

Feb. 1902.

Herbert T. Bardwell

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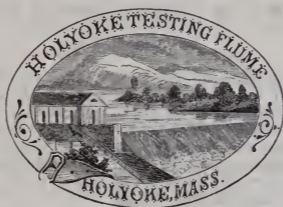
James Emerson

Greeting

TREATISE  
RELATIVE TO THE  
Testing of Water-Wheels  
AND  
MACHINERY,

ALSO OF

Inventions, Studies, and Experiments, with Suggestions  
from a Life's Experience.



BY JAMES EMERSON,  
WILLIMANSETT, MASS., U. S.

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*SIXTH EDITION.*

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PRICE, \$1.00.

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1894,

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Entered according to Act of Congress, September 20, 1894,

By JAMES EMERSON,

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A comparison of this work with any and all others treating of milling hydrodynamics, I think, will show that I have done more to make the matter a science than has been done by all other engineers that have lived during the past century. A few of the unthinking raised objections to the mixing of religion with business in the fourth edition, but it has ever seemed to me that any religion deserving of respect is good for everyday use, a comfort in sorrow, a joy in our pleasures. I have copyrighted the book that its contents may be kept together.

JAMES EMERSON.

## INTRODUCTION.

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Some ten years since, through the invention of an instrument for weighing the power required to drive machinery, I became interested in the testing of turbine water wheels. Previously such tests had only been possible for the wealthy. The apparatus used for the purpose, though expensive, was crude, clumsy and unreliable, while the formulas for computing water used were tedious for the initiated and impossible of application by the multitude, consequently few of those using wheels were able to demonstrate the absurdity of the fabulous claims made by the most of the turbine builders, and for years confusion had reigned, alike injurious to the manufacturer and honest builder. Years of experience that will be mentioned in the last part of this work made me fully aware of the task it would be to bring order out of such confusion; still the attempt was made, and has since been continued without a thought of abandonment. Those who have only witnessed the test of turbines at the Holyoke flume have little idea of the operation as conducted by engineers of the part; barrels of oil and a small army of assistants were required, so that the cost run up into the thousands. The average cost per wheel in 1869 was \$2,500. The superintendent of the Niles Iron Works of Cincinnati, O., came to me at Lowell, in order to make arrangements for the test of a Kindleberger wheel; he offered \$600, but under the then existing conditions it could not be done. Weeks and even months were consumed in the test of a single wheel. The experience that year convinced me that such expenditures of time and money were entirely unnecessary, and plans were soon completed for demonstrating that fact. Many ideas then prevalent had to be considered. In the first place, a testing flume with suitable apparatus was an expensive affair, while my means were very limited; then again it was supposed by all, that wheels of the same make were all of the same proportional efficiency, so that each builder would only need to have one wheel tested, consequently the patronage would be very irregular, while the expense would be constant, as experienced help would be required, and such help could only be retained by constant employment, or at least constant pay; the latter difficulty was surmounted by doing all of the most difficult and hardest work myself, simply employing a laborer for each test, while my daughter *timed*; kept the records of gauges during the trials, gave me the power every two minutes, in order to enable me to change the weight correctly, then made the computations and copied the results. This continued for a year or more; then Miss Charla A. Adams, "Charla" succeeded my daughter, and such success as I have had in aiding the improvement of turbines, by enabling builders of small means to ascertain the exact value of their numerous plans, and establishing the testing system, is due in a great measure to her unwearied patience, care and attention. She has had the entire mathematical part of the work to do, not only of the tests, but that necessary for the preparation of a large portion of the tables published in this work; she has kept records of all tests, and prepared numerous copies of the same for public institutions and for

turbine builders; in all, she has proved her fitness for the purpose, and not only her fitness, but woman's adaptability for such work. The practice of testing turbines has caused many changes and exploded many theories; of course this has not been done without destroying the hopes of many builders, at the same time it has been the means of bringing the best wheels prominently before the public. The tests have at all times been open to the public; builders have been desired to bring engineers to assist, and such have ever been welcome. It is a difficult matter to make purchasers realize that wheels made from the same patterns vary exceedingly in efficiency, yet there are few manufacturers ignorant of the fact that a wheel of any make doing well in a mill gives no assurance that another of the same make will give equal satisfaction. Ninety per cent. wheels are much sought for, but there are plenty of 80 per cent. wheels that will do far better than many that have given higher results. Ninety per cent. is only obtained under the most favorable conditions, and such can not be continued long in practical use.

Illustrations published in the first edition of this work have been found very convenient for reference in law and other cases, consequently a greater variety has been published in this edition.

That I know but little about the exact lines necessary for the production of a good turbine is not, perhaps, a legitimate excuse for the absence in this work of directions for turbine building, because the most minute formulas to be found upon the subject have undoubtedly been published by those who knew still less about it than myself, but such formulas seem to have hindered rather than to have aided turbine improvements, for it is very certain that the best turbine builders have given little heed to such formulas, hence I have not attempted to do what I could not do well.

Some of my Annual Reports were electrotyped, and various items from those have been used in this work, and where such reports of tests have been used, the numerous changes of weights are given in full; while in others only the best test at whole gate is given; and it may be well here to state that there is a certain speed at which any turbine does its best, and to find that point it is necessary to try many changes of weights. Wheels made from the same patterns seldom do their best at the same speed, and this variation is the cause of considerable loss of power through incorrect gearing for speed.

It is also necessary to state that there is always a leakage into the measuring pit during a test, which is to be deducted from the quantity flowing over the weir; this leakage may not be given in some of the reports, but if the depth on the weir is given, the difference between the quantity as found per tables for that depth, and the cubic feet given in the report of test will give the leakage, that is, if the length of weir is given. The omissions are owing to the use of only a part of the electrotyped reports.

JAMES EMERSON.

WILLIMANSETT, MASS., October 1, 1878.



## INTRODUCTION TO THE SIXTH EDITION.

The first edition of this work sold before it was out of the bindery, the second soon after it came out, over half of the fifteen hundred copies of the third edition within three weeks after it was issued; then I gave up my time to the purpose of finding a safe system for car heating, and for eleven years the electrotyped pages of my book were left without care, then were picked up and placed in the fourth edition as they could be found. The fourth and fifth editions were but stepping stones to this. I have desired to produce a work of value in which anyone taking it up can find something of interest. Years ago a widely known publisher informed me that technical or scientific works were seldom asked for except by the few interested in the subject treated, consequently were likely to remain upon his shelves until shopworn. It has been my study since to prevent such repose of my writings. I have shown something of my work that my claims for consideration may be estimated. Would it not be well for would-be leaders to do the same?

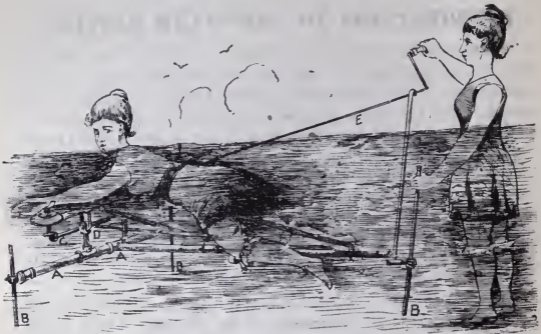
My wanderings and chances for observation have been wide, my reading extensive. I have found that from one to four hours sleep in each twenty-four is sufficient for me, consequently have been able to devote twenty of each twenty-four hours to study or thought, yet I have never found time to gain wealth or desire it.

If I have written slightly of Christianity, it is because I have studied its career from its foundation, if that can be determined within three centuries, without finding a single instance where it has benefited mankind. Of course I would not imply that there are not many good men and women that call themselves Christians, but how any intelligent person can recall the doings of the Christian devils who blotted out a higher civilization in Mexico and Peru, who annihilated the aborigines of this country, and who degraded and almost obliterated the Sandwich Islanders, and the shiploads of rum, rifles, gunpowder, Bibles and thin veneer of missionaries now being sent to Africa, and think Christianity less bloody than the superstition of Dahomey, is a mystery to me. Its blasphemous atonement hobby to me seems degrading to mankind and an impeachment of the Creator's wisdom and justice. Within fifty years I believe it will be considered an atrocity of the past.

JAMES EMERSON.

WILLIMANSETT, MASS., Oct. 1st, 1894.

## Emerson's Swimming Machine.



This device is designed particularly for women and children, though, of course, is equally suitable for men or boys. It gives the exact motions of the best swimmers, and is operated by a crank, as shown. It may be placed in a nursery tank or bath tub, or in a larger tank, where the water may be warmed for winter practice, or arranged singly or in groups like the merry-go-rounds near places of public amusement in the summer.

Men or boys may go to the rivers or ponds, strip and plunge in with but little restriction; women and girls are restrained by conventionalities from doing so, consequently have but little chance to learn to swim, though quite as capable as capable to do so as men or boys. Yet, as all travel, women are subject to the same dangers from shipwreck, the capsizing of boats, bridge disasters, etc., etc., as men.

All incapable of swimming cling together and drown in clusters, while if capable of swimming each would strive to keep apart as far as possible unless closing for the purpose of aiding the helpless.

The Kanaka children of the Pacific, like ducks, learn to swim almost as soon as born, giving their mothers little cause for anxiety about being in the water. Are our mothers less intelligent than those natives?

Every mother would enjoy seeing her wonderful baby swim, which is easily practicable with a nursery swimming machine for the bath tub. What beautiful sights the surf at our beaches would present summers if our home mermaids would all learn to swim and laughingly sport in the waves instead of as now shudderingly step into the water half way up to the knees, then squeal, as graphically expressed by a lady acquainted with the ways of lady bathers. Learn to swim at home in the winter, then have pleasant times at the beach in the summer.

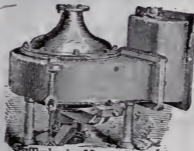
## EVOLUTION OF WATER WHEELS.



Hercules Wheel.



Houston Wheel.



Tyler's New Scroll



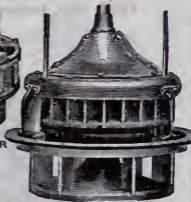
American



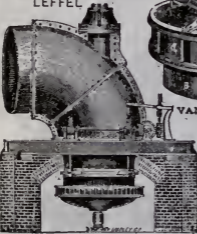
LEFFEL



VANDEWATER



Swain.



Boyden Fourneyron



JONVAL



FLUTTER WHEEL



UNDERSHOT WHEEL



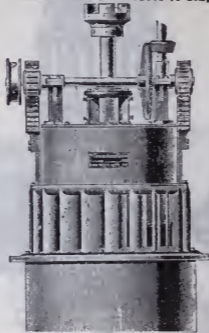
OVERSHOT WHEEL

T. H. Risdon and others whose names are familiar to manufacturers are entitled to much credit in connection with improvements of the turbine, but they used modified combinations of the illustrated devices above in which to obtain the results credited them in this work.

# MCCORMICK'S IMPROVED TURBINES,

1898

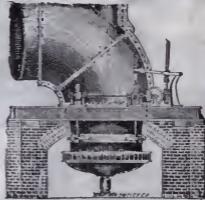
The Practical Effect of Efforts to Improve,



Fallen Idols, Destroyed by the Iconoclastic Testing System.



Fourneyron Wheel.



OVERSHOT WHEEL

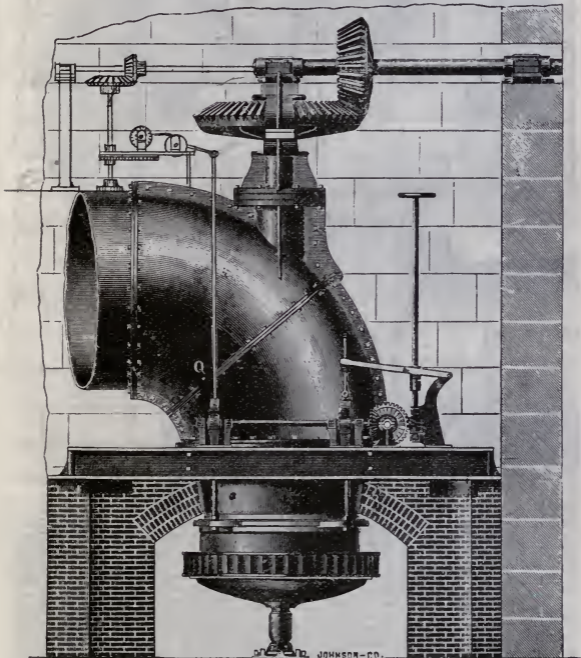


Uriah A. Boyden did much to establish faith in the practicability of determining the efficiency of turbines by tests, but his ideas were extravagantly expensive, and impracticable with ordinary means. There is no evidence however that he ever gained higher efficiency than that obtained by M. Fourneyron.

## BOYDEN'S

## IMPROVED FOURNEYRON TURBINE.

WITH EMERSON'S MEASURING, GATE REGISTER.



The White Elephant of the Lowell Corporations.

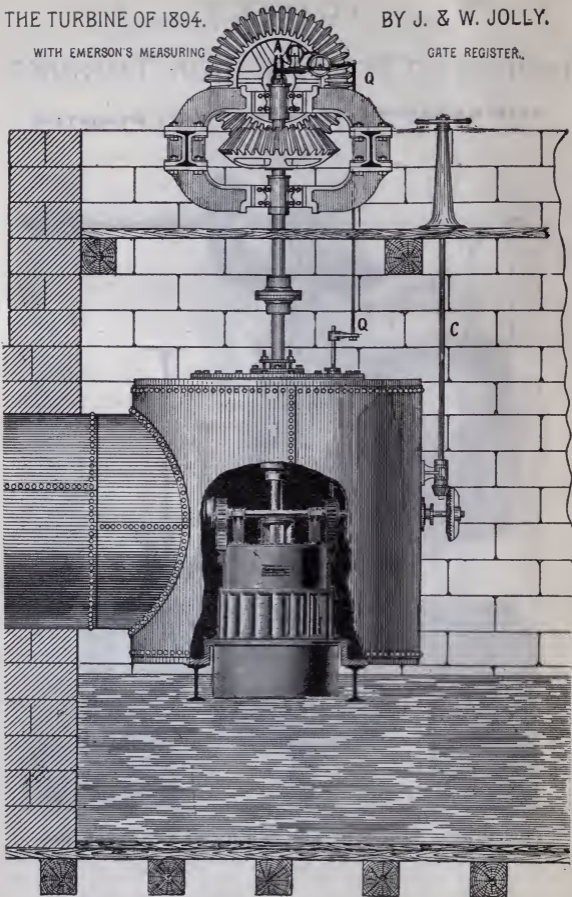


## THE TURBINE OF 1894.

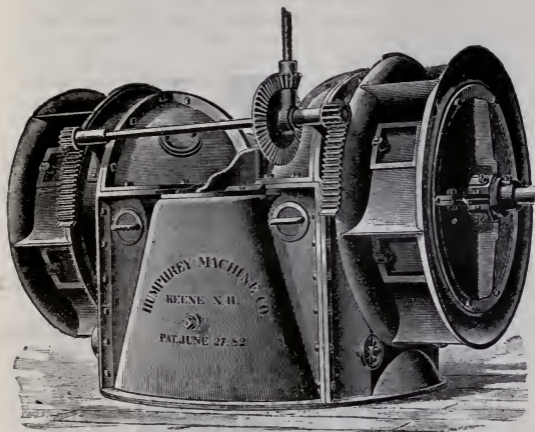
BY J. &amp; W. JOLLY.

WITH EMERSON'S MEASURING

GATE REGISTER.



## Horizontal Wheels.

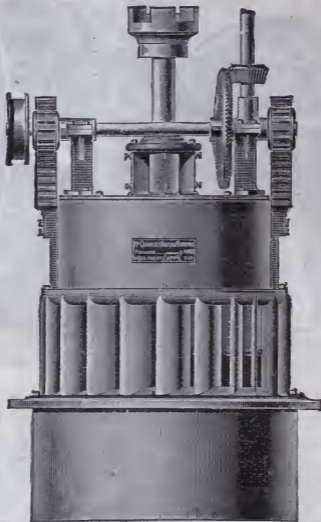


For a few years past there has been a craze for twin horizontal wheels, as was the case a few years ago for V shaped belts. For high falls and small wheels it may be well to have such, but for ordinary falls and wheels there is little to show in their favor, unless in coarse work such as pulp mills, where the grinder is placed upon the same shaft as the wheels, doing away with belts or gears; but good gears cause but little loss in transmission, say two per cent., and open belts not more than four, while the loss in horizontal wheels would be double that at least. See tests, page 351. In a recent case in litigation at Willimantic, Conn., a pair of Humphrey twin wheels tabled to transmit 100 h. p. under the 17 feet working head there were put into a mill supposed to require the power named. The wheels proved insufficient and two of tabled 125 h. p. capacity were substituted; those drove the machinery leaving but little surplus power. The race above was  $12\frac{1}{2} \times 6$  feet deep, the tail race  $6\frac{1}{2} \times 2$  feet depth of water, the velocity above was estimated one foot, below at six feet per second, or 72 cubic feet per second plump. From my knowledge of the Humphrey wheel, also of the loss from being placed upon horizontal shaft, my estimate was 35 per cent. efficiency.

An expert used to testing the same kinds of machinery in the linen mill there was put upon the witness stand. He knew nothing of our previous estimates, yet he estimated the force required to drive the machinery in the mill at 39 h. p.

Adding 25 per cent. to his estimate for driving the shafting, or say 9 h. p., which would be proper, as the mill had its full supply of shafting, though but partially filled with machinery, and his estimate would agree substantially with mine. Other wheels undoubtedly do much better, but for general use I think time will prove the turbine much the most economical; the plan is mechanically imperfect. All used to testing wheels know how the efficiency is cut down by the least rub at the side of curb, and the weight must soon cause the bearings and shaft to wear down, the lower side of the wheel will rub, and the upper side will be open and leaky.

**J. & W. Jolly's Holyoke Turbine, Holyoke,  
Mass., U. S.**



As the Messrs. Jolly unquestionably stand at the head as turbine builders, not only in this but in all other countries where turbines are known, this work would be incomplete without a brief account of their rise and method of doing business, in connection with the illustrated evolution and description of such improvements during the past half century.

JAMES EMERSON.

WILLIMANSETT, July 1, 1894.



## The Holyoke Turbine, Manufactured by J. & W. Jolly.

This turbine has been brought to its present perfection through the continuous labor of John B. McCormick, under the supervision and at the expense of the Messrs. Jolly, and is now without question the most perfect water wheel in existence. It has no pretended equal, and is so known throughout this country and the British Provinces, and has become so well known in Europe that the call for wheels from there the present season has kept the old shop of the Messrs. Jolly in constant operation during the past depression in business and a new shop has been opened for home work.

This turbine in name is made by several other builders and in fact is but the Hercules improved, yet the proximity of the testing flume and the enterprise of the Messrs. Jolly to make use thereof have caused their wheels to stand upon a plane not reached by any of their competitors and with such certainty that they will test against any and all contestants upon the conditions that the owners of the inferior wheel shall pay the expense for testing both wheels, and that from five to twenty-five per cent. will be allowed each contestant at the start, the exact allowance being determined by the make of wheel. So well is the fact of the superiority of Messrs. Jolly's wheel established that the Rodney Hunt Machine Co., of Orange, Mass., one of the largest turbine building firms in the past of the country, finding that the intelligent manufacturers of the times have come to realize the difference between the turbine of twenty years ago and the Jolly wheel of to-day, have contracted with the Messrs. Jolly for turbines with which to supply their customers instead of trying to force their own of inferior make upon those sufficiently intelligent to desire the best. This act speaks well for the honor and fair dealing of the Hunt company and opens the way for a new departure for turbine builders of the old styles that lack testing facilities that may enable them to produce turbines of modern efficiencies and capacities. An old style turbine builder of moderate intelligence trying to sell turbines of the past must feel something as the ancient blacksmith with his pod augers of Revolutionary days would feel if brought into competition with the effective and highly finished auger bit of the present time.

The certified tests published upon the next page represent the guaranteed capacities and efficiencies of several sizes of the Jolly turbines, and all of the many sizes have been or will be brought to the same standard before being offered for sale.

HOLYOKE, MASS., U. S., 1894.

Copied from certified tests made on the dates named, and signed by  
A. F. SICKMAN, engineer in charge of experiments, E. S. WATERS, Hyd. E.  
The originals of these certificates can be seen at any time at our office.

J. & W. JOLLY, HOLYOKE, MASS.

| Test of a 12-inch Wheel.        |       |               |              |                     | Jan. 8th, 1890.           |
|---------------------------------|-------|---------------|--------------|---------------------|---------------------------|
|                                 | Head. | Rev. per Min. | Horse Power. | Cubic feet per Sec. | Per Cent.                 |
| Whole Gate,.....                | 18.02 | 455.7         | 17.00        | 9.82                | 84.73                     |
| Part Gate,.....                 | 18.10 | 420.0         | 14.71        | 8.60                | 83.34                     |
| “ “ .....                       | 18.10 | 469.7         | 11.45        | 7.25                | 76.91                     |
| “ “ .....                       | 18.18 | 376.5         | 8.60         | 6.01                | 69.41                     |
| “ “ .....                       | 18.28 | 336.7         | 6.15         | 4.74                | 62.62                     |
| Test of a 27-inch Wheel.        |       |               |              |                     | April 21st, 1891.         |
| Whole Gate,.....                | 15.16 | 179.50        | 73.21        | 52.30               | 81.42                     |
| Part Gate,.....                 | 15.13 | 195.75        | 66.38        | 45.85               | 84.38                     |
| “ “ .....                       | 15.19 | 191.50        | 57.04        | 40.05               | 82.68                     |
| “ “ .....                       | 15.24 | 179.25        | 46.00        | 34.30               | 77.60                     |
| “ “ .....                       | 15.31 | 171.00        | 32.91        | 27.58               | 68.73                     |
| Test of a Second 27-inch Wheel. |       |               |              |                     | Nov. 18th and 19th, 1891. |
| Whole Gate,.....                | 16.83 | 187.75        | 84.63        | 54.74               | 80.99                     |
| Part Gate,.....                 | 17.14 | 194.25        | 80.46        | 49.57               | 83.49                     |
| “ “ .....                       | 17.21 | 180.00        | 69.07        | 43.97               | 80.48                     |
| “ “ .....                       | 17.44 | 184.00        | 56.04        | 37.50               | 75.55                     |
| “ “ .....                       | 17.68 | 181.50        | 40.91        | 30.26               | 67.41                     |
| Test of a 33-inch Wheel.        |       |               |              |                     | June 13th, 1890.          |
| Whole Gate,.....                | 14.57 | 140.00        | 101.36       | 74.60               | 82.30                     |
| Part Gate,.....                 | 14.87 | 144.50        | 95.83        | 67.99               | 83.65                     |
| “ “ .....                       | 14.98 | 138.50        | 82.58        | 59.91               | 81.21                     |
| “ “ .....                       | 15.06 | 145.33        | 65.43        | 50.48               | 75.96                     |
| “ “ .....                       | 15.35 | 134.50        | 47.46        | 39.94               | 68.32                     |
| Test of a 39-inch Wheel.        |       |               |              |                     | April 1st, 1891.          |
| Whole Gate,.....                | 16.60 | 124.40        | 179.74       | 118.72              | 80.41                     |
| Part Gate,.....                 | 16.77 | 127.25        | 166.79       | 105.49              | 83.13                     |
| “ “ .....                       | 17.14 | 126.33        | 146.33       | 92.57               | 81.31                     |
| “ “ .....                       | 17.34 | 125.75        | 122.66       | 81.11               | 76.89                     |
| “ “ .....                       | 17.65 | 112.33        | 89.03        | 64.68               | 68.76                     |
| Test of a 48-inch Wheel.        |       |               |              |                     | Oct. 10th, 1892.          |
| Whole Gate,.....                | 13.44 | 89.12         | 198.16       | 162.13              | 80.21                     |
| Part Gate,.....                 | 13.84 | 90.50         | 187.44       | 145.25              | 82.24                     |
| “ “ .....                       | 13.64 | 89.50         | 154.29       | 124.88              | 79.90                     |
| “ “ .....                       | 14.19 | 92.37         | 128.86       | 105.60              | 75.85                     |
| “ “ .....                       | 14.58 | 88.62         | 99.87        | 86.80               | 69.61                     |
| Test of a 51-inch Wheel.        |       |               |              |                     | June 28th, 1890.          |
| Whole Gate,.....                | 11.62 | 84.50         | 185.17       | 166.50              | 84.56                     |
| Part Gate,.....                 | 12.99 | 87.62         | 197.34       | 157.32              | 85.32                     |
| “ “ .....                       | 13.09 | 83.00         | 171.77       | 140.72              | 82.39                     |
| “ “ .....                       | 13.17 | 88.00         | 139.27       | 119.80              | 77.99                     |
| “ “ .....                       | 13.93 | 84.25         | 110.26       | 98.72               | 70.84                     |
| Test of a Second 51-inch Wheel. |       |               |              |                     | March 5th, 1891.          |
| Whole Gate,.....                | 12.13 | 85.50         | 198.04       | 173.12              | 83.16                     |
| Part Gate,.....                 | 12.26 | 81.50         | 176.36       | 153.28              | 82.75                     |
| “ “ .....                       | 12.19 | 80.20         | 144.21       | 131.23              | 79.49                     |
| “ “ .....                       | 12.35 | 77.50         | 111.02       | 109.38              | 72.47                     |
| “ “ .....                       | 12.48 | 73.12         | 81.56        | 87.90               | 65.56                     |

## John B. McCormick and Esoteric Science.

As producer of the most perfect water wheel, Mr. McCormick's name is likely to have a niche in the temple of turbine fame. No other person has had such chance to observe the effect of slight changes of construction and position of parts, yet, after causing the expenditure of a hundred and fifty thousand dollars in experimenting, should some accident destroy the patterns for his turbine the whole would have to be done over again upon the same "Cut and try" system, for not a drawing exists that would enable another to reproduce his results.

Who is to blame for this esoteric state of that science? We have just emerged from the bondage of superstition but, far from being freed therefrom, we are in a haze of mysticism. We may smile at the science of Lucretius or the elder Pliny, but a century hence I venture to predict that there will be cause for broad laughter for those who look back to the popular notions of to-day. A half century since, had a visionary crank hinted at the use of the bicycle or the telephone so common to-day it is easy to imagine the wise sneer of the Huxley type of scientist of the time.

Who will explain the fact that the turbine often does considerable work while running faster than the water that drives it, and at its best returns over ninety per cent. of the force expended?

Who can explain the cause of gravitation or cohesion, or disintegration and cohesion, as daily utilized in the electrotypers' art? Never was there the utterance of a weaker mess of bosh than that Newton discovered the law of gravitation; he simply discovered its effect in some cases, but as to its cause we know no more than was known by Pythagoras. I have seen the Andes mountains, every line, peak, and shadow sharply defined as though not ten miles distant, yet I was sailing a thousand miles away. Who will lucidly explain the cause of mirage? I believe such mirage is evidence that science will produce the means for seeing distant objects as we talk by telephone. A few years since double turbines were the rage, but science proved the idea to be erroneous, as I believe it will do with the "triple expansion" hobby; but let it be understood that steam compared to hydraulic science is in its childhood. Water as a motor returns ninety per cent. of its weight, steam but ten or fifteen per cent. of its heat force.

I have seen tables and chairs move without visible force being applied to cause the movement. I have seen the arms of a man placed through the arms of a chair; the hands tied firmly together; then wound over with adhesive plaster by the late J. C. Ayer; on turning off the light the hands were instantly withdrawn from the chair without separation of hands. I believe this was done through natural law not yet understood and that its study will aid in the understanding of the law of cohesion and disintegration, but the cause will be made clear through the crank instead of by the popular scientist.

## Emerson's Measuring Gate Register.

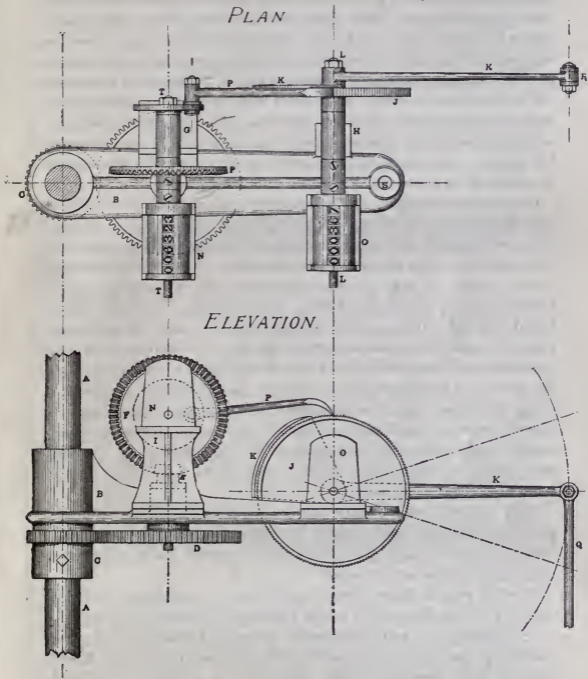
### Description and Operation.

The illustrations show plan and elevation, also connections to turbine gate.

In the elevation the bed-plate B is shown upon the wheel shaft A above the driving gear C, which drives gear D, on the arbor of which, back of the upright stand I, may be seen, represented by dotted lines, a small bevel pinion working into bevel gear F, the arbor of which is connected to the arbor of the counter N, which counts one for every ten revolutions of the turbine wheel shaft. On the end of the gear and counter arbor T, there is the disk or crank G, that through the catch P actuates the ratchet wheel J, which has some number of teeth equably divisible by ten, preferably two or more hundred, that the loss of a fraction of tooth may be as small as possible. The movement of the catch P is exactly one-tenth of the circumference of the ratchet, or twenty teeth of the two hundred in its periphery, consequently ten full strokes of the catch P give the ratchet wheel J a complete revolution, and an increase of one in the number shown by the counter O, or an increase of one for each hundred revolutions of the turbine shaft. An examination of the Holyoke turbine, second page, will show the connection of its gate with the shield K of the register by the rod Q. The rod C is the ordinary gate rod for opening the gate by hand. As the gate is raised the rod Q moves the shield K in proportion to the opening of the gate under the actuating catch P, and, of course, proportionally reducing the rotation of ratchet wheel J, consequently more movements of the catch P will be required to give the ratchet wheel J a complete revolution and change of figure on the counter O. At the close of any trial add a cipher to the sum shown by the counter N, and the revolutions of the wheel shaft will be given; add two ciphers to the product of the counter O, and, if the wheel has run with full gate during the whole trial, the representations of the two counters will be the same, but if the gate has been but partially open during the time, then the product of the counter O will be proportionally less, and a division of that sum by the greater sum shown by the counter N will give the true average percentage of gate opening during the time the count has been kept. For untested wheels it will be necessary to make such test to obtain the proportional discharge, but that will simply require a weir and control of wheel and discharge by the ordinary work of the mill.

MAY 1, 1894.

## EMERSON'S MEASURING GATE REGISTER



(For particulars apply to J. & W. Jolly, Holyoke, Mass., U. S.)

## Obsolete Methods of Lowell Water Power.

A prominent excuse for the low standard of wages paid the operatives at Lowell is the continued use of obsolete machinery and appurtenances. Now arises the question, Why this continuance? Why continue the use of turbines that waste water to such an extent that three thousand horse power have to be made good by burning thousands of tons of coal? Why go to Lawrence for an engineer to divide the Lowell water power when that engineer in twenty years has not made one step in advance towards simplicity, accuracy, and economy, when the division can be made by modern improvements at a tithe of the cost of the obsolete methods of Lawrence and with far greater accuracy?

Gentlemen, managers of the Lowell corporations, it is well to stop and consider at times. Early in the century, for the purpose of encouraging home manufactures, the control of the beautiful Merrimac river was given to a few capitalists; it naturally belonged to the people. It was pure, stocked with fish that any one might catch and enjoy as healthy food. Your works polluted its waters, killed the fish, and poisoned the atmosphere; and for this what return is made the true owners of the river? High salaries to a comparatively few officials and starvation wages to the many upon the excuse of continued use of obsolete machinery and methods of doing business. Is there any pretense that the corporations of Lowell have not paid fair returns for the money invested or are unable with intelligent management to have the use of the best machinery known as well as the most perfect turbines for the economy of its water power?

Why foolishly waste water power that justly belongs to the people, then uselessly expend large amounts to purchase coal to make the unnecessary waste good, then plead poverty as an excuse for low wages to your operatives?

Why do you do these things unless for the purpose of living in not only sylvan shades but in the retirement of grassy streets?

The puerility of your excuses for your low standard of wages is made so palpable by the yearly building of new mills at Fall River, and the rapid growth of that city, which is caused by the large profits obtained through the acceptance of your standard of remuneration of labor, that you even ought to be able to see the point, at any rate the laborer will see it, and the laboring class will ever have the most votes, and if the people gave the people can take away.



## Engineers with Many Gauge Hands.

After a century of conjecture, wild theories, and experimenting for the purpose of finding the most perfect engine of transmission of the power evolved from falling water, the Hercules type of turbine is accepted as the best. Reputable builders of intelligence are now trying to excel with that; to do so each builder should have a testing flume near by, for power is expensive, and the amount should no more be left to conjecture than is that of gold, coal, wool, or groceries.

A far better class of engineers is needed than such as has been dumped out by our colleges and schools for the last half century. Can any one of the lot be named who has made any improvement in milling hydraulics, dynamics, or machinery, or for ascertaining the power used, or for economy, accuracy, or convenience? A turbine of any size, proportionally changed, should give the same efficiency for any other size, but the "cut and try" system of building still continues. An engineer of the college class is best described by the term "Fussy," much formula, and many decimals.

Under the head of the testing system described in this work, two series of tests of a Leffel wheel may be seen, one by Hiram F. Mills, with a small army of gauge hands, the other by myself; my figures being taken from the same gauge hands, a difference of six per cent. is shown; that difference I have never been able to reconcile to myself satisfactorily.

The Victor turbine has furnished me a still stronger case. One of the make, a fifteen inch, was furnished to make gear, belt, and draft tube experiments reported in this work; it gave the remarkable efficiency of 92.58 per cent. Many experts with schools and colleges witnessed its trial; it was taken from flume, reset, and retested over and over. Another wheel made from the same patterns was then procured and tested; that gave 76.57 per cent. Of course such a difference caused a great sensation and inquiry; the ninety-two per cent. wheel was then set and again tested to make sure the apparatus was in order; less than one-fourth of one per cent. difference was found in the test of that wheel. A third fifteen inch was then tried that gave 77 per cent. and a trifling fraction over; then a twenty inch was tried that gave a little over 79 per cent. A few days later, during my absence, the wheels were reset and tested by Clemens Herschel; he, like Mills, required many gauge hands; he reported the efficiency of the three wheels a fraction above 86, 87, and 89 per cent. On my return, William A. Chase, agent of the Water Power Company, was called in to aid in making a retest of the wheels; the second fifteen inch wheel was set and tested, Mr. Chase keeping the time by a stop watch; the wheel gave an efficiency of 76.34, or less than one-fourth of one per cent. difference between that and its first trial. During the first ten years of the testing system various parties retested the same wheel as new, for the purpose of breaking up the system if it proved unreliable; it still continues, but three operators are sufficient in a properly constructed testing flume for reliable work.

## The Testing System.

Having terminated my connection with the business of testing turbines, it may be well to give a brief account of the conception of the business as a system.

Such tests were made in Europe early in the present century; in this country, by Uriah A. Boyden, from 1843 to 1859. I have found it impossible to obtain any authentic record of Mr. Boyden's tests, though there are rumors of fabulous results. Mr. Francis, in the work called "Lowell Hydraulic Experiments," states that data furnished him for computation gave 88 per cent. He does not vouch for the data furnished, nor does it appear that such data was furnished by a disinterested engineer in any case. Mr. Francis followed Mr. Boyden in making such tests, but he, like the former, made them so expensive as to be beyond the reach of any but wealthy corporations, while the manufacturing interest required a definite knowledge of the efficiency of the various kinds of turbine plans then springing into existence.

In 1859-60, the city of Philadelphia gratuitously tested a variety of small wheels for different builders, but the plan for doing it was so defective that the tests had but little influence. In 1867, the Chase Turbine Co., of Orange, Mass., employed me to construct a dynamometer or brake for testing turbines. The friction bands that may be seen on the ship windlass, in another part of this work, gave me the idea of controlling a turbine in that way, for I had brought many a ship to by such bands. The Prony brake had never been heard of by me at that time, nor until my brake was completed.

In 1868, A. M. Swain asked me to get up a suitable brake, and test one of his wheels at Putnam, Ct. Six months' time and \$1,700 were expended in preparing the instrument. The company was persuaded to construct a flume at the "overflow" of the Wamesit Power Co., Lowell, Mass. A 42-inch Swain wheel was set, and tested by Mr. Swain and myself. The results were such that the company was urged to employ an engineer with at least a theoretical knowledge of such tests. H. F. Mills, then of Boston, was selected for the purpose. The company then held a meeting and authorized Mr. Swain and myself to make arrangements for a public trial, and the following notice was issued:

**IMPORTANT TEST OF TURBINE WATER WHEELS, AT LOWELL, MASS.,**  
JUNE 16, 1869.

SIR: The Swain Turbine Co. has just completed extensive arrangements for a competitive test of Turbine Water Wheels. A flume and weir of the most approved plan, to supply and measure the water used, has been constructed. Emerson's Dynamometer will be used to test the power of the wheels.

The "pit" is fourteen feet in width; head of water varying from twelve to sixteen feet. Each competitor will select size and finish of wheel to suit himself. The Swain Wheel to be tested was built before the test was thought of, and is in no way superior to the average of wheels furnished by the company. It is forty-two inches in diameter, and will be tested on the 16th day of this month.

The Swain, Leffel, Bodine-Jonval and Bryson Turret wheels were entered. The measuring pit was fourteen feet wide, thirty in length and at first a little over three feet in depth below crest of weir—the wheels, standing inside at the upper end in a quarter turn or iron flume, being about twenty feet from the weir. In this distance there were three separate racks to check the rushing water.



The Swain wheel had thin sheet steel buckets, which made it very light for its diameter; yet, when set, it was barely possible to turn it by the coupling upon the top of its shaft—the coupling being twenty inches in diameter, made that size to connect with brake. Mr. Swain “guessed the wheel would go, only put the water to it.”

The Leffels knew better than to lose fifty or a hundred pounds in that way, so, when their wheel was set, it turned about as easy as a child's top. Of course, an engineer of experience would have refused to have tested a wheel running as hard as the Swain did, or to have tested a wheel of that size at all in a pit so small and filled with racks, for a good wheel would have little chance against one of low efficiency. The working surfaces of the brake and band were made of steel and iron. Both being fibrous, little strips tore from each, often checking, and at times bringing the wheel to a sudden stop, so that it was difficult to make steady tests of many minutes' duration. A bell was connected to the wheel-shaft, which struck at each fifty revolutions of the wheel. Instead of making each test with a given weight separate and distinct by itself, observers were placed at the different gauges, with watches set to the same time. As the wheel ran very unsteady at the best—often stopping entirely—it was necessary to reject many of the observations, and it will readily be seen that the difficulty would be in placing the right patches together. That this is not imaginary, the following tables of results are given. The first is a copy of Mr. Mills' report, the second is a record of tests taken by myself, the same gauge hands being employed in each case, and the conditions being precisely the same for both. My tests, however, were taken upon the same plan that I have followed continuously for more than ten years: that is, to make each test for a given weight complete and distinct in itself. Mr. E. A. Thissel made a record of the gauges, as given by each of the hands employed, and as it agreed exactly with the notes I had taken of all, his record is given in the table.

#### MODE OF CONDUCTING THE EXPERIMENTS.

Observers were stationed at various points, as follows:

Mr. J. B. Hale, at the hook-gauge, observed every minute, and a part of the time every thirty seconds, the reading of the hook-gauge, which indicated the depth of water upon the weir.

Mr. R. A. Hale observed the height of the water in the forebay and in the pit, by means of the scale (D) passing from the lower box to the upper every minute.

Mr. E. A. Thissel noted the time of the striking of the bell, which indicated the speed of the wheel, to the nearest quarter second.

Mr. James Emerson, by means of the hand-wheel (M) regulated the friction so that the index (E) should be kept as near to zero as possible, and thus the scale beam be kept level.

Another assistant observed as rapidly as possible the actual position of the index during the experiment.

Another kept the oil cups (T) supplied with oil, and, by a cock attached to each, regulated the amount flowing upon the friction surfaces.

Another attended the gate and kept the racks clear of obstructions.

The writer kept a record of the weights in the scale-pan, the heights of gate, all irregularities in the motion or disturbing causes of any kind that would affect the results of the experiment, and sufficient observations of each class to check the accuracy of all of the notes.

At intervals, during a series of experiments, all of the watches were compared with the standard, and differences noted, that there might be no difficulty in selecting the observations which applied to the time when the conditions for accurate results obtained. Recorded in the following manner:

EXPERIMENTS UPON THE 40-INCH LEFFEL WHEEL, AT LOWELL, MASS.

| Date.<br>1869. | Temp.<br>of<br>Water. | Fah. | Opening<br>of<br>Gate. | TIME. |      |      |       |              |            | Duration<br>of<br>Experi-<br>ments. | Total<br>No.<br>Revolu-<br>tions. | No.<br>Rev. of<br>Wheel<br>per<br>second. | Weight<br>in<br>Scale.<br>Pounds. | HEIGHT OF<br>WATER. |       | Fall<br>acting<br>on<br>Wheel. | Depth<br>of<br>Water<br>on<br>the<br>Weir. | Quan-<br>of<br>Water<br>passing<br>the<br>Weir.<br>c. ft. per<br>sec. | Rel.<br>Veloc | Rates<br>of<br>useful<br>effect.<br>to the<br>power<br>expen-<br>ded. |
|----------------|-----------------------|------|------------------------|-------|------|------|-------|--------------|------------|-------------------------------------|-----------------------------------|---|-----------------------------------|---------------------|-------|--------------------------------|--|---|---------------|---|
|                |                       |      |                        | FROM. |      | TO.  |       | In<br>Flume. | In<br>Pit. |                                     |                                   |   |                                   |                     |       |                                |  |   |               |   |
|                |                       |      |                        | Hour. | Min. | Sec. | Hour. |              |            |                                     |                                   |   |                                   | Min.                | Sec.  |                                |  |   |               |   |
| Oct. 11.       | 59°                   |      | 2.25                   | 12    | 19   | 15.0 | 12    | 22           | 57.5       | 222.5                               | 500                               | 2.2471                                    | 80.0                              | 15.575              | 1.140 | 14.435                         | 1.099                                      | 38.013  | .788          |   |
| " "            | "                     | "    | "                      | 12    | 23   | 27.0 | 12    | 29           | 46.0       | 319.0                               | 850                               | 2.2427                                    | 80.0                              | 15.563              | 1.140 | 14.423                         | 1.098                                      | 37.963  | .773          |   |
| " "            | "                     | "    | "                      | 12    | 39   | 32.0 | 12    | 42           | 10.0       | 198.0                               | 350                               | 2.2151                                    | 82.0                              | 15.560              | 1.140 | 14.420                         | 1.0985                                     | 37.983  | .797          |   |
| " "            | "                     | "    | "                      | 12    | 46   | 27.0 | 12    | 50           | 29.0       | 242.0                               | 800                               | 2.0661                                    | 87.0                              | 15.493              | 1.130 | 14.363                         | 1.0978                                     | 37.943  | .712          |   |
| " "            | 60°                   | "    | 2.10                   | 3     | 51   | 39.0 | 3     | 53           | 56.0       | 137.0                               | 300                               | 2.1898                                    | 85.0                              | 15.115              | 1.090 | 14.205                         | 1.0470                                     | 35.358  | .796          |   |
| " "            | "                     | "    | "                      | 3     | 3    | 53.0 | 3     | 7            | 42.0       | 229.0                               | 500                               | 2.1834                                    | 75.0                              | 15.190              | 1.080 | 14.110                         | 1.0480                                     | 35.408  | .788          |   |
| " "            | "                     | "    | "                      | 3     | 59   | 54.0 | 4     | 2            | 58.0       | 184.0                               | 400                               | 2.1739                                    | 75.0                              | 15.130              | 1.087 | 14.043                         | 1.0470                                     | 35.358  | .789          |   |
| 12.            | 59½°                  | "    | "                      | 4     | 00   | 4.0  | 4     | 6            | 11.0       | 367.0                               | 800                               | 2.1798                                    | 76.0                              | 15.245              | 1.057 | 14.195                         | 1.0517                                     | 35.589  | .755          |   |
| " "            | "                     | "    | "                      | 4     | 46   | 3.0  | 4     | 3            | 48         | 45.0                                | 350                               | 2.1605                                    | 76.0                              | 15.252              | 1.033 | 14.199                         | 1.0519                                     | 35.589  | .755          |   |
| " "            | "                     | "    | "                      | 4     | 14   | 11.0 | 4     | 18           | 49.0       | 162.0                               | 600                               | 2.1582                                    | 76.5                              | 15.235              | 1.053 | 14.172                         | 1.0510                                     | 35.559  | .749          |   |
| " "            | "                     | "    | 1.97                   | 3     | 19   | 56.0 | 3     | 23           | 25.5       | 209.5                               | 450                               | 2.1480                                    | 75.0                              | 15.240              | 1.030 | 14.210                         | 1.052                                      | 35.608  | .748          |   |
| " 19.          | 51°                   | "    | 1.86                   | 4     | 53   | 40.0 | 4     | 58           | 49.0       | 309.0                               | 650                               | 2.1030                                    | 72.0                              | 15.287              | 1.092 | 14.285                         | 1.0307                                     | 34.536  | .744          |   |
| " 11.          | 60°                   | "    | 1.84                   | 5     | 11   | 30.0 | 5     | 15           | 47.0       | 257.0                               | 550                               | 2.1400                                    | 72.5                              | 15.265              | 1.046 | 14.219                         | 1.0048                                     | 33.254  | .741          |   |
| " "            | "                     | "    | "                      | 5     | 5    | 16.0 | 5     | 11           | 7.0        | 351.0                               | 750                               | 2.1367                                    | 72.5                              | 15.255              | 1.042 | 14.213                         | 1.0050                                     | 33.264  | .740          |   |
| " "            | "                     | "    | "                      | 4     | 48   | 37.0 | 4     | 50           | 37.0       | 120.0                               | 250                               | 2.0833                                    | 75.0                              | 15.220              | 1.030 | 14.170                         | 1.0060                                     | 33.314  | .723          |   |
| " 19.          | 51°                   | "    | 1.80                   | 3     | 45   | 5.5  | 3     | 3            | 50         | 34.5                                | 700                               | 2.1276                                    | 72.0                              | 15.289              | 1.004 | 14.285                         | 0.9964                                     | 32.863  | .735          |   |
| " "            | "                     | "    | "                      | 3     | 58   | 19.0 | 4     | 1            | 29.0       | 192.0                               | 600                               | 2.1053                                    | 72.5                              | 15.223              | 1.007 | 14.216                         | 0.9983                                     | 32.954  | .729          |   |
| " 11.          | 60°                   | "    | 1.69                   | 4     | 31   | 20.0 | 4     | 36           | 12.5       | 290.5                               | 400                               | 2.0512                                    | 70.0                              | 15.232              | 0.983 | 14.249                         | 0.9540                                     | 30.779  | .710          |   |
| " "            | "                     | "    | "                      | 4     | 36   | 30.5 | 4     | 38           | 14.0       | 103.5                               | 200                               | 1.9324                                    | 75.0                              | 15.237              | 0.985 | 14.252                         | 0.9600                                     | 31.060  | .668          |   |
| " 12.          | 59°                   | "    | 1.68                   | 12    | 16   | 38.5 | 12    | 23           | 1.5        | 383.0                               | 800                               | 2.0888                                    | 67.0                              | 15.048              | 1.030 | 14.018                         | 0.9424                                     | 30.228  | .704          |   |
| " "            | "                     | "    | "                      | 12    | 26   | 9.0  | 12    | 32           | 59.0       | 410.0                               | 850                               | 2.0732                                    | 67.5                              | 15.060              | 1.044 | 14.016                         | 0.9440                                     | 30.239  | .723          |   |
| " "            | "                     | "    | "                      | 12    | 37   | 40.5 | 12    | 44           | 25.0       | 404.5                               | 850                               | 2.1013                                    | 66.0                              | 15.058              | 1.058 | 14.000                         | 0.9415                                     | 30.188  | .731          |   |
| Oct. 11.       | 59°                   |      | 2.25                   | 11    | 24   | 22.0 | 11    | 30           | 29.0       | 367.0                               | 900                               | 2.4523                                    | 60.0                              | 15.203              | 1.092 | 14.116                         | 1.070                                      | 36.525  | .862          |   |
| " "            | "                     | "    | "                      | 11    | 34   | 14.0 | 11    | 43           | 32.0       | 547.0                               | 1300                              | 2.3723                                    | 65.0                              | 15.159              | 1.100 | 14.059                         | 1.073                                      | 36.678  | .826          |   |
| " "            | "                     | "    | "                      | 11    | 46   | 12.0 | 11    | 52           | 29.0       | 388.0                               | 900                               | 2.3255                                    | 70.0                              | 15.199              | 1.110 | 14.088                         | 1.078                                      | 36.941  | .807          |   |
| " 12.          | 59½°                  | "    | 1.26                   | 4     | 33   | 3.0  | 4     | 35           | 54.5       | 171.5                               | 400                               | 2.3324                                    | 40.0                              | 15.373              | 0.770 | 14.603                         | 0.7842                                     | 22.994  | .797          |   |
| " "            | "                     | "    | "                      | 4     | 36   | 56.0 | 4     | 39           | 36.0       | 160.0                               | 350                               | 2.1900                                    | 45.0                              | 15.400              | 0.780 | 14.620                         | 0.7946                                     | 23.443  | .748          |   |
| " "            | "                     | "    | "                      | 4     | 40   | 26.0 | 4     | 43           | 53.0       | 207.0                               | 450                               | 2.1739                                    | 46.0                              | 15.413              | 0.780 | 14.633                         | 0.7957                                     | 23.495  | .742          |   |
| " "            | "                     | "    | "                      | 4     | 44   | 56.0 | 4     | 49           | 10.0       | 254.0                               | 550                               | 2.1653                                    | 46.5                              | 15.458              | 0.780 | 14.678                         | 0.7982                                     | 23.585  | .738          |   |
| " "            | "                     | "    | "                      | 4     | 51   | 13.0 | 4     | 53           | 17.0       | 124.0                               | 250                               | 2.0161                                    | 52.5                              | 15.470              | 0.795 | 14.675                         | 0.8093                                     | 24.096  | .687          |   |
| " "            | "                     | "    | 0.84                   | 5     | 6    | 46.0 | 5     | 10           | 15.0       | 209.0                               | 450                               | 2.1531                                    | 32.0                              | 15.553              | 0.615 | 14.938                         | 0.6256                                     | 16.422  | .675          |   |

## Tests on Leffel Wheel.

Date, Oct. 12, 1869. The first 19 tests L of weir was 10.052. Correction, .733.  
 " " 13, " The next 21 " " " " " "  
 " " 1, " The next 7 " " " " " " No correction.  
 " " 11, " The next 5 " " " " " "

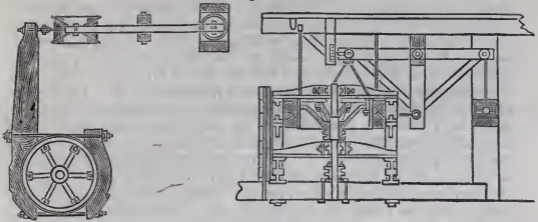
Weight of water used for all these tests was 62.33 lbs. per cubic foot. In the group of "7 tests," the first 3 were made with holes in wheel plates closed, and in the remaining 4 with holes open.

| No. Test. | Head.  | Weir. | Gate.      | Weight. | Rev. per min. | Horse Power. | Cu. feet per sec. | Per Cent. | Rel. Veloc. |
|-----------|--------|-------|------------|---------|---------------|--------------|-------------------|-----------|-------------|
| 1         | 14.28  | 1.730 | 4-5        | 670     | 138           | 42.03        | 32.66             | .795      | .795        |
| 2         | 14.17  | 1.727 | "          | "       | 135           | 41.11        | 32.52             | .787      | .799        |
| 3         | 14.01  | 1.671 | "          | "       | 127           | 38.68        | 29.84             | .817      | .739        |
| 4         | "      | 1.669 | "          | "       | 124           | 37.76        | 29.75             | .799      | .722        |
| 5         | "      | 1.674 | "          | 675     | 125           | 38.35        | 29.98             | .806      | .725        |
| 6         | "      | 1.673 | "          | "       | "             | "            | 29.94             | .807      | .725        |
| 7         | 13.98  | 1.672 | "          | 660     | 126           | 37.80        | 29.89             | .798      | .733        |
| 8         | 13.86  | 1.671 | "          | 700     | 120           | 38.18        | 29.84             | .815      | .701        |
| 9         | 14.48  | 1.761 | 7-8        | 740     | 130           | 43.73        | 34.18             | .780      | .744        |
| 10        | 14.21  | 1.761 | "          | 750     | 128           | 43.64        | 34.18             | .793      | .738        |
| 11        | 14.18  | 1.762 | "          | 755     | 126           | 43.24        | 34.22             | .786      | .728        |
| 12        | 14.16  | 1.780 | Full       | "       | 130           | 44.61        | 35.11             | .792      | .753        |
| 13        | 14.17  | 1.782 | "          | 760     | "             | 44.91        | 35.21             | .789      | .747        |
| 14        | 14.20  | 1.781 | "          | "       | "             | "            | 35.16             | .794      | .747        |
| 15        | 14.16  | 1.782 | "          | 765     | "             | 45.20        | 35.21             | .800      | .748        |
| 16        | 14.18  | 1.782 | "          | "       | "             | "            | 35.21             | .799      | .747        |
| 17        | 14.925 | 1.378 | 2-5        | 400     | 115           | 20.91        | 17.12             | .722      | .649        |
| 18        | "      | 1.364 | "          | 349     | 125           | 19.32        | 16.57             | .690      | .703        |
| 19        | "      | 1.354 | "          | 320     | 128           | 18.62        | 16.18             | .680      | .720        |
| 1         | 15.21  | 1.136 | 1-5        | 175     | 111           | 8.83         | 7.88              | .650      | .619        |
| 2         | "      | 1.134 | "          | 170     | 115.2         | 8.90         | 7.82              | .660      | .643        |
| 3         | 15.22  | 1.132 | "          | 160     | "             | 8.38         | 7.77              | .626      | .642        |
| 4         | 15.21  | 1.129 | "          | 150     | 122.4         | 8.35         | 7.68              | .630      | .683        |
| 5         | 15.23  | 1.127 | "          | 140     | 127.8         | 8.13         | 7.63              | .617      | .713        |
| 6         | 15.24  | 1.127 | "          | 135     | 130.2         | 7.99         | 7.63              | .606      | .726        |
| 7         | "      | 1.126 | "          | 130     | 133.2         | 7.69         | 7.60              | .586      | .742        |
| 8         | "      | 1.127 | "          | 135     | 130.2         | 7.99         | 7.63              | .606      | .726        |
| 9         | 14.26  | 1.526 | 3-5        | 500     | 122.4         | 27.82        | 23.26             | .740      | .705        |
| 10        | 14.21  | 1.527 | "          | "       | "             | "            | 23.01             | .741      | .707        |
| 11        | "      | 1.535 | "          | 475     | 124.8         | 26.95        | 23.33             | .707      | .720        |
| 12        | 14.23  | 1.521 | "          | 460     | 127.8         | 26.72        | 23.05             | .719      | .737        |
| 13        | "      | 1.521 | "          | 465     | "             | 27.01        | 23.05             | .727      | .737        |
| 14        | 14.56  | 1.147 | 1-5        | 130     | 133.2         | 7.87         | 8.18              | .583      | .760        |
| 15        | 14.46  | 1.149 | "          | 135     | 133.0         | 8.10         | 8.24              | .600      | .755        |
| 16        | 14.45  | 1.146 | "          | 140     | 127.8         | 8.14         | 8.15              | .610      | .732        |
| 17        | 14.16  | 1.741 | Full       | 725     | 133.2         | 43.90        | 33.20             | .822      | .770        |
| 18        | 14.13  | 1.736 | "          | "       | "             | "            | 32.95             | .832      | .771        |
| 19        | "      | 1.742 | "          | 730     | 127.8         | 43.41        | 33.24             | .797      | .740        |
| 20        | 14.15  | 1.745 | "          | 735     | 129.6         | 43.30        | 33.39             | .809      | .750        |
| 21        | 14.02  | 1.775 | "          | "       | 127.8         | 42.70        | 34.87             | .771      | .743        |
| 1         | 12.22  | 1.061 | None given | 700     | 120           | 38.18        | 35.81             | .770      | .747        |
| 2         | 12.09  | 1.045 | "          | 725     | 115.4         | 38.03        | 35.01             | .793      | .721        |
| 3         | 12.01  | 1.045 | "          | 675     | 125           | 38.35        | 35.01             | .804      | .784        |
| 4         | 12.73  | 1.077 | "          | "       | "             | "            | 36.61             | .726      | .761        |
| 5         | 12.51  | 1.077 | "          | 700     | 120           | 38.18        | 36.61             | .736      | .738        |
| 6         | 12.30  | 1.061 | "          | 725     | 115.38        | 38.02        | 35.81             | .762      | .715        |
| 7         | 12.12  | 1.061 | "          | 750     | 111           | 37.84        | 35.81             | .769      | .694        |
| 1         | 14.23  | 1.010 | "          | 725     | 127.6         | 42.05        | 33.29             | .783      | .737        |
| 2         | 14.08  | 1.047 | "          | 730     | 136.6         | 47.45        | 35.11             | .847      | .793        |
| 3         | 14.105 | 1.076 | "          | 800     | 127.6         | 46.40        | 36.56             | .794      | .741        |
| 4         | 14.08  | 1.011 | "          | 750     | 125           | 42.61        | 33.34             | .801      | .724        |
| 5         | 14.08  | 1.034 | "          | 600     | 150           | 40.91        | 34.47             | .744      | .870        |

I have seen sufficient the past year to convince me that tests made with so many gauge hands are very unreliable.

I would not be understood as vouching for the efficiency of the wheel, as given by Mr. Mills or myself, for my experience since has made me very skeptical about tests made in pits so limited as to require the use of racks to still the water discharged; but, as those tests were made under the same conditions, the discrepancies have made me cautious about using unnecessary formula for mere effect. That much of the formula for testing turbines, published by Mr. Francis, is for effect, it is charitable to believe. The plan is undoubtedly that followed by Mr. Boyden, and it is not creditable to his ability to suppose he believed several pipes, leading from different heads, would fill a tank to the average depth of the whole, yet that is what his perforated pipes around the wheel and across the pit leading to the gauge-tanks mean. With filtered water, plenty of help, abundance of time, and no regard for expense, the plan would not prevent accuracy; but for practical tests under ordinary conditions, with sediment in the water, such pipes are anything but desirable, and under no possible conditions are they necessary. The dash-pot is another source of error. It is absolutely necessary, with such a brake as Mr. Boyden used, also with the best brake that can be made, for some wheels, while there are others that can be tested without it; but the greatest care should be taken to have the plunger work as sensitively as possible. The pipes connecting the gauge-tanks with pit and forebay are matters of great importance. Of course, the smaller they are, the steadier the level of the surface in the tanks. The machine engineer likes small pipe connections, but the practical engineer has them large, that the surface of the water in the tanks may represent the true surface in pit or forebay. The water may rise and fall quick, as it should if it does so in pit or forebay, but it is easy to get the mean of the variations by observing the extremes. Racks, as usually constructed, take up one-half of the cross-section of the pit; a very fine rack more than that, if made of wood, and of course stops the water, causing it to be higher above than below them. This gives accelerated velocity to the water. Following the plan faithfully for two years, it proved to be a perfect trap for catching errors. The tank connections were then enlarged, the pit lengthened and made deeper; the perforated pipes and racks were abandoned, the dash-pot was reduced in size, and the plunger made perfectly free—after which changes, there was no difficulty in making tests that would repeat—a very necessary achievement in a business where suspicious patrons were in the habit of keeping tested wheels months, perhaps years; then, after repainting, return them as new to be retested, as was often done. The bane of engineering has been too much desire for display of mathematical exactitude, without much regard for the mechanical devices used with which to procure data to work from. Look at the coarse brake and scale beam used by Mr. Boyden, also by Mr. Francis, then at proportions as given by the latter in *Lowell Hydraulic Experiments* :

## Prony Brake.



Length of brake was found to be 9.745 feet.

Effective length of vertical arm, 4.500 "

Effective length of horizontal arm, 5.000 "

Consequently, effect in length was  $9.745 \times 5 \div 4.5 = 10.827778$  feet.

Why not have made the brake and arms of lengths readily expressed in whole numbers, thus doing away with decimals? Made in any lengths, a coarse oak timber, with an inch and a half round iron bolt through it for a fulcrum, would be a poor substitute for a light iron scale-beam with knife-edge pivots. Weighing what a turbine will pull, means the same as what groceries weigh, and needs the same perfection of weighing apparatus to do it well. The plan, when used by Mr. Boyden, was up to his time, perhaps, but a generation has since passed away, and vast improvements in almost every mechanical device have been made in the time, and practical engineers accept the improvements in turbine testing, as in other matters; but the machine engineer turns back to the oak brake and many decimals as anxiously as a duck takes to water. Turbine building is not a science, nor is it likely to be, until reputable builders, who would willingly test wheels before delivery, are protected from ruinous competition by the ignorant and irresponsible, who promise so readily, caring little about the efficiency of their wheels so long as they sell. To test each wheel before delivery would necessitate its being done quickly and cheaply, which would be impossible with the Boyden-Francis apparatus, nor would it be possible under any conditions with such an apparatus to make such tests as were easily taken to determine the effect of flanged cylinder gate and flaring draft tube, recorded in the report of Hydrodynamic Experiments.

## Engineers.

Of the hundreds of young men who yearly graduate from our educational institutions, how few of them are ever likely to reflect credit upon the name, simply because nature never intended them for the business. The term is derived from the word ingenuity; geniuses are not the product of schools, but of birth. No education will ever produce an engineer or mechanic, though it may machines. No mere aptitude for mathematics will make up for lack of fertility



in expedients so often demanded. An engineer should have ingenuity, sound judgment, and decision of character for emergencies. Without such characteristics no one will ever make a permanent reputation as an engineer. The calling has received the most of its renown from those who made no pretense of being engineers. Watt, Fulton, Stevenson, and others of the kind, were only considered engineers after their reputation had been made. Our yellow-plush propensity to accept heroes at their own estimate, if they only shout loud enough, has much to do with the continuance of unfounded pretensions. Many will remember the shout that went up at the *debut* of the Monitor. "Form a national society of engineers, and place John Erriesson at the head," was the cry. Had the Monitor encountered a storm on her passage out, as she did when she became the coffin for a hundred men, how different the result. For years previous, Mr. Erriesson had been the laughing stock of the country, and his achievements, before and since, indicate that, though he may have some original ideas, he lacks the judgment necessary to make them safely useful.

Of our many engineers, we doubtless have those who, if favored with opportunities, would deservedly become noted; but the terrible disasters of the past few years, caused by the destruction of dams and bridges, would hardly indicate that the best have been employed in the most responsible positions.

It is not my purpose to write of engineers in general, but of those who are called, or who call themselves, hydraulic engineers; of this class J. B. Francis has long stood at the head, so far as the calling relates to milling matters. For many years Mr. Francis has had charge of all the property of the Lowell Water Power Co., and general supervision of from twenty to forty large mills. He is thoroughly versed in all of the theories, but it would be absurd to suppose he has had much time to devote to the details that make up the supposed knowledge of a hydrodynamic engineer. The continued use of poor turbines, when those much better could be had at one-half the cost of those used, prove plainly that he knows but little of the common characteristics of the ordinary turbine. The Francis weir formula is excellent, but I have had very disagreeable reasons for doubting whether he, or any of the so-called hydraulic engineers, realize how slight a change in proportion of pit renders the formula worthless.

H. F. Mills of Lawrence, Mass., has experimented much, and, in my opinion, is as good an engineer of the class as can be found; but he travels in a fixed groove. That he measures the water used by the mills there as accurately as may be done by the machine methods, I have no doubt; nor any doubt that it might be done still more accurately by simpler plans, at one-tenth of the cost at which he does it. There are many others that might be named, but they are all of about the same pattern—much formula relating to ancient theories, but with little practical knowledge of the requirements necessary to make manufacturing profitable under the sharp competitive conditions of to-day. Economy seems to be one of the lost arts with the whole class, but the following cross-examination of one of them will speak for itself:

"EMINENT HYDRAULIC ENGINEER."

The announcement may often be seen in the papers that John Smith, the eminent hydraulic engineer, has been called in to examine some prospective water power, mill, reservoir, dam, embankment or some milling matter of interest. Civil engineering seems to cover canal, mill, reservoir and dam building, so it is reasonable to suppose Mr. Smith, as a hydraulic engineer, has been called in to advise about the use of water power or its transmission. And that those interested may banish future anxiety, should Mr. Smith report favorably, we will put him on the stand for examination. If the reader thinks some other engineer more eminent than Mr. Smith, No! well, then, Mr. Smith will you please take the stand.

Mr. Smith, what is your age?

*Ans.* Fifty-seven years.

What is your occupation or profession?

*Ans.* Hydraulic engineering.

How long have you followed that business?

*Ans.* I served seven years apprenticeship and have followed the business thirty years.

You are thoroughly informed in all the minutia of the business?

*Ans.* (Modestly) I believe I have the credit of being so.

You understand water power and the various means used for its transmission and application to drive machinery?

*Ans.* I think I do, thoroughly.

You also understand the various methods used for measuring water used to drive machinery?

*Ans.* I do.

Name the various methods with which you are familiar.

*Ans.* The weir, aperture, floats and current metre.

You are often called upon by mill owners to measure water?

*Ans.* Quite often.

Which of the methods named do you consider best?

*Ans.* Well, where it is convenient, the weir.

Have you ever personally verified measurements made by either methods, so as to be able to vouch for their accuracy?

*Ans.* W-e-l-l--N-o, not personally.

Suppose the flume leading to a wheel to be so large that the water flows, say, one-half foot per second, would not the slip with a current metre be so great as to leave little chance for accuracy?

*Ans.* W-e-l-l--it might.

Do you, of your own knowledge, know that accurate measurements of water can be made with a current metre under any conditions?

*Ans.* No.

In measuring with floats, do you make an allowance for the average instead of apparent velocity? If so, how much?

*Ans.* I make an allowance of 20 per cent.

Is 20 per cent. fixed upon as a matter of judgment or positive knowledge?

*Ans.* W-e-l-l--that is the allowance generally made with float measurements.

Then float and current metre measurements have considerable guess work about them?

*Ans.* W-e-l-l—under favorable conditions they may approximate. Can you personally vouch for the accuracy of aperture measurements?

*Ans.* W-e-l-l—N-o.

Do you know the least possible cross section of stream in measuring pit in proportion to the flow on the weir that will give correct measurement?

*Ans.* I do not.

Suppose the pit to be fourteen feet wide, with vertical sides; place a weir across, with end contractions, depth below the crest four feet, length of weir ten feet; then further down stream have another weir exactly the same, except the depth below the crest to be two feet; let the discharge from the mill flow over both weirs, would the depth on each show the same, supposing the discharge to be fifty feet per second?

*Ans.* W-e-l-l—r-e-a-l-l-y—I--well, I don't know.

Suppose the end contractions to be removed, what allowance would be necessary to deduct from the width to correct for the friction of the flowing water upon the rough side walls?

*Ans.* Well, something; I don't know just how much.

You have had experience with all of the water wheels in use from the old undershot to the modern turbine?

*Ans.* Constant experience for more than thirty years.

You often advise manufacturers as to the best kind for use?

*Ans.* Very often.

You understand the principle of each?

*Ans.* I think so, thoroughly.

The undershot is designed for low heads, is it not?

*Ans.* It is.

Which is the most efficient, undershot or breast wheel?

*Ans.* Oh, breast wheel, by all means.

Do you mean to say that for one foot head, a breast wheel would do better than an undershot?

*Ans.* Oh—w-e-l-l—for one foot—well, I don't know.

What is the maximum useful effect of an undershot wheel?

*Ans.* I don't know.

What is the exact relative velocity for an undershot wheel?

*Ans.* I don't know.

Have you had much to do with breast and overshot wheels?

*Ans.* Yes, indeed, very much.

Which is best?

*Ans.* W-e-l-l—some think the breast, others the overshot.

Never mind what others think. What do you know?

*Ans.* W-e-l-l—I never tested either, but I think—Don't want to know what you think. Do you know?

*Ans.* No.

What is the proper velocity for the periphery of either?

*Ans.* W-e-l-l—some say five feet per second; from five to eight feet per second is probably the—

Don't want any probably. Do you know?

*Ans.* No.



What is the maximum useful effect a breast wheel will give?

*Ans.* W-e-l-l—I have read of 75.

Don't care anything about what you have read. Do you know?

*Ans.* No.

Do you know any better about the overshot?

*Ans.* No.

Mr. Smith, you are well informed as to turbine wheels?

*Ans.* Certainly; intimately so.

Which is the best discharge for a turbine—inward, outward or downward?

*Ans.* W-e-l-l—there are many opinions about that.

Wasn't asking about opinions, but about what you know.

*Ans.* Well, the Boyden turbine is outward discharge, and I believe that—

Don't want to know about what you believe. Do you know?

*Ans.* Well, every body knows the Boyden has given the highest useful effect.

Don't care for what every body knows. Do you know?

*Ans.* Well, I know Mr. Boyden reported—

Did you ever test a Boyden wheel?

*Ans.* No.

Did you ever know of a disinterested engineer testing one who reported remarkably high efficiency?

*Ans.* W-e-l-l—no.

Did you ever know of a Boyden wheel being used where the water supply was insufficient for over half gate, or half of whole gate discharge, several months of the year, that gave satisfaction?

*Ans.* W-e-l-l—no—perhaps not.

Have you taken pains to ascertain whether there are other turbines that are better than the Boyden?

*Ans.* No, for I don't believe there are such.

Please give your reasons for such belief.

*Ans.* W-e-l-l—I—well—oh, cause I don't believe it.

So you have never taken pains to ascertain the real efficiency of the many other kinds of turbines?

*Ans.* No.

What is the proper relative velocity of the turbine with the water that drives it?

*Ans.* I don't know.

How do you know what proportional gears to use to connect turbine with the machinery to be driven?

*Ans.* Oh, I gear according to the table representing wheel.

What, when you know nothing certainly of the wheel?

*Ans.* W-e-l-l—yes—there is no other means of doing it.

Are all turbines of the same make of the same efficiency?

*Ans.* Certainly, or, at least, I suppose so.

You never have been to see such wheels tested in order to learn their peculiarities?

*Ans.* No, not I.

And why not? Has it not been your duty to do so before advising manufacturers in such matters?

*Ans.* Well, I have no faith in the testing that has been done. Why not? Have you any real cause for doubt?

*Ans.* Well, many wheels have been reported as giving better results than is claimed for the Boyden, and—well, I don't believe it at all.

Do you, of your own knowledge, know that there are not fifty kinds of turbines better than the Boyden?

*Ans.* Oh, of course I know there are not.

Do you solemnly swear that you know there are not?

*Ans.* Oh, well, perhaps I can not swear that I know, but then you know I—

Please remember you are under oath. Do you mean to be understood that, of your own knowledge, you know anything about the matter?

*Ans.* Well, perhaps not; but I know what I think.

Quite likely, but that is not important.

Are you aware that the turbine will do considerable work while running at a greater velocity than the water that drives it?

*Ans.* I have heard so, but do not know it to be so.

Supposing it to be so, can you account for its so doing?

*Ans.* I can not account for it.

What is the proper shape for a turbine bucket, and in what direction should it project from the center of the wheel?

*Ans.* Oh, there are many opinions; I don't know.

Please give the exact positions for the chutes to stand.

*Ans.* Oh, each builder suits himself; I don't know.

Which should have the largest openings, the chutes or buckets?

*Ans.* Some builders think the chutes, others the buckets; I don't know.

Why is it that two wheels, built exactly alike, placed in the same pit side by side—in one the step burns down every month, in the other never?

*Ans.* I don't know.

Which is best for buckets, sheet iron, sheet steel, bronze or cast iron.

*Ans.* I don't know.

In all parts of the country water powers of any size are owned by several parties. Do you know of any means for dividing the water so that each may have his proper share, whether the supply is much or little?

*Ans.* I do not know of any means for such division.

Does a turbine, having a draft tube for part of the fall, do as well as one set in the tail water?

*Ans.* I don't know.

Have you taken no pains to ascertain?

*Ans.* Well—no.

What is the proper diameter for draft tube for a given discharge?

*Ans.* I don't know.

Suppose a draft tube to lead down stream at an angle of forty-five degrees, or still nearer a horizontal line, what would be the effect?

*Ans.* I suppose they would do well ; I don't know.

Which transmits power with the least loss, belts or gears ?

*Ans.* Oh, belts, I think, decidedly.

Do you know anything about it positively ?

*Ans.* No.

Which causes the greatest loss, bevel or spur gears ?

*Ans.* Oh, bevel, by all means ; at least I think so.

Do you know ?

*Ans.* W-e-l-l—no.

Have you ever taken any pains to ascertain the loss, if there is any, caused by the use of belts, gears, or draft tubes ?

*Ans.* W-e-l-l—no, not personally.

Mr. Smith, will you be so kind as to state what knowledge about hydrodynamics is actually necessary to entitle a person to be considered an eminent hydraulic engineer ?

*Ans.* Oh, well—he must know all about water power and mills and things.

Certainly, but please give particulars.

*Ans.* Oh—well—he must know— why, he must know all about it.

Well, Mr. Smith, that will do for the present.

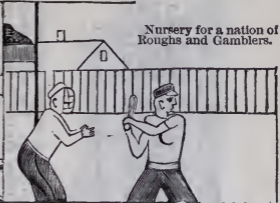
#### “OVER-EDUCATION.

“Like over-production, our caption is in some senses a misnomer, for no one can be over-educated in the true development of his best faculties for worthy ends. But there is a great deal of school and college education that is aimless, disproportionate, and cumbersome. There are too many mediocre professional men, lawyers, doctors, ministers, school teachers, writers ; few skilled artisans, farmers, gardeners, intelligent laborers technically educated for various spheres that are fundamental to well-ordered society. Society is top-heavy, with too much top and too little bottom. There is too much high-school dabbling that is not thorough enough for mental gymnastics, nor practical enough for the utilitarian necessities of those who must graduate into the hard work of the common and laborious pursuits which ballast society. The great law will assert itself, and all true education must lay its account with it, that by the sweat of the brow we must eat our bread. That is not good American education which would spoil a farmer's boy for the old homestead, or the farmer's girl for housekeeping. There is too large a crowd of unfit female school teachers. There are too many useless, third-rate lawyers hankering after office ; too many goodish ministers, unskilled doctors, ignorant apothecaries and engineers. Hence there are multitudes of our boys and girls who are over-educated, in the sense that they are unfitted by an aimless and merely bookish education for any patient and earnest life-work which will utilize

them as producers, and develop their individuality into the manly or womanly consummation of a stanch character and a robust and useful life."

Our common school system is at fault for this. What would be thought of the person who should treat everything growing upon his farm with the same care—planting beans, strawberries, cabbages, onions, wheat, weeds, and pumpkins all in the same way; plowing a little here, digging a little there, going over much surface—none deep? Would not the results resemble the product of our schools—a smattering of everything, a real knowledge of nothing? every graduate rushing for the position of major-general—not one willing to accept that of private? Is it not evident that the system is productive of the idea that honest labor is degrading? that the proper aim for the young man is office or a profession; for the young woman, wealthy marriage? Under its influence, are our Presidents, members of Congress and Legislatures, and officials in general, selected from the first or even second class minds of the country? Will our officers or teachers, male or female, compare favorably, intellectually, with our native mechanics? Pay high salaries, and get the best! is the constant shriek of the office-holder and teacher—which means, get those who will shriek loudest for more pay and less labor. Of all the trashy ideas prevalent, there is none more shallow than the pretense that high salaries insure the best services. High salaries to the few means degradation to the many—really a relic of barbarism—the feudal lord and subjected serf. Salaries so high as to be desirable in themselves are far more likely to be obtained by the unscrupulous pretender than the worthy proficient, as is patent to every one having any knowledge of the way the offices throughout the country are filled. I hope and think the time will come when our school system will limit the studies to the common English branches, and in those, give every child in the country a thorough course, leaving those desiring a higher education to obtain it at their own expense as a luxury—a real luxury—to the proper minds, but unappreciated by the multitude. Even were it possible to give every child a thorough education, gratuitously, in all the studies now merely skimmed over, it would be a matter of very doubtful utility. Possessions are valued somewhat in proportion to their difficulty of attainment; inherited property is seldom valued like that earned by years of hard labor. It can hardly dignify the high educational system to have the brilliant valedictorian wait idly for a year or two for something grand to turn up and then settle down as keeper of a peanut stand. Limiting the education at the public expense to the branches named will, I believe, produce a higher civilization than the present trashy method—less of the professional, more of the practical; better mechanics, farmers, engineers, doctors, teachers, fathers, mothers, and wives.

# The Effects of Forty Years of Massachusetts School System.



Nursery for a nation of Roughts and Gamblers.

First dude—going to the party this evening, dear boy?  
Second dude—No, mother isn't very well, and I can't go without a chap-iron, don't you know?



God made individuals. I wanted system! Alas and alas, behold the result!



Fitzadolphus — Why, the guvner wants me to help in the shop!  
Angelina' — Oh cruel! And ma wants me to darn my own stockings.

Prof. Sneezer — Can't spell? What have I to do with spelling? I'm professor of Greek!



Ma and the guvner.

The Noble Game of Football as played today.



The Hon. John, or Prof. Sullivan.





## Willimansett Spout Experiments,

Made to determine the co-efficient of discharge through such spouts.

These spouts were made one-eighth size of some used in a mill early in the century, at Plattsburgh, N. Y. From the flume downward they pitched four inches to the foot and had vent-holes in their tops just outside of flume. No. 1 was 24 inches in length through center of sides; the increased length was to determine the effect of the extra length; area of opening at lower end, 18 inches, or  $4 \times 4\frac{1}{2}$ ; area of opening at upper end, 28 inches, or  $4\frac{1}{2} \times 6\frac{1}{2}$ , which could be increased to 36 inches by withdrawing a wedge of plank.

No. 3 was the proportional standard, 15 inches in length through center of sides, with same openings as No. 1. No. 4 was of same size as No. 3, placed horizontally.

No. 2 was the same, curved.

No. 5 was one-eighth size of No. 3.

All were tested first with lower end submerged, under three feet head. All, whether long, curved, pitched, or placed horizontally, gave the same discharge and co-efficient, — No. 5 of course proportionally only. The wedge plank was then withdrawn, the opening of the upper end then being 36 inches. With that increase the discharge and co-efficient increased two per cent.

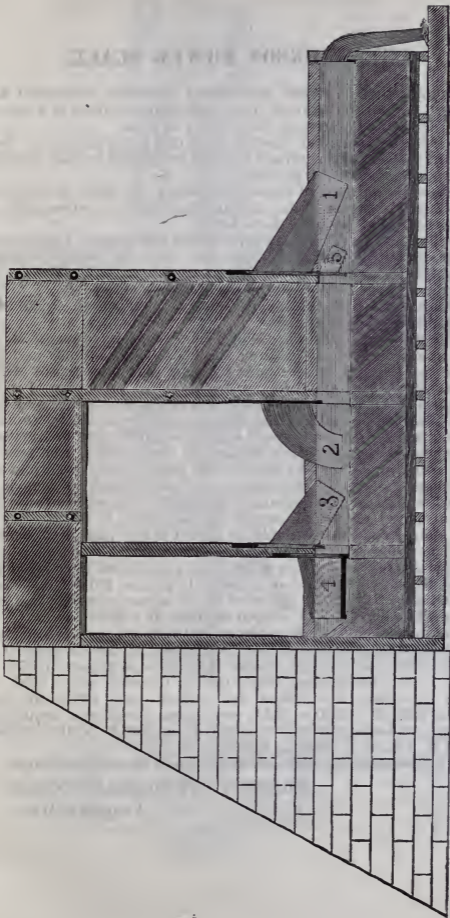
All were then raised, the center of opening of 1, 3, and 4 being three and one-half inches above surface of tail-water, the lower end of No. 2 three inches above the surface. With 2 feet 9 inches of head above lower end of curved spout and center of spouts 1, 3, and 4, the discharge and co-efficient were the same as when tested under three feet head and lower end of spout submerged, showing that the cohesion of water kept the column of discharge solid upon about two-thirds of the diameter of the column of discharge below lower end of spouts. The vents had no effect upon the discharge otherwise than to increase it to the extent of the spurt through the vent-hole. The co-efficient of discharge through the standard No. 3 was 91.39 per cent.

