

AZIMUTHS, GREAT-DIRCLE SAILING, inid reduction to the meridian. Lats and decles, 90° n. 10 90° d.

TABLES

203

FOURTH EDITION, 1918.

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M. S. BLACKBURNE.

YC 62540







TABLES

AZIMUTHS, GREAT-CIRCLE SAILING,

AND

REDUCTION TO THE MERIDIAN,

WITH A

NEW AND IMPROVED "SUMNER" METHOD:

LATITUDES -DECLINATIONS

- - - 90° N. то 90° S. - - - 90° N. то 90° S.

Azimuths through Tables A, B, and C (or separately through Table D) for all the Heavenly Bodies at any Time the Body is above the Horizon; and Great-circle Sailing-courses for all Latitudes.

Also other Useful Navigational Tables, with Numerous Examples of Double Altitudes, Equal Altitudes, Azimuths, &c.

BY

H. S. BLACKBURNE (Extra Master),

Principal Examiner of Masters and Mates in New Zealand, and Nautical Adviser to the Government.

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PREFACE.

THE tables and problems here published are a reprint, for the most part of the azimuth tables which have been published in the first three years' issues of the "New Zealand Nautical Almanac."

Tables D and G are now reprinted and brought up to date from the writer's original tables published in 1883, and Tables A, C, and D have been extended from 60° to 85° of latitude. This will meet the needs of Arctic and Antarctic explorers, as well as the traders to such places as Archangel. Some years ago the writer promised Captain Liddle, who was then trading to Archangel, that he would extend his tables to latitude 72° to meet the needs of those trading in these high latitudes, outside the limits of the ordinary azimuth tables. With this extension they now constitute the most complete and comprehensive azimuth tables yet submitted to the seafaring community, giving with great simplicity sufficient accuracy to meet even the requirements of the extra-masters' examination. By the aid of Tables A, B, and C (when the hour-angle is known) the true bearing of the sun, moon, planets, and fifty-one of the brightest stars may be found in a couple of minutes at *any* hour of the day or night by the use of only about half a dozen figures.

As requests have been made from candidates for examination for permission to use these A, B, and C tables for solving some of the problems in the examination for masters and mates, and recommendations have been made for their use in the local examinations in New Zealand, these tables are now published separately, and, for the sake of giving the azimuth with greater precision for examination purposes, the factors are given in Tables A and B to three places of decimals when hour-angles are between four and eight hours, except in the very high latitudes, where so many decimals are unnecessary.

The comprehensiveness of the A, B, and C tables for azimuth purposes is simply marvellous. They cover only forty-two pages, and give not only all the azimuths of the above-mentioned heavenly bodies comprised in the four large tables of inspection (which cover several hundred pages), but also a considerable number of azimuths which are outside the limits of the larger tables. They are therefore especially valuable for use in the "Sumner" and "double altitude" problems, where the large azimuth tables omit to give the azimuth when the body is near either the upper or lower meridian. It was this omission (which is especially felt in low latitudes) which first led the writer to calculate and publish his original A and B azimuth tables. When the price of the large azimuth tables is taken into consideration (Burdwood's and Davis's for the sun, and Davis's and Goodwin's for the higher-declination stars), amounting altogether to f_{III} , the boon to navigators in the

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price only, apart from the much greater extent of limit comprised in these small tables, must, I think, be recognized and appreciated by those who have only moderate means.

In the writer's old A and B tables the factors throughout were given to three places of decimals for the sake of being able to show that these tables would give the azimuth as accurately as the large tables of inspection. He has, however, often regretted having given the three places of decimals in the smaller hour-angles, as it makes interpolation at sight more difficult, and the azimuth is obtained with sufficient accuracy for practical purposes without it. In this edition three places of decimals have been given wherever necessary to give sufficient accuracy for examination purposes. Even in the Board of Trade extra-masters' examination any azimuth tables which give the azimuth correctly within half a degree may be used in the time-azimuth problem. These tables will nearly always give the azimuth correctly within 0'1° of the truth. To insure the most rigid accuracy in the second place of decimals, whenever the third place of decimals in the writer's old table came to 5 a fresh calculation has been made. In the parts where three places of decimals have been given, new calculations have been made and compared with the old tables.

In Table B all the stars not less bright than 1.0° magnitude have been computed separately for their actual declinations for the epoch 1910; and, as their annual change of declination is so small, these factors will be sufficiently accurate for all practical purposes for the next thirty or forty years, and no interpolation for declination will be needed.

The whole of Table C has been newly calculated on the lines of the late Mr. W. H. Rosser's table published in "Norie's Epitome," but this table (including latitudes to 85°) contains more than eight times the number of his computations, for the sake of giving greater accuracy and less interpolation. This plan will, I believe, be more popular with most navigators than that previously given in the writer's old table, as the azimuth is taken out more directly, and quite accurately enough for all practical purposes.

Tables A and B have been worked to five places of decimals where necessary, and Tables C and C^2 , though only given to the nearest decimal of a degree, have been calculated throughout to the nearest decimal of a minute for the sake of accurate checking by differences.

Table D has also been checked from the writer's old calculations, and, where necessary, seven-figure logarithms have been used to determine fine points; otherwise, with the exception of changed heading and the addition of two pages, giving latitudes from 61° to 85° , it remains the same as when first published in 1883.

Table A, from latitude 61° to 82° , was calculated with great care by Captain Thomas Liddle, who very kindly sent to the writer the whole of his work. This was carefully compared by the writer with his own calculations. Throughout the compilation of the whole of these tables such minute care has been taken and rigid accuracy aimed at that the writer has good reason for believing that not one factor in a thousand will be found in the slightest degree in error.

An important feature in this work, which the writer believes he was the first to introduce, and which should prove a boon to navigators, is the method here presented of working the "Sumner" problem on a plane chart in connection with these tables. This method is much shorter than that usually taught in the navigation schools in preparation for the Board of Trade examinations, and at the same time it gives greater accuracy, especially when the plan which is here advocated is adopted, of combining the ex-meridian and chronometer observations when one of the bodies observed is near the meridian; and it has the great advantage of only requiring one chart, instead of having to carry about "Sumner" charts for every change of latitude N. and S. of the Equator. The Marine Department of the New Zealand Government has published some very accurate charts on a convenient scale for this purpose.

As the request from the New Zealand Government to the Board of Trade to allow the use of these tables, and improved "Sumner" method for solving the "Sumner" and "double altitude" problems, in the New Zealand examination for masters and mates was not granted, two examples have been clearly worked and plotted on the chart (see pages 104 and IIO)---one of two observations of the sun as given in the masters' and mates' examinations, and the other of observations of two different stars as given in the extra-masters' examination. These examples illustrate the possible errors that may arise from the old method. This error is especially aggravated in low latitudes, where in the summer months one of the altitudes must always be great, and often within half an hour of the meridian. The error in such cases would sometimes amount to 6 or 7 minutes of latitude. The summer months, too, in these latitudes are generally the rainy season, when double altitudes are most needed. We trust that after further perusal and trial of these tables and the methods here advocated the Board of Trade may see fit to alter their decision, especially as the tables are now printed separately from the "New Zealand Nautical Almanac."

Although the examples above mentioned are purposely exceptional ones, for the sake of better illustration, smaller errors will often arise if the method at present used by the Board of Trade for the masters' and mates' examinations is always adopted. Many an opportunity of determining the ship's position is lost owing to the impression among many navigators that the "Sumner" method is not of value when one of the observations is within, or a little outside of, the ordinary ex-meridian limits. At other times a false confidence is encouraged about the accuracy of the ship's position by trusting too implicity to the latitude by ex-meridian following a chronometer observation for longitude, without due regard to the bearing when the first observation was taken.

An example from "Norie's Navigation" (the best-known epitome of navigation in the world) will illustrate both these contentions. On pages 368 and 369 of the 1900 edition an example is given of a longitude by chronometer at 8 h. 45 m. a.m., and an ex-meridian at 11 h. 30 m. a.m. At the close of the work the editor says, "Since by reference to the table, page 309, the hour-angle of the second observation is within the limits of the reduction to the meridian, it follows that the latitude found will be the *correct* latitude, unless the latitude and longitude used in the calculation are both very erroneous." He seems to have ignored the fact that when the first observation was taken the sun was not on, or even near, the prime vertical (and never is in the winter months in high

Inset-Azimuth.

latitudes), and therefore the time resulting from this observation was more than I minute in error; and, although the sun was only $8\frac{1}{2}^{\circ}$ from the meridian when the second observation was taken, the resulting position was over 2' in error in the latitude and about $2\frac{1}{2}$ ' in error in the longitude from the position given, and which the reader might naturally infer was correct. The editor afterwards goes on to say that "if the second observation had not been within the limits of the table on page 309, and the azimuth had been small, or if the estimated latitude and longitude had been very erroneous, neither the latitude nor the longitude could have been found with any degree of accuracy by the ordinary methods. Now what is termed the ' new navigation ' may prove useful." As this closes the chapter in "Norie" on the "Sumner" method, in which is included the above-mentioned example of finding position by chronometer longitude and an ex-meridian, it is presumed that these are what are referred to as the " ordinary methods."

Now, the author maintains that if the "Sumner" method is dealt with in a practical way, either as advocated in these pages by numerous examples, or as given in the "American Practical Navigator," by Bowditch, revised by Lieut. G. W. Logan, U.S. Navy, the "Sumner" position will give quite as accurate results as by the method which is termed the "new navigation," and he ventures to believe that this method, too, will be easier for most men to grasp. He guarantees that he will take any of the double-altitude or simultaneous-altitude problems out of the numerous examples given in Captain Thompson's "Navigation Simplified " (which we may presume are fair specimens of the problems given at the Board of Trade examinations) and by the methods here presented, by the aid of these tables, either with or without the aid of chart, will find the position of ship with similar accuracy to that obtained by the most rigorous methods of trigonometry, and well within the limit of accuracy required in the extra-masters' examination. His contention is that the papers set in the examination-room should above all things tend to make men better practical navigators, and he believes that any impartial judge must admit that the methods advocated in these pages for the "Sumner" problem are superior in many points to that which is at present encouraged by the Board of Trade examinations. The advantages may be thus summarized: (1) Greater accuracy; (2) fewer figures, and consequently less time required for the work; (3) one chart does for any navigable latitude; and (4) many observations which would be considered useless for the ordinary "Sumner" give excellent results with even fewer figures by combining ex-meridian and chronometer observations together, as illustrated in this work by various examples. Most officers pass the examination for master many years before they get command, and it is hardly to be expected that they will keep a supply of "Sumner" charts for the various latitudes that they trade in; consequently the practice of this method, which they have learnt for their examination, is sure to be neglected. The writer, speaking for himself, can testify that he never used it at sea, though, much to his regret, for more than ten years he has had to teach it or examine candidates in their knowledge of it.

Very shortly after the publication of the writer's first edition of the A and B azimuth tables the late Mr. W. H. Rosser published abridged A, B, and C tables for the same purpose, and afterwards slightly ex-

tended them for publication in "Norie's Epitome." They are excellent tables, and very concise, but even as enlarged in "Norie" require in most places considerable interpolation, the time-interval being sometimes 20 minutes and 30 minutes apart, which naturally could not admit of as much accuracy as a fuller table. A few years later Captain Lecky asked and obtained the writer's permission to publish the A and B azimuth tables in his famous "Wrinkles." Captain Lecky then extended and improved them, and later on published them in a separate book with further extensions and improvements, showing how the tables can be used for quite a number of navigational problems.

In closing, the author has much pleasure in acknowledging the kind help voluntarily tendered to him by Captain Thomas Liddle, and in thanking him for his disinterested labours in the calculation of much of the extension of these tables. But for his perseverance in continuing to urge the writer to extend his tables it is very improbable that they would ever have been published in their present revised form. He would also like to thank the Hon. Mr. Hall-Jones, Minister of Marine, and the New Zealand Government for valuable clerical assistance in the compilation of a portion of these tables, for the confidence they have reposed in him. and for their liberality and public spirit in the interest of navigation all over the world in thus publishing an extension of navigational tables far beyond the limits of New Zealand's own trade.

H. S. BLACKBURNE.

April, 1905.

PREFACE TO FOURTH EDITION.

SINCE the publication of the first edition of these tables in New Zealand by the New Zealand Marine Department the work has more than doubled in size, and the additional pages have no doubt increased the value and usefulness of the work.

At the request of the Commander and Navigating Lieutenant of the British Antarctic Expedition s.s. "Terra Nova," the limits of the A and B Tables have been further extended so as to include all latitudes and declinations between the terrestial and the celestial North and South Poles. The tables are thus made available for azimuth, greatcircle sailing, and reduction to the meridian for every part of the globe, and for every star in the heavens.

A Traverse Table and Table C^1 have been added giving the azimuth to the nearest minute of arc up to 45° from the meridian for use when special accuracy is required in conjunction with the Ex-meridian Table.⁵

This table, given to the decimal of a degree, was used in the author's original A and B Azimuth Tables published in 1883.

Table D has been extended to comprise all latitudes between 85° N. and 85° S.

Mr. H. B. Goodwin, R.N., formerly Examiner at the Royal Naval College, Greenwich, has drawn the writer's attention to the value of this table as an azimuth table, when both altitude and time are given, and he has in this edition given Mr. Goodwin's rule, and an example for using it in this direction, as well as explaining the purposes for which it was first calculated.

The possessor of the book can make his own choice as to whether he uses Table D or Tables A, B, and C in the calculation of azimuths. Probably he will find D the handiest when the body is near the meridian, and (as its accuracy depends principally on the *altitude*) it will give a more accurate azimuth than the time-azimuth tables when the D.R. latitude used in the calculation of the time azimuth is incorrect, while the other tables will certainly give greater accuracy, without any uncertainty as to the naming of the azimuth, when the body is near the prime vertical.

It is not, therefore, recommended that Table D should be used for azimuth purposes when the object of observation is too near the prime vertical, as close accuracy cannot then be expected, and there will then be uncertainty as to the naming of the bearing. A further extension and improvement on the Ex-meridian Table No. I has been made giving the reduction to the meridian with high altitudes up to 45° from the meridian.

This table, as well as Ex-meridian Table No. 2, were published in 1908 for use in conjunction with the A and B Tables. Although the tables only comprise a few pages they cover wider limits of use than most other ex-meridian tables, being available for every degree of latitude and declination from Pole to Pole, and they are equally available for below-Pole, as for above-Pole observations.

The table for correction of sun's and star's altitude has been extended for heights from 6 ft. to 80 ft.

The table giving the apparent times of the meridian passages of the principal fixed stars has been calculated with great care for the year 1910 (midway between two leap years), so that for any year for some time to come the error will not amount to more than about two minutes, with the single exception of Star Polaris, which has an increasing change in R.A. of nearly 29 sec.

In this table the times of *inferior* as well as the *superior* transits of no less than forty-five of the circumpolar stars are given.

This should be a great boon to navigators, as (so far as the author knows) no other navigational works give the times of star's meridian passages at the *inferior* transit, notwithstanding the special value of the below-Pole star for determining latitudes, on account of its slow motion in altitude and azimuth.

A small table comprising two pages has been added after the ex-meridian table showing the error in latitude by ex-meridian due to 4 seconds of error in the time. This table is especially useful in facilitating work in connection with the problem of finding the position of ship from two ex-meridians or one ex-meridian and a chronometer observation, and quite dispenses with any need of a chart.

A year or two ago the Board of Trade sanctioned the use of these tables for the time-azimuth problem in the New Zealand examinationrooms for candidates for foreign-going certificates for masters and mates, and already the great majority of the New Zealand candidates use them in preference to Burdwood's and Davis's Tables.

Even naval officers after a very short trial of our tables have written to the author expressing their preference for them to the larger tables which are in general use in the Navy, quite apart from the fact of their far greater limits of use.

I would again respectfully urge the Board of Trade to allow the use of our tables to candidates in the examinations for masters and mates in other countries, at least in Canada, where much of the Canadian coast-line is outside the latitude limits of the tables which they are obliged to use in the examinations.

It is a matter of regret, and has been much commented on, that, owing to New Zealand having to comply with Board of Trade Regulations in respect to certificates for foreign-going vessels, we are still unable to use in our examinations the methods and navigational tables which we have compiled, at much labour and cost, for facilitating various problems in navigation, notwithstanding that the methods advocated in this work and assisted by the tables published herein give proof of much greater accuracy in the problem of determining the ship's position from two observations of the sun out of the meridian than by the method which we are obliged to use in our examinations to comply with the Board of Trade Regulations.

The use, too, of the plane chart in the Sumner problem, which has been such a boon to the few who know about it, is still precluded from use in the examinations, and consequently it will take many years before the bulk of navigators know the advantages of it.

HAROLD S. BLACKBURNE.

Wellington, New Zealand, June, 1916.

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EXPLANATION OF TABLES.

The A, B, and C Azimuth Tables.

TABLES A and B are used in combination—(1) for finding the error of the longitude due to an error of one minute (1') of latitude, and (2) by the aid of Table C to find the azimuth or true bearing of celestial objects.

Enter Table A with the hour-angle and latitude, and Table B with the hour-angle and declination, naming the factors taken from these tables according to the following rule:—

For Table A—When hour-angle is less than 6 hours, name the factors taken from this table *contrary* to name of latitude.

When hour-angle is greater than 6 hours, name the factors taken from Table A the *same* as the name of the latitude.

For Table B—Always name the factors taken from Table B the same as the name of declination.

Add like and subtract unlike names. The sum or difference then of the factors from A and B will be the difference of longitude correction due to 1' of error in the latitude. The correction must be named according to the name of the greater factor.

The direction of this longitude correction (or the position-line, as it may be termed) is found by keeping the name thus obtained, and reversing the name of the object's bearing E. or W. of meridian.

For the Azimuth—With the A and B cor. thus found and named, enter Table C with the latitude and this cor.; the corresponding azimuth is then taken out direct, and is given to the nearest decimal of a degree. It is named N. or S. according to the name of the cor., and East or West as the hour-angle is east or west of the meridian. The azimuth with these tables never exceeds 90° . This saves the trouble (which also confuses some when using the large azimuth tables) of having to subtract the azimuth taken out from 180° , and change the name of azimuth.

For examples in use of the table see pages 119 and 120, and for great-circle sailing page 121.

Traverse Table and Table C¹.

For the Azimuth when greater accuracy is required.—When using the azimuth table to assist in the reduction to the meridian it is important to take out the azimuth with greater precision than is necessary under ordinary circumstances for compass-correction or position-lines. For this purpose a traverse-table (pages 58-67) and Table C¹ (pages 68-74 are used as follows:—

Rule.—Turn the A \pm B (= difference of longitude correction) into departure by the traverse table, and take out the *azimuth* corresponding to the factor from the azimuth Table C¹. The azimuth in this table is given to the nearest minute of arc for 45° from the meridian.

Examples: To find the Azimuth.

(1.) Lat.
$$4^{1'3}$$
 S.
 \bigcirc 's Decl. $23^{\circ}5$ S.
H.A. 7h. 10m. W. (p. 43) C $\overline{729}$ S. gives Az. S. $6^{\circ}1^{\circ}2$ W.

I-Azimuth.

(2.) Lat. $\stackrel{\circ}{43}_{30}$ S. (p. 20) A $\stackrel{\circ}{452}$ N. (p. 63) $\stackrel{\circ}{10}_{503} = \stackrel{\circ}{725}_{365}$ H.A. 4h. 18m. (p. 21) B $\stackrel{\circ}{1955}$ S. (p. 60) $\stackrel{\circ}{503} = \stackrel{\circ}{365}_{365}$ D. long. $\stackrel{\circ}{1503}_{503}$ Dep. $\stackrel{\circ}{1090}_{503}$ = Dep. $\stackrel{\circ}{1090}_{503}$ gives Az. (C¹, p. 69) S. $\stackrel{\circ}{42^{\circ}}_{32'}$.

For further examples see pages 119–120, and on page 121 for great-circle sailing-courses.

FORMULÆ USED IN THE CALCULATION OF THE TABLES.

A = tang of latitude \times cotang of hour-angle.

B = tang of declination \times cosec of hour-angle.

For C "Azimuths," cot azim. = cor. \times cos latitude, where cor. is the result of the sum or diff. of A and B.

For C¹ "Azimuths," cotan azim. = correction.

For C^2 "Position-lines," tan position-line = correction.

INTERPOLATION.

When it is deemed necessary to interpolate, this can usually be done at sight, except for the hour-angles up to the first hour from the meridian, and in a high latitude up to the second hour from the meridian.

For Table A, when both time and latitude are nearly midway between that given in the table, interpolate diagonally; for example, lat. 40° 30', hour-angle 2 h. 22 m., it will be seen at a glance that 1'20 is the correct factor. For Table B there is no appreciable difference in 4 m. of time (except in the very small hour-angles), and it is therefore only necessary to interpolate *vertically* for the fraction of the degrees of declination. For the bright stars no interpolation is necessary even for the declination, as the declination of a star does not appreciably change for many years, and the factors are here calculated for the stars' declination corresponding to the year 1910. For both Tables A and B the interpolation of the small hour-angles up to 1 hour should be effected by dividing the quantity given at 1 m. by the number of minutes that the body observed is from the meridian. The variation to 1' of latitude at 0 h. 1 m. is given to assist in the interpolation for the odd minutes of latitude, in case surveyors or others should require a very accurate azimuth.

The following example will illustrate how the interpolation may here be effected:—

Lat. 40° 36′, H.A. o h. 10 m.: required the azimuth.

Lat. 40° at o h. 1 m. A. = 192.3' var. to 1' of lat. = 6.82" or 6.82' to 1° of lat. Cor. to 36' = +4.110)196.4 Lat. $40^{\circ} 36' = 196.4 = \text{from Table C Az. } 3.8^{\circ}$

If greater accuracy is required, $19.64' \times \cos |at. 40^\circ 36' |accuracy | 36' = -$

19·64' 40° 36'	$\log \cos \theta$	1·2931 9·8804
3° 50'	cot	11.1735

Example to find the Difference of Longitude due to Error in the Latitude.

In lat, by D.R. 16° 30' N., hour-angle 2 h. 44 m. E. and \bigcirc 's declination 11° S., the longitude was found to be 40° 50' E. Required the longitude, in latitude 16° 38 N., the latitude previously worked with having been found to be 8' in error.

A = B =	· 34' 5. · 30' S.
Sum	$\overline{\begin{array}{c} \mathbf{64'} \\ 8 \end{array}}$ S. to W. = cor. or error in the longitude due to
Lat. found to be 8' N. of D.R.	8 r' of error in the latitude.
Cor. to 8' of lat	5'12' or 5' 7'2" S. to W. or N. to E.
Lat. 16° 3	o' N. gives long. 40° 50 50° E.
Cor. due	to 8' of lat. 0° 5 7 E.

Knowing the error of longitude due to an error of τ' of latitude, we have the means ready at hand of quickly determining both the latitude and longitude when two suitable observations have been taken of celestial objects.

40 55 7 E.

Lat. 16° 38' N. gives long.

This may be effected either by plotting the two positions and position-lines on the chart, which is the ordinary "Sumner" problem (worked with only two instead of the usual four hour-angles), or the position may be found even more expeditiously by simple proportion.

The actual trend of the position-line for plotting on the *plane* chart may be found from Table C², attending to the rule there given; or, by subtracting the azimuth as found from Table C from 90° , and reversing the name of the object's bearing, the *true* position-line will be found for plotting on a *Mercator* chart.

Any single observation, whether on or near the meridian, or prime vertical, or any other bearing, simply gives a position as being somewhere on a line of bearing at right angles to the bearing of object. If a second observation is taken after the body has changed its bearing, or another body is observed at the same time having a different bearing, we get another line of position, and the intersection of the two position-lines will give the latitude and longitude of the observer. Without the trouble of putting the position on the chart, the same principle may be worked out by a little proportion sum.

The three elements used in finding the time or longitude are latitude, altitude, and declination. If these three elements are correctly known, the *same* time or the *same* longitude will be found by every celestial body observed, whatever the bearing may be. If, therefore, the declination and altitude *are* correctly known, any difference of longitude found, resulting from the observation of different bodies (or the same body after an interval of time between the observations), must be due to error in the *latitude*.

The error in longitude due to 1' error of latitude is given by the A and B Tables. It becomes, therefore, a simple matter of proportion to find the correction to apply to the latitude used in finding the longitude. Say the longitudes resulting from the observation of two different stars are 15' apart, and with star No. 1 every 1' north of latitude throws the longitude 0.8' more to the east, with star No. 2 every 1' north of latitude throws the longitude 1.2' more to the west; then every 1' of error in the latitude will throw the longitude 2' apart, and the error of latitude will be found by the proportion 2' d. long. :: 1' lat. : $7\frac{1}{2}'$ lat.

This would be represented on the chart by the accompanying figure.

The writer has found the ship's position b this method many hundreds of times, and find that he gets a more accurate latitude in this wa than even by the meridian altitude, experience having shown that although an altitude may often be slightly in error, yet a correct *difference* in altitude is generally measured, or the same amount of error will generally be thrown into both observations, and when this is the case (if the observations are suitably chosen) small errors



in altitude practically make no difference in the latitude. Observations which have been taken in the quicksilver of two stars not near the meridian, or of two sun observations with a suitable interval of time between them, have generally given the latitude within o'i' of the truth, when taken where the position of places has been accurately known.

3

Table C².—Position-lines.

Table C² gives the position-lines corresponding to the A and B correction at any time for plotting on a plane scale chart. By the aid of this small table any one possessing a protractor rule with the ordinary diagonal, or any other scale of inches, can plot the "Summer" position in his sight-book with even greater accuracy than he could obtain it from the ordinary "Summer" Mercator charts. The table does not give the *true* geographical lines of position, but lines of position which will give the same result as to latitude and longitude on a plane chart as the true lines of position would give on a Mercator chart. See instruction at foot of page under the table (p. 75).

Table D.—Altitude and Time-azimuth Table, showing the Error produced in the time or Longitude by an Error of 1' in the Altitude.

This table gives best results for azimuth when body is near the meridan. It will not give accurate results when body is near the prime vertical, and there is then uncertainty as to naming the azimuth N. or S. of the prime vertical.

Rule for finding the Azimuth.

With H.A. as Az. and decl. as lat., go to Table D. Take out coefficient; call it M. With alt. as lat. and M., take out Az. at top or side.

EXAMPLE.

Lat. 41° S. * Canopus (decl. 52° 39' S.) H.A. 3h. 10m. 40s. = $47^{\circ} 40'$. Alt. 56° 5'.

Required the Azimuth.

Lat. (decl.) $52^{\circ} 39'$ gives M. = 8.92. Lat. (alt.) $56^{\circ} 5'$, and M. 8.92 gives Az. 532° .

Table D will be found very useful in working out separately a set of observations, both with artificial horizon and at sea; or for working out another person's observations, taken within a few minutes of the same time. It also shows at sight the degree of dependence of any observation. And if at any time it is found that an erroneous altitude has been worked with, the longitude will readily be corrected by this table, a greater altitude giving a smaller hour-angle, or with A.M. sights a greater altitude making the longitude more to the eastward, and a lesser altitude making the longitude more to the westward—*vice versa* with p.M. sights.

It will also be found useful when taking time azimuths by the sun or stars (when altitude is low) for readily obtaining the correct hour-angle, as in the following example: Lat. 20° N., * Arcturus bearing N. 71° E. (true), altitude 5°. Table D at lat. 20° and azimuth 71° gives 4.5 m. of time to 1° change of alt. Table 26 (Raper), lat. 20° N., decl. 20° N., gives *'s hour-angle at rising or setting 6 h. 30m.

$$4.5 \text{m.} \times 5^\circ = -22\frac{1}{2}$$

* 's H.A. at
$$5^{\circ} = 6 7\frac{1}{2}$$

The results of the table can be easily found by inspection from the traverse table. At the Equator, when the sun or any other heavenly body is on the prime vertical, it moves at the rate of 1° in 4° m., or 1' in 4° of time; and, in any other latitude, when the sun is on the prime vertical, the ratio of its movement will be dep.: diff. long. Having, then, the rate of movement in any latitude on the prime vertical, the rate of movement on any other bearing may be found by the traverse table.

Example.—In latitude 30° , and \odot 's bearing N. 63° E., required the rate at which it moves. In latitude 30° , against 4 in D. lat. column, is 4.62 in dist. column; with \odot 's bearing 63° , and 4.62 in dep. column, we have 5.18 in distance column = 5.18 s. to 1' of altitude.

The following formula was used in the calculation of the table: D = secant of latitude \times cosecant of azimuth \times 4.

Further examples in the use of the table are given on pages 105 and 125.

Table E.-Altitude Corrections of Sun and Stars.

This table (the upper half for the sun, and the lower half for the stars) gives the lump correction to apply to their observed altitudes, involving for the sun dip, refraction, semidiameter, and parallax, and for the stars dip and refraction.

As the correction for very small altitudes changes rapidly, a supplementary table is given on page 87 for the correction of both sun and stars, at a height of 40 ft. above sea-level, for altitudes between 3° and 11° , for every few minutes of altitude, and for other heights greater or less than 40 ft. a second correction is given in same table.

Heights are given from 6 ft. to 8 oft. so as to meet the need of navigators in every class of vessel, from the smallest to the largest. As standard authorities still slightly differ in their dip and refraction tables, a mean of the dip and refraction given in the three standard works (Raper, Inman, and Norie) has been used in the calculation of the table here given, and great care has been taken to insure accuracy.

Table F.-Acceleration Table.

This table is used for converting intervals of mean solar time into equivalent intervals of sidereal time. The seconds column which is given in most navigational tabular works has here been omitted for the sake of space, and because it is considered quite unnecessary in ordinary practical navigation. In practical navigation it becomes necessary in nearly all the problems where stars are used to convert mean solar time into sidereal time, as, for instance, in the time azimuth, longitude by chronometer, and the ex-meridian problems. In these problems the time is generally taken by a chronometer keeping mean solar time, and to compare this with the sidereal time found by the stellar observation it must be reduced to sidereal time.

Examples will be found among some of the worked-out problems which follow the tables in this book.

Table G.-Star Polaris Azimuth Table.

This table is useful especially in latitudes between 15° N. and 30° N., as, for instance, in the Red Sea. In a high latitude the altitude will be too high for compass-correction work, and it is not therefore given beyond 60° of latitude.

Examples in the use of table are given later on in this book.

The table has been calculated for stars' declination in 1910 - viz., $88^{\circ} 49' 33'57'' N$.

The Mean Places of 108 of the Brightest Stars, in order of Right Ascension, for 1st January, 1917.

On pages 7-8 the *mean* places of 108 of the brightest stars are given, in the order of their right ascension, for the 1st January, 1917. In the column headed "Mag." the adopted unit of brightness is designated 1°0. The magnitudes of stars are determined to tenths of a magnitude with reference to this adopted unit. The magnitudes of the ten stars brighter than the unit are indicated by figures less than 1°0: thus, the value o'3 for Arcturus indicates that that star is seven-tenths of a magnitude brighter than the unit; the value $-1^{\cdot}4$ for Sirius that it is 2'4 magnitudes brighter than the unit. As the right ascensions and declinations of the stars do not change uniformly throughout the year, the correction for intermediate months cannot be made accurately by multiplying the annual change by a fraction of the year; but the change is so small that for navigational purposes at sea the right ascensions and declinations here given may be used without appreciable error for azimuths and latitudes, and even for longitude the error due to using these elements would seldom exceed a mile. When accuracy is required the navigator should use the "Admiralty Nautical Almanac," where the right ascensions and declinations of these and many other stars are given very minutely for every ten days throughout the year.

Approximate Apparent, Times of the Meridian Passages of the Principal Fixed Stars.

The times are given in this table for the 1st of each month, and the meridian of Greenwich. To find the time for any other day subtract the portion of time corresponding to the day of the month in the day-correction table. Add 1 min. for every 90° of east longitude and subtract 1 min. for every 90° of west longitude.

 go° of east longitude and subtract 1 min. for every go° of west longitude. The time of the meridian passage of each star has been carefully calculated to the nearest second of time, and is given in the table to the nearest minute.

For the circumpolar stars which never set in higher latitudes than 50° N. or S. the times of the meridian passages of the *inferior* as well as the *superior* transit has been given.

EXAMPLE AND CAUTION IN USING THIS TABLE.

Required the meridian passage of * β Centauri on 31st October, in longitude 10° W.

	н. м.
Mer. pass. of $*\beta$ Centauri on 1st Oct.	is I 30 p.m.
Cor. for 31st day	- 1 52
	D
Approx. time	31, 23, 38 = 11, 38 a.m. on 1st Nov.
2nd cor. required	- 4
	D
Approx. mer. pass. $* \beta$ Centauri	31 23 34 or 11 34 a.m. on 1st. Nov.

The interval in this case is within 2 hours of 31 days instead of 30 days, therefore nearly 4 minutes more correction is required to be subtracted. The correction for longitude would be less than 10 seconds.

The table is calculated for the year 1910, but will be within $2 \min$ for many years, with the single exception of the * Polaris which has an annual and increasing change in R.A. of over 27 s., and will therefore be about $5 \min$. later in passing the meridian in 10 years' time.

Supplementary Ex-meridian Tables, &c.

Explanations given on pages 142 and 143.

7 THE MEAN PLACES OF 108 OF THE BRIGHTEST STARS

IN ORDER OF RIGHT ASCENSION,

FOR 1st JANUARY, 1917.

Star s Name.	Mag.	Mag. Right Ascension.			
a Andromedæ (Alpheratz) β Cassiopeiæa Phœnicisa Cassiopeiæ β Ceti(Deneb Kartos)	2°2 2°4 2°4 Var. 2°2	H. M. S. 0 4 5 6 0 4 44 4 0 22 11 0 0 35 47 2 0 39 25 4	s. +3.09 3.12 2.95 3.38 3.00	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+ 20.0 + 20.0 - 20.0 + 19.8 - 19.8
$\begin{array}{cccc} \gamma & \text{Cassiopeiæ} & \dots & \dots \\ \beta & \text{Andromedæ} & \dots & (Mirach) \\ \delta & \text{Cassiopeiæ} & \dots & \dots \\ a & \text{Ursæ Minoris} & \dots & (Polaris) \\ a & \text{Eridani} & \dots & \dots & (Achernar) \\ \end{array}$	2°3	0 51 41.2	+ 3.60	N. 60 16 3	+ 19.5
	2'4	1 5 4.8	3.34	N. 35 10 51	+ 19.2
	2'8	1 20 22.4	3.86	N. 59 48 16	+ 18.8
	2'1	1 30 13.2	28.99	N. 88 51 44	+ 18.5
	0'6	1 34 37.5	2.23	S. 57 39 29	- 18.4
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2·7	I 50 3'I	+ 3.30	N. 20 24 10	+17 ^{.8}
	2·3	I 58 47'8	3.67	N. 41 55 55	+17 ^{.4}
	2·2	2 2 29'4	3.36	N. 23 4 14	+17 ^{.3}
	2·8	2 57 56'3	3.13	N. 3 45 53	+14 ^{.3}
	1·9	3 18 23'3	4.27	N. 49 34 0	+13 ^{.0}
a Tauri $(Aldebaran)$ β Orionis $(Rigel)$ a Aurigæ $(Capella)$ γ Orionis $(Bellatrix)$ β Tauri $(Nath)$	1°1	4 31 9'4	+ 3 [.] 44	N. 16 20 36	+ 7.6
	0°3	5 10 32'9	2 [.] 88	S. 8 17 48	- 4.3
	0°2	5 10 33'3	4 [.] 42	N. 45 54 54	+ 4.3
	1°7	5 20 40'7	3 [.] 22	N. 6 16 31	+ 3.4
	1°8	5 21 2'6	3 [.] 79	N. 28 32 18	+ 3.4
a Leporis ε Orionis (Alnilam) ζ Orionis (Ist *) α Columbæ (Phact) κ Orionis (Saiph)	2·7	5 29 4'I	+ 2 65	S. 17 52 51	- 2.7
	1·7	5 32 0'I	3 04	S. 1 15 15	- 2.4
	2·0	5 36 34'2	3 03	S. 1 59 9	- 2.0
	2·7	5 36 38'5	2 17	S. 34 7 4	- 2.0
	2·2	5 43 49'2	2 84	S. 9 41 54	- 1.4
a Orionis(Betelguese) β Aurigæ(Menkalinan) θ Aurigæ β Canis Majorisa Argûs(Canopus)	Var.	5 50 40'7	+ 3 [.] 25	N. 7 23 33	+ 0.8
	2°1	5 53 26'4	4 [.] 41	N. 44 56 25	+ 0.6
	2°7	5 54 3'7	4 [.] 09	N. 37 12 29	+ 0.5
	2°0	6 19 2'7	2 [.] 64	S. 17 54 50	+ 1.7
	– 0 9	6 22 6'5	1 [.] 33	S. 52 39 0	+ 1.9
$\begin{array}{ccccccc} \gamma & Geminorum & \dots & (Alhena) & \dots \\ \alpha & Canis Majoris & \dots & (Strius) & \dots \\ \tau & Argûs & \dots & \dots & \dots \\ \epsilon & Canis Majoris & \dots & (Adara) & \dots \\ \delta & Canis Majoris & \dots & \dots & \dots \end{array}$	1'9 -1'6 2'8 1'6 2'0	6 32 55 1 6 41 29 3 6 47 52 6 6 55 21 8 7 5 1 0	+ 3.46 2.68 1.49 2.36 2.44	N. 16 28 16 S. 16 36 6 S. 50 30 56 S. 28 51 30 S. 26 15 39	$ \begin{array}{r} - 2.9 \\ + 3.6 \\ + 4.2 \\ + 4.8 \\ + 5.6 \\ \end{array} $
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2°7 2°4 2°0 0°5 1°2	7 14 12 6 7 20 48 8 7 29 18 3 7 34 57 4 7 40 14 4	+2.12 2.37 3.85 3.19 3.72	S. 36 56 52 S. 29 8 26 N. 32 4 19 N. 5 26 19 N. 28 13 40	$\begin{array}{r} + & 6.4 \\ + & 6.9 \\ - & 7.6 \\ - & 8.1 \\ - & 8.5 \end{array}$
	2.3	8 0 40°0	+ 2.11	S. 39 46 8	+10.1
	2.2	8 6 58°4	1.85	S. 47 5 29	+10.2
	1.7	8 20 48°7	1.24	S. 59 14 31	+11.6
	2.0	8 42 24°7	1.66	S. 54 24 15	+13.0
	1.8	9 12 17°7	0.70	S. 69 22 31	+14.9
$\begin{array}{ccccc} \iota \operatorname{Argûs} & \ldots & \ldots & (Tureis) & \ldots \\ \kappa \operatorname{Argûs} & \ldots & \ddots & \ddots \\ a \operatorname{Hydr} & \ldots & \ldots & (Alphard) & \ldots \\ a \operatorname{Leonis} & \ldots & \ldots & (Regulus) & \ldots \\ \gamma^1 \operatorname{Leonis} & \ldots & \ldots & (Algeiba) & \ldots \end{array}$	2·3	9 14 52.0	+ 1.61	S. 58 55 36	+ 15.1
	2·6	9 19 32.5	1.86	S. 54 39 21	+ 15.3
	2·2	9 23 30.6	2.95	S. 8 17 54	+ 15.5
	1·3	10 3 57.2	3.21	N. 12 22 24	- 17.5
	2·6	10 15 23.9	3.29	N. 20 15 43	- 18.0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2.8	10 43 11.7	+ 2·57	S. 48 58 53	+ 18.9
	2.4	10 56 50.6	3·63	N. 56 49 39	- 19.3
	2.0	10 58 37.1	3·74	N. 62 11 58	- 19.3
	2.6	11 9 41.8	3·18	N. 20 58 43	- 19.6
	2.2	11 44 49.6	3·10	N. 15 2 10	- 20.0

THE MEAN PLACES OF 108 OF THE BRIGHTEST STARS-continued.

8

Star's Na	me.	Mag.	Right Ascension.	Annual Change.	Declination-	Annual Change.
$\begin{array}{cccc} \gamma & \text{Ursæ Majoris} & \dots \\ \delta & \text{Centauri} & \dots \\ \gamma & \text{Corvi} & \dots \\ \alpha & \text{Crucis} (\text{mean}) & \dots \\ \gamma & \text{Crucis} & \dots \end{array}$	(Pheoda) 	2°5 2°9 2°8 1°1 1°6	H. M. S. II 49 28'3 I2 4 3'0 I2 II 32'I I2 2I 58'6 I2 26 33'0	s. +3'16 3'10 3'09 3'32 3'31	N. 54 9 22 S. 50 15 37 S. 17 4 52 S. 62 38 23 S. 56 38 54	- 20'0 + 20'0 + 20'0 + 20'0 + 20'0 + 19'9
$\begin{array}{cccc} \gamma & \text{Centauri} & \dots & \dots \\ \beta & \text{Crucis} & \dots & \dots \\ \epsilon & \text{Ursæ Majoris} & \dots \\ \zeta^1 & \text{Ursæ Majoris} & \dots \\ a & \text{Virginis} & \dots & \dots \end{array}$		2'4 1'5 1'7 2'4 1'2	12 36 55'9 12 42 51'7 12 50 22'9 13 20 35'2 13 20 49'1	+3.31 3.49 2.63 2.41 3.16	S. 48 30 15 S. 59 14 7 N. 56 24 36 N. 55 21 31 S. 10 43 43	+ 19 ^{.8} + 19 ^{.7} - 19 ^{.6} - 18 ^{.8} + 18 ^{.8}
	(Benetnasch) 	2.6 1.9 3.1 0.9 2.3	I3 34 37'I I3 44 16'3 I3 50 21'2 I3 57 57'2 I4 I 47'5	+3.79 2.38 3.73 4.21 3.56	S. 53 2 42 N. 49 43 38 S. 46 52 49 S. 59 58 24 S. 35 57 44	+18.4 -18.0 +17.8 +17.4 +17.3
α Boötis η Centauri α^2 Centauri α Lupi ϵ^2 Boötis	(Arcturus) 	0.2 2.7 0.3 2.9 2.7	14 11 52'5 14 30 13'8 14 33 57'7 14 36 24'0 14 41 21'7	+2.81 3.80 4.54 3.98 2.62	N. 19 36 50 S. 41 47 38 S. 60 29 31 S. 47 1 58 N. 27 25 25	$ \begin{array}{r} -16.8 \\ +15.9 \\ +15.7 \\ +15.6 \\ -15.3 \end{array} $
	(Kochab) (Alphacca) (Unukalhai)	2.2 2.8 2.3 2.8 2.5	14 50 56 0 14 53 5 3 15 31 10 4 15 40 10 7 15 55 25 3	$ \begin{array}{r} -0.20 \\ +3.92 \\ 2.53 \\ 2.94 \\ 3.54 \end{array} $	N. 74 29 41 S. 42 48 2 N. 26 59 36 N. 6 41 9 S. 22 23 12	$ \begin{array}{r} -14.7 \\ +14.6 \\ -12.1 \\ -11.5 \\ +10.4 \end{array} $
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	(Akrab) (Antares) 	2'9 1'2 2'7 1'9 2'4	16 0 36 5 16 24 18 9 16 32 35 2 16 39 51 8 16 44 47 0	+3.48 3.67 3.30 6.32 3.93	S. 19 34 45 S. 26 14 56 S. 10 24 0 S. 68 52 37 S. 34 8 37	+10.0 + 8.1 + 7.5 + 6.9 + 6.5
$ \begin{array}{ccccc} \eta & \text{Ophiuchi} & \dots & \dots \\ \beta & \text{Aræ} & \dots & \dots \\ \lambda & \text{Scorpii} & \dots & \dots \\ \alpha & \text{Ophiuchi} & \dots & \dots \\ \theta & \text{Scorpii} & \dots & \dots \end{array} $		2.6 2.8 1.7 2.1 2.0	17 5 37 0 17 18 23 8 17 27 58 2 17 31 4 9 17 31 21 1	+3.44 4.98 4.07 2.78 4.31	S. 15 37 24 S. 55 27 10 S. 37 2 40 N. 12 37 10 S. 42 56 47	$ \begin{array}{r} + 4.7 \\ + 3.6 \\ + 2.8 \\ - 2.5 \\ + 2.5 \\ \end{array} $
κ Scorpii γ Draconis ε Sagittarii α Lyræ σ Sagittarii	(Rastaban) (Kaus Australis) (Vega)	2`5 2`4 2`0 0`1 2`1	17 36 44'7 17 54 40'7 18 18 39'8 18 34 7'7 18 50 7'2	+4 ^{.15} 1 [.] 39 3 [.] 99 2 [.] 01 3 [.] 72	S. 38 59 17 N. 51 29 53 S. 34 25 30 N. 38 42 21 S. 26 24 3	+ 2.0 - 0.5 - 1.6 + 3.0 - 4.3
ζ Sagittarii σ Octantis α Aquilæ α Pavonis γ Cygni	'South Pole Star) (Altair)	2.7 5.5 0.9 2.1 2.3	18 57 19.9 19 27 42.2 19 46 44.0 20 19 5.4 20 19 14.9	+3.82 94.42 2.89 4.76 2.15	S. 30 0 0 S. 89 13 29 N. 8 38 54 S. 57 0 7 N. 39 59 25	- 5.0 - 7.5 + 9.0 - 11.4 + 11.4
a Cygni e Cygni a Cephei e Pegasi a Gruis	(Deneb) (Alderamin)	1·3 2·6 2·6 2·5 2·2	20 38 36.1 20 42 51.1 21 16 36.0 21 40 6.6 22 3 0.5	+2.04 2.40 1.41 2.94 3.78	N. 44 58 59 N. 33 39 31 N. 62 14 1 N. 9 29 38 S. 47 21 49	+12.8 +13.1 +15.2 +16.4 -17.5
$\begin{array}{ccc} \beta & \text{Gruis} & \dots \\ \alpha & \text{Piscis Australis} \\ \alpha & \text{Pegasi} & \dots \end{array}$. (Fomalhaut) . (Markab)	2.2 1.3 2.6	22 37 43.0 22 53 4.0 23 0 37.5	+3.58 3.30 2.98	S. 47 19 9 S. 30 3 45 N. 14 45 30	- 18·8 - 19·2 + 19·4

[NOTE.—In this table + means add, and - means subtract.]

In the column headed "Mag." the adopted unit of brightness is designated 1.0. The magnitudes of stars are determined to tenths of a magnitude with reference to this adopted unit : thus the value -1.6 for Sirius indicates that that star is 2.6 magnitudes brighter than the unit ; the value 0.3 for Arcturus indicates that that star is seven-tenths of a magnitude brighter than the unit.

Approximate Apparent Times of the Meridian Passages of the Principal Fixed Stars at Greenwich on the First Day of each Month, 1910.

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	Name.	Mag.	Jan.	Feb.	Mar.	April.	Мау.	June.	July. A	ug. Se	pt. O	ct.	Nov.	Dec.
†5 †5	δ Centauri α Andromedæ β Cassiopeiæ $α^1$ Crucis α Phœnicis 	2.8 2.1 2.4 1,0 2.4	н м. 5 18 5 18 5 19 5 36 5 36	н. м. 3 б 3 б 3 7 3 24 3 24	H. M. I 17 I 17 I 18 I 35 I 35	H M. 23 20 23 20 23 21 23 38 23 38	н. м. 21 29 21 29 21 30 21 47 21 47	н. м. 19 27 19 27 19 27 19 27 19 44 19 45	н м. н 17 23 15 17 23 15 17 23 15 17 23 15 17 40 15 17 41 15	м. н. 1813 1813 1913 3613 3613	M H. 2211 2311 2311 4011 4111	м. н 35 34 35 52 53	и. м. 9 39 9 39 9 40 9 57 9 57	н. м. 7 36 7 36 7 36 7 36 7 53 7 53 7 54
+S +S +S +N	$\begin{array}{ccc} \gamma \ Crucis & \\ \gamma \ Centauri & \\ \beta \ Ceti & . \\ \beta \ Crucis & \\ e \ Ursæ Majoris \end{array}$	1.6 2.4 2.2 1.5 1.8	5 41 5 51 5 54 5 57 6 4	3 29 3 39 3 41 3 45 3 52	1 40 1 50 1 52 1 56 2 3	23 43 23 53 23 55 0 2 0 10	21 51 22 2 22 4 22 8 22 15	19 49 19 59 20 2 20 5 20 13	17 45 15 17 55 15 17 58 15 18 1 15 18 9 16	41 13 51 13 53 13 57 14 4 14	45 I I 55 I 2 58 I 2 I I 2 9 I 2	57 10 7 10 10 19 13 10 21 10	0 1 0 12 0 14 0 18 0 25	7 58 8 8 8 11 8 14 8 22
†N	γ Cassiopeiæ β Andromedæ δ Cassiopeiæ ζ ¹ Ursæ Majoris Polaris	2·3 2·4 2·8 2·1 2·1	6 6 6 19 6 34 6 35 6 41	3 54 4 7 4 22 4 23 4 29	2 5 2 18 2 33 2 34 2 39	0 11 0 25 0 40 0 40 0 46	22 16 22 30 22 45 22 46 22 51	20 14 20 27 20 43 20 43 20 43	18 10 16 18 23 16 18 39 16 18 39 16 18 39 16 18 45 16	6 14 19 14 34 14 35 14 41 14	10 12 23 12 39 12 39 12 46 12	22 10 36 10 51 10 51 10 59 1	0 26 0 40 0 55 0 55 1 3	8 23 8 36 8 52 8 52 8 52 8 59
+S +N +S	e Centauri Achernar η Ursæ Majoris β Arietis β Centauri	2.6 0.5 1.9 2.7 0.8	6 48 6 49 6 58 7 4 7 12	4 36 4 37 4 46 4 5 ² 5 0	2 47 2 48 2 56 3 3 3 11	0 54 0 54 I 4 I 9 I 17	22 59 22 59 23 9 23 15 23 23	20 57 20 57 21 7 21 12 21 20	18 53 16 18 53 16 19 3 16 19 8 17 19 16 17	48 14 49 14 58 15 4 15 12 15	53 13 53 13 3 13 8 13 16 13	5 11 5 11 15 11 20 11 28 11	1 9 1 9 1 19 1 25 1 32	9 6 9 6 9 16 9 21 9 29
ts ts ts	$\begin{array}{c} \gamma^{1} \text{Andromed} \mathscr{Z} \\ \theta \\ \text{Centauri} \\ \alpha \\ \text{Arietis} \\ \alpha^{2} \text{Centauri} \\ \alpha \\ \text{Lupi} \\ \end{array}$	2°2 2°1 2°2 1°0 2°5	7 13 7 16 7 16 7 48 7 50	5 I 5 4 5 4 5 35 5 38	3 12 3 15 3 15 3 15 3 47 3 49	I 18 I 21 I 22 I 53 I 56	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	21 21 21 24 21 25 21 56 21 58	19 17 17 19 20 17 19 21 17 19 52 17 19 54 17	13 15 16 15 17 15 48 15 50 15	17 13 20 13 21 13 52 14 54 14	29 11 32 11 33 11 4 12 7 12	1 33 1 36 1 37 2 9 1 2 11	9 30 9 33 9 34 10 5
†N †S	β Ursæ Minoris α Ceti α Persei Aldebaran α Tri. Australis	2.2 2.8 1.9 1.1 1.9	8 5 8 12 8 32 9 44 9 53	5 53 6 0 6 20 7 32 7 4 ¹	4 4 4 11 4 31 5 44 5 5 ²	2 II 2 17 2 37 3 50 3 59	0 20 0 26 0 47 1 59 2 8	22 13 22 20 22 40 23 53 0 5	20 9 18 20 16 18 20 36 18 21 49 19 21 57 19	5 16 12 16 32 16 44 17 53 17	9 14 16 14 36 14 49 16 57 16	21 12 28 12 48 12 1 14 9 14	26 1 32 1 53 1 53 1 5 1	0 22 0 29 0 49 2 2 2 10
†S	CapellaRigelβ Aræγ Orionisβ Tauri	0.2 0.3 2.7 1.7 1.8	10 24 10 24 10 31 10 34 10 34	8 12 8 12 8 19 8 22 8 22 8 22	6 23 6 23 6 30 6 33 6 33	4 29 4 30 4 37 4 40 4 40	2 38 2 39 2 46 2 49 2 49	0 36 0 36 0 44 0 46 0 47	22 28 20 22 28 20 22 28 20 22 36 20 22 36 20 22 38 20 22 38 20 22 39 20	24 18 2 24 18 2 31 18 3 34 18 3 34 18 3	28 16 28 16 36 16 38 16 39 16	40 14 40 14 48 14 50 14 51 14	44 I 45 I 52 J 55 I 55 I	2 41 2 41 2 49 2 51 2 52
	a Leporis e Orionis 5 Orionis k Orionis Betelguese	2.7 1.7 2.0 2.2 Var.	10 42 10 45 10 50 10 57 11 4	8 30 8 33 8 38 8 45 8 52	6 41 6 44 6 49 6 56 7 3	4 48 4 51 4 55 5 3 5 9	2 57 3 0 3 4 3 12 3 19	0 55 2 0 58 2 1 2 2 1 9 2 1 16 2	22 47 20 22 50 20 22 54 20 23 1 20 23 8 21	42 18 4 46 18 5 51 18 5 57 19 4 19	7 16 50 17 54 17 1 17 8 17	59 15 2 15 6 15 14 15 20 15	3 1 6 1 11 1 18 1 25 1	3 0 3 3 3 7 3 14 3 21
†N	$ \begin{array}{c} \beta \ \text{Auriga} & & \\ \theta \ \text{Auriga} & & \\ \gamma \ \text{Draconis} & & \\ \beta \ \text{Canis Majoris} \\ \hline \text{Canopus} & & \\ \end{array} $	2'I 2'7 2'4 2'0 I'0	11 6 11 7 11 8 11 32 11 35	8 54 8 55 8 56 9 20 9 23	7 6 7 6 7 7 7 31 7 34	5 12 5 13 5 14 5 38 5 41	3 21 3 22 3 23 3 47 3 50	I 192 I 202 I 202 I 452 I 482	23 II 21 23 II 21 23 I2 21 23 37 21 23 40 21	6 19 1 7 19 1 8 19 1 32 19 3 35 19 4	I 17 1 17 2 17 7 17 0 17	23 15 24 15 25 15 49 15 52 15	27 I 28 I 29 I 53 I 56 I	3 24 3 25 3 25 3 50 3 53
†N	$\begin{array}{c} \gamma \text{ Geminorum } \\ Vega \\ Sirius \\ \tau \text{ Argûs } \\ \epsilon \text{ Canis Majoris } \end{array}$	1'9 0'1 -1'4 2'8 1'6	11 46 11 47 11 55 12 1 12 8	9 34 9 35 9 43 9 49 9 56	7 45 7 46 7 54 8 0 8 8	5 52 5 53 6 0 6 7 6 14	4 I 4 2 4 9 4 16 4 23	I 58 2 2 0 2 2 7 2 13 2 21	3 50 21 3 52 21 0 3 21 0 10 22 0 17 22	46 19 5 47 19 5 55 19 5 1 20 8 20 1	0 18 2 18 9 18 1 5 18 1 3 18 2	3 16 4 16 11 16 18 16 25 16	7 1. 8 1. 15 1. 22 1. 29 1.	4 3 4 5 4 12 4 18 4 26
	δ Canis Majoris π Argûs η Canis Majoris <i>Castor</i> <i>Procyon</i>	2.0 2.7 2.4 2.0 0.5	12 18 1 12 27 1 12 34 1 12 42 1 12 48 1	0 6 0 15 0 22 0 30 0 36	8 17 8 26 8 33 8 41 8 47	6 24 6 33 6 40 6 48 6 54	4 33 4 42 4 49 4 57 5 3	2 30 2 40 2 46 2 55 3 0	0 27 22 0 36 22 0 42 22 0 51 22 0 56 22	18 20 2 27 20 3 34 20 3 42 20 4 48 20 5	2 18 3 2 18 4 8 18 5 6 18 5 2 19	35 16 4 16 50 16 59 17 4 17	39 14 48 14 55 14 3 1 9 1	1 35 1 45 1 51 5 0 5 5
ts	Pollux ζ Argûs γ Argûs α Pavonis ϵ Argûs	1.2 2.3 1.9 2.0 1.7	12 53 1 13 14 1 13 20 1 13 32 1 13 34 1	0 41 1 2 1 8 1 20 1 23	8 52 9 13 9 19 9 31 9 33	6 59 7 19 7 26 7 38 7 4 0	5 8 5 28 5 35 5 46 5 49	3 5 3 26 3 32 3 44 3 46	I 2 22 I 22 23 I 28 23 I 40 23 I 42 23	53 20 5 14 21 1 20 21 2 32 21 3 34 21 3	7 19 1 8 19 3 4 19 3 6 19 4 8 19 5	0 17 0 17 7 17 8 17 0 17	14 1 34 1 41 1 52 1 55 1	5 10 5 31 5 37 5 49 5 51

+ N. or + S.—These times relate to the Meridian Passages of Circumpolar Stars at the Inferior Transit, N. or S. denoting the Declination of the Star.

10 Approximate Apparent Times of the Meridian Passages of the Principal Fixed Stars at Greenwich on the First Day of each Month, 1910—continued.

	Name.	Mag.	Jan.	Feb.	Mar.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
† N † N	α Cygni δ Argûs β Argûs ι Argûs α Cephei	1'3 2'0 1'7 2'2 2'6	н. м. 1351 1355 1425 1428 1429	H. M. II 40 II 43 I2 I3 I2 I6 I2 I7	н. м. 9 50 9 54 10 24 10 27 10 28	н. м. 7 57 8 1 8 31 8 33 8 33	H. M. 6 6 6 10 6 40 6 42 6 44	H. M. 4 4 4 8 4 38 4 40 4 42	H. M. 2 0 2 4 2 34 2 36 2 38	н. м. 23 51 23 55 0 29 0 32 0 33	H. M. 21 56 22 0 22 30 22 32 22 34	н. м. 20 8 20 12 20 42 20 44 20 46	H. M. 18 12 18 16 18 46 18 49 18 50	н. м. 16 9 16 13 16 42 16 45 16 45
†S	κ Argûs a Hydræ a Gruis Regulus γ ¹ Leonis	2.6 2.2 1.9 1.3	14 32 14 36 15 15 15 16 15 28	12 20 12 24 13 3 13 4 13 16	10 31 10 35 11 14 11 16 11 27	8 38 8 42 9 21 9 22 9 34	6 47 6 51 7 30 7 31 7 43	4 45 4 49 5 28 5 29 5 40	2 41 2 45 3 24 3 25 3 36	0 36 0 40 1 19 1 20 1 32	22 37 22 40 23 20 23 21 23 32	20 49 20 53 21 32 21 33 21 44	18 53 18 57 19 36 19 37 19 49	16 50 16 53 17 33 17 34 17 45
†S	$ \begin{array}{cccc} \beta & \text{Gruis} & \dots \\ \mu & \text{Argûs} & \dots \\ \beta & \text{Ursæ Majoris} \\ Dubhe & \dots \\ \delta & \text{Leonis} & \dots \end{array} $	2°1 2°8 2°4 2°0 2°6	15 50 15 55 16 9 16 11 16 22	13 38 13 44 13 57 13 59 14 10	11 49 11 55 12 8 12 10 12 21	9 56 10 1 10 15 10 17 10 28	8 5 8 10 8 24 8 26 8 37	6 2 6 8 6 22 6 23 6 34	3 59 4 4 4 18 4 19 4 30	I 54 I 59 2 I3 2 I5 2 26	23 55 0 4 0 17 0 19 0 30	22 7 22 12 22 26 22 28 22 39	20 11 10 16 20 30 20 32 20 43	18 7 18 13 18 26 18 28 18 39
†N	$ \begin{array}{c} \beta \text{ Leonis } \\ \gamma \text{ Ursæ Majoris} \\ \delta \text{ Centauri } \\ \beta \text{ Cassiopeiæ } \\ \gamma \text{ Corvi } \end{array} $	2°2 2°5 2°8 2°4 2°7	16 57 17 1 17 16 17 17 17 23	14 45 14 50 15 4 15 5 15 12	12 56 13 1 13 15 13 16 13 23	11 3 11 7 11 22 11 23 11 29	9 12 9 16 9 31 9 32 9 38	7 9 7 14 7 29 7 29 7 36	5 6 5 10 5 25 5 25 5 32	3 I 3 6 3 20 3 21 3 28	1 5 1 10 1 24 1 25 1 32	23 14 23 18 23 33 23 34 23 40	21 18 21 22 21 37 21 38 21 44	19 14 19 19 19 33 19 34 19 41
†S	$\begin{array}{cccc} a^{1} \text{Crucis} & \dots \\ a & \text{Phcenicis} & \dots \\ \gamma & \text{Crucis} & \dots \\ \gamma & \text{Centauri} & \dots \\ \beta & \text{Crucis} & \dots \end{array}$	1.0 2.4 1.6 2.4 1.5	17 34 17 34 17 38 17 49 17 55	15 22 15 22 15 27 15 37 15 43	13 33 13 33 13 38 13 48 13 54	II 40 II 40 II 44 II 55 I2 I	9 49 9 49 9 53 10 4 10 10	7 46 7 47 7 51 8 1 8 7	5 43 5 43 5 47 5 57 6 3	3 3 ⁸ 3 3 ⁸ 3 43 3 53 3 59	1 42 1 42 1 47 1 57 2 3	23 51 23 51 23 55 0 9 0 15	21 55 21 55 21 59 22 10 22 16	19 51 19 52 19 56 20 6 20 12
†N †N †N	 ε Ursæ Majoris γ Cassiopeiæ β Andromedæ δ Cassiopeiæ ζ¹Ursæ Majoris 	1.8 2.3 2.4 2.8 2.1	18 2 18 3 18 17 18 32 18 32	15 50 15 52 16 5 16 20 16 21	14 2 14 3 14 16 14 31 14 32	12 8 12 9 12 23 12 38 12 38	10 17 10 18 10 32 10 47 10 47	8 15 8 16 8 29 8 45 8 45	6 11 6 12 6 25 6 41 6 41	4 6 4 8 4 21 4 36 4 37	2 IT 2 I2 2 25 2 40 2 4I	0 23 0 24 0 37 0 53 0 53	22 23 22 24 22 38 22 53 22 53	20 19 20 21 20 34 20 49 20 50
†N †S	Spica \dots Polaris \dots Achernar \dots ϵ Centauri \dots η Ursæ Majoris	1°2 2°1 0°5 2°6 19	18 33 18 39 18 46 18 46 18 56	16 21 16 27 16 35 16 34 16 44	14 32 14 37 14 46 14 46 14 55	12 39 12 44 12 52 12 52 13 2	10 48 10 53 11 1 11 1 11 1	8 45 8 51 8 59 8 59 9 9	6 41 6 47 6 55 6 55 7 5	4 37 4 43 4 51 4 50 5 0	2 41 2 48 2 55 2 55 3 4	0 53 1 0 1 7 1 7 1 17	22 53 23 1 23 7 23 7 23 17	20 50 20 57 21 4 21 4 21 13
†N	ς Centauri β Centauri γ^{I} Andromedæ θ Centauri Arcturus	2.8 0.8 2.2 2.1 0.3	19 2 19 9 19 10 19 13 19 2 3	16 50 16 58 16 58 17 2 17 12	15 1 15 9 15 10 15 13 15 23	13 8 13 15 13 16 13 19 13 30	11 17 11 24 11 25 11 28 11 39	9 15 9 22 9 23 9 26 9 36	7 11 7 18 7 19 7 22 7 32	5 6 5 14 5 14 5 17 5 28	2 10 3 18 3 19 3 22 3 32	1 22 1 30 1 31 1 34 1 44	23 23 23 30 23 31 23 34 23 44	21 19 21 27 21 28 21 31 21 41
1.1	η Centauri a^2 Centauri a Lupi ϵ^2 Boötis β Ursæ Minoris	2.7 1.0 2.5 2.6 2.2	19 42 19 45 19 48 19 53 20 3	17 30 17 34 17 36 17 41 17 51	15 41 15 45 15 47 15 52 16 2	13 48 13 51 13 54 13 59 14 9	11 57 12 0 12 3 12 8 12 18	9 54 9 58 10 0 10 6 10 15	7 50 7 54 7 56 8 2 8 12	5 46 5 50 5 52 5 57 6 7	3 50 3 54 3 56 4 1 4 11	2 2 2 6 2 8 2 13 2 23	0 7 0 10 0 13 0 18 0 28	21 59 22 3 22 5 22 10 22 20
ŧΝ		2.7 1.9 2.3 2.8 2.5	20 4 20 30 20 43 20 51 21 7	17 53 18 18 18 31 18 40 18 55	16 4 16 29 16 42 16 51 17 6	14 10 14 36 14 49 14 5 ⁸ 15 13	12 19 12 45 12 58 13 7 13 22	10 17 10 42 10 55 11 4 11 19	8 13 8 38 8 5? 9 0 9 15	6 9 6 34 6 47 6 56 7 11	4 13 4 38 4 51 5 0 5 15	2 25 2 50 3 3 3 12 3 27	0 29 0 55 1 7 1 16 1 32	22 22 22 47 23 0 23 9 23 24
·	$ \begin{array}{c} \beta^{1} \operatorname{Scorpii} \\ Antares \\ \zeta \text{ Ophiuchi} \\ a \text{ Tri. Australis} \\ \epsilon \text{ Scorpii} \end{array} $	2.7 1.3 2.7 1.9 2.3	21 12 21 35 21 44 21 51 21 56	19 0 19 24 19 32 19 39 19 44	17 11 17 35 17 43 17 50 17 55	15 18 15 42 15 50 15 57 16 2	13 27 13 50 13 59 14 6 14 11	11 24 11 48 11 56 12 3 12 8	9 21 9 44 9 52 9 59 10 5	7 16 7 40 7 48 7 55 8 0	5 20 5 44 5 52 5 59 6 4	3 3 ² 3 5 ⁶ 4 4 4 11 4 16	I 37 2 0 2 9 2 16 2 21	23 29 23 53 0 5 0 12 0 18
†N	η Ophiuchi Capella β Aræ λ Scorpii a Ophiuchi	2.6 0.2 2.7 1.8 2.1	22 17 22 21 22 29 22 39 22 42	20 5 20 10 20 17 20 27 20 30	18 15 18 21 18 29 18 38 18 42	16 23 16 28 16 35 16 45 16 48	14 32 14 36 14 44 14 54 14 57	12 29 12 34 12 42 12 52 12 55	10 25 10 30 10 38 10 48 10 51	8 21 8 26 8 33 8 43 8 46	6 25 6 30 6 38 6 47 6 51	4 37 4 42 4 50 5 0 5 3	2 42 2 46 2 54 3 4 3 7	0 38 0 43 0 51 I I I 4

†N. or †S.—These times relate to the Meridian Passages of Circumpolar Stars at the *Inferior* Transit, N. or S. denoting the Declination of the Star.

11

Approximate	Apparent	Times of	the Me	ridian	Passages	of the	Principal	Fixed	Stars	at
	Greenwic	h on the l	First Da	y of ea	ach Month	, 1910-	-continue	d. '		

-		-				_			Contraction of the second					1.
	Name.	Mag.	Jan.	Feb.	Mar	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
+N +S +S	 θ Scorpii κ Scorpii β Aurigæ γ Draconis ε Sagittarii Canopus Vega τ Argûs σ Sagittarii ζ Sagittarii 	2.0 2.6 2.1 2.4 1.9 -1.0 0.1 2.8 2.1	H. M. 22 42 22 48 23 4 23 6 23 29 23 33 23 45 0 3 0 5	H. M 20 30 20 30 20 52 20 54 21 18 21 21 21 33 21 47 21 49 21 52	H. M. 18 42 18 47 19 4 19 5 19 29 19 33 19 44 19 58 20 0	H. M. 16 48 16 54 17 10 17 12 17 36 17 39 17 51 18 5 18 7 18 14	H. M. I4 57 I5 3 I5 19 I5 21 I5 44 I5 48 I6 0 I6 14 I6 16 I6 23	H. M. 12 55 13 0 13 17 13 18 13 42 13 46 13 58 14 11 14 13 14 13	H. M. H IO 51 IO 56 II I3 II 15 II 38 II 42 II 54 I2 7 IC I2 IO IC	м. 3 46 3 52 3 8 10 34 37 37 37 37 37 37 37 37 37 37	H. M. 6 51 6 56 7 13 7 14 7 38 7 42 7 53 8 7 8 9	H. M. 5 3 5 8 5 25 5 26 5 50 5 50 5 54 6 6 6 20 6 22 6 22	H. M. 3 7 3 13 3 29 3 31 3 54 3 58 4 10 4 24 4 26	H. M. I 4 I 9 I 26 I 28 I 51 I 54 2 7 2 21 2 23
ts ts ts ts ts	3 Sagittarin $Altair$ γ Argûs a Pavonis γ Cygni ϵ Argûs α Cygni δ Argûs ϵ Cygni δ Argûs α Cygni δ Argûs α Argûs	2.7 0.9 1.9 2.0 2.3 1.7 1.3 2.0 2.6 1.7 2.2	I 22 I 22 I 33 I 34 I 36 I 54 I 57 I 58 2 27 2 30	22 46 23 6 23 18 23 18 23 20 23 37 23 41 23 42 0 15 0 18	20 57 21 17 21 29 21 31 21 49 21 53 21 53 22 22 22 25	10 14 19 3 19 24 19 36 19 36 19 36 19 36 19 36 19 36 19 55 19 59 20 0 20 29 20 32	10 23 17 12 17 33 17 44 17 45 17 45 17 47 18 4 18 8 18 8 18 8 18 8 18 8 18 8 18 8 18 8 18 8 18 8 18 8 18 8 18 8 18 4 18 4	14 21 15 10 15 30 15 42 15 42 15 42 15 44 16 2 16 6 16 6 16 36 16 36 16 38	12 17 13 6 13 26 13 38 13 39 13 40 13 58 14 2 14 32 14 34 14 34	12 12 12 12 12 12 12 12 12 12 12 12 12 1	9 6 9 26 9 38 9 38 9 38 9 38 9 58 10 1 10 2 10 31 10 34	0 29 7 18 7 38 7 50 7 51 7 52 8 10 8 14 8 44 8 46	4 33 5 22 5 43 5 54 5 55 5 56 6 14 6 18 6 18 6 18 6 48 6 50	2 30 3 19 3 39 3 51 3 52 3 53 4 12 4 15 4 15 4 45 4 45 4 47
†N †N †N	a Cephei κ Argús ϵ Pegası a Gruis β Gruis β Ursæ Majoris Dubhe α Pegasi γ Ursæ Majoris Majoris	2.6 2.6 2.5 1.9 2.1 1.3 2.4 2.0 2.6 2.5	2 31 2 34 2 55 3 17 3 52 4 7 4 11 4 13 4 15 5 4	0 19 0 22 0 43 1 5 1 40 1 55 1 59 2 1 2 3 2 52	22 27 22 30 22 50 23 13 23 47 0 6 0 10 0 12 0 14 1 3	20 33 20 36 20 57 21 19 21 54 22 9 22 13 22 13 22 13 22 13 22 13 23 6	18 42 18 45 19 6 19 28 20 3 20 18 20 22 20 24 20 26 21 15	16 40 16 43 17 3 17 26 18 0 18 16 18 19 18 21 18 23 19 12	14 36 12 14 39 12 14 59 12 15 22 13 15 56 13 16 12 14 16 16 14 16 16 14 16 17 14 16 19 14 17 8 15	311 341 551 521 521 521 521 111 111 131 151 541	10 36 10 38 10 59 11 22 12 12 12 15 12 17 12 17 12 19 13 8	8 48 8 51 9 11 9 34 10 9 10 24 10 28 10 29 10 31 11 20	0 52 6 55 7 15 7 38 8 12 8 28 8 32 8 34 8 36 9 24	4 49 4 52 5 12 5 35 6 10 6 25 6 29 6 30 6 32 7 21

+N or +S.—These times relate to the Meridian Passages of Circumpolar Stars at the Inferior Transit, N. or S. denoting the Declination of the Star.

Correction of the	Times in th	he preceding	Table for the	Day of the	Month (te	o be	subtracted)
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$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					•	-					`		· · ·
H. M. H. M. <th< td=""><td>Days.</td><td>Jan.</td><td>Feb.</td><td>Mar.</td><td>April.</td><td>May.</td><td>June.</td><td>July.</td><td>Aug.</td><td>Sept.</td><td>Oct.</td><td>Nov.</td><td>Dec.</td></th<>	Days.	Jan.	Feb.	Mar.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
I 0		н. м.	H. M.	H M.	Н. М.	H. M.	Н. М	H. M.	Н. М.	Н. М.	н. М.	н. м.	н. м.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	I	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2	04	0 4	0 4	0 4	0 4	0 4	04	0 4	04	04	0 4	04
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	0 9	0 8	0 7	0 7	0 8	0 8	0 8	0 8	0 7	0 7	0 8	0 9
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4	0 13	0 12	OII	0 11	O II	0 12	0 12	0 12	O II	0 11	0 12	0 13
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	0 18	0 16	0 15	0 15	0 1 5	0 16	0 16	0 15	0 Í4	0 15	0 16	0 17
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	6	0 22	0 20	0 19	0 18	0 19	0 21	0 21	0 19	o 18	0 18	0 20	0 22
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	7	0 26	0 24	0 22	0 22	0 23	0 25	0 25	0 23	0 22	0 22	0 24	0 26
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	0 30	0 28	0 26	0 26	0 27	0 29	0 29	0 27	0 25	0 25	0 28	0 30
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	9	0 35	0 32	0 30	0 29	0 30	0 33	0 33	0 31	0 29	0 29	0 32	0 35
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	o 39	0 36	0 33	0 33	0 35	0 37	0 37	0 35	0 32	0 33	0 36	0 39
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	II	0 43	0 40	0 37	0 36	0 39	0 41	0 41	0 38	0.36	0 37	0 40	0 44
13 0 52 0 48 0 44 0 46 0 49 0 46 0 43 0 44 0 46 0 49 0 46 0 43 0 44 0 46 0 49 0 46 0 43 0 44 0 48 0 52 14 0 56 0 52 0 48 0 50 0 54 0 53 0 50 0 47 0 48 0 52 0 57 15 1 1 0 55 0 55 0 58 17 0 57 0 54 0 55 1 0 16 17 1 9 1 3 59 0 59 1 2 1 6 1 15 1 1 3 1 9 1 5 1 1 1 10 1 14 1 13 1 9 <td>12</td> <td>0 48</td> <td>0 44</td> <td>0 41</td> <td>0 40</td> <td>0 42</td> <td>0 45</td> <td>0 45</td> <td>0 42</td> <td>0 40</td> <td>0 40</td> <td>0 44</td> <td>0 48</td>	12	0 48	0 44	0 41	0 40	0 42	0 45	0 45	0 42	0 40	0 40	0 44	0 48
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	13	0 52	0 48	0 44	0 44	0 46	0 49	0 49	0 46	0 43	0 44	0 48	0 52
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	14	0 56	0 52	0 48	0 48	0 50	0 54	0 53	0 50	0 47	0 48	0 52	0 57
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	15	ГI	0 56	0 52	0 51	0 54	0 58	0 57	0 53	0 50	0 51	0 56	II
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	ıĞ	I 5	1 0	0 55	0 55	0 58	I 2	II	0 57	0 54	0 55	ΙΟ	I 6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	17	IЯ	II 3	0 59	0 59	I 2	і б	I 5	II	0 58	0 59	I 4	I IO
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	18	I I3	1 7	I 2	I 2	т б	I 10	19	15	II	I 3	I 9	I 15
20 I 22 I I5 I I0 I I4 I I9 I I7 I I2 I 8 I I0 I I7 I I2 I I0 I I1 I1 <thi1< th=""> <thi1< th=""> <th< td=""><td>19</td><td>1 18</td><td>III</td><td>1 G</td><td>I 6</td><td>1 10</td><td>I I4</td><td>1 13</td><td>I 8</td><td>1 5</td><td>1 G</td><td>I I 3</td><td>I 19</td></th<></thi1<></thi1<>	19	1 18	III	1 G	I 6	1 10	I I4	1 13	I 8	1 5	1 G	I I 3	I 19
21 1 26 1 19 1 14 1 13 1 18 1 23 1 21 1 16 1 12 1 14 1 21 1 28 21 21 1 20 1 19 1 14 1 13 1 18 1 23 1 21 1 16 1 12 1 14 1 21 1 28 21 21 1 20 1 10 1 10 1 10 1 10 1 10 1 1	20	I 22	I 15	I 10	1 10	I I4	1 19	1 17	I 12	I 8	I IO	I 17	I 24
	21	1 26	1 19	I I4	I I3	I 18	I 23	I 21	I 16	I 12	I I4	I 21	I 28
	22	I 3I	1 23	1 17	I 17	I 22	1 27	I 25	I 19	I 16	I 18	I 25	I 32
23 I 35 I 26 I 2I I 2I I 26 I 3I I 29 I 23 I 19 I 21 I 30 I 37	23	J 35	1 26	1 21	I 2I	126	I 3I	I 29	I 23	I 19	I 2I	1 30	J 37
24 I 39 I 30 I 24 I 25 I 30 I 35 I 33 I 27 I 23 I 25 I 34 I 4I	24	1 39	1 30	I 24	I 25	I 30	I 35	I 33	I 27	I 23	I 25	I 34	I 41
25 I 43 I 34 I 28 I 28 I 34 I 39 I 37 I 31 I 26 I 29 I 38 I 46	25	I 43	I 34	1 28	I 28	I 34	I 39	I 37	I 3I	I 26	I 29	138	I 46
26 I 47 I 38 I 32 I 32 I 38 I 44 I 41 I 34 I 30 I 33 I 42 I 50	26	I 47	I 38	I 32	I 32	I 38	I 44	I 4I	I 34	1 30	I 33	I 42	1 50
27 I 51 I 42 I 35 I 36 I 42 I 48 I 45 I 38 I 34 I 37 I 47 I 55	27	1 51	1 42	I 35	I 36	I 42	I 48	I 45	I 38	I 34	I 37	I 47	I 55
28 1 56 1 45 1 39 1 40 1 46 1 52 1 49 1 42 1 37 1 41 1 51 1 59	28	I 56	I 45	I 39	I 40	I 46	I 52	I 49	I 42	I 37	I 4I	I 5I	I 59
29 2 0 . I 43 I 44 I 50 I 56 I 53 I 45 I 41 I 44 I 55 2 3	29	2 0	.,	I 43	I 44	1 50	I 56	I 53	I 45	I 4I	I 44	I 55	2 3
30 2 4 . I 46 I 47 I 55 2 0 I 57 I 49 I 44 I 48 I 59 2 8	30	24		1 46	I 47	I 55	2 0	I 57	I 49	I 44	148 148	I 59	28
3I 2 8 I 50 I 59 2 I I 52 I 52 2 I2	31	2 8		I 50		I 59		2 I	I 52		1 52		2 12

 $\mathbf{12}$

Table n.

wi I	hen ho	uran	gle is	less th	han 6	hour	s, nan	ne the	ours	rs tal	ken fro	m Tal	ole A	contra	ry to r	ame	of lat.
Lat	m. 01	Var. to 1' of Lat.	m.	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 00
•		Lat.	1,			},	;	1.	1.		1.	1	,	,		,	
01	•0 4•0	4·00 4·00	1.00	•00 •50	°00 '33	°00 °25	·oc ·20	·00 17	00 [.] 00	.00 12	.00	.00	.00	.00 00	.00 .08	*00 *07	•00 •07
2	8.0	4.01	2.00	1.00	.67	•50	·40	:33	•28	.25	.22	'20	.18	.16	.12	.14	•13
3	12.0	4.01	3.00	2.00	1.00	1.00	·00 •80	·50	43	·37	·33	·30 ·40	·27 ·36	·25 ·33	•23 •30	•21 •28	·20 ·26
5	20.1	4.03	5.01	2.21	1.62	1.52	1.00	•83	71	•62	•55	•50	•45	•41	. 38	•35	.33
6	24'I	4.05	6.02	3.01	2.01	1.20	1.50	1.00	•86	:75	•66	•60	:54	.49	•46	.42	:39
7 8	32.2	4.08	8.03	3 ^{.52} 4 ^{.02}	2.34	2.01	1.40	1.17	1.14	1.00	-70	·70 •80	·03	·50 ·66	·53 ·61	·49 ·56	·40 ·52
9	36.3	4.10	9.07	4.54	3.02	2.27	1.81	1.21	1.29	1.13	1.00	.90 T.00	·81	.75	·69	•64	·59
	40 4	4.15	101	505	2.71	2.78	2.02	1.85	1 44 T'58	1 23	1.22	1.10	1.00	03	.84	•71	
12	44 5	4.18	12.5	6.00	4.06	3.04	2.43	2.02	1.73	1.21	1.34	1.51	1.00	1.00	·92	.85	73
13	52.9	4.21	13.5	6.61	4.41	3.30	2.64	2.20	1.88	1.64	1.46	1.31	1.18	1.00	1.00	.93	·86
15	61.4	4.29	15.4	7.67	5.11	3.83	3.00	2.55	2.18	1.01	1.69	1.25	1.38	1.56	1.10	1.02	1.00
16	65.7	4.33	16.4	8.21	5.47	4.10	3.28	2.73	2.34	2.04	1.81	1.63	1.48	1.32	1.24	1.12	1.02
17 18	70'I 74'5	4.37	17.5	8.75	5·83	4.37	3.49	3.00	2.49	5.1 8	1.03	1.23 1.84	1.22 1.62	1'44 1'53	1.35	1.30	I'I4 I'21
19	78.9	4.47	19.7	9.86	6.57	4.92	3.94	3.28	2.80	2.42	2.17	1.92	1.22	1.62	1.49	1.38	1.20
20	83.4	4.23	20.0	10.4	6.94	5.31	4.10	3.40	2.90	2.29	2.30	2.00	1.82	1.21	1.28	1.40	1.36
21 22	88.0 02.0	4.65	22.0 23.1	11.0 11.0	7.32	5.49	4°39 4°62	3.02	3.13	2.73	2.42	2.19	2.08	1.00	1.00	1.24 1.62	1'43 1'51
23	97'3	4.72	24.3	12.3	8.10	6.07	4.85	4.04	3.46	3.02	2.68	2.41	2.18	2.00	1.84	1.20	1.28
24 25	102.0	4·79 4·87	25.5 26.7	12'7 13'4	8.20	6.37 6.67	5.00	4.24	3.03	3.12	2.91	2°53 2°64	2.29	2.00	1.03 5.05	1.20 1.82	1.00 1.24
26	111.8	4.95	27.9	14.0	9.31	6.97	5.57	4.64	3.97	3.47	3.08	2.77	2.21	2.29	2.11	1.96	1.82
27	116.8	5.04	29.2	14.6	9.72	7:29	5.82	4.85	4.12	3.63	3.22	2.89	2.62	2.40	2.21	2.04	1.00
28 29	121.9	5·13 5·23	30.2	15'2 15'9	10 [.] 1	7.00	6.34	5.00	4 33 4 51	3.70	3.30	3.02	2.85	2.20	2'30 2'4C	2'13	2.02
30	132.3	5.33	33.1	16.2	11.0	8.26	6.60	5.49	4.20	4.11	3.62	3.22	2.97	2.72	2.20	2.32	2.12
31	137.7	5.44	34.4	17.2	11.2	8.59	6.87	5.72	4.89	4.28	3.79	3.41	3.09	2.83	2.60	2.41	2.24
32 33	143 2	5.69	35 0	179	11 9 12'4	9.29	7'42	6.18	5.29	4 45	3 95 4.10	3 54 3.68	3.34	3.06	2.81	2.60	2 33
34	154.6	5.82	38 [.] 6	19.3	12.0	9.65	7'71	6.42	5.49	4.80	4.26	3.83	3.47	3.17	2.92	2.71	2.52
33 26	166.2	0.90 6.11	401	20.8	*3 4 12.0	10.4	8.30	6.01	5.02	5.17	4 4*	597	3.24	3.43	2.12	2.01	2.01
37	172.7	6.27	43.2	21.6	14.4	10.8	8.01	7.17	6.14	5.36	4.76	4.27	3.88	3.22	3.26	3.02	2.81
38 30	179'1 185'6	6·44	44°8 46°4	22.4	14 ' 9 15'5	11 . 5	8.93 0.26	7'43	6.30 6.60	5.20	4°93	4'43 4'50	4.02	3.91	3.38	3.13	2.02
40	192.3	6.82	48.1	24.0	16.0	12.0	9.29	7.98	6.83	5.97	5.30	4.76	4.32	3.95	3.63	3.37	3.13
41	199.2	7.03	49.8	24.9	16.0	12.4	9 '94	8.27	7.08	6.19	5'49	4'93	4.47	4.09	3.77	3.49	3.24
42	200'4	7.25	51'0 53'4	25°8 26°7	17 ^{.2} 17.8	13.3	10'3 10'7	8.87	7.33	6.64	5.89	5.11	4.80	4'39	3.90	3.01	3.30
44	221.3	7.73	55'3	27.7	18.4	13.8	11.0	9.19	7.86	6.87	6.10	5.48	4.97	4.54	4.18	3.87	3.60
45	229.2	8.00	57'3	20.0	191	143	+1 4 77.9	9.21	8.42	7 12	6.7.1	507	5 14	4 70	4 33	1.1.6	373
40 47	245 ^{.8}	8.60	59 3 61 4	297 30'7	20.2	15.3	12.3	10.5	8.73	7.63	6·77	6.08	5 33 5 52	5.02	4 49 4	+ 130 + 130	4.00
48	254.5	8.93	63.6	31.8	21.2	15.9	12.7	10.0	9.05	7.90	7.01	6.30	5'71	5.23	4.81	4'45 1'61	4'14
49 50	273.1	9.69	68·3	34'I	22.7	17.0	13.6	11.3	9 3/ 9.71	8.48	7.52	6.76	6.13	5.61	5.16	1.78	4.45
51	283.0	10-1	70.7	35.4	23.6	17.7	14.1	11.2	10.1	8.79	7.80	7.00	6.35	5.81	5.35	1.92	4.61
52	293°3	10 [.] 6	73.3	36.7	24'4	10.0	14.6	12.0	10'4 10'8	0.11	8.08 8.38	7.26	6.28 6.83	6.02	5.54	5.35	4.78
55 54	315.4	11.6	78.9	39'4	26.3	19.7	15.7	13.1	11.5	9.79	8.69	7.81	7.08	6.48	5.96	5.52	5.14
.55	327.3	12.3	81.8	40.9	27'3	20'4	10.3	13.0	11.0	10.5	9.02	8.10	7.35	0.72	6.19	5.73	5.33
56 57	339'8 352'0	12·8 13·5	84'9 88'2	42°5 44°1	28.3	21 . 2 22.0	10'9 17'6	14'I 14'7	12'I 12'5	10.2	9.30 9.72	8.41 8.73	7.03	0.97	0.42 6.67	5 [.] 95	5.53
58	366.8	14.3	91.7	45.8	30.2	22.9	18.3	15.2	13.0	11.4	10.1	9.08	8.23	7.53	6.93	5.42	5.97
59 60	397.0	15·1 16·0	95'3 99'2	47 .7 49.6	33.0	24.8	19.8	15'0	14.1	12.3	10.5	9.44 9.82	8.91	8.12	7.50	5.95	6.46
	m.	1	m.	m.	m.	m	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	59]	50]	52	40	44	40 1	30	J2	20 RS.	24	20	10]	12	0	4	

When hour angle is more than 6 hours, name the factors taken from Table A the same as the name of the latitude.

1	3	

Table B.

Always name the factors taken from Table B the same as the name of declination.

1	1						(лон с	JRS.							
Decli- nation.	Var. to 1' of Decl.	m. 1	m. 4	m. 8	m. 12	m. 16	ւր. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	m. 48	m. 52	m. 56
• • • • • • • • • • • • • • • • • • •	" 4.00 4.00 4.01 4.01 4.02 4.03	'.0 4.0 8.0 12.0 16.0 20.1	, 1.00 2.00 3.00 4.01 5.01	, .50 1.00 1.50 2.00 2.51	.00 .33 .67 1.00 1.34 1.67	, 25 50 75 1.00 1.25	, 20 20 40 60 80 1.00	'00 '17 '33 '50 '67 '84	'00 '14 '29 '43 '57 '72	, 13 25 38 50 63	, 111 22 34 45 56	, 10 20 30 40 50	, .09 .18 .27 .37 .46	, .08 .17 .25 .34 .42	, .08 .16 .23 .31 .31	, .00 .07 .14 .22 .29 .36
6 7 8 9 10	4.05 4.06 4.08 4.10 4.12	24.1 28.1 32.2 36.3 40.4	6.02 7.04 8.05 9.08 10.1	3.01 3.52 4.03 4.54 5.05	2.01 2.35 2.69 3.03 3.37	1.21 1.76 2.01 2.27 2.53	1.21 1.41 1.61 1.82 2.02	1.01 1.17 1.34 1.52 1.69	·86 1·01 1·15 1·30 1·45	·76 ·88 1·01 1·14 1·27	.67 .78 .90 1.01 1.13	·61 ·71 ·81 ·91 1·02	*55 *64 *74 *83 *92	·51 ·59 ·68 ·76 ·85	*47 *55 *62 *70 *78	•43 •51 •58 •65 •73
11 12 13 14 15	4·15 4·18 4·21 4·25 4·29	44°5 48'7 52'9 57'1 61'4	11.1 12.2 13.2 14.3 15.4	5°57 6°09 6°62 7°14 7°68	3.71 4.06 4.41 4.76 5.12	2`79 3`05 3`31 3`57 3` ⁸ 4	2·23 2·44 2·65 2·86 3·07	1.86 2.03 2.21 2.39 2.56	1·59 1·74 1·89 2·05 2·20	1.40 1.53 1.66 1.79 1.93	1·24 1·36 1·48 1·59 1·71	1.12 1.22 1.33 1.44 1.54	1.02 1.11 1.31 1.40	.93 1.02 1.11 1.20 1.29	·86 ·94 1·03 1·11 1·19	·80 ·88 ·95 1·03 1·11
16 17 18 19 20	4·33 4·37 4·42 4·47 4·53	65°7 70°1 74°5 78°9 83°4	16·4 17·5 18·6 19·7 20·9	8·22 8·76 9·31 9 ^{.8} 7 10·4	5 [.] 48 5 [.] 84 6 [.] 21 6 [.] 58 6 [.] 95	4'11 4'38 4'66 4'94 5'22	3.29 3.51 3.73 3.95 4.18	2.74 2.92 3.11 3.29 3.48	2·35 2·51 2·67 2·83 2·99	2.06 2.20 2.33 2.47 2.62	1.83 1.95 2.08 2.20 2.33	1.65 1.76 1.87 1.98 2.10	1.20 1.60 1.70 1.80 1.91	1·38 1·47 1·56 1·66 1·75	1·27 1·36 1·44 1·53 1·62	1.19 1.26 1.34 1.42 1.50
21 22 23 23° 28' 24 25	4·59 4·65 4·72 4·75 4·79 4·87	88.0 92.6 97.3 99.5 102.0 106.9	22.0 23.2 24.3 24.9 25.5 26.7	11.0 11.6 12.2 12.4 12.8 13.4	7'33 7'72 8'11 8'29 8'51 8'91	5°50 5°79 6°09 6°22 6°38 6°68	4.40 4.64 4.87 4.98 5.11 5.35	3 ^{.67} 3 ^{.87} 4 ^{.06} 4 ^{.15} 4 ^{.26} 4 ^{.46}	3.15 3.32 3.48 3.56 3.65 3.83	2.76 2.90 3.05 3.12 3.20 3.35	2°45 2°58 2°71 2°78 2°85 2°98	2.21 2.33 2.44 2.50 2.56 2.69	2.01 2.12 2.22 2.28 2.33 2.44	1.85 1.94 2.04 2.09 2.14 2.24	1.71 1.80 1.89 1.93 1.98 2.07	1.59 1.67 1.75 1.79 1.84 1.93
26 27 28 29 30	4.95 5.04 5.13 5.23 5.33	111.8 116.8 121.9 127.0 132.3	27·9 29·2 30·5 31·8 33·1	14.0 14.6 15.2 15.9 16.5	9'32 9'74 10'2 10'6 11'0	6 · 99 7·30 7·62 7·95 8·28	5.60 5.85 6.10 6.36 6.62	4 ^{.67} 4 ^{.87} 5 ^{.09} 5 ^{.30} 5 ^{.52}	4.00 4.18 4.36 4.55 4.74	3.50 3.66 3.82 3.98 4.15	3°12 3°26 3°40 3°54 3°69	2.81 2.93 3.06 3.19 3.32	2·56 2·67 2·79 2·91 3·03	2·35 2·45 2·56 2·67 2·78	2·17 2·27 2·36 2·46 2·57	2°02 2°11 2°20 2°29 2°39
Names N. Decl Procy Altain Aldeb Arctu	n. Stars. n. Stars. yon paran rus	21 ·9 34 ^{.8} 67·1 81·9	5°47 8°69 16°8 20°5	2.74 4.35 8.39 10.2	1.83 2.90 5.60 6.82	1°37 2°18 4°20 5°12	1.10 1.74 3.36 4.10	91 1·45 2·80 3·42	•78 1•25 2•40 2•93	.69 1.09 2.11 2.57	.61 .97 1.87 2.28	·55 ·87 1·69 2·06	.50 .80 1.54 1.87	•46 •73 1•41 1•72	•42 •67 1•30 1•59	·39 ·63 1·21 1·48
Casto Vega Denel Capel	r b la	143'7 183'6 228'9 236'6	35'9 45'9 57'2 59'1	17*8 23*0 28*6 29*6	12°0 15°3 19°1 19°7	8·99 11·5 14·3 14·8	7'19 9'19 11'5 11'8	6°00 7°66 9°55 9°87	5°14 6°57 8°19 8°47	4°51 5°76 7°17 7°42	4.01 5.12 6.38 6.60	3.61 4.61 5.75 5.94	3.29 4.20 5.23 5.41	3°02 3°85 4°80 4°96	2·79 3·56 4·44 4·59	2°59 3°31 4°13 4°27
a Perse η Ursæ ε Ursæ a Ursæ	i Majoris Majoris Majoris	268·7 270·8 345·6 435·4	67°2 67'7 86'4 109	33 ^{.6} 33 ^{.9} 43 ^{.2} 54 [.] 4	22°4 22°6 28°8 36°3	16·8 16·9 21·6 27·2	13.5 13.6 17.3 21.8	11.3 14.4 18.2	9 [.] 62 9 [.] 70 12 [.] 4 15 [.] 6	8·43 8·49 10·8 13·6	7`50 7`55 9`64 12`1	6.75 6.81 8.68 10.9	6.12 6.19 7.90 9.96	5.64 5.68 7.25 9.14	5.21 5.25 6.70 8.44	4 ^{•85} 4 ^{•89} 6•23 7 ^{•85}
S. Deta Rigel Sirius ε Sagit λ Scorp γ Argûs	m. Stars. tarii pii s	33°5 68°3 157°1 172°9 246°4	8·36 17·1 39·3 43·2 61·6	4°18 8°54 19°6 21°6 30°8	2.79 5.69 13.1 14.4 20.5	2 ^{.09} 4 ^{.27} 9 ^{.83} 10 ^{.8} 15 [.] 4	1.67 3.42 7.86 8.66 12.3	1.40 2.85 6.56 7.22 10.3	1.20 2.44 5.62 6.19 8.82	1.05 2.14 4.92 5.42 7.72	'93 1'91 4'38 4'82 6'87	-84 1-72 3-95 4-35 6-19	·77 1·56 3·59 3·95 5·63	•70 1•43 3•30 3•63 5•17	·65 1·32 3·05 3·35 4·78	•60 1•23 2•83 3•12 4•44
a Gruis Cano γ Cruc a Pavo Ache	pus is nis rnar	249°2 300°3 347°7 353°2 362°4	62·3 75·1 86·9 88·3 90·6	31.2 37.5 43.5 44.2 45.3	20 [.] 8 25 [.] 0 29 [.] 0 29 [.] 4 30 [.] 3	15 ^{.6} 18 ^{.8} 21 ^{.7} 22 ^{.1} 22 ^{.7}	12.5 15.0 17.4 17.7 18.1	10'4 12'5 14'5 14'7 15'1	8 [.] 92 10 [.] 8 12 [.] 4 12 [.] 6 13 [.] 0	7.81 9.41 10.9 11.1 11.4	6·95 8·38 9·70 9·85 10·1	6·26 7·54 8·74 8·88 9·11	5.70 6.87 7.95 8.08 8.29	5°23 6°30 7°30 7°41 7°61	4 ^{.8} 3 5 ^{.82} 6 ^{.74} 6 ^{.85} 7 ^{.03}	4°49 5°42 6°27 6°37 6°54
β Cruc: ϵ Argû: β Centa a^2 Centa a^2 Centa a^2 Cruc a Trian β Argû	is or) s) auri auri is nguli Aus s	384.6 396.0 404.5 442.1 592.8 608.0	96 [.] 2 99 ^{.0} 101 111 148 152	48.1 49.5 50.6 55.3 74.1 76.0	32°1 33°0 33°7 36°9 49°4 50°7	24.1 24.8 25.3 27.7 37.1 38.0	19'3 19'8 20'2 22'1 29'7 30'4	16·1 16·5 16·9 18·5 24·7 25·4	13.8 14.2 14.5 15.8 21.2 21.8	12.1 12.4 12.7 13.9 18.6 19.1	10'7 11'0 11'3 12'3 16'5 17'0	9.66 9.95 10.2 11.1 14.9 15.3	8.79 9.06 9.25 10.1 13.6 13.9	8.07 8.31 8.49 9.28 12.4 12.8	7.46 7.68 7.85 8.58 11.5 11.8	6 [.] 94 7 [.] 14 7 [.] 30 7 [.] 97 10 [.] 7 11 0
		m. 59	m. 56	m. 52	m. 48	m. 44	m. 40	m. 36	m. 32 HOUI	m. 28	m. 24	m. 20	m. 16	m. 12	m. 8	m. 4

Whe	en hour	angle	is les	s than	n 6 hou	irs, na	me th	ne fac	tors ta	aken fi	om T	able A	a contr	ary to	name	of lat
Lat.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	0	4	8	12	16	20	24	28	32	36	40	44	48	52	56	00
° 0 1 2 3 4 5	*00 *07 *13 *20 *26 *33	'00 '06 '12 '18 24 '31	'00 '06 '11 '17 '23 '29	'00 '05 '11 '16 '22 '27	, .00 .05 .10 .15 .20 .25	, .00 .05 .10 .14 .19 .24	'00 '05 '09 '14 '18 '23	'00 '04 '09 '13 '17 '22	'00 '04 '08 '12 '16 '21	'00 '04 '08 '12 '16 '20	•00 •04 •07 •11 •15 •19	'00 '04 '07 '11 '14 '18	, .00 .03 .07 .10 .14 .17	, .00 .03 .07 .10 .13 .16	, .00 .03 .06 .09 .13 .16	, .00 .03 .06 .09 .12 .15
6	·39	·37	·34	•32	·31	·29	•27	·26	·25	·24	•23	·22	*21	·20	·19	·18
7	·46	·43	·40	•38	·36	·34	•32	·30	·29	·28	•26	·25	*24	·23	·22	·21
8	·52	·49	·46	•43	·41	·39	•37	·35	·33	·32	•30	·29	*28	·26	·25	·24
9	·59	·55	·52	•49	·46	·44	•41	·39	·37	·36	•34	·32	*31	·30	·29	·27
10	·66	·61	·58	•54	·51	·48	•46	·44	·42	·40	•38	·36	*35	·33	·32	·31
11	·73	·68	·64	·60	•56	·53	•51	*48	·46	·44	·42	'40	·38	-37	·35	·34
12	·79	·74	·70	·65	•62	·58	•55	*53	·50	·48	·46	'44	·42	-40	·38	·37
13	·86	·81	·76	·71	•67	·63	•60	*57	·54	·52	·50	'47	·45	-43	·42	·40
14	·93	·87	·82	·77	•72	·69	•65	*62	·59	·56	·53	'51	·49	-47	·45	·43
15	1·00	·93	·88	·82	•78	·74	•70	66	·63	·60	·57	'55	·53	-50	48	·46
16	1.07	1.00	'94	·88	·83	79	75	71	·68	·64	·61	·59	·56	54	•52	·50
17	1.14	1.07	1'00	·94	·89	-84	80	76	·72	·69	·66	·63	·60	57	•55	·53
18	1.21	1.13	1'06	1·00	·94	-89	85	80	·77	·73	·70	·67	·64	61	•59	·56
19	1.29	1.20	1'13	1·06	1·00	95	90	85	·81	·77	·74	·71	·68	65	•62	·60
20	1.36	1.27	1'19	1·12	1·06	1-00	95	90	·86	·82	·78	·75	·71	68	•66	·63
21	1.43	1.34	1.26	1·18	1.11	1.05	1 00	95	'90	·86	·82	·79	.75	·72	·69	·66
22	1.51	1.41	1.32	1·24	1.12	1.11	1 05	1.00	'95	·91	·87	·83	.79	·76	·73	·70
23	1.58	1.48	1.39	1·31	1.23	1.17	1 11	1.05	1'00	·95	·91	·87	.83	·80	·77	·74
24	1.66	1.55	1.46	1·37	1.29	1.22	1 16	1.10	1'05	1·00	·95	·91	.87	·84	·80	·77
25	1.74	1.63	1.53	1·44	1.35	1.28	1 21	1.15	1'10	1 05	1·00	·96	.92	·88	·84	·81
26	1.82	1.70	1.60	1.20	1.42	1°34	1.27	1.21	1.120	1.10	1.05	1.00	96	·92	88	·84
27	1.90	1.78	1.67	1.22	1.48	1°40	1.33	1.26	1.20	1.14	1.09	1.04	1.00	·96	•92	·88
28	1.98	1.85	1.74	1.64	1.54	1°46	1.39	1.32	1.25	1.19	1.14	1.09	1.04	1·00	•96	·92
29	2.07	1.93	1.81	1.71	1.61	1°52	1.44	1.37	1.31	1.24	1.19	1.14	1.09	1·04	1•00	·96
30	2.15	2.01	1.89	1.78	1.68	1°59	1.50	1.43	1.36	1.30	1.24	1.18	1.13	1·09	1•04	1·00
31	2°24	2·10	1.97	1.85	1.75	1.65	1.57	1.49	1.42	1·35	1.29	1.23	1.18	1.13	1.08	1.04
32	2°33	2·18	2.04	1.92	1.81	1.72	1.63	1.55	1.47	1·40	1.34	1.28	1.23	1.18	1.13	1.08
33	2°42	2·26	2.12	2.00	1.89	1.78	1.69	1.61	1.53	1·46	1.39	1.33	1.27	1.22	1.17	1.12
34	2°52	2·35	2.21	2.08	1.96	1.85	1.76	1.67	1.59	1·51	1.45	1.38	1.32	1.27	1.22	1.17
35	2°61	2· 44	2.29	2.16	2.03	1.92	1.82	1.73	1.65	1·57	1.50	1. 44	1.37	1.32	1.26	1.21
36	2.71	2·53	2·38	2·24	2.11	2.00	1.89	1.80	1.71	1.63	1.26	1.49	1°43	1°37	1.31	1.26
37	2.81	2·63	2·46	2·32	2.19	2.07	1.96	1.87	1.78	1.69	1.62	1.55	1°48	1°42	1.36	1.31
3 ⁸	2.92	2·72	2·56	2·40	2.27	2.15	2.04	1.93	1.84	1.75	1.68	1.60	1°53	1°47	1.41	1.35
39	3.02	2·82	2·65	2·49	2.35	2.22	2.11	2.00	1.91	1.82	1.74	1.66	1°59	1°52	1.46	1.40
40	3.13	2·93	2·74	2·58	2. 44	2.31	2.19	2.08	1.98	1.88	1.80	1.72	1°65	1°58	1.51	1.45
41	3 ^{•24}	3 ^{.0} 3	2·84	2.68	2·52	2·39	2·26	2·15	2.05	1.95	1.86	1.78	1.71	1.63	1.57	1.21
42	3 ^{•36}	3 ^{.1} 4	2·95	2.77	2·61	2·47	2·35	2·23	2.12	2.02	1.93	1.85	1.77	1.69	1.62	1.26
43	3 ^{•48}	3 ^{.25}	3·05	2.87	2·71	2·56	2·43	2·31	2.20	2.09	2.00	1.91	1.83	1.75	1.68	1.62
44	3 ^{•60}	3 [.] 37	3·16	2.97	2·80	2·65	2·52	2·39	2.28	2.17	2.07	1.98	1.90	1.82	1.74	1.67
45	3 ^{•73}	3 [.] 49	3·27	3.08	2·90	2·75	2·61	2·48	2.36	2.25	2.14	2.05	1.96	1.88	1.80	1.73
46	3 ^{.86}	3.61	3·39	3.19	3.01	2·85	2.70	2·56	2·44	2 33	2·22	2·12	2.03	1.95	1.87	1.79
47	4 ^{.00}	3.74	3·51	3.30	3.11	2·95	2.79	2·65	2·53	2.41	2·30	2·20	2.10	2.02	1.93	1.86
48	4 ^{.14}	3.87	3·63	3.42	3.23	3·05	2.89	2·75	2·62	2.49	2·38	2·28	2.18	2.09	2.00	1.92
49	4 ^{.29}	4.01	3·76	3.54	3.34	3·16	3.00	2·85	2·71	2.58	2·47	2·36	2.26	2.16	2.08	1.99
50	4 ^{.45}	4.16	3·90	3.67	3.46	3·27	3.10	2·95	2·81	2.68	2·56	2·44	2.34	2.24	2.15	2.06
51	4 [.] 61	4°31	4 [.] 04	3·80	3.59	3·39	3.22	3.06	2.91	2.77	2·65	2·53	2.42	2·32	2·23	2°14
52	4 [.] 78	4°46	4 [.] 19	3·94	3.72	3·52	3.33	3.17	3.02	2.87	2·74	2·62	2.51	2·41	2·31	2°22
53	4 [.] 95	4°63	4 [.] 34	4·08	3.85	3·65	3.46	3.28	3.13	2.98	2·85	2·72	2.60	2·50	2·39	2°30
54	5 [.] 14	4°80	4 [.] 50	4·24	4.00	3·78	3.59	3.41	3.24	3.09	2·95	2·82	2.70	2·59	2·48	2°38
55	5 [.] 33	4°98	4 [.] 67	4·40	4.15	3·92	3.72	3.53	3.36	3.21	3·06	2·93	2.80	2·69	2·58	2°47
56	5.53	5°17	4.85	4.56	4.31	4.07	3.86	3.67	3.49	3.33	3.18	3.04	2.91	2.79	2.67	2.57
57	5.75	5°37	5.04	4.74	4.47	4.23	4.01	3.81	3.63	3.46	3.30	3.16	3.02	2.90	2.78	2.67
58	5.97	5°58	5.23	4.93	4.65	4.40	4.17	3.96	3.77	3.59	3.43	3.28	3.14	3.01	2.89	2.77
59	6.21	5°80	5.44	5.12	4.83	4.57	4.34	4.12	3.92	3.74	3.57	3.41	3.27	3.13	3.00	2.88
60	6.46	6°04	5.67	5.33	5.03	4.76	4.51	4.29	4.08	3.89	3.71	3.55	3.40	3.26	3.12	3.00
	00	т. 5б	ш. 52	48	44	40	36	32	28	24	20	16	12	8	4	00

11 HR 10 HOURS. When hour angle is more than 6 hours, name the factors taken from Table A the same as the name of latitude.

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Table B.

Alv	ination.														0.11*	
Declination						1		100.	Ev.					1		<u>2 Hr.</u>
Decimation.	m. 00	m. 4	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 00
0	., 00	00	:00	•00	.00	:00	:00	:00	:00	.00	:00	:00	:00	:00	.00	. 00
I	·07	.00.	.06.	.06	.02	.05 .10	.05	•05	•04 •00	*04 *00	.04 .08	.04 .08	•04 08	.04 .07	.04 .07	.03 .07
3	.20	.19	.18	.17	.19	.12	.12	•14	.13	.13	.12	.15	.15	11	.11	.10
4 5	·27 ·34	·25 ·32	·24 ·30	•23 •28	·21 ·27	·20 ·26	·20 ·24	'19 '23	.18 .18	·17 ·22	.17 .21	.16 .20	.10 .12	.10 .10	.14 .18	'14 '17
6	.41	.38	•36	·3 4	.32	.31	.29	•28	•27	•26	•25	•24	•23	.22	.22	·21
7	·47	·45	·42	·40	.38	·36	·34	·33	.31 .30	·30	·29	·28	·27	·26	·25	•25
9	·61	.57	.54	.21	·49	•46	.44	.42	•41	.39	·37	.36	35	.34	.33	.32
10	.08	.04	.00	·57	·54	.52	·49	·47	*45 *50	43	·42	*40 · · · ·	·39	.38	.30	•35
11 12	.82	.77	.73	. 69	•65	·62	54 159	·57	·54	•52	·50	-44 -48	43 47	41	.44	- 39 - 4.3
13	•89 •06	·84	·79	.75 .81	·71	•68 •73	·64 ·70	•62 •67		·57	·55	·53	•51	·49	*48 *51	·46
15	1.04	.97	.92	•87	·82	•78	.75	.72	•69	·66	•63	·61	.59	.57	•55	.24
16	1.11	1.04	·98	·93	·88	·84	·80	·77	.73	·70	·68	·65	·63	·61	·59	·57
17 18	1.10	1.18	1.11	1.02	1.00	·95	.01	•87	.83	.80	.77	'74	.72	.69	.67	.65
19 20	1.33 1.33	1.32	1.18 1.18	1.18	1.02	1.00 1.01	·96 1·02	·92 ·97	·88 •93	·85 ·89	·81 ·86	.79 .83	·76 ·80	·73	·71	·69 ·73
21	1.48	1.39	1.31	1.24	1.18	1.15	1.02	1.05	·98	.94	91	·88	•85	·82	.79	.77
22	1.26	1.47	1.38	1.31	1.54	1.18	1.13	1.08	1.03	.99		.92 .07	·89	·86	·83 ·88	·81 ·85
23° 28'	1.68	1.57	1.48 1.48	1.40	1.33	1.54	1.51	1.10	1.11	1.04	1.03	.99	.96	.92	.90	.87
24 25	1.25 1.80	1.02	1.22 1.20	1.44 1.21	1.37 1.43	1.30	1.30 1.30	1.13 1.54	1.14	1.00	1.02 1.10	1.05 1.02		·95 ·99	·92 ·96	·89 ·93
26	1. 88	1.22	1.62	1.28	1.20	1.43	1.36	1.30	1.52	1.30	115	1.11	1.02	1.04	1.01	·98
27 28	1.97	1.82	1.74	1.02	1.24 1.22	1'49 1'55	1.42 1.48	1.30 1.43	1.30	1.31	1.51 1.52	1.10	1'12 1'17	1.13	1.02	1.05
20	2.14	2.01	1.00	1.29	1.20	1.65	1.22	1.48	1.42	1.30	1.31	1.30	1.55	1.18	1.14	1.11
30 Store	2.53	2'09	1.92	1.82	1.22	1.00	1.01	1.24	1'48	1.45	1.32	1.35	1.27	1.53	1.10	1.12
N. Decln.																
Altair	·37	·35	·33	.31 .70	·29 ·47	·28 ·45	·27 ·42	20' 41	'24 '39	·23	·23 ·36	°22 `35	·21 ·33	'20 '32	·20 ·31	.10 .31
Aldebar'n	1.13	1.00	1.00	.95	.90	·86	.82	.78	.75	.72	69	·67	•65	·62	·60	.59
Castor	2:42	2.27	2.14	3.03	1.10	1.04	1.00	95 1.67	1.60	1.24	1.94	1.43	79	1.34	1.20	1.22
Vega	3.10	2.91	2.74	2.29	2.46	2 .34	2.24	2.14	2.05	1.97	1.00	1.83	1.26	1.21	1.62	1.00
Capella	3.86	3.62 3.74	3.42	3.23 3.34	3.02 3.12	2.92 3.02	2.79 2.88	2.07 2.76	2.20 2.64	2.40	2°30 2°44	2.32	2.20	2.13	2 13	2.00 2.00
a Persei	4.23	4.25	4.01	3.79	3 [.] 60	3.43	3.27	3.13	3.00	2.88	2.77	2.67	2.28	2.20	2 [.] 42	2.35
η Ursæ Maj. «Ursæ Maj.	4.57	4.29	4.04	3.82	3.63	3.46	3.50	3.12	3.02	2.00 3.21	2.80	2.70 3.44	2.00	2.22 3.21	2°44 3°11	2.30 3.02
a Ursæ Maj.	7.34	6.89	6.20	6.12	5.83	5.22	5.30	5.02	4.86	4.67	4.20	4'33	4.18	4.02	3.92	3.80
S. Decln. Rigel	6			• 4 17	• A E	. 43		•20	.24	.26	.25	.33	.20	.51	'30	.20
Sirius	1.12	1.08	1.02	•96	45 192	·87	.83	.80	.76	.73	.21	.68	·66	•63	.61	.60
ϵ Sagittarii λ Scorpii	2.65 2.02	2°49 2°74	2°34 2°58	2.22	3.35 3.11	2.00 5.51	1.01 5.11	1.83	1.42 1.63	1.82 1.68	1.02	1.20	1.21 1.60	1.40	1.41 1.20	1.37
γ Argûs	4.12	3.90	3.68	3.48	3.30	3.14	3.00	2.87	2.75	2 ·64	2.24	2.45	2'37	2.30	2.55	1.12
α Gruis Canonus	4.20	3.94	3.72	3.52	3.34	3.18	3.03	2.90	2.78 3.35	2.67	2°57 3°10	2°48 2°00	2.40 2.80	2.32 2.70	2 `24 2`70	2.12 2.62
γ Crucis	5.86	5.20	5.19	4.01	4.66	4.44	4.23	4.02	3.88	3.73	3.29	3.46	3'34	3.23	3.13	3.03
a Favonis Achernar	5.96 2.11	5°59 5°74	5°27 5°41	4°99 5°12	4 [.] 73 4 [.] 86	4°51 4°62	4'30 4'41	4'11 4'22	3°94 4°05	3.79 3.89	3.05 3.74	3.22 3.61	3.40 3.48	3.37	3.50	3.10
β Crucis	6.48	6.00	5.71	5.42	5.15	4.01	₄ ∙68	4.48	4.20	4.13	3.02	3.83	3.70	3.57	3.46	3:36
ε Argûs ∫ β Centauri	6.68	6.27	5.01	5.20	5.31	5'05	4.82	4.61	4°42	4.25	4.00	3.94	3.81	3.68	3*56	3.46
a ² Centauri	6.82	6.40	6.04	5.71	5.42	5.16	4.92	4.71	4.52	4.34	4.18	4.03	3.89	3.76	3.04 3.08	3.53
a Tri. Aus.	7 45 9 99	9.38	8.85	8.37	5 93 7 95	7.56	5 30 7.22	6.01 2 1 2	4 93	6.36	4 5/ 6·12	5.90	5.70	5.21	5.34	5.17
βArgûs	10.22 m	9.62	9.07	8·59	8.12 m	7'75	7'40 m	7'08	6.79 m.	0.52	0.28 m.	0'05 m.	5'84 m.	5.65 m.	5'47 m.	<u>5'31</u> m.
	00	56	52	48	44	40	36	32	28	24	20	16	12	8	.4	00
	11 Hr.							10	HOUI	RS.						

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Table A.

c m

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		0				-,	2 H	OUR						1910	iname	3 Hr
Lat.	m. 00	m. 4	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 00
° 0 1 2 3 4 5	, 00 03 06 09 12 15	, .00 .03 .06 .09 .12 .15	, .00 .03 .06 .08 .11 .14	.00 .03 .05 .08 .11	, .00 .03 .05 .08 .10 .13	, .00 .02 .05 .07 .10 .12	, .02 .05 .07 .10 .12	, 00 02 05 07 09 12	, .02 .04 .07 .09 .11	,00 .02 .04 .06 .09 .11	.00 .02 .04 .06 .08 .10	.00 .02 .04 .06 .08 .10	·00 ·02 ·04 ·06 ·08 ·10	.00 .02 .04 .06 .07	.00 .02 .04 .05 .07	.00 .02 .03 .05 .07
6 7 8 9 10	·18 ·21 ·24 ·27 ·31	·17 ·20 ·23 ·26 ·29	·17 ·20 ·22 ·25 ·28	·16 ·19 ·22 ·24 ·27	·16 ·18 ·21 ·23 ·26	15 18 20 23 23	14 17 19 22	·14 ·16 ·19 ·21 ·23	·13 ·16 ·18 ·20 ·23	•13 •15 •17 •20 •22	·13 ·15 ·17 ·19 ·21	'12 '14 '16 '18 '20	·12 ·14 ·16 ·18 ·20	·11 ·13 ·15 ·17 ·19	·11 ·13 ·15 ·16 ·18	·11 ·12 ·14 ·16 ·18
11 12 13 14 15	*34 *37 *40 *43 *46	·32 ·35 ·38 ·41 ·45	·31 ·34 ·37 ·40 ·43	·30 ·33 ·36 ·38 ·41	·29 ·32 ·34 ·37 ·40	·28 ·30 ·33 ·36 ·38	·27 ·29 ·32 ·34 ·37	·26 ·28 ·31 ·33 ·36	·25 ·27 ·30 ·32 ·34	·24 ·26 ·29 ·31 ·33	·23 ·25 ·28 ·30 ·32	·22 ·24 ·27 ·29 ·31	•22 •24 •26 •28 •30	·21 ·23 ·25 ·27 ·29	·20 ·22 ·24 ·26 ·28	·19 ·21 ·23 ·25 ·27
16 17 18 19 20	·50 ·53 ·56 ·60 ·63	•48 •51 •54 •57 •61	·40 ·49 ·52 ·55 ·58	·44 ·47 ·50 ·53 ·56	.43 .45 .48 .51 .54	·41 ·44 ·46 ·49 ·52	·39 ·42 ·45 ·47 ·50	·38 ·41 ·43 ·46 ·48	·37 ·39 ·42 ·44 ·47	·35 ·38 ·40 ·43 ·45	·34 ·36 ·39 ·41 ·43	·33 ·35 ·37 ·40 ·42	·32 ·34 ·36 ·38 ·40	•31 •33 •35 •37 •39	·30 ·32 ·34 ·36 ·38	•29 •31 •32 •34 •36
21 22 23 24 25	·70 ·74 ·77 ·81	·67 ·71 ·74 ·78	·65 ·68 ·71 ·75	·62 ·65 ·69 ·72	57 •60 •63 •66 •69	·55 ·58 ·61 ·64 ·67	53 56 58 61 64	54 •56 •59 •62	49 •52 •54 •57 •60	·47 ·50 ·52 ·55 ·58	·40 ·48 ·51 ·53 ·56	·44 ·46 ·49 ·51 ·54	43 45 47 49 52	·41 ·43 ·46 ·48 ·50	·40 ·42 ·44 ·46 ·48	·38 ·40 ·42 ·45 ·47
20 27 28 29 30	·88 ·92 ·96 1·00	·81 ·85 ·88 ·92 ·96	·82 ·85 ·89 ·92	·75 ·78 ·82 ·85 ·89	·76 ·79 ·82 ·86	70 73 76 79 82	·70 ·73 ·76 ·79	·68 ·71 ·74 ·77	·65 ·68 ·71 ·74	•63 •66 •68 •71	·61 ·63 ·66 ·69	•50 •59 •61 •64 •66	54 57 59 62 64	·52 ·55 ·57 ·59 ·62	·53 ·55 ·57 ·60	·49 ·51 ·53 ·55 ·58
31 32 33 34 35	1.04 1.08 1.12 1.17 1.21	1.00 1.04 1.08 1.12 1.17	·96 1·00 1·04 1·08 1·12	.93 .96 1.00 1.04 1.08	-89 -93 -96 1-00 1-04	.80 .89 .93 .96 1.00	·83 ·86 ·89 ·93 ·96	80 •83 •86 •90 •93	77 •80 •83 •86 •90	·74 ·77 ·80 83 86	72 74 77 80 83	-69 -72 -75 -78 -81	·67 ·69 ·72 ·75 ·78	·64 ·67 ·70 ·72 ·75	62 65 67 70 73	•60 •62 •65 •67 •70
36 37 38 39 40	1.20 1.31 1.35 1.40 1.45	1.21 1.25 1.30 1.35 1.40	1 16 1 21 1 25 1 30 1 34	1.12 1.16 1.20 1.25 1.29	1.08 1.12 1.16 1.20 1.24	1.04 1.08 1.12 1.16 1.20	1.00 1.04 1.08 1.11 1.15	·96 1·00 1·04 1·07 1·11	.93 .96 1.00 1.04 1.07	·90 ·93 ·96 1·00 1·04	.87 .90 .93 .97 1.00	•84 •87 •90 •93 •97	·81 ·84 ·87 ·90 ·93	·78 ·81 ·84 ·87 ·90	·75 ·78 ·81 ·84 ·87	•73 •75 •78 •81 •84
41 42 43 44 45	1.21 1.26 1.62 1.67 1.73	1.45 1.50 1.55 1.61 1.66	1.39 1.44 1.49 1.55 1.60	1.34 1.39 1.44 1.49 1.54	1.38 1.38 1.43 1.48	1.24 1.29 1.33 1.38 1.43	1.20 1.24 1.28 1.33 1.38	1.15 1.19 1.24 1.28 1.33	1.11 1.15 1.19 1.24 1.28	1.07 1.11 1.12 1.13 1.19 1.23	1.04 1.07 1.11 1.15 1.19	1.00 1.04 1.07 1.11 1.15	.97 1.00 1.04 1.07 1.11	·93 ·97 1·00 1·04 1·07	·90 ·93 ·97 1·00 1·04	·87 ·90 ·93 ·97 1·00
40 47 48 49 50	1.79 1.86 1.92 1.99 2.06	1.72 1.78 1.85 1.91 1.98	1.00 1.72 1.78 1.84 1.91	1.29 1.65 1.71 1.77 1.84	1.24 1.29 1.65 1.71 1.77	1.48 1.53 1.59 1.64 1.70	1.43 1.48 1.53 1.58 1.64	1.37 1.42 1.47 1.53 1.58	1.33 1.37 1.42 1.47 1.53	1.32 1.32 1.37 1.42 1.47	1.23 1.28 1.32 1.37 1.42	1.19 1.23 1.28 1.32 1.37	1.15 1.19 1.23 1.28 1.32	1.11 1.12 1.13 1.23 1.28	1.07 1.11 1.15 1.19 1.23	1.04 1.07 1.11 1.15 1.19
51 52 53 54 55	2.14 2.22 2.30 2.38 2.47	2.00 2.13 2.21 2.29 2.38	1.98 2.05 2.12 2.20 2.29	1.90 1.97 2.04 2.12 2.20	1.90 1.97 2.04 2.12	1.90 1.83 1.90 1.97 2.04	1.70 1.76 1.83 1.89 1.97	1.04 1.70 1.76 1.83 1.90	1.28 1.64 1.70 1.76 1.83	1.52 1.58 1.64 1.70 1.76	1.47 1.53 1.58 1.64 1.70	1.42 1.47 1.53 1.58 1.64	1°37 1°42 1°47 1°53 1°59	1·32 1·37 1·42 1·48 1·53	1·28 1·33 1·37 1·43 1·48	1.23 1.28 1.33 1.38 1.43
50 57 58 59 60	2.57 2.67 2.77 2.88 3.00	2.47 2.56 2.66 2.77 2.88	2.37 2.46 2.56 2.66 2.77	2·28 2·37 2·46 2·56 2·67	2·20 2·28 2·37 2·47 2·57	2°12 2°20 2°29 2°38 2° 47	2.04 2.12 2.20 2.29 2.38	1.97 2.04 2.12 2.21 2.30	1.90 1.97 2.05 2.13 2.22	1.90 1.98 2.06 2.14	1.91 1.91 1.98 2.06	1.71 1.77 1.84 1.91 1.99	1.05 1.71 1.78 1.85 1.92	1 59 1.65 1.72 1.78 1.86	1.59 1.66 1.72 1.79	1.48 1.54 1.60 1.66 1.73
	00 10 Hr.	56	52	48	44	40	36	32	28 HOU	24 RS.	20	16	12	8	4	00

When hour angle is more than 6 hours, name the factors taken from Table A the same as the name of the latitude.

17 Table B.

Always name the factors taken from Table B the same as the name of declination.

1							2	HOUH	s.							3 Hr.
Declination.	m.	m.	m.	m.	m.	m.	m.	m.	111.	т.	m.	m.	m.	m .	m.	т.
	00	4	8	12	16	20	24	28	32	36	40	44	48	52	56	00
• • 1 3 4 5	, .00 .03 .07 .10 .14 .17	.00 .03 .07 .10 .14 .17	,00 .03 .07 .10 .13 .17	.00 .03 .06 .10 .13 .16	, .03 .06 .09 .13 .16	, •00 •03 •06 •09 •12 •15	, .03 .06 .09 .12 .15	,.00 .03 .06 .09 .12 .15	.00 .03 .06 .09 .11 .14	, .00 .03 .06 .08 .11 .14	, .00 .03 .05 .08 .11 .14	.00 .03 .05 .08 .11 .13	·00 ·03 ·05 ·08 ·10 ·13	.00 .03 .05 .08 .10	·00 ·03 ·05 ·08 ·10 ·13	, .00 .02 .05 .07 .10 .12
6	·21	•20	•20	•19	•19	·18	•18	•17	•17	•17	·16	•16	•16	·15	•15	·15
7	·25	•24	•23	•23	•22	·21	•21	•20	•20	•20	·19	•19	•18	·18	•18	·17
8	·28	•27	•27	•26	•25	·25	•24	•23	•23	•22	·22	•21	•21	·21	•20	·20
9	·32	•31	•30	•29	•28	·28	•27	•26	•26	•25	·25	•24	•24	·23	•23	·22
10	·35	•34	•33	•32	•32	·31	•30	•29	•29	•28	·27	•27	•26	·26	•25	·25
11	•39	•38	•37	•36	•35	*34	•33	•32	·32	•31	·30	·30	•29	•29	•28	•27
12	•43	•41	•40	•39	•38	*37	•36	•35	·35	•34	·33	·32	•32	•31	•31	•30
13	•46	•45	•44	•42	•41	*40	•39	•38	·37	•37	·36	·35	•35	•34	•33	•33
14	•50	•48	•47	•46	•45	*43	•42	•41	·40	•40	·39	·38	•37	•37	•36	•35
15	•54	•52	•51	•49	•48	*47	•46	•45	·44	•43	·42	·41	•40	•39	•39	•38
16	•57	•56	•54	·53	•51	•50	•49	•48	·47	·46	•45	*44	*43	•42	•41	•41
17	•61	•59	•58	·56	•55	•53	•52	•51	·50	·49	•48	*47	*46	•45	•44	•43
18	•65	•63	•61	·60	•58	•57	•55	•54	·53	·52	•51	*50	*49	•48	•47	•46
19	•69	•67	•65	·63	•62	•60	•59	•57	·56	·55	•54	*52	*51	•50	•50	•49
20	•73	•71	•69	·67	•65	•63	•62	•60	·59	·58	•57	*55	*54	•53	•52	•51
21 22 23 23° 28' 24 25	•77 •81 •85 •87 •89 •93	•75 •78 •82 •84 •86 •91	·72 ·76 ·80 ·82 ·84 ·88	•70 •74 •78 •80 •82 •86	•69 •72 •76 •78 •80 •83	·67 ·70 ·74 ·76 ·78 ·81	·65 ·69 ·72 ·74 ·76 ·79	·64 ·67 ·71 ·72 ·74 ·74	•62 •66 •69 •71 •72 •76	•61 •64 •67 •69 •71 •74	•60 •63 •66 •68 •69	•59 •62 •65 •66 •68 •71	•57 •60 •63 •65 •67 •67	•56 •59 •62 •64 •65 •68	•55 •58 •61 •62 •64 •67	·54 ·57 ·60 ·61 ·63 ·66
26	·98	.95	·92	•90	·87	·85	•83	•81	•79	•78	•76	•74	•73	•72	•70	•69
27	1·02	.99	·96	•94	·91	·89	•87	•85	•83	•81	•79	•78	•76	•75	•73	•72
28	1·06	1.03	1·00	•98	·95	·93	•90	•88	•86	•84	•83	•81	•79	•78	•77	•75
29	1·11	1.08	1·05	1•02	·99	·97	•94	•92	•90	•88	•86	•84	•83	•81	•80	•78
30	1·15	1.12	1·09	1•06	1·03	1·01	•98	•96	•94	•92	•90	•88	•86	•85	•83	•82
Stars. N. Decln. Procyon Altair Aldebar'n Arcturus	•19 •31 •59 •71	•19 •30 •57 •69	•18 •29 •55 •67	•18 •28 •54 •66	•17 •27 •52 •64	·17 ·26 ·51 ·62	•16 •26 •50 •61	•16 •25 •49 •59	•16 •25 •48 •58	•15 •24 •47 •57	•15 •24 •46 •56	•15 •23 •45 •54	•14 •23 •44 •53	•14 •22 •43 •52	•14 •22 •42 •51	•14 •21 •41 •51
Castor	1·25	1·22	1·18	1·15	1·12	1.09	1.07	1.04	1.02	1.00	·98	•96	•94	.92	•90	·89
Vega	1·60	1·56	1·51	1·47	1·43	1.40	1.36	1.33	1.30	1.27	1·25	1•22	1•20	1.17	1•15	1·13
Deneb	2·00	1·94	1·88	1·83	1·79	1.74	1.70	1.66	1.62	1.29	1·55	1•52	1•49	1.46	1•44	1·41
Capella	2·06	2·00	1·95	1·90	1·85	1.80	1.76	1.72	1.68	1.64	1·61	1•57	1•54	1.51	1•49	1·46
a Persei	2·35	2·28	2·21	2·15	2°10	2.04	1.99	1.95	1.90	1.86	1.82	1.20	1.75	1.72	1.69	1.66
η Ursæ Maj.	2·36	2·29	2·23	2·17	2°11	2.06	2.01	1.96	1.92	1.88	1.84	1.80	1.77	1.73	1.70	1.67
ϵ Ursæ Maj.	3·02	2·93	2·85	2·77	2°70	2.63	2.57	2.51	2.45	2.40	2.35	2.30	2.25	2.21	2.17	2.13
α Ursæ Maj.	3·80	3·69	3·58	3·49	3°40	3.31	3.23	3.16	3.09	3.02	2.96	2.90	2.84	2.79	2.73	2.69
S. Decln. Rigel Sirius ε Sagittarii λ Scorpii γ Argûs	·29 ·60 1·37 1·51 2·15	•28 •58 1•33 1•47 2•09	•28 •56 1•29 1•42 2•03	•27 •55 1•26 1•39 1•97	·26 ·53 1·23 1·35 1·92	·25 ·52 I·19 I·32 I·87	·25 ·51 1·17 1·28 1·83	·24 ·50 1·14 1·25 1·79	•24 •48 ••11 ••23 ••75	•23 •47 1•09 1•20 1•71	•23 •46 1•07 1•17 1•67	•22 •45 1•04 1•15 1•64	·22 ·45 1·02 1·13 1·61	•21 •44 1•00 1•11 1•58	•21 •43 •99 1•09 1•55	·21 ·42 ·97 1·07 1·52
α Gruis	2·17	2·11	2·05	2.00	1.94	1·90	1•85	1.81	1.77	1.73	1.69	1.66	1.63	1.59	1 57	1·54
Canopus	2·62	2·54	2·47	2.41	2.34	2·28	2•23	2.18	2.13	2.08	2.04	2.00	1.96	1.92	1·89	1·85
γ Crucis	3·03	2·95	2·86	2.79	2.71	2·64	2•58	2.52	2.46	2.41	2.36	2.31	2.27	2.22	2·18	2·15
α Pavonis	3·08	2·99	2·91	2.83	2.76	2·69	2•62	2.56	2.50	2.45	2.40	2.35	2.30	2.26	2·22	2·18
Achernar	3·16	3·07	2·98	2.90	2.83	2·76	2•69	2.63	2.57	2.51	2.46	2.41	2.36	2.32	2·28	2·24
$ \begin{array}{c} \beta \ \mathrm{Crucis} \\ \epsilon \ \mathrm{Argûs} \\ \beta \ \mathrm{Centauri} \\ a^2 \ \mathrm{Centauri} \\ a^1 \ \mathrm{Crucis} \\ a \ \mathrm{Tri. Aus.} \\ \beta \ \mathrm{Argûs} \\ \end{array} $	3·36	3·26	3.17	3.08	3.00	2.93	2.85	2.79	2.73	2.67	2.61	2·56	2·51	2·46	2·42	2·37
	3·46	3·35	3.26	3.17	3.09	3.01	2.94	2.87	2.81	2.74	2.69	2·63	2·58	2·53	2·49	2·44
	3·53	3·43	3.33	3.24	3.16	3.08	3.00	2.93	2.87	2.80	2.75	2·69	2·64	2·59	2·54	2·50
	3·86	3·75	3.64	3.54	3.45	3.36	3.28	3.21	3.13	3.07	3.00	2·94	2·88	2·83	2·78	2·73
	5·17	5·02	4.88	4.75	4.63	4.51	4.40	4.30	4.20	4.11	4.02	3·94	3·87	3·79	3·72	3·66
	5·31	5·15	5.01	4.87	4.74	4.63	4.51	4.41	4.31	4.22	4.13	4·04	3·96	3·89	3·82	3·75
	m. 00 10 Hr.	m. 56	m. 52	m. 48	m. 44	m. 40	т. 3б	m. 32	m. 28 HOU	m. 24 JRS.	m. 20	m. 16	m. 12	m. 8	m. 4	m. 00

2 - Azimuth.

18 Table A

	T (1)10 TT	
When hour angle is less than 6 hours.	, name the factors taken from	Table A contrary to name of lat.

							3	HOU	RS.							4 Hr.
Lat.	m. 00	m. 4	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 00
• •	:00	:00	:00	.00	.00	100	:00	00	:00	.00	00	:00	:00	:00	.00	.00
1 2	•02 •03	.02 .03	.02 .03	.02 .03	.02 .03	.01 .03	.01 .03	.03 .03	.01 03	.01 .03	·01 ·02	.01 .02	.01 .02	.01 .02	'01 'C2	.01 .02
3	•05 •07	·05 ·07	.05 .07	.05 .06	.02 .06	•04 •06	•04 •06	°04 °05	•04 •05	.04 .05	.04 .05	.04 .05	.03 .05	.03 .04	.03 .04	.03 .04
5	.09	·08	·08	·08	·08	.02	07	.02	•07	.oę	•06	.06	•06	·05	.02	.02
16 7	.11 .15	·10 ·12	.11 .10	.11 .00	.11 .00	.10 .03	.00 .00	.10	·08 ·09	•08 •09	•07 •09	.07 .08	.07 .08	.07 .08	•06 •07	.00 .02
8	.14 .16	·14 ·15	.13 .12	۲1. 13	·12 ·14	12	.13	.11 .12	·11	·10 ·12	.11	.00	.10 .09	.10 . 0 3	.08 .09	.08 .00
10	.18	.12	•16	.19	15	.12	•14	•14	.13	.13	.15	.15	.11	.11	.11	.10
11 12	·19 ·21	·19 ·21	.19	.18	·17 ·18	.18	.10	.12	·15 ·16	·14 •15	.14	.13 .14	.13 .14	.13 .13	·12 ·13	.11 .12
13 14	·23 ·25	·22 ·24	·22 ·23	21 22	•20 •22	·19 ·21	'19 '20	.18	.12	.17 .18	·16 ·17	•16 •17	°15 °16	•14 •16	·14 ·15	.13 .14
15	·27	·26	•25	·24	·23	·22	.22	·21	·20	.19	·19	.18	·17	.12	.16	.12
10	·31	•30	•29	-28	·27	•26	43 25	•24	•23	*22	20	·21	·20	.19	·18	.18
18 19	·32 ·34	.31	.30 .32	.29 .31	·28 ·30	·27 ·29	·20 ·28	·25 ·27	·24 ·26	·24 ·25	·23 ·24	·22 ·23	·21 ·22	·20 ·22	·20 ·21	·19 ·20
20 21	·30 ·38	·35	·34	·33	·32	.31 .35	·29	·28	·27 ·20	·26	·25	·25 ·26	·24 ·25	·23	·22 ·23	·21
22	·40	:39	•38	·36	·35	·34	·33	·32	.30	·29	·28	27	·26	25	·24	.23
23 24	·42	·41	·42	·40	·39	·37	- 34 - 36	33 35	·34	·31	.31	•30	.29	.28	·27	·26
25 26	·47	45 47	·43 ·45	·42 •44	·41 ·42	·39 •41	·30	·30	35	·34 ·35	·33	.33	• 30	•29	·20	·27 ·28
27	·51	·49	·48	·46	·44 •46	·43	·41	·40	·38	·37	·36	·34	·33	·32	·31	·29
20 29	·55	·54	.52	•50	·48	47	45	43	·42	·40	·39	·37	·36	·35	'33 '25	.32
30	·60	·58	-56 -56	54°	.52	•50	47 -49	45 -47	44 '45	44	.40 .42	-39 -41	.39	-30 -38	.30 .36	- 35 - 35
32	•62 •65	·60 ·63	·58 ·61	•56 •58	·54 ·56	•52 •54	·51	'49 '51	·47	·45	·44 ·45	·42	'41 '42	'39 '41	·38	·36
34 34	·67	·65	·63	·61	'59 '61	:57	55	·53	·51	·49	·47	·45	·44	·42	·41	·39
35 36	.73	•70	·68	•65	63	.61	·59	·57	·55	.53	.51	47 '49	43 -47	· 44	.44	.42
37	·75 ·78	73	·70 ·73	•68 •70	66 •68	·63 ·66	·61	·59 ·61	·57	·55	·53	·51 ·53	49	'47 '49	.45 .47	·44 ·45
39	·81	·78	·75	·73	·70	·68	•66 •68	·63	·61 ·62	·59	·57	·55	·53	.51	·49	·47
40	.87	·84	·81	·78	.76	.73	.70	·68	•65	·63	.61	•59	•56	.54	.52	.20
42	•90 •93	·87 ·90	·84 ·87	·81 ·84	·78 ·81	·76 ·78	·73 ·76	·70 ·73	·68 ·70	·65 ·68	•63 •65	•61 •63	·58 ·61	•56 •58	•54 •56	·52 ·54
44	.97 1.00	.93 .97	•90 •03	·87 00	·84 ·87	•81 •84	.78 .81	75	.73 .75	.70 .73	·68 ·70	·65 ·67	.63 .65	·60 ·62	·58 ·60	·56 ·58
45 46	1.04	1.00	•97	.93	.90	.87	•84	·81	·78	.75	.73	•70	·67	· 6 5	·62	.60
47	1.02	1.04 1.07	1 00 1 04		.93 .97	.90 .93	·87 90	·84 ·87	·81 ·84		·75 ·78	·72 ·75	·70 ·72	•67 •69	·64 ·67	·62 ·64
49	1.10	1.12	1.02	1.04	1.00		·93	'90' '03	·87	·84 ·87	•80 •83	·78 •80	·75	.72 .74	·69 ·72	•66 •69
51	1.53	1.10	1.12	1.11	1 07	1.04	1.00	•96	.93	.90	·86	•83	.80	.77	.74	.71
52 53	1.33	1.24 1.28	1.19 1.24	1.12	1.12	1.02	1 04 1 07	1.00 1.04	1.00 1.00	.93 .96	•90 •93	•86 •90	•83 •86	·80 ·83	·77 ·80	74
54	1.38 1.43	1.38 1.33	1.33 1.33	1.24 1.29	1.20 1.24	1.12 1 20	1.10	1.08	1 04 1 08	1.00 1.04	96 [.]	.93 .96	·89 ·93	·86 ·89	·83 ·86	.79 .82
56	1.48	1.43	1.38	1.33	1 29	1.54	1.50	1.10	1.12	1.08	1.04	1.00	·96	.93	.89	·86
57 58	1.60	1.49	1.44	1°39 1°44	1.34	1.34	1.30	1.20	1.10	1.15	1.15	1.04	1.04	1.00	.96	·92
59 60	1.00 1.23	1 61	1.22 1.62	1.20 1.20	1.45 1.51	1.40 1.45	1.32 1.40	1.30	1.31	1.51	1.12 1.51	1.15	1.08	1.04	1.00	1.00
	m. 00	т. 5б	m. 52	m. 48	m. 44	m. 40	m. 36	m. 32	m. 28	m. 24	m. 20	m. 16	m. 12	m. 8	m. 4	m. 00
1	9 Hr.								8 HOT	TRS						

When hour angle is more than 6 hours, name the factors taken from Table A the same as the name of the latitude.

19

 Table B.

 Always name the factors taken from Table B the same as the name of declination.

