# Hudson's TABLES 

## VOL.II.

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## TABLES

FOR

## calculating The cubic contents

OF

## EXCAVATIONS AND EMBANKIIENTS.

BY

## JOHN R. HUDSON,

 M. AM. SOC. C. E.Volume II.


> 49996
> Сорувіант, 1887,

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## PREFACE.

The methods of computing earthwork quantities given in Articles 9, 10 , and 11, are entirely distinct from those in the first volume. Each volume is independent of the other, and complete in itself. Article 8 is in both volumes. Attention is called to Article 9 ; the rule at the head of the article is very short and simple, and well adapted, in three-level ground, to take the place of the ordinary method of "averaging end areas;" it gives the same answer and the process is a third shorter. As is shown in the example, the entire process consists in addition, subtraction, and inspection of tables, and the errors that are liable to occur in the multiplications that are part of the usual methods are avoided. When, as is usual, three heights are taken at a station, the following examples will show by comparison the advantage of using the methods of computing earthwork quantities given in this work over the usual methods.

Example, computed by the usual method of "averaging end areas." Road-bed, 18 feet wide. Side slopes 1 to 1. Stations 100 feet long.


Below the same example is computed in two-thirds of the time by the
first rule in Article 9, the distances (under L. D. and R. D.), from center to slope stakes are not used.

Example. Road-bed, 18 feet wide. Side slopes 1 to 1. Stations 100 feet long.

| Station. | Left. | Center. | Right. |
| :---: | :---: | :---: | :---: |
| 1 | 8.6 | 4.6 | 3.6 |
| 2 | 7.6 | 2.0 | 10.2 |


| 8.6 | 4.6 | 12.2 | 136 | 7.6 | 2.0 | 17.8 | 222 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3.6 | 4.6 | 9.2 | 96 | 10.2 | 2.0 | 4.0 | 37 |  |  |
| 12.2 | 9.2 |  | 232 | 17.8 | 4.0 |  | 259 | $\begin{array}{r} 230 \\ 215 \end{array}$ | 1 |
|  |  | 3.0 | 2 |  |  | 13.8 | 44 |  |  |
|  |  |  | 230 |  |  | . | 215 | 445 | Ans. in cu. yds. |

The third example in Article 9 shows another method of finding the " average end area " answer.

Example. Road-bed, 24 feet wide. Slide slopes 1 to 1 . Stations 100 feet long.

| Station. | L. D. | Left. | Center. | Right. | R. D. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 18.2 | 6.2 | 2.4 | 1.2 | 13.2 |
| 2 | 24.8 | 12.8 | 8.6 | 6.4 | 18.4 |

The following is the computation of the above example by the common method of "averaging end areas."

| 18.2 | $\frac{2) 2.4}{1.2}$ | $\begin{array}{r} 31.4 \\ 1.2 \end{array}$ | $\begin{aligned} & 6.2 \\ & 1.2 \end{aligned}$ | $\begin{array}{r} 7.4 \\ 6 \end{array}$ | $\begin{aligned} & 37.68 \\ & 44.40 \end{aligned}$ | $\begin{array}{r} 82.08 \\ 300.96 \end{array}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 13.3 |  |  |  |  |  |  |  |
| 31.4 |  | 37.68 | 7.4 | 44.4 | 82 |  |  |
| 31.4 |  | 37.68 | 7.4 | 44.4 | 82.68 | 2)383.0 |  |
| 24.8 | 2)8.6 | 43.2 | 12.8 | 19.2 | 185.76 | $2 7 \longdiv { 1 9 1 . 5 }$ |  |
| 18.4 | 4.3 | 4.3 | 6.4 | 6 | 115.20 | 70 | Ans. in cubic yards. |
| 43.2 |  | 185.76 | 19.2 | 115.2 | 300.96 |  |  |

By the second method of Article 9, the (distances under L. D. and R. D.), from center to slope stakes are not used, and the answer is found in two-thirds of the time, as follows :

| 6.2 | 29.1 | 70 | 12.8 | 40.0 | 344 | 152 |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 1.2 | 2.4 | 82 | 6.4 | 8.6 | $\Sigma 13$ | 557 |  |
| $\overline{7.4}$ | $\overline{69.84}$ | $\overline{152}$ | $\overline{19.2}$ | $\overline{344.00}$ | $\overline{557}$ | $\overline{709}$ | Answer in cubic yards. |

By the last method in Article 9, the process is nearly one-half shorter
than the computation by the usual form of the prismoidal formula, while the answer is the same.

Example, computed by the usual form of the prismoidal formula :
Road-bed, 24 feet wide. Side slopes 1 to 1. Stations 100 feet long.

| Station. | L. D. | Left. | Center. | Right. | R. D. |
| :---: | :---: | ---: | :---: | :---: | :---: |
| 1 | 18.2 | 6.2 | 2.4 | 1.2 | 13.2 |
| 2 | 24.8 | 12.8 | 8.6 | 6.4 | 18.4 |



| 31.4 | 1.2 | 74.6 | 7.4 | 26.6 | 410.30 |
| ---: | ---: | ---: | ---: | ---: | ---: |
| $\overline{43.2}$ | $\frac{4.3}{74.6}$ | $\frac{5.5}{5.5}$ | $\overline{410.30}$ | $\overline{26.2}$ | $\frac{12}{319.2}$ |
| $\overline{319.20}$ | $\overline{729.50}$ |  |  |  |  |

If the last method of Article 9 is used, the computation is very much shortened and becomes :


In Article 11, methods for cross sections of five or more heights are given.

The cross-section pages in Article 10 and at the end of the volume show forms for cross-section books that will be found useful and conrenient for recording and preserving the field notes and office computation when these tables are used. The left hand pages of the cross-section books could be arranged for keeping field notes in the usual form. The num')er for 2.0 in Table VI, is the same as the number for 0.0 in Table VIII, and in many cases one table of side triangles may be used for several widths of road-hed by simply moring the numbers in the columns headed "Center Height." When, as is usual, three heights are taken at a station, much time is saved br using the tables of side triangles with either the "diagonal," " prismoidal formula," " mean proportional," or "averagng end sections" (with or without "prismoidal correction") methods
first rule in Article 9, the distances (under L. D. and R. D.), from center to slope stakes are not used.

Example. Road-bed, 18 feet wide. Side slopes 1 to 1. Stations 100 feet long.

| Station. | Left. | Center. | Right. |
| :---: | :---: | :---: | :---: |
| 1 | 8.6 | 4.6 | 3.6 |
| 2 | 7.6 | 2.0 | 10.2 |

$\begin{array}{rrrrrrrrrl}8.6 & 4.6 & 12.2 & 136 & 7.6 & 2.0 & 17.8 & 222 & & \\ \frac{3.6}{12.2} & \frac{4.6}{9.2} & -9.2 & 96 & 10.2 & 2.0 & 4.0 & 37 & 230 & \\ & & 3.0 & \frac{2}{232} & & \overline{4.0} & & \frac{259}{215} & \text {, } \\ & & & & & 13.8 & \frac{44}{230} & \frac{445}{45} & \text { Ans. in cu. yds. }\end{array}$
The third example in Article 9 shows another method of finding the " average end area" answer.

Example. Road-bed, 24 feet wide. Slide slopes 1 to 1. Stations 100 feet long.

| Station. | L. D. | Left. | Center. | Right. | R. D. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 18.2 | 6.2 | 2.4 | 1.2 | 13.2 |
| 2 | 24.8 | 12.8 | 8.6 | 6.4 | 18.4 |

The following is the computation of the above example by the common method of "averaging end areas."

| $\begin{aligned} & 18.2 \\ & 13.3 \end{aligned}$ | $\begin{array}{r} 22.4 \\ \frac{1.2}{} \end{array}$ | $\begin{array}{r} 31.4 \\ 1.2 \end{array}$ | $\begin{aligned} & 6.2 \\ & 1.2 \end{aligned}$ | $\begin{array}{r} 7.4 \\ 6 \end{array}$ | $\begin{aligned} & 37.68 \\ & 44.40 \end{aligned}$ | 82.08 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  | 300.96 |  |
| 31.4 |  | 37.68 | 7.4 | 44.4 | 82.68 |  |  |
| 24.8 | 2)8.6 | 43.2 | 12.8 | 19.2 | 185.76 | 27\% $2 \longdiv { 3 8 3 . 0 4 }$ |  |
| 18.4 | $\overline{4.3}$ | 4.3 | 6.4 | 6 | 115.20 | 709 | Ans. in cubic yards. |
| 43.2 |  | 85.76 | 19.2 | 115.2 | 300.96 |  |  |

By the second method of Article 9, the (distances under L. D. and R. D.), from center to slope stakes are not used, and the answer is found in two-thirds of the time, as follows :

| 6.2 | 29.1 | 70 | 12.8 | 40.0 | 344 | 152 |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $\overline{1.2}$ | 2.4 | 82 | 6.4 | 8.6 | $\Sigma 13$ | 557 |  |
| $\overline{7.4}$ | $\overline{69.84}$ | $\overline{152}$ | $\overline{19.2}$ | $\overline{344.00}$ | $\overline{557}$ | $\overline{709}$ | Answer in cubic yards. |

By the last method in Article 9, the process is nearly one-half shorter
than the computation by the usual form of the prismoidal formula, while the auswer is the same.

Example, computed by the usual form of the prismoidal formula :
Road-bed, 24 feet wide. Side slopes 1 to 1. Stations 100 feet long.

| Station. | L. D. | Left. | Center. | Right. | R. D. |
| :---: | :---: | ---: | :---: | :---: | :---: |
| 1 | 18.2 | 6.2 | 2.4 | 1.2 | 13.2 |
| 2 | 24.8 | 12.8 | 8.6 | 6.4 | 18.4 |


| 18.2 | 2)2.4 | 31.4 | 6.2 | 7.4 | 37.68 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 13.2 | 1.2 | 1.2 | 1.2 | 6 | 44.40 |  |
| 31.4 |  | 37.68 | 7.4 | 44.4 | 82.08 | 82.08 |
|  |  |  |  |  |  | 300.96 |
| 24.8 | 2)8.6 | 43:2 | 12.8 | 19.2 | 185.76 | 729.50 |
| 18.4 | 4.3 | 4.3 | 6.4 | 6 | 115.20 |  |
| - |  |  | - |  | - | 6)1112.54 |
| 43.2 |  | 185.76 | 19.2 | 115.2 | 300.96 | $2 \overline{7185.42}$ |
|  |  |  |  |  |  | 687 |


| 31.4 | 1.2 | 74.6 | 7.4 | 26.6 | 410.30 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| $\frac{43.2}{74.6}$ | $\overline{4.3}$ | $\frac{5.5}{5.5}$ | $\overline{410.30}$ | $\overline{29.2}$ | 12 |
| 319.2 | $\overline{319.20}$ |  |  |  |  |
| 729.50 |  |  |  |  |  |

If the last method of Article 9 is used, the computation is very much shortened and becomes :

| 2.4 | 6.2 | 9.7 | 8.6 | 12.8 | 13.3 | 7.4 | 130 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2.4 | 1.2 | 13.4 | 8.6 | 6.4 | 19.6 | 19.2 | 261 |
| 8.6 | - |  | 2.4 |  |  | - | 296 |
| - | 7.4 | 129.98 |  | 19.2 | 260.68 | 26.6 | - |
| 13.4 |  |  | 19.6 |  |  |  | 687 |

In Article 11, methods for cross sections of five or more heights are given.

The cross-section pages in Article 10 and at the end of the volume show forms for cross-section books that will be found useful and convenient for recording and preserving the field notes and office computation when these tables are used. The left hand pages of the cross-section books could be arranged for keeping field notes in the usual form. The number for 2.0 in Table VI, is the same as the number for 0.0 in Table VIII, and in many cases one table of side triangles may be used for several widths of road-hed by simply moring the numbers in the columns headed "Center Height." When, as is usual, three heights are taken at a station, much time is saved by using the tables of side triangles with either the "diagonal," " prismoidal formula," " mean proportional," or "averagng end sections" (with or without "prismoidal correction") methods
of computing earthwork quantities. Instead of finding the area of each cross section, the cubic yards in a solid, 100 feet long, of the given cross section, are found in three-fourths of the time from the tables, by the following rule: When the sum of the side heights is greater than twice the center height-multiply the cubic yards found for the given center height in the table of side triangles, by the difference between the sum of the two side heights and twice the center height, and $\begin{gathered}\text { subtract } \\ \text { add }\end{gathered}$ the product $\underset{\substack{\text { from } \\ \text { to }}}{\text { the cubic yards found for the given center height in the table of level }}$ cross sections. The cubic yards thus found can be used, as the areas are commonly used, in the different methods of computing earthwork quantities, omitting the multiplication by 100 and division by 27 , as the quantities are already in cubic yards.

Example. Road-bed 18 feet wide. Side slopes $1 \frac{1}{2}$ to 1 . Stations 100 feet long.

| Station. |  | Left. |  |  | $\begin{gathered} \text { Center. } \\ 15.0 \end{gathered}$ |  | $\begin{gathered} \text { Right. } \\ 9.0 \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 |  | 28.0 |  |  |  |  |  |
|  |  | 9.0 | 5.0 |  |  |  |
| 28 | 15 |  |  |  | 37 | 58.3 | 2250 |  |  |  |
| 9 | 2 | 30 | 7 | 408 |  |  |  |
| 37 | 30 | 7 | 408.1 | 2658 | 2658 |  |  |
|  |  |  |  |  | 1092 |  |  |
| 14 | 9 | 19 | 41.7 | 1050 | 2)3750 |  |  |
| 5 | 2 | 18 | 1 | 42 | 1875 | Answer |  |
| 19 | 18 | 1 | $\overline{41.7}$ | 1092 |  |  |  |

In the above example for Station 1, the sum of the two side heights is 37 , twice the center height is 30 , and 30 from $3 \%$ leaves \%. The number in Table VI for center height 15.0 is 58.3 , and 58.3 multiplied by 7 is 408 . In Table $V$ the number for height 15.0 is 2250 , and 2250 plus 408 equals 2658. In the same manner 1092 is found for station 2. Adding 2658 and 1092 and dividing 2 , will give the same answer, $18 \% 5$ cubic yards, as the common method of "averaging end areas." In Article 8, the above example is given with " prismoidal correction." In the cross-section book pages at the end of this volume are examples of the use of the above rule, with the "prismoidal formula" and "prismoidal correction" methods; and the first and second methods in Article 9 can be used with the "prismoidal formula" and "prismoidal correction" method; this is partly shown in Article 10. In the computation of earthwork quantities much time is saved if similar cross-section books are used; there is a place for nearly every number, so that crrors are less liable to occur. For comnarison the computation of the above example by the usual method of "areraging end areas" is given below :

Example. Road-bed 18 feet wide. Side slopes $1 \frac{1}{2}$ to 1 . Stations 100 feet long.

| Station. | L. D. |  | Left. |  | Center. | Right. | R. D. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 51.0 |  | 28.0 |  | 15.0 | 9.0 | 22.5 |
| 2 | 30.0 |  | 14.0 |  | 90 | 5.0 | 16.5 |
| 51.0 | -2)15.0 | 73.5 | 28 | 37 | 551.25 |  |  |
| 22.5 | 7.5 | 7.5 | 9 | 4.5 | 166.50 | 717.75 |  |
|  |  |  | - |  |  | 294.75 |  |
| 73.5 |  | 3675 | 37 | 185 | 717.75 |  |  |
|  |  | 5145 |  | 148 |  | 2)1012.50 |  |
|  |  |  |  |  |  | $2 7 \longdiv { 5 0 6 . 2 5 }$ |  |
|  |  | 551.25 |  | 166.5 |  | 1875 | cubic yds. |
| 30.0 | 2)9.0 | 46.5 | 14 | 19 | 209.25 | $\left[\frac{33}{1842}\right]$ |  |
| 16.5 | $\frac{10.0}{4.5}$ | 4.5 | 5 | 4.5 | 85.50 | [1842 |  |
| 46.5 |  | 2325 | 19 | 95 | 294.75 |  |  |
|  |  | 1860 |  | 76 |  |  |  |
|  |  | 209.25 |  | 85.5 |  |  |  |

The answer for the "prismoidal correction" has been added in brackets, so that the example can also be compared with the first example in Article 8, showing the advantage of using the latter method.

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| XXII. Side-triangles. | 100 | 20 | $\frac{1}{4}$ to 1 |
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| XXX. Side triangles. | 100 | 14 | $1 \frac{1}{2}$ to 1 |
| XXXI. Level cross-sections. | $1{ }^{10}$ | 16 | 1 to 1 |
| XXXII. Side triangles. | $1{ }^{10}$ | 16 | 1 to 1 |
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XLVI. Cubic yards $=\frac{(\text { height } \times r+b) 100}{12 \times 27}$.

PRISMS. ROAD-BED. FT. LONG. FT. WIDE. SIDE SLOPES.
$\frac{100}{4} 0 \quad 14 \quad 1 \frac{1}{2}$ to 1

100
48

24 1 to 1 24

24
1 tn 1

## ARTICLE 7.

The cubic yards in a prism 100 feet long, of level cross-section, can be found by multiplying the area of the cross-section by $\frac{10}{27}$. The area of a level cross-section can be found by adding the product of the side-slope ratio by the height to the width of the road-bed, and multiplying the sum by the height.

In any level cross-section let $r$ equal the ratio of the side-slope to one, then, as will be more clearly seen by making a diagram,

Area for height $0.1+$ area for height $0.9+2(0.9 \times 0.1 \times r)$
$=$ area for height 1.0.
To change to cubic yards, multiply both terms by $\frac{100}{27}$, and let the cubic yards for height 0.9 equal $Y$, and $2(0.9 \times 0.1 \times r)^{\frac{10}{20} 7^{\circ}}$ equal $y$, then

Cubic yards for height $0.1+Y+y=$ cubic yards for height 1.0, and in the same way,

Cubic yards for height $0.2+Y+2 y=$ cubic yards for height 1.1,
and for a general equation
Cubic yards for any height $x+Y+10 x y=$ cubic yards for height $(x+0.9)$.
This equation can be used in making a table of cubic yards in prisms 100 feet long, of level cross-section. For side-slope $1 \frac{1}{2}$ to $1, y$ will equal 1.0; and for side slope 1 to $1, y$ will equal $\frac{2}{3}$, or $0.6+$. Find the cubic yards for height 0.9 or $Y$, and place them below the space for height 0.0 in a table made similar in form to Table C, place $Y+y$ below the space for height 0.1 , and $Y+2 y$ below the space for height 0.2 , etc., to the end of the first part of the table. Adding $9 y$ to any number in the first part of tho table will give the number below it; this can be used as a check, or after the first line of $Y+y$ 's are in place the first part of the table can be completed by adding $9 y$ to each number to find the number below it; and this is the easier method when the side-slope is 1 to 1 , as then $9 y$ equals 6 , a whole number, while $y$ equals $\frac{2}{3}$, a fraction. Find the cubic yards for
herghts from 0.1 to 0.9 ，by the rule at the head of this article，or by the method given in Trautwine＇s＂Excavations and Embankments，＂and place them in the table；then add the cubic yards for height 0.1 to $Y+y$ ，the number just below，to find the cubic yards for height 1．0，and add the cubir yards for height 0.2 to $Y+2 y$ to find the cubic yards for heights 1.1 ，and so on to the end of the table，and the complete table will be similar to the second part of Table C．The cubic yards in the last line should be checked by the rule at the head of this article；and a line drawn through the quan－ tities $Y+y, Y+2 y$ ，etc．；then the table can be used，or copied into any more convenient form．Table C is for a road－bed 18 feet wide，side－slopes $1 \frac{1}{2}$ to $1 ; Y$ equals 64.5 ；$y$ equals $1.0 ; Y+y$ equals 65.5 ；the cubic yards for 0.1 are 6.7 ，and 6.7 plus 65.5 equals 72.2 ，the cubic yards for height 1．0， and so on to the end of the table；and if it is continued to height 40.0 and copied，will give Table V．

The rule given in the Preface shows the use of these tables with the tables of side－triangles．

TABLE C．
Road－bed 18 feet wide．
Side－slopes $1 \frac{1}{2}$ to 1.
FIRST PART．

| $\begin{aligned} & \text { Bo } \\ & \text { un } \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | 苟荡 |  |  |  | Ex |  | 搉 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 |  | 0.1 |  | 0.2 |  | 0.3 |  | 0.4 |  | 0.5 |  | 0.6 |  | ． |  | 0.8 |  |
|  | 64.5 |  | 65.5 |  | 66.5 |  | 67.5 |  | 68.5 |  | 69.5 |  | ． 5 |  | 71.5 |  | 72. |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 81. |
| 1.8 |  |  |  |  |  |  |  |  |  |  |  | 2.4 |  | 5 |  | 6 |  |
| 7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 99.5 |
|  | 100.5 |  | 101.5 |  | 102.5 |  | 103.5 |  | 104.5 |  | 10 |  | 106.5 | 2 | 107.5 | 5．3 | 108.5 |

SECOND PART．

| $\begin{aligned} & \text { 感 } \\ & \substack{\text { en }} \end{aligned}$ |  | $\left\lvert\, \begin{array}{l\|l\|} \substack{\text { 品 } \\ \text { 品 }} \end{array}\right.$ |  |  |  | $\begin{aligned} & \text { 总 } \\ & \text { 采 } \end{aligned}$ | 気登 |  |  | 药 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 0.1 | 6.7 | 0.2 | 13.6 | 0.3 | 20.5 | 0.4 | 27.6 | 0.5 | 34.7 |  | 42.0 |  | 49.4 |  | 56.9 |
|  | 5 |  | T2 |  |  |  | ． 5 |  | 68.5 |  | 69.5 |  | 70.5 |  | 71 |  | 5 |
|  | 64.5 |  | 722 | 1.1 | 80.1 |  | 88.0 | 1.3 | 96.1 | 4 | 104.2 | 1.5 | 5112.5 |  | 120.9 | 1.7 | 29.4 |
|  | 73.5 |  | 74.5 |  | 75.5 |  | 76.5 |  | 77.5 |  | 78.5 |  | 79.5 |  | 80.5 |  | 81.5 |
|  | 138.0 | 9 | 146.7 |  | 155.6 | 2.1 | 164.5 | 2.2 | 173.6 |  | 182.7 |  | 41920 |  | 201.4 |  | 10.9 |
|  | 82.5 |  | 83.5 |  | 84.5 |  | 85.5 |  | 86.5 |  | 87.5 |  | 88.5 |  | 89.5 |  | 90.5 |
|  | 220.5 |  | 330 |  | 240.1 |  | 250.4 | 3.1 | 260.1 | 2 | 270.2 |  | 3280.5 |  | 4290.9 |  | 301.4 |
|  | 91.5 |  | 92.5 |  | 93.5 |  | 94.5 |  | 95．5 |  | 96. |  | 97.5 |  | 98.5 |  | 89.5 |
|  | 312.0 |  |  |  |  | 3.9 | 344.5 | 4.0 | 355.6 | 4.1 | 366．7 |  | 3378.0 |  | 389.4 | 4 | 400.9 |
|  | 100.5 |  | 101.5 |  | 102.5 |  | 103.0 |  | 104.5 |  | 105.5 |  | 106.5 |  | 107.5 |  | 108.5 |
|  | 412.5 | 6 | 424.2 |  | 736.1 | 4.8 | 448.0 | 4.9 | 460.1 | 5.0 | 17．5 | 5.1 | 1484.5 | 5.2 | 10． |  | 509.4 |

In a three-level section in excaration, let the centre-cut equal $c$, the sum of the side-cuts equal $s$, the width of the road-bed equal $B$, the sideslope ratio equal $r$, the difference between the sum of the side-cuts and twice the centre-cut equal $D$, and the area of the cross-section equal $A$; then the following equation will be true :

$$
2 c \frac{B+c r}{2} \times \frac{100}{4 \times 27}+s \frac{B+\frac{s}{2} r}{2} \times \frac{100}{4 \times 27}-D \frac{D r}{4} \times \frac{100}{4 \times 27}=\frac{100 A}{2 \times 27} .
$$

To use this equation prepare a table, similar to Tables XLII and XLIII, for each width of road-bed, showing opposite $2 c$ the quantity

$$
2 c \frac{B+c r}{2} \times \frac{100}{4 \times 27},
$$

and opposite $s$ the quantity

$$
\frac{B+\frac{s}{2} r}{2} \times \frac{100}{4 \times 27}
$$

this will be seen to be a table of level cuttings with double heights (cats or fills) in the first column, and cubic yards in prisms 100 feet long in the second column.

Then prepare a table similar to Table XLI, for each side-slope ratio, showing opposite $D$ the quantity $D \frac{D r}{4} \times \frac{100}{4 \times 27}$. Find from the first table the cubic yards for $s$ and for $2 c$, add them, and from their sum subtract the cubic yards found in the second table for $D$. Add the cubic yards thus found for two adjacent stations to find the cubic yards in the prismoid, 100 feet long, between the stations; and the answer will be the same as that given by the common method of "averaging end-areas." In the following example the road-bed is 18 feet wide, the side-slope ratio 1 to 1 , and the stations 100 feet apart :

| Station. | Left. | Centre. | Right. |
| :---: | :---: | :---: | :---: |
| 1 | 19.6 | 12.0 | 9.2 |
| 2 | 25.2 | 17.6 | 4.4 |



The sum of the side-cuts at station 1 is 28.8 , twice the centre-cut is 24.0, and their difference is 4.8 . In Table XLIII the number for 28.8 is 432 , and the number for 24.0 is 333 ; and in Table XLI the number for 4.8 is 5 ; and 432 plus 333 minus 5 is 760 . In the same way, 1269 is found for station 2, and 760 plus 1269 equals 2029, the answer in cubic yards. From this answer the "prismoidal correction" of 19 cubic yards, found from Table XXXVII, for the difference of centre-cuts, $1 \% .6$ minus 12.0 equals 5.6 , can be deducted, leaving 2010 cubic yards for the answer.

To use the "prismoidal formula," find from the table the cubic yards for the mid-section, multiply by 4 , add the product to the cubic yards for the end-sections, and divide the sum by 3 , as follows :

| $\frac{s+s^{\prime}}{2}=$ | 34.2 | 556 |
| ---: | ---: | ---: |
| $c+c^{\prime}$ | $=$29.6  <br> 4.6 $\frac{449}{1005}$ | 760 <br>  <br>  <br>  <br>  <br>  <br> 1000 |

The same method can be used for embankments, and another example is shown in Article 9.

In a three-level section in excaration, let the centre-cut equal $C$, the sum of the two side-cuts equal $S$, the width of the road-bed equal $B$, the sideslope ratio equal $r$, the difference between the centre-cut and half the sum of the two side-cuts equal $D$, and the area of the cross-section equal $A$; then the following equation will be true :

$$
C(B+C r) \frac{100}{27}+\frac{S}{2}\left(B+\frac{S}{2} r\right) \frac{100}{27}-D^{2} r \frac{100}{27}=2 A \frac{100}{27}
$$

To use the equation find from the tables of level cross-sections the cubic yards for $C$ and for $\frac{S}{2}$, add them, and from their sum subtract the cubic yards found in Table XLVII for $D$. Add the cubic yards thus found for two adjacent stations, and divide the sum by 4 , to find the cubic yards in the prismoid, 100 feet long, between the stations, and the answer will be the same as that given by the common method of "averaging end-areas." In the following example the road-bed is 18 feet wide, the side-slope ratio $1 \frac{1}{2}$ to 1 , and the stations 100 feet apart.

| station. |  | $\begin{aligned} & \text { Left. } \\ & 28.0 \end{aligned}$ |  | $\begin{gathered} \text { Centre. } \\ 15.0 \end{gathered}$ | $\begin{aligned} & \text { Right. } \\ & 9.0 \\ & 5.0 \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 |  | 14.0 |  | 9.0 |  |  |
| $\frac{S}{2}=18.5$ | 3135 | $\frac{S^{\prime \prime}}{2}=9.5$ |  | 1135 | 5317 |  |
| $C=15.0$ | 2250 | $C^{\prime \prime}=9.0$ |  | 1050 | 2184 |  |
| $D=3.5$ | $\begin{array}{r} 5385 \\ 68 \end{array}$ | $D^{\prime}=0.5$ |  | $\begin{array}{r} 2185 \\ 1 \end{array}$ | 4)7501 |  |
|  | 5317 |  |  | 2184 | 18 | wer. |

Half the sum of the side-cuts at station 1 is 18.5 , the centre-cut is 15.0 , and their difference is 3.5 . In Table V the number for 18.5 is 3135 , and the number for 15.0 is 2250 , and in Table XLVII the number for 3.5 is 68 , and 3135 plus 2250 minus 68 is $531 \%$. In the same way, 2184 is found for station 2 ; and 5317 plus 2184 equals 7501, and 7501 divided by 4 gires 1875 , the answer in cubic yards. From the tables of level cross-sections, tables that give the cubic yards in prisms $\frac{100}{2}$ feet long could be computed, and with a table that gives opposite $D$ the quantity $D^{2} r \frac{100}{2 \times 2 \%}$ could be used as above, dividing by 2 instead of 4 , with the advantage of using smaller numbers. As shown, tables giving the cubic yards in prisms $\frac{100}{4}$ feet long can be used. In Tables XLII and XLIII double heights are used because it was thought easier to find twice the centre-height than half the sum of the side-heights. Double heights could be used in the ordinary tables of level cross-sections. This gives the choice of six methods of using the fact that twice the area of a three-level cross-section in excavation is equal to the area of the level cross-section of $C$, plus the area of the level cross-section of $\frac{S}{2}$, minus $D^{2} r ; C$ being the centre-cut, $S$ the sum of the two sidecuts, $D$ the difference between $C$ and $\frac{S}{2}$, and $r$ the side-slope ratio. The same methods can be used for embankments.

## ARTICLE 8.

## PRISMOIDAL CORRECTION.

The cubic yards given in Table XXXVII are found by multiplying the square of the difference of center heights (Diff. C. H.) by the ratio of the side slope to 1 , and by 100 , and dividing by 27 and 6 . If three heights are taken at a station, find from the tables by the rule in the Preface the cubic yards for each end cross-section, add them, divide by 2 , and subtract the cubic yards, given in Table XXXVII, for the difference of center heights; the answer will usually be a very little in excess of the answer by the prismoidal formuia.

Example. Road-bed 18 feet wide. Side slopes $1 \frac{1}{2}$ to 1 .


In the above example for station 1 , the sum of the side heights is 37 , twice the center height is 30 , and 30 from 37 leaves 7 . The number in Table VI for center height 15.0 is 58.3 , and 58.3 multiplied by ${ }^{7} 7$ is 408.1 . In Table V the number for height 15.0 is 2250 , and $2250+408=2658$. Proceed in the same manner for station 2, then add the results, divide by 2, and subtract 33 , the cubic yards found in Table XXXVII for the difference of center height 6.0 , for the answer in cubic yards.

When three heights are taken at a station, the number of cubic yards in the prismoid between two adjacent stations can be found by the following rule, and the answer will be the same as by the prismoidal formula : Multiply the horizontal distance between the slope stakes at the first station by twice the center height of the first station plus the center height of the
second station; multiply the horizontal distance between the slope stakes at the second station by twice the center height of the second station plus the center height of the first station ; and multiply the sum of the four side heights by $1 \frac{1}{2}$ times the width of the road-hed; add these three products, and find the cubic yards for the resulting area in Table XXXIX.

Example. Road-bed 14 feet wide. Side slopes $1 \frac{1}{2}$ to 1 .


At station 1 the horizontal distance between the slope stakes is 21.2 ; twice the center height is 5.2 , and 5.2 plus center height 1.4 is 6.6 ; the product of 21.2 by 6.6 is 139.92 . At station 2 the horizontal distance between the slope stakes is 21.8 , twice the center height is 2.8 , and 2.8 plus center height 2.6 is 5.4 ; the product of 21.8 by 5.4 is 117.72 ; the sum of the side heights is $10,1 \frac{1}{2}$ times the width of the road-bed is 21 , and the product of 21 by 10 is 210 . The sum of the three products is $46 \% .64$, and in Table XXXIX for the nearest area (466.56) we find 144 cubic yards.

When more than three heights are taken at a station, we can multiply the sum of the end-areas by 100 , and divide by 2 and 27 , and deduct the cubic yards given in Table XXXVII, for the difference of center heights, for an answer usually a little in excess of the answer by the prismoidal formula.

After finding the sum of the end-areas, instead of multiplying by 100 and dividing by 2 and 27 , we can find the cubic yards for 100 feet opposite the area nearest this sum in Table XXXVIII, and then deduct the cubic yards given in Table XXXVII for the difference of center heights.

Example. Side slopes $1 \frac{1}{2}$ to 1 , center heights 1.2 and 5.2 , end-areas 28 and 185. Sum of end-areas will be 213, and for area 212.76 in Table XXXVIII we find 394 cubic yards. The difference of center heights is 4.0 , and for 4.0 we find in Table XXXVII 15 cubic yards, and 15 cubic yards from 394 cubic yards leaves 379 cubic yards, answer.

## ARTICLE 9.

When three heights are taken at a station, find from tables of level cross sections that give the cubic yards in prisms 100 feet long, the cubic yards for the sum of the side heights and for twice the center height; add them, and from their sum subtract the cubic yards found in Table XLI, for the difference between the sum of the side heights and twice the center height.

Add the cubic yards thus found for two adjacent stations, to find the cubic yards in the prismoid 100 feet long between the stations. The answer is the same as that given by the common method of " averaging end areas."

Example. Road-bed 18 feet wide. Side slopes 1 to 1. Stations 100 feet long.

| Station. |  | Left. |  | Center. | Right. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 |  | 8.6 |  | 4.6 | 3.6 |
| 2 |  | 7.6 |  | 2.0 | 10.2 |
| $s=12.2$ | 136 | $8^{\prime}=17.8$ | 222 |  |  |
| $2 c=9.2$ | 96 | $2 c^{\prime}=4.0$ | 37 | 230 |  |
| - | - | - | - | 215 |  |
|  | 232 |  | 259 | - |  |
| $D=3.0$ | 2 | $D^{\prime}=13.8$ | 44 | 445 | Answer in cubic yards. |
|  | 230 |  | 215 |  |  |

Let the sum of the side heights at station 1 equal $s=8.6+3.6=$ 12.2 ; twice the center height equal $2 c=4.6+4.6=9.2$, and their difference equal $D=3.0$. The number in Table XLIII for 12.2 is 136 , and the number for 9.2 is 96 , and $136+96=232$. In Table XLI the number for 3.0 is 2 , and $232-2=230$. Let the sum of the side heights at station 2 equal $s^{\prime}=7.6+102=1 \% .8$; twice the center height equal $2 c^{\prime}$ $=2.0+2.0=4.0$; and their difference equal $D^{\prime}=13.8$. In Table XLIII the number for 17.8 is 222 , and the number for 4.0 is 37 , and $2: 2+3 \%$ $=259$. In Table XLI the number for 13.8 is 44 , and $259-44=215$. Adding 230 and 215 , we have 445 , the answer in cubic yards. To find
the prismoidal correction, we can multiply the difference of the sums of the side heights by the difference of the center heights, and by the ratio of the side slope to 1, and find in Table XXXIX the cubic yards for the product. In the example given, let $s^{\prime}-s=17.8-12.2=5.6$, and $c-$ $c^{\prime}=4.6-2.0=2.6$, and $5.6 \times 2.6 \times 1=14.56$, and in Table XXXIX for area 12.96 we have 4 cubic yards.

When, as is usual, the greater sum of the side heights is at the station with the greater center height, the prismoidal correction is to be subtracted, but in the example given, the greater center height is at station 1 , while the greater sum of the side heights is at station 2, so the prismoidal correction is to be added, and we have $445+4=449$, the answer in cubic yards by the prismoidal formula. Or, in most cases, Table XXXVII can be used as explained in Article 8. When, as is often the case, $D$ and $D^{\prime}$ are small, they can be neglected, and the operation reduced to finding from the table the cubic yards for twice the center height and the sum of the side heights at each of two adjacent stations, and adding them together to find the cubic yards in the prismoid between the stations.

Example. Road-bed 14 feet wide. Side slopes $1 \frac{1}{2}$ to 1 . Stations 100 feet long.

| Station. | Left. | Center. | Right. |
| :---: | :---: | ---: | :---: |
| 1 |  | 19.4 | 12.4 |
| 2 | 6.4 | 4.2 | 6.4 |
|  | 24.8 | 374 |  |
|  | 25.8 | 398 |  |
|  | 8.4 | 79 |  |
|  | 7.6 | 69 |  |
|  |  | 920 |  |
|  |  | Answer in cubic yards. |  |
|  |  |  |  |

For station 1, twice the center height is 24.8 , the sum of the side heights is 25.8 ; for station 2 , twice the center height is 8.4 , the sum of the side heights is 7.6 ; finding the cubic yards for each of these numbers in Table XLII and adding them, we have 920 cubic yards for the answer.

Calling the center height at the first station $c$, the sum of the side heights $s$, and the center height at the second station $c^{\prime}$, the sum of the side heights $s^{\prime}$, the width of the road-bed $b$, and the side slope ratio $r$, we can find the " average end area" volume by the following formula:

$$
c \frac{(s r+b) 100}{4 \times 27}+\frac{(s) b 100}{8 \times 27}+c^{\prime} \frac{\left(s^{\prime} r+b\right) 100}{4 \times 27}+\frac{\left(s^{\prime}\right) b 100}{8 \times 27}=\text { cubic yards. }
$$

For a road-bed 24 feet wide, side slopes 1 to 1 , we will find $\frac{(s r+b) 100}{4 \times 27}$ and $\frac{\left(s^{\prime} r+b\right) 100}{4 \times 2 \%}$ in Table XLIV, and $\frac{(s) b 100}{8 \times 27}$ and $\frac{\left(s^{\prime}\right) b 100}{8 \times 27}$ in Table XLV, opposite heights $s$ and $s^{\prime}$.

Example. Road-bed 24 feet wide. Side slopes 1 to 1 . Stations 100 feet long.

|  | Station. |  | Left. |  | Center. |  | Right. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 |  | 6.2 |  |  | 2.4 | 1.2 |
|  | 2 |  |  |  |  | 8.6 | 6.4 |
| 6.2 | 29.1 | 70 | 12.8 | 40.0 | 344 | 152 |  |
| 1.2 | 2.4 | 82 | 6.4 | 8.6 | 213 | 557 |  |
| 7.4 | 69.84 | 152 | $\overline{19.2}$ | 344.00 | 557 | 709 | bic yards. |

For station 1 the sum of the side heights is 7.4, and in Table XLIV the number for 7.4 is 29.1 , and 29.1 multiplied by center height 2.4 is 69.84. In Table XLV the number for 7.4 is 82 , and $70+82=152$. The sum of the side heights at station 2 is 19.2, and in Table XLIV the number for 19.2 is 40.0 , and 40.0 multiplied by center height 8.6 is 344 . In Table XLV the number for 19.2 is 213 , and $344+213=55 \%$. Adding 152 and $55 \%$, we have 709 cubic yards for the answer. From this we can subtract 24 cubic yards, found in Table XXXVII, for the difference of center heights 6.2 (giving in this case an answer a little less than that given by the prismoidal formula).

Where three heights are taken at a station, we can find the prismoidal contents of the prismoid between two adjacent stations by the following formula :

$$
\left(2 c+c^{\prime}\right) \frac{(s r+b) 100}{12 \times 27}+\left(2 c^{\prime}+c\right) \frac{\left(s^{\prime} r+b\right) 100}{12 \times 27}+\frac{\left(s+s^{\prime}\right) b 100}{8 \times 27}=c u . y d s .
$$

For a road-bed 24 feet wide, side slopes 1 to 1 , we will find $\frac{(s r+b) 100}{12 \times 27}$ and $\frac{\left(s^{\prime} r+b\right) 100}{12 \times 27}$ in Table XLVI, and $\frac{\left(s+s^{\prime}\right) b 100}{8 \times 27}$ in Table XLV, opposite heights $s$ and $s^{\prime}$.

Example. Road-bed 24 feet wide. Side slopes 1 to 1. Stations 100 feet long.

| Station. | Left. | Center. | Right. |
| :---: | ---: | :---: | :---: |
| 1 | 6.2 | 2.4 | 1.2 |
| 2 | 12.8 | 8.6 | 6.4 |


| 2.4 | 6.2 | 9.7 | 8.6 | 12.8 | 13.3 | 7.4 | 130 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2.4 | 1.2 | 13.4 | 8.6 | 6.4 | 19.6 | 19.2 | 261 |  |
| 8.6 | -- |  | 2.4 |  |  |  | 296 |  |
|  | 7.4 | 129.98 | - | 19.2 | 260.68 | 26.6 | - |  |
| 13.4 |  |  | 19.6 |  |  |  | 687 | Ans. in cu. yards. |

Twice the center height of station 1 plus the center height of station 2 is 13.4 , or $2 c+c^{\prime}=13.4$; the sum of the side heights at station 1 is
7.4 , or $s=7.4$; the number for 7.4 in Table XLVI is 9.7 , and $9.7 \times$ $13.4=129.98$.

Twice the center height of station 2, plus the center height of station 1 is 19.6 , or $2 c^{\prime}+c=19.6$; the sum of the side heights at station 2 is 19.2 , or $s^{\prime}=19.2$; the number for 19.2 in Table XLVI is 13.3 , and 13.3 $\times 19.6=260.63$. The sum of the four side heights is 26.6 , or $s+s^{\prime}=$ 26.6 ; the number for 26.6 in Table XLV is 296 . Adding 130 and 261 and 296, we have $68 \%$, the answer in cubic yards by the prismoidal formula.

## ARTICLE 10.

The last page of this article represents two pages of a cross-section book. The first page is like that of an ordinary level book with the addition of columns 2 and 3 for the left and right distances of the slope stakes from the center. $C, L$, and $R$, in the first column, stand for center, left, and right; they are not necessary, but show in what order the rod readings, and therefore the cuts and fills, are taken. The first page contains the field notes; on the second page the cubic yards have been computed by the methods in Article 9. For fills the road-bed has been taken 14 feet wide, side slopes $1 \frac{1}{2}$ to 1 , and the cubic yards have been computed by the first rule of Article 9. For station 21, twice the center height is 5.6, eleventh column, the sum of the side heights is 5.2 , eleventh column, and 5.2 from 5.6 leaves 0.4 , twelfth column. The number in Table XLII for 5.6 is 47 , thirteenth column, and the number for 5.2 is 43 , thirteenth column, and $47+43=90$; in Table XLI the number for 0.4 is 0 , fourteenth column, and $90-0=90$, fifteenth column. In the same way we find 173 , fifteenth column, for station 22 , and $90+173=263$, seventeenth column, the answer in cubic yards. From 263 we can deduct the prismoidal correction for the difference of center heights, as shown on the cross-section page at the end of this volume. In the prismoid between stations 22 and 23 , the cubic yards ( 172 , fifteenth column) found for the mid-section, are multiplied by 4 and the product added to the cubic yards found for stations 22 and $23 ; 173+688+167=1028$, eighteenth column, and $10: 8$ divided by 3 equal 343 , seventeenth column-the answer by the "prismoidal formula." Twice the center height for the midsection is found by adding the center heights of stations 22 and 23 ; $4.4+2.6=7.0$, eleventh column. Half the sum of the side heights, 9.2 and 13.2 , for stations 22 and 23 , is 11.2 , eleventh column, the sum of the side heights for the mid-section. The cuts at stations 1 and 2 are the same as those in the third and fourth examples of Article 9, and the computations are similar, but in a more convenient book form.

| Station. | $D$ from $C$. |  | Height Instrument. | $\begin{aligned} & \text { Fore } \\ & \text { Sight. } \end{aligned}$ | Back Sight. | Elevation. | Grade. | Cut. | Fill |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lert. | Right. |  |  |  |  |  |  |  |
| B. $M$. |  |  | 532.92 |  | 4.62 | 528.30 |  |  |  |
| 21 C . |  |  |  | 5.7 |  | 527.2 | 530.00 |  | 2.8 |
| $L$. | 13.3 |  |  | 7.1 |  | 525.8 |  |  | 4.2 |
| $R$. |  | 8.5 |  | 3.9 |  | 529.0 |  |  | 1.0 |
| 22 |  |  |  | 6.3 |  | 526.6 | 531.00 |  | 4.4 |
|  | 16.9 |  |  | 8.5 |  | 524.4 |  |  | 6.6 |
|  |  | 10.9 |  | 4.5 |  | 528.4 |  |  | 2.6 |
| 23 |  |  |  | 3.5 |  | 529.4 | 532.00 |  | 2.6 |
|  | 14.5 |  |  | 5.9 |  | 527.0 |  |  | 5.0 |
|  |  | 19.3 |  | 9.1 |  | 523.8 |  |  | 8.2 |
|  |  |  | 563.23 |  |  |  |  |  |  |
| 1 |  |  |  | 10.8 |  | 552.4 | 550.00 | 2.4 |  |
|  | 18.2 |  |  | 7.0 |  | 556.2 |  | 6.2 |  |
|  |  | 13.2 |  | 12.0 |  | 551.2 |  | 1.2 |  |
| 2 |  |  |  | 4.6 |  | 558.6 | 550.00 | 8.6 |  |
|  | 24.8 |  |  | 0.4 |  | 562.8 |  | 12.8 |  |
|  |  | 18.4 |  | 6.8 |  | 556.4 |  | 6.4 |  |
| 1 |  |  |  |  |  |  |  | 2.4 |  |
|  |  |  |  |  |  |  |  | 6.2 |  |
|  |  |  |  |  |  |  |  | 1.2 |  |
| 2 |  |  |  |  |  |  |  | 8.6 |  |
|  |  |  |  |  |  |  |  | 12.8 |  |
|  |  |  |  |  |  |  |  | 6.4 |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|  |  |  |  |  |  |  |  |  |  |


|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

## ARTICLE 11.

When heights are taken at the center and slope stakes, and over or under the edges of the road-bed, calling the width of the road-bed $B$, the side slope ratio $r$, the centel height $c$, the left slope stake height $h$, the right slope stake height $h^{\prime}$, the left edge height $n$, and the right edge height $n^{\prime}$; the cubic yards in a prism 100 feet long, of the given cross section, will equal

$$
n\left(\frac{h r}{2}+\frac{B}{4}\right) \frac{100}{27}+n^{\prime}\left(\frac{h^{\prime} r}{2}+\frac{B}{4}\right) \frac{100}{27}+c \frac{2 B \times 100}{4 \times 27}
$$

We will find $\left(\frac{h r}{2}+\frac{B}{4}\right) \frac{100}{2 y}$ and $\left(\frac{h^{\prime} r}{2}+\frac{B}{4}\right) \frac{100}{2 y}$ opposite heights $h$ and $h^{\prime}$ in the tables of side triangles, and if the road-bed is 12 feet wide, we will find $c \frac{2 B \times 100}{4 \times 27}$, or $c \frac{24 \times 100}{4 \times 27}$, opposite height $c$ in Table XL. (Tables similar to Table XL can easily be computed for any width of road-bed.) Add the cubic yards thus found for two adjacent stations and divide by 2 ; the answer will be the same as by the method of " averaging end areas."

Example. Road-bed, 12 feet wide. Side slopes, 1 to 1 . Stations, 100 feet long.

| Station. 1 |  | L. S. | L. E. |  | Center. | R. E. | R. S. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 12.4 | 9.6 |  | 5.4 | 4.2 | 3.6 |
| 2 |  | 14.8 | 12.0 |  | 8.8 | 7.2 | 5.4 |
| 34.1 | 17.8 | 327 | 38.5 | 21.1 | 462 | 522 |  |
| 9.6 | 4.2 | 75 | 12 | 7.2 | 152 | 810 |  |
| $\overline{327.36}$ | 74.76 | 120 | 462.0 | 151.92 | 196 | 2)$\overline{1332}$ |  |
|  |  | 522 |  |  | $\overline{810}$ | 666 Ans | bic yards. |

At station 1 the left slope stake height is 12.4 , or $h=12.4$, the left edge height is 9.6 , or $n=9.6$; in Table XXXVI the number for height 12.4 is 34.1 and $34.1 \times 9.6=327.36$. The right slope stake height is 3.6 , or
$h^{\prime}=3.6$, the right edge height is 4.2 , or $n^{\prime}=4.2$; in Table XXXVI the number for height 3.6 is 17.8 , and $17.8 \times 4.2=74.76$. In Table XL the number for center height 5.4 is 120 , and $327+75+120=522$. Proceed in the same manner for station 2 , then add the results and divide by 2 for the answer in cubic yards. We can find the answer as given by the prismoidal formula, by using Tables XXVIII and XLV as follows :


Twice the left edge height of station 1 plus the left edge height of station 2 is 31.2 , the number in Table XXVIII for slope stake height 12.4 is 5.7 , and $31.2 \times 5.7=17 \% .84$; twice the left edge height of station 2 plus the left cdge height of station 1 is 33.6 , the number in Table XXVIII for slope stake height 14.8 is 6.4 , and $33.6 \times 6.4=215.04$; twice the right edge height of station 1 plus the right edge height of station 2 is 15.6 , the number in Table XXVIII for slope stake height 3.6 is 3.0 , and $15.6 \times 3.0=46.80$; twice the right edge height of station 2 plus the right edge height of station 1 is 18.6 , the number in Table XXVIII for slope stake height 5.4 is 3.5 , and $18.6 \times 3.5=65.10$; the sum of the center heights 5.4 and 8.8 is 14.2 , and the number for height 14.2 in Table XLV is 158 ; and $178+215+47+65+158=663$, the answer in cubic yards. The following is an example of an irregular cross section of more than three heights :

Example. Road-bed 24 feet wide. Side slopes 1 to 1.
Station.

|  |  |  |
| :---: | :---: | :---: |
|  | $h$ | $n$ |
|  | $g$ | $f$ |
| 1 | 18.6 | 13.0 |
|  | $\overline{30.6}$ | $\overline{14.0}$ |
|  | $G$ | $F$ |

Left.

| $e$ |
| :---: |
| $\frac{14.4}{10.8}$ |
| $E$ |


|  |
| :---: |
| $d$ |
| 18.2 |
| 8.4 |
| $D$ |


| Center. | Right. $h^{\prime}$ |  |
| :---: | :---: | ---: |
|  | $n^{\prime}$ | $h^{\prime}$ |
| $c$ | $d^{\prime}$ | $e^{\prime}$ |
| 12.4 | 8.6 | 5.2 |
| 0.0 | $\frac{9.2}{}$ | $\overline{17.2}$ |
| $C$ | $D^{\prime}$ | $E^{\prime}$ |

In the above example the numerators, marked by small letters, are the heights, or cuts or fills, and the denominators, marked by large letters, are the distances from the center. Let $B$ equal the width of road-bed, $r$ the side slope ratio, $h$ and $h^{\prime}$ the heights at the slope stakes, and $n$ and $n^{\prime}$ the heights that come next to the slope stakes; then the cubic yards in a prism 100 feet long, of the given cross section, will equal

$$
\begin{aligned}
&\left(h+h^{\prime}\right) \frac{B \times 100}{4 \times 27}+n\left(\frac{h r}{2}+\frac{B}{4}\right) \frac{100}{27}+n^{\prime}\left(\frac{h^{\prime} r}{2}+\frac{B}{4}\right) \frac{100}{27}+ \\
& {\left[(c-e) D+(d-f) E+(e-g) F+\left(c-e^{\prime}\right) D^{\prime}\right] \frac{100}{2 \times 27} }
\end{aligned}
$$

When, as in this example, $B=24$, we will find $\left(h+h^{\prime}\right) \frac{B \times 100}{4 \times 27}$ in Table XL opposite height $h+h^{\prime}$, and $\left(\frac{h r}{2}+\frac{B}{4}\right) \frac{100}{2 \gamma^{\prime}}$, and $\left(\frac{h^{\prime} r}{2}+\frac{B}{4}\right) \frac{100}{27}$ in Table XVI opposite heights $h$ and $h^{\prime}$, and we will find

$$
\left[(c-e) D+(d-f) E+(e-g) F+\left(e-e^{\prime}\right) D^{\prime}\right] \frac{100}{2 \times 27}
$$

in Table XXXVIII opposite area $(c-e) D+(d-f) E+(e-g) F+\left(c-e^{\prime}\right) D^{\prime}$. Add the cubic yards thus found for two adjacent stations, and divide the sum by 2 for the answer, which will be the same as by the "average end area" method.

Example. Road-bed 24 feet wide. Side slopes 1 to 1. Stations 100 feet long.

| Station. | Left. |  |  | Center. |  | Right. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 18.6 | 13.0 | 14.4 | 18.2 | 12.4 | 8.6 | 5.2 |
| 1 | 30.6 | 14.0 | 10.8 | 8.4 | 0.0 | 9.2 | $\overline{17.2}$ |
| 2 |  |  |  | 9.4 | 6.8 | 3.2 |  |
| 2 |  |  |  | 21.4 | 0.0 | 15.2 |  |
| 18.6 |  | 56.7 | 31.9 | 12.4 | 8.4 | -16.80 |  |
| 5.2 |  | 13.0 | 8.6 | 14.4 | -2.0 | 56.16 | 529 |
|  |  |  |  |  |  | -58.80 | 737 |
| 23.8 | 529 | 737.10 | 274.34 | -2.0 | -16.80 | 66.24 | 274 |
| 18.2 | 10.8 | 14.4 | 14.0 | 12.4 | 9.2 | 46.80 | - |
| 13.0 | 5.2 | 18.6 | -4.2 | 5.2 | 7.2 |  | 1627 |
| 5.2 | 56.16 | -4.2 | $-58.80$ | 7.2 | 66.24 |  |  |
|  |  |  |  |  | 1627 |  |  |
| 9.4 |  | 39.6 | 67.7 | 280 | 740 |  |  |
| 3.2 |  | 28.1 | 6.8 | 460 |  |  |  |
| - |  | - |  | - | 2)2367 |  |  |
| 12.6 | 280 | 67.7 | 460.36 | 740 | 1184 | Answer in | ubic yards. |

At station 1, $h+h^{\prime}=18.6+5.2=23.8$, and in Table XL the number for $23: 8$ is $529 ; h=18.6$, and the number for 18.6 in Table XVI is $56.7 ; n=13.0$, and $56.7 \times 13.0=737.10 ; h^{\prime}=5.2$, and the number for 5.2 in Table XVI is $31.9 ; n^{\prime}=8.6$, and $31.9 \times 8.6=274.34 ;(c-e)$ $D+(d-f) E+(e-g) F+\left(c-e^{\prime}\right) D^{\prime}$ equal $(12.4-14.4) 8.4+(18.2$ $-13.0) 10.8+(14.4-18.6) 14.0+(12.4-5.2) 9.2=46.80$, and the
number for 46.80 in Table XXXVIII is 87 ; and $529+737+274+87$ $=162 \%$.

Since only three heights are taken at station 2, and $c=n=n^{\prime}$, the formula is reduced to :
$\left(h+h^{\prime}\right) \frac{B \times 100}{4 \times 27}+c\left[\left(\frac{h r}{2}+\frac{B}{4}\right) \frac{100}{27}+\left(\frac{h^{\prime} r}{2}+\frac{B}{4}\right) \frac{100}{27}\right]=$ cubic yards
for cross section of station 2.
In Table XL the number for $h+h^{\prime}$, or $9.4+3.2=12.6$, is 280 ; in Table XVI the number for height 9.4 is 39.6 , and the number for height 3.2 is 28.1 , and $39.6+28.1=67.7$; the product of 67.7 by center height 6.8 is 460.36 ; and $280+460=740$. Adding 740 to 1627 , the cubic yards for station 1, and diriding the sum by 2 , we have 1184, the answer in cubic yards.