The spouts in the old Plattsburgh mill varied considerably in the proportion of openings at their lower and upper ends, as would be likely to be the case with such in other mills, which would affect their co-efficients as shown by increasing the opening in the upper end of No. 1. The inside corner of the planks of all the spouts tested were rounded, producing a flare of the upper end of spout.

At Highgate, Vt., a tub wheel was in use in 1885, and I tested its efficiency by grinding and measuring the water used. The conduit conducting the water to the wheel was an open spout with parallel sides, the ends of planks inside of flume left square, as was the bottom of gate, forming an aperture with square corners which would allow of but sixty per cent. co-efficient. There was 7 feet 3 inches head over center of gate opening, the spout, 8 feet in length, pitched so that the water striking the half depth of wheel gave 11 feet of head acting thereon. Under such conditions it required 5.2 h. p. of water to grind a bushel of ordinary wheat, and 5.9 h. p. to grind a bushel of hard Minnesota wheat.

## Willmansett Spout Experiments.

Nos. 2, 3, and 4 are shown in the position of trial, but when tested were placed where No. 1 is shown, the testing pit not extending back of penstock.



## THE EMERSON POWER SCALE.

To produce the perfect instrument herewith illustrated has required perhaps a hundred plans and changes, made at a cost of some \$30,000, and a quarter of a century in time.

Each size is graduated upon a circle of a given number of feet, and the revolutions per minute must be multiplied by that number in computing the results of trial.

As these scales are all constructed upon the same principle as the ordinary platform scales, and are common in the best mills, it is unnecessary to describe them here.

The illustrations represent the perfected scale, which weighs after connection, let the shaft run either way; also the register counter.

The ability to weigh when the shaft is running in either direction is made practicable by the use of the double connections 11 to the bell crank levers K K, the connections 11 being slotted at connecting point as shown in Fig. 3.

The register counter shown in Fig. 1 consists of worm M on shaft, into which works gear N having a hundred teeth, and the head of pendulum B, which forms a shield over nine-tenths of the ratchet gear A back of shield.

The pendulum B raises one-tenth of a circle, the ratchet gear has one hundred teeth, and if the weight was always at the maximum, say 100 pounds, the hook C would rotate the ratchet gear at every ten movements, but as the weight constantly varies, often from zero to the maximum, the shield prevents the hook C from carrying the ratchet gear any more than due the weight at each movement.

As it requires ten operations of the hook C to cause a complete rotation of the ratchet A, supposing the weight to be at its maximum, a cipher must invariably be added to the registered figures shown on the register H, as 976 must read 9760.

To get the real revolutions of the shaft, two ciphers must be added to the registered figures on register I, as the 12035 must read 1203500, which divide by the number of minutes in the run, say for a week of sixty hours, or 3600 minutes, as follows:—

Maximum graduation of quadrant, 100 pounds; registered figures as shown, 976; add cipher, 9760; registered figures on register I, 12035; divide the figures of register H by those of register I,  $9760 \div 12035 = .81$  as the average weight during the sixty hours' trial.

Now to obtain revolutions per minute take 12035, add two ciphers,  $1203500 \div 3600 = 334.3$  revolutions per minute, multiplied by, say, graduation of No. 3 scale, 6 ft. = 2006 ft.  $\times$  81 pounds = 162486 ft. pounds  $\div$  33000 = 4.92 h.p.

For information about the scale inquire of the manufacturers,

EMERSON POWER SCALE CO.

FLORENCE, MASS.



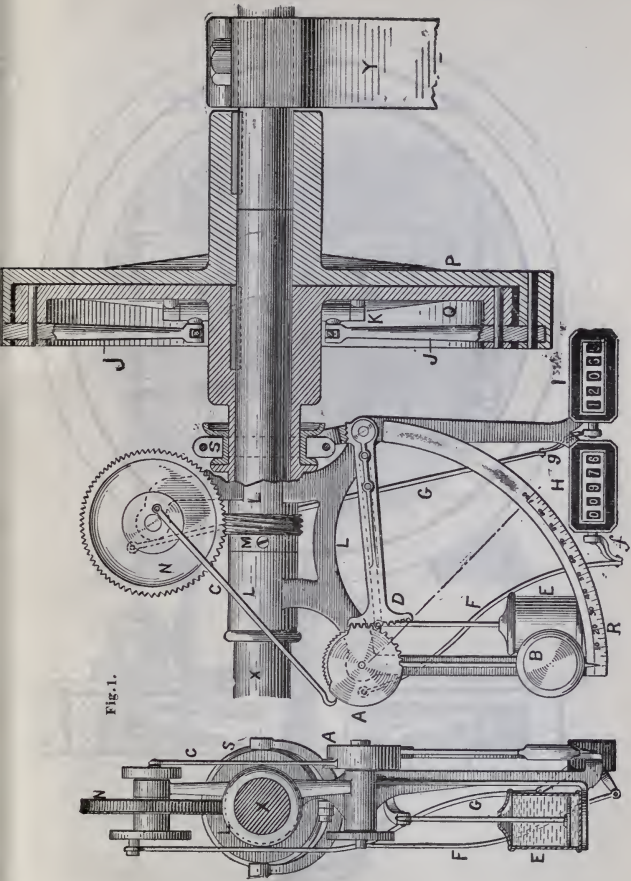


Fig. 1.

Perfected Scale, with Register Counter.

fig. 2.

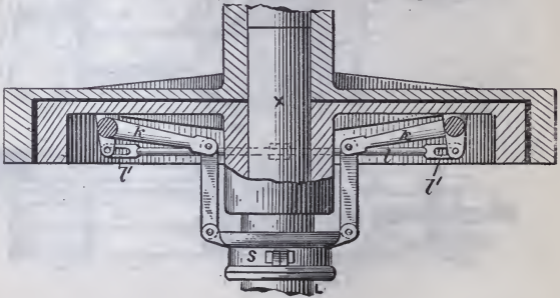
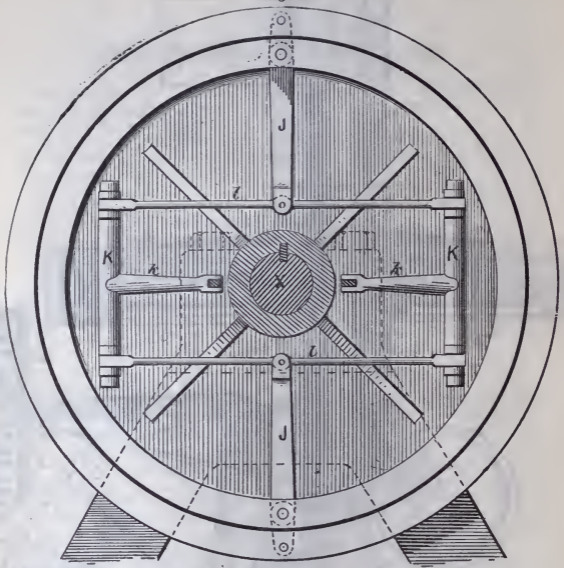


Fig. 3.

## THE COTTON MILL SCALE.

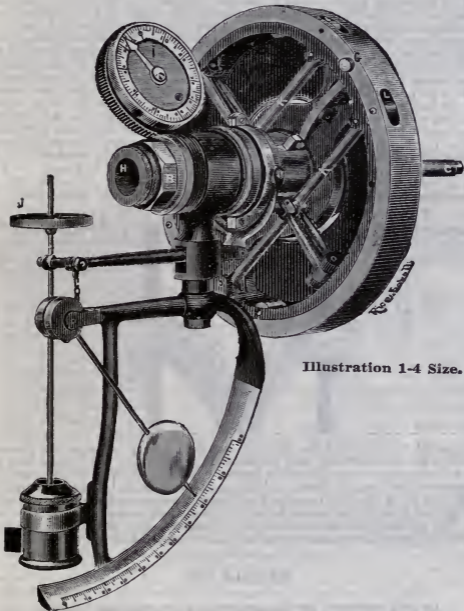


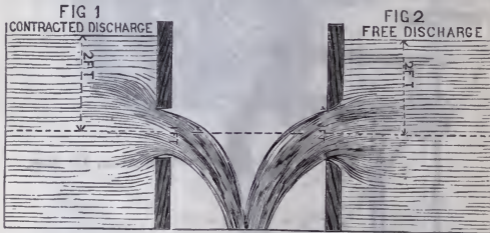
Illustration 1-4 Size.

The above illustration represents scales designed for cotton mills, to be used in testing the power required to drive spinning frames, fly frames, slubbers, and other light running machines, having tight and loose pulley outside of frames.

Graduated upon a two-foot circle.

## Water Measurements.

The lack of a practical knowledge of hydraulics a generation since caused a looseness in contracts pertaining to milling matters that has been productive of an immense amount of vexatious and expensive litigation. It is only necessary to glance at the methods adopted by the various Water Power Companies of the country for determining the quantity of water leased, as published on preceding pages, to learn that there has been no generally recognized standard for such measurements even among those claiming to be engineers and experts in such matters; it would seem that the average boy, ten years of age, who has ever played with toy water wheels would be able to provide something more definite than the Oswego plan. One great cause for the looseness in contracts has been the difference between the actual and theoretical discharge of water through an aperture of any size under a given head. The difference is only understood now by a very few. There are turbine builders who suppose that their wheels discharge the full quantity theoretically due their openings, while those calling themselves engineers generally believe the discharge of such wheels to invariably be about 60 per cent. due their openings, when in fact the discharge of turbines varies all the way from 35 to 100 per cent., and in special cases perhaps still more. The discharge through an aperture in the side of a penstock may be made to differ 50 per cent. An aperture one foot square, its center under two feet head, cut with edges at right angles with the face of the planks inside the penstock, leaving perfect sharp corners presented to the water as it issues, (see Fig. 1,) will dis-



charge about  $6\frac{3}{4}$  cubic feet per second; but with a proper flare of the aperture (as in Fig. 2,) the discharge will be about  $10\frac{1}{2}$  cubic feet per second, and the same relative percentage for other heads. An examination of the problems demonstrated in Evans' "Work on Milling, Hydraulics, &c.," published as late as 1848, will show that this important difference was not taken into consideration in preparing a work that was to be offered to the public as a guide in such matters. The following extract from the Work, page 96, is given, however, to show that the publisher had an impression that there was a difference.

### Article 55.

#### OF THE FRICTION OF THE APERTURES OF SPOUTING FLUIDS.

The doctrine of this species of friction appears to be as follows:—

1. The ratio of the friction of round apertures, is as their diameters nearly; while the quantity expended is as the squares of their diameter.
2. The friction of an aperture of any regular or irregular figure is as the length of the sum of the circumscribing lines, nearly; the quantities being as the areas of the apertures.\* Therefore,

\* This will plainly appear, if we consider that the friction does sensibly retard the velocity of the fluid to a certain distance; say half an inch from the side or edge of the aperture, towards its center; and we may reasonably conclude that this distance will be nearly the same in a two and twelve inch aperture; so that in the two inch aperture, a ring on the outside half an inch wide, is sensibly retarded, which is about three-fourths of the whole; while in the twelve inch aperture there is a ring on the outside half an inch wide, retarded about one-sixth of its whole area.

3. The less the head or pressure, and the larger the aperture, the less the ratio of the friction; therefore,

4. This friction need not be much regarded, in the large openings or apertures of undershot mills, where the gates are from 2 to 15 inches in their shortest sides; but it very sensibly affects the small apertures of high overshot or undershot mills, with great heads, where their shortest sides are from five-tenths of an inch to two inches.

This seems to be proved by Sineaton, in his experiments; (see table, Art. 67;) where, when the head was 33 inches, the sluice small, drawn only to the first hole, the velocity was only such as is assigned by theory to a head of 15.85 inches, which he calls virtual head. But when the sluice was larger, drawn to the sixth hole, and head 6 inches, the virtual head was 5.33 inches. But seeing there is no theorem yet discovered by which we can truly determine the quantity or effect of the friction according to the size of the aperture and height of the head, we cannot, therefore, by the established laws of hydrostatics, determine exactly the velocity or quantity expended through any small aperture; which renders the theory in these cases but little better than conjecture.

### OBSOLETE AUTHORITIES IN HYDRAULIC CASES IN LITIGATION.

\* In milling cases on trial, old English or American works are brought in as authority. These a half century since were useful because there was nothing better, but a revolution has taken place in such matters and there is now no difficulty in elucidating any matter pertaining to milling hydrodynamics so as to leave no just cause for dispute.

Oliver Evans has perhaps been considered the best milling authority up to 1860, but he simply copied the most of his ideas from old English works. His ideas of spouting fluids, article 55, show beyond chance for dispute that neither he nor his authorities knew anything about the law governing such spouting or the discharge through apertures.

It is now positively known that all apertures, large or small, round or square, discharge about 60 per cent. of the theoretical quantity due the opening, if the aperture is cut squarely through the plank, leaving sharp corners, as shown fig. 1st, opposite page.

The following note, copied from page 114 of his book, shows how little reliance can be placed in his authorities:—

“After having published the first edition of this work, I have been informed, that, by accurate experiments made at the expense of the British government, it was ascertained that the power produced by 40,000 cubic feet of water descending 1 foot will grind and bolt 1 bushel of wheat. If this be true, then to find the quantity that any stream will grind per hour, multiply the cubic feet of water that it affords per hour, by the virtual descent, (that is, half of the head above the wheel added to the fall after it enters an overshot wheel,) and divide that product by 40,000, and the quotient is the answer in bushels per hour that the stream will grind.”

It certainly should do so, for 40,000 cubic feet of water falling one foot evolves 75.5 h. p. Quite likely some essential feature of the experiment is left out so that the statement is worthless, as is invariably the case with their reports.

For, owing to their want of knowledge in such matters, they failed to give the necessary data to make their statements useful; for instance, in mentioning the discharge of water through apertures, they don't describe the form of the apertures, yet, as may be seen by the diagrams opposite, the discharge may be made to vary through the same sized aperture more than fifty per cent.



From personal acquaintance with turbine builders and their ways it has seemed doubtful to me whether any work published previous to the commencement of the testing system in 1869 has, except in a negative way, been of any help towards the improvement of the turbine or knowledge of milling hydrodynamics.

To ascertain whether the opinion was well or ill founded, the following letter was sent to John B. McCormick, who, through personal predilection, perseverance and unequalled opportunity for experimenting, unquestionably stands unrivaled in the knowledge of turbine construction.

*Willimansett, Mass., Feb. 27, 1892.*

*John B. McCormick, Holyoke, Mass.*

*Dear Sir:—Believing that the continued use of old text books as authority in matters pertaining to hydrodynamics has a tendency to cause the production of an inferior class of engineers, I would ask whether, except to avoid their errors, you have been aided in your turbine improvements by any hydraulic work published previous to the publication of tests in 1869.*

*Yours truly,*

JAMES EMERSON.

#### REPLY.

*Holyoke, Mass., March 1, 1892.*

*James Emerson, Willimansett, Mass.*

*Dear Sir:—Yours of the 27th duly received, and in reply will say: The old text books have not been beneficial to the writer, and their teachings were entirely disregarded in the production of the "Hercules" and other wheels which have been produced and perfected since by the undersigned.*

*Yours truly,*

JOHN B. McCORMICK.

But the worst of all is Haswell, who poses as universal instructor for the present time, and presents a *hash* of old theories that have been out of date for a generation past, seriously describing the construction of undershot, overshot, breast, Poncelet, Fourneyron, Boyden, Jouval, and other antique water wheels that have as little chance for future use as has the old stage coach of a half century since.

He gives the possible efficiency of the overshot at 84 per cent., and that of the breast wheel at 93. As actual trial under the same conditions proves that the turbine will do nearly double the work that can be done with the breast wheel, it may safely be stated without fear of successful contradiction that the breast or overshot wheel was never made that could exceed 67 per cent. useful effect.

Mr. Haswell asserts that large turbines give a higher efficiency than small ones, but the testing of twenty years proves the contrary to be the case, as quite likely it would with the breast and overshot.

Mr. Haswell's mind is in an excellent condition to receive instruction in hydrodynamics.

It is the study of such authorities that produce such depositions as the following:—

## ETHAN S. REYNOLDS

vs.

INDIANA PAPER CO. et al.

IN ST. JOSEPH CIRCUIT COURT, }  
STATE OF INDIANA. }

Complaint No. 2560.

Depositions of Mr. Clemens Herschel, duly sworn, testifies as follows :—

*Direct Examination.*

Q. You may state your name and residence and occupation ?

A. Clemens Herschel, hydraulic engineer, at Holyoke, Mass.

Q. How long have you been hydraulic engineer, located in Holyoke ?

A. I have been here since April, 1880.

Q. How long have you been practicing your profession as a hydraulic engineer ?

A. Twenty odd years.

Q. What institutions are you a graduate of ?

A. I am a graduate of the Lawrence Scientific School, Harvard University, and Polytechnic School of Karlsruhe, Germany.

Q. What position do you occupy in Holyoke with reference to the Holyoke Water Power Co. ?

A. I am their hydraulic engineer.

Q. Why is the amount of discharge different under different heads ? Will you explain that to us ?

A. That is because it is an impossibility that the head, acting on the wheel, shall ever be the same as the head contained in the race, and the allowance for that difference which I made to get the water off and on the wheel, as it is called, is one foot, that being my judgment, and also being a usual measurement, and contained in a great many leases with which I am acquainted.

Q. I understand you to say, as an engineer, that the allowance of one foot is a proper allowance to make, and one that is usually used or allowed ?

A. It is both a proper and a usual one. One foot off of six feet is a difference of  $16\frac{2}{3}\%$ , one foot off of ten feet is only a difference of  $10\%$ ; that is a reason the quantities I have reached vary from 2074 to 2156, at six and ten feet respectively.

Q. Would measurements of the depth of water at the flume alone indicate the head ?

A. It would not.

*Cross Examination by Mr. Hubbard, for the Plaintiff.*

Q. Mr. Herschel, why is the difference between  $16\frac{2}{3}\%$  off for six foot head and  $10\%$  off for ten foot head made ?

A. Because in any case, this per cent. represents just one foot, and one foot is the usual and customary allowance, and the proper one, in my opinion, and the one that obtains in actual practice.

Q. Would the same percentage be true as to the cubic feet discharged per second or per minute under the same head ? That is, six and ten feet off,  $16\frac{2}{3}\%$  and  $10\%$  respectively ?



A. By no means.

Q. Please explain how you arrive at the  $16\frac{2}{3}\%$  deduction on account of a difference of one foot between the actual level of the water in the canal and the tail race, and the actual level between the water immediately above and below the wheel?

A. That percentage is arrived at only in the case of a six foot head being the total, which we in Holyoke call available head. The allowance of one foot is made to get the water to and off the wheel, and one which is customary and proper, as I have explained. One foot being one-sixth of six, it results in reducing the head available, in order to get the head acting on the wheel, by one-sixth, or  $16\frac{2}{3}\%$  in this particular case.

Q. Is it not a fact, then, that if the mills were located at, say, ten rods distance from the main canal, and the flumes were too small in proportion to the amount discharged by the wheel to maintain a constant, or nearly so, level in the flume, then the loss of head might be more than one foot?

A. It would be, under those circumstances, more than one foot. I have known it to be one or two feet, and perhaps, in extreme cases, four feet. I arrived at the figure, one foot, from reports made to me by Mr. Smith of the locality, and in the exercise of such judgment as I have in these matters.

Q. This means, then, does it, in short, a deduction for the loss of head in getting the water to the wheel depending upon the distance of the wheel from the canal, and the size of the flume and fore-bay?

A. It depends upon that and other facts. The construction of what is called the rack, in front of the fore-bay, has usually quite an effect on it, the size of the flume, and whether the water turns at right angles or not, and how it turns. The mere length of the flume and tail race has rather a minor influence than some other structures and circumstances that occur in these cases.

Q. Then you include in addition to the items mentioned in my previous questions the loss of head by the means of the tail race?

A. Yes, sir.

Q. And you arrive at this from statements made to you by Mr. Smith of the conditions of the premises of the Indiana Paper Co., in September, 1888, do you not?

A. Partly so, but more largely from my judgment as to the propriety of the allowance of one foot from such loss of the total available head, in order to get the head acting in the wheel, which latter is the head which gives the discharge for the wheel.

Q. You have never seen the premises of the Indiana Paper Co.?

A. Never.

Q. Personally, you know nothing of the actual construction of the head and tail race except as reported by others?

A. I know it only from the report of Mr. Smith and others, and also from my judgment of what such structures look like in the Western states.

CLEMENS HERSCHEL.

HENRY K. HAWES,

*Notary Public.*

Had I not heard the foregoing deposition read in court, I should have been slow to believe that any one claiming to be an engineer would utter such stuff.

The slightest acquaintance with water powers shows that all vary in head more or less, consequently an allowance is made so that a tenant shall have no cause for action if the head drops somewhat from the usual height. This is done at Holyoke; nineteen feet are deeded, where there usually are twenty. Mr. Herschel has mistaken this practice for safety, as the rule for head when computing the discharge of a wheel.

All he was required to do for the Indiana Paper Co. was to measure the apertures of the several wheels, then give their discharge for given heads, say three, four, five, and six feet.

His success as engineer while at Holyoke hardly warranted his gratuitous fling at Western water powers.

There are many dams built by farmers and mechanics at the West, that such engineers as Mr. Herschel would find it difficult to equal; the one at South Bend, upon which the Indiana Paper Co. is located, is across the St. Joseph River, the bottom of which is so soft that the dam is constantly settling.

It was testified in court at the time Mr. Herschel's deposition was read, that the year before a part of the dam had been raised eighteen inches to restore it to its original height. At Mishawaka, fifteen miles east of South Bend, the dam was built by a farmer and is really a creditable piece of engineering for a professional dam builder, as are many other dams and mill arrangements that may be found West. Their worst feature is that they are nearly all over-worked.

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## DAMS.

Engineers differ much in opinion as to the proper way to construct dams. Stone dams, as a rule, have not proved so safe as one would naturally expect; yet with proper construction and sufficient material such dams should stand.

That pent up water has mighty force is proved by the vast ravines and notches in mountain ranges wherever such ranges exist.

I have had occasion to admire dams built of the boles of trees, the butts down stream packed closely and bolted one upon another from bottom to the top, then loaded down with rocks and gravel. These structures are often built upon soft mud bottoms or quicksand by men making no claim to be considered engineers, yet their work is perhaps superior to many professional engineering jobs.

There is a stone dam at Windsor, Vt., forty feet in height, that has stood a half century and seems good for the other half. The stones are laid without cement, but planked upon the up-stream side. A stone dam with earth embankment below to me seems a poor arrangement, frost or no frost, while such embankment above or up-stream should be very useful.

## Hercules Turbine.

As the "Hercules turbine" is placed at the head of the illustrated representation of the evolution of water wheels upon a preceding page, its history here is necessary. Early in 1876 Messrs. McCormick and Brown of Brookfield, Pa., sent four twenty-four inch turbines to the Holyoke Testing Flume to be tested. Up to that time turbines of various makes, twenty-four inches diameter, under eighteen feet head, ranged in capacity from fifteen to twenty-five horse power; these wheels transmitted seventy horse power under that head, and an efficiency so remarkable that the first was taken from the flume, examined, reset, and tested again and again. Experts and several turbine builders of acknowledged ability, such as T. H. Risdon, N. H. Whitten, and others, were called in to assist in making the test so that no chance for questioning the accuracy of the trials should remain. As may be seen upon another page further along in the book, I advised the abandonment of all earlier plans, and that builders should unite upon the plans of the Hercules and strive to perfect the turbine, but the inventor of the Hercules, and its wet nurse, Brown, hankered for the Golden Fleece. Before reaching Colchis, however, they were brought up by the Harpies at Dayton, Ohio, where, in imitation of the fabled gods, an illegitimate offspring of the third class order, called the "Victor," was born. **Hercules** feeling sadly shorn, called upon Stephen Holman of the Holyoke Machine Company for aid to help strangle the snakes that had invaded the infantile cradle of the young god. The implored aid was readily accorded and the creeping Hercules started out to annihilate the hydra with its hundred heads under the names of the Boyden, Jonval, Leffel, American, Humphrey, Craig, Ridgeway, Hunt Machine Company, Chase, Success, Burnham, Risdon, and a host of others, and then to clear the Augean stables of the dead rot of rubbish sent out by the colleges, under the names of hydraulic engineers, filled with obsolete formulas and mythical ideas that should have been condemned a half century since, for there is nothing in milling hydraulics that may not readily be elucidated so that all may understand.

To Stephen Holman vast credit is due for his liberality of expenditure in his efforts to perfect the turbine, but, after placing the Hercules upon a plane above that of all others, he has depended too much upon patents and trade-marks, for such obstacles are futile to stop the march of progress, so that the Hercules of to-day is but a second-class turbine. The first twenty-four inch Hercules tested under eighteen feet head gave over seventy horse power. Its guaranteed power for that head is but sixty-five, while J. & W. Jolly guarantee seventy-nine horse power for the same size and priced wheel; and each builder is equally reliable or responsible for guarantee.

MAY 1st, 1894.

## LITIGATION TO SETTLE QUESTIONS IN DISPUTE.

All who have read Juvenal's Satires will recall the surprise he expresses, that where ropes, daggers, and high buildings render suicide so easy, any man can be fool enough to marry; so it is equally a matter for surprise that a man having a mill pond large enough to drown himself in should resort to *law* to decide who owns the pond.

A lawyer that takes up a case desires to win, and, as is natural, will do so if he can, right or wrong. Any trickery that can be made to appear legal may be resorted to with approval.

A sucking Blackstone with impudent assurance may browbeat and bully a witness so long as he keeps within the legal ruts, and a very shallow fool can, and often does, ask questions that a wise man cannot answer simply because he is not allowed to explain and show that the question has no application to the case in hand. An annoyance that practical witnesses often have to contend with are works of shallow, conceited aspirants, who desire to shine as that "Eminent Hydraulic Engineer," or as the "Great Doctor Squills." The less such authors know, the more hair-splitting and profound will be their theories,—that is if profundity consists in unintelligibility. Could such frauds be examined by capable members of their calling their pretensions would at once be made apparent, as in the case of the eminent engineer, John Smith.\*

A sharp, unscrupulous attorney might, in fact often does, study up such shallow publications, and seemingly confounds an intelligent engineer or physician, simply because either has such contempt for the ignorant stuff presented as science, that, feeling that others should see the palpable absurdity as well as themselves, they treat the whole with contempt. There are few cases in milling matters that cannot readily be explained in a few minutes if the attorney would state the case clearly, then allow the witness to tell what he knows about it in as few words as possible. Certainly such would be much the quickest way to obtain the merits of a case from an intelligent expert; instead of which he is often kept under a shower of questions, for hours, nine-tenths of which have little bearing upon the case in hand, the attorney upon his side treating him like a charge of dynamite, likely to explode unexpectedly, the opposing attorney operating from the start as though he had a criminal to deal with.

For myself I can say with truth that I never took the witness stand with a desire to favor either side, and have seldom left it without feeling *outraged*. The dignity of the law and courts are often lauded, but my experience has not enabled me to see it.

Think of the immense flunkyism there must be latent in human nature to cause the free-born citizen to dress in his granny's old silk gown in order to equip himself for the supreme bench. No wonder the owl, the stupidest of birds, is selected to represent wisdom.

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\*For untold ages it has been found impossible to make laws that human ingenuity cannot evade; then why, like Mrs. Partington, continue to attempt the impossible? why not obliterate every statute, then re-enact a few broad principles and compel the settlement of all disputes by arbitration in the light of current intelligence?

## The Selection of Turbines

is a matter upon which a manufacturer's success in business often depends, yet in which the least practical knowledge is generally used. The common practice is to guess at the power required, the water at command, the best kind of wheel; finally, at the size of that. That such a system exists is owing to two facts; First, that we have had no really practical milling engineers; Second, to man's desire to get more than he is willing to pay for—to the same disposition that causes him to buy lottery tickets, or to gamble in stocks—and he exclaims: "I do not see why, if one is good, another of the same kind must not be so, too." Suppose he does not see, does he not know of plenty of cases to prove that it is not so? And there are good reasons for its not being so. For a number of years certain turbine builders made expensive efforts to gain high results. So long as the greatest possible care was given to each branch of the business, so long were high results generally obtained; but the moment such care was abandoned, and the business conducted with the ordinary care common in foundry and machine work, the ninety per cent. wheels dropped to eighty or less; then, in a little time, the patterns became warped or worn, or less care was used in setting them exact, as they were being molded, and the wheels made from them would give seventy-four or seventy-five per cent., though wheels made from the same patterns a year before often gave from eighty-five to ninety per cent. Too much time and money have been expended upon such wheels, any way, though in years past it was a matter of less consequence than now, except that it created or encouraged a false idea of the value of such wheels.

The Boyden and Tyler scroll wheels were rivals for a generation—the Boyden being used by large corporations under the most favorable conditions; the Tyler in the backwoods, under conditions in which the Boyden would have been unable to work at all. Many of each have been used twenty years without requiring repairs. If the point could be accurately determined as to the economy in the use of water, there is not a shadow of proof to show that the decision would be favorable to the Boyden; while the cost would be ten and the trouble in keeping the wheels clean and in working condition would be as a hundred to one in favor of the Tyler. Both are now, however, of the past, and out of place where economy is desirable. But, says a manufacturer, "My mill is on the upper level, where the head is always the same, and I buy so many cubic feet per second; so what use is it for me to have a particularly good part gate wheel?"

There are two good reasons for preferring such wheels: First, a good part gate wheel uses water in proportion to the work it has to do, and there are times in all mills when more or less of the work is stopped. Good part gate wheels save water at such times, which benefits all on the same fall; but a more important point is, that during low water in the dry season, when the supply is insufficient to do the work without the aid of steam, the mill having good part gate wheels can utilize whatever there is of water, while those having Boyden, or any of the popular whole gate wheels, can realize but little benefit from a two-thirds and nothing from a half supply.

There is one, and only one, method of securing a valuable turbine without any risk, and that is to ascertain first exactly what is needed, which may readily be done by measuring the water that is to be used and the power the mill requires; then apply to a respectable turbine builder, use ordinary common sense in the matter, and not expect that a wheel of a given capacity can be made in so perfect and durable a manner for four hundred as one that costs four thousand dollars. The idea is equivalent to the quandary of the young man who hesitated as to whether he should give his girl a piano or a pint of peanuts. Pay a fair price, and insist that the wheel shall be thoroughly made in every way, and tested before acceptance; and, unless it gives an average useful effect of 76 per cent. from half to whole gate, refuse to take it. A wheel that will give such an average is good, and will do a third more work with the same water, under the ordinary working conditions, than any Boyden or Victor ever made. There is another and very erroneous plan of fitting up mills; that is, to use wheels much too large for the work with the ordinary head, in order to avoid stoppage during backwater. Such wheels are entirely out of place, for if geared for the ordinary head they run at great loss through waste of water at all times—during the ordinary head, because too large; and, during backwater, because geared for a high speed.



## **Turbines Running Faster than the Water that Drives Them.**

We often hear of destructive collisions when heavy bodies meet, but never when two bodies are moving in the same direction—the forward one the faster; yet the turbine often moves faster than the water that drives it, and does good work. [See, for example, Upham wheel, test 13; weight, 100 pounds; revolutions, 300 per minute.] The wheel was 30 inches in diameter, on what would be the pitch-line of gear of that shape. Any one acquainted with such matters can get the circumference and spurting velocity of water for the head given, and thus verify the statement. Such turbine builders as claim to be scientific have a theory to fit the case, but do not agree well with each other. Will not some of our college professors or students, those engaged in such studies, give it attention? and in so doing take into consideration the fact that the Upham wheel discharges the water obliquely outwards near the periphery of the wheel, where its velocity is greatest, instead of near the center, where the velocity of the wheel is less than the spurting velocity of the water—seemingly a sufficient proof that theories based upon the central discharge idea are incorrect.

Many explanations have been sent to me in relation to the above, none from the colleges or engineers. Judge Waldron of Maine readily accounted for the fact upon the same principle that an ice boat often sails faster than the wind that drives it. Many of the explanations have been lengthy, accompanied with diagrams, but the simplest solution that occurs to me is the wedge that often flies from the frosty log; the wedge to open the cleft one inch may enter three, consequently moves three times as fast as the cleft parts when it flies out.

## **Backwater under Conditions Difficult of Settlement.**

Many cases of backwater for which complaints have been and still are being made, have arisen through the effect of a rapid current produced by a fall in the stream or the discharge of water from a mill located upon the fall—the current having carried the loose sand, mud, gravel, sawdust, bark, or other debris forming the bed of the stream down to a wider or more level place where the velocity was less, and there depositing it, forming a bar across of a greater or less height, as the case might be, raising the water above causing a fall below. In earlier times, when locating a mill upon such a fall, the wheels were seldom placed so low as to receive the full effect of the fall, for, through the abundance of water, the comparatively little power required could be obtained at less expense with a portion of the available head. In time, another mill was erected further down stream, the dam for which flowed the water back upon the bar above, without in any way interfering with the power of the mill above. These conditions continued for years without question. As the country became settled, the supply of water grew less, the power more valuable and better cared for. The upper mill was enlarged, the wheel-pit lowered, the wheels placed at the bottom, and the bar removed. Of course the water from the dam below flowed back into the upper wheel-pit and obstructed the wheels. Under such circumstances, it is apt to cause the owner of the upper mill to insist that the lower dam has gradually been raised above the title thereto. There are plenty of mills yet, the discharges from which are raising such bars, and so gradually as to be overlooked and neglected, which will surely cause trouble in time.

## Testing Flume and Turbine Testing.

The testing system, or practice of testing turbines before purchase to determine their value, has become so general that there is no turbine builder of any reputation, who has not found it necessary to submit his wheels to such trial, in order to enable him to sell them; this being the case it is proper that the method by which such tests are determined should be made familiar to all interested. Ten years since the testing of a turbine was a serious matter, and could only be accomplished at a great outlay of time and money, the expense extending into the thousands; while the apparatus used was so crude, and the complications were so numerous, that the matter was understood by but few, and was believed in by less; thousands and tens of thousands of dollars have since been expended in simplifying the process of computation of results obtained, the manner of obtaining them, and in ridding the system of rubbish of no earthly use. In the first place it should be thoroughly understood, that weighing the power of a wheel, or in other words what it will pull while running at a certain speed, is precisely the same in principle as to weigh what a horse or man can pull while traveling at a fixed speed, or as in weighing groceries; consequently an accurate scale beam with knife edges and sealed weights are required as much in the one case as the other; the pounds named in testing a wheel mean precisely the same as in weighing hay or sugar; and if a proper weighing and controlling instrument is used, the wheel will be kept at the same speed so long as a given weight is carried: consequently the gauges remain constant with the same weight on scale, and with the same head of water, so that six different persons taking the gauges add exactly six times to the chances for errors in testing a wheel, and as much more to the cost. Testing with proper apparatus and conveniences is a very simple matter, but it requires experience to make such test reliable; and though an engineer may have the formula committed to memory, he will need considerable experience practically before he will be able to make tests that can be depended upon.

### WEIR MEASUREMENTS.

Within the past few years much has been said and written for and against the reliability of measurements of water flowing over weirs; this has arisen through the great diversity of results obtained by different persons, who have used the same formula for computation of data. Turbines of almost every make, tested by their builders, have seemingly given high useful effect; while in actual use few of them have proved economical in the use of water. This has had a tendency to discredit weir measurements, but unjustly so, as may readily be explained, for the matter is one of great simplicity, notwithstanding the complications thrown around it by those who have supposed a long array of decimals denote profundity and accuracy. Any weir under exactly the same conditions will repeat results invariably; but a formula based upon certain conditions, will not give correct results if those conditions are changed. All brooks and rivers vary much in width and depth, yet the same water flows through the narrow as well as the wide places, the velocity, of course, varying with the cross section of the stream. The velocity, however, does not cease immediately upon entering a wider or deeper part, but continues until the momentum is lost, and the general level attained; this of itself would prove the necessity of placing a weir at a considerable distance from the discharge of a higher head. The Francis formula is based upon the natural flow of the water, which for a depth of one foot over a weir is about three feet four inches per second; and it must be evident that such formula is entirely inapplicable where the velocity is four or five feet per second, as it may be if the weir is placed close to the discharge of a poor turbine, where the water leaves the wheel with half the velocity due the head; or where a cross section of pit or stream approaching the weir is but little greater than the capacity of the weir itself. It is plain that under such conditions the velocity will vary according to the useful effect of the wheel, and equally plain that no reliable correction for velocity can be applied. Had this been considered, much trouble and expense might have been saved the past twenty-five years; for it is not likely any builder would have knowingly continued the manufacture of forty per cent. turbines. The cross section of a pit or stream, up stream from a weir, should be at least five times the cross section of the stream flowing over it; and for a discharge of two thousand cubic feet per minute, the weir should be fifty feet from the discharge of the turbine, or opening into pit. Racks should never be used, as they obstruct and raise the water so that it passes through with renewed velocity. If there is a horizontal discharge



towards the weir, check the current by zigzag breakwaters. For measuring the flow of a river the weir or dam cannot be too large, but it may be for measuring the discharge from a mill where a governor is used, as the varying discharge, caused by adding or throwing off machinery, may prevent accuracy if too much time is required for the water to find its proper level.

THE SAME WHEELS TESTED IN PITS OF DIFFERENT CAPACITY.

July 24 and 26, two wheels were tested at Holyoke flume; these had previously been tested in another flume, the measuring pit of which was about nine feet in width, two feet in depth below crest of weir, while the weir itself was twenty feet from the wheel. The following results were obtained:

Largest Wheel: Stilwell & Bierce Flume.

|                 |                                 |                   |
|-----------------|---------------------------------|-------------------|
| Head, 7.64 feet | Discharged, 1178.00 cubic feet. | Percentage, .8785 |
|                 | Holyoke Flume, largest wheel:   |                   |
| Head, 1840      | Discharged 2233.55 cubic feet.  | Percentage, .7520 |
|                 | Reset and again tested:         |                   |
| Head, 18.07     | Discharged 2214.66 cubic feet.  | Percentage, .7532 |

Theoretical discharge for head of 18.40 feet, based upon the Stilwell & Bierce test should be 1828.7 cubic feet.

Smallest Wheel: Stilwell & Bierce Flume.

|                 |   |                   |
|-----------------|---|-------------------|
| Head, 7.82 feet | Discharged 761 cubic feet.                          | Percentage, .8604 |
|                 | Holyoke Flume:                                      |                   |
| Head, 18.33     | Discharged 1387.27 cubic feet.                      | Percentage, .7777 |
|                 | Taken out, overhauled, then re-tested:              |                   |
| Head, 18.44     | Discharged 1400.31 cubic feet.                      | Percentage, .7753 |
|                 | The head was then reduced, and it was again tested: |                   |
| Head, 7.85      | Discharged 869.34 cubic feet.                       | Percentage, .7724 |

Theoretical discharge, based upon Stilwell & Bierce test, for 18.44 feet head, should be 1168.5 cubic feet.

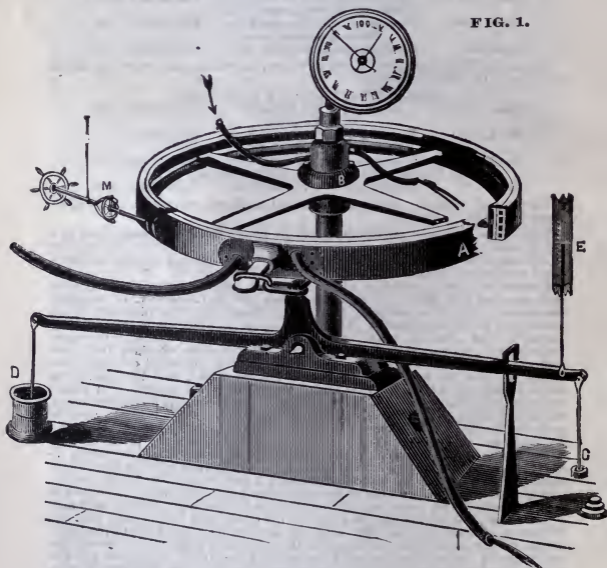
These tests show how little reliance can be placed in measurements made in a pit of insufficient capacity, yet how accurately a proper pit and weir will repeat; at the same time they explain how the high results reported so often by interested parties are obtained.

Illustrations and description of testing flume and apparatus of the present time are herewith given: Fig. 1, represents the dynamometer, or weighing instrument; Fig. 2, an elevation of a testing flume; Fig. 3, a plan view of the same; Fig. 4, the hook gauge. Through an opening in the side of fore-bay Fig. 1, may be seen a turbine wheel with its shaft extending upwards, on the upper end of which, above fore-bay, is secured the instrument for weighing the power transmitted from the water discharged. To ascertain the useful effect it is necessary to know the head under which the wheel works, also the quantity of water discharged by it in a given time. The head is the difference in height between the surface level of water in pit and fore-bay *when the wheel is running*. At which time there is generally too much disturbance in the water to allow of accuracy by direct measurement, thus necessitating the use of the tanks A and B; the tank A is connected with water in fore-bay by a short piece of three-fourths inch steam or gas pipe, through which the water flows too slowly to cause ebullition, but fast enough to keep the surface in tank equal in height with that in fore-bay; from the bottom of the tank a rubber pipe extends to the bottom of a glass tube, placed beside the measuring pole at the right. The tank B is connected with the water in pit by a rubber or flexible pipe, that the tank may be raised or lowered, in order to keep the top of the tank nearly even with the surface of tall water in the pit; with this arrangement the point of the hook, which may be seen at the lower end of the measuring pole, will be perceptible the instant it breaks the surface of the water in the tank. This hook and the pole is raised or lowered by a hand nut shown above the tank. The pole is graduated in tenths and hundredths of feet from the point of the hook to the top of the pole, so that after the point of the hook is adjusted to the surface of the water in the tank, the exact head may be found opposite the surface in the glass tube or tank A. The tank C, which is also connected with the water in the pit by a flexible pipe, slides up or down on two parallel rods, and is kept at any height by a counterpoise; above this the hook gauge is firmly fixed to a timber in such a position that the point of the hook will drop in a perpendicular line through the center of the tank, and it will save making corrections for each measurement by placing the point of the hook exactly level with the crest of the weir when the scale of the gauge is standing at zero.

## Emerson's Improved Brake.

*Manufactured by the Fales & Jenks Machine Co., Pawtucket, R. I.*

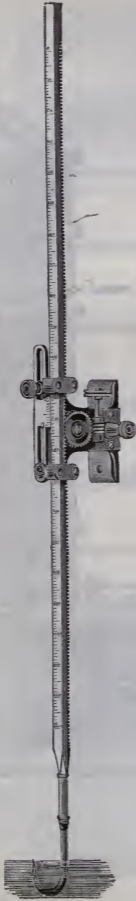
**FIG. 1.**



## The Emerson Hook Gauges.

*Manufactured by Hamilton J. Sawyer, Lowell, Mass.*

NO. 1.



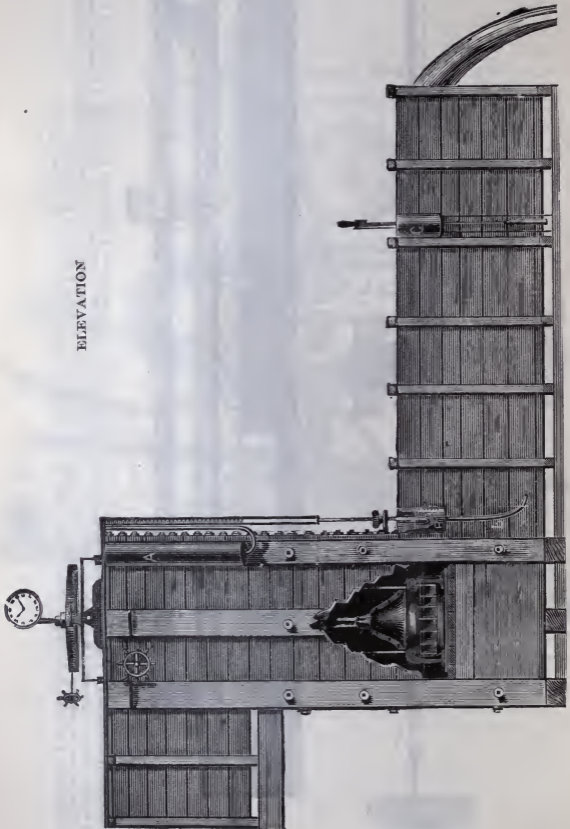
NO. 2.



The first hook gauge that I ever saw was some six or seven feet in length, and, when boxed, was a good load to shoulder. It seemed needlessly cumbersome and inconvenient. A short experience caused me to plan the one here illustrated, marked No. 2, that weighed 14 pounds, and was 30 inches in length, which still seemed too heavy for convenience. After much study, No. 1 was produced, that weighed about four pounds, and is so entirely superior in convenience to No. 2, or any other hook gauge that I have ever seen, that I consider it complete.

Those desiring to purchase, should apply direct to Mr. Sawyer, who owns the patterns, and is a very skillful workman.

ELEVATION



Plan of the Lowell Testing Flume and Pit of 1869.



FIG. 3.

The proper dimensions for a testing flume are, of course, determined by the size of the wheels to be tested. The fore-bay, in diameter, should at least be twice that of any wheel placed in it, while the width of the pit should equal one and a half times the length of the weir; below the crest of which the depth should equal four times the depth of the stream likely to flow over it. The weir should stand at least twenty feet from the wheel, and, at an exact right angle with the flow of the water.

The dynamometer, or instrument used to determine the power transmitted, is simply an improved "prony brake." The wheel B is secured to the shaft of the water-wheel, and its speed is controlled by the friction-band A, which is connected to the scale-beam as shown, the point of connection describing a circle of a given number of feet. The rim of the wheel and the friction-band are hollow, and are kept cool by streams of cold water passing through them; the water in the rim of the wheel being supplied through its hollow arms and the pipe, shown in the engraving. The wheel B, is made of cast iron, the friction-band of "composition" or "gun metal." The hands of the "counter" are so arranged in connection with a worm gear, that they can be made to rotate in the same direction the hands of a clock move, whichever way the wheel being tested may revolve.

The hand wheel for operating the friction-band through the screw M, has a "universal joint" in its shaft, which is arranged with a slide to prevent fraud while testing. The connection of the band with the scale-beam is made by knife-edged links, and the pivot of the beam is also knife-edged. The weights are suspended at one end of the beam as shown at C; at the other end is the "dash-pot" D, (it is better to have "dash-pot" at the same end as the weights,) filled with water to hold the beam steady. The pot is made of cast iron, bored out perfectly true. The plunger on the end of the rod is a thin disk of iron turned to fit the pot loosely, so as to allow it to move perfectly free; it has six three-eighths inch holes through it, stopped with brass thumb screws; one or more of these may be removed at any time to render the beam more sensitive, but the screws must be left lying on the plunger, that the weight may not be changed. To prepare the instrument for testing, the "dash-pot" should be filled with water, the screws removed from the holes in the plunger, but left upon it, the beam leveled with the indicator standing at zero, as shown at E: then place a small weight in the scale-pan, and observe the number of seconds required for the weighted end to settle one-half inch; then change the weight to the other end of the beam, the same distance from the fulcrum, and change the balance weight until the beam is balanced; then return the screws to the holes in the plunger, and connect the beam to the friction-band by the links for that purpose.

When testing, I find that the simplest and surest method of obtaining the correct number of revolutions of the wheel, is to hold the hands of the counter at zero until the "timer" is ready; then to run several minutes, and divide the number run to obtain the revolutions per minute.

The most perfect measurement with the hook gauge can be obtained by keeping the top of the tank C, nearly level with the surface of the water in it, then by looking across it the point of the hook may be seen the moment it breaks the surface.

In testing a wheel I begin with a light weight, say for a 30-inch wheel under fifteen feet head, start with 100 pounds, run two minutes—the man at the wheel keeping the beam level—then change to 125 pounds and repeat. Continue to change 25 pounds every two minutes until the speed of the wheel is reduced below its best point, which is reached, we will say, when it is carrying 250 pounds; then reduce the weight to 235 pounds, and change ten pounds every two minutes until the best point is again passed, which is found, say, when it is carrying 255 pounds; reduce the weight to again, say, 242½ pounds and change the weight five pounds at a time every five minutes. Sometimes, when not in a hurry, I commence with 100 pounds and run to 700, or even 800; then again, I might start on the same wheel (if I knew about the proper weight for it) say with 600 pounds, and not change more than 100 during the whole test. Some parties desire to have their wheels tested with as short a range of weights as can be used and the wheel's best speed be found, for the purpose of showing even results through the whole test; but to the initiated, such results would appear no better than where greater changes were recorded if the weights varied with the speed. Of course, the more the speed of a wheel can be varied without affecting its percentage the better, but that is only determined by using a long range of weights while testing it.



The power transmitted by the wheel is determined as follows: Suppose the scale beam is attached to the friction brake at a point, which, if revolving, would describe a circle of 20 feet, and the wheel running one hundred revolutions per minute, holds the beam at zero when loaded with 500 lbs.,  $20 \times 100 = 2000 \times 500 = 100000 \div 33000$  gives 30.30 horse-power; divide the transmitted power, by the power of the water used, to ascertain the useful effect of the wheel.

An example is here given of finding the useful effect, after testing a turbine, as followed in 1869; and when it is understood that a hundred different weights might be tried in testing a wheel, and that during the trial some six or seven different observers were taking notes every thirty seconds, and that all of these observations had to be made to agree it will readily be seen that there were wide openings for errors.

TEST 17—TYLER WHEEL, September 21 and 23, 1871.

|   |   |
|---|---|
| 149.2   | Rev. per m.                               |
| 20  | Circumference of circle                   |
| 2984.0  |   |
| 300   | Lbs.                                      |
| 33000   | Foot lbs.)                                |
| 895200  | 27.13 H. P. of wheel.                     |
| 66000   |   |
| 235200  |   |
| 231000  |   |
| 42000   |   |
| 33000   |   |
| 90000   |   |
| Q. per sec. = $3.33 (1 - 0.1n H) H^{\frac{3}{2}}$ |   |
| 1.0615  | Height of water on weir.                  |
| -.0145  | Correction for weir level.                |
| 1.0470  |   |
| .2  | Number of end contractions $\times 0.1$ . |
| .20940  |   |
| 6.00000   | Length of weir.                           |
| 5.79060   | = 0.7627236                               |
| 3.33  | = 0.5224442                               |
| 1.047   | = 0.0199467                               |
| 0.0099733   | } $H^{\frac{3}{2}}$                       |
| 60  | = 1.7781513                               |
| 1239.48   | = 3.0932391 = Q. per min.                 |
| 15.695  | = 1.1957613 = Fall.                       |
| 62.336  | = 1.7947389 = Weight of cubic foot.       |
| 33000 (a c)                                       | = 5.4814861 = Horse Power.                |
| 36.75   | = 1.5652254 = H. P. of water.             |
| 27 13   | = 1.4334498 = H. P. of wheel.             |
| .7383   | = 1.8682244 = Ratio, or, percentage.      |

The formula for correcting the depth for the velocity of the water approaching the weir is

$$H' = \left[ (H+h)^{\frac{3}{2}} - h^{\frac{3}{2}} \right]^{\frac{2}{3}}$$

in which the factor

$$h = \frac{v^2}{2g};$$



$v$  being the velocity found by dividing the  $Q$  per second by the section of the stream approaching the weir. As the flume approaching the weir was 14 feet wide, and the bottom of it was 3.5 feet below the crest of the weir, it follows that the area of a section of the stream, when there was 1.047 feet of water flowing over, is  $14(3.5+1.047)=63.658$  square feet.

$$\begin{aligned} Q \text{ per sec.} &= 20.658 = 1.3150883 \\ \text{Section} &= 63.658 = 1.8038530 \\ \hline &1.5112353 = v \\ &\quad \quad \quad 2 \\ \hline &1.0224706 = v^2 \\ \hline &2.1916206 = 2g(a+c) \\ \hline &.0016 = 3.2141002 = h \\ \hline &2.6070501 \\ \hline &.0001 = 5.8211503 = h^3 \\ \text{Then } H+h &= 1.047 + .0016 = 1.0486. \\ 1.0486 &= 0.0206099 \\ &0 \ 0103049 \end{aligned}$$

$$\begin{aligned} 1.0738 &= 0.0309148 = (H+h)^{\frac{3}{2}} \\ \text{Then } (H+h)^{\frac{3}{2}} - h^{\frac{3}{2}} &= 1.0738 - .0001 = 1.0737 \\ 1.0737 &= 0.0308830 \\ &0 \ 0102943 \\ \hline 1.0486 &= 0.0205887 \end{aligned}$$

$1.0486 = H' =$  corrected depth on the weir.

Substituting  $H'$  for  $H$  in the weir formula first given above, we find the corrected  $Q$  to be 1242.25 cubic feet per minute.

$$\begin{aligned} &1.0486 \\ &\quad \quad \quad .2 \\ \hline &.20972 \\ &6.00000 \\ \hline &5.79028 = 0.7626996 \\ &3.33 = 0.5224442 \\ &1.0486 = 0.9206099 \\ &\quad \quad \quad 0 \ 0103049 \\ &60 = 1.7781513 \\ \hline &1242.25 = 3.0942099 \\ &15.695 = 1.1957613 \\ &62.336 = 1.7947389 \\ \hline &33000 (a c) = 5.4814861 \\ &\quad \quad \quad 1.5661962 \\ &27.13 = 1.4334498 \end{aligned}$$

Ratio of useful effect .7366 = 1.8672536

To work out the foregoing without the use of logarithms, applying all of the corrections as was then done, would cover many pages of this work. A hundred different weights and speeds were likely to be tried in testing any wheel, each change requiring the same tedious process, so that days, perhaps weeks, were required to ascertain the value of a wheel. It was customary with some engineers to work out a few tests, then to "plot" the remainder on "diagram paper;" but this was found to be unreliable in working out my weir tables, and of course, was equally so in working out tests. With reliable apparatus for testing a wheel, but few corrections are necessary, and only three persons are required in making tests. One having the whole in charge, and who takes weight, revolutions of wheel, and the head and weir gauges, assisted by a "timer," and one

who controls the speed of the wheel. A testing flume is filled and emptied so often that it will leak more or less, and this leakage is into measuring pit, so that after a wheel is set ready to test, its gate is closed and sprinkled with sawdust to prevent leakage, that would affect results of trial; then the flume is filled with water, and the leakage of the flume taken at the weir. Suppose the length of weir to be six feet, and depth of leakage to be .183 of a foot; opposite to this in weir table and column for 6 ft. weir will be found 93.28 cubic feet per minute, and this quantity is to be taken from every test made of that particular wheel, supposing the water not to be drawn from the flume during the test; if it is, then the leakage must be taken as before. To illustrate, a test as now taken is here given. The point of attachment of brake to scale beam is ten feet, and each revolution must be multiplied by ten to get correct speed. Look in weir table below for cubic feet discharged. Test of an 18-inch Wetmore wheel, September 30, 1876:

| No. 7.   | Head.<br>18.80 | Weight.<br>162.5 | Rev. per min.<br>305 | Weir.<br>.650 |
|--|----------------|------------------|----------------------|---------------|
| Quantity as per table 624.62 - 93.28 = 521.34 cubic feet per minute. |                |                  |                      |               |
| $521.34 \times 18.80 \times 62.33$                                   |                |                  |                      |               |
| <hr style="width: 100%; border: 0.5px solid black;"/>                |                |                  |                      |               |
| 33000 = 17.91 H. P. of water.  |                |                  |                      |               |
| $305 \times 10 \times 162.5$   |                |                  |                      |               |
| <hr style="width: 100%; border: 0.5px solid black;"/>                |                |                  |                      |               |
| 33000 = 15.02  |                |                  |                      |               |
| $\frac{15.02}{17.91} = .8114$ Ratio of useful effect.                |                |                  |                      |               |

### Formula for Tabling Wheels.

Q = quantity discharged per second at any head, h.

V = velocity due head h.

Q' = quantity with any head h'

V' = velocity due head h'

R = relative velocity.

D = diameter of wheel.

The Q having been determined for any given head, to find it for any other head  $Q' = Q \times \frac{V'}{V}$

The horse power having been determined for any given head, to find it for any other head  $\frac{H. P. \times V' H'}{V \times H}$

The revolutions having been found for any given head, to find them for any other head  $\frac{V \times R}{D \times 3.1416} \times 60 = \text{number of revolutions per minute.}$

R = relative velocity, determined by experiment.

Having the outlet of one wheel of a certain pattern measured and its power determined, the power of another of similar pattern is approximately obtained by comparing the outlet with the one experimented upon.

### Steam and Pressure Gauges.

Is it a matter of importance that such instruments should indicate correctly, and if so, do those using them take pains to verify their accuracy? Recently while testing the turbines used at the water works of St. Johnsbury, Vt., it came in my way, also, to test the accuracy of the pressure gauges used there; these were made by the Utica Steam Gauge Co., Utica, N. Y. The test was made by getting the exact area of the waste valve, using a knife-edged pivoted beam resting on a knife-edged top of valve piston then with sealed weights the pressure in pipe was accurately ascertained, and to be 11 per cent. less than that shown by the pressure gauge.

## Elkhart Mills, Power, and the Water Used to Produce It.

**MESSRS. MILLER & MAXON.**—*Gentlemen:*—Nearly a year since, acting for the manufacturers hereinafter to be mentioned, you employed me to ascertain the power used by the said manufacturers, and the quantity of water necessary to produce the power used and the power deeded.

My only instructions were to do it by the most perfect methods known to me and do it right. A preliminary trial was made in June last, and all interested in such matters were invited to witness all tests, particularly the members of the Hydraulic Company and their attorney, and to all desirous of knowing the matter was fully explained.

Except in cases of indefinitely worded deeds, there is no feature in the use of water, or power in mills, that may not be elucidated and made so plain as to leave no shadow of excuse for litigation except that of a desire to get that which belongs to another.

The deeds in each case to be named give a definite amount of power with right to use sufficient water to produce it, under the conditions specified, a positive condition of which is that measurement of the water shall be after it issues from the wheel.

Two power scales of different capacities were purchased of their manufacturers, Emerson Power Scale Co., Florence, Mass.; these are made upon the same principle as the ordinary Fairbanks scale, but rotary. The largest carries its load nine, the smallest six, feet at each revolution of shaft to which it is affixed.

To operate: the key is removed from driving pulley, thus leaving pulley loose upon its shaft; the scale is then placed on shaft close to hub of pulley, and rigidly keyed to the shaft. There are spurs projecting from the rim of scale to which the levers of scale connect to the arms of the pulley, so that all of the strain from belt rests upon the scale, and that strain or weight is shown upon scale in pounds as on the ordinary scale beam.

**Muzzy's Starch Mill, capacity 1,000 bushels of corn or 24,000 pounds starch per day, 2 Eclipse turbines, one 48, the other 54, inches in diameter.**

|  |             |
|--|-------------|
| 48 inch or its work weighed January 5, rev. $118 \times 9 = 1062 \times 875 =$ |             |
| $929,250 \div 33,000$ .....  | 28.15 h. p. |
| 54 inch or its work weighed January 6, rev. $90 \times 9 = 810 \times 1150 =$  |             |
| $931,500 \div 33,000$ .....  | 28.22 h. p. |
| Total power used, all machinery in full operation.....                         | 56.37 h. p. |

**Globe Tissue Paper Mill, capacity one ton per day, 3 turbines, American 66, Victor 25 and 30 inches.**

|   |             |
|---|-------------|
| 66 inch American or its work weighed Jan. 15, rev. $99 \times 9 =$                                    |             |
| $891 \times 1325 = 1,180,575 \div 33,000$ .....   | 35.77 h. p. |
| 30 inch Victor, washer wheel, Jan. 17, rev. $90 \times 6 = 540 \times 825 =$                          |             |
| $445,500 \div 33,000$ .....   | 13.50 h. p. |
| 25 inch Victor, 84 inch paper machine, paper running 97 ft.   |             |
| per minute, rev. $44.5 \times 9 = 400.5 \times 1491 = 588,735 \div 33,000$ .....                      | 17.84 h. p. |
| Total power for 4 Beating engine, Washer, Jordan,<br>Pumps, Paper Machine, Rag Cutter and Duster..... | 67.11 h. p. |

### Elkhart Knitting Mills.

**2 set 48 inch Cards, 3 Jacks, in all 720 Spindles, 2 Parker Twisters, 96 spindles each, 4 Spoolers, Dusters, Dryer and Fan, Stocking Dryer and Fan, Kulp Winders, Hydro Extractor, 60 Knitting Machines.**

|  |             |
|--|-------------|
| Power to drive all weighed Jan. 9, rev. $250 \times 6 = 1500 \times 425 =$ |             |
| $637,500 \div 33,000$ .....  | 19.31 h. p. |

### Kulp & Umel Planing Mill.

**Two Rip Saws, Lathe, Matcher, Resaw, Daniels Planer, 26 inch Fay Planer, Molder, Sand Paper Machine, and Sticker.**

|   |             |
|---|-------------|
| Usual machinery running, rev. $200 \times 6 = 1200 \times 630 = 756,000 \div$ |             |
| $33,000$ .....  | 22.90 h. p. |
| With every machine in mill running, Jan. 12, rev. $175 \times 6 =$            |             |
| $1050 \times 825 = 866,250 \div 33,000$ .....                                 | 26.25 h. p. |

**C. G. Conn's Musical Instrument Works.**

Every machine in works running, rev., Jan. 21, 130x9=  
 1170x320=374,400 ÷ 33,000.....11.35 h. p.

**Sage Brothers' Flouring Mill, capacity 280 barrels per day.**

Decided right to use sufficient water to drive five runs of four foot buhrs to grind 15 bushels of red merchantable wheat per hour, one run to grind 40 bushels of corn per hour, also smut mills and all necessary machinery to prepare flour and meal for market ; as one wheel of same capacity is allowed for four runs of buhrs, the quantity decided is sufficient practically to drive seven and a half runs each, grinding 15 bushels of hard wheat per hour. Messrs. Kulp & Umel with similar deed to two and a half. A 4 foot buhr driven by spur gears was disconnected from turbine and connected to a horizontal shaft by a pair of bevel gears, the driver having 56, the driven 42, teeth; a belt running horizontally from another line of shafting drove the stone. The power scale was placed on shaft close to gears driving buhr.

Mr. J. W. Lamb, of Constantine, Michigan, an experienced miller, was employed to do the grinding, commencing Saturday, 19th. After making some experiments he had pulleys changed, stones redressed and seemed to take the utmost care to make the tests absolutely accurate, and I believe did so; four days were expended in making the several trials.

An excellent weir 20 feet in length was used for measuring the discharged water. There was a leakage of 185 feet per minute to be deducted from the quantity flowing over the weir indicated by the depth during each test except the last.

A 48-inch Leffel wheel was used, and nearly at its full capacity during the heaviest tests.

The largest scale was used, making the trials tabled below so that the revolution of shaft must be multiplied by 9 to get feet the load is carried; that sum must be multiplied by the weight, to find the foot pounds; dividing those by 33,000 will show the work done in h. p.

Multiply cubic feet by the head, and that sum by 62.34, weight of a cubic foot of water, to find power of water used.

Dividing the work power by the power of water will show useful effect of the turbine.

While making the experiment it required the miller's constant attention to grind fifteen bushels of wheat per hour; indeed it was evident that it would be impracticable to make a business of grinding that quantity, so it was found necessary to do it upon two stones, requiring 21 h. p. of water per each run, grinding seven and a

| Grinding bushels of wheat per hour.            | Head in Feet | Rev. of Stone | Dep. on Weir. | Cubic Feet. | Rev. of Shaft | W'gt in Lbs. | Work in h. p. | Power of Water in h. p. | Useful Effect. |
|--|--------------|---------------|---------------|-------------|---------------|--------------|---------------|-------------------------|----------------|
| 1. Indiana red, 15 bushels.....                | 8.85         | 205           | .709          | 2184        | 154           | 590          | 24.78         | 36.59                   | .678           |
| 2. Minnesota red spring, 15 bushels.....       | 8.70         | 197           | .725          | 2264        | 148           | 680          | 27.44         | 37.21                   | .733           |
| 3. Indiana white, 15 bushels.....              | 8.87         | 215           | .672          | 2001        | 161           | 440          | 19.32         | 33.52                   | .576           |
| 4. Minnesota red spring, 31 bushels per hour   | 6.17         | 201           | .544          | 1409        | 151           | 210          | 8.65          | 16.42                   | .527           |
| 5. " " " 31 " 7 1/2 "                          | 9.92         | 197           | .450          | 1014        | 148           | 270          | 10.87         | 19.00                   | .572           |
| 6. " " " 7 1/2 " 38 "                          | 9.92         | 197           | .476          | 1121        | 148           | 345          | 13.93         | 21.00                   | .663           |
| *7. Corn fine meal,                            | 9.50         | 181           | .740          | 2340        | 136           | 800          | 29.67         | 41.99                   | .706           |
| 8. Feed,                                       | 9.65         | 200           | .740          | 2340        | 150           | 675          | 27.61         | 42.40                   | .651           |
| 9. Driving stone without work.....             | 9.85         | 202           | .....         | .....       | 151           | .....        | .....         | .....                   | .....          |
| 10. Whole machinery in mill, 150 bbls. per day | 7.84         | .....         | 1.629         | 8173        | .....         | .....        | .....         | 121.00                  | .....          |

\*From 21 to 22 bushels were ground, but not fine enough to bolt. While making these tests the head was changed to ascertain the co-efficient of useful effect under such conditions.

half bushels per hour, or 42 horse power for grinding fifteen bushels, and that ten seven and a half runs and two and a half equal runs for machinery, to prepare the product for market, would equal  $262\frac{1}{2}$  h. p. of water for the quantities deeded. In grinding corn twenty bushels per hour was all that could be done well with forty-two h. p. of water; to grind the forty bushels would require at least eighty-four and the full hundred to grind and prepare the meal for market, making for the Sage Brothers' mill  $362\frac{1}{2}$  h. p. Indeed I believe it will be impossible under the existing conditions to do that amount of work with the quantity named.

Messrs. Kulp & Umel have the right to two fifteen bushel runs, and machinery equal to five run of buhrs grinding seven and a half bushels of wheat per hour; the same rate entitles them to one hundred and five h. p. of water.

Allowing the same rate for the other mills, that is, three h. p. of water for each two h. p. of work, Muzzy's starch mills are entitled by deed to one hundred and thirty-five h. p., the Globe Tissue Paper Co., ninety, C. G. Conn and the Knitting mill each forty-five. These are common rates, and the grinding tests show the allowance to be none too much, in fact not enough unless the head can be kept somewhere near the height at which the wheels are set for. A wheel set under nine feet head will of course give more power under ten, but it by no means follows that it will do it with less water.

There were two hundred and forty-seven h. p. of water flowing through a break in the flush boards on the dam January 3, current month, but the mills on the other side of the river were not at work, yet the water in race drew down during the day.

Sage Brothers, Kulp & Umel, Tissue Paper Co., Knitting Mill Co., C. G. Conn and Muzzy Starch Co. still have an unused right to 360 h. p. more of water than they take. If they call for that it is somewhat difficult to conceive where it is coming from.

My record of measurement of discharge from turbines used in the Combination board, Excelsior starch and Elkhart paper mills, proved them capable of using five hundred h. p. of water, which, added to the quantity deeded to the other six mills this side, make for the two-thirds this side the river 1282, plus 641 for the other side, equaling nineteen hundred and twenty h. p. for the whole.

Six inches water flowing over dam falling ten feet evolves about 398 h. p.; 9 inches, 730; 12 inches, 1120; 15 inches, 1569; 18 inches, 2048.

It should be borne in mind that though the rainfall may be equal now to what it was fifty years ago, yet the cultivation and drainage of the land causes a much more rapid evaporation and clearance of the supply than formerly.

The following results obtained from measurement of water used at different mills will prove my allowance for water to produce the deeded power to be moderate.

The rate of mills is based upon some generally understood matter pertaining thereto.

Cotton mills upon their number of spindles; woolen mills upon number of sets; paper mills upon number of tons made per day; flouring mills upon number of barrels of flour per day. As the rate of mill denotes its value, it is not likely to be underrated, and there is often reason to doubt whether the entire amount of work is done that its rate would indicate. Certainly the rate is rarely exceeded.

To ascertain how much power is required to grind a bushel of wheat, it is simply necessary to measure the water used when the mill is doing its ordinary work, and divide the power of that by the bushels ground per hour.

The least power per bushel used at any mill that I have ever tested was at Lanesboro, Minnesota, White & Beynon; 3.18 h. p. per bushel; test made in 1874. New mill in perfect order. Head about 24 feet.

The following results made four years ago at Mishawaka will show what a difference there is in such matters, and it is necessary that it should be considered, to understand what is necessary in the case in hand.

#### ST. JOSEPH MILLING COMPANY, MISHAWAKA, July 6, 1884.

Ordinary discharge of water  $8\frac{1}{2}$  feet head 6174 cubic feet per minute, the power of which is 93.35 h. p. Capacity of mill rated 100 barrels per day of 24 hours.



100 barrels at  $4\frac{1}{2}$  bushels=450 bushels  $\div$  24 hours=18.75 bushels per hour; 93.35 h. p.  $\div$  18.75 bushels=4.97 h. p. of water per bushel.

RIPPLE MILL, MISHAWAKA, IND., July 8, 1884.

A. & J. H. EBERHART & CO., PROPRIETORS.—Ordinary discharge of water 9540 cubic feet per minute, the power of which is 114.08 h. p. Capacity of mill rated 130 barrels in 24 hours.

130 barrels by  $4\frac{1}{2}$  bushels=585  $\div$  24 hours=24.4 bushels per hour; 114.08 h. p.  $\div$  24.4 bushels=4.68 h. p. of water per bushel.

MISHAWAKA MILL, MISHAWAKA, IND., July 11, 1884.

W. & J. MILLER, PROPRIETORS.—Ordinary discharge of water 1634 cubic feet per minute, the power of which is 185.72 h. p. Capacity of mill rated 175 barrels per day of 24 hours.

175 barrels x  $4\frac{1}{2}$  bushels=787.5  $\div$  24 hours=32.8; 185.72 h. p.  $\div$  32.8 bushels=5.66 h. p. of water per bushel.

Higgate, Vt., July 4, 5 and 6, 1885, I measured the water discharged from an excellent tub wheel grinding wheat, the result was to be used in a case in litigation and special care was taken.

To grind the ordinary wheat used there it required 5.2 h. p. per bushel. For the hard red wheat 5.9 h. p. per bushel.

Twenty years ago a revolution was taking place in regard to the best methods of utilizing the power of falling water; the turbine was taking the place of the earlier overshot and breast wheels, its compactness for its capacity astonished those interested, and the claims for it were so extravagant that manufacturers were bewildered and hardly knew what to do. The deeds of that and earlier times also were often very indefinite.

There were such doubts and conjectures about turbines, milling hydraulics, and dynamics that a series of experiments were instituted for the purpose of making such matters clear. Instruments of the simplest and most accurate effectiveness possible were substituted for the crude devices then in use.

It was a common idea then that a turbine to be really efficient should be built for the head under which it was to work; that an aperture would not discharge proportionally the same under different heads or different sizes; that more work could be done with the same wheel in the night than in the day-time, etc., etc.

A testing flume was constructed and for several years turbines were tested under 18, 12 and 6 foot heads. In round numbers the wheel that would give 100 h. p. under 18 feet, would give but 50 under 12 and 20 under 6 feet.

A short experience proved many common ideas to be fallacious, the same apertures discharged proportionally for any head and the turbine that was good under one head was proportionally efficient under all others, and gave the same results night or day.

At that time 73 to 75 per cent. seemed to be a sort of normal efficiency; almost any aspirant for fame as turbine builder could reach that point.

The deeds of the Elkhart Hydraulic Company are in a measure based upon the merits of the American turbine, and as various kinds are in use under those deeds it is essential to show such to be equally effective.

The following results obtained by tests of wheels built before the system of testing was established will show the efficiency of the ordinary American turbine for a range of sizes:



## AMERICANS TESTED THE DATES NAMED:

Test of 48-inch, January 29, 1874.

| No. of Test.     | Head. | Weight. | Rev. p'r<br>Min. | Horse<br>Power. | Cubic<br>Feet. | Per<br>Cent. |
|------------------|-------|---------|------------------|-----------------|----------------|--------------|
| Whole Gate ..... | 17.65 | 1320    | 107.8            | 86.24           | 3418.11        | .7598        |
| Part Gate .....  | 17.66 | 1100    | 110.3            | 73.53           | 3010.79        | .7316        |
| “ “ .....        | 17.76 | 960     | 104              | 60.51           | 2594.01        | .6948        |
| “ “ .....        | 18.16 | 500     | 106              | 32.12           | 1690.47        | .5548        |

September 29, 1873, 42-inch, right hand.

|                 |       |      |       |       |         |       |
|-----------------|-------|------|-------|-------|---------|-------|
| Whole Gate..... | 17.93 | 1200 | 112.5 | 61.36 | 2569.85 | .7095 |
| Part Gate.....  | 17.98 | 990  | 118.5 | 53.32 | 2218.55 | .7094 |
| “ “ .....       | 18.30 | 650  | 120   | 35.45 | 1452.72 | .7065 |
| “ “ .....       | 18.45 | 440  | 119.5 | 23.90 | 1213.58 | .5666 |

October 1, 1873, 42-inch, left hand.

|                 |       |      |       |       |         |       |
|-----------------|-------|------|-------|-------|---------|-------|
| Whole Gate..... | 17.90 | 1100 | 118   | 59.00 | 2536.02 | .6882 |
| Part Gate.....  | 18.00 | 980  | 120   | 53.45 | 2275.17 | .6946 |
| “ “ .....       | 18.13 | 820  | 121   | 45.10 | 1918.04 | .6884 |
| “ “ .....       | 18.43 | 420  | 116.5 | 22.24 | 1160.60 | .5479 |

November 11, 1873, 25-inch wheel.

|                 |       |     |     |       |         |       |
|-----------------|-------|-----|-----|-------|---------|-------|
| Whole Gate..... | 18.23 | 300 | 212 | 28.91 | 1158.24 | .7244 |
| Part Gate.....  | 18.30 | 260 | 207 | 24.46 | 983.53  | .7185 |
| “ “ .....       | 18.39 | 220 | 205 | 20.16 | 880.49  | .6565 |
| “ “ .....       | 18.60 | 110 | 208 | 10.40 | 555.69  | .5323 |

November 12, 1873, 20-inch wheel.

|                 |       |     |       |       |        |       |
|-----------------|-------|-----|-------|-------|--------|-------|
| Whole Gate..... | 18.85 | 120 | 253.5 | 14.97 | 606.54 | .6938 |
| Part Gate.....  | 18.55 | 110 | 243   | 12.15 | 528.55 | .6536 |
| “ “ .....       | 18.63 | 90  | 244   | 9.98  | 448.93 | .6313 |
| “ “ .....       | 18.77 | 50  | 225.5 | 5.13  | 285.15 | .5072 |

August 5, 1874, 60-inch wheel.

|                    |       |      |      |        |         |       |
|--------------------|-------|------|------|--------|---------|-------|
| Whole Gate, 1..... | 16.63 | 3000 | 88.1 | 147.27 | 6358.90 | .7315 |
| “ “ 3.....         | 15.94 | 2700 | 80.3 | 131.40 | 6220.86 | .7028 |
| “ “ 5.....         | 14.88 | 2500 | 80   | 121.21 | 5839.12 | .7394 |
| “ “ 7.....         | 14.82 | 2550 | 76.5 | 118.22 | 5849.43 | .6863 |
| “ “ 9.....         | 14.91 | 2300 | 79.5 | 110.81 | 5891.40 | .6690 |
| “ “ 11.....        | 14.73 | 2600 | 70.5 | 111.09 | 5961.55 | .6709 |
| “ “ 13.....        | 14.75 | 2450 | 74   | 109.88 | 5719.34 | .6908 |
| Part Gate, 15..... | 15.02 | 2450 | 74.2 | 110.17 | 5719.34 | .6800 |
| “ “ 17.....        | 15.12 | 2150 | 76   | 99.03  | 4049.47 | .7018 |
| “ “ 19.....        | 15.08 | 1850 | 79.5 | 82.16  | 4573.00 | .6832 |
| “ “ 21.....        | 16.41 | 1400 | 80.5 | 73.18  | 3693.02 | .6404 |
| “ “ 23.....        | 17.88 | 950  | 68.5 | 39.43  | 2296.70 | .5093 |
| “ “ 25.....        | 15.47 | 3900 | 000  | 000    | 5700.95 | .0000 |

June 7, 1873, 48-inch wheel.

|                    |       |     |       |       |         |       |
|--------------------|-------|-----|-------|-------|---------|-------|
| Whole Gate, 1..... | 11.91 | 700 | 103.5 | 43.90 | 2702.80 | .7224 |
| “ “ 2.....         | 11.88 | 750 | 99.5  | 45.22 | 2725.28 | .7398 |
| “ “ 3.....         | 11.86 | 800 | 95.5  | 46.30 | 2763.94 | .7482 |
| “ “ 4.....         | 11.92 | 850 | 96.5  | 49.41 | 2845.02 | .7484 |
| “ “ 5.....         | 11.89 | 870 | 90.5  | 47.11 | 2835.26 | .7383 |
| “ “ 6.....         | 11.90 | 900 | 88    | 48.00 | 2841.77 | .7525 |
| “ “ 7.....         | 11.87 | 920 | 86.8  | 48.40 | 2857.54 | .7555 |
| “ “ 8.....         | 11.88 | 940 | 84.5  | 48.13 | 2867.85 | .7489 |
| “ “ 9.....         | 11.92 | 960 | 83    | 48.29 | 2874.38 | .7491 |
| “ “ 10.....        | 11.92 | 860 | 88.5  | 46.43 | 2812.50 | .7535 |
| “ “ 11.....        | 11.92 | 880 | 90.5  | 48.26 | 2841.77 | .7546 |

Average per cent. under most favorable conditions, .7232.

## Leffel 30-Inch, Tested in 1872.

| No. of Test.                | Head.  | Weight | Rev. p'r<br>Min. | Horse<br>Power. | Cubic<br>Feet. | Per<br>Cent. |
|-----------------------------|--------|--------|------------------|-----------------|----------------|--------------|
| Whole Gate, 1.....          | 15.60  | 300    | 201              | 27.41           | 1429.12        | .650         |
| " 3.....                    | 15.54  | 320    | 194              | 28.22           | 1455.57        | .662         |
| " 5.....                    | 15.48  | 340    | 187              | 28.90           | 1463.74        | .675         |
| " 7.....                    | 15.425 | 360    | 181.5            | 29.70           | 1469.87        | .693         |
| " 9.....                    | 15.41  | 380    | 175              | 30.23           | 1469.87        | .706         |
| " 11.....                   | 15.395 | 400    | 175              | 31.82           | 1471.92        | .743         |
| " 13.....                   | 15.38  | 420    | 162.5            | 31.02           | 1471.92        | .725         |
| " 15.....                   | 15.38  | 440    | 151.5            | 30.30           | 1471.92        | .708         |
| " 17.....                   | 15.37  | 475    | 135.5            | 29.26           | 1469.87        | .686         |
| " 19.....                   | 15.32  | 405    | 137.5            | 28.99           | 1461.76        | .685         |
| " 21.....                   | 15.335 | 415    | 151              | 28.48           | 1465.78        | .655         |
| " 23.....                   | 15.33  | 415    | 154              | 29.05           | 1465.78        | .683         |
| " 25.....                   | 15.33  | 495    | 162              | 20.82           | 1461.69        | .704         |
| " 27.....                   | 15.31  | 415    | 154              | 29.05           | 1463.74        | .687         |
| $\frac{3}{4}$ Gate, 29..... | 15.65  | 300    | 161              | 21.95           | 1106.73        | .664         |
| $\frac{1}{2}$ " 31.....     | 16.037 | 180    | 165              | 13.13           | 637.42         | .591         |

Victor Turbine, Made by Stilwell & Bierce, Dayton, Ohio,  
Tested the Dates Named.