	3 HOURS.												4 Hr.			
Declination.	т. 00	m. 4	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	111. 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 00
° ° 2 3 4 5	*00 •02 •05 •07 •10 •12	, •00 •02 •05 •07 •10 •12	*00 *02 *05 *07 *10 *12	*00 *02 *05 *07 *09 *12	.00 .02 .05 .07 .09 .12	, .00 .02 .05 .07 .09 .11	, .02 .04 .07 .09 .11	, •02 •04 •07 •09 •11	•00 •02 •04 •07 •09 •11	.00 .02 .04 .06 .09 .11	, •02 •04 •06 •09 •11	•00 •02 •04 •06 •08	*00 *02 *04 *06 *08 *08	,00 .02 .04 .06 .08 .10	•00 •02 •04 •06 •08	, •02 •04 •06 •08 •10
6 7 8 9 10	*15 *17 *20 *22 *25	•15 •17 •20 •22 •25	•14 •17 •19 •22 •24	•14 •17 •19 •21 •24	•14 •16 •19 •21 •23	•14 •16 •79 •21 •23	•14 •16 •18 •20 •23	•13 •16 •18 •20 •22	•13 •15 •18 •20	•13 •15 •17 •20 •22	•13 •15 •17 •19 •22	•13 •15 •17 •19 •21	•13 •15 •17 •19 •21	•12 •14 •17 •19 •21	·12 ·14 ·16 ·18 ·21	·12 ·14 ·16 ·18 ·20
11 12 13 14 15	·27 ·30 ·33 ·35 ·38	•27 •30 •32 •35 •37	•27 •29 •32 •34 •37	•26 •29 •31 •34 •36	•26 •28 •31 •33 •36	•25 •28 •30 •33 •35	•25 •27 •30 •32 •34	•25 •27 •29 •32 •34	•24 •27 •29 •31 •34	·24 ·26 ·29 ·31 ·33	·24 ·26 ·28 ·30 ·33	•23 •26 •28 •30 •32	•23 •25 •28 •30 •32	•23 •25 •27 •29 •32	·23 ·25 ·27 ·29 ·31	·22 ·25 ·27 ·29 ·31
16 17 18 19 20	•41 •43 •46 •49 •51	•40 •43 •45 •48 •51	•39 •42 •44 •47 •50	•39 •41 •44 •46 •49	·38 ·41 ·43 ·46 ·48	·37 ·40 ·42 ·45 ·48	·37 ·39 ·42 ·44 ·47	•36 •39 •41 •44 •46	•36 •38 •41 •43 •46	•35 •38 •40 •43 •45	*35 *37 *40 *42 *44	•35 •37 •39 •42 •44	•34 •36 •39 •41 •43	•34 •36 •38 •41 •43	·33 ·36 ·38 ·40 ·42	•33 •35 •38 ••40 •42
21 22 23 23° 28' 24	·54 ·57 ·60 ·61 ·63	•53 •56 •59 •60 •62	•52 •55 •58 •59 •61	•52 •54 •57 •58 •60	·51 ·54 ·56 ·58 ·59	•50 •53 •55 •57 •58	•49 •52 •55 •56 •57	•49 •51 •54 •55 •57	•48 •51 •53 •54 •56	*47 *50 *52 *54 *55	•47 •49 •52 •53 •54	•46 •49 •51 •52 •54	•46 •48 •51 •52 •53	*45 *48 *50 *51 *53	·45 ·47 ·50 ·51 ·52	*44 *47 *49 *50 *51
25 26 27 28 29 30	·66 ·69 ·72 ·75 ·78 ·82	•65 •68 •71 •74 •77 •80	•64 •67 •70 •73 •76 •70	•63 •66 •69 •72 •75 •78	·62 ·65 ·68 ·70 ·73 ·76	•61 •64 •67 •69 •72 •75	·60 ·63 ·66 ·68 ·71 ·74	·59 ·62 ·65 ·67 ·70	•58 •61 •64 •67 •69	•58 •60 •63 •66 •69	•57 •60 •62 •65 •68	•56 •59 •61 •64 •67	•56 •58 •61 •63 •66	*55 *58 *60 *63 *65	·54 ·57 ·59 ·62 ·65 ·67	•54 •56 •59 •61 •64 •67
Stars. N. Decln. Procyon Altair Aldebar'n Arcturus	·14 ·21 ·41 ·51	•13 •21 •41 •50	•13 •21 •40 •49	•13 •20 •39 •48	·13 ·20 ·39 ·47	•12 •20 •38 •47	·12 ·20 ·38 ·46	•12 •19 •37 •45	•12 •19 •37 •45	•12 •19 •36 •44	•12 •19 •36	·12 ·18 ·35 ·43	•11 •18 •35 •43	•11 •18 •35	•11 •18 •34 •42	·11 •18 •34 •41
Castor Vega Deneb Capella	•89 1•13 1•41 1•46	•87 1•11 1•39 1•43	•86 1•10 1•37 1•41	•84 1•08 1•34 1•39	•83 1•06 1•32 1•37	·82 1·05 1·30 1·35	·81 1·03 1·28 1·33	•80 1•02 1•27 1•31	°79 1.00 1.25 1.29	•77 •99 1•23 1•28	•77 •98 1•22 1•26	•76 •97 1•20 1•25	•75 •96 1•19 1•23	•74 •94 1•18 1•22	•73 •93 1•16 1•20	·72 ·93 1·15 1·19
a Persei η Ursæ Maj. ε Ursæ Maj. a Ursæ Maj.	1.66 1.67 2.13 2.69	1.63 1.64 2.10 2.64	1.60 1.62 2.06 2.60	1·58 1·59 2·03 2·56	1.55 1.57 2.00 2.52	1·53 1·54 1·97 2·48	1.51 1.52 1.94 2. 44	1·49 1·50 1·91 2·41	1.47 1.48 1.89 2.38	1·45 1·46 1·86 2·35	1.43 1.44 1.84 2.32	1.41 1.43 1.82 2.29	1°40 1°41 1°80 2°27	1·38 1·39 1·78 2·24	1·37 1·38 1·76 2·22	1·35 1·36 1·74 2·19
S. Decln. Rigel Sirius ϵ Sagittarii λ Scorpii γ Argûs	•21 •42 •97 1•07 1•52	·20 ·41 ·95 1·05 1·49	•20 •41 •94 1•03 1•47	•20 •40 •92 1•02 1•45	·19 ·39 ·91 1·00 1·42	·19 ·39 ·89 ·99 1·40	·19 ·38 ·88 ·97 1·38	•19 •38 •87 •96 1•36	•18 •37 •86 •94 1•35	•18 •37 •85 •93 1•33	•18 •36 •84 •92 1•31	•18 •36 •83 •91 •91	•17 •36 •82 •90 1•28	•17 •35 •81 •89 1•27	·17 ·35 ·80 ·88 1·25	•17 •34 •79 •87 1•24
a Gruis Canopus γ Crucis a Pavonis Achernar	1.54 1.85 2.15 2.18 2.24	1.51 1.82 2.11 2.14 2.20	1°49 1°79 2°07 2°11 2°16	1.46 1.76 2.04 2.07 2.13	1·44 1·74 2·01 2·04 2·10	1.42 1.71 1.98 2.01 2.06	1.40 1.69 1.95 1.98 2.03	1.38 1.66 1.93 1.96 2.01	1·36 1·64 1·90 1·93 1·98	1·34 1·62 1·88 1·91 1·95	1.33 1.60 1.85 1.88 1.93	1·31 1·58 1·83 1·86 1·91	1.30 1.56 1.81 1.84 1.89	1·28 1·54 1·79 1·82 1·86	1·27 1·53 1·77 1·80 1·84	1·26 1·51 1·75 1·78 1·83
$\begin{array}{l} \beta \operatorname{Crucis} \\ \epsilon \operatorname{Argûs} \\ \beta \operatorname{Centauri} \\ a^{2}\operatorname{Centauri} \\ a^{1}\operatorname{Crucis} \\ a \operatorname{Tri. Aus.} \\ \beta \operatorname{Argûs} \\ \end{array}$	2·37 2·44 2·50 2·73 3·66 3·75 m.	2·33 2·40 2·45 2·68 3·60 3·69 m. 56	2·29 2·36 2·41 2·64 3·54 3·63 m. 52	2.26 2.32 2.37 2.60 3.48 3.57 m. 48	2·22 2·29 2·34 2·56 3·43 3·52 m. 44	2.19 2.26 2.30 2.52 3.38 3.46 m. 40	2.16 2.22 2.27 2.48 3.33 3.41 m. 36	2·13 2·19 2·24 2·45 3·28 3·37 m. 32	2·10 2·16 2·21 2·42 3·24 3·32 m. 28	2.07 2.14 2.18 2.38 3.20 3.28 m. 24	2.05 2.11 2.15 2.36 3.16 3.24 m. 20	2.02 2.08 2.13 2.33 3.12 3.20 m. 16	2.00 2.06 2.10 2.30 3.08 3.16 m. 12	1.98 2.04 2.08 2.27 3.05 3.13 m. 8	1.96 2.02 2.06 2.25 3.02 3.10 m. 4	1.94 2.00 2.04 2.23 2.99 3.06 m. 00
	9 Hr.			<u>ту</u> 1	77	45 1	55	8	HOU	RS.		1		/		•

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 Table A.

 When hour angle is less than 6 hours, name the factors taken from Table A contrary to name of lat.

	1	4 HOURS. 5 H													5 Hr.	
Lat	m. 00	m. 4	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 00
0 0 1 2 3 4	, 000 010 020 030 040	.000 .010 .019 .029 .039	·000 ·009 ·019 ·028 ·037	.000 .009 .018 .027 .036	.000 .009 .017 .026 .034	, 000 008 016 024 033	, 000 008 016 023 031	·000 ·007 ·015 ·022 ·030	'000 '007 '014 '021 '028	'000 '007 '013 '020 '027	, .000 .006 .013 .019 .025	·000 ·006 ·012 ·018 ·024	.000 .006 .011 .017 .023	, 000 005 011 016 021	·000 ·005 ·010 ·015 ·020	'000 '005 '009 '014 '019
5 6 7 8 9 10	·051 ·061 ·071 ·081 ·091 ·102	·048 ·058 ·068 ·078 ·088 ·098	*047 *056 *065 *075 *084 *094	·045 ·054 ·063 ·072 ·081 ·090	•043 •051 •060 •069 •077 •086	·041 ·049 ·057 ·066 ·074 ·082	·039 ·047 ·055 ·063 ·071 ·079	·037 ·045 ·052 ·060 ·067 ·075	·035 ·042 ·050 ·057 ·064 ·071	·034 ·040 ·047 ·054 ·061 ·068	·032 ·038 ·045 ·051 ·058 ·064	·030 ·036 ·042 ·048 ·055 ·061	·028 ·034 ·040 ·046 ·051 ·057	·027 ·032 ·038 ·043 ·048 ·054	·025 ·030 ·035 ·040 ·045 ·051	·023 ·028 ·033 ·038 ·042 ·047
11 12 13 14 15	·112 ·123 ·133 ·144 ·155	·108 ·118 ·128 ·138 ·149	·103 ·113 ·123 ·133 ·142	·099 ·108 ·118 ·127 ·137	.092 .104 .113 .122 .131	.091 .099 .108 .116 .125	·087 ·095 ·103 ·111 ·119	·083 ·090 ·098 ·106 ·114	·079 ·086 ·093 ·101 ·108	.075 .082 .089 .096 .103	·071 ·077 ·084 ·091 ·098	•067 •073 •079 •086 •092	•063 •069 •075 •081 •087	·059 ·065 ·071 ·076 ·082	•056 •061 •066 •071 •077	·052 ·057 ·062 ·067 ·072
16 17 18 19 20	·166 ·177 ·188 ·199 ·210	•159 •169 •180 •191 •202	·152 ·163 ·173 ·183 ·194	•146 •156 •166 •175 •185	•140 •149 •158 •168 •178	·134 ·143 ·152 ·161 ·170	·128 ·136 ·145 ·153 ·162	·122 ·130 ·138 ·146 ·154	•116 •124 •131 •139 •147	•110 •117 •125 •132 •140	·104 ·111 ·118 ·125 ·132	•099 •105 •112 •119 •125	•093 •099 •106 •112 •118	·088 ·093 ·099 ·105 ·111	·082 ·088 ·093 ·099 ·104	•077 •082 •087 •092 •098
21 22 23 24 25	·222 ·233 ·245 ·257 ·269	·213 ·224 ·235 ·247 ·258	·204 ·215 ·226 ·237 ·248	•196 •206 •216 •227 •238	·187 ·197 ·207 ·217 ·227	·179 ·188 ·198 ·208 ·217	•171 •180 •189 •198 •208	•163 •171 •180 •189 •198	•155 •163 •171 •180 •188	•147 •155 •163 •171 •179	•140 •147 •154 •162 •170	•132 •139 •146 •153 •161	·125 ·131 ·138 ·145 ·152	•117 •124 •130 •136 •143	•110 •116 •122 •128 •134	•103 •108 •114 •119 •125
26 27 28 29 30	·282 ·294 ·307 ·320 ·333	•270 •282 •295 •307 •320	•259 •271 •283 •295 •307	·249 ·260 ·271 ·282 ·294	•238 •249 •259 •270 •282	·227 ·238 ·248 ·258 ·269	·217 ·227 ·237 ·237 ·247 ·257	·207 ·216 ·226 ·235 ·245	·197 ·206 ·215 ·224 ·233	•187 •196 •204 •213 •222	•178 •185 •194 •202 •210	·168 ·175 ·183 ·191 ·199	•158 •166 •173 •180 •188	•149 •156 •163 •169 •177	*140 *146 *152 *159 *166	·131 ·137 ·142 ·149 ·155
31 32 33 34 35	·347 ·361 ·375 ·389 ·404	*333 *346 *360 *374 *388	·319 ·332 ·345 ·359 ·372	·306 ·318 ·331 ·344 ·357	·293 ·305 ·317 ·329 ·342	•280 •291 •303 •315 •327	·268 ·278 ·289 ·300 ·312	·255 ·265 ·276 ·286 ·297	*243 *252 *262 *273 *283	•231 •240 •249 •259 •269	·219 ·227 ·236 ·246 ·255	·207 ·215 ·224 ·232 ·241	·195 ·203 ·211 ·219 ·228	·184 ·191 ·199 ·206 ·214	·172 ·179 ·186 ·193 ·201	·101 ·167 ·174 ·181 ·188
30 37 38 39 40	·419 ·435 ·451 ·468 ·484	·403 ·418 ·433 ·449 ·465	·380 ·401 ·415 ·431 ·446	·370 ·384 ·398 ·413 ·428	·354 ·368 ·381 ·395 ·409	·339 ·351 ·364 ·378 ·391	•323 •336 •348 •361 •374	·308 ·320 ·332 ·344 ·356	·294 ·304 ·316 ·327 ·339	·279 ·289 ·300 ·311 ·322	·204 ·274 ·284 ·295 ·305	*259 *259 *269 *279 *289	*230 *245 *254 *263 *273	·222 ·230 ·239 ·248 ·257	•208 •216 •224 •232 •241	·202 ·209 ·217 ·225
41 42 43 44 45	·502 ·520 ·538 ·558 ·577	-482 -499 -517 -535 -554	·402 ·479 ·496 ·513 ·532	'443 '459 '475 '492 '510	*424 *439 *455 *471 *488	·405 ·420 ·435 ·450 ·466	·387 ·401 ·415 ·430 ·445	·309 ·382 ·396 ·410 ·424	·351 ·364 ·377 ·390 ·404	·334 ·346 ·358 ·371 ·384	·316 ·328 ·339 ·351 ·364	·299 ·310 ·321 ·333 ·344	·202 ·293 ·303 ·314 ·325	·200 ·275 ·285 ·295 ·306	•249 •258 •267 •277 •287	·233 ·241 ·250 ·259 ·268
40 47 48 49 50	·619 ·619 ·641 ·664 ·688	·574 ·594 ·616 ·638 ·661	·551 ·570 ·591 ·612 ·634	·528 ·546 ·566 ·586 ·607	·505 ·523 ·542 ·561 ·581	·483 ·500 ·518 ·536 ·556	·401 ·477 ·494 ·512 ·531	*440 *455 *471 *488 *506	·418 ·433 ·449 ·465 ·481	·398 ·412 ·426 ·442 ·457	·377 ·390 ·404 ·419 ·434	·357 ·369 ·382 ·396 ·410	•330 •348 •361 •374 •387	·317 ·328 ·340 ·352 ·364	·297 ·307 ·318 ·330 ·342	·287 ·298 ·308 ·319
51 52 53 54 55	713 739 766 795 825	·709 ·736 ·763 ·792	·681 ·706 ·732 ·759	•652 •676 •701 •728	•624 •647 •671 •697	·570 ·597 ·619 ·642 ·666	·550 ·570 ·591 ·613 ·636	524 543 563 584 606	499 517 536 556 556	474 491 509 528 548	449 •466 •483 •501 •520	425 •441 •457 •474 •492	401 416 431 447 464	378 391 406 421 437	354 •367 •381 •395 •410	331 343 356 369 383
50 57 58 59 60	·889 ·924 ·961 1·000	·854 ·887 ·923 ·960	·819 ·851 ·885 ·921	755 785 815 848 883	723 751 781 812 845	·718 ·746 ·776 ·808	·686 ·713 ·741 ·771	·654 ·679 ·706 ·735	599 •622 •647 •672 •700	·591 ·614 ·639 ·665	540 560 582 606 630	·530 ·551 ·573 ·596	402 •500 •520 •541 •563	453 •471 •489 •509 •530	425 442 459 477 497	397 •413 •429 •446 •464
	$\frac{00}{8 \text{ Hr.}}$	56	m. m. <th< td=""><td>0</td></th<>												0	

When hour angle is more than 6 hours, name the factors taken from Table A the same as the name of the latitude.

6
21 Table B.

							4 1	HOUR	s.							5 Hr.
Declination.	m. 00	m. 4	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 00
• 0 1 2 3 4 5	, .020 .040 .040 .061 .081 .101	, .020 .040 .060 .080 .100	, .020 .040 .059 .079 .099	, 020 039 059 078 098	.000 .019 .039 .058 .078 .078	, •019 •039 •058 •077 •097	, 019 038 057 077	, 019 038 057 076 095	, .019 .038 .057 .075 .094	, 019 037 056 075 094	, •019 •037 •056 •074 •093	•000 •018 •037 •055 •074 •093	•000 •018 •037 •055 •074 •092	, 000 018 037 055 073 091	, 000 018 036 055 073 091	, .000 .018 .036 .054 .054 .072 .091
6 7 8 9 10	•121 •142 •162 •183 •204	*120 *140 *161 *181 *202	·119 ·139 ·159 ·179 ·200	·118 ·138 ·158 ·178 ·178 ·198	•117 •137 •156 •176 •196	•116 •135 •155 •175 •175 •195	·115 ·134 ·154 ·173 ·193	·114 ·133 ·153 ·172 ·192	·113 ·132 ·152 ·171 ·190	•113 •132 •151 •170 •189	·112 ·131 ·150 ·169 ·188	·111 ·130 ·149 ·168 ·186	'111 '129 '148 '167 '185	•110 •128 •147 •166 •184	•109 •128 •146 •165 •183	·109 ·127 ·145 ·164 ·183
11 12 13 14 15	·224 ·245 ·267 ·288 ·309	·222 ·243 ·264 ·285 ·306 ·228	·220 ·241 ·261 ·282 ·303 ·325	·218 ·239 ·259 ·280 ·301	·210 ·236 ·257 ·277 ·298 ·310	•214 •235 •255 •275 •296	·213 ·233 ·253 ·273 ·273 ·293 ·314	·211 ·231 ·251 ·271 ·291	*210 *229 *249 *269 *289	·208 ·228 ·247 ·267 ·287 ·287	·207 ·226 ·246 ·265 ·285 ·305	·206 ·225 ·244 ·264 ·283	·204 ·223 ·243 ·262 ·282 ·302	·203 ·222 ·241 ·261 ·280 ·300	·202 ·221 ·240 ·259 ·279	·201 ·220 ·239 ·258 ·277 ·207
10 17 18 19 20 21	353 353 375 398 420	·350 ·371 ·394 ·416 ·439	·346 ·368 ·390 ·412	·343 ·365 ·386 ·408 ·431	·340 ·362 ·383 ·405 ·427	·337 ·359 ·380 ·402 ·424	·335 ·356 ·377 ·398 ·420	*332 *353 *374 *395 *417	·330 ·350 ·371 ·393 ·414	·327 ·348 ·369 ·390	·325 ·346 ·366 ·387 ·408	·323 ·344 ·364 ·385 ·406	·321 ·342 ·362 ·383 ·404	·320 ·340 ·360 ·381 ·401	·318 ·338 ·358 ·379 ·399	·317 ·336 ·356 ·355 ·377 ·397
22 23 23° 28' 24 25	·467 ·490 ·501 ·514 ·538	·462 ·485 ·496 ·509 ·533	*458 *481 *492 *504 *528	*453 *476 *487 *500 *523	*450 *472 *483 *495 *519	·446 ·468 ·479 ·479 ·491 ·515	·442 ·465 ·475 ·487 ·510	*439 *461 *472 *484 *507	•436 •458 •468 •480 •503	*433 *455 *465 *477 *499	•430 •452 •462 •474 •496	•427 •449 •459 •471 •493	•425 •446 •456 •468 •490	·422 ·444 ·454 ·466 ·488	·420 ·442 ·452 ·463 ·485	·418 ·439 ·449 ·461 ·483
26 27 28 29 30	*563 *588 *614 *640 *667	·558 ·583 ·608 ·634 ·660	·552 ·577 ·602 ·628 ·654	*547 *572 *597 *622 *648	*543 *567 *592 *617 *642	·538 ·562 ·587 ·612 ·637	*534 *558 *582 *607 *632	·530 ·554 ·578 ·602 ·627	·526 ·550 ·573 ·598 ·623	•522 •546 •570 •594 •618	·519 ·542 ·566 ·590 ·614	•516 •539 •562 •586 •611	·513 ·536 ·559 ·583 ·607	·510 ·533 ·556 ·580 ·604	·507 ·530 ·553 ·577 ·601	•505 •527 •550 •574 •598
Stars. N. Decln. Procyon Altair Aldebar'n Arcturus	·110 ·175 ·338 ·412	•109 •174 •335 •408	•108 •172 •332 •405	•107 •170 •329 •401	•106 •169 •326 •397	•105 •167 •323 •394	·105 ·166 ·321 ·391	•104 •165 •318 •388	•103 •164 •316 •385	•102 •163 •314 •383	·102 ·161 ·312 ·380	·101 •160 •310 •378	•100 •160 •308 •376	·100 ·159 ·306 ·373	·099 ·158 ·305 ·372	.099 .157 .303 .370
Castor Vega Deneb Capella	'724 '925 1'15 1'19	•717 •916 1•14 1•18	.907 1.13 1.17	•704 •899 1•12 1•16	·698 ·891 1·11 1·15	·692 ·884 1·10 1·14	·686 ·877 1·09 1·13	·681 ·870 1·08 1·12	·676 ·864 1·08 1·11	·672 ·858 1·07 1·11	·667 ·852 1·06 1·10	·663 ·847 1·06 1·09	·659 ·842 1·05 1·09	·656 ·838 1·04 1·08	·652 ·833 1·04 1·07	·649 ·829 1·03 1·07
a Persei η Ursæ Maj ε Ursæ Maj. α Ursæ Maj	1.35 1.36 1.74 2.19	1°34 1°35 1°72 2°17	1 33 1.34 1.71 2.15	1 32 1.93 1.69 2.13	1 30 1.31 1.68 2.11	1 29 1 30 1 66 2 10	1.29 1.65 2.08	1.27 1.28 1.64 2.06	1.20 1.27 1.63 2.05	1.20 1.27 1.62 2. 03	1.22 1.20 1.60 2.02	1 24 1·25 1·59 2·01	1·23 1·24 1·59 2·00	1 23 1·24 1·58 1·99	1.23 1.22 1.23 1.98	1.22 1.22 1.56 1.97
S. Decln. Rigel Sirius ε Sagittarii λ Scorpii γ Argûs	'169 '344 '791 '871 1'24	·167 ·341 ·784 ·863 1·23	•165 •337 •776 •855 1•22	•164 •334 •769 •847 1•21	•162 •332 •763 •840 1•20	•161 •329 •756 •833 1•19	•160 •326 •750 •826 1•18	•159 •324 •745 •820 1•17	•157 •321 •739 •814 1•16	•156 •319 •734 •808 1•15	•155 •317 •729 •803 1•14	·154 ·315 ·725 ·798 1·14	•153 •313 •721 •793 1•13	•153 •311 •717 •789 1•12	·152 ·310 ·713 ·785 1·12	'151 '308 '710 '781 1'11
α Gruis Canopus γ Crucis α Pavonis Achernar	1.26 1.21 1.75 1.78 1.83	1°24 1°50 1°73 1°76 1°81	1°23 1°48 1°72 1°75 1°79	1°22 1°47 1°70 1°73 1°77	1.21 1.46 1.69 1.71 1.76	1.20 1.45 1.67 1.70 1.74	1.19 1.43 1.66 1.69 1.73	1·18 1·42 1·65 1·67 1·72	1.17 1.41 1.64 1.66 1.71	1.16 1.40 1.63 1.65 1.69	1.16 1.39 1.61 1.64 1.68	1.15 1.39 1.60 1.63 1.67	1°14 1°38 1°60 1°62 1°66	1°14 1°37 1°59 1°61 1°65	1.13 1.36 1.58 1.60 1.65	1°13 1°36 1°57 1°60 1°64
$ \begin{array}{l} \beta \operatorname{Crucis} \\ \epsilon \operatorname{Argûs} \\ \beta \operatorname{Centauri} \\ \alpha^2 \operatorname{Centauri} \\ \alpha^1 \operatorname{Crucis} \\ \alpha \operatorname{Tri. Aus.} \\ \beta \operatorname{Argûs} \\ \end{array} $	1.94 2.00 2.04 2.23 2.99 3.06	1.92 1.98 2.02 2.21 2.96 3.03	1.90 1.96 2.00 2.18 2.93 3.00	1.88 1.94 1.98 2.17 2.90 2.98	1.87 1.92 1.96 2.15 2.88 2.95	1.85 1.91 1.95 2.13 2.85 2.93	1.84 1.89 1.93 2.11 2.83 2.90	1.82 1.88 1.92 2.10 2.81 2.88	1.81 1.86 1.90 2.08 2.79 2.86	1.80 1.85 1.89 2.07 2.77 2.84	1.79 1.84 1.88 2.05 2.75 2.82	1.77 1.83 1.87 2.04 2.74 2.81	1.76 1.82 1.86 2.03 2.72 2.79	1.75 1.81 1.85 2.02 2.70 2.77	1.75 1.80 1.84 2.01 2.69 2.76	1.74 1.79 1.83 2.00 2.68 2.75
	m. 00 8 Hr.	m. 56	m. 52	m. 48	m. 44	m. 40	т. 3б	m. 32 7	m. 28 HOUI	m. 24 R S.	m. 20	m. 16	m. 12	т. 8	ш. 4	00

Table F	١.
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Whe	n hour	angle	e is les	s than	6 ho	urs, na	ame tl	he fact	tors ta	ken fr	om Ta	able A	. contra	ry to	name	of lat.
-								5 HC	URS.							6 Hr.
La	m. 00	m. 4	m. 8	10. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 00
°	.000	.000	.000	.000	.000	.000	·000	.000	.000	.000	.000	.000	.000		.000	.000
I	.002	·004	.004	.004	.003	.003	.003	·002	.002	.002	.005	.001	.001	.001	°000	.000
2	.000	.000	.008	.002	.002	.000	·006	.002	.004	.004	.003	.002	'002	.001	.001	.000
3	.014	.013	'012	.0II	.010	.000	.008	. 007	•006	'006	.005	·004	.003	°00 [,] 2	100.	.000
4	1023	.022	·020	.010	.014	012	1101	'010	.000	*000	.000	1005	1004	*002	'002	.000
		1006	1024	:000	1000	1010	1017	1075				1007	1005	005	002	
7	020	.031	·024	·026	·020	.022	.010	1017	1013	.013	1009	1000	*000	·004	*002	1000
8	.038	·035	.032	.030	·027	.025	.022	·020	.012	.012	.012	.010	'007	.005	.003	.000
9	·042	·039	·037	.034	.031	·028	.022	.055	.019	.012	·014	.011	.008	'00Ő	.003	.000
to	'0 .17	·044	· 0 41	.032	·034	.031	.028	.022	'0 22	.010	.012	.015	.000	•006	.003	.000
II	·052	·048	•045	. 041	·038	·034	.031	·027	·024	·020	.012	.01 4	.010	.002	.003	.000
12	.057	.023	` 0 49	.042	•041	.032	.034	•030	.026	.022	.010	.012	.011	'007	•004	.000
13	067	·050	1053	1053	·045	·041	1037	·032	·028	·024	·020	010	.012	1000	·004	.000
15	.072	.067	·062	°057	'052	'047	°042	.038	.033	·028	.023	.010	.013	.000	.005	.000
16	.077	1071	.066	·061	·056	120	·045	.010	.035	.030	.025	.020	·015	.010	.005	.000
17	.082	.076	·071	.065	·059	.054	·048	.043	.038	.032	.027	.021	.010	.011	·005	.000
18	·087	·081	·075	•069	•063	.022	·051	.046	·040	.034	·028	.053	.012	.011	.000	.000
19	·092	.080	.079	.073	.067	.001	·055	.048	.042	•036	·030	·024	.018	.012	•006	.000
20	uya	091	004	0/7	071	004	050	051	045	030	032	025	019	013	000	000
21	.103	.000	.080	'082 '086	·075	.008	'061	.054	°047	·040	·034	027	·020	.013	*007	'000'
23	.114	.101	.003	.000	*083	.075	·067	1.020	·052	042	.032	.030	.022	014	.007	.000
24	.110	.111	103	·095	·087	.079	·07I	.063	.055	.047	.039	.031	.023	.010	.008	.000
25	•125	•110	.108	.099	.001	·082	·074	.000	•057	•049	·041	.033	·024	.010	.008	.000
26	.131	•122	.113	•104	·095	·086	·077	·069	• 0 60	.021	·043	.034	.026	.012	.000	.000
27	·137	•127	.118	•108	•099	.000	.081	.025	.063	.054	·045	·036	.027	.018	.000	.000
28	·142	.133	.123	.113	•103	·094	1084	075	·005	.050	·047	.037	028	.010	.000	.000
30	149	·I44	120	1123	100	102	.001	.081	·071	.001	·040	039	.030	.020	.010	.000
21	·161	.120	.130	.128	.117	106	.005	.084	.074	.062	.052	.042	·031	.021	010	.000
32	.167	156	144	.133	.121	.110	.000	.088	.077	.066	.022	.044	.033	.022	.011	.000
33	•174	•162	.120	•138	126	.112	.103	.001	.080	·068	·057	·045	.034	.023	.011	.000
34	.181	.168	.156	.143	.131	.110	107	.092	.083	.071	·059	.047	.032	.024	.015	.000
35	-100	175	102	149	.130	123	.111	1098	.090	.074	.001	049	1037	1024	1012	000
30	195	.181	.108	154	141	.159	.112	.102	.080	.070	·064	.051	038	.025	.013	.000
3/	.200	100	174	•166	140	.138	119	.110	093	·082	·068	.055	039	020	.013	.000
39	.217	•202	.187	.172	.157	•143	·128	'114	.099	·085	·071	·057	.042	·028	.014	.000
40	•225	•209	•194	•178	.163	•148	.133	.118	.103	·088	·073	.029	.044	.029	.012	.000
41	•233	•217	·201	.185	.160	•153	.138	.122	.107	.001	·076	·061	.046	.030	.012	·0 00
42	·241	*224	208	191	175	159	143	127	111.	.095	.079	.063	.047	1.031	016	.000
43	250	233 241	215	190	101	104	140	131	114	1098	084	·005	049	1.033	.010	1000
45	•268	.249	.231	.213	194	·176	158	•141	123	.105	·087	.070	.052	.035	.017	.000
46	•277	.258	.239	.220	.201	.183	.164	•146	.127	.100	·001	.072	.054	.036	·018	.000
47	•287	.267	1.248	.228	.208	.189	.170	.121	132	.113	.094	.075	1.056	.037	.019	.000
48	•298	277	.256	.236	*216	.196	176	•156	.130	·117	·097	.078	.058	.039	.019	.000
49	.308	207	200	245	224	203	180	102	141	121	101.	1.080	1000	040	1020 1021	1000
50	. 519	~9/	-/3	-33	-32				140			1.005	66-	1.0.12		
51	·331	308	205	202	240	218	.190	174	152	130	.115	1000	005	1043	022	.000
53	·356	.331	.306	.282	•258	.234	.210	187	163	139	·116	.093	070	.046	.023	.000
54	•369	343	.318	•293	.268	.243	.218	193	.169	145	·120	.096	.072	.048	.024	.000
55	.383	.356	.330	.304	1.278	.252	•226	201	•175	.120	.152	.100	.075	.020	.022	.000
56	397	•370	•342	°315	*288	261	*235	•208	•182	156	130	104	.078	.052	.026	.000
57	413	384	350	327	299	272	244	210	189	102	135	108	180.	1.054	1027	1000
50	429	399	1.309	340	324	202	·264	2234	190	100	140	.116	087	1.058	.029	.000
60	•464	1.432	1.400	1.368	337	.305	1.274	1.243	.213	182	•152	.131	.001	.060	.030	.000
	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
1	00	56	52	48	44	40	36	32	1 28	24	20	10	12	1 8	4	00

When hour angle is more than 6 hours, name the factors taken from Table A the same as the name of the latitude.

23 Table B.

							5 1	HOUR	s.							6 Hr.
Declination.	m. 00	m. 4	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 00
° 0 1 2 3 4	.000 .018 .036 .054 .072 .091	.000 .018 .036 .054 .072 .000	000 018 036 054 072	.000 .018 .036 .054 .071 .089	·000 ·018 ·036 ·053 ·071 ·080	.000 .018 .035 .053 .071 .089	, 000 018 035 053 071 089	, 018 035 053 071 088	.000 .018 .035 .053 .070 .088	.000 .018 .035 .053 .070 .088	.000 .018 .035 .053 .070 .088	, 017 035 053 070 088	.000 .017 .035 .052 .070 .088	, •000 •017 •035 •052 •070 •088	.000 .017 .035 .052 .070 .088	, 000 017 035 052 070
6 7 8 9 10	·109 ·127 ·145 ·164 ·183	·108 ·127 ·145 ·163 ·182	·108 •126 •144 •163 •181	·107 ·126 ·144 ·162 ·180	·107 ·125 ·143 ·161 ·180	·107 ·125 ·143 ·161 ·179	·106 ·124 ·142 ·160 ·179	·106 ·124 ·142 ·160 ·178	•106 •124 •142 •160 •178	·106 ·123 ·141 ·159 ·177	·106 ·123 ·141 ·159 ·177	·105 ·123 ·141 ·159 ·177	•105 •123 •141 •159 •177	·105 ·123 ·141 ·158 ·176	·105 ·123 ·141 ·158 ·176	*105 *123 *141 *158 *176
11 12 13 14 15 16	·201 ·220 ·239 ·258 ·277 ·297	·200 ·219 ·238 ·257 ·276 ·296	·199 ·218 ·237 ·256 ·275 ·294	·199 ·217 ·236 ·255 ·274 ·293	·198 ·217 ·235 ·254 ·273 ·292	·197 ·216 ·234 ·253 ·272 ·291	·197 ·215 ·234 ·252 ·271 ·290	·190 ·215 ·233 ·252 ·271 ·290	·190 ·214 ·233 ·251 ·270 ·289	·195 ·214 ·232 ·251 ·269 ·288	·195 ·213 ·232 ·250 ·269 ·288	·195 ·213 ·231 ·250 ·269 ·287	·195 ·213 ·231 ·250 ·268 ·287	·194 ·213 ·231 ·249 ·268 ·287	*194 *213 *231 *249 *268	·194 ·213 ·231 ·249 ·268 ·287
17 18 19 20 21	•317 •336 •356 •377 •397	·315 ·335 ·355 ·375 ·396	•314 •333 •353 •374 •394	*313 *332 *352 *372 *392	·311 ·331 ·351 ·371 ·391	·310 ·330 ·350 ·370 ·390	•310 •329 •349 •369 •389	•309 •328 •348 •368 •388	•308 •327 •347 •367 •387	·307 ·327 ·346 ·366 ·386	•307 •326 •346 •365 •385	·306 ·326 ·345 ·365 ·385	·306 ·325 ·345 ·364 ·384	·306 ·325 ·345 ·364 ·384	•306 •325 •344 •364 •384	·306 ·325 ·344 ·364 ·384
22 23°28' 24 25	•418 •439 •449 •461 •483	*410 *437 *447 *459 *481	·415 ·436 ·446 ·457 ·479	*413 *434 *444 *455 *477	·412 ·432 ·442 ·454 ·475 ·407	•410 •431 •441 •452 •474	'409 '430 '440 '451 '472	*408 *429 *438 *450 *471	*407 *428 *437 *449 *470	'400 '427 '437 '448 '469	·400 ·426 ·436 ·447 ·468	·405 ·426 ·435 ·446 ·467	·405 ·425 ·435 ·446 ·467	·404 ·425 ·434 ·445 ·467	·404 ·425 ·434 ·445 ·466	·404 ·424 ·434 ·445 ·466 ·488
20 27 28 29 30 Stars.	•527 •550 •574 •598	•525 •548 •571 •595	•523 •546 •569 •593	·521 ·544 ·567 ·590	•519 •542 •565 •588	495 •517 •540 •563 •586	·516 ·538 ·561 ·585	*95 *515 *537 *560 *583	•513 •536 •558 •582	·512 ·535 ·557 ·581	•511 •534 •556 •580	•5511 •533 •556 •579	·510 ·532 ·555 ·578	·510 ·532 ·555 ·578	·510 ·532 ·554 ·577	·510 ·532 ·554 ·577
N. Decln. Procyon Altair Aldebar'n Arcturus	•099 •157 •303 •370	•098 •156 •302 •368	·098 ·156 ·301 ·367	•098 •155 •300 •365	•097 •155 •298 •364	·097 ·154 ·297 ·363	•097 •154 •297 •362	·096 ·153 ·296 ·361	•096 •153 •295 •360	•096 •153 •295 •359	·096 ·152 ·294 ·359	•096 •152 •294 •358	•096 •152 •203 •358	·096 ·152 ·293 ·357	·096 ·152 ·293 ·357	•096 •152 •293 •357
Castor Vega Deneb Capella	.649 .829 1.03 1.07	•646 •826 1•03 1•06	°643 °822 1°02 1°06	•641 •819 1•02 1•06	.639 .816 1.02 1.05	.637 .813 1.01 1.05	•635 •811 1•01 1•05	·633 ·809 1·01 1·04	•632 •807 1•01 1•04	·630 ·806 1·00 1·04	·629 ·804 1·00 1·04	·628 ·803 1·00 1·03	·628 ·802 1·00 1·03	·627 ·802 1·00 1·03	•627 •801 1•00 1•03	.627 .801 1.00 1.03
a Persei η Ursæ Maj ϵ Ursæ Maj α Ursæ Maj	1°21 1°22 1°56 1°97	1.21 1.22 1.25 1.96	1.20 1.21 1.25 1.95	1.20 1.21 1.24 1.94	1.19 1.20 1.24 1.94	1.13 1.20 1.23 1.23	1.13 1.20 1.23 1.32	1.18 1.10 1.22 1.02	1.18 1.13 1.25 1.01	1.18 1.19 1.22 1.91	1.18 1.12 1.13 1.18	1.12 1.18 1.21 1.30	1.12 1.18 1.21 1.30	1.12 1.18 1.21 1.30	1.12 1.18 1.21 1.30	1·17 1·18 1·51 1·90
S. Decln. Rigel Sirius ε Sagittarii λ Scorpii γ Argûs	·151 ·308 ·710 ·781 1·11	·150 ·307 ·706 ·778 1·11	·150 ·306 ·703 ·774 1·10	•149 •305 •701 •771 1•10	•149 •303 •698 •769 •769	•148 •303 •696 •766 1•09	•148 •302 •694 •764 1•09	·147 ·301 ·692 ·762 1·09	•147 •300 •691 •760 1•08	'147 '300 '689 '759 1'08	·147 ·299 ·688 ·757 1·08	•146 •299 •687 •756 1•08	•146 •298 •686 •756 1•08	•146 •298 •686 •755 1•08	•146 •298 •686 •755 1•08	•146 •298 •685 •755 1•08
α Gruis Canopus γ Crucis α Pavonis Achernar	1°13 1°36 1°57 1°60 1°64	1.12 1.35 1.56 1.59 1.63	1°12 1°34 1°56 1°58 1°62	1°11 1°34 1°55 1°58 1°62	1.11 1.33 1.55 1.57 1.61	1.10 1.33 1.54 1.57 1.61	1°10 1°33 1°54 1°56 1°60	1°10 1°32 1°53 1°56 1°60	1.10 1.32 1.53 1.55 1.59	1.09 1.32 1.53 1.55 1.59	1.09 1.32 1.52 1.55 1.59	1.09 1.31 1.52 1.55 1.59	1.09 1.31 1.52 1.54 1.58	1.09 1.31 1.52 1.54 1.58	1.09 1.31 1.52 1.54 1.58	1.09 1.31 1.52 1.54 1.58
ϵ Argûs β Centauri a^2 Centauri a^1 Crucis a Tri. Aus. β Argûs	1.74 1.79 1.83 2.00 2.68 2.75	1.73 1.78 1.82 1.99 2.67 2.73	1.72 1.77 1.81 1.98 2.65 2.72	1.72 1.77 1.80 1.97 2.64 2.71	1.71 1.76 1.80 1.97 2.64 2.70	1.70 1.75 1.79 1.96 2.63 2.69	1.70 1.75 1.79 1.95 2.62 2.60	1.69 1.74 1.78 1.95 2.61 2.68	1.69 1.74 1.78 1.94 2.61 2.67	1.69 1.74 1.77 1.94 2.60 2.67	1.68 1.73 1.77 1.94 2.60 2.66	1.68 1.73 1.77 1.93 2.59 2.66	1.68 1.73 1.77 1.93 2.59 2.66	1.68 1.73 1.77 1.93 2.59 2.65	1.68 1.73 1.77 1.93 2.59 2.65	1.68 1.73 1.76 1.93 2.59 2.65
	m. 00 7 Hr.	m. 56	m. 52	m. 48	m. 44	m. 40	т. 3б	m. 32 6	m. 28 HOUI	m. 24 RS.	m. 20	m. 16	m. 12	m. 8	m. 4	m. 00

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Table A.

When hour angle is less than 6 hours, name the factors taken from Table A contrary to name of lat.

<u>م</u>								0	HOU	R.							1 Hr.
La	m. 1	Var. to 1' of L.	m. 4	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	m. 43	m. 52	m. 58	m. 00
o 61 62 63 64	413 431 450 470	" 17 [.] 0 18 [.] 2 19 [.] 4 20 [.] 8	/ 103 108 112 117	52 54 56 59	, 34 36 37 39	26 27 28 29	/ 21 21 22 23	, 17·2 17·9 18·7 19·5	14.7 15.3 16.0 16.7	12.8 13.4 14.0 14.7	, 11°4 11°9 12°4 12°9	, 10.2 10.2 11.1 11.6	, 9'3 9'7 10'1 10'5	8.5 8.8 9.2 9.6	7.8 8.1 8.5 8.9	7.2 7.5 7.9 8.2	6.7 7.0 7.3 7.7
65 66 67 68	491 515 540 567	22·4 24·2 26·2 28·6	123 129 135 142	61 64 67 71	41 43 45 47	31 32 34 35	25 26 27 28	20°4 21°4 22°4 23°5	17°5 18°3 19°2 20°2	15·3 16•0 16•8 17•6	13.5 14.2 14.9 15.6	12 ·2 12 ·7 13·4 14·0	11°0 11°6 12°1 12°7	11.0 11.1 10.0 10.1	9°3 9'7 10°2 10'7	8·6 9·0 9'4 9'9	8.0 8.4 8.8 9.2
69 70 71 72	597 630 666 705	31·2 34·3 37·8 42·0	149 157 166 176	75 79 83 88	50 52 55 59	37 39 42 44	30 31 33 35	24°8 26°1 27°6 29°3	21·2 22·4 23·7 25·1	18·5 19·5 20·7 21·9	16·4 17·3 18·3 19·4	14°8 15°6 16°5 17°5	13°4 14°1 14°9 15°8	12·3 12·9 13·7 14·6	11.3 11.9 12.6 13.3	10°4 11°0 11°6 12°3	9.7 10.3 10.8 11.5
	m. 59		m. 56	m. 52	m. 48	m. 44	m. 40	m. 36	m. 32 11 HO	m. 28 UBS.	m. 24	m. 20	т. 1б	m. 12	m. 8	m. 4	m. 00

								1 HC	UR.							2 Hr.
Lat	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	00	4	8	12	16	20	24	28	32	36	40	44	48	52	56	00
° 61 62 63 64	6.7 7.0 7.3 7.7	6·3 6·6 6·8 7·2	5.9 6.2 6.4 6.7	, 5:55 5:79 6:04 6:31	5·24 5·46 5·70 5·95	4*96 5*17 5*39 5*63	4.70 4.90 5.11 5.34	4.47 4.65 4.86 5.07	4·25 4·43 4·62 4·83	4.02 4.22 4.41 4.61	3 ^{.8} 7 4 ^{.03} 4 ^{.21} 4 ^{.40}	3.70 3.86 4.02 4.20	3.54 3.69 3.85 4.02	3·39 3·54 3·69 3·86	3·25 3·39 3·54 3·70	3.12 3.26 3.40 3.55
65	8.0	7°5	7.0	6.60	6·23	5•89	5°59	5°31	5.05	4*82	4.60	4°40	4°21	4°03	3 ^{.87}	3·71
66	8.4	7'8	7.3	6.91	6·52	6•17	5°85	5°56	5.29	5*04	4.82	4°61	4°41	4°22	4 ^{.05}	3·89
67	8.8	8'2	7.7	7.25	6·84	6•47	6°14	5°83	5.55	5*29	5.05	4°83	4°62	4°43	4 ^{.25}	4·08
68	9.2	8'6	8.1	7.62	7·19	6•80	6°45	6°13	5.83	5*56	5.31	5°07	4°86	4°65	4 ^{.47}	4·29
69	9'7	9.1	8.5	8 ·02	7°57	7·16	6·79	6·45	6·14	5.85	5°59	5°34	5.11	4.90	4°70	4'51
70	10'3	9.6	9.0	8·46	7°98	7·55	7·16	6·80	6·47	6.17	5°89	5°63	5.39	5.17	4°96	4'76
71	10'8	10.1	9.5	8·94	8°43	7·98	7·57	7·19	6·84	6.52	6°23	5°95	5.70	5.46	5°24	5'03
72	11'5	10.2	10.1	9·47	8°94	8·46	8·02	7·62	7·25	6.91	6°60	6°31	6.04	5.79	5°55	5'33
	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	т.	m.	m.	m.	m.
	00	56	52	48	44	40	36	32	28	24	20	1б	12	8	4	00

								2 HO	URS.							3 Hr.
Lat	m. 00	m. 4	m. 8	m. 12	m. 15	m. 20	111. 24	m. 28	m. 32	m 36	m. 40	m. 44	m. 43	m. 52	m. 56	m. 00
• 61 62 63 64 65 66 67 68	3.12 3.26 3.40 3.55 3.55 3.71 3.89 4.08 4.29	3.00 3.13 3.27 3.41 3.57 3.74 3.92 4.12	2.89 3.01 3.14 3.28 3.43 3.59 3.77 3.96	2.78 2.90 3.02 3.16 3.30 3.46 3.63 3.81	2.67 2.79 2.91 3.04 3.18 3.33 3.49 3.67	2.58 2.69 2.80 2.93 3.06 3.21 3.36 3.53	2.48 2.59 2.70 2.82 2.95 3.09 3.24 3.41	2.39 2.50 2.60 2.72 2.85 2.98 3.13 3.28	2.31 2.41 2.51 2.62 2.74 2.87 3.02 3.17	2.23 2.32 2.42 2.53 2.65 2.77 2.91 3.06	, 2°15 2°24 2°34 2°34 2°44 2°56 2°68 2°81 2°95	2.08 2.16 2.26 2.36 2.47 2.58 2.71 2.85	2.00 2.09 2.18 2.28 2.38 2.49 2.62 2.75	, 1.93 2.02 2.10 2.20 2.30 2.41 2.53 2.65	1.87 1.95 2.03 2.12 2.22 2.33 2.44 2.56	1.80 1.88 1.96 2.05 2.14 2.25 2.36 2.48
69 70 71 72	4.51 4.76 5.03 5.33 m. 00	4°34 4°57 4°83 5°12 m. 56	4°17 4'40 4'65 4'93 m. 52	4.01 4.23 4.47 4.74 m. 48	3.86 4.07 4.31 4.56 m. 44	3.72 3.92 4.15 4.40 m. 40	3.59 3.78 4.00 4.24 m. 36	3.46 3.65 3.85 4.08 m. 32	3°33 3°52 3°72 3°94 m. 28	3.22 3.39 3.59 3.80 m. 24	3°10 3°27 3°46 3°67 m. 20	3.00 3.16 3.34 3.54 m. 16	2·89 3·05 3·23 3·42 m. 12	2.79 2.95 3.11 3.30 m. 8	2.70 2.85 3.01 3.19 m. 4	2.61 2.75 2.90 3.08 m. 00
	10 Hr.							9	HOUR	s						

When hour angle is more than 6 hours, name the factors taken from Table A the same as the name of the latitude.

Table A.

-	1									_						
÷.							3	HOUR	s.							4 Hr.
I.a.	m.	m.	m.	m.	m.	m.	т.	m.	m.	m.	m.	m.	m.	m.	m.	111.
	00	4	8	12	16	20	24	28	32	36	40	44	48	52	56	00
61 62 63 64	1.80 1.88 1.96 2.05	1.74 1.82 1.90 1.98	1.68 1.75 1.83 1.91	, 1.62 1.69 1.77 1.85	, 1.57 1.63 1.71 1.78	1.51 1.58 1.65 1.72	1.46 1.52 1.59 1.66	' 1.41 1.47 1.53 1.60	1·36 1·42 1·48 1·55	, 1·31 1·37 1·43 1·49	1·26 1·32 1·37 1·44	/ 1·22 1·27 1·32 1·38	1.17 1.22 1.27 1.33	, 1.13 1.18 1.23 1.28	, 1.08 1.13 1.18 1.23	, 1.04 1.09 1.13 1.18
65	2·14	2.07	2.00	1.93	1.86	1.80	1°74	1.68	1.62	1°56	1°50	1°45	1°39	1°34	1°29	1•24
66	2·25	2.17	2.09	2.02	1.95	1.88	1°82	1.75	1.69	1°63	1°57	1°51	1°46	1°40	1°35	1•30
67	2·36	2.28	2.20	2.12	2.05	1.98	1°91	1.84	1.78	1°71	1°65	1°59	1°53	1°47	1°42	1•36
68	2·48	2.39	2.31	2.23	2.15	2.08	2°00	1.93	1.87	1°80	1°73	1°67	1°61	1°55	1°49	1•43
69	2.61	2°52	2°43	2·35	2·26	2°19	2°11	2°04	1.96	1.89	1.82	1•76	1.69	1.63	1°57	1°50
70	2.75	2°65	2°56	2·47	2·39	2°31	2°22	2'15	2.07	2.00	1.92	1•85	1.78	1.72	1°65	1°59
71	2.90	2°80	2°71	2·61	2·52	2°44	2°35	2'27	2.19	2.11	2.03	1•96	1.89	1.81	1°75	1°68
72	3.08	2°97	2°87	2·77	2·68	2°58	2°49	2'40	2.32	2.24	2.16	2•08	2.00	1.92	1°85	1°78
	m.	m.	m.	m.	m.	m.	т.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	00	56	52	48	44	40	36	32	28	24	20	16	12	8	4	00
	00 9 Hr.	56	52	48	44	40	30	32 8 I	28 IOURS	24		20	20 10	20 10 12	20 16 12 8	20 16 12 8 4

When hour angle is less than o hours, name the factors taken from Table A contrary to nat	name of lat
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								4 HC	URS.							5 Hr.
Lat	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	00	4	8	12	16	20	24	28	32	36	40	44	48	52	56	00
° 61 62 63 64	, 1.04 1.09 1.13 1.18	, 1.00 1.04 1.09 1.14	, 96 1.00 1.04 1.09	, .92 .96 1.00 1.04	·88 ·92 ·96 1*00	•84 •88 •92 •96	•80 •84 •87 •91	.77 .80 .83 .87	•73 •76 •79 •83	•69 •72 •75 •79	·66 ·68 ·71 ·75	•62 •65 •68 •71	•59 •61 •64 •67	•55 •57 •60 •63	·52 ·54 ·56 ·59	·48 ·50 ·53 ·55
65	1·24	1·19	1·14	1.09	1.02	1.00	•95	•91	·87	•82	·78	•74	•70	•66	•61	•57
66	1·30	1·24	1·19	1.14	1.10	1.02	1•00	•95	·91	•86	·82	•77	•73	•69	•64	•60
67	1·36	1·31	1·25	1.20	1.12	1.10	1•05	1•00	·95	•90	·86	•81	•77	•72	•68	•63
68	1·43	1·37	1·32	1.26	1.21	1.12	1•10	1•05	1·00	•95	·90	•85	•80	•76	•71	•66
69	1.20	1°44	1°39	1·33	1°27	1·21	1°16	1.11	1.05	1.00	•95	•90	•85	•80	•75	•70
70	1.29	1°52	1°46	1·40	1°34	1·28	1°22	1.12	1.11	1.02	1•00	•95	•89	•84	•79	•74
71	1.68	1°61	1°54	1·48	1°42	1·35	1°29	1.23	1.17	1.11	1•06	1•00	•94	•89	•83	•78
72	1.78	1°71	1°64	1·57	1°50	1·44	1°37	1.31	1.24	1.18	1•12	1•06	1•00	•94	•88	•82
	m. 00 8 Hr.	m. 56	m. 52	m. 48	m. 44	m. 40	т. 3б	m. 32 7 HO	m. 28	m. 24	m. 20	т. 1б	m. 12	m. 8	m. 4	m. 00

								5 HO	URS.							6 Hr.
Lat	m. 00	m. 4	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 00
° 61 62 63 64 65 66 67	•483 •504 •526 •549 •575 •602 •631	•450 •469 •489 •511 •535 •560 •587	•416 •434 •453 •473 •495 •519 •544	•383 •400 •417 •436 •456 •477 •501	•351 •366 •381 •399 •417 •437 •458	·318 ·332 ·346 ·362 ·362 ·378 ·396 ·415	•286 •298 •311 •325 •340 •356 •373	•254 •264 •276 •288 •301 •316 •331	•222 •231 •241 •252 •263 •276 •289	, 190 198 206 215 225 236 228	•158 •165 •172 •179 •188 •197 •206	·126 ·132 ·137 ·143 ·150 ·157 ·165	·095 ·099 ·103 ·107 ·112 ·118 ·123	•063 •066 •069 •072 •075 •075 •078 •082	•031 •033 •034 •036 •037 •039 •041	•000 •000 •000 •000 •000 •000
68 69 70 71 72	·663 ·698 ·736 ·778 ·825 m.	•617 •650 •685 •724 •767 m.	•571 •601 •634 •670 •711 m.	•526 •554 •584 •617 •654 m.	• 481 • 506 •534 •565 •598 m.	•436 •459 •484 •512 •543 m.	·392 ·413 ·435 ·460 ·487 m.	·348 ·366 ·386 ·408 ·433 m.	·304 ·320 ·337 ·357 ·378 m.	•260 •274 •289 •305 •323 m.	·217 ·228 ·240 ·254 ·269 m.	•173 •182 •192 •203 •215 m.	•130 •137 •144 •152 •161 m.	•086 •091 •096 •101 •107 m. 8	•043 •045 •048 •051 •054 m.	•000 •000 •000 •000 •000 m.
	00 7 Hr.	56	52	48	44	40	30	3 ²	HOUR	24 S.	20	10	14		4	

When hour angle is more than 6 hours, name the factors taken from Table A the same as the name of the latitude.

Table A.

Nh	en hou	ır an	gle is	less (han (5 hou	ırs, n	ame t	he fac	tors ta	aken fi	rom T	able A	contr	ary to	name	of lat.
فد								0	HOUI	R.							1 Hr.
I.at	т. 1	Var. to 1' of L.	m. 4	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	rn. 43	m. 52	m. 56	m. 00
° 73 74 75 76	, 750 799 855 919	47 53 60 69	187 200 214 230	94 100 107 115	62 67 71 77	47 50 53 57	, 37 40 43 46	31 33 36 38	26.6 28.4 30.4 32.7	23.3 24.8 26.6 28.5	20.7 22.0 23.6 25.3	18.5 19.8 21.2 22.7	16.8 17.9 19.2 20.6	15.4 16.4 17.6 18.9	14.2 15.1 16.2 17.4	13.1 14.0 15.0 16.1	12.2 13.0 13.9 15.0
77 78 79 80	993 1078 1179 1300	80 93 111 134	248 270 295 325	124 135 147 162	83 90 98 108	62 67 74 81	50 54 59 65	41 45 49 54	35°3 38°3 41°9 46°2	30·8 33·5 36·6 40·4	27·3 29·7 32·5 35·8	24 ·6 26·7 29·2 32·2	22°3 24°2 26°5 29°2	20.4 22.1 24.2 26.7	18*8 20*4 22*3 24*6	17·4 18·9 20·6 22·7	16·2 17·6 19·2 21•2
81 82 83 84 85	1447 1631 1867 2181 2620	165 210 275 377 548	362 408 467 545 655	181 204 233 272 327	120 136 155 181 218	90 102 116 136 163	72 81 93 109 131	60 68 77 91 109	51.4 58.0 66.3 77.5 93.1	44°9 50°6 58°0 67°7 81°3	39'9 44'9 51'4 60'1 72'2	35 ·8 40·4 46·2 54·0 64·8	32°5 36°6 41°9 48°9 58°8	29.7 33.5 38.3 44.8 53.8	27·3 30·8 35·3 41·2 49·5	25·3 28·5 32·7 38·2 45·8	23.6 26.6 30.4 35.5 42.7
	m. 59		т. 5б	m. 52	m. 48	m. 44	m. 40	т. 3б	m. 32	m. 28	m. 24	m. 20	m. 16	m. 12	m. 8	m. 4	m. 00

								1 HC	UR.							2 Hr.
L,at	m. 00	m. 4	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 00
° 73 74 75 76 77 78 79 80 81 82 83 84 85	12:2 13:0 13:9 15:0 16:2 17:6 19:2 21:2 23:6 26:6 30:4 35:5 42:7	11'4 12'2 13'0 14'0 15'1 16'4 17'9 19'8 22'0 24'8 28'4 33'2 39'9	10.7 11.4 12.2 13.1 14.2 15.4 16.8 18.5 20.7 23.3 26.6 31.1 37.4	10.1 10.7 11.5 12.3 13.3 14.5 15.8 17.5 19.4 21.9 25.1 29.3 35.2	9.5 10.1 10.8 11.6 12.6 13.7 14.9 16.5 18.3 20.7 23.7 23.7 23.2	, 9.0 9.6 10.3 11.0 12.9 14.1 15.6 17.3 19.5 22.4 26.1 31.4	8.5 9.1 9.7 10.4 11.3 13.4 14.8 16.4 18.5 21.7 24.8 29.8	8.1 8.6 9.2 9.9 10.7 11.6 12.7 14.0 15.6 17.6 20.2 23.5 28.3	777 8.2 8.8 9.4 10.2 11.1 12.1 13.4 14.9 16.8 19.2 22.4 26.9	7'3 7'8 8'4 9'0 9'7 10'6 11'6 12'7 14'2 16'0 18'3 21'4 25'7	7.0 7.5 8.0 9.3 10.1 11.0 12.2 13.5 15.3 17.5 20.4 24.5	6.7 7.2 7.7 8.2 8.9 9.6 10.5 11.6 12.9 14.6 16.7 19.5 23.4	6.4 6.8 7.3 7.9 8.5 9.2 10.1 11.1 12.4 14.0 16.0 18.7 22.4	6·2 6·6 7·0 7·5 8·1 8·8 9·7 10·7 11·9 13·4 15·3 17·9 21·5	5.9 6.3 6.7 7.2 7.8 8.5 9.3 10.2 11.4 12.8 14.7 17.2 20.6	5.7 6.5 6.5 7.5 8.2 9.8 9.8 10.9 12.3 14.1 16.5 19.8
	m. 00	т. 56	111. 52	111. 18	11. 44	 ⊿0	36	32	28	24	20	16 I	III. 12	111. 8	иі. 4	m. 00
	11 Hr.				<u>1 4 T</u>			10 HC	URS.						· · · ·	

								2 HO	JRS.							3 Hr.
Lat	m.	m.	m.	m.	m.	m.	m.	m.	m.	m	m.	m.	m.	m.	m.	m.
	00	4	8	12	16	20	24	28	32	36	40	44	48	52	56	00
° 73 74 75 76 77	5.7 6.0 6.5 6.9	5°4 5°8 6°2 6°7	5.2 5.6 6.0 6.4	5.0 5.4 5.7 6.2 6.7	4.8 5.2 5.5 5.9 6.4	4.7 5.0 5.3 5.7 6.2	4.5 4.8 5.1 5.5 6.0	4°3 4°6 5°0 5°3	4°2 4°5 4°8 5°1	4.0 4.3 4.6 5.0	3'9 4'2 4'4 4'8	3.8 4.0 4.3 4.6 5.0	3.6 3.9 4.1 4.5 4.8	3.5 3.7 4.0 4.3 4.6	3°4 3°6 3°9 4°2	3'3 3'5 3'7 4'0
78	8.1	7.8	7°5	7.2	7.0	6.7	6·5	6·2	6.0	5.8	5.6	5°4	5°2	5°0	4'9	4°7
79	8.9	8.6	8°2	7.9	7.6	7.3	7·1	6·8	6.6	6.4	6.1	5°9	5°7	5°5	5'3	5°1
80	9.8	9.4	9°1	8.7	8.4	8.1	7·8	7·5	7.3	7.0	6.8	6°5	6°3	6°1	5'9	5°7
81	10.9	10.2	10°1	9'7	9'4	9 °0	8.7	8.4	8·1	7*8	7°5	7'3	7.0	6.8	6·5	6.3
82	12.3	11.8	11°4	11:0	10'5	10 °2	9.8	9.4	9·1	8*8	8°5	8'2	7.9	7.6	7·4	7.1
83	14.1	13.6	13°0	12:5	12'1	11°6	11.2	10.8	10·4	10*1	9°7	9'4	9.0	8.7	8·4	8.1
84	16.5	15.8	15°2	14:7	14'1	13°6	13.1	12.6	12·2	11*7	11°3	10'9	10.6	10.2	9·9	9.5
85	19.8	19.0	18°3	17:6	16'9	16°3	15.7	15.2	14·6	14*1	13°6	13'1	12.7	12.3	11·8	11.4
	m.	m.	m.	m.	m.	m.	т.	m.	m.	m.	m.	т.	m.	m.	m.	m.
	00	56	52	48	44	40	3б	32	28	24	20	1б	12	8	4	00
	10 Hr.							9	HOUR	s.						

When hour angle is more than 6 hours, name the factors taken from Table A the same as the same of the latitude.

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Table A.

When hour angle is less than 6 hours, name the factors taken from Table A contrary to name of lat.

m. 00 3.3 3.5 3.7	m. 4 3*2 3*4	m. 8 3.1	m. 12	m. 18	m. 20	m. 24	m. 23	m.	m.	m.	m.	m	m	112	
3·3 3·5 3·7	3·2 3·4	3.1	2.0	1				32	36	40	44	43	52	56	m. 00
4.0	3.6 3.9	3°3 3°5 3°7	3°1 3°4 3°6	2·84 3·03 3·24 3·49	2·74 2·93 3·13 3·37	2.65 2.82 3.02 3.25	2·56 2·72 2·92 3·13	2·46 2·63 2·81 3·02	2·38 2·53 2·71 2·91	2·29 2·44 2·61 2·81	2·21 2·35 2·52 2·71	2.12 2.26 2.42 2.60	2.04 2.18 2.33 2.51	1.97 2.10 2.24 2.41	1.89 2.01 2.15 2.32
4°3 4°7 5°1 5°7	4°2 4°5 5°0 5°5	4°0 4°4 4°8 5°3	3°9 4°2 4°6 5°1	3°77 4°09 4°47 4°93	3.63 3.95 4.32 4.76	3*51 3*81 4*17 4*59	3°38 3°68 4°02 4°43	3°26 3'55 3'88 4°27	3°15 3°42 3°74 4°12	3°03 3°29 3°60 3°97	2·92 3·17 3·47 3·83	2·81 3·06 3·34 3·68	2·71 2·94 3·21 3·54	2.60 2.83 3.09 3.41	2°50 2°72 2°97 3°27
6·3 7·1 8·1 9·5 11·4	6·1 6·9 7·9 9·2 11·0	5.9 6.6 7.6 8.9 10.7	5.7 6.4 7.3 8.6 10.3	5°49 6°19 7°08 8°27 9°94	5°30 5°97 6°83 7°98 9°59	5°11 5°76 6°60 7°70 9°26	4·93 5·56 6·36 7·43 8·93	4.76 5.36 6.14 7.17 8.61	4°59 5°17 5°92 6°91 8°30	4°42 4°98 5°70 6°66 8°00	4°26 4°80 5°49 6°42 7°71	4'10 4'62 5'29 6'18 7'42	3'95 4'45 5'09 5'95 7'14	3.79 4.28 4.89 5.72 6.87	3.65 4.11 4.70 5.49 6.60
m. 00	m. 56	m. 52	m. 48	m. 44	m. 40	m. 36	m. 32	m. 28	m. 24	m. 20	т. 16	m. 12	m. 8	m. 4	m. 00
1	4.0 4.3 4.7 5.1 5.7 6.3 7.1 8.1 9.5 11.4 m. 00 Hr	4'0 3'9 4'3 4'2 4'7 4'5 5'1 5'0 5'7 5'5 6'3 6'1 7'1 6'9 8'1 7'9 9'5 9'2 11'0 m. moo 5'6 6'1 5'7	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4'0 3'9 3'7 3'6 3'49 4'3 4'2 4'0 3'9 3'77 4'7 4'5 4'4 4'2 4'09 5'1 5'0 4'8 4'6 4'47 5'7 5'5 5'3 5'1 4'93 6'3 6'1 5'9 5'7 5'49 7'1 6'9 6'6 6'4 6'19 8'1 7'9 7'6 7'3 7'08 9'5 9'2 8'9 8'6 8'27 1'1.4 11'0 10'7 10'3 9'94 m. m. m. m. m. m. $0'5$ 52 4'8 44 'Hr 'Hr 'Hr 'Hr 'Hr	4'0 3'9 3'7 3'6 3'49 3'37 4'3 4'2 4'0 3'9 3'77 3'63 4'7 4'5 4'4 4'2 4'09 3'95 5'1 5'0 4'8 4'6 4'4 4'2 5'7 5'5 5'3 5'1 4'93 4'76 6'3 6'1 5'9 5'7 5'49 5'30 7'1 6'9 6'6 6'4 6'19 5'97 8'1 7'9 7'6 7'3 7'08 6'83 9'5 9'2 8'9 8'6 8'27 7'98 11'0 10'7 10'3 994 9'59 m. m. m. m. m. m. o_0 56 52 4'8 44 40	4'0 3'9 3'7 3'6 3'49 3'37 3'25 4'3 4'2 4'0 3'9 3'77 3'63 3'51 4'7 4'5 4'4 4'2 4'09 3'95 3'81 5'1 5'0 4'8 4'6 4'47 4'32 4'17 5'7 5'5 5'3 5'1 4'93 4'76 4'59 6'3 6'1 5'9 5'7 5'49 5'30 5'11 7'1 6'9 6'6 6'4 6'19 5'97 5'76 8'1 7'9 7'6 7'3 7'08 6'83 6'60 9'5 9'2 8'9 8'6 8'27 7'98 7'70 11'0 10'7 10'3 9'94 9'59 9'26 m. m. m. m. m. m. m. 0'1 10'3 4'4 4'0 36 36 H'1 5'5 5'2 4'8 4'4 4'0 36	4'0 3'9 3'7 3'6 3'49 3'37 3'25 3'13 4'3 4'2 4'0 3'9 3'77 3'63 3'51 3'38 4'7 4'5 4'4 4'2 4'09 3'95 3'81 3'68 5'1 5'0 4'8 4'6 4'47 4'32 4'17 4'02 5'7 5'5 5'3 5'1 4'39 4'76 4'59 4'43 6'3 6'1 5'9 5'7 5'49 5'30 5'11 4'93 7'1 6'9 6'6 6'4 6'19 5'97 5'76 5'56 8'1 7'9 7'6 7'3 7'08 6'83 6'60 6'6'3 9'5 9'2 8'9 8'6 8'27 7'98 7'70 7'43 11'0 10'7 10'3 9'94 9'59 9'26 8'93 m. m. m. m. m. m. m. 3'3 0'0 56 52 4'8 4'4 4'0 36<	4'0 3'9 3'7 3'6 3'49 3'37 3'25 3'13 3'02 4'3 4'2 4'0 3'9 3'77 3'63 3'51 3'38 3'26 4'7 4'5 4'4 4'2 4'09 3'95 3'81 3'68 3'55 5'1 5'0 4'8 4'6 4'47 4'32 4'17 4'02 3'88 5'7 5'5 5'3 5'1 4'93 4'76 4'59 4'43 4'27 6'3 6'1 5'9 5'7 5'49 5'30 5'11 4'93 4'76 7'1 6'9 6'6 6'4 6'19 5'97 5'76 5'56 5'36 8'1 7'9 7'6 7'3 7'08 6'83 6'60 6'14 6'19 5'97 5'76 5'56 5'36 8'1 7'9 7'6 7'3 7'08 6'83 6'60 6'13 6'11 9'5 9'2 8'9 8'6 8'27 7'98 7'70 7'43 7'17	4'0 3'9 3'7 3'6 3'49 3'37 3'25 3'13 3'02 2'91 4'3 4'2 4'0 3'9 3'77 3'63 3'51 3'38 3'26 3'15 4'7 4'5 4'4 4'2 4'09 3'95 3'81 3'68 3'55 3'42 5'1 5'0 4'8 4'6 4'47 4'32 4'17 4'02 3'88 3'74 5'7 5'5 5'3 5'1 4'32 4'17 4'02 3'88 3'74 6'3 6'1 5'9 5'7 5'49 5'30 5'11 4'93 4'76 4'59 7'1 6'9 6'6 6'4 6'19 5'97 5'76 5'56 5'36 5'17 8'1 7'9 7'6 7'3 7'08 6'83 6'60 6'36 6'14 5'92 9'5 9'2 8'9 8'6 8'27 7'98 7'70 7'43 7'17 6'91 1'1'0 10'7 10'3 9'94 9'59 <t< td=""><td>4'03'93'73'63'493'373'253'133'022'912'814'34'24'03'93'773'633'513'383'263'153'034'74'54'44'24'093'953'813'683'553'423'295'15'04'84'64'474'324'174'023'883'743'605'75'55'35'14'324'174'023'883'743'605'75'55'35'14'934'764'594'424'123'976'36'15'95'75'495'305'114'934'764'594'427'16'96'66'46'195'975'765'565'365'174'988'17'97'67'37'086'836'606'366'145'925'709'59'28'98'68'277'987'707'437'176'916'661'1411'010'710'39'949'599'268'938'618'308'00m.m.m.m.m.m.m.m.m.m.0'056524'84'44'03632282420Hr</td><td>4'03'93'73'63'493'373'253'133'022'912'812'714'34'24'03'93'773'633'513'383'263'153'032'924'74'54'44'24'093'953'813'683'553'423'293'175'15'04'84'64'474'324'174'023'883'743'603'475'75'55'35'14'934'764'594'434'274'123'973'836'36'15'95'75'495'305'114'934'764'594'424'267'16'96'66'46'195'975'765'565'365'174'984'808'17'97'67'37'086'836'606'366'145'925'705'499'59'28'98'68'277'987'707'437'176'916'666'421'1411'010'710'39'949'599'268'938'618'308'007'71m.m.m.m.m.m.m.m.m.m.m.0'056524844403632282016Ht8 HOURS</td><td>4'03'93'73'63'493'373'253'133'022'91$2\cdot81$$2\cdot71$$2\cdot60$4'34'24'03'93'773'633'513'383'263'153'03$2\cdot92$$2\cdot81$4'74'54'44'24'093'953'813'683'553'423'293'173'065'15'04'84'64'474'324'174'023'883'743'603'473'345'75'55'35'14'934'764'594'434'274'123'973'833'686'36'15'95'75'495'305'114'934'764'594'424'264'107'16'96'66'46'195'975'765'565'365'174'984'804'628'17'97'67'37'086'836'606'366'145'925'705'495'209'59'28'98'68'277'987'707'437'176'916'666'426'181'1411'010'710'39'949'599'268'938'618'308'007'717'42m.m.m.m.m.m.m.m.m.m.m.16120'056524'84'40363228242016<t< td=""><td>4'03'93'73'63'493'373'253'133'022'912'812'712'602'514'34'24'03'93'773'633'513'383'263'153'032'922'812'714'74'54'44'24'093'953'813'683'553'423'293'173'062'945'15'04'84'64'474'324'174'023'883'743'603'473'343'215'75'55'35'14'934'764'594'434'274'123'973'833'683'546'36'15'95'75'495'305'114'934'764'594'424'264'103'957'16'96'66'46'195'975'765'565'365'174'984'804'624'458'17'97'67'37'086'836'606'366'145'925'955'955'365'174'984'804'624'459'59'28'98'68'277'987'707'437'176'916'666'426'185'951'1411'010'710'39'949'599'268'938'618'308'007'717'427'14m.m.m.m.m.m.m.m.m.m.<!--</td--><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td></td></t<></td></t<>	4'03'93'73'63'493'373'253'133'022'912'814'34'24'03'93'773'633'513'383'263'153'034'74'54'44'24'093'953'813'683'553'423'295'15'04'84'64'474'324'174'023'883'743'605'75'55'35'14'324'174'023'883'743'605'75'55'35'14'934'764'594'424'123'976'36'15'95'75'495'305'114'934'764'594'427'16'96'66'46'195'975'765'565'365'174'988'17'97'67'37'086'836'606'366'145'925'709'59'28'98'68'277'987'707'437'176'916'661'1411'010'710'39'949'599'268'938'618'308'00m.m.m.m.m.m.m.m.m.m.0'056524'84'44'03632282420Hr	4'03'93'73'63'493'373'253'133'022'912'812'714'34'24'03'93'773'633'513'383'263'153'032'924'74'54'44'24'093'953'813'683'553'423'293'175'15'04'84'64'474'324'174'023'883'743'603'475'75'55'35'14'934'764'594'434'274'123'973'836'36'15'95'75'495'305'114'934'764'594'424'267'16'96'66'46'195'975'765'565'365'174'984'808'17'97'67'37'086'836'606'366'145'925'705'499'59'28'98'68'277'987'707'437'176'916'666'421'1411'010'710'39'949'599'268'938'618'308'007'71m.m.m.m.m.m.m.m.m.m.m.0'056524844403632282016Ht8 HOURS	4'03'93'73'63'493'373'253'133'022'91 $2\cdot81$ $2\cdot71$ $2\cdot60$ 4'34'24'03'93'773'633'513'383'263'153'03 $2\cdot92$ $2\cdot81$ 4'74'54'44'24'093'953'813'683'553'423'293'173'065'15'04'84'64'474'324'174'023'883'743'603'473'345'75'55'35'14'934'764'594'434'274'123'973'833'686'36'15'95'75'495'305'114'934'764'594'424'264'107'16'96'66'46'195'975'765'565'365'174'984'804'628'17'97'67'37'086'836'606'366'145'925'705'495'209'59'28'98'68'277'987'707'437'176'916'666'426'181'1411'010'710'39'949'599'268'938'618'308'007'717'42m.m.m.m.m.m.m.m.m.m.m.16120'056524'84'40363228242016 <t< td=""><td>4'03'93'73'63'493'373'253'133'022'912'812'712'602'514'34'24'03'93'773'633'513'383'263'153'032'922'812'714'74'54'44'24'093'953'813'683'553'423'293'173'062'945'15'04'84'64'474'324'174'023'883'743'603'473'343'215'75'55'35'14'934'764'594'434'274'123'973'833'683'546'36'15'95'75'495'305'114'934'764'594'424'264'103'957'16'96'66'46'195'975'765'565'365'174'984'804'624'458'17'97'67'37'086'836'606'366'145'925'955'955'365'174'984'804'624'459'59'28'98'68'277'987'707'437'176'916'666'426'185'951'1411'010'710'39'949'599'268'938'618'308'007'717'427'14m.m.m.m.m.m.m.m.m.m.<!--</td--><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td></td></t<>	4'03'93'73'63'493'373'253'133'022'912'812'712'602'514'34'24'03'93'773'633'513'383'263'153'032'922'812'714'74'54'44'24'093'953'813'683'553'423'293'173'062'945'15'04'84'64'474'324'174'023'883'743'603'473'343'215'75'55'35'14'934'764'594'434'274'123'973'833'683'546'36'15'95'75'495'305'114'934'764'594'424'264'103'957'16'96'66'46'195'975'765'565'365'174'984'804'624'458'17'97'67'37'086'836'606'366'145'925'955'955'365'174'984'804'624'459'59'28'98'68'277'987'707'437'176'916'666'426'185'951'1411'010'710'39'949'599'268'938'618'308'007'717'427'14m.m.m.m.m.m.m.m.m.m. </td <td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td>	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

	1							4 HC	URS.							5 Hr
Lat	m.	m.	100.	m.	m	100.	m.	m	m.	m.	m	10.	m.	m.	m.	ш.
	00	4	8	12	16	20	24	28	32	36	40	44	48	52	56	00
° 73 74 75	1.89 2.01 2.15	1.81 1.93 2.07	1.74 1.85 1.98	1.67 1.78 1.90	1.60 1.70 1.82	1.53 1.63 1.74	1.46 1.55 1.66	1·39 1·48 1·58	1·32 1·41 1·51	1.34 1.43	1.19 1.27 1.36	, 1.13 1.20 1.29	1.06 1.13 1.21	, 1.00 1.07 1.14	'94 1'00 1'07	·88 ·93 1·00
76	2·32	2·22	2:13	2.04	1'96	1.87	1.79	1.70	1.62	1.54	1.40	1.38	1.30	1.23	1.15	1.07
77	2·50	2·40	2:30	2.21	2'11	2.02	1.93	1.84	1.75	1.66	1.58	1.49	1.41	1.32	1.24	1.16
78	2·72	2·61	2:50	2.40	2'29	2.19	2.09	2.00	1.90	1.81	1.71	1.62	1.53	1.44	1.35	1.26
79	2·97	2·85	2:74	2.62	2'51	2.40	2.29	2.18	2.08	1.97	1.87	1.77	1.67	1.57	1.48	1.38
80	3·27	3·14	3:02	2.89	2'77	2.64	2.53	2.41	2.29	2.18	2.06	1.95	1.84	1.73	1.63	1.52
81	3.65	3.50	3·36	3.22	3.08	2.94	2.81	2.68	2·55	2.42	2°30	2°17	2.05	1.93	1.81	1.69
82	4.11	3.94	3·78	3.63	3.47	3.32	3.17	3.02	2·87	2.73	2°59	2°45	2.31	2.18	2.04	1.91
83	4.70	4.51	4·33	4.15	3.97	3.80	3.63	3.46	3·29	3.13	2°96	2°80	2.65	2.49	2.34	2.18
84	5.49	5.27	5·06	4.85	4.64	4.44	4.24	4.04	3·84	3.65	3°46	3°28	3.09	2.91	2.73	2.55
85	6.60	6.34	6·08	5.82	5.57	5.33	5.09	4.85	4·62	4.39	4°16	3'94	3.71	3.49	3.28	3.06
	m	m	m.	m.	m.	m.	m	m.	m.	m.	m.	m.	m.	m.	m.	m.
	00	56	52	48	44	40	36	32	28	24	20	16	12	8	4	00
	8 Hr							7 HO	URS.							

								5 HO	URS							6 Hr.
Lat	ш. 90	m 4	20. 8	m 12	10 16	100. 20	m 24	m 28	m. 32	m 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 00
° 73 74 75 76 77 78 79	·88 93 1·00 1·07 1·16 1·26 1·38	·82 ·87 ·93 I·00 I·08 I·17 I·28	, 81 86 93 1.00 1.09 1.19	*70 *74 *85 *92 1*00 1*09	·64 ·68 ·73 ·78 ·84 ·91 1·00	·58 ·61 ·66 ·71 ·76 ·83 ·91	*52 *55 *59 *64 *69 *75 *81	*46 *49 *52 *56 *61 *66 *72	•40 •43 •46 •49 •53 •58 •63	*34 *37 *39 *42 *46 *49 *54	·29 ·31 ·33 ·35 ·38 ·41 ·45	*23 *24 *26 *28 *30 *33 *36	·17 •18 •20 •21 •23 •25 •27	*11 *12 *13 *14 *15 *16 *18	•06 •06 •07 •07 •07 •08 •08 •08	• • • • • • • • • • • • • • • • • • •
80 81 82 83 84 85	1.52 1.69 1.91 2.18 2.55 <u>3.06</u> 1.1.	1.41 1.57 1.77 2.03 2.37 2.85 m.	1.31 1.46 1.64 1.88 2.20 2.64 m.	1·21 1·34 1·51 1·73 2·02 2·43 m.	1.10 1.23 1.38 1.58 1.85 2.22 m.	1.00 1.11 1.25 1.44 1.68 2.02 m.	·90 1·00 1·13 1·29 1·51 1·81 m.	•89 •89 •100 •114 •134 •61 •.61	•70 •78 •87 1•00 1•17 1•40 m.	•66 •75 •86 1•00 1•20 m.	•50 •55 •62 •71 •83 1•90 m.	•40 •44 •50 •57 •67 •80 m.	•30 •33 •37 •43 •50 •60 m.	•20 •22 •25 •28 •33 •40 m.	•10 •11 •12 •14 •17 •20 m.	•00 •00 •00 •00 •00 •00 •00 •00
	00 7 Hr.	56	25	48	44	40	36	32 6	28 HOUR	24 .S.	20	16	12	8	4	00

When hour angle is more than 6 hours, name the factors taken from Table A the same as the name of the latitude.

\mathbf{T}	a	bl	e	\mathbf{B}

tion								0 H	OUR.								1 Hr.
Declina	m. 1	Var. to 1' of Decl.	m. 4	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	m. 48	m. 52	m, 58	m. 00
° 30 31 32 33 34	, 132 138 143 149 155	" 5·33 5·44 5·56 5·69 5·82	33°1 34°4 35°8 37°2 38°6	16'5 17'2 17'9 18'6 19'3	11.0 11.5 11.9 12.4 12.9	8 [°] 28 8°61 8°96 9°31 9°67	6 [.] 62 6.89 7 ^{.1} 7 7 ^{.45} 7 ^{.74}	5.52 5.75 5.98 6.21 6.45	4 [•] 74 4 [•] 93 5 [•] 13 5 [•] 33 5 [•] 53	4 [•] 15 4 [•] 32 4 [•] 49 4 [•] 67 4 [•] 85	3.69 3.84 3.99 4.15 4.31	3.32 3.46 3.60 3.74 3.88	3.03 3.15 3.27 3.40 3.53	2·78 2·89 3·01 3·12 3·24	2.57 2.67 2.78 2.89 3.00	2·39 2·48 2·58 2·68 2·79	2.23 2.32 2.41 2.51 2.61
35	160	5.96	4 0'1	20 ·1	13.4	10.0	8°03	6·70	5.75	5.03	4°48	4'03	3.67	3'37	3.11	2.89	2.71
36	167	6.11	41'6	20·8	13.9	10.4	8°34	6·95	5.96	5.22	4°64	4'18	3.81	3'49	3.23	3.00	2.81
37	173	6.27	43'2	21·6	14.4	10.8	8°65	7·21	6.18	5.41	4°82	4'34	3.95	3'62	3.35	3.11	2.91
38	179	6.44	44'8	22·4	14.9	11.2	8°96	7·47	6.41	5.61	4°99	4'50	4.09	3'76	3.47	3.23	3.02
39	186	6.62	46'4	23·2	15.5	11.6	9°29	7·75	6.64	5.82	5°18	4'66	4.24	3'89	3.60	3.35	3.13
40	192	6·82	48.1	24.0	16.0	12'0	9.63	8.03	6·89	6·03	5°36	4·83	4°40	4.04	3°73	3.47	3.24
41	199	7·03	49.8	24.9	16.6	12'5	9.97	8.32	7·13	6·25	5°56	5·01	4°56	4.18	3°86	3.59	3.36
42	206	7·25	51.6	25.8	17.2	12'9	10.3	8.61	7·39	6·47	5°76	5·19	4°72	4.33	4°00	3.72	3.48
43	214	7·48	53.4	26.7	17.8	13'4	10.7	8.92	7·65	6·70	5°96	5·37	4'89	4.49	4°15	3.85	3.60
44	221	7·73	55.3	27.7	18.5	13'8	11.1	9.24	7·92	6·94	6°17	5·56	5°06	4.64	4°29	3.99	3.73
45	229	8.00	57`3	28.7	19'1	14°3	11.5	9.57	8·21	7'19	6·39	5.76	5°24	4.81	4°45	4°13	3.86
46	237	8.29	59`3	29.7	19'8	14°8	11.9	9.91	8·50	7'44	6·62	5.96	5°43	4.98	4°60	4°28	4.00
47	246	8.60	61`4	30.7	20'5	15°4	12.3	10.3	8·80	7'71	6·86	6.18	5°62	5.16	4°77	4°43	4.14
48	255	8.93	63`6	31.8	21'2	15°9	12.7	10.6	9·11	7'98	7·10	6.40	5°82	5.34	4'94	4°59	4.29
49	264	9.30	65`9	33.0	22'0	16°5	13.2	11.0	9'44	8'27	7·35	6.62	6°03	5.53	5°11	4°76	4.44
50 51 52 53 53 54	273 283 293 304 315	9.69 10.1 10.6 11.1 11.6	68·3 70·8 73·3 76·0 78·9	34'1 35'4 36'7 38'0 39'4	22.8 23.6 24.5 25.4 26.3	17 [.] 1 17 [.] 7 18 [.] 3 19 [.] 0 19 [.] 7	13.7 14.2 14.7 15.2 15.8	11.4 11.8 12.2 12.7 13.2	9.7 ⁸ 10.1 10.5 10.9 11.3	8·56 8·87 9·20 9·54 9·89	7 ^{.62} 7 ^{.89} 8 ^{.18} 8 ^{.48} 8 ^{.80}	6·86 7·11 7·37 7·64 7·93	6·25 6·47 6·71 6·95 7·21	5.73 5.94 6.16 6.38 6.62	5·30 5·49 5·69 5·90 6·12	4 [.] 93 5 [.] 10 5 [.] 29 5 [.] 49 5 [.] 69	4.60 4.77 4.95 5.13 5.32
55	327	12·2	81.8	40'9	27·3	20'5	16.4	13'7	11.7	10'3	9'13	8·22	7'48	6·87	6·35	5.90	5.52
56	340	12·8	84.9	42'5	28·3	21'3	17.0	14'2	12.2	10'7	9'48	8·54	7'77	7·13	6·59	6.13	5.73
57	353	13·5	88.2	44'1	29·4	22'1	17.7	14'7	12.6	11'1	9'84	8·87	8'07	7·41	6·85	6.37	5.95
58	367	14·3	91.7	45'9	30·6	22'9	18.4	15'3	13.1	11'5	10'2	9·22	8'39	7·70	7·11	6.62	6.18
59	381	15·1	95.4	47'7	31·8	23'9	19.1	15'9	13.7	12'0	10'6	9·58	8'72	8·00	7·40	6.88	6.43
60	397	16°0	99'2	49.6	33'I	24·8	19'9	16.6	14·2	12.4	11.1	9 [.] 97	9.08	8·33	7.70	7.16	6.69
61	413	17°0	103	51.7	34'5	25·9	20'7	17.3	14·8	13.0	11.5	10.4	9.45	8·68	8.02	7.46	6.97
62	431	18°2	108	53.9	35'9	27·0	21'6	18.0	15·4	13.5	12.0	10.8	9.86	9·05	8.36	7.77	7.27
63	450	19°4	112	56.2	37'5	28·1	22'5	18.8	16·1	14.1	12.5	11.3	10.3	9·44	8.72	8.11	7.58
64	470	20°1	117	5 ^{8.} 7	39'2	29·4	23'5	19.6	16·8	14.7	13.1	11.8	10.7	9·86	9.11	8.48	7.92
65	491	22·4	123	61.4	41°0	30.7	24.6	20`5	17'6	15'4	13.7	12·3	11.2	10'3	9.53	8·86	8·29
66	515	24·2	129	64.4	42°9	32.2	25.8	21`5	18'4	16'1	14.4	12·9	11.8	10'8	9.98	9·28	8·68
67	540	26·2	135	67.5	45°0	33.8	27.0	22`5	19'3	16'9	15.1	13·6	12.3	11'3	10.5	9·74	9·10
68	567	28·6	142	70.9	47°3	35.5	28.4	23`7	20'3	17'8	15.8	14·3	13.0	11'9	11.0	10·2	9·56
69	597	31·2	149	74.6	49°8	37.3	29.9	24`9	21'4	18'7	16.7	15·0	13.7	12'5	11.6	10·8	10·1
70	630	34·3	157	78.7	52.5	39 [•] 4	31.5	26·3	22.5	19.7	17.6	15 ^{.8}	14'4	13 ^{.2}	12·2	11'4	10 ^{.6}
71	666	37·8	166	83.2	55.5	41 [•] 6	33.3	27·8	23.8	20.9	18.6	16 [.] 7	15'2	14 ^{.0}	12·9	12'0	11 ^{.2}
72	705	42·0	176	88.2	58.8	44 [•] 1	35.3	29·4	25.3	22.1	19.7	17 [.] 7	16'1	14 ^{.8}	13·7	12'7	11 ^{.9}
73	750	47	187	93.7	62.5	46 [•] 9	37.5	31·3	26.8	23.5	20.9	18 ^{.8}	17'1	15 ^{.7}	14·5	13'5	12 ^{.6}
74	799	53	200	99.9	66.6	50 [•] 0	40.0	33·4	28.6	25.1	22.3	20 [.] 1	18'3	16 ^{.8}	15·5	14'4	13 ^{.5}
75 76 77 78 78 79	855 919 993 1078 1179	60 69 80 93 111	214 230 248 270 295	107 115 124 135 147	71'3 76'6 82'8 89'9 98'3	53`5 57`5 62`1 67`4 73`8	42.8 46.0 19.7 54.0 59.0	35 '7 3 ⁸ '4 41'4 45'0 49 '2	30.6 32.9 35.5 38.6 42.2	26·8 28·8 31·1 33·8 37·0	23·9 25·6 27·7 30·1 32·9	21'5 23'1 24'9 27'1 29'6	19 [.] 6 21 [.] 0 22 [.] 7 24 [.] 7 27 [.] 0	18.0 19.3 20.8 22.6 24.7	16.6 17.8 19.3 20.9 22.9	15°4 16°6 17°9 19°4 21°3	14'4 15'5 16'7 18'2 19'9
80	1300	134	325	163	108	81·3	65'1	54'3	46.5	40'7	36·3	32·7	29'7	27'3	25·2	23 4	21'9
81	1447	165	362	181	121	90·5	72'4	60'4	51.8	45'4	40·4	36·4	33'1	30'4	28·0	26 1	24'4
82	1631	210	408	204	136	.102	81'6	68'1	58.4	51'1	45·5	41 ·0	37'3	34'2	31·6	29 4	27'5
83	1867	275	467	233	156	117	93'4	77'9	66.8	58'5	52·1	46·9	42'7	39'2	36·2	33 7	31'5
84	2180	377	545	273	182	136	109	91'0	78.1	68'4	60·8	54·8	49'9	45'8	42·3	39 3	36'8
85	2620	548	655	328	218	164	131	109	93.8	82'1	73·1	65·8	59'9	55'0	50·8	47 2	44'2
	m. _59		m. 56	m. 52	m. 48	m. 44	m. 40	m. 36	m. 32 OURS	m. 28	m. 24	m. 20	m. 16	m. 12	m. 8	m. 4	m. 00

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Table B.

-i	1							HOL	IR							0 11=0
Declinatio	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	00	4	8	12	16	20	24	28	32	36	40	44	48	52	58	00
1 30 31 32 33 34	2 ['] 23 2'32 2'41 2'51 2'61	2.09 2.18 2.27 2.36 2.45	1.97 2.06 2.14 2.22 2.31	1.87 1.94 2.02 2.10 2.18	1.77 1.85 1.92 1.99 2.07	1.69 1.76 1.83 1.90 1.97	1.61 1.68 1.74 1.81 1.88	1.54 1.60 1.67 1.73 1.80	1.48 1.54 1.60 1.66 1.73	1'42 1'48 1'54 1'60 1'66	1·37 1·42 1·48 1·54 1·60	, 1.32 1.37 1.43 1.48 1.54	, 1.27 1.32 1.38 1.43 1.49	, 1.23 1.33 1.38 1.44	1'19 1'24 1'29 1'34 1'39	1.15 1.20 1.25 1.30 1.35
35	2.71	2·54	2·39	2·27	2.15	2.05	1.95	1.87	1.79	1.72	1.66	1.60	1.54	1°49	1°44	1°40
36	2.81	2·64	2·48	2·35	2.23	2.12	2.03	1.94	1.86	1.79	1.72	1.66	1.60	1°55	1°50	1°45
37	2.91	2·73	2·58	2·44	2.31	2.20	2.10	2.01	1.93	1.85	1.78	1.72	1.66	1°61	1°55	1°51
38	3.02	2·83	2·67	2·53	2.40	2.28	2.18	2.09	2.00	1.92	1.85	1.78	1.72	1°66	1°61	1°56
39	3.13	2·94	2·77	2·62	2.49	2.37	2.26	2.16	2.07	1.99	1.92	1.85	1.78	1°72	1°67	1°62
40	3·24	3.04	2·87	2.72	2·58	2·45	2°34	2°24	2·15	2.06	1.99	1.91	1.85	1.79	1.73	1.68
41	3·36	3.15	2·97	2.81	2·67	2·54	2°43	2°32	2·22	2.14	2.06	1.98	1.91	1.85	1.79	1.74
42	3·48	3.27	3·08	2.91	2·77	2·63	2°51	2°40	2·30	2.21	2.13	2.05	1.98	1.92	1.86	1.80
43	3·60	3.38	3·19	3.02	2·86	2·73	2°60	2°49	2·39	2.29	2.21	2.13	2.05	1.99	1.92	1.87
44	3·73	3.50	3·30	3.13	2·97	2·82	2°69	2°58	2·47	2.37	2.29	2.20	2.13	2.0 6	1.99	1.93
45	3·86	3.63	3°42	3 ^{.24}	3 ^{.07}	2·92	2·79	2.67	2·56	2·46	2·37	2·28	2°20	2°13	2.06	2.00
46	4·00	3.76	3°54	3 ^{.35}	3 ^{.18}	3·03	2·89	2.76	2·65	2·55	2·45	2·36	2°28	2°21	2.14	2.07
47	4·14	3.89	3°67	3 ^{.47}	3 ^{.29}	3·14	2·99	2.86	2·74	2·64	2·54	2·45	2°36	2°28	2.21	2.14
48	4·29	4.03	3°80	3 ^{.59}	3 ^{.41}	3·25	3·10	2.96	2·84	2·73	2·63	2·53	2°45	2°37	2.29	2.22
49	4·44	4.17	3°93	3 ^{.72}	3 ^{.53}	3·36	3·21	3.07	2·94	2·83	2·72	2·62	2°53	2°45	2.37	2.30
50	4.60	4·32	4.08	3 ^{.86}	3.66	3°48	3·33	3*18	3.05	2·93	2·82	2·72	2.63	2·54	2·46	2·38
51	4.77	4·48	4.22	4 ^{.00}	3.79	3°61	3·45	3*30	3.16	3·04	2·92	2·82	2.72	2·63	2·55	2·47
52	4.95	4·64	4.38	4 ^{.14}	3.93	3°74	3·57	3*42	3.28	3·15	3·03	2·92	2.82	2·73	2·64	2·56
53	5.13	4·81	4.54	4 ^{.29}	4.08	3°88	3·70	3*54	3.40	3·26	3·14	3·03	2.92	2·83	2·74	2·65
54	5.32	4·99	4.71	4 ^{.54}	4.23	4°02	3·84	3*67	3.52	3·38	3·26	3·14	3.03	2·93	2·84	2·75
55	5·52	5·18	4·88	4.62	4°39	4*18	3 ·99	3.81	3.66	3.51	3°38	3.26	3.15	3.04	2·95	2.86
56	5·73	5·38	5·07	4.80	4°55	4*33	4 ·14	3.96	3.79	3.65	3°51	3.38	3.27	3.16	3·06	2.97
57	5·95	5·59	5·27	4.98	4°73	4*50	4 ·30	4.11	3.94	3.79	3°64	3.51	3.39	3.28	3·18	3.08
58	6·18	5·81	5·47	5.18	4°92	4*68	4 ·47	4.27	4.10	3.93	3°79	3.65	3.53	3.41	3·30	3.20
59	6·43	6·04	5·69	5.39	5°11	4*87	4 ·6 4	4.44	4.26	4.09	3°94	3.80	3.67	3.55	3·43	3.33
60	6·69	6·28	5.92	5.61	5·32	5 [.] 06	4 ·83	4.62	4°43	4.26	4°10	3.95	3.82	3.69	3°57	3.46
61	6·97	6·55	6.17	5.84	5·54	5 [.] 27	5 ·03	4.82	4°62	4.44	4°27	4.12	3.97	3.84	3°72	3.61
62	7·27	6·82	6.43	6.09	5·78	5 [.] 50	5·25	5.02	4°81	4.62	4°45	4.29	4.14	4.01	3°88	3.76
63	7·58	7·12	6.71	6.35	6·03	5 [.] 74	5·48	5.24	5°02	4.83	4°64	4.48	4.32	4.18	4°05	3.93
64	7·92	7·44	7.01	6.63	6·30	5[.]9 9	5 ·7 2	5.47	5°25	5.04	4°85	4.68	4.52	4.37	4°23	4.10
65	8·29	7·78	7°33	6·94	6·59	6·27	5·98	5.72	5°49	5°27	5.07	4·89	4°72	4°57	4·42	4°29
66	8·68	8·15	7°68	7·27	6·90	6·57	6·27	6.00	5°75	5°52	5.31	5·12	4'95	4'78	4·63	4°49
67	9·10	8·55	8°06	7·62	7·24	6·89	6·57	6.29	6°03	5°79	5.57	5·37	5'19	5'02	4·86	4°71
68	9·56	8·98	8°47	8·01	7·60	7·24	6·91	6.61	6°33	6°09	5.86	5·65	5'45	5'27	5·11	4°95
69	10·1	9·45	8°91	8·43	8·00	7·62	7·27	6.95	6°67	6°40	6. 16	5·94	5'74	5'55	5·37	5°21
70	10.6	9 [.] 97	9.40	8·89	8·44	8.03	7.67	7:33	7 [.] 03	6·75	6·50	6·27	6.05	5•85	5.67	5°49
71	11.2	10 [.] 5	9.93	9·40	8·92	8.49	8.10	7:75	7 [.] 43	7·14	6·87	6·63	6.40	6•19	5.99	5'81
72	11.9	11 [.] 2	10.5	9·96	9·45	9.00	8.59	8:22	7 ^{.88}	7·57	7·28	7·02	6.78	6•56	6.35	6°16
73	12.6	11 [.] 9	11.2	10·6	10·0	9.56	9.13	8:73	8 [.] 37	8·04	7·74	7·46	7.20	6•97	6.75	6°54
74	13.5	12 [.] 7	11.9	11 ·3	10·7	10.2	9.73	9:31	8 [.] 93	8·57	8·25	7·96	7.68	7•43	7.19	6'97
75	14.4	13°5	12 ·8	12°1	11.2	10'9	10'4	9 ·96	9.55	9.18	8.83	8.51	8·22	7 [.] 95	7.70	7.46
76	15.5	14°6	13·7	13°0	12.3	11'7	11'2	10·7	10.3	9.86	9.49	9.15	8·83	8 [.] 54	8.27	8.02
77	16.7	15°7	14·8	14°0	13.3	12'7	12'1	11·6	11.1	10.6	10.2	9.88	9·54	9 [.] 23	8.93	8.66
78	18.2	17°1	16·1	15°2	14.5	13'8	13'1	12·6	12.0	11.6	11.1	10.7	10·4	10 ^{.0}	9.70	9.41
79	19.9	18°7	17·6	16°6	15.8	15'0	14'4	13 · 7	13.2	12.6	12.2	11.7	11·3	11 ^{.0}	10.6	10.3
80	21'9	20.6	19.4	18·4	17'4	16.6	15.8	15.1	14.5	13.9	13.4	12.9	12.5	12·1	11.7	11'3
81	24'4	22.9	21.6	20·4	19'4	18.5	17.6	16.9	16.2	15.5	14.9	14.4	13.9	13·4	13.0	12'6
82	27'5	25.8	24.3	23·0	21'9	20.8	19.9	19.0	18.2	17.5	16.8	16.2	15.7	15·2	14.7	14'2
83	31'5	29.5	27.9	26·4	25'0	23.8	22.7	21.7	20.8	20.0	19.3	18.6	17.9	17·3	16.8	16'3
84	36'8	34.5	32.5	30·8	29'2	27.8	26.5	25.4	24.4	23.4	22.5	21.7	21.0	20·3	19.6	19'0
85	44'2	41.5	39.1	37 · 0	35'1	33.4	31.9	30.5	29.3	28.1	27.0	26.1	25.2	24·3	23.6	22'9
	m. 00	m. 56	m. . 52	m. 48	m. 44	m. 40	m. 36	m. 32 HOU	m. 28 URS.	m. 24	m. 20	т. 1б	m. 12	m. 8	m. 4	m. 00

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Table B.

tion.						-	2	HOU	RS.							3 Hrs.
Declina	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	00	4	8	12	16	20	24	28	32	36	40	44	48	52	56	00
° 30 31 32 33 34	1.15 1.20 1.25 1.30 1.35	1.12 1.12 1.20 1.31	1.09 1.13 1.18 1.23 1.27	1.06 1.10 1.15 1.19 1.24	1'03 1'07 1'12 1'16 1'21	1.01 1.05 1.09 1.13 1.18	·98 1·02 1·06 1·10 1·15	·96 1·00 1·04 1·08 1·12	'94 '98 1'01 1'05 1'10	.92 .95 .99 1.03 1.07	'90 '93 '97 1.01 1.05		•86 •90 •93 •97 1•01	·85 ·88 ·92 ·95 ·99	•83 •86 •90 •93 •97	·82 ·85 ·88 ·92 ·95
35 36 37 38 39	1.40 1.45 1.51 1.56 1.62	1·36 1·41 1·46 1·52 1·57	1·32 1·37 1·42 1·47 1·53	1.29 1.33 1.38 1.43 1.43	1.25 1.30 1.35 1.40 1.45	1.22 1.27 1.31 1.36 1.41	1.19 1.24 1.33 1.38	1.16 1.21 1.25 1.30 1.35	1.14 1.18 1.22 1.27 1.32	1°11 1°15 1°20 1°24 1°29	1.09 1.13 1.17 1.22 1.26	1.07 1.11 1.15 1.19 1.23	1.05 1.09 1.30 1.17 1.21	1.03 1.07 1.10 1.15 1.19	1.01 1.02 1.08 1.12 1.17	.99 1.03 1.07 1.10 1.15
40	1.68	1.63	1·58	1.54	1.20	1.46	1.43	1.39	1·36	1.33	1.31	1·28	1·25	1·23	1·21	1.19
41	1.74	1.69	1·64	1.60	1.22	1.52	1.48	1.44	1·41	1.38	1.35	1·33	1·30	1·27	1·25	1.23
42	1.80	1.75	1·70	1.65	1.61	1.57	1.53	1.50	1·46	1.43	1.40	1·37	1·35	1·32	1·30	1.27
43	1.87	1.81	1·76	1.71	1.67	1.63	1.59	1.55	1·51	1.48	1.45	1·42	1·39	1·37	1·34	1.32
44	1.93	1.81	1·82	1.77	1.73	1.68	1.64	1.60	1·57	1.53	1.50	1·47	1·44	1·42	1·39	1.37
45	2.00	1.94	1.89	1.84	1.79	1.74	1.70	1.66	1.62	1.59	1.26	1·52	1°49	1.47	1°44	1.41
46	2.07	2.01	1.95	1.90	1.85	1.81	1.76	1.72	1.68	1.65	1.61	1·58	1°55	1.52	1°49	1.46
47	2.14	2.08	2.02	1.97	1.92	1.87	1.82	1.78	1.74	1.70	1.67	1·63	1°60	1.57	1°54	1.52
48	2.22	2.16	2.10	2.04	1.99	1.94	1.89	1.85	1.80	1.76	1.73	1·69	1°66	1.63	1°60	1.57
49	2 .30	2.23	2.17	2.11	2.06	2.01	1.96	1.91	1.87	1.83	1.79	1·75	1°72	1.69	1°66	1.63
50	2·38	2.31	2·25	2·19	2°13	2°08	2.03	1.98	1.94	1.89	1.85	1.82	1.78	1.75	1°72	1.69
51	2·47	2.40	2·33	2·27	2°21	2°15	2.10	2.05	2.01	1.96	1.92	1.88	1.85	1.81	1°78	1.75
52	2·56	2.49	2·42	2·35	2°29	2°23	2.18	2.13	2.08	2.03	1.99	1.95	1.91	1.88	1°84	1.81
53	2·65	2.58	2·50	2·44	2°37	2°31	2.26	2.21	2.16	2.11	2.06	2.02	1.98	1.95	1°91	1.88
54	2·7 5	2.67	2·60	2·53	2°46	2°40	2.34	2.29	2.24	2.19	2.14	2.10	2.06	2.02	1°98	1.95
55	2·86	2·77	2·70	2.62	2.55	2°49	2·43	2·37	2·32	2°27	2·22	2·18	2°13	2.09	2°06	2°02
56	2·97	2·88	2·80	2.72	2.65	2°58	2·52	2·46	2·41	2°36	2·31	2·26	2°22	2.17	2°13	2°10
57	3·08	2·99	2·91	2.83	2.75	2°68	2·62	2·56	2·50	2°45	2·40	2·35	2°30	2.26	2°22	2°18
58	3·20	3·11	3·02	2.94	2.86	2°79	2·72	2·66	2·60	2°54	2·49	2·44	2°39	2.35	2°30	2°26
59	3·33	3·23	3·14	3.06	2.98	2°90	2·83	2·77	2·70	2°64	2·59	2·54	2°49	2.44	2°40	2°35
60	3°46	3·36	3 ^{•27}	3.18	3.10	3.02	2.95	2.88	2.81	2.75	2.69	2.64	2.59	2.54	2°49	2°45
61	3°61	3·50	3 ^{•40}	3.31	3.23	3.15	3.07	3.00	2.93	2.87	2.81	2.75	2.70	2.65	2°60	2°55
62	3°76	3·65	3 ^{•55}	3.45	3.36	3.28	3.20	3.13	3.05	2.99	2.93	2.87	2.81	2.76	2°71	2°66
63	3°93	3·81	3 ^{•70}	3.60	3.51	3.42	3.34	3.26	3.19	3.12	3.05	2.99	2.93	2.88	2°83	2°78
64	4°10	3·98	3 ^{•87}	3.76	3.67	3.57	3.49	3.41	3.33	3.26	3.19	3.13	3.06	3.01	2°95	2°90
65	4°29	4°16	4°05	3.94	3.84	3'74	3.65	3.26	3 [•] 48	3.41	3°34	3·27	3·20	3.14	3.09	3.03
66	4°49	4°36	4°24	4.12	4.02	3'92	3.82	3.73	3 [•] 65	3.57	3°49	3·42	3·36	3.29	3.23	3.18
67	4°71	4°57	4°45	4.33	4.21	4'11	4.01	3.91	3 [•] 83	3.74	3°67	3·58	3·52	3.45	3.39	3.33
68	4°95	4°81	4°67	4.54	4.43	4'32	4.21	4.11	4 [•] 02	3.93	3°85	3·77	3·70	3.63	3.56	3.50
69	5°21	5°06	4°92	4.78	4.66	4'54	4.43	4.33	4 [•] 23	4.14	4°05	3·97	3·89	3.82	3.75	3.68
70	5°49	5°33	5°18	5.04	4 ·91	4.79	4°67	4°57	4·46	4°37	4 ^{•27}	4.19	4.11	4.03	3.96	3.89
71	5°81	5°64	5°48	5.33	5·19	5.06	4°94	4°83	4·72	4°61	4 ^{•52}	4.43	4.34	4.26	4.18	4.11
72	6°16	5°98	5°81	5.65	5·50	5.37	5°24	5°11	5·00	4°89	4 ^{•79}	4.69	4.60	4.51	4.43	4.35
73	6°54	6°35	6°17	6.01	5·85	5.70	5°56	5°43	5·31	5°20	5 ^{•09}	4.99	4.89	4.80	4.71	4.63
74	6°97	6°77	6°58	6.40	6·24	6.08	5°93	5°79	5·66	5°5 4	5 ^{•43}	5.32	5.21	5.11	5.02	4.93
75	7'46	7:25	7.04	6·85	6.67	6·51	6·35	6·20	6.06	5:93	5.81	5.69	5·58	5.47	5·37	5 ^{.28}
76	8'02	7:79	7.57	7·36	7.17	6·99	6·82	6·66	6.51	6:37	6.24	6.11	5·99	5.88	5·77	5 ^{.67}
77	8'66	8:41	8.17	7·95	7.75	7·55	7·37	7·20	7.04	6:88	6.74	6.60	6·47	6.35	6·24	6 ^{.13}
78	9'41	9:13	8.88	8·64	8.41	8·20	8·00	7·82	7.64	7:4 ⁸	7.32	7.17	7·03	6.90	6·77	6 ^{.65}
79	10' 3	9:99	9.71	9·45	9.20	8·97	8·75	8·55	8.36	8:17	8.00	7.84	7·69	7.54	7 ·4 ¹	7 ^{.28}
80	11.3	11.0	10.7	10'4	10°1	9 [.] 89	9.65	9.42	9.21	9.01	8.82	8.64	8·48	8·32	8.16	8.02
81	12.6	12.3	11.9	11'6	11°3	11 ^{.0}	10.7	10.5	10.3	10.0	9.82	9.62	9·44	9·26	9.09	8.93
82	14.2	13.8	13.4	13'1	12°7	12 [.] 4	12.1	11.8	11.6	11.3	11.1	10.8	10·6	10·4	10.2	10.1
83	16.3	15.8	15.4	15'0	14°6	14 ^{.2}	13.9	13.5	13.2	12.9	12.7	12.4	12·2	11·9	11.7	11.5
84	19.0	18.5	18.0	17'5	17°0	16 ^{.6}	16.2	15.8	15.5	15.1	14.8	14.5	14·2	14·0	13.7	13.5
85	22.9	22.2	21.6	21'0	20°4	19 [.] 9	19.4	19.0	18.6	18.2	17.8	17.4	17·1	16·8	16.5	16.2
1	m. 00	m.	m.	m.	m.	m.	m. 36	m.	m. 28	m.	m. 20	m. 16	m. 12	m. 8	m. 4	m. 00
	10 Hrs.		<u>*, 1</u>	1 40	1 44	- 40		9 HOU	JRS.	1 -4			<u> </u>		. 4	

31 Table B.

ttion.							3	ноц	RS.	AND CONTRACTOR						4 Hrs.
Declina	m.	m.	m.	m.												
	00	4	8	12	16	20	24	28	32	36	40	44	48	52	56	00
° 30 31 32 33 34	·82 ·85 ·88 ·92 ·95	·80 ·84 ·87 ·90 ·94	*79 •82 •85 •89 •92	·78 ·81 ·84 ·87 ·91	·76 ·80 ·83 ·86 ·89	*75 *78 *82 *85 *85	·74 ·77 ·80 ·84 ·87	·73 ·76 ·79 ·82 ·86	·72 ·75 ·78 ·81 ·84	·71 ·74 ·77 ·80 ·83	·70 ·73 ·76 ·79 •82	*70 *72 *75 *75 *78	•69 •72 •75 •75 •77 •80	·68 ·71 ·74 ·77 ·80	·67 ·70 ·73 ·76 ·79	· ·67 ·69 ·72 ·75 ·78
35 36 37 38 39	.99 1.03 1.10 1.10	.97 1.01 1.05 1.09 1.13	·96 ·99 1·03 1·07 1·11	·94 ·98 1·01 1·05 1·09	.93 .96 1.00 1.04 1.07	'91 '95 '98 1'02 1'06	•90 •93 •97 1•01 1•04	·89 ·92 ·96 ·99 1·03	88 91 94 98 1 01	•87 •90 •93 •97 1•00	*85 *89 *92 *95 *99	- 84 -88 -91 -94 -98	•83 •87 •90 •93 •97	·83 ·86 ·89 ·92 ·95	·82 ·85 ·88 ·91 ·94	•81 •84 •87 •90 •94
40 41 42 43 44	1.19 1.23 1.32 1.32 1.37	1°17 1°21 1°25 1°30 1°34	1.15 1.19 1.23 1.28 1.32	1.13 1.17 1.25 1.30	1.11 1.15 1.19 1.24 1.28	1.10 1.13 1.18 1.22 1.26	1 08 1 12 1 16 1 20 1 24	1.00 1.10 1.14 1.18 1.23	1.05 1.09 1.13 1.17 1.21	1.04 1.07 1.11 1.15 1.19	1.02 1.06 1.10 1.14 1.18	1.01 1.02 1.03 1.12 1.16	1.00 1.04 1.07 1.11 1.15	.99 1.03 1.06 1.10 1.14	·98 1·01 1·05 1·09 1·13	·97 1·00 1·04 1·08 1·12
45 46 47 48 49	1.41 1.46 1.52 1.57 1.63	1.39 1.44 1.49 1.54 1.60	1'37 1'42 1'47 1'52 1'57	1°35 1°39 1°44 1°49 1°55	1°33 1°37 1°42 1°47 1°52	1°31 1°35 1°40 1°45 1°50	1,53 1,33 1,38 1,43 1,48	1 27 1 31 1 36 1 41 1 46	1.25 1.30 1.34 1.39 1.44	1.24 1.28 1.33 1.37 1.42	1.55 1.56 1.31 1.36 1.40	1.21 1.25 1.39 1.34 1.39	1.19 1.23 1.32 1.37	1.18 1.22 1.31 1.36	1°17 1°21 1°25 1°30 1°34	1·15 1 20 1·24 1·28 1·33
50	1.69	1.66	1.63	1.60	1.58	1.26	1.23	1.51	1.49	1°47	1°45	1.44	1.42	1.41	1.39	1,38
51	1.75	1.72	1.69	1.66	1.64	1.61	1.29	1.57	1.55	1°53	1°51	1.49	1.47	1.46	1.44	1,43
52	1.81	1.78	1.75	1.72	1.70	1.67	1.65	1.62	1.60	1°58	1°56	1.54	1.53	1.51	1.49	1,48
53	1.88	1.84	1.81	1.79	1.76	1.73	1.71	1.68	1.66	1°64	1°62	1.60	1.58	1.56	1.55	1,53
54	1.95	1.91	1.88	1.85	1.82	1.80	1.77	1.75	1.72	1°70	1°68	1.66	1.64	1.62	1.61	1,59
55	2.02	1'99	1'95	1.92	1.89	1.86	1 84	1 81	1 79	1.77	1.24	1.72	1.70	1.68	1.67	1.65
56	2.10	2'06	2'03	1.99	1.96	1.94	1 91	1 88	1 86	1.83	1.81	1.79	1.77	1.75	1.73	1.71
57	2.18	2'14	2'11	2.07	2.04	2.01	1 98	1 95	1 93	1.90	1.88	1.86	1.84	1.82	1.80	1.78
58	2.26	2'22	2'19	2.15	2.12	2.09	2 06	2 03	2 0	1.98	1.95	1.93	1.91	1.89	1.87	1.85
59	2.35	2'31	2'28	2.24	2.21	2.17	2 14	2 11	2 08	2.06	2.03	2.01	1.98	1.96	1.94	1.92
60	2.45	2°41	2°37	2°33	2`29	2°26	2°23	2°20	2.17	2°14	2°11	2.09	2.07	2.04	2.02	2.00
61	2.55	2°51	2°47	2°43	2`39	2°36	2°32	2°29	2.26	2°23	2°20	2.18	2.15	2.13	2.10	2.08
62	2.66	2°61	2°57	2°53	2`49	2°46	2°42	2°39	2.35	2°32	2°30	2.27	2.24	2.22	2.19	2.17
63	2.78	2°73	2°68	2°64	2`60	2°56	2°53	2°49	2.46	2°43	2°40	2.37	2.34	2.31	2.29	2.27
64	2.90	2°85	2°80	2°76	2`72	2°68	2°64	2°60	2.57	2°53	2°50	2.47	2.44	2.42	2.39	2.37
65	3.03	2.98	2·93	2·89	2.84	2.80	2·76	2·72	2.69	2.65	2.62	2°59	2·56	2·53	2.50	2·48
66	3.18	3.12	3·07	3·02	2.98	2.93	2·89	2·85	2.81	2.78	2.74	2°71	2·68	2·65	2.62	2·59
67	3.33	3.28	3·22	3·17	3.12	3.08	3·03	2·99	2.95	2.91	2.88	2°84	2·81	2·78	2.75	2·72
68	3.50	3.44	3·38	3·33	3.28	3.23	3·18	3·14	3.10	3.06	3.02	2°99	2·95	2·92	2.89	2·86
69	3.68	3.62	3·56	3·51	3.45	3.40	3·35	3·31	3.26	3.22	3.18	3°14	3·11	3·07	3.04	3·01
70	3 ^{.89}	3·82	3.76	3.70	3.64	3°59	3*54	3.49	3°44	3.40	3*35	3·31	3·28	3.24	3.21	3·17
71	4 ^{.11}	4·04	3.97	3.91	3.85	3'79	3*74	3.69	3°64	3.59	3*55	3·50	3·46	3.42	3.39	3·35
72	4 ^{.35}	4·28	4.21	4.14	4.08	4'02	3*96	3.91	3°85	3.80	3*76	3·71	3·67	3.63	3.59	3·55
73	4 ^{.63}	4·55	4.47	4.40	4.33	4'27	4*21	4.15	4°10	4.04	3*99	3'95	3·90	3.86	3.82	3·78
74	4 ^{.93}	4·85	4.77	4.69	4.62	4'55	4*49	4.43	4°37	4.31	4*26	4·21	4·16	4.11	4.07	4· 0 3
75	5 ^{.28}	5°19	5·10	5.02	4°95	4 ^{.8} 7	4·80	4.74	4 ^{.6} 7	4.96	4°56	4°50	4°45	4°40	4°35	4·31
76	5 ^{.6} 7	5°58	5·48	5.40	5°31	5 ^{.24}	5·16	5.09	5 [.] 02	4.96	4'90	4°84	4'78	4°73	4°68	4·63
77	6 ^{.13}	6°02	5·92	5.83	5°74	5 ^{.65}	5·57	5.50	5 [.] 42	5.35	5'29	5°22	5'16	5°11	5°05	5·00
78	6 ^{.65}	6°54	6·43	6.33	6°23	6 ^{.14}	6·05	5.97	5 ^{.89}	5.82	5'74	5°67	5'61	5°55	5°49	5·43
79	7 .2 8	7°15	7·03	6.92	6°82	6 ^{.72}	6·62	6.53	6 [.] 44	6.36	6'28	6°21	6'13	6°07	6°00	5·94
80	8.02	7 ^{.88}	7'75	7 ^{.6} 3	7.51	7'40	7.30	7.20	7'10	7.01	6·92	6.84	6.76	6.69	6.62	6.55
81	8.93	8 ^{.78}	8'63	8 ^{.50}	8.37	8'24	8.12	8.01	7'91	7.80	7·71	7.62	7.53	7.45	7.37	7.29
82	10.1	9 ^{.89}	9'73	9 ^{.57}	9.43	9'29	9.16	9.03	8'91	8.80	8·69	8.58	8.48	8.39	8.30	8.22
83	11.5	11 ^{.3}	11'1	11 ^{.0}	10.8	10'6	10.5	10.3	10'2	10.1	9·94	9.82	9.71	9.60	9.50	9.40
84	13.5	13 ^{.2}	13'0	12 ^{.8}	12.6	12'4	12.2	12.1	11'9	11.8	11·6	11.5	11.3	11.2	11.1	11.0
85	16.2	15 ^{.9}	15'6	15 ^{.4}	15.1	14'9	14.7	14.5	14'3	14.1	14·0	13.8	13.6	13.5	13.3	13.2
	m. 00 9 Hrs.	m. 56	m. 52	m. 48	m. 44	m. 40	m. 36	m. 32	m. 28 RS.	m. 24	m. 20	m. 16	m. 12	m. 8	m. 4	m. 00

32 Table B.

Always name the factors taken from Table B the same as the name of declination.

tion.							4	HOU	RS.							5 Hrs.
Declina	m.	т.	m.	m.	m.	m.	m.	m.								
	00	4	8	12	16	20	24	28	32	36	40	44	48	52	56	00
° 30 31 32 33 34	, .69 .72 .75 .78	·66 ·69 ·71 ·74 ·77	·65 ·68 ·71 ·74 ·76	·65 ·67 ·70 ·73 ·76	·64 ·67 ·70 ·72 ·75	·64 ·66 ·69 ·72 ·74	·63 ·66 ·68 ·71 ·74	·63 ·65 ·68 ·71 ·73	·62 ·65 ·67 ·70 ·73	·62 ·64 ·67 ·70 ·72	·61 ·64 ·66 ·69 ·72	·61 ·64 ·66 ·69 ·71	·61 ·63 ·66 ·68 ·71	·60 ·63 ·65 ·68 ·71	• 60 •63 •65 •68 •70	·60 ·62 ·65 ·67 ·70
35	·81	•80	·79	•79	·78	·77	·77	·76	·76	·75	*75	`74	·74	·73	·73	·72
36	·84	•83	·82	•82	·81	·80	·80	·79	·78	·78	*77	'77	·76	·76	·76	·75
37	·87	•86	·85	•85	·84	·83	·82	·82	·81	·81	*80	'80	·79	·79	·78	·78
38	·90	•89	·88	•88	·87	·86	·86	·85	·84	·84	*83	'83	·82	·82	·81	·81
39	·94	•93	·92	•91	·90	·89	·86	·85	·87	·87	*86	'86	·85	·85	·84	·84
40	'97	.96	·95	.94	.93	·93	.92	·91	.90	.90	.89	·89	·88	·88	·87	·87
41	1'00	.99	·98	.98	.97	·96	.95	·94	.94	.93	93	·92	·91	·91	·90	·90
42	1'04	1.03	1·02	1.01	1.0 0	·99	.99	·98	.97	.96	96	·95	·95	·94	·94	·93
43	1'08	1.07	1·06	1.05	1.04	1·03	1.02	1·01	1.01	1.00	.99	·99	·98	·98	·97	·97
44	1'12	1.10	1·09	1.08	1.07	1·07	1.06	1 ·05	1.04	1.03	1.03	1·02	1·02	1·01	1·00	1·00
45	1.15	1.14	1'13	1°12	1°11	1.10	1.09	1.09	1.08	1.07	1.06	1.06	1.05	1.05	1.04	1.04
46	1.20	1.18	1'17	1°16	1°15	1.14	1.13	1.12	1.12	1.11	1.10	1.10	1.09	1.08	1.08	1.07
47	1.24	1.23	1'21	1°20	1°19	1.18	1.17	1.16	1.16	1.15	1.14	1.13	1.13	1.12	1.12	1.11
48	1.28	1.27	1'26	1°25	1°24	1.23	1.22	1.21	1.20	1.19	1.18	1.17	1.17	1.16	1.16	1.15
49	1.33	1.32	1'30	1°29	1°28	1.27	1.26	1.25	1.24	1.23	1.22	1.22	1.21	1.20	1.20	1.19
50 51 52 53 54	1.38 1.43 1.48 1.53 1.59	1·36 1·41 1·46 1·52 1·57	1°35 1°40 1°45 1°50 1°56	1°34 1°39 1°44 1°49 1°54	1.33 1.37 1.42 1.48 1.53	1.31 1.36 1.41 1.46 1.52	1·30 1·35 1·40 1·45 1·51	1°29 1°34 1°39 1°44 1°50	1·29 1·33 1·38 1·43 1·43 1·48	1.28 1.32 1.37 1.42 1.47	1.27 1.31 1.36 1.41 1.46	1·26 1·31 1·35 1·40 1·46	1·25 1·30 1·35 1·40 1·45	1·25 1·29 1·34 1·39 1·44	1.24 1.28 1.33 1.38 1.43	1.53 1.33 1.37 1.42
55	1.65	1.63	1.62	1.60	1.29	1°58	1.56	1.55	1°54	1.23	1.22	1.21	1.50	1°49	1°49	1.48
56	1.71	1.70	1.68	1.66	1.65	1'64	1.62	1.61	1°60	1.29	1.28	1.22	1.56	1°55	1°54	1.53
57	1.78	1.76	1.74	1.73	1.71	1'70	1.69	1.67	1°66	1.65	1.64	1.63	1.62	1°61	1 60	1.59
58	1.85	1.83	1.81	1.80	1.78	1'77	1.75	1.74	1°73	1.71	1.70	1.69	1.68	1°67	1°66	1.66
59	1.92	1.90	1.88	1.87	1.85	1'84	1.82	1.81	1°79	1.78	1.77	1.76	1.75	1°74	1°73	1.72
бо	2.00	1.98	1.96	1 ·94	1.93	1.91	1.90	1.88	1.87	1.86	1.84	1.83	1.82	1.81	1.80	1.79
б1	2.08	2.06	2.04	2 ·02	2.01	1.99	1.97	1.96	1.95	1.93	1.92	1.91	1.90	1.89	1.88	1.87
б2	2.17	2.15	2.13	2 · 11	2.09	2.08	2.06	2.04	2.03	2.01	2.00	1.99	1.98	1.97	1.96	1.95
63	2.27	2.24	2.22	2 · 20	2.18	2.17	2.15	2.13	2.12	2.10	2.09	2.08	2.06	2.05	2.04	2.03
64	2.37	2.34	2.32	2 · 30	2.28	2.26	2.24	2.23	2.21	2.20	2.18	2.17	2.16	2.14	2.13	2.12
65	2°48	2°45	2.43	2·41	2.39	2°37	2·35	2·33	2·31	2.30	2·28	2·27	2°25	2·24	2°23	2·22
66	2°59	2°57	2.54	2·52	2.50	2°48	2·46	2·44	2·42	2.41	2·39	2·38	2°36	2·35	2°34	2·33
67	2°72	2°69	2.67	2·64	2.62	2°60	2·58	2·56	2·54	2.52	2·51	2·49	2°48	2·46	2°45	2·44
68	2°86	2°83	2.80	2·78	2.75	2°73	2·71	2·69	2·67	2.65	2·63	2·62	2°60	2·59	2°57	2·56
69	3°01	2°98	2.95	2·92	2.90	2°87	2·85	2·83	2·81	2.79	2·77	2·76	2°74	2·72	2°71	2·70
70	3 ^{.17}	3 ^{.14}	3.11	3.08	3.06	3.03	3.01	2·98	2·96	2·94	2·92	2·91	2·89	2·87	2·86	2·84
71	3 ^{.35}	3 ^{.32}	3.29	3.26	3.23	3.20	3.18	3·16	3·13	3·11	3·09	3·07	3·05	3·04	3·02	3·01
72	3 ^{.55}	3 ^{.52}	3.49	3.45	3.42	3.40	3.37	3·34	3·32	3·30	3·28	3·26	3·24	3·22	3·20	3·19
73	3 ^{.78}	3 ^{.74}	3.70	3.67	3.64	3.61	3.58	3·55	3·53	3·50	3·48	3·46	3·44	3·42	3·40	3·39
74	4 ^{.03}	3 ^{.99}	3.95	3.91	3.88	3.85	3.82	3·79	3·76	3·74	3·71	3·69	3·67	3·65	3·63	3·61
75	4·31	4°27	4°23	4·19	4°15	4.12	4.09	4.05	4.03	4.00	3 [.] 97	3 [.] 95	3·92	3·90	3 ^{.88}	3.86
76	4·63	4°59	4°54	4·50	4°46	4.43	4.39	4.36	4.33	4.30	4 [.] 27	4 [.] 24	4·22	4·19	4 ^{.17}	4.15
77	5·00	4°95	4°91	4·86	4°82	4.78	4.74	4.71	4.67	4.64	4 [.] 61	4 [.] 58	4·55	4·53	4 ^{.51}	4.48
78	5·43	5°38	5°33	5·28	5°23	5.19	5.15	5.11	5.07	5.04	5 [.] 01	4 [.] 98	4·95	4·92	4 ^{.89}	4.87
79	5·94	5°88	5°83	5·77	5°72	5.68	5.63	5.59	5.55	5.51	5 [.] 47	5 [.] 44	5·41	5·38	5 ^{.35}	5.33
80	6·55	6.48	6.42	6.37	6·31	6·26	6.21	6.16	6.12	6.07	6.04	6.00	5.96	5.93	5.90	5 ^{.87}
81	7·29	7.22	7.15	7.09	7·02	6·97	6.91	6.86	6.81	6.76	6.72	6.68	6.64	6.60	6.57	6 ^{.54}
82	8·22	8.14	8.06	7.99	7·92	7·85	7.79	7.73	7.67	7.62	7.57	7.53	7.48	7.44	7.40	7 ^{.37}
83	9·40	9.31	9.22	9.14	9·06	8·99	8.92	8.85	8.78	8.72	8.67	8.61	8.56	8.52	8.47	8 ^{.43}
84	11·0	10.9	10.8	10.7	10·6	10·5	10.4	10.3	10.3	10.2	10.1	10.1	10.0	9.95	9.90	9 ^{.85}
85	13·2	13.1	12.9	12.8	12·7	12·6	12.5	12.4	12.3	12.2	12.2	12.1	12.0	12.0	11.9	11 ^{.8}
	m. 00 8 Hrs.	m. 56	m. 52	m. 48	m. 44	m. 40	m. 36 7	m. 32 HOU	m. 28 RS.	m. 24	m. 20	m. 16	m. 12	m. 8	m. 4	m. 00

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Table B.

ion.							5	ноц	RS.				- or ac			6 Hrs.
Declinati	m.	m.	m.	m.	m.	m.	m.									
	00	4	8	12	16	20	24	28	32	36	40	44	48	52	56	00
o 30 31 32 33 34	·60 ·62 ·65 ·67 ·70	·60 ·62 ·64 ·67 ·70	·59 ·62 ·64 ·67 ·69	·59 ·61 ·64 ·66 ·69	, 59 61 64 66 .66	·59 ·61 ·63 ·66 ·68	·58 ·61 ·63 ·66 ·68	·58 ·61 ·63 ·66 ·68	·58 ·61 ·63 ·65 ·68	·58 ·60 ·63 ·65 ·68	, .60 .63 .65 .68	, -60 -63 -65 -68	, -60 -63 -65 -68	·58 ·60 ·63 ·65 ·67	·58 ·60 ·62 ·65 ·67	58 60 62 65 67
35	·72	·72	•72	•72	·71	·71	·71	·71	·71	·70	·70	·70	•70	•70	70	·70
36	·75	·75	•75	•74	·74	·74	·74	·73	·73	·73	·73	·73	•73	•73	73	·73
37	·78	·78	•77	•77	·77	·77	·76	·76	·76	·76	·76	·76	•75	•75	75	·75
38	·81	·81	•80	•80	·80	·79	·79	·79	·79	·79	·78	·78	•78	•78	78	·78
39	·84	·83	•83	•83	·82	·82	·82	·82	·82	·81	·81	·81	•81	•81	81	·81
40	•87	•86	•86	·86	·85	·85	·85	·85	•85	·84	·84	•84	·84	^{.8} 4	·84	•84
41	•90	•90	•89	·89	·89	·88	·88	·88	•88	·87	·87	•87	·87	.87	·87	•87
42	•93	•93	•92	·92	·92	·91	·91	·91	•91	·91	·90	•90	·90	.90	·90	•90
43	•97	•96	•96	·95	·95	·95	·94	·94	•94	·94	·94	•93	·93	.93	·93	•93
44	•97	••00	•99	·99	·98	·98	·98	·98	•97	·97	·97	•97	·97	.97	·97	•97
45	1.04	1.03	1.03	1.02	1.02	1.02	1.01	1.01	1.01	1.01	1.00	1.00	1.00	1.00	1.00	1°00
46	1.07	1.07	1.06	1.06	1.05	1.05	1.02	1.05	1.04	1.04	1.04	1.04	1.04	1.04	1.04	1°04
47	1.11	1.11	1.10	1.10	1.09	1.09	1.09	1.08	1.08	1.08	1.08	1.07	1.07	1.07	1.07	1°07
48	1.15	1.14	1.14	1.14	1.13	1.13	1.12	1.12	1.12	1.12	1.11	1.11	1.11	1.11	1.11	1°11
49	1.19	1.19	1.18	1.18	1.17	1.17	1.16	1.16	1.16	1.16	1.15	1.15	1.15	1.15	1.15	1°15
50 51 52 53 54	1'23 1'28 1'33 1'37 1'42	1.23 1.27 1.32 1.37 1.42	1·22 1·27 1·31 1·36 1·41	1·22 1·26 1·31 1·36 1·41	1°21 1°26 1°30 1°35 1°40	1°21 1°25 1°30 1°35 1°40	1.21 1.25 1.30 1.34 1.39	1.20 1.25 1.29 1.34 1.39	1.20 1.24 1.29 1.34 1.39	1 ·20 1·24 1·29 1·33 1·38	1.20 1.24 1.33 1.38 1.38	1.19 1.24 1.28 1.33 1.38	1°19 1°24 1°28 1°33 1°38	1.19 1.24 1.28 1.33 1.38	1.19 1.24 1.33 1.38	1.19 1.23 1.33 1.38 1.38
55	1.48	1°47	1.47	1.46	1°45	1`45	1°45	1°44	1'44	1°44	1'43	1°43	1.43	1.43	1°43	1°43
56	1.53	1°53	1.52	1.52	1°51	1`51	1°50	1°50	1'49	1°49	1'49	1°49	1.48	1.48	1°48	1°48
57	1.59	1°59	1.58	1.57	1°57	1`56	1°56	1°55	1'55	1°55	1'55	1°54	1.54	1.54	1°54	1°54
58	1.66	1°65	1.64	1.64	1°63	1`63	1°62	1°62	1'61	1°61	1'61	1°60	1.60	1.60	1°60	1°60
59	1.72	1°72	1.71	1.70	1°70	1`69	1°69	1°68	1'68	1°67	1'67	1°67	1.67	1.67	1°66	1°66
60	1.79	1.79	1.78	1.77	1°76	1.76	1.75	1.75	1.75	1.74	1.74	1.74	1.73	1.73	1.73	1.73
61	1.87	1.86	1.85	1.84	1°84	1.83	1.83	1.82	1.82	1.81	1.81	1.81	1.81	1.81	1.80	1.80
62	1.95	1.94	1.93	1.92	1'92	1.91	1.90	1.90	1.89	1.89	1.89	1.89	1.88	1.88	1.88	1.88
63	2.03	2.02	2.01	2.01	2.00	1.99	1.99	1.98	1.98	1.97	1.97	1.97	1.97	1.96	1.96	1.96
64	2.12	2.11	2.10	2.10	2'09	2.08	2.08	2.07	2.07	2.06	2.06	2.06	2.05	2.05	2.05	2.05
65	2·22	2.21	2°20	2°19	2°18	2.18	2·17	2.17	2.16	2°16	2°15	2.15	2·15	2°15	2.14	2°14
66	2·33	2.31	2°31	2°30	2°29	2.28	2·27	2.27	2.26	2°26	2°25	2.25	2·25	2°25	2.25	2°25
67	2·44	2.43	2°42	2°41	2°40	2.39	2·39	2.38	2.37	2°37	2°36	2.36	2·36	2°36	2.36	2°36
68	2·56	2.55	2°54	2°53	2°52	2.51	2·51	2.50	2.49	2°49	2°48	2.48	2·48	2°48	2.48	2°48
69	2·70	2.68	2°67	2°66	2°65	2.65	2·64	2.63	2.62	2°62	2°62	2.61	2·61	2°61	2.61	2°61
70	2·84	2·83	2·82	2.81	2·80	2.79	2·78	2·77	2.77	2.76	2·76	2.75	2.75	2·75	2·75	2`75
71	3·01	2·99	2·98	2.97	2·96	2.95	2·94	2·93	2.93	2.92	2·92	2.91	2.91	2·91	2·90	2`90
72	3·19	3·17	3·16	3.15	3·14	3.13	3·12	3·11	3.10	3.09	3·09	3.09	3.08	3·08	3·08	3`08
73	3·39	3·37	3·36	3.34	3·33	3.32	3·31	3·30	3.30	3.29	3·28	3.28	3.28	3·27	3·27	3`27
74	3·61	3·59	3·58	3.57	3·55	3.54	3·53	3·52	3.51	3.51	3·50	3.50	3.49	3·49	3·49	3`49
75	3 ^{.86}	3 ^{.85}	3.83	3.82	3 ^{.80}	3'79	3'78	3 [.] 77	3°76	3 ·75	3'75	3'74	3'74	3.73	3'73	3'73
76	4 ^{.15}	4 ^{.13}	4.12	4.10	4 ^{.09}	4'07	4'06	4 ^{.05}	4°04	4·03	4'03	4'02	4'02	4.01	4'01	4'01
77	4 ^{.48}	4 ^{.46}	4.45	4.43	4 ^{.41}	4'40	4'39	4 [.] 37	4°36	4·36	4'35	4'34	4'34	4.33	4'33	4'33
78	4 ^{.87}	4 ^{.85}	4.83	4.81	4 ^{.79}	4'78	4'76	4 [.] 75	4°74	4·73	4'72	4'72	4'71	4.71	4'71	4'70
79	5 [.] 33	5 ^{.30}	5.28	5.26	5 ^{.24}	5'22	5'21	5 [.] 20	5°18	5·17	5'16	5'16	5'15	5.15	5'15	5'14
80	5.87	5.84	5.82	5.80	5.78	5.76	5'74	5.73	5.71	5'70	5.69	5.69	5.68	5.67	5.67	5.67
81	6.54	6.51	6.48	6.45	6.43	6.41	6'39	6.38	6.36	6'35	6.34	6.33	6.32	6.32	6.31	6.31
82	7.37	7.33	7.30	7.27	7.25	7.23	7'20	7.19	7.17	7'15	7.14	7.13	7.13	7.12	7.12	7.12
83	8.43	8.39	8.36	8.33	8.30	8.27	8'25	8.22	8.21	8'19	8.18	8.16	8.16	8.15	8.15	8.14
84	9.85	9.81	9.76	9.73	9.69	9.66	9'63	9.61	9.59	9'57	9.55	9.54	9.53	9.52	9.52	9.51
85	11.83	11.78	11.73	11.69	11.64	11.61	11'57	11.54	11.52	11'49	11.47	11.46	11.45	11.44	11.43	11.43
	m.	m.	m.	m.	m.	m.	m,									
	00	56	52	48	44	40	36	32	28	24	20	16	12	8	4	00

6 HOURS.

10-11. D.d ~

7 Hrs. 3-Azimuth. 34 Table A.

When hour angle is less than 6 hours, name the factors taken from Table A contrary to name of lat.

نہ							0	HOU	JR.							
La	m. 1	m. 4	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 60
85 85 86 86 86 87 87 87	2620 2912 3277 3747 4373 5259	655 728 819 937 1093 1312	, 327 364 410 468 546 656	218 243 273 312 364 437	163 182 205 234 273 328	, 131 145 164 187 218 262	í 09 121 136 156 182 218	93·1 104 117 133 155 187	81.3 90.4 102 116 136 163	72·2 80·2 90·3 103 121 145	64.8 72.1 81.1 92.7 108 130	58.8 65.4 73.6 84.1 98.2 118	53.8 59.8 67.3 76.9 89.8 108	, 49·5 55·0 62·0 70·8 82·6 99·2	, 45·8 51·0 57·4 65·6 76·5 91·9	42·7 47·4 53·4 61·0 71·2 85·5
$88\frac{1}{2}$ 89 89 $39\frac{1}{2}$	8752 13129 26261	2188 3282 6565	1094 1641 3281	729 1093 2186	546 819 1639	436 655 1310	273 363 545 1090	233 311 467 933	204 272 408 815	241 362 723	217 325 650	196 295 590	135 180 270 539	124 165 248 496	115 153 230 460	107 143 214 428
	m. 59	m. 56	m. 52	m. 48	m. 44	m. 40	т. 3б	m. 32	m. 28	m. 24	m. 20	m. 16	m. 12	m. 8	m. 4	m. o
							11	HOU	JRS.							

							1	НО	UR.							
Lat	m.	m.	m.	m.	m.	m.	m.	m.	т.	m.						
	0	4	8	12	16	20	24	28	32	36	40	44	48	52	56	60
	, 42:7 47:4 53:4 61:0 71:2 85:5 107	39·9 44·3 49·9 57·0 66·5 79·9 99·9	37.4 41.6 46.8 53.5 62.4 74.9 93.7	35·2 39·1 44·0 50·3 58·7 70·5 88·1	33.2 36.9 41.5 47.5 55.4 66.5 83.2	, 31·4 34·9 39·3 44·9 52·4 62·9 78·7	29.8 33.1 37.3 42.6 49.7 59.7 74.6	28·3 31·4 35·4 40·5 47·2 56·7 70·9	26.9 29.9 33.7 38.5 45.0 54.0 67.5	25.7 28.5 32.1 36.7 42.9 51.4 64.3	24.5 27.2 30.7 35.1 40.9 49.1 61.4	23·4 26·1 29·3 33·5 39·1 47·0 58·7	22·4 24·9 28·1 32·1 37·4 45·0 56·2	21·5 23·9 26·9 30·7 35·9 43·1 53·9	20.6 22.9 25.8 29.5 34.4 41.3 51.7	19.8 22.0 24.8 28.3 33.0 39.7 49.6
$ \begin{array}{r} 88\frac{1}{2} \\ 89 \\ \cdot 89\frac{1}{2} \end{array} $	143	133	125	118	111	105	99·5	94·5	90·0	85·8	81·9	78·3	74·9	71·8	68·9	66•1
	214	200	187	176	166	157	149	142	135	129	123	117	112	108	103	99•2
	428	400	375	353	333	315	299	284	270	257	246	235	225	216	207	198
	т.	т.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	бо	5б	52	48	44	40	36	32	28	24	20	16	12	8	4	o
							10	HO	TIRS							

					and an and a second second		2	HO	URS.							
Lat	m.	m.	m.	m.	m.	m.										
	0	4	8	12	16	20	24	28	32	86	40	44	48	52	56	60
	19·8 22·0 24·8 28·3	19.0 21.1 23.8 27.2	18·3 20·3 22·9 26·2	17·6 19·6 22·0 25·2	16·9 18·8 21·2 24·2	16·3 18·2 20·4 23·4	15.7 17.5 19.7 22.5	15·2 16·9 19·0 21·7	14.6 16.3 18.3 20.9	14·1 15·7 17·7 20·2	, 13·6 15·1 17·0 19·5	13·1 14·6 16·5 18·8	, 12·7 14·1 15·9 18·2	12·3 13·6 15·3 17·5	11.8 13.2 14.8 16.9	11·4 12·7 14·3 16·3
87	33·0	31.8	30·5	29·4	28·3	27·3	26·3	25·3	24·4	23·6	22·7	22·0	21·2	20·5	19·8	19·1
87 ¹	39·7	38.1	36·7	35·3	34·0	32·7	31·5	30·4	29·3	28·3	27·3	26·3	25·4	24·6	23·7	22·9
88	49·6	47.7	45·8	44·1	42·5	40·9	39·4	38·0	36·7	35 [.] 4	34·1	32·9	31·8	30·7	29·7	28·6
88½	66-1	63·6	61·1	58·8	56·6	54 [.] 5	52·6	50·7	48·9	47·2	45 [.] 5	43·9	42·4	41.0	39·5	38·2
89	99-2	95·3	91·7	88·2	84·9	81.8	78·9	76·0	73·3	70·7	68.3	65·9	63·6	61.4	59·3	57·3
89½	198	191	183	176	170	164	158	152	147	142	137	132	127	123	119	115
	m.	m.	m.	m.	m.	m ,										
	60	56	52	48	44	40	36	32	28	24	20	16	12	8	4	o - ,
							9	HOU	JRS.							_

When hour angle is more than 6 hours, name the factors taken from Table A the same as the name of the latitude.