## TABLE NO．I．

## Level Cross Sections．

## CUBIC YARDS IN CORRESPONDING PRISMS 100 FEET LONG．

Road－bed 10 feet wide．
Side slopes $1 \frac{1}{2}$ to 1.

|  |  | $\begin{aligned} & \text { 㤩 } \\ & \text { 嵌 } \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { 药 } \\ & \text { 荷 } \end{aligned}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 5. |  | 10.0 |  |  | 1806 | 20.0 | 2963 | － | 4398 | 30.0 | 6111 | 35.0 | 8102 |
| 0 |  | 5.1 | 333 | 10.1 | 941 | 15.1 | 1826 | 20.1 | 2989 | 25.1 | 4430 | 30.1 | 6148 | 35.1 | 8145 |
|  | 8 | 5.2 | 34 | 10.2 | 956 | 15.2 | 1847 | 20.2 | 3015 | 25.2 | 4461 | 30.2 | 6185 | 35.2 | 8187 |
| 0.3 | 12 | 5. | 352 | 10.3 | 971 | 15.3 | 1867 | 20.3 | 3041 | 25.3 | 4493 | 30.3 | 6223 | 35.3 | 8230 |
| 0 | 16 | 5. | 36 | 10.4 | 986 | 15.4 | 1888 | 20.4 | 3068 | 25.4 | 4525 | 30.4 | 6260 | 35.4 | 273 |
| 0. | 20 | 5. | 37 | 10.5 | 1001 | 15.5 | 1909 | 20.5 | 3094 | 25.5 | 4557 | 30.5 | 6298 | 35.5 | 8316 |
| 0. | 24 | 5. | 382 | 10 | 1017 | 15.6 | 1930 | 20.6 | 3121 | 25.6 | 4589 | 30.6 | 6335 | 35.6 | 8359 |
| 0.7 | 29 | 5. | 392 | 10.7 | 1032 | 15.7 | 1951 | 20.7 | 3147 | 25.7 | 4621 | 30.7 | 6373 | 35.7 | 8403 |
| 0.8 | 33 | 5. | 402 | 10.8 | 1048 | 15.8 | 1972 | 20.8 | 3174 | 25.8 | 4654 | 30.8 | 6411 | 35.8 | 8446 |
| 0.9 | 38 | 5.9 | 412 | 10.9 | 1064 | 15.9 | 1993 | 20.9 | 3201 | 25.9 | 4686 | 30.9 | 6449 | 35.9 | 8490 |
|  | 43 |  | 422 |  |  |  | 2 |  | 3228 | 26.0 | 4719 | 31.0 | 6487 | 36.0 | $\bigcirc 533$ |
|  | 47 | 6.1 | 43 | 11.1 | 1096 | 16.1 | 2036 | 21.1 | 3255 | 26.1 | 4751 | 31.1 | 6525 | 36.1 | 8577 |
|  | 52 | 6. | 443 |  | 1112 | 16.2 | 2058 | 21.2 | 3282 | 26.2 | 4784 | 312 | 6564 | 36.2 | 8621 |
| 1.3 | 58 | 6.3 | 454 | 11 | 1128 | 16.3 | 2080 | 21.3 | 3309 | 26.3 | 4817 | 31.3 | 6602 | 36.3 | 8665 |
|  | 63 | 6. | 465 |  | 1144 | 16.4 | 2102 | 21.4 | 3.337 | 26.4 | 4850 | 31.4 | 6641 | 36.4 | 8709 |
| 1.5 | 68 | 6.5 | 475 | 11.5 | 1161 | 16.5 | 2124 | 21.5 | 3364 | 26.5 | 4883 | 31.5 | 6679 | 36.5 | 8753 |
|  | 73 | 6.6 | 486 | 11.6 | 1177 | 16.6 | 2146 | 21.6 | 3392 | 26.6 | 4916 | 31.6 | 6718 | 36.6 | 8798 |
| 1.7 | 79 | 6.7 | 498 | 11.7 | 1194 | 16.7 | 2168 | 21.7 | 3420 | 26.7 | 4949 | 31.7 | 6757 | 36.7 | 8842 |
| 1.8 | 85 | 6.8 | 509 |  | 1211 | 16.8 | 2190 | 21.8 | 3448 | 26.8 | 4983 | 31.8 | 6796 | 36.8 | 8887 |
| 1.9 | 90 | 6.9 | 520 | 11.9 | 1227 | 16.9 | 213 | 21.9 | 3476 | 26.9 | 5016 | 31.9 | 6835 | 36.9 | 8931 |
|  | ， | 7.0 |  |  |  |  |  | 22．0 | 3504 | 27.0 | 5050 | 32．0 | 6874 | 3． | 8976 |
| 2.1 | 102 | 7.1 | 543 |  | 1262 | 17.1 | 2258 | 22.1 | 3532 | 27.1 | 5084 | 32.1 | 6913 | 37.1 | 9021 |
| 2.2 | 108 | 7.2 | 555 | 12 | 1279 | 17.2 | 2281 | 22.2 | 3560 | 27.2 | 5118 | 32.2 | 6953 | 37.2 | 9066 |
| 2.3 | 115 | 7.3 | 566 | 12.3 | 1296 | 17.3 | 2303 | 22.3 | 3589 | 27.3 | 5152 | 32.3 | 6992 | 37.3 | 9111 |
| 2.4 | 121 | 7.4 | 578 | 12.4 | 1313 | 17.4 | 2326 | 22.4 | 3617 | 27.4 | 5186 | 32.4 | 7032 | 37. | 9156 |
|  | 127 | 7.5 | 590 | 12.5 | 1331 | 17.5 | 2350 | 22.5 | 3646 | 27.5 | 5220 | 32.5 | 7072 |  | 9201 |
| 2.1 | 134 | 7.6 | 602 | 12.6 | 1349 | 17.6 | 2373 | 22.6 | 3675 |  | 5254 | 32.6 | 7112 | 37.6 | 9247 |
|  | 141 | 7.7 | 615 |  | 1366 | 17.8 | 2396 | 22.7 | 3703 | 27.7 | 5289 | 32.7 | 7152 | 37.7 | 9292 |
| 2.8 | 147 | 7.8 | 6. | 12.8 | 1384 | 17.8 | 2419 | 22.8 | 3732 | 27.8 | 5323 | 32.8 | 7192 | 37.8 | 9338 |
| 2.9 | 154 | 7.9 | 639 | 12.9 | 1402 | 17.9 | 2443 | 22.9 | 3762 | 27.9 | 5358 | 32.9 | 7232 | 37.9 | 9384 |
|  |  | 8． |  | 13 | 1420 | 18 | 2467 | 23.0 | 3791 | 28.0 | 5393 | 33.0 | 7272 | 38.0 | 9430 |
|  | 168 | 8. | cos |  | 1439 |  | 2490 | 23.1 | 3820 | 28.1 | 5427 | 33.1 | 7313 | 38.1 | 9476 |
| 3.2 | 175 | 8.2 | 677 | 13.2 | 1457 | 18.2 | 2514 | 23.2 | 3849 | 28.2 | 5462 | 33.2 | 7353 | 38．2 | 9522 |
|  | 183 | 8.3 | 690 | 13.3 |  |  | 2538 | 23.3 | 3879 | 28.3 | 5498 | 33.3 | 7394 | 38.3 | 9568 |
| 3. | 190 | 8.4 | 703 | 13 | 1494 | 18. | 2562 | 23.4 | 3909 | 28.4 | 5533 | 334 | 7435 | 38.4 | 9614 |
|  | 198 | 8.5 | 716 | 13.5 | 1513 |  | 2587 | 23.5 | 3938 | 28.5 | 5568 | 33.5 | 7475 | 38.5 | 9661 |
| 3 | 205 | 8.6 | 729 | 13.6 | 153 | 18.6 | 2611 | 236 | 3968 | 28.6 | 5603 | 33.6 | 7516 | 38.6 | 9707 |
|  | 213 | 8.7 | 743 | 13.7 | 1550 | 18.7 | 2635 | 23.7 | 3998 | 28.7 | 5639 |  | 7558 | 38.7 | 9754 |
| 0.8 | 221 | 8.8 | 756 | 13.8 | 1569 | 18.8 | 2660 | 23.8 | 4028 | 28.8 | 5675 | 33.8 | 7599 | 38.8 | 9801 |
| 3.9 | 229 | 8.9 | 770 | 13.9 | 1588 | 18.9 | 2685 | 23.9 | 4059 | 28.9 | 5710 | 33.9 | 7640 | 38.9 | 9847 |
|  | 237 | 9.0 | 78 | 14 | 1607 | 19.0 | 2709 | 24.0 | 4089 | 29.0 | 5746 | 34.0 | 7681 | 39.0 | 9894 |
| 4. | 240 | 9.1 | 79 | 14.1 | 1627 | 19.1 | 2734 | 24.1 | 4119 | 29.1 | 5782 | 34.1 | 7723 | 39.1 | 9942 |
|  | 254 | 9.2 | 811 | 14.2 | 1646 | 19.2 | 2759 | 24.2 | 4150 | 29.2 | 5818 | 34.2 | 7765 | 39.2 | 9989 |
| 4 | 262 | 9.3 | 825 | 14.3 | 1666 | 19.3 | 2784 | 24.3 | 4181 | 29.3 | 5855 | 34.3 | 7806 | 39.3 | 0036 |
| 4 | 271 | 9.4 | 839 | 14.4 | 1685 | 19.4 | 2809 | 24.4 | 4211 | 29.4 | 5891 | 34.4 | 7848 | 39.4 | 10083 |
| 4.5 | 279 | 9.5 | 853 | 14.5 | 1705 | 19.5 | 2835 | 24.5 | 4242 | 29.5 | 5927 | 34.5 | 7890 | 39.5 | 10131 |
| 4.6 | 288 | 9.6 | 868 | 14.6 | 1725 | 19.6 | 2860 | 24.6 | 4273 | 29.6 | 5964 | 34.6 | 「932 | 39.6 | 10179 |
| 4.7 | 297 | 9.7 | 882 | 14.7 | 1745 | 19.7 | 2886 | 24.7 | 4304 | 29.7 | 6001 | 34.7 | 7975 | 39.7 | 10226 |
| 4.8 | 306 | 9.8 | 897 | 14.8 | 1765 | 19.8 | 2911 | 24.8 | 4335 | 29.8 | 6037 | 348 | 8017 | 39.8 | 10274 |
| 4.9 | 315 | 9.9 | 911 | 14.9 | 1785 | 19.9 | 2937 | 24.9 | 4367 | 29.9 | 6074 | 34.9 | 8059 | 39.9 | 10322 |

TABLE NO．II．
Side Triangles．
CUBIC YARDS IN CORRESPONDING PRISMS 100 FEET LONG．
Road－bed 10 feet wide．
Side slopes $1 \frac{1}{2}$ to 1.

|  |  |  | $\begin{aligned} & \text { 䈍彩 } \end{aligned}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 009.3 |  | ． 0 | 15.0 | 50.9 | 20.0 | 64.8 | 25 | 78.7 | 30. | 92.6 | 35.0 | ． 5 |
| 0.19 .5 | 仡 | 10.137 .3 | 15． | 51.2 | 20.1 | 65.1 | 25.1 | 79.0 | 30.1 | 92.9 | 35.1 | 106.8 |
| 9.8 | 5.223 | 10.237 | 15 | 51.5 | 20.2 | 65.4 | 25.2 | 79.3 | 30.2 | 93.1 | 35. | 07.0 |
| 0.310 .1 | 5.324 .0 | 10.337 .9 | 15.3 | 51.8 | 20.3 | 65. | 25.3 | 79.5 | 30.3 | 93.4 | 35. | 107.3 |
| 0.410 .4 | 5.424 .3 | 10.438 .1 | 15.4 | 52.0 | 20.4 | 65.9 | 25.4 | 79. | 30.4 | 93.7 | 35. | 107.6 |
| 0.510 .6 | 5.524. | 10.538 .4 | 15.5 | 52.3 | 20.5 | 66.2 | 25.5 | 80.1 | 30.5 | 94.0 | 35. | 107.9 |
| 610.9 | 5.624. | 10.638 .7 | 15.6 | 52.6 | 20.6 | 66.5 | 25.6 | 80.4 | 30.6 | 94.3 | 35.6 | 108.1 |
| \％ 11.2 | 5．725 | 10.739 .0 | 15.7 | 52.9 | 20.7 | 66.8 | 25.7 | 80.6 | 30.7 | 94.5 | 35. | 08.4 |
| 811.5 | 5.825 | 10.839 .3 | 15.8 | 53.1 | 20.8 | 67.0 | 25.8 | 80.9 | 30.8 | 94.8 | 35 | 8108.7 |
| 0.911 .8 | 5.925 | 10.939 .5 | 15.9 | 53.4 | 20.9 | 67.3 | 25.9 | 81.2 | 30.9 | 95.1 | 35. | 09.0 |
|  |  |  |  | 53.7 | 21.0 | 67.6 | 26 | 81.5 | ． | ． 4 |  |  |
| 112.3 | 6.126 | 11.140 .1 | 16.1 | 54.0 | 21.1 | 67.9 | 26.1 | 81 | 31.1 | 95. |  | 9.5 |
| 212.6 | 6.226 | 11.240 .4 | 16.2 | 54. | 21.2 | 68.1 | 26.2 | 82 | 31.2 | 95.9 | 36 | 109.8 |
| ． 312.9 | 6．3 26．8 | ． 340.6 | 16.3 | 54.5 | 21.3 | 68.4 | 26.3 | 82. | 31.3 | 96.2 | 36. | 110.1 |
| ． 413.1 | 6.427 .0 | 11.440 .9 | 16.4 | 54.8 | 21.4 | 68.7 | 26.4 | 82. | 31.4 | 96. | 36.4 | 110.4 |
| 513.4 | 6.527 .3 | 11.541 .2 | 16.5 | 55.1 | 21.5 | 69.0 | 26.5 | 82.9 | 31.5 | 96.8 | 36 | 110.6 |
| 613.7 | 6.627 .6 | 11.641 .5 | 16.6 | 55.4 | 21.6 | 69.3 | 26.6 | 83.1 | 31.6 | 97. | 36.6 | 110.9 |
| 714.0 | 6． 727.9 | 11.741 .8 | 16.7 | 55.6 | 21.7 | 69.5 | 26.7 | 83.4 | 31.7 | 97.3 | 36 | 111.2 |
| 1.814 .3 | 6.828 .1 | 11.842 .0 | 16.8 | 55. | 21.8 | 69. | 26.8 | 83.7 | 31.8 | 97.6 | 36 | 111.5 |
| ． 914.5 | 6.928 | 11.942 .3 | 16.9 | 56. | 21.9 | \％0． | 26.9 | 84.0 | 31.9 | 97.9 | 36.9 | 111.8 |
| 014.8 | 7.028 .7 | 12.042 .6 | 17.0 | 56.5 | 22.0 | r0．4 | 27.0 | 84.3 | 32.0 | 98.1 |  | 112.0 |
| 115.1 | 7.1290 | 12.142 .9 | 17.1 | 56.8 | 22.1 | 70.6 | 27.1 | 845 | 32.1 | 98. | 37.1 | 112.3 |
| 2.215 .4 | 7.229 .3 | 12.243 .1 | 17.2 | 57.0 | 22.2 | 70.9 | 27.2 | 84.8 | 32.2 | 98.7 | 7.2 | 112.6 |
| 315.6 | 7.329 .5 | 12.343 .4 | 17.3 | 57.3 | 22.3 | 71.2 | 27.3 | 85.1 | 32.3 | 99.0 | 37.3 | 112.9 |
| 415.9 | 7.429 .8 | 12.443 .7 | 17.4 | 57.6 | 22. | 71.5 | 27.4 | 85.4 | 32.4 | 99.3 |  | 13.1 |
| 516.2 | 7.530 | 12.544 .0 | 17 | 57 | 22 | 71 | 27. | 85 | 32.5 | 99.5 |  | ． 4 |
| 16.5 | 7.630 .4 | 12.644 .3 | 17.6 | 58 | 22.6 | 72 | 27.6 | 85.9 | 32.6 | 99.8 | 37.6 | 13.7 |
| 716.8 | 7.730 .6 | 12.744 .5 |  | 58. | 22.7 | 72．3 | 27.7 | 86.2 | 32.7 | 100.1 |  | 14.0 |
| 2.817 .0 | 7.830 .9 | 12.844 .8 | 17.8 | 58.7 | 22.8 | 72.6 | 27.8 | 86.5 | 32.8 | 100.4 | 3 | 114.3 |
| 2.917 .3 | 7.931 .2 | 12.945 .1 | 17.9 | 59.0 | 22.9 | 72.9 | 27.9 | 86.8 | 32.91 | 100.6 | 37 | 114.5 |
|  | 8．0 |  |  |  |  | 73.1 |  | 87.0 | 33.01 | 100.9 |  | 4.8 |
| 117.9 | 8.131 | 13.145 .6 | 18.1 | 59.5 | 23.1 | 73.4 | 28.1 | 87.3 | 33.1 | 101.2 |  | ． 1 |
| 218.1 | 8.232 .0 | 13.245 .9 | 18.2 | 59.8 | 23.2 | 73.7 | 28.2 | 87.6 | 33.2 | 101.5 |  | 15.4 |
| 318.4 | 8.332 .3 | 13.346 .2 | 18.3 | 60.1 | 23.3 | 74.0 | 28.3 | 87.9 | 33.31 | 101.8 | 38.3 | 115.6 |
| 418.7 | 8.4 32． 6 | 13.446 .5 | 18.4 | 60.4 | 23.4 | 74.3 | 284 | 88.1 | 33.4 | 102.0 | 38.4 | 115.9 |
| 3.519 .0 | 8.532 .9 | 13.546 .8 | 18.5 | 60.6 | 23.5 | 74.5 | 28.5 | 88.4 | 33.51 | 102.3 | 38.5 | 116.2 |
| 3.619 .3 | 8.633 | 13.647 .0 | 18.6 | 60.9 | 23.6 | 74.8 | 28.6 | 88.7 | 33.6 | 102.6 | 3．6 | 116.5 |
| 3.719 .5 | 8.733 .4 | 13.747 .3 | 18.7 | 61.2 | 23.7 | 75.1 | 28. | 89.0 | 33.71 | $10 \% .9$ | 3． | 116.8 |
| 3.819 .8 | 8.833 .7 | 13.847 .6 | 18.8 | 61.5 | 23.8 | 75.4 | 28.8 | 89.3 | 33.8 | 103.1 | 38.8 | 117.0 |
| ． 920.1 | 8.934 .0 | 13.947 .9 | 18.9 | 61.8 | 23.9 | 75. | 28.9 | 89.5 | 33.91 | 103.4 | 9 | 117.3 |
| 020.4 | 9．0 | 14.04 R． 1 | 19.0 | 62.0 | 24.0 | 75.9 | 29.0 | 89.8 | 34.0 | 103.7 | 39.0 | 117.6 |
| 120.6 | 9.134 .5 | 14.148 .4 | 19.1 | 62.3 | 24.1 | 76.2 | 29.1 | 90.1 | 34.1 | 104.0 | 39.1 | 117.9 |
| 4.220 .9 | 9. | 14.248 .7 | 19.2 | 62.6 | 24.2 | 76.5 | 29.2 | 90.4 | 34.2 | 104.3 | 39.2 | 118.1 |
| 321.2 | 9.335 .1 | 14.349 .0 | 19.3 | 62.9 | 24.3 | 76.8 | 29.3 | 90.6 | 34.3 | 104.5 | 39.3 | 118.4 |
| 4.421 .5 | 9.435 .4 | 14.449 .3 | 19.4 | 63.1 | 24.4 | 77.0 | 29.4 | 90.9 | 34.41 | 104.8 | 39. | 118.7 |
| 4.521 .8 | 9.535 .6 | 14.549 .5 | 19.5 | 63.4 | 24.5 | 77.3 | 29.5 | 91.2 | 34.5 | 105.1 | 39. | 19.0 |
| 4.622 .0 | 9.635 .9 | 14.649 .8 | 19.6 | 63.7 | 24.6 | 77.6 | 29.6 | 91.5 | 34.6 | 105.4 | 39.6 | 19.3 |
| 4.7 22．3 | 9736.2 | 14.750 .1 | 19.7 | 64.0 | 24.7 | 77.9 | 29.7 | 91.8 | 34.7 | 105.6 | 39.7 | 119.5 |
| 822.6 | 9.836 .5 | 14.850 .4 | 19.8 | 64.3 | 24.8 | 78.1 | 29.8 | 92.0 | 34.8 | 105.9 | 39.8 | 19.8 |
| 922.9 | 93 | 14.950 .6 | 19.9 | 64.5 | 24.9 | 78.4 | 29.9 | 92.3 | 34.91 | 106.2 | 39.9 | 120.1 |

## TABLE NO．III．

## Level Cross Sections．

## CUBIC YARDS IN CORRESPONDING PRISMS 100 FEET LONG．

Road－bed 14 feet wide．
Side slopes $1 \frac{1}{2}$ to 1.

| $\begin{aligned} & \text { 蒌 } \\ & \text { 要 } \end{aligned}$ |  |  |  | 開 |  |  | $\begin{aligned} & \text { Oixi in in } \\ & \text { Bign } \end{aligned}$ |  |  |  |  |  |  | $\begin{aligned} & \text { 范感 } \\ & \text { R } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 |  | 398 | 10 | 1074 | 15.0 | 2028 | 20.0 | 3259 | 25.0 | 4769 | 30.0 | 6556 | 35.0 |  |
|  | 5 |  | 409 | 10.1 | 1090 | 15.1 | 2050 | 20.1 | 3287 | 25. | 4802 | 30.1 | 6594 |  | 65 |
|  | 11 | 5.2 | 420 | 10.2 | 1107 | 15.2 | 2072 | 20.2 | 3314 | 25.2 | 4835 | 30.2 | 6633 | 35.2 | 8709 |
|  | 16 | 5.3 | 431 | 10.3 | 1123 | 15.3 | 2094 | 20.3 | 3342 | 25.3 | 4868 | 30.3 | $66{ }^{2}$ | 35.3 | 8753 |
| 0.4 | 22 | 5.4 | 442 | 10.4 | 1140 | 15.4 | 2116 | 20.4 | 3370 | 25.4 | 4901 | 30.4 | 6711 | 35.4 | 8798 |
|  | 27 | 5.5 | 453 | 10.5 | 1157 | 15.5 | 2138 | 20.5 | 3398 | 25.5 | 4935 | 30.5 | 6750 | 35 | $884 \%$ |
|  | 33 | 5.6 | 465 | 10.6 | 1174 | 15.6 | 2161 | 20.6 | 3426 | 25.6 | 4968 | 30.6 | 6789 | 35.6 | 887 |
|  | 39 | 5.7 | 476 | 10.7 | 1191 | 15.7 | 2183 | 20.7 | 3454 | 25.7 | 5002 | 30.7 | 6828 | 35.7 | 8932 |
|  | 45 | 5.8 | 488 | 10.8 | 1208 | 15.8 | 2206 | 20.8 | 3482 | 25.8 | 5036 | 30.8 | 6867 | 35.8 | 8977 |
| 0.9 | 51 | 5.9 | 499 | 10.9 | 1225 | 15.9 | 2229 | 20.9 | 3510 | 25.9 | $50 \% 0$ | 30.9 | 6507 | 35.9 | 9022 |
|  | 57 | 6.0 | 51 |  | 1243 | 16 | 2252 | 21.0 | 3539 | 26. | 5104 | 31.0 | 6946 | ． 0 | 9067 |
|  | 64 | 6.1 | 523 | 11 | 1260 | 16.1 | 2275 | 21.1 | 3567 | 26.1 | 5138 | 31.1 | 6986 | 36.1 | 9112 |
|  | 70 | 6.2 | 535 | 11.2 | 1278 | 16.2 | 2298 | 21.2 | 3596 | 26.2 | 5172 | 31.2 | 7026 | 36. | 9157 |
|  | 77 | 6.3 | 547 | 11.3 | 1295 | 16.3 | 2321 | 21.3 | 3625 | 26.3 | 520 | 31.3 | 7066 | 36. | 9203 |
|  | 83 | 6.4 | 559 | 11.4 | 1313 | 16.4 | 2345 | 21.4 | 3654 | 26.4 | 5241 | 31.4 | 7106 | 36. | 9248 |
|  | 90 | 6.5 | 572 | 11.5 | 1331 | 16.5 | 2368 | 21.5 | 3683 | 26.5 | 5275 | 31.5 | 7146 | 36.5 | 9294 |
| 1.6 | 97 | 6.6 | 584 | 11.6 | 1349 | 16.6 | 2392 | 21.6 | 3712 | 26.6 | 5310 | 31.6 | 7186 | 36.6 | 9340 |
|  | 104 | 6.7 | 597 | 11.7 | 1367 | 16.7 | 2415 | 21.7 | 3741 | 26. | 534 | 31.7 | 722 | 36.7 | 86 |
|  | 111 | 6.8 | 609 | 11. | 1385 | 16.8 | 2439 | 21.8 | 3771 | 26. | 538 | 31.8 | 720 | 36 | 32 |
| 1.9 | 119 | 6.9 | 622 | 11.9 | 1404 | 16.9 | 2463 | 21.9 | 3800 | 26. | 54 | 31. | 7307 | 36 | 78 |
|  | 126 | 7.0 | 635 | 12.0 | 1422 | 17.0 | 2487 | 22.0 | 3830 | 27．0 | 5450 | 32.0 | 7348 | 37.0 | 9524 |
| 2.1 | 133 | 7.1 | 648 | 12.1 | 1441 | 17.1 | 2511 | 22.1 | 3859 | 27. | 5485 | 32.1 | 7389 | 37. | 9570 |
|  | 141 | 7.2 | 661 | 12.2 | 1459 | 17.2 | 2535 | 22.2 | 3889 | 27.2 | 5521 | 32.2 | 7430 |  | 9617 |
|  | 149 | 7.3 | 675 | 12.3 | 1478 | 17.3 | 2560 | 22.3 | 3919 | 27.3 | 555 | 32.3 | 7471 |  | 63 |
|  | 156 | 7.4 | 688 | 12.4 | 1497 | 17.4 | 2584 | 22.4 | 3949 |  | 559 | 32.4 | 7512 | 37.4 | 10 |
|  | 164 | 7.5 | 701 | 12.5 | 1516 | 17 | 2609 | 22.5 | 3979 | 27 | 5627 | 32 | 75 | 37.5 | 57 |
|  | 172 | 7.6 | 715 | 12.6 | 1535 | 17. | 2633 | 22.6 | 4009 | 27.6 | 566 | 32.6 | 7595 | 37. | 9804 |
| 2.7 | 181 | 7.7 | 729 | 12.7 | 155： | 17.7 | 2658 | 22.7 | 4040 | 27.7 | 5699 | 32.7 | 7636 | 37. | 9851 |
| 2.8 | 189 | 7.8 | 74．3 | 12.8 | 1574 | 17.8 | 2683 | 22.8 | 4070 | 27.8 | 573 | 32.8 | 7678 | 37.8 | 9898 |
| 2.9 | 197 | 7.9 | 756 | 12.9 | 1593 | 17.9 | 2708 | 22.9 | 4101 | 27.9 | 5771 | 32.9 | 7719 | 37.9 | 45 |
|  | 206 | 8.0 | 770 | 13.0 | 1613 | 18.0 | 2733 | 23.0 | 4131 | 28.0 | 5807 | 33.0 | 7761 |  | 9993 |
|  | 214 | 8.1 | 785 |  | 1633 | 18.1 | 2759 | 23.1 | 4162 | 28.1 | 5844 | 33.1 | 7803 |  | 10040 |
| 3.2 | 223 | 8.2 | 799 | 13.2 | 1652 | 18.2 | 2784 | 23.2 | 4193 | 28.2 | 5880 | 33.2 | 7845 | 38.2 | 0088 |
| 3.3 | 232 | 8.3 | 813 | 18.3 | 1672 | 18.3 | 2809 | 23.3 | 4224 | 28.3 | 5917 | 33.3 | 7887 |  | 0135 |
| 3.4 | 241 | 8.4 | 828 | 13.4 | 1692 | 18.4 | 2835 | 23.4 | 4255 | 28.4 | 5953 | 33.4 | 7929 |  | 183 |
| 3.5 | 250 | 8.5 | 843 | 13.5 | 1713 | 18.5 | 2861 | 23.5 | 4287 | 28.5 | 5990 | 33.5 | 7972 | 38.5 | 0231 |
| 3.6 | 259 | 8.6 | 857 | 13.6 | 173 | 18.6 | 288 | 23.6 | 4318 | 28.6 | 6027 | 33.6 | 8014 | 38.6 | 0279 |
|  | 268 | 8.7 | 872 | 13.7 | 170 | 18.7 | 2912 | 23.7 | 4349 | 28.7 | 6064 | 33. | 8057 | 38.7 | 0327 |
| ． 8 | $27 \%$ | 8.8 | 887 | 1.8 | 174 | 18.8 | 2938 | 23.8 | 4381 | 28.8 | 6101 | 33.8 | 8099 | 38.8 | 0375 |
| 3.9 | 287 | 8.9 | 902 | 13.9 | 1794 | 18.9 | 2965 | 23.9 | 4413 | 28.9 | 6139 | 33.9 | 8142 | 38.9 | 0424 |
|  | 2 | 9.0 | 917 | 14.0 | 1815 | 19.0 | 2991 | 24.0 | 4444 | 29.0 | 6176 | 34.0 | 8185 | 39.0 | 472 |
|  | 306 | 9.1 | 932 | 14.1 | 1836 | 19.1 | 3017 | 24.1 | 4476 | 29.1 | 6213 | 34.1 | 8228 | 39. | 0521 |
| 2 | 316 | 9.2 | 947 | 14.2 | 185 | 19.2 | 3044 | 24.2 | 4508 | 29.2 | 6251 | 34.2 | 8271 | 39.2 | 0569 |
| 4.3 | 326 | 9.3 | 963 | 14.3 | 1878 | 19.3 | 3070 | 24.3 | 4541 | 29.3 | 6288 | 34.3 | 8315 | 39.3 | 618 |
| 4.4 | 336 | 9.4 | 978 | 14.4 | 1899 | 19.4 | 3097 | 24.4 | 4573 | 29.4 | 6326 | 34.4 | 8358 | 39.4 | 0667 |
| 4.5 | 316 | 9.5 | 994 | 14.5 | 1920 | 19.5 | 3124 | 24.5 | 4605 | 29.5 | 6364 | 34.5 | 8401 | 39 | 0716 |
| 4.6 | 356 | 9.6 | 1010 | 14.6 | 1941 | 19.6 | 3151 | 24.6 | 4638 | 29.6 | 6402 | 34.6 | 8445 | 39 | 765 |
| 7 | 366 | 9.7 | 1026 | 14.7 | 1963 | 19.7 | 3178 | 24.7 | 4670 | 29.7 | 6441 | 34.7 | 8489 | 39.7 | 0815 |
| ． 8 | 377 | 9.8 | 1042 | 14.8 | 1984 | 19.8 | 3205 | 24.8 | 4703 | 29.8 | 6479 | 34.8 | 8532 | 39.8 | 10864 |
| 4.9 | 387 | 9.9 | 1058 | 14.9 | 2006 | 19.9 | 3232 | 24.9 | 4736 | 29.9 | 6517 | 34.9 | 8576 | 39.9 | 10913 |

TABLE NO. IV.
Side Triangles.
CUBIC FARDS IN CORRESPONDING PRISMS 100 FEET LONG.

Road-bed 14 feet wide.
Side slopes $1 \frac{1}{2}$ to 1 .


## TABLE NO．V．

## Level Cross Sections．

## CUBIC YARDS in CORRESPONDING PRISMS 100 FEET LONG．

Road－bed 18 feet wide．
Side slopes $1 \frac{1}{2}$ to 1.

|  | 粆萢 | $\begin{aligned} & \text { 药 } \\ & \text { 㤩 } \end{aligned}$ |  |  |  | む̈ |  |  |  | 『 |  |  | O. | $0$ | $\begin{aligned} & \text { ed } \\ & \text { E. } \\ & \text { din } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 |  |  |  | 122： |  | 22.5 |  | 3.56 |  |  |  |  | 35.0 |  |
|  | 7 |  | 485 | 10.1 | 1240 | 15.1 | 22.3 | 201 | $35 \succ 5$ | 25. | 5173 | 30.1 | 7040 | 35 | 918．5 |
|  | 14 | 5.2 | 49 i | 10 | 1258 | 15.2 | 2＊97 | 20.2 | 361.1 | 25 | 5208 | 30.2 | 7080 | 35 | － |
|  | 21 | 5.3 | 09 | 10.8 |  | 15.3 | 232 | 20.3 | 3643 | 25.3 | 5243 | 30.3 | 7121 | 35 | 9276 |
|  | 28 | 5 | 522 | 10. | 1294 | 15 | 2344 | 20.4 | 3672 | 25.4 | 52 | 30.4 | 7161 | 35.4 | 2 |
|  | 35 | 5.5 | 535 | 10. | 1：313 | 15 | 2368 | 20.5 | 3701 | $2 \overline{5}$. | 5313 | 30.5 | 7201 | 3．） | 9368 |
|  | 42 | 5 | 548 | 10.6 | 1331 | 15.6 | 2392 | 20.6 | 378 | 25.6 | 5348 | 30.6 | 7242 | 35.6 | 14 |
|  | 49 | 5 | 561 | 10.7 | 1349 | 15.7 | 2416 | 20.7 | 3761 | 25.7 | 5383 | 30.7 | 7283 | 35 | 9461 |
|  |  |  | 574 | 10.8 | 1368 | 15.8 | 2440 | 20.8 | 3790 | 2 j .8 | 5418 | 30.8 | 7324 | 35.8 | 9507 |
| 0.9 | 65 | 5 |  | 10.9 | 13 | 159 | 2465 | 20.9 | $38: 0$ | 25.9 | 5433 | 30.9 | 7365 | 35.9 | 9553 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 00 |
|  | 80 | 6 | 613 | 11 | 1425 | 16.1 | 51 | 21 | 3880 | $\because 0$ | 5.525 | 31.1 | 7447 | 36.1 | 47 |
|  | 8 | 0 |  |  | 1444 | 16 | 2538 | 21 | 391 | 26 | 5560 |  | 7488 | 36.2 | 694 |
| 1.3 | 96 | 6 | 641 | 11. | 146： | 11.3 | 256 | 21 | 3941 | 26 | 5.596 |  | $75 \geqslant 9$ | 36 | 741 |
|  | 104 |  |  | －11．4 | 148： |  | 2588 |  | 39 | 26 | 5632 |  | 7571 | 36.4 | 88 |
|  | 113 |  |  | 11.5 | 1501 | 16.5 | 613 | $\sim 1.5$ | 400 | $\because 6$ | 5668 | 31.5 | 7613 | 36.5 | 9835 |
|  | 121 |  |  | 116 | 1521 | 16.6 |  |  | $403 \%$ | 26 | 5704 | 31.6 | r654 | 36.6 | 882 |
|  | $\pm 9$ |  | 696 | 11.7 | 1541 |  | 66 |  | 4063 | $\because 6$ ． | $5 \% 41$ |  | 7696 | 36.7 | 9929 |
|  | 138 | 6 | 710 | 11．i | 1560 | 16.8 | 2688 |  | 4094 |  | 577 |  | 7738 | 36.8 | 9977 |
| 1.9 | 147 | 6.9 | 725 | 11.9 | 1550 | 16.9 | 2713 | 21.9 | 4125 | 26 | 5813 | 31.9 | 7780 | 36. | 0025 |
|  | 帾 | 7.0 |  | 12.0 |  |  |  | 22.0 |  | 27.0 |  | －3．0 | 2 |  |  |
|  | 165 | 7.1 |  | 12.1 | 1600 | 17.1 | 2765 | 22.1 | 41 |  |  | 32.1 | 6.5 |  |  |
| 2.2 | 17 | 7. |  | 12 | 1640 |  |  | ごこ．2 | 421 |  | 5924 |  | 790\％ |  |  |
|  | 183 | 7.3 | 8 | 12.3 | 1661 | 17.3 | Y1 | 22． 3 | $4: 49$ | 27 | 5961 | 32.3 | 7949 |  | 6 |
| 2.4 | $19:$ | 7.4 |  | 12.4 | 1681 | 17.4 | 842 | 22.4 | 析 |  | 5998 | 33.4 | 99： |  |  |
|  | 201 | 7.5 |  | 12.5 | 1701 | 17.5 | 868 | 22.5 | 431 |  | 603．） | 32.5 | 8035 |  | 313 |
| 2.6 | 211 | 7.6 | 828 | 12.6 | 172\％ | 17.6 | 2894 | 22．6 | 4344 |  | 607： | 32.6 | 8078 |  | 61 |
|  | 221 | 7.7 | 843 | 12.7 | 1743 | 17.7 | 2921 | 32． 7 | 4376 |  | 6109 | 3こ． | 8121 |  | 409 |
|  | 230 | 7.8 | 858 | 12.8 |  |  | 2947 | 2.2 | 4408 |  | 6147 |  | 8164 |  |  |
| 2.9 | 240 | 7.9 | 873 | 12.9 | 1785 | 17.9 | 2973 | 22.9 | 4440 | 27.9 | 6185 | 32.9 | 8207 |  |  |
|  | 20 | 8 | 88 | 13 | 1 | 18.0 | 31 | 23.0 | 4412 |  | 6222 | O3． | 8250 |  |  |
|  | 260 |  | 905 |  |  |  |  |  |  |  |  |  | 8293 |  |  |
|  | 270 | 8.2 | 920 | 13 | 1848 | 18 | 3054 | 23.2 | 57 | 28.2 | $6 \div 98$ |  | 8337 |  |  |
|  | －81 |  | 936 | 13 | 1869 |  | 3081 | $\stackrel{2}{2} .3$ | 569 |  | 6336 |  | 8381 |  |  |
|  | 2 | 8. | 95 | 13. | 1891 | 18.4 | 3108 | 23.4 | 4602 |  | 6374 |  | 8494 |  |  |
|  | 301 | 8.5 | 968 | 13.5 | 1913 |  | 3135 | 23.5 | 4635 |  | 6413 |  | 8468 |  |  |
|  | ～ | 8.6 | 984 | 13．6 | 1934 |  |  | 23.6 | 4668 | 28.6 | 6451 |  | 8512 |  |  |
| 37 | 323 | 8.7 | 1001 | 13.7 | 19.6 | 18.7 | 3189 | 23.7 | $4 \% 01$ | 28.7 | 6489 | 33.7 | 8556 |  |  |
| 3.8 | 334 | 8.8 | 1017 | 13.8 | 1978 | 18.8 | 3217 | $\because 3.8$ | 4734 | 28.8 | $65 \geqslant 8$ | 33.8 | 8600 |  |  |
| 3.9 | $34{ }^{\prime \prime}$ | 8.9 | 1033 | 13.9 | 2000 | 18.9 | 3245 | 23.9 | 4767 | 28.9 | 6567 | 33.9 | S645 | 38 |  |
| 4.1 |  |  |  | 14. | 2022 | 19.0 | 2 | 24.0 | ， | 29.0 | 6606 | 34.0 | 8689 |  | 50 |
|  | 367 | 9. | 1067 | 14.1 | 204.$)$ | 19.1 | 0 |  | 㖪 | 29.1 | － | 34.1 | 8 |  |  |
| ． | 8 | 9. | 1084 | 14.2 | 2067 |  | 3328 | $\bullet 4.2$ | 867 | 29.2 | 6684 | 34.2 | 8778 |  | 150 |
| ， | 9 | 9 | 1101 | 14. | 2089 | 19.3 | 3350 | 243 | 901 | 29.3 | 6723 | 34.3 | 8823 |  | －1 |
| 4.4 | 1 | 9 | 1118 | 14. | 2112 | 19. | 3384 | 24.4 | 934 | 29.4 | 62 | 34.4 | 8868 |  | ， |
| ， | 13 | 9. | 1135 |  | 2135 | 19.5 | 3413 | 24.5 | 968 | 29.5 | 801 | 34.5 | 8913 |  |  |
| 4.6 | 424 | 9. | 1152 | 14.6 | 2158 | 19.6 | $3+41$ | 24.6 | （1）2 | 29.6 | 6841 | 34.6 | 8958 | 39 | 1352 |
| 4.7 | 436 | 9.7 | 1169 | 14.7 | 181 | 19.7 | 3469 | 24.7 | 036 | 29．7 | 6881 | 34.7 | 9003 | 39 | 403 |
| ． | 448 | 9.8 | 1187 | 14.8 | 2204 | 19.8 | 3498 | 24．8 | $50 \%$ | 29.8 | 6920 | 34. | 9048 | 39 | 1454 |
| 4.9 | 460 | 9.9 | 1205 | 14.9 | 222\％ | 19.9 | 3527 | 24.9 | 5105 | 29.9 | 6960 | 34.9 | 9093 | 39.9 | 11505 |

TABLE NO．VI．

## Side Triangles．

CUBIC YARDS IN CORRESPONDING PRISMS 100 FEET LONG．

Road－bed 18 feet wide．
Side slopes $1 \frac{1}{2}$ to 1 ．

|  |  |  | $\begin{aligned} & \text { gis } \\ & \text { 気感 } \end{aligned}$ |  | $\begin{aligned} & \text { 触薄 } \end{aligned}$ |  | $\begin{aligned} & \text { 然䓵感 } \end{aligned}$ | 우눌 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16. |  | 30.8 |  | 44.7 | 15 | 58.6 | 20.1 | \％2．5 | 25.1 | 86.4 | 30.1 | 100.3 | 35.11 | 114.2 |
| 17. |  | 31.1 | 10.2 | 45.0 | 15.2 | 58.9 | 20.2 | T2． 8 | 25.2 | 86.7 | 30.2 | 100.6 | 5． 2 |  |
| 317.5 | 5.3 | 31.4 | 10.3 | 45.3 | 15.3 | 59.2 | 20.3 | 73.1 | 25.3 | 86.9 | ：0．3 | 100.8 | 35.3 | 3114.7 |
| 0.417 .8 | 5.4 | 431.7 | 10.4 | 45.6 | 15.4 | 59.4 | 20.4 | 73.3 | 25. | 87.2 | 30.4 | 01.1 |  | 4115.0 |
| 518.1 | 5.5 | 31.9 | 10.5 | 45. | 15.5 | 59.7 | 20.5 | 73.6 | 25 | 87.5 | 30.5 | 101.4 | 35.5 | 5115.3 |
| 618.3 | 5.6 | （3．） | 10.6 | 46.1 | 15.6 | 60.0 | 20.6 | 73.9 | 2.5 | 87. | 30.6 | 101.7 |  | 6115.6 |
| 18. |  | 32.5 | 10. | 46.4 | 15 | 60.3 | 20.7 | 74.2 | －5 | 88 | 30.7 | 101.9 | 35.7 | 115.8 |
| 818.9 |  | 832.8 | 10.8 | 46.7 | 15.8 | 60.6 | 20.8 | 74.4 | 25.8 | 88.3 | 30.8 | 102. | 35.8 | 116.1 |
| 919.2 | 5.9 | 33.1 | 10 | 46.9 | 15.9 | 60.8 | 20.9 | 74.7 | 25.9 | 88.6 | 30.9 | 102.5 | 35.9 | 9116．4 |
|  |  |  |  |  |  |  |  |  |  | 88 |  |  |  |  |
| 19 |  | 33.6 |  | 4 | 16. | 61.4 |  | －5 | 215 | 89 | 31.1 | 103 |  |  |
| 20.0 |  | 33 | 11.2 | 47 | 16.2 | 61.7 | 21.2 | 75 | 26.2 | 89 | 31.2 | 103. | 36.2 | 2117.2 |
| 20.3 |  | 34.2 | ． | 48.1 | 10.0 | 61. | 21.3 | 75. | 26.3 | 89. | 31.3 | 103. | 6. | 7.5 |
| 420.6 |  | 54.4 | 11.4 | 48.3 | 16.4 | 62.2 | 21.4 | 76. | 26.4 | 90. | 31.4 | 108 | 6. |  |
| 520.8 | 6.5 | 534. | 11.5 | 48.6 | 16.5 | 62.5 | 21.5 | 76. | 26.5 | 90. | 31.5 | 104 | 36.5 | 有 |
| 621.1 | 6.6 | 35. | 11.6 | 48.9 | 16.6 | 62.8 | 21.6 | 76. | 26. | 90.6 | 31.6 | 104 | 36.6 |  |
| 721.4 | 6. | 35. | 11.7 | 49.2 | 16.7 | 63.1 | 21.7 | 76. | 26. | 90. | 31. | 104.7 | 36.7 | \％ |
| 821.7 |  | 35 | 11. | 49 | 16.8 | 63. | 21.8 | 77 | 26 | 91. | 31. | 105.0 | 36.8 |  |
| 921.9 |  |  | 11.9 | 49.7 | 16.9 | 63 | 21.9 | 77 | 26.9 | 91 | 31 |  | 36.9 |  |
| 22．2 |  |  |  | 50. |  | 3．9 |  |  |  | 91. | 2.0 | 05 | \％ | 19.4 |
| 122.5 | 7. | 36. | 12.1 | 50.3 | 17.1 | 64.2 | 22.1 | 78. | 27.1 | 91.9 | 32． 1 | 105 | 37 | 1119.7 |
| 222.8 | 7.2 | 36.7 | 12.2 | 50.6 | 17.2 | 64.4 | 22.2 | 78.3 | 27.2 | 92.2 | 32.2 | 106 |  | ． |
| 23． 1 | 7.3 | 36.9 | 12.3 | 50.8 | 17.3 | 64.7 | $2 \cdot 3$ | 78.6 | 27. | 92. | 32. | 106 |  |  |
| 23.3 | 7.4 | －7 |  | 51. | 17.4 | 65 |  | 78. | 27. | 92 | 32 | 106.7 |  | 4120.6 |
| 23 |  | 537.5 |  |  |  |  | 22 | 79 |  | 93 | 32.5 |  |  | 5120.8 |
| 2.623 .9 | 7.6 | 67．8 |  | 51. | 17 | 65 | 22.6 |  |  | 93.3 |  | 107 |  | 121.1 |
| 2.724 .2 | 7.7 | 38 | 12.7 | 51.9 |  |  | 22.7 |  |  | 93 |  | 07 |  | 121.4 |
| 2824.4 | 7.8 | 838. | 12.8 | 52.2 | 17.8 | 66.1 | 22.8 | 80.0 | 27. | 93.9 | 32.8 | 107.8 |  | 121.7 |
| 2.924 .7 | 7.9 |  | 12.9 | 52.5 | 17.9 | 66.4 | 22.9 | 80.3 | 27. | 94.2 | 32.9 |  |  |  |
| 2 |  |  |  |  |  |  |  |  |  | 94 | ． 0 | 1 |  |  |
| 2.5 |  |  |  |  | 18.1 | 66.9 |  | 80. | 28.1 | 94.7 | 33.1 | 108.6 | ， |  |
| 225.6 | 8.2 | 39 | 13.2 | 3. | 18.2 | － | 23.2 | 81. |  | 95.0 | $3: 3.2$ | 108.9 |  |  |
| 325.8 | 8.3 | 39.7 | 13.3 | 53.6 | 18.3 | 67.5 | 23.3 | 81. | $\because 8.3$ | 95. | 333 | 109 |  | 123．1 |
| 3.426 .1 | 8.4 | 40.0 | 13. | 53．9 | 18.4 | 67.8 | 23.4 | 81. | 28.4 | 9.5 | 33.4 | 109 |  |  |
| 26 | 8 | 40 | 13 | 54.2 | 18.5 | 68. | 23.5 | 81. | 28. | 95 | 33.5 | 109 |  |  |
| －6 | 8. | 80．6 |  | 54.4 | 18 | 68 | 2.3 .6 | 82. | 28. | 96 | 33. | 110 |  |  |
| － |  | 40.8 | 13. | 54.7 | 18.7 | 63.6 | 23.7 | 82. | 28.7 | 96. | 33. | 110. |  |  |
| 3.827 .2 | 8.8 | 41.1 | 13.8 | 55． | 18.8 | 68.9 | 23.8 | 82. | 28.8 | 96 | 33. | 110. |  |  |
| 3.927 .5 | 8.9 | 41.4 | 13.9 | 55.3 | 18.9 | 69.2 | 23.9 | 83. | 28 |  | 13 | 110.8 |  |  |
| 4.0 －7．8 |  |  | 14.0 |  |  | 6． |  | 8. | －． 0 | 97.2 |  | 111.1 |  |  |
| 4.123 .1 | 9. | 41 | 14 | 55. | 19. | 69.7 | 24.1 | 83.6 | －9．1 | 97.5 | 34.1 | 11. |  |  |
| 8 | 9.2 | 42． | 14.2 | 56. | 19 | 50.0 | 24.2 | 83.9 | 29.2 | 97.8 | 34.2 | 11.7 | 39.2 | 2125.6 |
| ． 228.6 | 9.3 | 42.5 | 14.3 | ．0． | 19.3 | \％． 0 | 24.3 | 84.2 | 29.3 | 98.1 | 34. | 111.9 | 39.3 | 3125.8 |
| $4.4-8.9$ | 9.4 | 42.8 | 14.4 | 56.7 | 19.4 | 70.6 | 24.4 | 84.4 | 29.4 | 98.3 | 34. | 112. |  |  |
| 4.599 .2 | 9.5 | 43.1 | 14.5 | 56.5 | 19.5 | 20.8 | 24.5 | 84.7 | 29.5 | $9 \times .6$ | 4. | 12. | 9.5 | ． |
| 629.4 | 9.6 | 43.3 | 14.6 | 57.2 | 19.6 | 71.1 | 24.6 | 85．0 | 29.6 | 98.9 | 44. | 12.8 | 39 | 26 |
| 729.7 | 9.7 | 43.6 | 14.7 | 57 | 19.5 | 71.4 | 24.7 | 85.3 | 29.7 | 99.2 | 34.7 | 113.1 | 39.7 | 7126.9 |
| $8: 30.0$ | 9.8 | 43.9 | 14.8 | 57.8 | 19.8 | 71.7 | 24.8 | 85.6 | 29.8 | 99.4 | 34.8 | 113.3 | 39.8 |  |
| 30 | 9.9 | 44 | 14.9 | 58.1 | 19.9 | 719 | 24.9 | 85.8 | 29.9 | 99.7 | 349 | 113.6 | 39.9 | 12 |

TABLE NO．VII．
Level Cross Sections．

## CUBIC yards in Corresponding prisms， 100 feet long．

Road－bed， 24 feet wide．

|  |  | $\begin{aligned} & \text { 薄㳦 } \end{aligned}$ |  |  |  |  |  | $\begin{aligned} & \text { 若 } \\ & \text { 荷 } \end{aligned}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | 4000 |  | 5694 | 30.0 | T667 | 35 | 9917 |
|  | 9 |  | 598 | 10.1 | 1465 | 15.1 | 2609 | 20.1 | 4031 | 25.1 | 5731 | 30.1 | 7709 | 35.1 | 9965 |
|  | 18 | 5.2 | 612 | 10.2 | 1485 | 15.2 | $26: 35$ | 20.2 | $440^{2} 2$ | 25.2 | 5768 | 30.2 | 7751 | 35.2 | 10012 |
|  | 27 | 5.3 | 627 | 10.3 | 150： | 15.3 | 2661 | 20.3 | 4094 | 25.3 | 580． | 30.3 | 7794 | 35. | 0061 |
|  | 36 | 5.4 | 642 | 10.4 | 152. | 15.4 | 2686 | 20.4 | 4125 | 25. | 5842 | 30.4 | 7836 | 35. | 10109 |
|  | 46 | 5.5 | 657 | 10.5 | 1546 | 15. | 2713 | 20.5 | 4157 | 2.5 .5 | 5879 | 30.5 | 7879 | 35. | 10157 |
|  | 55 | 5：6 | 672 | 10.6 | 566 | 15.6 | 2739 | 20.6 | 4189 | 25.6 | 5916 | 30.6 | 7922 | 35. | 10205 |
|  | 65 | 5.7 | 687 |  | 587 |  | 765 | 20.7 | 4221 | 25.7 | 5954 | 30.7 | 7965 | 35. | 0254 |
| 0. | 75 | 5.8 | 702 | 10.8 | 1608 | 15.8 | 2791 | 20.8 | 4252 | 25.8 | 5991 | 30.8 | 8008 | 35. | 0302 |
| 0.9 | 85 | 5.9 | 718 | 10.9 | 1629 | 15.9 | 2818 | 20.9 | 4285 | 25.9 | 6029 | 30.9 | 8051 | 35. | 0351 |
|  | 94 |  | \％ |  | 1 |  | 284 |  | 4317 | 2．0 | 60 | 31.0 | 8094 | 36 | 00 |
|  | 105 | 6.1 | 749 | 11.1 | 1671 | 16 | 2871 | 21. | 4349 | 26.1 | 6105 | 31.1 | 8138 | 36. | 49 |
|  | 115 | 6.2 | 765 | 11.2 | 1693 | 16.2 | 2898 | 21．2 | 4381 | 26.2 | 6142 | 31.2 | 8181 | 36.2 | 98 |
| 1.3 | 125 | 6.3 | 881 | 11.3 | 171 | 16.3 | 2925 | 21.3 | 4414 | $\because 6.3$ | 618 | 31.3 | 8225 | 36. | 0547 |
| 1.4 | 135 | 6.4 | 796 | 11.4 | 1735） | 16.4 | 2952 | 21.4 | 4446 | 26.4 | 6219 | 31.4 | 8269 | 36. | 0596 |
| 1.5 | 146 | 6.5 | 813 | 11.5 | 17.57 | 16.5 | 2979 | 21.5 | 4479 | 26.5 | 6257 | 31.5 | 8313 | 36 | 646 |
| 1.6 | 156 | 6.6 | 829 | 11.6 | 1779 | 16.6 | 3006 | 21.6 | 4512 | 26.6 | 629 | 31.6 | 83516 | 36 | 95 |
| 1.7 | 167 | 6 | 84 | 11.7 | 180 | 16. | 3034 | 21. | 4545 | 26.7 | 6334 | 31.7 | 8401 | 36 | 45 |
|  | 178 | 6.8 | 861 | 11. | 182？ | 16.8 | 306 | 21 | 457 | 26. | 637 | 31. | 8445 | 36. | 95 |
| 1.9 | 189 | 6.9 | 87 | 11.9 | 184 | 16.9 | 308 | 21. | 461 | 26. | 641 | 31. | 8489 | 36 |  |
| 2.0 | 200 | 7.0 |  |  |  |  | 3117 |  | 4644 | 27.0 | 450 | 32.0 | 8533 |  |  |
| 2.1 | 211 | 7.1 | 911 | 12.1 | 1889 |  | 3145 | 22.1 | 4678 | 27.1 | 648 | 32.1 | 8578 | 37 |  |
|  | 222 | 7.2 |  | 12.2 | 1911 | 17 | 3172 | 22.2 | 471 | 27.2 | 65 | 32.2 | 8622 | 37. | 95 |
| 2.3 | 234 | 7.3 | 945 | 12.3 | 1934 | 17. | 3201 | 22.3 | 4745 | 27. | 65 | 32.3 | 8667 | 37. | 45 |
| 2.4 | 245 | 7.4 | 962 | 12.4 | 19.5 | 17 | $3 \cdot 29$ | 23.4 | 4799 | 27.4 | 660 | 32. | 8712 | 37 | 95 |
| 2. | 257 | 7.5 | 979 | 12.5 | 1979 | 17.5 | 3257 | 22.5 | 813 | 27.5 | 664 | 32.5 | 875 |  | 1146 |
| 2.6 | 269 | 7.6 | 996 | 12． 6 | 2002 | 17.6 | 3285 | 22.6 | 4846 | 27.6 | 66 | 32.6 | 8802 | 37. | 1196 |
|  | 281 | 7. | 1014 | 12.7 | 2025 | 17.7 | 3314 | 22.7 | 4881 | 27.7 | 67 | 32.7 | 8847 | 37. | 1247 |
|  | 292 | 7． | 1031 | 12.8 | 2048 | 17.8 | 3342 | 22.8 | 4915 | 27.8 | 676 | 32.8 | 8892 | 37. | 1298 |
| 2.9 | 305 | 7 | 10 | 12.9 | 2071 | 17.9 | 3371 | 22.9 | 4949 | 27.9 |  | 32.9 | 8938 |  |  |
|  | 317 |  |  |  |  |  |  |  |  |  |  | 3． 0 | 8983 |  | 1400 |
| 3.1 | 329 | 8.1 | 1085 | 13.1 | 2118 | 18.1 | 3429 | 23.1 | 5018 | 28.1 | 6885 | 33.1 | 9029 | 38.1 | 11451 |
| 3.2 | 341 | 8.2 | 1102 | 13.2 | 2141 | 18.2 | 34.58 | 23.2 | 505 | 28.2 | 692 | 33.2 | 9075 | 38.2 | 1502 |
| 3.3 | 354 | 8.3 | 121 | 13.3 | 2165 | 18.3 | 3187 | 23.3 | 5087 | 28.3 | 696 | 33.3 | 9121 | 38 | 1554 |
| 3.4 | 366 | 8. | 139 | 13 | 21 | 18. | 3.516 | 23.4 | 51 | 28.4 | 700 | 33.4 | 9166 | 38.4 | 1605 |
|  | 379 | 8 | 119 | 13.5 | 22 | 18.5 | 35 | 23.5 | 51 | 28.5 | 70 | 33.5 | 9213 | 8． | 1657 |
|  | 392 | 8.6 | 1175 | 13.6 | 2 | 18.6 | 3570 | 23.6 | 5192 | 28.6 | ， | 33.6 | 9259 | 88．6 | 1709 |
| 3.7 | 405 | 8.7 | 1194 | 13.7 | 2261 |  | 00 | 23.7 | 5237 | 28.7 | 712 | 33.7 | 9305 | 38. | 1761 |
| 3.8 | 418 | 8.8 | 1212 | 13.8 | 2285 | 18.8 | 3635 | 23.8 | 5262 | 28.8 | 7168 | 33.8 | 9351 | 38.8 | 1812 |
| 3.9 | 431 | 8.9 | 1231 | 13.9 | 2309 | 18.9 | 3665 | 23.9 | 5298 | 28.9 | 7209 | 33.9 | 9398 | 38.9 | 1865 |
| 4.0 | 444 | 9.0 | ， | 14.0 | 2333 | 19.0 | 3694 | 24.0 | 5333 | 29.0 | 7250 | 34.0 | 9444 | 39.0 | 11917 |
|  | 458 | 9.1 | 269 | 14.1 | 2358 | 19.1 | 3725 | 24.1 | 5369 | 29.1 | 7291 | 34.1 | 9491 | 39.1 | 1969 |
|  | 471 | 9．2 | 1208 | 14.2 | 238 | 19.2 | 375 | 24.2 | 5405 | 29.2 | 7332 | 34.2 | 9538 | 39.2 | 2021 |
| 4.8 | 485 | 9.3 | 1307 | 14.3 | 2407 | 19.3 | 3785 | 24.3 | 5441 | 29.3 | 73 \％ | 34.3 | 9585 | 39.3 | 2074 |
| 4.4 | 499 | 9.4 | 1326 | 14.4 | 24：32 | 19.4 | 3815 | 24.4 | 5476 | 29.4 | 7415 | 34.4 | 9632 | 39.4 | 2126 |
| 4.5 | 513 | 9.5 | 346 | 14.5 | 2457 | 19.5 | 3846 | 24.5 | 5513 | 29.5 | 7457 | 34.5 | 9679 | 39.5 | 2179 |
| 4.6 | 526 | 9.6 | 365 | 14.6 | 2482 | 19.6 | 3876 | 24.6 | 5549 | 29.6 | 7499 | 34.6 | 9726 | 39.6 | 2232 |
| 4.7 | 541 | 9.7 | 385 | 14.7 | 2507 | 19.7 | 3907 | 24.7 | 5585 | 29.7 | 7541 | 34.7 | 9774 | 39.7 | 2285 |
|  | 550 | 9.8 | 1405 | 14.8 | 2.532 | 19.8 | 3938 | 24.8 | 5621 | 29.8 | 7582 | 34.8 | 9821 | 39.8 | 2338 |
| 4.9 | 569 | 9.9 | 1425 | 14.9 | 2558 | 19.9 | 3969 | 24.9 | 5658 | 29.9 | 7625 | 34.9 | 9869 | 39.9 | 2391 |

TABLE NO．VIII．
Side Triavgles．
CUBIC fards in corresponding prisms 100 feet long．

Road－bed 24 feet wide．

| 漒 |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { 淢 } \\ & \text { 譄 } \end{aligned}$ | Beit |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  | 30. |  |  |  |
| 22 |  | 36.4 | 10.1 | 50.3 | 15.1 | 64.2 | 20.1 | 78.1 | 25. | 91.9 | 30. | 105.8 | 35 |  |
| 22.8 |  | 36. | 10.2 | 50.6 | 15.2 | 64.4 | 20.2 | 78.3 | 25. | 92.2 | 30.2 | 106.1 | 3 | 0.0 |
| 23.1 |  | 36.9 | 10.3 | 50. | 15.3 | 64.7 | 20.3 | 78.6 | 25 | 92.5 | 30. | 106.4 |  | ． |
| 23.3 |  | 7. | 10.4 | 51. | 15.4 | 65.0 | 20.4 | 78. | 25.4 | 8 | 30. | 106．7｜ | 35． 4 | ． 6 |
| 23.6 |  | 37.5 | 10.5 | 51 |  | 65.3 | 20． | 79 | 25.5 | 93.1 | 30. | 106.9 | 55 | ． 8 |
| 23 |  |  | 10.6 | 51 |  | 65.6 | 20.6 | 79. | 25 | 93.3 | 30. | 107.2 |  | 1.1 |
| 0．724．2 |  |  |  | 51.9 | 15.7 | 65. | 20.7 | 79. | 25. | 93.6 | 30. | 107.5 | 35. | 121.4 |
| 24.4 |  | 38.3 | 10.8 | 52.2 | 15.8 | 66.1 | 20.8 | 80.0 | 25. | 93.9 | 30. | 07 | 35 | 121.7 |
| ， | 5.9 |  | 10.9 | 52． 5 | 15.9 | 66.4 | 20.9 | 80.3 | 25.9 | 94.2 | 30.9 | 08 |  | ． 9 |
|  |  |  |  |  |  |  |  |  |  | 4． |  |  |  |  |
| 25.3 |  |  | 11.1 | 5 | 16.1 | 66.9 | 21 | 80.8 | 26. | 94. | 31. | 108.6 |  |  |
| 1.225 .6 |  | 39.4 | 11.2 | 53.3 | 16.2 | 67.2 | 21.2 | 81.1 | 26.2 | 95.0 | 31.2 | 108.9 | 36 |  |
|  | 6. | 39.7 | 11.3 | 53.6 | 16.3 | 67. | 21.3 | 81.4 | 26. | 95.3 | 31. | 109.2 | 36 | 123.1 |
| 26.1 | 6.4 | 40.0 | 11.4 | 53.9 | 16.4 | 67 | 21.4 | 81.5 | 26 | 95. | 31. | 109.4 |  | 3.3 |
| 26.4 | 6.5 | 40.3 | 11.5 | 54.2 | 16 | 68 | 21 | 81.9 | 26 | 95. | 31 | 109. |  |  |
| 1.626 .7 | 6.6 | 40.6 | 11 |  | 16 | 68 | 21 | 82 | 26 | 6. |  | 110 |  |  |
| 1.726 .9 | 6.7 |  |  |  |  | 68 | 21 | 83.5 | 9 | 96. | 31 | 110.3 |  |  |
|  |  |  |  |  | 16.8 | 68.9 | 21.8 | 82.8 | 26. | 96.7 |  | 110. |  |  |
| $1.92 \% .5$ |  |  | 11.9 | 55 | 16.9 | 69.2 | 21.8 | 83.1 | 26. | 96.9 | 31 |  | 36.9 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2.128 .1 |  |  |  |  |  | （9 |  | 83 | 27 | 97.5 |  |  |  |  |
| 2.228 .3 |  |  |  |  |  | \％0．0 | 22 | 83 | 27 | 97.8 | 32 | 111.7 |  |  |
| 2.328 .6 |  |  |  | 56 | 17.3 | 70.3 | 22 | 4.2 | 27. | 98. | 32. | 11 |  | ． 8 |
|  |  |  | 12.4 | 56.7 | 17.4 | 70.6 | 23．4 | 84.4 | 27. | 98. | 32. | 112. |  |  |
| 29.2 | 7.5 | 43 | 12.5 | 56.9 | 17.5 | \％0．8 | 22.5 | 84.7 | 27.5 | 98.6 | 32.5 | 112.5 |  |  |
| 629 | 7.6 | 43.3 | 12.6 | 57.2 | 17.6 | 71.1 | 22.6 | 85.0 | 27.6 | 98. | 32.6 | 112. |  |  |
| 729.7 | 7.7 | 8．6 | 12 | 5 |  | 71.4 |  |  |  | 99.2 |  |  |  |  |
| $8: 30.0$ |  | 43.9 | 12.8 |  |  | －1 |  | 85 | \％ | 99.4 | 32 |  |  |  |
| 930.3 | 7.9 |  | 12.9 | 58 |  | 71. | 22. |  |  |  | 32. |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | 8.1 | 44.7 | 13.1 | 58.6 | 18.1 | 72.5 | 23.1 | 86.4 | 28. | 100.3 | 33.1 | 114.2 |  |  |
| 3.231 .1 | 8.2 | －5． 0 | 13.2 | 58.9 | 18.2 | 72.8 | 23.2 | 86. | 28. | 100.6 | 33.2 | 114.4 |  |  |
| 3.331 .4 | 8.3 | 4.5 .3 | 13 | 59 |  | \％．3． | 2：3 | 86 | 28 | 0 | 33.3 | 114.7 |  |  |
| 3.431. | 8.4 | 45． 6 |  | 50 |  | 73．3 | 23 |  | 28 | 101. |  |  |  |  |
| 3．531．9 |  |  | 13.5 | 59. | 18.5 | ． 6 | 20．0 | 87.5 | 28. | 101.4 | 33． | 115． |  |  |
|  |  |  |  | 60.0 |  |  |  |  |  | 01.7 |  |  |  |  |
| 3．7） $3 \cdot 2.5$ |  | 46.4 | 13.7 | 60.3 | 18. | \％4． | 23.7 | 88. | 28. | 101.9 | 33． |  |  |  |
| 832．s | 8. | 46.7 | 13.8 | 60.6 | 18.8 | 74.4 | 23.8 | 88.3 | 28.8 | 102．2 | 33.8 | 116.1 | 38. | 130.0 |
| 933.1 | 8.9 |  | 13.9 | 60.8 | 18.9 | 74.7 | 23.9 | 88.6 | 28.9 | 102．5 | 33.9 | 116.4 |  |  |
|  |  |  |  |  |  |  |  | 88.9 |  |  |  |  |  |  |
| 3． |  |  | 14. | 61.4 | 19.1 | \％．．． | 24 | 89.2 | 29. | 03．1 |  | 116.9 |  |  |
| 233.9 |  | 47.8 | 14.2 | 61.7 | 19.2 | 75． 6 | 24.2 | 89.4 | 29. | 03.3 | 34. | 117.2 |  |  |
| 334.2 |  | 48． 1 | 14.3 | 61.9 | 19.3 | 75． 8 | 24.3 | $\times 9 . \hat{1}$ | 29.3 | 103.6 | 34. | 17. |  |  |
| 4.434 .4 |  | 49.3 | 14.4 | 62.2 | 19.4 | \％6．1 | 24.4 | 90.0 | 29.4 | 103.9 | 34. | 117.8 |  | ． |
| 53 |  | 48.6 | 14.5 | 62.5 | 19.5 | 76.4 | 24.5 | 90.3 | 29. | 104.2 | 34. | 8.1 |  |  |
| 4．6，3．5． 0 |  | 48.9 | 14.6 | 62.8 | 19.6 | 66.7 | 24 | 90.6 |  | 104.4 | 34 | 8.3 |  | ． 2 |
|  |  | 49.2 | 14.7 | 63.1 | 19.7 | 76.9 | 24.7 | 90.8 |  | 04.7 |  | 8.6 |  |  |
| \％35．6 |  | 49.4 | 14.8 | 63.3 | 19.8 | 77.2 | 24.8 | 91.1 |  | 105.0 |  | 8.9 |  | 32.8 |
| ． 9 35．8 |  | 49.7 | 14.9 | 63.6 | 19.9 | 775 | 24.9 | 91.4 | 29. | 105.3 | 34 | 18． |  | 23． |