## Test of a 25-inch wheel, July 25, 1877.

| No. of Test.    | Head. | Weight | Rev. p'r<br>Min. | Horse<br>Power. | Cubic<br>Feet. | Per<br>Cent. |
|-----------------|-------|--------|------------------|-----------------|----------------|--------------|
| Whole Gate..... | 18.07 | 625    | 200              | 56.81           | 2214.55        | .7533        |
| Part Gate.....  | 18.04 | 600    | 198              | 54.00           | 2208.44        | .7192        |
| " ".....        | 18.13 | 500    | 208              | 47.27           | 1964.67        | .7042        |

## Test of a 26-inch wheel, July 26, 1877.

|                 |       |     |     |       |         |       |
|-----------------|-------|-----|-----|-------|---------|-------|
| Whole Gate..... | 18.33 | 500 | 246 | 37.27 | 1387.27 | .7777 |
| Part Gate.....  | 18.41 | 425 | 269 | 34.64 | 1284.30 | .7774 |
| " ".....        | 18.43 | 390 | 246 | 29.07 | 1145.59 | .7305 |
| " ".....        | 7.97  | 75  | 246 | 5.59  | 757.93  | .4911 |

## Test of a 15-inch wheel, March 26, 1878.

|                 |       |     |       |       |     |       |
|-----------------|-------|-----|-------|-------|-----|-------|
| Whole Gate..... | 18.34 | 300 | 323   | 29.36 | 974 | .8705 |
| Part Gate.....  | 18.10 | 300 | 321.5 | 29.22 | 970 | .8808 |
| " ".....        | 18.39 | 160 | 326.5 | 15.83 | 755 | .6035 |
| " ".....        | 18.74 | 100 | 320   | 9.09  | 492 | .5220 |

## Eclipse Double Turbine, Manufactured by the same Co.

## Test of a 30-inch Eclipse wheel.

|  | Head. | Rev. p'r<br>Minute. | H. P. | Cubic<br>feet. | Per<br>Cent. |
|--|-------|---------------------|-------|----------------|--------------|
|  | 18.79 | 184.5               | 33.85 | 1253           | .7628        |
|  | 18.93 | 170                 | 31.66 | 1214           | .7280        |
|  | 19.10 | 173.5               | 24.44 | 1026           | .6497        |
|  | 19.10 | 165                 | 18.00 | 862            | .5786        |
|  | 19.18 | 166.6               | 12.11 | 699            | .4779        |

It will be seen by the tabled tests of wheels that the American is not exceptionally economical, nor is it possible for any wheel to be economical where there is a variation in the head of one-third, though of course a good part gate wheel is better than one only efficient at whole gate. There is an idea that turbines discharge 60 per cent. of the theoretical quantity due their

openings. The idea originated from obsolete wheels of the Fourneyron type. Of the modern wheels I have had care of tabling hundreds, yet have never known of one reaching 55 per cent. of its opening; 52 perhaps is a fair average, 49 about all the American can do.

An aperture that will measure, will discharge a trifle short of 60 per cent. but such aperture can never be used in a forebay to determine the quantity of water used in a mill; it is absolutely impracticable for that purpose.

A weir in forebay is also impracticable unless a manager stands beside it at all times to give the proper depth for quantity, and then only at a serious loss of head, and if such weir is placed below discharge of wheel, it also causes such loss of head that wheels subject to such changes can never be economical.

To divide water in proportion to ownership at dam or conduit with weir belongs to the ideas of the past. The water may go through one opening two feet per second, the other six, depending upon the size of wheels below. It is true that the water cannot be drawn below crest of weir by either party, but the one with the most capacious wheel will take water in proportion, and the expense of weir may be saved by fixing upon a mark below which the water shall not be drawn.

A gate and float arrangement may be put in flume or forebay by which proportion or quantity of water may be delivered without perceptible loss of head, the whole working automatically; and while the quantity due is adhered to the gate will stand open, but if more is attempted to be taken the gate closes in proportion, and a proportional loss of head results, though the full quantity of water is still supplied. The arrangement is simple and more accurate than a weir, and with it the head is invariably kept at a standard height; if the supply is sufficient, it is given in full, if not, in proportion.

With such an arrangement and good wheels water may be economized to the highest practicable extent.

More precaution will be used in the selection of wheels when the fact becomes understood that turbine building is not a science, it is simply "cut and try." There are some who can do better than others, but the best cannot go to work and be perfectly sure to reach the results aimed at, and however well one may do himself he cannot teach another how to do the same. Owing to uncertain causes, such as warping of patterns, shrinking or expansion of castings, turbines made from the same patterns often differ exceedingly in useful effect. Large wheels in particular are the most likely to fail because the expense has prevented experimenting upon them. A case that almost every manufacturer of twenty years' experience will recall may interest. It is of the Manville, R. I., mill so profusely illustrated in the *Leffel* circular fifteen years since. The artist drew somewhat upon his imagination. The mill is shown with four 84-inch wheels, while it never had but three, those being helped out by an engine of 430 indicated h. p. The tabled power of the three 84-inch wheels and the 430 h. p. engine rate something like 1700 h. p. The manager ran under those conditions many years, then applied to me about procuring another 84-inch *Leffel* or some other of like capacity. In the conversation that ensued, the question of power was raised and I told him that the whole mill did not need 800 h. p. The idea was poohed at, but a test soon proved that fact, and the only thought since has been to exchange and get better turbines of less size but greater efficiency.

Intelligent co-operation between those who let and those who use power will prevent litigation and increase by far the effectiveness of the power used. But to do this it must be borne in mind that a turbine runs at a relative velocity with the water that propels it, and can only do its best work at one point for a given head, and declines rapidly either way at any deviation from that head; unless the wheel is exceptionally good at part gate.

Yours truly,

JAMES EMERSON.

ELKHART, IND., January 30, 1889.

## Division or Measurement of Water Power.

The time can not be distant when those interested will look back and smile at the crude methods continued in use up to this time to determine the quantity of water used by the different parties taking power from the same fall—methods well enough a half century since, when the most of such power was running to waste, but simply ridiculous now, when the demand is far beyond the supply.

The float method in use at Lowell can hardly be considered anything more than a preliminary to guessing at the quantity used. It, however, does not interfere with the operations of the mills, but any agent may favor his discharge while such measurement is being made, and there were rumors that such cases occurred at times. Mr. Francis has seemed ready to adopt a better plan, whenever such is found, though his many cares have prevented him from experimenting personally for the purpose of developing one.

There are or were various methods in use at Lawrence—wiers here, shanties there; weirs to measure leaks, a weir to test the *tester*—examinations of apparent gate opening, examinations in every conceivable place except, perhaps, the right one. Yet, what would the whole amount to in case those interested should combine for the purpose of deceiving those making the measurements? It is not likely that such a combination exists, but a method that can be affected in that way is a very imperfect one, and the use of such indicates the lack of the "fertility in expedients" necessary to meet emergencies so common in the engineering business. The continued dependence upon old foreign methods is discreditable alike to those having charge of the immense water powers of this country and the ingenuity of our people.

Several years ago, and before any arrangements were made for measuring the power at Holyoke, I advised the agent of the Water Power Co. to arrange to measure the discharge from the mills, then being constructed, in the tail-race of each; also to have all wheels that were to be used in Holyoke tested before being set in the wheel-pits for which they were designed. Reflection soon caused me to abandon ideas so crude. Measurements in the tail-race reduce the head and change the discharge and conditions generally, notifies the party interested of what is being done, and gives a chance to reduce the work and favor the discharge of water.

To attempt to determine the discharge of a wheel in a mill by comparison with a previous discharge in a testing flume, when the wheel was new and in perfect condition, would be unjust to both parties interested. Because a wheel can discharge 5000 cubic feet per minute, it by no means follows that quantity is used in the mill. A larger wheel is invariably put in than actually required, to have a surplus power for emergencies. The buckets and chutes of a wheel soon become rough, get broken, become clogged, or it would require but little ingenuity to so change the gate arrangement as to deceive completely as to the state of gate opening. Any pretense of giving the discharge of one wheel by comparison with that found by test of another of the same make, could only be done by ignoring the knowledge gained from a dozen years of constant experience in turbine testing, namely: That builders are constantly changing their plans; still further, that two wheels designed to be exactly alike, made from the same pattern, often vary wildly in their discharge. In short, the adoption of such a plan for measurement would have been the acknowledgment of such ignorance and incompetency in such matters, that I advised a series of experiments for the purpose of finding an accurate but simple and inexpensive plan for measurement of the water used by manufacturers, free from interference with the work of the mill, or that could be affected by parties interested. The purpose was suggested in the last edition of this work, in the description of the Holyoke

**Testing Flume.** It is a pleasure to state that that purpose has been accomplished by the finding of a simple automatic method by which the water flowing over any fall may be accurately measured or divided, so that each owner can have the exact quantity belonging to him and no more, unless by consent of the others. The operation is continuous. An illustration of the plan may be seen upon next page.

D represents the ordinary head gate to race, raised sufficiently to supply the mill and keep the water to its proper height. K represents a wicket gate placed in the lower end of race and near penstock, in which the turbine stands. T, a cylindrical tank, with a square recess on one side near the bottom. In this recess there are two openings: one to let the water in, and another to let it out down through the pipe, C, shown by dotted lines. These openings are opened or closed by the swinging cover or valve, e, which works upon the center pivot, t. The valve is connected to the float, F, by a rod connected at s. In the tank, T, there is placed the float, N, which has a rigid central shaft projecting upwards, connecting at the upper end to the wicket gate, K, by the bell crank, A, and rod, B.

#### OPERATION.

The head gate, D, is raised sufficiently to keep the canal, race or flume filled to a fixed water level, when the quantity agreed upon is being used. The float buoy, F, is half submerged at that time, and both the openings in the tank, T, are closed or opened alternately in a slight degree with the oscillations of the surface water acting upon the float, F. The wicket gate is kept at a fixed opening so long as the draught is constant. Suppose, however, the mill owner attempts to take more than agreed upon, and opens his wheel gates accordingly? The velocity of water in the race instantly increases, the surface level drops, and with it the float, F, which opens the inlet to the tank, T, and, as that fills, the floating buoy, N, rises, and the wicket, K, closes until the velocity is checked and the surface level is restored to its proper position. If it becomes too high, the float, F, opens the outlet and the water in tank, T, is discharged down through the pipe, C, shown by dotted lines. This opens the wicket more, so that the quantity due the mill is always ready, if the general supply is sufficient; if not, then all the head gates upon the fall are to be opened in proportion, so that each mill will invariably get its share. If one attempts to take more, he will simply lose power through loss of head, in proportion to the quantity he unjustly tries to appropriate.

To measure or deliver a given quantity, it is only necessary to adjust the wicket gate in unison with the proper surface level until the discharge is the exact quantity agreed upon, which may be determined by a weir below, or in any manner that may be selected; then, when the discharge is right, secure the wicket gate and floats in a manner beyond chance for change, unless by consent.

The method is not theoretical, for I have had it in use many months and have watched its operation daily. It is sensitive far beyond my anticipations when first planned. It may be easily applied to the turbines or other devices used to operate head or overflow gates. With its aid the surface level in a canal or race may be kept constant, so that the most perfect economy is practicable, for it prevents the drawing down of head and the use of an unnecessary quantity of water to make up therefor. It will not *strike* for higher pay, go to sleep, or become careless. I believe it to be perfectly practicable for measuring or dividing water used for power under any condition likely to occur, and far more accurately and cheaply than any other plan known.

By using a hanging balanced gate, like Fig 2, and which may be operated substantially as the wicket described, a perfect aperture discharge may be obtained. Such a gate may be used temporarily at almost any mill, as now arranged, and at any, as they may be arranged; so that wheels may be tested in the mills where they are used, without detention, instead of necessitating a testing flume made purposely for such tests.

A special testing flume in the future can only denote incompetency, for every mill may and should be a perfect testing apparatus by which the slightest defect in efficiency or power should instantly be made apparent. Competition will soon compel greater economy in manufactures, and particularly in the power required; and certainly a vast saving is possible in that, for there are thousands and tens of thousands of tons of coal annually consumed in the New England States alone, to make up for the water power wasted through ignorance or thriftless management.



**EMERSON'S WATER GOVERNOR,**  
OR PLAN FOR AUTOMATICALLY MEASURING OR DIVIDING WATER.

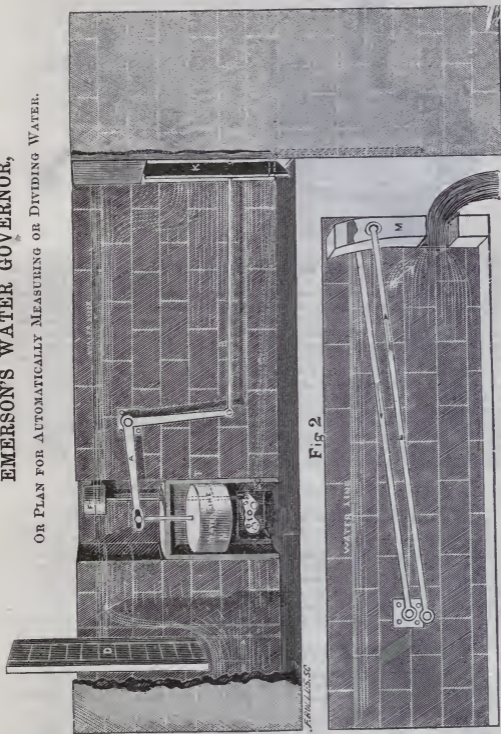
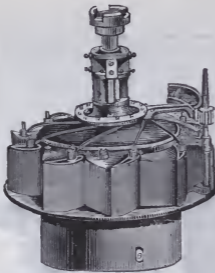


Fig 2



## Turbine Against Breast Wheel.



BREAST WHEEL

Messrs. Smith, Northam & Robinson, of Hartford, Ct., have a grist mill four miles from Hartford, that had a breast wheel 16 feet in diameter, 13 feet length of buckets, divided into three sections of 4 feet 4 inches each; the buckets were 18 inches in depth; three gates, in sections to correspond with wheel; the upper gate opening,  $5\frac{1}{2}$  inches; the next lower,  $3\frac{1}{2}$ ; the bottom one,  $3\frac{1}{4}$  inches; head, 12 feet. The breast wheel was supposed to be so superior to a turbine, that it had been kept in, though it was troubled much by ice during each winter. The firm consulted me upon the subject, and, after months of hesitation, concluded to change, and to follow my directions upon the following terms: The turbines to be selected by me, and tested before acceptance; the plans for change to be furnished by Wm. J. Sumner; my remuneration to be a barrel of bran or flour, according to my success. A weir was constructed in the stream below the mill; the breast wheel and turbine to be tested in the mill, by grinding—the discharge to be measured from each below the mill, under exactly the same conditions. The turbines, 20 and 25-inch New American, were tested by me at Hooke before acceptance. Results are given below.

### 25-INCH NEW AMERICAN WHEEL, TESTED OCT. 15, 1880.

| Head  | Weight | Rev per Minute | Horse Power | Cubic Feet | Percentage |
|-------|--------|----------------|-------------|------------|------------|
| 16.29 | 400    | 219.5          | 39.90       | 1583       | .8193      |
| 16.31 | 325    | 225            | 33.23       | 1337       | .8256      |
| 16.31 | 325    | 219            | 32.35       | 1249       | .8410      |
| 16.33 | 250    | 218.5          | 24.82       | 1032       | .7776      |
| 16.48 | 175    | 224.5          | 17.86       | 784        | .7318      |

### 20-INCH NEW AMERICAN WHEEL, TESTED OCT. 14, 1880.

| Head  | Weight | Rev per Minute | Horse Power | Cubic Feet | Percentage |
|-------|--------|----------------|-------------|------------|------------|
| 15.20 | 290    | 260.5          | 22.89       | 1001       | .7962      |
| 15.38 | 255    | 258            | 19.91       | 840        | .8160      |
| 15.41 | 230    | 258            | 17.98       | 754        | .8192      |
| 15.45 | 210    | 252            | 16.03       | 671        | .8188      |
| 15.63 | 155    | 253            | 11.88       | 522        | .7706      |

Before taking the breast wheel out, it was tested by grinding corn and measuring water below. The stones were sharp and in good condition. The head was 12 feet; gates opened in full. Ground old corn coarse, but very sharp, clean, even grit meal. The change was made; then the turbines were tested in the same way, but I think the corn stones were not in so good condition as when the breast wheel was tried, but may be mistaken. New corn was ground with the 25-inch turbine. The coarsest part of the meal was as near like that ground by the breast wheel as was possible to make it; but it was uneven, much of it being quite fine. This was attributed to its being made from new corn. The miller made every effort to make the trial fair. The results are given below. The rye stone was driven by the 20-inch wheel, the gate being opened about two-thirds—all that could be used. The flour produced was the nicest I have ever seen made from rye.

#### TEST OF BREAST-WHEEL, AT FULL GATE.

Head, 12 feet; length of weir, 10 feet; depth on weir, 8 13-16 inches; quantity of water, 1239 cubic feet per minute; 28.08 horse power. Ground 2050 pounds per hour, or 1.3 bushels per each horse power of water used.

#### TEST OF 25-INCH NEW AMERICAN WHEEL,

It having replaced the above-mentioned breast wheel. Head and length of weir the same.

*Full Gate.*—Depth on weir, 8 15-16 inches; 1266 cubic feet per minute; 28.7 horse power. Ground 3528 pounds per hour, or 2.2 bushels per each horse power of water used.

*Gate Opened Two-thirds.*—Depth on weir, 7 15-16 inches; 1059 cubic feet per minute; 24 horse power. Ground 2900 pounds per hour, or 2.15 bushels per each horse power of water used.

*Gate Half Opened.*—Depth on weir, 7 inches; 879 cubic feet per minute; 19.9 horse power. Ground 2400 pounds per hour, or 2.1 bushels per each horse power of water used.

#### TEST OF 20-INCH NEW AMERICAN WHEEL IN SAME MILL.

Depth on weir, 6½ inches; 789 cubic feet; 17.9 horse power. Ground four bushels of rye in seventeen minutes, or 14.1 bushels per hour. Eighty per cent. of power of water used; 14.3 horse power, or substantially a bushel per horse power.

After a few weeks' time, the proprietors sent me a barrel of "Pillsbury's best."

## Burning or Wearing Down of Step

May, and does happen with any make of turbines. Two turbines of the same make, seemingly exactly alike, and placed in a pit side by side, the step of one may wear down monthly, the other not at all. The cause was attributed to pressure from downward discharge; but if eighty per cent. is used to rotate wheel, the other twenty would be no more weight with downward than any other discharge. The Swain was noted for wearing down step. I knew of one 24-inch wheel that had nineteen steps in thirteen months. Others of the make had to be suspended by collars on shaft. A 36-inch wheel of the kind was sent to me to be tested. A collar that should have been on to keep wheel in place was left off. When the gate was opened, the pressure raised the wheel and brake, and it was impossible to test it until one hundred and fifty pounds were added to the brake to keep the wheel *down* upon the step. The Boyden wheels used at Lowell are suspended by neck on shaft, as are the Kilburn & Lincoln wheel of Fall River. The Risdon has a counterpoise above the wheel, drum-shaped (see his new wheel). Many plans have been tried. A common one is to channel top of step; another is to lead water from the penstock through a piece of ¾-inch steam pipe, to bottom of step—a hole up through first being made; some chamber the lower part of step, then make numerous small holes up through, like the top of a pepper-box, taking water from the flume through pipe. Great weight upon the step in the way of shafting, gearing, &c., should be avoided when possible.

## Railroad Suggestions.

It may be said that such suggestions are out of place in a work of this kind, but my experience has been gained from experiments made in many parts of the country—often in very distant parts—and the railroads have much to do with my ability to obtain such experience, consequently are part of the instruments I work with.

The rather common practice of roasting car-loads of passengers, when collisions or other accidents occur upon our railroads, has caused an agitation of the subject of car-heating. Safety as well as comfort is desired. The ancient and semi-barbarous plan of placing a stove at each end fails to give either, while such stoves take space for eight seats, disfigure and injure the cars, half roast a few near them, leaving the larger proportion to sit with cold feet and generally uncomfortable throughout the passage. Why not have a boiler for heating placed in the baggage car, to furnish steam for heating the passenger cars with safety?

Another want, is light trains between commercial centres and neighboring cities—trains that may readily be stopped and started, something as horse-cars are; that is, within reasonable distances. Such trains should be made up of light engines and cars, and have commutation fares. With such in operation, there would be no need of the heavy or through trains stopping so often. The manager of the ordinary railroad should feel ashamed to have a horse-railroad run for miles alongside, as from Boston to Lynn, and pay expenses.

Sunday trains on all roads are also much needed. Those who object to such, are impracticable persons, who do it through ignorance, and without consideration of the changes that have taken place since the Jewish Sabbath was instituted. At that time, labor was continued for from fourteen to sixteen hours per day; indeed, it is within the memory of those of middle age, when the hours of labor were nearly the same in the New England States. As a day for rest, Sunday has no such claim as formerly. The God of Moses had reason for requiring such a day; but the God of to-day has not. Besides, ages of experience has proved that He has been cheated constantly, for the most bigoted believer has never hesitated to lie in bed three hours later Sunday than other mornings; then, at evening, say: "Well, boys, we have got a hard day's work to do to-morrow, so we must go to bed early." All nature ignores the day: the billows rage as fiercely, the thunder is as loud, the tempest is as destructive, the blossoms as beautiful, vegetation and animal life as progressive upon that as upon any other day in the week. In Moses' time, families and tribes were separated but little. How different now! Business necessities often separate the nearest relations. The father of a family is often hundreds of miles away. It has happened three times in my own experience that telegrams, announcing the dying condition of members of my family, have been received late Saturday evening, and it is not likely my experience in that way is exceptional. Those who desire to observe the day as sacred, should be allowed to do so without hindrance; but it is very different when such believers try to compel all others to do the same. Our prisons are filled with theoretical believers in the idea, if we may judge from the declarations of those about to be hanged for murder. If such is the effect of believing one day better than another, would it not be better to teach that all days are good, and mix religion with business?

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## Water Supply for Cities.

Now that there is a general complaint of waste of water, and apprehension that the supply will soon be much less than the demand, would it not be well to have a high service for extinguishing fires, and a low one for domestic use, or have the discharge for the latter retarded? The unthinking user leaves a faucet open just as long, in most cases, where the pressure is a hundred pounds as such as where it is only five or ten.

## Apparatus for Regulating the Flow and Delivery of Water Through Canals, Flumes, and Water-Ways.

Specification Forming part of Letters Patent No. 275,371,  
dated April 10, 1883.

The object of my invention is, first, to maintain water in a canal or water-way at a uniform height during its passage to the outlet or flume; second, from this established uniform height of water in the canal or water-way to make a proportional division of the water at the outlets, giving to each consumer of water at his respective outlet the amount of water to which each is entitled, or a proportional amount of the whole to which each is entitled; third, to measure the amount given to each; and, fourth, to prevent any one of the consumers from using any more water than he is entitled to, the whole apparatus operating automatically, and being based on the *fixed law that any given velocity of water is acquired through a corresponding loss of head.*

This apparatus is applicable to be used at falls where the water is owned by several parties and is to be proportionally divided between them. It is also applicable for use where the water is owned by one company or owner, and is sold or leased, and a stated quantity is to be measured out to each purchaser or to each party leasing. It is also applicable for use for governing the flow of water from reservoirs, where water is stored for irrigation or for manufacturing purposes, and also for regulating the height of water in rivers or ponds to prevent backflowage in cases where movable dams or flush-boards are employed. I accomplish these objects by the apparatus substantially as hereinafter described, and illustrated in the accompanying drawings, in which—

Figure I. is a plan view representing a canal, and showing my invention as applied to the operation of wicket-gates, or those pivoted in a vertical position at one end of the canal, for the head-gates, and also at the other end, or at the flumes, where the water would be drawn from the canal and used for manufacturing or other purposes. Fig. II. is a vertical section of the same at line A of Fig. I. Fig. III. is a plan view representing a canal provided with vertical sliding head-gates at one end, and the gates at the other end or in the flumes, where the water would be drawn from the canal for use, being pivoted to or hung upon a bar placed in a horizontal position. Fig. IV. is an enlarged plan view of a flume and draft-tube, with a swinging gate hung in said flume and operated according to my invention in dividing and measuring the water drawn from the canal through said flume. Fig. V. is a part vertical section of the same at line B of Fig. IV., showing the swinging-gate and the lifting-float which operates it and the draft-tube and also a part vertical section at line D of Fig. IV., showing the construction of the governing-float which operates the valve controlling the flow of water into and out of the tank containing the lifting-float. Fig. VI. is a vertical section of the valve and its case, which controls the flow of water into and out of the tank containing the lifting-float, at line E of Fig. V. Figs. VII., VIII., and IX. are sectional views representing details of the valve and its case as applied to and used at the flumes or outlets of the canal.

In the drawings, let 1 represent the side walls of a canal or water-way, at one end of which is made the ordinary bulk-head, as *b*, provided with gates, as 2, to admit the water into the canal or water-way when opened for that purpose.

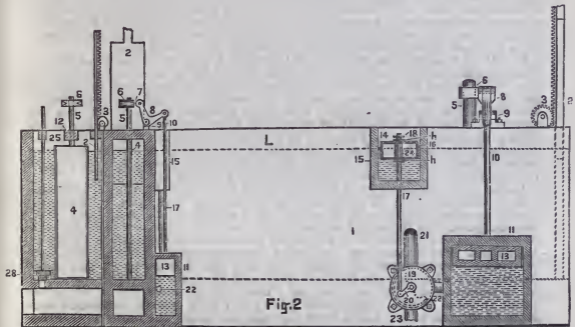
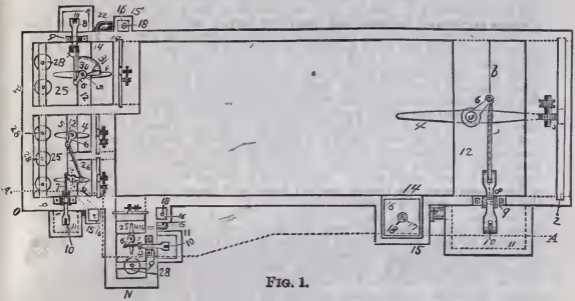
The ordinary head-gates may be used; but in this application I have shown pivoted gates, as being more easily operated, this class of gates being shown, as at 4, pivoted at 5 in the bulk-head at one end of the canal, 1, and in the

flumes at the opposite end of the canal, in Figs. I. and II. In the use of this pivoted gate to control the flow of water, the gate being set in an upright position to turn upon its post 5 as a pivot, an arm, as 6, is secured to its upper end, to which is attached a horizontal rod, 7, connected with one arm of a bell-crank lever, 8, pivoted at 9, the other arm being connected with a vertical rod, as 10, extending through the top of a tank containing a float, 13, to which the lower end of the rod 10 is secured. A smaller tank, as 15, is made upon or is so connected with the canal or its side wall that the water may flow freely into said tank, either by making the side next the canal wall open, as at 14, or by connecting said tank with the canal by a pipe, with its end opening into the canal, so that the water of the canal may flow through said pipe into the lower portion of the tank to fill the latter up to the same level as the water in the canal. This tank, as 15, I make preferably of rectangular form, and it contains a float, 16, which I make of a form in horizontal section to fit approximately the interior of the tank, but so that the float may move up and down freely, but not revolve therein. This float may be made of any suitable buoyant material; but I prefer to make it of some thin sheet metal, and hollow, and perfectly water-tight. A socket, as 24, extends vertically through this float, through which extends a rod, 17, whose upper end has a screw-thread made thereon, adapted to receive a nut, as 18, turned on to the upper end of the rod, with a shoulder, *b*, above and below the float, and this rod 17 extends down through the bottom of this tank 15, with its lower end attached to an arm, 20, secured to the hub of a valve, 73, inclosed within and fitting a cylindrical valve-case, 19, the hub extending out through the case at its axis. This valve-plug fits the interior of the case, so as to move freely therein, and is approximately of semi-cylindrical form, of sufficient extent in its circumference to cover the inlet and outlet ports in the case, and a pipe, 21, opens at one end into the canal and at the other end into the valve-case, 19, at the periphery, at the upper side, so that the water may pass from the canal through this pipe into the valve-case. The opening of this pipe in the valve-case forms its inlet-port, and the opening of a pipe, 23, into the valve-case, on its lower side and nearly opposite the pipe 21, forms the outlet-port of the valve-case, this pipe or opening 23 being merely to permit the water to flow out of the valve-case and to conduct it away to some waste-conduit, if desired. Another pipe, 22, opening into the valve-case at the side, extends to and opens within the tank 11, preferably in its lower portion.

It will be seen by referring to Fig. VII. that when the arm 20 (shown in dotted lines in that figure) is in a horizontal position the inlet-port or opening of the lower end of the pipe 21 in the valve-case is closed, being covered by the upper end of the valve 73, and the opening of the upper end of the pipe 23 in the valve-case or outlet-port is covered by the lower end of the valve 73.

By referring to Fig. VIII. it will be seen that when the arm 20 (shown in dotted lines) is inclined above a horizontal position the valve is moved so as to open the upper or inlet-port and close the lower or outlet port, and when this arm is inclined below its horizontal position the upper or inlet port is closed and the lower or outlet port is opened, as shown in Fig. IX. Of course with the valve in this position, shown in Fig. VII., water can neither flow into the valve-case through the pipe 21 nor out of it through the pipe 23; but with the valve in the position shown in Fig. VIII. water may flow into the valve-case through the pipe 21, and thence through the pipe 22 into the tank 11 to raise the float therein, and with the valve in the position shown in Fig. IX. water may flow out of the tank 11 into the valve-case, and thence out through the pipe 23. It will be seen that by this construction of valve the latter may be moved with the least possible friction in its case, and a very slight change in the height of the water in the canal to change the vertical position of the float 16 will be sufficient to operate the valve to open or close the ports in its case.

Referring to Fig. II., suppose it is desired to maintain the water in the canal at the height indicated by the dotted line *L*. The permanent or sliding head-gates, as 2, are raised to give the desired opening for the water to flow in, and the nut 18 is turned on to the upper end of the rod 17 until the float 16 in the tank 15 is sustained at the height shown in Fig. II. by the water which flows into said tank from the canal. While in this position the valve is held in the position shown in dotted lines in Fig. II., and the water flows





from the canal through the pipe 21, case 19, and pipe 22 into the tank 11, raising the float 13 into the upper part of the tank and holding the pivoted gate 4 wide open, or in a position lengthwise the canal, as shown in Fig. I., so that the water may flow into the canal past the gate 4, on each side the latter; but as the float 16 is so adjusted, if the water should rise in the canal, the float 16 would be raised, and the arm 20 of the valve would be inclined above a horizontal position and the valve moved into a position to open the outlet-port into the pipe 23 and close the inlet-port from the pipe 21, and the water would flow out from the tank 11 through the pipes 22 and 23, and the valve and the float 13 would fall and close the gate 4, or partially close it, until the water should fall nearly to the desired level at the line L, and when the inlet port or pipe 21 began to open as the float 16 was lowered by the fall of the water the tank would be slowly filled again and the float 13 would rise, and the gate 4 would be gradually opened to keep up the supply of water in the canal. This float 16 may be so nicely adjusted by turning the nut 18 either up or down that the slightest rise of water in the canal, and consequently in the tank 15, will operate the float 16, and the valve and the gate 4 will be shut sufficiently to keep out the excess of water over that required for use in the canal. The gate 4 is always wide open as long as the water remains at the lowest desired level, and when the water rises above this level the gate 4 is partially shut.

The flumes, as 25, at the points along the canal where the water is drawn therefrom, may be supplied with the same kind of gate, 4, each of which is operated by float 16, valve and its case 19, and lifting-float 13 in the same manner as the head-gate is operated, as above described, except that the arm 6 is attached to the post or pivot 5 of the gate in an opposite position from that in which it is attached to said post or pivot at the supply end of the canal. These flume-gates also operate to partially close and prevent any excess of water from passing into the flume over that amount previously determined upon. For example, suppose a manufacturing establishment to be located at any point along the canal, say at N, and to draw the water from the canal through the flume containing the single gate 4 at that point. This flume is provided with a tank, 15, containing a valve operating float, 16, like that hereinbefore described for the head-gate, into which tank the water may flow from the flume through a pipe whose orifice 14 opens into the flume, above the gate, in a direction opposite the flow of the current, and a valve and its case 19, like that above described for the operation of the head-gate, is connected with the float 16 by a rod, 17, with a tank connected by a pipe with said valve-case, and containing a lifting-float, as 13, which is connected with an arm, as 6, on the gate 4 in the flume by rods 10 and 7 and bell-crank lever 8, all as above described for the head-gate at the bulk-head.

It will be seen that in using the valve and its case 19 at the head-gate at the bulk-head *b* the arm 20 is so attached to the hub of the valve that as the float 16 is raised by the water in the tank 15 and in the canal the valve is moved so that the water may flow out of the tank 11, and by the falling of the lifting-float 13 the head-gate 4 will begin to close; but at the flumes the arm 20 is attached to the hub of the valve 73 in a reversed position, or as shown in dotted lines in Figs. V., VII., VIII., and IX., so that as the water falls in the flume the falling of the float 16 in the tank 15 would move the valve 73 into a position to permit the water to flow from the tank 11, and the lifting-float 13, in falling, would close the gate 4 in the flume 25.

In the above explanation I have referred to the details of the tanks and valve, as shown in Fig. I., at the head of the canal or bulk-head, because precisely the same arrangement is used at the flumes as at the bulk-head, with the exception that the arm 6 is attached to the pivot or post 4, and the arm 20 is secured to the valve 73 in a reversed position when applied and used at the flumes. For illustration, two other manufacturing establishments may be drawing water from the canal—one at O and another at P—and these flumes may be located any distance apart and along the side of the canal, or at its termination. For convenience I have represented them at the latter point, and side by side. Suppose that the party at N owns or has leased one-sixth of all the water which flows through the canal, the party at O three-sixths, and the party at P two-sixths, each flume-opening being of the proper area to permit that quantity of water to flow through at a given velocity—say of two feet per second. These flume openings being the ordinary head-gates, they may be changed to give different areas of opening at different sea-

sons of the year to meet the usual changes in the supply of water at such times, if found advisable. With the water at the height indicated by the line L the nut 18 on the rod 17 is turned so that the float 16 in the tank 15 holds the valve at the flume N in such a position that the float 13 in the tank 11 at that flume will hold its gate 4 in a position wide open, as shown in Fig. I. Inasmuch as the amount of water which can be drawn from a flume depends upon the velocity at the outlet of the flume at a given head, this additional use would tend to draw the water down or reduce its height in the flume, and the water in the tank 15 being always at the same level with that in the flume, the float 16 would fall and move the valve into a position to permit the water to flow out of the tank 11 through the pipe 22, valve 19, and outlet 23, and the lifting-float 13 would fall and partially shut the gate 4 in the flume, which would of course reduce the quantity of water passing into the flume at a greater velocity until his proper proportional quantity of one-sixth was reached, when the head and float would rise to their normal condition, allowing him still his proportional quantity, though at a loss of head in proportion to the quantity which he attempts to overdraw. In like manner the other owners or lessees at other points are governed or controlled in their use of water.

In Fig. I. there are two gates in the flume at O, one of which is provided with a double arm, 6, one of whose ends is connected with the arm of the other gate by a rod, 26, and the other end is connected with the bell-crank lever 8, connected with the lifting-float 13 in the tank 11, so that the movement of said float will operate both gates at the same time.

The flumes may be provided with the ordinary lifting or vertically-sliding gates 2, which may be closed at any time for the purpose of making repairs in the flume, or for any other purpose.

The tanks 15, connected with all the flumes, should all be securely locked and be kept under the charge of one man, so that no other person could have access to them; or the tanks 15 might be all located in one building or office and each be connected with its flume by a pipe, and all locked and in charge of one person.

If desired, a dial, 30, having a graduated scale, may be placed in any convenient fixed position near the pivot or post 5 of each gate in the flume, with an index secured to the post, as shown at P in Fig. I., so that a glance at the index and dial at any time would show how far open each gate was as to the area of its aperture, so that a slight computation might give approximately the quantity of water passing through.

It will be seen that this apparatus furnishes a very reliable system of maintaining the water in a water-way or canal at a standard height to give a uniform head, and with that head, to divide the water flowing through, giving to each owner or lessee the quantity to which he is entitled, and preventing any attempt on the part of either owner or lessee from using a greater quantity than that to which he is entitled.

In Figs. III., IV., and V. is shown a modification of the same invention as applied to gates arranged to move on a horizontal pivot for the purpose of measuring the amount of water passing through the gate-aperture, Figs. IV. and V., showing an enlarged detailed view, in which 33 represents a horizontal bar fixed in the sides of the flume, to which are hung, so as to swing freely thereon, the arms 34, whose free ends are secured to the gate 36. The outside of this gate should be made convex in its cross-section upon a curve whose radius is the distance from the outside of the gate to the horizontal bar 33, and the gate-aperture 71, made in front of the gate and through the front wall 32 of the flume, should have its ends curved vertically, as at 68, so that the ends of the gate 36 should approximately fit the aperture when the gate is shut.

The tank 11 for the lifting-float 13, when applied to a swinging gate of this construction and used in the position shown in the drawings, is made beneath the floor of the flume, and the lifting-rod 10 in this case extends up through this floor, and may be connected with a cross-bar extending from one arm, 34, to the other, of the gate 36, as shown in Figs. IV. and V.

The chamber 75 for the wheels 28 may be covered by a horizontal partition, 70, if desired, with a small horizontal aperture, as 69, through the front wall 32 of the flume, which would form a draft-tube in which the wheels were located, the water in the flume flowing through this aperture 69 and covering the horizontal partition 70, to pack the apertures to the wheel-

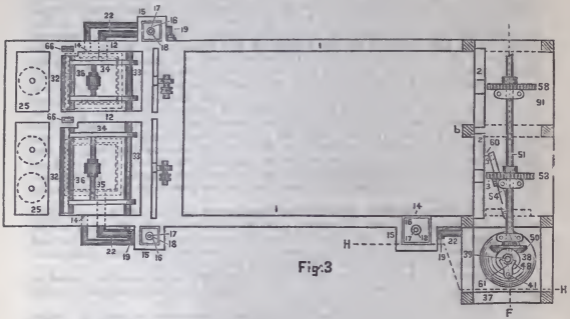


Fig. 3

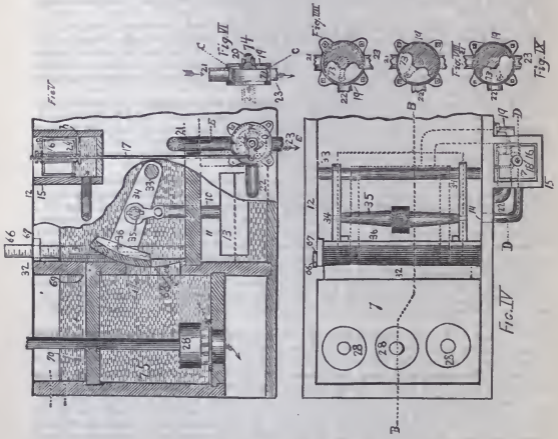


Fig. IV

Fig. VII

Fig. VIII

Fig. IX

chamber, these wheels representing those used by the establishment located at that point and drawing water from the canal.

A scale, 66, may extend up vertically in any convenient place, with its lower end pivoted to the end of the gate 36, and the graduations on the scale may indicate the vertical opening and fractions thereof of the gate-aperture. Suppose, for example, that the gate-aperture should be ten feet horizontally and two feet vertically, and a glance at the scale should indicate that the lower edge of the gate 36 was just one foot above the lower edge of the gate-aperture. It would require but a few minutes' computation, knowing the area of open aperture and velocity, to ascertain just how much water was flowing through the aperture beneath the gate, so that the quantity of water being used by the party drawing from that flume may be easily and accurately measured at any time by a glance at the scale to see how much it projects above the top of the wall of the flume, or any other horizontal line across the scale as an indicator.

The operation of the float 16 within its tank 15, connected with the flume shown in Figs. III., IV., and V., and also the valve-case 19, connected with said float and with the tank 11 of the lifting-float 13, is precisely like that hereinbefore described as used in Figs. I. and II., except that its action is reversed—that is to say, the tank is so connected with the flume in Figs. IV. and V. that the water may flow freely through the orifice 14 and the pipe leading therefrom into the tank 15, so that the float 16, being properly adjusted by the nut 18 on the rod 17 above the float, will be held at a certain height in the tank 15 by the water therein, the valve in the case 19 being held in a position to retain the proper quantity of water in the tank 11 to sustain the float 13 and gate 36 at such a height as to allow the quantity of water to flow through the gate-aperture 71 at the fixed velocity to which the party is entitled, at the given head which is maintained in the canal by the head-gates, as hereinbefore described. If the party wishes to use more water than that which would flow through the gate-opening 71 at a given velocity—say two feet per second—the water would begin to fall in that part of the flume in which the gate 36 is pivoted, and also would fall in the tank 15, owing to the increased velocity of the water passing through the gate-aperture 71, and the float 16 would fall and change the valve, so that the inlet from the pipe 21 would be opened and the outlet at 23 be closed, permitting the water to flow into the tank 11, raising the lifting-float 13 and opening the gate 36 to give a larger aperture and permit more water to pass through the gate aperture 71 until the velocity was reduced to the stated two feet per second, and this increased opening of the gate-aperture would be accurately indicated by the scale, and the amount of water could then easily be computed. If the water in the reservoir should be exceedingly low, so that the water in the canal should remain at a much lower level than at the line L, the nuts on the rods 17 above the floats 16 are readjusted according to the height of water in the canal, and each party will then be able to draw his proportional quantity of the water, and no more, instead of his full quantity, as when the water is abundant.

It will be seen that when the float 16 is once adjusted for any certain height at which it is desired to maintain the water, by turning the nut 18 on the rod 17 either up or down, the float will operate automatically to move the valve into such a position as to regulate the amount of water retained in the lifting tank 11 to operate the gate, and keep the proportions of the supply of water in the canal equal to the demand or amount used therefrom.

It will be seen that by merely reversing the position of the arm 20 on the hub of the valve 73 the falling of the water and the float 16 will operate the valve to permit the water to flow into the lifting-tank to close a gate, or to open it, according to the position in which the said arm is secured.

It is evident that in cases where a single individual, firm, or corporation owns all the water which runs in the canal or water-way, or owns the entire water privilege, and is only using from one flume, or when it is not desired to divide the water among the different flumes through which it is drawn from the canal to be used, but only to maintain the water in the canal or water-way at a uniform height, it may be done by using the apparatus as connected with the head-gates at the bulk-head alone. In any case, whether used at the head-gates or those in the flume, or both, the tanks 15, containing the operating floats 16, together with their respective valves, and the pipes or water-connections, should all be located under cover to avoid being frozen up

in winter, and the tanks 15, with their floats 16, might be located conveniently in some office, and under the control of one man; and instead of taking the water from the canal into the tank 11 through the valve-case 19 and inlet 21, it may be taken from the reservoir or river by connecting the pipe therewith, if it should be more convenient.

JAMES EMERSON.

Witnesses :

T. A. CURTIS,  
N. E. DWINNELL.

## QUESTIONS OFTEN ASKED ME IN COURT ANSWERED.

Have I ever been to college or technical school ?

No; but the teachers and graduates of such institutions often come to me for information.

Have I studied hydraulic works by different authors ?

I have looked through such occasionally.

Have I ever run levels between mills as a surveyor does ?

No; the cause for effect can better be ascertained by doing it by the water if one knows how to do it.

Why do I answer so positively while others professing to teach the science hesitate ?

Because my answers are based upon knowledge obtained by personal experiments.

How do I know that weir and aperture measurements are correct ?

By catching the discharge from weirs and apertures in tanks, then cubing the contents.

How did I prepare my weir tables, did I work them all personally ?

No; I never learned the formula for working up such tables, but employed cheap help to work up a set of tables from the Francis formulæ, then cubed the discharge in tanks varying in capacity from two feet up to twenty-five thousand feet.

How do I know that tests of wheels by such tables are correct ?

By testing the same wheels at several different testing flumes remote from each other.

How do I know that float and current meter measurements are worthless ?

By testing the same streams or discharges by weir.

## SUGGESTION FOR CAPITALISTS.

As the hours of labor are reduced so that invested capital in mills stands idle two-thirds of the time why not employ two or three sets of hands and keep the work in operation the most of the time, thus making a plant of a million turn out the same quantity now done by one of double that cost ?



## Preliminary Proceedings for Legal Division of Water Power.

State of Iowa, }  
Linn County. } ss.

To James Emerson of Willinansett, Massachusetts, Samuel Sherwood of Independence, Iowa, and S. N. Williams of Mt. Vernon, Iowa.

**GREETING**—Whereas, on November 1st, A. D. 1889, in an action now pending in the district court of said Linn county, wherein N. E. Brown is plaintiff, and Susan Brown, W. S. Cooper, Sarah E. Leach, E. E. Leach, Herman D. St. John, and Charles Clay are defendants, it was found by the said court that the said plaintiff, N. E. Brown, is the owner in fee simple of the undivided two sixty-fourths ( $\frac{2}{64}$ ) of the following described property situated in Linn county and the state of Iowa, to wit:—

The water power created, situated on, across and adjacent to the Cedar river at Cedar Rapids, Linn county, Iowa, consisting of a mill dam constructed across the Cedar river at said Cedar Rapids with an abutment or bulk head upon and against either bank of said river, including race ways on each side of said river from said dam, the water power and flowage created by said dam and race ways, and the right to have, build, and maintain said dam, race ways, and power; said dam, abutments, and bulk heads being more particularly described as follows, to wit:—

Said dam being at and between Fractional Block Two (2) in Cedar Rapids, Iowa, and Ely & Angle's addition to West Cedar Rapids, in Linn county, Iowa, one of said bulk heads and the east end of said dam being upon lots "J," "K," "L," and "M" in Fractional Block Two (2) in Cedar Rapids, Iowa, and the other of said bulk heads and the west end of said dam being on lots twenty-three (23) and twenty-four (24) of Ely & Angle's addition to West Cedar Rapids, in Linn county, Iowa, and the street and land adjacent thereto; that the defendant, Susan Brown, is the absolute owner of the undivided fifty-five sixty-fourths ( $\frac{55}{64}$ ), and the one-third ( $\frac{1}{3}$ ) of the two sixty-fourths ( $\frac{2}{64}$ ) in all of the one hundred sixty-seven one hundred ninety seconds ( $\frac{167}{180}$ ) of said property; that the said W. S. Cooper is the owner of the undivided one-sixteenth ( $\frac{1}{16}$ ) of the said property; that the defendants, Herman D. St. John and Charles Clay, are together the owners of the undivided one sixty-fourth ( $\frac{1}{64}$ ) of said property, and that the defendants, Sarah E. Leach and E. E. Leach, are together the owners of the one forty-eighth ( $\frac{1}{48}$ ) of said property and entitled to the use of the said one forty-eighth ( $\frac{1}{48}$ ) on the west side of said Cedar river.

And it was then and there ordered, adjudged, and decreed by said district court that the said shares and title of the said parties respectively in and to said property be confirmed, and that partition thereof between said parties be made. And that said water power and property hereinbefore described be partitioned and so measured and meted out to the several owners thereof according to their several rights and interests as hereinbefore set forth so that each of said owners shall receive and use of said water power, as developed, his or their own proper share and no more, at any and all stages of the water and in whatever condition said water power and improvements may be, viz:—

To said W. S. Cooper the four sixty-fourths ( $\frac{4}{64}$ ) of said power; to said Herman D. St. John and Charles Clay together the one sixty-fourth ( $\frac{1}{64}$ ) of said power; to said Susan Brown the one hundred sixty-seven one hundred ninety seconds ( $\frac{167}{180}$ ) of said power and property; to said N. E. Brown the two sixty-fourths ( $\frac{2}{64}$ ) of said power and property, and to said Sarah E. Leach and E. E. Leach together the one forty-eighth ( $\frac{1}{48}$ ) of the whole of said power and property, the latter to be used on the west side of said river, that each of them may enjoy and use the same severally, and, each to have his or their full use thereof, uninterrupted by interference, invasion, or diminution from the other, and no more.

And whereas, on the 19th day of November, A. D. 1889, and the 13th day of February, A. D. 1890, in said action it was ordered, adjudged, and decreed



by said court that to effect said partition, such partition of said property between said parties to said action be made by James Emerson of Willimansett, Massachusetts, Samuel Sherwood of Independence, Iowa, and S. N. Williams of Mt. Vernon, Iowa, referees and commissioners for that purpose; and that to enable such commissioners and referees to make such partition, they were authorized as against any and all persons to enter upon said premises and take control of said water power, dam, and race ways for the reasonable time required to do said work, opening and closing the same at pleasure and as in their judgment may be necessary, stopping any and all water wheels and mills operated by said power and for such time or times as may be necessary and reasonable, and that in making said partition the said referees ascertain the quantity or volume of water now used at and by said power and dam, and the exact power and quantity that each party shall be entitled to draw off or use under the varying stages of the water in the aforesaid river, and said referees are further authorized by said court to make such recommendation in their report as they deem advisable for the future maintenance and use of the interests of the several parties in said action in said water power.

Now, therefore, you are hereby empowered and commanded to make partition of the water power and property above described between the plaintiff, N. E. Brown, and the defendants, Susan Brown, W. S. Cooper, Sarah E. Leach, E. E. Leach, Herman D. St. John, and Charles Clay, by assigning to N. E. Brown, the two sixty-fourths ( $\frac{2}{64}$ ) thereof, to said W. S. Cooper, the four sixty-fourths ( $\frac{4}{64}$ ) thereof, to the defendants, Herman D. St. John and Charles Clay together, the one hundred sixty-seven one hundred ninety seconds ( $\frac{167}{190}$ ) thereof, and to the defendants, Sarah E. Leach and E. E. Leach together, the one forty-eighth ( $\frac{1}{48}$ ) thereof, the said one forty-eighth ( $\frac{1}{48}$ ) to be used on the west side of said river, all in severalty according to law, that each of said parties may enjoy the use and portion thereof belonging to him, her, or them, in severalty, and have his and their full use thereof, uninterrupted by interference, invasion, or diminution from the other, and no more; such partition to be made as hereinbefore provided and directed; and you are further directed to make report in writing of such partition, and your doings under this commission and said decree, and of all expenses and costs pertaining to the same, as soon as can be done with reasonable diligence, to our said district court. You are further authorized to make such recommendations in your said report as you deem advisable for the future maintenance and use of the interests of the several parties to said action in said water power.

WITNESS my hand and the seal of the said court hereto affixed this 9th day of June, A. D. 1890.

O. S. LAMB,  
Clerk of the district court of Linn County, Iowa.

N. E. BROWN, Plaintiff,

vs.

SUSAN BROWN, W. S. COOPER,  
SARAH E. LEACH, E. E. LEACH,  
HERMAN D. ST. JOHN, and CHARLES  
CLAY, Defendants.

} Partition  
In District Court of Linn  
County, Iowa.

State of Iowa, }  
Linn County. } ss.

We, James Emerson, Samuel Sherwood, and S. N. Williams, do severally swear, that we will well and faithfully perform the duties of referees in the above entitled cause, and make a just and equitable partition therein, according to the best of our knowledge and ability.

JAMES EMERSON,  
SAMUEL SHERWOOD, } Referees.  
S. N. WILLIAMS, }

Subscribed and sworn to before me by the said James Emerson, Samuel Sherwood, and S. N. Williams, on this 28th day of June, A. D. 1890.

U. C. BLAKE,  
Notary Public in and for Linn County, Iowa.

## REPORT OF REFEREES.

STATE OF IOWA, }  
LINN COUNTY. } ss.

Report of referees in answer to decree of Linn County District Court ordering the partition of the water power at Cedar Rapids of said County; N. E. Brown, plaintiff; Susan Brown, W. S. Cooper, Sarah E. and E. E. Leach, Herman D. St. John and Charles Clay, defendants.

We, the referees, met at Cedar Rapids July 29, 1890, and qualified as required. Mr. Emerson took charge of the numerous preparations necessary for dividing the water; Professor Williams having charge of various tests for ascertaining the cost of steam power at Cedar Rapids and estimated valuation of water power at Waterloo and Cedar Falls and other matters, while Mr. Sherwood, from his general knowledge of water power, and especially for his early acquaintance with the Cedar Rapids water power, was held in reserve as adviser and assistant.

The first act necessary was to put the dam in order that the whole flow of water in the river should pass over its crest for measurement.

The top of dam was raised some ten inches at the lowest point and divided into twenty-nine twenty feet sections and two of ten feet each; division planks were established between each section and a small post rigidly secured to the dam eighteen inches up stream, from crest of weirs at middle of each. These posts were leveled at the top to correspond to the exact level of weirs: then in case the weight of overflow should cause sectional depressions one end of crest plank would be likely to be as much above the top of post as the other would be below.

The bottom edges of cresting planks were well imbedded in Portland cement, making a perfectly tight joint the whole length of dam. The planking of dam is doubled, the upper ends of top planks are scoured off by ice and overflow so that water flowing over runs down back between the two layers, presenting the appearance of extensive leakage under the dam. The cresting planks are placed up stream from the worn off upper planks, and while the surface of water was below the crest of weirs there was no show of leakage through the planking from end to end of dam; at the bottom there were three leaks, but so small that there were no whirlpools or other indications of their source above. Gravel would make the dam as tight as a dam built upon seamy rock can be made, but gravel can only be procured at a cost of two dollars per cubic yard, and at that price with difficulty. Sawdust and other debris were used until the leakage was reduced to the lowest stage possible.

The openings to the races were stopped; on the west side by a temporary dam, on the east side by planks at the openings in wall at its head, and the leakage from each race was measured by weir or aperture.

Wednesday, August 13, water flowing over the crest of dam or weirs seemed to have reached its height and a hasty measurement was made, the result showing a flow of over thirty-nine thousand cubic feet per minute in the river. The next morning Messrs. Sherwood and Williams joined with me in making the most careful measurement possible. An improvised hook gauge and gauge tank for quieting the surface of the water were used, so that the greatest exactness was obtained, the measurements on dam and in the two races aggregating 39,699.43 cubic feet per minute, to which I add one-fourth additional, making the maximum flow of 49,624.28 cubic feet per minute as the largest quantity likely to flow in the river at any season of the year, except during freshets; or that can be made useful through the head-gate openings on east side of the river.

I make this addition not because I believe there is such quantity that can be utilized under existing conditions, but because the ownership of all the parties aside from Mrs. Brown is so small that it is better to do so than to leave any excuse for further litigation.

St. John & Clay's mill has wheels that under eight feet head will discharge 11,121 cubic feet of water per minute, = 167.9 h.p. of water, of which about 112

effective h.p. may be realized. Their  $\frac{1}{4}$  of the whole power is 775.4 cubic feet of water per minute, which falling 8 feet = 11.7 h.p., or 9 h.p. net.

N. E. Brown's wheels with eight feet head will discharge 14,000 cubic feet per minute, or 210.2 h.p. of water, but they are so out of repair that no accurate estimate of net effect can be made. His  $\frac{3}{8}$  of the whole power is 1,570.8 cubic feet per minute, which falling eight feet = 23.4 h.p. of water, or 16 to 18 effective h.p.

Cooper's wheels under seven feet head can discharge about 9,800 cubic feet per minute, = 129 h.p. of water, or from 76 to 100 h.p. net. His  $\frac{1}{8}$  of 49,624.3 cubic feet = 3,101.5 cubic feet per minute, which falling seven feet = 41 h.p. of which 28 to 35 may be made effective

Each's wheels under six feet head will discharge about 7,000 cubic feet per minute, or 79.3 h.p. of water, from which 50 to 60 h.p. net should be realized. His  $\frac{1}{8}$  of 49,624.3 cubic feet = 1,033.8 cubic feet per minute, which falling six feet = 11.6 h.p., of which 8 to 10 may be made effective.

Visits have been made to Waterloo and Cedar Falls for the purpose of examining the dams at those places, and to get an estimate of the value of water power there.

At Waterloo the dam is more leaky than the one here. At Cedar Falls the dams were not filled to the crest, yet showed free leakage.

Two owners at the Falls estimated the value of the water there at ten dollars per square inch, and more if free from litigation or diminution through the year.

At Waterloo the water power there is valued at twenty-five thousand dollars, and twice that could it be changed to Cedar Rapids, on account of better facilities here.

It was stated there by several millers, that the power there had been good for the season, though it had diminished somewhat lately—some said ten per cent.; others thought perhaps a little more, but all said that twenty-five per cent. additional would make a large supply.

One thousand inches of water under eight feet head = 9,450 cubic feet per minute, or less than either of the mills are fitted for using from the east race at Cedar Rapids

The decree requires a proportional division of the water here. Such division will shut down every mill concerned, except Cooper's, and his much of the time, for the maximum and minimum flow will be divided. The flow to-day, August 21, is but about 37,000 cubic feet, and has been less since the largest measurement was found, and at many times during the year is much less, for the water is often drawn down by the wheels in use two or three feet below the crest of dam

Preparations will at once be commenced for division according to the decree. The race is ample in capacity to carry several times the amount of water due the mills taking water therefrom, but that of necessity will have to be closed while the bulkheads are being put in and kept so until the work is completed. Wing dam and head-gates will have to be erected on the west side, that the division of water may be made at the head of that race that the loss from leakage of the race may fall upon the proper person. The decree will be carried out with all possible expedition.

But it will take time to complete arrangements for doing it, and soon the water will be so cold that workmen will be unwilling to work in it, besides the closing of the mills without notice has discommoded farmers very much, so that the water is let into the east race this 25th day of August with the distinct understanding that both races will be closed again the 1st day of May next, and kept so until preparations for the proportional partition of the water are completed, then each owner will receive the exact quantity due and no more, until settlement is made for the excess drawn from August 25, current month, to May 1, 1891. At least such will be the course recommended by the referees, for the value of such excess is shown by the tests of steam power herewith annexed.

The water power here is more valuable than the one at Waterloo or Cedar Falls, for the dam sets the water back six miles or more, furnishing a larger reservoir and steadier power if properly used, but for one-eighth of the ownership to draw all the water without paying any rent, leaves the one owning seven-eighths little encouragement for keeping dam and races in order. Properly used the power ought to be of great benefit to the city.

JAMES EMERSON.

Having had charge of the steam tests, an abstract of the more important is given herewith. I have carefully examined Mr. Emerson's statements of work done, with results, and find them correct. A complete report of details of statements, also testimony taken in connection with the water powers at Cedar Falls and Waterloo, has been prepared and can be furnished if desired.

S. N. WILLIAMS.

Tests have been made with a Westinghouse compound, a Buckeye, and a common slide valve engine, for the purpose of ascertaining the cost of steam power here. These were made by keying a No. 4 power scale to the main line of driving shaft, taking the key from the driving pulley, allowing its arms to rest upon projecting parts of the scale, thus weighing the power in transmission, the scale at each revolution carrying the load nine feet. The number of revolutions per minute, multiplied by nine, that product multiplied by the weight, giving the foot pounds.

**TEST OF ST. JOHN & CLAY'S MILL, AUGUST 21. WOODBURY DOUBLE SLIDE VALVE ENGINE, CYLINDER 13½ X 18.**

Speed of shaft and scale 189 revolutions per minute.

|  |            |
|--|------------|
| Power to run shafting and machinery, - - - -         | 20.85 h.p. |
| Maximum power developed during test, - - - -         | 46.18 h.p. |
| Pounds of nut coal per horse power per hour. - - - - | 11.3       |

11.3 pounds of coal multiplied by 24 = 12,570 pounds, at \$2.25 per ton = in round numbers \$14.09 for the 46.18 h.p. developed. Two engineers without fireman at \$2.50 per day each = \$5.00; added to the \$14.00 = \$19.00 per day for running such a mill with steam power. An engineer who fires and runs an engine twelve hours per day, and whose ability is such that his services are worth less than the price named, is a standing menace to the neighborhood.

The tests below were made at the electric light works and were made under more favorable conditions than generally prevail in manufacturing establishments.

**WESTINGHOUSE COMPOUND ENGINE, 10 X 18 X 10, HEINE BOILER WITH STOKER. RATED 65 H.P. AT 100 POUNDS STEAM. TEST NO. 1, AUG. 9.**

Slack coal; pump run by separate boiler.

|  |       |
|--|-------|
| Pounds of coal per horse power by power scale, - - - - | 11.17 |
| Average net weight as shown by power scale, - - - -    | 385.  |
| Average ampere load, - - - -                           | 19.70 |
| Average steam pressure, - - - -                        | 101.6 |
| Average speed, - - - -                                 | 314.8 |
| Average horse power, - - - -                           | 33.10 |

**WESTINGHOUSE ENGINE, HEINE BOILER, RONEY STOKER. TEST NO. 3, AUG. 11.**

|   |        |
|---|--------|
| Average steam pressure, - - - -                               | 114.6  |
| Average speed of shaft and scale, - - - -                     | 312.68 |
| Average net weight, - - - -                                   | 551.35 |
| Average horse power, - - - -                                  | 46.16  |
| Pounds coal per horse power, slack at \$1.25 per ton, - - - - | 8.24   |
| Maximum horse power steam at 112, - - - -                     | 56.71  |
| Maximum ampere load, - - - -                                  | 33.5   |

The maximum load on Westinghouse Engine shows 10.5 16 candle-power lamps to the horse power. This is not by actual count, but is estimated from ampere load after deducting liberal amount for loss in wire and converters.

BUCKEYE ENGINE, HEINE BOILER WITH STOKER, RATED 75 H.P. AT 80  
POUNDS STEAM. TEST NO. 5. AUGUST 17.

|   |        |
|---|--------|
| - Cylinder 12 by 24, slack coal, pump run by same boiler. |        |
| Pounds coal per horse power,                              | 9.64   |
| Average net weight,                                       | 647.30 |
| Average ampere load,                                      | 26.40  |
| Average steam pressure,                                   | 108.4  |
| Average speed,  | 434.   |
| Average horse power,                                      | 74.57  |

BUCKEYE ENGINE, BABCOCK, WILCOX & ERIE BOILERS. TEST NO. 4.  
AUGUST 15.

|   |       |
|---|-------|
| Average steam pressure,                         | 97.6  |
| Average speed of shaft and scale,               | 433.9 |
| Average weight, pounds,                         | 667.  |
| Average horse power,                            | 78.9  |
| Coal, pounds per horse power, air-slacked lump, | 7.88  |
| Maximum h.p. steam at 96,                       | 92.2  |
| Maximum ampere load,                            | 35.   |
| Maximum number of arc lamps,                    | 42.   |

I was here over forty years since, about mid winter; the water was lower then than it was the 14th of August, the day the measurement was taken. At that time Mr. Greene had leased his lumber mill to William Harmon from Maine, and in a few days after starting it parties running the mill now owned by Messrs. St. John & Clay said Mr. Harmon was drawing the water so much that it interfered very much with their mill. Mr. Harmon said the same, or that their mill drew the water from his mill. I do not know that there was any other water used at that time. Having been present August 14, the day the measurements were made here at Cedar Rapids, I can unhesitatingly state that they were correct, as they were made in the same way as the measurements were made at Lowell and Holyoke, Mass., in their testing flumes. I have proven these correct beyond a doubt by actual experiment in my own testing flume at Independence, Iowa, which I have had over ten years. I have been present many times at the water-wheel test at Holyoke, conducted by Mr. James Emerson. I have also been familiar with the Cedar River since 1847; have been employed at Cedar Falls; also at this place for forty years since at millwright work. I have seen the river at different stages, and at the time the measurement was made here, to the best of my knowledge, state that Mr Emerson has made a fair and honest report of the quantity of water, also of the power at the time of the measurement, which I am satisfied are as near correct as can be made.

S. SHERWOOD, SR.

Mrs. Susan Brown, defendant and principal owner, is hereby directed to see that all practicable preparations are made for carrying out the decree as soon after the closing of the mills, May 1, 1891, as is possible.

CEDAR RAPIDS, IOWA, August 28, 1890.

JAMES EMERSON,  
S. N. WILLIAMS,  
S. SHERWOOD, JR.

For more than twenty years parties owning less than one-eighth of this power have used the whole without paying rent, at the same time keeping up a continuous complaint that the principal owner would not keep the dam races, etc., in repair.

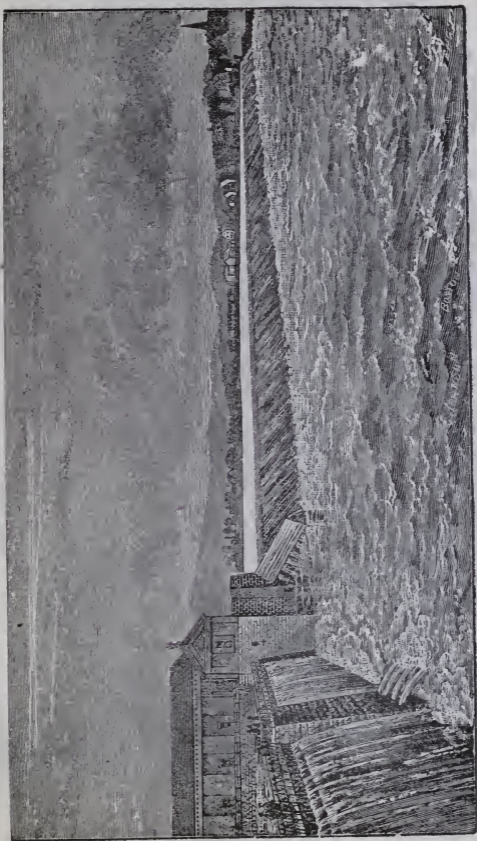
The commission was appointed to make a permanent automatic division of the water, according to ownership. To do this, permanent head gates at each race were required which the Browns declined to furnish, consequently the decree of the court could not be carried out.

January 1, 1892.

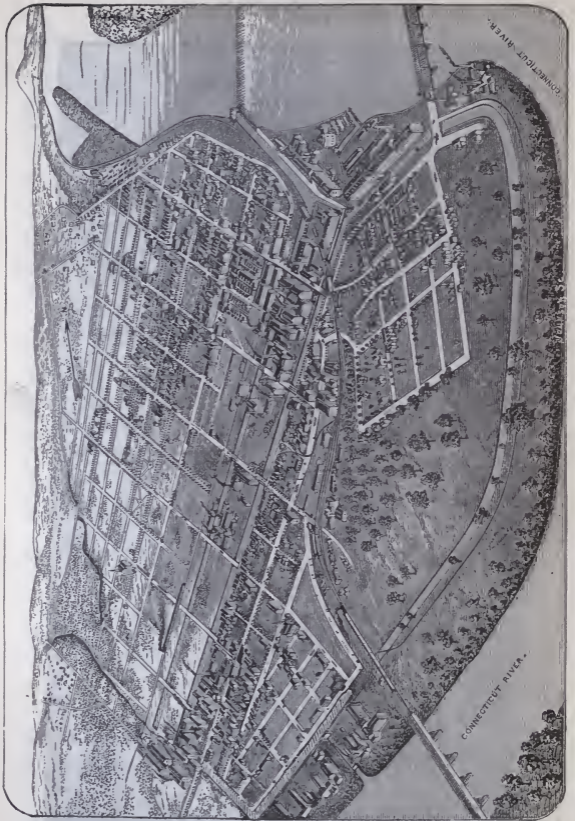
JAMES EMERSON.



HOLYOKE DAM.







## Holyoke and Its Water Power.

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Some eighty miles from the mouth of the beautiful Connecticut, almost in the shadow of Mounts Tom and Holyoke, there is a fall of nearly sixty feet in a short distance that once formed what was called the "Great Rapids," near which, from time immemorial, the aborigines of the country gathered in great numbers in quest of fish and game; and until within a few years "Indian fireplaces" have dotted the banks that are now covered with mills; indeed, Indian skeletons, implements and arrow heads are often found in the vicinity at this time. Near the foot of the falls the river makes a sharp turn to the right, and in this curve is situated the city of Holyoke. In 1831 this place was a part of West Springfield, known as "Ireland Depot," with but few inhabitants, and those of but little account. In that year the Hadley Falls Co. was formed, and a small cotton mill of 4000 spindles, (known until recently as Hampden, Jr.) was erected, receiving its power through a canal, and wing dam running obliquely up the river, which at this point is wide, with rock bottom. A power so immense and convenient to the business centers of the country was not likely to escape the notice of capitalists. The volume of water flowing in the river in ordinary seasons, was found to be about 6000 cubic feet per second, or for the fall about 30,000 h. p.; but allowing one-third diminution for the driest seasons the available minimum was rated at 20,000 h. p. In 1845, it was decided to construct a dam across the river, and one with a base of 60 and a height of 30 feet was completed Nov. 19, 1847, but before filling to the top it rolled over and went down stream; this was a severe loss, but the experience was valuable. The dam now standing was completed Oct. 22, 1849; it had a base of 80 and a height of 30 feet, the upstream incline having a face of 90 feet besides gravel filling at base. The dam is constructed of timber 12 inches square, crossed and bolted, the openings filled with stone. As the bed of the river is rock it was not supposed that the overflow would wear to any perceptible extent, but in 1868 it was found that cavities from

8 to 25 feet in depth had been cut close up to the dam, and in the years 1868, '69 and '70 the Holyoke Water Power Co. made expenditures amounting to \$400,000—in the construction of an apron of heavy timber work filled with stone—to fill the space caused by the action of the water. This apron is united to the dam in the strongest manner possible, is 50 feet in width and 52 in height, its base resting 22 feet below that of the dam. Starting from the crest, which is plated with iron, the apron slopes down stream nearly to the water below. The whole structure is 130 feet wide, 30 feet high from bed of river and 1019 feet in length between abutments. There are three levels of canals, with a total fall of 56 feet. The main artery of the system, starting with a width of 140, and a water depth of 22 feet, extends eastward past the great waste weir about a thousand feet and then sweeps southward in a right line for a distance of more than a mile. The second level canal extends northerly for a mile and more, parallel with the first, and 400 feet easterly from it, and thence easterly and southerly for a mile and a quarter more, at a distance of about 400 feet from the river, this marginal portion of the second level affording mill-sites along its whole length, from which the water used passes directly into the river. The third level canal, 100 feet wide and 10 feet deep, is also a marginal canal, with mill-sites along its entire length, and extends 3,550 to the other terminus of the same canal, thus making with the latter, a line of marginal canals, around and near the whole water front of the city.

“Like other commodities which are bought and sold, water-power here has its own unit of measurement, called a mill-power, which is thus defined in the deeds of the Holyoke Water Power Company:—

“Each mill-power at the respective falls is declared to be the right, during sixteen hours in a day, to draw from the nearest canal or water course of the grantors, and through the land to be granted, 38 cubic feet of water per second at the upper fall, when the head there is 20 feet, or a quantity inversely proportionate to the height at the other falls.’ ”

Thirty-eight cubic feet per second under 20 feet head is 86.20 horse-power, 67 per cent. of which is 57.75 horse-power that may be realized. The annual rental per mill-power is 260 ounces of silver of the standard fineness of the coinage of 1859, which is in practice paid in current funds, and amounts to about \$300 a year, for 16 hours per day, or \$450 for 24 hours per day. The regular supply is now exhausted and only surplus is now leased.

The claims in the foregoing were copied from printed statements at a time when the local idea prevailed that the Holyoke water power was nearly inexhaustible. Interested parties have criticised them, and blamed me for their publication. My desire is to make this work useful to the real engineer of the future, and to all interested in such matters. The Connecticut river, like a small brook, rises and falls rapidly; its extremes of supply are great; the maximum of 6000 cubic feet per second is moderate, as it is often more than six times that. During the eight years in which I have had occasion to notice its flow, the sheet over the dam for a large portion of each year has varied from one to ten feet in depth—often five or six. In two or three of the eight years, the overflow has continued through the entire year; in each of the others, for a brief period in summer, the dam has been dry. The minimum I should estimate at from 2000 to 2500 cubic feet per second; at any rate, the whole of the river passed into the main canal through the twelve head gates, each 8 x 15 feet. The past summer was exceptional—phenomenal, in fact. The water in the river was lower than ever before known; the supply was insufficient for the power required; consequently, the head was continually falling while the mills were running. The dam, when filled, sets the water back several miles; the banks are irregular, so there was no way to measure the supply except to keep the head gates shut a sufficient length of time to make it certain the natural supply was flowing over the dam. This was not done, and no measurement worth the name was made. I was up and down the river many times during the lowest stage of water. In many places the river was easily fordable. There was one place, in particular, some three miles above the dam, that attracted my attention most. The deepest part could not have exceeded three feet, while much of the width was less than a foot in depth. It was deeper above, so that the velocity over the bar was moderate. A cross section of two by two hundred feet, with a velocity of three, or twelve hundred cubic feet per second, I think, would cover the flow; but suppose it to have been fifteen hundred, that quantity, falling fifty-six feet, would evolve 9520 h. p., or, accumulated and used in ten of the twenty-four hours, would produce 22,848 h. p. There were a few days in which the supply was insufficient to run the whole of the mills, even that length of time, I think.

That the water power at Holyoke may at all times equal 30,000 h. p. is merely a question of reservoirs to retain some of the abundant surplus ten months of each year, to be used in the other two.

The haste for large immediate dividends has harnessed the noble river to a business insatiate in its demand for more; the paper manufacturer that has all the power he wants, is a phenomenon. Except the hebdomadal stop, more for repairs than prayers, the draught from the pond is unceasing. The water power sufficient to give employment to a thousand hands in the manufacture of paper would be abundant for the employment of six thousand in the manufacture of cotton goods. The effect of this upon the future of Holyoke is conceivable. The idea of an inexhaustible supply of water at Holyoke caused many of the wheel-pits to be made of less depth than that necessary for utilizing the whole head during the dry season, but the greatest loss occurs through the use of poor or ill-adapted turbines—turbines much too large for their capacity in ordinary times, that there may be no detention during backwater. But Holyoke is not exceptional in this, for at least one-third of all the water power of the country that is used is so wasted; and of the three great powers of this state—Holyoke, Lowell and Lawrence—it is safe to estimate the waste at a greater quantity than would be necessary at either of the falls to produce a greater power than that realized from the whole fall of the Merrimac river at either Lowell or Lawrence.

The rates of the principal Water Power companies of the country are here given for the convenience of those interested in such matters. It will be seen that a "Mill-Power" is a very indefinite matter, and it may be well here to give its origin, which is as follows: Early in the present century, there was a mill at Waltham, Mass., containing 3,584 spindles; the company owning that mill colonized Lowell, and the supposed power required at the Waltham mill, was that fixed upon as a "Mill Power" at Lowell, which is here given:

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LOWELL, MASS.

Each mill-power or privilege at the respective falls is declared to be the right to draw from the nearest canal or water course of the said proprietors so much water as, during 15 hours in every day of 24 hours, shall give a power equal to 25 cubic feet per second at the great fall, when the fall there is 30 feet, or enough to give the same power at any of the other falls. The whole owned by the Companies, none to let or sell.

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OFFICE OF ESSEX COMPANY, LAWRENCE, MASS., June 16, 1877.

JAMES EMERSON: DEAR SIR:—Your letter of this date is at hand. A "Mill Power" at Lawrence is defined to be the "right to draw so much water as shall give a power equal to 30 cubic feet of water per second, when the head is 25 feet," for not more than 16 hours in each day of 24 hours. For this the charge is an annual rent of \$1200, and this is at the same rate for small as well as large water takers. This is 85 gross h. p. for \$1200=\$14.12 per h. p. of water. It might be a fair general statement to say a horse power by steam would cost 50 or \$60 a year more than a horse power by water; but this would be modified by circumstances.

Yours truly,

HIRAM F. MILLS, Engineer.

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U. S. BUNTING COMPANY, LOWELL, MASS., Aug. 1, 1877.

MR. JAMES EMERSON: DEAR SIR:—Replying to your favor of June 16th last to D. W. C. Farrington, I have to say with regard to the subject upon which you made inquiries of him, that it is the custom of the Wamesit Power Company of Lowell to let floor room to their tenants at a stipulated sum, depending upon location, &c., &c; and then the power is hired at \$75 per year, per horse power extra. When any question is raised on either side as to the power actually used, we apply a Dynamometer of your make, and measure it as near as possible.

WALTER H. MCDANIELS, Supt.

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OFFICE OF AMERICAN PRINT WORKS,  
FALL RIVER, MASS., June 18, 1877.

JAMES EMERSON: DEAR SIR:—Your favor of the 16th inst. is at hand. In reply would say, that the water-power in Fall River is not let, but the stock in the Watuppa Reservoir Co., which controls the water-power, is held by the several Corporations using the power in proportion to the height of their respective falls, and no charge is made for use; but the expense of maintaining the Reservoir Company is borne by assessments upon the several Corporations, from time to time, pro rata, according to height of fall of each. There is but a single outlet from the Reservoir. The total fall from Reservoir to tide water is 128 feet; and the mills are located one below another, so that they each get precisely the same quantity of water, as each mill takes just what the one above it delivers. The quantity is about 122 cubic feet per second. I am just now unable to give an answer that would be satisfactory to myself as to the comparative cost of water and steam-power.

Yours truly,

THOS. J. BORDEN, Treas.,

Watuppa Reservoir Co.



OFFICE MINNEAPOLIS MILL Co.,  
MINNEAPOLIS, MINN., July 5, 1877.

JAMES EMERSON: DEAR SIR:—With reference to renting power, I would say that rentals are made at so much for Mill Power, which is designated as 30 cubic feet of water per second, with head of 22 feet. Present price for Mill Power \$1000 per year, but from this back to earlier dates rates decrease considerably.

Yours truly,

H. H. DOUGLASS, Eng. and Agt. M. M. Co.

BELLOWS FALLS, VT., June 28, 1877.

JAMES EMERSON: DEAR SIR:—Yours of the 22d is just received; a Mill Power, in our lease, is the right to draw equal to 30 cubic feet per second, under 25 feet head. Price for a Mill Power is 387 ounces Troy Weight of silver, of the present standard business of the silver coin of the United States, as an equivalent in gold, which is 450 dollars.

Yours truly,

ROBERTSON, MOORE & Co.

MANCHESTER, N. H., June 29, 1877.

JAMES EMERSON: DEAR SIR:—The rule for a Mill Power here is as follows: Divide 725 by the number of feet fall minus 1, and the quotient will be the number of cubic feet per second for a Mill Power on that fall. For instance: The fall at the upper level is 20 feet; then 725 divided by 19=38.1, which is number of cubic feet per second for that fall. The Mill Powers are let to manufacturing concerns at an annual rent of \$300 each. This includes the land necessary to use the power on, together with some room for tenement blocks, but no buildings or machinery.

Yours truly,

JOSEPH B. SAWYER, C. E.

THE OSWEGO CANAL COMPANY, OSWEGO, N. Y.

The Lessees at their joint option may be allowed for each run of classified water, either; 1st.—One thousand cubic feet per minute; or 2d.—So much as will be drawn through a central discharge water-wheel of the kind now used on the Canal, with a spout, the cross section of which shall be  $133\frac{1}{2}$  square inches at the smallest point, provided the outlet does not exceed in diameter one-half the diameter of the wheel, nor in clear opening a surface,  $3\frac{1}{2}$  times the section of the spout; or 3d.—So much as will be drawn through a Reynolds wheel with a spout, the cross section of which measures  $166\frac{2}{3}$  square inches at the smallest point, provided the total outlet does not exceed the section of the spout more than 50 per cent., and the superficial center of the outlet is not over  $\frac{2}{3}$  the radius of the wheel from the center thereof. The second and third alternatives are estimated to give the same quantity of water, and equal to about 1175 cubic feet per minute, when the clear head on the wheel is 16 feet.

DAYTON, OHIO, July 12, 1877.

