefore all Radii of the same Circle are equal.

13. The Diameter of a Circle is a Right Line drawn from one side of the Circumference to the other, passing through the Centre; and it divides the Circle into two equal parts, called Semicircles; as AB or DE. Fig. 5.

14. The Circumference of every Circle is supposed to be divided into 360 equal parts, called Degrees; and each Degree into 60 equal parts, called Minutes; and each Minute

into 60 equal parts, called Seconds; and these into Thirds, &c.

Note. Since all Circles are divided into the same number of Degrees, a Degree is not to be accounted a quantity of any determinate length, as so many inches or feet, &c. but is always to be reckoned as being the 360th part of the Circumference of any Circle, without regarding the bignessof the Circle.

15. An Arch or Arc of a Circle is any part of the Circumference; as BF or FD. Fig. 5; and is said to be an Arch of so many Degrees as it contains parts of 360 into which the whole Circle is divided.

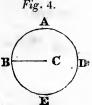


Fig: 5.

D

F



Fig. 3.

16. A Chord is a Right Line drawn from one end of an Arch to the other, and is the measure of the Arch; as HG is the Chord of Athe Arch HIG. Fig. 6.

Note. The Chord of an Arch of 60 degrees is equal in length to the Radius of the Circle of which the Arch is a part.

17. The Segment of a Circle is a part of a Circle, cut off by a Chord; thus the space comprehended between the Arch HIG and the Chord HG is called a Segment. Fig. 6.

18. A Quadrant is one quarter of a Circle; as ACB. Fig. 6. 19. A Sector of a Circle is a space contained between two Radii and an Arch less than a Semicircle; as BCD or ACD. Fig. 6.

20. The Sine of an Arch is a Line drawn from one end of the Arch, perpendicular to the Radius or Diameter drawn through the other end: Or, it is half the Chord of double the Arch; thus HL is the Sine of the Arch HB. Fig. 7.

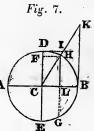
21. The Sines on the same Diameter in- \mathbf{A} crease in length till they come to the Centre, and so become the Radius. Hence it is plain that the Radius CD Fig. 7. is the greatest possible Sine, or Sine of 90 Degrees.

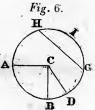
22. The Versed Sine of an Arch is that part of the Diameter or Radius which is between the Sine and the Circumference z thus LB is the Versed Sine of the Arch HB. Fig. 7.

23. The Tangent of an Arch is a Right Line touching the Circumference, and drawn perpendicular to the Diameter; and is terminated by a Line drawn from the Centre through the other end of the Arch; thus BK is the Tangent of the Arch BH. Fig. 7.

Note. The Tangent of an Arch of 45 Degrees is equal in length to the Radius of the Circle of which the Arch is a part.

24. The Secant of an Arch is a Line drawn from the Centre





through one end of the Arch till it meets the Tangent; thus CK is the Secant of the Arch BH. Fig. 7.

25. The Complement of an Arch is what the Arch wants of 90 Degrees, or a Quadrant; thus HD is the Complement of the Arch BH. Fig. 7.

26. The Supplement of an Arch is what the Arch wants of 180 Degrees, or a Semicircle; thus ADH is the Supplement of the Arch BH. Fig. 7.

27. The Sine, Tangent or Secant of the Complement of any Arch is called the Co-Sine, Co-Tangent, or Co-Secant of the Arch; thus, FH is the Sine, DI the Tangent, and CI the Secant of the Arch DH; or they are the Co-Sine, Co-Tangent, and Co-Secant of the Arch BH. Fig. 7.

28. The measure of an Angle is the Arch of a Circle contained between the two Lines which form the angle, the angular Point being the Centre; thus, the Angle HCB. Fig. 7. is measured by the Arch BH: and is said to contain so many Degrees as the Arch does.

Note. An Angle is esteemed greater or less according to the opening of the Lines which form it, or as the Arch intercepted by those Lines contains more or fewer Degrees. Hence it may be observed, that the bigness of an Angle does not depend at all upon the length of the including Lines; for all Arches described on the same Point, and intercepted by the same Right Lines, contain exactly the same number of Degrees, whether the Radius be longer or shorter.

29. The Sine, Tangent, or Secant of an Arch is also the Sine, Tangent, or Secant of the Angle whose measure the Arch is.

Fig. 8.

Fig. 9.

30. Parallel Lines are such as are equally **A**_____**B** distant from each other; as AB and CD. Fig. 8. **C**____**D**

31. A Triangle is a Figure bounded by three Lines; as ABC. Fig. 9.

32. An Equilateral Triangle has its three sides equal in length to each other. Fig. 9.

12

33. An Isocles Triangle has two of its sides equal, and the other longer or shorter. Fig. 10.

Fig. 11.

34. A Scalene Triangle has three unequal sides. Fig. 11.

35. A Right Angled Triangle has one Right Angle. Fig. 12.

36. An Obtuse Angled Triangle has one Obtuse Angle. Fig. 13.

37. An Acute Angled Triangle has all its Angles Acute. Fig. 9, or 10.

38. Acute and Obtuse Angled Triangles are called Oblique Angled Triangles, or simply Oblique Triangles; in which the bottom Side is generally called the Base and the other two, Legs.

39. In a Right Angled Triangle the longest side is called the Hypothenuse, and the other two, Legs, or Base and Perpendicular.

Note. The three Angles of every Triangle being added together will amount to 180 Degrees; consequently the two Acute Angles of a Right Angled Triangle amount to 90 Degrees, the Right Angle being also 90.



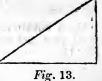


Fig. 10.

40. The perpendicular height of a Triangle is a Line drawn from one of the Angles to its opposite side; thus, the dotted Line AD. Fig. 14. is the perpendicular height of the Triangle ABC.

Note. This Perpendicular may be drawn from either of the Angles; and whether it falls within the Triangle, or on one of the Lines continued beyond the Triangle, is immaterial.

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41. A Square is a Figure bounded by four equal sides, and containing four Right Angles. *Fig.* 15.

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Fig. 16.

Fig. 15.

Fig. 14.

42. A Parallelogram, or Oblong Square, is a Figure bounded by four sides, the opposite ones being equal and the Angles Right. *Fig.* 16.

Fig. 17.

43. A Rhombus is a Figure bounded by four equal sides, but has its Angles Oblique. Fig. 17. -

B Fig. 18.

А

44. A Rhomboides is a Figure bounded by four sides, the opposite ones being equal, but the Angles Oblique. Fig. 18.

45. The perpendicular height of a Rhombus or Rhomboides is a Line drawn from one of the Angles to its opposite side; thus, the dotted Lines AB. Fig. 17. and Fig. 18. represent the perpendicular height of the Rhombus and Rhomboides.

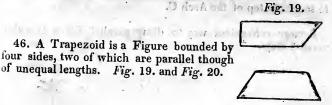


Fig. 20.

Note. Fig. 19. is sometimes called a Right Angled Trapezium.

Fig. 21.

47. A Trapezium is a figure bounded by four unequal sides. Fig. 21.

48. A Diagonal is a Line drawn between two opposite Angles; as the Line AB. Fig. 21.

49. Figures which consist of more than four sides are called Polygons; if the sides are equal to each other they are called regular Polygons, and are sometimes named from the number of their sides, as Pentagon, or Hexagon, a Figure of five or six sides, &c.; if the sides are unequal, they are called irregular Polygons.

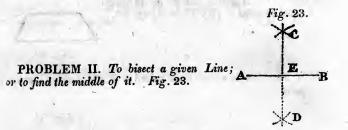
PART II.

Geometrical Problems.

PROBLEM I. To draw a Line parallel to another Line at any given distance; as at the Point D, to make a Line, parallel to the Line AB. Fig. 22.

With the Dividers take the nearest distance between the Point D and the given Line AB; with that distance set one foot of the Dividers any where on the Line AB, as at E, and draw the Arch C; through the Point D draw a Line so as just to touch the top of the Arch C.

A more convenient way to draw parallel Lines is with a parallel Rule.



Open the Dividers to any convenient distance, more than half the given Line AB, and with one foot in A, describe an Arch above and below the Line, as at C and D; with the same distance, and one foot in B, describe Arches to cross the former; lay a Rule from C to D, and where the Rule crosses the Line, as at E, will be the middle.

Fig. 24.

PROBLEM III. To erect a Perpendicular from the end, or any part of a given Line. Fig. 24.

Open the Dividers to any convenient distance, as from D to A, and with one foot on the Point D, from which the Perpendicular is to be erected, describe an Arch, as AEG; set off the same distance from A to E, and from E to G; upon E and G describe two Arches to intersect each other at H; draw a Line from H to D, and one Line will be perpendicular to the other.

Note. There are other methods of erecting a Perpendicular, but this is the most simple.

PROBLEM IV. From a given Point, as at C, to drop a Perpendicular on a A given Line AB. Fig. 25.

With one foot of the dividers in C describe an Arch to cut the given Line in two places, as at F and G; upon F and G describe two Arches to intersect each other below the Line as at D; lay a Rule from C to D and draw a Line from C to the given Line.

Perpendiculars may be more readily raised and let fall, by a small Square made of brass, ivory, or wood.

PROBLEM V. To make an Angle at E, A grant to a given Angle ABC. Fig. 26.

Open the dividers to any convenient distance, and with one foot in B describe the Arch FG; with the same distance and one foot in E, describe an Arch from H; measure the Arch FG, and lay off the same distance on the Arch from H to I; draw a Line through I to E, and the Angles will be equal.

Fig. 27.

F

Fig. 26.

PROBLEM VI. To make an Acute Angle equal to a given number of Degrees, suppose 36. Fig. 27.



Draw the Line AB to any convenient length; from a Scale of Chords take 60 Degrees with the dividers, and with one foot in B describe an Arch from the Line AB; from the same Scale take the given number of Degrees, 36, and lay it on the Arch from C to D; draw a line from B through D, and the Angle at B will be an Angle of 36 Degrees.

D

Fig. 25. C

Fig. 28.

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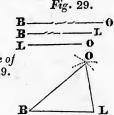
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PROBLEM VII. To make an Obtuse Angle, suppose of 110 Degrees. Fig. 28.

Take a Chord of 60 Degrees as before, and describe an Arch greater than a Quadrant; set off 90 Degrees from B to C, and from C to E set off the excess above 90, which is 20; draw a Line from G through E, and the Angle will contain 110 Degrees.

Note. In a similar manner Angles may be measured; that is, with a Chord of 60 Degrees describe an Arch on the angular Point, and on a Scale of Chords measure the Arch intercepted by the Lines forming the angle.

A more convenient method of making and measuring Angles_ is to use a Protractor instead of a Scale and Dividers.



PROBLEM VIII. To make a Triangle of three given Lines, as BO, BL, LO. Fig. 29.

Draw the Line BL from B to L; from B, with the length of the Line BO, describe an Arch as at O; from L, with the length of the Line LO, describe another Arch to intersect the former; from O draw the Lines OB and OL, and BOL will be the Triangle required.

Fig. 30.

PROBLEM IX. To make a Right Angled Triangle, the Hypothenuse and Angles being given. Fig. 30. 9.6 35° 30' B

Suppose the Hypothenuse CA 25 Rods or Chains, the angle

at C 35° 30' and consequently the Angle at A 54° 30'. See Note after the 39th Geometrical Definition.

Note. When degrees and minutes are expressed, they are distinguished from each other by a small cipher at the right hand of the degrees, and a dash at the right hand of the minutes; thus 35° 30' is 35 degrees and 30 minutes.

Draw the Line CB an indefinite length; at C make an Angle of 35° 30'; through where that number of Degrees cuts the Arch draw the Line CA 25 Rods, which must be taken from some Scale of equal parts; drop a Perpendicular from A to B, and the Triangle will be completed.

Note. The length of the two Legs may be found by measuring them upon the same scale of equal parts from which the Hypothenuse was taken.

PROBLEM X. To make a Right Angled Triangle, the Angles and one Leg being given. Fig. 31.

Suppose the Angle at C 33° 15', and the Leg AC 285.

Draw the Leg AC making it in length 285; at A erect a Perpendicular an indefinite length; at C make an Angle of 33° 15'; through where that number of Degrees cuts the Arch, draw a Line till it meets the Perpendicular at B.

Note. If the given Line CA should not be so long as the Chord of 60°, it may be continued beyond A, for the purpose of making the Angle.

PROBLEM XI. To make a Right Angled Triangle, the Hypothenuse and one Leg being given. Fig. 32.

Suppose the Hypothenuse AC 40, and the Leg AB 28. Draw the Leg AB in length 28; from B erect a Perpendicular an indefinite length; take 40 in the Dividers, and setting

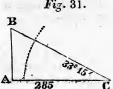


Fig. 32.

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R

one foot in A, wherever the other foot strikes the Perpendicular will be the point C.

Note. When the Triangle is constructed, the Angles may be measured by a Protractor, or by a Scale of Chords.

Fig. 33. Frig. 33. C PROBLEM XII. To make a Right Angled Triangle, the two Legs being given. Fig. 33. A 38

Suppose the Leg AB 38, and the Leg BC 46. Draw the Leg AB in length 38; from B erect a Perpendicular to C in length 46; and draw a Line from A to C. Fig. 34.

PROBLEM XIII. To make an Oblique Angled Triangle, the Angles and one Side being given. Fig. 34.



Suppose the side BC 98; the Angle at B 45° 15', the Angle at D 108° 30', consequently the other Angle 26° 15'.

'Draw the side BC in length 98; on the Point B make an Angle of 45° 15'; on the Point C make an Angle of 26° 15', and draw the Lines BD and CD.

Fig. 35.

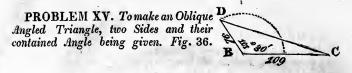
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PROBLEM XIV. To make an Oblique Angled Triangle, two Sides and an Angle opposite to one of them being given. Fig. 35.

Suppose the side BC 160, the side BD 79, and the Angle at C 29° 9'.

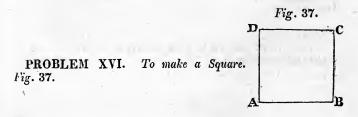
Draw the side BC in length 160; at C make an Angle of 29° 9', and draw an indefinite Line through where the Degrees cut the Arch; take 79 in the dividers, and with one foot in B lay the other on the Line CD; the point D will be the other Angle of the Triangle.

Fig. 36.



Suppose the side BC 109, the side BD 76, and the Angle at B 101° 30'.

Draw the side BC in length 109; at B make an Angle of 101° 30', and draw the side BD in length 76; draw a line from D to C and it is done.



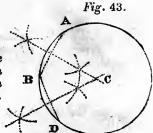
Draw the Line AB the length of the proposed Square; from B erect a Perpendicular to C and make it of the same length as AB; from A and C, with the same distance in the dividers, describe Arches intersecting each other at D, and draw the Lines AD and DC.



Draw the Line AB equal to the longest side of the Parallelogram; on B erect a Perpendicular the length of the shortest side to C; from C, with the longest side, and from A, with the shortest side, describe Arches intersecting each other at D, and draw the Lines AD and CD.

E

PROBLEM XVIII. To describe a Circle, which shall pass through any three given Points, not lying in a Right Line, as A, B, D. Fig. 43.



Draw Lines from A to B and from B to D; bisect those Lines by PROBLEM II. and the Point where the bisecting Lines inter sect each other, as at C, will be the centre of the Circle.

PROBLEM XIX. To find the centre of a Circle.

By the last PROBLEM it is plain, that if three Points be any where taken in the given Circle's Periphery, the centre of the Circle may be found as there taught.

Directions for constructing irregular Figures of four or more sides may be found in the following Treatise on SURVEYING.

TRIGONOMETRY is that part of practical GEOMETRY by which the Sides and Angles of Triangles are measured; whereby three things being given, either all sides, or sides and Angles, a fourth may be found; either by measuring with a Scale and Dividers, according to the PROBLEMS in GEOMETRY, or more accurately by calculation with Logarithms, or with Natural Sines.

TRIGONOMETRY is divided into two Parts, Rectangular and Oblique-angular.

PART I.

RECTANGULAR TRIGONOMETRY.

This is founded on the following methods of applying a Triangle to a Circle.

PROPOSITION I. In every Right Angled Triangle, as ABC, Fig. 44, it is plain from Fig. 7. compared with the Geometrical definitions to which that Figure refers, that if the Hypothenuse A AC be made Radius, and with it an Arch of a Circle be described from each end, BC will be the Sine of the Angle at A, and AB the Sine of the Angle at C; that is, the Legs will be Sines of their opposite Angles.

PROPOSITION II. If one Leg, AB, Fig. 45, be made Radius, and with it on the Point A an Arch be described, then BC, the other Leg, will be the Tangent and AC the Secant of the Angle at A; and if BC be made Radius, and an Arch be described with it on the Point C, then AB will be the Tangent and AC the Secant of the Angle at C; that is, if one Leg \checkmark



be made Radius the other Leg will be a Tangent of its opposite Angle, and the Hypothenuse a Secant of the same Angle.

Thus, as different sides are made Radius, the other sides acquire different names, which are either Sines, Tangents or Secants.

As the sides and Angles of Triangles bear a certain proportion to each other, two sides and one Angle, or one side and two Angles being given, the other sides or Angles may be found by instituting Proportions, according to the following Rules.

RULE I. To find a side, either of the sides may be made Radius, then institute the following Proportion:

As the name of the side given, which will be either Radius, Sine, Tangent or Secant;

Is to the length of the side given;

So is the name of the side required, which also will be either Radius, Sine, Tangent or Secant;

To the length of the side required.

RULE II. To find an Angle one of the given sides must be made Radius, then institute the following Proportion :

As the length of the given side made Radius;

Is to its name, that is Radius;

So is the length of the other given side;

To its name, which will be either Sine, Tangent or Secant.

Having instituted the Proportion, look for the corresponding Logarithms, in the Logarithms for numbers for the length of the sides, and in the Table of Artificial Sines, Tangents and Secants, for the Logarithmic Sine, Tangent or Secant.

Having found the Logarithms of the three given Terms, add together the Log. of the second and third Terms, and from their sum subtract the Log. of the first Term, the Remainder will be the Log. of the fourth Term, which, seek in the Tables and find its corresponding Number or Degrees and Minutes.

See the Introduction to the Table of Logarithms; which should be attentively studied by the Learner before he proceeds any further.

Note. The Logarithm for Radius is always 10, which is the Logarithmic Sine of 90°, and the Logarithmic Tangent of 45°.

The preceding PROPOSITIONS and RULES being duly attended to, the solution of the following CASES of *Rectangular Trigono*metry will be easy.

CASE I.

Fig. 39.

The Angles and Hypothenuse given to find the Legs. Fig. 39.

In the Triangle ABC, given the Hypothenuse AC 25 Rods or Chains; the Angle at A $35^{\circ} 30'$: and consequently the Angle at C $54^{\circ} 30'$: to find the Legs.

Making the Hypothenuse Radius, the Proportions will be :

To find the Leg AB.		To find the Leg BC.	
As Radius	10.00000	As Radius	10.00000
: Hyp. AC, 25	1.39794	: Hyp. AC, 25	1.39794
: : Sine ACB, 54° 30'	9.91069	:: Šine CAB, 35° 30'	9.76395
	11.30863		11.16189
	10.00000		10.00000
: Leg AB, 20.35 -	1.30863	L	1 10100
: Leg AB, 20.35 -	, 1.30003	: Leg BC, 14.52 -	1.16189
	Construction of the local division of the lo		terror of the second se

Note. When the first Term is Radius, it may be subtracted by cancelling the first figure of the Sum of the other two Terms.

Making the Leg AB Radius, the Proportions will be :

To find the Leg AB. As Secant CAB, 35° 30' : Hyp. AC, 25 :: Radius : Leg AB 20 35	To find the Leg BC. As Secant CAB, 35° $30'$: Hyp. AC, 25 : Tangent, CAB, 35° $30'$
: Leg AB, 20.35	: Leg BC, 14.52

Making the Leg BC Radius, the Proportions will be :

To find the Leg AB.	To find the Leg BC.
	10 jind the Leg DU.
As Secant ABC, 54° 30'	As Secant ACB, 54° 30'
: Hyp. AC, 25	: Hyp. AC, 25
:: Tangent ACB, 54° 30'	:: Radius
: Leg AB, 20.35	: Leg. BC, 14.52

The Logarithms of the four last Proportions being looked out, and added and subtracted according to the Rule, the result will be found to be the same as the two first Proportions.

F

By Natural Sines.

This CASE may be solved by Natural Sines,* according to the following Proportions :

As Unity or 1, is to the length of the Hypothenuse, so is the Natural Sine of the smallest Angle, to the length of the shortest Leg. Or, so is the Natural Sine of the largest Angle, to the length of the longest Leg.

Or, which is the same thing, multiply the Natural Sines of the two Angles by the Hypothenuse, the Products will be the length of the two Legs.

EXAMPLE.

Nat. Sine of 35° 30'	Nat. Sine of 54° 30' 0.81412	
Нур. 25	Hyp. 25	
290350 116140	407060 162824	
14.51750	20.35300	
Leg BC 14.52	Leg AB 20.35	

Note. The third Decimal figure in the first Product being 7, the preceding figure may be called one more than it is, viz. 2. And whenever in any Product, &c. there are more places of Decimals than you wish to work with, if the one at the right hand of the last which you wish to retain is more than 5, add a Unit to the last, because a greater number than 5 is more than half.

As the Table of Artificial or Logarithmic Sines, Tangents and Secants, contained in this book, is calculated only for every 5 Minutes of a Degree, whenever any Question is to be solved where the Minutes cannot be found in that Table; or where the length of the Hypothenuse is such a number as cannot be found in the Table of Logarithms for Numbers, the Question may be solved by Natural Sines as above taught.

* See the Introduction to the Table of Natural Sines.

CASE II.

The Angles and one Leg given, to find the Hypothenuse and the other Leg. Fig. 40.

In the Triangle ABC, given the Leg AB 325, the Angle at A 33° 15' and the Angle at C 56° 45': to find the Hypothenuse and the Leg BC.

Making the given Leg Radius, the Proportions will be :

To find the Hypothenuse		To find the Leg BC.	
As Radius,	10.00000	As Radius,	10.00000
: Leg AB, 325	2.51188	: Leg AB, 325	2.51198
: : Sec. CAB, 33° 15'	10.07765	: Leg AB, 325 : : Tan. CAB, 33° 15'	9.81666
: Hyp. 388.6	12.58953	: Leg BC, 213.1	12.32854
			Come to state designed as a second

Note. Reject the first figure, which is the same as subtracting Radius, and seek the numbers corresponding to the other figures.

Making the Leg BC Radius,	the Proportions will be ;
To find the Hypothenuse	To find the Leg BC.
As Tang. ACB, 560 45'	As Tang. ACB, 56° 45'
: Leg AB, 325	: Leg AB, 325
: : Sect. ACB. 56° 45'	: : Radius
: Hyp. 388.6	: Leg BC, 213.1
Making the Hypothenuse Ra	dius, the Proportions will be ;
To find the Hypothenuse.	To find the Leg BC.
As Sine BCA, 56° 45'	As Sine BCA, 56° 45'
: Leg AB, 325	: Leg AB, 325
: : Radius	:: Sine BAC, 33° 15'
: Hyp. 388.6	: Leg BC, 213.

Note. If the Leg BC had been given, instead of the Leg AB, the Proportions would have been the same mutatis mutandis.

By Natural Sines.

To solve this CASE by Natural Sines, institute the following Proportions :

Fig. 40.

325

C

To find the Hypothenuse. As the Natural Sine of the Angle opposite the given Leg, is to the length of the Leg, so is Unity or 1, to the length of the Hypothenuse.

Or, which is the same thing, Divide the given Leg by the Natural Sine of its opposite Angle, and the Quotient will be the Hypothenuse.

To find the other Leg. As the Natural Sine of the Angle opposite the given Leg, is to the length of the given Leg, so is the Natural Sine of the Angle opposite the other Leg, to the length of the other Leg.

EXAMPLE.

Given Leg 325. Nat. Sine of 56° 45', the Angle opposite the given Leg 0.83629. Nat. Sine of 33° 15', the Angle opposite the other Leg 0.54829.

As 0.83629 : 325 : : 1 : 388.6

As 0.83629 : 325 : : 0.54829 : 213.07.

CASE III.

Fig. 41.

50

40

The Hypothenuse and one Leg given, to find the Angles and the other Leg. Fig. 41.

In the Triangle ABC, given the Hypothenuse ΛC 50 and the Leg AB 40, to find the Angles and Leg BC.

Making the Hypothenuse Radius, the Proportion to find the Angle ACB will be :

As Hyp. 50 - : Radius	1.69897
: Radius '	10.00000
:: Leg AB, 40	1.60206
	11.60206
	1.69897
: Sine ACB, 53° 10'	9.90309

The Angle ACB being 53° 10' the other is consequently 36° 50'.

Making the Leg AB Radius, the Angle BAC may be found by the following Proportion;

	As Leg AB,	40	-	
	: Radius		-	Ę
-	:: Hyp. 50	• 1	-	1

1.60206 10.00000 1.69897 29

1.60206

: Sec. BAC, 36° 50' 10.09691

The Angles being found, the Leg BC may be found by either of the preceding CASES. It is 30.

By Natural Sines.

The Angle opposite the given Leg may be found by the following Proportion;

As the Hypothenuse is to Unity or 1, so is the given leg to the Nat. Sine of its opposite Angle.

Or, which is the same thing, Divide the given Leg by the Hypothenuse, and the Quotient will be the Nat. Sine.

EXAMPLE.

The Leg AB 40 divided by the Hypothenuse 50 quotes 0.80000 which looked in the Table of Nat. Sines, the nearest corresponding number of Degrees and Minutes will be found to be 53° 8′, the Angle ACB.

Note. The reason why the Angle as found by Nat. Sines differs 2 Minutes from the Angle as found by Logarithms, is that the Table of Logarithmic Sines, &c. contained in this book, is calculated only for every 5 minutes. By a Table of Logarithmic Sines, &c. calculated for every minute, the Angle will be found the same.

By the Square Root.

In this CASE the required Leg may be found by the Square Boot, without finding the Angles; according to the following PROPOSITION;

In every Right Angled Triangle, the Square of the Hypothenuse is equal to the Sum of the Squares of the two Legs. Hence,

The Square of the given Leg being subtracted from the Square of the Hypothenuse, the Remainder will be the Square of the required Leg.

As in the preceding EXAMPLE; the Square of the Leg AB 40 is 1600; this subtracted from the Square of the Hypothenuse 50 which is 2500, leaves 900, the Square of the Leg BC, the Square Root of which is 30, the length of Leg BC as found by Logarithms.

CASE IV:

Fig. 42.

The Legs given to find the Angles and Hypothenuse. Fig. 42.

In the Triangle ABC, given the Leg AB 78.7 and the Leg BC 89; to find the Angles and Hypothenuse.

Making the Leg AB Radius, the Proportion to find the Angle BAC will be;

As Leg AB, 78.7 : Radius	1.89597 10.00000
-:: Leg BC, 89 -	1.94939
	11.94939
	1.89597
: Tang. BAC, 48° 30'	10.05342

The Angle ACB is consequently 410.30'.

Making the Leg BC Radius, the Proportion to find the Angle BCA will be the same as the above, *mutatis mutandis*.

The Angles being found, the Hypothenuse may be found by CASE II. It is nearest 119.

By the Square Root.

In this Case the Hypothenuse may be found by the Square Root, without finding the Angles; according to the following PROPOSITION.

In every Right Angled Triangle, the sum of the Squares of the two Legs is equal to the Square of the Hypothenuse.

In the above Example, the Square of AB 78.7 is 6193.69, the Square of BC 89 is 7921; these added make 14114.69 the Square Root of which is nearest 119.

By Natural Sines.

The Hypothenuse being found by the Square Root, the Angles may be found by Nat. Sines, according to the preceding CASE.

- Hyp. Leg. BC. Nat. Sine. 119) 89.00000 (74789

83 3

570

476

940

833

1070

The nearest degrees and minutes corresponding to the above Nat. Sine are 48° 24', for the Angle BAC. The difference between this and the Angle as found by Logarithms is occasioned by dividing by 119, which is not the exact length of the Hypothenuse, it being a Fraction too much.

PART II.

OBLIQUE TRIGONOMETRY.

The solution of the two first Cases of Oblique Trigonometry depends on the following PROPOSITION.

In all Plane Triangles, the Sides are in proportion to each other as the Sines of their opposite Angles. That is, as the

Sine of one Angle is to its opposite Side, so is the Sine of another Angle to its opposite Side. Or, as one Side is to its opposite Angle, so is another Side to the Sine of its opposite Angle.

Note. When an Angle exceeds 90° make use of its Supplement, which is what it wants of 180°. As the Sine of 90° is the greatest possible Sine, the Sine of any number of Degrees will be as much less as that number of Degrees, exceeds 90, and will be the same as the Sine of the Supplement of that number of Degrees; thus, the Sine of 100° is the same as the Sine of S0°, and the Sine of 130° the same as the Sine of 50°, &c.

CASE I.

Fig. 47.

The Angles and one Side given, to find the other Sides. Fig. 47.

In the Triangle ABC, given the Angle at B 48°, the Angle at C 72°, consequently the Angle at Λ 60°, and the Side AB 200, to find the Sides AC and BC.

To find the	Side A	C.	To find the S	ide B	C.
As Sine ACB, 72°	-	9.97821	As Sine ACB, 73°	-	9.97821
: Side AB, 200 -	-	2.30103	: Side AB, 200 -	-	2.30103
:: Sine ABC, 48°	•	9.87107	:: Sine BAC, 60°	-	9.93753
		12.17210 9.97821	•		12.32856 9.97821
Side AC, 156 -	-	2.19389	: Side BC, 182 -	-	2.26035

By Natural Sines.

As the Nat. Sine of the Angle opposite the given Side is to the given Side, so is the Nat. Sine of the Angle opposite either of the required Sides to that required Side.

Given Side 200; Nat. Sine of 72°, its opposite Angle, 0.95115; Nat. Sine of ABC 48°, 0.74334; Nat. Sine of BAC 60°, 0.86617.

As 0.95115 : 200 : : 0.74334 : 156 As 0.95115 : 200 : : 0.86617 : 182.

CASE II.

Two Sides, and an Angle opposite to one of them given, to find the other Angles and Side. Fig. 48.

In the Triangle ABC, given the Side AB 240, the Side BC 200, and the Angle at A 46° 30'; to find the other Angles and the Side AC.

To find the Angle	ACB.		
As Side BC, 200	2.30103	Angle at A	46° 30'
: Sine BAC, 46° 30'	9.86056	C	60 30
:: Side AB, 240	2.38021		
	12.24077		107.00
	2.30103	Sum of the three Angles Sum of two	180° 107
: Sine ACB, 60° 30'	9,93974	Sum or two	107
		Angle at B	. 73

The Side AC will be found by CASE I. to be nearest 253. Note. If the given Angle be Obtuse, the Angle sought will be Acute; but if the given Angle be Acute, and opposite a given lesser Side, then the Angle found by the operation may be either Obtuse or Acute. It ought therefore to be mentioned which it is, by the conditions of the question.

By Natural Sines.

As the Side opposite the given Angle is to the Nat. Sine of that Angle, so is the other given Side to the Nat. Sine of its opposite Angle.

One given Side 200, Nat. Sine of 46° 30′, its opposite Angle, 0.72537, the other given Side 240.

As 200 : 0.72537 : : 240 : 0.87044=60° 30'.

н

Fig. 48.

46 30

CASE III.

Fig. 49. C 36[°]40' 240 B

The solution of this Case depends on the following Proro-

Two Sides and their contained Angle given, to find the other Angles and Side. Fig. 49.

SITION. In every Plane Triangle, as the sum of any two Sides is to their difference, so is the Tangent of half the sum of the two opposite Angles to the Tangent of half the difference between them. Add this half difference to half the sum of the Angles and you will have the greater Angle, and subtract the half difference from the half sum and you will have the lesser Angle.

In the Triangle ABC, given the Side AB 240, the Side AC 180, and the Angle at A 36° 40' to find the other Angles and Side.

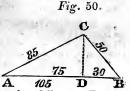
Sum of the tw	vo Sides	420	Dif	ference	60
					240 180

The given Angle BAC 36° 40', subtracted from 180°, leaves 143° 20' the sum of the other two Angles, the half of which is 71° 40'.

As the sum of two Sides, 420			0 6000*
	-		2.62325
: Their difference 60 -		-	1.77815
: : Tangent half unknown Ang. 710	40 ′	-	10.47969
diament of the base		0	12.25784
			2.62325
: Tangent half difference, 23° 20'			9.63459
The half sum of the two unknown	Angles.		710 40'
The half difference between them,			23 20
Add, gives the greater Angle ACB	20	10	95 00
Subtract, gives the lesser Angle AF	BC	- 1 () m	48 20
The Side BC may be found by C	ASE I OF	IF.	

CASE IV.

The three Sides given to find the Angles. Fig. 50.



The solution of this CASE depends on the following PROPO-SITION.

In every Plane Triangle, as the longest Side is to the sum of the other two Sides, so is the difference between those two Sides to the difference between the Segments of the longest Side, made by a Perpendicular let fall from the Angle opposite that Side.

Half the difference between these Segments, added to half the sum of the Segments, that is, to half the length of the longest Side, will give the greatest Segment; and this half difference subtracted from the half sum will be the lesser Segment. The Triangle being thus divided, becomes two Right Angled Triangles, in which the Hypothenuse and one Leg are given to find the Angles.

In the Triangle ABC, given the Side AB 105, the Side AC S5, and the Side BC 50, to find the Angles.

ue DC 50	, to nna th	e Angle	S		
-	85	AC	-		85
- ,	50	BC	-	-	- 50
o Sides	135		Differ	ence	35
					e .
			- .	1	2.02119
ther two	Sides, 135	-	-		2.13033
between f	those Sides	s, 35			1.54407
				-	3.67440
					2.02119
etween th	ne Segmen	ts, 45		1.	1.65321
do AR	1.00		1.0	- 11	52.5
	of the Segr	nents		-	22.5
1. 1. 1. 1. 1.	Marrie So	Contraction of the local division of the loc		1.1	
the great	er Segmen	t AD	-	-	75.0
ves the le	sser Segm	ent BD			30.0
	o Sides est Side A ther two between etween the de AB fference of the great	- 85 50 o Sides 135 est Side AB, 105 ther two Sides, 135 between those Sides etween the Segmen de AB fference of the Segr the greater Segmen	- 85 AC - 50 BC o Sides 135 est Side AB, 105 ther two Sides, 135 between those Sides, 35 etween the Segments, 45 de AB fference of the Segments the greater Segment AD	- 50 BC - o Sides 135 Differ est Side AB, 105 - ther two Sides, 135 - between those Sides, 35 - etween the Segments, 45 de AB - fference of the Segments -	- 85 AC - 50 BC - 50 BC - 50 BC

Thus the Triangle is divided into two Right Angled Triangles, ADC and BDC; in each of which the Hypothenuse and one Leg are given to find the Angles.

To find the	Ang	le D		To find th	e Ang	le D	CB.
As Hyp. AC, 85		•	1.92942	As Hyp. BC, 50		-	1.69897
: Radius -	-	-	10.00000	: Radius -	•	•	10.00000
:: Seg. AD, 75	•	-	1.87506	:: Seg. BD, 30	-	4	1.47712
			11.87506				11.47712
			1.92942		-		1.69897
DOL DOL			0.04504				
: Sine DCA, 61°	55'	-	9.94564	: Sine DCB, 36°	50'		9.77815
							and the second second second

The Angle DCA 61° 55' subtracted from 90° leaves the Angle CAD 28° 5'.

The Angle DCB 36° 50' subtracted from 90° leaves the Angle CBD 53° 10'.

The Angle DCA 61° 55' added to the Angle DCB 36° 50' gives the Angle ACB 98° 45'.

This Case may also be solved according to the following PROPOSITION.

In every Plane Triangle, as the Product of any two Sides containing a required Angle is to the Product of half the sum of the three Sides, and the difference between that half sum and the Side opposite the Angle required, so is the Square of Radius to the Square of the Co-Sine of half the Angle required.

Those who make themselves well acquainted with TRIGONO-METRY will find its application easy to many useful purposes, particularly to the mensuration of Heights and Distances; called ALTIMETRY and LONGIMETRY. These are here omitted, because, as this work is designed principally to teach the Art of common FIELD-SURVEYING, it was thought improper to swell its size, and consequently increase its price, by inserting any thing not particularly connected with that Art.

It is recommended to those who design to be Surveyors to study TRIGONOMETRY thoroughly; for though a common field may be measured without an acquaintance with that Science, yet many cases will occur in practice where a knowledge of it will be found very beneficial; particularly in dividing Land, and ascertaining the boundaries of old Surveys. Indeed no one who is ignorant of TRIGONOMETRY, can be an accomplished Surveyor.

SURVEYING,

SURVEYING is the Art of measuring, laying out, and dividing Land.

PART I.

MEASURING LAND.

The most common measure for Land is the Acre; which contains 160 Square Rods, Poles or Perches; or 4 Square Roods, each containing 40 Square Rods.

The instrument most in use, for measuring the Sides of Fields, is GUNTER'S Chain, which is in length 4 Rods or 66 Feet; and is divided into 100 equal parts, called Links, each containing 7 Inches and 92 Hundredths. Consequently, 1 Square Chain contains 16 Square Rods, and 10 Square Chains make 1 Acre.

In small Fields, or where the Land is uneven, as is the case with a great part of the Land in New-England, it is better to use a Chain of only two Rods in length; as the Survey can be more accurately taken.

SECTION I.

PRELIMINARY PROBLEMS.

PROBLEM I. To reduce Two Rod Chains to Four Rod Chains.

Rule. If the number of Two Rod Chains be even, take half the number for Four Rod Chains, and annex the Links if any: thus, 16 Two Rod Chains and 37 Links make 8 Four Rod Chains and 37 Links.

But if the number of Chains be odd, take half the greatest even number for Chains, and for the remaining number add 50 to the Links : Thus, 17 Two Rod Chains and 42 Links make 8 Four Rod Chains and 92 Links.

PROBLEM II. To reduce Two Rod Chains to Rods and Decin. al Parts.

RULE. Multiply the Chains by 2, and the Links by 4, which will give Hundredths of a Rod: thus, 17 Two Rod Chains and 21 Links make 34 Rods and 84 Hundredths; expressed thus, 34.84 Rods.

If the Links exceed 25, add 1 to the number of Rods and multiply the excess by 4: thus, 15 Two Rod Chains and 38 Links make 31.52 Rods.

PROBLEM III. To reduce Four Rod Chains to Rods and Decimal parts.

RULE. Multiply the Chains, or Chains and Links, by 4; the Product will be Rods and Hundredths : thus, 8 Chains and 64 Links make 34.56 Rods.

Note. The reverse of this Rule, that is, dividing by 4, will reduce Rods and Decimals to Chains and Links : thus, 105.12 Rods make 26 Chains and 28 Links.

PROBLEM IV. To reduce Square Rods to Acres.

RULE. Divide the Rods by 160, and the Remainder by 40, if it exceeds that number, for Roods or Quarters of an Acre: thus, 746 Square Rods make 4 Acres, 2 Roods, and 26 Rods.

PROBLEM V. To reduce Square Chains to Acres.

Rule. Divide by 10; or, which is the same thing, cut off the Right hand figure: thus, 1460 Square Chains make 146 Acres; and 846 Square Chains make 84 Acres and 6 Tenths.

PROBLEM VI. To reduce Square Links to Acres.

RULE. Divide by 100000; or, which is the same thing, cut off the 5 Right-hand figures : thus, 3845120 Square Linksmake 38 Acres and 45120 Decimals.

Note. When the Area of a Field, by which is meant its Superficial Contents, is expressed in Square Chains and Links, the whole may be considered as Square Links, and the number of Acres contained in the Field, found as above. Then multiply the figures cut off by 4, and again cut off 5 figures, and you have the Roods; multiply the figures last cut off by 40, and again cut off 5 figures, and you have the Rods.

EXAMPLE. How many Acres, Roods, and Rods, are there in 156 Square Chains and 3274 Square Links?

15)63274 Square Links,

2)53096 40 21)23840

Answer. 15 Acres 2 Roods and 21 Rods.

PROBLEMS for finding the Area of Right Lined Figures, and also of Circles.

PROBLEM VII. To find the Area of a Square or Parallelogram.

RULE. Multiply the length into the breadth; the Product will be the Area.

PROBLEM VIII. To find the Area of a Rhombus or Rhomboides.

RULE. Drop a Perpendicular from one of the Angles to its opposite Side, and multiply that Side into the Perpendicular; the Product will be the Area.

PROBLEM IX. To find the Area of a Triangle.

RULE 1. Drop a Perpendicular from one of the Angles to its opposite Side, which may be called the Base; then multiply the Base by half the Perpendicular, or the Perpendicular by half the Base; the Product will be the Area. Or, multiply the whole Base by the whole Perpendicular, and half the Product will be the Area.

RULE 2. If it be a Right Angled Triangle, multiply one of the Legs into half the other; the Product will be the Area. Or, multiply the two Legs into each other, and half the Product will be the Area.

RULE 3. When the three Sides of a Triangle are known, the Area may be found Arithmetically, as follows :

Add together the three Sides; from half their Sum subtract each side, noting down the Remainders; multiply the half Sum by one of those Remainders, and that Product by another Remainder, and that Product by the other Remainder; the Square Root of the last Product will be the Area.

-EXAMPLE. Suppose a Triangle whose three Sides are 24, 20, and 18 Chains. Demanded the Area.

24+20+18=62, the Sum of the three Sides, the half of which is 31. From 31 subtract 24, 20, and 18; the three Remainders will be 7, 11, and 13.

 $31 \times 7 = 217$; $217 \times 11 = 2387$; $2387 \times 13 = 31031$, the Square Root of which is 176.1, or 17 Acres 2 Roods and 17 Rods.

By Logarithms.

As the Addition of Logarithms is the same as the Multiplication of their corresponding Numbers; and as the Number answering to the one half of a Logarithm will be the Square Root of the Number corresponding to that Logarithm: it follows, That if the Logarithm of the half Sum of the three Sides and the Logarithms of the three Remainders be added together,

the Number corresponding to one half the Sum of those Logarithms will be the Area of the Triangle.

The half Sum, 31 -		-	1.49136
The first Remainder, 7 -	-		0.84510
The second Remainder, 11		-	1.04139
The third Remainder, 13	•	-	1.11394
The Square of the Area, 31000	-		4.49179
Area 176 Square Chains	-	110	2.24589

RULE 4. When two Sides of a Triangle and their contained Angle, that is, the Angle made by those Sides, are given, the Area may be found as follows:

Add together the Logarithms of the two Sides and the Logarithmic Sine of the Angle; from their sum subtract the Logarithm of Radius, the Remainder will be the Logarithm of double the Area.

EXAMPLE. Suppose a Triangle one of whose Sides is 105 Rods and another 85, and the Angle contained between them 28° 5'. Demanded the Area.

One Side, 105 -	- 1		-	2.02119
The other Side, 85		•.	- 1	1.92942
Sine Angle, 28° 5' -	•	-	-	9.67280
	• •			13.62341
Subtract Radius -	-	-	-	10.00000
Double Area, 4200 Rods	-	-	÷	3.62341

Answer. 2100 Rods.

Note. Radius may be subtracted by cancelling the Left-hand figure of the Index, or subtracting 10, without the trouble of setting down the Ciphers.

By Natural Sines.

Multiply the two given Sides into each other, and that Product by the Natural Sine of the given Angle; the last Product will be double the Area of the Triangle.

Nat. Sine of the Angle 28° 5' 0.47076

 $105 \times 85 = 8925$, and $8925 \times 0.47076 = 4201$ the double Area of the Triangle.

PROBLEM X. To find the Area of a Trapezoid.

RULE. Multiply half the Sum of the two parallel Sides by the perpendicular distance between them, or the sum of the two parallel Sides by half the perpendicular distance, the product will be the Area.

PROBLEM XI. To find the Area of a Trapezium, or irregular Four Sided Figure.

RULE. Draw a Diagonal between two opposite Angles, which will divide the Trapezium into two Triangles. Find the Area of each Triangle and add them together. Or, multiply the Diagonal by half the Sum of the two perpendiculars let fall upon it, or the Sum of the two perpendiculars by half the Diagonal, the product will be the Area.

Note. Where the length of the four Sides and of the Diagonal is known, the Area of the two Triangles, into which the Trapezium is divided, may be calculated Arithmetically, according to PROF. IX. Rule 3.

PROBLEM XII. To find the Area of a Figure containing more than Four Sides.

RULE. Divide the Figure into Triangles, and Trapezia, by drawing as many Diagonals as are necessary, which Diagonals must be so drawn as not to intersect each other; then find the Area of each of the several Triangles or Trapezia, and add them together; the sum will be the Area of the whole Figure.

Note. A little practice will suggest the most convenient way of drawing the Diagonals; but whichever way they are drawn, provided they do not intersect each other, the whole Area will be found the same.

PROBLEM XIII. Respecting Circles.

RULE 1. If the Diameter be given the Circumference may be found by one of the following proportions: as 7 is to 22, or more exactly, as 113 is to 355, or in Decimals, as 1 is to 3.14159, so is the Diameter to the Circumference.

RULE 2. If the Circumference be given the Diameter may be found by one of the following proportions: as 22 is to 7, or as 355 is to 113, or as 1 is to 0.31831, so is the Circumference to the Diameter.

RULE 3. The Diameter and Circumference being known, multiply half the one into half the other, and the product will be the Area.

RULE 4. From the Diameter only, to find the Area: multiply the Square of the Diameter by 0.7854, and the product will be the Area.

RULE 5. From the Circumference only to find the Area:

multiply the Square of the Circumference by 0.07958, and the product will be the Area.

RULE 6. The Area being given to find the Diameter: divide the Area by 0.7854, and the Quotient will be the Square of the Diameter; from this extract the Square Root, and you will have the Diameter.

RULE 7. The Area being given to find the Circumference : divide the Area by 0.07958, and the quotient will be the Square of the Circumference; from this extract the Square Root, and you will have the Circumference.

SECTION II.

The following CASES teach the most usual methods of taking the Survey of Fields; also, how to protract or draw a Plot of them, and to calculate their Area.

Note. The FIELD Book is a Register containing the length of the Sides of a Field, as found by measuring them with a Chain; also the Bearings or Courses of the Sides, or the Quantity of the several Angles, as found by a Compass or other instrument for that purpose; together with such Remarks as the Surveyor thinks proper to make in the Field.

CASE I.

To survey a Triangular Field.

Measure the Sides of the Field with a Chain, and enter their several lengths in a FIELD BOOK, protract the Field on Paper, and then find the Area by PROB. IX. Rule 1. Or, without plotting the Field, calculate the Area by PROB. IX. Rule 3. Fig. 46.

			1 02 0 100	
FIELD	BOOK.		6. C	
		Chains.	Ň	
AB	-	- 20		
BC	• .	- 24	22	
CA	-	- 18	D CE	
To	find the	Area.	S Va	
		Ch. L.	100 60	
Base BC		24.00	P.	
Half Perp.	AD -	7.34	A	R
	1.4	1	20 Ch.	-
		9600		

9600 7200 16800

Acres 17)61600

Roods 2) 46400 40

Rods 18) 56000

Acres Roods Rods Area 17 — 2 — 18.56

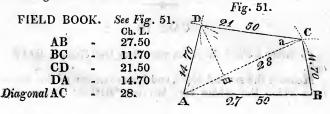
Note. When there are ciphers at the Right Hand of the Links, they may be rejected; remembering to cut off a proper number of figures according to Decimal Rules.

Observe, That in measuring with a Chain, slant or inclined Surfaces, as the Sides of Hills, should be measured horizontally, and not on the Plane or Surface of the Hill; otherwise, a survey cannot be accurately taken. To effect this, the lower end of the Chain must be raised from the ground, so as to have the whole in a horizontal Line; and the end thus raised must be directly over the Point where the Chain begins or ends, according as you are ascending or descending a Hill; which Point may be ascertained by a Plummet and Line.

CASE II.

To survey a Field in the form of a Trapezium.

Measure the several sides, and a Diagonal between two opposite Angles; protract the Field, and find the Area by PROB-LEM XI. Or, without protracting the Field, calculate the Area according to the *Note* at the end of that PROBLEM.



Large Mill and

To protract this Trapezium.

Draw the Side AB the given length; with the Diagonal AC 28 and the Side BC 11.70 describe cross Arches as at C, from A and B as Centres; and the point of intersection will represent that corner of the Field: then, with the Side CD 21.50 and the Side AD 14.70, describe cross Arches as at D, from A and C as Centres; and the point of intersection will represent that corner of the field.

To find the Area.

Perpendicular B a		-	11.34
Dm	1.00	•	11.10
			22.44
Half Diagonal AC	-	-	14.00
e	· · ·		397600 244
and the second second	Ac	res 3	1)416 4
and an and a second s	R	Lood.	1)664 40
		-	

Rods 26)560

Acres Rood Rods: Area 31 — 1 — 26.56

Note. The Perpendiculars need not be actually drawn; their length may be obtained as follows: From the Angle opposite the Diagonal open the Dividers so as when one Foot is in the angular Point, as at B, the other, being moved backwards and forwards, may just touch the Diagonal at a, and neither go the least above or below it; that distance in the Dividers being measured on the Scale will give the length of the Perpendicular.

CASE III.

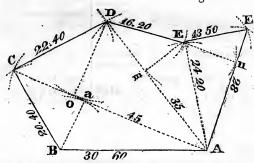
To survey a Field which has more than four Sides, by the Chain only.

Measure the several Sides, and from some one of the Angles, from which the others may be seen, measure Diagonals to

them; draw a Plot of the Field, and find the Area by PROB-LEM XII.

FIELD BOOK. See Fig. 52.

Fig. 52.



AB		-	Ch. L. 30.60			Diago	nals.	
BC	4	-	20.40			0		Ch. L.
CD	-	-	22.40	AC	-	-	-	45.
DE	-	-	16.20	AC	-	-	-	35.
EF	-	-	13.50	AE	-	· -		24.20
FA	-		28.					

To protract this Field.

Draw the side AB, making it the given length 30.60; with the Diagonal AC 45 and the Side BC 20.40, describe cross Arches as at C, from the Points A and B as Centres, and the Point of intersection will represent that Corner of the Field: draw the Side BC and the dotted Diagonal AC; with the Diagonal AD 35 and the Side CD 22.40, describe cross Arches as at D, from the Points A and C, and draw the Side CD and the dotted Diagonal AD. Proceed in this manner till all the Sides, and Diagonals are drawn.

To find the Area.

The Field, being plotted, may be divided into one Trapezium and two Triangles; the Area of which is calculated as follows :--

The Trape.	zium ABCD.		The Tr	iangle	ADE.	
Perpend. B a	1 1	11.68 17.10	Half Perp. E m Diag. AD		-	4.90 35
Half Diag. AC	1.	28.78 22.50			,	2450 1470
· *		143900 5756 5756	Square Chains		-	171.50
Square Chains	- 6	47.5500		-		
The Tri	angle AFE.		Trap. ABCD	-	-	647.55.
Perpend. E n		11.65	Triangle ADE	-	-	171.50
Half Side AF		14	Triangle AFE	-	•	163,10
		4660 1165	1		Acres	98)2 15 4
Square Chains	• ~~	163.10			Roo	ds .860 40
Acres Roos	ds Rods					-
.1rea 98 — 0	- 34.4				Rod	ls 34)400

REMARKS.

As each of the Sides of the several Triangles, into which the preceding Plot of a Field is divided, is known from the Field Book, the Area of the Field may be calculated Arithmetically, by finding the Area of each Triangle, according to PROB. IX. Rule 3; and then adding the whole together. This method, though it may require more time, is preferable to the other, because more accurate. : Indeed it is always better to calculate the Area of a Field Arithmetically than Geometrically; for in the former; no two persons) can differ in their calculations; whereas, according to the latter, which is the common method of casting the contents of a Field, it is hardly to be expected that any two persons will perfectly agree. The inaccuracy of Scales, and the difficulty of determining with precision the length of Sides and Perpendiculars with a Scale and Dividers, render it almost if not quite impossible to obtain the exact Area of a Field, in the method commonly practised, even if the Surveyor has measured it accurately in the first place.

Other methods of taking the Survey of a Field by the Chain only are mentioned in some Treatises on this subject, but they

are rather curious than useful; and it is much better to ascertain the Angles by an accurate Compass, or some instrument designed purposely for taking Angles.

CASE IV.

To Survey a Field with a Chain and Compass.

Measure the length of the Sides with a Chain, and take their bearing or Course with a Compass;* enter these in a Field Book; plot the Field on paper, and calculate the Area by the directions already given.

To protract or draw a Map of a Field.

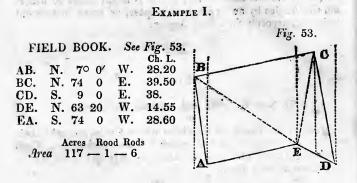
Draw a Line to represent a Meridian, or North and South Line, from which lay off a Bearing or Course of the first Side of the Field, with a Protractor or from a Line of Chords; and from a Scale of equal parts, measure the length of the Side and draw a Line to represent it.

At the end of this Line draw a Line parallel to the Meridian Line, and then lay off the second Side of the Field as before taught; proceed in the same manner to draw parallel Lines, and lay off the several Sides till the whole is protracted.

In protracting a Field, let the top of the paper be considered as North, the bottom South, the right hand East, and the left hand West; lay the Course to the right or left of the Meridian Line, according as it is East or West, and from the upper or lower part of the Line, according as it is North or South.

In all protractions, if the end of the last distance falls exactly on the point from which you began, the Course also being right, the Field work and protraction are truly taken and performed; if not, an error must have been committed in one of them: in such cases, make a second protraction; if this agrees with the former, it is to be presumed the fault is in the Field work; a re-survey must then be taken.

* A Compass may be so constructed with two Indexes, one moveable and the other fixed, as to ascertain the Angle made by two Sides, without reference to the Bearing of those Sides. Such a Compass would be particularly useful in surveying Land where there are mineral substances which have an influence upon the Compass Needle, attracting it one way or the other, and thus rendering it impossible to take a Course by it with precision.



REMARKS.

The Sides of the several Triangles into which the Plot of a Field is divided may be found by Trigonometry; and then the Area of each Triangle may be calculated according to PROB. IX. Rule 3. The Sum of the Areas of the several Triangles will be the Area of the whole Field. This method may require more time, but it is perfectly accurate, since no dependence is placed on the uncertain measurement of Scale and Dividers.

In the preceding EXAMPLE, suppose the Field divided into three Triangles. See Fig. 53. In the Triangle EAB, the Sides EA and AB are known from the FIELD BOOK, and their contained Angle is known from the Bearing of the Sides. The other Angles and the Side EB may be found by OBLIQUE TRIGONOME-TRY, CASE III.; and then there will be the three Sides to find the Area. In the Triangle EBC, the Side BC is known from the FIELD BOOK, and the Side EB is found as above mentioned ; the Angle EBA is also found as above; this subtracted from the Angle ABC, which may be found from the bearing of the Sides AB and BC, will leave the Angle EBC : there will then be the two Sides and their contained Angle to find the third Side; and this being found, there will be the three Sides to find the Area. In the Triangle EDC, the Sides DE and DC are known from the FIELD BOOK, and their contained Angle is known from the bearing of the Sides. The Side EC and the Area may be found as above.

It is recommended to the Learner to make these calcula-

tions, as it will improve him in the knowledge of Trigonometry.

Note. Two Sides and their contained Angle being given, the Area may be found by PROB. IX. Rule 4.

Another Method of protracting Fields.

Without drawing parallel Lines at the end of each Side, a Field may be protracted by the Angles made by the several Sides; and the Angle made between any two Sides may be found by the following RULES.

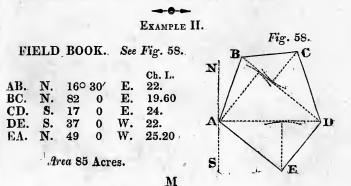
RULE 1. If the course or bearing of one of the Sides is northerly and the other southerly, one easterly and the other westerly, subtract the less Course from the greater, the remainder will be the Angle between them.

RULE 2. If one is northerly and the other southerly, and both easterly or westerly, add both Courses together; the sum will be the Angle between them.

Rule 3. If both are northerly or southerly, and one easterly and the other westerly, subtract the sum of both from 180° ; the remainder will be the Angle between them.

RULE 4. If both are northerly or southerly, and both easterly or westerly, add 90° , the less Course, and the Complement of the greater together; the sum will be the Angle between them.

To protract a Field according to the preceding Rules is preferable to the method of doing it by parallel Lines, though it may not be so easy to the Learner at first. It is difficult to draw parallel Lines with perfect accuracy, particularly without a parallel Rule; and a small deviation from a true Line may make considerable difference in the Plot of a Field.



To draw a Plot of this Field, according to the preceding RULES.

Having drawn the Side AB, according to the directions before given for laying off the first Course and Distance, compare the first and second Courses together, and they will be found to be both northerly and both easterly; consequently, the Angle between them is found by Rule 4, as follows: 90° added to 16° 30' the less Course, and 8° the Complement of the greater, the sum is 114° 30', for the Angle at B. Compare the second and third Courses, and they will be found to be one northerly and one southerly, and both easterly; consequently, according to RULE 2, 82° the second Course added to 17° the third Course, the sum 99° is the Angle at C. The third and fourth Courses are both southerly, and one easterly and the other westerly. -The Angle between them at D is 126°; for 17° the third Course added to 37° the fourth Course is 54°, which subtracted from 180° leaves 126°, according to RULE 3. The fourth and fifth Courses are one southerly and the other northerly, and both westerly. According to RULE 2, 37° the fourth Course added to 49° the fifth Course, the sum 86° is the Angle at E.

A little practice will render this mode of protracting a Field familiar and easy, and an attention to the Courses will show in what direction the Angle is to be made.

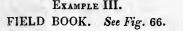
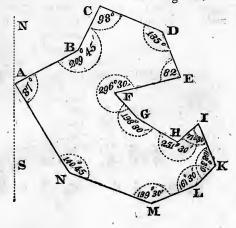


Fig. 66.



			. 24		Ch. L.
AB.	N.	560	15'	Ε.	21.60
BC.	N .	26	30	· E.	13.44
CD.	S.	71	30	E.	18.96
DE.	S	26	30	Ε.	13.44
EF.	S.	71	30	W.	18.96
• FG.	S.	45	-0	E.	8.47
GH.	S.	63	30	E.	13.44
HI.	N.	45	0	E.	8.47
IK.	S.	26	30	Ε.	13.44
KL.	S.	45	0	W.	8.47
LM.	S.	63	30	W.	13.44
MN.	N.	76	0	W.	24.73
NA.	N.	36	45	W.	30.
Acres R		Rods			
167	1	30			

The above Field may be protracted, and its Area calculated according to the directions given in the preceding EXAMPLES.

-

Area

Several Field Books to exercise the Learner in plotting Fields and calculating their Area.

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
2.N. 37 30E.16010.N. 22 30E.14.3.East12011.S. 76 45E.12.4.S.11 0E.20012.S.15 0W.10.855.South21613.S.16 45W.10.126.West160Acres Roods Rods.Area 7042 238.N.38 15W.136Area 110-2 - 239.Area 744-3 - 281.S.65°40'W.49.7
3.East12011.S.7645E.12.4.S.110E.20012.S.150W.10.855.South21613.S.1645W.10.126.West160Acres Roods Rods.Acres Roods Rods.Area $110 - 2 - 23$ 8.N.3815W.136Area $110 - 2 - 23$ 8.Acres Roods Rods.Area $744 - 3 - 28$ 1.S.65°40' W.49.7
4.S.110E.20012.S.150W.10.855.South2166.West1607.S.3630W.1607.S.3630W.1608.N.3815W.136Acres Roods Rods $Area$ 744 - 3 - 28No. III.Rods. $Area$ 744 - 3 - 281.S.65°40'W.49.7
5. South 216 13. S. 16 45 W. 10.12 6. West 160 Acres Roods Rods. 7. S. 36 30 W. 160 Area 110 - 2 - 23 8. N. 38 15 W. 136 Acres Roods Rods. Acres Roods Rods. No. III. Rods. Area 744 - 3 - 28 1. S. 65°40' W. 49.7
6. West 160 7. S. 36 30 W. 160 8. N. 38 15 W. 136 Acres Roods Rods Acres Roods Rods Area 110 - 2 - 23 No. III. Rods. 1. S. 65°40' W. 49.7
7. S. 36 30 W. 160 Area Area 110 2 23 8. N. 38 15 W. 136 Image: Constraint of the second
S. N. 38 15 W. 136 Acres Roods Rods No. III. Rods. Area 744 — 3 — 28 I. S. 65°40' W. 49.7
Acres Roods Rods No. III. Rods. Area 744 - 3 - 28 1. S. 65°40' W. 49.7
Area 744 - 3 - 28 1. S. 65°40' W. 49.7
No. II. Ch. L. 3. S. 54 0 W. 17.9
1. N. 75° 0' E. 13.70 4. S. 20 0 W. 5.8
2. N. 20 30 E. 10.30 5. S. 7 30 E. 29.4
3. East 16.20 6. N. 83 0 E. /107.4
4. S. 33 30 W. 35.30 7. N. 5 50 W. / 22.
5. S. 76 0 W. 16. 8. N. 18 30 W. 46.
6. North 9. Acres Rood Rods.
7. S. 84 0 W. 11.60 Area 34 - 1-19

		No. IV	2.5	Rods.					Rods.
1.	N.	430 0'	W.	12.44	16.	N.	18030	/ W.	39.
2.	N.	64 0	W.	8.	17.	N.	86 .5	E.	26.7
3.	N.	52 0	W.	14.60			cres R		
4.	N.	37 5	W.	51.36		Arec	48	1 - 1	2
5.	N.	15 30	W.	21.76		• • • • •		-	
6.	N.	20 40	W.	44.60			No. V	II.	Ch. L.
7.	N.	88 20	E.	167.60	1.	N.	0045		9.
8.	S.	34 40	Ē.	71.20	2.	N.	19 30		5.35
9.	ŝ.	75 0	w.	69.72	3.	N.	23 0		4.09
10.	S.	55 0	W.	64.60	4.	N.	41 35		6.15
11.	S.	25 0	W.	18.12	5.	N.	3 (36.75
		cres Roo			6.	S.	86 50		13.33
		97 - 2			7.	N.	2 15		17.65
		4	•	-	8.	N.	85 45	5 E.	12.56
		No. V		Rods.	9.	S.	2 10		8.
1.	S.	11050'	W.	34.6	10.	N.	86 45	E.	7.38
2.	S:	63 20	E.	93.6	11.	S.	3 15		13.20
3.	N.	4 0	W.	34.9	12.	N.	87 0	E.	29.92
4.	S.	89 55	E.	40.1	13.	N.	49 20	E .	4.04
5.	N.	5 20	W.	35.5	14.	No	rth		2.23
6.	N.	69 40	W.	60.	15.	N.	50 35	Е.	6.50
7.	S.	78 0	W.	30.6	16:	S.	22 50		17.94
8.	N.	67 20	W.	1.2	17.	S.	34 0		3.50
9.	S.	72 30	W.,	10.4	18.	S.	41 0	W.	3.
10.	S.	66 55	W.	15.2	19.	S.	22 50	· W.	9.25
		cres Roc	d Ro	ds.	20:	S.	3 40	E .	2.64
		41 - 1			21.	S.	86 0	W.	2.50
					22.	S.	0 25	W.	14.50
		No. VI	ŀ.	Rods.	23.	S.	2 (5.38
1.	S.	340 0'	Ε.	42.8	24.	S.	10 0) E.	. 11.75
2.	S.	29 0	E.	69.4	25.	S.	86 0		34.60
3.	S.	64 50	W.	53.			Acres F	loods]	Rods
4.	S.	25 0	Е.	4.		Arec	268 -	- 3	7
5.	S.	66 30	W.	,89.		1.00		_	
6.	N.	25 0	w.	4.			No. V	III.	Rods
7.	S.	64 45	w.	32.2	1.	S.	6030	E.	19.1
8.	N.	30 30	W.	18.3	2.	S.	63 30	Е.	14.36
9.	N.	56 30	Ε.	34.5	3.	S.	67 0	E.	10.68
10.	N.	64 0	Ε.	12.5	4.	N.	88 0	E.	13.3
11.	N.	49 0	Ε.	14.	5.	S.	31 30	w.	32.44
12.	N.	26 10	w.	19.3	6.	S.	31 55	W.	96.5
13.	N.	21 0	W.	18,3	7.	S.	33 25	W.	34:9
14.	N.	44 10	W.	18.	8.	S.	20 45	. E.	3.68
15.	N.	4 40	E.	30.5	1	S.	16 15		64.
¥.0.		01 TU	11,	00.0	0.	N.	10 10		011

10.	N.	52	030	w.	12.8	21.	N.	36	0 0'	E.	41.56
11.	S.	45	0	W.	18.24	22.	S.	68	0	E.	80.6
12.	S.	69	0	W.	21.4	23.	N.	44	30	E.	20.4
13.	S.	12	40	W.	9.4	24.	N.	2	30	W.	41.
14.	S.	84	20	W.	9.5	25.	N.	14	45	W.	62.32
15.	N.	22	15	W.	24.	26.	N.	16	0	W.	14.8
16.	No	th	- 3	• •	9.8	27.	N.	1	45	W.	14.8
17.	N.	29	15	W	30.6	28.	N.	82	30	W.	99.
18.	N.	44	25	W	21.8	nel j	- 2		e		
19.	N.	61	30	W	23.1	124	A	cres	Rood	Rode	5
20.	N.	41	0	W	10.8	A	rea 1	35 -	- 1 -	- 15	

CASE V.

To survey a field from one station, at any place within the Field, from which the several Angles may be seen.

Take the Bearing of the Angles, and measure their Distance from the Station.

FIELD BOOK. See Fig. 61.

Fig. 61.

From Station to	A.	N.	200	w.	Ch. L. 8.70	
		N.			10	
					11.40	
	D.				10.50	
	E.				12.	
		N.			8,78	
	m.			.7 .	779 7 7	

To protract this Field.

Draw a Meridian Line as N. S. From some point in that Line as a Centre lay off the Bearing and Distance to the several Angles, and draw Lines from one Angle to another, as AB, BC, CD, &c.

To find the Area.

The Area may be calculated according to PROB. XII. by measuring Diagonals and Perpendiculars; or more accurately according to PROB. IX. Rule 4.

As the Bearing and Distance of the Lines from the Station to the several Angles are known, two Sides and their contained Angle are given in each of the Triangles into which the Plot is divided; the Area may, therefore, be readily calculated by the *Rule* above referred to.

Note. As in the operation, the Logarithm of Radius is to be subtracted from the Sum of the other Logarithms, it may be done by rejecting the Left-hand figure, without the trouble of putting down the Ciphers and subtracting.

Triangle aAB.		Think als opt	
aA, 8.70	0.93952	aD, 10.50 Triangle aDE.	1.02119
aB, 10	1.00000	aE, 12	1.07918
Sine AaB, 80°	9.99335	Sine DaE, 75°	9.98494
Sine Mab, ou	0.00000	Sine Dale, 75	3.30434
Doub. Area, 85.7 -	1.93287	Doub. Area, 122 -	2.08531
Triangle aBC.	1.00	Triangle aEF.	
aB, 10	1.00000	aE, 12	1.07918
aC, 11.40	1.05690	aF, 8.78	0.94349
Sine BaC, 27°	9.65705	Sine EaF, 55°	9.91336
Doub. Area, 51.8 -	1.71395	Doub. Area, 86.3 -	1.93603
miles CD			-
Triangle aCD.	+ 05000	Triangle aFA.	0.04940
aC, 11.40	1.05690	aF, 8.78	0.94349 0.93952
Sine CaD, 78°	9.99040	aA, 8.70	0.93952 9.84948
Sine CaD, 78	9.99040	Sine FaA, 45°	9.84946
Doub. Area, 117 -	2.06849	Doub. Area, 54	1.73249
Triangle aAB	Sec. 1	85.7	
	11.0		
aBC		51.8	
aCD		117.	
aDE		122.	
aEF		86.3	
aFA	_	54.	
Double Area		516.8	
isouble Area		010.0	- 2
		25204	-
Area	-	25)84	

SURVEYING,

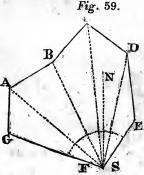
14)40

Acres Roods Rods Area 25 — 3 — 14.4

CASE VI.

To survey a Field from some one of the Angles, from which the others may be seen.

From the stationary Angle take the Bearing and Distance to each of the other Angles, with a Compass and Chain.



FIELD BOOK. See Fig. 59.

	4			Ch. L.
FG.	N.	700	W.	14.60
FA.	N.	50	W.	18.20
FB.	N.	30	W.	16.80
FC.	N.	10	W.	21.20
FD.	N.	7	Е.	16.95
FE.	N.	30	E .	8.50
To	dagan	~ D]	A . C	17 . 17

To draw a Plot of this Field.

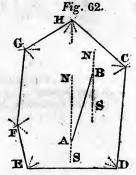
Draw a Meridian Line to pass through the stationary Angle as at F. From the Point F, lay off the Bearing and Distance to the several Angles, and connect them by Lines, as FG, FA, FB, &c.

The Area may be calculated as taught in the preceding CASE.

CASE VII.

To survey a Field from two Stations within the Field, provided the several Angles can be seen from each Station.

Find the Bearing from each Station to the respective Angles; and also the Bearing and Distance from one Station to the other.



FIELD BOOK. See Fig. 62.

	First	t Stati	on.			Second Station.						
AC.	N.	380	30'	E.			BC.	S.	820	0'	E.	
AD.	S.	69	0	Е.			BD.	S.	17	0.	E.	
AE.	S.	59	0	W.			BE.	S.	28	0	W.	
AF.	N.	63	0	W.			BF.	S.	49	0	W.	
AG.	N.	21	0	W.			BG.	N.	76	0	W.	
AH.	No	rth.					BH.	N.	24	0	W.	
	6	Statio	nom	Tino	IR N	140	T 00	Cho	ina			

tationary Line AB. N. 14° E. 20 Chains.

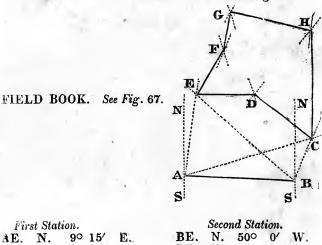
To protract this Field.

At the first Station A, draw a Meridian Line and lay off the Bearings to the respective Angles; draw the Stationary Line AB, according to the Bearing and Distance; at B, draw a Meridian Line parallel to the other, and lay of the Bearings to the Angles, as taken from this Station; from each Station draw Lines through the Degree which shows the Bearing of each Angle, as marked by the Protractor or Line of Chords, and the Points where those Lines intersect each other will be the Angles of the Field. Connect those angular Points together by Lines, and those Lines will represent the several Sides of the Field.

CASE VIII.

To Survey an inaccessible Field.

Fix upon two Stations, at a convenient distance from the Field, from each of which the several Angles may be seen; from each Station take the Bearing of the Angles; and take the Bearing and Distance from one Station to the other. Fig. 67.



AE.	N.	90	15'	E.,		BE.	Ν.	500	0'	W.
AF.	N.	16	0	Ε.		BF.	N.	29	15	W.
AG.	N.	14	30	Е.		BD.	N.	24	0	W.
AD.	N.	39	0	Ε.		BG.	N.	21	30	W.
AH.	N.	40	0	E.	9	BH.	N.	5	0	Ε.
AC.	N.	72	0	Ε.		BC.				
								Ch.	L.	

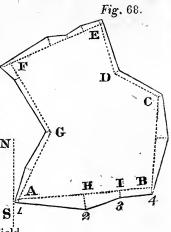
Stationary Distance AB, S. 88° 30' E. 19.20.

The directions given in the last CASE for plotting the Field, will apply in this CASE also; and the Area in this and the preceding CASE may be calculated in the manner pointed out in CASE IV. by dividing the Plot into Triangles and measuring Diagonals and Perpendiculars. Or the Sides may be found by Trigonometry, and the Area calculated Arithmetically, as already taught.

CASE IX.

To survey a Field where the boundary Lines are very irregular, without noticing with the Compass every small Bend.

Begin near one corner of the Field, as at A, Fig. 68. and measure to the next large Corner, as B, in a straight Line; noticing also the Bearing of From the Line this Line. take Offsets to the several Bends, at Right Angles from the Line; noticing in the FIELD BOOK at what part of N the Line they are taken, as at A 1, H 2, I 3, B 4. Proceed in the same manner round the Field. In the Figure the dotted Lines represent the stationary Lines, and the black Lines the Boundaries of the Field.



FIELD BOOK.

Bearing and Dist	ance,	Offsets	Bearing and	Distance.	Offsets
	Ch. L.	Ch. L.		Ch. L.	Ch. L.
AB. N. 85° 0' E.	11.20	0.56	EF. S. 379 50'	W. 8.20	0.40
	at 5.40	1.40		at 1.4	
	8.26	0.36		2.96	0.33
	the end	0.36		5.88	1.
				the end	0.12
BC. N. 7º 20' E.	7.96	0.20			
	at 2.36	0.36	FG. S. 27º 40'	E. 7.06	1.20
	4.28	0.96		at 2.	0.24
	the end	0.30	· ·	the end	0.16
CD. N. 62º 0' W.	4.68		GA. S. 25º 20'	W. 6.48	
	at 4.34	0.30		' at 3.80	
				the end	0.40
DE. N. 11º 10' W	. 4.20	0.30	d		

To protract this Field.

Draw the stationary Lines according to the directions in C_{ASE} IV. From A make an Offset of 56 Links to I; measure from A to H 540 Links and make the Offset H 2, 140 Links; measure from A to I 826 Links and make the Offset I 3, 36 Links: at B make the Offset B 4, 36 Links. Proceed in the same manner round the Field, and connect the ends of the Offsets by Lines, which will represent the Boundaries of the Field.

To find the Area.

Find the Area within the Stationary Lines as before taught; then of the several small Trapezoids, Parallelograms and Triangles made by the stationary Lines, Offsets and boundary Lines, and add the whole together : thus, add 56 Links the Offset A I to 140 Links the Offset H 2 and multiply their sum 196 by half 540 the length of the line AH, and the Product 52920 Square Links will be the Area of the Trapezoid AH 21 : again, add 140 the Offset H 2 to 36 the Offset I 3 and multiply their Sum 176 by half 286 the length of the Line HI, and the product 25168 Square Links will be the Area of the Trapezoid HI 32. Proceed in the same manner to calculate the Area of all the Trapezoids, Triangles, &c.

CASE X.

To survey a Field by taking Offsets both to the Right and Left; that is, within and without the Field, as occasion shall require, in consequence of the Stationary Lines crossing the boundary Lines : also, by Intersections, that is, taking the bearing of an inaccessible Corner from two Stations.

The directions given in the preceding CASE, together with the following FIELD BOOK, will show the Learner how to survey a Field like the following, and also to protract it when surveyed.

Fig. 69.

10

N

FIELD BOOK. See Fig. 69.