TABLE NO．IX．
Level Cross Sections．

## CUBIC fards in Corresponding prisms， 100 feet long．

Road－bed 26 feet wide．

| $\begin{aligned} & \text { 㤩 } \\ & \text { 惢 } \end{aligned}$ |  | $\begin{aligned} & \text { 苞 } \\ & \text { 药 } \end{aligned}$ | 佥荡 |  | 枵装 |  |  | $\begin{aligned} & \text { 右 } \\ & \text { 蔦 } \end{aligned}$ |  | $\begin{aligned} & \text { 荮 } \\ & \text { 要 } \end{aligned}$ | 䜾然 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 10 |  |  |  | 1539 |  | 27 | 20 | 41 | 25.1 | 5917 | 30 | 7932 |  |  |
|  | 19 |  |  |  | 1560 | 15.2 | 2747 | 20.2 | 4212 | 25. | 5955 | 30.2 | 5975 | 35. | 10273 |
|  | 29 |  |  | 10. | 1581 |  | 774 | 20.3 | 4244 | 2.5 | 595 | 30.3 | 018 |  | 23 |
|  | 39 | 5.4 | 682 |  | 02 |  | 2801 | 20. | 276 | 25. | 6030 | 30.4 | 062 |  |  |
|  | 5 | 5.5 | 698 | 10 | 1624 | 15. | 2827 | 20. | 4309 | 25. | 606 | 30.5 | 810 |  |  |
|  | 60 | 5.6 | 713 | 10.6 | 1645 | 15.6 | 2854 | 20. | 4341 | 25. | 6106 | 30.6 | 8149 | 35 | 10469 |
|  | 70 |  | 729 | 10 | 1666 |  | $\because 881$ | 20. | 4374 | 25 | 614 | 30.7 | 8192 | 35 | 518 |
|  | 8 |  | 745 |  | 688 |  | 2908 | $\because 0$ | 4407 |  | 6182 | 30.8 | 82：36 | 35 |  |
| 0.9 | 91 | 5. | 5 | 10.9 | 1710 | 15 | 2936 | 20. | 4439 | $2 \overline{2}$ | 6221 | 30.9 | 828 |  |  |
|  | 102 |  |  |  |  |  |  |  |  |  | 59 | 31.0 | 224 |  |  |
|  | 113 |  | 794 |  | 175 | 16.1 | 299 | 21. | 4505 | 26 | 6298 | 31．1 | 8368 | 36.1 |  |
| 1.2 | 124 | 6.2 | 811 | 11.2 | 177 | 16.2 | 3018 | 21. | 4.3 | 26. | 633 | 31.2 | 412 | 36 | 10766 |
|  | 135 | 6.3 |  | 11.3 |  | 16.3 | 3046 | 21. | 457 | 26 | 637 | 31.3 | 8457 | 36 | 10816 |
|  | 14 | 6.4 | 844 |  | 1820 |  | 3073 | 21 | 460 | 26 | 641 | 31 | 8501 | 36 | 10866 |
|  | 157 | 6.5 | 861 | 11.5 | 1842 |  | 01 | 21. | 638 | 26 | 645 | 31.5 | 546 | 36.5 | 10916 |
|  | 168 | 6.6 | 878 | 11.6 | 186 | 16. | 129 | 21. | 4672 | 26 | 649 | 31. | 8.591 | 36 | 0966 |
|  | 180 |  | 85. |  | 888 |  | 3158 | 21. | $4{ }^{4}$ | 26 | 6.53 | 31. | 63 | 36. | 17 |
| 1.8 | 191 | 6.8 | 912 | 11.8 | 1910 | 10.8 | $31 \times 6$ | 21. | 4739 | 26. | 6571 | 31.8 | 868 | 36 | 11067 |
| 1.9 | 203 | 6.9 | 92： | 11.9 | 1933 | 16.9 | $3: 14$ | 21.9 | 4773 | 26. | 6610 | 31.9 | 872 | 36. |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 227 | 7 | 964 | 12.1 | 1979 |  | $3 \cdot 71$ | 22.1 | 4842 |  | 66 | 32.1 | 6 | 37.1 |  |
| 2.2 | 239 | 7.2 | S1 | ， | 2002 | 17.2 | 00 | 22.2 | 876 | 27. | 672 | 32. | 8861 | 37.2 |  |
| 2.3 | 251 | 7.3 | 999 | 12.3 | 2025 | 17.3 | 3329 | 22.3 | 4910 | 27. | 6769 | 32. | 890 | 37. | 砛 |
| 2.4 | 263 | 7.4 | 1017 | 12.4 | 2048 | 17.4 | 33.58 | ご． | 4945 | 27. | 6809 | 32. | 89.5 |  | 372 |
|  | 275 | 7.5 | 035 | 12.5 | 207： | 17.5 |  | 2\％． | 497 | 27. | 6850 | 32. | 999 |  |  |
|  | 28 | 7.6 | 0．53 | 12.6 | 2095 |  | 311 | $2 \cdots$ | 5014 | 27. | 6890 |  | 904 |  |  |
|  | 301 | 7. | 071 |  | 2119 |  |  |  | 504 |  | 6930 |  | 088 |  |  |
|  | 313 | 7.8 | 1089 | 12 | 2143 | 17.8 | 474 | 22.8 | 5084 |  | 6971 |  | 9135 |  |  |
| 2.9 | $3: 2$ | 7. | 1107 | 12.9 | 2167 |  | 3504 | 22 9 | 5119 | 27 | 7011 |  | 91 |  |  |
|  | 32 | 8.0 | 126 |  | 2191 |  | 3533 | 23. | 5154 |  | 705 |  | 922 |  |  |
|  | 359 | 8.1 | 145 | 13.1 | 2215 |  | 3563 | 23.1 | 5189 | 28. | 709 | 33. | 9274 |  |  |
|  | 36 | 8. | 18． | 13.2 | 2. |  | 3．193 | 23. | 522 | 28 | 713 |  | 9321 |  |  |
|  | $3 i 8$ |  | $18:$ |  | 2203 |  | 362 | 23. | 526 | 2 8． | 1 |  | 907 |  |  |
|  | 392 |  | 01 |  | 218 |  | － |  | 5295 |  | 721 |  | 9414 |  |  |
|  | 40.5 | 8. | 230 | 13 | 2313 | 18.5 | 683 |  |  |  | 725 |  | 9461 |  |  |
|  | 419 | 8.6 | 239 | 13.6 | $23: 37$ |  | 3713 | 23.6 | 367 | 28. | 729 |  | 9508 |  | 995 |
|  | $43 \%$ | 8.7 | 2.58 | 13.7 | 2362 | 18.7 | 3743 | 23.7 | 5403 | 28. | 7340 | 33 | 95.5 |  | 047 |
|  | 446 | 8.8 | 278 | 13.8 | 2387 | 18.8 | 3774 | 23.8 | 5439 | 28.8 | 7381 | 33. | 960 | 38.8 | 12 |
| 3.9 | 46 |  | 12 | 13 | 2412 | 18.9 |  | 23.9 |  | 28.9 | 7423 | 33. | 96 |  |  |
|  | 484 |  |  |  |  | 1.0 |  |  |  | 29.0 | 846. | 34.0 | 9696 | 39.0 | 1226 |
| 4.1 | 488 | 9.1 | 13：36 | 14.1 | 2462 | 19.1 | 3866 | 24.1 | 5547 | 29.1 | 7507 | 34.1 | 9744 | 39.1 | 225 |
| 4.2 | 502 | 9.2 | 356 | 14.2 | 2488 | 19.2 | 3897 | 24.2 | 5584 | 29.2 | 7549 | 34.2 | 9791 | 39.2 | 3312 |
| 4.3 | 517 | 9. | 376 | 14.3 | 2513 | 19.3 | 3928 | 24. | 56.1 | 29. | 7591 | 34. | 9839 | 39 | 365 |
| 4.4 | 53 | 9.4 | 396 | 14 | 2539 | 19. | 3959 | 24. | 5657 | 29. | 763 | 34. | 9887 |  |  |
| 4.5 | 546 | 9. | 416 | 14.5 | （104 | 19.5 | 3990 | 24.5 | 694 | 29. | 7675 | 34.6 | 9935 | 39. | 472 |
|  | 51 | 9. |  | 14.6 | 2．）90 | 19.6 | $402 \cdot$ | 24.6 | T31 | 9． | 7718 | 34.6 | 9983 | 39. | 2520 |
|  | 575 | 9.7 | 45 | 14.7 | 2616 | 19.7 | 4053 | 24.7 | 5768 | 29. | 7761 | 34.7 | 0031 | 39. | 2579 |
|  | 590 | 9.8 | 477 | 14.8 | 2642 | 19.8 | 4085 | 24.8 | 580.5 | 29.8 | 7803 | 34.8 | 0079 | 39.8 | 12633 |
| 4.9 | 605 | 9.9 | 1493 | 14.9 | 2668 | 19.9 | 4116 | 24.9 | 5842 | 29.9 | 7846 | 34.9 | 10127 | 39.9 | 12087 |

TABLE NO． $\mathbf{X}$ ．

## Side Triangles．

CUBIC YARDS IN CORRESPONDING PRISMS， 100 FEET LONG．
Road－bed 26 feet wide．
Side slopes $1 \frac{1}{2}$ to 1.

| . |  |  | 号筑 | Ex |  |  | 율 |  | 을 | Ex |  |  | $\begin{aligned} & \text { 열 } \\ & \text { Bu } \\ & \text { By } \\ & \hline \end{aligned}$ | 毕感 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 38.2 | 10 | 52. | 15 | 66 | 20 | 79.9 | 25. | 93.8 | 30. |  | 35. |  |
|  |  |  | 38.5 | 10 | 52 | 15. | 66 | 30.2 | 80. | 25. | 94 | 31. | 108.0 | 35. | 121.9 |
|  | 24.9 | 5 | 38.8 | 10 | 52 | 15. | 66. | 20.3 | 80.5 | 25 | 94.4 | 30 |  | 35. |  |
|  |  |  | 39.1 |  | 53 | 15 | 66 | 20.4 | 80.7 | 25 | 94.6 | 30. | 18.5 | － | 4 |
|  | 25 |  | 19 | 10 | 53 | 15. | 67 | 20. | 81.0 | 25 | 94.9 | 30. | 108.8 | 35. | 1 |
|  |  |  | 39.6 | 10. | 03 |  |  | 20.6 | 81 | 25 | 95.2 | 30. | 109.1 |  | 123.0 |
|  |  |  | 39. | 10. | 53 | 15. | 67 | 20. | 81.6 | 25.7 | 95.5 | 30 | 09.4 |  | ． 2 |
|  |  |  | 40.2 | 10.8 | 5 |  |  | 20.8 | 81.9 | 25．8 | 95.7 | 30. | 109.6 | 35 |  |
|  | 20 |  | 10. | 10.9 | 54.4 | 15.9 | 68 | 20.9 | 82.1 | 25.9 | 96.0 | 30. | 9 | 35 | 8 |
|  |  |  |  |  |  |  |  |  | 82． 4 |  |  |  |  |  |  |
|  |  |  | 41 | 11. | 54 | 16 |  | 21.1 |  |  | 96.6 |  |  |  |  |
|  |  |  |  | 11. |  | 16 | 69 | 21 | 83.0 | 26. | 96.9 | 31 | 7 | 36.2 | 124.6 |
|  | 7 | 6. | 41.6 | 11. | 55 | 16. | 69 | 21 | 83 |  | 97.1 |  | 11.0 |  |  |
|  |  |  | 41.9 | 11.4 |  |  | 69 |  |  | 26.4 | 97.4 | 31 | 11.3 |  | 25.2 |
|  | 28.2 | 6. | 42.1 | 11.5 | 56 | 16 | 69 | 21.5 |  |  | 97.7 | 31 | 11.6 |  | ． 5 |
|  |  |  | 42.4 |  | 56 | 16.6 |  | 21.6 |  | 26 | 98.0 | 31 | 1.9 |  |  |
|  |  | 6. |  |  | 56 | 16. | 70 | 21.7 | 84 | 26 | 98.2 |  | 2.1 |  |  |
|  |  |  |  |  | 56.9 | 16.8 | 70.7 | 21.8 | 84 | 26.8 | 98.5 |  | 12.4 |  |  |
|  | 20 | 6. | 43. | 11.9 | 57.1 | 16.9 | 71.0 | 21.9 | 84 | 26.9 | 98.8 |  | 12.7 | 30 | 126.6 |
|  |  |  |  |  |  |  |  |  |  |  | ． |  |  |  | 9 |
|  | 29.9 |  |  | 12 |  |  |  | 22.1 |  |  |  |  | 3.2 |  |  |
|  | 30.2 | 7. | 44 | 12 |  | 17. | 71.9 | 22.2 |  |  | 99.6 |  | 113.5 |  |  |
|  | － | 7 |  | 12. |  | 17. | 72.1 | 22.3 |  |  | 99.9 |  | 3.8 |  |  |
|  | 30.7 |  | 44.6 | 12.4 | 58 | 17. |  | 22.4 | 86 |  | 00.2 |  |  |  |  |
|  | ， | 7 |  | 12.5 |  | 17. | 7 | 22.5 |  |  | 0.5 | 32 | ． 4 |  | ． 2 |
|  | 31 |  |  | 12.6 | 59.1 | 17 |  | 22.6 | 86.9 |  | 00.7 |  |  |  | 128.5 |
|  | 31 |  |  | 12.7 | 59. |  |  | 22.7 |  |  |  |  |  |  |  |
|  | 31.9 |  |  | 12.8 |  | 17.8 |  | 22.8 | 87.4 |  |  |  | 2 |  |  |
| 2. | 32.1 | 7 |  | 12.9 | 59.9 | 17.9 |  | 22.9 |  |  |  |  |  |  |  |
|  | ． |  |  | 13.0 |  | 18， |  | 2．0 | 88.0 |  | ． |  |  |  | ． 6 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 13 | 8. |  | 13.2 | 60. | 18 | 74 | 23.2 | 88 |  | ， | 33 | 16.3 |  | ． |
|  |  |  |  |  |  |  |  |  |  |  | 2.7 |  | 6.6 |  |  |
|  |  |  |  | 13. | 61. | 18 |  | 23.4 | 89.1 |  | 03.0 | 33 | 16.9 |  | 30.7 |
|  |  |  |  | 13.5 | 61.6 |  |  |  | 89.4 |  | 03.2 |  | 17.1 |  |  |
|  | 34.1 | 8. |  | 13.6 | 61.9 | 18 |  |  | 89.6 |  | 03. |  | 7.4 |  | 131.3 |
|  |  |  |  | 13. |  |  |  | 23.7 | 89.9 |  |  |  | 7． |  |  |
|  | 34．6 |  |  | 13 |  | 18 | 76 | 23 | 90.2 |  |  |  | 8． |  | 1． |
|  | 34.9 | 8. | 48.8 | 13.9 | 62.7 | 18. | 76.6 | 23.9 | 90.5 |  |  |  | 18.2 | 38 | 1 |
|  |  |  |  | ． |  |  |  |  | 00． |  |  |  | 18. |  | 132．4 |
|  |  | 9 | 4， |  |  |  |  |  |  |  | 104.9 |  | 18 |  |  |
|  | － | 9. | 49.6 | 14 | 63.5 | 19.2 |  | ． | 91. |  | 05.2 |  | 19.1 |  | ． |
|  | 36.0 | 9. | 49.9 | 14. | 63.8 | 19 |  | 24. | 91.6 | 29. | 05．5 |  | 10.4 |  |  |
|  | 36.3 | 9. | 50 | 14 | 64.1 |  |  |  | 91.9 | 29 | 105.7 | 34 | 19.6 | 39 | 133.5 |
|  | 36． |  | ． | 4.0 | 64.4 | 19.5 |  | 24.5 | 92.1 |  | 06.0 |  | 19.9 |  |  |
|  | 6.9 |  | ．20 |  | 64.6 | 19.6 | 78.5 | 24.6 | 93.4 | 29 | 06.3 | 34. | 20.2 |  | 134.1 |
|  |  |  |  | 14. | 64.9 | 19.7 | ． 8 | 24.7 | 92． 7 | 29.7 | 106．6 | 34. | 120.5 |  |  |
|  |  | 9. | 51. | 14. | 65.2 | 19 | 79.1 | 24.8 | 9：3．0 | 29.8 | 106.9 | 34. | 120.7 |  | 34．6 |
| 4.8 | 37.7 | 9. | 51.6 | 14.9 | 65.5 | 19.9 | \％9．4 | 24.9 | 93.2 | 29.9 | 107.1 | 34. | 121.0 | 35.9 | 34.9 |

## TABLE NO．XI．

## Level Cross Sections．

CUBIC YARDS IN CORRESPONDING PRISMS 100 FEET LONG．
Road－bed 16 feet wide．

|  |  | B | $0$ |  | 㴔我 |  |  |  |  |  |  | $\begin{aligned} & \text { 范 } \\ & \text { 㳦 } \end{aligned}$ | 节登然 | $\begin{aligned} & \text { 芘淢 } \\ & \text { 2 } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | 1722 | 20.0 | 2667 | 25.0 | 6 | 30.0 | 111 | 35.0 |  |
|  | 6 |  | 399 | 10 | 976 |  | 1739 | $\because 0.1$ | 2687 | 27. | 3821 | 30. | 5139 | 35 | 643 |
|  | 12 | 5.2 |  | 10.2 | 90 | 15 | 1756 | 20.2 | $2 \% 08$ | 25 | 3845 | 30 | 5168 | 35 | 6675 |
|  | 18 |  | 418 | 10.3 | 1003 | 15.3 | 1774 | 20.3 | 2729 | 2Ј． 3 | 3870 | 30. | 5196 | 35 | 6707 |
|  | 24 | 5.4 | $42 \cdots$ | 10.4 | 1017 |  | 179 | 20 | 2750 | 25.4 | 3895 | 30 | $5 \because 24$ | 35.4 | 39 |
|  | 31 | 5.5 | 438 |  | 031 |  | 1808 | 20 | 2771 | 25 | 3919 | － | 553 |  | 6771 |
|  | 37 | 5.6 | 448 | 10.6 | 1044 | 15.6 | 826 | 20.6 | 2792 | 25.6 | 3944 | 30. | 5281 | 35.6 | 80 |
| 0.7 | 43 | 5.7 | 458 | 10.7 | 10.78 | 15.7 | 1843 | $\because 0.7$ | 281 | 20．7 | 3969 | 30. | 5310 | 35.7 | 6836 |
|  | 5 |  |  | 10.8 | 107 |  | 1861 | 20.8 | 283 | 35.8 | 3994 | 30. | 5339 |  | 6868 |
| 0.9 | 56 | 5.9 | 4 | 10.9 | 108 | 15. | 1879 | 20.9 | 285 | $\bullet 5.9$ | 4019＇ | 30.9 | 5367 | 35 |  |
|  |  |  |  |  |  |  |  |  |  |  | 4 |  |  |  |  |
|  | 70 | 6.1 | 499 |  | 1114 | 16.1 | 1914 | 21.1 | 2899 | 26 | 4070 | 31. | 425 | 36. |  |
| 1.2 | 76 | 6.2 | 510 | 11.2 | 112 | 16.2 | 1932 | 21.2 | 2931 | 26. | 4095 | 31 | 545 | 36.2 | 6999 |
| 1.3 | 83 | 6.3 | 520 | 11.3 | 11 | 16.3 | 155 | 31.3 | 2943 | 26. | 4120 | 31. | 54 | 36.3 | 03 |
| 1.4 | 90 |  | 531 | 11 | 115 |  | 19 | 31.4 | 296 | 26 | 4146 | 31. | 55 | 36.4 | 06 |
|  |  |  |  |  |  |  | 1986 | 21 | 29 |  | 4171 | 31 | 2 | 36.5 | 7097 |
|  | 104 |  |  |  |  |  | 2004 | －11．6 | 30 |  | 4197 | 31.6 | 571 | 36.6 | 30 |
|  | 111 |  |  |  | 1200 |  | 2023 | 21.7 | 030 | － | 223 | 31. | 500 |  | 163 |
| 1.8 | 119 | 0.8 | 58 | 11.8 | 1215 | 1.8 | 2041 | 21.8 | 3052 | ¢． | $4: 48$ | 31.8 | 563 | 3. | 1030 |
| 1.9 | 126 | 6.9 | 58－ | 11.9 | 1230 | 16.9 | 2059 | 21.9 | 3074 | 26. | 4274 | 31.9 | 565 | 36 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 14 |  |  |  | 1259 |  |  |  | 31 |  | 4326 |  | 9 |  | 7296 |
|  | 1 |  | 619 |  | 1274 |  | 2115 | 22 | ， | 27. | 4352 | 32 | 5748 |  | 0 |
|  | 1.56 |  |  |  | 1259 |  |  | 22.3 | 3163 | 27. | 4378 | 32.3 | 5778 |  |  |
|  | 164 | 7.4 | 641 | 12.4 | 304 |  | 215 | 22.4 | 3186 | 27. | 4404 | 32. | 5808 |  | 397 |
|  | 171 | 7.5 | 6.3 | 12.5 | 319 | 17.5 | 217 | 32.5 | $3: 0$ | 27. | 4431 | 32.5 | 583 |  | 431 |
|  | 179 |  |  |  |  |  | 218 | 22.6 | $3: 31$ | 27 | 44.57 | 32. | 586 |  | 464 |
|  | 10 |  |  |  |  |  |  | 22.7 | $3: 54$ |  | 4483 |  | 589 |  | 8 |
|  | 12． |  |  |  |  |  |  |  | 3276 |  | 4510 | 2． | 5928 |  | ว32 |
| 2.9 | 203 | 7.8 | 699 | 12 | 1381 | 17.9 | $2 \cdot$ | 22.9 | 3299 | －r | 4536 | 32. | 595 |  |  |
|  | 21 |  | 711 |  |  |  |  | －3．0 | 322 |  | 63 |  | 598 |  | 600 |
|  | 219 | 8.1 | 72： | 13.1 | 141 | 18 | 2286 | 23.1 | 3：34 |  | 4590 |  | 6019 |  | 7634 |
|  | 2 |  | 73.5 |  |  | 18 | 230 | 23.2 | 3368 | 38.2 | 4616 |  | 6050 |  | 608 |
|  | 2 |  | 747 |  |  |  |  | 23 | 3391 | 28.3 | 4643 | 33 | 111 |  | \％03 |
|  | 24 |  | 75.9 |  | 14.99 |  |  | 23.4 | 3415 |  | 4670 | 334 | 6111 |  | \％71 |
|  | 253 |  | 771 | 退 | 1475 |  | 2 | 23.5 | 348 | 38.5 | 4697 | ， | 6142 |  | 7771 |
|  | 261 |  |  |  |  |  |  |  | 3461 |  | 42.24 |  | 172 |  | － |
|  | $2 \% 0$ |  | － | 13.7 | 1507 |  | 240： | 23.7 | 3485 |  | $4 \%$ |  | 6203 |  | 840 |
| 3.8 | 279 | 8.8 | 80 | 13.8 | 15 | 18.8 | 2423 | 23.8 | 3508 | 28.8 | 4759 | 33.8 | 6234 |  | 875 |
| 3.9 | 287 | 8.9 | 8 | 13.9 |  |  |  | 23.9 |  | 28.9 |  | 33.9 | 626 |  |  |
|  |  |  |  |  |  |  |  | 24 | \％ | ． | 48.3 | ， | 6296 | ． 0 | 944 |
|  | 30.5 |  | 8 | 14.1 |  |  |  | 24.1 |  | ． | 析 | 34． | 632 | 3 | 7979 |
| 4.2 | 314 | 9.2 | 859 | 14.2 |  | 19.2 | 25113 | 24.2 | 3103 | 29.2 | 4888 | 34.2 | 6359 | 39. | 8014 |
| 43 | 32 | 9.3 | 871 | 14.3 | 160 | 19.3 | 2523 | 24.3 | 3627 | 29.3 | 4916 | 34. | 6390 | 39. | 049 |
| 4.4 | 33. |  | 8 | 14.4 | 162 | 19.4 | 2.54 | 24.4 | 36 ¹ | 29.4 | 4944 | 34.4 | 6421 | ， | 084 |
| 4.5 | $3{ }^{3}$ |  | 897 | 14 | $16: 3$ | 19.5 | 2564 | 24.5 | 3675 | 29.5 | 4971 | 34. | 645： | 39 | 19 |
|  | 3.3 | 9.6 | 910 | 14 | 16 | 19.6 | 2584 | 24.6 | 3699 | 29.6 | 4999 | 34.6 | 6484 | 99． | 50 |
|  | $3{ }^{3}$ |  | 92：3 | 14． | $1{ }^{\text {d }}$ | 19.7 | 2605 | 24.7 | 372． | 29.7 | 5027 | 34. | 6516 | 39. | 90 |
|  | 370 | ． | 95 | 14.8 | 1688 | 19.8 | 2625 | 24.8 | 3748 | 29.8 | 505.5 | 348 | 6548 | 39.8 | 8225 |
| 4.9 | $3: 9$ | 9.9 | 950 | 14.9 | 120 | 19.9 | 2646 | 24.9 | $37 \% 2$ | 29.9 | 5083 | 34.9 | 6579 | 39.9 | 8261 |

TABLE NO．XII．
Side Triatgles．
cubic yards in corresponding prisms 100 feet long．

Road bed 16 feet wide．

|  |  |  |  | 請感 |  |  |  | 烈感感 |  |  | 号离感 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 014. | 5.024 .1 | 10 | 33.3 | 15.0 | 42.6 | 20 | 51 | 25.0 | 1 | 30.0 | 70.4 |  | 79.6 |
| 15 | 5.124 .3 | 10 | 33.5 | 15. | 42.8 | 20 | 52.0 | 25.1 | 61.3 | 30 | \％0．6 |  |  |
| 15 | 24 | 10.2 | 33.7 |  | 43.0 | 20. | 52．2 | 25. | 61.5 | 30.2 | \％0． | 5. |  |
| 15.4 | 5.324 .6 | 10.3 | 33.9 | 15.3 | 43.1 | 20. | 52.4 | 25.3 | 61.7 | 30.3 | \％0． | 35.3 | 80．2 |
| 15.6 | 5.424 .8 | 10.4 | 34.1 | 15. | 43.3 | 20.4 | 52.6 | 25.4 | 61.9 | 30.4 | 71 | 35.4 | 80.4 |
| 15.7 | 5.525 .0 | 10.5 | 34.3 | 15. | 43.5 | 20.5 | 52. | 25.5 | 62.1 | 30.5 | 71.3 | 35 | 80.6 |
| 15.9 | 5.625 .2 | 10.6 | 34.4 | 15.6 | 43.7 | 20.6 | 53. | 25.6 | 62.2 | 30.6 | 71 | 35.6 | 80 |
| 16.1 | 5.60 .4 |  | 34.6 |  | 43.9 | 20 | 53 | 25. | 62 | 30 | 71 | 35． 7 | 80 |
| 16 | 5.825 .6 |  | 34.8 |  | 44. | 20.8 | 53.3 | 25.8 | 62.6 | 30.8 | 71 | 35.8 | 81 |
| 916.5 | 5.92 | 10.9 | 35.0 | 15.9 | 44.3 | 20.9 | 53.5 | 25.9 | 62. | 30.9 | 22．0 | 35.9 | 81.3 |
|  |  |  |  |  |  |  |  |  |  |  | ז2．2 |  |  |
| 16.9 | 6.126 .1 | 11.1 | 35.4 | ， | 44 | 21. | 53 | $\because 6$ | 63. | 31.1 | T2 | 36.1 | 81.7 |
| 17.0 | 6.226 .3 | 11. | 35.6 | 16. | 44 | 21. | 54 | $\because 6$ | 63 | 31.2 | － |  | 81.9 |
| 17. | 6.320 | 11.3 | 35.7 | 16. | 45.0 | 21.3 | 54.3 | 26.3 | 63 | 31 | i2 | 36.3 | 82.0 |
| 17.4 | 6.426. | 11.4 | 35.9 | 16． | 45.2 | 21. | 54. | 26. | 63. | 31. | \％3． | 36.4 | 82.2 |
| 517.6 | $6.5 \sim 6.9$ | 11.5 | 36.1 | 16.5 | 45.4 | 21.5 | 54. | 26.5 | 63. | 31.5 | \％3． | 36.5 | 82 |
| 617.8 | 6.62 \％． 0 | 11.6 | 36.3 | 16.6 | 45.6 | 21.6 | 54. | 26.6 | 64. | 31.6 | \％3． | 36. | 82.6 |
| 18.0 | 6.727 .2 | 11.7 | 36.5 | 16.7 | 45.7 | 21.7 | 55. | 26. | 64. | 31. | 13. | 36.7 | 82.8 |
| 818.1 | 6.8 | 11.8 | 36.7 | 16.8 | 45.9 | 21.8 | 55 | 26. | 64 | 31. | \％3． | － | 83 |
| 18.3 | 6.927 | 11.9 | 36.9 | 16.9 | 46.1 | 21.9 | 55. | 26. | 64 | 31.9 | \％3 | 36 | 83.1 |
| 018.5 |  | 12.0 | 37．0 |  | 46.3 | 22.0 |  |  | 64.8 | ， | 4. |  | 3．3 |
| 18.7 | 7.128. | 12.1 | 37.2 | 17.1 | 46.5 | 22.1 | ธ5． | 27.1 | 65. | 32.1 | 14. |  | 83.5 |
| 218.9 | 7.228 .1 | 12.2 | 37.4 | 17．2 | 46.7 | 22.2 | 55.8 | 27.2 | 65. | 32. | 74. | 37 | 83 |
| 319.1 | 7．328．3 | 12.3 | 37.6 | 17.3 | 46.8 | 22. | 56.1 | 27.3 | 65. | 32 | 74. |  | 83. |
| 19.3 | 7.428 | 12.4 |  |  |  | 22. |  | 27. | 65. | 32 | 74 |  | 84.1 |
| 19.4 | 7.5 | 12. | ． 0 | 17.5 |  |  |  |  | 65 | 32 | 55 |  | 84.3 |
| 19.6 | 7.628 | 12. | 38.1 |  |  |  |  |  | 65. | 32 | \％ |  |  |
| 19.8 |  |  | 38.3 |  |  |  | 56 |  | 66.1 | 32 | 75.4 |  | 84.6 |
| 820.0 | 7.829 .3 | 12.8 | 38.5 | 17.8 | 47.8 | 22.8 | 57.0 | 27.8 | 66. | 32.8 | 75. |  | 84.8 |
| 920.2 | 7.929 .4 | 12.9 | 38.7 | 17.9 | 48.0 | 22.9 | 57.2 | 27.9 | 66.5 | 32.9 |  |  |  |
|  |  |  |  |  |  | 23.0 |  |  | 06.7 |  |  |  | 8． 2 |
| 20.6 | 29.8 | 13. | 39.1 | 18. |  | 23.1 | 57． | 28.1 | 66.9 | 33. | 76. |  | 85.4 |
| 20.7 | 8.230 .0 | 13.2 | 39.3 | 18.2 | 48.5 | 23.2 | 57.8 | 28.2 | 67.0 | 33.2 | 66 |  | 85.6 |
| 20.9 | 8．3：30．2 | 13.3 | 39.4 | 18.3 |  | 23.3 | 58.0 | 28.3 | 67. | 33.3 | \％0． |  | 85. |
| 21.1 | 8.430 .4 | 13.4 | 39.6 | 18.4 | 48.9 | 23.4 | 58.1 | 284 | 67. | 33.4 | 76. |  | 85.9 |
| 21.3 | 8.530 .6 | 13. | 39.8 | 18.5 | 49.1 | 23.5 | 58.3 | 28.5 | 67. | 33.5 | 76. |  | 86.1 |
| 21．5 | 8. | 13 | 40.0 | 18.6 | 49.3 | 23.6 | 58. | 28.6 | 67.8 | 33 | 77. |  | 86 |
| ¢ 21.7 | 8． 7 8． 9 | 13.7 | 40．2 | 18.7 | 49.4 | 23 | 58.7 | 28.6 | 68.0 | 33.7 | TT． 2 |  | 86.5 |
| 821.9 | ． 1 | 13.8 | 40.4 | 18.8 | 49.6 | 23.8 | 58.9 | 28.8 | 68.1 | 33.8 | 77.4 | 38.8 | 86.7 |
| $92 \geqslant .0$ | 31 | 13.9 | 40. | 18 |  | 23 | 59 | 28 | 68 | 33.9 |  | 38.9 | 86.9 |
| 4.022 .2 |  |  |  |  |  | 24.0 | 59.3 | 2． | 63.5 |  |  | 39.0 | 87.0 |
| 2． | 9.131 .7 | 14.1 | 40.9 | 19.1 | 50.2 | 24.1 | 59.4 | 29.1 | 68.7 | 34.1 | \％ | 39.1 | 87．2 |
| 22.6 | 9.231 .9 | 14.2 | 41.1 | 19.2 | 50.4 | 24.2 | 59.6 | 29.2 | 68.9 | 34.2 | 78 | 39 | 87.4 |
| 323.8 | 9.3 32． 0 | 14.3 | 41.3 | 19.3 | 50.6 | 24. | 59.8 | 29.3 | 69.1 | 34.3 | 78． | 9 | 87.6 |
| 423.0 | 9.432 .2 | 14.4 | 41.5 | 19.4 | 50.1 | 24. | 60.0 | 9. | 69.3 | 34.4 | 78. | 9．4 | 87.8 |
| 523.1 | 9.532 .4 | 14.5 | 41.7 | 19.5 | 50.9 | 24.5 | 60.2 | 29.5 | 69.4 | 34.5 | 78. | ． | 0 |
| 623.3 | 9.632 .6 | 14.6 | 41.9 | 19.6 | 51.1 | 24.6 | 60.4 | 29.6 | 69.6 | 34.6 | T8．9 | 39.6 | 88.1 |
| 23.5 | 9 \％ 32.8 | 14.7 | 42.0 | 19.7 | 51.3 | 24.7 | 60.6 | 29.7 | 69.8 | 34. | \％9．1 | 39.7 | 88 |
| 823.7 | 9.8333 .0 | 14.8 | 42.2 | 19.8 | 51.5 | 24.8 | 60.7 | 29. | 70．0 | 34.8 | 79．3 | 39.8 | 88.5 |
| 23.9 | 933 | 14.9 | 42.4 | 19.9 | 51.7 | 24.9 | 60.9 | 29.9 | \％0．2 | 34.9 | 79. | 39.9 | 88.7 |

## TABLE NO．XIII．

## Level Cross Sections．

## cubic yards in corresponding prisms 100 feet long．

Road－bed 20 feet wide．
Side slopes 1 to 1 ．

| $\frac{3 x}{3}$ |  | $\begin{aligned} & \text { 总 } \\ & \text { 荡 } \end{aligned}$ | 邑势势 | 药 |  | $\begin{aligned} & \text { 荮 } \\ & \text { 苞 } \end{aligned}$ | 翟部需 |  |  | $\begin{aligned} & \text { 毞 } \\ & \stackrel{y y y y}{*} \end{aligned}$ | $\begin{aligned} & \text { 률률 } \\ & \text { n } \end{aligned}$ |  | $\begin{aligned} & \text { gen } \\ & \text { 咅名 } \end{aligned}$ | $\begin{aligned} & \text { 总 } \\ & \text { 感 } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 5.0 |  | 10 | 1111 | 15 | 1944 | 20 | 2963 | 25 | 4167 | 30.0 | 5556 | 35.0 | 7130 |
|  | 7 |  |  |  | 1126 | 15. | 1963 | 20.1 | 2985 | 25. | 4193 | 30.1 | 5.585 |  | 71 |
|  | 15 |  |  | 10.2 | 41 | ． | 1982 | 20.2 | 3008 | 25.2 | 4219 | 30.2 | 5615 | 35.2 | 7196 |
|  | 23 | 5.3 | 4 | 10.3 | 1156 | 15.3 | 2000 | 20.3 | 3030 | 2．）． 3 | 4245 | 30.3 | 564．） | 35.3 | 72：30 |
|  | 30 | 5.4 | 508 | 10.4 | 1171 | 15.4 | 2019 | 20.4 | 30 万2 | $\because 5$. | 4271 | 30. | 5675 | 3 3． | 7264 |
|  | 38 | 5.5 | 519 | 10.5 | 1186 | 15.5 | 2038 | 20.5 | 3075 | 25. | 4297 | 30.5 | 5705 | － | 97 |
|  | 46 |  | $5 \cdot 1$ | 10.6 | 1201 | 15.6 | 2057 | 20.6 | 3098 | 25. | $43 \geqslant 4$ | 30.6 | 5735 | 3.56 | 831 |
|  | 54 |  | 543 | 10.7 | 1217 |  | 2076 | 20.7 | 3120 |  | 4350 |  | 576. |  | 365 |
|  | 62 |  | 5.4 | 10.8 | 32 |  | 2095 | 20.8 | 3143 | 25 | 4376 | 30.8 | 5795 | 35.8 | 7399 |
| 0.9 | 70 | 59 | 566 | 10.9 | 1247 | 15.9 | 2114 | 20.9 | 3166 | 25 | 4403 | 30. | $58 \%$ | 35.9 | 33 |
|  |  |  |  |  |  |  |  |  |  |  | 4430 |  |  |  | 67 |
|  |  |  | 590 | 11 | 1279 |  | 215 | 21.1 | 3212 | 26 | 4456 | 31.1 | 588 | 36 | 01 |
|  | $9+$ |  |  | 11.2 | 294 | 16 | 2172 | 31.2 | 3235 | 26. | 4483 | 31.2 | 591 | 36.2 | 535 |
|  | 103 |  | 614 | 11 | 1310 | 16.3 | 2191 | 21.3 | 325 | 26. | 4510 | 31.3 | 94 | 6.3 | 569 |
|  | 111 | 6.4 | 626 | 11.4 | 26 | 16.4 | 11 | 21. | 3281 | 26. | 453 | 1. | 97 | 6.4 | 04 |
|  | 119 | 6.5 | 638 | 11.5 | 1342 | 16.5 | 2231 | 21.5 | 3305 | 26. | 4564 | 31.5 | 600 | 6. | 638 |
| 1.6 | 128 | 6.6 | 650 | 11.6 | 135 s | 16.6 | 2250 | 21.6 | 3328 | 26. | 4591 | 31.6 | 60：3 | 36. | 672 |
|  | 137 | 6.7 | 66： | 11.7 | 1374 | 16.7 | 2270 | 21.7 | 3351 | 36. | 4618 | 31. | $60 \%$ | 36 | 07 |
|  | 14．） |  | 675 | 11.8 | 1390 | 16.4 | 2：90 | 21. | 337 | 26 | 4645 | 31. | 610 | 36 | 43 |
| 1.9 | 154 | 6. | 68 | 11.9 | 1406 | 16.9 | 2310 | 21. | 339 | 26 | 467 | 31.9 | 61 | 36 |  |
|  |  | ． | ． 0 |  |  |  | （1） | 2 | 3422 |  | 4700 | ． | 163 | 7．0 | 相 |
|  | 172 | 7.1 | 713 | 12.1 | 1439 | 17. | 2350 | 22.1 | 3446 | 27. | 4727 | 32.1 | 619 | 37.1 | 7846 |
| 2.2 | 181 | 7.2 | 725 | 12.2 | 14.5 | 17.2 | 2370 | 22.2 | 3470 | 27.2 | 4755 | 32.2 | 622 | － | 881 |
|  | 190 | 7. | 738 | 12.3 | 1471 | 17.3 | 2390 | 22.3 | 3494 | 27. | 4783 | 32.3 | 625 | 37.3 | 916 |
|  | 199 |  |  |  | 1488 |  | 2410 |  | 3518 | 27. | 4810 | 32.4 | 6． 98 | 37 |  |
|  | 20 | 7.5 | 764 | 12 | 1505 |  | 2431 | 22. | $354 *$ | 27 | 4838 | 33.5 | 631 | 37 | 986 |
|  | 21 | 7. | 777 | 12.6 | 1521 |  | 2451 | 22.6 | 5.56 | 27. | 4866 | 32.6 | 635 |  | 8021 |
|  | 221 |  | 790 | 13.7 | 1538 |  | 2471 | 22.7 | ， | 97. | 4894 |  | 638 |  | 8057 |
| 2．8 | 236 | 7.8 | 803 | 12.8 | 1.55 .5 | 17.8 | 2492 | 23.8 | 3614 | 27.8 | 4922 | 32.8 | 6414 | 37.8 | 8093 |
|  | 216 | 7.9 | 816 | 12.9 | 1572 | 17.9 | 2513 | 23.9 | 3639 | 27.8 | 4950 | 32.9 |  |  |  |
|  |  | 8. |  |  |  |  |  | 23.0 | 2603 |  | 4978 |  |  |  |  |
|  | 2． | 8． | 843 | 13.1 | 1 | 18.1 |  | 23.1 | 3687 | 28.1 | 5006 | 33. | 6510 |  | 199 |
|  |  | 8.2 | 856 | 13． | 1623 | 18.2 | 2.575 | 23.2 | 3712 | 28.2 | 034 | 33. | 654 | ， | 34 |
|  | 28.5 |  | 870 |  | 1640 |  | 2591 | 23.3 | 373 | 28. | 5063 |  | 57 |  | 270 |
|  | 29. | 8.4 | 884 | 13.4 | 1658 | 18.4 | $261 \%$ | 23.4 | 3761 | 28.4 | 091 | 33.4 | 660 |  | 8306 |
|  | 30. | 8.5 | 897 | 13.5 | 1675 | 18.5 | 2638 | 2：3．5 | 3786 | 28.5 | 5119 | 33. | 663 |  | 8342 |
|  | 31 | 8. | 91 | 13 | 169. | 18 | 26.9 | 23.6 | 3811 | 28.6 | 5148 | 33 | 66 |  | 83 |
|  | $32 \cdot$ | 8.7 |  | 13 | 1710 | 18. | 2650 | 23. | 536 | 28.7 | 177 | 33.7 | 670 |  | 8414 |
|  | 3：35 | 8.8 | ， | 10 | 1728 | 18.8 | 2 | 23.8 | 3861 | 28.8 | 5 | 33.8 | 673 |  |  |
| 3.9 | 345 | 8.9 | － | 13 | 1745 | 18.9 | $2 \pi$ | 23.9 | 38 | 28 | 52 | － | 6767 |  |  |
|  | ， | 3.0 | 96 | 14.0 | 178 | 19.0 | 274 | 24.0 | 3911 | 29.0 | 5263 | 34.0 | 6800 | 39.0 | 552 |
|  | 366 | ， | 981 | 14.1 | 1781 | 19.1 | 276 | 24 | 3936 | 29.1 | 5292 | 34.1 | 683 | 39 | 559 |
| 4.2 |  | 9.2 | 99． | 14.2 | 1799 | 19.2 | 278 | 24. | 3962 | 29.2 | 321 | 34.2 | 686 | 39.2 | 3595 |
| 4.3 | 387 | 9.3 | 1009 | 14.3 | 172 | 19.8 | 2809 | 24. | 3987 | 29.3 | 53．20 | 34.3 | 6898 | 39. | 5031 |
|  | 33 | 9.4 | $10 \cdot 4$ | 14.4 | 183 | 19.4 | 2831 | 24.4 | 4012 | 29.4 | 318 | 34.4 | 6931 | 39.4 | 8663 |
| 4.5 | 408 | 9.5 | 10：38 | 14.5 | 1853 | 19.5 | 2853 | 24.5 | 4038 | 29.5 | 5408 | 34.5 | 6964 | 39.5 | 8705 |
|  | 419 | 9.6 | 1052 | 14.6 | 1871 | 19.6 | 2875 | 24.6 | 4064 | 29.6 | 5438 | 34.6 | 6997 | 39.6 | 8741 |
|  | 430 | 9.7 | 1067 | 14.7 | 1889 | 19.7 | 2897 | 24. | 4089 | 29.7 | 5467 | 34.7 | ז030 | 39. | $87 \% 8$ |
|  | 441 | 9.8 | 1082 | 14.8 | 1908 | 19.8 | 2915 | 24.8 | 4115 | 29.8 | 5496 | 34.8 | ¢063 | 39.8 |  |
|  | 45 |  | 1096 | 149 | 1926 | 19.9 | 2941 | 24.9 | 414 | 29.9 | 55：6 | 34.9 | 7096 | 39.9 | 8852 |

Side Tmiangles.
CUBIC Yards in corresponding prisms 100 feet long.
Road-bed 20 feet wide.
Side slopes 1 to 1.


TABLE NO．XV．
Level Cross Sections．
cubic yapds in corresponding prisms， 100 feet long．
Road－bed， 24 feet wide．
Side slopes， 1 to 1.

| $\begin{aligned} & \text { 澧 } \\ & \text { 畐 } \end{aligned}$ | $\begin{aligned} & \text { 유를 } \\ & \text { By } \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { 荮 } \\ & \stackrel{\text { ex }}{\text { an }} \end{aligned}$ | 品我 | 䓲 |  |  | 言器 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | 59 |  |  |  | 00 |  |  |
|  | 9 |  | 5.50 | 10 | $12 \pi 6$ | 15 | 2187 | 20.1 | 3283 | 25. | 4564 | 30 | 6031 | 35.1 | 7683 |
|  | 18 | 5.2 | 52 | 10.2 | 1292 | 15.2 | 2：07 | 20.2 | 3307 | 25.2 | 4592 | 30.2 | 6062 | 35.2 | 7718 |
|  | 27 | 5.3 | － | 10.3 | 1308 | 15.3 | 2227 | $\because 0.3$ | 3331 | 25.3 | 4620 | 30.3 | 6094 | 35.3 | 7753 |
|  | 36 | 5. |  |  | 1325 |  | 2247 | 20.4 | 3355 | ， 5 | 4647 | 30.4 | 6125 | 35 | 7788 |
|  | 45 |  | 601 | 10.5 | 42 | 15. | 2 268 | 20. | \％9 | 25.5 | 4635 | 30 | 6156 | 35.5 | 7823 |
|  | 55 | 5.6 | 614 | 10.6 | 1358 | 15.6 | 2288 | $\because 0.6$ | 3403 | －5 | 470：3 | 30. | 6188 | 35.6 | 858 |
|  | 6 | 5. | 627 | 10 | 1375 | 15 | 2308 | 20 | 3427 | 25.7 | 4731 | 30. | 6320 | 35. | 894 |
|  | ， | 5. | 640 | 10.8 | 1392 | 15．8 | 2329 | 20.8 | 3451 |  | $4 i 59$ | 30. | 6251 | 35 | 929 |
| 0.9 | 83 | 5.9 | 5 | 10.9 | 1409 | 15.3 | 2350 | 20.9 | 3476 | 25 | 4787 | 30.9 | 6283 | 35.9 | ¢964 |
|  | 93 |  |  |  |  |  |  |  |  |  |  |  | 5 | 36.0 | 00 |
|  | 102 |  | 680 |  |  |  | 391 | 21. | 24 | 2 | 484：3 | 3 | 347 | 36 | 36 |
|  | 112 |  | 93 | 11 | 146 | 16． | 2412 | 21.2 | 3.74 | 26 | 4871 | 31.2 | 6379 | ：36．2 | 71 |
|  | 122 | 6.3 | $70 \%$ | 11.3 | 1477 | 16.3 | 2433 | 21.3 | 3574 | 26 | 4900 | 31. | 6411 | 36.3 | 8107 |
|  | 132 | 6.4 | 721 | 11.4 | 149.5 | 16. | 24.54 | 21.4 | 359 | 26. | 4928 | 31 | 644 | 36. | 8143 |
|  | 14． | 6.5 | 734 | 11 | 1512 | 16. | 475 | $\because 1$. | 3623 | 26 | 4956 | 31 | 6475 | 36. | 79 |
|  | 152 | 6.6 |  |  | 29 | 16 | 2496 | 21. | 3648 | 26 | 4985 | 31 | ） | 36 | 8215 |
|  | 163 |  |  |  |  | 16. | 2517 | 21 | 3673 | 26 | 5014 | 31.7 | 540 | 36 | 8251 |
|  | 17. |  |  | 11.8 |  | 16.8 | 539 | 21. | 3698 | 26 | 042 | 31.8 | 6572 | 36 | 287 |
|  | 18．） | 6.9 | 790 | 11 |  | 16.9 | 2560 | 21. | 37 | 26 | 5071 |  | 66 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 59 |
|  | ， |  |  |  | 1618 |  |  | 22. | 37 | 97 | ， | 32.1 |  |  |  |
|  | 213 | 7.2 |  |  | 1636 |  | $2(125$ | 22.2 | 3799 |  | 5158 |  | 6702 |  | 8432 |
|  | 224 | 7. | 846 | 12.3 | 16.54 | 17.3 | 6 | 22.3 | 8.4 | 27. | 187 | 32.3 | 6735 |  | 8468 |
|  | 23.5 | 7.4 | 861 |  | 1672 |  | 2668 | $2 \%$ ． | 3849 |  | 216 | 32.4 | ¢768 |  | 505 |
|  | 24．） | 7.5 | 875 | 12.5 | 1690 | 17.5 | 2690 | 22.5 | 3875 | 27 | 45 | 32 | 6801 |  | 542 |
| 2.6 | 2.56 | 7.6 | 889 | 12.6 | \％ 0 | 17.6 | 2712 | 22.6 | 3901 | 27. | 5275 | 33.6 | 683 |  | 578 |
|  | 26 | 7.7 | 0 | －12．7 |  |  | 2734 | 22.7 | 392 | 27 | 5.304 | 32.7 | 6867 |  | 15 |
|  | 278 |  | 91 | 12.8 | 174.5 |  | 2756 | 22．8 | 39.5 | 27. | 5，33 | 32. | 6900 |  | 8652 |
| 2.9 | 289 | 7. | 933 | 12.9 |  | 17 |  | 22.9 |  | 27. |  | 32. | 693 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 311 | 8.1 | 963 | 13 | 800 | 18.1 | 822 | 23.1 | 4030 | 28 | 22 | 38. | 000 |  | \％63 |
| 3.2 | $3 \stackrel{ }{ }$ | 8. | 978 | 13.2 | 1819 | 18.2 | 2845 | 23.2 | 4056 | 28. | 52 | 33.2 | \％03 |  | 800 |
|  | 3334 |  | 993 | 13.8 | 1837 | 18. | 2867 | 23. | 4082 | 28 | 5482 | 33. | 067 |  | 8837 |
|  | 345 |  | 1008 |  |  |  | ． |  | 410 |  | 12 | 33 | 101 |  | 88.5 |
|  | 3.56 |  | 1023 |  | 18 | 18.0 | 2912 | $2 . .6$ | 4134 | 28. | 5542 | 33. | T13 |  | 8912 |
|  |  |  |  |  | 394 | 18.6 | 293.$)$ | －3． | 4161 | 28 | － | 33.6 | ， |  | 8949 |
|  | 380 |  | 54 |  | 1913 |  |  |  | 418. |  | 602 |  | 硣 |  | 8987 |
| 3.8 | 391 | 8.8 | 069 | 13.8 | 1932 | 18.8 | 29＞0 | 23.8 | 4213 | 28. | 5632 | 33. | T236 | 8． | 9025 |
| 3.9 | 403 | 8.8 | 1084 | 13.9 | 1951 | 18.9 | 3003 | 23.9 | $4: 40$ | 28. | $566^{2}$ | 33.9 | 7270 |  | 0 |
|  | 位 |  | 1100 | 14.0 |  | 10 | 2 |  | 4268 | 29. | 5693 | 34 | ז304 | 39 | 9100 |
|  |  |  |  |  |  | 19 | － | 24.1 | 4293 | 2 | 5723 | 34． | 773 | 39.1 | 9138 |
|  | 1 | 9． | 131 | 14.2 | 2009 | 19.2 | 3105 | 24.2 | 4．220 | 29. |  | 34. | 2372 | 39.2 | 176 |
|  | 4.11 | 9.3 | 147 | 14.3 | $20 \geq 8$ | 19.3 | 3095 | 24.3 | $434 \sim$ | 29. | 5T84 | 34. | 7406 | 39.3 | 2214 |
| 4.4 | 463 | 9. | 1163 | 14.4 | 2048 | 19.4 | 3118 | 24.4 | 4374 | 29. | 581.5 | 34. | 8441 | 39.4 | 3252 |
| 4.5 | 47. | 9. | 179 | 14. | 2088 | 19.5 | 3142 | 24.5 | 4401 | 29.5 | 5845 | 34.5 | 2475 | $: 39$ | 9290 |
|  | 487 | 9 | 95 | 14 | 208 T | 19.6 | 3165 | 24.6 | 442 | 29. | 5876 | 34. | 5509 | 39.6 | 3328 |
|  | 500 |  | 1211 |  | \％ | 19.7 | 189 | 24.7 | 4455 | 29.7 | 5907 | 34.7 | 7544 | 9. | 9：366 |
|  | 512 |  | 122 | 14.8 | 2127 | 19 | 3212 | 24.8 | 4482 | 29.8 | 5938 | 34．8 | 7579 | 39.8 |  |
| ， | 524 | 9.9 | 1243 | 14.9 | 2147 | 19 |  | 24.9 | 4510 | 29.9 | 5969 | 34.9 | －13 | 39.9 |  |

## TABLE NO. XVI.

## Side Triangles.

CUBIC fards in corresponding prisms 100 feet long.
Road-bed 24 feet wide.