- 52	25
	le J
0	

Table B.

na- 1.							0	нои	RS.							
Decli	m.	m.	m.	m.	m.	m.	т.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	1	4	8	12	16	20	24	28	32	36	40	44	4 8	52	56	60
$85 \frac{1}{2}$ 85 $\frac{1}{2}$ 86 $\frac{1}{2}$	2620 2912 3277 3747	655 728 819 937	, 328 364 410 468	218 243 273 312	164 182 205 234	í31 146 164 188	, 109 122 137 156	93.8 104 117 134	82·1 91·3 103 117	73·1 81·2 91·4 105	65.8 73.2 82.4 94.2	, 59·9 66·6 74·9 85·7	55.0 61.1 68.8 78.6	50·8 56·5 63·6 72·7	47·2 52·5 59·1 67·6	44·2 49·1 55·3 63·2
87	4373	1093	547	365	274	219	183	157	137	122	110	100	91·8	84·8	78·9	73 [.] 7
871	5259	1312	656	438	328	263	219	188	165	146	132	120	110	102	94·7	88.5
88	6563	1641	821	547	411	329	274	235	206	183	165	150	138	127	118	111
	8752	2188	1094	730	547	438	365	313	274	244	220	200	184	170	158	148
	13129	3283	1642	1095	821	657	548	470	412	366	330	300	276	255	237	221
	26261	6566	3283	2190	1643	1315	1096	940	823	733	660	601	551	509	474	443
	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	59	56	52	48	44	40	36	32	28	24	20	16	12	8	4	o
	-						11	но	URS.							

na- 1.							1	HOU	JR.							
Declin	m. 0	m. 4	ın. 8	m. 12	m 16	т. 2)	m. 24	m. 28	m. 3 2	m. 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 60
	44·2 49·1 55·3 63·2	41.5 46.1 51.9 59.3	, 39·1 43·5 48·9 55·9	37·0 41·1 46·3 52·9	, 35·I 39·0 43·9 50·2	, 33·4 37·2 41·8 47·8	31.9 35.5 39.9 45.6	30.5 33.9 38.2 43.6	29·3 32·5 36·6 41·8	28·1 31·2 35·2 40·2	27·0 30·1 33·8 38·7	26·1 29·0 32·6 37·3	25·2 28·0 31·5 36·0	, 24·3 27·1 30·5 34·8	23.6 26.2 29.5 33.7	22.9 25.4 28.6 32.7
87 871 88	73·7 88·5 111	69·2 83·1 104	65·3 78·3 97·9	61·7 74·1 92·7	58∙6 70∙4 88∙0	55·8 67·0 83·7	53·2 63·9 79·9	50·9 61·1 7 ^{6·} 4	48·8 58·6 73·3	46·9 56·3 70·4	45·1 54·2 67·8	43·5 52·2 65·3	42·0 50·4 63·1	40.6 48.8 61.0	39·4 47·2 59·1	38·2 45·8 57·3
88 <u>1</u> 89 89 <u>1</u> 89 <u>1</u>	148 -221 443	139 208 416	131 196 392	124 185 371	117 176 352	112 168 33 5	107 160 320	102 153 306	97·7 147 293	93 [.] 9 141 282	90·4 136 271	87·1 131 261	84·1 126 252	81·3 122 244	78.8 118 236	76·4 115 229
	m. 60	m. 56	m. 52	m. 48	m. 44	m. 40	m. 36	m. 32	m. 28	m. 24	m. 20	т. 16	m. 12	m. 8	m. 4	m. o
							10	но	URS							

1a-							2	HOU	JRS.							
Declir	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
tion	0	4	8	12	16	20	24	28	32	36	40	44	43	52	56	60
85 85 ¹ 86 86 ¹ 87 87 ¹ 87 ²	22.9 25.4 28.6 32.7 38.2 45.8	22·2 24·7 27·8 31·7 37·0 44·5	21.6 24.0 27.0 30.9 36.0 43.2	21.0 23.3 26.3 30.0 35.0 42.1	20·4 22·7 25·6 29·2 34·1 41·0	, 19·9 22·2 24·9 28·5 33·3 39·9	19·4 21·6 24·3 27·8 32·5 39·0	19.0 21.1 23.8 27.2 31.7 38.1	18.6 20.6 23.2 26.6 31.0 37.2	18·2 20·2 22·7 26·0 30·3 36·4	17.8 19.8 22.2 25.4 29.7 35.6	17·4 19·4 21·8 24·9 29·1 34·9	17.1 19.0 21.4 24.4 28.5 34.2 42.8	16.8 18.6 21.0 24.0 28.0 33.6 42.0	16.5 18.3 20.6 23.5 27.5 33.0 41.2	16·2 18·0 20·2 23·1 27·0 32·4 40·5
88 <u>1</u>	76·4	74·I	72·1	70·1	68·3	66·6	65·0	63·5	62·0	60·7	59·4	58·2	57·1	56·0	55.0	54 ^{.0}
89	115	111	108	105	102	99·9	97·5	95·2	93· 1	91·0	89·1	87·3	85·6	84·0	82.5	81 ^{.0}
89 <u>1</u>	229	222	216	210	205	200	195	190	186	182	178	175	171	168	165	162
	m.	т.	m.	m.	m.	m.	т.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	60	5б	52	48	44	40	36	32	28	24	20	16	12	8	4	o
							9	ног	RS.							

36 Table A.

When hour angle is less than 6 hours, name the factors taken from Table A contrary to name of lat.

ند ا							3	нои	RS.							
Lai	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	0	4	8	12	16	20	24	28	32	36	40	44	48	52	56	60
85 85 85 85 85 86 86 86 86	11·4 12·7 14·3 16·3	11.0 12.3 13.8 15.8	10.7 11.8 13.3 15.2	10·3 11·4 12·9 14·7	9·9 11·1 12·4 14·2	9.6 10.7 12.0 13.7	9·3 10·3 11·6 13·2	8.9 9.9 11.2 12.8	8.6 9.6 10.8 12.3	8.3 9.2 10.4 11.9	· 8·0 8·9 10·0 11·4	, 7·7 8·6 9·7 11·0	, 7·4 8·3 9·3 10·6	, 7·1 7·9 8·9 10·2	6.9 7.6 8.6 9.8	6.6 7.3 8.3 9.4
87	19·1	18·4	17·8	17·2	16·6	16·0	15·5	14·9	14·4	13·9	13·4	12·9	12·4	11·9	11·5	11.0
871	22·9	22·1	21·4	20·6	19·9	19·2	18·5	17·9	17·3	16·6	16·0	15·4	14·9	14·3	13·8	13.2
88	28·6	27·7	26·7	25·8	24·9	24·0	23·2	22·4	21·6	20·8	20·1	19·3	18·6	17·9	17·2	16.5
88 <u>1</u>	38·2	36·9	35·6	34·4	33∙2	32·0	30·9	29·8	28·8	27·7	26·7	25·8	24·8	23·9	23·0	22·1
89	57·3	55·3	53·4	51·6	49∙8	48·1	46·4	44·8	43·2	41·6	40·1	38·6	37·2	35·8	34·4	33·1
89 <u>1</u>	115	111	107	103	99∙6	96·2	92·8	89·5	86·3	83·3	80·2	77·3	74·4	71·6	68·9	66·2
	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	60	56	52	48	44	40	36	32	28	24	20	16	12	8	4	o
							8 F	IOUI	RS.							

							41	HOU	RS.							
Lat	m. 0	m. 4	m. 8	m. 12	m. 16	m. 20	m. 2 4	ın. 28	m. 32	m. 3 6	m. 40	m. 44	m. 48	m. 52	m. 56	m. 60
	6.60 7.34 8.26 9.44 11.0 13.2	6.34 7.04 7.93 9.06 10.6 12.7	6.08 6.76 7.60 8.69 10.1 12.2	5.82 6.47 7.29 8.33 9.72 11.7	, 5·57 6·20 6·97 7·97 9·31 11·2	, 5·33 5·93 6·67 7·62 8·90 10·7	5.09 5.66 6.37 7.28 8.50 10.2	4.85 5.39 6.07 6.94 8.10 9.72	4.62 5.13 5.78 6.61 7.71 9.25	4·39 4·88 5·49 6·28 7·32 8·79	4.16 4.62 5.21 5.95 6.94 8.34	, 3·94 4·38 4·92 5·63 6·57 7·89	, 3·71 4·13 4·65 5·31 6·20 7·44	3.49 3.88 4.37 5.00 5.83 7.00	3.28 3.64 4.10 4.69 5.47 6.57	3.06 3.40 3.83 4.38 5.11 6.14
88 <u>1</u> 89 89	$ \begin{array}{c} 10.5 \\ 22.1 \\ 33.1 \\ 66.2 \\ \hline m. \\ 60 \end{array} $	21·2 31·8 63·5 m.	20·3 30·5 60·9 m.	$ \begin{array}{r} 19.5 \\ 29.2 \\ 58.4 \\ m. \\ 48 \\ \end{array} $	14.0 18.6 27.9 55.9 m.	13.4 17.8 26.7 53.4 m.	17.0 25.5 51.0 m.	$ \begin{array}{r} 15 \cdot 2 \\ 24 \cdot 3 \\ 48 \cdot 6 \\ m. \\ 22 \end{array} $	15·4 23·2 46·3 m.	14.7 22.0 44.0 m.	$ \begin{array}{r} 10.4 \\ 13.9 \\ 20.9 \\ 41.7 \\ m. \\ 20 \end{array} $	13·1 19·7 39·5 m.	12·4 18·6 37·2 m.	11.7 17.5 35.0 m.	11.0 16.4 32.9 m.	10·2 15·4 30·7 m.
		50	54	40		70	7 H	IOUI	RS.	-4		10			4	

				3 			5	HOU	RS.							
Lat	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	0	4	8	12	16	20	24	28	32	36	40	44	48	52	56	60
	, 3∙06 3∙40 3∙83 4∙38	2.85 3.17 3.57 4.08	2.64 2.93 3.30 3.77	2·43 2·70 3·04 3·48	, 2·22 2·47 2·78 3·18	2.02 2.24 2.52 2.88	1.81 2.01 2.27 2.59	1.61 1.79 2.01 2.30	1.40 1.56 1.76 2.01	, 1·20 1·34 1·50 1·78	, 1.00 1.11 1.25 1.43	0.80 0.89 1.00 1.14	0.60 0.67 0.75 0.86	0.40 0.44 0.50 0.57	0.20 0.22 0.25 0.29	, .00 .00 .00
87	5·11	4·76	4·41	4∙06	3·71	3∙36	3·02	2·68	2·34	2·01	1.67	1·33	1.00	0·67	0·33	·00
87 ¹	6·14	5·71	5·29	4∙87	4·45	4∙04	3·63	3·22	2·81	2·41	2.00	1·60	1.20	0·80	0·40	·00
88	7·67	7·14	6·61	6∙09	5·57	5∙05	4·54	4·05	3·52	3·01	2.51	2·00	1.50	1·00	0·50	·00
88½	10·2	9 ·52	8·82	8·12	7·42	6·73	6·05	5·37	4·69	4·01	3·34	2·67	2·00	1·33	0.67	•00
89	15·4	14·3	13·2	12·2	11·1	10·1	9·07	8·05	7·03	6·02	5·01	4·01	3·00	2·00	1.00	•00
89½	3 ^{0·} 7	28·6	26·5	24·4	22·3	20·2	18·1	16·1	14·1	12·0	10·0	8·01	6·01	4·00	2.00	•00
	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	60	56	52	48	44	40	36	32	28	24	20	16	12	8	4	o
							6 H	IOUI	RS.							

When hour angle is more than 6 hours, name the factors taken from Table A the same as the name of the latitude.

37	
Table	В.

na-	-						3]	HOU	RS.							
Decli	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
tio	0	4	8	12	16	20	24	28	32	26	40	44	48	52	56	60
85 85½ 86 86½	16·2 18·0 20·2 23·1	15.9 17.7 19.9 22.7	15.6 17.4 19.6 22.4	/ 15·4 17·1 19·2 22·0	, 15·1 16·8 18·9 21·7	14·9 16·6 18·7 21·3	14:7 16·3 18·4 21·0	, 14·5 16·1 18·1 20·7	, 14·3 15·9 17·9 20·5	, 14·1 15·7 17·7 20·2	14·0 15·5 17·5 20·0	13.8 15.3 17.2 19.7	13.6 15.2 17.1 19.5	13·5 15·0 16·9 19·3	, 13·3 14·8 16·7 19·1	13·2 14·7 16·5 18·9
87	27·0	26·5	26·1	25·7	25·3	24·9	24·6	24·2	23·9	23·6	23·3	23·0	22·8	22·5	22·3	22·0
87 1	32·4	31·8	31·3	30·8	30·3	29·9	29·5	29·1	28·7	28·3	28·0	27·6	27·3	27·0	26·7	26·4
88	40·5	39·8	39·2	38·5	37·9	37·4	36·8	36·3	35·9	35·4	35·0	34·5	34·1	33·8	33 [.] 4	33·I
88 <u>1</u>	54·0	53·1	52·2	51·4	50·6	49·9	49·1	48·5	47·8	47·2	46·6	46·1	45·5	45·0	44·6	44·I
89	81·0	79·6	78·3	77·1	75·9	74·8	73·7	72·7	71·7	70·8	69·9	69·1	68·3	67·6	66·8	66·2
89 <u>1</u>	162	159	157	154	152	150	147	145	143	142	140	138	137	135	134	I 32
	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
	60	56	52	48	44	40	36	32	28	24	20	16	12	8	4	o
							8 1	HOU	RS.							

na-							4 1	HOU	RS.							
Decli tior	m. 0	m. 4	m. 8	m. 12	m. 16	m. 20	m. 24	m. 28	m. 32	m. 36	m. 40	m. 44	m. 48	m. 52	m. 56	m. 60
85 85 86 86 86 87 87 87 88	, 13·2 14·7 16·5 18·9 22·C 26·4 33·1	í3·1 14·5 16·4 18·7 21·8 26·2 32·7	, 12:9 14:4 16:2 18:5 21:6 25:9 32:4	12.8 14.3 16.1 18.3 21.4 25.7 32.1	, 12·7 14·1 15·9 18·2 21·2 25·5 31·9	12.6 14.0 15.8 18.0 21.1 25.3 31.6	12.5 13.9 15.7 17.9 20.9 25.1 31.3	12·4 13·8 15·5 17·8 20·7 24·9 31·1	12·3 13·7 15·4 17·6 20·6 24·7 30·9	12·2 13·6 15·3 17·5 20·4 24·5 30·7	, 12·2 13·5 15·2 17·4 20·3 24·4 30·5	12·1 13·4 15·1 17·3 20·2 24·2 30·3	12.0 13.4 15.0 17.2 20.1 24.1 30.1	12.0 13.3 15.0 17.1 20.0 24.0 29.9	11.9 13.2 14.9 17.0 19.9 23.8 29.8	11.8 13.2 14.8 16.9 19.8 23.7 29.6
88 <u>1</u> 89 89 <u>1</u>	44·1 66·2 132 m. o	$ \begin{array}{r} 43.7 \\ 65.5 \\ 131 \\ \hline m. \\ 4 \end{array} $	43·3 64·9 130 m. 8	42·9 64·3 129 m. 12	42·5 63·7 127 m. 16	42·1 63·2 126 m. 20	41.8 62.7 125 m. 24	41·5 62·2 124 m. 28	$ \begin{array}{r} 41.2 \\ 61.8 \\ 124 \\ \hline m. \\ 32 \end{array} $	40.9 61.4 123 m. 36	40.6 61.0 122 m. 40	40·4 60·6 121 m. 44	40·2 60·2 120 m. 48	39·9 59·9 120 m. 52	39·7 59·6 119 m. 56	39·5 59·3 119 m. 60
							7 1	HOU	RS.				,			

-a-							5	HOU	RS.							
Declir	m.	m.	m.	m.	m.	m.	т.	m.	m.	m.	m.	m.	m.	m.	m.	m.
tion	0	4	8	12	16	20	2 4	28	32	3 6	40	44	48	52	56	60
85 85 86 86 86 87 87 87 87 88	11.8 13.2 14.8 16.9 19.8 23.7 29.6	11.8 13.1 14.7 16.8 19.7 23.6 29.5	11.7 13.0 14.7 16.8 19.6 23.5 29.4	11.7 13.0 14.6 16.7 19.5 23.4 29.3	11.6 13.0 14.6 16.7 19.4 23.3 29.2	11.6 12.9 14.5 16.6 19.4 23.3 29.1	11.6 12.9 14.5 16.6 19.3 23.2 29.0	11.5 12.8 14.4 16.5 19.3 23.1 28.9	í11.5 12.8 14.4 16.5 19.2 23.1 28.9	, 11:5 12·8 14·4 16·4 19·2 23·0 28·8	, 11.5 12.8 14.4 16.4 19.2 23.0 28.7	, 11·5 12·7 14·3 16·4 19·1 23·0 28·7	, 11.5 12.7 14.3 16.4 19.1 22.9 28.7	, 11·4 12·7 14·3 16·4 19·1 22·9 28·7	11.4 12.7 14.3 16.4 19.1 22.9 28.6	11.4 12.7 14.3 16.3 19.1 22.9 28.6
88 <u>1</u>	39 [.] 5	39·4	39·2	39.0	38·9	38·8	38·7	38.6	38·5	3 ^{8.} 4	38·3	38·3	38·2	38·2	38·2	38·2
89	59 [.] 3	59·0	58·8	58.6	5 ^{8·4}	58·2	58·0	57.9	57·7	57.6	57·5	57·4	57·4	57·3	57·3	57·3
89 <u>1</u>	119	118	118	117	117	116	116	116	115	115	115	115	115	115	115	115
	m.	m.	m,	m.	m.	m.	m.	m.								
	o	4	8	12	16	20	24	28	32	36	4 ⁰	44	48	52	56	60
							6]	HOU	RS.							

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

Azimuth is named N or S according to the name of the A and B correction.

A and B							LAT	ITUL	DES.						
Cor- rection.	00°	5°	10°	1 3 °	16°	18°	20°	220	24°	25°	26°	27°	28°	29°	30°
							Azimu	THS.							
·000	90.0	90.0	90.0	90'0	90.0	90.0	90.0	90.0	90:0	°	90.0	90.0	90.0	90.0	90.0
·010	89.4	89.4	89.4	89'4	89.4	89.5	89.5	89.5	89:5	89 ·5	89.5	89.5	89.5	89.5	89.5
·020	88.9	88.9	88.9	88'9	88.9	88.9	88.9	83.9	89:0	89 ·0	89.0	89.0	89.0	89.0	89.0
·030	88.3	88.3	83.3	88'3	88.3	88.4	88.4	88.4	88:4	88·4	88.5	88.5	88.5	88.5	88.5
·040	87.7	87.7	87.7	87'8	87.8	87.8	87.8	87.9	87:9	87·9	87.9	88.0	88.0	88.0	88.0
*050	87 1	87'1	87 [.] 2	87 ·2	87 ·2	87'3	87°3	87·3	87'4	87·4	87'4	87'4	87.5	87'5	87:5
*060	86.0	86'6	86 [.] 6	86·7	86·7	86'7	86°8	86·8	86'9	86·9	86'9	86'9	87.0	87'0	87:0
*070	86.0	86'0	86 [.] 1	86·1	86·2	86'2	86°2	86·3	86'3	86·4	86'4	86'4	86.5	86'5	86:5
*080	85.4	85'4	85 [.] 5	85 ·5	85·6	85'6	85°2	85·8	85'8	85·9	85'9	85'9	86.0	86'0	86:0
*090	84.9	84'9	84 [.] 9	85 · 0	85·1	85'1	85°2	85·2	85'3	85·3	85'4	85'4	85.5	85'5	85:5
·100	84*3	84°3	84.4	84'4	84.5	84.5	84.6	84 .7	84·8	84·8	84·9	84*9	85°0	85.0	85°1
·110	83'7	83'7	83.8	83'9	84.0	84.0	84.1	84.2	84·3	84·3	84·4	84*4	84°5	84.5	84°6
·120	83'2	83'2	83.3	83'3	83.4	83.5	83.6	83.7	83·7	83·8	83·8	83*9	84°0	84.0	84°1
·130	82*6	82'6	82.7	82'8	82.9	83.0	83.0	83.1	83·2	83·3	83·3	83*4	83°5	83.5	83°6
·140	82*0	82'1	82.1	82'2	82.3	82.4	82.5	82.6	82·7	82·8	82·8	82*9	83°0	83.0	83°1
·150 ·160 ·170 ·180 ·190	81.5 80.9 80.4 79.8 79.2	81·5 80·9 80·4 79·8 79·3	81.6 81.0 80.5 79.9 79.4	81.7 81.1 80.6 80.1 79.5	81.8 81.3 80.7 8c.2 79.6	81.9 81.3 80.8 80.3 79.8	82.0 81.4 80.9 80.4 79.9	82.1 81.6 81.0 80.5 80.0	82·2 81·7 81·2 80·7 80·2	82·3 81·7 81·2 80·7 80·2	82.3 81.8 80.8 80.3	82'4 81'9 81'4 80'9 80'4	82.5 82.0 81.5 81.0 80.5	82.5 82.0 81.5 81.1 80.6	82.6 82.1 81.6 81.1 80.7
·200	78.7	78.7	78.9	79 °0	79 ^{•1}	79 [.] 2	79'4	79`5	79'6	79'7	79 ^{.8}	79'9	80°0	80'1	80°2
·210	78.1	78.2	78.3	78°4	7 ^{8•6}	78.7	78'8	79`0	79'1	79'2	79 [.] 3	79'4	79°5	79'6	79°7
·220	77.6	77.6	77.8	77°9	78•1	78.2	78'3	78`5	78'6	78'7	78 ^{.8}	78'9	79°0	79'1	79°2
·230	77.0	77.1	77.2	77°4	77•5	7 7. 7	77'8	78`0	78'1	78'2	7 ^{8.3}	78'4	78°5	78'6	78°7
·240	76.5	76.6	76.7	76°8	77•0	77.1	77'3	77`5	77'6	77'7	77 ^{.8}	77'9	78°0	78'1	78°3
·250	76'0	76°0	76·2	76'3	76.5	76 [.] 6	76·8	76·9	77'1	77 ^{.2}	77'3	77'4	77 ^{.6}	77.7	77 [.] 8
·260	75'4	75°5	75·6	75'8	76.0	76 [.] 1	76·3	76·4	76'6	76.7	76'8	77'0	77 ^{.1}	77.2	77 [.] 3
·270	74'9	74°9	75·1	75'3	75.5	75 [.] 6	75·8	75·9	76'1	76.2	76'4	76'5	76 ^{.6}	76.7	76 [.] 8
·280	74'4	74°4	74·6	74 '7	74.9	7 5 .1	75·3	75·4	75'7	75.8	75'9	76'0	76 ^{.1}	76.2	76 [.] 4
·290	73'8	73°9	74·1	74'2	74.4	74 [.] 6	74·8	75·0	75'2	75.3	75'4	75'5	75 ^{.6}	75.8	75 [.] 9
·300	73'3	73'4	73'5	73 ^{.7}	73'9	74 ·1	74'3	74'5	74'7	74 ^{.8}	74'9	75 ^{.0}	75 ^{.2}	75'3	75'4
·310	72'8	72'8	73'0	73 ^{.2}	73'4	73·6	73'8	74'0	74'2	74 ^{.3}	74'4	74 ^{.6}	74 ^{.7}	74'8	75'0
·320	72'3	72'3	72'5	72 ^{.7}	72'9	73·1	73'3	73'5	73'7	73 ^{.8}	74'0	74 ^{.1}	74 ^{.2}	74'4	74'5
·330	71'7	71'8	72'0	72 ^{.2}	72'4	72·6	72'8	73'0	73 2	73 ^{.3}	73'5	73 ^{.6}	73 ^{.8}	73'9	74'1
·340	71'2	71'3	71'5	71 ^{.7}	71'9	72·1	72'3	72'5	72'7	72 ^{.9}	73'0	73 ^{.1}	73 ^{.3}	73'4	73'6
·350	7 0'7	70 [.] 8	71.0	71 ·2	71.4	71.6	71.8	72.0	72'3	72.4	72`5	72 .7	72.8	73 ^{.0}	73 ^{•1}
·360	70'2	70 [.] 3	70.5	70·7	70.9	71.1	71.3	71.5	71'8	71.9	72`1	72.2	72.4	72 ^{.5}	72 ^{•7}
·370	69'7	69 [.] 8	70.0	70·2	70.4	70.6	70.8	71.1	71'3	71.5	71`6	71.8	71.9	72 ^{.1}	72 ^{•2}
·380	69'2	69 [.] 3	69.5	69·7	69.9	70.1	70.3	70.6	70'9	71.0	71`1	71.3	71.5	71 ^{.6}	71 ^{•8}
·390	68'7	68 [.] 8	69.0	69·2	69.4	69.6	69.9	70.1	70'4	70.5	70`7	70.8	71.0	71 ^{.2}	71 ^{•3}
'400	68 ·2	68·3	68·5	68·7	69°0	69 [.] 2	69'4	69'7	69 ·9	70°1	70'2	70'4	70 ⁻⁵	70 ^{.7}	70'9
'410	67 · 7	67·8	68·0	68·2	68°5	68 [.] 7	68'9	69'2	69 ·5	69°6	69'8	69'9	70 ⁻¹	70 [.] 3	70'5
'420	67 ·2	67·3	67·5	67·7	68°0	68 [.] 2	68'5	68'7	69 ·0	69°2	69'3	69'5	69 ⁻⁷	69 ^{.8}	70'0
'430	66 · 7	66·8	67·0	67·3	67°5	67 [.] 8	68'0	68'3	68 ·6	68°7	68'9	69'0	69 ⁻²	69 ^{.4}	69'6
'440	66 ·3	6 6·3	66·6	66·8	67°1	67 [.] 3	67'5	67'8	68 ·1	68°3	68'4	68'6	68 ⁻⁸	69 ^{.0}	69'1
*450	65*8	65 [.] 9	66.1	66*3	66.6	66·8	67'1	67'4	67.7	67·8	68.0	68·2	68·3	68·5	68.7
*460	65*3	65 [.] 4	65.6	65*9	66.1	66·4	66'6	66'9	67.2	67·4	67.5	67·7	67·9	68·1	68.3
*470	64*8	64 [.] 9	65.2	65*4	65.7	65·9	66'2	66'5	66.8	66·9	67.1	67 ·3	67·5	67·7	67.9
*480	64*4	64 [.] 4	64.7	64*9	6 5. 2	65·5	65'7	66'0	66.3	66·5	66.7	66·8	67·0	67·2	67.4
*490	63*9	64 [.] 0	64.2	64*5	64.8	65·0	65'3	6 5'6	65.9	66·1	66.2	66·4	66·6	66·8	67.0

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AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

A and B							LA	TITUI	DES.						
Cor- rection.	00°	5°	10°	13°	16°	18°	20°	22°	24°	25°	26°	27°	28°	29°	30°
				'		Az	IMUTI	is.							
, 500 510 520 530 540	° 63'4 63'0 62'5 62'1 61'6	63.5 63.1 62.6 62.2 61.7	° 63.8 63.3 62.9 62.4 62.0	° 64.0 63.6 63.1 62.7 62.2	° 64·3 63·9 63·4 63·0 62·6	° 64.6 64.1 63.7 63.2 62.8	° 64.8 64.4 64.0 63.5 63.1	° 64.7 64.3 63.8 63.4	65·5 65·0 64·6 64·2 63·7	° 65·6 64·8 64·3 63·9	° 65 [.] 8 65 [.] 4 64 [.] 9 64 [.] 5 64 [.] 1	° 66'0 65'6 65'1 64'7 64'3	° 65 [.] 8 65 [.] 3 64 [.] 9 64 [.] 5	° 66.4 66.0 65.5 65.1 64.7	° 66·6 65·2 65·8 65·3 64·9
*550 *560 *570 *580 *590	61.2 60.8 60.3 59.9 59.5	61.3 60.8 60.4 60.0 59.6	61.6 61.1 60.7 60.3 59.8	61.8 61.4 61.0 60.5 60.1	62·1 61·7 61·3 60·9 60·4	62°4 62°0 61°5 61°1 60°7	62.7 62.2 61.8 61.4 61.0	63.0 62.6 62.1 61.7 61.3	63·3 62·9 62·5 62·1 61·7	63 ^{.5} 63 ^{.1} 62 ^{.7} 62 ^{.3} 61 ^{.9}	63.7 63.3 62.9 62.5 62.1	63.9 63.5 63.1 62.7 62.3	64'I 63'7 63'3 62'9 62'5	64'3 63'9 63'5 63'1 62'7	64'5 64'1 63'7 63'3 62'9
•600 •610 •620 •630 •640	59°0 58°6 58°2 57°8 57°4	59'1 58'7 58'3 57'9 57'5	59'4 59'0 58'6 58'2 57'8	59.7 59.3 58.9 58.5 58.1	60°0 59°6 59°2 58°8 58°4	60°3 59'9 59'5 59'1 5 ^{8°7}	60°6 60°2 59°8 59°4 59°0	60'9 60'5 60'1 59'7 59'3	61 ·3 60·9 60·5 60·1 59 ·7	61·5 61·1 60·7 60·3 59·9	61.7 61.3 60.9 60.5 60.1	61.9 61.5 61.1 60.7 60.3	62'1 61'7 61'3 60'9 60'5	6.3 61.9 61.5 61.1 60.8	62.5 62.2 61.8 61.4 61.0
-630 -660 -670 -680 -690 -	57°0 56°6 56°2 55°8 55°4	57'I 56'7 56'3 55'9 55'5	57'4 57'0 56'6 56'2 55'8	57'7 57'3 56'9 56'5 56'1	58.0 57.6 57.2 56.8 56.4	5 ^{8·3} 57·9 57·5 57·1 5 ^{6·7}	58.6 58.2 57.8 57.4 57.0	58·9 58·5 58·2 57·8 57·4	59'3 58'9 58'5 58'2 57'8	59 [•] 5 59 [•] 1 5 ^{8•} 7 5 ^{8•} 4 5 ^{8•} 0	59'7 59'3 58'9 58'6 58'2	59 [.] 9 59 [.] 5 59 [.] 2 58 [.] 8 58 [.] 4	60°1 59°8 59°4 59°0 58°6	60°4 60°0 59°6 59°3 58°9	60.6 60.2 59.9 59.5 59.1
·700 ·710 ·720 ·730 ·740	55°0 54°6 54°2 53°9 53°5	55'1 54'7 54'3 54'0 53'6	55'4 55'0 54'7 54'3 53'9	55'7 55'3 54'9 54'6 54'2	56°1 55°7 55°3 54°9 54°6	56·3 56·0 55·6 55·2 54·9	56·7 56·3 55·9 55·6 55·2	57°0 56°6 56°3 55°9 55°5	57'4 57'0 56'7 56'3 55'9	57 ^{.6} 57 ^{.2} 56 [.] 9 56 [.] 5 56 [.] 2	57 ^{.8} 57 ^{.5} 57 ^{.1} 56 [.] 7 56 [.] 4	58.0 57.7 57.3 57.0 56.6	58·3 57·9 57·6 57·2 56·8	58·5 58·2 57·8 57·4 57·1	58.8 58.4 58.1 57.7 57.3
·750 ·760 ·770 ·770 ·780 ·790	53°1 52°8 52°4 52°0 51°7	53.2 52.9 52.5 52.2 51.8	53 ^{.6} 53 ^{.2} 52 ^{.8} 52 ^{.5} 52 ^{.1}	53.8 53.5 53.1 52.8 52.4	54·2 53·8 53·5 53·1 52·8	54°5 54°1 53°8 53°4 53°4 53°1	54 ^{.8} 54 ^{.5} 54 ^{.1} 53 ^{.8} 53 ^{.4}	55 [.] 2 54 [.] 8 54 [.] 5 54 [.] 1 53 [.] 8	55 ^{.6} 55 ^{.2} 54 ^{.9} 54 ^{.5} 54 ^{.2}	55 ^{.8} 55 ^{.4} 55 ^{.1} 54 ^{.7} 54 ^{.4}	56°0 55°7 55°3 55°0 54°6	56·2 55·9 55·5 55·2 54`9	56·5 56·1 55·8 55·4 55·1	56 [.] 7 56 [.] 4 56 [.] 0 55 [.] 7 55 [.] 4	57.0 56.6 56.3 56.0 55.6
·800 ·810 ·820 ·830 ·840	51.3 51.0 50.6 50.3 50.0	51.4 51.1 50.8 50.4 50.1	51.8 51.4 51.1 50.7 50.4	52·1 51·7 51·4 51·0 50·7	52°4 52°1 51°8 51°4 51°1	52.7 52.4 52.1 51.7 51.4	53·1 52·7 52·4 52·0 51·7	53°4 53°1 52°8 52°4 52°1	53.8 53.5 53.2 52.8 52.5	54·1 53·7 53·4 53·0 52·7	54°3 53°9 53°6 53°3 52°9	54°5 54°2 53°8 53°5 53°2	54·8 54·4 54·1 53·8 53·4	55°0 54°7 54°4 54°0 53°7	55°3 55°0 54°6 54°3 54°0
·850 ·860 ·870 ·880 ·890	49.6 49.3 49.0 48.7 48.3	49'7 49'4 49'1 48'8 48'4	50°1 49°7 49°4 49°1 48°8	50'4 50'0 49'7 49'4 49'1	50.7 50.4 50.1 49.8 49.5	51.0 50.7 50.4 50.1 49.8	51.4 51.1 50.7 50.4 50.1	51.8 51.4 51.1 50.8 50.5	52·2 51·8 51·5 51·2 50·9	52.4 52.1 51.7 51.4 51.1	52.6 52.3 52.0 51.7 50.3	52.9 52.5 52.2 51.9 50.6	53°1 52°8 52°5 52°2 50°8	53 [.] 4 53 [.] 1 52 [.] 7 52 [.] 4 52 [.] 1	53.6 53.3 53.0 52.7 52.4
·900 ·910 ·920 ·930 ·940	48.0 47.7 47.4 47.4 47.1 46.8	48·1 47·8 47·5 47·2 46·9	48.4 48.1 47.8 47.5 47.2	48.8 48.4 48.1 47.8 47.5	49 [•] 1 48 [•] 8 48 [•] 5 48 [•] 2 47 [•] 9	49'4 49'1 48'8 48'5 48'2	49 ^{.8} 49 ^{.5} 49 ^{.2} 48 ^{.8} 48 ^{.5}	50°2 49°8 49°5 49°2 48°9	50.6 50.3 50.0 49.6 49.3	50·8 50·5 50·2 49·9 49·6	51.0 50.7 50.4 50.1 49.8	51.3 51.0 50.7 50.4 50.1	51.5 51.2 50.9 50.6 50.3	51.8 51.5 51.2 50.9 50.6	52°1 51°8 51°5 51°2 50°9
•950 •960 •970 •980 •990	46.5 46.2 45.9 45.6 45.3	46.0 46.3 46.0 45.7 45.4	46.9 46.6 46.3 46.0 45.7	47°2 46°9 46°0 46°3 46°0	47 ^{.6} 47 ^{.3} 47 ^{.0} 46 ^{.7} 46 ^{.4}	47'9 47'0 47'3 47'0 47'7 46'7	48.2 47.9 47.7 47.4 47.1	48.6 48.3 48.0 47.7 47.5	49 ^{.0} 48 ^{.7} 48 ^{.5} 48 ^{.2} 47 ^{.9}	49'3 49'0 48'7 48'4 48'1	49 ^{.5} 49 ^{.2} 48 ^{.9} 48 ^{.6} 48 ^{.3}	49 ^{.8} 49 ^{.5} 49 ^{.2} 4 ^{8.9} 4 ^{8.6}	50°0 49°7 49°4 49°1 48°8	50°3 50°0 49'7 49'4 49'1	50.6 50.3 50.0 49.7 49.4

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

A and B							LA'	TITUE	ES.						
Cor- rection.	00°	5°	10°	13°	16°	18º	20°	22°	240	25°	26°	270	28°	29°	30°
						į	ZIMU	rus.							
1'00	45.0	45.1	0	0	16.1	16:4	16.8	17.2	17.6	47.8	°	48.3	18.6	18.8	0 10°T
1.05	44.4	44.5	44.9	45'2	45.6	45.9	46.2	46.6	47.0	47.2	47.5	47.7	48 0	48.3	48.5
1.04 1.06	43°9 43°3	44.0	44'3 43'8	44'0 44'I	45°0 44°5	45.3	45'7 45'1	40.0	40.5	40.7 40.1	40.9	47.2	47.4 46.9	47.7	48.0
1.08	42.8	42.9	43.5	43.2	43'9	44'2	44.6	45.0	45.4	45.6	45'9	46.1	46.4	46.6	46.9
1.10	42.3	42.4	42.7	43.0	43'4	43'7	44'1	44.4	44'9	45'1	45.3	45.6	45.8	46.1	46.4
1.12 1.14	41.9	41.9	42.2	42.0	42'9 42'4	43.2	43.5	43.9	44 3 43 8	44 U 44 I	44.0	45 4	45'3	45.0	45 9 45 4
1.18 1.19	40.8	40'9 40'4	41°2 40°7	41.2	41'9 41'4	42°2 41°7	42°5 42°0	42.9 42.4	43°3	43 [.] 6 43 [.] I	43 ^{.8}	44°1 43'6	44°3 43°8	44°6 44°1	44 ° 9 44 ° 4
1'20	20.8	20.0	10.2	40.5	40.0	41.2	41.6	41'0	12.4	12.6	12.8	43'1	12.2	42.6	13.0
1.55	39.3	39'9 39'4	39.8	40'1	40.2	40.8	41.1	41.2	41.9	42'1	42'4	42.6	42.9	43.1	43.4
1.54 1.50	38.9 38.4	39.0 38.2	39'3 38'9	39°0	40°0 39°5	40°3 39°8	40.0	41'0 40'6	41'4 41'0	41.7	41.9	41.7	42'4 42'0	42.7	43.0
1.58	38.0	38.1	38.4	38.7	39.1	39'4	39.7	40'I	40.2	40.8	41.0	41.5	41.2	41.8	42'I
1.30	37.6	37.7	38.0	38.3	38.7	39.0	39.3	39.7	40'1	40.3	40 [.] 6	40.8	41.1	41.3	41.6
1 32 1.34	36.7	37 3 36.8	37.2	37 9 37 4	37.8	30.2	38.5	39.3	397 39.2	39°5	39'7	39.9	40.0	40.5	40.8
1.36 1.38	36.3	36.4 36.0	36.2	37°0 36°6	37'4 37'0	37.7	38.0 37.6	38°4 38°0	38.8	39 .1 38.6	39°3	39°5 39°1	39.8 39.4	40°I 39°6	40°3 39°9
1:40	25.2	25.6	26.0	26.2	36.6	26.0	27.2	27.6	28.0	38.2	28.5	38.7	30.0	30.3	30.2
1.45	35.2	35.3	35.6	35.9	36.2	36.2	36.8	37.2	37.6	37.8	38.1	38.3	38.6	38.8	39.1
1.44 1.46	34°8 34°4	34'9 34'5	35 ^{.2} 34 ^{.8}	35°5 35°1	35.0	30.1	30.2 30.1	36.8	37°2 36°9	37.2	37'7 37'3	37'9 37'6	38°2 37°8	38.1	38·3
1.48	34.0	34.1	34'5	34'7	35.1	35'4	35.7	36.1	36.2	36.2	36.9	37.2	37'4	37'7	38.0
1.20	33.7	33.8	34.1	34.4	34'7	35.0	35.4	35.7	36.1	36.3	36.6	36.8	37.1	37.3	37.6
1.54	33.0 33.0	33.1	33'4	33.7	34 4 34 0	34 / 34 3	33°0 34°6	35 4 35 0	35.4	35.6	35.8	36·1	36.3	36.6	36.9
1.26 1.28	32.7 32.3	32.8	33°1 32°7	33°3 33°0	33'7 33'4	34'0 33'6	34°3 34°0	34'7 34'3	35°1 34°7	35'3 34'9	35°5 35°1	35°7 35°4	36.0 32.6	30°2 35°9	36°5 36°2
1.60	32.0	32.1	32.4	32.7	33.0	33'3	33.6	34.0	34.4	34.6	34.8	35'0	35.3	35'5	35.8
1.62	31.2	31.8	32.1	32.4	32.7	33.0	33.3	33'7	34.0	34.3	34.5	34'7	35.0	35.2	35.2
1.66	31.4 31.1	31.2	31.9	32.0	32.1	32°7 32°4	33.0	33.3 33.0	33'7 33'4	33.9	34°2 33'8	34'4 34'1	34'0	34 9 34 6	34.8
1.68	30.8	30.9	31.1	31.4	31.8	32.0	32'4	32.2	33.1	33'3	33.2	33'7	34.0	34.5	34.2
1.20	30.2	30.0	30.0	31.1	31.2	31.7	32.0	32.4	32.8	33.0	33.2	33.4	33.7	33.9	34.2
1.24	29.9	30.0	30.3	30.2	30.0	31 4 31 1	31.4	31.8	32.2	32.4	32.6	32.8	33.1	33.3	33.6
1.26 1.28	29.6 29.3	29'7 29'4	30°0 29°7	30°2 30°0	30.2 30.3	30.9 30.6	31.5	31.2	31.0 31.0	32.1	32°3 32°0	32.2	32.8	33.0 32.7	33.3
1.80	20.1	20.1	20'4	20.7	30'0	30'2	30.6	30'0	31.3	31.2	31.4	31.0	32'2	32.4	32.7
1.82	28.8	28.9	29.2	29.4	29.8	30.0	30.3	30.7	31.0	31.2	31.4	31.7	31.9	32.1	32.4
1.86	28.3	28.4	28.9	29.2	29.5	29.7	29.8	30.4	30.7	30.9	30.0	31.4	31.3	31.0	31.8
1.88	28.0	28.1	28.4	28 .6	29.0	29.2	29.5	29.8	30.3	30.4	30.6	30.8	31.1	31.3	31.0
1.05	27.8	27.8	28.1	28.4	28.7	29.0	29.3	29.6	29.9	30.1	30.4	30.0	30.8	31.0	31.0
1.94	27.3	27.4	27.6	27.9	28.2	28.5	28.7	29.1	29.4	29.6	29.8	30.1	30.3	30.2	30.8
1.98	27.0 26.8	27.1	27.4	27.6	28.0	28·2 28·0	28.5	28.8	29.2 29.0	29.4 29.1	29.6	29.8 29.5	30'0 29'8	30.3	30.2
			1	1 ' '	J. ''					-	1				-

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

A and B							LA	FITUI	DES.						
Cor- rection.	00°	50	10°	13°	16°	18°	20°	22°	24°	25°	28°	27°	28°	29°	80°
	•	•	•	•	0	A	ZIMUT	тня. •	• 1	0	0	•	0 1	0 1	o
2.00	26.6	26.7	26·9	27.2	27.5	27.7	28.0	28·3	28.7	28·9	29 [.] 1	29 [.] 3	29 [·] 5	29'8	30°0
2.05	26.0	26.1	26·4	26.6	26.9	27.2	27.4	27·7	28.1	28·3	28 [.] 5	28 [.] 7	28·9	29'1	29°4
2.10	25.5	25.5	25·8	26.0	26.4	26.6	26.9	27·2	27.5	27·7	27 [.] 9	28 [.] 1	28·3	28'6	28°8
2.15	24.9	25.0	25·3	25.5	25.8	26.1	26.3	26·6	27.0	27·2	27 [.] 4	27 [.] 6	27·8	28'0	28°2
2.20	24.4	24.5	24·8	25.0	25.3	25.5	25.8	26·1	26.5	26·6	26 [.] 8	27 [.] 0	27·2	27'5	27°7
2°25	24.0	24.0	24'3	24'5	24.8	25.0	25'3	25 ^{.6}	25 [.] 9	26·1	26·3	26·5	26.7	26·9	27.2
2°30	23.5	23.6	23'8	24'0	24.3	24.6	24'8	25 ^{.1}	25 [.] 5	25·6	25·8	26·0	26.2	26·4	26.7
2°40	22.6	22.7	22'9	23'2	23.4	23.7	23'9	24 ^{.2}	24 [.] 5	24·7	24·9	25·1	25.3	25·5	25.7
2°50	21.8	21.9	22'1	22'3	22.6	22.8	23'1	23 ^{.3}	23 [.] 6	23·8	24·0	24·2	24.4	24·6	24.8
2°60	21.0	21.1	21'3	21'5	21.8	22.0	22'3	22 ^{.5}	22 [.] 8	23·0	23·2	23·3	23.5	23·7	23.9
2·70	20'3	20'4	20°6	20'8	21.1	21.3	21.5	21.8	22°1	22°2	22'4	22.6	22.8	23.0	23.2
2·80	19'7	19'7	19°9	20'1	20.4	20.6	20.8	21.1	21°4	21°5	21'7	21.8	22.0	22.2	22.4
2·90	19'0	19'1	19°3	19'5	19.7	19.9	20.2	20.4	20°7	20°8	21'0	21.2	21.3	21.5	21.7
3·00	18'4	18'5	18°7	18'9	19.1	19.3	19.5	19.8	20°0	20°2	20'3	20.5	20.7	20.9	21.1
3·10	17'9	17'9	18°1	18'3	18.6	18.7	18.9	19.2	19°4	19°6	19'7	19.9	20.1	20.2	20.4
3.20	17'4	17'4	17.6	17 ^{.8}	18.0	18·2	18·4	18.6	18.9	19.0	19 ^{.2}	19.3	19.5	19.7	19 ^{.8}
3.30	16'9	16'9	17.1	17 [.] 3	17.5	17·7	17·9	18.1	18.4	18.5	18 ^{.6}	18.8	18.9	19.1	19 ^{.3}
3.40	16'4	16'4	16.6	16 ^{.8}	17.0	17·2	17·4	17.6	17.8	18.0	18 ^{.1}	18.3	18.4	18.6	18 ^{.8}
3.60	15'5	15'6	15.8	15 ^{.9}	16.1	16·3	16·5	16.7	16.9	17.0	17 ^{.2}	17.3	17.5	17.6	17 ^{.8}
3.80	14'7	14'8	15.0	15 ^{.1}	15.3	15·5	15·6	15.8	16.1	16.2	16 ^{.3}	16.5	16.6	16.7	16 ^{.9}
4.00	14'0	14'I	14.2	14'4	14.6	14'7	14.9	15.1	15.3	15.4	15.5	15.7	15 ^{.8}	16.0	16.1
4.20	13'4	13'4	13.6	13'7	13.9	14'1	14.2	14.4	14.6	14.7	14.8	15.0	15 ^{.1}	15.2	15.4
4.40	12'8	12'9	13.0	13'1	13.3	13'4	13.6	13.8	14.0	14.1	14.2	14.3	14 ^{.4}	14.6	14.7
4.60	12'3	12'3	12.4	12'6	12.7	12'9	13.0	13.2	13.4	13.5	13.6	13.7	13 ^{.8}	14.0	14.1
4.80	11'8	11'8	11.9	12'1	12.2	12'4	12.5	12.7	12.8	12.9	13.1	13.2	13 ^{.3}	13.4	13.5
5.00 5.50 6.00 6.50 7.00	11.3 10.3 9.5 8.7 8.1	11.4 10.3 9.5 8.8 8.2	11.5 10.5 9.6 8.9 8.3	11.6 10.6 9.7 9.0 8.3	11.8 10.7 9.8 9.1 8.5	11.9 10.8 9.9 9.2 8.5	12'0 11'0 10'1 9'3 8'6	12.2 11.1 10.2 9.4 8.8	12.3 11.3 9.6 8.9	12'4 11'3 10'4 9'6 9'0	12.5 11.4 10.5 9.7 9.0	12.7 11.5 10.6 9.8 9.1	12.8 11.6 10.7 9.9 9.2	12.9 11.7 10.8 10.0 9.3	13.0 11.9 10.9 10.1 9.4
8.0	7'1	7*2	7.2	7'3	7°4	7'5	7.6	7.7	7 ^{.8}	7'9	7'9	8.0	8·1	8·1	8·2
9.0	6'3	6*4	6.4	6'5	6°6	6'7	6.7	6.8	6·9	7'0	7'0	7.1	7 ^{.2}	7·2	7·3
10.0	5'7	5*7	5.8	5'9	5°9	6'0	6.1	6.2	6·2	6'3	6'3	6.4	6·5	6·5	6·6
11.0	5'2	5*2	5.3	5'3	5°4	5'5	5.5	5.6	5 ^{.7}	5'7	5'8	5.8	5 ^{.9}	5·9	6·0
12.0	4'8	4*8	4.8	4'9	5°0	5'0	5.1	5.1	5 ^{.2}	5'3	5'3	5.3	5 ^{.4}	5·5	5·5
13.0	4°4	4'4	4°5	4°5	4°6	4.6	4°7	4'7	4 ^{.8}	4.9	4'9	4 9	5°0	5.0	5°1
15.0	3°8	3'8	3°9	3°9	4°0	4.0	4°1	4'1	4 ^{.2}	4.2	4'2	4 3	4°3	4.4	4°4
17.0	3°4	3'4	3°4	3°5	3°5	3.5	3°6	3'6	3 ^{.7}	3.7	3'7	3 8	3°8	3.8	3°9
20.0	2°9	2'9	2°9	2°9	3°0	3.0	3°0	3'1	3 ^{.1}	3.2	3'2	3 2	3°2	3.3	3°3
25.0	2°3	2'3	2°3	2°4	2°4	2.4	2°4	2'5	2 ^{.5}	2.5	2'5	2 6	2°6	2.6	2°6
30°0 40°0 50°0 70°0 100°0	1.3 1.4 1.1 0.8 0.6	1.9 1.4 1.2 0.8 0.6	1.9 1.5 1.2 0.8 0.6	2.0 1.5 1.2 0.8 0.6	2.0 1.5 1.2 0.9 0.6	2:0 1:5 1:2 0:9 0:6	2.0 1.5 1.2 0.9 0.6	2.1 1.2 0.9 0.6	2.1 1.9 0.9 0.6	2.1 1.6 1.3 0.0 0.6	2.1 1.9 0.9 0.6	2.1 1.9 0.9 0.6	2.2 1.0 1.3 0.9 0.0	2.2 1.6 1.3 0.9 0.7	2.2 1.3 0.9 0.7
150°0 200°0 300°0 400°0 800°0	0'4 0'3 0'2 0'1 0'1	0'4 0'3 0'1 0'1	0'4 0'3 0'1 0'1	0°4 0°3 0°2 0°1 0°1	0'4 0'3 0'2 0'1 0'1	0'4 0'3 0'2 0'2 0'1	0'4 0'3 0'2 0'2 0'1	0'4 0'3 0'2 0'2 0'1	0'4 0'3 0'2 0'1	0'4 0'3 0'2 0'1	0'4 0'3 0'2 0'2 0'1	0'4 0'3 0'2 0'1	0'4 0'3 0'2 0'1	0'4 0'3 0'2 0'1	0'4 0'3 0'2 0'2 0'1

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

A and B							LAT	TUD	ES.						
Cor- rection.	31°	32°	33°	34°	35°	36°	37°	3 8 °	3 9 °	40 °	41°	42°	43°	440	45°
l , ,	0	•	• 1	0	0	•	Azimu	THS.	•	0	. • :	•	0	0	
-000	90'0	90°0	90°0	90°0	90'0	90°0	90°0	90°0	90°0	90°0	90.0	90°0	90°0	90°0	90°0
-010	89'5	89°5	89°5	89°5	89'5	89°5	89°5	89°5	89°6	89°6	89.6	89°6	89°6	89°6	89°6
-020	89'0	89°0	89°0	89°1	89'1	89°1	89°1	89°1	89°1	89°1	89.1	89°1	89°2	89°2	89°2
-030	88'5	88°5	88°6	88°6	88'6	88°6	88°6	88°6	88°7	88°7	88.7	88°7	88°7	88°8	88°8
-040	88'0	88°1	88°1	88°1	88'1	88°1	88°2	88°2	88°2	88°2	88.3	88°3	88°3	88°8	88°4
·050	87.5	87 ^{.6}	87.6	87 ^{.6}	87.7	87 ^{.7}	87·7	87 [.] 7	87 [.] 8	87.8	87.8	87'9	87.9	87'9	88.0
·060	87.1	87 ^{.1}	87.1	87 ^{.2}	87.2	87 ^{.2}	87·3	87 [.] 3	87 [.] 3	87.4	87.4	87'4	87.5	87'5	87.6
·070	86.6	86 ^{.6}	86.6	86 ^{.7}	86.7	86 [.] 8	86·8	86 [.] 8	86 [.] 9	86.9	87.0	87'0	87.1	87'1	87.2
·080	86.1	86 ^{.1}	86.2	86 ^{.2}	86.3	86 [.] 3	86·3	86 [.] 4	86 [.] 4	86.5	86.5	86'6	86.7	86'7	86.8
·090	85.6	85 ^{.6}	8 5.7	85 ^{.7}	85.8	85 [.] 8	85·9	85 [.] 9	86 [.] 0	86.1	86.1	86'2	86.2	86'3	86.4
'100	85 [.] 1	85 ^{.2}	85 [.] 2	85 [.] 3	85'3	85'4	85 [.] 4	85.5	85 ^{.6}	85 ^{.6}	85'7	85.7	85 [.] 8	85 [.] 9	86°0
'110	84 [.] 6	84 ^{.7}	84 [.] 7	84 [.] 8	84'9	84'9	85 [.] 0	85.0	85 ^{.1}	85 ^{.2}	85'3	85.3	85 [.] 4	85 [.] 5	85°6
'120	84 [.] 1	84 ^{.2}	84 [.] 3	84 [.] 3	84'4	84'5	84 [.] 5	84.6	84 ^{.7}	84 [.] 7	84'8	84.9	85 [.] 0	85 [.] 1	85°1
'130	83 [.] 6	83 ^{.7}	83 [.] 8	83 [.] 8	83'9	84'0	84 [.] 1	84.2	84 ^{.2}	84 [.] 3	84'4	84.5	84 [.] 6	84 [.] 7	84°7
'140	83 [.] 2	83 ^{.2}	83 [.] 3	83 [.] 4	83'5	83'5	83 [.] 6	83.7	83 ^{.8}	83 ^{.9}	84'0	84.1	84 [.] 2	84 [.] 2	84°3
·150	82.7	82·8	82.8	82·9	83.0	83.1	83.2	83·3	83 [.] 4	83.4	83.5	83 ^{.6}	83.7	83 [.] 8	83.9
·160	82.2	82·3	82.4	82·4	82.5	82.6	82.7	82·8	82 [.] 9	83.0	83.1	83 ^{.2}	83.3	83 [.] 4	83.5
·170	81.7	81·8	81.9	82·0	82.1	82.2	82.3	82·4	82 [.] 5	82.6	82.7	82 ^{.8}	82.9	83 [.] 0	83.1
·180	81.2	81·3	81.4	81·5	81.6	81.7	81.8	81·9	82 [.] 0	82.1	82.3	82 ^{.4}	82.5	82 [.] 6	82.7
·190	80.7	80·8	80.9	81·0	81.2	81.3	81.4	81·5	81 [.] 6	81.7	81.8	82 ^{.0}	82.1	82 [.] 2	82.3
*200	80'3	80 [.] 4	80 [.] 5	80 ^{.6}	80.7	80 [.] 8	80°9	81.0	81·2	81·3	81.4	81·5	81.7	81.8	82.0
*210	79'8	79 [.] 9	80 [.] 0	80 ^{.1}	80.2	80 [.] 4	80°5	80.6	80·7	80·9	81.0	81·1	81.3	81.4	81.6
*220	79'3	79 [.] 4	79 [.] 5	79 ^{.7}	79.8	79 [.] 9	80°0	80.2	80·3	80·4	80.6	80·7	80.9	81.0	81.2
*230	78'8	79 [.] 0	79 [.] 1	79 ^{.2}	79.3	79 [.] 5	79°6	79.7	79 [.] 9	80·0	80.2	80·3	80.5	80.6	80.8
240	78'4	78 [.] 5	78 [.] 6	7 ^{8.} 7	78.9	79 [.] 0	79°1	79.3	79 [.] 4	79·6	79.7	79·9	80.0	80.2	80.4
·250	77'9	78.0	78·2	78·3	78.4	78 ^{.6}	7 ^{8·7}	7 ^{8·9}	79°0	79 ^{•2}	79'3	79`5	79 ^{.6}	79 ^{.8}	80°0
·260	77'4	77.6	77·7	77·8	78.0	78 ^{.1}	78·3	78·4	78°6	7 ^{8•7}	78'9	79`1	79 ^{.2}	79 ^{.4}	79°6
·270	77'0	77.1	77·2	77·4	77.5	77 ^{.7}	77 ^{·8}	78·0	78°1	7 ^{8•3}	78'5	78`7	78 ^{.8}	79 ^{.0}	79°2
·280	76'5	76.6	76·8	76·9	77.1	77 ^{.2}	77 ^{·4}	77·6	77°7	77 ^{•9}	78'1	78`2	7 ^{8.4}	78 ^{.6}	78°8
·290	76'0	76.2	76·3	76·5	76.6	76 ^{.8}	77 ^{·0}	77 ^{·1}	77°3	77 ^{•5}	77'7	77`8	7 ^{8.0}	78 ^{.2}	78°4
·300	75 ^{.6}	75'7	75'9	76.0	76·2	7 ^{6•4}	76·5	7 ^{6·7}	76 [.] 9	77'1	77°2	77`4	77 ^{.6}	77 ^{.8}	78.0
·310	75 ^{.1}	75'3	75'4	75.6	75·8	75•9	76·1	76·3	76 [.] 5	76'6	76°8	77`0	77 ^{.2}	77 ^{.4}	77.6
·320	74 [.] 7	74'8	75'0	75.1	75·3	75•5	75 ·7	75 ^{·8}	76 [.] 0	76'2	76°4	76`6	76 ^{.8}	77 ^{.0}	78.3
·330	74 ^{.2}	74'4	74'5	74.7	74·9	75•1	75·2	75 ^{·4}	75 [.] 6	75'8	76°0	76`2	76 [.] 4	76 ^{.6}	76.9
·340	73 ^{.8}	73'9	74'1	74.3	74·4	74•6	74 ^{·8}	75 ^{·0}	75 [.] 2	75'4	75°6	75`8	76 [.] 0	76 ^{.3}	76.5
•350	73°3	73`5	73 ^{.6}	73 ^{.8}	74 ^{.0}	74 ⁻²	74'4	74 ^{.6}	74 ^{.8}	75°0	75°2	75'4	75 ^{.6}	75 [.] 9	76·1
•360	72°9	73'0	73 ^{.2}	73 ^{.4}	73 ^{.6}	73 ⁻⁸	74'0	74 ^{.2}	74 ^{.4}	74°6	74°8	75'0	75 ^{.2}	75 [.] 5	75·7
•370	72°4	72'6	72 ^{.8}	72 ^{.9}	73 ^{.1}	73 ⁻³	73'5	73 ^{.7}	74 ^{.0}	74°2	74°4	74'6	74 ^{.9}	75 [.] 1	75·3
•380	72°0	72'1	72 ^{.3}	72 ^{.5}	7 ^{2.7}	7 ²⁻⁹	73'1	73 ^{.3}	73 ^{.5}	73°8	74°0	74'2	74 ^{.5}	74 [.] 7	75·0
•390	71°5	71'7	71 ^{.9}	72 ^{.1}	7 ^{2.3}	7 ²⁻⁵	72'7	72 ^{.9}	73 ^{.1}	73°4	73°6	73'8	74 ^{.1}	74 [.] 3	74·6
•400	71'1	71•3	71'5	71.7	71.9	72'1	72·3	72.5	72.7	73.0	73 ^{.2}	73'4	73'7	73 ^{.9}	74 ^{•2}
•410	70'6	70•8	71'0	71.2	71.4	71'6	71·9	72.1	72.3	72.6	72 ^{.8}	73'1	73'3	73 ^{.6}	73 ^{•8}
•420	70'2	70•4	70'6	70.8	71.0	71'2	71·5	71.7	71.9	72.2	72 ^{.4}	72'7	72'9	73 ^{.2}	73 ^{•5}
•430	69'8	70•0	70'2	70.4	70.6	70'8	71·0	71.3	71.5	71.8	72 ^{.0}	72'3	72'5	72 ^{.8}	73 ^{•1}
•440	69'3	69•5	69'7	70.0	70.2	70'4	70·6	70.9	71.1	71.4	71 ^{.6}	71'9	72'2	72 ^{.4}	72 [•] 7
•450	68·9	69'1	69'3	69 ·5	69 8	70 .0	70°2	70'5	70'7	71 .0	71.2	71.5	71.8	72'I	72'3
•460	68·5	68'7	68'9	69·1	69 4	69.6	69°8	70'1	70'3	70.6	70.9	71.1	71.4	71'7	72'0
•470	68·1	68'3	68'5	68·7	68 9	69.2	69°4	69'7	69'9	70.2	70.5	70.7	71.0	71'3	71'6
•480	67 [.] 6	67'9	68'1	68·3	68 5	68.8	69°0	69'3	69'5	69.8	70.1	70.4	70.7	71'0	71'3
•490	67 [.] 2	67'4	67'7	67·9	68 1	68.4	68°6	68'9	69'2	69.4	69.7	70.0	70.3	70'6	70'9

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

A and B							LA	TITUI	DES.						
Cor- rection.	31 5	32°	33°	24°	35°	36°	3 7°	38°	39°	40°	41°	4 3°	43°	4 4°	45°
						Az	IMUTI	is.							
, 500 510 520 530 540	° 66·8 66·4 66·0 65·6 6 5 ·2	° 65.6 66.2 65.8 65.4	° 65.8 66.4 66.0 65.6	° 67'5 67'1 66'7 66'3 65'9	° 67.7 67.3 66.9 66.5 66.1	0 68.0 67.6 67.2 66.8 66.8	° 67·8 67·8 67·4 67·1 66·7	° 68·5 68·1 67·7 67·3 66·9	° 68·8 68·4 68·0 67·6 67·2	o 69.0 68.7 68.3 67.9 67.5	0 69·3 68·9 68·6 68·2 67·8	° 69 [.] 6 69 [.] 2 68 [.] 9 68 [.] 5 68 [.] 1	° 69 [.] 9 69 [.] 2 68 [.] 8 68 [.] 4	° 69`9 69`5 69`1 68`8	° 70`5 70`2 69`8 69`5 69`1
•550	64.8	65 ^{.0}	65°2	65*5	65.7	6 6.0	66·3	66 [.] 6	66·9	67·2	67.5	67.8	68'1	68:4	68.7
•560	64.4	64 ^{.6}	64°8	65*1	65.4	6 5 .6	65·9	66 [.] 2	66·5	66·8	67.1	67.4	67'7	68:1	68.4
•570	64.0	64 ^{.2}	64°5	64*7	65.0	65.2	65·5	65 [.] 8	66·1	66·4	66.7	67.0	67'4	67:7	68.0
•580	63.6	63 ^{.8}	64°1	64*3	64.6	64.9	65·1	65 [.] 4	⁶ 5·7	66·0	66.4	66.7	67'0	67:4	67.7
•590	63.2	63 ^{.4}	63°7	•63*9	64.2	64.5	64·8	65 [.] 1	65·4	65·7	66.0	6 6.3	66'7	67:0	67.4
-600	62.8	63.0	63·3	63 [.] 6	63.8	64 ·1	64°4	64.7	65°0	65 ·3	65.6	66°0	66·3	66·7	67.0
-610	62.4	62.6	62·9	63 [.] 2	63.4	63·7	64°0	64.3	64°6	65·0	65.3	65°6	66·0	66·3	66.7
-620	62.0	62.3	62·5	62 [.] 8	63.1	63·4	63'7	64.0	64°3	64·6	64.9	65'3	65·6	66·0	66.3
-630	61.6	61.9	62·1	62 [.] 4	62.7	63 ·0	63'3	63.6	63°9	64 · 2	64.6	64'9	65·3	65·6	66.0
-640	61.3	61.5	61·8	62 [.] 1	62.3	62·6	62'9	63.2	63°6	63·9	64.2	64°6	6 4·9	65·3	65.7
-650	60°9	61·1	61.4	61.7	62.0	62·3	62.6	62.9	63 [.] 2	63.5	63.9	64.2	64.6	64·9	65.3
-660	60°5	60·8	61.0	61.3	61.6	61·9	62.2	62.5	62 [.] 8	63.2	63.5	63.9	64.2	64·6	65.0
-670	60°1	60·4	60.7	60.9	61.2	61·5	61.8	62.2	62 [.] 5	62.8	63.2	63.5	63.9	64·3	64.7
-680	59°8	60·0	60.3	60.6	60.9	61·2	61.5	61.8	62 [.] 1	62.5	62.8	63.2	63.6	63·9	64.3
-690	59°4	59 [.] 7	59.9	60.2	60.5	60·8	61.1	61.5	61 [.] 8	62.1	6 2. 5	62.9	63.2	63·6	64.0
·700	59 ^{.0}	59°3	59 ^{.6}	59'9	60·2	60°5	60.8	61·1	61.2	61.8	62.2	62·5	62 [.] 9	63'3	63.7
·710	5 ^{8.} 7	58°9	59 ^{.2}	59'5	59·8	60°1	60.4	60·8	61.1	61.5	61.8	62·2	62 [.] 6	62'9	63.3
·720	58.3	58°6	5 ^{8.9}	59'2	59·5	59°8	60.1	60·4	60.8	61.1	61.5	61·9	62 [.] 2	62'6	63.0
·730	58.0	58°2	5 ^{8.5}	5 ^{8'8}	59·1	59°4	59.8	60·1	60.4	60.8	61.1	61·5	61.9	62'3	62.7
·740	57.6	57°9	5 ^{8.2}	5 ^{8'5}	58·8	59°1	59.4	59·8	60.1	60.5	60.8	61·2	61.6	6 2' 0	62.4
·750 ·760 ·770 ·780 ·790	57°3 56°9 56°6 56°2 55°9	57°5 57°2 56°9 56°5 56°2	57 ^{.8} 57 ^{.5} 57 ^{.1} 56 ^{.8} 56^{.5}	58·1 57·8 57 ·4 57 ·1 56·8	58.4 58.1 57.8 57 .4 57.1	58·8 58·4 58·1 57'7 57'4	59 ^{•1} 5 ^{8•7} 5 ^{8•4} 5 ^{8•1} 57•8	59'4 59'1 58'8 58'4 58'1	59 [.] 8 59 [.] 4 59 [.] 1 5 ^{8.} 8 5^{8.}5	60°1 59°8 59°5 59°1 58°8	60°5 60°2 59°8 59°5 59°5	60'9 60'5 60'2 59'9 59'6	61.3 60.9 60.6 60.0	61.7 61.3 61.0 60.7 60. 4	62·1 61·7 61·4 61·1 60·8
·800	55 ^{.6}	55.8	56·1	56·4	56·8	57*1	57' 4	57*8	58·1	5 ^{8•5}	58·9	59°3	59'7	60°1	60°5
·810	55 ^{.2}	55.5	55·8	56·1	56·4	56*8	57'1	57*4	57·8	58•2	58·6	59°0	59'4	59°8	60°2
·820	54 ^{.9}	55.2	55·5	55·8	56·1	56*4	56'8	57*1	57·5	57•9	58·2	58°6	59'0	59°5	59°9
·830	54 ^{.6}	54.9	55·2	55·5	55·8	56*1	56'5	56*8	57·2	57•6	57·9	58°3	58'7	59°2	59°6
·840	54 ^{.2}	54.5	54·8	55·1	55·5	5 5 *8	56'1	56*5	56·9	57•2	57 ^{.6}	58°0	58'4	58°9	59°3
•850 •860 •870 •880 •880 •890	53.9 53.6 53.3 53.0 52.7	54•2 53•9 53•6 53•3 53•0	54.5 54.2 53.9 53.6 53.3	54*8 54*5 54*2 53*9 53*6	55°2 54°8 54°5 54°2 53°9	55*5 55*2 54*9 54*6 54*2	55.8 55.5 55.2 54.9 54.6	56·2 55·9 55·6 55·3 55·0	56·6 56·2 55·9 55 ^{.6} 55 ^{.3}	56·9 56·6 56·3 56·0 55· 7	57°3 57°0 56°7 56°4 56°1	57'7 57'4 57'1 56'8 56'5	58·1 57·8 57·5 57·2 56·9	58.6 58.3 58.0 57.7 57.4	59 °0 58°7 58°4 58°1 57°8
•900	52°4	52.6	53 .0	53' 3	53.6	53·9	54°3	54°7	55°0	55°4	55*8	56·2	56·6	57°1	57°5
•910	52°0	52.3	52.6	53'0	53.3	53·6	54°0	54°4	54°7	55°1	55*5	55·9	56·4	56°8	57°2
•920	51°7	52.0	52.3	52'7	53.0	53·3	53°7	54°1	54°4	54°8	55*2	55·6	56·1	56°5	57°0
•930	51°4	51.7	52.0	52'4	52.7	53·0	53°4	53°8	54°1	54°5	54*9	55·4	55·8	56°2	56°7
•940	51°1	51.4	51.7	52'1	52.4	52·7	53°1	53°5	53°9	54°2	54*6	55·1	55·5	55°9	56°4
•950	50·8	51·1	51.5	51.8	52·1	52.5	52·8	53 ^{.2}	53.6	54 .0	54'4	54.8	55°2	55°7	56·1
•960	50·5	50·9	51.2	51.5	51·8	52.2	52·5	52 ^{.9}	53.3	53.7	54'1	54.5	54°9	55°4	55·8
•970	50·3	50·6	50.9	51.2	51·5	51.9	52·2	52 ^{.6}	53.0	53.4	53'8	54.2	54°6	55°1	55·6
•980	50·0	50·3	50.6	50.9	51·2	51.6	52·0	52 ^{.3}	52.7	53.1	53'5	53.9	54°4	54°8	55 ·3
•990	49 [.] 7	50·0	53.3	50.6	51·0	51.3	51·7	52 ^{.0}	52.4	52.8	53'2	53.7	54°1	54°5	55 ·0

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

Azimut	h is	named	Ν	or	S	according	to	the	name	of	the	A	and	в	correction.	,
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A and B							LA	TITU	DES.						
Cor- restion.	31°	32°	33°	34º	35°	36°	37°	38°	3 9 °	40°	41°	42°	43°	44 °	45°
					2		Azimu	THS.			0	•		•	
1.00	49'4	49 ^{.7}	50°0	50'3	50.7	51.0	51.4	51.8	52.1	52°5	53.0	53'4	53.8	54'3	54°7
1.02	48'8	49 ^{.1}	49°5	49'8	50.1	50.5	50.8	51.2	51.6	52°0	52.4	52'8	53.3	53'7	54°2
1.04	48'3	48 ^{.6}	48°9	49'2	49.6	49.9	50.3	50.7	51.1	51°5	51.9	52'3	52.7	53'2	53°7
1.06	47'7	48 ^{.0}	48°4	48'7	49.0	49.4	49.8	50.1	50.5	50°9	51.3	51'8	52.2	52'7	53°1
1.08	47'2	47 ^{.5}	47°8	48'2	48.5	48.9	49.2	49.6	50.0	50°4	50.8	51'2	51.7	52'2	52°6
1.10	46'7	47.0	47'3	47 6	48°0	48·3	48.7	49'1	49 ^{.5}	49'9	50'3	50'7	51.2	51.6	52°1
1.12	46'2	46.5	46'8	47 1	47°5	47 ^{·8}	48.2	48'6	49 ^{.0}	49'4	49'8	50'2	50.7	51.1	51°6
1.14	45'7	46.0	46'3	46 6	47°0	47·3	47.7	48'1	4 ^{8.5}	48'9	49'3	49'7	50.2	50.6	51°1
1.16	45'2	45.5	45'8	46 1	46°5	46·8	47.2	47'6	48 ^{.0}	48'4	48'8	49'2	49.7	50.2	50°6
1.18	44'7	45.0	45'3	45 6	46°0	4 6 ·3	46.7	47'1	47 ^{.5}	47'9	48'3	48'8	49.2	49.7	50°2
1°20	44 ^{.2}	44`5	44 ^{.8}	45 ^{•1}	45 ^{.5}	45 ^{.8}	46'2	46 [.] 6	47 °0	47`4	47 [.] 8	48'3	4 ^{8.7}	49 ^{.2}	49'7
1°22	43 ^{.7}	44`0	44 ^{.3}	44 ^{•7}	45 ^{.0}	45 [.] 4	45'7	46 [.] 1	46°5	46`9	47 [.] 4	47'8	4 ^{8.3}	4 ^{8.7}	49'2
1°24	43 ^{.3}	43`6	43 ^{.9}	44 ^{•2}	44 ^{.6}	44 [.] 9	45'3	45 [.] 7	46°1	46`5	46 [.] 9	47'3	47 ^{.8}	4 ^{8.3}	48'8
1°26	42 ^{.8}	43`1	43 ^{.4}	43 ^{•8}	44 ^{.1}	44 [.] 5	44'8	45 [.] 2	45°6	46`0	46 [.] 4	46'9	47.3	47 ^{.8}	48'3
1°28	42 ^{.3}	42`7	43^{.0}	43 ^{•3}	43 ^{.6}	44 [.] 0	44'4	44 [.] 8	45°2	45`6	46 [.] 0	46'4	46.9	47 ^{.4}	47'9
1·30	41'9	42'2	42.5	42'9	43°2	43 ^{.6}	43'9	44'3	44`7	45'1	45.5	46°0	46·4	46·9	47'4
1·32	41'5	41'8	42.1	42'4	42°8	43 ^{.1}	43'5	43'9	44`3	44'7	45.1	45°6	46·0	46·5	47'0
1·34	41'0	41'3	41.7	42'0	42°3	4 ^{2.7}	43'1	43'4	43`8	44'3	44.7	45°1	45 ^{.6}	46·1	46'5
1·36	40'6	40'9	41.2	41 ' 6	41°9	4 ^{2.3}	42'6	43'0	43`4	43'8	44.3	44°7	45 ^{.2}	45·6	46'1
1·38	40'2	40'5	40.8	41' 2	41°5	4 ^{1.9}	42'2	42'6	43`0	43'4	43.8	44°3	44 ^{.7}	45·2	45'7
1'40	39 [.] 8	40.1	40'4	40.7	41'1	41.4	41.8	42.2	42.6	43°0	43 [.] 4	43 ^{.9}	44'3	44 ^{.8}	45'3
1'42	39 [.] 4	39.7	40'0	40.3	40'7	41.0	41.4	41.8	42.2	42°6	43 ^{.0}	43 ^{.5}	43'9	44 ^{.4}	44'9
1'44	39 [.] 0	39.3	39'6	39.9	40'3	40.6	41.0	41.4	41.8	42°2	42 ^{.6}	43 ^{.1}	43'5	44 ^{.0}	44'5
1'46	3 ^{8.} 6	38.9	39'2	39.6	39'9	40.3	40.6	41.0	41.4	41°8	42 ^{.2}	4 ^{2.7}	43'1	43 ^{.6}	44'1
1'48	3 ^{8.} 2	38.5	38'9	39.2	39'5	39.9	40.2	40.6	41.0	41°4	41 ^{.8}	4 ^{2.3}	42'7	43 ^{.2}	43'7
1°50 1°52 1°54 1°56 1°58	37 [.] 9 37 [.] 5 37 [.] 1 36 [.] 8 36 [.] 4	38·2 37·8 37·4 37·1 36·7	38·5 38·1 37·7 37·4 37·0	38.8 38.4 38.1 37.7 37.4	39'1 38'8 3 ^{8'4} 38'0 37'7	39 [.] 5 39 [.] 1 38 [.] 8 38 [.] 4 38 [.] 0	39 [.] 9 39 [.] 5 39 [.] 1 3 ^{8.8} 3 ^{8.8}	40°2 39°9 39°5 39°1 38°8	40 ^{.6} 40 ^{.2} 39 ^{.9} 39 ^{.5} 39 ^{.2}	41.0 40.7 40.3 39.9 39.6	41.5 41.1 40.3 40.0	41.9 41.5 41.1 40.8 40.4	42.4 42.0 41.6 41.2 40.9	42.8 42.4 42.1 41.7 41.3	43'3 42'9 42'6 42'2 41'8
1.60	36.1	36·4	36.7	37°0	37°3	37'7	38.0	38.4	38.8	39 ^{.2}	39·6	40'1	40.5	41°0	41.5
1.62	35.8	36·1	36.4	36°7	37°0	37'3	37.7	38.1	38.5	3 ^{8.9}	39·3	39'7	40.2	40°6	41.1
1.64	35.4	35·7	36.0	36°3	36°7	37'0	37.4	37.7	38.1	3 ^{8.5}	38·9	39'4	39.8	40°3	40.8
1.66	35.1	35·4	35.7	36°0	36°3	36'7	37.0	37.4	37.8	3 ^{8.2}	38·6	39'0	39.5	39°9	40.4
1.68	34.8	35·1	35.4	35°7	36°0	36'3	36.7	37.1	37.4	37 ^{.8}	38·3	3 ⁸ '7	39.1	39°6	40.1
1.70	34°5	34 ^{.7}	35 ^{.0}	35'4	35'7	36°0	36·4	36.7	37'1	37.5	37'9	38·4	38.8	39'3	39 ^{.8}
1.72	34°1	34 ^{.4}	34 ^{.7}	35'0	35'4	35'7	36·1	36.4	36'8	37.2	37'6	38·0	38.5	38'9	39 ^{.4}
1.74	33°8	34 ^{.1}	34 ^{.4}	34'7	35'1	35'4	35·7	36.1	36'5	36.9	37'3	37·7	38.2	38'6	39 ^{.1}
1.76	33°5	33 ^{.8}	34 ^{.1}	34'4	34'7	35'1	35·4	35.8	36'2	36.6	37'0	37·4	37.8	38'3	3 ^{8.8}
1.78	33°2	33 ^{.5}	33 ^{.8}	34'1	34'4	34'8	35·1	35.5	35'9	36.3	3 ⁶ '7	37·1	37.5	38'0	3 ^{8.5}
1.80	32.9	33.2	33 ^{.5}	33 ^{.8}	34'I	34°5	34·8	35 ^{.2}	35 ^{.6}	36·0	36·4	36·8	37.2	3 7 •7	38·2
1.82	32.7	32.9	33 ^{.2}	33 ^{.5}	33'9	34°2	34·5	34 ^{.9}	35 ^{.3}	35'7	36·1	36·5	36.9	37•4	37·8
1.84	32.4	32.7	3 ^{2.9}	33 ^{.2}	33'6	33°9	34·2	34 ^{.6}	35 ^{.0}	35'4	35·8	36·2	36.6	37•1	37·5
1.86	32.1	32.4	3 ^{2.7}	33 ^{.0}	33'3	33°6	33·9	34 ^{.3}	34 ^{.7}	35'1	35·5	35·9	36.3	36•8	37·2
1.88	31.8	32.1	3 ^{2.4}	3 ^{2.7}	33'0	33°3	33·7	34 ^{.0}	34 ^{.4}	34'8	35·2	35·6	36.0	36•5	37·0
1.90	31.6	31.8	32.1	32'4	32.7	33°0	33'4	33.7	34·1	34 °5	34°9	35°3	35.7	36·2	36.7
1.92	31.3	31.6	31.8	32'1	32.4	32°8	33'1	33.5	33 ^{.8}	34 °2	34°6	35°0	35.5	35·9	36.4
1.94	31.0	31.3	31.6	31'9	32.2	32°5	32'8	33.2	33 ^{.6}	33°9	34°3	34°7	35.2	35·6	36.1
1.96	30.8	31.0	31.3	31'6	31.9	32°2	32'6	32.9	33 ^{.3}	33°7	34°1	34°5	34.9	35·3	35.8
1.98	30.5	30.8	31.1	31'3	31.7	32°0	32'3	32.7	33 ^{.0}	33°4	33°8	34°2	34.6	35·1	35.5

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

Azimuth is named N or S according to the name of the A and B correction.

Aand	в							LA	TITU	DES.						
Cor rectio	on.	31°	32°	33°	34°	35°	36°	37°	3 8 °	39°	40°	41°	42°	4 3°	44 °	45°
,		0 1	•	0	0	0	1 0	AZIMU 0	THS.		0		0			0
2°C 2°C 2°C 2°C 2°C 2°C	00 05 10 15 20	30'3 29'6 29'1 28'5 27'9	30'5 29'9 29'3 28'7 28'2	30 ^{.8} 30 ^{.2} 29 ^{.6} 29 ^{.0} 28 ^{.5}	31·1 30·5 29·9 29·3 28·7	31.4 30.8 30.2 29.6 29.0	31.7 31.1 30.5 29.9 29.3	32.0 31.4 30.8 30.2 29.6	32.4 31.8 31.1 30.6 30.0	32.8 32.1 31.5 30.9 30.3	33°1 32°5 31°9 31°3 30°7	33.5 32.9 32.3 31.6 31.1	33.9 33.3 32.7 32.0 31.5	34°4 33°7 33°1 32°5 31°9	34.8 34.1 33.5 32.9 32.3	35'3 34'6 34'0 33'3 32'7
2** 2* 2* 2* 2*	25 30 40 50 50	27'4 26'9 25'9 25'0 24'2	27'7 27'1 26'2 25'3 24'4	27'9 27'4 26'4 25'5 24'6	28·2 27·7 26·7 25·8 24·9	28.5 28.0 27.0 26.0 25.2	28·8 28·3 27·2 26·3 25·4	29°1 28°6 27°6 26°6 25°7	29'4 28'9 27'9 26'9 26'0	29.8 29.2 28.2 27.2 26.3	30'1 29'6 28'5 27'6 20'7	30'5 29'9 28'9 27'9 27'0	30'9 30'3 29'3 28'3 27'4	31.3 30.7 29.7 28.7 27.7	31.7 30.1 29.1 28.1	32·2 31·6 30·5 29·5 28·5
2.5 2.6 3.0 3.1	70 80 90 00 10	23.4 22.6 21.9 21.2 20.6	23.6 22.8 22.1 21.5 20.8	23.8 23.1 22.4 21.7 21.0	24'1 23'3 22'6 21'9 21'3	24·3 23·6 22·8 22·1 21·5	24 ^{.6} 23 ^{.8} 23 ^{.1} 22 ^{.4} 21 ^{.7}	24 [.] 9 24 [.] 1 23 [.] 4 22 [.] 7 22 [.] 0	25.2 24.4 23.6 22.9 22.3	25.5 24.7 23.9 23.2 22.5	25.8 25.0 24.2 23.5 22.8	26·1 25·3 24·6 23·8 23·1	26·5 25·7 24·9 24·2 23·5	26·9 26·0 25·2 24·5 23·8	27·2 26·4 25·6 24·9 24·2	27.6 26.8 26.0 25.2 24.5
3.3 3.3 3.4 3.6 3.8	20 30 40 50 30	20'0 19'5 18'9 18'0 17'1	20.2 19.7 19.1 18.1 17.2	20.4 19.9 19.3 18.3 17.4	20.7 20.1 19.5 18.5 17.6	20'9 20'3 19'8 18'7 17'8	21.1 20.5 20.0 19.0 18.0	21.4 20.8 20.2 19.2 18.2	21.6 21.0 20.5 19.4 18.5	21.9 21.3 20.7 19.7 18.7	22.2 21.6 21.0 19.9 19.0	22.5 21.9 21.3 20.2 19.2	22.8 22.2 21.6 20.5 19.5	23.1 22.5 21.9 20.8 19.8	23.5 22.8 22.2 21.1 20.1	23.8 23.2 22.6 21.4 20.4
4.0 4.2 4.4 4.6 4.8		16'3 15'5 14'9 14'2 13'7	16.4 15.7 15.0 14.4 13.8	16.6 15.8 15.2 14.5 14.0	16.8 16.0 15.3 14.7 14.1	17.0 16.2 15.5 14.9 14.3	17'2 16'4 15'7 15'0 14'4	17'4 16'6 15'9 15'2 14'6	17 ^{.6} 16 [.] 8 16 [.] 1 15 [.] 4 14 8	17.8 17.0 16.3 15.6 15.0	18·1 17·3 16·5 15·8 15·2	18·3 17·5 16·8 16·1 15·4	18.6 17.8 17.0 16.3 15.7	18.9 18.0 17.3 16.6 15.9	19.2 18.3 17.5 16.8 16.2	19 ^{.5} 18 ^{.6} 17 ^{.8} 17 ^{.1} 16 [.] 4
5.5 5.5 6.6 7.0		13.1 12.0 11.0 10.2 9.5	9.6 13.3 13.3	13'4 12'2 11'2 10'4 9'7	13 ^{.6} 12 ^{.4} 11 ^{.4} 10 ^{.5} 9 ^{.8}	13.7 12.5 11.5 10.6 9.9	13.9 12.7 11.6 10.8 10.0	14.1 12.8 11.8 10.9 10.1	14.2 13.0 11.0 10.3	I4'4 I3'2 I2'I II'2 I0'4	14 ^{.6} 13 [.] 4 12 [.] 3 11 [.] 4 10 ^{.6}	14.8 13.5 12.5 11.5 10.7	15'1 13'7 12'6 11'7 10'9	15.3 14.0 12.8 11.9 11.1	15.5 14.2 13.0 12.1 11.2	15 ^{.8} 14 ^{.4} 13 ^{.3} 12 ^{.3} 11 ^{.4}
8°C 9°C 10°C 11°C 12°C		8·3 7·4 6·7 6·1 5·6	8·4 7·5 6·7 6·1 5 ·6	8·5 7·5 6·8 6·2 5·7	8·6 7·6 6·9 6·3 5·7	8·7 777 7·0 6·3 5·8	8·8 7·8 7·0 6·4 5·9	8·9 7'9 7'1 6·5 6·0	9°0 8°0 7°2 6°6 6°0	9'1 8'1 7'3 6'7 6'1	9 ^{.3} 8 [.] 3 7 [.] 4 6 ^{.8} 6 ^{.2}	9'4 8'4 7'5 6'9 6'3	9.5 8.5 7.7 7.0 6.4	9.7 8.6 7.8 7.1 6.5	9 [.] 9 8 [.] 8 7 [.] 9 7 [.] 2 6 [.] 6	10.0 8.9 8.0 7.3 6.7
13.0 15.0 17.0 20.0 25.0		5°1 4°4 3°9 3°3 2°7	5°2 4°5 4°0 3°4 2°7	5°2 4°5 4°0 3°4 2°7	5·3 4·6 4·1 3·5 2·8	5.4 4.7 4.1 3.5 2.8	5'4 4'7 4'2 3'5 2'8	5`5 4`8 4`2 3`6 2`9	5 ^{.6} 4 ^{.8} 4 ^{.3} 3 ^{.6} 2 ^{.9}	5'7 4'9 4'3 3'7 2'9	5.7 5.0 4.4 3.7 3.0	5.8 5.0 4.5 3.8 3.0	5'9 5'1 4'5 3'8 3'1	6.0 5.2 4.6 3.9 3.1	6·1 5·3 4·7 4·0 3·2	6.2 5.4 4.8 4.0 3.2
30°0 40°0 50°0 70°0 100°0		2.2 1.7 1.3 1.0 0.7	2·3 1·7 1·4 1·0 0·7	2·3 1·7 1·4 1·0 0·7	2·3 1·7 1·4 1·0 0·7	2·3 1·7 1·4 1·0 0·7	2.4 1.8 1.4 1.0 0.7	2°4 1°8 1°4 1°0 0°7	2'4 1'8 1'5 1'0 0'7	2.5 1.8 1.5 1.1 0.7	2.2 1.9 1.5 1.1 0.7	2.2 1.9 1.5 1.1 0.8	2.6 1.9 1.5 1.1 0.8	2.0 2.0 1.6 1.1 0.8	2.7 2.0 1.6 1.1 0.8	2.7 2.0 1.6 1.2 0.8
150°0 200°0 300°0 400°0 800°0		0'4 0'3 0'2 0'1	0'5 0'3 0'2 0'2 0'1	0.2 0.3 0.2 0.2 0.1	0.2 0.3 0.2 0.1	0.2 0.3 0.2 0.2 0.1	0'5 0'4 0'2 0'2 0'1	0'5 0'4 0'2 0'2 0'1	0'5 0'4 0'2 0'2 0'1	0'5 0'4 0'2 0'2 0'1	0'5 0'4 0'2 0'2 0'1	0'5 0'4 0'3 0'2 0'1	0.2 0.4 0.3 0.2 0.1	0.2 0.4 0.3 0.2 0.1	0.2 0.4 0.3 0.5 0.1	0'5 0'4 0'3 0'2 0'1

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

A and B							LAT	TUTI	DES.						
Cor- rection.	46°	47°	48°	49 °	50°	51°	52°	53°	54°	55°	56°	57°	58°	59°	60°
,	° 1	٥	•	•	٥	•	Azimu	THS. O	•	0	•	0	ο	0	0
.000	90°0	90°0	90°0	90°0	90°0	90°0	90°0	90°0	90°0	90°0	90°0	90°0	90'0	90°0	90°0
.010	89°6	89°6	89°6	89°6	89°6	89°6	89°6	89° 7	89°7	89°7	89'7	89°7	89'7	89°7	89°7
.020	89°2	89°2	89°2	89°2	89°3	89°3	89°3	89°3	89°3	89°3	89'4	89°4	89'4	89°4	89°4
.030	88°8	88°8	88°9	88°9	88°9	88°9	88°9	89°0	89°0	89°0	89'0	89°1	89'1	89°1	89°1
.040	88°4	88°4	88°5	88°5	88°5	88°6	88°6	88°6	88°7	88°7	88'7	88°8	88'8	88°8	88°9
•050	88.0	88.0	88.1	88'1	88·2	88·2	88 ·2	88·3	88·3	88°4	88.4	88'4	88·5	88.5	88.6
•060	87.6	87.7	87.7	87'7	87·8	87·8	87·9	87·9	88·0	88°0	88.1	88'1	88·2	88.2	88.3
•070	87.2	87.3	87.3	87'4	87·4	87·5	87·5	87·6	87·6	87°7	87.8	87'8	87·9	87.9	88.0
•080	86.8	86.9	86.9	87'0	87·1	87·1	87·2	87·2	87·3	87°4	87.4	87'5	87·6	87.6	87.7
•090	86.4	86.5	86.6	86'6	86·7	86·8	86·8	86·9	87·0	87°0	87.1	87'2	87·3	87.3	87.4
'100	86 ·0	86.1	86 ·2	86·2	86·3	86·4	86°5	86.6	86·6	86·7	86·8	86·9	87'0	87'1	87'1
'110	85·6	85.7	85·8	85·9	86·0	86·0	86°1	86.2	86·3	86·4	86·5	86·6	86'7	86'8	86'9
'120	85 ·2	85.3	85·4	85·5	85·6	85·7	85°8	85.9	86·0	86·1	86·2	86·3	86'4	86'5	86'6
'130	84·8	84.9	85·0	85·1	85·2	85·3	85°4	85.5	85·6	85·7	85·8	86·0	86'1	86'2	86'3
'140	84·4	84.5	84·6	84·8	84·9	85·0	85°1	85.2	85·3	85·4	85·5	85·6	85'8	85'9	86'0
'150	84'1	84.2	84'3	84'4	84.5	84.6	84'7	84·8	85.0	85.1	85°2	85'3	85°5	85 ^{.6}	85.7
'160	83'7	83.8	83'9	84'9	84.1	84.3	84'4	84·5	84.6	84.8	84°9	85'0	85°2	85 ^{.3}	85.4
'170	83'3	83.4	83'5	83'6	83.8	83.9	84'0	84·2	84.3	84.4	84°6	84'7	84°9	85 ^{.0}	85.1
'180	82'9	83.0	83'1	83'3	83.4	83.5	83'7	83·8	84.0	84.1	84°3	84'4	84°6	84 ^{.7}	84.9
'190	82'5	82.6	82'8	82'9	83.0	83.2	83'3	83·5	83.6	83.8	83°9	84'1	84°3	84 ^{.4}	84.6
'200	82'1	82.2	82.4	82.5	82.7	82.8	83.0	83'1	83.3	83.5	83 ^{.6}	83 [.] 8	84.0	84'I	84°3
'210	81'7	81.8	82.0	82.2	82.3	82.5	82.6	82'8	83.0	83.1	83 ^{.3}	83 [.] 5	83.7	83'8	84°0
'220	81'3	81.5	81.6	81.8	82.0	82.1	82.3	82'5	82.6	82.8	83 ^{.0}	83 [.] 2	83.4	83'5	83°7
'230	80'9	81.1	81.3	81.4	81.6	81.8	81.9	82'1	82.3	82.5	82 ^{.7}	82 [.] 9	83.1	83'2	83°4
'240	80'5	80.7	80.9	81.1	81.2	81.4	81.6	81'8	82.0	82.2	82 ^{.4}	82 [.] 6	82.8	83'0	83°2
•250	80'1	80'3	80°5	80'7	80'9	81°1	81.2	81'4	81.6	81.8	82.0	82.2	82.5	82.7	82.9
•260	79'8	79'9	80°1	80'3	80'5	80°7	80.9	81'1	81.3	81.5	81.7	81.9	82.2	82.4	82.6
•270	79'4	79'6	79°8	80'0	80'2	80°4	80.6	80'8	81.0	81.2	81.4	81.6	81.9	82.1	82.3
•280	79'0	79'2	79°4	79'6	79'8	80°0	80.2	80'4	80.7	80.9	81.1	81.3	81.6	81.8	82.0
•290	78'6	78'8	79°0	79'2	79'4	79°7	79.9	80'1	80.3	80.6	80.8	81.c	81.3	81.5	81.7
·300	78·2	78.4	78 ^{.6}	78.9	79'I	79'3	79'5	79 ^{.8}	80'0	80 [.] 2	80'5	80'7	81.0	81.2	81.5
·310	77·8	78.1	78 ^{.3}	78.5	78'7	79'0	79'2	79 ^{.4}	79'7	79 [.] 9	80'2	80'4	80.7	80.9	81.2
·320	77·5	77.7	77 ^{.9}	78.1	78'4	78'6	78'9	79 ^{.1}	79'3	79 [.] 6	79'9	80'1	80.4	80.6	80.9
·330	77·1	77.3	77 ^{.5}	77.8	78'0	78'3	78'5	78 ^{.8}	79'0	79 [.] 3	79'5	79'8	80.1	80.4	80.6
·340	76·7	76.9	77 ^{.2}	77.4	77'7	77'9	78'2	7 ^{8.8}	7 ^{8'} 7	79 [.] 0	79'2	79'5	79.8	80.1	80.4
·350	76·3	76 ^{.6}	76·8	77'1	77'3	77 ^{.6}	77 ^{.8}	78.1	78·4	78.6	78.9	79 ^{•2}	79'5	79 ^{.8}	80°1
·360	76·0	76 ^{.2}	76·5	76'7	77'0	77 ^{.2}	77 ^{.5}	77.8	78·1	78.3	78.6	78 [•] 9	79'2	79 ^{.5}	79°8
·370	75 ^{.6}	75 ^{.8}	76·1	76'4	76'6	76 [.] 9	77 ^{.2}	77.4	77·7	78.0	78.3	78 [•] 6	78'9	79 ^{.2}	79°5
·380	75 ^{.2}	75 ^{.5}	75·7	76'0	76'3	76 ^{.6}	76 ^{.8}	77.1	77·4	77.7	78.0	78 [•] 3	78'6	7 ^{8.9}	79°2
·390	74 ^{.8}	75 ^{.1}	75·4	75'6	75'9	76 ^{.2}	76 ^{.5}	76.8	77 ^{·1}	77.4	77.7	7 ^{8•} 0	78'3	7 ^{8.6}	79°0
'400	74'5	74°7	75°0	75'3	75 ·6	75'9	76·2	76·5	76·8	77 ^{•1}	77'4	77'7	78.0	78·4	78.7
'410	74'1	74°4	74'7	74'9	75 ·2	75'5	75 ^{·8}	76·1	76·5	76•8	77'1	77'4	77.7	78·1	78.4
'420	73'7	74°0	74'3	74'6	74·9	75'2	75·5	75·8	76·1	76•5	76'8	77'1	77.5	77·8	78.1
'430	73'4	73°7	73'9	74'2	74·5	74'9	75 ^{·2}	75·5	75·8	76•1	76'5	76'8	77.2	77·5	77.9
'440	73'0	73°3	73'6	73'9	74 · 2	74'5	74 ^{·8}	75·2	75·5	75•8	76'2	76'5	76.9	77·2	77.6
'450	72.6	72'9	73'2	73 ^{.6}	73 [.] 9	74'2	74`5	74*8	75°2	75 ^{.5}	75 [.] 9	76·2	76.6	77'0	77'3
'460	72.3	72'6	72'9	73 ^{.2}	73 [.] 5	73'9	74'2	74*5	74°9	75 ^{.2}	75 [.] 6	75·9	76.3	76'7	77'0
'470	71.9	72'2	72'5	72 ^{.9}	73 [.] 2	73'5	73'9	74*2	74°6	74 ^{.9}	75 [.] 3	75·6	76.0	76'4	76'8
'480	71.6	71'9	72'2	72 ^{.5}	72 [.] 9	73'2	73'5	73*9	74°2	74 ^{.6}	75 ^{.0}	75·3	75.7	76'1	76'5
'490	71.2	71'5	71'8	72 ^{.2}	72 [.] 5	72'9	73'2	73*6	73°9	74 ^{.3}	74 [.] 7	75·1	75.4	75'8	76'2

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

A and B							ĿΑ	TITU	DES.						
Cor- rection.	4 6°	47°	48°	49°	50°	51°	52°	53°	54°	55°	55°	57°	58°	59°	60°
,	•	0	1 0) 0	1 0	A		HS.	. 0	1 0		, 0	1 0	, 0	0
·500	70°8	71.2	71.5	71.8	72.2	72.5	72 ·9	73 ³	73 ^{.6}	74°0	74°4	74 ^{.8}	75 ^{.2}	75°6	76.0
·510	70°5	70.8	71.2	71.5	71.8	72.2	72·6	72 ⁹	73 ^{.3}	73°7	74'1	74 ^{.5}	74 ^{.9}	75°3	75.7
·520	70°1	70.5	70.8	71.2	71.5	71.9	72·2	72 ⁶	73 ^{.0}	73°4	73°8	74 ^{.2}	74 ^{.6}	75°0	75.4
·530	69°8	70.1	70.5	70.8	71.2	71.6	71·9	72 ³	72 ^{.7}	73°1	73°5	73 ^{.9}	74 ^{.3}	74°7	75.2
·540	69°4	69.8	70.1	70.5	70.9	71.2	71·6	72 ⁰	72 ^{.4}	72°8	73°2	73 ^{.6}	74 ^{.0}	74°5	74.9
·550	69'1	69'4	69.8	70'2	70'5	70'9	71.3	71.7	72'1	72.5	72'9	73'3	73 ^{.8}	74 ^{.2}	74.6
·560	68'7	69'1	69.5	69'8	70'2	70'6	71.0	71.4	71'8	72.2	72'6	73'0	73 ^{.5}	73 ^{.9}	74.4
·570	68'4	68'8	69.1	69'5	69'9	70'3	70.7	71.1	71'5	71.9	72'3	72'8	73 ^{.2}	73 ^{.6}	74.1
·580	68'1	68'4	68.8	69'2	69'6	69'9	70.3	70.8	71'2	71.6	72'0	72'5	72 ^{.9}	73 ^{.4}	73.8
·590	67'7	68'1	68.5	68'8	69'2	69'6	70.0	70.5	70'9	71.3	71'7	72'2	72 ^{.6}	73 ^{.1}	73.6
·600	67'4	67.7	68·1	68.5	68·9	69°3	69 [.] 7	70'1	70°6	71.0	71.5	71.9	72'4	72.8	73'3
·610	67'0	67.4	67·8	68.2	68·6	69°0	69 [.] 4	69'8	70°3	70.7	71.2	71.6	72'1	72.6	73'0
·620	66'7	67.1	67·5	67.9	68·3	68°7	69 [.] 1	69'5	70°0	70.4	70.9	71.3	71'8	72.3	72'8
·630	66'4	66.7	67·1	67.5	68·0	68°4	68 [.] 8	69'2	69°7	70.1	70.6	71.1	71'5	72.0	72'5
·640	66'0	66.4	66·8	67.2	67·6	68°1	68 [.] 5	68'9	69°4	69.8	7 0.3	70.8	71'3	71.8	72'3
•650	65'7	66'1	66.5	66.9	67 · 3	67.8	68:2	68.6	69.1	69.6	70'0	70'5	71.0	71.5	72.0
•660	65'4	65'8	66.2	66.6	67·0	67.4	67:9	68.3	68.8	69.3	69'7	70'2	70.7	71.2	71.7
•670	65'0	65'4	65.9	66.3	66·7	67.1	67:6	68.0	68.5	69.0	69'5	70'0	70.5	71.0	71.5
•680	64'7	65'1	65.5	66.0	66 · 4	66.8	67:3	67.7	68.2	68.7	69'2	69'7	70.2	70.7	71.2
•690	64'4	64'8	65.2	65.6	66·1	66.5	67:0	67.4	67.9	68.4	68'9	69'4	69.9	70.4	71.0
*700	64'I	64·5	64·9	65°3	65·8	66·2	66.7	67'2	67.6	68 ·1	68.6	69 ·1	69 [.] 6	70°2	70'7
*710	63'7	64·2	64·6	65°0	65·5	65·9	66.4	66'9	67.3	67·8	68.3	68 ·9	69 [.] 4	69°9	70'5
*720	63'4	63·8	64·3	64°7	65·2	65·6	66.1	66'6	67.1	67·6	68.1	68 · 6	69 [.] 1	69°7	70'2
*730	63'I	63·5	64·0	64°4	64·9	65 ·3	65.8	66'3	66.8	67·3	67.8	68·3	68 [.] 9	69°4	69'9
*740	62'8	63·2	63·7	64°1	64·6	65· 0	65.5	66'0	66.5	67 · 0	67.5	68·0	68 [.] 6	69°1	69'7
750	62°5	62.9	63.4	63.8	64 ·3	64·7	65 [•] 2	65.7	66·2	66·7	67'2	67*8	68·3	68 ·9	69'4
760	62°2	62.6	63.0	63.5	64·0	64·4	64 [•] 9	65.4	65·9	66·4	67'0	67*5	68·1	68·6	69'2
770	61°9	62.3	62.7	63.2	63·7	64·1	64 [•] 6	65.1	65·6	66·2	66'7	67*2	67·8	68·4	68'9
780	61°5	62.0	62.4	62.9	63·4	63·9	64 [•] 3	64.9	65·4	65·9	66'4	67*0	67·5	68·1	68'7
790	61°2	61.7	62.1	62.6	63·1	63·6	64 [•] 1	64.6	65·1	65·6	66'2	66*7	67·3	67·9	68'4
.*800	60°9	61·4	61·8	62·3	62·8	63'3	63·8	64·3	64·8	65·4	65·9	66·5	67.0	67.6	68·2
**810	60°6	61·1	61·5	62·0	62·5	63'0	63·5	64·0	64·5	65·1	65·6	66·2	66.8	67.4	68:0
**820	60°3	60·8	61·2	61·7	62·2	62'7	63·2	63·7	64·3	64·8	65·4	65·9	66.5	67.1	67·7
**830	60°0	60·5	61·0	61·4	61·9	62'4	62·9	63·5	64·0	64·5	65·1	65·7	66.3	66.9	67·5
**840	59°7	60·2	60·7	61·1	61·6	62'1	62·7	63·2	63·7	64·3	64·9	65·4	66.0	66.6	67·2
*850	59'4	59'9	60·4	60·9	61·3	61·9	62·4	62·9	63·5	64.0	64.6	65·2	65·8	66·4	67.0
*860	59'1	59'6	60·1	60·6	61·1	61·6	62·1	62·6	63·2	63.7	64.3	64·9	65·5	66·1	66.7
*870	58'9	59'3	59·8	60·3	60·8	61·3	61·8	62·4	62·9	63.5	64.1	64·6	65·2	65·9	66.5
*880	58'6	59'0	59·5	60·0	60·5	61·0	61·6	62·1	62·6	63.2	63.8	64·4	65·0	65·6	66.3
*890	58'3	5 ⁸ '7	59·2	59·7	60·2	60·7	61 ·3	61·8	62·4	63.0	63.5	64·1	64·8	65·4	66.0
•900	58.0	5 ^{8·5}	5 ^{8•9}	59'4	60°0	60·5	61.0	61.6	62·1	62.7	63·3	63·9	64·5	65 ·1	65·8
•910	57.7	5 ^{8·2}	5 ^{8•7}	59'2	59°7	60·2	60.7	61.3	61·9	62.4	63·0	63·6	64·3	64·9	65·5
•920	57.4	57 ^{·9}	5 ^{8•4}	58'9	59°4	59·9	60.5	61.0	61·6	62.2	62·8	63·4	64·0	64·6	65·3
•930	57.1	57 ^{·6}	5 ^{8•1}	58'6	59°1	59·7	60.2	60.8	61·3	61.9	62·5	63·1	63·8	64·4	65·1
•940	56.9	57 ^{·3}	57•8	58'3	58°9	59·4	59.9	60.5	61·1	61.7	62·3	62·9	63·5	64·2	64·8
•950	56·6	57°1	57 ·6	58·1	58·6	59·1	59°7	60°2	60·8	61.4	62.0	62.6	63·3	63·9	64.6
•960	56·3	56°8	57·3	57 ^{.8}	58·3	5 ^{8·9}	59°4	60°0	60·6	61.2	61.8	62.4	63·0	63·7	64.4
•970	56·0	56°5	57·0	57 ^{.5}	58·1	5 ^{8·6}	59°2	59°7	60·3	60.9	61.5	62.2	62·8	63·5	64.1
•980	55·8	56°2	5 ⁶ ·7	57 ^{.3}	57·8	5 ^{8·3}	58°9	59°5	60·1	60.7	61.3	61.9	62·6	63·2	63.9
•990	55·5	56°0	5 ⁶ ·5	57 ^{.0}	57·5	5 ^{8·1}	58°6	59°2	59·8	60.4	61.0	61.7	62·3	63·0	63.7

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION

A and B							LA'	FITUI	DES.						
Cor- rection.	46°	47°	48 °	49°	5 0°	51°	52°	53°	54°	55°	56°	57°	58°	59°	60°
							Azimu	THS.							
1.00 1.02 1.04 1.06 1.08	55 ^{.2} 54 ^{.7} 54 ^{.2} 53 ^{.6} 53 ^{.1}	55 ^{.7} 55 ^{.2} 54 ^{.7} 54 ^{.1} 53 ^{.6}	° 55'7 55'2 54'7 54'1	56.7 56.2 55.7 55.2 54.7	57°3 56°7 56°2 55°7 55°2	57'8 57'3 56'8 56'3 55'8	58'4 57'9 57'4 56'9 56'4	59°0 58°5 58°0 57°5 57°5	59.6 59.1 58.6 58.1 57.6	° 59.7 59.2 58.7 58.2	60.8 60.3 59.8 59.3 58.9	° 60'9 60'5 60'0 59'5	° 62·1 61·6 61·1 60·7 60·2	° 62.7 62.3 61.8 61.4 60.9	° 63'4 63'0 62'5 62'1 61'6
1.10	52.6	53'1	53.6	54'2	54.7	55°3	55°9	56.5	57°1	57.8	5 ^{8•4}	59'1	59 ^{.8}	60'5	61·2
1.12	52.1	52'6	53.2	53'7	54.2	54°8	55'4	56.0	56°6	57.3	57•9	58'6	59 ^{.3}	60'0	60·8
1.14	51.6	52'1	52.7	53'2	53.8	54°3	54'9	55.5	56°2	56.8	57•5	58'2	58 ^{.9}	59'6	60·3
1.18	51.1	51'7	52.2	52'7	53.3	53°9	54'5	55.1	55°7	56.4	57•0	57'7	5 ^{8.4}	59'1	59·9
1.18	50.7	51'2	51.7	52'3	52.8	53°4	54'0	54.6	55°3	55.9	56•6	57'3	5 ^{8.0}	5 ^{8'} 7	59·5
1°20	50°2	50.7	51'2	51.8	52°4	52.9	53'5	54'2	54·8	55°5	56°1	56·8	57'5	5 ^{8•} 3	59°0
1°22	49'7	50.2	50'8	51.3	51°9	52.5	53'1	53'7	54·4	55°0	55'7	56·4	57'1	57 [•] 9	58°6
1°24	49'3	49.8	50'3	50.9	51°4	52.0	52'6	53'3	53·9	54°6	55'3	56·0	56'7	57 [•] 4	58°2
1°26	48'8	49.3	49'9	50.4	51°0	51.6	52'2	52'8	53·5	54°1	54'8	55·5	56'3	57 [•] 0	57°8
1°28	48'4	48.9	49'4	50.0	50°6	51.1	51'8	52'4	53·0	53°7	54'4	55·1	55'9	56•6	57°4
1`30	47'9	48.4	49 ^{.0}	49'5	50'1	50'7	51'3	52.0	52.6	53'3	54'0	54'7	55'4	56·2	57°0
1`32	47'5	48.0	4 ^{8.5}	49'1	49'7	50'3	50'9	51.5	52.2	52'9	53'6	54'3	55'0	55·8	56°6
1`34	47'1	47.6	4 ^{8.1}	4 ⁸ '7	49'3	49'9	50'5	51.1	51.8	52'5	53'2	53'9	54'6	55·4	55°2
1`36	46'6	47.2	47 ^{.7}	4 ⁸ '3	48'8	49'4	50'1	50.7	51.4	52'0	52'7	53'5	54'2	55·0	55°8
1`38	46'2	46.7	47 ^{.3}	47' ⁸	48'4	49'0	49'6	50.3	51.0	51'6	52'3	53'1	53'8	54·6	55°4
1'40	45 [.] 8	46·3	46·9	47'4	48°0	48.6	49 ^{•2}	49'9	50'5	51°2	51.9	52.7	53'4	54°2	55°0
1'42	45 [.] 4	45·9	46·5	47'0	47°6	48.2	48 ^{•8}	49'5	50'1	50°8	51.5	52.3	53'0	53°8	54°6
1'44	45 [.] 0	45·5	46·1	46'6	47°2	47.8	48 ^{•4}	49'1	49'8	50°4	51.2	51.9	52'7	53°4	54°2
1'46	44 [.] 6	45·1	45·7	46'2	46°8	47.4	48 ^{•0}	48'7	49'4	50°1	50.8	51.5	52'3	53°1	53°9
1'48	44 [.] 2	44·7	45·3	45'8	46°4	47.0	47 ^{•7}	4 ⁸ '7	49'0	49°7	50.4	51.1	51'9	52°7	53°5
1·50	43 ^{.8}	44'3	44 ^{.9}	45°5	46 °0	46'7	47'3	47 9	48.6	49'3	50°0	50.8	51.5	52'3	53'I
1·52	43 ^{.4}	44'0	44 ^{.5}	45°1	45 °7	46'3	46'9	47 5	48.2	48'9	49°6	50.4	51.1	51'9	52'8
1·54	43 ^{.1}	43'6	44 ^{.1}	44°7	45°3	45'9	46'5	47 2	47.8	48'5	49°3	50.0	50.8	51'6	52'4
1·56	42 ^{.7}	43'2	43 ^{.8}	44°3	44°9	45'5	46'2	46 8	47.5	48'2	48°9	49.6	50.4	51'2	52'0
1·58	42 ^{.3}	42'9	43 ^{.4}	44°0	44°6	45'2	45'8	46 4	47.1	47'8	48°5	49.3	50.1	50'9	51'7
1.60	42.0	42.5	43°0	43 ^{.6}	44.2	44'8	45'4	46'1	46·8	47`5	48·2	48.9	49'7	50°5	51.3
1.62	41.6	42.1	42°7	43 ^{.3}	43.8	44'4	45'1	45'7	46·4	47`1	47·8	48.6	49'4	50°2	51.0
1.64	41.3	41.8	42°3	42 ^{.9}	43.5	44'1	44'7	45'4	46·1	46`8	47·5	48.2	49'0	49°8	50.6
1.66	40.9	41.5	42°0	42 ^{.6}	43.1	43'7	44'4	45'0	45·7	46`4	47·1	47.9	48'7	49°5	50.3
1.68	40.6	41.1	41°7	42 ^{.2}	42.8	43'4	44'0	44'7	45·4	46`1	46·8	47.5	4 ⁸ '3	49°1	50.0
1.70	40'3	40.8	41.3	41.9	42.5	43'I	43'7	44'3	45 ^{.0}	45'7	46.4	47 ·2	48.0	48.8	49 ^{.6}
1.72	39'9	40.4	41.0	41.5	42.1	42'7	43'4	44'0	44 [.] 7	45'4	46.1	46·9	47.7	48.5	49 ^{.3}
1.74	39'6	40.1	40.7	41.2	41.8	42'4	43'0	43'7	44 [.] 4	45'1	45.8	46·5	47.3	48.1	49 ^{.0}
1.76	39'3	39.8	40.3	40.9	41.5	42'I	42'7	43'4	44 ^{.0}	44'7	45.5	46·2	47.0	47.8	48 ^{.7}
1.78	39'0	39.5	40.0	40.6	41.2	41'8	42'4	43'0	43 [.] 7	44'4	45.1	.45·9	46.7	47.5	48 ^{.3}
1·80	38.7	39.2	39'7	4 0'3	40.8	41.4	42'I	42'7	43'4	44'I	44 ^{.8}	45 ^{.6}	46.4	47·2	48°0
1·82	38.3	38.9	39'4	39'9	40.5	41.1	41'7	42'4	43'1	43'8	44 ^{.5}	45 ^{.3}	46.0	46·9	47°7
1·84	38.0	38.6	39'1	39'6	40.2	40.8	41'4	42'1	42'8	43'5	44 ^{.2}	44 ^{.9}	45.7	46·5	47°4
1·86	37.7	38.2	38'8	39'3	39.9	40.5	41'1	41'8	42'4	43'I	43 ^{.9}	44 ^{.6}	45.4	46·2	47°1
1·88	37.4	38.0	38'5	39'0	39.6	40.2	40'8	41'5	42'1	42'8	43 ^{.6}	44 ^{.3}	45.1	45·9	46°8
1.90	37°1	37°7	38·2	38·7	39'3	39'9	40°5	41·2	41.8	42.5	43'3	44.0	44 ^{.8}	45 ^{.6}	46 ·5
1.92	36°9	37°4	37·9	38·4	39'0	39'6	40°2	40·9	41.5	42.2	43'0	43.7	44 ^{.5}	45 ^{.3}	46·2
1.94	36°6	37°1	37·6	38·2	3 ⁸ '7	39'3	39°9	40·6	41.2	41.9	42'7	43.4	44 ^{.2}	45 ^{.0}	45 ·9
1.96	36°3	36°8	37·3	37·9	3 ⁸ '4	39'0	39°6	40·3	41.0	41.7	42'4	43.1	43 ^{.9}	44 ^{.7}	45·6
1.98	36°0	36°5	37·0	37·6	3 ⁸ '2	3 ⁸ '7	39°4	40·0	40.7	41.4	42'1	42.8	43 ^{.6}	44 ^{.4}	45 · 3

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Table	С

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

Azimuth is named N or S according to the name of the A and B correction.

1.	A and B							LAT	ITUD	ES.						
Section Section	Cor- rection.	46 °	47°	48 °	49°	50°	51°	52°	53°	54°	55°	56°	57°	58°	59°	60°
	, ,	0 1	• •	0 1	0 1	0	A	ZIMU	CHS.	•	0		•			
the second s	2.00	35'7	36·2	36·8	37'3	37.9	38·5	39'I	39 ^{.7}	40 [.] 4	41°1	41.8	42.6	43'3	44°2	45 ^{.0}
	2.05	35'1	35·6	36·1	36'6	37.2	37·8	38'4	39 ^{.0}	39 [.] 7	40°4	41.1	41.8	42'6	43°4	44 ^{.3}
	2.10	34'4	34·9	35·4	36'0	36.5	37·1	37'7	38 ^{.4}	39 [.] 0	39°7	40.4	41.2	41'9	42°8	43 ^{.6}
	2.15	33'8	34 ·3	34·8	35'3	35.9	36·5	37'I	37 ^{.7}	3 ^{8.} 4	39°0	39.8	40.5	41'3	42°1	42 ^{.9}
	2.20	33'2	33·7	34·2	34'7	35.3	35·8	36'4	37 ^{.1}	37 [.] 7	38°4	39.1	39.8	40'6	41°4	42 ^{.3}
The second secon	2·25	32.6	33'I	33.6	34'I	34'7	3 5'2	35.8	36.4	37'1	37.8	38·5	39 °2	40°0	40.8	41.6
	2·30	32.0	32'5	33.0	33'5	34'1	34'6	35.2	35.8	36'5	37.2	37·9	38°6	39°4	40.2	41.0
	2·40	31.0	31'4	31.9	32'4	33'0	33'5	34.1	34.7	35'3	36.0	36·7	37°4	38°2	39.0	39.8
	2·50	29.9	30'4	30.9	31'4	31'9	32'4	33.0	33.6	34'2	34.9	35·6	36°3	37°0	37.8	38.7
	2·60	29.0	29'4	29.9	30'4	30'9	31'4	32.0	32.6	33'2	33.8	34·5	35°2	36°0	36.8	37.6
H	2.70	28·1	28·5	29.0	29'4	30°0	30'5	31.0	31.6	32.2	32.9	33`5	34 .2	35°0	35'7	36·5
	2.80	27·2	27·6	28.1	28'6	29°1	29'6	30.1	30.7	31.3	31.9	32'6	33.3	34°0	34'7	35·5
	2.90	26·4	26·8	27.3	27'7	28°2	28'7	29.3	29.8	30.4	31.0	31'7	32.3	33°1	33'8	34·6
	3.00	25·6	26·0	26.5	26'9	27°4	27'9	28.4	29.0	29.6	30.2	30'8	31.5	32°2	32'9	33·7
	3.10	24·9	25·3	25.7	26'2	26°6	27'1	27.7	28.2	28.8	29.4	30'0	30.6	3 1°3	32'1	32·8
The second se	3·20	24 ·2	24.6	25.0	25 ^{.5}	25.9	26.4	26·9	27'4	28.0	28.6	29·2	29'8	30'5	31.2	32.0
	3·30	23·6	24.0	24.4	24 ^{.8}	25.2	25.7	26·2	26'7	27.3	27.8	28·5	29'1	29'8	30.5	31.2
	3·40	22·9	23.3	23.7	24 ^{.1}	24.6	25.0	25·5	26'0	26.6	27.1	27·7	28'4	29'0	29.7	30.5
	3·60	21·8	22.2	22.5	22 ^{.9}	23.4	23.8	24·3	24'8	25.3	25.8	26·4	27'0	27'7	28.3	29.1
	3·80	20·7	21.1	21.5	21 ^{.9}	22.3	22.7	23·1	23'6	24.1	24.6	25·2	25'8	26'4	27.1	27.8
the state of the state of the	4'00	19 ^{.8}	20'I	20'5	20'9	21.3	21.7	22°1	22.6	23.0	23.6	24'I	24.7	25'3	25.9	26.6
	4'20	18 ^{.9}	19'2	19'6	19'9	20.3	20.7	21°1	21.6	22.1	22.5	23'I	23.6	24'2	24.8	24.5
	4'40	18 ^{.1}	18'4	18'8	19'1	19.5	19.9	20 3	20.7	21.1	21.6	22'I	22.7	23'2	23.8	24.4
	4'60	17 ^{.4}	17'7	18'0	18'3	18.7	19.1	19°4	19.9	20 3	20.8	21'2	21.8	22'3	22.9	23.5
	4'80	16 ^{.7}	17'0	17'3	17'6	18.0	18.3	18°7	19.1	19.5	20.0	20'4	20.9	21'5	22.0	22.6
and the second second second	5.00	16·1	16.3	16 ^{.6}	17.0	17.3	17.6	18.0	18.4	18.8	19 [.] 2	19.7	20.2	20.7	21·2	21.8
	5.20	14·7	14.9	15 ^{.2}	15.5	15.8	16.1	16.5	16.8	17.2	17 [.] 6	18.0	18.5	18.9	19·4	20.0
	6.00	13·5	13.7	14 ^{.0}	14.3	14.5	14.8	15.1	15.5	15.8	16 [.] 2	16.6	17.0	17.5	17·9	18.4
	6.20	12·5	12.7	12 ^{.9}	13.2	13.5	13.7	14.0	14.3	14.7	15 [.] 0	15.4	15.8	16.2	16·6	17.1
	7.00	11·6	11.8	12 ^{.1}	12.3	12.5	12.8	13.1	13.4	13.7	14 [.] 0	14.3	14.7	15.1	15·5	15.9
NAMES OF TAXABLE PARTY.	8.0	10.2	10.4	10 ^{.6}	10 ^{.8}	9.8	11.2	11.5	11.7	12.0	12·3	12.6	12.9	13.3	13.6	14.0
	9.0	9.1	9.3	9 ^{.4}	9 ^{.6}	9.8	10.0	10.2	10.5	10.7	11·0	11.2	11.5	11.8	12.2	12.5
	10.0	8.2	8.3	8 ^{.5}	8 ^{.7}	8.8	9.0	9.2	9.4	9.7	9·9	10.1	10.4	10.7	11.0	11.3
	11.0	7.5	7.6	7 ^{.7}	7 ^{.9}	8.0	8.2	8.4	8.6	8.8	9·0	9.2	9.5	9.7	10.0	10.3
	12.0	6.8	7.0	7 ^{.1}	7 ^{.2}	7.4	7.5	7.7	7.9	8.1	8·3	8.5	8.7	8.9	9.2	9.5
A THE MAN TO A	13.0	6·3	6·4	6·6	6.7	6·8	7:0	7'1	7'3	7'5	7 ^{.6}	7 ^{.8}	8.0	8·3	8·5	8·7
	15.0	5·5	5·6	5·7	5.8	5·9	6:0	6'2	6'3	6'5	6 ^{.6}	6 ^{.8}	7.0	7·2	7·4	7·6
	17.0	4·8	4·9	5·0	5.1	5·2	5:3	5'5	5'6	5'7	5 ^{.9}	6 ^{.0}	6.2	6·3	6·5	6·7
	20.0	4·1	4·2	4·3	4.4	4·4	4:5	4'6	4'7	4'9	5 ^{.0}	5 ^{.1}	5.2	5·4	5·5	5·7
	25.0	3·3	3·4	3·4	3.5	3·6	3:6	3'7	3'8	3'9	4 ^{.0}	4 ^{.1}	4.2	4·3	4 4	4·6
A State of the sta	30°0 40°0 50°0 70 °0 100°0	2.7 2.1 1.6 1.2 0.8	2.8 2.1 1.7 1.2 0.8	2.9 2.1 1. 7 0.9	2.9 2.2 1.7 1.2 0.9	3.0 2.2 1.8 1.3 0.9	3.0 2.3 1.8 1.3 0.9	3.1 5.3 1.3 0.3	3'2 2'4 1'9 1'4 1'0	3'2 2'4 1'9 1'4 1'0	3'3 2'5 2'0 1'4 1'0	3'4 2'6 2'0 1'5 1'0	3'5 2'6 2'1 1'5 1'1	3.6 2.7 2.2 1.5 1.1	3°7 2.8 2.2 1.6 1.1	3.8 2.9 2.3 1.6 1.1
Service and a se	150°0 200°0 300°0 400°0 800°0	0'5 0'4 0'3 0'2 0'1	0 ^{.6} 0 [.] 4 0 [.] 3 0 [.] 2 0 [.] 1	0.6 0.4 0.3 0.2 0.1	0 [.] 6 0 [.] 4 0 [.] 3 0 [.] 2 0 [.] 1	0.6 0.4 0.3 0.2 0.1	0.6 0.2 0.3 0.1	0.6 0.2 0.3 0.1	0.0 0.2 0.3 0.1	0.6 0.2 0.3 0.1	0.7 0.2 0.3 0.1	0'7 0'5 0'3 0'3 0'1	0.7 0.5 0.4 0.3 0.1	0.7 0.5 0.4 0.3 0.1	0.7 0.6 0.4 0.3 0.1	0.8 0.6 0.4 0.3 0.1

4-Azimuth

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

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45 77'7 78'1 78'5 78'8 79'2 79'6 80'0 80'4 80'8 81'0 81'3 81'5 81'7 81'9 82'1 46 77'4 77'8 78'2 78'6 70'0 70'4 70'8 80'2 80'6 80'8 81'1 81'3 81'5 81'7 81'9 82'1
·47 77.2 77.6 78.0 78.4 78.8 79.2 79.6 80.0 80.4 80.7 80.9 81.1 81.3 81.5 81.7
48 76'9 77'3 77'7 78'1 78'5 79'0 79'4 79'8 80'2 80'5 80'7 80'9 81'1 81'3 81'6 40 76'6 77'0 77'5 77'0 78'3 78'7 70'2 70'6 80'0 80'3 80'5 80'7 80'0 81'2 81'4
·50 76'4 76'8 77'2 77'6 78'I 78'5 78'0 70'4 70'8 80'I 80'3 80'5 80'8 81'0 81'2
·51 76·1 76·5 77.0 77·4 77·8 78·3 78·7 79·2 79·6 79·9 80·1 80·3 80·6 80·8 81·0
52 75.9 70.3 70.7 77.2 77.0 78.1 78.5 79.0 79.4 79.7 79.9 80.2 80.4 80.0 80.9 53 75.6 76.0 76.5 76.9 77.4 77.8 78.3 78.8 70.2 79.5 79.7 80.0 80.2 80.5 80.7
·54 75·3 75·8 76·2 76·7 77·1 77·6 78·1 78·6 79·0 79·3 79·5 79·8 80·0 80·3 80·5

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

A and B							\mathbf{LA}	TITUI	DES.						
Cor- rection.	61 °	62°	63°	64 °	65°	66°	67°	68°	69°	69 <u>1</u> °	70°	70 <u>3</u> °	71°	71 <u>1</u> °	72°
			0	0	0		Azim	JTHS.							
•55	75°1	75°5	76.0	76.4	76.9	77°4	77'9	78.4	78.8	79' 1	79°3	79.6	79*8	80°1	80°4
•56	74°8	75°3	75.7	76.2	76.7	77°2	77'7	78.2	78.7	78' 9	79°2	79.4	79*7	79°9	80°2
•57	74°6	75°0	75.5	76.0	76.5	76°9	77'4	77.9	78.5	78'7	79°0	79.2	79*5	79'7	80°0
•58	74°3	74°8	75.2	75.7	76.2	76°7	77'2	77.7	78.3	78'5	78°8	79.0	79*3	79'6	79°8
•58	74°0	74°5	75.0	75.5	76.0	76°5	77'0	77.5	78.1	78'3	78°6	78.9	79*1	79'4	79°7
•60 •61 •62 •63 •64	73*8 73*5 73*3 73*0 72*8	74°3 74°0 73°8 73°5 73°5 73°3	74 ^{.8} 74 ^{.5} 74 ^{.3} 74 ^{.0} 73 ^{.8}	75°3 75°0 74°8 74°6 74°3	75°8 75°5 75°3 75°1 74°9	76·3 76·1 75·8 75·6 75·4	76.8 76.6 76.4 76.2 76.0	77°3 77°1 76°9 76°7 76°5	77'9 77'7 77'5 77'3 77'1	78.1 77.9 77.7 77.6 77.4	78.4 78.2 78.0 77.8 77.7	78.7 78.5 78.3 78.1 77.9	78.9 78.8 78.6 78.4 78.2	79°2 79°0 78°9 77°7 78°5	79°5 79°3 79°2 79°0 78°8
•65 •66 •67 •68 •69	72°5 72°3 72°0 71°8 71°5	73°0 72°8 72°5 72°3 72°1	73.6 73.3 73.1 72.8 72.6	74'I 73'9 73'6 73'4 73'2	74°6 74°4 74°2 74°0 73°7	75 ^{•2} 75 ^{•0} 74 ^{•8} 74 ^{•5} 74 ^{•3}	75°7 75°5 75°3 75°1 74°9	76·3 76·1 75·9 75·7 75·5	76·9 76·7 76·5 76·3 76·1	77 °2 77 °0 76•8 76•6 76•6	77°5 77°3 77°1 76°9 76°7	77*8 77*6 77*4 77*2 77*0	78°1 77°9 77°7 77°5 77°3	78·3 78·2 78·0 77·8 77·8 77·7	78•6 78•5 78•3 78•1 78•0
•70	71·3	71.8	72°4	72°9	73°5	74°1	74°7	75°3	75'9	76•2	76•5	76.8	77°2	77°5	77*8
•71	71·0	71.6	72°1	72°7	73°3	73°9	74°5	75°1	75'7	76•0	76•4	76.7	77°0	77°3	77*6
•72	70·8	71.3	71°9	72°5	73°1	73°7	74°3	74°9	75'5	75•8	76•2	76.5	76°8	77°1	77*5
•73	70·5	71.1	71°7	72°3	72°9	73°5	74°1	74°7	75'3	75•7	76•0	76.3	76°6	77°0	77*3
•74	70·3	70.8	71°4	72°0	72°6	73°2	73°9	74°5	75'1	75•5	75•8	76.1	76°5	76°8	77*1
•75	70°0	70°6	71.2	71.8	72°4	73°0	73'7	74°3	75°0	75°3	75°6	75°9	76·3	76.6	77°0
•76	69°8	70°4	71.0	71.6	72°2	72°8	73'5	74°1	74°8	75°1	75°4	75°8	76·1	76.4	76•8
•77	69°5	70°1	70.7	71.3	72°0	72°6	73'3	73°9	74°6	74°9	75°2	75°6	75·9	76.3	76•6
•78	69°3	69°9	70.5	71.1	71°8	72°4	73'1	73°7	74°4	74°7	75°1	75°4	75·8	76.1	76•4
•79	69°0	69°7	70.3	70.9	71°5	72°2	72'8	73°5	74°2	74°5	74°9	75°2	75·6	75.9	76•3
·80	68·8	69 ° 4	70°0	70°7	71.3	72.0	72°6	73'3	74'0	74°3	74°7	75°0	75°4	75 ^{•8}	76°1
·81	68·6	69 ° 2	69°8	70°5	71.1	71.8	72°4	73'1	73'8	74°2	74°5	74°9	75°2	75 ^{•6}	75°9
·82	68·3	68 ° 9	69°6	70°2	70.9	71.6	72°2	72'9	73'6	74°0	74°3	74°7	75°1	75 ^{•4}	75°8
·83	68·1	68 ° 7	69°4	70°0	70.7	71.3	72°0	72'7	73'4	73°8	74°2	74°5	74°9	75 ^{•2}	75°6
·84	67·8	68°5	69°1	69°8	70.5	71.1	71°8	72'5	73'2	73°6	74°0	74°3	74°7	75 ^{•1}	75°4
•85	67.6	68·2	68·9	69°6	70°2	70'9	71.6	72.3	73'I	73'4	73 ^{.8}	74°2	74°5	74'9	75°3
•86	67.4	68·0	68·7	69°3	70°0	70'7	71.4	72.1	72'9	73'2	73 ^{.6}	74°0	74°4	74'7	75°1
•87	67.1	67·8	68·4	69°1	69°8	70'5	71.2	71.9	72'7	73'1	73 ^{.4}	73°8	74°2	74'6	75°0
•88	66.9	67·6	68·2	68°9	69°6	70'3	71.0	71.8	72'5	72'9	73 ^{.2}	73°6	74°0	74'4	74°8
•89	66.7	67·3	68·0	68°7	69°4	70'1	70.8	71.6	72'3	72'7	73 ^{.1}	73°5	73°8	74'2	74°6
•90	66•4	67'I	67.8	68·5	69·2	69'9	70°6	71.4	72°1	72.5	72 · 9	73'3	73°7	74 ^{•1}	74°5
•91	66•2	66'9	67.6	68·3	69·0	69'7	70°4	71.2	71°9	72.3	72·7	73'1	73°5	73 ^{•9}	74°3
•92	66•0	66'6	67.3	68·0	68·8	69'5	70°2	71.0	71°8	72.1	72·5	72'9	73°3	73 ^{•7}	74°1
•93	65•7	66'4	67.1	67·8	68·5	69'3	70°0	70.8	71°6	72.0	72·4	72'8	73°2	73 ^{•6}	74°0
•94	65•5	66'2	66.9	67·6	68·3	69'1	69°8	70.6	71°4	71.8	72·2	72'6	73°0	73 ^{•4}	73°8
*95	65°3	66.0	66•7	67.4	68·1	68.9	69°6	70'4	71.2	71.6	72.0	72'4	72.8	73 ²	73.6
*96	65°0	65.7	66•5	67.2	67·9	68.7	69'4	70'2	71.0	71.4	71.8	72'2	72.6	73 ¹	73.5
*97	64°8	65.5	66•2	67.0	67·7	68.5	69'2	70'0	70.8	71.2	71.6	72'1	72.5	72 ⁹	73.3
*98	64°6	65.3	66•0	66.8	67·5	68.3	69'0	69'8	70.6	71.1	71.5	71'9	72.3	72 ⁷	73.2
*99	64°4	65.1	65•8	66.5	67·3	68.1	68'9	69'7	70.5	70.9	71.3	71'7	72.1	72 ⁶	73.0
1°00	64°1	64·9	65.6	66'3	67°1	67.9	68.7	69*5	70'3	70'7	71·1	71.5	72.0	72.4	72.8
1°02	63°7	64·4	65.2	65'9	66°7	67.5	68.3	69*1	69'9	70'3	70·8	71.2	71.6	72.1	72.5
1°04	63°2	64·0	64.7	65'5	66°3	67.1	67.9	68*7	69'6	70'0	70·4	70.9	71.3	71.7	72.2
1°06	62°8	63·5	64.3	65'1	65°9	66.7	67.5	68*3	69'2	69'6	70·1	70.5	71.0	71.4	71.9
1°08	62°4	63·1	63.9	64'7	65°5	66.3	67.1	68*0	68'8	69'3	69·7	70.2	70.6	71.1	71.5
1.10 1.12 1.14 1.16 1.18	61.9 61.5 61.1 60.6 60.2	62.7 62.3 61.8 61.4 61.0	63·5 63·0 62·6 62·2 61·8	64·3 63·9 63·4 63·0 62·6	65°1 64°7 64°3 63°9 63°5	65 ·9 65·5 65·1 64·7 64 · 4	66•7 66•4 66•0 65•6 65•2	67.6 67.2 66.9 66.5 66.2	68.5 68.1 67.8 67.4 67.1	68.6 68.2 67.9 67.5	09°4 69°0 68°7 68°4 68°0	09°8 69°5 69°2 68°8 68°5	70°3 70°0 69°6 69°3 69°0	70'8 70'4 70'1 69'8 69'5	70.9 70.6 70.3 70.0

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

1	A and B							LA'	FITUE	ES.						
	Cor- rection.	61°	62°	63°	64 °	65°	66°	67°	68°	69 °	69 ⁴ °	70°	70 ¹ 2°	71°	71 <u>1</u> °	720
	,	0	0	0	0	o	•	Azimu	oTHS.	0	0	0	0	, 0	0	
	1·20	59*8	60°6	61°4	62·3	63·1	64.0	64·9	65·8	66•7	67·2	67 . 7	68·2	68•7	69·2	69·7
	1·22	59*4	60°2	61°0	61·9	62·7	63.6	64·5	65·4	66•4	66 ·9	67 . 4	67·8	68•3	68·8	69·3
	1·24	59*0	59°8	60°6	61·5	62·3	63.2	64·1	65·1	66•0	66·5	67.0	67·5	68•0	68·5	69·0
	1·26	58*6	59°4	60°2	61·1	62·0	62.9	63·8	64·7	65•7	66·2	66.7	67·2	67•7	68·2	68·7
	1·28	58*2	59°0	59°8	60·7	61·6	62.5	63·4	64·4	65•4	65·9	66.4	66 ·9	67•4	67·9	68·4
N. Contraction	1*30	57°8	58.6	59 ·5	60°3	61·2	62·1	63°1	64.0	65.0	65·5	66 ·0	66·5	67°1	67.6	68·1
	1*32	57°4	58.2	59 · 1	59°9	60·8	61·8	62°7	63.7	64.7	65·2	65 · 7	66·2	66°7	67.3	67·8
	1*34	57°0	57.8	58 7	59°6	60·5	61·4	62°4	63.3	64.3	64·9	65 · 4	65·9	66°4	67.0	67·5
	1*36	56°6	57.4	58 ·3	59°2	60·1	61·1	62°0	63.0	64.0	64·5	65 · 1	65·6	66°1	66.7	67·2
	1*38	56°2	57.1	57 · 9	58°8	59·7	60·7	61°7	62.7	63.7	64·2	64 · 7	65·3	65°8	66.4	66·9
	1.40	55.8	56°7	57°6	58.5	59'4	60'3	61·3	62°3	63·4	63·9	64·4	65.0	65·5	66•0	66•6
	1.42	55.5	56°3	57°2	58.1	59'0	60'0	61·0	62°0	63·0	63·6	64·1	64.6	65·2	65•7	66•3
	1.44	55.1	55°9	56°8	57.7	58'7	59'6	60·6	61°7	62·7	63·2	63·8	64.3	64·9	65•4	66•0
	1.46	54.7	55°6	56°5	57.4	58'3	59'3	60·3	61°3	62·4	62·9	63·5	64.0	64·6	65•1	65•7
	1.48	54.3	55°2	56°1	57.0	58'0	59'0	60·0	61°0	62·1	62·6	63·2	63.7	64·3	64•8	65• 4
	1·50	54°0	54°8	55°7	56•7	57.6	58.6	59·6	60 °7	61.7	62·3	62.8	63.4	64°0	64 •5	65·1
	1·52	53°6	54°5	55°4	56•3	57.3	58.3	59·3	60°3	61.4	62·0	62.5	63.1	63°7	64•3	64·8
	1·54	53°3	54°1	55°0	56•0	56.9	57.9	59·0	60°0	61.1	61·7	62.2	62.8	63°4	64•0	64·6
	1·56	52°9	53°8	54°7	55•6	56.6	57.6	58·6	59°7	60.8	61·4	61.9	62.5	63°1	63•7	64·3
	1·58	52°5	53°4	54°3	55•3	56.3	57.3	58·3	59°4	60.5	61·0	61.6	62.2	62°8	63•4	64·0
	1.60	52°2	53'I	54.0	55°0	55'9	56 ·9	58.0	59°1	60°2	60°7	61·3	61.9	62.5	63°1	63.7
	1.62	51°9	52'7	53.7	54°6	55'6	56·6	57.7	58°7	59°9	60°4	61·0	61.6	62.2	62°8	63.4
	1.64	51°5	52'4	53.3	54°3	55'3	56·3	57.3	58°4	59°6	60°1	60·7	61.3	61.9	62°5	63.1
	1.66	51°2	52'I	53.0	54°0	54'9	56·0	57.0	58°1	59°3	59°8	60·4	61.0	61.6	62°2	62.8
	1.68	50°8	51'7	52.7	53°6	54'6	55·7	56.7	57°8	58°9	59°5	60·1	60.7	61.3	61°9	62.6
a statement of the stat	1.70 1.72 1.74 1.76 1.78	50°5 50°2 49°9 49°5 49°2	51°4 51°1 50°8 50°4 50°1	52°3 52°0 51°7 51°4 51°1	53'3 53'0 52'7 52'3 52'0	54°3 54°0 53°7 53°4 53°0	55°3 55°0 54°7 54°4 54°1	56°4 56°1 55°8 55°5 55°2	57°5 57°2 56°9 56°6 56°3	58.6 58.4 58.1 57.8 57.5	59·2 58·9 58·6 58·4 58·1	59 ^{.8} 59 ^{.5} 59 ^{.2} 59 ^{.0} 5 ^{8.7}	60°4 60°1 59°9 59°6 59°3	61.0 60.8 60.2 59.9	61.7 61.4 61.1 60.8 60.5	62·3 62·0 61·7 61·5 61·2
and	1.80	48·9	49 ^{.8}	50°7	51°7	52.7	53·8	54°9	56.0	57°2	57.8	58°4	59°0	59.6	60·3	60°9
	1.82	48·6	49 ^{.5}	50°4	51°4	52.4	53·5	54°6	55.7	56°9	57.5	58°1	58°7	59.4	60·0	60°6
	1.84	48·3	49 ^{.2}	50°1	51°1	52.1	53·2	54°3	55.4	56°6	57.2	57°8	58°4	59.1	59·7	60°4
	1.86	48·0	48 ^{.9}	49°8	50°8	51.8	52·9	54°0	55.1	56°3	56.9	57°5	58°2	58.8	59·5	60°1
	1.88	47·7	48 ^{.6}	49°5	50°5	51.5	52·6	53°7	54.8	56°0	56.6	57°3	57°9	58.5	59·2	59°8
	1.90	47°4	48·3	49'2	50°2	51°2	52°3	53°4	54.6	55°7	56°4	57 °0	57.6	58·3	58·9	59.6
	1.92	47°1	48·0	48'9	49°9	50°9	52°0	53°1	54.3	55°5	56°1	56 °7	57.3	58·0	58·6	59.3
	1.94	46°8	47·7	48'6	49°6	50°7	51°7	52°8	54.0	55°2	55°8	56°4	57.1	57·7	58·4	59.1
	1.96	46°5	47·4	48'3	49°3	50°4	51°4	52°6	53.7	54°9	55°5	56°2	56.8	57·5	58·1	58.8
	1.98	46°2	47·1	48'0	49°0	50°1	51°2	52°3	53.4	54°6	55°3	55°9	56.5	57·2	57·9	58.5
The second se	2'00	45°9	46•8	47.8	48·8	49 ^{.8}	50 ·9	52°0	53°2	54°4	55°0	55°6	56°3	56·9	57.6	58·3
	2'05	45°2	46•1	47.1	48·1	49 ^{.1}	50·2	51°3	52°5	53°7	54°3	55°0	55°6	56·3	57.0	57·6
	2'10	44°5	45•4	46.4	47·4	4 ^{8.4}	49 · 5	50°6	51°8	53°0	53°7	54°3	55°0	55·6	56.3	57·0
	2'15	43°8	44•7	45.7	46·7	47 ^{.7}	48·8	50°0	51°2	52°4	53°0	53°7	54°3	55·0	55.7	56·4
	2'20	43°2	44•1	45.0	46·0	47 ^{.1}	48·2	49°3	50°5	51°7	52°4	53°0	53°7	54·4	55.1	55·8
	2*25	42°5	43°4	44°4	45°4	46•4	47°5	48.7	49 '9	51°1	51.8	52°4	53·1	53.8	54°5	55°2
	2*30	41°9	42°8	43°8	44°8	45•8	46°9	48.1	49'3	50°5	51.1	51°8	52·5	53.2	53°9	54°6
	2*40	40'7	41°6	42°5	43°5	44•6	45°7	46.8	48'0	49°3	50.0	50°6	51·3	52.0	52°7	53°4
	2*50	39°5	40°4	41°4	42°4	43•4	44°5	45.7	46'9	48°1	48.8	49° 5	50·2	50.9	51°6	52°3
	2*60	38°4	39°3	40°3	41°3	42•3	43°4	44.5	45'8	47°0	47.7	48°4	49·0	49.8	50°5	51°2
	2'70	37'4	38•3	39°2	40.2	41.2	42°3	43°5	44'7	45°9	46.6	47°3	48.0	48.7	49'4	50°2
	2'80	36'4	37•3	38°2	39.2	40.2	41°3	42°4	43'6	44°9	45.6	46°2	46.9	47.6	48'4	49°1
	2'90	35'4	36•3	37°2	38.2	39.2	40°3	41°4	42'6	43°9	44.6	45°2	45.9	46.6	47'4	48°1
	3'00	34'5	35•4	36°3	37.2	38.3	39°3	40°5	41'7	42°9	43.6	44°3	45.0	45.7	46'4	47°2
	3'10	33'6	34•5	35°4	36.3	37.4	38°4	39°5	40'7	42°0	42.6	43°3	44.0	44.7	45'5	46°2

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Table C.