Offsets to the Left.	Bearing and Dist	ance.	Offsets to the Right.	Remarks.
Ch. L. 1.12 3.40 1.25		Ch. L. 22.12 at 4.25 7.40 13.	Ch. L.	A Tower bears from A. N. 48° W.
0.45	BC. N. 27º 45' W.	21.12 at 4.10 10.25 15.	1.20 1.15	From B the Tower bears N. 38° 30' E.
	C 1. S. 82° 15' E. 1, 2. N. 70 0 E. 2 D. N. 20 0 E.			From C go into the Field to 1, on account of some impediment on on near the boundary Line. At D, you get into another Corner of the Field.
1	DF. S. 35° 0' E.	15.15		E, an inaccessible Corner, bears from D. S. 65° 30' E.
2.20 2.32		15.10 at 1.20 7.45 12.25	0.36	E, the inaccessible Corner bears from F N. 4º W.

в

Note. To draw a Tree, House, Tower, or any other remarkable object, in its proper place, in the Plot of a Field—From any two stations, while surveying the Field, take the bearing of the object, and the intersection of the Lines, which represent the bearings, will determine the place of the object, in the same manner that the Tower is drawn in the Figure.

60

To find the Area of the above Field.

Find the Area within the stationary Lines, and then of the several small Trapezoids, &c. remembering to distinguish those without the stationary Lines from those which are within. Subtract the Area of those within the stationary Lines from the Area of those without, and add the Remainder to the Area contained within the stationary Lines; the sum will be the whole Area of the Field.

SECTION III.

RECTANGULAR SURVEYING, or an accurate method of calculating the Area of a Field Arithmetically, from the FIELD BOOK, without the necessity of protracting it and measuring with a Scale and Dividers, as is commonly practised.

I. Survey the Field in the usual method with an accurate Compass and Chain, and from the FIELD BOOK set down, in a Traverse Table, the Course or Bearing of the several Sides, and their length in Chains and Links, or Rods and Decimal parts of a Rod; as in the 2d and 3d Columns of the following EXAMPLE.

		00	1	6	61	#	ω	N	1	NO.
		8N. 38 15 W.	S. 36 30 W.	6 West	5 South	S. 11 0 E.	3 East	N. 37 30 E.	1 N. 15° 0' E.	Courses
		34	40	40	54	50	30	40	88	ch
100.40	135.70	26.70 26.65	-	5				31.73 31.66	77.27 77.15	N.
133.40 133.40 34.12 34.12	135.70 135.23 84.60 84.84	:	32.15 32.21	:	54. 0 54.10	49.08 49.15				s.
154.12	84.60					9.54 9.56	30. 0 30.04	24.35 24.38	20.71 20.74	E.
104.12	84.84	21.05	23.79	40. 0 39.95						W.
-			21.02	44.77	84.72	S4.72	75.16	45.12	20.74	1 Dep. Col.
		0. 0 21.02	65.79	129.49	169.44	159.88	120.28	65.86	20.74	1 Dep. 2 Dep. Col. Col.
-	4245.4016	560.1830						2085.1276	20.74 1600.0910	North Areas
	4245.4016 19143.9019		2119.0959		• 9166.7040	7858.1020	-			South Areas

19143.9019 Sum of South Areas 4245.4016 North Do.

2)14898.5003 Double Area of the Field.

Acres 744)92501

Roods 3)70004 40

Rods 28)00160

Acres Roods Rods Area 744 — 3 — 28

2. Calculate by RIGHT ANGLED TRIGONOMETRY, CASE 1, or find by the Table of Difference of Latitude and Departure,* or by the Table of Natural Sines,† the northing or southing, easting or westing, made on each Course, and set them down against their several Courses, in their proper Columns, marked N. S. E. W.

Note. To determine whether the Latitude and Departure for any particular Course and Distance are accurately calculated, square each of them; and if they are right, the Sum of their Squares will equal the Square of the distance, for the following reason: the Latitude and Departure represent the two Legs of a Right Angled Triangle, and the Distance the Hypothenuse; and it is a Mathematical truth, that the Square of the Hypothenuse of any Right Angled Triangle is equal to the Sum of the Squares of the two Legs.

3. If the Survey has been accurately taken, the sum of the northings will equal the southings, and the eastings will equal the westings. If, upon adding up the respective Columns, these are found to differ very considerably, the Field should be again surveyed; as some error must have been committed, either in taking the Courses or measuring the Sides. If the difference is small, a judicious, experienced Surveyor will judge from the nature of the ground or shape of the Field surveyed, where the mistake was most probably made, and will correct accordingly. Or, the northings and southings and the eastings and westings may be equalled by balancing them, as follows; subtract one half the difference from that Column which is the largest, and add the other half to that Column which is the smallest; and let the difference, to be added or subtracted, be divided among the several Courses, according to their length.

In EXAMPLE I. the upper numbers are the northings, &c. as found by a Table of Difference of Latitude and Departure. The several Columns being added, the northings are found to exceed the southings 47 Links, and the westings to exceed the eastings 24 Links. They may be balanced by taking 24 Links from the northings, and adding 23 Links to the southings; and taking 12 Links from the westings, and adding 12 Links to the eastings. Take from the first Course of the northings 12 Links, from the second 7, and from the third 5; to the first southing add 7 Links, to the second 10, and to the third 6: add to the first easting 3 Links, to the second 3, to the third 4, and to the

* For an explanation of this Table, and the manner of using it, see the remarks preceding the Table.

f See the Remarks preceding the Table of Natural Sings.

fourth 2; take from the first westing 5 Links, from the second 4, and from the third 3. The lower numbers will then represent the northings, &c. as balanced.

4. These Columns being balanced, proceed to form a Departure Column, or a Column of Meridian Distances; which shows how far the end of each Side of the Field is east or west of the station where the calculation begins. This Column is formed by a continual addition of the eastings and subtraction of the westings; or by adding the westings and subtracting the eastings : See EXAMPLE I.

The first easting 20.74 is set for the first number in the Departure Column; to this add 24.38 the second easting, and it makes 45.12, for the second number; to this add 30.04 the third easting, and it makes 75.16, for the third number; to this add 9.56 the fourth easting, and it makes 84.72, for the fourth number; the fifth Course being south, it is evident the Meridian Distance will remain the same, therefore, place against it the same easting as for the preceding Course; from this subtract 39.95, the first westing, and it leaves 44.77, for the sixth Course; from this subtract 23.75, the second westing, and it leaves 21.02, for the seventh Course ; from this subtract 21.02 the last westing, and it leaves 0.0, to be set against the last Course, which shows that the additions and subtractions have been accurately made. For as the eastings and westings equal each other, it is evident that one being added and the other subtracted, there will in the end be no remainder.

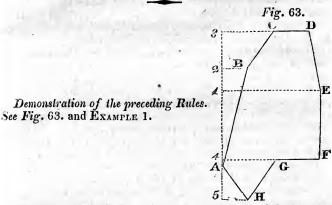
5. The next step in the process is to form a second Departure Column, the numbers in which show the Sum of the Meridian Distances at the end of the first and second, second and third, third and fourth Courses, &c.

The first number in this column will be the first in the other Departure Column; to which add the second number in that Column for the second in this; for the third add the second and third; and for the fourth, the third and fourth; and so on till the Column be completed. See EXAMPLE I.

The first number to be placed in the second Departure Column is 20.74; to this add 45.12, and it makes 65.86, for the second number; to 45.12 add 75.16, and it makes 120.28, for the third number; to 75.16 add 84.72, and it makes 159.88 for the fourth number; to 84.72 add 84.72, and it makes 169.44 for the fifth number; to 84.72 add 44.77, and it makes 129.49 for the sixth number; to 44.77 add 21.02, and it makes 65.79 for the seventh number; to 21.02 add 0.0, and it makes 21.02 for the eighth number.

65

6. When the work is thus far prepared, multiply the several numbers in the second Departure column by the northings or southings standing against them respectively; place the products of those multiplied by the northings in the column of north areas, and of those multiplied by the southings in the column of south areas; add up these two columns and subtract the less from the greater; the remainder will be double the area of the field in square rods or square chains and links, whichever measure was used in the survey.



The dotted line A 2 represents the northing, and the line 2 B the easting made by the first course; these multiplied together, that is, $77.15 \times 20.74 = 1600.0910$, which is double the area of the triangle A2B, as is evident from the Rule to find the area of a triangle, PROB. IX. Rule 1. This number is to be placed for the first number in the column of north areas. The line 3C represents the sum of the eastings made by the first and second courses, which is 45.12 the second number in the first departure column; if to this you add 20.74 the length of the line 2B you. have 65.86, which is the second number in the second departure column, and which represents the sum of the two lines 3C and 2B. These two lines with the line 2, 3 which represents the northing made by the second course, and the line BC, one of the sides of the field, form a Right Angled Trapezoid. Now, by the rule to find the area of such a Trapezoid, See PROB. X. 65.86 × 31.66=2085.1276, double the area of the Trapezoid 2 BC 3. Place this product for the second number in the column of north areas.

To the line 3C add CD 30.04, the easting made by the third course, and you have 75.16. which is the sum of the eastings made by the three first courses, and the third number in the first departure column. To this add 9.56, the easting of the fourth course, and you have 84.72, the length of the line 1E, which represents the sum of the eastings made by the four first courses, and is the fourth number in the first departure column. These two, viz. the lines 3D 75.16 and 1E 84.72, added together make 159.88, the fourth number in the second departure column; which, being multiplied by 49.15, the length of the line 3, 1 which represents the southing made by the fourth course, will give double the area of the Trapezoid 1 ED 3. The number thus produced is 7858.1020, which is to be placed for the first number in the column of south areas.

The fifth course being due south, it is evident the sum of the eastings will remain the same as at the end of the fourth course; that is, the line 4F equals the line 1E, which is 84.72. These added make 169.44, the fifth number in the second departure column. This, being multiplied by 54.10, the length of the line EF, which is the southing of the fifth course as corrected in balancing, and the same as the line 1, 4—will give double the area of the parallelogram 1 EF 4, which is 9166.7040, the second number in the column of south areas.

From the line AF 84.72 subtract 39.95, which is a west course, and it leaves 4G 44.77, the sum of the eastings, or the Meridian distance, at the end of the sixth course, and the sixth number in the first departure column. From this subtract 23.75 the westing made by the seventh course, and you have 21.02, the length of the line 5H, which is the Meridian distance at the end of the seventh course, and the seventh number in the first departure column. The line 4G 44.77 added to the line 5H 21.02 make 65.79, the seventh number in the second departure column. This being multiplied by 32.21, the length of the line 4, 5—which is the southing of the seventh course, will give double the area of the Trapezoid 4GH5, which is 2119-.0959, the third number in the column of south areas.

The line H5, 21.02, is the westing of the last course, and, the last number in the second departure column. This being multiplied by 26.65, the length of the line 5A, and the northing of the last course, produces 560.1830, which is double the area of the Triangle A5H, and the last number in the column of north areas.

Note. It will be observed that against the third and sixth Courses there are no Areas; the reason is, that these Courses being one east and the other west, there is no northing or southing to be multiplied into them : regard can therefore be had to them only in forming the Departure Corlumns.

By inspecting the Figure, and attending to the preceding illustrations, it will be seen that the three North Areas represent double the Area of the Triangle A2B, the Trapezoid 2BC3, and the Triangle A5H, all of which are without the boundary lines of the field : also, that the three South Areas represent double the Area of the Trapezoid 3DE1, the Parallelogram 1EF4, and the Trapezoid 4GH5; and that these include not only the field but also what was included in the North Areas. Therefore the North Areas subtracted from the South, the remainder will be double the Area of the field, contained within the black lines.

Additional Directions and Explanations.

The northings and southings may be added and subtracted instead of the eastings and westings; then there will be two Latitude columns instead of Departure columns, and the numbers in the second Latitude column must be multiplied into the eastings and westings, and you will have east and west Areas.

When the course is directly north or south, the distance must be set in the north or south column; when east or west, in the east or west column. There will therefore sometimes be no number to be added to or subtracted from the number last set in the Latitude or Departure column; then the number last placed in the column must be brought down and set against such Course; as in EXAMPLE I. at the 5th Course. It may also sometimes be the case that there will be no number to multiply into the number in the second Latitude or Departure column; then that number must be omitted, and against such Course there will be no Area as in EXAMPLE I. at the 3d and 6th Courses.

When the northings or southings, eastings or westings, beginning at the top, will not admit of a continual addition of the one and subtraction of the other, without running out before you get through the several Courses, you may begin at such a Course as will admit of a continual addition and subtraction; and when you get to the bottom go to the top, and you will end in cipher

at the Course next above that where you began; as in EXANPLE. II. which begins at the 9th Course to add the eastings and subtract the westings.

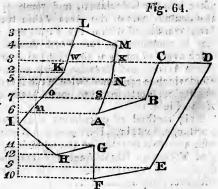
EXAMPLE II.

No.	~	Dist. Rods		s.	E.				North Areas	South Areas
	N. 75° 0' E.								3341.26	
	N. 2030 E.									
	East .									
	S. 33 30 W.									
	S. 76 OW.									
6	North									
	S. 84 0 W.									
8	N. 5315 W.									
9	N. 36 45 E.	76.8	61.5		46		46	46	2829	
10	N. 2230 E.	56	51.7		21.4		67.4	113.4	5862.78	
11	S. 76 45 E.	48		11	46.7		114.1	181.5		1996.50
12	S. 15 0 W.	43.4		41.9		11.2	102.9	217		9092.30
13	S. 1645 W.	40.5		38.8		11.7	91.2	191.1		7531.0

Area 110 Acres, 2 Roods, 23 Rods.

Note. In the above EXAMPLE you might begin at the 4th Course to add the westings and subtract the eastings; or at the 6th Course to add the northings and subtract the southings: or at the 11th Course to add the southings and subtract the northings. So in every survey, some place may be found where you may begin to add and subtract, without running out before you get through all the Courses.

When a field is very irregularly shaped, it will often happen that parts of the same Area will be contained in several different products in the columns of Areas; but in the final result, one column being subtracted from the other will leave what is included within the boundary lines of the field.



Demonstration. See Fig. 64, and Ex-AMPLE II.

The Area standing against the 9th Course, which is where the calculation begins, is the Triangle I2K, all without the Field.

The Area against the 10th Course is the Trapezoid 2KL3, also without the Field.

The Area against the 11th Course is the Trapezoid 4ML3. This is a South Area, and contains a part of the Field and also part of the preceding North Area.

The Area against the 12th Course is the Trapezoid 5NM4, part within and part without the Field.

The Area against the 13th Course is the Trapezoid 6AN5, part within and part without the Field.

The Area against the 1st Course is the Trapezoid 6AB7, part within and part without the Field. This is a North Area, and to be ultimately subtracted from the South Areas; but this includes a part of the preceding South Area, viz. the space nAso; it will, however, be seen hereafter that this same space is included in another South Area. This North Area contains also a part of the first North Area, viz. the space 6no7; but the same space is also included in another South Area.

The Area against the 2d Course is also a North Area, and is the Trapezoid 7BC8. This Trapezoid contains the space sBCx, without the Field; the space osxw, within the Field; and the space 70w8, without the Field. But the space osxw will be contained in the next south Area; and the space 70w8, which was contained in the two first North Areas, will be contained in the next South Area.

By examining the whole Figure in this manner, it will be seen that the North Areas contain all without the Field that is

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taken into the Calculation, and some of it twice over; they also contain part of the Area within the Field. The South Areas contain all within the Field, and all without the Field that is contained in the North Areas. They also contain, twice over, so much of the Field as is included in any of the North Areas; and likewise, twice over, that part without the Field which is contained twice in the North Areas. So that subtracting the North from the South Areas leaves double the Area of the Field.

This method of calculating the Area of a Field by the Northings, Southings, Eastings, and Westings, divides the Field, with a certain quantity of the adjoining ground, into Right Angled Triangles, Right Angled Trapezoids, Parallelograms, or Squares, as may be seen by the *Figures*. It may therefore with propriety be called RECTANGULAR SURVEYING.

A USEFUL PROBLEM.

To find the true Area of a Field which has been measured by a Chain too long or too short.

Calculate the Area as if the Chain was of a true length, then institute the following Proportion :

As the Square of the length of the true Chain; Is to the Area, as found by the Chain made use of; So is the Square of the length of that Chain; To the true Area of the Field.

EXAMPLE.

Suppose a Field, measured by a Two Rod Chain 3 Inches too long, is found to contain 41 Acres 1 Rood and 33 Rods, what is the true Area?

As the Square of 33 Feet, the true length of a Two Rod Chain; Is to 41 Acres 1 Rood and 33 Rods; So is the Square of 33 Feet 3 Inches, the length of the Chain used in the Survey; To 42 Acres and 13 Rods. 33 Feet=396 Inches. 396 × 396=156816 Square Inches.

41 Acres 1 Rood 33 Rods=6633 Rods.

33 Feet 3 Inches=399 Inches. 399×399=159201 square inches.

159201 × 6633 - 156316 - 6733 Rods.

6733--160-42 Acres 13 Rods, the true Area.

PART II.

LAVING OUT LAND.

PROBLEM I. To lay out any number of Acres in the form of a Square.

Annex 5 Ciphers to the number of Acres, which will turn them into Square Links, the Square Root of which will be the Side of the Square in Links.

EXAMPLE. It is required to lay out 810 Acres in the form of a Square.

Answer. Each Side of the Square must be 9000 Links, or 90 Chains.

PROBLEM II. To lay out any number of Acres in the form of a Parallelogram, whereof one Side is given.

Divide the number of Acres, when turned into Square Links, by the given Side ; the Quotient will be the Side required.

EXAMPLE. What must be the longest side of a Parallelogram, which is to contain 25 Acres, when the shortest side is 5 Chains and 50 Links?

Answer. 2500000-550-4545 Links for the longest Side.

PROBLEM III. To lay out any number of Acres in a Field, 3, 4, 5, 6, &c. times as long as it is broad.

Divide the Acres, when turned into Square Links, by the proportion between the length and breadth; the Square Root of the Quotient will be the shortest Side.

EXAMPLE. It is required to lay out 100 Acres 5 times as long as it is broad.

Answer. $10000000 \div 5 = 2000000$ the Square Root of which is 1414 Links for the shortest Side, and the longest will be 7070 Links.

PROBLEM IV. To make a Triangle which shall contain a given number of Acres, being confined to a certain Base.

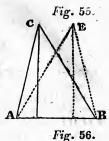
Double the given number of Acres, to which, annex 5 Ciphers, and divide by the Base; the Quotient will be the Perpendicular in Links.

EXAMPLE. Upon a Base of 40 Chains to lay out 100 Acres in a Triangular form.

Answer. 5000 Links or 50 Chains will be the length of the Perpendicular.

The Perpendicular may be erected from any part of the Base: Thus, the Triangle ABC. See Fig. 55. is the same as ABE, each containing 100 Acres.

When the given Base is so situated that a Perpendicular of sufficient length cannot be erected therefrom, continue the Base as from B to **D**. Fig. 56. from which erect the Perpendicular DC, and complete the Triangle ABC, which will contain 100 Acres.



B



DIVIDING LAND.

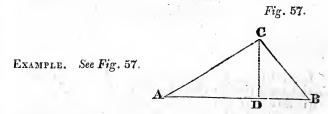
As different Fields are so variously, and many of them irregularly shaped, and as they are required to be divided in many different proportions, it is difficult to give Rules which will apply to particular cases. The business of dividing Land must therefore be left, in a great measure, to the skill and judgment of the Surveyor; who, if he is well acquainted with Trigonometry, and with measuring Land, will not find it difficult, after a little practice, to divide a Field in such a manner as shall be desired. If he has before him a plot of the Field, and knows the number of parts into which it is to be divided, and the proportion which each part is to bear to the others, he will readily find out where the dividing Lines are to be drawn.

A few RULES and EXAMPLES will be given for the general instruction of the Learner.

PROBLEM I. To cut off any number of Acres from a Square or Parallelogram. Say, as the whole number of Acres in the Field; Is to the length of the Square or length or breadth of the Parallelogram; So is the number of Acres proposed to be cut off; To their proportion of the length or breadth.

PROBLEM II. To cut off any number of Acres by a Line proceeding from any Angle of a Triangle.

Measure the Base, or Side opposite the Angle from which the dividing Line is to be drawn; Then say, As the number of Acres in the whole Triangle; Is to the whole Base; So is the given number of Acres; To their part of the Base.

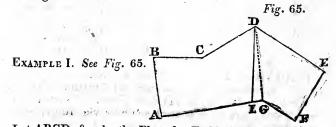


In the Triangle ABC, which contains 48 Acres, it is required to cut off 18 Acres, by a Line proceeding from C to the Base AB, which is 40 Chains.

As 48:40::18:15

Lay 45 Chains on the Base from B to D, and draw the Line CD. The Triangle will then be divided as was proposed; BCD containing 18 Acres.

PROBLEM III. To take off any given number of Acres from a multangular Field.



Let ABCD, &c. be the Plot of a Field containing 11 Acres, from which it is required to cut off 5 Acres.

Join two opposite Corners of the Field as D and G, with the

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Line DG (which you may judge to be near the partition Line) and find the Area of the part DEFG, which, suppose, may want 140 Rods of the quantity proposed to be cut off. Measure the Line DG, which, suppose to be 70 Rods; divide 140 by 35 the half of DG, and the Quotient 4 will be the length of a Perpendicular whose Base is 70 and the Area 140. Lay off 4 Rods from G to I, and draw the Line DI, which will be the dividing Line.

EXAMPLE II. See Fig. 60.

Fig. 60.

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Let ABCD, &c. be a tract of land to be divided into two equal parts, by a line from I to the opposite side CD;Ato find arithmetically on what part of the line CD the dividing line IN will fall; or to find the Distance CN.

FIELD	BOOK.

		Rods.		Rods.
AB. N.	19º 0' E.	109	GF. West	70.9
	. 77 0 E.	91	GH. N. 36° 0' W	. 47
CD. S	. 27 0 E.		HI. North	64.3
DE. S			– IA. N. 62 15 W	. 59
EF. S	15 30 E.	76	Acres Rood I	Rods
			Whole Area 152 - 1 -	25

Find the Area of the part IABCI, according to SECTION III. Page 57, as follows: set the Latitude and Departure of the three first Sides, IA, AB, and BC, in their proper columns, in a Traverse Table; and place as much southing, viz. 109.1, equal to the line CK, and as much westing, viz. 71.7, equal to the line KI, as will balance the columns. This southing and westing will be the Latitude and Departure made by the line CI. The Area of IABCI will be found to be 8722 Rods, which is less than half the Area of the whole Field by 3470 Rods, the quantity to be contained in the Triangle ICN.

Find the bearing and distance of CI by RIGHT ANGLED TRIGO-NOMETRY, CASE IV. as follows :

As CK, the southing : Radius : : KI, the westing of	-	-	- 0		:	••••			2.03743 10.00000 1.85552
		·					-		11.85552 2.03743
: Tangent Course S.	330 2	o' w.			- 6		-	-	9.81809
									-
As Sine Course 33º	20			-	-	- 1		-	9.73997
: Departure KI 71.7	-	-		-	-		-	-	1.85552
::Radius -	-	-	-	-	-	-	-	-	10.00000
									11.85552
									9.73997
									5.13551
Distance IC 130	-	-		-	1-2-5		а. К. т.		2.11555

Note. In this way the Course and Distance may be found from one Angle of a Field to another.

Having found the line CI, divide 3470; the number of Rods to be contained in the Triangle ICN, by one half the line CI, viz. 65, the quotient will be the length of the Perpendicular PN, viz. 53.4.

Now, by the bearings of CI and CD, it appears that they form an Angle of $60^{\circ} 20'$; wherefore, in the Triangle CPN are given the side PN 53.4, and the Angle at C $60^{\circ} 20'$, to find the Hypothenuse CN.

As Sine PC:	N 60° 20'	·	9.93898
: Side PN 5	3.4 -		1.72754
: : Radius			10.00000
	- `.	r 1	
	1		11.72754
			9.93898
1.0			
: Hyp. CN	61.5 -		1.78856
			and the second se

Thus the dividing line must go from I to a point on the line CD, which is 61.5 Rods from C. The bearing and distance of

this line may be found by the directions given above for finding the bearing and distance of the line Cl. Or, they may be found by Oblique Trigonometry, CASE 111.

Another Method of finding the Distance CN.

Having ascertained the Latitude and Departure of the line Cl, set them down in a Traverse Table; find the Latitude and Departure of the line CD, and place them in the Table; the difference between the northing of the line IC, and the southing of the Line CD will be the southing of the line DI, viz. 6.6; and the sum of the eastings of those lines, as they are both easterly, will be the westing of the line DI, viz. 123.9. Proceed to calculate the Area of the Triangle ICD, which will be found to be 6522 Rods, nearest.

Note. As in this Triangle two sides and their contained Angle are given, the Area may be found by PROB. IX. Rule 4, Page 38.

Having found the Area of this Triangle, proceed to find CN according to Prob. II. Page 73, as follows:

As the Area of the Triangle; Is to CD the Base; So is the quantity to be contained in the Triangle ICN; To CN its proportion of the Base.

As 6522: 115:: 3470: 61.2

A third method of finding the Distance CN.

To the Logarithm of double the Area to be contained within the 'Triangle ICN add Radius; from this Sum subtract the Logarithmic Sine of the angle at C; and from the Remainder subtract the Logarithm of the Side IC; the last Remainder will be the Logarithm of the Side CN.

The double Area of the Triangle ICN is 6940; the Angle at C is $60^{\circ} 20'$; the Side IC is 130.

Double Area 6940 Radius -	-	-	$3.84136 \\ 10.00000$
		-	13.84136
Sine ICN 60° 20'		-	9.93898

	and house and	5 5. 10.		(F 1 -	3.90238	
	Side IC 130		-		2.11394	
-	Side CN 61.5	· -	-	-	1.78844	

Note. Radius may be added by placing a Unit before the Index of the Logarithm for the double Area, without the trouble of setting down the Ciphers:

By Natural Sines.

Divide the Double Area by the Natural Sine of the given Angle, and that quotient by the given Side; the last Quotient will be the Side CN.

Nat. Sine of the Angle at C 60° 20′ 0.86892 6940--0.86892=7986.92 7986.92--130=61.43

From the above the following general Rule may be drawn. To find the Side of a Triangle when the Area is given, with one of the Sides and the Angle contained between the given Side and the Side required.

To the Logarithm of double the Area add Radius; from this Sum subtract the Logarithmic Sine of the given Angle, and from the Remainder subtract the Logarithm of the given Side; the last Remainder will be the Logarithm of the Side required.

Or, By Natural Sines: Divide the double Area by the Nat. Sine of the given Angle, and that Quotient by the given Side; the last Quotient will be the Side required.

CONCLUDING REMARKS.

Other methods of surveying Fields are taught by some authors on this subject. The preceding, however, will be found most useful in actual practice. Other instruments besides those mentioned in this Book are also sometimes used; such as the Plain Table, Semicircle, Perambulator, Theodo-

lite, &c. But of these instruments very little use is made in New-England; and they are not often to be met with. For general practice none will be found more useful than a common Chain, and a Compass upon Rittenhouse's construction. A Surveyor should also provide himself with an Offset Staff, ten Links in length, and accurately divided into Links. This should be made of firm hard wood, and will be found very convenient in taking Offsets, and also in measuring the Chain; which should be often done, as from a variety of causes a Chain is liable to become inaccurate.

It will be observed that in this Work there are no descriptions of Mathematical and Surveying instruments. The Compiler omitted such descriptions from a belief that nothing which can be written on the subject will enable a person to understand them without an actual inspection of the instruments themselves, and some instruction from those acquainted with them.

The general principles here taught may be applied to the surveying of Townships, Roads, Rivers, Harbours, &c.

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OF THE VARIATION OF THE COMPASS AND ATTRACTION OF THE NEEDLE.

THE Variation of the Compass is the number of Degrees that the Magnetic Needle points from the true North, either East or West. This differs in different places, and in the same place at different times. It is, at present, in Connecticut, a few degrees to the Westward. That is, the Needle points to the Westward of North, and is gradually approaching the true North.

The following method of ascertaining the Variation, by the North Star, has been adopted by many Surveyors, as the most eligible to be practised on Land. It was communicated to the Compiler by Moses Warren, Jun. Esq. of Lyme, an experienced Surveyor, with permission to publish it.

The Star commonly called the North Star, is not directly North but revolves round the Pole in a small circle, once in 24 hours. It cannot therefore be due North but twice in that period; and that is within a very few minutes of the time when a Star, called *Alioth*, in the Constellation of Ursa Major, or the Great Bear, is directly over or under it. There is also another Star nearly in an opposite direction from the Pole, called *Gamma*, in the Constellation of Cassiopeia. When these three Stars are vertical the North Star is very near the Meridian; and where they are horizontal, it is at its greatest Elongation, that is, at its greatest distance East or West of the Pole, and on the same side as the Star in Cassiopeia. The Variation may be calculated when the Star is on the Meridian, or when at its greatest Elongation; more accurately, however, at the latter period, because its motion being then nearly vertical for some time gives the observer a better opportunity to complete his observation.*

To find the Elongation of this Star in any Latitude, its Decknation must be known; that is, its distance North of the Equator. This being found, institute the following Proportion:

As Co-Sine of the Latitude; Is to Radius; So is Co-Sine of the Declination; to Sine of the Elongation.

The Declination of the North Star, January 1, 1810, was SSO 17' 28", and increasing at the rate of about 19 seconds and one half annually.

The following Table Shows the Elongation, in several different Latitudes, for 5 years successively. It is calculated for the first of January in each year; and in using it, if the time, when the Elongation is required, be past the middle of the year, take it for the beginning of the next year.

Latitude.		18:	20		182	21		182	22		182	23		189	24
380	20	5	34″	20	5	7″	20	4	39//	20	4	13″	20	3	47
39	2	7	23	2	6	54	2	6	25	2	5	59	2	5	33
40	2	9	12	2	8	41	2	8	14	2	7	46	2	7	20
41	2	11	11	2	10	40	2	10	12	2	9	44	2	9	18
42	2	13	10	2	12	39	2	12	11	2	11	43	2	11	16
43	2	15	22	2	14	51	2	14	22	2	13	54	2	13	26
14	2	17	33	2	17	4	2	16	34	2	16	5	2	15	37

A Table showing the Elongation of the North Star.

^{*} * The following Figure exhibits a view of the relative situation of these Stars as they appear, when in a horizontal position: or when the North Star is in its greatest Eastern Elongation.

The Great Bear.

* Alioth

North Star Pole *

Cassiopeia. Gamma .

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The Elongation for the Latitude of the observation being calculated, or taken from the above Table, proceed to find its range, according to the following directions;

Take a pole 18 or 20 feet in length; to the end of it fasten a small line; raise it to an elevation of 45° or 50°; and support it by two crotches of suitable height to keep it firm in its place. At the end of the line, near the ground, fasten a weight of half a pound or more, which should swim in water to prevent the air from moving the line. Southward of the line, fix a Compass sight, or other piece of metal or wood, with a narrow, perpendicular aperture at a convenient height from the ground, say about 2 or 2 1-2 feet; and let it be so fixed that it can be moved a small distance East or West at pleasure. Let an assistant hold a light either NE. or NW.of the line, nearly as high as the range from the sight to the North Star, in such a position that the line may be plainly seen; then, (the three Stars above mentioned being parallel or nearly so with the Horizon) move the sight-vane East or West, until through the aperture, the line is seen to cut the Star; and continue to observe, at short intervals, till the Star is seen at its greatest Elongation. Let a lighted candle be placed in an exact range with the sight-vane and line at the distance of 20 Rods or more, which should stand perpendicularly, be made fast, extinguished, and left till morning. Then the sight-vane, the line, and the candle, will be the range of Elongation, which observe accurately with a Compass ; and if the Elongation be East and the Variation West, the former must be subtracted from the latter; and if they are both West they must be added, and their difference or sum will be the true Variation.

OF THE ATTRACTION OF THE NEEDLE.

It is well known that any iron substance has an influence upon the magnetic Needle, attracting it one way or the other from the point where it would settle, were there no such attraction. A surveyor should therefore be careful to see that no iron is near the compass when taking a bearing. But as the Earth in certain spots contains, near its surface, iron or other minerals which attract the Needle, it will frequently happen that it will point wrong. To ascertain whether this is the case, the surveyor, at each station, should take a back view of the one last left; and if he finds that the compass does not reverse truly, he

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may be sure, provided the compass be accurately graduated and placed horizontally, that he either made a mistake at the last station, or that in one of the other of the stations, the Needle was attracted from the true point. When he finds a place where he suspects there is an attraction, he should go a few rods backward or forward, and see whether the Needle points differently. In this way he may prevent mistakes in his field notes, by putting down a wrong course. To take back sights is particularly necessary in running long lines, and laying out new lands, where the Needle is the only thing to guide the surveyor.

By practice and experience a knowledge will be acquired on this subject, and with regard to many other things in surveying, which cannot be taught by books; and after all the directions which can be written, the practitioner will frequently find occasion for the exercise of his own judgment.

A Rule to find the difference between the present variation of the Compass, and that at a time when a Tract was formerly surveyed, in order to trace or run out the original lines.

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Go to any part of the premises where any two adjacent corners are known; and if one can be seen from the other, take their bearing; which, compared with that of the same line in the former survey, shows the difference. But if one corner cannot be seen from the other, run the line according to the given bearing, and observe the nearest distance between the line so run and the corner; then work by the following proportion:

As the length of the whole line,

Is to 57.3 degrees,*

So is the said distance,

To the difference of variation required.

EXAMPLE.

Suppose it be required to run a line, which, some years ago, bore N. 45° E., distance 20 chains, and in running this line by the given bearing, the corner is found 20 links to the left hand; what is the present bearing of this line?

* 57.3 degrees is the Radius of a circle (nearly) in such parts as the circumference contains 360.

$\begin{array}{c} \text{Ch.} & \text{Deg.} & \text{L} \\ \text{As 20} & : & 57.3 : : 20 \\ \hline 100 & 20 \\ \hline 2000 & 1146.0 \\ \hline 60 \\ \hline \end{array}$

2000)68760(34 Minutes. Answer-34 Minutes to the left hand is the allowance required, and the line in question bears N. 44° 26' E.

The compiler of this work acknowledges himself under obligations to George Gillett, Esq. Surveyor General of the state of Connecticut, for the following illustrations, remarks, and miscellaneous questions, considering them calculated to be useful to the learner, and the practical surveyor. They came to hand too late to be inserted in their proper places, in the body of the work, and are here put together in the Appendix. ತ್ತು ಸರ್ವಾಟಕ್ ಬ್ಯಾಂಗ್ ಸರ್ಕಾರ್ ಸ್ಟ್ರೆಸ್ ಸ್ಟ್ರೆಸ್ ಸ್ಟ್ರೀ ಸ್ಟ್ರೇಕ್ ಮಾಡಿದ್ದಿ ಸ್ಟ್ರೈ ಸ್ಟ್ರಿಸ್ಟ್ ಸ್ಟ್ರಿ ಪೋರ್ಟ್ ಸ್ಟ್ರಿ ಸ್ಟ್ರೇಸ್ ಸ್ಟ್ರೀಸ್ ಸ್ಟ್ರೀಸ್ ಸ್ಟ್ರಿಸ್ ಸ್ಟ್ರಿಸ್ ಸ್ಟ್ರಿಸ್ ಸ್ಟ್ರಿಸ್ ಸ್ಟ್ರಿಸ್ ವಿಶೆಟ್ ಕ್ರಾಂಗ್ರಕ್ಟೇ ಕೇಟ್ರಾಲ್ ಪ್ರಾವೇ ವ್ಯಕ್ತಿಸುವ ಸರ್ವಾ**ಧಿಕಿದ್ದ**್ರೆ ಸ್ಟ್ರೀಸ್ ಸ್ಟ್ರೀಸ್ ಸ್ಟ್ರಿಸ್ ಸ್ಟ್ರಿಸ್ ಸ್ಟ್ರಿಸ್ ಸ್ಟ

Remarks on the Irregularities of the Magnetic Needle. story it . I of paise

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By a statute of this state, applicants for the appointment of County Surveyor are required to be well skilled in point of science in the theory of the most approved methods of surveying lands. It is also as necessary that they should be as well skilled in practical surveying. A practical knowledge must be acquired by experience, and no one can have a thorough knowledge of correct practice without being made acquainted with the imperfections and irregularities of the Magnetic Needle.

It is supposed, by most people, that this instrument, in all places, points directly to the Poles of the earth, and that it remains as permanent as the Poles themselves-an infallible guide.* This is a mistaken idea. A few remarks on this submash. 130 10 gamme the H . . .

* There is one line around the globe on which there is no variation. The general course of this line, on this side of the globe, is from northwest to southeast, but is crooked and irregular in its course. According to Dr. Holly's chart, made in 1700, the line of no variation crossed the meridian of London in 55° South latitude-crossed the equator in 17° W. longitude-from thence, by various windings, to the island of Bermuda, from

ject will here be offered, and some facts respecting it will be stated.

Notwithstanding the great utility derived from the Magnetic

thence nearly a west course until it struck the continent near Charleston, in South Carolina. This line is not stationary, but is ever varying its position; and, notwithstanding the irregularity of its courses, it never crosses itself. About 1756, another variation chart was made, when it was found that the line had fallen so far to the west that it struck the continent near the coast of Florida. On the cast side of this line, the Magnetic Needle points to the west of north, and on the west side it points to the east of north, and a regular increase of either east or west variation is found from it, depending on the course that is taken. The line of no variation now runs through Pennsylvania, and not far from Norfolk, in Virginia. When the Connecticut Western Reserve was surveyed into townships, the variation at that place was easterly from one 'to two degrees.' In 1813, at New-Orleans, the variation was easterly, about eight or nine degrees. In 1701, at Philadelphia, the variation was westerly, eight degrees and a half. In 1794, at the same city, the west variation had diminished to one degree and a half, which proves that the progress of the line of no variation had been from west to east. In 1813, by observations at this city, it was found that the west variation had increased to about two or three degrees. ! By a series of observations, commenced at Hebron in Connecticut, by the writer of this, in 1805, and continued to 1813, it was found that the west variation during that period increased more than half a degree. The result of these observations agree with those at Philadelphia, that there had been a retrograde motion of the Needle. Since 1813, the west variation has diminished, or certainly it has not increased. The west variation at Hebron is now (1825) a few minutes more than five degrees. In 1580, at London, the Magnetic Needle pointed eleven degrees and a half to the east of north, which proves that the line of no variation was east of that place. The east variation diminished until 1657, when the line of no variation arrived there and soon passed by; of course west variation began, and continued to increase until 1806, when it exceeded twenty-four degrees. 1: 22

The line of no variation must have had a rapid progress through the Atlantic and through a great part of the United States, to have arrived at Charleston in 1700, and at the coast of Florida in 1756. The present bearing of all old lines in this state prove that there has been a considerable decrease of west variation since the first surveys were made ; which also proves that the progress of the line of no variation, in the United States, has, for a long time, been from west to east. How far the line of no variation progressed westward in the interior of this country before it turned, no one can It is unaccountable how the west variation in London should increase, tell. while at Philadelphia it was diminishing, when both places are on the same The variation of the Needle has long been side of the line of no variation. a subject of much perplexity. Observations have been made in abundance. Many facts have been ascertained, but the difficulty is, they are not reducible to system. The polarity of the Magnetic Needle, with its variations and irregularities, is a hidden mystery, which is never to be searched out by map. It is sufficient in itself, without any other evidence, to cause the reflecting mind to wonder at, admire, and adore the wisdom, knowledge, and power of HIM who planned and directs it.

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Needle, it cannot be relied on where great accuracy is required, on account of the irregularities to which it is subject, such as its annual motion in variation, its diurnal motion, and, what is attended with greater difficulty, its local attraction. When an old course is given to renew a line, it cannot be depended on, on account of the difference in variation between the time of the first running and the renewal of it.

No annual rate can be fixed on for the variation of the Magnetic Needle, as its motion is much more rapid in some years than in others. By observations made at London during a period of more than two hundred years, it appears that in some years the motion of the Needle was rapid, in others, but little would be discovered, and, in some years, the motion was retrograde. There is no regularity is its motion in any place.

Another difficulty in retracing a line from an old course or from one recently given is, that it is often found that two compasses do not make the same course. It was well known to the celebrated Rittenhouse, that his compasses did not all agree, or make the same course, and he never was satisfied as to the reason of it. It has also been ascertained that different Needles do not point alike at the same place. French writers, on Magnetism, have lately treated on this subject. Two compasses may differ a quarter of a degree or more or less, when no defect can be discovered in either. A survey may be taken as correctly with one as with the other. The question then naturally arises, which of the two is right? The answer is, both are right; neither of them points directly to the Poles of the earth, except on the line of no variation. All that can be said of them is, that one has a greater variation than the other, and that which has the least cannot have the preference. The diurnal motion of the Magnetic Needle is another defect in it. As the sun rises in the forenoon, and the earth becomes heated, it has an effect on the unknown something which gives polarity to the Needle, and turns the north end of it to the west. In the afternoon and night following, it returns to its position.

For several years, the writer of this made observations with Rittenhouse's compass, to ascertain the diurnal motion; and in the summer season usually found about a sixth part of a degree. In the winter, but little or none could be discovered. The diurnal motion of the Needle has been known in Europe about a century.* The local attraction is an irregularity to which the Magnetic Needle is subject. These are found oftener in hilly,

The diurnal motion is mentioned in Dr. Williams' History of Vermont.

broken lands, filled with ledges, than in level, feasible land, where there are no ledges. As attractions are out of sight, they must be searched out, as before directed in this work, by local experiment. They often amount to a quarter, a half, and sometimes to a whole degree or more. The writer of this has known a difference of more than five degrees within a distance of forty rods.

When an old line is to be renewed where the bounds are lost, the circumstances attending the case must govern. These may be various, such as giving the lots on each side of the line and contiguous thereto, their full width or quantity, or by dividing the overplus or the wantage, as the case may happen. It would be difficult to mention all the circumstances which may govern, or which may serve as evidence in such cases.

After all, the Magnetic Needle is the best guide that has yet been discovered, and it cannot be dispensed with in land surveying; but the surveyor who is best acquainted with it, will make as little use of it as he can. In small surveys, where one angle may be seen from another, the quantity of each angle may be taken by an instrument constructed for that purpose, without the use of the Magnetic Needle; and the sides may be measured, and one side, no matter which, may be made a meridian, and from that meridian courses may be calculated for the other sides. and the survey may be calculated by the rules of rectangular surveying. This method has been recommended by theorists. and the ingenuity displayed in the invention, together with the correctness of it, so far as it is practicable, must be acknowledged; but in larger surveys, it cannot be introduced to practice, on account of the obstructions which intervene between the angular point and the termination of two contiguous lines which contain the angle : in such cases, the danger in taking the quantity of an angle will be greater than that of the Magnetic Needle.

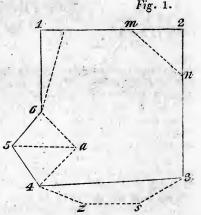
If in every town in the state, a meridian line was established by the motion of the heavenly bodies, and such meridians were perpetuated by durable monuments, whenever a survey was to be taken in the vicinity of a meridian, a surveyor might set his compass on it and note the variation found, and that variation should be inserted in the deed or in whatever writing or instrument by which the land is conveyed and made a record; this would assist a surveyor at any future period in retracing those lines, by setting his compass on the same meridian and allowing the same variation that was allowed when the survey was made. This would the dreatly to the security of landed property, and

perhaps would be the best remedy for the variation of the Magnetic Needle, and for the difference between two compasses which differ, that can be invented.

On Practical Surveying.

It would be no easy matter to describe all the different methods which may be taken in different cases, in taking the fieldwork of a survey. Only one case will be given here, which is represented by the following figure. See Fig. 1.

The survey was begun at the corner numbered 1. The corner numbered 2 was in a pond. The course and distance were taken from 1 to m, then from m to n. The angle at 2 was a right one, of course there was a right angled triangle, wherein the angles and hypothenuse were given, to find the sides m2 and 2n. From n to 3, the course and distance were taken on the line. The next



line ran through a thicket in a swamp, where nothing could be done correctly. Courses and distances were taken from 3 to s, thence to z, thence to 4, and the course and distance of the line 3-4 were calculated by a traverse from those courses and distances. At the angle 5, a tree stood on a high bluff of ledges, inaccessible on either line terminating at that point. The course from 4 to 5 was taken at 4. Next, the course and distance were taken from 4 to a, and from a the course was taken to 5. Next, the course and distance were taken from a to 6, and from 6 the course was taken to 5. Two oblique triangles, with the angles and one side in each, were given to find the sides 4-5 and 5-6. The closing line ran through thick bushes and water, and the course and distance were taken on the dotted

line to the line 1-2, at a point twenty rods from 1. The course and distance of 6-1 were calculated accordingly.

Whenever a line runs through or over a place where it is difficult to take either course or distance correctly, if, by taking a traverse around at a little distance, the surveyor can have level, clear land, and then calculates his course and distance by the traverse, he will be more likely to ascertain the true course and distance than by continuing on the line.

Directions for running Lines.

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Many people suppose that a surveyor at the beginning of a line, by intuition or by some magic art, can set his compass directly to the terminating point, whatever obstructions may intervene, and that he needs no assistants ; but this is a mistaken idea. In running a line of considerable length, a surveyor should have two assistants to carry the chain, and two to carry flags, in whose ability and correctness he can confide, and a fifth to use an axe. If the surveyor is not furnished with such a set of assistants, his employer need not place too much confidence in his work. The flag staves should be as much as two and a half inches in diameter, or what would be better, two stripes of a board of that width and seven or eight feet in length. If they are not so wide, they cannot be seen through the sights of the compass, at any great distance. On one end of each staff, a red flag of a yard in length should be wound tight, and not left to hang loose and flutter in the wind. Red will be seen quicker through bushes than any other colour, and the brighter the colour the better. Being thus manned and equipped, at the beginning of the line, he must set his compass as near the true line as he can, or, what would be better, he may set up one of the flags at the place of beginning, and go forward as far as he can have a fair view of the back flag, there set his compass on his random line, and send the other assistant, as far forward as he can conveniently see the flag. When each flag is clearly seen through the sights of the compass, the back flag must be brought up and placed where the compass stood. In this manner, he must proceed on his random line, taking care each time he sets his compass to turn the sights to the back flag. Great care must be taken to keep these flags perpendicular; also, the surveyor must keep the staff and the sights of his compass perpendicular. A little leaning of the flags, or turning the sights.

of the compass from a perpendicular, will make a crooked line. In looking through the sights of the compass to the flags, the surveyor must look as near the ground as he can, and, when practicable, the flag should be turned down, on account of the danger of being leaned when kept up.

All obstructions, such as bushes, brush, &c. must be cleared away. The random line must be measured, and at convenient distances, perhaps at every twenty rods, stakes must be set directly in it. Every stake must be numbered, that no mistake may be made in calculating, to set them in the true line. If, in the course of the random line, the Magnetic Needle does not traverse as at first, or traverse alike at different places, no regard must be paid to it-the two flags must direct the course ; neither should the surveyor be turned aside or terrified by the cry of either of the parties, You are wrong, You are wrong, (for he will most certainly hear it,) but he must continue his random line, until turning at right angles either to the right or to the left, as the case may be, he will exactly strike the bound, or the point where a bound is to be erected; there he may stop, and measure the distance from the termination of it to the bound. Then, having the length of the random line and the distance to the true bound, he has the less of a right angled triangle, the hypothenuse will be the length of the true line; also, the angle contained between the true and the random line must be added to or subtracted from the course of the random line, (as the case may happen,) which will give the course of the true line. Suppose the whole length of the random line is 200 rods, and the distance from the termination of it to the bound is 90 links, the calculation for setting the stakes on the true line may be made thus :- As the whole distance is to 90 links, so is 180, or any other 20 rods stake, to the distance that such stake is to be moved. The answer is, the first stake is to be moved 9 links, the second 18 links, and so adding 9 links at each stake until the whole are moved at right angles from the random on the true line. Most of the crooked lines and consequent disputes and law-suits between farmers have arisen for the want of this care and attention. - A J. L'A gant

When a long line is to be run over a number of ridges and through intervening valleys, it should first be run and established from one ridge to another, and the intermediate spaces in the valleys may be taken afterward. By taking long sights there will be less danger of turning from a straight line. In all cases, the forward flag should be carried as far as it can be distinctly seen, unless it is at the termination of a line.

commit much error on them; while other lines, on other parts of the same survey, are attended with so many difficulties, that when they have done their best, it will scarcely be possible for them to avoid some error, and the surveyor who takes the survey will best judge on what lines the errors were committed, and whether they are in the courses or in the distances. In all cases the corrections should be made on the lines containing the errors. When the errors are in the distances, the correction should be in them: or the corrections may be in both courses and distances as the surveyor may judge proper.

When a course is northwesterly and southeasterly, or northeasterly and southwesterly, if the correction of it increases the latitude and diminishes the departure, or if it diminishes the latitude and increases the departure, so as to bring the differences to an even balance, it is good evidence that the course contains some error.

On Rectangular Surveying.

Rectangular Surveying is a name given to the method here treated of, by the late Governor Treadwell.

A more appropriate name could not have been given; for the whole survey is reduced to right lined figures, such as triangles, trapezia, squares, and parallelograms. It is simply multiplying the latitudes by the longitudes from a meridian from which the survey is calculated.

The calculations are made from a meridian, drawn, either at the eastern or at the western extremity of the map. All the spaces lying between the field and the meridian from which the survey is calculated, and between the parallels of latitude of the northern and southern extremities of it, are included in the calculation. Parallels of latitude are drawn from each angle to the meridian, which are called meridian distances.

In forming the column of meridian distances, when the meridian is drawn at the eastern extremity, the westings are added and the eastings are subtracted. When the meridian is drawn at the western extremity, the eastings are added, and the westings are subtracted.

The meridian distances proceeding from each end of a line, are added together, to form the column of double mean distances, which the compiler of the foregoing work has called second departure column.

The whole is illustrated by the following figure. See Fig. 2:

Directions for calculating meridian distances by several methods; also, for plotting a survey, from the several latitudes and meridian distances, without the use of the protractor, or the line of chords.

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		70.33	144.15	153.89	102.18	39.01	16.90	M.D. D. M. D.
		70.33	144.15 140.66	153.89 147.64	102.18 160.14	39.01 44.22 19.50	100	
		70.33 35.16	72.07	76.94	51.09	19.50	8.45	H.D.
	3351.83				1586.86	1152.35	612.62	H.D. N. Areas S. Areas.
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A. Q. R. 25 3 15

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commit much error on them; while other lines, on other parts of the same survey, are attended with so many difficulties, that when they have done their best, it will scarcely be possible for them to avoid some error, and the surveyor who takes the survey will best judge on what lines the errors were committed, and whether they are in the courses or in the distances. In all cases the corrections should be made on the lines containing the errors. When the errors are in the courses they should be corrected, and when the errors are in the distances, the correction should be in them: or the corrections may be in both courses and distances as the surveyor may judge proper.

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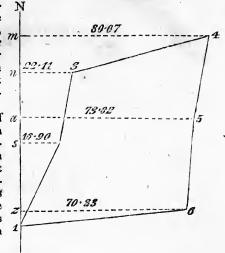
Directions for calculating meridian distances by several methods; also, for plotting a survey, from the several latitudes and meridian distances, without the use of the protractor, or the line of chords.

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		81.32				15.53	29.54	36.25	N
		81.32 81.32 80.07 80,07	6.02	39.85	35.45				ŝ
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Meridian Distances, and Double Mean Distances, are more proper terms or names for the eighth and ninth columns, than first Departure, and second Departure.

The meaning of the term Meridian Distance is the distance made from any Meridian. It is not very essential by what names the columns are called, as names have no effect on the final result.



This survey is calculated from the meridian of the first station.

To form the first column, marked at the top, Merid. Dist., set the easting 16.90 against the first station into the column, which is the meridian distance of 2, or the distance from 2 to 1 : to this number add the next easting, and they make 22.11, the meridian distance of 3; to this number add the next easting, and they make 80.07, the meridian distance of 4; from this number, subtract the first westing, and 73.82 remains, the meridian distance of 5; from this number, subtract the next westing, and 70.33 remains, the meridian distance of 6, or the westing of the closing line. Subtract the last westing, and This is on the principle of going around a 00.00 remains. circle. Next, form the column of double mean distances by adding two opposite sides of the different figures. Set the first Merid. Dist. into the column. To the first meridian distance, add the second, and they make 39.01, the double of the figure 23ns. To the second, add the ,hird, and they make 102.18, the double of the figure 34mn. To the third, add the fourth, and they make 153.89, the double of the figure 45am. To the fourth, add the fifth, and they make 144.15, the double of the figure 56az. To the fifth, add the sixth, and they make 70.33.

Fig. 2.

The second column, marked at the top, Merid. Dist., is commonly called the Pennsylvania method. Only one column is used in finding the meridian distances, but the operation and final results are the same as that when two columns are used. This method is not so easily explained to the learner, but is preferable in practice only because an error may be committed in forming the column of double mean distances which may not be discovered, but in this method an error cannot be committed without being detected.

To form this column, set the first easting 16.90 in the upper place, and add it to itself and they make 33.80; to this number, add the next easting, and they make 39.01; add the same easting again, and they make 44.22; to this number, add the last easting, and they make 102.18; add the same easting again, and they make 160.14; from this number, subtract the first westing, and 153.89 remains; subtract the same westing again, and 147.64 remains; from this number, subtract the second westing, and 144.15 remains; subtract the same westing again, and 140.66 remains; from this number subtract the last westing, and 70.33 remains; subtract the same westing again, and 00.00 remains.

The upper numbers in this column are the same as the double mean distances which stand against them.

For the remainder of the process in finding the areas, proceed as before taught in this work.

The north area against the first station is the double of the triangle 12s; that against the second, is the double of the figure 23ns; that against the third, is the double of the figure 34mn; the south area against the fourth station, is the double of the figure 45am; that against the fifth, is the double of the figure 56za; that against the sixth, is the double of the triangle 61z.

The three north areas all lie without the field, and are bounded north on the line m4. The three south areas contain all within, and all without the field, which is included in the calculation. It is obvious then that when the less is subtracted from the greater, the contents of the field will remain.

Another column may be formed as the eleventh in this example, which, for distinction, is here called half departure. It contains half the sum of the numbers in the double mean column. These numbers when multiplied by their respective northings or southings, give the simple areas of the different figures. This method is preferable in practice, as the multiplications are greatly diminished. When the last decimal in the double mean distance is an odd number, a unit may be taken

off, and take half the remainder rather than annex another decimal. Perhaps this would not make the difference of a rod in a survey of one hundred acres, or the odd numbers in the last place of decimals may be balanced by sometimes adding a unit. If the numbers are diminished a trifle, it may be remarked, that, on account of the uneven surfaces, there is danger of making the distances too much rather than falling short of the true measure.

To plot the foregoing Field from the several Latitudes and Meridian Distances, without the use of the protractor, or the line of Chords.

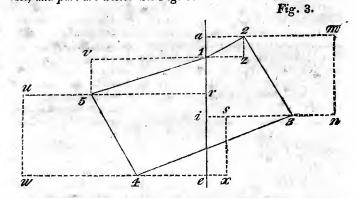
First, set the northing of the first line from 1 to s; set the northing of the second line from s to n; set the northing of the third line from n to m; set the southing of the fourth line from m to a; set the southing of the fifth line from a to z; next, from these points, draw parallels of latitude perpendicular to the meridian; then, on these parallels of latitude, set the meridian distances of the several stations from s to 2, 16.90; from n to 3, 22.11; from m to 4, 80.07; from a to 5, 73.82; from z to 6, 70.33. From one of these last points to another, draw the boundary lines of the field, and if the plan does not perfectiv close, it is because some error was committed in the process, or the scale was incorrect. In practical surveying, it is next to an impossibility in any case, to work so accurately that the survey will exactly close without some correction. The difference between the two columns of latitude, and the two columns of departure, are the legs of a right angled triangle, the hypothenuse of which will be the distance which the survey will fail of closing.

These differences, as before taught in this work, must be balanced, and the column of meridian distances must be formed by the numbers as balanced. When the survey is balanced, and this method of plotting is taken, the parallels of latitude must be laid down according to the balancing, and the map will perfectly close.

When the courses and distances are corrected according to the balancing, they will form a survey which will contain no error.

N. B. Great care must be taken to keep the latitudes parallel and perpendicular to the meridian. The better to effect this, a meridian line may be laid on each side of a sheet, or a half sheet of paper, as the occasion may require.

The following survey is calculated from a meridian running through the map : of course, part of the meridian distances are east, and part are west. See Fig. 3.



				w.	E.	s.	N.	Rods	Courses	NO.
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212.10	-	E. W	8.86 56.92	65.78		23.94		70.00	s.70 00W.	3
2664.50		ww	76.92 96.92	20.00			34.64	40.00	N.30 00W	4
675.53			48.46 00.00		48.46		13.94	50.42	N.74 00E	5
5444.86	173.20									

173.20

2)5271. A. Q. R. 160)2635(16 1 35 160 1035 960

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T 2

The column of meridian distances in this example is formed by adding twice, and subtracting twice against each station, as in the Pennsylvania method. Set the first easting in the upper place, which is the distance from a to 2, being east meridian distance; add it to itself, and it makes 34.64; to this number, add the next easting, and they make 54.64, east meridian distance from a to m; add the same easting again, and they make 74.64; from this number, subtract the first westing, and there remains 8.86 east meridian distance from i to s. As the first westing cannot be subtracted again, the last east meridian distance, 8.86, must be subtracted from the first westing; this crosses the meridian, and gives 56.92 west meridian distance in the lower place. Having crossed the meridian, the westings must now be added, and the eastings subtracted.

To the 56.92 in the lower place, add the last westing, and they make 76.92 west meridian distance from r to u; add the same westing again, and they make 96.92; from this number, subtract the easting of the closing line, and there remains 48.46 west meridian distance, from v to 1, or the easting of the closing line; subtract again, and 00.00 remains. Having completed the column of meridian distances, next multiply the upper number against each station, by its northing or southing, and set the products on the east side of the meridian, in their respective columns of north or south areas; but on the west side of the meridian, the order is reversed; the north products are set in the column of south areas, and the south products are set in the column of north areas. The north area against the first station, is the figure 2zla; the south area against the second station, is the figure mnia; the south area against the third station, is the figure sxie; the south area against the fourth station, is the figure uwer, made by the northing of the fourth line; the south area against the last station, is the figure v5r1.

The foregoing columns of meridian distances might have been commenced, by setting the first easting in the lower place, and the additions and subtractions, made as before directed, and the last subtraction would end in 00.00 at the upper place, against the first station. In this case, as there would be no upper number against the first station, there would be no product in either column of areas against it. The east meridian distance against the second station would extend no further east than the third station, and the meridian distance against the third station, would be on the west side of the meridian; and the meridian distances, against the fourth and fifth stations, would extend as much farther west, as the easting of the first line.

The products against the second, fourth, and fifth stations, would be set in the column of south areas, and that against the third station, on account of its being on the west side of the meridian, would be placed in the column of north areas, and would be subtracted from the footing of the south areas.

When a survey is calculated from a meridian running through the map, it is always best to set the first departure in the lower place, as it saves one multiplication.

On Distributing Estates.

A farm is to be distributed among a number of heirs. survey is made, and the difference between the columns of latitude, and between those of departure, are two rods for each. The survey is balanced, and calculated arithmetically, and is found to contain two hundred acres. The surveyor next draws. his map, by which the divisions are to be made, according to the courses and distances. The plan does not close by nearly two rods and three-quarters. He next corrects the lines, and makes the map close as well as he can; and when the divisions are made, they may not agree with the first calculation by two or three acres, or more. Should the map be drawn as before directed, by the meridian distances and the latitudes as balanced, it would close, and would be in exact conformity to the calculation made arithmetically. If the divisions are made arithmetically, without the use of the scale and dividers, the calculations must be made according to the balancing, or the divisions will not agree with the first calculation.

It will be acknowledged by every experienced surveyor, that it is a difficult matter to make the amount of a considerable number of divisions agree with the whole, when calculated by itself.

It is the common practice in distributions, to make the divisions with scale and dividers; this method will answer very well provided the map is drawn on a large scale.

The following is a useful rule in dividing lands, when any quantity is to be added to, or taken from, a division in the form of a triangle.

Having the area, the contained angle, and one side of a triangle given, to find the adjoining side, including the angle.

Rule. Bullin - Rule.

To the sine of the given angle, or its supplement if obtuse, add the logarithm of the given side; subtract radius from this sum, and subtract the remainder from the logarithm of the double area, the last remainder will be the logarithm of the side required.

In taking a survey, go around with the sun, not that you can work more correctly, or that it will have any effect in calculating, but when you put your courses and distances on your map they will follow around with the lines, from the left to the right.

Wherever you begin, set your compass on the angle and cause a stake or a flag-staff to be erected at the next. When your line runs over a hill, cause a stake to be erected at each end of it, and take your station on the top of the hill, directly between them. If bushes obstruct the sight, make an offset, or set your compass a little distance from the line, from whence you may see the back flag, and cause the forward flag or stake to be set against the bound in a direction with the compass and the back flag. When the line is measured, measure the distance from the flag to the bound, and calculate your true course by Trigonometry. If your next line is of such a distance that you cannot see through the whole length of it, run as near the true line as you can, and if you do not exactly strike the bound, measure the distance from the termination of your random line, and calculate your course as before directed, or if you can discover a tree standing near the termination of your line, take the course and distance to that, thence to the bound, and calculate your true course and distance.

By practice and experience, a method for taking courses will soon become familiar, in all cases. In measuring hills and inclined surfaces, the horizontal distances must be taken. A plummet should be suspended from the end of the chain, when it is levelled. Where hills are very steep, the surveyor should assist the chainmen, and when the best is done in levelling and plumbing the chain, judgment must frequently be called into exercise. Even when rises and descents are easy, there is danger of making too much measure. In such cases, chainmen often make allowances, but the surveyor would do better to keep them to close measure, and from the shape of the ground judge himself what allowances ought to be made. If he is experienced in his business, he will form a more correct judgment

10.0

- 1 - 1 - -

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than inexperienced chainmen. Particular care must be taken that the chain is carried on a straight line, and that it is well straightened. When a tally is ended, and the hinder chainman brings up the sticks, they must be counted.

When on counting the sticks it is discovered that one is lost, the chainmen should not leave the chain and go back to find it, but, from the last mark, should measure back to the point where the tally began, to see whether one chain is lost from their measure. Many blunders in this way have been left undetected by not taking this care.

A careful accurate chainman never lost a stick or miscounted a tally. Young surveyors should practice much for their own instruction, and should make correct practice familiar, before they offer their services. It is as necessary that they should spend some time in acquiring a practical knowledge, as it is that they should spend any time in acquiring a knowledge of theory.

A young surveyor should bear in mind that if he is detected in one error in the beginning of his practice, it will be more to his disadvantage than to be detected in two when he shall be well established. If an error is committed in a survey, it is not against the surveyor provided he detects and corrects it, but if he cannot detect and correct his own errors, that is sufficient evidence of his deficiency in point of knowledge and skill.

Form of a Field Book.

Beginning at a murstone at the southwest corner,

Rods Links

1. N. 25° 00' E. 40 00 to a white-oak tree, 2: N. 10 00 E. 30 00 to a heap of stones, 3. N. 75 00 E. 60 00 to a maple tree, 4. S. 10 00 W. 36 00 to a pine tree, 5. S. 5 00 W. 40 00 to a spruce tree, 6. S. 85 05 W. 70 12 to the place of begin

6. S. 85 05 W. 70 12 to the place of beginning. When a survey is calculated by chains and links, the numbers are less than when it is calculated by rods and decimal parts. Every method by which the numbers are diminished is an improvement. In a hilly country, the two-pole chain is preferable and is more commonly used, because it can be levelled better.

Hills are often found so steep that even the two-pole chain cannot be levelled.

MISCELLANEOUS.

When a survey is calculated by chains and links, and the contents stand in acres and decimal parts of an acre, it may be multiplied by the price of an acre, and the product will be the amount.

EXAMPLE.

A piece of land, 12 chains and 25 links in length, and 10 chains and 25 links in breadth, is sold for \$20 25, per acre;—what is the price of it?

	Length 12.25 Freadth 10.25
1	6125
	2450 1225
Acres and decimal pa Price of an a	
	6278125
	2511250 2511250

Answer \$254,26.40625

The writer of these pages knows not who invented the following rules for finding contained angles. For plainness, none of the kind exceeds them.

N. 62° E. N. 44 W.) When the first letters are alike, and the two
	{ last are unlike, add the degrees of both courses
) together, which gives the contained angle.

When the two first and the two last letters are alike, subtract one course from the other, and the remainder will be the contained angle.

When the two first letters are unlike, and the two last alike, add both courses together, and subtract their sum from 180, the remainder will be the contained angle.

W. When the two first and the two last letters are unlike, subtract one course from the other, the remainder from 180, and the remainder will be the contained angle.

Application of the above Rules.

Two courses are given, viz. N. 67º W. and N. 28º E. to find

570 25	
	570 25

S. 72° E.

S. 25 E.

N. 64° E.

S. 35 E.

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APPENDIX.

the angle .- Suppose yourself standing at the point where these courses meet. Reverse the letters of the first course, and they will stand thus.

> S. 67º E. ? The third rule applies in this N. 28 E. Case.

When the quantity of any angle in a survey is wanted, the preceding course must be reversed ; then both courses will run from the same point.

Converging of Meridians.

The breadth of a degree of longitude in any parallel of latitude is to the breadth of a degree upon the equator, as the Co-sine of that Lat. is to Radius.

R. : 60 Miles : : Co-sine of the Lat. : the breadth of a degree on that Lat.

As Radius - Is to 60 Miles, - So is Co-sine Lat. 60°	10.00000 1.77815 9.69897
	11.47712 10.00000
To 30 Miles -	1.47712

MISCELLANEOUS QUESTIONS.

1. At a certain point I took the elevation of a tower 3° 15' -then measured toward the tower on an angle of depression 7º 333 feet to a level with the base of the tower, when I took the elevation again 8° .- Required the height of the tower and the distance from the second place of observation to the base ; also how much higher the land was at the place of the first observation than at the second.

Ans.—Height, 99.6 feet.
Distance required, - 708.6 feet.
Difference in the height of land, 40.58 feet.
2. Two persons made observations on the altitude of a me-
teor, both being on the same side of it, and in a vertical plane
passing through it. The distance of their stations were 200
rods apart, and at one the angle of elevation was 36° 25', at
the other 32° 50', and at the last the outer limb of the meteor

APPENDIX.

subtended an angle of 2'.--Required the distance from the last place of observation, also the height and diameter of it.

M. Q. R. Answer.-The distance, 5 .. 3 .. 60 Height, 3 .. 0 .. 70

Diameter, 18 feet 2 inches.

3. From the top of a steeple 165 feet high, the angle of depression of the nearest bank of a river is 11° 15', that of the opposite bank is 6° 15'. Required the width of the river. Answ. 41.13 rods.

4. What length of cart-tire will it take to band a wheel 5 feet in diameter ? Answ. 15 feet 8 1-2 inches.

5. A gentleman laid out a garden in a circle, containing one acre, one quarter, and one rod, with a gravelled walk on the outer side of it within the circle which took up twelve rods of ground. What is the diameter of the circle, and what is the width of the walk ? Answ. The diameter 16 rods-Width of the walk 4 feet.

6. Neptune laid out 1000 square miles of the surface of the sea in a circle, and sold to Aeolus all that part of it which lies without a concentric circle of one third of the diameter. What is the diameter, and how much was sold ?

Answ. The diameter 35.68 miles. The quantity sold 888.92 square miles. 7. A Farmer laid out an elliptical orchard, the longest diameter of which was 30 rods, and the shortest was 20 rods, and surrounded the same with a wall two feet thick, within the figure. What is the quantity within the wall, and how much is covered by it? A. Q. R.

Within the wall 2 .. 3 .. 22 Answ.

Covered by the wall, 9.3 rods.

8. From a point in an equilateral triangle, I measured the distances to each corner, and found them 20, 29, and 30 rods. Required the area and the length of the sides.* A. Q. R.

Answ. The Area 5 .. 1 .. 33

Length of each side 45 rods.

9. Required the dimensions of a parallelogram, containing one acre and a half, bounded by 64 rods of fence. Answ. 12 by 20 rods.

10. The area of a parallelogram is five acres one quarter and thirty-five rods, and the diagonal is forty-three rods. Required the length of the sides. Answ. 35 by 25 rods.

11. Required the dimensions of a parallelogram containing twenty-six acres one quarter and twenty-four rods, when the length exceeds the breadth by fifty-two rods. Answ. 44 by 96 rods.

12. Required the dimensions of a parallelogram containing 250 acres, when the sides are in the proportion of 7 to 3. Answ. 130.93 by 305 1-2.

13. The state of Connecticut contains a little upwards of 4828 square miles, or 3,090,000 acres, including rivers, harbours, creeks, roads, &c. if this quantity of land is laid in a square, what will be the length of each side ? M. Q. R.

Answ. 69 .. 1 .. 75.11

Note. In the Preface, it is observed that the Traverse Table in this book is calculated for any distance up to 50. After the Preface was printed, it was thought best to extend that Table to 70. The table of Logarithms is also much more extensive, than is noticed in the Preface.

* This may be solved geometrically.

MATHEMATICAL TABLES.

VIZ :

- 1. A Table of Logarithms for Numbers. 11. A Table of Logarithmic or Artificial Sines, Tangents, and Secants.
- 111. A Traverse Table, or Table of Difference of Latitude and Departure.

IV. A Table of Natural Sines.

I. A TABLE OF LOGARITHMS FOR NUMBERS.

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is

3.81578

APPENDIX.

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ERRATA.

Appendix, page 89, line 22, for "less," read legs. 94 line 25, for "from 2 to 1" read from 2 to S. 98 line 33, for "columns" read column. 66 "

" 101 line 25, for "murstone," read meerstone. 1.3 In the engraving on page 04 of the appendix, and opposite the second angle (near the figures 16, 90) should have been inserted the figure 2; this deficiency, can easily be supplied by the pen or pencil.

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The Log. of	6543	is	3.81578
	654.3	-	2.81578
	65.43	-	1.81578
	6.543	-	0.81578

The Log. of a Decimal Fraction is the same as that of an Integer, only the Index is negative, and is distinguished from a positive one, by placing a Point, or a negative Sign before it : Thus,

The Log. of 0.6543	is	.9.81578 or -1.81578.
0.06543	-	.8.81578 or -2.81578.

Note.—In the following Table the Index is not prefixed. It may be easily supplied as it is always a unit less than the number of figures in the corresponding natural whole number.

LOGARITHMS.

To find the Logarithm of any Number.

If the Number is less than 100, its Log. is found in the first page of the Table, directly opposite thereto: Thus, the Log. of 34 is 1.53148.

If the Number consists of three figures, find it in the first column of the following part of the Table, opposite to which, and under 0, is the Log. : Thus the Log. of 346 is .53908 to which prefix 2 for the Index, because there are three places of figures in the whole Number.

If the given Number contains four figures, the first three are to be found, as before, in the side column, and under the fourth at the top of the table is the Log. to which the Index 3 is to be prefixed, if the given Number is an Integer : Thus the Log. of 3467 is .53995 to which prefix 3 for the Index.

If the given Number exceeds four figures, find the difference between the Log. of the first four figures, and the next following Log. Multiply this difference by the remaining figure or figures in the given Number; point off as many figures to the right hand as there are in the multiplier; and the remainder, added to the Log. of the first four figures, will be the required Log.

To find the Number corresponding to any given Logarithm.

Find the next less Log. to that given in the column marked 0 at the top, and continue the sight along that horizontal line, and the Log. the same as that gives, or very near it, will be found; then the first three figures of the corresponding Number will be found opposite, in the first side column, and the fourth figure directly above, at the top of the page. If the Index of the given Log. is 3, the four figures thus found are whole numbers; if the Index is 2, the first three figures are whole numbers, and the fourth is a Decimal, and so on.

To find the nearest number corresponding to any Log. for more than four figures, find the Log. next less than the given one, and take the difference between that and the given one; also take the difference between the next greater and the next less Log. than the given one; divide the former difference by the latter, according to the Rule in Division of Decimals for dividing a less number by a greater; add the Quotient to the number answering to the Log. next less than the given one, and you will have the required Number; whether a whole, or a mixed Number will be determined by the Index.

The addition and subtraction of Logarithms answers the same purpose as the multiplication and division of their corres-

LOGARITHMS.

ponding Numbers : That is, the Log. of any two Numbers being added, their sum will be the Log. of the Product of those Numbers ; and the Log. of one Number being subtracted from the Log. of another Number, the Remainder will be the Log. of the Quotient of one of those Numbers divided by the other. Again, the Log. of any Number being doubled will produce the Log. of the Square of that number ; and one half the Log. of any Number is the Log. of the Square Root of that Number.

II. Of the Table of Logarithmic or Artificial Sines, Tangents, and Secants.

To find the Logarithmic Sine, S.c. for any number of Degrees and Minutes, within the compass of the Table.

If the Degrees be less than 45, look for them at the top of the columns, and under Sine, Tangent or Secant, whichever is wanted, and for the Minutes at the left hand; but if more than 45, look for the Degrees at the bottom over Sine, &c. and for the Minutes at the right hand; under or over the Degrees and against the Minutes will be the required Log. Sine, &c.

To find the Degrees and Minutes corresponding to a given Logarithmic Sine, &c.

Look in the proper column for the nearest Log. to the given one; and the Degrees and Minutes standing over or under and against it, are those required.

Note. When the Log. Sine, &c. for more than 90° is re-

quired, subtract the given number of Degrees from 180°, and make use of the Remainder.

It will be observed that this Table is calculated only for every 5 Minutes. This was thought sufficient for Surveyors, as few Compasses will take a course to greater exactness. If, however, a Question is to be solved where greater accuracy is required, work by natural Sines. Or,

The Log. Sine, &c. for any Minute may be found as follows:

Look in the Table for the Log. of the nearest number of Minutes greater than the given one, and from this subtract the next less Log. contained in the Table : Then say, as 5 Minutes, is to this difference; So is the excess of the given Minutes above 5, 10, 15, 20, 25, &c.; To a fourth number, which add to the Log. of the Minutes next less than the given number, and the sum will be the Log. required.

LOGARITHMS,

EXAMPLE.

Required the Logarithmic Sine Sine of	of 34° 23' 34° 25' 34 20	9.75221 9.75128
	Difference	93
As 5 : 93 : : 3 : 56 Sine of 34° 20'	9.75128	
Add	- 56	
Sine of 34° 23'	9.75184	

To find the nearest Minutes corresponding to a given Logawithmic Sine, &c.

Look in the Table, in the proper column, for the Log. next less than the given one, and take the difference between that and the given one; also take the difference between the next greater and the next less Log. than the given one; Then say, As the latter difference; is to 5 Minutes; so is the former difference; to the number of Minutes to be added to the Minutes of the Log. next less than the given one.

EXAMPLE.

Required the Degrees and Minutes corresponding to the Logarithmic Tangent 9.73597.

Given Log.		Next greater Log.	9.73627
Next less		Next less -	9.73476
Difference	121	Difference	151

As 151 : 5 : : 121 : 4

The Degrees and Minutes for the Log, next less than the given one are 28° 30' to which add 4' and it makes 28° 34'.