## TABLE NO．XVII．

## Level Cross Sections．

cubic yards in corresponding prisms， 100 feet long．

Road－bed 28 feet wide．

| $\begin{aligned} & \text { 戒 } \\ & \text { 呺 } \end{aligned}$ |  |  | 号荡 |  |  |  | $\begin{aligned} & \text { yed ix ix } \\ & \text { bun } \end{aligned}$ |  |  | 荘 |  | $\begin{aligned} & \text { 品 } \\ & \substack{\text { co }} \end{aligned}$ |  | 毞 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 |  |  | 10.0 |  | 15．0 |  | 20.0 | 35．6 |  |  |  |  |  |  |
|  | 10 | 5.1 | 6 | 10.1 | 1425 | 15.1 | 2410 | $\because 0.1$ | 3581 | 25. | 4936 | 30.1 | 647\％ | 3.5 | 03 |
|  | 21 | 5.2 | 639 | 10.2 | 1443 | 15.2 | 2432 | 20.2 | 3606 | 25.2 | 491i5 | 30.2 | 6.510 | 35. | 39 |
| 0.3 | 31 | 5. | （6）t | 10.3 | 1461 | 15.3 | 24.4 | 20.3 | 3631 | 25.3 | $499+$ | 30．：3 | 6\％43 | 35. | 8276 |
|  | 42 | 5.4 | 668 | 10.4 | 1479 | 15.4 | 2475 | 20.4 | $365 \%$ | 25.4 | $50 \geqslant 4$ | 30.4 | 6.55 | 3.5 | 8312 |
|  | 53 |  | ce | 10.5 | 1497 | 15.5 | 2497 | 20.5 | 36 S 2 | 25.5 | 50.3 | 30.5 | 6608 | 3.5 | 8349 |
|  | 64 |  | 697 | 10.6 | 1515 | 15.6 | 2519 | 20.6 | 3708 | 25.6 | 5082 | 30.6 | 6641 | 33 | $83 \leq 6$ |
|  | 7 |  | 711 | 10.7 | $15: 34$ | 15. | 41 | $\because 0.7$ | $3 \sim 34$ | －5． 7 | 5111 | 30. | 6674 | 35 | 23 |
|  | 8 |  | 726 | 10.8 | 552 | 15.8 | 56 | 20.8 | 3759 | －5． | 5141 | 30.8 | 6708 | 35.8 | 8459 |
| 0.9 | 96 | 5.9 | T | 10.9 | 1570 | 15.9 | 2585 | 20.9 | 3 358 | 23.9 | 5170 | 30.9 | 6.4 | 35.9 | 8496 |
|  | 107 |  | 7.6 |  |  |  | 7 |  | 381 | 26.0 | 5200 |  | ， 4 |  | 33 |
|  | 119 |  | 770 | 11.1 | 1607 | 16.1 | 2630 | 21.1 | 3837 | 26.1 | 5230 | 31 | 6807 | 36.1 | T0 |
|  | 130 | 6.2 | 785 | 11.2 | 1626 | 16.2 | 2652 | 21.2 | 3863 | $\because 6.2$ | 5259 | 31.2 | 6841 | 315.2 | 08 |
|  | 141 | 6.3 | 800 | 11.3 | 164. | 16.3 | 267 | 21.3 | 3889 | 26.3 | 5289 | 31. | 6874 | 36.3 | 8645 |
| 1.4 | 15. | 6.4 | 815 | 11.4 | 1664 | 16.4 | 2697 | 21.4 | 3915 | 26.4 | 5319 | 31. | 6908 | 36. | 8682 |
| 1.5 | 164 | 6.5 | $8: 31$ | 11.5 | 168： | 16.5 | 2719 | 21.5 | 394. | －6．5 | 5349 | 31.5 | 6942 | 36. | 8719 |
| 1.6 | 175 | 6.6 | 846 | 11.6 | 1701 | 16.6 | 2749 | 21.6 | 3968 | 26.6 | 5339 | 31. | 697 | 36 | 8757 |
| 1.7 | 187 | 6.7 | 861 | 11.7 | 1720 | 16. | $2 \pi 6$ | 21.7 | 3994 | 26. | 5409 | 31. | 7009 | 36 | 94 |
| 1.8 | 199 | 6. | 87 | 11 | 1739 | 16. | 27 | 21.8 | 4021 | 26.8 | 5439 | 31. | 7043 | 36 | 8832 |
| 1.9 | 210 | 6.9 | 80 | 11.9 | 175 | 16.9 | 281 | 21.9 | 4047 | 26.9 | 5470 | 31 | 70 | 36 | \％ |
| 2.0 | 2 | 7. | 907 | 12.0 |  | 17. | ． | 2.0 | 4074 | 2．0 | 5500 | 32.0 | 7111 | 37.0 | 8907 |
| 2.1 | 234 | 7.1 | 923 | 12.1 | 179 | 17.1 | 285 | 22.1 | 410 | 27.1 | 5530 | $3 \cdot .1$ | 7145 | 37. | 8945 |
| 2.2 | 246 | 7.2 | 939 | 12.2 | 1816 | 17.2 | 2879 | 22.2 | 4128 | 27.2 | 5501 | 32. | 7179 | 37. | 83 |
| 2.3 | 2.78 | 7. | 9 | 12.3 | 1836 | 17.3 | 2903 | 22.3 | 4154 | 27. | 5.51 | 32. | 7214 | 37. | 21 |
| 2.4 | 270 | 7. |  | 12.4 | 185 | 17.4 | 2926 | $2 \cdot 2$ | 4181 | 27. | 5622 | 32. | 7248 |  | 5 |
| 2.5 | 28. | 7.5 | 986 | 12.5 | 18 | 17 | 2949 | $2 \pm .5$ | 420s | 27.5 | 5653 | 32. | 728 |  | 3097 |
| 2.6 | 29.5 | 7. | 1002 | 12.6 | 1895 | 17.6 | 2972 | $3 \cdot 6$ | 4235 |  | 5684 | 32. | 7317 | 37.6 | 35 |
| 2.7 | 307 | 7.7 | 1018 | 12.7 | 1914 | 17.7 | 2991 | 22. | 426 |  | 5714 |  | 735 |  | 9174 |
| 2.8 | 319 | 7.8 | 1034 | 12.8 | 1934 | 17.8 | 3019 | 22.8 | 4290 | 27.8 | 5745 | 32.8 | 7386 | 37. | 9212 |
| 2.9 | 332 | 7.9 | 1050 | 12.9 | 19.5 | 17.9 | 3043 | 22.9 | 4317 | $\checkmark 7.9$ | 5776 | 32.9 | 7421 | 37 | 9250 |
|  | 314 | 8.0 |  |  | 197 |  |  | 23.0 | 4344 | 28.0 | 5807 | 33.0 | 7456 |  | 9289 |
|  | 3.7 | 8.1 | 1083 | 13.1 | 1994 | 18.1 | 3090 | 23.1 | 4372 | 28.1 | 5839 | 33.1 | 7491 | 8， |  |
| 3.2 | 370 | 8.2 | 1099 | 13.2 | 2014 | 18.2 | 3114 | 23.2 | 4399 | 28.2 | 5870 | 33.2 | 7525 |  | 9366 |
| 3.3 | 38：3 | 8.3 | 1116 | 13.3 | 2034 | 18.3 | 3138 | 23.3 | 4427 | 28.3 | 5901 | 33.3 | 7560 | 38. | 9405 |
| 3.4 | 395 | 8.4 | 1132 | 13.4 | 2055 | 18.4 | 3162 | 23.4 | 44．5： | 28.4 | 5932 | 33. | 7595 | 38. | 9444 |
| 3.5 | 408 | 8.5 | 1149 | 13.5 | 2075 | 18.5 | 3186 | 23.5 | 448\％ | 28.5 | 5964 | 33.5 | 763 |  | 9482 |
|  | 421 | 8.6 | 1166 | 13.6 | 20 | 18.6 | 3210 | 23.6 | 4510 | 28.6 | 5995 | 33.6 | 766 | 38 | 9.21 |
|  | 434 | 8. | 1183 | 13 | 16 | 18.7 | 3234 | 23.7 | 4.5 | 28.7 | 6027 | 33.7 | 7701 | 38． | 9560 |
|  | 仡 | 8．8 | － | 13.8 | ， |  | 3259 | 23.8 | 4.56 | 28.8 | 6059 | 33.8 | 773 | 38. | 9599 |
| 3.9 | 461 | 8.9 | 1216 | 13.9 | 215 | 18.9 | 3 | 23.9 | － | 28 | 60 | 33 | 77 | 38.9 | 39 |
|  | 474 | 9.0 |  | 14.0 | 2178 | 19.0 | 3307 | 24.0 | 4632 | 29.0 | 6122 | 34.0 | 7807 | 3.0 | 678 |
|  | 487 | 9.1 | 1250 | 14.1 | 2199 | 19.1 | 3332 | 24.1 | 46：30 | 29.1 | 6154 | 34. | 784 | 39 | 717 |
| 4.2 | 501 | 9. | 1268 | 14.2 | 2219 | 19.2 | 3356 | 24.2 | 4679 | 29.2 | 6186 | 34. | 7879 | 39. | ${ }^{9756}$ |
|  | 514 | 9.31 | 128 | 14.3 | 2240 | 19.3 | 3381 | 24.3 | 4707 | 29.3 | $6: 18$ | 34.3 | 7914 | 39. | 9796 |
| 4． | 598 | 9.4 | 1302 | 14.4 | 2261 | 19.4 | 3416 | 24.4 | 4735 | 29.4 | 6250 | 34.4 | \％ | 39.4 | 8835 |
| 4.5 | 542 | 9.51 | 1319 | 14.5 | 2282 | 19.5 | 3431 | 34.5 | 4764 | 29.5 | $628:$ | 34.5 | 79ะ6 | 39.5 | 9875 |
| ． 6 | 50.5 | 9.6 | 1337 | 14.6 | 2304 | 19.6 | 3455 | $\because 4.6$ | 4792 | 29.6 | 6315 | 34.6 | 812： | 39.6 | 9915 |
| 4.7 | 569 | 9.7 | 1354 | 14.7 | 2325 | 19.7 | 3480 | 24.7 | 4821 | $\because 9.7$ | 6345 | 34.7 | 8058 | 39. | 9954 |
| 4.8 | 583 | 9.8 | 1372 | 14.8 | 2346 | 19.8 | 3505 | 24.8 | 48.50 | 29.8 | 6379 | 34.8 | 8094 | 39.8 | 9994 |
| 4.9 | 597 | 9.9 | 1390 | 14.9 | 2367 | 19.9 | 3530 | 24.9 | 4879 | 29.9 | 6412 | 34.9 | 813 | 39.9 | 4 |

## TABLE NO．XVIII．

Side Triangles．
CUBIC FARDS IN CORRESPONDING PRISMS， 100 FEET LONG．
Road－bed 28 feet wide．
Side slopes 1 to 1.

|  |  |  |  | ex |  |  |  |  |  |  | 曾荡 | on | 会荡荡 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  | 72.2 | 30.0 | 81.5 |  | 90.7 |
|  |  |  |  | 10.1 | 44. | 15.1 | 03．9 | 20.1 | 63.1 | 25． 1 | 72． 4 | 30.1 | 81.7 | 3．）． | 90.9 |
|  | － 3 |  | 35.6 | 10．2 | 44.8 | 15.2 | 54 | $\because 0.2$ | 63.3 | 25.2 | 72.6 | 30.2 | 81.9 | 3．）． 2 | 91.1 |
|  |  |  | 35.7 | 10.3 | 45.0 | 15.3 | 54.3 | 20.3 | 63.5 | 25．3 | T2． 8 | 30.3 | $8: .0$ | 35.3 | 91.3 |
|  | 96 | 5 | 35.9 | 10.4 | 45．2 | 15. | 54 | 20.4 | 6：3．7 | 2i）． 4 | 73.0 | 30.4 | 82．2 | 35 | 91.5 |
|  | 26.9 |  | 36.1 | 10.5 | 45.4 | 15.5 | 54 | 20.5 | 63.9 | －${ }^{\text {¢ }} 5$ | 73.1 | 30.5 | 82.4 | 3 3 .5 | 91.7 |
|  | 27.0 |  | 36. | 10. | 45.6 | 15.6 |  | 20.6 | 64.1 | 25.6 | 73.3 | 30.6 | 82.6 | 35 | 91.9 |
|  | 2 |  | 36.5 | 10.7 | 45.7 | 15.7 | 5. | 20.7 | 64.3 | 25.7 | 73.5 | 30.7 | 82． 8 | 35． 7 | 92.0 |
|  |  |  |  | 10.8 | 45.9 | 15．8 | 5 | 20.8 | 64.4 | 25.8 | 83．7 | 30.8 | 83.0 | 35. | 92.2 |
| 0. | 27.6 | 5 | 36.9 | 10.9 | 46.1 | 15.9 | 55 | 20.9 | 64.6 | 25.9 | 73.9 | 30.9 | 83.1 | 3 3． 9 | 92.4 |
|  |  |  |  |  | 46.3 | 16.0 |  |  | 64.8 | 2．0 |  |  |  |  | 92.6 |
|  |  |  |  |  |  | 16.1 |  |  | 65.0 | 26.1 |  | 31.1 | 83.5 | 36.1 | 92.8 |
|  | 28.1 | 6. | 37 | 11.2 | 46 | 16.2 | $5 \overline{5}$ | 21.2 | 65.2 | ？6．2 | 74. | 31.2 | 83.7 | 36.2 | 93.0 |
|  | 28.3 |  |  | 11. | 46.9 | 16.3 | 50.1 | 21.3 | 65.4 | 26.3 | 74 | 31.3 | 83.9 | 36.3 | 93.1 |
|  | 28.5 | 6. | 37.8 | 11.4 | 47.0 | 16.4 | 56.3 | 21.4 | 65.6 | 26.4 | 74. | 31 | 84.1 | 36.4 | 93.3 |
|  | 28.7 |  | 38.0 | 11.5 | 47.2 | 16.5 | 56 | 21.5 | 65.7 | 26.5 | 75. | 31.5 | 84.3 | 36.5 | 93.5 |
|  | 28.9 | 6. | 39.1 | 11.6 | 47.4 | 16.6 | 56 |  | 65.9 | 26.6 | 75. | 31.6 | 84.4 | 36. | $93 . \dot{4}$ |
|  |  | 6. | 38.3 | 11.7 | 47.6 | 16.7 | 56.9 |  | 66.1 | $\because 6.7$ | \％ | 31.7 | 84.6 | 36.7 | 93.9 |
|  | 3 | 6. | 38.5 |  | 47.8 |  |  |  | 66.3 | 26.8 | （5） |  | 84 |  | 94.1 |
| 1 | 29.4 | 6. | 28 7 | 11.9 | 48.0 | 16.9 | 57．2 | 21.9 | 66.5 | $\because 6.9$ | 75.7 | 31.9 | 85.0 | 36.9 | 94.3 |
|  |  |  |  |  | 48． |  |  |  | 66.7 |  |  |  | 2 |  | 94.4 |
|  | 29.8 | 7. | 39 | 12.1 | 48.3 | 17.1 |  | $\because 2.1$ |  |  |  |  | 85.4 |  | 94.6 |
|  | 30.0 | 7.2 | 39.8 | 12.2 | 48.5 | 17.2 | 57 | 22.2 | 67.0 | 27.2 | 10 | 32． 2 | 85．6 | 37 | 94.8 |
| 2 | 30.2 | 1 | ：39．4 | 12.3 | 48.7 | 17.3 | 58.0 | 22.3 | 67.2 | 27.3 |  | 32.3 | 85 | 37.3 | 95.0 |
|  | 30.4 | 7. | 39.6 | 12.4 | 48.9 | 17.4 | 58.1 | 22． 4 | 67.4 |  | 76 | 32.4 | 85.9 |  | 95.2 |
|  | 30.6 |  | 39.8 | 12.5 | 49.1 | 17.5 | 58.3 | 22.5 | 67.6 |  | 76.9 | 39．5） | 86.1 | 37.5 | 95.4 |
| 2.6 | 30.7 | 7. | 40.0 | 12.6 | 49.3 | 17.6 | 58.5 | 22.6 | 67.8 | 27.6 | 77.0 | 32.6 | 86.3 |  | 95.6 |
| 2 | 30.9 | 7 | 40.2 | 12.7 | 49.4 | 17.7 |  | 22.7 | 68.0 |  | 77.2 | 32.7 | 6.5 | － | 95.7 |
| 2． | 31． | 7.8 | 40.4 | 12.8 | 49.6 | 17.8 | 58.9 | 22.8 | 68.1 |  |  | $32 . \mathrm{N}$ | 86. | 37 | 95.9 |
| 2.9 | 31.3 | 7. | 40.6 | 12.9 | 49.8 | 17.9 | 59.1 | 22.9 | 68.3 | 27 | 77.6 | 32.9 | 86.9 | 37.9 | 96.1 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 87.0 |  | 96.3 |
| 3 |  | 8. | 40.9 |  | 50.2 | 18.1 |  |  |  |  |  |  | 87.2 | 38.1 | 96.5 |
|  |  |  | 41.1 |  | 50.4 | 18.2 | 59.6 | 23． | 68.9 |  |  | 33． 2 | 87.4 | 38 | 96.7 |
|  | 32.0 | 8 | 41 | 13 |  | 18.3 | 59.8 | 23 | 69. | 28.3 |  | 33． 3 |  | 38 | 96.9 |
|  | 33． 2 |  | 41.5 | 13 | 50.7 | 18.4 | 60.0 | 23.4 | 69.3 | 28.4 | 78.5 | 33.4 | 87.8 | 38 | 97.0 |
|  | 32.4 |  |  | 13.5 | 50.9 | 18.5 | 60.2 |  | 69.4 |  | 78.7 | 33.5 | 88.0 | 38.5 | 97.2 |
|  | 32.6 | 8 | 41.9 | 13.6 | 51.1 | 18.6 | 60.4 | 23.6 | 69.6 |  | 78.9 | 33.6 | 88.1 | 38.6 | 97.4 |
|  | 32.8 |  |  | 13.7 |  | 18.7 | 60.6 | 23.7 | 69.8 | 28.7 | 79.1 | 33.7 | 88.3 | ：38．7 | 97.6 |
| 3.8 | 33.0 | 8.8 | 42．2 | 13.8 |  | 18.8 | 60.7 | 23.8 | 50.0 | 28.8 | 79.3 |  | 88.5 | 38.8 | 97.8 |
| 3.9 | 33.1 | 8.9 | 42.4 | 13.9 | 51.7 | 18.9 | 60.9 | 23.9 | 70.2 | 28.9 | 79.4 | 33.9 | 88．7 | 38.9 | 98.0 |
|  | 33.3 |  | 42.6 | 14.0 | 51.8 | 19.0 | 61.1 | ～．n | 50.4 | 2.0 | ． 0.6 | 34． | 88.9 | －3． | 98.1 |
|  | 33.5 | 9. | 42.8 | 14.1 | 52.0 | 19.1 |  | 24.1 | 10 | 29.1 | 79.8 | 34.1 | 89.1 | 39.1 | 98.3 |
|  | 33.7 | 9. | 43.0 | 14.2 | 52．2 | 19.2 | 61.5 | 24.2 | 70.7 | 29.2 | 80.0 | 34.2 | 89.3 | 39.2 | 98.5 |
| 4.3 | 3.3 .9 | 9. | 43.1 | 14.8 | 52.4 | 19.3 | 61.7 |  | 70.9 | 29.3 | 80.2 | 34.3 | 89.4 | 39.3 | 98.7 |
| 4.4 | 34.1 | 9.4 | 43.3 | 14.4 | 52.6 | 19.4 | 61.9 | 24.4 | 71.1 | 29.4 | 80.4 | 34.4 | 89.6 | 39.4 | 98.9 |
| 4. | $3+3$ | 9. | 43.5 | 14.5 | 52．8 | 19.5 | 62.0 | 24.5 | 71.3 | 29. | 80.6 | 34.5 | 89.8 | 39.5 | 99.1 |
|  | 34.4 | 9.6 | 43.7 | 14.6 | 53.0 | 19.6 | 62.2 | 24.6 | 71.5 | 29.6 | 80.7 | 34.6 | 90.0 | $: 19.6$ | 99.3 |
| 4.7 | 34.6 | 9.7 | 43.9 | 14.7 | 53.1 | 19.7 | 62.4 | 24.7 | 71.7 | 29.7 | 80.9 | 34.7 | 90.2 | 39.7 | 99.4 |
| 4.8 | 34.8 | 9. | 44.1 | 14.8 | 53.3 | 19.8 | 62.6 | 24.8 | 71.9 | 29.8 | 81.1 | 34.8 | 90.4 | 39.8 | 99.6 |
| 4. | 35.0 | 9.9 | 44.3 | 14.9 | 53.5 | 19.9 | 62．8 | 24.9 | 72.0 | 29.9 | 81.3 | 34.9 | 90.6 | 39.9 | 99.8 |

## TABLE NO．XIX．

## Level Cross Sections．

CUBIC YARDS IN CORRESPONDING PRISMS 100 FEET LONG．
Road－bed $\approx 8$ feet wide．

| $\begin{aligned} & \text { 总 } \\ & \text { 䁍 } \end{aligned}$ |  | $\begin{aligned} & \text { 薄 } \\ & \text { E. } \end{aligned}$ |  |  |  |  |  |  | gex |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 |  |  |  | 1222 |  | 2 | 20 |  | 25.0 |  |  | 8 | 35.0 |  |
|  | 10 |  |  |  | 36 |  | 1988 | 20 | － | 25.1 |  |  | 4799 ： |  |  |
|  | 21 |  |  |  | 1250 | 15.2 | 2004 | $\because 0.2$ | 2850 | 25.2 | 3789 |  | $48!1$ |  |  |
|  | 31 | 5. |  | 10 | 1265 | 15.3 | $20: 0$ | 20.3 | 2868 | 25.3 | 3809 | 30. | 4842 | 35. | 5968 |
|  | 42 | 5. | 614 | 10.4 | 1279 | 15. | 2036 | 20.4 | 2886 | 25． | 3829 | 30. | 4864 | 35. | 5992 |
|  | 52 | 5. |  | 10.5 | 1293 | 15.5 | 2052 | 20.5 | 2904 | $2 \overline{5}$ | 3849 | 30.5 | 4886 | 35 | 6015 |
|  | 63 |  | 639 | 10.6 | 1307 | 15.6 | 06 | 20.6 | 2922 | 25 | 3868 | 30 | 4907 |  | 39 |
|  | 7 |  | 651 | 10.7 | 322 | 15. | 085 | 20. | 2940 | 25.7 | 3888 | 30.7 | 49：9 |  | 062 |
|  | 8 |  | 664 | 10 | 336 | 15 | 2101 | 20. | 2958 | 25 | 390 | 30. | 4951 |  | 6086 |
| 0.9 | 95 | 5.9 | 676 | 10.9 | 50 | 15.9 | 2115 | 20.9 | $29 \% 6$ | 25. | 3928 | 30. | 4973 | 35.9 | 6110 |
|  | 10 |  |  |  |  |  |  |  |  |  |  |  | 994 |  |  |
|  | 116 |  | 702 |  | 1379 |  | 21 | 21 | 013 | 26.1 | 396 | 31.1 | 50 |  |  |
|  | 127 | 6.2 | 714 | 11.2 | 394 | 16. | 2166 | 21 | 3031 | 26 | 3988 | 31.2 | 50 | ¢ | 6181 |
|  | 138 | 6.3 | 727 | 11.3 | 08 | 16. | 2182 | 21.8 | 3049 | 26. | 400 | 31. | 06 | 36.3 |  |
|  | 149 | 6.4 |  | 11.4 | 1423 | 16. | 2199 | 21.4 | 306 | 26. | 4028 | 31. | 0 | 36.4 | － |
|  | 160 | 6.5 | 752 | 11.5 | 1438 | 16.5 | 2215 | 21.5 | 3086 | 26. | 4049 | 31. | 510 | 36.5 | 252 |
|  | 171 | 6.6 | 76.5 | 116 | 1452 | 16.6 | 223： | 21.6 | 3104 | 26. | 406 | 31.6 | 512 |  | 62 r6 |
|  | 182 |  | 77 | 11.7 | 1467 | 16.7 | 224 | 21.7 | 3122 | 26 | 40 | 31. | 514 |  | 6300 |
|  | 193 |  | 791 | 11 | 1 | 16 | 2265 | 21. | 314 | 2 | 410 | 31 | 517 |  | 63：4 |
| 1.9 | 20 |  | 804 | 11.9 | 49 | 16. | $2: 8$ | 21. | 3159 | 26 | 413 | 31 | 51 | 36 |  |
|  |  |  |  |  |  |  | S | 22．0 | 178 | \％． | 4150 | 22． | 5215 |  |  |
|  | 226 | \％ | 830 | 12.1 | 1520 | 17. | 2315 | 22.1 | 3196 | 27. | 4170 | 32.1 | 5 |  | 6396 |
|  | 237 | 7.2 | 84 | 12.2 | 1541 |  |  | 22.2 | 321 | 27. | 419 | 32.2 | 52 |  | 6420 |
|  | 24 | 7.3 |  | 12. |  |  | 23 | 22.3 | 3．3 |  | 421 | 32.3 | 520 |  |  |
|  | 26 |  | 869 | 12 | 1571 | 17.4 | 2365 | 22. | 32 |  | 4232 | 32 | 520 |  | 646 |
|  | 27 | 7.5 | 88： | 12 | 1586 | 17. | 2382 | 22 | 271 |  | 425 | 32 | 5326 |  | 649 |
|  | 28 | 7.6 | 89 | 12.6 | 1601 | 17 | 2399 | 22.6 | 329 |  | 427 | 3. | 534 |  | 651 |
|  | 294 | 7.7 | 908 | 12.7 | 1616 | 17. | 2416 | 22.7 | 330 | 27 | 429 | 32. | 537 |  | 6542 |
|  | 305 | 7.8 | 92 | 12.8 | 1631 | 17.8 | 2433 | 22.8 | 3327 | 27. | 431 | 32.8 | 539 |  | ． |
| 2.9 | 316 | 7.9 | 935 | 12.9 |  | 17.9 | 2450 | 22.9 | 3346 | 27.9 | 433 | 32.9 |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  | ， |  |  |
|  | 33 |  |  |  | ， |  |  |  |  |  | 4376 |  | 546 |  |  |
|  | 351 | 8 | 975 | 13.2 | 992 | 18.2 | 2501 | 23.2 | 40 |  | 11 |  |  |  |  |
|  | 362 | 8 | 988 | 13.3 | 207 | 18.3 | 2518 | 23.3 | 3422 | 28 | 441 | 33.3 | 5.50 |  | 688 |
|  | 374 | 8 | 1002 | 13.4 | 172 | 18.4 | 253 | 23.4 | 3441 | 28 | 443 | 33.4 | 553 |  | 613 |
|  |  | 8 | 1015 | 13 |  | 18. | 2552 | 23.5 | 346 | 28 | 446 | 33 | 55. |  | 13 |
|  | 39 | 8.6 | 研 | 15 |  | 18.6 | 25.0 | 23.6 | 4 |  | 4481 |  | 55 |  | 63 |
|  | 409 | 8. | 1042 | 1 |  | 18. | 2587 | 23. | 349 |  | 4502 | ¢ | 5598 |  | 6787 |
|  | 421 | 8.8 |  | 13.8 | 808 | 18.8 | 20 | 23.8 | 3517 |  | － | 83． | 5621 |  | ， |
| 3.9 | 433 |  |  | 13.9 |  | 18.9 | 262 | 23.9 | 35 | 28. | 454 | 33.9 |  |  |  |
|  | 444 | ， |  | 14. | ， | 1.0 | 2639 | 24.0 | 506 | 29.0 | 456 | 34.0 | 5667 | ． | 861 |
|  | 456 | 9. | 1097 | 14.1 | 1830 | 19.1 | 2656 | 24.1 | 3575 | 29.1 | 4586 | 34. | 569 |  | 886 |
| 4.2 | 468 | 9 | 1111 | 14.2 | 1846 | 19.2 | 2674 | 24.2 | 3594 | 29.2 | 4607 | 34.2 | 5713 | 9. | 611 |
|  |  | $\bigcirc$ | 12． | 14.2 |  | 19.3 | 69 | 24. | 14 | 29.3 | 402 | 34.3 | － |  | 明 |
|  | 492 | 94 | 1138 | 14.4 | 18 | 19.4 | 2709 | 24.4 | 030 | 29.4 | 4650 | 34.4 | 75 | 39. | 961 |
| 4.5 | 504 | 9.5 | 1152 | 14.5 | 189： | 19.5 | 2726 | 24.5 | 3652 | 29.5 | 4671 | 34.5 | 78 | 39. | 6886 |
| 4.6 | 516 | 9.6 | 1166 | 14.6 | 1909 | 19.6 | 2744 | 24.6 | 3672 | 29.6 | 4692 | 34.6 | 580 | 39. | 011 |
|  | 5 | 9.7 | 1180 | 14.7 | 1925 | 19.7 | 276 | 24.7 | 3691 | 29.7 | 4714 | 34. | 5828 | 39. | 036 |
| 4 | 5 | 9. | 1194 | 14.8 | 1940 | 19.8 | 2779 | 24.8 | 3711 | 29.8 | 4735 | 34.8 | 58. | 39. | ，061 |
| 4.9 | 553 | ． 9 | 120 | 14.9 | 1956 | 19.9 | 2797 | 24.9 | 3730 | 29.9 | 4756 | 34 | 875 | 39 | \％086 |

TABLE NO. XX.
Side Triangles.
cubic fards in corresponding prisms 100 feet long.
Road-bed 28 feet wide.


TABLE NO．XXI．

## Level Cross Sections．

cubic yards in corresponding prisms 100 feet long．
Road－bed 20 feet wide．
Side slopes $\frac{1}{1}$ to 1 ．

| $\begin{aligned} & \text { 范 } \\ & \text { 范 } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { 感 } \\ & \stackrel{y}{0} \end{aligned}$ |  |  |  |  |  | $\begin{aligned} & \text { 感 } \\ & \stackrel{y}{4} \end{aligned}$ | 号然荡 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | 19 |  | 1852 |  | 2431 |  | 3056 |  |  |
|  |  | 5. | 40 | 10.1 | 843 | 15． | 1330 | 0.1 | 1863 |  | 2443 |  | 3069 |  | 3741 |
|  | 15 | 5.2 | 410 | 10.2 | 85： | 15.2 | 1340 | 20.2 | 1874 |  | 2455 | 30.2 | 3082 | 35.2 | 3755 |
|  | 22 | 5.3 | 419 | 10.3 |  | 15.3 | 1350 | 20.3 | 1885 | 25 | 2467 | 30.3 | 3095 | 35.3 | 3769 |
|  | 30 | 5.4 | $42 \%$ | 10.4 |  |  | 1360 | 20.4 | 1896 | 25. | 479 | 30.4 | 3108 | 35 | 783 |
|  |  | 5.5 | 43.5 | 10.5 |  |  | 81 | 20 | 1908 | 25.5 | 1 | 30 | 1 | 35.5 | \％97 |
|  | 45 | 5 | 444 | 10.6 | 89 | 15.6 | 381 | 20.6 | 919 | 25， | 2503 | 30.6 | 3134 | 35.6 | 811 |
|  | 52 | 5.7 | 45 | 10 | 899 | 15. | 391 | 20. | 1930 | 25 | 2515 | 30.7 | 3147 | 35 | $38: 5$ |
|  | 6 | 5.8 | 461 | 10.8 | 908 |  | 1402 | 20. | 1941 | 25. | 2.527 | 30.8 | 316 | 35 | － |
| 0.9 | 67 | 5.9 | 469 | 10.9 | 917 |  | 1412 | 20.9 | 1953 | 25.9 | 2540 | 30.9 | 31 | 35 | 803 |
|  |  |  |  |  |  |  |  |  | 1964 | 2 |  |  | 3186 |  | ， |
|  |  | 6.1 |  | 11.1 |  |  | 33 | 21 | 1975 | 26 | 2564 | 31.1 | 3199 | 36 | 81 |
|  | 90 | 6.2 | 495 | 11.2 | 946 |  | 1443 | 21.2 | 1987 | 26.2 | 2576 | 31.2 | 3212 | 36 | 3895 |
|  | 98 | 6.3 | $50: 3$ | 11.3 | 5ั | 16.3 | 453 | 21.3 | 1993 | 26. | 258 | 31.3 | $3 \geqslant 2$ | 36. | 3909 |
|  | 106 | 6.4 | 512 | 11.4 | 6．） | 16 | 46 | 21.4 | 20 | 26. | 2601 | 31.4 | 3239 | 36 | 3923 |
|  | 113 | 6.5 | 521 | 11.5 | 974 | 16.5 | 1474 | 21.5 | 203 | 26. | 2613 | 31 | 3252 |  | 393 |
|  | 121 | 6.6 | 529 |  | 984 | 16. | 148.5 | 21. | $203 \%$ | 26. | 2626 | 31 | 265 |  | 951 |
|  | 129 | 6. |  |  | 993 |  | 149.5 | 21.7 | 2043 | 26. | 2638 | 31 | $32 \sim 9$ | 36 | 3966 |
|  | 136 | 6.8 |  | 11.8 | 1003 | 5． | 506 | 21.8 | 20.3 | 26.8 | 265 | 31.8 | 29 | 3 | 980 |
| 1.9 | 144 | 6.9 |  | 11.9 | 1013 | 16.9 | 16 | 21.9 | 206 | 26 | 266 | 31.8 |  |  | 09 |
|  | 15 | 7.0 | 56 | 12.0 | 1022 | 17. | ， | 22. |  |  |  | － | 3319 |  | 4008 |
|  | 160 | 7.1 |  | 12.1 | $103:$ | 17 | 1537 |  | 208 |  | 26 | 32 | 393 |  | 4023 |
|  | 167 | 7．2 |  | 12.2 | 1042 |  | 1548 | 22 | 2101 | 27 | 270 | 32. | 3345 | 37.2 | 4037 |
|  | 175 | 7.3 |  | 12 | 51 | 17.3 | 15.59 | 2 | 112 | 27.3 | 271 | 32.3 | 3359 | 37.3 | 4051 |
|  | $1 \times 3$ | 7.4 | 593 | 12 | 061 | 17. | 1569 | 22. | 2124 | 27. | 272 | 32.4 | 3372 | 37.4 | 4066 |
|  | 191 | 7.5 |  | 12.5 | 1071 | ． | 80 | 22.5 | 2135 | 27. | 273 | 32.5 | 硅 | 37 | 4080 |
|  | 199 | 7.6 | 616 | 13.6 | 1030 | 17.6 | 591 | 22.6 | 2147 | 27. | 275 |  | 338 |  | 4094 |
|  | 207 | 7.7 | 625 | 12.7 | 1090 |  | 1601 | 22 | 2159 |  |  |  | 31 |  | 4109 |
|  | 215 | 7.8 | 63 | 12.8 | 1110 |  | 1612 | ～． 8 | 21 | 27 | 27 | 32.8 | 342 |  | 4123 |
| 2.9 | 2\＃3 | 7.9 | － | 12.9 | 1110 | 17 | 16 | 22.9 |  | 27 |  | 32.9 | 34 |  |  |
|  |  |  |  |  | 19 |  |  | 23.0 | 2194 |  | 2800 | 3. | 345 |  | 152 |
|  | 239 | 8.1 | 661 | 13.1 | 1129 | 15 |  | 23.1 | 220. | 28.1 | 28 |  | 34 |  | 166 |
|  | 247 | 8.2 | 71 | 13.2 | 1139 | 18. | 16 5 | 23.2 | 2217 | 28.2 | 28 |  | 348 |  | 181 |
|  | 25. | 8.3 | $67!$ | 13. | 1149 |  |  | 23. | 2229 | 28.3 | 2838 | 33.3 | 349 |  | 195 |
|  | 263 | 8.4 |  |  | 9 | 18. | 1676 | 23 | 2240 | 28 | 2851 | 33.4 | 5 |  | 4210 |
|  | 27 | 8 | 697 |  | 1169 |  | 1687 | 23． | 2 5 | 28.5 | 28 |  | 35゙2 |  | 4224 |
|  | 27 | 8.6 |  |  | 1179 | 88． | 169 | 23.6 | 2264 | 28.6 | 287 | 33.6 | 35 |  | 239 |
|  | － | 8.7 |  |  | 189 |  | 析 | 23.7 | 2276 |  | 288 | 33.7 | 5 |  | 253 |
|  | 29.5 | 8.8 | 724 | 13.8 | 1199 | 18.8 | 1720 | 23.8 | 2287 | 28.8 | 2901 | 33.8 | 356 | 38.8 | 4268 |
| 3.9 | 303 | 8.9 | \％33 | 13.9 | 1209 |  |  | 23.9 | 2299 |  | 291 | 33.9 |  |  |  |
|  | 31 |  | \％ | 14.0 | 19 |  | 1742 | 24. | 231 | － 0 | 292． | 34.0 | ， | 39.0 | 97 |
|  | 319 | 9.1 | 7.1 | 14.1 | 9 | 1 | 1753 | 24.1 | 23 | 29.1 | 294 | 4． | 3603 | ， | 312 |
|  | ， | 9.2 | 760 | ． | 1239 | 19.2 | 176 | 24.2 | 2335 | 29.2 | 295 | 34.2 | 361 | 9． | 327 |
|  | 330 | 9.3 | 769 | 14.3 | 1249 | 19.3 | 1775 | 24. | 2347 | 29.3 | 296 | 34.3 | 3630 | ． | 341 |
|  | 344 | 9.4 | 778 | 14.4 | 1259 | 19. | 178 | 24 | 235. | 29.4 | 297 | 34.4 | 364 | 39. | 356 |
| 4.5 | 35. | 9.5 | 787 | 14.5 | 1269 | 19. | 1797 | 24. | 2371 | 29.5 | 991 | 34.5 | 36 | 39. | 4371 |
|  | 36 | 9.6 | 796 | 14.6 | 1279 | 19. | 1808 | 24.6 | 2 | 29.6 | 3004 | 34.6 | 3071 | 9， | 8380 |
|  | 36 | ． | 806 | 14.7 | 1289 | 19. | 1819 | $\because 4.7$ | 2 | 29 | 3017 | 34.8 | 3685 | 9． | 4400 |
| 4.8 | 3 | 9.8 | 815 | 14.8 | 1299 | 19.8 | 1830 |  | 2407 | 29.8 | 3030 |  | 3699 | 39 | 4430 |
| 4.9 | 385 | 9 | 824 | 14.9 | 1309 | 19.9 | 1841 | 24.9 | 2419 | 29.9 | 3043 | 34.9 | 371 | 39 | 4430 |

TABLE NO．XXII．
Side Triangles．
cubic fards in corresponding prisms 100 feet long．
Road－bed 20 feet wide．
Side slopes $\frac{1}{6}$ to 1.

|  | $\begin{aligned} & \text { ex 霞 } \end{aligned}$ |  |  | 部感 |  |  |  |  | $\begin{aligned} & \text { ex } \\ & \text { 品 } \\ & \hline \end{aligned}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 18.5 |  | 20.8 | 10.0 | 23.1 | 15 | 25.5 | 20.0 | 27.8 | 25.0 | 30.1 | 30.0 | 32.4 | 35.0 | 37.7 |
| 0 | 18.6 | 5.1 | 20.9 | 10.1 | 23.2 | 15.1 | 25.5 | 20.1 | 27.8 | 25.1 | 30.1 | 30.1 | 32.5 | 35. | 34.8 |
| 0.2 | 18.6 |  | 20.9 | 10.2 | 23.2 | 15.2 | 25.6 | 20.2 | 27.9 | 25.2 | 30.2 | 30.2 | 32.5 | 35.2 | 348 |
| 0.3 | 18.7 |  | $2 \cdot 1.0$ | 10.3 | 23.3 | 15.3 | 25.6 | 20.3 | 27.9 | 25.3 | 30.2 | 30.3 | 32.5 | 35.3 | 34.9 |
|  | 18.7 | 5.4 | 21 | 10.4 | 23 | 15.4 | 25 | 20.4 | 28.0 | 25． 4 | 30.3 | 30.4 | 32.6 | 35. | 34.9 |
|  | 18.8 |  | 21.1 | 10.5 | 3. | 15.5 | 25.7 | 20.5 | 28.0 | 25.5 | 30.3 | 30.5 | 32.6 | 35.5 | 35.0 |
|  | 18.8 | 5.6 | 621．1 | 10.6 | 23.4 | 15.6 | 25.7 | 20.6 | 28.1 | 25.6 | $31) .4$ | 30.6 | 32.7 | 35.6 | 35.0 |
| 0.1 | 18.8 | 5.7 | 21.2 | 10.7 | 23.5 | 15.7 | 25.8 | 20.7 | 28.1 | 25.7 | 30.4 | 30.7 | 32．7 | 35.7 | 35.0 |
| 0. | 18.9 | 5． | 821.2 | 10.8 | 23.5 | 15.8 | 25.8 | 20.8 | 28.1 | 25.8 | 30.5 | 30.8 | 32.8 | 35. | 35.1 |
| 0.9 | 18.9 | 5.9 | 21.3 | 10.9 | 23.6 | 15.9 | 25.9 | 20.9 | 28.2 | 25.9 | 30.5 | 30.9 | 32.8 | 35.9 | 35.1 |
|  | 19.0 |  |  |  | 23.6 |  | 25． 9 | 21.0 | 28.2 | 26.0 | 30.6 | 31.0 | 32.9 | ． | 35．2 |
|  | 19.0 | 6.1 | 21.3 | 11.1 | 23.7 | 16.1 | 26.0 | 21.1 | 28.3 | 26.1 | 30.6 | 31.1 | 32.9 | 36.1 | 35.2 |
| 1.2 | 19.1 | 6.2 | 21.4 | 11.2 | 23.7 | 16.2 | 26.0 | 21.2 | 28.3 | 26.2 | 30.6 | 31.2 | 33.0 | 36. | 5． 3 |
| 1.3 | 19.1 | 6. | 21.4 | 11.3 | 23.8 | 16.3 | 26.1 | 21.3 | 28. | 26.3 | 30.7 | 31.3 | 33.0 | 36 | 35.3 |
|  | 19.2 | 6 | 21.5 | 11.4 | 23.8 | 16.4 | 26.1 | 21.4 | 28. | 26.4 | 30. | 31.4 | 33.1 | 36 | 35.4 |
| 1.5 | 19 |  | 51 | 11.5 | 23.8 | 16.5 | 26.2 | 21.5 | 28. | 26.5 | 30.8 | 31.5 | 33.1 | 36 | 35.4 |
| 1. | 19.3 |  | 221．6 | 11.6 | 23.9 | 16.6 | 26.2 | 21.6 | 28.5 | 26.6 | 30.8 | 31.6 | 33.1 | 6 | 35.5 |
| 1.1 | 19.3 |  | \％ 21.6 | 11.7 | 23.9 | 16.7 | 26.3 | 21.7 | 28. | 26.7 | 30.9 | 31.7 | 33.2 | 1 | 35.5 |
| 1.8 | 19.4 | 6.8 | 21.7 | 11.8 | 24.0 | 16.8 | 26.3 | 21.8 | 28.6 | 26.8 | 30.9 | 31.8 | 33.2 | 36. | 35.6 |
| 1.9 | 19.4 | 6.9 | 21.7 | 11.9 | 24.0 | 16.9 | 26.3 | 21.9 | 28.7 | 26.9 | 31.0 | 31.9 | 33.3 | 36.9 | 35.6 |
|  | 19 |  |  | 12 | 2 |  | 26.4 |  | 28.7 |  | a | 32.0 |  |  | 35.6 |
|  | 19 | 7 | 21 | 12.1 | 24.1 | ． 1 | 26. | 22.1 | 28 | 27.1 | 31. | 32.1 | 33 |  | 35.7 |
| 2.2 | 19.5 |  | 21.9 | 12.2 | 24.2 | 17.2 | 26. | 22.2 | 28. | 27.2 | 31.1 | 32.2 | 33. | 77. | 35 |
| 3 | 19.6 | 7.3 | 21.9 | 12.3 | 24.2 | 17.3 | 26.5 | 22.3 | 28.8 | 27.3 | 31.2 | 32.3 | 33.5 | 37.3 | 8 |
| 2 | 19.6 | 7.4 | 21.9 | 12.4 | 24.3 | 17.4 | 26.6 | 22.4 | 28.9 | 27.4 | 31.2 | 32.4 | 33.5 | 37. | 35.8 |
|  | 19.7 | 7.5 | 22.0 | 12.5 | 24.3 | 17.5 | 26.6 | 22.5 | 28.9 | 27.5 | 31.3 | 32.5 | 33.6 | 37. | 35.9 |
|  | 19.7 | 7.6 | 22.0 | 12.6 | 24.4 | 17.6 | 26 | 22.6 | 29.0 | 27.6 | 31.3 | 32.6 | 33.6 | 37. | 35.9 |
|  | 19.8 |  | － | 12.7 | 24.4 | 17.7 | 26. | 22.7 | 29.0 | 27.7 | 31 | 32.7 | 33.7 | 37. | 36.0 |
|  | 19.8 | 7.8 | 822.1 | 12.8 | 24.4 | 7.8 | 26.8 | 22.8 | 29.1 |  | 31 | 32.8 | 33.7 |  | 36.0 |
| 9 | 19.9 | 7.9 | 22． 2 | 12.9 | 24.5 | 17.9 | 26.8 | 22.9 | 29.1 | 27 | 31 | 32.9 |  |  | 36.1 |
|  | 19.9 |  | 22.2 | 13.0 | 24.5 | 18.0 | 26.9 | 23.0 | 29.2 | 28 | 31.5 | 33.0 | 33.8 | 0 | 36.1 |
|  | 20.0 | 8.1 | $2 \cdot 3$ | 13.1 | 24.6 | 18.1 | 26.9 | 23.1 | 29. | 28.1 | 31.5 | 33.1 | 33.8 |  | 36.2 |
|  | 20.0 | 8． | 23.3 | 13.2 | 24.6 | 18.2 | 26.9 | 23.2 | 29.3 | 28.2 | 31.6 | 33.2 | 33.9 | 38. | 36.2 |
|  | 20.0 |  | 322.4 | 13.3 | 24.7 | 18.3 | 27.0 | 23.3 | 29.3 | 28.3 | 31.6 | 33.3 | 33.9 | －8．0 | 36.3 |
|  | 20.1 | 8.4 | 22.4 | 13.4 | 24.7 | 18.4 | 27.0 | 23.4 | 29.4 | 284 | 31.7 | 33.4 | 34.0 | 38.4 | 36.3 |
| 3.5 | 30.1 | 8.5 | 52．5 | 13.5 | 24.8 | 18.5 | 27.1 | 23.5 | 29.4 | 28.5 | 31.7 | 33.5 | 34.0 | 38.5 | 36.3 |
| 3.6 | 20.2 | 8.6 | 22.5 | 13.6 | 24.8 | 18.6 | 27.1 | 23.6 | 29.4 | 28.6 | 31.8 | 33.6 | 34.1 | 38.6 | $3{ }^{\text {bi }} 4$ |
|  | 20.2 | 8. | 2 | 13.7 | 24.9 | 18.7 | 27.2 | 23.7 | 29. | 28.7 | 31.8 | 33.7 | 34.1 | 38. | 36.4 |
|  | 20.3 | 8.8 | 22.6 | 13.8 | 24.9 | 18.8 | 27.2 | 23.8 | 29.5 | 28.8 | 31.9 | 33.8 | 34.2 | 38.8 | 36.5 |
| 3.9 | 20.3 | 8.9 | 92. | 13.9 | 25 | 18.9 | 27.3 | 23.9 | 29.6 | 28.9 | 31.9 | 33.9 | 34.2 | 38.9 | 36.5 |
|  | 20.4 | 9．0 | 2． | 14.0 | 25.0 | 19.0 | 27.3 | 24.0 | 29.6 | 29.0 | 31.9 | 34.0 | 34.3 | 99．0 | 36.6 |
|  | 0.4 | 9.1 | 22.7 | 14.1 | 25.0 | 19.1 | 27.4 | 24.1 | 29.7 | 29.1 | 32.0 | 34.1 | 34.3 | 39.1 | 36.6 |
| 4.2 | 0.5 | 9.2 | 22 | 14.2 | 25.1 | 19.2 | 27. | 24.2 | 29. | 29.2 | 32.0 | 34.2 | 34.4 | 39. | 36.7 |
|  | 20.5 | 9.3 | 22．8 | 14.3 | 25.1 | 19.3 | 27.5 | 24.3 | 29.8 | 29. | 32.1 | 34.3 | 34.4 | 39. | 36.7 |
|  | 20.6 | 9.4 | 22.9 | 14.4 | 25.2 | 19.4 | 27.5 | 24.4 | 29.8 | 29.4 | 32.1 | 34.4 | 34.4 | 39.4 | 36.8 |
|  | 20.6 |  | 23.9 | 14.5 | 25.2 | 19.5 | 27.5 | 24.5 | 29.9 | $\because 9.5$ | 32.2 | 34.5 | 34.5 | 39.5 | 36.8 |
|  | 20.6 |  | $6 \geq 3.0$ | 14.6 | 25.3 | 19.6 | 27.6 | 24.6 | 29.9 | 29.6 | 32.2 | 34.6 | 34.5 | 39.6 | 36.9 |
|  | 20.5 |  | 23.0 | 14.7 | 25.3 | 19.7 | 27.6 | 24.7 | 30.0 | 29.7 | 32.3 | 34.7 | 34.6 | 39.7 | 3.6 .9 |
|  | $\therefore 0.7$ | 9.8 | 23.1 | 14.8 | 25 | 19.8 | 27.7 | 24.8 | 30.0 | 29.8 | 32.3 | 34.8 | 34.6 | 39.8 | 36.9 |
| 9 | $\because 0.8$ | 9. | 23.1 | 14.9 | 25.4 | 19.9 | 27.7 | 24.9 | 30.0 | 29.9 | 32.4 | 34.9 | 34.7 | 39.9 | 37.0 |

TABLE NO．XXIII．
Level Cross Sections．
CUBIC YARDS IN CORRESPONDING PRISMS 100 FEET LONG．
Road－bed 28 feet wide．
Side slopes $\frac{1}{4}$ to 1 ．

| $\begin{aligned} & \text { 蕞 } \\ & \text { 喜 } \\ & \text { an } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { 嵒 } \\ & \text { 要 } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { 跑 } \\ & \text { 荡 } \end{aligned}$ |  | $\begin{aligned} & \text { 总 } \\ & \text { 案 } \end{aligned}$ |  | $\begin{aligned} & \stackrel{\rightharpoonup}{u_{0}^{0}} \\ & \stackrel{y y y y}{*} \end{aligned}$ |  | 茹 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 542 | 10 | 1130 | 15 | 1764 | 20.0 | 2444 | 25. | 3171 | 30. | 3944 | 35 | 4764 |
|  | 10 | 5 | 553 | 10.1 | 1142 | 15.1 | 1777 | 20. | 2459 | 25. | 3186 | 30. | 3960 | 35 | 81 |
|  | 21 | 5. | 564 | 10.2 | 1154 | 15.2 | 1790 | 20. | 2473 | 25. | 3201 | 30.2 | 3976 | 35.2 | 4798 |
|  | 31 | 5 | 576 | 10.3 | 1166 | 15.3 | 1803 | 20.3 | 2487 | 25. | 3216 | 30.3 | 399： | 35.3 | 4815 |
|  | 42 | 5.4 | 587 | 10 | 179 | 15 | 817 | 20.4 | 2501 | 25 | 3231 | 30 | 4008 | 35 | 4831 |
|  | 52 | 5.5 | 598 | 10.5 | 1191 | 15.5 | 1830 | 20.5 | 2515 | $2 \overline{2}$. | 3247 | 30. | 4024 | 35 | 4848 |
| 0.6 | 63 | 5.6 | 610 | 10.6 | 1203 | 15.6 | 1843 | 20.6 | 2529 | 25. | 3262 | 30. | 4040 | 35. | 865 |
| 0.7 | 73 | 5. | 621 | 10.7 | 1216 | 15. | 1856 | 20.7 | 2543 | 25 | 3：77 | 30. | 4056 | 35 | 4882 |
| 08 | 84 | 5.8 | 633 | 10.8 | 1228 |  | 1870 | 20.8 | 2558 | 25. | 3292 | 30. | 4072 |  | 4899 |
| 0.9 | 94 | 59 | 644 | 10.9 | 1240 | 15.9 | 1883 | 20.9 | 2572 | 25.9 | 3307 | 30.9 | 4089 | 35 | 4916 |
|  | 1 |  |  |  |  |  | 896 |  | 6 |  | 322 |  | 5 | ． | 3 |
|  | 115 | 6.1 | 667 | 11.1 | 1265 | 16.1 | 1910 | 21.1 | 2600 | 26.1 | 3337 | 31. | 4121 | 36.1 | 50 |
| 1.2 | 126 | 6.2 | 679 | 11.2 | 127． | 16.2 | 19：3 | 21.2 | 2615 | 26.2 | 3353 | 31.2 | 4137 | 36. | 67 |
| 1.3 | 136 | 6.3 | 690 | 11.3 | $1 \geqslant 90$ | 16.8 | 1936 | 21.3 | 2629 | 26. | 33 | 31. | 415 | 36 | 5 |
| 1.4 | 147 | 6. | 0 | 11.4 | 1303 | 16 | 1950 | 21. | 2643 | 26 | 338 | 31. | 4169 | 36. | 02 |
| 1.5 | 158 | 6.5 | 713 | 11 | 15 | 16 | 1963 | 21 | 2658 | 26 | 3398 | 31. | 185 | 8． | 19 |
|  | 168 | 6.6 | 725 |  | 1328 | 16 | 1977 | 21. | 2672 | 26 | 3414 | 31 | 4202 | 36 | 036 |
|  | 179 | 6.7 | 736 | 11 | 40 | 16. | 1990 | 21. | 2686 | 26. | 3429 | 31. | 421 | 36.7 | 53 |
|  | 190 | 6.8 | 74 | 11.8 | 1353 | 16.8 | 2004 | 21.8 | 2701 | 26.8 | 3444 | 31. | 4234 | 36. | 5070 |
| 1.9 | 200 | 6.9 | 760 | 11.9 | 1365 | 16.9 | 2017 | 21.9 | 2715 | 26.9 | 3460 | 31.9 | 4250 | 36. | 5087 |
|  | 211 |  |  |  |  |  | 2031 |  |  |  | 3475 |  |  |  |  |
|  | 22 | 7. | T81 | 12 | 90 | 17 | 2044 | 22 | 27 | 27 | 3490 | 32 | 4283 | 37.1 | 22 |
|  | 233 | 7.2 | 795 | 12 | 03 | 17.2 | 2058 | 22.2 | 759 | 27 | 350 | 32. | 429 | 37.2 | 5139 |
|  | 243 | 7.3 | 06 | 12.3 | 1416 | 17.3 | 2071 | 22.3 | 2775 | 27. | 3521 | 32. | 4316 | 37.3 | 56 |
| 2.4 | 254 | 7.4 | 818 | 12.4 | 1428 | 17.4 | 2085 | 22.4 | 2788 | 27.4 | 3537 | 32. | 4332 | 37 | 74 |
| 2.5 | 265 | 7.5 | 830 | 12.5 | 1441 | 17.5 | 2098 | 22.5 | 2802 | 27.5 | 3552 | 32.5 | 4348 | 37 | 91 |
|  | 276 | 7.6 | 842 | 12.6 |  | 17.6 | 2112 | 22.6 | 2817 | 27.6 | 356 | 32. | 4365 |  |  |
|  | 28 |  |  |  |  |  | 2126 | 22. | 2831 | 27 | 3583 | 32. | 4381 |  | 26 |
|  | 298 | 7. | 872 | 12.8 | 1479 |  | 2139 | 22.8 | 2846 | 27. | 3599 | 32. | 439 |  | 43 |
| 2.9 |  | 7.9 |  | 12.9 | 1492 | 17.9 | 215 | 22.9 | 286 | 27.9 | 3614 | 32. | 44 | 37 |  |
|  | 319 | 8.0 | 889 | 13 |  |  | 2167 | 3. | 2875 | 28 | 3630 | 33.0 | 4431 | 8．0 | 5278 |
|  | 330 | 8.1 | 901 | 13.1 | 1517 | 18. | 2180 | 23.1 | 2890 | 28.1 | 364 | 33. | 444 |  | 95 |
|  | 341 | 8.2 | 913 | 13.2 | 1530 | 18 | 219 | 23.2 | 2904 | 28.2 | 3661 | 33 | 4464 | 88 | 13 |
|  | 3.52 | 8 | 925 | 13.3 | 1543 | 18.3 | 2208 | 2. | 2919 | 28 | 3676 | － | 4480 |  | 30 |
|  | 30 | 8.4 | d | 1 | 1556 | 18 | 2222 | 2.4 | 2934 | 28．4 | 3692 | －3． | 448 | 8. | 48 |
|  | 硅 | 8． |  |  |  |  | 2235 | 23.5 | 2948 | 28.5 | 3708 | 3． | 4513 |  | 65 |
|  | 385 | 8.6 | 960 | 13.6 | 82 | 18.6 | 2249 | 23.6 | 2963 | 28.6 | 3723 | 33. | 4530 | 8. | 383 |
|  | 396 | 8.7 | 972 | 13.7 | 1595 | 18.7 | 2263 | 23.7 | 2978 | 28.7 | 3739 | 33. | 4546 | 38. | 400 |
| ， | 407 | 8.8 | 984 | 13.8 | 1607 | 18.8 | 2277 | 23.8 | 2993 | 28.8 | 3755 | 33. | 456 | 38. | 5418 |
| 3.9 | 419 | 8.9 | 996 | 13.9 | 1620 | 18.9 | 2291 | 23.9 | 3007 | 28.9 | 37 | 33.9 | 458 | 38 |  |
|  | 43 |  |  | 14. |  | 19.0 | 2305 | 20 | 3022 | 2.0 | 3786 | 34.0 | 596 | 39.0 | 5453 |
|  | 441 | 9.1 | 10：0 | 14.1 | 1646 | 19.1 | 2319 | 24.1 | 3037 | 29.1 | 3802 | 34.1 | 4613 | 39.1 | 5470 |
|  | 452 | 9.2 | 1032 | 14.2 | 1659 | 19.2 | 2332 | 24.2 | 3052 | 29.2 | 3818 | 34.2 | 4630 | 39. | 488 |
| 4.3 | 463 | 9.3 | 1045 | 14.3 | 1672 | 19.3 | 2346 | 24.3 | 3067 | 29.3 | 3833 | 34.3 | 4646 | 39 | 506 |
|  | 474 | 9.4 | 1057 | 14. | 1685 | 19. | 2360 | 24.4 | 3082 | 29. | 3849 | 34. | 4663 | 39 | 523 |
|  | 485 | 9 | 1069 | 14.5 | 1698 | 19 | 2374 | 24. | 3097 | 29. | 3865 | 34.5 | 4680 | 39 | 541 |
| 4.6 | 497 | 9.6 | 1081 | 14.6 | 1711 | 19.6 | 2388 | 24.6 | 3111 | 29.6 | 3881 | 34.6 | 4697 | 93． | 5559 |
| 4.7 | 508 | 9.7 | 093 | 14.7 | 1725 | 19.7 | 2402 | 24.7 | 3126 | 29.7 | 3897 | 34.7 | 4713 | 39. | 5576 |
|  | 519 | ． | 1105 | 14.8 | 108 | 19.8 | 2416 | 24.8 | 3141 | 29.8 | 3913 | 34.8 | 4730 | 39 | 5594 |
| 4.9 | 530 | 9.9 | 1117 | 14.9 | 1751 | 19.9 | 2430 | 24.9 | 3156 | 29.9 | 3929 | 34.9 | 4747 | 39.9 | 5612 |

## TABLE NO．XXIV．

## Side Triangles．

CUBIC yards in corresponding prisms 100 feet long．
Road－bed 28 feet wide．
Side slopes $\frac{1}{4}$ to 1.