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

A and B							LA'	FITUE	ES.						
Cor- rection.	61°	62°	63°	64°	65°	66°	67°	68°	69°	69 <u>1</u> °	70°	70 <u>1</u> °	71°	71 <u>3</u> °	720
		0	0	0			Azimu	THS.	0	0				0	
3°20 3°30 3°40 3°60 3°80	32.8 32.0 31.2 29.8 28.5	33.6 32.8 32.1 30.6	34°5 33°7 32°9 31°5	35.5 34.7 33.9 32.4	36·5 35·6 34·8 33·3	37.5 36.7 35.9 34.3	38.7 37.8 37.0 35.4	39°8 39°0 38°1 36°6	41°1 40°2 39°4 37°8	41.7 40.9 40.0 38.4 36.0	42°4 41°5 40°7 39°1	43°1 42°2 41°4 39°8	43.8 42.9 42.1 40.5 38.0	44°6 43°7 42°8 41°2	45'3 44'4 43'6 42'0
4.00	27.3	28.0	28.8	29°7	30.6	31.6	32.6	33'7	34'9	35°5	36°2	36.8	37°5	38·2	39°0
4.20	26.2	26.9	27.7	28°5	29.4	30.3	31.4	32'4	33'6	34°2	34°8	35.5	36°2	36·9	37°6
4.40	25.1	25.8	26.6	27°4	28.3	29.2	30.2	31'2	32'4	33°0	33°6	34.2	34°9	35·6	36°3
4.60	24.2	24.8	25.6	26°4	27.2	28.1	29.1	30'1	31'2	31°8	32°4	33.1	33°7	34·4	35°1
4.80	23.3	23.9	24.6	25°4	26.2	27.1	28.1	29'1	30'2	30°7	31°3	32.0	32°6	33·3	34°0
5.00	22'4	23°1	23.8	24.5	25°3	26·2	27·1	28·1	29°2	29.7	30°3	30'9	31.6	32°2	32°9
5.20	21'6	22°3	23.0	23.7	24°5	25·3	26·2	27·2	28°2	28.8	29°3	29'9	30.6	31°2	31°9
5.40	20'9	21°5	22.2	22.9	23°7	24·5	25·4	26·3	27°3	27.9	28°4	29'0	29.6	30°3	30°9
5.60	20'2	20°8	21.5	22.2	22°9	23·7	24·6	25·5	26°5	27.0	27°6	28'1	28.7	29°4	30°0
5.80	19'6	20°2	20.8	21.5	22°2	23·0	23·8	24·7	25°7	26.2	26°8	27'3	27.9	28°5	29°2
6.00	19°0	19°5	20°2	20.8	21°5	22°3	23°1	24.0	24.9	25.4	26.0	26.5	27 * 1	27.7	28·3
6.20	18°4	19°0	19°6	20.2	20°9	21°6	22°4	23.3	24.2	24.7	25.2	25.8	26 * 4	26.9	27·6
6.40	17°9	18°4	19°0	19.6	20°3	21°0	21°8	22.6	23.6	24.0	24.6	25.1	25*6	26.2	26·8
6.60	17°4	17°9	18°5	19.1	19°7	20°4	21°2	22.0	22.9	23.4	23.9	24.4	25*0	25.5	26·1
6.80	16°9	17°4	17°9	18.5	19°2	19°9	20°6	21.4	22.3	22.8	23.3	23.8	24*3	24.9	25·4
7.00	16.4	16·9	17.5	18.0	18.7	19'4	20°1	20'9	21.7	22'2	22.7	23 ^{.2}	23.7	24°2	24 ^{.8}
7.20	16.0	16·5	17.0	17.6	18.2	18'9	19°6	20'3	21.2	21'6	22.1	22 ^{.6}	23.1	23°6	24 ^{.2}
7.40	15.6	16·1	16.6	17.1	17.7	18'4	19°1	19'8	20.7	21'1	21.6	22 ^{.0}	22.5	23°1	23 ^{.6}
7.60	15.2	15·7	16.2	16.7	17.3	17'9	18°6	19'4	20.2	20'6	21.0	21 ^{.5}	22.0	22°5	23 ^{.1}
7.80	14.8	15·3	15.8	16.3	16.9	17'5	18°2	18'9	19.7	20'1	20.5	21 ^{.0}	21.5	22°0	22 ^{.5}
8.00	14.5	14.9	15.4	15'9	16°5	17.1	17.7	18.5	19 ·2	19.6	20°1	20°5	21°0	21.5	22°0
8.20	14.1	14.6	15.0	15'5	16°1	16.7	17.3	18.0	18·8	19.2	19°6	20°1	20°5	21.0	21°5
8.40	13.8	14.2	14.7	15'2	15°7	16.3	16.9	17.6	18·4	18.8	19°2	19°6	20°1	20.6	21°1
8.60	13.5	13.9	14.4	14'9	15°4	16.0	16.6	17.2	18·0	18.4	18°8	19°2	19°7	20.1	20°6
8.80	13.2	13.6	14.1	14'5	15°1	15.6	16.2	16.9	17·6	18.0	18°4	18°8	19°2	19.7	20°2
9.00	12.9	13'3	13.8	14.2	14.7	15°3	15.9	16.5	17°2	17.6	18.0	18.4	18·8	19·3	19.8
9.20	12.6	13'0	13.5	13.9	14.4	15°0	15.5	16.2	16°9	17.2	17.6	18.0	18·5	18·9	19.4
9.40	12.4	12'8	13.2	13.6	14.1	14°7	15.2	15.9	16°5	16.9	17.3	17.7	18·1	18·5	19.0
9.60	12.1	12'5	12.9	13.4	13.8	14°4	14.9	15.5	16°2	16.6	16.9	17.3	17·7	18·2	18.6
9.80	11.9	12'3	12.7	13.1	13.6	14°1	14.6	15.2	15°9	16.2	16.6	17.0	17·4	17·8	18.3
10'0	11.7	12.0	12.4	12.9	13.3	13.8	14'4	14.9	15°6	15.9	16.3	16.7	17°1	17°5	17°9
11'0	10.6	11.0	11.3	11.7	12.1	12.6	13'1	13.6	14°2	14.6	14.9	15.2	15°6	16°0	16°4
12'0	9.8	10.1	10.4	10.8	11.2	11.6	12'0	12.5	13°1	13.4	13.7	14.0	14°4	14°7	15°1
13'0	9.0	9.3	9.6	10.0	10.3	10.7	11'1	11.6	12°1	12.4	12.7	13.0	13°3	13°6	14°0
14'0	8.4	8.7	8.9	9.3	9.6	10.0	10'4	10.8	11°3	11.5	11.8	12.1	12°4	12°7	13°0
16.0 18.0 20.0 22.0 24.0	7'3 6'5 5'9 5'4 4'9	7.6 6.7 5.5 5.1	7.8 7.0 6.3 5.7 5.2	8·1 7·2 6·5 5·9 5·4	8·4 7·5 6·7 6·1 5·6	8·7 7·8 7·0 6·4 5·8	9·1 8·1 7·3 6·6 6·1	9.5 8.4 7.6 6.9 6.3	9.9 8.8 7.9 7.2 6.6	10'1 9'0 8'1 7'4 6'7	10.4 9.2 8.3 7.6 6.9	10.6 9.4 8.5 7.8 7.1	10.9 9.7 8.7 7.9 7.3	11°1 9°9 9°0 8°2 7°5	11.4 10.2 9.2 8.4 7.7
26.0	4°5	4.7	4.8	5.0	5.2	5°4	5.6	5.9	6·1	6•3	6·4	6.6	6.7	0°9	7·1
28.0	4°2	4.4	4.5	4.7	4.8	5°0	5.2	5.4	5·7	5•8	6·0	6.1	6.3	6°4	6·6
30.0	3°9	4.1	4.2	4.3	4.5	4°7	4.9	5.1	5·3	5•4	5·6	5.7	5.8	6°0	6·2
40.0	3°0	3.0	3.2	3.3	3.4	3°5	3.7	3.8	4·0	4•1	4·2	4.3	4.4	4°5	4·6
50.0	2°4	2.4	2.5	2.6	2.7	2°8	2.9	3.1	3·2	3•3	3·3	3.4	3.5	3°6	3·7
70°0 100°0 200°0 400°0 800°0	1.7 1.2 0.6 0.3 0.1	1.7 1.2 0.6 0.3 0.2	1.8 1.3 0.6 0.3 0.2	1.3 0.7 0.3 0.2	1.3 1.4 0.2 0.3 0.3	2.0 1.4 0.7 0.4 0.2	2·1 1·5 0·7 0·4 0·2	2.2 1.5 0.8 0.4 0.2	2·3 1·6 0·8 0·4 0·2	2°3 1°6 0°8 0°4 0°2	2'4 1'7 0'8 0'4 0'2	2.5 1.7 0.9 0.4 0.2	2°5 1°8 0°9 0°4 0°2	2.0 1.8 0.9 0.2	1.9 0.9 0.5 0.2

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

ĺ	A and B							LAI	TITUD	ES.						
	Cor- rection.	73°	7 4 °	75°	76°	77 °	78°	79 °	80 °	81°	82 °	83°	83 ¹ / ₂ °	84°	84 ¹ / ₂ °	85°
				<u></u>				AZIMO	THS.							
l	'	0	•	٥	•	٥	°	0	0	0	0	°	0	0	0	0
	.00	90°0 80°7	90.0 80.7	90°0 80°7	90.0 80.7	90.0 80.7	90.0 80.8	90°0 80°8	90.0 80.8	90.0 80.8	90°0	90.0	90°0	90.0	90.0	90.0
ł	·04	89.3	89.4	89.4	89.4	89.5	89.5	89.6	89.6	89.6	89.7	89.7	89.7	89.8	89.8	89.8
1	•06	89.0	89.1	89.1	89.2	89.2	89.3	89.3	89.4	89.5	89.5	89.6	89.6	89.6	89.7	89.7
	.09	00.7	00.7	00.0	00.9	89.0	89°0	09.1	09.2	09.3	89 [.] 4	89°4	89.5	89.2	89.0	89.0
	.10	88.0	88°4 88°1	88.2	88.3	88.2	88.6	88.2	89.0 88.8	88.0	80.0	80.3	89.4	89.4	89.2	89.2
1	.14	87.7	87.8	87.9	88.1	88.2	88.3	88.5	88.6	88.7	88.9	89 .0	89.1	89.2	89.2	89.3
1	.10	87.3	87.5	87.6	87.8	87.9	88.1	88.3	.88.4	88.6	88.7	88.9	89.0	89.0	89.1	89.2
	.19	07.0	07.2	07.3	075	0/1/	079	000	00 2	00.4	00.0	00.7	00.0	00.9	09.0	89.1
ł	·20 ·22	86.3	86.2	86.2	87.0	07°4 87°2	87.4	87.0 87.0	87.8	88.0	88.2	88.2	88.6	88.2	88.8	89.0
Į	·24	86.0	86.2	86.4	86.7	86.9	87.1	87.4	87.6	87.8	88.1	88.3	88.4	88.6	88.7	88.8
1	•26	85.7	85.9	86.2	86.4	86.7	86.9	87.2	87.4	87.7	87.9	88.2	88.3	88.4	88.6	88.7
Į	-20	05.3	050	059 0-16	001	00 4	00 7	009	0.07 2	0/5	070	00.0	00.2	00.3	00.5	00.0
l	· 30	84.7	85.0	85.3	85.0	85.0	86.2	86.2	86.8	87.1	87.4	87.8	87.0	88.1	88.2	88.4
I	.34	84.3	84.6	85.0	85.3	85.6	86.0	86.3	86.6	87.0	87.3	87.6	87.8	88 ·o	88.1	88.3
1	• 36	84.0	84.3	84.7	85.0	85.4	85.7	86.1 82.0	86.4	86.8	87.1	87.5	87.7	87.8	88.0	88.2
	30	037	8.2.2	844	8.05	8.00	85.0	86	8610	86.4	86.8	87.0	8	8011	0/9	00 1
ł	·40 ·42	83.0	83.4	83.8	84.2	84.6	85.0	85.4	85.8	86.2	86.7	87.1	87.3	87.5	87.7	87.9
	.44	82.7	83.1	83.2	83.9	84.3	84.8	85.2	85.6	86.1	86.5	86.9	87.1	87.4	87.6	87.8
	:46	843	82.8	83.2	83.7	84°I 82'8	84.5	85.0	85.4	85.9	86.3	86.8	87.0	87.2	87.5	87.7
1	40	81.0	8010	82.6	8217	82.6	8	8.06	85.0	80.0	86.0	86.5	86.8	87.0	87.2	80.0
1	*52	81.4	81.8	82.3	82.8	83.3	83.8	84.3	84.8	85.3	85.9	86.4	86.6	86.9	87.1	87.4
	•54	81.0	81.2	82.0	82.6	83.1	83.6	84.1	84.6	85.2	85.7	86.2	86.2	86.8	87.0	87.3
	•56 •58	80.4	80.0	81.2	82.3	82.8	83'4 83'T	83.9	84.4	85.0 84.8	85.2	86.0	86.2	86.2	86.8	87°2
	.60	80'T	80.6	81.3	81.7	82.2	82.0	82.5	84.1	84.6	85.2	85.8	86°T	86.4	86.7	87.0
	·62	79.7	80.3	80.0	81.2	83.1	82.7	83.3	83.9	84.5	85.1	85.7	86.0	86.3	86.6	86.9
	•64	79.4	80.0	80.6	81.5	81.8	82.4	83.0	83.7	84.3	84.9	85.5	85.9	86.2	86.5	86.8
I	·66	79°1	79.7	80.3	80.2	81.3	82.0	82.8 82.6	83°5 83°3	83.0	84.9 84.6	85.3	85.6	85.0	86.3	86.6
	.70	78.4	70'T	70.7	80.4	81.1	81.7	82.4	82°T	82.8	84.4	85.1	85.5	85.8	86.2	86.5
	.72	78.1	78.8	79.4	80.1	80.8	81.2	82.2	82.9	83.6	84.3	85.0	85.3	85.7	86.1	86.4
	.74	77.8	78.5	79.2	79.9	80.2	81.3	82.0	82.7	83.4	84.1	84.8	85.2	85.6	85.9	86.3
	·70 ·78	77.5	77.9	78.6	79.0	80.0	80.8	81.2	82.3	83.0	83.8	84.6	85.0	85.3	85.7	86.1
	·80	76.8	77.6	78.3	70.0	79.8	80.6	81.3	82.1	82.9	83.6	84.4	84.8	85.2	85.6	86 ·o
	·82	76.5	77.3	78.0	78.8	79.5	80.3	81.1	81.0	82.7	83.5	84.3	84.7	85.1	85.5	85.9
	·84	76.2	77.0	77.7	78.5	79.3	80.1	80.9	81.2	82.5	83.3	84.0	84.6	85.0	85.4	85.8
	·88	75.6	76.4	77.2	78.0	78.8	79.6	80.2	81.3	82.2	83.0	83.9	84.3	84.7	85.2	85.6
	.90	75'3	76.1	76.9	77.7	78.6	79.4	80.3	81.1	82.0	82.9	83.7	84.2	84.6	85.1	85.5
	.92	74.9	75.8	76.6	77.5	78.3	79.2	80.0	80.0	81.8	82.7	83.6	84.1	84.5	85.0	85.4
	·94 ·06	74.0	75'5	70.3	77.2	78.1	78.9	79.8	80.2	81.2	82.4	03.2	83.8	84.3	84.7	°5 3 85°2
	.98	74.0	74.9	75.8	76.7	77.6	78.5	79.4	80.3	81.3	82.2	83.2	83.7	84.2	84.6	85.1
	1.00	73.7	74.6	75.5	76.4	77.3	78.3	79.2	80.1	81.1	82.1	83.1	83.5	84.0	84.5	85.0
	1.05	73.4	74'3	75.2	76.1	77'1	78.0	79.0	80.0	80.9	81.0	82.9	83.4	83.9	84.4	84.9
	1.04	73.1	74.0	74.9	75.9	76.6	77.6	78.6	79.6	80.0	81.0	82.6	83.2	83.7	84.2	84.7
	1.08	72.5	73.4	74.4	75.4	76.3	77.3	78.4	79.4	80.4	81.2	82.2	83.0	83.6	84.1	84.6
1			1		1			1	1	1	1		1	1		

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

Azimuth is named N or S according to the name of the A and B correction.

A and B							LAT	ITUD	ES.						
Cor- rection.	73°	74°	75°	76°	770	78°	79°	80 °	81°	820	83°	83 ¹ 2°	84 °	84 <u>1</u> °	85°
		0	0 1	0	0	0 1	Azimu	THS.	0	0.1		0	0	0	0
1.08	72.5	73.4	74°4	75'4	76·3	77'3	78.4	79 [•] 4	80.4	81.5	82.5	83.0	83.6	84.1	84.6
1.10	72.2	73.1	74°1	75'1	76·1	77'1	78.1	79 [•] 2	80.2	81.3	82.4	82.9	83.4	84.0	84.5
1.20	70.7	71.7	72°7	73'8	74·9	76'0	77.1	78 [•] 2	79.4	80.5	81.7	82.3	82.9	83.4	84.0
1.30	69.2	70.3	71°4	72'5	73·7	74'9	76.1	77 [•] 3	78.5	79.7	81.0	81.6	82.3	82.9	83.5
1.40	67.7	68.9	70°1	71'3	72·5	73'8	75.0	76 [•] 3	77.6	79.0	80.3	81.0	81.7	82.4	83.0
1.20	66·3	67·5	68·8	70'1	71.4	72 ^{.7}	74'0	75°4	76·8	78·2	79 [.] 6	80.4	81.1	81.8	82.6
1.60	64·9	66·2	67·5	68'8	70.2	71 ^{.6}	73'0	74°5	75·9	77·4	79 [.] 0	79.7	80.5	81.3	82.1
1.40	63·6	64·9	66·3	67'6	69.1	70 ^{.5}	72'0	73°6	75·1	76·7	78 [.] 3	79.1	79.9	80.7	81.6
1.80	62·2	63·6	65·0	66'5	68.0	69 ^{.5}	71'0	72°6	74·3	75·9	77 [.] 6	78.5	79.3	80.2	81.1
1.90	60·9	62·4	63·8	65'3	66.9	68 ^{.4}	70'1	71 °7	73·4	75·2	77 [.] 0	77.9	78.8	79.7	80.6
2.00	59 ^{.7}	61·1	62.6	64·2	65·8	67'4	69 [•] 1	70°8	72.6	74°4	76°3	77 ^{•2}	78·2	79'1	80°1
2.10	5 ^{8.5}	59·9	61.5	63·1	64·7	66'4	68 [•] 2	70°0	71.8	73°7	75°6	76•6	77·6	78'6	79°6
2.20	57 .3	58·8	60.3	62·0	63·7	65'4	67 [•] 2	69°1	71.0	73°0	75°0	76•0	77·0	78'1	79°1
2.30	56.1	57·6	59.2	60·9	62·6	64'4	66 [•] 3	68°2	70.2	72°2	74°3	75•4	76·5	7 7'6	78°7
2.40	54.9	56·5	58.2	59·9	61·6	63' 5	65 [•] 4	67°4	69.4	71°5	73°7	74•8	75·9	7 7'0	78°2
2.50	53.8	55'4	57°1	58·8	60.6	62·5	64·5	66·5	68·6	70.8	73 ¹	74 ^{•2}	75 [•] 4	76.5	77 [•] 7
2.60	52.8	54'4	56°1	57·8	59.7	61·6	63·6	65·7	67·9	70.1	72 ⁴	73 ^{•6}	74 [•] 8	76.0	77 [•] 2
2.70	51.7	53'3	55°1	56·8	58.7	60·7	62·7	64·9	67·1	69.4	71 ⁸	73 ^{•0}	74 [•] 2	75.5	76 [•] 8
2.80	50.7	52'3	54°1	55·9	57.8	59·8	61·9	64·1	66·3	68.7	71 ²	7 ² •4	73 [•] 7	75.0	76 [•] 3
2.90	49.7	51'4	53°1	54·9	56.9	58·9	61·0	63·3	65·6	68.0	70 ⁵	7 ^{1•8}	73 [•] 1	74.5	75 [•] 8
3.00	4 ^{8·7}	50°4	52°2	54°0	56.0	58.0	60°2	62·5	64·9	67°3	69·9	71.2	72.6	74'0	75 [.] 3
3.10	47 ^{·8}	49°5	51°3	53°1	55.1	57.2	59°4	61·7	64·1	66°7	69·3	70.7	72.0	73'5	74 [.] 9
3.20	46·9	48°6	50°4	52°3	54.3	56.4	58°6	60·9	63·4	66°0	68·7	70.1	71.5	72'9	74 [.] 4
3.30	46·0	47°7	49°5	51°4	53.4	55.5	57°8	60·2	62·7	65°3	68·1	69.5	71.0	72'4	74 [.] 0
3.40	45 ^{·2}	46°9	48°7	50°6	52.6	54.7	57°0	59·4	62·0	64°7	67·5	68.9	70.4	72'0	73 [.] 5
3.20	44°3	46.0	47 ^{.8}	49 ^{.7}	51.8	54.0	56·3	58.7	61·3	64.0	66·9	68·4	69·9	71.5	73.0
3.60	43°5	45.2	47 ^{.0}	48 ^{.9}	51.0	53.2	55·5	58.0	60·6	63.4	66·3	67·8	69·4	71.0	72.6
3.70	42°8	44.4	46 ^{.2}	48 ^{.2}	50.2	52.4	54·8	57.3	59·9	62.8	65·7	67·3	68·9	70.5	72.1
3.80	42°0	43.7	45 ^{.5}	47 ^{.4}	49.5	51.7	54·1	56.6	59·3	62.1	65·2	66·7	68·3	70.0	71.7
3.90	41°3	42.9	44 ^{.7}	46 ^{.7}	48.7	51.0	53·3	55.9	58·6	61.5	64·6	66·2	67·8	69.5	71.2
4'00	40°5	42°2	44'0	45 ^{.9}	48.0	50'3	52.6	55 ^{.2}	58.0	60·9	64.0	65.6	67·3	69.0	70 ^{.8}
4'10	39°8	41°5	43'3	45 ^{.2}	47.3	49'6	52.0	54 ^{.6}	57.3	60·3	63 .5	65.1	66·8	68.5	70 ^{.3}
4'20	39°2	40°8	42'6	44 ^{.5}	46.6	48'9	51.3	53 ^{.9}	56.7	59·7	62.9	64.6	66·3	68.1	69 ^{.9}
4'30	38°5	40°2	41'9	43 ^{.9}	46.0	48'2	50.6	53 ^{.3}	56.1	59·1	62.3	64.0	65·8	67.6	69 ^{.5}
4'40	37°9	39°5	41'3	43 ^{.2}	45.3	47'5	50.0	52 ^{.6}	55.5	58·5	61.8	63.5	65·3	67.1	69 ^{.0}
4°50	37 ^{•2}	38·9	40.6	42.6	44 ^{.7}	46°9	49'3	52.0	54°9	57 [.] 9	61·3	63.0	64.8	66·7	68.6
4°60	36 ^{•6}	38·3	40.0	41.9	44 ^{.0}	46°3	48'7	51.4	54°3	57 [.] 4	60·7	62.5	64.3	66·2	68.2
4°70	36 ^{•0}	37·7	39.4	41.3	43 ^{.4}	45°7	48'1	50.8	53°7	56 [.] 8	60·2	62.0	63.8	65·7	67.7
4°80	35 ^{•5}	37·1	38.8	40.7	42 ^{.8}	45°1	47'5	50.2	53°1	56 [.] 3	59·7	61.5	63.4	65·3	67.3
4°90	34 ^{•9}	36·5	38.3	40.2	42 ^{.2}	44°5	46'9	49.6	52°5	55 [.] 7	59·2	61.0	62.9	64·8	66.9
5.00	34°4	36.0	37 ^{.7}	39.6	41.6	43 ^{.9}	46·3	49 ^{.0}	52.0	55°2	58.6	60·5	62.4	64°4	66·5
5.20	33°3	34.9	36 ^{.6}	38.5	40.5	42 ^{.8}	45·2	47 ^{.9}	50.9	54°1	57.6	59·5	61.5	63°5	65·6
5.40	32°3	33.9	35 ^{.6}	37.4	39.5	41 ^{.7}	44·1	46 ^{.8}	49.8	53°1	56.7	58·6	60.6	62°6	64·8
5.60	31°4	32.9	34 ^{.6}	36.4	38.4	40 ^{.7}	43·1	45 ^{.8}	48.8	52°1	55.7	57·6	59.7	61°8	64·0
5.80	30°5	32.0	33 ^{.7}	35.5	37.5	39 ^{.7}	42·1	44 ^{.8}	47.8	51°1	54.7	56·7	58.8	60°9	63·2
6.00	29.7	31.2	32.8	34.6	36·5	38.7	41°1	43 ^{.8}	46·8	50'1	53.8	55.8	57 ^{.9}	60°1	62.4
6.20	28.9	30.3	31.9	33.7	35·6	37.8	40°2	42 ^{.9}	45·9	49'2	52.9	54.9	57 ^{.1}	59°3	61.6
6.40	28.1	29.5	31.1	32.9	34·8	36.9	39°3	42 ^{.0}	45·0	48'3	52.0	54.1	56 ^{.2}	58°5	60.8
6.60	27.4	28.8	30.3	32.1	34·0	36.1	38°5	41 ^{.1}	44·1	47'4	51.2	53.2	55 ^{.4}	57°7	60.1
6.80	26.7	28.1	29.6	31.3	33·2	35.3	37°6	40 ^{.3}	43·2	46'6	50.4	52.4	54 ^{.6}	56°9	59.3
7'00	26.0	27'4	28.9	30.6	32'4	34°5	36·8	39 [•] 4	42.4	45.7	49°5	51.6	53.8	56°1	58.6
7'20	25.4	26'7	28.2	29.9	31'7	33°7	36·1	38 [•] 7	41.6	44.9	48°7	50.8	53.0	55°4	57.9
7'40	24.8	26'1	27.6	29.2	31'0	33°0	35·3	37 [•] 9	40.8	44.2	48°0	50.0	52.3	54°7	57.2
7'60	24.2	25'5	26.9	28.5	30'3	32°3	34·6	37 [•] 2	40.1	43.4	47°2	49.3	51.5	53°9	56.5
7'80	23.7	24'9	26.4	27.9	29'7	31°7	33·9	36 [•] 4	39.3	42.7	46°5	48.6	50.8	53°2	55.8

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AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION.

A and B		LATITUDES.													
Cor- rection.	73°	74°	75°	76°	77 °	78°	79°	80°	81°	82°	83°	8 3 ¹⁰ / ₂	84 °	8430	85°
	Azimuths.														
'	°	0	0	0	0	°	0	0	0	0	°	0	0	0	0
8.0	23.1	24.4	25.8	27.3	29.1	31.0	33.2	35.7	38.6	41.0	45.7	47.8	50'1	52.5	55.1
8.4	22.0	23.9	25 2	20.0	20.5	20.8	32.0	35 1	37.9	41.2	45.0	47.1	49'4	51.0	54.4
8.6	21.7	22.9	24.2	25.7	27.3	29.2	31.4	33.8	36.6	39.9	43.7	45.8	48.0	50.2	53'I
8.8	21.5	22.4	23.7	25.2	26.8	28.7	30.8	33.5	36.0	39.2	43.0	45'1	47'4	49.9	52.5
0.0	20.8	22.0	23.2	24.7	26.3	28.1	30.2	32.6	35.4	38.6	42.4	44.5	46.7	49'2	51.0
9.2	20'4	21.2	22.8	24.2	25.8	27.6	29.7	32.0	34.8	38.0	41.7	43.8	46.1	48.6	51.3
9.4	20.0	21.1	22.3	23.7	25.3	27'1	29.1	31.2	34'2	37.4	41'I	43.2	45'5	48.0	50.2
9.6	19.0	20.7	21.0	23.3	24.8	20.0	28.0	31.0	33.7	30.8	40.2	42.0	44'9	47'4	50'1
98	19 2	20 3	21 5	22.9	44 4	201	20 1	50 4	33 +	30 2	59.9	420	44 3	400	49 5
10.0	18.9	19.0	21.1	22.2	24.0	25.7	27.7	29.9	32.0	35.7	39.4	41.2	43'7	40'2	48.9
10.7	18.2	10.5	20.4	21.7	23.1	24.8	26.7	20.0	31.6	34.6	38.3	40 9	43 2	45'1	40 4
10.0	17.9	18.0	20.1	21.3	22.8	24.4	26.3	28.5	31.1	34'I	37.7	39.8	42.1	44.5	47.3
10.8	17.0	18.0	19.7	20.9	22.4	24.0	25.9	28.1	30.6	33.0	37.5	39.3	41.2	44.0	46.2
11.0	17.3	18.3	19.4	20.6	22.0	23.6	25.5	27.6	30.5	33.5	36.7	38.8	41.0	43.5	46.2
11.5	17.0	17.9	10.0	20.3	21.0	23.5	25.1	27.2	29.7	32.7	36.5	38.3	40.2	43.0	45.7
II'4	10.7	17.7	18.7	19.9	21.3	22.9	24.7	20.8	29.3	32.2	35.7	37.8	40'0	42'5	45.2
11.0	10 4	174	18.1	19.0	20.6	22.5	23.0	20.4	28.4	31.3	35 3	36.8	39.5	420	44 7
		76.8	TM-8	100	2012	27.8	-5 5	0.00	28:0	3- 5	54 0	2614	28.6	4- 5	17 -
12.0	15.7	16.6	17.6	190	20.0	21.2	23.2	25.3	27.7	30.2	34 4	35.0	38.1	41 0	43 /
12.4	15.4	16.3	17'3	18.4	19.7	21.2	22.9	24.9	27.3	30.1	33.2	35.5	37.7	40'1	42.8
12.6	15.5	16.1	17.0	18.2	19'4	20.0	22.0	24.6	26.0	29.7	33.1	35.0	37.2	39.6	42'3
12.8	15.0	15.8	16.8	17.9	19.2	20.6	22.3	24.5	26.2	29.3	32'7	34.6	36.8	39.5	41.0
13.0	14.2	15.0	16.6	17.0	18.0	20.3	22.0	23.9	26.2	28.9	32.3	34'2	36.3	38.7	41'4
13.5	14.2	15.4	10.3	17.4	18.0	20'0	21.7	23.0	25.8	28.0	31.0	33.8	35.9	38.3	41.0
134 13.6	14 3 14'T	121	15.0	10.0	10 4 18 1	197	21.4	22.0	25.2	27.8	31.1	33.0	35 5	3/9	400
13.8	13.0	14'7	15.0	16.7	17.9	19.2	20.8	22.7	24.9	27.5	30.2	32.6	34.7	37'1	39'7
14.0	13.2	14.5	15.4	16.2	17.6	10.0	20.5	22.4	24.5	27.2	30.4	32.3	34.3	36.7	39.3
14.2	13.2	14.3	15.5	16.3	17.4	18.7	20.3	22.1	24.2	26.8	30.0	31.0	34.0	36.3	38.9
14.4	13.4	14.1	15.0	10.0	17.2	18.2	20.0	21.8	23.9	26.2	29.7	31.2	33.0	35.6	38.2
14.6	13.5	14.0	14.8	15.8	10.0	18.0	19.7	21.2	23.0	20.2	29.3	31.2	33.2	35.0	38.2
14 0	130	130	14 0	130	10 7	10 0	19.5	213	-34	239	290	30 0	34 9	35 4	3/0
15.0	12.8	13.0	14.4	15'4	10.2	17.8	19.3	21.0	23.1	25.0	28.7	30.2	32.2	34.8	37.4
15.4	12.2	13.3	14 5	15.0	10.3	17.3	18.8	20.5	22.5	25.0	28.0	20.8	31.8	34 J 34'I	36.7
15.6	12.4	13.1	13.9	14.8	15.0	17.1	18.0	20.3	22.3	24.7	27.7	29.5	31.2	33.8	36.3
15.8	12.2	12.0	13.2	14.2	15.2	16.0	18.4	20.0	22.0	24.2	27.4	29.2	31.5	33.4	36.0
16.0	12'1	12.8	13.0	14.2	15.2	16.2	18.1	19.8	21.8	24 ·2	27.2	28.9	30.9	33.1	35.6
16.5	11.0	12.Q	13.4	14.3	15.3	16.2	17.9	19.0	21.2	23.9	26.9	28.6	30.6	32.8	35.3
10'4	11.8	12.2	13.3	14.1	15.5	10.3	17.7	19.3	20.3	23.7	20.0	28.3	30.3	32.2	35.0
16.8	11.2	12.2	13.0	13.8	14.8	10.5	17.3	18.0	20.8	45 4 23'2	26.0	27.7	29.7	31.8	34.3
17:0	11.4	12:0	12.8	12.4	T	15.8	-/ 3	18.0	20.6	22:0	25.8	2715	20.4	27 5	24.0
17.2	11.5	11.0	12.7	+3 / 13'5	14 7	15.0	16.0	18.5	20.4	22.7	25'5	4/ J 27'2	29 4 29 I	31.5	33.7
17.4	11.1	11.8	12.5	13.4	14.3	15.2	16.8	18.3	20.2	22.4	25.2	26.9	28.8	30.0	33.4
17.6	11.0	11.0	12.4	13.3	14.2	15.3	16.6	18.1	20.0	22.2	25 .0	26.7	28.5	30.2	33.1
17.8	10.0	11.2	15.5	13.1	14.0	15.1	10.4	17.9	19.8	22.0	24.7	20.4	28.3	30.4	32.8
18.0	10.8	11.4	12.1	12.0	13.0	15.0	16.5	17.2	19.6	21.8	24'5	26.1	28.Ò	30.1	32.2
18.2	10.0	11.3	12.0	12.8	13.7	14.8	10.1	17.0	19.4	21.2	24'3	25.9	27.7	29.8	32.5
18.6	10.4	11.0	11.2	12.2	13.4	14 0	+3 9 15'7	-1/4 17.2	19.0	21.3	23.8	25.4	27.2	20.3	31.7
18.8	10.3	10.0	11.6	12.4	13.3	14.3	15.6	17.0	18.8	20.9	23.6	25.2	27.0	29.0	31.4
							-	·		-	-				
Table C.

AZIMUTHS CORRESPONDING TO THE A AND B CORRECTION

Azimuth is named N or S according to the name of the A and B correction.

A and B							LA	TITUI	DES.						
Cor- rection.	73°	74°	75°	76°	77 °	78°	79°	80 °	81°	820	830	83 ¹ 2°	84°	8410	85°
							AZIMU	THS.	_	_					
1		1018	0	100	0		0	1.6.0	1 - 9.6	0			0	0	0
19.0	10.7	10.3	11.7	12.1	13.0	14 2	15.4	16.7	18.4	20.7	23.4	24.9	20.7	28.5	30.0
19.4	10.0	10.6	11.3	12.0	12.9	13.0	15.1	16.2	18.2	20.3	22.9	24.5	26.2	28.3	30.6
19.6	9.9	10.2	11.5	11.0	12.8	13.8	15.0	16.4	18.1	20 ° I	22.7	24.3	26.0	28.0	30.3
19.9	9.9	10.4	11.0	11.9	12.7	13.7	14.9	10.5	17.9	19.9	22.2	24.0	25.8	27.8	30.1
20.0	9.7	10.3	10.0	11.2	12.2	13.2	14.7	16.1	17.7	19.8	22.3	23.8	25.6	27.5	29.8
22'0	8.8	9.0 9.4	10.4	10.6	120	12.3	14.0	15'3	16.2	18.1	20.5	22.0	23.5	25.4	20.7
23.0	8.5	9.0	9.2	10.5	10.0	11.8	12.8	14.1	15.2	17.3	19.6	21.0	22.6	24.4	26.5
24.0	8.1	8.6	0. 1	9.8	10.2	11.3	12.3	13.2	14.9	16.2	18.0	20.3	21.2	23.2	25.6
25.0	7.8	8.3	8.8	9°4	10.1	10.0	11.8	13.0	14.3	16.0	18.3	19.2	20.9	22.6	24.7
20.0	7.5	7.9	8.2	9°0	9.7	10.2	11.4	12.2	13.8	15'4	17.5	18.8	20.2	21.0	23.8
28.0	7.0	7.4	7.9	8.4	0.0	9.7	10.0	11.6	12.0	14.4	16.3	17.5	18.0	20.4	22.3
29.0	6.2	7°1	7.6	8·1	8.7	9.4	10.5	11.5	12.4	13.0	15.8	16.0	18.3	19.8	21.6
30.0	6.2	6.9	7'3	7.8	8.4	9.1	9.9	10.0	12.0	13.2	15.3	16.4	17.7	19.5	20.9
31.0	6.3	6.7	7°1	7.6	8.2	8.8	9.6	10.2	11.2	13.0	14.8	15.9	17.2	18.6	20.3
32.0	5.0	6.3	6.2	7.4	7.9	8.3	9.3	0.0	11.3	12.7	14.4	15.4	10.0	17.5	19.7
34.0	5.7	6.1	6.2	6.9	7.4	8.1	8.8	9.6	10.0	11.0	13.0	14.6	15.7	17.1	18.6
35.0	5.6	5.9	6.3	6.7	7.2	7.8	8.5	9.3	10.4	11.6	13.5	14'2	15.3	16.6	18.2
36.0	5.4	5.8	6.1	6.6	7.0	7 •6	8.3	9.1	10.1	11.3	12.8	13.8	14.9	16.3	17.7
37.0	5.3	5.6	6.0	6'4	6.0 6.0	7.4	8.1	8.8	9.8	11.0	12.2	13.4	14.2	15.7	17.2
40.0	7.0	5.2	5.5	5.0	6.3	6.0	79	8.2	0'I	10'2	11.6	12.2	13.2	14.6	16.0
42.0	4.7	4.0	5'3	5.6	6.0	6.2	7.1	7.8	8.7	0.2	11.1	11.0	12.8	14.0	15'3
44'0	4.4	4.7	5.0	5'4	5.8	6.2	6.8	7.5	8.3	9.3	10.0	11.4	12.3	13.3	14.6
46.0	4'3	4.5	4.8	5°1	5.2	6.0	6.2	7'1	7.9	8.9	10.1	10.0	11.2	12.8	14.0
48.0	4'I	4'3	4.0	4.9	5.3	5.7	6.0	6°0	7.0	8.2	9'7 0'3	10.4	10.8	12.3	13'4 12'0
52.0	2.8	4.0	4.2	4.5	4.0	5.2	E•8	6.2	7.0	7'0	0.0	0.0	10.4	11.3	12.4
54.0	3.6	3.8	4.1	4'4	49	5°I	5.2	6.1	6.8	7.6	8.6	9.3	10.0	10.0	12.0
56.0	35	3.7	3.9	4'2	4.5	4'9	5.3	5'9	6.2	7'3	8.3	9.0	9 °7	10.0	11.0
58.0	3.4	3.6	3.8	4°I	4'4	4.7	5.2	5.7	6°3	7°1	8.1 2.8	8.7	9'4 0'1	10.5	11.5
000	33	33	37	39	4 4	40	50	55	01	6.6	,	0 4 0	0.0	99	100
64.0	3.5	3.3	3.0	3.0	4'1	4'4	4.0	5'3	5.9	6°4	7.3	7.0	8.5	0.3	10.2
6 6•0	3.0	3.1	3.4	3.6	3.9	4'2	4.5	5.0	5.5	6.5	7.1	7.6	8.2	9.0	9.9
68 ·o	2.0	3.1	3.3	3.2	3.2	4.0	4'4	4*8	5°4	6.0	6.9	7.4	8.0	8.7	9.6
70.0	2.8	3.0	3.5	3.4	3.0	3'9	4'3	4'7	5.5	5.9	0.7	12	10	0.2	9.3
80.0	2.4	2.6	2.8	3.0	3.2	3.4	3.7	4'I	4.6	5'1	5°9	0°3	0'ð 6'1	7'4 6.6	0'2 7'2
100.0	2.0	2.1	2.2	2.4	2.5	2.8	30	3.3	3.7	4°I	3 ≁ 4°7	5.0	5.5	6.0	6.2
120.0	1.6	1.7	1.8	2.0	2.1	2.3	2.5	2.7	3.0	3'4	3.9	4'2	4.6	5.0	5.2
140.0	1.4	1.2	1.0	1.2	1.8	2.0	2.1	2.4	2.6	2.9	3'4	3.0	3.9	4'3	4.7
160.0	1.5	1.3	1.4	1.2	1.0	1.2	1.0	2.1	2.3	2.6	2.9	3.2	3.4	3.7	4.1
180.0	1.1	1.5	1.5	1.3	I'4	1.2	1.2	1.9	2.0	2.3	2.0	2.0	3.0	3.0	3.3
300.0	0.2	0.2	0.2	0.8	0.8	0.0	1.0	1.1	1.5	I'4	1.6	1.2	1.8	2.0	2.2
400'0	0.2	o•5	0.6	0.6	6•0	0.2	o•8	o •8	0.0	1.0	I.3	1.3	1°4	1.2	1.6
500.0	0.4	0.4	0.4	0.2	0.2	0.6	0.6	0.2	0.2	8•0	0.0	1.0	1.1	1.5	1.3
600.0	0.3	0.3	0.4	0.4	0.4	0.2	0.2	0.2	0.0	0.2	0.8	0.9	0.0	1.0	0.0
700°0 800°0	0.3	0.3	0.3	0.3	0.4	0.4	0'4	0.4	0'5	0.2	0.6	0.6	0.2	0.2	0.8
1000.0	0.2	0.5	0.5	0.5	0.3	0.3	0.3	0.3	0.4	0.4	0.2	0.2	0.2	0.6	0.2
1			1						1	1					

SHOWING DIFFERENCE OF LONGITUDE AND CORRESPONDING DEPARTURE.

.at.					DI	FFER	ENC	E O	F LC)NGI7	ΓUDE					
	•10	•11	•12	•13	•14	•15	·16	•17	•18	·19	·20	•21	•22	•23	•24	•25
° 2 4 6 8 10	•100 •100 •099 •099 •098	·110 ·110 ·109 ·108	·120 ·120 ·119 ·119 ·118	·130 ·130 ·129 ·129 ·128	·140 ·140 ·139 ·139 ·138	·150 ·150 ·149 ·148 ·148	·160 ·160 ·159 ·158 ·158	·170 ·170 ·169 ·168 ·167	·180 ·180 ·179 ·178 ·177	·190 ·190 ·189 ·188 ·187	·200 ·200 ·199 ·198 ·197	·210 ·209 ·209 ·208 ·207	·220 ·219 ·219 ·218 ·217	·230 ·229 ·229 ·228 ·227	·240 ·239 ·239 ·238 ·238 ·236	·250 ·249 ·249 ·248 ·248 ·246
11 12 13 14 15	•098 •098 •097 •097 •097	·108 ·108 ·107 ·107 ·107	•118 •117 •117 •116 •116	·128 ·127 ·127 ·126 ·126	·137 ·137 ·136 ·136 ·135	•147 •147 •146 •146 •145	·157 ·157 ·156 ·155 ·155	•167 •166 •166 •165 •164	•177 •176 •175 •175 •175 •174	·187 ·186 ·185 ·184 ·184	•196 •196 •195 •194 •193	·206 ·205 ·205 ·204 ·203	·216 ·215 ·214 ·213 ·213	•226 •225 •224 •223 •222	·236 ·235 ·234 ·233 ·232	·245 ·245 ·244 ·243 ·241
16	·096	·106	·115	·125	·135	·144	·154	•163	·173	·183	•192	·202	•211	•221	·231	·240
17	·096	·105	·115	·124	·134	·143	·153	•163	·172	·182	•191	·201	•210	•220	·230	·239
18	·095	·105	·114	·124	·133	·143	·152	•162	·171	·181	•190	·200	•209	•219	·228	·238
19	·095	·104	·113	·123	·132	·142	·151	•161	·170	·180	•189	·199	•208	•217	·227	·236
20	·094	·103	·113	·122	·132	·141	·150	•160	·169	·179	•188	·197	•207	•216	·226	·235
21	·093	·103	·112	•121	·131	•140	·149	·159	·168	·177	·187	·190	·205	·215	·224	·233
22	·093	·102	·111	•121	·130	•139	·148	·158	·167	·176	·185	·195	·204	·213	·223	·232
23	·092	·101	·110	•120	·129	•138	·147	·156	·166	·175	·184	·193	·203	·212	·221	·230
24	·091	·100	·110	•119	·128	•137	·146	·155	·164	·174	·183	·192	·201	·210	·219	·228
25	·091	·100	·109	•118	·127	•136	·145	·154	·163	·172	·181	·190	·199	·208	·218	·227
20	·090	·099	·108	·117	•120	•135	·144	·153	·162	·171	•180	·189	·198	·207	·210	·225
27	·089	·098	·107	·116	•125	•134	·143	·151	·160	•169	•178	·187	·196	·205	·214	·223
28	·088	·097	·106	·115	•124	•132	·141	·150	·159	•168	•177	·185	·194	·203	·212	·221
29	·087	·096	·105	·114	•122	•131	·140	·149	·157	•166	•175	·184	·192	·201	·210	·219
30	·087	·095	·104	·113	•121	•130	·139	·147	·156	•165	•173	·182	·191	·199	·208	·217
31 32 33 34 35	·080 ·085 ·084 ·083 ·082	·094 ·093 ·092 ·091 ·090	·103 ·102 ·101 ·099 ·098	·111 ·110 ·109 ·108 ·106	•120 •119 •117 •116 •115	·129 ·127 ·126 ·124 ·123	•137 •136 •134 •133 •131	·140 ·144 ·143 ·141 ·139	·154 ·153 ·151 ·149 ·147	·163 ·161 ·159 ·158 ·156	•171 •170 •168 •166 •164	•180 •178 •176 •176 •174 •172	·189 ·187 ·185 ·182 ·180	·197 ·195 ·193 ·191 ·188	·200 ·204 ·201 ·199 ·197	·214 ·212 ·210 ·207 ·205
36	·081	·089	·097	·105	·113	·121	·129	·138	·146	·154	•162	·170	·178	•186	·194	·202
37	·080	·088	·096	·104	·112	·120	·128	·136	·144	·152	•160	·168	·176	•184	·192	·200
38	·079	·087	·095	·102	·110	·118	·126	·134	·142	·150	•158	·165	·173	•181	·189	·197
39	·078	·085	·093	·101	·109	·117	·124	·132	·140	·148	•155	·163	·171	•179	·187	·194
40	·077	·084	·092	·100	·107	·115	·123	·130	·138	·146	•153	·161	·169	•176	·184	·192
41	·075	·083	·091	·098	·106	•113	·121	·128	·136	·143	•151	·158	•166	·174	·181	•189
42	·074	·082	·089	·097	·104	•111	·119	·126	·134	·141	•149	·156	•163	·171	·178	•186
43	·073	·080	·088	·095	·102	•110	·117	·124	·132	·139	•146	·154	•161	·168	·176	•183
44	·072	·079	·086	·094	·101	•108	·115	·122	·129	·137	•144	·151	•158	·165	·173	•180
45	·071	·078	·085	·092	·099	•106	·113	·120	·127	·134	•141	·148	•156	·163	·170	•177
40	•069	·076	·083	·090	·097	·104	·111	·118	·125	·132	•139	·140	·153	·160	·167	·174
47	•068	·075	·082	·089	·095	·102	·109	·116	·123	·130	•136	·143	·150	·157	·164	·170
48	•067	·074	·080	·087	·094	·100	·107	·114	·120	·127	•134	·141	·147	·154	·161	·167
49	•066	·072	·079	·085	·092	·098	·105	·112	·118	·125	•131	·138	·144	·151	·157	·164
50	•064	·071	·077	·084	·090	·096	·103	·109	·116	·122	•129	·135	·141	·148	·154	·161
51	•063	•069	·076	·082	·088	•094	·101	·107	•113	·120	•120	·132	·138	·145	·151	·157
52	•062	•068	·074	·080	·086	•092	·099	·105	•111	·117	•123	·129	·135	·142	·148	·154
53	•060	•066	·072	·078	·084	•090	·096	·102	•108	·114	•120	·126	·132	·138	·144	·150
54	•059	•065	·071	·076	·082	•088	·094	·100	•106	·112	•118	·123	·129	·135	·141	·147
55	•057	•063	·069	·075	·080	•086	·092	·098	•103	·109	•115	·120	·126	·132	·138	·143
56	·056	·062	·067	·073	·078	·084	·089	·095	·101	•106	·112	·117	·123	·129	·134	·140
57	·054	·060	·065	·071	·076	·082	·087	·093	·098	•103	·109	·114	·120	·125	·130	·136
58	·053	·058	·064	·069	·074	·079	·085	·090	·095	•101	·106	·111	·117	·122	·127	·132
59	·052	·057	·062	·067	·072	·077	·082	·088	·093	•098	·103	·108	·113	·118	·124	·129
60	·050	·055	·060	·065	·070	·075	·080	·085	·090	•095	·100	·105	·110	·115	·120	·125
61	·048	·053	058	·063	·068	·073	•078	·082	·087	*092	·097	·102	•107	·112	·116	·121
62	·047	·052	•056	·061	·066	·07c	•075	·080	·085	*089	·094	·099	•103	·108	·113	·117
63	·045	·050	•054	·059	·064	·068	•073	·077	·082	*086	·091	·095	•100	·104	·109	·113
64	·044	·048	•053	·057	·061	·066	•070	·075	·079	*083	·088	·092	•096	·101	·105	·110
65	·042	·046	•051	·055	·059	·063	• 0 58	·072	·076	*080	·085	·089	•093	·097	·101	·106

SHOWING DIFFERENCE OF LONGITUDE AND CORRESPONDING DEPARTURE.

at.					DIFF	ERENC	E O	F LC	ONGI	TUDE					
н 	•26	•27	·28	•29	•30	•31	•32	•33	•34	•35	•36	•37	•38	•39	•40
°2 4 6 8 10	·260 ·259 ·259 ·257 ·257 ·256	·270 ·269 ·269 ·267 ·266	·280 ·279 ·278 ·277 ·276	·290 ·289 ·288 ·287 ·286	·300 ·299 ·298 ·297 ·295	·310 ·309 ·308 ·307 ·305	·320 ·319 ·318 ·317 ·315	·330 ·329 ·328 ·327 ·325	·340 ·339 ·338 ·337 ·335	·350 ·349 ·348 ·347 ·345	·360 ·359 ·358 ·356 ·355	·370 ·369 ·368 ·366 ·364	·380 ·379 ·378 ·376 ·374	·390 ·389 ·388 ·386 ·386 ·384	·400 ·399 ·398 ·396 ·394
11	·255	·265	·275	·285	·294	·304	·314	·324	·334	·344	·353	•363	·373	·383	·393
12	·254	·264	·274	·284	·293	·303	·313	·323	·333	·342	·352	•362	·372	·381	·391
13	·253	·263	·273	·283	·292	·302	·312	·322	·331	·341	·351	•361	·370	·380	·390
14	·252	·262	·272	·281	·291	·301	·310	·320	·330	·340	·349	•359	·369	·378	·388
15	·251	·261	·270	·280	·290	·299	·309	·319	·328	·338	·348	•357	·367	·377	·386
16	·250	·260	·269	·279	·288	·298	·308	·317	·327	·336	·346	·356	·365	·375	·385
17	·249	·258	·268	·277	·287	·296	·306	·316	·325	·335	·344	·354	·363	·373	·383
18	·247	·257	·266	·276	·285	·295	·304	·314	·323	·333	·342	·352	·361	·371	·380
19	·246	·255	·265	·274	·284	·293	·303	·312	·321	·331	·340	·350	·359	·369	·378
20	·244	·254	·263	·273	·282	·291	·301	·310	·319	·329	·338	·348	·357	·366	·376
21 22 23 24 25	·243 ·241 ·239 ·238 ·236	·252 ·250 ·249 ·247 ·245	·261 ·260 ·258 ·256 ·256 ·254	·271 ·269 ·267 ·265 ·263	·280 ·278 ·276 ·274 ·272	·289 ·287 ·285 ·283 ·283	·299 ·297 ·295 ·292 ·290	·308 ·306 ·304 ·301 ·299	·317 ·315 ·313 ·311 ·308	·327 ·325 ·322 ·320 ·317	·336 ·334 ·331 ·329 ·326	·345 ·343 ·341 ·338 ·335	·355 ·352 ·350 ·347 ·344	·364 ·362 ·359 ·356 ·353	·373 ·371 ·368 ·365 ·363
26	·234	·243	·252	·261	·270	·279	·288	·297	·306	·315	·324	·333	342	•351	·360
27	·232	·241	·249	·258	·267	·276	·285	·294	·303	·312	·321	·330	·339	•347	·356
28	·230	·238	·247	·256	·265	·274	·283	·291	·300	·309	·318	·327	·336	•344	·353
29	·227	·236	·245	·254	·262	·271	·280	·289	·297	·306	·315	·324	·332	•341	·350
30	·225	·234	·242	·251	·260	·268	·277	·286	·294	·303	·312	·320	·329	•338	·346
31 32 33 34 35	·223 ·220 ·218 ·216 ·213	·231 ·229 ·226 ·224 ·221	·240 ·237 ·235 ·232 ·232 ·229	·249 ·246 ·243 ·240 ·238	·257 ·254 ·252 ·249 ·246	·266 ·263 ·260 ·257 ·254	·274 ·271 ·268 ·265 ·262	·283 ·280 ·277 ·274 ·270	·291 ·288 ·285 ·282 ·282	·300 ·297 ·294 ·290 ·287	·309 ·305 ·302 ·298 ·295	·317 ·314 ·310 ·307 ·303	·326 ·322 ·319 ·315 ·311	·334 ·331 ·327 ·323 ·319	·343 ·339 ·335 ·332 ·328
36	·210	·218	·227	·235	·243	·251	·259	·267	·275	·283	·291	•299	·307	·316	·324
37	·208	·216	·224	·232	·240	·248	·256	·264	·272	·280	·288	•295	·303	·311	·319
38	·205	·213	·221	·229	·236	·244	·252	·260	·268	·276	·284	•292	·299	·307	·315
39	·202	·210	·218	·225	·233	·241	·249	·256	·264	·272	·280	•288	·295	·303	·311
40	·199	·207	·214	·222	·230	·237	·245	·253	·260	·268	·276	•283	·291	·299	·306
41	·196	·204	·211	·219	·226	·234	·242	·249	·257	·264	·272	·279	·287	·294	·302
42	·193	·201	·208	·216	·223	·230	·238	·245	·253	·260	·268	·275	·282	·290	·297
43	·190	·197	·205	·212	·219	·227	·234	·241	·249	·256	·263	·271	·278	·285	·293
44	·187	·194	·201	·209	·216	·223	·230	·237	·245	·252	·259	·266	·273	·281	·288
45	·184	·191	·198	·205	·212	·219	·226	·233	·240	·247	·255	·262	·269	·276	·283
46	·181	·188	·195	·201	·208	·215	·222	·229	·236	·243	·250	·257	·264	·271	·278
47	·177	·184	·191	·198	·205	·211	·218	·225	·232	·239	·246	·252	·259	·266	·273
48	·174	·181	·187	·194	·201	·207	·214	·221	·228	·234	·241	·248	·254	·261	·268
49	·171	·177	·184	·190	·197	·203	·210	·216	·223	·230	·236	·243	·249	·256	·262
50	·167	·174	·180	·186	·193	·199	·206	·212	·219	·225	·231	·238	·244	·251	·257
51	•164	·170	·176	·183	·189	·195	·201	·208	·214	·220	·227	·233	·239	·245	·252
52	•160	·166	·172	·179	·185	·191	·197	·203	·209	·215	·222	·228	·234	·240	·246
53	•156	·162	·169	·175	·181	·187	·193	·199	·205	·211	·217	·223	·229	·235	·241
54	•153	·159	·165	·170	·176	·182	·188	·194	·200	·206	·212	·217	·223	·229	·235
55	•149	·155	·161	·166	·172	·178	·184	·189	·195	·201	·206	·212	·218	·224	·229
56	·145	·151	·157	·162	·168	·173	·179	·185	·190	·196	·201	·207	·212	·218	·224
57	·142	·147	·152	·158	·163	·169	·174	·180	·185	·191	·196	·202	·207	·212	·218
58	·138	·143	·148	·154	·159	·164	·170	·175	·180	·185	·191	·196	·201	·207	·212
59	·134	·139	·144	·149	·155	·160	·165	·170	·175	·180	·185	·191	·196	·201	·206
60	·130	·135	·140	·145	·150	·155	·160	·165	·170	·175	·180	·185	·190	·195	·200
61	·126	·131	·136	·141	·145	·150	·155	·160	·165	·170	·175	·179	•184	·189	·194
62	·122	·127	·131	·136	·141	·146	·150	·155	·160	·164	·169	·174	•178	·183	·188
63	·118	·123	·127	·132	·136	·141	·145	·150	·154	·159	·163	·168	•173	·177	·182
64	·114	·118	·123	·127	·132	·136	·140	·145	·149	·153	·158	·162	•167	·171	·751
65	·110	·114	·118	·123	·127	·131	·135	·139	·144	·148	·152	·156	•161	·165	·169

Showing Difference of Longitude and Corresponding Departure.

at.				DI	FFERI	ENCE	OF	LON	GITU	JDE.					
	•41	•42	•43	• 44]	·45	•46	•47	•48	•49	•50	•51	•52	•53	•54	•55
° 2 4 6 8 10	·410 ·409 ·408 ·406 ·404	·420 ·419 ·418 ·416 ·414	·430 ·429 ·428 ·426 ·423	•440 •439 •438 •436 •433	·450 ·449 ·448 ·446 ·446	•460 •459 •457 •456 •453	·470 ·469 ·467 ·465 ·463	·480 ·479 ·477 ·475 ·473	·490 ·489 ·487 ·485 ·485 ·483	·500 ·499 ·497 ·495 ·492	·510 ·509 ·507 ·505 ·502	·520 ·519 ·517 ·515 ·512	·530 ·529 ·527 ·525 ·522	·540 ·539 ·537 ·535 ·532	·550 ·549 ·547 ·545 ·542
11 12 13 14 15	·402 ·401 ·399 ·398 ·396	·412 ·411 ·409 ·408 ·406	·422 ·421 ·419 ·417 ·415	·432 ·430 ·429 ·427 ·425	·442 ·440 ·438 ·437 ·437	·452 ·450 ·448 ·446 ·444	·461 ·460 ·458 ·456 ·454	·471 ·470 ·468 ·466 ·464	·481 ·479 ·477 ·475 ·473	·491 ·489 ·487 ·485 ·483	·501 ·499 ·497 ·495 ·493	·510 ·509 ·507 ·505 ·502	·520 ·518 ·516 ·514 ·512	·530 ·528 ·526 ·524 ·522	·540 ·538 ·536 ·534 ·531
16 17 18 19 20	·394 ·392 ·390 ·388 ·385	·404 ·402 ·399 ·397 ·395	·413 ·411 ·409 ·407 ·407	·423 ·421 ·418 ·416 ·413	·433 ·430 ·428 ·425 ·423	·442 ·440 ·437 ·435 ·432	·452 ·449 ·447 ·444 ·444 ·442	·461 ·459 ·457 ·454 ·451	·471 ·469 ·466 ·463 ·460	·481 ·478 ·476 ·473 ·470	·490 ·488 ·485 ·482 ·479	·500 ·497 ·495 ·492 ·489	·509 ·507 ·504 ·501 ·498	·519 ·516 ·514 ·511 ·507	·529 ·526 ·523 ·520 ·517
21 22 23 24 25	·383 ·380 ·377 ·375 ·372	·392 ·389 ·387 ·387 ·384 ·384	·401 ·399 ·396 ·393 ·390	·411 ·408 ·405 ·402 ·399	·420 ·417 ·414 ·411 ·408	·429 ·427 ·423 ·420 ·417	·439 ·436 ·433 ·429 ·426	·448 ·445 ·442 ·439 ·435	·457 ·454 ·451 ·448 ·444	·467 ·464 ·460 ·457 ·453	·476 ·473 ·469 ·466 ·462	·485 ·482 ·479 ·479 ·475 ·471	·495 ·491 ·488 ·484 ·484	·504 ·501 ·497 ·493 ·489	·513 ·510 ·506 ·502 ·498
26 27 28 29 30	·369 ·365 ·362 ·359 ·355	·377 ·374 ·371 ·367 ·367 ·364	· 386 · 383 · 380 · 376 · 376 · 372	•395 •392 •388 •385 •381	·404 ·401 ·397 ·394 ·390	·413 ·410 ·406 ·402 ·398	•422 •419 •415 •415 •411	·431 ·428 ·424 ·420 ·416	·440 ·437 ·433 ·429 ·424	•449 •446 •441 •437 •433	·458 ·454 ·450 ·446 ·442	·467 ·463 ·459 ·455 ·455 ·450	·476 ·472 ·468 ·464 ·459	·485 ·481 ·477 ·472 ·468	·494 ·490 ·486 ·481 ·476
31 32 33 34 35	·351 ·348 ·344 ·340 ·336	: ·360 3 ·356 • ·352 • ·348 • ·344	0 ·369 5 ·365 2 ·361 3 ·356 4 ·352	•377 •373 •369 •365 •360	·386 ·382 ·377 ·373 ·369	·394 ·390 ·386 ·381 ·377	·403 ·399 ·394 ·394 ·390 ·385	·411 ·407 ·403 ·398 ·393	·420 ·416 ·411 ·406 ·401	·429 ·424 ·419 ·415 ·410	·437 ·433 ·428 ·423 ·418	9 •446 •441 •436 •436 •431 •426	·454 ·449 ·444 ·439 ·434	·463 ·458 ·453 ·453 ·448 ·442	·471 ·466 ·461 ·456 ·451
36 37 38 39 40	·332 ·327 ·323 ·319 ·314	2 ·340 7 ·335 3 ·331 9 ·326 4 ·322	0 ·348 5 ·343 5 ·339 5 ·334 2 ·329	3 ·356 3 ·351 9 ·347 • ·342 9 ·337	·364 ·359 ·355 ·350 ·345	·372 ·367 ·362 ·357 ·352	· 380 · 375 · 376 · 365 · 360	·388 ·383 ·378 ·378 ·378 ·378	·396 ·391 ·386 ·386 ·381	·405 ·399 ·394 ·389 ·383	·413 ·407 ·402 ·396 ·391	3 ·421 7 ·415 2 ·410 5 ·404 1 ·398	·429 ·423 ·418 ·412 ·412	·437 ·431 ·426 ·426 ·426 ·426	·445 ·439 ·433 ·427 ·421
41 42 43 44 45	·300 ·300 ·300 ·290	9 ·317 5 ·312 5 ·307 5 ·307 5 ·307	7 ·325 2 ·320 7 ·314 2 ·300 7 ·304	5 ·332 0 ·327 • ·322 • ·317 • ·311	·340 ·334 ·329 ·324 ·318	·347 ·342 ·336 ·331 ·325	·355 ·349 ·344 ·338 ·332	· 362 · 357 · 351 · 345 · 345 · 339	·370 ·364 ·358 ·352 ·352	·377 ·372 ·366 ·366 ·360 ·354	•385 •379 •373 •367 •361	5 · 392 9 · 386 3 · 386 7 · 374 t · 368	·400 ·394 ·388 ·381 ·375	·408 ·401 ·395 ·388 ·382	·415 ·409 ·402 ·396 ·389
46 47 48 49 50	·28 ·280 ·274 ·260 ·264	5 ·292 •286 •286 •281 •281 •276 •276 •276 •276	2 ·299 5 ·293 1 ·288 5 ·282 5 ·282 5 ·276	9 ·306 3 ·300 8 ·294 2 ·289 5 ·283	·313 ·307 ·301 ·295 ·289	·320 ·314 ·308 ·302 ·296	0 ·326 • ·321 3 ·312 2 ·308 5 ·302	5 ·333 1 ·327 4 ·321 3 ·315 2 ·300	340 334 328 328 321 321	·347 ·341 ·335 ·328 ·321	·354 ·348 ·341 ·335 ·328	4 ·361 3 ·355 1 ·348 5 ·341 3 ·334	· 368 · 361 · 355 · 348 · 341	3 · 375 · 368 · 361 · 361 · 354 · 347	·382 ·375 ·368 ·361 ·354
51 52 53 54 55	·258 ·253 ·244 ·244 ·23	8 ·264 2 ·259 7 ·253 1 ·24 5 ·24	4 ·271 9 ·269 3 ·259 7 ·253 1 ·24	1 ·277 5 ·271 9 ·265 3 ·259 7 ·252	·283 ·277 ·271 ·265 ·258	·280 ·283 ·277 ·270 ·264	$ \begin{array}{c} 9 \cdot 296 \\ 3 \cdot 286 \\ 7 \cdot 286 \\ 5 \cdot 276 \\ 4 \cdot 276 \\ 4 \cdot 276 \\ \end{array} $	5 · 302 9 · 296 3 · 289 5 · 282 5 · 282	2 · 308 5 · 302 9 · 295 2 · 288 5 · 281	3 ·315 2 ·308 5 ·301 3 ·294 1 ·287	·321 ·314 ·307 ·300 ·293	1 ·327 4 ·320 7 ·31 5 ·306 3 ·298	7 ·334 9 ·326 9 ·316 9 ·316 9 ·312 9 ·312	· 340 · 332 · 325 · 317 · 310	·346 ·339 ·331 ·323 ·315
56 57 58 59 60	·22 ·22 ·21 ·21	9 ·23 3 ·22 7 ·22 1 ·21 5 ·21	5 ·240 9 ·23 3 ·22 6 ·22 0 ·21	$ \begin{array}{c} 0 & \cdot 246 \\ 4 & \cdot 246 \\ 8 & \cdot 233 \\ 1 & \cdot 227 \\ 5 & \cdot 226 \\ \hline 0 & \cdot 227 \\ 0 & \cdot 226 \\ $	·252 ·245 ·238 ·232 ·232 ·225	·257 ·251 ·244 ·237 ·230	7 ·26 1 ·250 4 ·249 7 ·242 0 ·23	3 ·268 5 ·261 9 ·254 2 ·242 5 ·240	8 ·274 1 ·267 1 ·267 1 ·260 7 ·252 0 ·24	+ ·280 7 ·272 0 ·265 2 ·258 5 ·250	·28 ·278 ·278 ·270 ·263 ·255	5 ·291 8 ·283 9 ·276 3 ·268 5 ·266	·296 3 ·289 5 ·281 3 ·273 5 ·273 5 ·265	5 · 302 9 · 294 1 · 286 3 · 278 5 · 276	2 ·308 ·300 ·291 3 ·283 ·275
61 62 63 64 65	·199 ·192 ·180 ·180 ·180	9 ·202 2 ·197 5 ·197 5 ·197 5 ·182 3 ·177	4 ·202 7 ·202 1 ·192 4 ·182 7 ·182	8 ·213 2 ·207 5 ·200 8 ·193 2 ·186	·218 ·211 ·204 ·197 ·190	·223 ·210 ·200 ·200 ·194	3 ·228 5 ·221 9 ·213 2 ·206 4 ·196	8 ·233 1 ·223 3 ·218 5 ·210 9 ·203	3 ·238 5 ·230 3 ·222 0 ·215 3 ·207	8 ·242 • ·235 2 ·227 5 ·219 7 ·211	·242 ·239 ·232 ·222 ·216	$7 \cdot 252 \\ 2 \cdot 244 \\ 2 \cdot 236 \\ 4 \cdot 228 \\ 5 \cdot 226 \\ 2 \cdot 236 \\ 2 \cdot 226 \\ 3 \cdot $	2 ·257 4 ·249 5 ·241 3 ·232 5 ·232	7 ·262 9 ·254 1 ·245 2 ·237 1 ·228	2 ·267 4 ·258 5 ·250 7 ·241 8 ·232

Showing Difference of Longitude and Corresponding Departure.

at.]	DIFFE	ERENC	e of	r lo	NGI	TUDE					
	•56	•57	·58	•59	•60	•61	•62	•63	•64	•65	•66	•67	•68	•69	·70
° 2 4 6 8 10	·560 ·559 ·557 ·555 ·555	·570 ·569 ·567 ·564 ·561	·580 ·579 ·577 ·574 ·571	·590 ·589 ·587 ·584 ·584 ·581	·600 ·599 ·597 ·594 ·591	·610 ·609 ·607 ·604 ·601	-620 -618 -617 -614 -611	·630 ·628 ·627 ·624 ·620	•640 •638 •636 •634 •630	·650 ·648 ·646 ·644 ·640	·660 ·658 ·656 ·654 ·650	·670 ·668 ·666 ·663 ·660	·680 ·678 ·676 ·673 ·670	·690 ·688 ·686 ·683 ·683	·700 ·698 ·696 ·693 ·689
11 12 13 14 15	·550 ·548 ·546 ·543 ·543 ·541	·560 ·558 ·555 ·553 ·553 ·551	·569 ·567 ·565 ·563 ·560	·579 ·577 ·575 ·572 ·570	·589 ·587 ·585 ·582 ·580	·599 ·597 ·594 ·592 ·589	·609 ·606 ·604 ·602 ·599	·618 ·616 ·614 ·611 ·609	·628 ·626 ·624 ·621 ·618	·638 ·636 ·633 ·631 ·628	·648 ·646 ·643 ·640 ·638	·658 ·655 ·653 ·650 ·647	·668 ·665 ·663 ·660 ·657	·677 ·675 ·672 ·670 ·666	·687 ·685 ·682 ·679 ·676
16	·538	·548	·558	·567	·577	·586	·596	·606	·615	·625	·634	·644	·654	·663	·673
17	·536	·545	·555	·564	·574	·583	·593	·602	·612	·622	·631	·641	·650	·660	·669
18	·533	·542	·552	·561	·571	·580	·590	·599	·609	·618	·628	·637	·647	·656	·666
19	·529	·539	·548	·558	·567	·577	·586	·596	·605	·615	·624	·633	·643	·652	·662
20	·526	·536	·545	·554	·564	·573	·583	·592	·601	·611	·620	·630	·639	·648	·658
21	·523	·532	·541	·551	·560	·569	579	·588	·597	·607	·616	·625	•635	•644	·654
22	·519	·528	·538	·547	·556	·566	575	·584	·593	·603	·612	·621	·630	•640	·649
23	·515	·525	·534	·543	·552	·562	571	·580	·589	·598	·608	·617	·626	•635	·644
24	·512	·521	·530	·539	·548	·557	566	·576	·585	·594	·603	·612	·621	•630	·639
25	·508	·517	·526	·535	·544	·553	562	·571	·585	·589	·598	·607	·616	•625	·634
26	·503	·512	·521	·530	·539	·548	·557	·566	·575	·584	·593	·602	·611	·620	·629
27	·499	·508	·517	·526	·535	·544	·552	·561	·570	·579	·588	·597	·606	·615	•624
28	·494	·503	·512	·521	·530	·539	·547	·556	·565	·574	·583	·592	·600	·609	·618
29	·490	·499	·507	·516	·525	·534	·542	·551	·560	·569	·577	·586	·595	·603	·612
30	·485	·494	·502	·511	·520	·528	·537	·546	·554	·563	·572	·580	·589	·598	·606
31 32 33 34 35	·480 ·475 ·470 ·464 ·459	·489 ·483 ·478 ·473 ·473 ·467	·497 ·492 ·486 ·481 ·475	·506 ·500 ·495 ·489 ·483	·514 ·509 ·503 ·497 ·491	·523 ·517 ·512 ·506 ·500	·531 ·526 ·520 ·514 ·508	·540 ·534 ·528 ·522 ·516	·549 ·543 ·537 ·531 ·524	·557 ·551 ·545 ·539 ·532	·566 ·560 ·554 ·547 ·541	•574 •568 •562 •555 •549	·583 ·577 ·570 ·564 ·557	·591 ·585 ·579 ·572 ·565	·600 ·594 ·587 ·580 ·573
36	·453	·461	·469	·477	·485	·494	·502	·510	·518	·526	·534	·542	·550	·558	·566
37	·447	·455	·463	·471	·479	·487	·495	·503	·511	·519	·527	·535	·543	·551	·559
38	·441	·449	·457	·465	·473	·481	·489	·496	·504	·512	·520	·528	·536	·544	·552
39	·435	·443	·451	·459	·466	·474	·482	·490	·497	·505	·513	·521	·528	·536	·544
40	·429	·437	·444	·452	·460	·467	·475	·483	·490	·498	·506	·513	·521	·529	·536
41	·423	·430	·438	·445	·453	·460	·468	·475	·483	·491	·498	·506	·513	·521	·528
42	·416	·424	·431	·438	·446	·453	·461	·468	·476	·483	·490	·498	·505	·513	·520
43	·410	·417	·424	·431	·439	·446	·453	·461	·468	·475	·483	·490	·497	·505	·512
44	·403	·410	·417	·424	·432	·439	·446	·453	·460	·468	·475	·482	·489	·496	·504
45	·396	·403	·410	·417	·424	·431	·438	·445	·453	·460	·467	·474	·481	·488	·495
46	·389	·396	·403	·410	·417	·424	·431	·438	·445	·452	·458	·465	·472	·479	•486
47	·382	·389	·396	·402	·409	·416	·423	·430	·436	·443	·450	·457	·464	·471	•477
48	·375	·381	·388	·395	·401	·408	·415	·422	·428	·435	·442	·448	·455	·462	•468
49	·367	·374	·381	·387	·394	·400	·407	·413	·420	·426	·433	·440	·446	·453	•459
50	·360	·366	·373	·379	·386	·392	·399	·405	·411	·418	·424	·431	·437	·444	•450
51 52 53 54 55	·352 ·345 ·337 ·329 ·321	·359 ·351 ·343 ·335 ·327	·365 ·357 ·349 ·341 ·333	·371 ·363 ·355 ·347 ·338	·378 ·369 ·361 ·353 ·344	·384 ·376 ·367 ·359 ·359	·390 ·382 ·373 ·364 ·356	·396 ·388 ·379 ·370 ·370 ·361	·403 ·394 ·385 ·376 ·367	·409 ·400 ·391 ·382 ·373	·415 ·406 ·397 ·388 ·379	·422 ·412 ·403 ·394 ·384	·428 ·419 ·409 ·400 ·390	·434 ·425 ·415 ·406 ·396	·441 ·431 ·421 ·411 ·402
56	·313	·319	·324	·330	·336	·341	·347	·352	·358	·363	·369	·375	·380	·386	·391
57	·305	·310	·316	·321	·327	·332	·338	·343	·349	·354	·359	·365	·370	·376	·381
58	·297	·302	·307	·313	·318	·323	·329	·334	·339	·344	·350	·355	·360	·366	·371
59	·288	·294	·299	·304	·309	·314	·319	·324	·330	·335	·340	·345	·350	·355	·361
60	·280	·285	·290	·295	·300	·305	·310	·315	·320	·325	·330	·335	·340	·345	·350
61 62 63 64 65	·271 ·263 ·254 ·245 ·237	·276 ·268 ·259 ·250 ·250 ·241	·281 ·272 ·263 ·254 ·245	·286 ·277 ·268 ·259 ·249	·291 ·282 ·272 ·263 ·254	·296 ·286 ·277 ·267 ·258	·301 ·291 ·281 ·272 ·262	·305 ·296 ·286 ·276 ·266	·310 ·300 ·291 ·281 ·270	·315 ·305 ·295 ·285 ·275	•320 •310 •300 •289 •279	·325 ·315 ·304 ·294 ·283	·330 ·319 ·309 ·298 ·287	·335 ·324 ·313 ·302 ·292	·339 ·329 ·318 ·307 ·296

SHOWING DIFFERENCE OF LONGITUDE AND CORRESPONDING DEPARTURE.

at.				D	IFFEI	RENCE	OF	LON	GIT	UDE.					
Г	•71	·72	•73	•74	•75	•76	•77	• 7 8	•79	·80	•81	·82	•83	•84	•85
° 2 4 6 8 10	·710 ·708 ·706 ·703 ·699	·720 ·718 ·716 ·713 ·709	·730 ·728 ·726 ·723 ·719	·740 ·738 ·736 ·733 ·729	·750 ·748 ·746 ·743 ·739	·760 ·758 ·756 ·753 ·748	•770 •768 •766 •763 •758	·780 ·778 ·776 ·772 ·768	·790 ·788 ·786 ·782 ·782	·800 ·798 ·796 ·792 ·788	·810 ·808 ·806 ·802 ·798	·819 ·818 ·816 ·816 ·812 ·808	·829 ·828 ·825 ·825 ·822	·839 ·838 ·835 ·832 ·827	·849 ·848 ·845 ·842 ·837
11 12 13 14 15	·697 ·694 ·692 ·689 ·686	·707 ·704 ·702 ·699 ·695	·717 ·714 ·711 ·708 ·705	·726 ·724 ·721 ·718 ·715	·736 ·734 ·731 ·728 :724	·746 ·743 ·741 ·737 ·734	·756 ·753 ·750 ·747 ·744	·766 ·763 ·760 ·757 ·753	·775 ·773 ·770 ·767 ·763	·785 ·783 ·779 ·776 ·773	·795 ·792 ·789 ·786 ·786	·805 ·802 ·799 ·796 ·792	·815 ·812 ·809 ·805 ·802	•825 •822 •818 •815 •815	·834 ·831 ·828 ·825 ·825 ·821
16 17 18 19 20	·682 ·679 ·675 ·671 ·667	·692 ·689 ·685 ·681 ·677	·702 ·698 ·694 ·690 ·686	·711 ·708 ·704 ·700 ·695	·721 ·717 ·713 ·709 ·705	·731 ·727 ·723 ·719 ·714	·740 ·736 ·732 ·728 ·724	·750 ·746 ·742 ·738 ·733	·759 ·755 ·751 ·747 ·742	·769 ·765 ·761 ·756 ·752	·779 ·775 ·770 ·766 ·761	·788 ·784 ·780 ·775 ·771	·798 ·794 ·789 ·785 ·785	·807 ·803 ·799 ·794 ·789	·817 ·813 ·808 ·804 ·799
21 22 23 24 25	·663 ·658 ·654 ·649 ·643	*672 •668 •663 •658 •658	·682 ·677 ·672 ·667 ·662	·691 ·686 ·681 ·676 ·671	·700 ·695 ·690 ·685 ·680	·710 ·705 ·700 •694 •689	·719 ·714 ·709 ·703 ·698	·728 ·723 ·718 ·713 ·707	·738 ·732 ·727 ·722 ·722 ·716	·747 ·742 ·736 ·731 ·725	·756 ·751 ·746 ·740 ·734	·766 ·760 ·755 ·749 ·743	·775 ·770 ·764 ·758 ·752	·784 ·779 ·773 ·767 ·761	·794 ·788 ·782 ·777 ·770
26 27 28 29 30	·638 ·633 ·627 ·621 ·615	·647 ·642 ·636 ·636 ·636	·656 ·650 ·645 ·638 ·632	·665 ·659 ·653 ·647 ·641	·674 ·668 ·662 ·656 ·650	·683 ·677 ·671 ·665 ·658	·692 ·686 ·680 ·673 ·667	·701 ·695 ·689 ·682 ·675	·710 ·704 ·698 ·691 ·684	·719 ·713 ·706 ·700 ·693	·728 ·722 ·715 ·708 ·701	·737 ·731 ·724 ·717 ·710	·746 ·740 ·733 ·726 ·719	·755 ·748 ·742 ·735 ·727	·764 ·757 ·751 ·743 ·736
31 32 33 34 35	·609 ·602 ·595 ·589 ·582	·617 ·611 ·604 ·597 ·596	·626 ·619 ·612 ·612 ·605 ·598	·634 ·628 ·621 ·613 ·606	·643 ·636 ·629 ·622 ·614	·651 ·645 ·637 ·630 ·623	·660 ·653 ·646 ·638 ·631	·669 ·661 ·654 ·647 ·639	·677 ·670 ·663 ·655 ·647	·686 ·678 ·671 ·663 ·655	·694 ·687 ·679 ·672 ·664	·703 ·695 ·688 ·680 ·672	·711 ·704 ·696 ·688 ·680	·720 ·712 ·704 ·696 ·688	·729 ·721 ·713 ·705 ·696
36 37 38 39 40	*574 *567 *559 *552 *544	·582 ·575 ·567 ·560 ·552	·591 5 ·583 7 ·575 0 ·567 2 ·559	·599 ·591 ·583 ·575 ·567	·607 ·599 ·591 ·583 ·575	·615 ·607 ·599 ·591 '582	·623 ·615 ·607 ·598 ·590	·631 ·623 ·615 ·606 ·598	·639 ·631 ·623 ·614 ·605	·647 ·639 ·630 ·622 ·613	·655 ·647 ·638 ·629 ·620	·663 ·655 ·646 ·637 ·628	·671 ·663 ·654 ·645 ·636	·680 ·671 ·662 ·653 ·643	·688 ·679 ·670 ·661 ·651
41 42 43 44 45	·530 ·528 ·519 ·511 ·502	543 535 535 527 518 5518	$5 \cdot 551$ $5 \cdot 542$ $7 \cdot 534$ $5 \cdot 525$ $5 \cdot 516$	·558 ·550 ·541 ·532 ·523	·566 ·557 ·549 ·540 ·530	·574 ·565 ·556 ·557 ·547 ·537	·581 ·572 ·563 ·554 ·544	·589 ·580 ·570 ·561 ·552	·596 ·587 ·578 ·568 ·559	·604 ·595 ·585 ·575 ·566	·611 ·602 ·592 ·583 ·573	·619 ·609 ·600 ·590 ·580	·626 ·617 ·607 ·597 ·5 ⁸ 7	·634 ·624 ·614 ·604 ·594	·642 ·632 ·622 ·611 ·601
46 47 48 49 50	·493 ·484 ·475 ·466 ·456	·500 ·491 ·482 ·482 ·472 ·463	·507 ·498 ·488 ·488 ·479 ·469	·514 ·505 ·495 ·485 ·476	·521 ·511 ·502 ·492 ·482	·528 ·518 ·509 ·499 ·489	·535 ·525 ·515 ·505 ·495	·542 ·532 ·522 ·512 ·501	·549 ·539 ·529 ·518 ·508	·556 ·546 ·535 ·525 ·514	· ·563 ·552 ·542 ·531 ·521	·570 ·559 ·549 ·538 ·527	·577 ·566 ·555 ·545 ·534	·584 ·573 ·562 ·551 ·540	•590 •580 •569 •558 •546
51 52 53 54 55	·447 ·437 ·427 ·417 ·407	7 •453 •443 •433 •423 •423	3 ·459 3 ·449 3 ·439 3 ·429 3 ·429 3 ·419	·466 ·456 ·445 ·445 ·435 ·424	·472 ·462 ·451 ·441 ·430	·478 ·468 ·457 ·447 ·436	·485 ·474 ·463 ·453 ·442	·491 ·480 ·469 ·458 ·447	·497 ·486 ·475 ·464 ·453	·503 ·493 ·481 ·470 ·459	·510 ·499 ·487 ·476 ·465	·516 ·505 ·493 ·482 ·482	·522 ·511 ·500 ·488 ·476	·529 ·517 ·506 ·494 ·482	·535 ·523 ·512 ·500 ·488
56 57 58 59 60	·397 ·387 ·376 ·366 ·355	·403 ·392 ·382 ·382 ·371 ·360	·408 ·398 ·387 ·376 ·365	·414 ·403 ·392 ·381 ·370	·419 ·408 ·397 ·386 ·375	·425 ·414 ·403 ·391 ·380	·431 ·419 ·408 ·397 ·385	·436 ·425 ·413 ·402 ·390	·442 ·430 ·419 ·407 ·395	·447 ·436 ·424 ·412 ·400	·453 ·441 ·429 ·417 ·405	·459 ·447 ·435 ·422 ·410	·464 ·452 ·440 ·427 ·415	·470 ·457 ·445 ·433 ·420	·475 ·463 ·450 ·438 ·425
61 62 63 64 65	·344 ·333 ·322 ·311 ·300	·349 ·338 ·327 ·316 ·304	·354 ·343 ·331 ·320 ·309	·359 ·347 ·336 ·324 ·313	·364 ·352 ·340 ·329 ·317	·368 ·357 ·345 ·333 ·321	·373 ·361 ·350 ·338 ·325	·378 ·366 ·354 ·342 ·330	·383 ·371 ·359 ·346 ·334	·388 ·376 ·363 ·351 ·338	·393 ·380 ·368 ·355 ·342	·398 ·385 ·372 ·359 ·347	·402 ·390 ·377 ·364 ·351	·407 ·394 ·381 ·368 ·355	·412 ·399 ·386 ·373 ·359

SHOWING DIFFERENCE OF LONGITUDE AND CORRESPONDING DEPARTURE.

at.				D	IFFER	ENCE	OF	LON	GIT	UDE.					
Γ	•86	•87	•88	•89	•90	·91	• 9 2	•93	•94	•95	•96	•97	•98	•99	1.00
° 2 4 6 8 10	·859 ·858 ·855 ·855 ·852 ·847	·869 ·868 ·865 ·862 ·857	·879 ·878 ·875 ·871 ·867	·889 ·888 ·885 ·881 ·876	·899 ·898 ·895 ·891 ·886	·909 ·908 ·905 ·901 ·896	·919 ·918 ·915 ·911 ·906	·929 ·928 ·925 ·921 ·916	·939 ·938 ·935 ·931 ·926	·949 ·948 ·945 ·941 ·936	·959 ·958 ·955 ·951 ·945	·969 ·968 ·965 ·961 ·955	·979 ·978 ·975 ·970 ·965	·989 ·988 ·985 ·980 ·975	·999 ·998 ·995 ·990 ·985
11 12 13 14 15	·844 ·841 ·838 ·834 ·831	·854 ·851 ·848 ·844 ·840	·864 ·861 ·857 ·854 ·850	·874 ·871 ·867 ·864 ·860	·883 ·880 ·877 ·873 ·869	·893 ·890 ·887 ·883 ·879	·903 ·900 ·896 ·893 ·889	·913 ·910 ·906 ·902 ·898	·923 ·919 ·916 ·912 ·908	·933 ·929 ·926 ·922 ·918	·942 ·939 ·935 ·931 ·927	·952 ·949 ·945 ·941 ·937	·962 ·959 ·955 ·951 ·947	·972 ·968 ·965 ·961 ·956	·982 ·978 ·974 ·970 ·966
16 17 18 19 20	·827 ·822 ·818 ·813 ·808	·836 ·832 ·827 ·823 ·818	·846 ·842 ·837 ·832 ·827	·856 ·851 ·846 ·842 ·836	·865 ·861 ·856 ·851 ·846	·875 ·870 ·865 ·860 ·855	·884 ·880 ·875 ·870 ·865	·894 ·889 ·884 ·879 ·874	•904 •899 •894 •889 •883	·913 ·908 ·904 ·898 ·893	·923 ·918 ·913 ·908 ·902	·932 ·928 ·923 ·917 ·912	·942 ·937 ·932 ·927 ·921	·952 ·947 ·942 ·936 ·930	·961 ·956 ·951 ·946 ·940
21 22 23 24 25	·803 ·797 ·792 ·786 ·779	·812 ·807 ·801 ·795 ·788	·822 ·816 ·810 ·804 ·79 ⁸	•831 •825 •819 •813 •807	·840 ·834 ·828 ·822 ·816	·850 ·844 ·838 ·831 ·825	·859 ·853 ·847 ·840 ·834	·868 ·862 ·856 ·850 ·843	·878 ·872 ·865 ·859 ·852	·887 ·881 ·874 ·868 ·861	·896 ·890 ·884 ·877 ·870	·906 ·899 ·893 ·886 ·879	·915 ·909 ·902 ·895 ·888	·924 ·918 ·911 ·904 ·897	·934 ·927 ·921 ·914 ·906
26 27 28 29 30	·773 ·766 ·759 ·752 ·745	·782 ·775 ·768 ·761 ·753	·791 ·784 ·777 ·770 ·762	·800 ·793 ·786 ·778 ·778 ·771	·809 ·802 ·795 ·787 ·779	·818 ·811 ·803 ·796 ·788	·827 ·820 ·812 ·805 ·797	·836 ·829 ·821 ·813 ·805	·845 ·838 ·830 ·822 ·814	·854 ·846 ·839 ·831 ·823	·863 ·855 ·848 ·840 ·831	·872 ·864 ·856 ·848 ·840	·881 ·873 ·865 ·857 ·849	·890 ·882 ·874 ·866 ·857	·899 ·891 ·883 ·875 ·866
31 32 33 34 35	·737 ·729 ·721 ·713 ·704	·746 ·738 ·730 ·721 ·713	·754 ·746 ·738 ·730 ·721	·763 ·755 ·746 ·738 ·729	·771 ·763 ·755 ·746 ·737	·780 ·772 ·763 ·754 ·745	·789 ·780 ·772 ·763 ·754	·797 ·789 ·780 ·771 ·762	·806 ·797 ·788 ·779 ·779 ·770	·814 ·806 ·797 ·788 ·778	·823 ·814 ·805 ·796 ·786	·831 ·823 ·814 ·804 ·795	·840 ·831 ·822 ·812 ·803	-849 -840 -830 -821 -811	·857 ·848 ·839 ·829 ·819
36 37 38 39 40	·696 ·687 ·678 ·668 ·659	·704 ·695 ·686 ·686 ·676 ·666	·712 ·703 ·693 ·684 ·674	·720 ·711 ·701 ·692 ·682	·728 ·719 ·709 ·699 ·689	·736 ·727 ·717 ·707 ·697	·744 ·735 ·725 ·715 ·705	·752 ·743 ·733 ·723 ·712	·760 ·751 ·741 ·731 ·720	·769 ·759 ·749 ·738 ·728	·777 ·767 ·756 ·746 ·735	·785 ·775 ·764 ·754 ·743	·793 ·783 ·772 ·762 ·751	·801 ·791 ·780 ·769 ·758	-809 -799 -788 -777 -766
41 42 43 44 45	·649 ·639 ·629 ·619 ·618) ·657) ·647) ·636) ·626] ·615	·664 ·654 ·644 ·633 ·622	·672 ·661 ·651 ·640	·679 ·669 ·658 ·647 ·636	·687 ·676 ·666 ·655 ·643	·694 ·684 ·673 ·662 ·651	·702 ·691 ·680 ·669 ·658	·709 ·699 ·687 ·676 ·675	·717 ·706 ·695 ·683 ·672	·725 ·713 ·702 ·691 ·679	·732 ·721 ·709 ·698 ·686	·74C ·728 ·717 ·705 ·693	·747 ·736 ·724 ·712 ·700	•755 •743 •731 •719 •707
46 47 48 49 50	·592 ·582 ·572 ·562 ·562	7 ·604 7 ·593 5 ·582 4 ·571 3 ·559	·611 ·600 ·580 ·577	1 ·618 0 ·607 0 ·596 7 ·584 0 ·572	8 ·625 7 ·614 5 ·602 1 ·590 2 ·579	·632 ·621 ·600 ·597 ·585	2 ·639 (·627) ·616 7 ·604 ; ·591	·646 ·634 ·622 ·610 ·598	·653 ·641 ·629 ·617 ·604	·660 ·648 ·636 ·623 ·611	·667 ·655 ·642 ·630 ·617	·674 ·662 ·649 ·636	·681 ·668 ·656 ·656 ·643 ·630	·088 ·675 ·662 ·662 ·649	· 095 · 682 · 669 · 656 · 643
51 52 53 54 55	·54 ·520 ·518 ·503 ·493	1 ·54 ⁸ 9 ·536 8 ·524 5 ·511 3 ·499	3 ·554 5 ·544 1 ·539 1 ·539 1 ·595	4 ·560 2 ·548 5 ·536 7 ·523 5 ·510	0 ·566 3 ·554 5 ·542 3 ·529 5 ·516	·573 ·560 ·548 ·535 ·522	3 ·579 5 ·566 3 ·554 5 ·541 2 ·528	585 5 •573 • •560 • •547 • •547 • •533	5 ·592 3 ·579 5 ·566 7 ·553 3 ·539	·598 ·585 ·572 ·558 ·545	·604 ·591 ·578 ·564 ·551	·610 ·597 ·584 ·579	- 017 7 · 603 1 · 590 0 · 576 5 · 562	· ·023 · · · · · · · · · · · · · · · · · · ·	5 ·029 5 ·616 5 ·602 2 ·588 5 ·574
56 57 58 59 60	·48 ·460 ·450 ·44 ·430	1 ·48(8 ·474 5 ·461 3 ·44 ⁸ 2 ·435	5 ·49: 1 ·479 1 ·460 3 ·460 3 ·453 5 ·449	2 ·498 9 ·485 5 ·472 3 ·458 0 ·445	5 ·503 5 ·490 2 ·477 3 ·464 5 ·450	·509 ·490 ·482 ·482 ·469 ·455	9 ·514 6 ·501 2 ·488 9 ·474 5 ·460	+ ·520 - ·507 - ·493 + ·479 - ·465	526 7 ·512 3 ·498 3 ·484 5 ·470	·531 ·517 ·503 ·489 ·475	·537 ·523 ·509 ·494 ·480	·54 ·528 ·514 ·514 ·514 ·500 ·48	2 ·54 ⁸ 8 ·534 4 ·519 5 ·505 5 ·490	55- 539 525 5-510 -525 -510 -495	+ '559 - 545 5 · 530 - 515 5 · 500 - • • • •
61 62 63 64 65	·41 ·404 ·399 ·377 ·365	7 •42: 4 •408 0 •395 7 •381 3 •368	2 ·42 3 ·41 5 ·400 1 ·380 3 ·37	7 ·43 3 ·418 5 ·402 5 ·390 2 ·370	1 ·436 8 ·423 4 ·409 0 ·395 5 ·380	·44 ·42 ·41 ·399 ·38	1 ·44(7 ·432 3 ·418 9 ·403 5 ·389	2 ·45 ¹ 2 ·437 3 ·422 3 ·408 9 ·393	1 ·45(7 ·441 2 ·427 3 ·412 3 ·397	•461 •446 7 •431 •416 7 •401	·465 ·451 ·436 ·421 ·406	0 ·479 ·45. 0 ·449 ·449 ·42. 0 ·419	5 ·475 5 ·460 5 ·445 5 ·445 5 ·430 5 ·412	5 ·480 5 ·465 5 ·449 5 ·434 1 ·41	4°5 •469 •454 •438 3 •423

SHOWING DIFFERENCE OF LONGITUDE AND CORRESPONDING DEPARTURE.

at.					DIFI	EREI	NCE	OF I	LONG	GITU	DE.					
	•10	•11	•12	•13	•14	•15	•16	•17	•18	•19	•20	•21	•22	·23	•24	·25
65 66 67 68 69	·042 ·041 ·039 ·037 ·036	·046 ·045 ·043 ·041 ·039	·051 ·049 ·047 ·045 ·043	·055 ·053 ·051 ·049 ·047	·059 ·057 ·055 ·052 ·050	•06; •06; •059 •056	3 ·068 1 ·065 9 ·063 9 ·063 •063 •057	•072 •069 •066 •064 •061	·076 ·073 ·076 ·076 ·067	5 ·080 3 ·077 0 ·074 7 ·071 5 ·068	·08: ·081 ·078 ·075 ·072	5 ·089 1 ·085 3 ·082 5 ·079 2 ·075	·093 ·089 ·086 ·082 ·082	·097 ·094 ·090 ·086 ·082	·101 ·098 ·094 ·096 ·086	·106 ·102 ·098 ·094 ·090
70 71 72 73 74	·034 ·033 ·031 ·029 ·028	·038 ·036 ·034 ·032 ·030	·041 ·039 ·037 ·035 ·033	·044 ·042 ·040 ·038 ·036	·048 ·046 ·043 ·041 ·039	·051 ·049 ·046 ·044 ·041	·055 ·052 ·049 ·047 ·044	·058 ·055 ·053 ·050 ·047	·062 ·059 ·056 ·053 ·050	·065 ·062 ·059 ·056 ·052	·068 ·062 ·062 ·058 ·055	3 ·072 5 ·068 2 ·065 3 ·061 5 ·058	·075 ·072 ·068 ·064 ·061	·079 ·075 ·071 ·067 ·063	·082 ·078 ·074 ·074 ·070 ·066	•086 •081 •077 •073 •069
75	·026	·028	·031	·034	·036	·039	·041	·044	·047	·049	·052	·054	·057	·060	·062	·065
76	·024	·027	·029	·031	·034	·036	·039	·041	·044	·046	·048	·051	·053	·056	·058	·060
77	·022	·025	·027	·029	·031	·034	·036	·038	·040	·043	·045	·047	·049	·052	·054	·056
78	·021	·023	·025	·027	·029	·031	·033	·035	·037	·040	·042	·044	·046	·048	·050	·052
79	·019	·021	·023	·025	·027	·029	·031	·032	·034	·036	·038	·040	·042	·044	·046	·048
80	·017	·019	·021	·023	·024	·026	·028	·030	·031	·033	·035	·036	·038	·040	·042	·043
81	·016	·017	·019	·020	·022	·023	·025	·027	·028	·030	·031	·033	·034	·036	·038	·039
82	·014	·015	·017	·018	·019	·021	·022	·024	·025	·026	·028	·029	·031	·032	·033	·035
83	·012	·013	·015	·016	·017	·018	·019	·021	·022	·023	·024	·026	·027	·028	·029	·030
84	·010	·011	·013	·014	·015	·016	·017	·018	·019	·020	·021	·022	·023	·024	·025	·026
85	·009	·010	•010	·011	·012	·013	·014	·015	·016	·017	·017	·018	·019	·020	·021	·022
86	·007	·008	•008	·009	·010	·010	·011	·012	·013	·013	·014	·015	·015	·016	·017	·017
87	·005	·006	•006	·007	·007	·008	·008	·009	·009	·010	·010	·011	·012	·012	·013	·013
88	·003	·004	•004	·005	·005	·005	·006	·006	·006	·007	·007	·007	·008	·008	·008	·009
89	·002	·002	•002	·002	·002	·003	·003	·003	·003	·003	·003	·004	·004	·004	·004	·004
at.				L	IFFF	EREN	CE O	F LO	ONG	ITUD	E.					
п	•25	•26	•27	·28	•29	•30	•31	•32	•33	•34	•35	•36	•37	•38	•39	•40
65	·106	·110	·114	·118	·123	·127	·131	·135	·139	·144	·148	·152	·156	·161	·165	·169
66	·102	·106	·110	·114	·118	·122	·126	·130	·134	·138	·142	·146	·150	·155	·159	·163
67	·098	·102	·105	·109	·113	·117	·121	·125	·129	·133	·137	·141	·145	·148	·152	·156
68	·094	·097	·101	·105	·109	·112	·116	·120	·124	·127	·131	·135	·139	·142	·146	·150
69	·090	·093	·097	·100	·104	·108	·111	·115	·118	·122	·125	·129	·133	·136	·140	·143
70	·086	·089	·092	·096	·099	 ∙103 •098 •093 •088 •083 	·106	·109	·113	·116	·120	·123	·127	·130	·133	·137
71	·081	·085	·088	·091	·094		·101	·104	·107	·111	·114	·117	·120	·124	·127	·130
72	·077	·080	·083	·087	·090		·096	·099	·102	·105	·108	·111	·114	·117	·121	·124
73	·073	·076	·079	·082	·085		·091	·094	·096	·099	·102	·105	·108	·111	·114	·117
74	·069	·072	·074	·077	·080		·085	·088	·091	·094	·096	·099	·102	·105	·107	·110
75	·065	·067	·070	·072	·075	·078	·080	·083	·085	·088	·091	·093	·096	·098	·101	·104
76	·060	·063	·065	·068	·070	·073	·075	·077	·080	·082	·085	·087	·090	·092	·094	·097
77	·057	·058	·061	·063	·065	·067	·070	·072	·074	·076	·079	·081	·083	·085	·088	·090
78	·052	·054	·056	·058	·060	·062	·064	·067	·069	·071	·073	·075	·077	·079	·081	·083
79	·048	·054	·052	·053	·055	·057	·059	·061	·063	·065	·067	·069	·071	·073	·074	·076
80 81 82 83 84	·043 ·039 ·035 ·030 ·026	•045 •041 •036 •032 •032 •027	047 042 038 033 028	·049 ·044 ·039 ·034 ·029	·050 ·045 ·040 ·035 ·030	·052 ·047 ·042 ·037 ·031	·054 ·048 ·043 ·038 ·032	·056 ·050 ·045 ·039 ·033	·057 ·052 ·046 ·040 ·034	·059 ·053 ·047 ·041 ·036	·061 ·055 ·049 ·043 ·037	·063 ·056 ·050 ·044 ·038	·064 ·058 ·051 ·045 ·039	·066 ·059 ·053 ·046 ·040	·068 ·061 ·054 ·048 ·041	·069 ·063 ·056 ·049 ·042
85	·022	·023 ·	024	·024	·025	·026	·027	·028	·029	·030	·031	·031	·032	·033	·034	·035
86	·017	·018 ·	019	·020	·020	·021	·022	·022	·023	·024	·024	·025	·026	·027	·027	·028
87	·013	·014 ·	014	·015	·015	·016	·016	·017	·017	·018	·018	·019	·019	·020	·020	·021
88	·009	·009 ·	009	·010	·010	·010	·011	·011	·012	·012	·012	·013	·013	·013	·014	·014
89	·004	·005 ·	005	·005	·005	·005	·005	·006	·006	·006	·006	·006	·006	·007	·007	·007

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SHOWING DIFFERENCE OF LONGITUDE AND CORRESPONDING DEPARTURE.

at.					DIF	FERE	NCE	OF	LON	GITU	DE.					
	•40	•41	•42	•43	•44	•45	•46	•47	•48	·49	•50	-51	•52	•53	•54	•55
65 66 67 68 69	·169 ·163 ·156 ·150 ·143	·173 ·167 ·160 ·154 ·147	·177 ·171 ·164 ·157 ·151	·182 ·175 ·168 ·161 ·154	·186 ·179 ·172 ·165 ·158	·190 ·183 ·176 ·169 ·161	·194 ·187 ·180 ·172 ·165	·199 ·191 ·184 ·176 ·168	·203 ·195 ·188 ·180 ·172	·207 ·199 ·191 ·184 ·176	·211 ·203 ·195 ·187 ·179	·216 ·207 ·199 ·191 ·183	·220 ·212 ·203 ·195 ·186	·224 ·216 ·207 ·199 ·190	·228 ·220 ·211 ·202 ·194	·232 ·224 ·215 ·206 ·197
70 71 72 73 74	·137 ·130 ·124 ·117 ·110	·140 ·133 ·127 ·120 ·113	·144 ·137 ·130 ·123 ·116	·147 ·140 ·133 ·126 ·119	·150 ·143 ·136 ·129 ·121	·154 ·147 ·139 ·132 ·124	·157 ·150 ·142 ·134 ·127	·161 ·153 ·145 ·137 ·130	·164 ·156 ·148 ·140 ·132	·168 ·160 ·151 ·143 ·135	·171 ·163 ·155 ·146 ·138	·174 ·166 ·158 ·149 ·141	·178 ·169 ·161 ·152 ·143	·181 ·173 ·164 ·155 ·146	·185 ·176 ·167 ·158 ·149	·188 ·179 ·170 ·161 ·152
75 76 77 78 79	•104 •097 •090 •083 •076	·106 ·099 ·092 ·085 ·078	·109 ·102 ·094 ·087 ·080	·111 ·104 ·097 ·089 ·082	·114 ·106 ·099 ·091 ·084	·116 ·109 ·101 ·094 ·086	·119 ·111 ·103 ·096 ·088	·122 ·114 ·106 ·098 ·090	•124 •116 •108 •100 •092	·127 ·119 ·110 ·102 ·193	·129 ·121 ·112 ·104 ·095	·132 ·123 ·115 ·106 ·097	·135 ·126 ·117 ·108 ·099	·137 ·128 ·119 ·110 ·101	·140 ·131 ·121 ·112 ·112	·142 ·133 ·124 ·114 ·105
80 81 82 83 84	·069 ·063 ·056 ·049 ·042	·071 ·064 ·057 ·050 ·043	·073 ·066 ·058 ·051 ·044	·075 ·067 ·060 ·052 ·045	·076 ·069 ·061 ·054 ·046	·078 ·070 ·063 ·055 ·047	·080 ·072 ·064 ·056 ·048	·082 ·074 ·065 ·057 ·049	·083 ·075 ·067 ·058 ·050	·085 ·077 ·068 ·060 ·051	·087 ·078 ·070 ·061 ·052	·089 ·080 ·071 ·062 ·053	·090 ·081 ·072 ·063 ·054	·092 ·083 ·074 ·065 ·055	·094 ·084 ·075 ·066 ·056	·096 ·086 ·077 ·067 ·057
85 86 87 88 89	·035 ·028 ·021 ·014 ·007	·036 ·029 ·021 ·014 ·007	·037 ·029 ·022 ·015 ·007	·037 ·030 ·023 ·015 ·008	·038 ·031 ·023 ·015 ·008	·039 ·031 ·024 ·016 ·008	·040 ·032 ·024 ·016 ·008	·041 ·033 ·025 ·016 ·008	·042 ·033 ·025 ·017 ·008	·043 ·034 ·026 ·017 ·009	·044 ·035 ·026 ·017 ·009	·044 ·036 ·027 ·018 ·009	·045 ·036 ·027 ·018 ·009	·046 ·037 ·028 ·018 ·009	·047 ·038 ·028 ·019 ·009	·048 ·038 ·029 ·019 ·010
at.					DIF	FERE	ENCE	C OF	LOI	NGITU	JDE					
	-55	•56	•57	•58	•59	•60	•61	·62	•63	•64	•65	•66	•67	•58	•69	•70
65 66 67 68 69	·232 ·224 ·215 ·206 ·197	·237 ·228 ·219 ·210 ·201	•241 •232 •223 •214 •204	·245 ·236 ·227 ·217 ·208	·249 ·240 ·231 ·221 ·211	·254 ·244 ·234 ·225 ·215	·258 ·248 ·238 ·229 ·219	·262 ·252 ·242 ·232 ·222	·266 ·256 ·246 ·236 ·236 ·226	·270 ·260 ·250 ·240 ·229	·275 ·264 ·254 ·243 ·223	·279 ·268 ·258 ·247 ·237	·283 ·273 ·262 ·251 ·240	·287 ·277 ·266 ·255 ·244	·292 ·281 ·270 ·258 ·247	·296 ·285 ·274 ·262 ·251
70 71	·188								1		~33	57				
72 73 74	·179 ·170 ·161 ·152	·192 ·182 ·173 ·164 ·154	•195 •186 •176 •167 •157	·198 ·189 ·179 ·170 ·160	·202 ·192 ·182 ·172 ·163	·205 ·195 ·185 ·175 ·175 ·165	·209 ·199 ·189 ·178 ·178 ·168	·212 ·202 ·192 ·181 ·171	·215 ·205 ·195 ·184 ·174	·219 ·208 ·198 ·187 ·176	·222 ·212 ·201 ·190 ·179	•226 •215 •204 •193 •182	·229 ·218 ·207 ·196 ·185	·233 ·221 ·210 ·199 ·187	·236 ·225 ·213 ·202 ·190	·239 ·228 ·216 ·205 ·193
72 73 74 75 76 77 78 79	·179 ·170 ·161 ·152 ·142 ·133 ·124 ·114 ·105	·192 ·182 ·173 ·164 ·154 ·145 ·135 ·126 ·116 ·107	·195 ·186 ·176 ·167 ·157 ·148 ·138 ·128 ·128 ·119 ·109	·198 ·189 ·179 ·170 ·160 ·150 ·140 ·130 ·121 ·111	·202 ·192 ·182 ·172 ·163 ·153 ·143 ·133 ·123 ·113	·205 ·195 ·185 ·175 ·165 ·155 ·145 ·135 ·125 ·125 ·114	·209 ·199 ·189 ·178 ·168 ·158 ·148 ·137 ·127 ·116	·212 ·202 ·192 ·181 ·171 ·160 ·150 ·139 ·129 ·118	·215 ·205 ·195 ·184 ·174 ·163 ·152 ·142 ·131 ·120	·219 ·208 ·198 ·187 ·176 ·166 ·155 ·144 ·133 ·122	·233 ·222 ·212 ·201 ·190 ·179 ·168 ·157 ·146 ·135 ·124	•226 •215 •204 •193 •182 •171 •160 •148 •137 •126	·229 ·218 ·207 ·196 ·185 ·173 ·162 ·151 ·139 ·128	·233 ·221 ·210 ·199 ·187 ·176 ·165 ·153 ·141 ·130	·236 ·225 ·213 ·202 ·190 ·179 ·167 ·155 ·143 ·132	·239 ·228 ·216 ·205 ·193 ·181 ·169 ·157 ·146 ·134
72 73 74 75 76 77 78 79 80 81 82 83 84	·179 ·170 ·161 ·152 ·142 ·133 ·124 ·114 ·105 ·096 ·086 ·077 ·067 ·057	·192 ·173 ·173 ·164 ·154 ·145 ·135 ·126 ·116 ·107 ·097 ·088 ·078 ·068	·195 ·186 ·176 ·167 ·157 ·148 ·138 ·128 ·119 ·109 ·099 ·089 ·079 ·069	-198 -189 -179 -170 -160 -150 -140 -130 -121 -111 -091 -081 -071 -061	·202 ·192 ·182 ·172 ·163 ·153 ·143 ·133 ·123 ·113 ·102 ·092 ·082 ·072 ·062	·205 ·195 ·185 ·175 ·165 ·145 ·145 ·145 ·145 ·144 ·094 ·084 ·073 ·063	·209 ·199 ·189 ·178 ·168 ·158 ·148 ·137 ·127 ·116 ·106 ·095 ·085 ·074 ·064	·212 ·202 ·192 ·181 ·171 ·160 ·150 ·139 ·129 ·118 ·108 ·097 ·086 ·076 ·065	·215 ·205 ·195 ·184 ·174 ·163 ·152 ·142 ·131 ·120 ·109 ·099 ·088 ·077 ·066	-219 -208 -198 -176 -176 -155 -144 -133 -122 -111 -100 -089 -078 -067	- 33 - 222 - 212 - 201 - 190 - 179 - 168 - 135 - 124 - 113 - 102 - 090 - 068	·226 ·215 ·204 ·193 ·182 ·171 ·160 ·148 ·137 ·126 ·115 ·103 ·092 ·080 ·069	·229 ·218 ·207 ·196 ·185 ·173 ·162 ·151 ·139 ·128 ·116 ·105 ·093 ·082 ·070	·233 ·221 ·199 ·187 ·176 ·165 ·153 ·141 ·130 ·118 ·106 ·095 ·083 ·071	·236 ·225 ·213 ·202 ·190 ·179 ·167 ·155 ·143 ·132 ·120 ·108 ·096 ·084 ·072	·239 ·228 ·216 ·205 ·193 ·181 ·169 ·157 ·146 ·134 ·122 ·110 ·097 ·085 ·073

5-Azimuth.

SHOWING DIFFERENCE OF LONGITUDE AND CORRESPONDING DEPARTURE.

æt.					DIFF	EREN	ICE	OF I	ONC	HTUI	DE.					
T	•70	•71	•72	•73	•74	•75	•76	•77	•78	•79	•80	•81	•82	•83	•84	•85
65	·296	·300	·304	·309	·313	·317	·321	·325	·330	·334	·338	·342	·347	·351	·355	·359
66	·285	·289	·293	·297	·301	·305	·309	·313	·317	·321	·325	·329	·334	·338	·342	·346
67	·274	·277	·281	·285	·289	·293	·297	·301	·305	·309	·313	·316	·320	·324	·328	·332
68	·262	·266	·270	·273	·277	·281	·285	·288	·292	·296	·300	·303	·307	·311	·315	·318
69	·251	·254	·258	·262	·265	·269	·272	·276	·280	·283	·287	·290	·294	·297	·301	·305
70	·239	·243	·246	·250	·253	·257	·260	·263	·267	·270	·274	·277	·280	·284	·287	·291
71	·228	·231	·234	·238	·241	·244	·247	·251	·254	·257	·260	·264	·267	·270	·273	·277
72	·216	·219	·222	·226	·229	·232	·235	·238	·241	·244	·247	·250	·253	·250	·260	·263
73	·205	·208	·211	·213	·216	·219	·222	·225	·228	·231	·234	·237	·240	·243	·246	·249
74	·193	·196	·198	·201	·204	·207	·209	·212	·215	·218	·221	·223	·226	·229	·232	·234
75	•181	·184	•186	·189	·192	·194	·197	·199	·202	·204	·207	·210	·212	·215	·217	·220
76	•169	·172	•174	·177	·179	·181	·184	·186	·189	·191	·194	·196	·198	·201	·203	·206
77	•157	·160	•162	·164	·166	·169	·171	·173	·175	·178	·180	·182	·184	·187	·189	·191
78	•146	·148	•150	·152	·154	·156	·158	·160	·162	·164	·166	·168	·170	·173	·175	·177
79	•134	·135	•137	·139	·141	·143	·145	·147	·149	·151	·153	·155	·156	·158	·160	·162
80	·122	·123	·125	·127	·128	·130	·132	·134	·135	·137	·139	·141	·142	·144	·146	·148
81	·110	·111	·113	·114	·116	·117	·119	·120	·122	·124	·125	·127	·128	·130	·131	·133
82	·097	·099	·100	·102	·103	·104	·106	·107	·109	·110	·111	·113	·114	·116	·117	·118
83	·085	·087	·088	·089	·090	·091	·093	·094	·095	·096	·097	·099	·100	·101	·102	·104
84	·073	·074	·075	·076	·077	·078	·079	·080	·082	·083	·0 ⁸ 4	·085	·086	·087	·088	·089
85	·061	·062	·063	·064	·064	·065	·066	·067	·068	·069	·070	·071	·071	·072	·073	·074
86	·049	·050	·050	·051	·052	·052	·053	·054	·054	·055	·056	·057	·057	·058	·059	·059
87	·037	·037	·038	·038	·039	·039	·040	·040	·041	·041	·042	·042	·043	·043	·044	·044
88	·024	·025	·025	·025	·026	·026	·027	·027	·027	·028	·028	·028	·029	·029	·029	·030
89	·012	·012	·013	·013	·013	·013	·013	·013	·014	·014	·014	·014	·014	·014	·015	·015
Lat.				D	IFFE	RENC	EO	F LC	ONGI	TUDI	E.					
	•85	•86	•87	[~] 88	•89	•90	•91	•92	•93	•94	•95	•96	•97	•98	•99	1.00
65	·359	·363	·368	·372	·376	·380	·385	·389	·393	·397	·401	·406	·410	·414	·418	·423
66	·346	·350	·354	·358	·362	·366	·370	·374	·378	·382	·386	·390	·395	·399	·403	·407
67	·332	·336	·340	·344	·348	·352	·356	·359	·363	·367	·371	·375	·379	·383	·387	·391
68	·318	·322	·326	·330	·333	·337	·341	·345	·348	·352	·356	·360	·363	·367	·371	·375
69	·305	·308	·312	·315	·319	·323	·326	·330	·333	·337	·340	·344	·348	·351	·355	·358
70	·291	·294	·298	·301	·304	·308	·311	·315	·318	·321	·325	·328	·332	·335	·339	·342
71	·277	·280	·283	·287	·290	·293	·296	·300	·303	·306	·309	·313	·316	·319	·322	·326
72	·263	·266	·269	·272	·275	·278	·281	·284	·287	·290	·294	·297	·300	·303	·306	·309
73	·249	·251	·254	·257	·260	·263	·266	·269	·272	·275	·278	·281	·284	·287	·289	·292
74	·234	·237	·240	·243	·245	·248	·251	·254	·256	·259	·262	·265	·267	·270	·273	·276
75	·220	·223	·225	·228	·230	·233	·236	·238	·241	·243	·246	·248	·251	·254	·256	·259
76	·206	·208	·210	·213	·215	·218	·220	·223	·225	·227	·230	·232	·235	·237	·240	·242
77	·191	·193	·196	·198	·200	·202	·205	·207	·209	·211	·214	·216	·218	·220	·223	·225
78	·177	·179	·181	·183	·185	·187	·189	·191	·193	·195	·198	·200	·202	·204	·206	·208
79	·162	·164	·166	·168	·170	·172	·174	·176	·177	·179	·181	·183	·185	·187	·189	·191
80	·148	·149	·151	·153	·155	·156	·158	·160	·161	·163	·165	·167	·168	·170	·172	·174
81	·133	·135	·136	·138	·139	·141	·142	·144	·145	·147	·149	·150	·152	·153	·155	·156
82	·118	·120	·121	·122	·124	·125	·127	·128	·129	·131	·132	·134	·135	·136	·138	·139
83	·104	·105	·106	·107	·108	·110	·111	·112	·113	·115	·116	·117	·118	·119	·121	·122
84	·089	·090	·091	·092	·093	·094	·095	·096	·097	·098	·099	·100	·101	·102	·103	·105
85 86 87 88	·074 ·059 ·044	·075 ·060 ·045	·076 ·061 ·046	•077 •061 •046	∙078 ∙062 ∙047	·078 ·063 ·047	∙079 ∙063 ∙048	∙080 ∙064 ∙048	·081 ·065 ·049	•082 •066 •049	∙083 ∙066 ∙050	∙084 ∙067 ∙050	·085 ·068 ·051	∙085 ∙068 ∙051	·086 ·069 ·052	·087 ·070 ·052

SHOWING DIFFERENCE OF LONGITUDE AND CORRESPONDING DEPARTURE.

at.				DI	FFER	ENCE	OF	LON	GIT	UDE.						
Ľ	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07	1·0 8	1.09	1.10	1•11	1.12	1.13	1.14	1•15
65 66 67 68 69	·423 ·407 ·391 ·375 ·358	·427 ·411 ·395 ·378 ·362	·431 ·415 ·399 ·382 ·366	·435 ·419 ·402 ·386 ·369	·440 ·423 ·406 ·390 ·373	·444 ·427 ·410 ·393 ·376	·448 ·431 ·414 ·397 ·380	·452 ·435 ·418 ·401 ·383	·456 ·439 ·422 ·405 ·387	·461 ·443 ·426 ·408 ·391	·465 ·447 ·430 ·412 ·394	·469 ·451 ·434 ·416 ·398	·473 ·456 ·438 ·420 ·401	·478 ·460 ·442 ·423 ·405	•482 •464 •445 •427 •409	·486 ·468 ·449 ·431 ·412
70 71 72 73 74	·342 ·326 ·309 ·292 ·276	·345 ·329 ·312 ·295 ·278	·349 ·332 ·315 ·298 ·281	·352 ·335 ·318 ·301 ·284	·356 ·339 ·321 ·304 ·287	·359 ·342 ·324 ·307 ·289	·363 ·345 ·328 ·310 ·292	·366 ·348 ·331 ·313 ·295	·369 ·352 ·334 ·316 ·298	·373 ·355 ·337 ·319 ·300	·376 ·358 ·340 ·322 ·303	·380 ·361 ·343 ·325 ·306	·383 ·365 ·346 ·327 ·309	·386 ·368 ·349 ·330 ·311	·390 ·371 ·352 ·333 ·314	·393 ·374 ·355 ·336 ·317
75 76 77 78 79	·259 ·242 ·225 ·208 ·191	·261 ·244 ·227 ·210 ·193	·264 ·247 ·229 ·212 ·195	·267 ·249 ·232 ·214 ·197	·269 ·252 ·234 ·216 ·198	·272 ·254 ·236 ·218 ·200	·274 ·256 ·238 ·220 ·202	·277 ·259 ·241 ·222 ·204	·280 ·261 ·243 ·225 ·206	·282 ·264 ·245 ·227 ·208	·285 ·266 ·247 ·229 ·210	·287 ·269 ·250 ·231 ·212	·290 ·271 ·252 ·233 ·214	·292 ·273 ·254 ·235 ·216	·295 ·276 ·256 ·237 ·218	·298 ·278 ·259 ·239 ·219
80 81 82 83 84	·174 ·156 ·139 ·122 ·105	·175 ·158 ·141 ·123 ·106	·177 ·160 ·142 ·124 ·107	·179 ·161 ·143 ·126 ·108	·181 ·163 ·145 ·127 ·109	•182 •164 •146 •128 •128	•184 •166 •148 •129 •111	·186 ·167 ·149 ·130 ·112	·188 ·169 ·150 ·132 ·132	·189 ·171 ·152 ·133 ·114	·191 ·172 ·153 ·134 ·115	·193 ·174 ·154 ·135 ·116	·194 ·175 ·156 ·136 ·117	·196 ·177 ·157 ·138 ·118	·198 ·178 ·159 ·139 ·139	·200 ·180 ·160 ·140 ·120
85 86 87 88 89	·087 ·070 ·052 ·035 ·017	·088 ·070 ·053 ·035 ·018	·089 ·071 ·053 ·036 ·018	·090 ·072 ·054 ·036 ·018	·091 ·073 ·054 ·036 ·018	·092 ·073 ·055 ·037 ·018	·092 ·074 ·055 ·037 ·018	·093 ·075 ·056 ·037 ·019	·094 ·075 ·057 ·038 ·019	·095 ·076 ·057 ·038 ·019	·096 ·077 ·058 ·038 ·019	·097 ·077 ·058 ·039 ·019	·098 ·078 ·059 ·039 ·020	·098 ·079 ·059 ·039 ·020	·099 ·080 ·060 ·040 ·020	·100 ·080 ·060 ·040 ·020
at.				D	IFFEI	RENC	e oi	r LO	NGI	TUDE						
	•	1			1		1									
	1.15	1•16	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1•30
r 65 66 67 68 69	1.15 .486 .468 .449 .431 .412	1.16 .490 .472 .453 .435 .416	1·17 ·494 ·476 ·457 ·438 ·419	1.18 .499 .480 .461 .442 .423	1.19 .503 .484 .465 .446 .426	1.20 .507 .488 .469 .450 .430	1·21 ·492 ·473 ·453 ·434	1·22 ·516 ·496 ·477 ·457 ·437	1·23 ·520 ·500 ·481 ·461 ·441	1.24 .524 .504 .485 .465 .444	1.25 .528 .508 .488 .468 .468	1·26 3 ·532 3 ·512 3 ·492 3 ·472 3 ·472	•537 •517 •496 •476	•541 •521 •500 •479 •459	1•29 •545 •525 •504 •483 •462	1.30 .549 .529 .508 .487 .466
65 66 67 68 69 70 71 72 73 74	1.15 .486 .468 .449 .431 .412 .393 .372 .355 .336 .317	1-16 -490 -472 -453 -435 -416 -397 -378 -339 -326	1.17 .494 .476 .457 .438 .419 .400 .381 .362 .342 .322	1.18 .499 .480 .461 .442 .423 .424 .384 .365 .345 .325	1.19 .503 .484 .465 .446 .426 .426 .407 .387 .368 .348 .328	1·20 ·507 ·488 ·469 ·450 ·430 ·410 ·391 ·371 ·351 ·331	1.21 .492 .473 .453 .434 .434 .394 .354 .354 .334	1.22 .516 .496 .477 .457 .437 .437 .437 .397 .357 .357	1.23 ·520 ·500 ·481 ·461 ·441 ·421 ·421 ·400 ·380 ·380 ·360	1.24 .524 .504 .485 .444 .444 .424 .404 .383 .363 .342	1.25 .528 .508 .468 .448 .448 .448 .448 .448 .447 .386 .365 .345	1·26 3 ·532 3 ·512 3 ·492 3 ·472 3 ·572 3 ·572 3 ·472 3 ·472	1.27 .537 .517 .496 .476 .455 .434 .413 .392 .371 .350	1.28 .541 .521 .500 .479 .459 .438 .417 .396 .374 .353	1·29 ·545 ·525 ·504 ·483 ·462 ·441 ·420 ·399 ·377 ·356	1:30 :549 :529 :508 :487 :466 :445 :423 :402 :380 :358
65 66 67 68 69 70 71 72 73 74 75 76 77 78 79	1.15 .486 .468 .449 .431 .412 .393 .372 .336 .337 .336 .317 .228 .228 .228 .239 .219	1.16 . 4900 . 4722 . 4533 . 4355 . 416 . 3377 . 3358 . 33588 . 33588 . 33588 . 33588 . 335	1.17 .494 .476 .457 .438 .419 .362 .342 .322 .323 .283 .263 .243 .223	1.18 .4999 .480 .461 .442 .442 .442 .384 .384 .384 .385 .325 .285 .285 .265 .245 .225	1.19 .503 .484 .465 .446 .426 .407 .387 .368 .348 .328 .328 .308 .288 .268 .247 .227	1.20 .507 .488 .460 .450 .430 .410 .371 .351 .331 .311 .290 .270 .249 .229	1-21 	1.222 -516 -496 -477 -457 -437 -377 -377 -357 -357 -356 -295 -274 -254 -254 -254	1-23 -52C -50C -481 -461 -441 -421 -421 -386 -386 -386 -339 -318 -298 -277 -256 -235	1.24 .524 .504 .485 .445 .444 .424 .404 .383 .363 .342 .300 .279 .258 .237	1.25 .528 .508 .488 .468 .448 .448 .448 .448 .428 .365 .345 .345 .345 .322 .302 .281 .266 .239	1-26 - 532 - 532 - 542 - 492 - 431 - 431 - 432 - 389 - 368 - 347 - 389 - 368 - 368 - 368 - 368 - 368 - 262 - 240 - 2400 - 2400 - 2400 - 2400 - 2400 - 2400 - 24	1-27 -537 -517 -496 -476 -4455 -434 -413 -392 -371 -350 -329 -307 -286 -264 -242	1-28 -541 -521 -500 -479 -459 -438 -417 -396 -374 -3310 -288 -266 -244	1-29 -545 -525 -504 -483 -462 -441 -420 -399 -377 -356 -334 -312 -268 -246	1:30 :549 :529 :529 :466 :445 :445 :423 :402 :380 :358 :336 :314 :292 :270 :248
r 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84	1.15 .486 .468 .449 .412 .393 .372 .355 .336 .298 .226 .239 .226 .239 .219 .200 .186 .144 .120	1-16 - 4900 - 4722 - 4533 - 4355 - 3166 - 3397 - 326 - 3385 - 3385 - 3385 - 3395 - 326 - 3395 - 326 - 3395 - 326 - 3395 - 326 - 221 - 22	1-17 -494 -476 -457 -438 -457 -438 -457 -438 -362 -342 -243 -243 -243 -243 -243 -243 -163 -143 -122	1.18 .499 .480 .461 .442 .423 .404 .384 .365 .325 .325 .245 .225 .245 .225 .185 .164 .144 .123	1.19 .503 .484 .465 .446 .426 .426 .407 .387 .368 .328 .328 .328 .238 .238 .247 .227 .186 .166 .145 .124	1.20 .507 .488 .469 .450 .430 .311 .331 .311 .290 .249 .249 .249 .249 .249 .249 .249 .188 .169 .146	1.21 .492 .473 .453 .434 .354 .374 .354 .374 .354 .293 .272 .252 .223 .225 .223 .225 .223 .216 .142 .126	1-22 -516 -496 -497 -477 -457 -457 -337 -337 -337 -337 -337 -337 -337 -3	1-23 -52cc -50cc -50cc -30c -332 -335 -335 -335 -335 -335 -256 -277 -256 -277 -256 -277 -256 -277 -256 -277 -256 -277 -256 -277 -256 -277 -256 -277 -256 -275 -275 -275 -275 -275 -275 -275 -275	1·24 · 524 · 504 · 485 · 465 · 444 · 424 · 404 · 383 · 363 · 342 · 321 · 300 · 279 · 258 · 237 · 215 · 194 · 173 · 151 · 130	1.25 .528 .508 .488 .448 .448 .448 .448 .448 .365 .345 .345 .345 .322 .302 .281 .266 .236 .217 .196 .172 .151 .131	1+26 -532 -512 -472 -472 -452 -452 -368 -368 -368 -368 -368 -368 -368 -368 -368 -368 -368 -369 -262 -272 -212 -175 -1754 -132	1·27 ·537 ·496 ·476 ·455 ·434 ·392 ·371 ·350 ·329 ·377 ·350 ·329 ·377 ·350 ·286 ·264 ·242 ·271 ·199 ·177 ·1555 ·133	1-28 -541 -521 -500 -479 -438 -417 -396 -374 -353 -3311 -310 -244 -222 -200 -178 -156 -134	1·29 ·545 ·525 ·504 ·441 ·420 ·377 ·356 ·334 ·246 ·224 ·2224 ·202 ·180 ·157 ·135	1:30 549 529 508 487 445 445 380 336 336 336 336 334 292 270 248 226 203 181 158 136

68	
Table	C1.

A & B	Az.	A & B	Az.	А & В	Az.	A & B	Az.	A & B	Az.	A & B	Az.	A & B	Az.
·000	90°0	·112	8 [°] 3·6	·227	$\overset{\circ}{77\cdot 2}$	·348	$\overset{\circ}{70.8}$	•479	6°4·4	.627	57.9	.798	5 ^{1.} 4
•002	89.9	·114	•5	•229	· I	•350	•7	•481	.3	•630	.8	·801	• 3
1003	•0	.110		.231	77.0	.352	2015	.403	•2	.632	.7	.804	•2
.007	.6	.110	•2	~33 ·235	.8	.356	.4	.488	64.0	.637	57.5	.810	51.0
.009	89.5	.121	$\cdot \mathbf{I}$	·236	.7	·358	• 3	·490	63.9	.640	•4	·813	50.9
·010	•4	·123	83.0	·238	•6	·360	·2	492	.8	.642	•3	·816	.8
·012	• 3	·125	82.9	·240	76.5	·362	٠I	•494	.7	·644	$\cdot 2$	·818	.7
·014	•2	·126	.8	•242	•4	•364	70.0	•496	•6	•647	٠ı	·821	.6
.010	·1 80.0	·128	.7	*244	• 3	.300	-09-9	•499	03.5	.652	57.0	·824	50.5
.010	88.0	.130	82.5	.248	· 1	+300	.7	.503	• 4	-654	-50.9	.830	·4
·021	.8	·I33	•4	·249	76.0	.372	-6	.505	•2	.657	.7	.833	-2
·023	•7	·135	•3	·251	75·9	•374	69.5	.507	٠ı	.659	·6	·836	50·1
·024	•6	·137	·2	·253	·8	·376	•4	.210	63.0	·662	56.5	·839	50.0
•026	88.5	·139	•1	·255	•7	·378	•3	.215	6 2·9	•664	•4	·842	49.9
.028	'4	•141	82.0	·257	.0	·380	-2	.514	.8	·007	.3	.845	•8
.030	.3	142	.8	.259	75.5	+281	60.0	-510	.6	.672	.2	-040 -851	.6
.033	• I	·144	.7	·262	+	·386	68.9	.521	62.5	.674	56.0	.854	49.5
·035	88.0	·148	-6	·264	·2	·388	· 8	·523	•4	.677	55.9	.857	•4
·037	87.9	•149	81.5	·266	٠ı	.390	•7	·525	•3	·680	.8	·860	•3
·038	·8	·151	.4	·268	75.0	·392	•6	•527	•2	·682	.7	·863	·2
•040	•7	· 15 3	• 3	·270	74.8	•394	68.5	.530	• I	•685	·6	·866	٠I
.042	·0 87.7	155	•2	·272	•8	-390	*4	·532	61.0	.600	55.5	·809	49.0
-044	0/.5	.150	81.0	-275	.6	-390	.3	534	.8	-602	.4	.875	40.9
.047		·160	80.0	~73 ·277	74.5	.402	·ī	.538	•7	.695	•2	.878	.7
.049	·2	·162	.8	·279	•4	·404	68·0	·541	.6	·698	· 1	·882	·6
·051	٠I	-164	•7	·281	.3	·406	67 ·9	.543	61.5	.700	55.0	·885	48.5
.052	87.0	166	6	·283	•2	·408	·8	·545	•4	•703	54.9	·888	•4
·054	86.9	•167	80.5	·285	· I	.410	.7	•547	• 3	•705	.8	·891	.3
1050	·0	.109	.4	.287	72.0	·412	67.5	.550	•2	.708	.6	·807	.2
.059	•6	•173	.2 .2	·209	.8	·416	•7.5	.554	61.0	.713	54.5	.900	48.0
·061	86.5	$\cdot 175$	٠I	·292	•7	·418	• 3	.557	60 ·9	.716	•4	·904	47.9
·063	•4	·176	80.0	·294	٠Ġ	·420	• 2	·559	·8	.719	•3	•907	.8
.065	•3	·178	79.9	·296	73.5	•422	•1	.561	.7	.721	•2	·910	.7
·000	•2	.180	.8	·298	•4	.424	66.0	•503	•0	.724	· I	·913	.0
-070	86.0	·102	.7	.300	.3	427	-8	.500	00.5	.720	54.0	-010	47.5
·072	85.9	.185	79.5	-304	. ĩ	·43I	.7	.570	-3	.732		•923	.3
·073	.8	.187	•4	·306	73.0	•433	·6	.573	·2	·735	.7	·926	•2
.075	•7	189	.3	·308	72.9	•435	66.5	·575	٠ı	.737	•6	·929	٠ı
·077	•6	.191	·2	.310	·8	•437	•4	•577	60·0	•740	53.5	·932	47.0
•079	85.2	·193	٠I	.311	.7	•439	• 3	.580	59.9	•743	•4	•936	40.9
.082	·4	.194	79.0	-313	·0 72.5	•441	·2	.502	·0	.745	.3	.939	•0
·084	.2 ·2	190	.8	-313	·- 5	445	66.0	.587	.6	.751	• I	·942	.6
·086	٠ı	.200	.7	.319	•3	.447	65.9	.589	59.5	.754	53.0	·949	46.5
·087	85.0	·202	•6	.321	·2	•449	.8	.591	•4	.756	52.9	·952	•4
·089	84.9	·203	•5	·323	٠ı	·452	•7	·594	•3	·759	·8	·956	•3
.031	•8	.205	.4	.325	72.0	•454	•6	·596	•2	·762	.7	·959	•2
.093	.7	+207	-3	.327	71.9	*450	05.5	·598	1.	.705	·0 = 2 · 5	·902	16.0
2006	84.5	-209	-T	-329	.7	450	+	.603	59.0	.770	54.2	-060	15.0
.098	-4	·213	78.0	•333	.6	.462	.2	.606	.8	.773	•3	.972	.8
·100	•3	.214	77.9	.335	71.5	464	·1	.608	•7	·776	•2	·976	.7
·102	$\cdot 2$	·216	·8	·336	•4	•466	65.0	.610	·6	.778	·I	·979	·6
.103	·I	·218	.7	.338	•3	.468	64.9	.613	58.5	.781	52.0	.983	45.5
.105	82.0	·220	.0	·340	2	·471	.7	-618	·4	.704	51.9	-900	.4
.100	-3.9	.224	11.2	-344 -344	71.0	413	.6	.620	.2	.790	.7	.993	.2
:110	•7	·225	·3	·346	70.9	.477	64.5	.622	·I	.793	•6	·996	٠I
·I12	·6	·227	•2	·348	.8	.479	•4	.625	58.0	.795	51.2	1.000	45.0
			1										1

Table C'.

A & B	3	Az.	A & 1	В	Az.	A & B		Az.	A & I	3	Az.	A & 1	3	Az.	A&I	3	Az.	A & E	3	Az.
	0	,	1.029	0	1	1	0	1		0	,	1.10	0	,		0	- ,		00	,
1.000	45	50	1.030	43	55	1.078	42	51	1.120	41	47	1.102	40	43	1.207	39	39	1.253	38	35
1.001	44	58	1.010		53	1.079	44	10	1.120	41	40	1.103		42	1.207		30	1.254		34
1.002		57	1.040		52	1.080		48	1.121	4.4	44	1.164	40	10	1.200		- 36	1.256		33
1.002		56	1.041		51	1.080		47	1.122		43	1.165	T	39	1.209	39	35	1.256		31
1.003	44	55	1.045	-43	50	1.081		46	I·122		42	1.165		38	1.310		34	1.257	38	30
1.003		54	1.042		49	1.082	42	45	1.153	_	41	1.166		37	1.211		-33	1.258		29
1.004		53	1.043		40	1.082		44	1.124	41	- 40	1.107		30	1.212		32	1.259		28
1.005		51	1.043		47	1.081		43	1.124		- 39	1.168	40	35	1.212	20	31	1.259		26
1.000	44	50	1.045	43	45	1.084		41	1.126		37	1.169		-33	1.214		29	1.261	38	25
1.006		49	1.045		44	1.085	42	40	1.126		36	1.169		32	1.214		28	1.262	0	24
1.002		48	1.0 46		43	1.086		39	1.127	41	35	1.170		зı	1.215		27	1.262		23
1.008		47	1.040		42	1.080		38	1.128		34	1.171	40	30	1.210		20	1.203		22
1.000	4.4	40	1.047	12	41	1.087		37	1.120		- 33	1.171		29	1.217	39	25	1.204	28	21
1.000	77	44	1.048	43	39	1.088	42	35	1.130		31	1.173		27	1.218		23	1.265	30	10
1.010		43	1.049		38	1.089		34	1.130	41	30	1.174		26	1.219		22	1.266		18
1.010		42	1.049		37	1.089		33	1.131		29	1.174	40	25	1.220		21	1·2 67		17
1.011		41	1.050	. /	36	1.000		32	1.132		28	1.175		24	1.220	39	20	1.268		16
1.012	44	40	1.051	43	35	1.001	12	31	1.132		27	1.176		23	1.221		19	1.208	38	15
1.013		38	1.052		34	1.002	44	20	1.133	41	25	1.177		21	1.222		17	1.209		13
1.013		37	1.053		32	1.093		28	1.134	,	24	1.178	40	20	1.223		16	1.271		12
1.014		36	1.053		31	1.093		27	1.135		23	1.178	·	19	I.224	39	15	1.271		II
1.012	44	35	1.054	43	30	1.001		26	1.136		22	1.179		18	1.5225		14	1.272	38	10
1.015		34	1.054		29	1.004	42	25	1.130		21	1.180		17	1.220		13	1.273		9
1.010		32	1.056		27	1.006		23	1.137	41	10	T-T8T	40	15	1.227		14	1.275		7
1.017		31	1.056		26	1.096		22	1.138		18	1.182	40	14	1.228	39	10	1.275		- 6
1.018	44	30	1.057	43	25	1.092		21	1.139		17	1.183		13	1.228		9	1.276	38	5
1.018		29	1.057		24	1.098	42	20	1.140		16	1.183		I 2	1.229		8	1.277		- 4
1.010		20	1.050		23	1.000		19	1.140	41	15	1.184	10	II	1.230		7	1.278		- 3
1.020		26	1.059		21	1.100		17	1.141		13	1.185	40	9	1.231	39	ī	1.270		Ĩ
1.021	44	25	1.060	43	20	1.100		16	1.142		12	1.186		8	1.232	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	4	1.280	38	0
I.051		24	1.001		19	1.101	42	15	1.143		II	1.187		7	1.233		3	1.281	37	59
1.022		23	1.001		18	1.102		14	1.144	41	10	1.187		6	2.233		2	1.281		58
1.022		24	1.002		-17 -16	1.102		13	1.144		- 9	1.180	40	2	1.234	20	0	1.282		56
1.023	44	20	1.063	43	15	1.103		II	1.146		7	1.100		3	1.236	38	59	1.284	37	55
1.024		19	1.064		14	1.104	42	10	1.146		б	1.190		2	1.236		58	1.285		54
1.025		18	1.064		13	1.102		9	1.147	$4\mathbf{I}$	5	1.101		Ι	1.237		57	1.285		53
1.025		17	1.065		12	1.105		8	1.148		4	1.192	40	-0	1.238	28	50	1.280		52
1.026	4.4	10	1.005	32	10	1.100		6	1.140		5	1.103	39	59 58	1.230	30	55 54	1.288	37	50
1.027	- T *T	14	1.067	40	9	1.107	42	5	1.150		I	1.194		57	1.240		53	1.288	51	49
1.028		13	1.067		8	1.108	·	4	1.120	41	0	1.195		56	1.241		52	1.289		48
1.028		12	1.068		7	1.100		3	1.121	40	59	1.195	39	55	1.241		51	1.290		47
1.029		II	1.000	17	- 0 -	1.109		2	1.152		58 =7	1.190		54	1.242	30	50	1.291	27	40
1.030	44	10	1.070	4.5	3 4	I-III	12	- 0	1.122		56	1.107		52	- ~43 I·244		48	1.292	57	44
1.031		8	1.070		3	1.111	41	59	1.154	40	55	1.198		51	1.244		47	1.293		43
1.031		7	1.071		2	1.112	·	58	1.154		54	1.199	39	50	1.245		46	1.294		42
1.032		6	1.072		I	1.113		.57	1.155		53	1.199		49	1.246	38	45	1.295	2.77	41
1.032	44	- 5	1.072	43	0	1.113	4.1	50	1.150		52	1.200		40	1.247		44	1.295	37	30
1.033		4	1.073	42	59	1.114	41	52	1.150	40	50	I·201 I·202		4/	1.247		43	1.297		38
1.034		2	I.074		57	1.115		53	1.158	T	49	I·202	39	45	1.249		41	1.298		37
1.035		I	1.075		56	1.116		52	1.158		48	1.203		44	1.250	38	40	1.298		36
1.035	44	0	1.075	42	55	1.110		51	1.159		47	1.204		43	1.250		39	1.299	37	35
1.030	43	59	1.070		54	1.117	41	50	1.100	10	40	1.204		42	1.222		30	1.300		34
1.037		57	1.077		53 52	1.118		48	1.101	+0	45 44	1.206	39	40	1.253		36	1.302		32
1.038		56	1.078		51	1.119		47	1.162		43	1.207		39	1.253	38	35	1.302		31

Table C¹.