Note. As after the most careful attention of the Printers some figures in the Table may be wrong; and as some may be so blurred as to be illegible, let it be observed, that the Sines and Co-Secants, the Co-Sines and Secants, and the Tangents and Co-Tangents, standing against each other respectively, being added together, will amount to 20,00000, if the Tables are accurate. Thus against 28° 20' the Sine 9.67533 added to the Co-Secant 10.3236~

LOGARITHMS.

their sum is 20.00000; so also is the sum of the Co-Sine 9.94458 and the Secant 10.05542, and likewise the sum of the Tangent 9.73175 and the Co-Tangent 10.26825. An error may consequently be easily detected, or any defaced figure be supplied.

To calculate the Northing or Southing, &c. for any Course and Distance by Logarithms.

This is done by the first CASE of RIGHT ANGLED TRIGONOME-TRY, as follows :

Find the Log. Sine and Co-Sine of the Course; to each of these add the Log. of the Distance; subtract Radius or 10.00000 from their sums, and the remainders will be the Log. of the required Latitude and Departure.

Note. When the Angle is very small or very large, and the Distance short, the sum of the Log. Sine or Co-Sine and the Log. of the Distance may be less than 10.00000 or Radius, which cannot therefore be subtracted. In such cases look for the Log. without regard to the Index, and the corresponding number will be a Decimal, the first figure of which will be tenths if the Index be 9, and hundredths if the Index be 8.

Ν	o. 1-100).				Log	. 0.00000	-2.	00000.
N.	Log.	N.	Log.	N.	Log.	N.	Log.	N.	Log.
1	0.00000	21	1.32222	41	1.61278	61	1.78533		1.90849
2	0.30103	22	1.34242	42	1.62325	62	1.79239		1.91381
3	0.47712	23	1.36173	43	1.63347	63	1.79934		1.91908
$\frac{4}{5}$	0.60206	24	1.38021	44	1.64345	64	1.80618		1.92428
	0.69897	25	1.39794	45	1.65321	65	1.81291	85	1.92942
6	0.77815	26	1.41497	46	1.66276	66	1.81954	86	1.93450
7	0.84510	27	1.43136	47	1.67210	67	1.82607	87	1.93952 1.94448
8	0.90309	28	1.44716	48	1.68124	68	1.83251	88 89	1.94445
9	0.95424	29	1.46240	49	1.69020	69	1.83885	- 89 - 90	1.94939
10	1.00000	_30	1.47712	50	1.69897	70	1.84510		
11	1.04139	31	1.49136	51	1.70757	71	1.85126	91	1.95904
12	1.07918		1.50515	52	1.71600	72	1.85733	92	1.96379
13	1.11394	33	1.51851	53	1.72428	73	1.86332	93	1.96848
14	1.14613	34	1.53148	54	1.73239	74	1.86923	94	1.97313
15	1.17609	35	1.54407	55	1.74036	75	1.87506	95	1.97772
16	1.20412	36	1.55630	56	1.74819	76	1.88081	96	1.98227
17	1.23045	37	1.56820	57	1.75587	77	1.88649	97	1.98677 1.99123
18	1.25527	38	1.57978	58	1.76343	78 79	1.89209 1.89763	98 99	1.99123
19	1.27875	39	1.59106	59	1.77085			100	2.00000
20	1.30103	40	1.60206	60	1.77815	801	1.903091	100	2.000004

A TABLE OF LOGARITHMS.

N	0. 100	-1600					Log	. 00000)-204	12.
NO.	0	1	2	3	4	5	6	7 1	8	9
100		00043								00389
101 102	0432 0860	0475 0903	0518	0561	0604	0647	0689	0732	0775	0817
102	1284	1326	0945 1368	0988 1410	1030 1452	1072 1494	$1115 \\ 1536$	1157 1578	1199 1620	1242 1662
104	1703	1745	1787	1828	1870	1912	1953	1995	2036	2078
105	2119	2160	2202	2243	2284	2325	2366	2407	2449	2490
106	2531	2572	2612	2653	2694	2735	2776	2816	2857	2898
107 108	2938 3342	2979 3383	3019	3060	3100	3141	3181	3222	3262	3302
108	3743	3782	3423 3822	3463 3862	3503 3902	3543 3941	3583 3981	3623 4021	3663 4060	3703
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111	4135	4179	4218	4258	4297 4689	4336 4727	4376 4766	4415 4805	4454 4.844	4493 4883
112	4922	4961	4999	5038	5077	5115	5154	5192	5231	5269
113	5308	5346	5385	5423	5461	5500	5538	5576	5614	5652
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118	7188	7225	7262	7298	6967 7335	7004 7372	7041 7408	7078	7115	7151
119	7555	7591	7628	7664	7700	7737	7773	7809	7846	7882
120	7918	7954	7990	8027	8063	8099	8135	8171	8207	8243
121	8279	8314	8350	8386	8422	8458	8493	8529	8565	8600
122	8636	8672	8707	8743	8778	8814	8849	8884	8920	8955
123		9026	9061	9096	9132		9202	9237	9272	9307
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126		10072					10243		10312	10003 0346
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128		0755		0823	0857		0924	0958	0992	1025
129				1160	1193	1227	1261	1294	1327	1361
130				1494	1528		1594		1661	1694
131 139									1992	2024
13									2320 2646	2352 2678
13									2969	3001
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13										4270
14	-	_	-							4891
14										
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15									812	8156
15 15										
15										
15	5 903									
15	6 931	2 934								
15							8 975	6 978	981	9838
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162	0952	0978	1005	1032	1059	1085	1112	1139	1165	1192
163	1219	1245	1272	1299	1325	1352	1378	1405	1431	1158
164	1484	1511	1537	1564	1590	1617	1643	1669	1696	1722
165	1748	1775	1801	1827	1854	1880	1906	1932	1958	1985
166	2011	2037	2063	2089	2115	2141	2167	2194	2220	2246
167	2272	2298	2324	2350	2376	2401	2427	2453	2479	2505
168	2531	2557	2583	2608	2634	2660	2686	2712	2737	2763
169	2789	2814	2840	2866	2891	2917	2943	2968	2994	3019
170	3045	3070	3096	3121	3147	3172	3198	3223	3249	3274
171	3300	3325	3350	3376	3401	3426	3452	3477	3502	3528
172	3553	3578	3603	3629	3654	3679	3704	3729	3754	3779
173	3805	3830	3855	3880	3905	3930	3955	3980	4005	4030
174	4055	4080	4105	4130	4155	4180	4204	4229	4254	4279
175	4304	4329	4353	4378	4403	4428	4452	4477	4502	4527
176	4551	4576	4601	4625	4650	4674	4699	4724	4748	4773
177	$4797 \\ 5042$	4822	4846	4871	4895	4920	4944	4969	4993	5018
178 179	5042 5285	5066	5091	5115	5139	5164 5406	5188	5212	5237	5261
		5310	5334	5358	5382		5431	5455	5479	5503
1180	5527	5551	5575	5600	5624	5648	5672	5696	5720	5744
181	5768	5792	5816.	5840	5864	5888	5912	5935	5959	5983
182	6007	6031	6055	6079	6102	6126	6150	6174	6198	6221
183	6245	6269	6293	6316	6340	6364	6387	6411	6435	6458
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185	6951	$6741 \\ 6975$	6764 6998	6788 7021	6811 7045	7068	6858 7091	6881	6905	6928
187	7184	7207	7231	7254	7277	7300	7323	7114 7346	7138 7370	7161
188	7416	7439	7462	7485	7508	7531	7554	7540	7600	7393 7623
189	7646	7669	7692	7715	7738	7761	7784	7807	7830	7852
190	7875	7898			7967	7989	8012			
190	8103	8126	7921 8149	7944	8194	8217	8012 8240	8036	8058	8081
191	8330	8353	8149	8171 8398	8421	8443	8240	8262	8285	8307
192	8556	8578	8601	8623	8646	8668	8691	8488 8713	8511 8735	8533 8758
194	8780	8803	8825	8847	8870	8892	8914	8937	8959	8981
195	9003	9026	9048	9070		9115	9137	9159		9203
196	9226	9248	9270	9292	9314	9336	9358			9425
197	9447	9469	9491	9513	9535	9557	9579	9601	9623	9645
198	9667	9688	9710	9732	9754	9776	9798			9863
199		9907	9929	9951	9973	9994		30038		
200	30103	30125			30190	30211	0233	0255		0276
201	0320	0341	0364	0384		0428	0449		0270	0270
202		0557	0578	0600		0643	0664	0685		0728
203		0771	0792	0814		0856	0878	0899		0942
204		0984	1006	1027	1048	1069	1091			1154
205	1175	1197	1218	1239			1302	1323		1366
206	1387	1408	1429	1450		1492	1513	1534		1576
207		1618	1639	1660		1702	1723		1765	1785
208		1827	1848	1869			1931		1973	1994
209	2015	2035	2056	2077	2098	2118	2139	2160	2181	2201
210		2243		2284			2346	2366	2387	2408
211	2428	2449		2490			2552			
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213	2838	2858		2899						3021
214	3041	3062		3102						3224
215	3244			3304						
216	3445			3506						
217										
218							3965			4025
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220					34321		34361		34400	
221	4439	4459	4479	4498	4518	4537 4733	4557	4577	4596 4792	4616
$\frac{222}{223}$	4635 4830	4655 4850	4674 4869	4694 4889	4713 4908	4928	4753 4947	4772 4967	4792	4811 5005
224	5025	5044	5064	5083	5102	5122	5141	5160	5180	5199
225	5218	5238	5257	5276	5295	5315	5334	5353	5372	5392
226		5430	5449	5468	5488	5507	5526	5545	5564	5583
227	5603	5622	5641	5660	5679	5698	5717	5736	5755	5774
$\frac{228}{229}$		5813 6003	5832 6021	5851 6040	5870 6059	5889 6078	5908 6097	5927 6116	5946 6135	5965 6154
1			-	6229	6248				6324	
230 231		6192 6380	$6211 \\ 6399$	6229	6248 6436	$6267 \\ 6455$	$\begin{array}{c} 6286\\ 6474 \end{array}$	6305 6493	6524	6342 6530
232		6568	6586	6605	6624	6642	6661	6680	6698	6717
233	6736	6754	6773	6791	6810	6829	6847	6866		6903
234	6922	6940	6959	6977	6996	7014	7033	7051	7070	7088
235		7125	7144	7162	7181	7199	7218	7236	7254	7273
236 237		7310	7328	7346		7383	7401	7420	7438 7621	7457
238		7493	7511 7694	7530		$7566 \\ 7749$	7585 7767	7603	7803	7639 7822
239		7858	7876	7894		7931	7949	7967	7985	8003
240	-	8039	8057	8075		8112	8130	8148	8166	8184
241			8238	8256		8292	8310	8328	8346	8364
242	8382		8417	8435		8471	8489	8507	8525	8543
243		8578		8614		8650	8668	8686	8703	8721
244				8792		8828	8846	8863	8881	
243 240		8934 9111	8952 9129	8970 9146		9005 9182	9023 9199	9041 9217	9058 9235	9076 9252
24				9322		9358	9375	9393	9410	9428
248						9533		9568		9602
24						9707	9724	9742	9759	
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25						40054				
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25 25				0364		0398			0449	0466
25	4 0483 5 0654					0739			0790	0807
25	6 0824					0909				0976
25	7 0993	3 1010	1027	1044	1 1061	1078	1095	1111	1128	1145
25						1246				
25		1347			-	1414			1464	
26						1581		1614		1647
26						1747				1814
26 26			$ \begin{array}{c cccccccccccccccccccccccccccccccccc$			1913 2078				
26										
26	5 232			2378	5 2390	2406	2423	2439	2455	2472
26	6 2488	3 2504								2635
26	7 265					2732				2797
26 26	8 2813 9 297					2894 3056				
27	-	-	-			3217	1	*		
27						3377				
27						3537				
27	3 361	6 3639	2 3648	3 3664	4 3680	3696	3712	3727	3743	3759
27	4 377.									
27										4075
27										4232
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27	19 456									4700
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283	5179			5225	5240	5255	5271	5286	5301	5317
284	5332			5378	5393	5408			5454	5469
285	5484	5500	5515	5530	5545	5561	5576	5591	5606	5621
286	5637	5652	5667	5682	5697	5712	5728	5743	.5758	5773
287	5788	5803	5918	5834	5849	5864	5879	5894	5909	5924
288	5939	5954	5969	5984	6000	6015	6030	6045	6060	6075
289	6090	6105	6120	6135	6150	6165	6180	6195	6210	6225
290	6240	6255	6270	6285	6300	6315	6330	6345	6359	6374
291	6389	6404		6434	6449	6464	6479	6494		6523
292	6538	6553		6583	6598	6613	6627	6642		6672
293	6687			6731	6746	6761	6776			6820
294	6835	6850	6864	6879	6894	6909	6923	6938	6953	6967
295	6982	6997	7012	7026	7041	7056	7070	7085	7100	7114
296	7129	7144	7159	7173	7188	7202	7217	7232	7246	7261
290	7276	7290	7305	7319	7334	7349	7363	7378	7392	7407
298	7422	7436	7451	7465	7480	7494	7509	7524	7538	7553
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301	7857	7871	7885	7900	7914	7929	7943	7958	7972	7986
302	8001	8015	8029	8044	8058	8073	8087	8101	8116	8130
303	8144	8159	8173	8187	8202	8216	8230	8244	8259	8273
304	8287	8302	8316	8330	8344	8359	8373	8387	8401	8416
305	8430	8444	8458	8473	8487	8501	8515	8530	8544	8558
306	8572	8586	8601	8615	8629	8643	8657	8671	8686	8700
307	8714	8728	8742	8756	8770	8785	8799	8813	8827	8841
308	8855	8869	8883	8897	8911	8926	8940	8954	8968	8982
309	8996	9010	9024	9038	9052	9066	9080	9094	9108	9122
310	9136	9150	9164	9178	9192	9206	9220	9234	9248	9262
311	9276	9290	9304	9318	9332	9346	9360	9374	9388	9402
312	9415	9429	9443	9457	9471	9485	9499	9513	9527	9541
313	9554	9568	9582	9596	9610	9624	9638	9651	9665	9679
314	9693	9707	9721	9734	9748	9762	9776	9790	9803	9817
315	9831	9845	9859	9872	9886	9900	9914	9927	9941	9955
316	9969	9982	9996		50024	50037	50051	50065		50092
	50106	50120	50133	0147	0161	0174	0188	0202	0215	0229
318	0243	0256	0270	0284	0297	0311	0325	0338	0352	0365
319	0379	0393	0406	0420	0433	0447	0461	0474	0488	0501
320	0515	0529	0542	0556	0569	0583	0596	0610	0523	0637
21	0651	0664	0678	0691	0705	0718	0732	0745	0759	0772
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123	0920	0934	0947	0961	0974	0987	1001	1014	1028	1041
24	1055	1068	1081	1095	1108	1121	1135	1148	1162	1175
25	1188	1202	1215	1228	1242	1255	1268	1282	1295	1308
26	1322	1335	1348	1362	1375	1388	1402	1415	1428	1441
27	1455	1468	1481	1495	1508	1521	1534	1548	1561	1574
28	1587	1601	1614	1627	1640	1654	1667	1680	1693	1706
29	1720	1733	1746	1759	1772	1786	1799	1812	1825	1838
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31	1983	1996	2009	2022	2035	2048	2061	2075		
32	2114	2127	2140	2153	2055	2179	2192	2075	2088 2218	2101 2231
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334	2375	2388	2401	2414	2427	2310	2323			
35	2504	2500	2530	2414 2543		2569		2466	2479	2492
336	2634	2647			2556		2582	2595	2608	2621
337	2034 2763	2776	2660 2789	2673	2686 2815	2699	2711	2724	2737	2750
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345	3782	3794	3807	3820	3832	3845	3857	3870	3882	3895
346	3908	3920	3933	3945	3958	3970	3983	3995	4008	4020
347	4033	4045	4058	4070	4083	4095	4108	4120	4133	4145
348	4158	4170	4183	4195	4208	4220	4233	4245	4258	4270
349	4283	4295	4307	4320	4332	4345	4357	4370	4382	4394
350	4407	4419	4432	4444	4456	4469	4481	4494	4506	4518
351	4531	4543	4555	4568	4580	4593	4605	4617	4630	4642
352	4654	4667	4679	4691	4704	4716	4728	4741	4753	4765
353	4777	4790	4802	4814	4827	4839	4851	4864	4876	4888
354	4900	4913	4925	4937	4949	4962	4974	4986	4998	5011
355	5023	5035	5047	5060	5072	5084	5096	5108	5121	5133
356 357	5145	5157	5169	5182	5194 5315	5206 5328	5218 5340	5230 5352	5242 5364	5255 5376
358	5267 5388	5279 5400	5291 5413	5303 5425	5315	5449	5461	5352	5485	5497
359	5509	5522	5534	5546	5558	5570	5582	5594	5606	5618
360	5630	5642	5654	5666	5678	5691	5703	5715	5727	5739
361	5751	5763	5775	5787	5799	5811	5823	5835	5847	5859
362	5871	5883	5895	5907	5919	5931	5943	5955	5967	5979
363	5991	6003	6015	6027	6038	6050	6062	6074	6086	6098
364	6110	6122	6134	6146	6158	6170	6152	6194	6205	6217
365	6229	6241	6253	6265	6277	6289	6301	6312	6324	6336
366	6348	6360	6372	6384	6396	6407	6419	6431	6443	6455
367	6467	6478	6490	6502	6514	6526	6538	6549	6561	6573
368	6585	6597	6608	6620	6632	6644	6656	6667	6679	6691
369	6703	6714	6726	6738	6750	6761	6773	6785	6797	6808
370	6820	6832	6844	6855	6867	6879	6891	6902	6914	6926
371	6937	6949	6961	6972	6984		7008		7031	7043
372	7054	7066	7078	7089	7101	7113	7124		7148	7159
373	7171	7183	7194	7206	7217		7241	7252	7264	7276
374	7287	7299	7310	7322	7334		7357			7392
375 376	7403 7519	7415	7426	7438	7449		7473	7484		7507
377	7634	7646	7657	7669	7680		7703			7738
378	7749	7761	7772	7784	7795		7818			7852
379	7864	7875	7887	7898			7933			7967
380	7978	7990	8001	8013		-	8047	-	-	8081
381	8092	8104	8115							8195
382	8206	8218	8229							8309
383	8320	8331	8343							8422
384	8433	8444	8456	8467	8473	8490	8501			
385	8546	8557	8569							
386	8659	8670	8681	8692						
387	8771	8782	8794							8872
388	8883		8906							
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391	9218									9318
392	9329	9340 9450								
393 394	9439 9550									
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397	9879						9945			
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402	0423	0433	0444	0455	0466	0477	0487	0498	0509	0520
403 404	0531 0638	0541 0649	0152	0563	0574	0584	0595	0606	0617	0627
404	0746	0756	0767	0670 0778	0681 0788	0692 0799	0703 0810	0713 0821	0724 0831	0735 0842
406	0853	0863	0874	0885	0895	0906	0917	0821	0938	0842
407	0959	0970	0981	0991	1002	1013	1023	1034	1045	1055
408	1066	1077	1087	1098	1109	1119	1130	1140	1151	1162
409	1172	1189	1194	1204	1215	1225	1236	1247	1257	1268
410	1278	1289	1300	1310	1321	1331	1342	1352	1363	1374
411	1384	1395	1405	1416	1426	1437	1448	1458	1469	1479
412 413	1490 1595	1500 1606	1511 1616	1521 1627	1532 1637	1542 1648	1553 1658	1563	1574	1584
414	1700	1711	1721	1731	1742	1752	1763	1669 1773	1679 1784	1690 1794
415	1805	1815	1826	1836	1847	1857	1868	1878	1888	1899
416	1909	1920	1930	1941	1951	1962	1972	1982	1993	2003
417	2014	2024	2034	2045	2055	2066	2076	2086	2097	2107
418 419	2118 2221	2128 2232	2138	2149	2159	2170	2180	2190	2201	2211
			2242	2252	2263	2273	2284	2294	2304	2315
420	2325	2335	2346	2356	2366	2377	2387	2397	2408	2418
$\frac{421}{422}$	2428 2531	2439 2542	2449 2552	2459 2562	2469 2572	2480 2583	2490	2500 2603	2511 2613	2521 2624
423	2634	2644	2655	2665	2675	2685	2696	2603	2613	2624
424	2737	2747	2757	2767	2778	2788		2808	2818	2829
425	2839	2849	2859	2870	2880			2910		2931
426	2941	2951	2961	2972	2982			3012	3022	3033
427	3043	3053	3063	3073	3083			3114	3124	3134
428 429	3144	3155	3165	3175	3185	3195	3205	3215	3225	3236
	3246	3256	3266	3276	3286			3317	3327	3337
430 431	3347	3357 3458	3367 3468	3377 3478	3387 3488	3397		3417	3428	3438
432	3548	3558	3568		3589			3518 3619	3528 3629	3538 3639
433	3649	3659	3669	3679	3689			3719	3729	3739
434	3749	3759	3769	3779	3789		3809	3819		3839
435	3849	3859	3869		3889			3919	3929	3939
436	3949	3959	3969		3988			4018	4028	4038
437 438	4048	4058	4068	4078	4088 4187	4098	4108	4118	4128	4137
439	4246	4256	4266		4187			4217 4316	4227 4326	4237
440	4345	4355	4365	4375	4385				4424	4333
441	4444		4305					4414 4513		4434
442	4542		4562		4582		4601	4611	4621	4631
443	4640	4650	4660	4670	4680	4689	4699	4709	4719	4729
444	4738		4758			4787	4797	4807	4816	4826
445	4836					4885		4904	4914	4924
446 447						4982	4992 5089	5002	5011	5021
441			5050		5167	5176	5186	5099 5196	5108 5205	5118 5215
449	5225		5244		5263	5273	5283	5292	5302	5312
450	-	-	5341	5350	5360	5369	5379	5389	5398	5408
451			5437	5447	5456	5466	5475	5485	5495	5504
452	5514	5523	5533	5543	5552	5562	5571	5581	5591	5600
453			5629		5648	5658	5667	5677	5686	5696
454			5725		5744	5753	5763	5772	5782	5792
455 456			5820 5916		5839 5935	5849 5944	5858 5954	5868	5877	5887
450			6011	6020		6039	6049	5963 6058	5973 6068	5982 6077
458					6124	6134	6143	6153	6162	6172
459			6200	6210	6219	6229	6238	6247	6257	6266
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461	6370	6390	6389	6398	6408	6417	6427	6436	6445	6455
462	6464	6474	6483	6492	6502	6511	6521		6539	6549
463	6558	6567	6577	6586	6596	6605	6614	6624	6633	6642
464	6652	6661	6671	6680	6689	6699	6708	6717	6727	6736
465	6745	6755	6764	6773	6783	6792	6801	6811	6820	6829
466	6839	6848	6857	6867	6876	6885	6894	6904	6913	6922
467	6932	6941	6950	6960	6969	6978	6987	6997	7006	7015
468	7025	7034	7043	7052	7062	7071	7080		7099	7108
469	7117	7127	7136	7145	7154	7164	7173	7182	7191	7201
470	7210	7219	7228	7237	7247	7256	7265	7274	7284	7293
471	7302	7311	7321	7330	7339	7348	7357	7367	7376	7385
472	7394	7403	7413	7422	7431	7440	7449	7459	7468	7477
473	7486	7495	7504	7514	7523	7532	7541	7550	7560	7569
474	7578	7587	7596	7605	7614	7624	7633	7642	7651	7660
475	7669	7679	7688	7697	7706	7715	7724	7733	7742	7752
476	7761	7770	7779	7788	7797	7806	7815	- 7825	7834	7843
477	7852	7861	7870	7879	7888	7897	7906	7916	7925	7934
478 479	7943 8034	7952 8043	7961 8052	7970	7979	7988	7997	8006 8097	8015	8024
in succession in the succession of the successio				8061	8070	8079	8088	Summer of the local division of the local di	8106	8115
480	8124	8133	8142	8151	8160	8169	8178		8196	8205
481	8215	8224	8233	8242	8251	8260	8269	8278	8287	8296
482	8305	8314	8323	8332	8341	8350	8359	8368	8377	8386
483	8395	8404	8413	8422	8431	8440	8449	8458	8467	8476
484 485	8485 8574	8494 8583	8502 8592	8511 8601	8520	8529	8538 8628	8547 8637	8556 8646	8565 8655
486	8664	8673	8681	8690	8610 8699	8619 8708	8717	8726	8735	8744
487	8753	8762	8771	8780	8789	8797	.8806	8815	8824	8833
488	8842	8851	8860	8869	8878	8886	8895	8904	8913	8922
489	8931	8940	8949	8958	8966	8975	8984	8993	9002	9011
490	9020	9028	9037	9046	9055	9064	9073	9082	9090	9099
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492	9197	9205	9214	9223	9232	9241	9249	9258	9267	9276
193	9285	9294	9302	9311	9320	9329	9338	9346	9355	9364
494	9373	9381	9390	9399	9408	9417	9425	9434	9443	9452
495	9461	9469	9478	9487	9496	9504	9513	9522	9531	9539
496	9548	9557	9566	9574	9583	9592	9601	9609	9618	9627
497	9636	9644	9653	9662	9671	9679	9688	9697	9705	9714
498	9723	9732	9740	9749	9758	9767	9775	9784	9793	9801
499	9810	9819	9827	9836	9845	9854	9862	9871	9880	9888
500	9897	9906	9914	9923	9932	9940	9949	9958	9966	9975
501	9984	9992	70001	70010	70018	70027	70036	70044		70062
502	70070	70079	0088	0096	0105	0114	0122	0131	0140	0148
503	0157	0165	0174	0183	0191	0200	0209	0217	0226	0234
504	0243	0252	0260	0269	0278	0286	0295	0303		0321
505	0329	0338	0346	0355	0364	0372	0381	0389	0398	0406
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507	0501	0509	0518	0526	0535	0544	0552	0561	0569	0578
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509	0672	0680	0689	0697	0706	0714	0723	0731	0740	0749
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511	0842	0851	0859	0868	0876	0885	0893	0902	0910	0919
512	0927	0935	0944	0952	0961	0969	0978	0986	0995	1003
513	1012	1020	1029	1037	1046	1054	1063	1071	1079	1088
514	1096	1105	1113 1198	1122 1206	1130 1214	1139 1223	1147	1155	1164	1172
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517	1205	1357	1282	1290	1299	1307	1315		1332	1341
517	1349	. 1441	1450	1374	1385	1391	1399	1408 1492	1416 1500	1425 1509
519	1517	1525	1533	1542	1550	1559	1465	1492	1500	1509
	- 0	10.00	2		4		A			
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IN	10. 520	0-58	00.				Los	. 7160	0-76	343.
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521	1684	1692	1700	1709	1717	1725	1734	1742	1750	1759
522	1767	1775	1784	1792	1800	1809	1817	1825	1834	1842
523	1850	1858	1867	1875	1883	1892	1900	1908	1917	1925
524	1933	1941	1950	1958	1966	1975	1983	1991	1999	2008
525 526	2016 2099	2024 2107	2032 2115	2041 2123	2049 2132	2057 2140	2066 2148	2074 2156	2082 2165	2090 2173
520	2099	2189	2198	2206	2132	2140	2230	2130	2105	2255
528	2263	2272	2280	2288	2296	2304	2313	2321	2329	2337
529	2346	2354	2362	2370	2378	2387	2395	2403	2411	2419
530	2428	2436	2444	2452	2460	2469	2477	2485	2493	2501
531	2509	2518	2526	2534	2542	2550	2558	2567	2575	2583
532	2591	2599	2607	2616	2624	2632	2640	2648	2656	2665
533	2673	2681	2689	2697	2705	2713	2722	2730	2738	2746
534	2754	2762	2770	2779	2787		2803	2811	2819	2827
535	2835	2843	2852	2860	2868	2876	2884	2892	2900	2908
536 537	2916	2925 3006	2933 3014	2941	2949 3030	2957 3038	2965 3046	2973	2981 3062	2989 3070
538	2997 3078	3086	3094	3022 3102	3030	3119	3127	3054 3135	3143	3151
539	3159	3167	3175	3183	3191	3199	3207	3215	3223	3231
540	3239	3247	3255	3263	3272	3280	3288	3296	3304	3312
540	3239	3247	3336	3263	3272	3280	3288	3296	3384	3392
542	3400	3408	3416	3424	3432	3440	3448	3456	3464	3472
543	3480	3488	3496	3504	3512	3520	3528	3536	3544	3552
544	3560	3568	3576	3584	3592	3600	3608	3616	3624	3632
545	3640	3648	3656	3664	3672	3679	3687	3695	3703	3711
546	3719	3727	3735	3743	3751	3759	3767	3775	3783	3791
547	3799	3807	3815	3823	3830	3838	3846	3854	3862	3870
548 549	3878 3957	3886 3965	3894 3973	3902 3981	3910 3989	3918 3997	3926 4005	3933 4013	3941 4020	3949 4028
	Transmission in the		4052	4060	4068	4076	4084	4092	4099	4107
550 551	4036 4115	4044 4123	4052	4060	4068	4076	4084	4092	4099	4107
552	4194	4202	4210	4218	4225	4233	4241	4249	4257	4265
553	4273	4280	4288	4296	4304	4312	4320	4327	4335	4343
554	4351	4359	4367	4374	4382	4390	4398	4406	4414	4421
555	4429	4437	4445	4453	4461	4468	4476	4484	4492	4500
556	4507	4515	4523	4531	4539	4547	4554	4562	4570	4578
557	4586	4593	4601	4609	4617	4624	4632	4640	4648	4656
558	4663	4671	4679	4687	4695	4702	4710	4718	4726	4733
559	4741	4749	4757	4764	4772	4780	4788	4796	4803	4811
560	-4819	4827	4834	4842	4850	4858	4865	4873	4881	4889
561	4896 4974	4904 4981	4912 4989	4920 4997	4927 5005	4935 5012	4943 5020	4950 5028	4958 5035	4966 5043
562 563	4974 5051	4981 5059	4989 5066	4991 5074	5005	5012	5020	5105	5035	5043 5120
564	5128	5136	5143	5151	5159	5166	5174	5182	5189	5197
565	5205	5213	5220	5228	5236	5243	5251	5259	5266	5274
566	5282	5289	5297	5305	5312	5320	5328	5335	5343	5351
567	5358	5366	5374	5381	5389	5397	5404	5412	5420	5427
568	5435	5442	5450	5458	5465	5473	5481	5488	5496	5504
569	5511	5519	5526	5534	5542	5549	5557	5565	5572	5580
570	5587	5595	5603	5610	5618	5626	5633	5641	5648	5656
571	5664	5671	5679	5686	5694	5702	5709	5717	5724	5732
572	5740	5747	5755 5831	5762	5770	5778	5785 5861	5793	5800	5808
573 574	5815 5891	5823 5899	5906	5838 5914	5846 5921	5853	5937	5868 5944	5876 5952	5884 5959
575	5967	5974	5982	5989	5997	6005	6012	6020	6027	6035
576	6042	6050	6057	6065	6072	6080	6087	6095	6103	6110
577	6118	6125	6133	6140	6148	6155	6163	6170	6178	6185
578	6193	6200	6208	6215	6223	6230	6238	6245	6253	6260
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NO.	0	1 .	2	3	4	5	6	7	8	9
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Ň	0, 580	0-64	00.				Log	7634	3-806	18.
NO.	0	1	2	3	4	5	6	7 2 1	8	9
580	76343	76350	76358	76365	76373	76380	76388	76395	76403	76410
581	6418	6425	6433	6440	6448	6455	6462	6470	6477	6485
582	6492	6500	6507	6515	6522	6530	6537	6545	6552	6559
583	6567	6574	6582	6589	6597	6604	6612	6619	6626	6634
584 585	6641 6716	6649 6723	6656 6730	6664 6738	6671 6745	6678 6753	6686 6760	6693 6768	6701 6775	6708
586	6790	6797	6805	6812	6819	6827	6834	6842	6849	6782 6856
587	6864	6871	6879	6886	6893	6901	6908	6916	6923	6930
588	6938	6945	6953	6960	6967	6975	6982	6989	6997	7004
589	7012	7019	7026	7034	7041	7048	7056	7063	7070	7078
590	7085	7093	7100	7107	7115	7122	7129	7137	7144	7151
591	7159	7166	7173	7181	7188	7195	7203	7210	7217	7225
592	7232	7240	7247	7254	7262	7269	7276	7283	7291	7298
593	7305	7313	7320	7327	7335	7342	7349	7357	7364	7371
594	7379	7386	7393	7401	7408	7415	7422	7430	7437	7444
595	7452	7459	7466	7474	7481	7488	7495	7503	7510	7517
596	7525 7597	7532	7539	7546 7619	7554 7627	7561 7634	7568 7641	7576	7583 7656	7590 7663
597 598	7670	7605 7677	7612 7685	7692	-7699	7706	7714	7721	7728	7735
598 599	7743	7750	7000	7764	7772	7779	7786	7793	7801	7808
600	7815	7822	7830	7837	7844	7851	7859	7866	7873	7880
600 601	7887	7822	7902	7909	7916	7924	7931	7938	7945	7952
602	7960	7967	7974	7981	7988	7996	8003	8010	8017	8025
603	8032	8039	8046	8053	8061	8068	8075	8082	8089	8097
604	8104	8111	8118	8125	8132	8140	8147	8154	8161	8168
605	8176	8183	8190	8197	8204	8211	8219	8226	8233	8240
606	8247	8254	8262	8269	8276	8283	8290	8297	8305	8312
607	8319	8326	8333	8340	8347	8355	8362	8369	8376	8383
608	8390 8462	8398	8405	8412 8483	8419 8490	8426 8497	8433 8504	8440 8512	8447 8519	8455 8526
609		8469	8476							
610	8533 8604	8540	8547 8618	8554 8625	8561 8633	8569 8640	8576 8647	8583 8654	8590 8661	8597
611 612	8675	8611 8682	8689	8696	8704	8711	8718	8725	8732	8668 8739
613	8746	8753	8760	8767	8774	8781	8789	8796	8803	8810
614	8817	8824	8831	8838	8845	8852	8859	8866	8873	8880
615	8888	8895	8902	8909	8916	8923	8930	8937	8944	8951
616	8958	8965	8972	8979	8986	8993	9000	9007	9014	9021
617	9029	9036	9043	9050	9057	9064	9071	9078	9085	9092
618	9099	9106	9113	9120	9127	9134	9141	9148	9155	9162
619	9169	9176	9183	9190	9197	9204	9211	9218	9225	9232
620	9239	9246	9253	9260	9267	9274	9281	9288	9295	9302
621	9309	9316	9323	9330	9337	9344	9351	9358	9365	9372
622	9379	9386	9393	9400 9470	9407 9477	9414 9484	9421 9491	9428 9498	9435 9505	9442 9511
623 624	9449 9518	9456	9463 9532	9470	9546	9464	9491	9498	9505	9581
625	9588	9525	9602	9609	9616	9623	9630	9637	9644	9650
626	9657	9664		9678	9685	9692	9699	9706	9713	9720
627	9727	9734		9748	9754	9761	9768	9775	9782	9789
628	9796		9810	9817	9824		9837	9844	9851	9858
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630		9941	9948	9955	9962	9969	9975	9982	9989	- 9996
631	80003	80010		80024		80037		80051		80065
632	0072			0092	0099	0106	0113	0120	0127	0134
633				0161	0168	0175	0182	0188	0195	0202
634	0209			0229	0236	0243		0257	0264	0271
635	0277			0298	0305	0312	0318	0825 0393	0332	0339
636	0346		0359	0434	03/3	0448	0455	0393	0400	0401
637				0454	0509	0516	0455	0462	0408	0415
638 639				0570		0584	0523	0598	0604	0611
-			2	3	4	5	6	7	8	9
NO.	0	1	1 10	1 3	1 44	0	0		0	

N	0. 640	0-700	00.	ب المعاطفة الم			Lop	. 8061	8-84	510.
NO.	0	1	2	3	4	- 5	6	7	8	9
	80618				80645	80652	80659		80672	
641	0686	0693	0699	0766	0713	0720	0726	0733	0740	0747
642	0754	0760	0767	0774	0781	0787	0794	0801	0808	0814
643 644	0821	0828 0895	0835	0841 0909	0848	0855	0862	0869	0875	0882
645	0956	0963	0969	0909	0916 0983	0922	0929 0996	0936	0943 1010	0949 1017
646	1023	1030	1037	1043	1050	1057	1064	1000	1077	1084
647	1090	1097	1104	iiii	1117	1124	1131	1137	1144	1151
648	1158	1164	1171	1178	1184	1191	1198	1204	1211	1218
649	1224	1231	1238	1245	1251	1258	1265	1271	1278	1285
650	1291	1298	1305	1311	1318	1325	1331	1338	1345	1351
651	1358	1365	1371	1378	1385	1391	1398	1405	1411	1418
652	1425	1431	1438	1445	1451	1458	1465	1471	1478	1485
653	1491	1498	1505	1511	1518	1525	1531	1538	1544	1551
654 655	1558 1624	1564 1631	1571 1637	1578	1584		1598	1604	1611	1617 1694
656	1624	1631	1057	1644 1710	1651 1717	1657 1723	1664	1671	1677 1743	1750
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727	6153	6159	6165	6171	6177	6183	6189	6195	6201	620
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729	6273	6279	6285	6291	6297	6303	6308	6314	6320	632
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735	6629	6635	6641	6646	6652	6658	6664	6670	6676	668
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157 158	7910 7967	7915	7978	7984	7990	7996	8001	8007	8013	8018
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783	9376	9382	9387	9393					421	426
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787	9597	9603	9609	9614						
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819	1328	3 1334	1339	1344	4 1350	1355	i 1360	136	5 1371	1376
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832 833	2012 2065	2018	2023	2028	2035	2038	2044	2045	2054	2035
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394 395	5134 5182	5139 -5187	5143 5192	5148 5197	5153 5202	5158 5207	5163 5211	5168 5216	5173 5221	517
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918	6284	6289	6294	6298	6303	6308	6313	6317	6322	
919	6332	6336	6341	6346	6350	6355	6360	6365	6369	-
920	6379	6384	6388	6393	6398	6402	6407	6412	6417	
921	6426	6431	6435	6440	6445	6450	6454	6459	6464	
922	6473	6478	6483	6487	6492	6497	6501	6506		
23	6520 6567	6525	6530	6534	6539	6544 6591	6548	6553	6558	
)24)25	6614	6572. 6619	6577 6624	6581 6628	6586 6633	6638	6595 6642	6600 6647	6605 6652	
925	6661	6666	6670	6675	6680	6685	6689	6694		
927	6708	6713	6717	6722	6727	6731	6736	6741	6745	675
28	6755	6759	6764	6769	6774	6778	6783	6788	6792	679
929	6802	6806	6811	6816	6820	6825	6830	6834	6839	684
30	6848	6853	6858	6862	6867	6872	6876	6881	6886	
931	6895	6900	6904	6909	6914	6918	6923	6928		
32	6942	6946	6951	6956	6960	6965	6970	6974		698
933	6988	6993	6997	7002	7007	7011	7016	7021	7025	705
934	7035	7039	7044	7049	7053	7058	7063	7067	7072	707
35	7081	7086	7090	7095	7100	7104	7109	7114	7118	712
)36)37	7128 7174	7132 7179	7137	7142	7146 7192	7151	7155	7160 7206	7165	716
938	7220	7225	7183	7188 7234	7192	7197 7243	7202	7206	7211	726
,00										
39	7267	7271	7276	7280	7285	7290	7294	7299	7304	730

N	o. 9400							97313	store the stated	
NO.	0	1	2	3	4 .	5	6	7 :	8	9.
							97340.9			
941	7859		7368	7373	7377	7382	7387	7391	7396	7400
942 943	7405	7410	7414	7419	7424	7428	7433	7483	7488	7447
944		7502	7506	7511	7516	7520	7525	7529	7534	7539
945	7543	7548	7552	7557	7562	7566	7571	7575	7580	7585
946	7589	7594	7598	7603	7607	7612	7617	7621	7626	7630
947	7635	7640	7644	7649	7653	7658	7663	7667	7672	7676
948	7681	7685	7690	7695	7699	7704	7708	7713	7717	7722
949	7727	7731	7736	7740	7745	7749	7754	7759	7763	7768
950	7772	7777	7782	7786	7791	7795	7800	7804	7809	781
951	7818	7823	7827	7832	7836	7841	7845	7850	7855	785
952	7864	7868		7877	7882	7886	7891	7896	7900	790
953 954	7909 7955	7914	7918	7923	7928	7932	7937	7941 7987	7946	795
954 955	8000	7950 8005	7964 8009	7968 8014	7973 8019	7978		8032	7991	799
956	8046	8050	8055	8059	8064	8068		8078	8082	808
957	8091	8096	8100	8105	. 8109	8114	8118	8123	8127	813
958	8137	8141	8146	8150	8155	8159	8164	8168	8173	817
959	8182	8186	8191	8195	8200	8204	8209	8214	8218	822
960	8227	8232	8236	8241	8245	8250	8254	8259	8263	826
961	8272	8277	8281	8286	8290	8295	8299	8304	8308	831
962	8318	8322	8327	8331	8336	8340		8349	8354	
963	8363		8372	8376	8381	8385	8390	8394	8399	840
964 965	8408		8417	8421	8426	8430	8435	8439	8444	
966	8453 8498	8457 8502	8462 8507	8466 8511	8471 8516	8475 8520	8480 8525	8484 8529	8489 8534	
967	8543	8547	8552		8561	8565	8570	8574	8579	858
968	8588		8597	8601	8605	8610	8614	8619	8623	862
969	8632	8637	8641	8646	8650	8655	8659	8664	. 8668	
970	8677	8682	8686	8691	8695	8700	8704	8709	8713	-
971	8722	8726	8731	8735	8740	8744	8749	8753	8758	
972	8767		8776	8780	8784	8789	8793	8798	8802	880
973	8811	8816	8820	8825	8829	8834	8838	8843	8847	
974	8856	8860		8869	8874	8878	8883	8887	8892	
975	8900	8905	8909.		8918	8923	8927	8932	8936	
976 977	8945 8989	8949 8994	8954 8998	8958 9003	8963 9007	8967 9012	8972 9016	8976 9021	8981 9025	
978	9034	8994 9038	9043	9003 047	052		061	065	069	
979	9078	9083	9087	092	096		105	109	114	ii
980	9123	9127			140	145	149	154	158	16
981	9167	9171	9176	180	185	189	193	198	202	20
982	9211	9216			229	233	238	242	247	25
983	9255	9260			273	277		286	291	29
984	9300	9304	9308	313	317	322		330	335	
985	9344	9348			361			374	379	38
986	9388	9392	9396	401	405	410		419	423	
987 988	9432 9476	9436		445	449	454		463	467	47
989	9470	9480 9524						506	511 555	51
990	9564	-	and the second second	-		-		594		
990 991	9607	9568 9612	9572 9616	577		585			599	60 64
992		9612						682	642 686	69
993	9695	9699						726	730	
994		9743						760	774	
995	9782	9787	9791		800	804		813	817	8
996	9826	9830		839	843			856	861	86
997	9870	9874						900	904	90
998	9913	9917						944	948	
999	9957	9961		1		-	-	987	991	99
NO.	0	1	2	3	4	5	6	7	8	9

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M	Sine	C. Sine	Tang.	C.Tang.	Secant.	C. Sec.	M
0	0.00000	10.00000	0.00000	Infinite	10.00000	Infinite	60
5	7.16270	00	7.16270	12.83730		12.83730	55
10	46373	00	46373	53627	00	53627	50
15	63982	00	63982	36018	00	36018	45
20	76475	9.99999	76476	23524	01		40
25	86166	99	86167	13833	őî	13834	35
30	94084	- 98	94086	05914	02	05915	30
35	8.00779	9,99998		11.99219			2
40	06578	97	06581	93419	03		20
45	11693	96	11696		04		11
50	16268	95	16273		04		10
55	20407	94	20413	79587	06		1
60	24186	93	24192		07	75814	i
M	C. Sine						
1411	C. Sme	Sine	C.Tang.		C. Sec.	Secant	M
-			- 59 De	grees.			-
M	<u>.</u>	0.0		gree.		-	
	Sine	C. Sine		C.Tang.			V
0	8.24186	9.99993				11.75814	60
5	27661	92	27669	72331	08		5
10	30879	91	30888	69112	09	69121	50
15	33875	89	33886	66114	11	66125	4
20	36678	88	36689	63311	12	63322	4
25	39310	87	39323	60677	13	60690	3
30	41792	85	41807	58193	15	58208	30
35	8.44139	9.99983	8 44156	11.55844	10.00017	11 55961	2
40	46366	82	46385				20
45	48485	80	48505		20		ĩ
50	50505	78	50527				
55	52434	76	52459				1
60	54282	74	54308				
M	C. Sine	Sine	C. Tang.		C. Sec.	Secant.	N
-				grees.		-	-
				grees.			
M	Sine	C. Sine	Tang.	C.Tang.	Secant	C. Sec.	N
0	8.54282	9.99974	8.54308	11.45692	10.00026	11.45718	6
5	56054	71	56083	43917			5
10	57757	69	57788				5
15	59395	66	59428				4
20	60973	64	61009				4
25	62496	61	62535		39		3
30	63968	59	64009		41		3
35	8.65391	9.99956				11.34609	0
40	66769	53	66816	33184	10.00044		2
45	68104	50	68154				
40 50	69400	47	69453				1
55	70658	41	70714		53		10
60	71880	44	71940				
M	C. Sine		C.Tang		60 C. Sec.		1
		Sino				Secant	A

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M	Sine	C. Sine	Tang.	C.Tang.	Secant	C. Sec.	M
0	8.71880	9.99940	8.71940	11.28060	10.00060	11.28120	60
5	-						
10	74226	34	74292	25708	66	25774	.50
15	75353	37 34 30 26 23 19	75423	24577 23475 22400	63 66 70	24647	45
20	76451	26	76525	23475	74	23549	40
25	77522	23	77600	22400	77	22478	35
30	78567	19	78649	21351	* 81	21433	.30
35	8.79588	9.99915	8.79673 80674	11.20327	10.00085	11.20412	25
.40	80585	9.99915 11 07 03 99898 894	80674	19326	89	19415	20
45	81560	07	81653	18347	93	18440	15
50	82513	03	82610	17390	97	17487	10
55	83446	99898	83547	16453	102	16554	5
60	01000	004	0.110.1	15536	89 93 97 102 106	15642	0
M	C. Sine	Sine	C.Tang.	Tang.	C. Sec.	Secant	M
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-			4 Deg				
M		C. Sine	Tang.	C.Tang.	Secant	C. Sec.	M
0	8.84358		8.84464	11.15536	10.00106	11.15642	60
5	85252	- 890		14637	110		55
10	86128		86243	13757	115	13872	50
15	86987	880	87106	12894	120	13013	45
20	87829	876	87953	12047	124	12171	40
25	88654	871	88783	11217	129		
30	89464	866	89598	10402	134	10536	30
35	8.90260	9.99861	8.90399	11.09601	10.00139	11.09740	25
40	91040	856	91185 91957 92716 93462	08815	144	08960	20
45	91807	851	91957	08043	149	08193	15
50	92561	845	92716	07284	155	07439	10
55	93302			06538	160	06698	5
60	94030			0538	149 155 160 166	05970	0
M	C. Sine	Sine	C.Tang.	Tang.	C. Sec.	Secant	M
		-	85 Deg	grees.			
			Deg	rees.			
M	Sine		Tang.				
0		9.99834		11.05805	10.00166		60
5	94746	829	94917	05083	171	05254	55
10	95450	823	95627	03083 04373 03675 02987	177 183	04550	50
15	96143	817 812	96325	03675	183	03857	45
20	96825	812	97013	02987	188	03175	40
25	97496	806	97691 98358	02309	194	02504	35
30	98157	800	98358	01642	200	01843	-
35	8.98808	9.99794	8.99015	11.00985	10.00206	11.01192	25
40	99450	787	99662	00338	213	00550	20
45	9.00082	781	9.00301	10.99699	219	10.99918	15
50	00704	775	00930	99070	225	99296	10
55	01318	768	01550	98450	232	98682	5
60	01923	761	99662 9.00301 00930 01550 02162 C.Tang.	97838	239	98077	9
M	C. Sine	Sine	C.Tang.	Tang.	C. Sec.	Secant	M
			84 Deg	rees.			_

-			6 De	grees.			
M	Sine	C. Sine			Secant	C. Sec.	M
0	9.01924	9.99761		10.97838			60
5	02520	755	02765			97480	55
10	03109	748	03361	96639	252	96891	50
15	03690	741	03949	96051	259	96310	45
20	04263	734	04528	95472	266	95737	40
25	04828	727	05101				35
30	05386	720	05666	94334	280	94614	30
35	9.05937	9.99713	9.06224	10.93776	10.00287	10.94063	25
40	06481	705	06775	93225			20
45	07018	698	07320	92680			15
50	07548	690					10
55	08072	683					5
60	08589	675	08914				0
M	C. Sine	Sine			C. Sec.	Secant	M
			83 De	grees.	-		_
	~	~ ~	7 Deg				
M	Sine	C. Sine		C.Tang.	Secant	C. Sec.	M
0	9.08589	9.99675	9.08914	10.91086	10.00325		60
5	09101	667	09434				55
10	09606	659					50
15	10106	651					45
20	10599	643					40
25	11087	635	11452				35
30	11570	627					30
35	9.12047	9.99618	9.12428	10.87572	10.00382	10.87953	25
40	12519	610					20
45	12985	602					15
50	13447	593				00000	10
55	13904	584					-E
60	14356	575	14780				(
M	C. Sine	Sine		Tang.	C. Sec.	Secant	M
-				grees.			
NT	611	0 0		grees.		0.0	-
M	Sine	C. Sine	0			C. Sec.	-
0	9.14356	9.99575	9.14780	10.85220	10.00425	10.85644	60
5	14803	566					55
10 15	15245 15683	557 548					50
15 20	16116						45
20	16545	539 530	16577 17016				40
30	16970	530 520	17450				38
35	9.17391	9.99511				10.82609	2
40	17807	501					20
45	18220	492	18728				15
50	18628	482					10
55	19033	472	19561	80439			
60	19433	462	19971	80029			i
	C. Sine	Sine	C.Tang.	Tang.	C. Sec.	Secant	M

				grees.			-
M	Sine	C. Sine	Tang.	C.Tang.	Secant	C. Sec.	M
0	9.19433	9.99462	9.19971	10.80029	10.00538	10.80567	60
5	19830	452	20378	79622	548	80170	. 55
10	20223	442	20782	79218	558	79777	50
15	20613	432	21182	78818	568		45
20	20999	421	21578	78422	579	79001	40
25	21382	411	21971	78029	589	78618	35
30	21761	400	22361	77639	600	78239	30
35	9.22137	9.99390	9.22747	10.77253			25
40	22509	379		76870	621	77491	20
45	22878	368	23510		632	77122	15
50	23244	357		76113	643	76756	10
55	23607	346	24261	75739	654	76393	5
60	23967	335	24632	75368	665	76033	ő
M	C. Sine		C.Tang.		C. Sec.		_
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M.	Sine I	C. Sine		C.Tang.	Secant	C. Sec.	M
ō	9.23967	9.99335		10.75368			60
5	24324	324	25000		676	75676	55
10	24677	313	25365	74635	687	75323	50
15	25028	301	25727	74033	699		45
13 20	25376	290	26086	73914	699 710		
20 25		290				74624	40
	25721		26443	73557	722	74279	35
30	26063	267	26797	73203	733	73937	30
35	9.26403	9.99255		10.72852			25
40	26739	243	27496		757	73261	20
45	27073	231	27842	72158	769	72927	15
50	27405	219	28186	71814	781	72595	10
55	27734	207	28527	71473	793	72266	5
60	28060	195	28865	71135	805	71940	0
M	C. Sine	Sine	C.Tang.		C. Sec.	Secant	M
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			11 Deg				_
M	Sine	C. Sine		C.Tang.	Secant		M
0	9.28060	9.99195		10.71135			60
5	28384	182	29201	70799	818	71616	55
10	28705	170	29535	70465	830	71295	50
15	29024	157	29866	70134	843	70976	45
20	29340	145	30195	69805	855	70660	40
25	29654	132	30522	69478	868	70346	35
30	29966	119	30846	69154	881	70034	30
35	9.30275	9.99106	9.31168	10.68832	10.00894		25
40	30582	093	31489	68511	907	69418	20
45	30887	080	31806	68194	920	69113	15
50	31189	067	32122	67878	933	68811	10
55	31490	054	32436	67564	946	68510	5
	31788	040	32748	67252	960	68212	ő
55 60							
60	C. Sine		C.Tang.	Tang.	C. Sec.	Secant	M

			12 De	grees.			-
M	Sine	C. Sine	Tang.	C.Tang.	Secant	C. Sec.	M
Õ	9.31788	9.99040	9.32747	10.67253	10.00960	10.68212	60
5	32084	99027	33057	66943	00973		55
10	32378	99013	33365	66635	00987	67622	50
15	32670	99000	33670	66330	01000 01014 01028	67330	45
20	32960	98986	33974	66026	01014	67040	40
25	33248	98972	34276	65724	01028	66752	33
30	33534	98958	34576	65124	01028	66466	30
35	9.33818	9.98944	9.34874	10.65126	10.01056	10.66182	2
40	34100	98930	35170	64830			20
45	34380	39310	55404	04000		65620	18
50	34658		35757			65342	10
55	34934	98887	36047	63953	01113	65066	1
60	35209	98872	36336	63664	01128	65066 64791	(
M	C. Sine	Sine	C. Tang.	Tang.	C. Sec.	Secant	Ŋ
_				grees.			
				grees.			
M		C. Sine				C. Sec.	N
0	9.35209			10.63664			60
5	35482	98858	36624		01142		5
10	35752	98843	36909	63091	01157		5
15	36022	98828	37193	62807	01172		4
20	36289	98813	37476	62524	01187		4
25	36555	98798	37756	62244	01202	63445	3
30	36818	98783	38035	62807 62524 62244 61965	01217	63182 10.62919 62659 62400	3
35	9.37081	9.98768	9.38313	10.61687	10.01232	10.62919	2
40	37341	98753	38589	61411	01247	62659	2
45	37600	98737	38863	61137	01263		
50	37858	98722	39136	60864	01278	62142	1
55	38113	98706	39407	61411 61137 60864 60593	01294		
60	38368		39677	60323	01310		_
M	C. Sine	Sine	C.Tang.	Tang.	C. Sec.	Secant	N
-		_		egrees.			
				egrees.			_
M		C. Sine				C. Sec.	N
0	9.38368	9.98690	9.39677	10.60323	10.01310	10.61632	6
5	38620	98675			01325		5
10	38871	98659	40212	59788	01341		5
15	39121	98643		59788 59522 59258 58996	01357		4
20	39369	98627	40742	59258	01373		4
25	39615	98610	41004	00000	01000		3
30	39860	98594					
35		9.98578	9.41526	10.58474	10.01422	10.59896	
40	40345	-98561	41784	58216			2
45	40586	98545	42042 42297	57958 57703	01455		1
50	40825		42297	57703	01472	.59175	1
55	41063	98511	42552	57448	01489	58937	
60	41300	98494	42805	57195	01506	58700 Secant	_
	C. Sine	Sine	U. Tang.	ano.	Sec.	Secont	N
M	0.0110	~ me		egrees.	101 000	Decaut	-

15 Degrees.									
M	Sine	C. Sine	Tang.	C.Tang.	Secant	C. Sec.	M		
Ō		9.98494		10.57195	10.01506	10.58700	60		
5	41535	98477		56943			55		
10	'41768			56692			50		
15	42001	98443	43558	56442	01557		45		
20	42232	98426	43806	56194	01574		40		
25	42462	98409	44053	55947	01591		35		
30	42690	98391	44299	55701			30		
35	9.42917	9.98374	9.44544	10.55456	10.01626	10.57083	25		
40	43143	98356	A1797	55019	01644	56857	20		
45	43368 43591	98338	45029	54971	01662		15		
50	43591	98320	45271	54971 54729 54489	01680	56409	10		
55	43813	98302	45511	54489	01698	56187	5		
60	44034	98302 98284	45750	54250	01716	55966	0		
M	C. Sine	Sine			C. Sec.	Secant	M		
-				grees.			_		
		•	16 De						
M	Sine		Tang.	C. Tang.	Secant	C. Sec.	M		
0	9.44034	9.98284	9.45750	10.54250	10.01716	10.55966	60		
5	44253	98266	45987		01734	55747	55		
10	44472	98248	46224	53776	01734 01752 0177 1	55528	50		
15	44689	98229	46460	53776 53540 53306	01771	55311	45		
20	44905	98211	46694	53306	01789	55095	40		
25	45120	98192	40928	53072	01808		35		
30	45334	98174	47160	52840	01826		30		
35	9.45547	9.98155	9.47392	10.52608	10.01845	10.54453	25		
40	45758	98136	47622	52378	01864	54242			
45	45969	98117	4/032	52148	01883	54031	15		
50	46178	98098	48080	51920	01902	53822	10		
55	46386	98079	48307	51693	01921	53614	5		
60	46594	98060	48534	51466	01921 01940	53406	0		
M	C. Sine		C.Tang.	Tang.	C. Sec.	Secant	M		
			73 De	grees			-1		
			17 De	grees.			-		
M	Sine	C. Sine	Tang.	C. Tang.	Secant	C. Sec.	M		
0	9.46594	9.98060	9.48534		10.01940	10.53406	60		
5	46800	98040	48759	51241	01960	53200	55		
10	47005	98021	48984	51016	01979	52995	50		
15	47209	98001		50793	01999	52791	45		
20	47412	97982	49430	50570	02018	52588	40		
25	47613	97962			02038	52387	35		
30	47814	97942		50128	02058		30		
35	9.48014	9.97922	9.50092	10.49908	10.02078	10.51986	25		
40	48213	97902	50311	49689	02098	51787	20		
45	48411	97882	50599	49471	02118		15		
50	48608	97861	50746	49254	02139		10		
55	48803	97841	50746 50962	49038	02159	51197	5		
60	48998	97821	51178	488221	02179	51002	θ		
M	C. Sine	Sine (C.Tang.	Tang.	C. Sec.	Secant	M		
			72 De	rees.			-		

	-		. 18 De	rees.			-
M	Sine	C. Sine:	Tang.	C.Tang.	Secant	C. Sec.;	M
0	9.48998	9.97821		10,48822			60
5	49192	97800	51392	48608	02200		55
10	49385	97779	51606	48394	02221		50
15	49577	97759		48181	02241		45
20	49768	97738		47969	02262		40
25	49958	97717	52242	47758	02283	- 50042	35
30	50148	97696		47548			30
35	9.50336	9.97674	9.52661	10.47339	10.02326	10.49664	25
40	50523	97653	52870	47130	02347		
45	50710	97632	53078	46922			15
50	50896	97610	53285	46715	02390	49104	10
55	51080		53492		02411		t
60	51264		53697		02433		(
M	C. Sine	Sine	C.Tang.	Tang.	C. Sec.	Secant	M
			71 De	grees.	-		
M	Sino	C. Sine	19 De		C	0 0	-
	Sine		I ang.	U. Tang.	Secant	C. Sec.	
0	9.51264	9.97567				10.48736	60
5	51447	97545	53902		02455		5
10	51629 51811	97523 97501	54106	45894	02477		5
15			54309		02499		4
20 25	51991 52171		54512		02521		4
30	52350		54714 54915	45280	02543		3
35						3 10.47473	2
40	52705	97390					2
45	52881		55514		02639	47119	Ĩ
50	53056		55712		0265	46944	i
55	53231	97322	55910		0267	6 46944 5 46769	1
60	53405	97299	56107	43893	0270	1 46595	
M	C. Sine	Sine	C.Tang	. Tang.	C. Sec	. Secant	N
_				egrees.			
				egrees.			
M	Sine					C. Sec.	
0	9.53405					1 10.46595	
5							
10	53751		56498				
15	53922			4330	0277	1 46078	
20	54093						
25	54263						
30	54433						
35						5 10.45399	
40	54769						
45	54936						
50				4196	0293	7 44898	3 1
55				4177	0296	1 44732 5 AAFG7	
60 M		97015 Sine		4108: Tang	0298	1 44732 5 44567 . Secant	
				· A ang.			

0 9.55433 9.97015 9.58418 10.41582 10.02985 10.44567 66 5 55597 96991 58606 41394 03009 44408 55 10 55761 96696 58794 41206 03034 44295 55 15 55923 96942 58981 41019 03058 44077 44 20 56085 96917 59168 40832 03083 43915 44 25 56247 966933 59334 40646 03132 43532 24 40 56727 96818 59909 40091 03182 43273 24 50 57044 95767 60276 39724 03233 42642 0 60 57358 96717 60641 10.39355 10.32831 10.42642 64 5 57514 96691 60823 39177 03309 42486 5 10 57639	-	21 Degrees.										
5 55597 96991 58606 41394 03009 44409 555 10 55761 96942 58981 41006 03034 44299 56 20 55083 96942 58981 41019 03058 44077 44 20 56085 96817 59168 40632 03083 43915 44 20 56085 96813 59540 40460 03132 43592 30 30 56408 96868 59540 40460 03132 43592 32 40 56727 96818 59909 40091 03182 43273 24 41 56868 96793 60033 39907 03207 43141 15 50 57044 96767 60276 39724 03235 10.42642 65 60 57356 9.6717 9.60643 10.39355 10.03283 10.42642 65 57514 96614	M	Sine	C. Sine	Tang.	C.Tang.	Secant	C. Sec.	M				
M Sine C. Sine Tang. C. Tang. Secant C. Sec. N 0 55734 96640 68194 41019 03058 44077 44 25 556247 96893 59354 40646 03107 43753 34 30 56408 96868 59540 40460 03132 43592 36 35 9.56568 9.69843 9.59725 10.40275 10.03157 10.43432 22 45 56886 96793 60093 39907 03207 43114 14 50 57044 96767 60276 39724 03233 42642 0 60 57358 96717 60641 39355 03283 42642 0 7 9.6616 60459 39517 03309 42466 5 10 57568 9.96717 9.60641 10.39359 10.03283 10.42642 60 10 57669 966	0	9.55433	9.97015	9.58418	10.41582	10.02985	10.44567	60				
15 55923 96942 58981 41019 03058 44077 44 20 56085 96917 59168 406832 03083 43915 44 20 56085 96917 59168 406832 03083 43915 44 30 56408 96868 59540 40460 03132 43592 36 40 56727 96818 59909 40091 03182 43273 20 40 56727 96818 59909 40091 03182 43273 20 50 57044 95767 60276 39724 03233 42642 0 50 57358 96717 60641 10.39359 10.32833 10.42642 6 60 57358 9.6717 9.60641 10.39359 10.32833 10.42642 6 7 9.67646 6104 38966 03335 42331 5 10 57639 966436		55597	96991	58606	41394	03009	44403	55				
20 56085 96917 59168 40832 03083 43915 44 25 56247 96893 59334 40646 03107 43753 33 35 55568 9.96843 9.59725 10.40275 10.03157 10.43432 24 40 56727 96818 59909 40091 03182 43273 24 40 56727 96818 59909 40091 03182 43273 24 45 5686 96793 60093 39907 03234 429561 11 50 57044 95767 60276 39724 03238 42642 0 60 57358 96717 60641 10.39359 10.03283 42642 0 7 96717 960641 10.39359 10.03283 42642 60 5 57514 96619 60823 39177 03309 424865 55 50 57978 96614		55761	96966	58794	41206	03034	44239	50				
25 56247 96893 59354 40646 03107 43753 33 30 56408 96668 59540 40460 03132 43592 33 35 9.56568 9.96843 9.59725 10.404275 10.03157 10.43432 22 45 56568 9.69643 9.59725 10.404275 10.03157 10.43432 22 45 56886 96793 60093 39907 03207 43114 14 50 57044 93767 60276 39724 03233 42642 0 60 57358 96717 60641 39355 03283 42642 0 70 9.57356 9.96717 9.60641 10.39359 10.03283 10.42642 60 0 9.57356 9.96717 9.60641 10.39359 10.03283 10.42642 60 10 57669 96665 61004 38996 03316 423176 423176		55923	96942	58981	41019		44077	45				
30 56408 95868 59540 40460 03132 43592 36 35 9.56568 9.96843 9.59725 10.40275 10.03157 10.43432 24 40 56727 96818 59909 40091 03182 43273 20 40 56727 96818 59909 40091 03182 43273 20 50 57044 95767 60276 39724 03233 42956 10 55 57201 96742 60453 39541 03228 42642 10 60 57358 96717 60641 39355 03283 42642 10 70 9.57356 9.96717 9.06641 10.39359 10.42642 6 5 57514 96691 60823 39177 03309 42486 5 10 57689 9.96613 61043 38966 03335 42315 5 57514 96640 61143		56085	96917	59168	40832	03083	43915	40				
35 9.56566 9.96843 9.59725 10.40275 10.03157 10.43432 24 40 56727 96818 59909 40091 03182 43232 24 45 56866 96793 60093 39907 03207 43114 14 50 57044 95767 60276 39724 03233 429661 14 60 57358 96717 60641 39359 03283 42642 0 M C. Sine Tang. C. Sec. Secant N. 84242 0 0 9.57356 9.96717 9.06041 10.39359 10.03283 10.42642 66 5 57514 96619 60823 39177 03309 424865 57 10 57669 96656 61004 38996 033354 42331 51 15 57824 96640 61184 38636 03462 42176 44 20 579		56247	96893		40646	03107	43753	35				
40 56727 96818 59909 40091 03182 43273 20 45 56886 96793 60093 39907 03207 43114 14 50 57044 95767 60276 39724 03233 42966 14 60 57358 96717 60641 39355 03283 42642 0 60 57358 96717 60641 39355 03283 42642 0 60 5.57514 96691 60.39559 10.03283 10.42642 66 5 57514 96615 61004 33959 10.3283 10.42642 66 5 57514 96610 61184 38816 03360 42315 15 10 57669 96652 61704 38969 033184 41716 42 20 57978 96614 6164 38636 033184 41764 42 20 57978 96614 <	30	56408	96868	59540	40460	03132	43592	30				
45 56886 96793 60093 39907 03207 43114 14 50 57044 93767 60276 39724 03233 42956 10 50 57044 93767 60276 39724 03233 42956 10 60 57358 96717 60641 39355 03283 42642 0 M C. Sine Sine C.Tang. Tang. C. Sec. Secant N 22 Degrees. - 22 Degrees. - - - - 0 9.57358 9.96717 9.60641 10.39359 10.03283 10.42642 60 5 57514 96691 60823 39177 03309 42466 51 10 57669 96665 61004 38996 03355 42331 54 25 5813 96588 61544 38456 03412 41869 36 25 5813	35	9.56568	9.96843	9.59725	10.40275	10.03157	10.43432	25				
50 57044 93767 60276 39724 03233 42956 II 55 57201 96742 60459 39541 03233 42956 II 55 57201 96742 60459 39541 03258 42642 M C. Sine Sine C. Tang. Tang. C. Sec. Secant N 0 9.57366 9.6717 9.60641 10.39359 10.432642 65 0 9.57366 9.6661 60823 39177 0309 42486 65 10 57514 96661 61004 38996 03335 42331 54 10 57669 96665 61004 38996 03335 42381 54 10 57678 96614 61364 38636 03386 42022 44 20 57978 96614 61364 38636 03346 420642 64 30 82849 95652 97744	40	56727	96818	59909	40091	03182	43273	20				
55 57201 96742 60459 39541 03258 42799 4 60 57358 96717 60641 39355 03283 42642 0 M C. Sine Sine C. Tang. Tang. C. Sec. Secant N 60 9.57356 9.96717 9.60641 10.39359 10.03283 10.42642 66 70 9.57356 9.96717 9.60641 10.39359 10.03283 10.42642 66 5 57514 9669 60823 39177 0309 42486 56 10 57669 966640 61184 38816 03360 42176 44 20 57978 96614 6164 38946 03312 41869 33 30 58284 96562 61722 38278 03438 41716 33 35 9.58436 9.96535 9.61901 10.38099 10.03457 144261 24 45	45	56886	96793	60093	39907	03207	43114	15				
60 57358 96717 60641 39359 03283 42642 0 M C. Sine Sine C.Tang. Tang. C. Sec. Secant M	50	57044	95767	60276	39724	03233	42956	10				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	55	57201	96742	60459	39541	03258	42799	5				
	60	57358	96717	60641	39359	03283	42642	0				
	M	C. Sine	Sine	C.Tang.	Tang.	C. Sec.	Secant	M				
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$\begin{array}{c c c c c c c c c c c c c c c c c c c $	_			22 De	grees.							
5 57514 96691 60823 39177 03309 42486 5. 10 57669 96665 61004 38996 03335 42331 54 10 57669 96665 61004 38996 03335 42331 54 10 57976 96614 61184 38816 03360 42176 44 20 57976 96614 61364 38636 03386 42022 44 20 58284 96562 61722 38278 03438 41716 33 30 58284 96562 61722 38278 03438 41716 42 40 58578 96438 62263 37764 03517 42061 42 50 58889 96456 62433 37567 03544 41111 10 50 58939 96429 62009 37391 03571 40812 6 M C. Sine Tang.				Tang.				M				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0	9.57358	9.96717	9.60641	10.39359	10.03283	10.42642	60				
15 57824 96640 61184 38816 03360 42176 44 20 57978 96614 61364 38636 03386 42022 44 25 5813 96588 61544 38436 03386 42022 44 30 58284 96562 61722 38278 03438 41716 36 30 58284 96562 61722 38278 03438 41716 36 40 58588 96509 62079 37921 03491 41412 24 45 56739 96423 62256 37767 03544 41111 10 50 5889 96403 62785 37215 03597 40812 6 40 5818 96403 62785 37215 03597 40812 6 50 59039 96429 62609 3731 03571 40961 4 50 59188 96403		57514		60823				55				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				61004				50				
25 58131 96588 61544 38456 03412 41869 33 30 58284 96562 61722 38278 03438 4171.6 33 35 9.58436 9.66502 61722 38278 03438 4171.6 34 35 9.58436 9.66509 62079 37921 03491 41412 24 40 58588 96509 62079 37921 03491 41412 24 45 58739 96483 62266 37744 03517 41261 14 50 58939 96429 62009 37391 03571 409812 6 60 59188 96403 62785 37215 03597 40812 6 M C. Sine Tang. C. Tang. Secant C. Sec. M 60 59188 9.96403 9.62785 10.37215 10.03597 10.40812 6 10 5.59188 9.96				61184				45				
30 58284 96562 61722 38278 03438 41716 36 35 9,58436 9,96535 9,61901 10.38099 10.03645 10.41564 22 40 58588 96509 62079 37921 03491 41412 24 45 58739 96483 62256 37744 03517 41261 12 50 58889 96426 62433 37567 03544 41111 10 55 59039 96429 62609 37321 03571 40961 4 60 59188 96403 62785 37215 03597 40812 6 M C. Sine Tang. C. Tang. Secant C. M 60 59188 9.6403 6.2785 10.37215 10.03597 10.40812 6 5 59336 96376 62961 37039 03624 40664 55 10 59434 96349		57978	96614	61364	38636			40				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$								35				
40 58588 96509 62079 37921 03491 41412 24 45 58739 96483 62256 37744 03517 41261 14 50 58899 96456 62433 37567 03544 41111 12 55 59039 96429 62609 37391 03571 40961 40961 60 59188 96403 62785 37215 03597 40812 0 M C. Sine Sine C. Tang, Tang, C. Sec. Secant N 60 9.59188 9.96403 9.62785 10.37215 10.03597 10.40812 60 5 59336 96376 62961 37039 03624 40664 55 10 59484 96349 63135 36865 03651 40516 56 15 59632 96322 63310 366900 03678 403684 20 59778 96294 636	30	58284	96562	61722	38278	03438	41716	30				
40 58588 96509 62079 37921 03491 41412 24 45 58739 96483 62256 37744 03517 41261 14 50 58899 96456 62433 37567 03544 41111 12 55 59039 96429 62609 37391 03571 40961 40961 60 59188 96403 62785 37215 03597 40812 0 M C. Sine Sine C. Tang, Tang, C. Sec. Secant N 60 9.59188 9.96403 9.62785 10.37215 10.03597 10.40812 60 5 59336 96376 62961 37039 03624 40664 55 10 59484 96349 63135 36865 03651 40516 56 15 59632 96322 63310 366900 03678 403684 20 59778 96294 636	35	9.58436	9.96535	9.61901	10.38099	10.03465	10.41564	25				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$								20				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	45	58739	96483	62256	37744	03517	41261	15				
55 59039 96429 62609 37391 03571 40961 40812 M C. Sine Sine C. Tang. Tang. C. Sec. Secant M 60 S9188 96403 62785 37215 03597 40812 0 M C. Sine Sine C. Tang. Tang. C. Sec. Secant N 67 Degrees. 23 Degrees. 10.37215 10.03597 10.40812 66 9 9.59188 9.96403 9.62785 10.37215 10.03597 10.40812 66 5 59336 96376 62961 37039 03624 40664 55 10 59484 96349 63135 36865 03651 40516 56 15 59632 96322 63310 36690 03678 40368 4 25 59924 96267 63657 36343 03733 40076 322 4 36430	50	58889		62433		03544		10				
M C. Sine Sine C. Tang. Tang. C. Sec. Secant M. 67 Degrees. 23 Degrees. 23 Degrees. M. Secant C. Sec. M. M. Secant Secant M. Secant Secant M. Secant Secant Secant M. Secant Secant M. Secant Secan	55		96429	62609	37391	03571	40961	5				
M Sine C. Sine Tang. C. Tang. Secant C. Sec. M. 0 9.59188 9.96403 9.62785 10.37215 10.03597 10.40812 66 5 59336 96376 62961 315 36624 40664 53 10 59434 96349 63135 36865 03651 40516 54 15 59632 96322 63310 36690 03678 40368 42 25 59924 96267 63657 36343 03733 40076 32 25 59924 96267 63657 36343 03760 40322 4 36 36 37 30763 3236 33 35 9.60215 9.96212 9.64003 36170 03760 393930 32 35 9.60215 9.96212 9.64003 10.35997 10.03785 10.39785 22	60	59188	96403	62785	37215			0				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	M	C. Sine	Sine			C. Sec.	Secant	M				
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	-			67 De	grees.			-				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		<u></u>					0 0	-				
5 59336 96376 62961 37039 03624 40664 5. 10 59484 96349 63135 36865 03651 40516 56 15 59632 96322 63135 36865 03671 40368 4 20 59778 96294 63434 36516 03706 40282 4 25 59924 96267 63657 36343 03733 40076 3 30 60070 96240 63830 36170 03760 39303 3 35 9.60215 9.96212 9.64003 10.35997 10.03785 10.39785 22												
10 59484 96349 63135 36865 03651 40516 50 15 59632 96322 63310 36690 03678 40368 42 20 59778 96294 63434 36516 03706 40222 40 25 59924 96267 63657 36343 03733 40076 32 30 60070 96240 63830 36170 03760 39930 30 35 9.60215 9.96212 9.64003 10.35997 10.03788 10.39785 22												
15 59632 96322 63310 36690 03678 40368 43 20 59778 96234 63434 36516 03706 40222 40 25 59924 96267 63657 36343 03733 40076 32 30 60070 96240 63830 36170 03760 39930 33 35 9.60215 9.96212 9.64003 10.35997 10.03788 10.39785 22												
20 59778 96294 63434 36516 03706 40222 44 25 59924 96267 63657 36343 03733 40076 33 30 60070 96240 63830 36170 03760 39330 35 35 9.60215 9.96212 9.64003 10.35997 10.03785 10.39785 22								50				
25 59924 96267 63657 36343 03733 40076 32 30 60070 96240 63830 36170 03760 39930 30 35 9.60215 9.96212 9.64003 10.355997 10.03788 10.39785 22												
30 60070 96240 63830 36170 03760 39930 30 35 9.60215 9.96212 9.64003 10.35997 10.03788 10.39785 25												
35 9.60215 9.96212 9.64003 10.35997 10.03788 10.39785 24												
	40	60359	96185	64175	35825	03815	39641	20				
								15				
								10				
								5				
								M				
66 Degrees.		C. Maler										