|  |  |  |  |  |  |  |  | 象我密 | $\begin{aligned} & \text { ex ex fix } \\ & \text { ed } \end{aligned}$ | $\begin{aligned} & \text { bex } \\ & \text { ex } \\ & \text { ex } \end{aligned}$ |  |  | $\begin{aligned} & \text { oing in } \\ & \text { By } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25.9 | 28.2 | 10 | 30.6 | 15.0 | 32.9 | 20.0 | 35.2 | 25 | 37.5 | ． | 39.8 | 35.0 |  |
| 26.0 | $1 \because 8.3$ | 10.1 | 30.6 | 15.1 | 32.9 | 20.1 | 35.2 | 25. | 37. | 30.1 | 39.9 | 35.1 | 42.2 |
| 26.0 | 28.3 | 10.2 | 30.6 | 15.2 | 33.0 | 20.2 | 35.3 | 25 | 37 | 30.2 | 39.9 | 35.2 | 42.2 |
| 326.1 | 28 | 10.3 | 30.7 | 15 | 33.0 | 20.3 | 35 | 25 | 37 | 30.3 | 40.0 | 35 | 42.3 |
| 426.1 | 428.4 | 10.4 | 30.7 | 15.4 | 33. | 20.4 | 35 | 25. | 37. | 30.4 | 40.0 | 35.4 | 3 |
| 526.2 | $5.5 \geqslant 8.5$ | 10.5 | 30.8 | 15.5 | 33.1 | 20.5 | 35. | 25.5 | 37. | 30.5 | 40.0 | 35 | 42.4 |
| 626.2 | 5.628 .5 | 10.6 | 30.8 | 15.6 | 33.1 | 20.6 | 35. | 25.6 | 37. | 30.6 | 40.1 | 35 | 42.4 |
| 0.726 .3 | ．728．6 | 10.7 | 30.9 | 15.7 | 33.2 | 20.7 | 35. | 25. | 37. | 30.7 | 40.1 | 35 | 42 |
| 0.826 .3 | $8,28.6$ | 10.8 | 30.9 | 15.8 | 33.2 | 20.8 | 35. | 25.8 | 37.9 | 30.8 | 40.2 | 35 | 42.5 |
| 0.926 .3 | 928.7 | 10.9 | 31.0 | 15.9 | 33.3 | 20.9 | 35. | 25.9 | 37.9 | 30.9 | 40.2 | 35.9 | 42.5 |
| － |  |  | ． |  |  |  |  |  | 38.0 |  | ． 3 |  |  |
| 26.4 | 6.128. | 11.1 | 31.1 | 16.1 | 33 | 21.1 | 35. | 26.1 | 38.0 | 31.1 | 40.3 | 36.1 |  |
| 26.5 | ． 28. | 11.2 | 31.1 | 16.2 | 33 | 21.2 | 35. | 26.2 | 38. | 31.2 | 40.4 | 36. | 4 |
| 26.5 | 28.8 | 11.3 | 31.2 | 16.3 | 33 | 21.3 | 35. | 26.3 | 38 | 31.3 | 40 | 36 | 42.7 |
| 26 | 28.9 | 11.4 | 31.2 | 16.4 | 33 | 21.4 | 35 | 26.4 | 38 | 31.4 | 40.5 | 36.4 | 42.8 |
| 526 | 528. | 11.5 | 31. | 16.5 |  | 21.5 | 35. | 26. | 38 | 31.5 | 40 | 36.5 | 42 |
| 20 | $6.6 \geq 9.0$ | 11.6 | 31.3 | 16.6 | 33 | 21.6 | 35.9 | 26.6 | 38.2 | 31.6 | 40. | 36.6 | 42.9 |
| 726.7 | 6.729 .0 | 11.7 | 31.3 | 16.7 | 33.7 | 21.7 | 36.0 | 26.7 | 38 | 31.7 | 40. |  | 42.9 |
| $1.8 \sim 6.8$ | 6.829 .1 | 11.8 | 31.4 | 16.8 | 33.7 | 21.8 | 36.0 | 26.8 | 38.3 | 31.8 | 40.6 | ， | 43.0 |
| $1.9 \sim 6.8$ | 6.929 .1 | 11.9 | 31.4 | 16.9 | 33.8 | 21.9 | 36.1 | 26.9 | 38.4 | 31.9 | 40.7 | 36.9 | 43.0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 126.9 | 129 | 12.1 | 31 |  | 33.8 |  | 36.2 | 27.1 |  | 32. | ， |  | 1 |
| $2 \because 6.9$ | 7．229．3 | 12.2 | 31.6 | 17.2 | 33.9 | 22.2 | 36 | 27.2 | 38 | 32.2 | 40.8 |  |  |
| $2.3 \cdot 27.0$ | 7．3 29．3 | 12.3 | 31.6 | 17.3 | 33.9 | 22.3 | 36. | 27.3 | 38.6 | 32.3 | 40.9 | 37.3 | 43.2 |
| 2.427 .0 | $7.4 \geqslant 9.4$ | 12.4 | 31.7 | 17.4 | 34.0 | 22.4 | 36.3 | 27.4 | 38.6 | 32.4 | 40.9 | 7. | 4 |
| 2.527 .1 | 7.529 .4 | 12.5 | 31.7 | 17.5 | 34.0 | 22.5 | 36. | 27.5 |  | 32.5 | 41.0 | 37. | 3 |
| 2.627 .1 | 629 | 12.6 | 31 | 17.6 |  | 22.6 |  |  |  | 32.6 | 41.0 |  | 43.3 |
|  | 7.729 | 12.7 | 31 |  | 34 |  | 36 | 27. |  | 32. |  |  | 43． |
| 2.8 .37 .2 | 7.829 .5 | 12.8 | 31.9 | 17.8 | 34.2 |  | 36 |  | 38.8 | 32.8 | 41 |  | 43.4 |
| 2.927 .3 | 7．9．29．6 | 12.9 | 31.9 | 17.9 | 34.2 | 22 | 36 | 27.9 | 38.8 | 22． |  |  |  |
| 27 |  |  | 31.9 |  |  | 23.0 | 36.6 | 28.0 | 38.9 | 33.0 | 41.2 | 38.0 | 43.5 |
| 3.127 .4 | 29. |  | 33.0 | 18 | 34 | 23.1 | 36.6 | 28.1 | 38.9 | 33.1 | 41.3 |  | 43.6 |
|  | 8.229 .7 | 13.2 | 32.0 | 18 | 34.4 | 23.2 | 36. | 28.2 | 39.0 | 33.2 | 41.3 | 88， | 43.6 |
| － | 8.329 .8 | 13.3 | ， |  | 34.4 | 23.3 |  | 28.3 | 39.0 | 33.3 | 41. |  | 43.7 |
| 42 | 8．429．8 | 13.4 | 32.1 | 18.4 | 34.4 | 23.4 | 36.8 | 28.4 | 39.1 | 33.4 | 41. | 38.4 |  |
| 3.527 .5 | 8.529 .9 | 13.5 | 32.2 | 18.5 | 34.5 | 23.5 | 36.8 | 28.5 | 39.1 | 33.5 | 41. | 38.5 | 43.8 |
| 3.627 .6 | 8.629 .9 | 13.6 | 32.2 | 18.6 | 34.5 | 23.6 | 36.9 | 28.6 | 39.2 | 33.6 | 41.5 | 38.6 | 43.8 |
| 27.6 | 8.730 .0 | 13.7 | 32.3 | 187 | 34.6 | 23.7 | 36.9 | 28.7 | 39.2 | 33.7 | 41.5 | 38.7 | 43.8 |
| 827 | 8.830 .0 | 13.8 | 32.3 | 18.8 | 34.6 | 23.8 | 36.9 | 28.8 | 39.3 | 33.8 | 41.6 | 38.8 | 43.9 |
| 2\％ | 8.930 | 13.9 |  | 18 | 34 | 23.9 | 37 | 28.9 | 39 | 33.9 | 41.6 | 38.9 |  |
| 027.8 | 0.0 30．1 | 14．0 | 3. | 19.0 | 34． | 24.0 | 37.0 | 29.0 | 3.4 | 34.0 | 41.7 | 39.0 | 44.0 |
| ． 127.8 | 9.130 .1 | 14.1 | $3 \because .5$ | 19.1 | 34.8 | 24.1 | 37.1 | $\stackrel{29.1}{ }$ | 39.4 | 34.1 | 41.7 | 39.1 | 44.0 |
| ． 227.9 | 9.230 .2 | 14.2 | 32.5 | 19.2 | 34.8 | 24.2 | 37.1 | 29.2 | 39.4 | 34.2 | 41.8 | 39.2 | 44.1 |
| 3.27 .9 | 9.330 .2 | 14.3 | $3 \because .5$ | 19.3 | 34.9 | 24.3 | 37.2 | 29.3 | 39.5 | 34.3 | 41.8 | 39.3 | 44.1 |
| 4 －8．0 | 9.430 .3 | 14.4 | 32.6 | 19.4 | 34.9 | 24.4 | 37.2 | $\because 9.4$ | 39. | 34.4 | 41.9 | 39.4 | 44.2 |
| － 2.0 | 9.5 e0．3 | 14.5 | 32． 6 | 19.5 | 35.0 | 24.5 | 37.3 | 29.5 | 39.6 | 34.5 | 41.9 | 39.5 | 44.2 |
| ． 628.1 | 9.630 .4 | 14.6 | 32.7 | 19.6 | 35.0 | 24.6 | 37.3 | 29.6 | 39.6 | 34.6 | 41.9 | 39.6 | 44.3 |
| ． 728.1 | 9.730 .4 | 14.7 | 32． 7 | 19.7 | 35.0 | 24.7 | 37.4 | 29.7 | 39. | 34.7 | 42.0 | 39.7 | 44.3 |
| 8.28 .1 928.2 | 9.830 .5 | 14.8 | 32.8 | 19.8 | 35.1 | 24.8 | 37.4 | 29.8 | 39.7 | 34.8 | 42.0 | 39.8 | 44.4 |
| 98．2 | 9.930 .5 | 14.9 | 32． 8 | 19.9 | 35.1 | 24.9 | 37.5 | 29.9 | 39 | 34.9 | 42.1 | 39.9 | 44.4 |

TABLE NO．XXV．

## Level Cross Sections．

CUBIC yards in Corresponding Prisms，$\frac{100}{6}$ FEET LONG．
Road－bed， 10 feet wide．
Side slopes， $1 \frac{1}{2}$ to 1.

|  |  | $\begin{aligned} & \text { 总 } \\ & \text { 采 } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { 药 } \\ & \text { 感 } \end{aligned}$ |  | 要 |  | $\begin{aligned} & \text { 苑 } \\ & \text { Bü } \end{aligned}$ |  |  |  | 萢 | 䔒热 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 |  | 54 | 10.0 | 154 |  | 301 | 20. | 4 | 25 | 33 | 30. | 1019 | 35 | 1350 |
|  | 0.6 | 5 | 56 | 10.1 | 157 | 15.1 | 304 | 20.1 | 498 | 25.1 | 738 | 30. | 025 | 35.1 | 557 |
|  | 1.3 | 5.2 | 57 | 10.2 | 159 | 15.2 | 308 | 20.2 | 503 | 25.2 | 744 | 30.2 | 1031 | 35.2 | 1365 |
|  | 1.9 | 5 | $5!$ | 10 | 162 | 15. | 11 | 20.3 | 507 | 25.3 | 749 | 30.3 | 1037 | 35.3 | 1372 |
|  | 2.6 | 5.4 | 60 | 10.4 | 研 | 15. | 315 | 20.4 | 511 | 25.4 | 754 | 30.4 | 1043 | 35.4 | 1379 |
|  | 3.3 | 5.5 | 62 | 10.5 | （00 | 15. | 318 | 20. | 516 | 25.5 | 759 | 30.5 | 1050 | 35 | 386 |
|  | 4.0 | 5.6 | 64 | 10.6 | 169 | 15.6 | 22 | $\because 0.6$ | 520 | 25.6 | 765 | 30.6 | 056 | 35.6 | 93 |
|  | 4.8 | 5.7 | 65 | 10.7 | 72 | 15.7 | 5 | 20.7 | 25 | 25. | 770 | 30. | 1062 | 35. | 400 |
|  | 5.5 | 5.8 | 67 | 10.8 | 175 | 15.8 | 329 | 20.8 | 529 | 25.8 | 776 | 30.8 | 1068 | 35.8 | 1408 |
| 0.9 | 6.3 | 5.9 | 69 | 10.9 | $17 \%$ | 15.9 | 332 | 20.9 | 533 | 25.9 | 781 | 30.9 | $10 \% 5$ | 35.9 | 1415 |
|  |  |  |  |  |  |  |  |  |  |  |  | 31.0 | 081 |  | 2 |
|  | 8 | 6.1 | 72 | 11.1 |  | 16.1 | 39 | 21.1 | 42 | 26.1 | 92 | 31. | 1088 | 36.1 | 1430 |
|  | 9 | 6.2 | 74 | 11.2 | 8.5 | 16.2 | 43 | 21.2 | 4， | 26.2 | 99 | 31.2 | 1094 | 6. | 437 |
|  | 10 | 6.3 | 76 | 11.3 | 88 | 16.3 | 47 | 21.3 | 52 | 26.3 | 803 | 31.3 | 1100 | 36. | 444 |
|  | 10 | 6.4 | 77 | 11.4 | 191 | 16.4 | 50 | 21.4 | 556 | 26.4 | 808 | 31.4 | 1107 | 36. | 452 |
|  | 11 | 6.5 | 79 | 11 | 193 | 16. | 354 | 21.5 | 61 | 26.5 | 814 | 31. | 111 | 36 | 459 |
|  | 12 | 6.6 | 81 | 11 | 196 | 16. |  | 21.6 | 565 | 26.6 | 819 | 31. | 1120 | 36 | 466 |
|  | 13 | 6.7 | 8.3 | 11.7 | 99 | 16 | 361 | 21. | 570 | 26. | 825 | 31. | 1126 | 36.7 | 1474 |
| 1.8 | 14 | 6.8 | 85 | 11.8 | 2 | 16.8 | 65 | 21.8 | 575 | 26.8 | 830 | 31. | 1133 | 36. | 1481 |
| 1. | 15 | 6.9 | 87 |  | － | 16.9 | 69 | 21.9 | 579 | 26.9 | 836 | 31. | 113 | 36. |  |
|  | 16 |  | 8 |  | 207 |  |  |  | 4 |  | 842 | 32.0 | 1146 | 7． | 96 |
|  | 17 | 7 | 91 | 12.1 | 210 | 17.1 | 376 | 90 |  | 27.1 | 847 | 32. | 115 ？ |  | 1503 |
|  | 18 | 7.2 | 92 | 12.2 | 213 | 17.2 | 380 |  | 93 | 27.2 |  | 32. | 115 | 37.2 | 1511 |
|  | 19 | 7.3 | 94 | 12 | 216 | 17.3 | 384 | 22.3 | 598 | 27.3 | 859 | 32. | 1165 | 37.3 | 518 |
|  | 20 | 7.4 | 96 | 12.4 | 219 | 17.4 | 88 | 22．4 | 603 | 27.4 |  | 32. | 1172 | 37. | 526 |
|  | 21 | 7.5 | 98 | 12.5 | 232 | 17.5 | 392 | 22.5 | 68 | 27.5 | 8 | 32. | 1179 | 37. | 534 |
|  | 22 | 7.6 | 100 | 12.6 | 225 | 17.6 | 395 | 22.6 | 12 | 27.6 | 86 | 32.6 | 1185 | 37. | 541 |
|  | 23 | 7. | 103 | 12.7 |  |  | 399 | 22.7 | 517 | 27.7 | 881 | 32.7 | 1192 | \％ | 549 |
|  | 0 | 7.8 | 104 | 12.8 | 1 |  | 403 | 22．8 | － | 27.8 | 88 | 32.8 | 1199 | 37.8 | 5 |
| 2.9 | 26 | 7.9 | 107 | 12．9 | 1 | 17 | 407 | 22.9 | $62 \%$ | 27.9 | 893 | 32.9 | 120 | 37.9 |  |
|  | 27 | 8.0 | 109 |  | 237 |  | 411 |  |  |  |  | 33.0 | 212 | ． 0 | 572 |
| 3.1 | 2 | 8.1 | 111 | 13.1 | 40 | 18.1 | 415 | 23.1 | 37 | 28.1 | 905 | 33.1 | 1219 | 38.1 | 579 |
| 3.2 | 29 | 8.2 | 113 | 13.2 | 24. | 18.2 | 419 | 23.2 | 642 | 28.2 | 910 | 33.2 | 1226 | 38.2 | 587 |
|  | 30 | 8. | 110 | 13 | 240 | 18.3 | 42 | 23.3 |  | 28.3 | 916 | 33. | 1232 | 38. | $59 . \%$ |
|  | 32 | 8. | 117 |  | 249 |  |  | 23 |  | 28.4 | 922 | 33. | 1239 | 38. | 602 |
|  | 3 | 8.5 | 119 | 13.5 | 252 | 18.5 | 431 |  | ， |  | 928 | 33.5 | 246 | 38.5 | 610） |
|  | 34 | 8.6 | 122 | 13.6 |  | 18 | 硅 |  |  |  | 34 | 33. | 203 | 8.6 | 618 |
|  | 36 | 8.7 | 124 | 13.7 | 2.58 | 18.7 | 439 | 23.7 | 66 |  | 40 | 33. | 260 |  | $6 \because 6$ |
| 3.8 | 37 | 8.8 | 126 | 13.8 | 262 | 18.8 | 443 | 23.8 | 671 | 28.8 | 946 | 33.8 | 1266 | 38.8 | 16：3 |
| 3.9 | 38 | 8.9 | 128 | 13.9 | 265 | 18.9 | 44 | 23.9 | 676 | 38.9 | 952 | 33.8 | 1273 | 38.9 | 1641 |
|  | 40 | 9 | 1 | 14.0 | 268 | 10．0 |  |  |  |  |  | 84．0 | 1280 | 39.0 | 1649 |
|  | 4 | 9.1 | 103 | 14.1 | － | 19．1 | 50 | 24.1 | 687 | 29.1 | 964 | 34.1 | 1287 | 39 | 1657 |
|  | 42 | ． | 135 | 14.2 | 27 | 19.2 | 460 | 24.2 | 2 | 29.2 | \％ | 34.2 | 1294 | 9． | 065 |
| 4.3 | 44 | 9.3 | 137 | 14.3 | 278 | 19.3 | 464 | 24.3 | 697 | 29.3 | 76 | 34.3 | 1301 | 39. | 673 |
|  | 45 | 9.4 | 140 | 14.4 | 281 | 19.4 | 468 | 24.4 | 02 | 29.4 | 982 | 34. | 1308 | 39. | 1681 |
| 4.5 | 47 | 9.5 | 14. | 14.5 | 294 | 19.5 | 47.3 | 24.5 | 807 | 29.5 | 988 | 34.5 | 1315 | 39. | 1689 |
| 4.6 | 48 | 9.6 | 145 | 14.6 | 257 | 19.6 | $4 \pi 7$ | 24.6 | 712 | 29.6 | 994 | 34.6 | 1322 | 39.6 | 1696 |
| 4.7 | 49 | 9.7 | 147 | 14.7 | 291 | 19.7 | 481 | 24.7 | 717 | 29.7 | 1000 | 34.7 | 1329 | 39.7 | 1704 |
| 4.8 | 51 | 9.8 | 14 |  | 294 | 19.8 | 85 |  | 72：3 | 29.8 | 1006 | 34.8 | 1336 | 39.8 | 712 |
| 4.9 | 5 | 9.9 | 15 | 14.9 | 298 | 19.9 | 490 | 24.9 | 728 | 29. | 10 |  | 13 | 39.9 | 1）20 |

## TABLE NO．XXVL．

Side Triangles．
CUBIC Yards LN CORRESPONDING PRISMS $\frac{100}{6}$ FEET LONG．
Road－bed 10 feet wide．
Side slopes $1 \frac{1}{2}$ to 1 ．

|  |  |  |  |  | 誉忽 |  |  |  | $\begin{aligned} & \text { oux ix in } \\ & \text { 譁 } \end{aligned}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1.5 | 5.0 | 3.9 | 10.0 | 2 | 15.0 | 8.5 | 20 | 10.8 | ， | 13.1 | 30.0 | 15.4 | 35.0 | 17.7 |
|  | 1.6 | 5. | 3.9 | 10.1 | ． 2 | 15.1 | ． 5 | 20.1 | 10.8 | 25. | 13.2 | 30. | 15.5 | 35.1 | 17.8 |
|  | 1.6 |  | 4.0 | 10 | 6.3 | 15.2 | 8.6 | 20.2 | 10.9 | ． 2 | 13.2 | 30.2 | 15. | 35.2 | 8 |
|  | 1. |  | 4.0 | 10.3 | ． 3 | 15.3 | 8.6 | 20.3 | 10.9 | 25.3 | 13.3 | 30.3 | 15.6 | 35.3 | 17.9 |
|  | 1.7 |  | 4.0 | 10.4 | 6.4 | 15.4 | 8.7 | 20.4 | 11.0 | 25.4 | 13.3 | 30. | 15.6 | 35． 4 | 17.9 |
|  | 1.8 | 5.5 | 4.1 | 10.5 | 6.4 | 15.5 | 8.7 | 20.5 | 11.0 | 25.5 | 13.3 | 30.5 | 15. | 35. | 18.0 |
|  | 1.8 | 5. | 4.1 | 10.6 | 6.5 | 15.6 | 8.8 | 20.6 | 11.1 | 25.6 | 13.4 | 30.6 | 15.7 | 35 | 18.0 |
|  | 1.9 | 5.7 | 4.2 | 10.7 | 6.5 | 15.7 |  | 20.7 | 11.1 | 25.7 | 13.4 | 30. | 15. | 35. | 18.1 |
|  | 1.9 |  | 4.2 | 10.8 | ． 5 | 15.8 | ． 9 | 20.8 | 11.2 | 25.8 | 13.5 | 30 | 15 | 35.8 | 18.1 |
| 0.9 | 2.0 | 5.9 | 4.3 | 10.9 | 6 | 15.9 | 8.9 | 20.9 | 11.2 | 25.9 | 13.5 | 30. | 15 | 35.9 | 18.2 |
|  |  |  |  |  | ． | 10.0 | ． | 21.0 | 11.3 | 26.0 | 13.6 | 1． | 15.9 |  | 18.2 |
|  | 2.1 | 6.1 | 4.4 | 11.1 | 6.7 | 16.1 | 9.0 | 21.1 | 11. | 26. | 13.6 | 31. | 15.9 | 36 | ． 3 |
| 1.2 | 2.1 | 6.2 | 4.4 | 11.2 | 6.7 | 16.2 | 9.0 | 21.2 | 11. | 26. | 13.7 | 31. | 16. | 36 | ． 3 |
| 1.3 | 2.1 | 6.3 | 4.5 | 11. | 6.8 | 16.3 | 9.1 | 21.3 | 11.4 | 26. | 13.7 | 31. | 16.0 | 36 | 18.3 |
| 1.4 | 2.2 | 6.4 | 4.5 | 11.4 | 6.8 | 16. | 9.1 | 21.4 | 11.5 | 26 | 13.8 | 31 | 16.1 | 36 | 18.4 |
|  | 2.2 | 6. | 6 | 11.5 | 6.9 | 16.5 | ． 2 | 21.5 | 11.5 | 26. | 13.8 | 31. | 16. | 36 | 18.4 |
|  | 2.3 | 6.6 | 4.6 | 11.6 | 6.9 | 16.6 | ． 2 | 21.6 | 11.5 | 26. | 13.9 | 31. | 16. | 0 | 18.5 |
|  | 2.3 | 6.7 | 4.6 | 11.7 | 7.0 | 16.7 | 9.3 | 21.7 | 11.6 | 26. | 13.9 | 31. | 16.2 | 36 | 18.5 |
| 1.8 | 2.4 | 6.8 | 4.7 | 11.8 | 7.0 | 16.8 | 9.3 | 21.8 | 11.6 | 26.8 | 14.0 | 31. | 16.3 | 36. | 18.6 |
| 9 | 2.4 | 6.9 | 4.7 | 11.9 | 7.1 | 16.9 | 9.4 | 21.9 | 11.7 | 26.9 | 14.0 | 31.9 | 16.3 | 36.9 | 18.6 |
|  | 2.5 |  | 4.8 |  | 1 |  | 9.4 |  | 11.7 | 27.0 | 14.0 | 32.6 | 16.4 |  | ． 7 |
| 2.1 | 2.5 | 7.1 | ． 8 | 12 | ． 1 | 7.1 | 5 | 22. | 11.8 | 27.1 | 14.1 | 32.1 | 6. | 37.1 | ． 7 |
| 2.2 | 2.6 | 7. | 4.9 | 12.2 | 7.2 | 17.2 | ． 5 | 22.2 | 11.8 | 27.2 | 14. | 32. | 16. | 31. | 18.8 |
| 2.3 | 2.6 | 7.3 | 4.9 | 12.3 | 7.2 | 17.3 | 9.6 | 22.3 | 11.9 | 27.3 | 14.2 | 32. | 16. | 37. | 18.8 |
|  | 2.7 | 7.4 | 5.0 | 12.4 | 7.3 | 17.4 | 9.6 | 22.4 | 11.9 | 27. | 14. | 32. | 16. | 37 | 18.9 |
|  | 2.7 | － | 5.0 | 12.5 | 7.3 | 17. | 9.6 | 22.5 | 12.0 | 27. | 14. | 32. |  |  |  |
|  |  | 7.6 | 5.1 |  | 7.4 |  | － | 22 | 12.0 | ${ }^{27}$ | 14 |  |  | 37 | 0 |
|  |  |  | 5 | 12.7 | 7.4 |  | 9.7 | 22. | 12.1 | 27 |  |  |  |  | 19.0 |
| 2.8 | 2.8 | 7． | 5.2 | ， | 7.5 | 17.8 | 9.8 | 22.8 | 2.1 | 27.8 |  | 32. | 16.7 |  | 19.0 |
| 2.9 | 2.9 | 7.9 | 5.2 | 12.9 | 5 | 17.5 | 9.8 | 22.9 | 12.1 | 27.8 | 14.5 | 32.9 | 16.8 | 37 | 19.1 |
|  | 2.9 |  | 5.2 |  |  |  | ． 9 | 23. | 12.2 | 28.0 | 14.5 | 33.0 | 16.8 | S | 19.1 |
|  | 3. | 8. | 5.3 | 13. | 7.6 | 18. | ， | 23 | 12. | 28 | 14.6 |  | 16.9 |  | 19.2 |
|  | 3.0 | 8.2 | 5.3 | 13.2 | 7.7 | 18.2 | 10.0 | 23. | 12.3 | 28. | 14.6 |  | 16.9 |  | 19.2 |
|  | 3.1 | 8.3 |  | 13.3 | ． 7 | 18 | 10.0 | 23. | 12.3 | 28. | 14.6 | 3． | 17.0 | d | 19.3 |
|  | 3.1 | 8.4 | ． 4 | 13.4 | 7 | 18. | 10.1 | 23. | 12.4 | 28. | 14. | 33 | 17.0 |  | 19.3 |
|  | 3.2 | 8.5 | 5.5 | 13.5 | 8 | 18.5 | 10.1 | 23.5 | 12.4 | 28. | 14. | 33. | 17.1 | 38. | 19.4 |
|  | 3.2 | 8.6 | 5.5 | 13.6 | 7．8 | 18. | 10.2 | 23.6 | 12.5 | 28. | 14. | 33. | 17.1 | 38 | 19.4 |
|  | 3.3 | 8.7 | 5.6 | 13.7 | 7.9 | 18 | 10.2 | 23. | 12.5 | 28 | 14 | 33. | 17.1 |  | 19.5 |
| 3.8 | 3.3 | 8.8 | 5.6 | 13.8 | 7.9 | 18.8 | 10.2 | 23．8 | 12.6 | 28.8 | 14.9 | 33. | 17. | 38 | 19.5 |
| 3.9 | 3.3 | 8.9 | 5.7 | 13 | 8.0 | 18 | 10 | 23.9 | 12.6 | 28. | 14 | 33. | 17. |  | 19.6 |
|  | 3.4 | 0． | ． 7 | 14. | ， | 19.0 | 10.3 | 4． | 12.7 | 2.0 | 15.0 | 34.0 | 17.0 | 30．0 | 19.6 |
|  | 3.4 | 9.1 | 5.8 | 14.1 | 8.1 | 19.1 | 10.4 | 24.1 | 12.7 | 29.1 | 15.0 | 34. | 17.3 | 39. | 19.6 |
|  | 3.5 | 9.2 | 5.8 | 14.2 | 8.1 | 19.2 | 10.4 | 24.2 | 12.7 | 29.2 | 15.1 | 34.2 | 17.4 | 39. | 19.7 |
|  | 3.5 | 9.3 | 5.8 | 14.3 | 8.2 | 19. | 10.5 | 24.3 | 12.8 | 29. | 15. | 34.3 | 17 | 39 | 19.7 |
|  | 3.6 | 9.4 | 5.9 | 14.4 | ． 2 | 19. | ． 5 | 24. | 12.8 | 29. | 15.2 | 34.4 | 17. | 39 | 19.8 |
|  | 3.6 | 9.5 | 0.9 | 14.5 | ． 3 | 19.5 | 10.6 | 24． | 12.9 | 29. | 15．2 | 34.5 | 17.5 | 39 | 19.8 |
|  | 3.7 | 9.6 | 6.0 | 14.6 | 8.3 | 19.6 | 10.6 | 24.6 | 12.9 | 29. | 15．2 | 34.6 | 17.6 | 39. | 19.9 |
|  | 3.7 | 9.7 | 6.0 | 14.7 | 8.3 | 19.7 | 10.7 | 34.7 | 13.0 | 29. | 15.3 | 34.7 | 17.6 | 39. | 19.9 |
|  | 3.8 | 9.8 | 6.1 | 14.8 | 8.4 | 19.8 | 10.7 | 24.8 | 13.0 | 29.8 | 15.3 | 34.8 | 17.7 | 39.8 | 20.0 |
| 4.9 | 3.8 | 9.9 | 6.1 | 14.9 | 8.4 | 19.9 | 10.8 | 24.9 | 13.1 | 29.9 | 15.4 | 34.9 | 17.7 | 39.9 | 20.0 |

TABLE NO．XXVII．
Level Cross Sections．
CUBIC yards in corresponding Prisms，$\frac{100}{6}$ feet lowg．
Road－bed 12 feet wide．

|  |  | $\begin{aligned} & \text { 范 } \\ & \text { 蕆 } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { 葆 } \\ & \text { 密 } \end{aligned}$ |  |  | $\begin{aligned} & \text { oini ix } \\ & \text { Bid } \end{aligned}$ | $\begin{aligned} & \text { 薄 } \\ & \text { 范 } \end{aligned}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 | 0.0 |  | 52 |  | 36 | 15.0 | 250 | 20.0 | 395 | 25.0 | 571 | 30.0 | 778 | 35.0 | 1015 |
|  | 0.7 | 5. | 54 | 10.1 | 138 | 15.1 | 253 | 20.1 | 398 | 25.1 | 575 | 30.1 | 782 | 3 5． 1 | 1021 |
| 0 | 1.5 | 5.2 | 55 | 10.2 | 140 | 15.2 | 255 | 20.2 | 402 | 25.2 | 579 | 30.2 | 787 | 35.2 | 1026 |
| 0 | 2.3 | 5.3 | 57 | 10.3 | 142 | 15.3 | 258 | 20.3 | 405 | 25.3 | 583 | 30.3 | 791 | 35.3 | 31 |
|  | 3.1 | 5.4 | 58 | 10.4 | 144 | 15.4 | 60 | 20.4 | 408 | 25.4 | 586 | 30.4 | 796 | 35. | 1036 |
|  | 4.0 | 5.5 | 59 | 10.5 | 46 | 15.5 | 63 | 20.5 | 411 | 25.5 | 590 | 30.5 | 800 | 35.5 | 1041 |
|  | 4.7 | 5.6 | 61 | 10.6 |  | 15.6 | 266 | 20.6 | 415 | 25.6 | 594 | 30.6 | 805 | 35.6 | 046 |
|  | 5.5 | 5.7 | 62 | 10.7 | 150 | 15.7 | 268 | 20.7 | 418 | 25.7 | 598 | 30.7 | 309 | 35.7 | 051 |
| 0.8 | 6.3 | 5. | 64 | 10.8 | 152 | 15.8 | 271 | 20.8 | 421 | 25.8 | 602 | 30.8 | 814 | 35.8 | 1056 |
| 0.9 | 7.2 | 5.9 | $6 \overline{5}$ | 10.9 | 154 | 15.9 | 274 | 20.9 | 424 | 25.9 | 606 | 30.9 | 818 | 25.9 | 1061 |
|  |  | 6. | 67 | 11.0 | 156 | 16 | 277 | 1 | 8 | 26 | 10 | 31.0 | 23 | 36.0 | 67 |
|  | 9 | 6.1 | 68 | 11.1 | 158 | 16.1 | 279 | 21.1 | 431 | 26.1 | 614 | 31.1 | $8: 7$ | 36.1 | 1072 |
| 1.2 | 10 | 6.2 | 70 | 11.2 | 160 | 16.2 | 82 | 21.2 | 434 | 26.2 | 618 | 31.2 | 832 | 36.2 | 1077 |
| 1.3 | 11 | 6.3 | 71 | 11.3 | 163 | 16.3 | 285 | 21.3 | 438 | 26.3 | 622 | 31.3 | 837 | 36.3 | 082 |
| 1. | 12 | 6.4 | 73 | 11.4 | 165 | 16.4 | 288 | 21.4 | 441 | 26.4 | 6：6 | 31.4 | 841 | 36. | 1088 |
| 1. | 13 | 6.5 | 74 | 11.5 | 167 | 16.5 | 290 | 21.5 | 445 | 26.5 | 630 | 31.5 | 846 | 36. | 1093 |
| 1. | 13 | 6.6 | 76 | 11.6 | 169 | 16.6 | 293 | 21.6 | 448 | 26.6 | 634 | 31.6 | 850 | 36. | 1098 |
| 1.7 | 14 | 6.7 | 77 | 11.7 | 171 | 16.7 | 96 | 21.7 | 451 | 26.7 | 638 | 31.7 | 855 | 36. | 1103 |
| 1.8 | 15 | 6.8 | 79 | 11.8 | 173 | 16.8 | 299 | 21.8 | 455 | 26.8 | 642 | 31.8 | 860 | 36. | 1109 |
| 1.9 | 16 | 6.9 | 81 | 11.9 | 176 | 16.9 | 0 | 21.9 | 458 | 26. | 646 | 31. | 864 | 36.9 | 1114 |
|  | 17 | 7.0 | 82 | 12.0 | 㤑 | 17.0 | ， | 22.0 | 62 | 27.0 | 50 | 32.0 | 69 | 37.0 | 119 |
|  | 18 | 7.1 | 84 | 12.1 | 180 | 17.1 | 07 | 22.1 | 465 | 27.1 | 654 | 32.1 | 874 | 37.1 | 1124 |
|  | 19 | 7.2 | 85 | 12.2 | 18. | 17.2 | 310 | 22.2 | 469 | 27.2 | 658 | 32.2 | 879 | 37.2 | 1130 |
| 2.3 | 20 | 7.3 | 87 | 12.3 | 185 | 17.3 | 313 | 22.3 | 432 | 27.3 | 662 | 32.3 | 883 | 37.3 | 1135 |
|  | 21 | 7.4 | 89 | 12.4 | 87 | 17.4 | 316 | 23.4 | 476 | 27. | 666 | 32.4 | 888 | 37.4 | 1140 |
| 2.5 | 23 | 7.5 | 90 | 12.5 | 189 | 17.5 | 319 | 22.5 | 479 | 27.5 | 671 | 32.5 | 893 | 37.5 | 1146 |
| 2.6 | 23 | 7.6 | 92 | 12.6 | 191 | 17.6 | 322 | 23． 6 | 483 | 27.6 | 675 | 32.6 | 898 | 37.6 | 1151 |
| 2.7 | 25 | 7.7 | 94 | 12.7 | 194 | 17.7 | 325 | 22.7 | 486 | 27.7 | 679 | 32.7 | 902 | 37. | 1157 |
| 2.8 | 26 | 7.8 | 95 | 12.8 | 196 | 17.8 | 327 | 22.8 | 490 | 27.8 | 683 | 32.8 | 907 | 37.8 | 1162 |
| 2.9 | 27 | 7.9 | 9 9 | 12.9 | 198 | 17.9 | 330 | 22.9 | 493 | 27.9 | 687 | 32.9 | 912 | 37.9 | 1167 |
|  | 28 | 8.0 | 99 | 13.0 | 1 | 18.0 |  | 2．0 | 97 |  | 91 | 33.0 | 17 | 0 | 1173 |
|  | 29 | 8.1 | 101 | 13.1 | 203 | 18.1 | 36 | 23.1 | 01 | 28. | 696 | 33.1 | 921 | 38.1 | 1178 |
| 3.2 | 30 | 8.2 | 102 | 13.2 | 205 | 18.2 | 339 | 23.2 | 504 | 28.2 | 700 | 33.2 | 926 | 38.2 | 1184 |
| 3.3 | 31 | 8.3 | 104 | 13.3 | 208 | 18.3 | ＋2 | 23.3 | 508 | 28.3 | 704 | 33.3 | 931 | 38.3 | 1189 |
|  | 32 | 8.4 | 106 | 13.4 | 210 | 18.4 | 345 | 23.4 | 51 | 28.4 | 708 | 33.4 | 9：36 | 38.4 | 1195 |
|  | 3 | 8.5 | 108 | 13.0 | 13 | 18.5 | 348 | 23.5 | 515 | 28.5 | 713 | 33.5 | 941 | 38.5 | 1200 |
|  | 35 | 8.6 | 109 | 13.6 | 215 | 18.6 | 351 | 23.6 | 19 | 28.6 | 717 | 33.6 | 946 | 38.6 | 1206 |
|  | 36 | 8.7 | 111 | 13.7 | 217 | 18.7 |  | 23.7 |  | －28．7 | 721 | 33.7 | 9.51 | 38.7 | 1211 |
| 3.8 | 37 | 8.8 | 113 | 13.8 | 220 | 18.8 | 35. | 23.8 | 52 | 28.8 | 725 | 33.8 | 956 | 38.8 | 1217 |
| 3.9 | 38 | 8.9 | 115 | 13.9 | 222 | 18.9 | 361 | 23.9 | 530 | 28.9 | 730 | 33.9 | 961 | 38.9 | 122\％ |
| 4.0 | 40 | 9.0 | 117 | 14.0 | 2 | 19.0 | 64 | 24.0 | 533 | 29.0 | 734 | 34.0 | 965 | 39.0 | 1228 |
| 4.1 | 41 | 9.1 | 119 | 14.1 | 22. | 19.1 | 36 亿 | 24.1 | 537 | 29.1 | 738 | 34.1 | 9 9\％） | 39.1 | 1233 |
| 4.2 | 42 | 9.2 | 121） | 14.2 | 230 | 19.2 | 5． | 24.2 | 541 | 29.2 | 743 | 34.2 | 97.5 | 39.2 | 1239 |
| 4.3 | 43 | 9.3 | 122 | 14.3 | 232 | 19.3 | 373 | 24.3 | 545 | 29.3 | 747 | 34.3 | 980 | 39.3 | 1245 |
| 4.4 | 45 | 9.4 | 124 | 14.4 | 235 | 19.4 | 376 | 24.4 | 548 | 29.4 | 751 | 34.4 | 98.5 | 39.4 | 1250 |
| 4.5 | 46 | 9.5 | 126 | 14.5 | 237 | 19.5 | 379 | 24.5 | 552 | 29.5 | 756 | 34.5 | 490 | ：99．5 | 1256 |
|  | 47 | 9.6 | 12S | 14.6 | 240 | 19.6 | 382 | 24.6 | 556 | 29.6 | 760 | 34.6 | 995 | ：39．6 | 1261 |
|  | 48 | 9.7 | 130 | 14.7 | 242 | 19.7 | 385 | 24.7 | 560 | 29.7 | 765 | 34.7 | 1000 | 39.7 | 1267 |
| 1 | 50 | 9.8 | 132 | 14.8 | 45 | 19.8 | 389 | 24.8 | 563 | 29.8 | 769 | 34.8 | 1005 | 39.8 | 1273 |
| 1 | 5 | 9. | 134 | 14.9 | 247 | 19.9 | 392 | 24.9 | 56 | 29.9 | 773 | 34.9 | 1010 | 39.9 | 1278 |

## TABLE NO．XXVIII．

Side Triangles．
CUBIC yards in Corresponding prisms， 100 feet long．
Road－ved 12 feet wide．
Side slopes 1 to 1.

|  | $\begin{aligned} & \text { 으를 } \\ & \text { 陪 } \end{aligned}$ |  |  |  |  |  | ouxin | 害害感 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1.9 |  |  |  | ， |  | ． | 20.0 | 8.0 | 25.0 | 9.6 | 30.0 | 11.1 | 35.0 |  |
|  | 1.9 | 5. | 3.4 | 10.1 | 5.0 | 15.1 | 6.5 | 20.1 | 8 | 25. | 9.6 | 30. | 11.1 | 35. | 12.7 |
| 0.2 | 1.9 | 5.2 | 3.5 | 10.2 | 5.0 | 15．2 | 6.5 | 20.2 | 8 | 25. | 9.6 | 30.2 | 11.2 | 35 | 12.7 |
| 0.3 | 1.9 | 5.3 | 3.5 | 10.3 | 5.0 | 15.3 | 6.6 | 20.3 | 8.1 | 25.3 | 9.7 | 30.3 | 11.2 | 35.3 | 12.7 |
| 0.4 | 2.0 | 5.4 | 3． 5 | 10.4 | 5 | 15 | ． 6 | 20.4 | 8.1 | 25.4 | 9.7 | 30.4 | 11.2 | 35.4 | 12.8 |
| 0.5 | 2.0 | 5.5 | ， | 10.5 | 5.1 | 15.5 | ． 6 | ${ }^{2} 0.5$ | 8.2 | 25.5 | 9.7 | 30.5 | 11.3 | 35.5 | 12.8 |
|  | 2.0 | 5.6 | 3.6 | 10.6 | 5.1 | 15.6 | 6.7 | 20.6 | 8.2 | 25.6 | 9.8 | 30.6 | 11.3 | 35.6 | 12.8 |
| 0.7 | 2.1 | 5.7 | 3.6 | 10.7 | 5.2 | 15.7 | 6.7 | 20.7 | 8.2 | 25.7 | 9.8 | 30.7 | 11.3 | 35. | 12 |
| 0.8 | 2.1 | 5. | 3.6 | 10.8 | 5.2 | 15.8 | 6.7 | 20.8 | 8.3 | 25.8 | 9. | 30.8 | 11.4 | 35. | 12.9 |
| 0.9 | 2.1 | 5.9 | 3.7 | 10.9 | 5.2 | 15.9 | 6.8 | 20.9 | 8.3 | 25.9 | 9.8 | 30.9 | 11.4 | 35.9 | 12.3 |
|  |  |  |  |  |  |  | 6.8 |  | ． 3 |  | ． 9 |  | 11.4 |  | 13.0 |
|  | 2.2 | 6.1 | 3.7 | 11.1 | ． 3 | 16.1 | 6.8 | 21.1 | 8.4 | 26.1 | 9.9 | 31.1 | 11.5 | 36.1 | 13.0 |
| 1.2 | 2.2 | 6.2 | 3.8 | 11.2 | 5.3 | 16.2 | 6.9 | 21.2 | 8.4 | 26.2 | 9.9 | 31.2 | 11.5 | 36.2 | 13.0 |
| 3 | 2.3 | 6.3 | 3.8 | 11.3 | 5.3 | 16.3 | 6.9 | 21.3 | 8.4 | 26.3 | 10.0 | 31.3 | 11.5 | 36. | 13.1 |
| 1.4 | 2.3 | 6.4 | 3.8 | 11.4 | ． 4 | 16.4 | 6.9 | 21.4 | 8.5 | 26. | 10.0 | 31. | 11.5 | 36 | 13.1 |
| 1.5 | 2.3 | 6.5 | 3.9 | 11.5 | 5.4 | 16.5 | 6.9 | 21.5 | 8.5 | 26.5 | 10.0 | 31.5 | 11.6 | 36.5 | 13.1 |
| 1.6 | 2.3 | 6.6 | 9 | 11.6 | 5.4 | 16.6 | 7.0 | 21.6 | 8.5 | 26.6 | 10.1 | 31.6 | 11.6 | 36 | 13.1 |
|  | 2.4 | 6.7 | 3.9 | 11 | 5.5 | 16.7 | 7.0 | 21.7 | 8.5 | 26.7 | 10.1 | 31.7 | 11.6 | 36. | 13. |
| 1.8 | 2.4 | 6.8 | 4.0 | 11.8 | 5.5 | 16.8 | 7.0 | 21.8 | 8.6 | 26.8 | 10.1 | 31.8 | 11.7 | 36.8 | 13.2 |
| 1.9 | 2.4 | 6.9 | 4.0 | 11.9 | 5.5 | 16.9 | 7.1 | 21.9 | 8.6 | 26.9 | 10.2 | 31.9 | 11.7 | 36.9 | 13.2 |
|  |  | ． | 4.0 |  | 5.6 |  |  |  | 8.6 | 27.0 | 10.2 | 32.0 | 11 |  | 13.3 |
|  | 2． | 7. | 4.0 | 12.1 | 6 | 17.1 | 7.1 | 22.1 | 8.7 | 27.1 | 10.2 | 32.1 | 11 | 37.1 | 13.3 |
| 2.2 | 2.5 | 7.2 | 4.1 | 12.2 | 5.6 | 17.2 | 7.2 | 22． 2 | 8.7 | 27.2 | 10.2 | 32.2 | 11 | 37.2 | 13.3 |
| 2.3 | 2.6 | 7.3 | 4.1 | 12 | 5.6 | ． 3 | 7.2 | 22.3 | 8.7 | 27.3 | 10.3 | 32. | 11.8 | 37.3 | 13 |
| 2.4 | 2.6 | 7.4 | 4.1 | 12.4 | 5.7 | 17.4 | 7.2 | 22.4 | 8.8 | 27.4 | 10.3 | 32.4 | 11.9 | 37. | 13. |
| 2.5 | 2.6 | 7.5 | 4.2 | 12.5 | 5.7 | 17.5 | 7.3 | 22.5 | 8.8 | 27.5 | 10.3 | 32.5 | 11.9 | 37.5 | 13 |
|  | 2.7 | 7. | 4.2 | 12.6 | 5.7 | 17.6 | 7.3 | 22.6 | 8.8 | 27. | 10.4 | 32. | 11.9 | 37 | 13 |
|  | 2. | 7.7 | 4.2 | 12.7 | 5.8 | 17.7 | 7.3 | 22.7 | 8.9 | 27.7 | 10.4 | 32. | 11.9 |  | 13. |
|  | 2． | 7．8 | 4.3 | 12.8 | ． 8 | 17.8 | ． 3 | 22.8 | 8.9 | 27.8 | 10.4 | 32. | 12.0 | 3． | 13.5 |
| 2.9 | 2.7 | 7.9 | 4.3 | 12.9 | 5.8 | 17.9 | 7.4 | 22.9 | 8.9 | 27.9 | 10.5 | 32. | 12.0 | 37. | 13 |
|  | 2.8 | 8.0 | 4.3 | ． | ． 9 |  | ． 4 | 23.0 | 9.0 | 28 | 10.5 | 3.0 | 12.0 |  | 13.6 |
| 3.1 | 2.8 | 8.1 | 4.4 | 13.1 | 5.9 | 18.1 | 7.4 | 23.1 | 9.0 | 28.1 | 10.5 | 33.1 | 12.1 |  | 13.6 |
|  | 2.8 | 8.2 | 4.4 | 13.2 | 5.9 | 18.2 | 7.5 | 23. | 9.0 | 28. | 10.6 | 33. | 12.1 | 8． | 13.6 |
|  | 2.9 | 8.3 | 2.4 | 13.3 | 6.0 | 18.3 | 7.5 | 23.3 | 9.0 | 28. | 10.6 | 33. | 12.1 | 38.3 | 13.7 |
|  | 2.9 | 8. | 4.4 | 13.4 | ． | 18.4 | 7.5 | 23.4 | 9.1 | 28.4 | 10.6 | 33.4 | 12.2 | 38.4 | 13.7 |
|  | 2.9 | 8.5 | 5 |  | 6．0 | 18.5 | 7.6 | 23.5 | 9.1 | 28.5 | 10.6 | 33.5 | 12.2 | 38.5 | 13.7 |
| 3.6 | 3.0 | 8.6 | 4.5 | 13.6 | 6.0 | 18.6 | 7.6 | 23.6 | 9.1 | 28.6 | 10.7 | 33.6 | 12.2 | 38.6 | 13.8 |
| 3.7 | 3.0 | 8.7 | 4.5 | 13.7 | 6.1 | 18.7 | 7.6 | 23.7 | 9.2 | 28.7 | 10.7 | 33.7 | 12.3 | 38. | 13.8 |
| 3.8 | 3.0 | 8.8 | 4.6 | 13.8 | 6.1 | 18.8 | 7.7 | 23.8 | 9.2 | 28.8 | 10.7 | 33.8 | 12.3 | 38.8 | 13.8 |
| 3.9 | 3.1 | 8.9 | 4.6 | 13.9 | 6.1 | 18.9 | 7.7 | 23.9 | 9.2 | 28.9 | 10.8 | 33.9 | 12.3 | －8 | 13.9 |
|  | 3. | 9.0 | 4.6 | 14.0 | ． 2 | 19.0 |  | 24.0 | 9.3 | 29.0 | 10.8 | 34.0 | 12.3 | 39.0 | 13.9 |
|  | 3.1 | 9.1 | 4.7 | 14.1 | 6.2 | 19.1 | 7.7 | 24.1 | 9.3 | 29.1 | 10.8 | 34.1 | 12.4 | 39.1 | 13.9 |
| 4.2 | 3.1 | 9.2 | 4.7 | 14.2 | 6.2 | 19.2 | 7.8 | 24.2 | 9.3 | 29.2 | 10.9 | 34.2 | 124 | 39.2 | 14.0 |
| 4.3 | 3.2 | 9.3 | 4.7 | 14.3 | 6.3 | 19.3 | 7.8 | 24.3 | 9.4 | 29.3 | 10.9 | 34.3 | 12.4 | 39.3 | 14.0 |
| 4.4 | 3.2 | 9. | 4.8 | 14.4 | 6.3 | 19.4 | 7.8 | 24.4 | 9.4 | 29.4 | 10.9 | 34.4 | 12.5 | 39.4 | 14.0 |
| ． 5 | 3. | 9 | 4.8 | 14.5 | 6.3 | 19.5 | 7.9 | 24.5 | 9.4 | 29.5 | 11.0 | 34.5 | 12.5 | 39.5 | 14.0 |
| ． 6 | 3.3 | 9.6 | 4.8 | 14.6 | ． 4 | 19.6 | 7.9 | 24.6 | 9.4 | 29.6 | 11.0 | 34.6 | 12.5 | 39.6 | 14.1 |
| 4.8 | 3.3 | 9.7 | 4.8 | 14.7 | 6.4 | 19.7 | 7.9 | 24.7 | 9.5 | 29.7 | 11.0 | 34.7 | 12.6 | 39.7 | 14.1 |
| 4.8 | 3.3 | 9.8 | 4.9 | 14.8 | 6.4 | 19.8 | 8.0 | 24.8 | 9.5 | 29.8 | 11.0 | 34.8 | 12.6 | 39.8 | 14.1 |
| ， | 3.4 | 9.9 | 4.9 | 14.9 | 6． | 19.9 | 8.0 | 24.9 | 9.5 | 29.9 | 11． | 34.9 | 12. | 39.9 | 14.2 |

## TABLE NO．XXIX．

## Level Cross Sections．

CUBIC YARDS IN CORRESPONDING PRISMS 100 FEET LONG．

Road－bed 14 feet wide．

|  |  |  |  |  |  |  |  | 芭 |  | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 | 0．0 | 5.0 | 66.4 | 10.0 | 79.0 | 15.0 | 338.0 | 20.0 | 543.2 | 25.0 |
| 0.1 | 0.9 | 5.1 | 68．2 | 10.1 | 181.7 | 15.1 | 341.6 | 20. | 547.8 | 25.1 |
| 0.2 | 1.8 | 5.2 | 70.0 | 10.2 | 184.5 | 15.2 | 345.3 | 20.2 | 552． 4 | 25.2 |
| 0.3 | 2.7 | 5.3 | 71.8 | 10.3 | 187.2 | 15.3 | 349.0 | 20.3 | 557.0 | 25.3 |
| 0.4 | 3.6 | 5.4 | 73.7 | 10.4 | 190.0 | 15. | 352.7 | 20.4 | 561.6 | 25.4 |
| 0.5 | 4.6 | 5.5 | 75.5 | 10.5 | 192.8 | 15.5 | 356.4 | 20.5 | 566.3 | 25.5 |
| 0.6 | 5.5 | 5.6 | 77.4 | 10.6 | 19.5 .6 | 15.6 | 360.1 | 20.6 | 571.0 | 25.6 |
| 0.7 | 6.5 | 5.7 | 79.3 | 10.7 | 198.5 | 15.7 | 363.9 | 20.7 | 575.6 | 25.7 |
| 0.8 | 7.5 | 5.8 | 81.2 | 10.8 | 201.3 | 15.8 | 367.7 | 20. | 580.3 | 25． |
| 0.9 | 8.5 | ． 9 | 83.2 | 10.9 | $\because 04.2$ | 15.9 | 37 | 20 | － | 25.9 |


$\begin{array}{lllll}1.0 & 9.6 & 6.0 & 85\end{array}$ 1.110 .66 .1887 $1.211 .76 .2 \quad 89.2$ $1.312 .86 .3 \quad 91.2$ | 1.4 | 13.9 | 6.4 | 93.2 |
| :--- | :--- | :--- | :--- | $\begin{array}{llll}1.5 & 15.0 & 6.5 & 95.3\end{array}$ $\begin{array}{llll}1.6 & 16.2 & 6.6 & 97.4\end{array}$ $1.7|17.46 .7| 99.5$ $1.813 .6 \quad 0.8101 .6$ $1.919 .8 \quad 6.9103 .7$ 2.021 .07 .0105 .9 $2.122 .2{ }^{7} .1108 .0$ $2.223 .5 \quad 7.2110 .2$ $2.324 .8 \quad 7.3112 .4$ 2.426 .178 .4114 .7 2.527 .47 .5116 .9 $2.628 .7 \quad 7.6119 .2$ 2.730 .17 .7121 .4 2.831 .57 .8123 .7 2.932 .87 .9126 .1

3.034 .38 .0128 .4 $3.135 .78 .1 \quad 130.8$ 3.237 .1 ४．こ 133.1 3.338 .68 .3135 .5 3.440 .1 ४． 4137.9 $\begin{array}{llllll}3.5 & 41.6 & 8.5 & 140.4\end{array}$ 3.643 .1 8．6 142.8 $3.7 \mid 44.78 .714 .5 .3$ 3.846 .28 .8147 .8 3.947 .88 .9150 .3 $4.049 .4 \quad 9.0152 .8$ 4.151 .09 .115 5． 3 4.252 .6 9．2 157.9 $4.354 .3 \quad 9.3160 .5$ 4.456 .094163 .0 $4.557 .6 \quad 9.5165 .7$ $4.659: 3 \quad 9.6168 .3$ $4.761 .1 \quad 9.71709$ 4.862 .89 .8173 .6 4.964 .69 .9176 .3
$12.0237 .0 \quad 17.0414 .5$

$$
\begin{array}{l|l|l|l|}
12.1 & 240.1 & 17.1 & 418.5
\end{array}
$$

$$
12.2243 .2 \text { 17.2422.6 }
$$

$$
\begin{array}{l|l|l|l|}
12.3 & 246.4 & 17.3 & 426.6
\end{array}
$$

$12.4249 .5 \quad 17.4430 .7$
 $\begin{array}{llllll}12.6 & 2 \text { ปั．} 9 & 17.6 & 438.9\end{array}$ $12.7 \mid 259.117 .7443 .0$
 12.9265 .6 13.0268 .8 13.1272 .1 13.2275 .4 13.3278 .7 18.3468. 282． 18.4472. 13.5 28．5． 418.5476 .8


 $13.9299 .0 \quad 18.9494 .1$ $\begin{array}{lllllllll}14.0 & 302.5 & 19.0 & 498.5 & 24.0 & 740.7\end{array}$ 14.1305 .919 .1 502．8 14.2309 .419 .2507 .8
 $14.4316 .4 \quad 19.4516 .1$ 14.5320 .0 14.6323 .5 14.7327 .1 $14.9334 .3 \mid 19.9538 .7$ Side slopes $1 \frac{1}{2}$ to 1 ．

 $\begin{array}{lllllllll}794.8 & 30.0 & 1092.6 & 35 & 0 & 1436.7\end{array}$
 $\begin{array}{llllll}805.8 & 30.2 & 1105.5 & 35.2 & 1451.5\end{array}$







$850.6|31.0 \quad 1157.7| 36.0 \mid 1511.1$
 $862.0|31.2| 171.0 \mid 36.21526 .2$ $867.7 \mid 31.31177 .6 ~ 36.31533 .8$ $873.5 \quad 31.41184 .3 \quad 36.41541 .4$ $879.2 \quad 31.5 \quad 1191.0 \quad 36.51549 .0$ $885.0 \quad 31.61197 .7 \quad 36.61556 .6$

 902.5 31．9 1217.9 36．9 1579.6
908.3 32．0 1224.7 37．0 1587.3 914.2 32．1 $1231.5 \quad 37.11595 .1$

 931.9 32． $41252.0 \quad 37.41618 .4$ 937.9 32．5 1258.9 37．5 $1626 .{ }^{〔}$
 949.8 32．7 12 22．7 37.71641 .8
 961.9 32．9 1286.6 37．9 1657.5
 974.0 З3． $1 \quad 1300.5 \mid 38.11673 .3$











 | 24.2 | 751.4 | 29.2 | 1041.8 | 34.2 | 1378.6 | 39.2 | 1761.6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

 $24.4762 .1|29.410 .54 .4| 34.41393 .0 \mid 39.41777 .9$






TABLE NO. XXX.
Side Triangles.
cubic yards in corresponding prisms $\frac{100}{6}$ feet long.

Road-bed 14 feet wide.
Side slopes $1 \frac{1}{2}$ to 1 .