A & B	A	ız.	A & E	3.	Az.	A & E		Az.	A & E	3 .	Az.	A & B	4	١z.	A & B	A	١z.	A & B		Az.
1.303	3°7	30 30	1.355	3Å	25	1.410	3Ŝ	21 21	1.467	°	17	1.527	° 33	í3	1.591	32	, 9	1 .659	3Î	· 5
1.304		29	1.356		24	1.411	35	20	1.468		16	1.528		16	1.592		8	1 .660		4
1.305		20	1.357		23	1.411		19	1.409	34	15	1.529	2.2	11	1.593		7	1.662		3
1.306		26	1.359		21	1.413		17	1.470		13	1.531	55	9	1.595	32	5	1.663		ĩ
1.307	37	25	1.360	36	20	1.414		16	1.471		12	1.532		8	1.596	5	4	1.664	31	0
1.308		24	1.360		19	1.412	35	15	1.472		II	1.533		7	1.202		3	1.665	30	59
1.309		23	1.361		18	1.410		14	I·473	34	10	1.534		6	1.598		2	1.668		58
1.309		21	1.302		17	1.417		13	1.474		- 9	1.535	33	5	1.599	22	1	1.009		57
1.311	37	20	1.364	36	15	1.418		II	1.476		7	1.537		3	1.601	31	59	1.670	30	55
1.312	01	19	1.365	5	14	1.419	35	10	I·477		6	1.538		2	1.602	.,	58	1.671	5	54
1.313		18	1.365		13	1.420		9	1 ·478	34	5	1.539		I	1.603		57	1.672		53
1.313		17	1.360		12	1.421		8	I·479		4	1.540	33	0	1.604	2.1	50	1.673		52
1.314	37	15	1.307	36	10	1.422		6	1.480		3	1.541	32	59 58	1.607	31	53 54	1.675	30	50
1.316	57	14	1.369	50	9	1.424	35	5	1.482		ī	1.543		57	1.608		53	1.676	50	49
1.317		13	1.370		8	1.425		4	1.483	34	0	1.544		56	1.609		52	1.677		48
1.312		12	1·370		7	1.425		3	1 ·483	33	59	1.242	32	55	1.010		51	1.679		47
1.318	27	11	1.371	26	6	1.420		2	1.484		58	1.540		54	1.611	31	50	1.681	20	46
1.320	37	01	1.372	30) - 1	1.427	35	0	1.485	•	57	1.547		53 52	1.613		49	1.682	30	45
1.321		8	- 373 1·374		3	1.429	34	59	1.487	33	55	1.549		51	1.614		47	1 .683		43
1.321		7	1.375		2	1.430	• .	58	1.488		54	1.550	32	50	1.615		46	1 .684		42
1.322		6	I·375	~	I	1.431		57	1.489		53	1.221		49	1.616	31	45	1.685		4 I
1.323	37	5	1.376	36	0	1.432	2.4	56	1.490		52	1.552		48	1.617		44	1.687	30	40
1.324		4	1.377	35	59	1.433 1.433	34	55	1.491	22	50	1.222		47	1.610		43	1.680		- <u>39</u> - 38
1.325		2	1.379		57	I·434		53	1.493	55	49	I.555	32	45	1.620		41	1.690		37
1.326		I	1.380		56	1.435		52	1.494		48	1.556		44	1.621	31	40	1.691		36
1.327	37	0	1.381	35	55	1 ·436		51	I·495		47	1.557		43	1.622		39	1.692	30	35
1.328	30	59 = 8	1.381		54	1.437	34	50	1.490	2.2	40	1.558		42	1.623		38	1.604		34
1.329		57	1.382		52	1.430		49	1.497	33	40	1·560	32	41	1.625		36	1.605		33
1.330		56	1.384		51	I·440		47	1.498		43	1.561	J-	39	1.626	31	35	1.696		31
1.331	36	55	1.385	35	50	1.441		46	1·499		42	1.562		38	1.628		34	1 .698	30	30
1.332		54	1.386		49	1.441	34	45	1.200		4 I	1.563		37	1.629		33	1.699		29
1.333		53	1.386		48	1.442		44	1.501	33	40	1.564	22	30	1.630		32	1.700		28
1.334		51	1.387		47	1·443		43	1.503		- 39 - 38	1.566	34	33	1.632	31	30	1.702		26
1.335	36	50	1.389	35	45	1.445		41	1.504		37	1.567		33	1.633	5	29	1.703	30	25
1.336		49	1.390		44	1.446	34	40	1.202		36	1 ·568		32	1 .634		28	1.704		24
I·337		48	1.301		43	1·447		39	1.206	- 33	35	1 ·569		31	1.635		27	1.706		23
1.337		47	1.392		42	1.448		38	1.507		34	1.570	32	30	1.630	21	20	1.707		22
1.330	36	40	1.392	35	41	1 449 1·450		- 37	1.500		33	1.572		28	1.638	51	24	1.709	30	20
1.340	5-	44	I ·394	55	39	1.450	34	35	1.210		31	1 ·573		27	1.639		23	1.710	5	19
1.341		43	1.395		38	1.451		34	1.211	33	30	I ·574		26	1 .640		22	1.711		18
1.342		42	1.396		37	1.425		33	1.212		29	1.575	32	25	1.641	- T	21	1.712		17
1.342	26	41	1.397	25	30	1.453		32	1.513		28	1.570		24	1.643	31	20	1.714	20	10
1.343	30	30	1.308	33	30	1.454	34	30	1.515		26	1.578		22	1.645		18	1.716	50	14
1.345		38	1.399		33	1.456	54	29	1.516	33	25	1.579		21	1 .646		17	1.717		13
1.34 6		37	1.400		32	1.457		28	1.517	00	24	1.580	32	20	1 .647		16	1.718		12
1.346		36	1.401		31	1.428		27	1.212		23	1.581		19	1.648	31	15	1.719		II
1.347	30	35	1.402	35	30	1.459	2.4	20	1.518		22	1.582		10	1.049		14	1.720	30	10
1.340		34	1.403		28	1.400	34	3 - 24	1.520	33	20	1.584		16	1.651		12	1.723		8
1.350		32	1.404		27	1.461		23	1.521		19	1.585	32	15	1.652		II	1.724		7
1.351		31	1.405		26	1.462		22	1.522		18	1.586		14	1.653	31	10	1.725		6
1.351	36	30	1.406	35	25	1.463		21	1.523		17	1.282		13	1.654		9	1.726	30	5
1.352		29	1.407		24	1.404	34	20	1.524		10 	1.500		12	1.055		0 7	1.727		4
1.354		27	1.400		43 22	1·405		18	1.526	33	10	1.590	32	10	1.658		6	1.730		2
1.355		26	1.410		21	1.467		17	1.527		13	1.591	5	9	1.659	31	5	1.731		I
															1			1		

Table C¹.

Azimuth Corresponding to A and B Correction in Departure.

A&B		Az.	A & B		Az.	A & B		Az.	A & E	; _	Az.	A & B	. 1	Az.	A & B	A	Az.	A&B		Az.
1.732	3°	, 0	1.810	2 [°] 8	55	1 .893	27	5 ^{́1}	1 .981	2°6	47	2.076	2°5	43	2·179	° 24	3 ['] 9	2·291	23°	35
1.733	29	59	1.811		54	1.894	27	50	1.982	_	46	2.078		42	2.181		38	2.293		34
1.734		50	1.813		53	1.895		49	1.984	26	45	2.079		4I	2.182		37	2.294		33
1.730		57 56	1.814		5- 5 T	1.808		40	1.905		44	2.082	20	20	2.186	24	30	2.290		32
1.738	29	55	1.816	28	50	1.899		46	1.088		43	2.084		39	2.188	~+	34	2.300	23	30
1.739	-	54	1.818		49	1.901	27	45	1.990		41	2.086		37	2.189		33	2:302	5	29
1 .740		53	1.819		48	1.902		44	1.991	26	40	2.087		36	2.191		32	2.303		28
1.741		52	1.820		47	1.903		43	1.993		39	2.089	25	35	2.193		31	2.305		27
1.743	20	51	1.822	28	40	1.905		44	1.994		30	2.090		34	2.194	24	30	2.307	22	20
1.745	49	49	1.824	20	43	1.900	27	41	I 995		36	2.092		32	2.190		28	2.311	40	21
1.746		48	1.825		43	1.909	- /	39	1.998	26	35	2.095		31	2.199		27	2.313		23
1.747		47	1.826		42	1.910		38	2.000		34	2.096	25	30	2.201		26	2.315		22
1.748		46	1.828	~	4 I	1.911		37	2.001		33	2.098		29	2.203	24	25	2.316		21
1.750	29	45	1.829	28	40	1.913		36	2.003		32	2.100		28	2.204		24	2.318	23	20
1.751		44	1.822		39	1.914	27	35	2.004	26	31	2.101		27	2.200		23	2.320		19 18
1.753		43	1.833		37	1.017		34	2.007	20	20	2.103	25	25	2.210		21	2.324		17
1.754		41	1.834		36	1.918		32	2.009		28	2.106	~5	24	2.211	24	20	2.326		16
1.756	29	40	1.835	28	35	1.920		31	2.010		27	2.108		23	2.213		19	2.328	23	15
1.757		39	1.837		34	1.921	27	30	2.011		26	2.109		22	2.215		18	2.329		1 4
1.758		38	1.838		33	1.922		29	2.013	26	25	2.111		21	2.216		17	2.331		13
1.759		37	1.8.0		32	1.924		28	2.014		24	2.112	25	20	2.218	21	10	2.333		12
1.761	20	30	1.840	28	31	1.925		27	2.017		23	2.114		19	2.222	44	13	2.335	23	IO
1.763	-9	34	1.843	40	29	1.928	27	25	2.017		21	2.113		17	2.223		13	2.339	-5	9
1.764		33	1.844		28	1.929	- /	24	2.020	26	20	2.119		16	2.225		12	2.341		8
1.765		32	1.846		27	1.931		23	2.022		19	2.120	25	15	2.227		II	2.343		7
1.766		31	1.847	-	26	1.932		22	2.023		18	2.132		14	2.229	24	10	2.344		6
1.767	29	30	1.848	28	25	1.933		21	2.025		17	2.123		13	2.230		9	2.340	23	5
1.709		29	1.049		24	1.935	27	20	2.020	26	10	2.125		12	2.232		7	2.340		4
1.771		27	1.852		22	1.037		18	2.020	40	13	2.127	25	10	2.235		6	2.352		2
1.772		26	1.853		21	1.939		17	2.031		13	2.130	-5	9	2.237	24	5	2.354		I
1.773	29	25	1.855	28	20	1.940		ıб	2.032		12	2.131		8	2.239		4	2.356	23	0
1.775		24	1.856		19	1.945	27	15	2.034	_	II	2 ·133		7	2.241		3	2.358	22	59
1.776		23	1.857		18	1.943		14	2.035	26	10	2.135	~ ~	6	2.242		2	2.300		50
1.777		22	1.860		17	1.944		13	2.037		- 9	2.130	25	5	2.244	24	0	2.302		56
1.780	20	20	1.861	28	15	1.940		11	2.030		7	2.130		4	2.248	23	59	2.365	22	55
1.781	~)	19	1.862		14	1.949	27	10	2.041	•	6	2.141		2	2.250	5	58	2.367		54
1.782		18	1·864		13	1.950		9	2.043	26	5	2.143		I	2.221		57	2.369		53
1.783		17	1.865		12	1.921		8	2.044		4	2·1 44	25	0	2.253		56	2.371		52
1.784		16	1.800	- 0	II	1.953		7	2.046		3	2.140	24	59	2.255	23	55	2.373	22	51
1.787	29	15	1.860	20	10	1.954	27	5	2.047		2	2.140		50	2.258		53	2.375		40
1.788		13	1.870		8	1.957	~/	3	2.050	26	ō	2.149		56	2.260		52	2.379		48
1.789		12	1.871		7	1.958		3	2.052	25	59	2.153	24	55	2.262		51	2.381		47
1.790		II	1.873		6	1.960		2	2.053		58	2.154		54	2.264	23	50	2.383		46
1.792	29	10	1.874	28	5	1.961		1	2.055		57	2.156		53	2.265		49	2.385	22	45
1 .793		9	1.875		4	1.963	27	0	2.050		50	2.158		52	2.207		40	2.307		44
1.794		8	1.877		3	1.964	20	59	2.058	25	55	2.159	24	51	2.209		47	2.309		43
1.795		6	1.870		- T	1.067		57	2.059		53	2.101	-4	49	2.273	23	45	2.392		41
1.798	29	5	1.881	28	ō	1.968		56	2.062		52	2.164		48	2.274	0	44	2.394	22	40
1.799	-	4	1.882	27	59	1.970	26	55	2.064		51	2.166		47	2.276		43	2.396		39
1.800		3	1.883		58	1.971		54	2.065	25	50	2.167		46	2.278		42	2.398		38
1.802		2	1.885		57	1.972		53	2.067		49	2.169	24	45	2.280	22	41	2.400		37
1.803	20	I	1.887	27	50	1.974		52	2.009		40	2.171		44	2.283	~ j	39	2.404	22	35
1.805	28	50	1.880	-1	57 54	1.077	26	50 50	2.072		47 46	2.174		43 42	2.285		38	2.406		34
1.806		58	1.890		53	1.978	20	49	2.073	25	45	2.176		41	2.287		37	2.408		33
1.808		57	1.891		52	1.980		48	2.075	-	44	2.177	24	40	2.290		36	2.410		32
1.809		56	1.893		51	1.981		47	2.076		43	2.179		39	2.291	23	35	2.412		31
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Table C¹.

A & B		Az.	A & 1	3	Az.	A & 1	3	Az.	A & E	5	Az.	А & В		Az.	A & 1	3	Az.	A & E	3 A	٩z.
2.414	22	30	2.549	° 21	25	2.696	20	21	2.858	° 19	· 17	3.038	ı [°] 8	í3	3.240	ı°7	, 9	3.468	ıő	, 5
2.416		29	2.552		24	2.699	20	20	2.861		16	3.041		12	3.244		8	3.472		4
2.418		28	2.554		23	2.701		19	2.864	19	15	3.044		II	3.247		7	3.476		3
2.420		27	2.556		22	2.203		18	2.866		14	3.047	18	10	3.221		6	3.480		2
2.422	~ ~	26	2.558		21	2.706		17	2.869		13	3.020		9	3.254	17	ĩ	3.484	_	1
2.424	22	25	2.500	21	20	2.708	20	10	2.872		12	3.053		0	3.257		4	3.487	10	0
2.428		23	2.565		18	2.713	20	10	2.877	то	10	3.050		6	3.261		3	3.491	15	59
2.430		22	2.567		17	2.715		13	2.880	19	0	3.062	18	5	3.267		ĩ	3.493		57
2.432		21	2.569		16	2.718		12	2.882		8	3.066		4	3.271	17	0	3.203		56
2.434	22	20	2.21	2I	15	2.720		II	2.885		7	3.069		3	3.274	16	59	3.207	15	55
2.436		19	2.574		14	2.723	20	10	2.888		6	3.072		2	3.278		58	3.210		54
2.438		18	2.576		13	2.725		- 9	2.891	19	5	3.075	- 0	I	3.281		57	3.214		53
2.440		17	2.570		12	2.720		0	2.806		4	3.070	10	50	3.204	т6	50	3.518		52
2.444	22	15	2.583	21	10	2.733		- 6	2.800		2	3.081	1/	58	3.201	10	54	3.526	T 5	50
2.446		14	2.585		9	2.735	20	5	2.001		ī	3.087		57	3.295		53	3.530	- 5	19
2.448		13	2.587		8	2.737		4	2.904	19	0	3.090		56	3.298		52	3.534		48
2.420		12	2.589		7	2.740		3	2.907	18	59	3.093	17	55	3.302		51	3.538		47
2.422		II	2.592		6	2.742		2	2.910		58	3 ∙09 6		54	3.302	16	50	3.242		46
2.454	22	10	2.594	21	5	2.745		I	2.912		57	3.099		53	3.309		49	3.546	15	45
2.451		8	2.590		4	2.747	20	50	2.915	т 8	50	3.102		52	3.312		40	3.550		44
2.401		7	2.601		2	2.752	19	59 58	2.021	10	57	3.103	17	50	3.310		47	3 334		43
2.463		6	2.603		1	2.755		57	2.923		53	3.111	- /	49	3.323	16	45	3.562		41
2.465	22	5	2.605	21	0	2.757		56	2.926		52	3.115		48	3.326		44	3.566	15	40
2.467		4	2.607	20	59	2.760	19	55	2.929	-	51	3.118		47	3.330		43	3.220		39
2.469		3	2.610		58	2.762		54	2.932	18	50	3.121		46	3.333		42	3.574		38
2.471		2	2.612		57	2.765		53	2.935		49	3.124	17	45	3.337	+6	41	3.578		37
2.475	22	1	2.614	20	50	2.707		52	2.937		40	3.127		44	3.340	10	40	3.502	75	30
2.477	21	50	2.610	20	53 54	2.773	10	50	2 940		4/	3.133		43	3.344		- 39 - 38	3.500	13	33
2.479		58	2.621		53	2.775	-)	49	2·946	18	45	3.136		41	3.321		37	3.594		33
2.481		57	2.623		52	2.778		48	2.949		44	3.140	17	40	3.354		36	3.598		32
2.483		56	2.626		51	2.780		47	2.951		43	3.143		39	3.328	16	35	3.602		31
2.485	21	55	2.628	20	50	2.783		46	2.954		42	3.146		38	3.362		34	3.606	15	30
2.400		54	2.630		49	2.785	19	45	2.957	T 8	41	3.149		37	3.305		33	3.010		29
2.490		52	2.625		40	2.700		44	2.900	10	20	2.156	17	30	3.309		34	3.614		20
2.494		51	2.637		47	2.793		43	2.965		39	3.159	- /	34	3.375	16	30	3.622		26
2.496	21	50	2.639	20	45	2.795		41	2.969		37	3.162		33	3.379		29	3.626	15	25
2.498		49	2.642		44	2.798	19	40	2.971		36	3.165		32	3.383		28	3.630	-	24
2.200		48	2.644		43	2.801		39	2.974	18	35	3.168		31	3·387		27	3.635		23
2.502		47	2.646		42	2.803		38	2.977		34	3.172	17	30	3.300	- (26	3.639		22
2.504	21	40	2.049	20	41	2.800		37	2.980		33	3.175		29	3.394	10	25	3.043	τ =	21
2.500	41	45 47	2.652	20	30	2.811	10	30	2.086		34	3.170		27	3.201		23	3.651	- 0	ĩo
2.511		43	2.656		38	2.813	+9	34	2.989	18	30	3.184		26	3.405		22	3.655		18
2.513		42	2.658		37	2.816		33	2.992		29	3.188	17	25	3.409		21	3.660		17
2.515		41	2.660		36	2.819		32	2.994		28	3.191		24	3.412	16	20	3.664		16
2.517	21	40	2.663	20	35	2.821		31	2.997		27	3.194		23	3.416		19	3.668	15	15
2.519		39	2.665		34	2.824	19	30	3.000	- 0	26	3.192		22	3.420		18	3.672		14
2.521		30	2.007		33	2.820		29	3.003	18	25	3.201	T /7	21	3.423		17	3.070		13
2.526		36	2.672		34	2.832		20	3.000		23	3.204	17	10	3.44/	16	15	3.685		II
2.528	21	35	2.675	20	30	2.834		26	3.012		22	3.211		18	3.434		14	3.689	15	10
2.530		34	2.677		29	2.837	19	25	3.015		21	3.214		17	3.438		13	3.693	5	9
2.532		33	2.679		28	2.840		24	3.018	18	20	3.217		16	3.442		12	3.698		8
2.534		32	2.682		27	2.842		23	3.021		19	3.220	17	15	3.446	_ /	11	3.702		7
2.530		31	2.684	0.0	26	2.845		22	3.024		18	3.224		14	3.450	10	10	3.706	т-	0
2.541	41	30	2.080	20	25	2.850	10	21	3.027		17	3.227		13	3.453		- 9	3.710	10	2
2.543		28	2.601		-4 23	2.853	19	10	3.030	18	15	3.234		11	3.451		7	3.719		3
2.545		27	2.694		22	2.856		18	3.036		- J I 4	3.237	17	10	3.465		6	3.723		2
2.547		26	2.696		21	2.858		17	3.038		13	3.240	'	9	3.468	16	5	3.728		I
1																				

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Table	C1.

A & 1	В	Az	. A &	в	Az.	A &	в	Az.	Α&	в	Az.	A & 1	В	Az.	A & E	3	Az.	A & B	3	Az.
3.732	I	5 0	4.03(Ì	3 55	4.384	I	251	4.794	ļ I	1 47	5.284	IO	, 43	5.881	ç	39	6.625	8	35
3.730	, 1	4 59	1.04	5	53	4.390		2 50 10	4.80	Зт	40	5.292		42	5.891		38	6.638		34
3.745		57	4.051		52	4.401		48	4.81	·	43 43	5.301	τo	41	5.012		37	0.051		33
3.749		56	4.056	5	51	4.407		47	4.822	2	43	5.318	10	39	5.923	С	30	6.678		32
3.754	I	4 55	4.061	1	3 50	4.413		46	4.829)	42	5.326		-38	5.933	2	34	6.691	8	30
3.758		54	4.066)	49	4.419	12	2 45	4.836)	4 I	5 ·335		37	5.944		33	6.704		29
3.703		53	4.071		40	4.425		44	4.843		[40	5.343		36	5.954		32	6.718		28
3.771		51	4.081		- 46	4.437		43	4.857	,	- 39	5·354	10	35	5.905	0	31	6.731		27
3.776	I	4 50	4.087	I	3 45	4.443		41	4.864		37	5.369		33	5.986	9	20	6.758	8	20
3.780		49	4.092		44	4.449	12	: 40	4.871		36	5.378		32	5.997		28	6.772		24
3.785		48	4.097		43	4.455	12	39	4.879	II	35	5·387		31	6.008		27	6.786		23
3.789		47	4.102		42	4.401		30	4.880		34	5.395	10	30	6.010		26	6.799		22
3.794	I.	40	4.113	I	3 40	4 400		36	4 093		33	5.412		29	6.040	9	25	0.813 6.827	8	21
3.803		44	4.118		39	4.480	12	35	4.908		31	5.422		27	6.051		23	6.841	0	10
3.807		43	4.123		38	4.486		34	4.915	II	30	5.431		26	6.062		22	6.855		18
3.812		42	4.128		37	4.492		33	4.922		29	5.440	10	25	6.073		21	6.869		17
3.821	T.	41	4.133	T	30	4.490		32	4.930		28	5.449		24	.6.084	9	20	6.883	0	16
3.825	14	30	4 - 59	13	34	4 504	12	30	4.937		26	5.457		23	0.095 6.107		19	0.997 6.011	δ	15
3.830		38	4.149		33	4.517		29	4.952	II	25	5.475		21	6.118		17	6.925		13
3.834		37	4.155		32	4.523		28	4.959		24	5.484	10	20	6.129		16	6.939		12
3.839		36	4.160		31	4.529		27	4.967		23	5 [.] 494		19	6.140	9	15	6.954		11
3.044	14	35	4.105	13	30	4.530	1.2	20	4.974		22	5.203		18	6.151		14	6.968	8	10
3.853		34	4 171		28	4 542	14	24	4.982	TT	20	5.521		17	6.174		13	6.007		- 8
3.857		32	4.181		27	4.554		23	4.997		19	5.530	10	15	6.186		11	7.012		7
3.862		31	4.187		26	4.561		22	5.005		18	5.539		14	6.197	9	10	7.026		6
3.867	14	30	4.192	13	25	4.567		21	5.012		17	5.548		13	6.208		- 9	7.041	8	5
3.871		29	4.197		24	4.574	12	20	5.020	тт	10	5.558		12	6.220		8	7.056		4
3.881		27	4 203		22	4 586		18	5.027	11	13	5.576	10	10	6.243		- 6	7.071		3
3.885		26	4.214		21	4.593		17	5.043		13	5.586		9	6.255	9	5	7·100		1
3.890	14	25	4.219	13	20	4.299		16	5.050		12	5.595		8	6.267	-	4	7.115	8	0
3.895		24	4.225		19	4.600	12	15	5.058		II	5.604		7	6.278		3	7.130	7	59
3.004		23	4.230		17	4.012		14	5.000	11	10	5.014	10	0	0·290		- 2 T	7.140		50
3.909		21	4.241		16	4.625		12	5.081		8	5.633	10	4	6.314	9	0	7.176		56
3.914	14	20	4.247	13	15	4.632		11	5.089		7	5.642		3	6.326	8	59	7.191	7	55
3.918		19	4.252		14	4.638	12	10	5.097		6	5.652		2	6.338		58	7.207		54
3.923		18	4.258		13	4.645		2	5.105	II	5	5.662	10	I	6.350		57	7.222		53
3.920		17	4.203		11	4.051		7	5.121		4	5.681	10	50	6.271	8	50	7.252		57
3.937	14	15	4.275	13	10	4.665		6	5.129		2	5.691	9	58	6.386	0	54	7·269	7	50
3.942		14	4.280	0	9	4.671	12	5	5.136		I	5.700		57	6.398		53	7.284	,	49
3.947		13	4.286		8	4.678		4	5.142	II	0	5.710		56	6.410		52	7.300		48
3.952		12	4.292		7	4.085		3	5.153	10	59	5.720	9	55	0.422	8	51	7.310		47
3.957	T-1	10	4.29/	13	5	4·691 4·608		ī	5.101		57	5.730		54 53	6·435	0	<u>30</u>	7.332	7	40
3.967	- 4	9	4.309	*J	4	4.705	12	0	5.177		56	5.749		52	6.460		48	7·364	'	44
3.971		8	4.314		3	4.711	II	59	5.185	10	55	5.759		51	6.472		47	7.380		43
3.976		7	4.320		2	4.718		58	5.193		54	5.769	9 3	50	6.485	0	46	7.396		42
3.981	т.	0	4.320	т э	1	4.725		57	5.201		53	5.779	4	49	0.497	ō	45	7.412	7	41
3.001	14	2	4.331	13 12	59	4.732	11	55	5.217		51	5·799	2	47	6.522		43	7.445	1	39
3.996		3	4.343		58	4.745		54	5.226	10	50	5.809	2	46	6.535		42 7	•461		38
1.001		2	4.349		57	4.752		53	5.234		49	5.820	9 4	45	5.548	0	41 7	^{7.} 478		37
1.000		I	4.355		56	4.759		52	5.242		48	5.830	4	44	5.561	8	40 7	[•] 495	~	30
4.011 1.016	14	50	4.300	12	55	4.700	τī	511	5.250		47	5.820	4	43	5.586		39 7	.528	1	33
1.021	+3	58	4.372		53	+ 113 4·780	**	49	5·267	10	45	5·860	4	41	5.599		37 7	1.545		33
1.026		57	4.378		52	4.787		48	5.275		44	5.871	94	40 0	5.612		36 7	r·562		32
4·031		56	4.384		51	4.794		47	5.284		43	5.881	3	39	5.625	8	35 7	^{7•579}		31
											1			1			1			_

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Table	C1.

Azimuth Corresponding to A and B Correction in Departure.

A&B	Az.	A & B	Az.	A & B	Az.	A & B	Az.	A & B	Az.	A & B	Az.	A & B	Az .
7.60	7 30	8.89	° 25	10.71	° 20	13.4	°4 16	17.9	° / 3 12	26.8	° / 8	53.7	0 / T /
7.61	29	8.92	24	10.75	19	13.5	4 15	18.0	<i>и</i> п	27·I	7	54.6	- 4
7.63	28	8.94	23	10.78	18	13.2	14	18.1	3 10	27.3	6	55.4	2
7.65	27	8.96	22	10.81	17	13.0	13	18.2	9	27.5	2 5	56.4	I
7.00	20	8.99	21	10.85	10	13.0	12	18.3	8	27.7	4	57.3	I O
7.70	7 45	0.02	0 20	10.00	5 15	13.7	4 10	18.5	6	27.9	3	58.3	° 59
7.72	23	0.06	18	10.92	13	13.8	4 10	18.6	3 5	28.1	2 T	59.3	50
7.73	22	9.08	17	10.99	12	13.8	8	18.7	3 3	28.6	2 0	61.4	57
7.75	21	9.11	16	11.02	II	13.9	7	18.8	3	28.9	I 59	62.5	0 55
7.77	7 20	9.13	6 15	11.00	5 IO	14.0	6	18.0	2	29·I	58	63.7	54
7.79	19	9.16	14	11.10	9	14.0	45	19.0	I	29.4	57	64.9	53
7.81	18	9.18	13	11.13	8	14.1	4	19.1	3 0	29.6	56	66·I	52
7.84	17	9.21	12	11.17	7	14.1	3	19.2	2 59	29·9	1 55	69-4	51
7.86	7 15	0.26	6 10	11.24	5 5	14.2	ř	19.5	57	30.1	52	70.2	0 50
7.88	/ -J	9.28	9	11.28	J J 4	14.3	4 0	19.5	56	30.7	52	71.6	49
7.90	13	9.31	8	11.32	3	14.4	3 59	19.6	2 55	31.0	51	73·I	47
7.92	12	9.33	7	11.35	2	14.4	58	19.7	54	31.2	1 50	74.7	46
7.93	II	9.36	6	11.39	I	14.2	57	19.9	53	31.2	49	76.4	0 45
7.95	7 10	9.38	6 5	11.43	5 0	14.5	56	20.0	52	31.8	48	78.1	44
7.97	9	9.41	4	11.47	4 59	14.0	3 55	20.1	51	32.1	47	79.9	43
8.01	7	9.44	3	11.51	57	14.7	53	20.2	2 50	34.4	40 T 45	82.8	42
8.03	. 6	9.49	ī	11.59	56	14.8	52	20.4	49	33.0	- 4J 44	85.0	0 40
8.05	7 5	9.51	6 o	11.62	4 55	14.9	51	20.6	47	33.4	43	88.1	39
8.07	4	9.54	5 59	11.67	54	14.9	3 50	20.7	46	33.7	42	90.5	38
8.09	3	9·57	58	11.71	53	15.0	49	20.8	2 45	34.0	41	92.9	37
8.10	2	9.59	57	11.74	52	15.1	48	20.9	44	34.4	I 40	95.2	36
8.12	I	9.62	50	11.78	51	15.1	47	21.1	43	34.7	39	98.2	° 35
8.16	6 50	0.68	3 55	11.03	4 50	15.2	3 45	21.2	42	35.1	30	101	34
8.18	58	9.00	53	11.01	49	15.3	5 45 44	21.5	2 10	35.8	3/	104	33
8.20	57	9.73	52	11.95	47	15.4	43	21.6		36.2	I 35	111	31
8.22	56	9.76	51	11.99	46	15.5	42	21.7	38	36.6	34	115	0 30
8.24	6 55	9.79	5 50	12.03	4 45	15.2	- 4 I	21.9	37	37.0	33	118	29
8.26	54	9.82	49	12.08	44	15.6	3 40	22.0	36	37.4	32	123	28
8.20	53	9.84	48	12.12	43	15.7	39	22.2	2 35	37.8	31	127	27
8.22	57 51	0.00	47	12.21	44	15.8	30	22.5	34	30.2	1 30	132	0.25
8.34	6 50	9.93	5 45	12.25	1 40	15.9	36	22.6	32	39.0	28	143	24
8.36	49	9.96	44	12.29	39	16.0	3 35	22.8	31	39.5	27	149	23
8.39	48	9.99	43	12.34	38	16· 0	34	22.9	2 30	40.0	26	156	22
8.41	47	10.05	42	12.38	37	16.1	33	23.1	29	40.4	I 25	164	21
8.43	40	10.02	41	12.43	36	16.2	32	23.2	28	40.9	24	172	0 20
0.45	° 45	10.08	5 40	12.47	4 35	10.3	31	23.4	27	41.4	23	181	19
8.40	44	10.12	39	12.57	34	16.4	3 30	23.7	2 25	41.9	21	202	10
8.51	42	10.17	37	12.61	32	16.5	28	23.9	24	43.0	1 20	215	16
8.53	41	10.20	36	12.66	31	16.6	27	24.0	23	43.5	19	229	0 15
8.56	6 40	10.23	5 35	12.71	4 30	16.7	26	24.2	22	44·1	18	246	14
8.58	39	10.26	34	12.75	29	16.7	3 25	24.4	21	44.6	17	264	13
8.60	38	10.29	33	12.80	28	16.8	24	24.5	2 20	45.2	16	286	12
8.64	37	10.32	32	12.85	27	10.9	23	24.7	19	45.8	1 15	313	II
8.66	6 35	10.35	5 30	12.90	4 25	17.1	21	24.9	10	40.4 47.T	14	344	0 10
8.69	- 33	10.42	29	13.00	24	17.2	3 20	25.2	16	47.7	12	430	8
8.71	33	10.45	28	13.05	23	17.3	Ŭ 19	25.5	2 15	48.4	II	491	7
8.73	32	10.48	27	13.10	22	17.3	18	25.6	14	49·I	I 10	573	6
8.75	31	10.21	26	13.12	21	17.4	17	25.8	13	49.8	9	688	0 5
8.80	0 30	10.55	5 25	13.20	4 20	17.5	16	20.0	12	50.5	8	859	4
8.82	29	10.20	24	13.25	19 18	17.7	3 15 T4	20.2	2 10	51.3	7	1140	3
8.85	27	10.65	~ 3 22	13.35	17	17.8	12	26.6	2 10	52.0	I 5	3438	I
8.87	26	10.68	21	13.40	16	17.9	-3	26.8	8	53.7	- 5	Infinit	eo o
1						1		1		1			

Table C²

POSITION-LINES CORRESPONDING TO THE A AND B CORRECTION. FOR USE WITH THE PLANE-SCALE CHART IN THE SUMNER PROBLEM.

Name the position-line according to the name of the A and B correction, and contrary to the name of the bearing of the body observed.

A and B	Position-	A and B	Position-	A and B	Position-	A and B	Position-	A and B	Position-	A and B	Position-	A and B	Position-	A and B	Position-
Correction.	lines.	Correction.	lines.	Correction.	lines.	Correction.	lines.	Correction.		Correction.	lines.	Correction.	lines.	Correction.	liues.
·00 ·01 ·02 ·03 ·04	= 0.0 0.0 1.1 1.7 2.3	·25= ·26 ·27 ·28 ·29	° 14.0 14.6 15.1 15.6 16.2	·50 = ·51 ·52 ·53 ·54	= 26°6 27°0 27°5 27°9 28°4	75= ·76 ·77 78 ·79	= 36.9 37.2 37.6 38.0 38.3	1.00 1.01 1.02 1.03 1.04	45'3 45'6 45'8 45'8 46'1	1.42 1.44 1.46 1.48 1.50	= 54.8 55.2 55.6 56.0 56.3	1'92: 1'94 1'96 1'98 2'00	62.5 62.7 63.0 63.2 63.4	4'2= 4'4 4'6 4'8 5'0	= 76°6 77°2 77°7 78°2 78°7
•05 •06 •07 •08 •09	2·9 3·4 4·3 4·6 5·1	•30 •31 32 •33 •34	16.7 17.2 17.7 18.3 18.8	•55 56 •57 •58 •59	28·8 29·2 29·7 30·1 30·5	·80 ·81 ·82 ·83 ·84	38.7 39.0 39.4 39.7 40.0	1.02 1.02 1.03 1.10	46·4 46·7 46·9 47·2 47·7	1.22 1.24 1.26 1.28 1.60	56.7 57.0 57.3 57.7 58.0	2.05 2.10 2.15 2.20 2.25	64.0 64.5 65.1 65.6 66.0	5.2 6.0 6.2 7.0 8.0	79'7 80'5 81'3 81'9 82'9
·10 ·11 ·12 ·13 ·14	5°7 6 3 6'8 7'4 8'0	·35 ·36 ·37 ·38 ·39	19 3 19 8 20 3 20 8 21 3	•60 •61 •62 •63 •64	31.0 31.4 31.8 32.2 32.6	•85 •86 •87 •88 •89	40'4 40'7 41'0 41'3 41'7	1.15 1.14 1.16 1.18 1.20	48·2 48·7 49·2 49.7 50·2	1.62 1.64 1.66 1.68 1.70	58·3 58·6 58·9 59·2 59·5	2.30 2.40 2.50 2.60 2.70	66`5 67`4 68`2 69`0 69`7	9.0 10.0 11.0 13.0	83°7 84°3 84°8 85°2 85°6
·15	8.5	'40	21.8	·65	33.0	•90	42.0	1.22	50.7	1.72	59 ^{.8}	2.80	70'3	15.0	86·2
·16	9.1	'41	22.3	·66	33.4	•91	42.3	1.24	51.1	1.74	60 [.] 1	2.90	71'0	17.0	86·6
·17	9.6	'42	22.8	·67	33.8	•92	42.6	1.26	51.6	1.76	60 [.] 4	3.00	71'6	20.0	87·1
·18	10.2	'43	23.3	·68	34.2	•93	42.9	1.28	52.0	1.78	60 [.] 7	3.10	72'1	25.0	87·7
·19	10.8	'44	23.7	·69	34.6	•94	43.2	1.30	52.4	1.80	60 [.] 9	3.20	72'6	30.0	88·1
•20	11.3	45	24·2	·70	35.0	95	43 ^{.5}	1•32	52·9	1.82	61·2	3·30	73 ^{•1}	40.0	88.6
•21	11.9	•46	24·7	·71	35.4	96	43 ^{.8}	1•34	53·3	1.84	61·5	3·40	73 ^{•6}	50.0	88.9
•22	12.4	•47	25·2	72	35.8	97	44 ^{.1}	1•36	53·7	1.86	61·7	3·60	74 ^{•5}	100.0	89.4
•23	13.0	•48	25·6	·73	36.1	98	44 ^{.4}	1•38	54·1	1.88	62·0	3·80	75 ^{•3}	200.0	89.7
•24	13.5	•49	26·1	·74	36.5	98	44 ^{.7}	1•40	54·5	1.90	62·2	4·00	76 [•] 0	Infinite	90.0

It must be borne in mind that this table does not give the *true* geographical lines of position, but lines of position which will give the same result as to latitude and longitude on a plane chart as the true lines of position would give on a Mercator's chart. It is given here for the purpose of saving the trouble of getting out a chart. All that is required for plotting the Sumner position will be a horizontal line in the work-book representing the D.R. latitude, and a perpendicular line to the former for use in laying off the position-lines by a protractor. On the horizontal line set off the points of two longitudes at a distance from one another of, say, I in. to IO' of longitude. From these two points lay down the Sumner lines, and from the point where they intersect draw a perpendicular to the line of D.R. latitudes. The longitude at the point struck by the perpendicular is the longitude required, and can be measured from either of the points of longitude. The same scale is used for the latitude as for the longitude.

A small 5 in. boxwood protractor rule with a diagonal scale of inches for measuring to $\frac{1}{100}$ part of an inch may be bought for 1s., and is the only instrument which will be required.

To find the *true* position-line from this table consider the A and B correction as a diff. long., the dep. corresponding to this diff. long. will then give the true line of position, and will give the same position—*i e.*, latitude and longitude—on the Mercator chart that the other dines of position give on the plane chart.

Example for true position-line: In lat 47° S. a.m. sun's obsn., when A and B cor. = d. long. *85' N. dep = '58' N. = true position-line N. 30° W.

Showing the Error produced in the Time or Longitude by an Error of i' in the Altitude.

Tat							А	ZIMUI	'HS.						
1/8.9.	90°	89°	88 °	87°	86°	85°	84°	83°	82°	81º	80°	79 °	78 °	770	76º
•	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.
0	4'00	4'00	4'00	4°01	4'01	4'02	4'02	4 [.] 03	4°04	4°05	4'06	4°07	4'09	4'10	4'12
1 2 3	4'00 4'00 4.01	4.00 4.00 4.01	4.00 4.00 4.01	4.01 4.01 4.01	4'01 4'01 4'02	4'02 4'02 4'02	4.02 4.02 4.03	4.03 4.03 4.04	4.04 4.04 4.04	4.05 4.05 4.06	4.06 4.06 4.07	4.08 4.08 4.08	4.09 4.09	4'II 4'II	4°12 4°12
45	4'01 4'01	4°01 4°02	4.01 4.02	4.02 4.02	4.02 4.03	4.03 4.03	4°03 4°04	4°04 4°05	4.05 4.05	4.06 4.07	4.07 4.08	4°08 4°09	4.10	4.12 4.12	4'I3 4 I4
6	4.02	4'02	4.02	4.03	4.03	4.04	4.04	4.05	4.06	4.07	4'08	4.10	4.11	4.13	4°15
7	4.03	4'03	4.03	4.04	4.04	4.05	4.05	4.06	4.07	4.08	4'09	4.11	4.12	4.14	4°15
8	4.04	4'04	4.04	4.04	4.05	4.05	4.06	4.07	4.08	4.09	4'10	4.11	4.13	4.15	4°16
9 10	4°05 4°06	4.05	4.05	4.06	4.06 4.07	4.07 4.08	4°07 4°08	4.08	4.09 4.10	4°10 4'11	4'11 4'12	4.13 4.14	4°14 4°15	4°16 4°17	4'17 4'19
11 12 13 14 15	4.07 4.09 4.10 4.12 4.14	4'00 4'09 4'11 4'12 4'14	4°09 4°11 4°12 4°14	4.09 4.11 4.13 4.15	4.10 4.12 4.13 4.15	4.09 4.10 4.12 4.14 4.14	4°10 4°11 4°13 4°15 4°16	4°11 4°12 4°14 4°15 4°17	4°13 4°13 4°15 4°16 4°18	4.13 4.14 4.16 4.17 4.19	4°14 4°15 4°17 4°19 4°20	4°15 4°17 4°18 4°20 4°22	4°17 4°18 4°20 4°21 4°23	4'18 4'20 4'21 4'23 4'25	4°20 4°21 4°23 4°25 4°27
16 17 18 19	4'16 4'18 4'21 4'23 4'26	4.16 4.18 4.21 4.23 4.26	4.16 4.19 4.21 4.23 4.26	4'17 4'19 4'21 4'24 4'26	4°17 4°19 4°22 4°24	4°18 4°20 4°22 4°25 4°27	4.18 4.21 4.23 4.25 4.28	4.19 4.21 4.24 4.26 4.20	4°20 4°22 4°25 4°27 4°30	4.21 4.23 4.26 4.28	4°23 4°25 4°27 4°30	4.24 4.26 4.28 4.31	4°25 4°28 4°30 4°32	4'27 4'29 4'32 4'34	4°29 4°31 4°33 4°36
21 22 23 24 25	4.28 4.31 4.34 4.38 4.41	4.31 4.35 4.38 4.41	4.29 4.32 4.35 4.38 4.42	4.29 4.32 4.35 4.38 4.42	4 30 4 32 4 36 4 39 4 4	4°30 4°33 4°36 4°40	4°31 4°34 4°37 4°40 4°44	4'32 4'35 4'38 4'41	4'33 4'36 4'39 4'42 4'46	4'34 4'37 4'40 4'43	4 35 4 35 4 38 4 41 4 45 4 45	4 34 4 36 4 39 4 43 4 46 4 50	4 33 4 38 4 41 4 44 4 48 4 51	4°40 4°43 4°46 4°49 4°53	4 39 4 42 4 45 4 45 4 48 4 51 4 51
26	4°45	4°45	4°45	4°46	4.46	4°47	4°47	4.48	4°49	4.51	4.52	4°53	4.55	4.57	4°59
27	4°49	4°49	4°49	4°49	4.50	4°51	4°51	4.52	4°53	4.55	4.56	4°57	4.59	4.61	4°63
28	4°53	4°53	4°53	4°54	4.54	4°55	4°55	4.56	4°57	4.59	4.60	4°62	4.63	4.65	4°67
29	4°57	4°57	4°58	4°58	4.58	4°59	4°60	4.61	4°62	4.63	4.64	4°66	4.68	4.69	4°71
30	4°52	4°62	4°62	4°63	4.63	4°64	4°64	4.65	4°66	4.68	4.69	4°71	4.72	4.74	4°76
31	4.67	4.67	4.67	4.67	4.68	4.68	4.69	4°70	4.71	4 ·72	4`74	4°75	4°77	4°79	4·81
32	4.72	4.72	4.72	4.72	4.73	4.73	4.74	4°75	4.76	4·78	4`79	4°80	4°82	4°84	4·86
33	4.77	4.77	4.77	4.78	4.78	4.79	4.80	4°81	4.82	4·83	4`84	4°86	4°88	4°89	4·92
34	4.82	4.82	4.83	4.83	4.84	4.84	4.85	4°86	4.87	4·89	4`90	4°92	4°93	4°95	4·97
35	4.88	4.88	4.89	4.89	4.90	4.90	4.91	4°92	4.93	4 · 94	4`96	4°97	4°99	5°01	5·03
36	4°94	4°95	4°95	4°95	4°96	4.96	4`97	4'98	4°99	5.01	5.02	5.04	5.05	5.07	5°10
37	5°01	5°01	5°01	5°02	5°02	5.03	5`04	5'05	5°06	5.07	5.09	5.10	5.12	5.14	5°16
38	5°08	5°08	5°08	5°08	5°09	5.10	5`10	5'11	5°13	5.14	5.15	5.17	5.19	5.21	5°23
39	5°15	5°15	5°15	5°15	5°16	5.17	5`18	5'18	5°20	5.21	5.23	5.24	5.26	5.28	5°30
40	5°22	5°22	5°22	5°23	5°23	5.24	5`25	5'26	5°27	5.29	5.30	5.32	5.34	5.36	5°38
41	5·30	5°30	5°30	5°31	5°31	5°32	5`33	5'34	5'35	5°37	5'3 ⁸	5°40	5·42	5'44	5·46
42	5·38	5°38	5°39	5°39	5°40	5°40	5'41	5'42	5'44	5°45	5'47	5°48	5·50	5'52	5·55
43	5·47	5°47	5°47	5°48	5°48	5°49	5'50	5'51	5'52	5°54	5'55	5°57	5·59	5'61	5·64
44	5·56	5°56	5°56	5°57	5°57	5°58	5'59	5'60	5'62	5°63	5'65	5°66	5·68	5'71	5·73
45	5·66	5°66	5°66	5°66	5°67	5°68	5'69	5'70	5'71	5°73	5'74	5°76	5·78	5'81	5·83
46	5.76	5°76	5.76	5.77	5°77	5.78	5'79	5.80	5.81	5·83	5 ^{.85}	5 ^{.87}	5.89	5.91	5.93
47	5.87	5°87	5.87	5.87	5°88	5.89	5'90	5.91	5.92	5·94	5 ^{.96}	5 ^{.97}	6.00	6.02	6.04
48	5.98	5°98	5.9 8	5.99	5°99	6.00	6'01	6.02	6.04	6·05	6 ^{.07}	6 ^{.09}	6.11	6.14	6.16
49	6.10	6°10	6.10	6.11	6°11	6.12	6'13	6.14	6.16	6·17	6 ^{.19}	6 ^{.21}	6.23	6.26	6.28
50	6.22	6°22	6.23	6.23	6°24	6.25	6'26	6.27	.6.28	6·30	6 ^{.32}	6 ^{.34}	6.36	6.39	6.41
51	6·36	6·36	6.36	6.36	6·37	6·38	6·39	6·40	6·42	6·44	6·45	6·48	6·50	6·52	6·55
52	6·50	6·50	6.20	6.21	6·51	6·52	6·53	6·55	6·56	6·58	6·60	6·62	6·64	6·67	6·70
53	6·65	6·65	6.62	6.66	6·66	6·67	6·68	6·70	6·71	6·73	6·75	6·77	6·80	6·82	6·85
54	6·81	6·81	6.81	6.81	6·82	6·83	6·84	6·86	6·87	6·89	6·91	6·93	6·96	6·98	7·01
55	6·97	6·97	6.98	6.98	6·99	7·00	7·01	7·03	7·04	7·06	7·08	7·10	7·13	7·16	7·19
56	7°15	7°15	7°16	7°16	7°17	7°18	7'19	7°21	7°22	7°24	7°26	7°29	7 [.] 31	7'34	7'37
57	7°34	7°35	7°35	7°35	7°36	7°37	7'38	7°40	7°42	7°44	7°46	7′48	7 [.] 51	7'54	7'57
58	7°55	7°55	7°55	7°56	7°57	7°58	7'59	7°61	7°62	7°64	7°66	7°69	7 [.] 72	7'75	7'78
59	7°77	7°77	7°77	7°78	7°79	7°80	7'81	7°82	7°84	7°86	7°89	7°91	7 [.] 94	7'97	8'00
60	8°00	8°00	8°00	8°01	8°02	8°03	8'04	8°06	8°08	8°10	8°12	8°15	8 [.] 18	8'21	8'24

To convert time into longitude divide by 4. Thus $8 \cos s + 4 = 2'$ long.

"Showing the Error produced in the Time or Longitude by an Error of i' in the Altitude.

Let							А	ZIMUT	HS.						
	75°	740	730	72°	71°	70°	697	°68°	67°	6 6 °	65°	64°	63°	62°	61°
。 0 1 2 3 4 5	s. 4'14 4'14 4'14 4.15 4'15 4'16	s. 4'16 4'16 4'16 4'17 4'17 4'18	s. 4'18 4'19 4'19 4'19 4'19 4'20	S. 4'21 4'21 4'21 4'21 4'21 4'22 4'22	s. 4 ^{·23} 4 ^{·23} 4 ^{·23} 4 ^{·24} 4 ^{·24} 4 ^{·25}	s. 4°26 4°26 4°26 4°26 4°27 4°27	s. 4·28 4·29 4·29 4·29 4·30 4·30	s. 4'31 4'32 4'32 4'32 4'32 4'32	s. 4·35 4·35 4·35 4·35 4·36 4·36	s. 4·38 4·38 4·38 4·38 4·38 4·38 4·39 4·40	s. 4'4I 4'42 4'42 4'42 4'42 4'42	s. 4'45 4'45 4'45 4'46 4'46 4'46	s. 4*49 4*49 4*49 4*50 4*50 4*51	s. 4*53 4*53 4*53 4*53 4*54 4*54	s. 4°57 4°57 4°58 4°58 4°58 4°58
6 7 8 9 10 11 12	4°16 4°17 4°18 4°19 4°20 4°22 4°23	4.18 4.19 4.20 4.21 4.23 4.24 4.25	4.21 4.22 4.23 4.25 4.26 4.28	4.23 4.24 4.25 4.26 4.27 4.28 4.30	4*25 4*26 4*27 4*28 4*30 4*31 4*32	4 ·28 4 ·29 4·30 4·31 4·32 4·34 4·35	4.31 4.32 4.33 4.34 4.35 4.36 4.38	4·34 4·35 4·36 4·37 4·38 4·39 4·41	4.37 4.38 4.39 4.40 4.41 4.43 4.44	4.40 4.41 4.42 4.43 4.43 4.45 4.46 4.48	4'44 4'45 4'46 4'47 4'48 4'50 4'51	4'47 4'48 4'49 4'51 4'52 4'53 4'55	4.51 4.52 4.53 4.55 4.56 4.57 4.59	4.56 4.56 4.57 4.59 4.60 4.62 4.63	4.60 4.61 4.62 4.63 4.64 4.66 4.66 4.68
13 14 15 16 17 18	4.25 4.27 4.29 4.31 4.33 4.35	4.29 4.31 4.33 4.35 4.38	4.31 4.33 4.35 4.37 4.40	4°32 4°33 4°35 4°38 4°40 4°42	4°34 4°36 4°38 4°40 4°42 4°42	4°37 4°39 4°41 4°43 4°45 4°48	4°40 4°42 4°44 4°46 4°48 4°51	4°43 4°45 4°47 4°49 4°51 4°54	4.40 4.48 4.50 4.52 4.52 4.54 4.57	4°49 4°51 4°53 4°56 4°58 4°58 4°60	4.53 4.55 4.57 4.59 4.62 4.64	4.57 4.59 4.61 4.63 4.65 4.68	4.61 4.63 4.65 4.67 4.69 4.72	4.65 4.67 4.69 4.71 4.74 4.76	4.69 4.71 4.73 4.76 4.78 4.78 4.81
19 20 21 22 23 24 25	4°38 4°41 4°44 4°47 4°50 4°53 4°57	4'40 4'43 4'46 4'49 4'52 4'56 4'59	4°42 4'45 4'48 4'51 4'54 4'58 4'62	4°45 4°48 4°51 4°54 4°57 4°60 4°64	4'47 4'50 4'53 4'56 4'60 4'63 4'67	4.50 4.53 4.56 4.59 4.62 4.66 4.70	4.53 4.56 4.59 4.62 4.65 4.65 4.69 4.73	4.56 4.59 4.62 4.65 4.69 4.72 4.76	4.60 4.62 4.65 4.69 4.72 4.76 4.70 4.79	4.63 4.66 4.69 4.72 4.76 4.79 4.83	4.67 4.70 4.73 4.76 4.79 4.83 4.87	4.71 4.74 4.77 4.80 4.83 4.83 4.87 4.91	4.75 4.78 4.81 4.84 4.88 4.91 4.91	4.79 4.82 4.85 4.89 4.92 4.96 5.00	4.84 4.87 4.90 4.93 4.97 5.01 5.05
26 27 28 29 30	4.61 4.65 4.69 4.73 4.78 4.83	4.63 4.67 4.71 4.76 4.80 4.85	4.65 4.69 4.74 4.78 4.83 4.88	4.68 4.72 4.76 4.81 4.86 4.80	4.71 4.75 4.79 4.84 4.88	4°74 4°78 4°82 4°87 4°92	4°77 4°81 4°85 4°90 4°95	4.80 4.84 4.89 4.93 4.98	4 ^{.8} 3 4 ^{.88} 4 ^{.92} 4 ^{.97} 5 ^{.02}	4.87 4.91 4.96 5.01 5.06	4.91 4.95 5.00 5.05 5.10	4.95 5.00 5.04 5.09 5.14	4.99 5.04 5.08 5.13 5.18	5.04 5.08 5.13 5.18 5.23	5.09 5.13 5.18 5.23 5.28
32 33 34 35 36	4.88 4.94 5.00 5.06	4.91 4.96 5.02 5.08 5.14	4 93 4 99 5 0 5 5 1 1 5 1 7	4·96 5·01 5·07 5·13 5·20	4'99 5'04 5'10 5'16	5.02 5.08 5.13 5.20 5.20	5.05 5.11 5.17 5.23 5.30	5.09 5.14 5.20 5.27 5.33	5°12 5°18 5°24 5°30 5°37	5.16 5.22 5.28 5.35 5.41	5°20 5°26 5°32 5°39 5°46	5.25 5.31 5.37 5.43 5.50	5·29 5·35 5·42 5·48	5°34 5°40 5°46 5°53 5°60	5 34 5 39 5 45 5 52 5 58 5 58
37 38 39 40 41	5.19 5.26 5.33 5.41 5.49	5.21 5.28 5.35 5.43 5.51	5·24 5·31 5·38 5·46 5·54	5·27 5·34 5·41 5·49 5·57	5-30 5-37 5-44 5-52 5-61	5·33 5·40 5·48 5·56 5·64	5·36 5·44 5·51 5·59 5·68	5°40 5°47 5°55 5°63 5°72	5.44 5.51 5.59 5.67 5.76	5.48 5.56 5.63 5.72 5.80	5.60 5.68 5.76 5.85	5.57 5.65 5.73 5.81 5.90	5.62 5.70 5.78 5.86	5.67 5.75 5.83 5.91 6.00	5.73 5.80 5.88 5.97 6.06
42 43 44 45 46	5*57 5*66 5*76 5*86	5.60 5.69 5.78 5.88 5.99	5.63 5.72 5.81 5.92 6.02	5.66 5.75 5.85 5.95 6.05	5.69 5.78 5.88 5.98 5.98	5.73 5.82 5.92 6.02 6.13	5.77 5.86 5.96 6.06 6.17	5.81 5.90 6.00 6.10 6.21	5.85 5.94 6.04 6.15 6.26	5.89 5.99 6.09 6.19 6.30	5'94 6'03 6'14 6'24 6'35	5'99 6'09 6'19 6'29 6'41	6.04 6.14 6.24 6.35 6.46	6.10 6.19 6.30 6.41 6.52	6·15 6·25 6·36 6·47 6·58
47 48 49 50	6.07 6.19 6.31 6.44 6.58	6.10 6.22 6.34 6.47 6.61	6.13 6.25 6.38 6.51 6.65	6.17 6.29 6.41 6.54 6.68	6·20 6·32 6·45 6·58 6·72	6.24 6.36 6.49 6.62 6.76	6·28 6·40 6·53 6·67 6·81	6·33 6·45 6·58 6·71 6·86	6·37 6·49 6·62 6·76 6·00	6.42 6.54 6.67 6.81 6.06	6·47 6·60 6·73 6·87	6·53 6·65 6·78 6·92 7·07	6.58 6.71 6.84 6.98 7.13	6.64 6.77 6.91 7.05 7.20	6·71 6·83 6·97 7·11
51 52 53 54 55 55	6·73 6·88 7·05 7·22	6.76 6.91 7.08 7.25	6.79 6.95 7.12 7.29	6.83 6.99 7.16 7.33	6.87 7.03 7.20 7.38	6.91 7.07 7.24 7.42	6.96 7.12 7.29 7.47	7.01 7.17 7.34 7.52	7.06 7.22 7.39 7.58	7.11 7.28 7.45 7.63	7°17 7°33 7°51 7°69	7°23 7°39 7°57 7°76	7 * 5 7 * 29 7 * 46 7 * 64 7 * 83 8 * 02	7·36 7·53 7·71 7·90 8·10	7 43 7 60 7 78 7 97 8 78
57 58 59 60	7 41 7 60 7 81 8 04 8 28	7 44 7 64 7 85 8 08 8 32	7.68 7.68 7.89 8.12 8.37	7.52 7.72 7.94 8.17 8.41	7.57 7.77 7.98 8.21 8.46	7.82 8.03 8.26 8.51	7.87 8.09 8.32 8.57	7'92 8'14 8'38 8'63	7 '98 8 20 8 44 8 69	8.04 8.26 8.50 8.76	8.10 8.33 8.57 8.83	8.17 8.40 8.64 8.90	8·24 8·47 8·72 8·98	8·32 8·55 8·80 9·06	8·40 8·63 8·88 9·15

To convert time into longitude divide by 4. Thus $8.28 \text{ s.} \div 4 = 2.07' \text{ long.}$

Showing the Error produced in the Time or Longitude by an Error of I' in the

ALTITUDE.

Let							ΔZ	IMUT	18.						
	60°	59°	58°	57°	56°	55°	54°	58 °	52°	51°	50°	49°	4 8°	470	46°
° 0 1 2 3 4 5	s. 4·62 4·62 4·63 4·63 4·63 4·64	s. 4·67 4·67 4·67 4·67 4·68 4·68	s. 4 [.] 72 4 [.] 72 4 [.] 72 4 [.] 72 4 [.] 73 4 [.] 73	s. 4·77 4·77 4·77 4·78 4·78 4·78 4·79	s. 4·82 4·83 4·83 4·83 4·84 4·84	s. 4*88 4*89 4*89 4*89 4*90 4*90	s. 4'94 4'95 4'95 4'95 4'96 4'96	s. 5.01 5.01 5.01 5.02 5.02 5.02 5.03	s. 5.08 5.08 5.08 5.08 5.09 5.10	s. 5*15 5*15 5*15 5*15 5*15 5*16 5*17	s. 5 ²² 5 ²² 5 ²² 5 ²³ 5 ²³ 5 ²⁴	8. 5'30 5'30 5'30 5'31 5'31 5'31 5'32	8. 5*38 5*39 5*39 5*39 5*40 5*40	8. 5'47 5'47 5'47 5'48 5'48 5'48 5'49	s. 5*56 5*56 5*56 5*57 5*57 5*57 5*58
6 7 8 9 10	4.64 4.65 4.66 4.68 4.69	4.69 4.70 4.71 4.72 4.74	4°74 4°75 4°76 4°78 4°79	4.80 4.81 4.82 4.83 4.83 4.84	4*85 4*86 4*87 4*89 4*90	4*91 4*92 4*93 4*94 4*96	4°97 4°98 4°99 5°01 5°02	5.04 5.05 5.06 5.07 5.09	5°10 5°11 5°13 5°14 5°15	5.17 5.19 5.20 5.21 5.23	5°25 5°26 5°27 5°29 5°30	5°33 5°34 5°35 5°37 5°38	5°41 5°42 5°44 5°45 5°47	5°50 5°51 5°52 5°54 5°55	5.59 5.60 5.62 5.63 5.63
11 12 13 14 15	4.71 4.72 4.74 4.76 4.78	4°75 4°77 4°79 4°81 4°83	4 ·81 4 ·82 4 · 84 4 · 86 4 · 88	4.86 4.88 4.89 4.92 4.94	4 ` 92 4`93 4`95 4`97 5 ` 00	4'97 4'99 5'01 5'03 5'06	5°04 5°05 5°07 5°10 5°12	5.10 5.12 5.14 5.16 5.19	5.17 5.19 5.21 5.23 5.26	5.24 5.26 5.28 5.30 5.33	5°32 5°34 5°36 5°38 5°41	5°40 5°42 5°44 5°46 5°49	5.48 5.50 5.52 5.55 5.55 5.57	5.57 5.59 5.61 5.64 5.66	5.66 5.68 5.71 5.73 5.76
16	4.80	4°85	4'91	4°96	5.02	5.08	5°14	5°21	5°28	5.35	5°43	5.51	5.60	5.69	5.78
17	4.83	4°88	4'93	4°99	5.05	5.11	5°17	5°24	5°31	5.38	5°46	5.54	5.63	5.72	5.81
18	4.86	4°91	4'96	5°01	5.07	5.13	5°20	5°27	5°34	5.41	5°49	5.57	5.66	5.75	5.85
19	4.88	4°94	4'99	5°04	5.10	5.16	5°23	5°30	5°37	5.44	5°52	5.60	5.69	5.78	5.88
20	4.92	4°97	5'02	5°08	5.13	5.20	5°26	5°33	5°40	5.48	5°56	5.64	5.73	5.82	5.92
21	4°95	5.00	5.05	5°11	5°17	5°23	5°30	5·36	5°44	5.51	5°59	5.68	5.77	5.86	5.96
22	4°98	5.03	5.09	5°14	5°20	5°27	5°33	5·40	5°47	5.55	5°63	5.72	5.81	5.90	6.00
23	5°02	5.07	5.12	5°18	5°24	5°30	5°37	5·44	5°51	5.59	5°67	5.76	5.85	5.94	6.04
24	5°06	5.11	5.16	5°22	5°28	5°34	5°41	5·48	5°56	5.63	5°72	5.80	5.89	5.99	6.09
25	5°10	5.15	5.20	5°26	5°32	5°39	5°46	5·53	5°60	5.68	5°76	5.85	5.94	6.03	6.13
26	5°14	5°19	5°25	5°31	5·37	5°43	5.50	5.57	5.65	5'73	5.81	5.90	5.99	6.09	6.19
27	5°18	5°24	5°29	5°35	5·42	5°48	5.55	5.62	5.70	5'78	5.86	5.95	6.04	6.14	6.24
28	5°23	5°28	5°34	5°40	5·46	5°53	5.60	5.67	5.75	5'83	5.91	6.00	6.10	6.19	6.30
29	5°28	5°34	5°39	5°45	5·52	5°58	5.65	5.73	5.80	5'88	5.97	6.06	6.15	6.25	6.36
30	5°33	5°39	5°45	5°51	5·57	5°64	5.71	5.78	5.86	5'94	6.03	6.12	6.22	6.32	6.42
31	5°39	5°44	5°50	5.56	5.63	5.70	5.77	5.84	5.92	6.00	6.09	6.18	6·28	6·38	6·49
32	5°45	5°50	5°56	5.62	5.69	5.76	5.83	5.91	5.99	6.07	6.16	6.25	6·35	6·45	6·56
33	5°51	5°56	5°62	5.69	5.75	5.82	5.90	5.97	6.05	6.14	6.23	6.32	6·42	6·52	6·63
34	5°57	5°63	5°69	5.75	5.82	5.89	5.96	6.04	6.12	6.21	6.30	6.39	6·49	6·60	6·71
35	5°64	5°70	5°76	5.82	5.89	5.96	6.04	6.11	6.20	6.28	6.37	6.47	6·57	6·68	6·79
36	5.71	5°77	5.83	5.90	5.96	6.04	6·11	6·19	6·27	6·36	6·45	6.55	6.65	6.76	6·87
37	5.78	5°84	5.91	5.97	6.04	6.11	6·19	6·27	6·36	6·44	6·54	6.64	6.74	6.85	6·96
38	5.86	5°92	5.99	6.05	6.12	6.20	6·27	6·36	6·44	6·53	6·63	6.73	6.83	6.94	7·06
39	5.94	6°00	6.07	6.14	6.21	6.28	6·36	6·44	6·53	6·62	6·72	6.82	6.93	7.04	7·16
40	6.03	6°09	6.16	6.23	6.30	6.37	6·45	6·54	6·63	6·72	6·82	6.92	7.03	7.14	7·26
41	6·12	6·18	6·25	6·32	6·39	6·47	6·55	6.64	6·73	6·82	6·92	7.02	7.13	7 ^{•25}	7°37
42	6·22	6·28	6·35	6·42	6·49	6·57	6·65	6.74	6·83	6·93	7·03	7.13	7.24	7 ^{•36}	7°48
43	6·32	6·38	6·45	6·52	6·60	6·68	6·76	6.85	6·94	7·04	7·14	7.25	7.36	7 ^{•48}	7°60
44	6·42	6·49	6·56	6·63	6·71	6·79	6·87	6.96	7·06	7·16	7·26	7.37	7.48	7 ^{•60}	7°73
45	6·53	6·60	6·67	6·75	6·82	6·91	6·99	7.08	7·18	7·28	7·38	7.50	7.61	7 ^{•73}	7°86
46	6·65	6·72	6·79	6·87	6·95	7°03	7 ^{•12}	7 ·21	7`31	7°41	7.52	7.63	7°75	7.87	8.00
47	6·77	6·84	6·92	6·99	7·07	7°16	7 ^{•25}	7·34	7`44	7°55	7.66	7.77	7'89	8.02	8.15
48	6·90	6·97	7·05	7·13	7·21	7°30	7 ^{•39}	7·49	7`59	7°69	7.80	7.92	8'04	8.17	8.31
49	7·04	7·11	7·19	7·27	7·35	7°44	7 ^{•54}	7·63	7`74	7°85	7.96	8.08	8'20	8.34	8.48
50	7·19	7·26	7·34	7·42	7·51	7°60	7 ^{•69}	7·79	7`90	8°01	8.12	8.25	8'37	8.51	8.65
51	7°34	7°42	7°49	7·58	7.67	7'76	7·86	7·96	8.07	8·18	8·30	8.42	8·55	8.69	8·84
52	7°50	7°58	7°66	7·75	7.84	7'93	8·03	8·14	8.24	8·36	8·48	8.61	8·74	8.88	9·03
53	7°67	7°75	7°84	7·93	8.02	8'11	8·22	8·32	8.43	8·55	8·68	8.81	8·94	9.09	9·24
54	7°86	7°94	8°02	8·11	8.21	8'31	8·41	8·52	8.64	8·76	8·88	9.02	9·16	9.30	9·46
55	8°05	8°14	8°22	8·32	8.41	8'51	8·62	8·73	8.85	8·97	9·10	9.24	9·38	9.54	9·69
56	8·26	8·35	8·43	8·53	8.63	8·73	8·84	8·96	9.08	9°20	9'34	9.48	9.63	9.78	9'94
57	8·48	8·57	8·66	8·76	8.86	8·97	9·08	9·20	9.32	9°45	9'59	9.73	9.88	10.04	10'21
58	8·72	8·81	8·90	9·00	9.10	9·21	9·33	9·45	9.58	9°71	9'85	10.00	10.16	10.32	10'49
59	8·97	9·06	9·16	9·26	9.37	9·48	9·60	9·72	9.86	9°99	10'14	10.29	10.45	10.62	10'80
60	9·24	9·33	9·43	9·54	9.65	9·77	9·89	10·02	9.86	10°29	10'44	10.60	10.77	10.94	11'12

To convert time into longitude divide by 4. Thus 9.24 s. + 4 = 2.31' long.

Table	D.

Showing the Error produced in the Time or Longitude by an Error of i' in the ALTITUDE.

Lat							A	ZIMUI	PHS.						
	4 5°	44°	43 °	42°	41°	40°	39°	380	37°	36°	350	34°	33°	320	310
• 0 1 2 3 4 5	s. 5.60 5.60 5.60 5.60 5.67	s. 5'70 5'70 5'70 5'70 5'70 5'70 5'70	s. 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.	s. 7 5.98 7 5.98 7 5.98 7 5.99 5.99 6.00	s. 6·10 6·10 6·11 6·11 6·11	s. 6·2: 6·2: 6·2: 6·2: 6·2: 6·2:	s. 2 6·3 2 6·3 3 6·3 3 6·3 4 6·3 5 6·3	s. 6 6·50 6 6·50 6 6·50 6 6·50 7 6·50 8 6·50	s. 6 6 6 6 6 6 6 6 6 1 6 6 1 6 6 1 6 6	s. 5 6.81 5 6.81 5 6.81 6 6.81 6 6.82 7 6.83	s. 6·9 6·9 6·9 6·9 7·0	S. 7 7 1 7 7 1 8 7 1 8 7 1 8 7 1 8 7 1 9 7 1 7 1 7 1	s. 5 7'3 5 7'3 6 7'3 6 7'3 7 7'3 7 7'3 8 7'3	8. 4 7°5 5 7°5 5 7°5 5 7°5 7 55 7 55 7 55 7 55 7 55	s. 5 7'77 5 7'77 5 7'77 5 7'78 7'78 7'79 7'80
6 7 8 9 10	5.69 5.70 5.71 5.73 5.73 5.74	5.80 5.81 5.83 5.83 5.83	5.90 5.91 5.92 5.94 5.96	6.01 6.02 6.04 6.05 6.05	6.13 6.14 6.16 6.17 6.19	6·26 6·27 6·28 6·30 6·32	5 6·39 6·40 6·44 6·44 6·44	6.55 6.55 6.56 6.58 6.58 6.58	6.7 6.7 6.7 6.7 6.7	8 6.84 6.86 6.87 8 6.87 8 6.89 5 6.91	7°0 7°0 7°0 7°0	7.10 7.21 7.24 7.24 7.24 7.24 7.24	7.40 7.40 7.40 7.44 7.44 7.44	7.62 7.62 7.64 7.66	7.81 7.82 7.84 7.86 7.89
11 12 13 14 15	5.76 5.78 5.81 5.83 5.86	5.87 5.89 5.91 5.93 5.96	5.97 6.00 6.02 6.04 6.04	6.09 6.11 6.14 6.19	6.21 6.23 6.26 6.28 6.31	6·34 6·36 6·39 6·41 6·44	6.48 6.50 6.52 6.55 6.58	6.62 6.64 6.67 6.70 6.73	6.80 6.80 6.80 6.80 6.80	7 6.93 6.96 2 6.98 7.01 7.05	7.10 7.13 7.16 7.19 7.22	7 * 29 7 * 31 7 * 34 7 * 37 7 * 41	7 48 7 51 7 54 7 57 7 57	7.69 7 72 7 75 7 78 7.81	7 . 91 7.94 7.97 8.00 8.00
16 17 18 19 20	5.88 5.92 5.95 5.98 6.02	5.99 6.02 6.05 6.09 6.13	6.10 6.13 6.17 6.20 6.24	6·22 6·25 6·28 6·32 6·36	6·34 6·38 6·41 6·45 6·49	6.47 6.51 6.54 6.58 6.62	6.61 6.65 6.68 6.72 6.76	6.76 6.79 6.83 6.87 6.91	6·91 6·95 6·95 7·03 7·03	7.08 7.12 7.16 7.20 7.24	7*25 7*29 7*33 7*38 7*42	7.44 7.48 7.52 7.57 7.61	7 64 7 68 7 72 7 72 7 77 7 82	7 ^{.8} 5 7 ^{.8} 9 7 94 7 [.] 98 8 [.] 03	8.08 8 12 8 17 8.21 8.26
21	6.06	6·17	6·28	6·40	6•53	6.67	6.81	6.96	7.12	7·29	7*47	7.66	7*87	8.09	8·32
22	6.10	6·21	6·33	6·45	6•58	6.71	6.86	7.01	7.17	7·34	7*52	7.71	7*92	8.14	8·38
23	6.15	6·26	6·37	6·49	6•62	6.76	6.90	7.06	7.22	7·39	7*58	7.77	7*98	8.20	8·44
24	6.19	6·30	6·42	6·54	6•67	6.81	6.96	7.11	7.28	7·45	7*63	7.83	8*c4	8.26	8·50
25	6.24	6·35	6·47	6·60	6•73	6.87	7.01	7.17	7.33	7·51	7*69	7.89	8*10	8.33	8·57
26	6·29	6·41	6·53	6.65	6·78	6·92	7°07	7:23	7°39	7.57	7·76	7.96	8·17	8·40	8.64
27	6·35	6·46	6·58	6.71	6·84	6·98	7°13	7:29	7°46	7.64	7·83	8.03	8·24	8·47	8.72
28	6·41	6·52	6·64	6.77	6·91	7·05	7°20	7:36	7°53	7.71	7·90	8.10	8·32	8·55	8.80
29	6·47	6·58	6·71	6.83	6·97	7·11	7°27	7:43	7°60	7.78	7·97	8.18	8·40	8·63	8.88
30	6·53	6·65	6·77	6.90	7·04	7·19	7°34	7:50	7°67	7.86	8·05	8.26	8·48	8·72	8.97
31	6.60	6·72	6·84	6·97	7'11	7·26	7'42	7:58	7°75	7'94	8.14	8·35	8·57	8.81	9.06
32	6.67	6·79	6·92	7·05	7'19	7·34	7'49	7:66	7°84	8 02	8.22	8·43	8·66	8.90	9.16
33	6.74	6·87	6·99	7·13	7'27	7·42	7'58	7:75	7°93	8'11	8.32	8·53	8·76	9.00	9.26
34	6.82	6·95	7·07	7·21	7'35	7·51	7'67	7:84	8°02	8'21	8.41	8·63	8·86	9.10	9.37
35	6.91	7·03	7·16	7·30	7'44	7·60	7'7 6	7:93	8°11	8'31	8.51	8·73	8·97	9.21	9.48
36	6·99	7'12	7°25	7'39	7°54	7.69	7·86	8.03	8·22	8*41	8.62	8·84	9°08	9°33	9.60
37	7·08	7'21	7'34	7'49	7°63	7.79	7·96	8.14	8·32	8*52	8.73	8·96	9°20	9°45	9.72
38	7·18	7'31	7'44	7'59	7°74	7.90	8·07	8.24	8·43	8*64	8.85	9·08	9°32	9°58	9.86
39	7·28	7'41	7'55	7'69	7°85	8.01	8·18	8.36	8·55	8*76	8.97	9·20	9°45	9°71	9.99
40	7·38	7'52	7'66	7'80	7°96	8.12	8·30	8.48	8·68	8*88	9.10	9·34	9°59	9°85	10.14
41	7°50	7.63	7°77	7'92	8.08	8·25	8·42	8.61	8·81	9.02	9°24	9'48	9'73	10.00	10°29
42	7°61	7.75	7°89	8'04	8.20	8·37	8·55	8.74	8·94	9.16	9°38	9'63	9'88	10.16	10°45
43	7°73	7.87	8°02	8'17	8.34	8·51	8·69	8.88	9·09	9.30	9°54	9'78	10'04	10.32	10°62
44	7°86	8.00	8°15	8'31	8.48	8·65	8·84	9.03	9·24	9.46	9°69	9'94	10'21	10.49	10°80
45	8°00	8.14	8°29	8'45	8.62	8·80	8·99	9.19	9·40	9.62	9°86	10'12	10'39	10.67	10°98
46	8·14	8·29	8·44	8.61	8·78	8·96	9'15	9°35	9.57	9.80	10°04	10'30	10°57	10.87	11·18
47	8·29	8·44	8·60	8.77	8·94	9·12	9'32	9°53	9.75	9.98	10°23	10'49	10°77	11.07	11·39
48	8·45	8·61	8·77	8.93	9·11	9·30	9'50	9°71	9.93	10.17	10°42	10'69	10°97	11.25	11·61
49	8·62	8·78	8·94	9.11	9·29	9·49	9'69	9°90	10.13	10.37	10°63	10'90	11°19	11.51	11·84
50	8·80	8·96	9·12	9.30	9·49	9·68	9'89	10°11	10.34	10.59	10°85	11'13	11°43	11.74	12·08
51	8·99	9.15	9°32	9'50	9.69	9.89	10'10	10.30	10.26	10.81	11.08	11.37	11.67	11.99	12·34
52	9·19	9.35	9°53	9'71	9.90	10.11	10'32	10.22	10.80	11.05	11.33	11.62	11.93	12.26	12·61
53	9·40	9.57	9°75	9'93	10.13	10.34	10'56	10.80	11.04	11.31	11.59	11.89	12.20	12.54	12·90
54	9·62	9.80	9°98	10'17	10.37	10.59	10'81	11.02	11.31	11.58	11.86	12.17	12.50	12.84	13·21
55	9·86	10.04	10°23	10'42	10.63	10.85	11'08	11.33	11.59	11.86	12.16	12.47	12.80	13.16	13·54
56 57 58 59 60	10°12 10°39 10°67 10°98 11°31	10'30 10'57 10`87 11'18 11'52	10'49 10'77 11'07 11'39 11'73	10°69 10°97 11°28 11°61 11°96	10'90 11'19 11'51 11'84 12'19	11.13 11.43 11.74 12.08 12.45	11°37 11°67 11°99 12°34 12°71	11.62 11.92 12.26 12.61 12.99	11.89 12.20 12.54 12.90 13.29	12.17 12.49 12.84 13.21 13.61	12'47 12'80 13'16 13'54 13'95	12.79 13.13 13.50 13.89 14.31	13.13 13.48 13.86 14.26 14.69	13°50 13°86 14°24 14°66 15°10	13 ^{.89} 14 ^{.26} 14 ^{.66} 15 ^{.08}

To convert time into longitude divide by 4. Thus $12 \circ s$. $\div 4 = 3'$ long.

Table D.

Showing the Error produced in the Time or Longitude by an Error of i' in the Altitude.

							AZ	IMUTI	is.						
Lat.	30°	292	230	27 °	26°	25°	24 °	23°	22°	21 °	20 °	19°	1 8 °	17°	160
° 0 1 2 3 4 5	s. 8.00 8.00 8.00 8.01 8.02 8.03	s. 8·25 8·25 8·26 8·26 8·27 8·28	s. 8*52 8*53 8*53 8*53 8*54 8*55	s. 8*81 8*81 8*82 8*82 8*83 8*83 8*84	s. 9'12 9'13 9'13 9'14 9'15 9'16	s. 9'46 9'47 9'47 9'48 9'49 9'50	s. 9*83 9*84 9*84 9*85 9*86 9*87	s. 10°2 10°2 10°3 10°3 10°3	s. 10'7 10'7 10'7 10'7 10'7	S. 11'2 11'2 11'2 11'2 11'2 11'2	s. 11.7 11.7 11.7 11.7 11.7 11.7	s. 12°3 12°3 12°3 12°3 12°3 12°3	s. 13.0 13.0 13.0 13.0 13.0 13.0	s. 13'7 13'7 13'7 13'7 13'7 13'7	s. 14·5 14·5 14·5 14·5 14·5 14·5 14·6
6 7 8 9 10	8.04 8.06 8.08 8.10 8.12	8.30 8.31 8.33 8.35 8.38	8.57 8.58 8.60 8.63 8.65	8.86 8.88 8.90 8.92 8.95	9'17 9'19 9'21 9'24 9'27	9.52 9.54 9.56 9.58 9.61	9.89 9.91 9.93 9.96 9.99	10.3 10.3 10.4 10.4	10.2 10.8 10.8 10.8 10.8	11.3 11.3 11.3	11.8 11.8 11.8 11.8 11.8	12°4 12°4 12°4 12°4 12°4 12°5	13.0 13.1 13.1 13.1	13.8 13.8 13.8 13.9 13.9	14.6 14.6 14.7 14.7 14.7
11 12 13 14 15	8.15 8.18 8.21 8.24 8.28	8.41 8.43 8.47 8.50 8.54	8.68 8.71 8.74 8.78 8.82	8.98 9.01 9.04 9.08 9.12	9°30 9°33 9°36 9°40 9°45	9.64 9.68 9.71 9.75 9.80	10.0 10.1 10.1 10.2	10.4 10.5 10.5 10.6 10.6	11.1 11.0 11.0 10.0 10.3	11.4 11.4 11.5 11.5 11.6	11.9 12.0 12.1 12.1 12.1	12.5 12.6 12.6 12.7 12.7	13.2 13.2 13.3 13.3 13.4	13.9 14.0 14.0 14.1 14.2	14.8 14.8 14.9 15.0 15.0
16 17 18 19 20	8·32 8·37 8·41 8·46 8·51	8.58 8.63 8.68 8.73 8.73 8.78	8.86 8.91 8.90 8.91	9.17 9.21 9.26 9.32 9.38	9'49 9'54 9'59 9'65 9'71	9.85 9.90 9.95 10.0 10.1	10.2 10.3 10.3 10.4 10.5	10.6 10.7 10.8 10.8 10.9	11.1 11.2 11.3 11.4	11.6 11.7 11.7 11.8 11.9	12°2 12°2 12°3 12°4 12°4	12.8 12.9 13.0 13.1	13.2 13.2 13.6 13.7 13.8	14·2 14·3 14·4 14·5 14·6	15°1 15°2 15°3 15°3 15°4
21 22 23 24 25	8.57 8.63 8.69 8.76 8.83	8.84 8.90 8.96 9.03 9.10	9.13 9.19 9.26 9.33 9.40	9*44 9*50 9*57 9*64 9*72	9.77 9.84 9.91 9.99 10.1	10'1 10'2 10'3 10'4 10'4	10.2 10.6 10.7 10.8 10.9	11.3 11.1 11.0 11.0	11.4 11.2 11.6 11.7 11.8	12.0 12.0 12.1 12.2 12.3	12.5 12.6 12.7 12.8 12.9	13.2 13.3 13.3 13.4 13.6	13.9 14.0 14.1 14.2 14.3	14.7 14.8 14.9 15.0 15.1	15.5 15.7 15.8 15.9 16.0
26 27 28 29 30	8.90 8.98 9.06 9.15 9.24	9°18 9°26 9°34 9°43 9°53	9*48 9*56 9*65 9*74 9*84	9.80 9.89 9.98 10.1 10.2	10.2 10.2 10.3 10.4 10.5	10.2 10.0 10.2 10.8 10.8	10'9 11'0 11'1 11'2 11'4	11.4 11.5 11.6 11.7 11.8	11.9 12.0 12.1 12.3	12'4 12'5 12'6 12'8 12'9	13.0 13.1 13.2 13.4 13.5	13.7 13.8 13.9 14.0 14.2	14°4 14°5 14°7 14°8 14°9	15°2 15°3 15°5 15°6 15°8	16.1 16.3 16.4 16.6 16.8
31 32 33 34 35	9°33 9°43 9°54 9°55 9°77	9.63 9.73 9.84 9.95 10.1	9'94 10'0 10'2 10'3 10'4	10'3 10'4 10'5 10'6 10'8	11.1 11.0 10.8 10.6	11.0 11.2 11.3 11.4 11.6	11°5 11°6 11°7 11°9 12°0	11.9 12.1 12.3 12.3	12.5 12.6 12.7 12.9 13.0	13.0 13.2 13.3 13.6	13.6 13.8 14.0 14.1 14.3	14°3 14°5 14°6 14°8 15°0	15.1 15.3 15.4 15.6 15.8	16.0 16.1 16.3 16.5 16.7	16.9 17.1 17.3 17.5 17.7
36 37 38 39 40	9.89 10.0 10.2 10.3 10.4	10°2 10°3 10°5 10°6 10°8	10'5 10'7 10'8 11'0 11'1	10'9 11'0 11'2 11'5	11.3 11.4 11.6 11.7 11.9	11.7 11.9 12.0 12.2 12.4	12°2 12°3 12°5 12°7 12°8	12.7 12.8 13.0 13.2 13.4	13.2 13.4 13.6 13.7 13.7	13.8 14.0 14.2 14.4 14.6	14°5 14°6 14°8 15°0 15°3	15°2 15°4 15°6 15°8 16°0	16.0 16.2 16.4 16.7 16.9	16.9 17.1 17.4 17.6 17.9	17.9 18.2 18.4 18.7 18.9
41 42 43 44 45	10.0 10.8 10.9 11.1 11.3	10.9 11.1 11.3 11.5 11.7	11°3 11°5 11°6 11°8 12°0	11.7 11.9 12.0 12.2 12.5	12'1 12'3 12'5 12'7 12'9	12'5 12'7 12'9 13'2 13'4	13.0 13.2 13.4 13.7 13.9	13.6 13.8 14.0 14.2 14.5	14°1 14°4 14°6 14°8 15°1	14.8 15.0 15.3 15.5 15.8	15°5 15°7 16°0 16°3 16°5	16·3 16·5 16·8 17·1 17·4	17°2 17°4 17°7 18°0 18°3	18.1 18.4 18.7 19.0 19.3	19 ^{.2} 19 ^{.5} 19 ^{.8} 20 ^{.2} 20 ^{.5}
46 47 48 49 50	11.5 11.7 12.0 12.2 12.4	11.9 12.1 12.3 12.6 12.8	12°3 12°5 12°7 13°0 13°3	12.7 12.9 13.2 13.4 13.7	13'1 13'4 13'6 13'9 14'2	13.6 13.9 14.1 14.4 14.7	14.2 14.4 14.7 15.0 15.3	14.7 15.0 15.3 15.6 15.9	15.4 15.7 16.0 16.3 16.6	16·1 16·4 16·7 17·0 17·4	16.8 17.1 17.5 17.8 18.2	17.7 18.0 18.4 18.7 19.1	18.6 19.0 19.3 19.7 20.1	19'7 20'1 20'4 20'9 21'3	20'9 21'3 21'7 22'1 22'6
51 52 53 54 55	12.7 13.0 13.3 13.6 13.9	13'1 13'4 13'7 14'0 14'4	13.5 13.8 14.2 14.5 14.9	14.0 14.3 14.6 15.0 15.4	14°5 14°8 15°2 15°5 15°9	15.0 15.4 15.7 16.1 16.5	15.6 16.0 16.3 16.7 17.1	16·3 16·6 17·0 17·4 17·8	17.0 17.3 17.7 18.2 18.6	17'7 18'1 18'5 19'0 19'5	18.6 19.0 19.4 19.9 20.4	19'5 20'0 20'4 20'9 21'4	20°6 21°0 21°5 22°0 22°6	21.7 22.2 22.7 23.3 23.9	23·1 23·6 24·1 24·7 25·3
56 57 58 59 60	14'3 14'9 15'1 15' 5 16'0	14.8 15.1 15.6 16.0 16.5	15°2 15°6 16°1 16°5 17°0	15.8 16.2 16.6 17.1 17.6	16·3 16·8 17·2 17·7 18·2	16.9 17.4 17.9 18.4 18.9	17.6 18.1 18.6 19.1 19.7	18.3 18.8 19.3 19.9 20.5	19'1 19'6 20'1 20'7 21'4	20°0 20°5 21°1 21°7 22°3	20'9 21'5 22'1 22'7 23'4	22.0 22.6 23.2 23.9 24.6	23'I 23'8 24'4 25'1 25'9	24°5 25°1 25°8 26°6 27°4	26°0 26°4 27°4 28°2 29°0

To convert time into longitude divide by 4. Thus 16 s. $\div 4 = 4'$ long.

SHOWING THE ERROR PRODUCED IN THE TIME OR LONGITUDE BY AN ERROR OF I' IN THE ALTITUDE.

Lat							ΑZ	IMUTI	is.						
Lia.e.	15°	14°	13°	12°	11°	10°	9°	3 °	7°	6°	5°	4 °	30	2°	1°
° 0 1 2 3 4 5	s. 15 [.] 4 15 [.] 5 15 [.] 5 15 [.] 5 15 [.] 5	s. 16·5 16·5 16·6 16·6 16·6	s. 17·8 17·8 17·8 17·8 17·8 17·8	s. 19.2 19.3 19.3 19.3 19.3 19.3	S. 21.0 21.0 21.0 21.0 21.0 21.0 21.0	s. 23.0 23.0 23.0 23.1 23.1 23.1	s. 25.6 25.6 25.6 25.6 25.6 25.6 25.7	s. 28.7 28.7 28.8 28.8 28.8 28.8 28.9	s. 32.8 32.8 32.8 32.9 32.9 32.9 32.9	s. 38·3 38·3 38·3 38·3 38·3 38·4 38·4	s. 45°9 45°9 45°9 46°0 46°0 46°1	s. 57°4 57°4 57°4 57°4 57°5 57°6	s. 76·4 76·4 76·5 76·5 76·6 76·7	s. 115 115 115 115 115 115	 S. 229 229 229 230 230 230 230
6 7 8 9 10	15.5 15.6 15.6 15.6 15.7	16.6 16.7 16.7 16.7 16.8	17.9 17.9 18.0 18.0 18.1	19.3 19.4 19.4 19.5 19.5	21'1 21'1 21'2 21'2 21'3 21'4	23·2 23·2 23·3 23·3 23·4	25.7 25.8 25.8 25.9 26.0	28·9 29·0 29·0 29·1 29·2	33.0 33.1 33.1 33.2 33.3	38.5 38.6 38.6 38.7 38.9	46.1 46.2 46.3 46.5 46.6	57°7 57°8 57°9 58°1 58°2	76·9 77·0 77·2 77·4 77·6	115 115 116 116 116	230 231 231 232 233
12 13 14 15	15.8 15.9 15.9 16.0	16·9 17·0 17·0 17·1	18.2 18.2 18.3 18.4	19.7 19.7 19.8 19.9	21.4 21.5 21.6 21.7	23.5 23.6 23.7 23.8	26°0 26°1 26°2 26°4 26°5	29'3 29'4 29'5 29'6 29'8	33.6 33.7 33.8 34.0	39°3 39°3 39°4 39°6	40.0 46.9 47.1 47.3 47.5	58.6 58.9 59.1 59.4	77 9 78·1 78·4 78·8 79·1	117 117 118 118 119	233 234 235 236 237
10 17 18 19 20	16.1 16.2 16.3 16.4	17 2 17 3 17 4 17 5 17 6	18.5 18.6 18.7 18.8 18.9	20°1 20°2 20°3 20°5	21 0 21.9 22.0 22.2 22.3	24 0 24 1 24 2 24 2 24 4 24 5	20 0 26·7 26·9 27·0 27·2	29 9 30·1 30·2 30·4 30·6	34 1 34 3 34 5 34 7 34 9	39°8 40°0 40°2 40°5 40°7	47.7 48.0 48.3 48.5 48.8	59.7 60.0 60.3 60.6 61.0	79 [•] 5 79 [•] 9 80 [•] 4 80 [•] 8 81 [•] 3	119 120 121 121 122	238 240 241 242 244
21	10.0	17.7	19.0	20.0	22.5	24.7	27°4	30.8	35°2	41.0	49°2	61.4	81·9	123	246
22	16.7	17.8	19.2	20.7	22.6	24.8	27°6	31.0	35°4	41.3	49°5	61.8	82·4	124	247
23	16.8	18.0	19.3	20.9	22.8	25.0	27°8	31.2	35°7	41.6	49°9	62.3	83·0	125	249
24	16.9	18.1	19.5	21.1	22.9	25.2	28°0	31.5	35°9	41.9	50°2	62.8	83·7	125	251
25	17.1	18.2	19.6	21.2	23.1	25.4	28°2	31.7	36°2	42.2	50°6	63.3	84·3	126	253
26	17°2	18.4	19°8	21.4	23·3	25.6	28.4	32.0	36.5	42°6	51.1	63.8	85°0	128	255
27	17°3	18.6	20°0	21.6	23·5	25.8	28.7	32.3	36.8	42°9	51.5	64.4	85°8	129	257
28	17°5	18.7	20°1	21.8	23·7	26.1	29.0	32.6	37.2	43°3	52.0	64.9	86°6	130	260
29	17°7	18.9	20°3	22.0	24·0	26.3	29.2	32.9	37.5	43°8	52.5	65.6	87°4	131	262
30	17°8	19.1	20°5	22.2	24·2	26.6	29.5	33.2	37.9	44°2	53.0	66.2	88°3	132	265
31	18.0	19'3	20'7	22.4	24°5	26 ·9	29.8	33°5	38°3	44°6	53°5	66·9	89°2	134	267
32	18.2	19'5	21'0	22.7	24°7	27·2	30.2	33°9	38°7	45°1	54°1	67·6	90°1	135	270
33	18.4	19'7	21'2	22.9	25°0	27·5	30.5	34°3	39°1	45°6	54°7	68·4	91°1	137	273
34	18.6	19'9	21'4	23.2	25°3	27·8	30.8	34°7	39°6	46°2	55°4	69·2	92°2	138	276
35	18.9	20'2	21'7	23.5	25°6	28·1	31.2	35°1	40°1	46°7	56°0	70·0	93°3	140	280
36	19°1	20'4	22.0	23.8	25.9	28.5	31.6	35 ^{.5}	40.6	47'3	56.7	70'9	94 [•] 5	142	283
37	19°4	20'7	22.3	24.1	26.2	28.8	32.0	36 ^{.0}	41.1	47'9	57.5	71'8	95 [•] 7	144	287
38	19°6	21'0	22.6	24.4	26.6	29.2	32.4	36 ^{.5}	41.7	48'6	58.2	72'8	97 [•] 0	145	291
39	19°9	21'3	22.9	24.8	27.0	29.6	32.9	37 ^{.0}	42.2	49'2	59.1	73'8	98 [•] 3	147	295
40	20°2	21'6	23.2	25.1	27.4	30.1	33.4	37 ^{.5}	42.8	50'0	59.9	74'9	99 [•] 8	150	299
41	20°5	21.9	23.6	25.5	27 ^{.8}	30°5	33°9	38.1	43 ^{.5}	50.7	60·8	76.0	101	152	304
42	20°8	22.2	23.9	25.9	28 [.] 2	31°0	34°4	38.7	44 ^{.2}	51.5	61·8	77.2	103	154	308
43	21°1	22.6	24.3	26.3	28 [.] 7	31°5	35°0	39.3	44 ^{.9}	52.3	62·8	78.4	105	157	313
44	21°5	23.0	24.7	26.7	29 [.] 1	32°0	35°5	40.0	45 ^{.6}	53.2	63·8	79.7	106	159	319
45	21°9	23.4	25.1	27.2	29 [.] 6	32°6	36°2	40.6	46 [.] 4	54.1	64·9	81.1	108	162	324
46	22·2	23.8	25.6	27'7	30°2	33·2	36.8	41°4	47 ^{•2}	55°1	66·1	82°5	110	165	330
47	22·7	24.2	26.1	28'2	30°7	33·8	37.5	42°1	48 ^{•1}	56°1	67·3	84°1	112	168	336
48	23·1	24.7	26.6	28'8	31°3	34·4	38.2	43°0	49 ^{•1}	57°2	68·6	85°7	114	171	343
49	23·6	25.2	27.1	29'3	32°0	35·1	39.0	43°8	50 ^{•0}	58°3	70·0	87°4	116	175	349
50	24·0	25.7	27.7	29'9	32°6	35·8	39.8	44°7	51 ^{•1}	59°5	71·4	89°2	119	178	357
51 53 53 54 55	24.6 25.1 25.7 26.3 26.9	26·3 26·9 27·5 28·1 28·8	28·3 28·9 29·5 30·3 31·0	30.6 31.2 32.0 32.7 33.5	33°3 34°1 34°8 35°7 36°5	36.6 37.4 38.3 39.2 40.2	40.6 41.5 42.5 43.5 44.6	45°7 46°7 47°8 48°9 50°1	52·2 53·3 54·5 55·8 57·2	60.8 62.2 63.6 65.1 66.7	72.9 74.5 76.3 78.1 80.0	91.1 93.1 92.3 97.6	121 124 127 - 130 133	182 186 190 195 200	364 372 381 390 400
56	27.6	29.6	31.8	34°4	37°5	41.2	45°7	51.4	58.7	68.4	82.1	102°5	137	205	410
57	28.4	30.4	32.6	35°3	38°5	42.3	46°9	52.8	60.3	70.3	84.3	105°3	140	210	421
58	29.2	31.2	33.6	36°3	39°6	43.5	48°3	54.2	61.9	72.2	86.6	108°2	144	216	432
59	30.0	32.1	34.5	37°4	40°7	44.7	49°6	55.8	63.7	74.3	89.1	111°3	148	223	445
60	30.9	33.1	35.6	38°5	41°9	46.1	51°1	57.5	65.6	76.5	91.8	114°7	153	229	458

To convert time into longitude divide by 4. Thus $35.6 \text{ s.} \div 4 = 8.9' \text{ long.}$

:

6-Azimuth

82

Table D.

ALTITUDE.

ths.							LATIT	UDES.							
Azimı	61 °	62°	63°	64°	65°	66°	67°	68°	69°	70 °	71°	72°	73 °	74°	75°
0 0 1 1 1 2 2 1 2	s. 945 473 315 236 189	s. 976 488 325 244 195	s. 1010 505 337 252 202	s. 1046 523 349 262 209	s. 1085 542 362 271 217	s. 1127 563 376 282 225	s. 1173 5 ⁸ 7 391 293 235	s. 1224 612 408 306 245	s. 1279 640 426 320 256	s. 1340 670 447 335 268	s. 1408 704 469 352 282	s. 1483 742 495 371 297	s. 1568 784 523 392 314	s. 1663 832 554 416 333	s. 1771 886 590 443 354
3	158	163	168	174	181	188	196	204	213	223	235	247	261	277	295
32	135	140	144	150	155	161	168	175	183	192	201	212	224	237	253
4	118	122	126	131	136	141	147	153	160	168	176	186	196	208	222
4	105	109	112	116	121	125	130	136	142	149	157	165	174	185	197
5	94°7	97 ^{.8}	101	105	109	113	117	123	128	134	141	149	157	167	177
51 6 6 7 7 7	86°1 79°1 72°9 67°7 63°2	88.9 81.5 75.3 69.9 65.3	91.9 84.3 77.8 72.3 67.5	95°2 87°3 80°6 74°9 69°9	98.8 90.5 83.6 77.7 72.5	103 94.1 86.9 80.7 75 .3	107 97'9 90'4 84'0 78'4	111 102 94 [.] 3 87 [.] 6 81 [.] 8	116 107 98.6 91.6 85.5	122 112 103 96°0 89°6	128 118 109 101 94°1	135 124 114 106 99°2	143 131 121 112 105	151 139 128 119 111	161 148 137 127 118
8 81 9 91 92 10	59°3 55°8 52°7 50°0 47°5	61·2 57·6 54·5 51·6 49·1	63·3 59·6 56·3 53·4 50·7	65.6 61.7 58.3 55.3 52.6	68.0 64.0 60.5 57.3 54.5	70 [.] 7 66 [.] 5 62 [.] 9 59 [.] 6 56 [.] 6	73.6 69.3 65.4 62.0 59.0	76.7 72.2 68.3 64.7 61.5	80 ^{.2} 75 ^{.5} 71 ^{.4} 67 ^{.6} 64 ^{.3}	84.0 79.1 74.8 70.9 67.4	88.3 83.1 78.5 74.4 70.8	93.0 87.6 82.7 78.4 74.5	98·3 92·6 87·5 82·9 78·8	104 98.2 92.8 87.9 83.6	111 105 98·8 93·6 89·0
$ 10\frac{1}{2} 11 11\frac{1}{2} 12 12\frac{1}{2} 12\frac{1}{2} $	45°3	46.8	48·3	50'1	51'9	54°0	56.2	58.6	61·2	64·2	67°4	71.0	75°1	79°6	84.8
	43°2	44.7	46·2	47'8	49'6	51°5	53.7	56.0	58·5	61·3	64°4	67.8	71°7	76°1	81.0
	41°4	42.7	44·2	45'8	47'5	49°3	51.3	53.6	56·0	58·7	61°6	64.9	68°6	72°8	77.5
	39°7	41.0	42·4	43'9	45'5	47°3	49.2	51.4	53·7	56·3	59°1	62.3	65°8	69°8	74.3
	38°1	39.4	40·7	42'2	43'7	45°4	47.3	49.3	51·6	54·0	56°8	59.8	63°2	67°0	71.4
$ \begin{array}{r} 13 \\ 13\frac{1}{2} \\ 14 \\ 14\frac{1}{2} \\ 15 \\ \end{array} $	36.7	37 ^{.9}	39°2	40.6	42'1	43'7	45°5	47 ^{.5}	49 ^{.6}	52°0	54°6	57°5	60.8	64 [.] 5	68·7
	35.3	36 ^{.5}	37°7	39.1	40'5	42'1	43°9	45 ^{.7}	47 ^{.8}	50°1	52°6	55°4	58.6	62 [.] 2	66·2
	34.1	35 ^{.2}	36°4	37.7	39'1	40'7	42°3	44 ^{.1}	46 ^{.1}	48°3	50°8	53°5	56.6	60 [.] 0	63·9
	33.0	34 ^{.0}	35°2	36.4	37'8	39'3	40°9	42 ^{.6}	44 ^{.6}	46°7	49°1	51°7	54.6	58 [.] 0	61·7
	31.9	32 ^{.9}	34°0	35.3	36'6	38'0	39°6	41 ^{.3}	43 ^{.1}	45°2	47°5	50°0	52.9	56 [.] 1	59·7
15 ¹	30.9	31.9	33.0	34°1	35'4	36·8	38·3	40°0	41.8	43 ^{.8}	46°0	48.4	51.2	54°3	57 ^{.8}
16	29.9	30.9	32.0	33°1	34'3	35·7	37·1	38°7	40.5	4 ^{2.4}	44°6	47.0	49.6	52°6	56 ^{.1}
16 ¹	29.1	30.0	31.0	32°1	33'3	34·6	36·0	37°6	39.3	4 ^{1.2}	43°3	45.6	48.2	51°1	54 ^{.4}
17	28.2	29.1	30.1	31°2	32'4	33·6	35·0	36°5	38.2	40 ^{.0}	42°0	44.3	46.8	49°6	5 ^{2.9}
17 ¹	27.4	28.3	29.3	30°3	31'5	32·7	34·0	35°5	37.1	38 ^{.9}	40°9	43.0	45.5	48°3	5 ^{1.4}
18	26.7	27.6	28·5	29.5	30 .6	31.8	33 ^{.1}	34.6	36.1	37 ^{.8}	39·8	41.9	44'3	47 ^{.0}	50°0
18 <u>1</u>	26.0	26.9	27·8	28.8	29.8	31.0	3 ² .3	33.7	35.2	36 ^{.9}	3 ⁸ ·7	40.8	43'1	45 ^{.7}	48°7
19	25.3	26.2	27·1	28.0	29.1	30.2	3 ¹ .4	32.8	34.3	35 ^{.9}	37·7	39.8	42'0	44 ^{.6}	47°5
191	24.7	25.5	26·4	27.3	28.4	29.5	3 ⁰ .7	32.0	33.4	35 ^{.0}	36·8	38.8	41'0	43 ^{.5}	46°3
20	24.1	24.9	25·8	26.7	27.7	28.8	29.9	31.2	32.6	34 ^{.2}	35·9	37.8	40'0	4 ^{2.4}	45°2
$20\frac{1}{2}$ 21 21 $\frac{1}{2}$ 22 22 22 $\frac{1}{2}$	23.6	24·3	25°2	26'1	27'0	28·1	29 °2	30 .5	31.9	33'4	35'I	37.0	39'1	41'4	44'I
	23.0	23·8	24°6	25'5	26'4	27·4	28°6	29.8	31.1	32'6	34'3	36.1	38'2	40'5	43'I
	22.5	23·2	24°0	24'9	25'8	26·8	27°9	29.1	30.5	31'9	33'5	35.3	37'3	39'6	42'2
	22.0	22·7	23°5	24'4	25'3	26·3	27°3	28.5	29.8	31'2	32'8	34.6	36'5	3 ⁸ '7	41'3
	21.6	22·3	23°0	23'8	24'7	25·7	26°8	27.9	29.2	30'6	32'I	33.8	35'8	37'9	40'4
23	21°1	21.8	22.5	23'3	24·2	25°2	26°2	27.3	28.6	29 '9	31'4	33°1	35°0	37°1	39.6
232	20°7	21.4	22.1	22'9	23·7	24°7	25°7	26.8	28.0	29'3	30'8	32°5	34°3	36°4	38.8
24	20°3	20.9	21.7	22'4	23·3	24°2	25°2	26.3	27.4	28'8	30'2	31°8	33°6	35°7	38.0
242	19°9	20.5	21.2	22'0	22·8	23°7	24°7	25.7	26.9	28'2	29'6	31°2	33°0	35°0	37.3
25	19°5	20.2	20.8	21'6	22·4	23°3	24°2	25.3	26.4	27'7	29'1	30°6	32°4	34°3	36.6
25 ¹ 26 26 ¹ 27 27 ¹ 27 ¹	19°2 18°8 18°5 18°2 17°9	19 [.] 8 19 [.] 4 19 [.] 1 18 [.] 8 18 [.] 5	20.5 20.1 19.7 19.4 19.1	21°2 20°8 20°4 20°1 19°8	22.0 21.6 21.2 20.8 20.5	22.8 22.4 22.0 21.7 21.3	23.8 23.4 22.9 22.5 22.2	24.8 24.4 23.9 23.5 23.1	25.9 25.5 25.0 24.6 24.2	27 ² 26 ⁷ 26 ² 25 ⁸ 25 ³	28.5 28.0 27.5 27.1 26.6	30°1 29°5 29°0 28°5 28°0	31.8 31.2 30.7 30.1 29.6	33'7 33'1 32'5 32'0 31'4	* 35*9 35*3 34*6 34*0 33*5
28	17.6	18·1	18·8	19.4	20°2	20'9	21.8	22.7	23.8	24 [.] 9	26·2	27.6	29 [•] 1	30'9	32.9
28 <u>1</u>	17.3	17·9	18·5	19.1	19°8	20'6	21.5	22.4	23.4	24 [.] 5	25·7	27.1	28 [•] 7	30'4	32.4
29	17.0	17·6	18·2	18.8	19°5	20'3	21.1	22.0	23.0	24 [.] 1	25·3	26.7	28 [•] 2	29'9	31.9
29 <u>1</u>	16.8	17·3	17·9	18.5	19°2	20'0	20.8	21.7	22.7	23 [.] 8	25·0	26.3	27 [•] 8	29'5	31.4
30	16.5	17·0	17·6	18.2	18°9	19'7	20.5	21.4	22.3	23 [.] 4	24·6	25.9	27 [•] 4	29'0	30.9

To convert time into longitude divide by 4. Thus $29^{\circ}2s. \div by 4 = 7^{\circ}3'$ longitude.

Showing the Error produced in the Time or Longitude by an Error of 1' in the ALTITUDE.

uths.							LATIT	UDES.							
Azim	76°	77 °	78°	79°	80°	8 0½°	81 °	$81\frac{1}{2}^{\circ}$	82°	$82^{1\circ}_{2}$	83 °	83 ¹⁰ /2	8 4 °	84 ¹ / ₂ °	85°
$ \begin{array}{c} 0 \\ 0 \\ 1 \\ 1 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2$	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.
	1895	2038	2205	2402	2640	2777	2930	3101	3294	3512	3761	4049	4385	4782	5259
	947	1019	1102	1201	1320	1389	1466	1551	1647	1756	1881	2025	2193	2391	2630
	632	679	735	801	880	926	977	1034	1098	1171	1254	1350	1462	1594	1753
	474	510	551	601	660	694	733	775	824	878	940	1012	1096	1193	1315
	379	408	441	481	528	556	586	620	659	703	752	810	877	957	1052
3	316	340	368	401	440	463	489	517	549	586	627	675	731	797	877
3 ¹ 2	271	291	315	343	377	397	419	443	471	502	538	579	627	684	752
4	237	255	276	301	330	347	367	388	412	439	471	507	549	598	658
4 ¹ 2	211	227	245	267	294	309	326	345	366	391	418	450	488	532	585
5	190	204	221	241	2 64	278	293	310	330	352	377	405	439	479	527
$5\frac{1}{2} \\ 6\\ 6\frac{1}{2} \\ 7\\ 7\frac{1}{2} \\ 7$	173	186	201	219	240	253	267	282	300	320	342	369	399	435	479
	158	170	184	201	220	232	245	259	275	293	314	338	366	399	439
	146	157	170	185	203	214	226	239	254	27 I	290	312	338	369	405
	136	146	158	172	189	199	210	222	236	25 I	269	290	314	343	377
	127	136	147	161	176	186	196	207	220	235	251	271	293	320	352
8	119	128	138	151	166	174	184	194	207	220	236	254	275	300	330
8 <u>1</u>	112	120	130	142	156	164	173	183	194	207	222	239	259	282	311
9	106	114	123	134	147	155	163	173	184	196	210	226	245	267	293
91	100	108	117	127	140	147	155	164	174	186	199	214	232	253	278
10	95 [.] 2	102	111	121	133	140	147	156	166	176	189	203	220	240	264
$10\frac{1}{2}$ II	90°7	97.6	106	115	126	133	140	148	158	168	180	194	210	229	252
	86'7	93.2	101	110	121	127	134	142	151	161	172	185	201	219	241
	82'9	89.2	96 [.] 5	105	116	122	128	136	144	154	165	177	192	209	230
	79'5	85.5	92 [.] 5	101	111	117	123	130	138	147	158	170	184	201	221
	76'4	82.2	88 [.] 9	96.9	106	112	118	125	133	142	152	163	177	193	212
$13 \\ 13\frac{1}{2} \\ 14 \\ 14\frac{1}{2} \\ 15 $	73 [•] 5	79 ^{.0}	85 [.] 5	93 ^{.2}	102	108	114	120	128	136	146	157	170	186	204
	70 [•] 8	76 [.] 2	82 [.] 4	89 ^{.8}	9 ^{8·7}	104	110	116	123	131	141	151	164	179	197
	68 [•] 3	73 [.] 5	79 [.] 5	86 ^{.7}	95·2	100	206	112	119	127	136	146	158	173	190
	66 [•] 0	71 ^{.0}	76 [.] 8	83 ^{.7}	92·0	96.8	102	108	115	122	131	141	153	167	183
	63 [•] 9	68 . 7	74 [.] 3	81 ^{.0}	89·0	93. 6	98.8	105	111	118	127	137	148	161	177
$15\frac{1}{2}$	61'9	66.5	72.0	78.4	86·2	90'7	95°7	101	108	115	123	132	143	156	172
16	60'0	64.5	69.8	76.0	83·6	87'9	92°8	98·2	104	111	119	128	139	151	167
16 $\frac{1}{2}$	58'2	62.6	67.7	73.8	81·1	85'3	90°0	95·3	101	108	116	124	135	147	161
17	56'6	60.8	65.8	71.7	78·8	82'9	87°5	92·6	98·3	105	112	121	131	143	157
17 $\frac{1}{2}$	55'0	59.1	64.0	69.7	76·6	80'6	85°0	90·0	95·6	102	109	118	127	139	153
18	53'5	57`5	62·3	67·8	74 [•] 5	78.4	82·7	87 ^{.6}	93.0	99.2	106	114	124	135	149
18 1	52'1	56•0	60·6	66·1	72 [•] 6	70.4	80·6	85 ^{.3}	90.6	96.6	103	111	121	132	145
19	50'8	54•6	59·1	64·4	70 [•] 8	74.4	78·5	83 ^{.1}	88.3	94.1	101	109	118	128	141
19 1	49'5	53•3	57·6	62·8	69 [•] 0	72.6	76·6	81 ^{.1}	86.1	91.8	98.3	106	115	125	137
20	48'3	52•0	56·3	61·3	67 [•] 4	70.9	74·8	79 ^{.1}	84.0	89.6	96.0	103	112	122	134
$ \begin{array}{c} 20\frac{1}{2} \\ 21 \\ 21\frac{1}{2} \\ 22 \\ 22\frac{1}{2} \end{array} $	47 ^{•2}	50.8	54 [.] 9	59 [.] 9	65·8	69·2	73 ^{.0}	77 [.] 3	82·1	87 ^{.5}	93'7	101	109	119	131
	46 [•] 1	49.6	53 [.] 7	58 [.] 5	64·3	67·6	71 [.] 4	75 [.] 5	80·2	85 ^{.5}	91'6	98.6	107	116	128
	45 [•] 1	48.5	5 ² [.] 5	57 [.] 2	62·9	66·1	69 ^{.8}	73 [.] 8	78·4	83 ^{.6}	89'6	96.4	104	114	125
	44 [•] 1	47.5	5 ^{1.} 4	5 ^{0.} 0	61·5	64·7	68 [.] 3	72 [.] 2	76·7	81 ^{.8}	87'6	94.3	102	111	123
	43 [•] 2	46.5	5 ^{0.} 3	54 [.] 8	60·2	63·3	66 ^{.8}	70 [.] 7	75 ^{·1}	80 ^{.1}	85'8	92.3	100	109	120
23	42°3	45 ^{.5}	49 [•] 2	53.7	59 ^{.0}	62.0	65.4	69·3	73.6	78.4	84.0	90.4	97'9	107	117
$23\frac{1}{2}$	41°5	44 ^{.6}	48 [•] 2	52.6	57 ^{.8}	60.8	64.1	67·9	72.1	76.9	82.3	88.6	96'0	105	115
24	40°7	43 ^{.7}	47 [•] 3	51.5	56 ^{.6}	59.6	62.9	66·5	70.7	75.3	80.7	86.9	94'1	103	113
$24\frac{1}{2}$	39°9	4 ^{2.9}	46 [•] 4	50.5	55 ^{.5}	58.4	61.7	65·3	69.3	73.9	79.1	85.2	92'3	101	111
25	39°1	42 ^{.1}	45 [•] 5	49.6	54 ^{.5}	57.3	60.5	64·0	68.0	72.5	77.7	83.6	90'5	98.8	109
$ \begin{array}{r} 25\frac{1}{2} \\ 26 \\ 26\frac{1}{2} \\ 27 \\ 27\frac{1}{2} \end{array} $	3 ⁸ ·4	41.3	44'7	48.7	53 ^{.5}	56·3	59 [.] 4	62 9	66·8	71.2	76·2	82·1	88.9	96.9	107
	37·7	40.6	43'9	47.8	52 ^{.5}	55·3	5 ^{8.} 3	61.7	65·6	69.9	74·9	80·6	87.3	95.2	105
	37·1	39.9	43'1	47.0	51 ^{.6}	54·3	57 [.] 3	60.6	64·4	68.7	73·6	79·2	85.8	93.5	103
	36·4	39.2	42'4	46.2	50 ^{.7}	53·4	5 ^{6.} 3	59.6	63·3	67.5	72·3	77·8	84.3	91.9	101
	35·8	38.5	41'7	45.4	49 ^{.9}	52·5	55 [.] 4	58.6	62·2	66.4	71·1	76·5	82.9	90.4	99'4
28	35 ^{.2}	37 ^{.9}	41.0	44 [.] 7	49 [•] 1	51.6	54°5	57'6	61°2	65.3	69 [.] 9	75'3	81.5	88.9	97 ^{.8}
$28\frac{1}{2}$	34 ^{.7}	37 ^{.3}	40.3	43 [.] 9	48 [•] 3	50.8	53°6	56'7	60°2	64.2	68 [.] 8	74'1	80.2	87.5	96 [.] 2
29	34 ^{.1}	36 ^{.7}	39.7	43 [.] 2	47 [•] 5	50.0	52°7	55'8	59°3	63.2	67 [.] 7	72'9	78.9	86.1	94 ^{.7}
$29\frac{1}{2}$	33 ^{.6}	36 ^{.1}	39.1	42 [.] 6	46 [•] 8	49.2	51°9	55'0	58°4	62.2	66 [.] 7	71'8	77.7	84.8	93 ^{.2}
3^{0}	33 ^{.1}	35 ^{.6}	38.5	41 [.] 9	46 [•] 1	48.5	51°1	54'1	57°5	61.3	65 [.] 6	70'7	76.5	83.5	91 ^{.8}

To convert time into longitude divide by 4. Thus $50.8s. \div by 4 = 12.7'$ longitude.

Showing the Error produced in the Time or Longitude by an Error of i' in the Altitude.

hs.							τı	TITUT	ES.						
imut												7010			
Αz	610	620	630	64.	65,	66.	575	683	630	0942	90 ³	40 ³ 0	419	7130	720
。 30 31 32 33 34	s. 16·5 16·0 15·6 15·1 14·8	s. 17°0 16°5 16°1 15°6 15°2	s. 17°6 17°1 16°6 16°2 15°8	s. 18·2 17·7 17·2 16·8 16·3	s. 18·9 18·4 17·9 17·4 16·9	s. 19·7 19·1 18·6 18·1 17·6	s. 20·5 19·9 19·3 18·8 18·3	s. 21°4 20°7 20°1 19°6 19°1	s. 22°3 21°7 21°1 20°5 20°0	s. 22*8 22*2 21*6 21*0 20*4	s. 23'4 22'7 22'1 21'5 20'9	s. 24.0 23.3 22.6 22.0 21.4	s. 24·6 23·9 23·2 22·6 22·0	s. 25°2 24°5 23°8 23°1 22°5	s. 25·9 25·1 24·4 23·8 23·1
35 36 37 3 ⁸ 39	14.4 14.0 13.7 13.4 13.1	14.9 14.5 14.2 13.8 13.5	15.4 15.0 14.6 14.3 14.0	15.9 15.5 15.2 14.8 14.5	16·5 16·1 15·7 15·4 15·0	17°1 16°7 16°3 16°0 15°6	17.8 17.4 17.0 16.6 16.3	18.6 18.2 17.7 17.3 17.0	19 •5 19•0 18•5 18•1 17•7	19·9 19·4 19·0 18·6 18·1	20'4 19'9 19'4 19'0 18'6	20'9 20'4 19'9 19'5 19'0	21°4 20°9 20°4 20°0 19°5	22°0 21°4 20°9 20°5 20°0	22.6 22.0 21.5 21.0 20.6
40 41 42 43 44	12·8 12·6 12·3 12·1 11·9	13'3 13'0 12'7 12'5 12'3	13.7 13.4 13.2 12.9 12.7	14·2 13·9 13·6 13·4 13·1	14.7 14.4 14.1 13.9 13.6	15°3 15°0 14°7 14°4 14°2	15.9 15.6 15.3 15.0 14.7	16.6 16.3 16.0 15.7 15.4	17 . 4 17.0 16.7 16.4 16.1	17·8 17·4 17·1 16·7 16·4	18·2 17·8 17·5 17·1 16·8	18.6 18.3 17.9 17.6 17.3	19.1 18.7 18.4 18.0 17.7	19.6 19.2 18.8 18.5 18.1	20°1 19°7 19°3 19°0 18°6
45 46 47 48 49	11.2 11.2 11.3 11.1 10.9	12'0 11'8 11'6 11'5 11'3	12.5 12.2 12.0 11.9 11.7	12'9 12'7 12'5 12'3 12'1	13'4 13'2 12'9 12'7 12'5	13.9 13.7 13.4 13.2 13.0	14.5 14.2 14.0 13.8 13.6	15°1 14°8 14°6 14°4 14°1	15.8 15.5 15.3 15.0 14.8	16·2 15·9 15·6 15·4 15·1	16·5 16·3 16·0 15·7 15·5	16.9 16.7 16.4 16.1 15.9	17.4 17.1 16.8 16.5 16.3	17·8 17·5 17·2 17·0 16·7	18·3 18·0 17·7 17·4 17·2
50 51 52 53 54	10.8 10.6 10.3 10.3 10.2	11.1 11.0 10.8 10.2 10.2	11.2 11.3 11.3 11.0 10.9	11.3 11.3 11.3	12°4 12°2 12°0 11°9 11°7	12.8 12.7 12.5 12.3 12.2	13.4 13.2 13.0 12.8 12.7	13.9 13.7 13.6 13.4 13.2	14°6 14°4 14°2 14°0 13°8	14·9 14·7 14·5 14·3 14·1	15°3 15°0 14°8 14°6 14°5	15.6 15.4 15.2 15.0 14.8	16.0 15.8 15.6 15.4 15.2	16·5 16·2 16·0 15·8 15·6	16·9 16·7 16·4 16·2 16·0
55 56 57 5 ⁸ 59	10°1 9'95 9'84 9'73 9'63	10'4 10'3 10'2 10'0 9'94	10.8 10.6 10.5 10.4 10.3	10.8 10.8 11.0	11.2 11.4 11.3 11.2 11.0	12.0 11.9 11.7 11.6 11.5	12.2 12.3 12.1 12.1 11.9	13.0 12.9 12.7 12.6 12.5	13.6 13.5 13.3 13.2 13.0	13.9 13.8 13.6 13.5 13.3	14°3 14°1 13°9 13°8 13°6	14.6 14.5 14.3 14.1 14.0	15°0 14°8 14°6 14°5 14°3	15·4 15·2 15·0 14·9 14·7	15·8 15·6 15·4 15·3 15·1
60 61 62 63 64	9'53 9'43 9'34 9'26 9'18	9·84 9·74 9·65 9·56 9·48	10°2 10°1 9°89 9°80	10'5 10'4 10'3 10'2 10'2	10 [.] 9 10 [.] 8 10 [.] 7 10 [.] 6 10 [.] 5	11.4 11.5 11.1 11.0 10.0	11.8 11.7 11.6 11.5 11.4	12°3 12°2 12°1 12°0 11°9	12.9 12.8 12.6 12.5 12.4	13·2 13·1 12·9 12·8 12·7	13.5 13.4 13.2 13.1 13.0	13.8 13.7 13.6 13.4 13.3	14·2 14·0 13·9 13·8 13·7	14.6 14.4 14.3 14.1 14.0	14.9 14.8 14.7 14.5 14.4
65 66 67 68 69	9.10 9.03 8.96 8.90 8.84	9'40 9'33 9'26 9'19 9'13	9*72 9*64 9*57 9*50 9*44	10.1 9.99 9.91 9.84 9.77	10'4 10'4 10'3 10'2 10'1	10.9 10.8 10.7 10.6 10.5	11.3 11.2 11.1 11.0 11.0	11.8 11.7 11.6 11.5 11.4	12°3 12°2 12°1 12°0 12°0	12.6 12.5 12.4 12.3 12.2	12·9 12·8 12·7 12·6 12·5	13.2 13.1 13.0 12.9 12.8	13.6 13.4 13.3 13.3 13.2	13.9 13.8 13.7 13.6 13.5	14°3 14°2 14°1 14°0 13°9
70 71 72 73 74	8·78 8·73 8·68 8·63 8·58	9.07 9.01 8.96 8.91 8.86	9°38 9°32 9°26 9°21 9°17	9 [.] 71 9.65 9.59 9.54 9.49	10.1 10.0 9.95 9.90 9.85	10.2 10.4 10.3 10.3 10.2	10.9 10.8 10.8 10.7 10.6	11.4 11.3 11.2 11.2 11.1	11.9 11.8 11.7 11.7 11.6	12°2 12°1 12°0 11°9 11°9	12'4 12'4 12'3 12'2 12'2	12.8 12.7 12.6 12.5 12.5	13.1 13.0 12.9 12.8 12.8	13.4 13.3 13.3 13.2 13.1	13.8 13.7 13.6 13.5 13.5
75 76 77 78 79	8·54 8·50 8·47 8·44 8·41	8·82 8·78 8·74 8·71 8·68	9.12 9.08 9.04 9.01 8.98	9'45 9'40 9'36 9'33 9'30	9·80 9·75 9·71 9·68 9·64	10°2 10°1 10°1 10°1 10°0	10.6 10.6 10.5 10.5 10.4	10.3 10.3 11.0 11.0 11.1	11.6 11.2 11.2 11.4 11.4	11.8 11.8 11.7 11.7 11.6	12°1 12°1 12°0 12°0 11°9	12'4 12'3 12'3 12'3 12'2	12.7 12.7 12.6 12.6 12.5	13.1 13.0 12.9 12.9 12.8	13.4 13.3 13.3 13.2 13.2
80 31 82 83 84	8•38 8•35 8•33 8•31 8•30	8·65 8·63 8·60 8·58 8·58	8·95 8·92 8·90 8·88 8·87	9°27 9°24 9°21 9°19 9°17	9·61 9·58 9·56 9·54 9·52	9·99 9·96 9·93 9·91 9·89	10.4 10.4 10.3 10.3 10.3	10.8 10.8 10.8 10.8 10.8	11.3 11.3 11.3 11.2 11.2	11.6 11.6 11.5 11.5 11.5	11.8 11.8 11.8 11.8	12°2 12°1 12°1 12°1 12°0	12°5 12°4 12°4 12°4 12°4	12.8 12.8 12.7 12.7 12.7	13°1 13°1 13°0 13°0
85 86 87 88 89 90	8·28 8·27 8·26 8·26 8·25 8·25	8·55 8·54 8·53 8·53 8·52 8·52	8·84 8·83 8·82 8·82 8·81 8·81	9.16 9.15 9.14 9.13 9.13 9.13 9.12	9·50 9·49 9·48 9·47 9·47 9·47 9·46	9.87 9.86 9.85 9.84 9.84 9.84 9.83	20'3 10'3 10'2 10'2 10'2	10'7 10'7 10'7 10'7 10'7	11.2 11.2 11.2 11.2 11.2 11.2 11.2	11.2 11.4 11.4 11.4 11.4 11.4	11.7 11.7 11.7 11.7 11.7 11.7	12.0 12.0 12.0 12.0 12.0 12.0	12'3 12'3 12'3 12'3 12'3 12'3	12.7 12.6 12.6 12.6 12.6 12.6 12.6	13.0 13.0 13.0 13.0 12.9 12.9

To convert time into longitude divide by 4. Thus 128. + 4 = 3' long.

SHOWING THE ERROR PRODUCED IN THE TIME OR LONGITUDE BY AN ERROR OF I' IN THE ALTITUDE.

uths.	LATITUDES.														
Azim	73°	7 4 °	75°	76°	77°	78°	79 °	80 °	81°	82°	83°	83 ¹ 2°	840	84 ¹⁰ / ₂	85°
° 30 31 32 33 34 35 36 27	s. 27.4 26.6 25.8 25.1 24.5 23.9 23.3 22.7	s. 29.0 28.2 27.4 26.6 26.0 25.3 24.7 24.1	s. 30.9 30.0 29.2 28.4 27.6 26.9 26.3 25.7	s. 33'1 32'1 31'2 30'4 29'6 28'8 28'1 27'5	s. 35 ^{.6} 34 ^{.5} 33 ^{.6} 32 ^{.6} 31 ^{.8} 31 ^{.0} 30 ^{.3} 20 ^{.5}	s. 38·5 37·4 36·3 35·3 34·4 33·5 3 ² ·7 32·0	s. 41·9 40·7 39·6 38·5 37·5 36·5 35·7 34·8	s. 46·1 44·7 43·5 42·3 41·2 40·2 39·2 38·3	s. 51·1 49·6 48·3 46·9 45·7 44·6 43·5 42·5	s. 57 [·] 5 55 [·] 8 54 [·] 2 52 [·] 8 51 [·] 4 50 [·] 1 48 [·] 9 47 [·] 8	s. 65.6 63.7 61.9 60.3 58.7 57.2 55.8 54.5	s. 70'7 68'6 66'7 64'9 63'2 61'6 60'1 58'7	s. 76 [•] 5 74 [•] 3 72 [•] 2 70 [•] 3 68 [•] 4 66 [•] 7 65 [•] 1 63 [•] 6	s. 83 ^{.5} 81 ^{.0} 78 ^{.8} 76 ^{.6} 74 ^{.6} 72 ^{.8} 71 ^{.0}	s. 91.8 89.1 86.6 84.3 82.1 80.0 78.1 76.2
38 39 40 41 42 43	22·2 21·7 21·3 20·9 20·4 20·1	23.6 23.1 22.6 22.1 21.7 21.3	25°1 24°0 23°6 23°1 22°7	26·9 26·3 25·7 25·2 24·7 24·2	28.9 28.3 27.7 27.1 26.6 26.1 25.6	31.2 30.6 29.9 29.3 28.8 28.2 27.7	34°0 33°3 32°6 32°0 31°3 30°7	37.4 36.6 35.8 35.1 34.4 33.8 33.2	41.5 40.6 39.8 39.0 38.2 37.5 36.8	46.7 45.7 44.7 43.8 43.0 42.1	53'3 52'2 51'1 50'0 49'1 48'1	57'4 56'1 55'0 53'9 52'8 51'8 50'0	62·2 60·8 59·5 58·3 57·2 56·1	67.8 66.3 64.9 63.6 62.4 61.2	74°5 72°9 71°4 70°0 68°6 67°3 66°1
44 45 46 47 48 49	19 7 19 3 19 0 18 7 18 4 18 1	20 9 20 5 20 2 19 8 19 5 19 2	21.9 21.5 21.1 20.8 20.5	23.4 23.0 22.0 22.2 21.9	25·1 24·7 24·3 23·9 23·6 23·2	27·2 26·7 26·3 25·9 25·5	29.6 29.1 28.7 28.2 27.8	32.6 32.0 31.5 31.0 30.5	36·2 35·5 35·0 34·4 33·9	40.6 40.0 39.3 38.7 38.1	47 2 46.4 45.6 44.9 44.2 43.5	50.0 49.1 48.3 47.5 46.8 46.1	53 1 54 · I 53 · 2 52 · 3 51 · 5 50 · 7	59°0 58°0 57°1 56°2 55°3	64.9 63.8 62.7 61.8 60.8
50 51 52 53 54	17'9 17'6 17'4 17'1 16'9	18 9 18 7 18 4 18 2 17 9	19.9 19.6 19.4 19.1	21.0 21.3 21.0 20.7 20.4	22.9 22.6 22.3 22.0	24·8 24·4 24·1 23·8	27 4 27 0 26 6 26 2 25 9	29.6 29.2 28.8 28.5	32.9 32.5 32.0 31.6	37 5 37 0 36 5 36 0 35 5	42 9 42 2 41 7 41 1 40 6	45°5 44°8 44°2 43°7	49 [•] 2 48 [•] 6 47 [•] 9 47 [•] 3	54 5 53.7 53.0 52.3 51.6	59 9 59 1 58 2 57 5 56 7
55 56 57 58 59	10.7 16.5 16.3 16.1	17.7 17.5 17.3 17.1 16.9	18.0 18.6 18.4 18.2 18.0	19.9 19.7 19.5 19.3	21 7 21 4 21 2 21 0 20 7	23.2 23.2 22.9 22.7 22.4	25.0 25.3 25.0 24.7 24.5	27.8 27.5 27.2 26.9	30.8 30.2 30.2 29.8	34'7 34'3 33'9 33'5	39.6 39.1 38.7 38.3	42.6 42.1 41.7 41.2 40.8	407 46°2 45°6 45°1 44°6	50.3 49.8 49.2 48.7	55.4 54.7 54.1 53.5
60 61 62 63 64	15°8 15°6 15°5 15°3 15°2	10.8 10.6 10.4 10.3 10.1	17.7 17.5 71.3 17.2	19.1 18.9 18.7 18.6 18.4	20°3 20°1 20°0 19°8	22.0 21.8 21.6 21.4	24.2 24.0 23.7 23.5 23.3	26.3 26.1 25.9 25.6	29·2 29·0 28·7 28·4	32.9 32.6 32.3 32.0	37.5 37.2 36.8 36.5	40.4 40.0 39.7 39.3 30.0	44 2 43.8 43.3 42.9 42.6	40°2 47°7 47°3 46°8 46°4	52.5 52.0 51.5 51.1
05 66 67 68 69	15°0 14°9 14°8 14°7	15.9 15.8 15.7 15.5	16.9 16.8 16.7 16.6	18·1 18·0 17·8 17·7	19°5 19°3 19°2 19°0	21·1 20·9 20·7 20·6	22.9 22.8 22.6 22.5	25.2 25.0 24.8 24.7	28.0 27.8 27.6 27.4	31.2 31.0 30.8	35°9 35°7 35°4 35°2	38.7 38.4 38.1 37.8 37.6	41.9 41.6 41.3 41.0	45.7 45.3 45.0 44.7	50°2 49°9 49°5 49°2 48°8
70 71 72 73 74	14.0 14.5 14.4 14.3 14.2	15.3 15.3 15.2 15.1	16.3 16.3 16.1	17.0 17.5 17.4 17.3 17.2	18.8 18.7 18.6 18.5	20'3 20'2 20'1 20'0	22°2 22°2 21°9 21°8	24.4 24.2 24.1 24.0 22.8	27.0 26.9 26.7 26.6	30'4 30'2 30'1 29'9	34.7 34.5 34.3 34.1	37 [•] 4 37 [•] 2 36 [•] 9 36 [•] 8	40°5 40°2 40°1 39°8	44.1 43.9 43.6 43.4	48·3 48·0 47·7
75 76 77 78 79	14.2 14.1 14.0 14.0 13.9	15.0 15.0 14.9 14.8 14.8	10.0 15.9 15.8 15.8 15.7	17.1 17.0 17.0 16.9 16.8	18.3 18.2 18.2 18.1	19'9 19'8 19'7 19'7 19'6	21.7 21.6 21.5 21.4 21.4	23.7 23.6 23.5 23.5	26.4 26.2 26.1 26.0	29 ^{.6} 29 ^{.5} 29 ^{.4} 29 ^{.3}	34 0 33.8 33.7 33.6 33.4	36·4 36·3 36·1 36·0	39.4 39.3 39.1 39.0	43 2 43 0 42 8 42 7 42 5	47'3 47'3 47'1 46'9 46'8
80 81 82 83 84	13.8 13.8 13.8	14.7 14.7 14.7 14.6 14.6	15.7 15.6 15.6 15.6 15.5	16·8 16·7 16·7 16·7 16·6	18.0 18.0 17.9 17.9	19°5 19°5 19°4 19°4 19°3	21·3 21·2 21·2 21·1 21·1	23.4 23.3 23.3 23.2 23.2	25.9 25.8 25.8 25.8 25.7	29°2 29°1 29°0 29°0 28°9	33.3 33.1 33.0 33.0	35.8 35.8 35.7 35.6 35.5	38.7 38.6 38.6 38.6 38.5	42°4 42°3 42°1 42°0 42°0	46.5 46.3 46.2 46.1
85 86 87 88 89 90	13.7 13.7 13.7 13.7 13.7 13.7 13.7	14.6 14.5 14.5 14.5 14.5 14.5 14.5	15.5 15.5 15.5 15.5 15.5 15.5	16.6 16.6 16.5 16.5 16.5	17.8 17.8 17.8 17.8 17.8 17.8 17.8	19.3 19.3 19.2 19.2 19.2	21.0 21.0 21.0 21.0 21.0 21.0 21.0	23 ^{.2} 23 ^{.1} 23 ^{.1} 23 ^{.0} 23 ^{.0} 23 ^{.0}	25.7 25.6 25.6 25.6 25.6 25.6	28.8 28.8 28.8 28.8 28.7 28.7	32.9 32.9 32.9 32.8 32.8 32.8 32.8	35°4 35°4 35°4 35°4 35°3 35°3	38·4 38·3 38·3 38·3 38·3 38·3 38·3	41.9 41.8 41.8 41.8 41.7 41.7	46°0 46°0 45°9 45°9 45°9

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Table E.

96

CORRECTIONS OF ALTITUDE OF THE SUN AND STARS (Involving Dip, Refraction, O's Sem diameter, and Parallas). Add the Cor. to the Alt. of the O's Lower Limb.

Alt.				Heigh	nt of the	Eye, iz	h Feet.			
Sur Obs.	6 ft.	8 ft.	10 ft.	12 ft.	14 ft.	16 ft.	18 ft.	20 ft.	22 ft.	24 ft.
• 5 6 7 7 8 9 10 11 12 13 14 15 16 17 17 19 20 22 24 26 28 30 35 50 55 50 60 65 70 0 65 90	3'9 5'2 6'4 7'2 7'9 8'4 8'9 9'3 9'9 9'3 9'9 10'2 10'4 10'6 10'8 10'9 11'1 11'3 11'6 10'8 10'9 11'1 11'3 11'6 12'4 12'6 12'8 12'9 13'1 13'2 13'3 13'4 13'6 13'7	3'55 4'85 5'99 6'88 7'55 8'99 9'55 8'99 9'55 8'99 9'55 9'89 10'00 10'3 10'4 10'61 10'7 11'00 11'2 11'4 11'55 11'7 12'00 12'2 12'4 12'5 12'7 12'8 12'9 13'0 13'2	3'I 4'5 5'6 6'5 7'2 7'7 8'2 8'6 8'9 9'5 9'7 9'7 9'7 9'7 9'7 9'7 9'7 9'7 10'3 10'4 10'7 10'9 11'1 11'2 11'4 11'7 11'9 12'1 12'2 12'2 12'6 12'7 12'9 13'0	2.8 4.2 5.3 6.2 6.8 7.4 7.9 8.3 8.6 8.9 9.2 9.4 9.6 9.9 9.4 9.6 9.9 9.4 9.6 9.9 10.1 10.3 10.6 10.7 10.9 11.1 11.3 11.6 11.8 11.2 12.2 12.2 12.2 12.2 12.2 12.2	2.5 3.9 5.0 5.9 6.6 7.1 7.6 8.0 8.4 8.0 8.4 8.0 8.9 9.1 9.4 9.7 9.7 9.8 10.3 10.5 10.6 10.8 11.1 11.3 11.5 11.6 11.8 11.9 12.0 12.1 12.3	2 ^{'2} 3 ^{'7} 4 ^{'8} 5 ^{'6} 6 ^{'3} 6 ^{'9} 7 ^{'4} 7 ^{'8} 8 ^{'1} 8 ^{'1} 8 ^{'1} 8 ^{'1} 8 ^{'1} 8 ^{'1} 8 ^{'1} 8 ^{'1} 8 ^{'1} 8 ^{'1} 9 ^{'1} 1 ^{'1} 1	1.9 3.4 5.5 4.5 5.4 6.1 6.6 7.1 7.5 7.9 8.1 8.4 8.6 8.9 9.2 9.3 9.8 10.0 10.2 10.3 10.6 10.8 11.0 11.2 11.4 11.5 11.6 11.6 11.6 11.6	1.7 3.2 5.8 6.9 7.3 7.6 7.9 8.4 8.6 8.9 9.1 9.4 9.6 9.8 9.9 10.4 10.6 10.8 10.6 10.8 10.9 11.1 11.2 11.3 11.4 11.7	1.5 2.9 4.9 5.6 6.7 7.1 7.4 7.7 8.0 8.2 8.4 8.6 8.7 8.9 9.2 9.7 9.7 9.7 9.7 9.7 9.7 9.7 9.7 9.7 9.7	1.3 2.7 3.8 4.7 5.4 6.0 6.5 6.9 7.2 7.5 8.0 8.2 8.4 8.5 9.0 9.2 9.3 9.5 9.7 9.0 9.2 10.3 10.5 10.7 10.8 10.9 11.0 11.2 11.
i, mourselere	C	ORREC'	TION (OFAS	TAR'S	ALTIT	UDE.	(Subtr	act.)	
Alt.				Heigh	t of the	Eye, in	Feet.		•	
Star's	6 ft.	8 ft.	10 ft.	12 ft.	14 ft.	16 ft.	18 ft.	20 ft.	22 ft.	24 ft.
* 5 6 7 8 9 9 10 11 12 13 14 15 16 17 18 19 20 22 24 26 28 30 35 5 5 60 60 55 70 80 90	12'3 10'9 9'0 8'3 7'3 6'5 6'5 6'5 5'5 5'5 4'6 4'4 4'1 8'6 3'4 2'1 3'6 3'2 1'0 9'8 3'2 1'0 9'7 9'0 8'3 7'7 6'5 5'5 5'5 5'5 5'5 4'6 4'4 3'3 3'2 2'8 6'5 2'2 8'3 7'7 9'0 8'3 7'7 6'5 5'5 5'5 5'5 5'5 5'5 4'6 4'4 3'10 9'7 8'3 7'7 8'5 5'5 5'5 5'5 4'6 4'6 4'7 8'6 5'5 5'5 5'5 5'5 5'5 5'5 5'5 5'5 5'5 5	12.6 11.3 10.2 9.3 8.7 7.6 7.2 6.9 6.3 6.7 2.6 9.6 6.3 6.1 5.9 5.7 5.6 5.4 5.2 4.9 4.8 4.6 4.4 4.2 3.8 3.6 3.8 3.6 3.3 3.2 3.1 2.8 3.1 2.8 3.1 2.8 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1	13.6 10.5 9.7 9.0 8.4 7.5 7.2 6.6 6.4 6.2 6.7 5.7 5.5 5.7 5.5 5.7 4.8 5.7 5.5 5.7 4.8 8 4.5 3.3 6.5 3.3 3.5 3.3 3.1	13.4 12.0 9.3 8.3 7.5 7.2 0 8.5 7.5 7.5 7.5 7.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5 5.5 18.6 6.5 5.5 18.6 4.4 4.2 14.0 9 3.6 5.5 4.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5		, 9 13.9 11.4 10.5 9.8 8.4 8.0 7.3 9.7 6.7 6.7 6.3 1.1 9.8 8.4 8.0 8.8 7.3 7.0 9.6 6.3 1.5 5.7 5.6 3.5 5.7 4.7 4.7 4.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5	14.2 12.8 11.6 10.8 10.1 9.5 8.3 8.3 8.3 8.3 8.3 7.7 7.5 7.3 7.7 7.5 7.3 7.7 7.5 6.5 5.5 5.7 5.6 4.7 4.5 4.2 4.2	14'4 13'0 10'3 9'3 8'5 8'5 8'5 8'5 8'5 8'5 8'5 8'5 7'5 7'5 7'5 7'5 7'5 7'5 7'5 7'5 7'5 6'8 6'4 6'1 5'6 6'4 5'5 5'4 5'5 5'4 5'5 5'4 5'5 5'4 5'5 5'4 5'5	14.6 13.2 12.1 11.2 10.5 9.5 9.1 8.7 8.5 8.2 8.0 7.7 6.8 8.2 8.0 7.7 6.8 6.4 6.3 6.5 5.4 5.2 5.1 5.8 5.4 5.2 5.1 5.8 4.6	, 14.8 13.4 12.3 11.4 10.7 9.7 9.7 8.9 7.6 7.5 7.2 7.6 8.6 6.5 5.6 5.5 5.5 4.8 5.5 5.4 5.3 5.2 5.6 5.5 4.8

		Accelerat	tion.	
H. 1 2 3 4 5 6 7 8 9 10 11 13 14 15 16 17 18 19 21 22 23 24	M. 0 0 0 0 0 0 0 0 0 0 0 0 0	s. 9'86 19'71 29'57 39'43 49'28 59'14 9'00 18'85 28'71 38'56 48'42 27'82 37'70 48'42 27'82 37'70 47'56 57'42 7'27 17'13 26'99 36'84 46'70 56'56	M. I 2 3 4 5 6 7 8 9 10 11 12 3 4 5 6 7 8 9 10 11 12 3 4 5 6 7 8 9 10 11 12 3 14 15 16 17 18 19 20 21 22 23 24 25 25 16 17 18 19 20 21 22 23 25 25 16 17 17 18 19 20 21 22 23 25 25 17 17 17 18 19 20 21 22 23 25 25 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17	s. 0.16 0.33 0.49 0.66 0.82 0.98 1.15 1.31 1.48 1.64 1.81 1.97 2.13 2.30 2.46 3.279 2.96 3.12 3.29 3.45 3.61 3.78 3.94 1.11
Morr Sum Jan. Feb Mar Apri July July Sep. Oct. Nov Dec.	th C to to 's A + + + + + + + + + + + + + + + + + + +	or. lt. 0'3 0'2 0'1 0'2 0'2 0'3 0'2 0'1 0'2 0'3 0'2 0'3 0'2 0'3	26 27 28 30 31 32 33 45 37 37 39 40 42 43 44 50 51 52 34 55 55 57 8 59 60	4 27 4 44 4 60 4 706 4 93 5 09 5 542 5 59 5 75 5 591 6 24 6 57 6 540 6 57 6 57 6 57 6 57 6 57 6 7 23 7 756 7 72 7 80 5 8 21 8 8 57 1 8 8 8 77 7 780 5 8 21 8 8 8 7 756 9 9 36 9 9 36 9 9 86

Table F.

Table E.