JAMES EMERSON: DEAR SIR:—Water-power is supplied to the mills on the three levels or falls through *metallic gauges*; calculated and adapted to pass under a certain head so many cubic feet per minute. For example, in the Dayton Hydraulic Company we give a head of 15 inches above the center of the gauge, and with that head give  $233\frac{1}{2}$  cubic feet per minute for *one power*. The Company below us, under I believe the same head, over a  $10\frac{1}{2}$  feet overshot, give 300 cubic feet per minute for one power. The price per power (or "run of stone," as it was originally called,) is, I believe, uniformly here \$200 per year. You wish, also the relative cost between steam and water-power. Water-power at \$200 per year for one run of  $5\frac{1}{4}$  horse-power, would cost eleven sixty-eight one hundredths dollars per day for 100 horse power. Steam, with the latest improved steam-engine, as tested by experts, will give one horse power with 3 lbs. coal per hour; coal at \$3 per ton would be ten eighty one hundredths dollars for 100 horse power per day of 24 hours. An engine of this kind, with boilers, would cost about \$5000. Water-wheel, with the same power, "under an ordinary fall 12 or 13 feet," with penstock and flume would cost about \$2000. The foundation for steam-engine would cost about the same as it would to dig a wheel pit. With



an ordinary slide valve engine, such as we use, costs about \$27 per day "24 hours" for 100 horse power. If I can give you further information, will cheerfully do so.

Very respectfully,

JOHN G. LOWE, Sec'y & Sup't D. H. Co.

OUSATON'S WATER COMPANY,  
BIRMINGHAM, CONN., July 16, 1877.

JAMES EMERSON: DEAR SIR:—Yours of the 14th is at hand. Our terms for the rent of water, per year, are \$250 per square foot, 12 hours per day,—one square foot being a discharge of five cubic feet per second. We use the weir measurement adopting J. B. Francis' formula for the computations. What we designate as a square foot of water under our head is equivalent to 12.5 horse-power, in short \$20 per horse-power per year is about the cost of water here. With reference to lot and building, the Company offer inducements in proportion to the desirability of the business to be located.

Respectfully yours,

D. S. BRINSMADE, Secretary.

WINDSOR LOCKS, CONN.

Usual head 24 to 28 feet. Water rented so much per inch, yearly, price varying with date of lease; extra water now charged at the rate of from two to two and a half dollars per inch; quantity determined by apertures through iron plate; apertures, parallelograms with parallel interior edges, center of aperture to be  $2\frac{1}{2}$  feet below the surface.

UNIONVILLE, CONN.

Water rented as follows: The one hiring to be entitled to such quantity as can be drawn through an opening one foot square, the center of the opening to be under two feet head; I think the power is now owned by the several companies, and that there is none to rent.

COHOES, N. Y., July 14, 1877.

JAMES EMERSON: DEAR SIR:—Your favor of 10th inst. to hand. I understand the charges of the Cohoes Company to be \$200.00 per Mill Power per year, or \$20.00 per horse power which includes use of water and rent of land. The leases define the term "Mill Power," as "a Water-Power equivalent to the power given by the discharge and use of six cubic feet of water in each second, when the fall is 20 feet."

Yours truly,

WM. T. HORROBIN.

OFFICE OF THE DUNDEE WATER-POWER & LAND CO.,  
87 Leonard Street, NEW YORK, July 12, 1877.

JAMES EMERSON: DEAR SIR:—Your letter of 10th inst., received. The Company leases its Mill Sites with one or more "Mill Powers," charging \$700 per year for each Mill Power. This price includes the rental of Mill Site. By one Mill Power is conveyed the right to draw from the nearest race-way or canal  $8\frac{1}{2}$  cubic feet of water per second, fall of 22 feet.

Respectfully, &c.,

M. WALKER, Secretary.

TURNER'S FALLS, MASS.

Rent per year for each h. p. of water used \$7.50 or about \$10 for each h. p. that may be utilized by the use of good water wheels.

## DISPUTE ABOUT THE QUANTITY OF WATER USED.

In a case at Jordan, N. Y., there was a dispute about the discharge of a wheel. The lease granted the right to use what water could be drawn through an opening 10x17 inches into a scroll wheel. The discharge of the wheel was measured over a weir; the builder objected on the excuse that he knew nothing about such matters; to get over that difficulty a mark was made to indicate the depth from the discharge of the wheel; then its gate was closed and an opening 10x17 inches cut in the bottom of the penstock near the wheel; the water was then let in and the discharge through the opening compared, and was found to be considerably less than that of wheel. Of course there was no chance to dispute that point.

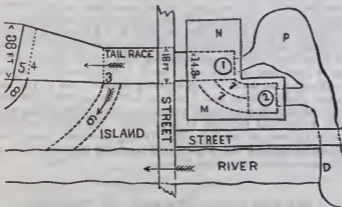
## DISPUTE ABOUT WORK DONE.

In a recent case at North Sunderland, Mass., that had been in dispute four years, and quite a sum had been expended in litigation, my services were required in court, where the *expert* testimony was so scientific that it was beyond my comprehension. A proposal was made and adopted, that the court adjourn to meet at the mill, where the case could be settled so that all could understand. The case was as follows: A turbine had been put into the mill, under the agreement that with 15 inches of water, under 62 feet head, it should grind 35 bushels of corn per hour. Arriving at the mill, a weir was constructed below the wheel, the gate was then raised until 15 inches or 394.6 cubic feet of water per minute flowed over the weir; with that quantity the wheel ground 61 and a fraction bushels per hour. The suit ended there, and the owner seemed pleased that he owned a more valuable power than he had thought. Other tests were made, from which it appeared that 2.07 bushels were ground per each horse-power utilized. The turbine was five feet in diameter, and kept down to 145 revolutions per minute.

## DISPUTE AS TO WHICH USED THE MOST WATER.

To settle a case at Auburn, N. Y., where a fine power is owned by L. W. Nye and the Auburn Mfg Co., weirs were put in above their mills, the wheel gates opened in full, then a thousand cubic feet per minute was allowed to flow into each tail race through flume and wheel; permanent marks were made on iron scales, firmly secured to the wall of each tail race, then marks were added for 1500, 2000, 2500, 3000, 3500, 4000, 4500, 5000, and finally 5236, as the maximum the Manufacturing Company's wheel could discharge. The discharge of Mr. Nye's wheel had stopped at 3908 cubic feet per minute. The scales in the tail races remain and denote at any time the quantity of water used by each party. The weirs above the mills were removed as soon as the scales were marked. In well constructed tail races the quantity used may be very accurately denoted, though, of course, the plan will not answer where the water from different mills is discharged into the same pit, or where there is backwater.

## Backwater Suits.



There are mill-owners in all parts of the country, who believe themselves injured by backwater from dams below; to such, the case of L. L. Brown & Co. vs. H. N. Dean & Son of South Adams, Mass., will be of interest. Where Brown's paper mill, M. M., now stands, was started 60 years since a saw and grist mill;

as may be seen in sketch; this is near the head of one of the branches of the river which forms the island. Deau's tannery was afterwards located on the race 6; the dotted line 3 represents the dam therefor; the crest of this dam was about level with the bottom of the saw mill wheel pit; flush boards were used to raise the dam still higher, as the bed of the stream above was then so high as to prevent flowage back into saw-mill pit as claimed by Mr. Dean. There seems to have been a dispute about the right to use the flush boards, though it was conceded that they were almost constantly in use, though at times removed when power was not required at the tannery. Afterwards Mr. Dean purchased an old fulling mill privilege, and moved his tannery further down stream; erecting a new dam which is marked 5, the water being conveyed to tannery through the race 8. The dotted line 4 represents the fulling mill dam but little of which remains, though there is sufficient to show that it was at least  $5\frac{1}{2}$  inches higher than the new dam, the crest of which is six or seven inches higher than the floor of wheel pit in what is now Brown's paper mill; the stream over the new dam is  $38\frac{1}{2}$  feet in width; at the old tannery dam it is considerably narrower. The crest of the old dam is removed, still the foundation is but a little lower than the crest of the new dam. Two 48-inch Swain turbines, 1 and 2, have been placed in Brown's mill to drive the machinery; these take the water from the pond p, through the sluices shown; the discharge from the upper one passes down through arched races 7, 7, and is discharged below the lower turbine into the main race, which is here but a little, if any, over 14 feet in width; this race has rough stone side walls. These wheels unitedly discharge from 125 to 133 cubic feet of water per second; and the depth in race is 25 inches where the width is 14 feet;  $23\frac{1}{2}$  inches where the width is 18 feet, and still less as the width increases; as it flows over the new dam it is but nine inches in depth; the velocity is much greater below the old tannery dam than above. Mr. Brown claims that the new dam backs the water on to his wheels; to prove this, witnesses testify that until the new dam was constructed there never was any water in his wheel pit when his gates were closed, but now there always is. It was proved by Brown's witness that in race 6 Dean had  $5\frac{1}{2}$  to 6 ft. head, and he now has but 5, while he discharges into the river much lower down. Mr. Brown denies that the race has ever been lowered, but the bottom is now composed of small pebbles and gravel, while for miles, above or below the mill, the bed of the river is literally paved with stones rounded by attrition, varying in size from two inches to as many feet. With a discharge from good wheels of 133 cubic feet per second, the depth over a 14 foot weir would be 25 inches, so that it is plain that Dean's dam is not the cause of the depth in the tail race of Brown's mill. That there was no water in the saw mill pit while Dean's mill was at race 6 is readily accounted for from the fact that that race drained the saw mill pit while it was open, but that race was filled up when the new dam was constructed. The water in the pit since, when wheel gates are shut, is simply *standing*, not backwater. Though denying that the race had been lowered it was not denied by Mr. Brown that the boulders had been cleared out of the race, and of course it would have been useless to remove these boulders unless they had obstructed the discharge from the mill above. From the character and tone of Brown's witnesses it was evident that they were sincere in their statements; but nature furnishes better evidence that the tail race had been lowered, also, that if Dean had a right of  $5\frac{1}{2}$  to 6 feet head at race 6 he could not possibly encroach upon the privilege above, with a 5 foot dam at race 8. I was not called into the case until the day before the trial commenced, and had no knowledge of the place before, so that I was unable to account for the water standing in Brown's pit after Dean's new dam was constructed, until it happened to be mentioned that the race 6 was filled up as soon as the tannery was moved to the new dam; then the cause became plain, but it was too late to explain, and the fact is only mentioned that lawyers engaged in such cases may understand that *STANDING* water in a wheel pit is beneficial instead of injurious. As the wheels in Brown's mill discharge double the water used by Mr. Dean, it would have been much less expensive to have furnished Mr. Dean with a larger wheel so that he could have obtained more power even with less head.

### Vexatious Waste of Water.

One of the most vexatious grievances suffered by manufacturers arises through the following circumstances. Suppose a dozen mills to be located within a short distance upon the same fall, one above the other; eleven of them have wheels

with which the natural flow of the stream is amply sufficient to keep their machinery in constant motion; but the upper mill of the dozen has wheels of the poorest kind, so that they require double the water necessary to do the work of mill, and the owner, through mulish perverseness, continues their use, each day exhausting his pond by noon, then as half of the water has flowed over the dams below, all of the mills have to stand idle the rest of the day. Of the equity in such a case there can be but one opinion; no engineering skill can aid, and only the strong arm of the law can remedy the matter. Such cases are very common.

### **“Efficiency, Useful Effect, or Percentage.”**

Are terms used to denote the economy of a wheel in its use of water, or the number of gallons it will pump back into the pond for each one hundred gallons drawn therefrom to drive the wheel. There are wheels that for each hundred gallons used will return but twenty-five, others will return fifty, while medium wheels return seventy-five, a better class eighty to eighty-five; the very highest, under favorable circumstances will return something over ninety per cent., and of course, other merits being equal, are by far the most desirable.

### **What is the Real Working Head?**

The term “Head” as used in connection with water-power means the difference in height from the surface of water in wheel pit to the surface in the penstock above, when the wheel is running.

### **What is a Square Inch of Water?**

A square inch of water means a stream exactly an inch square, its length depending upon the head from which it issues; for a head of four feet, it means a stream an inch square, 16.04 feet in length, per second; for a head of a hundred feet, a stream an inch square, 80.35 feet in length, per second. To turn this into cubic feet, multiply by 12, then divide by 1728.

### **Pressure of Water on Dams and Boilers.**

The pressure depends upon the length of dam and depth of water. It makes no difference whether the pond extends back a rod or a mile. So of steam boilers—the large boiler requires thicker iron, simply because there are more square inches of surface.

### **What Power is Required to Drive a Run of Stones.**

A more difficult question to answer, because the quantity ground in a given time has much to do with it; experienced millers west do not use more than fifteen horse-power per run, including receiving grain, flouring and delivery in barrels. White & Beynon, Lanesboro, Minn. have six run of stones; have 89 horse-power of water, about 72 horse-power actual; keep five run at work, the sixth being stopped for sharpening. White, Nash & Co. of the same place have the same power, five run of stones, four kept constantly running; use their wheel at part gate. It will be seen by examination of the Dayton, Ohio, water renting rate that  $5\frac{1}{4}$  h. p. has been considered sufficient for a run of stones, while with the 1000 cubic feet allowed at Oswego, N. Y., used on a Reynolds wheel would not realize more than 15 h. p., so that 15 h. p. for each run of stone and necessary machinery is a liberal allowance.

## Loss of Head through the Use of Small Conduit.

A belief prevails among turbine builders that where the water approaches a wheel with perceptible velocity that there is a corresponding loss of head so that the wheel can not transmit the power due the head. Such is not my belief, for there seems to be no good reason for ignoring the momentum gained by such velocity, that is within reasonable limits. The wooden mill of Beebe, Webber & Co., of Holyoke, is located below the second level. Head varies from eleven to twelve feet. Originally the use of only five sets of machinery was contemplated. The water is brought to the mill through a round wooden trunk 75 feet in length, with an inside diameter of 57 inches. The wheel pit is circular, 14 feet in diameter, and 2½ feet in depth. A five foot Tyler Scroll wheel had been used fourteen years, but was unable to transmit sufficient power to drive the eight sets of machinery now in the mill, and it was found to be necessary to obtain more power, but the small size of trunk and shallowness of pit caused wheel builders to hesitate, through fear that the loss from head would more than equal any gain that could be obtained through increase in size of wheel. I recommended the use of a 60-inch turbine, and the builders, Messrs. Fales, Jenks & Sons were induced to guarantee eighty-five horse-power under the existing conditions. The wheel was set and my brake applied. Before the gate was opened the difference between the level of the two canals was found to be 11 feet, 8 inches. For that head I calculated that 4000 pounds should balance the force of the discharge with the gate open and the wheel held stationary by the brake, and on opening the gate that weight which had been put on the beam was found to exactly balance, though the head on the wheel was less than ten feet. Under ordinary conditions the wheel used will carry at its best speed exactly half what it will balance when held stationary by the brake; but the velocity of the water seemed to change its character somewhat, for it gave its highest result, 83.66 h. p., carrying 1900 pounds at 77 revolutions per minute; its tabled speed was several revolutions less; at that speed the head as shown by a glass tube inserted in penstock directly over the wheel was found to be 10½ feet.

## Turbine Builders' Theories.

It is an old theory in turbine building that turbines should carry about half what they can lift when held stationary; with gate opened in full, the Houston wheel almost invariably do so, and there are a few others that approach that rate, while there are many that do not. Many of the Risdon wheels run with three-fourths of what they can lift. Some wheels will run with, say, nine hundred pounds, and only lift one thousand. A few days since a wheel was brought to be tested; it was set and tried first while held by brake; gate opened in full, it balanced 470 pounds, head 18.59 feet, discharging 928 cubic feet per minute. It was started with 300 pounds making 178 revolutions per minute, and discharging 1241 cubic feet of water; weight was gradually added, the speed decreasing with each addition, while the discharge increased. Discharging 1289 cubic feet, it made 124 revolutions per minute and carried 475 pounds. It was stopped by brake, then of course could not start until partially unloaded. It will be obvious to all that the more surplus lifting power a turbine has the steadier it will run under sudden changes produced by adding or throwing off machinery; the wheel was a central discharge. Builders starting with such are behind the age.

## A Proposition of Seeming Equity that has no Merit.

A common proposition, and to those unacquainted with the subject a seemingly fair one, is that two turbines shall be connected together and their merits determined by ascertaining which shall drive the other. Such a test would be perfectly worthless. The pitch of the buckets of one might be such that it would under the head tried carry 100 pounds, and make 200 revolutions per minute, while those of the other might be such that it would carry 200 pounds and



make 100 revolutions per minute, both using the same quantity of water during the trial. Of course the slow wheel would drive the fast one, but other things being equal the fast wheel would be the best.

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### Backwater.

Turbines of any make are not perceptibly effected by backwater except through loss of head. I think a slight difference was found by a commission appointed by the French government to experiment with the Fourneyron wheels. I have in two or three cases where long draft-tubes were used, thought the loss greater than should occur from the loss of head, but have had no chance to determine the matter by actual test.

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### Submerging Turbines.

Many builders insist that it is essential that a turbine should discharge under water, but it is doubtful for the same head whether it makes any difference if the wheel is properly made, though it prevents trouble from ice and generally extra head is gained by submerging lower part of wheel.

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### Draft Tubes.

If a draft-tube for any considerable proportion of the head is used, its lower end should be submerged to such depth as to render its immersion constant, otherwise when first starting up only the head above the wheel will be available until the discharge has exhausted the air from the tube, then when it does take hold, unless the gate of the wheel works very quick the speed is wild for a short time. Where there is backwater some length of time, a short draft-tube renders it convenient to get at the wheel in case it is necessary to do so, but in most cases I should prefer to have the lower part of a turbine stand in the tail water.

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### Percentage of Discharge.

The discharge of a turbine in proportion to its openings depends upon its construction. With those of a central discharge it is the least; with such wheels of fair efficiency it is likely to range between 40 and 50 per cent., with outward discharge, 60 per cent. and upwards, while with those discharging the water downwards it averages about 55 per cent. The chutes of a curb are made much larger at their outer than their inner ends, consequently, can pass much more water than the wheel will discharge, though the openings of the wheel may be somewhat the largest, so that the openings of the wheel govern the discharge. In the past, engineers have expended more time inventing impossibilities and hair splitting theories than in determining by simple tests points in dispute easy of solution. It is hardly possible that a case can ever arise in milling matters that a really intelligent engineer cannot readily solve the difficulty, and make it so simple and plain as to give no excuse for litigation, and what is more to the point, in many cases both parties can be benefited at a tithe of the expense caused by a suit at law. If there is a difference of opinion about power used, the matter may readily be determined, as may be the case if the dispute is about the quantity of water used; and the power of steam is as readily determined as that of falling water. A few plans tried by myself are here given:

#### "DISPUTE ABOUT EFFICIENCY OF TURBINE."

Thomas Harris, of Providence, R. I. expended something like \$9,800 experimenting with four Leffel wheels in a mill at Putnam, Ct., head of 28 feet. A 40-inch wheel was tried first, then a deeper wheel, same size, then a 48-inch wheel, then a second 48-inch of extra depth; the speed of looms could not be got above 125 picks per minute. I was called in to test the power and select a suitable wheel. By stopping eleven spinning frames the rest of the machinery was brought up to speed. The wheel was then tested and found to give 186 h. p. Allowing 17 h. p. for the eleven spinning frames, and 20 additional for cold mornings and backwater. I selected a wheel of 220 h. p. Since that wheel was placed in the mill, the production has been increased 1000 yards per day, 40-inch sheeting, while the discharge of water has been one-fifth less than required for the Leffel wheel. The expense of changing, my charge included, was \$1,500.



## Highest Possible Results Guaranteed.

For years past turbine builders of a certain class have unhesitatingly promised what they well knew at the time their wheels could not do. The practice has been so general that even in court it has been offered and rather accepted as an excuse, that though the wheel only accomplished one-half what was promised, the guarantee was no more extravagant than the average turbine builder would give, simply because there was no means within the reach of ordinary builders for determining such matters. The case is very different now and purchasers are less inclined to submit or juries to excuse, and builders will do well to take heed accordingly. It has been my lot within two years to be employed as expert in four different cases in which the same builder has been interested.

### "Chipping Buckets."

Has been mentioned frequently in these reports; the plan has been tried with many kinds, not always successfully; it does not have much effect on the Risdon wheel, the reversed curves of the buckets of that wheel seeming to answer the same purpose. Chipping away the edge of buckets reduces diameter of wheel above the bottom of chutes, so that its speed is usually increased thereby. (See Tyler's tests.) While increasing whole gate results it usually injures the wheel at part gate. It would seem that where the edges of the buckets extend close to end of chutes that they act like a fan or rotary pump and draw the water into the wheel. Chipping the buckets away often reduces the discharge. Increasing gate opening does not increase discharge beyond a certain limit, though it may have good effect by changing direction of water through the chutes.

### Tight Gates, or Good Part Gates.

Probably a hundred objections have been made to wheels with leaky gates where one has been made to those only reasonably efficient while working with gate opened in full, which can never be the case if a governor is necessary. The most leaky, fly-trap gate in use can not waste more than four or five per cent., while the Boyden, Houston, Collins, Hunt, Geyeline and many other wheels of the same nature waste from 25 to 50 per cent. daily, if run from one-third to three-fourths gate as wheels are often used.

### Variation of Turbines.

One of the most difficult matters in relation to turbines, is to make purchasers realize the fact that wheels made from the same patterns vary exceedingly in useful effect; yet it has been well understood for twenty years past that a turbine doing well in a mill affords no guarantee that another of the same make will give equal satisfaction in another mill; hence the uncertainty that has prevailed for years past. My report of tests will show this to be the case with wheels of all makes. But a few special cases are given here: The Tyler wheel first; a 30-inch flume wheel tested April 20, 1876.

| Remarks.                      | No. of Test.                   | Head. | W'ht. | Rev.  | H. P. | Weir. | Cubic feet. | Per Cent. |
|-------------------------------|--------------------------------|-------|-------|-------|-------|-------|-------------|-----------|
| Leakage, 70.77<br>Cubic feet, | April 20, 1876.<br>Who'e Gate. | 18.43 | 375   | 168 5 | 23.72 | 765   | 1245.64     | .6618     |

The buckets were cut back to first white line shown on diagram of wheel, (see next page), then it was tested again.

|                               |          |       |     |     |       |     |         |       |
|-------------------------------|----------|-------|-----|-----|-------|-----|---------|-------|
| Leakage, 59.32<br>Cubic feet. | April 21 | 18.65 | 375 | 202 | 34.43 | 753 | 1226.55 | .7970 |
|-------------------------------|----------|-------|-----|-----|-------|-----|---------|-------|

The buckets were then chipped back to the second line; the gate, an inside register, had six openings  $2\frac{1}{2} \times 12$  inches; these openings were increased to three

inches in width, to twelve inches in height; then the wheel was tested a third time, April 22.

|   |       |     |       |       |      |         |       |
|---|-------|-----|-------|-------|------|---------|-------|
| Whole Gate.   | 18.50 | 640 | 000   | 000   | .786 | 1302.57 | .0000 |
| Leakage, 67.83 cubic feet.  | 18.50 | 375 | 219   | 37.32 | .742 | 1190.25 | .8966 |
| Length of Weir 10 feet. Temp. of water, 45 Fah.   | 18.50 | 385 | 215.3 | 37.67 | .738 | 1180.19 | .9127 |
| Weight of water per cubic foot, 62.578.   | 18.48 | 395 | 209   | 37.52 | .745 | 1197.81 | .8966 |
| Circumference of Circle 15 ft., application of two pounds at the periphery rotated wheel. | 18.49 | 400 | 205   | 37.27 | .745 | 1197.81 | .8904 |
|   | 18.50 | 390 | 211   | 37.40 | .743 | 1192.77 | .8966 |
|   | 18.50 | 380 | 215   | 37.13 | .740 | 1185.22 | .8958 |
|   | 18.50 | 370 | 220   | 37.00 | .738 | 1180.19 | .8966 |
| Part Gate   | 18.60 | 325 | 215   | 31.76 | .680 | 1037.38 | .8709 |
| " "   | 18.62 | 300 | 209   | 28.50 | .650 | 965.60  | .8386 |
| " "   | 18.67 | 275 | 212.5 | 26.56 | .628 | 914.01  | .8234 |
| " "   | 18.76 | 220 | 213.5 | 21.35 | .562 | 764.49  | .7880 |
| " "   | 18.85 | 160 | 215   | 15.63 | .486 | 602.53  | .7280 |
| " "   | 58.93 | 105 | 213.5 | 10.18 | .417 | 465.71  | .6109 |
| " "   | 19.01 | 60  | 197   | 5.37  | .345 | 334.25  | .4471 |

The tests of the 221 were too regular to allow of doubt as to their accuracy; they were not made in haste; the wheel was stopped after the third test, result worked out and the matter considered.

The wheel was returned to shop and refinished; the edges of the buckets being smoothed up, holes were drilled in the heavy side of wheel and plugged with wood to balance it, then it was sent to Centennial, afterwards returned to me for re-test. The moment its gate was opened after it was set for test, it was evident if had been changed; it was so sensitive that it was almost impossible to control it with the brake. It could not be made to work easy, though tried in various ways. The data and results below are the best obtained:

| Head. | Weight. | Revolutions. | Horse Power. | Weir. | Discharge. | Per Cent. |
|-------|---------|--------------|--------------|-------|------------|-----------|
| 18.38 | 375     | 221          | 37.67        | .794  | 1318.42    | .8242     |

The leakage into pit from flume was 72.73 cubic feet per minute; adding ten pounds to the weight to make up for the difference required to rotate the wheel, would have increased the power to 38.67, and percentage to 84.62. After the trial the step was found to be cnted over; the wheel was taken to machine shop and changed three times after the first trial, making four trials in all, varying but slightly from the first test. The last time it was taken to the shop the lower rim was reduced by a chip 1-32 of an inch all around it, causing an increased discharge. The data and results of best tests of the trial, before and after reducing rim, are given below to show the accuracy of weir measurements compared with theoretical discharge due the increased area of opening. Results of test before the rim was turned off, then after it was reduced:

|                  | Head. | Weight. | Rev.  | Horse Power. | Discharge. | Per Cent. |
|------------------|-------|---------|-------|--------------|------------|-----------|
| Before . . . . . | 18.40 | 375     | 218   | 37.16        | 1328.45    | .8061     |
| After . . . . .  | 18.39 | 385     | 214.4 | 37.52        | 1353.80    | .8010     |

Actual increase as per weir measurement, . . . . . 25.36 cubic feet  
Theoretical discharge due the increased opening, . . . . . 25.31 cubic feet

Test of a 43-inch Risdon wheel, April 28, 1874. Same brake used as for testing the Tyler. Correction for leakage into pit 77.74 cubic feet. Weight of water per cubic foot, 62.38. Length of weir, 10 feet. Temperature of water, 40 Fah.

|             | Head. | Weight. | Rev.  | Horse Power. | Weir. | Cubic feet. | Per Cent. |
|-------------|-------|---------|-------|--------------|-------|-------------|-----------|
| Whole Gate, | 17.91 | 1200    | 151   | 82.36        | 1.256 | 2664.03     | .9132     |
| " "         | 17.93 | 1200    | 148   | 80.72        | 1.260 | 2676.91     | .8877     |
| " "         | 17.92 | 1200    | 148.3 | 80.89        | 1.261 | 2680.14     | .8910     |
| " "         | 17.90 | 1250    | 144.5 | 82.10        | 1.264 | 2689.82     | .9021     |
| " "         | 17.98 | 1150    | 146.5 | 76.58        | 1.195 | 2469.92     | .9121     |
| " "         | 18.00 | 1200    | 137.5 | 75.00        | 1.203 | 2495.13     | .8834     |
| " "         | 18.17 | 1000    | 147   | 66.82        | 1.127 | 2258.84     | .8613     |
| " "         | 18.29 | 850     | 150   | 57.95        | 1.045 | 2012.02     | .8331     |
| " "         | 18.30 | 700     | 138.6 | 41.10        | .932  | 1686.47     | .7559     |
| " "         | 18.43 | 650     | 148   | 43.72        | .932  | 1686.47     | .7439     |

The report of the foregoing test caused Otto Troost of Wiuona, Minn., to order one like it. The order was to get one as good, let the cost be what it would. Mr. Risdon built one from the same patterns and sent it to me to be tested. Eight pounds rotated the wheel. The results are given below:

|                      |       |      |       |       |       |         |       |
|----------------------|-------|------|-------|-------|-------|---------|-------|
| Whole Gate, July 8,  | 17.83 | 1200 | 142.5 | 77.73 | 1.290 | 2795.31 | .8264 |
|                      | 17.82 | 1220 | 138.5 | 76.80 | 1.291 | 2798.25 | .8159 |
|                      | 17.82 | 1240 | 136   | 76.65 | 1.290 | 2795.31 | .8153 |
| Leakage 56.57 cu.ft. | 17.80 | 1180 | 143.5 | 76.95 | 1.286 | 2782.27 | .8157 |
|                      | 17.79 | 1160 | 145.5 | 76.72 | 1.284 | 2775.77 | .8231 |
| Wgt. of water 62 285 | 17.79 | 1140 | 147.5 | 76.43 | 1.282 | 2769.27 | .8220 |
|                      | 17.84 | 1100 | 142.5 | 71.25 | 1.230 | 2601.93 | .8136 |
| Part Gate,           | 17.84 | 1125 | 139.7 | 71.50 | 1.232 | 2608.31 | .8140 |
|                      | 17.92 | 940  | 148   | 63.23 | 1.160 | 2381.74 | .7886 |
| “ “                  | 17.92 | 960  | 146.5 | 63.92 | 1.162 | 2387.94 | .7915 |
| “ “                  | 17.92 | 980  | 143.5 | 63.95 | 1.164 | 2394.16 | .7997 |
| “ “                  | 17.91 | 1000 | 142   | 64.54 | 1.166 | 2400.38 | .7954 |

Taken to machine shop, then re-tested July 9th; required 11 pounds to rotate wheel.

|  |       |  |       |       |       |         |       |
|--|-------|--|-------|-------|-------|---------|-------|
|  | 18.00 |  | 141.5 | 77.18 | 1.289 | 2782.45 | .8168 |
|--|-------|--|-------|-------|-------|---------|-------|

Again taken to shop, then re-tested July 13.

|  |       |  |     |       |       |         |       |
|--|-------|--|-----|-------|-------|---------|-------|
|  | 17.97 |  | 146 | 76.32 | 1.286 | 2772.69 | .8119 |
|--|-------|--|-----|-------|-------|---------|-------|

Taken to machine shop a third time, re-tested July 16.

|  |       |  |       |       |       |         |       |
|--|-------|--|-------|-------|-------|---------|-------|
|  | 17.97 |  | 152.5 | 76.24 | 1.284 | 2766.19 | .8131 |
|--|-------|--|-------|-------|-------|---------|-------|

I will here explain about slight changes mentioned in report of Risdon's tests. First, a 25-inch Risdon wheel was tested. June 16, 1874; it gave 75 per cent useful effect. Mr. Risdon had it taken to shop and the rim of wheel reduced the lightest chip possible; the wheel was re-tested the next day and gave .8704 per cent. A second 25-inch was tested July 20.

| Head. | Weight. | Rev. per M. | Horse Power | Cubic feet. | Per Cent. |
|-------|---------|-------------|-------------|-------------|-----------|
| 18.41 | 320     | 232         | 22.49       | 845.93.     | .7655     |

The wheel was taken to the shop and the bridge tree lowered one and a half inches; then re-tested July 21.

| Head. | Weight. | Rev. per M. | Horse Power | Cubic feet. | Per Cent. |
|-------|---------|-------------|-------------|-------------|-----------|
| 18.61 | 320     | 256         | 24.82       | 823.06      | .8593     |

A 54-inch Risdon was tested, July 12, 1876

| Head. | Weight. | Rev. per M. | Horse Power | Cubic feet. | Per Cent. |
|-------|---------|-------------|-------------|-------------|-----------|
| 17.06 | 1900    | 107         | 123.21      | 5047.72     | .7586     |

When the wheel was put together the chutes projected too far inward, and the inner ends were cut off leaving them square across, and about half an inch in thickness; after the test the wheel was taken out and the back side of the inner end of chutes were clipped away, leaving the ends a "quarter round;" this added ten square inches to the openings; the wheel was re-tested Aug 1.

| Head. | Weight. | Rev. per M. | Horse Power | Cubic feet. | Per Cent. |
|-------|---------|-------------|-------------|-------------|-----------|
| 8.66  | 1400    | 78.5        | 49.95       | 3742.54     | .8177     |

Similar variations will be found in testing any make of wheels. When the system of testing commenced some ten years since, there was hardly a wheel tried that was in a condition to run until various alterations had been made: the step was out of place, or the followers were made of seasoned wood and would swell and bind the wheel as soon as wet. Few balanced their wheels, and it really needed a machine shop to put wheels in order before they could be tested; days, sometimes weeks were required to test a wheel. Builders do better now, still many wheels are yet sent to me that are in no condition to be tried in a testing flume or mill. The test of an Eclipse wheel is given on next page to show the effect of tight followers and swollen step; these were loosened before second trial:

## THE POWER REQUIRED TO GRIND WHEAT, CORN, Etc.

When the testing system commenced it was supposed that there was great waste of power, as the opinion prevailed that a bushel of wheat per hour could be ground for each horse power expended.

Much pains was taken to obtain data to determine that point, and several imperfect trials were reported in the second and third editions of this work.

The first, a trial at North Sunderland, Mass., a half insane miller doing what he called the grinding, which simply consisted of cracking the corn, leaving it about the same as what is called *hominny*. The same was the case in the turbine against breast wheel test, near Hartford, Conn. "What power is required to drive a run of stones," is another case often referred to. The value of the TURBINE AGAINST BREAST WHEEL tests consists in showing the comparative merit of the breast wheel and turbine, and the difference in power required for cracking corn or grinding it, and to show that where everything is in perfect condition for a spurt, a bushel of rye or wheat perhaps may be ground per hour per horse power, as a horse may trot a mile in two and one-fourth minutes, but the same horse would be killed in a week if compelled to do ten miles per hour ten hours per day. So I will refer those desirous of information about grinding to the report of the Elkhart, Indiana, tests. These were made by the most exhaustive method possible.

No pains or expense was spared in preparation or testing, then the results were carefully worked up while every point was fresh in mind, and it was my urgently expressed wish that the opposing party, upon the completion of the making up of the report of results, should immediately be furnished freely with copies thereof; other counsel prevailed and the reports were held for two years, then brought into court. In that time I had patented many inventions, acted as expert in numerous cases of hydrodynamics, and the Elkhart case had passed from my mind as though it had never been there. The printer in making up the report seemed to have pried the form containing the table of results of grinding, after I had read the proof, so there were numerous errors, but that was a matter of little consequence, for the summing up for the report was done from the results of tests before the table was made, and I here state that those results are as perfect as I believe it is possible to make such.

While in charge of a testing flume, it was my invariable rule to refuse to make any test that could not be openly witnessed and publicly reported; the Elkhart tests were the first and will be the last made by me that cannot be reported as soon as made.

It was a practice for wheel builders to have wheels tested, hold them awhile, repaint, then send them as new wheels to be retested. Messrs. Stout, Mills & Temple of Dayton, Ohio, Messrs. Fales & Jenks of Pawtucket, R. I., and John Tyler of Claremont, N. H., did so, quite likely others. I presume that any party who did so will give their experience upon application.

A retest of the same wheel, unless some change has been made therein, should not vary over one-fourth of one per cent.

## Water Wheel Royalties.

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Upon what system of reasoning does the turbine patentee claim royalty upon plans of no certain value? To render a patent valid the inventor must have plans so well defined that he can describe them so that those skilled in the art may readily build from such plans or description thereof; if he can not do so, what right has he in the invention? There has been too much sympathy for the "poor inventor" and not enough generally for those who find means to carry out such inventions; an arrangement generally that the inventor shall find experience or plans, the capitalist money for the inventor to live upon and experiment with. For months, perhaps years, the inventor slashes away with little consideration for anything but his own fancies, and if a true inventor, enjoying much in witnessing the development of his ideas; while the capitalist too often finds that he has changed positions, that in fact he has the experience, while his money has turned to moonshine, or something as unsubstantial. Capitalists do not invest in 70 per cent. turbines, and there are no good reasons for expecting royalties for such.

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## Numerous Sizes of Turbines.

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In looking over the piles of circulars issued by the hosts of turbine builders one is surprised at the numerous sizes tabled by each; and when it is understood that these tables represent both right and left hand wheels, the question arises as to how any man could ever expect to do a profitable business where so many expensive patterns are required, unless such wheels can be sold at an immense profit. A list so numerous acknowledges the fact, that such wheels can only be used economically when exactly adapted to a fixed quantity of water; in short, that they are extravagant in its use unless working with gates completely opened; this has been the case since the first introduction of the turbine, and in some cases may now be done more through habit than necessity; but if necessary, then it is plain that such wheels can not economize the power of our variable streams; either there must be a waste of one-half of the power during eight or nine months of the year, or a total stoppage through the dry season. Then, again, what earthly use is there for "right and left hand" wheels of the same size? By turning the teeth of the crown gear up or down, the shafting is rotated in the direction desired. With thirty-two sizes of turbines to work up to a desirable percentage, farewell hope! Manufacturers and turbine builders must consider and work together, if wheels of high useful effect are invariably to be expected. Numerous sizes add much to cost and the purchaser has to pay for it. If left hand wheels were impossible they would soon be found unnecessary, for preparations can easily be made to meet the case. Seven or eight sizes only, would allow the builder to work them up right, and the purchaser would soon be able to procure a turbine that would utilize the whole power of his stream, either summer or winter.

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## Hard Running Wheels.

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For several years after the testing system began there was hardly a builder who took any particular pains to have his wheels run easy. "Oh it will go, only put the water to it," would be the reply when the subject was mentioned. I can recall several that would have gained very different results had their wheels been in proper condition, but the matter was not so well understood then as now. Even now it requires constant attention to avoid errors in that way, for it is very common for wheels to turn perfectly free at the start, then after running a few minutes become bound through swelling of step or followers, so as to lose a number of revolutions per minute, carrying the same weight as at first starting; Risdon's highest result 91.32 and Tyler's 91.27 were supposed to be erroneous, because neither could be repeated, but from the cause named above they could not be rejected.



## Test of Wheel to Determine Loss of Power in Transmission Through Gears.

In making the experiments to determine the loss of power in transmission through gears, mitre gears twenty-seven inches in diameter, five inch face, fifty-seven teeth, were used on wheel and "jack-shaft," the last being six feet in length, and three inches in diameter; a spur gear twenty-four inches in diameter, four and one half inch face, forty-four teeth, was secured upon the "jack-shaft," which worked into another gear of the same size upon a second horizontal shaft same size and length as the first; the second representing the main line of shafting through a mill, both horizontal shafts worked in common babbitted bearings. The dynamometer was placed upon the end of shaft representing the main line, and the wheel tested through the two pairs of gears; then upon the wheel shaft

|                                  | Tests     | Head.       | Revolutions.   | Horse Power. | Percentage. |
|----------------------------------|-----------|-------------|----------------|--------------|-------------|
| Dynamometer on horizontal shaft. | 1st test, | 16.03 feet, | 160 per minute | 25.55        | 75.90       |
| Dynamometer on Wheel shaft.      | 2d "      | 16.08 "     | 168 "          | 26.73        | 77.40       |

## Important Tests to those Gearing Wheels where the Head Varies.

The best speed for each head is first given: 20-inch wheel.

| Head. | Weight. | Revolutions per minute. | Horse Power. | Cubic feet. | Percentage. |
|-------|---------|-------------------------|--------------|-------------|-------------|
| 18.44 | 500     | 249                     | 39.92        | 1400.31     | .7753       |
| 7.85  | 200     | 164                     | 9.94         | 869.84      | .7724       |
| 18.35 | 640     | 161                     | 31.22        | 1418.94     | .6663       |
| 7.99  | 75      | 246                     | 5.50         | 757.93      | .4911       |

48-inch wheel.

|        |      |       |       |         |       |
|--------|------|-------|-------|---------|-------|
| *17.55 | 1100 | 121   | 80.66 | 3586.83 | .6733 |
| 9.79   | 600  | 90.5  | 32.90 | 2340.80 | .7018 |
| 17.47  | 1525 | 90    | 83.18 | 3618.81 | .6982 |
| 10.00  | 200  | 120.5 | 14.60 | 2199.34 | .2522 |

\*121 revolutions per minute was found to be the best speed for whole and part gate.

## Turbine Buckets.

Ten years since turbine builders added much to the cost of their wheels by making the buckets of sheet iron, steel, brass, or bronze; shaped in iron moulds. The best turbines yet produced have been made entirely of cast iron. Wrought iron is decidedly the poorest material that can be used for that purpose.

## A Word to Aspirants for Fame as Turbine Builders.

The incentive to turbine building is probably its supposed profit. A wood-sawyer, so little of a mechanic as to be unable to file his own saw, unhesitatingly rushes into the business, yet it is one requiring the highest possible skill; experience soon causes the adventurer to regret his haste. *A strictly honorable turbine business under existing circumstances, can not be made to pay*; that is, to sell every wheel by test on its real merits would leave half the number made on the builders' hands, for purchasers require the highest results at the lowest prices, and there are scores of builders ready to guarantee such so far as talk is concerned.



## Professional Experts.

If those acting as above could see themselves as those thoroughly acquainted with the subject in hand see them, it would have a tendency to lower their pretensions. Could the arts be put back to what from our standpoint they seem to have been 3,000 years ago, one of our best mechanics might prepare himself to act as general expert without seeming presumptuous, but to pretend to be able to do so now, when the mere word mechanic covers a thousand occupations, each having numerous variations, renders the pretense ridiculous. Yet we have such, and those who have great influence in court, particularly in patent suits. The turbine has been studied for more than a half century by the best mechanics, and the matter is not sufficiently understood to fairly allow of its being considered a science; yet the professional expert will look the matter up in a day, then go into court and testify to points of which it is simply impossible that he can know anything about. No one man can be an expert in all kinds of business, life is too short. The most intelligent and skillful telegraph operator must be the best expert in a telegraphing case, so of the shoemaker, the blacksmith, the miller, merchant, turbine builder, or engineer. In either of these callings an apprenticeship of years is required to render a person proficient; then is it reasonable to suppose that the professional expert can master any of them in a few hours' study? We would not go to a shoemaker to inquire about a turbine, or the turbine builder to learn about telegraphing. If the matter is simple and plain, an expert is unnecessary; if difficult to be understood, then certainly one skilled in the matter is the best qualified to make it plain. In cases where litigation is contemplated an expert well versed in the matter should be employed first, then if he understands his business, in three cases out of four, he will cause the matter to be settled, often advantageously to both parties interested; if he can not cause it to be settled, he can prepare it for the lawyer, so that it may be legally determined expeditiously and at the least expense. To employ the lawyer first is like trying to learn a child to read without learning it the letters; that, however, would be no more absurd than to suppose that any one man can be proficient in all kinds of business.

Faith in expert testimony is undoubtedly decreasing, simply because those called as experts are generally mere theorists, or perhaps edit some so-called scientific paper that is published on speculation—the editor, like the paper upon which it is printed, being picked up where it can be had the cheapest. A graduate from our technical schools might readily study up horse-shoeing, and testify in such a learned manner as to astonish the court with his profundity, yet his shallowness would at once become apparent could the cross-examination be conducted by an ordinary blacksmith, as I have often wished I could do with hydraulic experts. Yet, in almost any case in litigation relative to milling matters, the testimony of such men as A. M. Swain, George A. Houston, F. H. Risdon, Wm. M. Mills, and others that could be named, would be very valuable; but such men would require time to consider the matter before testifying. "Why, I thought you experts were so full of knowledge upon such matters that you were always ready to gush over," said an applicant for my services. Such may be the case with others; it is not with myself. I want, invariably, to hear both sides of a case, and time to compare the circumstances with facts gained from my own experience, before acting for any one.

## Slip of Belt.

The speed of machinery is computed from size of pulleys or gears in connection with the driving shaft; in such computations the slip of belt is seldom or never taken into consideration, yet that slip is an important item. In testing the power of a steam-engine, the counter of my dynamometer showed such a difference from the engineer's estimate, that the matter was thoroughly investigated. The driving pulley on the engine was 12 feet in diameter, that on the main line of shafting 6 feet; running light or simply driving shafting, the fly wheel making 75 revolutions the main line made 150, but with weight applied to scale beam of brake, the belt began to slip, the slip increasing with each weight added; at the maximum power of engine, the main line made 144 revolutions while the fly wheel made 75. Belt and pulleys were in perfect condition.

## Gearing Turbines by Tables.

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The practice of gearing turbines from tables prepared by guess, has been productive of much loss of power. In testing wheels it is a rare thing to find two of the same size and make, that do their best at the same speed; the best speed of the Leffel wheels is invariably wide from their tabled rate. At Bridgton, Maine, Pondicherry mill, a 54-inch Leffel wheel has been in use for ten years, working under twelve feet head and running at ninety revolutions per minute; the mill has six sets of woolen machinery, but from lack of power only five sets have been used. By test a short time since it was found that by running the wheel at seventy-eight revolutions instead of ninety, it would give twelve h. p. more than it ever had done; so that for ten years it had been running at four-fifths of its capacity, and at a time when its greatest capacity was much needed.

## Testing Curbs.

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The fact is well established now that the chutes of a turbine have as much to do with giving high results as does the wheel itself; also, that each part of the complete turbine has relation to all of the other parts, so that a change of one piece may have a serious effect upon the whole. Builders have prepared several turbines with interchangeable parts in order to test understandingly; but it would seem better to make a testing curb with changeable chutes, so constructed that their number or direction might readily be changed, and their capacity of discharge increased or diminished. With such a curb it should be possible to determine the merits of any wheel that could be tested therein.

## V Shaped Belts, Cable Transmission, etc.

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Some time since there was a mania for driving machinery with belts of the above named shape, but experience soon cured the desire. Transmission by wire cable is another matter that should be well considered before adoption; it will answer the purpose in places where shafting can not be used, but it is a very poor substitute at the best. Light shafting is still another subject for consideration; if used, the pulleys should be placed close to the hangers, for if placed any distance therefrom, the shafting will spring, and require a much tighter belt, which soon gets the shaft out of line. There is a proper limit either way.

## The Metric System.

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And why the metric instead of that so generally in use wherever the English language is spoken? Does the practical mechanic or engineer desire such change, or do the comparatively few who use that system surpass us in mechanism or general intelligence? Taking the foot as the unit, divide it into tenths, hundredths, etc., and the most perfect measurements possible may readily be made and expressed thereby. Then why change for new terms, when our language is now so unwieldy and overburdened with useless words and synonyms, that it would be a blessing if one-half of its words could be obliterated, and the other half simplified in spelling. Simplicity should be the aim, that all may comprehend; change has not always been improvement. It would be well if the engineers and professors, who are so much better known through their pretensions than achievements, could be made to understand that muddiness does not always denote depth. A change to the metric system would cause immense confusion in our standards, boundaries and records, without bringing a shadow of benefit in return. Our language now is almost the *universal* language dreamed of, and it seems idiotic to change for that of a people occupying less of the earth's surface than is covered by some of our states.

## SILK.

Silk consists of the pale yellow, buff colored, or white fiber, which the silkworm spins around about itself when entering the chrysalis state. Silkworms are divided into two classes, the mulberry-feeding worm, from the cocoons of which is reeled the ordinary raw silk, and the wild silkworms which feed upon certain kinds of oak, ailanthus, castor-oil plant, etc. The product of the latter specimens (amongst which the *Tussah-worm* is found, producing the *Tussah-silk*) was little heard of in this country and Europe until recently, and but for the outbreak of the silkworm disease in Europe would probably have remained in India and China, although it had been utilized in both these countries for many centuries. The date when the use of silk for textile purposes was first discovered is not exactly known. Some of the Chinese historians claim that it was about 2700 years B. C., whereas others only go as far back as about 1703 B. C., or the reign of *Hoang-ti*, the third of the Chinese emperors. He, the legend tells us, was desirous that his legitimate wife *Si-ling-chi* should contribute to the happiness of his people, so he charged her to examine the silkworms and test the practicability of using the thread. In accordance with this wish, she collected insects and feeding them in a specially prepared place commenced her studies and examinations, discovering not only the means of raising them, but also the manner of reeling the silk and its use for textile purposes. It is claimed that even to the present day the empresses of China on a certain day go through the ceremony of feeding the silkworms, and rendering homage to *Si-ling-chi* as *Goddess of Silk Worms*.

The principal countries for carrying on the silkworm culture are Southern Europe, China, Japan, and India. In our country silk culture is only in its infancy, yet it is rapidly assuming proportions of importance.

When full grown the worm ceases to feed, climbs up from the feeding tray to the bush, or whatever may have been prepared for it, and commences to form itself in a loose envelopment of silken fibers, gradually enwrapping itself in a much closer covering forming an oval ball or *cocoon* about the size of a pigeon's egg, generally requiring from four to five days in its construction.

### RAW SILK OR REELED SILK

constitutes the raw material for the American silk manufacturer. When imported the same generally comes in picul bales of one hundred and thirty-three and a third pounds. Such as come from China are made up in bundles weighing from eight to twenty-five pounds each and are protected at the corners by floss or waste. The Italian silk comes in bales made up in skeins. Before it reaches the loom this raw silk must pass several manipulations and processes. First the same is taken to the sorting-room, and the various sizes of thread, or, in other words, the different degrees of fineness, are assorted each by itself. The next process is the transferring of the silk from the skeins (which are of irregular length) to the bobbins. A parcel of skeins enclosed in a light cotton bag is soaked in

water having a temperature of 110° F. for a few hours so as to soften the gum. After taking these bags out of the water they are submitted for from 5 to 10 minutes to the action of a hydro-extractor to liberate the superfluous water, and the silk with its gum thus sufficiently softened is ready for winding. The next manipulation the silk thread undergoes is cleaning.

In this process the thread is simply transferred from one bobbin to another and passes during the transfer through the cleaner, which consists of two sufficiently close parallel plates to catch any irregularity upon the silk. Chinese silk always requires cleaning, whereas Italian silk does not usually.

### WILD SILKS.

The most important of them is Tussah, and is principally found in India. This silk has until lately been greatly neglected, but at present commences to attract great notice. The cocoons are larger than those of the Bombyx mori, have the shape of an egg, and are of a silver-drab color. The outside silk of the cocoon is slightly reddish, and consists of separate fibers of different lengths, while the remainder of the cocoon is generally unbroken to its center. In India the report compiled by that government gives particulars of no less than thirty-six varieties of wild silkworms feeding upon different forest trees and shrubs

### “SPUN SILK.”

It is to be understood that the raw silk of commerce is spun by the worm as the spider spins its web, but in reeling this there is waste; then there are cocoons from which the worm has eaten its way out, of course spoiling the cocoon for reeling; then much of the product of the wild worm cannot be reeled. All such silk has to be carded and spun substantially the same as cotton, and as the fiber is short it has to be twisted hard to make it strong, so that hose or other goods made of spun silk have not the soft feeling of the raw silk, though the silk itself may be of quite as good quality.

### MOIRE ANTIQUE AND WATERED SILKS.

For these the silks must be broad and of substantial make. They are first wet and then folded with particular care to insure the threads of the fabric lying all in the same direction; they are then submitted to great pressure. By this pressure the air is slowly expelled, and in escaping draws the moisture into curious waved lines, which leave the permanent markings called watering. Moire antique silk is streaked in veins like the veins in the antique marbles. Figured silks are woven in Jacquard looms. Very heavy silks are often made so by dye-stuffs. Honest manufacturers will say that two dollars per yard at retail should purchase the best dress silks that can be made.

## FLAX, ITS CULTURE AND MANUFACTURE.

Early in the present century almost every farmer in the Eastern States raised flax, its product then being a necessity for all. The apothecary depended upon its seed for soothing the ailing; the painter for its unequaled oil for his paints; the farmer for the fiber of its pachydermatous stalks for his clothing; his wife for her bedding, laces, embroideries, etc.; the ship owner and sailor for sails and cordage. To prepare the flax it was pulled and cured, then in bundles submerged in water until the woody outside rotted or became so brittle as to readily separate from the fiber when dry and beaten in the "flax breaker." The farmer then with a "swingle," a sort of two edged heavy wooden sword, in his right hand, seized a handful of the broken stalks in his left, held the stalks over the top of the swingling plank, striking them close to the side of the plank with the edge of swingle. The swingling plank was thin at the top, made of hard wood, standing about three feet above the floor, to which it was firmly secured. The repeated blows of the swingle caused the woody shell to fly off in minute pieces or "shives." Every few blows the fiber would be drawn through the teeth of a "hatchel" or comb as a woman clears her hair. The tow trousers of the Continental times were produced from the coarse refuse combed from the flax while it was being hatcheled. This hatchel was formed by placing a gross of smooth sharp pointed steel spikes firmly in a square base secured to a bench, the spikes projecting vertically upwards six inches above the base. The fiber thus prepared was taken by the wife and wound upon the distaff of the linen spinning wheel, at which she sat and produced the thread for the shoemaker, tailor, sailmaker, and other artisans too numerous to mention, also all necessary for household use. The little flax spinning wheel was a very different affair from that of the spinning wheel for wool, as may be seen in illustrations on opposite page. At the former the woman sat and operated the wheel with her foot, using the fingers of both hands to draw the thread, the spindle being of the flier pattern; while with the wool spinning wheel she stood at its side, turning the wheel with her right hand and drawing the thread from the roll of wool with her left, the twisting being done on the end of the plain spindle.

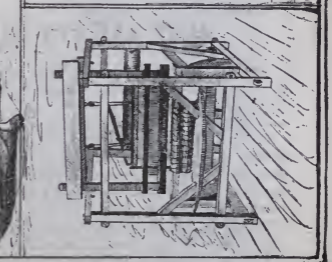
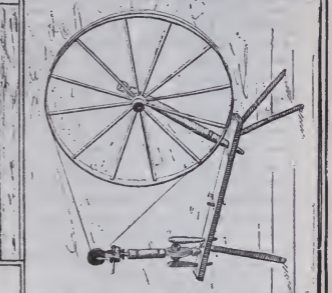
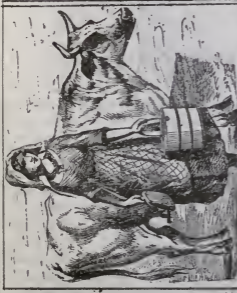
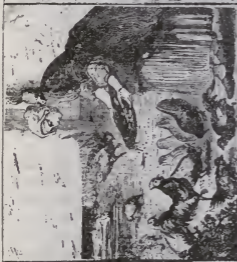
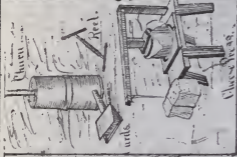
The spinning for the fabulous laces, linens, edgings, lawns, etc., of the earlier times was done substantially in the manner described or in a still more primitive way.

Spinning street yarn is not a figment of the imagination; in South America, near the equator, the writer has often seen the native women walking the street, talking, and spinning on the way, the cotton being carried under the arm, the thread being drawn by the dropping of the bobbin on which it was wound as spun, a twirling motion being given to the bobbin as it was dropped; then it was skillfully caught at the arm's length, without seeming effort.

Flax is raised in the Northwestern States and Canada, but mostly for its seed, though its fiber is in some demand for manufacture into thread, and is beginning to be used in the manufacture of paper.

Early in the century, all farmers' wives were supposed to be capable of attending to all of the duties indicated by the implements shown opposite,







spinning both flax and wool, carding the latter from the fleece for the spinning, after which going through a series of preparatory processes such as spooling, reeling, sizing, warping, drawing in, etc., etc., from the spinning wheel to the loom, where from the coarsest to the most delicate fabric for family use was produced, often very intricate patterns of bed coverings, carpets, and other ornamental designs.

The man that can realize the multifarious duties accomplished by the wife of a century since and then consider her sex inferior in constructive or mental ability to that of his own must be conceited indeed.

A half century since, our farm houses and mills contained as fair women and girls as could be desired, dressed perhaps in homespun, but their nimble fingers, in their leisure moments, were ever busy making edging, embroidery, or fancy trimmings for their underclothing or household use; in their place we have *ladies*, outwardly dressed fine but with ten cent undervests. The washings of the former weekly displayed volumes of refinement, of the latter sweat-stained and often ragged undervests that indicate continued use without change. The tobacconist ornaments his goods with beautiful forms clad in diaphanous and delicately trimmed under garments, but does not seem to take to the lady and ten cent undervest.

The woman with her heelless shoes, white stockings, and zephyr step, had feet that were things of beauty, while the lady of to-day, with her high heels and distorted feet that require large bay windows on her boots to accommodate her abnormal toe joints which intimate the evolution of thumbs and a return to the quadrumana family, is certainly less attractive.

If the continuation of the robber tariff, which has so benefited the rich, has not reduced wages to the standard common in all highly protected countries, it is solely because the irrepressible inventor has by improved machinery reduced the cost of manufacturing. It certainly has been the cause of a much lower grade of working men and women than formerly, but a revolution is taking place in the status of woman from which a progression may spring.

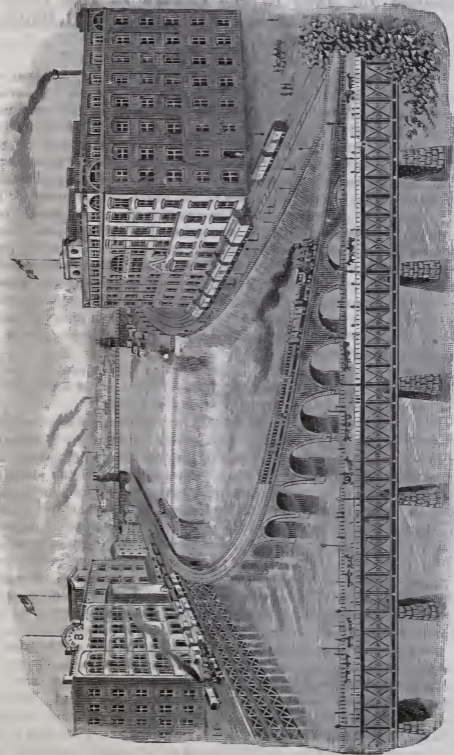
## JUTE AND ITS MANUFACTURE.

Jute is raised in India, having, while growing, something the appearance of oats, though much larger, as it reaches a height of fifteen feet or more, but like rushes it grows in water, two crops each year; its fiber, the reverse of that of flax, is on the outside of the stalk.

The ground is prepared and seeded, then flowed; with plenty of water, the growth is very rapid. At maturity the stalks are cut, then, like flax, are immersed in water to soften the fiber; the process is then similar to that of flax; the ends are cut even to prepare the fiber for baling, the ends cut off being known as "jute butts."

There are various places of its manufacture in this country, one, quite extensive, at Ludlow, Mass., from whence my information has been obtained.

The machinery used is similar to that of cotton manufacture but coarser and much heavier. The product of the Ludlow mills is the covering matting used by furniture dealers for their furniture in transit.



VIEW OF MINNEAPOLIS, AND FLOURING MILLS IN THE FOREGROUND.

## THE ROLLER PROCESS OF FLOUR MAKING.

Revised for 1891 by The Edward P. Allis Company of Milwaukee, Wisconsin, U. S., Flour Mill Builders and Furnishers.

To prepare wheat for milling, it is good practice to run it through a dustless receiving separator to free the grain of coarse trash like straw-joints, corn, oats, etc.; then through a dustless milling separator to remove finer trash, like cheat, screenings, oats, sand, and seeds, and through two separate scouring and polishing machines to remove dust, and scour off smut, the fuzz on the ends of the berry and as much of the outer woody bran coatings as may be easily detachable. The most complete flour mills attach dust collectors to the exhaust air trunk of the above grain cleaners for the sake of cleanliness. To remove metallic particles the wheat should be passed through an automatic magnetic separator. During dry winter weather the bran of the wheat often becomes brittle and consequently easily pulverized when passed through the rolls. To obviate this, a wheat heater is employed, using steam at about 98 degrees Fahrenheit, as a heating agent. This attracts the latent moisture from the interior of the berry to the surface, thus toughening it. Some varieties of wheat require steaming in place of heating, and wheat raised by irrigation generally requires wetting down in bulk for 24 to 48 hours before being used.

Briefly speaking, the roller system has for its object, 1st, the gradual reduction of wheat into middlings, 2d, the purification of the middlings, and 3d, the gradual reduction of the middlings into flour.

This method of flour making is divided into two systems popularly known as the "long" and the "short" system. These terms apply principally to the number of reductions used to convert the wheat into middlings. The long system is used in the larger mills, especially those doing a merchant or shipping business, and produces a maximum amount of middlings, and for this reason is the more profitable system. Not less than five reductions on wheat are employed in the long system. Each reduction is technically known as a "break." Each break is made on a pair of corrugated or fluted rolls. The corrugations of the first break rolls are rather coarse, but they are finer on each succeeding break. The number of corrugations on each pair of break rolls varies with the kind and condition of the wheat and the number of reductions employed, so that exact information on this point cannot be given here. One roll of each pair of break rolls has a speed  $2\frac{1}{2}$  or 3 times greater than its mate. After each reduction of the wheat on the break rolls it is bolted or "scalped" on coarse mesh wire or silk cloth to separate the middlings and flour from the broken wheat so that the latter may be sent to the succeeding break and be further reduced. These scalpers are of a revolving hexagon or round reel form, or on the reciprocating sieve design. The miller in charge so graduates the breaks from first to last that the bran issues after the last break (and the subsequent scalping operation) free of flour, as long as the grain is in good milling condition. Should it be

damp or tough, or the weather be murky, a bran duster is necessary to remove all remaining traces of flour from the bran. The middlings and flour derived by the foregoing process is collected from the various scalpings and sent to a grading reel, clothed with silk cloth of varying fineness. This reel separates the flour from the middlings. The flour is bolted on round reel flour dressers or centrifugal bolts to prepare it for the market and forms a commercial grade known as "bakers' flour." It constitutes about 50 to 70% of the entire floury product when made from winter wheat, or about 20 to 40% when made from spring wheat. The middlings are divided into three or four grades or sizes and sent to middlings purifiers, which, by means of reciprocating sieves and a graduated air suction, remove all free bran particles and fiber. Three grades of middlings are formed by this operation, viz.: middlings free from impurities, middlings containing a small amount of fine adhering bran particles, and coarse middlings attached to germ or bran. A fine fiber or cellular tissue permeates each particle of middlings, which is of a white color and undistinguishable from flour until it is wet or baked into bread, when it imparts a dark color. To remove this fiber successfully it is necessary to gradually reduce the middlings in size, by successive passages through smooth rolls, separating the flour derived before the middlings pass to the following reduction. This sizing operation also liberates adhering bran and germ impurities. The various grades of middlings are at first reduced separately on individual pairs of rolls, according to their size and quality, but, at an advanced stage in the process, when a similarity in size and quality is reached they may be mixed and worked to a finish. The flour from the foregoing operations is bolted on flour dressers and is known as patent flour, and commands the highest price on account of its pureness. Spring wheat produces from 50 to 75% of patent flour, and winter wheat 15 to 35%. In finishing up, a small percentage of flour results, varying from 3 to 10% of the entire flour product, which is too dark in color to be incorporated with the other grades. This forms the low grade. In large mills, any or all of the above three grades of flour may be subdivided according to quality and sold as separate brands.

In the short system, it is, as its name implies, a curtailing of the above process. For instance, where five breaks on wheat and seven or more crushes on middlings are used in the long system, only three breaks on wheat and five crushes on middlings would be used in the short system. It is claimed by excellent authority that owing to the more abrupt method of reducing and crushing as practiced in the short system, a smaller percentage of middlings results and consequently a reduced percentage of high grade and high-priced flour. Short system mills are usually of small capacity, ranging in size from twenty-five to seventy-five barrels per day, and usually mix all the flour to form one straight grade, and are more adapted to winter wheat than to spring wheat.

## A WORKING FLOURING MILL.

According to the Plans of The Edward P. Allis Co., Milwaukee, Wis.

The engraving opposite shows a perspective view of a working flour mill having a capacity of 50 barrels of flour in 24 hours. This engraving and the description thereof is given in connection with the adjoining article on "The Roller Process of Flour Making." A small mill is selected for these modest sized pages in preference to one of large capacity, to enable us to show the details on as large a scale as possible.

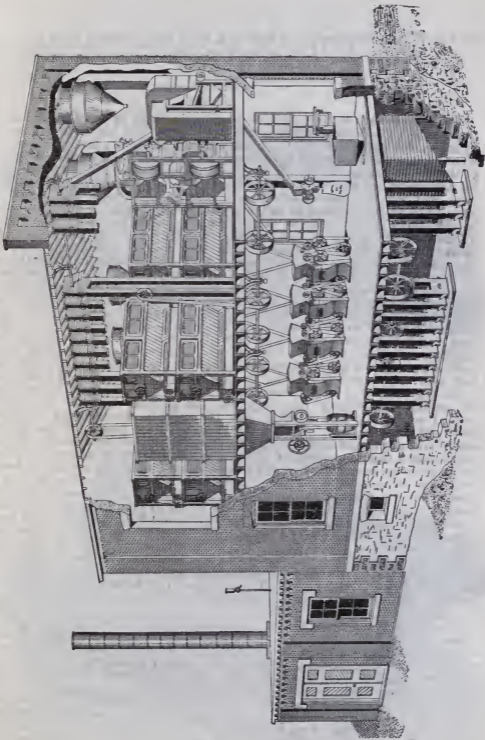
The operation of the mill commences by putting the wheat, as it comes from wagons or cars, into the hopper scale seen in the right hand corner of the first floor in the engraving, which weighs 40 to 60 bushels per draft.

From the scale the wheat descends to the bin shown in the basement directly underneath, which will hold sufficient grain to operate the mill one day. The adjoining elevator serves to elevate the wheat, as needed, to the milling separator shown on the second floor. Here the wheat is relieved of all foreign particles and shrunken grains unfit for milling. The grain is now re-elevated to the upper one of the two adjoining smutters and scourers, and after the wheat has been acted upon by these two machines it is stored temporarily in a bin on the second floor, not shown in the engraving, where it is ready for passage through the rolls and bolts in its conversion into flour, as described in detail on other pages. The shrunken wheat, taken out by the separator is spouted to a screenings grinder placed against the far side wall and is converted into feed for horses or cattle. The dust from the three wheat cleaners is blown into Cyclone dust collectors, those conical affairs shown near the ceiling of the second floor, which separate the air from the dust, discharging the dust at the bottom and the air at the top. In the background of the second floor are shown the various flour dressers, centrifugal finishers, and middlings purifiers. On the first floor are shown the four double roller machines with automatic feeders, each machine containing two pairs of rolls, each pair working entirely independent of the other. Three pairs of these rolls are corrugated for the purpose of gradually reducing the floury part of the wheat to middlings, while the remaining five pairs are smooth to gradually reduce the middlings, after purification, to flour. Near the side wall in the foreground is shown a flour packer with its flour storage bin on the floor above. In the rear is the power room, containing the engine, boiler, pumps, and heater. A bushel of 60 lb. wheat produces 38 to 44 lbs. of flour, 6 to 10 lbs. of bran, 6 to 8 lbs. of ship stuff, 1 to 3 lbs. of screenings, and  $\frac{1}{2}$  to  $\frac{3}{4}$  lb. invisible loss during milling. These quantities vary with the kind and condition of the wheat, the condition of the weather, the size, kind, and condition of the mill, and the skill of the miller in charge. From 6 to 14 horse power per barrel per hour is required as motive power, depending on the size of mill and the proximity of power to the machinery.

Following is a list of the flouring mills of Minneapolis, with names of owners and capacity of each per day:—

Pillsbury (A) Mill, 7200 bbls., Pillsbury Washburn Flour Mill Co.; Pillsbury (B) Mill, 2500 bbls., Pillsbury Washburn Flour Mill Co.; Anchor Mill, 1600 bbls., Pillsbury Washburn Flour Mill Co.; Palisade Mill, 2000 bbls., Pillsbury Washburn Flour Mill Co.; Lincoln Mill, 1000 bbls., Pillsbury Washburn Flour Mill Co.; Washburn (A) Mill, 4200 bbls., Washburn-Crosby Co.; Washburn (B) Mill, 1300 bbls., Washburn-Crosby Co.; Washburn (C) Mill, 3000 bbls., Washburn-Crosby Co.; Crown Roller Mill, 2100 bbls., Northwestern Consolidated Mill Co.; Columbia Mill, 1600 bbls., Northwestern Consolidated Mill Co.; Northwestern Mill, 1600 bbls., Northwestern Consolidated Mill Co.; Galaxy Mill, 1500 bbls., Northwestern Consolidated Mill Co.; Zenith Mill, 1000 bbls., Northwestern Consolidated Mill Co.; Excelsior Mill, 1100 bbls., Minneapolis Flour Mfg. Co.; St. Anthony Mill, 650 bbls., Minneapolis Flour Mfg. Co.; Standard Mill, 1700 bbls., Minneapolis Flour Mfg. Co.; Humboldt Mill, 1150 bbls., Hinkle, Greenleaf & Co.; Dakota Mill, 350 bbls., H. F. Brown & Co.; Holly Mill, 500 bbls., Holly Mill Co.; Minneapolis Mill, 1200 bbls., Crocker, Fisk & Co.; Cataract Mill, 800 bbls., D. R. Barber & Son; Phoenix Mill, 275 bbls., Stamwitz & Schober. Total 38,325 bbls.

THE EDWARD F. ALLIS COMPANY, MILWAUKEE, WIS





## COTTON MANUFACTURE.

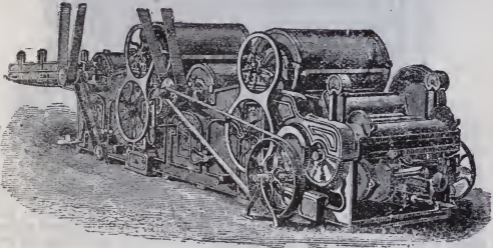
The manufacture of cotton goods, now so enormous in quantity and so varied in multiplicity of uses, is of comparatively recent date. The fibre was first introduced in England about 1640; a century latter, or in 1741, but 1,160,000 pounds were used there—a quantity that would but partially have loaded a single ship of that period, or a freight train of to-day. The invention of the spinning frame, by Arkwright, in 1768-71; the spinning jenny, by Haregrave, about the same time, and the combination of the two by Crompton, thus forming the mule, gave the first great impetus to the business, which was enormously increased by Eli Whitney's invention of the cotton gin, and of the card setting machine by Amos Whittemore, both Massachusetts men. The really successful power-loom seems to have been invented by the Rev. Edmund Cartwright of England. Fear that such machinery would render their employment unnecessary, caused the working class to gather in mobs, and destroy it, so that, as late as 1813 it was supposed that there were only about 2400 power-looms in use in all England. The war of 1812 with that country made it more necessary to manufacture cotton goods in this country, and it was done in several of the states, but with what would now be considered a ludicrous division of labor, as the spinning was done with water or horse-power, then distributed among the farmers' families, and there woven in hand-looms. Power-looms were tried in various places, but without being able to compete with hand-looms. Probably the first mill ever constructed for taking in raw cotton, and turning it out as finished cloth, was completed in Waltham, Mass., in 1813. This had 1700 spindles, and all the other machinery necessary for the purpose named. The enterprise proved successful, and another and larger mill, having 3584 spindles, was soon added to the first. [See Lowell water-power rate.] From such beginnings have grown the immense cotton manufactures of the country. Six million one hundred thousand bales of cotton were raised in this country the past year. Spinning is the heavy work of the business, and upon the spindle is based the estimates of cost, value, capacity and power required for the mill. Circumstances in each case, of course, affect such estimates. Suppose a new mill to be constructed where a dam and canal are ready to take the water for power, the cost for race, wheel-pit, mill and machinery would be estimated, under favorable circumstances, at about \$14.50 per spindle. Sixteen dollars per spindle at this time should fit up such a mill with machinery of the most perfect kind. If canal, dam and boarding houses were to be added, the cost would probably be \$20 per spindle. At Fall River, where steam is used for power, the estimate at this time is \$17 per spindle, but Fall River does not furnish boarding houses. A mill 45 x 100 feet, four stories and attic, would require one floor for spindles. A spinning frame, having 128 spindles, requires 56 feet floor space, 16 x 3½ feet, or about 2.3 spindles per foot; but a passage way is required each side of the frame, so that 5000 spindles would be a good outfit for such a mill or floor. Six thousand might be used, but would hardly be advisable, unless room was scarce for the power at command. The power should equal two h. p. for each one hundred spinning spindles in a mill. There are light running spindles and machinery that could be driven with something less than that rate—others that would require more; but the rate is a fair average estimate. Warp and thread mills require more power in proportion to the number of spinning spindles than mills that make cloth. Two h. p. per each hundred spinning spindles is a fair estimate for the power required in silk mills. Thirty-five to fifty spindles in cotton mills are required per loom, the number depending upon the No. of yarn used or fineness of cloth produced.

The census for 1880 will give the number of spindles in the Southern states as 714,078; looms, 15,222, or about forty-seven spindles per loom, which would indicate that their product is quite fine cloth, or, what is more probable, that many of the spindles are employed in making yarn that is not woven there.

## COTTON MANUFACTURE.

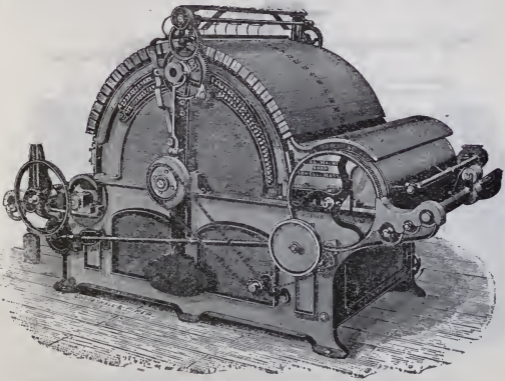
From the bale the cotton goes to the Pickers, Opener, Breaker, and Finisher. All similar in appearance.

### PICKER.

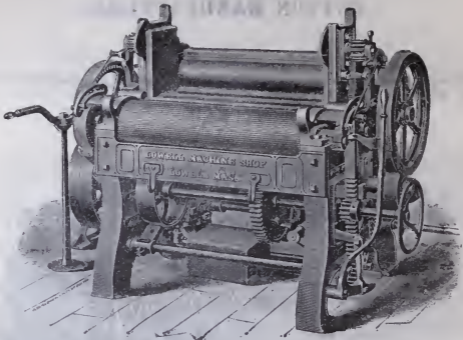


From Finishing Picker in "laps" the cotton goes to Breaker Card.

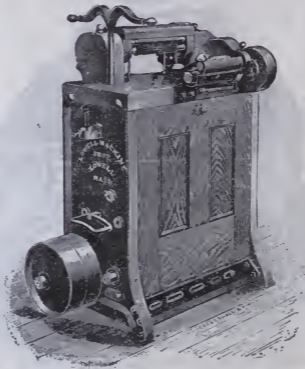
### CARD.



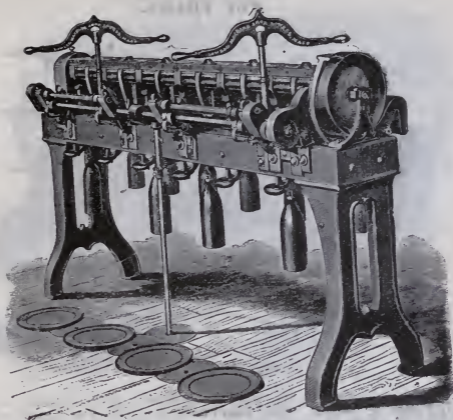
Thence in slivers from sixty to a hundred cards to the Doubler.

**DOUBLER.**

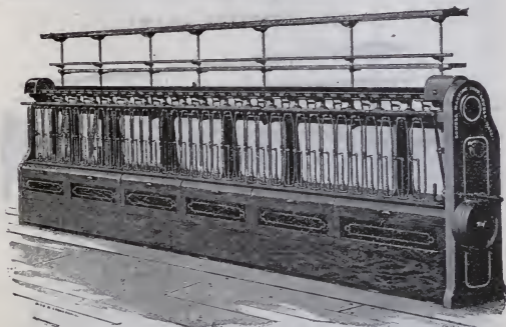
Which turns it into laps ; these are taken to the Finishing Card ; this is similar to the Breaker Card in appearance. From Finishing Card cotton in slivers goes to the Railway Head, which delivers into cans, from six to ten cards, to Railway Head.

**RAILWAY HEAD.**

From Railway Head to Drawing Frame, which leaves it in cans.

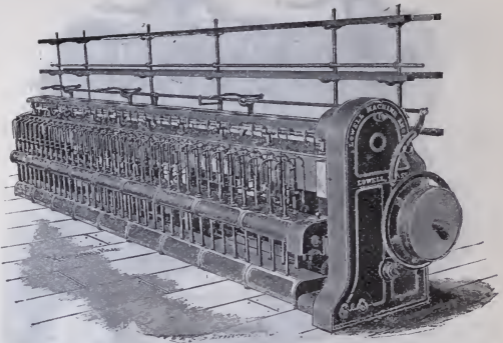
**DRAWING FRAME.**

From Drawing Frame it goes to the Slubber, which turns it into bobbins  
**SLUBBER.**



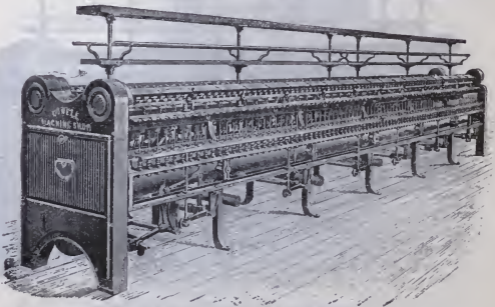
Thence to the Intermediate or Fly Frame.

## FLY FRAME.

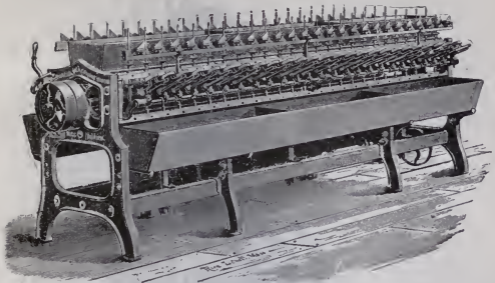


From Intermediate or Fly Frame on bobbins to the Fine Frame, similar to Fly Frame or Slubber. From Fine Frame to the Ring Spinning Frame and Mule. The Ring Frame makes the warp, the Mule makes filling, the filling going direct from the Mule to the Loom. In general appearance the Mule resembles the illustration of mule in woolen manufactures on another page.

## RING SPINNING FRAME.



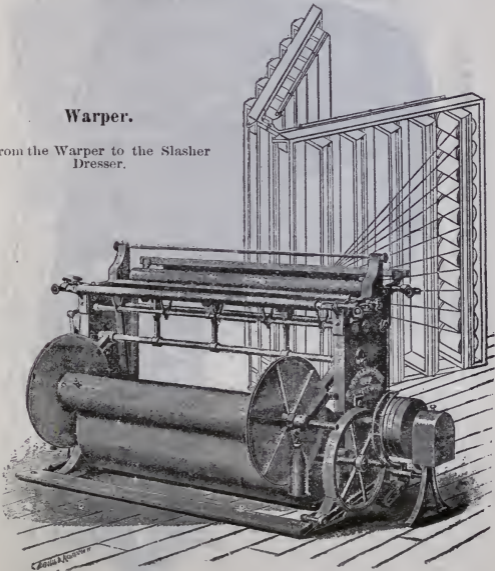
From Spinning Frame the warp goes to the Spooler.

**SPOOLER.**

From the Spooler to the Warper.