## TABLE NO．XXXI．

Level Cross Sections．

## CUBIC yards in Corresponding prisms，$\frac{100}{6}$ feet long．

Road－bed 16 feet wide．

|  |  |  |  |  | 을르률 |  |  |  |  | $\begin{aligned} & \text { 岕 } \\ & \text { 㳦 } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { 淢 } \\ & \stackrel{y y y y}{*} \end{aligned}$ | 으률 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0.0 | 5.0 | 64.8 | 10.0 | 160.5 | 15.0 | 287.0 | 20.0 | 444.4 | 25.0 | 632.7 | 30.0 | 851.9 | 35.0 | 1101.9 |
| 0.1 | 1.0 | 5． 1 | 66.4 | 10.1 | 162．7 | 15.1 | 289.9 | 20.1 | 447.9 | 25.1 | 636.8 | 30.1 | 855.5 | 35． 1 | 1107.2 |
| 0.2 | 2.0 | 5．2 | 68.0 | 10.2 | 165.0 | 15.2 | 292.7 | 20.2 | 4 51．4 | 25.2 | 640.9 | 30.2 | 861.3 | 35.2 | 1112.5 |
| 0.3 | 3.0 | 5.3 | 69.7 | 10.3 | 167.2 | 15.3 | 295.6 | 20.3 | 454.9 | 25.3 | 645.11 | 30.3 | 866.0 | 35.3 | 1117.8 |
| 0.4 | 4.0 | 5.4 | 71.3 | 10.4 | 169.5 | 15.4 | 298.5 | 20.4 | 458.4 | 25.4 | 649.1 | 30.4 | 870.7 | 35.4 | 1123.2 |
| 0.5 | 5.1 | J． 5 | 73.0 | 10.5 | 171.8 | 15.5 | 301.4 | 20.5 | 461.9 | 25.5 | 653．2 | 30.5 | 875.5 | 3 3 .5 | 1128.5 |
| 0.6 | 6. | 5.6 | 74.7 | 10.6 | 174.0 | 15.6 | 304.3 | 20.6 | 465.4 | 25.6 | 657．4 | 30.6 | 880.2 | 35.6 | － 1133.9 |
| ， | 7.2 | ． 7 | 76.4 | 10.7 | 176.4 | 15.7 | 307.2 | 20.7 | 468.9 | 25.7 | 661.5 | 30.7 | 88.5 | 35.7 | 1139.3 |
| ． | 8.3 | 58 | 78.0 | 10.8 | 178.7 | 15.8 | 310.1 | 20.8 | 472.5 | 25.8 | 66 ธ． 7 | 30.8 | 889.8 | 35.8 | 1144．7 |
| 9 | 8． | 5． 9 | 78.8 | 10.9 | 181.0 | 15.9 | 313.1 | 20.9 | 476.1 | 25.9 | 669.9 | 30.9 | 894.6 | 35.9 | 50.1 |

1.010 .56 .0

$1.212 .7 \quad 6.2 \quad 85.0$
$1.313 .9 \quad 6.386 .7$
1.415 .06 .488 .5
$1.516 .26 .5 \quad 90.3$ 11．5 19．）． 2
1．6 17.4 6．6 $93.1 \mid 11.6197 .6$
$1.718 .6 \quad 6.7 \quad 93.911 .7 \times 00.1$
$\begin{array}{llllllllll}1.8 & 19.8 & 6.8 & 9.5 .7 & 11.8 & 203.5\end{array}$

2.022 .27 .099 .4 2.123 .57 .1101 .2 2.224 .7 7．2103．1 $2.326 .07 .3_{10.5}$ 2.427 .37 .4106 .9 $2.528 .57 .5108,8$ 2.629 .97 .6110 .7 2.731 .27 .7112 .6 2.832 .57 .8114 .6 $2.933 .8 \quad 7.9116 .5$

3．035． 28.0118 .5 3.136 .58 .1120 .5 3.237 .9 8．2 122.5 3.339 .38 .3124 .5 $3.440 .7 \quad 8.4126 .5$ 3.542 .1 ४．5 128.5 3.643 .6 ४． 6130.6 3.745 .0 ४． 7132.6 $3.846 .5 \quad$ 子． 8134.7 3.947 .98 .9136 .8 4．049．4 9．0 138. 4.150 .9 9．1 141.0 4．2 52．4 9.2143 .1 4.3 โ3．9 9 9． 3 145．2 4．455． 4 9 4147.4
 4.658 .5 9．6 151.7 4.760 .1 9．7 153.9 4.861 .69 .8156 .1 4.963 .29 .9158 .3

Side slopes 1 to 1 ．

## TABLE NO．XXXII．

## Side Triangles．

## CUBIC rards in corresponding prisms $\frac{100}{6}$ FEET long．

Road－bed 16 feet wide．
Side slopes 1 to 1.

|  |  | Red |  |  |  |  | 長要范 |  | $\begin{aligned} & \text { 을̃̃ } \\ & \text { On } \end{aligned}$ | 淢 | eg 品 | an | Og fi |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 4. | 10 | 5.59 | 15 | 7. | 20.1 | 8.67 | 25 | 10.22 | 30 |  |  | 30 |
|  |  |  |  |  | 5.62 | 15 |  | 20.2 | 8.70 |  |  | 30. |  | 35 |  |
|  | 2 |  | 1 | 10 | 5.65 | 15. | 7.19 | 20.3 | 8.73 | 25． | 0.28 | 30 |  |  |  |
|  | 2.59 |  |  | 10 | 5.68 | 15.4 | 7.22 |  | 8. | 25 |  | 30 |  |  |  |
|  |  |  |  | 10 | 5. | 15 | 7. |  | 8.80 | $2{ }^{2}$ | 34 | 30 |  |  |  |
|  | 2.65 |  |  | 10 | 5. | 15.6 | 7.28 | 20.6 | 8. | 25 | 3 | 30. |  |  |  |
|  |  |  |  | 10. |  | 15.7 | 7. | 20.7 |  | 25 | 10.40 | 30. |  |  |  |
|  | 2.72 |  | 4.26 | 10.8 | 5 | 15 | 7.35 | 20. | 8.89 | 25. | 10.43 | 30.8 | 98 | 35 | 13.52 |
| 0.9 | 2 | 5 | 29 | 10.9 | 5.83 | 15.9 | 7.38 | $\because 0.9$ | 8.92 | 25.91 | 10.46 | 30.9 | 12.01 | 35 | 13.55 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 2 | 6 | 4.35 | 11.1 | 5.90 | 16 | 7.44 | 21 | 8.98 | 26 | 10.52 | 31 | ， |  | 61 |
|  | 2.84 |  |  |  | ， | 16. | 7.47 | 21.2 | 9. |  | 56 |  | 0 |  | 64 |
|  | 2.87 |  | 4.41 | 11.3 | 96 | 16. | 7.50 | 21.3 | 9.04 | 20 | 10.59 |  | 3 |  |  |
|  | 9 |  |  |  | 99 | 16. | 7. |  | 9. |  | 62 |  | 16 |  | 70 |
|  | 93 |  | 4.48 |  | 6．02 | 16. | 7.56 |  | 9.10 |  | 10.65 |  | 12.19 |  |  |
|  | 96 |  |  |  | 6.05 | 16. | 7.59 |  | 9.14 |  |  | 31 | 2．22 |  | 77 |
|  | 99 |  |  |  | 6.08 | 16. | 7.62 |  | 9. |  | 10.71 |  | 5 |  |  |
|  | 02 |  |  |  | 6 | 16 | 7.65 |  | 9.20 | 26 | 10.74 | 31 | 2.28 |  | 83 |
|  | ， | 6 |  |  |  | 16 | 7.69 |  | 9.23 |  |  |  | 12.31 | 36.9 |  |
|  |  |  |  | 12.0 |  | 17.0 | 7．12 |  | 9．26 |  |  |  |  |  |  |
|  | 3.12 |  |  | 12.1 | 6.20 | 17.1 |  |  | 9.29 |  | 10.83 | 32 | 12.38 |  | 13.92 |
|  | 15 | 7. | ． 69 | 12.2 |  | 17.2 |  | 22.2 | 9.32 | 27.2 | 10.86 | 32 | ． 41 |  |  |
|  | 3.18 |  |  | 12.3 | 6. |  |  | 22.3 | 9.35 |  | 10.90 | 32 | ． 44 |  |  |
|  | 3.21 |  | 4.75 | 12.4 | 6.30 | 17 | 7.84 | 22.4 | 9. |  | 10.93 |  | 47 |  | 01 |
|  | 3.24 | 7 | 4.78 | 12.5 | 6.3 |  | 7.87 |  | 9. |  | 10.9 |  | 12.50 |  |  |
|  | 27 |  |  |  |  |  | 7.90 |  | 9. |  | 10.99 |  |  |  |  |
|  | 3.30 |  |  |  |  |  |  |  | 9. |  |  |  |  |  |  |
|  | 3.33 |  |  |  | 6.42 |  | 7.96 |  | 9.51 |  |  |  |  |  |  |
|  | 3.36 | 7. | 4. | 12 | 6. | 17 | 7.99 | 22 | 9.5 |  |  |  |  |  |  |
|  |  |  |  |  |  |  | 8．02 |  | 9.51 |  |  |  |  |  |  |
|  |  |  |  | 13.1 | 6.51 | 18.1 | 8.06 |  | 9.60 |  | 11.14 |  |  |  |  |
|  |  |  |  |  |  |  | 8.09 |  | 9.63 |  |  |  |  |  |  |
|  | 3.49 | 8 |  | 13.3 | 6.5 | 18.3 | 8.12 | 23.3 | 9.66 | 28.3 | 11.20 |  |  |  | 14.29 |
|  | 3.52 |  |  |  |  | 18.4 | 8.15 |  | 9.69 |  | 11.23 |  |  |  |  |
|  | 3.55 | 8. |  | 13.5 | 6.64 |  | 8.18 | 23.5 | 9.72 |  | 11.27 | 33 | ． 81 |  | 4.35 |
|  |  |  |  | 13. |  |  | 8.21 | 23.6 | 9.75 |  | 11.30 |  |  |  |  |
|  | 3.61 |  |  | 13. |  |  | 8.24 | 23.7 | 9.78 | 28.7 | 11.33 |  |  |  |  |
|  |  |  |  | 13.8 |  |  | 8.27 | 23.8 | 9.81 |  | 11.36 |  | ． 90 |  |  |
|  | 3.67 | 8. | 5.22 | 13.9 | 6.7 | 18.9 | 8.30 | 23.9 | 9.85 | 28.9 | 11.39 |  |  |  | 14.48 |
|  |  |  |  |  |  |  | 8.33 |  | 9.88 |  |  |  |  |  |  |
|  |  |  |  | 14. |  | 19.1 | 8.36 |  | 9.91 |  | 11.45 |  | 12.99 |  | 14.54 |
|  |  | 9. |  | 14.2 | 6.85 | 19.2 | 8.40 | 24.2 | 9.94 |  | 11.48 |  |  | 39 |  |
|  |  |  |  |  | 6.88 | 19.3 | 8.43 | 24.3 | 9.97 |  | 11.51 |  | 3.06 |  | 14.60 |
|  | 83 | 9. | ． | 14.4 | 6.91 | 19.4 | 8.46 |  | 10.00 |  | 11.54 | ． | 3.09 | 39 | 14.63 |
|  |  |  |  | 14. | 6.94 | 19.5 | 8.49 | 24 | 10.03 | 29 | 11.57 |  | 3.12 |  | 14.66 |
|  | 3.89 | 9. | 5 | 14. | 6.98 | 19.6 | 8.52 | 24.6 | 10.06 |  | 11.60 |  |  |  | 14.69 |
|  | 3.92 | 9. | 5.46 | 14. | 7.01 | 19.7 | 8．5．5 | 24.7 | 10.09 |  | 11.64 |  | 3.18 | 39. | 14.72 |
| 4.8 | 3.95 |  | 5.49 |  | 7.04 | 19.8 | 8.58 | 24.8 | 10.12 |  | 11.67 |  | ． 21 | 39. | 14．75 |
| 4.9 | 3.98 | 9. | 5.52 | 14.9 | 7.07 | 19.9 | 8.61 | 24.9 | 10.15 | 29.9 | 11.70 | 34. | 3.24 | 39.9 | 14.78 |

## TABLE NO. XXXIII

CUBIC YARDS, IN 100 FEET LENGTHS, FOR GIVEN AREAS.

| Area. | Cubic yards. | Area. | Cubic yards. | Area. | Cubic yards. | Area. | Cubic yards. | Area. | Cubic yards |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.62 | 1 | 82.62 | 51 | 163.63 | 101 | 244.6 | 151 | 325. 62 | 201 |
| 3.24 | 2 | 84.24 | $5 \cdot 3$ | 1 (i5. 24 | 102 | 246.24 | 152 | $3 \times 7.24$ | 20.3 |
| 4.86 | 3 | 85.86 | 53 | 166.86 | 103 | 247.86 | 153 | 328.86 | 203 |
| 6.48 | 4 | 87.48 | 54 | 168.48 | 104 | 249.48 | 154 | 3330.48 | 204 |
| 8.10 | 5 | 89.10 | 55 | 170.10 | 105 | $2 \overline{5} 1.10$ | 15.) | 335.10 | 205 |
| 9.72 | 6 | 90.72 | 56 | 171.72 | 106 | 252.72 | 156 | 333.72 | 206 |
| 11.34 | 7 | 92.34 | 57 | 173.34 | 107 | 254.34 | 157 | 335.34 | 207 |
| 12.96 | 8 | 93.96 | 58 | 174.96 | 108 | 25 ). 96 | 158 | 3336.96 | 208 |
| 14.58 | 9 | 95.58 | 59 | 176.58 | 109 | 257.58 | 159 | 338.58 | 209 |
| 16.20 | 10 | 97.20 | 60 | 178.20 | 110 | 259.20 | 160 | 340.20 | 210 |
| 17.82 | 11 | 98.82 | 61 | 179.82 | 111 | 260.82 | 161 | 341.82 | 211 |
| 19.44 | 12 | 100.44 | 62 | 181.44 | 112 | 262.44 | 162 | 343.44 | 212 |
| 21.0; | 13 | 102.06 | 63 | 183.06 | 113 | 264.06 | 163 | 345.06 | 213 |
| 22.68 | 14 | 103.68 | 64 | 184.68 | 114 | 26.). 68 | 164 | 346.68 | 214 |
| 24.30 | 15 | 105.30 | 6.5 | 186.30 | 115 | 267.30 | 165 | 348.30 | 215 |
| 25.92 | 16 | 106.92 | 66 | 18\%.9\% | 116 | 268.92 | 166 | 349.9 \% | 216 |
| 27.54 | 17 | 108.54 | 67 | 189.54 | 117 | 270.54 | 167 | 351.54 | 217 |
| 29.16 | 18 | 110.16 | 68 | 191.16 | 118 | $27 \pm .16$ | 168 | 353.16 | 218 |
| 30.78 | 19 | 111.78 | 69 | 192.78 | 119 | 273.78 | 169 | 354.78 | 219 |
| 32.40 | 20 | 113.40 | 70 | 194.40 | 120 | 275.40 | 170 | 356.40 | 220 |
| 34.02 | 21 | 115.02 | 71 | 196.02 | 121 | 277.02 | 171 | 358.02 | 221 |
| 35.64 | 22 | 116.64 | 72 | 197.64 | 122 | 278.64 | 172 | 359.64 | 222 |
| 37.26 | 23 | 118.26 | 73 | 199.26 | 123 | 280.26 | 173 | 361.26 | 223 |
| 38.88 | 24 | 119.88 | 74 | 200.83 | 124 | 281.83 | 174 | 362.88 | 224 |
| 40.50 | 25 | 121.50 | 7.$)$ | 202.50 | 125 | 283.50 | 175 | 364.50 | 225 |
| 42.12 | 26 | 123.12 | 76 | 204.12 | 126 | 28.). 12 | 176 | 366.12 | 226 |
| 43.74 | 27 | 124.74 | 77 | 20.5 .74 | 127 | 286.74 | 177 | 367.74 | 227 |
| 45.36 | 28 | 126.36 | 78 | 207.36 | 128 | 288.36 | 178 | 369.36 | 228 |
| 46.98 | 29 | 127.98 | 79 | 204.98 | 129 | 289.98 | 179 | 370.98 | 229 |
| 48.60 | 30 | 129.60 | 80 | 210.60 | 130 | 291.60 | 180 | 372.60 | 230 |
| 50.22 | 31 | 131.22 | 81 | 212.22 | 131 | 293.22 | 181 | 374.23 | 231 |
| 51.84 | 32 | 132.84 | 82 | 213.84 | 132 | 294.84 | 182 | 375.84 | 232 |
| 53.46 | 33 | 134.46 | 83 | 215.46 | 133 | 296.46 | 183 | 377.46 | 233 |
| 55.08 | 34 | 136.08 | 84 | 217.08 | 134 | 298.08 | 184 | 379.08 | 234 |
| 56.70 | 35 | 137.70 | 8.) | 218.70 | 135 | 299.70 | 185 | 380.70 | 235 |
| 58.32 | 36 | 139.32 | 86 | $220.3 \geqslant$ | 136 | 301.32 | 186 | 382.32 | 2:36 |
| 59.94 | 37 | 140.94 | 87 | 221.94 | 137 | 302.94 | 187 | 383.94 | 237 |
| 61.56 | 38 | 142.56 | 88 | 223.56 | $1: 38$ | 204.56 | 188 | 385.56 | 238 |
| 63.18 | 39 | 144.18 | 89 | 225.18 | 139 | 306.18 | 189 | 387.18 | 239 |
| 64.80 | 40 | 145.80 | 90 | 226.80 | 140 | 307.80 | 190 | 388.80 | 240 |
| 66.42 | 41 | 147.42 | 91 | 228.42 | 141 | 309.42 | 191 | 390.42 | 241 |
| 68.04 | 42 | 149.04 | 92 | 230.04 | 142 | 311.04 | 192 | 392.04 | 242 |
| 69.66 | 43 | 150.66 | 93 | 231.66 | 143 | 312.66 | 193 | 393.66 | 243 |
| 71.28 | 44 | 152.28 | 94 | 233.28 | 144 | 314.28 | 194 | 395.28 | 244 |
| 72.90 | 45 | 153.90 | 95 | 234.90 | 145 | 315.90 | 195 | 396.90 | 24.5 |
| 74.52 | 46 | 155.52 | 96 | 236.53 | 146 | 317.52 | 196 | 398.52 | 246 |
| 76.14 | 47 | 157.14 | 97 | 238.14 | 147 | 319.14 | 197 | 400.14 | 247 |
| 77.76 | 48 | 158.76 | 98 | 239.76 | 148 | 320.76 | 198 | 401.76 | 248 |
| 79.38 | 49 | 160.38 | 99 | 241.38 | 149 | 322.38 | 199 | 403.38 | 249 |
| 81.00 | 50 | 162.00 | 100 | 243.00 | 150 | 324.00 | 200 | 405.00 | 250 |
|  |  |  |  |  |  |  |  |  |  |

TABLE NO. XXXIII.-Continued.

CUBIC YARDS, IN 100 FEET LENGTHS, FOR GIVEN AREAS.

| Area. | Cubic yards. | Area. | Cuble yards. | Area. | Cubic yards | Area. | Cubic yards. | Area. | Cubic yarus. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 406.62 | 251 | 487.62 | 301 | 568.62 | 351 | 649.62 | 401 | 730.62 | 451 |
| 408.24 | 252 | 489.24 | 302 | 570.24 | 3.22 | 651.24 | 402 | 732.24 | 452 |
| 409.86 | 2.53 | 490.86 | 303 | 571.86 | 3\%3 | $6.5) .86$ | 403 | 733.86 | 453 |
| 411.48 | 254 | 492.48 | 304 | 573.4M | 354 | 654.48 | 404 | 735.48 | 454 |
| 413.10 | 255 | 494.10 | 305 | 575.10 | 3.55 | 656.10 | 405 | 737.10 | 455 |
| 414.72 | 256 | 495. 72 | 306 | $5 \% 6.72$ | 356 | 657.72 | 406 | 738.72 | 4.56 |
| 416.34 | 257 | 497.34 | 307 | 578.34 | 357 | 6 59 9.34 | 407 | 740.34 | 457 |
| 417.96 | 258 | 498.96 | 308 | 579.96 | $35 \square$ | 660.96 | 4118 | 741.96 | $4 \overline{3} 8$ |
| 419.58 | 259 | $500.5 \bigcirc$ | 309 | 581.58 | 359 | 662.58 | 409 | 743.58 | 459 |
| 421.20 | 260 | 502.20 | 310 | 583.20 | 360 | 664.20 | 410 | 745.20 | 460 |
| 422.82 | 261 | 503.82 | 311 | 584.82 | 361 | 665.82 | 411 | 746.82 | 461 |
| 424.44 | 262 | 505.44 | 312 | 586.44 | 362 | 667.44 | 412 | 748.44 | 462 |
| 426.06 | 263 | 507.06 | 313 | $5 \times 8.06$ | 363 | 66906 | 413 | 750.06 | 463 |
| 42768 | 264 | 508.68 | 314 | 589.68 | 364 | $6 \% 0.68$ | 414 | 751.68 | 464 |
| $4: 9.30$ | 265 | 510.30 | 315 | 591.30 | 365 | 672.30 | 415 | 753.30 | 465 |
| 430.92 | 266 | 511.92 | 316 | 592.92 | 366 | 673.92 | 416 | $754.9{ }^{\circ}$ | 466 |
| 43:2.54 | 267 | 513.54 | 317 | 594.54 | 367 | 675.54 | 417 | 756.54 | 467 |
| 434.16 | 2 ¢i | 515.16 | 318 | 596.16 | 368 | 677.16 | 418 | 755.16 | 468 |
| 435.78 | $\stackrel{29}{ }$ | 516.78 | 319 | 597.78 | 369 | 678.78 | 419 | 759.78 | 469 |
| 437.40 | 270 | 518.40 | $3 \pm 0$ | 599.40 | 370 | 680.40 | 420 | 761.40 | 470 |
| 439.02 | 271 | 520.02 | 321 | 601.02 | 371 | 682.02 | 421 | 763.02 | 471 |
| 440.64 | 272 | 521.64 | 32\% | 602.64 | 372 | 683.64 | 422 | 764.64 | 472 |
| 442.26 | 273 | 523.26 | $3 \because 3$ | 604.26 | 373 | 685.26 | 423 | 766.26 | 473 |
| 443.88 | 274 | 524.88 | 324 | 605.88 | 374 | 686.88 | 424 | 567.88 | 474 |
| 445.50 | 275 | 526.50 | 325 | 607.50 | $3 \% 5$ | 688.50 | 425 | 769.50 | 475 |
| 447.12 | 276 | 528.12 | 326 | 609.12 | 376 | 690.12 | 426 | 771.12 | 476 |
| 448.74 | 277 | 529.74 | $3: 27$ | 610.74 | 377 | 691.74 | 427 | 772.74 | 477 |
| $451) .36$ | $2 \sim 8$ | 531.36 | 328 | 61236 | 378 | 693.36 | 428 | \%74.36 | 478 |
| 451.98 | 27!) | 532.98 | $3: 9$ | 613.98 | 379 | 694.98 | $4 \geqslant 9$ | 775.98 | 479 |
| 453.60 | 280 | 534.60 | 330 | 615.60 | 380 | 696.60 | 430 | 7\%7.60 | 480 |
| 455.22 | 281 | 536.22 | 331 | 617.22 | 381 | 698.22 | 431 | 779.22 | 481 |
| 456.84 | $28 \%$ | $50: 37.84$ | $3 \%$ | 61884 | 382 | 699.84 | 432 | 780.84 | 482 |
| 458.46 | 283 | 5:39.46 | 333 | 620). 46 | 383 | 701.46 | 433 | 782.46 | 483 |
| 460.08 | 284 | 541.08 | 334 | 622.08 | 384 | 703.08 | 434 | 784.08 | 484 |
| 461.70 | $2 \times 5$ | 542.70 | 335 | 623.70 | 38.) | \%04.70 | 435 | 785. 70 | 485 |
| 463.32 | $2 \times 6$ | $544.3 \%$ | 336 | $6 \div 5.32$ | 356 | 706.3 | 436 | 787.32 | 486 |
| 464.94 | $2 \times 7$ | 54.5 .94 | 337 | 626.94 | 387 | \%07.94 | 487 | \%88.94 | 487 |
| 466.56 | 288 | $54 \% .56$ | 338 | 628.56 | 388 | 709.56 | 438 | 790.56 | 488 |
| 468.18 | 259 | 549.18 | 339 | 630.18 | 389 | 711.18 | $4: 39$ | 792.18 | 489 |
| 469.80 | 290 | 550.50 | 340 | 631.80 | 390 | 712.80 | 440 | 793.80 | 490 |
| 471.42 | 291 | 552.42 | 341 | 633.42 | 391 | 714.42 | 441 | \%95.42 | 491 |
| $4 \% 3.04$ | 29.2 | 5.54 .04 | 342 | 635.04 | 392 | 716.04 | 442 | 797.04 | 492 |
| $4 \% 4.66$ | 293 | 55\%). 66 | 343 | 636.66 | 393 | 717.66 | 443 | 798.66 | 493 |
| 476.28 | 29.1 | 557.28 | 344 | 638.28 | 394 | 719.28 | 444 | 800.28 | 494 |
| 477.90 | 295 | 558.90 | 345 | 639.90 | $39 \%$ | 720.90 | 445 | 801.90 | 495 |
| 479.52 | 296 | 560.52 | 346 | 641.52 | 396 | 72.52 | 446 | 803. 52 | 496 |
| 481.14 | 297 | $56: .14$ | 347 | 643.14 | 397 | 724.14 | 447 | 805.14 | 497 |
| 482.76 | 298 | 563.76 | 348 | 644.76 | 398 | 725.76 | 448 | 806.76 | 498 |
| 484.38 | 299 | 565.38 | 349 | 646.38 | 399 | 727.38 | 449 | 808.38 | 499 |
| 486.00 | 300 | 567.00 | 350 | 648.00 | 400 | \%29.00 | 450 | 810.00 | 500 |

TABLE NO. XXXIII.-Continued.

CUBIC YARDS, IN $\frac{100}{6}$ FEET LENGTHS, FOR GIVEN AREAS.

| Area | Cubic yards. | Area. | Cubic yards. | Area. | Cubic yards | Area. | Cubic yards. | Area. | Cubic yards. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 811.62 | 501 | 892.62 | 551 | 973.62 | 601 | 1054.6\% | 651 | 1135.62 | 701 |
| 813.24 | 502 | 894.24 | 552 | 975.24 | 602 | 1056.24 | 652 | 1137.24 | 702 |
| 814.86 | 503 | 895.86 | 553 | 976.86 | 603 | 1057.26 | 653 | 1138.86 | 703 |
| 816.48 | 504 | 897.48 | $5 \overline{4}$ | 978.48 | 604 | 1059.48 | 654 | 1140.48 | . 04 |
| 818.10 | 505 | 899.10 | 555 | 980.10 | 605 | 1061.10 | 655 | 1142.10 | \%(0) |
| 819.72 | 506 | 900.72 | 556 | 981.72 | 606 | 1062.72 | 656 | 1143.72 | 706 |
| 821.34 | 507 | 902.34 | 557 | 983.34 | 607 | 1064.34 | 657 | 1145.34 | 707 |
| 822.96 | 508 | 903.96 | 558 | 984.96 | 608 | 1065.96 | 658 | 1146.96 | 708 |
| 824.58 | 509 | 90 ¢. 58 | 559 | 986.58 | 609 | 1067.58 | 659 | 1148.58 | 709 |
| 826.20 | 510 | 907.20 | 560 | 988.20 | 610 | 1069.20 | 660 | 1150.20 | 710 |
| 897.82 | 511 | 908.82 | 561 | 989.82 | 611 | 1070.82 | 661 | 1151.82 | 711 |
| 829.44 | 512 | 910.44 | 562 | 991.44 | 612 | 1072.44 | 662 | 1153.44 | 712 |
| 831.06 | 513 | 912.06 | 563 | 993.06 | 613 | 1074.06 | 663 | 1155.06 | 713 |
| 833.63 | 514 | 913.68 | 564 | 994.68 | 614 | 1075.68 | 664 | 1156.68 | 714 |
| 834.30 | 515 | 915.30 | 565 | 996.30 | 615 | 1077.30 | 665 | 1158.30 | 715 |
| 835.92 | 516 | 916.92 | 566 | 997.92 | 616 | 1078.92 | 666 | 1159.92 | 716 |
| 837.54 | 517 | 918.54 | 567 | 999.54 | 617 | 1080.54 | 667 | 1161.54 | 717 |
| 839.16 | 518 | 920.16 | 568 | 1001.16 | 618 | 108\%.16 | 668 | 1163.16 | 718 |
| 840.78 | 519 | $9: 31.78$ | 569 | 1002.78 | 619 | 1083.78 | 669 | 1164.78 | 719 |
| 842.40 | 590 | 923.40 | 570 | 1004.40 | 620 | 1085.40 | 670 | 1166.40 | 720 |
| 844.02 | 521 | 925.02 | 571 | 1006.02 | 621 | 1087.02 | 671 | 1168.02 | 721 |
| 845.64 | 52. | 926.64 | 572 | 1007.64 | 622 | 1088.64 | 672 | 1169.64 | 72 |
| 847.26 | $5 \geqslant 3$ | 928.26 | 573 | 1009.26 | $6 \cdot 3$ | 1090.26 | 673 | 1171.26 | 723 |
| 848.88 | 524 | 929.88 | 574 | 1010.88 | 624 | 1091.88 | 674 | 1172.88 | 724 |
| 8.50 .50 | 525 | 931.50 | 575 | 1012.50 | 625 | 1093.50 | 675 | 1174.50 | 725 |
| 852.12 | 526 | 933.12 | 576 | 1014.12 | 626 | 1095.12 | 676 | 1176.12 | 726 |
| 853.74 | 527 | 934.74 | 577 | 1015.74 | 627 | 1096.74 | 677 | 1177.74 | 727 |
| 855.36 | 528 | 936.36 | 578 | 1017.36 | 628 | 1098.36 | 678 | 1179.36 | 728 |
| 856.98 | $5: 9$ | 937.98 | 579 | 1018.98 | 629 | 1099.98 | 679 | 1180.98 | 7\%9 |
| 858.60 | 530 | 939.60 | 580 | 1020.60 | 630 | 1101.60 | 680 | 1182.60 | 730 |
| 860.22 | 531 | 941.22 | 581 | 1022.22 | $6: 31$ | 1103.22 | 681 | 1184.22 | 731 |
| 861.84 | 532 | 942.84 | 582 | 1023.84 | 632 | 1104.84 | 682 | 1185.84 | 732 |
| 863.46 | 533 | 944.46 | 583 | 1025.46 | 633 | 1106.46 | 683 | 1187.46 | 733 |
| 865.08 | 534 | 946.08 | 584 | 1027.08 | 634 | 1108.08 | 684 | 1189.08 | 734 |
| 866.70 | 535 | 947.70 | 585 | 1028.70 | 635 | 1109.70 | 685 | 1190.70 | 735 |
| $868.3 \%$ | 536 | 949.32 | 586 | 1030.32 | 636 | 1111.32 | 686 | 1192.32 | 736 |
| 869.94 | 537 | 950.94 | 587 | 1031.94 | 637 | 1112.94 | 687 | 1198.94 | 737 |
| 871.56 | 538 | 952.56 | 588 | 1033.56 | 638 | 1114.56 | 688 | 119.). 56 | 738 |
| 873.18 | 539 | 954.18 | 589 | 1035.18 | 639 | 1116.18 | 689 | 1197.18 | 739 |
| 874.80 | 540 | 955.80 | 590 | 1036.80 | 640 | 1117.80 | 690 | 1198.80 | 740 |
| 876.42 | 541 | 9.37 .42 | 591 | 1038.42 | 641 | 1119.42 | 691 | 1200.42 | 741 |
| 878.04 | 542 | 959.04 | 592 | 1040.04 | 642 | 1121.04 | 692 | 1202.04 | 742 |
| 879.66 | 543 | 960.66 | 593 | 1041.66 | 643 | 1122.66 | 693 | 1203.66 | 743 |
| 881.28 | 544 | 962.28 | 594 | 1043.28 | 644 | 1124.28 | 694 | 1205.28 | 744 |
| 882.90 | 545 | 963.90 | 595 | 1044.90 | 645 | 1125.90 | 695 | 1206.90 | 745 |
| 884.52 | 546 | 965.52 | 596 | 1046.52 | 646 | 1127.52 | 696 | 1208.52 | 746 |
| 886.14 | 547 | 967.14 | 597 | 1048.14 | 647 | 1129.14 | 697 | 1210.14 | 747 |
| 887.76 | 548 | 968.76 | 598 | 1049.76 | 648 | 1130.76 | 698 | 1211.76 | 748 |
| 889.38 | 549 | 970.38 | 599 | 1051.38 | 649 | 1132.38 | 699 | 1213.38 | 749 |
| 891.00 | 550 | 972.00 | 600 | 1053.00 | 650 | 1134.00 | 700 | 1215.00 | 750 |

TABLE NO. XXXIII.-Continued.

CUBIC YARDS, IN $\frac{100}{6}$ FEET LENGTHS, FOR GIVEN AREAS

| Area | Cubic jards. | Area. | Cubic yards. | Area. | Cubic yards. | Area. | Cubic yards. | Area | Cubic yards. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1216.62 | 751 | 1297.62 | 801 | 1378.62 | 851 | 1459.62 | 901 | 1540.62 | 951 |
| 1218.24 | $75 \%$ | 1299.24 | 802 | 1380.24 | 852 | 1461.24 | 902 | 1542.24 | 952 |
| 1219.86 | 753 | 1300.86 | 803 | 1381.86 | 853 | 1462.86 | 903 | 1543.86 | 953 |
| 1221.48 | 754 | 1302.48 | 804 | 1383.48 | 854 | 1464.48 | 904 | 1545.48 | 954 |
| 1223.10 | 75.5 | 1304.10 | 805 | 1385.10 | 855 | 1466.10 | 905 | 1547.10 | 955 |
| 1224.72 | 756 | 1305.72 | 806 | 1386.72 | 856 | 1467.72 | 906 | 1548.72 | 956 |
| 1226.34 | 757 | 1307.34 | 807 | 1388.34 | 8.57 | 1469.34 | 907 | 1550.34 | 957 |
| 1227.96 | 753 | 1308.96 | 808 | 1389.96 | 858 | 1470.96 | 908 | 1551.96 | 958 |
| 1229.58 | 759 | 1310.58 | 809 | 1391.58 | 859 | 1472.58 | 909 | 1553.58 | 959 |
| 1231.20 | 760 | 1312.20 | 810 | 1393.20 | 860 | 1474.20 | 910 | 1555.20 | . 960 |
| 1232.82 | 761 | 1313.82 | 811 | 1394.82 | 861 | 1475.82 | 911 | 1556.82 | 961 |
| 1234.44 | 762 | 1315.44 | 812 | 1396.44 | 862 | 1477.44 | 912 | 1558.44 | 962 |
| 1236.06 | 763 | 1317.06 | 813 | 1398.06 | 863 | 1479.06 | 913 | 1560.06 | 963 |
| 1237.68 | 764 | 1318.68 | 814 | 1399.68 | 864 | 1480.68 | 914 | 1561.68 | 964 |
| 1239.30 | 765 | 1320.30 | 815 | 1401.30 | 865 | 1482.30 | 915 | 1563.30 | 965 |
| 1240.92 | 766 | 1321.92 | 816 | 1402.92 | 866 | 1483.92 | 916 | 1564.92 | 966 |
| 1242.54 | 767 | 1323.54 | 817 | 1404.54 | 867 | 1485.54 | 917 | 1566.54 | 967 |
| 1244.16 | 768 | 1325.16 | 818 | 1406.16 | 868 | 1487.16 | 918 | 1568.16 | 968 |
| 1245.78 | 769 | 1326.78 | 819 | 1407.78 | 869 | 1488.78 | 919 | 1569.78 | 969 |
| 1247.40 | 770 | 1328.40 | 820 | 1409.40 | $8 \% 0$ | 1490.40 | 920 | 1571.40 | 970 |
| 1249.02 | 781 | 1330.02 | 821 | 1411.02 | 871 | 1492.02 | 921 | 1573.02 | 971 |
| 1250.64 | 772 | 1331.64 | 822 | 1412.64 | 872 | 1493.64 | 922 | 1574.64 | 972 |
| 1252.26 | 773 | 1333.26 | 823 | 1414.26 | 873 | 1495. 26 | 923 | 1576.26 | 973 |
| 1253.88 | $7 \% 4$ | 1334.88 | 8:4 | 1415.88 | 874 | 1496.88 | 924 | 1577.88 | 974 |
| 1255.50 | 775 | 1336.50 | 825 | 1417.50 | 875 | 1498.50 | 925 | 1579.50 | 975 |
| 1257.12 | 776 | 1338.12 | 826 | 1419.12 | 876 | 1500.12 | 926 | 1581.12 | 976 |
| 1258.74 | 777 | 1339.74 | 827 | 1420.74 | 877 | 1501.74 | 927 | 1582.74 | 977 |
| 1260.36 | 778 | 1341.36 | 828 | 1422.36 | $8 \% 8$ | 1503.36 | 928 | 1584.36 | 978 |
| 1261.98 | 779 | 1342.98 | 829 | 1423.98 | 879 | 1504.98 | 929 | 1585.98 | 979 |
| 1263.60 | 780 | 1344.60 | 830 | 1425.60 | 850 | 1506.60 | 930 | 1587.60 | 980 |
| 1265.22 | 781 | 1346.22 | 831 | 1427.22 | 881 | 1508.22 | 931 | 1589.22 | 981 |
| 1266.84 | 782 | 1347.84 | 832 | 1428.84 | 882 | 1509.84 | 932 | 1590.84 | 982 |
| 1268.46 | 783 | 1349.46 | 833 | 1430.46 | 883 | 1511.46 | 933 | 1592.46 | 983 |
| 1270.08 | 784 | 1351.08 | 834 | 1432.08 | 884 | 1513.08 | 934 | 1594.08 | 984 |
| 1271.70 | 785 | 13.52.70 | 835 | 1433.70 | 885 | 1514.70 | 935 | 1595.70 | 985 |
| 1273.32 | 786 | 1354.32 | 836 | 1435.32 | 886 | 1516.32 | 936 | 1597.32 | 986 |
| 1274.94 | 787 | 13.55 .94 | 837 | 1436.94 | 887 | 1517.94 | 937 | 1598.94 | 987 |
| 1276.56 | 788 | 1357.56 | 838 | 1438.56 | 888 | 1519.56 | 938 | 1600.56 | 988 |
| 1278.18 | 789 | 1359.18 | 839 | 1440.18 | 889 | 1521.18 | 939 | 1602.18 | 989 |
| 1279.80 | 790 | 1360.80 | 840 | 1441.80 | 890 | 1522.80 | 940 | 1603.80 | 990 |
| 1281.42 | 791 | 1362.42 | 841 | 1443.42 | 891 | 1524.42 | 941 | 1605.42 | 991 |
| 1283.04 | 792 | 1364.04 | 842 | 1445.04 | 892 | 1526.04 | 942 | 1607.04 | 992 |
| 1284.66 | 793 | 1365.66 | 843 | 1446.66 | 893 | 1527.66 | 943 | 1608.66 | 993 |
| 1286.28 | 794 | 1367.28 | 844 | 1448.28 | 894 | 1529.28 | 944 | 1610.28 | 994 |
| 1287.90 | 795 | 1368.90 | 845 | 1449.90 | 895 | 1530.90 | 945 | 1611.90 | 995 |
| 1289.52 | 796 | 1370.52 | 846 | 1451.52 | 896 | 1532.52 | 946 | 1613.52 | 996 |
| 1291.14 | 797 | 1372.14 | 847 | 1453.14 | 897 | 1534.14 | 947 | 1615.14 | 997 |
| 1292.76 | 798 | 1373.76 | 848 | 1454.76 | 898 | 1535.76 | 948 | 1616.76 | 998 |
| 1294.38 | 799 | 1375.38 | 849 | 1456.38 | 899 | 1537.38 | 949 | 1618.38 | 999 |
| 1296.00 | 800 | 1377.00 | 850 | 1458.00 | 900 | 1539.00 | 950 | 1620.00 | 1000 |

TABLE A.

## Level Cross Sections.

## cubic fards in corresponding prisms, 100 feet long.

## PART FIRST.

Road-bed 18 feet wide.


TABLE A.-Continued.

PART SECOND.


TABLE B.

## Level Cross Sections.

CUBIC YARDS IN CORRESPONDING PRISMS, 100 FEET LONG.
Road-bed 28 feet wide.

| Height. |  | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 |  | 0.0 | 10.4 | 20.8 | 31.3 | 41.8 | 52.3 | 62.9 | 73.5 | 84.1 | 94.8 |
|  | 94. | 95. | 295. | $5 \quad 95$. | 896. | 196. | 596. | 897. | 297. | 597. | 9 |
| 1 |  | 105.6 | 1163 | 127.1 | 137.9 | 148.8 | 159.7 | 170.7 | 181.6 | 192.7 | 203.7 |
|  | 98. | 98. | 598. | 899. | 299. | 99. | 9100. | 1100. | 5100. | 8101. | 2 |
| 2 |  | 214.8 | 225.9 | 237.1 | 248.3 | 259.6 | 270.8 | 282.1 | 293.5 | 304.9 | 316.3 |
|  | 101. | 5101. | 9102. | 2102. | 5102. | 8103. | 2103. | 5103. | 8104. | 2104. | 5 |
| 3 |  | 327.8 | 339.3 | 350.8 | 362.4 | 374.0 | 385.6 | 397.3 | 409.1 | 420.8 | 432.6 |
|  | 104. | 8105. | 1105. | 5105. | 8106. | 2106 | 5106. | 9107. | 1107. | 5107. | 8 |
| 4 |  | 444.4 | 456.3 | 468.2 | 480.2 | 492.1 | 504.2 | 516.2 | 528.3 | 540.4 | 552.6 |
|  | 108. | 2108. | 5108. | 9109. | 1109. | 5109. | 8110. | 2110. | 5110. | 9111. | 2 |
| 5 |  | 564.8 | 577.1 | 589.3 | 601.6 | 614.0 | 626.4 | 638.8 | 651.3 | 663.8 | 676.3 |
|  | 111. | 5111. | 8112. | 2112. | 5112.8 | 8113. | 2113. | 5113. | 8114. | 1114. | 5 |
| 6 |  | 688.9 | 701.5 | 714.1 | 726.8 | 739.6 | 752.3 | 765.1 | 777.9 | 790.8 | 803.7 |
|  | 114. | 8115. | 2115. | 5115. | 9116. | 1116. | 5116. | 8117. | 2117. | 5117. | 9 |
| 7 |  | 816.7 | 829.6 | 842.7 | 855.7 | 868.8 | 881.9 | 895.1 | 908.3 | 921.6 | 934.8 |
|  | 118. | 1118.5 | 5118. | 8119. | 2119. | 5119. | 9120. | 2120. | 5120. | 8121. | 2 |
| 8 |  | 948.1 | 961.5 | 974.9 | 988.3 | 1001.8 | 1015.3 | 1028.8 | 1042.4 | 1056.0 | 1069.6 |
|  | 121. | 5121. | 8122. | 2122. | 5122.8 | 8123. | 1123. | 5123. | 8124. | 2124. | 5 |
| 9 |  | 1083.3 | 1097.1 | 1110.8 | 1124.6 | 1138.4 | 1152.3 | 1166.2 | 1180.2 | 1194.1 | 1208.2 |
|  | 124. | 9125. | 1125. | 5125. | 8126. | 2126. | 5126. | 9127. | 1127. | 5127. | 8 |
| 10 |  | 1222.2 | 1236.3 | 1250.4 | 1264.6 | 1278.8 | 1293.1 | 1307.3 | 1321.6 | 1336.0 | 1350.4 |

TABLE NO. XXXIV.
Level Cross Sections.

## cubic fards in lengtis of 100 feet.

Road-bed 24 feet wide.
Side slope $1 \frac{1}{2}$ to 1.

| Height. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1.0 | 1.1 | 1.2 | 1.3 | 1.4 | 1.5 | Height. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 | 0 | 4 | 9 | 14 | 18 | 23 | 27 | 32 | 37 | 42 | 46 | 51 | 56 | 61 | 66 | 71 | 0.0 |
| 0.1 | 4 | 9 | 13 | 18 | 23 | 27 | 32 | 37 | 41 | 46 | 51 | 56 | 61 | 66 | 71 | 76 | 0.1 |
| 0.2 | 9 | 13 | 18 | 23 | 27 | 32 | 37 | 41 | 46 | 51 | 56 | 61 | 65 | 70 | 75 | 80 | 0.2 |
| 0.3 | 14 | 18 | 23 | 27 | 32 | 36 | 41 | 46 | 51 | 56 | 60 | 65 | 70 | 75 | 80 | 85 | 0.3 |
| 0.4 | 18 | 23 | 27 | 32 | 36 | 41 | 46 | 51 | 55 | 60 | 65 | 70 | 75 | 80 | 85 | 90 | 0.4 |
| 0.5 | 23 | 21 | 32 | 36 | 41 | 46 | 51 | 55 | 60 | 65 | 70 | 75 | 80 | 85 | 90 | 95 | 0.5 |
| 0.6 | 27 | 32 | 37 | 41 | 46 | 51 | 55 | 60 | 65 | 70 | 75 | 80 | 85 | 90 | 95 | 100 | 0.6 |
| 0.7 | 32 | 37 | 41 | 46 | 51 | 55 | 60 | 65 | \% 0 | 75 | 80 | 85 | 90 | 95 | 100 | 105 | 0.7 |
| 0.8 | 37 | 41 | 46 | 51 | 55 | 60 | 65 | 70 | 75 | 80 | 85 | 90 | 95 | 100 | 105 | 110 | 0.8 |
| 0.9 | 42 | 46 | 51 | 56 | 60 | 65 | 70 | 75 | 80 | 85 | 89 | 94 | 100 | 105 | 110 | 115 | 0.9 |
| 1.0 | 46 | 51 | 56 | 60 | 65 | \% 0 | 75 | 80 | 85 | 89 | 94 | 99 | 105 | 110 | 115 | 120 | 1.0 |
| 1.1 | 51 | 56 | 61 | 65 | 70 | 75 | 80 | 85 | 90 | 94 | 99 | 105 | 110 | 115 | 120 | 125 | 1.1 |
| 1.2 | 56 | 61 | 65 | 70 | 75 | 80 | 85 | 90 | 95 | 100 | 105 | 110 | 115 | 120 | 125 | 130 | 1.2 |
| 1.3 | 61 | 66 | 70 | 75 | 80 | 85 | 90 | 95 | 100 | 105 | 110 | 115 | 120 | 125 | 130 | 135 | 1.3 |
| 1.4 | 66 | 71 | 75 | 80 | 85 | 90 | 95 | 100 | 105 | 110 | 115 | 120 | 125 | 130 | 135 | 141 | 1.4 |
| 1.5 | 71 | 76 | 80 | 85 | 90 | 95 | 100 | 105 | 110 | 115 | 120 | 125 | 130 | 135 | 141 | 146 | 1.5 |
| Height. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1.0 | 1.1 | 1.2 | 1.3 | 1.4 | 1.5 | Height. |

TABLE NO．XXXV．

## Level Cross Sections．

## cubic yards in Corresponding prisms 100 feet long．

Road－bed 12 feet wide．
Side slopes 1 to 1.

| $\begin{aligned} & \text { 淢 } \\ & \text { 密 } \end{aligned}$ |  | $\begin{aligned} & \text { 总 } \\ & \text { 要 } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { 范 } \\ & \text { 覂 } \end{aligned}$ |  | $\begin{aligned} & \text { 感 } \\ & \stackrel{\rightharpoonup}{3} \end{aligned}$ |  | 嵒 |  | 范 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 | 0 | 5.0 | 315 | 10.0 |  | 15 | 1500 | 20.0 | 2370 | 25.0 | 3426 | 30.0 | 4667 | 35.0 | 93 |
|  | 4 |  | $3 \because 3$ | 10.1 | 827 | 15.1 | 1516 | 2.1 | 2390 | 2．）． 1 | 3449 | 30.1 | 4693 | 35.1 | 6123 |
|  | 9 | 5.2 | 3：31 | 10.2 | 39 | 15.2 | 15：31 | 20.2 | 2409 | 25.2 | 3472 | 30.2 | 4720 | 35 | 6153 |
|  | 14 | 5.3 | 340 | 10.3 | 851 | 15.3 | 1547 | 20.3 | 2429 | 25.3 | 3495 | 30.3 | 4747 | 35. | 84 |
|  | 18 | 5.4 | 348 | 10.4 | 863 | 15.4 | 1563 | 20.4 | 244 | 25. | 3518 | 30. | 4774 | 35. | 6115 |
| 0.5 | 23 | 5.5 | 350 | 10.5 | 875 | 15.5 | 1579 | 20.5 | 2468 | 25.5 | 3542 | 30.5 | 4801 | 35 | 6245 |
|  | 28 | 5 | 365 | 10.6 | 887 | 15.6 | 1595 | 20.6 | 2487 | 25.6 | 3565 | 30.6 | 4828 | 35 | 6276 |
|  | \％ | 5.7 | 374 | 10.7 | 900 | 15.7 | 1611 | 20.7 | 2507 | 25． 7 | 3588 | 30.7 | 4855 | 35 | 6307 |
|  | 38 | 5 | 382 | 10.8 | 12 | 15.8 | 1627 | 20.8 | 2527 | 25.8 | 3612 | 30.8 | 4882 | 35 | 6338 |
| 0.9 | 43 | 5.9 | 391 | 10.9 | 34 | 15.9 | 1643 | 20.9 | 2547 | $\because 5.9$ | 3636 | 30.9 | 4910 | 35.9 | 6369 |
| 1.0 | 48 | － |  |  |  |  | 1659 | 21.0 | 5 | 26.0 | 3659 | 31.0 | 4937 | 36. | 00 |
| 1.1 | 5 | 6.1 | 409 | 11.1 | 950 | 16. | 167 | 21.1 | 25 | $\because 6.1$ | 368 | 31. | 4964 | 36. | 31 |
| 1.2 | 59 | 6.2 | 418 | 11.2 | 96. | 16.2 | 169： | 21.2 | 260 | 26.2 | 3707 | 31. | 499 | 36 | 62 |
|  | $6 \pm$ | 6.3 | 427 | 11 | 975 | 16.3 | 1708 | 21.3 | 2627 | 26.3 | 3731 | 31. | 5020 | 36 | 94 |
|  | 69 | 6.4 | 436 | 11.4 | 95 | 16.4 | 1725 | 21.4 | 2647 | $\because 6.4$ | 3755 | 31.4 | 5047 | 36 | 6525 |
|  | 75 | 6.5 | 445 | 11.5 | 1001 | 16.5 | 1742 | 21.5 | 266 | 26.5 | 3779 | 31.5 | 507 | 36. | 556 |
|  | 81 | 6.6 | 455 | 11.6 | 1014 | 16.6 | 1758 | 21.6 | 263 | $\because 6.6$ | 380 | 31.6 | 5103 | 36. | 588 |
| 1.7 | 86 | 6.7 | 464 | 11.7 | 1027 | 16.7 | 1775 | 21.7 | 270 | 26.7 | $38: 7$ | 31.7 | 5131 | 36. | 6620 |
|  | 92 | 6.8 | 473 | 11.8 | 1040 | 16.8 | 179 | 21.8 | 272 | 26.8 | 3851 | 31. | 5159 | 36. | 6651 |
| 1.9 | 98 | 6.9 | $48:$ | 11.9 | 1053 | 16.9 | 1809 | 21.9 | 275 | 26.9 | 3876 | 31. | 5187 | 36.9 | 6683 |
|  | 104 | 7.0 | 49 |  | 1067 |  | 18.6 |  | 27.0 |  | 3900 |  | 5215 |  | 715 |
|  | 110 | 7.1 | 50 | 12.1 | 1080 | 17.1 | 1843 | 22.1 | 279 | 27.1 | 3924 | 32. | 52 | 37 | 747 |
| 2.2 | 116 | 7.2 | 512 | 12.2 | 1093 | 17.2 | 1860 | 22.2 | 281 | 27.2 | 3949 | 32.2 | 527 | 37. | 779 |
| 2.3 | 12： | 7.3 | 52 | 12.3 | 1107 | 17.3 | 1877 | 22.3 | 283 | 27.3 | 3974 | 32. | 5300 | 37. | 6811 |
|  | 128 |  | 53 | 12.4 | 112 |  | 1895 | 22.4 | 285 | 27. | 3998 | 32. | 5328 | 37 | 6843 |
|  | 134 | 7.5 | 54 |  | 113 |  | 1912 |  | 287 | 27. | 4023 | 32. | 5356 | 37 | 6875 |
|  | 141 | 7.6 | 5 | 12． | 114 |  | 1929 | 22.6 | 28 | －27．6 | 4048 |  | 538 |  | 6907 |
|  | $14 \%$ | 7. | 56 | 12.7 | 1162 |  | 1947 | 22.7 | 2917 | 27.7 | 4073 | 32. | 5414 |  | 6940 |
| 2.8 | 153 | \％ | 572 | 12.8 | 1176 | 17.8 | 1965 | 22.8 | 2939 | 27.8 | 4098 | 32. | 5442 | 37. | 6972 |
| 2.9 | 160 | 7.9 | 582 | 12.9 | 1190 | 17.9 | 198： | 22.9 | 2960 | 27.9 | 4123 | 32.9 | 5471 | 37.9 |  |
|  | 167 | 8.0 | 59 | 13.0 | 1204 | 18.0 | 2000 | 23.0 | 2981 | 28 | 4148 | 33 | 5500 | 38 | 7037 |
|  | 173 | 8． |  | 13. | 121 | 18.1 | 2018 | 23.1 | 300 | 28. | 41 | 33. | 5529 |  | 5070 |
|  | 180 | 8.2 | 613 | 13.2 | 1232 | 18.2 | 20.36 | 23.2 | 3025 | 28.2 | 4199 | 33.2 | 55． | 88． | 7102 |
|  | 187 | 8.3 | 624 | 13.3 | 1246 | 18.3 | 2054 | 23.3 | 3046 | 28.3 | 42：2 | 33.3 | 558 | 88． | 713.5 |
|  | 194 | 8.4 | 635 | 13.4 | 1261 | 18.4 | 2072 | 23.4 | 3068 | 28. | 4249 | 33. | 5616 | 38. | 168 |
| 3.5 | 201 | 8.5 | 645 | 13.5 | 1275 | 18.5 | 2090 | 23.5 | 309. | 28.5 | 4275 | 33. | 564 | 38. | 7201 |
|  | 208 | 8.6 | 656 | 13.6 | 128 | 18.6 | 210 | 23.6 | 3112 | 28.6 | 4301 | 33. | 567 | 38. | 234 |
|  | 215 | 8.7 | 66 | 13 | 1304 | 18 | 212 | 23.7 | 313 | 28 | 4326 | 33. | 570 | 38. | 7267 |
|  | 22 | 8.8 | 678 | 13.8 | 13 | 18.8 | 214 | 23.8 | 3156 | 28.8 | 4352 | 33.8 | 573 | 38. | 7300 |
| 3.9 | 230 | 8.9 | 68 | 13.9 | 13 | 18.9 | 21 | 23.9 | 31 | 28.9 |  | 33.9 | 5r | 38 | 析 |
|  | 23 | 9.0 | 700 | 14.0 | 1348 | 19.0 | 2181 | 24.0 | 3200 | 2．0 | 4404 | 34． | 5793 | 39.0 | 7367 |
| 4.1 | 244 | 9.1 | 711 | 14.1 | 1363 | 19.1 | 2200 | 24.1 | 3222 | 29.1 | 4430 | 34.1 | 5822 | 39. | 7400 |
| 4.2 | 2.92 | 9. | 722 | 14.2 | 1378 | 19.2 | 2219 | 24.2 | 3245 | 29.2 | 445 | 34.2 | 5852 | 39. | 7433 |
| 4.3 | ${ }^{260}$ | 9.3 | 734 | 14.3 | 1393 | 19.3 | 2237 | 24.3 | $3 \because 67$ | 29.3 | 4482 | 34. | 588 | 39. | 7467 |
| ． | 267 | 9.4 | 745 | 14.4 | 1408 | 19.4 | 225 | 24.4 | 3289 | 29.4 | 4508 | 34.4 | 5912 | 39.4 | 7501 |
| 4.5 | 275 | 9． | 5 | 14.5 | 1423 | 19.5 | 2275 | 24.5 | 3312 | 29.5 | 4534 | 34.5 | 5942 | 39.5 | 7534 |
| 4.6 | 283 | 9.6 | 768 | 14.6 | 1438 | 19.6 | 2294 | 24.6 | 3335 | 29.6 | 4561 | 34.6 | 5972 | 39.6 | 7508 |
|  | 291 | 9. | 780 | 14.7 | 1454 | 19.7 | 2313 | 24.7 | 3357 | 29.7 | 4587 | 34.7 | 6002 | 39.7 | 7602 |
| ， | 299 | 9 | 791 | 14.8 | 1469 | 19.8 | 2332 | 24.8 | 3380 | 29.8 | 4613 | 34.8 | 6032 | 39.8 | ¢636 |
| 4.9 | $30 \sim$ | 9.9 | 803 | 14.9 | 1484 | 19.9 | 2351 | 24.9 | 3403 | 29.9 | 4640 | 34.9 | 6062 | 39.9 | 26i0 |

TABLE NO. XXXVI.
Side Thiangles.

## cubic yards in corresponding prisms 100 feet long.

Road-bed 12 feet wide.
Side slopes 1 to 1.


Cubic yards, corresponding to differences of center heights, to be deducted when the method of averaging end sections is used.

Side Slope, 1 to 1.

| ${ }_{\text {Diff }} \mathrm{H}$. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 | Diff. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 1 |
| 2 | 2 | 3 | 3 | 3 | 4 | 4 | 4 | 5 | 5 | 5 | 2 |
| 3 | 6 | 6 | 6 | 7 | 7 | 8 | 8 | 8 | 9 | 9 | 3 |
| 4 | 10 | 10 | 11 | 11 | 12 | 13 | 13 | 14 | 14 | 15 | 4 |
| 5 | 15 | 16 | 17 | 17 | 18 | 19 | 19 | 20 | 21 | 21 | 5 |
| 6 | 22 | 23 | 24 | 25 | 25 | 26 | 27 | 28 | 29 | 29 | 6 |
| 7 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 7 |
| 8 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 8 |
| 9 | 50 | 51 | 52 | 53 | 55 | 56 | 57 | 58 | 59 | 61 | 9 |
| 10 | 62 | 63 | 64 | 65 | 67 | 68 | 69 | 71 | 72 | 73 | 10 |
| 11 | 75 | 76 | 77 | 79 | 80 | 82 | 83 | 85 | 86 | 87 | 11 |
| 12 | 89 | 90 | 92 | 93 | 95 | 96 | 98 | 100 | 101 | 103 | 12 |
| 13 | 104 | 106 | 108 | 109 | 111 | 113 | 114 | 116 | 118 | 119 | 13 |
| 14 | 121 | 123 | 124 | 126 | 128 | 130 | 132 | 133 | 135 | 137 | 14 |
| 15 | 139 | 141 | 143 | 145 | 146 | 148 | 150 | 152 | 154 | 156 | 15 |
| 16 | 158 | 160 | 162 | 164 | 166 | 168 | 170 | 172 | 174 | 176 | 16 |
| 17 | 178 | 181 | 183 | 185 | 187 | 189 | 191 | 193 | 196 | 198 | 17 |
| 18 | 200 | 202 | 204 | 207 | 209 | 211 | 214 | 216 | 218 | 221 | 18 |
| 19 | $2: 3$ | 225 | 228 | 230 | 232 | 235 | 237 | 240 | 242 | 244 | 19 |
| Dif. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 | Diff. |

TABLE NO. XXXVII.-Continued.
Cubic yards, corresponding to differences of center heights, to be deducted when the method of averaging oud sections is used.

Side Slope, $1 \frac{1}{2}$ to 1.

| Diff. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 | Diff. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 1 |
| 2 | 4 | 4 | 4 | 5 | 5 | 6 | 6 | 7 | 7 | 8 | 2 |
| 3 | 8 | 9 | 9 | 10 | 11 | 11 | 12 | 13 | 13 | 14 | 3 |
| 4 | 15 | 16 | 16 | 17 | 18 | 19 | 20 | 20 | 21 | 22 | 4 |
| 5 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 5 |
| 6 | 33 | 34 | 36 | 37 | 38 | 39 | 40 | 42 | 43 | 44 | 6 |
| 7 | 45 | 47 | 48 | 49 | 51 | 52 | 53 | 55 | 56 | 58 | 7 |
| 8 | 59 | 61 | 62 | 64 | 65 | 67 | 68 | 70 | 72 | 73 | 8 |
| 9 | 75 | 77 | 78 | 80 | 82 | 84 | 85 | 87 | 89 | 91 | 9 |
| 10 | 93 | 94 | 96 | 98 | 100 | 102 | 104 | 106 | 108 | 110 | 10 |
| 11 | 112 | 114 | 116 | 118 | 120 | 122 | 125 | 127 | 129 | 131 | 11 |
| 12 | 133 | 136 | 138 | 140 | 142 | 145 | 147 | 149 | 152 | 154 | 12 |
| 13 | 156 | 159 | 161 | 164 | 166 | 169 | 171 | 174 | 176 | 179 | 13 |
| 14 | 181 | 184 | 187 | 189 | 192 | 195 | 197 | 200 | 203 | 206 | 14 |
| 15 | 208 | 211 | 214 | 217 | 220 | 222 | 225 | 228 | 231 | 234 | 15 |
| 16 | 237 | 240 | 243 | 246 | 249 | 252 | 255 | 258 | 261 | 264 | 16 |
| 17 | 268 | 271 | 274 | 277 | 280 | 284 | 287 | 290 | 293 | 297 | 17 |
| 18 | 300 | 303 | 307 | 310 | 313 | 317 | 320 | 324 | 327 | 331 | 18 |
| 19 | 334 | 338 | 341 | 345 | 348 | 352 | 356 | 359 | 363 | 367 | 19 |
| ${ }_{\text {Ciff. }}$ C. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 | Diff. |

TABLE NO. XXXVIII.