Artificial Sines, Tangents, and Secants. 29

			24 Deg	rees.			-
M	Sine	C. Sine	Tang.	C.Tang.	Secant	C. Sec.	M
Ō	9.60931	9.96073	9.64358	10.35142	10.03927	10.39069	60
5	61073	96045	65028	34972	03955	38927	55
10	61214	96017	65197	34803	03983	38786	50
15	61354	95988	65366		04012	38646	45
20	61494	95960	65535	34465	04040	38506	40
25	61634	95931	65703	34297			35
30	61773	95902	65870	34130	04098	38227	30
35		9.95873					25
40	62049	95844	66204	33796	04156	37951	
45	62186	95815	66371	33629	04185	37814	15
50	62323	95786	66537	33463 33298	04214 04243	37677	10
55	62459	95757 95728	66702 66867	33298	04245	37541	5
60	62595		00007	30135	04272	37405	0
M	C. Sine	Sine	. 65 De	Tang.	C. Sec.	Secant	M
			25 De	grees.			
M	Sine	C. Sine			Secant	C. Sec.	M
0	9.62595	9.95728				10.37405	
5	62730	95698	67032	20068	04902	37270	
10	62865	95668		32804	04332		50
15	62999			32640	04361	37001	45
20	63133		67524	32476	04391	36867	4
25	63266		67687	32313	04421		
30	63398	95549	67687 67850	32804 32640 32476 32313 32150	04451	36602 10.36469	30
35	9.63551	9.95519	9.68012	10.31988	10.04481	10 96469	2
40	63662	95488	68174	31826	04512	36338	20
45	63794			31664			
50	63924			31503	04573		
55	64054				04609		
60	64184	95366	68818	31182	04634	35816	(
M	C. Sine	Sine	C.Tang.	Tang.	C. Sec.	Secant	N
			64 De	grees.			
_				grees.			_
M	Sine	C. Sine				C. Sec.	
0	9.64184					10.35816	
5	64313						
10	64442		69138	30862	04696		
15	64571			30702 30543 30385	0472		
20	64698			30543	04758		4
25				30385	04789	35174	3
30	64953			30226	0482		3
35	9.65079	9.95148	9.69932			10.34921	
40			70089	29911	04884		2
45		95084	10241	29753	04910	34669	
-50		95052				3 34544	
	65580	30040			0498	34420	
55	65705						
55 60 M	-				C See	2 34295 Secant	

			27 De				
M	Sine	C. Sine			Secant	C. Sec.	M
Ō	9.65705	9.94988		10.29283			60
5	65828	94956	70873	29127	05044		55
10	65952	94923	7:028		05077		50
15	66075	94891	71184		05109	33925	45
20	66197	94858	71339		05142		40
25	66319	94826	71493	28507	05174	33681	35
30	66441	94793	71648	28352	05207		30
35	9.66562	9.94760	9.71802	10.28198	10.05240	10.33438	25
40	66682	94727	71955		05273		20
45	66803	94694	72109		05306		15
50			72262	27738			10
55	66922 67042	94627	72415	27585	05373		E
60		94593	72567			32839	Č
M	C. Sine		C.Tang.	Tang.	C. Sec.	Secant	M
		~	62 De	grees.			
		/		grees.			-
M	Sine	C. Sine	Tang.	C.Tang.	Secant	C. Sec.	N
0	9.67161	9.94593	9.72567	10.27433	10.05407	10.32839	60
5	67280	94560	72720		05440		
10	67398	94526	72872				50
16	67515	94492	73023				4
20	67633		73175				40
25	67750		73326				3
30	67866			1			30
35	9.67982		9 73627		10 0564	10.32018	2
40	65098	94321	73777	26223	05679	31902	
45	68213	94286	73927	26073	05714	1 31787	ĩ
50		94252	74077	25923	05748		10
55	68443		74226			31557	
60	68557		74375		05818	31443	1
	C. Sine			Tang	C See	Secant	N
	C, one	, Mile ,		grees.	10. 500	becane	
				grees.			
M	Sine	C. Sine			Secant	C. Sec.	A
0	9.68557	9.94182	9 74375	10 25625	10.05819	3 10.31443	6
5	68671	94147					
10	68784						
15							
20				25031			
25			75117	24883			
30							
35	1			10.24589	10.0606	6 10.30655	
40	69456	93898			0610		
45	69567	93862		24295	0613		
40 50		93826		2 24148			
55	69787	93789	7599	24002			
60							
	C. Sine				C See	. Secant	
111	U. 101110	JUIC I	U. I ally	· rang.	10. DCC	. Decall	1 4

-			30 D	egrees.			
M	Sine	C. Sine	Tang.	C. Tang,	Secant.	C. Sec.	M
0	9.69897	9.93753		10.23856			60
5	70006	93717	76290	23710	06283	29994	55
10	70115	93680	76435	23565	06320		50
15	70224	93643	76580	23420	06357	29776	45
20	70332	93606	76725	23275	06394	29668	40
25	70439	93569	76870	23130	06431	29561	35
30	70547	93532	77015	22985	06468	29453	30
35	9.70654	9.93495		10.22841			25
40	70761	93457	77303	22697	06543	29239	20
45	70867	93420	77447	22553	06580		15
50	70973	93382	77591		06618		10
55	71079	93344	77734	22266	06656	28921	5
60	71184	93307	77877	22123	06693	28816	0
M	C. Sine	Sine	C.Tang.	Tang.	C. Sec.	Secant	M
-			31 De	grees.			-
M	Sine	C. Sine		C.Tang.	Secont	C Sec .	M
0	9.71184	9.93307		10.22123			60
5	71289	93269	78020	21980	06731	28711	55
10	71393	93230	78163	21837	06770	28607	50
15	71498	93192	78306		06808	28502	45
20	71602	93154	78448		06846	28398	40
25	71705	93115	78590	21410	06885	28295	35
30	71809	93077	78732	21268	06923	28191	30
35	9.71911	9.93038		10.21126	10.06962		25
40	72014	92999	79015	20985	07001	27986	20
45	72116	92960	79156	20844	07040	27584	15
50	72218	92921	79297	20703	07079	27782	10
55	72320	92881	79438	20562	07119	27680	5
60	72421	92842	79579	20421	07158		Ō
M	C. Sine	Sine	C.Tang.	Tang.	C. Sec.	Secant.	M
			58 De	grees.			_
			32 Des				
M	Sine	C. Sine		C. Tang.			M
0	9.72421	9.92842		10.20421			60
5	72522	92803	79719	20281	07197	27478	55
10	72622	92763	79860	20140	07237	- 27378	50
15	72723	92723	80000	20000	07277	27277	45
20	72823	92683	80140	19860	07317	27177	40
25	72922	92643	80279	19721	07357	27078	35
30	73022	92603	80419	19581	07397	26978	30
35	9.73121	9.92563		10.19442			25
40	73219	92522	80697	19303	07478	26781	20
.45	73318	92482	80836	19164	07518	26682	15
50	73416	92441	80975	19025	07559	26584	10
55	73513	92400	81113	18887	07600	26487	5
60	73611 C. Sine	92359 Sine	81252 C.Tang.	18748	07641 C. Sec.	26389	0 M

-	· - ·		33 De	grees.			-
M	Sine	C. Sine	Tang.	C.Tang.	Secant	C. Sec.	M
0	9.73611	9.92359	9.81252	10.18748		10.26389	60
5	73708	92318	81390	18610	07682	26292	55
10	73805	92277	81528		07723	26195	50
15	73901	92235	81666	18334	07765	26099	45
20	73997	92194	91803	18197	07806	26003	40
25	74093	92152	81941	18059	07848	25907	35
30	74189	92111	82078	17922	07889	25811	30
35	9.74284	9.92069		10.17785	10.07931	10.25716	25
40	74379	92027	82352	17648	07973	25621	20
45	74474	91985	82489		08015	25526	15
50	74568	91942	82626		08058	25432	10
55	74662	91900	82762	17238	08100		5
60	74756	91857	82899	17101	08143	25244	0
M	C. Sine	Sine	C.Tang.		C. Sec.	Secant	M
_				grees.			-
M	Sinc 1	0 8:		grees.	C	0 0-	3.5
	Sine	C. Sine	Tang.	C.Tang.		C. Sec.	M
0	9.74756	9.91857		10.17101	10.08143		60
5	74850	91815	83035		08185	25150	55
10	74943	91772	83171	16829	08228	25057	50
15	75036	91729	83307	16693	08271	24964	45
20	75128	91686	83442	16558		24872	40
25 30	75221 75313	91643 91599	83578 83713	16422 16287	08357	24779 24687	35 30
35	9.75405	9.91556		10.16151			25
40	75496	91512	83984	16016	08488	24504	20
45	75587	91469	84119	15881		24413	15
50	75678	91425	84254	15746	08575		10
55	75769	91381	84388	15612	08619	24231	5
60	75859	91336	84523	15477	08664		ŏ
	C. Sine		C.Tang.		C. Sec.		-
TAT :	U. omei	ыще	0	grees.	0. 500.	Secant	141
-		NAME OF TAXABLE PARTY.		grees.			
M	Sine	C. Sine	Tang:	C.Tang.	Secant.	C. Sec.	M
0	9.75859	9.91336		10.15477	10.08664		60
5	75949	91292	84657	15343	08708		55
10	76039	91248	84791	15209	08752		50
15	76129	91203	84925	15075	08797	23871	45
20	76218	91158	85059	14941	08842	23782	40
25	76307	91114	85193	14807	08886	23693	35
30	76395	91069	85327	14673	08931	23605	30
35	9.76484	9.91023	9.85460	10.14540	10.08977		25
40	76572	90978	85594	14406	09022	23428	20
45	76660	90933	85727	14273	09067	23340	15
50	76747	90887	85860	14140	09113	23253	10
55	76835	90842	85993	14007	09158	23165	5
60	76922	90796	86126	13874	09204	23078	Ő
M	C. Sine	Sine	C. Tang.		C. Sec.	Secant	M
			54 De	grees.			-

Artificial Sines, Tangents, and Secants. 33

	× ×	-	36 Deg	rees.	_		Ξ,
M	Sine	C. Sine	Tang.	C.Tang.	Secant	C. Sec.	M
	9.76922			10.13874 1			60
5	77009	90750	86259	13741	09250	22991	55
IŎ	77095	90704	86392	13608	09296	22905	50
15	77181	90657	86524	13476	09343	22819	45
20	77268	90611	86656	13344	09389	22732	40
25	77353	90565	86789	13211	09435	22647	35
30	77439	90518	86921	13079	09482	22561	30
35	9.77524	9.90471	9.87053	10.12947	0.09529	10.22476	25
40	77609	90424	87185	12815	09576	22391	20
45	77694	90377	87317	12683	09623	22306	15
50	77778	90330	87449	12552	09670	22222	10
55	77862	90282	87580	12420	09718		5
60	77946	90235	87711	12289	09765	22054	0
	C. Sine	Sine	C.Tang	Tang.	C. Sec.	Secant	M
TAT	U. Sille	Sine in		grees.	0. 500.	i becant	
				grees.			
M	Sine	C. Sine	Tang.	0	Secant	C. Sec.	M
0	9.77946	9.90235		10.12289			
5	78030	90187	87843		09813		
10	78113	90139	87974		0986		
15	78197	90091	8810		0990		
20	78280	90043	88230		0995		
25	78362	89995	8836		1000		
30	78445	89947	88498		1005		
35	9.78527	9.89898	9.8862	0 10.11371	10.1010	2 10.21473	2
40	78609	89849	8875				
45	77691	89801	8889				
50	78772	89752	8902	0 10980			
55	78853	89702	8915	1 10849			
60	78934	89653	8928		1034	7 2106	3 - 0
M	C. Sine	Sine	C.Tang	g. Tang.	C. See	. Secant	IN
		(egrees.			
		-		egrees.			
M	Sine	C. Sine		C.Tang		t C. Sec	
0	9.78934			1 10.10719			
-5	79015						
10	79095						
15	79176						
20							
25	7933						
30							
35				0 10.09810			
40							
45							
50							
5							
60							
IN.	I C. Sin	e Sine	C.Tan	g. Tang. Degrees.	C. Se	c. Secan	t

34 Artificial Sines, Tangents, and Secants.

			39 De			1	-
M	Sine	C. Sine	Tang.	C.Tang.	Secant	C. Sec.	M
0	9.79887	9.89050	9.90837	10.09163	10.10950	10.20113	60
5	79965	88999	90966	09034	11001	20035	55
10	80043	88948	91095	08905	11052	19957	50
15	80120	88896	91224	08776	11104	19880	45
20	80197	88844	91353	08647	11156	19803	40
25	80274	88793	91482	08518		19726	35
30	80351	SS741	91610	08390	11259	19649	30
35	9.80428	9.88688	9.91739	10.08261	10,11312	10.19572	25
40	80504	88636	91868	08132	11364		20
45	80580	88584	91996	08004	11416	19420	15
50	80656	88531	92125	07875			10
55	80731	88478	92253	07747	11522		1
60	80807	88425	92381	07619	11575	19193	0
M	C. Sine	Sine	C.Tang.	Tang.	C. Sec.	Secant	M
			50 De	grees.			
			40 De				1
M,	Sine	C. Sine,	Tang.	C.Tang.	Secant	C. Sec.	Ŋ.
Õ	9.80807	9.88425	9.92381	10.07619	10.11575	10.19193	60
5	80882	88372	92510	07490	11628		54
10	80957	88319	92638	07362	11681	19043	50
15	81032	88266	92766	07234	11734		4
20	81106	88212	92894	07106		18894	4
25	81180	88158	93022	06978	11842	18820	3
30	81254	88105	93150		11895	18746	30
35	9.81328	9.88050	9.93278	10.06722	10.11950	10.18672	2
40	81402	81996	93406	06594	12004	18598	20
45	81475	87942	93533	06467	12058	18525	13
50	81549	87887	93661	06339	-12113	18451	10
55	81622	87833	93789	06211	12167		-
60	81694	87778	93916	06084	12222	18306	
M	C. Sine	Sine	C.Tang.	Tang.	C. Sec.	Secant	i
			49 De	grees.			
-				grees.			
M	Sine	C. Sine	Tang.	C.Tang.		C. Sec.	N
0	9.81694	9.87778	9.93916	10.06084		10.18306	61
5	81767	87723	94044	05956	12277	18233	53
10	81839	87668	94171				50
15	81911	87613					4
20	81983	87557	94426				4
25	82055	87501	94554				3
30	82126	87446	94681			17874	3
35	9.82198	9.87390	9.94808	10.05192	10.12610	10.17802	2
40	82269	87334	94935			17731	20
45	82340	87277	95062				1.
50		87221	95190				10
55	82481	87164					-
60	82551	87107	95444	04556	12893	17449	(
44							
M	C. Sine	Sine	C.Tang.	Tang.	C. Sec.	Secant	N

Artificial Sines, Tangents, and Secants. 35

			42 D	egrees.			-
M	Sine	C. Sine		C.Tang.	Secant.	C. Sec.	M
Ō	9.82551	9.87107		10.04556	10.12893	10.17449	60
5	82621	87050	95571	04429	12950	17379	55
10	82691	86993	95698	04302	13007	17309	50
15	82761	86936	95825	04175	13063	17239	45
20	82830	86879	95952	04048	13121	17170	40
25	82899	86821	96078	03922	13179	17101	35
30	82968	86763	96205	03795	13237	17032	30
35	9.83037	9.86705	9.96332	10.03668	10.13295	10.16963	25
40	83106	86647	96459	03541	13353	16894	20
45	83174	86589	96586	03414	13411	16826	15
50	83242	86530	96712		13470	16758	16
55	83310	86472	96839	03161	13528	16690	5
60	83378	86413	96966		13587	16622	0
M	C. Sine	Sine	C.Tang.		C. Sec.	Secant	M
-		_		egrees.			-
3.4	G ¹	0.0		egrees.		0.0	
M	Sine	C. Sine		C.Tang.			N
0	9.83378	9.86413		10.03034			60
5	83446	86354	97092		13646		5
10	83513	86295	97219			16487	50
15	83581		97345				4
20	83648	86176					40
25	83715	86116					3
30	83781	86056	97725				30
35	9.83848			10.02149			2:
40	83914	85936	. 97978				20
45	83980		98104				1;
50	84046	85815	98231				10
55	84112	85754					4
60	84177		98484				_
M	C. Sine	Sine			C. Sec.	Secant.	M
-				egrees.	-		-
-	- C!	0.0		egrees.			
M	Sine	C. Sine		C.Tang.		C. Sec.	N
0	9.84177	9.85693				10.15823	6
5	84242	85632					5
10	84308	85571	98737				5
15	84373	85510	98863				4
20	84437	85448			14552		40
25	84502	85386					3
30	84566	85324					30
35	9.84630					10.15370	2
40	84694		99493				20
45	84758						1,
50	84822						10
55	84885		99874				-
60	84949			10.00000			(
	C. Sine	Sine	CI CI	. Tang.	0 0	Secant	N

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1.0

III. A TRAVERSE TABLE, or TABLE OF DIFFERENCE OF LATI-TUDE AND DEPARTURE, calculated for degrees and quarters of degrees, and for any distance up to 100 Rods, Chains, &c.; by which the northings and southings, eastings and westings made in a Survey may be found.

Note. Northings and southings are called Difference of Latitude, or simply Latitude; eastings and westings are called Departure, Meridian Distance, or Longitude.

Explanation of the Table.

To find the Latitude and Departure, or Northing, &c. for any Course and Distance.

If the Course be less than 45° , look for it at the top, but if more than 45° at the bottom of the page, and look for the Distance in the right or left hand column; against the Distance, and directly under or over the Course, stand the northing, &c. in whole numbers and decimals.

If the Course be less than 45° , the northing or southing will be greater than the easting or westing; but if more than 45° , the easting or westing will be the greatest.

When the Distance exceeds 100, take any two or more numbers, which, added together, will equal the Distance, and find the Latitude and Departure for each of those numbers; add the several Latitudes together and the sum will be the whole Latitude; and so for the Departure. And when the Distance is in Chains and Links, or whole numbers and decimals, find the Latitude, &c. for the Chains or whole numbers, and then for the Links or decimals, remembering to remove the decimal point in the Table further to the left, according to the given decimal.

EXAMPLES.

1. Required the Latitude and Departure for 45 Rods, on a Course N. 15° 15' W.

Under 15° 15' and against 45 is 43.42 for the northing, and 11.84 for the westing.

2. Required the Latitude and Departure for 120 Rods, on a Course S. 58° 30' E.

Take one third of 120 which is 40; against this number, over 58° 30' is 29.90 for the Latitude and 34.11 for the Departure. These multiplied by 3 give 62.70 for the Southing and 102.33 for the Easting.

3. Required the Latitude and Departure for 37.36 Rods or 37 Chains and 36 Links, on a Course N. 26° 45' E.

For 37. 0.36	Lat. 33.04 .32	Dep. 16.65 .16
37.36	33.36	16.81
57.50	00.00	10.01

Northing 33.36 Easting 16.81

Note. When the Minutes are not 15, 30, or 45, the Northings, &c. must be calculated by Natural Sines, or by Trigonometry.

38 TRAVERSE TABLE.

The second second

20							
D	$\frac{1}{4}$ D	e g:	$\frac{1}{2}$ D	eg.	3 D	eg.	D
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	st.
1	1.00	0.00	1.00	0.01	1.00	0.01	1
2	2.00	0.01	2.00	0.02	2.00	0.03	2
.3	3.00	0.01	3.00	0.03	3.00	0.04	3
45	4.00	0.02	4.00 5.00	0.03	4.00 5.00	0.05	5
6	6.00	0.03	6.00	0.05	6.00	0.08	6
7	7.00	0.03	7.00	.0.06	7.00	0.09	7
8	8.00	0.03	. 8.00	0.07	8.00	0.10	8
9 10	9.00 10.00	0.04 0.04	9.00 10.00	0.08	9.00 10.00	0.12	9 10
11	11.00	0.05	11.00	0.10	$11.00 \\ 12.00$	0.14	11 12
12	12.00 13.00	0.05	$12.00 \\ 13.00$	0.10	12.00	0.16 0.17	13
	14.00	0.06	14.00	0.12	14.00	0.18	14
15	15.00		15.00	0.13	15.00	0.20	15
16	16.00	0.07	16.00	0.14	16.00	0.21	16
17	17.00	0.07	17.00	0.15	17.00	0.22	17
	18.00	0.08	18.00	0.16	18.00 19.00	0.24 0.25	18 19
19	19.00 20.00	0.08	19.09 20.00	0.17	20.00	0.25	20
							-
21	21.00 22.00		21.00	0.18	21.00 22.00	0.27 0.29	21 22
	22.00		22.00 23.00	0.20	23.00	0.29	23
	24.00		24.00	0.21	24.00	0.31	24
	25.00		25.00	0.22	25.00	0.33	25
	26.00	0.11	26.00	0.23	26.00	0.34	26
	27.00	0.12	27.00	0.24	27.00	0.35	27
	28.00		28.00	$0.24 \\ 0.25$	28.00 29.00	0.37	28 29
	30.00		29.00 30.00	0.26	30.00	0.38	30
01	21.00	0.14	21.00	0.27	31.00	0.41	31
	31.00		31.00 32.00		32.00		32
	33.00		33.00		33.00		33
34	34.00	0.15	34.00	0.30	34.00	0.45	34
	35.00		35.00		35.00		35
	36.00		36.00		36.00		36
	37.00 38.00		37.00 38.00		37.00 38.00	0.48	37
	39.00		39.00				39
	40.00		40.00				40
41	41.00	0.18	41.00	0.36	41.00	0.54	41
42	2 42.00	0.18	42.00	0.37	42.00	0.55	42
4	3 43.00	0.19	43.00	0.38	43.00	0.56	43
	44.00		44.00				
	5 45.00		45.00		45.00		45
	546.00 7 47.00		46.00		40.00		
48	3 48.00	0.21	48.00		48.00		
	9 49.00	0.21	49.00	0.43	49.00	0.64	49
50	50.00	0.22	50.00	0.44	50.00	0.65	50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
ā	893	Deg.	$89\frac{1}{2}$	Deg.	891	Deg.	Í.

	1 D	eg.	1 De	or I	1 3 D	eg.	-
Dis	4	cg.	200	5.	. 4	cg.	2
st.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	st.
51	51.00	0.22	51.00	0.45	51.00	0.67	51
52	52.00	0.23	52.00	0.45	52.00	0.68	52
53 54	53.00	0.23	53.00	0.46	53.00	0.69	53
55	54.00 55.00	0.24 0.24	54.00 55.00	0.47	54.00 55.00	0.71 0.72	54 55
56	56.00	0.24	56.00	0.49	56.00	0.73	56
57	57.00	0.25	57.00	0.50	57.00	0.75	57
58	58.00	0.25	58.00	0.51	57.99	0.76	58
59	59.00	0.26	59.00	0.51	58.99	0.77	59
60	60.00	0.26	60.00	0.52	59.99	0.79	_ 60
61	61.00	0.27	61.00	0.53	60.99	0.80	61
62 63	62.00	0.27	62.00	0.54	61.99	0.81	62
64	63.00 64.00	0.27	63.00	0.55	62.99	0.82	63 64
65	65.00	0.28	64.00 65.00	0.56	63.99 64.99	0.84	65
66	66.00	0.29	66.00	0.58	65.99	0.86	66
67	67.00	0.29	67.00	0.58	66.99	0.88	67
68	68.00	0.30	68.00	0.59	67.99	0.89	68
69 70	69.00 70.00	0.30	69.00 70.00	0.60	68.99	0.90	69
			10.00	0.61	69.99	0.92	70
71	71.00	0.31	71.00	0.62	70.99	0.93	71
72 73	72.00	0.31	72.00	0.63	71.99	0.94	72
74	74.00	0.32	73.00	0.64 0.65	72.99	0.96	73 74
75	75.00	0.33	75.00	0.65	74.99	0.97	75
76	76.00	0.33	76.00	0.66	75.99	0.99	76
77	77.00	0.34	77.00	0.67	76.99	1.01	77
78	78.00	0.34	78.00	0.68	77.99	1.02	78
79 80	79.00 80.00	0.34	79.00 80.00	0.69	78.99 79.99	1.03	79 80
		0.50		0.70	13.33	1.05	00
81	81.00		81.00	0.71	80.99	1.06	81
82 83	82.00 83.00		82.00 83.00	0.72	81.99 82.99		82 83
84	84.00		84.00	0.72	83.99	1.10	84
85	85.00		85.00	0.74	84.99		85
86	86.00		86.00	0.75	85.99	1.13	86
87	87.00	0.38	87.00	0.76 0.77	86.99		87
88 89	88.00 89.00		88.00 89.00	0.77	87.99 88.99		
90	90.00		90.00	0.79	89.99		
91	91.00	0.40	91.00	0.79	90.99	1.19	91
92	92.00		92.09	0.80	91.99	1.20	
93	93.00	.0.41	93.00	0.81	92.99	1.22	93
94	94.00		94.00	0.82	93.99	1.23	
95	95.00		95.00	0.83	94.99		
96 97	96.00		96.00 97.00	0.84	95.99	1.26	96
98	98.00		98.00	0.86	97.99		
99	99.00	0.43	99.00	0.86	98.99	1.30	99
100	160.00	0.44	100.00	0.87	99.99	1.31	100
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
Ā	89 <u>3</u> 1	Deg.	891C	eg.	891	Deg.	ñ

TRAVERSE TABLE.

						-	-	-	
D	1 D	eg.		Deg.	111	Deg.	13	Deg.	Di
st.	Lat.	Dep,	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	st.
1	1.00	0.02	1.00	0.02	1.00	0.03	1.00		1
23	2.00	0.03	2.00	0.04	2.00	0.05	2.00	0.06	23
4	4.00	0.03	4.00	0.09	4.00	0.10	4.00	0.12	4
5	5.00	0.09	5.00	0.11	5.00		5.00		5
6	6.00	0.10	6.00	0.13	6.00		6.00		
78	7.00	0.12	7.00	0.15	7.00		7.00		8
9	8.00 9.00	0.14 0.16	8.00	0.17	8.00	0.21	8.00		
10	10.00	0.17	10.00	0.22	10.00		10.00		10
	11.00	0.19	11.00	0.24	11.00	0.28	10.99	0.34	
	12.00	0.21	12.00	0.26	12.00		11.99	0.37	
		0.23	13.00	0.28	13.00	0.34	12.99		
	$14.00 \\ 15.00$	0.24 0.26	14.00 15.00	0.31	14.00	0.37	13.99		
		0.28	16.00	0.35	15.99	0.42	15.99		
17	16.00 17.00	0.30	17.00	0.37	16.99	0.45	16.99	0.52	17
	18.00	0.31	18.00	0.39	17.99		17.99		
	19.00 20.00	0.33 0.35	19.00 20.00	0.41 0.44	18.99 19.99		18.99 19.99		
21	21.00	0.37	21.00	0.46	20.99	0.55	20.99	0.64	21
22	22.00	0.38	21.99	0.48	21.99	0.58	21.99		
23	23.00	0.40	22.99	0.50			22.99		
	24.00	0.42	23.99	0.52		0.63	23.99		
25	25.00	0.44 0.45	24.99 25.99	0.55	24.99 25.99	0.65	24.99 25.99		
27	26.00 27.00	0.43	26.99	0.59	26.99		26.99	0.83	
	28.00	0.49	27.99	0.61			27.99		
	29,00	0.51	28.99	0.63			28.99		
30	30.00	0.52	29.99	0.65	29.99	0.79	29.99	6.92	30
	31.00	0.54	30.99	0.68		0.81	30.99		
	32.00 32.99	0.56	$31.99 \\ 32.99$	0.70	31.99 32.99	0.84	31.99 32.98		
34	33.99	0.59	33.99	0.74		0.89	33.98		
	34.99	0.61	34.99	0.76	34.99	0.92	34.98	1.07	35
	35.99	0.63	35.99	0.79			35.98		
	36.99 37.99	0.65	36.99 37.99	0.81 0.83	36.99 37.99	0.97	36.98		
	38.99	0.68	38.99	0.85		1.02	38.98		
	39.99	0.70	39.99	0.87			39.98		
	40.99	0.72	40.99	0.89	40.99	1.07	40.98		
	41.99	0.73	41.99	0.92			41.98		
	42.99 43.99	0.75	42.99	0.94	42.99 13.99	1.13	42.98 43.98	1.31	43 44
	43.39	0.79	43.93	0.98	44.99	1.13	43.98	1.34	44
46	45.99	0.80	45.99	1.00	45.99	1.20	45.98		
	46.99	0.82	46.99	1.03	46.99	1.23	46.98	1.44	47
	47.99	0.84	47.99	1 05	47.98	1.26	47.98	1.47	48
	48.99 49.99	0.86 0.87	48.99 49.99	1.07 1.09	48.98 49.98	$1.28 \\ 1.31$	48.98 49.98	$1.50 \\ 1.53$	49 50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	it.
Die	89	Deg.	883	Deg.	881	Deg.	881	Deg.	Dist
_		-0.1	4	-0.1	2	-0.1	4	-0.	

D	1 D	eg.	$1\frac{1}{4}$	Deg.	11	Deg.	$1\frac{3}{4}I$	Deg.	D
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
51	50.99	0.89	50.99	1.11	50.98	1.34	50.98	1.56	51
52		0.91	51.99	1.13	51.98	1.36	51.98	1.59	52
	52.99	0.92	52.99	1.16	52.98	1.39	52.98	1.62	53
	$53.99 \\ 54.99$	0.94	$53.99 \\ 54.99$	1.18	53.98 54.98	1.41 1.44	53.97	1.65	54 55
	55.99	0.98	55.99	1.20	55.98	1.47	54.97 55.97	1.71	56
	56.99	0.99	56.99	1.24	56.98	1.49	56.97	1.74	57
	57.99	1.01	57.99	1.27	57.98	1.52	57.97	1.77	58
59	58.99	1.03	58.99	1.29	58.98	1.54	58.97	1.80	59
60	59.99	1.05	59.99	1.31	59.98	1.57	59.97	1.83	60
	60.99		60.99	1.33	60.98	1.60	60.97	1.86	61
62	61.99		61.99	1.35	61.98	1.62	61.97	1.89	62
63	62.99		62.99	1.37	62.98	1.65	62.97	1.92	63
65	63.99		63.98	1.40	63.98	1.68	63.97	1.95	64
66	64.99 65.99	1.15	64.98 65.98	$1.42 \\ 1.44$	64.98 65.98	1.70 1.73	64.97 65.97	$1.99 \\ 2.02$	65 66
67	66.99	1.17	66 98	1.46	66.98		66.97	2.05	67
68	67.99	1.19	67.98	1.48	67.98		67.97	2.08	68
69	68.99	1.20	68.98	1.51	68.98		68.97	2.11	69
70	69.99	1.22	69,98	1.53	69.98		69.97	2.14	70
71	70.99	1.24	70.98	1.55	70.98	1.86	70.97	2.17	71
72	71.99	1.26	71.98	1.57	71.98		71.97	2.20	72
73	72.99	1.27	72.98	1.59	72.97	1.91	72.97	2.23	73
74	73.99	1.29	73.98	1.61	73.97	1.94	73.97	2.26	74
75 76	74.99 75.99	$1.31 \\ 1.33$	74.98	1.64	74.97	1.96	74.97	2.29	75
77	76.99	1.33	76.98	1.68	76.97	$1.99 \\ 2.02$	75.96	$2.32 \\ 2.35$	76 77
78	77.99	1.36	77.98	1.70	77.97	2.04	77.96	2.38	78
79		1.38	78.98	1.72	78.97		78.96	2.41	79
80		1.40	79.98	1.75	79.97		79.96	2.44	80
81	80.99	1.41	80.98	1.77	80.97		90.96	2.47	81
82		1.43	81.98	1.79	81.97		81.96	2.50	82
83 84		1.45	82.98		82.97		82.96	2.53	83
	84.95	$1.47 \\ 1.48$	83.98 84.98	1.83	83.97 84.97	$2.20 \\ 2.23$	83.96 84.96	2.57	84 85
	85.95	1.40	85.98		85.97		85.96		86
	86.99	1.52	86.98		86.97		86.96	2.66	87
88		1.54	87.98		87.97		87.96		88
89	88.99	1.55	88.98	1.94	88.97	2.33	88.96		89
90	89.99	1.57	89.98	1.96	89.97	2.36	89.96	2.75	90
91	90.99	1.59	90.98		\$0.97		90.96		91
	91.99	1.61	91.98		91.97		91.96		92
	92.99	1.62	92.98		92.97		92.96	2.84	
94 95	93.99	$1.64 \\ 1.66$	93.98 94.98		93.97		93.96 94.96		94
	95.99	1.68	95.98		95.97		94.90		
97		1.69	96.98	2.12	96.97	2.54			
	97.99	1.71	97.98		97.91		97.95		98
99		1.73	98.98	2.16	98.97	2.59	98.95	3.02	99
100	99.98	1.75	99,98	2.18	99.97	2.62	99.95	3.05	100
-	1	1			1			1	

Dep.

89

Lat.

Deg.

st.

41

10

Dep.

Lat.

881 Deg. 881 Deg

Lat.

Dep.

883 Deg.

Dist.

Dep. Lat.

IE	21	Deg.	21/4	Deg.	$2\frac{1}{2}$	Deg.	23	Deg.	E
ist.	Lat.	Dep.	Lat.	Dep.	Lat	.Dep.	Lat.	Dep.	ist.
1			1.00						
23	2.00		2.00						
4			3.00						
5			5.00						
6			6.00						
7	7.00	0.24	6.99						
-8			7.99		7.99				
9			8.99	0.35	8.9				
10	9.99	0.35	9.99	0.39	9.99	0.44	9.99	0.48	10
11	10.99	0.38	10.99	0.43	10.99	0.48	10.99	0.53	n
	11.99		11.99	0.47	11.99				
	12.99		12.99	0.51	12.99		12.99	0.62	13
	13.99	0.49	13.99	0.55	13.99		13.98 14.98	0.67	14
	14.99 15.99	0.52	14.99 15.99	0.59				0.77	16
	16.99	0.59	16.99	0.67	16.98				
	17.99	0.63	17.99	0.71	17.98		17.98	0.86	18
	18.99	0.66	18.99	0.75	18.98				19
20	19.99	0.70	19.98	0.79	19.98	8 0.87	19.98	0.96	20
21	20.99	0.73	20.98	0.82	20.98	0.92	20.98	1.01	21
22	21.99	0.77	21.98	0.86	21.98		21.97	1.06	22
	22.99	0.80	22.98	0.90	22.98		22.97	1.10	23
	23.99	0.84	23.98	0.94	23.98		23.97	1.15	24
25	24.98 25.98	0.87	24.98 25.98	0.98	24.98 25.98		24.97 25.97	$1.20 \\ 1.25$	$\frac{25}{26}$
20	26.98	0.91	26.98	1.02	26.97		26.97	1.30	27
	27.98		27.98	1.10	27.97		27.97	1.34	28
29	28.98	1.01	28.98	1.14	28.97	1.26	28.97	1.39	29
30	29.98	1.05	29.98	1.18	29.97	1.31	29.97	1.44	301
31	30.98	1.08	30.98	1.22	30.97	1.35	30.96	1.49	31
32	31.98	1.12	31.98	1.26	31.97		31.96	1.54	32
	32.98	1.15	32.97	1.30	32.97		32.96	1.58	33
	33.98	1.19	33.97	1.33	33.97	1.48	33.96	1.63	34
	34.98	1.22	34.97	1.37	34.97	1.53	34.96	1.68	35
	35.98 36.98	$1.26 \\ 1.29$	35.97 36.97	1.41 1.45	35.97 36.96	$1.57 \\ 1.61$	35.96 36.96	1.73	$\frac{36}{37}$
38	37.98	1.29	37.97	1.49	37.96		37.96	1.82	38
	38.98	1.36	38.97	1.53	38.96	1.70	38.96	1.87	39
	39.98	1.40	39.97	1.57	39.96		39.95	1.92	.40
41	40.98	1.43	40.97	1.61	40.96	1.77	40.95	1.97	41
	41.97	1.47	41.97	1.65	41.96	1.83	41.95	2.02	42
43	42.97	1.50	42.97	1.69	42.96	1.88	42.95	2.06	43
	43.97	1.54	43.97	1.73	43.96	1.92	43.95	2.11	44
	44.97	1.57	44.97	1.77	44.96 45,96	1.96 2.01	$44.95 \\ 45.95$	2.16	45
	$45.97 \\ 46.97$	1.61 1.64	45.96 46.96	1.81 1.85	45.96	2.01	46.95	$2.21 \\ 2.25$	46 47
	47.97	1.68	47.96	1.88	47.95	2.09	47.95	2.30	48
	48.97	1.71	48.96	1.92	48.95	2.14	48.94	2.35	49
	49.97	1.74	49.96	1.96	49.95	2.18	49.94	2.40	50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
i	881	Jeg.	87 <u>3</u> 1	Deg.	$87\frac{1}{2}$	Deg.	87 <u>1</u>)eg.	5

E	2 D	eg.	21	Deg.	21	Deg.	23	Deg.	E
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
51	50.97	1.78	50.96	2.00	50.95	2.22	50.94	2.45	51
52 53	51.97 52.97	1.81 1.85	51.96 52.96	2.04	51.95	2.27 2.31	51.94 52.94	2.50 2.54	52 53
54	53.97	1.88	53.96	2.08 2.12	52.95 53.95	2.31	53.94	2.54	54
55	54.97	1.92	54.96	2.16	54.95	2.40	54.94	2.64	55
56 57		1.95	55.96	2.20	55.95	2.44	55.94	2.69	56 57
58	56.97 57.96	1.99 2.02	56.96 57.96	$2.24 \\ 2.28$	56.95 57.94	2.49 2:53	56.93 57.93	2.73 2.78	58
59	58.96	2.06	58.95	2.32	58.94	2.57	58.93	2.83	59
60	59.96	2.09	59.95	2.36	59.94	2.62	59.93	2.88	60
61	60.96	2.13	60.95	2.39	60.94	2.66	60.93	2.93	61
62 63	61.96	$2.16 \\ 2.20$	61.95	2.43	61.94	2.70	61.93	2.97	62 63
	62.96 63.96	2.20	62.95 63.95	$2.47 \\ 2.51$	$62.94 \\ 63.94$	$2.75 \\ 2.79$	62.93 63.93	3.02 3.07	64
65	64.96	2.27	64.95	2.55	64.94	2.84	64.93	3.12	65
66	65.96	2.30	65.95	2.59	65.94	2.88	65.92	3.17	66
67	66.96 67.96	$2.34 \\ 2.37$	66.95 67.95	$2.63 \\ 2.67$	66.94 67.94	2.92 2.97	66.92	3.21 3.26	67 68
69	68.96	2.41	68.95	2.71	68.93	3.01	67.92 68.92	3.31	69
	69.96	2.44	69.95	2,75	69.93	3.05	69.92	3.36	70
71	70.96	2.48	70.95	2.79	70.93	3.10	70.92	3.41	71
	71.96	2.51	71.94	2.83	71.93	3.14	71.92	3.45	72
	72.96	2.55	72.94	2.87	72.93	3.18	72.92	3.50	73
	73.95 74.95	$2.58 \\ 2.62$	73.94 74.94	$2.91 \\ 2.94$	73.93 74.93	3.23 3.27	73.91 74.91	3.55 3.60	74 75
	75.95	2.65	75.94	2.98	75.93	3.31	75.91	3.65	76
77	76.95	2.69	76.94	3.02	76.93	3.36	76.91	3.70	77
	77.95	2.72	77.94	3.06	77.93	3.40	77.91	3.74	78
79 80	78.95 79.95	$2.76 \\ 2.79$	78.94 79.94	3.10 3.14	78.92 79.92	$3.45 \\ 3.49$	78.91 79.91	3.79 3.84	79 80
81	80.95	2.83	80.94	3.18	80.92	3.53	80.91	3.89	81
	81.95	2.86	81.94	3.22	81.92	3.58	81.91	8.93	82
83	82.95	2.90	82.94	3.26	82.92	3.62	82.90	3.98	83
	83.95	2.93	83.94 84.93	3.30	83.92	3.66	83.90	4.03	84
86	84.95 85.95	3.00	85.93	3.34 3.38	84.92 85.92	$3.71 \\ 3.75$	84.90 85.90	4.08 4.13	85 86
	86.95	3.04	86.93	3.42	86.92	3.79	86.90	4.17	87
88	87.95	3.07	87.93	3,45	87.92	3.84	87.90	4.22	88
89 90	88.95 89.95	$3.11 \\ 3.14$	88.93 89.93	3.49 3.53	88.92 89.91	3.88 3.93	88.90 89.90	4.27 4.32	89 90
-		3.18							_
	$90.95 \\ 91.94$	3.18	90.93 91.93	3.57 3.61	90.91 91.91	3.97 4.01	90.90 91.89	4.37	91 92
	92.94	3.25	92.93	3.65	92.91	4.06	92.89	4.40	92 93
94	93.94	3.28	93.93	3.69	93.91	4.10	93.89	4:51	94
	94.94	$3.32 \\ 3.35$	94.93	3.73	94.91	4.14	94.89	4.56	95
	95,94 96.94	3.35	95.93 96.93	3.77 3.81	$95.91 \\ 96.91$	4.19 4.23	95.89 96.89	4.61 4.65	96 97
	97.94	3.42	97,92	3.85	97.91	4.27	97.89	4.70	98
	$98.94 \\ 99.94$	3,46 3.49	98,92 99.92	3.89 3.93	98.91 99.91	4.32 4.36	98.89 99.88	4.75 4.80	99 100
-									
ist		Lat.	Dep.		Dep.		Dep.		ist.
8	88 1	Deg.	$[87\frac{3}{4}]$	Deg.	$87\frac{1}{2}$	Deg.	871	Deg.	9

TRAVERSE TABLE.

	9.0		101 1		911) Dan II	921		-
D	3 D	eg.	341	Deg.	$3\frac{1}{2}$	Deg.	34 1	Deg.	5
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1	1.00	0.05	1.00	0.06	1.00	0.06	1.00	0.06	1
2	2.00	0.10	2.00	0.11	2.00	0.12	2.00	0.13	2
3 4	3.00 3.99	0.16 0.21	3.00	0.17 0.23	2.99 3.99	0.18	2.99	0.20	3 4
- 5	4.99	0.26	4.99	0.28	4.99	0.31	4.99	0.33	5
6	5.99	0.31	5.99	0.34	5.99	0.37	5.99	0.39	6
7	6.99	0.37	6.99	0.40	6.99	0.43	6.99	0.46	7
8 9	7.99 8.99	0.42 0.47	.7.99 8.98	0.45	7.99 8.98	0.49	7.98		8 9
10	9.99	0.52	9.98	0.57	9.98	0.61	9.98		10
11	10.98	0.58	10.98	0.62	10.98	0.67	10.98		
12	11.98	0.63	11.98	0.68	11.98	0.73	11.97		12
13	12.98 13.98	0.68	$12.98 \\ 13.98$	0.73 0.79	12.98 13.97	0.79	12.97	0.85	
	13.98	0.79	14.98	0.19	14.97	0.85	14.97		14
16	15.98	0.84	15.97	0.91	15.97	0.98	15.97	1.05	16
	16.98	0.89	16.97	0.96	16.97	1.04	16.96		17
	17.98 18.98	0.94 0.99	17.97 18.97	1.02	17.97	1.10	17.96		
20	19.97	1.05	19.97	1.13	19.96		19.96		
21	20.97	1.10	20.97	1.19	20.96	1.28	20.96		21
22	21.97	1.15	21.96	1.25	21.96	1.34	21.95		
	22.97	1.20	22.96	1.30	22.96	1.40	22.95		
24	23.97 24.97	1.26 1.31	23.96 24.96	1.36	23.96 24.95	$1.47 \\ 1.53$	23.95		
26	25.96	1.36	25.96	1.47	25.95	1.59	25.94		
27	26.96	1.41	26.96	1.53	26.95	1.65	26.94	1.77	27
	27.96	1.47	27.95	1.59	27.95	1.71	27.94		
	28.96 29.96	1.52 1.57	28.95 29.95	1.64 1.70	28.95 29.94	1.77 1.83	28.94 29.94		
31	30.96	1.62	30.95	1.76	30.94	1.89	30.93	2.03	31
	31.96	1.67	31.95	1.81	31.94		31.93		1
	32.95	1.73 1.78	32.95	1.87	32.94		32.93		
	33.95		33.95	1.93	33.94		33.93		
	34.95 35.95	1.83	34.94 35.94	1.98	34.93 35.93		34.92 35.92		
	36.95		36.94	2.10	36.93	2.26	36.92		
	37.95		37.94	2.15	37.93		37.92	2.49	
39 40	38.95 39.95	2.04	38.94 39.94	2.21 2.27	38.93 39.93		38.92 39.91		
-	40.94		40.93	2.32	40.92	2.50	40.91		
	41.94	2.20	41.93	2.38	41.92	2.56	41.91	2.75	42
43	42.94	2.25	42.93	2.44	42.92	2.63	42.91	2.81	43
	43.94		43.93	$2.49 \\ 2.55$	43.92		43.91		
	44.94 45.94		44.93 45.93	2.55	44.92 45.91	$2.75 \\ 2.81$	44.90		
	46.94			2.66	46.91		46.90		
48	47.93	2.51	47.92	2.72	47.91	2.93	47.90	3.14	48
	48.93		48.92 49.92	2.78	48.91 49.91		48.90		
1.	Dep.	Lat.	Dep.	Lat.	Dep.		Dep.	Lat.	t.
Dis			863	Der		Deg.	861	Dec	Dis
E	101	Deg.	004	Deg.	002	Deg.	004	Deg.	

D	31)eg.	31	Deg.	31	Deg.	33	Deg.	10
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ISC.
51	50.93	2.67	50.92	2.89	50.90	3.11	50.89	3.34	5
52	51.93	2.72 2.77	51.92	2.95	51.90	3.17	51.89	3.40	5
53	52.93	2,77	52,91	3,00	52.90	3.24	52.89	3.47	
	53.93	2.83	53.91		53.90	3,30	53.88	-3.53	
.55	54.92	2.88	54.91	3,12	54.90	3.36	54.88	3.60	
50	55.92	2,93	55,91	3.17	55.90	3.42	55.88		5
51	56.92	2.98	56.91	3.23	56.89	3.48	56.88	3.73	5
	57.92	3.04	57.91	3.29	57.89	3.54	57.88	3.79	
60	58.92 59.92	3.14	58,91 59,90	3.34 3.40	58.89 59.89	3.60 3,66	58.87 59.87	3.86	
61	60.92	3.19	60.90	3.46	60.89	3.72	60.87	3.99	6
	61.92	3.24	61.90	3.51	61.88	3.79	61.87	4.05	
63	62.91	3.30	62.90	3.57	62.88	3.85	62.87	4.12	6
64	62.91 63.91	3.35	63.90	3.63	63.88	3.91	63.86	4.19	
	64.91	3.40	64.90	3.69	64.88	3.97	64.86	4.25	
66	65,91	3.45	65.89	3.74	65.88	4.03	65.86	4.32	6
67	66.91	3.51	66.89	3.80	66.88	4.09	66.86	4.39	6
68	67.91	3.56	67.89	3,86	67.87	4.15	67.85	4.45	6
	68,91	3.61	68.89	3.91	68.87	4.21	68.85	4.51	6
70	69,90	3.66	69.89	3,97	69.87	4.27	69.85	4.58	7
	70.90	3.72	70.89	4.03	70,87	4.33	70.85	4.64	
	71.90	3.77	71.88	4.08	71.87	4.40	71.85	4.71	7
	72.90	3.82	72.88	4.14	72.86	4.46	72.84	4.77	7
	73.90	3.87	73.88	4.20	73.86	4.52	13.84	4.84	
	74,90	3.93	74.89	4.25	74.86	4.58		4.91	7
	75.90 76.89	3.99 4.03	75.88	4.31 4.37	75.86	4.64	75.84	4.97	7
78	77.89	4.08	77.87	4.42	77.85	4.70	76.84	5.04	
79	78.89	4.13	78.87	4.49	78.85	4.82	78.83	5.17	7
	79.89	4.19	79.87	4.54	79.85	4.88		5.23	
81	80.89	4.24	80.87	4.59	80.85	4.94	80.83	5.30	8
	81.89	4.29	81.87	4.65	81.85	5.01	81.82	5.36	
	82.89	4.34	82.87	4.71	82.85	5.07	82.82	5.43	8
84	83.88	4.40	83.86	4.76	83.84	5.13	83.82	5.49	8
85	84.88	4.45	84.86	4.82	84.84	5.19	84.82	5.56	8
	85.88	4.50	85.86	4.98	85.84	5.25	\$5.82	5.62	8
	86.88	4.55	86.86	4.93	86.24	5.31		5.69	8
	87.88	4.61	87.86	4.99	87.84	5.37	87.81	5.76	8
	88.88 89.88	4.66	88.86	5.05 5.10	88.83 89.83	5.43	88.81 89.81	5.82	8
<u>.</u>									-
	90.88	4.76	90.85	5.16	90.83	5.56	90.81	5.95	9
	91.87 92.87	4.81	91.85 92.85	5.22	91.83 92.83	5.62 5.68	91.80	6.02	9: 9:
	93.87	4.92	93.85	5.33	93.82	5.74	92.80 93.80	6.08 6.15	9.
	94,87	4.97	94.85	5.39	94.82	5.80	94.80	6.21	9
	95.87	5.02	95.85	5.44	95.82	5.86	95.79	6.28	.90
	96,87	5.08	96.84	5.50	96.82	5.92	96.79	6.34	9
	97.87	5.13	97.84	5.56	97.82	5.98	97.79	6.41	95
	98.86	5.18	98.84	5.61	98.82	6.04	97.79 98.79	6.47	99
00	99,86	5.23	99.84	5.67	99.81	6,10		6.54	
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
5	87	Deg.	863	Deg.	861	Deg.	8611	Deg.	ā

E	4 I	Deg.	41	Deg.	41/2	Deg.	43	Deg.	10
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
12			1.00	0.07	1.00	0.08	1.00		
. 3	2.99	0.21	2.99	0.22	2.99	0.24	1.99	0.25	3
45		0.28	3.99	0.30	3.99	0.31	3.98 4.98		
6	5.99	0.42	5.98	0.44	5.98	0.47	5.98	0.50	6
7		0.49	6.98 7.98	0.52	6.98	0.55 0.63	6.97 7.97		
9	8.98	0.63	8.98	0.67	8.97	0.71	8.97	0.75	9
10	9.98	0.70	9.97	0.74	9.97	0.78	9.97	0.83	10
	10.97	0.77	10.97	0.82	10.97		10.96		
13	11.97 12.97	0.84	11.97 12.96	0.89 0.96	11.96 12.96	0.94 1.02	11.96 12.96	0.99	
14	13.97	0.98	13.96	1.04	13.96	1.10	13.95	1.16	14
16	14.96 15.96	1.05	14.96 15.96	1.11 1.19	14.95 15.95	1.18	14.95 15.95	1.24	
17	16.96 17.96	1.19	16.95 17.95	1.26	16.95	1.33	16.94	1.41	17
19	18.95	1.20	18.95	1.33	17.94 18.94	1.41 1.49	17.94	1.49	19
20	19.95	1.40	19.95	1.48	19.94	1.57	19.93	1.66	20
21	20.95	1.46	20.94	1.56	20.94	1.65	20.93	1.74	
	21.95 22.94	1.53	21.94 22.94	1.63	21.93 22.93	1.73	21.92 22.92	1.82	
24	23.94	1.67	23.93	1.78	23.93	1.88	23.92	1.99	24
	24.94 25.94	1.74	24.93 25.93	1.85 1.93	24.92 25.92	$1.96 \\ 2.04$	24.91 25.91	2.07	25
27	26.93	1.88	26.93	2.00	26.92	2.12	26.91	2.24	27
	27.93 28.93	$1.95 \\ 2.02$	27.92 28.92	2.08 2.15	27.91 28.91	$2.20 \\ 2.28$	27.90 28.90	2.32	28 29
	29.93	2.02	29.92	2.22	29.91	2.20	29.90	2.40 2.48	
31	30.92	2.16	30.91	2.30	30.90	2.43	30.89	2.57	31
32	31.92	2.23	31.91	2.37	31.90	2.51	31.89	2.65	32
	32.92 33.92	2.30 2.37	32.91 33.91	$2.45 \\ 2.52$	32.90 33.90	2.59	32.89 33.88	$2.73 \\ 2.82$	33 34
35	34.91	2.44	34.90	2.59	34.89	2.75	34.88	2.90	35
	35.91 36.91	2.51 2.58	35.90 36.90	2.67	35.89 36.89	2.82	35.88 36.87	2.98	36
38	37.91	2.65	37.90	2.82	37.88	2.98	37.87	3.15	38
	38.90 39.90	2.72	38.89 39.89	2.89	38.88 39.88	3.06	38.87 39.86	3.23 3.31	39 40
	40.90 41.90	2.86	40.89 41.88	3.04 3.11	40.87 41.87	3.22 3.30	40.86 41.86	3.40 3.48	41 42
43	42.90	3.00	42.88	3.19	42.87	3.37	42.85	3.56	43
	43.89 44.89		43.88 44.88	3.26	43.86 44.86	3.45	43.85 44.85	3.64 3.73	44 45
46	45.89	3.21	45.87	3.41	45.86	3.61	45.84	3.81	46
	46.89 47.88	3.28 3.35	46.87	3.48	46.86 47.85	3.69	40.84 47.84	3.89 3.97	47
49	48.88 49.88	3.42 3.49	48.87 49.86	3.63	43.85 49.85	3.84	43.83 49.83	4.06	49
								4.14	50
ist.	Dep.				Dep.		Dep.		ist.
9	86 I	Deg.	853I	Jeg.	85 <u>1</u>	Deg.	85 <u>1</u> I)eg.	9

D	4 D	eg.	41	Deg.	$4\frac{1}{2}$	Deg.	43	Deg.	E
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
51	50.88	3.56	50.86	3.78	50.84	4.00	50.82	4.22	51
	51.87	3.63	51.86	3.85	51.84	4.08	51.82	4.31	52
	52.87	3.70	52.85 53.85	3.93	52.84		52.82	4.39	53
	53.87 54.87	3.84	54.85	4.00	53.83 54.83		53.81 54.81	4.47	54 55
	55.86	3.91	55.85	4.15	55.83	4.39	55.81	4.64	56
	56.86	3.98	56.84	4.22	56.82		56.80		57
	57.86	4.05 4.12	57.84	4.30	57.82	4.55	57.80		58
	58.86 59.85	4.12	58.84 59.84	4.37	58.82 59.82	4.63	58.80 59.79	4.89 4.97	59 60
61	60.85	4.26	60.83	4.52	60.81	4.79			61
	61.85	4.32	61.83	4.59	61.81	4.86			62
	62.85	4.39	62.83	4.67	62.81	4.94			63
	63.84 64.84	4.46	63.82 64.82	4.74	63.80 64.80		63.78 64.78		64 65
	65.84	4.60	65.82	4.89	65.80				66
	66.84	4.67	66.82	4.97	66.79	5.26	66.77	5.55	67
	67.83 68.83	4.74	67.81 68.81	5.04	67.79		67.77		68
	69.83		69.81	5.19	69.78				69 .70
	70.83	4.95	70.80		70.78		70.76		71
	71.82	5.02	71.80		71.78		71.75		72
	72.82	5.09	72.80		72.77		72.75		73 74
	74.82	5.23	74.79	5.56	74.77		74.74		75
	75.81	5.30	75.79		75.77		75.74		76
	76.81	5.37	76.79		76.76	6.04			77
	77.81 78.81	5.44	77.79	5.78	77.76	6.12 6.20	77.75		78
	79.81	5.58			79.75		78.75		
81	80.80	5.65	80.78	6.00	80.75		80.72		81
82	81.80	5.72	61.78	6.08	81.75	6.43	81.72	6.79	82
	82.80 83.80		82.77	6.15 6.23	82.74 83.74		82.71		83 84
	84.79		84.77		84.74		84.71		85
86	85.79	6.00	85.76	6.37	85.73	6.75	85.70	.7.12	86
	86.79		86.76		86.73		86.70	7.20	87
	87.79 88.78		87.76		87.79		87.70		88
	89.78		89.75		89.72		89.69		90
91	90.78	6.35	90.75	6.74	90.72		90.69		
	91.78		91.75	6.82	91.72	7.22			92
	92.77 93.77		92.74 93.74		92.71 93.71		92.68		
	93.77		93.74				93.60		95
	95.77	6.70	95.74	7.11	95.70	7.53	95.6	7.95	96
	96.76		96.79		96.70		96.6		97
98	97.76 98.76	6.84	97.75 98.75	7.26	97.70 98.69		97.60		
	99.76		99.75	7.41					
st.	-	Lat.		_		Lat.		Lat.	st.
Ä	86	Deg.	853	Deg.	851	Deg.	854	Deg.	Ā

D	5 D	eg.	51 I)eg.	5 <u>1</u> 1	Deg.	53	Deg.	0
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1	1.00	0.09	1.00	0.09	1.00	0.10	0.99	0.10	_ 1
23	1.99	0.17	1.99	0.18	1.99	0.19	1.99	0.20	Se on
	2.99	0.26	2.99	0.27	2.99	0.29	2.98	0.30	
45	3.98	0.35	3.98	0.37	3.98	0.38	3.98		4
6	5.98	0.52	5.97	0.55	5.97	0.40	5.97	0.60	
7	6.97	0.61	6.97	0.64	6.97	0.67	6.96		
8	7.97	0.70	7.97	0.73	7.96	0.76	7.96		, (
9	.8.97	0.78	8.96	0.82	8.96	0.86	8.95		
10	9.96	10.87	.9.96	0.92	.9.95	0.96	9.95	1.00	10
	10.96	.0.96	10.95		10.95	1.05	10.94		1
	11.95	1.05	11.95		11.94	1.15	11.94		
	$12.95 \\ 13.95$	1.15	12.95 13.94	1.19	12.94 13.94	$1.25 \\ 1.34$	12.93		1:
	14.94	1.31	14.94	1.37	14.93		14.92		i
			15.93	1.46	15.93	1.53	15.92		i
	16.94	1.48	16.93		16.92		16.91		1
	17.93	1.57	17.92	1.65	17.92	1.73	17.91		
	18.93	1.66		1.74	18.91	1.82	18.90		
20	19.92	1.74	19.92	1.83	19.91	.1.92	19.90	2.00	2
	20.92	1.83	20.91	1.92	20.90	2.01	20.88		
	21.92	1.92	21.91	2.01	21.90	2.11	21.89		
23	22.91 23.91	2.00	22.90	2.10	22.89 23.89		22.88		
	23.91	2.09 2.18	23.90 24.90	2.20	24.88		24.87		
	25.90	2.27	25.89	2.38	25.88		25.8		
	26.90	2.35	26.89	2.47	26.88		26.86		
	27.89	2.44		2.56	27.87		27.86		
	28.89	2.53	28.88	2.65	28.87		28.8		
30	29.89	.2.61	29.87	2.75	29.86	.2.88	29.8	3.01	3
	30.88		30.87	2.84			30.84		
	31.88	2.79	31.87		31.85		31.84		
	32.87		32.86		32.85		32.8		
	33.87 34.87	2.96	33.86 34.85	3.11	33.84 34.84				
	35.86		35.85	3.29	35.89		35.8		
	36.86		36.84	3.39	36.83		36.8		
38	37.86	3.31	37.84	3.48	37.83	3.64	37.8	3.81	3
	38.85		38.84	3.57			38.80		
40	39.85	3.49	39.83	3.66	39.82	3.83	39.80	4.01	4
	40.84		40.83	3.75	40.81		40.79	4.11	
	41.84				41.81		41.79		
	42.84			3.93	42.80		42.78		
	43.83			4:12	44.79		43.70	4.41 4.51	
	45.82			4.21			45.77		
	46.82			4:30	46.78	4.50	46.76	4.71	
	47.82			.4.39		.4.60	47.76		
	48.81			4.48			48.78	5.4.91	4
50	49.81	4.36	49.79	.4.58	49.77	4.79	49.75	5.01	.5
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	St.
-		-	843	-	10.4.	0		-	1.5

-	ET	lam I	151D	an I	151	Dog	531	Dog	
Di	5 L	reg.	$5\frac{1}{4}D$	eg.	01	Deg.	$5\frac{3}{4}$	Deg.	Di
st.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	st.
51	50.81	4.44	50.79	4.67	50.77	4.89	50.74	5.11	51
	51.80 52.80	4.53 4.62	51.78 52.78	4.76 4.85	51.76 52.76	4.98	51.74 52.73	5.21 5.31	52 53
	53.79	4.71	53.77	4.94	53.75	5.18	53.73	5.41	54
55	54.79	4.79	54.77	5.03	54.75	5.27	54.72	5.51	55
	55.79 56.78	4.88	55.77 56.76	5.12 5.22	55.74 56.74	5.37 5.46	55.72 56.71	5.61 5.71	56 57
	57.78	5.06	57.76	5.31	57.73	5.56	57.71	5.81	58
59	58.78	5.14	58.75	5.40	58.73	5.65	58.70	5,91	59
60 	59.77	5.23	59.75	5.49	59.72	5.75	59.70	6.01	60
	60.77	5.32	60.74	5.58	60.72	5.85	60.69	6.11	61
63	$61.76 \\ 62.76$	5.40 5.49	61.74 62.74	5.67 5.76	61.71 62.71	5.94 6.04	61.69 62.68	6.21 6.31	62 63
64	63.76	5.58	63.73	5.86	63.71	6.13	63.68	6.41	64
	64.75	5.67	64.73	5.95	64.70	6.23	64.67	6.51	65
	65.75 66.75	$5.75 \\ 5.84$	65.72 66.72	6.04 6.13	65.70 66.69	6.33 6.42	65.67 66.66	6.61 6.71	66 67
68	67.74	5.93	67.71	6.22	67.69	6.52	67.66	6.81	68
	68.74	6.01	68.71	6.31	68.68	6.61	68.65	6.91	69
	69.73	6.10	69.71	6.41	69.68	6.71	69.65	7.01	70
	70.73 71.73	6.19	70.70 71.70	6.50 6.59	70.67	6.81	70.64	7.11	·71 72
	72.72	6.28 6.36	72.69	6.68	72.66	7.00	72.63	7.21	73
74	73.72	6.45	73.69	6.77	73.66	7.09	73.63	7.41	7.4
	74.71	6.54	74.69	6.86	74.65	7.19	74.62		75
	75.71 76.74	6.62	75.68 76.68	6.95 7.05	75.65	7.28	75.62	7.61 7.71	76 77
78	77.70		77.67	7.14	77.64	7.48	77.61	7.81	78
	78.70		78.67	7.23	78.64	7.57	78.60		79
	79.70	6.97	79.66	7.32	79.63	7.67	79.60	8.02	80
	80.69	7.06	80.66	7.41	80.63	7.76	80.59	8.12	81
	81.69 82.68	7.15	81.66 82.65	7.50 7.59	81.62 82.62	7.86	81.59 82.58	8.22 8.32	82 83
84	83.68	7.32	83.65	7.69	83.61	8.05	83.58	8.42	84
	84.68		84.64	7.78	84.61	8.15	84.57	8.52	85
	85.67	7.50	85.64 86.64	7.87	85.60 86.60	8.24 8.34	85.57	8.62 8.72	86
88	87.67	7.67	87.63	8.05	87.59	8.43	87.56	8.82	88
	88.66	7.76	88.63	8.14	88.59	8.53	88.55	8.92	89
	89.66	7.84	89.62	8.24	89.59	8.63	89.55	9.02	90
91		7.93	90.62	8.33	90.58	8.72	90.54		91
	91.65 92.65	8.02	91.61 92.61	8.42 8.51	91.58 92.57	8.82	91.54 92.53	9.22 9.32	92 93
94	93.64	8.19	93.61	8.60	93.57	9.01	93.53	9.32	94
95	94.64	8.28	94.60	8.69	94.56	9.11	94.52	9.52	95
	95.63 96.63	8.37	95.60 96.59	8.78	95.56 96.55	9.20	95.52 96.51	9.62 9.72	96 97
98	97.63	8.54	97.59	8.97	97.55	9.39	97.51	9.82	98
	98.62	8.63	98.59	9.06	98.54		98.50	9.92	99
	99.62	8.72		9.15	99.54			10.02	100
ist.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
1	85	Deg.	843	Deg.	841	Deg.	841	Deg.	D
					2	3	1+	- 8.	
					-				

TRAVERSE TABLE.

D	6 D	eg.	$6\frac{1}{4}$]	Deg.	6 <u>1</u>	eg.	63	Deg.	B
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1 2	0.99	0.10 0.21	0.99	0.11 0.22	0.99	0.11 0.23	0.99	0.12	1 2
3	2.98	0.31	2.98	0.33	2.98	0.34	2.98	0.35	3
45	3.98 4.97	$0.41 \\ 0.52$	3.98	0.44 0.54	3.97	0.45	3.97	0.47	4
6	5.97	0.63	5.96	0.65	5.96	0.68	5.96	0.59	6
78	6.96 7.96	0.73	6.96 7.95	0.76	6.96 7.95	0.79	6.95 7.94	0.82	7
9	8.95	0.94	8.95	0.98	8.94	1.02	8.94	1.06	9
10	9.95	1.05	9.94	1.09	9.94	1.13	9.93	-1.18	10
	10.94	1.15	10.93		10.93	1.25	10.92	1.29	11
	11.93 12.93	1.25	11.93 12.92	$1.31 \\ 1.42$	$11.92 \\ 12.92$	1.36	11.92 12.91	1.41 1.53	12 13
14	13.92	1.46	13.92	1.52	13.91	1.59	13.90	1.65	14
	14.92 15.91	1.57	14.91 15.90	1.63	14.90 15.90	1.70	$14.90 \\ 15.89$	1.76	15 16
17	16.91	1.78	16.90	1.85	16.89	1.92	16.88	2.00	17
	17.90 18.90	1.88	17.89 18.89	1.96 2.07	$17.88 \\ 18.88$	2.04 2.15	17.88 18.87	2.12	18 19
	19.89	2.09	19.88	2.18	19.87	,2.26	19.86	2.35	20
	20.88	2.20	20.88	2.29	20.87	2.38	20.85	2.47	21
	$21.88 \\ 22.87$	$2.30 \\ 2.40$	21.87 22.86	$2.40 \\ 2.50$	21.86 22.85	2.49 2.60	$21.85 \\ 22.84$	2.59 2.70	22 23
24	23.87	2.40	23.86	2.61	23.85	2.72	23.83	2.10	24
	24.86 25.86	2.61 2.72	24.85 25.85	2:72	24.84 25.83	2.83 2.94	24.83 25.82	2.94 3.06	25 26
	26.85	2.82	26.84	2.94	26.83	2.94	25.82	3.00	20
28	27.85 28.84	2.93	27.83 28.83	3.05 3.16	27.82 28.81	3.17 3.28	27.81	3.29	28 29
	29.84	3.03 3.14	29.82	3.27	29.81	3.40	28.80 29.79	3.41 3.53	30
	30.83	3.24	30.82	3.37	30.80	3.51	30.79	3.64	31
	31.82 32.82	3.34 3.45	$31.81 \\ 32.80$	3.48 3.59	31.79 32.79	$3.62 \\ 3.74$	31.78 32.77	3.76	32 33
34	33.81	3.45	33.80	3.70	33.78	3.85	33.76	4.00	34
	34.81 35.80	3.66 3.76	34.79 35.79	3.81 3.92	34.78 35.77	3.96 4.08	34.76	4.11 4.23	35 36
37	36.80	3.10	36.78	4.03	36.76	4.19	35.75 36.75	4.25	37
	37.79 38.79	3.97	37.77 38.77	4.14 4.25	37.76 38.75	4.30	37.74 38.73	4.47	38 39
	39.78	4.08 4.18	39.76	4.25	39.74	4.41 4.53	39.72	4.50	40
	40.78	4.29	40.76	4.46	40.74	4.64	40.72	4.82	41
42 43	41.77 42.76	4.39	41.75 42.74	4.57	41.73 42.72	4.76 4.87	41.71 42.70	4.94	43 43
44	43.76	4.60	43.74	4.79	43.72	4.98	43.70	5.17	41
45 46	44.75 45.75	4.70 4.81	44.73 45.73	4.90 5.01	44.71 45.70	5.09 5.21	44.69 45.68	5.29 5.41	45 46
47	46.74	4.91	46.72	5.12	46.70	5.32	46.67	5.52	47
48	47.74 48.73	5.02 5.12	47.71 48.71	5.23 5.34	47.69 48.69	5.43 5.55	47.67 48.66	5.64	48 49
	49.73	5.23	49.70	5.44	49.68	5.66	49.65	5.88	50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
ā	84 1	Deg.	833	Deg.	831	Deg.	831	Deg.	â

1	6 [leg.	61	Deg.	6 1	Deg.	63]	Deg.	
Dis									Dist.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.72	5.33		5.55	50.67	5.77	50.65	5.99	51
	51.72	5.44	51.69	5.66	51.67	5.89	51.64	6.11	52
	52.71 53.70	5.54	52.68	5.77	52.66 53.65	6.00	52.63 53.63	6.35	53 54
	54.70	5.75	54.67	5.99	54.65	6.23	54.62	6.46	55
	55.69	5.85	55.67	.6.10	55.64		55.61	6.58	56
	56.69	5.96	56.66	6.21	56.63	6.45	56.60	6.70	57
	57.68 58.68	6.06 6.17	57.66	6.31 6.42	57.63 58.62		57.60 58.59	6.82 6.93	58 59
	59.67	6.27	59.64	6.53	59.61	6.79	59.58		60
61	60.67	6.38	60.64	6.64	60.61	6.91	60.58	7.17	61
62	61.66	6.48	61.63	6.75	61.60	7.02	61.57	7.29	62
	62.65	6.59	62.63		62.60		62.56	7.40	
	63.65 64.64	6.69 6.79	63.62 64.61	6.97 7.08	63.59 64.58		63.56 64.55	7.52	64
	65.64	6.90	65.61	7.19	65.58		65.54	7.76	66
67	66.63	7.00	66.60	7.29	66.57	7.58	66.54	7.88	67
	67.63	7.11	67.60	7.40	67.56		67.53	\$7.99	
	68.62 69.62	7.21 7.32	68.59 69.58	7.51 7.62	68.56 69.55	7.81	68.52 69.51	8.11 8.23	69 70
71	70.61	7.42	70.58	7.73	70.54	8.04	70.51	8.35	71
	71.61	7.53	71.57	7.84	71.54	8.15	71.50	8.46	72
	72.60	7.63	72.57	7.95	72.53	8.26	72.49	8.58	
	73.59 74.59	7.74	73.56	8.06	73.52	8.38	73.49	8.70	
	75.58	7.94	74.55	8.17 8.27	74.52	8.49 8.60	74.48	8.82	76
	76.58	8.05	76.54		76.51	8:72	76.47	9.05	77
	77.57	8.15	77.54		77.50		77.46		78
	78.57	8.26 8.36	78.53	8.60 8.71	78.49	8.94 9.06	78.45		79 80
81	80.56	8.47	80.52	8.82	80.48		80.44	9.52	81
	81.55	8.57	81.51	8.93	81.47		81.43		
83	82.55	8.68	82.51	9.04	82.47	9.40	82.42	9.76	83
	83.54	8.78	83.50				83.42	9.87	84
	84.53 85.53	8.88	84.50 85.49		84.45 85.45		84.41	9.99	85 86
	86.52	9.09	86.48		86.44	9.74	86.40		87
88	87.52	9.20	87.48	9.58	87.43	9.96	87.39		88
	88.51	9.30	88.47	9.69	88.43			10.46	89
90	89.51	9.41	89.47	9.80	89.42	10.19	89.38	10.58	90
	90.50 91.50	9.51 9.62	90.46 91.45		90.42		90.37		
	92.49	9.72	92.45		92.40	$10.41 \\ 10.53$	91.36	10.81	92 93
94	93.49	9.83	93.44	10.23	93.40	10.64		11.05	94
	94.48	9.93		10.34	94.39	10.75	94.34	11.17	95
	95.47 96.47	10.03 10.14		10.45 10.56	95.38 96.38	10.87	95.33	11.28	.96
	97.46			10.67	97.37		96.33	$11.40 \\ 11.52$	97 -98
99	98.46	10.35	98.41	10.78	98.36	11.21	98:31	11.64	99
100	99.45	10.45	99.41	10.89	99.36	11.32		11.75	100
ist.	Dep.	Lat.	Dep.	Lat.	Dép.	Lat.	Dep.	Lat.	st.
P	84	Deg.	834	Deg.	$83\frac{1}{2}$	Deg.	83:1	Deg.	ā

TRAVERSE TABLE.