CORRECTIONS OF ALTITUDE OF THE SUN AND STARS (INVOLVING DIP, REFRACTION, O'S SEMIDIAMETER, AND PARALLAX). Add the Cor. to the Alt. of the O's Lower Limb, except where marked – (minus).

n's Alt.				He	ight of	the E	ye, in	Feet.			
Sur Obs.	26 ft.	28 ft.	30 ft.	35 ít.	40 ft.	45 ft.	50 ft.	55 ft.	60 ft.	70 ft.	80 ft.
° 56 78 910 11	1.1 2.5 3.6 4.5 5.2 5.8 6.3	0.9 2.4 3.5 4.3 5.0 5.6 6.1	0.7 2.2 3.3 4.2 4.8 5.4 5.9	0'3 1'7 2'8 3'7 4'4 5'0 5'5	-0'1 1'3 2'4 3'3 4'0 4'6 5'0	- 0'5 0'9 2'1 3'0 3'6 4'2 4'7	-0.8 0.6 1.7 2.6 3.3 3.8 4.3	- 1'2 0'2 1'3 2'2 2'9 3'5 4'0	- 1.6 - 0.1 1.0 2.6 3.2 3.6	- 2'8 - 0'7 0'4 1'3 2'0 2'5 3'0	$-3^{'}3$ $-1^{'}3$ $-0^{'}2$ $0^{'}7$ $1^{'}4$ $2^{'}0$ $2^{'}5$
12 13 14 15 16 17 18 19 20 22 24 26 28 30 35	0.7 70 7.3 7.6 7.8 8.0 8.2 8.3 8.5 8.5 8.7 9.0 9.1 9.3 9.5 9.7	0 5 6 8 7 1 7 4 7 6 7 8 8 0 8 3 8 6 8 3 8 6 8 3 8 6 8 9 0 9 1 9 3 9 0 8	6 3 6 6 6 9 7 2 7 4 7 6 7 8 8 0 8 1 8 4 8 6 8 8 9 9 1 9 1 9 2	592 658 72 74 75 79 835 857 857 857 892	555 561 64 66 66 70 71 73 75 78 79 81 83 83 85 8	5 1 5 4 5 7 6 0 6 2 6 4 6 6 6 9 7 2 7 4 7 6 7 7 7 9 2 8 4	477 51 54 56 59 61 63 63 64 65 68 70 72 74 75 75 88	4 4 4 7 5 0 5 3 5 5 5 7 5 9 6 1 6 2 6 7 6 9 7 0 7 2 7 7 7 7 7 7	4 1 4 4 7 5 0 5 2 5 4 5 6 5 9 6 2 6 7 6 9 2 6 7 6 9 2 7 4	3 58 3 4 4 6 4 6 8 0 1 5 5 3 5 5 8 9 1 5 5 5 5 9 1 6 5 8 6 5 8 6 5 8	2 9 9 3 · 2 3 · 5 3 · 8 4 · 2 4 · 4 4 · 6 4 · 7 5 · 2 5 · 4 5 · 5 5 · 7 6 · 2
45 50 55 60 65 70 80 90	10'1 10'3 10'5 10'6 10'7 10'8 11'0 11'1	10.0 10.1 10.3 10.4 10.5 10.6 10.8 10.9	9.8 9.9 10.1 10.2 10.3 10.4 10.6 10.8	9 ² 9 ⁴ 9 ⁵ 9 ⁷ 9 ⁸ 9 ⁹ 10 ⁰ 10 ² 10 ³	9.0 9.1 9.3 9.4 9.5 9.6 9.8 9.8	8.6 8.7 8.9 9.0 9.1 9.2 9.4 9.6	8.2 8.4 8.5 8.6 8.7 8.8 9.0 9.2	7 9 8 0 8 2 8 3 8 4 8 5 8 7 8 9	7.6 7.7 7.9 8.0 8.1 8.2 8.4 8.5	7.0 7.1 7.3 7.4 7.5 7.6 7.8 7.8 7.9	6.4 6.5 6.7 6.8 7.0 7.2 7.4

SUPPLEMENTARY TABLES FOR LOW ALTITUDES.

Correction for Small Altitudes. 40 ft. and Correction, Sun's Obs. Altitude. Various Heights Height, Add to) Alt. Subt. from Ft. 0 +3.8- 4'9 б 3 0 3 10 4'4 8 3'4 3.1 3.9 10 20 3 3 30 3.4 12 2.8 3.0 2.2 3 40 14 5.1 5.3 3 50 2.5 1Ġ 2'1 18 0 4 1.8 4 10 20 1.8 1'4 4 20 22 1.6 1.4 30 1.0 24 4 o.8 26 1.5 4 40 5 0 0.5 28 1.0 +0.4 o[.]8 5 20 30 40 32 o.ġ o.4 5 1.3 0 34 0'5 0.3 6 20 1.2 36 38 6 40 2'I 0.5 40 7 ်၀ **2**'4 0.0 42 20 2.7 -0'2 7 4**0** 3.0 **o**'3 78 44 46 0.2 3'3 0 3°5 3'8 48 0.6 8 20 8 50 40 0'7 0.9 8 50 3.9 52 I.0 0 4'0 54 9 4'2 9 20 56 1.1 . 4'4 60 1'4 9 40 10 ်၀ 4[.]6 65 1.4 4·8 70 2'0 10 30 5.0 75 2.3 II 0

CORRECTION OF A STAR'S ALTITUDE.

DE. (Subtract.)

Alt.		Height of the Eye, in Fect.									
Star's	26 ft.	28 ft.	3 0 ft.	35 ft.	40 ft.	45 ft.	50 ft.	55ft.	60 ft.	70 ft.	80ft.
0	15:0	15:0	7	15.8	16:2	16.6	17:0	17.4	17.7	18.4	18.0
6	130	13 2	134	12.0	10 5	15.2	15.0	15.0	16.3	16.0	17.5
7	12.2	12.2	12.0	T3'3	13.7	14.1	14.9	14.8	15.1	15.8	16.3
8	11.0	11.8	12.0	12.4	12.8	13.2	13.6	13.0	14.3	14.9	15.4
0	10.0	11.1	11.3	11.2	15.1	12.2	12.0	13.2	13.2	14'2	14.7
10	10.4	10.6	10.2	11.5	11.0	11.0	12.3	12.0	13.0	13.6	14.2
11	9.9	10.1	10.3	10.2	11.1	11.2	11.0	12.5	12.2	13.1	13.2
12	9.5	9.7	9·8	10.3	10.7	11.0	11.4	11.8	12.1	12.7	13.3
13	9·1	9.3	9.2	9.9	10.3	10.7	11.1	11.4	11.2	13.3	12.0
14	8.9	9.0	9.2	9.2	10.1	10.4	10.8	11.1	11.4	15.1	12.0
15	8.6	8.8	8.9	9.4	9.8	10.1	10.2	10.8	11.5	11.8	15.3
16	8.4	8.2	8.7	9.5	9.6	9.9	10.3	10.0	10.0	11.0	15.1
17	8.1	8.3	8.2	8.9	9.3	9.7	10.1	10'4	10.2	11.4	11.0
18	7.9	8.1	8.3	8.8	9.5	9.2	9.9	10.5	10.2	11.5	11.2
19	7.8	8.o	8.5	8.6	9.0	9'4	9.2	10.1	10.4	11.0	11.0
20	7.7	7.8	8.0	8.2	8.9	9.5	9.6	9.9	10.5	10.0	11.4
22	7'4	7.6	7.8	8.3	8.6	0. 0	9.3	9.7	10.0	10.0	I1'2
24	7.2	7.4	7.2	8.0	8.4	8.7	0.1	9.4	9.8	10.4	10.0
26	7.0	7.2	7'4	7.8	8.5	8.6	8.0	9.3	9.6	10.5	10.8
28	6.8	7.0	7'2	7.6	8.0	8.4	8.8	0 .1	9.4	10.0	10.0
30	6.7	6.9	7.0	7.5	7.9	8.2	8.6	8.9	9.3	9.9	10.4
35	6'4	6.6	6.8	7.2	7.6	8.0	8.3	8.7	9.0	9.0	10.2
40	6.2	6.4	6.2	7.0	7.4	7.7	8.1	0.4	0.0	9.4	9.9
45	0.0	6.2	6.4	6.8	7.2	7.0	2.8	0.3	0.0	9.2	90
50	5.8	0.0	0.5	0.0	7.0	7.4	70	01	8.2	8.0	0.2
55	5.7	5.8	0.1	0.2	6.9	7.3	70	79	8.2	8.8	95
67	50	5.0	5.9	612	6.0	7.1	75	70	8.1	8.7	9.2
05	55	57	50	6.0	6.6	6.0	7 4	7.6	8.0	8.6	0.1
80	54	5.0	57	6.0	6.1	6.8	/ 3	7. 6	7.8	8.4	0.0
00	5'0	5.2	5.4	5.8	6.2	6.6	6.0	73	7.6	8.2	8.8

s r	i n	40 ft.	2nd Vario	Correction, us Heights.
Star	אווות	Height,		$\frac{Add \text{ to}}{Subt.} \neq \forall$
0	1		Ft.	1 2:0
3	10	21.1	8	+30
3	20	20.0		34
3	20	10.2	12	2.8
3	10	10.1	IA	2.5
3	50	18.7	16	2.3
4	0	18.3	18	2. I
4	IO	17.9	20	1.8
4	20	17.2	22	1.0
4 3	30	17.2	24	I'4
44	10	16.0	26	I.3
5	0	16.3	28	1.0
5	20	15.8	30	0.8
54	10	15'3	32	0.2
6	0	14'8	34	0.2
62	20	14'4	30	0'3
64	10	14.1	30	0.2
7	0	13.2	40	0.0
7 2	20	13.4	42	-0'2
7 -	10	13.1	44	0.3
8	0	12.0	40	0'5
0 2	20	12.0	40	0.0
		12.2	52	0.0
	0	12.1	54	1.0
0 2	20	11.0	56	1.1
94	10	11.2	60	I'4
10	0	11.6	65	1.2
10 3	30	11.3	70	2.0
11	0	11.1	75	2.3

|--|

STAR POLARIS AZIMUTH TABLE.

*'s Hr.	LATITUDES.											
Angle.	0 °	10°	20 °	30 °	35°	40 °	4 5°	50°	55°	60°	Angle.	
	AZIMUTHS,											
Н. М.	•	•	•	•	•	0	0	°	•	°	н. м.	
0 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	12 00	
0 20	0.1	0.1	0.1	0.1	0.1	0.1	0.I	0.5	0*2	0.5	11 40	
0 40	0'2	0'2	0'2	0.5	0.3	0.3	0.3	0.3	0 *4	0.4	II 20	
I 00 I 20 I 40	0'3 0'4 0'5	0'3 0'4 0'5	0'3 0'4 0'5	0'4 0'5 0'6	0'4 0'5 0'6	0'4 0'5 0'7	0'4 0'6 0'7	0°5 0°6 0°8	0°5 0°7 0°9	0.6 0.8 1.0	11 00 10 40 10 20	
2 00 2 20 2 40	0.0 0.2 0.8	0.6 0.7 0.8	0.0 0.7 0.8	0.2 0.8 0.9	0.7 0.8 0.9	0.8 0.8	1.1 1.0 0.8	0°9 1°0 1°2	1.1 1.3	1.5 1.4 1.0	10 00 9 40 9 20	
3 00 3 20 3 40	0.8 0.3 1.0	1.0 0.8 0.8	1.0 1.0 0.0	1,1 1,0 1,0	1.0 1.1 1.5	1.1 1.3 1.3	1.3 1.4	1·3 1·4 1·5	1.2 1.6 1.7	1.7 1.8 2.0	9 00 8 40 8 20	
4 00 4 20 4 40	1.1 1.1 1.0	1,1 1,1 1,0	I'I I'I I'2	1.3 1.3	1.3 1.4	1.3 1.4 1.4	1.2 1.2 1.2	1.6 . 1.7 1.7	1.0 1.3 1.8	2.1 2.2 2.2	8 00 7 40 7 20	
5 00 5 20 5 40 6 00	I'I I'2 I'2 I'2	I·2 I·2 I·2	I'2 I'2 I'2 I'2	1.3 1.3 1.4 1.4	1·4 1·4 1·4 1·4	1°5 1°5 1°5 1°5	1.6 1.6 1.7 1.7	1.8 1.8 1.8	2.0 2.0 2.0 2.0	2·3 2·3 2·3 2·4	7 00 6 40 6 20 6 00	

For the twelve hours before the meridian passage (above the Pole) it is east of north, and for the twelve hours after it is west of north.

DIAGRAM to illustrate the Apparent Motion of Star a Ursæ Minoris (Polaris) round the Pole. Declination of Star in 1910, 88° 49¹/₂ N.; Right Ascension, 1 h. 27 m.



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REDUCTION TO THE MERIDIAN TABLE FOR * POLARIS,

AT HOUR-ANGLES FROM UPPER MERIDIAN. Add Reduction to obtain Meridian Altitude. AT HOUR-ANGLES FROM LOWER MERIDIAN. Subtract Reduction to obtain Meridian Altitude.

angle.			LATIT	UDES.				tr. in /ears	angle.			LATIT	UDES.		
Hour	10°	20 °	30°	40 °	50°	60°	·	U Va	Hour-	10°	20 °	30 °	40 °	50°	60°
н. м. 0 10 20 30 40 50	° ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′	• 0'I 0'3 0'6 1'I 1'7	° ' 0'I 0'3 0'6 1'I 1'7	° 0'1 0'3 0'6 1'1 1'7	° '0'I 0'3 0'6 1'1 1'7	• 0'1 0'3 0'6 1'1 1'7		0 Subt. froi	н. м. 0 10 20 30 40 50	° 0'1 0'3 0'6 1'1 1'7	° 0'1 0'3 0'6 1'1 1'7	° ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′ ′	° c'1 0'3 0'6 1'1 1'7	° ' 0'1 0'3 0'6 1'1 1'7	° 0'I 0'3 0'6 1'0 1'6
1 0 20 30 40 50	2.4 3.3 4.3 5.4 6.6 8.0	2.4 3.3 4.3 5.4 6.6 8.0	2.4 3.3 4.3 5.4 6.7 8.0	2.4 3.3 4.3 5.4 6.7 8.0	2·5 3·3 4·4 5·5 6·7 8·1	2.5 3.4 4.4 5.5 6.8 8.2		0'I 0'1 0'2 0'3 0'3	1 0 20 30 40 50	2.4 3.3 4.2 5.3 6.6 7.9	2.4 3.2 4.2 5.3 6.6 7.9	2.4 3.2 4.2 5.3 6.5 7.9	2'4 3'2 4'2 5'3 6'5 7'8	2°3 3°2 4°1 5°2 6°4 7°8	2°3 3°1 4°1 5°2 6°4 7°7
11 0 20 30 40 50	9.5 11.0 12.8 14.6 16.5 18.6	9.5 11.1 12.8 14.6 16.6 18.6	9'5 11'2 12'9 14'7 16'7 18'7	9.6 11.2 12.9 14.8 16.7 18.8	9'7 11'3 13'0 14'9 16'8 18'9	9.8 11.4 13.2 15.0 17.0 19.1		0.4 0.5 0.5 0.7 0.7 0.8	11 0 20 30 40 50	9'4 11'0 12'7 14'5 16'4 18'5	9'4 10'9 12'6 14'5 16'4 18'4	9'3 10'9 12'6 14'4 16'3 18'3	9.3 10.9 12.5 14.3 16.2 18.2	9 ^{.2} 10 ^{.8} 12 ^{.5} 14 ^{.2} 16 ^{.1} 18 ^{.1}	9'I 10'7 12'3 14'I 16'0 18'0
111 0 20 30 40 50	20'7 22'9 25'2 27'6 30'1 32'7	20.8 23.0 25.3 27.7 30.2 32.8	20.8 23.1 25.4 27.8 30.3 32.9	20'9 23'2 25'5 27'9 30'4 33'0	21°1 23°3 25°7 28°1 30°6 33°2	21·3 23·5 25·9 28·4 30·9 33·5		0'9 1'0 1'1 1'2 1'3 1'4	III 0 10 20 30 40 50	20.6 22.8 25.1 27.5 29.9 32.5	20.5 22.7 25.0 27.4 29.9 32.4	20.4 22.6 24.9 27.3 29.8 32.3	20.3 22.5 24.8 27.2 29.6 32.2	20°2 22°4 24°7 27°0 29°5 32°0	20°0 22°2 24°5 26°8 29°2 31°7
IV 0 20 30 40 50	35'3 38'0 40'8 43'6 46'5 49'4	35 [•] 4 38 [•] 1 40 [•] 9 43 [•] 7 46 [•] 6 49 [•] 5	35°5 38°2 41°0 43°9 46°7 49°6	35'7 38'4 41'2 44'0 46'9 49'8	35 ^{.9} 3 ^{8.6} 4 ^{1.4} 44 ^{.2} 47 ^{.1} 50 ^{.1}	36.2 38.9 41.7 44.6 47.4 50.4		1.5 1.6 1.7 1.9 2.0 2.1	Ⅳ 0 10 20 30 40 50	35°1 37°8 40°6 43°4 46°2 49°1	35°0 37°7 40°5 43°3 46°1 49°0	34'9 37'6 40'3 43'1 46'0 48'9	34.8 37.4 40.2 43.0 45.8 48.7	34.6 37.2 40.0 42.8 45.6 48.5	34'3 36'9 39'7 42'4 45'2 48'1
V 0 10 20 30 40 50	52'3 55'3 58'3 1 1'4 1 4'4 1 7'5	52.4 55.4 58.5 1 1.5 1 4.5 1 7.6	52.6 55.6 58.6 1 1.7 1 4.7 1 7.8	52.8 55.8 58.8 1 1.8 1 4.9 1 8.0	53.0 56.0 59.0 1 2.1 1 5.1 1 8.2	53 [.] 3 56 [.] 3 59 [.] 4 1 2 [.] 5 1 5 [.] 5 1 8 [.] 6		2·2 2·4 2·5 2·6 2·8 2·9	V 0 10 20 30 40 50	52°1 55°1 58°1 1 1°1 1 4°2 1 7°2	52°0 54°9 58°0 1 1°0 1 4°0 1 7°1	51.8 54.8 57.8 1 0.8 1 3.9 1 7.0	51.6 54.6 57.6 1 0.6 1 3.7 1 6.8	51'4 54'4 57'4 1 0'4 1 3'4 1 6'5	51.0 54.0 57.0 1 0.0 1 3.1 1 6.1
VI o	1 10.0	I 10'7	1 10.8	I II.0	I II'3	I II'7	1	3'I	VI o	I IO.3	I IO'2	1 10.0	1 0.8	1 0.0	I 0'2

For Azimuths of * Polaris see page 88.

Examples in the Use of the above Table.

Example 1.—On April 2nd, 1914, at 3 h. 30 m. a.m., A.T. Sp. in latitude by D.R. 40° 15' N., longitude 11° W. Required the approximate altitude of \star Polaris for setting the sextant for an observation to obtain the latitude. Height of eye, 40 ft.

Mer. pass of $\mathbf{*}$ in 1910 (p. 10) o 44 a.m. below Pole. Cor. for 4 years (see p. 6) $+$ 2	Lat. by D.R. P.D. of X	40° 15 N. -1 9'2	*'s Dl.	88 50.8 N. 90 0.0
Mer. pass. in 1914 0 46 a.m. Time at ship 3 30 a.m.	Mer. alt. 40 ft. cor. (p. 87)	39 5 ^{.8} + 7 ^{.5}	P.D.	1 9'2 N.
*'s Approx. H.A. (below Pole) 2 44 gives reduction 16'7.	Reduction	39 13°3 + 16'7		
Reduction at $2 = 16'2' + 2'' + 4'' = 16'' + 16''' + 16''' + 16'' + 16'' + 16'' + 16'' + 16'' + 16'$	Alt. for sextant	39 30 N.		
True reduction 16.7 + .5		•		

Example 2.—On April 2nd, 1914, at 3 h. 35 m. a.m., A.T. Sp. in latitude by D.R. 40° 15' N., longitude 11° W. Observed altitude of $\frac{1}{2}$ Polaris was found to be 39° 40' N. Height of eye, 37 ft. Required the latitude.

Obsd. alt. of X Eye, 40ft. (cor. p. 87) Reduction	$\begin{array}{r} \stackrel{\circ}{39} 40 \text{ N.} \\ - 7.5 \\ \hline 39 32.5 \\ - 17.7 \end{array}$	Mer. pass. of ¥ in 1914 – Time of observation *'s Approx. H.A. (below Pole)	H. M. 0 46 a.m. 3 35 a.m. 2 49 gives reduction 17'7.	Reduction $18' \circ$ Cor. for 4 years -3 True reduction $17'7$
Mer. alt. (below Pole) P. dist. in 1914	39 14 [.] 8 1 9 [.] 2	*'s Sidereal H.A. would	be nearly $\frac{1}{2}$ m. greater; this	s correction, if required,
Latitude	40 24 0 N.	greater for 6 hours.	eleration table, (page 60).	it will be nearly rin.

DIAGRAM TO AID IN FINDING THE.POSITION OF SOUTH POLE.

This diagram represents the apparent motion of the bright high-declination stars Achernar, Canopus, and those in the constellations of the Southern Cross and Centaurs to an observer in the latitude of Wellington, New Zealand, in about 41° S. In this latitude none of these stars ever set, and they appear to describe a circle round an imaginary South Pole, with a radius equal to the co-declination of the star. The radius of a Crucis, for instance, is about $27\frac{1}{2}^{\circ}$. It will be seen from the diagram that β Centauri and Achernar are always on opposite sides of the circle to one another, and that both stars are at nearly equal distances from the Pole; therefore the *approximate* position of the South Pole in the heavens will always be at a point midway between these two stars. When β Centauri is on the meridian above the Pole, Achernar will be close to the meridian below the Pole, or when β Centauri is east of the Pole Achernar will be about the same distance west of the Pole. The Centaurs will appear in almost exactly the same position in the heavens at, say, 6 p.m. on any given day that Achernar was in at 6 a.m. on the same day, or the Centaurs will appear in almost exactly the same position at 6 p.m. on one day that Achernar was in at the same hour of the day six months previously.



GENERAL REMARKS. RULES, AND EXAMPLES,

GENERAL! REMARKS ON THE DOUBLE-ALTITUDE AND "SUMNER" PROBLEM.

Many navigators undervalue "Sumner's" method in low latitudes; first, because of the small change of bearing between the usual times of taking the observations, and, secondly, because with a high altitude the circle of altitude or line of position is not to the; same extent a straight line on the chart. But in practice I have found "Sumner's" method give equally good, or better results in low latitudes than in high, if the observations are taken—or, at any rate, the second one is taken—within an hour of noon, or considerably less than an hour when in the tropics and latitude and declination are of the same name, in which case the "Sumner" or double-altitude method is all the more valuable, as an ex-meridian of the sun by itself would not give a dependable latitude unless the observation has been taken nearly an hour from the meridian. In low latitudes, when observations are taken on both sides of the meridian, 90° change of bearing may often be obtained within an hour, and by the aid of Blackburne's and Westland's exmeridian tables a good "Sumner" position may be very quickly and accurately obtained from ex-meridian east and west of the meridian. To illustrate this an extreme case is given in this work where the greater altitude is 89° , and the change in bearing in 5 m. amounted to 72° .

It is impressed on navigators in these pages by the numerous examples and illustrations following that the lines of position need never be of great length, so that they may always be considered as straight lines even in tropical latitudes. When D.R. latitude is very uncertain, and one of the observations has been taken anywhere near the meridian, it may be worked out as an ex-meridian, plotted on the chart, and combined with another observation taken nearer the prime vertical, which would be worked out for a longitude; or two ex-meridian observations may be be taken and plotted on the chart, examples of which are given on pp. 152 and 153. Reviewers of former editions of this work have been much struck with the simplicity and practical value of this problem. Although the work is simplified and graphically illustrated by plotting the latitudes or longitudes on the chart, the resulting position is readily obtained by calculation without the aid of chart, as shown on pp. 92 to 95.

As most ex-meridian tables and methods of calculation only give a correct latitude when the observation is taken not far from the meridian, a method is given in this work which gives a correct latitude corresponding to a given hour-angle when the sun or other celestial body is several hours away from the meridian. The D.R. latitude is not used in this calculation.

In obtaining the latitude by the double-altitude or "Sumner" method it is best, if the observations are taken on the same side of the meridian, for the same person to observe both; and generally the truest *latitude* will be found if both observations are taken on the *same* side of the meridian, as it is probable that, if for any reason the altitude is observed too high or too low, the same thing will occur in both observations. For the same reason the truest *longitude* will be found from observations taken on *different* sides of the meridian. An example to illustrate this is given on pp. 114 and 115.

REMARKS ON P.M. OBSERVATIONS.

Any one who is in the habit of regularly taking p.m. sights must have noticed the large differences which sometimes occur between a.m. and p.m. observations, which is generally attributed to current, and some men have even been led to believe from this that p.m. sights are not of any value, as though the sun—or, rather, the earth—did not move as uniformly in the afternoon as in the forenoon. The principal *difference* between the result of the two observations is probably generally due to erroneous altitude, especially in rough weather, and sometimes, of course, to erroneous latitude, and the mean of the results from the two observations will generally be nearest the true position. It has often been noticed when there is a heavy sea on that p.m. sights place the longitude a long way to the eastward of the a.m. ones, owing probably to the sun being observed on the top of a wave, and consequently, the altitude being too small, an error which in the morning would place the ship to the westward of the true position, but in the afternoon just as much to the eastward of it; so that, supposing the ship to be in latitude 48° and the sun to be 30° from meridian at each observation, an error in the latitude of 2' too little on both occasions would make a *difference* of 12' of longitude, as may be seen from Table D, on p. 80. Suppose, then, that on the same occasion both observations have been worked with an error of 2' south of the true latitude; this would make another difference of about $10\frac{1}{2}$ ' of longitude, making the p.m. sights $22\frac{1}{2}$ ' of longitude to eastward of the a.m. observation, and a slight easterly current in the interval between the two observations might easily make over 30' difference. Generally, no doubt, one of these errors will in a measure counteract another, but exceptional occasions are almost sure to arise when they will all combine in the same direction.

RULE FOR FINDING THE POSITION OF SHIP FROM TWO OBSERVA-TIONS BY AID OF TABLES A, B, AND C² WITHOUT THE USE OF , CHART.

FROM TWO CHRONOMETER OBSERVATIONS OF THE SUN.

(I.) Let two chronometer observations be taken at an interval of about an hour and a half or two hours,* and let the first be worked out with the D.R. latitude at the time of observation.

(2.) Let the D.R. latitude and longitude thus obtained be corrected for the run of the ship in the interval between the observations, and let the second observation be worked with the *corrected* latitude. Name these longitudes (1) and (2).

(2.) With the hour-angle, latitude, and declination at each observation, take out the difference of longitude correction from Tables A and B, and name the position-lines corresponding to these corrections according to the instruction under the heading of Table C² (p. 75).

Tables $A \pm B$ give the error in longitude due to 1' of error in latitude.

When both Position-lines go through the Same or Opposite Quadrants.

(3.) The *difference* between the two A and B corrections will give the difference in the resulting longitudes due to 1' of error in the latitude. (See example on p. 100.)

When both Position-lines go through Adjacent Quadrants.

(4.) The sum of the two A and B corrections will give the difference in the resulting longitudes due to 1' of error in the latitude. (See example on pp. 102 and 107.) The three elements used in the calculation of time, or longitude, are altitude,

The three elements used in the calculation of time, or longitude, are altitude, latitude, and polar distance. Presuming that the altitude and polar distance are correct, the resulting difference in longitude between the two observations must be due to error in the latitude. The sum or difference of the two A and B corrections give the difference of longitude in the two observations due to $\mathbf{1}'$ of error in the latitude used in the calculation, and the amount of error in the latitude will therefore be found by a simple proportion sum (see p. 100) from which it will be seen that the error or corrections to be applied to the D.R. latitude will be found by dividing the difference between longitudes (1) and (2) by the sum or difference of the A and B corrections. It must be applied to the latitude used in the *last* observation, and to the N. or S. according to whether the position-lines cut one another N. or S. of the D.R. latitude used in the calculation. The true longitude is then found by multiplying either of the A and B corrections by the latitude error, and applying the correction according to the trend of the position-line.

To prevent the possibility of making a mistake in the application of the correction to the latitude, a short horizontal line representing the parallel of D.R. latitude may be drawn with a free hand in the work-book; on this line put down longitudes (I) and (2), and roughly draw the position-lines through each longitude, following the rule for naming the position-lines given on p. 75, under the heading of Table C², also bearing in mind that if the line runs in a north-easterly direction it is equally
true that the line must also run in the opposite direction or south-westerly. No scale for longitude need be used, or protractor for laying down the bearings, but simply put longitude (τ) or (2) to the right or left of the other, as they are to the east or west of one another, then draw the general trend of the position-lines through these two longitudes, thus :—



FOR STELLAR OBSERVATIONS.

When finding the position of ship from stellar observations, it is best to observe the altitude of two stars which have a considerable difference in bearing from one another, and to take both observations within a few minutes of the same time. If the ship has not appreciably changed her position during the interval between the observations, both observations may be worked with the same latitude, and no correction for run need be applied to the first-observation latitude or longitude. Otherwise the same rules apply as for the observations by the sun.

When the ship has appreciably changed her position during the interval between the observations, rules Nos. 1 and 2 must be observed as in the sun observations.

FROM EX-MERIDIAN AND CHRONOMETER OBSERVATION COMBINED. 2880

Let two observations be taken with a suitable difference in bearing between them, and let the one nearest the prime vertical be used for a longitude (working it with the D.R. latitude), and the other one for a latitude, using the time deduced from the longitude found by observation in the calculation for latitude: bring both results up to the same instant of time by applying the run in interval between the observations.

Take out the A and B correction for the H.A. and latitude of each observation, and with this enter Table C² (p. 75) and take out the corresponding position-lines. We have then two latitudes and their corresponding position-lines starting from different points on the same meridian. Where these lines cut with one another on a plane chart will be the position of the ship.



From the figure representing these positions and position-lines it will be easy for any one having a knowledge of plane trigonometry to complete the calculation. For the sake of those who have not this knowledge, examples taken from the problems given in this book are now given to illustrate the different cases.

EXAMPLE I (p. 109).—Observations East and West of Meridian.

With lat. 41° o' S., long. by chron. from * Canopus gave 174° 30' E. and position-line S. $44\frac{1}{2}^{\circ}$ E.

S. $44\frac{1}{2}^{\circ}$ E. With long. 174° 30' E., lat. by ex-mer. of * a Centauri gave 41° 26' 40" S. and positionline N. 61° E.

For the figure. – From A, in lat. 41° o' S, and long. 174° 30' E., draw a meridian-line to B, in lat. 41° 26' 40'' S.; from A and B draw the lines S. $44\frac{1}{2}^{\circ}$ E, and N. 61° E. respectively to cut one another at C. From C drop a perp. on A B at D.

In the right-angled triangles ADC and BDC the angles at C will be respectively $45\frac{1}{2}^{\circ}$ and 29° , and therefore the angle at C in the \triangle ABC will = $74\frac{1}{2}^{\circ}$. We then have in the \triangle ABC, A = $44\frac{1}{2}^{\circ}$, C = $74\frac{1}{2}^{\circ}$, and AB = $26^{\circ}7^{\circ}$. First find *a*, then BD, and next CD.

	For	rmula.			
a = B I C I	$ A B \cdot D = a \cdot D = $	$\sin A \cdot co$ $\cos B$ $\cos C$.	osec C	;	
	A B B C	26.7' $44\frac{1}{2}^{\circ}$ $74\frac{1}{2}^{\circ}$	Log Sin Cosec	1°4265 9°8457 0°0161	
	a B	19'42' 61°	Log Cos	1.2883 9.6856	
Cor. for lat.	ΒD	9°42′	Log	0.9739	
	a C	19'42' 29°	Log Cos	1·2883 9·9418	
Cor. for long.	C D	17.0'	Log	1.5301	
Lat. by ex-mer. 41264 Cor. 92	0 S		Long. Cor.	by chron.	174 30 E 17 E
Correct lat. 41 17 1	7 S		Cor	rect long.	174 47 E

FROM TWO EX-MERIDIAN OBSERVATIONS ON DIFFERENT SIDES OF THE MERIDIAN.

Let two observations be taken with a suitable difference in bearing between them, one east and the other west of the meridian, deducing the hour-angle by applying the equation of time and longitude by D.R. Bring both results up to the same instant of time by applying the run in interval between the observations. The latitude from either observation (if worked by a correct method) is the latitude where the circle of altitude of the body observed cuts the meridian used in deducing the time. If both latitudes agree when observations have a considerable difference in bearing between them the longitude must be correct. If the latitudes do not agree the true latitude and longitude may readily be found by plotting on the chart, or by the formula used in preceding example, or by No. 2 method explained below.

Method No. 2.

By Aid of Table giving the Error in Latitude by Ex-meridian due to 4 sec. Error in Time or 1' of Longitude.

By the aid of the above-named table the double altitude problem may be worked from the meridian, on the same principle as two chronometer observations are worked from a parallel of latitude. If the azimuth is not over 70° (the limit of the table), the problem may be worked from the meridian with either an exmeridian and chronometer observation combined or from two ex-meridians.

When both observations are on same side of meridian, the difference between the two errors in latitude, due to 1' of error in the longitude, taken from the table, will be the divisor for the two differences of latitude resulting from the two observations, and will give the correction for the longitude used.

When one observation is east and the other west of meridian the error of longitude will be found by dividing the differences of latitude resulting from the two observations by the sum of the factors taken from the table. The error in latitude will then be found by multiplying the error in longitude by the correction taken from the table (in preference using the azimuth nearest to the meridian) and applying this to the ex-meridian latitude in the direction of the trend of the position-line, which is always at right angles to the bearing of object.

When the altitude is high and near the meridian the azimuth should be obtained by the time and altitude. This may be done either by Table D or by the rule of sines. (See examples on p. 105.)

94



Cor.

Long.

46 30°4 N

Lat. in

59 E

14 41'0 W

95

EXAMPLE 2 (p. 105). Both Observations on Same Side of Meridian.

à 5.665F

Long. 14 46.9' W.

EXAMPLE 3.-Two Ex-meridians on Different Sides of the Meridian. AT TIME OF 2ND OBSERVATION.

With long, D.R. 2° 35′ 40″ W., lat. by ex-mer. a.m. ⊙ Obsn. 10° 10·4′ S. and position-line for plane chart N. 64·8° W. With long, D.R. 2° 35′ 40″ W., lat. by ex-mer. p.m. ⊙ Obsn. 9° 55·9′ S. and position-line for plain chart S. 63·7° W. For the figure.—From A in lat. 10° 10·4′ S.'and long. 2° 35·7′ W. draw a meridian line to B at 9° 55·9′ S. and from A and B draw two lines N. 64·8° W. and S. 63·7° W. respectively to cut one another at C. From C drop a perpendicular on A B at D.

In the right-angled triangles A C D and B C D the angles at C will be respectively $25 \cdot 2^{\circ}$ and $26 \cdot 3^{\circ}$, and therefore the angle at C in the triangle A B C will equal $51 \cdot 5^{\circ}$. We then have in the triangle A B C, A = $64 \cdot 8^{\circ}$, C = $51 \cdot 5^{\circ}$, and A B (diff. lat.) = $14 \cdot 5'$. First find *a*, then B D = lat. cor., and C D = long. cor.





BY NO. 2 METHOD



P.1	M.obsn. ()'s Az N	26.7 W	gives (Table	M, pp. 156-1	(57) 50 S to Wd,
					Sum	'97 : 1' long"
	Lat. err '97'	or	Long.	Dif :: 14	f. lat. :5' :	Long. cor. 15' W.
	Lat. (2) Cor.	9 55'9 7'5	S S	Long. Long. cor.	^o 35'7 W 15'0 W	
5	Lat. in	10 3.4	S	Long. in	2 50'7 W	

Lat. (1) 10 10'4 S Lat. (2) 9 55'9 .97) 14.5 (15 × .5 = 7.5 S

REMARKS ON THE POSITION-LINE AND "SUMNER" PROBLEM IN CONNECTION WITH EX-MERIDIANS.

Although most navigators are now fully alive to the value of the position-line in connection with the longitude by chronometer, the value of the position-line in connection with the latitude by ex-meridian is seldom presented in works of navigation. It is generally supposed that an ex-meridian, if taken within a certain time from noon, will give a correct latitude, and that therefore the ship's line of position is anywhere on that parallel of latitude. This, however, is only the case when the ship time (which depends on the longitude) is nearly correct.

The further the object is in bearing away from the meridian the greater will be the error due to an error in the time. (See Table M, pp. 156 and 157). The time, however, might be uncertain to 4 or 5 minutes, and yet the ex-

meridian observation may be of great value in connection with the position-line, either when near the land by combining this line of bearing with some sounding or bearing of the land (see p. 170), or by combining it with another astronomical position-line, as in the "Sumner" problem. When the body which is used as an ex-meridian is within the limits of ex-meridian tables, an accurate starting point for a position-line may be obtained with very few figures. For cases where the body is outside the usual ex-meridian limits, a formula is here given (pp. 97 to 98) which will give a correct latitude for *any time* from the meridian corresponding to the true hour-angle of the sun or other heavenly body, and the latitude on an approximate D.R. longitude will give the starting point for the position-line which these tables give, cutting this longitude meridian, at that latitude.

It is very generally believed by navigators that an observation taken near the meridian is of no use in connection with the "Summer" problem. To some extent this is true when the problem is worked by the usually taught methods, and the D.R. latitude is much in error. I have endeavoured to show by the following examples how the ex-meridian problem may be combined with the chronometer observation in the "Sumner" problem : and, if this is done, it matters little how the sun or stars bear when the observations are taken, provided there is a suitable *difference* in bearing (say, 3 points or more) between the two position-lines.

The latest ex-meridian tables by Blackburne and Westland enable the navigator to very readily obtain his position from two ex-meridians, or by an exmeridian and chronometer observation, which may be worked as a double altitude, or plotted on the chart, just as accurately and even more rapidly than it could be done from two chronometer observations.

When observations are taken at the best possible time-shortly before sunrise and after sunset, when probably only three or four of the brightest stars are visible-we can not expect always to get two stars sufficiently far from the meridian and prime vertical as is considered by some necessary (*vide* "Wrinkles," gth Ed., p. 514) for a satisfactory double altitude to be worked on the "Sumner" principle. However, if advantage is taken of the methods shown in the following examples, it will be seen how little this matters. The only necessary condition of importance to insure good results is that the stars should be sufficiently far apart in bearing to give a good cut; and if one observation be near the prime vertical, and the other one near the meridian, the writer would say so much the better, rather than that this should be looked upon as an objection.

The following figures give the cases for any time from the meridian, when from a given hour-angle the latitude is required to be found.

LATITUDE BY EX-MERIDIAN WHEN OUTSIDE ORDINARY LIMITS,

CASE No. 1.—Object above the Pole, Angle at Z (= Bearing of Object) more than 90° reckoned from Observer's Pole.

In the spherical triangle Z P D, let Z P =co-lat., Z D = co-alt, and P D = Polar Dist.Given Z D, P D, and angle at P: to find PZ = co-lat.

From D drop a perpendicular on the meridian at M, then in the right-angled spher. triangle PMD we have PD and angle at P

to find PM = arc (r). Formula. -Cos $P = tan (r) \cdot cot PD :: tan (r) = cos P \cdot tan PD$.

Next find ZM = arc(2)

In the spher. triangle P M D, cos P D = $\cos(1) \cdot \cos M D$.

In the spher. triangle Z M D, $\cos Z D =$ $\cos(2) \cdot \cos M D$.

Cos (2) Cos Z D $\begin{cases} \cos (2) = \cos (1) \\ \cos Z D \\ \cdot \sec P D. \end{cases}$.: -... Cos (I) Cos P D PZ (co-lat. = arc (1) - arc (2).

Fig. 1. N Q Μ ñ F Ŵ z PM = Arc (1) ZM = ., (2) M Q = Comp. P Arc (1) ۰S

7-Azimuth.



By using the complements of PD and ZD, and comp. of PM for arc (1) when object is above the Pole, or comp. of ZM when object is below the Pole, the formula may be arranged as follows, and the rule as below applied:—

OBJECT ABOVE THE POLE.

Cot arc $(1) = \cos H.A. \times \cot decl.$ Cos arc $(2) = \csc decl. \times \sin arc (1) \times \sin alt.$ Name arc (1) same as decl. Name arc (2) contrary to bearing of object—*i.e.*, N. or S. of the prime vertical. Add like and subtract unlike names. Sum or diff. of arc (1) and arc (2) = latitude.

OBJECT BELOW THE POLE.

Tan arc $(I) = \cos$ suppt. of H.A. \times cot decl. Sin arc $(2) = \csc$ decl. $\times \cos$ arc $(I) \times \sin$ alt. Name both arc (I) and arc (2) same as the decl. Latitude = sum of arc (I) and arc (2) always named same as the decl.

NOTE.- It is not advisable to use the formulæ here given when other methods can be used, if the declination of object is within 3° or 4° N. or S. decl. If it is then used, six-figure logarithms should be taken out, and the corrections made for odd seconds of arc.

Examples in the use of these formulæ are given in the problems following.

FORMULÆ FOR EX-MERIDIANS.

WORKED-OUT EXAMPLES TO ILLUSTRATE EACH CASE.

As some have been puzzled in trying to follow the ex-meridian formulæ from the figures here given when latitude and declination are of contrary names, owing to P D and P M being over 90° , the reader is reminded that to take out the tan and sec of an arc if over 90° he must take out the cotan and cosec of amount in excess of 90° . If the *rule* is followed independently of the figure this confusion will be avoided, as decl. and alt, are used, instead of P.D. and Z.D.

Examples of each case, following either figure or rule, are here fully worked out which can be easily followed.

CASE NO. 1.-Hour-angle 2 h. 17 m. 10 s., Lat. S., Decl. 23° N., and Altitude 16° N. Required the latitude.

FORMULA FROM THE FIGURE.

Co

FORMULA DEDUCED AS PER RULE.

H.A. PD	н. м. s. 2 17 10 113 ⁰	Cos 9'91707 Tan 0'37215	Sec 0'40812	H.A. Dl.	н. м. s. 2 17 10 23° N	Cos 9'91707 Cot 0'37215	Cosed	0'40812
PM	117° 11 <u>1</u> ′	Tan 0'28922	Cos 9.65989	Arc (1) 27° 11½' N	Cot 0'28922	Sin	9.65989
		ZD 74°	Cos 9'44034			Alt. 16°	Sin	9'44034
$Z\mathrm{M}$	$71 \ 11\frac{1}{2}$		Cos 9'50835	Arc (2)71 11 <u>1</u> S		Cos	9'50835
Co-lat. PZ	46 O			Lat.	44 o S			
Lat.	44 o S		1					

CASE No. 2.—Hour-angle 1 h. 38 m. 12 s., Lat. N., Decl. 40° N., and Altitude 61° N. Required the latitude.

	H.A. PD	1 38 12 50°	Cos 9 · 95885 Tan 0·07619	Sec 0'19193	H.A. 1 38 12 Decl. 40°	Cos 9'95885 Cot 0'07619	Cosec 0'19193
	$\mathbf{P}\mathbf{M}$	47° 1812'	Tan 0'03504	Cos 9'83126	Arc (1) 42° 41 ¹ / ₂ N	Cot 0'03504	Sin 9.83126
			Z D 29°	Cos 9'94182		Alt. 61°	Sin 9'94182
	Z M	22 $41\frac{1}{2}$		Cos 9'96501	Arc (2) 22 41 ¹ / ₂ S		Cos 9'96501
-lat.	Р <i>Z</i>	70 0			Lat. 20 0 N		
	Lat.	20 O N					

CASE No. 3.-Hour-angle 9 h. 23 m. 47 s., Lat. S., Decl. 62° 34' S., and Altitude 22° S. Required the latitude.

	H.A.	н. м. s. 9 23 47 12 0 0			H. M. S. H.A. 9 23 47 12 0 0		
	Supt. PD	2 36 13 27° 26'	Cos 9 ^{.8} 9017 Tan 9 ^{.71524}	Sec 0'05181	Supt. 2 36 13 Decl. 62° 34' S	Cos 9 ^{.8} 9017 Cot 9 ^{.71524}	Cosec 0'05181
	РМ	21° 57 ¹ ′	Tan 9'60541 Z D 68°	Cos 9'96731 Cos 9'57357	Arc (1) 21° 574' S	Tan 9.60541 Alt. 22°	Cos 9'96731 Sin 9'57357
	<i>Z</i> M	66 57 1		Cos 9.59269	(Comp) Arc (2) 23 2 ⁸ / ₄ S		Sin 9'59269
Co-lat.	$\mathbf{P}Z$	45 O			Lat. 45 0 S		
	Lat.	45 o S					

The accuracy of this method may easily be proved by reversing the process, and finding the hour-angle from the latitude, declination, and altitude given.

Case No. 3 is especially useful, as with high-declination stars the latitude will generally be fairly correct, even when the time is in error a couple of minutes and the body observed is an hour or more from the meridian below the Pole. For instance, in the latitudes of last example, an ex-meridian of $* \alpha$ Crucis with hour-angle 11 h., or 1 h. from meridian below the Pole, and 2 m. of error in the time used, would only cause an error of $2\frac{1}{2}$ ' in the resulting latitude.

DOUBLE-ALTITUDE POSITION BY TWO SUN OBSERVATIONS.

1902 .- March 29th, p.m., the following observations were taken in the artificial horizon, at 56 Hawker Street, Wellington :-

D. H. M. S. M. T. G. by chron. 28 13 17 31 " 28 15 51 18 Obsd. alt. of 0 89 0 30 # "

Required the true bearing of the sun at each observation, and the position of place, assuming latitude to be 41° o' S. Index error of sextant + 1' 23''; ther. 70° ; bar. 30° oin.

52 5 10

	IST OBS	SERVATION.		2ND OBSERVATION.					
M. T. G.	D. H. M. S. 28 I3 I7 3I	Dl. var. 58.52 × 10.71	и М.Э	г.G. <u>28</u>	н. м. s. 15 51 18	Dl. var. 58'51 × 8'15			
Before noon, 29 Eq. T. var.	oth 10 42 29 S. H. 0'7б7 × 10'7	Cor. $\stackrel{\circ}{-}$ 10 26.7 Dl., 29th 3 7 20.7	Befe N Eq.	T. var.	8 8 42 = 8'15 hr. s. H. $767 \times 8'1$	Cor. $-\frac{0}{7}, \frac{7}{56.8}$ Dl., 29th 3 7 207 N			
Cor. Eq. T., 29th	M. S. + 8'2 5 5'1	Cor. Dl. 2 56 54 P. D. 92 56 54	N Cor Eq.	- T., 29th	M. S. + 6'2 5 5'I	Cor. Dl. 2 59 24 N P. D. 92 59 24 1			
Cor. Eq. T.	5 13'3 + A	. T.	Cor	. Eq. T.	5 11.3				
Obsd. alt. Ō I. E.	[°]			Obsd. alt. ⊙ I. E.	52 5 10 + 1 23				
	2)89 1 53				2) 52 6 33				
App. alt. Ref. and par.	44 30 56 · 5 50·5			App. alt. Ref. and par	26 3 16.5 - 1 44				
Semi-d.	44 30 6 - 16 2			Semi-d.	26 I 32.5 - I6 2.5				
T. alt. Lat. P. D.	44 I4 4 4I 0 0 92 56 54	Sec 0'122220 Cosec 0'000575		T. alt. Lat. P. D.	25 45 30 41 0 0 92 59 24	Sec 0'122220 Cosec 0'000591			
•.	178 10 58				159 44 54				
S – A	89 5 29 44 51 25	Cos 8 200237 Sin 9 848398		S = A	79 52 27 54 6 57	Cos 9 [.] 245045 Sin 9 [.] 908594			
H.A. Eq. T.	oh 55m 58.6s + 5 13.3	Sin ² 8.171430		H.A. Eq. T.	3h 26m 8.8s + 5 11.3	Sin ² 9 ^{.276450}			
M. T. place M. T. G.	29 I I II'9 28 I3 I7 3I'0	A 3'49 N B 22 N		M. T. place M. T. G.	29 3 31 20 [.] 1 28 15 51 18 [.] 0	A '69 N B '07 N			
Long. in T.	II 43 40'9	Cor. 3'71 N		Long. in T.	II 40 2'I	Cor. '76 N			
Long. (1)	175° 55' 13" E	C gives Az. N 19.7°	w	Long. (2) Long. (1)	175 0 31 E 175 55 13 E	C gives Az. N 60'2°W			
	T. C ² giv	N 75° E	chart	Diff. long.	54 42 = 54	Posline T. C ² N 37 ^{·2³} E			
		Long. (1) cor. = ; Long. (2) "	3'71 N to E '76 N to E	(1) to A (2) to A	} in Fig.				
		D. long.	2'95 : d. lor	ng. 54'7 :: lat	. 1 : lat. cor. 18.5				
	A (2) 2.9	5 (1)	Lat. used 4 Cor.	.1 0 0 S 18 30 S	Long. (2) $18.5' \times .76' =$	$ $			
1.0	° Co	or. to S	Lat. in 4	1 18 30 S	Long. in	174 46 27 E			

In this example, with the latitude used in the calculation $17\frac{1}{7}$ in error, the resulting latitude is 1' in error. This is due to the sun's azimuth differing nearly 2° at the position corresponding to the hour-angle found with 41° lat. from that of the true hour-angle and latitude. If the position had been worked in the usual way as given in the Board of Trade examinations with two latitudes, say, 17° in error on each side of the true latitude, the resulting latitude would have been just 2' north of that here found, or 1' north of the true latitude. When the hour-angle is small, and the two latitudes used on each side of the true latitude, use a ship on the Equatorial side of the true latitude are far apart, the resulting position-line always places the ship on the Equatorial side of the true latitude is even the robier of 30° in the D.R. latitude in either case will sometimes make 2' of 3' error in the latitude. When one of the hour-angles is not far from the meridian, as in this case, the problem as worked on the following page will give a more accurate position, and the work is not longer. more accurate position, and the work is not longer.

These observations when reworked on the same principle, when using a latitude near the the truth, give the latitude of position within o'r' of the truth. Several observations were taken at the same time, and all the resulting latitudes agreed within a few seconds of one another.

For position of place plotted on the chart, see chartlet on next page.

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DOUBLE-ALTITUDE POSITION BY TWO SUN OBSERVATIONS

(COMBINING CHRON. LONG. OBSERVATION WITH AN EX-MERIDIAN).

1902.—March 29th, p.m. In assumed latitude 41° o' S. the true altitude of sun's centre was 44° 14' 4" when a chronometer showed M. T. G. 28 d. 13 h. 17 m. 31 s. ; and again on the same afternoon the true altitude of sun's centre was found to be 25° 45' 30'' when a chronometer showed M. T. G. 28 d. 15 h. 51 m. 18 s. Required the position of place by projection on the chart.

	IST OB	SN. WEST OF M	feridian.		2ND OBSN	. West	of Merid	IAN.
M. T. Gre Long. in T	enwich . by 2nd obsn.	D. H. M. S. 28 13 17 31 + 11 40 2 E			T. alt. Lat.		⁰ 4 4 25 45 30 41 0 0	sec
M. T. plac Eq. T.	e				r, D.		92 59 24 159 44 54	cosec
⊙'s H.A.		0 52 20	Cos 9'988578		S		79 52 27	cos
⊙'s Dl.		2° 56' 54" N	Cot11'288163 Cose	c11.288738	3 - A		54 0 57	5111
Arc (1)	3 1 36 N		Cot 11.276741 Sin	8.722640		Sec Cosec	0'122220	
		True a	lt. 44° 14' 4" Sin	9*843604		Cos Sin	9°245045 9°908594	
Arc (2)	44 15 56 S		Cos	9'854982		Sin^2	9.276450	
Latitude	41° 14' 20" S							
					H.A.= Eq. T.	A.T.plac	$H. M. S. e_3 26 8.8 + 5 11.3$	
		oh. 5	2 m.)		М. Т. р М. Т. С	lace 29 5. 28	3 31 20'I 15 51 18	
		Dl. 3°	$N \int B 23 N$		Long. i	n T.	11 40 2'1	
	Posline from	n Table C ² N	76° E 4.03 N		Longitu	ide i	75° 0′ 31″ E	

Position by Chart. Lat. $41 imes 17\frac{1}{2}$ S Long. 174 47 E

H L D	.A. 3h. 261 at. 41° S l. 3° N	n. A B	·69 ·07	N N
Posline from Table C	² N 37 ² °	E	•76	N



Position by two chron. observations = Lat 41 181 S. (see previous page) Long. 174 461 E.

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The following example is taken from Captain Thompson's excellent book, "Navigation Simplified," which, I presume, is now in the hands of nearly all those navigators who desire to obtain the highest certificates. This example is taken as the work is there given in detail, with the plotting on the chart, so that the reader can compare the working, and see for himself the saving in figures, while maintaining equal, if not greater, accuracy by using the A and B Tables.

POSITION BY DOUBLE ALTITUDE OF SUN.

1900.—July 2nd, at about 6 h. 50 m. a.m., and again at 11 a.m., from the following observations :—

Mean Time at Greenwich by Chron.	True Altitude of the Sun's Centre
D. H. M. S. I 7 43 12 I II 57 36	25 51 6 69 50 25

Find the true bearing of the sun when the first altitude was observed, and the position of the ship when the second altitude was taken, assuming the ship to be between latitudes 49° 50' N. and 50° 20' N. The ship's course and distance between the observations was N. 67° W., dist. 30 miles.

ıst obsn. ⊙'s Cor. Dl.=	= 23 6 49 N	M. S. Cor. Eq. T. 3 35+A. T.	2nd obsn. ⊙'s Cor.Dl.=	23	ć	7 N	м. s. Cor. Eq. T. з 36 [.] 4
	<u>9</u> 000			90	0	0	
N. P. D.	66 53 11		N. P. D.	66	53 5	53	

Run betwe	en observatio	ons, N	67° W 30 m. = 11.7' Ν	27.6' W	= 43' d. long.		Lat. (1) Run. d. la	49 :	50	0 N 42 N
A L P	1ST OBSN. 25 51 6 49 50 0 66 53 11	Sec Cose	0'190431 c 0'036340	A L P	2ND OBSN. 60 50 25 50 1 42 66 53 53	Sec Cosec	Lat. (2) 0.192188 0.036302	50	I	42 N
S S – A	142 34 17 71 17 8.5 45 26 2.5	Cos Sin	9`506301 9`852750	S S – A	$ \begin{array}{r} 177 \ 46 \ 0 \\ $	Cos Sin	8'289773 9'672223			
H. A. east A. T. ship	H. M. S. $24 ext{ o 0}$ $-5 ext{ 6 58}$ $18 ext{ 53 } 2$	Sin ²	9.585822	H.A. A. T. ship	H. M. S. 24 0 0 $- 0 57 13^{\circ}5$ $23 2 46^{\circ}5$	Sin ²	8.190486			
Eq. T. M. T. S. M. T. G.	+ 3 35 18 56 37 7 43 12	A B C	[•] 28 S • <u>44</u> N • <u>16</u> N gives Az. N 84° E	Eq. T. M. T. S. M. T. G.	$ \begin{array}{r} + & 3 & 36^{\circ}5 \\ \hline 23 & 6 & 23 \\ 11 & 57 & 36 \\ \end{array} $	A B T.C	4.68 S 1.72 N 2.96 S P	osnl	ine	for
Long. in T	. 11 13 25	Pos Ta	line for plane chart, ble C ² , gives N 9 [.] 1° W	Long. in T	. 11 8 47		_	S 71 See T	'3° ab	W. le C ²
Long. Run d. long	168 21 15 E 3. 43 0 W			Long. (2) Long. (1)	167 11 45 E 167 38 15 E	2.96	S to W as N to W	nd N	to	Е
Long. (1) Cor 16' × 8	167 38 15 E 5′ 1 22 W			D. long.	26' 30"	3.13	sum of A	and I	3 c	or.

Long. in 167 36 53 E at time of 2nd observation.



For position of ship when plotted on the chart, see chartlet on next page.

DOUBLE ALTITUDE OF THE SUN

(COMBINING CHRON. LONG. OBSERVATION WITH AN EX-MERIDIAN).

1900.—2nd July, at about 6 h. 50 m. a.m., and again at 11 a.m., from the following observations :—

Mean Time at Greenwich by Chron.

D.

I

True Altitude of the Sun's Centre.

н.	м.	s.	
7	43	12	

 $\begin{array}{c}
\circ & ' & '' \\
25 & 51 & 6 \\
60 & 50 & 25
\end{array}$

1 11 57 36

60 5

Find the true bearing of the sun when first altitude was observed, and the position of the ship when the second altitude was taken, assuming the ship to be between latitudes 49° 50' N. and 50° 20' N. The ship's course and distance between the observations was N. 67° W., dist. 30 miles.

Ist obsn.
$$\bigcirc$$
's Cor. Dl. = $\stackrel{\circ}{23}$ '6 $\stackrel{\circ}{49}$ N
 Cor. Eq. T. = $\stackrel{\circ}{3}$ $\stackrel{\circ}{33}$ + A. T.

 $\stackrel{90}{0}$ $\stackrel{\circ}{0}$ $\stackrel{\circ}{0}$
 N. P. D.
 $\stackrel{\circ}{66}$ $\stackrel{\circ}{53}$ $\stackrel{\circ}{11}$
 Cor. Eq. T. = $\stackrel{\circ}{3}$ $\stackrel{\circ}{36'}$ + A. T.

 2nd obsn. \bigcirc 's Cor. Dl. = $\stackrel{\circ}{23}$ $\stackrel{\circ}{6}$ $\stackrel{''}{7}$ N
 Cor. Eq. T. = $\stackrel{\circ}{3}$ $\stackrel{\circ}{36'}$ + A. T.

 $\stackrel{\circ}{N}$ N. P. D.
 $\stackrel{\circ}{66}$ $\stackrel{\circ}{53}$ $\stackrel{\circ}{53}$
 Cor. Eq. T. = $\stackrel{\circ}{3}$ $\stackrel{\circ}{36'}$ + A. T.

Run between observations, N 67° W $_{30}$ m. = 27° 6 m. dep. = 43' W d. long.



Cor. Table C $\frac{16}{16}$ N gives Az. N 84'1° E and Pos.-line for plane chart, Table C², N 9° W



For above Problem.



With the desire to show the especial utility of these tables for obtaining accuracy of position and conciseness in work, and the superiority of the method here advocated over the method still employed in the Board of Trade Examinations of Masters and Mates, for the "Summer" problem, the following example is given and plotted on the chart by both methods. For the sake of better illustrating the possible error due to the old method, a wider range of latitude has been taken than is usually given in the examination papers, though, considering the high speed of some of the present-day steamers, the range is not excessive, as the run in interval itself might often amount to over 1° of latitude

"SUMNER" PROBLEM AS GIVEN IN THE B. OF T. EXAMINATIONS.

1898.—On 20th June, a.m., at ship, at sea, and uncertain of my ship's position: when a chronometer indicated M. T Green. 19d. 22 h. 30 m. the true altitude from some consistent matrix and again, a.m. on same day, when chronometer indicated 20 d. oh. 16 m. the true altitude of sun's centre was 65° 18', the ship having made 23 miles on a true N. 24° E. course during the interval between the observations. Required the line of position and true bearing of the sun at time of 1st observation ; and the position of the ship when 2nd observation was taken assuming latitudes 46° N. and 47° N.

rst obsn.	M. T. Green. Eq. of time	D. H. M. S. 19 22 30 0 - 1 16'7	2nd obsn.	D. H. M. S. 20 0 16 0 - I 17'7	Decl. 23 27 N 90 0
	A. T. Green.	19 22 28 43'3	A. T. G.	20 0 14 42'3	P. D. 66 33

0			IST OBSERVATION	•	0 /		
A 52 9 L 46 0 P 66 33	Sec Cosec	0°158229 0°037438		A L P	52 9 47 0 66 33	Sec Cosec	0*16621 7 0*037438
164 42					165 42		
$S = A = \frac{82 \ 21}{30 \ 12}$	Cos Sin	9°124248 9°701585	3	s-	A 30 42	Cos Sin	9*095056 9*708032
H.A. D. H. M. S. 2 31 18'8 E	Sin^2	9'021500		H. A.	о. н. м. s. 2 28 40'3 Е	Sin ²	9*006743
A. T. ship 19 21 28 41'2 A. T. G. 19 22 28 43'3				A.T.ship A.T.G.	19 21 31 19'7 19 22 28 43'3		
Long. in T. I O 2'I				Long. in T	0 57 23.6		
Long. A $15^{\circ} \circ 31'' W$				$\frac{\text{Long. B}}{=}$	14° 20′ 54″ W		

2ND OBSERVATION.

A 65 18 L 46 0 P 66 33	Sec Cosec	0*158229 0*037438	i	A L P	65 18 47 0 66 33	Sec Cosec	0 *166217 0*037438
$\begin{array}{c} 177 51 \\ \hline 88 55\frac{1}{2} \\ S-A 23 37\frac{1}{2} \end{array}$	Cos Sin	8°273260 '9°602872		S S – A	178 51 89 25 1 24 73	Cos Sin	8.001538 9.611435
H.A. D. H. M. S. 0 49 53'I E	Sin ²	8*071799	Н.А.	D.	н.м. s. 037 9*2 Е	Sin ²	7.816628
A.T. ship 19 23 10 6'9 A.T G. 19 24 14 42'3			A.T.s A.T.C	hip 19 G. 19	23 22 50 [.] 8 24 14 42 [.] 3		
Long. in T. I 4 35'4			Long.	in T.	0 51 51.2		
Long. C 16° 8' 51" W			Long.	D	12° 57' 52" W		
				-		-	

Line of position N 24¹/₂° E Sun's bearing S 65¹/₂° E

Position at 2nd obsn. Lat. 46° 27' N Long. 14° 43' W True posn.--Lat. 46° 30' 20" N Long. 14° 41' 0" W





SUMNER PROBLEM FACILITATED BY A, B, AND C² TABLES.

1898.— On 20th June, a.m., at ship, at sea, and uncertain of my ship's position: when a chronometer indicated M. T. Green. 19d. 22h. 30m. the true altitude of sun's centre was 52° 9'; and again on same day when chronometer indicated 20d. 0h. 16m. the true altitude of sun's centre was 65° 18', the ship having made 23 miles on a true N. 24° E. course during the interval between the observations. Required the line of position and true bearing of the sun at time of 1st observation; and the position of the ship when 2nd observation was taken, assuming D.R. latitude to be 46° N. when 1st observation was taken.

IST OBSN.		2	2ND	OBSN.		i	>	
D. H. M. T. Green. 19 22 3 Eq. of time –	1. S. 0 0 1 16'7		M.T.G. Eq. of time	D. H. M. S. 20 0 IG 0 - I I7'7	Run N $\overset{\circ}{_{24}}$ Lat. (1)	E ${}^{M.}_{46^{\circ}}$ ${}^{O}_{O}$ N	9'4 E = 1	3.6 d. long.
A. T. Green 19 22 2	8 43'3		A.T. Green. Long. (1)	- 0 14 42'3 - 0 59 7'7 W	Lat. D.R.	46 21 N	at time of	2nd obsn.
Decl. 23° 27'	N = P.D.	66° 33'	A.T. ship	19 23 15 34 ^{.6} 24 0 0				
$ \begin{array}{cccc} A & & & \circ \\ L & & 46 & \circ \\ P & & 66 & 33 \\ \hline & & 164 & 42 \end{array} $	Sec Cosec	0.158229 0.037438	H.A.	0 44 25.4	Az. (H.A.) Lat. (decl.) Lat. (alt.)	For Az. by M. 44'4 = 11 23'5'' 65'3'') (p. 4	Table D. 'I) (p. 8 N) M = 32)	1) : 22'6
	Cos Sin	9 [.] 124248 9 [.] 701585			М. А&В	22'6 } give (1 3'10' gives (Plan	s Áz. 25°, v o. 49) A & p. 75) po: e Chart N	vhi c h gives B 3'10'. snline for . 72° E.
H.A. D. H. M. S. 2 31 18	8 Sin ²	9.021500						
A.T.ship 19 21 28 41 A.T.G. 19 22 28 43	- 2 H.A. 3 Lat.	$\frac{2 h. 32 m.}{46^{\circ} N}$	A 1°33 S B 0'71 N		LAT	. by'Ex-mer	. TABLE	No. 3.
Long. in T. I 0 2	·I Dl.	$23\frac{10}{2}$ N	C 0.62 S	gives Az. S 66.7 E.	Decl.	23° 27' N	Arc. cor.	+ 23.8
Long. 15° 0' 31' Run. d. long. 13 36	E C	C ² gives Post	nline for pla	ne chart N 31.8° E	Arc (1)	••••		23 50.8 N
Long. (I) I4 46 55	W	60 art N an	d Deen line l	N and E	A	° ′	A	0 /
Long. in T. oh 59m 7	7 ⁸	40° 21' N an	i rosniiile i	N 32" E	Alt.	65 18 S	Z D	24 42'0 N
:		Position fro	om chart.—L	at. 46 30 5 N	ZD	24 42 N	Arc (2)	22 37'8 N
			L	ong. 14 41.0 W			Lat.	46 28.6 N

RULE FOR FINDING LATITUDE BY EX-MERIDIAN TABLE No. 3 (ABOVE POLE OBSERVATION).

With declination at side and hour-angle from top take out arc reduction.

Add this reduction to the declination for arc (1). Name it the same as declination.

With altitude at the side and azimuth from the top take out 2nd arc reduction.

Subtract the reduction from Z D for arc (2). Name arc (2) contrary to bearing of object.

Latitude = arc (1) \pm arc (2).

+ when arcs are of like names.

- when arcs are of unlike names.



Nore.—This problem worked by the old method (which is still used in the Board of Trade examinations) would give a result $3\frac{1}{2}$ ' in error in the latitude and 2' in error in the longitude. (See page 104.)

EXAMPLE TO SHOW METHOD OF FINDING THE TRUE LINE OF POSITION OR CIRCLE OF ALTITUDE BY USE OF THE A AND B TABLES.

This is given in response to an inquiry by a correspondent, who asked for an explanation of author's remark about the tables doing this, in the preface to the first edition in 1883.

	EXAMPLE	PLOTTED	ON	CHARTLET	FACING	PAGE	104.
--	---------	---------	----	----------	--------	------	------

Lat. $\stackrel{0}{46}$ o N A 4 77 S Dl. 23 27 N B 2 275 N H. A. 0 49 E C 272 S to W or N to E Cor. for 10' N = 27'2 E = 1 49	Lat. $4\hat{6}$ o gives Long. $1\hat{6}$ 8.9 W Cor. for 10 N = 27'2 E Lat. $4\hat{6}$ 10 N gives Long. $15 41'7$ W	H. M. S H.A. $0 \ 49 \ 53$ $-1 \ 49$ $0 \ 48 \ 4$ $-1 \ 0$ $0 \ 47 \ 0$ for next.
Lat. $\stackrel{\circ}{46} \stackrel{1}{15} \stackrel{N}{N}$ A $\stackrel{\circ}{5} \stackrel{\circ}{25} \stackrel{N}{25} \stackrel{N}{B}$ B $\stackrel{\circ}{2} \stackrel{1}{12} \stackrel{N}{N}$ H. A. $\stackrel{\circ}{0} \stackrel{47}{47} \stackrel{E}{E}$ C $\stackrel{\circ}{2} \stackrel{90}{290} \stackrel{S}{5}$ Cor. for 10' N = 29'0 E = 1 56	Lat. $\stackrel{46}{}_{10}$ io N gives Long. $\stackrel{15}{}_{15}$ 41'7 W Cor for 10 N = 29'0 E Lat. $\stackrel{46}{}_{20}$ N gives Long. 15 12'7 W	H. M. S. H.A. 0 48 4 -156 0 46 8 -10 0 45 0 for next.
Lat. 46 25 N A 3'28 S Dl. 23 27 N B 2'22 N H.A. 0 45 E C $3'06$ S Cor. for 10' N = 30'6 E = 2 2	Lat. 46 20 N gives Long. 15 127 W Cor. for 10 N = 30.6 E Lat. 46 30 N gives Long. 14 42.1 W	H. M. S. H.A. $0\ 46\ 8$ $-\ 2\ 2$ $0\ 44\ 6$ $-\ 1\ 0$ $0\ 43\ 0$ for next.
Lat. 40 35 N A 556 S Dl. 23 27 N B 232 N H.A. \circ 43 E C 324 S Cor. for 10' N = 32'4 E = 2 10	Lat. $46 \frac{4}{30}$ N gives Long. $14 \frac{42}{14}$ W Cor. for 10 N = $32'4$ E Lat. $46 \frac{4}{0}$ N gives Long. $14 \frac{9'7}{14}$ W	H. M. S, H.A. $0 44 6$ -2 10 0 41 56 -1 6 0 40 50 for next.
Lat. $40^{\circ} 45^{\circ} N$ A $5^{\circ} 88^{\circ} S$ Dl. $23^{\circ} 27^{\circ} N$ B $2^{\circ} 44^{\circ} N$ H.A. $0^{\circ} 41^{\circ} C$ $3^{\circ} 44^{\circ} S$ Cor. for 10' N = $34'4^{\circ} E = 2^{\circ} 18^{\circ}$	Lat. 4640 N gives Long. 1497 W Cor. for 10 N = 34'4 E Lat. 4650 N gives Long. $1335'3$ W	H. M. S. H.A. 0 41 56 - 2 18 0 39 38 - 1 10 0 38 28 for next,
Lat. 4° 55 N A 6 30 S Dl. 23 2 N B 254 N H. M. H. A. 0 381 C 376 S Cor. for 10' N = 376 E = 2 30	Lat. 4°_{0} 50 N gives Long. 1°_{3} 35' 3 W Cor. for 10 N = 37' 6 E Lat. 4°_{7} 0 N gives Long. 12 57' 7 W	

[Note.—It will be seen that as the latitude increases so the H.A. will decrease, according to the change of longitude, 15' of long, making 1^{m} change of time in the H.A. Therefore, to get the true cor. we must use the *mean* H.A. and the *mean* lat. corresponding to the two parallels which we require the cor. for. The long, found by the application of the A and B cor. at 47° N is practically the same as that found by direct calculation.]

DOUBLE-ALTITUDE POSITION BY TWO STELLAR OBSERVATIONS.

1902.—On 15th March, p.m., the following observations were taken in the artificial horizon, at 56 Hawker Street, Wellington: True position from chart, lat. 41° 17′ 32″ S., long. 174° 46′ 57″ E.:—

Required the true bearing of both stars, and the position of place, assuming latitude to be 41° o' S. ($17\frac{1}{2}$ ' in error). Index error of sextant + 1' 20''.

M.T.G. M. ⊙'s R	D. H. M. $14 \ 21 \ 6$ A. $+ \ 23 \ 28$	S. 6 Sid. T. (8'45 Accl. 21 b	H. M. S. G. noon) $23 \ 24 \ 40^{\circ}46$ h. 6m. + 3 27'99	M.T.G. M. ⊙'s R.A. Sid. T. G	H. M. S. 22 26 7 23 28 21.6	Sid. T. (G. noon) Accl.	H. M. S. 23 24 40'46 + 3 41'13 22 28 21'50
Ju. 1. 0.	20 34	* SIRIUS TO	N.Wo.	• • • • •	CANOPUS TO	S.WD.	
OI I.	osd. alt. of ÷ E.	° ′ ″ ¥ 116 33 0 + 1 20	D1. $16_{35} 14_{5}$ $90_{0} 0$	Obsd. alt. of X I. E	0 1 " 112 10 10 + 1 20	Dl. 52 38 90 0	59 S
Ap Re	2 op. alt.	$ \begin{array}{r} 58 17 10 \\ - 34 \end{array} $	P. D. <u>73 24 46</u>	2 App. alt. Ref.) 112 11 30 56 5 45 - 38	P. D. <u>37</u> 21	I
A L P		58 16 36 41 0 0 73 24 46	Sec 0'122220 Cosec 0'018460	A L P	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Sec 0'12 Cosec 0'21	12220 17036
S	- A	86 20 41 28 4 5	Cos 8 [.] 804503 Sine 9 [.] 672578	$\frac{\varepsilon}{S-A}$	67 I3 4 II 7 57	Cos 9'58 Sin 9'28	37969 35798
*	's H.A. 's R.A.	H. M. S. I 34 0°2 6 40 51°6	Sine ² 8.617761	米 's H.A 米 's R.A.	н. м. s. 3 10 41'3 V 6 21 47'6	N Sin ² 9'21	13023
Si	d. T. place "Green.	8 14 51 [.] 8 20 34 14 [.] 45	A 2.00 N B .75 S	Sid. T. place. Sid. T. Green	9 32 28.9 21 54 28.6	$\frac{B}{C} = \frac{1.77}{0.08} \frac{S}{S} t_0$	я
Lo	ong. in time	11 40 37'35	C 1'25 N to	Long. in time	11 38 0.3		
Lo 17 Lo	ong. (1) '6' × 1'25' ong. in	$\begin{array}{c} 175^{\circ} & 9' & 20'' \\ 22 & 0 \\ \hline 174 & 47 & 20 \\ \hline \end{array}$	gives Az. N 46.6° W and C ² gives Posline N $51^{\circ}3 E$	Long. (2) Long. (1) Diff. long.	$\frac{174^{\circ} 30' 5'' E}{175 9 20}$ $39' 15''$	and C ² gives Pos. S 44'4° E	··line
			3 51 3 11				

Long. (1) cor. = 1^{25} S to W (2) , 0^{98} S to E

101

1...

D. long. 2'23 : d. long. 39'25' :: lat. I' : lat. cor. 17'6'

	Lat. used Cor.	4 [°] 0 0 S 17 36 S	Long. by Canopus 17'6' × 0'98' =	1 74	; 30 17	5 15	E E
Cortos	Lat. in	41 17 36 S	Long. in	174	47	20	E

The above were *bona fide* observations taken on a windy night, needing patience to wait till the quicksilver was quite steady; being on different sides of the prime vertical, the observations naturally give a good latitude, as 1' error of altitude due to instrument or refraction would make practically *no* difference in the resulting latitude. This problem reworked with a latitude near the truth only makes a few seconds difference in the resulting position.

[Note.-A, true alt.; L, lat.; P, Polar dist.; S, half sum of A + L + P; S - A, diff. between S and A; H.A., hour-angle.]

DOUBLE-ALTITUDE POSITION BY TWO STELLAR OBSERVATIONS.

1902.—On 15th March, p.m., the following observations were taken in the artificial horizon:—

D. H. M. S. M.T. at Greenwich by chron. 14 21 23 43 Obsd. alt. of * a Centauri 69 36 50 to S.Ed. " " 14 22 26 7 " Canopus 112 10 10 to S.Wd.

Required the true bearing of both stars, and the position of place, assuming latitude to be 41° o' S. Index error of sextant + 1' 20".

	IST OBSERV	VATION.	2ND OBSERVATION.						
M. T. Green. Sid. T. (G. noon) Accl.	H. M. S. 21 23 43 23 24 40'46 + 3 30'89	Dl. of $*$ a Centauri. 60 25 $\frac{37}{37}$ S 90 0 0	M. T. G. Sid. T. (G. noon) Accl.	H. M. S. 22 26 7 23 24 40'46 + 3 41'13	Dl. of $*$ Canopus 5°_{2} 3°_{3} 5°_{9} S 9°_{9} 0°_{9} 0°_{9}				
Sid. T. Green.	20 51 54'35	P. D. 29 34 23	Sid. T. Green.	21 54 28.59	P. D. 37 21 1				

* a CENTAURI TO S.ED.

* CANOPUS TO S.WD.

Obsd. alt. of I. E.	¥ 69 36 50 + 1 20			Obsd. alt. of ¥ I.E.	$ \begin{array}{c} $		
2) 69 38 10			2	2)112 11 30		
App. alt. Ref.	34 49 5 — I 22			App. alt. Ref.	56 5 45 - 38		
T. alt. Lat. P. D.	34 47 43 41 0 0 29 34 23	Sec Cose	0°12222 C 0°306684	T. alt. Lat. P. D.	56 5 7 41 0 0 37 21 1	Sec Cosec	0°122220 0°217036
	105 22 6				134 26 8		
$\frac{S}{S} - A$	52 41 3 17 53 20	Cos Sin	9'782622 9'487382	S S – A	67 13 4 11 7 57	Cos Sin	9°587969 9°285798
★ 's H.A. ★'s R.A.	н. м. s. 5 59 58°о Е 14 33 1°3	Sin ²	9.698908	米's H.A. ★'s R.A.	н. м. s. 3 10 41 [.] 3 W 6 21 47 [.] 6	Sin ²	9'213023
Sid. T. place Sid. T. G.	8 33 3'3 20 51 54'3	A B	.00 1.76 S	Sid. T. lace Sid. T. G.	9 32 28 [.] 9 21 54 28 [.] 6	A B	79 N 177 S
Long. in T.	11 41 9'0	С	1.76 S gives Az. S 37° E	Long. in T.	11 38 0'3	С	'98 S to E
Long. (1) Long. (2)	175° 17' 15" H 174 30 5 H	2 C	C ² Posline S 60 [.] 4 ^o W	Long. (2)	174° 30′ 5″ E	gives.	Az. S 531° W
Diff. long.	47 10 =	47.17				C⁴ POS.	-inte 5 44.4° E

Long. (1) cor. = 1.76 S to W (2) ,, 0.98 S to E

D. long. 2'74 : d. long. 47'17' : lat. 1' : lat. cor. 17'22' = 17' 13"

Lat. used	41 0 0 S	Long. (2)	174 30 5 E	(2) 2.74 (1)
Cor.	17 13 5	$17^{\circ}22^{\circ} \times {}^{\circ}98^{\circ} = cor.$	10 53 E	1.0
Lat. in	41 17 13 S	Long. in	174 46 58 E	Cor to S

These observations were taken on the same evening as those given on the preceding page. As one star was east of the meridian and the other one west, the case is not good for latitude; but it should give the truest longitude, as instrumental errors, &c., will practically eliminate one another in the resulting longitude. This problem reworked with a latitude near the truth makes no appreciable difference in the resulting position.

For position of ship when plotted on chart, see chartlet on next page.

DOUBLE ALTITUDE OF TWO STARS

(COMBINING CHRON. LONG. OBSERVATION WITH AN EX-MERIDIAN).

1902 .- On 15th March, p.m., the following observations were taken :--

D. H. M. S.

Л.	Т.	G. by	chron.	14	21	23	43	T. alt. of	×	a Centauri	34	47	43 to) S.	Ed.
Æ	T	c ·		- 1	~~	~ Ē				Canonia	-6		m + /	S C	W

M. T. G. " 14 22 26 7 " * Canopus 56 5 7 to S.Wd.

0 1 4

Required position of place by projection on the chart, assuming the approximate latitude to be $41^{\circ} o'$ S.

	* CANOPUS TO	5 S.W	D.	*	a CENTAURI '	ro S.ED.	
M. T. G. Sid. T. (G. noon	м. н. s. 22 2б 7 1) 23 24 40'4б	DI -		M.T.G. Long. in T.	н.м.s. 21 23 43 +11 38 0'3	Sid. T. G. no Accl.	н. м. s. on 23 24 40'46 + 3 30'89
Acci.	+ 3 41.13	DI. 0	1 × 52 38 59 5	M. T. place	0 1 43'3	M. O's R.A.	23 28 11.35
Sid. T. Green.	21 54 28.59	P. D.	37 21 1	M. ⊙'s R.A.	23 28 11.3		-9 -0 99
A	56 5 7	Sec	0.122220	Sid. T. place ¥'s R.A.	8 29 54 ^{.6} 14 33 1 ^{.3}	★ 's Dl.	$= \frac{0}{60} \frac{1}{25} \frac{1}{37} \text{ S}$
P	37 21 1	Cose	c 0'217036	¥'s H.A.	6 3 6.7		
	134 26 8			Supt.	5 56 53'3	Cos 8.132720	
S .	67 13 4	Cos	9.587969	Dl.	60 25 37	Cot 9'753933	Cosec 0.060617
5 – A	11 7 57	Sin	9*285798	Arc (1)*	0° 26′ 29″ S	Tan 7.886653	Cos 9.999987
¥'s H.A. ¥'s R.A.	H. M. S. 3 10 41'3 W 6 21 47'6	Sin^2	9.213023	Arc (2)	41 0 11 S	Alt. 34° 47' 43"	Sin 9.756366
Sid T plana	0.00.08:0	٨	in N	L atitude	47 26 40 S		Sin 9'816970
Sid. T. G.	21 54 28 [.] 6	B	1.77 S	Latitude	41 20 40 3	1.0	
Long. in T.	11 38 0.3	Co	r <u>98 S</u> Posline from	n C ² gives S 44'4	°E B	.01 S 1.77 S	
Long. 1	74° 30′ 5″ E				Co	or 1'78 S gives Pos	line S 60'7° W

The chartlet below serves to illustrate both the problem above and the one on previous page. In the first case the position-lines are laid down from the two longitudes corresponding to the parallel of latitude 41° S., and in the second case the position-lines are laid down from the meridian of longitude 174° 30' E., the longitude found by chronometer from observation of star Canopus in latitude 41° S. The observation of star α Centauri is worked as an ex-meridian from the time deduced from longitude 174° 30' E. Though the hour-angle in this case is a little over six hours, the latitude found is perfectly correct.



* As the logs for sines and tangents are practically the same for very small angles are (1) may be taken out from the log sine table to save calculating for the seconds.

SIMULTANEOUS(*) OBSERVATIONS OF TWO DIFFERENT STARS BY THE OLD "SUMNER" METHOD.

1898. — Shortly after sunset on March 3rd, somewhere between the parallels of 51° 15' N. and 51° 50' N., a chronometer indicated mean time at Greenwich 3d. 6h. 48m. 38s. when the true altitude of * Procyon was 31° 57' east of meridian; again, after running east (true) $3\frac{3}{4}$ m., a chronometer indicated 3d. 6h. 59 m. 20 s. when the true altitude of * Capella was 83° 50' east of meridian.

Required the position of the ship at time of last observation, and the true bearing of the stars by Sumner's method of progression on the chart.

IST OBSER	VATION: * P	ROCYON TO S.ED.	2ND OBSERVATION: * CAP	ELLA TO S.ED.
M.T. Green. Sid. T. (G. noon)	D. H. M. S. 3 6 48 38 22 45 7 9	T. alt. of $\frac{3157}{2157}$ E	D. H. M. S. M.T. Green. 3 6 59 20 Sid. T. (G. noon) 22 45 7.9	T. alt. of $\frac{8}{3}$ 50 E
Accl.	+ 1 71		Accl. + 1 8.9	0 /
Sid T Green	5 24 52'0	*'s DI. 5 29 N	Sid T Green 5 45 a6'8	X'S DL 45 54 N
and it offern	5 34 35 0	PD 84 31 N	<u> </u>	PD 44 6 N

Run between observations, East 3'75m. = d. long. 6'0' E

A L	31 57 51 15 84 31	Sec Cosec	0'203479 0'001992	A L P	83 50 51 15 44 6	Sec Cosec	0 °20 348 0°15745
	167 43				179 11		
S S – A	$8_3 51\frac{1}{2}$ 51 54 $\frac{1}{2}$	Cos Sin	9°029332 9°895988	S S – A	89 35 ¹ / ₂ 5 45 ¹ / ₂	Cos Sin	7 [.] 85289 9'00144
*'s H.A. *'s R.A.	н. м. s. - 2 52 33°0 Е 7 34 0°3	Sin ²	9'130791	米 's H.A. 米 ′s R.A.	н.м.s. - о 18 34°6 Е 5 9 11°4	Sin ²	7.21526
Sid. T. Sp Sid. T. G.	2. 4 4I 27'3 5 34 53'0			Sid. T. Sp. Sid. T. G.	4 50 36 ^{.8} 5 45 36 ^{.8}		
Long. in T	Г. 0 53 25.7			Long. in T	. 0 55 0'0		
Long Run	$13^{\circ} 21' 25'' W = 6 \circ E$			Long. C	13° 45′ 0″ W		
Long. A	13 15 25 W						
A L P	31 57 51 50 84 31	Sec Cosec	0'209046 0'001992	A L P	83 50 51 50 44 6	Sec Cosec	0° 209 05 0°15744
	168 18				179 46		
S S – A	84 9 52 12	Cos Sin	9`008278 9`897712	S S – A	89 53 6 3	Cos Sin	7°30882 9°02283
米 's H.A. 米 's R.A.	H. M. S. - 2 49 42'3 E 7 34 0'3	Sin ²	9.117028	米 's H.A. 米's R.A.	н. м. s. – о ю 14'4 Е 5 9 11'4	Sin ²	6.69814
Sid. T. Sp Sid. T. G.	0. 4 44 18'0 5 34 53'0			Sid. T. Sp. Sid. T. G.	4 58 57°0 5 45 36°8		
Long. in 7	Г. о 50 35°0			Long. in T	o 46 39 ^{.8}		
Long. Run	^{12°} 38' 45" W 6 0 E			Long. D	11° 39′ 57″ W		
Long. B	13 32 45 W						

Position of ship by Sumner: Lat. $51^{\circ} 27\frac{1}{2}$ ' N., long. 13° o' W. True position of ship: Lat. $51^{\circ} 32'$ N., long. $12^{\circ} 55'$ W. Bearing of * Procyon, S. 53° E.; and bearing of * Capella, S. 24° E.

(a) Practically though not absolutely simultaneous.

Note.—This is the problem (b) of the Board of Trade Examination for Extra Master, with the exception that as set for that examination both observations are taken at the same instant, only one chronometer time being given. As this is probably never realized in practice, the more usual experience of having a few minutes' interval between the observations is here given. Position by "Sumner" plotted on chart from four calculated hour-angles, as required to be worked when the chart is used for Board of Trade Examination of an Extra Master.



that it could not be well shown on this charlet. The straight ine cuts the circle of altitude between C and D at late SI 32 & N.

and long 1254 W. The true position of ship, where the two circles of altitude would cut, is lat. 5132 N and lona 1255 N.

8-Azimuth.



SIMULTANEOUS (a) OBSERVATIONS OF TWO DIFFERENT STARS BY THE IMPROVED "SUMNER" METHOD.

1898.—Shortly after sunset on March 3rd, in latitude by D.R. 51° 15' N., longitude 13° 40' W., a chronometer indicated mean time at Greenwich 3d. 6h. 48 m. 38 s. when the true altitude of * Procyon was 31° 57' east of meridian; again, after running east (true) $3\frac{3}{4}$ m., a chronometer indicated 3d. 6h. 59 m. 20 s. when the true altitude of * Capella was 83° 50' east of meridian.

Required the position of the ship at the time of last observation, and the true bearing of each star at the time of their observation.

ist Obser	VATION: * PROCYON TO S.ED.	2ND OBSERVATION: ¥ C	APELLA TO S.ED.
M.T. Green. Sid. T. (G. noon) Accl. Sid. T. Green	$\begin{array}{c} \text{H. M. S.} \\ 6 \ 48 \ 38 \\ 22 \ 45 \ 79 \\ + \ 1 \ 7'1 \\ \hline 5 \ 34 \ 53'0 \end{array} \begin{array}{c} \text{T. alt. of } \bigstar \begin{array}{c} \bigstar \\ 3^{\circ} \\ 5' \\ \hline 5 \ 29 \\ \hline \end{array} \\ \begin{array}{c} \text{N.} \\ \text{P.D.} \\ \hline \end{array} \\ \begin{array}{c} \text{S.} \\ \text{S.}$	M.T. Green. Long. in T. – – 659 20 M.T. Sp. 6 6 18'3 Sid.T. (G. noon) 22 45 7'9 Accl. + 1 8'9	T. alt. of $\frac{8}{3}$ 50 Sd Z.D. $\frac{6}{50}$
Run between obs A 3° 57	ervations, East 3'75 m.= d. long. 6'0' E.	Sid. T. Sp. 28 52 35'1 *'s R.A. (+24) 29 9 11'4	
I. 57.75	Sec 0.202470		

P ě	4 31	Cosec	0.001995
16	7 43		
$S \rightarrow A $	$351\frac{1}{2}$ $54\frac{1}{2}$	Cos Sin	9°029332 9°895988
* 's H.A. * 's R.A.	H. M. S. 2 52 33'0 E 7 34 0'3	Sin ²	9'130791
Sid. T. Sp. Sid. T. G.	4 41 27'3 5 34 53'0	Tat s	· · · · · · · · · · · · · · · · · · ·
Long. in T.	0 53 25.7	* Pro	cyon B 14 N
Long. Run	13°21'25"W 6 o E	H.A.	2 52) C 1.19 S
Long. (1)	13° 15' 25" W	Gives Posl	Az. S 53 [.] 3° E and ine N 36 [.] 7° E
Long. in T.	н.м. s. о 53 г.7		

M. T. Sp. 5id. T. (G. noon) Accl.	6 6 18 ³ 22 45 79 + 1 89		
Sid. T. Sp. ¥'s R.A. (+24)	28 52 35.1 29 9 11.4		
*'s H.A.	0 16 36'3 E	Sin	8.8595
Dec. Alt.	45° 54' N 83° 50'	Cos Sec	9°8426 0°9689
Az.	S 27° 57' E	Sin	9.6710
Posline	N 62° E.		

LAT. BY EX-MER. TABLE NO. 3 OF BLACKBURNE'S AND WESTLAND'S TABLES.

H. M. H.A. 0 16 [.] 6 Dec. 45 [°] 54' N	Cor. $\stackrel{\circ}{+}$ $\stackrel{\prime}{4}$ $\stackrel{\prime}{5}$ $\stackrel{\prime}{45}$ 54	Alt. 83 50 Cor. Az. 27 57 Z D	$\frac{3}{6}$ $\frac{43}{10}$ N
Arc (I)	45° 58°5' N	Arc (2)	5 57 N
Arc (2)	5 57 N		_
Lat.	51° 25.5' N		

long.

long. cor.

1st obsn. *****'s Az. S 53'3°E gives lat. error from Table M ' $\overset{\circ}{5}$ 4 N to E at lat. $\overset{\circ}{5}$ 1 f 5 N 2nd obsn. *****'s Az. S 28° E gives lat. error from Table M '33 N to E at lat. 51 25'5 N



			. 200 21
Long. Cor.	°3 15.4 W 20.6 E		
Long. in	12 54.8 W		
		Long. cor.	20.6 × '33
Lat. Cor.	51 25.5 N 6.8 N		.018 .018
Lat. in	51 32'3 N	Lat. cor.	6.798 N

1010

diff lat

NOTE.-This example illustrates very forcibly the superiority of the improved Sumner method over the old Sumner method which the Board of Trade so tenaciously hold on to in their examinations. By the old method the work is about twice as long, requires the aid of a chart, and gives a result $4\frac{1}{3}$ ' in error in the latitude and 5' of error in the longitude. By the improved method no chart is required (though it may be used if preferred with the same result), and the position is less than $\frac{1}{2}$ in error in either latitude or longitude.

The Marcq St. Hilaire method of calculation gives 2' of error in latitude and 2' in the longitude.

(a) Practically though not absolutely simultaneous.

IMPROVED "SUMNER" POSITION FROM TWO STELLAR OBSERVA-TIONS

(COMBINING CHRON, LONG, OBSERVATION WITH AN EX-MERIDIAN BELOW THE POLE).

1898.—Soon after sunset on 25th December, at about 8 h. 2 m. p.m., in latitude by

M. T. Green. 21 h. 7 m. 265. when T. alt. of a Crucis was $20^{\circ} 45^{\circ}$ E. of meridian. Run in interval between observations, S. 80° , E. 1 m. = dep. 0.98° = d. long. 1.4' E. Required the position of ship at time of second observation.

IST OBSERVATION.					
A. T. Gree Sid. T. (G. Accl.	н. n. 21 noon) 18	M.S. I 20 I2 8'3 3 27'2	Dl. (of $\frac{1}{16}$	Sirius. $\frac{1}{35}$ S
Sid. T. Gre	en. 15	16 55.5	P.D	. 73	25
	* Siri	us to	N.Ed.		
A L P	28 26 46 0 73 25		Sec Cosec	0.128 0.018	229 451
S S – A	$ \begin{array}{r} 147 51 \\ 73 55\frac{1}{2} \\ 45 29\frac{1}{2} \end{array} $		Cos Sin	9'442 9'853	316 180
¥'s H.A. ¥'s R.A.	н.м. - 4 23 6 40	s. 59 E 44	Sin^2	9'472	176
Sid. T. Sp. Sid. T. Gre	2 16 en. 15 16	45 55°5		A B	·46 N ·33 S
Long. in T	. 10 59	49°5		C^2	·13 N
Long. Run	164° 57 1	′ 22″ E 24 E	Posli	ne N	7 <u>1</u> ° W
Long. (I) at time of a	164 58 2nd	46 E	= 10h.	59 m.	<u>55s.</u>

S

4

• 3/3 . Position Post line • • • • • • • • • • 40 • • • •
•
• 50 • • • 164°50 165

M. T. Green. Long. E +	н. м. s. 21 7 2б 10 59 55	Sid.T. (G. noon) Accl.	н. 18 +	м. 12 3	8. 8. 28.0
M. T. Sp. M. O's R A	8 7 21	M. ⊙'s R.A.	18	15	36.
	10 1 30 3	н м			

2ND OBSERVATION : * a CRUCIS.

Sid. T. Sp. * 's R.A.	- 2 22 57'3 12 20 59'6	$\begin{array}{ccc} H.A. & 9 & 58 \\ Lat. & 46^{\circ} & S \end{array} \begin{array}{c} A \\ B \end{array}$	1.76 S 3.80 S
* 's H.A.	- 9 58 2'3E	* a Crucis) C	5.26 S
Supt.	2 1 58	gives Az. S	S 14°'5 E

Table C2 gives Posn.-line for Plane Chart, S 793° W

For Latitude by Ex-meridian Table No. 3 of Blackburne's and Wfstland's Tables.

Decl. H.A.	62° 32' S 2h. 2m. }p. 149{	Arc cor. P D	- 3 20.3 27 28.0 S
		Arc(1)	24 7.7 S
Alt. Az.	$\begin{array}{c} \circ & 45 \\ 20 & 45 \\ 14 & 30 \\ \end{array}$ $\left. \begin{array}{c} p \\ p \\ p \end{array} \right. $ 145 $\left. \begin{array}{c} \circ \\ p \\ \end{array} \right.$	Arc cor. Alt.	+ ° 37'3 20 45'0 S
		Arc (2) " (1)	21 22'3 S 24 7'7 S
		Lat.	45 30°0 S

RULE FOR USE OF EX-MERIDIAN TABLE No. 3.

With Hour-angle from Lower Meridian.

With declination and hour-angle take out arc reduction; subtract this reduction from PD for arc (1).

With altitude and azimuth take out 2nd arc reduction: add this reduction to altitude for arc (2).

Arc (1) + arc (2) = latitude.

* Sirius with latitude 46° S. gives longitude 164° 58' 45" E., and position-line for plane chart N. $7\frac{1}{2}^{\circ}$ W.

* a Crucis with longitude $164^{\circ} 58' 45'' E$. gives latitude $45^{\circ} 30' S$., and position-line S. 80° W.

Chart position: Latitude 45° 30.7' S., longitude 164° 55' E.

High-declination stars, such as a Crucis, are very useful for ex-meridians, as, if the time is only approximately correct, the lati-tude will not be far from the truth if the body is within an hour from the meridian below the Pole.

In this example, notwithstanding that the star a Crucis is over 2 hours from the lower meridian passage, 1 m. of error in the time used for ex-meridian would only make $2\frac{1}{2}$ ' of error in the resulting latitude.

THE SUPERIORITY OF STELLAR OVER SOLAR OBSERVATIONS.

The two great advantages of stellar over solar observations are (1) that by the stars the latitude and longitude can be obtained simultaneously, instead of having an interval of three or four hours between the observations as is often the case when the sun is used, and (2) that uncertain errors in altitude resulting from personal equation, arc errors of sextant, or exceptional refraction may be practically eliminated by a proper choice of stars. If meridian altitudes can be obtained about the same time to the north and south of observer, it will be apparent to any one that the errors would be eliminated by taking the mean result of the two observations for the true latitude; and in the same way the true longitude would be found by the mean result of observations taken nearly But it may happen that stars are not to be found north, east and west of meridian. south, east, and west of observer during the short time that the horizon is good for observation. The following is the plan that the writer used for several years with great success: Take three stars, and of these choose two on the same side of the meridian northward and southward of the observer for a good latitude. If they both happen to be the same distance from the meridian, as in the following example, 10' of error in the altitude will make practically *no difference* in the resulting latitude as found by the "Sumner" or double-altitude problem. Then choose another star on the other side of the meridian, as near as possible the same distance from the meridian; calculate the longitude with the latitude found from the previous observations, and the true longitude will be obtained by taking the mean between the eastern and western stars worked with the correct latitude.

Elimination of Errors in Altitude.

Diagram showing how the true latitude may be found by the "Sumner" method even when altitudes have been observed by a sextant with large unknown arc errors.



See worked-out example from which this is taken on the following two pages.

POSITION OF SHIP FROM OBSERVATION OF THREE STARS,

THEREBY ELIMINATING ERRORS IN POSITION RESULTING FROM UNKNOWN ERRORS IN ALTITUDE.

1898.—On March 18th, at 8 h. 11 m. p.m., A.T. at ship, in latitude by D.R. 44° 32' S., longitude 152° 20' E. Required the position of ship from the following observations :--

 (1) * Achernar's corrected alt. 3°_{3} 27 W of mer. when chron. showed M. T. Green.
 D. H. M. S.

 (2) * Betelguese
 " 30 13 W "
 " " 17 22 9 33

 (3) * β Centauri
 " " " 17 22 12 17

 Ship making a true east course at speed of 12 miles per hour. [°]59 52 58 S 90 0 0 7 23 16 N (I) Decl. 57 45 17 S 90 0 0 (2) Decl. (3) Decl. 90 Ö 0 P. D. P. D. P. D. 30 7 2 32 14 43 97 23 16 SID. T. (G. NOON). SID. T. (G. NOON). SID. T. (G. NOON). н. м. s. н.м. s. н. м. s. Accl. 22 h. $9\frac{1}{2}$ m. + 3 38'40 Accl. 22 h. 12¹/₄ m. + 3 38.86 Cor. Sid. T. M. T. G. Cor. Sid. T. M. T. G. Cor. Sid. T. M. T. G. 23 43 57°47 22 5 5 3 23 43 58.07 22 9 33 23 43 58'53 22 12 17 Sid. T. Green. 21 49 47'47 Sid. T. Green. Sid. T. Green. 21 53 31.07 21 56 15.53

* ACHERNAR TO S.WD.

* BETELGUESE TO N.WD

A L P	33 27 44 32 32 15	Sec 0.147006 Cosec 0.272772	A L P	30 13 44 32 97 23	Sec 0'147006 Cosec 0'003616
S S – A	55 7 21 40	Cos 9.757326 Sin 9.567269	S S – A	86 4 55 51	Cos 8:836297 Sin 9:917805
*'s H.A. *'s R.A.	н. м. s. 6 25 18 [.] 5 W 1 33 54 [.] 4	Sin ² 9'744337	*'s H.A. *'s R.A.	H. M. S. 2 II 41'6 W 5 49 40'6	Sin ² 8'904724
Sid. T. Sp. Sid. T. Green	7 59 12'9 1. 21 49 47'5	A '11 S B 1'59 S	Sid. T. Sp. Sid. T. Green.	8 I 22°2 2I 53 3I°1	A 1.52 N B 1.24 N
Long. in T.	10 9 25.4	C ² 1'70 S gives	Long. in T.	10 7 51'1	C^2 1.76 N gives
Longitude Run	152° 21' 21" E 1 0 E	Pos -line $\overline{S 59^{10}_2} E$	Longitude (2) I " (1) I	51° 57′ 46″ E 52 22 21 E	Posline N 602° E
Long. (I)	152 22 21 E		Diff. long.	24 35 = 24.6	5'

* β CENTAURI TO S.ED.

A	38 32		Long. (1) cor. = 1.70 S to E Long. (2) cor. = 1.76 N to E				
P P	44 25 30 7	Sec 0'146138 Cosec 0'299502	D. long. 3'46	5 : d. long. 24.6 :: lat. 1 : lat. cor. 7.1 N			
S – A *'s H.A. *'s R.A. Sid. T. Sp. Sid. T. Green Long. in T. Long.	$\begin{array}{c} 113 & 4 \\ 56 & 32 \\ 18 & 0 \\ \hline \\ H. M. S. \\ - & 5 & 48 & 45'3 E \\ 13 & 56 & 41'2 \\ \hline \\ 8 & 7 & 55'9 \\ 0. & 56 & 15'6 \\ \hline 10 & 11 & 40'3 \\ \hline \\ 152^{\circ} & 55' & 5'' E \end{array}$	$\begin{array}{c} Cos \\ Sin \\ 9'741508 \\ 9'489982 \\ Sin^2 \\ \hline 9'677130 \\ \hline \\ A \\ ro5 \\ N \\ B \\ r'73 \\ S \\ C^2 \\ r'68 \\ S \\ give \\ Posline \\ \hline S \\ 59'2^0 \\ V \\ Long. by W \end{array}$	Lat. used Cor. Lat. in Long. (1) $7'1' \times 1'7'$ Long. in Run in interval Long. V star 152 55	$\begin{array}{c} 44 & 32 & 0 & S \\ 7 & 6 & N \\ 44 & 24 & 54 & S \\ 152 & 22 & 21 & E \\ 152 & 12 & 4 & W \\ 152 & 10 & 17 & E \\ 45 & E \\ 152 & 11 & 2 & E & when & \beta & Centauri was \\ 6 & 5 & E \\ \end{array}$			
		# 15	2) 304 66	7			
				-			

" by mean of obsns. 152 33 3 E

POSITION OF SHIP FROM OBSERVATION OF THREE STARS.

(This is previous example worked with 10' less altitude for each star. Result the same.) 1808 - On 18th March at 8 h μ m n m A T ship in latitude by D R 44° 32' S

1898.—On 18th March, at 8 h. 11 m. p.m., A.T. ship, in latitude by D.R. 44° 32' S., longitude 152° 20' E. Required the position of ship from the following observations :—

				0						D. D	a. :	$n \cdot z$	э.
(1)	×	Achernar	true alt.	33	17	W.	of mer.	when chron.	showed M. T. Green.	17 2	2	5 5	0
(2)	×	Betelguese	"	30	3	W.	"	17	"	17 2	2 9	9 3.	3
(3)	×	β Centauri	w	38	22	E.	*	11		17 2	2 I	2 I	7

Ship making a true east course at speed of 12 miles per hour.

1) Decl.	57 45 17 S 90 0 0	2) Decl.	72316N 9000	(3) Decl.	59 52 58 S
P. D.	32 14 43		97 23 16		30 7 2

SID. T. (G. NOON).		Sid. T. (G.	SID. T. (G. NOON).			SID. T. (G. NOON).		
17th Accl. 22 h. 5 ⁸ / ₄ m.	н. м. s. 23 40 19 [.] 67 + 3 37 [.] 80	Accl. 22 h. 9½m.	н. м. s. 23 40 19 [.] 67 + 3 38 [.] 40		Accl. 22 h. 124 m.	н.м. s. 23 40 19.67 + 3 38.86		
Cor. Sid. T. M. T. Green.	²³ 43 57 47 22 5 50	Cor. Sid. T. M. T. Green.	23 43 58 ^{.07} 22 9 33		Cor. Sid. T. M. T. Green.	23 43 58 [.] 53 22 12 17		
Sid. T. Green.	21 49 47 47		21 53 31.07		Sid. T. Green.	21 56 15.53		

×	ACHERNAR	то	S.WD.	
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1

* BETELGUESE TO N.WD.

A L P	$\begin{array}{c} 33 & 17 \\ 44 & 32 \\ 32 & 15 \\ \hline 110 & 4 \end{array}$	Sec 0'147006 Cosec 0'272772	A L P	$ \begin{array}{r} 30 & 3 \\ 44 & 32 \\ 97 & 23 \\ \hline 171 & 58 \\ \end{array} $	Sec Cosec	0'147006 0'003616/
$\frac{S}{S} - A$	55 2 21 45	Cos 9'758230 Sin 9'568856	$\frac{S}{S} - A$	85 59 55 56	Cos Sin	8.845387 9.918233
*'s H.A. *'s R.A.	H. M. S. 6 26 46'9 W I 33 54'4	Sin ² 9'746864	★'s H.A. ★'s R.A.	11. m. s. 2 13 11'2 W 5 49 40'6	Sin ²	8'914242
Sid. T. Sp. Sid. T. Green.	8 0 41'3 21 49 47'5	A 12 S B 159 S	Sid. T. Sp. Sid. T. Green.	8 2 51 [.] 8 21 53 31 [.] 1	A i B	50 N 24 N
Long. in T.	10 10 53.8	C2 1.71 S gives	Long. in T.	10 9 20'7	C2 1	'74 N gives
Longitude Run	¹ 52° 43' 27″ E I O E	Posline S 59'6° E	Longitude (1) " (2)	152° 20' 10" E 152° 44° 27 E	Poslin	e N 60'1° E
Long. (1)	152 44 27 E		Diff. long.	24 17 = 24	·3′	

* β CENTAURI TO S.ED.

0 1

A L D	38 22 44 25	Sec 0.146138	Long. (1) cor. 1 Long. (2) cor.	1.71 S to E 1.74 N to E
Р	<u>30 7</u> 112 54	Cosec 0'299502	D. long. 3	3'45 : d. long. 24'3' : : lat. 1' : lat. cor. 7'04'
S S – A	56 27 18 5	Cos 9'742462 Sin 9'491922	Lat. used Cor.	44 32 0 S 7 0 N
*'s H.A. *'s R.A.	н. м. s. 5 50 12.8 Е 3 56 41.2	Sin ² 9.680024	Lat. in	44 25 0 S
Sid. T. Sp. Sid. T. Gree	8 6 28.4 n. 21 56 15.5		Long. (1) 7'04' × 1'71	^o 1, ^f E 152 44 27 E 12 2 W
Long. in T.	10 10 12'9		Run in interv	152 32 25 E al 45 E
-		0 1 41	Long.	$\frac{152 \ 33 \ 10}{\text{ observed.}} $ E when β Centauri was observed.
Lon.	g. by W star E star	152 33 14 E 152 33 10 E	With the al calculated with	bove correct altitudes, the longitude th correct latitude, 44° 25' S, would
	by mean of obs	DS. 152 22 12 E	be practically	the same by all three stars.

EXAMPLES TO FIND STARS SUITABLE FOR DETERMINING POSITION BY SIMULTANEOUS ALTITUDES.

EXAMPLE 1.

1898.—On 22nd February, at about 5 h. 30 m. p.m., in lat. by D.R. 49° 20' N., long, 8° 45' W. Find what stars not less bright than mag. o 5 are suitable for determining the position of ship by simultaneous altitudes.

A. ⊙'s R.A. A. T. Sp. +	22 24 5 30						
R.A. mer. * Capella R.A.	3 54 · · · 5 9	* Rigel	н.м. 354 · · 510	* Sirius	н.м. 354 640	* Procyon	н.м. 354 734
★ 's H.A.	1 15 E	H.A.	1 16 E	H.A.	2 46 E	¥'s H.A.	3 40 E
R.A. mer. + 24 h * Vega *'s H.A.	H. M. 2754 1833 <u>921</u> W	pl C ai	The only anets) which apella, Rige	stars of th h would be l, Sirius, a he west	his magnitu e above the nd Procyon	de (not ir horizon w 1 east of m	icluding vould be ieridian.

Rigel and Capella, having nearly the same R.A. and a large difference in declination, will always make a good cut with one another; also, position-lines from Vega and Capella will nearly always cross one another at a good angle in the Northern Hemisphere, as these stars are about $10\frac{1}{2}$ hours apart in R.A., and in high northern latitudes they both remain almost continuously above the horizon. In this case either Capella or Procyon, worked for longitude, would make a good cut with any of the other three stars, which would be nearer the meridian than the prime vertical, and could therefore be worked for latitude, Rigel and Sirius being to the south and Vega to the north.

EXAMPLE 2.

40-4 51-51

н. м.

1898.—On 25th June, at about 5 h. p.m., in lat. by D.R. 40° S., long. 171° E. Find what stars not less bright than mag. 0.5 are suitable for determining the position of ship by simultaneous altitudes.

A. O's R.A. A. T. Sp. + R.A. mer. * Achernar R.A	$ \begin{array}{c} 6 & 16 \\ 5 & 0 \\ \hline 11 & 16 \\ \cdot & 1 & 34 \end{array} $	* Rigel R.A.	н. s. 11 1б 5 10	* Canopus R.A.	н.м. 11 16 6 22
*'s H.A.	9 42 W	*'s R.A.	6 6 W	¥'s Ĥ.A.	4 54 W
R.A. mer. ¥ Sirius	н.м. 1116 641	* Procyon	н.s. 11 16 7 33	* Arcturus	н.м. 11 16 14 11
*'s H.A.	4 35 W	* 's H.A.	<u>3 43</u> W	*'s H.A.	2 55 E

It will be seen at once that Sirius, nearly on the prime vertical, and Achernar, near the meridian below the Pole, will give a splendid position. Canopus would also give a good longitude in combination with Achernar, or position-line from Procyon to N.W. would cross well with Arcturus to N.E. Rigel, having a very small altitude, would probably not be seen.

NOTE.—The planets Venus, Jupiter, Saturn, and Mars make good daylight stars for observation. Venus, the brightest of all, is nearly always available for longitude either in the early morning or evening. The relative positions of the other planets with the sun vary continuously.

⁴In the Northern Hemisphere Vega and Altair, or Rigel and Capella, nearly always pair well together: when the first pair are morning the other are evening stars, and *vice versa*. In the Southern Hemisphere Canopus and Sirius, or either a or β Centauria and Arcturus, make good pairs for determining positions. In higher latitudes, in place-of Arcturus, Achernar will always make a good cut with either of the Centaurs.

DOUBLE-ALTITUDE POSITION BY SUN AND MOON.

LONGITUDE BY CHRONOMETER, AND EX-MERIDIAN 3 HOURS FROM THE MERIDIAN.

1898.—On 2nd January, at about 3 p.m., A.T. at ship, observed altitude of moon's U.L. was 26° 33' o'' E. of meridian when chronometer showed M.T. Green. 3 h. 48 m. 30 s., and observed altitude of sun's L.L. was 5° 30' 45'' W. of meridian when chronometer showed M.T. Green. 3 h. 53 m. 7 s. Latitude by D.R. 51° 30' N., longitude 12° 20' W. Height of eye, 33 ft. Run in interval between observations, 1 m. on a true S. 85° E. course = dep. 1.0' = d. long. 1.6' E.

Required the position of ship at time of second observation.

Obsd. alt. of (Dip 33 ft.	26 33 o E ('s R.A. 4 h. 5 39 2'035 s. × 11'5 m.	H. M. S. 2 40 33'3 ('s d - 23'4 8'3" ×	ecl. 4 h. 2 11'5 m.	20 54 29 N I 35 S
Semi-d. App. alt. (('s centre Cor. T. 39 Raper) H.P. 54' 10''	26 27 21 - 14 55 26 12 26 + 46 39	2 40 9'9 Cor. o P. D.	lecl.	80 52 54 N 69 7 6
T. alt. ('s centre	26 59 5 Accl. 3 h. 483 M. ⊙'s R.A.	$\begin{array}{r} \text{H. M. S.}\\ \text{pon)} & 18 \ 48 \ 34^{5}53\\ \text{m.} & + \ 37^{5}54\\ \hline & 18 \ 48 \ 12^{\circ}07\\ \hline \hline & 18 \ 48 \ 12^{\circ}07\\ \hline \end{array}$	Obsd. alt. ⊙ 33 ft. T. E. ī·4' Jan. + `3 T. alt⊖-	$\begin{cases} 5 & 30 & 45 \\ + & 1 & 42 \\ \hline 5 & 32 & 27 \\ \hline \end{array}$
$ \begin{array}{cccc} A & & & 26 & 5 \\ L & & 51 & 3 \\ P & & 69 \\ \hline & & 147 & 3 \\ S & - A & & 46 & 4 \\ \end{array} $	/9 10 Sec 0'205850 7 Cosec 0'029510 	O's decl. 14'0" × 3'9 h	$\frac{1}{12}$ S Eq. T 5 1.16 s. 5 7 S Cor. Eq. $\frac{1}{2}$ S Cor. Eq.	M. S. 4 23'25 4 23'25 + 4'52 q. T. 4 27'77
()'s H.A. -45 ()'s R.A. $+24$ h. 264 R.A. mer. 215 M. \odot 's R.A. 184 M. T. Sp. 3	4. S. 0 3'4 E Sin ² 9'543777 0 9'9 0 6'5 A '40 S 8 12'1 B '40 N 0 54'4 C '00 gives Az, N 90° E	M. T. G. 3 53 7 Long. W 0 47 29'2 M. T. Sp. 3 5 37'8 Eq. T 4 27'8		
M. T. Green. 34 Long. in T. 04 Long. 11° 5	8 30°0	A. T. Sp. $3 ext{ 1 0}$ \bigcirc 's decl. 22 52 47 Arc (1) $30^{\circ} 57' 28'' S$	Cos 9.847263 Cot 0.374688 Cot 0.221951	Cosec 0.410276 Sin 9.711306
Kun Long. (1) 11	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Arc (2) 82 39 34 N	1. alt. 5° 325'	Sin 8'984840 Cos 9'106422

Position of ship = Lat. $51^{\circ} 42'$ N., Long. $11^{\circ} 52\frac{1}{4}'$ W.

Lat,

51° 42' 6" N

As the moon was on the prime vertical when the altitude was taken, the time deduced from this observation should be absolutely correct, and the latitude by exmeridian of the sun will also be correct without any additional work.

Note.—The work of correcting the moon's semidiameter and horizontal parallax is not here shown. These elements should be taken from the Nautical Almanac (p. III) of the month, where they are given for Greenwich noon, and midnight, for every day of the year. For accuracy, a correction is necessary for the number of hours from noon or midnight, and also two other small corrections—one for parallax, for the figure of the earth, and the other for moon's augmentation with increase of altitude. For sea observations these corrections can usually be made with sufficient accuracy at sight.

POSITION FROM TWO CHRONOMETER LONGITUDES BY SUN AND MOON.

1898.—On 10th July, at about 8 h. 5 m. a.m., A.T. ship, the observed altitude of \odot 's L.L. was 35° 12′ 30″ when a chronometer showed M. T. Green. 20 h. 45 m. 40 s., and observed altitude of ('s U.L. was 39° 47′ 20″ W. of meridian when the chronometer showed M. T. Green. 20 h. 48 m. 48 s. Latitude by D.R. 49° N., longitude 10° 45′ W. Height of eye, 28 ft. Run in interval between observations, N. 80° E. 0'5′ = d. lat. 0'1′ N.; dep. 0'5′ E. = d. long. 0'66′ = 0′ 40″ E.

Obsd. alt. of ⊙ Cor. Table E 28	35 12.5 3ft. + 9.5	⊙'s Dl. 11th 3¼ h. × 19″	22 13 1N + 1 2	Obsd. alt Dip•28 ft.	. of (39	47 20 5 13	₫ 's R.A. 11'2 m. ×	21 h. 2'0 s.	0 44 6.65 22.4
T. alt⊖-	35 22	Cor. decl. P. D.	22 14 3 N 67 46	Semi-d.*	39	42 7	Cor. R.A	۱.	0 43 44.25
Eq. T. 11th	м. s. 5 5°б7	Sid. T. (G. noc	н. м. s. m) 7 9 47'03	App. alt. H.P. 56' Cor. Rap	$er^{26_{2}''}$ $+$ er^{7} \cdot $_{39}$ $+$ $+$	9 26 31 - 42 25	ℂ's Dl. 11'2 m.×	21 h. 12.8"	10 29 20 N - 2 23
h. × '35 s.	- 1.14	Accl. 20 h. 484	m. + 3 25.15	T. alt. 🕡	's centre 40	0 8 56	Cor. dec	:I.	10 26 57 N
Cor. Eq. T.	5 4°53	M. ⊙'s R .A.	7 13 12.18				P. D.		79 33 3
A L P	35 22 49 0 67 46	Sec of Cosec of	830 57 033 55 3	A I. P	40 9 49 0 79 33		Sec o [.] Cosec o [.]	183057 007265	
$\frac{S}{S} - A$	76 4 40 42	Cos 9 Sin 9	381643 314313	S S – A	84 21 44 12		Cos 8 [.] Sin 9 [.]	993222 843336	
⊙'s H.A.	н. м. 4 4	s. 30'4E Sin ² 9'	412566	∉'s H.A. ∉'s R.A.	н. м 2 32 0 43	. s. 17'4 W 44'2	Sin ² 9	02688 0	
A. T. Sp. Eq. T.	19 55 + 5	29.6 4.5 A	·64 S	R.A. Mer.	3 16	1.0	A	1.47 S	
M. T. Sp. M. T. Gre	20 0 20 45	34'I 40 C ²	4/ N	M. U.S.	A. = 713	12.2	Б С2		to R
Long. in 7	Г. 045	6		M. T. G.	20 48	48	÷		
Longitude	11° 16	' 30" W		Long. in	T. 0 45	58.6	Cor	1	Staff
Long. (1)	11 15	50 W		Long. (2)	11 1	5 50 W	Cor.	.17	S to W
				Diff. long	. 13	49	d. long	1.34	
					1.34) 13.6	3' (10'3 '4			
						400 402			
			(2)		1.17	-		A	·17 (1)
d	. long. 1.3	34':lat. 1.0'							
.d. 1	ong. 13.8	: lat. cor. 10	3' S						1
								2.1	
L C	at. used 49	0 0 N 10 18 S	Long. (1) 11 17' × 10'3' =	15 50 W 1 45 W					/
L	at. in 48	49 42 N	Long. in	17 35 W					
									1
									Cortas

* See note on previous page about correcting moon's semidiameter and horizontal parallax for Greenwich date.

EXAMPLES TO FIND THE ERROR AND DEVIATION OF THE COMPASS.

(I.) BY SUN'S AZIMUTH.

1903.—On 23rd June, p.m., at ship, in latitude 35° 30' S., long. 175° o' E., when a chronometer which kept mean time at Greenwich showed 22 d. 16 h. 11 m. 39 s. the sun bore by compass N. 70° W.

Required the true azimuth and error of the compass by the A, B, C, Azimuth Tables; and supposing the variation to be 13° 30' E., required the deviation of the compass for the direction of the ship's head.



(2.) BY STAR'S AZIMUTH.

1903.—On 15th November, at about 3 h. 20 m. a.m., at ship, in latitude 39° 30′ S., longitude 177° 30′ E., when a chronometer (corrected) indicated mean time at Greenwich 14 d. 3 h. 30 m. the star a^2 Centauri bore by compass S. 41° E.

Required the true azimuth and error of compass by the A, B, C, Time Azimuth Tables; and supposing the variation to be 15° 30' E., required the deviation of the compass for the direction of the ship's head.

M. T. G. Long. E	D. 14 +	н. 3 11	м. 30 50	s. 0 0		Sid. T. (G Accl. 3 h.	. no 30 m	н.м. on) 15 29 . +	s. 38.6 34.5	
M.T. ship M. ⊙'s R.A.	14 +	15 15	20 30	0 13		M. ⊙'s R.	. A.	15 30	13'1	
Sid. T. ship ¥'s R. A.	-	6 14	50 33	130	or R. A.	of the mer	idia	n		
* 's H.A.		7	42	48)		A B	·39 S 1·96 S		
Lat. ¥ a Centauri		39° Ta	30 ble	S B	Ĵ	Table	С	2'35 S g	ives True Az. Compass bearing	S 28'9 E S 41'0 E
									Error Var.	12'I E 15'5 E
									Deviation	3'4 W

NOTE.—The H.A. of a star is found by taking the difference between the Sid. T. at ship and the star's R.A. The H.A. is east when Sid. T. is least, and west when Sid. T. is best.

EXAMPLES TO FIND THE CORRECT HOUR-ANGLE AND AZIMUTH WHEN TIME IS GIVEN IN NEW ZEALAND MEAN TIME.

(I.) SUN'S AZIMUTH.

1904.—On 24th May, at 3 h. om. p.m., New Zealand mean time. Required the sun's true azimuth by the A, B, C, Azimuth Tables, at Nelson, in lat. 41° 17' S. and long. 173° 15' E. = 11 h. 33 m.

M. T. N. <i>Z</i> . Long. 170° 30' E	D. H. M. 24 3 0 11 30	\odot 's Decl., 23rd Hr. var. 29" × 15'5 h. = cor.	20 24 11 N + 7 30	Eq. of Time Hr. var. 0'18 s. × 15'5 h. = cor.	M. S. 3 32°3. - 2°8
M. T. Green. Long. Nelson	23 15 30 + 11 33 E	Cor. Decl.	20 31 41 N	Cor. Eq. Time	3 29.5
M. T. Nelson Eq. of Time	$ \begin{array}{r} 24 & 3 & 3 \\ + & 3\frac{1}{2} \end{array} $	Lat. 41°3 S Decl. 20°5 N	A ·84 N B ·51 N		
A. T. Nelson	$24 \ 3 \ 6\frac{1}{2}$	H.A. 3h.6m.	C 1.35 N gives \odot 's	s true Az. N 44.7 W	

O's Azimuth by Burdwood's Tables, N 44º6 W

(2.) SUN'S AZIMUTH.

1904.—On 23rd December, at 7 h. o m. p.m., New Zealand mean time. Required the sun's true azimuth by the A, B, C, Azimuth Tables, at Wellington, in lat. $41^{\circ} 17'$ S. and long. $174^{\circ} 45'$ E.

Long. for Standard ti Wellington Cor. for diff. of long.	$me \frac{172}{174} \frac{30}{45} E$ $2 \frac{15}{15} = + 1$	9 m. to N.Z. M. time	[NOTE.—The Decl. and Eq. of Time may be taken out at sight with sufficient accuracy for azimuth purposes.]		
M. T. N.Z. Cor. for long.	D. н. м. 23 7 0 + 9				
M. T. at Wellington Eq. of Time	23 7 9 + I	Lat. 41.3 S Decl. 23.5 S	Ì	A '28 S named S because H. A. is more than 6 h. B '45 S	
A. T. Wellington	23 7 10	H.A. 7h. 10m.)	C 73 S gives ⊙'s Az. S 61 2 W	

⊙'s Azimuth by Burdwood's Tables, S 61'2 W

(3.) STAR'S AZIMUTH.

1904.—On 15th September, at 7 h. 30 m. p.m., New Zealand mean time, in lat. 43° 30' S. and long. 169° 40' E. Required the true azimuth of star α Centauri by the A, B, C, Azimuth Tables.

M. T. N.Z. Long. 172° 30' E	D. H. M. S. 15 7 30 0 - 11 30 0	Sid. T. (Green. noon) 14th Accl. for 20 h.	H M. S. II 29 8'8 + 3 17'I
M. T. Green. Long. 169° 40' E	14 20 0 0 + 11 18 40	M. ⊙'s R. A.	11 32 25'9
M.T. ship M.⊙'s R.A.	15 7 18 40 + 11 32 26	Lat. 43°5 S	A :45 N
Sid. T. ship ¥'s R. A.	18 51 6 14 33 1	H. A. 4h. 18 m.	C 1.50 S gives Azimuth S 42°6 W
*'s H. A.	4 18 5 W	True Azimuth by calculat	ion, S 42°55

GREAT-CIRCLE SAILING-COURSES.

The initial great-circle courses between any two places on the globe comprised within the zones of latitudes 85° N. and 85° S. may be quickly determined by the aid of the A, B, and C Tables. (See rule and examples below.) RULE.-Turn the difference of longitude between the two places into time, and

RULE.—Turn the difference of longitude between the two piaces into time, and consider this as the *hour-angle*; with this H.A. and the latitude of *departure* as latitude, take out the factor from Table A, and with the latitude of *destination* as declination, enter Table B. Follow the same rules as for finding and naming the azimuth, and Table C (azimuths) will give the *initial* course. Reverse the process, and we have the course at point of destination.

The following examples are taken from Norie's Epitome, so that it may be readily seen that there is no appreciable difference between the course as found by these tables and that obtained by the more rigorous and lengthy calculation which is generally used :---

Example (1).—Required the great-circle initial courses between Cape Runaway, New Zealand, in latitude $37^{\circ} 31'$ S., longitude $178^{\circ} 1'$ E., and Cape Horn, in latitude $55^{\circ} 59'$ S., longitude $67^{\circ} 16'$ W.

	(1.) Lat. 37 31 S. Long. 1 (2.) Lat. 55 59 S. Long.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	н. м. s. 7 38 5 2.
н.м. Н.А. 739	A '35 S.	н. м. Н.А. 739	A
Lat. $37\frac{1}{2}$ o S.	B 1.64 S.	Lat. 56 o S.	В [•] 84 S.
Decl. 56 o S.) C 1.99 S. gives Co. S. $32\frac{10}{2}$ E.	Decl. $37\frac{1}{2}$ o S.)	C $1^{+}52$ S. gives Co. S. $49\frac{1}{2}^{\circ}$ W.
		k	

Course from Cape Runaway, S. 32¹° E; or from Cape Horn, S. 49¹° W.

Example (2).—Required the initial great-circle courses between Otago, in latitude 45° 47' S., longitude 170° 45' E., and Panama, in latitude 8° 57' N., longitude 79° 31' W.

(1.) Lat. $\overset{\circ}{45}$ 47 S. Long. $\overset{\circ}{170}$ 45 E. d. long. H. M. S. (2.) Lat. 8 57 N. Long. 79 31 W. 109° 44' = 7 18 56.

H.A.	н.м. 719)	A	'37 S.	H.A.	н.м. 719	A	06 N.
Lat.	45 ³ / ₄ o S.	}	В	'17 N.	Lat.	9 0 N.	в	1.09 S.
Decl.	9 o N.)	С	'20 S. gives Co. S. 82° E.	Decl.	$45\frac{3}{4}$ o S.)	С	1'03 S. gives Co. S. 44 ¹ / ₂ ° W.

Course from Otago, S. 82° E.; or from Panama, S. 441° W.

Example (3).—Required the initial great-circle courses between a position off Lizard, in latitude 49° 50' N., longitude 5° 12' W., and 5 m. E. of Barbadoes, in latitude 13° 6' N, longitude 59° 20' W.

LI A	н. м.	٨		Н. М.	A
п.л.	3 30	A	00 3.	n.a. 3 30	A 175.
Lat.	49 50 N.	В	'29 N.	Lat. 13 0 N.	B 1.46 N.
Decl.	13 O N.	с	'57 S. gives Co. S. 69°'8 W.	Decl. 49 50 N.	C 1'20 N. gives Co. N. 38 ¹⁰ E
	5			15 0	

Course from Lizard, S. 70° W. ; or from Barbadoes, N. $38\frac{1}{2}^{\circ}$ E.

EXAMPLES TO FIND THE ERROR OF COMPASS FROM BEARINGS OF THE MOON AND OF THE STAR POLARIS.

(I.) BY MOON'S AZIMUTH.

1898.—On 6th January, at about 9h. 46m. a.m., M.T. at ship, in latitude 72° N., and longitude 25° 15' E., when a chronometer showed M.T. Green. 20h. 5m. 3s. the moon bore by compass N. 25° W. Required the moon's true bearing and the error of compass for the direction of ship's head.

M. T. Green. 5 d. Long. E	н.м.s. 2053 ⊢1410	('s R.A. 20h. 5 49 2 2 s. × 5 m. = +	s. 34 (*) 11 1"*8	s decl. $20 h$ 26 $36 \times 5 m$. = -	o 28 N 9
M. T. Sp. Sid. T. (G. noon) Accl. 20 h. 5 m.	21 46 3 19 0 24 + 3 18	Cor. R.A. 5 49	45 Co	r. de c l. 26	0 19 N
R.A. mer. ('s R.A. ('s H.A.	16 49 45 5 49 45 11 0 0W	H.A. 11 h. om. Lat. 72° N Decl. 26° N	} A B C	11'5 N 1'88 N 13'38 N gives Az.	N 13.6 W
				Compass bearing Error	N 25.0 W

(2.) BY STAR POLARIS AZIMUTH.

1906.—On 6th February, at 10 h. 30 m. p.m., A.T. at ship, in latitude 25° N., longitude $35^{\circ}45'$ E. Suppose * Polaris bore N. 4° E. Required the error of compass for the direction of ship's head.

A O's R.A 21 18 *'s R.A. + (24 h.) 25 25	Lat. 25° N. H.A. 6 h. 23 m. Table C. 32 m. Bible C. 32 m.
A.T. of \star 's mer. pass. 4 7 A.T. at ship 10 30	Compass bearing N 4.º E.
*'s approximate H.A. 6 23 W	Compass error 5'3 W.

ILLUSTRATIONS TO SHOW HOW LIVES AND SHIPS MAY BE SAVED BY THE CAREFUL OBSERVER, AND, CONVERSELY, HOW LIVES MAY BE LOST.

As it has been the duty of the writer for the last few years to carefully go over all the evidences in connection with strandings, &c., on the New Zealand coast, he has been more than ever impressed with the value of keeping up regular systematic bearings and astronomical observations. Personally, he has known the comfort and benefit of doing so by several years' experience, and of late has many times noted the sad consequences of neglect to do so.

As an illustration, let us take the case of a barque which stranded a few years ago, about 11 miles south of Kaipara Harbour. She was bound to Kaipara Harbour from Sydney in ballast, and at noon was about 143 miles from Kaipara Heads, with a fresh fair wind for her port. Towards evening (the weather apparently still fine) the barometer began to fall, and at 3 a.m. the wind had increased to gale force from W.S.W. Shortly afterwards land was seen, estimated to be 6 to 8 miles off. The land sighted was considerably to the southward of Kaipara Harbour, and the ship being in ballast it was impossible to beat off the coast to make either Kaipara or Manukau Harbours; there was therefore nothing left to be done but to run the ship on the softest spot on a lee shore. Now, had the master of this vessel been in the *habit* of getting the ship's position shortly after sunset by stellar observations, he would in all probability have been able to get a very accurate determination of the ship's position at about 7 p.m., or a little later, when only 50 miles or less from the range of Kaipara light, which he could then have steered for with confidence, and a certainty of making; and, as it happened to be H.W. at about 2 a.m., he would have had everything in his favour for an easy run into the harbour.

Another case was that of a large passenger steamer which was wrecked on the Three Kings—a disaster which caused the loss of many lives. So far as we are able to gather from the evidence given at the inquiry, the weather was fine, on the evening before the disaster, and in all probability the position of the ship might have been very accurately determined at about 7 p.m., when the ship was about 90 miles in advance of the noon position. Such an observation would most likely have shown which way the current was setting, and many lives would have been saved.

The third case within three years which has come before the New Zealand Courts in which a ship has been totally lost, but would in all human probability have been saved had the master taken stellar observations before dark, was that of a barque (2,192 tons) which was wrecked on Palmerston Island, Cook Islands.

At noon on 6th November observations were taken which showed that the South Point of islands bore S. 52° W. 98 miles, and north end bore S. 55° W. distant 95 miles. The ship was then on port tack, wind S.S.E. (true). The Captain then decided to go to leeward of the islands, and kept away a point. At 4 a.m. the look-out reported land on the starboard beam, and almost immediately afterwards the ship was on the reef.

From the evidence it was stated that the sky was clear at that time, so that there is little doubt but that a position obtained by stellar observation at about 7 p.m. would have shown the master how the current was setting, and enabled him to set a safe course to go clear of all dangers.

A fourth and more recent case was that of an auxiliary schooner which was stranded and wrecked on Minerva Reef in about 24° south latitude in June, 1915.

At 4 p.m. an observation was taken which made the ship to be 5 or 6 miles to westward of D.R. longitude from the noon position, but the master stated that he did not place much reliance on this observation.

Had the master been conversant with the problem of determining his position by two stars he could no doubt have got an accurate latitude and longitude simultaneously at twilight, at about 5.30 p.m., about two hours before the time when the ship was wrecked.

Since the loss of some of the vessels just mentioned I have received the more cheering news of the probable salvation of two large steamers owing to the master, or his officers, taking stellar observations, and so being warned in time of a dangerous set by an unusually strong current. The captain of a large liner of over 7,500 tons gross register wrote to the author in March, 1906, as follows: "During my ten years of command I have always used your tables for sun and star navigation, and invariably with excellent results and great success. In one instance particularly (of which I send you the working) it saved me from a narrow escape off Lincoln Island (northern extreme Island of Paracel group). Having experienced unusually strong currents setting to westward I kept well over to Macclesfield Bank, but nevertheless I took good observations in the morning and obtained cross bearings of stars, and was able to alter my course in time. Another shipmaster expressed gratitude that these tables had taught him the value of stellar observatiors, as such observations had been the means of saving his ship from stranding in the Bay of Bengal."

VALUE OF TWILIGHT STELLAR OBSERVATIONS.

Twilight (a few minutes after sunset, or a few minutes before sunrise) is far and away the best time out of the twenty-four hours for reliable observations. The horizon at that time is generally very clearly defined, without any glare, requiring no shades for the sextant, and two or three of the brightest stars with a suitable difference of bearing between them can often be observed, which will give a perfect position in both latitude and longitude at practically the same instant of time. The writer having made a regular practice of taking these observations for several years of his sea life knows well from experience that no other observations are to be compared with them. The noon position is as best only an approximation, and should never be relied on too implicitly, for though half a dozen men may take the meridian altitude and get the same result they may all be several miles in error, owing to some unusual excessive refraction near the horizon. The very agreement of so many observers would only give a false confidence, which is the more dangerous as there is no opportunity with the sun observation (except when near land) of checking it, and thereby determining the error. Then, again, the so-called noon longitude generally depends on an observation taken at about 8 or 9 a.m., and the calculation of the time from this observation is often made with an erroneous latitude, thereby giving a wrong result; and currents, or bad steering, &c., may again combine to still further throw the position out. With the position, however, obtained by simultaneous observations of two or three stars, errors resulting from uncertainty of refraction, &c., may be eliminated, and the position altogether should be much more accurate.

POWER OF SHIPOWNERS AND BOARD OF TRADE TO MINIMIZE DISASTER.

If shipowners made it compulsory for their officers to obtain the ship's position whenever possible by stellar observations at twilight, it would, I believe, be the means of saving many ships from disaster, and the saving of not a few lives; also, if this problem were given in our Board of Trade examinations for master and mate it would help greatly in making our ship officers familiar with it, and to further encourage the more frequent observations of this very important problem we would advocate that short and accurate methods of solving the problem by the use of up-to-date tables for facilitating the work should be allowed in the examination. The problem is now given in the voluntary examination for extra master, but it is given in a very unpractical way, requiring two observers with sextants as well as an officer to take the time; and the lengthy way in which it is required to be worked in the examination-room will be quite enough to deter most men from making anything like a daily practice of such an observation after their examination is over. To obtain confidence in the result of observations for any problem the navigator must make more than an occasional trial of it.

VALUE OF COMBINED OBSERVATIONS OF MOON AND PLANETS WITH THE SUN.

It may not be amiss here to remind navigators that when the moon is up in the daytime observations of moon and sun will also give both latitude and longitude at the same instant of time. Reference to example on p. 117, shows that the moon may often be observed on the prime vertical when, in the winter months, the sun never comes near to it. When the sun has a high south declination, the moon, when near the full, will have a high north declination, and *vice versa*, so that in the winter months it is especially good when in this quarter for longitude, and during the summer months for latitude. This observation, however, is even less frequently taken that of simultaneous observations of two stars, as this problem is not given even in the extra masters' examination; it also entails more work in the calculation, and the upper limb has often to be taken, which without practice is liable to be confusing. The planet Venus, too, may sometimes be utilized in the daytime. The writer has occasionally obtained the latitude from an observation of "Venus when on or near the meridian, at about 9 a.m., or 3 p.m., when the usual sights were taken for longitude. Captain W. P. Dawson, R.N., of H.M. surveying-ship "Penguin," has informed him that he has sometimes observed Jupiter, Sirius, and Canopus during the daytime. This must require good eyesight and a very clear atmosphere. The approximate altitude of the planet should, of course, be calculated, and the sextant set to it ; then, it the observer looks at the horizon in the direction of the meridian through a good telescope, he may see a little white speck near the horizon, which will be the reflected star. A pelorus set to the true north or south will be found helpful in directing to the spot.

On the back of the United States pilot chart of the North Pacific Ocean for November, 1909, published by the Hydrographic Office of the United States of America Navy Department, some very interesting experiences of stellar observations during strong daylight were given by Captain R. E. Thomas, of the British steamer "Swedish Prince." He states that on the passage from New York to the Brazils noon observations of Venus for longitude were made simultaneously with observations of the sun for latitude on fourteen dates, between September 21st and October 8th, 1906. On another occasion, while on a passage from Rio to New York, similar observations were taken on sixteen dates, between February 8th and February 26th, 1907. Using Venus and Jupiter in conjunction with the sun while on the passage from Cape San Roque to Barbadoes, in a current varying in strength and direction, he was able for a number of days to obtain four absolute positions in broad daylight during each day-viz., about 9 a.m., longitude sun, latitude Venus; about '10.30 a.m., latitude and longitude by observing Venus S.W. and sun S.E.; at noon, latitude sun, longitude Venus W.; and about 4 p.m., latitude Jupiter, longitude sun. During these days the noon longitude obtained solely by the sun could not but be considerably in error. In concluding he says: "I may add that Jupiter, though not so easily observed as Venus, is still worthy, of a place as an observable object by daylight, and one that will repay the patience and practice which its successful observing calls for."
EXAMPLE OF FINDING THE ERROR OF CHRONOMETER BY OBSER-VATIONS IN ARTIFICIAL HORIZON,

Showing the Use of Table D in working out several Observations separately.

1898.—On 16th April, at about 7 h. 10 m. a.m., M.T. at place. Suppose the following observations to have been taken at Observation Spot, Suez Dock. Index error of sextant -0' 34". Lat. 29° 56' 3" N., long. 32° 33' 12" E. = 2 h. 10 m. 12 8 s.

Approx. times	at Green. by chro	H. M. S n. 16593 165957 17023 17047 17113 17135	3. Obsd. alt. 7'5 7'5 7'5	$ \underbrace{\bigcirc}_{(1)}^{\circ} \underbrace{(1)}_{39} \underbrace{39}_{(2)}^{\circ} \underbrace{(2)}_{39} \underbrace{39}_{4} \underbrace{(3)}_{40} \underbrace{40}_{(4)} \underbrace{40}_{40} \underbrace{1}_{(5)} \underbrace{40}_{40} \underbrace{2}_{(6)} \underbrace{40}_{40} \underbrace{2}_{(7)} \underbrace{(6)}_{40} \underbrace{40}_{40} \underbrace{2}_{(7)} \underbrace{40}_{10} \underbrace{40}_$	A A A A A A A A A A A A A A	lt. diff. , " 10 40 11 0 10 30 10 20 10 30 11 40
Required the e	rror of chronon	neter.		(7) 40 2	5 20	11 40
M. T. G. D. H. M. S. 5 17 0 47 24 0 0	⊙'s Dl. 10 53'1" × 7 h.	6 12 S	Eq. T. 06s. × 7h.	M. S. 0 16 [.] 65 - 4 [.] 2	No. 4.— M	iddle Sight
From noon 6th 7 h.	Cor. Dl.	7 38 N	Cor. E. T.	0 12'45	I. E.	- 0 34
	P. D. 7	52 22				2) 40 10 16
A 20 18 35 L 29 56 3 P 79 52 22	Sec 0'062182 Cosec 0'006820	L. 30° , Az. 6°	Table D. 50° , gives 4.62 s. because altitude	to 1' alt. \div 2 e is doubled	App. lat. Ref. & par S. D.	$\begin{array}{r} 20 & 5 & 8 \\ r. & - & 2 & 30 \\ \hline 20 & 2 & 38 \\ + & 15 & 57 \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Cos 9 [.] 624999 Sin 9 [.] 847572	in artifici	ial horizon.		T. alt. −⊖	- 20 18 35
н. м. s. 4 49 12 ³	Sin ² 9'541573					
A. T. Sp. 19 10 47'7 Eq. T. – 12'4	A '19 S					
M. T. Sp. 19 10 35'3 Long. E - 2 10 12'8	C '00	gives Az. 90	° .			- ,?
M. T. G. 17 0 22'5 Chron. (4) 17 0 47'0	M.T.G	. (No. 4)	H. M. S. 17 0 22'5	M. T. G. (N	н √о.з) т	с. м. s. 6 59 58 3
	M. T. C Chron.	10 <u>2</u> 6. (No. 3)	16 59 58'3 17 0 23'0	M. T. G. (1 Chron.	No. 2) I	- 25°4 6 59 32°9 6 59 57°5
	Chron.	fast	0 24.7	Chron, fast		0 24.6
Н. М. M. T. G. (No. 2) 16 59 3 2'31 s. × 10 ² / ₃ ' – 2	s. 2'9 M.T.G 4'6 2'31 s. ×	(No. 4)	н. м. s. 17 о 22°5 + 23°9	M. T. G. (1 2'31 s. × 10	1 No. 5) I	и. м. s. 7 о 46°4 + 24°2
M. T. G. (No. 1) 16 59 Chron. 16 59 3	8'3 M. T. G 3'0 Chron.	. (No. 5)	17 0 46'4 17 I II'0	M. T. G. (1 Chron.	No. 6) 1	7 I 10 [.] 6 7 I 35 [.] 5
Chron. fast 0 2	4'7 Chron.	fast	0 24.6	Chron. fast	-	0 24'9
$\begin{array}{c} \text{H. M. };\\ \text{M. T. G. (No. 6)} & \text{i7 i i}\\ \text{2'3 i s. } \times \text{i1}\frac{3'}{3'} & + 2\\ \text{M. T. G. (No. 7)} & \text{i7 i 3}\\ \text{Chron.} & \text{i7 2} \end{array}$	s o'6 7 I 7 owi 7 6 inco 0 0 othe	t is eviden ng to the a prectly. It er six.	t that the last ltitude having is therefore re	observation been either ejected, and	was in err read off c a mean t	or, probably or put down aken of the

Results. Chron, fast

s

24'7 24'6

Observations with artificial horizon are not so much needed as they were twenty

 Observations with artificial horizon are not so much needed as they were twenty
 24.7

 or thirty years ago, as of late years time signals giving G.M.T. have been esta-blished at most places of importance. Still, it is well to be independent of such aids.
 24.6

 In the first place, they are not always reliable, and, secondly, in these days of steam
 24.6

 and rush a vessel sometimes arrives at and leaves a port again, as at Port Said, 24.9
 24.96

 before the time when the signal is given; and here are still many places where such aids are not to be found. The writer, when second officer, used sometimes to check the chronometer by observations of stars in the quicksilver, in his middle watch at night, when tied up in the Suez Canal or at anchor in the Bitter Lakes. Results were very astisfactory, as proved by observations east and west of the meridian, which did not generally differ more than 1s. from one other.
 44.66

 He never found it to social to gets unch observations of the sum on heard skip as in the daytime so many
 45.00

He never found it possible to get such observations of the *sun* on board ship, as in the daytime so many people are moving about; but in a large ship at anchor in smooth water observations in the quicksilver can often be taken at night, when all on board except the observer and time-taker are in bed, and everything is quiet.

9-Azimuth.

Chron. fast

0 22'4

REMARKS ON THE VALUE OF EQUAL ALTITUDES BY SEA.

We would draw attention here to the value of the short equal-altitude problem, as this method of obtaining the longitude, though very simple and useful, is seldom noticed by nautical writers. The problem is more especially useful in the case of stars, owing to there being no appreciable change in a star's declination, and because suitable ones can generally be found in any latitude. Even on dark nights a very fair longitude can generally be obtained, errors of altitude eliminating one another in a similar way as when stars are observed for latitude north and south of the meridian. An equally good result is obtained if both altitudes are observed the same amount too great, or too small. as if they had both been correct, and the problem is so simple that it takes very little longer than to get the latitude by meridian altitude-we mean, of course, when within the limits where correction for change of latitude and declination are not necessary.

The writer has often taken these equal altitudes about the same time as other observations have been taken-sometimes before daylight with an indifferent horizon, and at others with a good horizon a little before survise or after sunset—and they have nearly always agreed splendidly with the star-position longitude obtained by double altitude.

The navigator should not, however, use this method beyond its proper limits, and when the sun is observed it will seldom be useful except in the tropics, and then principally when running nearly due east or west, as on passages from Penang to Ceylon and Aden. When running due east or west *no* correction of altitude or time is required for ship's change of position, as she would change her longitude only by the portion of time which she gains or loses on the sun in the interval. Also, when the body observed bears east or west, *no* correction is required for several miles' change of latitude to the north or south; therefore it follows that when the observed body is near the prime vertical, and the change of latitude is small, it is not practically necessary to make any corrections for change of ship's position. Table 29 in Raper gives the hour-angle and altitude of a body on the prime vertical; and most other epitomes also have a table at any rate for giving the hour-angle of same, which is always useful for showing the best time to observe for longitude.

(1.) THE COMPUTATION (Raper, p. 801).

Take the mean of a.m. and p.m. times by chronometer : this, when the ship does not change her latitude, is the time by chronometer of apparent noon; when the latitude changes, this time is the time of approximate noon. Apply chronometer error and equation of time (p. II., N.A.), which will then show the A.T.G.; the difference between that and the apparent noon at ship being the longitude in time.

(2.) CORRECTION FOR CHANGE OF LATITUDE.