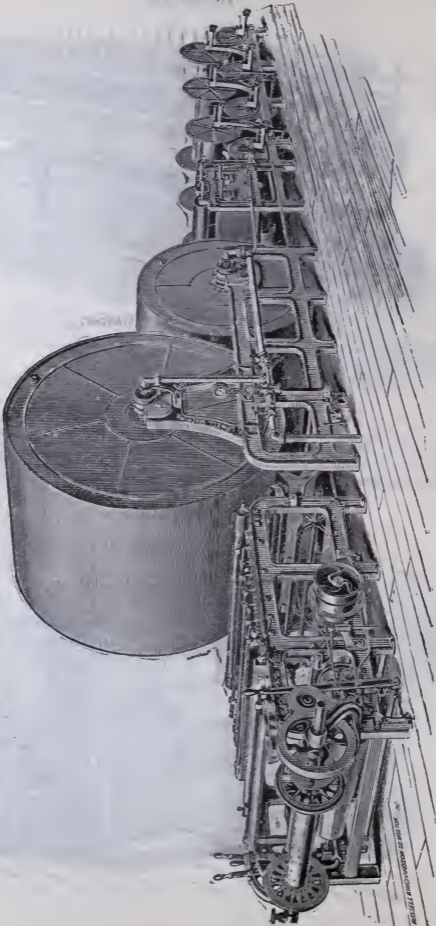
**Warper.**

From the Warper to the Slasher Dresser.

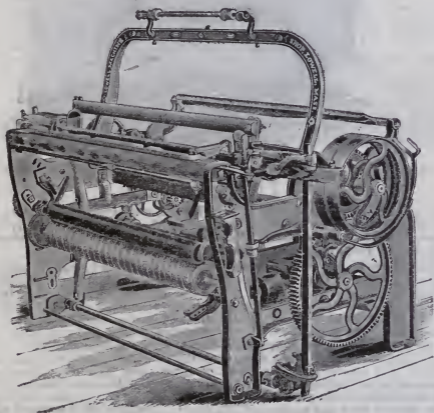




## SLASHER DRESSER.



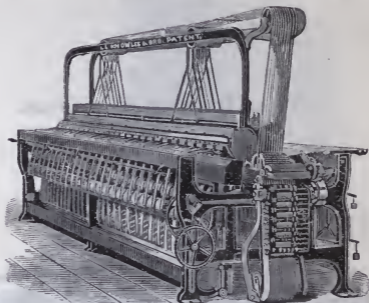
From Slasher to Drawing-in Girls (Hand Work)

**From Drawing-in to Loom.****LOOM.**

For spool cotton the process is similar up to the spooler, then there are doublers, twisters, thread spoolers, etc., etc. Bleaching, calico printing, and a thousand other varieties of work such as tape, fringe, counterpanes, each requires special machinery, looms, etc.

## Ribbon, Webbing and Tape Loom.

*Manufactured by L. J. Knowles & Brother, Worcester, Mass.*



TESTS MADE AT THE MILL OF EDWARD O. DAMON DURING THE MONTH OF SEPTEMBER, 1880.

The machinery consisted of 73 Tape Looms, carrying 2003 shuttles; 2 Quillers of 36 spindles each, and 1 of 18 spindles; 2 Warp Dressers; 1 2-ply Warper; 1 Yarn Spooler; 1 Tape Reel; 1 Yarn Warper, single; 2 Tape Spoolers; 2 Tape Presses; 30 Counter Shafts, average length, six feet.

The power for the above machinery was taken from below, through the floor, on to a short main shaft about ten feet in length, the main pulley being forty-one inches in diameter and about eighteen inches face; belt, fourteen inches wide. One-ply. From this shaft the power was transmitted through a pair of bevel gears (about 30-inch diameter, 4-inch face) to the short counter-shafts. The power scale was applied to the main driving pulley, and examined and tested at short intervals, to see that it was working smoothly and correctly. Gen. Theo. G. Ellis, of Hartford, made a very thorough examination and test during the month, and reported, as the result of these tests, that the amount of power transmitted to the machinery, at 145 revolutions of the main shaft, was 10.61 h. p. At 136 revolutions of this main shaft, he reports the approximate power as 9 h. p. The tests of the same machinery, leaving the dressers off, was found to be about 2 h. p. less.

H. A. FOSTER, *Supt.*

TESTS MADE AT MILL OF NASHAWANNUCK MFG CO., EASTHAMPTON, MASS.  
[Elastic Goods, Suspenders and Ribbons.]

The machinery consisted of 149 Looms (Knowles' and various kinds), 15 Spoolers, 14 Warpers, 11 Quillers.

Power required to drive all the above machinery to speed, 23.2 h. p.

EDWARD PAINTER, *Supt.*

TESTS MADE AT MILL OF GLENDALE ELASTIC FABRIC COMPANY,  
EASTHAMPTON, MASS.

The machinery consisted of 100 Looms, 10 Spoolers, 12 Quillers, 775 Braiders.  
Power required to drive all to speed, 25.4 h. p.

E. C. KOENG, *Supt.*

## Test of Turbine Wheel and Power Required to drive Machinery in Mill at Natick, R. I.

To ascertain power required to drive machinery, the gate was opened until designated machines ran at regulator speed, then the power of wheel was found, with same head and gate opening. The turbine replaced breast wheels, and the discharge from the turbine as shown by the old water mark in tail-race 35 feet in width was 8 inches less in depth than from breast wheels.

Test of Machinery, March 14, 1874.

The first test, shafting alone. The gate  $3\frac{1}{2}$  turns open, with 21 feet,  $3\frac{1}{2}$  inches fall. Wheel making 77 revolutions per minute, horse power, 43.

The second test, all the shafting and 457 Mason Looms, (print goods, 64 sq., 150 picks per minute.) The gate  $5\frac{1}{2}$  turns open, with 21 feet,  $1\frac{1}{2}$  inches fall. Revolutions of wheel 77, horse power, 88.

The third test, all the above and 77 ring spinning frames, of 9,856 Rabbeth spindles, 6750 revolutions per minute, also 8 warpers, 8 spoolers of 64 spindles each, and 17 mules with 10,364 spindles. The gate  $9\frac{1}{2}$  turns open, with 20 feet, 9 inches fall. Revolutions of wheel 77, horse power, 192.

The fourth test, all the machinery in the mill, or in addition to the above, 1 Kitson opener, 2500 revolutions, 6 30-inch Whitin's lappers, 3 beaters, each 2200 revolutions, 70 30-inch breaker cards with 125 revolutions of cylinders, with 5 Mason Railway heads, 2 doublers, 70 30-inch finisher cards with 125 revolutions of cylinders, with 5 Lanphear railway heads, 10 drawing frames with 59 deliveries, 6 slubber speeders with 420 spindles, 554 revolutions of flyers, 12 fine speeders, 1248 spindles, 770 revolutions of flyers. The gate  $10\frac{1}{2}$  open, 20 feet,  $5\frac{1}{2}$  inches fall. Revolutions of wheel 76, horse power, 263. Gate opened in full to get power of wheel,  $20\frac{1}{2}$  feet fall,  $291\frac{1}{2}$  horse-power.

## Nelson Mill, Winchendon, Mass.

Denims, Sheetings, and Colored Goods—

|   |                 |
|---|-----------------|
| 4 pickers, 64 cards, 7300 spindles, 2 drawing frames and 180 looms, | F. P.<br>158.80 |
| All the above, except pickers,                                      | 130 10          |
| All except pickers and cards,                                       | 89.46           |
| Only looms running,   | 57.85           |
| Shafting,   | 39.33           |

## Monohansett Mill, Putnam, Conn.

Two hundred horse-power drives two hundred and ninety two 40-inch wide looms to 140 picks per minute, 5632 frame spindles, 6768 mule spindles with all the other necessary machinery.

## Eagle Mill, Connecticut.

This is to certify that I weighed up the power for John L. Ross, of the following machinery and shafting at his mill, in Eagleville, Conn., with a Dynamometer on main shaft, and the power developed was found as follows, to wit:

|  |            |
|--|------------|
| Test No. 1—Run the shafting, 1 dresser, 1 spooler, and 12 frames, indicating | 27.64 h.p. |
| Test No. 2—shafting, 1 dresser, 1 spooler, 15 spinning frames,               | 30.81 "    |
| Test No. 3— " 1 " 1 " 18 " "   | 34.86 "    |
| Test No. 4— " 1 " 1 " 18 " "   | 34.86 "    |
| Test No. 5— " 1 " 1 " 15 " "   | 31.12 "    |
| Test No. 6— " 1 " 1 " 12 " "   | 27.27 "    |
| Test No. 7— " 1 " 1 " 12 " "   | 27.27 "    |
| Test No. 8— " 1 " 1 " 15 " "   | 31.12 "    |
| Test No. 9— " 1 " 1 " 18 " "   | 34.86 "    |
| Test No. 10—All of shafting connected to run the above machinery,            | 10.89 "    |

## Experiments at Massachusetts Cotton Mills.

LOWELL, MASS., MARCH, 1872.

Trial of power required to drive 15 stretchers. (3d speeders) 52 spindles each =780 spindles. Speed main shaft of machine, 396 revolutions. Speed of flyer, 1121 revolutions. Frames driven by a train of 8 counter-shafts—two frames by each, except the last, which drives one. These shafts are driven, the first from the main line, and the others in succession from each other. 1st. Machines and shafting required 8056 lbs. per sec =14.65 horse-power=537 lbs. or .976 horse-power each=10.3 lbs. per spindle=53 24 spindles per horse-power. 2d. Shafting and loose pulleys, 2000 lbs.=3.64 horse-power. 3d. Shafting alone, belts off, 732 lbs.=1.33 horse-power.

Trial of power to drive 6 throstle spinning frames, (warp), 5 having 128 spindles each, and one 112 spindles, =752 spindles, driven by a train of 6 counter-shafts, the first belted from the main line, and the others in succession from each other. This being an odd row of frames, only one frame is belted from each shaft. Spinning No. 20 yarn, cylinder running 750 revolutions, and flyers 4312 revolutions per minute. 1st. Shafting and loose pulleys, 1150 lbs.=2.09 horse-power. 2d. Shafting alone, machine belts off, 767 lbs.=1.39 horse-power. 3d. Frames and shafting, 6900 lbs.=12.54 horse-power.

Trial of power required for 112 looms, weaving 36-inc'l sheetings, No. 20 yarn, 60 threads to the inch each, warp and filling. Speed, 130 picks per minute. These looms are placed in the back part of the middle portion of No. 1 mill—one-half in the basement and half in the room above—being belted from 5 lines of shafting in the lower room. These shafts are driven in succession, one from the other, the first from the main line. Size of shafting, 2 3-16 inches, except the first piece in each line, on which the counter-pulleys are placed; these are of several different sizes, but about 2½ inch on an average. The driving pulleys are 12 inch diameter, and the loom pulleys 14 inch. 1st. 112 looms with shafting lubricated with tallow. Average of several trials: 8870 lbs.=16.13 horse-power =79 20 lbs. per loom=7.24 looms per horse-power. 2d. The same, after oiling the journals of the shafting: 8492 lbs.=15.44 horse-power=75 82 lbs. per loom=7.24 looms per horse-power. 3d. Trial of shafting and loose pulleys, lubricated with tallow. Average of several trials: 2876 lbs.=5.23 horse-power. 4th. Same after freshly oiling: 2245 lbs.=4.08 horse-power. 5th. Shafting alone, belts off: 913 lbs.=2.40 horse-power.

Trial of power required to drive 8 Lowell Machine Shop Mules, 624 spindles each, with Emerson's Dynamometer. Five mules were running on No. 22 yarn, spindles making 5500 revolutions per minute, and three mules on No. 37 yarn, spindles making 6230 revolutions per minute. 1st. The 8 mules including shafting. 12,250 lbs.=22.25 horse-power, =2 45 lbs. per spindle, =224 spindles per horse-power. 2d. Shafting alone, 17.10 lbs.=3.11 horse-power, =14 per cent. of the whole power. 3d. 8 mules without shafting, 19.16 horse-power=211 lbs. per spindle=260 spindles per horse-power.

### Test of Machinery at the Alpaca Mill, Holyoke, Mass.

Looms made by George Hatterly & Sons, Keighley, Yorkshire, England. These looms were supposed to require but one-tenth of a horse-power each to drive them; 250 of them in use there. Two sets of four each were tried, each set taking exactly the same power.

|  | H. P. |
|--|-------|
| Four looms (plain,) 40-inch reed space, 180 picks per minute,    | 1.13  |
| Spinning frame, 144 flyer spindles, 2500 revolutions per minute, | 2.60  |
| Lister Comb, 18 inch nip, combing long wool,                     | .68   |
| Preparer for comb, second of five, fair average of the set,      | .69   |
| Dandy roving frame, 24 spindles, 1300 revolutions per minute,    | .78   |
| Six spindle way box,   | .68   |
| Six spindle finisher,  | .56   |

Many patents have been taken out for the purpose of protecting devices supposed to produce very light running spindles, but there are spinning frames in this vicinity (with unpatented devices,) 128 spindles each that run lighter than any frames that I have seen elsewhere; these are driven with 5-8 of an inch belt, and can and have been driven with belts of but 1-4 of an inch in width.

## Test of Turbine and Power Required to Drive Machinery.

Clyde Bleachery, River Point, R. I.

To ascertain power required to drive machinery, the gate was opened until certain machines ran at speed, afterwards the power of the wheel was tested with the same gate opening, head and speed.

|  | H. P. |
|--|-------|
| 1st Test. Gate open 2 1-2 turns,<br>Driving shafting of mill and small pump.   | 15.47 |
| 2d Test Gate opened 6 turns,<br>One 5 bole water mangle, 1 Scotch starching mangle, 2 boles, 1 spindle calendar, 5 boles, 1 3-bole calendar, 1 5-bole calendar and 1 cloth winder.   | 53.18 |
| 3d Test. Gate opened 8 turns,<br>All the machinery in the bleaching room, viz: 3 washing machines, 10 feet log, 2 washing machines, 6 feet log, 2 souring machines, 4 feet log, 1 chemic machine, 4 feet log, 1 liming machine, 4 feet log, and 3 squeezers. | 62.73 |
| 4th Test. Gate opened in full,<br>All the above, with machinery in drying room additional. The latter is 1 drying machine, 11 cylinders. 30x120 inches, 1 squeezer, 1 opening mangle, 2 shearers. 4 sets knives each, and 1 Canroy winder.                   | 75.34 |
| The 15.47 h. p. required to drive shafting must be deducted from the second, third and fourth tests to get the power required to drive the machinery named.  |       |

Memoranda of power required for operating certain bleaching, finishing and dyeing machines, at S. H. Greene & Sons' Bleach and Print Works, Riverpoint, R. I., tested with Emerson's Lever Dynamometer, April 1874.

|   | H. P. |
|---|-------|
| Washing Machine with 2 boles—21 inches diameter. 10 feet long with squeezers attached; consisting of 2 boles—21 inches diameter, 12 inches long,                  | 13.60 |
| Limer, brown sour, chemic and white sour machines—2 boles each—21 inches diameter, 4 feet long, each required   | 3.01  |
| Water mangle—5 boles,   | 11.39 |
| Friction mangle—2 boles,  | 16.38 |
| Calendar—5 boles,   | 7.53  |
| Calendar—3 boles,   | 5.91  |
| Calendar—4 boles, (one bole being a 4-inch spindle,)  | 8.07  |
| Shearing machines—4 sets knives,  | 9.98  |
| Burrows' patent dye beck—40 ps.,  | 3.86  |
| Washing Machine, Madder Dye House, with 2 boles—10 feet long, 20 inches diameter, with squeezers—2 boles, 12 inches long, attached with cloth loose in water pit, | 7.97  |
| Hot water machines—2 boles, in dye house,   | 1.79  |
| Canroy Winder—for printing machines,  | 6.32  |
| Power to drive shafting and spring water pumps of bleachery, drying room and mangle, and finishing rooms for white work,  | 18.18 |

All the above were trials while the machines were at work. cloth threaded in. A number of trials were made. The above give the average in practical work.

HENRY L. GREENE.



## Tests of Various Kinds of Machinery.

During the past ten years I have tested the power required to drive a great variety of machinery, but have kept no record of such until recently, because such tests to others are of but little value unless the conditions are exactly the same, which is unlikely to be the case.

The following were taken in the mills named and represent the power required to drive the machines while doing their regular work; by the tests it will be seen that the greater the number of spindles in a frame, the greater the number is likely to be per horse power. It will also be apparent that much depends upon the make of the frame.

**DWIGHT MFG CO., CHICOPEE, MASS. J. W. Cumnoek, Agent, Nov. 1878.**  
MANUFACTURE SHEETINGS SHIRTINGS AND P. K'S.

|   |                   |
|---|-------------------|
| Test of Lan shear frame, 128 Rabbeth spindles.  |                   |
| To drive empty spindles, required   | 1.06 horse power. |
| To drive spindle and bobbin, without connection,  | 1 14              |
| Mean, from empty to full bobbins, required  | 1 30              |
| Revolutions of drum per minute,   | 810               |
| Computed revolutions of spindle per minute,   | 7800              |
| Revolutions of front roll,  | 72                |
| No. of yarn,  | 40                |
| Length of travers on bobbin in inches,  | 5                 |
| Foot lbs. per spindle when at work,   | 336 5             |
| Number of spindles per horse power,   | 98                |
| Another Rabbeth frame, supposed to be exactly like the above required more power. Spindles per horse power, |                   |
|   | 92                |

|   |                   |
|---|-------------------|
| Lowell frame, 202 light long spindles No. 4 mill.                             |                   |
| Mean, from empty to full bobbins,   | 2.52 horse power. |
| Revolutions of drum per minute,   | 1025              |
| Computed revolutions of spindles,   | 7800              |
| Revolutions of front roll,  | 97                |
| Length of travers on bobbin in inches   | 5¼                |
| Number of yarn,   | 22                |
| Foot lbs. per spindle,  | 412               |
| Spindles per horse power,   | 78                |
| To drive the cylinder and spindles, rolls stopped, required 1.96 horse power. |                   |

|   |                  |
|---|------------------|
| Lowell frame having 208 short spindles in No. 4 mill. |                  |
| Mean, from empty to full bobbins,                     | 3 31 horse power |
| Revolutions of drum per minute,                       | 1025             |
| Computed revolutions of spindles,                     | 7800             |
| Revolutions of front roll,                            | 97               |
| Length of travers on bobbin in inches,                | 5¼               |
| No. of yarn,  | 22               |
| Foot lbs. per spindle,                                | 525              |
| Spindles per horse power,                             | 63               |

These spindles were reduced in weight, then required 2.84 h. p. or 73.8 spindles per h. p. To drive the cylinder and spindles, the rolls being stopped, required 2.2 horse power.

|  |                   |
|--|-------------------|
| Lowell frame, (old) 208 long spindles. |                   |
| Mean, from empty to full bobbins,      | 3.54 horse power. |
| Revolutions of drum per minute,        | 1025              |
| Computed revolutions of spindles,      | 7800              |
| Revolutions of front roll,             | 95                |
| Length of travers on bobbins in inches | 5¼                |
| No. of yarn,                           | 22                |
| Foot lbs. per spindle,                 | 563               |
| Spindles per horse power,              | 59                |

|   |                   |
|---|-------------------|
| Whitin frame, 128 long spindles, in No. 1 mill. |                   |
| Mean, from empty to full bobbins,               | 1.45 horse power. |
| Revolutions of drum per minute,                 | 720               |
| Computed revolutions of spindles,               | 5040              |
| Revolutions of front roll,                      | 82                |

|  |     |
|--|-----|
| Length of travers on bobbin in inches, | 5½  |
| No. of yarn,                           | 14  |
| Foot lbs. per spindle,                 | 375 |
| Spindles per horse power,              | 98  |

Another frame, same row, supposed to be exactly like the above, carried 98 spindles per horse power.

|   |                   |
|---|-------------------|
| Bidd-ford frame, 144 long spindles, No. 5 mill. |                   |
| Mean, from empty to full bobbins,               | 1.57 horse power. |
| Revolutions of drum per minute,                 | 789               |
| Computed revolutions of spindles,               | 5523              |
| Revolutions of front roll,                      | 78                |
| Length of travers on bobbin in inches,          | 5¼                |
| No. of yarn,                                    | 22                |
| Foot lbs. per spindle                           | 359               |
| Spindles per horse power,                       | 73                |

|  |                   |
|--|-------------------|
| Biddeford frame, 144 Pearl spindles, No. 5 mill. |                   |
| Mean, from empty to full bobbins,                | 1.91 horse power. |
| Revolutions of drum per minute,                  | 797               |
| Computed revolutions of spindles,                | 7000              |
| Revolutions of front roll,                       | 92                |
| Length of travers on bobbin in inches,           | 5¼                |
| No. of yarn,                                     | 22                |
| Foot lbs. per spindle,                           | 439               |
| Spindles per horse power,                        | 75                |

|  |                   |
|--|-------------------|
| Whitin one rail frame, 128 Buttrick & Flanders' spindles, in No. 1 mill. |                   |
| Mean, from empty to full bobbins,  | 1.16 horse power. |
| Revolutions of drum per minute,  | 720               |
| Computed revolutions of spindles,  | 6720              |
| Revolutions of front roll,   | 100               |
| Length of travers on bobbin in inches,                                   | 6¼                |
| No. of yarn,   | 14                |
| Foot lbs. per spindle,   | 307.5             |
| Spindles per horse power,  | 107               |

Another frame in the same row supposed to be exactly like the above, required more to drive it only carrying 94 spindles per horse power.

|  |                   |
|--|-------------------|
| Biddeford one rail fram, 144 Buttrick spindles in No. 5 mill, using Pearl bobbins. |                   |
| Mean, from empty to full bobbins,  | 1.77 horse power. |
| Revolutions of drum per minute,  | 825               |
| Computed revolutions of spindles,  | 7300              |
| Revolutions of front roll,   | 98                |
| Length of travers on bobbin in inches,   | 5¼                |
| No. of yarn,   | 22                |
| Foot lbs. per spindle,   | 405               |
| Spindles per horse power,  | 81                |

|   |                   |
|---|-------------------|
| Biddeford two rail frame of 144 Buttrick spindles, using Pearl bobbins. |                   |
| Mean, from empty to full bobbins,                                       | 1.68 horse power. |
| Revolutions of drum per minute,   | 825               |
| Computed revolutions of spindles,                                       | 7300              |
| Revolutions of front roll,  | 98                |
| Length of travers on bobbin in inches,                                  | 5¼                |
| No. of yarn,  | 22                |
| Foot lbs. per spindle,  | 385               |
| Spindles per horse power,   | 85.5              |

Lowell Doubler, doffing 64 cards. Required, 4.28 horse power.

Howard & Bullock Slasher, 16 inch fans, making 1200 revolutions per minute. Yarn moving 35 yards per minute. Required, 5.04 horse power.

Lowell Machine Shop Looms. 12 on 36-inch goods, 64 picks per inch. 11 on 40-inch goods, 76 picks per inch, 145 picks per minute. Required, 4.08 h. p. or 5.6 looms per horse power.

Lowell Coarse Speeders, 40 spindles, .36 hank roving. Eight and half inch space, 12-inch travers. 1¼ roll, making 196 revolutions per minute. Flyers, 625 revolutions per minute. Required, 1.41 h. p., 117 foot lbs. per spindle or 283 spindles per h. p.

Intermediate, 56 spindles. .90 hank roving.  $6\frac{1}{2}$ -inch space. 9 $\frac{1}{2}$ -inch travers. Front roll,  $1\frac{1}{2}$  inches in diameter, making 200 revolutions per minute. Flyers 940 revolutions per minute. Required, 1.43 h. p., 340 foot lbs. per spindle or 89.2 spindles per horse power.

Fine, 72 spindles, 5-inch space,  $8\frac{1}{4}$ -inch travers, 2-83 hank roving. Diameter of front roll  $1\frac{1}{2}$ -inch, making 140 revolutions per minute. Flyers 1215 revolutions per minute. Required, 1.68 h. p., 783 foot lbs. per spindle or 42 spindles per horse power,

Two Drawing Frames, 3 to 1, 4 deliveries each. Roll  $1\frac{3}{4}$  inch diameter, making 308 revolutions per minute. Required, 1.09 horse power.

Two Pawtucket Spoolers, 80 spindles each, or 160 per pair. Revolutions of cylinder 165 and of spindles 785 per minute. No. of yarn 22, warp. Required, .74 h. p. Spindles per horse power, 217.

Five Howard & Bullock Warpers (English) Cylinder making 45 revolutions per minute. Width of section, 54 inches Average No. of threads to each warper, 350. Required, .83 h. p., or .16 h. p. per warper.

**CHICOPEE MFG CO., CHICOPEE FALLS, MASS. George H. Jones, Agent, Nov. 1878.**

**MANUFACTURE COTTON FLANNELS, QUILTS AND SHEETINGS.**

|  |                   |
|--|-------------------|
| Test of frame having 256 Sawyer spindles, in a mill of that company. |                   |
| To drive the empty spindles, required                                | 1.26 horse power. |
| To drive bobbins before connection with yarn, required               | 1.46              |
| Mean, from empty to full bobbins,                                    | 2.09              |
| Revolutions of drum per minute,                                      | 863               |
| Computed revolutions of spindle,                                     | 7612              |
| Revolutions of front roll,   | 88                |
| No. of yarn,   | 25                |
| Length of travers on bobbin in inches,                               | 5                 |
| Foot lbs. per spindle when at work,                                  | 269.6             |
| Spindles per horse power,  | 122               |

**WARP MILL, HOLYOKE, MASS. J. L. Burlingame, Agent, Dec. 1878.**

**MANUFACTURE WARPS.**

|  |                   |
|--|-------------------|
| Lowell Frame, 160 Sawyer spindles (old frame.) |                   |
| Mean power required                            | 1.87 horse power. |
| Revolutions of drum,                           | 860               |
| Calculated revolutions of spindles,            | 7166              |
| Revolutions of front roll,                     | 103               |
| No. of yarn,                                   | 18                |
| Travers on bobbin in inches,                   | $5\frac{3}{4}$    |
| Foot lbs. per spindle,                         | 387               |
| Spindles per horse power,                      | 85.2              |

|  |                   |
|--|-------------------|
| Another in same mill; New Lowell Frame, 160 Sawyer spindles. |                   |
| Mean power required  | 1.74 horse power. |
| Revolutions of drum,   | 935               |
| Calculated revolutions of spindles,                          | 7480              |
| Revolutions of front roll,                                   | 84                |
| No. of yarn,   | 28                |
| Travers on bobbin in inches,                                 | $5\frac{3}{4}$    |
| Foot lbs. per spindle,                                       | 358               |
| Spindles per horse power,                                    | 92.1              |

**HADLEY CO., HOLYOKE, MASS. William Grover, Agent, Dec. 1878.**

**MANUFACTURE YARN, THREAD AND TWINE.**

|  |                   |
|--|-------------------|
| Whitin Frame, 144 Buttrick spindles, ring $1\frac{1}{2}$ inches. |                   |
| Mean power required  | 1.58 horse power. |
| Revolutions of drum,   | 913               |
| Revolutions of front roll,                                       | 93                |
| Calculated revolutions of spindle,                               | 7606              |
| Travers on bobbin in inches,                                     | $5\frac{1}{4}$    |
| No. of yarn,   | 22                |
| Foot lbs. per spindle,   | 361               |
| Spindle per horse power,   | 91.2              |

Whitin Frame, 144 common long spindles, ring  $1\frac{1}{4}$  inches.

|                                     |                   |
|-------------------------------------|-------------------|
| Mean power required                 | 1.62 horse power. |
| Revolutions of drum,                | 940               |
| Revolutions of front roll,          | 87                |
| Calculated revolutions of spindles, | 6043              |
| No. of yarn,                        | 22                |
| Travers on bobbin in inches,        | $5\frac{1}{4}$    |
| Foot lbs. per spindle,              | 368               |
| Spindles per horse power,           | 90                |

Two Whitin Frames, 160 long light spindles each, or 320 spindles per pair.

|                                     |                   |
|-------------------------------------|-------------------|
| Mean power required                 | 2.60 horse power. |
| Revolutions of drum,                | 941               |
| Revolutions of front roll,          | 68                |
| Calculated revolutions of spindles, | 6761              |
| No. of yarn,                        | 40                |
| Travers on bobbin in inches,        | $4\frac{1}{2}$    |
| Foot lbs. per spindle,              | 268               |
| Spindles per horse power,           | 123               |

Whitin Frame, 144 Sawyer spindles, ring  $1\frac{1}{2}$  inches.

|                                     |                   |
|-------------------------------------|-------------------|
| Mean power required                 | 1.30 horse power. |
| Revolutions of drum,                | 926               |
| Revolutions of front roll,          | 78                |
| Calculated revolutions of spindles, | 7408              |
| No. of yarn,                        | 30                |
| Travers on bobbin in inches,        | $5\frac{1}{4}$    |
| Foot lbs. per spindle,              | 298               |
| Spindles per horse power,           | 111               |

Whitin 9-inch Slubber of 72 spindles, hank roving one-third.

|                           |                  |
|---------------------------|------------------|
| Mean power required       | .59 horse power. |
| Revolutions of roll,      | 95               |
| Revolutions of spindles,  | 582              |
| Foot lbs. per spindle,    | 268              |
| Spindles per horse power, | 123              |

Whitin Intermediate Frame, 120 spindles, hank roving  $4\frac{1}{4}$ .

|   |                  |
|---|------------------|
| Mean power required                         | .47 horse power. |
| One and one-eighth inch rolls. Revolutions, | 96.5             |
| Revolutions of spindles,                    | 850              |
| Foot lbs. per spindle,                      | 130              |
| Spindles per horse power,                   | 254              |

Whitin's Jack Roving Frame, 144 spindles, hank roving 15.

|   |                  |
|---|------------------|
| Mean power required   | .48 horse power. |
| Revolutions of roll, $7\frac{1}{2}$ . Diameter of same in inches, | $1\frac{1}{2}$   |
| Revolutions of spindles,  | 1086             |
| Foot lbs. per spindle,  | 110              |
| Spindles per horse power,   | 300              |

Whitin's Drawing Frame, 16 ends, 4 cans.

|                      |                  |
|----------------------|------------------|
| Power required       | .58 horse power. |
| Revolutions of roll, | 280              |

Fales & Jenks' Frame, 272 Rabbeth spindles, ring  $1\frac{1}{8}$  inches.

|                                     |                   |
|-------------------------------------|-------------------|
| Mean power required                 | 2.36 horse power. |
| Seven inch drum. Revolutions,       | 725               |
| Revolutions of front roll,          | 100               |
| Calculated revolutions of spindles, | 6767              |
| Travers on bobbin in inches,        | $5\frac{1}{2}$    |
| No. of yarn,                        | 20                |
| Foot lbs. per spindle,              | 286               |
| Spindles per horse power,           | 115               |

Another Fales & Jenks' Frame, 272 Rabbeth spindles, ring  $1\frac{1}{8}$  inches.

|                                     |                   |
|-------------------------------------|-------------------|
| Mean power required                 | 2.15 horse power. |
| Revolutions of drum                 | 725               |
| Revolutions of front roll,          | 73                |
| Calculated revolutions of spindles, | 6767              |

|                              |     |
|------------------------------|-----|
| No. of yarn,                 | 30  |
| Travers on bobbin in inches, | 5½  |
| Foot lbs. per spindle,       | 261 |
| Spindles per horse power,    | 126 |

Fales & Jenks' 1876, Twister, 248 Rabbeth spindles, two cylinders.

|  |                  |
|--|------------------|
| Mean power required                                      | 4.80 horse power |
| No. of yarn,   | 40—3 ply.        |
| No. of Traveler, 14. 2-inch ring.                        |                  |
| Diameter of drum, 8 inches. Revolution of same,          | 750              |
| Three inch roll. Revolutions,                            | 27¾              |
| Diameter of whirl, 1 5-16 inch. Revolutions of spindles, | 4562             |
| Foot lbs. per spindle                                    | 639              |
| Spindles per horse power,                                | 51.6             |

Two cylinders in the same frame can hardly be desirable

Fales & Jenks' 1872, Single Cylinder Twister, 144 Rabbeth spindles.

|   |                   |
|---|-------------------|
| Mean power required                                   | 1.74 horse power. |
| No. of yarn,  | 40—2 ply.         |
| No. of Traveler,                                      | 16                |
| Seven inch drum. Revolutions.                         | 823               |
| One and one-half inch roll. Revolutions of spindle,   | 43                |
| One and one-sixteenth whirl. Revolutions of spindles, | 5435              |
| Foot lbs. per spindle,                                | 400               |
| Spindles per horse power,                             | 82.5              |

Higgins' Sons & Co. Slubber, 60 spindles

|                           |                   |
|---------------------------|-------------------|
| Revolutions front roll,   | 118½              |
| Revolutions of spindles,  | 676               |
| Required                  | 1.02 horse power. |
| Spindles per horse power, | 68.6              |

Higgins' Sons & Co. 7-inch intermediate frame, 128 spindles, hank roving 3¼.

|                                       |                  |
|---------------------------------------|------------------|
| Mean power required                   | 1.58 horse power |
| Diameter of roll 1½ inch. Revolutions | 128              |
| Revolutions of spindles,              | 1118             |
| Foot lbs. per spindle,                | 408              |
| Spindles per horse power,             | 81               |

Higgins' Sons & Co. (English) 5½ inch Jack Frame, 144 spindles, hank roving 11.

|  |                   |
|--|-------------------|
| Mean power required                                  | 1.45 horse power. |
| Revolutions of roll, 83. Diameter of same in inches, | 1½                |
| Revolutions of spindles,                             | 1400              |
| Foot lbs. per spindle,                               | 333               |
| Spindles per horse power,                            | 99                |

English Twister, 286 Rabbeth spindles, 1½ inch ring.

|   |                   |
|---|-------------------|
| Mean power required                         | 3.97 horse power. |
| No. of yarn,                                | 36—2 ply.         |
| No. of Traveler,                            | 15                |
| Eight inch drum. Revolutions,               | 600               |
| Three inch roll. Revolutions,               | 23.5              |
| One and one-fourth inch whirl. Revolutions, | 2840              |
| Foot lbs. per spindle,                      | 458               |
| Spindles per horse power,                   | 72                |

Crighton & Son (English) Doubler, 16 ends, Lap 187 pwt. to the yard.  
Driving pulley, making 600 revolutions per minute. Required, .55 horse power.

Boyd's (Glasgow) Spooler or winding machine, 50 spindles or drums. One side winding from three bobbins; the other side winding from three cops.  
Driving pulley and drums, making 228 revolutions per minute.

|                           |                 |
|---------------------------|-----------------|
| Mean power required       | .15 horse power |
| Foot lbs. per spindle,    | 99              |
| Spindles per horse power, | 333             |

Pair of Dobson & Barlow (English) Mules, 832 spindles each.  
 Ten stretches in 4 minutes, 25 seconds.  
 Diameter of front roll, 1 inch. Revolutions of same per minute, 72  
 No. of yarn, 70. Calculated revolutions of spindles, 5663  
 Maximum force required, 7.83 horse power.  
 Spindles per horse power, 212.5

Pair of Mason Mules, 832 spindles each.  
 Ten stretches in 3 minutes, 55 seconds.  
 Revolutions of front roll, 78  
 No. of yarn, 70. Calculated revolutions of spindles, 6000  
 Maximum force required, 4.40 horse power.  
 Spindles per horse power 375

French Comber made by Hethrington & Sons, Manchester, England.  
 Making 62 strokes per minute. Required, .24 horse power.

Platt Bros' Jaek Frame, 144 spindles, hank roving.  
 Mean power required .73 horse power.  
 Roll 1½ inch diameter. Revolutions of same 61  
 Revolutions of spindles, 1181  
 Foot lbs. per spindle, 167  
 Spindles per horse power, 198

Kitson Picker (changed) using Whitehead & Atherton's.  
 Whipper beater.  
 Diameter of roll, 9 inches. Revolutions of same per minute, 8½  
 Revolutions of 24-inch whipper, 1130  
 Revolutions of 16-inch beaters, 1545  
 Revolutions of fans, 2000 and 1500  
 Yards of lap per minute, 6.86  
 Maximum force required, 10.24 horse power.

Whitehead & Atherton's Picker.  
 Diameter of rolls, 9 inches. Revolutions of same per minute, 8½  
 Revolutions of 24-inch whipper, 1070  
 Revolutions of 16-inch beater, 1380  
 Revolutions of fans, 1900 and 1340  
 Yards of lap per minute, 6.67  
 Maximum force required, 9.35 horse power.

Kitson's 2d Picker or Finisher.  
 Diameter of rolls 9 inch. Revolutions of same per minute, 7  
 Revolutions of 1st beater, 16-inch, 1475  
 Revolutions of 2d beater, 16-inch, 1410  
 Revolutions of fans, 1430. Yards of Lap, 5.5  
 Maximum force required, 7.8 horse power.

Whitehead & Atherton's 2d Picker or Finisher.  
 Diameter of rolls, 9 inch. Revolutions of same per minute, 7½  
 Revolutions of 1st beater, 16-inch, 1410  
 Revolutions of 2d beater, 16-inch, 1410  
 Revolutions of fans, 1374  
 Yards of lap per minute, 5.9  
 Maximum force required, 6.64 horse power.

The Kitson picker had a six inch belt, the Whitehead & Atherton a four inch; by timing the two and weighing laps, a difference of more than ten per cent. was found in favor of the Kitson, but this was done away with by soaping the pulleys and a belt of the Whitehead & Atherton machine. As arranged, for doing the same amount of work, each required the same power.



## THE EVOLUTION OF ONE OF EMERSON'S PATENTS.

We print herewith an article from the *Boston Advertiser* of Nov., 1889, describing a business that originated with James Emerson, of Willimansett, and which was under his control until 1860. He commenced in 1852.

The windlass was so radically different from all previous devices for the purpose, that it was laughed at by seafaring men, particularly naval officers, etc. Four years of persistent effort and a gift to an impecunious ship-owner gained the privilege of putting one on a ship. The war through the improvised battle ships from the merchant service introduced it into the navy. Perhaps some of the readers of this will recollect about a year since reading of the "Gov. Ames," a five masted schooner, being dismantled on the "Georges" and that her salvation depended on her windlass. The patterns for that windlass were made by Mr. Emerson or from his plans. A 2½ inch chain weighs 15 tons or 40 pounds to a link, the two chains and anchors 37 tons; the windlass has to sustain not only that weight but the entire strain the two chains will hold, and such chains often part and let vessels go ashore. Yet after nearly 40 years of continued labor upon devices for ships, mills, hydraulics, dynamics and steam heating devices, it is a pleasant thought that of the numerous lives and millions of property often dependent upon his judgment, no life nor serious loss of property has ever occurred.

The circular of Emerson, Walker & Thompson, of 11 Leadenhall street, London, Eng., of 1885, claims to have fitted up 6000 vessels with the windlass.

A little more than 12 years ago travelers across "Red Bridge," in the eastern suburbs of Providence, noticed a small wooden building erected not far from the bank of the Seekonk river. A modest sign over the door told that this was the new plant of the American Ship Windlass Co. The building soon became too small. In six months a second fully as large as the first went up by its side. The next year there was another enlargement and the next year still another. Thus, year by year, the plant has grown, until, at the present time the value of the land and buildings of the American Ship Windlass Co. is fully nine times that of the original plant. Extensions are still in progress, for the business is still increasing rapidly, and to-day the sound of the hammer is heard as a new building is in process of erection upon the site of the old. Its windlasses and capstans were well known, while they were manufactured under the old regime. As long ago as 1856 the Massachusetts Charitable Mechanics' Association\* awarded a gold medal to the Emerson patent windlass. The present American windlass is based upon the Emerson patents.

Since 1856 the windlass has received many medals and other awards from fairs and expositions and has always taken the highest award or prize offered for windlasses whenever exhibited. More than 20 years after the Emerson windlass received the gold medal of the Massachusetts Charitable Mechanics' Association, the same society again recognized its merits in a similar manner. A gold medal was also awarded it by the World's Industrial and Cotton Centennial Exposition held at New Orleans in 1884-5. The North, Central, and South American Exposition of 1885-6 granted to it the first degree of merit. The only award given for windlasses and capstans at the U. S. Centennial Exposition was granted to the American Ship Windlass Co.

The best proofs of the complete success of this windlass is found in the fact that the finest steam and sailing vessels afloat are fitted with these machines. The U. S. government has repeatedly recognized their merit. The new steel U. S. cruisers, the Chicago, Boston, and Atlanta are furnished with them, as are also the dispatch boat Dolphin, the Thetis, Bear, Baltimore, Vesuvius, Yorktown, and Petrel; the coast survey vessels Hassler and Blake; the lighthouse boats Haze, Dahlia, and Myrtle, and so great a number of the U. S. revenue cutters that to enumerate them would be to write almost a complete list of these vessels. Steamers of the Mallory, Pacific Mail, Ward's, Ocean, Clyde, Morgan, Old Colony, New Brazil, Cromwell, Norwich, Winsor, and many other lines, transatlantic and coastwise, are furnished with the "American" windlasses, which have always given the fullest satisfaction. At present at least 95 per cent. of the windlasses made and sold in the American market come from the works of the American Ship Windlass Co.

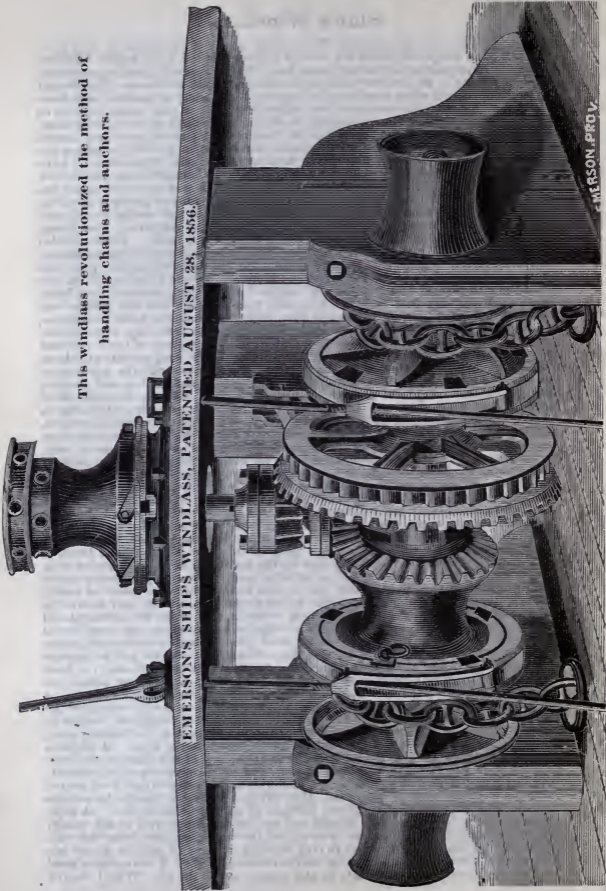
\*The same Association also awarded a gold medal to the Emerson Power Scale, an instrument that now has no competitor.

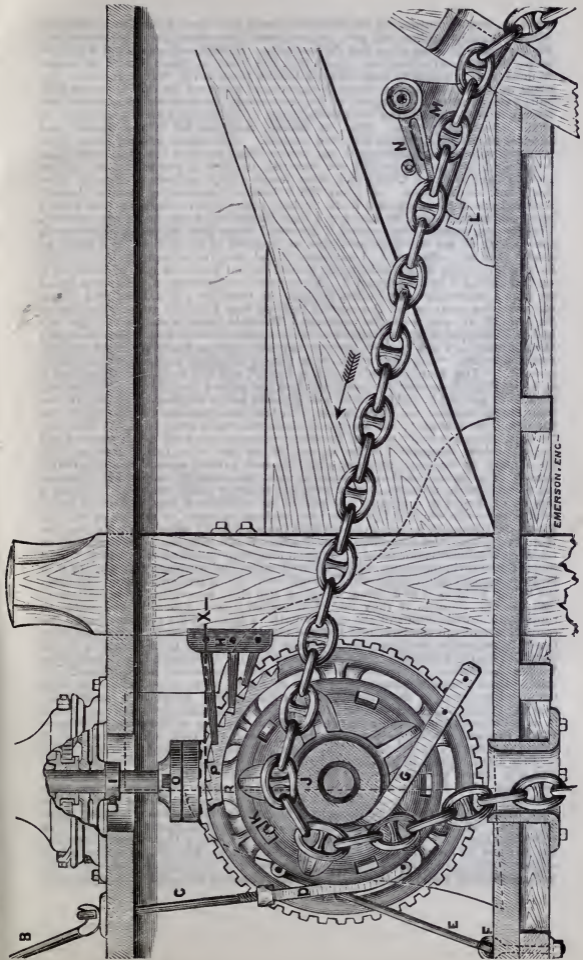
## Ship's Windlass.

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It has often happened, when low results have compelled me to report unfavorably of turbine plans, that the designers have intimated that if I had experienced the vicissitudes of an inventor's life, more leniency would be shown. The Patent Office Reports will show that quite a number and variety of patents have been granted to me, and the records of the office will show a still larger number of applications for others, some of which were rejected, others granted, then abandoned. Two causes have prevented me from realizing much pecuniary benefit from patents. First, because my inventions have been a generation before the age. Secondly, because my plans have been very expensive to develop. I have never cared to immortalize myself by the invention of a mouse trap, pie fork or clothes pin. One patent I have ever felt ashamed of; it was taken out under the following circumstances. A lady friend as a joke asked me to get up a device to keep her husband's mustache out of his coffee. A plan was readily found, consisting of a peculiarly shaped comb with guards and nippers. Two young ladies asked to have a patent taken out and assigned to them. It was applied for. The model proved so attractive that it was purloined, and the commissioner had to send for another; in the meantime, the man for whom the plan was devised took his comb to the Fifth Avenue Hotel, N. Y., and exhibited it; in less than a month several hundred dollars' worth of orders were received from fancy goods dealers. By that time the joke had become stale and the matter was dropped in disgust, though I believed then, and continue in the same belief now, that more money could have been made from that than from any other patent granted me. It is not my purpose to go into a general history of my inventions but there are several, now very popular and lucrative devices, patents of others, that were offered to leading men thirty years since by myself; the plans were pronounced chimerical. The self coupling for cars, steam brakes and heating cars by steam—the plans, almost identical with those now so common, were urged by me upon the managers of the several railroads as early as 1850, but in vain. My experience in introducing the ship's Windlass, herewith illustrated, will be sufficient to show my turbine friends that I have known something of an inventor's troubles. Readers who are not acquainted with such matters, may, by looking in "Webster's Unabridged," see an illustration of a ship's windlass; such as was in use on all merchant vessels of any size forty years since. Such windlasses were made of a single oak log, varying in length from six to twenty-five feet, according to the size of the vessel; three or four turns of the cable would be wound around the windlass, the inner or loose end of cable next to the bitt; in heaving in, the chain, like a nut or screw, would work towards the middle or pawl bitt, so that after a few turns the cable would have to be made fast forward of the windlass, then the three or four turns of the chain slipped back towards the bitt. The cables were stowed below by the mainmast in order to have a long stretch of chain back of the windlass to help hold it from slipping when icy or muddy. Now, by considering that the largest chain cables are made of round iron,  $2\frac{1}{4}$  inches in diameter, the links being eight inches wide and twelve in length—fifty pounds to each foot in length of chain, each cable five hundred and forty feet in length with an anchor of three tons in weight at the end—and it will readily be understood that a crew had a hard job to handle such a cable, more particularly in deep water; besides, it was often impossible to get an anchor ready to let go before a ship would be ashore, for it was always necessary to haul up sufficient length of cable from the chain locker to reach bottom before the anchor could be let go; for to drop a heavy anchor and chain in ten fathoms, or sixty feet of water and allow it to bring up on the windlass, would endanger the safety of cable, windlass or bows of the ship; consequently, sufficient length to reach bottom had to be ranged forward of the windlass as a preliminary step, the turns of the cable around the windlass adding much to the labor. A careless word drew my thoughts to the matter, and in 1850 some of the plans in the illustrations were presented to seafaring friends, and by them very coolly received: "What! Trust lives and such immense amounts of property to cast iron gears? might as well have a glass windlass. How are you going to handle the swivels and shackles, placed at every fifteen fathoms of cable?" said another. A capitalist offered to assist me, if a certain old sea captain approved of my plans; they were submitted to him; he was one of the old school, a regular old salt. He examined the plans, a model in fact, worked it, hove in and let go anchor for an hour; then got up, came to me and exclaimed: "Well, I have seen a good many d—d fools, but you seem to be the biggest one of the lot. What! do you

This windlass revolutionized the method of handling chains and anchors.







want to commit murder by the wholesale, with your d—d cast iron jimcrack? Why, let a ship anchor in a gale, and ship and crew would go to h—ll together.” My capitalist declined to go into the business. Finally, one was found willing to help; then the objection was raised that the links of cables varied in length so much that it would be impossible to handle them in the way proposed. My plans were modified, and a device designed and patented for obviating the difficulty; then an owner was found willing to furnish his ship with chains of a better make—the links being sufficiently equal in length to work on the *grubs* or chain wheels illustrated. This, of course, rendered all of the trouble and expense of the special plan patented useless. A windlass, costing some eight hundred dollars was constructed, but before being finished the ship owner had been frightened so that he did not dare risk its use; it was offered as a gift to Donald McKay, Paul Curtis and other leading ship builders of Boston, New York and other places. One day while listlessly wandering around, hoping against hope, I met a Captain R. B. Forbes, a man who through various causes had been flattered until he had got a high idea of the value of his own opinion. Timidly approaching him I asked if he would be so kind when passing by as to take a look at my windlass, and give an opinion of its merits. “What!” he said, “that big coffee mill? I have seen it and can give my opinion now; which is, that it is worth nearly a cent per pound for old iron, less cost of breaking it up and carting it to the foundry.” After months of waiting a place was found for it on a large ship being built at Kennebunk Port, Me. (Wm. Lord, Jr.) When the ship was ready to sail the captain insisted that I should go with the ship to St. John, N. B., and work the windlass. The tide there is strong and the ship had to be moored in fifteen fathoms of water; we arrived an hour before daylight; the morning dark and foggy; the port captain came on board and took charge. Some one said: “Captain, we have a patent windlass and expect to moore quick.” “The windlass ain’t worth a daum,” was the reply—he supposing it to be an English capstan that some one had put upon a few ships. A steam tug took us to our berth, and the order was given to let go starboard anchor. In less than three minutes we were riding with forty-five fathoms of chain out; the tug towed hard to port; the starboard chain was eased away to eighty fathoms; the port anchor was let go, and in twenty minutes we were safely moored and the tug called alongside for the captain of the port, who, before leaving, held his lantern to my face, grunting out, “d—ned yankee saved me half a day’s time.” The captain of the ship congratulated me as being sure of having made my fortune by the invention. But prejudice is not so easily overcome. To ask a builder or owner of a ship to use one of my windlasses, was certain to bring some sneer as to whether I proposed to send an engineer or machinist with it. Pilots and insurance agents were strongly opposed to it; after much urging one was placed upon the insurance agent’s steamer as a gift, the old windlass to be replaced if mine was not liked. Impecunious ship builders, who found it hard to get the old windlass upon credit, favored mine, and were ready to pay for it in large promises, and it was really through such that it gained a place. In time, the better builders would listen, but were still shy; an engineer was necessary, was the cry; besides, if they lost their cables it was generally impossible to replace them with others of the same length of link. This continued until the convenience of the windlass had become so apparent that commanders of ships began to importune for them. In the mean time, one had been placed upon the *Pomona*, ship of a thousand tons, belonging to the “Dramatic Line,” from New York to Liverpool. As those ships brought large numbers of immigrants, I had watched her proceedings closely because of what had been said about trusting lives and property to the strength of cast iron gears. Suddenly a rumor came that the *Pomona* had been lost, and that four hundred passengers had gone down in her; little was known, only that she had been wrecked on the coast of Ireland. It was two or three weeks before particulars were received, and in that time it seems as though I never slept. Four hundred lives were more of a responsibility than I felt capable of carrying in peace; but the time named brought relief. The ship struck before there was thought of danger. It may as well be stated here, that while I had control of the manufacture of the windlass, no loss ever occurred through its use; on the contrary, ships were often saved through the immense strain that could be brought to bear on the cables when heaving them off shore. In only a single instance was a tooth from a gear broken, and that was when two boat crews from a man-of-war was added to the ship’s crew for the purpose of heaving up the anchor, while it was a-foul of the man-of-war’s anchor; both were hove up together. The merits of the windlass had become so well established previous to 1860, that I had furnished that and other devices to

the Russian and Egyptian governments; had had orders from China, Spain, Italy, England, Scotland, and throughout this country wherever ships were built. The following certificates will show the change of opinion.

MASSACHUSETTS CHARITABLE MECHANIC ASSOCIATION, 1856.

Emerson's Patent Windlass, worked by slow or fast power by a Capstan on the forecastle. This machine can perform with four men, the work usually requiring a dozen, and is a valuable element in the safety of life and property, more especially in these days of "ordinary seamen." To this valuable machine the Committee award a *Gold Medal*.

R. B. FORBES,  
JOHN S. SLEEPER,  
BENJAMIN L. ALLEN,  
JOHN H. GLIDDEN,  
ELIAS E. DAVIDSON, } *Committee.*

BOSTON, April 10, 1860.

This will certify that after a careful inspection of Emerson's Patent Windlass, together with some acquaintance with its working on the steamer R. B. Forbes, we are satisfied that it is superior to any modern Patent Windlass that we have seen. It has great power and can apparently be used with ease and safety.

CHARLES PEARSON, }  
EBENEZER DAVIS, } *Marine Inspectors.*  
RICHARD BAKER, }

BOSTON PILOTS.

The undersigned, having known the Emerson Patent Windlass for several years, believe it to be superior to any Windlass in use. Its great power or speed renders it peculiarly applicable for getting under way in heavy weather, or where there is but little room, and the improved lever and screw nippers render it perfect for bringing a ship to.

JACOB K LUNT, SAMUEL C. MARTIN, JOHN T. GARDNER,  
H. A. TEWKSBURY, WM. F. TEWKSBURY, JONATHAN BRUCE, Jr.  
STEPHEN BURROWS, WM. CRISPIN, P. H. CHANDLER,  
ALFRED NASH. W. G. BAILEY, A. F. HAYDEN, ROBERT KELLY.

BOSTON, March 28, 1860.

MR. EMERSON:—Recently at the Cape of Good Hope, I had many chances to test the power of your patent Windlass. As I had both anchors down it was often necessary to heave up to clear the chains, and I have no hesitation in saying, that for power or speed, or for general convenience, your Windlass is far superior to any other that I have ever seen.

JAMES HALL,  
*Master of Bark Win. G. Anderson.*

MR. EMERSON:—I readily join Captain Hall in speaking of the satisfactory working of your patent Windlass on board the Wm. G. Anderson. I can say also, that the Windlass put by you on the bark Ethan Allen, has been very severely tested (the bark having parted her largest chain) and has given entire satisfaction. I recommend them to ship owners with great confidence.

BOSTON, March 28, 1860. EDWARD BOYNTON, Owner.

BUFFALO, December 10th, 1867.

CAPTAIN JAMES AVRELL. DEAR SIR:—I have used the Emerson Windlass purchased of you for the barque Annie Vought of Buffalo (one thousand tons), and have always found it work to my entire satisfaction. For strength, compactness and convenience, it cannot be excelled. Its motions are simple and positive, hence there is no lost motion; it does away entirely with the old tedious way of ranging chain before letting go anchor. With the Emerson Windlass the chains are always ready for letting go, and as a matter of great importance, can never get foul on the windlass, which is frequently the case with the old style windlass. Its power is unlimited. We had occasion to use our best bower anchor (3500 pounds), with 65 fathoms chain (13-4 bar link). It required only one man to let go anchor and veer away chain, whereas, with the old style windlass it would require the whole crew. And in heaving up, it required only 35 minutes till the anchor broke ground, then half our crew (five men) were sufficient to work the windlass, leaving the others free to work the yards, make sail, or be wherever required. It is superior to any windlass I have ever seen in use, and would unhesitatingly recommend its general adoption for large class vessels especially.

Respectfully, JAMES G. ORR, Master Barque Annie Vought.

Commodore Stringham and Gregory were very friendly and aided me in many ways as did several of the naval constructors; with others, John Lenthal, chief of the bureau of construction at the navy department; but the prejudice was too strong to allow of the use of my windlass on naval vessels. "If we should lose a chain in some out of the way port, we could not replace it, perhaps, with anything near what would be required." So I went to work and got up a plan that would take any sized chain, spending much time and money in doing it; then carried it to



the naval constructor who had been the strongest in that objection. "By George! that is simple, I didn't think it could be done; but, after all, the other plan is best; a chain is not often lost," was his comment. Such was the frivolous treatment experienced for years. Owing to the war, many merchant vessels having my windlass in use were turned into naval or war vessels. The following certificate will show how the windlass answered its purpose:

U. S. STEAMER SOUTH CAROLINA, OFF GALVESTON, Aug. 20, 1861.

STATE:—In accordance with instructions from Flagg Officer Mervine, which direct me to inform the Department as to the merits of the "Emerson Windlass," now in use on board this vessel, I have the honor to report that it has been used by us constantly for the past three months, and that our opportunities for judging of its utility have been amply sufficient. We find it certain and quick in its operations, not only in heaving in, but also in veering; it is strong and compact, taking up less room than any thing of the kind I ever saw. In fact, it reduces the tedious, old fashioned, and I may say, often dangerous way of handling our heavy anchors and chain cables, to the simple process [in heaving up] of walking around with the capstan, the chain taking care of itself as it comes in; while in veering, a small "plug" is removed, leaving the whole control of the heaviest chain in the hands of one man, who by the aid of a "lever" on a friction band, manages it with perfect ease. Besides, it is always ready. I have been lying with fifteen fathoms of chain out, on several occasions, and have, without giving previous notice to any one, been under weigh and steaming along at the rate of four knots, in five minutes after the order was given to man the capstan. It will be seen, therefore, that the facility thus afforded for getting underweigh is a positive saving of fuel in a blockading steamer, for otherwise, she might deem necessary, for entire efficiency, to keep underweigh almost all the time.

Respectfully, I am sir, your obedient servant.

JAMES ALDEN, Commanding U. S. Steamer South Carolina.

Hon. GIDEON WELLES, Secretary U. S. Navy, Washington, D. C.

In 1858 there was no chain making in this country, our cables all being imported. The following circular will explain itself. The lengths named were readily adopted, and I presume still continue to be the standard lengths.

TO CHAIN MANUFACTURERS OF GREAT BRITAIN. *Gentlemen*:—Being engaged in the manufacture of Windlasses which hold the chains by the links instead of by a turn around the windlass, I often find a great difference in the length of links of the different manufacturers' chains. This seriously affects the working of the windlass, and is sometimes very inconvenient in replacing a lost chain. As this kind of windlass and capstan is fast taking the place of the wooden windlass, it would be much better to have some regular length of link for each size chain. I herewith give a graduated scale of lengths for different sizes, which is very near the same as the scale of the Messrs. H. Wood & Co. of Liverpool; it, however, is a little more even than theirs. The shackle is another cause of difficulty. These should be made so that the inside of them, that is from the inside of the bolt to the inside of the other end, should be the same length as the inside of a link, and then the shackle link in the end of the chain which the bolt of the shackle goes through, should be long enough to make up for the butt of the shackle. There should be a long link at one end only, of each piece of chain, which should be for the bolt end of the shackle. There should also be a good swivel next the anchor shackle in all cases.

JAMES EMERSON.

| Inches. | Stud Link. | Length. | Inches | Short Link. | Length |
|---------|------------|---------|--------|-------------|--------|
| 1       | .          | 5 7-8   | 1-2    | .           | 2 3-8  |
| 1 1-16  | .          | 6 1-4   | 9-16   | .           | 2 3-4  |
| 1 1-8   | .          | 6 1-2   | 5-8    | .           | 3      |
| 1 3-16  | .          | 6 3-4   | 11-16  | .           | 3 1-4  |
| 1 1-4   | .          | 7 1-8   | 3-4    | .           | 3 1-2  |
| 1 5-16  | .          | 7 3-8   | 13-16  | .           | 3 7-8  |
| 1 3-8   | .          | 7 3-4   | 7-8    | .           | 4 1-8  |
| 1 7-16  | .          | 8 1-8   | 15-16  | .           | 4 3-8  |
| 1 1-2   | .          | 8 1-2   | 1      | .           | 4 5-8  |
| 1 9-16  | .          | 8 7-8   | 1 1-16 | .           | 5      |
| 1 5-8   | .          | 9 1-4   | 1 1-8  | .           | 5 3-8  |
| 1 11-16 | .          | 9 5-8   | 1 3-8  | .           | 5 3-4  |
| 1 3-4   | .          | 10      | 1 1-4  | .           | 6 1-8  |
| 1 13-16 | .          | 10 1-4  |        |             |        |
| 1 7-8   | .          | 10 1-2  |        |             |        |
| 1 15-16 | .          | 10 3-4  |        |             |        |
| 2       | .          | 11 1-8  |        |             |        |
| 2 1-8   | .          | 11 3-4  |        |             |        |

Our views correspond with the above.  
 FEARING, THACHER & Co.,  
 WHITON, BROWNE & WHEELWRIGHT,  
 BAXTER & SUMNER,  
 J. NICKERSON & Co.,  
 J. BAKER & Co.,

BOSTON, August, 1858.

Imp'ters of Chain Cables, Anchors, &c.

## THE AMERICAN SHIP WINDLASS COMPANY.

The following article copied from the Boston Commercial Bulletin of August 24, 1878, will show what has become of my windlass: "The American Ship Windlass Company, of Providence, R. I., seems to be a good illustration of the results which are achieved at the present day by division of labor, and by the devotion of all the skill and capital of an entire establishment, as far as practicable, to a single branch of manufacture. The productions of this company, comprising windlasses for every size and class of vessels, have attained a marked degree of excellence, and at our Centennial Exposition they received the only award given for windlasses and capstans.

The American Ship Windlass Company was established in 1857 and incorporated in 1860, and up to the present time, they have made nearly 3000 windlasses. John Roach & Son, of Chester, Pa., use their windlasses exclusively, putting them into all their vessels. Nearly all of the United States revenue cutters are now provided with them.

The company are now building windlasses for vessels which are being constructed at all of the different points along the coast of Maine, and for the steamers "Miantonomo," and "Puritan," which John Roach & Son have now in process of construction at their yard, and Wm. Cramp & Sons, of Philadelphia, are putting in the American Company's windlasses upon the steamers which they have built for the Russian Government.

The windlasses of the American Company are made to be operated either by hand, messenger chains or steam, and six different kinds of windlasses are manufactured for either of these motors. The windlasses are also made in eleven different sizes, for cables varying from  $\frac{1}{2}$  inch to  $2\frac{1}{2}$  inches in size; and the company are consequently able to provide windlasses for the smallest yachts as well as for the largest ships. Their works are model ones and are supplied with all of the latest and most improved machinery and other appliances, including many tools specially designed and constructed for the company. They are located on East River Street, near the Red Bridge, and are under the active management of Frank S. Manton, agent, and George Metcalf, treasurer; and one evidence of the executive ability of the managers is the perfect system which pervades the establishment throughout.

## Hydraulic Mortars and Cements.

Certain limestones, which contain upward of 10 per cent. silica, possess the property, when burned, of forming a cement or mortar which hardens under water. Such limestone is called hydraulic lime, and the mortar is called hydraulic mortar. This stone, before burning, consists of a mixture of carbonate of lime and silica, or a silicate, chiefly a silicate of alumina. The latter is insoluble in hydrochloric acid, hence remains undissolved when the stone is treated with this acid, but in burning this silicate is fluxed by the alkaline carbonates and becomes soluble in acid, the carbonic acid being expelled. When common lime is slacked it swells enormously and develops a great deal of heat; this is not the case in slacking hydraulic lime, which absorbs water without any considerable increase of temperature.

If ordinary lime be mixed with a suitable quantity of silica or sand, an artificial hydraulic mortar is obtained, to which we apply the name of cement. These cements may be either natural or artificial. The former are found in volcanic regions, having been produced by the terrestrial heat. Pozzuolana, found at Pozzuoli, near Naples, is a natural cement of the following composition: Silica, 44.5; alumina, 15.0; lime, 8.8; magnesia, 4.7; oxide of iron, 12.0 (with oxide of titanium); potash and soda, 5.5; water, 9.3; total, 100.8.

The quantity of lime, is, however, so small that it requires to be mixed with ordinary lime to form hydraulic mortar. It was employed in combination with an equal quantity of lime in building the Eddystone Lighthouse.

Artificial cement, also called "Roman cement," has been manufactured in England on the Thames and in the Isles of Wight and Sheppey, since 1796. It is made by burning the calcareous nodules which overlie the chalk in that country. A sample analyzed by Michaëlis contained: lime, 58.38; magnesia, 5; silica, 28.83; alumina, 6.40; oxide iron, 4.80. When mixed with water it hardens in fifteen or twenty minutes, and possesses great firmness and strength.

Portland cement was patented in England by Joseph Aspdin in 1824. He took the limestone of Leeds, pulverized and burned it, then mixed it with water and an equal weight of clay to a plastic mass. When dry this was broken up

and burned again until all the carbonic acid was expelled. It was then pulverized and ready for use. Pasley made it from chalk or limestone with Medway river clay, which contains salt. Pettenkofer suggests that cement is improved by soaking the clay in salt water.

Portland cement is now made, says Wagner, by making bricks of an intimate mixture of limestone and clay, drying them in the air and burning them in a tall shaft furnace from 45 to 100 feet, 12 feet in diameter, with a strong grate 4 feet from the bottom. It is charged with alternate layers of coal and cement stone. The properties of the cement are largely dependent on the temperature employed in burning; a white heat is best, but if the temperature is too high it will no longer unite with water, and may even be melted to a glass. If the temperature does not exceed a red heat it unites readily with water and gets hot like ordinary lime, but possesses very little strength. The color changes with the burning and forms a criterion for judging the quality. In normal condition it forms a gray, sharp powder, with a shade of green, but not glassy.

The manufacture of Portland cement is now carried on in every part of the world where limestone and clay are to be found. In order to obtain a good cement, not only must the proper heat be employed in burning, but the proper proportion of clay, usually 25 per cent., must be used, and the clay must have certain properties, such as a large proportion of silica, must be very finely divided, and must be very intimately mixed with the limestone. Analysis of Portland cement from various sources show the percentage of lime to vary from 55 to 62; silica, 23 to 25; alumina, 5 to 9; oxide of iron, 2 to 6; soda and potash, usually less than 1 per cent.

## Horse Power and other Matters.

When Watt began to introduce his steam-engines, he wished to be able to state their power as compared with that of horses, which were then generally employed for driving mills. He accordingly made a series of experiments, which led him to the conclusion that the average power of a horse was sufficient to raise about 33,000 lbs. one foot in vertical height per minute, and this has been adopted in England and this country as the general measure of power.

A waterfall has one-horse power for every 33,000 lbs. of water flowing in the stream per minute, for each foot of fall. To compute the power of stream, therefore, multiply the area of its cross section in feet by the velocity in feet per minute, and we have the number of cubic feet flowing along the stream per minute. Multiply this by 62½, the number of pounds in a cubic foot of water, and this by the vertical fall in feet, and we have the foot-pounds per minute of the fall; dividing by 33,000, gives us the horse-power.

For example: a stream flows through a flume 10 feet wide, and the depth of the water is 4 feet; the area of the cross section will be 40 feet. The velocity is 150 feet per minute— $40 \times 150 = 6000$ —the cubic feet of water flowing per minute. The fall is 10 feet;  $10 \times 375,000 = 3,750,000$ —the foot-pounds of the waterfall. Divide 3,750,000 by 33,000, and we have 113.63 h. p., as the power of the fall.

The power of a steam-engine is calculated by multiplying together the area of the piston in inches, the mean pressure in pounds per square inch, the length of the stroke in feet, and the number of strokes per minute, and dividing by 33,000.

Water-wheels yield from 50 to 91 per cent. of the water. The actual power of a steam-engine is less than the indicated power, owing to a loss from friction; the amount of this loss varies with the arrangement of the engine and the perfection of the workmanship.

To compute the number of teeth in a pinion to have any given velocity. Multiply the velocity or number of revolutions of the driver by its number of teeth or its diameter, and divide the product by the desired number of revolutions of the pinion or driven.

To compute the diameter of a pinion, when the diameter of driver and the number of teeth in driver and pinion are given. Multiply the diameter of driver by the number of teeth in the pinion, and divide the product by the number of teeth in the driver, and the quotient will be the diameter of pinion.

To compute the number of revolutions of a pinion or driven, when the number of revolutions of driver and the diameter or the number of teeth of driver and driven are given. Multiply the number of revolutions of driver by its number of teeth or its diameter, and divide the product by the number of teeth or the diameter of the driven.

To ascertain the number of revolutions of a driver, when the revolutions of driven and teeth or diameter of driver and driven are given. Multiply the number of teeth or the diameter of driven by its revolutions, and divide the product by the number of teeth or the diameter of the driver.

## WHAT IS POETRY ?

The best explanation that occurs to me may be found in Paine's Age of Reason; but what seems poetry to one may seem trash to another. The gloomy Puritan liked that of the "Hark from the tombs" order, while the unperverted nature admires something more human.

Popularity has much to do with the average taste in poetry as it has with dress.

We often see in some standard print an essay, say by Jonathan Dubkins, bursting with admiration for the versatility of Shakespeare's works, or of the intense beauty of Milton's Paradise Lost; but it is rare to find a copy of either that seems much worn, while the popular seal skin cloak or an imitation may be seen upon the form of every girl or woman that can procure it, from which fact it would almost seem that the pretense of admiration for those authors is less than claimed, and that the purpose of such essays is more to display the greatness of the Dubkinses than those written of.

For myself, admiration for poetry only comes as it touches my feelings, and it may be found in prose as well as in verse; much of the book of Job seems poetry to me. I would sooner be the author of Pope's Essay on Man, than of any other English work, because I believe it to be an inspiration from a higher source, as I also do of Uncle Tom's Cabin.

Ninety-nine per cent. of the pretended admiration for Shakespeare, Tennyson, and many other popular heroes, may justly be attributed to pure flunkeyism. It is true that many popular sayings may be found in works of Shakespeare, and equally true that the same may be found in works written two thousand years ago. The Comedy of Errors is taken in the lump from Plautus Comedies, the two Dromios being added to bring it down to an Englishman's idea of humor. There may be immense invention in his works, but such have not caught my attention.

"'Tis not so deep as a well, nor so wide as a church door; but 'tis enough, 'twill serve: ask for me to-morrow, and you shall find me a grave man," may be witty, but certainly is not common with those wounded to the death, any more than it is for those in deep sorrow, as were Juliet and her nurse, to make puns, and dirty puns at that.

The author of a dime novel would scorn the conception of such wretched stuff as makes up the Taming of a Shrew.

Lavinia, in Titus Andronicus, is certainly a marvelous creation. A young lady of our time having her tongue cut out and hands cut off would feel sick, to say the least; not so with Shakespeare's maiden, "*Good uncle Marcus, see how swift she comes!*"

Shylock has been a butt for general execration, but in excuse it should be borne in mind that for centuries his people had, through superstitious prejudice, been treated worse than the dogs of the street, and it is hardly to be wondered at that he turned upon one of his oppressors. The sagacity of Portia was not phenomenal.

## LISLE THREAD.

Lisle thread proper is prepared from *pure cotton*—the finest staple that can be had, the best quality of Sea Island being generally used. However, of late years it has been found by observation and experience that the softness and pliability necessary to the easy and safe working of this yarn or thread in hosiery and glove frame, as well as in the machinery making fine imitation laces of it, are best secured by the use of South American (Pernambuco) cotton, the latter being less harsh, softer, more elastic and regular in fiber, as well as being very fine in quality. The peculiarity of this thread, says the *Economist*, is its hard finish and the peculiar twist or manipulations which it undergoes before being ready for use. Each thread or strand passes through a flame, which divests it of all attaching fiber. This thread is also more elastic than the finest linen thread and breaks less. It also gives the finished article a more brilliant appearance, and is less costly than the latter. It derives its name from Lisle, a town in France, where it was first manufactured to a large extent, and, like many of the industrial arts, was originally brought from the East. It is now not only extensively produced in France, Belgium, and in

other portions of Continental Europe, but in Great Britain as well, and is sometimes called "Scotch thread," when made in that country, in contradistinction to that made on the Continent. It is not only used largely for gloves, hosiery, and trinnings, but also quite extensively in the manufacture of imitation laces, embroideries, etc. We believe some few years ago a suit was before the United States court of this district, which involved the question of what constituted Lisle thread gloves, and was decided in favor of the importer, who proved that Lisle thread proper was made of the purest and finest cotton, and not of flax, as some maintained who had not investigated the subject of its manufacture. As far as we can learn, none of this thread is made in this country, although we understand attempts have been made to manufacture it, but from the cost and light demand prevailing were abandoned. The imports of it are also light, being confined chiefly to a few of our hosiery manufacturers.

*En passant* it may not be amiss to state that all the dictionaries fail to give a definition of the word "Lisle," which is not in reality the proper word after all, but a corruption of L'Isle, Ryssel, in the French Netherlands (called the island, from its standing in a kind of lake formerly; but the waters are now drained off), situated in east longitude 3°, latitude 50° 42', on the river Deule, twenty-five miles north of Arras, and twelve miles from Tournay. It is a large, populous city, the capital of French Flanders, beautifully built, and was once strongly fortified. It has been noted for its silk manufacture, and fine linen or cambric, which have been made to great perfection there, as well as for its camlets, which are much admired.

## PROTECTIVE TARIFF.

Of all the fallacies that ever became embedded in the brain of an intelligent people, none was ever greater than the idea that high protective duties will permanently help the manufacturer and employee. In all highly protected countries, wages are low and manufactures primitive. We at times see children phenomenally precocious in growth or intellect, but such usually die young or shrink below the average; so of manufactures, if the profits are large, home competition keeps pace, each tries to produce at the least cost without regard to real quality so long as shoddy can be made to appear fair on the surface.

Combinations are formed by which the lowest class of help can be brought in to compete with our native employees. Through this combination workmen are transported from Bremen or Liverpool to Chicago, for ten dollars. Inventors, who have done so much in advancing the country's prosperity, have little chance comparatively under such conditions. Manufacturers will not bother with new devices while their profits are from twenty-five to a hundred per cent. Necessity is the mother of invention. Free competition is productive of efforts to excel in devices that enable the production of the best goods at the lowest cost. If protection is right for the manufacturer, then the employee should be protected by a high duty on imported labor.

## FIRE ESCAPES.

Constant travel with its concomitant hotel experience has brought me into proximity with many styles of fire escapes, but the only kind I believe to be reliable are the balconies or towers with fixed iron stairways; but such stairways should never be placed against windows through which the fire from the inside can flash out upon them. I think where there are adjoining buildings of the same height it will always be well to have stairs from the upper stories of hotels and manufactories lead upwards to walks leading along the roof to the other buildings for the employees to escape upon.



## TIDE POWER.

Tide power once quite common in this country when land and space was of little account is now hardly known though often called to mind by the various trade papers.

It has seemed to me that where the rise and fall of the tides is considerable large tanks as weights might be made to develop convenient power for light manufacturing purposes at little expense if properly suspended.

## MEDDLING WITH THE MAILS.

I think up to the time of Postmaster-General Holt the mails had been considered sacred, to be used by all unquestioned. Slavery had then become rampant and a demand was made that all matter inimical to that barbarism should be searched for and excluded; a subservient North yielded. Since then Anthony Comstock in the interest of a hierarchy, a twin barbarism, has insisted upon deciding what shall and shall not be excluded. Suppose some intelligent person should insist, as well might be done, that the Bible, Shakespeare's works, and plenty others should be excluded. There could only be another travesty of trial, as in the George Train case, or the Bible and many popular works would have to go. Who is to say where the exclusion is to stop?

The better way is to follow the Creator, serve all alike and allow no meddling whatever with the mails.

Before trying to purify the world by law, first purify the law, so that it may not be necessary for a coterie of old grannies at Washington, four years behind their work, to brood over the decisions of Alfred the Great or Edward the Little in order to ascertain whether John Doe or Richard Roe owns a stray jackass.

Blot out all laws once in twenty years, re-enact the few necessary, then select judges from the most intelligent men or women, never from lawyers. Make the law conform to the right; faugh! law and plows of Edward's time.

## CHOOSING ALL OFFICIALS BY THE PEOPLE.

Members of Congress are chosen and paid for doing certain specific duties. Why are they allowed to spend so much time electioneering for themselves and others, and what business have they to meddle with appointments? What right has a president or other official to appoint to an important office one who has been rejected by his own constituents? We have ten officials where one would be better, and nominally the highest are selected because they can be used rather than for their ability—fourth rate men. Who can remember who was governor of this state three years since?

Why not elect all officials, from president down, directly by the people, elect yearly, have but few, and make those responsible? Have it understood that such officials are really servants instead of masters. Eschew lawyers generally, take business men, but for merit. Allow no official consecutive re-election, high or low.

## UNDESIRABLE NAMES AND FLUNKYISH TITLES.

Owing to fanaticism, predilection, interested motive, or lack of taste, parents often load children down with names that prove an incubus through life; as such children become legally responsible at a fixed age, why not at that time make it customary for children to select names to suit? Think of being loaded down with Peleg, Ichabod, Nehemiah, etc., etc.

Why has the publication of a newspaper become so low a business that the editor now prefers to be called colonel rather than editor?

Why does any man of brains desire to be known by any prefix or suffix to his name?

Think of Mr. Washington, Abraham Lincoln, Esq. or Ph.D., Prof. Benjamin Franklin, Royal Lightning Catcher to her Majesty, etc. It would seem that the smaller the mind the greater the desire for titles.



## ADULTERATIONS AND SHORT MEASURES.

Adulteration of almost every commodity sold is now so general as to hardly cause comment. The same is the case with goods sold by the piece as so many yards, or so many articles in packages.

Why not make a law to confiscate all such goods wherever found?

## THE REPUBLICAN PARTY.

As I have never desired office my vote has invariably been cast for what to me has seemed to be for the best result.

I voted for Fremont, and for Lincoln twice, and still believe that the latter was the best man ever elected to the presidency. The abolition of slavery was caused by the spontaneous rising of the masses to blot out an institution of such barbarism. Nominally it was done as the Republican party, but men of all parties united for that purpose, then withdrew as it was accomplished; it was then the residuum crystallized into the real Republican party, a party for power and plunder. Its carpet-bag governments were the reproach of the civilized world.

The North was quite as much to blame for the rebellion as was the South, and the settlement should have been magnanimous and universal, instead of which the small minded leaders made heroes of Jeff Davis and others. Grant was nominated for president, not because the party believed him a hero, statesman, or republican, but because the leaders expected to ride into power on his popularity. And here it may be stated that a great wrong has been done to the earlier generals who really took the brunt of the fighting, in giving so much credit to Grant and Sherman, but it is a fact worthy of notice that their greatest eulogists now were called copper-heads during the war. From the beginning the party has been honey-combed with corruption up to the present time. Its carpet-bag governments, its stealing of the presidency, its outrageous pension acts for selfish influence, its gerrymandering of congressional districts, its favoring of monopolies, its numerous commissions for the centralization of power, the giving of a cabinet office as a reward for a corruption fund, its unseating of members and admissions of unpeopled states for party purpose regardless of honor, honesty, or the country's welfare, show that the party is under the control of a class unworthy of respect. The selfish, downward tendency of the party is well represented by its known men.

Henry Wilson went first for Henry Wilson, then for the Republican party, leaving as residuary legatee the country. George D. Robinson goes first for George D. Robinson, second for George D. Robinson, and as residuary legatee, George D. Robinson.

May the shadow of the Republican party become less and a better take its place.

## THE NORTH POLE.

As some years have passed since any expedition has been sent out to look for that long-sought but yet unreachd place, it is likely some ambitious country, institution, or person will soon be urging the matter upon the notice of the public, and I will suggest a plan that to me has long seemed practicable.

It is to construct fifty houses of light, non-conducting but strong material, to be sent in parts in ships, as far north as possible, to be put together on the ice and placed upon runners. The ice there is undoubtedly rough, but boats with few hands, and those in feeble condition, have been moved long distances. Sledges for the transportation of coal, food, clothing, bedding, and oil for lights should be provided in plenty, with plenty of men to handle them. A house accompanied by the sledges should be started, and continue north, then return to repeat the operation. Several gangs should be employed so as to work and rest alternately; stations twenty miles apart would insure relief and safety and give confidence. I believe road engines might be made to do the leveling of rough ice, and drawing the houses and sledges.