E	71)eg.	71	Deg.	$7\frac{1}{2}$	Deg.	73	Deg.	H
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
12	0.99	0.12 0.24	0.99	0.13	0.99	0.13	0.99	0.13	1
3 4	2.98	0.37	2.98	0.38	2.97	0.39	2.97	0.40	34
56	4.96 5.96	0.61 0.73	4.96	0.63	4.96	0.65	4.95	0.54	5
78	6.95 7.94	0.85	6.94 7.94	0.88	6.94	0.91	6.94	0.81	7
9 10	8.93	1.10	8.93	1.14	8.92 9.91	1.04 1.17 1.31	7.93 8.92 9.91	1.08 1.21 1.35	8 9 10
11	10.92	1.34	10.91	1.39	10.91	1.44	10.90	1.48	11
	11.91 12.90	1.46	11.90 12.90	1.51	11.90 12.89	1.57	11.89 12.88	1.62 1.75	12 13
	13.90 14.89	$1.71 \\ 1.83$	13.89	1.77	13.88 14.87	1.83 1.96	13.87 14.86	1.89	14 15
16	15.88 16.87	1.95 2.07	15.87 16.86	$2.02 \\ 2.15$	15.86 16.85	2.09	15.85	2.16	16 -17
18	17.87 18.86	2.19	17.86	2.27 2.40	17.85	2.35	17.84	2.43	18
	19.85	2.44	19.84	2.52	18.84 19.83	2.48 2.61	18.83 19.82	2.56 2.70	19 20
	$20.84 \\ 21.84$	2.56	20.83 21.82	2.65 2.78	20.82 21.81	2.74 2.87	20.81 21.80	2.83 2.97	21 22
23	22.83 23.82	2.80	22.82 23.81	2.90 3.03	22.80 23.79	3.00 3.13	22.79 23.78	3.10	23 24
25	24.81 25.81	3.05 3.17	24.80 25.79	$3.15 \\ 3.28$	24.79	3.26	24.77	3.37	25 26
.27	26.80	3.29	26.78	3.41	25.78 26.77	3.39 3.52	25.76 26.75	3.51 3.64	27
29	27.79 28.78 29.78	3.41 3.53 3.66	28.77 29.76	3.53 3.66 3.79	27.76 28.75 29.74	3.65 3.79 3.92	27.74 28.74 29.73	3.78 3.91 4.05	28 29 30
-	30.77	3.78	30.75	3.91	30.73	4.05	30.72	4.18	31
32	$31.76 \\ 32.75$	3.90 4.02	31.74 32.74	4.04 4.16	31.73 32.72	4.18	$31.71 \\ 32.70$	4.32	32 33
34	33.75 34.74	4.14 4.27	33.73 34.72	4.29	33.71 34.70	4.44	33.69	4.58	34 35
36	35.73	4.39	35.71 36.70	4.54	35.69	4.57	34.68 35.67	4.72	36
38	36.72 37.72	4.51	37.70	4.67	36.68	4.83	36.66 37.65	4.99 5.12	38
	38.71 39.70	4.75	38.69 39.68	4.92 5.05	38.67 39.66	$5.09 \\ 5.22$	38.64 39.63	$5.26 \\ 5.39$	39 40
	40.70	5.00 5.12	40.67	5.17 5.30	40.65	5.35 5.48	40.63 41.62	5.53 5.66	41 42
43	42.68	5.24	42.66	$5.43 \\ 5.55$	42.63	5.61	42.61	5.80	43 44
45	44.67	5.48	44.64	5.68	44.62	5.74	43.60 44.59	5.93	45
47	45.66 46.65	$5.61 \\ 5.73$	45.63 46.62	5.81	$45.61 \\ 46.60$	6.00 6.13	45.58 46.57	$6.20 \\ 6.34$	46 47
49	47.64	5.85 5.97	47.62	6.06	47.59	$6.27 \\ 6.40$	47.56 48.55	6.47 6.61	48 49
-	49.63	6.09	49.60	6.31	49.57	6.53	49.54	6.74	50
Dist.	Dep.	Lat.	Dep.		Dep.			Lat.	list.
9	83 I	Deg.	82 ³ ₄ I	Deg.	$82\frac{1}{2}I$	Deg.	82 <u>1</u> I	Deg.	91

D	7 D	eg.	71	Deg.	$7\frac{1}{2}$]	Deg.	73	Deg.	D
st.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	st.
	50.62	6.22	50.59	6.44	50.56	6.66	50.53	6.88	51
	51.61 52.60	6.34	51.58 52.58	6.56	51.56	6.79	51.53 52.52		52 53
	53.60	6.58	53.57	6.81	52.55 53.54	6.92	53.51		54
	54.59	6.70	54.56	6.94	54.53	7.18	54.50		
56	55.58	6.82	55.55	7.07	55.52	7.31		7.55	56
	56.58	6.95	56.54	7.19	56.51	7.44			
	57.57 58.56	7.07	$57.54 \\ 58.53$	7.32 7.45	57.50 58.50	7.57	57.47 58.46		
	59.55	7.31	59.52	7.57	59.49	7.83			
	60.55	7.43	60.51	7.70	60.48	7.96	60.44	8.23	61
62	61.54	7.56	61.50	7.82	61.47	8.09	61.43		
63	62.53 63.52	7.68	62.50	7.95	62.46	8.22	62.42		
	64.52	7.80	63.49 64.48	8.08	63.45 64.44	8.35 8.48	63.42 64.41		
66	65.51	8.04	65.47	8.33	65.44	8.61	65.40		
67	66.50	8.17	66.46	8.46	66.43	8.75	66.39		
	67.49	8.29	67.46	8.58	67.42	8.88	67.38		
	68.49 69.48	8.41 8.53	68.45 69.44	8.71 8.83	68.41 69.40	9.01 9.14	68.37 69.36		
71	70.47	8.65	70.43	8.96	70.39	9.27	70.35	9.57	71
	71.46	8.77	71.42	9.09	71.38	9.40	71.34		
	72.46	8.90	72.42	9.21	72.38	9.53	72.33	9.84	73
	73.45	9.02	73.41	9.34	73.37	9.66	73.32		
	74.44 75.43	9.14 9.26	74.40	9.46 9.59	74.36	9.79 9.92		10.11	75
	76.43	9.38	76.38	9.72		10.05		10.23	
78	77.42	9.51	77.38	9.84		10.18		10.52	
	78.41 79.40	9.63 9.75	78.37	9.97 10.10		10.31 10.44		10.65	
	80.40	0.07							
	81.39	9.87		$10.22 \\ 10.35$		$10.57 \\ 10.70$		10.92	
	82.38	10.12	82.34			10.83		11.19	
	83.37	10.24		10.60		10.96	83.23	11.33	84
	84.37	10.36 10.48	84.32	10.73		11.09			
87	86.35	10.48		10.85 10.98		11.23 11.36		11.60	
88	87.34	10.72		11.11	87.25	11.49		11.87	1 2 2
89	88.34	10.85		11.23		11.62		12.00	
90	89.33	10.97	89.28	11.36	89.23	11.75	89.18	12.14	90
		11.09			90.22		90.17	12.27	91
		11.21		11.61		12.01		12.41	
		11.33 11.46		11.74	92.20 93.20			12.54 12.68	
95	94.29	11.58		11.99		12.40		12.00	
96	95.28	11.70	95.23	12.12	95.18	12.53	95.12	12.95	96
		11.82		12.24	96.17		96.11	13.08	97
99	98.26	11.94 12.07	97.22	12.37	97.16 98.15	12:79	97.10	13.22 13.35	98 99
		12.19	99.20	12.62	99.14	13.05	99.09	13.49	100
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
Di	83	Deg.	823	Deg.	821	Deg	821	Deg.	Dis

TRAVERSE TABLE.

U	81)eg.	81	Deg.	81	Deg.	83	Deg.	E
ist.	Lat.	Dep.	·Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
12	0.99	0.14 0.28	0.99	0.14	0.99	0.15	0.99	0.15 0.30	12
3	2.97	0.42	2.97	0.43	2.97	0.44	2.97	0.46	3
45	3.96	0.56	3.96	0.57 0.72	3.96	0.59	3.95	0.61	45
6	5.94	0.84	5.94	0.86	5.93	0.89	5.93		6
78	6.93 7.92	0.97	6.93	1.00	6.92	1.03	6.92		8
9	8.91	1.25	8.91	1.15	7.91 8.90	1.18	7.91 8.90	1.22	9
10	9.90	1.39	9.90	1.43		1.48	9.88	1.52	10
	10.89 11.88	1.53	10.89	1.58	10.88 11.87	1.63		1.67	11
	12.87	1.81	12.87	1.87	12.86	1.77 1.92	11.86	1.83	13
	13.86	1.95	13.86	2.01	13.85	2.07	13.84	2.13	14
	14.85 15.84	2.09 2.23	14:85	2.15	14.84 15.82	2.22 2.36	14.83	2.28	15 16
17.	16.83	2.37	16.83	2.44	16.81	2.51	16.80	2.59	17
	17.82 18.82	$2.51 \\ 2.64$	17.81 18.80	2.58 2.73	17.80 18.79	2.66	17.79 18.78	2.74	18 19
	19.81	2.78	19.79	2.87	19.78	2.96	19.77	3.04	20
	20.80	2.92	20.78	3.01	20.77	3.10	20.76	3.19	21
	21.79 22.78	3.06 3.20	21.77 22.76	3.16 3.30	21.76	3.25 3.40	21.74 22.73	3.35	22 23
24	23.77	3.34	23.75	3.44	22.75 23.74	3.55	23.72	3.65	24
	24.76 25.75	3.48 3.62	24.74 25.73	3.59	24.73	3.70	24.71	3.80	25 26
	26.74	3.76	26.72	3.73	25.71 26.70	3.84 3.99	25.70 26.69	3.96	27
	27.73	3.90	27.71	4.02	27.69	4.14	27.67	4.26	28
	28.72 29.71	4.04 4.18	28.70 29.69	4.16 4.30	28.68 29.67	4.29 4.43	28.66 29.65	4.41 4.56	29 30
31	30.70	4.31	30.68	4.45	30.66	4.58	30.64	4.72	31
	31.69	4.45	31.67		31.65		31.63	4.87	32
	32.68 33.67	4.59 4.73	32.66 33.65		32.64 33.63	4.88	32.62 33.60	5.02	33 34
35	34.66	4.87	34.64	E 00'	91 60	5.17	34.59	5.32	35
	35.65	5.01	35.63	5.17	35.60	5.32	35.58	5.48	36
	36.64 37.63	5.15	36.62 37.61		36.59 37.58		36.57	5.63 5.78	37 38
	38.62	5.43	38.60	5.60	38.57	5.76	38.55		39
40	39.61	5.57	39.59	5.74	39.56	5.91	39.53	6.08	40
	40.60 41.59		40.58		40.55	6.06 6.21	40.52	6.24	41
	42.58		42.56		42.53	6.36	$41.51 \\ 42.50$	6.39 6.54	42 43
44	43.57	6.12	43.54	6.31	43.52	6.50	43.49	6.69	44
	44.56		44.53 45.52	6.46	44.51 45.49	6.65	44.48	6.85	45
	46.54		46.51		45.49		45.46	7.00	46 47
48	47.53	6.68	47.50	6.89	47.47	7.09	47.44	7.30	48
	48.52 49.51		48.49 49.48	7.03	48.46 49.45	7.24	48.43 49.42	7.45	49 50
	Dep.	Lat.	Dep.	;					
Dis	82 1	Deg.	813	Deg.	81 <u>+</u> 1	Deg.	81 <u>1</u>	Deg.	Dis

D	80	eg.	81 I	Deg.	81/1	Deg.	834	Deg.	D
st.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	st.
	50.50	7.10	50.47	7.32	50.44	7.54	50.41	7.76	51
	51.49	7.24	51.46	7.46	51.43	7.69	51.39	7.91	52
	52.48 53.47	7.38 7.52	52.45 53.44	7.61 7.75	52.42 53.41	7.83	52.38 53.37	8.06 8.21	53 54
	54.46	7.65	54.43	7.89	54.40	8.13	54.36	8.37	55
56	55.46	7.79	55.42	8.04	55.38	8.28	55.35	8.52	56
57	56.45	7.93	56.41	8.18	56.37	8.43	56.34	8.67	57
	57.44	8.07 8.21	57.40 58.39	8.32	57.36	8.57 8.72	57.32 58.31	8.82	58
	58.43 59.42	8.35	59.38	8.47 8.61	58.35 59.34	8.87	59.30	9.13	59 60
61	60,41	8.49	60.37	8.75	60.33	9.02	60.29	9.28	61
	61.40	8.63	61.36	8.90	61.32	9.16	61.28	9.43	62
63	62.39	8.77	62.35	9.04	62.31	9.31	62.27	9.58	63
	63.38	8.91	63.34	9.18	63.30	9.46	63.26	9.74	64
	64.37 65.36	9.05	64.33 65.32	9.33 9.47	64.29	9.61 9.76	64.24	9.89	65 66
	66.35	9.19 9.32	66.31	9.47	65.28 66.26	9.90			67
	67.34	9.46	67.30	9.76	67.25			10.34	68
69	68.33	9.60	68.29	9.90	68.24	10.20	68.20	10.50	69
70	69.32	9.74	69.28	10.04	69.23	10.35	69.19	10.65	70
71	70.31	9.88	70.27	10.19	70.22	10.49		10.80	71
	71.30			10.33		10.64		10.95	72
	72.29			10.47		10.79		11.10	73
	73.28 74.27	$10.30 \\ 10.44$	73.23		73.19 74.18	10.94		11.26	74 75
	75.26			10.91	75.17			11.56	76
	76.25			11.05	76.15			11.71	77
	77.24		77.19	11.19	77.14			11.87	78
	78.23			11.34		11.68		12.02	79
80	79.22	11.13	79.17	11.48	79.12	11.82	79.07	12.17	80
81	80.21	11.27	80.16	11.62	80.11	11.97		12.32	81
82	81.20	11.41	81.15	11.77	81.10	12.12	81.05	12.47	82
83	82.19	11.55	82.14			12.27		12.63	83
85	83.18	11.69		12.05		12.42		$12.78 \\ 12.93$	84 85
86	84.17 85,16	11.03	84.12	12.20 12.34	84.07	12.56		12.95	86
87	86.15	12.11	86.10			12.86		13.23	87
88	87.14	12.25	87.09	12.63	87.03	13.01	86.98	13.39	88
89	88.13	12.39	88.08		88.02	13.16		13.54	89
90	89.12	12.53	89,07	12.91	89.01	13.30	88.95	13.69	90
91	90.11	12.66		13.06	90.00	13.45	89.94	13.84	91
92	91.10	12.80	91.05	13.20	90.99	13.60	90.93	14.00	92
		12.94	92.04			13.75		14.15	93
	93.09		93.03		92.97			14.30	94 95
	94.08	13.22		13.63 13.78	93.96	14.04		14.45 14.60	96
		13.50				14.13		14.76	97
		13.64	96.99	14.06		14.49		14.91	98
99	98.04	13.78 13.92		14.21 14.35	97.91	14.63	97.85	15.06 15.21	99 100
-									
IS.	Dep.			Lat.				Lat.	2
A	82	Deg.	813]	Deg.	811	Deg.	814	Deg.	A

H	9 D	eg.	911	Deg.	$9\frac{1}{2}$	Deg.	93	Deg.	-
Dist		Dep.		Dep.		Dep.	- 47	Dep.	Dist.
-						Dep.			-
12	0.99	0.16 0.31	0.99	0.16 0.32	0.99	0.17	0.99		12
3	2.96	0.47	2.96	0.32	2.96	0.50	1.97 2.96	0.34	3
4	3.95	0.63	3.95	0.64	3.95	0.66	3.94	0.68	4
56	4.94 5.93	0.78 0.94	4.93	0.80	4.93 5.92	0.83	4.93		5
7	6.91	1.10	6.91	1.13	6.90	1.16	6.90		7
8	7.90	1.25	7.90	1.29	7.89	1.32	7.88	1.35	8
9 10	8.89 9.88	1.41 1.56	8.88	1.45	8.88	1.49	8.87 9.86		9 10
_									_
11	10.86	1.72	10.86	1.77	10.85	1.82	10.84		11
12	$11.85 \\ 12.84$	1.88 2.03	11.84 12.83	1.93	$11.84 \\ 12.82$	$1.98 \\ 2.15$	11.83		12 13
14	13.83	2.19	13.82	2.25	13.81	2.15	13.80		14
	14.82	2.35	14.80	2.41	14.79	2.48	14.78	2.54	15
	15.80 16.79	2.50 2.66	15.79	2.57	15.78 16.77	2.64	15.77		16
	17.78	2.82	17.77	2.89	17.75	2.97	17.74		18
19	18.77	2.97	18.75	3.05	18.74	3.14	18.73	3.22	19
20	19.75	3.13	19.74	3.21	19.73	3.30	19.71	3.39	20
21	20.74	3.29	20.73	3.38	20.71	3.47	20.70	3.56	21
22	21.73	3.44	21.71	3.54	21.70	3.63	21.68	3.73	22
	$22.72 \\ 23.70$	3.60 3.75	22.70 23.69	3.70 3.86	22.68 23.67	3.80 3.96	22.67		23 24
	24.69	3.91	24.67	4.02	24.66	4.13	24.64		25
26	25.68	4.07	25.66	4.18	25.64	4.29	25.62	4.40	26
27	26.67 27.66	4.22	26.65	4.34	26.63	4.46	26.61		27
	28.64	4.50	27.64 28.62	4.50	27.62 28.60	4.62	27.60 28.58		28 29
	29.63	4.69	29.61	4.82	29.59	4.95	29.57		30
01	30.62	1 01	20 00	4 00	30.57	= 10	30.55	EOF	91
	31.61	4.85 5.01	$30.60 \\ 31.58$	4.98	31.56	5.12 5.28	31.54		31 32
33	32.59	5.16	32.57	5.30	32.55	5.45	32.52	5.59	33
	33.58	5.32	33.56	5.47	33.53	5.61	33.51		34
	$34.57 \\ 35.56$	5.48 5.63	$34.54 \\ 35.53$	5.63	34.52 35.51	5.78 5.94	34.49		35 36
37	36.54	5.79	36.52	5.95	\$6.49	6:11	36.47	6.27	37
	37.53		37.51	6.11	37.48	6.27	37.45		38
	$38.52 \\ 39.51$	6.10 6.26	38.49 39.48	6.27 6.43	38.47 39.45	6.44 6.60	38.44 39.42		39 40
									-
	40.50	6.41	40.47	6.59	40.44	6.77	40.41		41
	41.48	6.57	41.45 42.44	6.75 6.91	41.42 42.41	6.92 7.10	41.39		42
44	43.46	6.88	43.43	7.07	43.40	7.26	43.36	7.45	44
	44.45	7.04	44.41	7.23	44.38	7.43	44.35		45
	$45.43 \\ 46.42$	7.20	$45.40 \\ 46.39$	7.39	45.37 46.36	7.59	$45.34 \\ 46.32$		46
48	47.41	7.51	47.38	7.72	47.34	7.92	47.31	8.13	48
	48.40	7.67	48.36	7.88	48.33	8.09	48.29	8.30	49
50	49.38	7.82	49.35	8.04	49.32	8.25	49.28	8.47	50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
ā	81	Deg.	803I	Deg.	801	Deg.	801]	Deg.	q

D	9 D)eg.	91	Deg.	912	Deg.	94	Deg.	D
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
	50.37		50.34		50.30	8.42	50.26	8.64	51
52 53	51.36 52.35	8.13	51.32 52.31	8.36 8.52	51.29 52.27	8.58 8.75	51.25 52.23	8.81	52 53
54	53.34	8.45	53.30	8.68	53.26	8.91	53.22	9.14	54
55 56	54.32 55.31	8.60	54.28 55.27	8.84	54.25	9.08 9.24	54.21	9.31 9.48	55 56
57	56.30		56.26	9.16	55.23 56.22	9.41	55.19 56.18	9.40	57
58	57.29		57.25	9.32	57.20	9.57	57.16	9.82	58
60	58.27 59.26		58.23 59.22		58.19 59.18	9.74 9.90	58.15 59.13	9.99 10.16	59 60
61		0.74		0.01	0.10	10.05			
62	60.25 61.24	9.54 9.70	60.21 61.19	9.81 9.97	$60.16 \\ 61.15$		60.12 61.10		61 62
63	62.22	9.86	62.18	10.13	62.14	10.40	62.09	10.67	63
64 65	63.21 64.20	10.01	63.17 64.15		63.12 64.11		63.08	10.84	64 65
66	65.19	10.32	65.14	10.61	65.09		$64.06 \\ 65.05$	11.18	66
67	66.18	10.48	66.13	10.77	66.08		66.03	11.35	67
69	67.16 68.15	10.64	67.12 68.10		67.07 68.05		67.02 68.00		68 69
70	69.14	10.95	69.09		69.04		68.99		70
71	70.13	<u>11 11</u>	70 08	11 41	70.03	11 70	60 97	19 09	71
72	71.11	11.26	70.08 71.06	11.57	71.01		69.97 70.96	12.19	72
73	72.10	11.42	72.05	11.73	72.00	12.05	71.95	12.36	73
75	73.09 74.08	11.58	73.04 74.02		72.99	12.21	72.93 73.92	12.53	74
76	75.06	11.89	75.01		74.96	12.50	74.90		75 76
77	76.05	12.05	76.00	12.38	75.94	12.71	75.89	13.04	77
78	77.04 78.03	12.20	76.99		76.93		76.87 77.86	13.21	78
	79.02		78.96		78.90		78.84	13.55	79 80
81	80.00	10 67	79.95	13 00	79.89	19 97	79.83	19 70	81
	80.99			13.18	80.88		80.82		-82
83	81.98	12.98	81.92	13.34	81.86	13.70	81.80	14.06	83
	82.97		82.91 83.89		82.85 83.83		82.79 83.77	14.23	84
			84.88		84.82		84.76	14.59	85 86
87	85.93	13.61	85.87	13.98	85.81	14.36	85.74	14.73	87
	86.92 87.90	13.77	86.86 87.84		86.79		86.73		88
	88.89				87.78 88.77		87.71 88.70	15.07	89 90
91	39.8 8	14 94	89.82	14 63	89.75	15 02	89.69	15 41	
	90.87		90.80		90.74		90.67	15.41	91 92
93	91.86	14.55	91.79	14.95	91.72	15.35	91.66	15.75	93
	92.84 93.83		92.78		92.71 93.70		92.64		94
		15.02	94.75	15.43	94.68		93.63 94.61	16.09	95 96
97	95.81	15.17	95.74	15.59	95.67	16.01	95.60	16.43	97
	96.79		96.73		96.66		96.58	16.60	98
			97:71 98.70		97.64 98.63	16.50	97.57 98.56	16.77	99 100
S			Dep.				Dep.	Lat.	st.
ā	81 1	Deg.	803	Deg.	801	Deg.	801	Dee	ā
-			4	-0.	12	-8.	4	-B.	-

D	10 L	eg.	101	Deg.	$10\frac{1}{2}$	Deg.	103	Deg.	D
ist.	Lat,	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist:
1	0.98	0.17		0.18		0.18	0.98	0.19	1
23	2.95	0.35 0.52	1.97	0.36		0.36 0.55	1.96	0.37	. 2
4	3.94	0.69	3,94	0.71	3,93	0.73	3.93	0.75	4
56	4.92 5.91	0.87	4.92 5.90	0.89	4.92	0.91	4.91 5.89	0.93	5
7	6.89	1.22	6.89	1.25	6.88	1.28	6.88	1.31	7
8 9	7.88	1.39	7.87	1.42	7.87	1.46	7.86	1.49	8
10	9.85	1.74	9.84	1.78	9.83	1.82	9.82	1.87	10
	10.83	1.91	10.82	1.96	10.82	2.00	10.81	2.05	11
	12.80	2.08	$11.81 \\ 12.79$	2.14 2.31	11.80 12.78	2.19 2.37	11.79 12.77	$2.24 \\ 2.42$	12 13
14	13.79	2.43	13.78	2.49	13.77	2.55	13.75	2.61	14
	$14.77 \\ 15.76$	2.60 2.78	14.76	2.67	14.75 15.73	2.73	14.74	$2.80 \\ 2.98$	15 16
17	16.74	2.95	15.74 16.73	3.03	16.72	3.10	$15.72 \\ 16.70$	3.17	17
	17.73 18.71	3.13 3.30	17.71 18.70	3.20 3.38	17.70 18.68	3.28 3.46	17.68 18.67	3.36 3.54	18 19
20	19.70	3.47	19.68	3.56	19.67	3.64	19.65	3.75	20
21	20.68	3.65	20.66	3.74	20.65	3.83	20.63	3.92	21
	21.67 22.65	3.82 3.99	21.65 22.63	3.91 4.09	21.63 22.61	4.01 4.19	21.61 22.60	4.10	22 23
24	23.64	4.17	23.62	.4.27	23.60	4.37	23.58	4.48	24
	24.62 25.61	4.34 4.51	24.60 25.59	4.45	$24.58 \\ 25.56$	4.56	24.56 25.54	4.66	25 26
27	26.59	4.69	26.57	4.80	26.55	4.92	26.53	5.04	27
28	27.07	4.86	27.55 28.54	4.98	27.53 28.51	5.10 5.28	27.51	5.22	28
	29.54	$5.04 \\ 5.21$	29.52	5.34	29.50	5.47	28.49 29.47	5.41 5.60	29 30
31	30.53	5.38	30.51	5.52	30.48	-5.65	30.46	5.78	31
32	$31.51 \\ 32.50$	5.56	31.49 32.47	5.69 5.87	31.46	5.83	31.44 32.42	5.97	32 33
	33.48	5.73 5.90	33.46	6.05	32.45 33.43	6.20	33.40	6.16 6.34	31
	34.47	6.08	34.44	6.23	34.41	6.38	34.39	6.53	35
30	35.45 36.44	6.25 6.42	35.43 36.41	6.41 6.58	35.40 36.38	6.56 6.74	35.37 36.35	6.71 6.90	36 37
38	37.42	6.60	37.39	6.76	37.36	6.92	37.33	7.09	38
	38.41 39.39	6.77 6.95	38.38 39.36	6.94 7.12	38.35 39.33	7.11 7.29	38.32 39.30	7.27 7.46	39 40
41	40.38	7.12	40.35	7.30	40.31	7.47	40.28	7.65	41
42	41.36	7.29	41.33	7.47	41.50	7.65	41.26	7.83	42
43	42.35 43.33	7.47	42.31 43.30	7.65	42.28 43.26	$7.84 \\ 8.02$	$42.25 \\ 43.23$	8.02 8.21	43 44
45	44.32	7.81	44.28	8.01	44.25	8.20	44.21	8.39	45
	45.30 46.29	7.99 8.16	45.27	8.19 8.36		8.38	45.19 46.18	8.58 8.77	46 47
48	47.27	8.34	47.23	8.54	47.20	8.75	47.16	8.95	48
49 50	48.26 49.24	8.51 8.68	48.22 49.20	8.72 8.90	48.18 49.16	8.93 9.11	48.14 49.12	9.14 9.33	49 50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Ďep.	Lat.	st.
Di	80 Deg.		79 <u>3</u>]	Deg.	$79\frac{1}{2}$	Deg.	$79\frac{1}{4}$	Deg.	ā

D	10 D	eg.	10 ¹ / ₄ I	Deg.	101	Deg.	103	Deg.	U
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	st.
	50.23	8.86	50.19	9.08	50.15	9.29	50.10		51
	51.21	9.03	51.17	9.25 9.43	51.13	9.48	51.09 52.07	9.70 9.89	52 53
	$52.19 \\ 53.18$	9.20 9.38	53.14	9.45	52.11 53.10	9.66 9.84		10.07	54
	54.16	9.55	54.12	9.79	54.08		54.03	10.26	55
56	55.15	9.72	55.11	9.96	55.06			10.45	56
	56.13	9.90	56.09 57.07		56.05 57.03			10.63	57 58
59	57.12 58.10	10.07	58.06			10.57		11.00	59
	59.09		59.04			10.93		11.19	60
	60.07		60.03		59.98			11.38	61
62	$61.06 \\ 62.04$	10.77	61.01 61.99			$11.30 \\ 11.48$		11.56	62 63
	63.03		62.98			11.40		11.94	64
65	64.01	11.29	63.96	11.57	63.91	11.85	63.86	12.12	65
	65.00		64.95			12.03		12.31	66 67
	65.98 66.97		65.93 66.91			12.21 12.39		12.50	68
	67.95		67.90			12.57	67.79	12.87	69
	68.94		68.88			12.76		13.06	70
71	69.92	12.33	69.87	12.63	69.81	12.94	69.75	13.24	71
72	70.91	12.50	70.85		70.79	13.12	70.74	13.43	72
	71.89		71.83		71.78	13.30	71.72	13.62	73
	72.88 73.86		72.82		72.76	13.49		13.80	74 75
	74.85			13.52		13.85		14.18	76
77	75.83	13.37		13.70	75.71	14.03	75.65	14.36	77
	76.82			13.88		14.21		14.55	78
	77.80 78.78			14.06 14.24		$14.40 \\ 14.58$		14.74 14.92	
81	79.77	14.07	79.71	14.41	79.64	14.76	79.58	15.11	81
		14.24	80.69	14.59		14.94	80.56		
		14.41	81.68			15.13		15.48	83
	82.72 83.71		82.66			15.31	83.5	15.67	84 85
86	84.69	14.93	84.63	15.30	84.56	15.67	84.49		
	85.68			15.48		15.85		16.23	
	86.66 87.65	15.28	86.60	15.66	86.53	16.04 16.22	87.44	16.41	88 89
	88.63		88.56			16.40	88.42	16.79	
91	89.62	15.80	89.55		89.48	16.58	89.40	16.97	91
	90.60		90.53			16.77		17.16	
	91.59		91.52			16.95		17.35	93
	92.57 93.56	16.32	92.50 93.48			17.13	92.35 93.33		94 95
96	94.54	16.67	94.47	17.68	94.39	17.49	94.32	17.91	96
		16.84	95.45		95.38	17.68	95.30	18.09	97
		$17.02 \\ 17.19$	96.44 97.42			17.86 18.04		18.28	98 99
	98.48				98.33	18.22	98.25	18.47	99 100
t.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	t.
Dis	80 Deg. 793Deg.)eg.	7911)er	791	Der	Dis

U	11 1	Jeg.	111	Deg.	111	Deg.	113	Deg.	E
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1 2	0.98	0.19 0.38	0.98	0.20	0.98	0.20	0.98		12
ŝ	2.94	0.58	2.94	0.39	1.96 2.94	0.40	1.96 2.94	0.41 0.61	.3
4	3.93	0.76	3.92	0.78	3.92	0.80	3.92	0.82	4
· 5 6	4.91 5.89	0.95	4.90	0.98	4.90	1.00	4.90	1.02	56
7	6.87	1.34	6.87	1.37	6.86	1.40	6.85	1.43	.7
8 9	7.85	1.53 1.72	7.85	1.56	7.84	1.59	7.83	1.63	8
10	9.82	1.91	9.81	1.95	9.80	1.99	9.79		1
	10.80	2.10	10.79	2.15	10.78	2.19	10.77		
	11.78 12.76	2.29 2.48	11.77 12.75	$2.34 \\ 2.54$	11.76	2.39 2.59	11.75	2.44	
14	13.74	2.67	13.73	2.73	12.74 13.72	2.79	12.73 13.71	2.85	
	14.72	2.86	14.71	2.93	14.70	2.99	14.69	3.06	
16	$15.71 \\ 16.69$	3.05	15.69 16.67	3.12 3.32	15.68 16.66	3.19 3.39	15.66		
18	17.67	3.43	17.65	3.51	17.64	3.59	17.62		
	18.65	3.63	18.63	3.71	18.62	3.79	18.60		
20	19.63	3.82	13.62	3.90	19.60	3.99	19.58	4.07	20
21	20.61	4.01	20.60	4.10	20.58	4.19	20.56		
	21.60 22.58	4.20 4.39	21.58 22.56	4.29	21.56 22.54	4.39 4.59	21.54 22:56		
	23.56	4,58	23.54	4.68	23.52	4.78	23.50		
25	24.54	4.77	24.52	4.88	24.50	4.98	24.48	5.09	25
	25.52 26.50	4.96	25.50		25.48	5.18	25.46 26.43		
	20.50	5.15	26.48 27.46	5.27	26.46	5.38	27.41		
	28.47		28.44	5.66	28.42	5.78	28.39	5.91	, 29
30	29.45	5.72	29.42	5.85	29.40	5.98	29.37	6.11	30
	30.43		30,40		30.38	6.18	30.35		
	31.41 32.39	6.11 6.30	31.39 32.37	6.24 6.44	31.36	6.38 6.58	31.33	6.52	32
	33.38	6.49	33.35	6.63	33.32	6.78	33.29		
35	34.36	6.68	34.33	6.83	34.30	6.98	34.27	7.13	35
	35.34 36.32	6.87 7.06	35.31		35.28 36.26	7.18	35.25		
	37.30	7.25	36.29 37.27	7.22	30.20	7.58	37.20		
39	38.28	7.44	38.25	7.61	38.22	7.78	38.18	7.94	39
40	39.27	7.63	39.23	7.80	39.20	7.97	39.16	8.15	40
	40.25 41.23	7.82 8.01	40.21 41.19		40:18 41.16	8.17	40.14		
	41.23	8.20	42.17	8.39	42.14	8.57			10
44	43.19	8.40	43.15	8.58	43.12	8.77	43.08	8.96	44
	44.17	8.59	44.14	8.78	44.10	8.97	44.06		
	45.15 46.14	8.78	45.12 46.10		45.08 46.06	9.37	46.02		
48	47.12	9.16	47.08	9.36	47.04	9.57	46.99	9.78	48
	48.10 49.08		48.06		48.02 49.00	9.77 9.97	47.97		
-		Lat.					Dep.	· · ·	-
)ist									IS.
-	79	Deg.	783	Deg.	781	Deg.	784	Deg.	-

	11 Deg.		Reference - Andrews		pressonal.				-
	11 L)eg.	$11\frac{1}{4}I$	Deg.	$11\frac{1}{2}$	Deg.	113	Deg.	U
									Dist.
t.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	5
	50.06		50.02			10.17		10.39	51
	51.04		51.00			10.37	50.91	10.59	52
	52.03		51.98		51.94	10.57	51.89	10.79	53
54	53.01	10.30	52.96			10.77		11.00	54
55	53.99	10.49	53.94	10.73	53.90	10.97		11.20	55
56	54.97	10.69	54.92			11.16		11.40	56
	55.95		55.90			11.36		11.61	57
58	56.93	11.07	56.89			11.56	56.78	11.81	58
	57.92		57.87			11.76	57.76	12.01	59
60	58.90	11.45	58.85	11.71	58.80	11.96	58.74	12.22	60
61	50 00	11 64	E0 00	11 00	10 70	10 16	50 70	12.42	61
	59.88 60.86		59.83 60.81			12.16	60 70	12.63	62
	61.84		61.79			12.56		12.83	63
	62.82		62.77			12.76		13.03	64
	63.81		62.75			12.96	63.64	13.24	65
	64.79		64.73			13.16	64.62	13.44	66
67	65.77	12.78	65.71	13.07	65.66	13.36	65.60	13.64	67
68	65.77 66.75	12.98	66.69			13.56	66.58	13.85	68
69	67.73	13.17	67.67	13.46		13.76		14.05	69
70	68.71	13.36	68.60	13.66	68.59	13.96	68.53	14.25	70
	69.70		69.64			14.16	69.51	14.46	71
	70.68		70.62	14.05		14.35	70.49	14.66	72
	71.66		71.60			14.55		14.87	73
	72.64		72.58			14.75		15.07	74
	73.62 74.60		73.56			14.95		15.27	75 76
	75.59		74.54			15.15		15.68	77
	76.57			15.02		15.55		15.88	78
70	77.55	15.07	77.48		77 41	15.75		16.09	79
	78.53		78.46			15.95		16.29	80
_			10.40	10.01	10.00	10.00		10.20	
81	79.51	15.46	79.44	15.80	79.37	16.15	79.30	16.49	81
82	80.49	15.65		16.00		16.35		16.70	82
83	81.48	15.84	81.41	16.19		16.55	81.26	16.90	83
	82.46		82.39	16.39	82.31	16.75	82.24	17.11	84
	83.44			16.58		16.95	83.22	17.31	85
86	84.42	16.41	84.35	16.78	84.27	17.15	84.20	17.51	86
87	85.40	16.60	85.33			17 35	85.18	17.72	87
	86.38			17.17		3 17.54	86.16	17.92	88
	87.36			17.36	87.21	17.74			89
90	88.35	17.17	88.27	17.56	88.19	17.94	88.11	18.33	90
01	89.33	17 96	80 01	17.75	80.1	18,14	80 00	18 50	91
	90.31			17.95	90 1	18.14	90.05	18 74	92
	91.29			18.14	91 19	3 18.54	91 0	18 04	93
	92.27			18.34		18.74			
	93.25			18.53	93.09	18.94	93.01	19.35	
	94.24		94.16	18.73	94.07	18.94	93.99	19.55	96
97	95.22	18.51	95.14	18.92	95.05	19.34	94.97	19.75	97
98	96.20	18.70	96.12	19.12	96.05	3 19.54	95.95	19.96	98
		18.89	97.10	19.31	97.01	19.74	96.93	20.16	99
		19.08	98.08	19.51	97.99	19.94	.97.90	20.36	100
	-				-				
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	÷
0	mo	0	Dep.						3
2	1.7.9 1	Deg.	784	Deg.	781	Deg.	784	Deg.	

D	12 1)eg.	121	Deg.	$12\frac{1}{2}$	Deg.	1231	Deg.	H
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1	0.98	0.21	0.98	0.21	0.98	0.22	0.98	0.22	
23	1.96	0.42	1.95 2.93	0.42 0.64	1.95 2.93	0.43	1.95	0.44	3
4	3.91	0.83	3.91	0.85	3.91	0.87	3.90	0.88	4
56	4.89	1.04	4.89	1.06	4.88	1.08	4.88	1.10	
7	5.87	1.25	5.86	1.27	5.86	1.30	5.85	1.32	1 24
8	7.83	1.66	7.82	1.70	7.81	1.73	7.80	1.77	8
9 10	8.80 9.78	1.87 2.08	8.80 9.77	$1.91 \\ 2.12$	8.79 9.76	1.95 2.16	8.78 9.75	1.99	10
	10.76	2.29	10.75	2.33	10.74		10.73		
12	11.74 12.72	2.49 2.70	11.73 12.70	$2.55 \\ 2.76$	11.72 12.69	2.60	11.70 12.68		
14	13.69	2.91	13.68	2.97	13.67	3.03	13.65	3.09	14
	14.67	3.12	14.66	3.18	14.64	3.25	14.63		
17	15.65	3.53	15.64 16.61	3.61	15.62		15.61		
	17.61	3.74	17.59	3.82					
	18.58 19.56	3.95 4.16	18.57 19.54		18.55		18.53 19.51		
	20.54	4.37	20.52	4.46			20.48		
	21.52 22.50	4.57 4.78	21.50 22.48	4.67	21.48 22.45		21.46		
24	23.48	4.99	23.45	5.09	23.43	5.19	23.41	5.30) 24
	24.45 25.43		24.43	5.30	24.41		24.38		
	26.41		26.39	5.73	26.36	5.84	26.33		3 27
	27.39		27.36	5.94	27.34		27.31		
	28.37 29.34		28.34 29.32	6.15 6.37	28.31 29.29		28.28		
	30.32						30.24		
	31.30 32.28		31.27 32.25	6.79 7.00					
34	33.26	7.07	33.23	7.21	33.19	7.36	33.16	7.50	34
	34.24 35.21	7.28	34.20 35.18				34.14		
37	36.19	7.69	36.16	7.85	36.12	8.01	36.09	8.1	7 37
38	37.17 38.15	7.90 8.11	37.13 38.11						
	39.13		39.09		39.05				
	40.10		40.07		40.03		39.99		
	42.06		42.02		41.98		40.9		
44	43.04	9.15	43.00			9.52	42.9	2 9.7	1 44
	44.02		43.98		43.95				
47	45.97	9.77	45.99	9.97	45.89	10.17	45.8	1 10.3	7 47
48	46.95	5 9.98 3 10.19	46.91	10.18	46.80	6 10.39 1 10.61	46.8	2 10.5	9 48 1 49
		10.40							
st.	Dep	Lat.	Dep	Lat.	Dep	Lat.	Dep	Lat	st.
Ā	78	Deg.	773	Deg.	771/2	Deg.	77	Deg	ā

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0	12 I)eg.	$12\frac{1}{4}$	Deg.	$12\frac{1}{2}$	Deg.	$12\frac{3}{4}$	Deg.	E
ist	Tet	D	Tat	Dem	Tat	Den	Tet	Dam	ist
	Lat.	Dep.	Liat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	49.89	10.60	49.84	10.82	49.79	11.04	49.74	11.26	51
52	50.86		50.82	11.03		11.25		11.48	52
	51.84			11.25		11.47		11.70	53
	52.82 53,80		52.77	11.46		11.69		11.92	54 55
	54.78		54.72	11.88		12.12	54.62	12.36	56
.57	55.75	11.85	55.70	12.09	55.65	12.34	55.59	12.58	57
		12.06		12.31		12.55		12.80	58
	57.71 58.69			12.52 12.73		12.77		$13,02 \\ 13,24$	59 60
_		14.41		12.10	00.00	1.0.00		10,44	
61	59.67	12 68	59.61	12.94	59.55	13.20	59.50	13.46	61
		12.89		13.16	60.53	13.42	60.47	13.68	62
	61.62			13.37	61.51	13.64		13.90	63
	62.60 63.58			13.58 13.79	62.48 63.46			14.12 14.35	64 65
	64.56			14.00	64.44			14.57	66
67	65.54	13.93	65.47	14.22	65.41	14.50	65.35	14.79	67
		14.14		14.43		14.72		15.01	68
	67.49 68.47			$14.64 \\ 14.85$		14.93 15.15		$15.23 \\ 15.45$	69 .70
		14.00	00.31	14.00	00.04	10.10	00.41	13.40	
.71	69.45	14.76	69.38	15.06	69.32	15.37	69.25	15.67	71
	70.43		70.36	15.28	70.29		70.22		72
73	71.40	15.18	71.34	15.49	71.27	15.80		16.11	73
	72.38 73.36		73.29	15.70		$16.02 \\ 16.23$		16.33 16.55	74 75
	74.34		74.27	16.13		16,45	74.13	16.77	76
	75.32	16.01	75.25	16.34	75.17	16.67	75.10	16.99	77
		16.22	76.22	16.55		16.88		17.21	78
	77.27	16.43	78 18	16.76 16.97	77.13	17.10		17.44 17.66	79 80
-00	10.40	10.00		10.51	10.10	11.02	10.00	17.00	-00
81	79.23	16.84	79.16	17.19	79.08	17.53	79.00	17.88	81
	80.21		80.13	17.40	80.06	17.75		18.10	82
83	81.19	17.26		17.61	81.03	17.96	80.95	18.32	83
84	83.14	17.46	83.06	17.82 18.04		18.18 18.40		18.54	84 85
		17.88		18.25	83.96		83.88	18.98	86
87	85.10	18.09	85.02	18.46	84.94	18.83	84.85	19.20	87
		18.30		18.67		19.05		19.42	88
	87.06	18.50	86.97	18.88	86.89 87.87			19.64	89 90
		10.11		10.10		13.40	01.18	19.86	30
	89.01		88.93	19.31	88.84	19,70	88.76	20.08	91
	89.99	19.13	89.91	19.52	89.82	19.91	89.73	20.30	92
	90.97	19.34	90.88	19.73		20.13		20.52	93
	91.95 92.92	19.54 19.75	92.84	19.94	91.77 92.75			20.75 20.97	94 95
	93.90	19.96	93.81	20.37		20.78		21.19	96
97	94.88	20.17	94.79	20.58	94.70	20.99	94.61	21.41	97
98	95.86	20.38		20.79		21.21		21.63	38
	96.84 97.81	20.58 20.79	96.75	21.01 21.22	96.65	21.43 21.64		21.85 22.07	99 100
						-1.04			100
÷	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
)is									ist
	78]	Deg.	773	Deg.	771	Deg.	771	Deg.	9

E	13]	Deg.	134	Deg.	13 ¹ / ₂	Deg.	133	Deg.	D
ist.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1 2					0.97		0.97	0.24	12
3	2.92	0.67	2.92	0.69	2.92	0.70	2.91	0.71	3
45			3.89	0.92	3.89		3.89	0.95	
6	5.85		5.84	1.38		1.40	5.83	1.43	
78			6.81 7.79	1.60	6.81	1.63	6.80	1.66 1.90	
9		2.02	8.76	2.06	7.78	1.87	7.77	2.14	9
10		2.25	9.73	2.29	9.72	2.33	9.71	2.38	10
	10.72	2.47	10.71	$2.52 \\ 2.75$	10.70	2.57	10.68	2.61	11 12
13	11.69	2.10	11.68 12.65	2.15	11.67 12.64	2.80	11.66	3.09	12
	12.67 13.64	3.15	13.63	3.21	13.61	3.27	13.60	3.33	14
15	14.62	3.37	14.60 15.57	3.44	14.59	3.50 3.74	14.57	3.57	15 16
17	15.59 16.57	3.60 3.82	16.55	3.90	16.53	3.97	15.54 16.51	4.04	17
18	17.54	4.05	17.52	4.13	17.50	4.20	17.48	4.28	18
19 20	18.51 19.49	4.27	18.49 19.47	4.35 4.58	18.48	4.44	18.46 19.43	4.52 4.75	19 20
21	20.46	4.72	20.44	4.81	20.42	4.90	20.40	4.99	21
22	21.44	4.95	21.41	5.04	21.39	5.14	21.37	5.23	22
	$22.41 \\ 23.38$	5.17 5.40	22 39 23.36	$5.27 \\ 5.50$	22.36	$5.37 \\ 5.60$	22.34 23.31	5.47 5.70	23 24
	24.36	5.62	24.33	5.73	23.34	5.84	23.31	5.94	25
26	25.33	5.85	25.31	5.96	25.28	6.07	25.25	6.18	26
	26.31 27.28	6.07 6.30	26.28	6.19 6.42	26.25 27.23	6.30 6.54	26.23 27.20	6.42 6.66	27 28
	28.26	6.52	28.23	6.65	28.20	6.77	28.17	6.89	29
	29.23	6.75	29.20	6.88	29.17	7.00	29.14	7.13	30
	30.21	6.97	30.17	7.11	30.14	7.24	30.11	7.37	31
	31.18 32.15	7.20	31.15 32.12	7.33 7.56	$31.12 \\ 32.09$	7.47	31.08	7.61	32 33
	33.13	7.42	33.09	7.79	33.06	7.94	32.05 33.03	8.08	34
35	34.10	7.87	34.07	8.02	34.03	8.17	34.00	8:32	35
	35.08	8.10	35.04 36.02	$8.25 \\ 8.48$	35.01	8.40	34.97	8.56	36 37
	36.05 37.03	8.32	36.99	8.71	35.98 36.95	8.64	$35.94 \\ 36.91$	8.79 9.03	38
39	38.00	8.77	37.96	8.94	37.92	9.10	37.88	9.27	39
40	38.97	9.00	38.94	9.17	38.89	9.34	38.85	9.51	40
	39.95 40.92	9.22 9.45	39.91 40.88	9.40 9.63	39.87 40.84	9.57 9.80	39.83 40.80	9.75	41 42
	41.90	9.45	41.86	9.86	41.81		41.77		43
44	42.87	9.90	42.83	10.08	42.78	10.27	42.74	10.46	44
	43.85 44.82	10.12	43.80 44.78		43.76 44.73	10.51	43.71 44.68	10.70	45 46
	45.80		45.75		45.70		45.65		47
48	46.77	10.80	46.72		46.67	11.21	46.62	11.41	48
	47.74 48:72		47.70 48.67		47.65 48.62		47.60 48.57		49 50
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$\begin{array}{c c c c c c c c c c c c c c c c c c c $	51	49.69	11.47	49.64	11.69	49.59	11.91	49.54	12.12	51
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	52	50.67	11.70							
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$\begin{array}{c c c c c c c c c c c c c c c c c c c $				53.54	12.61	53.48	12.84	53.42	13.07	
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$\begin{array}{c c c c c c c c c c c c c c c c c c c $	58	56.51	13.05			56.40	13.54			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	59	57.49	13.27			57.37	13.77	57.31	14.02	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $										
$\begin{array}{c} 62 \ 60.41 \ [3.95 \ [60.35 \ [4.21 \ [60.29 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.22 \] 4.47 \ [60.2 \] 15.15 \] 64 \ [64.21 \] 15.21 \ [64 \] 65 \ 63.33 \] 4.42 \ [63.27 \] 14.90 \ [63.20 \] 15.17 \ [63.14 \] 15.45 \ [65 \] 66 \] 64.31 \] 14.85 \ [64.24 \] 15.15 \] 64 \ [64.11 \] 15.69 \ [66 \] 67 \] 65.20 \] 15.97 \ [66.05 \] 15.96 \] 66.12 \] 15.87 \ [66.05 \] 15.93 \] 67 \] 67 \] 66.25 \] 15.97 \ [66.25 \] 15.97 \] 66.12 \] 15.87 \] 66.05 \] 16.40 \] 69 \] 67.23 \] 15.52 \ [67.16 \] 15.52 \] 67.09 \] 16.11 \] 67.02 \] 16.40 \] 69 \] 67.23 \] 15.52 \] 67.16 \] 16.52 \] 69.04 \] 16.57 \] 68.97 \] 16.88 \] 71 \] 72 \ 70.15 \] 16.20 \] 70.06 \] 16.50 \] 70.01 \] 16.81 \] 69.94 \] 71.17 \] 72 \ 70.15 \] 16.20 \ [70.06 \] 16.50 \] 70.01 \] 16.81 \] 69.94 \] 17.17 \] 72 \] 72 \ 70.15 \] 16.20 \] 70.06 \] 16.50 \] 70.01 \] 16.81 \] 69.94 \] 17.17 \] 72 \] 72 \ 70.15 \] 16.87 \] 73.00 \] 17.19 \] 72.93 \] 17.50 \] 72.85 \] 17.59 \] 74 \] 72 \] 70 \] 16.87 \] 73.00 \] 17.19 \] 72.93 \] 17.50 \] 72.85 \] 17.50 \] 77 \] 72 \] 72 \] 75 \] 76 \] 74.72 \] 70.75 \] 75.97 \] 74 \] 72 \] 75 \] 76 \] 74.72 \] 75 \] 76 \] 74.72 \] 75 \] 76 \] 74.72 \] 75 \] 76 \] 74.72 \] 75 \] 76 \] 74 \] 75 \] 76 \] 75 \] 75 \] 76 \] 74 \] 75 \] 76 \] 75 \] 7$										-
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						60.29	14.47	60.22	14.74	62
$\begin{array}{c} 65\ 63.33\ 14.62\ 63.27\ 14.90\ 63.20\ 15.17\ 63.14\ 15.45\ 65\\ 66\ 4.31\ 14.85\ 64.24\ 15.13\ 64.18\ 15.41\ 64.11\ 15.69\ 66\\ 67\ 65.28\ 15.07\ 65.22\ 15.36\ 65.15\ 15.64\ 65.08\ 15.93\ 67\\ 68\ 66.26\ 15.50\ 66.19\ 15.59\ 66.19\ 15.87\ 66.05\ 16.16\ 68\\ 99\ 67.23\ 15.52\ 67.16\ 15.81\ 67.09\ 16.11\ 67.02\ 16.40\ 69\\ 99\ 67.23\ 15.52\ 67.16\ 15.81\ 67.09\ 16.11\ 67.02\ 16.40\ 69\\ 97\ 68.21\ 15.75\ 68.14\ 16.04\ 68.07\ 16.34\ 67.99\ 16.64\ 70\\ 71\ 69.18\ 15.97\ 69.11\ 16.27\ 69.04\ 16.57\ 68.97\ 16.88\ 71\\ 72\ 70.15\ 16.20\ 70.00\ 16.50\ 70.01\ 16.81\ 69.94\ 17.11\ 72\\ 73\ 71.13\ 16.42\ 71.06\ 16.73\ 70.96\ 17.28\ 71.88\ 17.99\ 74\ 72.00\ 16.57\ 72.05\ 17.88\ 17.97\ 72.83\ 17.88\ 17.97\ 72.83\ 17.88\ 17.97\ 72.83\ 17.88\ 17.97\ 72.83\ 17.86\ 17.97\ 72.83\ 17.86\ 17.97\ 72.83\ 17.86\ 17.97\ 72.85\ 17.88\ 17.97\ 76.90\ 18.11\ 76.8\ 18.21\ 75.76\ 18.54\ 18.20\ 77\ 75.03\ 17.22\ 78.54\ 18.27\ 17.87\ 77.1\ 19.01\ 80\ 77\ 75.03\ 17.22\ 78.54\ 18.27\ 77.71\ 19.01\ 80\ 77\ 75.63\ 18.57\ 18.34\ 77.77\ 18.88\ 77.71\ 19.01\ 80\ 77\ 77.50\ 18.57\ 18.34\ 77.77\ 18.88\ 77.71\ 19.01\ 80\ 77\ 77.50\ 18.57\ 18.34\ 77.77\ 18.88\ 77.71\ 19.01\ 80\ 77\ 77.50\ 18.57\ 78\ 75.84\ 18.27\ 75.76\ 18.54\ 18.77\ 77.71\ 19.01\ 80\ 77\ 77.8\ 18.34\ 77.77\ 18.88\ 77.71\ 19.01\ 80\ 77\ 77.8\ 18.78\ 77\ 77.1\ 19.57\ 84.68\ 19.94\ 84.60\ 20.31\ 84.51\ 15.90\ 83.54\ 20.20\ 83\ 85.74\ 20.44\ 85\ 83\ 80.71\ 19.57\ 84.68\ 19.94\ 84.60\ 20.31\ 84.51\ 89.99\ 85\ 85.74\ 19.90\ 85.52\ 82.9\ 19.12\ 82.74\ 19.48\ 84.51\ 19.90\ 85.52\ 82.9\ 19.12\ 82.74\ 19.48\ 84.50\ 19.48\ 84.50\ 18.51\ 89\ 90\ 87.68\ 20.20\ 85\ 85.74\ 20.20\ 85\ 85.74\ 20.20\ 85\ 85.74\ 20.20\ 85\ 85.74\ 20.20\ 85\ 85.74\ 20.20\ 85\ 85.74\ 20.20\ 85\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.5$						61.26	14.71	61.19	14.97	63
$\begin{array}{c} 65\ 63.33\ 14.62\ 63.27\ 14.90\ 63.20\ 15.17\ 63.14\ 15.45\ 65\\ 66\ 4.31\ 14.85\ 64.24\ 15.13\ 64.18\ 15.41\ 64.11\ 15.69\ 66\\ 67\ 65.28\ 15.07\ 65.22\ 15.36\ 65.15\ 15.64\ 65.08\ 15.93\ 67\\ 68\ 66.26\ 15.50\ 66.19\ 15.59\ 66.19\ 15.87\ 66.05\ 16.16\ 68\\ 99\ 67.23\ 15.52\ 67.16\ 15.81\ 67.09\ 16.11\ 67.02\ 16.40\ 69\\ 99\ 67.23\ 15.52\ 67.16\ 15.81\ 67.09\ 16.11\ 67.02\ 16.40\ 69\\ 97\ 68.21\ 15.75\ 68.14\ 16.04\ 68.07\ 16.34\ 67.99\ 16.64\ 70\\ 71\ 69.18\ 15.97\ 69.11\ 16.27\ 69.04\ 16.57\ 68.97\ 16.88\ 71\\ 72\ 70.15\ 16.20\ 70.00\ 16.50\ 70.01\ 16.81\ 69.94\ 17.11\ 72\\ 73\ 71.13\ 16.42\ 71.06\ 16.73\ 70.96\ 17.28\ 71.88\ 17.99\ 74\ 72.00\ 16.57\ 72.05\ 17.88\ 17.97\ 72.83\ 17.88\ 17.97\ 72.83\ 17.88\ 17.97\ 72.83\ 17.88\ 17.97\ 72.83\ 17.86\ 17.97\ 72.83\ 17.86\ 17.97\ 72.83\ 17.86\ 17.97\ 72.85\ 17.88\ 17.97\ 76.90\ 18.11\ 76.8\ 18.21\ 75.76\ 18.54\ 18.20\ 77\ 75.03\ 17.22\ 78.54\ 18.27\ 17.87\ 77.1\ 19.01\ 80\ 77\ 75.03\ 17.22\ 78.54\ 18.27\ 77.71\ 19.01\ 80\ 77\ 75.63\ 18.57\ 18.34\ 77.77\ 18.88\ 77.71\ 19.01\ 80\ 77\ 77.50\ 18.57\ 18.34\ 77.77\ 18.88\ 77.71\ 19.01\ 80\ 77\ 77.50\ 18.57\ 18.34\ 77.77\ 18.88\ 77.71\ 19.01\ 80\ 77\ 77.50\ 18.57\ 78\ 75.84\ 18.27\ 75.76\ 18.54\ 18.77\ 77.71\ 19.01\ 80\ 77\ 77.8\ 18.34\ 77.77\ 18.88\ 77.71\ 19.01\ 80\ 77\ 77.8\ 18.78\ 77\ 77.1\ 19.57\ 84.68\ 19.94\ 84.60\ 20.31\ 84.51\ 15.90\ 83.54\ 20.20\ 83\ 85.74\ 20.44\ 85\ 83\ 80.71\ 19.57\ 84.68\ 19.94\ 84.60\ 20.31\ 84.51\ 89.99\ 85\ 85.74\ 19.90\ 85.52\ 82.9\ 19.12\ 82.74\ 19.48\ 84.51\ 19.90\ 85.52\ 82.9\ 19.12\ 82.74\ 19.48\ 84.50\ 19.48\ 84.50\ 18.51\ 89\ 90\ 87.68\ 20.20\ 85\ 85.74\ 20.20\ 85\ 85.74\ 20.20\ 85\ 85.74\ 20.20\ 85\ 85.74\ 20.20\ 85\ 85.74\ 20.20\ 85\ 85.74\ 20.20\ 85\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 85\ 78\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.57\ 18.5$	64	62.36	14.40	62.30	14.67	62.23	14.94	62.17	15.21	64
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$\begin{array}{c} 67\ 65.28\ 15.07\ (65.22\ 15.36\ 65.15\ 15.64\ 65.08\ 15.93\ 67\\ 68\ 66.26\ 15.30\ (66.19\ 15.59\ 66.12\ 15.87\ (66.05\ 16.16\ 68\\ 69\ 67.23\ 15.52\ (67.16\ 15.81\ (67.09\ 16.11\ 167.02\ 16.40\ 69\\ 70\ 68.21\ 15.75\ 68.14\ 16.04\ (68.07\ 16.34\ 67.99\ 16.64\ 70\\ 71\ 69.18\ 15.97\ 69.11\ 16.27\ 69.04\ 16.57\ 68.97\ 16.88\ 71\\ 72\ 70.15\ 16.20\ 70.08\ 16.50\ 70.01\ 16.81\ 69.94\ 17.11\ 72\\ 73\ 71.13\ 16.42\ 71.06\ 16.73\ 70.96\ 17.04\ 70.91\ 17.35\ 73\\ 73\ 70.15\ 16.65\ 72.001\ 16.81\ 69.94\ 17.11\ 72\\ 73\ 71.13\ 16.42\ 71.06\ 16.73\ 70.96\ 17.04\ 70.91\ 17.35\ 73\\ 73\ 70.8\ 16.65\ 72.001\ 16.96\ 17.96\ 17.26\ 17.88\ 17.88\ 17.83\ 75\\ 73\ 76\ 74.05\ 17.10\ 73.96\ 17.42\ 73.90\ 17.74\ 73.82\ 18.80\ 77\\ 77\ 57.30\ 81\ 6.87\ 73.00\ 17.42\ 73.90\ 17.74\ 73.82\ 18.80\ 77\\ 77\ 57.60\ 17.32\ 74.95\ 17.65\ 74.87\ 17.98\ 74.79\ 18.30\ 77\\ 77\ 75\ 76.00\ 17.55\ 75.92\ 17.83\ 75.84\ 18.21\ 75.76\ 18.54\ 78.77\ 71\ 19.01\ 80\\ 79\ 76.98\ 17.77\ 76.90\ 18.11\ 76.82\ 18.44\ 76.74\ 18.78\ 79\\ 79\ 76.98\ 17.77\ 76.90\ 18.17\ 78\ 75.84\ 18.21\ 75.76\ 18.94\ 78.74\ 18.878\ 79\\ 79\ 76.98\ 17.77\ 76.90\ 18.17\ 78\ 76.86\ 19.94\ 82.56\ 20.20\ 85\\ 82\ 82\ 18.20\ 81.76\ 19.42\ 81.57\ 78.76\ 18.97\ 78\ 80.62\ 19.48\ 82.56\ 20.20\ 85\\ 83\ 80\ 81\ 76\ 19.22\ 81.68\ 19.48\ 82.56\ 20.02\ 85\\ 83\ 80\ 81\ 81\ 90\ 81.76\ 19.25\ 81.68\ 19.48\ 82.56\ 20.20\ 85\\ 83\ 85\ 74\ 19.90\ 81.66\ 19.48\ 82.56\ 20.20\ 85\\ 83\ 85\ 74\ 19.80\ 85\ 66\ 20.74\ 85\ 85\ 78\ 85\ 81\ 81\ 90\ 83\ 85\ 74\ 19.80\ 85\ 81\ 81\ 90\ 81\ 77\ 19\ 88\ 85\ 74\ 19.80\ 85\ 81\ 81\ 90\ 85\ 81\ 81\ 19\ 81\ 81\ 81\ 81\ 81\ 81\ 81\ 81\ 81\ 81$	66	64.31	14.85	64.24		64 18	15 41	64 11	15 69	60
$\begin{array}{c c c c c c c c c c c c c c c c c c c $				65.22	15.36	65.15	15.64	65.08	15.93	67
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	68	66.26	15.30	66.19	15.59					
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	69	67.23	15.52			67.09	16.11	67.02	16.40	69
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	70	68.21	15.75	68.14	16.04	68.07	16.34	67.99	16.64	70
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$								i		
$\begin{array}{c c c c c c c c c c c c c c c c c c c $			15.97	69.11	16.27			68.97	16.88	71
$\begin{array}{c c c c c c c c c c c c c c c c c c c $				70.08	16.50	70.01	16.81	69.94	17.11	72
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$										
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						71.96	17.28	71.88	17.59	74
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						72.93	17.50	72.85		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						73.90	17.74	73.82		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						74.87	17.98	74.79		
$\begin{array}{c c c c c c c c c c c c c c c c c c c $								75.76	18.54	78
$\begin{array}{c c c c c c c c c c c c c c c c c c c $										
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	80	77.95	18.00	77.87	18.34	77.79	18.68	77.71	19.01	80
$\begin{array}{c c c c c c c c c c c c c c c c c c c $					10.00					
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$\begin{array}{c c c c c c c c c c c c c c c c c c c $				86.63	20.40					
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$								0	21.09	1 30
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	91	88.67	20,47	88.58	20,86	88.49	21.94	88 90	21 69	01
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$										
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				90.52	21.32					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	94	91.59	21.15	91.50	21.54					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$										
$\begin{array}{c} 97 \ 94 \ 51 \ 21 \ 82 \ 94 \ 42 \ 22 \ 23 \ 94 \ 43 \ 22 \ 64 \ 54 \ 22 \ 23 \ 64 \ 54 \ 22 \ 23 \ 28 \ 55 \ 19 \ 23 \ 29 \ 53 \ 22 \ 64 \ 54 \ 22 \ 23 \ 28 \ 55 \ 19 \ 23 \ 29 \ 53 \ 29 \ 53 \ 22 \ 53 \ 29 \ 53 \ 22 \ 53 \ 29 \ 53 \ 22 \ 53 \ 23 \ 51 \ 97 \ 23 \ 23 \ 51 \ 97 \ 23 \ 23 \ 51 \ 97 \ 23 \ 23 \ 51 \ 97 \ 23 \ 23 \ 51 \ 97 \ 23 \ 23 \ 51 \ 97 \ 23 \ 23 \ 51 \ 97 \ 23 \ 23 \ 51 \ 97 \ 23 \ 23 \ 53 \ 53 \ 53 \ 53 \ 53 \ 53$										
$\begin{array}{c} 98 \ 95.49 \ 22.05 \ 95.39 \ 22.46 \ 95.29 \ 22.88 \ 95.19 \ 23.29 \ 98 \ 99 \ 96.46 \ 22.27 \ 96.36 \ 22.69 \ 96.26 \ 23.11 \ 96.16 \ 23.53 \ 99 \ 100 \ 97.44 \ 22.50 \ 97.34 \ 22.92 \ 97.24 \ 23.34 \ 97.13 \ 23.77 \ 100 \ 100 \ 97.44 \ 22.50 \ 97.34 \ 22.92 \ 97.24 \ 23.44 \ 97.13 \ 23.77 \ 100 \ 100 \ 97.44 \ 22.50 \ 22.50$	97	94.51	21.82	94.42	22.23	94.32				
$\begin{array}{c} 99 \ 96.46 \ 22.27 \ 96.36 \ 22.69 \ 96.26 \ 23.11 \ 96.16 \ 23.53 \ 99 \ 100 \ 97.44 \ 22.50 \ 97.34 \ 22.92 \ 97.24 \ 23.34 \ 97.13 \ 23.77 \ 100 \$				95.39	22.46					
100 97.44 22.50 97.34 22.92 97.24 23.34 97.13 23.77 100 : Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;										
; Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. ;										
	1.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
$\widehat{\square} 77 \text{ Deg.} 76\frac{3}{4} \text{Deg.} 76\frac{1}{2} \text{Deg.} 76\frac{1}{4} \text{Deg.} \widehat{\square} $	S									S
	â	77	Der	763	Der	761	Der	763	Dor	í
	_			104	5.	102	Deg.	104	Deg.	

TRAVERSE TABLE.

D	14 I	Deg.	14 <u>1</u>)eg.	$14\frac{1}{2}$ I	Deg.	1431)eg.	E
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1	0.97	0.24	0.97	0.25	0.97	0.25	0.97	0.25	1
23	1.94 2.91	0.48	$1.94 \\ 2.91$	0.49	1.94 2.90	0.50 0.75	1.93 2.90	0.51	23
4	3.88	0.97	3.88	0.98	3.87	1.00	3.87	1.02	4
5 6	4.85 5.82	1.21	4.85	1.23	4.84 5.81	$1.25 \\ 1.50$	4.84	1.27	56
7	6.79	1.69	6.78	1.72	6.78	1.75	6.77	1.78	7
8 9	7.76 8.73	$1.94 \\ 2.18$	7.75 8.72	1.97	7.75	$2.00 \\ 2.25$	7.74 8.70	2.04 2.29	8 9
10	9.70	2.42	9.69	2.46	9.68	2.50	9.67	2.55	10
11	10.67	2.66		2.71	10.65	2.75	10.64	2.80	11
	11.64 12.61	2.90 3.15	11.63 12.60	2.95	11.62 12.59	3.00 3.25	11.60 12.57	3.06 3.31	12 13
14	13.58	3.39	13.57	3.45	13.55	3.51	13.54	3.56	14
15 16	$14.55 \\ 15.52$	3.63	14.54 15.51	3.69	14.52 15.49	3.76 4.01	$14.51 \\ 15.47$	3.82 4.07	15 16
17	16.50	4.11	16.48	4.18	16.46	4.26	16.44	4.33	17
	17.47 18.44	4.35 4.60	$17.45 \\ 18.42$	4.43	17.43 18.39	4.51 4.76	$17.41 \\ 18.37$	4.58	18 19
	19.41	4.84	19.38	4.92	19.36	5.01	19.34	5.09	20
21	20.38	5.08	20.35	5.17	20.33	5.26	20.31	5.35	21
	21.35	5.32 5.56	$21.32 \\ 22.29$	5.42	21.30 22.27	5.51 5.76	$21.28 \\ 22.24$	5.60 5.86	22
24	23.29	5.81	23.26	5.91	23.24	6.01	23.21	6.11	24
	24.26 25.23	6.05 6.29	$24.23 \\ 25.20$	6.15 6.40	24.20 25.17	6.26 6.51	24.18 25.14	6.37	25 26
	26.20	6.53	26.17	6.65	26.14	6,76	26.11	6.62 6.87	27
	27.17	6.77	27.14	6.89	27.11	7.01	27.08	7.13	28
	28.14 29.11	7.02 7.26	28.11 29.08	7.14 7.38	28.08 29.04	7.26 7.51	28.04 29.01	7.38 7.64	29 30
31	30.08	7.50	30.05	7.63	30.01	7.76	29.98	7.89	31
32	31.05 32.02	7.74	31.02 31.98	7.88	30.98 31.95	8.01 8.26	30.95 31.91	8.15	
34	32.02	8.23		8.37	32.92	8.51	32.88	8.40	
35	33.96	8.47	33.92	8.62	33.89	8.76	33.85	8.91	35
30	34.93 35.90	8.71 8.95	34.89 35.86	8.86 9.11	$34.85 \\ 35.82$	9.01	34.81 35.78		
- 38	36.87	9.19	36.83	9.35	36.79	9.51	36.75	9.67	38
39 40	37.84	9.44	37.80 38.77	9.60 9.85	37.76 38.73	9.76 10.02	37.71 38.68	9.93 10.18	
41	39.78	9.92	39.74	10.09	39.69	10.27	39.65	10.44	41
42	2 40.75 3 41.72	10.16		10.34 10.58	40.66	10.52 10.77	40.62	10.69	42
43	41.72 42.69	10.40	41.68	10.58		10.77	41.58	10.95	43
4	43.66	10.89	43.62	11.08	43.57	11.27	43.52	11.46	45
	44.63		44.58	11.32		11.52	44.48	11.71	46
48	3 46.57	11.61	46.52	11.82	46.47	12.02	46.42	12.22	48
49 50	47.54	11.85	47.49	12.06 12.31		12.27 12.52		12.48	
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	t.
A	76	Deg.	754	Deg.	751/2	Deg.	751	Deg.	Dis

1	E	14	Deg.	141	Deg.	141	Deg.	143	Deg.	E
l	ist.		Dep.		Dep.		Dpe.		Dep.	ist.
ŀ										
l		49.49 50.46			$12.55 \\ 12.80$		$12.77 \\ 13.02$		12.98 13.24	
ł		51.43			13.05		13.27		13.49	
ł		52.40			13.29		13.52		13.75	
I		53.37			13.54	53.25			14.00	
I		54.34 55.31			13.78 14.03		$14.02 \\ 14.27$		14.26	
l		56.28			14.28		14.52		14:77	
I	59	57.25	14.27		14.52		14.77		15.02	
	60	58.22	14.52	58.15	14.77	58.09	15.02	58.02	15.28	60
l		59.19		59.12	15.02	59.06	15.27	58.99	15.53	61
L	62	60.16	$15.00 \\ 15.24$	60.09	15.25		15.52		15.79	
F	63	61.13	15.24		15.51		15.77		16.04	
I		62.10 63.07			$15.75 \\ 16.00$		16.02 16.27		16.29	
		64.04			16.25		16.53		16.80	
I	67	65.01	16.21	64.94	16.49	64.87	16.78		17.06	
		65.98			16.74		17.03		17.31	
L		66.95 67.92			16.98 17.23		17.28	66.73 67.69	17.57	
	10	01.92	10.95	07.85	11.20	01.11	17.55	07.03	17.82	
l	71	68.89	17.18	68.82	17.48	68.74	17.78	68.66	18.08	71
Ľ	72	69.86	17.42		17.72		18.03	69.63		
l		70.83			17.97		18.28		18.59	
Ľ		71.80			$18.22 \\ 18.46$		18.53 18.78	71.56	18.84	
l		73.74			18.71		19.03		19.35	
I	77	74.71	18.63		18.95		19.28	74.46	19.60	77
l		75.68			19.20		19.53		19.86	
L		76.65			19.45		19.78		20.11	
ŀ		77.62	19.35	11.94	19.69	11.40	20.03	11.30	20.37	80
l		78.59			19.94		20.28		20.62	
		79.56			20.18		20.53		20.88	
l	83	80.53	20.08		20.43		20.78 21.03		21.13	
	85	81.50 82.48	20.52	82.38	20.68 20.92		21.03		21.39	
Ľ	86	83.45	20.81	83.35	21.17		21.53		21.90	
	87	84.42	21.05	84.32	21,42	84.23	21.78	84.13	22.15	87
	88	85.39	21.29		21.66		22.03	85.10		
ŀ		86.36 87.33		86.26	21.91		$22.28 \\ 22.53$		22.66	
-				01.20		07.13	42.00	01.00	22.91	90
1		88.30			22.40		22.78		23.17	
I		89.27 90.24		89.17 90.14	22.65 22.89		$23.04 \\ 23.29$		23.42	
I		91.21		91.11			23.54		23.68 23.93	93 94
1	95	92.18	22.98	92.08	23.38	91.97	23.79		24.19	95
	96	93.15 94.12	23.22	93.05	23.63	92.94	24.04	92.84	24.44	96
					23.88	93.91		93.80		97
I		95.09 96.06		94.98 95.95		94.88 95.85		94.77 95.74		98 99
1		97.03		96.92		96.81		96.70		100
	St.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
k	ā	76]	Deg.	753)eg	751	Der	751	Dag	Dis
	-		8'				-ug.	104	Ces.	