With half the interval as an hour-angle, compute the azimuth. To the log. sine of half the D. lat. made good, add the log. sec. of the lat. and the log. cotan. of the azimuth ; the sum, rejecting tens, is the log. sine of the correction in time.

When the ship has approached the sun or star in the interval, subtract this time The result is the from the above mean; when she has receded from the sun, add it. time by chronometer at apparent noon.

NOTE.—When the observed body is within 10° or so of meridian, the D. lat. made good in the interval may be added or subtracted from the altitude according as the ship has approached or receded from the sun, instead of going through the longer but more accurate computation.

LONGITUDE BY EQUAL ALTITUDES OF THE SUN.

EXAMPLE 1.—Ship steering nearly East or West. In lat. by D.R. 6° N. and \odot 's decl. 5° N. Equal altitudes of the sun were taken when chronometer times, a.m. and p.m., showed respectively 18 h. 10 m. 36 s. and 18 h. 42 m. 52 s. Chronometer fast on G.M.T. 10 m. 6 s. Required the longitude.

Chron. time a.m. Chron. time p.m	H. M. S. 18 10 36 18 42 52
	2) 36 53 28
Middle time by chron. Chron. fast	18 26 44 - 10 6
M. T. G. of Sp. A. noon Eq. T.	18 16 38 - 3 34
A. T. G. of Sp. A. noon A. T. Sp.	18 13 4 24 0 0
Long. in. time	5 46 56
Longitude	86° 44' o" E

EXAMPLE 2.- Where Ship has changed her Latitude between Sights.

Using the preceding example, with course made good N. 73° E. 7 m. = D. lat. 2'.

Half intl. as H.A Lat. 6° N Decl. 5° N	H. 1 A. 0 1 Table	M.S. 68 8 8 8 8	1.50 S 1.25 N	Half D. lat. 1°0′ Sin 6°464 Lat. 6° Sec 0°002 Az. 76° Cot 9°397			
Az. S 76°	"	С	•25 S	15'' = 1 s. to add. Sin $5'863$	н.	м.	s.
				Correction for change of latitude	18	20 + 26	44 1 45

Here the sun is to the southward and the course is to the northward, or the ship has *receded* from the sun.

As the change in \odot 's decl. never exceeds 1' in an hour, the correction for this may be disregarded when observations are taken within a few minutes of noon.

EXAMPLE 3. - Longitude by Equal Altitudes of a Star near the Meridian.

* 1898.—On 6th September, at about 5 h. 26 m. and 5 h. 36 m. a.m., A.T. at ship, in lat. by D.R. 9° 30' N., long. 63° E. Observed equal altitudes of * Aldebaran to the northward at 13 h. 49 m. 5 s. and 13 h. 59 m. 5 s. by chronometer which was fast of G.M.T. 37 m. 36s. Run in interval between observations, S. 75° E. 2 m. = D. lat. 0.5'.

1st chron. time 2nd chron. time	H. M. S. 13 49 5 13 59 5
	2)27 48 10
Chron. time of transit Chron. error	$ \begin{array}{r} 13 54 5 \\ - 37 36 \end{array} $
M. T. G. of transit Sid. T. (G. noon), 5th Accl. for 13 h . $16\frac{1}{2} \text{ m}$.	$\begin{array}{r} 13 & 16 & 29 \\ 10 & 58 & 2 & \cdot 2 \\ + & 2 & 107 \cdot 8 \end{array}$
Sid. T. at Green. Sid. T. at Sp. (*'s R.A.)	24 17 7.0 28 30 8
Long. in time	4 13 1 = 63° 15' 15" E

In this example, as the star was only 10° from the meridian, and the ship had receded from the star, o' 30'' less altitude was set to the sextant for the second observation.

There is no more work here than with the sun, as there is no equation of time to apply, and it is even easier to correct the sidereal time than the equation of time.

The writer's usual morning double altitude was taken 3 m. before this first sight, by Saturn and Sirius, both east of meridian, the resultant giving longitude, when brought up to the same time, within 1' of the equal-altitude longitude. He has taken several with equally good results, though in this case it was probably accidental that so near an agreement with the other observations was obtained, as better results might have been expected with a longer interval of time, when the star would have been nearer the prime vertical; daylight, however, prevented this.

It is best to choose stars with declination nearly the same as latitude, or else of the same name and the declination less than the latitude. If the declination is greater than the latitude, as in the last example, it does not come to the prime vertical at all; neither does it if the declination and latitude are of contrary names. With latitude and declination of same name, when the numbers corresponding to the hour-angles in Tables A and B nearly agree is always a good time. For instance, in latitude 46° N., at hourangle oh. 20 m., with * Capella, the numbers in Tables A and B exactly agree, both being 11° ; Capella, therefore, with that latitude and hour-angle would be exactly on the prime vertical.

The following example (on p. 128) will show how a star may sometimes be observed almost on the prime vertical to within 2 or 3 minutes of its meridian passage, or at any time within 2 or 3 hours of its transit.

^{*} The actual observations for this and the following example were taken in 1885, but for the sake of uniformity are here worked for the year 1898.

EXAMPLE 4.—Longitude by Equal Altitudes of a Star nearly East or West. 1898.—Colombo towards Aden. On 13th October, at 6 h. 24 m. and 6 h. 34 m. p.m. (ship time). Observed equal altitudes of * Altair at 2 h. 16 m. 55 s. and 2 h. 28 m. 24 s. by a chronometer which was fast of G.M.T. 39 m. 4 s. Star's azimuth at 1st obns., S. 80° E. Lat. by meridian altitude, 8° 46' N. Run in interval, N. 80° W., distance $2\frac{1}{2}$ m.

1st chron. time	2 16 55
2nd chron. time	2 28 24
	2)4 45 19
Chron. time of transit	2 22 39 ^{.5}
Chron. error	- 39 4
M.T.G. of transit Sid. T. (G. noon) Accl. for 1 h. 43 ¹ / ₂ m.	$ \begin{array}{r} 1 43 35'5 \\ 13 28 16'3 \\ + 17 \end{array} $
Sid. T. at Green.	15 12 8 ^{.8}
Sid. T. at Sp. (*'s R.A.	19 45 51 ^{.6}
Long. in time	$4 33 42'8 = $ long. $68^{\circ} 25' 42'' E$

Equal altitudes of this star were taken in the twilight for three or four evenings running. A few miles change of ship's position N. or S. in this case would not have affected the longitude 1'.

The following example gives the position of ship, latitude by ex-meridian (with azimuth 45°), and longitude from equal altitude observations. The problem is also plotted on the chart, and the same result obtained.

POSITION OF SHIP BY SHORT EQUAL ALTITUDE OBSERVATIONS OF SUN.

1898.—On March 20th, about noon, approximate position of ship on Equator in longitude 75° E. Observed alt. of \odot 's L.L. was 89° 20' S.E. when a chronometer indicated M.T.G. 19d. 19h. 6 m. 9 s., and again (p.m.) the observed alt. of \odot 's L.L. was 89° 20' S.W. when chronometer indicated M.T.G. 19d. 19h. 9 m. 1 s. Course and distance run between the observations west o $\frac{1}{2}$ m. Height of eye 40 ft. Required position of the ship at apparent noon.

D. H. M. S. M. S. Obsd. alt. 89 20 Sd. 19 19 6 9 19 9 1 Interval 2 52 M.T.G. (a.m.) Run W M.T.G. (p.m.) ----2 Cor. (p. 87) + 10 89 30 2) 38 15 10 2) 2 50 True alt. Middle time by Chron. 7 35 19 H. A. 1 29 Eq. of time . Var. hrs. M. S. Eq. T. A.T.G. A.T. Sp. Hr. var. 59'3 × 5 7 31.4 s. hrs. 0 0 Cor. '75 × 5 24 0 0 3.2 1 57 S Decl: 296.2 ō Long. in time 57 S Cor. eq. T 7 35'I 5 0 0 4 3'75 4 56.5 Longitude noon 75 0 0 E 74 59 45 E o o E Cor. decl. o 6 54 S Long. at 2nd Obn FOR REDUCTION. T. Alt. 89 30'0 S Redn + 8.8 FOR AZIMUTH. Mer. Alt. 89 38'8 S M. S. Az. 45°, Table C (p. 40) gives in Lat. o° A and B Cor. 1°0' which gives (p. 145) Redⁿ at 1 m. = 6°2' × 1°42 m. H.A. Sin 7'791 90 1 25 0.0 89° 30 Alt. Sec 2.059 45° Az. 6 Sin 9.850 M.Z.D. 0 21.2 N = Redn 8.8'Decl. 0 6'9 S Lat. 0 14'3 N





The accompanying chartlet gives a good illustration of the "Sumner" principle in connection with this problem without any logarithmic calculations for H.A., azimuth, or reduction, and it confirms the above method of calculation.

We are indebted for this method to the writer's old friend Captain T. S. Angus, Nautical Inspector for the P. and O. S. N. Company, one of the keenest and most enthusiastic navigators he ever met. The method is as follows, viz.: Observe an altitude while the azimuth is yet large, and as soon as the Z.D. is small enough to be conveniently measured on the chart with a pair of dividers. Plot the geographical position of the sun (lat. = decl., long. = G.A.T.), and from this position as centre sweep an arc with Z.D. as radius. This is a position-line. Wait until the azimuth has sufficiently changed to give a good cut, and repeat the operation, the intersection gives the position at once without any further calculation.

The following figures give all that is necessary for plotting on the chart.

1st obsn. A.T.G.	H. M. S. 18 58 34 W or 5 1 26 E	Lat. (decl.) $\stackrel{\circ}{o}$ 6'9 S Z.D. 0 30 as radius	2nd obsn.	H. M. S. 19 I 26 W or 4 58 34 E
Long. Run west	75 21 30 E 30 W		Long.	74° 38′ 30″ E
Long. at time of 2nd obsn.	75 21 OE	Chart position at 2nd obsn. Lat Long. 74° 59' 45" E	. 0° 14.2' N	3

REMARKS ON EX-MERIDIAN AND MERIDIAN ALTITUDES.

Although we have at the present day quite a number of special very useful exmeridian tables, apart from the standard navigational epitomes, we would here remind those who use Raper that there are tables in that epitome which make very short work of this problem when within the ordinary ex-meridian limits, and the limits of 35° of declination. When within the limits of latitude 35° these tables may also be used for stars of any declination up to 62° N. or S., by using the declination as latitude, and vice versa. The following examples will illustrate this :--

EXAMPLE 1.—In lat. by D.R. 10° N., T. alt. of $* \alpha$ Crucis 16° 10', hour-angle of star 1 h. 10 m. Required the reduction to meridian.

at. 10° N. as decl.	$\begin{cases} \text{decl. } 62^\circ 35' \text{ S.} \\ \text{as lat.} \end{cases}$	(Table 70 (1 h. 10 m.	Log 9 [.] 978 Sin ² 8 [.] 364	
	Reduction True reduction	°′′′′ 1 15 34 . 1 15 19	Sine 8'342	

EXAMPLE 2.—In lat. by D.R. 23° 30' S., T. alt. of * α Crucis 50° 53', hour-angle oh. 10 m. Required the reduction to meridian.

H.A. oh. 10 m. Lat. $23^{\circ} 30'$ S. decl. $62^{\circ} 35'$ S. as decl. as lat.	{	Table 75 o h. 10 m.	Log. Sin ²	0'127 6'678	
Reduction 2' 12"			Sine	6.805	

In the first example the error from the calculated reduction by Raper's table only amounted to 15'' with no error in the second, although the first example was outside the limits of the ex-meridian tables of Brent, Walter, and Williams, which tables until lately were considered to have exceptional limits, especially on account of comprising declination limits up to 70° .

of comprising declination limits up to 70° . The tables, however, at the end of this book are available for any latitude, or declination from Pole to Pole, and the time-limits of the first example might have been extended for another 50 min. without making more than about $\frac{1}{2}'$ of error in the reduction. See limits on pp. 144 and 152.* Larger ex-meridian tables by the author, which are published in another volume, give still more extensive limits, sometimes as much as 3 hours from the meridian (and in a new edition of the work now in the Press) when the azimuth is sometimes over 70° from the meridian.

^{*} Tables of Calculated Hour-angles and Altitude Azimuth Tables (30° N. to 30° S.), Ex-meridian Tables (70° N. to 70° S.), and Calculated Reduction and Azimuths of 30 Bright Stars (64° N. to 60° S.), by H. S. Blackburne. Second Edition. Price 105. 6d. Published in United Kingdom by Thos. Ainsley, James Brown and Son, and J. D. Potter.

In this work the actual reductions and azimuths are taken out at sight for 30 of the brightest stars for limits far exceeding that of any other reduction tables, and as the reductions and azimuths have been calculated for the actual declination of the stars a minimum of interpolation is required in the use of the table. It would be impossible to make position-finding from two stars simpler than by the aid of these tables. An example is given on p. 128 of this work with an altitude of $80\frac{1}{2}^{\circ}$ and azimuth of 45° . In this example the hour-angle was accurately determined by equal altitudes close to the meridian, otherwise this latitude by ex-meridian would only be of value as giving a latitude on the meridian of the D.R. longitude, and the position-line or circle of altitude at right angles to the bearing of the object, to be used in conjunction with another observation. Taken as a single observation 4 sec. of error in the time would make 1' of error in the latitude. (See Table M, pp. 156 and 157.)

EXTENSION OF LIMITS IN USE OF TABLES NO. 1 AND No. 2.

A very considerable extension of the ex-meridian limits of Tables No. 1 and No, 2 in this work can also be obtained by transposing latitude and declination as shown in example on p. 163. For instance, in Table 1, in latitude 25° and declination 50° , contrary names, the limits of time within which a correct reduction can be obtained by the table is 150 m., but with latitude 50° and declination 25° it is only 49 m. *Caution.*—It must, however, be remembered that you cannot get the correct azimuth or position-line by transposing latitude and declination, so that if latitude and declination as transposed for the reduction a further determination of the A and B correction will be required to find the position-line.

VALUE OF HIGH DECLINATION STARS FOR EX-MERIDIANS.

Stars with high declinations are especially valuable for ex-meridian observations, and in high latitudes it is best to choose circumpolar stars, near the meridian below the Pole, as these stars change very slowly both in altitude and azimuth, and consequently errors in time only produce small errors in the resulting latitude. The amount of error due to 4 sec. of time is seen at a glance from Table M, pp. 156 and It was the recognition of the great value of these stars for both latitude and 157. azimuth that induced the writer to calculate the actual true reduction and azimuth for twenty of the brightest circumpolar stars up to 2 to 3 hours from the meridian at the inferior transit. These tables make it almost as easy to determine the latitude by ex-meridian as by the meridian altitude when within the limits of the table, and also to set the sextant to the approximate altitude, which is a great advantage when taking twilight stars. The writer has lately calculated the reduction and azimuth in the same way for thirty of the brightest stars when near the meridian at the superior transit. High-declination stars are also preferable for observations of the meridian altitude, as a few minutes will then generally elapse without any appreciable change of altitude, both before and after meridian passage; and it is a good plan to take several observations—say, 5 m. before to 5 m. after meridian passage—unclamping the index each time, and to take the *mean* of these observations for meridian altitude. This plan is far preferable with stellar observations for latitude (except when altitude is very high) to that which is so often adopted of watching for the star beginning to fall.

It is necessary to caution against this prevailing plan (in these days of rapid steam navigation) even with the sun, as by so doing the observation is sometimes taken 10m. or more after *noon*, and at others a few minutes before noon. This was brought prominently to the writer's notice many years ago, when second officer of a new mailsteamer. He made it a practice always to correct his watch and the ship clock before noon by comparison with chronometer and longitude applied. On one occasion when proceeding due south off Cape Finisterre, in a winter month, the captain and a couple of officers were observing for the meridian altitude. The writer reported that it was noon when his watch came round to the hour, but the captain said he did not make it so, and the sun was still rising; we all therefore remained aft by compulsion until the captain made the sun to dip, at about 10m. after noon, and the writer was wrongly and thoughtlessly blamed for the clock being in error. In this particular case the ship was steaming directly towards the sun at about 14 knots an hour, and by this change of position, had the sun been stationary, the altitude would have increased 14" in 1 m. of time, or 70'' in 5 m. of time, and had the *ship* been stationary the sun would have only dipped o' 36'' in that time; therefore the altitude would have increased to observer o' 34". The sun's change of declination in 10 m. would only amount to 2", and is not therefore taken into account.

If the clock had then been put back, and bearings of the land had been obtained, the supposed meridian altitude would have given a latitude $2\cdot 4'$ N. of that by bearings; or if the time had been taken by chronometer, and the observation worked out as an ex-meridian, it would be found that a correction of 2'4' was required to be added to the altitude. Should the observation be taken of a high-declination star, such as a Crucis, anywhere in the tropics, either north or south of the Equator, the natural fall of altitude in 10m. would be less than $2\frac{1}{2}$ if latitude and declination were of same name, and barely $1\frac{1}{2}$ with latitude and declination of contrary name. When the meridian altitude of the moon is observed for latitude the moon's change of declination must also be remembered, which is very rapid when near the Equator, varying in different years from a little over of to a little over 18' an hour.

Mr. C. Westland has drawn the writer's attention to a method of finding the hourangle of maximum altitude by the help of the A & B Tables, as follows :-

Assume reduction at 1 m. from meridian $=\frac{15'}{2 [A \pm B]}$ (Formula of Ex-meridian Table No. 2.)

Then H.A. of maximum altitude is given in minutes of time by $\frac{K [A \pm B]}{I}$ and since 15' 1 m. of time is equal to 15' of arc it follows that the numerator of this fraction is the

required H.A. expressed in arc. $Rule. - Express the difference in motion of lat. \pm decl. (that is K) in minutes of arc$

per minutes of time, and multiply it by A ± B for 1 m. To reduce to time subtract one third and move decimal point one place to left.

Example .--- Using data above, and disregarding change of decl. (as it only amounts 'to 0.2'' in 1 m. of time), K = 14'' = 0.233'. °. N. A

1

Lat. 43 N A 2137 S
Decl. 23 S B 973 S
C
$$3110 \times \text{K o}^2 23 = 7246 = 4.83 \text{ m.} = 4 \text{ m. 50 s.}$$
 Required H.A. of maximum altitude.
Subt. $\frac{1}{3} = \frac{24.15}{48.31}$

This method is considerably shorter and easier to remember than the methods usually given in navigational books.

A FEW NAVIGATIONAL NOTES AND CAUTIONS.

EXCEPTIONAL EXCESSIVE REFRACTION NEAR THE HORIZON.*

It has often been pointed out in text-books of navigation and elsewhere that altitudes observed at sea are subject to error when peculiar atmospheric conditions operate to produce an extraordinary deflection of the ray of light from the horizon, and thus to make the actual angle of dip vary from its tabulated value. It is believed that attention can not be too frequently directed to this important subject, for the reason that there are undoubtedly many navigators who do not realize the magnitude of the error that may be involved: some have the impression that this error is such as to throw the results out by no more than a mile or so, and hence may be neglected for all practical purposes; others, while knowing that in the Red Sea and other special localities the error is to be guarded against, do not consider that it need ordinarily be feared by the navigator. It can be demonstrated that this error may attain a value so great as to jeopardize a vessel, even if a very large margin be allowed for inaccuracy of the sights, and that the conditions under which it is produced are such that it may occur in any region of the ocean. It has been seen that the conditions necessary to produce extraordinary deflections

of the rays require that the atmosphere shall arrange itself in a series of horizontal strata of uniformly varying density. It follows, therefore, that the mere difference in temperature between air and water is not sufficient in itself to produce the error, and that any cause that interferes with the formation of strata will prevent the occurrence of the deflection. As wind, by keeping the air in motion, renders the conditions unfavourable for the existence of layers of unequal density, it follows that a light breeze will,

* Extract from a publication issued by the Bureau of Equipment, Department of the Navy, Washington D.C.; by Lieutenant G. W. Logan, U.S. Navy.

in general, greatly reduce the error, and that a strong one will effectually prevent it. Hence it is that the maximum bending of rays is to be expected in calm weather. It seems probable that the stratification is more likely to be disturbed when the air is colder than the sea than in the opposite condition, since the heavier particles are then above the lighter, and the atmosphere is in a state of unstable equilibrium that may be easily disturbed.

Both theory and experience show that the higher the eye of the observer is placed above sea-level the smaller are the deflections from the causes under consideration. It is therefore well, especially when there is reason to suspect the conditions that produce abnormal deflections, to observe altitudes from the highest available position.

One of the most dangerous features of this error is that there is no satisfactory method of arriving at a correct estimate of its amount. If the conditions with which it is necessary to deal were fixed in their nature, such, for example, as the mean atmospheric conditions for which the ordinary dip-table is computed, it would be a simple matter to arrive, either by theory or experiment, at the amount of the deflection. But the elements of the problem can not, in their nature, be known. For instance, the conditions of temperature and wind at a distance of several miles from the observer, which can not be determined at the ship, have an important bearing on the solution; so also with the amount of moisture in the air, which is doubtless a material factor. The navigator may, however, recognize the existence of the disturbing conditions and the probable direction in which the disturbance will affect the results of his observations, and with this knowledge he must make ample allowance for possible errors.

From a very large number of recorded instances of abnormal deflections of the rays of light from the horizon, due to inequality of temperature between sea and air, a few will be chosen to illustrate the possible magnitude of this error.

It is related that on one of Captain Cook's voyages the meridian altitude of the sun was being taken when a light snow-squall came on. The horizon and sun remaining visible, the altitude shown by the sextant had almost instantly to be altered 32' to maintain contact, the horizon having appeared to fall by that amount when the air surrounding the observers was cooled by the snow-squall. At the same time a distant mountain-peak, which before had stood well above the horizon, almost disappeared from view. Both of these effects vanished with the passing of the squall, the measured altitude resuming its former value and the peak rising again above the horizon. Even if we are inclined to doubt the instruments of those times, and therefore the exactness of the observed difference, this account is of interest in showing at how early a day the presence of this error was recognized in navigation.

According to Raper, Mr. Fisher observed in the Arctic regions a variation of 18' in the place of the horizon.

The late Captain Lecky, in his "Wrinkles," states that on a clear day in midwinter, off the coast of Long Island, five observers at noon closely agreed upon an altitude which gave a certain latitude; in less than two hours afterwards the land was sighted, and the latitude brought forward from the meridian altitude was found to be 14' in error.

Lieutenant Koss and Ensign Thun-Hohenstein, of the Austrian Navy, while conducting observations near Pola for finding the variation in the dip of the horizon, observed on a quiet day a rise of the apparent horizon above its computed position of 8' 47'' at a height of 5_0 ft., and of g' 23'' at a height of 33 ft. above water. Of the numerous instances that might be cited of extraordinary errors in the results

Of the numerous instances that might be cited of extraordinary errors in the results given by astronomical sights in the Red Sea (so extraordinary as to have given rise to an erroneous belief as to the currents existing in that body of water), it may be mentioned briefly that Lieutenant Marshall, U.S. Navy, of the U.S.S. "Detroit," found errors of position from 12' to 18' arising from sights of the sun; Captain Nedden, of the s.s. "Madeline," found the latitude by observation to differ 10 miles from the correct one, and images of islands to be greatly distorted; and Captain Lecky discovered the positions of certain islands to be apparently 7 to 8 miles in error in one direction from morning sights, and a similar amount in error in the opposite direction from afternoon sights.

A similar instance of error in the region of the Gulf Stream was reported by Lieutenant-Commander W. L. Rodgers, U.S. Navy, of the U.S.S. "Lancaster," two lines of position from the sun intersecting at about 7 miles to the south-east of the ship's true position, and two from stars intersecting at a like distance in the opposite direction, the direction of the error in each case according with that which was to be expected from the observed differences in temperature of air and water.

As a result of what has been set forth, the following brief summary may be given for the guidance of navigators:--

(a.) The inaccuracy of tables showing the dip and the visibility of objects should always be suspected when there is a marked difference between the temperature of the air and that of the sea-water.

(b.) The errors will be largest in calm weather and when the eye is not far elevated above the sea, and will decrease as the wind increases and the eye is raised.

(c.) When the air is warmer than the water, the visible horizon is raised above its normal position; the altitude corrected by the ordinary dip-table will be too small, and the resulting Summer line will be farther from the observed body than the true line. An object will be sighted from a greater distance than usual.

(d.) When the water is warmer than the air, the visible horizon is lowered below its normal position; the altitude corrected by the ordinary dip-table will be too large, and the resulting Summer line will be nearer the observed body than the true line. An object will be sighted from a less distance than usual.

A few years before the time of writing this a very well authenticated case of undoubted excessive refraction was brought to the notice of the writer by an old pupil (Captain W. H. Sweny), then commanding the P. and O. s.s. "Mooltan." At about 6 p.m. on April 11th, 1910, he took observations of four different stars for a position—viz., Procyon (ex-meridian) to northward, Rigel to north-westward, Canopus to south-westward, and β Centauri to south-eastward, to cross with one another. The chief officer took an ex-meridian of Pollux to northward, and Rigel and β Centauri toria cross. Shortly afterwards the fourth officer took Procyon, Canopus, β Cen-tauri, and Jupiter to eastward. Captain Sweny first sent the writer his own observations, asking him to work them out and let him know what he made the resulting position. This was done, and when the captain afterwards sent the results of his work both positions were in agreement and evidently not more than about 1' in error in either latitude or longitude. The captain also sent the workedout observations of the other two officers, and from all these observations the writer was able to deduce fairly accurate separate positions, and it was evident from these observations that refraction was excessive all round the horizon, but greatest to the northward, where it was about 11.0', and in other parts of the horizon averaging about $6\frac{3}{4}$, the altitudes being smaller by these amounts than they should have been by allowing the usual tabular corrections. The height of eye when these observations were taken was 50 ft. If the captain had been satisfied with the ex-meridian observations of Procyon and Pollux, and the longitude of β Centauri, he would have been 11' or 12' out in the latitude and 33' out in the longitude. By using the observations intelligently he was practically correct in his position, and made Rottnest Light nearly ahead at 2 a.m. His position at the time was about 30° 4' S. and 113° 47' E.

The above related experiences, though undoubtedly very exceptional, should tend to warn navigators not to trust too implicitly even in daylight to observations taken on one side only of the meridian, or prime vertical; for though such excessive refraction is very rare, and may not be experienced in the lifetime of a frequent observer, it is probable that such amounts as 2' difference from the tabulated value of refraction is not uncommon.

EFFECT OF ALTITUDE ERRORS.

With a.m. sights too great an altitude will place a ship to eastward of true position, and *vice versa* with p.m. sights and too small an altitude. The amount of error in longitude or time due to 1' error of altitude is shown in Table D.

OBSERVATIONS IN ARTIFICIAL HORIZON.

In correcting the altitude taken in artificial horizon, *first* apply index error, then halve the altitude after which apply the other corrections—viz., refraction, parallax, and semidiameter.

When the lower limb is taken with a.m. sights the suns appear to be separating, and when the upper limb is taken the suns appear to be closing in on one another. *Vice versa* with p.m. sights.

NUMBER OF FIGURES TO USE WITH LOGARITHMS.

Using more than four figures of logarithms in working any of the sailings is generally a waste of figures; as also in working an altitude or time azimuth or the time when hour-angle is less than 2 hours.

In Bowditch's "American Practical Navigator" not more than five figures are given in any of the tables, and the work is thereby much facilitated.

CORRECTIONS OF SUN'S DECLINATION AND EQUATION OF TIME.

For ordinary sea practice it is generally useless precision when correcting the sun's declination to take out the hourly variation to decimals of a second; also, one place of decimal is amply sufficient when correcting the equation of time.

CORRECTION OF A PLANET'S R.A. AND DECL.

Daily change of R.A. was 236'3 s., and of decl. 28.8'.

To find correction for R.A. due to 96h. from noon: Add a cipher to 24 h., then with 240 in dist. column look out the nearest number abreast it in either the dep. or d. lat. column. This will be found at 10° in d. lat. column—viz., 236'4. Having added a cipher to 24 h. the decimal point in 96 h. must be removed one figure to the right; then look out the number in d. lat. column against 96 in dist. column and the correction 94.5 s. will be found.

To find correction for decl. due to 9.6 h. from noon : 28.8' is the change in 24 h. At 33° in the traverse-table we find 239 9 in d. lat. column against 286 in dist. column, and again 96.4 in d. lat. against 115 in dist. .: 11.5' will be the correction (nearly).

NOTES ON MERCATOR AND MIDDLE-LATITUDE SAILINGS.

Mercator's sailing should be used generally when the course is between 1° and 70° , especially with long distances and in high latitudes. With a large course, and using either Raper or Norie, the distance may sometimes be considerably in error owing to the meridional parts not being given to decimals. The following examples will illustrate this :-

Find the true course and distance from lat. 5° 28' N., long. 85° 30' E., to lat. 5° 34' N., long. 91° o' E.

BY MERCATOR'S SAILING (RAPER'S TABLES).

	Lat. 5 2 Lat. 5 3	28 N 39 N	Mer. pts. Mer. pts.	328 340	Long. 8 Long. 9	ο 5 30 Ε 1 0 Ε					
	D. lat.	II N	M. d. lat.	12		5 30 E 60					
					D. long, M. d. lat.	330' 12'	Log Log	12°5185 1°0792	D. lat. L	og 1.0414	
				Cou	rse N. 87° 5	5' E.	Tan	11'4393	Sec	1*4396	
									Log	2.4810	
								•	Distance	302.7 mil	les
				By	INMAN'S	TABL	.es.				
	5 28 N 5 39 N	Mer. p Mer. p	ts. 328.50 s. 339.55	L M). long. 330 I. d. lat. 11	' Log 05' Log	g 12.5 g 1.0	185 434 D.	lat. 11' I	og 1.0414	
D.1	at. 11 N	M. d. l	at. 11.05	Ċ	Course N.88	°5′ Tai	n 11.4	751 Se	c of Co.	1*4753	
						Dis Raj	tance	328.6 m 302.7	iles I	og 2.2167	

By MIDDLE-LATITUDE SAILING.

25'9 miles

Difference

Lat. $5 28$ N Lat. $5 39$ N Mid. L. $5 33\frac{1}{2}$	D. long. 330' Mid. lat. 5° 332' Dep. 328'5 D. lat. 11'	Log 2'5185 Cos 9'9980 Log 12'5165 Log 1'0414	Course 88° 5' D. lat. 11' Dist. 328 6 miles	Sec Log Log	1'4753 1'0414 2'5167	
	Course 88° 5'	Tan 11.4751		0		

To take out the distance accurately for a large course, as between 85° and 90° , the log. of secant should be taken out to seconds; this may be practically done by bearing in mind that the secant and tangent differences here are almost the same. Thus in the last example the difference between the sec. and tan. in the fourth figure is about 2; then add 2 to the log. tan. of course.

When the course is large the distance is very readily found from the traverse-table by a comparison of the dep. with the dist. column. For instance, with an 88° course, distance 329 is 0.2 greater than the departure; with an 87° course, distance 329 is 0.5 greater than the departure. In the same way, when the course is within 3° or 4° of the meridian, the distance will be nearly the same, but a trifle greater than the d. lat.

SIMPLE METHODS OF FINDING THE SHIP'S DISTANCE FROM A POINT BY TWO BEARINGS AND THE RUN IN INTERVAL BETWEEN THEM.

As so many strandings have occurred on the New Zealand coast owing to the neglect to take or make use of bearings, it has been thought advisable to give the following simple methods for *approximately* determining the ship's distance from a single point or light when cross-bearings are not obtainable. The methods here given have the advantage of being determined quickly, with a minimum of calculation, without leaving the deck or having to plot the bearings on a chart. Figure 3 and Table H were first published in the writer's first edition of "A and B Tables," &c., and their value has since been further impressed on navigators by the late Captain Lecky in the latest editions of his famous "Wrinkles." The writer has also been pleased to notice that some of the local steamers now have a brass plate on the bridge marked somewhat after the style of Figure 3.

PROBLEM I.—To find the Distance from a Point when the Angle on Bow is doubled.

Whenever the angle between the course and object is doubled, the distance run in the interval is the distance off at second bearing. The well-known four-point bearing illustrates this, and, as the second bearing then gives the distance off abeam, it is most frequently used; but it is often very useful to be able to know the distance off at an earlier period, as illustrated by Fig. 1.



Example.—A ship making 10 miles an hour on a S.E. course by compass sighted Kaipara light, bearing E.S.E.; after continuing to make good the same course and speed for 57 m. the light bore E. Required the distance from the light when second bearing was taken.

First bearing E.S.E. 2 points on bow; second bearing E. 4 points on bow; angle doubled: the distance run in interval between bearings will be the distance off at last bearing. Interval 57 m. $=\frac{57}{60}$ or 0.95 of an hour x 10 gives run in interval, 9.5 m. the distance off.

It is apparent from the figure that if this course is continued the ship will probably run foul of the North Spit. (See Fig. 1.)

Problem 2 will illustrate how by the aid of the traverse-table the course may quickly be set to pass a safe distance off.

PROBLEM 2.—From a known Distance from Object, to set Course to pass any required Distance from it.

Rule.—Enter the traverse-table with the distance required to pass off in the dep. column and the present distance off in dist. column. The course heading this will be the angle to bring the object on the bow.

Example as shown in Fig. 2.—Ship steering S. 45° E. by compass, Kaipara light bore E. distant 9.5 m. Set the course to pass 8 m. off the light. Enter the traverse-table with distance 9.5 in dist. column, and turn over until the nearest to 8.0 is found in dep. column. This is found at 57° . Bring the lighthouse 57° on bow, or course by compass S. 33° E. 9.5 in dist. column gives 7.97 in dep., and 5.17 in D. lat. column, the distance to run. Fig. 2 illustrates this



The advantage of knowing the distance that a ship will *pass off* a point on a given course, in good time before coming up to it, struck the writer many years ago when he was quite a junior officer, and he then made out the figure given below, which has often been used since.

The distance run in the interval between any two of the following bearings will give the distance that the ship will *pass off* the object if the same course is continued and *made good*.

PROBLEM 3.—To find the Distance a Ship will pass off an Object when abeam by the Distance run in Interval between certain Bearings as given below.



Between 22° and 34° " 41° 25° The distance run will be 45° 2630 the distance the ship will 32° 59° " pass off 37° 72° 45° 90° 45° $63^{1\circ}_{2}$ the distance run will be half the distance the ship will pass off.

The numbers under base of figure represent the length of the base of the rightangled triangle proportionate to the perpendicular of 10. Thus, should the ship be passing 10 miles off an object, and the object be 22° on bow, ship will be 24.8 miles from the beam bearing.

The traverse-table gives the three sides of right-angled triangles for every degree of angle subtending the base or perpendicular. If, therefore, we know the angle on bow and the perpendicular—i.e., the distance the ship will pass off the point when abeam—the other two sides of the triangle—viz., the distance off at the time, and the distance to run to beam bearing—are seen at a glance from the table.

Say angle on bow is 32° , and previous bearings give distance to pass off 10 m. Open traverse-table at 32° and against 10 in dep. column, we have 18'9 in dist. column as the distance off, and 16'0 in the D. lat. column as the distance to run to beam bearing.

Example.—A ship steering north observes a light bearing N. 32° E.; after running on same course for 6 o miles the light bears N. 59° E. Required the distance the ship will pass off the light if she continues on the same course, and the distance from the light at time of second bearing.—*Answer*: Distance run in interval (6 o miles) will be the distance the ship will pass off the light. Then, opening the traverse-table with 59° as course, and 6 in dep. column, we find 7 in dist. column as the distance the ship will be from object at that time.

As a ship changes the bearing of an object much more rapidly when nearing the beam bearing than at any other time, the distance that a ship passes off a point will be better determined by the run in interval between the two bearings of $63\frac{1}{2}^\circ$ on bow and $63\frac{1}{2}^\circ$ from stern—or, in other words, when it is $26\frac{1}{2}^\circ$ from the beam bearing before and abaft—than at any other time.

It sometimes happens that a light or point is not sighted till after the ship has passed the four-point bearing. In such case Table H will be found useful, and might be copied out and put inside the wheel-house for ready reference.

PROBLEM 4 (by Table H).—To find the Distance from an Object when abeam by the Distance run between Beam Bearing and any other Bearing before or abaft the Beam.

					010 L L.				
° 35 36 37 38 39 40 41 42 43 44	·70 ·73 ·75 ·78 ·81 ·84 ·87 ·90 ·93 ·97	• 45 46 47 48 49 50 51 52 53 54 •	1.00 1.04 1.07 1.11 1.15 1.19 1.23 1.28 1.33 1.38	55 56 57 58 59 60 61 62 63 64	1.43 1.48 1.54 1.60 1.66 1.73 1.80 1.88 1.96 2.05	° 65 66 67 68 69 70 71 72 73 74	2°14 2°25 2°36 2°48 2°61 2°75 2°90 3°08 3°27 3°49	° 75 76 77 78 79 80 81 82 83 84	3'73 4'01 4'33 4'70 5'14 5'67 6'31 7'12 8'14 9'51

Table H.

Rule — Enter the table above with the number of degrees that the object is on the bow, and take out the factor given in the table abreast it. This factor multiplied by

the run in the interval between the bearing on the bow and the bearing of the object when abeam will give the distance off when abeam.

Example. — A lighthouse is observed 70° on bow, ship's speed 10 m., and interval in time to beam bearing 48 min.

 $_{48}$ min. = 0.8 of an hour × 10 m. = 8 m. for the run in the interval.

Against 70° in the table is 2.75, which $\times 8 \text{ m}$. gives 22 m., the distance off when abeam; or by traverse-table, enter with 70°, and with distance run 8 m. in D. lat. column, gives distance off in dep. column = 22 m., and 23.4 m. the distance off when first bearing was taken.

CHART METHODS.

PROBLEM I.—To find the Distance from an Object by Two Bearings, and the Run in Interval between them.

Rule.—Lay off the first bearing and the ship's course, then lay off the last bearing, and measure off the distance run on the course since the first one was taken; through this distance draw a line parallel to the first bearing: the point of intersection between this line and the second bearing should be the ship's position.

Example (see Fig. 5).—A ship steering from A towards B on a N. 20° E. course sights a point bearing N. 65° E.; after running on this course for $18^{\circ}5$ m. the point bears S. 70° E. Required the distance off at second bearing by plotting on the chart.

Lay off the course N. 20° E., also the bearing of P. N. 65° E.; then measure 185 m. on the line of course from this bearing, and make a mark; through this mark draw a line parallel to the bearing N. 65° E.; then the intersection of this line with the second bearing will be the ship's position, which gives 185 m. as the distance off.

PROBLEM 2.—To find the Distance from an Object by Two Bearings of Differen Objects with Run in Interval between the Two Bearings.

This problem is exactly the same in principle as the "Sumner" with two sun observations, and the writer when at sea often found it of great practical use, though he never found other navigators make use of the method (except after he had drawn their attention to it), nor is the method presented, so far as he is aware, in other nautical works. It is now given occasionally in New Zealand in the examination of masters and mates in the chart-examination problems.

Rule.—The rule for problem 2 will be exactly the same as for problem I.

Example (see Fig. 6).—A ship steering from C towards D on a N. 45° E course sights a point N. bearing S. 15° E.; after running on this course for 15° 6 m. point R is sighted bearing N. 85° E. Required the distance from R at second bearing.

Lay off the course N. 45° E. from C to D, also the bearing of N. S. 15° E.; then measure $15^{\circ}6$ m. on the line of course from this bearing, and make a mark; through this mark draw a line parallel to the bearing S. 15° E.; then the intersection of this line with the second bearing will be the ship's position—viz., S. 85° W. $17^{\circ}2$ m. from point R.

This problem may often be used with advantage at night-time with two lights when one light is sighted shortly after the other one has been lost; or where the simultaneous bearing of two lights or two points makes too large an angle for a good fix. It will also be found useful in foggy weather in close navigation, where one near point after another may be just seen for a few minutes and then obscured



again. The bearing of these points in combination (the first bearing having been moved forward for the run in interval) will then generally give a good fix.

The distances in these plottings have been taken from the diagonal scale below the figures; the opportunity having been taken to draw attention to this handy useful scale, which any one can easily make for himself.



EXPLANATION OF THE DIAGONAL SCALE AND PROTRACTOR.

In the diagonal scale, the shorter lines dividing the length into equal portions (units) are crossed perpendicularly by 10 others extending the length of the scale. The end division, or unit, has its upper and lower edge subdivided into 10 equal parts, and diagonal lines are drawn from the beginning of one division to the end of the opposite one. This effects a further subdivision by 10, as an example will show. To take the No. 18'5 from this scale by the compasses: Set one foot at 1, and the other at the 8th line on the lower edge of the subdivided unit; this gives 18. Now follow up the diagonal line at the 8 to the 5th line of the long parallel lines, and fixing the point there, extend the other point to meet the line which rises at 1, crossing the breadth; and the number is taken.

10-Azimuth.

The same process serves for tens and units as for units and tenths, and so on; thus the No. 1.85 or 185 is taken as above.

To lay off or measure an angle by the marked divisions. Place the middle point of the scale or ruler (which is strongly marked) on the meridian line, and, keeping it there, incline the ruler to the required angle, which is shown by the graduated scale of degrees coinciding with the upper part of the meridian line. Field's parallel ruler is marked in this way, and is very useful in laying off true bearings.

Caution.—The distance found by any of these methods from bearings with a run interval must only be considered as an *approximation*, as they depend on the course and distance run in interval having been made good. If, therefore, a current is known to exist, allowance must be made for it.

Cross-bearings of two (or, better still, three) prominent points will give a more certain position, provided the error of compass is known, and the angles are neither too large nor too small for a good "fix," and the points are accurately laid down on the chart; but every careful man will have at least two strings to his bow, and the position as found by run and interval will be a good check against possible errors. I think every one will admit their liability to such mistakes as reading off the wrong bearing, or applying the variation the wrong way, &c., and for this reason it is therefore always better to take *three* cross-bearings, when such are available.

Examples in the use of all these methods of finding the position of the ship by bearings, either with or without the chart, are given in the New Zealand examinations of either the home or foreign-going candidates for masters and mates.

THE COMPASS AND PELORUS.

Some owners do not seem to realize the value of having a proper compass, with a suitable position selected for it in the ship. Dozens of New Zealand ships would but for the Adjusters' reports be without any proper appliances for taking bearings, and many of the compasses are so closely surrounded by iron that no deviation card can be depended on. I would like here to point out the value in coastal navigation of having a Pelorus, which can be shifted to a stand made for it from one side of the bridge to the other, as is needed. The instrument is generally made of brass, being a *dumb* compass card without needles. It is a convenient plan to have the Pelorus set to the true geographical course, or else the magnetic course the ship is steering; then any bearings taken by it will be true, or magnetic, as the case may be, and free from the trouble of applying the error or variation of the compass. It may also be set to zero, N. or S., and the angle on the bow will then be readily read off for greater convenience in finding the distance off points, as in the problems which have been here mentioned.

the distance off points, as in the problems which have been here mentioned. Warning.—Do not use the Pelorus for long-distance bearings, such as Mount Egmont, 50 miles off.

LECKY'S DANGER-ANGLE TABLE.

When mentioning up-to-date methods of finding the ship's position at sea, Lecky's splerdid little book, "The Danger-angle and Off-shore Distance Tables," ought not to be passed over. The book is in two parts: The tables in Part I comprise heights from 50ft. to I.100 ft., and distances from a cable's length up to five miles; they can only be used in connection with objects lying on or within the bounding line of the observer's horizon; for objects beyond the horizon Part II has been calculated. The tables in Part II comprise heights from 200 ft. to 18,000 ft., and distances from five miles up to roo miles. They are intended to be used with objects lying beyond the horizon, and the observed altitude must be corrected after the index has been applied by subtracting the true depression corresponding to the height of the eye, and also one-twelfth of the roughly estimated distance from the mountain. Under the result as a corrected altitude, and abreast the height of the summit in the left-hand margin of the tables, will be found a very close approximation to the true distance. This distance, combined with a bearing of the mountain, fixes the ship's position with a minimum of labour. For an example, suppose the peak of Mount Egmont to be observed from the ship's deck 25 ft. above the water, bearing east magnetic,

Altitude	••	••	2 °	32'	o″	
25 ft. dip (from table)	••	••	-	5	19	
Approximate distance One-twefth of approxima	 ate distar	 nce	2	26 2	41 30	
Corrected altitude Height of Mount Egmor	 it	•••	2 8,	24 270	ft.	gives distance off $29\frac{1}{2}$ m.

SUPPLEMENTARY EX-MERIDIAN TABLES.

EXPLANATION OF TABLES.

Ex-meridian Table No. 1.

The factor under the heading of Reduction abreast the A and B Correction is the reduction at τ min. from the meridian to apply to an altitude to reduce it to the meridian altitude.

INSTRUCTIONS CONCERNING THE USE OF TABLE AND RULE FOR APPLICATION.

Multiply the factor corresponding to the A and B correction under the heading of Reduction by the number of minutes and decimals in the hour-angle from the meridian, which then gives the correction to apply to the observed altitude to reduce it to the meridian altitude. *Add* this correction to the observation taken near the upper meridian passage, and *subtract* the correction when observation is taken near the meridian below the Pole.

This reduction will not be more than $\frac{1}{2}'$ in error when the hour-angle is less than that shown in the accompanying table immediately following, which shows the limits within which it is safe to use the table without appreciable error.

The table gives the correct reduction at 1 m. from the meridian for any azimuth up to 45° from the meridian, or the equivalent A \pm B correction in latitude 0° , and has been rigorously calculated by seven figure logarithms from the following formula: ----

Cot. Z.D. = sin. azim. \cdot cot. H.A. I m. Tan. decl. = sin. H.A. I m. \cdot cot. azim. Cot. az. = A \pm B correction.

In latitude o° decl. = M.Z.D. and Z.D. - M.Z.D. = reduction.

TABLE SHOWING LIMITS OF REDUCTION TABLES NO. 1 AND NO. 2.

These two tables show at a glance the hour-angles at which it is safe to use Reduction Tables No. 1 and No. 2, so that with the *correct time* the reduction will not be in error more than $\frac{1}{2}$ '. It must, however, be borne in mind that the resulting latitude is the latitude corresponding to the meridian of longitude used in the deduction of the time. The A and B correction through Table C readily gives the azimuth, which subtracted from 90° gives the true line of position for a Mercator Chart; or through Table C² it gives at once the position-line for use with a plane chart. This position-line must be laid down from the meridian of the D.R. longitude used in determining the time.

When the H.A. is on, or four or five minutes less than the limit given in the table, 0.4' may be added to or subtracted from the reduction calculated by Ex-meridian Tables No. 1 and No. 2, according as the letter against the minutes is g or l. If the H.A. is more than 5 m. less than the limits in the table the reduction may be considered as correct, and in either case the resulting reduction would seldom be as much as $\frac{1}{4}'$ in error.

When the letter n is marked after the minutes in the table the resulting reduction will seldom be as much as $\frac{1}{4}'$ in error. When the altitude is over 75° both time and altitude should be used in the determination of the azimuth, and the A and B correction corresponding to this azimuth should be used in finding the reduction. See examples on pages 105, 128, 158, 160, &c.

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Ex-meridian Table No. 2.

The instructions and rules relating to this table are exactly the same as for Table No. r.

Formula used in the calculation:

Reduction for
$$i \min = \frac{15'}{2 [A \pm B]}$$
.

NOTE.—This table is entirely independent of Table No. 1, which will generally give the best results and widest limit. Table No. 2 is given on account of the wide limits of reduction which it gives with high declinations and low latitudes; and the same wide limits may be obtained when in high latitudes, and low declinations by transposing latitude for declination, and *vice versa*. A glance at the tables showing the limits of the two ex-meridian tables will at once show whether it is most advantageous to use No. 1 or No. 2 Ex-meridian Tables. (See example page 163.)

Table M.

Showing the Error in Latitude due to an Error of 4 Seconds in Time or 1' of Longitude.

This table (pages 156 and 157) shows at a glance the error which would result in the latitude from any single observation out of the meridian for every 4 sec. of error in the time.

When two observations are taken the factors given in this table facilitate the problem of finding the ship's position from two ex-meridian observations, or one chronometer observation, and an ex-meridian (see page 95).

Formula used in the calculation: Lat. error = Tan. azim. cos. lat.

Table	showing	the	Hour	-angle	Limits	within	which	the	Error	of	the	Reduction
	calc	ulate	ed by	Ex-me	ridian	Table N	0. 1 w	ll no	t excee	ed ()•5.	

					LATI	TUDE	AND	DECLI	NATIO	N OF 3	SAME	NAME				
it.								Dr	CLINATI	ON.						
La	0 -	2 °	4 °	6 °	8 °	10 °	15°	20 °	25°	30 °	35 °	40 °	45 °	50 °	60 °	70 °
	M. 4n 8n 12n 20n 24l 25l 27l 26l 27l 30l 30l 30l 35l 38l 39l 40l	M. 8n 4 ⁿ 16l 20l 22l 25l 27l 28l 30l 32l 30l 32l 34l 36l 37l 40l	M. 16n 12n 8n 4n 8n 4n 16l 17l 20l 22l 22l 27l 29l 31l 33l 34l 35l 38l	M. 24n 20n 16n 12n 8n 4 ⁿ 8n 14l 17l 20l 23l 26l 22l 30l 32l 33l 35l 37l	M. 32n 28n 20n 16n 12n 8n 8l 13l 17l 20l 24l 28l 32l 32l 32l 32l	M. 4°g 35g 28g 24g 20n 16n 8n 8l 19l 22l 27l 30l 32l 35l 37l	M. 42g 39g 36g 35g 34g 30g 20n 12l 11l 17l 21l 27l 30l 33l 36l 20g	M. 44g 42g 38g 35g 35g 35g 34g 35g 18l 10l 16l 20l 23l 27l 32l 34l	M. 46g 45g 42g 41g 39g 37g 36g 35g 40g 16l 9l 15l 20l 24l 28l 32l	M. 48g 47g 46g 45g 44g 43g 44g 39g 37g 36g 51g 13l 9l 16l 21l 25l 29l	M. 51g 50g 48g 48g 47g 46g 46g 46g 42g 39g 39g 39g 29l 12l 16l 21l 25l	M. 53g 51g 50g 49g 48g 48g 47g 44g 44g 43g 427l 13l 16l 21l 26l	M. 55g 55g 53g 50g 50g 50g 50g 50g 50g 48g 48g 44g 44g 43g 54g 26l 11l 17l 22l	M. 58g 56g 56g 55g 52g 52g 52g 52g 52g 50g 48g 46g 46g 46g 13 <i>l</i> 	M. 63g 62g 62g 62g 62g 62g 62g 57g 57g 55g 51g 48g 47g 50g 65g 30l 15l	M. 71g 71g 70g 69g 68g 68g 66g 66g 66g 65g 63g 61g 59g 57g 54g 54g 54g
00	420	411	401	391	390	401	IN	FERIC	R TRA	NSIT.	1 290	201	1230	190		1 400
		NO	TF			ţ;					Decli	NATION.				
						й 	25°	30°	35°	40 °	45°	50°	55°	60°	65°	70 °
g s l s n s	ignifi ducti tabul ignifi ducti tabul signif no er: withi angle great	es th on is ar re es th on is ar re ies th ror as n lim e whic er th	hat t great ducti hat t great ducti hat t great its o ch giv an 1	rue r ev that on. rue r s that on. here taso. f hout $e A \pm 000'$	re- an is 5' Ir- B	° 25 30 35 40 45 55 60 65 70 75 80 85	M. 53 <i>l</i> 58 <i>l</i> 66 <i>l</i>	M. 48 <i>l</i> 53 <i>l</i> 54 <i>l</i> 59 <i>l</i> 68 <i>l</i>	M. 54 <i>l</i> 55 <i>l</i> 55 <i>l</i> 56 <i>l</i> 69 <i>l</i>	M. 56 <i>l</i> 57 <i>l</i> 55 <i>l</i> 55 <i>l</i> 57 <i>l</i> 58 <i>l</i> 62 <i>l</i> 70 <i>l</i>	M. 60 <i>l</i> 60 <i>l</i> 59 <i>l</i> 59 <i>l</i> 59 <i>l</i> 60 <i>l</i> 63 <i>l</i> 72 <i>l</i>	M. 68 <i>l</i> 65 <i>l</i> 63 <i>l</i> 62 <i>l</i> 61 <i>l</i> 61 <i>l</i> 64 <i>l</i> 72 <i>l</i>	M. 80 <i>l</i> 75 ^{<i>j</i>} 70 <i>l</i> 68 <i>l</i> 67 <i>l</i> 65 <i>l</i> 62 <i>l</i> 62 <i>l</i> 62 <i>l</i> 66 <i>l</i> 74 <i>l</i>	M. 1 30 <i>l</i> 100 <i>l</i> 80 <i>l</i> 74 <i>l</i> 70 <i>l</i> 69 <i>l</i> 63 <i>l</i> 66 <i>l</i> 68 <i>l</i> 74 <i>l</i>	M. I03g I80l I1cl 90l 86l 78l 78l 74l 70l 70l 72l 76l	M. 88g 95g 107g 123g 120l 105l 92l 84l 79l 78l 75l 78l
				L.	ATITU	DE A	ND DE	CLINA	TION (OF CON	VTRAK	Y NAM	IES.			
at.		1		1	1		1	Di	ECLINAT	ION.	-		1		1	
–	0°	2 °	4 °	6 °	8 °	10°	15°	20 °	25 °	30 °	35°	40 °	45 °	50°	60°	70 °
° 1 2 3 4 5 6 8 10 12 15 20 25 30 35 40 45 55 60	M. 4n 8n 10n 20n 24l 25l 26l 27l 28l 30l 32l 32l 35l 38l 39l 40l 42l	M. 12n 16n 2cn 26l 28l 30l 29l 30l 32l 34l 35l 36l 38l 40l 41l 42l	M. 20n 24n 28n 32l 32l 32l 32l 32l 32l 32l 32l	M. 28n 32n 36l 40l 38l 34l 34l 34l 35l 35l 35l 35l 37l 38l 39l 41l 42l 44l	M. 36n 40n 44l 48l 44l 41l 40l 39l 36l 36l 36l 36l 37l 39l 40l 41l 42l 42l 42l 42l 42l 42l 42l 42	$\begin{array}{c} \text{M.} \\ 42g \\ 44g \\ 50n \\ 56n \\ 60l \\ 48l \\ 44l \\ 40l \\ 39l \\ 39l \\ 39l \\ 39l \\ 40l \\ 40l \\ 42l \\ 43l \\ 44l \\ 45l \end{array}$	$\begin{array}{c} \text{M.} \\ 45g \\ 48g \\ 52g \\ 56g \\ 80n \\ 85n \\ 60l \\ 48l \\ 48l \\ 43l \\ 43l \\ 42l \\ 42l \\ 42l \\ 42l \\ 42l \\ 42l \\ 44l \\ 45l \\ 46l \\ 46l \\ 46l \end{array}$	M. 45g 48g 53g 58g 62g 72g 12n 64l 58l 53l 53l 49l 46l 46l 45l 46l 45l 46l 45l 48l 48l 48l 48l 48l 48l 48l 48	M. 48g 50g 54g 56g 59g 62g 76g 115 ¹ 74 ¹ 60 ¹ 54 ¹ 54 ¹ 54 ¹ 49 ¹ 48 ¹ 49 ¹ 49 ¹ 49 ¹ 49 ¹ 49 ¹ 50 ¹	M. 50g 52g 54g 56g 59g 58g 68g 80g 74l 60l 53l 52l 52l 52l 52l	M. 52g 54g 55g 58g 58g 66g 72g 88g 140m 72l 61l 56l 55l 55l	M. 55g 56g 57g 58g 68g 68g 68g 98g 90l 70l 62l 66l 62l 66l 62l 60l	M. 578 588 588 588 608 648 648 648 648 130n 861 721 691 651 	M. 59g 59g 60g 61g 62g 64g 66g 70g 70g 1501 861 781 	M. 62g 63g 64g 67g 68g 70g 72g 74g 90g 90g 	M. 71g 72g 74g 74g 75g 76g 76g 76g 76g 70g 80g

A and B Cor.	Reduc- tion.	A and B Cor∎	Reduc- tion.	A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.						
1.000	6.212	1.070	5:018	1.1.0	5.647	1,210	=	1.280	5.165	1.250		1,120	1.752
1.001	6.209	1.071	5.014	1.140	5.647	1.210	5.390	1.281	5.162	1.350	4.951	1.420	4.732
1.002	6.205	1.072	5.910	1.142	5.639	1.212	5.390	1.282	5.158	1.352	4.945	1.422	4.746
1.003	6.200	1.073	5.906	1.143	5.636	1.213	5.386	1.283	5.155	1.353	4.942	1.423	4.744
. 1 .004	6.196	1.074	5.902	1.144	5.632	1.214	5.382	1.284	5.152	1.354	4.939	1.424	4'74I
1.005	6.191	1.075	5.898	1.145	5.628	1.215	5.379	1.285	5.149	1.355	4.936	1.425	4.738
1.000	6.187	1.070	5.894	1.140	5.024	1.210	5.370	1.280	5.140	1.350	4.933	1.420	4.735
1.008	6.178	1.078	5.886	1.14/	5.617	1.218	5.374	1.288	5.143	1.35/	4.930	1.427	4.733
1.000	6.174	1.079	5.882	1.149	5.613	1.219	5.365	1.289	5.136	1.359	4.924	1.429	4.727
1.010	6.170	1.080	5.878	1.150	5.610	1.220	5.362	1.290	5.133	1.360	4.921	1.430	4.724
1.011	6.165	1.081	5.874	1.121	5.606	1.321	5.358	1.291	5.130	1.361	4.918	1.431	4.722
1.012	6.157	1.082	5.870	1.152	5.002	1.222	5.355	1.282	5.127	1.302	4.915	1.432	4.719
1.017	6.152	1.084	5.862	1.153	5.505	1.223	5.354	1.293	5.121	1.303	4.010	1.433	4.710
1.015	6.148	1.085	5.858	1.155	5.591	1.225	5.345	1.295	5.118	1.365	4.907	1.434	4 /14 4·7II
1.019	6.144	1.086	5.854	1.156	5.588	1.226	5.342	1.296	5.115	1.366	4.904	1.436	4.708
1.012	6.139	1.087	5.850	1.157	5.584	1.227	5.338	1.297	5.111	1.367	4.901	I·437	4.705
1.018	6.135	1.088	5.846	1.158	5.580	1.228	5.335	1.298	5.108	1.368	4.898	1.438	4.203
1.020	6.127	1.089	5.828	1.159	5.577	1.229	5.331	1.299	5.105	1.369	4.895	1.439	4.700
1.021	6.122	1.001	5.834	1.101	5.260	1.230	5.340	1.300	5.000	1.370	4.880	1.440 1.44T	4.098
I.022	6.118	1.092	5.830	1.162	5.566	1.232	5.321	1.302	5.096	1.372	4.886	1.442	4.692
1.023	6.114	1.093	5.826	1.163	5.562	1.233	5.318	1.303	5.093	1.373	4.883	1.443	4.690
1.024	6.110	1.094	5.823	1.164	5.559	1.234	5.315	1.304	5.089	I·374	4.881	1.444	4.687
1.025	6.105	1.095	5.819	1.165	5.555	1.235	5.311	1.302	5.086	1.375	4.878	1.442	4.684
1.020	6.007	1.0007	5.815	1.100	5.551	1.236	5.308	1.300	5.083	1.376	4.875	1.440	4.682
1.028	6.003	1.008	5.807	1.165	5.540	1.237	5.305	1.307	5.000	1.377	4.860	1.447	4.676
1.029	6.089	1.099	5.803	1.169	5.54I	1.239	5.298	1.309	5.074	1.379	4.866	1.440	4.674
1.030	6.084	1.100	5.799	1.170	5.537	1.240	5.295	1.310	5.071	1.380	4.864	1.450	4.671
1.031	6.080	1.101	5.795	1.171	5.533	1.241	5.291	1.311	5.068	1.381	4.861	1.421	4.668
1.032	6.076	1.102	5.201	1.172	5.530	1.242	5.288	1.312	5.065	1.382	4.858	1.425	4.666
1.033	6.067	1.103	5.787	1.173	5.520	1.243	5.285	1.313	5.062	1.383	4.855	1.423	4.663
1.034	6.063	1.104	5.780	1.174	5.510	1.244	5.278	1.314	5.056	1.304	4.840	1.454	4.658
1.036	6.059	1.100	5.776	1.176	5.515	1.246	5.275	1.316	5.053	1.386	4.847	1.456	4.655
1.037	6.055	1.107	5.772	1.177	5.512	1.247	5.272	1.317	5.049	1.387	4.844	1.457	4.652
1.038	6.050	1.108	5.768	1.178	5.208	1.248	5.268	1.318	5.046	1.388	4.841	1.428	4.650
1.039	6.040	1.109	5.764	1.179	5.505	1.249	5.265	1.319	5.043	1.389	4.838	1.429	4.647
1.040	6.028	T.TTT	5.757	1.180	5.501	1.250	5.202	1.320	5.040	1.300	4.835	1.400	4.044
1.042	6.033	1.112	5.753	1.182	5.497	1.252	5.255	1.322	5.034	1.391	4.830	1.401	4.630
1.043	6.029	1.113	5.749	1.183	5.490	1.253	5.252	1.323	5.031	1.393	4.827	1.463	4.637
1.044	6.025	1.114	5.745	1.184	5.487	1.254	5.249	1.324	5.028	1.394	4.824	1.464	4.634
1.045	6.021	1.115	5·741	1.185	5.483	1.255	5.246	1.325	5.025	1.392	4.821	1.465	4.631
1.040	6.012	1.110	5.737	1.180	5.480	1.250	5.242	1.326	5.022	1.396	4.819	1.460	4.629
1.048	6.008	1.118	5.730	1.188	5.473	1.258	5.236	1.328	5.016	1.308	4.813	1.467	4 020
1.049	6.004	1.119	5.726	1.189	5.469	1.259	5.233	1.329	5.013	1.399	4.810	1.469	4.621
1.020	6.000	I·I20	5.722	1.130	5.466	1.260	5.229	1.330	5.010	1.400	4.807	1.470	4.618
1.051	5.996	1.121	5.718	1.191	5.462	1.261	5.226	1.331	5.007	1.401	4.805	1.471	4.616
1.052	5.088	1.122	5.714	1.192	5.459	1.202	5.223	1.332	5.004	1.402	4.802	1.472	4.013
1.054	5.983	1.123	5.707	1.193	5.455	1.203	5.220	1.333	1.008	1.403	4.799	1.473	4.011
1.055	5.979	1.125	5.703	1.195	5.448	1.265	5.213	1.335	4.995	1.405	4.793	1.475	4.605
1.056	5.975	1.126	5.699	1.196	5.445	1.266	5.210	1.336	4.992	1.406	4.790	1.476	4.603
1.057	5.971	1.127	5.696	1.197	5.44I	1.267	5.207	1.332	4.989	1.402	4.788	1.477	4.600
1.058	5.967	1.128	5.092	1.198	5.438	1.268	5.203	1.338	4.986	1.408	4.785	1.478	4.598
1.059	5.050	I·I 20	5.684	1.199	5.434	1.209	5.102	1.339	4.983	1.409	4.782	1.479	4.595
1.061	5.955	1.131	5.681	1.201	5.427	1.271	5.191	- 340 I•34I	4.977	1.411	4.776	1.481	4.590
1.062	5.951	1.132	5.677	1.202	5.424	1.272	5.190	1.342	4.974	1.412	4.774	1.482	4.588
1.063	5.947	1.133	5.673	1.303	5.421	1.273	5.187	1.343	4.971	1.413	4.77I	1.483	4.585
1.064	5.943	1.134	5.669	1.204	5.417	1.274	5.184	1.344	4.968	1.414	4.768	1.484	4.582
1.005	5.034	1.135	5.000	1.205	5.414	1.275	5.181	1.345	4.965	1.415	4.705	1.485	4.580
1.067	5.930	I.137	5.658	1.207	5.407	1.277	5.174	· 540 I·347	4 902	1.417	4.760	1.487	4 5//
1.068	5.926	1.138	5.654	1.208	5.403	1.278	5.171	1.348	4.957	1.418	4.757	1.488	4.572
1.069	5.922	1.139	5.651	1.209	5.400	I.279	5.168	1.349	4.954	1.419	4.755	1.489	4.570

A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.
1.400	4.567	1.560	4.306	1.630	4.235	, 1.700	4.085	1.770	3.011	1.840	3.812	L'OLO	2.680
1.491	4.564	1.561	4.393	1.631	4.232	1.701	4.083	1.771	3.944	1.841	3.811	1.011	3.688
1.492	4.561	1.562	4.390	1.632	4.230	1.702	4.081	1.772	3.941	1.842	3.809	1.912	3.686
1.493	4.559	1.563	4.388	1.633	4.228	1.203	4.078	1.773	3.939	1.843	3.807	1.913	3.684
1.494	4.557	1.564	4.386	1.634	4.226	1.704	4.076	1.774	3.937	1.844	3.805	1.914	3.682
1.495	4.554	1.565	4.383	1.635	4.224	1.705	4.074	1.775	3.935	1.845	3.804	1.915	3.681
1.490	4.532	1.567	4 301	1.637	4 221	1.707	4.072	1.777	3.833	1.840	3.802	1.017	3.079
1.498	4.547	1.568	4.376	1.638	4.217	1.708	4.068	1.778	3.929	1.848	3.798	1.018	3.676
1.499	4.544	1.569	4.374	1.639	4.215	1.709	4.066	1.779	3.927	1.849	3.796	1.919	3.674
1.200	4.542	1.220	4·371	1.640	4.513	1.210	4.064	1.780	3.925	1.850	3.794	1.920	3.672
1.201	4.239	1.221	4.369	1.641	4.311	1.711	4.062	1.781	3.923	1.851	3.793	1.921	3.670
1.502	4.537	1.572	4.307	1.042	4.200	1.712	4.058	1.782	3.921	1.852	3.791	1.922	3.669
1.504	4 534	1.573	4 304	1.643	4 200	1.714	4.056	1.784	3.017	1.854	3.789	1.024	3.007
1.202	4.529	1.575	4.360	1.645	4.202	1.715	4.054	1.785	3.915	1.855	3.786	1.925	3.664
1.506	4.527	1.576	4.357	1.646	4.200	1.716	4.052	1.786	3.914	1.856	3.784	1.926	3.662
1.202	4.254	1.577	4.355	1.647	4.192	1.717	4.020	1.787	3.912	1.857	3.782	1.927	3.660
1.508	4.522	1.578	4.353	1.648	4.195	1.718	4.048	1.788	3.910	1.858	3.780	1.928	3.659
1.509	4.519	1.579	4.350	1.049	4.193	1.719	4.040	1.789	3.908	1.860	3.778	1.929	3.657
1.511	4 31/	1.581	4 340	1.651	4.180	1.721	4 044	1.701	3.004	1.861	3.775	1.031	3.055
1.512	4.512	1.582	4.343	1.652	4.186	1.722	4.040	1.792	3.902	1.862	3.773	1.932	3.652
1.213	4.509	1.583	4·341	1.653	4.184	1.723	4.038	1.793	3.900	1.863	3.771	1.933	3.650
1.214	4 . 502	1.584	4.339	1.654	4.182	1.724	4 · 036	1.794	3.898	1.864	3.769	1.934	3.649
1.515	4.204	1.585	4.336	1.655	4.180	1.725	4.034	1.795	3.896	1.865	3.768	1.932	3.647
1.510	4.502	1.580	4.334	1.650	4.178	1.720	4.031	1.796	3.894	1.860	3.760	1.936	3.645
1.518	4.499	1.588	4.334	1.658	4.170	1.728	4.029	1.708	3.801	1.807	3.704	1.037	3.044
1.519	4.494	1.589	4.327	1.659	4.171	1.729	4.025	1.799	3.888	1.869	3.761	1.030	3.640
1.520	4.492	1.590	4.325	1.660	4.169	1.730	4.023	1.800	3.887	1.870	3.759	1.940	3.639
1.251	4.489	1.201	4.323	1.661	4.167	1.731	4.021	1.801	3.885	1.871	3.757	1.941	3.637
1.252	4.487	1.292	4.320	1.662	4.165	1.732	4.019	1.802	3.883	1.872	3.755	1.942	3.635
1.523	4.484	1.593	4.318	1.003	4.103	1.733	4.017	1.803	3.881	1.873	3.753	1.943	3.634
1.524	4.402	1.594	4.310	1.665	4.101	1.734	4.013	1.805	3.879	1.875	3.754	1.944	3.032
1.526	4.477	1.596	4.311	1.666	4.156	1.736	4.011	1.806	3.876	1.876	3.748	1.945	3.620
1.527	4.475	1.597	4.309	1.667	4.154	1.737	4.009	1.807	3.874	1.877	3.746	1.947	3.627
1.528	4.472	1.598	4.302	1.668	4.122	1.738	4.007	1.808	3.872	1.878	3.745	1.948	3.625
1.529	4.470	1.599	4.304	1.669	4.150	1.739	4.005	1.809	3.870	1.879	3.743	1.949	3.624
1.530	4.407	1.000	4.302	1.670	4.140	1.740	4.003	1.810	3.808	1.880	3.741	1.950	3.622
1.531	4.405	1.602	4.300	1.672	4.140	1.741	3.000	1.812	3.864	1.882	3.739	1.951	3.020
1.533	4.460	1.603	4-295	1.673	4·14I	1.743	3.997	1.813	3.863	1.883	3.736	1.953	3.617
1.534	4.457	1.604	4.293	1.674	4.139	1.744	3.995	1.814	3.861	1.884	3.734	1.954	3.615
1.535	4.455	1.605	4.291	1.675	4.137	1.745	3.993	1.815	3.859	1.885	3.732	1.955	3.614
1.536	4.423	1.606	4.288	1.676	4.135	1.746	3.991	1.816	3.857	1.886	3.731	1.956	3.612
1.537	4.450	1.007	4.286	1.077	4.133	1.747	3.989	1.817	3.855	1.887	3.729	1.957	3.610
1.230	4.440	1.600	4.2.82	1.670	4.131	1.740	3.900	1.810	3.851	1.880	3.725	1.950	3.607
1.540	4.443	1.610	4.279	1.680	4.127	1.750	3.984	1.820	3.849	1.890	3.724	1.920	3.606
1.541	4.441	1.611	4.277	1.681	4.124	1.751	3.982	1.821	3.848	1.891	3.722	1.961	3.604
1.242	4.438	1.612	4.275	1.682	4.122	1.752	3.980	1.822	3.846	1.892	3.720	1.962	3.602
1.243	4.436	1.613	4.273	1.683	4.120	1.753	3.978	1.823	3.844	1.893	3.718	1.963	3.601
1.544	4.433	1.614	4.270	1.084	4.118	1.754	3.976	1.824	3.842	1.894	3.717	1.964	3.599
1.545	4.431	1.015	4.200	1.005	4.110	1.755	3.974	1.825	3.828	1.806	3.715	1.905	3.297
1.547	4 4 - 9 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 -	1.617	4.261	1.687	4.112	1.757	3.972	1.827	3.836	1.897	3.712	1.967	3.594
1.548	4.424	1.618	4.261	1.688	4.110	1.759	3.968	1.828	3.835	1.898	3.710	1.968	3.593
1.549	4 421	1.619	4.259	1.689	4.108	1.759	3.966	1.829	3.833	1.899	3.708	1.969	3.201
1.520	4.419	1.620	4.257	1.690	4.102	1.760	3.964	1.830	3.831	1.900	3.706	1.970	3.589
1.551	4.417	1.621	4.255	1.691	4.103	1.761	3.962	1.831	3.829	1.001	3.705	1.971	3.288
1.552	4.414	1.622	4.252	1.602	4.000	1.762	3.900	1.822	3.825	1.902	3.703	1.972	3.200
- 555 1.554	4.400	1.624	4.248	1.694	4.097	1.764	3.956	1.834	3.824	1.001	3.699	1.974	3.583
1.555	4.407	1.625	4.246	1.695	4.095	1.765	3.954	1.835	3.822	1.905	3.698	1.975	3.581
1.556	4.405	1.626	4.244	1.696	4.093	1.766	3.952	1.836	3.820	1.906	3.696	- 1.976	3.580
1.557	4.402	1.627	4.241	1.697	4.091	1.767	3.950	1.837	3.818	1.907	3.694	1.977	3.578
1.558	4.400	1.628	4.239	1.098	4.089	1.768	3.948	1.838	3.816	1.000	3.693	1.978	3.570
- 339	4 390	11 021	4 4 37	1 099	400/	1 /09	5.940	1 0,19	5 014	- 909	5 091	. 9/9	5 515

A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion	A and B Cor.	Reduc- tion.								
			2. 162	2,120	2,260	2.100	2,262	12:260	2.1.70	1			
1.980	3.573	2.050	3.403	2.120	3.300	2.190	3.203	2.200	3.170	2.330	3.082	2.400	3.001
1.982	3.570	2.052	3.460	2.122	3.357	2.192	3.260	2.262	3.168	2.332	3.081	2.402	2.999
1.983	3.568	2.053	3.459	2.123	3.356	2.193	3.259	2.263	3.167	2.333	3.080	2.403	2.997
1.985	3.507	2.054	3.457	2.124	3.322	2.194	3.256	2.264	3.105	2.334	3.079	2.404	2.990
1.986	3.563	2.056	3.454	2.126	3.352	2.196	3.255	2.266	3.163	2.336	3.076	2.406	2.994
1.987	3.562	2.057	3.453	2.127	3.350	2.197	3.253	2.267	3.162	2.337	3.075	2.407	2.993
1.080	3.500	2.058	3.451	2.128	3.349	2.198	3.252	2.200	3.100	2.338	3.074	2.408	2.992
1.999	3.557	2.060	3.448	2.130	3.346	2.200	3.249	2.270	3.158	2.340	3.071	2.409	2.989
1.991	3.555	2.061	3.447	2.131	3.345	2.201	3.248	2.271	3.156	2.341	3.070	2.411	2.988
1.003	3.554	2.062	3.445	2.132	3.343	2.202	3.240	2.272	3.155	2.342	3.069	2.412	2.987
1.993	3·551	2.064	3.444	2.133	3.340	2.204	3.244	2.274	3.153	2.343	3.067	2.413	2.985
1.995	3.549	2.065	3.441	2.135	3.339	2.205	3.242	2.275	3.121	2.345	3.065	2.415	2.984
1.996	3.547	2.060	3.439	2.136	3.337	2.200	3.241	2.276	3.150	2.340	3.064	2.410	2.982
1.997	3.540	2.007	3.430	2.13/	3.335	2.208	3.238	2.278	3.149	2.347	3.003	2.417	2.980
1.999	3.543	2.069	3.435	2.139	3.333	2.209	3.237	2.279	3.146	2.349	3.061	2.419	2.979
2.000	3.241	2.070	3.433	2.140	3.332	2.210	3.236	2.280	3.145	2.350	3.059	2.420	2.978
2.001	3.539	2.071	3.432	2.141	3.330	2.211	3.234	2.281	3.144	2.351	3.050	2.421	2.977
2.003	3.536	2.073	3.429	2.143	3.328	2.213	3.232	2.283	3.141	2.353	3.056	2.423	2.975
2.004	3.535	2.074	3.427	2.144	3.326	2.214	3.230	2.284	3.140	2.354	3.055	2.424	2.973
2.005	3.533	2.075	3.420	2.145	3.325	2.215	3.229	2.205	3.139	2.355	3.053	2.425	2.972
2.007	3.530	2.077	3.423	2.140	3.322	2.217	3.226	2.287	3.136	2.357	3.051	2.427	2.970
2.008	3.528	2.078	3.421	2.148	3.321	2.218	3.225	2.288	3.135	2.358	3.050	2.428	2.969
2.009	3.527	2.079	3.420	2.149	3.319	2.219	3.224	2.289	3.134	2.359	3.049	2.429	2.968
2.010	3.524	2.081	3.417	2.130	3.316	2.220	3.221	2.298	3.131	2.361	3.046	2.430	2.965
2.012	3.522	2.082	3.416	2.152	3.315	2.222	3.220	2.292	3.130	2.362	3.045	2.432	2.964
2.013	3.521	2.083	3.414	2.153	3.314	2.223	3.218	2.293	3.129	2.363	3.044	2.433	2.963
2.014	3.519	2.084	3.413	2.154	3.312	2.224	3.217	2.294	3.120	2.304	3.043	2.435	2.961
2.016	3.516	2.086	3.410	2.156	3.309	2.226	3.215	2.296	3.125	2.366	3.040	2.436	2.960
2.017	3.514	2.087	3.408	2.157	3.308	2.227	3.213	2.297	3.124	2.367	3.039	2.437	2.959
2.010	3.213	2.089	3.407	2.150	3.307	2.220	3.212	2.290	3.123	2.300	3.030	2.430	2.950
2.020	3.210	2.090	3.404	2.160	3.304	2.230	3.209	2.300	3.120	2.370	3.036	2.440	2.955
2.021	3.208	2.091	3.402	2.161	3.302	2.231	3.208	2.301	3.119	2.371	3.035	2.441	2.954
2.022	3.500	2.092	3.300	2.102	3.301	2.232	3.207	2.302	3.110	2.372	3.033	2.442	2.953
2.024	3.203	2.094	3.398	2.164	3.298	2.234	3.204	2.304	3.115	2.374	3.031	2.444	2.951
2.025	3.202	2.095	3.396	2.165	3.297	2.235	3.203	2.305	3.114	2.375	3.030	2.445	2.950
2.020	3.200	2.090	3.395	2.100	3.290	2.230	3.201	2.300	3.113	2.370	3.029	2.440	2.949
2.028	3.497	2.098	3.392	2.168	3.293	2.238	3.199	2.308	3.110	2.378	3.026	2.448	2.947
2.029	3.496	2.099	3.301	2.169	3.291	2.239	3.197	2.309	3.109	2.379	3.025	2.449	2.945
2.030	3.494	2.100	3.389	2.170	3.290	2.240	3.102	2.310	3.109	2.380	3.024	2.420	2.944
2.032	3.491	2.102	3.386	2.172	3.287	2.242	3.194	2.312	3.105	2.382	3.022	2.452	2.942
2.033	3.490	2.103	3.385	2.173	3.286	2.243	3.192	2.313	3.104	2.383	3.021	2.453	2.941
2.034	3.488	2.104	3.383	2.174	3.284	2.244	3.101	2.314	3.103	2.384	3.019	2.454	2.940
2.035	3.485	2.105	3.380	2.175	3.282	2.246	3.188	2.316	3.101	2.386	3.017	2.456	2.938
2.037	3.483	2.107	3.379	2.177	3.280	2.247	3.187	2.317	3.099	2.387	3.016	2.457	2.937
2.038	3.482	2.108	3.378	2.178	3.279	2.248	3.186	2.318	3.098	2.388	3.012	2.450	2.935
2.039	3.479	2.110	3.375	2.179	3.276	2.249	3.183	2.319	3.096	2.390	3.012	2.460	2.933
2.041	3.477	2.111	3.373	2.181	3.275	2.251	3.182	2.321	3.094	2.391	3.011	2.461	2.932
2.042	3.476	2.112	3.372	2.182	3.274	2.252	3.181	2.322	3.093	2.392	3.010	2.462	2.031
2.043	3.474	2.113	3.370	2.103	3.272	2.253	3.178	2.323	3.091	≁ 393 2•394	3.008	2.464	2.929
2.045	3.471	2.115	3.367	2.185	3.269	2.255	3.177	2.325	3.090	2.395	3.007	2.465	2.928
2.046	3.470	2.116	3.366	2.186	3.268	2.256	3.176	2.326	3.088	2.396	3.005	2.466	2.927
2.047	3.400	2.117	3.305	2.187	3.207	2.257	3.174	2.327	3.087	2.397	3.004	2.467	2.924
2.049	3.465	2.119	3.362	2.189	3.264	2.259	3.172	2.329	3.085	2.399	3.002	2.469	2.923

A and B Cor.	Reduc- tion.												
		10/210	218.17	2.660	2.727	2.800	2.508	2:040	2.182	2:080	2.274	2:220	21276
2.470	2.922	2.540	2.047	2.662	2.725	2.802	2.593	2.940	2.480	3.082	2·373	3.220	2.270
2.472	2.920	2.542	2.845	2.664	2.723	2.804	2.595	2.944	2.478	3.084	2.371	3.224	2.273
2.473	2.919	2.543	2.844	2.666	2.721	2.806	2.593	2.946	2.477	3.086	2.370	3.226	2.272
2.474	2.918	2.544	2.843	2.008	2.719	2.810	2.592	2.940	2.475	3.000	2.308	3.228	2.270
2.475	2.91/	2.545	2.841	2.672	2.715	2.812	2.588	2.952	2.472	3.092	2.366	3.232	2.269
2.477	2.914	2.547	2.840	2.674	2.714	2.814	2.586	2.954	2.470	3.094	2.364	3.234	2.266
2.478	2.913	2.548	2.839	2.676	2.712	2.816	2.585	2.956	2.469	3.096	2.363	3.236	2.265
2.479	2.011	2.549	2.030	2.680	2.708	2.820	2.581	2.950	2·407	3.100	2.301	3.230	2.204
2.481	2.910	2.551	2.836	2.682	2.706	2.822	2.579	2.962	2.464	3.102	2.358	3.242	2.261
2.482	2.909	2.552	2.835	2.684	2.704	2.824	2.578	2.964	2.463	3.104	2.357	3.244	2.260
2.483	2.908	2.553	2.834	2.080	2.702	2.828	2.570	2.900	2.401	3.100	2.355	3.240	2.258
2.485	2.906	2.555	2.832	2.690	2.698	2.830	2.573	2.970	2.458	3.110	2.352	3.250	2.256
2.486	2.905	2.556	2.831	2.692	2.696	2.832	2.571	2.972	2.456	3.115	2.351	3.252	2.254
2.487	2.904	2.557	2.830	2.694	2.694	2.834	2.569	2.974	2.455	3.114	2.350	3.254	2.253
2.480	2.003	2.550	2.829	2.698	2.693	2.838	2.566	2.978	433 2·452	3.118	2.340	3.250	2.252
2.490	2.900	2.560	2.826	2.700	2.689	2.840	2.564	2.980	2.450	3.120	2.345	3.260	2.249
2.491	2.899	2.562	2.824	2.702	2.687	2.842	2.562	2.982	2.448	3.122	2.344	3.262	2.248
2.492	2.898	2.564	2.822	2.704	2.682	2.844	2.501	2.984	2.447	3.124	2.342	3.204	2.246
2.493	2.897	2.568	2.818	2.708	2.681	2.848	2·557	2.988	~ 44J 2·444	3.128	2.339	3.268	2.245
2.495	2.895	2.570	2.816	2.710	2.680	2.850	2.536	2.990	2.442	3.130	2.338	3.270	2.242
2.496	2.894	2.572	2.814	2.712	2.678	2.852	2.554	2.992	2.441	3.132	2.337	3.272	2.241
2.497	2.893	2.574	2.810	2.714	2.070	2.054	2·552 2·551	2.994	2.439	3.134	2.335	3.274	2.240
2.499	2.891	2.578	2.808	2.718	2.672	2.858	2.549	2.998	2.436	3.138	2.332	3.278	2.237
2.500	2.890	2.580	2.806	2.720	2.670	2.860	2.547	3.000	2.435	3.140	2.331	3.280	2.236
2.501	2.889	2.582	2.804	2.722	2.667	2.862	2.546	3.002	2.433	3.142	2.330	3.282	2.234
2.502	2.886	2.586	2.802	2.726	2.665	2.866	- 544 2.542	3.004	2.430	3.144	2.320	3.286	2.233
2.504	2.885	2.588	2.797	2.728	2.663	2.868	2.540	3.008	2.428	3.148	2.325	3.288	2.231
2.505	2.884	2.590	2.796	2.730	2.661	2.870	2.539	3.010	2.427	3.120	2.324	3.290	2.229
2.506	2.883	2.592	2.794	2.732	2.059	2.872	2.537	3.012	2.425	3.152	2.322	3.292	2.228
2.508	2.881	2.596	2.792	2.736	2.656	2.876	~ 555 2·534	3.016	2.422	3.156	2.320	3.296	2.225
2.509	2.880	2.598	2.788	2.738	2.654	2.878	2.532	3.018	2.421	3.158	2.318	3.298	2.224
2.510	2.879	2.600	2.786	2.740	2.652	2.880	2.530	3.020	2.419	3.160	2.317	3.300	2.223
2.511	2.877	2.602	2.704	2.742	2.648	2.884	2.529	3.022	2.410	3.102	2.315	3.302	2.221
2.513	2.876	2.606	2.780	2.746	2.646	2.886	2.525	3.026	2.415	3.166	2.313	3.306	2.219
2.514	2.875	2.608	2.778	2.748	2.645	2.888	2.524	3.028	2.413	3.168	2.311	3.308	2.218
2.515	2.874	2.010	2.776	2.750	2.043	2.802	2.522	3.030	2.412	3.170	2.310	3.310	2.216
2.517	2.871	2.614	2.772	2.754	2.639	2.894	2.519	3.034	2.409	3.174	2.307	3.314	2.213
2.518	2.870	2.616	2.770	2.756	2.637	2.896	2.517	3.036	2.407	3.176	2.306	3.316	2.212
2.519	2.869	2.618	2.768	2.758	2.636	2.898	2.516	3.038	2.406	3.178	2.304	3.318	2.211
2.520	2.867	2.622	2.764	2.762	2.632	2.900	2.512	3.040	2.404	3.182	2.303	3.320	2.210
2.522	2.866	2.624	2.762	2.764	2.630	2.904	2.511	3.044	2.401	3.184	2.300	3.324	2.207
2.523	2.865	2.626	2.760	2.766	2.628	2.906	2.509	3.046	2.400	3.186	2.299	3.326	2.206
2.524	2.864	2.620	2.758	2.768	2.625	2.908	2.507	3.048	2.398	3.188	2.297	3.328	2.205
2.526	2.862	2.632	2.754	2.772	2.623	2.912	2.504	3.052	2.395	3.190	2.295	3.332	2.202
2.527	2.861	2.634	2.752	2.774	2.621	2.914	2.503	3.054	2.394	3.194	2.293	3.334	2.201
2.528	2.860	2.636	2.750	2.776	2.620	2.916	2.501	3.056	2.392	3.196	2.292	3.336	2.200
2.529	2.858	3 2.640	2.740	2.780	2.010	2.918	2.499	3.050	2.391	3.200	2.291	3.330	2.199
2.531	2.857	7 2.642	2.744	2.782	2.614	2.922	2.496	3.062	2.388	3.202	2.288	3.342	2.196
2.532	2.856	2.644	2.742	2.784	2.613	2.924	2.494	3.064	2.386	3.204	2.286	3.344	2.195
2.533	2.855	5 2.646	2.740	2.786	2.600	2.926	2.493	3.066	2.385	3.206	2.285	3.346	.2.193
2.535	2.85	2.650	2.737	2.790	2.607	2.930	2.490	3.070	2.382	3.210	2.282	3.350	2.192
2.536	2.852	2.652	2.735	2.792	2.605	2.932	2.488	3.072	2.380	3.212	2.281	3.352	2.190
2.537	2.850	2.654	2.733	2.794	2.604	2.934	2.486	3.074	2.379	3.214	2.280	3.354	2.188
2.530	2.848	3 2.658	2.731	2.790	2.002	2.030	2.405	3.070	2.377	3.210	2.270	3.350	2.187
- 5.59			- /-9	- 190	2 000	- 9,0	- 40,)	0-10		, _ 10		3 3 3 5 5	

$ \begin{array}{c} 3'_{3}60 & 2'_{1}63 & 3'_{5}00 & 2'_{1}01 & 3'_{6}64 & 2'_{0}22 & 3'_{7}80 & 1'_{9}02 & 1'_{8}83 & 4'_{6}06 & 1'_{2}02 & 4'_{2}00 & 1'_{7}0 \\ 3'_{3}3'_{6}2 & 2'_{1}83 & 3'_{5}02 & 2'_{1}00 & 3'_{6}42 & 2'_{0}22 & 3'_{7}81 & 1'_{9}0 & 3'_{9}24 & 1'_{8}81 & 4'_{6}01 & 1'_{8}18 & 4'_{2}04 & 1'_{7}5 \\ 3'_{3}3'_{6}6 & 2'_{1}80 & 3'_{5}08 & 2'_{9}03 & 3'_{6}64 & 2'_{9}02 & 3'_{7}80 & 1'_{9}44 & 3'_{9}24 & 1'_{8}81 & 4'_{6}01 & 1'_{8}18 & 4'_{2}04 & 1'_{7}5 \\ 3'_{3}3'_{7}2 & 2'_{1}70 & 3'_{5}12 & 2'_{9}03 & 3'_{6}65 & 2'_{9}01 & 3'_{7}92 & 1'_{9}44 & 3'_{9}31 & 1'_{8}7 & 4'_{7}4 & 1'_{7}4 & 1'_{1}4 & 1'_{1}17 & 1'_{1}73 \\ 3'_{3}72 & 2'_{1}77 & 3'_{1}512 & 2'_{9}03 & 3'_{6}65 & 2'_{9}01 & 3'_{7}92 & 1'_{9}44 & 3'_{9}31 & 1'_{8}7 & 4'_{7}4 & 1'_{8}1 & 4'_{2}12 & 1'_{7}3 \\ 3'_{3}74 & 2'_{1}75 & 3'_{1}512 & 2'_{9}03 & 3'_{6}65 & 2'_{9}01 & 3'_{7}91 & 1'_{9}44 & 3'_{9}31 & 1'_{8}7 & 4'_{7}4 & 1'_{8}1 & 4'_{2}12 & 1'_{7}3 \\ 3'_{3}76 & 2'_{1}75 & 3'_{1}512 & 2'_{9}08 & 1'_{6}66 & 2'_{1}21 & 3'_{7}78 & 1'_{9}49 & 1'_{8}7 & 4'_{9}74 & 1'_{8}1 & 4'_{2}22 & 1'_{7}3 \\ 3'_{3}76 & 2'_{1}75 & 1'_{5}22 & 2'_{9}08 & 1'_{6}66 & 2'_{0}21 & 3'_{8}04 & 1'_{9}01 & 1'_{9}1 & 4'_{9}21 & 1''_{1}4'_{2}2 & 1''_{7}3 \\ 3'_{3}76 & 2'_{1}76 & 1'_{5}32 & 2'_{9}08 & 1'_{6}66 & 2'_{0}21 & 3'_{8}04 & 1'_{9}01 & 1''_{9}1 & 4''_{9}1 & 1''_{8}2 & 1''_{9}1 \\ 3'_{3}76 & 2'_{1}76 & 1'_{5}32 & 2'_{9}08 & 1''_{6}66 & 2''_{0}21 & 3''_{8}04 & 1''_{9}1 & 1''_{9}1 & 1''_{9}1 & 1''_{9}1 \\ 3'_{3}76 & 2'_{1}76 & 1''_{1}73 & 1''_{1}73 & 1''_{1}18 & 1''_{1}18 & 1''_{1}18 & 1''_{1}18 & 1''_{1}18 & 1''_{1}18 & 1''_{1}18 & 1''_{1}18 & 1''_{1}11 \\ 3'_{3}76 & 2''_{1}76 & 1''_{1}73 & 1''_{1}18 & 1''_{1}18 & 1''_{1}18 & 1''_{1}18 & 1''_{1}18 & 1''_{1}18 & 1''_{1}11 & 1''_{1}18 & 1''_{1}11 \\ 3''_{3}76 & 2''_{1}76 & 1''_{1}73 & 3''_{1}18 & 1''_{1}18 & 1''_{1}18 & 1''_{1}11 & 1''_{1}11 \\ 3''_{3}76 & 1''_{1}76 & 1''_{1}73 & 1''_{1}18 & 1''_{1}18 & 1''_{1}18 & 1''_{1}11 & 1''_{1}11 & 1''_{1}11 & 1''_{1}11 \\ 3''_{3}76 & 1''_{1}16 & 1''_{1}73 & 1''_{1}18 & 1''_{1}18 & 1''_{1$	A and B Cor.	Reduc- tion.												
1362 2183 1594 2003 1544 2021 1784 1994 3024 1784 1994 3024 1784 1994 3024 1784 1994 3024 1784 1994 3024 1784 1994 1924 1784 1947 1924 1785 1947 1924 1737 1946 1737 1934 1737 1934 1737 1934 1737 1934 1737 1934 1737 1934 1737 1934 1737 1934 1737 1934 1737 1934 1934 1875 4976 1814 1212 1213 1213 1213 1214 1735 3134 1737 1935 1217 1222 1735 3134 1217 1222 1735 3134 1217 1222 1735 3134 1217 1222 1735 3134 1217 1222 1735 3134 1217 1222 1735 1233 1224 1233 1234 <td< td=""><td>3.360</td><td>2.185</td><td>3.500</td><td>2.101</td><td>3.640</td><td>2.023</td><td>3.780</td><td>1.051</td><td>3.020</td><td>1.883</td><td>1.060</td><td>1.820</td><td>4.200</td><td>1.761</td></td<>	3.360	2.185	3.500	2.101	3.640	2.023	3.780	1.051	3.020	1.883	1.060	1.820	4.200	1.761
	3.362	2.183	3.502	2.100	3.642	2.022	3.782	1.950	3.922	1.882	4.062	1.819	4.202	1.760
$ \begin{array}{c} 3:36 & 2:18 & 3:50 & 2:09 \\ 3:76 & 2:18 & 3:50 & 2:09 \\ 3:76 & 2:16 & 3:50 & 2:06 \\ 3:75 & 2:17 & 3:71 & 2:05 \\ 3:72 & 2:17 & 3:71 & 2:05 \\ 3:76 & 2:17 & 3:71 & 2:09 \\ 3:76 & 2:17 & 3:71 & 2:09 \\ 3:76 & 2:17 & 3:71 & 2:09 \\ 3:76 & 2:17 & 3:71 & 2:09 \\ 3:76 & 2:17 & 3:71 & 2:09 \\ 3:76 & 2:17 & 3:71 & 2:09 \\ 3:76 & 2:17 & 3:71 & 2:09 \\ 3:76 & 2:17 & 3:71 & 2:09 \\ 3:76 & 2:17 & 3:71 & 2:09 \\ 3:76 & 2:17 & 3:72 & 2:17 \\ 3:76 & 2:17 & 3:72 & 2:08 \\ 3:76 & 2:17 & 3:72 & 2:08 \\ 3:76 & 2:17 & 3:72 & 2:08 \\ 3:76 & 2:17 & 3:72 & 2:08 \\ 3:76 & 2:17 & 3:72 & 2:08 \\ 3:76 & 2:17 & 3:72 & 2:08 \\ 3:76 & 2:17 & 3:72 & 2:08 \\ 3:76 & 2:17 & 3:72 & 2:08 \\ 3:76 & 2:17 & 3:72 & 2:08 \\ 3:76 & 2:17 & 3:72 & 2:08 \\ 3:76 & 2:17 & 3:72 & 2:08 \\ 3:76 & 2:10 & 3:20 & 2:66 \\ 3:76 & 2:00 & 3:80 & 1:03 \\ 3:79 & 2:16 & 3:32 & 2:68 \\ 3:66 & 2:00 & 3:80 & 1:03 \\ 3:90 & 2:16 & 3:32 & 2:68 \\ 3:66 & 2:00 & 3:80 & 1:03 \\ 3:90 & 2:16 & 3:33 & 2:68 \\ 3:66 & 2:00 & 3:80 & 1:03 \\ 3:90 & 2:16 & 3:33 & 2:68 \\ 3:67 & 2:00 & 3:81 & 1:03 \\ 3:90 & 2:16 & 3:33 & 2:68 \\ 3:67 & 2:00 & 3:81 & 1:03 \\ 3:90 & 2:16 & 3:33 & 2:68 \\ 3:73 & 3:70 & 3:76 & 4:80 & 4:00 & 1:80 & 1:23 \\ 3:90 & 2:16 & 3:33 & 2:68 & 1:00 \\ 3:73 & 2:16 & 3:33 & 2:68 & 1:00 \\ 3:74 & 2:16 & 3:33 & 2:68 & 1:00 \\ 3:74 & 2:16 & 1:73 & 1:80 & 1:75 \\ 3:30 & 2:16 & 3:33 & 2:67 & 3:67 & 2:00 \\ 3:74 & 2:16 & 1:41 & 1:80 & 1:22 & 1:73 \\ 3:30 & 2:16 & 3:33 & 2:67 & 3:66 & 1:00 & 3:81 & 1:93 \\ 3:90 & 1:60 & 4:00 & 1:60 & 1:80 & 1:75 \\ 3:30 & 2:16 & 3:33 & 2:67 & 3:66 & 1:00 & 1:38 & 1:33 \\ 3:90 & 1:60 & 4:00 & 1:60 & 1:75 & 1:73 \\ 3:30 & 2:16 & 3:34 & 2:77 & 3:68 & 2:00 & 3:81 & 1:93 & 1:367 & 4:06 & 1:60 & 1:60 & 1:60 & 1:75 \\ 3:30 & 2:16 & 3:34 & 2:77 & 3:68 & 2:00 & 3:84 & 1:73 & 3:95 & 1:86 & 4:00 & 1:60 & 1:60 & 1:80 & 1:75 \\ 3:40 & 2:14 & 2:14 & 2:17 & 3:68 & 1:60 & 1:81 & 1:70 & 1:81 & 1:71 \\ 3:40 & 2:14 & 2:14 & 2:17 & 3:68 & 1:60 & 1:81 & 1:70 & 1:81 & 1:71 \\ 3:40 & 2:14 & 3:40 & 1:75 & 3:68 & 1:90 & 3:84 & 1:90 & 1:86 & 1:60 & 1:16 & 1:70 & 1:81 & 1:74 \\ 3:41 & 2:15 & 3:34 & 2:07 & 3:68 & $	3.364	2.182	3.204	2.098	3.644	2.021	3.784	1.949	3.924	1.881	4.064	1.818	4.204	1.759
$ \begin{array}{c} 3_{33} 6 2_{16} 2_{17} 3_{37} 2_{17} 3_{17} 3_{17} 2_{17} 3_{17} 3_{17} 2_{17} 3_{17} 3_{17} 2_{17} 3_{17} 3_{17} 2_{17} 3_{17} 3_{17} 2_{17} 3_{17} 3_{17} 2_{17} 3_{17} 3_{17} 3_{17} 2_{17} 3_{17} 3_{17} 2_{17} 3_{17} 3_{17} 2_{17} 3_{17}$	3.366	2.181	3.206	2.097	3.646	2.020	3.786	1.948	3.926	1.880	4.066	1.818	4.206	1.759
$ \begin{array}{c} 3737 & 2178 & 3731 & 2998 & 3692 & 2018 & 3799 & 1946 & 3930 & 1878 & 4070 & 1810 & 4212 & 173 \\ 3737 & 2176 & 3734 & 2993 & 3656 & 2016 & 3796 & 1944 & 3934 & 1877 & 4074 & 1884 & 4214 & 173 \\ 3736 & 2173 & 3218 & 2990 & 3656 & 2013 & 3800 & 1941 & 3930 & 1875 & 4078 & 1821 & 4228 & 173 \\ 338 & 2173 & 3222 & 2888 & 3666 & 2013 & 3800 & 1941 & 3940 & 1875 & 4078 & 1812 & 4228 & 173 \\ 338 & 2177 & 3222 & 2888 & 3666 & 2003 & 3804 & 1940 & 3944 & 1877 & 4078 & 1814 & 4228 & 173 \\ 338 & 2177 & 3222 & 2888 & 3666 & 2008 & 3868 & 1937 & 3944 & 1875 & 4088 & 1808 & 4224 & 173 \\ 338 & 2167 & 3326 & 2083 & 3666 & 2008 & 3868 & 1937 & 3944 & 1875 & 4088 & 1808 & 4224 & 173 \\ 3390 & 2166 & 3330 & 2416 & 3666 & 2008 & 3868 & 1937 & 3948 & 1887 & 4088 & 1808 & 4224 & 173 \\ 3190 & 2160 & 3332 & 2083 & 3672 & 2006 & 3811 & 1935 & 3936 & 1867 & 4094 & 1869 & 4228 & 1733 \\ 3190 & 2160 & 3332 & 2083 & 3672 & 2006 & 3818 & 1933 & 3964 & 1867 & 4094 & 1869 & 4234 & 174 \\ 3194 & 2163 & 3344 & 2077 & 3682 & 2003 & 3818 & 1933 & 3966 & 1867 & 4096 & 1869 & 4238 & 174 \\ 3196 & 2160 & 3342 & 2078 & 3686 & 2002 & 3816 & 1933 & 3966 & 1867 & 4096 & 1869 & 4238 & 174 \\ 3196 & 2160 & 3342 & 2078 & 3686 & 2002 & 3828 & 1033 & 3966 & 1867 & 4096 & 1863 & 4744 & 174 \\ 3196 & 2160 & 3348 & 2077 & 3682 & 2003 & 3818 & 1033 & 3966 & 1866 & 4908 & 1804 & 1808 & 4248 & 174 \\ 3190 & 2156 & 3346 & 207 & 3686 & 1908 & 3828 & 1027 & 3966 & 1861 & 4108 & 1802 & 424 & 174 \\ 3192 & 2153 & 3352 & 2071 & 3608 & 1908 & 383 & 1027 & 3968 & 1861 & 4108 & 1802 & 4124 & 174 \\ 3192 & 2153 & 3356 & 2069 & 3060 & 1994 & 3831 & 1023 & 3961 & 1857 & 4116 & 1769 & 4258 & 1733 \\ 3140 & 2158 & 3356 & 2063 & 3706 & 1938 & 3836 & 1024 & 3974 & 1858 & 4112 & 1768 & 4226 & 1733 \\ 3142 & 2148 & 3150 & 2068 & 3608 & 1993 & 3838 & 1027 & 3988 & 1854 & 4128 & 1794 & 4268 & 1733 \\ 3142 & 2153 & 3356 & 2063 & 3706 & 1938 & 3856 & 1013 & 3996 & 1857 & 4116 & 1768 & 4268 & 1733 \\ 3142 & 2148 & 3750 & 2058 & 3761 & 1938 & 3856 & 1013 & 3996 & 1858 & 4138 & 1768 & 4728 & 17$	3.368	2.180	3.208	2.096	3.648	2.019	3.788	1.947	3.928	1.879	4.068	1.817	4.208	1.758
$\begin{array}{c} 3374 & 2776 & 3341 & 2938 & 3054 & 2047 & 3794 & 1948 & 3034 & 1977 & 4774 & 1841 & 4214 & 1757 \\ 3376 & 2173 & 3318 & 2998 & 3054 & 2041 & 3706 & 1943 & 3036 & 1876 & 4776 & 1781 & 4216 & 1757 \\ 338 & 2177 & 3722 & 2088 & 3660 & 2041 & 3786 & 1948 & 3036 & 1876 & 4776 & 1781 & 4221 & 1757 \\ 338 & 2177 & 3722 & 2088 & 3660 & 2041 & 3786 & 1946 & 3042 & 1876 & 4778 & 1781 & 4222 & 1757 \\ 338 & 2177 & 3722 & 2088 & 3666 & 2040 & 3860 & 1938 & 3046 & 1857 & 4066 & 1800 & 4224 & 1737 \\ 338 & 2177 & 3722 & 2085 & 3666 & 2040 & 3866 & 1338 & 3046 & 1857 & 4066 & 1800 & 4224 & 1737 \\ 338 & 2167 & 3222 & 2085 & 3668 & 2040 & 3866 & 1336 & 3046 & 1857 & 4066 & 1800 & 4224 & 1737 \\ 339 & 2165 & 3332 & 2085 & 3668 & 2040 & 3816 & 1336 & 3046 & 1857 & 4066 & 1806 & 4228 & 1737 \\ 339 & 2165 & 3332 & 2083 & 3672 & 2040 & 3816 & 1336 & 3357 & 1866 & 4000 & 1.867 & 4238 & 1747 \\ 339 & 2165 & 3332 & 2083 & 3672 & 2040 & 3816 & 1332 & 3568 & 4000 & 1.867 & 4238 & 1747 \\ 339 & 2165 & 3334 & 2058 & 3668 & 2040 & 3818 & 1332 & 3558 & 1866 & 4001 & 1806 & 4238 & 1747 \\ 339 & 2165 & 3342 & 2073 & 3668 & 2040 & 3822 & 1331 & 3357 & 1886 & 4001 & 1805 & 4238 & 1747 \\ 339 & 2165 & 3342 & 2073 & 3668 & 2040 & 3822 & 1331 & 3357 & 1886 & 4001 & 1805 & 4248 & 174 \\ 349 & 2256 & 3344 & 2077 & 3684 & 2040 & 3824 & 1948 & 3036 & 1864 & 4061 & 1800 & 4248 & 174 \\ 3440 & 2255 & 3344 & 2077 & 3684 & 1908 & 3826 & 1928 & 1928 & 1966 & 1864 & 1061 & 1800 & 4248 & 174 \\ 3440 & 255 & 3346 & 2073 & 3668 & 1908 & 3828 & 1928 & 1928 & 1867 & 4101 & 1799 & 4259 & 1741 \\ 4416 & 255 & 3345 & 2071 & 3668 & 1993 & 3826 & 1928 & 1928 & 1928 & 1867 & 4101 & 1799 & 4259 & 1741 \\ 3442 & 245 & 3356 & 2061 & 3768 & 1993 & 3826 & 1928 & 1976 & 1867 & 4101 & 1799 & 4258 & 1741 \\ 4416 & 253 & 3356 & 2063 & 3704 & 1996 & 3824 & 1926 & 1867 & 4110 & 1796 & 4258 & 1733 \\ 442 & 245 & 3356 & 2063 & 3704 & 1996 & 3826 & 1928 & 1926 & 1867 & 4110 & 1796 & 4258 & 1733 \\ 3442 & 244 & 3376 & 2063 & 3704 & 1996 & 3836 & 1926 & 1976 & 1857 & 4110 & 1796 & 4258 & 1733 \\ 4$	3.370	2.178	3.510	2.095	3.050	2.018	3.790	1.940	3.930	1.878	4.070	1.815	4.210	1.75/
	3.374	2.176	3.514	2.003	3.654	2.017	3.794	1 945	3.034	1.877	4.074	1.814	4212	1.755
$ \begin{array}{c} 1,2,2 \\ 1,2,3 \\ 2,1,2 \\ 1,2,2 \\ 2,1,2 $	3.376	2.175	3.210	2.092	3.656	2.015	3.796	1.943	3.936	1.876	4.076	1.813	4.216	1.755
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3.378	2.173	3.218	2.090	3.658	2.014	3.798	1.942	3.938	1.875	4.078	1.812	4.218	1.754
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3.380	2.172	3.20	2.089	3.660	2.012	3.800	1.941	3.940	1.874	4.080	1.811	4.220	1.723
$ \begin{array}{c} 3:36 & 2160 & 3:562 & 2063 & 3:660 & 2006 & 3:806 & 1.938 & 3:946 & 1.871 & 4.968 & 1.806 & 1.824 & 1.753 \\ 3:388 & 2167 & 3:532 & 2.085 & 3:661 & 2.006 & 3:808 & 1.937 & 3:948 & 1.870 & 4.088 & 1.808 & 1.4228 & 1.755 \\ 3:392 & 2165 & 3:532 & 2.083 & 3:672 & 2.006 & 3:812 & 1.935 & 3:952 & 1.866 & 4:902 & 1.806 & 4:223 & 1.744 \\ 3:394 & 2164 & 3:534 & 2.076 & 3:681 & 2.076 & 3:816 & 1.934 & 3:954 & 1.867 & 4:948 & 1.825 & 4:234 & 1.744 \\ 3:396 & 2160 & 3:538 & 2.079 & 3:768 & 2.002 & 3:816 & 1.933 & 3:956 & 1.865 & 4:908 & 1.804 & 4:238 & 1.744 \\ 3:306 & 2160 & 3:538 & 2.077 & 3:682 & 2.003 & 3:812 & 1.931 & 3:956 & 1.866 & 4:098 & 1.804 & 4:248 & 1.744 \\ 3:400 & 2160 & 3:548 & 2.077 & 3:682 & 2.001 & 3:822 & 1.931 & 3:906 & 1.865 & 4:100 & 1.800 & 4:240 & 1.744 \\ 3:400 & 2156 & 3:546 & 2.075 & 3:686 & 1.908 & 3:828 & 1.927 & 3:968 & 1.866 & 4:108 & 1.709 & 4:248 & 1.744 \\ 3:406 & 2155 & 3:548 & 2.074 & 3:688 & 1.998 & 3:828 & 1.927 & 3:970 & 1.866 & 4:100 & 1.800 & 4:240 & 1.744 \\ 3:410 & 2.153 & 3:552 & 2.073 & 3:694 & 1.995 & 3:834 & 1.924 & 3:974 & 1.859 & 4:112 & 1.799 & 4:245 & 1.744 \\ 3:412 & 2.153 & 3:552 & 2.068 & 3:696 & 1.993 & 3:838 & 1.923 & 3:976 & 1.859 & 4:110 & 1.796 & 4:258 & 1.734 \\ 3:412 & 2.153 & 3:552 & 2.066 & 3:706 & 1.983 & 3:846 & 1.918 & 3:986 & 1.854 & 4:128 & 1.794 & 4:228 & 1.734 \\ 3:426 & 2.144 & 3:566 & 2.063 & 3:706 & 1.983 & 3:846 & 1.918 & 3:936 & 1.854 & 4:128 & 1.794 & 4:228 & 1.734 \\ 3:426 & 2.144 & 3:566 & 2.063 & 3:706 & 1.983 & 3:866 & 1.914 & 3:998 & 1.852 & 4:128 & 1.794 & 4:226 & 1.733 \\ 3:426 & 2.144 & 3:568 & 2.063 & 3:706 & 1.983 & 3:866 & 1.916 & 3:990 & 1.854 & 4:120 & 1.794 & 4:226 & 1.733 \\ 3:426 & 2.144 & 3:568 & 2.063 & 3:706 & 1.983 & 3:866 & 1.914 & 3:94 & 1.854 & 4:128 & 1.748 & 1.778 & 4:228 & 1.724 \\ 3:436 & 2.143 & 3:568 & 2.056 & 3:706 & 1.985 & 3:866 & 1.914 & 3:908 & 1.853 & 4:128 & 1.794 & 4:226 & 1.733 \\ 3:438 & 2.137 & 3:578 & 2.058 & 3:766 & 1.938 & 3:866 & 1.914 & 4:000 & 1.847 & 4:140 & 1.786 & 4:224 & 1.724 \\ 3:446 & 2.138 & 3:576 & 2.$	3.382	2.171	3.522	2.088	3.662	2.011	3.802	1.940	3.942	1.873	4.082	1.811	4.222	1.752
$ \begin{array}{c} 3,38 & 2,109 \\ 3,38 & 2,208 \\ 3,39 & 2,208 $	3.384	2.170	3.524	2.087	3.004	2.010	3.804	1.038	3.944	1.872	4.086	1.800	4.226	1.751
$ \begin{array}{c} 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 2 \\ 1 \\ 3 \\ 3 \\ 3 \\ 2 \\ 1 \\ 3 \\ 1 \\ 3 \\ 3 \\ 2 \\ 1 \\ 3 \\ 1 \\ 3 \\ 1 \\ 3 \\ 1 \\ 3 \\ 1 \\ 3 \\ 1 \\ 1$	3.300	2.169	3 520	2.085	3.668	2.009	3.808	1.037	3.940	1.870	4.088	1.808	4.228	1.750
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	3.300	2.166	3.530	2.084	3.670	2.007	3.810	1.936	3.950	1.869	4.090	1.807	4.230	1.749
$ \begin{array}{c} 3:36 & 2:164 \\ 3:56 & 2:06 \\ 3:56 & 2:06 \\ 3:56 & 2:07 \\ 3:67 & 2:06 \\ 3:56 & 2:07 \\ 3:68 & 2:07 \\ 3:68 & 2:07 \\ 3:68 & 2:07 \\ 3:68 & 2:07 \\ 3:68 & 2:07 \\ 3:68 & 2:00 \\ 3:54 & 2:07 \\ 3:68 & 2:00 \\ 3:54 & 2:07 \\ 3:68 & 2:00 \\ 3:54 & 2:07 \\ 3:68 & 2:00 \\ 3:82 & 1:92 \\ 3:96 \\ 1:85 \\ 4:100 \\ 1:80 \\ 4:110 \\ 1:80 \\ 4:$	3.392	2.165	3.532	2.083	3.672	2.006	3.812	1.935	3.952	1.868	4.092	1.806	4.232	1.748
$\begin{array}{c} 3:396 & 2:102 & 3:30 & 2:080 & 3:670 & 2:04 & 3:810 & 1:933 & 3:050 & 1:807 & 4:090 & 1:805 & 4:30 & 1:74 \\ 3:300 & 2:106 & 3:540 & 2:078 & 3:680 & 2:002 & 3:820 & 1:931 & 3:060 & 1:805 & 4:100 & 1:803 & 4:240 & 1:74 \\ 3:400 & 2:158 & 3:544 & 2:077 & 3:684 & 2:001 & 3:824 & 1:293 & 3:064 & 1:805 & 4:106 & 1:803 & 4:241 & 1:74 \\ 3:406 & 2:153 & 3:544 & 2:077 & 3:684 & 1:098 & 3:828 & 1:927 & 3:060 & 1:805 & 4:106 & 1:801 & 4:244 & 1:74 \\ 3:410 & 2:153 & 3:545 & 2:071 & 3:662 & 1:996 & 3:828 & 1:926 & 3:970 & 1:860 & 4:100 & 1:799 & 4:250 & 1:74 \\ 3:410 & 2:153 & 3:552 & 2:071 & 3:691 & 1:996 & 3:831 & 1:924 & 3:974 & 1:853 & 4:114 & 1:795 & 4:251 & 1:744 \\ 3:410 & 2:153 & 3:552 & 2:071 & 3:691 & 1:996 & 3:831 & 1:924 & 3:974 & 1:857 & 4:116 & 1:795 & 4:258 & 1:734 \\ 3:414 & 2:152 & 3:554 & 2:070 & 3:694 & 1:993 & 3:831 & 1:924 & 3:974 & 1:857 & 4:116 & 1:795 & 4:258 & 1:733 \\ 3:426 & 2:147 & 3:552 & 2:066 & 3:608 & 1:993 & 3:836 & 1:922 & 3:976 & 1:857 & 4:116 & 1:795 & 4:258 & 1:733 \\ 3:424 & 2:143 & 3:564 & 2:065 & 3:704 & 1:089 & 3:844 & 1:919 & 3:984 & 1:854 & 4:124 & 1:791 & 4:264 & 1:733 \\ 3:424 & 2:143 & 3:564 & 2:065 & 3:704 & 1:089 & 3:844 & 1:918 & 3:986 & 1:853 & 4:126 & 1:791 & 4:266 & 1:733 \\ 3:424 & 2:143 & 3:576 & 2:063 & 3:706 & 1:988 & 3:856 & 1:913 & 3:990 & 1:851 & 4:132 & 1:791 & 4:268 & 1:73 \\ 3:434 & 2:138 & 3:576 & 2:058 & 3:724 & 1:083 & 3:855 & 1:913 & 3:991 & 1:848 & 4:136 & 1:788 & 4:74 & 1:733 \\ 3:436 & 2:138 & 3:576 & 2:058 & 3:724 & 1:981 & 3:856 & 1:913 & 3:996 & 1:884 & 4:136 & 1:788 & 4:274 & 1:733 \\ 3:442 & 2:138 & 3:584 & 2:054 & 3:724 & 1:981 & 3:856 & 1:911 & 4:000 & 1:845 & 4:144 & 1:784 & 4:286 & 1:72 \\ 3:444 & 2:134 & 3:584 & 2:054 & 3:724 & 1:979 & 3:864 & 1:901 & 4:000 & 1:843 & 4:148 & 1:788 & 4:276 & 1:733 \\ 3:442 & 2:133 & 3:584 & 2:054 & 3:744 & 1:978 & 3:856 & 1:914 & 4:006 & 1:844 & 4:146 & 1:784 & 4:286 & 1:72 \\ 3:444 & 2:134 & 3:564 & 2:054 & 3:724 & 1:979 & 3:864 & 1:901 & 4:000 & 1:843 & 4:144 & 1:784 & 4:286 & 1:72 \\ 3:446 & 2:133 & 3:584 & 2:054 & 3:74$	3.394	2.164	3.534	2.081	3.674	2.005	3.814	1.934	3.954	1.867	4.094	1.805	4.234	1.747
$ \begin{array}{c} 3;30 & 2:101 \\ 3;340 & 2:106 \\ 3;540 & 2:078 \\ 3;680 & 2:002 \\ 3;680 & 2:000 \\ 3;540 & 2:078 \\ 3;680 & 2:073 \\ 3;680 & 2:073 \\ 3;680 & 2:073 \\ 3;680 & 2:073 \\ 3;680 & 1:906 \\ 1:801 \\ 4:100 \\ 1:802 \\ 4:100 \\ 1:802 \\ 4:100 \\ 1:801 \\ 4:100 \\ 1:801 \\ 4:100 \\ 1:790 \\ 4:240 \\ 1:741 \\ 3:400 \\ 2:156 \\ 3;540 \\ 2:071 \\ 3:620 \\ 2:071 \\ 3:620 \\ 2:071 \\ 3:620 \\ 2:071 \\ 3:620 \\ 1:790 \\ 3:620 \\ 1:997 \\ 3:620 \\ 1:997 \\ 3:620 \\ 1:997 \\ 3:620 \\ 1:997 \\ 3:620 \\ 1:997 \\ 3:620 \\ 1:997 \\ 1:800 \\ 1:923 \\ 3:970 \\ 1:800 \\ 1:801 \\ 4:100 \\ 1:790 \\ 4:250 \\ 1:790 \\ 4:250 \\ 1:790 \\ 4:250 \\ 1:791 \\ 4:250 \\ 1:791 \\ 4:250 \\ 1:791 \\ 4:250 \\ 1:791 \\ 4:250 \\ 1:791 \\ 4:250 \\ 1:791 \\ 4:250 \\ 1:791 \\ 4:250 \\ 1:791 \\ 4:250 \\ 1:791 \\ 3:420 \\ 2:143 \\ 3:550 \\ 2:061 \\ 3:700 \\ 1:990 \\ 3:840 \\ 1:921 \\ 3:980 \\ 1:851 \\ 4:120 \\ 1:791 \\ 4:250 \\ 1:791 \\ 4:260 \\ 1:731 \\ 3:420 \\ 2:143 \\ 3:560 \\ 2:061 \\ 3:700 \\ 1:990 \\ 3:841 \\ 1:910 \\ 3:981 \\ 1:851 \\ 4:120 \\ 1:791 \\ 4:20 \\ 1:731 \\ 3:420 \\ 2:143 \\ 3:560 \\ 2:061 \\ 3:700 \\ 1:990 \\ 3:841 \\ 1:910 \\ 3:981 \\ 1:851 \\ 4:120 \\ 1:791 \\ 4:20 \\ 1:731 \\ 3:420 \\ 2:143 \\ 3:560 \\ 2:061 \\ 3:700 \\ 1:980 \\ 3:851 \\ 1:910 \\ 3:851 \\ 1:910 \\ 3:980 \\ 1:851 \\ 4:120 \\ 1:791 \\ 4:20 \\ 1:731 \\ 3:420 \\ 2:143 \\ 3:560 \\ 2:061 \\ 3:700 \\ 1:980 \\ 3:851 \\ 1:911 \\ 3:900 \\ 1:811 \\ 4:130 \\ 1:791 \\ 4:70 \\ 1:731 \\ 3:430 \\ 2:143 \\ 3:750 \\ 2:061 \\ 3:700 \\ 1:980 \\ 3:851 \\ 1:911 \\ 4:000 \\ 1:847 \\ 4:130 \\ 1:791 \\ 4:70 \\ 1:731 \\ 3:430 \\ 2:173 \\ 3:430 \\ 2:130 \\ 3:560 \\ 2:051 \\ 3:720 \\ 1:910 \\ 3:650 \\ 1:911 \\ 4:000 \\ 1:847 \\ 4:140 \\ 1:781 \\ 4:28 \\ 4:721 \\ 1:731 \\ 3:440 \\ 2:130 \\ 3:560 \\ 2:051 \\ 3:720 \\ 1:910 \\ 3:650 \\ 1:911 \\ 4:000 \\ 1:847 \\ 4:140 \\ 1:781 \\ 4:781$	3.396	2.162	3.530	2.080	3.676	2.004	3.816	1.933	3.056	1.867	4.096	1.805	4.230	1.747
$ \begin{array}{c} 3 + 0 & 2 + 10 & 3 + 4 & 2 + 07 \\ 3 + 0 & 2 + 15 & 3 + 4 & 2 + 07 \\ 3 + 0 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 0 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 0 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 0 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 0 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 0 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 10 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 10 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 10 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 12 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 12 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 14 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 14 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 14 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 14 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 14 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 14 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 14 & 2 + 15 & 3 + 5 + 2 + 07 \\ 3 + 14 & 2 + 14 & 3 + 5 + 2 + 07 \\ 3 + 14 & 2 + 14 & 3 + 5 + 2 + 07 \\ 3 + 14 & 2 + 14 & 3 + 5 + 2 + 07 \\ 3 + 14 & 2 + 14 & 3 + 5 + 2 + 07 \\ 3 + 14 & 2 + 14 & 3 + 5 + 2 + 06 \\ 3 + 2 & 2 + 14 & 3 + 5 + 2 + 06 \\ 3 + 2 & 2 + 14 & 3 + 5 + 2 + 06 \\ 3 + 2 & 2 + 14 & 3 + 5 + 2 + 06 \\ 3 + 2 & 2 + 14 & 3 + 5 + 2 + 06 \\ 3 + 2 & 2 + 14 & 3 + 5 + 2 + 06 \\ 3 + 2 & 2 + 14 & 3 + 5 + 2 + 06 \\ 3 + 2 & 2 + 14 & 3 + 5 + 2 + 06 \\ 3 + 2 & 2 + 14 & 3 + 5 + 2 + 06 \\ 3 + 2 & 2 + 14 & 3 + 5 + 2 + 16 \\ 3 + 2 & 2 + 14 & 3 + 5 + 2 + 2 + 16 \\ 3 + 2 & 2 + 14 & 3 + 5 + 2 + 2 + 16 \\ 3 + 3 + 2 & 2 + 14 & 3 + 17 \\ 3 + 2 & 2 + 14 & 3 + 5 + 2 + 16 \\ 3 + 3 + 2 + 1 & 3 + 5 + 2 + 16 \\ 3 + 3 + 2 + 1 & 3 + 5 + 2 + 16 \\ 3 + 3 + 2 + 1 & 3 + 5 + 2 + 16 \\ 3 + 3 + 2 + 1 & 3 + 5 + 2 + 16 \\ 3 + 3 + 2 + 1 & 3 + 5 + 2 + 16 \\ 3 + 3 + 1 & 3 + 17 + 2 + 17 \\ 3 + 3 + 2 + 1 & 3 + 5 + 2 + 16 \\ 3 + 3 + 1 & 3 + 17 + 17 \\ 3 + 3 + 2 + 1 & 3 + 15 + 2 + 16 \\ 3 + 1 & 3 + 17 + 17 \\ 3 + 15 + 2 + 17 \\ 3 + 15 + 2 + 15 + 17 \\ 3 + 16 + 17 + 1 & 17 + 17 \\ 3 + 16 + 2 + 15 + 17 \\ 3 + 16 + 17 + 1 & 17 + 17 \\ 3 + 16 + 2 + 15 + 17 \\ 3 + 16 + 17 + 17 \\ 3 + 16 + 2 + 15 + 17 \\ 3 + 16 + 17 + 17 \\ 3 + 16 + 17 \\ 3 + 16 + 2 + 15 + 17 \\ 3 + 16 + 17 + 17 \\ 3 + 16 + 2 + 15 + 17 \\ 3 + 16 + 17 + 17 \\ 3 + 17 + 17 \\ 3 + 17 + 17 \\ 3 + 17 + 17 \\ 3 + 17 + 17 \\ 3 + 17 + 17 \\ 3 + 17 + 17 \\ 3 + 17 + 17 \\ 3 + 17 + 17 \\ 3$	3.398	2.101	3.530	2.079	3.078	2.003	3.810	1.932	3.950	1.800	4.098	1.804	4.230	1.740
$\begin{array}{c} 3:406 & 2:158 & 3:544 & 2:076 & 3:684 & 2:000 & 3:824 & 1:926 & 3:964 & 1:863 & 4:104 & 1:801 & 4:246 & 1:744 \\ 3:406 & 2:156 & 3:540 & 2:074 & 3:688 & 1:999 & 3:826 & 1:928 & 3:966 & 1:861 & 4:108 & 1:799 & 4:248 & 1:744 \\ 3:410 & 2:154 & 3:550 & 2:072 & 3:690 & 1:997 & 3:83a & 1:926 & 3:970 & 1:866 & 4:110 & 1:799 & 4:248 & 1:744 \\ 3:412 & 2:153 & 3:552 & 2:071 & 3:691 & 1:926 & 3:972 & 1:859 & 4:112 & 1:798 & 4:252 & 1:744 \\ 3:414 & 2:152 & 3:554 & 2:070 & 3:694 & 1:995 & 3:834 & 1:924 & 3:974 & 1:858 & 4:114 & 1:797 & 4:254 & 1:733 \\ 3:416 & 2:159 & 3:556 & 2:063 & 3:698 & 1:993 & 3:838 & 1:922 & 3:978 & 1:857 & 4:116 & 1:796 & 4:256 & 1:733 \\ 3:422 & 2:148 & 3:566 & 2:067 & 3:700 & 1:992 & 3:841 & 1:921 & 3:986 & 1:855 & 4:122 & 1:794 & 4:202 & 1:733 \\ 3:422 & 2:143 & 3:564 & 2:063 & 3:704 & 1:989 & 3:844 & 1:919 & 3:984 & 1:855 & 4:122 & 1:794 & 4:206 & 1:733 \\ 3:428 & 2:143 & 3:568 & 2:062 & 3:708 & 1:987 & 3:848 & 1:917 & 3:988 & 1:853 & 4:126 & 1:792 & 4:266 & 1:733 \\ 3:428 & 2:143 & 3:576 & 2:061 & 3:712 & 1:985 & 3:852 & 1:915 & 3:992 & 1:851 & 4:132 & 1:786 & 4:274 & 1:733 \\ 3:438 & 2:143 & 3:574 & 2:059 & 3:712 & 1:985 & 3:852 & 1:915 & 3:992 & 1:851 & 4:132 & 1:786 & 4:274 & 1:733 \\ 3:438 & 2:137 & 3:578 & 2:053 & 3:726 & 1:981 & 3:856 & 1:912 & 3:998 & 1:848 & 4:136 & 1:786 & 4:274 & 1:733 \\ 3:442 & 2:138 & 3:576 & 2:053 & 3:726 & 1:973 & 3:866 & 1:911 & 4:000 & 1:845 & 4:144 & 1:788 & 4:276 & 1:732 \\ 3:444 & 2:134 & 3:584 & 2:054 & 3:726 & 1:973 & 3:866 & 1:914 & 4:004 & 1:845 & 4:144 & 1:788 & 4:286 & 1:722 \\ 3:444 & 2:134 & 3:584 & 2:054 & 3:726 & 1:973 & 3:866 & 1:904 & 4:064 & 1:784 & 4:28 & 1:724 & 1:733 \\ 3:456 & 2:126 & 3:596 & 2:043 & 3:736 & 1:973 & 3:876 & 1:904 & 4:848 & 4:138 & 1:786 & 4:224 & 1:733 \\ 3:456 & 2:128 & 3:594 & 2:054 & 3:726 & 1:973 & 3:876 & 1:904 & 1:846 & 4:154 & 1:778 & 4:288 & 1:724 \\ 3:456 & 2:129 & 3:592 & 2:049 & 3:732 & 1:975 & 3:878 & 1:993 & 4:018 & 1:839 & 4:158 & 1:776 & 4:28 & 1:724 \\ 3:456 & 2:129 & 3:596 & 2:043 & 3:786 & 1:973 & 4:046 & 1:836 & 4$	3.400	2.100	3 540	2.077	3.682	2.001	3.822	1.030	3.900	1.864	4.102	1.802	4.242	1.744
$ \begin{array}{c} 3 + 66 & 2+156 & 3:546 & 2-074 & 3:686 & 1-999 & 3:826 & 1-928 & 3:966 & 1:862 & 4:106 & 1:800 & 4:246 & 1:744 \\ 3:408 & 2:155 & 3:558 & 2:072 & 3:690 & 1997 & 3:838 & 1:925 & 3:972 & 1:859 & 4:112 & 1:798 & 4:252 & 1:744 \\ 3:414 & 2:153 & 3:552 & 2:071 & 3:692 & 1:996 & 3:831 & 1:924 & 3:974 & 1:858 & 4:114 & 1:797 & 4:254 & 1:734 \\ 3:416 & 2:159 & 3:556 & 2:069 & 3:696 & 1:994 & 3:836 & 1:923 & 3:976 & 1:857 & 4:118 & 1:795 & 4:256 & 1:733 \\ 3:426 & 2:144 & 3:566 & 2:067 & 3:700 & 1:992 & 3:841 & 1:924 & 3:948 & 1:857 & 4:118 & 1:795 & 4:258 & 1:733 \\ 3:426 & 2:144 & 3:566 & 2:067 & 3:700 & 1:992 & 3:841 & 1:943 & 3:986 & 1:855 & 4:122 & 1:794 & 4:262 & 1:733 \\ 3:426 & 2:143 & 3:566 & 2:063 & 3:706 & 1:988 & 3:841 & 1:918 & 3:986 & 1:855 & 4:122 & 1:794 & 4:262 & 1:733 \\ 3:426 & 2:143 & 3:566 & 2:063 & 3:706 & 1:988 & 3:841 & 1:918 & 3:986 & 1:855 & 4:128 & 1:791 & 4:268 & 1:733 \\ 3:426 & 2:143 & 3:566 & 2:063 & 3:706 & 1:988 & 3:850 & 1:916 & 3:900 & 1:851 & 4:130 & 1:790 & 4:270 & 1:733 \\ 3:428 & 2:143 & 3:566 & 2:063 & 3:711 & 1:985 & 3:852 & 1:915 & 3:992 & 1:851 & 4:132 & 1:794 & 4:266 & 1:733 \\ 3:430 & 2:142 & 3:570 & 2:061 & 3:710 & 1:986 & 3:850 & 1:916 & 3:900 & 1:851 & 4:134 & 1:788 & 4:271 & 1:733 \\ 3:436 & 2:138 & 3:576 & 2:958 & 3:724 & 1:938 & 3:856 & 1:913 & 3:906 & 1:848 & 4:134 & 1:788 & 4:276 & 1:733 \\ 3:440 & 2:136 & 3:582 & 2:055 & 3:722 & 1:980 & 3:862 & 1:911 & 4:000 & 1:847 & 4:144 & 1:788 & 4:276 & 1:732 \\ 3:446 & 2:137 & 3:578 & 2:056 & 3:724 & 1:978 & 3:861 & 1:911 & 4:002 & 1:846 & 4:144 & 1:788 & 4:276 & 1:723 \\ 3:446 & 2:136 & 3:580 & 2:056 & 3:724 & 1:978 & 3:861 & 1:911 & 4:002 & 1:846 & 4:144 & 1:788 & 4:286 & 1:722 \\ 3:446 & 2:132 & 3:562 & 2:055 & 3:724 & 1:978 & 3:861 & 1:904 & 4:068 & 1:748 & 4:286 & 1:722 \\ 3:458 & 2:138 & 3:592 & 2:049 & 3:734 & 1:971 & 3:861 & 1:904 & 1:841 & 4:148 & 1:788 & 4:286 & 1:722 \\ 3:456 & 2:122 & 3:502 & 2:043 & 3:724 & 1:970 & 3:861 & 1:904 & 4:046 & 1:744 & 1:788 & 4:286 & 1:722 \\ 3:456 & 2:123 & 3:502 & 2:043 & 3:738 & 1:972 & 3:866 $	3.404	2.158	3.544	2.076	3.684	2.000	3.824	1.929	3.964	1.863	4.104	1.801	4.244	1.743
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	3.406	2.156	3.546	2.075	3.686	1.999	3.826	1.928	3.966	1.862	4.106	1.800	4.246	1.743
$ \begin{array}{c} 3:412 2:154 \\ 3:450 2:071 3:692 1:997 3:831 1:925 3:971 1:850 4:110 1:798 4:252 1:744 \\ 3:414 2:152 3:555 2:068 3:694 1:994 3:836 1:923 3:976 1:857 4:116 1:795 4:254 1:733 \\ 3:416 2:149 3:556 2:066 3:698 1:994 3:836 1:922 3:986 1:857 4:116 1:795 4:256 1:733 \\ 3:422 2:148 3:560 2:067 3:700 1:992 3:841 1:921 3:980 1:855 4:120 1:794 4:260 1:733 \\ 3:422 2:143 3:564 2:065 3:704 1:988 3:846 1:918 3:986 1:853 4:126 1:794 4:266 1:733 \\ 3:426 2:144 3:564 2:062 3:708 1:988 3:846 1:918 3:986 1:853 4:124 1:794 4:266 1:733 \\ 3:426 2:144 3:562 2:067 3:704 1:988 3:846 1:917 3:988 1:854 4:124 1:794 4:266 1:733 \\ 3:430 2:142 3:570 2:061 3:710 1:986 3:850 1:916 3:990 1:851 4:130 1:796 4:277 1:733 \\ 3:430 2:143 3:572 2:056 3:714 1:983 3:856 1:913 3:996 1:848 4:134 1:788 4:277 1:733 \\ 3:436 2:138 3:576 2:058 3:716 1:983 3:856 1:911 3:990 1:848 4:134 1:788 4:276 1:733 \\ 3:442 2:136 3:580 2:056 3:722 1:981 3:866 1:911 4:000 1:847 4:140 1:786 4:226 1:723 \\ 3:442 2:136 3:580 2:056 3:722 1:9978 3:866 1:904 4:006 1:843 4:146 1:788 4:276 1:724 \\ 3:446 2:132 3:586 2:055 3:724 1:973 3:866 1:904 4:006 1:843 4:144 1:784 4:286 1:724 \\ 3:446 2:132 3:566 2:052 3:726 1:973 3:866 1:904 4:066 1:843 4:144 1:784 4:286 1:724 \\ 3:450 2:129 3:590 2:059 3:736 1:973 3:876 1:903 4:06 1:843 4:146 1:784 4:266 1:723 \\ 3:450 2:130 3:590 2:059 3:730 1:976 3:860 1:904 4:006 1:843 4:146 1:784 4:286 1:724 \\ 3:446 2:132 3:566 2:052 3:726 1:973 3:876 1:904 4:06 1:843 4:146 1:784 4:286 1:724 \\ 3:450 2:129 3:590 2:049 3:734 1:974 3:876 1:903 4:06 1:843 4:146 1:778 4:226 1:723 \\ 3:450 2:129 3:590 $	3.408	2.155	3.548	2.074	3.688	1.998	3.828	1.927	3.968	1.861	4.108	1.799	4.248	1.742
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.410	2.154	3.520	2.072	3.690	1.992	3.830	1.926	3.970	1.860	4.110	1.799	4.250	1.741
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3.412	2.153	3.552	2.071	3.692	1.002	3.832	1.925	3.972	1.859	4.112	1.798	4.252	1.740
$\begin{array}{c} 3+18 & 2+149 & 3+58 & 2+068 & 3+698 & 1+991 & 3+88 & 1+921 & 3+98 & 1+857 & 4+118 & 1+794 & 4+258 & 1+733 \\ 3+220 & 2+148 & 3+560 & 2+067 & 3+700 & 1+992 & 3+84 & 1+921 & 3+980 & 1+855 & 4+122 & 1+744 & 1+726 & 1+733 \\ 3+242 & 2+147 & 3+560 & 2+063 & 3+706 & 1+988 & 3+846 & 1+918 & 3+986 & 1+853 & 4+124 & 1+794 & 4+266 & 1+733 \\ 3+242 & 2+143 & 3+560 & 2+063 & 3+706 & 1+988 & 3+846 & 1+918 & 3+986 & 1+853 & 4+124 & 1+794 & 4+266 & 1+733 \\ 3+242 & 2+143 & 3+560 & 2+063 & 3+706 & 1+988 & 3+846 & 1+917 & 3+988 & 1+852 & 4+128 & 1+794 & 4+266 & 1+733 \\ 3+342 & 2+144 & 3+572 & 2+061 & 3+710 & 1+986 & 3+850 & 1+916 & 3+994 & 1+849 & 4+134 & 1+788 & 4+274 & 1+733 \\ 3+342 & 2+138 & 3+576 & 2+058 & 3+716 & 1+983 & 3+856 & 1+913 & 3+994 & 1+849 & 4+138 & 1+788 & 4+274 & 1+733 \\ 3+436 & 2+138 & 3+576 & 2+058 & 3+716 & 1+983 & 3+856 & 1+913 & 3+994 & 1+849 & 4+138 & 1+788 & 4+276 & 1+733 \\ 3+436 & 2+138 & 3+576 & 2+058 & 3+726 & 1+983 & 3+856 & 1+914 & 4+000 & 1+847 & 4+140 & 1+786 & 4+226 & 1+724 \\ 3+442 & 2+135 & 3+586 & 2+055 & 3+722 & 1+978 & 3+866 & 1+911 & 4+000 & 1+847 & 4+140 & 1+786 & 4+286 & 1+724 \\ 3+446 & 2+132 & 3+586 & 2+053 & 3+724 & 1+979 & 3+866 & 1+904 & 4+06 & 1+845 & 4+144 & 1+784 & 4+284 & 1+724 \\ 3+446 & 2+132 & 3+586 & 2+053 & 3+726 & 1+977 & 3+866 & 1+904 & 4+06 & 1+844 & 4+156 & 1+783 & 4+286 & 1+724 \\ 3+456 & 2+123 & 3+596 & 2+053 & 3+726 & 1+977 & 3+876 & 1+904 & 4+154 & 1+784 & 4+294 & 1+724 \\ 3+456 & 2+123 & 3+596 & 2+043 & 3+734 & 1+977 & 3+876 & 1+904 & 1+844 & 4+154 & 1+784 & 4+294 & 1+724 \\ 3+456 & 2+124 & 3+600 & 2+043 & 3+734 & 1+973 & 3+876 & 1+904 & 1+834 & 4+154 & 1+784 & 4+294 & 1+724 \\ 3+456 & 2+124 & 3+606 & 2+043 & 3+734 & 1+973 & 3+876 & 1+904 & 1+834 & 4+154 & 1+778 & 4+294 & 1+724 \\ 3+456 & 2+124 & 3+604 & 2+043 & 3+734 & 1+973 & 3+886 & 1+904 & 1+834 & 4+156 & 1+777 & 4+316 & 1+774 \\ 3+462 & 2+124 & 3+604 & 2+043 & 3+734 & 1+973 & 3+886 & 1+904 & 1+834 & 4+156 & 1+776 & 4+324 & 1+724 \\ 3+466 & 2+124 & 3+604 & 2+043 & 3+734 & 1+967 & 3+884 & 1+766 & 1+774 & 4+306 & 1+774 $	3.414	2.152	3.224	2.070	3.094	1.001	2.836	1.023	3.974	1.857	4.114	1.797	4-256	1.739
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.418	2.149	3.558	2.068	3.698	1.003	3.838	1.923	3.978	1.857	4.118	1.795	4.258	1.738
$ \begin{array}{c} 3+22 & 2:147 \\ 3+24 & 2:143 \\ 3+56 \\ 2:056 \\ 3+70 \\ 4:198 \\ 3+84 \\ 4:191 \\ 3+84 \\ 4:191 \\ 3+84 \\ 4:185 \\ 4+124 \\ 1:791 \\ 4:126 \\ 1:733 \\ 3+28 \\ 2:144 \\ 3:568 \\ 2:052 \\ 3:706 \\ 1:983 \\ 3*84 \\ 1:917 \\ 3:984 \\ 1:854 \\ 4:124 \\ 1:791 \\ 4:126 \\ 1:732 \\ 3:426 \\ 2:141 \\ 3:572 \\ 2:060 \\ 3:712 \\ 1:985 \\ 3:850 \\ 1:916 \\ 3:850 \\ 1:916 \\ 3:902 \\ 1:851 \\ 4:130 \\ 1:851 \\ 4:132 \\ 1:780 \\ 4:126 \\ 1:733 \\ 3:432 \\ 2:141 \\ 3:572 \\ 2:060 \\ 3:757 \\ 2:060 \\ 3:712 \\ 1:985 \\ 3:856 \\ 1:915 \\ 3:920 \\ 1:851 \\ 4:130 \\ 1:74 \\ 3:990 \\ 1:851 \\ 4:130 \\ 1:780 \\ 4:138 \\ 1:78 \\ 4:138 \\ 1:787 \\ 4:276 \\ 1:733 \\ 3:438 \\ 2:137 \\ 3:578 \\ 2:057 \\ 3:718 \\ 1:982 \\ 3:856 \\ 1:912 \\ 3:906 \\ 1:848 \\ 4:136 \\ 1:784 \\ 4:136 \\ 1:786 \\ 4:142 \\ 1:786 \\ 4:276 \\ 1:733 \\ 3:438 \\ 2:137 \\ 3:578 \\ 2:055 \\ 3:720 \\ 1:981 \\ 3:856 \\ 1:912 \\ 3:908 \\ 1:848 \\ 4:136 \\ 1:787 \\ 4:276 \\ 1:733 \\ 3:438 \\ 2:137 \\ 3:578 \\ 2:055 \\ 3:720 \\ 1:981 \\ 3:856 \\ 1:912 \\ 3:908 \\ 1:848 \\ 4:138 \\ 1:787 \\ 4:276 \\ 1:733 \\ 3:442 \\ 2:136 \\ 3:580 \\ 2:055 \\ 3:720 \\ 1:981 \\ 3:856 \\ 1:912 \\ 3:908 \\ 1:848 \\ 4:138 \\ 1:787 \\ 4:276 \\ 1:733 \\ 3:442 \\ 2:136 \\ 3:580 \\ 2:055 \\ 3:720 \\ 1:978 \\ 3:856 \\ 1:909 \\ 4:06 \\ 1:844 \\ 4:140 \\ 1:784 \\ 4:140 \\ 1:784 \\ 4:281 \\ 1:724 \\ 1:$	3.420	2.148	3.560	2.067	3.700	1.992	3.840	1.921	3.980	1.856	4.120	1.794	4.260	1.737
$\begin{array}{c} 3:424 & 2:145 & 3:564 & 2:065 & 3:706 & 1:988 & 3:846 & 1:918 & 3:986 & 1:851 & 4:124 & 1:793 & 4:204 & 1:733 \\ 3:428 & 2:143 & 3:568 & 2:062 & 3:708 & 1:987 & 3:848 & 1:917 & 3:988 & 1:852 & 4:128 & 1:791 & 4:268 & 1:733 \\ 3:430 & 2:142 & 3:572 & 2:061 & 3:710 & 1:986 & 3:850 & 1:916 & 3:990 & 1:851 & 4:130 & 1:790 & 4:270 & 1:733 \\ 3:432 & 2:141 & 3:572 & 2:050 & 3:712 & 1:985 & 3:852 & 1:915 & 3:992 & 1:851 & 4:130 & 1:788 & 4:274 & 1:733 \\ 3:434 & 2:138 & 3:574 & 2:059 & 3:714 & 1:984 & 3:854 & 1:914 & 3:994 & 1:849 & 4:134 & 1:788 & 4:274 & 1:733 \\ 3:436 & 2:138 & 3:576 & 2:057 & 3:718 & 1:982 & 3:858 & 1:912 & 3:996 & 1:848 & 4:138 & 1:787 & 4:278 & 1:733 \\ 3:438 & 2:137 & 3:578 & 2:057 & 3:720 & 1:981 & 3:860 & 1:911 & 4:000 & 1:847 & 4:140 & 1:786 & 4:280 & 1:723 \\ 3:444 & 2:136 & 3:586 & 2:052 & 3:722 & 1:980 & 3:862 & 1:911 & 4:000 & 1:847 & 4:140 & 1:785 & 4:286 & 1:723 \\ 3:444 & 2:134 & 3:584 & 2:054 & 3:724 & 1:979 & 3:864 & 1:900 & 4:064 & 1:845 & 4:144 & 1:783 & 4:286 & 1:723 \\ 3:444 & 2:134 & 3:588 & 2:051 & 3:728 & 1:977 & 3:868 & 1:909 & 4:068 & 1:843 & 4:148 & 1:783 & 4:286 & 1:723 \\ 3:450 & 2:130 & 3:590 & 2:050 & 3:730 & 1:975 & 3:872 & 1:997 & 4:010 & 1:842 & 4:150 & 1:788 & 4'290 & 1:722 \\ 3:454 & 2:128 & 3:594 & 2:048 & 3:734 & 1:973 & 3:876 & 1:904 & 4:016 & 1:839 & 4:156 & 1:778 & 4'298 & 1:724 \\ 3:456 & 2:122 & 3:598 & 2:046 & 3:738 & 1:972 & 3:878 & 1:903 & 4:016 & 1:839 & 4:156 & 1:778 & 4'298 & 1:724 \\ 3:456 & 2:123 & 3:602 & 2:044 & 3:734 & 1:971 & 3:887 & 1:903 & 4:016 & 1:839 & 4:156 & 1:778 & 4'300 & 1:724 \\ 3:466 & 2:123 & 3:602 & 2:044 & 3:748 & 1:963 & 3:861 & 1:904 & 4:04 & 1:58 & 1:778 & 4'308 & 1:724 \\ 3:466 & 2:123 & 3:602 & 2:044 & 3:748 & 1:966 & 3:884 & 1:900 & 4:024 & 1:836 & 4:164 & 1:776 & 4:304 & 1:724 \\ 3:466 & 2:123 & 3:606 & 2:043 & 3:746 & 1:967 & 3:884 & 1:900 & 4:024 & 1:831 & 4:776 & 1:778 & 4:308 & 1:772 \\ 3:456 & 2:113 & 3:612 & 2:038 & 3:752 & 1:965 & 3:806 & 1:899 & 4:024 & 1:831 & 4:176 & 1:777 & 4:314 & 1:776 \\ 3:476 & 2:119 & 3:608 & 2:046 & 3$	3.422	2.147	3.562	2.066	3.702	1.900	3.842	1.920	3.982	1.855	4.122	1.794	4.262	1.736
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3.424	2.145	3.564	2.065	3.704	1.989	3.844	1.010	3.984	1.854	4.124	1.793	4.204	1.735
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.420	2.144	3.566	2.063	3.700	1.988	3.840	1.918	3.980	1.853	4.120	1.792	4.200	1.735
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.420	2.143	3.500	2.002	3.700	1.086	3.040	1.016	3.000	1.851	4.120	1.700	4 200	1.733
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.430	2.141	3.572	2.060	3.712	1.985	3.852	1.915	3.992	1.851	4.132	1.789	4.272	1.732
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.434	2.139	3.574	2.059	3.714	1.984	3.854	1.914	3.994	1.849	4.134	1.788	4.274	1.732
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.436	2.138	3.576	2.058	3.716	1.983	3.856	1.913	3.996	1.848	4.136	1.788	4.276	1.731
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.438	2.137	3.578	2.057	3.218	1.982	3.858	1.912	3.998	1.848	4.138	1.787	4.278	1.730
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.440	2.130	3.280	2.050	.3.720	1.981	3.860	1.011	4.000	1.847	4.140	1.785	4.280	1.728
$\begin{array}{c} 3+446 & 2\cdot 132 & 3\cdot 586 & 2\cdot 051 & 3\cdot 747 & 1\cdot 975 & 3\cdot 866 & 1\cdot 909 & 4\cdot 066 & 1\cdot 844 & 4\cdot 146 & 1\cdot 783 & 4\cdot 286 & 1\cdot 724 \\ 3\cdot 448 & 2\cdot 131 & 3\cdot 588 & 2\cdot 051 & 3\cdot 728 & 1\cdot 977 & 3\cdot 868 & 1\cdot 909 & 4\cdot 008 & 1\cdot 843 & 4\cdot 148 & 1\cdot 783 & 4\cdot 288 & 1\cdot 724 \\ 3\cdot 450 & 2\cdot 130 & 3\cdot 590 & 2\cdot 050 & 3\cdot 730 & 1\cdot 975 & 3\cdot 872 & 1\cdot 907 & 4\cdot 010 & 1\cdot 842 & 4\cdot 150 & 1\cdot 781 & 4\cdot 294 & 1\cdot 724 \\ 3\cdot 452 & 2\cdot 128 & 3\cdot 594 & 2\cdot 048 & 3\cdot 734 & 1\cdot 974 & 3\cdot 874 & 1\cdot 905 & 4\cdot 012 & 1\cdot 841 & 4\cdot 152 & 1\cdot 781 & 4\cdot 294 & 1\cdot 724 \\ 3\cdot 456 & 2\cdot 126 & 3\cdot 594 & 2\cdot 048 & 3\cdot 734 & 1\cdot 971 & 3\cdot 876 & 1\cdot 905 & 4\cdot 014 & 1\cdot 840 & 4\cdot 154 & 1\cdot 780 & 4\cdot 294 & 1\cdot 724 \\ 3\cdot 456 & 2\cdot 126 & 3\cdot 596 & 2\cdot 047 & 3\cdot 736 & 1\cdot 971 & 3\cdot 880 & 1\cdot 902 & 4\cdot 016 & 1\cdot 839 & 4\cdot 156 & 1\cdot 778 & 4\cdot 296 & 1\cdot 723 \\ 3\cdot 458 & 2\cdot 122 & 3\cdot 600 & 2\cdot 045 & 3\cdot 744 & 1\cdot 971 & 3\cdot 880 & 1\cdot 902 & 4\cdot 022 & 1\cdot 833 & 4\cdot 160 & 1\cdot 778 & 4\cdot 300 & 1\cdot 724 \\ 3\cdot 464 & 2\cdot 122 & 3\cdot 600 & 2\cdot 043 & 3\cdot 744 & 1\cdot 969 & 3\cdot 884 & 1\cdot 900 & 4\cdot 024 & 1\cdot 836 & 4\cdot 164 & 1\cdot 776 & 4\cdot 304 & 1\cdot 724 \\ 3\cdot 466 & 2\cdot 121 & 3\cdot 606 & 2\cdot 041 & 3\cdot 744 & 1\cdot 969 & 3\cdot 884 & 1\cdot 900 & 4\cdot 024 & 1\cdot 836 & 4\cdot 164 & 1\cdot 776 & 4\cdot 304 & 1\cdot 726 \\ 3\cdot 466 & 2\cdot 121 & 3\cdot 606 & 2\cdot 041 & 3\cdot 748 & 1\cdot 967 & 3\cdot 888 & 1\cdot 899 & 4\cdot 026 & 1\cdot 835 & 4\cdot 166 & 1\cdot 775 & 4\cdot 306 & 1\cdot 716 \\ 3\cdot 476 & 2\cdot 118 & 3\cdot 610 & 2\cdot 038 & 3\cdot 752 & 1\cdot 966 & 3\cdot 899 & 1\cdot 897 & 4\cdot 030 & 1\cdot 833 & 4\cdot 170 & 1\cdot 771 & 4\cdot 310 & 1\cdot 716 \\ 3\cdot 476 & 2\cdot 112 & 3\cdot 616 & 2\cdot 036 & 3\cdot 758 & 1\cdot 966 & 3\cdot 899 & 1\cdot 897 & 4\cdot 038 & 1\cdot 831 & 4\cdot 177 & 1\cdot 773 & 4\cdot 312 & 1\cdot 716 \\ 3\cdot 476 & 2\cdot 112 & 3\cdot 616 & 2\cdot 036 & 3\cdot 758 & 1\cdot 962 & 3\cdot 898 & 1\cdot 896 & 4\cdot 038 & 1\cdot 830 & 4\cdot 178 & 1\cdot 769 & 4\cdot 324 & 1\cdot 712 \\ 3\cdot 476 & 2\cdot 114 & 3\cdot 618 & 2\cdot 036 & 3\cdot 758 & 1\cdot 961 & 3\cdot 900 & 1\cdot 829 & 4\cdot 048 & 1\cdot 820 & 4\cdot 188 & 1\cdot 766 & 4\cdot 324 & 1\cdot 712 \\ 3\cdot 488 & 2\cdot 108 & 3\cdot 628 & 2\cdot 03 & 3\cdot 768 & 1\cdot 957 & 3\cdot 908 & 1\cdot 839 & 4\cdot 038 & 1\cdot 830 & 4\cdot 178 & 1\cdot 769 & 4\cdot 328 & 1\cdot 713 \\ 3\cdot 488 & 2\cdot 108 & 3\cdot 628 & 2\cdot 03 & 3\cdot 768 & 1\cdot 957 & 3\cdot 908 & 1\cdot 889 & 4\cdot 046 & 1\cdot 8226 & 4\cdot 188 & 1\cdot 766 & 4\cdot 324 & 1\cdot 713 \\ 3\cdot 488 & 2\cdot 108 & 3\cdot 628 $	3.444	2.135	3.584	2.054	3.724	1.070	3.864	1.010	4.002	1.845	4 142	1.784	4.284	1.728
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.446	2.132	3.586	2.052	3.726	1.978	3.866	1.000	4.006	1.844	4.146	1.783	4.286	1.727
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.448	2.131	3.588	2.051	3.728	1.977	3.868	800.1	4.008	1.843	4.148	1.783	4.288	1.726
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.450	2.130	3.290	2.050	3.730	1.976	3.870	1.902	4.010	1.842	4.120	1.782	4.290	1.725
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.422	2.129	3.265	2.049	3.732	1.975	3.872	1.956	4.012	1.841	4.152	1.781	4.292	1.725
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.454	2.128	3.594	2.048	3.734	1.974	3.074	1.002	4.014	1.040	4.156	1.770	4.494	1.723
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.450	2.125	3.590	2.04/	3.738	1.072	3.878	1.003	4.018	1.839	4.158	1.778	4.298	1.722
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.460	2.124	3.600	2.045	3.740	1.971	3.880	1.902	4.020	1.838	4.160	1.778	4.300	1.721
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.462	2.123	3.602	2.044	3.742	1.970	3.882	1.001	4.022	1.837	4.162	1.777	4.302	1.721
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3.464	2.122	3.604	2.043	3.744	1.969	3.884	1.000	4.024	1.836	4.164	1.776	4.304	1.720
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.466	2.121	3.606	2.041	3.746	1.968	3.886	1.899	4.026	1.835	4.100	1.775	4.300	1.719
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.408	2.119	3.008	2.040	3.748	1.907	3.888	1.898	4.028	1.034	4.170	1.773	4 300	1.717
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.470	2.110	3.010	2.039	3.750	1.065	3.890	1.806	4.030	1.832	4 · 1 72	1.773	4.312	1.717
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.474	2.116	3.614	2.037	3.754	1.964	3.894	1.895	4.034	1.831	4.174	1.772	4.314	1.716
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	3.476	2.115	3.616	2.036	3.756	1.963	3.896	1.894	4.036	1.831	4.176	1.771	4.316	1.715
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3.478	2.114	3.618	2.035	3.758	1.962	3.898	1.893	4 · 038	1.830	4.178	1.770	4.318	1.714
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.480	2.112	3.620	2.034	3.760	1.961	3.900	1.892	4.040	1.829	4.180	1.769	4.320	1.713
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.482	2.111	3.022	2.033	3.702	1.960	3.902	1.801	4.042	1.827	4.102	1.768	4.324	1.712
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.404	2.110	3.024	2.032	3.704	1.028	3.004	1.800	4.044	1.826	4.186	1.767	4.326	1.711
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	3.488	2.108	3.628	2.030	3.768	I 957	3.908	1.889	4.048	1.825	4.188	1.766	4.328	1.710
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.490	2.107	3.630	2.029	3.770	1.956	3.910	1.888	4.050	1.824	4.190	1.765	4.330	1.710
5.494 2.104 3.634 2.026 3.774 1.954 3.914 1.886 4.054 1.823 4.194 1.708 3.496 2.103 3.636 2.025 3.776 1.953 3.016 1.885 4.056 1.822 4.196 1.763 4.336 1.707	3.492	2.105	3.632	2.027	3.772	1.955	3.912	1.887	4.052	1.824	4.192	1.764	4.332	1.709
3*490 2*103 3*630 2*025 3*776 I*053 3*916 I*885 4*056 I*822 4*190 I*703 4*330 I*707	5.494	2.104	3.634	2.026	3.774	1.954	3.914	1.886	4.054	1.823	4.194	1.764	4.334	1.708
2:108 2:100 2:628 2:021 2:278 1:022 2:02 1:028 1:028 1:108 1:762 4:228 1:707	3.496	2.103	3.636	2.025	3.776	1.953	3.916	1.885	4.050	1.022	4.190	1.703	4.330	1.707