CUBIC YARDS, IN $\frac{100}{2}$ FEET LENGTHS, FOR GIVEN AREAS.

| Area. | Cubic yards. | Area. | Cubic yards. | Area. | Cubic yards | Area. | Cubic yards. | Area. | Cubic |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 54 | 1 | 27.54 | 51 | 54.54 | 101 | 81.54 | 151 | 108.54 | 201 |
| 1.08 | 2 | 28.08 | 52 | 55.08 | 102 | 82.08 | 152 | 109.08 | 202 |
| 1.62 | 3 | 28.62 | 53 | 55.62 | 103 | 82.62 | 153 | 109.62 | 203 |
| 2.16 | 4 | 29.16 | 54 | 56.16 | 104 | 83.16 | 154 | 110.16 | 204 |
| 2.70 | 5 | 29.70 | 55 | 56.70 | 105 | 83.70 | 155 | 110.70 | 205 |
| 3.24 | 6 | 30.24 | 56 | 57.24 | 106 | 84.24 | 156 | 111.24 | 206 |
| 3.78 | 7 | 30.78 | 57 | 57.78 | 107 | 84.78 | 157 | 111.78 | 207 |
| 4.32 | 8 | 31.32 | 58 | 58.32 | 108 | 85.32 | 158 | 112.32 | 208 |
| 4.86 | 9 | 31.86 | 59 | 58.86 | 109 | 85.86 | 159 | 112.86 | 209 |
| 5.40 | 10 | 32.40 | 60 | 59.40 | 110 | 86.40 | 160 | 113.40 | 210 |
| 5.94 | 11 | 32.94 | 61 | 59.94 | 111 | 86.94 | 161 | 113.94 | 211 |
| 6.48 | 12 | 33.48 | 62 | 60.48 | 112 | 87.48 | 162 | 114.48 | 212 |
| 7.02 | 13 | 34.02 | 63 | 61.02 | 113 | 88.02 | 163 | 115.02 | 213 |
| 7.50 | 14 | 34.56 | 64 | 61.56 | 114 | 88.56 | 164 | 115.56 | 214 |
| 8.10 | 15 | 35. 10 | 65 | 62.10 | 115 | 89.10 | 165 | 116.10 | 215 |
| 8.64 | 16 | 35.64 | 66 | 62.64 | 116 | 89.64 | 166 | 116.64 | 216 |
| 9.18 | 17 | 36.18 | 67 | 63.18 | 117 | 90.18 | 167 | 117.18 | 217 |
| 9.72 | 18 | 36.72 | 63 | 63.72 | 118 | 90.72 | 168 | 117.72 | 218 |
| 10.26 | 19 | 37.26 | 69 | 64.26 | 119 | 91.26 | 169 | 118.26 | 219 |
| 10.80 | 20 | 37.80 | 70 | 64.80 | 120 | 91.80 | 170 | 118.80 | 220 |
| 11.34 | 21 | 38.34 | 71 | 65.34 | 121 | 92.34 | 171 | 119.34 | 221 |
| 11.88 | 22 | 38.88 | 72 | 65.88 | 122 | 92.88 | 172 | 119.88 | 222 |
| 12.42 | 23 | 39.42 | 73 | 66.42 | 123 | 93.42 | 173 | 120.42 | 223 |
| 12.96 | 24 | 39.96 | 74 | 66.96 | 124 | 93.96 | 174 | 120.96 | 224 |
| 13.50 | 25 | 40.50 | 75 | 67.50 | 125 | 94.50 | 175 | 121.50 | 225 |
| 14.04 | 26 | 41.04 | 76 | 68.04 | 126 | 95.04 | 176 | 122.04 | 226 |
| 14.58 | 27 | 41.58 | 77 | 68.58 | 127 | 95.58 | 177 | 122.58 | 227 |
| 15.13 | 28 | 42.12 | 78 | 69.12 | 128 | 96.12 | 178 | 123.12 | 228 |
| 15.66 | 29 | 42.66 | 79 | 69.66 | 129 | 96.66 | 179 | 123.66 | 229 |
| 16.20 | 30 | 43.20 | 80 | 70.20 | 130 | 97.20 | 180 | 124.20 | 230 |
| 16.74 | 31 | 43.74 | 81 | 70.74 | 131 | 97.74 | 181 | 124.74 | 231 |
| 17.28 | 32 | 44.28 | 82 | 71.28 | 132 | 98.28 | 182 | 125.28 | 232 |
| 17.82 | 33 | 44.82 | 83 | 71.82 | 133 | 98.82 | 183 | 125.82 | 233 |
| 18.36 | 34 | 45.36 | 84 | 72.36 | 134 | 99.36 | 184 | 126.36 | 234 |
| 18.90 | 35 | 45.90 | 85 | 72.90 | 135 | 99.90 | 185 | 126.90 | 235 |
| 19.44 | 36 | 46.44 | 86 | 73.44 | 136 | 100.44 | 186 | 127.44 | 236 |
| 19.98 | 37 | 46.98 | 87 | 73.98 | 137 | 100.98 | 187 | 127.98 | 237 |
| 20.53 | 38 | 47.52 | 88 | 74.52 | 138 | 101.52 | 188 | 128.52 | 238 |
| 21.06 | 39 | 48.06 | 89 | 75.06 | 139 | 102.06 | 189 | 129.06 | 239 |
| 21.60 | 40 | 48.60 | 90 | 75.60 | 140 | 102.60 | 190 | 129.60 | 240 |
| 22.14 | 41 | 49.14 | 91 | 76.14 | 141 | 103.14 | 191 | 130.14 | 241 |
| 22.68 | 42 | 49.68 | 92 | 76.68 | 142 | 103.68 | 192 | 130.68 | 242 |
| 23.22 | 43 | 50.22 | 93 | 77.22 | 143 | 104.22 | 193 | 131.22 | 243 |
| 23.76 | 44 | 50.76 | 94 | 77.76 | 144 | 104.76 | 194 | 131.76 | 244 |
| 24.30 | 45 | 51.30 | 95 | 78.30 | 145 | 105.30 | 195 | 132.30 | 245 |
| 24.84 | 46 | 51.84 | 96 | 78.84 | 146 | 105.84 | 196 | 132.84 | 246 |
| 25.38 | 47 | 52.38 | 97 | 79.38 | 147 | 106.38 | 197 | 133.38 | 247 |
| 25.92 | 48 | 52.92 | 98 | 79.92 | 148 | 106.92 | 198 | 133.92 | 248 |
| 26.46 | 49 | 53.46 | 99 | 80.46 | 149 | 107.46 | 199 | 134.46 | 249 |
| 27.00 | 50 | 54.00 | 100 | 81.00 | 150 | 108:00 | 200 | 135.00 | 250 |

CUBIC YARDS, IN $\frac{100}{2}$ FEET LENGTHS, FOR GIVEN AREAS.

| Area. | Cubic yards. | Area. | Cuble yards. | Area. | Cubic yards. | Area. | Cuble yards. | Area. | Cuble yards. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 135.54 | 251 | 162.54 | 301 | 189.54 | 351 | 216.54 | 401 | 243.54 | 451 |
| 136.08 | $25:$ | 163.08 | 302 | 150.08 | 352 | 217.08 | 402 | 244.08 | 45 |
| 136.62 | 2.53 | 163.62 | 303 | 190.62 | 303 | 217.62 | 403 | 244.6 | 453 |
| 137.16 | $25 \pm$ | 164.16 | 304 | 191.16 | 354 | 218.16 | 404 | 245. 16 | 454 |
| 137.70 | 255 | 164.70 | 305 | 191.70 | 355 | 218.70 | 405 | 245.70 | 455 |
| 138.24 | 256 | 165.24 | 306 | 192.24 | 356 | 219.24 | 406 | 246.24 | 456 |
| 138.78 | 257 | 165.78 | 307 | 192.78 | 357 | 219.78 | 407 | 246.78 | 457 |
| 139.32 | 258 | 166.32 | 308 | 193.32 | 358 | 220.32 | 408 | 247.32 | 458 |
| 139.86 | 259 | 166.86 | 309 | 193.86 | 359 | 220.86 | 409 | 247.86 | 459 |
| 140.40 | 260 | 167.40 | 310 | 194.40 | 360 | 221.40 | 410 | 248.40 | 460 |
| 140.94 | 261 | 167.94 | 311 | 194.94 | 361 | 221.94 | 411 | 248.94 | 461 |
| 141.48 | 262 | 168.48 | 312 | 195.48 | 362 | 222.48 | 412 | 249.48 | 462 |
| 142.02 | 263 | 169.02 | 313 | 196.02 | 363 | 223.02 | 413 | 250.02 | 463 |
| 142.56 | 264 | 169.56 | 314 | 196.56 | 364 | 223.56 | 414 | 250.56 | 464 |
| 143.10 | 265 | 170.10 | 315 | 197.10 | 365 | 224.10 | 415 | 251.10 | 465 |
| 143.64 | 266 | 170.64 | 316 | 197.64 | 366 | 224.64 | 416 | 251.64 | 466 |
| 144.18 | 267 | 171.18 | 317 | 198.18 | 367 | 225.18 | 417 | 252.18 | 467 |
| 144.72 | 268 | 171.72 | 318 | 198.72 | 368 | 225.72 | 418 | 252.72 | 468 |
| 145.26 | 269 | 172.26 | 319 | 199.26 | 369 | 226.26 | 419 | 253.26 | 463 |
| 145.80 | 270 | 172.80 | 320 | 199.80 | 370 | 226.80 | 420 | 253.80 | 470 |
| 146.34 | 271 | 173.34 | 321 | 200.34 | 371 | 227.34 | 421 | 254.34 | 471 |
| 146.88 | 272 | 173.88 | 322 | 200.88 | 372 | 227.88 | 422 | 254.88 | 472 |
| 147.42 | 273 | 174.42 | 323 | 201.42 | 373 | 228.42 | 423 | 255.42 | 473 |
| 147.96 | 274 | 174.96 | 324 | 201.96 | 374 | 228.96 | 424 | 255.96 | 474 |
| 148.50 | 275 | 175.50 | 325 | 202.50 | 375 | 229.50 | 425 | 256.50 | 475 |
| 149.04 | 276 | 176.04 | 326 | 203.04 | 376 | 230.04 | 426 | 257.04 | 476 |
| 149.58 | 277 | 176.58 | 327 | 203.58 | 377 | 230.58 | 427 | 257.58 | 477 |
| 150.12 | 278 | 177.12 | 328 | 204.12 | 378 | 231.12 | 428 | 258.12 | 478 |
| 150.66 | 279 | 177.66 | 329 | 204.66 | 379 | 231.66 | 429 | 258.66 | 479 |
| 151.20 | 280 | 178.20 | 330 | 205.20 | 380 | 232.20 | 430 | 259.20 | 480 |
| 151.74 | 281 | 178.74 | 331 | 205.74 | 381 | 232.74 | 431 | 259.74 | 481 |
| 152.28 | 282 | 179.28 | 332 | 206.28 | 382 | 233.28 | 432 | 260.28 | 482 |
| 152.82 | 283 | 179.82 | 333 | 206.82 | 383 | 233.82 | 433 | 260.82 | 483 |
| 153.36 | 284 | 180.36 | 334 | 207.36 | 384 | 234.36 | 434 | 261.36 | 484 |
| 103.90 | 285 | 180.90 | 335 | 207.90 | 385 | 234.90 | 435 | 261.90 | 485 |
| 154.44 | $2 \times 6$ | 181.44 | 3336 | 208.44 | 386 | 235.44 | 436 | 262.44 | 486 |
| 154.98 | 287 | 181.98 | 337 | 208.98 | 387 | 235.98 | 437 | 262.98 | 487 |
| 155.52 | 288 | 182.52 | 338 | 209.52 | 388 | 236.52 | 438 | 263.52 | 488 |
| 156.06 | 289 | 183.06 | 339 | 210.06 | 389 | 237.06 | 439 | 264.06 | 489 |
| 156.60 | 290 | 183.60 | 340 | 210.60 | 390 | 237.60 | 440 | 264.60 | 490 |
| 157.14 | 291 | 184.14 | 341 | 211.14 | 391 | 238.14 | 441 | 265.14 | 491 |
| 157.68 | 292 | 184.68 | 342 | 211.68 | 392 | 238.68 | 442 | 265.68 | 492 |
| 158.22 | 293 | 185.22 | 343 | 212.22 | 393 | 239.22 | 443 | 266.22 | 493 |
| 158.76 | 294. | 185.76 | 344 | 212.76 | 394 | 239.76 | 444 | 266.76 | 494 |
| 159.30 | 295 | 186.30 | 345 | 213.30 | 395 | 240.30 | 445 | 267.30 | 495 |
| 159.84 | 296 | 186.84 | 346 | 213.84 | 396 | 240.84 | 446 | 267.84 | 496 |
| 160.38 | 297 | 187.38 | 347 | 214.38 | 397 | 241.38 | 447 | 268.38 | 497 |
| 160.92 | 298 | 187.92 | 348 | 214.92 | 398 | 241.92 | 448 | 268.92 | 498 |
| 161.46 | 299 | 188.46 | 349 | 215.46 | 399 | 242.46 | 449 | 269.46 | 499 |
| 162.00 | 300 | 189.00 | 350 | 216.00 | 400 | 243.00 | 450 | 270.00 | 500 |

TABLE NO. XXXVIII.-Continued.

CUBIC yards, in $\frac{100}{2}$ FEET LENGTHS, FOR GIVEN AREAS.

| Area. | Cubic yards. | Area. | Cubic yards. | Area. | Cubic yards. | Area. | Cubic yards. | Area. | Cubic yards. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 270.54 | 501 | 297.54 | 551 | 324.54 | 601 | 351.54 | 651 | 378.54 | 701 |
| 271.08 | 502 | 298.08 | 552 | 325.08 | 602 | 352.08 | 652 | 379.08 | 702 |
| 271.62 | 503 | 298.62 | 553 | 325.62 | 603 | 352.62 | 653 | 379.62 | 703 |
| 272.16 | 504 | 299.16 | 554 | 326.16 | 604 | 353.16 | 654 | 380.16 | 704 |
| 272.70 | 505 | 299.70 | 555 | 326.70 | 605 | 353.70 | 655 | 380.70 | 705 |
| 273.24 | 506 | 300.24 | 556 | 327.24 | 606 | 354.24 | 656 | 381.24 | 706 |
| 273.78 | 507 | 300.78 | 557 | 327.78 | 607 | 354.78 | 657 | 381.78 | 707 |
| 274.32 | 508 | 301.32 | 558 | 328.32 | 608 | 355.32 | 658 | 382.32 | 708 |
| 274.86 | 509 | 301.86 | 559 | 328.86 | 609 | 355.86 | 659 | 382.86 | 709 |
| 275.40 | 510 | 302.40 | 560 | 329.40 | 610 | 356.40 | 660 | 383.40 | 710 |
| 275.94 | 511 | 302.94 | 561 | 329.94 | 611 | 350.94 | 661 | 383.94 | 711 |
| 276.48 | 512 | 303.48 | 562 | 330.48 | 612 | 357.48 | 662 | 384.48 | 712 |
| 277.02 | 513 | 304.02 | 563 | 331.02 | 613 | 358.02 | 663 | 385.02 | 713 |
| 277.56 | 514 | 304.56 | 564 | 331.56 | 614 | 358.56 | 664 | 385.56 | 714 |
| 278.10 | 515 | 305.10 | 565 | 332.10 | 615 | 359.10 | 665 | 386.10 | 715 |
| 278.64 | 516 | 30.). 64 | 566 | 332.64 | 616 | 359.64 | 666 | 386.64 | 716 |
| 279.18 | 517 | 306.18 | 567 | 333.18 | 617 | 360.18 | 667 | 387.18 | 717 |
| 279.72 | 518 | 306.72 | 568 | 333.72 | 618 | 360.72 | 668 | 387.72 | 718 |
| 280.26 | 519 | 307.26 | 569 | 334.26 | 619 | 361.26 | 669 | 388.26 | 719 |
| 280.80 | 520 | 307.80 | 570 | 334.80 | 620 | 361.80 | 670 | 388.80 | 720 |
| 281.34 | 521 | 308.34 | 571 | 335.34 | 621 | 362.34 | 671 | 389.34 | 721 |
| 281.88 | 522 | 308.88 | 572 | 335.88 | 622 | 362.88 | 672 | 389.88 | $72 \%$ |
| 282.42 | 523 | 309.42 | 573 | 33642 | 623 | 363.42 | 673 | 390.42 | 723 |
| 282.96 | 524 | 309.96 | 574 | 336.96 | 624 | 363.96 | 674 | 390.96 | 724 |
| 283.50 | 525 | 310.50 | 575 | 337.50 | 625 | 364.50 | 675 | 391.50 | 725 |
| 284.04 | 526 | 311.04 | 576 | 338.04 | 626 | 365.04 | 676 | 392.04 | 726 |
| 284.58 | 527 | 311.58 | 577 | 338.58 | 627 | 365.58 | 677 | 392.58 | 727 |
| 285.12 | 528 | 312.12 | 578 | 339.12 | 628 | 366.12 | 678 | 393.12 | 728 |
| 285.66 | 529 | 312.66 | 579 | 339.66 | 629 | 366.66 | 679 | 393.66 | 729 |
| 286.20 | 530 | 313.20 | 580 | 340.20 | 630 | 367.20 | 680 | 394.20 | 730 |
| 286.74 | 531 | 313.74 | 581 | 340.74 | 631 | 367.74 | 681 | 394.74 | 731 |
| 287.28 | 532 | 31.4 .28 | 582 | 341.28 | 632 | 368.28 | 682 | 395.28 | 732 |
| 287.83 | 533 | 314.82 | 583 | 341.82 | 633 | 368.82 | 683 | 395.82 | 733 |
| 288.36 | 534 | 315.36 | 584 | 342.36 | 634 | 369.36 | 684 | 396.36 | 734 |
| 288.90 | 535 | 315.90 | 585 | 342.90 | 635 | 369.90 | 685 | 396.90 | 735 |
| 289.44 | 536 | 316.44 | 586 | 343.44 | 636 | 370.44 | 686 | 397.44 | 736 |
| 289.98 | 537 | 316.98 | 587 | 343.98 | 637 | 370.98 | 687 | 397.98 | 737 |
| 290.52 | 538 | 317.52 | 588 | 344.52 | 638 | 371.52 | 688 | 398.52 | 738 |
| 291.06 | 539 | 318.06 | 589 | 345.06 | 639 | 372.06 | 689 | 399.06 | 739 |
| 291.60 | 540 | 318.60 | 590 | 345.60 | 640 | 372.60 | 690 | 399.60 | 740 |
| 292.14 | 541 | 319.14 | 591 | 346.14 | 641 | 373.14 | 691 | 400.14 | 741 |
| 292.68 | 542 | 319.68 | 592 | 346.68 | 642 | 373.68 | 692 | 400.68 | 742 |
| 293.22 | 543 | 320.22 | 593 | 347.22 | 643 | 374.22 | 693 | 401.22 | 743 |
| 293.76 | 544 | 320.76 | 594 | 347.76 | 644 | 374.76 | 694 | 401.76 | 744 |
| 294.30 | 545 | 321.30 | 595 | 348.30 | 645 | 375.30 | 695 | 402.30 | 745 |
| 294.84 | 546 | 321.84 | 596 | 348.84 | 646 | 375.84 | 696 | 402.84 | 746 |
| 295.38 | 547 | 322.38 | 597 | 349.38 | 647 | 376.38 | 697 | 403.38 | 747 |
| 295.92 | 548 | 322.92 | 598 | 349.92 | 648 | 376.92 | 698 | 403.92 | 748 |
| 296.46 | 549 | 323.46 | 599 | 350.46 | 649 | 377.46 | 699 | 404.46 | 749 |
| 297.00 | 550 | 324.00 | 600 | 351.00 | 650 | 378.00 | 700 | 405.00 | 750 |

TABLE NO. XXXVIII.-Continued.

CUBIC FARDS, IN 100 FEET LENGTHS, FOR GIVEN AREAS.

| Area. | Cubic yards | Area. | Cuble yards | drea | Cubic | Area. | Cuble yards. | Area. | Cuble yards. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 405.54 | 751 | 432.54 | 801 | 459.54 | 851 | 486.54 | 901 | 513.54 | 951 |
| 406.08 | 752 | 433.08 | 802 | 450.08 | 852 | 487.08 | 902 | 514.08 | 952 |
| 406.62 | 753 | 433.62 | 803 | 460.62 | 853 | 487.62 | 903 | 514.62 | 953 |
| 407.16 | 754 | 434.16 | 804 | 461.16 | 854 | 488.16 | 904 | 515.16 | 954 |
| 407.70 | 755 | 434.70 | 805 | 461.70 | 855 | 488.70 | 905 | 515.70 | 955 |
| 408.24 | 756 | 435.24 | 806 | 462.24 | 856 | 489.24 | 906 | 516.24 | 956 |
| 408.78 | 757 | 435.78 | 807 | 462.78 | 857 | 489.78 | 907 | 516.78 | 957 |
| 409.32 | 758 | 436.32 | 808 | 463.32 | 858 | 490.32 | 908 | 517.32 | 958 |
| 409.86 | 759 | 436.86 | 809 | 463.86 | 859 | 490.86 | 909 | 517.86 | 959 |
| 410.40 | 760 | 437.40 | 810 | 464.40 | 860 | 491.40 | 910 | 518.40 | 960 |
| 410.94 | 761 | 437.94 | 811 | 464.94 | 861 | 491.94 | 911 | 518.94 | 961 |
| 411.48 | 762 | 438.48 | 812 | 465.48 | 862 | 492.48 | 912 | 519.48 | 962 |
| 412.02 | 763 | 439.02 | 813 | 466.02 | 863 | 493.02 | 913 | 520.02 | 963 |
| 412.56 | 764 | 439.56 | 814 | 466.56 | 864 | 493.56 | 914 | 520.56 | 964 |
| 413.10 | 765 | 440.10 | 815 | 467.10 | 865 | 494.10 | 915 | 521.10 | 965 |
| 413.64 | 766 | 440.64 | 816 | 467.64 | 866 | 494.64 | 916 | 521.64 | 966 |
| 414.18 | 767 | 441.18 | 817 | 468.18 | 867 | 495.18 | 917 | 522.18 | 967 |
| 414.72 | 768 | 441.72 | 818 | 468.72 | 868 | 495.72 | 918 | 522.72 | 968 |
| 415.26 | 769 | 442.26 | 819 | 469.26 | 869 | 496.26 | 919 | 523.26 | 969 |
| 415.80 | 770 | 442.80 | 820 | 469.80 | 870 | 496.80 | 920 | 523.80 | 970 |
| 416.34 | 771 | 443.34 | 821 | 470.34 | 871 | 497.34 | 921 | 524.34 | 971 |
| 416.88 | 772 | 443.88 | 822 | 470.88 | 872 | 497.88 | 922 | 524.88 | 972 |
| 417.42 | 773 | 444.42 | 823 | 471.42 | 873 | 498.42 | 923 | 525.42 | 973 |
| 417.96 | 774 | 444.96 | 824 | 471.96 | 874 | 498.96 | 924 | 525.96 | 974 |
| 418.50 | 775 | 445.50 | 825 | 472.50 | 875 | 499.50 | 925 | 526.50 | 975 |
| 419.04 | 776 | 446.04 | 826 | 473.04 | 876 | 500.04 | 926 | 527.04 | 976 |
| 419.58 | 777 | 446.58 | 827 | 473.58 | 877 | 500.58 | 927 | 527.58 | 977 |
| 420.12 | 778 | 447.12 | 828 | 474.12 | 878 | 501.12 | 928 | 528.12 | 978 |
| 420.66 | 779 | 447.66 | 829 | 474.66 | 879 | 501.66 | 929 | 528.66 | 979 |
| 421.20 | 780 | 448.20 | 830 | 475.20 | 880 | 502.20 | 930 | 529.20 | 980 |
| 421.74 | 781 | 448.74 | 831 | 475.74 | 881 | 502.74 | 931 | 529.74 | 981 |
| 422.28 | 782 | 449.28 | 832 | 476.28 | 882 | 503.28 | 932 | 530.28 | 982 |
| 422.82 | 783 | 449.82 | 833 | 476.82 | 883 | 503.82 | 933 | 530.82 | 983 |
| 423.36 | 784 | 450.36 | 834 | 477.36 | 884 | 504.36 | 934 | 531.36 | 984 |
| 423.90 | 785 | 450.90 | 835 | 477.90 | 885 | 50490 | 935 | 531.90 | 985 |
| 424.44 | 786 | 451.44 | 836 | 478.44 | 886 | 505.44 | 936 | 532.44 | 986 |
| 424.98 | 787 | 451.98 | 837 | 478.98 | 887 | 505.98 | 937 | 532.98 | 987 |
| 425.52 | 788 | 452.52 | 838 | 479.52 | 888 | 506.52 | 938 | 533.52 | 988 |
| 426.06 | 789 | 453.06 | 839 | 480.06 | 889 | 507.06 | 939 | 534.06 | 989 |
| 426.60 | 790 | 453.60 | 840 | 480.60 | 890 | 507.60 | 940 | 534.60 | 990 |
| 427.14 | 791 | 454.14 | 841 | 481.14 | 891 | 508.14 | 941 | 535.14 | 991 |
| 427.68 | 792 | 454.68 | 842 | 481.68 | 892 | 508.68 | 942 | 535.68 | 992 |
| 428.22 | 793 | 455.22 | 843 | 482.22 | 893 | 509.22 | 943 | 536.22 | 993 |
| 428.76 | 794 | 455.76 | 844 | 482.76 | 894 | 509.76 | 944 | 536.76 | 994 |
| 429.30 | 795 | 456.30 | 845 | 483.30 | 895 | 510.30 | 945 | 537.30 | 995 |
| 429.84 | 796 | 45.84 | 846 | 483.84 | 896 | 510.84 | 946 | 537.84 | 996 |
| 430.38 | 797 | 457.38 | 847 | 484.38 | 897 | 511.38 | 947 | 538.38 | 997 |
| 430.92 | 798 | 457.92 | 848 | 484.92 | 898 | 511.92 | 948 | 538.92 | 998 |
| 431.46 | 799 | 458.46 | 849 | 485.46 | 899 | 512.46 | 949 | 539.46 | 999 |
| 432.00 | 800 | 459.00 | 850 | 486.00 | 900 | 513.00 | 950 | 540.00 | 1000 |

## TABLE NO. XXXIX.

CUBIC YARDS, IN $\frac{100}{12}$ FEET LENGTHS, FOR GIVEN AREAS.

| Area. | Cubic yards. | Area. | Cubic yards. | Area. | Cubic yards. | Area. | Cubic yards. | Area. | $\underset{\text { Cubic }}{\text { yards. }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3.24 | 1 | 165.24 | 51 | 327.24 | 101 | 489.24 | 151 | 651.24 | 201 |
| 6.48 | 2 | 168.48 | 52 | 330.48 | 102 | 492. 48 | 152 | 6.74 .48 | 202 |
| 9.70 | 3 | 171.72 | 53 | 333.7 | 103 | 49.5 .72 | 153 | 657.72 | 203 |
| 12.96 | 4 | 174.96 | 54 | 336.96 | 104 | 498.96 | 154 | 660.96 | 204 |
| 16.20 | 5 | 178.20 | 55 | 340.20 | 105 | 502.20 | 155 | 664.20 | 205 |
| 19.44 | 6 | 181.44 | 56 | 343.44 | 106 | 505.44 | 156 | 667.44 | 206 |
| 23.68 | 7 | 184.68 | 57 | 346.68 | 107 | 508.68 | 157 | 670.68 | 207 |
| 25.92 | 8 | 187.92 | 58 | 349.92 | 108 | 511.92 | 158 | 673.93 | 208 |
| 29.16 | 9 | 191.16 | 59 | 353.16 | 109 | 515.16 | 159 | 677.16 | 209 |
| $3 \pm .40$ | 10 | 194.40 | 60 | 356.40 | 110 | 518.40 | 160 | 680.40 | 210 |
| 35.64 | 11 | 197.64 | 61 | 359.64 | 111 | 521.64 | 161 | 683.64 | 211 |
| 38.88 | 12 | 200.88 | 62 | 362.88 | 112 | 524.88 | 163 | 686.88 | 212 |
| 42.12 | 13 | 204.12 | 63 | 366.12 | 113 | 528.12 | 163 | 690.12 | 213 |
| 45.36 | 14 | 207.36 | 64 | 369.36 | 114 | 531.36 | 164 | 693.36 | 214 |
| 48.60 | 15 | 210.60 | 65 | 372.60 | 115 | 534.60 | 16.) | 696.60 | 215 |
| 51.84 | 16 | 213.84 | 66 | 375.84 | 116 | 537.84 | 166 | 699.84 | 216 |
| 55.08 | 17 | 217.08 | 67 | 379.08 | 117 | 541.08 | 167 | 703.08 | 217 |
| 58.32 | 18 | 220.32 | $6 \times$ | 382.32 | 118 | 544.32 | 168 | 706.32 | 218 |
| 61.56 | 19 | 223.56 | 69 | 385.56 | 119 | 547.56 | 169 | 709.56 | 219 |
| 64.80 | 20 | 226.80 | 70 | 338.80 | 120 | 550.80 | 170 | 712.80 | 220 |
| 68.04 | 21 | 230.04 | 71 | 392.04 | 121 | 554.04 | 171 | 716.04 | 221 |
| 71.28 | 22 | 233.28 | 72 | 395.28 | 122 | 55728 | 172 | 719.28 | 222 |
| 74.52 | 23 | 236.52 | 73 | 398.52 | 123 | 560.52 | 173 | 722.52 | 223 |
| 77.76 | 24 | 239.76 | 74 | 401.76 | 124 | 563.76 | 174 | 725.76 | 224 |
| 81.00 | 25 | 243.00 | 75 | 405.00 | 125 | 567.00 | 175 | 729.00 | 225 |
| 84.24 | 26 | 246.24 | 76 | 408.24 | 126 | 570.24 | 176 | 732.24 | 226 |
| 87.48 | 27 | 249.48 | 77 | 411.48 | 127 | 573.48 | 177 | 735.48 | 227 |
| 90.72 | 28 | 252.72 | 78 | 414.72 | 128 | 576.72 | 178 | 738.72 | 228 |
| 93.96 | 29 | 255.96 | 79 | 417.96 | 129 | 579.96 | 179 | 741.96 | 229 |
| 97.20 | 30 | 259.20 | 80 | 421.20 | 130 | 583.20 | 180 | 745.20 | 230 |
| 100.44 | 31 | 262.44 | 81 | 424.44 | 131 | 586.44 | 181 | 748.44 | 231 |
| 103.68 | 32 | 265.68 | 82 | 497.68 | 132 | 589.68 | 182 | 751.68 | 232 |
| 106.92 | 33 | 268.92 | 83 | 430.93 | 133 | 592.92 | 183 | 754.92 | 233 |
| 110.16 | 34 | 272.16 | 84 | 434.16 | 134 | 596.16 | 184 | 758.16 | 234 |
| 113.40 | 35 | 275.40 | 85 | 437.40 | 135 | 599.40 | 185 | 761.40 | 235 |
| 116.64 | 36 | 278.64 | 86 | 440.64 | 136 | 602. 64 | 186 | 764.64 | 236 |
| 119.88 | 37 | 281.88 | 87 | 443.88 | 137 | 605.88 | 187 | 767.88 | 237 |
| 123.12 | 38 | 285.12 | 88 | 447.12 | 138 | 609.12 | 188 | 771.12 | 238 |
| 126.36 | 39 | 288.36 | 89 | 450.36 | 139 | 612.36 | 189 | 774.36 | 239 |
| 129.60 | 40 | 291.60 | 90 | 453.60 | 140 | 615.60 | 190 | 777.60 | 240 |
| 132.84 | 41 | 294.84 | 91 | 456.84 | 141 | 618.84 | 191 | 780.84 | 241 |
| 136.08 | 42 | 298.08 | 92 | 460.08 | 142 | 622.08 | 192 | 784.08 | 242 |
| 139.32 | 43 | 301.32 | 93 | 463.32 | 143 | 625. 32 | 193 | 787.32 | 243 |
| 142.56 | 44 | 304.56 | 94 | 466.56 | 144 | 628.56 | 194 | 790.56 | 244 |
| 145.80 | 45 | 307.80 | 95 | 469.80 | 145 | 631.80 | 195 | 「93.80 | 24.5 |
| 149.04 | 46 | 311.04 | 96 | 473.04 | 146 | 635.04 | 196 | 797.04 | 246 |
| 152.28 | 47 | 314.28 | 97 | 476.28 | 147 | 638.28 | 197 | 800.28 | 247 |
| 155.52 | 48 | 317.52 | 98 | 479.52 | 148 | 641.52 | 198 | 803.52 | 248 |
| 158.76 | 49 | 320.76 | 99 | 482.76 | 149 | 644.76 | 199 | 806.76 | 249 |
| 162.00 | 50 | 324.00 | 100 | 486.00 | 150 | 648.00 | 200 | 81000 | 250 |

TABLE NO. XXXIX. - Continued.

CUBIC FARDS, IN $\frac{100}{12}$ FEET LENGTHS, FOR GIVEN AREAS.

| Area. | Cuble yards. | Area | Cuble yards. | Area. | Cuble yards. | Area. | Cubic yards. | Area | Cubic yards. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 813.24 | 251 | $9 \% 5.24$ | 301 | 1137.24 | 351 | 1299.24 | 401 | 1461.24 | 4.51 |
| 816.48 | 25: | 978.48 | 302 | 1189.48 | $35 \sim$ | 1302.48 | 402 | 1464.48 | $45 \cdot 3$ |
| 819.72 | 253 | 981.72 | 303 | 1143.72 | 353 | 1305.72 | 403 | 1467. 72 | 453 |
| 822.96 | $25 \pm$ | 984.96 | 304 | 1146.96 | 35 - | 1308.96 | 404 | 14:0.96 | 4.15 |
| 826.20 | 255 | 988.20 | 305 | 1150.20 | 35) | 1312. 20 | 405 | 1474.20) | 45.) |
| 829.44 | 256 | 991.44 | 306 | 1153.44 | 3 ¢5 | 1315.44 | 406 | 147\%.44 | 456 |
| 832.68 | 257 | 994.68 | 307 | 1156.68 | 357 | 1318.68 | 407 | 1480.68 | 4.97 |
| 835.92 | 258 | 997.92 | 308 | 1159.92 | 358 | 1321.92 | 408 | 1483.92 | 4.58 |
| 839.16 | 259 | 1001.16 | 309 | 1163.16 | 359 | 1325.16 | 409 | 1487.16 | 4.99 |
| 842.40 | 260 | 1004.40 | 310 | 1166.40 | 360 | 1328.40 | 410 | 1490.40 | 460 |
| 845.64 | 261 | 1007.64 | 311 | 1169.64 | 361 | 1331.64 | 411 | 1493.64 | 461 |
| 848.88 | 262 | 1010.88 | 312 | 1172.88 | 362 | 1334.88 | 412 | 1496.88 | 462 |
| 855.12 | 263 | 1014.12 | 313 | 1176.12 | 363 | 1338.12 | 413 | 1500.12 | 463 |
| 85 วิ. 36 | 264 | 1017.36 | 314 | 1179.36 | 364 | 1341.36 | 414 | 1503.36 | 464 |
| 8 858.60 | 265 | 1020.60 | 315 | 118:.60 | 365 | 1344.60 | 415 | 1506.60 | 465 |
| 861.84 | 266 | 1023.84 | 316 | 1185.84 | 366 | 1347.84 | 416 | 1509.84 | 466 |
| 865.08 | 267 | 1027.08 | 317 | 1189.08 | 367 | 13.51 .08 | 417 | 1513.08 | 467 |
| 868.32 | 268 | 1030.33 | 318 | 1192. 32 | 368 | 1354.32 | 418 | 1516.82 | 468 |
| 871.56 | 269 | 1033.56 | 319 | 1195.56 | 369 | 1357.56 | 419 | 1519.56 | 469 |
| 874.80 | 270 | 1036.80 | 320 | 1198.80 | 370 | 1360.80 | 420 | 1522.80 | 470 |
| 878.04 | 271 | 1040.04 | 321 | 1202.04 | 371 | 1364.04 | 421 | 1526.04 | 471 |
| 881.28 | 272 | 1043.28 | 322 | 1205.28 | 37. | 1367.28 | 42:3 | 1529.28 | 472 |
| 884.52 | 273 | 1046.52 | 323 | 1208.52 | 373 | $13 \% 52$ | 423 | 1232.52 | 473 |
| 887.76 | 274 | 1049.76 | $3 \because 4$ | 1211.76 | 374 | 1373.76 | 424 | 1535. 76 | 474 |
| 891.00 | 275 | 1053.00 | 325 | 1215.00 | 375 | 1377.00 | 425 | 1539.00 | 475 |
| 894.24 | 276 | 1056.24 | 326 | 1218.24 | 376 | 1380.24 | 426 | 1542.24 | 476 |
| 897.48 | 277 | 1059.48 | 327 | 1221.48 | 377 | 1383.48 | 427 | 1545. 48 | 477 |
| 900.72 | 278 | 1062.72 | 328 | 1224.72 | 378 | 1386.72 | 428 | 1548.72 | 478 |
| 903.96 | 279 | 1065.96 | 329 | 12.7 .96 | 379 | 1389.96 | 429 | 1551.96 | 479 |
| 907.20 | 280 | 1069.20 | 330 | 1231.20 | 380 | 1393.20 | 430 | 1555.20 | 480 |
| 910.44 | 281 | $10 \% 2.44$ | 331 | 1234.44 | 381 | 1396.44 | 431 | 1558.44 | 481 |
| 913.68 | 282 | 1075.68 | 332 | 1237.68 | 382 | 1399.68 | 432 | 1561.68 | 482 |
| 916.92 | 283 | 1078.92 | 333 | 1240.92 | 383 | 1402.92 | 433 | 1564.92 | 483 |
| 9:0.16 | 284 | 1082. 16 | 334 | 1244.16 | 384 | 1406.16 | 434 | 1568.16 | 484 |
| 923.40 | 28.5 | 1085.40 | 335 | 1247.40 | 385 | 1409.40 | 435 | 1571.40 | 485 |
| 926.64 | $2 \times 6$ | 1088.64 | 3:36 | 1250.64 | 386 | 1412.64 | 436 | $15 \% 4.64$ | 486 |
| 929.88 | 287 | 1091.88 | 337 | 1253.88 | 387 | 1415.88 | 437 | 1577.88 | 487 |
| 9333.12 | $2 \times 8$ | 1095.12 | 338 | 1257.12 | 388 | 1419.12 | 438 | 1581.12 | 488 |
| 9:36.36 | 289 | 1098.36 | 339 | 1260.36 | 389 | 1422.36 | 439 | 1584.36 | 489 |
| 939.60 | 290 | 1101.60 | 340 | 1263.60 | 390 | 1425.60 | 440 | 1587.60 | 490 |
| 942.84 | 291 | 1104.84 | 341 | 1266.84 | 391 | 1428.84 | 441 | 1590.84 | 491 |
| 946.08 | 292 | 1108.08 | 342 | 1270.08 | 392 | 1432.08 | 442 | 1594.08 | 492 |
| 949.32 | 293 | 1111.32 | 343 | 1273.32 | 393 | 143.). 32 | 443 | 1597.32 | 493 |
| 952.56 | 294 | 1114.56 | 344 | 1276.56 | 394 | 1438.56 | 444 | 1600.56 | 494 |
| 955.80 | 29.5 | 1117.80 | 345 | 1279.80 | 395 | 1441.80 | 44.5 | 1603.80 | 495 |
| 959.04 | 296 | 1121.04 | 346 | 1283.04 | 396 | 1445.04 | 446 | 1607.04 | 496 |
| 962.28 | 297 | 1124.28 | 347 | 1286.28 | 397 | 1448.28 | 447 | 1610.28 | 497 |
| 965.52 | 298 | 1127.52 | 348 | 1289.52 | 398 | 1451.52 | 448 | 1613.52 | 498 |
| 968.76 | 299 | 1130.76 | 349 | 1292.76 | 399 | 1454.76 | 449 | 1616.76 | 499 |
| 972.00 | 300 | 1134.00 | 350 | 1296.00 | 40.5 | 1458.00 | 450 | 1620.00 | 500 |

TABLE NO. XXXIX.-Continued.

CUBIC YARDS, IN $\frac{100}{12}$ FEET LENGTHS, FOR GIVEN AREAS.

| Area. | Cubic yards. | Area. | Cubic yards. | Area. | Cubic yards. | Area. | Cubic yards. | Area. | Cubic yards. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1623.24 | 501 | 1785.24 | 551 | 1947.24 | 601 | 2109.24 | 651 | 2271.24 | 701 |
| 1626.48 | 502 | 1788.48 | 552 | 1950.48 | 602 | 2112.48 | 652 | 2274.48 | \%02 |
| $1629.7{ }^{\text {2 }}$ | 503 | 1791.72 | 553 | 1953.72 | 603 | 2115.72 | 653 | 2277.72 | 70:3 |
| 1632.96 | 504 | 1794.96 | 554 | 19.56 .96 | 604 | 2118.96 | 654 | 2280.96 | \%04 |
| 1636.20 | 50.5 | 1798.20 | 555 | 1960.20 | 605 | 2122.20 | 655 | 2284.20 | r05 |
| 1639.44 | 506 | 1801.44 | 556 | 1963.44 | 606 | 2125.44 | 656 | 2287.44 | 706 |
| 1642.68 | 507 | 1804.68 | $55 \%$ | 1966.68 | 607 | 2128.68 | 657 | 2290.68 | 707 |
| 1645.92 | 508 | 1807.92 | 558 | 1969.92 | 608 | 2131.92 | 658 | 2293.92 | 708 |
| 1649.16 | 509 | 1811.16 | 559 | 1973.16 | 609 | 2135.16 | 6.99 | 2297.16 | 709 |
| $165 \pm .40$ | 510 | 1814.40 | 560 | 1976.40 | 610 | 2138.40 | 660 | 2300.40 | 710 |
| 1655.64 | 511 | 1817.64 | 561 | 1979.64 | 611 | 2141. C4 | 661 | 2303.64 | 711 |
| 1658.88 | 512 | 1820.88 | 562 | 1982.88 | 612 | 2144.88 | 662 | 2306.88 | 712 |
| 1662.12 | 513 | 1824.12 | 563 | 1986.12 | 613 | 2148.12 | 663 | 2310.12 | 713 |
| 1665.36 | 514 | 1827.36 | 564 | 1989.36 | 614 | 2151.36 | 664 | 2313.36 | 714 |
| 1668.60 | 515 | 1830.60 | 565 | 1992.60 | 615 | 2154.60 | 665 | 2316.60 | 715 |
| 1671.84 | 516 | 1833.84 | 566 | 1995.84 | 616 | 2157.84 | 666 | 2319.84 | 716 |
| 1675.08 | 517 | 1837.08 | 567 | 1999.08 | 617 | 2161.08 | 667 | 2323. 08 | 717 |
| 1678.32 | 518 | 1840.32 | 568 | 2002.32 | 618 | -2164.32 | 668 | 2326.32 | 718 |
| 1681.56 | 519 | 1843.56 | 569 | 2005.56 | 619 | 2167.56 | 669 | 2329.56 | 719 |
| 1684.80 | 520 | 1846.80 | 570 | 2008.80 | 620 | 2170.80 | 670 | 2332.80 | 720 |
| 1688.04 | 521 | 1850.04 | 571 | 2012.04 | 621 | 2174.04 | 671 | 2336.04 | 721 |
| 1691.28 | 522 | 1853.28 | 572 | 2015.28 | 622 | 2177.28 | 672 | 2339.28 | 722 |
| 1694.52 | 523 | 1856.52 | 573 | 2018.52 | 623 | 2180.52 | 673 | 2342.52 | 723 |
| 1697.76 | 524 | 1859.76 | 574 | 2021.76 | 624 | 2183.76 | 674 | 2345.76 | 724 |
| 1701.00 | 525 | 1863.00 | 575 | 2025.00 | 625 | 2187.00 | 675 | 2349.00 | 795 |
| 1704.24 | 526 | 1866.24 | 576 | 2028.24 | 626 | 2190.24 | 676 | 2352. 24 | 726 |
| 1707.48 | 527 | 1869.48 | 577 | 2031.48 | 627 | 2193.48 | 677 | 2355.48 | 727 |
| 1710.72 | 528 | 1872.72 | 578 | 2034.72 | 628 | 2196.72 | 678 | 2358.72 | 728 |
| 1713.96 | 529 | 1875.96 | 579 | 2037.96 | 629 | 2199.96 | 679 | 2361.96 | 729 |
| 1717.20 | 530 | 1879.20 | 580 | 2041.20 | 630 | 2203.20 | 680 | 2365.20 | 730 |
| 1720.44 | 531 | 1882.44 | 581 | 2044.44 | 631 | 2206.44 | 681 | 2368.44 | 731 |
| 1723.68 | 532 | 1885.68 | 582 | 2047.68 | 632 | 2209.68 | 682 | 2371.68 | 732 |
| 1726.92 | 533 | 1888.92 | 583 | 2050.92 | 633 | 2212.92 | 683 | 2374.92 | 733 |
| 1730.16 | 534 | 1892.16 | 584 | 20.54 .16 | 634 | 2216.16 | 684 | 2378.16 | 734 |
| 1733.40 | 535 | 1895.40 | 585 | 2057.40 | 635 | 2219.40 | 685 | 2381.40 | 735 |
| 1736.64 | 536 | 1898.64 | 586 | 2060.64 | 636 | 2222.64 | 686 | 2384.64 | 736 |
| 1739.88 | 537 | 1901.88 | 587 | 2063.88 | 637 | 2225.88 | 687 | 2387.88 | 737 |
| 1743.12 | 538 | 1905.12 | 588 | 2067.12 | 638 | 2229.12 | 688 | 2391.12 | r38 |
| 1746.36 | 539 | 1908.36 | 589 | 2070.36 | 639 | 2232.36 | 689 | 2394.36 | r39 |
| 1749.60 | 540 | 1911.60 | 590 | $20 \% 3.60$ | 640 | 2235.60 | 690 | 2397.60 | 740 |
| 1752.84 | 541 | 1914.84 | 591 | 2076.84 | 641 | 2238.84 | 691 | 2400.84 | 741 |
| 1756.08 | 542 | 1918.08 | 592 | 2080.08 | 642 | 2242.08 | 692 | 2404.08 | 742 |
| 1759.32 | 543 | 1921.32 | 593 | 2083.32 | 643 | 224532 | 693 | 2407.32 | 743 |
| 1762.56 | 544 | 1924.56 | 594 | 2086.56 | 644 | 2248.56 | 694 | 241056 | 744 |
| 1765.80 | 545 | 1927.80 | 59.5 | 2089.80 | 645 | 2251.80 | 695 | 2413.80 | 745 |
| 1769.04 | 546 | 1931.04 | 596 | 2093.04 | 646 | 2255.04 | 696 | 2417.04 | 746 |
| 1772.28 | 547 | 1934.28 | 597 | 2096.28 | 647 | 2258.28 | 697 | 2420.28 | 747 |
| 1775.52 | 548 | 1937.52 | 598 | 2099.52 | 648 | 2261.52 | 698 | 2423.52 | 748 |
| 1778.76 | 549 | 1940.76 | 599 | 2102.76 | 649 | 2264.76 | 699 | 2426.76 | 749 |
| 1782.00 | 550 | 1944.00 | 600 | 2106.00 | 650 | 2268.00 | 700 | 2430.00 | 750 |

TABLE NO. XXXIX.-Continued.

CUBIC YARDS, IN $\frac{100}{12}$ FEET LENGTHS, FOR GIVEN AREAS.

| Area. | $\begin{aligned} & \text { Cubic } \\ & \text { yards } \end{aligned}$ | Area. | $\begin{aligned} & \text { Cubic } \\ & \text { yards. } \end{aligned}$ | Irea | $\begin{aligned} & \text { Cubic } \\ & \text { yards. } \end{aligned}$ | Area. | Cubic | Area. | Cubic |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2433.24 | 751 | 2595.24 | 801 | 2757.24 | 851 | 2919.24 | 901 | 3081.24 | 951 |
| 2436.48 | 752 | 2598.48 | 802 | 2760.48 | 852 | 2922.48 | 902 | 3084.48 | 952 |
| $2439.7 *$ | 753 | 2601.72 | 803 | 2763.72 | 853 | 2925.72 | 903 | 3087.72 | 953 |
| 2442.96 | 754 | 2604.96 | 804 | 2766.96 | 854 | 2928.96 | 904 | 3090.96 | 954 |
| 2446.20 | 755 | 2608.20 | 805 | 2770.20 | 855 | 2932. 20 | 905 | 3094. 20 | 955 |
| 2449.44 | 756 | 2611.44 | 806 | 2773.44 | 856 | 2935.44 | 906 | 3097.44 | 956 |
| 2452.68 | 757 | 2614.68 | 807 | 2776.68 | 857 | 2938.68 | 907 | 3100.68 | 957 |
| 2455.92 | 758 | 2617.92 | 808 | 2779.92 | 858 | 2941.92 | 908 | 3103.92 | 958 |
| 2459.16 | 759 | 2621.16 | 809 | 2783.16 | 859 | 2945.16 | 909 | 3107.16 | 959 |
| 246\%.40 | 760 | 2624.40 | 810 | 2786.40 | 860 | 2948.40 | 910 | 3110.40 | 960 |
| 2465.64 | 761 | 2627.64 | 811 | 2789.64 | 861 | 2951.64 | 911 | 3113.64 | 961 |
| 2468.88 | 762 | 2630.85 | 812 | 2793.88 | 862 | 2954.88 | 912 | 3116.88 | 962 |
| 2472.12 | 763 | 2634.12 | 813 | 2796.12 | 863 | 2958.12 | 913 | 3120.12 | 963 |
| 2475.36 | 764 | 2637.36 | 814 | 2799.36 | 864 | 2961.36 | 914 | 3123.36 | 964 |
| 2478.60 | 765 | 2640.60 | 815 | 2802.60 | 865 | 2964.60 | 915 | 3126.60 | 965 |
| 2481.84 | 766 | 2643.84 | 816 | 2805.84 | 866 | 2967.84 | 916 | 3129.84 | 966 |
| 2485.08 | 767 | 2647.08 | 817 | 2809.08 | 867 | 2971.08 | 917 | 3133.08 | 967 |
| 2488.32 | 768 | 2650.32 | 818 | 2812.32 | 868 | 2974.32 | 918 | 3136.32 | 968 |
| 2491.56 | 769 | 2653.56 | 819 | 2815.56 | 869 | 2977.56 | 919 | 3139.56 | 969 |
| 2491.80 | 770 | 2656.80 | 820 | 2818.80 | 8.0 | 2980.80 | 920 | 3142.80 | 970 |
| 2498.04 | $7 / 71$ | 2660.04 | 821 | 2822. 04 | 871 | 2984.04 | 921 | 3146.04 | 971 |
| 2501.28 | 772 | 2663.28 | 822 | 2825.28 | 872 | 2987.28 | 922 | 3149.28 | 972 |
| 2504.5 | 773 | 2666.52 | 823 | 2828.52 | 873 | 299052 | 923 | 3152.52 | 973 |
| 2507.76 | 774 | 2669.76 | 824 | 2831.76 | 874 | 2993.76 | 924 | 3155.76 | 974 |
| 2511.00 | 775 | 2673.00 | 825 | 2835.00 | 875 | 2997.00 | 925 | 3159.00 | 975 |
| 2514.24 | 776 | 2676.24 | 826 | 2838.24 | 876 | 3000.24 | 926 | 3162.24 | 976 |
| 2517.48 | 777 | 2679.48 | 827 | 2841.48 | 877 | 3003.48 | 927 | 3165.48 | 977 |
| 2520.72 | 778 | 2682.72 | 828 | 2844.72 | 878 | 3006.72 | 928 | 3168.72 | 978 |
| 2523.96 | $7 \% 9$ | 2685.96 | 829 | 2847.96 | 879 | 3009.96 | 929 | 3171.96 | 979 |
| 2527.20 | 780 | 2689.20 | 830 | 2851.20 | 880 | 3013.20 | 930 | 3175.20 | 980 |
| 2530.44 | 781 | 2692.44 | 831 | 2854.44 | 881 | 3016.44 | 931 | 3178.44 | 981 |
| 2533.68 | 782 | 2695.68 | 832 | 2857.68 | 882 | 3019.68 | 932 | 3181.68 | 982 |
| 2536.92 | 783 | 2698.92 | 833 | 2860.92 | 883 | 3022.92 | 933 | 3184.92 | 983 |
| 2540.16 | 784 | 2702.16 | 834 | 2864.16 | 884 | 3026.16 | 934 | 3188.16 | 984 |
| 2543.40 | 785 | 2705.40 | 835 | 2867.40 | 885 | 3029.40 | 935 | 3191.40 | 985 |
| 2546.64 | 786 | 2708.64 | 836 | 2870.64 | 886 | 3032.64 | 936 | 3194.64 | 986 |
| 2549.88 | 787 | 2711.88 | 837 | 2873.88 | 887 | 3035.88 | 937 | 3197.88 | 987 |
| 2553.12 | 788 | 2715.12 | 838 | 2877.12 | 888 | 3039.12 | 938 | 3201.12 | 988 |
| 2556.36 | 789 | 2718.36 | 839 | 2880.36 | 889 | 3042.36 | 939 | 3204.36 | 989 |
| 2559.60 | 790 | 2721.60 | 840 | 2883.60 | 890 | 3045.60 | 940 | 3207.60 | 990 |
| 2562.84 | 791 | 2724.84 | 841 | 2886.84 | 891 | 3048.84 | 941 | 3210.84 | 991 |
| 2566.08 | 792 | 2728.08 | 842 | 2890.08 | 892 | 3052.08 | 942 | 3214.08 | 992 |
| 2569.32 | 793 | 2731.32 | 843 | 2893.32 | 893 | 3055.32 | 943 | 3217.32 | 993 |
| 2572.56 | 794 | 2734.56 | 844 | 2896.56 | 894 | 3058.56 | 944 | 3220.56 | 994 |
| 2575.80 | 795 | 2737.80 | 845 | 2899.80 | 895 | 3061.80 | 945 | 3223.80 | 995 |
| 2579.04 | 796 | 2741.04 | 846 | 2903.04 | 896 | 3065.04 | 946 | 3227.04 | 996 |
| 2582.29 | 797 | 2744.28 | 847 | 2906. 28 | 897 | 3068.28 | 947 | 3230.28 | 997 |
| 2585.52 | 798 | 2747.52 | 848 | 2909.52 | 898 | 3071.52 | 948 | 3233.52 | 998 |
| 2588.76 | 799 | 2750.76 | 849 | 2912.76 | 899 | 3074.76 | 949 | 3236.76 | 999 |
| 2592.00 | 800 | 2754.00 | 850 | 2916.00 | 900 | 3078.00 | 950 | 3240.00 | 1000 |

TABLE NO．XL．
Cubic yards equal height $\frac{24 \times 100}{4 \times 27}$ ．

|  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { 隠 } \\ & \text { تٌ } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { 范 } \\ & \text { 荡 } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 |  | 111 | 10.0 | 222 | 15.0 | 333 | 20.0 | 444 | 25.0 | 556 | 30.0 | 667 | 35.0 | 8 |
|  | 2 | 5.1 | 113 | 10.1 | 224 | 15.1 | 336 | 20.1 | 447 | 25.1 | 558 | 30.1 | 669 | 35.1 | 780 |
| 0.2 | 4 | 5.2 | 116 | 10.2 | 227 | 15.2 | 338 | 20.2 | 449 | 25.2 | 560 | 30.2 | 671 | 35.2 | 782 |
| 0.3 | 7 | 5.3 | 118 | 10.3 | 229 | 15.3 | 340 | 20.3 | 451 | 25.3 | 562 | 30.3 | 673 | 35.3 | 784 |
|  | 9 | 5.4 | 120 | 10.4 | 231 | 15.4 | 342 | 20.4 | 453 | 25.4 | 564 | 30.4 | 676 | 35.4 | 787 |
|  | 11 | 5.5 | $1 \because 2$ | 10.5 | 233 | 15.5 | 344 | 20.5 | 456 | 25.5 | 567 | 30.5 | 678 | 35.5 | 789 |
|  | 13 | 5.6 | 124 | 10.6 | 236 | 15.6 | 347 | 20.6 | 458 | 25.6 | 569 | 39.6 | 680 | 35.6 | 791 |
|  | 16 | 5.7 | 127 | 10.7 | 238 | 15.7 | 349 | 20.7 | 460 | 25.7 | 571 | 30.7 | 682 | 35. | 793 |
| 0.8 | 18 | 5.8 | 129 | 10.8 | 240 | 15.8 | 351 | 20.8 | 462 | 25.8 | 573 | 30.8 | 684 | 35. | ¢96 |
| 0.9 | 20 | 5.9 | 131 | 10.9 | 242 | 15.9 | 353 | 20.9 | 464 | 25.9 | 576 | 30.9 | 687 | 35.9 | 798 |
|  | 22 | 6. | 133 | 11.0 | 44 | 16 | 356 | 21.0 | 467 | 26 | 57 | 31.0 | 689 | 36.0 | 800 |
| 1.1 | 24 | 6.1 | 136 | 11.1 | 247 | 16.1 | 358 | 21.1 | 469 | 26.1 | 580 | 31.1 | 691 | 36.1 | 802 |
| 1.2 | 27 | 6.2 | 138 | 11.2 | 249 | 16.2 | 360 | 21.2 | 471 | 26.2 | 582 | 31.2 | 693 | 36. | 804 |
| 1.3 | 29 | 6.3 | 140 | 11.3 | 251 | 16.3 | 362 | 21.3 | 473 | 26.3 | 584 | 31.3 | 696 | 36. | 807 |
|  | 31 | 6.4 | 142 | 11.4 | 25. | 16.4 | 364 | 21.4 | 476 | 26.4 | 587 | 31.4 | 698 | 36. | 809 |
| 1.5 | 33 | 6.5 | 144 | 11.5 | 25.6 | 16.5 | 367 | 21.5 | 478 | 26.5 | 589 | 31.5 | 700 | 36. | 811 |
| 1.6 | 36 | 6.6 | 147 | 11.6 | 258 | 16.6 | 369 | 21.6 | 480 | 26.6 | 591 | 31.6 | 702 | 36 | 813 |
| 1. | 38 | 6.7 | 149 | 11.7 | 260 | 16. | 371 | 21.7 | 482 | 26.7 | 593 | 31.7 | 704 | 36 | 816 |
| 1.8 | 40 | 6.8 | 151 | 11.8 | 262 | 16.8 | 373 | 21.8 | 484 | 26.8 | 596 | 31.8 | 707 | 36. | 818 |
| 1.9 | 42 | 6.9 | 153 | 11.9 | 264 | 16.9 | 376 | 21.9 | 487 | 26.9 | 598 | 31.9 | 709 | 36.9 | 20 |
|  | 44 | 7.0 | 156 | 12.0 | 267 | 17.0 | 378 | 22.0 | 489 | 27.0 | 600 | 32.0 | 711 | 37.0 | 822 |
|  | 47 | 7.1 | 158 | 12.1 | 269 | 17.1 | 380 | 22.1 | 491 | 27.1 | 602 | 32.1 | 713 | 37.1 | 824 |
| 2. | 49 | 7.2 | 160 | 12.2 | 271 | 17.2 | 382 | 22.2 | 493 | 27.2 | 604 | 32.2 | 716 | 37.2 | 827 |
| 2.3 | 51 | 7.3 | 162 | 12.3 | 273 | 17.3 | 384 | 22.3 | 496 | 27.3 | 607 | 32.3 | 718 | 37. | 829 |
| 2.4 | 53 | 7.4 | 164 | 12.4 | 276 | 17.4 | 387 | 22.4 | 498 | 27.4 | 609 | 32.4 | 720 | 37. | 831 |
| 2.5 | 56 | 7.5 | 167 | 12.5 | $2 i 8$ | 17.5 | 389 | 22.5 | 500 | 27.5 | 611 | 32.5 | 722 | 37. | 833 |
| 2 | 58 | 7.6 | 169 | 12.6 | 280 | 17.6 | 391 | 23.6 | 502 | 27.6 | 613 | 32.6 | 724 | 37.6 | 836 |
|  | 60 | 7.7 | 171 | 12.7 | 282 | 17.7 | 393 | 22.7 | 504 | 27.7 | 616 | 32.7 | 727 | 37.7 | 838 |
|  | 62 | 7.8 | 173 | 12.8 | 284 | 17.8 | 396 | 22.8 | 507 | 27.8 | 618 | 32.7 | 729 | 37.8 | 840 |
| 2.9 | 64 | 7.9 | 176 | 12.9 | 287 | 17.9 | 398 | 22.9 | 509 | 27.9 | 620 | 32.9 | 731 | 37.9 | 842 |
|  | 67 | 8.0 | 178 | 13.0 | 289 | 18.0 | 400 | 23.0 | 511 | 28.0 | 622 | 33.0 | 733 | 38.0 | 844 |
| 3.1 | 69 | 8.1 | 180 | 13.1 | 291 | 18.1 | 402 | 23.1 | 513 | 28.1 | 624 | 33.1 | 736 | 38.1 | 847 |
|  | 71 | 8.2 | 182 | 13.2 | 293 | 18.2 | 404 | 23.2 | 516 | 28.2 | 627 | 33.2 | 738 | 38.2 | 849 |
| 3.3 | 73 | 8.3 | 184 | 13.3 | 296 | 18.3 | 407 | 23.3 | 518 | 28.3 | 629 | 33.3 | 740 | 38.3 | 851 |
| 3．t | 76 | 8.4 | 187 | 13.4 | 298 | 18.4 | 409 | 23.4 | 520 | 28.4 | 631 | 33.4 | 742 | 38.4 | 853 |
|  | 78 | 8.5 | 189 | 13.5 | 300 | 18.5 | 411 | 23.5 | $5 \geqslant 2$ | 28.5 | 633 | 33.5 | 744 | 38.5 | 856 |
| 3.6 | 811 | 8.6 | 191 | 13.6 | 302 | 18.6 | 413 | 23.6 | 524 | 28.6 | 636 | 33.6 | 747 | 38.6 | 858 |
| 3.7 | 82 | 8.7 | 193 | 13.7 | 304 | 18.7 | 416 | 23.7 | 527 | 28.7 | 638 | 33.7 | 749 | 38.7 | 860 |
| 3.8 | 84 | 8.8 | 196 | 13.8 | 307 | 18.8 | 418 | 23.8 | 529 | 28.8 | 640 | 33.8 | 751 | 38.8 | 862 |
| 3.9 | 87 | 8.9 | 198 | 13.9 | 309 | 18.9 | 420 | 23.9 | 531 | 28.6 | 642 | 33.9 | 753 | 38.9 | 864 |
| 4.0 | 89 | 9.0 | 200 | 14.0 | 311 | 19.0 | 422 | 24.0 | 533 | 29.0 | 644 | 34.0 | 756 | 39.0 | 867 |
| 1 | 91 | 9.1 | 202 | 14.1 | 313 | 19.1 | 424 | 24.1 | 536 | 29.1 | 647 | 34.1 | 758 | 39.1 | 869 |
| 4.2 | 93 | 9.2 | 204 | 14.2 | 316 | 19.2 | 427 | 24.2 | 538 | 29.2 | 649 | 34.2 | 760 | 39.2 | 871 |
| 4.3 | 96 | 9.3 | 207 | 14.3 | 318 | 19.3 | 429 | 24.3 | 540 | 29.3 | 651 | 34.3 | 762 | 39.3 | 873 |
| 4.4 | 98 | 9.4 | 209 | 14.4 | 320 | 19.4 | 431 | 24.4 | 542 | 29.4 | 653 | 34.4 | 764 | 39.4 | 876 |
| 4.5 | 100 | 9.5 | 211 | 14.5 | 322 | 19.5 | 433 | 24.6 | 544 | 29.5 | 656 | 34.5 | 767 | 39.5 | 878 |
| 4.6 | 102 | 9. | 213 | 14.6 | 324 | 19.6 | 436 | 24.6 | 547 | 29.6 | 658 | 34.6 | 769 | 39.6 | 880 |
| 4 | 104 | 9. | 216 | 14.7 | 327 | 19.7 | 433 | 24.7 | 549 | 29.7 | 660 | 34.7 | 771 | 39.7 | 882 |
| 4.9 | 107 109 | 9.8 9.9 | 218 | 14.8 14.9 | 329 331 | 19.8 19.9 | 440 | 24.8 | 551 | 29.8 29 | 662 664 | 34.8 34.9 | 773 | 39.8 | 884 |
| 9 |  |  |  |  | 331 | 19.9 | 442 | 24.9 | 553 | 29.9 | 664 | 34.9 | 776 | 39.9 | 887 |

TABLE NO. XLI.
Cubic yards equal $100 \frac{D^{2}}{27 \times 16 \times 1}$.
Side slopes 1 to 1.