D	15	Deg.	151	Deg.	151	Deg.	154	Deg.	U
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
12	0.97	0.26 0.52	0.96	0.26 0.53	0.96	0.27	0.96	0.27	1
ŝ	2.90	0.78	2.89	0.55	2.89	0.53	£.92 2.89	0.54	23
4	3.86	1.04	3.86	1.05	3.85	1.07	3.85	1.09	4
56	4.83	1.29 1.55	4.82 5.79	1.32 1.58	4.82	1.34 1.60	4.81	1.36	1 5 6
7	6.76	1.81	6.75	1.84	6.75	1.87	6.74	1.90	7
8	7.73	2.07	7.72	2.10	7.71	2.14	7.70	2.17	8
9 10	8.69 9.66	2.33 2.59	8.68 9.65	2.37 2.63	8.67 9.64	2.41 2.67	8.66		9 10
			10.01						-
	10.63 11.59	$2.85 \\ 3.11$	10.61	2.89 3.16	10.60	2.94	10.59	2.99	11
	12.56	3.36	12.54	3.42	12.53	3.21 3.47	$11.55 \\ 12.51$	3.26	12 13
14	13.52	3.62	13.51	3.68	13.49	3.74	13.47	3.80	14
	14.49 15.45	3.88	14.47	3.95	14.45	4.01	14.44	4.07	15
	15.45	4.14	16.40	4.21 4.47	15.42 16.38	4.28 4.54	15.40 16.36	4.34	16 17
18	17.39	4.66	17.37	4.73	17.35	4.81	17.32	4.89	18
	18.35	4.92	18.33	5.00	18.31		18.29	5.16	19
-20	19.32	5.18	19.30	5.26	19.27	5.34	19.25	5.43	20
	20.28	5.44	20.26	5.52	20.24	5.61	26.21	5.70	21
	21.25	5.69	21.23	5.79	21.20	5.88	21.17	5.97	22
	22.22 23.18	5.95 6.21	22.19 23.15	6.05 6.31	22.16 23.13	6.15 6.41	22.14 23.10	6.24 6.51	23 24
	24.15	6.47	24.12	6.58	24.09	6.68	24.06	6.79	25
26	25.11	6.73	25.08	6.84	25.05	6.95	25.02	7.06	26
	26.08 27.05	6.99 7.25	26.05 27.01	7.10 7.36	26.02 26.98	7.22	25.99 26.95	7.33	27 28
	28.01	7.51	27.98	7.63	27.95	7.75	27.91	7.87	29
30	28.98		28.94	7.89	28.91	8.02	28.87	8.14	30
.31	29.94	8.02	29.91	8.15	29.87	8.28	29.84	8.41	31
	30.91 31.88	8.28	30.87 31.84	8.42	30.84	8.55	30.80	8.69	32 33
	32.84	8.54 8.80	32.80	8.68 8.94	31.80 32.76	8.82 9.09	31.76	8.96 9.23	34
35	33.81	9.06	33.77	9.21	33.73	9.35	33.69	9.50	35
	34.77	9.32	34.73	9.47	34.69	9.62	34.65	9.77	36
	35.74 36.71	9.58 9.84	35.70 36.66	9.73	35.65	9.89 10.16	35.61 36.57		37 38
39	37.67	10.09	37.63	10.26	37.58	10.42	37.54	10.59	39
40	38:64	10.35	38.59	10.52	38.55	10.69	38.50	10.86	40
	39.60	10.61		10.78		10.96	39.46	11.13	41
	40.57 41.53	10.87 11.13	40.52	$11.05 \\ 11.31$		11.22	40.42	11.40	42 43
44	42.50	11.39	42.45	11.57	42.40	11.76	42.35	11.94	44
45	43.47	11.65	43.42	11.84	43.36		43.31		45
		11.91 12.16		12.10 12.36	44.33	12.29	44.27 45.24		46 47
	46.36	12.42	46.31		46.25	12.83	46.20		48
49	47.33	12.68	47.27	12.89	47.22	13.09	47.16	13.30	49
50	48.30	12.94	48.24	13.15	48.18	13.36	48.12	13.57	50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	St
Di	75]	Deg.	743	Deg.	$74\frac{1}{2}$ I	Deg.	74	Deg	āl

$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Lat. Dep 9.09 13.6 0.05 14. 1.01 14. 1.97 14. 2.94 14. 3.90 15.5 4.86 15. 5.82 15. 5.82 15. 6.78 16. 7.75 16. 8.71 16. 9.67 16. 0.63 17. 1.60 17. 2.56 17. 3.52 17.	84 51 11 52 39 53 66 54 93 55 20 56 47 57 74 58 01 59 29 60 56 61
$\begin{array}{c} 52\ 50.23\ 18.46\ 50.17\ 13.68\ 50.11\ 13.90\ 5\\ 53\ 51.19\ 13.72\ 51.13\ 13.94\ 51.07\ 14.16\ 5\\ 54\ 52.16\ 13.96\ 52.10\ 14.20\ 52.04\ 14.43\ 5\\ 55\ 53.13\ 14.24\ 53.06\ 14.47\ 53.00\ 14.70\ 5\\ 56\ 54.09\ 14.49\ 54.03\ 14.73\ 53.96\ 14.97\ 5\\ 56\ 54.09\ 14.49\ 54.03\ 14.73\ 53.96\ 14.97\ 5\\ 56\ 55.06\ 14.75\ 54.99\ 14.99\ 54.93\ 15.23\ 5\\ 58\ 56.02\ 15.01\ 55.96\ 15.26\ 55.89\ 15.50\ 5\\ 59\ 56.99\ 15.27\ 55.92\ 15.52\ 56.85\ 15.77\ 5\\ 50\ 57.96\ 15.53\ 57.89\ 15.78\ 57.82\ 16.03\ 5\\ 56\ 57.96\ 15.53\ 57.89\ 15.78\ 57.82\ 16.03\ 5\\ 56\ 50.99\ 15.27\ 59.82\ 16.04\ 58.78\ 16.30\ 5\\ 56\ 50.99\ 16.55\ 57.89\ 15.78\ 57.82\ 16.16\ 5\\ 56\ 25.99\ 16.55\ 57.89\ 15.78\ 5\\ 61\ 58.92\ 15.77\ 59.82\ 16.44\ 58.78\ 16.30\ 5\\ 56\ 50.85\ 16.57\ 15.65\ 60.77\ 16.84\ 6\\ 64\ 61.82\ 16.56\ 61.75\ 16.83\ 61.67\ 17.10\ 6\\ 65\ 62.75\ 17.70\ 63.68\ 17.86\ 63.60\ 17.84\ 6\\ 64\ 61.82\ 17.60\ 65.68\ 17.80\ 63.60\ 17.84\ 6\\ 64\ 56.57\ 17.10\ 66\ 56.57\ 17.16\ 65\ 56.57\ 18.17\ 6\\ 65\ 56.57\ 17.80\ 65.57\ 18.17\ 6\ 65.51\ 17.90\ 68\ 55.81\ 17\ 6\\ 56\ 55.81\ 17.60\ 56.57\ 18.17\ 5\ 66.57\ 18.17\ 6\\ 56\ 56.57\ 17.80\ 56\ 56.57\ 18.17\ 5\ 56\ 56.57\ 18.17\ 5\ 56\ 55\ 18.17\ 5\ 56\ 55\ 18.17\ 5\ 56\ 55\ 58\ 18.17\ 5\ 56\ 55\ 18.17\ 5\ 56\ 55\ 18.17\ 5\ 56\ 55\ 18.17\ 5\ 56\ 55\ 58\ 18.17\ 5\ 56\ 55\ 18.17\ 5\ 56\ 55\ 18\ 57\ 5\ 56\ 55\ 58\ 18\ 17\ 5\ 56\ 55\ 58\ 17\ 5\ 56\ 55\ 58\ 18\ 17\ 5\ 56\ 55\ 18\ 17\ 5\ 56\ 55\ 58\ 18\ 17\ 56\ 55\ 58\ 18\ 17\ 5\ 56\ 55\ 18\ 17\ 5\ 56\ 55\ 58\ 18\ 17\ 5\ 56\ 55\ 58\ 18\ 17\ 5\ 56\ 55\ 58\ 18\ 17\ 5\ 56\ 56\ 56\ 57\ 18\ 56\ 56\ 56\ 57\ 18\ 56\ 56\ 56\ 57\ 18\ 56\ 56\ 57\ 18\ 56\ 56\ 57\ 56\ 56\ 56\ 57\ 56\ 56\ 56\ 56\ 57\ 56\ 56\ 56\ 56\ 57\ 56\ 56\ 56\ 56\ 56\ 56\ 56\ 56\ 56\ 56$	0.05 14. 1.01 14. 1.97 14. 2.94 14. 3.90 15. 4.86 15. 5.82 15. 6.78 16. 7.75 16. 8.71 16. 9.67 16. 0.63 17. 1.60 17. 2.56 17.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 58 51.19 \ 13.72 \ 51.13 \ 13.94 \ 51.07 \ 14.16 \ 5 \\ 54 \ 52.16 \ 13.98 \ 52.10 \ 14.20 \ 52.0414.43 \ 5 \\ 55 \ 53.13 \ 14.24 \ 53.06 \ 14.47 \ 53.00 \ 14.70 \ 5 \\ 56 \ 54.09 \ 14.49 \ 54.03 \ 14.73 \ 53.96 \ 14.97 \ 55 \\ 57 \ 55.06 \ 14.75 \ 54.99 \ 14.99 \ 54.93 \ 15.23 \ 55 \\ 55 \ 55.06 \ 14.75 \ 54.99 \ 14.99 \ 54.93 \ 15.23 \ 55 \\ 56 \ 56.02 \ 15.01 \ 55.96 \ 15.26 \ 55.89 \ 15.50 \ 56 \\ \mathbf{595 66.99} \ 15.27 \ 56.92 \ 15.52 \ 56.85 \ 15.77 \ 57 \\ 60 \ 57.96 \ 15.53 \ 57.89 \ 15.78 \ 57.82 \ 16.03 \ 56 \\ 52 \ 59.89 \ 16.05 \ 59.82 \ 16.31 \ 59.75 \ 16.57 \ 56 \\ 56 \ 50.85 \ 16.31 \ 59.75 \ 60.71 \ 16.84 \ 64 \\ 64 \ 61.82 \ 16.56 \ 61.75 \ 16.86 \ 61.67 \ 17.10 \ 66 \\ 65 \ 62.79 \ 16.82 \ 62.71 \ 17.10 \ 62.64 \ 17.37 \ 66 \\ 66 \ 65.75 \ 17.70 \ 66 \ 65.68 \ 17.80 \ 65.58 \ 17.64 \ 67 \ 64.55 \ 18.17 \ 66 \\ 68 \ 65.68 \ 17.60 \ 65.65 \ 17.89 \ 65.58 \ 18.17 \ 66 \\ 68 \ 65.68 \ 17.60 \ 65.57 \ 18.15 \ 66.54 \ 18.18.17 \ 68 \\ 68 \ 65.68 \ 17.80 \ 65.57 \ 18.15 \ 66.54 \ 18.44 \ 68 \ 18.44 \ 18.4$	1.01 14.: 1.97 14. 2.94 14.: 3.90 15.: 4.86 15 5.82 15. 6.78 16. 7.75 16.: 8.71 16. 9.67 16. 0.63 17. 1.60 17. 2.56 17.	39 53 66 54 93 55 20 56 47 57 74 58 01 59 29 60 56 61
$\begin{array}{c} 54 52.16 & 13.98 & 52.10 & 14.20 & 52.04 & 14.43 & 5 \\ 55 53.13 & 14.24 & 53.06 & 14.47 & 53.00 & 14.70 & 5 \\ 56 & 54.09 & 14.49 & 54.00 & 14.73 & 53.96 & 14.97 & 55 \\ 57 & 55.06 & 14.75 & 54.99 & 14.99 & 54.93 & 15.23 & 55 \\ 59 & 56.92 & 15.01 & 55.96 & 15.26 & 55.89 & 15.50 & 55 \\ 50 & 57.96 & 15.53 & 57.89 & 15.27 & 56.92 & 15.77 & 56 \\ 57.96 & 15.53 & 57.89 & 15.78 & 57.82 & 16.03 & 56 \\ 57.96 & 57.89 & 58.85 & 16.04 & 58.78 & 16.30 & 56 \\ 52 & 59.99 & 16.05 & 59.82 & 16.31 & 59.75 & 16.57 & 56 \\ 56 & 62.79 & 16.55 & 57.717.10 & 62.64 & 17.710 \\ 66 & 63.75 & 17.08 & 63.68 & 17.66 & 63.60 & 17.64 & 66 \\ 67 & 64.72 & 17.38 & 64.64 & 17.62 & 64.56 & 17.90 & 68 \\ 68 & 65.68 & 17.60 & 65.57 & 18.176 & 66.53 & 18.177 \\ 68 & 66.65 & 17.89 & 66.57 & 18.15 & 66.49 & 18.44 & 66 \\ 68 & 65.66 & 17.89 & 65.57 & 18.177 \\ 68 & 65.66 & 17.89 & 65.57 & 18.177 \\ 68 & 65.66 & 17.89 & 65.57 & 18.177 \\ 68 & 65.68 & 17.60 & 65.57 & 18.177 \\ 68 & 65.66 & 17.89 & 65.57 & 18.177 \\ 68 & 65.66 & 17.89 & 65.57 & 18.177 \\ 68 & 65.66 & 17.89 & 65.57 & 18.177 \\ 68 & 65.66 & 17.89 & 65.57 & 18.177 \\ 68 & 65.66 & 17.89 & 65.57 & 18.177 \\ 68 & 65.68 & 17.60 & 65.57 & 18.178 \\ 66.59 & 15.89 & 15.69 \\ 15.89 & 15.69 & 15.89 & 15.89 \\ 15.89 & 15.69 & 15.89 \\ 15.89 & 15.89 & 15.89 \\ 15.89 & 15.89 & 15.89 \\ 15.89 & 15.89 & 15.89 \\ 15.89 & 15.89 & 15.89 \\ 15.89 & 15.89 & 15.89 \\ 15.89 & 15.89 & 15.89 \\ 15.89 & 15.89 & 15.89 \\ 15.89 & 15.89 & 15.89 \\ 15.89 & 15.89 & 15.89 \\ $	1.97 14.0 2.94 14.3 3.90 15.5 4.86 15.5 5.82 15.6 6.78 16.7 7.75 16.3 8.71 16.9 9.67 16.0 0.63 17.1 1.60 17.1 2.56 17.	66 54 93 55 20 56 47 57 74 58 01 59 29 60 56 61
$\begin{array}{c} 56554.0914.4954.0314.7353.9614.975,\\ 5755.0614.7554.9914.9954.9954.9315.235,\\ 5856.0215.0155.9615.2655.8915.605,\\ 59560215.0155.9615.2756.9215.5256,8515.775,\\ 6057.9615.5357.8915.7857.8216.035,\\ 6158.9215.7958.8516.0458.7816.305,\\ 6259.8916.0559.8216.3159.7516.575,\\ 6360.8516.3160.7816.5760.7116.846,\\ 6461.8216.5661.7516.8361.6717.106,\\ 6562.7916.8262.7117.1062.6417.376,\\ 6562.7917.1063.6817.3663.6017.646,\\ 6764.7217.3063.6817.3863.5017.646,\\ 6764.7217.3063.6817.3863.5017.646,\\ 6865.6817.6065.6117.8965.5318.1766,\\ 6865.6817.8065.518.1566.4918.446417.6665.5318.176665.5318.476665.5318.446417.6665.5318.446415.6415.6415.6415.6415.6415.6415.6415.6415.6415.6416.5516.5518.5616.5616.5616.5616.5616.5617.5616.5616.5616.5616.5616.5616.5617.5616.56$	3.90 15.3 4.86 15.4 5.82 15.4 6.78 16.4 7.75 16.4 9.67 16.4 0.63 17.4 11.60 17.4 12.56 17.4	93 55 20 56 47 57 74 58 01 59 29 60 56 61
$\begin{array}{c} 57 \\ 55.06 \\ 14.75 \\ 58.56.02 \\ 15.01 \\ 59.56.99 \\ 15.27 \\ 56.92 \\ 15.92 \\ 15.92 \\ 15.92 \\ 15.92 \\ 15.92 \\ 15.92 \\ 15.92 \\ 15.77 \\ 56.82 \\ 15.77 \\ 56.82 \\ 15.78 \\ 15.78 \\ 57.82 \\ 16.30 \\ 57.96 \\ 15.78 \\ 15.78 \\ 57.82 \\ 16.30 \\ 57.88 \\ 15.78 \\ 57.82 \\ 16.30 \\ 57.88 \\ 15.78 \\ 57.82 \\ 16.30 \\ 57.88 \\ 15.78 \\ 57.82 \\ 16.30 \\ 57.88 \\ 15.78 \\ 57.82 \\ 16.30 \\ 57.88 \\ 15.7$	4.86 15. 5.82 15. 6.78 16. 7.75 16. 8.71 16. 9.67 16. 0.63 17. 1.60 17. 2.56 17.	47 57 74 58 01 59 29 60 56 61
$\begin{array}{c} 58 \ 66.02 \ 15.01 \ 55.96 \ 15.26 \ 55.89 \ 15.50 \ 5\\ 59 \ 56.99 \ 15.27 \ 56.92 \ 15.52 \ 56.85 \ 15.77 \ 5\\ 60 \ 57.96 \ 15.53 \ 57.89 \ 15.78 \ 57.82 \ 16.03 \ 5\\ 61 \ 58.92 \ 15.79 \ 58.82 \ 16.04 \ 58.78 \ 16.30 \ 5\\ 62 \ 59.89 \ 16.05 \ 59.82 \ 16.04 \ 58.78 \ 16.57 \ 5\\ 63 \ 60.85 \ 16.31 \ 60.78 \ 16.57 \ 60.71 \ 16.84 \ 6\\ 64 \ 61.82 \ 16.56 \ 61.75 \ 16.83 \ 61.67 \ 17.10 \ 6\\ 65 \ 62.79 \ 16.82 \ 61.75 \ 17.17.10 \ 62.64 \ 17.37 \ 6\\ 66 \ 63.75 \ 17.08 \ 63.68 \ 17.36 \ 63.60 \ 17.64 \ 6\\ 67 \ 64.72 \ 17.34 \ 64.64 \ 17.82 \ 64.56 \ 17.90 \ 68 \ 56.58 \ 17.60 \ 65.57 \ 18.17 \ 6\\ 68 \ 65.65 \ 17.80 \ 65.57 \ 18.17 \ 6\\ 68 \ 65.65 \ 17.80 \ 65.57 \ 18.17 \ 6\\ 68 \ 65.65 \ 17.80 \ 65.57 \ 18.17 \ 6\\ 68 \ 65.65 \ 17.80 \ 65.57 \ 18.44 \ 6\\ 64 \ 61.84 \ 14.44 \ 61 \ 18.44 \ 64.44 \ 18.44 \ 64.56.57 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.45 \ 64.56 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.45 \ 64.56 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.44 \ 64.56 \ 18.45 \ 18.45 \ 64.56 \ 18.45 \ 64.56 \ 18.45 \ 64.56 \ 18.45 \ 64.56 \ 18.45 \ 18.45 \ 64.56 \ 18.45 \ 18$	5.82 15. 6.78 16. 7.75 16. 8.71 16. 9.67 16. 0.63 17. 1.60 17. 2.56 17.	74 58 01 59 29 60 56 61
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7.75 16. 8.71 16. 9.67 16. 0.63 17. 1.60 17. 2.56 17.	29 60 56 61
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	8.71 16. 9.67 16. 0.63 17. 1.60 17. 2.56 17.	56 61
$\begin{array}{c} 62 \ 59.89 \ 16.05 \ 59.82 \ 16.31 \ 59.75 \ 16.57 \ 5\\ 63 \ 60.85 \ 16.31 \ 60.78 \ 16.87 \ 60.71 \ 16.84 \ 6\\ 64 \ 61.82 \ 16.56 \ 61.75 \ 16.82 \ 61.67 \ 17.10 \ 6\\ 65 \ 62.79 \ 16.82 \ 62.71 \ 17.10 \ 62.64 \ 17.37 \ 6\\ 66 \ 63.75 \ 17.08 \ 63.68 \ 17.36 \ 63.60 \ 17.64 \ 6\\ 67 \ 64.72 \ 17.34 \ 64.64 \ 17.62 \ 64.56 \ 17.90 \ 6\\ 68 \ 65.68 \ 17.60 \ 65.53 \ 18.17 \ 6\\ 69 \ 66.65 \ 17.86 \ 66.57 \ 18.15 \ 66.49 \ 18.44 \ 6\\ \end{array}$	9.67 16. 0.63 17. 1.60 17. 2.56 17.	
$\begin{array}{c} 68\ 60.85\ 16.31\ 60.78\ 16.57\ 60.71\ 16.84\ 6\\ 64\ 61.82\ 16.56\ 61.75\ 16.83\ 61.67\ 17.10\ 6\\ 65\ 62.79\ 16.82\ 62.71\ 17.10\ 62.64\ 17.37\ 6\\ 66\ 63.75\ 17.08\ 63.68\ 17.36\ 63.60\ 17.64\ 6\\ 67\ 64.72\ 17.34\ 64.64\ 17.62\ 64.56\ 17.90\ 6\\ 68\ 65.68\ 17.60\ 65.51\ 17.80\ 65.53\ 18.17\ 6\\ 69\ 66.65\ 17.80\ 65.57\ 18.15\ 66.49\ 18.44\ 6\end{array}$	0.63 17. 1.60 17. 2.56 17.	
$\begin{array}{c} 64\ 61.82\ 16.56\ 61.75\ 16.83\ 61.67\ 17.10\ 6\\ 65\ 62.79\ 16.82\ 62.71\ 17.10\ 62.64\ 17.37\ 6\\ 66\ 63.75\ 17.08\ 63.68\ 17.36\ 63.60\ 17.64\ 6\\ 67\ 64.72\ 17.34\ 64.64\ 17.82\ 64.56\ 17.90\ 6\\ 68\ 65.68\ 17.60\ 65.61\ 17.89\ 65.53\ 18.17\ 6\\ 69\ 66.65\ 17.80\ 66.57\ 18.15\ 66.49\ 18.44\ 6\end{array}$	1.60 17.	
$\begin{array}{c} 66 \\ 63.75 \\ 17.08 \\ 67 \\ 64.72 \\ 17.34 \\ 64.64 \\ 17.62 \\ 65.53 \\ 17.60 \\ 65.65 \\ 17.86 \\ 65.65 \\ 17.86 \\ 65.57 \\ 18.15 \\ 66.49 \\ 18.44 \\ 68 \\ 65.68 \\ 18.44 \\ 68 \\ 65.68 \\ 18.44 \\ 68 \\ 65.57 \\ 18.15 \\ 66.49 \\ 18.44 \\ 68 \\ 18.44 \\ 68 \\ 18.44 \\ 18.4$		37 64
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.02 11.	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4.48 18.	
	5.45 18.	46 68
	6.41 18.	
70 67.61 18.12 67.54 18.41 67.45 18.71 6	7.37 19.	00 70
71 68.58 18.38 68.50 18.68 68.42 18.97 6	8.33 19.	
	9.30 19.	
	0.26 19.	
75 72.44 19.41 72.36 19.73 72.27 20.04 7	2.18 20.	
76 73.41 19.67 73.32 19.99 73.24 20.31 7	3.15 20.	63 76
	4.11 20.	
	15.07 21. 16.03 21.	
	7.00 21.	
81 78.24 20.96 78.15 21.31 78.05 21.65 7	7.96 21.	99 81
82 79.21 21.22 79.11 21.57 79.02 21.91	18.92 22.	26 82
83 80.17 21.48 80.08 21.83 79.98 22.18	79.88 22.	
	30.85 22. 31.81 23.	
86 83.07 22.26 82.97 22.62 82.87 22.98	32.77 23.	
	33.73 23.	
	34.70 23. 35.66 24.	
	36.62 24	
91 87.90 23.55 87.80 23.94 87.69 24.32	37.58 24	70 91
	38.55 24	
93 89.83 24.07 89.73 24.46 89.62 24.85	89.51 25.	24 93
	90.47 25	
	91.43 25. 92.40 26.	
97 93.69 25.11 93.58 25.51 93.47 25.92	93.36 26.	.33 97
98 94.66 25.36 94.55 25.78 94.44 26.19	94.32 26.	.60 98
	95.28 26. 96.25 27.	
Dep. Lat. Dep. Lat. Dep. Lat.]	Dep. L	at. +:
75 Deg. 743 Deg. 741 Deg.		

D	16 I	Deg.	1611	Deg.	$16\frac{1}{2}$	Deg.	163	Deg.	E
st.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
12	0.96	0.28	0.96	0.28	0.96	0.28 0.57	0.96	0.29 0.58	12
3	2.88	0.83	2.88	0.84	2.88	0.85	2.87	0.86	
4	3.85 4.81	1.10	3.84	1.12 1.40	3.84	1.14	3.83 4.79	1.15	45
6	5.77	1.65	5.76	1.68	5.75	1.70	5.75	1.73	6
7	6.73	1.93	6.72	1.96	6.71		6.70	2.02	
89	7.69	2.21	7.68	2.24 2.52	7.67	2.27 2.56	7.66 8.62	2.31 2.59	
10	9.61	2.76	9.60	2.80	9.59		9.58	2.88	
	10.57		10.56	3.08	10.55	3.12	10.53	3.17	
	11.54 12.50	3.31 3.58	11.52 12.48	3.36 3.64	11.51	3.41	11.49	3.46	
	13.46	3.86		3.92	13.40	3.69 3.98	12.45 13.41	4.03	
15	14.42	4.13	14.40	4.20	14.33	4.26	14.36	4.32	15
	15.38	4.41 4.69	15.36 16.32	4.48	15.34 16.30		15.32	4.61	
19	16.34 17.30	4.96	17.28	-5.04	17.26		16.28 17.24		
19	18.26	5.24	18.24	5.32	18.22	5.40	18.19		19
20	19.23	5.51	19.20	5.60	19.18	5.68	19.15	5.76	20
21	20.19		20.16		20.14		20.11	6.05	
	21.15 22.11	6.06	$21.12 \\ 22.08$	6.16 6.44	21.09 22.05	6.25 6.53	21.07 22.02	6.34	
23	23.07		23.04	6.72	23.01		22.98		
25	24.03	6.89	24.00	7.00	23.97	7.10	23.94	7.20	25
26	24.99	7.17	24.96 25.92	7.28	24.93		24.90		
27	25.95 26.92	7.44	26.88	7.84	25.89 26.85	7.67	25.85 26.81	7.78	
29	27.88	7.99	27.84	8.11	27.81	8.24	27.77		29
30	28.84	8.27	28.80	8.39	28.76	8.52	28.73	8.63	30
31	29.80	8.54	29.76		29.72		29.68		
32	30.76 31.72	8.82	30.72 31.68	8.95 9.23	30.68 31.64		30.64		
34	32.68	9.37	32.64	9.51	32.60				
35	33.64	9.65	33.60	9.79	33.56	9.94	33.51	10.09	35
36	34.61	9.92 10.20	34.56 35.52	10.07	34.52	10.22	34.47	10.38	
37	36.53	10.47	36.48			10.51			
39	37.49	10.75	37.44		37.39	11.08	37.35	11.24	1 39
40	38.45	11.03	38.40	11.19	38.35	11.36	38.30	11.55	3 40
			39.36			11.64		11.8	
42	40.37	11.58	40.32	12.03	40.27	11.93	40.22	12.10	
44	42.30	12.13	42.24	12.31	42.19	12.50			
45	43.26	12.40	43.20	12.59	43.15	12.78	43.09	12.97	45
46	44.22	12.68	44.16 45.12	12.87	44.11	13.06	44.05	13.26	
		13.23	46.08	13.43	46.02	13.63	45.96		
49	47.10	13.51	47.04	13.71	46.98	13.92	46.92	14.12	49
50						14.20			
st.	Dep	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
Ā	74	Deg	734	Deg.	$73\frac{1}{2}$	Deg.	731	Deg.	Ā

Di	16 l	Deg.	164	Deg.	161	Deg.	164	163Deg.	
st.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
	49.02 49.99		48.96 49.92		48.90 49.86	14.48	48.84 49.79		51 52
	49.99		50.88			15.05	49.79		53
54	51.91	14.88	51.84	15.11	51.78	15.34	51.71	15.56	54
	52.87 53.83		52.80 53.76		52.74	$15.62 \\ 15.90$	52.67	15.85	55 56
	54.79		54.72		54.65	16.19	54.58		57
	55.75		55.68			16.47	55.54	16.72	58 59
	56.71 57.68		56.64 57.60			16.76 17.04	56.50 57.45		59 60
	58.64		58.56		58.49			17.58	61
	59.60		59.52		59.45		59.37		62 63
	60.56 61.52	17.64	60.48 61.44	17.91	60.41 61.36	18.18	60.33 61.28		64
65	62.48	17.92	62.40	18.19	62.32	18.46	62.24	18.73	65
	63.44		63.36		63.28		63.20		66
	64.40 65.37		64.32 65.28		64.24 65.20		64.16 65.11		67 68
	66.33		66.24			19.30	66.07		69
70	67.29	19.29	67.20	19.59	67.12	19.88	67.03	20.17	70
	68.25	19.57	68.16	19.87	68.08		67.99	20.46	71
	69.21		69.12			20.45	68.95		72
	70.17		70.08 71.04		69.99 70.95	20.73	69.90 70 86	21.04 21.33	73
75	72.09	20.67	72.00		71.91	21.02 21.30		21.61	75
76	73.06	20.95	72.96	21.27	72.87	21.59	72.78	21.90	76
77	74.02 74.98	21.22	73,92 74.88			21.87 22.15		22.19 22.48	77
79	75.94	21.78	75.84			22.44	75.65	22.77	79
80	76.90	22.05	76.80	22.39		22.72		23.06	80
	77.86		77.76	22.67		23.01		23.34	81
	78.82		78.72		78.62	23.29	78.52	23.63	82
	79.78 80.75		79.68 80.64			23.57 23.86		23.92 24.21	83 84
	81.71		81.60			24.14	81.39	24.50	85
86	82.67	23.70	82.56	24.07	82.46	24.43	82.35	24.50 24.78	86
	63.63 84.59		83.52		83.42	24.71 24.99	83.31 84.27	25.07 25.36	87
88 89	84.59 85.55		84.48			24.99	85.22		89
	86.51		86.40			25.56		25,94	90
91	87.47	25.08	87.36			25.85		26.23	91
92 93		25.30	88.32 89,28	25.74		26.13 26.41		26.51 26.80	92 93
94	90.36	25.91	90.24			26.70	90.01	27.09	94
05	91 39	26.19	91.20	26.58		26.98	90.97	27.38	95
96	92.28 93.24	26.46	92.16 93.12	26.86		27.27	91.93	27.67 27.95	96 97
	93.24 94.20		94.08			27.83		28.24	98
99	95.16	27.29	95.04	27.70	94.92	28.12		28.53	99
100	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	100
ist.			Dep.			Lat.			ist.
P	74	Deg.	733	Deg.	$73\frac{1}{2}$	Deg.	731	Deg.	P

TRAVERSE TABLE.

D	17 D	eg.	1711	Deg.	171	Deg.	173	Deg.	J
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
12	0.96	0.29	0.95	0.30	0.95	0.30	0.95	0.30	1
3	2.87	0.89	2.87	0.89	2.86	0.90	2.86	0.91	23
4	3.83 4.78	1.17	3.82 4.78	1.19	3.81 4.77	1.20	3.81	1.22	45
5 6	5.74	1.75	5.73	1.78	5.72	1.80	5.71	1.83	6
7	6.69 7.65	2.05 2.34	6.69 7.64	2.08	6.68	2.10	6.67 7.62	2.13	7
8 9	8.61	2.63	8.60	2.57	7.63 8.58	2.41 2.71	8.57	2.44	9
10	9.56	2.92	9.55	2.97	9.54	3.01	9.52	3.05	10
	10.52 11.48	3.22	10.51	3.26	10.49	3.31	10.48	3.35	11
	12.43	3.51 3.80	11.46 12.42	3.56	$11.44 \\ 12.40$	3.61 3.91	11.43 12.38	3.66 3.96	12 13
	13.39	4.09	13.37	4.15	13.35	4.21	13.33	4.27	14
	14.34 15.30	4.39	14.33 15.28	4.45	14.31 15.26	4.51	14.29 15.24	4.57	15
17	16.26	4.97	16.24	5.04	16.21	5.11	16.19	5.18	17
18	17.21 18.17	.5.26	17.19 18.15	5.84 5.63	17.17 18.12	5.41 5.71	17.14 18.10	5.49 5.79	18 19
	19.13	5.85	19.10	5.93	19.07	6.01	19.05	6.10	20
21	20.08	6.14	20.06	6.23	20.03	6.31	20.00	- 6.40	21
	21.04 21.99	6.43 6.72	21.01 21.97	6.52	20.98 21.94	6.62	20.95 21.91	6.71	22
	21.99	7.02	22.92	6.82 7.12	21.94	6.92 7.22	21.91 22.86	7.01	23 24
25	23.91	7.31	23.88	7.41	23.84	7.52	23.81	7.62	25
20 27	24.86 25.82	7.60	24.83 25.79	7.71 8.01	24.80 25.75	7.82 8.12	24.76 25.71	7.93	26 27
28	26.78	8.19	26.74	8.30	26.70	8.42	26.67	8.54	28
	27.73 28.69	8.48 8.77	27.70 28.65	8.60 8.90	27.66 28.61	8.72 9.02	27.62 28.57	8.84 9.15	29 30
31	29.65	9.06	29.61	9.19	29.57	9.32	29.52		
32	30.60	9.00	30.56	9.19	30.52	9.62	30.48	9.45	31 32
33	31.56	9.65	31.52		31.47	9.92		10.06	33
35	32.51 33.47	9.94 10.23	32.47	10.08	32.43 33.38		32.38 33.33	10.37	34 35
36	34.43	10.53	34.38	10.68	34.33	10.83	34.29	10.98	36
37	35.38 36.34	$10.82 \\ 11.11$		10.97 11.27	35.29 36.24	11.13	35.24	11.28	37
39	37.30	11.40	37.25	11.57	37.19	11.73		$11.58 \\ 11.89$	39
40	38.25	11.69	38.20	11.86	38.15	12.03	38.10	12.19	40
	39.21	11.99	39.16			12.33		12.50	41
42	40.16 41.12	12.28 12.57		12.45 12.75		12.63 12.93	40.00 40.95	12.80	42
44	42.08	12.86	42.02	13.05	41.96	13.23	41.91	13,41	44
45	43.03 43.99			$13.34 \\ 13.64$	42.92		42.86 43.81	13.72	45
	43.99	13.45 13.74		13.64	43.87 44.82		43.81		46 47
48	45.90	14.03	45.84	14.23	45.78	14.43	45.71	14.63	48
49 50	46.86 47.82	14.33		14.53 14.83	46.73 47.69		46.67 47.62	$14.94 \\ 15.24$	49 50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st. [
ā	73]	Deg.	723	Deg.	$72\frac{1}{2}$	Deg.	$72\frac{1}{4}$	Deg.	Di

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D	17 1	Deg.	1711	Deg.	$17\frac{1}{2}$	Deg.	173	Deg.	H
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
	48.77 49.73		48.71 49.66			15.34 15.64	48.57 49.52		51 52
53	50.68	15.50	50.62	15.72	50.55	15.94	50.48	16.16	53
	51.64 52,60		$51.57 \\ 52.53$			16.24 16.54	51.43 52.38	16.46	54 55
56	53.55	16.37	53.48	16.61	53.41	16.84	53.33	17.07	56
	54.51 55.47		54.44 55.39			17.14			57 58
59	56.42	17.25	56.35	17.50	56.27	17.74	56.19	17.99	59
60	57.38	17.54	57.30	17.79	57.22	18.04	57.14	18.29	60
61	58.33		58.26			18.34		18.60	61
	59.29 60.25		59.21 60.17			18.64 18.94		18.90 19.21	62 63
64	61.20 62.16	18.71	61.12	18,98	61.04	19.25	60.95	19.51	64
65 66	62.16 63.12	19.00	62.08 63.03	19.28		19.55 19.85		19.82 20.12	65 66
67	64.07	19.59	63.99	19.87	63.90	20.15	63.81	20.43	67
	65.03 65.99			20.16 20.46	64.85	20.45 20.75	64.76 65.72	20.73 21.04	68 69
	66.94			20.76		21.05		21.34	70
71	67.90	20.76	67.81	21.05	67.71	21.35	67.62	21.65	71
72	68.85	21.05	68.76	21.35	68.67	21.65	68.57	21.95	72
73	69.81 70.77	$21.34 \\ 21.64$	69.72 70.67	21.65 21.94	69.62 70.58	21.95 22.25		22.26 322.56	73 74
75	71.72	21.93	71.63	22.24	71.53	22.55	71.43	3 22.86	75
76	72.68	22.22 22.51	72.58	22.54		22.85 23.15		3 23.17	76
78	74.59	22.80	74.49	$22.83 \\ 23.13$	74.39	33.46	74.29	23.78	78
79	75.55	23.10 23.39		23.43		23.76		4 24.08 24.39	
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81	77.46	23.68 23.97	77.36	24.02 24.32	77.2	24.36	77.14	1 24.69	
82 83	79.37	24.27		24.61		24.00		25.00 5 25.30	
	180.33			24.91		25.26		25.61	
	81.29 82.24			$25.21 \\ 25.50$		25.56		5 25.91 1 26.22	
8	83.20	25.44	83.09	25.80	82.9	26.16	82.8	6 26.52	87
88	84.15	25.73	84.04	26.10 26.39		3 26.46		$126.83 \\ 627.13$	
90	86.07	26.31	85.95	26.69		3 27.06		2 27.44	
9	87.02	26.61		26.99		27.36	86.6	7 27.74	91
	2 87.98 3 88.94			27.28		4 27.66 0 27.97		2 28.05 7 28.35	
9	4 89.85	27.48	8 89.77	27.87	89.6	5 28.27		3 28.66	
1 9.	5 90.85	27.78	8 90.7	3 28.17	90.6	28.57	90.4	8 28.96	95
9	6 91.81 7 92.70	328.36	91.6	3 28.47 1 28.76	92.5	6 28.87 1 29.17	91.4	3 29.27 8 29.57	96
	7 92.70		5 93.5	9 29.00	93.4	6 29.47	7 93.3	3 29.88	3 28
	9 94.6 [°] 0 95.6 [°]			5 29.36 0 29.63		2 29.77 7 30.07		9 30.18 4 30.49	
1	Dep	Lat	. Dep	. Lat	. Dep	Lat.	Dep	Lat.	it.
1	73	Deg	. 72	Deg	72	Deg	721	Deg	Q
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$ \begin{array}{c} 4 & 3.80 & 1.24 & 3.80 & 1.25 & 3.79 & 1.27 & 3.79 & 1.29 & 4 \\ 5 & 4.76 & 1.55 & 4.76 & 1.57 & 4.74 & 1.59 & 4.73 & 1.61 & 5 \\ 6 & 5.71 & 1.85 & 5.70 & 1.88 & 5.69 & 1.90 & 5.68 & 1.93 & 6 \\ 7 & 6.66 & 2.16 & 6.65 & 2.19 & 6.64 & 2.22 & 6.63 & 2.25 & 7 \\ 8 & 7.61 & 2.47 & 7.60 & 2.51 & 7.59 & 2.54 & 7.58 & 2.57 & 8 \\ 9 & 8.56 & 2.78 & 8.55 & 2.82 & 8.53 & 2.86 & 8.52 & 2.89 & 9 \\ 9 & 8.56 & 2.78 & 8.55 & 2.82 & 8.53 & 2.86 & 8.52 & 2.89 & 9 \\ 10 & 9.51 & 3.09 & 9.50 & 3.13 & 9.48 & 3.17 & 9.47 & 3.21 & 100 \\ 11 & 10.46 & 3.40 & 10.45 & 3.44 & 10.43 & 3.49 & 10.42 & 3.54 & 11 \\ 12 & 11.41 & 3.71 & 11.40 & 3.76 & 11.38 & 3.61 & 11.36 & 3.86 & 12 \\ 13 & 12.36 & 4.02 & 12.35 & 4.07 & 12.33 & 4.12 & 12.31 & 4.18 & 13 \\ 14 & 13.31 & 4.33 & 13.30 & 4.38 & 13.28 & 4.44 & 13.26 & 4.50 & 14 \\ 15 & 14.27 & 4.64 & 14.25 & 4.70 & 14.22 & 4.76 & 14.20 & 4.82 & 15 \\ 16 & 15.22 & 4.94 & 15.20 & 5.01 & 15.17 & 5.08 & 15.15 & 5.14 & 16 \\ 17 & 16.17 & 5.25 & 16.14 & 5.32 & 16.12 & 5.39 & 16.10 & 5.46 & 17 \\ 19 & 17.12 & 5.56 & 17.09 & 5.64 & 17.07 & 5.71 & 17.04 & 5.79 & 18 \\ 19 & 18.07 & 5.87 & 18.04 & 5.95 & 18.02 & 6.03 & 17.99 & 6.11 & 19 \\ 19 & 18.07 & 5.87 & 18.04 & 5.95 & 18.02 & 6.68 & 18.97 & 6.35 & 18.94 & 6.43 & 20 \\ 22 & 20.92 & 6.80 & 20.89 & 6.89 & 20.86 & 6.98 & 20.83 & 7.07 & 22 \\ 22 & 22 & 2.87 & 7.71 & 24.77 & 75.2 & 27.6 & 7.62 & 22.73 & 7.71 & 24 \\ 22 & 20.92 & 6.80 & 20.89 & 6.89 & 20.86 & 6.98 & 20.83 & 7.07 & 22 \\ 22 & 22 & 5.87 & 7.33 & 23.74 & 7.83 & 23.71 & 7.93 & 23.67 & 8.04 & 25 \\ 24 & 22.83 & 8.24 & 5.65 & 8.77 & 26.55 & 8.88 & 26.51 & 9.00 & 26 \\ 27 & 5.68 & 8.65 & 26.59 & 8.77 & 26.55 & 8.88 & 26.51 & 9.00 & 26 \\ 27 & 5.68 & 8.65 & 26.59 & 8.77 & 26.55 & 8.88 & 26.51 & 9.00 & 26 \\ 23 & 27.58 & 8.96 & (27.54 & 9.08 & 27.50 & 9.20 & 27.46 & 9.32 & 23 \\ 32 & 30.43 & 9.69 & 30.39 & 10.02 & 30.35 & 10.57 & 30.30 & 10.29 & 32 \\ 33 & 31.38 & 10.20 & 31.34 & 10.33 & 31.29 & 10.47 & 31.25 & 10.61 & 33 \\ 34 & 32.94 & 9.58 & 9.39 & 10.2 & 30.55 & 0.57 & 30.30 & 10.29 & 32 \\ 33 & 31.38 & 10.20 & 31.34$		18 L	eg.	181	Deg.	181	Deg.	1841	Deg.	D
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	ist.	Lat.	Dep.	Lat.	Dep,	Lat.	Dep.	Lat.	Dep.	ist.
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$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	ŝ									ŝ
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					1.25	3.79	1.27	3.79		4
$\begin{array}{c c c c c c c c c c c c c c c c c c c $										
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$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		7.61					2.54			8
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$\begin{array}{c c c c c c c c c c c c c c c c c c c $										
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	12	11.41				11.38				
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	14	13.31								14
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	15	14.27	4.64	14.25	4.70	14.22	4.76	14.20	4.82	15
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	16	15.22		15.20						16
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	18	17.12								17
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$\begin{array}{c c c c c c c c c c c c c c c c c c c $	20	19.02	6.18	18.99	6.26	18.97	6.35	18.94	6.43	20
$\begin{array}{c c c c c c c c c c c c c c c c c c c $										21
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$\begin{array}{c c c c c c c c c c c c c c c c c c c $										24
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	25	23.78	7.73	23.74	7.83	23.71	7.93	23.67	8.04	25
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	26	24.73	8.03							26
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$\begin{array}{c c c c c c c c c c c c c c c c c c c $	30	28.53	9.27	28.49	9.39	28.45	9.52	28.41	9.64	30
$\begin{array}{c c c c c c c c c c c c c c c c c c c $			9.58	29.44	9.71					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						30.35	10.15			32
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			10.20							33
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	36	34.24	11.12	34.19	11.27	34.14	11.42		11.57	36
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	37	35.19	11.43							
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$										39
$\begin{array}{c} 4239.94 \\ 12.98 \\ 39.64 \\ 12.98 \\ 13.29 \\ 40.84 \\ 13.47 \\ 40.78 \\ 13.67 \\ 40.78 \\ 13.67 \\ 40.78 \\ 13.67 \\ 40.78 \\ 13.67 \\ 40.78 \\ 13.67 \\ 40.78 \\ 13.67 \\ 40.78 \\ 13.67 \\ 40.78 \\ 13.67 \\ 40.78 \\ 13.67 \\ 40.78 \\ 13.67 \\ 40.78 \\ 13.67 \\ 40.78 \\ 13.67 \\ 14.79 \\ 13.78 \\ 40.67 \\ 11.67 \\ 14.64 \\ 11.67 \\ 14.64 \\ 14.79 \\ 42.67 \\ 14.28 \\ 42.61 \\ 16.61 \\ 14.46 \\ 42.67 \\ 14.28 \\ 42.61 \\ 16.61 \\ 14.46 \\ 42.67 \\ 14.28 \\ 42.67 \\ 14.28 \\ 42.61 \\ 16.61 \\ 14.46 \\ 43.65 \\ 14.83 \\ 45.65 \\ 14.83 \\ 45.59 \\ 15.03 \\ 45.52 \\ 15.23 \\ 45.45 \\ 15.43 \\ 49 \\ 46.60 \\ 15.14 \\ 46.54 \\ 15.35 \\ 46.40 \\ 15.75 \\ 45.56 \\ 47.42 \\ 15.66 \\ 47.42 \\ 15.67 \\ 47.85 \\ 16.07 \\ 50 \\ 50 \\ 7.55 \\ 16.07 \\ 50 \\ 7.5 \\ 10.7$	40	38.04	12.36	37.99	12.53				12.86	40
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$										41
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				40.84	13.15			40.72	13.80	42 43
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	44	41.85	13.60	41.79	13.78	41.73	13.96	41.66	14.14	44
47 44.70 14.52 44.64 14.72 44.57 14.91 44.51 15.11 47 48 45.65 14.83 45.59 15.03 45.52 15.23 45.45 15.43 46 94 46.60 15.14 46.54 15.85 46.47 15.55 46.40 15.75 45 50 47.55 15.45 47.48 15.66 47.42 15.87 47.35 16.07 50 <u>50 17.55 15.45 47.48 15.66 47.42 15.87 47.35 16.07 50</u> <u>50 17.55 15.45 47.48 15.66 47.42 15.87 47.35 16.07 50</u>										
48 45.65 14.83 45.59 15.03 45.52 15.23 45.45 15.43 46 49 46.60 15.14 46.54 15.35 46.47 15.55 46.40 15.75 45 50 47.55 15.45 47.48 15.66 47.42 15.87 47.35 16.07 50 Dep. Lat. Dep. Lat. Dep. Lat.										40
50 47.55 15.45 47.48 15.66 47.42 15.87 47.35 16.07 50	48	45.65	14.83	45.59	15.03	45.52	15.23	45.45	15.43	48
Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat.										49 50
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E	18 [)eg.	181	Deg.	181	Deg.	$18\frac{3}{4}$	Deg.	D
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	st.
		15.76		15.97		16.18		16.39	51
52 53	49.45	16.07 16.38		16.28		16.50 16.82	49.24	16.71 17.04	52 53
54	51.36	16.69	51.28	16.91	51.21	17.13	51.13	17.36	54
		17.00 17.30		17.22 17.54		17.45 17.77		17.68	55
	54.21			17.85	54.05	18.09	53.98	18.32	57
		17.92		18.16		18.40 18.72		18.64	- 58
		18.23 18.54		18.48 18.79	56,90	19.04		19.29	59 60
61	58.01	18.85	57.93	19.10	57.85	19.36		19.61	61
		19.16		19.42		19.67		19.93	62 63
	59.92	19.47		19.73 20.04		19.99 20.31		20.25 20.57	64
65	61.82	20.09	61.73	20.36	61.64	20.62	61.55	20.89	
66	62.77	20.40 20.70		20.67 20.98		20.94 21.26	62.50	21.22 21.54	66
	64.67			20.98		21.58	64.39	21.86	68
69	65.62	21.32		21.61	65.43	21.89	65.34	22.18	69
70	66.57	21.63	66.48	21.92	66.38	22.21	66.29	22.50	70
		21.94		22.23		22.53		22.82	
	68.48	22.25		22.55		22.85 23.16		23.14 23.47	
	70.38			22.86 23.17	70.18	23.48		23.79	74
75	71.33	23.18	71.23	23.49	71.12	23.80	71.02	24.11	75
	72.28	23.49 23.79		23.80 24.11		24.12 24.43		24.43 24.75	
		23.19		24.11		24.45		25.07	78
79	75.13	24.41	75.03	24.74	74.92	25.07	74.81	25.39	79
80	76.08	24.72	75.98	25.05	75.87	25.38	75.75	25.72	80
81	77.04	25.03		25.97	76.81	25.70	76.70	26.04	
82	77.99	25.34		25.68	77.76	26.02	77.65	26.36 26.68	82 83
	78.94			25.99		26.34 26.65		20.08	84
	80.84		80.72	26.62		26.97	80.49	27.32	85
		26.58		26.93		27.29	81.44		86
	82.74	26.88 27.19	82.62 83,57			27.61 27.92		27.97 28.29	87 88
89	84.64	27.50	84.52	27.87		28.24		28.61	89
	85.60		85.47			28.56		28.93	90
	86.55		86.42			28.87		29.25	91
	87.50 88.45		87.37 88.32		87.25	29.19		29.57 29.89	92 93
94	89.40	29.05		29.44		29.83	89.01	30.22	94
95	90.35	29.36	90.22	29.75	90.09	30.14	89.96	30.54	95
96	91.30 92.25	29.67		30.06	91.04 91.99	30.46	90.91	30.86	96 97
98	93.20	30.28	93.07		92.94	31.10	92.80	31.18 31.50	98
99	94.15	30.59	94.02	31.00	93.88	31.41	93.75	31.82	99
100		30.90			94.83			32.14	
ist.	Dep.	Lat. Deg.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
A	72	Deg.	713]	Deg.	711	Deg.	7111	Deg.	Ā

D	19 1	Deg.	1941	Deg.	191	Deg.	1931	Deg.	E
st.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1	0.95	0.33	0.94	0.33	0.94	0.33	0.94	0.34	7 1
23	1.89 2.84	0.65	1.89	0.66	1.89	0.67	1.88	0.68	23
4	3.78	1.30		1.32	3.77	1.34	3.76	1.35	4
5	4.73	1.63	3.78 4.72	1.65	4.71	1.67	4.71	1.69	* 5
6	5.67	$1.95 \\ 2.28$	5.66 6.61	1.98 2.31	5.66	2.00 2.34	5.65	2.03	6 7
8	7.56	2.60	7.55	2.64	7.54	2.67	7.53	2.70	8
. 9	8.51	2.93	8.50	2.97	8.48	3.00	8.47	3.04	9
10	9.46	3.26	9.44	3.30	9.43	3.34	9.41	3.38	10
	10.40	3.58	10.38	3.63	10.37	3.67	10.35	3.72	11
	11.35 12.29	3.91 4.23	11.33	3.96	11.31	4.01	11.29	4.06	12 13
	12.29	4.23	$12.27 \\ 13.22$	4.29 4.62	12.25 13.20	4.34 4.67	12.24 13.18	4.39 4.73	13
15	14.18	4.88	14.16	4.95	14.14	5.01	14.12	5.07	15
	15.13	5.21	15.11	5.28	15.08	5.34	15.06	5.41	16 17
	16.07 17.02	5.86	16.05 16.99	5.60 5.93	16.02 16.97	5.67	16.00 16.94	5.74	18
19	17.96	6.19	17.94	6.26	17.91	6.34	17.88	6.42	19
20	18.91	6.51	18.88	6.59	18.85	6.68	18.82	6.76	20
21	19.86	6.84	19.83	6.92	19.80	7.01	19.76	7.10	21
22	20.80	7.16	20.77	7.25	20.74	7.34	20.71	7.43	22
	21.75 22.69	7.49	21.71	7.58 7.91	21.68 22.62	7.68	21.65	7.77	23 24
	22.69	8.14	22.66 23.60	8.24	23.57	8.01 8.35	22.59 23.53	8.11 8.45	25
26	24.58	8.46	24.55	8.57	24.51	8.68	24.47	8.79	26
	25.53	8.79 9.12	25.49	8.90 9.23	25.45 26.39	9.01	25.41 26.35	9.12	27 28
	$26.47 \\ 27.42$	9.12	26.43 27.38		20.39	9.35	20.35	9.46	29
	28.37	9.77	28.32	9.89	28.28		28.24		30
			29.27		29.22	10.35		10.48	31
		10.42		10.55		10.68		10.81	82 33
	32.15	10.74		10.88		11.02		11.15	34
35	33.09	11.39	33.04	11.54	32.99	11.68	32.94	11.83	35
		11.72		11.87		12.02		12.17	36
		12.05	34.93	12.20		12.35 12.68		12.50 12.84	38
39	36.88	12.70	36.82	12.86	36.76	13.02	36.71	13.18	39
40	37.82	13.02	37.76	13,19	37.71	13.35	37.65	13.52	40
	38.77			13.52		13.69		13.85	41
	39.71	13.67		13.85 14.18		14.02 14.35		14.19	43
44	41.60	14.32		14.51		14.69	41.41	14.87	44
45	42.55	14.65	42.48	14.84	42.42	15.02	42.35	15.21	45
		14.98 15.30		15.17 15.50		15.36		15.54	46
		15.63		15.83		16.02		16.22	48
49	46.33	15.95	46.26	16.15	46.19	16.36	46.12	16.56	49
50	47.28	16.28	47.20	16.48	47.13	16.69	47.06	16.90	50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
ā	71	Deg.	703	Deg.	701	Deg.	701]	Deg.	Ā

E	19	Deg.	191	Deg.	191	Deg.	193	Deg.	H
ist.	Lat.	Dep.	Lat.	Dep.	Lat:	Dep.	Lat.	Dep.	list.
		16.60		16.81	48.07	17.02		17.23	51
52 53	49.17	16.93		17.14		17.36		17.57	52 53
54	51.06	17.58	50.98	17.80	50.90	18.03	50.82	18.25	54
50 56	52.00 52.95	17.91	51.92 52.87	18.13 18.46		18.36		18.59 18.92	55 56
57	53.89	18.56	53.81	18.79	53.73	19.03	53.65	19.26	57
59	54.84 55.79	18.88 19.21	54.76 55.70		54.67	19.36		19.60	58 59
60	56.73	19.53	56.65	19.78	56.56	20.03	56.47	20.27	60
61	57.68	19.86	57.59			20.36		20.61	61
62 63	58.62 59.57	20.19 20.51	58.53	20.44 20.77		20.70 21.03	59.29	20.95 21.29	62 63
64	60.51	20.84	60.42	21.10	60.33	21.36	60.24	21.63	64
65 66	61.46	21.16 21.49	61.37 62.31		61.27	21.70 22.03		21.96	65 66
67	63.35	21.81	63.25			22.37		22.64	67
		$22.14 \\ 22.46$	64.20	22.42 22.75		22.70 23.03	64.00	22.98 23.32	68 69
70	66.19	22.79		23.08		23.03	65.88	23.65	70
71	67 19	23.12	67.03	03 11	66 99	23.70	66 89	23.99	71
72	68.08	23.44	67.97	23.74	67.87	24:03	67.76	24.33	72
73 74	69.02 69.97	23.77	68.92	24.07 24.40		24.37 24.70	68.71	24.67	73
75	70.91	24.42	70.81			25.04	70.59	25.34	75
76	71.86	24.74 25.07		$25.06 \\ 25.39$		25.37		25.68	76
78	73.75	25.39		25.72		25.70		26.02	78
		25.72 26.05	74.58	26.05 26.39		26.37	74.35	26.70	
F								_	-
		26.37 26.70		26.70 27.03		27.04 27.37		27.37	81 82
83	78.48	27.02	78.36	27.36		27.71	78.12	28.05	83
84 85	79.42	27.35	79.30 80.25			28.04 28.37	79.06	28.39	84
86	81.31	27.67 28.00 28.32	81.19	28.35		28.71	80.94	29.06	85
87	82.26	28.32 28.65	82.14	28.68 29.01		29.04 29.37	81.88	29.40 29.74	87
89	84.15	28.98		29.34		29.57	83.76	30.07	88
90	85.10	29.30	84.97	29.67	84.84	30.04	84.71	30.41	90
91	86.04	29.63 29.95		30.00		30.38	85.65	30.75	91
92 93	86.99	29.95 30.28		30.33 30.66		30.71 31.04	86.59	31.09	92
94	88.88	30.60	88.74	30.99	88.61	31.38	88.47	31.76	93 94
95 96	89.82	30.93 31.25	89.69	31.32 31.65	89.55	31.71 32.05	89.41	32.10	95
97	91.72	31.58	91.58	31.98	91.44	32.38	91.29	32.78	96 97
98 99	92.66	31.91 32.23	92.52	32.31 32.64	92.38	32.71 33.05	92.24	33.12	98
100	94.55	32.25	94.41	32.97	94.26	33.38	94.12	33.45 33.79	99 100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	t.
Dis	71	Deg.	703	Der	701	Dog	-	-	Dis
1	11	Deg,	4	reg.	102	Deg.	104	Deg.	-

D	20]	Deg.	$20\frac{1}{4}$	Deg.	$20\frac{1}{2}$	Deg.	203	Deg.	E
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
.1	0.94		0.94		0.94	0.35	0.94	0.35	1
3	2.82	1.03	2.81	1.04	2.81	1.05	2.81	1.06	23
45	3.76 4.70		3.75	1.38 1.73	3.75		3.74	1.42	45
6	. 5.64	2.05	5.63	2.08	5.62	2.10	5.61	2.13	6
78	6.58	2.39	6.57 7.51	2.42 2.77	6.56		6.55	2.48	
9	8.46	3.08	8.44	3.12	8.43	3.15	7.48	3.19	
10	9.40	3.42	9.38	3.46	9.37	-3.50	9.35	3.54	10
	10.34	3.76	10.32	3.81	10.30		10.29	3.90	11
	11.28 12.22	4.10	11.26 12.20	4.15 4.50	$11.24 \\ 12.18$	4.20	11.22 12.16	4.25	12 13
14	13.16	4.79	13.13	4.85	13.11	4.90	13.09	4.96	14
	14.10 15.04	5.13	14.07	5.19	14.05	5.25	14.03	5.31 5.67	15
17	15.97	5.81	15.95	5.88	15.92	5.95	15.90	6.02	17
	16.91	6.16 6.50	16.89	6.23 6.58	16.86	6.30	16.83	6.38	18
	17.85 18.79	6.84	17.83 18.76	6.92	17.80 18.73	6.65 7.00	17.77 18.70	6.73 7.09	19 20
21	19.73	7.18	19.70	7.27	19.67	7.35	19.64	7.44	21
22	20.67	7.52	20.64		20.61	7.70	20.57	7.79	22
	21.61 22.55	7.87 8.21	21.58 22.52	7.96	21.54 22.48	8.05	21.51 22.44	8.15 8.50	23 24
25	23.49	8.55	23.45	8.65	23.42	8.76	23.38	8.86	25
	24.43	8.89	24.39	9.00	24.35		24.31	9.21	26
	25.37 26.31	9.23	25.33	9.35 9.69	25.29 26.23	9.46	25.25 26.18	9.57 9.92	27 28
	27.25	9.92		10.04	27.16	10.16	27.12	10.27	29
30	26.10	10.96	98.15		28.10		28.05	10.63	30
	29.13 30.07			10.73	29.04 29.97		28.99		31
	31.01			11.42	29.97	11.21	29.92 30.86		32 33
34	31.95	11.63	31.90	11.77	31.85	11.91	31.79	12.05	34
	32.89 33.83			12.11 12.46	32.78 33.72	12.26	32.73 33.66	12.40	35 36
37 :	34.77	12.65	\$4.71	12.81	34.66	12.96	34.60	13.11	37
	35.71 36.65		35,65		35.59 36.53		35.54 36.47		38
	37.59		37.53		37.47		37.41		39 40
	38.53		38.47		38.40	14.36	38.34		41
	39.47 40.41		39.40 40.34	14.54	$39.34 \\ 40.28$		39.28 40.21		42 43
44	40.41	15.05	41.28	15.23	41.21	15.41	40.21		43
45	42.29	15.39	42.22		42.15		42.08	15.94	45
40	43.23 44.17	16.07	44.09	15.92 16.27	44.02	16.46	43.02 43.95		46
	44.17 45.11		45.03	16.61	44.96	16.81	44.89	17.01	48
	46.04 46.98			16.96 17.31			45.82 46.76		49 50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	ŝt.
A	70 I	Deg.	69 ³ ₄ I	Deg.	$69\frac{1}{2}$	Deg.	691I)eg.	Dis.

	20 L)eg.	201	Deg.	201	Deg.	203	Deg.	
5						10			Dis
st.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	st.
51		17.44		17.65		17.86		18.07	51
52		17.79		18.00		18.21		18.42	52 53
	49.80			18.34		18.56 18.91		18.78 19.13	54
	51.68		51.60	19.04		19.26		19.49	55
56	52.62	19.15	52.54		52.45	19.61	52.37		56
	53.56			19.73		19.96 20.31	53.30		57 58
	54.50 55.44		54.42 55.35	20.07		20.66	54.24 55.17	20.55 20.90	59
	56.38		56.29			21.01	56.11	21.26	60
61	57.32	20.86	57.23	21.11	57.14		57.04		61
62	58.26	21.21		21.46			57.98		62
63	59.20 60.14	21.55	59.11 60.04			22.06	58.91	22.32 22.67	63 64
65	61.08	22.23		22.50			60.78		65
66	62.02	22.57	61.92	22.84	61.82	23.11	61.72	23.38	66
	62.96		62.86			23.46	62.65	23.74	67
	63.90 64.84		63.80	23.54		23.81 24.16		24.09 24.45	68 69
	65.78			24.23		24.51		24.80	70
71	66.72	24.28	66.61	24.57	66.50	24.86	66.39	25.15	71
72	67.66	24.63	67.55		67.44		67.33	25.51	72
	68.60		68.49		68.38			25.86	73
74	69.54	25.31	69.43 70.36			25.92	69.20	26.22 26.57	74
76	70.48 71.42	25.99		26.30		26.62		26.93	76
77	72.36	26.34	72.24	26.65	72.12	26.97		27.28	77
	73.30		73.18	27.00		27.32		27.63	78
	74.24 75.18			27.34 27.69		27.67 28.02		27.99 28.34	79 80
81	76.12	07 70	75 00	28.04	75.07	28.37		28.70	
82	77.05			28.38		28.72		29.05	81 82
83	77.99	28.39	77.87	28.73	77.74	29.07	77.62	29.41	83
	78.93			29.07		29.42		29.76	84
	79.87 80.81		79.75			29.77 30.12		30.11 30.47	85 86
87	81.75	29.76	81.62			30.47	81.36	30.82	87
			82.56	30.46	82.43	30.82	82.29	31.18	88
	$83.63 \\ 84.57$		83.50 84.44			31.17 31.52		31.53	89
							84.16		90.
	85.51			31.50		31.87	85.10		91
92 93	86.45 87.39	31.81	86.31 87.25			32.22 32.57		32.59 32.95	92 93
	88.33		88.19	32.54	88.05	32.92	87.90		94
95	89.27	32.49	89.13	32.88	88.98		88.84	33.66	95
	90.21 91.15		90.07 91.00	33.23	89.92 90.86		89.77		96
	91.15 92.09		91.90		91.79		90.71 91.64		97 98
99	93.03	33.86	92.88	34.27	92.73	34.67	91.64 92.58	35.07	99
100	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	100
ist.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	ist.
A	70 I	Deg.	69 ₄ 1	Deg.	$69\frac{1}{2}$	Deg.	69 <u>1</u>	Deg.	A

U	21	Deg.	214	Deg.	$21\frac{1}{2}$	Deg.	213	Deg.	U
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1	0.93	0.36	0.93	0.36	0.93	0.37	0.93	0.37	31
23	2.80	1.08	2.80	1.09	2.79	1.10	1.86	1.11	23
45	3.73	1.43 1.79	3.73 4.66	1.45	3.72	1.47	3.72	1.48	4
67	5.60	2.15	5.59 6.52	2.17	5.58 6.51	2.20	5.57		6 7
8	7.47	2.87	7.46	2.90	7.44	2.93	7.43	2.96	8
9 10	8.40 9.34	3.23 3.58	8.39 9.32	3.26 3.62	8.37 9.30	3.30 .3.67	8.36 9.29	3.34 3.71	9 10
	10.27		10.25	3.99	10.23	4.03	10.22	4.08	11
13	$11.20 \\ 12.14$	4.66	11.18	4.35 4.71	11.17 12.10	4.40 4.76	$11.15 \\ 12.07$	4.45	12 13
	13.07 14.00	5.02	13.05	5.07	13.03	5.13 5.50	13.00 13.93		14 15
16	14.94	5.73	14.91	5.80	14.89	5.86	14.86	5.93	16
	15,87 16.80	6.09 6.45	15.84 16.78		15.82	6.23 6.60	15.79 16.72	6.30 6.67	17 18
19	17.74 18.67				17.68	6.96 7.33	17.65		19 20
			10,04	-1.20	10.01	1.55	10.00	1.41	40
21	19.61 20.54	7.53 7.88	19.57 20.50		19.54 20.47	7.70 8.06	19.50 20.43	7.78	21 22
23	21.47	8.24	21.44	8.34	21.40	8.43	21.36	8.52	23
	22.41 23.34	8,60 8,96	22.37 23.30	8.70 9.06	22.33 23.26	8,80 9,16	22.29	8.89 9.26	24
26	24.27	9.32	24.23	9.42	24.19	9.53	23.22 24.15		26
	25.21 26.14		25,16 26.10	9.79	25.12 26.05	9.90 10.26		10.01 10.38	27 28
29	27.07	10.39	27.03	10.51	26.98	10.63	26.94	10.75	29
30	28.01	10.75	27.96	10.87	27.91	11.00	27.86	11.12	30
	28.94		28.89		28.84			11.49	31
32	29.87 30.81	11.47	29.82	11.60	29.77 30.70	$11.73 \\ 12.09$	29.72	11.86	32
34	30.81 31.74	12.18	30.76 31.69		31.63	12.46		$12.23 \\ 12.60$	
35	32.68 33.61	12.54	32.62 33.55		32.56 33.50	12.83		12.97	35
37	34.54	13.26	34.48	13.41	34.43	13.56	34.37	13.71 14.08	37
	35.48 36.41		35.42 36.35		35.36 36.29		35.29 36.22	14.08 14.45	38 39
40	37.34	14.33	37.28	14.50	37.22			14.82	40
41	38.28 39.21	14.69		14.86 15.22	38.15	15.03	38.08	15.19 15.56	41
43	40.14	15.41	40.08	15.58		15.39 15.76	39.94	15.93	43
	41.08 42.01		41.01 41.94		40.94 41.87		41.80	16.30 16.68	44 45
46	42.94	16.48	42.87	16.67	42.80	16.86	42.73	17.05	46
	43.88 44.81	16.84		17.03	43.73 44.66	17.23	43.65	17.42	47
49	45.75	17.56	45.67	$17.40 \\ 17.76$	45.59	17.96	45.51	18.16	49
		17.92	46.60	18.12	46.52	18.33	46.44	18.53	50
st.		Lat.				Lat.		_	ist.
â	69	Deg.	683	Deg.	681	Deg.	681	Deg.	Q

D	21	Deg.	21 <u>4</u> E) eg.	$21\frac{1}{2}$	Deg.	214	Deg.	D
Ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.		Dep.	Dist.
51	47.61	18.28	47.53	18.48	47.45	18.69 19.06 19.42	47.37	18.90	5
52	48.55	18.64	48.46	18.85	48.38	19.06	48.30	19.27	59
		18.99 19.35	49.40	19.21	49.31	19.42	49.23	19.64 20.01	5
55	51.35	19.71	51 96	10 03	51 17	20.16		20.38	5
56	52.28	19.71 20.07	52.19	20.30	52.10	20.52	52.01	20.75	5
57	58.21	20.43	53.12	20.66	53.03	20.89	52.94	21.12	5
83	54.15	20.79	54.06	21.02	53.90	21.26		21.49 21.86	55
59 60,	56.01	21.14 21.50		21.38	55.83	21.99	55.73	22.23	6 0
61	56.95	21.86	56.85	22.11	56.76	22.36	56.66	22.60	6
62	57.88	22.22	57.78	00 17	167 60	00 70		22.97	6
63	58.82	22.58	58.72	22.47	58.62	23.09		23.35	6
		22.94		23.20 23.56	59.55 60.48			23.72	6
		23.29 23.65		23.92		24.19		24.09	
67	62.55	24.01	62.44	24.28	62.34	24.56	62.23	24.83	6
68	63.48	24.37	63.38	24.65	63.27	24.92	63.16	25.20	6
		24.73		25.01		25.29		25.57 25.94	
-									-
		25.44 25.80	67 10	25.13	66 99	26.02 26.39	66 87	26.31	
		26.16		26.46		26.75		27.05	2
74	69.08	26.52	68.97	26.82		27.12	68.73	27.42	17
		26.88	69.90	27.18	69.78	27.49	69.66	\$ 27.79	17
76	70.95	27.24		27.55		27.85		28.16	
		27.59	71.76	27.91 28.27		28.22		28.53	
		28.31		28.63		28.95		5 28.90 3 29.27	
		28.67		29.00		29.32	74.30	29.64	8
		29.03		29.36		29.69		3 30.02	
82	76.55	29.39		29.72		30.05		3 30.39	
84	77.49	29.74		30.08		30.42		30.76	8
85	79.35	30.46		30.44		\$0.79 31.15		231.13	
86	80.29	30.82		31.17		31.52		331.87	
87	81.22	31.18	81.08	31.53	80.95	31.89	80.81	1 32.24	8
88	82.16	31.54		31.89		32.25		1 32,61	8
		31.89 32.25		32.26 32.62		32.62 32.99		32.98 33.35	
91	84.96	32.61	84.81	32.98	84.67	33.35	84.59	2 33.72	-
		32.97				33.72		5 34.09	
93	86.82	\$3.33	86.68	33.71	86.53	\$4.08	86.38	34.46	9
		33.69	87.61	34.07	87.46	34.45		34.83	
		34.04 34.40		34.43		34.82		135.20	
		34.76				35.55		35.57	
98	91.49	35.12	91.34	35.52	91.18	35.92		36.31	9
		35.48	92.27	35.88	92.11 93.04	36.28 36.65	91.95	36.69	9
						-		_	
Dis	69	Lat. Deg.	683	Deg	681	Der	681	Der	Dist
	00	Jeg.	1.004	Deg.	6	Deg.	004	Deg.	

D	22 1	Deg.	221	Deg.	221	Deg.	223	Deg.	E
st.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1	0.93	0.37 0.75	0.93	0.38	0.92	0.38	0.92	0.39	1
3	2.78	1.12	2.78	1.14	2.77	1.15	2.77	1.16	3
45	3.71	1.50	3.70	1.51	3.70	1.53	3.69	1.55	4
6	4.64	1.87	4.63	1.89 2.27	4.62	1.91	4.61	1.93	56
7	6.49	2.62	6.48	2.65	6.47	2.68	6.46	2.71	7
8 9	7.42 8.34	3.00	7.40	3.03	7.39	3.06	7.38		8
10	9.27	3.37	9.26	3.41 3.79	8.31 9.24	3.44	8.30 9.22	3.48 3.87	9 10
11	10.20	4.12	10.18	4.17	10.16		10.14		11
	11.13 12.05	4.50	11.11		11.09		11.07		12
13		4.87	12.03	4.92 5.30	12.01 12.93	4.97	11.99 12.91	5.03	13 14
15	13.91	5.62	13.88	5.68	13.86	5.74	13.83	5.80	15
	14.83	5.99	14.81	6.06	14.78	6.12	14.76		16
17 18		6.37 6.74	15.73 16.66	6.44 6.82	15.71 16.63	6.51	15.68		17 18
	17.62	7.12	17.59	7.19	17.55	7.27	17.52		19
20	18.54	7.49	18.51	7.57	18.48	7.65	18.44		20
	19.47	7.87	19.44	7.95	19.40		19.37		21
	20.40 21.33	8.24 8.62	20.36 21.29	8.33 8.71	20.33 21.25	8.42	20.29 21.21	8.51	22 23
24	22.25	8.99	22.21	9.09	22.17	9.18	22.13		24
25	23.18	9.37	23.14	.9.47	23.10		23.05		25
20	24.11 25.03	9.74	24.06	9.84	24.02			10.05	26
28	25.96	10.49	25.92			10.33		10.44	28
29	26.89	10.86	26.84	10.98	26.79	11.10	26.74	11.21	.29
	27.82		27.77	11.36	27.72	11.48	27.67	11.60	30
31	28.74	11.61	28.69	11.74		11.86		11.99	31
32	29.67	11.99	29.62			12.25		12.37	
1 34	30.60 31.52	10 74	30.54 31.47			12.63 13.01		12.76	
35	32.45	13.11	32.39	13.25		13.39		13.53	
1 .00	West 198	10 10		13.63		13.78		13.92	
	34.31 35.23	1.01	34.24 35.17	14.01	34.18	14.16	34.12	14.31	37
39	36.16	14.61		14.39	36.03	14.92	35.97	15.08	39
40	37.09	14.98	37.02	15.15	36.96	15.31	36.89	15.47	40
-41	38.01	15.36		15.52		15.69		15.86	
42	38.94	15.78 16.11	38.87	15.90	38.80	16.07	38.73	16.24	42
44	39.87	16.11		16.28	39.73 40.65			16.63	
45	41.72	16.86	41.65	17.04	41.57	17.22	41.50	17.40	45
40	42.65	17.23		17.42	42.50		42.42	17.79	46
-48	43.58	17.61	43.50	17.80	43,42	17.99		18.18	
49	45.43	18.36	45.35	18.55	45.27	18.75	45.19	18.95	49
50	46.36	18.73	46.28	18.93		19.13		19.34	
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	ist.
þ	68	Deg.	673	Deg.	671	Deg.	671	Deg.	a

022	5 .	Deg.	221	Deg.	221	Deg.	223	Deg,	H
ist.	at.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
		19.10		19.31		19.52		19.72	
52 48. 53 49.			49.05	19.69 20.07	48.97	19.90 20.28	48.88	20.11 20.50	
54 50. 55 51.			49.98	20.45	49.89	20.66 21.05		20.88	54
56 51.				20.83 21.20		21.05	50.72 51.64	21.27	
57 52.	85	21.35	52.76	21.58		21.81		22.04	
58 53. 59 54	76	21.73	53.68	21.96		22.20 22.58		22.43	
60 55			55.53	22.72	55.43	22.96	55.33	23.20	
61 56	56	22.85	56.47			23.34		23.59	
62 57.		23.23 23.60	57.38 58.31			23.73 24.11		23.98	
64 59.	34	23.97	59.23	24.23	59.13	24.49	59.02	24.75	64
65 60. 66 61.	27	24.35	60.16			24.87 25.26		25.14	
67 62.	12	25.10	62.01	24.99 25.37		25.64	61.79	25.52	
68 63.	.05	25.47	62.94			26.02	62.71	26.30	68
69.63. 70.64				26.13		26.41 26.79	63.63 64.55	26.68	
	-								_
71 65.				26.88		27.17	65.48	27.46	
72 66, 73 67.				27.26		27.55 27.94	66.40 67.32	27.84	
74 68.				28.02	68.37	28.32	68.24	28.62	74
75 69.				28.40 28.78		28.70	69.17 70.09		
		28.84		29.16		29.00	71.01	29.39	
78 72.	.32	29.22	72.19	29.53	72.06	29.85	71.93	30.16	78
79 73. 80 74.	25	29.59		29.91 30.29		30.23 30.61	72.85	30.55	
	-								
81 75.		30.34	75.89	30.67		31.00 31.38	74.70	31.32 31.71	
83 76.	96	31.09	76.82	31.43	76.68	\$1.76		32.10	89
84 77.	88	31.47	77.75	31.81 32.19	77.61	32.15 32.53	77.46		
86 79.			79.60			32.91		32.87	
87 80.	.66	32.59	80.52	32.94	80.38	33.29	80.23	33,64	87
88 SI. 89 82			81.45			33.68 34.06		34.03	
90 83			83.30			34.44	83.00		
		34.09		34.46		34.82	83.92		
		34.46 34.84	85.15	34.84 35.21		35.21 35.59		35.58 35.96	
94 87	.16	35.21	87.00	35.59	86.84	35.97	86.69	36.35	94
95 88	.08	35.53	87.93 88.85	35.97	87.77	36.35		36.74	
		35.96 36. 3 4	89.78	36.73		36.74 37.12	88.53	37.12 37.51	96
98 90	86	36.71	90.70	37.11	90.54	37.50	90.38	37.90	. 98
99 91 100 92		37.09 37.46	91.63 92.55			37.89 38.27	91.30 92.22		99 100
		Lat.	Dep.			Lat.			
- 12,		Deg.							Dis

-	23	Deg.	234	Deg.	231	Deg.	233]	Deg.	-
)ist.		Dep.			Lat.			Dep.	Dist.
1		0.39	0.92	0.39	0.92	0.40	0.92	0.40	1
23	1.84	0.78	1.84	0.79 1.18	1.93	0.80	1.83	0.81	2 3
4	3.68	1.56	3.68	1.58	3.67	1.59	3.66	1.61	4
5	4.60	1.95 2.84	4.59	1.97 2.37	4.59	1.99 2.39	4.58	2.01	56
7	6.44	2.74	6.43	2.76	6.42	2.79	6.41	2.82	7
89	7.36	3.13	7.35	3.16 3.55	7.34	3.19	7.32	3.22	89
10	9.20		9.19	3.95	9.17	3.99	9.15	4.03	10
	10.13	4.30	10.11	4.34	10.09	4.39			
	11.97	4.69	11.03	4.74 5.13	11.00	4.78	10.98	4.83	12
14	12.89	5.47	12.86	5.53	12.84	5.58	12.81	5.64	14
	13.81 14.73	5.86	13.78 14.70	5.92 6.32	13.76	5.98	13.73	6.04	15
17	15.65	6.64	15.62	6.71	15.59	6.78	15.56	6.85	17
	16.57 17.49	7.03	16.54 17.46	7.11 7.50	16.51 17.42	7.18	16.48	7.25	18 19
	18.41	7.81	18.38		18.34	7.97	18.31	8.05	20
	19.33	8.21	19.29	8.29	19.26	8.37	19.22	8.46	21
	20.25 21.17	8.60 8.99	20.21 21.13	8.68 9.08	20.18 21.09	8.77 9.17	20.14 21.05	8.86	22 23
24	22.09	9.38	22.05	9.47	22.01	9.57	21.97	9.67	24
	23.01 23.93	9.77	22.97 23.89	9.87	22.93 23.84	9.97	22.88		25
	24.85		24.81		24.76			10.47 10.87	27
	25.77 26.69		25.73			11.16	25.63	11.28	28
	20.65		26.64 27.56		26.59 27.51	11.56 11.96		11.68 12.08	29 30
	28.54		28.48		28.43	12.36	28.37	12.49	31
	29.46 30.38		29.40 30.32		29.35 30.26	12.76		12.89 13.29	32
33	31.30	13.28	31.24		31.18		31.12	13.69	34
	32.22		32.16			13.96	32.04	14.10	35
	33.14 34.06	14.07	33.08 34.00		33.93	14.35	32.95	14.50 14.90	36 37
38	34.98	14.85	34.91		34.85	15.15	33.87 34.78		38
	35.90 36.82		35.83 36.75		35.77 36.68			15.71 16.11	39 40
41	37.74	16.02	37.67	16.18	37.60		37.53	16.51	41
	38.66			16.58		16.75	38.44	16.92	42
			39.51 40.43		\$9.43 40.35	17.15	39.36 40.27	17.32	43 44
45	41.42	17.58	41.35	17.76	41.27	17.94	41.19	18.12	45
	42.34 43.26	17.97 18.36	42.26	18.16	42.18 43.10	18.34	42.10 43.02		46
.48	44.18	18.76	44.10	18.95	44.02	19.14	43.93	19.33	48
	45.10 46.03		45.02 45.94		44.94 45.85		44.85 45.77		49 50
t	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	÷
Dis	67	Deg.	663	Deg.	661	Deg.	6611	Jeg.	ä

-	23	Deg.	234	Deg.	231	Deg.	233]	Deg.	
Dist.		Dep.		Dep.		Dep.		Dep.)ist.
	46.95	10.02	16 86	20.13	48 77	20.34	46.68	20 54	51
51 52	40.95	20.32		20.13		20.34	47.60	20.94	52
53	48.79	20.71	48.70	20.92	48.60	21.13	48.51	21.35	53
	49.71		49.61	$21.32 \\ 21.71$		21.53		21.75 22.15	54
	50.63 51.55			22.11		21.93 22.33		22.55	55 56
57	52.47	22.27	52.37	22.50		22.73	52.17	22.96	57
	53.39			22.90		23.13		23.36	58
	54.31 55.23			23.29 23.68		23.53 23.92		23.76 24.16	59 60
							111		
	56.15			24.08		24.32		24.57	61
	57.07			24.47		24.72 25.12		24.97 25.37	62
	57.99 58.91			25.26		25.12		25.78	63 64
65	59.83	25.40	59.72	25.66	59.61	25.92	59.50	26.18	65
	60.75			26.05		26.32		26.58	66
	61.67 62.59			$26.45 \\ 26.84$	62 36	26.72		27.39	67 68
69	63.51	26.96		27.24	63.28	27.51	63.16	27.79	69
70	64.44	27.35	64.32	27.63	64.19	27.91	64.07	28.19	70
71	65 96	27.74	65 99	28.03	65 11	28.31	64 00	28.59	71
		28.13		28.42		28.51		29.00	72
73	67.20	28.52	67.07	28.82		29.11	66.82	29.40	73
74	68.12	28.91		29.21		29.51	67.73	29.80	74
		29.30 29.70		29.61		29.91 30.30		30.21	75
77	70.88	30.09		30.40		30.70		31.01	77
	71.80	30.48		30.79	71.53	31.10	71.39	31.41	78
		30.87 31.26		31.18 31.58		31.50 31.90		31.82 32.22	79 80
	10.04				13.50	51.80			
		31.65		31.97		32.30		1 32.62	81
82		32.04		32.37		32.70		33.03	82
		32.43 32.82	77.18	32.76 33.16		83.10		1 33.4 3) 3 3.83	83 84
	78.24	33.21	78.10	33.55		5 33.89	77.80	34.23	85
86	79.16	33.60		33.95		34.29		2 34.64	86
		33.99 34.38		34.34 34.74		334.69 35.09		3'35.04 5'35.44	87
		34.78		35.13		35.49			89
90	82.85	35.17	82.69	35.53	82.54	35.89	82.38	35.84 36.25	90
01	09 7	25 50	89.6	35.92	02 4	00 00	00 00	20 0	01
		35.56	84.5	35.92		5 36.29 7 36.68		36.65 37.05	91 92
93	85.61	36.34	85.4	36.71	85.29	37.08	85.1	2 37.46	93
94	86.53	36.73	86.3	37.11	86.20	37.48	86.04	1 37.86	
95 96	87.45	37.12	88.2	37.50		237.88 138.28		5 38.26 7 38.66	95 96
		37.90	89.1	2 38.29	88.9	38.68	88.7	39.07	
98	90.21	38.29	90.0	138.68	89.8	39.08	89.70	39.47	98
		38.68		5 39.08 3 39.47		39.48		2 39.87	99 100
1							-		100
4	Dep	Lat.	Dep	. Lat.	Dep	Lat.	Dep	Lat.	نه
is:									is
P	67	Deg.	"66 ₁	Deg.	66	Deg.	661	Deg.	P
-		-	-		1.07	-		-	in succession.