Of course this would require a million or more of dollars, but there are plenty of men in the country that could easily furnish all the necessary cash and not mind it, or the country could easily do it. If younger, such a job would suit me to a dot. Who of our millionaires will undertake it instead of endowing some college of which we already have more than are needed?

## EVOLUTION.

Evolution is an idea as old as history and was well considered in Chambers' "Vestiges of Creation" long before Darwin rode the hobby. That man evolved from the monkey is an old idea and one of the earliest that I can remember to have heard expressed, uttered by a hard-shell Baptist minister who cobbled shoes week days and preached Sundays under the inspiration of rum and molasses.

"The survival of the fittest," good in itself, offers no proof of evolution though it may of progression.

The mollusk of the earliest times is the mollusk of to-day. The old idea that man contains the pith of every previous product is perhaps correct, and to me it seems reasonable that the spirit or germ of life may evolve step by step from the lowest to the highest, also that man may so stultify his intellect that at the change called death his spirit will naturally gravitate to the body of a flea in order to find a suitable home. As for physical evolution it will be time to believe in that when a single instance in proof can be offered.

Progression will be more rapid when the brawling multitude that think but little yet invariably condemn everything out of the ordinary rut, think more and object only from conviction, and less credit is given to those who brood upon eggs that never hatch. What good ever came from the brooding of an old monk sitting in a dark cell or cave, or a dervish sitting upon the top of a column? Thought, like steam heat, to be useful requires ventilation. There are plenty who thus sit and brood, look profoundly wise and think that they *think*.

The prefix of professor, or any title added to a name, is more than likely to be the reverse of a guarantee of ability.

## DIET.

As it was a rule in ancient times for those who had been sick to publicly state how they had been cured that others might benefit thereby, I will state how for nearly a half century I have lived without being sick.

First, my diet has always been spare, at the same time I have invariably eaten anything that I have desired and at any time without any regard to regular hours, often at midnight or later if restless; a piece of mince pie or a biscuit well buttered soon brings sleep to me. Very little meat, pork never, raised bread is an abomination to me. Hot biscuit, hot doughnuts, pies of all kinds, puddings, strawberry short cakes, buckwheats, fruit, and a few of the ordinary vegetables constitute my ordinary meals, with hot tea or coffee, no liquor, beer, or tobacco in any form.

Think of firing a boiler three times a day instead of as required.

## Notes on Water Flow, &amp;c.

## NOTE FIRST.

Water, like all other bodies when in motion, dislikes to change the direction of that motion and this resistance to change increases with the square of its velocity. For instance, to turn a quarter circle in a pipe which is bent on a circle of ten times its own diameter, requires additional force or "head"; when the water moves but one foot per second; this additional head is but the one-thousandth of a foot, but at a velocity of ten feet per second the resistance is one-tenth of a foot head (100 times as much), this is an easier bend than is generally found in mill work; when the circle is  $2\frac{1}{2}$  times the diameter of the pipe this resistance is double; and here begins the heavier resistance, for from this to turning a square corner it has increased to 16 times that first noted; and as will be easily seen, in the case of short turns with high velocity, destroys much of its power.

One of the commonest and easiest turns which we see given to water is in the scroll of an ordinary wooden wheel. Supposing this scroll to be 72 inches in diameter with a 12-inch spout leading to it; that is, the diameter of the scroll is 6 times that of the spout and the velocity of water 25 feet per second (=10 feet head). To maintain this velocity requires an additional head of  $2\frac{1}{2}$  feet, but as this loss is hidden by the reduced velocity of the water caused by its impact on the buckets, and also rapidly grows less with its reduced velocity as shown in the first part of the note, it is very generally ignored and sometimes denied altogether.

## NOTE SECOND.

As a corollary of note 1st we see that as an abrupt change of direction requires power to overcome, the less we have of it in the chutes which admit water to the wheel, the better, as any force expended here is so much taken from the amount which can reach the wheel; while changing the direction of the water by the form of the wheel itself, is applying this force where it does its work.

## NOTE THIRD.

Loss of head from insufficient conduit. Water wheel builders lay great stress on this and generally give rather exaggerated views. The error is on the safe side, and when practicable it is well to follow their suggestions. It sometimes becomes necessary, however, to use trunks for supplying wheels which from original construction or want of room have less size than would be desired. It therefore becomes necessary to know what this loss is. Here comes the mooted question, whether this loss is that due to the head necessary to produce the required velocity or only that necessary to maintain this velocity in the conduit. Without entering into the arguments on the subject, some of which are rather more curious than useful, it is sufficient to say that but little if any loss is found to exist, except that due to the frictional resistance of the conduit, and this is measurable.

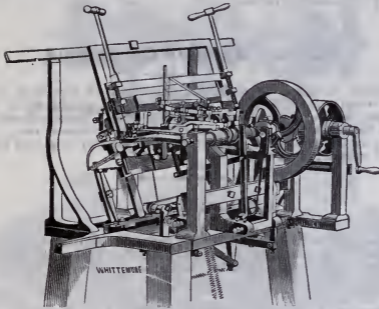
The following table, abridged from "Beardman's Manual of Hydrology," covers most of the cases required in ordinary practice.

Table of slope or fall in feet, and cubic feet discharged by pipe running full.

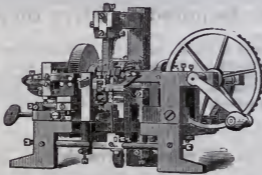
| Size of Pipe<br>in inches. | Slope<br>1 foot in 528.      |                           | Slope<br>1 foot in 264.      |                           | Slope<br>1 foot in 150.      |                           | Slope<br>1 foot in 66.       |                           |
|----------------------------|------------------------------|---------------------------|------------------------------|---------------------------|------------------------------|---------------------------|------------------------------|---------------------------|
|                            | Vel'y in feet<br>per minute. | Cubic feet<br>per minute. | Vel'y in feet<br>per minute. | Cubic feet<br>per minute. | Vel'y in feet<br>per minute. | Cubic feet<br>per minute. | Vel'y in feet<br>per minute. | Cubic feet<br>per minute. |
| 12                         | 130                          | 102                       | 196                          | 155                       | 243                          | 192                       | 392                          | 310                       |
| 18                         | 160                          | 282                       | 226                          | 399                       | 300                          | 528                       | 452                          | 798                       |
| 24                         | 184                          | 580                       | 261                          | 820                       | 345                          | 1,085                     | 522                          | 1,640                     |
| 30                         | 206                          | 1,013                     | 292                          | 1,432                     | 386                          | 1,895                     | 584                          | 2,864                     |
| 36                         | 226                          | 1,598                     | 319                          | 2,259                     | 423                          | 2,989                     | 638                          | 4,518                     |
| 42                         | 244                          | 2,350                     | 345                          | 3,321                     | 457                          | 4,395                     | 690                          | 6,642                     |
| 48                         | 261                          | 3,281                     | 369                          | 4,637                     | 488                          | 6,137                     | 738                          | 9,274                     |
| 54                         | 276                          | 4,403                     | 391                          | 6,223                     | 518                          | 8,237                     | 782                          | 12,446                    |
| 60                         | 291                          | 5,731                     | 412                          | 8,100                     | 546                          | 10,720                    | 824                          | 16,200                    |

From this table the mill owner can find what he can do with different sized conduits; making these square instead of round would be an ample allowance in size for roughness or irregularity of construction.

## Card Setting Machine.



This machine holds the leather used for the base of card clothing, feeds and cuts the wire, bends it for the teeth, pierces the holes, places the teeth therein, then clinches them tightly. Few machines so perfectly demonstrate the possibilities of mechanical movements as does this; but, as an invention, there are many others far superior, for the card machine is a combination of several separate devices. Aside from the device for cutting and bending the wire for the teeth, the other movements are mostly of a feed character, but the adjustments are so numerous that a mind of great organizing, rather than inventive ability, was required to bring them into harmonious operation. Amos Whittemore, of Cambridge, Mass., obtained the patent for the machine, but Eleazar Smith, of Walpole, Mass., claimed to be the inventor. It is difficult, however, to obtain much information about its early history, though it has had an immense influence upon the textile manufacture. Mr. Kent has been engaged in the manufacture of the machine for nearly a half century. He informs me that when he commenced, a separate machine, worked by hand [here illustrated],



was used to make the teeth, from which it would seem that the complete machine was many years in working its way into general use.

## Steam Engine.

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New, made by Brown of Fitchburg, Mass. 18-inch cylinder, 42-inch stroke, rated 75 horse-power with 60 pounds of steam; tested by Prony brake, steam pressure ranging from 65 to 70 pounds during the trial; the power varied from 60 to 65 h. p. according to pressure.

## Putnam Machine Co. Engine.

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New 15-inch cylinder, 3-feet stroke, guaranteed to give 60 h. p. with 60 pounds of steam; tested by Prony brake; gave 44 h. p. with 65 to 70 pounds steam. Such has been my general experience, and I doubt whether a steam-engine can be found that realizes more than 3-4 of its claimed rate. Indicator cards may give the pressure in cylinder, but the only way to get the efficiency of an engine is to take it from shaft.

## Compound Engine.

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Steam working first in a 6-inch cylinder, from that into one of 12 inches, 20 h. p. was claimed; dynamometer on shaft showed 7. Then it was found that the most of the force was used in working the engine.

## Power Required to Drive Woolen Machinery.

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THE POWER required to drive sets of woolen machinery depends upon the quality of goods and number of sets in a mill; the more sets the less power in proportion is required. I have tested the power used at many mills, but a few cases will show the general average.

VASSELBORO WOOLEN MILLS, VASSELBORO, ME. 22-set mill, light cassimeres; required, 135 horse-power.

WM. WALKER & CO., LOWELL, MASS. 4-set mill, flannels; required or used, 30 horse-power.

JAMES O. INMAN, PASCOAG, R. I. Heavy doeskin, pant goods, 4 sets; used, 40 horse-power.

BEEBE, WEBBER & CO., HOLYOKE, MASS. Pant goods, eight sets; 64 horse-power.

## Power Required to Drive Elevators.

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These elevators were in Boston stores, the belts when not at work running on loose pulleys. To operate the first kind tried, without load, when running at the common speed, 1.89 horse power. With a load of 1006 pounds, 3.92 horse power.

The second was a Tuft's elevator, running at the same speed as the first, without load, 2.46 horse power. With a load of 1004 pounds, required 5.29 horse power.

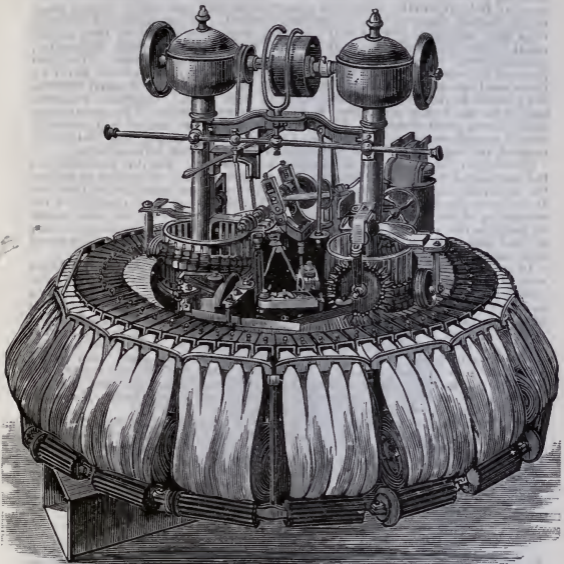
## Hydro-Extractor.

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Extractors start hard unless started very slowly, but lose their resistance instantly; three-fourths of a horse power would be a liberal average for such as I have tested, though from one to two horse power may be expended for a moment, if started hastily.



## Noble's Wool Comb.



## Woolen Manufacture.

The production of wool and manufacture of woolen goods constitute an old, perhaps the oldest, industry carried on among us. The fabled search by Jason for the golden fleece of Colchis typifies the esteem of the ancients for wool. Wherever we turn, in sacred or profane history, we find the lamb the symbol for tenderness, and wool, the cherished product of the sheep, always highly prized by man. Wild sheep are found everywhere, but all domestic breeds are derived from the Asiatic variety, which was developed from the argah, or big horn of Siberia. Originally, all were covered with long hair, and wool beneath; the hair has been bred out, but appears when the animal is neglected. The merino is the most valuable of all, dating back some two thousand years. The word shows in its own structure the choice nature of this sheep. The Spanish noun means judge or inspector of the *transhumance* (pasture-changing) flocks. Merino, the adjective, means wandering or the pasture-changing and best chosen flocks. Thus, the word brings down the process by which the flocks were



selected, and also by which they were managed and developed. It is the treasury of fine fibre for all varieties, and was introduced here in 1801-12. The Saxon, the finest variety, is too delicate for common use. Merino furnishes the best clothing or card wool and the fine or soft combing varieties. Leicester developed by Bakewell in the eighteenth century, Cotswold and similar coarse, long, bright English varieties yield the lustrous worsted. The manchamp, a variation from pure merino in France half a century since, has a lustrous fibre almost equal to the silky Cashmere goat. Carpet wools are long, rough and coarse, generally from South America, East India and the Mediterranean. The great pastoral districts for the merino and its crossing are now Australasia, River La Plata and Cape of Good Hope. These lands produced last year nearly 600,000,000 pounds in the grease, or 258,000,000 of pure wool. California produces largely for us, rather more than 50,000,000 grease pounds. The manufacture falls into two great divisions. First, woolens, which are carded and generally felted; second, worsteds, named from a village near Norwich, Eng., which are combed, the lustre of the wool preserved, and are finished without fulling.

Christopher Columbus was the son of a wool comber. But it is probable that the combing of wool at that time was but a simple process of carding or getting the wool ready for twisting into yarn upon the rude hand machines of that day. It has been the work of later years to perfect the art of wool combing or the separating of the long worsted fibres or hairs of the wool from the short down, or noils, as the combing waste is now called. The wool of commerce is now divided into three distinct classes—clothing wools, worsted or combing wools and coarse or carpet wools.

In order to fully understand the difference between the ordinary old-fashioned woolen goods and the more modern worsted fabrics, turn for a moment to the yarn from which each is woven. Place a bit of ordinary woolen yarn under a microscope, after untwisting it. You observe that the yarn was made up of numerous minute fibres, running in every direction, interlaced, hooked and curled together in such a snarl that it would not be possible to tell in what direction a majority of the fibres run. Give a little twist to the snarl and it is ordinary yarn again. Put a bit of worsted yarn under the glass, after taking out the twist in the same manner as before. You now observe that the hairs or fibres all run in the same direction; that they are all nearly straight or much more so than those of the ordinary yarn; that each fibre presents, instead of a downy appearance, almost a transparent lustre.

Until within a few years the separating of the worsted fibres from the short wool or noils was all done by hand, and a very tedious and unsatisfactory process it was; but by the more recent invention of very curious and almost life-like machines, an illustration of one of which may be seen at the head of this article, this separation or combing has reached such a stage of perfection as to have greatly increased the demand for and consumption of goods made of wool. The prices of goods of the finest texture and most beautiful lustre have been reduced to within the reach of people of moderate means.

### ORDINARY WOOLEN MANUFACTURING

Is carried on in mills with machinery classed as "sets," the cost of which at this time are about \$8,000 each. A mill building 50 x 160 feet, with four stories and an attic, gives room for ten "sets," though this does not include room for sorting, washing, drying, dyeing, picking, and boiler for heating. Such a mill driven by water-power would cost somewhere about \$150,000, or \$15,000 per set, varying somewhat, according to the conditions, cost of land, dam, &c.

Sets are based upon the number of cards used. These cards are of various lengths, but those of 48-inch are used most now.

#### MACHINES NECESSARY TO MAKE UP A SET OF WOOLEN MACHINERY.

Wool and Waste Duster answer for six sets.

Wool Mixing Picker answers for six sets.

Cards—three per set: first and second Breaker and Finisher.

Mule—four hundred spindles per set.

Spoolers—two per set.

Dresser, Reel and Beamer answer for six sets.

Looms—five broad or ten narrow per set.

Fulling Mill—two per set.

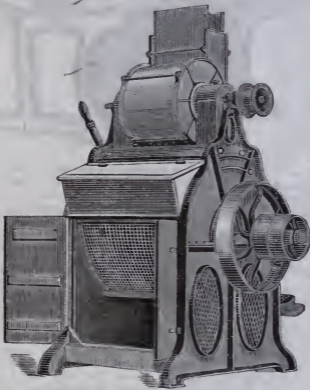
Washer answers for eight sets.

Hydro Extractor answers for six sets.

Gig—two per set.  
 Shears answers for four sets.  
 Brush answers for four sets.  
 Press answers for six sets.

The manufacture is conducted in the following manner: The wool must be sorted with reference to weight, softness, fineness, strength, color and cleanness. Wools of the best kind are separated into sorts, technically called *picklocks*, *prime*, *choice* and *super*. The first named is the most superior, and the others

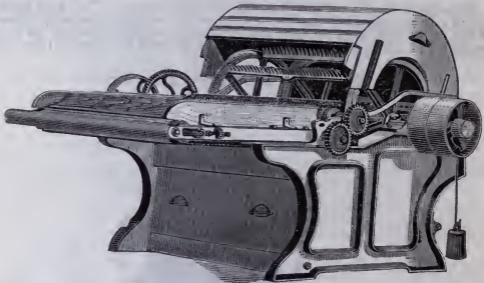
### Wool and Waste Duster.



follow in the order of their gradation to the last, which is the most inferior in quality. Inferior wools are sorted into *downrights*, *seconds*, *abb*, *livery* and *short coarse*. *Seconds* is wool grown on the throat and breast, and *livery*, that grown about the belly of the animal. *Abb* is an inferior kind of *seconds*, and *short coarse* is also derived from the breast. This operation is performed by hand and by skilled sorters. It is then scoured with a weak aqueous solution of alkali, then thoroughly rinsed in pure water and dried. It then goes to the dye-vats and is colored or "dyed in the wool"; then oiled, to prevent matting or felting; then goes to the Picker, which prepares it for carding.

Wool carding by machinery was first accomplished at West Riding, Yorkshire, England, about 1787. John and Arthur Scholfield, from that vicinity, came to this country in 1793 and, a year later, commenced to card wool by machinery in a mill at Byfield, near Newburyport, Mass. At that time, and, in fact, for many years later, each farmer in the New England States kept a sufficient number of sheep to supply his family with clothing, and a spinning-wheel and loom were to be found in each family; indeed, were often a part of the outfit of daughters, when they were married, instead of the piano, now required. There are many now living that can well remember the process of carding wool by hand, and from that the practice of sending the family supply of wool to the carding mills, where it was carded, and left in rolls about two feet in length to be spun upon the old spinning-wheels by the farmers' wives, daughters, or the "hired girl." In the

## Wool Mixing Picker.



earlier years of machine carding, the machines were very crude—merely strips of card clothing nailed upon flat surfaces beneath a single large cylinder. Such cards, however, were equal to the spinning-wheels, but the production of the spinning-jenny necessitated continuous rolls. For a time the short rolls were pieced by children as they were spun, the rolls being carried on the left and joined by the right hand—an operation that wore the skin from the fingers, and often caused the blood to flow therefrom. A piecer commonly supplied twenty spindles, so that three were required for each machine of sixty spindles. The “Finisher Card” is the outcome of the persistent efforts made to do away with the really crude, expensive and inefficient system of piecing. Many patents have been granted for different plans, and numerous prejudices have had to be overcome in order to accomplish the purpose.

The covering of card cylinders, known as “card clothing,” consists of wire teeth, of suitable form, set in a base of leather or its equivalent, made in many degrees of fineness, so as to meet the wants of carders of every variety of wool. The first breaker card has clothing made with coarse wire; the second breaker has finer; the finisher card the finest. From this card, the wool is delivered in numerous continuous soft cord-like rolls ready for spinning. The wool is weighed out and spread upon a feed-apron to the first breaker card. The licker-in presents it to the main cylinder, where it is worked by various devices; then, by what is called the Apperly feed, it is taken to the second breaker, and from that to the Finisher Card.

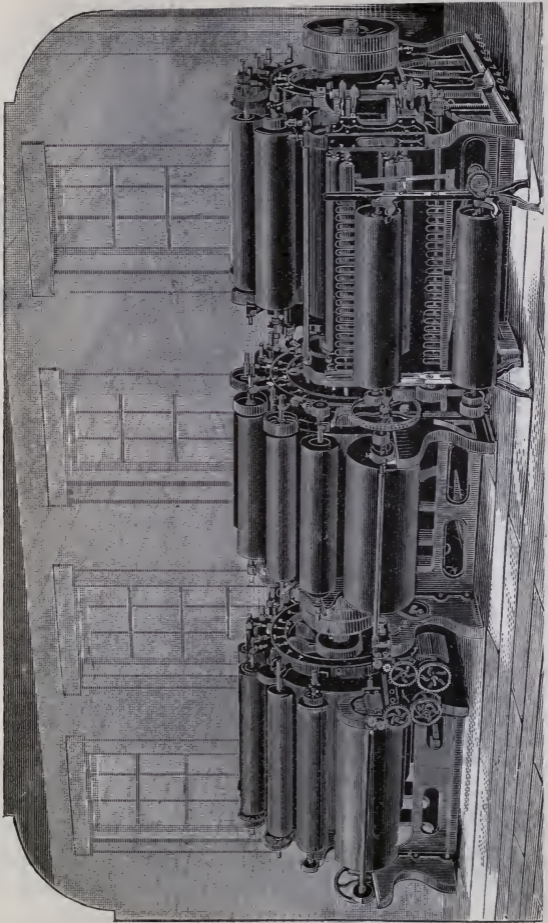
From the finisher card, the wool goes to the Mule. The illustration following the Card represents a Self-acting Mule, a machine that would have been looked upon with wonder a century since, and certainly with reason, if compared with the spinning-wheel of that period. A brief extract from the builders’ circular will give their claims for the special merits of their mule:

“This mule has a low carriage, an improved acceleration speed motion for spindles for spinning warp or other yarn requiring much twist, and is adapted for spinning all kinds of stock, and grades of yarn. It has a patent adjustable draft scroll, which can be so changed in a few minutes as to adapt it for giving any desired motion to the carriage when running out, whether for long draft or for twisting yarn without drawing at all, whereby much time and labor are saved that would be required to change scrolls.”

Messrs. Johnson & Bassett make mule building a specialty. Their mules usually have four hundred spindles each, or enough for a set each.

From the mule, the yarn is taken to the Spooler, which is used for transferring the yarn from the bobbins on to jaek or dresser spools for forming wool warps and also for doubling two or more threads together, the twist being put in on

Set of Wool Cards, in Position.

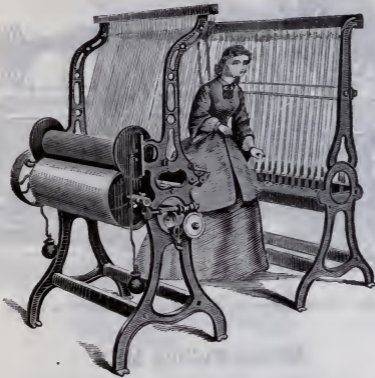


## SELF-ACTING MULE.



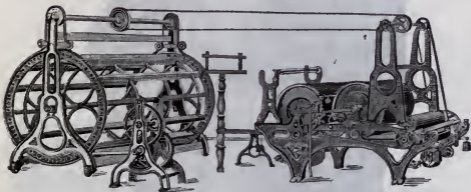


## Dead Spindle Spooler and Bobbin Stand.



the jack. A Dresser, Reel and Beamer are next required, in order to get the yarn on beams for weaving.

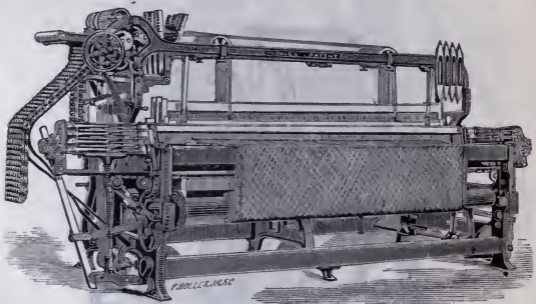
## Dresser, Reel and Beamer.



From the beamer, it goes to the Loom. For plain goods, the ordinary cam loom is sufficient, but the competition for superiority of styles necessitates looms capable of producing new patterns at will. This want seems to have been met by the production of the Knowles' Chain Loom, in which from two to forty harnesses and seven shuttles may be used, and of course capable of weaving an almost endless variety of styles, from plain to the most elaborate of patterns. The illustration annexed shows one of their looms, with any length of pattern required, easily changed to any style desired in a few moments, and so convenient as to be likely to supersede the ordinary cam looms in future, though for common use the twelve to twenty-five harness looms are sufficient.

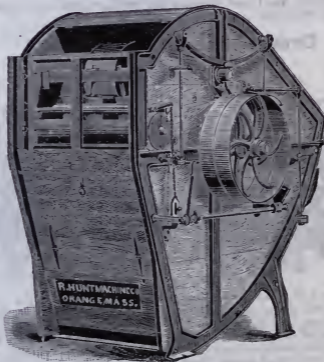


## Twenty-five Harness, Open Shed, Fancy Loom.



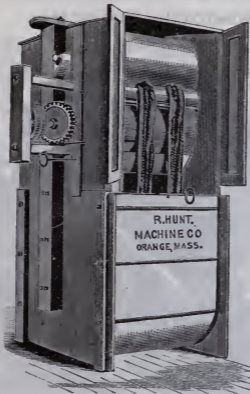
From the loom, the fabric goes to the Fulling Mill, where it is fulled. It then

## Rotary Fulling Mill.



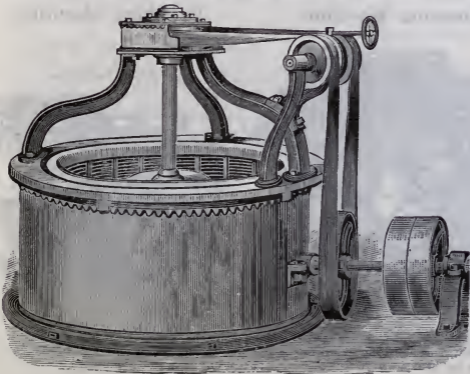
goes to the Washer, where it is soaped, scoured and rinsed. It then

## Cloth Washer.



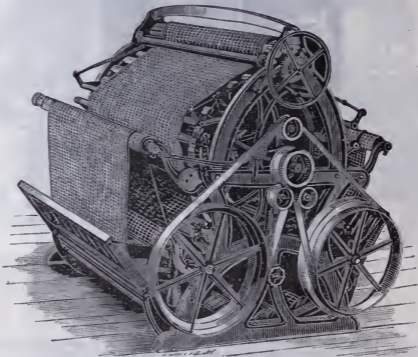
goes to the Hydro-Extractor, and is dried. This machine is also used in the preliminary operation of drying the wool after it is seoured and dyed.

## Hydro-Extractor.



From the hydro-extractor, it goes to the Gig, in which the nap is raised with teasels, the natural hooks of which many attempts have been made to equal by mechanical substitutes; but, up to this time, without success. In this gig the

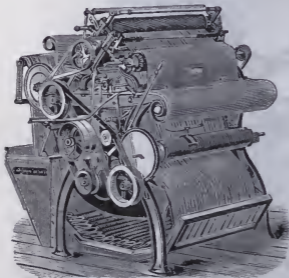
### Quadruple Acting Gig.



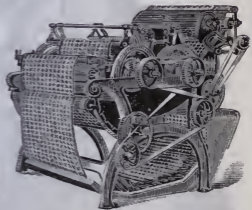
cloth is acted upon at four different points while passing through the machine. If a lustre like broadcloth is desired, the cloth is boiled or steamed to lay the fibre of the nap. From the gig, the cloth goes to the Shearing Machine, which has revolving blades working against one that is stationary, or a "ledger blade."

### Shearing Machine.

### Brushing Machine.

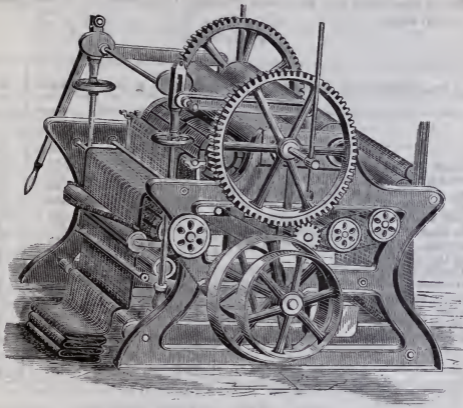


### DOUBLE-ACTING.



In this machine the nap is made even by shearing it. From the shearing machine, the fabric is sent to the Brushing Machine. From the brushing machine, it is sent to the Press, where it is passed between hot rolls to lay the nap.

Press.



WILLIMANSETT, MASS., May 21, 1881.

JAMES DUGDALE, LOWELL, MASS.

*Dear Sir:* I think you have been engaged for a number of years in the manufacture of worsted yarn, and that formerly you combed the wool by hand on instruments or devices substantially the same as the old hatchel used for combing flax, and that you now comb by machinery or machine combs. That the inventive and liberal patent system may be compared with that of the conservative or older method, will you be so kind as to state the difference in cost and efficiency of the two plans, and oblige,

Yours truly,

JAMES EMERSON.

LOWELL, MASS., May 25, 1881.

JAMES EMERSON, WILLIMANSETT, MASS.

*Dear Sir:* In reply to your letter of 21st inst., I have to say—The price paid for combing wool by hand was governed by the quality and length of staple. In 1863-64, the price paid in Lowell was 17 cents per pound for medium quality. A good workman was able to comb only from ten to twelve pounds per day—about twelve slivers weighing one pound. The first cost of the Improved Wool Combing Machinery is very high; consequently, repairs are very expensive. Still, the average cost is about five cents per pound, with the advantage of the sliver weighing from twelve to sixteen pounds. I shall be pleased to hear from you again.

Respectfully yours,

JAMES DUGDALE.

## Germania Mills, Holyoke, Mass.

Test of machinery with Emerson's Portable Dynamometer. Tables prepared by A. M. Swain.

### WEAVE ROOM.

| DESCRIPTION OF MACHINERY.                | TIME. | W'GHT. | SPEED. | H. P. |
|--|-------|--------|--------|-------|
|  | A. M. |        |        |       |
|  | 6.20  | 52     | 190    | 2.99  |
| Shaft 136 feet long, 150 revolutions. 21 | 6.30  | 55     | 182    | 3.03  |
| Broad Crompton Looms driven from the     | 6.45  | 55     | 192    | 3.19  |
| line. An average of 10 looms were prob-  | 7.    | 50     | 190    | 2.87  |
| ably in operation. Counted them in       | 7.15  | 60     | 190    | 3.45  |
| rapid succession over and over again.    | 7.30  | 53     | 190    | 3.05  |
| The least number in operation was 5 at   | 7.45  | 54     | 190    | 3.10  |
| one time. The most was 15; 9, 10 and 11  | 8.    | 60     | 188    | 3.41  |
| was the usual count.                     | 8.15  | 55     | 188    | 3.13  |
| Goods, heavy doeskin and cassimeres,     | 8.45  | 50     | 192    | 2.90  |
| 76 inches wide, 56 picks to the inch, 26 | 9.    | 60     | 192    | 3.49  |
| ounces to the yard, in a portion of the  | 9.15  | 60     | 192    | 3.49  |
| Looms.                                   | 9.30  | 86     | 192    | 5.    |
| April 12, 1873.                          | 10.30 | 80     | 190    | 4.60  |
|  | 10.35 | 60     | 192    | 3.49  |
|  | 10.36 | 65     | 193    | 3.80  |
|  | 11.40 | 15     | 192    | .87   |
|  | 12.15 | 651    | 188    | 2.90  |

### TESTS IN PICKING AND DRYING ROOMS.

| DESCRIPTION OF MACHINERY.                               | TIME. | W'GHT.  | SPEED.  | H. P. |
|---|-------|---------|---------|-------|
|   | P. M. |         |         |       |
| 2 Fans, 8 vanes each.                                   | 12.15 | 80 lbs. | 180     | 4.36  |
| 2 Fans, 8 vanes, 2 Fans, 5 vanes,                       |       | 122½    | 180     | 6.68  |
| 4 Fans, 1 Sargent's Burr Picker,                        | 1.30  | 230     | 181     | 12.61 |
| 4 Fans, 1 Sargent's Burr Picker,                        | 1.45  | 222     | 180     | 12.11 |
| 4 Fans, 1 Sargent's Burr Picker,                        | 2.    | 230     | 180     | 12.54 |
| 4 Fans, 1 Burr, 1 Kellogg Picker,                       | 2.05  | Belt    | Slipped |       |
| 1 Sargent's Burr, 2 Kellogg Pickers,                    | 2.30  | 180     | 179     | 9.76  |
| 1 Sargent's Burr, 2 Kellogg Pickers,                    | 2.45  | 180     | 179     | 9.76  |
| 4 Fans, 1 Burr, 2 Kellogg,                              | 3.    | 290     | 178     | 15.64 |
| 4 Fans, 1 Burr, 2 Kellogg,                              | 3.15  | 295     | 178     | 15.91 |
| 4 Fans, 1 Burr,   | 3.45  | 231     | 178     | 12.46 |
| 1 Burr,   | 4.    | 125     | 180     | 6.81  |
| 1 Burr, 4 Fans,   | 4.15  | 235     | 179     | 12.74 |
| 1 Burr, 4 Fans,   | 4.25  | 234     | 180     | 12.76 |
| 2 Kellogg Pickers,                                      | 5.    | 65      | 182     | 3.58  |
| 1 Kellogg Picker, large,                                | 5.05  | 40      | 181     | 2.19  |
| 1 Kellogg Picker, small,                                | 5.10  | 30      | 181     | 1.64  |
| Counter Shaft and loose Pulleys for<br>above machinery. |       | 25      | 180     | 1.36  |
| April 9, 1873.  |       |         |         |       |

## PAPER MANUFACTURE.

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Like the ordinary historian, I might draw upon my imagination for my facts, and give time and place where the first idea of paper was conceived, but the reader will be quite as well informed if the truth is given instead; and that is, that I do not know anything about it. It is evident, however, that it must have been centuries upon centuries ago. Writing would necessitate paper or a substitute. Writing, from the nature of the case, must have been understood before the commencement of history, for, without writing, there could have been no record. A mark was placed upon Cain for the purpose of warning those he might meet that he was not to be molested. The statement plainly implies that such mark or writing was generally understood, or it would have been useless; and it furnishes a plausible pretext for the Irish historian's genealogical tree springing from an Irish root, with Adam placed high among the branches, and the statement that the Irish had a written language at the time of Adam, all of which may be true; but if Old Israel was the son of an Irish emigrant, it would be an interesting study for the scientist to trace out the cause of such a radical change in the form of the nose. Evidence bearing upon that point might be difficult to find; but such would hardly be the case about paper, for the word is derived from that of papyrus, and papyrus was paper essentially the same as the paper of to-day, though crude and coarse, perhaps, in comparison with the best now made: the interior part of a reed or flag indigenous to Egypt, and places where papyrus was known.

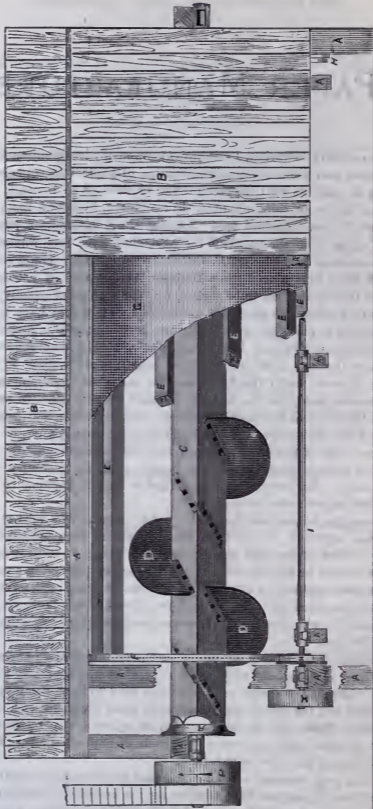
Its preparation for use was similar to that of paper. The part of the reed to be used was selected; it was then sized or glued, then subjected to heavy pressure. Sheets of any size desired could be made, as is proved by the fact that it was carried or kept in rolls. Vellum, often mentioned in connection with the early manuscript copies of Scripture and the printing of the first books, was white, finely prepared calf-skin. The object of this article, however, is more for the purpose of briefly describing the manufacture of paper now than to treat of its use in the past.

Until within a generation past, paper, or the finer qualities of paper, has been produced from rags, and the pulp has been worked into sheets by hand. Forms or sieves of the size of sheets required were used to take up the pulp; as the water drained out, the sheet formed, and when dried it was pressed. John Ames, of Springfield, Mass., now living, invented the cylinder paper machine, which is still in use in some mills where a cheap grade of paper is made. The Fourdrinier improvement has since been added.

Paper is in such demand now that constant investigation is going on for the purpose of discovering new fibre suitable for the purpose. Many kinds of stock are now used: rags, ground wood pulp, wood pulp chemically prepared, waste of many kinds, old rope, hemp, manila, fishing lines, jute, jute butts, straw, etc. Clay of various kinds is used, but by a neighboring manufacturer the individual does not do so.

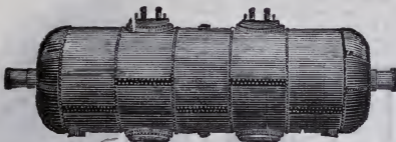


## Rag Duster.



Large quantities of rags are imported. Italy and Egypt furnish many of them, but rags from these countries mean rags, clothing worn until the strength is gone. There are certain qualities imported that are used for fine writing papers, but domestic rags are the best. An American has a very indefinite idea of what rags mean. One morning, in my early-boyhood, my slumbers were broken by a clattering and confusion of sound that would have matched Babel itself. Starting from my berth, a collection of rags and patchwork

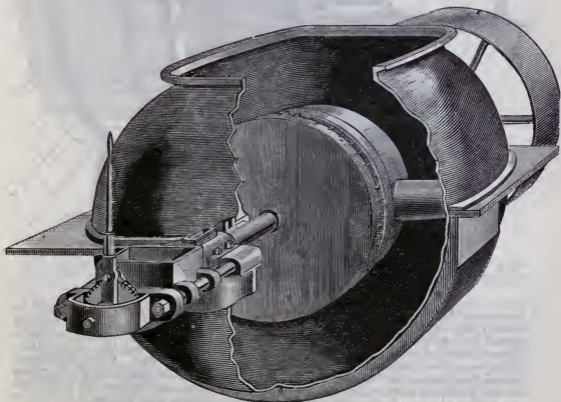
## Bleach Boiler.



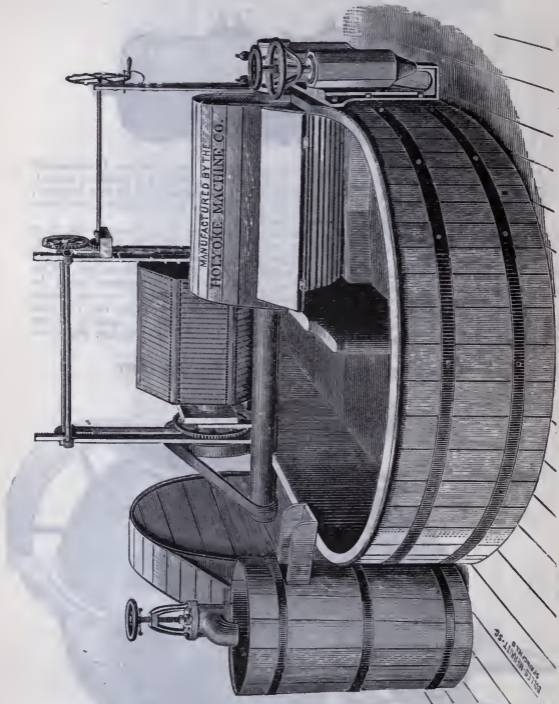
was presented to my sight that exceeded anything of the kind my imagination had ever conceived of. It is a blessing to the right kind of a Yankee to travel, for in many places he can see much to make him thankful that he is a Yankee. If he can get rid of some of his conceit, he will also see much that it is desirable to learn. The manufacture is conducted as follows:

The rags for fine paper are first dusted by running them through the Rag Duster. They are then cut into pieces, two or three inches in area of extent; this is done by women, each one of whom has the point half of a scythe firmly fixed vertically in a bench in front, the edge of the scythe being from her. With this instrument she cuts large handfuls of rags in various directions, until the mass is reduced into pieces the size required. She has to cut off buttons, hooks and eyes, seams, hems, and everything objectionable. After being cut, the rags are sorted, and everything rejected that is likely to injure the quality of the paper. They are then again dusted, and then placed in the Bleach Boiler—a

## Gould's Improved Beating Engine.



## Rag Engine.

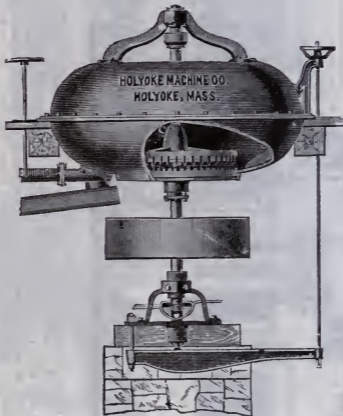


horizontal boiler, varying from five to eight feet in diameter, and from fifteen to twenty feet in length. Lime is put in with the rags. The boiler is rotated slowly for twelve hours, steam being introduced through the hollow journals; the pressure of steam being kept up to sixty pounds during the whole time. This is done to soften and aid in the disintegration of the rags. From the bleach boiler, the rags are dumped into large boxes on trucks, in which they are taken to the Washers, almost identical in their operation and appearance with the rag engine above. Indeed, in many mills the washing and beating are done in

the same engine. All the water that can be used is applied during the process of washing, but the roll is not pressed down so hard as it is while beating. The washing is continued from four to eight hours—usually about six, by which time the rags have become soft, pulpy stuff, which is then let down into the Drainers—tanks with perforated bottoms. Chloride of lime is added here to bleach the mass perfectly white. From the drainers, the stuff is taken up and put into the Beating Engines, where it is kept in constant motion, and continuously passing between the beating or tearing knives and roll. Coloring is here added to give the paper the desired tint. The mass is kept in the beaters until it is reduced to the condition required—usually about six hours. Then it is discharged into the "Stuff Chest" below.

For a long time—perhaps a century, more or less—there has been little change in the general character of the beating engine, except increase in size. Recently, attempts at improvement have been made, and now the Gould Engines are gaining favor from their increased productiveness, saving of labor and even quality of pulp.

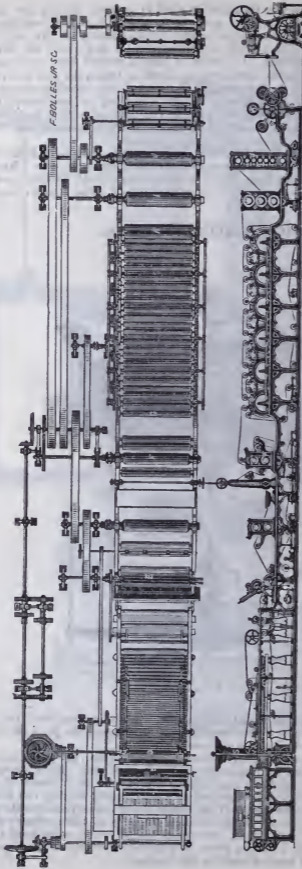
### Gould Beating Engine.



A charge for the engine is about 60 barrels, which is prepared for paper machines in about three hours. The centrifugal force keeps the pulp in constant motion, rendering stirring by hand unnecessary.

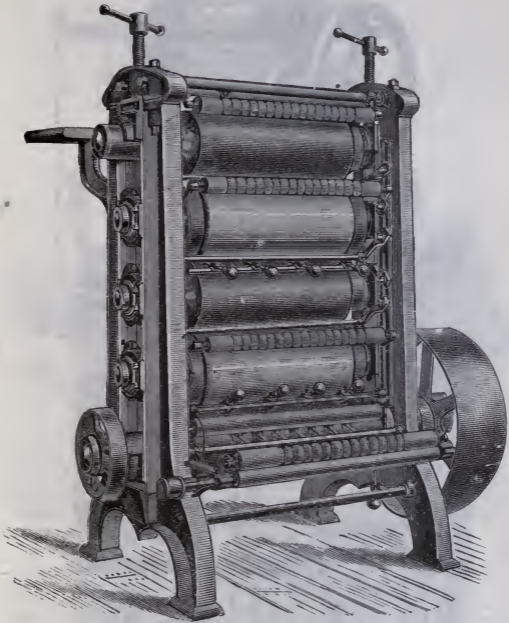
Experiments made for the Messrs. Stanwood, Tower & Co., at their paper mill at Gardiner, Me., a four ton mill, manila paper, jute stock. Regular speed of Beater 108 revolutions per minute, but during a test trial of 12 hours it varied from 106 to 112, requiring 55.36 horse-power as a maximum; during the trial 2400 pounds of excellent paper was weighed off, while there was a perceptible gain of pulp in stuff-chest at the close. Four 40-inch engines of the ordinary style in the same mill beating the same stock were then tested; with rolls hard down it required 103.64 horse-power to drive them to a speed of 160 revolutions per minute; this included shafting from wheels to the engines.

## Ames Cylinder and Fourdrinier Paper Machine Combined.



From the stuff chest, the pulp in a liquid state—the color of the paper being made—is pumped up into the Stuff Box, A. From that, it runs down into the Vat, B, and is strained off by passing down through the fine Screen or Strainer, C; then flows out on to an endless apron, made of fine wire cloth, working round the Roll, E. In connection with the urn-shaped column, there is a device called the Shake, which keeps the wire apron in constant oscillation or tremor. This part of the machine, from the Vat, B, to the Roll, E, is the Fourdrinier improvement of the Ames Cylinder Paper Machine. As the pulp moves along on the wire apron, the water is drained and extracted from the sheet of pulp by exhaust pumps beneath. It then passes on to the Cooch Rolls, E, and from there to an endless apron of felt, and is carried along to and between the Press Rolls, F, which leave the sheet in a condition to bear its own weight until it arrives at the Drying Rolls, G, along and around which it is carried by another endless apron of felt, and is dried, the rolls being kept hot by steam. After passing the drying rolls, the sheet or web passes through a solution of hot liquid glue or animal size, and then between rolls that extract or press out the superfluous size; then, by rotary cutters, it is divided into sheets the size required, and is then placed upon a table, in regular square packs, by a mechanical device called a Lay-boy, invented by J. C. Kneeland, of Northampton, Mass.

## Sheet Super Calender.

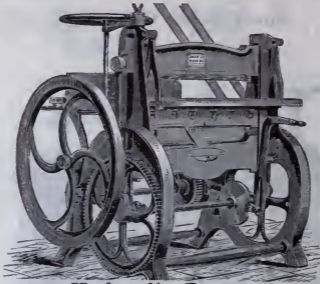


These packs are then taken to the Drying Loft, separated into sheets, which are hung evenly upon poles to dry, the loft being kept hot by steam. When dried, the sheets are sent to the finishing room, and are passed between rolls under great pressure. The process is called calendering, the Sheet Calender being used.

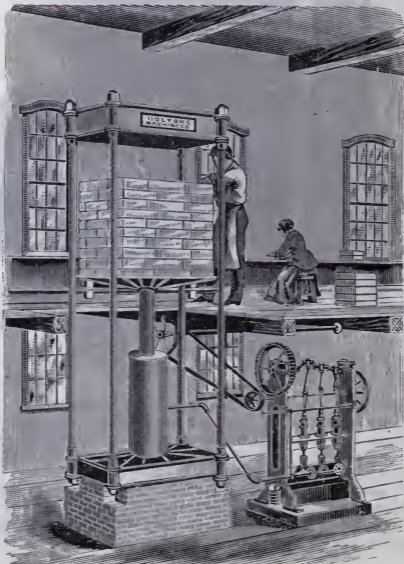
Ordinary paper for writing or commercial purpose is cut into sheets known as Flat Cap, 14 x 17½; Foolscap, 13 x 16; Letter, 10 x 16; Note, 8 x 10 inches. These sheets are counted into reams of 480 sheets each, folded, then trimmed in the Trimming Press. See cut, next page.



## Trimming Press, or Paper Cutter.

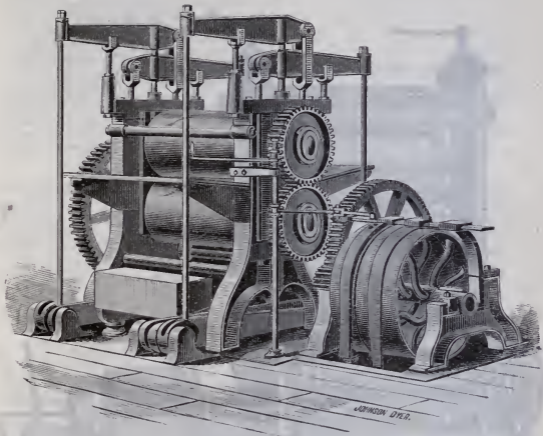


Hydraulic Press.



It is then subjected in packages to a pressure of several hundred tons in Hydraulic Press.

## Lever Plater.



After pressing, the packages are boxed, ready for delivery.

A finer grade of paper, used for wedding or fancy cards, and various purposes, is calendered in the sheet calender; then placed between metal plates, and passed between the rolls of the Lever Plater; then cut into sheets the size required, and boxed for shipment.

Book paper, often quite fine and nice, is of a somewhat inferior grade—often, if not generally, made of mixed stock: rags and wood pulp, sized with resin size in the beating engine, instead of with animal size in the paper machine.

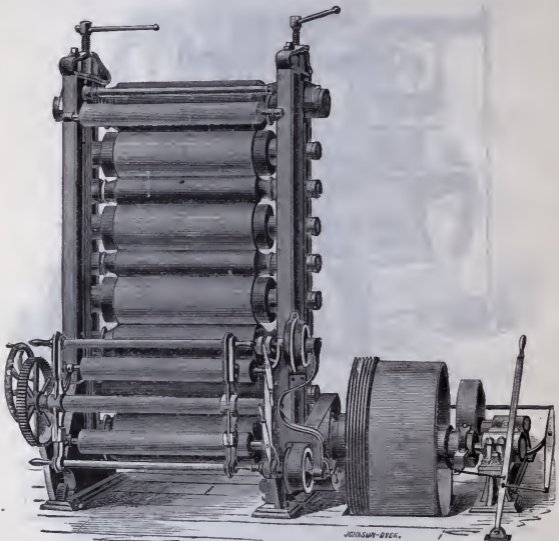
The process in the paper machine at the commencement is the same as before described, but instead of being divided into sheets, it goes in the web through the stack of Chilled Rolls, J, near the right end of the machine, which give what is called "machine finish." It is reeled or rolled, as represented on the Rolls, K. If a finer finish is desired, it is super-calendered. (See cut on next page.) It is then divided into sheets, the size required, by rotating cutters.

Newspaper is made of a cheaper grade of stock: rags, ground wood pulp, straw, waste of various kinds, etc.

Cheap wrapping paper is also made of straw, or something cheaper.

The best manila paper is made of jute, jute butts, old rope, hemp, manila, fishing lines, etc.

## Web Super Calender.



Fine tissue paper is also made of jute, but the process of beating requires twenty-four instead of six hours in order to disintegrate the stock more slowly, leave the fibre longer, and the product more tenacious.

The cost of a paper mill of course depends upon circumstances to a certain extent. The rough estimate of cost for a one-ton fine paper mill would be \$75,000 to \$100,000; larger capacity, in proportion. [A ton mill means one capable of producing a ton of paper per day.]

## Whiting Paper Co., Holyoke, Mass., No. 1 Mill.

## 4-Ton Mill, Fine Writing Paper.

Following machinery driven by the main wheel, which by test gave 180 h. p.

2 1250 pound washing engines.

2 1200 pound beating engines.

2 800 pound beating engines.

2 6 inch Littlefield pumps.

1 Andrews pump.

4 rag dusters; 2 rag boilers.

1 Elevator, 2 boiler pumps, 1 engine lathe, 1 sheet calendar, 5 rolls, 1 small pump, 1 circular saw for box work.

Finishing room wheel,

±2.92 h. p.

Drives 6 5-roll calendars, 2 platers, 5 ruling machines, 3 trimming presses, 1 elevator, 1 grind stone.

These two wheels do the work named, but 20 horse-power additional would be acceptable on large wheel.

## Test by Emerson's Dynamometer.

Experiment upon an 800 pound paper engine for rag stock; furnished with 800 pounds of bleached stock in the evening of March 26, 1875, at the Housatonic Mill of the Smith Paper Co. at Lee, Mass. The roll was 46 inches long by 40 inches diameter. Experiment began with a stock nearly finished, which was finished, discharged and the engine replenished.

| Time.<br>P. M. | Rev. of<br>Roll. | Rev. of<br>Dynamom. | Weight. | Horse<br>Power. |
|----------------|------------------|---------------------|---------|-----------------|
| 7.00           | 118              | 284                 | 165     | 14.20           |
| 7.30           | 124              | 294                 | 131     | 13.45           |
| 7.35           | 124              | 300                 | 135     | 12.27           |
| 7.45           | 124              | 288                 | 131     | 13.17           |
| *9.30          | 124              | 274                 | 184     | 15.27           |
| *9.35          | 124              | 274                 | 184     | 15.27           |

\*Roll down and stock half finished.

Experiments upon a 300 pound paper engine for rag stock: furnished with 300 pounds of bleached stock on the afternoon of March 24, 1875, at the Housatonic Mill of the Smith Paper Co., at Lee, Mass. The Roll was 33 inches long by 28 inches in diameter.

| Time.<br>P. M. | Rev. of<br>Roll. | Rev. of<br>Dynamom'r | Weight. | Horse<br>Power. |
|----------------|------------------|----------------------|---------|-----------------|
| 3.50           | 131              | 230                  | 28      | 1.95            |
| 4.00           | 131              | 230                  | 63      | 4.39            |
| 4.15           | 143              | 250                  | 57      | 4.31            |
| 4.20           | 149              | 260                  | 73      | 5.75            |
| 4.25           | 152              | 270                  | 49      | 4.00            |
| 5.00           | 166              | 291                  | 93      | 8.20            |
| 5.05           | 150              | 264                  | 93      | 7.44            |
| 5.30           | 146              | 257                  | 94      | 7.31            |
| 6.00           | 143              | 250                  | 95      | 7.19            |
| 6.45           | 149              | 260                  | 104     | 8.19            |
| 7.00           | 144              | 252                  | 107     | 8.17            |
| 7.30           | 149              | 260                  | 118     | 9.26            |
| 8.00           | 126              | 220                  | 119     | 7.93            |
| 8.15           | 133              | 233                  | 122     | 8.61            |
| 8.30           | 146              | 255                  | 119     | 9.19            |
| 8.45           | 149              | 261                  | 105     | 8.30            |
| 9.00           | 123              | 215                  | 105     | 6.84            |
| 9.15           | 137              | 240                  | 104     | 7.56            |
| 9.30           | 150              | 264                  | 101     | 8.08            |
| 9.45           | 137              | 240                  | 101     | 7.34            |
| 10.15          | 132              | 232                  | 100     | 7.03            |
| 10.30          | 137              | 240                  | 26      | 1.89            |

Experiment on a 62 inch paper machine making news print from rag stock. This machine is ordinarily run with a speed that will deliver the paper at the rate of 90 feet per minute; but during these experiments it delivered 61 feet per minute the first experiment and 78 feet per minute during the last experiment.

| Time.<br>P. M. | Rev. of<br>Dynamom'tr | Weight. | Horse<br>Power. | H. Power of<br>Pump. | Table<br>Power. |
|----------------|-----------------------|---------|-----------------|----------------------|-----------------|
| 4 00           | 200                   | 101     | 6.12            | 2.78                 | 8.90            |
| 4.20           | 230                   | 104     | 7.26            | 3.56                 | 10.82           |

The main line of shafting makes 108 revolutions per minute when 90 feet of paper is delivered per minute. From this main line the agitator, the water pump and the shaker at the head of the machine are driven and are not included in the test by the Dynamometer; but are calculated from the speed and width of belts by which they are driven, on the theory that a belt 1 inch wide, running 1000 feet per minute is a horse-power.

|   |               |
|---|---------------|
| The Shaker belt moves 600 feet and is 3 inches wide, equals 1800,   | H. P.<br>1.80 |
| The Agitator belt moves 329 feet and is 4 inches wide, equals 1316. | 1.32          |
| The Pump belt moves 251 feet and is 6 inches wide, equals 1506,     | 1.50          |
|   | 4.12          |

But as this pump is single acting, only acting during one-half of the revolution, I have called it two-thirds of the apparent power equals 1.00 h. p., and deduct  $\frac{1}{2}$  a h. p., then leaving 4.12 h. p. for the paper moving 90 feet per minute. Then by simple proportion of 78 to 96 with paper moving 78 feet per minute equals 3.56 horse power; with paper moving 61 feet per minute equals 2.78 horse power.

[Copy.]

I. M. WRIGHT, C. E.

## Holyoke Paper Co., Holyoke, Mass.

Four 500 pound beating engines took the whole power of a wheel that by test gave 80 horse-power; even with that power care was required in furnishing or they would not run to speed; after running so for some years, the Beaters were altered or put into better condition, so that the wheel now gives a large surplus of power. Mill makes fine writing paper.

## Test of a 72-Inch Wheel and Machinery, Fitchburg, Mass.

These experiments were made to determine power required to drive Beating-engines, 36-inch rolls, paper and rag stock. Before testing the wheel, the speed of the main shaft was taken under different conditions to ascertain the power required to drive machinery at the following speeds, the water in the pond being one inch below the lowest part of the crest of the dam.

1st TRIAL.—3 Engines beating, 1 washing, and all machinery attached. Speed of main shaft, 120 revolutions per minute, 49 h. p.

2d TRIAL.—2 Engines beating, 2 washing, all machinery attached. Speed of main shaft, 146 revolutions per minute, 49 h. p.

3d TRIAL.—2 Engines beating, 2 washing, duster thrown off. Speed of main shaft, 160 revolutions per minute, 48.3 h. p.

During the above trials the head was about 14 feet. The dynamometer was then applied to the end of main shaft, and the power of the wheel, at nearly same speed, obtained.

With the flush-boards off, leaving 13 feet head, under which the wheel was designed to give 60 horse-power, its power would have been 43.16.

No attempt was made to measure the water, it simply took the whole river. Capacity of Beater 450 pounds.

## Paper and Shoemaking Machinery.

Report of a test to determine the power required to run one of the Rag Engines at Bacon's Paper Mill, in North Lawrence, Massachusetts.

LOWELL, December 16, 1870

*J. A. Bacon, Esq.:*

DEAR SIR:—I have worked up carefully the tests made yesterday with Emerson's Dynamometer, at your mill in North Lawrence. When the engine roll made 145 revolutions per minute, the dial hand of the Dynamometer made 3.8 revolutions per minute. I have estimated the speed of the roll, upon the supposition that it varied during the different tests in the same proportion as the speed of the dial hand. I give the results obtained, in the order in which the tests were made.

| Number of Test. | CONDITION OF THE ENGINE. | Revolutions of Roll per minute. | Horse-Power indicated by Dynamometer. |
|-----------------|--------------------------|---------------------------------|---------------------------------------|
| 1               | No paper in.....         | 137                             | 2.5                                   |
| 2               | Paper being put in.....  | 149                             | 7.26                                  |
| 3               | “ “ “ “.....             | 141                             | 3.36                                  |
| 4               | Washing paper.....       | 153                             | 4.                                    |
| 5               | “ “.....                 | 145                             | 4.03                                  |
| 6               | “ “.....                 | 147                             | 4.41                                  |
| 7               | “ “.....                 | 144                             | 4.57                                  |
| 8               | “ “.....                 | 145                             | 5.19                                  |
| 9               | “ “.....                 | 153                             | 5.2                                   |
| 10              | “ “.....                 | 148                             | 4.71                                  |
| 11              | Beating pulp.....        | 149                             | 5.08                                  |
| 12              | “ “.....                 | 147                             | 5.02                                  |
| 13              | “ “.....                 | 149                             | 5.08                                  |
| 14              | Brushing the paper.....  | 149                             | 3.9                                   |

While the paper was being put in, the power indicated gradually rose from 2.5 horse-power to\*7.26 horse-power. It stood at 7.26 horse-power for about three minutes, after which it gradually fell to 3.36 horse-power. From test 4 to test 8, the roll was gradually set down harder and harder. At test No. 7, the roll was down as hard as is usual in making paper. At test No. 8, the roll was down harder than is common.

Very respectfully yours,

(Signed,)

CHANNING WHITAKER,  
Mechanical Engineer.

Report of a test to determine the power required to drive Shoemaking Machinery, at the State Prison, in Charlestown, Massachusetts.

LOWELL, July 13th, 1871.

*Rodney S. Tay, Esq., Treasurer Tucker Mfg Co., Boston:*

DEAR SIR:—On the 13th inst., I made a test with Emerson's small Dynamometer, of the power required to drive Mr. Blanchard's Shoemaking Machinery at the State Prison, in Charlestown. In Mr. Blanchard's lower room there are, besides the counter-shafting, 12 sewing machines, 2 peggers, 2 skivers, 1 heel trimmer, 1 bottom roller, 1 buffer, 1 roller, 1 splitter. All of the machinery is not in use at any one time. But making such allowance for this fact as seems to be fair, there is required for driving the machinery and counter-shafting in this room, 4.9 horse-power. In Mr. Blanchard's upper room, there are, besides the counter-shafting, 2 brushes and 4 buffers. There is required, for driving the machinery and counter-shafting in this room, 2.3 horse-power. Making a total of 7.2 horse-power used by Mr. Blanchard.

Very respectfully yours,

(Signed,)

CHANNING WHITAKER,  
Mechanical Engineer.

\*I tested an ordinary 450 pound Beater in same mill that took something over 13 horse power.



[From American Engineer.]

## A Man of Courage.

We publish elsewhere a communication from Mr. James Emerson giving some further facts in regard to warming of railway cars. Mr. Emerson has given the last five years of his life to this work, and so far, as we believe, he is the only man who has made extended experiments in heating by steam. He is well known as an hydraulic engineer. What he accomplished in that department of engineering is well told by a writer in the December, 1885, number of the *Milling Engineer*. The writer says:—

It will be sixteen years on April 1st next, since James Emerson, an inventor, of Lowell, Mass., issued a small, one-page circular, saying that he had purchased of the Swain Turbine Company their testing flume, built for the purpose of privately testing their own water-wheels, and that he was about to open a series of public competitive tests. It marked the commencement of an era of wonderful progress in turbines.

Mr. Emerson was a man of irreproachable integrity. He could not be bribed. He was too independent to be held as the tool of any one. He was fearless in his criticisms, and many a poor miller who had been defrauded by some unprincipled water-wheel agent, rejoiced to find that at last a man had arisen who knew and was not afraid to publish the truth. When he attacked a certain water-wheel builder, who circulated most elegant pamphlets, and who loudly claimed that his wheel was the best in the country, and that it had an efficiency of 90 per cent., although in reality it was worthless,—when Mr. Emerson drove him out of hydraulics into the patent medicine business, the whole fraternity of water-wheel users rejoiced. When he stated that the wheels of several loud talking, ignorant men had so passed out of use that they were more likely to be found at the junk-shop than anywhere else, and of a certain inventor, who claimed his wheel gave 135 per cent., that he had no doubt of his sincerity, but he had much doubt of his intelligence, there was great popular sympathy with a man who could so fearlessly say what he thought. The influence of his tests was marvelous. Nine-tenths of the water-wheels brought to him that first year only gave three-fourths of the power which their builders claimed and represented that they would give. At the present time all the leading water-wheels honestly give the power they claim, and the reason is because Mr. Emerson taught builders to estimate power correctly. Then nearly all the leading firms claimed and published that their turbines possessed the same economy of water at every stage of gate. None of them claim it now.

The influence of these tests was beneficial to every honest builder. The first wheel tested by the Stillwell & Bierce Manufacturing Co. only gave 68 per cent., although they honestly believed it could be relied upon to give 85. When they discovered the truth they commenced experimenting and improving their wheels until they gained records of over 90 per cent. A similar improvement was made by Stout, Mills & Temple, T. H. Risdon & Co., the Holyoke Machine Co., and many others. The effect of his tests, in the introduction of the best forms of water-wheels, was also remarkable. The attachment of a plate to a cylinder gate to raise and lower with the gate and to form the top of the stationary water course was then used by no builder of prominence. Now every firm building a cylinder gate wheel uses it to obtain good results at the part gate. He was the first to establish the fact that the discharge of water through a wheel of a given diameter could be increased to double the amount then customary, without injuring the efficiency of the wheel, and now there is hardly a prominent builder in the country who is not making use of that discovery.

I have not written this article as an eulogy of James Emerson, but because his name is inseparably linked to the recent progress of water-wheel science. Like every other prominent man, he was not perfect. The time had come when a better water-wheel, and more accurate information about the weakness and excellencies of the various systems in use, was demanded. Mr. Francis' valuable formulæ, upon which the whole system depended, were a locked-up mystery of little benefit to the majority of water-wheel builders. Location, experience, and remarkable fitness to the requirements of that special work made Mr. Emerson the means of creating such an improvement in a certain class of machines as few men have ever accomplished.

## Water Wheels.

In treating of water-power, means for its utilization is an important feature to be considered. As a motor, running or falling water was used back in the earliest ages of which we have authentic history; and the various devices employed for transmitting its power were hardly more crude than many that are patented for the same purpose at the present time. Volumes would be required to illustrate and describe the multitudinous plans that have been devised, but a very few pages would suffice for describing the principles of all. Our country is lavishly supplied with this natural motive power; and, as might be expected from a race so energetic, many devices have been produced for utilizing it advantageously. I have before me the copy of a patent granted to Benjamin Tyler, grandfather of John Tyler, of the well known Tyler wheel, which reads as follows:—

By the President, THO. JEFFERSON.

JAMES MADDISON, *Secretary of State.*

*City of Washington*—To wit:

I DO HEREBY CERTIFY, that the foregoing Letters Patent were delivered to me on the twelfth day of March in the year of our Lord one thousand eight hundred and four to be examined; that I have examined the same and find them conformable to law, and I do hereby return the same to the Secretary of State, within fifteen days from the date aforesaid, to wit:—on this nineteenth day of March in the year aforesaid.

LEVI LINCOLN, *Atty-Gen. of the United States.*

THE SCHEDULE referred to in these Letters Patent and making a part of the same, containing a description in the words of the said Benjamin Tyler himself, of the Wry Fly, which may be applied by wind or water to various machines, viz.: Grist mills, Hulling mills, Spinning mills, Fulling mills, Paper mills, and to the use of Furnaces, etc.

The Wry Fly is a wheel which, built upon the lower end of a perpendicular shaft in a circular form, resembling that of a tub. It is made fast by the insertion of two or more short cones, which, passing through the shaft, extends to the outer side of the wheel. The outside of the wheel is made of plank, jointed and fitted to each other, doweled at top and bottom, and hooped by three bands of iron, so as to make it water-tight; the top must be about one-fifth part larger than the bottom in order to drive the hoops, but this proportion may be varied, or even reversed, according to the situation of place, proportion of the wheel, and quantity of water. The buckets are made of winding timber, and placed inside of the wheel, made fast by strong wooden pins drove in an oblique direction; they are fitted to the inside of the tub, or wheel, in such a manner as to form an acute angle from the wheel, the inner edge of the bucket inclining towards the water, which is poured upon the top, or upper end of it, about twelve and a half degrees; instead of their standing perpendicular with the shaft of the wheel they are placed in the form of a screw, the lower ends inclining towards the water, and against the course of the stream, after the rate of forty-five degrees; this however may be likewise varied, according to the circumstances of the place, quantity of water, and size of the wheel; over this wheel, and exactly fitted to the top of it, is a cup, or short cylinder, made fast and immovable by timbers connected with other parts of the building. Said Wry Fly may be used with or without said cylinder.

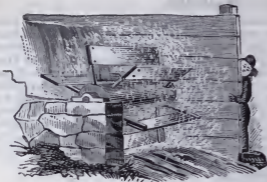
BENJAMIN TYLER.

P. HENDERSON,  
SAMUEL HITCHCOCK, } *Witnesses.*

From the description of the Wry Fly it will be seen that, except the chutes, it contained the principal features of the modern turbine, the merits of which are due to many minds; while still greater skill is required to bring it to that state of perfection it is undoubtedly destined to attain. The increasing importance of the manufacturing interest necessitated the improvement of devices for utilizing to the greatest possible extent the water-power of the country. An article suggested by the change of wheels at Lowell, Mass., is here quoted from the *Courier* of that city published in 1871.

“The removal of the last in the city (except two or three on the Concord River) of the old-fashioned and unwieldy breast-wheels suggests to us that a chapter of information on the hydraulic motors now in use here, and the history of their improvement and adoption, may prove of interest

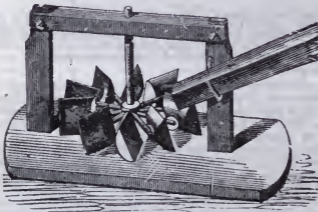
Devices of the Past.



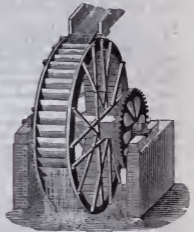
FLUTTER WHEEL.



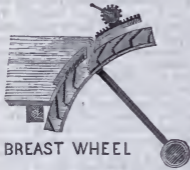
UNDERSHOT WHEEL



IMPACT WHEEL.



OVERSHOT WHEEL



BREAST WHEEL

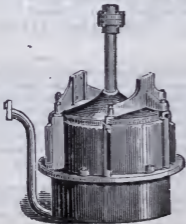
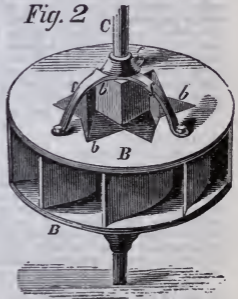


Fig. 2



to all the readers of the *Courier* who take a just pride in whatever aids Lowell to substantiate her claim to the title of "the first manufacturing city in America." And first, let us glance at the old style of wheels, of which those now being removed from the mills of the Lawrence and Prescott companies are fair examples. These, generally known as "breast-wheels," are dependent for their useful effect simply upon the weight of the water, admitted to the buckets near the top, and retained as long as possible, or until nearly at the bottom of the wheel, where its force is spent and it is discharged. These wheels have in Lowell been constructed of wood, and of great size, varying in diameter from 13 to 30 feet, and usually about 12 feet long. Wheels of this class are still in use to a great extent, and in rare instances reach the enormous size of 70 feet in diameter. From the starting of the first mill (Merrimack) in 1823, up to the year 1845, when the number of spindles was about one-half that present running, the breast-wheels alone were in use, and were considered the most perfect in all respects of the kinds generally known. But although held in such high estimation, they were very extravagant in the use of water; for although the proportion of the useful effect given by the wheel to the power expended sometimes reached as high as 75 per cent., the average performance fell far below this point, being only about 60 per cent. And the importance of overcoming this radical defect becoming more and more obvious, improvements were gradually devised which resulted finally in the invention of a class of wheels known as turbines.

The word turbine is derived from the Latin *turbo*, which means among other things, a top; and also, the whirling or spinning motion of a top. The name, though sometimes given a wider range of meaning, is properly applied to a re-action wheel with vertical axis. The wheel itself is a French invention, dating back to 1830, or thereabouts; and it was introduced into this country several years later by an eminent engineer of Pennsylvania, Mr. Ellwood Morris, who built and put in operation two of these wheels, and published the results of his experiments upon them about the year 1843. The advantages of the turbine were found to be mainly these; a greater economy in the use of water; adaptation to any fall; greater velocity, compactness and durability, and that it was not obstructed by backwater. Since Mr. Morris' experiments there have appeared before the public almost innumerable varieties of turbines, each inventor claiming for his wheel some advantage over all its predecessors; and up to the present time several hundred patents have been granted in this country alone for modifications and alleged improvements of the turbine as first invented. Many of these wheels are quite popular, and are in use in small establishments all over the country; but being roughly and cheaply made, none of them have yet been found to compare with the original Fourneyron turbine as improved by the inventions of Uriah A. Boyden, whose name is familiar to every one who is at all acquainted with the history of our city.

In 1844 Mr. Boyden designed a 75 horse-power turbine for the Appleton Company's Picker-house, introducing, as has been said, several changes of his own devising. This wheel was tested immediately after its completion, and found to give a useful effect of 78 per cent. of the power of the water. Encouraged by this success, Mr. Boyden proceeded in 1846 with the construction, for the same company, of three more turbines of 190 horse-power each, which upon being similarly tested gave the remarkable result of a useful effect of 88 per cent. In experiments since that time results have been obtained as high as 92 per cent.; but it is considered that a fair average for these wheels is about 75 per cent. against 60 for the breast-wheels as above stated. From the date of the Appleton Company's adoption of turbines, they have come rapidly into use; being substituted for the clumsy affairs first used as fast as the latter became unserviceable from wear and decay.

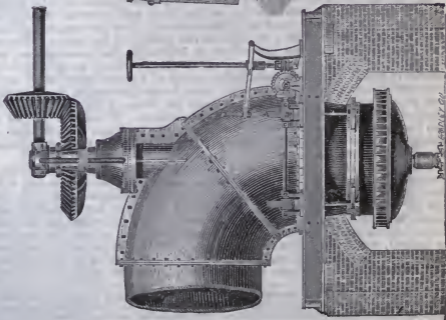
One of the advantages of the turbine, as already stated, lies in the fact of its occupying so much less space, in proportion to the power, than any other wheels. And this will be more fully realized when it is considered that there are in actual use for manufacturing purposes turbines of only 6 inches diameter; and though these, it must be owned, are rare, those of 10 and 12 inches are not unfrequently met with; usually operating, however, in localities where the amount of water is limited, while the fall is considerable. Of the 70 powerful turbines in use in the mills of Lowell, the smallest has a diameter of 5\*, and the largest of 11 feet, and the capacity of a single wheel reaches, in several cases, 675 horse power.

\*At the time the foregoing was written there were many turbines in use at Lowell of less diameter than 5 feet, though perhaps none of the Fourneyron style; since that time the large companies there have taken the Swain turbine in preference. The following article gives the origin of the Fourneyron wheel, and will enable the reader to consider Mr. Boyden's claim as inventor, understandingly.

# FOURNEYRON WHEEL.

Holyoke Machine Co., Holyoke, Mass.

MacAdam Bros., Belfast, Ireland.





The whole power given by the fall of the Merrimaek at Lowell, of 33 feet, is estimated at about 10,000 horse-power, the entire amount of which is already leased to the corporations. In addition to this, there are in the mills 31 steam-engines, furnishing 5000 horse-power additional; and besides these sources there are the three falls of Concord River, the power of which we have no means of estimating.

### \*Fourneyron Wheel.

[*Extract from a Treatise on the power of water, by Joseph Glynn.*]

M. Fourneyron, who began his experiments in 1823, erected his first turbine in 1827, at Point sur l'Oignon, in France. The result far exceeded his expectations, but he had much prejudice to contend with, and it was not until 1834 that he constructed another, in Franche Comté at the iron-works of M. Caron, to blow a furnace. It was of 7 or 8 horse-power, and worked at times with a fall of only 9 inches. Its performance was so satisfactory that the same proprietor had afterwards another of 50 horse-power erected, to replace 2 water-wheels, which together, were equal to 30 horse power.

The fall of water was 4 feet 3 inches, and the useful effect, varied with the head and the immersion of the turbine, 65 to 80 per cent.

Several others were now erected: 2 for falls of 7 feet; 1 at Inval, near Gisors, for a fall of 6 feet 6 inches, the power being nearly 40-horse, on the river Epte, expending 35 cubic feet of water per second, the useful effect being 71 per cent. of the force employed.

One with a fall of 63 feet gave 75 per cent.; and when it had the full head or column for which it was constructed—namely, 79 feet—its useful effect is said to have reached 87 per cent. of the power expended.

Another, with 126 feet, gave 81 per cent.; and 1 with 144 feet fall, gave 80 per cent.

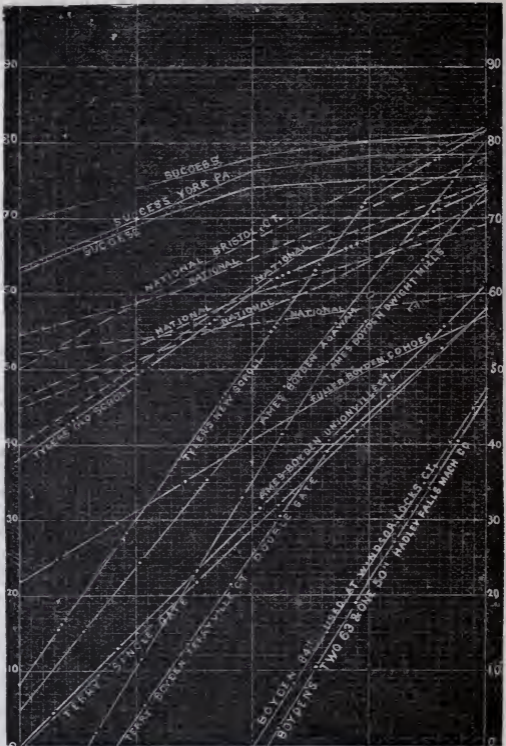
At the instance of M. Arago, a commission of inquiry was instituted by the Government of France, for examining the turbine of Inval, near Paris, the total fall of water being 6 feet 6 inches, as has been before mentioned. By putting a dam in the river, below the turbine, so as to raise the tail water, and diminish the head to 3 feet 9 inches, the effect was still equal to 70 per cent.; with the head diminished to 2 feet, the effect was 64 per cent.; and when the head was reduced to 10 inches, it gave 58 per cent. of the power expended, notwithstanding the great immersion of the machine.

In the year 1837, M. Fourneyron erected a turbine at St. Blasier (St. Blaise,) in the Black Forest of Baden, for a fall or column of water of 72 feet (22 mètres). The wheel is made of cast-iron, with wrought-iron buckets; it is about 20 inches in diameter, and weighs about 105 pounds; it is said to be equal to 56 horse-power, and to give an useful effect equal to 70 or 75 per cent. of the water power employed. It drives a spinning-mill belonging to M. d'Eichtal. A second turbine, at the same establishment, is worked by a column of water of 108 mètres, or 354 feet high, which is brought into the machine by cast-iron pipes of 18 inches diameter of the local measure, or about 16½ inches English. The diameter of the water-wheel is 14½, or about 13 inches English, and it is said to expend a cubic foot of water per second; probably the expenditure may be somewhat more than this.

The width of the water-wheel across the pier is .225, or less than a quarter of an inch. It makes from 2200 to 2300 revolutions per minute; and on the end of

\*The Fourneyron wheel receives the water from the inside, discharging it outwards. The gate, a thin hoop somewhat deeper than the wheel, is placed between the chutes and wheel, and is opened by being raised. With such an arrangement, economical part gate results are impossible; and M. Fourneyron and many others have made the wheel with divisions in the buckets as shown in the MacAdam plan. The "quarter turn" of the Holyoke Machine Co. is the invention of Mr. Boyden. MacAdam places the wheel at the small end of a vertical cone-shaped tube. Valentine and others have placed it in scroll and various kinds of curbs. It has been constructed so as to receive the water from below by many parties. It has been made with register gate inside of chutes, between chutes and wheel, and in one case in my experience, with two register gates, one inside of chutes, the other outside of wheel. It has been made with short straight chutes, also long curved ones. It has been suspended by the upper end of its shaft in various ways, instead of resting upon a step. It has been made of iron in the coarsest and cheapest style, and of bronze at an enormous cost. It has proved as variable in useful effect as any of the other kinds of turbines.





The Boyden turbine is highly recommended by its builder, and is much admired by the corporation superintendent, in kids, whose responsibility is remote; but the practical manufacturer, who has his own bills to pay, lets it severely alone. As may be seen by the diagrams, wheels constructed upon any of the popular plans represented in this work, may be made far superior in every respect, at one half its cost. Its continued use is owing solely to the low state of intelligence in milling engineering. It is idle to expect perfection or any constant efficiency in turbines until purchasers become sufficiently awake to their own interests to be willing to pay a fair price, and then to insist upon knowing exactly what the very wheel that is to be purchased will do before accepting it. The same quality of workmanship will make any other kind of turbine as durable as the Boyden.

the spindle or upright shaft of the turbine is a bevelled pinion, of 19 teeth, working into two wheels, on the right and left, each of which has 300 teeth. These give motion to the machinery of the factory, and drive 8,000 water spindles, roving frames, carding engines, cleansers and other accessories. The useful effect is reported to be from 80 to 85 per cent. of the theoretical water-power. The water as filtered at the reservoir before it enters the conduit pipes; and it is important to notice this, since the apertures of discharge in the wheel are so small as to be easily obstructed or choked.