A and B Cor.	Reduc- tion.												
4.340	1.706	4.480	1.654	4.620	1.605	4.760	1.550	1:000	1.515	5.500	1.252	6,200	1.202
4.342	1.705	4.482	1.653	4.622	1.604	4.762	1.558	4.900	1.513	5.200	1.353	6.210	1.202
4.344	1.704	4.484	1.652	4.624	1.604	4.764	1.557	4.904	1.514	5.520	1.348	6.220	1.198
4.346	1.703	4.486	1.652	4.626	1.603	4.766	1.557	4.906	1.213	5.230	1.345	6.230	1.196
4.340	1.702	4 400	1.650	4.630	1.602	4.700	1.550	4.000	1.513	5.540	1.343	6.250	1.194
4.352	1.701	4.492	1.649	4.632	1.601	4.772	1·555	4.912	1.511	5.560	1.341	6.260	1.192
4.354	1.200	4.494	1.649	4.634	1.600	4.774	1.554	4.914	1.211	5.570	1.336	6.270	1.189
4.356	1.700	4.496	1.648	4.636	1.599	4.776	1.554	4.916	1.210	5.580	1.333	6.280	1.187
4'350	1.608	4.490	1.047	4.030	1.599	4.778	1.553	4.918	1.510	5.590	1.331	6.200	1.185
4.362	1.697	4.502	1.646	4.642	1.597	4.782	1.552	4.920	1.508	5.000	1.329	6.310	1.181
4.364	1.697	4.204	1.645	4.644	1.597	4.784	1.551	4.926	1.507	5.620	1.324	6.320	1.179
4.366	1.696	4.506	1.645	4.646	1.596	4.786	1.520	4.930	1.506	5.630	1.322	6.330	1.177
4.300	1.095	4.500	1.044	4.040	1.595	4.700	1.550	4.940	1.203	5.640	1.320	6.340	1.176
4.372	1.694	4.512	1.642	4.652	1.202	4 790	1.549	4 950	1.402	5.660	1.317	6.360	1.174
4.374	1.693	4.214	1.642	4.654	1.593	4.794	1.548	4.970	1.494	5.670	1.313	6.370	1.170
4.376	1.692	4.216	1.641	4.656	1.203	4.796	1.242	4.980	1.491	5.680	1.310	6.380	1.168
4.378	1.001	4.518	1.040	4.058	1.592	4.798	1.547	4.990	1.488	5.690	1.308	6.390	1.167
4 300	1.600	4.522	1.639	4.662	1.201	4.802	1.540	5.010	1.482	5.710	1.300	6.410	1.105
4.384	1.689	4.524	1.638	4.664	1.590	4.804	1.545	5.020	1.480	5.720	1.301	6.420	1.161
4.386	1.688	4.526	1.637	4.666	1.589	4.806	1.544	5.030	1.477	5.730	1.299	6.430	1.159
4.388	1.687	4.528	1.637	4.668	1.589	4.808	1.544	5.040	I.474	5.740	1.297	6.440	1.158
4.390	1.686	4.530	1.635	4.672	1.587	4.812	1.543	5.050	1.471	5.750	1.294	0·450	1.150
4.394	1.685	4.534	1.635	4.674	1.587	4.814	1.542	5.070	1.465	5.770	1.290	6.470	1.152
4.396	1.685	4.536	1·634	4.676	1.586	4.816	1.541	5.080	1.462	5.780	1.288	6.480	1.150
4.398	1.684	4.538	1.633	4.678	1.585	4.818	1.540	5.090	1.460	5.790	1.286	6•490	1.149
4.400	1.082	4.540	1.032	4.682	1.585	4.820	1.540	5.100	1.457	5.800	1.284	6.510	1.147
4.404	1.682	4.544	1.631	4.684	1.583	4.824	1.538	5.120	1.451	5.820	1.279	6.520	1.143
4.406	1.681	4.546	1.630	4.686	1.583	4.826	1.538	5.130	1.448	5.830	1.277	6.530	1.142
4.408	1.680	4.548	1.630	4.688	1.582	4.828	1.537	5.140	1.446	5.840	1.275	6.540	1.140
4'410	1.679	4.550	1.629	4.690	1.281	4.830	1.537	5.150	1.443	5.850	1.273	6·550	1.138
4 412	1.678	4.554	1.628	4.692	1.580	4.834	1.535	5.170	1.440	5.870	1.268	6.570	1.137
4.416	1.677	4.556	1.627	4.696	1.579	4.836	1.535	5.180	1.435	5.880	1.266	6.580	1.133
4.418	1.676	4.558	1.626	4.698	1.579	4.838	1·534	5.190	1.432	5.890	1.264	6.590	1.131
4.420	1.676	4.560	1.625	4.700	1.578	4.840	1.533	5.200	1.429	5.900	1.262	6.610	1.130
4.422	1.674	4.564	1.624	4.702	1.577	4.842	1.533	5.220	1.427	5.020	1.258	6.620	1.120
4.426	1.673	4.566	1.623	4.706	1.576	4.846	1.532	5.230	1.421	5.930	1.256	6.630	1.125
4.428	1.673	4.568	1.623	4.708	1.576	4.848	1.231	5.240	1.418	5.940	1.254	6.640	1.123
4.430	1.672	4.570	1.622	4.710	1.575	4.850	1.530	5.250	1.416	5.950	1.252	6.650	1.122
4.432	1.671	4.574	1.621	4.712	1.574	4.052	1.520	5.200	1.413	5.900	1.250	6.670	1.120
4.436	1.670	4.576	1.620	4.716	- 574 I•573	4.856	1.528	5.280	1.408	5.980	1.245	6.680	1.117
4.438	1·669	4.578	1.619	4.718	1.572	4.858	1.528	5.290	1.405	5.990	1.243	6.690	1.115
4.440	1.668	4.580	1.618	4.720	1.572	4.860	1.527	5.300	1.403	6.000	1.241	6.700	1.113
4.442	1.008	4.582	1.019	4.722	1.571	4.864	1.527	5.310	1.400	6.020	1.239	6.720	1.112
4 444	1.666	4.586	1.616	4.726	1.570	4.866	1.525	5.330	1.395	6.030	1.235	6.730	1.108
4.448	1.665	4.588	1.616	4.728	1.569	4.868	1.525	5.340	1.392	6.040	1.233	6.740	1.107
4.420	1.665	4.230	1.615	4.730	1.568	4.870	1.524	5.350	1.300	6.050	1.231	6.750	1.102
4.452	1.662	4.592	1.014	4.732	1.568	4.872	1.524	5.360	1.387	0.000 6.070	1.229	6.760	1.103
4 4 5 4 4 5 6	1.663	4.596	1.613	4.736	1.566	4.876	1.522	5.380	1.382	6.080	1.225	6.780	1.100
4.458	1.662	4.598	1.612	4.738	1.566	4.878	2.522	5.390	1.380	6.090	1.223	6.790	1.099
4.460	1.661	4.600	1.612	4.740	1.565	4.880	2.521	5.400	I·377	6.100	1.221	6.800	1.092
4.462	1.000 1.000	4.002	1.011	4.742	1.565	4.882	2.521	5.410	1.375	0.110	1.219	0.810	1.001
4 404	1.620	4.604	1.610	4 /44 4.746	1.563	4.886	2.520	5.430	1.370	6.130	1.217	6.830	1.002
4.468	1.658	4.608	1.609	4.748	1.563	4.888	2.519	5.440	1.367	6.140	1.213	6.840	1.001
4.470	1.657	4.610	1.608	4.720	1.562	4.890	2.518	5.420	1.365	6.150	1.211	6.850	1.089
4.472	1.057	4.012	1.008	4.752	1.561	4.892	2.517	5.460	1.362	0.100	1.210	0.800 6.870	1.088
4 4/4	1.655	4.614	1.606	4 754	1.560	4.894	2.516	5.480	1.357	6.180	1.206	6.880	1.084
4.478	1.655	4.618	1.606	4.758	1.559	4.898	2.516	5.490	1.355	6.190	1.204	6.890	1.083

A and B Cor.	Reduc- tion,	A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion,	A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.	A and B Cor.	Redu c - tion,	A and B Cor.	Reduc- tion.
6.90	1.081	7.60	.983	8.60	·869	10.00		11.40	·657	12.80	• 585	14.20	.527
6.91	1.080	7.61	.981	8.62	•867	10.05	`747	11.45	.652	12.82	•584	14.35	·527
6.92	1.028	7.62	.980	8.64	.865	10.04	745	11.44	.654	12.84	:583	14'24	.526
6.01	1.077	7.03	.979	8.68	·803	10.08	744	11.40	·653	12.80	.582	14.20	.525
6.02	1.024	7.65	·076	8.70	.850	10.00	742 741	11 40	·651	12.00	.201	14 20	·524
6.96	1.022	7.66	·975	8.72	.857	10.15	.739	11.2	.650	12.02	.580	14.32	.523
6.97	1.021	7.67	.974	8.74	·855	10.14	.738	11.24	·649	12.94	.579	14.34	.522
6.98	1.020	7.68	.972	8.76	·853	10.10	.736	11.20	·648	12.96	•578	14.36	.522
6.99	1.068	7.69	·971	8.78	.852	10.18	.735	11.28	·646	12.98	·577	14.38	.251
7.00	1.000	7.70	.970	8.80	·850	10.50	.734	11.00	.645	13.00	• 576	14'40	.520
7'02	1.002	7.71	1909	8.8	1040	10.22	732	11.02	.644	13.02	575	14'42	-519
7.03	1.003	7.72	.066	8.86	-840	10 24	731	11 04	.643	13:04	572	14 44	.519
7.04	1.000	7.74	·065	8.88	·842	10.28	.728	11.68	·641	13.08	•573	14.48	.517
7.05	1.020	7.75	.964	8.90	.840	10.30	.726	11.40	.640	13.10	•572	14.50	.517
7.06	1.022	7.76	.962	8.92	.838	10.32	.725	11.72	639	13.15	.221	14.00	.213
7.02	1.020	7.77	·961	8.94	·836	10.34	.724	11.24	·638	13.14	.220	14.20	.210
7.08	1.024	7.78	·960	8.96	.832	10.36	.722	11.20	.637	13.10	.269	14.80	.206
7.09	1.023	7.79	.959	8.98	.833	10.38	.721	11.28	.636	13.18	568	14.90	.203
7.11	1.020	7.81	950 *056	9.00	1820	10 40	720	11.00	622	13 20	507	15.10	499
7.12	1.048	7.82	·055	0.04	.827	10 42	.717	11.02	.632	13.54	.200	15.20	490
7.13	1.047	7.83	·954	9.00	·825	10.40	.715	11.86	.631	13.50	.262	15'30	490
7.14	1.042	7.84	.953	9.08	·824	10.48	.714	11.88	·630	13.28	.564	15.40	·487
7.12	1.044	7.85	·952	0.10	·822	10.20	.713	11.00	·629	13.30	.263	15.20	•483
7.10	1.045	7.86	·950	9.15	·820	10.25	.711	11.05	·628	13.35	.262	15.60	·480
7.17	1.041	7.87	·949	9'14	.818	10.24	.210	11.94	.627	13.34	'561	15.70	.477
7.10	1.040	7.00	.012	9.10	·810	10.20	.709	11.08	·020	13.30	.201	15'80	474
7'20	1.032	7.00	947	9.10	-812	10 50	.706	11 90	.624	13.40	- 550	15.00	471
7'21	1.032	7'01	.044	9.22	.811	10.05	.705	12.02	.623	13'42	.558	10.10	465
7.22	1.034	7.92	.943	9.24	.809	10.64	.703	12'04	622	13.44	.557	16.30	•463
7'23	1.035	7.93	·942	9.26	·808	10.66	.702	12.00	·621	13.40	.556	16.30	·460
7.24	1.031	7'94	·941	9.28	.806	10.08	.701	13.08	·620	13.48	.226	16.40	. 457
7'25	1.030	7.95	.940	9.30	.804	10.20	·699	12.10	.619	13.20	555	10.20	454
7 20	1 020	7.90	.939	9'32	802	10.72	600	12.12	610	13.52	554	10.00	451
7.28	1.022	7.08	.036	9 34	.700	10.74	.606	12.14	-616	13 54	.552	10 /0	449
7.29	1.024	7.99	.035	9.38	.797	10.78	.601	12.18	615	13.28	.221	16.00	•443
7.30	1.023	8.00	.934	9.40	796	10.80	.693	12.30	·614	13.60	.221	17.00	·441
7.31	1.051	8.05	.935	9'42	'794	10.85	·692	12.35	·613	13.65	.520	17.10	·438
7'32	1.020	8.04	. 929	9'44	'792	10.84	.690	12.54	.612	13.64	•549	17.50	•436
7'33	1.012	8.00	·927	9.40	.791	10.80	.689	12.20	110.	13.00	:548	17.30	433
7.35	1.010	8.10	.022	9 40	.789	10.00	.687	12 20	.600	13.00	540	17 40	431
7.36	1.014	8.12	.020	9 50	.786	10.02	.685	12.32	·608	13.72	.546	17.60	.426
7.37	1.013	8.14	.918	9.54	.784	10.04	·684	12.34	.607	13.74	.545	17.70	.423
7.38	1.015	8.19	·916	9.26	.782	10.00	•683	12.36	606	13.46	.544	17.80	·421
7.39	1.010	8.18	.013	9.28	.481	10.08	•682	12.38	.602	13.28	.543	17'90	.410
7.40	1.000	8.20	.911	9.60	779	11.00	*680	12.40	.004	13.80	:543	18.10	410
7.42	1.009	8.24	.909	9.02	778	11.05	679	12.42	.003	13.95 13.95	542	18.30	414
7'43	1.002	8.26	1005	0.66	.774	11.04	.677	12°46	·601	13.86	·540	18.30	414
7.44	1.004	8.28	.002	9.68	1/4	11.08	.676	12.48	.600	13.88	.540	18.40	.407
7.45	1.005	8.30	.900	9.70	·771	11.10	·674	12.20	·599	13.00	.539	18 [.] 50	.405
7.46	1.001	8.32	·898	9.72	.770	11.13	.673	12.25	•598	13.92	.538	18.00	.403
7.47	.999	8.34	•896	9.74	.768	11.14	.672	12.24	.262.	13.94	537	18.70	' 401
7.48	.998	8.30	.894	9.76	.766	11.10	.671	12.20	•596	13.90	•536	19.90	399
7 49	997	8:40	-800	9.70	705	11.19	-070	12.20	595	13.99	530	10.00	397
7.51	.004	8.42	·888	0.82	.703	11.20	667	12:00	594	14.02	.534	10.10	394
7.52	.993	8.44	.885	9.84	.760	11.54	.666	12.64	*502	14.04	1533	19.20	.390
7.53	.992	8.46	·883	9.86	7.59	11.50	.665	12.66	.591	14.00	.533	19.30	·388
7.54	.990	8.48	·881	9.88	.757	11.58	·664	12.68	·591	14.08	•532	19'4 0	•386
7.55	.989	8.50	.879	9. 90	.756	11.30	·662	12.70	.200	14.10	·531	19.20	384
7.50	.988	8.52 8.5	·877	9.92	754	11.32	100.	12.72	:589	14.12	.530	19.00	382
7.58	1085	8.56	872	9.94	753	11.34	·000	12.74	-500	14 14 14.16	530	19.70	300
7.59	.984	8.58	·871	9.08	131	11.30	.658	12.78	•586	14.18	.528	20.00	375
		5-	-/-	5.55	150	30	~ <u>_</u>	/0	550	·· T **	5-0		5/5

Table showing the Hour-angle Limits within which the Error of the Reduction calculated by Ex-meridian Table No. 2 will not exceed 0.5'.

Γ						LAI	TT	UDE .	AND	DE	CLIN	ATI	ON	OF S/	AME	NA	ME.				
										D	ECLIN	ATIO	N.								
-	54	° 55	i° 5	6° 8	5 7 °	58	0	59°	6	30°	62	>	64°	66	1	38°	70	73	° 76	° 80°	85°
	о м D 72 2 71 4 68 5 66 8 63	. M 21 77 1 76 21 75 21 75 21 75 1 74	. N 7l 8 5l 8 5l 8 5l 8 5l 8 1 8 1 8	1. 6 <i>l</i> 1 3 <i>l</i> 1 3 <i>l</i> 1 3 <i>l</i> 1 3 <i>l</i> 1 3 <i>l</i> 1	м. 231 02 <i>l</i> 09 <i>l</i> 13 <i>l</i> 10 <i>l</i>	N 12 12 12 12 12 11	1. 8n 6n 2n 0n 8n	М. 130g 122g 116g 113g 110g		м. 10g 18g 04g 03g 99g	м. 98g 93g 90g 87g 84g	y 1	м. 91g 86g 84g 83g 80g	м. 81g 81g 77g 77g 76g		м. 80g 78 76 66 66 66 66	м. 78g 78g 77g 76g 76g	M 78 80 78 80 79 79 76	. м g 80 g 80 g 80 g 80 g 80 g 80 g 78	. M. g 85g g 85g g 85g g 85g g 85g g 84g	M. 102g 102g 102g 102g 101g
10 12 14 16 18	0 61 60 59 57 56	$\begin{array}{c c}l & 73 \\ 1 & 65 \\ l & 60 \\ l & 59 \\ l & 59 \\ l & 59 \end{array}$	l = 8: l = 70 l = 72 l = 72 l = 72	1/ 1 5/ 1 4/ 1 4/ 2/	08l 06l 04l 94l 85l	11. 110 100 100	4n 5n 8n 5n 2n	108g 106g 104g 104g 107g)6g)2g)2g)2g)2g	848 818 808 808 808		79g 78g 77g 76g 7 5 g	738 738 728 728 728 728	7 7 7 7 7 7 7 7	3g 3g 2g 2g 2g	758 738 738 728 728	75 75 75 75 74 74	g 776 g 766 g 766 g 766 g 766 g 766 g 746	g 84g g 84g g 84g g 84g g 84g g 83g	101g 101g 101g 100g 99g
20 22 24 26 28 30	54 52 49 45 45 43 39	$\begin{array}{c c c} l & 58 \\ 58 \\ 56 \\ 56 \\ 52 \\ 49 \\ 42 \\ 42 \end{array}$	l = 62 l = 60 l = 58 l = 54 l = 52 l = 46		76 <i>l</i> 72 <i>l</i> 64 <i>l</i> 55 <i>l</i> 51 <i>l</i>	100 88 73 65 61 54	57 37 37 37 37 37 37 37 37 37 37 37 37 37	106g 102g 98n 94l 77l 66l	9 9)2g)7g)0g)2g 8n 4l	80g 81g 82g 83g 84g 86g	7777	75g 74g 74g 72g 71g 73g	69g 69g 69g 69g 68g 68g	7 6 6 6 6 6	1 g 8g 8g 7g 7g 7g	69g 69g 68g 68g 67g 67g	74 70 70 70 68 67	g 748 g 738 g 728 g 728 g 728 g 728 g 728 g 728	g 83g g 82g g 80g g 80g g 80g g 79g g 78g	99g 98g 98g 98g 98g 98g
							- 1		INF	ERI	IOR 7	[RA]	NSI	г.	_						
		JOTI	7			at.			,]	Declin	ATIO	N.					
g si	gnifie	es tha	- - it tru	le re-			68°	7)°	72	• 7	′ 4 °	76	3° 7	′8°	80	0	82°	84 °	86°	88°
l si	duction than duction gnifie duction abula	on i tab on. s tha on is ar rec	s <i>gr</i> ular ular t tru <i>less</i> lucti	eater re- e re- than on.		° 4 6 8 0	м. 	N		м.	•	м. 	м	. 1	M. 	м. • •	•	м. 94g	M. 100g 100g	м. 107g 108g 108g	M. 128g 128g 128g 128g 129g
n si I I I	gnifie 10 err 0'5' w 10ur-a give A han a	es that or as ithin angle $\Delta \pm B$	t the grea limi w gre	ere is at as ts of hich ater	1 2 2 3	2 5 5 5 1 5 1 5	00 18 36	g 9 g 10 g 12 l 15	9g 4g 3g	90 100 106	g g g ic	 90g 97g	90 92 93	• • • • • • • • • • • • • • • • • • •	 90g 90g 94g	90 92 94 96 98	g g g g I I	94 <i>g</i> 94 <i>g</i> 96 <i>g</i> 98 <i>g</i> 00 <i>g</i>	100g 100g 102g 103g 104g	108g 108g 110g 112g 109g	130g 130g 130g 130g 130g
,	inum c	, 000	•		4	0 1	10		$\begin{bmatrix} -5\\ -n \end{bmatrix}$	150		4g	11	3g 10	8g	104		04g	100g 108g	112g 114g	130g
				I	ATI.	TUD	ΕA	AND 1	DECI	LINA	ATIO	N O	F C	ONTR.	ARY	NA	MES.				
at.]	Decli	NATI	ON.								
I	54°	55°	56°	5'	7° .	58°		59°	60	° .	62°	64	l°	66°	68	0	70°	73°	76 °	80°	85°
。 2 4 6 8	м. 72 <i>l</i> 70 <i>l</i> 70 <i>l</i> 70 <i>l</i> 70 <i>l</i> 70 <i>l</i>	м. 77l 77l 77l 76l 76l	м. 861 831 821 821 801	N 12 92 92 93 90 88	1. 3 <i>n</i> 4 <i>l</i> 3 <i>l</i> 3 <i>l</i> 3 <i>l</i>	м. 1281 122 114 106 97		M. 130g 134g 140g 142n 142 <i>l</i>	M. 110 120 130 136 150	g g g g g g	м. 98g 98g 102g 108g 113g	M 9 9 9 9	1. 1g 1g 2g 6g 0g	м. 81g 83g 84g 85g 86g	м 80 81 82 82	g g g g g g g g g	м. 78g 81g 81g 83g 83g 84g	м. 78g 81g 81g 81g 82g	м. 80g 82g 84g 84g 84g	м. 85g 88g 88g 90g 90g	м. 102g 104g 105g
10 12 14 16 18	70 <i>l</i> 70 <i>l</i> 69 <i>l</i> 69 <i>l</i> 68 <i>l</i>	75l 75l 73l 73l 73l 73l	80 <i>l</i> 78 <i>l</i> 76 <i>l</i> 75 <i>l</i> 75 <i>l</i>	86 85 83 81 79		92 <i>l</i> 90 <i>l</i> 87 <i>l</i> 86 <i>l</i> 84 <i>l</i>	I	091 031 961 921 901	154 131 110 102 98		120g 133g 145g 162g 178n	10 11 11 12 13	3g 0g 4g 4g 4g	89g 94g 104g 106g 109g	8: 8: 90 95		84g 86g 90g 93g 94g	82g 85g 88g 	85g 86g 	••• •• ••	
20 22 24 26 28 30	681 681 681 661 651 651	72 <i>l</i> 72 <i>l</i> 69 <i>l</i> 68 <i>l</i> 68 <i>l</i> 68 <i>l</i>	74l 73l 72l 72l 72l 72l 70l 70l	78 77 76 75 73 72		82 <i>l</i> 80 <i>l</i> 78 <i>l</i> 76 <i>l</i> 76 <i>l</i> 76 <i>l</i>		88 <i>l</i> 86 <i>l</i> 84 <i>l</i> 82 <i>l</i> 80 <i>l</i> 78 <i>l</i>	94 90 86 84 82		116 <i>l</i> 108 <i>l</i> 100 <i>l</i> 92 <i>l</i> 	150 140 110	og on on	120g 110n 	100		· · · · · · ·	· · · · · · ·	•••	· · · · · · · · · · · · · · · · · · ·	· · · · · · ·

A and B Cor.	Reduc- tion.												
1		1		1.1.00	1	1				6.			,
3.00	2.200	3.20	2.027	4'40	1.401	5.10	1.421	5.80	1.501	6.20	1.124	7.20	1.045
3.02	2.483	3.72	2.010	4'42	1.697	5.12	1.465	5.82	1.589	6.52	1.120	7.22	I.030
3.03	2.472	3.73	2.011	4'43	1.603	5.13	1.465	5.83	1.580	6.23	1.148	7.23	1.032
3.04	2.467	3.74	2.002	4'44	1.082	5.14	1.459	5.84	1.284	6.24	1.147	7.24	1.036
3.00	2 459	375	1.002	4 45	1.682	5.10	1.420	5.86	1.580	6.20	1 145	7.26	1'034
3.02	2.443	3.77	1.989	4.47	1.628	5.17	1.421	5.87	1.278	6.57	1.145	7.27	1.035
3.08	2.432	3.28	1.984	4.48	1.624	5.18	1.448	5.88	1.326	6.28	1.140	7.28	1.030
3.00	2.427	3.79	1.024	4'49	1.020	5.19	1.445	5.89	1.223	6.20	1.138	7.29	1.052
3.11	2'419	3.81	1.000	4 50	1.663	5'21	1 442	5'91	1.500	6.01	1.130	7.31	1.020
3.12	2.404	3.82	1.963	4.52	1.620	5.22	1.437	5.92	1.267	6.62	1.133	7.32	1.052
3.13	2.396	3.83	1.928	4.23	1.622	5.23	1°434	5.93	1.562	6.63	1.131	7.33	1.053
3.14	2.389	3.84	1.018	4.54	1.648	5'24	1.431	5.94	1.503	6.64	1.130	7'34	1.055
3.10	2 301	3 05	1 940	4 55	1.645	5 25	1 429	5.00	1.258	6.66	1.150	7.35	1'020
3.12	2.366	3.87	1.938	4.57	1.641	5.27	1.423	5.97	1.256	6.67	1.154	7.37	1.018
3.18	2.328	3.88	1.033	4.28	1.638	5.28	1.420	5.98	1.524	6.68	1.153	7.38	1.010
3.10	2.321	3.89	1.035	4.59	1'634	5.29	1.418	5.99	1.522	6.69	1.151	7.39	1.012
3.21	4 344 2°336	3.01	1.018	4.00	1.030	5.31	1.412	6.01	1.578	6.71	1.118	7.40	1.015
3.22	2.329	3.92	1.013	4.62	1.623	5.32	1.410	6.02	1.540	6.72	1.116	7.42	1.011
3.53	2.355	3.93	1.308	4.63	1.650	5'33	1.402	6.03	I'244	6.73	1.114	7.43	1.000
3.24	2.315	3.94	1.904	4.64	1.010	5.34	1.404	6.04	1.242	6.74	1.113	7.44	1.008
3 25	2.301	3.06	1.807	4.05	1.003	5 35	1 402	6.00	1.238	6.26	1.100	7 45	1.002
3.27	2.294	3.97	1.880	4.67	1.000	5.37	1.392	6.02	1.530	6.77	1.108	7.47	1.004
3.58	2.287	3.98	1.884	4.68	1.603	5.38	1.394	6.08	1.534	6.78	1.100	7.48	1.003
3.29	2'280	3.99	1.880	4.69	1.200	5.39	1.301	6.09	1.535	6.79	1.102	7.49	1.001
3.31	2.266	4.00	1.870	4.70	1 590	5'40	1.300	6.11	1.230	6.81	1.103	7.51	.000
3.32	2.259	4'02	1.866	4.72	1.280	5.42	1.384	6.13	1.552	6.82	1.100	7.52	·997
3.33	2.252	4.03	1.801	4.73	1.280	5'43	1.381	6.13	I.553	6.83	1.008	7.53	•996
3'34	2.246	4.04	1.856	4.74	1.285	5.44	1.379	6.14	1.551	6.84	1.002	7.54	.995
3.32	2 2 39	4.05	1.842	4 /5	1.220	5.45	1.320	6.12	1.518	6.86	1.002	7.55	·993
3.37	2.226	4.07	1.843	4.77	1.22	5.47	1.371	6.12	1.510	6 87	1.005	7.57	.991
3.38	2.510	4.08	1.838	4.78	1.260	5.48	1.369	6.18	1.514	6.88	1.000	7.58	•989
3.39	2.515	4.09	1.834	4.79	1.266	5.49	1.366	6.10	I.515	6.89	1.080	7.59	•988
3 40	2.100	4 10	1.829	4.81	1 503	5.20	1.304	6.21	1.508	6.01	1.082	7.00	·086
3.42	2.193	4.15	1.820	4.82	1.222	5.52	1.320	6.22	1.300	6.92	1.084	7.62	·984
3.43	2.187	4.13	1.810	4.83	1.223	5.23	1.326	6.23	1.504	6.93	1.085	7.63	.983
3.44	2.180	4'14	1.812	4.84	1.220	5.24	1.324	6.24	I'202	6.94	1.081	7.64	·982
3 45	2.174	4 15	1.803	4.86	1.540	5.22	1.321	6.52	1.108	6.06	1.079	7.05	·070
3.47	5.1 01	4.17	1.200	4.87	1.240	5.57	1.340	6.27	1.100	6.92	1.020	7.67	.978
3.48	2.122	4.18	1.204	4.88	1.232	5.28	1.344	6.28	1.194	6.98	1.024	7.68	.977
3.49	2.149	4'19	1.790	4.89	1.234	5.29	1.342	6.30	1.105	0.99	1.023	7.69	975
3.21	2.137	4 20	1.481	4 90	1.231	5.00	1.339	6'31	1.180	7 01	1.021	7.71	974 1973
3.25	2.131	4.22	1.777	4.92	1.24	5.62	1.332	6.32	1.187	7.02	1.068	.7.72	.972
3.23	2.125	4'23	1.773	4.93	1.251	5.63	1.335	6.33	1.182	7.03	1.062	7.73	.970
3.54	5.113	4'24	1.769	4.94	1.218	5.64	1.330	6°34	1.183	7.04	1.062	7.74	·969
3.22	2.107	4 4 2 5	1.402	4 95	1.212	5.02	1.327	6.32	1.120	7.05	1'062	775	·066
3.22	2.101	4.27	1.756	4.97	1.200	5.67	1.353	6.37	1.177	7.07	1.001	7.77	.965
3.28	2.095	4.28	1.752	4.98	1.200	5.68	1.320	6.38	1.120	7.08	1.020	7.78	·964
3.59	2.083	4'29	1.748	4'99	1.203	5.69	1.318	0°39	1.124	7.09	1.028	7.79	·963
3.01	2.078	4.31	1.740	5'01	1'497	570	1.313	6.41	1'170	7'11	1.022	7.81	.960
3.62	2.025	4'32	1.736	5.02	1'494	5.72	1.311	6.42	1.168	7.12	1.023	7.82	.959
3.63	2.066	4'33	1.732	5.03	1'491	5.73	1.300	6.43	1.160	7.13	1.025	7.83	· 958
3 04	2.000	4.34	1.728	5.04	1'488	5.74	1.302	0°44 6'45	1'105	7.14	1.020	7.85	·957
3.66	2.040	4.30	1.720	5.00	1 405	5.76	1.304	6.40	1.101	7.10	1'049	7.86	955
3.67	2.044	4'37	1.716	5.07	1.479	5.77	1.300	6.47	1.120	7.17	1.046	7.87	953
3.68	2.038	4.38	1'712	5.08	1.476	5.78	1.298	6.48	1.122	7.18	1.042	7.88	·952
3 09	2 033	4 39	1.708	5.09	1.423	5'79	1.502	0.49	1.120	7.19	1.043	7.09	951

A and B Cor,	Reduc- tion.	A and B Cor.	Reduc- tion,	A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.						
7.00	•040	8.60	.877	0.30	.806	10.00	.750	10.70	.701	11:40	.6=8	12:20	.61-
7.91	•949	8.61	·871	9.31	·806	10.01	•749	10.71	.700	11.40	.657	12.20	.614
7.92	.947	8.62	·870	9.32	.805	10.02	•749	10.72	•700	11.42	·657	12.24	·613
7.93	•946	8.63	•869	9.33	•804	10.03	•748	10.73	•699	11.43	•656	12.26	.612
7.94	·945	8.65	·868 ·867	9.34	·803	10.04	.747	10.74	·698	11.44	·656	12.28	•611
7.06	·943	8.66	•866	9.36	·801	10.09	•746	10.75	.693	11.45	•654	12.30	.600
7.97	•941	8.67	·865	9.37	•800	10.07	.745	10.77	•696	11.47	.654	12.34	.608
7.98	•940	8.68	•864	9.38	•800	10.08	•744	10.78	•696	11.48	·653	12.36	.607
7·99 8·00	·939	8.69	·863	9.39	·799	10.00	7.43	10.79	·695	11.49	·653	12.38	·606
8.01	·936	8.71	·861	940	•797	10.10	•742	10.81	·694	11.50	·652	12.40	·604
8.02	·935	8.72	·860	9.42	•796	10.13	•741	10.82	•693	11.52	.651	12.44	.603
8.03	•934	8.73	·859	9.43	.795	10.13	•740	10.83	·693	11.23	.650	12.46	•602
8.04	·933	8.74	·858	9.44	·794	10.14	•740	10.84	·692	11.54	•650	12.48	•601
8.06	·932	8.76	·856	945	.794	10.19	.738	10.86	·691	11.55	•6.10	12.50	.500
8.07	·929	8.77	·855	9.47	.792	10.17	.737	10.87	•690	11.57	.648	12.54	•598
8.08	·928	8.78	·854	9•48	•791	10.18	•737	10.88	·689	11.58	•648	12.56	•597
8.09	·927	8.79	•853	9.49	•790	10.19	•736	10.89	•689	11.59	•647	12.58	•596
8.10	·920	8.81	·851	9.50	·789	10.20	•735	10.00	·687	11.00	•646	12.00	·595
8.12	.924	8.82	·850	9.52	.788	10.22	.734	10.92	.687	11.62	.645	12.64	.593
8.13	·923	8.83	·849	9.53	.787	10.23	•733	10.93	•686	11.63	.645	12.66	.592
8.14	·921	8.84	*848	9.54	•786	10.24	•732	10.94	•686	11.64	•644	12.68	.201
8·15 8·16	·920	0°05 8·86	·847	9.55	.705	10.25	•732 •731	10.02	·085	11.65	·044	12.70	·591
8.17	·918	8.87	·846	9.57	.784	10.20	•730	10.97	.684	11.67	•643	12 72	.589
8.18	.917	8.88	·845	9.58	.783	10.28	.730	10.98	·683	11.68	.642	12.76	·588
8.19	·916	8.89	•844	9.59	•782	10.29	•729	10.99	•682	11.69	•642	12.78	·587
8.20	·915	8.01	·843	9.00	.781	10.30	.728	11.00	·082	11.70	·641	12.80	·586
8.22	·912	8.92	·841	9.62	.780	10.32	.727	11.02	.681	11.72	.640	12.84	.584
8.23	.911	8.93	·840	9.63	.779	10.33	•726	11.03	•680	11.73	·639	12.86	·583
8.24	.910	8.94	·839	9.64	•778	10.34	•725	11.04	•679	11.24	•639	12.88	·582
8.25	·909	8.95	·838	9·65	.777	10.35	.725	11.05	·679	11.75	·638	12.90	.581
8.27	·907	8.97	·836	9.67	.776	10.30	.723	11.07	.678	11.70	.637	12.92	•580
8.28	·906	8.98	·835	9.68	.775	10.38	.723	11.08	.677	11.78	·637	12.96	.579
8.29	·905	8.99	·834	9.69	.774	10.39	.722	11.09	•676	11.79	·636	12.98	·578
8.30	•904	9.00	•833	9.70	.773	10.40	.721	11.10	·676	11.80	•636	13.00	•577
8.32	·001	9.01	·831	9.71	.772	10.41	.720	11.11	·674	11.82	•635	13.02	.575
8.33	·900	9.03	·831	9·73	·771	10.43	.719	11.13	.674	11.83	.634	13.06	.574
8.34	·899	9.04	•830	9.74	.770	10.44	.718	11.14	·673	11.84	·633	13.08	·573
8.35	•898	9.05	•829	9.75	•769	10.45	.718	11.15	•673	11.85	•633	13.10	•573
8.30	·897	9.00 0.07	.827	9.70 0.77	.768	10.40	.716	11.10	·671	11.90	·032	13.12	·572
8.38	·895	9.08	·826	9·78	.767	10.48	.716	11.18	.671	11.88	.631	13.16	.570
8.39	·894	9.09	·825	9.79	•766	10.49	.715	11.19	·670	11.89	·631	13.18	·569
8.40	•893	9.1 0	·824	9.80	•765	10.50	.714	11.20	·070	11.00	•630	13.20	•568
8.42	·801	0.12	·822	0.82	.764	10.51	.714	II·21	•668	11.02	.620	13.22	•566
8.43	.890	9.13	·821	9.83	.763	10.53	.712	11.23	.668	11.93	.629	13.26	·566
8.44	·889	9.14	·821	9.84	•762	10.24	.712	11.24	•667	11.94	•628	13.28	·565
8.45	·888	9.15	•820	9·85	•761	10.55	•711	11.25	•667	11.95	•628	13.30	•564
8.40	·887	9·10 0·17	·819	0.87	.760	10.50	•710	11.20	•665	11.90	·027	13.32	.503
8.48	·884	9·18	·817	9·88	.759	10.58	.709	11.28	•665	11.98	·626	13.36	.561
8.49	·883	9.19	·816	9.89	•758	10.29	•708	11.29	•664	11.99	•626 1	1 3•38	·561
8.50	•882	9.20	·815	9.90	•758	10.60	.708	11.30	•664	12.00	•625	13.40	•560
8.52	-880	9·21 0·22	·813	0.05	.756	10.01	•706	11.31	*662	12.02	.623	13.42	559
8.53	.879	9.23	.813	9.93	.755	10.63	.706	11.33	·662	12.06	.622	-3 44 13•46	.557
8.54	·878	9.24	.812	9.94	•755	10.64	.705	11.34	·661 :	12.08	·621	13.48	.556
8.55	•877	9.25	·811	9.95	.754	10.65	.704	11.35	•661	12.10	•620	13.20	.556
8.57	·876	9.20	·810	9.90	•753	10.00	•704 •70	11.30	•000 :	12.12	·019	13.52	·555
8.58	.874	9.28	.808	9.98	.752	10.68	.702	11.38	•659	12.16	.617	13.56	.553
8.59	.873	9•29	.807	9.99	•751	10.69	•702	11.39	•658	12.18	•616	13.58	.552

Showing the Reduction at 1 min. from the Meridian corresponding to the A and B Corrections given on Pages 12 to 37 of this Work.

A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.	A and B Cor.	Reduc- tion.
· · · ·		1		20,60			1-1			1	-		,
13.00	.551	17.10	·439	20.00	·304 ·363	24.50	·305	31.50	•238	45.20	·166	77.0	·097
13.70	·547	17.20	•436	20.70	·362	24.70	•304	31.20	•237	45.60	•165	79.0	.090
13.75	•545	17.25	.435	20.75	•361	24.80	.302	31.80	·236	45.80	·164	80.0	.094
13.80	•543	17.30	•434	20.80	•361	24.90	•301	32.00	·234	46.00	•163	81.0	.093
13.85	•542	17.35	•432	20.85	•360	25.00	•300	32.20	•233	46.20	•162	82.0	•091
13.90	·540	17.40	•431	20.00	•359	25.10	·299	32.40	•232	40.40	·162	83.0	·090
13 95	•536	17.50	43° •429	21.00	•357	25.30	•296	32.80	•220	40.00	•160	85.0	·089
14.05	·534	17.55	•427	21.05	·356	25.40	·295	33.00	•227	47.00	•160	86.0	.087
14.10	•532	17.60	•426	21.10	•355	25.20	•294	33.20	•226	47.20	·1 59	87.0	·086
14.12	•530	17.65	•425	21.15	•355	25.60	•293	33.40	•225	47.40	•158	88.0	·085
14.20	•528	17.70	•424	21.20	*354	25.70	•292	33.00	•223	47.00	•158	89.0	·084
14.20	•524	17.80	•443	21.20	·353	25.00	•2.00	33.00	•221	47.00	•156	90.0	·082
14.35	.523	17.85	•420	21.35	•35I	26.00	·289	34.20	•219	48.20	·156	92.0	·082
14.40	.521	17.90	.419	21.40	·351	26.10	·287	34.40	·218	48.40	·155	93.0	·081
14.42	•519	17.95	.418	21.45	·350	26.20	•286	34.60	·217	48.60	•154	94.0	•080
14.20	•517	18.00	·417	21.50	•349	26.30	·285	34.80	•216	48.80	·154	95.0	·079
14.55	•515	18.10	•410	21.55	•348	26.50	·284	35.00	•214	49.00	•153	90.0	·078
14.00	.512	18.15	4-4	21.65	-347	26.60	·282	35.10	•212	49.20	·1 52	08.0	+077
14.70	.510	18.20	•412	21.70	•346	26.70	·281	35.60	·211	49.60	·151	99.0	.076
14.75	.508	18.25	411	21.75	•345	26.80	·280	35.80	·210	49.80	·151	100.0	·075
14.80	•507	18.30	.410	21.80	•344	26.90	·279	36.00	•208	50.00	·1 50	110.0	•068
14.85	•505	18.35	·409	21.85	•343	27.00	•278	36.20	•207	50.20	•149	120.0	•063
14.90	•503	18.40	•408	21.90	*343	27.10	·277	36.40	·200	50.40	•149	130.0	•058
14.95	.502	18.50	•407	22.00	•344	27.20	•270	26.80	•205	50.00	•148	140.0	*050
15.05	·498	18.55	•404	22.05	•340	27.40	•274	37.00	·203	51.00	•147	160.0	•047
15.10	.497	18.60	•403	22.10	.339	27.50	.273	37.20	·202	51.20	·147	170.0	·044
15.15	•495	18.65	402	22.12	•339	27.60	•272	37.40	- 201	51.40	•146	180.0	•042
15.20	•493	18.70	·401	22.20	·338	27.70	•27I	37.60	•200	51.60	·145	190.0	·039
15.25	·492	18.75	·400	22.25	*337	27.80	•270	37.80	·198	51.80	•145	200.0	·038
15.30	•490	18.85	-399	22.30	•330	27.90	·209	38.20	.19/	52.00	•144	220.0	.030
15.40	•487	18.00	•397	22.40	•335	28.10	.267	38.40	.195	52.40	•I43	230.0	.033
15.45	•485	18.95	·396	22.45	.334	28.20	·266	38.60	.194	52.60	·143	240.0	·0.3I
15.20	•484	19.00	•395	22.50	•333	28.30	·265	38.80	·193	52.80	·142	250.0	•030
15.55	·482	19.05	•394	22.55	•333	28.40	•264	39.00	·192	53.00	·142	260.0	·029
15.00	.481	19.10	.393	22.60	·332	28.50	•203	39.20	•191	53.20	•141	270.0	·028
15.70	•479	1915	·301	22.05	•331	28.00	·202	39.40	.180	53.40	•140	200.0	.026
15.75	•476	19:25	•390	22.75	•330	28.80	·260	39.80	·188	53.80	·I 39	300.0	.025
15.80	.475	19.30	.389	22.80	.329	28.90	•260	40.00	·188	54.00	·139	320.0	.023
15.85	•473	19.35	·388	22.85	•328	29.00	.259	40.20	·187	54.40	•I 38	340.0	·022
15.90	·472	19.40	•387	22.90	•328	29.10	·258	40.40	•186	54.80	·137	360.0	·021
15.95	·470	19.45	.380	22.95	·327	29.20	·257	40.00	•185	55.20	.130	300.0	·020
16.05	•467	19.55	.384	23.05	·325	29.30	·255	40.00	·183	56.00	·131	420.0	.018
16.10	•466	19.60	·383	23.10	·325	29.50	·254	41.20	•182	57.00	·I 32	440.0	·017
16.15	•464	19.65	·382	23.15	·324	29.60	·253	41.40	·181	58.00	·129	460.0	·016
16.20	.463	19.70	.381	23.20	•323	29.70	·253	41.60	•180	59.00	·127	480.0	.010
16.25	·462	19.75	.380	23.25	•323	29.80	•252	41.80	·179	61.00	·125	500.0	·015
16.30	.400	19.80	379	23.30	•322	29.90	·251	42.00	·179	62.00	123	540.0	·014
16.40	*457	10.00	.377	~ 3· 33 23·40	·321	30.10	·240	44 20	·177	63.00	.119	560.0	·013
16.45	.456	19.95	·376	23.45	.320	30.20	·248	42.60	176	64.00	·117	580.0	·013
16.50	.455	20.00	·375	23.50	.319	30.30	·248	42.80	·175	65.00	115	600.0	·013
16.55	' 453	20.02	•374	23.55	.319	30.40	247	43 ^{.co}	·174	66.00	·II4	650.0	·012
16.67	·452	20.10	.373	23.60	•318	30.20	•246	43.20	·174	68.00	·II2	700.0	·011
16.05	450	20.15	·372	23.05	·317	30.00	-245	43.40	•173	60.00	·100	800+0	.000
16.75	•448	20.25	.370	23.80	-315 -315	30.80	·244	43.80	·171	70.00	·107	900.0	.008
16.80	•446	20.30	.370	23.90	·314	30.90	·243	44.00	·171	71.00	·106	0000	·008
16.85	•445	20.35	·369	24.00	.313	31.00	•242	44.20	·170	72:00	·104	200.0	•006
16.90	•444	20.40	·368	24.10	.311	31.10	·24I	44.40	•169	73'00	·103	1 500 ·O	.005
10.95	·442	20.45	•367	24.20	.310	31.20	•240	44.00	·108	74.00	101	2500.0	·004
17.05	441	20.50	+365	24.30	*307	31.30	·230	44 00	.167	75.00	.000	3000.0	.003
		3- 33	., .,	~+ +~	., 71	+	171	T.J 22	/ 1		22		.7.

11-Azimuth.

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TABLE M.

Error in Latitude due to an Error of 4 Seconds in Time or 1' of Longitude.

uth.							LAT	ITUI	DE.							
Azim	0°	5°	10°	15°	18°	20°	22°	24°	26°	28°	30°	32°	34°	36°	38°	4 0°
°2 4 6 8 10	, •03 •11 •14 •18	, •03 •07 •10 •14 •18	, 07 •10 •14 •17	, •03 •07 •10 •14 •17	, .03 .07 .10 .13 .17	·03 ·07 ·10 ·13 ·17	, .03 .06 .10 .13 .16	, •03 •10 •13 •16	, •03 •06 •09 •13 •16	, •03 •06 •09 •12 •16	, •03 •06 •09 •12 •15	, •03 •06 •09 •12 •15	, .03 .06 .09 .12 .15	, •03 •06 •09 •11 •14	, .03 .06 .08 .11 .14	, .03 .05 .08 .11 .14
12	·21	·21	·21	·21	·20	·20	·20	·19	·19	·19	·18	•18	·18	·17	·17	·16
14	·25	·25	·25	·24	·24	·23	·23	·23	·22	·22	·22	•21	·21	·20	·20	·19
16	·29	·29	·28	·28	·27	·27	·27	·26	·26	·25	·25	•24	·24	·23	·23	·22
18	·32	·32	·32	·31	·31	·31	·30	·30	·29	·29	·28	•28	·27	·26	·26	·25
20	·36	·36	·36	·35	·35	·34	·34	·33	·33	·32	·32	•31	·30	·29	·29	·28
21	·38	·38	·38	·37	·37	•36	·36	·35	·35	·34	·33	·33	·32	·31	·30	·29
22	·40	·40	·40	·39	·38	•38	·37	·37	·36	·36	·35	·34	·33	·33	·32	·31
23	·42	·42	·42	·41	·40	•40	·39	·39	·38	·37	·37	·36	·35	·34	·33	·33
24	·45	·44	·44	·43	·42	•42	·41	·41	·40	·39	·39	·38	·37	·36	·35	·34
25	·47	·46	·46	·45	·44	•44	·43	·43	·42	·41	·40	·40	·39	·38	·37	·36
26	·49	·49	·48	·47	·46	·46	·45	·45	·44	·43	·42	·41	·40	·39	·38	·37
27	·51	·51	·50	·49	·48	·48	·47	·47	·46	·45	·44	·43	·42	·41	·40	·39
28	·53	·53	·52	·51	·51	·50	·49	·49	·48	·47	·46	·45	·44	·43	·42	·41
29	·55	·55	·55	·54	·53	·52	·51	·51	·50	·49	·48	·47	·46	·45	·44	·42
30	·58	·58	·57	·56	·55	·54	·54	·53	·52	·51	·50	·49	·48	·47	·45	·44
31	·60	·60	·59	58	·57	·56	·56	·55	·54	·53	·52	·51	·50	·49	·47	·46
32	·62	·62	·62	•60	·59	·59	·58	·57	·56	·55	·54	·53	·52	·51	·49	·48
33	·65	·65	·64	•63	·62	·61	·60	·59	·58	·57	·56	·55	·54	·53	·51	·50
34	·67	·67	·66	•65	·64	·63	·63	·62	·61	·60	·58	·57	·56	·55	·53	·52
35	·70	·70	·69	•68	·67	·66	·65	·64	·63	·62	·61	·59	·58	·57	·55	·54
36	·73	·72	·72	·70	·69	·68	·67	·66	·65	·64	·63	·62	·60	•59	·57	·56
37	·75	·75	·74	·73	·72	·71	·70	·69	·68	·67	·65	·64	·62	•61	·59	·58
38	·78	·78	·77	·75	·74	·73	·72	·71	·70	·69	·68	·66	·65	•63	·62	·60
39	·81	·81	·80	·78	·77	·76	·75	·74	·73	·72	·70	·69	·67	•66	·64	·62
40	·84	·84	·83	·81	·80	·79	·78	·77	·75	·74	·73	·71	·70	•68	·66	·64
41	·87	·87	·86	·84	·83	·82	•81	·79	·78	·77	·75	·74	·72	·70	·69	·67
42	·90	·90	·89	·87	·86	·85	•83	·82	·81	·79	·78	·76	·75	·73	·71	·69
43	·93	·93	·92	·90	·89	·88	•86	·85	·84	·82	·81	·79	·77	·75	·73	·71
44	·97	·96	·95	·93	·92	·91	•90	·88	·87	·85	·84	·82	·80	·78	·76	·74
45	I·00	I·00	·98	·97	·95	·94	•93	·91	·90	·88	·87	·85	·83	·81	·79	·77
46	1.05	1.03	1.02	1.00	·98	•97	·96	·95	·93	·91	·90	-88	·86	•84	·82	·79
47	1.07	1.07	1.06	1.04	1·02	1•01	·99	·98	·96	·95	·93	-91	·89	•87	·84	·82
48	1.11	1.11	1.09	1.07	1·06	1•04	1·03	1·01	1·00	·98	·96	-94	·92	•90	·88	·85
49	1.15	1.15	1.13	1.11	1·09	1•08	1·07	1·05	1·03	1·02	I·00	98	·95	•93	·91	·88
50	1.19	1.19	1.17	1.15	1·13	1•12	1·10	1·09	1·07	1·05	I·03	1-01	·99	•96	·94	·91
51	1.23	I·23	1·22	1.19	I·17	1.16	I·I4	1.13	1.11	I·09	1.07	1.05	1.02	1.00	·97	·95
52	1.28	I·28	1·26	1.24	I·22	1.20	I·I9	1.17	1.15	I·I3	1.11	1.09	1.06	1.04	1·01	·98
53	1.33	I·32	1·31	1.28	I·26	1.25	I·23	1.21	1.19	I·17	1.15	1.13	1.10	1.07	1·05	1·02
54	1.38	I·38	1·36	1.33	I·31	1.29	I·28	1.26	1.24	I·22	1.19	1.17	1.14	1.11	1·08	1·05
55	1.43	I·42	1·41	1.38	I·36	1.34	I·32	1.30	1.28	I·26	1.24	1.21	1.18	1.16	1·13	1·09
56	1·48	1·48	1·46	1·43	I·41	1·39	1·37	1·35	1·33	1·31	1·28	1·26	1·23	I·20	1.17	1·14
57	1·54	1·53	1·52	1·49	I·46	1·45	1·43	1·41	1·38	1·36	1·33	1·31	1·28	I·25	1.21	1·18
58	1·60	1·59	1·58	1·55	I·52	1·50	1·48	1·46	1·44	1·41	1·39	1·36	1·33	I·29	1.26	1·23
59	1·66	1·66	1·64	1·61	I·58	1·56	1·54	1·52	1·50	1·47	1·44	1·41	1·38	I·35	1.31	1·27
60	1·73	1·73	1·71	1·67	I·65	1·63	1·61	1·58	1·56	1·53	1·50	1·47	1·44	I·40	1.36	1·33
61	1.80	1.80	1.78	I·74	1.72	1.71	1.67	1.65	1.62	1.59	1.56	1.53	1.50	1·46	1·42	1·38
62	1.88	1.87	1.85	I·82	1.79	1.77	1.74	1.72	1.69	1.66	1.63	1.59	1.56	1·52	1·48	1·44
63	1.96	1.95	1.93	I·90	1.87	1.84	1.82	1.79	1.76	1.73	1.70	1.66	1.63	1·59	1·55	1·50
64	2.05	2.04	2.02	I·98	1.95	1.93	1.90	1.87	1.84	1.81	1.78	1.74	1.70	1·66	1·62	1·57
65	2.14	2.14	2.11	2·07	2.04	2.02	1.99	1.96	1.93	1.89	1.86	1.82	1.78	1·74	1·69	1 64
66	2·25	2·24	2·21	2·17	2·14	2·11	2.08	2.05	2.02	1.98	1.95	1·90	1.86	1.82	1·77	1·72
67	2·36	2·35	2·32	2·28	2·24	2·21	2.18	2.15	2.12	2.08	2.04	2·00	1.95	1.91	1·86	1·80
68	2·48	2·47	2·44	2·39	2·35	2·33	2.30	2.26	2.22	2.19	2.14	2·10	2.05	2.00	1·95	1·90
69	2·61	2·59	2·57	2·52	2·48	2·45	2.42	2.38	2.34	2.30	2.26	2·21	2.16	2.11	2·05	2·00
70	2·75	2·74	2.71	2·65	2·61	2·58	2.55	2.51	2.47	2.43	2.38	2·33	2.28	2.22	2·16	2·10

TABLE M.

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Error in Latitude due to an Error of 4 Seconds in Time or 1' of Longitude.

uth.		LATITUDES														
Azim	42°	44°	46°	48°	49°	50°	51°	-52°	53°	54°	55°	56°	57°	58°	59°	60°
° 2 4 6 8 10	, •03 •05 •08 •10 •13	, •03 •05 •08 •10 •13	, •02 •05 •07 •10 •12	, •02 •05 •07 •09 •12	, •02 •05 •07 •09 •12	, •02 •04 •07 •09 •11	, •02 •04 •07 •09 •11	, •02 •04 •06 •09 •11	, •02 •04 •06 •08 •11	, •02 •04 •06 •08 •10	, •02 •04 •06 •08 •10	, •02 •04 •06 •08 •10	, •02 •04 •06 •08 •10	, •02 •04 •06 •07 •09	•02 •04 •05 •07 •09	·02 ·03 ·05 ·07 ·09
12	•16	·15	•15	•14	•14	•14	·13	•13	•13	·12	·12	•12	·12	•11	•11	•11
14	•19	·18	•17	•17	•16	•16	·16	•15	•15	·15	·14	•14	·14	•13	•13	•12
16	•21	·21	•20	•19	•19	•18	·18	•18	•17	·17	·16	•16	·16	•15	•15	•14
18	•24	·23	•23	•22	•21	•21	·20	•20	•20	·19	·19	•18	·18	•17	•17	•16
20	•27	·26	•25	•24	•24	•23	·23	•22	•22	·21	·21	•20	·20	•19	•19	•18
21	·29	·28	·27	·26	·25	·25	·24	·24	·23	·23	·22	·21	·21	·20	·20	·19
22	·30	·29	·28	·27	27	·26	·25	·25	·24	·24	·23	·23	·22	·21	·21	·20
23	·32	·31	·29	·28	·28	·27	·27	·26	·26	·25	·24	·24	·23	·22	·22	·21
24	·33	·32	·31	·30	·29	·29	·28	·27	·27	·26	·26	·25	·24	·24	·23	·22
25	·35	·34	·32	·31	·31	·30	·29	·29	·28	·27	·27	·26	·25	·25	·24	·23
26	·36	·35	·34	•33	·32	•31	•31	·30	•29	•29	·28	·27	·27	·26	·25	·24
27	·38	·37	·35	•34	·33	•33	•32	·31	•31	•30	·29	·28	·28	·27	·26	·25
28	·40	·38	·37	•36	·35	•34	•33	·33	•32	•31	·30	·30	·29	·28	·27	·27
29	·41	·40	·39	•37	·36	•36	•35	·34	•33	•33	·32	·31	·30	·29	·29	·28
30	·43	·42	·40	•39	·38	•37	•36	·36	•35	•34	·33	·32	·31	·31	·30	·29
31	·45	·43	·42	•40	·39	·39	·38	·37	·36	·35	·34	·34	·33	·32	•31	·30
32	·46	·45	·43	•42	·41	·40	·39	·38	·38	·37	·36	·35	·34	·33	•32	·31
33	·48	·47	·45	•43	·43	·42	·41	·40	·39	·38	·37	·36	·35	·34	•33	·32
34	·50	·49	·47	•45	·44	·43	·42	·42	·41	·40	·39	·38	·37	·36	•35	·34
35	·52	·50	·49	•47	·46	·45	·44	·43	·42	·41	·40	·39	·38	·37	•36	·35
36	·54	·52	·50	•49	•48	•47	•46	·45	•44	•43	•42	•41	·40	·39	·37	·36
37	·56	·54	·52	•50	•49	•48	•47	·46	•45	•44	•43	•42	·41	·40	·39	·38
38	·58	·56	·54	•52	•51	•50	•49	·48	•47	•46	•45	•44	·43	·41	·40	·39
39	·60	·58	·56	•54	•53	•52	•51	·50	•49	•48	•46	•45	·44	·43	·42	·40
40	·62	·60	·58	•56	•55	•54	•53	·52	•51	•49	•48	•47	·46	·44	·43	·42
41	·65	·63	•60	•58	•57	•56	•55	•54	•52	•51	•50	·49	·47	•46	·45	*43
42	·67	·65	•63	•60	•59	•58	•57	•55	•54	•53	•52	·50	·49	•48	·46	*45
43	·69	·67	•65	•62	•61	•60	•59	•57	•56	•55	•53	·52	·51	•49	·48	*47
44	·72	·69	•67	•65	•63	•62	•61	•59	•58	•57	•55	·54	·53	•51	·50	*48
45	·74	·72	•69	•67	•66	•64	•63	•62	•60	•59	•57	·56	·54	•53	·52	*50
46	•77	•74	·72	·69	•68	•67	·65	•64	•62	·61	•59	•58	·56	·55	·53	·52
47	•80	•77	·74	·72	•70	•69	·67	•66	•65	·63	•62	•60	·58	·57	·55	·54
48	•83	•80	·77	·74	•73	•71	·70	•68	•67	·65	•64	•62	·60	·59	·57	·56
49	•85	•83	·80	·77	•75	•74	·72	•71	•69	·68	•66	•64	·63	·61	·59	·58
50	•89	•86	·83	·80	•78	•77	·75	•73	•72	·70	•68	•67	·65	·63	·61	·60
51	•92	·89	•86	•83	·81	•79	•78	•76	•74	•73	•71	•69	·67	·65	·64	·62
52	•95	·92	•89	•86	·84	•82	•81	•79	•77	•75	•73	•72	·70	·68	·66	·64
53	•99	·95	•92	•89	·87	•85	•84	•82	•80	•78	•76	•74	·72	·70	·68	·66
54	1•02	·99	•96	•92	·90	•88	•87	•85	•83	•81	•79	•77	·75	·73	·71	·69
55	1•06	1·03	•99	•96	·94	•92	•90	•88	•86	•84	•82	•80	·78	·76	·74	·71
56	I·10	1.07	1.03	·99	·97	·95	·93	·91	·89	•87	•85	•83	•81	•79	•76	·74
57	I·14	1.11	1.07	1·03	1·01	·99	·97	·95	·93	•91	•88	•86	•84	•82	•79	·77
58	I·19	1.15	1.11	1·07	1·05	1·03	1·01	·99	·96	•94	•92	•89	•87	•85	•82	·80
59	I·24	1.20	1.16	1·11	1·09	1·07	1·05	1·02	1·00	•98	•95	•93	•91	•88	•86	·83
60	I·29	1.25	1.20	1·16	1·14	1·11	1·09	1·07	1·04	1•02	•99	•97	•94	•92	•89	·87
61	1·34	1·30	1.25	1·21	1.18	1.16	1·14	1.11	1.09	1.06	1.05	1.01	•98	·96	·93	·90
62	1·40	1·35	1.31	1·26	1.23	1.21	1·18	1.16	1.13	1.11	1.08	1.05	1•02	1·00	·97	·94
63	1·46	1·41	1.36	1·31	1.29	1.26	1·24	1.21	1.18	1.15	1.13	1.10	1•07	1·04	1·01	·98
64	1·52	1·47	1.42	1·37	1.34	1.32	1·29	1.26	1.23	1.21	1.18	1.15	1•12	1·09	1·06	1·03
65	1·59	1·54	1.49	1·43	1.41	1.38	1·35	1.32	1.29	1.26	1.23	1.20	1•17	1·14	1·10	1·07
66	1.67	1.62	1.56	1.50	1·47	1·44	1·41	1·38	1·35	1·32	1·29	1·26	1·22	1·19	1.16	1·12
67	1.75	1.69	1.64	1.58	1·55	1·51	1·48	1·45	1·42	1·38	1·35	1·32	1·28	1·25	1.21	1·18
68	1.84	1.78	1.72	1.66	1·62	1·59	1·56	1·52	1·49	1·45	1·42	1·38	1·35	1·31	1.27	1·24
69	1.94	1.87	1.81	1.74	1·71	1·67	1·64	1·60	1·57	1·53	1·49	1·46	1·42	1·38	1.34	1·30
70	2.04	1.98	1.91	1.84	1·80	1·77	1·73	1·69	1·65	1·61	1·58	1·54	1·50	1·46	1.41	1·37

POSITION OF SHIP FROM TWO SUN EX-MERIDIAN OBSERVATIONS, USING A AND B EX-MERIDIAN TABLES AND LOGARITHMS.

1917.—On January 21st, a.m. at ship, in lat. by D.R. 8° o' N. and long. 74° 22' E., when a chronometer indicated M.T. Green. 20 d. 17 h. 33 m. 51 s., the true altitude of sun's centre was $52^{\circ} 34'$ S.; and again on same afternoon when chronometer indicated 20 d. 21 h. 1 m. 21 s., the true altitude of sun's centre was $52^{\circ} 12'$ S., the ship having made $52\frac{1}{2}$ miles on a true N. 79° W. course during the interval between the observations. Required the position of ship at time of 2nd observation, and prove work by two different methods.

TIMI. OUSCIDATION DATIMAL OF LA-MOTATION I GOL	A.M.	ObservationLatitude	by	Ex-meridian	Tables
--	------	---------------------	----	-------------	--------

M.T. Green, 2 Long. 74° 22' E.	н. м. s. 20 17 33 51 + 4 57 28	Decl. (21st) 33·2" × 6·5 h.	19 57 56 S. + 3 36	Eq. T. •71 s. × 6•5 l	M. S. II 23.4 n.— 4.6	T. alt $-\ominus$ -Redn.	5 ² 34.0 + 9 13.7	s.
M.T. ship Eq. of time	22 31 19 - 11 10	Cor. dl.	20 I 32 S.	Cor. Eq. T.	11 18.8	Mer. alt.	61 47.7	-
A.T. ship	22 20 0	2 1				M.Z.D. Decl.	28 12·3 20 1·5	N S.
H.A. Decl. $20^{\circ} \frac{11}{2}'$ Alt. $52^{\circ} \frac{34'}{4}$	I 40 0	Sin. 9.6259 Cos. 9.9729 Sec. 0.2162	Run N.	$79^{\circ} \text{ W. } 52\frac{1}{2} = 51 \cdot 5' \text{ W.} =$	10.0' N. 52' W.	Lat. Run	8 10.8	N.
Azim, S. 40° 47' E. B 1·17' which g	gives A and ives (p. 75)	Sin. 9.8150				Lat. at tim 2nd obsn	e of 8 20.8	N.
(p. 145) Redn. at \times 100 m. = R	1 m. 5.537' Redn. 553.7,	Az. 40° 47'	Long. Run	74 22 52	••о Е. 2•о W.			
= 9 13.7.			Long. a 2nd o	t time of 73 30	POE.			
	,							

P.M. Observation.-Ex-meridian Latitude by Spherical Calculation.

M.T. Gree Long. 73°	n. 30' E.	D, 20 +	н. 21 4	м. 1 54	s. 21 0		T. a	lt. –⊖–	<u>5</u> 2 1	2.0	s.	D V	ecl. ar. 3	(21st 3·2″) × 3 h	. 1 9 . +	57 50 I 40	5 S.	Eq Va	. T. r. •7	(215 1 S.	t) ×`3 h.	M. 11 —	s. 23°4 2·1
M.T. ship Eq. time		21		55 11	21 21		<i>u</i> .y.	-	3/ 4		•	C	or. d	ecl.		19	593	5 S.	Co	r. Eo	1. Ť	·	11	21.3
						1											For	Azı	muth.					
A.T. ship Decl. 19°	(H.A.) 59' 36"	s.	I	44	ο.	Co Co	s. ot.	9·9536 0·4390	6. 19.	. •	:	: :	:	: :	•		Sin Cos	· 9· · 9·	64184 97300					
Arc. (1)	° ′ 22 2	18 S				. Co	t.	0.3937	5				Al	t. 52	° 12'		Sec	e.⁺o	•21261			Cot.	9.88	8968
Arc. (2)	29 52	14 N	ι.					-		Α	zim	. S. 4	2° 1	3' 52	″ W.	,	Sir	1. 9	82745			Cos.	9.86	5949
Latitude	749	56 N														A	c. (2)	29	° 52' :	14″ I	٩.	Tan	9.7	5917

As a Check on the Work the Ex-meridian Table No. I may be used.

Lat. 7° 50 N. DI. 20 0 S. H.A. Th. 44m. $C. \underline{1112}$ S. gives position-line N. 48° W. and redn. at 1 min. 5.753' × 104 m. = Redn. 598'3' = + 9° 58'3'

7.0	° (°)	Positic	on on Chart.
Z.D. Redn.	$-\frac{37}{9}\frac{48.0}{58.3}$	Lat.	8 5.8 N.
M.Z.D. Decl.	27 49.7 N. 19 59.6 S.	Long.	73 12.4 E.
Latitude	7 50·1 N.		

With Long. at time of 2nd obsn.	73 30 E.	Gives position on Chart
Lat. (I) ,, ,, (2) ,,	8 20°8 N. ∫ 7 50°0 N. ∫	Lat. 8 5'8 N.
EXAMPLE FROM PREVIOUS PAGE WORKED FROM TWO LONGITUDE CALCULATIONS.

	A.M. 0	Observation.			P.M. Observatio	2.	
M.T. Green. Eq. time A.T. Green.	L. H. M. S. 20 17 33 51 11 19 20 17 22 32	True alt. $-\ominus$ - Decl. $2\dot{c}$	5°_{2} 3°_{4} S.	M.T. Green. Eq. time A.T. Green.	H. M. S. 21 I 21 - II 21·3 20 49 59·7	True alt. Decl.	52 12.0 S. 19 59 36 S.

Run N. 79°	' W. 52½ m.	= 10'0' N.	51.2'	=52.0'	w.
------------	-------------	------------	-------	--------	----



Position by chart Lat. 8° 5'8 N. Long. 73° 12'2' E.

• T 4

$\begin{array}{cccc} A & 5^{\circ} & 1^{\circ} & 0 \\ L & 8 & 10 & 0 \end{array}$	Sec. 0.00443		H. M. S.	
P 109 59 36	Cosec. 0.02700	A.T. ship	I 42 29.7	
170 21 26		A.1. Green.	20 49 59.7	A •30 S. B •84 S
		Long. in time	4 52 30 E.	
$ \begin{array}{c} S \\ S \\ -A \\ 3^2 \\ 5^8 \\ 4^8 \end{array} $	Cos. 8·92441 Sin. 9·73588	Longitude	73° 7′ 30″ E.	C^2 1.14 S. gives posnline S. 48.7° E.
H.A. 1h. 42m. 29.75.	Sin.2 8.69172			

Worked without the aid of Chart.

P.M. Observation.

Long. (1)	73 17∙0 E.	A & B 1.16S. to	o W.
,, (2)	73 7∙5 E.	,, 1.14S. to	o E.
Diff. long.	9.5	\div $2 \cdot 30 = I$	Lat. Cor. 4.1'S × 1 Long. Cor. 4.7' E.
Lat. (2)	8 10.0 N.	Long. (2)	73 7.5 E.
Cor.	4.1 S.	Cor.	4.7 E.
Lat. in	8 5·9 N.	Long. in	73 12·2 E.

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Example from 2nd edition of "Calculated Hour-angles and Ex-meridian Tables," &c., by H. S. Blackburne, giving a true position from a right-angle cross of two sun observations less than 5 minutes from noon.

POSITION FROM TWO EX-MERIDIAN OBSERVATIONS OF SUN WITH ALTITUDES LESS THAN 11° FROM ZENITH.

1917.---March 19th, in approximate position in lat. 0° and long. 45° W., with the following observations find the position of ship at time of second observation :-

H. M. s. (A.M. at ship) M.T. Greenwich 3 2 51 T. alt. of --- 88 41 S.Ed. (P.M. at ship) 9 27 88 47.4 S.Wd. 3 Run in interval between observations West. 11 miles.





This example as an extreme case where both altitudes were near the zenith, and the D.R. position considerably in error illustrates clearly the errors which would result from considering the position-lines as straight lines; the resulting position being 0° 27.7' N. and 44° 46.8' W. A perfectly true position, however, is obtained by the method here shown.

On the meridian of 45° W. lat. (1) was found to be 0° 12.2' S. when sun bore S. 72° E. with

Z.D. 79'. On the meridian of 45° W. lat. (2) was found to be 0° 32 0' N. when sun bore S. 18° W. with Z.D. 72.6'.

In such an extreme case, if inconvenient to adopt this method, a second calculation could very quickly be made by the use of the ex-meridian table with a new hour-angle deduced from the approximate longitude obtained by the first calculation. When nearly under the sun the longitude is seldom likely to be much in error as the sun would be close to the prime vertical during almost the whole day.

DOUBLE PROOF OF CORRECTNESS OF POSITION AS DETERMINED BY THE METHOD AND CALCULATION OF PREVIOUS EXAMPLE.

The following is a very good and simple way of proving the accuracy of double altitude observations, viz. :-

With the resulting *longitude* deduce a new hour-angle, and recalculate the latitude by a true method from both observations. If both latitudes are the same as from previous determinations it is a good guarantee of the correctness of position; or

With the resulting *latitude* recalculate the longitude from both observations. If they both agree with previous results we may rely with confidence on the correctness of the calculations, but of course this will not guarantee the correctness of position if a wrong altitude has been observed or a wrong declination used in the calculations.

A.M. Observation.				P.M. Observation.				
A.T. Green. Long. 44° 37'2' W.	н. м. s. 2 54 54 2 58 29			A.T. Green. Long. 44° 38·7′ W	н. м. s. 3 I 30 V. 25835			
A.T. Sp.	23 56 25			A.T. Sp. West Alt.	0 2 55 88° 47.4'	Sin. Sec.	8·1047 8·6754	
H.A. East Alt.	0 3 35 88° 41'	Sin. Sec.	8·1941 1·6387	Azim. S. 37° 4' W.	gives Redn.	Sin.	6.7801	
Azim. S. $42^{\circ} 53' E. 8$ at 1 m. = $5 \cdot 89'$ = Red. 21.1'.	gives Redn. ′×3.58 m.	Sin.	9.8328	$\min = \operatorname{Red}$	14.7'.			

FOR DETERMINATION OF	LATITUDES.
----------------------	------------

True alt. ⊙	88 41.0 S.	True alt. ⊙	88 47.4 S.
Redn.	+ 21.1	Redn.	+ 14.7
Mer. alt.	89 2.1	Mer. alt.	89 2.1
M.Z.D.	o 57·9 N.	M.Z.D.	0 57 9 N.
Decl.	o 37·0 N.	Decl.	0 37 0 N.
Latitude	0 20.9 N.	Latitude	0 20.9 N.

DETERMINATION OF LONGITUDES:

A L P	88 41 0 21 90 37	Sec. Cosed	0.0000 C. 0.0000	A L P	88 47 24 0 21 0 90 37 0		
	179 39				179 45 24		1
$\stackrel{\rm S}{\rm s}$ – A		Cos. Sin.	7·4849 8·2994	S – A	89 52 42 1 5 18	Cos. Sin.	7·3270 8·2786
H.A. oh	. 3 m. 34°5 s.	Sin^2	5.7843	H.A. oh. 2	m. 54 6 s.	Sin^2	5.6056
	A.T. Shir A.T. Gree	en.	H. M. S. 23 56 25.5 26 54 54.0	A.T. Ship A.T. Green.	H. M. S. 0 2 54 3 1 30	5	
	Long. in	time	2 58 28.5	Long. in tim	e 2 58 35.	1	
	Longitud Run	e	44° 37·1′W. 1·5 W.	Longitude	44° 38.8'	<u>v</u> .	
Longitud	e at time of 2	nd obsn	. 44° 38.6' W.				

NOTE.-The determination of latitude by the use of Table VIII should only be nade within the limits of time given in Tables VII or VIIA, as it will not give a true result outside these limits.

"SUMNER" POSITION FROM A.M. AND P.M. SUN OBSERVATIONS NEAR THE MERIDIAN.

1898.—On August 31st, in lat. by D.R. $7^{\circ} 42'$ N., long. $73^{\circ} 50'$ E. Obsd. alt. of \bigcirc 's L.L. (a.m. at ship) was 88° 50' N. when a chronometer indicated M.T.G. 30 d. 19 h. 2m. 53 s., and again (p.m.) the obsd. alt. of \bigcirc 's L.L. was 88° 44' when chronometer indicated M.T.G. 30 d. 19 h. 7m. 57 s. Run in interval, N. 80° W., 1m., gives 0.2' N., 1.0' W. Height of eye, 35 ft. Required, posn. of ship by "Sumner's" method from ex-meridian tables.

		A.M. Observatı	0n.	
M.T. Green. Long. 73° 50' E	D. H. M. S. 30 19 2 53 4 55 20	Obsd. alt. ⊙'s L.L. Cor. 35 ft. (p. 87)	88 50 N Ed + 10	Decl. 31st $8^{\circ}33^{\circ}$ N 54'4" \times 5 h. + 4 32
M.T. at ship Eq. time	23 58 13 - 13	True alt⊖- Red ⁿ	89 0'0 + 7'8	Decl. 8 37 32 N
A.T. Sp.	23 58 0	Mer ⁿ Alt.	89 7 [.] 8N	м. s. Eq. of time o 9 '36 '78 s. × 5 h. + 3'9
H.A.	E. 2 0			Cor. Eq. T. 0 13'26

For Azimuth and Reduction.

H.A.	2 m.	Sin.	7'9408	Mern Alt.	89 7.8 N
Alt.	89°	Sec.	1.7581	M.Z.D.	0 52'2 S
Az.	29° 3712'	Sin.	9.6940	Lat.	7 45 2 N
s (p.	40) A & B	1'78' g	ives (p. 75)	Run.	2 N

For the Latitude.

7 45'5 N

Lat. at time of 2nd Obsn

give and (p. 146) Redⁿ at 1 min. $3.92' \times 2$ m. = Redn 7.8'.

P.M. Observation.

M.T Long	. Green. 3. 73° 49' E	в. 30 +	н. м s. 19 7 57 4 55 16	For the Lati	tude.
M.T Eq.	. at Sp. T.	31	0 <u>3</u> 12 — 13	Obsd. alt. ⊙'s L.L. 35 ft. cor.	88 44N Wd + 10
Ä.T.	Sp.	31	0 3 0	T. altO-	88 54 N
H.A.			W. <u>3</u> 0	Redn	+ 17'3
	East A	~i		Mern Alt.	89 11'3 N
	FOF A.	stmutn;-		 M.Z.D.	0 48.7 S
H.A.	3 m.	Sin.	8.1160	Decl.	8 37 5 N
Alt.	8° 37±' 88° 54'	Sec.	9'9951 1'7168	Latitude	7 48.8 N
Az.	42° 24'	Sin.	9.8288		

gives (p. 40) A & B 1'11' gives (p. 37) position-line for plane chart N 48° E, or S 48° W., and (p. 145) Redⁿ at i min. 5.76' × 3 m. = Reduction 17'3'



NOTE .- The long by chron at 2nd observation, calculated with this lat. found from the two observations, was 73° 46′ 30″ E., and the lat. reworked from the H.A. resulting from this long. was 7° 47' N.

POSITION BY CHRONOMETER AND EX-MERIDIAN OBSERVATIONS OF SUN AND MOON.

1898.—On March 30th, at about 1 h. 24 m. p.m., at ship, observed alt. of \mathbb{C} 's U.L. was 27° 57' east of meridian when a chronometer indicated M.T.G. 2 h. 18 m. 57 s., and after running on an east course 2 miles the \odot 's L.L. was observed to be 32° 51' when the chronometer indicated 2 h. 26 m. 35 s. Lat. by D.R. 58° 2½' N., long. 12° 30' W., height of eye 35 ft.

		1st Obse	rvation, c.				
M.T. Green Sid. T. (G. noon) Accl. 2 h. 19 m.	D. H. M. S. 30 2 18 57 + 31 34.8 + 22.8	Obsd. alt. C's U.L. Dip. 35 ft.	$ \begin{array}{r} 27 57 0 \\ - 5 50 \\ \hline 27 51 10 \end{array} $	A L P	$\begin{array}{c} 28 & 22\frac{1}{2} \\ 58 & 2\frac{1}{2} \\ 66 & 15 \end{array}$	Sec. Cosec.	0*27630 0*03843
Sid. T. Green.	2 50 54.6	Semi-d.	- 14 58	·	152 40		
		App. alt. \mathfrak{q} 's centre Cor. T. (39, Raper) H.P. 54' 16"	27 36 12 + 46 1 5	$\frac{S}{S} - A$	76 20 47 57 ¹ / ₂	Cos. Sin.	9°37341 9°87079
g's R.A. 2 hrs. 2'13 s. × 19 m.	H. M. S. 6 55 51.6 + 40.5	T. alt. \mathfrak{C} 's centre	28 22 27	Н.А. ∉'s R.A.	н.м.s. 456 о 65632'1	Hav.	9'55893
Cor. R.A.	6 56 32.1	A	•459 S.	Sid. T. Sp. Sid. T. G.	2 0 32°I 2 50 54°6		
α's decl. 2 hrs. 5*44″ × 19 m.	° 46 57 N. - I 43	C gives A	•001 S.	Long. Run	⁵⁰ 22 ⁵ ¹² 35 38 W. 3 48 E.		
Cor. decl.	23 45 14 N.			Long. at 2nd obsn.	12 31 50 W.		•
P.D.	66 14 46 N.			Long. in time	50 ^m . 7'3 ^s .		•
		Run east $2 \text{ m.} = \text{d.}$ le	ong. 3.8' E.				

2nd Observation, ⊙.

LAT. BY EX-MERIDIAN TABLE NO. 2.

By reference to page 152 it will be seen that with a low latitude and high declination this table may be used without appreciable error to about 2 hours from the meridian. Therefore, by transposing lat. and dec. the same wide range may be obtained. The example below illustrates this case.

M.T.G. Long. W	2 26 35 - 50 7'3	Obsd. alt. of ⊙'s L.L. 35 ft. cor. (p. 87)	32 51 S. + 9	⊙'s de c l. 58°2″ × 2°4 hrs.	3 53 21 N 2 20 N
M.T. Sp. Eq. T.	I 36 27'7 - 4 27'0	T. alt. Red ⁿ .	33 0°0 S. 2 55°2	Cor. decl.	3 55 41 N.
H.A.	1 32 0.7	Mer. alt.	35 55.2		N S
Lat. (dec.) Dec. (lat.)	3 56 N A '16 S. 58 0 N B 4 10 N.	M.Z.D. Decl.	54 4°8 N. 3 55°7 N.	Eq. time *76 s × 2*4 hrs.	4 28.8 - 1.8
	C 3.94 N. gives (p. 15	Lat.	58 0°5 N.	Cor. Eq. T.	4 27'0

 $1'904' \times 92 \text{ m.} = 175'168' = 2^{\circ} 55'2' \text{ red}^{n}$.

CORRECTNESS OF WORK BY THE ABOVE METHODS WITH EX-MERIDIAN TABLE NO. 2 PROVED BY RIGOROUS CALCULATION.

н м

H.A. Decl.	^I 32 3° 55' 41" N	Cos. Cot.	9*964026 1*163267	Cosec.	1*164289
Arc (1)	4 15 58 N	Cot.	1*127293	Sin.	8.871502
		⊙'s alt.	33° 0'	Sin.	9.736109
" (2)	53 44 30 N.	• •		Cos.	9.771900
Lat.	58 0 28 N.				

As the moon was on the prime vertical when the altitude was taken, the time deduced from this observation should be absolutely correct, and the latitude by ex-meridian of the sun will also be correct without any additional work.

See note on page 117 about correcting moon's semidiameter and horizontal parallax for Greenwich date.

POSITION OF SHIP FROM COMBINED EX-MERIDIAN OBSERVATIONS OF TWO STARS, USING STAR-REDUCTION AND AZIMUTH EX-MERIDIAN TABLES.

1917.—On March 26th, soon after sunset, at about 6h. 5m. and 6h. 12m. p.m., in approximate latitude 18° S., and longitude D.R. 3° 36' W., the true altitude of * Capella was 24° 5' N.Wd., when chronometer showed M.T.G. 6h. 24 m. 18 s., and after running N. 45° W. $1\frac{1}{2}$ miles the true altitude of * Sirius was 87° 10 $\frac{1}{2}'$ N.Ed. when chronometer showed 6h. 31 m. 17s. Required, the position of ship at 2nd observation. Run N. 45° W. 1.5 m. = 1.0' N. I'I'W.

* CAPELLA TO NORTH-WESTWARD.

M.T. Green. Long. 3° 36' W.	н. м. s. 6 24 18 -0 14 24	★ 's Alt. Redn.	$24^{\circ} 50^{\circ} N.$
M.T. Ship	6 9 54	Mer. alt.	26 14.1
Accl.	+ 1 3	M.Z.D. Decl.	63 45.9 S. 45 55.1 N
Sid. T. Ship ¥'s R.A.	6 24 23 5 10 35	Lat.	17 50.8 S.
* 's H.A. W.	I I3 48	Lat. at time of 2nd obsn.	17 49.8 S.
Gives (p. 210*)	Redn 2° ort'		

and Azim. N. 14° W.

For Position-line on Plane Chart. Az. N. 14° W. gives (Table IV, p. 260*) lat. var. 17.0 s., which gives (p. 270*) posn-line S. 76.8° W.

D LUL	0			•	/
Position on chart	77	5T 14 S	and	2	4 2 · # W
- obtion on onalt	÷/	5140.	ana	5	43 5
True position	17	STIT S		2	4 2+2 W
at do posteron	÷/	.11 1 0.		· ·	4 3 3 11 4

* SIRIUS TO NORTH-EASTWARD.

M.T.G. Long. 3° 37' W	H. M. S. 6 31 17 14 28	∗ 's Alt. Redn.	87 10:5 N. + 1 23.8
M.T. Sp.	6 16 49	Mer. alt.	88 34.3
Accl.	+ I 4	M.Z.D.	I 25.7 S.
S.T. Sp. *'s R.A.	6 31 19 6 41 31	Latitude	18 2.0 S.
∗' s H.A. E.	0 10 12	Sin. 8.6	483
Decl. 16 Alt. 87	36·3 S. 10·5 N.	Cos. 9.9 Sec. 1.3	815 073
		Sin. 9.9.	371

Azim. N. 59° 54'E. gives (p. 291*) Redn. at 1 min. 8.22' × 10.2 m. = Redn. 83.8'

1° 23.8'

For Position-line on Plane Chart. Az. N. 59.9° E. gives (p. 258*) lat. var. 2.44 s., which gives (p. 270*) posn.-line N. 31.4° W.



* Page references to "Tables of Calculated Hour-angles," &c., by Blackburne. 2nd Edition.

Extract of Azimuth Ex-meridian Table, from Blackburne's New Book.

ıde.							AZI	MUTI	HS.						
Latitı	。 58·6	。 58·7	。 58·8	。 58·9	。 59·0	。 59•1	。 59·2	。 59·3	59·4	。 59•5	。 59·6	59·7	。 59·8	。 59·9	。 60·0
			R	EDUCTI	ON TO	THE	Meric	DIAN A	т Нот	UR-ANG	GLE OI	7 I MI	N.		
°0 2 4 6 8 9	8·42 8·41 8·40 8·37 8·34 8·31	8·43 8·43 8·41 8·39 8·35 8·33	8·45 8·45 8·43 8·43 8·41 8·37 8·35	8·47 8·46 8·45 8·42 8·39 8·37	8·49 8·48 8·47 8·47 8·44 8·40 8·38	8.50 8.50 8.48 8.46 8.42 8.40	8.52 8.52 8.50 8.47 8.44 8.42	8.54 8.53 8.52 8.49 8.46 8.43	8.56 8.55 8.54 8.51 8.47 8.45	8.57 8.57 8.55 8.53 8.49 8.47	8.59 8.58 8.57 8.54 8.51 8.48	8.61 8.60 8.59 8.56 8.52 8.50	8.63 8.62 8.61 8.58 8.54 8.54	8.64 8.64 8.62 8.60 8.56 8.54	8.66 8.65 8.64 8.61 8.58 8.55
10 11 12 13	8·29 8·26 8·23 8·20	8.31 8.28 8.25 8.22	8.32 8.30 8.27 8.23	8·34 8·31 8·28 8·25	8·36 8·33 8·30 8·27	8·37 8·35 8·32 8·29	8·39 8·37 8·34 8·30	8·41 8·38 8·35 8·32	8·43 8·40 8·37 8·34	8·44 8·42 8·39 8·35	8·46 ·8·43 8·40 8·37	8·48 8·45 8·42 8·39	8·49 8·47 8·44 8·40	8·51 8·48 8·45 8·45 8·42	8·53 8·50 8·47 8·44
14 15 16 17 18	8.17 8.13 8.09 8.05 8.01	8·18 8·15 8·11 8·07 8·02	8.20 8.16 8.12 8.08 8.04	8.22 8.18 8.14 8.10 8.05	8·23 8·20 8·16 8·12 8·07	8·25 8·21 8·17 8·13 8·09	8.27 8.23 8.19 8.15 8.10	8.29 8.25 8.21 8.17 8.12	8.30 8.26 8.22 8.18 8.14	8·32 8·28 8·24 8·20 8·15	8·34 8·30 8·26 8·22 8·17	8.35 8.31 8.27 8.23 8.19	8·37 8·33 8·29 8·25 8·20	8·39 8·35 8·31 8·27 8·22	8.40 8.36 8.32 8.28 8.28 8.24

EXAMPLE FROM PREVIOUS PAGE WORKED FROM TWO CALCULATED LONGITUDES AND PLOTTED ON PLANE CHART.

		* CAPELIA TO N.WD		*	SIRIUS TO N.ED.	
	M.T.G. M. ⊙'s R.A.	H. M. S. 6 24 18 True A 0 14 29	$\frac{24}{24} \frac{5}{5}$	M.T.G. 6 31 M. O's R.A. 0 14	17 True alt.	87 1012
	Sid. T.G.	6 38 47		Sid. T.G. 6 45	47	
		Run	N. 45° W. 1.5 m. =	= 1'0' N. 1'1' W.		
A. L. P.	$\begin{array}{c} 24 & 5 & 0 \\ 17 & 49 & 0 \\ 135 & 55 & 6 \\ \hline 177 & 49 & 6 \end{array}$	Sec. 0.0213 Cosec. 0.1576	A. $\cdot 96 \text{ N.}$ B. $3 \cdot 24 \text{ N.}$	A. 87 10 30 L. 17 48 0 P. 73 23 42 178 22 12	Sec. 0.0213 Cosec. 0.0185	A. 6.86 N. B. 6.38 S.
5. 5 — A	88 54 33 64 49 33	$\begin{array}{c} \text{Cos.} & 8 \cdot 2796\\ \text{Sin.} & 9 \cdot 9567 \end{array}$	C. <u>4.20 N.</u> Gives posnline S. 76.6° W.	S. $89 \text{ II } 6$ S - A $2 \text{ o } 36$	$\begin{array}{c} \text{Cos.} & 8 \cdot 1530 \\ \text{Sin.} & 8 \cdot 5450 \\ \end{array}$	C. 0.48 N. Gives posn-line S. $25\frac{1}{2}^{\circ}$ E.
	*'s H.A. We *'s R.A. Sid. T. Ship	$\begin{array}{c} \text{Sin.}^2 & 8.4132 \\ \text{H. M. S.} \\ \text{est} & \text{I 14 15} \\ 5 & 10 35 \\ \hline 6 24 50 \\ 6 & 6 \\ \end{array}$		*'s H.A. *'s R.A. Sid. T. Sh	$\begin{array}{r} \text{Sin.}^2 & 6.7378 \\ \text{H. M. S.} \\ \text{East} & -0 & 10 & 43 \\ 6 & 41 & 31 \\ \text{ip} & 6 & 30 & 48 \\ \text{resp.} & 6 & 45 & 47 \end{array}$	
	Long. in tim	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		Long. in t	$\frac{0}{14} \frac{43}{59} \frac{44}{59} \frac{44}{45} \frac{45}{7} V$	V.
	Long at time	$= of 2nd \qquad \frac{1}{3} \frac{5}{30} \frac{1}{21} W.$		Position of	on chart 17 51.1S.	and 3 43.3 W.

obs... NOTE.—To get accurate results with so high an altitude when working from the meridian the D.R. longitude should not be more than 5' or 6' in error if the azimuth is large, or when working from a parallel of latitude the D.R. latitude should not be much in error when the azimuth is small. The slight error $(o_4^{1'})$ in latitude from the ex-meridian observation is due to neglect to interpolate in the reduction table for * Capella for 10' of error in the D.R. latitude, and the o_3' of error in the longitude is due to curvature in the position-line in $12\frac{1}{2}'$ of arc, with a small Z D.

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POSITION OF SHIP BY COMBINED OBSERVATIONS OF SUN AND PLANET VENUS. LONGITUDE AND EX-MERIDIAN OBSERVATIONS.

1917.—December 29th, p.m. at ship, in approximate latitude 30° S., the true altitude of sun's centre was 52° 3' when a chronometer (corrected) indicated M.T.G. 1 h. 51 m. 58 s., and about the same time the true altitude of planet Venus (centre) was 74° 43' N. when chronometer (corrected) indicated M.T.G. 1 h. 53 m. 15 s. Run in interval N. 41° W. 0.3 m. = d. long. o' 15" W. Required, position of ship at time of second observation.

O P.M. Observation for Longitude.	Planet Venus. Ex-merida	ian for Latitude.
M. T. Green. Eq. time $\begin{array}{c} H. M. S. \\ I 51 58 \\ -2 2 \\ A. T. Green. \end{array}$ True alt. $-\Theta - \begin{array}{c} 5^{\circ} 2 & 3 \\ -2 & 3 \\ Decl. \end{array}$ True alt. $-\Theta - \begin{array}{c} 5^{\circ} 2 & 3 \\ -2 & 3 \\ -2 & 3 \\ -2 & 5 \\ -2 & 3 \\ -2 & 5 \\ -2 & 3 \\ -2 & 5 \\ -2 & 3 \\ -2 & 5 \\ -2 & 3 \\ -2 & 5 \\ -2 & 3 \\ -2 & 5 \\ -2 & 3 \\ -2 & 5 \\ -2 $	$ \begin{array}{c} \text{M.T. Green.} & \text{H. M. S.} \\ \text{Sid. T.G. noon} & \text{IS 39 } 28 \cdot 7 \\ \text{Accl.} & + 18 \cdot 6 \\ \text{Sid. T. Green.} & \text{20 } 23 & 2 \cdot 3 \\ \text{Long. E.} & 0 & 58 & 6 \cdot 7 \\ \text{Sid. T. Sp.} & 21 & 21 & 9 \cdot 0 \\ \text{Sid. T. Sp.} & 21 & 21 & 9 \cdot 0 \\ \text{Sid. T. Sp.} & 21 & 31 & 39 \\ \end{array} $	True alt. of $*$ 7^4 43° o N. Reduction $+$ 11° 5 Mer. alt. 74 54° 5 M.Z.D. 15 5° 5 S. Decl. 15 4° 8 S. Lat. 30 10° 3 S.
$\begin{array}{c} & By \ Black burne's \ Hour-angle \ Tables.\\ Lat. \ 30 \ 0S.\\ Decl. \ 23 \ 15S.\\ Alt. \ 52 \ 3\end{array} \right) \begin{array}{c} S.\\ Dl. \ var. \ +1'56 \ \times \ 15 = +23'40\\ Alt. \ var. \ -4'62 \ \times \ 3 = -13'86\end{array}$	*'s H.A. 10 30 E.	
Cor. to Tabular H.A. + 9.54 H. M. H. M. D. 23 S. Gives H.A. 24 S. Cor. A T. Skin	For Azim. and	Reduction.

м. s. 1030 155 7443	Sin. Cos. Sec.	8.6609 9.9848 0.5791
' E. gives cor. 6.80' Redn. at 1.10' × Reduction	Sin.	9.2248
	M. S. 10 30 15 5 74 43 ' E. gives cor. 6.80' Redn. at 1.10' × Reduction	M. S. 10 30 Sin. 15 5 Cos. 74 43 Sec. 'E. gives Sin. cor. 6.80' Redn. at 1:10' × Reduction

	Latitude by	Spheric	al Calculation.					
H.A.	M. S. 10 30	Cos.	9.999544				Tru	e Position.
D1.	ı5 4 4 ⁸	Cot.	0.569527	Cosec.	0.584747		Lat.	30 10.3 S.
Arc. (1)	15 5 42 ¹ / ₂ S.	Cot.	0.269071	Sin.	9.415679		Long.	14 31.7 E.
		Alt.	74° 43′	Sin.	9•984363			· ·
,, (2)	15 4 33 S.			Cos.	9.984789	$\gamma = \gamma + \epsilon$		
Lat.	$30 10 15^{\frac{1}{2}}$ S.							

NOTE.—As the sun was on the prime vertical when the observation for longitude was taken 10' of error in the latitude worked with makes no difference in the longitude; the hour-angle deduced from this longitude for calculation of ex-meridian would be correct, and consequently the latitude by ex-meridian will also be correct without any plotting on the chart or further calculation. The hour-angle worked by direct spherics by logarithms gives exactly the same result to the decimal of a second.

52 3) Alt. var.	— 4·62 ×	3 ==	-	13.86
Cor. te	o Tabular H.A.			+	9.54
30 S.)	Gives H.A.		н. 2	м. 47	54:2
23 S. 52	Cor. A.T. Ship A.T. Green.		2 1	48 49	3.7 56.0
	Long. in time		Ö	58	7.7
	Longitude Run		14	31	55 E. 15 W.

Long. at time of 2nd obsn. 14 31 40 E

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POSITION FROM TWO STELLAR OBSERVATIONS.

(COMBINING CHRON. LONG. OBSERVATION WITH AN EX-MERIDIAN BELOW THE POLE.)

1898.—On October 8th, at about 6h. 44 m. p.m. A.T. at ship, observed altitude of * Canopus east of meridian was 15° 14′ S., when a chronometer indicated mean time at Greenwich 7d. 19h. 36m. 16s., and after running on a true S. 55° E. course for three-quarters of a mile observed altitude of * Fomalhaut to north-eastward was 49° 20′, when chronometer indicated 7d. 19h. 40m. 6s. Height of eye, 28 ft. Required, true bearing of stars and position of ship at time of second observation, the approximate position at the time being latitude 51° S. and longitude 163° E.



Position of ship, 51° 123' S. 163° 313' E.

Note.—As time is often lost in getting hold of the log-book and working up the D.R. position, this example is worked with the nearest whole degree of latitude and longitude, and this will generally be near enough for a pretty accurate result when working by the improved "Sumner" method. This problem worked closely by spherics gives within $\frac{1}{4}$ of same result.

TO FIND APPROXIMATE ALTITUDES AND BEARINGS OF SUITABLE STARS FOR **OBSERVATION TO QUICKLY OBTAIN POSITION OF SHIP.***

1917.—On July 9th, soon after sunset, at about 7 h. 50 m. p.m. and 7 h. 54 m., in approximate latitude 47° N. and longitude 7° W., find what stars of first magnitude within the limits of the Reduction and Azimuth Tables would be suitable for quickly determining the ship's position, and the approximate altitudes and bearings of the stars. Height of eye, 40 ft.

First find the Sid. Time at $ship = A.T. Sp. + A. \odot$'s R.A.

	H. M.						
A.T. Sp.	7 50	Next look up	Table of Stars in	order of R.A. (p.	283) and see	what stars in adj	acent quad-
A. O's R.A.	+7 13 rant	ts come within	n the limits of thi	s Sid. Time.			•
•		It will be see	en at a glance tha	at Capella to N.W	. and Arctur	us to S.W. are th	e two most
Sid. T. Sp.	15 3 suit	able stars.	0	*			
	н. м.				H. M.		
Sid. Time	15 3	*'s Decl.	45 54.9 N.	Sid. Time	15 7	*'s Decl.	10 36.7 N.
* Capella	17 II below		15 54 5	* Arcturus	14 12	Lat.	17 0.0 N.
Mer. Pass.	Pole.	P.D.	-44 5'I N.	Mer. Pass.			17
*'s H.A.	2 8)	Lat.	47 0.0 N.	*'s H.A.	0.55)	M.Z.D.	27 23.3
Lat.	47° N.		47 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Lat.	17° N.		-/ -]]
Gives Redn.	4° 8.8'	Mer. Alt.	2 54 9 N.	Gives Redn	- 2° 13'	Mer. Alt.	62 36.7 S.
and Azim, N	V. 22° W.	Redn.	+ 4 8.8	and Azim, S	5. 27° W.	Redn.	-2 13
		Cor. 40 ft.	+ 12.7				
		0011 40 111				True Alt.	60 22.7
		Alt. for sext	ant 7 17.4 N.			40 ft. Cor.	+7
			, 1/410			40.10, 001,	. /
						Alt. for sextai	t 60 20.7 S.
						and for boundary	00 30 7 01

POSITION FROM COMBINED ALTITUDES OF TWO EX-MERIDIAN STARS.

1917.—On July 9th, soon after sunset, at about 7 h. 50 m. p.m., in approximate latitude 47° N. and longitude 7° W., the true altitude of *Capella was 7° 2.2′ N.W., when chronometer showed M.T.G. 8 h. 23 m. 48 s., and true altitude of *Arcturus was 60° 23.7′ S.W., when chronometer showed M.T.G. 8 h. 26 m. 59 s. Run in interval N. 32° E. 0.7 m. Required, position of ship at time of 2nd observation.

		* CAPELLA	то N.W.		
M.T.G. Long. 7° W.	н. м. s. 8 23 48 — 28 о	Alt. of × Redn.	$- \begin{array}{c} \circ & 2 \cdot 2 \mathbf{N} \\ - 4 & 1 \cdot 3 \end{array}$	Sid. T.G. Noon Accl. 8 h. 23½ m.	H. M. S. 7 7 24.7 + 1 22.7
M.T. Sp. M. ⊙'s R.A.	75548 + 7847	Mer. Alt. ★'s P.D.	3 0.9 44 5.1 N.	M. O's R.A. (1) Accl. 3 m.	7 8 47·4 + 0·5
Sid. T. Sp. * 's R.A.	$ \begin{array}{r} 15 & 4 & 35 \\ -5 & 10 & 35 \end{array} $	Approx. Lat. Cor. for 6'	47 6.0 N. + 0.4	M. ⊙'s R.A. (2)	7 8 47.9
* 's H.A.	-954 oW. 1200	Lat. Run	47 6·4 N. o·6 N.	*'s Decl. 45 54	4·9 N.
Supt. or below Pole H.A. Gives from Reducti	2 6 oW.	Lat. at time of 2r Obsn. able (p. 346) Posneline S 6810	nd 47 7.0 N.	P.D. 44 5 Run N. 32° E.	0.7 m. = 0.6' N.

* ARCTURUS TO S.W.

		н. м. s.		Lat(I)	47°7'N.		
	M.T.G. Long. 6° 59½'	8 26 59 27 58		o's°W	Cartie	Alt. of * Redn.	60 23.7 S. + 2 16.8
	M.T. Sp. M. ⊙'s R.A.	7591 +7848	Pos?	5.602	COT:505	Mer. Alt.	62 40.5
	Sid. T. Sp. ¥'s R.A.	15 7 49 14 11 55		long.Coi. 18·2 W		M.Z.D. *'s Decl.	27 19·5 N. 19 36·7
	*'s H.A.	0 55 54 W.		N 62:	·	Approx. Lat. Cor. for 4'	46 56·2 -·5
giv	res from Reduct Table (p. 325 and Azim. S.	ion and Azimuth) Redn. 2° 16.8 27 ¹ / ₂ ° W.; Posn.	1 6'	N.		Lat.	46 55•7 N
	line N. $62\frac{1}{2}^{\circ}$ V	V.		Lat. (2)	46°55'7 N.		
				(Table IX, p. 301.)			
	01 T °	1. N. A.t.	NT 0 117	STAR 40 W	Lot or N	I ong (2)	6 FOIF W

1st Obs. Lat. 4^{7} $7 \cdot 0 N.$ 2nd ,, ,46 $55 \cdot 7 N.$ Diff. Lat. 11 \cdot 3	Azim. N. 21.5 W. gives ,, S. 27.5 W. ,, Lat. E	$\begin{array}{c} 0.27 \text{ S. to W.} \\ 0.35 \text{ N. to W.} \\ \text{cor.} \\ \text{cor.} \\ \text{cor.} \\ \text{cor.} \\ \text{cor.} \\ \text{Lat.} \end{array}$	47 7 N. 5 S. 47 2 N.	Long. (2) Cor. Llng.	6 59·5 W. 18·2 W. 7 17·7 W.
Lat. Error. D. Lat.	Long. Long. C	Dr. Lat. Cor. 0.27' = 5.01' S.			

* This example is taken from "Tables of Calculated Hour-angles and Altitude Azimuths, Ex-meridian Tables, and Calculated Reductions and Azimuths of Bright Stars," by H. S. Blackburne. James Brown and Son, Glasgow. 105. 6d.

POSITION FROM CALCULATED EX-MERIDIAN OF TWO STARS, EACH OVER FOUR HOURS FROM THE MERIDIAN OF INFERIOR TRANSIT.

1898.—On 10th Nov., at about 7 h. 25 m. p.m. A.T. at ship in lat. by D.R. 40° 30' S. and long. 173° o' E. Observed altitude of * Canopus was 17° 10' to S.E. when a chronometer indicated M.T.G. 9d. 19h. 35 m. 28 s., and again after running east (true) for $\frac{1}{2}$ m. observed altitude of * a^2 Centauri 22° $51\frac{1}{4}$ ' to S.W. when a chronometer indicated M.T.G. 19h. 37 m. 48 s. Height of eye, 36 ft. Required the position of ship at the time of second observation.



Note.—These observations worked as two chronometer problems gave exactly the same results, but had the second ex-meridian latitude been worked with the azimuth as found by the A and B Tables the latitude would have been nearly 1' in error, due to a slight change in the star's declination in twelve years; the B Table having been calculated for \star 's declination in 1910 It is well to remember, however, that the best results will always be obtained by using the sine method with hour angle and altitude in the calculation of the azimuth, and this is especially the case where the altitude is high.

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BELOW POLE EX-MERIDIAN AND POSITION-LINE.

1910.—On April 1st, soon after sunset, at 6h. 42m. p.m., observed altitude of $* \alpha$ Cygni (Deneb) 8° 46′ W. of meridian when a chronometer indicated mean time at Greenwich 7h. 34m. 13s. Approximate latitude 52° N., and longitude 12° W. Required, latitude of meridian, and positionline from it.

		* a CYGNI TO NO	ORTHWARD.		
M.T. Green. Long. 12° W.	н. м. s. 7 34 13 — 48 о	Sid. T. (G. noon) Accl. 7h. 34m.	н.м. s. 0 35 51°6 + 1 14°6	Obsd. alt. of * Cor. (40ft.)	8 46 0 N. - 12'3
M.T. Sp. M. ⊙'s R.A.	6 46 13 + 0 37 6	M. ⊙'s R.A.	0 37 6.2	T. alt. Redn.*	8 33'7 - 1 20'2
Sid. T. at Sp. ¥'s R.A.	7 23 19 20 38 21	A simuth from tobles		Mer. alt. P.D.	7 13°5 N. 45 2°9 N.
∗ 's H.A	10 44 58 W.	Azimutii from table	90.0 90.0	Lat. Cor, for 16'	52 16·4 N. + 0·4
Supt.	I 15 2 W.	Position-line	N. 76.7 E.	Lat.	52 16.8 N.

H.A. at Inferior Transit.



The above example is given to draw special attention to the great value of the ex-meridian problem when near the meridian below the Pole. The observation gives with a minimum amount of work (when within the limits of these tables) the latitude on a certain meridian, and the positionline from this meridian. The curvature of this position-line is seen at a glance from the azimuth table, which is given on the same page as the reduction table. In this example the change of

azimuth only amounts to or of a degree in 4m. of time, or 1° of longitude. The position-line at Loop Head would be N. 78° E. This position-line crossed by a bearing of Tearaght Island light (if sighted) would give a good reliable position, provided the observation was good. A sounding in conjunction with this position-line would give a faith converte a solition. line would also give a fairly accurate position.

The latitude and position-line could also have been found at the same time from these tables by * Sirius, the position-line of which would have then been S. 79° E. The crossing of these two position-lines would give an excellent latitude, but the longitude would not be reliable, as the angle is small, and both observations are west of the meridian.

* From Blackburne's and Westland's "Azimuth and Reduction Tables."

FORMULÆ FOR CALCULATION OF EX-MERIDIAN LATITUDE WHEN AZIMUTH IS KNOWN.

It will be seen from the accompanying figure that if we drop a perpendicular on the meridian from D at M the following arcs, P M arc (1), and Z M arc (2), are readily calculated. The sum or difference of arc (1) and arc (2) = latitude.

Rule for Object above the Pole.

- Name arc (1) same as declination.
- Name arc (2) contrary to bearing of object-i.e., N. or S. of the prime vertical.
- Add like and subtract unlike names, which will give the required latitude.

Formulæ of Calculation.

Cot. PM arc (I) = Cos H.A.

× Cot. decl. Tan Z M arc (2) = Cos. Az. × Cot. Alt.

Rule for Object below the Pole.

- Name both arc (1) and arc (2)same as the decl.
- Latitude = Sum of arc (I)and arc (2).

Formulæ for the Calculation.

- H.A. = Supplement of H.A.from upper meridian.
- For Arc (2) use comp. of Z M, or M N, then
- Tan. arc (1) = Cos. H.A. \times Cot. decl.
- Cot. arc (2) =Cos. Az. \times Cot. alt. PM + MN = comp. PZ =
- latitude.





Arc (I) is found by the same formula as is used on p. 97, and the same arc is used for arc (2), but with a trifle less work; and as an ex-meridian outside the ordinary limits of ex-meridian tables is seldom of much use without the azimuth, this method is recommended in preference, if the azimuth is calculated with the H.A. and altitude. This method should always be used in preference when the declination of object is small. The writer's attention was first drawn to this excellent method of obtaining the latitude by a letter to the *Nautical Magazine*, August, 1899, p. 581, from E. S. Haynes, master of the tug "Cuzuni," and the value of it has been further impressed on him by a study of Admiral H. E. Purey Cust's valuable little book on "Sumner's" method. In this work Admiral Cust, R.N. (late Hydrographer to the Admiralty), strongly advocates this method.

Formulæ to compute Altitudes.

Using the accompanying figure. From Z drop a perp. on the hour circle at N. This will be outside the usual spherical triangle when the hour-angle is over 6 h. Arc (I) = P N. Arc (2) = P D - P N = N D when H.A. is less than 6 h. Arc (2) = P D + P N when H.A. is more than 6 h. Then Tan. Arc $(I) = Cos. P \times Cot.$ Lat.

Sin. Alt. = sin. lat. \times sec. arc (1) \times Cos. arc (2).

H.A. $6 h = 90^{\circ}$ Formula. Sin. Alt. = sin. decl. \times sin. lat.

12—Azimuth.



DIAGRAMS WITH EXPLANATIONS

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H. S. BLACKBURNE,

WITH WHICH ARE EMBODIED THE

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From CAPTAIN E. W. OWENS, Examiner, Local Marine Board, London. "I certainly have no objection to make, but much approval; your work is concise, clear, and, from my point of view, correct."

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"It seems to me that you have taken great pains to make a clear explanation of the 'weather rule' position, and, what is sometimes a very difficult question to determine, how a vessel is steering when her green light is seen three points on the port bow of your own vessel, which at the same time has the wind on her port beam, and what is to be done under these circumstances."

CAPTAIN J. NETHERCLIFT JUTSUM, Principal of the Nautical Academy.

61 FITZHAMON EMBANKMENT, CARDIFF.

"Many thanks for your little book re Rule of the Road. I consider it is as near perfection as any graphic method could be brought for illustrating this subject, and, although it is striking in its simplicity, its conciseness bears the impress of very careful and painstaking consideration in its production."

CAPTAIN GEO. SHIELDS, Principal of Naval Academy, 40 CLYDE PLACE.

"Allow me to thank you for the copy of your book, which is perfection itself. I wish you every success, and shall be pleased to recommend it to my pupils at all times."

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TABLES FOR AZIMUTHS, GREAT-CIRCLE SAILING.

174

REDUCTION TO THE MERIDIAN, WITH A NEW AND IMPROVED "SUMNER" METHOD.

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Principal Examiner of Masters and Mates in New Zealand, and Nautical Adviser to the Government [Fourth Edition, 1916]. PRICE. 68.

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Every single chart is available for any latitude through the aid of the above-men-tioned tables, by which greater accuracy of position is found, as well as a wider range for observation, than is given by the usually taught "Sumner's" method. NOTE. -With reference to the above, Lieutenant G. W. Logan, United States Navy,

editor of a provious revised edition of Bowditch's "American Practical Navigator," states In that "the plane chart for plotting the intersection of 'Summer' lines is excellent, and I freely concede that your method by means of Table C^2 is an improvement on my own for those who work 'Summer's 'with one position and an azimuth.—U.S.S. 'Castine,' Santo Domingo City, S.D., 17th January, 1905."

Mr. H. B. Goodwin, R.N., M.A., author of several works on navigation, &c., formerly Examiner in Nautical Astronomy at the Royal Naval College, Greenwich, says :-

"I notice several interesting features in your present edition, notably the adaptation of 'Sumner' methods to plane charts, which should be more generally known."-Aug., 1905.

Published by Marine Department, New Zealand Government, Wellington, New Zealand Sold in New Zealand at the Shipping Offices, and by Booksellers. Sole Agents in United Kingdom: James Brown and Son, 52-58 Darnley Street, Glasgow.

EXTRACTS FROM PRESS REVIEWS

ON THE

Tables for Azimuths, Great - circle Sailing,

REDUCTION TO THE MERIDIAN.

[From the Syren and Shipping, 23rd August, 1905, and 4th November, 1908.]

Captain Blackburne's labour-saving aids for navigators are known all over the world by his brethren who keep themselves posted in up-to-date methods; and this collection of tables now published leaves nothing to desire by the navigator wishful of finding his ship's geographical position, or the error of her compass, with the least possible chance of error, and in the shortest possible interval of time, anywhere within the usual limits of navigation. There is one point in connection with these tables which is deserving of the close consideration of the Board of Trade. Although the practical seaman will almost invariably use such data at sea, yet the Board compels the candidates for certificates to plod along in a way which gives admittedly erroneous results under certain conditions. That the Board of Trade should examine along one line---that of antiquity---and that practical navigators should work along quite another line---that of labour-saving tables----is surely ludicrous. The New Zealand Government requested the Board of Trade to allow the use in the examinationroom of tables like those of Captain Blackburne's, together with improved methods of working, but the request has not been granted. We sincerely trust that the Board of Trade will see fit to adopt modern methods by allowing the candidates permission to use the A, B, C Azimuth Tables of Blackburne, or any similar labour-saving work. More convenient in form or more utilitarian in application these tables could not be.

[Extract from the Nautical Magazine, September and December, 1908.]

In the new edition of his well-known A, B, C, and D Tables, Captain Blackburne must surely have cut all existing records. . . . Captain Blackburne is as indefatigable as ever in his efforts to lighten the labours of those who go down to the sea in ships. Early in the present year he published an edition of the A, B, and C Tables. They are now republished, with an appendix entitled Ex-meridian and Azimuth Inspection Tables. . . . The author seems here to have hit upon a happy idea, for we have a maximum of information in a minimum of space; and, as he points out, once calculated, the reduction and azimuths will hold good for a long series of years.

[Extract from the Shipping World, 9th December, 1908.]

The new issue of his A, B, and C Tables for Azimuth, &c., is undoubtedly the most complete and comprehensive volume on this subject yet published. . . .

[Extract from the United Service Magazine, December, 1908.]

These tables now make it possible to determine the position of the ship more readily at any time, and with less trouble than ever before.

[Extract from the Mariner, 15th December, 1908.]

Sufficient is it to say that the various navigation tables, rules and examples, including a new and improved "Sumner" method, make the volume on all counts one of the most complete and authoritative that we know in nautical literature.

[Extract from *Shipping Illustrated*, New York, 5th December, 1909.] These tables, as set forth in the present edition, are the most complete and comprehensive Azimuth and Ex-meridian Tables for practical work yet published.

[Extract from New Zealand Military Journal, October, 1913.]

As an adjunct to marching or flying by day and night without a compass may be taken another work for the reason that the tables it contains practically enabled a revolution to be made in the old methods of night marching. This is "Tables for Azimuths and Great-circle Sailing," by H. S. Blackburne.

Inset-Azimuth.

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EXTRACTS FROM LETTERS TO THE AUTHOR

RE THE

TABLES FOR AZIMUTHS AND REDUCTION TO THE MERIDIAN.

Mr. W. H. SWENY, Chief Officer, P. and O. s.s. "Mooltan," writes,— I have now had your new edition of Azimuth and Reduction to the Meridian Tables in use for one Australian voyage, using them almost daily for stellar observation. The results obtained have been surprising, and so satisfactory that I have discarded all other books on these problems.—23rd January, 1909.

Captain JOHN OWEN, Teacher of Navigation, Cardiff, writes,-

Your method of solving the Time Azimuth problem by the A, B, C Tables is concise, and easy of solution. If these tables were more generally known I think seafarers would use them in preference to Burdwood's or any other special tables employed at present.— 25th January, 1909.

Mr. JOHN BLENCOWE, late Second Officer, B.I. s.s. "Shirala," writes,-

In Lyttelton I obtained a copy of your new Azimuth and Ex-meridian Tables, and on showing them to my brother officers they were so taken with them that they all bought a copy for themselves. I think the tables are splendid, and for the sake of the profession will do all I can to make them more widely known.—9th February, 1909.

Captain P. THOMPSON, late Secretary to the Local Marine Board, and Examiner of Masters and Mates, London; Author of "Navigation Simplified," &c., writes,-

Having gone carefully through your book I am satisfied that your short methods of solving the most practical problems in navigation will commend themselves to the officers of the Mercantile Marine; for myself, I cannot too strongly express how highly I appreciate what you have done to simplify the every-day calculations of those navigators whose duties in the ordinary work of a steamer leave them little leisure for working out a ship's position by the longer methods expected from them when undergoing the Board of Trade examination for a qualifying certificate.—12th February, 1909.

Mr. S. C. WARNER, Chief Officer, P. and O. s.s. "Socotra," writes,-

I should like to add my humble testimonial to the new A, B, C book you have brought out, and to tell you how much it is appreciated here on board. I certainly think it is the very best book of navigation ever printed.—13th September, 1910.

Captain GEORGE BURTON, Instructor of Cadets, Ocean Training-ship "Port Jackson," writes,—

I have shown your book to all our senior cadets, and advised them to procure copies. The book is certainly altogether the most complete education in modern navigation yet published. - 26th November, 1910.

Captain HERBERT H. EDMONDS, Teacher of Navigation, Sydney, Australia, writes,— Of the two systems the Maroq-Hilaire and that which you so strongly advocate I decidedly prefer the latter. . . I like your Ex-meridian Tables; it is no extra work finding the azimuth beforehand, since it is required in the after-plctting. It is a great pity the Board of Trade do not keep abreast of the times in adopting this system.—17th December, 1910.

Captain J. KING DAVIS, commanding the Australasian Antarctic Expedition, S.Y. "Aurora," writes,-

Macquarie Island, 16th December, 1911.

We have already several copies of the previous edition, as I use nothing else, and have insisted on my officers learning to use them, as they are the only suitable tables for our work, and are much handier, in my opinion, for any latitude. Mr. H. ROCHFORD HUGHES, Navigating Officer, H.M. Cable Steamer "Iris," writes,

Having just returned from Sydney, New South Wales, after sounding proposed track for the new cable from Auckland to that port, I hasten to write to say what a boon your splendid A, B, C Tables have proved during the expedition, more especially the C² Table. . . I have tried "new navigation" methods, and all the principal tables of the day, during my search for the shortest and most accurate methods, and have come to the conclusion that for our work your tables and system generally are the best.—5th and 8th February, 1912.

Commander RICHARD HYDE, R.N., Navigation School, Portsmouth, writes,— I have just returned from a cruise with our gunboats the "Dryad" and "Harrier," when I used your tables exclusively for finding azimuths, and personally I prefer them to Burdwood or Weir's diagram.—12th April, 1912.

Lieutenant EDWARD R. G. R. EVANS, R.N., who Commanded the British Antarctic Expedition R.Y.S. "Terra Nova" from England to Antarctic in 1910, writes,-

I shall endeavour to bring your tables into more general use in the Navy, as I consider them *facile princeps* of their kind. Burdwood and Davis are so cumbersome. I think you will be pleased to hear that on the southern journey I used your tables exclusively, and worked out all magnetic variations and true bearings by means of them up to latitude 85° and hence to 88° almost by exterpolation.—17th April, 1912.

Captain L. B. BENNETT GILLMAN, s.s. "Matatua," writes,-

Before leaving Wellington on our last homeward voyage I procured a 1911 edition of your tables for azimuth and reduction to the meridian. I think it is the cheapest and best book on practical navigation ever offered to the seafaring community. Had the price been two guineas instead of six shillings it would have been nearer the intrinsic value of the book. The tables are absclutely the last word in modern and up-to-date navigation.—30th April, 1912.

Lieutenant HARRY PENNELL, R.N., Commanding the British Antarctic Expedition R.Y.S. "Terra Nova," writes,-

I have used your A, B, C and Ex-meridian Tables whenever the "Terra Nova" has made a voyage south, and have found them invaluable. In parts of Boss Sea the variation changes 1° for every four miles run at right angles to the lines of equal variation, and the large number of azimuths that it is necessary to take during the twenty-four hours would mean a prohibitive amount of work if your all-embracing tables were not at hand.—3rd June, 1912.

Captain THOMAS LIDDLE, Sunderland, writes,-

Your last 1911 edition is undoubtedly the best book published for navigators, and the cheapest.—28th December, 1912.

Lieut.-Col. W. A. TILNEY, commanding 17th Lancers, Sialkot, India, writes, – Your tables have practically enabled us to revolutionize night marching, as you see by the enclosed report.-29th July, 1913.

Lieut. E. BALLARD DALBY, R.N.R., Extra Master (London), H.M.S. "Carmania," at sea, writes,—

The officers who joined this ship in Liverpool when she was converted into an armed cruiser were drawn from nearly every company under the British flag, and no less than six of them had brought copies of your A and B Tables with them. It is a significant fact that once an officer commences to use them he never goes back to Burwood and Davis, where interpolation is in many cases tedious. Your tables ertainly are the tables par excellence for an officer of the watch.—10th May, 1915.

EXTRACTS FROM PAPER REVIEWS

AND LETTERS ON

MODERN UP-TO-DATE NAVIGATION.

[The Nautical Magazine, Glasgow, July, 1914.]

One advantage that should accrue to this little book and to all those who use it is the fact that its editor and compiler, in addition to being a good theoretical man, is also an experienced navigator and practical shipmaster. Having spent some time in preparing candidates for the Board of Trade examinations, he has acquired the "knack" of putting things as men can understand them, and in a way in which they will be most useful to them. The book throughout shows a sound knowledge of the subject, and will, with the help of the worked examples and chartlets, surely be the means of a larger number of navigators becoming interested in modern up-to-date navigation.

[The United Service Gazette, London, 15th October, 1914.]

The book contains some nautical tables of great value for ready position-finding from observations of two stars out of the meridian. They also give by simple inspection the true bearing within certain limits of a few bright stars, and the calculated reduction to the meridian up to about an hour or a little over from the meridian, enabling a navigator to determine his latitude and position-line from a single observation of a star, with little more trouble than when the star is on the meridian. The book also contains several fully worked-out examples showing the use of the tables, with some well executed diagrams illustrating the problems; the different methods of determining the ship's position by the "Old Summer Method," the "Improved Sumner Method," and the "New Navigation Method" are contrasted, and the author clearly exposes some of the fallacious claims which have been made by one or two recent writers for the so-called "New Navigation" or "Marcq St. Hilaire" system of dealing with observations for position-finding. The value of the below Pole reduction and Azimuth Tables is well illustrated by the example on page 47. Small as the work is, having been printed on thin paper, it contains the tabulated results of about 19,900 calculations.

Captain H. H. EDMONDS, Teacher of Navigation, Sydney, writes,-

I thoroughly endorse all you say on the Marcq St. Hilaire method; it is the truest thing that has been written on the subject.

Captain T. L. EVANS, F.R.G.S., Manager, Donald Steamship Company, Bristol, writes,-

I am convinced that the book "Modern Up-to-date Navigation" is one of the best auxiliaries to the navigator that I have yet perused, and would have been glad of such a book during my career as master in the foreign service. I must congratulate you on the very excellent methods which you have published in your book, which I consider most valuable to all navigators who wish to ascertain the position of their ship, by the splendid methods contained in your book, and which are so simply illustrated and explained that any one with an ordinary amount of intelligence can grasp without any instructions except that which is contained in your book. I shall certainly have the greatest pleasure in recommending it to all my younger friends who are now masters and officers of ships.

Captain THOS. LIDDLE, Sunderland, writes,-

It's wonderful the information you have got in such a small space, and so far I have never seen any book to equal it. Why the Board of Trade will not sanction the use of your books for the examinations I cannot understand.

Captain J. W. MAXWELL, King Edward VII Nautical School, London E, writes,-

I agree with your remarks, and see in this little work how very clear and sound your knowledge is.

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NEW ZEALAND

NAUTICAL ALMANAC & TIDE-TABLES:

ALSO

Information with Plans about the Principal Ports of New Zealand,

AND

SUPPLEMENTARY INFORMATION TO DATE RELATING TO THE "NEW ZEALAND PILOT," EDITION 1908.

Published by Direction of the Hon. the Minister of Marine. Wellington, N.Z.

PRICE - - 3/-.

The above-mentioned work is published annually towards the end of the year for the following year. It contains the usual Nautical Almanac data required in the ordinary navigation of ships, tide-tables (calculated by the N.Z. Lands and Survey Department), giving time and heights of high and low water at Wellington and Auckland, as standard ports, and constants to about eighty other places in the Dominion; also the tidal stream predictions for Tory Channel and French Pass, where the tidal streams attain a rate of five to seven knots at springs. Next to the tide-tables the special purpose of the work is to supplement and keep the "New Zealand Pilot" up to date, by collating all the notices to mariners and latest information since the last edition of the "New Zealand Pilot." It also gives somewhat fuller information, with plans of wharves, &c., about all the ports of any importance in the Dominion.

The last edition of the work contains about 530 pages, and over thirty folded maps and plans of harbours, wharves, &c., with latest alterations, and much information relating to the principal ports and harbours of New Zealand and of value to mariners.

Courses and distances between all the principal ports in New Zealand, also between New Zealand, Australia, Fiji, South Africa, San Francisco, Vancouver, Valparaiso, Panama, New York, and to England, via Cape Horn, and Panama, with the return via Capetown, are given in the work.

Some very valuable nautical tables and examples of problems worked by their aid are published in the Almanac, which it is hoped will greatly encourage masters and officers generally to make a practice of determining the ship's position from two stars at twilight, as these tables make the problems very easy, and also enable the observer to make sure that he is taking the right star by the easy calculation of the approximate altitude, and the bearing of the stars is given at sight.

The Almanac now finds its way not only to England and Australia, but has been sent for from North America and Jamaica. Mr. G. H. Halligan, Inspecting Engineer and Hydrographer in New South Wales, wrote of a previous year's edition, "This most valuable publication is now almost indispensable in Australia, and I find it of the utmost value in my hydrographic investigations."

and I find it of the utmost value in my hydrographic investigations." The Editor of the "Rudder" Magazine, New York, U.S.A., wrote to the Secretary, Marine Department, when acknowledging receipt of a copy,—"I am always pleased to receive this publication, and congratulate you on its excellence. It is far better than anything we have published in this country."

PUBLISHED BY MARINE DEPARTMENT, N.Z. GOVERNMENT, WELLINGTON, N.Z.

Sold in New Zealand at the Shipping Offices and Customhouses, and can be obtained in United Kingdom from the New Zealand High Commissioner, Victoria Street, London, S.W.



[Extract from Shipping Illustrated, New York, U.S.A., April 3rd, 1915.]

The main purpose of these tables is to make as easy as possible the problem of finding the ship's position from combined altitudes of the sun, moon, or stars, and especially to facilitate the much-neglected practice of determining the ship's position from two or three stars at twilight, a few minutes before sunrise, and a few minutes after sunset. By the aid of the calculated star reduction and azimuth tables in this book a latitude and position line can be obtained at any time when the stars are visible almost as easily as by meridian altitude of a star. This method is the simplest yet brought forth for quickly and accurately solving the problem of determining position from stellar observations out of the meridian, or for determining latitude and position line from a single observation, which may be used in connection with a sounding, or the bearing of some mountain peak or light.

Captain G. N. TOMLIN, R.N., H.M.S. "Agincourt," writes,—"I have already found your tables most useful and simple; I hope they will meet with the success they deserve."

Commander HARRY PENNELL, R.N., H.M.S. "Duke of Edinburgh," writes,—"These hour-angle and azimuth tables reduce sights now to the minimum of work conceivable when they fall within its limits.

Captain THOS. WASHINGTON, U.S. Navy, Hydrographer, writes,—"I am sure your tables are going to prove to be a most useful and accurate help for shipmasters and others interested in navigation; I congratulate you upon the excellence of the work."

Captain HERBERT H. EDMONDS, Teacher of Navigation, Sydney, writes, —"Received my copy of your book with which I am greatly pleased. I have tested a few critical cases and find results all that can be desired, both with hour-angle and azimuths. What a boon to have all you want with a position-line in one act."

Commander EDWARD R. G. R. EVANS, R.N., H.M.S. "Viking," writes, — "Very many thanks for 'Tables of Calculated Hour-angles, Star Reductions, and Azimuth Tables.' Like all your works this is excellent, and simple enough for any navigator who will read the explanation and work a few examples until he is familiar with their use—then they are a pleasure."

Lieut. E. B. DALBY, R.N.R., H.M.S. "Carmania," writes,—"I have purchased a copy of your new book, and hasten to say how much I like it. The printing is good, the arrangement could not be bettered, the explanations are copious, and the whole book a marvel of cheapness. I have checked the hour-angles in Table 1 by working out quite a number of sights in the usual way and then working the same sights by this table. In no case did I get a difference of over a second, and in most cases the error was under half a second. The facility and accuracy with which the azimuth is obtained through the latitude variation (with a little mental interpolation in some cases) is certainly remarkable. For your star reduction and azimuth tables I have nothing but admiration. For stellar navigation I know of nothing to equal these incomparable tables."

Captain ROBERT W. FERGUSON, of Brisbane, Queensland, writes,—"The tables are magnificent, and the most singular part of them is the truly graphic Altlude Azimuth Table No. IV, it being the best and most ingenious I have ever seen. . . . These and your 'Tables for Azimuth, Great-circle Sailing, and Reduction to the Meridian' 90° N. to 90° S. are of inestimable value to the science of navigation, and your methods supersede all others in accuracy and brevity, for which you deserve well and worthily at the hands of the profession."

Authority: MARCUS F. MARKS, Government Printer, Wellington, 1916.



[Extract from N.Z. Gazette No. 103, 14th Sept., 1916.]

Notice to Mariners No. 74 of 1916.

NEW EDITION OF NAUTICAL TABLES PUBLISHED.

Marine Department,

Wellington, N.Z., 11th September, 1916. N OTICE is hereby given that the New Zealand Marine Department have just published a fourth edition of

N Department have just published a fourth edition of "Tables for Azimuth, Great Circle Sailing, and Reduction to the Meridian," Lats. 90° N. to 90° S.

The azimuth tables, which for some years have been acknowledged to be the most complete and comprehensive azimuth tables published, remain the same as in last edition. They include limits from pole to pole for sun, moon, and all the stars in the heavens, for any hour angle from the meridian.

The reduction tables, though still very compact, have been more than doubled in size since issue of last edition, and their limits of use have been considerably enlarged. They are available for all latitudes and declinations, and for any altitude, often with more than double the hour-angle limits from the meridian given in the ex-meridian tables in the standard works of navigation in general use.

They are also available for below pole hour-angles as well as the hour-angles from upper meridian. As an illustration of the wide limits of these tables an example is given on page 158, which will no doubt surprise navigators generally. The position of ship is accurately determined from two ex-meridian latitudes where the reduction to both zenith distances was over 9°, hour-angles over 1 h. 40 m., and azimuth over 40° from the meridian.

The accuracy of resulting position from these observations is proved by a fresh calculation of two longitudes from a near parallel of latitude, by the ordinary double altitude method, with the use of the A and B Tables. Other new and interesting problems have also been added in this edition.

Published by Marine Department, New Zealand Government, Wellington, New Zealand. Price 6s.

Sold in New Zealand at the shipping offices and by booksellers. Sole agents in United Kingdom : James Brown and Son, 52–58 Darnley Street, Glasgow, Scotland.

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GEORGE ALLPORT,

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