IE	24	Deg.	$ 24\frac{1}{4} $	Deg.	241	Deg.	244	Deg.	19
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1		0.41 0.81	0.91	0.41 0.82	0.91	0.41 0.83	0.91		
3	2.74	1.22	2.74	1.23	2.73	1.24	2.72	1.26	3
4		1.63		1.64	3.64		3.63		
5			5.47	2.05	4.55		4.54	2.09	56
1 7	6.39	2.85	6.38	2.87	6.37	2.90	6.36	2.93	7
8		3.25	7.29	3.29 3.70	7.28		7.27		
10			9.12	4.11	8.19 9.10		8.17 9.08	3.77 4.19	9 10
11	10.05	4.47	10.03	4.52	10.01	4.56	9.99		11
12	10.96	4.88 5.29		4.93 5.34	10.92 11.83	4.98	10.90	5.02	12
13	11.88	5.69		5.75	12.74	5.81	12.71	5.86	13 14
15	13.70	6.10	13.68	6.16	13.65	6.22	13.62	6.28	15
1 16	14.62	6.51		6.57 6.98	14.56	6.64 7.05	14.53	6.70 7.12	16
	15.55			7.39	16.38	7.46	16.35	7.54	17 18
19	17.36	7.73	17.32	7.80	17.29	7.88	17.25	7.95	19
20	18.27	8.13	18.24	8.21	18.20	8.29	18.16	8.37	20
21			19.15 20.06	8.63 9.04	$19.11 \\ 20.02$	8.71 9.12	19.07 19.98	8.79 9.21	$\frac{21}{22}$
22	21.01		20.97	9.04	20.92	9.54	26.89	9.63	23
24			21.88	9.86	21.84	9.95	21.80	10.05	24
25	22.84	10.17	22.79			10.37	22.70		25
26	23.75	10.58	23.71	10.68 11.09		$10.78 \\ 11.20$	23.61 24.52		26 27
28	0	11.39	25.53		25.48	11.61	25.43	11.72	28
29		11.80	26.44	11.91		12.03	26.34		29
30	27.41	12.20		12.32	27.30	12.44	27.24	12.56	30
31		12.61	28.26	12.73	28.21		28.15		31
	29.23 30.15	$13.02 \\ 13.42$	29.18 30.09		29.12 30.03	$13.27 \\ 13.68$	29.06 29.97		32 33
	31.06		31.00	13.96		14.10	30.88		34
	31.97		31.91		31.85		31.78		35
36	32.89 33.80	$14.64 \\ 15.05$	$32.82 \\ 33.74$	$14.79 \\ 15.20$	32.76 33.67		32.69 33.60		36 37
38	34.71	15.46		15.61		15.76	34.51		38
39	35.63	15.86	35.56	16.02	35.49	16.17	35.42	16.33	39
40	36.54		36.47	16.43	36.40		36.33		40
41	37.46 38.37		37.38 38.23	16.84 17.25	$37.31 \\ 38.22$	$17.00 \\ 17.42$	37.23 38.14		41 42
42	39.28	17.49	39.21	17.66	39.13		39.05		42
44	40.20	17.90	40.12	18.07	40.04	18.25	39.96	18.42	44
45	$41.11 \\ 42.02$	18.30		18.48 18.89	40.95 41.86	18.66	40.87 41.77	18.84	45
	42.02 42.94		41.94		41.80		41.68	19.26 19.68	46
48	43.85	19.52	43.76	19.71	43.68	19.91	43.59	20.10	48
49	44.76 45.68	19.93	44.68 45.59	20.13	44.59 45.50	20.32 20.73		20.51 20.93	49 50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Bt.
ā	66 I)eg.	65 <u>3</u> I	Deg.	65 <u>1</u> I)eg.	65 <u>1</u>)eg.	al

H	24	Deg.	241	Deg.	241	Deg.	243	Deg.	E
)ist.									list
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	<u> </u>
	46.59		46.50			21.15		21.35	51
52 59	47.50 48.42	21.15	47.41 48.32		47.32	$21.56 \\ 21.98$	47.22 48.13	21.77	52 53
54	49.33	21.96	49.24		49.14	22.39	49.04	22.61	54
55	50.24	22.37		22.59	50.05	22.81 23.22	49.95		55
	51.16 52.07		51.06 51.97	23.00		$23.22 \\ 23.64$		23.44 23.86	56 57
58	52.99	23.59		23.82		24.05	52.67		58
59	53.90	24.00		24.23		24.47		24.70	59
60	54.81	24.40	54.71	24.64	54.60	24.88	54.49	25.12	. 60
	55.73		55.62	25.05	55.51	25.30		25.54	61
		25.22		25.46	56.42	25.71	56.30	25.96	62
		$25.62 \\ 26.03$		$25.88 \\ 26.29$	57.33	$26.13 \\ 26.54$	57.21	26.38 26.79	63 64
65	59.38	26.44	59.26	26.70	59.15	26.96	59.03	27.21	65
		26.84		27.11	60 06	27.37	59.94	27.63	66
		27.25		$27.52 \\ 27.93$	60.97	$27.78 \\ 28.20$	60.85	28.05 28.47	67 68
		28.06		28.34		28.61		28.89	69
70	63.95	28.47	63.82	28.75		29.03		29.31	70
71	64.86	28.88	64.74	29.16	64 61	29.44	64 49	29.72	71
72	65.78	29.28	65.65		65.52	29.86		30.14	72
		29.69		29.98	66.43	30.27		30,56	73
		30.10 30.51		30.39	67.34	30.69 31.10		30.98	74 75
76	69.43	30.91	69.29	$\begin{array}{c} 30.80\\ 31.21 \end{array}$	69.16	31.52		31.82	
77	70.34	31.32	70.21	31.63	70.07	31.93	69.93	32.24	77
78 79		31.73 32.13		$32.04 \\ 32.45$	70.98	32.35 32.76	70.84	32.66	78 79
		32.54		32.86		33.18		33.07	80
81 82		32.95 33.35		33.27 33.68		33.59 34.00		33.91	81 82
	75.82	33.76		34.09		34.42	75.38	34.75	83
84		34.17		34.50		34.83		35.17	84
		34.57 34.98		34.91 35.32	77.35	35.25	77.19	35.59	85
87	79.48	35.39	79.32		79.17	35.66 36.08	79.01	36.00	87
		35.79		36.14	80.08	36.49	79.92	36.84	88
		36.20 36.61	81.15	36.55 36.96		36.91		37.26 37.68	
_									
91	83.13	37.01		37.38		37.74		38.10	
92	84.96	37.42 37.83		37.79 38.20		38.15 38.57		38.52 38.94	
94	85.87	38.23	85.71	38.61	85.54	38.98	85.3	39.35	94
95	86.79	38.64		39.02	86.45	39.40	86.2	39.77	95
96	87.70	39.05 39.45		39.43 39.84		39.81 40.23		340.19 40.61	96 97
		39.86		40.25		40.23	89.00)41.03	98
99	90.44	40.27	90.26	40.66	90.09	41.05	89.9	41.45	99
100	91.35	40.67	91.18	41.07	91.00	41.47	90.8	41.87	100
÷	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	t.
ā	66	Der	653	Dar	651	Dee	GEL	De	Dis
L	100	Deg	003	Deg.	$ 00\frac{1}{2} $	Deg	10.5	De".	

E	25	Deg.	251	Deg.	$25\frac{1}{2}$	Deg.	253	Deg.	U
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1			0.90		0.90		0.90		
23	1.81	0.85	1.81 2.71	0.85	1.81 2.71		1.80 2.70	0.87	23
45	3.63	1.69	3.62	1.71	3.61	1.72	3.60	1.74	4
6			4.52	2.13 2.56	4.51 5.42		4.50	2.17 2.61	5
7			6.33	2.99	6.32	3.01	6.30	3.04	7
89			7.24 8.14		7.22	3.44	7.21 8.11	3.48 3.91	8
10			9.04	4.27	9.03		9.01		10
11	9.97 10.88	4.65 5.07	9.95 10.85	4.69 5.12	9.93 10.83	4.74	9.91	4.78 5.21	11
13	11.78		11.76	5.55	11.73		10.81 11.71	5.65	12 13
	12.69 13.59	5.92	12.66 13.57	5.97 6:40	12.64 13.54		12.61	6.08	14
16	14.50	6.34 6.76	14.47	6.83	14.44	6.89	$13.51 \\ 14.41$	6.52	15 16
17	$15.41 \\ 16.31$	7.18	$15.38 \\ 16.28$	7.25 7.68	15.34		15.31	7.39	17
19	17.22	7.61 8.03	17.18	8.10	16.25		16.21 17.11	7.82	18 19
20	18.13	8.45	18.09	8.53	18.05		18.01	8.69	20
21	19.03 19.94	8.87 9.30	18.99 19.90	8.96 9.38	18.95 19.86	9.04	18.91 19.82	9.12 9.56	21 22
23	20.85	9.72	20.80	9.81	20.76		20.72	9.99	23
24	21.75	10.14		10.24			21.62		24 25
26	$22.66 \\ 23.56$	10.99	23.52	11.09	23.47	11.19	22.52 23.42 24.32	11.30	26
27	24.47	11.41	24.42	11.52	24.37	11.62	24.32	11.73	27
29	$25.38 \\ 26.28$	12.26	25.32 26.23		25.27	12.05	25.22 26.12	12.16	28. 29
30	27.19	12.68	27.13		27.08	12.92	26.12 27.02	13.03	30
31	28.10	13.10	28.04	13.22	27.98	13.35	27.92	13.47	31
32	29.00 29.91	$13.52 \\ 13.95$	28.94 29.85	13.65	28.88	13.78	28.82 29.72	13.90	32
34	30.81	14.37	30.75	14.50	30.69	14.64	30.62	14.77	34
35	31.72 32.63	14.79	31.66	14.93	31.59	15.07	31.52 32.43	15.21	35 36
37	33.53	15.64	33.46	15.78	33.40	15.93	33.33	16.07	37
38	34.44	16.06	34.37	16.21	34.30	16.36	33.39 34.23 35.13	16.51	38
40	35.35 36.25	16.48 16.90	36.18	17.06	36.10	17.22	36.03	17.38	39 40
41	37.16	17.33	37.08		37.01		36.93		41
42	38.06 38.97	17.75			37.91 38.81		37.83 38.73		42 43
44	39.88	18.60	39.80	18.77	39.71	18.94	39.63	19.12	44
	40.78 41.69		40.70 41.60		40.62 41.52	19.37	40.53 41.43		45 46
47	42.60	19.86	42.51	20.05	42.42	20.23	42.33	20.42	47
48 49	43.50	20.29	43.41	20.48	43.32 44.23	20.66	43.23		48
49 50	44.41 45.32	21.13			44.25		44.13		49 50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
Ā	65]	Deg.	643	Deg.	641	Deg.	64 1	Deg.	ā

Þ	25	Deg.	25_{4}^{1}	Deg.	251	Deg.	253	Deg.	U
st.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	st.
	46.22 47.13		46.13	21.75	46.03	21.96		22.16 22.59	51 52
53	48.03	22.40	47.94	22.18 22.61	47.84	22.82		23.03	53
	48.94 49.85		48.84	23.03 23.46	48.74	23.25		23.46	54 55
56	50.75	23.67	50.65	23.40	49.04	23.68		23.89 24.33	56
57	51.66	24.09	51.55	24.31	51.45	24.54	51.34	24.76	57 58
59	53.47	24.51 24.93		24.74			52.24	25.20 25.63	59
		25.36	54.27	25.59	54.16	25.83		26.07	60
	55.28			26.02		26.26		26.50	61
	56.19 57.10	26.20		26.45 26.87		26.69		26.94 27.37	62 63
	58.00		57.89	27.30	57.77	27.12 27.55		27.80	64
65	58.91	27.47	58.79	27.73	58.67	27.98	58.55	28.24	65
67	59.82 60.72	27.89	59.69	28.15 28.58	59.57 60.47	28.41		28.67 29.11	66 67
68	61.63	$28.32 \\ 28.74$					61.25	29.54	68
69 70	62.54 63.44	29.16		29.43 29.86				29.98 30.41	69 70
									_
71	64.35	30.01	64.22	30.29				30.85	71
	65.25		65.12 66.03			31.00 31.43	64.85 65.75	31.28 31.71	72
	67.07 67.97		66.93 67.83		66.79	31.86	66.65	32.15	74
75	67.97	31.70 32.12	67.83	31.99	67.69		67.55 68.45		75 76
77	69.79	32.54	69.64	32.85	69.50	33.15	69.35		77
78	70.69	32.96	70.55	33.27	70.40	33.58	70.25		78
79 80	72.50	33.39 33.81	72.36	33.70		34.01 34.44	71.16	34.32	79 80
							· <u> </u>		
		34.23 34.65	73.26	34.55 34.98	73.11	34.87 35.30	72.96	35.19	81 82
		35.08	75.07	35.41	74.91	35.73			-83
84	76.13	35.50	75.97	35.83	75.82	36.16	75.66	36.49	84
86	77.94	35.92 36.35	77.78	36.68	76.72	36.59 37.02	76.56	36.93	85 86
87	78.85	36.77	78.69	36.68 37.11	78.52	37.45	78.36	37.80	87
88	79.76	37.19	79.59	37.54	79.43	37.88 38.32	79.26	38.23 38.67	88 89
90	81.57	38.04	81.40	38.39	81.23	38.75	81.06	39.10	90
91	82.47	38.46		38.82	82.14	39.18	81.96	39.53	91
92	83.38	38.88			83.04	39.61	82.86	39.97	92
		39.30 39.73	85.02	39.67 40.10		40.04 40.47		40.40	93 94
95	86.10	40.15	85.92	40.52	85.75	40.90	85.57	41.27	95
		40.57 40.99	86.83	40.95	86.65	41.33	86.47	41.71	96 97
98	88.82	41.42	88.64	41.80	88.45	41.76 42.19	88.27	42.14	97
99	89.72	41.84 42.26	89.54	42.23	89.36	42.62	89.17	43.01	99
		42.20				43.05			100
ist.		Lat.	-		-	Lat.	-		ist.
P	65	Deg.	643	Deg.	641	Deg.	641	Deg.	2

			-				-		6
D	26	Deg.	261 L)eg.	$26\frac{1}{2}$	Jeg.	$26\frac{3}{4}$	Deg.	9
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1	0.90	0.44	0.90	0.44	0.89	0.45	0.89	0.45	
.2	1.80	0.88	1.79	0.88	1.79	0.40	1.79	0.90	2
34	2.70 3.60	1.32	2.69	1.33	2.68	1.34	2.68	1.35	3 4
45	4.49	1.75 2.19	3.59 4.48	1.77 2.21	3.58	$1.78 \\ 2.23$	3.57	$1.80 \\ 2.25$	5
6	5.39	2.63	5.38	2.65	5.37	2.68	5.36	2.70	6
78	6.29	3.07	6.28	3.10	6.26	3.12	6.25	3.15	78
9	7.19 8.09	3.51 3.95	7.17	3.54 3.98	7.16 8.05	3.57 4.02	7.14	3.60 4.05	. 9
10	8.99	4.38	8.97	4.42	8.95	4.46	8.93	4.50	10
11	9.89	4.82	9.87	4.87	9.84	4.91	9.82	4.95	11
12	10.79	5.26	10.76	5.31	10.74	5.35	10.72	5.40	12 13
	11.68 12.58	5.70 6.14	11.66	5.75 6.19	11.63	5.80 6.25	11.61	5.85 6.30	13
15	13.48 14.58	6.58	13.45	6.63	13.42	6.69	13.39		15
16	14.58	7.01	14.35	7.08	14.32	7.14			16
	15.28 16.18		15.25	7:52 7.96	15.21 16.11		15.18		17 18
	17.08		17.04	8.40	17.00	8.48			19
20	17.98	8.77	17.94	8.85	17.90	8.92	17.86		20
	18.87		18.83	9.29	18.79	9.37			21
		9.64	19.73	9.73	19.69				22 23
		10.08	$20.63 \\ 21.52$			10.26			24
25	22.47	10.96	22.42	11.06	22.37	11.15	22.32	2 11.25	
		11.40			23.27	11.60	23.29	2 11.70	
		11.84		12.38		12.05		12.15	-
29	26.06	12.71	26.01	12.83		12.94		13.05	29
30	26.96	5 13.15	26.91	13.27	26.85	13.39	26.79	13.50	30
31	27.86	13.59	27.80	13.71		13.83		3 13.95	
		5 14.03 5 14.47		14.15		14.28		8 14.40 7 14.85	
		5 14.90		14.60 15.04		3 14.72 3 15.17	30.3	6 15.30	
35	31.46	5 15.34	31.39	15.48	31.3	2 15.69	2 31.2	6 15.30 5 15.75	35
		515.78 516.22		$15.92 \\ 16.36$				5 16.20 $4 16.65$	
		5 16.63		16.81				3 17.10	38
39	35.0	5 17.10	34.98	17.25			34.8		
40	35.9	5 17.5	3 35.87	17.69	35.8	17.8	5 35.7	2 18.00	40
			36.77						
			1 37.67 5 38.57			9 18.7 8 19.1		1 18.90 0 19.3	
44	1 39.5	5 19.29	39.46	19.46	39.3	8 19.6	3 39.2	9 19.80	5 44
			3 40.36						
			$7 41.26 \\ 42.15$					8 20.70 7 21.1	·
48	8 43.1	421.0	4 43.05	21.25	42.9	6 21.4	2 42.8	6 21.6	5 48
		4 21.4	8 43.95	21.67		5 21.8 5 22.3		6 22.0. 5 22.5	
-		1	-	-	-	-	-	_	
ist.	Dep	Lat	. Dep.	Lat	Dep	. Lat	. Dep	. Lat	ist.
19	64	Deg	· 63 ³ / ₄	Deg	63	Deg	. 63	Deg	A.

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1-	26	Deg.	261	Deg.	1261	Deg.	263	Deg	1-
Jist	1								
Ĩ	Lat	. Dep.	Lat.	Dep.	Lat.	Dep.	Lat	Dep	Ist.
-	-								
51		4 22.36		22.56		22.76		22.9	
5%	46.7	4 22.80 4 23.23		23.00		23.20		23.4	
		3 23.67		23.88	47.43	24.09		24.3	
		3 24.11		24.33		24.54		24.7	
		3 24.55		24.77	50.12		50.01	25.2	56
		3 24.99		25.21	51.01	25.43	50.90	25.66	5 57
		3 25.43		25.65		25.88		26.1	
		3 25.86		26.09	52.80	26.33		26.56	
OL	55.90	3 26.30	55.81	26.54	33.70	26.77	33.58	27.0	60
61	54.89	3 26.74	54 71	26.98	54.59	27.22	54 47	27.46	61
		27.18		27.42		27.66		27.91	
		27.62		27.86		28.11		28.36	
		28.06		28.31	57.28	28.56	57.15	28.8	64
		28.49		28.75	58.17	29.00		29.26	
		28.93		29.19		29.45		29.71	
		29.37		29.63		29.90		30.16	
		29.81		$30.08 \\ 30.52$	61.75	30.34 30.79		30.61	
		30.69		30.96		31.23		31.51	
							0		
71	63.81	31.12	63.68	31.40	63.54	31.68	63.40	31.96	71
		31.56	64.57	31.84		32.13		32.41	
		32.00	65.47	32.29	65.33			32.86	
		32.44	66.37	32.73		33.02		33.31	
		32.88	67.27		67.12			33.76	
		33.32 33.75	68.16	$33.61 \\ 34.06$	68.01			34.21	
		34.19	69.96		68.91 69.80			34.66	
		34.63		34.94	70.70			35.56	
80		35.07	71.75			35.70	71.44	36.01	80
									_
81		35.51	72.65	35.83	72.49	36.14	72.33	36.46	81
82		35.95	73.54 74.44	36.27		36.59		36.91	
83		36.38	74.44	36.71	74.28			37.36	
		36.82	75.34	37.15	75.17			37.81	
85		37.26 37.70	76.23 77.13	37.59	76.07	37.93	75.90	38.26	85
		38.14	78.03	38.48	76.96 77.86			38.71	
		38.58	78.92		78.75			39.61	88
89		39.01	79.82			39.71		40.06	
		39.45	80.72		80.54			40.51	
91		39.89	81.62			40.60		40.96	
	82.69		82.51			41.05		41.41	92
	83.59 84.49		$83.41 \\ 84.31$		83.23 84.12	41.50		41.86	93
			85.20			41.94 42.39	83.94 84.83		94 95
		42.08	86.10			42.83	85.73		96
97	87.18	42.52	87.00		86.81	43.28	86.62		97
98	88.08	42.96	87.89	43.34		43.73	87.51		98
99	88.98	43.40	88.79	43.79	88.60	44.17	88.40	44.56	99
100	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	100
-	Der								
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep	Lat.	it.
5	CA.		00.01		0017		001		i.
	04	Deg.	6331	Jeg.	031	Jeg.	631	Jeg.	

U	27	Deg.	$27\frac{1}{4}$	Deg.	$27\frac{1}{2}$	Deg.	273	Deg.	H
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1	0.89	0.45	0.89	0.46	0.89	0.46	0.88	0.47	1
. 2	1.78	0.91	1.78	$0.92 \\ 1.37$	1.77	0.92	1.77	0.93	23
4	3.56	1.82	3.56	1.83	3.55	1.85	3.54	1.86	4
5	4.45	2.27	4.45	2.29	4.44	2.31	4.42	2.33	5
67	$5.35 \\ 6.24$	2.72 3.18	5.33	$2.75 \\ 3.21$	5.32	2.77	5.31	2.79 3.26	6 7
8	7.13	3.63	7.11	3.66	7.10	3.69	7.08	3.72	8
9	8.02	4.09	8.00	4.12	7.98	4.16	7.96	4.19	9
10	8.91	4.54	8.89	4.58	8.87	4.62	8.85	4.66	10
11	9.80	4.99	9.78	5.04	9.76	5.08	9.73	5.12	11
	10.69 11.58	5.45	10.67	5.49	10.64	5.54	10.62	5.59	12
	12.47		11.56 12.45	5.95 6.41	11.53	6.00 6.46	11.50 12.39	6.05 6.52	13 14
	13.37	6.81	13.34	6.87	13.31	6.93	13.27	6.98	15
	14.26 15.15	7.26 7.72	$14.22 \\ 15.11$	7.33	14.19	7.39	14.16	7.45	16 17
	16.04	8.17	15.11	$7.78 \\ 8.24$	15.08 15.97	7.85	15.04 15.93	8.38	18
19	16.93	8.63	16.89	8.70	16.85	8.77	16.81	8.85	19
20	17.82	9.08	17.78	9.16	17.74	9.23	17.70	9.31	20
21	18.71	9.53	18.67	9.62	18.63	9.70	18.58	9.78	21
22	19.60	9.99	19.56	10.07	19.51	10.16	19.47	10.24	22
23	$20.49 \\ 21.38$	10.44	20.45	10.53	20.40	$10.62 \\ 11.08$	20.35		23 24
25	22.28	11.35	21.34 22.23			11.08	$21.24 \\ 22.12$		24
26	23.17	11.80	23.11	11.90	23.06	12.01	23.01	12.11	26
27	$24.06 \\ 24.95$	12.26	24.00 24.89		$23.95 \\ 24.84$		23.89 24.78		27 28
29	25.84	13.17	24.09		24.84 25.72			13.50	20
30	26.73	13.62		13.74	26.61		26.55		30
31	27.62	14.07	27.56	14 10	27.50	14 31	27.43	14 13	31
32	28.51	14.53	28.45			14.78		14.90	32
33	29.40	14.98	29.34	15.11	29.27	15.24	29.20		.33
35	30.29	15.44	30.23	15.57 16.03	30.16 31.05			15.83 16.30	34 35
36	32.08	16.34	32.00		31.93			16.76	36
37	32.97	16.80	32.89	16.94	32.82	17.08	32.74	17.23	37
38	33.86 34 75	$17.25 \\ 17.71$	33.78 34.67		33.71	17.55 18.01	33.63 34.51		38 39
40	35.64	18.16	35.56		35.48			18.62	40
	00 20	10 01	00 45	10 55	00 0	10.00	00.00	10.00	-
41	36.53 37.42	18.61	36.45 37.34	18.77	36.37	18.93		19.09 19.56	41 42
43	38.31	19.52		19.69	38.14	19.86	38.05	20.02	43
	39.20		39.12		39.03			20.49	44
	40.10 40.99	$20.43 \\ 20.88$	40.01 40.89		39.92 40.80			20.95 21.42	45 46
47	41.88	21.34	41.78			21.70	41.59	21.88	47
43	42.77	21.79	42.67	21.98	42.58	22.16	42.48	22.35	48
		22.25 22.70	43.56		43.46		43.36	22.82	49 50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	ist.
Ā	63	Deg.	623	Deg.	621/2	Deg.	621	Deg.	D

E	27 L)eg.	271	Deg.	$27\frac{1}{2}$	Deg.	$27\frac{3}{4}$	Deg.	E
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
51	45.44 46.33	23.15		23.35 23.81	45.24	23.55		23.75 24.21	51 52
53	47.22	24.06	47.12	24.27	47.01	24.47		24.21	53
	48.11 49.01			24.73 25.18		24.93 25.40		25.14 25.61	54 55
56	49.90	25.42		25.64		25.86		25.01	
		25.88		26.10 26.56		26.32		26.54	
59	52.57	26.33 26.79		27.01		27.24	52.21	27.47	59
		27.24	53.34	27.47	53.22	27.70	53.10	27.94	60
		27.69		27.93		28.17		28.40	
	55.24 56.13	28.15		28.39 28.85		28.63 29.09		28.87 29.33	
64	57.02	29.06	56.90	29.30	56.77	29.55		29.80	64
	57.92	29.51 29.96		29.76 30.22		30.01 30.48		30.26	
67	59.70	30.42		30.68		30.48		31.20	
68	60.59	30.87		31.14	60.32	31.40	60.18	31.66	68
	61.48 62.37	31.33 31.78		31.59 32.05		31.86 32.32		32.13	
-									_
71	63.26	32.23		32.51		32.78		33.06	
	64.15 65.04			32.97		33.25 33.71		33.52 33.99	
74	65.93	33.60	65.79	33.88	65.64	34.17	65.49	34.46	74
75	66.83	34.05 34.50		34.34 34.80		34.63 35.09		34.92	
77	68.61	34.96	68.45	35.26			68.14		
78	69.50	35.41		35.71		36.02		36.32	
	70.39 71.28			36.17 36.63		36.48 36.94		36.78 37.25	
	72.17		72.01	37.09	71.85	37.40	71.68	37.71	81
82 83	73.06 73.95			37.55		37.86 38.33		38.18	82
	74.84			38.46		38.33		38.65 39.11	84
85	75.74	38.59		38.92		39.25		39.58	
86	76.63	39.04 39.50		39.38 39.83		39.71 40.17		40.04	86
88	78.41	39.95	78.23	40.29	78.06	40.63	77.88	40.97	88
	79.30 80.19	40.41		40.75	78.94	41.10 41.56		41.44	89 90
						41.00	19.00	41.31	
		41.31	80.90			42.02		42.37	
		$41.77 \\ 42.22$	81.79 82.68	42.12 42.58		42.48 42.94		42.84 43.30	
94	83.75	42.68	83.57	43.04	83.38	43.40	83.19	43.77	94
		43.13				43.87		44.23	95 96
97	86.43	44.04	86.23	44.41		44.33	85.84		97
		44.49				45.25	86.73		98
		44.95 45.40			87.81 88.70	45.71 46.17		46.10 46.56	
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	ŗ.
Dis	63 1	Dag	69 21	Jam	6911	200	col	Dan	Sic
	001	Deg.	0241	ack.	042	Jeg.	024	Deg.	-1

									-
	28 L)eg.	2841	Jeg.	$28\frac{1}{2}$	Deg.	2841	Deg.	U
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	st.
1	0.88	0.47	0.88	0.47	0.88			0.48	1
2	1.77	0.94	1.76	0.95	1.76	0.95	1.75	0.96	23
-34	2.65	1.41	2.64	1.42	2.64	1.45	3.51	1.44	4
5	4.41	2.35	4.40	2.37	4.39	2.39	4.38	2.40	. 5
6	5.30	2.82	5.29	2.84	5.27	2.86	5.26	2.89	6
7	6.18	3.29	6.17	3.31	6.15	3.34	6.14	3.37	7
8	75.3	3.76	7.05		7.03		7.01		8
9 10	7.95	4.23	7.93	4.26 4.73	7.91 8.79	4.29 4.77	7.89	4.33 4.81	9 10
	0.00		0.01	3.10	0.10		0.71		
11	9.71	5.16	9.69	5.21	9.67	5.25	9.64	5.29	11
12	10.60		10.57	5.68	10.55	5.73	10.52	5.77	12
	11.48	6.10	11.45	6.15	11.42	6.20	11.40	6.25	13
14 15	12.36 13.24	6.57	12.33	6.63	12.30		12.27	6.75	14
	13.24	7.04	13.21	7.10	13.18 14.06	7.16	13.15 14.03	7.21	15 16
	15.01	7.98	14.98	8.05	14.94		14.00	8.18	17
18	15.89	8.45	15.86		15.82	8.59	15.78	8.66	18
19	16.78	8.92	16.74	8.99	16.70		16.66	9.14	19
20	17.66	9.39	17.62	9.47	17.58	9.54	17.53	9.62	20
21	18.54	9.86	18.50	9.94	18.46	10.02	18.41	10.10	21
		10.33	19.38	10.41	19.33	10.50	19.29	10.58	22
23	20.31	10.80	20.26			10.97		11.06	23
24	21.19	11.27	21.14		21.09			11.54	24 25
20	22.07	11.74	22.02 22.90		21.97	12.41		12.02	25
		12.68		12.31		12.88		12.99	27
28	24.72	13.15	24.66	13.25		13.36		13.47	28
		13.61	25.55	13.73		13.84		13.95	29
30	26.49	14.08	26.43	14.20	26.36	14.31	26.30	14.43	39
31	27.37	14.55	27.31	14.67	27.24	14.79	27.18	14.91	31
	28.25		28.19	15.15	28.12	15.27	28.06	15.39	32
		15.49		15.62		15.75		15.87	33
34	30.02	15.96	29.95	16.09		16.22		16.35	34
36	31.70	16.43 16.90	30.83	16.57 17.04	31 64	16.70 17.18		16.83	35
37	32.67	17.37	32.59			17.65		17.80	37
38	33.55	17.84	33.47	17.99	33.39	18.13	33.32	18.28	38
39	34.43	18.51	34.35	18.46		18.61		18.76	39
40	35.32	18.78	35.24	18.93	35.15	19.09	35.07	19.24	40
			36.12			19.56	35.95	19.72	41
		19.72		19.88		20.04		20.20	42
		20.19	37.88			20.52		20.68	43
	38.85 39.73	20.66 21.13	38.76	20.83	38.67	20.99		21.16 21.64	44 45
		21.13		21.30		21.47		21.64 22.13	45
	41.50	22.07		22.25		22.43		22.61	47
48	42.38	22.58	42.28	22.72	42.18	22,90		23.09	48
49	43.26	23.00		23.19	43.06	23.38	42.96	23.57	49
50	44.15	23.47	44.04	23.67	43.94	23.86	43.84	24.05	50
8		Lat.		Lat.	-	Lat.	-		ist.
A	62	Deg.	613	Deg.	611	Deg.	614	Deg.	Q

D	28 L	eg.	2811	Deg.	$28\frac{1}{2}$	Deg.	$28\frac{3}{4}$	Deg.	E
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	st.
51	45.03	23.94	44.93	24.14	44.82	24.34	44.71 45.59	24.53	51
		24.41	45.81	24.61	45.70				52
		24.88 25.35					46.47		53
				25.56				26.45	54 55
56	49.45	26.29		26.51				26.94	56
		26.76		26.98	50.09	27.20	49.97		57
58	51.21	27.23	51.09	27.45	50.97	27.68	50.85	27.90	58
59	52.09	27.70	51.97				51.73	28.38	59
60	52.98	28.17	52.85	28.40	52.73	28.63	52.00	28.86	60
61	53.86	28.64	53.73	28.87	53.61	29.11	53.48	29.34	61
		29.11	54.62			29.58		29.82	62
63	55.63	29.58 30.05	55.50		55.37	30.06	55.23	30.30	63
			56.38		56.24	30.54	56.11	30.78	64
		30.52	57.26			31.02		31.26	65
		30.99 31.45	58.14 59.02	31.24		31.49 31.97		31.75 32.23	66 67
		31.92	59.02			32.45		32.23	68
		32.39	60.78			32.92		33.19	69
		32.86	61.66	33.13	61.52	33.40	61.37	33.67	70
71	62.69	33.33	62.54			33.88			71
		33.80		34.08		34.36			72
		34.27 34.74		34.55 35.03	65 09	34.83 35.31	64.00	35.11	73 74
		35.21		35.50	65.91	35.79	65.75	36 07	75
		35.68		35.97	66.79	36.26	66.63	36.56	76
		36.15		36.45	67.67	36.74 37.22	67.51	37.04	77
		36.62		36.92	68.55	37.22	68.38		78
		37.09		37.39		37.70			79
80	10.04	37.56	10.41	37.87	10.51	38.17	10.14	38.48	80
81	71.52	38.03	71.35	38.34	71.18	38.65	71.01	38,96	81
		38.50		38.81	72.06	39.13		39.44	
		38.97		39.29		39.60		39.92	83
		39.44		39.76		40.08	73.64	40.40	84
85	75.05	39.91	74.88	40.23	74.70	40.56	74.52	40.88	85
		40.37 40.84		40.71 41.18		41.04		41.36	86 87
		40.84		41.18		41.51		41.85	88
		41.78		42.13	78.21	42.47	78.03	42.81	89
		42.25		42.60		42.94		43.29	90
		42.72		43.07		43.42		43.77	
92	81.23	43.19		43.55		43.90		44.25	92 93
94	83.00	43.66		44.02		44.38		44.73	94
		44.60		44.97		45.33		45.69	
96	84.76	45.07	84.57	45.44	84.37	45.81	84.17	46.17	96
		45.54				46.28		46.66	
		3 46.01		46.39		46.76			
		46.48		46.86					
	00.2	46.95	05.00	41.33	01.80	41.12	01.01	48.10	100
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
A.	62	Deg.	613	Deg.	611	Deg.	614	Deg.	Â

90	-				-				
D	29]	Deg.	291	Deg.	29 <u>1</u>	Deg.	294	Deg.	D
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep:	Lat.	Dep.	st.
1	0.87	0.48	0.87	0.49	0.87	0.49	0.87	0.50	;1
23	1.75 2.62	0.97	1.74 2.62	0.98	1.74	0.98	1.74 2.60	0.99	23
4	3.50	1.94	3.49	1.95	2.61		3.47	1.98	4
5	4.37	2.42	4.36	2.44	4.35	2.46			5
6	5.25	2.91	5.23	2.93	5.22			2.98	
7	6.12	3.39	6.11	3.42 3.91	6.09	3.45	6.08		7
8 9	7.00	3.88 4.36	6.98 7.85	4.40	6.96 7.83		6.95		8
10	8.75	4.85	8.72	4.89	8.70		8.68		10
11	9.62	5.33	9.60	5.37	9.57		9.55		11
12	10.50	5.82	10.47	5.86	10.44		10.42	5.95	12
	11.37	6.30 6.79	11.54	6.35 6.84	11.31	6.40 6.89	11.29 12.15		13 14
	13.12	7.27	13.09	7.33	13.06		13.02		
16	13.99	7.76	13.96	7.82	13.93		13.89		
17	14.87	8.24	14.83	8.31	14.80		14.76		17
	15.74	8.73	15.70	8.80	15.67		15.63		18
19 20	16.62 17.49	9.21 9.70	16.58 17.45	9.28 9.77	$16.54 \\ 17.41$	9.36 9.85	16.50 17.36		19 20
21	18.37	10.18	18.32	10.26	18.28	10.34	18.23	10.42	21
22	19.24	10.67	19.19	10.75	19.15	10.83	19.10	10.92	22
	20.12		20.07			11.33		11.41	23
24	20.99	11.64	20.94			11.82		11.91	24
	21.87	12.12	21.81	12.22		12.31 12.80		12.41	26
		13.09	23.56			13.30		13.40	27
28	24.49	13.57	24.43	13.68	24.37	13.79	24.31	13.89	28
		14.06	25.30			14.28		14.39	29
30	26.24	14.54	26.17	14.66	26.11	14.77	26.05	14.89	30
		15.03	27.05			15.27		15.38	31
		15.51	27.92	15.64	27.85	15.76		15.88	32
	28.86 29.74	16.00	28.79 29,66		28.72	16.25		16.38 16.87	33
		16.97	30.54			17.23		17.37	35
	31.49		31.41	17.59	31.33	17.73		17.86	36
	32.36		32.28		32.20	18.22		18.36	37
		18.42				18.71		18.86	38
	34.11 34.98	18.91		19.66 19.54	33.94 34.81	19.20 19.70		19.35 19.85	39 40
41	35.86	19.88	35.77	20,03	35.68	20.19	35.60	29.34	41
42	36.73	20.36	36.64	20.52	36.55	20.68	35.46	20.84	42
	37.61			21.01	37.43	21.17	37:33	21.34	43
		21.33		21.50	35.30	21.67		21.83	44
	39.36	21.82 22.30		21.99 22.48	39.17	22.16 22.65	39.07 39.94	22.33	45
	41.11					22.05			46
	41.98					23.63			48
49	42.86	23.76	42.75	23.94	42.65	24.13	42.54	24.31	49
50	43.73	24.24	43.62	24.43	43.52	24.62	43.41	24.81	50
ist.	-		Dep.				Dep.		ist.
9	.61	Deg.	6031	Deg.	601	Deg.	601 I	Deg.	

E	29	Deg.	29%	Deg.	291	Deg.	294	Deg.	B
ist,	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
		24.73		24.92		25.11		25.31	
52	45.48	25.21		25.41 25.90		25.61 26.10	45.15 46.01	25.80	
		26.18		28.39		26.59	46.88		
55	48.10	26.66		26.87		27.08	47.75	27.29	55
		27.15	48.86	27.36 27.85		27.58	48.62	27.79	56
		27.63 28.12		28.34	49.61 50.48		49.49 50.36		
59	51.60	28.60		28.83		29.05	51.22	29.28	. 59
60	52:48	29.09	52.35	29.32	52.22	29.55	52.09	29.77	60
		29.57		29.81		30.04	52.96	30.27	61
		30.06		30.29		30.53 31.02	53.83 54.70		
		31.03		\$1.27		31.52	55.56		
65	56.85	31.51	56.71	31.76	56.57	32.01	56.43	32.25	65
		32.00 32.48	57.58	32.25 32.74		32.50 32.99	57.30		
		32.97		33.23		33.48	58.17 59.04		
69	60.35	33.45	60.20	33.71		33.98	59.91	34.24	69
70	61.22	33.94	61.07	34.20	60.92	34.47	60.77	34.74	70
		34.42	61.95	34.69	61.80	34.96	61.64	35.23	71
		34.91		35.18	62.67		62.51	35.73	72
		35.39 35.88	63.69 64.56		63.54 64.41	35.95	63.38 64.25		73
		36.36		36.65	65.28		65.11		75
		36.85	66.31	37.14	66.15	37.42	65.98 66.85	37.71	76
		37.33 37.82	67.18 68.05		67.02		66.85	38.21	77
79	69.09	38.30	68.93		68.76	38.41	67.72 68.59		79
80	69.97	38.78	69.80		69.63		69.46		80
81	70.84	39.27	70.67	39.58	70.50	39.89	70.32	40.19	81
82	71.72	39.75		40.07		40.38	71.19	40.69	82
83	72.59	40.24	72.42		72.24	40.87	72.06	41.19	83
85	74 94	40.72 41.21	73.29		73.11 73.98		72.93		84 85
86	75.22	41.69	75.03	42.02	74.85		73.80 74.67		86
87	76.09	42.18	75.91	42.51	75.72	42.84	75.53	43.17	87
88	76.97	42.66	76.78		76.59		76.40		86 89
90	77.84 78.72	43.63	77.65	43.98	77.46 78.33	43.83 44.32	77.27 78.14	44.16 44.66	90
91	79.59	44.12	79.40	44.46	79.20		79.01	45 16	91
92	80.46	44.60	79.40 80.27	44.95	80.07		79.87		92
	81.34		81.14	45.44	80.94		80.74	46.15	93
	82.21 83.09		82.01 82.89	45.93	81.81 82.68	46.29	81.61	46.64	94 95
.96	83.96	46.54	83.76	46.91	83.55	47.27	82.48 83.35	47.64	96
97	84.84	47.03	84.63	47.40	84.42	47.77	84.22	48.13	97
		47.51	85.50 86.38	47.88	85.29	48.26	85.08	48.63	98
100	87.46	48.00 48.48	86.38		86.17 87.04	48.75	85.95 86.82		99 100
÷	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.		-
Ō	61 1	Der	6031				60 L		Ois
-		Jeg.	0041	1	0021	Jeg.	0041	Jeg.	

	30	Deg.	301	Deg.	3012	Deg.	303]	Deg.	U
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
12	0.87 1.73	0.50 1.00	0.86	0.50 1.01	0.86	0.51 1.02	0.86	0.51 1.02	12
2 3 4	2.60	1.50	2.59	1.51	2.58	1.52	2.58	1.53	3
5	3.46 4.33	2.00 2.50	3.46 4.32	$2.02 \\ 2.52$	3.45 4.31	$2.03 \\ 2.54$	3.44 4.30	2.05 2.56	45
67	5.20 6.06	3.00 3.50	5.18 6.05	3.02	5.17 6.03	$3.05 \\ 3.55$	5.16	3.07 3.58	67
8 9	6.93 7.79	4.00	6.91	4.03	6.89	4.06	6.88	4.09	8
10	8.66	4.50 5.00	7.77 8.64	4.53 5.04	7.75 8.62	4.57 5.08	7.73 8.59	4.60	9 10
11	9.53 10.39	5.50 6.00	9.50 10.37	5.54 6.05	9.48 10.34	5.58 6.09	9.45 10.31	5.62 6.14	11 12
13	11.26	6.50	11.23	6.55	11.20	6.60	11.17	6.65	13
	12.12 12.99	7.00 7.50	$12.09 \\ 12.96$	7.05	12.06	7.11 7.61	12.03	7.16	14 15
16	13.86 14.72	8.00 8.50	13.82 14.69	8.06 8.56	13.79	8.12 8.63	13.75 14.61	8.18	16 17
18	15.59	9.00	15.55	9.07	15.51	9.14	15.47	9.20	18
	16.45 17.32	9.50 10.00	$16.41 \\ 17.28$	9.57 10.08	16.37 17.23	9.64 10.15	16.33 17.19	9.71 10.23	19 20
	18.19 19.05			10.58	18.09		18.05 18.91	10.74	21 22
23	19.92	11.50	19.87	11.59	19.82	11.67	19.77	11.76	23
	20.78 21.65		20.73 21.60	12.09 12.59		12.18 12.69	20.63 21.49	12.27 12.78	24
26	22.52	13.00	22.46	13.10	22.40	13.20	22.34	13.29	26
28		14.00	24.19	14.11	23.26 24.13	13.70		13.80 14.32	27 28
	$25.11 \\ 25.98$			14.61 15.11	24.99 25.85		24.92 25.78	$14.83 \\ 15.34$	
31	26.85	15.50	26.78	15.62	26.71	15.73	26.64	15.85	31
	$27.71 \\ 28.58$		27:64	$16.12 \\ 16.62$		16.24 16.75	27.50	16.36 16.87	32 33
34	29.44	17.00	29.37	17.13	29.30	17.26	29.22	17.38	34
36	30.31 31.18	18.00		17.63 18.14		17.76 18.27		17.90	35 36
37	32.04	18.50 19.00	31.96	18.64 19.14	31.88	18.78 19.29		18.92 19.43	37
39	33.77	19.50	33.69	19.65	33.60	19.79	33.52	19.94	39
	34.64		34.55			20.30		20.45	40
41 42	35.51 36.37	$20.50 \\ 21.00$	35.42 36.28	20.65 21.16		20.81 21.32	36.10	20.96 21.47	41 42
43	37.24	21.50	37.14 38.01	21.66	37.05	21.82 22.33	36.95	21.99	43
45	38.97	$22.00 \\ 22.50$	38.87	22.67	38.77	22.84	38.67	22.50 23.01	44 45
	39.84 40.70	$23.00 \\ 23.50$	39.74 40.60			23.35 23.85		23,52 24.03	46 47
48	41.57	24.00	41.46	24.18	41.36	24.36	41.25	24.54	48
49 50	42.44 43.30	24.50 25.00	42.33 43.19			24.87 25.38	42.11 42.97		49 50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
Ā	60]	Deg.	593	Deg.	$59\frac{1}{2}$	Deg.	591	Deg.	ā

D	30	Deg.	30¥	Deg.	30 <u>1</u>	Deg.	303	Deg.	D
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
51	44.17	25.50	44.06	25.69		25.88		26.08	51
52	45.03 45.90	26.00		$26.20 \\ 26.70$	44.80 45.67	26.39		26.59 27.10	52 53
54	46.77	27.00	46:65	27.90	46.53			27.61	54
55	47.63	27.50	47.51	27.71	47.39	27.91	47.27	28.12	55
56	48.50	28.00		28.21	48.25	28.42	48.13		56
57	49.36 50.23	28.00	49.24	28.72 29.22		28.93 29.44	48.99	29.14 29.65	57 58
59	51.10	29.50	50.97	29.72	50.84	29.94		30.17	59
60	51.96	30.00	51.83	30.23	51.70	30.45	51.56	30.68	60
61	52.83	30.50	52.69	30.73		30.96		31.19	61
62	53.69	31.00	53.56	31.23		31.47		31.70	62
	54.56			31.74		31.97 32.48		32.21	63 64
65	55.43 56.29	32.50		32.24 32.75		32.99		32.72 33.23	65
66	57.16	33.00	57.01	33.25		33.50		33.75	66
67	58.02	33.50		33.75		34.01	57.58	34.26	67
68	58.89	34.00	58.74	34.26		34.51	58.44	34.77	68 69
	59.76 60.62			34.76 35.26		35.02 35.53		35.28	70
71	61.49	35.50	61.33	35.77	61.18	36.04	61.02	36.30	71
72	62.35	36.00	62.20	36.27	62.04	36.54		36.81	72
73	63.22	36.50		36.78		37.05		37.32	73
74	64.09	37.00 37.50		$37.28 \\ 37.78$		37.56		37.84	74
		38.00		38.29		38.57		38.86	
		38.50		38.79		39.08		39.37	
78	67.55	39.00		39.29		39.59		39.88	
		39.50 40.00		39.80		40.10	67.89	40.39	
						!			
	70.15		69.97	40.81		41.11		41.41	81 82
		41.00 41.50	71.70	$41.31 \\ 41.81$		42.13		41.93	
		42.00		42.32		42.63		42.95	
		42.50		42.82		43.14		43.46	
	74.48		74.29			43.65		43.97	
	75.34	43.50		43.83 44.33		44.16		44.48	
	77.08		76.88			45.17	76.49		1
		45.00		45.34		45.68	77.35		
	78.81		78.61	45.84		46.19	78.2		
		46.00 46.50		46.35 46.85		46.69		47.04	
		47.00		47.35		47.71		48.06	
95	82.27	47.50	82.06	47.86	31.85	48.22	81.64	48.57	95
		48.00		48.36		48.72		49.08	
98	84.00	48.50 49.00		48.87 49.37		49.23		649.60 50.11	97
		49.50		49.87		50.25		50.62	
		50.00		50.38		50.75		51.13	100
)ist.		Lat.		Lat.		Lat.		Lat.)ist.
	60	Deg	159 <u>3</u>	Deg.	159 <u>1</u>	Deg.	59 <u>↓</u>	Deg.	1

	31	Deg.	311	Deg.	311	Deg.	313	Deg.	E
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1	0.86		0.85	0.52	0.85	0.52	0.85	0.53	1
2	1.71	1.03	1.71	1.04	1.71	1.04	1.70	1.05	2
34	2.57	1.55 2.06	2.56	1.56	2.56		2.55	1.58	3
5	4.29	2.58	4.27			2.61	4.25	2.63	5
6	5.14	3.09	5.13	3.11		3.13	5.10	3.16	6
7	6.00	3.61	5.98	3.63	5.97		5.95	3.68	-7
8 9	6.86 7.71	4.12	6.84	4.15	6.82 7.67	4.18	6.80 7.65	4.21	9
10	8.57	5.15	8.55	5.19	8.53	5.22	8.50	5.26	10
11	9.43	5.67	9.40	5.71	9.38	5.75	9.35	5.79	11
	10.29 11.14		10.26	6.23	10.23	6.27 6.79	10.20	6.31 6.84	12 13
	12.00	6.70	11.97	7.26	11.08	7.31	11.90	7.37	14
15	12.86	7.73	12.82	7.78	12.79	7.84	12.76	7.89	15
16	13.71	8.24	13.68	8.30	13.64	8.36	13.61	8.42	16
	14.57 15.43	8.76	14.53 15.39	8.82 9.34	14.49	8.88 9.40	14.46	8.93 9.47	17 18
	16.29	9.79	16.24		16.20	9.93		10.00	
	17.14	10.30		10.38		10.45			20
	18.00			10.89		10.97	17.86		21
22	18.86 19.71	11.33	18.81 19.66	11.41	18.76 19.61	11.49	18.71 19.56		22 23
24	20,57	12.36	20.52				20.41		24
	21.43		21.37	12.97		13.06			25
	22.29		22.23		22.17	13.58			26
27	23.14 24.00	13.91	23.08	14.01 14.53	23.02	14.11 14.63	22.96		27 28
	24.86		24.79		24.73		24.66		29
30	25.71	15.45	25.65			15.67	25.51		30
31	26.57	15.97	26.50		26.43		26.36		31
32	27.43	16.48	27.36 28.21	16.60	27.28		27.21 28.06		32 33
34	29.14	17.51	29.07			$17.24 \\ 17.76$			34
35	30.00	18.03	29.92	18.16	29.84	18.29	29.76	18.42	35
36	30.86	18.54	30.78	18.68	30.70		30.61		36 37
38	31.72 32.57	19.06	31.63 32.49		31.55 32.40		31.46 32.31		38
39	33.43	20.09		20.23			33.16		39
40	34.29	20.60	34.20	20.75	34.11		34.01	21.05	40
41	35.14	21.12	35.05		34.96		34.86		41 42
42	36.00 36.86	21.63	35.91 36.76		35.81 36.66		$35.71 \\ 36.57$		42
44	30.80	22.66	37.62		37.52		37.42		44
45	38.57	23.18	38.47	23.34	38.37	23.51	38.27	23.68	45
	39.43		39.33		39.22		39.12		46
48	40.29 41.14	24.21		24.38 24.90	40.07 40.93		39.97 40.82		48
	42.00		41.89		41.78		41.67	25.78	49
		25.75		25.94	42.63		42.52		50
st.	-	Lat.	-	Lat.		Lat.	Dep.		ist.
ā	59 I	Deg.	583]	Deg.	$58\frac{1}{2}$]	Deg.	581	Deg.	91

				-					
0	31	Deg.	314	Deg.	$31\frac{1}{2}$	Deg.	313	Deg.	D
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist:
51		26.27	43.60			26.65	43.37 44.22	26.84	51
		26.78	44.46			27.17 27.69	44.22	27.30	52 53
	46.29		46.17	28.01		28.21	45.92		54
55	47.14	28.33	47.02	28.53	46.90	28.74	46.77	28.94	55
		28.84	47.88			29.26	47.62		56
	40.00	29.36 29.87	48.73 49.58			29.78 30.30	48.47	29.99	57 58
	50.57		50.44			30.83		31.05	59
		30.90	51.29			31.35		31.57	60
61	52.29	31.42	52.15	31.65	52.01	31.87	51.87	32.10	61
62	53.14	31.93	53.00	32.16	52.86	32.39		32.63	62
63	54.00 54.86	32.45	53.86 54.71	32.68		32.92 33.44	53.57	33.15 33.68	63
	55.72		55.57			33.96	54.42		64
	56.57		56.42	34.24		34.48	56.12	34.73	66
	57.43		57.28		57.13		56.98 57.82	35.26	67
	58.29		58.13			35.53			-68
	59.14 60.00		58.99 59.84			36.05 36.57	58.67 59.52	36.83	69 70
71	60.86		60.70			37.10		37.36	71
	61.72		61.55			37.62	61.23 62.08	37.89	72
	62.57 63.43		62.41 63.26			38.14 38.66		38.94	73
75	64.29	38.63	64.12	38.91		39.19	63.78	39.47	75
	65.14		64.97	39.43	64.80	39.71		39.99	76
	66.00		65.83			40.23	65.48	40.52	77
78	66.86 67.72	40.17	66.68 67.54		67.36	40.75 41.28	66.33	41.04	78 79
	68.57		68.39			41.80		42.10	80
81		41.72	69.25			42.32		42.62	81
82 83	71.14	42.23	70.10			42.84 43.37		43.15 43.68	82
	72.00		71.81			43.89		44.20	84
85	72.86	43.78	72.67	44.10	72.47	44.41	72.28	44.73	85
	73.72		73.52			44.93		45.25	86
	74.57 75.43		74.38			45.46 45.98	73.98	45.78	87
	76.29		76.09			46.50	75.68		89
90	77.15	46.35	76.94	46.69	76.74	47.02	76.53	47.36	90
	78.00 78.86		77.80			47.55		47.89	91 92
	18.80		79.51			48.07		48.41	92
94	80.57	48.41	80.36	48.76		49.11		49.47	94
	81.43		81.22			49.64		49.99	95
	82.29 83.15		82.07 82.93			50.16		50.52 51.04	96
	84.00		83.78			51.20		51.57	98
99	84.86	50.99	84.64	51.36	84.41	51.73	84.18	52.10	99
100	85.72	51.50	85.49	51.88	85.26	52.25		52.62	100
ist.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	ist.
A	59 1	Deg.	583	Deg.	$58\frac{1}{2}$	Deg.	581	Deg.	0

D	32]	Deg.	$32\frac{1}{4}$ l)eg.	32 <u>1</u>	Deg.	3241	Deg.	E
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
12	0.85	0.53	0.85	0.53	0.84	0.54	0.84	0.54	1
ŝ	2.54	1.06	1.69 2.54	1.07	1.69 2.53	1.07	1.68 2.52	1.08	23
4	3.39	2.12	3.38	2.13	3.37	2.15	3.36	2.16	45
5	4.24	2.65	4.23	2.67	4.22	2.69	4.21	2.70	
67	5.09 5.94	3.18 3.71	5.07 5.92	3.20 3.74	5.06 5.90	3.22 3.76	5.05 5.89	3.25 3.79	6 7
8	6.78	4.24	6.77	4.27	6.75	4.30	6.73	4.33	8
9	7.63	4.77	7.61	4.80	7.59	4.84	7.57	4.87	9
10	8.48	5.30	8.46	5.34	8.43	5.37	8.41	5.41	10
11	9.33	5.83	9.30	5.87	9.28	5.91	9.25	5.95	11
12	10.18	6.36	10.15	6.40	10.12	6.45	10.09	6.49	12
	11.02 11.87	6.89 7.42	10.95	6.94	10.96 11.81	6.98	10.93	7.03	13
	12.72		$11.84 \\ 12.69$	7.47 8.00	12.65	7.52 8.06	11.77 12.62	7.57	14 15
	13.57	8.48	13.53	8.54	13.49	8.60	13.46		16
	14.42		14.38	9.07	14.34	9.13	14.30		17
	15.26		15.22	9.61	15.18	9.67	15.14	9.74	
	$16.11 \\ 16.96$	10.07 10.60	16.07 16.91	10.14 10.67	16.02 16.87	$10.21 \\ 10.75$	$15.98 \\ 16.82$	10.28 10.82	19 20
21	17.81	11.13	17.76	11.21	17.71	11.28	17.66	11.36	21
22			18.61	11.74	18.55	11.82		11.90	
23	19.51	12.19	19.45	12.27		12.36		12.44	
	20.35	12.72		12.81 13.34		$12.90 \\ 13.43$		12.98	24 25
26	22.05	13.78	21.99	13.87		13.97	21.87		26
27	22.90	14.31		14.41	22.77	14.51	22.71		27
		14.84		14.94	23.61	15.04		15.15	
29 30	24.59	15.37 15.90	24.53 25.37	15.47 16.01		$15.58 \\ 16.12$		15.69	
31	26.29	16.43	26.22	16.54	26.15	16.66	26.07	16.77	31
32	27.14	16.96		17.08		17.19		17.31	
33	27.99	17.49		17.61		17.73		17.85	
35	28.83		28.75	18.14 18.68	28.08	18.27	29.44	18.39	
		19.08		19.21		19.34		19.48	
37	31.38	19.61	31.29	19.74	31.21			20.02	
30	32.23	20.14		20.28 20.81	32.05		31.96	20.56	38 39
		21.20		21.34		21.49		21.64	40
41	34.77	21.73	34.67			22.03		22.18	
42	35.62	22.26				22.57		22.72	
	36.4	22.79			36.27	23.10		23.26	
45	38.16	23.85	37.21	23.48	37.95	23.64 24.18		23.80	
46	39.0	24.38	38.90	24.55	38.80	24.72	38.69	24.88	3 46
47	39.8	6 24.91	39.75			25.25	39.53		
40	40.7	1 25.44	40.59	25.61		25.79		25.97	
		26.50		26.15 26.68		26.33 26.86		26.51	
st.	Dep	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
ä	58	Deg.	573	Deg.	571	Deg.	571	Deg.	Di

-	1					-	-		
U	32	Deg.	$32\frac{1}{4}$	Deg.	$32\frac{1}{2}$	Deg.	$32\frac{3}{4}$	Deg.	D
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
51		27.03	43.13			27.40	42.89		51
	44.10 44.95		43.98	27.75 28.28		27.94 28.48	43.73 44.58		52 53
	45.79		45.67	28.82	45.54	29.01	45.42		54
55	46.64	29.15	46.51	29.35	46.39	29.55	46.26	29.75	55
	47.49			29.88	47.23		47.10		56
57	48.34 49.19	30.21	48.21 49.05	30.42 30.95	48.07 48.92		47.94 48.78		57 58
	50.03		49.90	31.48		31.70	49.62		59
	50.88			32.02		32.24	50:46		60
61	51.73	32.33		32.55	51.45	32.78	51.30	33.00	61
	52.58		52.44	33.08	52.29		52.14		62
	53.43 54.28			$33.62 \\ 34.15$	53.13 53.98	33.85	52.99 53.83		63 64
	55.12			34.68	54.82		54.67		65
66	55.97	34.97		35.22	55.66	35.46	55.51		66
67	56.82	35.50		35.75	56.51	36.00	56.35		67
	57.67 58.52			36.29 36.82		36.54 37.07	57.19 58.03		68 69
	59.36		59.20			37.61	58.87		70
	60.21			37.89	59.88	38.15	59.71		71
	61.06 61.91			$38.42 \\ 38.95$	60.72		60.55		72 73
	62.76			39.49	61.57 62.41	39.22 39.76	61.40 62.24		74
75	63.60	39.74	63.43	40.02	63.25		63.08		75
	64.45			40.55	64.10	40.83	63.92		76
		40.80 41.33		41.09 41.62	64.94 65.78	41.37	64.76		77
		41.86	66.81		66.63	41.91 42.45		42.20 42.74	79
		42.39		42.69	67.47			43.28	80
81		42.92 43.45		43.22 43.76	68.31	43.52		43.82	81
		43.98		44.29		44.06		44.36 44.90	82 83
84	71.24	41.51		44.82	70.84			45.44	84
	72.08			45.36	71.69	45.67	71.49	45.98	85
86	72.93	45.57		45.89 46.42		46.21		46.52 47.06	86
88	74.63	46.63		46.96		46.75 47.28		47.61	87 88
89	75.48	47.16	75.27	47.49	75.06	47.82		43.15	89
90	76.32	47.69	76.12	48.03	75.91	48.36	75.69	48.69	90
91 92		48.22		48.56	76.75	48.89 49.43		49.23 49.77	91 92
93		49.28		49.63	78.44			50.31	93
94	79.72	49.81	79.50	50.16	79.28	50.51	79.06	50.85	94
		50.34		50.69	80.12			51.39	95
	82.26	50.87 51.40		51.23 51.76	80.97 81.81	51.58 52.12		51.93 52.47	96 97
98	83.11	51.93	82.88	52.29	82.65	52.66		53.02	98
		52.46		52.83	83.50	53.19	83.26	53.56	99
100		52.99		53.36		53.73		54.10	100
ist.	Dep.	·		Lat.		Lat.			ist.
P	58	Deg.	573	Deg.	$57\frac{1}{2}$	Deg.	571	Deg.	P

D	33	Deg.	331	331	3312Deg. 832Deg.			B	
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Dist.
1	0.84	0.54	0.84	0.55	0.83		0.83	0.56	11
23	1.68	1.09	1.67	1.10	2.50	1.10	1.66	1.11	23
4	3.35	2.18	3.35	2.19	3.34		2.49	1.67	4
5	4.19	2.72	4.18	2.74	4.17	2.76	4.16	2.78	5
67	5.03	3.27	5.02	3.29	5.00		4.99	8.33	6
8	5.87	3.81 4.35	5.85 6.69	3.84 4.39	5.84	3.86	5.82	3.89	78
9	7.55	4.90	7.53	4.93	7.50	4.97	7.48	5.00	9
10	8.39	5.45	8.36	5.48	8.34	5.52	8.31	5.56	10
	9.23	5.99	9.20	6.03	9.17	6.07	9.15	6.11	11
	10.06	6.54	10.04		10.01	6.62	9.98	6.67	12
	10.90 11.74	7.08	10.87 11.71	7.13	10.84	7.18	10.81	7.22	13
	12.58	8.17	12.54	7.68	11.67 12.51	7.73	11.64	7.78	14 15
16	13.42	8.71	13.38	8.77	13.34	8.83	13.30	8.89	16
	14.26	9.26	14.22	9.32	14.18	9.38	14.13	9.44	17
	15.10 15.93	9.80	15.05 15.89	9.87	$15.01 \\ 15.84$	9.93	14.97 15.80	10.00	18 19
	16.77	10.89	16.73		16.68	10.49 11.04	16.63	10.56 11.11	20
	17.61		17.56		17.51	11.59	17.46		21
	18.45 19.29		18.40	12.06	18.35	12.14		12.22	22 23
	20.13		19.23 20.07	12.61	19.18 20.01			12.78 13.33	23
	20.97		20.91			13.20		13.89	25
	21.81		21.74	14.26	21.68	14.35	21.62	14.44	26
	22.64		22.58		22.51			15.00	27
	$23.48 \\ 24.32$		23.42 24.25		23.35 24.18	$15.45 \\ 16.01$		15.56	28 29
	25.16		25.09		0 - 00	16.56		16.67	30
	26.00		25.92		25.85	17.11		17.22	31
	26.84 27.68		26.76 27.60		26.68 27.52	17.66		17.78 18.33	82 33
34	28.51	18.52	28.43			18.77		18.89	34
35	29.35	19.06	29.27	19.19	29.19	19.32	29.10	19.44	35
36	30.19	19.61	30.11			19.87		20.00	36
38	31.03	20.15	30.94 31.78		30.85 31.69	20.42 20.97	30.76	20.56 21.11	37 38
39	32.71	20.70 21.24	32.62	21.38	32.52	21.53	32.43	21.67	39
40	33.55	21.79		21.93	33.36	22.08		22.22	40
	34.39		34.29		34.19		34.09		41
	35.22		35.12 35.96		35.02 35.86	23.18 23.73	34.92 35,75	23.33 23.89	42
44	36.90	23.96	36.80		36.69		36.58	24.45	44
45	37.74	24.51	37.63	24.67	37.52	24.84	37.42	25.00	45
46	38.58 39.42	25.05	38.47		38.36	25.39	38.25	25.56 26.11	46 47
	40.26		39.31 40.14		39.19 40.03			26.11 26.67	47
49	41.09	26.69	40.98		40.86		40.74		49
	41.93		41.81		41.69		41.57		50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	ist.
ā	57]	Deg.	563 Deg. 561		561	Deg. 561 Deg		Deg.	ā

10	33	Deg.	334	Deg.	331	Deg.	3331	Deg.	D
ist	Tat	Dep.	Lat	Dep.	Lat	Den	Lat	Dep.	ist.
-	Liat.	Deb.	Lat.	Dep.	Lat.	Dep.		Dep.	-
		27.78		27.96		28.15	42.40		51
		28.32	43.49	28.51 29.06		28.70 29.25	43.24 44.07		52 53
	44.45 45.29			29.61		29.80	44.90		54
55	46.13	29.96	46.00	30.16	45.86	30.36	45.73	30.56	55
		30.50	46.83			30.91	46.56 47.39	31.11	56
	47.80	31.04 31.59	47.67	31.25	48.37	31.46 32.01	48.23		57 58
		32.13	49.34	32.35	49.20	32.01 32.56	49.06	32.78	59
60	50.32	32.68	50, 18	32.90	50.03	33.12	49.89	33.33	60
61	51.16	33.22	51.01	33.45	50.87	33.67	50.72	33.89	61
	52.00		51.85		51.70	34.22			62
63	52.84	34.31	52.69				52.38		63
	53.67 54.51	34.86 35.40		35.09 35.64		35.32 35.88			64 65
	55.35			36.19		36.43			66
		36.49		36.74		36.98			67
		37.04 37.58		37.28 37.83		37.53 38.08	57.97		68 69
	58.71			38.38		38.64			70
		38.67		38.93		39.19			71
		39.21 39.76		39.48 40.03		39.74 40.29	59.87		72 73
		40.30		40.57		40.84		41.11	74
		40.85		41.12			62.36		75
		41.39 41.94		41.67 42.22		41.95 42.50	63.19 64.02	42.22	76
		42.48		42.77		43.05		43.33	78
		43.03		43.32		43.60			79
80	67.09	43.57	66.90	43.86	66.71	44.15	66.52	44.45	80
81	67.93	44.12	67.74	44.41	67.54	44.71	67.35	45.00	81
82	68.77	44.66		44.96		45.26			82
		45.20		45.51		45.81			83
		45.75 46.29		46.06		46.36		46.67	84 85
86	72.13	46.84		47.15		47.47		47.78	86
87	72.96	47.38	72.76	47.70	72.55	48.02	72.34	48.83	87
		47.93 48.47		48.25 48.80	73.38	48.57	73.17	48.89 49.45	88 89
		49.02		49.35		49.67	74.83	50.00	90
-									
		49.56 50.11		49.89 50.44		50.23 50.78	75.66	50.56 51.11	91
		50.65		50.99		51.33		51.67	92 93
94	78.83	51.20	78.61	51.54	78.39	51.88	78.16	52.22	94
95		51.74		52.09		52.43		52.78	95
		52.29 52.83		52.64		52.99 53.54		53.33 53.89	96 97
98	82.19	53.37	81.96	53.73	81.72	54.09		54.45	98
		53.92		54.28	82.55	54.64	82.32	55.00	99
100	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	100
4	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
is		-	-		-				Dist
P	57	Deg.	563	Deg.	561	Deg.	561	Deg.	A
	Concession in the	No. of Concession, name	-		and some from				

-				_				2	
	34	Deg.	$34\frac{1}{4}$	Deg.	$34\frac{1}{3}$	Deg.	34 ³	Deg.	D
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1	0.83	0.56	0.83	0.56	0.32	0.57	0.82	0.57	1
23	1.66 2.49	1.12	1.65 2.48	1.13	1.65	1.13	1.64	1.14	23
4	3.32	2.24	3.31	1.69 2.25	2.47	$1.70 \\ 2.27$	2.46	1.71 2.28	3
5	4.15	2.80	4.13	2.81	4.12	2.83	4.11		5
6	4.97	3.36	4.96	3.38	4.94	3.40	4.93		6
7	5.80	3.91	5.79	3.94	5.77	3.96	5.75		
8	6.63	4.47	6.61	4.50	6.59	4.53	6.57		
9 10	7.46 8.29	5.03	7.44	5.07	7.42		7.39		
10	0.20	5.59	0.21	5.63	8.24	5.66	8.22	5.70	10
11	9.12	6.15	9.09	6.19	9.07	6.23	9.04	6.27	11
12	9.95	6.71	9.92	6.75	9.89		9.86		
13	10.78	7.27	10.75	7.32	10.71		10.68		13
14	11.61	7.83	11.57	7.88	11.54	7.93	11.50		
	12.44 13.26		12.40	8.44	12.36		12.32		
	13.20		$13.23 \\ 14.05$	9.00 9.57	13.19	9.06 9.63	13.15 13.97		
		10.07		10.13	14.83			10.26	
		10.62	15.71	10.69	15.66			10.83	
		11.18	16.53		16.48			11.40	
01									
21		11.74 12.30		11.82	17.31	11.89 12.46		11.97	
23	10.24	12.30	18.18	$12.38 \\ 12.94$		12.46		12.54 13.11	
24	19.90	13.42		13.51		13.59		13.68	
25	20.73	13.98		14.07		14.16		14.25	
26	21.55	14.54		14.63	21.43	14.73		6 14.82	
27	22.38	15.10	22.32	15.20	22.25	15.29	22.18	3 15.39	27
28	23.21	15.66		15.76	23.08	15.86		15.96	
29	24.04	16.22		16.32		16.43		3 16.53	
	24.87	16.78	24.80	16.88	24.12	16.99	24.65	5 17.10	30
31	25.70	17.33	25.62	17.45	25.55	17.56	25.47	17.67	31
32	26.53	17.89		18.01		18.12	26.29	18.24	
33	27.36	18.45		18.57	27.20	18.69		18.81	
34	28.19	19:01		19.14		19.26		19.38	
35	29.02	19.57		19.70	28.84	19.82		5 19.95	
37	29.05	20.13 20.69		$20.26 \\ 20.82$	30.40	20.39 20.96		3 20.52) 21.09	
38	31.50	20.09		21.39	31.32	21.52		21.66	
39	32.33	21.81		21.95		22.09		1 22.23	
40	33.16	22.37	33.06	22.51	32.97	22.66		7 22.80	
41	33.99	22.93	33.89	23.07	33.79	23.22	33.69	23.37	41
		23.49		23.64		23.79		23.94	
43	35.65	24.05	35.54	24.20		24.36		3 24.51	43
		24.60		24.76		24.92		5 25.08	
		25.16		25.33		25.49		25.65	
46	38.14	25.72	38.02	25.89		26.05) 26.22 2 26.79	
41	30.90	26.28	30.80			26.62		25.79	
49	40 69	20.64	40.50	27.58		27.75		27.93	
		27.96	41.33	28.14		28.32		28.50	
t.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep	Lat.	st.
Ois	56	Deg.	553	Dea	551	Der	551	Der	Die
	00	Deg.	004	Deg.	002	Leg.	4	Deg.	1