The water enters the buckets in the direction of the tangent to the last element of the guide-curves, which is a tangent to the first element of the curved buckets. The water ought to press steadily against the curved buckets, entering them without shock or impulse, and quitting them without velocity, in order to obtain the greatest useful effect; otherwise a portion of the water's power must be wasted or expended, without producing useful effect on the wheel.

It is difficult to imagine that a machine so small as this can give motion to the works of a cotton mill on so large a scale. Professor Ruhlmann says, that when he saw it actually doing so, he could not for some time credit the evidence of his senses; and, although he went purposely to examine it, his astonishment prevented him from comprehending, in the first instance, that the fact was really as it appeared.

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## The Jonval Turbine

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[From J. E. Stevenson's Circular.]

By referring to our certificate on another page, it will be seen that it is impossible to construct a turbine greatly to exceed in useful effect a "Jonval," when properly constructed and well finished; and by reference to the table of experiments here inserted, it will be noticed that the efficiency of the Jonval turbine depends not upon the name "Jonval," neither upon the simple fact that one wheel is placed above another—as from 6 Jonvals tested, but one gave 90.77 per cent., that being the *one made by us*; whereas one other gave only 50.34 per cent., the *lowest of all tested*. And why this difference? Simply because one builder knew what he was doing, and the other did not. There are many parties, purporting to manufacture the Jonval turbine, who state in their circulars that "at a trial of turbine wheels, at Fairmount Water Works, at Philadelphia, in 1859 and 1860, the Jonval wheel gave the highest percentage of all tested;" and they would have the public believe that with their rough, unfinished castings, guide and bucket curves, of whatever form they may happen to be, they give this wonderful result, when none of them possess more than one feature of the Jonval turbine; and these experiments show that a "Jonval," made by a man of experience, and tested under the most favorable circumstances, gave the *poorest result of all*, simply because he failed in the application of the principles embodied in its construction.

The following is a table of the experiments at the Fairmount Water Works, at Philadelphia, in 1859 and 1860, as taken from the report of the Chief Engineer. The table explains itself.

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At a trial of water wheels, at Fairmount Works, by order of the Select and Common Council of the City of Philadelphia, a Jonval turbine, made by "J. E. Stevenson," of Paterson, New Jersey, was tested March 9th, 1860, and produced a co-efficient of useful effect of .8777 per cent. under the following circumstance: 925 pounds were raised 25 feet by 70.25 cubic feet of water under a head and fall of 6 feet. To this must be added the friction of the transmitting machinery, estimated at 3 per cent., making a total useful effect of .9077 of the power employed.

O. H. P. PARKER,

*Chairman of the Water Com.*

(SEAL OF CITY.)

HENRY P. M. BIRKINBINE,

*Chief Engineer.*

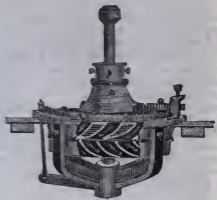
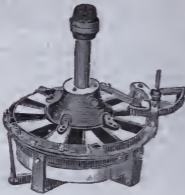
In attestation of the above signatures of O. H. P. Parker and Henry P. M. Birkinbine, I set my hand and affix the seal of the City of Philadelphia, this, 3rd day of April, 1860.

ALEXANDER HENRY,

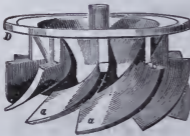
*Mayor of Philadelphia.*

Jonval Wheels, with Variations.

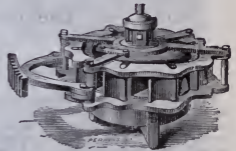
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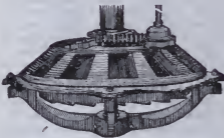
BODINE JONVAL.



BLACKSTONE.



ELMER.



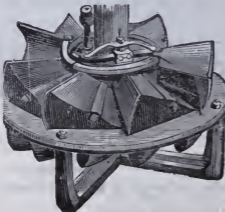
HOUSTON.



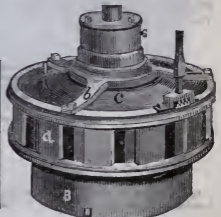
CURTIS.



DELPHOS.



CASE



VANDEWATER-BURNHAM.

Table of Experiments.

| NAME OF WHEEL.                     | Kind of Wheel. | Per cent. of effect. | 3 per ct. added for friction. | Where Built.          |
|------------------------------------|----------------|----------------------|-------------------------------|-----------------------|
| Stevenson's 2nd wheel.....         | Jonval..       | .8777                | .9077                         | Paterson, N. J.       |
| Geyelin's 2nd wheel.....           | Jonval..       | .8210                | .8510                         | Philadelphia, Pa.     |
| Andrews & Kalbach's 3rd wheel..... | Spiral...      | .8197                | .8497                         | Bernville, Pa.        |
| Collins' 2nd wheel.....            | Jonval..       | .7672                | .7972                         | Troy, N. Y.           |
| Andrews & Kalbach's 2nd wheel..... | Spiral...      | .7591                | .7891                         | Bernville, Pa.        |
| Smi'h's Parker's 4th trial....     | Spiral...      | .7569                | .7869                         | Reading, Pa.          |
| Smith's Parker's 3rd trial...      | Spiral...      | .7467                | .7767                         | Reading, Pa.          |
| Stevenson's 1st wheel.....         | Jonval..       | .7335                | .7635                         | Paterson, N. J.       |
| Blake .....                        | Scroll ..      | .7169                | .7469                         | East Pepperell, Mass. |
| Tyler .....                        | Scroll ..      | .7123                | .7423                         | West Lebanon, N. H.   |
| Geyelin's 1st wheel.....           | Jonval..       | .6799                | .7099                         | Philadelphia, Pa.     |
| Smith's Parker's 2nd wheel ..      | Spiral ..      | .6726                | .7026                         | Reading, Pa.          |
| Merchant's Goodwin.....            | Scroll ..      | .6412                | .6712                         | Guilford, N. Y.       |
| Mason's Smith.....                 | Scroll...      | .6324                | .6624                         | Buffalo, N. Y.        |
| Andrew's 1st wheel .....           | Spiral...      | .6205                | .6505                         | Bernville, Pa.        |
| Rich .....                         | Scroll ..      | .6132                | .6432                         | Salmon River, N. Y.   |
| Littlepage.....                    | Spiral...      | .5415                | .5715                         | Austin, Texas.        |
| Monroe.....                        | Scroll...      | .5359                | .5659                         | Worcester, Mass.      |
| Collins' 1st wheel.....            | Jonval..       | .4734                | .5034                         | Troy, N. Y.           |

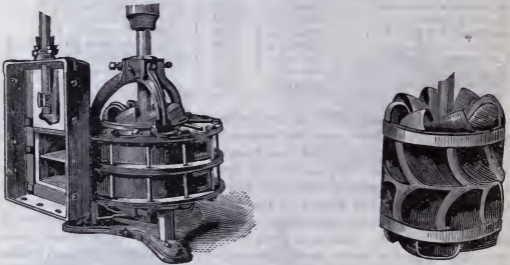
Turbine builders may object to my classification of the various wheels represented upon the opposite page; but because M. Jonval defined certain lines for a turbine, he no more proved that those lines covered the principle than he would have proved that the only place to walk upon a street is exactly three feet from its centre on a line parallel therewith, had he defined such a line. The wheel itself was common and known as the Tub wheel. Two wheels made upon the Wry-Fly specification, placed one above the other, would have covered the plan of M. Jonval; placing a fixed wheel above the wheel proper would have little originality unless done before any other builder had made an application of chutes to turbines. The experiments of D. P. Blackstone, show plainly that the vertical part of the buckets of the Vandewater-Burnham wheel, represented with the others, is of little practical utility; indeed, the vertical part of such buckets have often been proved to be decidedly injurious. Wheels constructed in that way, however, render it more convenient to apply the water economically at part gate. Many plans for gates have been tried with the Jonval, but none that has not in some way proved objectionable. Many have been made without any gate, simply letting the water on from the head gate of flume. Geyelin of Philadelphia has a telescopic tube below the wheel, the bottom thereof being lowered to the apron beneath, in order to stop the water. Wicket gates have also been tried in a tube below the wheel, but both plans cause an extravagant use of water, unless the wheel runs at whole gate. "Outside register gates" are the most common; these also render it impossible to economize water at part gate. The inside register, like that of Gates Curtis is far better in that way, but like the other register gates it works hard. Downward discharge wheels were objected to because they were supposed to press heavily upon the step; such an idea could only have gained a place through very superficial reasoning, for if 75 or 80 per cent. of the weight of the water forced the wheel ahead, the balance of the weight could only press down upon the step, whether downward, central or outward discharge.

## Perpetual Motion.

For ages past the above idea has been the constant dream of a certain class of minds, and is as prevalent to-day as in the past. To save such minds from the trouble of re-inventing for the thousandth time the same old wornout devices, a few of the most common are here sufficiently illustrated to show those engaged in such efforts that their plans are old. It is rather singular that such hydraulic geniuses almost invariably select the poorest kind of wheels to be combined, in order to get 175 per cent. from a double use of the water. The plan of Mr. Jones only contemplated increased capacity for diameter and part gate economy, but his plans have long been abandoned by more intelligent builders.

### Little Giant.

George H. Jones, Auburn, N. Y.

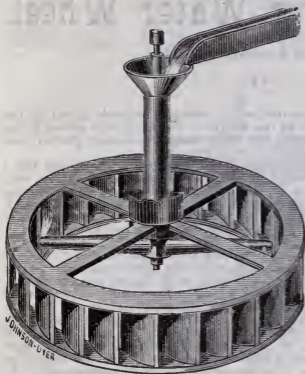


"Our wheel discharges its water inward, downward and outward, and discharges as much inward as any central discharge wheel of same diameter; as much outward as a Fourneyron, and downward as much as any Jonval, &c., &c."

There is not the slightest reason to doubt the ability of such devices to discharge an abundance of water, but years of experience and demonstrations by decisive tests prove beyond chance for dispute that all double arrangements are less effective than simple single turbines. Various kinds have been tested and invariably with the same results; the single wheel has proved the best in every way. The Leffel turbine has been continued in its original form simply because all the claims hinge upon the use of the double wheel, and to give up that would invalidate the whole patent.



## Double Wheels.

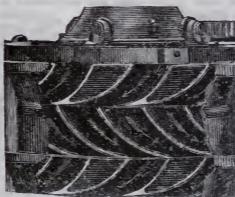


DEVICE BROUGHT FROM MEXICO. Barker Mill discharging into a Fourneyron wheel; connected by gears same as Wynkoop; small gear on rim of the funnel.

Same device used in a tanning mill. See Weisbach.



The Plan Represented below has caused the Expenditure of much Time and Money.



The plan consists simply of placing several Jonval wheels in a tube, one above another, each pair rotating in opposite directions. H. Twitchell of Pulaski, N. Y., furnished a set for trial, three wheels; the upper one stationary, acting as chutes; the two beneath rotating in opposite directions, being connected together by gears, hollow and solid shaft, arranged the same as those connecting Wynkoop wheels. First test was with upper wheel, lower wheel removed.

| Test of upper wheel with lower wheel removed. |       |             |           | Test of the two wheels connected by gears. |       |             |           |
|---|-------|-------------|-----------|--|-------|-------------|-----------|
| Head.   | H. P. | Cubic feet. | Per Cent. | Head.                                      | H. P. | Cubic feet. | Per Cent. |
| 18.59   | 6.96  | 353.04      | .5615     | 18.49                                      | 4.97  | 325.12      | .4486     |



L. D. WYNKOOP'S

**Double Power Water Wheel.**

Patented January 30, 1866.

In this improvement we have a device for combining wheels driven by the force of running water, and also by the weight of the fluid, both acting in the same direction, and the latter using the water which has already given power to the former.

Fig. 1 shows the external appearance of the case of the wheel, and Fig. 2 the two motors with their gearing. The stream is received at A, Fig. 1, and, by the spiral form of the case, is forced to receive a rotary motion as in the common Turbine. This water acts directly on the buckets, B, Fig. 2, which radiate from the center. They are connected to a hollow shaft, which carries the large bevel gear, C, gearing into the pinion, D, on the horizontal shaft.

Passing through the inside of this main shaft is the shaft, E, to which the scroll wheel, F, is secured at the bottom, and a bevel gear, smaller than C, at the top. This gear meshes with the pinion, G, on the horizontal shaft. After the water, by its rotary force, has done its work on B, it falls and operates F, giving it twice the speed of B. By this combination we claim that this device has twice the power of an ordinary wheel with the same weight and force of water. It has been tested by practical men with even greater results. There is now one of these wheels in successful operation in the machine shop of Messrs. CLAPP & HAMBLIN'S, of this City, who have the exclusive right for the manufacture of the same in this State, and the public are invited to call and test it for themselves. The proprietors, L. D. Wynkoop and S. P. Stone, are now prepared to negotiate with any responsible parties for the right to manufacture the same in any State of the Union. In offering this to the public, we are aware that the cry of humbug will be made, but we guarantee all we claim for it, and we wish no one to engage in it until he is satisfied that what we claim is true. Any inquiries addressed to the proprietors, at Owosso, Mich., will be promptly attended to.

L. D. WYNKOOP.  
S. P. STONE.

We the undersigned have seen the Wynkoop Wheel in operation and believe it to be all the inventor claims for it.

J. B. BARNES, Mayor,  
A. BARTLETT, City Marshal,  
E. D. GREGORY,  
C. W. CLAPP & CO.,  
D. R. STONE,  
N. McBAIN,  
GREEN & LEE, Editors "Press,"  
DANIEL LYON,  
WILLIAM FLETCHER,

JAMES W. STEDMAN,  
P. M. ROWELL,  
J. H. CHAMPION,  
EDWARD SMITH, Machinist,  
A. J. PATTERSON,  
C. A. BALDWIN,  
E. SALSBUURY,  
H. S. GALUSHE,  
C. OSBURN.

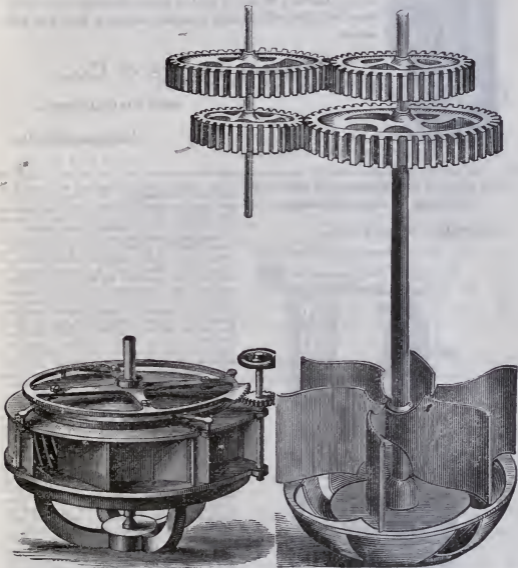
**CERTIFICATE:**

From the experiments performed with the Wynkoop Wheel in the Foundry of Messrs. Clapp & Hamblin of this city, I find it to utilize more than 175 per cent. of the absolute weight of water used; probably nearer 200. This I regard as no violation of the principle laid down in our natural philosophy, viz: that no wheel can be invented which will utilize 100 per cent., as the wheel in question is not a single one, but such a combination of wheels, as can not fail to give a vast increase of power.

I. C. COCHRAN, Principal of Owosso Union School.  
HENRY GOULD, Millwright, Owosso City.

## WYNKOOP'S

## DOUBLE POWER WATER WHEEL.



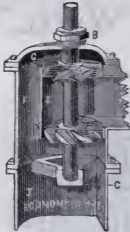
EFFICIENCY CLAIMED IN TABLES.

EFFICIENCY OBTAINED BY TEST.

| Head in feet. | Horse Power. | Cubic ft. Disch'd. | Percent- age. | Head in feet. | Horse Power. | Cubic ft. Disch'd | Percent- age. |
|---------------|--------------|--------------------|---------------|---------------|--------------|-------------------|---------------|
| 15            | 36.18        | 944                | 135           | 15.12         | 86.51        | 2318 23           | .5513         |

The debut of this wheel furnished ample proof that "Perpetual Motion" theories take as readily with those ranking with the learned, as with those having little knowledge of books. Several College Professors, (one at the head of a State Board of Education,) endorsed the claims of Mr. Wynkoop, furnished means to develop the merits of his device, and were present at its test and quietus.

## The Economy Water Wheel.



COMPLETE AND READY FOR SETTING UP.

We offer a challenge of \$1000 to the country to produce a Turbine Water Wheel of same diameter and under same fall that will furnish one-half as much power as our wheel.

Fulton, Myers & Co.,

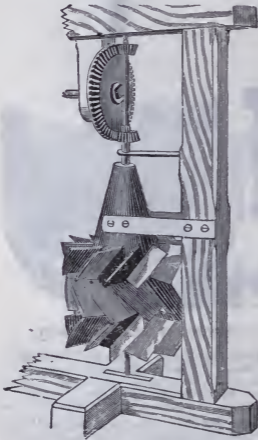
SOLE MANUFACTURERS,

Indianapolis, Ind.

## The Great Compound I.-X.-L.-- Turbine Water Wheels.

JOSEPH HOUGH, Sole Patentee,

BUCKINGHAM P. O., BUCKS CO., PA.



My father was a practical miller and a thorough millwright; he contended that there was no water wheel then in existence that utilized but a little over half the power of the water that passed over, under, or through any water wheel in use; and how to utilize this lost power was a difficult problem to an inventive mind to solve; nevertheless, perseverance and a determination to conquer all obstacles in the way, I finally invented and completely overcame this great difficulty, the utilizing of this otherwise lost power of water. I will give a complete description of the construction and action of the water on my Double Light and Left Reacting Turbine Water Wheels. The one-half diameter of their size are blocked or filled up in the centre, to cause the water by a tapering centre, a suitable height above the chutes, to spread all around from the inlets above, striking every bucket at the same time, at the farthest part from the wheel's centre, at the point of the wheel where the water exerts the greatest force and power. The chutes and also the buckets of both water wheels are straight blades, set at an angle of 45 degrees, that the current of water from the chutes above may strike the buckets of the upper wheel squarely at right angles, and as these buckets recede from the force of the current, the water escapes off these blades with still greater force by adding the second wheel of the same dimensions immediately under the first, with blades set also at 45 degrees in an opposite direction to again receive this otherwise lost force of the current of water, turning said wheel to the left hand. This is the important feature in my great improvement on all single turbines, by utilizing this otherwise lost force, utilizing the water twice over.

*Smith's Upper Spring Valley Mills.*

This is to certify, that the undersigned, millers and millwrights of Buckingham, were present at the testing trial of J. Hough's Great Compound I.-X.-L. Double Right and Left Reacting Turbine Water Wheels, and we are free to say, they far exceeded our most sanguine expectations by doing one-third more work with the same amount of water as it takes for the old ordinary single turbine water wheel. This we were eye witnesses to.

WM. B. SMITH,  
LEWELLEN FRIES,  
SAMUEL DELHAVEN,

JOHN C. VANDERGRIFT,  
JAMES M. VANDERGRIFT,  
ELI DOAN.

## Efficiency of Turbines.

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In reporting the efficiency of the many water wheels brought to be tested during the past ten years, it has been a very difficult matter to suit all that have been interested, yet no builder has ever expressed a doubt that any other builder has ever received a less favorable report than he deserved; but in their own particular case something a little more favorable should have been said, or something unfavorable left unsaid. Thousands have asked my advice in turbine matters, and many hundreds, if not thousands of turbines have been selected upon the advice given; yet not a single complaint has ever been made that the wheel recommended proved unworthy of the recommendation, nor in the ten years, has a wheel that I have reported poor, proved by practical use to be good. Time will determine whether my opinions, statements and reports relative to turbine matters have been well founded, and to that decision I am willing to trust.

In making up the following reports, my purpose has been more to aid builders in selecting the best plans than to sell wheels constructed upon any of those now existing; to do so requires a knowledge of the lowest as well as of the highest results obtained by test of each, and such are given.

The extreme variations in the results obtained from every kind tested, should convince purchasers that there is no certain way of procuring a good turbine otherwise than by testing, before acceptance, as they would do if purchasing a horse.

The wheel of B. J. Barber might properly have been placed in the group with the Wynkoop and others of that class—not that Mr. Barber believed in perpetual motion or 175 per cent. wheels; but he believed that an unexpended force remained in the water discharged by any single turbine, and that that force could be utilized by adding a second wheel below the first. His plan, however, carried out as shown, simply produces the ordinary downward discharge wheel. Mr. Barber erred in using the central discharge at all for much better results are possible with the plain downward discharge than can be obtained from the central, or his combination.

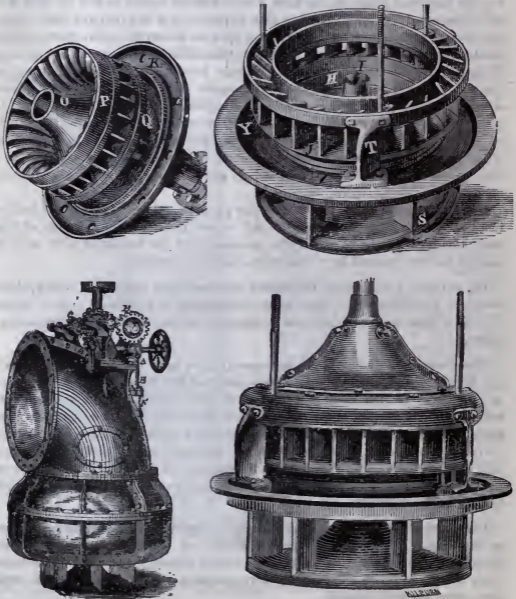
The other wheels with double discharge, reported in the following pages, such as the Swain, Leffel, Eclipse, Angell, Walsh and others, were so constructed, under the expectation of obtaining increased capacity for a given diameter, but a comparison with the capacity of recent plans will show that such expectations were not well founded.

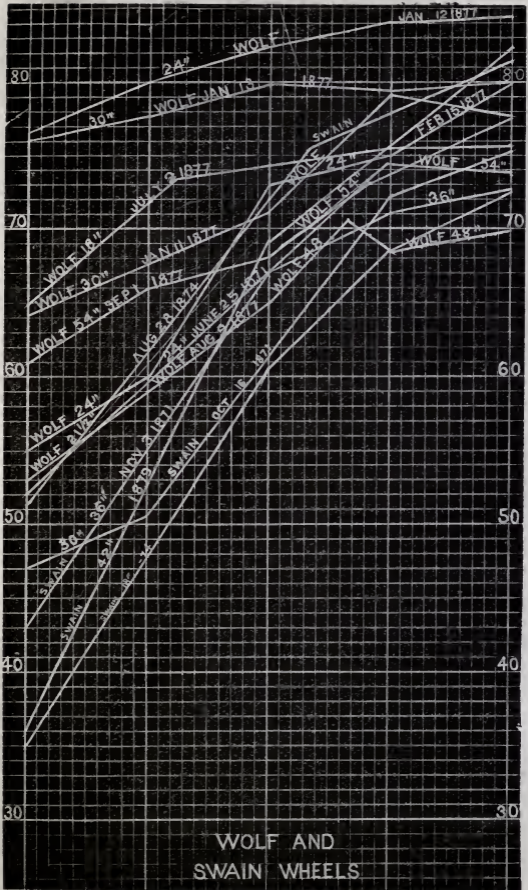
A. M. Swain, North Chelmsford, Mass.

SWAIN TURBINE.

One of the earlier high class wheels, made with many buckets and small openings, placed in "quarter turn" or "flume curb." Mr. Swain had much to do about starting the testing system. Quite a number of these wheels, ranging in size from 18 to 42 inches in diameter have been tested.

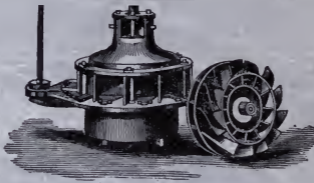
| Test of a 21-inch. | Head. | Weight. | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|--------------------|-------|---------|------------------|-------|-------------|-----------|
| Whole Gate,.....   | 17.91 | 300     | 281              | 25.55 | 936.55      | .8072     |
| Part Gate,.....    | 18.25 | 275     | 282.5            | 23.54 | 804.94      | .7902     |
| ".....             | 18.34 | 290     | 280.5            | 19.55 | 742.22      | .7611     |
| ".....             | 18.44 | 165     | 241.5            | 12.08 | 562.20      | .6175     |







## C. B. Walsh's Double Turbine, Waupaca, Wis



| Test of a 35-inch wheel. |       |       |          |         | Test of a 13-inch wheel. |       |       |          |         |
|--------------------------|-------|-------|----------|---------|--------------------------|-------|-------|----------|---------|
| Head.                    | Rev.  | H. P. | Cub. ft. | Per Ct. | Head.                    | Rev.  | H. P. | Cub. ft. | Per Ct. |
| 17.97                    | 166   | 61.19 | 2298     | .784    | 18.18                    | 368.5 | 9.49  | 508      | .544    |
| 18.09                    | 154.5 | 56.18 | 1980     | .830    | 18.28                    | 410   | 9.93  | 443      | .649    |
| 18.22                    | 151.5 | 44.76 | 1564     | .833    | 18.37                    | 377   | 8.00  | 355      | .650    |
| 18.33                    | 156.5 | 35.56 | 1291     | .800    | 18.41                    | 394   | 8.09  | 346      | .672    |
| 18.43                    | 151   | 24.02 | 935      | .735    | 18.51                    | 420   | 6.36  | 275      | .661    |
| 18.57                    | 154.5 | 17.55 | 755      | .663    | 18.52                    | 409   | 6.20  | 271      | .656    |
| 18.68                    | 152   | 10.36 | 523      | .562    | 18.56                    | 410   | 5.59  | 257      | .618    |

## Wetmore Wheel, Upham Machine Co., Claremont, N. H.

Test of a 36-inch, Sept. 17, 1873.

|                  | Head. | Weight. | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|------------------|-------|---------|------------------|-------|-------------|-----------|
| Whole Gate,..... | 17.94 | 810     | 146              | 53.76 | 1913.68     | .3291     |
| Part Gate,.....  | 17.98 | 650     | 143.5            | 42.40 | 1794.63     | .6959     |
| “ “ .....        | 18.09 | 450     | 151              | 30.88 | 1441.34     | .6270     |
| “ “ .....        | 18.18 | 320     | 141              | 20.51 | 1201.11     | .4975     |
| “ “ .....        | 18.28 | 150     | 143.5            | 9.78  | 946.76      | .2970     |

Test of an 18-inch, Sept. 29, 1876.

|                  |       |     |       |       |        |       |
|------------------|-------|-----|-------|-------|--------|-------|
| Whole Gate,..... | 18.69 | 150 | 303   | 13.77 | 501.32 | .7781 |
| Part Gate,.....  | 18.71 | 120 | 307   | 11.16 | 423.66 | .7454 |
| “ .....          | 18.79 | 75  | 305   | 6.93  | 304.45 | .6414 |
| “ .....          | 18.82 | 60  | 292.5 | 5.31  | 262.16 | .5699 |

Same wheel, buckets having been chipped.

|                  |       |     |       |       |        |       |
|------------------|-------|-----|-------|-------|--------|-------|
| Whole Gate,..... | 18.71 | 150 | 320.6 | 14.57 | 507.41 | .8125 |
| Part Gate,.....  | 18.87 | 80  | 304   | 7.46  | 323.50 | .6632 |
| “ .....          | 18.90 | 55  | 313.5 | 5.22  | 263.18 | .5577 |

Test of a 24-inch, Oct. 2, 1876.

|                  |       |     |       |       |        |       |
|------------------|-------|-----|-------|-------|--------|-------|
| Whole Gate,..... | 18.34 | 350 | 228   | 24.18 | 960.21 | .7270 |
| Part Gate,.....  | 18.58 | 185 | 230   | 12.89 | 582.25 | .6300 |
| “ .....          | 18.66 | 135 | 229.5 | 9.35  | 483.83 | .5611 |

Second test of same, buckets having been chipped.

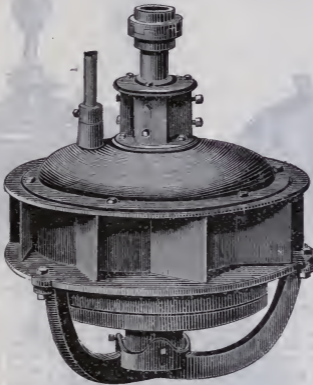
|                  |       |     |       |       |        |       |
|------------------|-------|-----|-------|-------|--------|-------|
| Whole Gate,..... | 18.30 | 360 | 249.5 | 27.21 | 963.51 | .8170 |
| Part Gate,.....  | 18.49 | 225 | 234.5 | 15.98 | 671.85 | .6810 |
| “ .....          | 18.67 | 100 | 237.5 | 7.20  | 424.49 | .4810 |

Test of a 48-inch, Oct. 5, 1876.

|                  |       |      |      |       |         |       |
|------------------|-------|------|------|-------|---------|-------|
| Whole Gate,..... | 10.15 | 1350 | 83.5 | 51.23 | 3713.65 | .7195 |
| Part Gate,.....  | 11.06 | 1100 | 80.5 | 40.25 | 3201.64 | .6018 |
| “ .....          | 10.63 | 700  | 83   | 26.41 | 2354.21 | .5588 |
| “ .....          | 11.02 | 400  | 82   | 14.90 | 1827.39 | .3834 |

## Perry Turbine.

Perry &amp; Taylor, Bridgton, Maine.



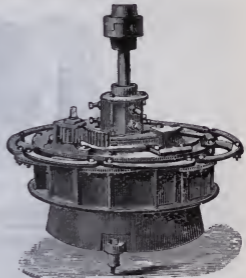
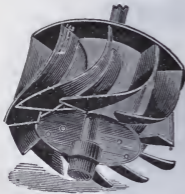
Downward discharge, with inside register gate. Messrs. Perry & Taylor have provided themselves with apparatus for testing their wheels before delivery, and guarantee the results furnished at each sale.

| Sept. 1, 1877.   | Head. | Rev'n<br>Per Min. | Horse<br>Power. | Cubic<br>feet. | Per<br>Cent. |
|------------------|-------|-------------------|-----------------|----------------|--------------|
| Whole Gate,..... | 13 12 | 271               | 6.15            | 300.65         | .8288        |
| “ “ .....        | 13.12 | 247.3             | 6.18            | 302.70         | .8223        |
| “ “ .....        | 13.12 | 274               | 6.22            | 300.65         | .8382        |
| “ “ .....        | 13.13 | 303.7             | 6.21            | 299.29         | .8382        |
| Part Gate,.....  | 13.22 | 261               | 4.74            | 246.85         | .7703        |
| “ “ .....        | 13.31 | 248.5             | 3.38            | 191.31         | .7039        |
| “ “ .....        | 13.33 | 280.5             | 3.18            | 184.13         | .6871        |

## SECOND WHEEL.

|                  |       |       |       |         |       |
|------------------|-------|-------|-------|---------|-------|
| Whole Gate,..... | 11.80 | 162.5 | 19.94 | 1086.89 | .8246 |
| “ “ .....        | 11.78 | 158   | 20.11 | 1093.57 | .8280 |
| “ “ .....        | 11.77 | 154   | 20.30 | 1090.23 | .8390 |
| “ “ .....        | 11.76 | 151   | 20.59 | 1100.25 | .8440 |
| “ “ .....        | 11.74 | 145.7 | 20.53 | 1110.30 | .8354 |
| “ “ .....        | 11 73 | 141.5 | 20.58 | 1115.34 | .8343 |
| Part Gate,.....  | 12.13 | 150   | 10.52 | 709.16  | .6486 |
| “ “ .....        | 11.98 | 164   | 11.18 | 762.55  | .6492 |
| “ “ .....        | 12 06 | 150.5 | 11.97 | 780.61  | .6589 |
| “ “ .....        | 12.23 | 151.5 | 8.60  | 628.50  | .5887 |
| “ “ .....        | 12.36 | 148   | 6.39  | 525.33  | .5221 |
| “ “ .....        | 12.42 | 139   | 4.73  | 464.96  | .4341 |

## C. G. Mullikin, Lansing, Iowa.



Test of wheel, 28 inches in diameter, the buckets extending to edge of the crown plate, and filling bore of curb. (The first test in all of the tables is at whole gate; the others at part gate.) The following results were obtained.

| Head. | Rev.  | H. P. | Cub. ft. | Per'tge |
|-------|-------|-------|----------|---------|
| 18.54 | 178.5 | 30.32 | 1087.39  | .7950   |
| 18.55 | 188   | 29.64 | 1038.32  | .8141   |
| 18.59 | 189.3 | 28.65 | 960.35   | .8492   |
| 18.65 | 182.5 | 24.72 | 818.23   | .8569   |
| 18.73 | 183.5 | 20.69 | 689.91   | .8470   |
| 18.83 | 181.8 | 14.71 | 513.39   | .8049   |
| 18.96 | 186   | 9.90  | 358.68   | .7702   |

The next trial was with a 44-inch wheel, with buckets of different curve or pitch from those of the 28-inch.

| Head. | Rev.  | H. P. | Cub. ft. | Per'tge |
|-------|-------|-------|----------|---------|
| 18.16 | 125   | 48.90 | 1994     | .7157   |
| 18.27 | 127   | 40.41 | 1735     | .6754   |
| 18.37 | 121.5 | 33.13 | 1504     | .6353   |
| 18.48 | 120   | 23.45 | 1187     | .5660   |
| 18.67 | 125   | 11.36 | 764      | .4125   |

The buckets were then cut away to line marked 2, and again tested.

| Head. | Rev.  | H. P. | Cub. ft. | Per'tge |
|-------|-------|-------|----------|---------|
| 18.06 | 133.5 | 63.71 | 2435     | .7670   |
| 18.07 | 137.5 | 60.93 | 2326     | .7676   |
| 18.17 | 131.5 | 53.79 | 2048     | .7652   |
| 18.29 | 135.5 | 44.33 | 1759     | .7295   |
| 18.44 | 136.3 | 30.47 | 1370     | .6490   |
| 18.58 | 137.5 | 20.00 | 1021     | .5594   |

Buckets cut to line 3, third test.

| Head. | Rev.  | H. P. | Cub. ft. | Per'tge |
|-------|-------|-------|----------|---------|
| 18.02 | 135.5 | 63.71 | 2389     | .7837   |
| 18.22 | 136.5 | 62.04 | 2276     | .7919   |
| 18.32 | 138.5 | 56.65 | 2075     | .7891   |
| 18.46 | 136   | 43.27 | 1671     | .7442   |
| 18.62 | 132   | 30.60 | 1319     | .6594   |
| 18.48 | 133   | 19.64 | 969      | .5809   |

30-inch wheel, buckets on line 1.

| Head. | Rev.  | H. P. | Cub. ft. | Per'tge |
|-------|-------|-------|----------|---------|
| 18.65 | 194.5 | 32.71 | 1188     | .7824   |
| 18.65 | 199.2 | 28.97 | 1081     | .7621   |
| 18.70 | 196.5 | 25.42 | 965      | .7740   |
| 18.77 | 190.5 | 19.48 | 811      | .6772   |
| 18.84 | 193   | 15.35 | 799      | .5399   |

Buckets chipped to line 2, re-tested.

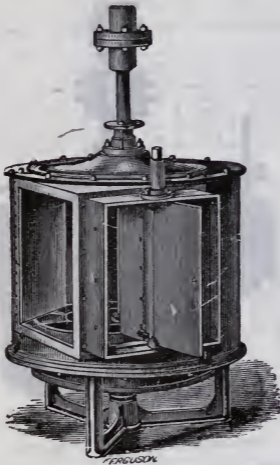
| Head. | Rev. | H. P. | Cub. ft. | Per'tge |
|-------|------|-------|----------|---------|
| 18.74 | 205  | 37.27 | 1218     | .8646   |
| 18.58 | 200  | 26.36 | 982      | .7649   |
| 18.70 | 199  | 15.82 | 699      | .6405   |
| 18.77 | 202  | 10.55 | 549      | .4941   |

Buckets of 28-inch chipped to line 2, and again tested.

| Head  | Rev.  | H. P. | Cub. ft. | Per'tge |
|-------|-------|-------|----------|---------|
| 18.48 | 171   | 30.70 | 1189.57  | .7393   |
| 18.50 | 179   | 29.29 | 1184.49  | .7077   |
| 18.53 | 178   | 28.31 | 1074.58  | .7489   |
| 18.60 | 175   | 24.59 | 934.59   | .7489   |
| 18.68 | 172.5 | 17.66 | 729.08   | .6865   |
| 18.80 | 179   | 10.57 | 498.86   | .5967   |

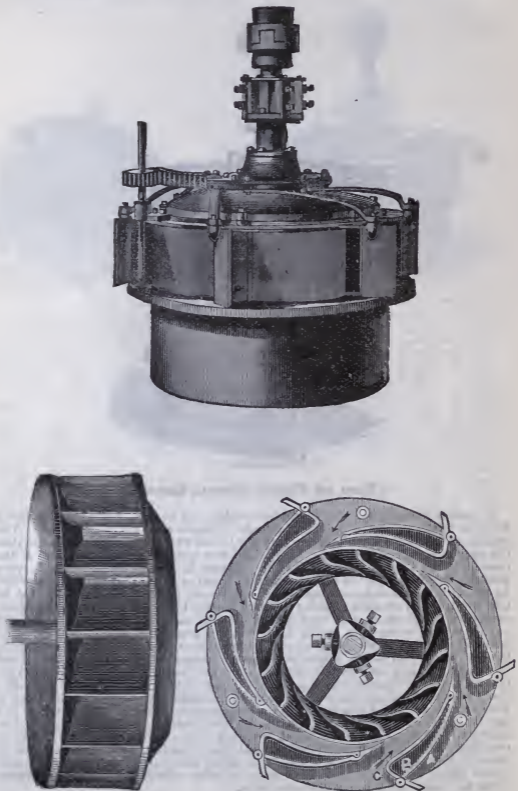
## Collins' Wheel.

Manufactured by J. P. Collins & Co., Norwich, Conn.



[FROM MY FOURTH ANNUAL REPORT.]

Is local in reputation and only made to order. A 24-inch, brass bucket, nicely finished wheel in a curb similar to the above was sent to me to be tested. The sender stated that \$900, had been paid for it and that Mr. Collins had sold it as the very best he could make. Mr. Collins was notified of the matter with the time fixed for the trial. Two days in advance he put in an appearance, very pleasantly remarking: "*I acknowledge the right of every purchaser to ascertain by actual trial the value of any wheel purchased;*" he further stated, that he had brought his overalls in order to put the wheel in order if it was not in good condition. Indeed, he was very genial, and one may judge of my surprise the next morning when just as the wheel was deposited at my flume, Mr. Collins, accompanied by sheriff, three or four appraisers, and other appurtenances of the law, stepped in with a writ of replevin and demanded the wheel. As I knew the purchaser had offered to sell it for a third of its price, I thought it an excellent sale, and, of course, made no unnecessary objections, but recalled to Mr. Collins his acknowledgment of the right of purchaser, to ascertain the value of wheel purchased; and was met with the statement that that particular wheel was not his present wheel at all; that he did not make such now; that he had no objection to his regular wheel being tested, &c. &c. Now, at the Philadelphia test, 1860, Mr. Collins produced the wheel that gave the lowest result of all, or about 47 per cent., as reported there. and as the wheel sent here was made somewhere about two years since, it becomes a rather interesting point to ascertain when he commenced to make good wheels.

**American Turbine.**

MANUFACTURED BY

## Stout, Mills &amp; Temple, Dayton, Ohio.

Test of a 36-inch Dayton wheel, Nov. 20, 1872.

|                   | Head. | Weight. | Rev. per Min. | Horse Power. | Cubic feet. | Per Cent. |
|-------------------|-------|---------|---------------|--------------|-------------|-----------|
| Whole Gate, ..... | 19.00 | 750     | 144           | 49.09        | 1780.14     | .768      |
| Part Gate, .....  | 19.11 | 615     | 140.3         | 39.22        | 1350.02     | .804      |
| " " .....         | 19.21 | 500     | 139.7         | 31.44        | 1123.75     | .770      |
| " " .....         | 19.30 | 350     | 146.5         | 23.31        | 888.29      | .719      |

November 13, 1873, 36-inch wheel.

|                   |       |     |       |       |         |       |
|-------------------|-------|-----|-------|-------|---------|-------|
| Whole Gate, ..... | 18.26 | 630 | 146.5 | 42.01 | 1625.77 | .7503 |
| Part Gate, .....  | 18.36 | 600 | 137.5 | 37.50 | 1440.20 | .7501 |
| " " .....         | 18.46 | 450 | 148   | 30.27 | 1174.92 | .7400 |
| " " .....         | 18.66 | 290 | 137.5 | 18.12 | 790.83  | .6496 |

June 11, 1873, 48-inch wheel.

|                   |       |      |       |       |         |       |
|-------------------|-------|------|-------|-------|---------|-------|
| Whole Gate, ..... | 18.10 | 1530 | 107.7 | 99.86 | 3514.90 | .8314 |
| Part Gate, .....  | 18.18 | 1320 | 109   | 87.20 | 3068.46 | .8280 |
| " " .....         | 18.41 | 1130 | 109.5 | 74.99 | 2647.48 | .8149 |
| " " .....         | 18.60 | 880  | 108.2 | 57.71 | 2200.89 | .7467 |
| " " .....         | 18.86 | 640  | 108.7 | 42.16 | 1772.46 | .6964 |

Test of 48-inch, January 29, 1874.

|                   |       |      |       |       |         |       |
|-------------------|-------|------|-------|-------|---------|-------|
| Whole Gate, ..... | 17.65 | 1320 | 107.8 | 86.24 | 3418.11 | .7598 |
| Part Gate, .....  | 17.66 | 1100 | 110.3 | 73.53 | 3010.79 | .7316 |
| " " .....         | 17.76 | 960  | 104   | 60.51 | 2594.01 | .6948 |
| " " .....         | 18.16 | 500  | 106   | 32.12 | 1690.47 | .5548 |

September 23, 1873, 42-inch right hand.

|                   |       |      |       |       |         |       |
|-------------------|-------|------|-------|-------|---------|-------|
| Whole Gate, ..... | 17.93 | 1200 | 112.5 | 61.36 | 2569.85 | .7095 |
| Part Gate, .....  | 17.98 | 990  | 118.5 | 53.32 | 2218.55 | .7094 |
| " " .....         | 18.30 | 650  | 120   | 35.45 | 1452.72 | .7065 |
| " " .....         | 18.45 | 440  | 119.5 | 23.90 | 1213.58 | .5666 |

October 1, 1873, 42-inch, left hand.

|                   |       |      |       |       |         |       |
|-------------------|-------|------|-------|-------|---------|-------|
| Whole Gate, ..... | 17.90 | 1100 | 118   | 59.00 | 2536.02 | .6882 |
| Part Gate, .....  | 18.00 | 980  | 120   | 53.45 | 2275.17 | .6946 |
| " " .....         | 18.13 | 820  | 121   | 45.10 | 1918.04 | .6884 |
| " " .....         | 18.43 | 420  | 116.5 | 22.24 | 1160.60 | .5479 |

November 11, 1873, 25-inch wheel.

|                   |       |     |     |       |         |       |
|-------------------|-------|-----|-----|-------|---------|-------|
| Whole Gate, ..... | 18.23 | 300 | 212 | 28.91 | 1158.24 | .7244 |
| Part Gate, .....  | 18.30 | 260 | 207 | 24.46 | 983.53  | .7185 |
| " " .....         | 18.39 | 220 | 205 | 20.16 | 880.49  | .6565 |
| " " .....         | 18.60 | 110 | 208 | 10.40 | 555.69  | .5323 |

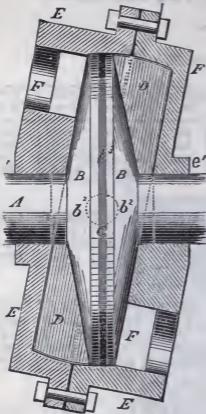
November 12, 1873, 20-inch wheel.

|                   |       |     |       |       |        |       |
|-------------------|-------|-----|-------|-------|--------|-------|
| Whole Gate, ..... | 18.85 | 130 | 253.5 | 14.97 | 606.54 | .6938 |
| Part Gate, .....  | 18.55 | 110 | 243   | 12.15 | 528.55 | .6536 |
| " " .....         | 18.63 | 90  | 244   | 9.98  | 448.93 | .6313 |
| " " .....         | 18.77 | 50  | 225.5 | 5.13  | 285.15 | .5072 |

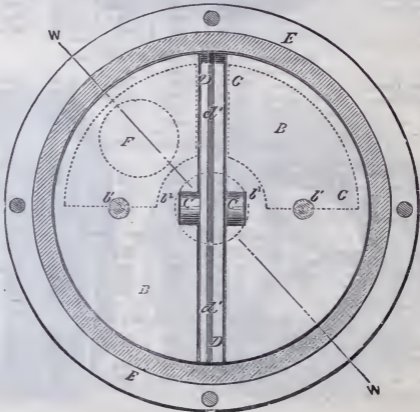


## Rotary Engine, or Water Wheel.

John Lucas, Hastings, Minn.



A slight examination of this device renders it obvious that it will utilize the full power of the water used, less loss from friction and leakage. In case E the Piston wheel B, works in bearings in the case, on shaft A. Wheel and shaft are slotted through the center; in this slot hangs on its pivot C, the Piston D, which oscillates in line with shaft A, as the Piston wheel is rotated by the passing water or steam. Used as a water wheel it does not need packing, consequently seems likely to prove durable, particularly as it does best when running very slow. In testing one, 12 inches in diameter at my flume under 18 feet head, it was found that the percentage increased rapidly as the speed decreased; the screw for tightening the brake was so coarse that the speed could not be got below 126 revolutions per minute without stopping it; at that speed it gave 87 per cent. For driving sewing machines, church organs, printing presses and other light machinery where a high head is available it seems to be the best device yet produced, as, unlike the turbine, it requires but a small supply or discharge pipe, it is noiseless, runs slow and utilizes the full power of the water used whether working at the maximum or minimum of its capacity. It may be placed upon the shaft of the sewing machine and driven by a supply through a small, flexible pipe connected to the sink faucet, or other convenient place. One the size of the illustration herewith would be abundant in capacity under the ordinary city pressure.



## Success Turbine, S. M. Smith, York, Pa.

Downward discharge. Only one wheel tested, that tested several times; first as it came to the flume, then it was taken to machine shop, put in proper condition and again tested.



| Head. | Weight. | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|-------|---------|------------------|-------|-------------|-----------|
| 18.22 | 330     | 197              | 29.55 | 1137        | .7564     |
| 18.32 | 300     | 198              | 27.00 | 1022        | .7647     |
| 18.43 | 240     | 204.5            | 22.61 | 877         | .7419     |
| 18.56 | 175     | 193.7            | 15.41 | 662         | .6653     |

### Second Test of Same.

| Head. | Weight. | Rev. per minute. | H. P. | Cub c feet. | Per Cent. |
|-------|---------|------------------|-------|-------------|-----------|
| 18.30 | 340     | 198.5            | 30.67 | 1095        | .8119     |
| 18.35 | 315     | 203.7            | 29.16 | 1025        | .8198     |
| 18.55 | 220     | 202.5            | 20.25 | 742         | .7800     |
| 18.64 | 160     | 202.5            | 14.72 | 593         | .7064     |

## Bollinger Turbine, O. J. Bollinger, York, Pa.

| Central Discharge. | Head. | Weight. | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|--------------------|-------|---------|------------------|-------|-------------|-----------|
| Whole Gate,.....   | 18.21 | 370     | 193              | 32.45 | 1343.25     | .7034     |
| Part Gate,.....    | 18.24 | 340     | 187.5            | 28.97 | 1196.20     | .7042     |
| " ".....           | 18.40 | 250     | 190              | 21.59 | 948.11      | .6577     |
| " ".....           | 18.58 | 160     | 193.5            | 14.07 | 678.43      | .5784     |

## Delphos Turbine, Delphos, Ohio.



### Test of a 24-inch Wheel.

| Head. | Weight. | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|-------|---------|------------------|-------|-------------|-----------|
| 18.38 | 280     | 248.             | 21.04 | 786.52      | .7726     |
| 18.43 | 205     | 246.5            | 15.31 | 696.78      | .6329     |
| 18.60 | 115     | 248.5            | 8.65  | 540.57      | .4567     |
| 18.76 | 55      | 204              | 3.40  | 373.06      | .2582     |

### Another 24-inch Wheel.

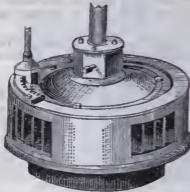
|                  | Head. | Weight. | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|------------------|-------|---------|------------------|-------|-------------|-----------|
| Whole Gate,..... | 18.38 | 275     | 246.6            | 20.55 | 806.70      | .7350     |
| Part Gate,.....  | 18.42 | 235     | 238              | 16.94 | 750.58      | .6498     |
| " ".....         | 18.47 | 170     | 246.5            | 12.69 | 654.01      | .5570     |
| " ".....         | 18.56 | 95      | 247              | 7.11  | 505.31      | .4025     |

### Test of a 36-inch Wheel.

|                  | Head. | Weight. | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|------------------|-------|---------|------------------|-------|-------------|-----------|
| Whole Gate,..... | 18.18 | 700     | 175              | 55.68 | 2069.54     | .7856     |
| Part Gate,.....  | 18.25 | 510     | 173.5            | 40.22 | 1785.56     | .6552     |
| " ".....         | 18.38 | 320     | 176              | 25.60 | 1483.77     | .4983     |
| " ".....         | 18.54 | 120     | 173              | 9.24  | 1041.36     | .2540     |

## National Water Wheel Co., Bristol, Conn.

## J. T. CASE WHEEL.



Made with sixteen chutes, in groups of four each, as shown in cut. Thin outside register gate, so arranged that four, eight, twelve, or the whole sixteen may be closed as desired, in order to utilize one-fourth, one-half, three-fourths or the whole discharge advantageously. The wheel has central and downward discharge, and is claimed to be like the Swain, but in reality has little resemblance to that wheel. The Company have had about a dozen different wheels tested at my flume; the results may be found below and on next page. The "part gates" revolutions are those that gave the highest results.

Test of 30-inch, Aug. 19, 1872.

|                        | Head. | Weight. | Rev. per minute. | Horse Power. | Cubic Feet. | Per Cent. |
|------------------------|-------|---------|------------------|--------------|-------------|-----------|
| Whole Gate,.....       | 18.35 | 500     | 133              | 30.23        | 1477.64     | .610      |
| 12 chutes opened,..... | 18.61 | 265     | 153              | 18.43        | 900.34      | .583      |
| 8 chutes opened,.....  | 18.78 | 150     | 154.5            | 10.53        | 588.99      | .505      |
| 4 chutes opened,.....  | 18.19 | 65      | 141              | 4.16         | 336.80      | .377      |

Test of 20-inch, August 22, 1872.

|                        |       |       |       |       |        |      |
|------------------------|-------|-------|-------|-------|--------|------|
| Whole Gate,.....       | 18.63 | 187.5 | 237.2 | 20.78 | 773.98 | .763 |
| 4 chutes opened,.....  | 19.03 | 30    | 249   | 3.39  | 215.66 | .438 |
| 8 chutes opened,.....  | 18.88 | 95    | 247   | 10.36 | 492.99 | .590 |
| 12 chutes opened,..... | 18.80 | 160   | 237.5 | 17.67 | 700.59 | .712 |

Another 20-inch, in same curb, but with different shaped buckets.

|                        |       |      |       |       |        |      |
|------------------------|-------|------|-------|-------|--------|------|
| Whole Gate,.....       | 18.63 | 180  | 249   | 20.37 | 765.59 | .758 |
| 4 chutes opened,.....  | 19.07 | 27.5 | 242.5 | 3.03  | 218.16 | .386 |
| 8 chutes opened,.....  | 18.86 | 80   | 248.5 | 9.04  | 424.76 | .599 |
| 12 chutes opened,..... | 18.70 | 130  | 252   | 14.89 | 610.48 | .692 |

Another 20-inch, different from the others, same curb.

|                        |       |     |       |       |        |      |
|------------------------|-------|-----|-------|-------|--------|------|
| Whole Gate,.....       | 18.61 | 155 | 342.5 | 17.08 | 700.80 | .695 |
| 12 chutes opened,..... | 18.81 | 110 | 254.5 | 12.42 | 545.32 | .642 |
| 8 chutes opened,.....  | 18.95 | 75  | 247   | 8.34  | 386.29 | .604 |
| 4 chutes opened,.....  | 19.12 | 25  | 242.5 | 2.75  | 199.21 | .383 |

Another wheel in same curb, but with compound register gate.

|                        |       |     |       |       |        |      |
|------------------------|-------|-----|-------|-------|--------|------|
| Whole Gate,.....       | 18.91 | 140 | 247.5 | 15.75 | 616.96 | .716 |
| 12 chutes opened,..... | 19.05 | 70  | 249   | 7.92  | 373.37 | .591 |
| 8 chutes opened,.....  | 19.13 | 40  | 248   | 4.31  | 257.32 | .464 |
| 4 chutes opened,.....  | 19.23 | 20  | 197.5 | 1.79  | 150.85 | .327 |

Test of a 24-inch wheel in shape like the Houston, Sept. 27, 1872.

|                                |       |     |       |       |        |      |
|--------------------------------|-------|-----|-------|-------|--------|------|
| Whole Gate,.....               | 18.84 | 180 | 175   | 14.31 | 843.14 | .477 |
| Part Gate,.....                | 18.91 | 135 | 186.5 | 11.44 | 699.47 | .456 |
| Part Gate,.....                | 18.99 | 95  | 178.5 | 7.71  | 544.45 | .395 |
| Head Reduced, Whole Gate,..... | 12.43 | 100 | 655.1 | 7.52  | 647.55 | .495 |

Another of the same kind and shape.

|                                |       |     |       |       |        |      |
|--------------------------------|-------|-----|-------|-------|--------|------|
| Whole Gate,.....               | 18.79 | 160 | 195   | 14.18 | 832.16 | .480 |
| Head Reduced, Whole Gate,..... | 12.25 | 110 | 139.5 | 6.97  | 665.39 | .453 |

Test of a 40-inch, January 21st, 1873.

|                        |       |     |       |       |         |      |
|------------------------|-------|-----|-------|-------|---------|------|
| Whole Gate,.....       | 17.76 | 650 | 163.5 | 48.30 | 1974.81 | .729 |
| 12 chutes opened,..... | 18.40 | 450 | 158   | 32.31 | 1510.78 | .616 |
| 8 chutes opened,.....  | 18.85 | 245 | 158   | 17.59 | 1031.50 | .479 |
| 4 chutes opened,.....  | 19.26 | 65  | 156   | 4.61  | 618.24  | .205 |

## J. T. CASE WHEEL.

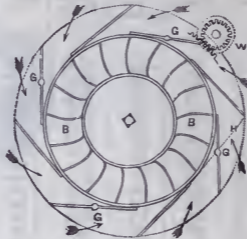
| No. of Test.                      | Head. | Weight. | Rev. per Minute. | Horse Power. | Weir. | Cubic Feet. | Per Cent. |
|-----------------------------------|-------|---------|------------------|--------------|-------|-------------|-----------|
| Whole Gate, 1...                  | 17.85 | 600     | 174              | 47.42        | 1.046 | 2038.74     | .689      |
| " 2...                            | 17.82 | 620     | 178              | 50.16        | 1.050 | 2050.56     | .726      |
| " 3...                            | 17.78 | 650     | 168.5            | 49.78        | 1.054 | 2061.36     | .719      |
| " 4...                            | 17.75 | 675     | 165              | 50.62        | 1.057 | 2070.31     | .729      |
| " 5...                            | 17.73 | 700     | 162.5            | 51.70        | 1.064 | 2092.16     | .737      |
| " 6...                            | 17.70 | 725     | 160              | 52.72        | 1.070 | 2110.10     | .747      |
| " 7...                            | 17.69 | 750     | 157              | 53.52        | 1.074 | 2122.10     | .754      |
| " 8...                            | 17.67 | 775     | 155              | 54.60        | 1.080 | 2140.06     | .764      |
| " 9...                            | 17.63 | 800     | 153              | 55.63        | 1.084 | 2152.08     | .776      |
| " 10...                           | 17.62 | 825     | 150              | 56.25        | 1.088 | 2163.51     | .781      |
| " 11...                           | 17.62 | 850     | 146              | 56.41        | 1.088 | 2163.51     | .783      |
| " 12...                           | 17.61 | 875     | 144              | 57.27        | 1.090 | 2170.14     | .793      |
| " 13...                           | 17.60 | 900     | 142              | 55.09        | 1.096 | 2188.26     | .774      |
| " 14...                           | 17.58 | 925     | 132              | 55.50        | 1.100 | 2200.36     | .759      |
| " 15...                           | 17.58 | 950     | 123              | 53.11        | 1.104 | 2212.48     | .722      |
| <b>Head Reduced.</b>              |       |         |                  |              |       |             |           |
| Whole Gate, 17...                 | 12.15 | 650     | 111              | 32.79        | .972  | 1825.86     | .782      |
| " 18...                           | 12.14 | 625     | 117              | 33.24        | .970  | 1819.74     | .796      |
| " 19...                           | 12.15 | 600     | 118.5            | 32.32        | .968  | 1814.02     | .776      |
| " 20...                           | 12.17 | 575     | 122.5            | 32.01        | .965  | 1805.47     | .771      |
| " 21...                           | 12.15 | 615     | 117              | 32.71        | .969  | 1816.97     | .784      |
| " 22...                           | 12.14 | 635     | 115              | 33.19        | .972  | 1825.86     | .792      |
| <b>Head Reduced.</b>              |       |         |                  |              |       |             |           |
| Whole Gate 24...                  | 6.74  | 350     | 84               | 13.36        | .802  | 1361.90     | .770      |
| " 25...                           | 6.71  | 330     | 80.8             | 13.22        | .803  | 1364.51     | .765      |
| " 26...                           | 6.70  | 370     | 77.5             | 13.00        | .805  | 1369.84     | .749      |
| " 27...                           | 6.73  | 340     | 86               | 13.29        | .801  | 1359.39     | .769      |
| " 28...                           | 6.75  | 330     | 87               | 13.05        | .800  | 1356.78     | .754      |
| Part Gate,<br>12 p'ts op'n, 30... | 17.84 | 800     | 132.6            | 48.22        | .944  | 1743.95     | .820      |
| 8 " " 31...                       | 18.04 | 400     | 134              | 24.35        | .730  | 1173.98     | .609      |
| 8 " " 32...                       | 18.41 | 350     | 142              | 22.48        | .712  | 1129.28     | .560      |
| 8 " " 33...                       | 18.32 | 500     | 120              | 27.27        | .749  | 1221.74     | .646      |
| 8 " " 34...                       | 18.94 | 150     | 139              | 9.48         | .512  | 670.49      | .395      |

| Test of 50 inch, Aug. 1873. | Head. | Weight. | Rev. per minute. | Horse Power. | Cubic Feet. | Per Cent. |
|-----------------------------|-------|---------|------------------|--------------|-------------|-----------|
| Whole Gate, .....           | 16.39 | 1500    | 114              | 103.63       | 4627.66     | .7242     |
| " .....                     | 16.37 | 1600    | 111              | 107.63       | 4721.55     | .7381     |
| " .....                     | 16.37 | 1700    | 105.6            | 108.80       | 4801.70     | .7356     |
| " .....                     | 16.35 | 1800    | 101.5            | 110.72       | 4836.17     | .7422     |
| " .....                     | 16.34 | 1900    | 97               | 111.70       | 4840.00     | .7486     |
| " .....                     | 16.35 | 2000    | 92               | 111.50       | 4874.55     | .7415     |

At Unionville, Conn., Platner & Porter M'g Co., I tested the power of one of the latest style National wheels; it was far below its table rate for power, and so extraordinarily extravagant in the use of water that it was immediately removed to make room for one of a better kind.

## Angell Wheel, Providence, R. I.

Double discharge, gates similar to Leffel, though each alternate piece forming side of chutes is stationary, as represented in the diagram. Buckets bolted to hub of wheel, and often shear off.



TEST OF A 36-INCH WHEEL.

| No. of Test.               | Head  | Weight. | Rev. per Min. | Horse Power | Cubic feet. | Per Cent. |
|----------------------------|-------|---------|---------------|-------------|-------------|-----------|
| May, 1873, Whole Gate,.... | 17.96 | 880     | 147.3         | 58.92       | 2328.86     | .7451     |
| $\frac{7}{8}$ Gate,.....   | 18.12 | 790     | 143           | 51.35       | 2052.24     | .7305     |
| $\frac{3}{4}$ " .....      | 18.29 | 650     | 145.5         | 42.99       | 1760.51     | .7063     |
| $\frac{1}{2}$ " .....      | 18.47 | 475     | 140           | 30.22       | 1362.77     | .6366     |
| $\frac{1}{4}$ " .....      | 18.48 | 370     | 142           | 23.85       | 1179.99     | .5786     |

A 30-INCH WHEEL SENT TO BE TESTED.

| No. of Test.             | Head. | Weight. | Rev. per Min. | Horse Power. | Cubic feet. | Per Cent. |
|--------------------------|-------|---------|---------------|--------------|-------------|-----------|
| Nov. 3, Whole Gate,..... | 18.27 | 520     | 184           | 43.50        | 1475.36     | .8539     |
| $\frac{7}{8}$ Gate,..... | 18.31 | 490     | 184           | 40.98        | 1398.86     | .8465     |
| $\frac{3}{4}$ " .....    | 18.46 | 380     | 182.5         | 31.09        | 1094.11     | .8114     |
| $\frac{1}{2}$ " .....    | 18.54 | 270     | 187           | 22.95        | 902.17      | .7260     |
| 7-16 " .....             | 18.65 | 190     | 184.5         | 14.25        | 677.38      | .5968     |

On report of results, a wheel of the same size and made in same lot was sold to Otto Troost, of Winona, Minn., sent to me to be tested for verification. Results are here given.

| No. of Test.              | Head. | Weight. | Rev. per Min. | Horse Power. | Cubic feet. | Per Cent. |
|---------------------------|-------|---------|---------------|--------------|-------------|-----------|
| Dec. 15, Whole Gate,..... | 18.40 | 520     | 176.6         | 41.74        | 1583.40     | .7579     |
| " .....                   | 18.43 | 500     | 180.6         | 41.04        | 1575.21     | .7479     |
| " .....                   | 18.42 | 480     | 186.5         | 40.66        | 1564.21     | .7465     |
| " .....                   | 18.47 | 550     | 167           | 41.11        | 1616.24     | .7285     |

Of course the wheel was rejected; then the wheel tested, Nov. 3, was repaired by the Angell Company, and returned to fill the order. It was placed in the flume, and found to run so hard, that I at once refused to test it until put in order; it was taken out and reset some five or six times, but could never be got in condition to run, so that it would not require thirty or forty pounds to start it, where ten should have done so, and the wheel was returned to the shop for inspection.

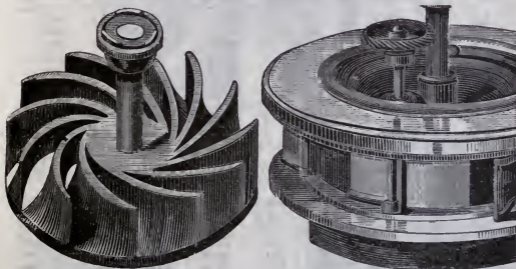
January 14, 1874, a 48 inch wheel was sold conditionally to take the place of a Leffel, where at least 80 per cent. average useful effect was required; it was sent to be tested, and gave the following results:

| No. of Test.     | Head. | Weight. | Rev. per Min. | Horse Power. | Cubic feet. | Per Cent. |
|------------------|-------|---------|---------------|--------------|-------------|-----------|
| Whole Gate,..... | 17.62 | 1450    | 108           | 94.90        | 3802.70     | .7667     |
| Part Gate,.....  | 17 88 | 1180    | 108.2         | 77.38        | 3158.79     | .7249     |
| " .....          | 18.02 | 1000    | 105.4         | 68.88        | 2765.80     | .6780     |
| " .....          | 18.21 | 750     | 108           | 49.09        | 2271.58     | .6279     |
| " .....          | 18.42 | 500     | 102           | 30.90        | 1698.00     | .5228     |
| " .....          | 18.46 | 450     | 108.2         | 29.50        | 1709 18     | .4947     |

TEST OF A 40-INCH WHEEL, AT FITCHBURG, MASS., JULY 2, 1872.

| Head in Feet.           | Weir. | Rev. per Minute. | Weight. | Horse Power. | Cubic ft. Discharg'd | Percentage. |
|-------------------------|-------|------------------|---------|--------------|----------------------|-------------|
| 21.80                   | 10.85 | 240              | 260     | 28.36        | 1757 47              | .3999       |
| 21.63                   | 11.18 | 215              | 310     | 30.29        | 1837 70              | .4034       |
| 20.99                   | 14.00 | 156              | 510     | 36.16        | 2555.08              | .3502       |
| Tabled rate, same head, |       | 280              |         | about 103    | about 2800           | .9000       |

Flenniken Brothers, Rockford, Ill.



Test of a 20-inch wheel.

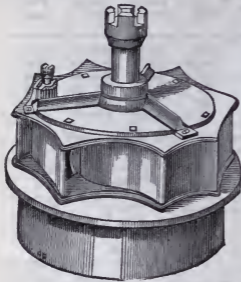
|                  | Head. | Weight. | Rev. per minute. | Horse Power. | Cubic feet. | Per Cent. |
|------------------|-------|---------|------------------|--------------|-------------|-----------|
| Whole Gate,..... | 18.37 | 110     | 342              | 17 10        | 605.44      | .8083     |
| Part Gate,.....  | 18.49 | 90      | 315              | 12.88        | 524.43      | .7025     |
| " .....          | 18.53 | 60      | 321              | 8 75         | 448.92      | .5566     |
| " .....          | 18.63 | 35      | 351              | 5.58         | 362.70      | .4368     |
| " .....          | 18.72 | 20      | 280              | 2.54         | 278.14      | .2244     |

Gardiner Cox, Ellsworth, N. Y.

Furnished a wheel that he called double; it consisted of a hub, with a Jonval wheel around its lower end, the buckets above being continued by sheet iron spirals to the top of the hub, forming a twelve threaded screw, the pitch being twelve degrees from line of rotation.



## T. H. Risdon &amp; Co., Mount Holly, N. J.



Mr. Risdon seems to have a passion for the turbine business, and has continued to experiment for many years to an almost unlimited extent; his first experiment at my flume was in 1871, with a 30-inch Vandewater wheel in a curb here represented. It gave a useful effect of .7714 per cent. He then tried a 36-inch of the same kind, which gave .7871 per cent. His next effort was with a wheel of his own designing; (see next page, Fig. 2;) but in a curb similar to that used by the National Water Wheel Co., of Bristol, Conn. The test is given in full in the second table below. As may be seen, the part gates were not proportionally good, while the rim of the curb was so nearly divided by the ports that it was too fragile for durability, consequently it was abandoned and a new one, represented by cut B was constructed; in that, the following results were obtained by the test of a 43-inch wheel.

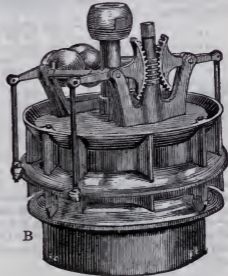
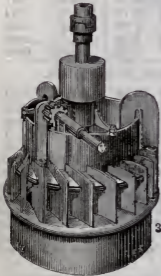
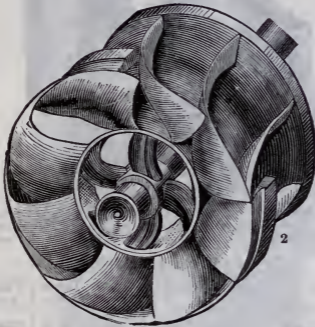
| Head. | Weight. | Rev. per min. | H. Power. | Cubic feet. | Percentage. |
|-------|---------|---------------|-----------|-------------|-------------|
| 17.91 | 1200    | 151           | 82.36     | 2664.03     | .9132       |
| 17.93 | 1200    | 148           | 80.72     | 2676.91     | .8897       |
| 17.92 | 1200    | 148.3         | 80.89     | 2680.14     | .8910       |
| 17.90 | 1250    | 144.5         | 82.10     | 2689.82     | .9021       |
| 17.98 | 1150    | 146.5         | 76.58     | 2469.92     | .9121       |
| 18.00 | 1200    | 137.5         | 75.00     | 2495.13     | .8834       |
| 18.17 | 1000    | 147           | 66.82     | 2258.84     | .8613       |
| 18.29 | 850     | 150           | 57.95     | 2012.82     | .8331       |
| 18.30 | 700     | 138.6         | 44.10     | 1686.07     | .7559       |
| 18.43 | 650     | 148           | 43.72     | 1686.07     | .7459       |

| No. of Test.         | Head. | Weight. | Rev.  | Horse Power. | Weir. | Cubic Feet. | Per Cent. |
|----------------------|-------|---------|-------|--------------|-------|-------------|-----------|
| Whole Gate, 1...     | 18.25 | 700     | 163.5 | 52.02        | 1.193 | 1749.33     | .863      |
| " 2...               | 18.25 | 750     | 151.5 | 51.65        | 1.201 | 1766.64     | .850      |
| " 3...               | 18.28 | 705     | 162.5 | 52.07        | 1.196 | 1755.81     | .869      |
| " 4...               | 18.28 | 710     | 162   | 52.28        | 1.196 | 1755.81     | .863      |
| " 5...               | 18.30 | 715     | 160   | 52.00        | 1.199 | 1762.29     | .854      |
| " 6...               | 18.32 | 720     | 159.6 | 52.20        | 1.199 | 1762.29     | .856      |
| " 7...               | 18.34 | 725     | 158.6 | 52.26        | 1.200 | 1764.47     | .854      |
| " 8...               | 18.33 | 730     | 157.6 | 52.29        | 1.201 | 1766.64     | .855      |
| " 9...               | 18.32 | 735     | 156.5 | 52.29        | 1.202 | 1768.81     | .854      |
| " 10...              | 18.32 | 740     | 155.5 | 52.30        | 1.201 | 1766.64     | .856      |
| " 11...              | 18.34 | 745     | 155   | 52.48        | 1.202 | 1768.81     | .857      |
| " 12...              | 18.32 | 750     | 153   | 52.16        | 1.203 | 1770.98     | .832      |
| " 13...              | 18.34 | 760     | 149.5 | 51.65        | 1.203 | 1770.98     | .842      |
| " 14...              | 18.34 | 690     | 167   | 52.37        | 1.199 | 1762.29     | .858      |
| " 15...              | 18.34 | 680     | 169   | 52.24        | 1.198 | 1760.13     | .857      |
| " 16...              | 18.35 | 670     | 171.5 | 52.22        | 1.197 | 1757.97     | .858      |
| 1 Pt. closed, 18...  | 18.51 | 560     | 154   | 39.20        | 1.047 | 1442.53     | .779      |
| " 19...              | 18.51 | 545     | 158   | 39.14        | 1.045 | 1438.45     | .778      |
| 2 Pts. closed, 21... | 18.85 | 190     | 162   | 13.99        | .723  | 831.05      | .473      |
| Whole Gate, 22...    | 18.37 | 745     | 154.6 | 52.35        | 1.200 | 1764.47     | .855      |

## T. H. Risdon &amp; Co., Mount Holly, N. J.

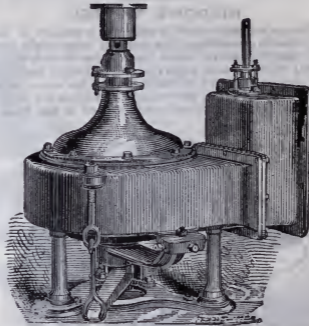
## RISDON'S WHEEL.

Of the many Risdon wheels tested by me, quite a number of them have ranged along in the seventies in percentage, but through some slight change after a first trial every wheel tested, (except two or three of the 20-inch size) has been made to return a useful effect of over eighty per cent. before delivery to purchaser, quite a number from eighty-five to ninety, and a few even higher than ninety. Figure 3 represents the curb Mr. Risdon now considers the best, but he also furnishes wheels in the register gate curb, represented at the head of the opposite page.



| Test of a 20-inch. | Head. | Weight. | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|--------------------|-------|---------|------------------|-------|-------------|-----------|
| Whole Gate,.....   | 18.58 | 175     | 295.5            | 15.67 | 640.26      | .7131     |
| Part Gate,.....    | 18.62 | 165     | 300              | 15.00 | 593.93      | .7175     |
| " " .....          | 18.67 | 165     | 272.5            | 13.62 | 540.42      | .7143     |
| " " .....          | 18.68 | 140     | 308              | 13.06 | 532.32      | .6936     |

## Tyler's New Scroll Wheel.



Scroll wheels are passing away, still there are many places yet where they may be advantageously used; of the many plans devised for this class of wheels, John Tyler of Claremont, N. H., has undoubtedly produced the very best, and decidedly so.

Test of a 30-inch, Sept. 19, 1873.

| Whole Gate.       | Head. | Weight. | Rev. per minute. | Horse Power. | Cubic feet. | Per Cent. |
|-------------------|-------|---------|------------------|--------------|-------------|-----------|
| Whole Gate, ..... | 18.30 | 385     | 189              | 33.07        | 1208.65     | .7917     |
| Part Gate, .....  | 18.32 | 330     | 196.5            | 29.78        | 1121.64     | .7674     |
| " .....           | 18.41 | 200     | 187              | 17.00        | 900.47      | .5433     |
| " .....           | 18.50 | 60      | 192              | 5.24         | 718.35      | .2088     |
| " .....           | 18.54 | 17.5    | 183              | 1.46         | 680.58      | .0612     |

Wheel reset and made to run easier, then re-tested, Sept. 23, 1873.

|                   |       |     |       |       |         |       |
|-------------------|-------|-----|-------|-------|---------|-------|
| Whole Gate, ..... | 18.48 | 390 | 191   | 33.86 | 1188.49 | .8164 |
| Part Gate, .....  | 18.55 | 330 | 195.5 | 29.33 | 1097.36 | .7630 |
| " .....           | 18.62 | 250 | 191   | 21.71 | 954.50  | .6469 |
| " .....           | 18.65 | 200 | 197.5 | 17.95 | 892.28  | .5713 |
| " .....           | 18.72 | 100 | 185   | 8.41  | 730.75  | .3256 |

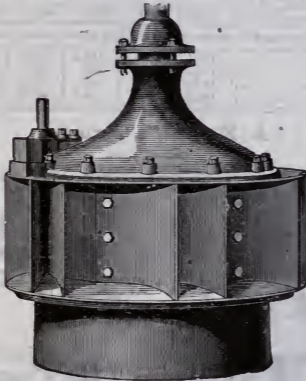
This wheel was kept as a sample wheel; its gate raises  $13\frac{1}{2}$  inches; the opening to scroll being  $13\frac{1}{2} \times 12$ , while the openings in wheel equalled 218 square inches; raising the gate three inches caused a discharge of one-half that could pass through the wheel at whole gate. February 1st, 1877, the buckets of this wheel were slightly chipped on the edge, then it was sent to me to be tested, but without any intimation that it was the same previously tried. The weather was bad at the time and it stood exposed for two weeks; was then set and tested with the ordinary care.

|  | Head. | Weight. | Rev. per minute. | Horse Power. | Cubic feet. | Per Cent. |
|--|-------|---------|------------------|--------------|-------------|-----------|
| Gate opened $13\frac{1}{2}$ inches, .... | 18.47 | 360     | 202.2            | 33.08        | 1179.66     | .8050     |
| " " 9 inches, .....                      | 18.52 | 300     | 204              | 27.81        | 1074.91     | .7407     |
| " " 8 inches, .....                      | 18.59 | 225     | 201.5            | 20.61        | 927.18      | .6421     |
| " " 7 inches, .....                      | 18.65 | 150     | 193.3            | 13.17        | 795.14      | .4709     |

## Tyler's Flume Wheel and Curb.

John Tyler, Claremont, N. H.

This curb has an inside register gate, one side of each chute being cast in chute rim; the other part is bolted to the register hoop or gate. The wheel is the same whether used in scroll or flume curb.



Test of 30-inch Flume wheel.

| April 20, 1876.  | Head. | Weight. | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|------------------|-------|---------|------------------|-------|-------------|-----------|
| Whole Gate,..... | 18.43 | 375     | 168.6            | 28.72 | 1245.64     | .6618     |
| Part Gate,.....  | 18.44 | 360     | 169.2            | 27.68 | 1207.50     | .6677     |
| “ “ .....        | 18.65 | 185     | 167.5            | 14.08 | 722.18      | .5530     |

Buckets were chipped back. Re-tested April 21.

|                   |       |     |       |       |         |       |
|-------------------|-------|-----|-------|-------|---------|-------|
| Whole Gate, ..... | 18.65 | 375 | 202   | 34.43 | 1226.55 | .7970 |
| Part Gate,.....   | 18.62 | 325 | 196.5 | 29.01 | 1094.45 | .7531 |
| “ “ .....         | 18.84 | 190 | 202   | 17.45 | 755.40  | .6487 |

Buckets chipped back more and gate opening enlarged. Again tested April 22

|                   |       |     |       |       |         |       |
|-------------------|-------|-----|-------|-------|---------|-------|
| Whole Gate, ..... | 18.50 | 385 | 215.3 | 37.67 | 1180    | .9127 |
| Part Gate,.....   | 18.60 | 325 | 215   | 31.76 | 1037.38 | .8709 |
| “ “ .....         | 18.67 | 275 | 212.5 | 26.56 | 914.01  | .8234 |
| “ “ .....         | 18.76 | 220 | 213.5 | 21.35 | 764.49  | .7880 |
| “ “ .....         | 18.85 | 160 | 215   | 15.63 | 602.53  | .7280 |
| “ “ .....         | 18.93 | 105 | 213.5 | 10.18 | 465.71  | .6109 |
| “ “ .....         | 19.01 | 60  | 197   | 5.37  | 334.25  | .4471 |

Chipping the buckets threw the wheel out of balance so that it was returned to builders, where it was balanced by drilling holes on heavy side and filling them with wood; the wheel was smoothed up generally, then sent to Centennial test, then sent to me for re-test; on trying it again it was found that some change

had been made that rendered it almost impossible to control it with brake. Re-tested Feb. 13, 1877.

|                   | Head. | Weight. | Rev. per minute. | Horse Power. | Cubic feet. | Per Cent. |
|-------------------|-------|---------|------------------|--------------|-------------|-----------|
| Whole Gate, ..... | 18.9  | 375     | 221              | 37.67        | 1318.42     | .8242     |

The wheel was taken to machine shop, altered and re-tested four times, but without material change in results.

Oct. 13, 1877, tested 42-inch Tyler Flume wheel.

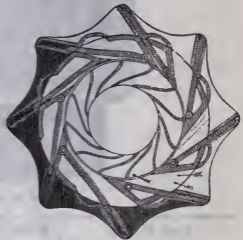
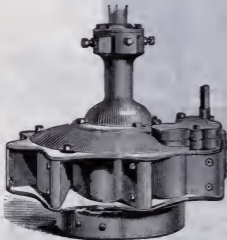
|                   |       |      |     |       |         |       |
|-------------------|-------|------|-----|-------|---------|-------|
| Whole Gate, ..... | 18.10 | 1000 | 146 | 66.36 | 2619.73 | .7409 |
|-------------------|-------|------|-----|-------|---------|-------|

Taken to machine shop and alterations made, then re-tested.

|                   |       |      |       |       |         |       |
|-------------------|-------|------|-------|-------|---------|-------|
| Whole Gate, ..... | 18.01 | 1025 | 146.5 | 68.24 | 2586.61 | .7750 |
| Part Gate, .....  | 18.15 | 800  | 152   | 55.27 | 2181.25 | .7391 |
| " " .....         | 18.25 | 725  | 144   | 47.45 | 1917.22 | .7181 |
| " " .....         | 18.27 | 750  | 130.5 | 44.48 | 1843.14 | .6992 |

### A. N. Wolf's Turbine.

Manufactured by Barber & Sons, Allentown, Pa.