| D. | . 0 | . 1 | . 2 | . 3 | . 4 | ${ }_{8} 5$ | . 6 | . 7 | . 8 | . 9 | D. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 |  |  |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 |
| 2 | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 2 |
| 3 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 3 | 4 | 3 |
| 4 | 4 | 4 | 4 | 4 | 4 | 5 | 5 | 5 | 5 | 6 | 4 |
| 5 | 6 | 6 | 6 | 7 | 7 | 7 | 7 | 8 | 8 | 8 | 5 |
| 6 | 8 | 9 | 9 | 9 | 9 | 10 | 10 | 10 | 11 | 11 | 6 |
| 7 | 11 | 12 | 12 | 12 | 13 | 13 | 13 | 14 | 14 | 14 | 7 |
| 8 | 15 | 15 | 16 | 16 | 16 | 17 | 17 | 18 | 18 | 18 | 8 |
| 9 | 19 | 19 | 20 | 20 | 20 | 21 | 21 | 22 | 22 | 23 | 9 |
| 10 | 23 | 24 | 24 | 25 | 25 | 26 | 26 | 27 | 27 | 28 | 10 |
| 11 | 28 | 29 | 29 | 30 | 30 | 31 | 31 | 32 | 32 | 33 | 11 |
| 12 | 33 | 34 | 34 | 35 | 36 | 36 | 37 | 37 | 38 | 39 | 12 |
| 13 | 39 | 40 | 40 | 41 | 42 | 42 | 43 | 43 | 44 | 45 | 13 |
| 14 | 45 | 46 | 47 | 47 | 48 | 49 | 49 | 50 | 51 | 51 | 14 |
| 15 | 53 | 53 | 53 | 54 | 55 | 56 | 56 | 57 | 58 | 59 | 15 |
| 16 | 59 | 60 | 61 | 62 | 62 | 63 | 64 | 6.5 | 6.5 | 66 | 16 |
| 17 | 67 | 68 | 68 | 69 | 70 | 71 | 72 | 73 | 73 | 74 | 17 |
| 18 | \%5 | 76 | 77 | 78 | 78 | \%9 | 80 | 81 | 82 | 83 | 18 |
| 19 | 84 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 19 |
| D. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | 5 | . 8 | . 9 | D. |

Cubic yards equal $100 \frac{D^{2}}{27 \times 16 \times \frac{2}{3}}$.
Side slopes $1 \frac{1}{2}$ to 1 .

| D. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . $C$ | . 7 | . 8 | . 9 | D. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 2 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 2 |
| 3 | 3 | 3 | 4 | 4 | 4 | 4 | 5 | 5 | 5 | 5 | 3 |
| 4 | 6 | 6 | 6 | 6 | 7 | 7 | 7 | 8 | 8 | 8 | 4 |
| 5 | 9 | 9 | 9 | 10 | 10 | 11 | 11 | 11 | 12 | 12 | 5 |
| 6 | 13 | 13 | 13 | 14 | 14 | 15 | 15 | 16 | 16 | 17 | 6 |
| $\tau$ | 17 | 18 | 18 | 19 | 19 | 20 | 20 | 21 | 21 | 22 | 7 |
| 8 | 22 | 23 | 23 | 24 | 25 | 2.5 | 26 | 26 | $\because 7$ | 28 | 8 |
| 9 | 28 | 29 | 29 | 30 | 31 | 31 | 33 | 33 | 33 | 34 | 9 |
| 10 | 35 | 35 | 36 | 37 | 38 | 38 | 39 | 40 | 41 | 41 | 10 |
| 11 | 43 | 43 | 44 | 44 | 45 | 46 | 45 | 49 | 48 | 49 | 11 |
| 12 | 50 | 51 | 53 | 53 | $5: 3$ | 54 | 55 | 56 | 57 | 58 | 12 |
| 13 | 59 | 60 | 61 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 13 |
| 14 | 68 | 69 | \%0 | 71 | 72 | 73 | \%4 | 75 | ¢6 | T7 | 14 |
| 15 | 78 | \%9 | 80 | 81 | 82 | 83 | 85 | 86 | 87 | 88 | 15 |
| 16 | 89 | 90 | 91 | 92 | 93 | 95 | 96 | 97 | 98 | 99 | 16 |
| 17 | 100 | 102 | 103 | 104 | 105 | 106 | 108 | 109 | 110 | 111 | 17 |
| 18 | 113 | 114 | 115 | 116 | 118 | 119 | 120 | 121 | 123 | 124 | 18 |
| 19 | 125 | 127 | 128 | 129 | 131 | 132 | 133 | 135 | 136 | 138 | 19 |
| D. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | 6 | . 7 | . 8 | . 9 | D. |

TABLE NO XLII．

## Level Cross Sections．

CUBIC YARDS IN CORRESPONDING PRISMS，$\frac{100}{4}$ FEET LONG．
Road－bed 14 feet wide．
Side slopes $1 \frac{1}{2}$ to 1.

| 送家家 |  |  |  |  | 気苞荡 |  |  |  |  | 第䫆 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 5. | 4： | 10.1 | 101 | 15.1 | 1 | 20.1 | 2.1 | 25.1 | 381 | 30.1 | 510 |  |  |
|  |  | 5.2 | 43 | 10.2 | 102 | 15.2 | 179 | 20.2 | 273 | 25.2 | 384 | 30.2 | 512 |  |  |
|  |  | 5.3 | 44 | 10.3 | 104 | 15. | 180 | 20.3 | 275 | 25. | 386 | 30.3 | 515 |  |  |
|  |  |  | 45 | 10.4 | 105 | 15. | 182 | 20.4 | 277 | 25. | 389 | 30.4 | 518 |  | 66 |
|  |  |  | 46 | 10.5 | 106 |  | 84 | 20.5 | 79 | 2．） | 391 | 30. | 21 |  | 66 |
|  |  |  | 47 | 10.6 | 108 | 15 | 86 | 20.6 | 281 | $\bigcirc 5$ | 393 | 30 | 523 | 35 | $6{ }^{6}$ |
|  |  | 5.7 | 48 | 10 | 109 |  | 187 | 20.7 | 283 | 25. | 96 | 30. | 526 |  |  |
|  |  | 5．8 | 49 | 10.8 | 111 | 15.8 | 189 | 20.8 | 285 |  | 398 | 30. | 529 | 35. |  |
| 0.9 | 6 | 5.9 | 50 | 10.9 | 112 | 15.9 | 191 | 20.9 | 287 | 25.9 | 401 | 30.9 | 532 | 35.9 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | 36.0 |  |
|  |  | 6.1 |  | 11.1 |  | 16.1 | 194 | 21. | 291 | 26 | 406 | 31 |  | 36 | 1：86 |
|  | 8 | 6.2 | 54 | 11.2 |  | 16. | 196 | 21.2 | 293 | 26.2 | 08 | 31. | 540 | 36.2 | 690 |
|  | 9 | 6.3 | 55 | 11.3 | 118 | 16.3 | 98 | 21.3 | 296 | 26. | 411 | 31.3 | 4 |  | 93 |
|  | 10 | 6.4 | 5 | 11.4 | 119 | 16. | 00 | 21.4 | 298 | 26. | 413 | 31. |  | 36. | 96 |
|  | 11 | 6.5 | 57 | 11.5 | 12 | 16. | 201 | 21.5 | 30 | 26. | 416 | 31. | 49 | 36 | 699 |
|  | 11 | 6.6 | 58 | 11.6 | 122 | 16. | 203 | 216 | 302 | 26.6 | 418 | 31. | 552 | 36 | 02 |
|  | 12 |  | 59 | 11 | 123 |  | 205 | 21.7 | 304 | 26. | 421 | 31 |  | 36. | i06 |
|  | 13 | 6.8 | 60 | 11.8 |  | 16 | 207 | 21.8 | 30 | 26. | 423 | 31. | 557 | \％ 6.8 | 70 |
| 1.9 | 14 | 6.9 | 61 | 11.9 |  | 16 | 208 | 21. | 308 | 26 | 426 | 31. |  |  |  |
|  |  |  |  | 12.0 |  | 17. |  | 2. | 31 | 27.0 | 28 | 32.0 | 563 | 37 |  |
|  | 15 |  | 64 | 12.1 |  | 17.1 | 12 | 22. | 31 | 27.1 | 31 |  |  |  |  |
|  | 16 | 7.2 | 65 | 12.2 | 131 |  | 214 | 22. |  | 27 | 913 | 32. | 569 |  |  |
|  |  |  |  | 1 | 13 |  | 216 | 22.3 |  | 27 | 436 | 32. | 572 | 37 | 25 |
|  | 18 | 7.4 | 67 | 12.4 | 13 |  |  | 22.4 | 319 | 27 | $4: 8$ | 32. | 575 | 37.4 |  |
|  | 18 | 7.5 | 68 | 12.5 | 135 | 17. | 220 | 23 | 222 | 27.5 | 441 | 32. | 57 | 37. | 3 |
|  | 19 | 7.6 | 9 | 12.6 | 137 | 17.6 | 2 | 226 | 324 | 27.6 | 443 | 33.6 |  |  | 35 |
|  | 20 | 7. | 70 | 12.7 |  | 17.7 | 224 | 22.7 | 326 | 27. | 446 | 32. |  | 37. | 38 |
|  | 21 | 7.8 | 2 | 12.8 | 140 | 17.8 | 2 | 22.8 | 321 | 27.8 | 449 | 32.8 | 586 |  | 741 |
| 2.9 | 22 | 7. | 73 | 12.9 | 141 | 17.9 | 227 | 22.9 | 331 | 27.9 | 451 | 32.8 | 589 | 37.9 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 23 | 8.1 | 75 | 13.1 | 144 | 18. | 231 | 23.1 |  | 281 | 56 | 33.1 |  |  | 51 |
|  | 24 | 8.2 | 76 | 13.2 | 146 | 18.2 | 233 | 23.2 | ， | 28.2 | 459 | 33.2 | 598 | 38.2 | 54 |
|  | 25 | 8. | 78 | 133 | 148 | 18.3 | 235 | 23.3 | 340 | 28.3 | 462 | 33.3 |  |  | 58 |
|  |  | 8.4 | 79 | 13.4 | 149 |  | 237 | 23. | 342 | 28 | 464 | 33. | 604 | 38.4 | 61 |
|  |  | 8． | 8 | 13.5 | 1 | 18. | ， | 23.5 |  | 28. | 4 \％ | נ3． | 607 | ． | 64 |
|  |  |  | 81 | 13.6 |  |  |  | 23.6 |  | 28. | 碞 | 33. | 610 |  |  |
|  | 29 | 8.7 | 83 | 13.7 |  |  |  | 23. | 49 | 28. | 472 | 33. | 13 |  |  |
|  | 30 | 8.8 | 84 | 13.8 | 156 | 18.8 | 245 | 23.8 | 351 | 28.8 | 475 | 33.8 | 616 | 38.8 | 74 |
| 3.9 | 31 | 8.9 | 85 | 13.9 | 157 | 18.9 | 247 | 23.9 | 5－8 | 28.9 | 47 | 33.9 | 61 |  |  |
|  |  | 9.0 |  | 14. |  |  |  | 24.0 |  | 29.0 |  | 34.0 | 2 | 39.0 |  |
|  | － | 9.1 | 8 |  | 160 | 19 |  | 24.1 |  | 29.1 | 5 | 34.1 | 20 | 39.1 |  |
|  | 33 | 92 | 89 | 14.2 | 102 | 19.2 |  | 24.2 | 60 | 29.2 | 485 | 34.2 | 698 | 39.2 | 88 |
| 4.3 | 34 | 9.3 | 90 | 14.3 | 164 | 19.3 | 254 | 24.3 | 63 | 29.3 | 488 | 34.3 | 631 | 39.3 | 91 |
|  | 35 | 9.4 | 92 | 14.4 | 165 | 19.4 | 56 | 24.4 | 65 | 29.4 | 491 | 34.4 | 63 | 39. | 94 |
|  | 36 | 9.5 | 93 | 14.5 | 167 | 19.5 | 58 | 24.5 | 367 | 29.5 | 493 | 34.5 | 637 | 39.5 | 旺 |
|  | 37 | 9.6 | 94 | 14.6 | 169 | 19.6 | 260 | 24.6 | 170 | 29.6 | 496 | 34. | 640 | 39.6 | 01 |
|  | 38 | 9.7 | 96 | 14.7 | 170 | 19.7 | 262 | 24.7 | 372 | 29.7 | 499 | 34.7 | 643 | 39.7 | 805 |
| 4.8 | 39 | 9.8 | 9 | 14.8 | 172 | 19.8 | 64 | 24.8 | 37 | 29.8 | 501 | 34.8 | 646 | 3.8 | 808 |
| 4.9 | 40 | 9.9 | 98 | 14.9 | 174 | 19.9 |  | 24.9 | 377 | 29.9 | 504 | 34.9 | 649 | 39.9 | 811 |

TABLE NO. XLIII.
Level Cross Sections.
CUBIC YARDS IN CORRESPONDING PRISMS, $\frac{100}{4}$ FEET LONG.
Road-bed 18 feet wide.
Side slopes 1 to 1.

|  |  |  |  |  |  |  |  |  |  |  |  |  | 言荖 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 5.0 | 47 | 10.0 | 106 | 15.0 | 177 | 20.0 | 59 | 25.0 | 353 | 30.0 | 458 | 35.0 | 75 |
|  | 1 | 5.1 | 49 | 10.1 | 108 | 15.1 | 179 | 20.1 | 261 | 25.1 | 355 | 30.1 | 461 | 35.1 | 578 |
| 0. | 2 | 5.2 | 50 | 10.2 | 109 | 15.2 | 180 | 20.2 | 263 | 2 กั. 2 | 357 | 30.2 | 463 | 35.2 | 580 |
| 0.3 | 3 | 5.3 | 51 | 10.3 | 110 | 15.3 | 182 | 20.3 | 265 | 25.3 | 3.59 | 30.3 | 465 | 35.3 | 583 |
| 0.4 | 3 | 5.4 | 52 | 10.4 | 112 | 15.4 | 183 | 20.4 | 266 | 224 | 361 | 30.4 | 467 | 35.4 | 585 |
| 0 | 4 | 5.5 | 53 | 10.5 | 113 | 15.4 | 185 | 20.5 | 268 | 25.5 | 363 | 30.5 | 470 | 35.5 | 588 |
| 0 | 5 | 5.6 | 54 | 10.6 | 114 | 15.6 | 186 | 20.6 | 270 | 25.6 | 365 | 30.6 | 472 | 35.6 | 590 |
|  | 6 | 5.7 | 55 | 10.7 | 116 | 15.7 | 188 | 20.7 | 272 | 25.7 | 367 | 30.7 | 474 | 35.7 | 593 |
| 0.8 | 7 | 5.8 | 56 | 10.8 | 117 | 15.8 | 189 | 20.8 | 273 | 25.8 | 369 | 30.8 | 476 | 35.8 | 595 |
| 0.9 | 8 | 5.9 | 57 | 10.9 | 118 | 15.9 | 191 | 20.9 | 275 | 25.9 | 371 | 30.9 | 479 | 35.9 | 598 |
| 1.0 | 9 | 6 | 58 | 11.0 | 120 | 16.0 | 193 | 21.0 | 277 | 26.0 | 373 | 31.0 | 481 | 36.0 | 600 |
| 1. | 9 | 6.1 | 59 | 11.1 | 121 | 16.1 | 194 | 21.1 | 279 | 26.1 | 375 | 31.1 | 483 | 36.1 | 603 |
| 1.2 | 10 | 6.2 | 61 | 11.2 | 122 | 16.2 | 196 | 21.2 | 281 | 26.2 | 377 | 31.2 | 485 | 36.2 | 605 |
| 1.3 | 11 | 6.3 | 62 | 11.3 | 124 | 16.3 | 197 | 21.3 | 283 | 26.3 | 379 | 31.3 | 488 | 36.3 | 608 |
| 1.4 | 12 | 6.4 | 63 | 11.4 | 125 | 16.4 | 199 | 21.4 | 284 | 26.4 | 381 | 31.4 | 490 | 36.4 | 610 |
| 1.5 | 13 | 6.5 | 64 | 11.5 | 126 | 16.5 | 201 | 21.5 | 286 | 26.5 | 383 | 31.5 | 492 | 36.5 | 613 |
| 1.6 | 14 | 6.6 | 65 | 11.6 | 128 | 16.6 | 202 | 21.6 | 288 | 26.6 | 385 | 31.6 | 494 | 36.6 | 615 |
| 1.7 | 15 | 6.7 | 66 | 11.7 | 129 | 16.7 | 204 | 21.7 | 290 | 26.7 | 388 | 31.7 | 497 | 36.7 | 618 |
| 1.8 | 16 | 6.8 | 67 | 11.8 | 131 | 16.8 | 205 | 21.8 | 292 | 26.8 | 390 | 31.8 | 499 | 36.8 | 620 |
| 1.9 | 17 | 6.9 | 69 | 11.9 | 132 | 16.9 | 207 | 21.9 | 294 | 26.9 | 392 | 31.9 | 501 | 36.9 | 623 |
|  | 18 | 7.0 | 70 | 12.0 | 133 | 17.0 | 209 | 22.0 | 295 | 27.0 | 394 | 32.0 | 504 | 37.0 | 635 |
| , 1 | 19 | 7.1 | 71 | 12.1 | 135 | 17.1 | 210 | 22.1 | 297 | 27.1 | 396 | 32.1 | 506 | 37.1 | 628 |
| 2 | 19 | 7.2 | 72 | 12.2 | 136 | 17.2 | 212 | 22.2 | 299 | 27.2 | 398 | 32.2 | 508 | 37.2 | 630 |
| 2.3 | 20 | 7.3 | 73 | 12.3 | 138 | 17.3 | 213 | 22.3 | 301 | 27.3 | 400 | 32.3 | 511 | 37.5 | 633 |
| 2.4 | 21 | 7.4 | 74 | 12.4 | 139 | 17.4 | 215 | 22.4 | 303 | 27.4 | 402 | 32.4 | 513 | 37.4 | 635 |
| 2.5 | 22 | 7.5 | 76 | 12.5 | 140 | 17.5 | 217 | 22.5 | 305 | 27.5 | 404 | 32.5 | 515 | 37.5 | 633 |
| 2.6 | 23 | 7.6 | 75 | 12.6 | 142 | 17.6 | 218 | 22.6 | 307 | 27.6 | 406 | 32.6 | 518 | 37.6 | 641 |
| 2.7 | 24 | 7.7 | 78 | 12.7 | 143 | 17.7 | 220 | 22.7 | 308 | 27.7 | 408 | 32.7 | 520 | 37.7 | 643 |
| 8 | 25 | 7.8 | \%9 | 128 | 145 | 17.8 | 222 | 22.8 | 310 | 27.8 | 411 | 32.8 | 522 | 37.8 | 646 |
| 2.9 | 25 | 7.9 | 80 | 12.9 | 146 | 17.9 | 223 | 22.9 | 312 | 27.9 | 413 | 32.9 | 525 | 37.9 | 648 |
| 3.0 | 27 | 8.0 | 81 | 13.0 | 147 | 18.0 | 225 | 23.0 | 314 | 28.0 | 415 | 33.0 | 527 | 38.0 | 651 |
| 3.1 | 28 | 8.1 | 83 | 13.1 | 149 | 18.1 | 227 | 23.1 | 316 | 28.1 | 417 | 33.1 | 529 | 38.1 | 654 |
| 3.2 | 29 | 8.2 | 84 | 13.2 | 150 | 18.2 | 228 | 23.2 | 318 | 28.2 | 419 | 33.2 | 532 | 38.2 | 656 |
| 3.3 | 30 | 8.3 | 85 | 13.3 | 153 | 18.3 | 230 | 23.3 | 320 | 28.3 | 421 | 33.3 | 534 | 38.3 | 659 |
| , | 31 | 8.4 | 86 | 13.4 | 15:3 | 18.4 | 2:32 | 23.4 | 322 | 28.4 | 423 | 33.4 | 537 | 38.4 | 661 |
| 3.5 | 32 | 8.5 | 88 | 13.5 | 155 | 18.5 | 233 | 23.5 | 324 | 28.5 | 426 | 33.5 | 539 | 38.5 | 664 |
| 3.6 | 33 | 8.6 | 89 | 13.6 | 156 | 18.6 | 235 | 23.6 | 326 | 28.6 | 428 | 23.6 | 541 | 38.6 | 667 |
| 3.7 | 34 | 8.7 | 90 | 13.7 | 153 | 18.7 | 237 | 23.7 | 328 | 28.7 | 430 | 33.7 | 544 | 38.7 | 669 |
| 3.8 | 3.5 | 8.8 | 91 | 13.8 | 1.99 | 18.8 | 238 | 23.8 | 329 | 28.8 | 432 | 3:3.8 | 546 | 388 | 672 |
| 3.9 | 36 | 8.9 | 93 | 13.9 | 161 | 18.9 | 240 | 23.9 | 331 | 28.9 | 434 | 33.9 | 549 | 38.9 | 674 |
| 4. | 37 | 9.0 | 94 | 14.0 | 162 | 19.0 | 242 | 24.0 | 333 | 29.0 | 436 | 34.0 | 551 | 39.0 |  |
| 4.1 | 38 | 9.1 | 95 | 141 | 164 | 19.1 | 244 | 24.1 | 335 | 29.1 | 439 | 34.1 | 553 | 39.1 | 680 |
| 4.2 | 39 | 9.2 | 96 | 14.2 | 165 | 19.2 | 245 | 24.2 | 337 | 29.2 | 441 | 34.2 | 556 | 39.2 | 682 |
| 4.3 | 40 | 9.3 | 98 | 14.3 | 167 | 19.8 | 247 | 24.3 | 3:39 | 29.3 | 413 | 34.3 | 558 | 39.3 | 685 |
| 4.4 | 41 | 94 | 99 | 14.4 | 168 | 19.4 | 249 | 24.4 | 341 | 29.4 | 445 | 34.4 | 561 | 39.4 | 688 |
| 4.5 | 4.3 | 9.5 | 100 | 14.5 | 170 | 19.5 | 251 | 24.5 | 343 | 29.5 | 447 | 34.5 | 5613 | 39.5 | 690 |
| 4.6 | 43 | 9.6 | 101 | 14.6 | 171 | 19.6 | 252 | 24.6 | 34.5 | 29.6 | 449 | 34.6 | 565 | 39.6 | 693 |
| 4.7 | 44 | 9.7 | 103 | 14.7 | 173 | 19.7 | 254 | 24.7 | $34 i$ | 29.7 | 452 | 34.7 | 568 | 39.7 | 696 |
| 4.8 | 4.5 | 9.8 | 104 | 14.8 | 174 | 19.8 | 256 | 24.8 | 349 | 29.8 | 454 | 34.8 | 570 | 39.8 | 698 |
| 4.9 | 46 | 9.9 | 105 | 14.9 | 176 | 19.9 | 258 | 24.9 | 351 | 29.9 | 456 | 349 | 573 | 39.9 | 701 |

TABLE NO．XLIV．

## Cubic yards equal $\frac{(\text { height } \times r+b \text { ）} 100}{4 \times 27}$ ．

Road－bed 24 feet wide．
Side slopes 1 to 1.

| $\begin{aligned} & \text { 㵄 } \\ & \text { Bu } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { 范 } \\ & \text { 跒 } \end{aligned}$ |  |  |  |  | 을루률 | 茄 |  | 感 | 을 | 感 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | 20 |  |  |  |  |  |  |  |
|  | 22 |  | 26 |  | 31.6 |  |  | 20. | 40. | 25 | 45. | 30. |  |  |  |
|  | 20 | 5.2 | 27.0 | 10 | 31.7 |  |  | 20 | 40.9 | 5 | 45 | 30. | 2 |  |  |
|  | 23 |  |  |  | 31.8 |  |  | 0 | 41.0 | 25.3 | 45.6 | 30.3 | 50．3 |  |  |
|  | 22 |  |  |  |  |  |  | 20 |  | 25.4 |  | 30 | 450.4 |  |  |
|  | 22.7 | 5.5 | 27.3 |  | 31.9 |  |  |  | 41. | 25 | 45. | － | 50.5 |  |  |
|  | 22.8 | 5.6 | 27.4 | 10.6 | 32.0 |  |  | 20 | 41 | 25 | 45.9 | 30.6 | 60．6 |  |  |
|  | 22.9 | 5.7 | 27.5 | 10 | 32.1 | 15. |  | 20 | 41.4 | 25. | 46. | 30. | 750.6 |  |  |
|  | 23.0 |  | 27. |  | 32.2 |  |  | 20. | 11 | 2 | 46. | 30. |  |  |  |
| 0.9 | 23.1 | 5 | 27. | 10.9 | 32.3 |  | 36.9 | 20. |  |  | 46 | 30 |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  | ． 3 |  | ． 9 |  |  |
|  | 23.2 | 6． | 27 | 11 | 32.5 |  | 37.1 | 21 | 41.8 | 26 | 46. | d | 51.0 |  |  |
|  | 23.3 | 6.2 | 28.0 | 11 | 32.6 | 16. | 37.2 | 21. | 41 | 26. | 46 | 31. | 51.1 | 36.2 |  |
|  | 23. | 6.3 | 28. | 11 | 32. | 16. |  | 21. | 41. | 26 |  | 31 | 51. | 36.3 |  |
|  | 2 | 6 | 28 |  | 32 |  |  |  | 4． | 26 |  | 31 | 51 | 36 |  |
|  | 23 | 6 | 28.2 |  | 32.9 |  |  |  | 42.1 |  |  | 31 | 51.4 |  |  |
|  | 23.7 | 6.6 | 28.3 |  | 33.0 |  |  | 21. |  | 26. |  |  | 51.5 |  |  |
|  | 23.8 |  | 28.4 | 11.7 | 33. |  |  | 21. | 2． |  |  |  | 51.6 |  |  |
| 1.8 | 23.9 | 0.8 | 28.5 | 11.8 | 33.1 | 16. |  | 21.8 | 42. | 26.8 | 47.0 | 31 | 51.7 |  | ． 3 |
| 1.9 | 24.0 | 6.9 | 28.6 | 119 | 33.2 | 16.9 | 37. | 21.9 | 42. | 26.9 | 47 | 31.9 | 51 | 36 | 4 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 24.2 | 7.1 | 28.8 |  |  |  |  |  |  |  | 47.3 | 2 | ． 9 |  |  |
|  | 24.3 | 7.2 | 28.9 | 12.2 |  |  |  | 22.2 | 42.8 | 27. | 47. | 32.2 | 22．0 |  |  |
|  | 24.4 | 7.3 | 29.0 | 12.3 | 33.6 | 17.3 |  | 22.3 | 42.9 | 27. | 47. | 32.3 |  |  | ． 8 |
|  | 24. |  | 29. | 12 | 33 |  |  | 22. |  | 27 |  | 32 | ． |  |  |
|  |  |  | 29.2 | 12.5 |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 7. |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 7 | 9 |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 24.8 |  |  |  |  |  |  | 22.8 |  |  | 48.0 |  |  |  |  |
| 2.9 | 24.9 | 7. | 29.5 | 12.9 | 34 |  |  | 22.9 |  | 27.9 | 48 |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  | 48.1 |  |  |  |  |
|  |  |  |  |  |  |  |  | 23 |  |  |  |  |  |  |  |
|  |  | 8 | 29 |  |  |  |  | 23.2 |  | 20. |  |  |  |  |  |
|  |  | 8 | 29.9 |  |  |  |  |  |  | 28. |  |  |  |  |  |
|  | 25. | 8.4 | 30.0 |  | ． 6 |  |  |  |  |  |  |  |  |  |  |
|  | 25.5 | 8.5 | 30.1 | 18.5 | 34.7 | 18.5 | ． 4 | 23.5 | ． 0 | 28.5 | ． 6 | 33 |  |  |  |
|  | 25. | 8.6 | 30.2 |  | 34.8 |  |  |  |  |  | ． |  |  |  |  |
|  | 25 |  | 30.3 |  | 34.9 | 18 | 39.5 |  | 44 |  | 8 | 33 |  |  |  |
|  |  | 8.8 | 30 | 13 |  | 18 | 39.6 | 23.8 | 44.3 | 28.8 | 48.9 | 33． | 53．5 |  | 8.1 |
| ． | 25 | 8.9 | 30 | 13 |  |  | 3 | 23.3 |  | 28. | 49.0 |  |  |  |  |
|  | 2 |  |  |  |  |  |  | 24.0 |  | ． 0 | 9．1 | 34.0 | 5．7 |  |  |
|  | 26.0 | 9.1 | 30.6 | 14.1 |  | 19.1 | 39.9 | 24. |  | 29.1 | 49.2 | 34. | 538 |  |  |
|  | 26. | 9 | 30 | 14. | 35.4 | 19.2 | 40.0 | 24.2 |  | 29.2 | 49.3 | 34. | 53.9 |  |  |
|  | 26.2 | 9.3 | ． 8 | 143 | 35. | 19.3 | 40.1 | 24. |  | 29.3 | 49.4 |  | 4.0 |  | ． |
| 44 | 26.3 | 9.4 | 30.9 | 14. | 35.6 | 19.4 | 40.2 | 24.4 | 44.8 | 29. | 49.4 |  | 54.1 |  |  |
|  | 26.4 | 9.5 | 31.0 | 14. |  | 19.5 | 40.3 | 24. | 4.9 | 29.0 | 49.5 | 34. | ． |  |  |
|  | 26.5 |  | 31.1 | 14.6 | 35. | 19.6 | 40.4 | 24.6 | 5.0 | 29.6 | 49.6 | 34 | 4.3 |  |  |
|  | 26.6 |  | 31.2 | 14.7 | 35.8 | 19.7 | 40.5 | 24.7 | 45.1 | 29. | 49.7 | 34.7 | 4．4 | 90． |  |
|  |  |  | 31.3 |  | 35.9 | 19.8 | 40.6 | 24.8 | 45.2 | 29.8 | 49.8 | 34. | 54.4 | 39. | 59.1 |
|  | 26.8 | 9.9 | 31.4 | 4.9 |  |  |  | 24.9 | 45.3 | 29.9 | 49.9 |  | 54.5 | 9. | 59.2 |

TABLE NO．XLV．

$$
\frac{\text { (height) } b 100}{8 \times 27}
$$

Road－bed 24 feet wide．

| $\frac{\stackrel{\rightharpoonup}{u n}}{\substack{0 \\ \hline}}$ |  |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \text { 淢 } \\ & \stackrel{\rightharpoonup}{0} \end{aligned}$ |  | $\begin{aligned} & \stackrel{\rightharpoonup}{c} \\ & \stackrel{0}{0} \\ & \underset{\sim}{0} \end{aligned}$ | $\begin{aligned} & \text { 总㤩 } \\ & \text { Ég } \end{aligned}$ | $\begin{aligned} & \text { 去 } \\ & \text { 淢 } \\ & \stackrel{y y y}{*} \end{aligned}$ |  |  | $\left\lvert\, \begin{array}{l\|} 0 \\ \text { 으를 } \\ \text { Un } \end{array}\right.$ |  | $\begin{aligned} & \text { 另害 } \\ & \text { 品 } \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0. | 0 |  | 5 | 10.0 | 11 | 15.0 | 167 | 20.0 | 222 | 5．0 | 2 | 30.0 | 333 | 35.0 | 389 |
| 0.1 | 1 | 5.1 | 57 | 10.1 | 112 | 15.1 | 168 | 20.1 | 223 | 25.1 | 279 | 30.1 | 334 | 35.1 | 90 |
| 0.2 | 2 | 5.2 | 58 | 10.2 | 113 | 15.2 | 169 | 20.2 | 224 | 25.2 | 280 | 30.2 | 336 | 35. | 391 |
| 0.3 | 3 | 5.3 | 59 | 10.3 | 114 | 15.3 | 170 | 20.3 | 226 | 25.3 | 281 | 30.3 | 337 | 35 | 392 |
| 0.4 | 4 | 5.4 | 60 | 10.4 | 116 | 15.4 | 171 | 20.4 | 227 | 25.4 | 282 | 30.4 | 338 | 35 | 393 |
| 0.5 | 6 | 5.5 | 61 | 10.5 | 117 | 15.5 | 172 | 20.5 | 228 | 25.5 | 283 | 30.5 | 339 | 35 | 394 |
| 0.6 | ¢ | 5.6 | 62 | 10.6 | 118 | 15.6 | 173 | 20.6 | 229 | 25.6 | 284 | 30.6 | 340 | 35. | 396 |
| 0.7 | 8 | 5.7 | 63 | 10.7 | 119 | 15.7 | 174 | 20.7 | 230 | 25.7 | 286 | 30.7 | 341 | 35.7 | 397 |
| 0.8 | 9 | 5.8 | 64 | 10.8 | 120 | 15.8 | 176 | 20.8 | 231 | 25.8 | 287 | 30.8 | 342 | 35. | 398 |
| 0.9 | 10 | 5.9 | 66 | 10.9 | 121 | 15.9 | 177 | 20.9 | 232 | 25.9 | 288 | 30.9 | 343 | 35.9 | 399 |
|  | 11 |  | 6 | 110 | 122 | 16.0 | 178 | 21.0 | 233 | 20.0 | 289 | 31.0 | 344 | 36.0 | 400 |
| 1.1 | 12 | 6.1 | 68 | 11.1 | 123 | 16.1 | 179 | 21.1 | 234 | 26.1 | 290 | 31.1 | 346 | 36.1 | 401 |
| 1.2 | 13 | 6.2 | 69 | 11.2 | 124 | 16.2 | 180 | 21.2 | 236 | 26.2 | 291 | 31.2 | 347 | 36.2 | 402 |
| 1.3 | 14 | 6.3 | 80 | 11.3 | 126 | 16.3 | 181 | 21.3 | 237 | 26.3 | 292 | 31.3 | 348 | 36. | 403 |
| 1.4 | 16 | 6.4 | 71 | 11.4 | 127 | 16.4 | $18:$ | 21.4 | 238 | 26.4 | 293 | i31．4 | 349 | 36.4 | 404 |
| 1. | 17 | 6.5 | 72 | 11.5 | 128 | 16. | 183 | 21.5 | 239 | 26. | 294 | 31. | 350 | 36 | 406 |
| 1.6 | 18 | 6.6 | 73 | 11.6 | 129 | 16.6 | 184 | 21.6 | 240 | 26.6 | 296 | 31.6 | 351 | $\because 6.6$ | 407 |
| 1. | 19 | 6.7 | 74 | 11.7 | 130 | 16.7 | 186 | 21.7 | 241 | 26 | 297 | 31.7 | 352 | 36 | 408 |
| 1.8 | 20 | 6.8 | 76 | 11.8 | 131 | 16. | 187 | 21.8 | 242 | 26.8 | 298 | 31.8 | 353 | 36.8 | 409 |
| 1.9 | 21 | 6. | 75 | 11.9 | 132 | 16.9 | 188 | 21.9 | 243 | 26.9 | 299 | 31. | 354 | 36.9 | 410 |
| 2.0 | 22 | 7.0 | 1 | 12.0 | 133 | 17.0 | 189 | 22.0 | 244 | 27.0 | 300 | 32.0 | 356 | 37.1 | 411 |
| 2.1 | 23 | 7.1 | 79 | 12.1 | 134 | 17.1 | 190 | 22.1 | 246 | 27.1 | 301 | 32.1 | 357 | 37.1 | 412 |
| 2.2 | 24 | 7.2 | 80 | 12.2 | 136 | 17.2 | 191 | 22.2 | 247 | 27.2 | 302 | 32.2 | 358 | 37.2 | 413 |
| 2.3 | 26 | 7.3 | 81 | 12.3 | 137 | 17.3 | 192 | 22.3 | 248 | 27.3 | 303 | 32.3 | 359 | 37 | 414 |
| 2.4 | 27 | 7.4 | 82 | 12.4 | 138 | 17.4 | 193 | 22.4 | 249 | 27.4 | 304 | 32.4 | 360 | 37.4 | 416 |
| 2.5 | 28 | 7.5 | 83 | 12.5 | 139 | 17.5 | 194 | 22.5 | 250 | 27.5 | 306 | 32.5 | 361 | 37 | 417 |
| 2.6 | 29 | 7.6 | 84 | 12.6 | 140 | 17.6 | 196 | 22.6 | 251 | 27.6 | 307 | 32.6 | 362 | 37.6 | 418 |
| 2.7 | 30 | 7.7 | 86 | 12.7 | 141 | 17.7 | 197 | 22.7 | 252 | 27.7 | 308 | 32.7 | 363 | 37.7 | 419 |
| 2.8 | 31 | 7.8 | 87 | 12.8 | 142 | 17.8 | 198 | 22.8 | 253 | 27.8 | 309 | $3 \cdot .8$ | 364 | 37.8 | 420 |
| 2.9 | 32 | 7.9 | 88 | 12.9 | 143 | 17.9 | 199 | 22.9 | 254 | 27.9 | 310 | 32.9 | 366 | 37.9 | 421 |
| 3. | 33 | 8.0 | 89 | 13.0 | 144 | 18.0 | 200 | 23.0 | 256 | 28.0 | 311 | 330 | 367 | 38.0 | 422 |
| 3.1 | 34 | 8.1 | 90 | 13.1 | 146 | 18.1 | 201 | 23.1 | 257 | 28.1 | 312 | 33.1 | 368 | 38.1 | 423 |
| 3.2 | 36 | 8.2 | 91 | 13.2 | 147 | 18.2 | 202 | 22.3 | 258 | 28.2 | 313 | 33.2 | 369 | 38.2 | 424 |
| 3.3 | 37 | 8.3 | 92 | 13.3 | 148 | 18.3 | 203 | 23.3 | 259 | 28.3 | 314 | 33.3 | 370 | 38.3 | 426 |
| 3.4 | 38 | 8.4 | 93 | 13.4 | 149 | 18.4 | 204 | 23.4 | 260 | 28.4 | 316 | 33.4 | 371 | 38.4 | 427 |
| 3.5 | 39 | 8.5 | 94 | 13.5 | 150 | 18.5 | 206 | 23.5 | 261 | 28.5 | 317 | 33.5 | 372 | 38.5 | 428 |
| 3.6 | 40 | 8.6 | 96 | 13.6 | 151 | 18.6 | 207 | 23.6 | 262 | 28.6 | 318 | 33.6 | 373 | 38.6 | 429 |
| 3.7 | 41 | 8.7 | 97 | 13.7 | 152 | 18.7 | 208 | 23.7 | 263 | 28.7 | 319 | 33.7 | 374 | 38.7 | 430 |
| 3.8 | 42 | 8.8 | 98 | 13.8 | 153 | 18.8 | 209 | 23.8 | 264 | 28.8 | 320 | 33.8 | 376 | 38.8 | 431 |
| 3.9 | 4：3 | 8.9 | 99 | 13.9 | 154 | 18.9 | 210 | 23.9 | 266 | 28.9 | 321 | 33.9 | 377 | 38.9 | 432 |
| 4. | 4 | 9.0 | 100 | 14.0 | 156 | 19.0 | 211 | 24.0 | 267 | 29.0 | 322 | 34.0 | 378 | 39.0 | 433 |
| 4.1 | 46 | 9.1 | 101 | 14.1 | 157 | 19.1 | 212 | 24.1 | 268 | 29.1 | ：23 | 34.1 | 379 | 39.1 | 434 |
| 4.2 | $4 i$ | 9.2 | 102 | 14.2 | 158 | 19.2 | 213 | 24.2 | 269 | 29.2 | 324 | 34.2 | 380 | 39.2 | 4：6 |
| 4.3 | 48 | 9.3 | 103 | 14.3 | 159 | 19.3 | 214 | 24.3 | 270 | 29.3 | 326 | 34.3 | 381 | 39.3 | 437 |
| 4.4 | 49 | 9.4 | 104 | 14.4 | 160 | 19.4 | 216 | 24.4 | 271 | 29.4 | 327 | 34.4 | 382 | 39 | 438 |
| 4.5 | $5:$ | 9.5 | 106 | 145 | 161 | 19.5 | 217 | 24.5 | 272 | 29.5 | $3 \geqslant 8$ | 34.5 | 383 | 39. | 439 |
| 4.6 | 51 | 9.6 | 107 | 14.6 | 162 | 19.6 | 218 | 24.6 | 273 | 29.6 | 329 | 34.6 | 384 | 39.6 | 440 |
| 4.7 | 52 | 9.7 | 108 | 14.7 | 163 | 19.7 | 219 | 24.7 | 274 | 29.7 | 330 | 34.7 | 386 | 39.7 | 441 |
| 4.8 | 53 | 9.8 | 109 | 14.8 | 164 | 19.8 | 220 | 24.8 | 276 | 29.8 | 331 | 34.8 | 387 | 39.8 | 442 |
| 4.9 | 54 | 9.9 | 110 | 14.9 | 166 | 19.9 | 221 | 24.9 | 277 | 29.9 | $3: 2$ | 34.9 | 388 | 39.9 | 443 |

TABLE NO．XLVI．
Cubic yards equal $\frac{(\text { height } \times r+b) 100}{12 \times 27}$ ．

Road－bed 24 feet wide．

|  |  |  | 気咢感 |  |  |  |  | $\begin{aligned} & \text { 淢 } \\ & \text { Ha } \end{aligned}$ | 苟皆 | ت̈ |  | 荷 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  | ． 7 |  |  |
|  | 7.4 |  | 9.0 |  |  |  |  |  |  |  |  | 30. | 6.7 |  |  |
|  | 7.5 |  | 9.0 | 10 | 10.6 |  |  | 20.2 | 13 | 25 |  | 30. | 16.7 |  |  |
|  | 7.5 | 5.8 | ． | 10.3 | 10.6 | 15.3 |  | 20. | 13 | 25. | ． 2 | 30.3 | 16.8 |  | ． 3 |
|  | 7.5 | 5. | 9.1 | 10.4 | 10.6 | 15.4 | 12 | 20 | 13 | 25 | 15.2 | 30.4 | 8 |  |  |
|  | 7.6 | J． |  | 10.5 | 10. | 15 | 12 | 20. |  | 25 |  | 30.5 | 16.8 |  |  |
|  | 7 |  | 9.1 |  |  |  |  | 20. |  | 25 |  | 30.6 | 16.9 |  |  |
|  | 7.6 |  | 9.2 |  |  |  |  | 20 |  | 25 |  | 30.7 | 6.9 |  | 8． |
|  | 7 | 5． | 9.2 |  | 10.7 |  |  | 20.8 |  | 25 | ． | 30. | 16.9 |  |  |
| 0.9 | 7. | 5.9 | ， | 10. | 0 |  |  | 20.9 | 13.9 | 5 | 4 | 30.9 | 16.9 |  | 18.5 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 6.1 | 9.3 |  |  |  |  | 2 |  |  |  |  |  |  |  |
|  | 7.8 | 6.2 | 9.3 |  | ． 9 |  |  | 21.2 |  | 26. | 155 | 31 | 7.0 |  |  |
|  | \％ | 6.3 | 9.4 |  | 10.9 |  |  | 21.3 |  | 26 | 15.5 | 31 |  |  |  |
|  | 7.8 | 6.4 | 9.4 |  | 10.9 | 16 | 12.5 |  | 14.0 |  | 15.6 | 31. | 17.1 |  | ． 6 |
|  | 7.9 | 6.5 | 9.4 | 11. | 11.0 |  | 12.5 | 21. | 14.0 | 26 | 15.6 | 31. | T |  | 7 |
|  | 7.9 | 6.6 | － | 11. | 11.0 |  | 12. | 21. | 14.1 | 26 |  | 31 | 17.2 |  |  |
|  | 7.9 | 6.7 | 9.5 |  | 11.0 |  |  | 21 |  |  |  | 31 | ， |  |  |
|  |  | 6.8 |  |  | 11.0 |  |  |  |  |  |  | 31 | 17.2 | 36.8 | ． 8 |
| 9 | 8. | 6.9 | 9.5 |  | 11.1 |  | 12 | 21.9 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 7.1 |  |  |  |  | 12 | 22 |  |  |  | 32 |  |  |  |
|  |  | 7.2 |  |  |  |  |  | 22 | 14 |  |  | 32 |  |  |  |
|  |  | 7.3 |  |  |  |  |  | 22 |  |  |  | 32 |  |  |  |
|  | 8.1 | 7.4 | 9.7 |  | 11.2 |  |  |  | 14.3 |  |  | 32 | 17.4 |  |  |
|  | 8.2 | 7.5 | ． | 12. | 11.3 |  |  | 22. |  |  | 15.9 | 32. | 17.4 |  |  |
| 2.6 | 8 | 7.6 | 9.8 | 12. | 11.3 | 17 | 12.8 | 22.6 |  |  | 15.9 | 32.6 | 17.5 |  | 0 |
|  | 8. | 7.7 | 9.8 | 12.7 | 11.3 |  | 12.9 | 22.7 | 14. | 27 | ． | 32.7 | 17.5 |  |  |
|  | 8 | 7.8 | 9.8 |  |  |  | 12.9 | 22 | 14. | 27 | － | 32.8 | 17.5 |  |  |
| 2.9 | 8. | 7.9 | 9.8 |  |  |  | 12.9 | 22.9 | 14. |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 8.4 | 8.1 | 9.9 | 13. | 11.5 |  | 13.0 | 23.1 | 14.5 |  | 16.1 | 33 | 176 |  |  |
|  | 8 | 8.2 | 9.9 | 13.2 | 11.5 |  | 13.0 | 23.2 | 14.6 |  | 16.1 | 33.2 | 17.7 |  |  |
|  | 8.4 | 8.3 | 10.0 |  |  |  | 13.1 | 23. | 14.6 |  |  |  |  |  |  |
|  | 8.5 | 8. | 10.0 |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 8.5 | 8. | ． |  |  |  |  |  |  |  | 10． | 33． | 17.7 |  |  |
|  | 8.5 | 8.6 | 0.1 |  | 1.6 |  |  |  |  |  |  |  |  |  |  |
|  | 8. | 8.7 | 10.1 |  | 11.6 |  |  |  |  |  | 16. |  |  |  |  |
| 3.8 | 8.6 | 8.8 | 10.1 | 13.8 | 11．7 | 18.8 | 13.2 | 23.8 | 14.8 | 28 | 16.3 | 33.8 | 17.8 | 38. | 19.4 |
| 3.9 | 8.6 | 8.9 | 10.2 |  |  |  | 13.2 |  | 14.8 |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 8.7 | ． 1 | 10.2 |  | 11. |  |  | 24.1 | 14.8 |  |  |  |  |  |  |
|  | 8.7 |  | 102 | 14.2 | 11.8 | 19. | 13.3 | 24.2 | 14.9 |  | ． | ． | 18.0 |  | 19. |
|  | 8.7 | 9.3 | 10.3 | 14.3 | 11.8 | 19.3 | 13.4 | 24.3 | 14.9 | 29 | 16. | 34.3 | 18.0 |  |  |
|  | 8. | 9.4 | 10.3 | 14.4 | 11.9 | 19.4 | 13.4 | 24.4 | 14.9 | 29 | 16 | 34.4 | 18.0 |  |  |
|  | 8.8 | 9.5 | 10.3 | 14.5 | ，11．9 | 19.5 | 13.4 | 24. | 15.0 |  | 16 |  |  |  |  |
|  | 8.8 | 9.6 | 10.4 | 14. | 11.9 | 19.6 | 13．5 | 24.6 | 15.0 |  | 16.5 |  | 18 |  | 619. |
|  | 8.9 | 9. | 10.4 |  | 11.9 | 19. | 13.5 | 24.7 | 15.0 | 29 | 16.6 | 34.7 | 18 |  | ¢19． |
|  | 8.9 | 98 | 10.4 | 8 | 12.0 |  | 13.5 | 24.8 | 15.1 | 29 | 16.6 | 34．8 | 18.1 |  |  |
|  |  |  | 10 |  | 12.0 |  | 13.5 | 4.9 | 15.1 | 29.9 | 16.6 |  | 18.2 |  | $919 .$ |

TABLE NO. XLVII.
Cubic yards equal $D^{2} 1 \times \frac{100}{27}$.
Side slopes 1 to 1 .

| D. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 | D. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 |  |  |  |  | 1 | 1 | 1 | 2 | 2 | 3 | 0 |
| 1 | 4 | 4 | 5 | 6 | 7 | 8 | 9 | 11 | 12 | 13 | 1 |
| 2 | 15 | 16 | 18 | 20 | 21 | 23 | 25 | 27 | 29 | 31 | 2 |
| 3 | 33 | 36 | 38 | 40 | 43 | 45 | 48 | 51 | 53 | 56 | 3 |
| 4 | 59 | 62 | 65 | 68 | 72 | \%5 | 78 | 82 | 85 | 89 | 4 |
| 5 | 93 | 96 | 100 | 104 | 108 | 112 | 116 | 120 | 125 | 129 | 5 |
| 6 | 133 | 133 | $14:$ | 147 | 152 | 156 | 161 | 166 | 171 | 176 | 6 |
| 7 | 181 | $18 i$ | 192 | 197 | 203 | 208 | 214 | 220 | 225 | 231 | 7 |
| 8 | 2:37 | 243 | 249 | 255 | 261 | 268 | 274 | 280 | 287 | 293 | 8 |
| 9 | 300 | 307 | 313 | 320 | 327 | 334 | 341 | 348 | 356 | 363 | 9 |
| 10 | 370 | 378 | 88.5 | 393 | 401 | 408 | 416 | 424 | 432 | 440 | 10 |
| 11 | 448 | 456 | 465 | 473 | 481 | 491) | 498 | 507 | 516 | $5 \geqslant 4$ | 11 |
| 12 | 5:33 | 543 | 5.11 | 560 | 569 | 579 | 588 | 597 | 607 | 616 | 1.2 |
| $1: 3$ | $6: 6$ | 636 | 645 | 655 | 665 | 6.5 | 685 | 695 | 705 | 716 | 13 |
| 14 | 72.5 | 76 | $74 \%$ | 757 | ¢68 | 779 | 789 | 800 | 811 | 822 | 14 |
| 15 | 833 | 844 | 856 | 867 | 878 | 890 | 901 | 913 | 925 | 936 | 15 |
| 16 | 848 | 960 | 9:2 | 984 | 996 | 1008 | 1021 | 1033 | 1045 | 10.58 | 16 |
| 17 | 1070 | 1083 | 1096 | 1108 | 1121 | 1134 | 1147 | 1160 | 1173 | 1187 | 17 |
| 18 | 1200 | 1213 | 1227 | 1240 | 1254 | 1268 | 1281 | 1295 | 1309 | 1323 | 18 |
| 19 | 1337 | 1351 | 1365 | $13 ¢ 0$ | 1394 | 1408 | 1423 | 1437 | 1452 | 1467 | 19 |
| D. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 | D. |

Cubic yards equal $D^{2} 1 \frac{1}{2} \times \frac{100}{27^{\circ}}$.
Side slopes $1 \frac{1}{2}$ to 1.

| D. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 | D. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 |  |  |  | 1 | 1 | 1 | 2 | 3 | 4 | 5 | 0 |
| 1 | 6 | 7 | 8 | 9 | 11 | 13 | 14 | 16 | 18 | 20 | 1 |
| 2 | 22 | 25 | 27 | 29 | 32 | 35 | 38 | 41 | 44 | 47 | 2 |
| 3 | 50 | 53 | 57 | 61 | 64 | 68 | 72 | 76 | 80 | 85 | 3 |
| 4 | 89 | 93 | 98 | 103 | 108 | 113 | 118 | 123 | 128 | 133 | 4 |
| 5 | 139 | 145 | 150 | 156 | 162 | 168 | 174 | 181 | 187 | 193 | 5 |
| 6 | 200 | 207 | 214 | 221 | 228 | 235 | 242 | 249 | 257 | 265 | 6 |
| 7 | 272 | 280 | $2 \div 8$ | 296 | 304 | 313 | 321 | 329 | 338 | 347 | 7 |
| 8 | 3515 | 36.5 | 374 | 383 | 392 | 401 | 411 | 421 | 430 | 440 | 8 |
| 9 | 450 | 460 | $4 \% 0$ | 481 | 491 | 501 | 512 | 5:3 | 5:34 | 54.) | 9 |
| 10 | 556 | 567 | 5:8 | 589 | 601 | 613 | 624 | 636 | 648 | 660 | 10 |
| 11 | 672 | 685 | 697 | \%09 | 722 | 735 | 748 | 761 | 774 | 787 | 11 |
| 12 | 890 | 813 | 827 | 841 | 8.4 | 868 | 88\% | 896 | 910 | 92.5 | 12 |
| 13 | 939 | 953 | 968 | 983 | 998 | 1013 | 1028 | 1043 | 1053 | 1073 | 13 |
| 14 | 103.3 | 1105 | 1120 | 1136 | 1152 | 1163 | 1184 | 1201 | $121 \%$ | 1233 | 14 |
| 15 | 1259 | 1267 | 1284 | 1301 | 1318 | 1335 | 1352 | 1369 | 1387 | 1405 | 15 |
| 16 | 1422 | 1440 | 1458 | 1476 | 1494 | 1513 | 1531 | 1549 | 1.568 | 1587 | 16 |
| 17 | 1606 | 1625 | 1644 | 1663 | 1682 | 1701 | $1 \% 21$ | 1741 | 1760 | 1780 | 17 |
| 18 | 1800 | 1820 | 184) | 1861 | 1881 | 1901 | 1922 | 1943 | 1964 | 1985 | 18 |
| 19 | 2006 | 2027 | 2048 | 2069 | 2091 | 2113 | 2134 | 2156 | 2178 | 2200 | 19 |
| D. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 | D. |

A Cross-section Book is indicated and represented (as to form, size, and arrangement) on the succeeding pages, which will be found useful and convenient for keeping both the field-notes and office computations by adopting the following method: In the seventh column is the elevation, 528.30, of the bench-mark; in the fourth columu is the back sight, 4.62; and in the second column their sum, or the height of instrument, 532.9\%. 'Iake the grade from the height of instrument and place the difference in the fourth column, and from this difference take the side fore sights, that are placed in the fifth column, to find the side cuts or fills. Taking the grade, 529.00 , at station 20 , from the height of instrument, the difference is 3.9 , the left fore sight is 5.5 , and 5.5 from 3.9 leaves -1.6 , or fill 1.6 , in sixth column, for the left side. The right fore sight, 4.1, placed under the left fore sight, taken from 3.9 leaves -0.2 , or fill 0.2 , in eighth column, for the right side. The road-bed is taken 14 feet wide, side slopes $1 \frac{1}{2}$ to 1 , and the left and right side distances, 9.4 and 7.3 , are placed in the sixth and eighth columns under the left and right fills. The center fill is supposed to have been previonsly found and copied into the cross-section book, but there is room to place a center fore sight in the fore-sight column ; this has been done at station $23+50$, where 2.2 is the center fore sight. Under the center cut or fill, seventh column, is a space for the center elevation, which it is sometimes convenient to have in the cross-section book.

The field-notes are all in the first eight columns; the remaining columns are for the computation of the earthwork quantities. Multiply the number found in the table of side triangles for the center height by the difference between the sum of the two side heights and twice the center height; add this product to the number found in the table of level cross-sections for the center height, when the sum of the two side heights is greater than twice the center height; subtract when it is less. For station 20 the sum of the side heights is 1.8 , ninth column, twice the center height is 2.0 , tenth column, and 2.0 from 1.8 leaves -0.2 , eleventh column. The number in Table IV for center height 1.0 is 15.7 , twelfth column, and the product of 15.7 by -0.2 is -3 , thirteenth column. The number in Table III for height 1.0 is $5 \%$, fourteenth column, and 3 from 57 leaves 54 , fifteenth column. In the same way we find 181, fifteenth column, for station 21 ; and $54+181=235$, fifteenth column, and half of 236 is 118 , seventeenth column, the answer in cubic yards by the common method of "averaging end-sections volumes." The cubic yards in the 100 feet between 21 and 22 have been computed by the method of "averaging endsections volumes" and then deducting the "prismoidal correction" for the
difference of center heights (see Article 8). The difference of center heights is 1.6, and in Table XXXVII, side slope $1 \frac{1}{2}$ to 1 , the number for 1.6 is 2 nineteenth column, and 2 from 263, eighteenth column, leaves 261, serenteenth column, answer in cubic yards. The cubic yards in the 100 feet between 22 and 23 are computed by the "prismoidal formula," Article 4. Twice the center height, 7.0 , tenth column, for the mid-section is found by adding the center heights of stations 22 and $23 ; 4.4+2.6=$ 7.0 , tenth column ; the difference 4.2 , eleventh column, is found by taking half the sum of the numbers in the eleventh column for stations 22 and 23 ; half the sum of 0.4 and 8.0 is 4.2 .

The number for the mid-section is 345 , fifteenth column, and 4 times $345=1380$; the number for station 22 is 346 , the number for station 23 is $i 34$, and the sum of 346,1380 , and 334 , eighteenth column, is 2060 , nineteenth column, and $2060 \div 6=343$, seventeenth column, the answer in cubic yards.

After the field-notes for a certain number of stations have been completed, first complete the twelfth column, and then the fourteenth column, from the tables for that number of stations, and then proceed to compute the quantities; this will be found the most rapid method. Where more than three heights are taken at a station, some of the columns can be ignored, and the small squares will be found useful for keeping the fieldnotes of very irregular cross-sections.


| Statiox. | $\underset{\text { Height }}{\substack{\text { Height } \\ \text { Inctunt. }}}$ | Grade. | $\begin{gathered} \text { Differ-। } \\ \text { eneeand } \\ \text { Baek } \\ \text { Sight. } \end{gathered}$ | Fore | Left. | $\begin{gathered} \text { Center } \\ \text { Elevation. } \\ \text { Elever } \end{gathered}$ | light. | $\begin{gathered} \text { Sum } \\ \text { Heighte } \\ \text { Heighs. } \end{gathered}$ | $\begin{aligned} & \text { Twice } \\ & \text { Center } \\ & \text { Height. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bench Mark. | 532.92 |  | 4.6 ~ |  |  | 5 28.30 |  |  |  |
| 20 |  | 529.00 | 3.9 | 5.5 | -1.6 | $-1.0$ | $-0.2$ | 1.8 | 2.0 |
|  |  |  |  | 4.1 | 9.4 | 528.0 | 7.3 |  |  |
| 21 |  | 530.00 | 2.9 | 7.1 | $-4.2$ | -2.8 | $-1.0$ | 5.2 | 5.6 |
|  |  |  |  | 3.9 | 13.3 | 527.2 | 8.5 |  |  |
| 22 |  | 531.00 | 1.9 | 8.5 | $-6.6$ | $-4.4$ | $-2.6$ | 9.2 | 8.8 |
|  |  |  |  | 4.5 | 16.9 | 526.6 | 10.9 |  | 7.0 |
| 23 |  | 532.00 | 0.9 | 5.9 | $-5.0$ | $-2.6$ | -8.2 | 13.2 | 5.2 |
|  |  |  |  | 9.1 | 14.5 | 5 29.4 | 19.3 |  |  |
| Turuing | 530.51 |  | 3.83 | 6.24 |  | 526.68 |  |  |  |
| +50 |  | 532.50 | -2.0 | 2.2 | $-12.6$ | $-4.2$ | -2.4 | 15.0 | 8.4 |
|  |  |  |  | 0.4 | $\pm 5.9$ | 528.3 | 10.6 |  |  |
| 24 |  | 533.00 | $-2.5$ | 11.7 | -14.2 | $-9.4$ | -6.2 | 20.4 | 18.8 |
|  |  |  |  | 3.7 | 28.3 | 523.6 | 16.3 |  |  |
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| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |


| Differ ence. | $\begin{aligned} & \text { Hyom. } \\ & \text { TruTe. } \end{aligned}$ | Product. |  | Volume. | Excaration. | Embaikmont. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | On oak, 70 | ft. Rt. Sta. 20 |
| $-0.2$ | 15.7 | -3 | 57 | 54 |  |  |  |  |
|  |  |  |  | 235 |  | 118 |  |  |
| -0.4 | 20.7 | -8 | 189 | 181 |  |  |  |  |
|  |  |  |  | $52 \%$ |  | 261 | 263 | 2 |
| 0.4 | 25.2 | 10 | 336 | 346 |  |  | 346 |  |
| 4.2 | 22.7 | 95 | 250 | 345 |  | 343 | 1380 | 2060 |
| 8.0 | 20.2 | 162 | 172 | 334 |  |  | 334 |  |
|  |  |  |  | 812 |  | 203 |  |  |
| 6.6 | 24.6 | 162 | 316 | 47 s |  |  |  |  |
|  |  |  |  | 15519 |  | 380 |  |  |
| 1.6 | 39.1 | 63 | 978 | 1041 |  |  |  |  |
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