-	94	Dor	13411	Dogi	2411	Deg.	2431	Dog	
D	04	Deg.	4	Jeg.	0421	Jeg.		Jeg.	Di
st.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
			42.16			28.89	41.90		51
			42.98		42.85	29.45		29.64	52
			43.81 44.64			30.02	43.55	30.21	53 54
					45.33			31.35	55
56	46.43	31.31	45.46 46.29	31.52	46.15	31.72	46.01	31.92	56
57	47.26	31.87		32.08		32.29		32.49	57
			47.94 48.77			32.85 33.42		33.06	58 59
		33.55	49.60			33.98		34.20	60
61	50.57	84 11	50 49	34.33	50 97	34.55	50.12	34.77	61
	51.40	34.67	51.25	34.89		35.12		35.34	62
63	52.23	35.23	52.08	35.46		35.68		35.91	63
64	53.06	35.79 36.35		36.02		36.25 36.82		36.48	64
66	55.89 54.72	36.91	53.73 54.55	37.15		37,38		37.05	65 66
67	55.55	37.46		37.71		37.95		38.19	
68	56.37	38.03		38.27		38.52	55.87	38.76	68
69	57.20	38.58		38.83		39.08		39.33	
	58.03	39.14	57.80	39.40	57.69	39.65	51.52	39.90	70
		39.70		39.96		40.21		40.47	
		40.26		40.52				41.04	
		40.82	61.17	41.08	60.10	41.35		41.61	
		41.94		42.21				42.75	
			62.82	42.77	62.63	43.05		43.32	
		43.06		43.34	63.46	43.61		43.89	
		43.62 44.18		43.90 44.46		44.18 44.75		44.46	
		44.74		45.02				45.60	
81	67.15	45.29	66.95	45.59	66.75	45.88	66.55	46.17	81
		45.85		46.15		46.45		46.74	
		46.41		46.71		47.01 47.58		47.31	
		46.97 47.53		47.28 47.84		47.58		47.88	
		48.09		48.40		48.71		49.02	
		48.65		48.96		49.28	71.48	49.59	87
		49.21	72.74	49.53 50.09		49.84		50.16	
		49.77 50.33		50.65	74.17	50.98		50.73 51.30	
91	75.44	50.89	75.22	51.22	75.00	51.54	74.77	51.87	91
92	76.27	51.45	76.05	51.78	75.82	52.11	75.59	52.44	92
		52.00		52.34 52.90		52.68		53.01	
		52.56		52.90		53.24 53.81		53.58 54,15	
96	79.59	53.68	79.35	54.03	79.12	54.37	78.88	3 54.72	96
97	80.42	54.24	80.18	54.59	79.94	54.94	79.70	55.29	97
98	81.25	54.80	81.01	55.15	80.76	55.51		55.86	
						56.64		56.43	
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
ā	56	Deg.	553	Deg.	551	Deg.	55!	Deg.	Dis

		_			-			-	-
	35	Deg.	351	Deg.	$35\frac{1}{2}$	Deg.	354	Deg.	J
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1		0.57	0.82	0.58	0.81	0.58	0.81		
23		1.15	1.63	1.15	1.63	1.16	1.62		2
4		1.72 2.29	2.45	1.73	2.44	1,74 2.32	2.43		
5	4.10	2.87	4.08	2.89	4.07	2.90	4.06		
6		3.44	4.90	3.46	4.88	3.48			
78		4.01 4.59	5.72 6.53	4.04	5.70	4.06	5.68		
9		5.16	7.35	5.19	7.33	5.23	7.30		
10		5.74	8.17	5.77	8.14		8.12		
11		6.31	8.98	6.35	8.96	6.39	8.93		
	.9.83	6.88	9.80	6.93	9.77	6.97	9.74		
	10.65	7.46	10.62	7.50	10.58	7.55	10.55		
	12.29	8.60	12.25	8.66	12.21	8.71	12.17		
	13.11	9.18	13.07	9.23	13.03	9.29	12.99		16
	13.93 14.74	9.75	13.88 14.70		13.84	9.87	13.80	9.93	
19	15.56	10.92	15.52			11.03		11.10	
	16.38		16.33			11.61		11.68	
	17.20		17.15			12.19		12.27	
22	18.02 18.84	12.62		12.70	17.91 18.72	12.78		12.85	
24	19.66	13.19	18.78 19.60		19.54	13.94		13.44	
25	20.48	14.34	20.42		20.35	14.52	20.29	14.61	25
	21.30			15.01				15.19	
	22.12 22.94		22.05	15.58	21.98	15.68		15.77	
	23.76		23.68	16.74	23.61	16.84		16.94	
30	24.57	17.21	24.50	17.31	24.42	17.42	24.35	17.53	30
31	25.39	17.78	25.32		25.24			18.11	31
32	26.21 27.03	18.35	26.13		26.05	18.58		18.70 19.28	
34	27.85	19.50	26.95 27.77			19.10			
35	28.67	20.08	28.58	20.20	28.49	20.32	28.41	20.45	35
36	29.49	20.65	29.40		29.31	20.91	29.22	21.03	36
38	30.31 31.13	21.22	30.22 31.03		30.12 30.94			21.62 22.20	
	31.95		31.85		31.75			22.79	39
	32.77		32.67		32.56	23.23	32.46	23.37	40
	33.59		33.48		33.38		33.27	23.95	
42	34.40	24.09	34.30 35.12		34.19 35.01		34.90	24.54	42 43
	36.04		35.93	25.39	35.82		35.71		43
45	36.86	25.81	36.75	25.97	36.64	26.13	36.52	26.29	45
46	37.68	26.38	37.57		37.45		37.33		46
48	38.50 39.32	20.96	38.38 39.20		38.26 39.08		38.14 38.96		47 48
49	40.14	28.11	40.02	28.28	39.89	28.45	39.77	28.63	49
50	40.96	28.68	40.83		40.71	29.04	40.58	29.21	50
ist.	-		Dep.				Dep.		st.
A	55 I	Deg.	543I	Deg.	$54\frac{1}{2}$)eg.	544	Deg.	ā

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D	35	Deg.	351	Deg.	$35\frac{1}{2}$	Deg.	354	Deg.	D
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
51	41.78	29.25 29.83		29.43 30.01		29.62 30.20	41.39	29.80 30.38	51 52
		30.40		30.59	42.33	30.20		30.97	53
54	44.23	30.97	44.10		43.96	31.36	43.82	31.55	54
55	45.05 45.87	31.55 32.12	44.92	31.74 32.32	44.78	31.94 32.52	44.64	32.13 32.72	55 56
57	46.69	32.69	46.55	32.90	46.40	33.10	46.26	33.30	57
58	47.51	33.27	47.37			33.68 34.26	47.07	33.89	58 59
	48.33 49.15			34.63		34.84		34.47 35.05	60
61	49.97	34.99	49.82	35.21	49.66	35.42	49.51	35.64	61
62	50.79	35.56	50.63	35.78	50.48	36.00	50.32	36.22	62
	51.61 52.43			36.36 36.94		36.58 37.16	51.13	36.81 37.39	63 64
	53.24		53.08			37.10	52.75	37.98	65
66	54.06	37.86	53.90	38.09	53.73	38.33	53.56	38.56	66
	54.88 55.70		54.71	38.67 39.25		38.91 39.49	54.38	39.14	67 68
	56.52		56.35	39.82		40.07	56.00	39.73 40.31	69
	57.34			40.40		40.65		40.90	70
	58.16			40.98		41.23		41.48	71
	58.98 59.80		58.80 59.61		58.62	41.81 42.39	58.43 59.24	42.07	72 73
	60.62		60.43		60.24			42.03	13
75	61.44	43.02	61.25	43.29	61.06	43.55	60.87	43.82	75
	62.26 63.07		62.06 62.88	43.86	61.87	44.13	61.68		76
	63.89		63.70	45.02	62.69 63.50	44.71	62.49 63.30	45.57	77
79	64.71	45.31	64.51	45.59	64.32	45.88	64.11	46.16	79
80	65.53	45.89	65.33	46.17	65.13	46.46	64.93	46.74	80
	66.35		66.15		65.94	47.04	65.74		81
82 83	67.17 67.99	47.61	66.96 67.78		66.76 67.57	47.62	66.55 67.36		82 83
84	68.81	48.18	67.78 68.60	48.48	68.39	48.78	68.17		84
85	69.63	48.75	69.41		69.20	49.36	68.98		85
87	70.45 71.27	49.90	70.23 71.05		70.01 70.83		69.80 70.61	50.25	86 87
88	72.09	50.47	71.86	50.79	71.64	51.10	71.42	51.41	88
	72.90		72.68 73.50		72.46	51.68	72.23		89
	73.72				73.27		73.04	52.58	90
91	74.54	52.20	74.31		74.08	52.84	73.85		91
93	75.36 76.18	53.34	75.95		74.90 75.71	54.01	74.66		92 93
94	77.00	53.92	76.76	54.25	76.53	54.59	76.29		94
	77.82 78.64	\$4.49 55 OC	77.58		77.34	55.17	77.10		95
	79.46		79.21		78.16 78.97	56.33	77.91 78.72		96 97
98	80.28	56.21	80.03	56.56	79.78	56.91	79.53	57.26	98
	81.10 81.92		80.85 81.66	57.14 57.71	80.60 81.41	57.49 58.07	80.35		99 100
	Dep.		Dep.	Lat.	Dep.		Dep.		
IS									list
-	00 1	Jeg.	54 ³ I	reg.	0421	Deg.	54 1 L	Jeg.	-1

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-	36]	Der	36 <u>1</u>	Der	361	Der	3631	Der	
Die									$\mathbf{\Sigma}$
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1	0.81	0.59	0.81	0.59	0.80		0.80	0.60	
23	-1.62 2.43	1.18	1.61	1.18	1.61	1.19 1.78	1.60 2.40	1.20	23
4	3.24	2.35	3.23	2.37	3.22	2.38	3.20		4
5	4.05	2.94	4.03	2.96	4.02	2.97	4.01		5
67	4.85 5.66	3.53	4.84	3.55	4.82	3.57 4.16	4.81 5.61	3.59 4.19	67
8	6.47	4.70	6.45	4.73	6.43	4.76	6.41		8
9	7.28	5.29	7.26	5.32	7.23	5.35	7.21	5.38	9
10	8.09	5.88	8.06	5.91	8.04	5.95	8.01	5.98	10
11	8.90	6.47	8.87	6.50	8.84	6.54	8.81		
12	9.71 10.52	7.05	9.68 10.48	7.10 7.69	9.65 10.45	7.14	9.61 10.42	7.18	
	11.33	8.23	11.29		11.25	8.33	11.22	8.38	14
	12.14	8.82	12.10	8.87	12.06	8.92	12.02	8.97	15
10	12.94 13.75	9.40 9.99	12.90 13.71	9.46	12.86	9.52	12.82	9.57	16
	14.56		14.52			10.71		10.17	11
	15.37		15.32	11.23	15.27	11.30		11.37	19
20	16.18	11.76	16.13	11.83	16.08	11.90	16.03	11.97	29
	16.99		16.94		16.88		16.83		21
	17.80		17.74 18.55		17.68		17.63	13.16 13.76	22 23
24	18.61 19.42	14 11	19.35		18.49 19.29		19.23		23
25	20.23	14.69	20.16	14.78	20.10	14.87	20.03	14.96	25
	21.03		20.97		20.90		20.83		26
28	21.84 22.65	15.87	21.77 22.58	16.56	21.70 22.51	16.65	21.63 22.44		27 28
29	23.46	17.05	23.39	17.15	23.31	17.25	23.24		29
30	24.27	17.63	24.19	17.74	24.12	17.84	24.04	17.95	30
31	25.08	18.22	25.00	18.33	24.92	18.44	24.84	18.55	31
32	25.89	18.81	25.81		25.72		25.64		32
	26.70 27.51		26.61 27.42		26.53 27.33		26.44 27.24		33
		20.57	28.23		27.55		28.04		34 35
36	29.12	21.16	29.03	21.29	28.94	21.41	28.85	21.54	36
	29.93 30.74		29.84 30.64		29.74 30.55	22.01	29.65 30.45		37
	30.74 31.55		31.45		31.35		31.25		38 39
	32.36		32.26		32.15			23.93	40
41	33.17	24.10	33.06	24.24	32.96		32.85	24.53	41
42	33.98	24.69	33.87		33.76	24.98	\$3.65	25.13	42
	34.79 35.60		34.68 35.48		34.57 35.37		34.45 35.26	25.73	43 44
45	36.41	26.45	36.29	26.61	36.17		36.06	26.92	44
46	37.21	27.04	37.10	27.20	36.98	27.36	36.86	27.52	46
	38.02	27.63 28.21	37.90 38.71		37.78 36.59		37.66 38.46		47
49	39.64	28.80	39.52	28.97		29.15	39.26		48 49
	40.45		40.32		40.19		40.06		50
8t.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
ā	54 1	Deg.	5341	Deg.	53 <u>1</u>	Deg.	531I	Deg.	ā

E	36	Deg.	361	Deg.	$36\frac{1}{2}$	Deg.	36 3	Deg.	E
list.		Dep.		Dep.		Dep.		Dep.	ist.
51	41.26	29.98 30.56	41.13	30.16	41.00	30.34	40.86	30.51 31.11	51
				30.75	41.80	30.93	41.67	31.11	52
		31.15 31.74		31.34 31.93	42.60	31.55	43.27	31.71 32.31	53 54
55	44.50	32.33		32.52	43.41 44.21	32.72	44.07	32.31 32.91	55
56	45.30	32.92	45.16	33.11	45.02	33.31	44.87	33.51	56
57	46.11	33.50 34.09	45.97	33.70 34.30	45.82 46.62	33.90	45.67	34.10 34.70	57 58
59	47.73	34.68		34.89		35.09	47.27	35.30	
		35.27	48.39	35.48		35.69	48.08	35.90	60
61	49.35	35.85	49.19	36.07	49.04	36.28	48.88	36.50	61
62	50.16	36.44 37.03	50.00	36.66	49.84	36.88	49.68	37.10 37.69	62
63	50.97	37.03 37.62	50.81	37.25	50.64	37.47	50.48	37.69	63 64
			52.42	38.44	51.45	38.66	52.08	38.29 38.89	65
66	53.40	38.79	53.23	39.03	53.05	38.66 39.26	52.88	38.89 39.49	66
		39.38	54.03	39.62	53.86	39.85	53.68	40.09	67
68	55.01	39.97	54.84	40.21	54.66 55.47	40.45		40.69	68 69
70	56.63	40.56 41.14	56.45	41.39	56.27	41.64		41.28	70
71	57 14	41.73	57 96	41.98	57 07	42.23	56 90	42.48	71
72	58.25	42.32		42.57		42.83			72
73	59.06	42.91	58.87	43 17	58.68	43.42 44.02	58.49	43.68	73
74	59.87	43.50 44.08	59.68	43.76	59.49	44.02	59.29	44.28	74
75	60.68	44.08		44.35	60.29		60.09 60.90		75 76
		45.26		45.53	61.90		61.70		77
78	63.10	45.85	62.90	46.12	62.70	46.40	62.50	46.67	78
		46.43 47.02				46.99 47.59			79 80
81	65.53	47.61			65.11	48.18	64.90		81 82
		48.79	66.93	48.49	65.92 66.72	49.37		49.06 49.66	83
84	67.96	49.37	67.74	49.67	67.52	49.97	67.31	50.26	84
85	68.77	49.96 50.55	68.55	50.26	68.33	50.56		50.86	85
80	69.58	50.55 51.14			69.13 69.94			51.46 52.05	86 87
88	71.19	51.73	70.97	52.04	70.74	52.34		52.65	88
89	72.00	52.31		52.04 52.63	71.54	52.94	71.31	53.25	89
90	72.81	52.90	72.58	53.22	72.35	53.53	72.11	53.85	90
		53.49	73.39			54.13	72.91	54.45	91
		54.08 54.66	74.19	54.40	73.95	54.72	73.72	55.05	92 93
94	76.05	55.25		55.58	75.56	55.32 55.91	75.32	56.24	
95	76.86	55.84		56.17	76.37	56.51	76.12	56.84	95
96	77.67	56.43	77.42	56.77	77.17	57.10	76.92	57.44	96
		57.02 57.60	79 02	57 95	78 78	57.70 58.29	78 59	58.04	97 98
		58.19	79.84	58.54	79.58	58.89	79.32	59.23	99
		58.78				59.48			
ist.	Dep.	Lat. Deg.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	ist.
A	54	Deg.	5331	Deg.	$53\frac{1}{2}$	Deg.	5311	Deg.	9

E	-	37	Ī	Deg	-	37	[] 4	Deg	•	37	1	Deg	•	37	PD	eg	r .	D
1	1st	La	t.	Dep		La	t.	Dep		La	t.	Dep	•	La	t.]1	Dej	p.	ist.
	12345	0.8 1.6 2.4 3.1 3.9	60 10 19	0.6 1.2 1.8 2.4 3.0	011	0.8 1.5 2.5 3.1 3.9	59 39 8	0.6 1.2 1.8 2.4 3.0	122	0.1 1.4 2.5 3.1 3.9	59 18 17	0.6 1.2 1.8 2.4 3.0	233	0.7 1.5 2.3 3.1 3.9	876	0.6 1.2 1.8 2.4 3.0	22	12345
1	6 7 8 9 0	4.7 5.5 6.3 7.1 7.9	9 9 9	3.6 4.2 4.8 5.42 6.02		4.7 5.5 6.3 7.1 7.9	7 7 6	3.63 4.24 4.84 5.45 6.05	1	4.7 5.5 6.3 7.1 7.9	554	3.68 4.26 4.87 5.48 6.09	3	4.7 5.5 6.3 7.1 7.9	3 3 2	3.6 4.2 4.9 5.5 6.1	901	6 7 8 9 10
1-	3 4 5	8.7 9.5 0.3 1.1 1.9	8 8 8 8	6.62 7.22 7.82 8.43 9.03		8.7 9.5 10.3 11.1	5 5 4	6.66 7.26 7.87 8.47 9.08		8.7 9.5 10.3 11.1 11.9	2 1 1 0	6.70 7.31 7.91 8.52 9.13		8.7 9.4 0.2 1.0 1.8	9 3 7 1 3	6.7 7.9 7.9 8.5 9.1	5 6 7	11 12 13 14 15
11	7 8 9	4.38	5 1 5 1 7 1	9.63 0.23 0.83 1.43 2.04		4.3	3 1 3 1 2 1	9.68 10.29 10.90 11.50 12.11		14.2 15.0	9 1 8 1 7 1	9.74 10.35 10.96 11.57 12.18	1	2.6 3.4 4.2 5.0 5.8		1.6	123	16 17 18 19 20
22222	21 31 41 51	7.57 8.37 9.17 9.97		2.64 3.24 3.84 4.44 5.05	1111	7.5 8.3 9.10 9.90		2.71 3.32 3.92 4.53 5.16		17.4 18.2 19.04 19.8		12.78 13.39 14.00 14.61 15.22	11111	6.60 7.40 8.19 8.98 9.77		1.08 1.69	7	21 22 23 24 25
2	72	$2.36 \\ 3.16$		5.65 5.25 5.85 7.45 8.05	22	1.49 2.29 3.08		5.74 6.34 6.95 7.55 8.16	NO NO NO	21.42 22.21 23.01		5.83 6.44 7.05 7.65 8.26	2 25 25	0.56 1.35 2.14 2.93 3.72	16 17 17	.14	3	26 27 28 29 30
32 33 34	222	4.76 5.56 6.35 7.15 7.95	19 19 20	.26 .86 .46	2222	5.47 6.27 7.06	112	8.76 9.37 9.97 0.58 1.19	0X 0X 0X	4.59 5.39 6.18 6.97	122	9.48 0.09 0.70	222	4.51 5.30 6.09 6.88 7.67	19 20 20	.59		31 32 33 34 35
36 37 38 39	52 2 3 3 3 3 3	8.75 9.55 0.35 1.15 1.95	21 22 22 23	.67 .27 .87 .47	2233	8.66 9.45 0.25 1.04	22222	1.79 2.40 3.00 3.61 4.21	N N N N N	8.56 9.35 0.15	2222	1.92 2.52 3.13 3.74	233	8.46 9.26 0.05 0.84 1.63	22 22 23 23	.04 .65 .26		36 37 38 39 40
42 43 44	3	2.74 3.54 4.34 5.14 5.94	25 25 26	.28 .88 .48	333	3.43 4.23 5.02	2220	4.82 5.42 6.03 6.63 7.24	3 3 3	2.53 3.32 4.11 4.91 5.70	222	5.57 6.18	32	2.42	25 26 26	.71 .33 .94	-	41 42 43 44
46 47 48 49	30 37 38 39	3.74 7.54 3.33 9.13	27 28 28 29	.68 .29 .89 .49	303	6.62 7.41 8.21 9.00	222	7.84 8.45 9.05 9.66 0.26	3939		22222	8.00 8.61 9.22 9.83	36 37 37 56		28 28 29 30	.16 .77 .39 .00	4 4 4	15 16 17 18 19 50
Dist.	D	ep.	I	at.	D	ep.	1	Lat.	••	Dep.	-	Lat.	D	ep.	L	at.	ict	
	5	3]	De	g.	5	2^{3}_{4}	D	eg.	5	$2\frac{1}{2}$	D	eg.	5	241	De	g.	F	1

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10	37	Deg.	374	Deg.	$37\frac{1}{2}$	Deg.	373	Deg.	10
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
51	40.73	30.89		30.87		31.05		31.22	
52	41.53	31.29		31.48		31.66 32.26		31.84	
	42.55			32.08 32.69		32.87	41.91	33.06	54
55	43.92	33.10		33.29		33.48	43.49	33.67	55
56	44.72	33.70	44.58	33.90	44.43	34.09	44.28	34.28	56
57	45.52	34.30		34.50		34.70		34.90	
58	46.32	34.91		35.11		35.31 35.92	45.86	35.51 36.12	58
	47.12 47.92			35.71 36.32		36.53		36.73	
	40 80	00 01			48.39	37.13	48.23	07 95	61
	48.72 49.52			36.92 37.53		37.74		37.35	
69	50.31	37.91	50.15	38.13		38.35		38.57	63
64	51.11	38.52	50.94	38.13 38.74	50.77	88.96	50.60	39.18	
65	51.91	39.12	51.74	39.34		39.57		39.79	65
	52.71		52.54			40.18 40.79		40.41	66
	53.51 54.31		53.33 54.13			41.40		41.02 41.63	
	55,11		54.92		54.74	42.00		42.24	
	55,90		55.72		55.53			42.86	
71	56.70	42.73	56.52	49 98	56.33	43.22	56.14	43.47	71
	57.50		57.31		57.12	43.83		44.08	72
	58,30		58.11			44.44	57.72		73
	59.10		58.90		58.71	45.05	58.51		
	59.90		59.70			45.66 46.27		45.92	75
	60.70 61.49		60.50 61.29			46.87	60.09 60.88	46.53	76
	62.29		62.09			47.48		47.75	
	63.09		62.88		62.67	49.09		48.37	79
80	63.89	48.15	63.68	48.42	63.47	48.70	63.26	48.98	80
	64.69		64.48	49.03	64.26		64.05	49.59	81
	65.49		65.27			49.92		50.20	
	66.29		66.07		66.64	50.53	65.63		83
	67.09 67.88		66.86 67.66		67.43	51.14	66.42 67.21		84
	68.68		68.46			52.35		52.65	
87	69.48	52.36	69.25		69.02	52.96		53.26	87
	70.28		70.05		69.82		69.58	53.88	
	71.08		70.84		70.61	54.18 54.79		54.49	
	71.85		71.64				11.16	55.10	90
	72.68		72.44		72.20	55.40		55.71	91
	73.47		73.23		73.78	56.01 56.61	72.74	56.32 56.94	92 93
	75.07		74.82		74.58	57.22		57.55	94
	75.87		75.62	57.50	75.37	57.83	75.12	58.16	
	76.67		76.42			58.44		58.77	96
97	77.47	58.38	77.21			59.05		59.39	97
	78.27		78.01			59.66 60.27	77.49	60.00	98 99
	79.86		79.60			60.88	79.07		100
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
Di	53	Deg.	523I)er	5211	Deg	5211	Dev	Di
_				8.1	- 2 -	8.	4	8.	

E	38	Deg.	381	Deg.	381	Deg.	38%	Deg.	E
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1	0.79	0.62	0.79	0.62	0.78	0.62	0.78	0.63	1
23	1.58	1.23	1.57 2.36	1.24 1.86	1.57	1.24 1.87	1.56	1.25	23
4	3.15	2.46	3.14	2.48	3.13	2.49	3.12	2.50	4
5	3.94	3.08 3.69	3.93 4.71	3.10 3.71	3.91 4.70	3.11 3.74	3.90		5
7	5.52	4.31	5.50	4.33	5.48	4.36	5.46	4.38	7
8 9	6.30 7.09	4.93 5.54	6.28 7.07	4.95 5.57	6.26 7.04	4.98 5.60	6.24		89
10	7.88	6.16	7.85	6.19	7.83	6.23	7.80		10
11	8.67	6.77	8.64	6.81	8.61	6.85	8.58 9.36	6.89	11
12 13	9.46	7.39	9.42 10.21	7.43	9.39	7.47 8.09	9.36		12 13
14	11.03	8.62	10.99	8.67	10.96	8.72	10.92	8.76	14
15 16	11.82 12.61	9.23 9.85	11.78 12.57	9.29 9.91	$11.74 \\ 12.52$	9.34 9.96	11.70	9.39	15 16
17	13.40	10.47	13.35	10.52	13.30	10.58	13.26	10.64	17
18 19	14.18	11.08 11.70	14.14	11.14 11.76	14.09	11.21 11.83		11.27	18 19
	15.76		14.92 15.71	12.38	15.65			12.52	
21	16.55		16.49	13.00	16.43	13.07		13.14	21
	$17.34 \\ 18.12$	13.54	17.28	13.62 14.24		13.70 14.32		13.77	
24	18.91	14.78	18.85		18.78			15.02	24
		15.39 16.01		15.48	19.57	15.56		15.65	25 26
20 27	21.28			16.10 16.72	21.13	16.19 16.81		16.27	
28		17.24	21.99	17.33	21.91	17.43		17.53	
		17.85		17.95 18.57	22.10	18.05 18.68		18.15	
31	24.43		24.34		24.26			19.40	
32	25.22	19.70	25.13		25.04			20.03	
34	26.79	20.32	25.92		25.83 26.61	21.17	26.52	20.66	
35	27.58	21.55	27.49	21.67	27.39	21.79	27.30	21.91	35
30	28.37	22.16 22.78		22.29 22.91	28.17	22.41 23.03		22.53 23.16	
38	29.94	23.40	29.84	23.53	29.74	23.66	29.64	23.79	38
39 40	30.73 31.52	24.01 24.63	30.63 31.41	24.14 24.76	30.52 31.30	24.28 24.90		24.41	39 40
41			32.20		32.01			3 25.66	
		25.86	32.98	26.00 26.62	32.87	26.15 26.77		6 26.29 3 26.91	
44	33.88	26.47	34.55	27.24	34.43	27.39	34.31	27.54	44
45	35.46	27.70	35.34	27.86	35.22	28.01	35.09		45
		28.32		28.48 29.10		28.64 29.26		28.79	
48	37.82	29.55	37.70	29.72	37.57	29.88	37.45	30.04	48
		30.17 30.78		30.34 30.95		30.50 31.13		30.67	
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
Þ	52	Deg.	513	Deg.	$51\frac{1}{2}$	Deg.	514	Deg.	Di

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D	38]	Deg.	$38\frac{1}{4}$]	Deg.	$38\frac{1}{2}$	Deg.	$38\frac{3}{4}$	Deg.	D
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
51	40.19	31.40	40.05		39.91		39.77		51
	40.98 41.76		40.84 41.62		40.70 41.48		40.55 41.33		52 53
	41.70		42.41		42.26			33.80	54
	43.34		43.19		43.04	34.24		34.43	55
	44.13		43.98		43.83		43.67		56
	44.92		44.76		44.61			35.68	57
50	45.70 46.49	35.11	45.55	35.91	45.39 46.17		45.23 46.01	36.30 36.93	58 59
	47.28			37.15		37.35		37.56	60
_									
61		37.56		37.76	47.74	37.97	47.57	38.18	61
	48.86			38.38		38.60	48.35	38.81	62
	49.64		49.47	39.00 39.62	49.30			39.43	63 64
64 65	51.22	39.40		40.24		39.84 40.46	49.91 50.69	40.06 40.68	65
		40.63		40.86		41.09		41.31	66
67	52.80	41.25		41.48		41.71	52.25		67
		41.86		42.10		42.33		42.56	68
		42.48		42.72		42.95		43.19	69
10	55.10	43.10	54.97	43.34	54.78	43.58	54.59	43.81	70
71	55.95	43.71	55.76	43.96	55.57	44.20	55 37	44.44	71
		44.33		44.57		44.82	56.15		72
73	57.52	41.94		45.19	57.13		56.93		73
		45.56		45.81		46.07	57.71	46.32	74
		46.17		46.43		46.69		46.94	75
		46.79	59.68 60.47	47.05	59.48 60.26	47.31 47.93	59.27		76
		48.02		48.29		48.56		48.82	78
70	69 9	48 64	62 04	48.91		49.18		49.45	79
80	63.04	49.25	62.83	49.53	62.61	19.80	62.39	50.07	80
81	63.83	49.87	63.61	50.15	63.39	50.42	63.17	50.70	81
		2 50.48		50.77	64.17			51.33	
		51.10		51.38	64.96			3 51.95	83
		51.72 52.33		52.00	65.74 66.52			52.58	
		52.95		52.62 53.24	67.30		66.29 67 0	53.20 53.83	
		53.56		53.86	68.09			5 54.40	
		1 54.18		54.48	68.87	54.78	68.6	3 55.08	88
		3 54.79		55.10	69.65			55.71	
1 30	10.95	2 55.41	10.00	55.72	70.43	56.03	70.1	56.33	90
91	71.7	56.03	71.4	56.34	71.29	2 56.65	70.9	7 56.96	91
		56.64		56.96		57.27	71.7	5 57.58	92
		3 57.26		57.58		57.89		3 58.21	
94		57.87 558.49		2 58.19 58.81	73.5			1 58.84	
		5 58.48 5 59.10		59.43		3 59.14 3 59.76	74.8	59.40 7 60.09	
9	7 76.4	1 59.79	76.18	60.05	75.9	60.38		5 60.71	
98	8 77.2	2 60.33	3 76.9	6 60.67	76.70	61.01	76.4	3 61.34	98
9	9 78.0	1 60.95	5 77.7	5 61.29		861.63		1 61.9	
10	078.8	0 61.57	78.5	3 61.91	18.2	6 62.25	77.9	9 62.59	100
ł	Dep	. Lat	. Dep	Lat	Dep	Lat.	Dep	. Lat	4
10	100		1	D)is
1-4	52	Deg	.151	Deg	1013	Deg	514	Deg	-

116 .

			4				-		
	39	Deg.	394	Deg.	39 <u>1</u>	Deg.	393	Deg.	U
Dist.	Lat	. Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1					0.77	0.64	0.77	0.64	12
34	3 2.3	3 1.89	2.32	1.90	2.31	1.91	2.31	1.92	34
5	5 3.89	3.15	3.87	3.16	3.09	3.18	3.08 3.84	3.20	5
6			4.65		4.63		4.61	3.84	67
89	6.22	5.03	6.20	5.06	6.17	5.09	6.15	5.12	89
10			6.97 7.74		6.94 7.72		6.92 7.69	5.75 6.39	10
11 12			8.52 9.29		8.49	7.00	8.45	7.03	11 12
13	10.10	8.18	10.07	8.23	9.26 10.03	8.27	9,99	7.67	13
14 15	10.88		10.84	8.86	10.80		10.76	8.95	14 15
16	12.43	10.07	12.39	10.12	12.35	10.18	12.30	10.23	16 17
17	13.99	10.70 11.33		10.76 11.39		10.81 11.45	13.07 13.84	10.87 11.51	18
19 20		11.96 12.59		$12.02 \\ 12.65$		12.09 12.72		12.15 12.79	19 20
21	16.32			13.29	16.20		16.15	13.43	21
22 23	17.10	13.84 14.47		13.92 14.55		13.99 14.63	16.91 17.68		22 23
24	18.65	15.10 15.73	18.59	15.18 15.82		15.27	18.45 19.22	15.35	24 25
26	20.21	16.36	20.13	16.45	20.06	$15.90 \\ 16.54$	19.99	16.63	26
	20.98 21.76			17.08 17.72	20.83 21.61	17.17 17.81	20.76 21.53		27 28
29	22.54 23.31	18.25	22.46	18.35 18.98	22.38 23.15	18.45	22.30 23.07	18.54	29 30
	24.09		24.01		23.92	19.72	23.85	19.82	31
32	24.87	20.14	24.78	20.25	24.69	20.35	24.60	20.46	32
	25.65 26.42		25.55	$\begin{array}{c} 20.88\\ 21.51 \end{array}$	25.46 26.24		25.37 26.14		33 34
35	27.20 27.98	22.03	27.10 27.88	22.14	27.01 27.78	22.26	26.91 27.68		35 36
37	28.75	23.28	28.65	23.41	28.55	23.53	28.45	23.66	37
38	29.53 30.31	23.91	29.43 30.20		29.32 30.09	24.17 24.81	29.22 29.98		38 39
	31.09		30.98		30.86		30.75		40
41	31.86 32.64	25.80	31.75 32.52	25:94	31.64 32.41		31.52 32.29		41 42
43	33.42	27.06	33.30	27.21	33.18	27.35	33.06	27.50	43
	34.19 34.97		34.07 34.85	27.84	33.95 34.72	27.99 28.62	33.83 34.60		44 45
46	35.75	28.95	35.62	29.10	35,49	29.26	35.37	29.41	46
	36.53 37.30		36.40 37.17	29.74 30.37	36.27 37.04		36.14 36.90		47 48
49	38.08	30.84	37.95 38.72	31.00	37.81 38.58		36.90 37.67 38.44		49 50
	38.86	Tet	Dan	Lat	Den	Lat	Dan	Lat	-
Dist.	Dep.	Lat.	Dep.	Lat.	EOIT	Deg.	For F	Ligt.	Cist
	91 Ļ	leg.	10041	Jeg.	2021	Jeg.	DU [‡] I	eg.	_

-	ś.			1211.01	n them	DLLLA	1.5.57	11 L	
U	39	Deg.	394	Deg.	$39\frac{1}{2}$	Deg.	394	Deg.	
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
51	39.63 40.41	32.10	39.49	32.27	39.35 40.12	32.44		32.61 33.25	
53	41.19	33.35	41.04	32.90 33.53	40.12	33.71	40.75	33.89	53
54	41.97	33.98	41.82	34.17	41.67	34.35	41.52	34.53	54
55	42.74	34.61		34.80 35.43				35.17 35.81	
57	43.32	35.24 35.87	43.37	36.06	43.98	36.26	43.82	36.45	57
58	45.07	36.50	44.91	36.70	44.75	36.89	44.59	37.09	58
59	45.85	37.13 37.76		37.33	45.53	37.53	45.36	37.73	
60	46.63	37.76	46.46	37.96	46.30	38.16	46.13	38.37	60
.61	47.41	38.39	47.24	38.60	47.07	38.80	46.90	39.01	61
62	48.18	39.02	48.01 48.79	39.23	47.84	39.44	47.67	39.65	62
63	48.96	39.65 40.28	48.79	39.86 40.49	48.61	40.07	48.44 49.21	40.28	63 64
		40.91	50.34	41.19	50.16	41.35	49.97	41.56	65
66	51.29 52.07	41.64	51.11	41.76 42.39	50.93	41.98	50.74	42.20	66
67	52.07	42.16	51.88	42.39 43.02	51.70	42.62	51.51	42.84	67
	53.52	42.79		43.66			52.28 53.05		68 69
	54.40		54.21		54.01	44.53	53.82		70
71	55.18	14 68	54 98	44.92	54 70	45 16	54.59	45 40	71
72	55.95	45.31	55.76	45.55	155.56	45.80	55.36		72
13	50.73	45.94	56.53	46.19	56.33	46.43	56.13		73
	57.51			46.82			56.89		74
76	58.29 59.06	47.83	58.85	47.45 48.09	57.87 58.64	41.11	57.66 58.43		75
77	59.84	48.46	59.63	48.72	59.42		59.20	49.24	77
78	60.62	49.09		49.35	60.19	49.61	59.97		78
80	61.39 62.17	49.72 50.35	61.18 61.95	49.98 50.62	60.96 61.73	50.25	60.74 61.51		79 80
							<u>`</u>		-
82	62.95 63.73	50.97	62.73 63.50		62.50 63.27		62.28 63.04	51.79	81 82
83	64.50	52.23	64.27		64.04		63.81	53.07	83
84	65.28	52.86	65.05	53.15	64.82	53.43	64.58	53.71	84
85	66.06	53.49	65.82	53.78	65.59		64.58 65.35 66.12	54.35	85 86
87	66.83 67.61	54.12	66.60 67.37		67.13	54.70	66.89	55 69	87
88	68.39	55.38	68.15	55.68	67.90	55.97	67.66		88
89	69.17	56.01	68.92	56.32	68.67	56.61	68.43	56.91	89
90	69.94	56.64	69.70	56.94	69.45	57.25	69.20	57.55	90
91	70.72	57.27	70.47	57.58 58.21	70.22	57.88	69.96	58.19	91
92	71,50	57.90	71.24	59.21		58.52	70.73	58.83	92 93
	72.27 73.05		72.02	58.84 59.47	71.76 72.53		71.50		93
.95	73.83	59.79	73.57	60.11	73:30	60.43	73.04	60.75	95
	74.61			60.74	74.08	61.06	73.81	61.39	96
	75.38			61.37 62.01			74.58		97 98
99	76.94	62.30	76.66	62.64	76.39	62.97	76.12	63.30	99
100	77.71	62.93	77.44	62.64 63.27	77.16	63.61	76.88	63.94	100
ist.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
Q	51	Deg.	5 031	Deg.	5011	Deg.	5011)eg.	Ä
	-	<u> </u>	- 4	-0	2	5.	4	-8	

D	40]	Deg.	4011	Deg.	4011	Deg.	403	Deg.	Б
st.	Lat.	Dep.	Lat:	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
12	0.77	0.64 1.29	0.76	0.65	0.76	0.65	0.76	0.65	1 2
ŝ	2.30	1.29	$1.53 \\ 2.29$	1.29	1.52	1.30 1.95	1.52	1.31	3
4	3.06	2.57	3.05	2.58	3.04	2.60	3.03	2.61	4
5 6	3.83 4.60	3.21 3.86	3.82	$3.23 \\ 3.88$	3.80 4.56	3.25 3.90	3.79	3.26	56
7	5.36	4.50	5.34	4.52	5.32	4.55	4.55	3.92	7
8	6,13	5.14	6.11	5.17	6.08	5.20	6.06	5.22	8
9 10	6.89 7.66	5.79 6.43	6.87 7.63	5.82 6.46	6.84 7.60	5.84 6.49	6.82 7.58	5.87 6.53	9 10
11	8.43	7.07	8.40	7.11	8.36	7.14	8.33	7.18	11
12	9.19	7.71	9.16	7.75	9.12	7.79	9.09		
13 14	9.96 10.72	8.36	9.92 10.69	8.40 9.05	9.89 10.65	8.44 9.09	9.85 10.61	8.49 9.14	
15	11.49	9.64	11.45	9.69	11.41	9.74	11.36	9.79	15
16	12.26	10.28		10.34	12.17	10.39	12.12		
		10.93 11.57	12.97	11.63	12.93 13.69	11.04	12.88	11.10	
19	14.55		14.50	12.28	14.45	12.34	14.39	12.40	19
20	15.32	12.86	15.26	12.92	15.21	12.99	15.15	13.06	20
	16.09 16.85	13.50 14.14	16.03	13.57 14.21	15.97	13.64	15.91	13.71 14.36	21 22
23	17.62	14.78	17.55	14.86		14.23	17.42	14.30	23
24	18.39	15.43	18.32	15.51	18.25	15.59	18.18	15.67	24
25	19.15	16.07	19.08	16.15 16.80		16.24	18.94	16.32	25 26
20	19.92	17.36	20.61	17.45		16.89 17.54	20.45	16.97 17.62	27
28	21.45	18.00	21.37	18.09	21.29	18.18	21.21	18.28	28
		18.64 19.28		18.74 19.38		18.83 19.48	21.97	18.93 19.58	29 30
			23.66				-		31
32	23.75	19.93 20.57		20.68	23.57	20.13 20.78		20.24	32
33	25.28	21.21	25.19	21.32		21.43	25.00	21.54	33
		21.85	25.95			22.08		22.19	34 35
		$22.50 \\ 23.14$	26.71 27.48			22.73 23.38	20.31	22.85 23.50	1
		23.78	28.24	23.91		24.03	28.03	24.15	37
38	29.11	24.43	29.00	24.55 25.20		24.68		24.80	
40	29.88 30.64	25.07 25.71		25.84		25.33 25.98		25.46 26.11	40
		26.35	31.29			26.63	31.06	26.75	41
		27.00		27.14		27.28		27.42	
		27.64 28.28	32.82 33.58	27.78 28.43		27.93 28.58	33.33	28.07 28.72	
45	34.47	28.93	34.35	29.08	34.22	29.23	34.09	29.37	45
46	35.24	29.57	35.11			29.87	34.85	30.03	
		30.21		30.37 31.01		30.52 31.17		30.68 31.33	
49	37.54	30.85 31.50		31.66		31.82	37.12	31.33	49
50	38.30	32.14		32.31		32.47	37.88	32.64	50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
D	50	Deg.	493	Deg.	491	Deg.	491]	Deg.	ā,

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10	40	Deg.	404	Deg.	401	Deg.	404	Deg.	
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Dist.
=	90.07	32.78	20 00	32.95	20 70	33.12	38 64	33.29	51
		33.42		33.60		33.77		33.94	52
53	40.60	34.07		34.24		34.42		34.60	53
	41.37			34.89	41.06	35.07		35.25	54
	42.13		41.98	35.54		35.72	41.67	35.90	55
	42.90		42.74	36.18		36.37	42.42	36.55	56
	43.66			36.83		37.02		37.21	57 58
50	44.45	37.28		37.48 38.12		37.67 38.32		37.86 38.51	59
	45.96			38.77		38.97		39.17	60
61	46.73	39.21	16 66	39.41	16 98	39.62	46 91	39.82	61
	47.49			40.06	47.15			40.47	62
	48.26		48.08		47.91		47.73	41.12	63
		41.14		41.35	48.67		48.48	41.78	64
	49.79			42.00	49.43			42.43	65
66	50.56	42.42		42.64	50.19			43.08	66 67
69	51.32 52.09	43.07	51.14	43.29	50.95 51.71		50.76	43.73	68
	52.86			44,58	52.47			45.04	69
	53.62		53.43		53.23		53.03		70
21	54.39	45.64	54.19	45.87	53.99	46.11	58.79	46.35	71
	55.16		54.95	46.52	54.75		54.54	47.00	72
	55.92		55.72		55.51		55.30	47.65	73
74	56.69	47.57	56.48		56.27			48.30	74
75	57.45		57.24	48.46	57.03			48.96	75
		48.85	58.01 58.77	49.11	57.79 58.55	49.36	57.57	49.61	77
	58.99 59.75		59.53		59.31			50.92	78
		50.78	60.30		60.07			51.57	79
	61.28		61.06		60.83		60.61	52.22	80
81	62.05	52.07	61.82	52.34	61.59	52.61	61.36	52.87	81
	62.82		62.59		62.35		62.12	53.53	82
	63.58		63.35		63.11		62.88		83
	64.35		64.11		63.87		63.64		84 85
	65.11			54.92	64.63 65.39		64.39 65.15	55.48 56.14	86
	65.88 66.65		65.64 66.40		66.16		65.91		87
	67.41		67.16	56.86		57.15		57.44	88
	68.18			57.50	67.68		67.42	58.10	89
	68.94		68.69		68.44	58.45	68.18	58.75	90
	69.71		69.45	58.80	69.20			59.40	91
92	70.48			59.44	69.96		69.70		92 93
93		59.78	70.98 71.74		70.72 71.48			60.71 61.36	93 94
	72.01 72.77		72.51		72.24		71.97		95
	73.54		73.27		73.00		72.73	62.66	96
	74.31		74.03		73.76		73.48	63.32	97
98	75.07	62.99	74.80	63.32	74.52	63.65	74.24	63.97	98
	75.84		75.56		75.28		75.00		99 100
100	76.60	64.28	76.32	64.61	76.04	04.94	15.76	65.28	
st.	Dep,	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	ist.
Ā	50 1	Deg.	493	Deg.	49 ¹ / ₂	Deg.	491	Deg.	0

120 Martine Contract										
	41	Deg	414	Deg	$.41\frac{1}{2}$	Deg	413	Deg.		
ISU.	Lat	. Dep	Lat.	Dep.	Lat	Dep	Lat.	Dep.)ist.	
	1 0.7								1	
	2 1.5	6 1.9			2.2				3	
	4 3.0	2 2.6		2.64	3.00				4	
	5 3.7 5 4.5			3.30						
1. 1	1 5.2	8 4.5	9 5.26	4.62	5.24	4.64	5.22	4.66	7	
. 8	6.0									
10				5.93 6.59						
11				7.25					11	
12				7.91						
14	10.5	7 9.18	8 10.53	9.23	10.49	9.28	10.44		14	
15	11.32			9.89		9.94	11.19	9.99	15	
						10.60		10.65		
18	13.58	3 11.81	1 13.53	11.87	13.48	11.95	13.43	11.99	18	
19		12.4	7 14.28 2 15.04			12.5		12.65		
								13.32	-	
21		13.78				13.91		$13.98 \\ 14.65$		
00	17 90	15 00	17 00	15.16	17.23	15.24		15.32	23	
24	18.11	15.75	18.04			15.90	17.91	15.98	24	
		16.40	18.80			16.57		16.65	25 26	
27	20.38	17.71	20.30	17.80	20.22	17.89	20.14	17.98	27	
20	21.13	18.37	21.05			18.55 19.22	20.89	18.64	28 29	
30	22.64	19.68	22.56			19.88		19.31 19.98	30	
31		20.34	23.31			20.54			31	
32	24.15	20.99 21.65	24.06 24.81	21.10	23.97	21.20 21.87	23.87 24.62	21.31	32 33	
34	25.66	22.31	25.56	22.42	25.46	22.53	25.37		34	
35	26.41	199 96	26.31		26.21	23.19	26.11	23.31	35	
37	27.92	23.62	27.07		26.96 27.71		26.86 27.60		36 37	
38	28.68	24.93	28.57	25.06	28.46	25.18	28.35		S 8	
39 40	29.43 30.19	25.59 26.24	29.32 30.07	25.71	29.21 29.96	25.84 26.50	29.10 29.84		39 40	
41	30.94	26.90	30.83	27.03	30.71	97 17	30.59	07 90	41	
42	31.70	27.55	31.58 9	27.69	31.46	27.83	31.33	27.97	42	
43	32.45	28.21 28.87	32.33 2		32.21	28.49	32.08	28.63	43	
45	33.96	29.52	33.83		32.95	29.16	32.83 33.57	29.30	44 45	
46	34.72	30.18	34.58 3	30.33	33.70 34.45	30.48	34.32	30.63	46	
47	35.47 36.23	30.83	35.34 3 36.09 3		35.20 35.95	31.14	35.06	31.30	47	
49	36.98	32.15	36.84 5		36.70	32.47	35.81 3 36.56 3	32.63	48. 49	
50	37.74	32.80	37.59 3		37.45	33.13	37.30		50	
Dist.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.	
9	49 I	Deg.	483 D	eg.	48 <u>1</u>	eg.	481D	eg.	51	

-		-							-
	41	Deg.	414	Deg.	411	Deg.	413	Deg.	-
is									ist.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
		33.46	38.34		38.20	33.79	38.05		51
	39.24 40.00		39.10		38.95	34.46 35.12	38.79 39.54		52
	40.00			34.95 35.60		35.12			53 54
		36.08	41.35						55
56	42.26	36.74	42.10	36.92	41.94	36.44 37.11	41.78	37.29	56
57	43.02	37.40	42.85	37.58	42.69	37.77	42.53	37.96	57
	43.77			38.24		38.43			58
	44.53					39.09			59
-60	45.28	39.36	45.11	39.56	44.94	39.76	44.76	39.95	60
	10.01		15.00	10.00				10.00	-
	46.04			40.22		40.42	45.51	40.62	61
	40.79	40.68		40.88	40.44	41.08	40.20		62 63
	48.30			42.20	47.93		47.75		64
	49.06		48.87		48.68	43.07	48.49	43.28	65
	49.81		49.62	43.52	49.43		49.24		66
67	50.57	43.96	50.37	44.18	50.18	41.40	49.99		67
	51.32			44.84		45.06	50.73		68
	52.07		51.88			45.72	51.48		69
70	52.83	45.92	52.63	46.15	52.43	46.38	52.22	46.61	70
-	-0 10	10 10	-0 00	40.01	10.10	10.00		18 00	
		46.58	53.38			47.05	52.97		71
		47.24 47.89	54.13 54.88		53.92 54.67	41.11	53.72 54.46		72
	55.85		55.64		55.42		55.21	49 98	74
		49.20	56.39		56.17		55.95		75
		49.86	57.14		56.92		56.70		76
	58.11		57.89		57.67		57.45		77
	58.87		58.64			51.68			78
		51.83	59.40		59.17		58.94		79
80	60.38	52.48	60.15	52.75	59.92	53.01	59.68	53.27	80
01	01 10	10 14	00.00	FQ 41	00.00		0 40	10.04	
	61.13	53.14 53.80	60.90 61.65			53.67	60.43		81
	62.64		62.40			54.33 55.00			82 83
	63.40		63.15		62.91		62.67		84
	64.15			56.04		56.32			85
86	64.90	56.42			64.41		64.16		86
87	65.66	57.08	65.41		65.16	57.65	64,91		87
88	66.41	57.73	66.16		65.91	58.31	65.65		88
	67.17		66.91		66.66	58.97	66.40		89
30	67.92	59.05	07.67	59.34	07.41	59.64	07.15	59.93	90
01	69 69	59.70	68 40	60.00	68 15	60.30	67.89	60 60	91
		60.36	69.17			60.96	68.64		92
		61.01	69.92		69.65		69.38		93
	70.94		70.67		70.40			62.59	94
95	71.70	62.33		62.64	71.15	62.95	70.88	63.26	95
		62.98		63.30		63.61		63.92	96
		63.64		63.96		64.27	72.37		97
98	73.96	64.29		64.62		64.94		65.26	98
		64.95 65.61		65.28 65.93		65.60 66.26		65.92 66.59	99 100
100	10.41	00.01	10.10	00.00	14.00	00.20	14.01	00.09	100
	Dep	Lat.	Den	Lat.	Dep	Lat	Dep.	Lat	•
st	Dop.	- Addet o		Late	Dep.	Lines	Dep.	Liato	st
Ô	49	Dec	183	Deg.	481	Der	181	Der	ā
	40	Deg.	1404	Deg.	402	Deg.	+04	peg.	

TRAVERSE TABLE.

D	42	Deg.	424	Deg.	421	Deg.	423	Deg.	
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.)ist.
1	0.74	0.67	0.74	0.67	0.74	0.68	0.73	0.68	1
23	1.49 2.23	1.34 2.01	1.48	1.34 2.02	1.47	1.35	1.47 2.20	1.36 2.04	23
- 4	2.97	2.68	2.96	2.69	2.95	2.70	2.94	2.72	4
5	3.72	3.35	3.70	3.36	3.69	3.38	3.67	3.39	5
67	4.40	4.01	4.44	4.03	4.42 5.16	4.05	4.41 5.14	4.07	6
8	5.95	5.35	5.92	5.38	5.90	5.40	5.87	5.43	8
9	6.69	6.02	6.66	6.05	6.64		6.61	6.11 6.79	9
10	7.43	6.69	7.40	6.72	1.01	6.76	7.34	0.13	10
11	8.17	7.36	8.14	7.40	8.11	7.43	8.08	7.47	11
12	8.92	8.03	8.88	8.07	8.85		8.81		12
13	9.66		9.62 10.36	8.74 9.41	9.58 10.32	8.78 9.46	9.55	8.82 9.50	13 14
		10.04	11.10		11.06	10.13	11.01	10.18	15
		10.71		10.76		10.81	11.75		16
		11.38 12.04		11.43 12.10		$11.48 \\ 12.16$		11.54	17
		12.71		12.77	14.01	12.84	13.95	12.90	19
20	14.86	13.38	14.80	13.45	14.75	13.51	14.69	13.58	20
21	15.61	14.05	15 54	14.12	15.48	14.19	15.42	14.25	21
22	16.35	14.72	16.28	14.79	16.22	14.86	16.16	14.93	22
23	17.09	15.39	17.02	15.46	16.96	15.54		15.61	
25	17.84	16.06 16.73		16.14 16.81		16.21 16.89	17.62	16.29	24 25
26	19.32	17.40		17.48	19.17	17.57	19.09	17.65	26
27	20.06	18.07		18.15	19.91	18.24		18.33	
29	20.81	18.74 19.40		18.83 19.50		18.92 19.59	20.55	19.69	28 29
		20.07	22.21			20.27		20.36	
31	23.04	20.74	22.95	20.84	22.86	20,94	22.76	21.04	31
32	23.78	21.41		21.52		21.62		21.72	
33	24.52	22.08 22.75		22.19 22.86		22.29		22.40 23.08	
35	23.01	23.42		22.00		22.91		23.76	
. 36	26.75	24.09	26.65	24.21		24.32		24.44	
		24.76 25.43		24.88 25.55		25.00 25.67		25.12 25.79	
39	28.98	26.10	28.87	26.22	28.75	26.35		26.47	
40	29.73	26.77	29.61	26.89	29.49	27.02	29 37	27.15	40
		27.43		27.57	30.23	27.70		27.83	
		28.10 28.77		28.24 28.91	30.97	28.37 29.05		28.51 29.19	
		28.11		29.58		29.03		29.19	
45	33.44	30.11	33.31	30.26		30.40	33.04	30.55	45
		30.78		30.93 31.60		31.08		31.22 31.90	
		32.12		32.27	35.39	32.43		32.58	48
: 49	36.41	32.79	36.27	32.95	36.13	33.10	35.98	33.26	49
50	37.16	33.46	37.01	33.62	30.86	33.78	36.72	33,94	50
st.		Lat.	-			Lat.			ist.
P	48	Deg.	473	Deg.	471	Deg.	474	Deg.	A

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-	10		10.1		101		140.01		
	42	Deg.	42	Deg.	42	Deg.	424	Deg.	D
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
			37.75	34.29	37.60	34.46	37.45	34.62	51
		34.79		34.96	38.34	35.13	38.18	35.30	52
		35.46		35.64		35.81			53 54
55	40.13	36.13	39.97	36.31	39.81	36.48	39.65	36.66	55
56	41.62	36.80 37.47 38.14	41.45	37.65	41.29	37.83	41.12	38.01	56
57	42.36	38.14	42.19	38.32		38.51		38.69	57
58	43.10	38.81	42.93	39.00	42.76	39.18	42.59	39.37	58
- 59 60	43.85	39.48	43.67	39.67		39.86			59 60
	44.59	40.15	44.41	40.34	44.24	40.54	44.00	40.13	
61	45.33	40.82	45.15	41.01	44.97	41.21	44.79	41.41	61
62	46.07	41.49	45.89			41.89		42.09	
		42.16	46.63			42.56	46.26		63
		42.82	47.37			43.24		43.44	64 65
		43.49 44.16		43.70 44.38	47.92	43.91 44.59		44.12 44.80	
67	49.79	44.83	49.59			45.26		45.48	
68	50.53	45.50		45.72		45.94	49.93	46,16	68
69	51.28	46.17	51.07				50.67		69
70	52.02	46.84	51.82	47.07	51.61	47.29	51.40	47.52	70
71	52.76	47.51	59 56	47.74	52.35	17 97	59.14	48.19	71
		48.18	53.30	48.41		48.64		48.87	72
		48.85	54.04			49.32	53.61	49.55	73
		49.52		49.76		49.99		50.23	74
		50.18 50.85	55.52			50.67		50.91 51.59	75
77	57.22	51.52		51.77	56.77	51.34 52.02	56.54	52.27	77
78	57.97	52.19		52.44		52.70		52.95	78
79	58.71	52.86		53.12		53.37		53.63	79
80	59.45	53.53	59.22	53.79	58.98	54.05	58.75	54.30	80
		54.20	59.96	54.46		54.72		54.98	81
		54.87	60.70			55.40		55.66	82
		55.54		55.81	61.19			56.34 57.02	83 84
85	63.17	56.21 56.88	62.92	56.48	69.67	56.75 57.43		57.70	85
		57.55	63.66		63.41	58.10	63.15		86
87	64.65	58.21	64.40	58.50	64.14	58.78	63.89	59.06	87
		58.88		59.17		59.45		59.73	88
		59.55 60.22		59.84 60.51		60.13 60.80		60.41 61.09	90
		60.89 61.56				61.48		61.77	
		62.23		61.86 62.53		62.83		63.13	
94	69.86	62.90	69.58	63.20		63.51		63.81	94
95	70.60	63.57	70.32	63.87	70.04	64.18	69.76	64.49	95
		64.24		64.55		64.86		65.16	
		64.91 65.57	79 54	65.22 65.89		65.53		65.84	
		66.24		66.56		66.88	72.70	67.20	99
		66.91		67.24		67.56		67.88	
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat. Deg.	Dep.	Lat.	st.
Â	48	Deg.	473	Deg.	47!	Deg.	47!	Deg.	ā

	43	Deg.	431	Deg.	$43\frac{1}{2}$	Deg.	433	Deg.	T
)ist.		Dep.		Dep.		Dep.		Dep.	ist.
1	0.73	0.68	0.73	0.69	0.73	0.69	0.72	0.69	1
2 3	1.46 2.19	1.36 2.05	1.46	1.37 2.06	1.45	1.38 2.07	1.44 2.17	1.38	23
4	2.93	2.73	2.91	2.74	2.90	2.75	2.89	2.77	4
5 6	3.66 4.39	3.41 4.09	3.64	3.43	3.63		3.61	3.46 4.15	5 6
7	5.12	4.77	5.10	4.80	5.08		5.06	4.84	7
8	5.85	5.46	5.83	5.48	5.80		5.78	5.53	8 9
9 10	6.58 7.31	6.14 6.82	6.56 7.28	6.17 6.85	6.53 7.25	6.20 6.88	6.50 7.22	6.22 6.92	9 10
11	8.04	7.50	8.01	7.54	7.98		7.95		11
12 13	8.78 9.51	8.18 8.87	8.74 9.47	8.22 8.91	8.70 9.43	8.26 8.95	8.67 9.39		12 13
14	10.24	9.55	10.20	9.59	10.16	9.64	10.11	9.68	14
		10.23		10.28		10.33		10.37	15
	11.70 12.43	10.91		10.96 11.65		11.70	12.28	11.06	16 17
18	13.16	12.28	13.11	12.33	13.06	12.39	13.00	12.45	18
-19 -20	13.90 14.63	12.96 13.64	13.84 14.57	13.02 13.70		13.08 13.77		13.14 13.83	. 19 20
21	15.36	14.32	15.30	14.39	15.23	14.46	15.17	14.52	21
		15.00		15.07		15.14	15.89		22 23
23	16.82	$15.69 \\ 16.37$		15.76	17.41	$15.83 \\ 16.52$		15.90	24
25	18.28	17.05	18.21	17.13	18.13	17.21	18.06	17.29	25
		17.73 18.41	18.94			17.90	18.78	17.98	26
28	20.48	19.10	20.39	19.19	20.31	19.27	20.23	19.36	28
		19.78 20.46		19.87 20.56			20.95 21.67		29 30
31	22.67	21.14	22.58	21.24	22.49	21.34	22.39	21.44	31
32	23.40	21.82	23.31	21.93	23.21	22.03	23.12	22.13	32
33	$24.13 \\ 24.87$	22.51		22.61 23.30		22.72		22.82	33 34
35	25.60	23.87	25.49	23.98	25.39	24.09	25.28	24.20	35
36	26.33	24.55	26.22	24.67	26.11	24.78	26.01		36
38	27.79	25.92	27.68	25.35 26.04	27.56	26.16	26.73	25.59 26.28	37
39	28.52	26.60 27.28	28.41	26.72 27.41	28.29	26.85	28.17	26.97	39 40
41	29.99	27.96 28.64		28.09	29.74	28.22	29.62	28.35	41
42	30.72 31.45	28.64	30.59	28.78 29.46	30.47	28.91	30.34	29.04	42
44	32.18	30.01	32.05	30.15	31.92	30.29	31.78	30.43	43 44
45	32.91	30.69 31.37	32.78	30.83	32.64	30.98	32.51	31.12	45
47	34.37	32.05	34.23	31.52 32.20	34.09	31.66 32.35	33.95	32.50	46 47
48	35.10	32.74 33.42	34.96	32.89	34.82	33.04	34.67	33.19	48
49 50	35.84 36.57	33.42 34.10	35.69 36.42	33.57 34.26	35.54 36.27	33.73 34.42	35.40 36.12	33.88 34.58	49 50
st.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	st.
Ā	47	Deg.	463	Deg.	461	Deg.	464	Deg.	ā

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F	43	Deg.	431	Deg.	1431	Deg.	143ª	Deg.	-Te
JISL									- 5.
15	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep	
5	37.30	34.78	37.15	34.94	36.99	35.11	36.84	35.2	51
	38.03			35.63		35.79			
5	3 38.76	36.15	38.60	36.31	38.44	36.49	38.29	36.6	5 53
	1 39.49			37.00		37.17	39.01	37.34	
50	5 40.22 5 40.96	37.51		37.69		37.86	39.73 40.45	38.0	
5	41.69	38.87	41.52	39.06		89.24	41.17	39.4	2 57
	42.42			39.74		39.92	41.90		
59	43.15	40.24		40.43		40.61	42.62		
60	43.88	40.92	43.70	41.11	43.52	41.30	43.34	41.49	60
61	44.61	4) 60	44.43	41.80	44.95	41.99	44.06	42.18	61
				42.48		42.68	44.79	42.87	
63	46.08	42.97	45.89	43.17		43.37	45.51	43.57	
	46.81			43.85		44.05	46.23		
65	47.54	44.33		44.54 45.22		44.74	46.95		
	49.00			45.91	48.60		48.40		
	49.73			46.59		46.81		47.02	
	50.46		50.26			47.50	49.84	47.71	69
70	51.19	47.74	50.99	47.96	50.78	49.18	50.57	48.41	70
	51.93	48.42	51.71	48.65	51.50	10 07	51 00	40.10	71
	52.66		52.44	48.05	52.23		51.29 52.01	49.10 49.79	
	53.39			50.02	52.95			50.48	
	54.12			50.70	53.68		53.45	51.17	74
	54.85				54.40			51.86	75
		51.83			55.13		54.90		76
	56.31 57.05		56.08 56.81		55.85 56.58		55.62 56.34	53.25 53.94	77 78
	57.78		57.54		57,30		57.07	54.63	79
	58.51		58.27		58.03			55.32	80
	59.24		59.00		58.76			56.01	81
	59.97 60.70		59.73 60.45		59.48 60.21			56.70	82 83
	61.43		61.18		60.93		60.68	57.40 58.09	84
.85	62.17	57.97	61.91		61.66			58.78	85
86	62.90	58.65	62.64		62.38			59.47	86
87	63.63	59.33	63.37		63.11			60.16	87
	64.36 65.09		64.10 64.82		63.83 64.56			60.85 61.54	88 89
	65.82		65.55		65.28			62 24	90
	66.55		66.28		66.01		65.74		91
92	67.28	62.74	67.01 67.74		66.73 67.46		66.46		92 93
	68.02 68.75		68.47		68.19		67.18 67.90		93 94
	69.48		69.20		68.91		68.62		95
96	70.21	65.47	69.92	65.78	69.64.	66.08	69.35	66.39	96
97	70.94	66.15	70.65		70.36		70.07	67.08	97
98 99	71.67		$71.37 \\ 72.11$		71.09		70.79 71.51		98 99
	73.14		72.84		72.54		72,24		100
-									_
4	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	1
)is									isi
-	47 I	Jeg.	46 <u>3</u> I)eg.	$46\frac{1}{3}I$)eg.	$46\frac{1}{4}$ [)eg.	-
	interesting i		-	-	-		and the second		

Ď	44	Deg.	44 ₄	Deg.	441	Deg.	4431	Deg.	45	Deg.	16
ist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ist.
1	0.72		0.72	0.70	0.71	0.70	0.71	0.71	0.71	0.71	1
23	1.44 2.16	1.39	1.43	1.40	1.43	$1.40 \\ 2.10$	1.42	$1.41 \\ 2.11$	1.41	1.41	23
4	2.88	2.78	2.87	2.79	2.85	2.80	2.84	2.82	2.83	2.83	4
5 6	3.60		3.58	3.49	3.57 4.28	3.50 4.21	3.55	3.52 4.22	3.54		
7	5.04	4.86	5.01	4.88	4.99	4.91	4.97		4.95		7
8 9	5.75 6.47		5.73	5.58	5.71	5.61	5.68	5.63	5.60		
10	7.19		6.45 7.16	6.28 6.98	6.42 7.13	6.31 7.01	6.39 7.10		6.36		1 10
11	7.91	7.64	7.88	7.68	7.85	7.71	7.81	7.74	7.78	7.78	11
12	8.63	8.34	8.60	8.37	8.56	8.41	8.52	8.45	8.4	8.49	12
13	9.35		9.31 10.03	9.07 9.77	9.27	9.11 9.81	9.23		9.19		
		10.42		10.47	9.99	10.51		10.56		10.61	
16	11,51	11.11	11.46	11.16	11.41	11.21		11.26		11.31	
		11.81		11.86 12.56		11.92		11.97		2 12.02	
		13.20		13.26		13.32		13.38		3 13.43	19
20	14.39	13.89	14.33	13.96	14.26	14.02	14.20	14.08	14.14	1 14.14	20
		14.59	15.04	14.65		14.72		14.78		5 14.85	
		8 15.28 1 15.98		$15.35 \\ 16.05$		15.42		2 15.49 3 16.19		5 15.5t	
		6 16.67	17.19	16.75		16.82		16.90			
		3 17.37	17.91	17.44	17.83	17.52	17.75	5 17.60	17.6	8 17.68	3 25
		0 18.06 2 18.76	19.34	18.14 18.84		18.22		5 18.30 7 19.01		8 18.38 9 19.09	
		1 19.45	20.06	19.54		19.63	19.89	9 19.71	19.8	0 19.80	28
		6 20.15		20.24		20.33		20.42		1 20.5	
_		3 20.84		20.93	21.40	21.03	21.31	21.12		1 21.2	
		21.53		21.63		21.73		2 21.82		2 21.99	
		2 22.23		22.33		22.43		322.53 423.23		3 22.6	
34	24.4	5 23.62	24.35	23.72		23.8	24.15	5 23.94	24.0	4 24.0	4 34
		324.31				6 24.53		5 24.64		5 24.7. 6 25.4	
		25.01 225.70		25.12		3 25.23 25.93		7 25.34		6 26.1	
-38	27.3	3 26.40	27.22	26.52	27.10	26.63	3 26.99	9 26.75	26.8	7 26.8	7 38
		5 27.09 7 27.79				27.34) 27.46 1 28.16		8 27.5 8 28.2	
		9 28.48				1 28.74		2 28.86	.	9 28.9	
		129.18				5 29.44		3 29.57		0 29.7	
4	30.9	3 29.87	30.80	30.00	30.6	30.14	1 30.54	4 30.27	30.4	1 30.4	1 43
		5 30. 56 7 31.26			31.38	30.84 31.54	31.2	5 30.98 6 31.68		1 31.1	
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61	43.88	42.37	43.69	42.57	43.51	42.76	43.32	42.94	43.13	43.13	61	
62	44.60	43.07	44.41	43.26	44.22	43.46	44.03	43.65	43.84	43.84		
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NATURAL SINES.

IV. A TABLE of NATURAL SINES, calculated to five places of figures, for every Minute.

NATURAL SINES are Decimals bearing the same proportion to Unity or 1 that the Sine of the corresponding number of Degrees and Minutes bears to Radius or Sine of 90°. That is, 1 is assumed as the Nat. Sine of 90°, and the Table calculated accordingly.

Explanation of the Table.

To find the Natural Sine of any number of Degrees and Minutes.

If the degrees be less than 45, look for them at the Top of the Columns, and for the Minutes at the left-hand; but if more than 45, look for them at the Bottom, and for the Minutes at the right-hand; under or over the Degrees and against the Minutes will be the Natural Sine required.

The reverse of this will give the Degrees and Minutes corresponding to any Natural Sine.

To calculate the Northing or Southing, &c. for any Course and Distance, by Nat. Sines.

Find the Nat. Sine and Co-Sine of the Course, and into each of these multiply the Distance; the Products will be the Latitude and Departure required.

EXAMPLE.

Required the Latitude and Departure for 6 Chains and 22 Links, on a Course N. 38° 27' W.

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20 21	443	440 433	123 150	964 956	793 821	459 450	454 482	924 915	106 134	361 351	40 39
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27 28	640 668	386	318	907	987 30015	398	648	860	298 326	293	33 32
29	696	379 371	346 374	890	043	389 380	675 703	851 842	353	284 274	31
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37 38	948	308 301	597	824 816	265 292	310 301	923 951	768	573 600	196 186	23 22
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44 45	144	253 246	792 820	766 757	435	248	116 144	702 693	704 792	127 118	16 15
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22	775 803	748	406 434	127	38026 053	488 477			231 257	002	39 38
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39	266	575	894			287	115				
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42		544		913		254	- 195				18
43		534 524	37002 029	902 892	617 644	243 231					
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49		472	164	838	3 778	3 175	381	484	972	766	
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59					5 859 4 886		46	449 3 437	051	729	
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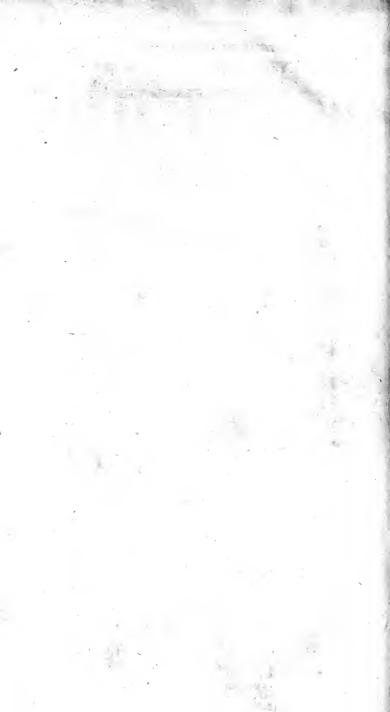
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1 9			072	764	632	581	178	172	710		51
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33		221	698	454	252	6611	793	840		86993	27
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49 50	575	019	140	245.	690	431	226	603	748	762 748	11 10
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56 57	733 759	930 918	295 321	153° 140.	844 870	349 336	379 405	518 504	899 924	661	4
58	785	905	347	127	896	322	405	490	924 950	646 632	32
59	811	892	373	114.	921	308	456	476	975	617	ĩ
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11 12	277	442	778	551		635	732	692			49
12	302 327	427 413	803 828	536 521		619 604	756 781	676			48 47
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12	643	714		696	460					494	48
13	667	698								476	47
14	691	681			506					458	46
15	715	-	1	644	529		5	532	1	439	45
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17	762									402	43
18	786				599						
19	810				622		62001				41 40
20 21	833 857										39
22	881				651						38
23	904				714						37
24	925										36
25	952				761					255	36
26	976				784						34
27	999			438							33
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29	047				853					181	31
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32	118										28
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30	236										29
38	260								787		29
39	283							098	810		2
40	307	242	716								20
41	330	225	739	195	130	140	502	061		959	19
42	354	208	763								18
43	378				176						17
44	401				199						16
45	425				222		2	77988		1	18
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47	472				263						15
48	496				291	015		934	64011		
49 50	519				314				033		10
50 51	567				360				030		
52					383			861	100		
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55		80987	065	951		891	819	806	167	698	1
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1	301	586	628	452	935	295	221	116	487	914	59
2	323	567	650	433	956	276	242	096		894	58
3	346	548		414	978	256	264	076		873	57
4	368	530	694	395	999	237	285	056	549	853	56
5 6	390	511	716		67021	217	306	036		833	55
7	412 435	492 473	738	356	048 064	198	327	016		813	54
8	455	475	759 781	337	064	178	349	72996	612	792	53
9	479	436	803	318 299	086	159 139	370 391	976		772 752	52
10	501	417	825	280	129	120		957 937		732	51 50
11	524	398	847	261	151	100	433	917	696	711	49
12	546	380	869	241		080		897		691	48
13	568	361	891	222	194	061		877		671	47
14	590	342	913	203		041	497	857	758	650	46
15	612	323		184	237	022	518	837	779	630	45
	64635	76304	65956	75165.	67258	74002	68539	72817	69800	71610	44
17	657	286	978	146			561	797	821	590	43
18	679		66000	126		963		777	842	569	42
19	701	248		107		844		757	862	549	41
20	723	229		088	344	924	624	737		529	40
21 22	746 768	210 192		069		904		717	904	508	39
23	790	192		· 050 030		885		697	925	488	38
24	812	154		011		865 846	688 709	677	946 966	468 447	37 36
25	834	135		74992	452	826				427	35
26	856	116		973		806	751		70008		34
27	878	097		953		787	772	597	029	386	33
28	901	078		934		767			049	366	32
29	923	059		915	538	747			070	345	31
30	9.15	041	262	896	559	729	835	537	091	325	30
31	64967		66284	74876	67580	73708	68857	72517	70112	71905	29
32	989	003		857		688					28
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34	033	965	349	818		649					26
35 36	055	946	371 393	799		629		437			25
37	077	927 908		780		610 590					24
38	099 · 122	889		741			983 69004				
39	144	870		722							21
40	166	851	480	703							20
41	188	832	501	683							19
42	210	813	523	664	816	491	088	297	339	080	18
43	232	794		644							
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