The first Wolf wheels sent to be tested gave exceeding good results and were reported accordingly, which caused manufacturers to order others; as these were sent to be tested they were found to be not only less efficient, but also not well made. The 48-inch wheel reported on next page was ordered for the Newton & Ramage Paper Co. of Holyoke; it was so poorly made that while handling it in order to lower it into testing flume it came apart and the wheel dropped to the bottom; it was sent to machine shop and put into much better condition than when first received. The edges of the buckets were left by the builders square, varying in thickness from one-half to three-fourths of an inch; these were partially rounded, then the wheel was tested, giving the results reported. Mr. Wolf took the wheel out and chipped the buckets to an edge, made it run easier then had it tested again, obtaining the results reported of second 48-inch wheel. In examining the wheel and curb I found the casting to be so thin as to be hardly safe for the pressure of the 24 feet head for which it was ordered; the crown plate or cover was five feet in diameter. Mr. Barber insisted that it was three-fourths of an inch in thickness, but on drilling through, it was found to be but three-eighths; it was rejected.

Test of 24-inch. Multiply revolutions of wheel by 10 to get speed for computing power.

|                   | Head. | Weight. | Rev.per Min. | Horse Power. | Cubic feet. | Per Cent. |
|-------------------|-------|---------|--------------|--------------|-------------|-----------|
| Whole Gate, ..... | 18.21 | 425     | 255.3        | 32.87        | 1134.57     | .8436     |
| Part Gate, .....  | 18.29 | 400     | 240          | 29.09        | 1002.07     | .8416     |
| " " .....         | 18.41 | 325     | 247.5        | 24.37        | 853.76      | .8202     |
| " " .....         | 18.55 | 250     | 249          | 18.86        | 673.63      | .8003     |
| " " .....         | 18.69 | 150     | 234.5        | 10.65        | 445.86      | .6777     |

Test of a second 24-inch. Multiply revolutions by 10.

|                   |       |     |       |       |         |       |
|-------------------|-------|-----|-------|-------|---------|-------|
| Whole Gate, ..... | 18.45 | 420 | 255   | 32.45 | 1166.27 | .7997 |
| Part Gate, .....  | 18.50 | 350 | 252   | 26.72 | 1004.33 | .7626 |
| " " .....         | 18.55 | 300 | 250   | 22.72 | 884.27  | .7374 |
| " " .....         | 18.73 | 175 | 251.5 | 13.33 | 628.87  | .6001 |
| " " .....         | 18.83 | 80  | 248   | 6.01  | 445.39  | .3018 |

Test of a third 24-inch. Multiply revolutions by 15.

|                   |       |     |       |       |         |       |
|-------------------|-------|-----|-------|-------|---------|-------|
| Whole Gate, ..... | 18.23 | 280 | 253.5 | 32.26 | 1164.28 | .8078 |
| Part Gate, .....  | 18.32 | 220 | 262.2 | 26.22 | 1001.40 | .7578 |
| " " .....         | 18.41 | 190 | 261.5 | 22.53 | 891.93  | .7275 |
| " " .....         | 18.47 | 150 | 262.5 | 17.89 | 755.83  | .6796 |

Test of a fourth 24-inch.

|                   |       |     |       |       |         |       |
|-------------------|-------|-----|-------|-------|---------|-------|
| Whole Gate, ..... | 18.20 | 300 | 245   | 33.40 | 1183.46 | .8206 |
| Part Gate, .....  | 18.24 | 270 | 243   | 29.82 | 1093.77 | .7910 |
| " " .....         | 18.38 | 220 | 241   | 24.10 | 922.11  | .7700 |
| " " .....         | 18.45 | 170 | 251.3 | 19.41 | 791.52  | .7033 |
| " " .....         | 18.70 | 75  | 235.5 | 8.92  | 470.67  | .5376 |

Test of a 30-inch. Multiply revolutions by 15.

|                   |       |     |       |       |         |       |
|-------------------|-------|-----|-------|-------|---------|-------|
| Whole Gate, ..... | 17.86 | 500 | 183.5 | 41.70 | 1547.74 | .8000 |
| Part Gate, .....  | 18.01 | 435 | 182.5 | 36.08 | 1325.98 | .8011 |
| " " .....         | 18.06 | 400 | 180.5 | 32.81 | 1233.06 | .7814 |
| " " .....         | 18.43 | 230 | 182.5 | 19.07 | 819.71  | .6850 |

Test of a 36-inch. Multiply revolutions by 15.

|                   |       |     |       |       |         |       |
|-------------------|-------|-----|-------|-------|---------|-------|
| Whole Gate, ..... | 18.03 | 825 | 160.7 | 60.26 | 2308.08 | .7665 |
| Part Gate, .....  | 18.02 | 825 | 161.5 | 60.25 | 2248.75 | .7699 |
| " " .....         | 18.12 | 700 | 160   | 50.91 | 1958.80 | .7594 |
| " " .....         | 18.27 | 550 | 149   | 37.25 | 1507.43 | .7161 |
| " " .....         | 18.49 | 300 | 157.2 | 21.42 | 983.49  | .6228 |

Test of a 18-inch. Multiply revolutions by 10.

|                   |       |     |       |       |        |       |
|-------------------|-------|-----|-------|-------|--------|-------|
| Whole Gate, ..... | 18.38 | 165 | 304   | 15.20 | 579.07 | .7574 |
| Part Gate, .....  | 18.50 | 160 | 287   | 13.91 | 517.71 | .7702 |
| " " .....         | 18.55 | 135 | 291.5 | 11.92 | 454.00 | .7506 |
| " " .....         | 18.59 | 105 | 267   | 9.30  | 357.42 | .7425 |
| " " .....         | 18.61 | 80  | 315   | 7.63  | 338.38 | .6422 |

Test of a 48-inch. Sent to machine shop for alterations. Multiply revolutions by 20.

|                   |       |      |       |       |         |       |
|-------------------|-------|------|-------|-------|---------|-------|
| Whole Gate, ..... | 17.47 | 1525 | 90    | 83.18 | 3618.81 | .6982 |
| Part Gate, .....  | 17.65 | 1000 | 121   | 73.33 | 3110.36 | .7088 |
| " " .....         | 18.01 | 600  | 111.5 | 40.54 | 2127.43 | .5615 |

Test of the 48 a second time. Rejected by intended purchaser.

|                   |       |      |       |       |         |       |
|-------------------|-------|------|-------|-------|---------|-------|
| Whole Gate, ..... | 17.60 | 1300 | 117   | 92.18 | 3640.50 | .7630 |
| Part Gate, .....  | 17.71 | 1250 | 117   | 81.54 | 3263.49 | .7482 |
| " " .....         | 17.80 | 1050 | 118   | 75.09 | 2953.76 | .7562 |
| " " .....         | 17.94 | 875  | 117.3 | 62.20 | 2566.52 | .7165 |
| " " .....         | 18.17 | 700  | 114.3 | 48.49 | 2112.31 | .6701 |

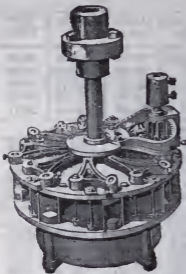
Test of a 54-inch. Rejected by intended purchaser. Multiply revolutions by 20

|                   |       |      |       |        |         |       |
|-------------------|-------|------|-------|--------|---------|-------|
| Whole Gate, ..... | 17.24 | 1700 | 112.6 | 116.01 | 4841.07 | .7373 |
| Part Gate, .....  | 17.42 | 1600 | 106.3 | 103.07 | 4201.41 | .7469 |
| " " .....         | 17.73 | 1000 | 112   | 67.87  | 3107.58 | .6686 |



## Clark &amp; Chapman, Turner's Falls, Mass.

## COLEMAN WHEEL.



Have had several of the kind tested, and the results given herewith, obtained from the test of a 30-inch, represent the general characteristics of the wheel.

| March 31, 1874.  | Head. | Weight. | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|------------------|-------|---------|------------------|-------|-------------|-----------|
| Whole Gate,..... | 18.45 | 425     | 176.3            | 34.15 | 1297.40     | .7584     |
| Part Gate,.....  | 18.57 | 370     | 173              | 29.09 | 1144.55     | .7935     |
| " " .....        | 18.71 | 330     | 174.5            | 26.18 | 963.24      | .7687     |
| " " .....        | 18.66 | 175     | 171.5            | 13.63 | 687.60      | .5696     |

## Wm. F. Mosser &amp; Co., Allentown, Pa.

Two 36-inch wheels. Results below. First wheel had chutes and gate similar to Stout, Mills & Temple curb; wheels downward discharge.

|                  | Head. | Weight. | Rev. per minute. | Horse Power. | Cubic Feet. | Per Cent. |
|------------------|-------|---------|------------------|--------------|-------------|-----------|
| Whole Gate,..... | 17.80 | 770     | 155.5            | 54.32        | 2148.20     | .7545     |
| Part Gate,.....  | 17.87 | 680     | 156.5            | 48.37        | 1866.51     | .7708     |
| " .....          | 17.96 | 580     | 157.5            | 41.52        | 1611.01     | .7610     |
| " .....          | 18.10 | 460     | 156              | 32.62        | 1331.37     | .7195     |
| " .....          | 18.21 | 300     | 169              | 23.00        | 1047.20     | .6709     |
| " .....          | 18.10 | 220     | 157.5            | 15.41        | 802.86      | .5624     |

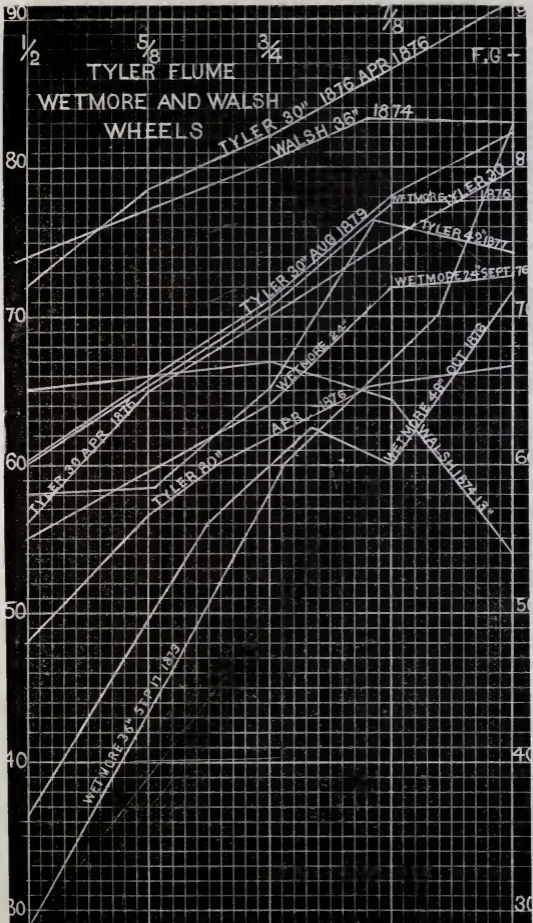
## Test of Second Wheel, Inside Register Gate.

|                  |       |     |       |       |         |       |
|------------------|-------|-----|-------|-------|---------|-------|
| Whole Gate,..... | 18.04 | 725 | 176.5 | 58.44 | 2175.31 | .7879 |
| Part Gate,.....  | 18.10 | 650 | 164.6 | 48.64 | 1916.99 | .7415 |
| " .....          | 18.21 | 520 | 164.5 | 38.88 | 1591.18 | .7100 |
| " .....          | 18.34 | 375 | 163.5 | 27.84 | 1294.82 | .6202 |
| " .....          | 18.45 | 245 | 165   | 18.40 | 1008.06 | .5234 |

## "Excelsior," Roland, Benedict &amp; Co., Reading, Pa.

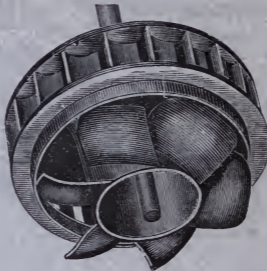
## Test of a 42-inch Wheel.

|                   | Head. | Weight | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|-------------------|-------|--------|------------------|-------|-------------|-----------|
| Whole Gate, ..... | 18.48 | 460    | 149.5            | 31.26 | 1136.34     | .7880     |
| Part Gate,.....   | 18.52 | 300    | 158.6            | 21.62 | 1055.49     | .6003     |
| " .....           | 18.64 | 160    | 160              | 11.60 | 910.64      | .3892     |
| " .....           | 18.72 | 50     | 164              | 3.12  | 785.78      | .1123     |



## B. J. BARBER, BALLSTON SPA, N. Y.

[From my Report of 1871.]



Test of a 30 inch.

| No. of Test.            | Head. | Weight. | Rev. per Minute. | Horse Power. | Weir. | Cubic Feet. | Per Cent. |
|-------------------------|-------|---------|------------------|--------------|-------|-------------|-----------|
| Whole Gate, 1. . . . .  | 18.80 | 380     | 198.5            | 34.28        | 1.081 | 1279.46     | .766      |
| " 2. . . . .            | 18.84 | 390     | 196.3            | 34.80        | 1.085 | 1286.49     | .760      |
| " 3. . . . .            | 18.87 | 400     | 195              | 35.45        | 1.089 | 1293.53     | .768      |
| " 4. . . . .            | 18.88 | 410     | 191.5            | 35.69        | 1.091 | 1297.07     | .783      |
| " 5. . . . .            | 18.60 | 400     | 192              | 34.91        | 1.083 | 1282.98     | .778      |
| " 6. . . . .            | 18.60 | 410     | 189              | 35.25        | 1.088 | 1291.77     | .778      |
| " 7. . . . .            | 18.60 | 420     | 186.5            | 35.63        | 1.090 | 1295.30     | .783      |
| " 8. . . . .            | 18.60 | 430     | 181.5            | 35.47        | 1.092 | 1299.15     | .777      |
| " 9. . . . .            | 18.61 | 440     | 181              | 36.20        | 1.096 | 1305.90     | .788      |
| " 10. . . . .           | 18.60 | 450     | 177              | 36.18        | 1.098 | 1309.44     | .788      |
| " 11. . . . .           | 18.59 | 445     | 178              | 36.04        | 1.096 | 1305.90     | .785      |
| " 12. . . . .           | 18.58 | 435     | 181.5            | 35.89        | 1.094 | 1302.30     | .785      |
| " 13. . . . .           | 18.60 | 425     | 185              | 35.78        | 1.092 | 1299.15     | .775      |
| " 14. . . . .           | 18.61 | 415     | 188.5            | 35.66        | 1.088 | 1291.77     | .787      |
| " 15. . . . .           | 18.61 | 405     | 191.5            | 35.25        | 1.085 | 1286.49     | .779      |
| <b>HEAD REDUCED.</b>    |       |         |                  |              |       |             |           |
| Whole Gate, 16. . . . . | 12.32 | 315     | 136              | 19.47        | .962  | 1074.49     | .778      |
| " 17. . . . .           | 12.32 | 320     | 131.5            | 19.10        | .964  | 1078.83     | .760      |
| " 18. . . . .           | 12.31 | 330     | 128.5            | 19.27        | .968  | 1085.51     | .763      |
| " 19. . . . .           | 12.31 | 310     | 137.5            | 19.37        | .962  | 1074.49     | .775      |
| " 20. . . . .           | 12.32 | 305     | 139              | 19.27        | .960  | 1072.15     | .772      |
| Unreliable, 21. . . . . | 12.32 | 287.5   | 154.3            | 20.22        | .956  | 1065.49     | .816      |
| <b>HEAD REDUCED.</b>    |       |         |                  |              |       |             |           |
| Whole Gate, 22. . . . . | 8.91  | 200     | 128              | 11.63        | .844  | 884.00      | .781      |
| " 23. . . . .           | 8.85  | 225     | 114.5            | 12.01        | .855  | 901.38      | .797      |
| " 24. . . . .           | 8.85  | 250     | 103              | 11.71        | .866  | 918.83      | .762      |
| <b>HEAD REDUCED.</b>    |       |         |                  |              |       |             |           |
| Whole Gate, 25. . . . . | 6.79  | 135     | 119.5            | 7.33         | .766  | 763.82      | .748      |
| " 26. . . . .           | 6.77  | 140     | 117.5            | 7.75         | .769  | 768.35      | .769      |
| " 27. . . . .           | 6.77  | 150     | 111.5            | 7.60         | .775  | 777.41      | .764      |
| Part Gate, 28. . . . .  | 12.57 | 225     | 154.5            | 15.80        | .856  | 901.97      | .786      |
| " 29. . . . .           | 12.77 | 150     | 154.8            | 10.55        | .789  | 723.45      | .694      |
| " 30. . . . .           | 13.02 | 95      | 150              | 6.47         | .587  | 528.59      | .497      |
| " 31. . . . .           | 12.52 | 25      | 161              | 1.81         | .445  | 380.59      | .217      |

HOLYOKE, MASS., September 30, 1872.

JAMES EMERSON.

## Humphrey Turbine.

Manufactured by the Humphrey Machine Co., Keene, N. H.

Of all the turbine builders extant, perhaps excepting J. P. Collins of Norwich, Ct., there is no other probably that can be named, so immensely scientific and so boiling over with theories as is Mr. Humphrey. The tests below will aid the reader to judge whether such theories are practically beneficial. In placing the 21-inch wheel reported below, a Collins' brass bucket wheel was removed, and advantageously so, I believe, it was admitted. The Humphrey wheel has downward and outward discharge, register gate. Tests of three of the wheels for Rawitser & Brother, Stafford Springs, Conn., Nov. 1878. These wheels were manufactured, fitted for their positions, set by the Humphrey Machine Co., and have been in use but a few months. A weir was constructed for each of the wheels. These weirs were of less capacity than desirable, but if there were any errors in measurements through this lack of capacity, such errors would be entirely in favor of the wheels. Each wheel was thoroughly cleaned, previous to its test.

## Test of 42-inch wheel, Nov. 13, 1878.

|                  | Head. | Weight. | Rev. | Horse Power. | Weir. | Cubic Feet. | Per-centage |
|------------------|-------|---------|------|--------------|-------|-------------|-------------|
| Whole Gate,..... | 5.00  | 375     | 68   | 7.72         | 1.005 | 1167.34     | .7000       |
| " ".....         | 5.00  | 400     | 64   | 7.75         | 1.000 | 1167.34     | .7020       |
| Part Gate,.....  | 5.30  | 225     | 62.5 | 4.26         | .755  | 766 65      | .555        |
| " ".....         | 5.45  | 325     | 65   | 6.40         | .870  | 944.59      | .6582       |

## Test of 24-inch wheel, Nov. 15, 1878.

|                  | Head. | Weight. | Rev. | Horse Power. | Weir. | Cubic Feet. | Per-centage |
|------------------|-------|---------|------|--------------|-------|-------------|-------------|
| Whole Gate,..... | 29.00 | 135     | 320  | 13.09        | 1.028 | 589.98      | .4051       |
| " ".....         | 29.00 | 150     | 310  | 14.09        | 1.030 | 591.60      | .4348       |
| " ".....         | 29.00 | 175     | 291  | 15.43        | 1.032 | 593.26      | .4748       |
| " ".....         | 29.00 | 200     | 265  | 16 06        | 1.077 | 629 84      | .4655       |
| Part Gate,.....  | 29.50 | 150     | 293  | 13.31        | .921  | 497 26      | .4803       |
| " ".....         | 29.50 | 115     | 270  | 9.41         | .750  | 269.86      | .4566       |

## Test of 21-inch wheel, Nov. 17, 1878.

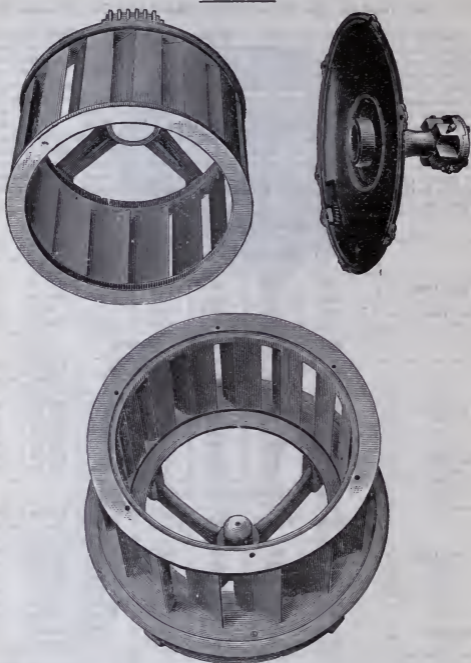
|                  | Head. | Weight. | Rev.  | Horse Power. | Weir. | Cubic Feet. | Per-centage |
|------------------|-------|---------|-------|--------------|-------|-------------|-------------|
| Whole Gate,..... | 47.00 | 350     | 379   | 40.20        | 1.300 | 824.72      | .5491       |
| " ".....         | 47.00 | 300     | 403   | 36.63        | 1.290 | 815.49      | .5060       |
| " ".....         | 47.00 | 275     | 424   | 35.33        | 1.284 | 800.42      | .4972       |
| " ".....         | 47.00 | 250     | 435   | 32.95        | 1.272 | 798.99      | .4646       |
| " ".....         | 47.00 | 225     | 455   | 31.02        | 1.242 | 773.00      | .4520       |
| " ".....         | 47.00 | 200     | 462.5 | 28 03        | 1.230 | 762 78      | .4139       |
| Part Gate,.....  | 47.00 | 125     | 446.6 | 16.91        | .994  | 554.55      | .3434       |
| " ".....         | 47.00 | 85      | 416.6 | 10.73        | .852  | 444.61      | .2718       |

In the mill where the 24-inch wheel is used the main line of shafting is designed to run 100 revolutions per minute; the gears connecting the wheel are one to three, consequently Mr. Humphrey prepared the wheel to run 300 revolutions per minute under 32 feet head.

The main shaft in mill where the 21 inch wheel is used is arranged in connection with the machinery used to run at 160 revolutions per minute. This shaft is connected to the wheel by gears, one to three, consequently, the wheel was prepared to run at a velocity of 480 revolutions per minute. It will be seen, however, by the tests, that Mr. Humphrey was very wild in his calculations for speed.

Mr. Humphrey took a very active interest in the hydrodynamic experiments made by the Holyoke Water Power Co., and promised distinctly, several times, to furnish one of his wheels for trial, but failed to do so.

Stilwell & Bierce Manufacturing Co.,  
DAYTON, OHIO.

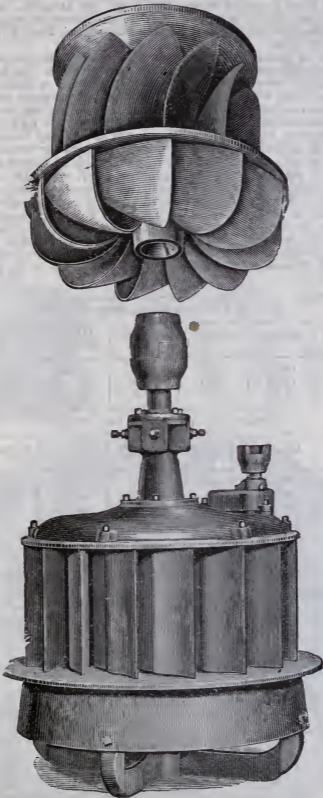


This turbine to be properly classed must be placed with the "Hercules" under the head of the New Departure, established by the production of that wheel.

As may be seen by the cuts, the Victor turbine is very simple in construction, having but few pieces, and those unlikely to get out of order; its inside register gate, so far as my experience goes, works with rapidity and ease, its long, peculiarly shaped buckets may be framed or cast into the rims of the wheel, as may be deemed advisable. Its capacity for its diameter, to be fully realized, must be compared with that of other turbines that were popular but a few years since, when Swain, Houston and Leffel & Co., each claimed to construct wheels of greater capacity for their diameter than those of any other make, and in support

**Victor Turbine.**

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of their claims, published tables at least fully up to the capacity of their wheels, the tables of Swain and Houston being computed upon a supposed useful effect of 80 per cent. of the water used; those of the Leffel at 88. Under 18 feet head, the Swain, 15¼ inch, is tabled to give 13½ h. p.; the Houston, 15 inch, 8½; and the Leffel, 15¼ inch, 11.1 h. p.; while the Victor, 15 inch, as may be seen by the test herewith annexed, under 18.34 head, actually gave 29.36 h. p., and a useful effect of .8808 per cent.

There can be no question but what the Victor, with the exception of the Hercules, has taken a position in advance of all other turbines—not because the same efficiency of useful effect may not be obtained by other wheels, but because at the same cost no other wheel can be made to transmit the same amount of power. Instead of acting the part of Mrs. Partington in opposing the inevitable, it will be well for turbine builders to accept the fact and strive to do still better, for the turbine is a long way from being the perfect engine it may be made. The tests will show that Mr. Stilwell has steadily improved, showing conclusively that the wild variations of other builders are owing to the lack of settled plans. At part gate the Victor is about as good as the average, but it would be well for Mr. Stilwell to try a thinner shell next his wheel so that the gate opening may be as near as possible to the wheel. The suggestion will be best understood by observing the filling of a bottle, or what is better, the filling of a canal through a small head gate, where the river may be several feet higher than the surface of the canal; yet the power due that difference is used up by passing through the small head gate, or in the inertia of the water in the canal, so that the part gate efficiency of a wheel must be somewhat in proportion to the size of the chamber inside of the gate.

Test of a 25-inch wheel, July 25, 1877.

|                      | Head. | Weight. | Revolutions. | Horse Power. | Cubic ft. | Percentage. |
|----------------------|-------|---------|--------------|--------------|-----------|-------------|
| Whole Gate, . . .    | 18.07 | 625     | 200          | 56.81        | 2214.55   | .7533       |
| Part Gate, . . . . . | 18.04 | 600     | 198          | 54.00        | 2208.44   | .7192       |
| “ “ . . . . .        | 18.13 | 500     | 208          | 47.27        | 1964.67   | .7042       |

Test of a 20-inch wheel, July 26, 1877.

|                       | Head. | Weight. | Revolutions. | Horse Power. | Cubic ft. | Percentage. |
|-----------------------|-------|---------|--------------|--------------|-----------|-------------|
| Whole Gate, . . . . . | 18.33 | 500     | 246          | 37.27        | 1387.27   | .7777       |
| Part Gate, . . . . .  | 18.41 | 425     | 269          | 34.64        | 1284.30   | .7774       |
| “ “ . . . . .         | 18.43 | 390     | 246          | 29.07        | 1145.59   | .7305       |
| “ “ . . . . .         | 7.97  | 75      | 246          | 5.59         | 757.93    | .4911       |

Test of a 20-inch wheel, Feb. 21, 1878.

|                       | Head. | Weight. | Revolutions. | Horse Power. | Cubic ft. | Percentage. |
|-----------------------|-------|---------|--------------|--------------|-----------|-------------|
| Whole Gate, . . . . . | 18.01 | 490     | 266.5        | 38.76        | 1362.39   | .8363       |
| Part Gate, . . . . .  | 18.08 | 415     | 265          | 33.32        | 1242.03   | .7853       |
| “ “ . . . . .         | 18.28 | 310     | 266          | 24.98        | 1014.03   | .7134       |
| “ “ . . . . .         | 18.40 | 240     | 263          | 19.12        | 870.79    | .6310       |
| “ “ . . . . .         | 18.58 | 100     | 271.5        | 8.33         | 602.23    | .3941       |

Test of a 15-inch wheel, March 26, 1878.

|                       | Head. | Weight. | Revolutions. | Horse Power. | Cubic ft. | Percentage. |
|-----------------------|-------|---------|--------------|--------------|-----------|-------------|
| Whole Gate, . . . . . | 18.34 | 300     | 323          | 29.36        | 974       | .8705       |
| Part Gate, . . . . .  | 18.10 | 300     | 321.5        | 29.22        | 970       | .8808       |
| “ “ . . . . .         | 18.39 | 160     | 326.5        | 15.83        | 755       | .8035       |
| “ “ . . . . .         | 18.74 | 100     | 320          | 9.09         | 492       | .5220       |

Test of a 25-inch wheel, Oct. 28, 1878.

|                  | Head. | Weight. | Revolutions. | Horse Power. | Cubic ft. | Percentage. |
|------------------|-------|---------|--------------|--------------|-----------|-------------|
| Whole Gate,....  | 17.96 | 700     | 209          | 68.62        | 2356.54   | .8584       |
| Part Gate,,..... | 17.93 | 650     | 208          | 61.45        | 2237.00   | .8112       |
| " " .....        | 18.00 | 450     | 200          | 40.90        | 1792.69   | .6710       |
| " " .....        | 18.25 | 350     | 205          | 32.61        | 1567.18   | .6036       |
| " " .....        | 18.37 | 175     | 211.5        | 16.81        | 1180.27   | .4098       |

Test of a 30-inch wheel, Oct. 29, 1878.

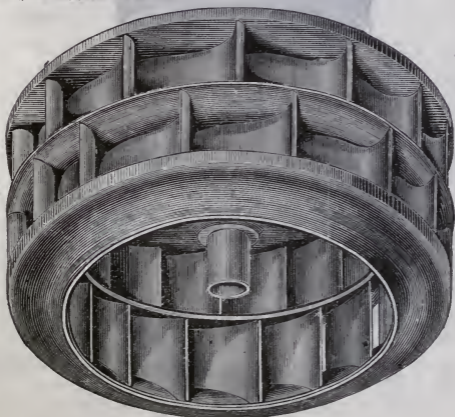
|                  | Head. | Weight. | Revolutions. | Horse Power. | Cubic ft. | Percentage. |
|------------------|-------|---------|--------------|--------------|-----------|-------------|
| Whole Gate, ...  | 11.65 | 800     | 144.5        | 52.54        | 2751.87   | .8676       |
| Part Gate, ..... | 11.78 | 675     | 136.5        | 41.88        | 2456.38   | .7663       |
| " " .....        | 11.92 | 606     | 142.5        | 38.87        | 2335.58   | .7392       |
| " " .....        | 11.83 | 450     | 145          | 29.65        | 1996.36   | .6648       |
| " " .....        | 12.10 | 300     | 144.5        | 19.70        | 1621.84   | .5316       |

## Eclipse Double Turbine, Manufactured by the same Co.



Test of a 30-inch Eclipse wheel.

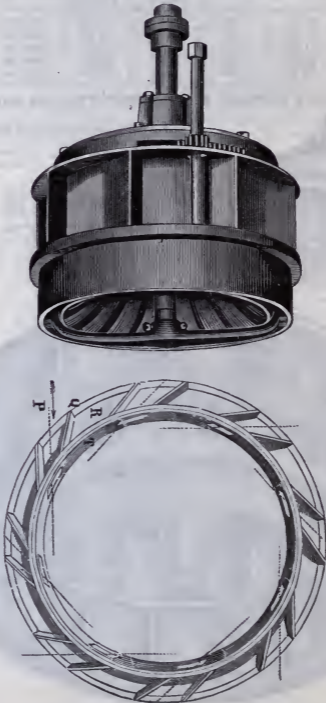
| Head. | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|-------|------------------|-------|-------------|-----------|
| 18.79 | 184.5            | 33.85 | 1253        | .7628     |
| 18.93 | 170              | 31.66 | 1214        | .7280     |
| 19.10 | 173.5            | 24.44 | 1026        | .6497     |
| 19.10 | 165              | 18.00 | 862         | .5736     |
| 19.18 | 166.6            | 12.11 | 699         | .4779     |



## Waldo Whitney, Leominster, Mass.

Wheel downward, and central discharge, similar to the Swain, but with fewer buckets. Inside register gate, the chutes and outer rim, R, being stationary; the thin hoop or gate T, rotating sufficiently to open or close the ports. After my report of the test at the top of next page, Mr. Whitney sent three other wheels for verification, that he had sold with guarantee that they should be as good as the one reported, and he undoubtedly believed them to be so until tested.

First wheel reported, tested January 10, 1873.



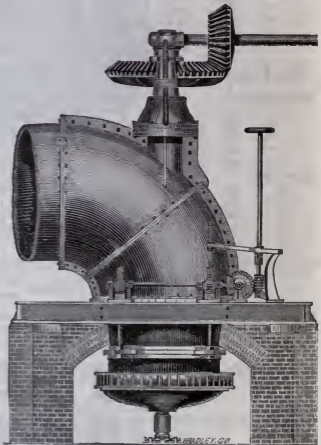
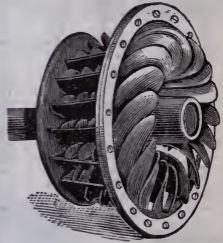
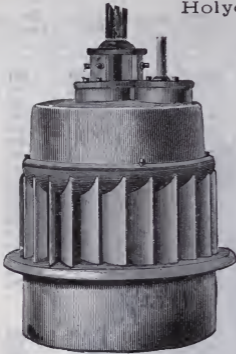
## WALDO WHITNEY, LEOMINSTER, MASS.

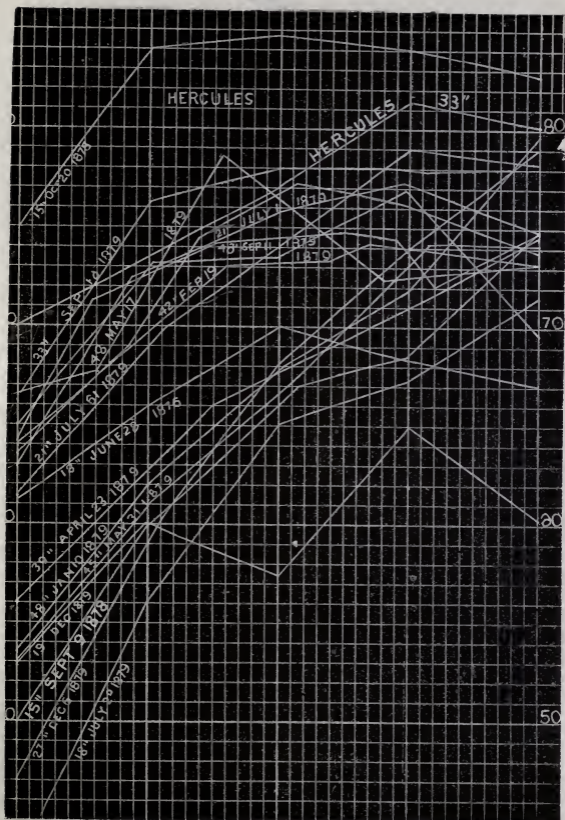
| No. of Test.         | Head. | Weight. | Rev. per Minute. | Horse Power. | Weir. | Cubic Feet. | Per Cent. |
|----------------------|-------|---------|------------------|--------------|-------|-------------|-----------|
| Whole Gate, 1...     | 18.48 | 400     | 195              | 35.45        | .765  | 1293.41     | .791      |
| " 2...               | 18.48 | 410     | 192              | 35.78        | .768  | 1291.09     | .793      |
| " 3...               | 18.47 | 420     | 188.5            | 35.99        | .771  | 1.98 77     | .794      |
| " 4...               | 18.46 | 430     | 188              | 36.35        | .775  | 137 9.03    | .796      |
| " 5...               | 18.46 | 440     | 184              | 36.80        | .777  | 1311 61     | .804      |
| " 6...               | 18.50 | 450     | 181              | 37.00        | .779  | 1316.77     | .803      |
| " 7...               | 18.50 | 460     | 178              | 37.21        | .781  | 1321.93     | .805      |
| " 8...               | 18.50 | 470     | 175.5            | 37.49        | .784  | 1322.23     | .805      |
| " 9...               | 18.51 | 480     | 173              | 37.74        | .786  | 1337.39     | .807      |
| " 10...              | 18.50 | 490     | 171              | 38.09        | .790  | 1347.76     | .806      |
| " 11...              | 18.49 | 500     | 168              | 38.18        | .792  | 1352.96     | .807      |
| " 12...              | 18.49 | 510     | 166              | 38.48        | .793  | 1355.76     | .812      |
| " 13...              | 18.48 | 520     | 163              | 38.52        | .796  | 1371.19     | .804      |
| " 14...              | 18.47 | 530     | 162              | 39.00        | .800  | 1373.78     | .813      |
| " 15...              | 18.48 | 540     | 159.5            | 39.15        | .802  | 1379.00     | .813      |
| " 16...              | 18.46 | 550     | 155              | 38.75        | .804  | 1383.22     | .803      |
| " 17...              | 18.45 | 560     | 149              | 37.92        | .806  | 1388.44     | .783      |
| <b>Head Reduced.</b> |       |         |                  |              |       |             |           |
| Whole Gate, 19...    | 12.67 | 350     | 131              | 20.84        | .706  | 1137.50     | .765      |
| " 20...              | 12.63 | 370     | 123              | 20.68        | .710  | 1159.69     | .747      |
| " 21...              | 12.61 | 390     | 116              | 20.56        | .718  | 1166.53     | .740      |
| " 22...              | 12.62 | 560     | 128              | 20.94        | .709  | 1157.22     | .759      |
| " 23...              | 12.63 | 340     | 133              | 20.55        | .702  | 1139.94     | .755      |
| " 24...              | 12.64 | 330     | 137              | 20.55        | .699  | 1120.31     | .768      |
| " 25...              | 12.65 | 320     | 141              | 20.51        | .695  | 1110.51     | .772      |
| <b>Head Reduced.</b> |       |         |                  |              |       |             |           |
| Whole Gate, 27 ..    | 6.81  | 150     | 111.5            | 7.60         | .554  | 785.43      | .752      |
| " 28...              | 6.77  | 160     | 105              | 7.61         | .558  | 792.53      | .750      |
| " 29...              | 6.75  | 170     | 99               | 7.65         | .564  | 807.72      | .742      |
| " 30...              | 6.72  | 180     | 98.5             | 8.06         | .567  | 814.66      | .779      |
| " 31...              | 6.70  | 190     | 88               | 7.60         | .573  | 825.68      | .727      |
| " 32...              | 6.66  | 200     | 86.5             | 7.83         | .580  | 841.31      | .739      |
| Part Gate,           |       |         |                  |              |       |             |           |
| $\frac{7}{8}$ 34...  | 18.51 | 450     | 163              | 33.34        | .731  | 1197 48     | .796      |
| $\frac{3}{4}$ 35...  | 18.74 | 390     | 162              | 28.72        | .660  | 1024.16     | .792      |
| $\frac{1}{2}$ 36...  | 19.20 | 200     | 157              | 14.27        | .500  | 666.34      | .590      |
| $\frac{1}{4}$ 37...  | 19.45 | 50      | 211              | 4.79         | .378  | 460.83      | .282      |
| $\frac{1}{4}$ 38...  | 19.45 | 50      | 142              | 3.22         | .310  | 342.70      | .255      |

| Whole Gate.                   | Head. | Weight. | Rev. per minute. | Horse Power. | Cub. ft. | Per Cent. |
|-------------------------------|-------|---------|------------------|--------------|----------|-----------|
| 2d wheel, June 25, 1873, ...  | 18.40 | 450     | 174              | 35.59        | 1345     | .762      |
|                               | 18.39 | 480     | 163              | 35.56        | 1374     | .746      |
|                               | 18.39 | 500     | 154.5            | 35.11        | 1389     | .728      |
| 3d wheel, July 17, 1873,..... | 18 24 | 450     | 166.5            | 34.51        | 1342     | .747      |
|                               | 18 22 | 480     | 158.5            | 34.58        | 1370     | .734      |
|                               | 18.22 | 440     | 169              | 33.80        | 1332     | .738      |
| 4th wheel, Aug. 16, 1873, ... | 17.91 | 400     | 184.3            | 33.51        | 1317     | .753      |
|                               | 17.90 | 450     | 168              | 34.36        | 1348     | .755      |
|                               | 17.88 | 480     | 161              | 35.11        | 1371     | .759      |

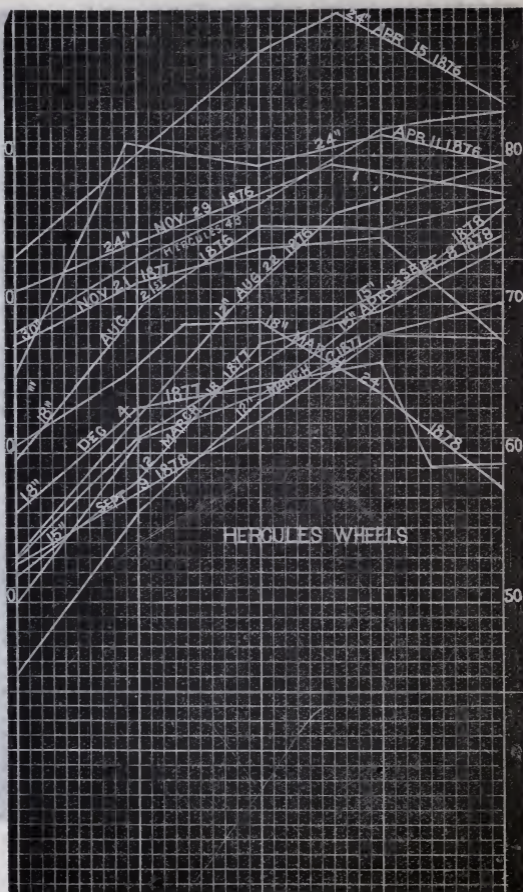
# HOLYOKE MACHINE CO.,

Holyoke, Mass.









## Holyoke Machine Company, Holyoke, Mass.

This company build the Boyden and Hercules turbines, the latter invented by John B. McCormick, of Brookville, Pa. Of the former, it is unnecessary to say anything here, as its merits are given on several other pages of this work.

### THE HERCULES.

In March, 1876, several of the above named wheels, 24 inches in diameter, each differing somewhat from the others, were brought to Holyoke to be tested. All gave remarkable results: one, 87 per cent. useful effect, and a power so extraordinary that the wheel was taken up and examined. A few changes were made, then it was reset and again tested, when the following results were obtained:

| Gate Opened           | Head  | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-----------------------|-------|----------------|-------------|------------|----------|
| Whole Gate, . . . . . | 18.02 | 217            | 70.58       | 2478.60    | .8361    |
| “ “ . . . . .         | 18.04 | 206            | 70.52       | 2466.04    | .8386    |
| Part Gate, . . . . .  | 18.06 | 214            | 70.03       | 2391.04    | .8579    |
| “ “ . . . . .         | 18.17 | 214.5          | 64.35       | 2167.29    | .8644    |
| “ “ . . . . .         | 18.23 | 213.5          | 64.05       | 2083.25    | .8922    |
| “ “ . . . . .         | 18.26 | 212            | 57.81       | 1944.50    | .8612    |
| “ “ . . . . .         | 18.34 | 210            | 53.45       | 1820.13    | .8470    |
| “ “ . . . . .         | 18.38 | 209.5          | 48.56       | 1690.89    | .8267    |
| “ “ . . . . .         | 18.57 | 211            | 32.12       | 1250.50    | .7291    |

As high useful effect at whole gate had been obtained by several builders, but no such average at all stages of gate opening. In capacity, however, the Hercules took a stand so entirely above that of any turbine ever before produced, that it seemed a good starting point for bringing all builders into harmony for their own and the public good. I immediately opened a correspondence with the best builders of the country, urging the abandonment of inferior wheels and the advantage of uniting upon the plans of the Hercules, paying the patentees a small royalty, and each builder striving to excel. The idea was favorably received. In the meantime the patentees hastily disposed of their right to build for the Western States. This, of course, ended the chance for a union of builders. The contract, however, was soon canceled; then the patentees offered the Holyoke Machine Company certain exclusive rights in their patent. I opposed the negotiations, because I believed then, and continue to believe, that it would be better for all to have a union of the best builders, instead of a continuance of the ruinous competition of the past upon inferior plans, which only serves to hinder the perfection of the best. Turbine building is not sufficiently understood to allow of its being considered a science; it is simply "cut and try." I know of no builder that with certainty can make two turbines that will give the same results, even made from the same pattern. Until that can be done, the manufacturing interest must suffer, unless manufacturers use the greatest care in the selection of turbines. What is almost invariably needed, is a wheel that will economize water at any stage of gate opening, so that either the abundance of the spring and fall months, or the scarcer quantity of summer, may be utilized in full. To do this, turbine builders must be able to produce turbines that will give their best percentage at either one-half, five-eighths, three-fourths, seven-eighths, or whole gate, as may best adapt each for the place where it is to be used. Such a wheel should be good at any stage of gate opening, and when such can be produced with certainty, then turbine building may properly be considered a science and not before, for such wheels are possible. Our rivers and streams are all extremely variable in supply of water—that of the summer months often being less than one-fourth of what it is for the rest of the year; and three-fourths of the larger quantity is almost invariably allowed to run to waste, because wheels of sufficient capacity to utilize the maximum have generally proved to be incapable of transmitting any power from the use of the minimum supply.

I have tested about eighty of these wheels, and, as may be seen by the diagrams, the variations have been great, and there are no good reasons for believing

that they will be less so in the future. Many of them are sent to purchasers without flanges on gate. In such case, in my opinion, the Victor would be preferable. That the company desire to do an honorable business, may be seen by the following extract, taken from second edition of this work:

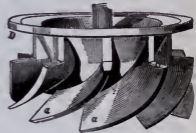
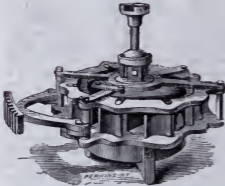
"From our experience we are satisfied the interest of the purchaser requires that wheels should be tested before acceptance, and hereafter we shall furnish tested wheels when desired to do so; and if a purchaser desires to have his wheel tested after it is set in his mill, we will make the test there, if the purchaser will pay the extra expense incurred thereby. And we believe the safest and most economical way to furnish mills with power, is to first ascertain exactly what is required, and we will send an engineer at the expense of the purchaser, to any mill, who will consult with the proprietor, make examinations, using suitable instruments when deemed necessary, ascertain the quantity of water available, etc., etc., and then furnish wheels that we will guarantee to do the work in an economical manner and to give the maximum of power promised by us; but it must be plainly understood that we do not promise to furnish a given amount of power with a less quantity of water than fixed upon at the time of making the examination, or that our wheel or wheels will run the mill if additional machinery is added.

"HOLYOKE MACHINE COMPANY.

"November 20, 1875."

The constant variations of the wheels, and a lack of appreciation of purchasers, caused an abandonment of the the plan suggested in the card, and now the wheels are sent away without any knowledge of their efficiency.

## D. P. Blackstone's Wheel, Berlin, Wis.



The Blackstone wheel has been tested in the Elmer curb represented above; in the Lefel; also, the Stout, Mills & Temple.

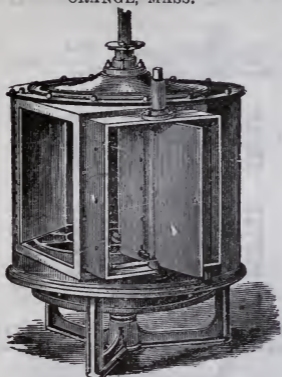
Test of a 40-inch, in Elmer curb.

|                  | Head. | Weight. | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|------------------|-------|---------|------------------|-------|-------------|-----------|
| Whole Gate,..... | 17.60 | 925     | 158              | 66.73 | 2416.89     | .8313     |
| Part Gate,.....  | 17.69 | 800     | 157              | 57 57 | 2184.17     | .7895     |
| ".....           | 17.88 | 520     | 156              | 36.87 | 1744.10     | .6435     |
| ".....           | 18.20 | 240     | 156.5            | 17.07 | 1261.62     | .3940     |

Another 40-inch, in Lefel curb.

|                   | Head. | Weight | Rev. per minute. | H. P. | Cubic feet | Per Cent. |
|-------------------|-------|--------|------------------|-------|------------|-----------|
| Whole Gate, ..... | 17.75 | 1000   | 172              | 78.18 | 3143.27    | .7424     |
| Part Gate,.....   | 17.87 | 900    | 170              | 69 54 | 2734.01    | .7543     |
| ".....            | 18.05 | 750    | 168              | 57.27 | 2239.64    | .7310     |
| ".....            | 18.29 | 450    | 175              | 35.79 | 1621.44    | .6394     |

CHASE WHEELS, FURNISHED BY THE ORANGE TURBINE CO.,  
ORANGE, MASS.



| No. of Test.          | Head. | Weight. | Rev. per Minute. | Horse Power. |
|-----------------------|-------|---------|------------------|--------------|
| <b>42-inch Wheel</b>  |       |         |                  |              |
| Whole Gate, 1 .....   | 15.17 | 500     | 194              | 44.09        |
| " 2 .....             | 15.17 | 700     | 161.5            | 51.17        |
| " 3 .....             | 15.17 | 750     | 158              | 53.86        |
| " 4 .....             | 15.17 | 800     | 149              | 54.18        |
| " 5 .....             | 13.17 | 850     | 143              | 55.25        |
| " 6 .....             | 15.17 | 9.0     | 135              | 55.22        |
| " 7 .....             | 15.17 | 950     | 123              | 55.27        |
| " 8 .....             | 15.17 | 1050    | 116              | 55.36        |
| " 9 .....             | 15.17 | 1100    | 104              | 52.00        |
| <b>54-inch Wheel.</b> |       |         |                  |              |
| Whole Gate, 11 .....  | 15.00 | 500     | 148              | 33.63        |
| " 12 .....            | 15.00 | 600     | 141              | 38.38        |
| " 13 .....            | 15.00 | 700     | 138              | 43.91        |
| " 14 .....            | 15.00 | 1000    | 117              | 53.20        |
| " 15 .....            | 15.00 | 1000    | 120.6            | 54.82        |
| " 16 .....            | 15.00 | 1050    | 118              | 56.32        |
| " 17 .....            | 13.00 | 1100    | 117              | 58.50        |
| " 18 .....            | 15.00 | 1260    | 112              | 61.09        |
| " 19 .....            | 15.00 | 1500    | 100              | 68.18        |
| " 20 .....            | 15.00 | 1800    | 90               | 73.63        |
| " 21 .....            | 15.00 | 2000    | 82               | 74.55        |

The 54-inch wheels were tabled and were geared to run at 138 revolutions per minute, to give 112 horse power; actual results obtained, 43.91, while the percentage of useful effect from the water used could not have exceeded 25 per cent., but at 82 revolutions it might have reached 35 or 40.

The water in the race below the mill was 30 inches average depth, 29 feet in width, its velocity being so great as to cause it to break white, the fall being at least one foot in a hundred.

TESTS OF A 36-INCH AND OF A 48-INCH TUTTLE WHEEL AT  
SMITH & MEADER'S MILL, WATERVILLE, ME.

| <b>36-inch.</b>  | Rev.<br>per<br>Minute. | Weight<br>in<br>Pounds. | Horse<br>Power. | Head<br>in<br>Feet. | Weir. | Cubic<br>Feet<br>Disch'd | Per<br>Cent. |
|------------------|------------------------|-------------------------|-----------------|---------------------|-------|--------------------------|--------------|
| No. of Test.     |                        |                         |                 |                     |       |                          |              |
| Whole Gate, 1... | 190.8                  | 425                     | 36.86           | 15.85               | 1.438 | 2746.83                  | .4479        |
| " 11...          | 162.6                  | 600                     | 44.32           | 15.84               | 1.450 | 2779.65                  | .5325        |
| " 12...          | 161.                   | 615                     | 45.01           | 15.79               | 1.446 | 2768.70                  | .5572        |
| Part Gate, 13... | 175                    | 325                     | 25.82           | 16.58               | 1.250 | 2227.83                  | .3698        |
| " 14...          | 168                    | 130                     | 9.93            | 17.22               | .963  | 1489.98                  | .2066        |
| <b>48-inch.</b>  |                        |                         |                 |                     |       |                          |              |
| Whole Gate, 1... | 148.4                  | 900                     | 60.71           | 14.53               | 1.634 | 4135.02                  | .5243        |
| " 8...           | 140                    | 1000                    | 63.63           | 14.47               | 1.630 | 4145.97                  | .5612        |
| " 9...           | 138.5                  | 1025                    | 64.53           | 14.45               | 1.630 | 4145.97                  | .5831        |
| " 10...          | 137                    | 1050                    | 65.38           | 14.48               | 1.632 | 4149.62                  | .5625        |
| " 11...          | 130                    | 1100                    | 65.00           | 14.48               | 1.630 | 4145.97                  | .572         |
| " 12...          | 125                    | 1150                    | 66.38           | 14.48               | 1.632 | 4149.62                  | .571         |
| 1/3 Gate, 13...  | 161                    | 425                     | 31.11           | 15.73               | 1.312 | 2992.99                  | .346         |

TESTS OF A 42-INCH TYLER, AND A 42-INCH REYNOLDS WHEEL,  
AT VASSALBORO' WOOLEN MILLS, VASSALBORO', ME.

| <b>Tyler.</b>    | Rev.<br>per<br>Minute. | Weight<br>in<br>Pounds. | Horse<br>Power. | Head<br>in<br>Feet. | Weir. | Cubic<br>Feet<br>Disch'd. | Per<br>Cent. |
|------------------|------------------------|-------------------------|-----------------|---------------------|-------|---------------------------|--------------|
| No. of Test.     |                        |                         |                 |                     |       |                           |              |
| Whole Gate, 1... | 168.6                  | 700                     | 53.65           | 27.21               | 1.264 | 2609.50                   | .3999        |
| " 2...           | 164.4                  | 750                     | 56.05           | 27.21               | 1.282 | 2661.84                   | .4089        |
| " 3...           | 160.8                  | 800                     | 58.47           | 27.21               | 1.282 | 2661.84                   | .4266        |
| " 4...           | 144.6                  | 1100                    | 72.30           | 27.21               | 1.297 | 2776.10                   | .5063        |
| <b>Reynolds.</b> |                        |                         |                 |                     |       |                           |              |
| Part Gate, 1...  | 139                    | 800                     | 50.54           | 28                  | 1.210 | 2436.82                   | .3918        |
| " 2...           | 168.5                  | 750                     | 57.44           | 28                  | 1.210 | 2436.82                   | .4453        |
| " 3...           | 172.5                  | 775                     | 57.74           | 28                  | 1.210 | 2436.82                   | .4477        |
| " 4...           | 173.5                  | 800                     | 63.09           | 28                  | 1.210 | 2436.82                   | .4892        |
| " 5...           | 161                    | 850                     | 62.20           | 28                  | 1.210 | 2436.82                   | .4823        |
| " 6...           | 149.6                  | 900                     | 61.20           | 28                  | 1.210 | 2436.82                   | .4745        |
| Whole Gate, 7... | 166                    | 1000                    | 75.45           | 28                  | 1.297 | 2776.10                   | .4683        |
| " 8...           | 161.6                  | 1100                    | 80.80           | 28                  | 1.297 | 2776.10                   | .5015        |

This certifies, that on the 8th and 9th of this month I tested two 42-inch water-wheels at the Vassalboro' Woolen Mills, Vassalboro', Me., George Wilkins, Agent.

The first was called a Tyler wheel, though not made or furnished by Mr. Tyler. Regulator speed of wheel 170 revolutions per minute. The test proved that it was run at a velocity much too high to utilize its greatest effectiveness.

Second wheel, a "Reynolds." Testing first with gate open the same as when running all the machinery attached to it, six tests; then the gate was opened in full; with 1100 pounds on the scale beam the wheel ran very unsteadily, so much so that it was considered useless to try it with more weight.

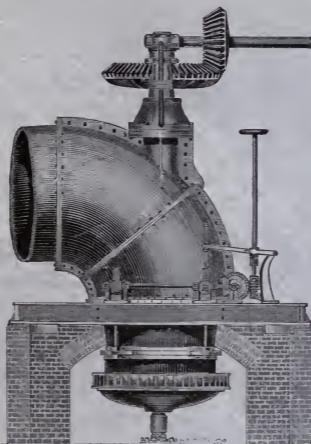
Weir 10 feet in length, sectional area approaching weir 25 feet in width, depth below crest 2.5 feet.

April 15, 1872.

JAMES EMERSON.



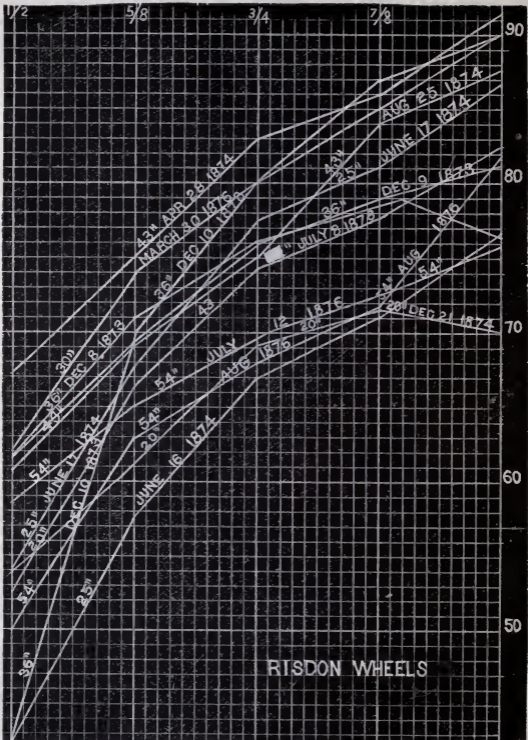
## Boyden Turbine.



In the purchase of this turbine, more ignorance is displayed than a well-wisher of his race likes to acknowledge lies dormant in the average business man of the times; in purchasing any other kind of turbine the purchaser almost invariably makes inquiries in order to get the best; the Boyden seeker makes no inquiries except, perhaps, as to capacity and cost, supposing all to be alike as to efficiency, whether made by an expert mechanic or the veriest botch. There is no reason to doubt but what a whole gate an outward discharge wheel may be made to give a high useful effect, but every intelligent turbine builder knows that of all wheels the outward discharge is the most difficult to get just right; also, that good part gate results are impossible with such discharge. There are vague rumors of remarkable results obtained by Mr. Boyden, as there are of the Humphrey and every other turbine, but such results are rarely confirmed when the wheels are tested by competent disinterested engineers. Of four Boyden wheels tested in a Connecticut mill, three were found to be giving 46 per cent. useful effect, the fourth gave 47. At Unionville, Conn., Plattner & Porter Mfg Co., a test of one gave 61 per cent. The wheel was built by the Ames Mfg Co., of Chicopee, and is named in a recent circular of that Company in commendation of that style of turbine. A nice brass bucket wheel, made by the same Company in 1871, 72 inches in diameter, 51 openings, each 7.26 inches in height, 1½ inches in width, rated to discharge 6360 cubic feet of water under 24 feet head, at 98 revolutions per minute, and to give 217 horse power, was tested at the Dwight No. 7 mill, Chicopee, Mass., Nov. 6, 1878. The tests at its geared speed are given below:

|                      | Head in Feet. | Weight. | Revolutions. | Horse Power. | Cubic ft. | Percentage. |
|----------------------|---------------|---------|--------------|--------------|-----------|-------------|
| Whole Gate, . . .    | 22.1          | 3730    | 97           | 219.2        | 7141.70   | .7353       |
| Part Gate, . . . . . | 23.20         | 2000    | 98           | 118.78       | 5446.80   | .4977       |
| “ “ . . . . .        | 23.50         | 1000    | 96.4         | 58.43        | 4341.98   | .3031       |





From the time of the Philadelphia turbine tests in 1859-60, up to the present, Mr. Risdon has continued an almost unbroken series of experiments for the purpose of perfecting the turbine; yet the lines above show decided variations in useful effect. If such is the case with wheels constructed by one so skillful, how must it be with those turned out by machine companies merely as a business, without other supervision than that of the ordinary foreman? The 54-inch, represented above, was put together by the Holyoke Machine Co., though Mr. Risdon furnished plans and core-boxes for forming the buckets. Many more of the Holyoke made wheels were tested than those made wholly by Mr. Risdon. As a general thing the wheels, when first tested, were rather low in efficiency; but, after making alterations suggested by such tests, the results were often very high at whole gate, and the tests proved conclusively that purchasers who accept untested turbines, generally do so at a loss of from ten to twenty per cent. of what they might have with more care.

## THOMPSON &amp; HOLCOMB WHEEL.

This certifies that a Water Wheel, 30 inches in diameter, made of cast iron, fly-trap gates—downward discharge,—in form somewhat like the Houston, known as the Thompson Turbine, was sent to the Holyoke Testing Flume by A. P. Holcomb of Silver Creek, N. Y., to be tested. The figures showing the results obtained by me, may be found below. During the test, the scale beam was attached to the brake at a point, which, if revolving, would describe a circle fifteen feet in circumference, consequently the revolutions of the wheel must be multiplied by fifteen to obtain the correct speed.

|   |                   |
|---|-------------------|
| Length of Weir, . . . . .                       | 6 feet.           |
| Temperature of Water, . . . . .                 | 32° Fah.          |
| Weight of Water, per cubic foot, . . . . .      | 62.375.           |
| Correction for Leakage, 18 feet head, . . . . . | 13.10 cubic feet. |
| Correction for Leakage, 12 feet head, . . . . . | 11.10 cubic feet. |
| Correction for Leakage, 6 feet head, . . . . .  | 9.10 cubic feet.  |

A second trial of the same wheel to ascertain the effect of short extensions added to the outer end of chutes, for the purpose of rounding or flaring them when open. These extensions prevented the gates from being opened quite as wide as without them, consequently less water was discharged. The partial gate at first trial gave best percentage, but owing to a brackage of the gates by the ice at the second trial, no part gate tests could be taken.

The wheel run very steady, was easily regulated, and from its high speed is a favorite with those who have it in use; its gates, like the Lefel and all of that class, would be likely to become leaky.

| No. of Test.   | Head. | Weight | Rev. per Minute. | Horse Power. | Weir. | Cubic Feet. | Per Cent. |
|--|-------|--------|------------------|--------------|-------|-------------|-----------|
| Whole Gate, 2 . . . . .                              | 18.44 | 390    | 220.5            | 89.09        | 1.226 | 1547.76     | .725      |
| " 3 . . . . .  | 18.45 | 400    | 220              | 40.00        | 1.243 | 1579.39     | .726      |
| " 4 . . . . .  | 18.42 | 410    | 221              | 41.18        | 1.954 | 1590.95     | .741      |
| " 5 . . . . .  | 18.40 | 420    | 218              | 41.62        | 1.262 | 1614.97     | .748      |
| " 6 . . . . .  | 18.39 | 490    | 215              | 42.02        | 1.260 | 1611.20     | .742      |
| " 7 . . . . .  | 18.38 | 440    | 211              | 42.20        | 1.258 | 1607.46     | .756      |
| " 8 . . . . .  | 18.38 | 450    | 207.5            | 42.44        | 1.261 | 1613.09     | .757      |
| " 9 . . . . .  | 18.35 | 460    | 203              | 42.42        | 1.260 | 1611.20     | .759      |
| " 10 . . . . .                                       | 18.26 | 450    | 205.3            | 41.99        | 1.260 | 1611.20     | .755      |
| <b>HEAD REDUCED.</b>                                 |       |        |                  |              |       |             |           |
| Whole Gate, 13 . . . . .                             | 12.19 | 500    | 183              | 21.62        | 1.080 | 1285.00     | .730      |
| " 14 . . . . .                                       | 12.18 | 270    | 178              | 21.84        | 1.082 | 1280.47     | .736      |
| " 15 . . . . .                                       | 12.18 | 280    | 172              | 21.89        | 1.085 | 1294.73     | .734      |
| " 16 . . . . .                                       | 12.18 | 290    | 170              | 22.40        | 1.088 | 1300.03     | .745      |
| " 17 . . . . .                                       | 12.17 | 300    | 161.5            | 21.95        | 1.091 | 1305.30     | .731      |
| " 18 . . . . .                                       | 12.17 | 310    | 156.7            | 22.08        | 1.091 | 1305.30     | .735      |
| " 19 . . . . .                                       | 12.18 | 285    | 169.5            | 21.91        | 1.087 | 1294.27     | .735      |
| " 20 . . . . .                                       | 12.18 | 295    | 164              | 21.99        | 1.088 | 1300.03     | .731      |
| <b>HEAD REDUCED.</b>                                 |       |        |                  |              |       |             |           |
| Whole Gate, 23 . . . . .                             | 6.60  | 130    | 139              | 8.34         | .875  | 940.26      | .711      |
| " 24 . . . . .                                       | 6.59  | 135    | 140              | 8.21         | .878  | 948.28      | .695      |
| " 25 . . . . .                                       | 6.58  | 140    | 132.5            | 8.43         | .876  | 945.08      | .717      |
| " 26 . . . . .                                       | 6.58  | 145    | 128              | 8.43         | .877  | 946.68      | .700      |
| <b>July 12th.</b>                                    |       |        |                  |              |       |             |           |
| Test of the same wheel before extensions were added. |       |        |                  |              |       |             |           |
| Whole Gate, 28 . . . . .                             | 18.10 | 460    | 206              | 43.07        | 1.174 | 1718.41     | .737      |
| " 29 . . . . .                                       | 6.41  | 160    | 103.5            | 7.53         | .800  | 974.88      | .689      |
| Part Gate, 30 . . . . .                              | 18.25 | 400    | 203              | 36.60        | 1.040 | 1433.27     | .742      |
| " 31 . . . . .                                       | 18.33 | 325    | 206              | 30.70        | .984  | 1280.52     | .722      |
| " 32 . . . . .                                       | 18.44 | 250    | 207              | 23.81        | .818  | 1004.54     | .673      |
| " 33 . . . . .                                       | 18.50 | 200    | 207.5            | 18.56        | .720  | 880.88      | .651      |
| " 34 . . . . .                                       | 6.60  | 125    | 102              | 6.28         | .669  | 747.68      | .679      |

JAMES EMERSON.

HOLYOKE, MASS., December 18, 1872

# Rodney Hunt Machine Co.,

ORANGE, MASS.

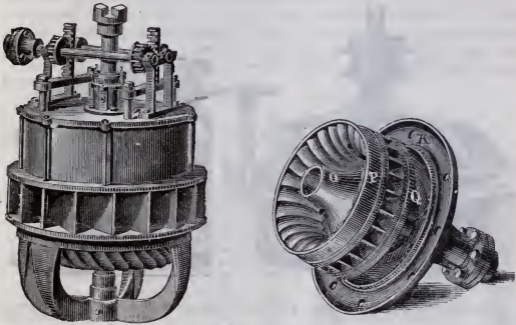
THIS certifies that a WATER WHEEL, thirty inches in diameter, made of cast iron, central and downward discharge, known as the Hunt Double Action Turbine was sent to the HOLYOKE TESTING FLUME by the Rodney Hunt Machine Co., of Orange, Mass., to be tested. The date of each test and the figures showing the exact results obtained by me, may be found on the following pages. During the test the scale beam was attached to the brake at a point, which, if revolving, would describe a circle fifteen feet in circumference, consequently the revolutions of the wheel must be multiplied by fifteen to obtain the correct speed. Data for one minute :

Length of Weir, . . . . . 6 feet.  
 Temperature of Water, . . . . . 40° Fah.  
 Weight of Water, per cubic foot, . . . . . 62.373.  
 Correction for Leakage, 18 feet head, . . . . . 14.20 cubic feet.  
 Correction for Leakage, 12 feet head, . . . . . 12.20 cubic feet.  
 Correction for Leakage, 6 feet head, . . . . . 10.20 cubic feet.

| No. of Test.     | Head. | Weight. | Rev. per Minute. | Horse Power. | Weir. | Cubic Feet. | Per Centage. |
|------------------|-------|---------|------------------|--------------|-------|-------------|--------------|
| Whole Gate,      | 18.34 | 650     | 125.5            | 37.08        | 1.192 | 1473.94     | .7245        |
|                  | 18.36 | 525     | 177.5            | 42.36        | 1.179 | 1460.17     | .8388        |
| " 12...          | 18.35 | 540     | 171              | 41.06        | 1.180 | 1461.99     | .8187        |
| " 13...          | 18.35 | 550     | 168.5            | 42.12        | 1.184 | 1469.80     | .8275        |
| " 14...          | 18.34 | 560     | 166              | 42.25        | 1.187 | 1474.80     | .8260        |
| " 15...          | 18.34 | 530     | 176.5            | 42.52        | 1.181 | 1463.82     | .8385        |
| " 16...          | 18.35 | 520     | 180.5            | 42.66        | 1.178 | 1458.34     | .8433        |
| " 17...          | 18.36 | 510     | 183              | 42.42        | 1.173 | 1449.23     | .8425        |
| " 18...          | 18.35 | 500     | 185              | 42.04        | 1.170 | 1443.77     | .8409        |
| Part Gate, 19... |       |         |                  |              |       |             |              |
| " 20...          | 18.37 | 475     | 190              | 41.02        | 1.178 | 1422.00     | .8306        |
| " 21...          | 18.38 | 490     | 186              | 41.42        | 1.160 | 1425.62     | .8374        |
| " 22...          | 18.36 | 500     | 183              | 41.59        | 1.163 | 1427.43     | .8395        |
| " 23...          | 18.42 | 440     | 182.7            | 36.54        | 1.123 | 139.02      | .7722        |
| " 24...          | 18.40 | 450     | 185.5            | 37.94        | 1.125 | 1392.02     | .8055        |
| " 25...          | 18.40 | 460     | 176.6            | 36.92        | 1.128 | 1368.59     | .7756        |
| " 26...          | 18.61 | 250     | 179              | 20.34        | .932  | 1030.04     | .5613        |
| " 27...          | 18.60 | 235     | 185              | 19.76        | .927  | 1022.66     | .5495        |
| " 28...          | 18.86 | 75      | 176.2            | 6.01         | .727  | 710.89      | .2376        |
| Head Reduced.    |       |         |                  |              |       |             |              |
| " 30...          | 12.24 | 250     | 173.3            | 19.69        | .963  | 1117.88     | .7630        |
| " 31...          | 12.20 | 275     | 165              | 20.62        | .995  | 1138.16     | .7856        |
| " 32...          | 12.19 | 300     | 157.5            | 21.47        | 1.007 | 1158.55     | .804         |
| " 33...          | 12.17 | 320     | 151              | 21.96        | 1.018 | 1187.33     | .804         |
| " 34...          | 12.15 | 310     | 145              | 22.41        | 1.027 | 1192.77     | .8199        |
| " 35...          | 12.13 | 350     | 141.5            | 22.51        | 1.032 | 1201.37     | .817         |
| " 36...          | 12.13 | 360     | 137              | 22.41        | 1.036 | 1208.27     | .8089        |
| " 37...          | 12.13 | 370     | 134.5            | 22.62        | 1.037 | 1209.99     | .8172        |
| " 38...          | 12.13 | 380     | 129              | 22.28        | 1.037 | 1109.99     | .803         |
| " 39...          | 12.13 | 390     | 124              | 21.98        | 1.040 | 1215.17     | .7888        |

## Hunt's Double Action Turbine Wheel.

The cut at the left represents the Hunt curb, with the downward and outward discharge wheel which gave the results reported in the second table below; the other cut represents the wheel generally used by the Hunt Machine Co., (the Swain); and the one giving the results reported in the first table below, also, those upon the opposite page.



Test of a 48-inch Hunt-Swain wheel.

|                   | Head. | Weight. | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|-------------------|-------|---------|------------------|-------|-------------|-----------|
| Whole Gate, ..... | 11 71 | 1500    | 83               | 56.59 | 3454.74     | .757      |
| Part Gate, .....  | 11.89 | 1275    | 86.5             | 50.13 | 3252.31     | .681      |
| “ “ .....         | 12.30 | 850     | 85.5             | 33.03 | 2713.01     | .524      |
| “ “ .....         | 12.61 | 200     | 87.7             | 7.97  | 1617.18     | .254      |

Test of a Hunt-Flint wheel, downward and outward discharge; see bottom of buckets in curb above.

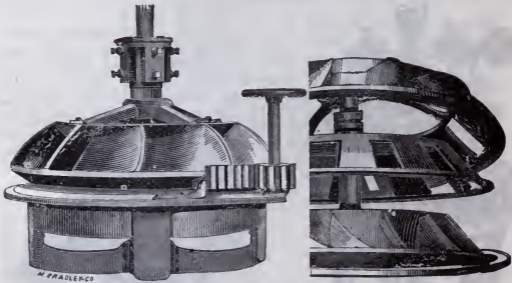
|                   | Head. | Weight. | Rev. per minute. | H. P. | Cubic feet. | Per Cent. |
|-------------------|-------|---------|------------------|-------|-------------|-----------|
| Whole Gate, ..... | 18.31 | 675     | 176.3            | 54.09 | 1732.10     | .9050     |
| Part Gate, .....  | 18.31 | 575     | 176.5            | 46.13 | 1672.72     | .7992     |
| “ “ .....         | 18.33 | 500     | 175              | 39.77 | 1564.08     | .7361     |
| “ “ .....         | 18 53 | 200     | 175              | 15.71 | 1067.10     | .4215     |

Test of a Hunt wheel, downward discharge, in the same curb as the one above.

|                   | Head. | Weight. | Rev. per Min. | Horse Power. | Cubic feet. | Per Cent. |
|-------------------|-------|---------|---------------|--------------|-------------|-----------|
| Whole Gate, ..... | 18.28 | 665     | 180           | 54.40        | 1800.73     | .8780     |
| Part Gate, .....  | 18 32 | 525     | 178           | 42.47        | 1681.87     | .7314     |
| “ “ .....         | 18.40 | 395     | 178           | 31.95        | 1435.63     | .6432     |
| “ “ .....         | 18.4) | 270     | 181           | 22.21        | 1245.48     | .5184     |
| “ “ .....         | 18.63 | 150     | 188           | 12.81        | 870.44      | .4082     |

## Gates Curtis, Ogdensburg, N. Y.

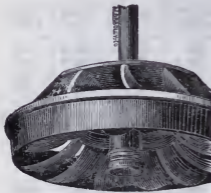
## CURTIS TURBINE.



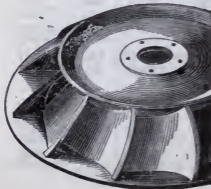
This wheel is diagonal in shape, like the Houston, but has an Inside Register Gate.

## Test of a 47-inch wheel.

|             | Head. | W'ht. | Rev.  | H. P. | Cubic Feet. | P. C. |
|-------------|-------|-------|-------|-------|-------------|-------|
| Whole Gate, | 17.71 | 1150  | 115   | 80.15 | 3041.00     | .788  |
| Part Gate,  | 17.98 | 1000  | 115.5 | 70.00 | 2648.24     | .778  |
| "           | 18.07 | 850   | 111.5 | 57.44 | 2345.83     | .717  |
| "           | 18.17 | 570   | 116.5 | 40.24 | 1846.92     | .635  |
| "           | 18.32 | 450   | 107   | 29.58 | 1470.12     | .582  |
| "           | 18.32 | 400   | 114   | 27.63 | 1441.54     | .554  |



Mr. Curtis also makes the wheel with open chutes, omitting gate, allowing the wheel to run at full gate at all times, regulating speed by head in forebay, using a wicket gate between flume and forebay. A 25-inch made in that way, tested at my flume gave the following results



|  | Head. | W'ht. | Rev.  | H. P. | Cubic Feet | P. C. |
|--|-------|-------|-------|-------|------------|-------|
| Whole Gate,                            | 18.21 | 500   | 220   | 33.33 | 1095.93    | .8842 |
| Same wheel in another set of chutes.   |       |       |       |       |            |       |
| Whole Gate,                            | 18.20 | 465   | 223.2 | 31.45 | 1069.41    | .8322 |
| 2 chutes stopped,                      | 18.29 | 400   | 213   | 25.81 | 957.63     | .7801 |
| 4 chutes stopped,                      | 18.37 | 300   | 214   | 19.75 | 816.29     | .6973 |
| Same wheel tested in a curb with gate. |       |       |       |       |            |       |
| Whole Gate,                            | 18.40 | 415   | 224.5 | 28.23 | 1017.27    | .7984 |
| Part Gate,                             | 18.42 | 360   | 211.3 | 23.05 | 886.22     | .7510 |
| "                                      | 18.51 | 290   | 209.5 | 18.41 | 751.00     | .7012 |
| "                                      | 18.60 | 215   | 213   | 13.87 | 615.70     | .6413 |
| "                                      | 18.68 | 165   | 199.2 | 9.96  | 491.65     | .5742 |

## Humming Bird Wheels.

*18-inch wheels, sent by Willis Read, Danbury, Conn.*

Through some peculiarity of construction, which, without illustration, is indescribable, these wheels keep up a constant humming sound while running; hence their name. Mr. Read was promptly on hand with his wheel, which was tested Sept. 6. From information obtained by the test, he took a new departure and constructed another wheel, which was tested Oct. 15. The results of each may be found below. The workmanship of the wheels would hardly cause manufacturers to look for machinery in Danbury.

Data below for one minute. Multiply revolutions by 20.

| Gate Opened | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. | 17.95 | 1550   | 000            | 000         |            | 000      |
| " "         | 18.02 | 750    | 103            | 46.81       | 2187.30    | .6287    |
| " "         | 18.02 | 775    | 1 2            | 47.91       | 2211.71    | .6366    |
| " "         | 18.00 | 800    | 100 5          | 48.72       | 2218.70    | .6473    |
| " "         | 18.00 | 825    | 98.2           | 49.60       | 2232.70    | .6533    |
| " "         | 17.98 | 850    | 97.5           | 50.22       | 2246.73    | .6581    |
| " "         | 17.98 | 875    | 96             | 50.90       | 2260.77    | .6620    |
| " "         | 17.97 | 900    | 95             | 51.81       | 227 1.33   | .6720    |
| " "         | 17.95 | 925    | 93.5           | 52.42       | 2306.62    | .6702    |
| " "         | 17.94 | 950    | 90             | 51.82       | 2338.53    | .6537    |
| Part Gate.  | 18.40 | 425    | 98.3           | 24.03       | 1210.67    | .5734    |
| " "         | 18.41 | 400    | 100            | 21.24       | 1196.08    | .5828    |
| " "         | 18.45 | 400    | 92             | 22.30       | 1089.69    | .5872    |
| " "         | 18.41 | 420    | 96.7           | 24.78       | 1255.49    | .5670    |
| " "         | 18.40 | 500    | 91.5           | 27.72       | 1269.56    | .6283    |
| " "         | 18.34 | 600    | 88.5           | 32.18       | 1398.88    | .6640    |
| " "         | 18.32 | 600    | 91             | 33.09       | 1472.63    | .6493    |
| " "         | 18.18 | 700    | 96             | 40.72       | 1827.76    | .6488    |
| " "         | 18.16 | 750    | 93.2           | 42.36       | 1887.49    | .6541    |
| " "         | 18.13 | 775    | 93.5           | 43.94       | 1944.34    | .6598    |
| " "         | 18.22 | 650    | 95             | 37.42       | 1732.81    | .6275    |

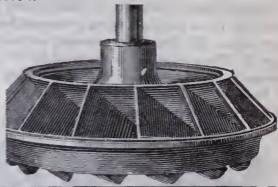
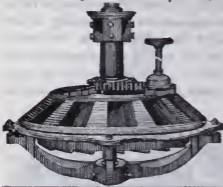
Tested October 15.

|             |       |      |       |       |         |       |
|-------------|-------|------|-------|-------|---------|-------|
| Whole gate. | 17.81 | 1600 | 000   | 000   | 2642.89 | 000   |
| " "         | 17.85 | 800  | 107.5 | 52.12 | 2474.00 | .6246 |
| " "         | 17.85 | 850  | 103   | 53.06 | 2485.76 | .6331 |
| " "         | 17.84 | 900  | 95.8  | 52.25 | 2551.18 | .6078 |
| " "         | 17.83 | 825  | 106   | 53.00 | 2503.88 | .6286 |
| " "         | 17.83 | 850  | 103.3 | 53.21 | 2514.77 | .6288 |
| " "         | 17.85 | 875  | 99.6  | 52.78 | 2554.83 | .6127 |
| Part Gate.  | 18.06 | 700  | 97.3  | 41.27 | 2042.38 | .5923 |
| " "         | 18.02 | 675  | 100 3 | 41.03 | 2035.56 | .5922 |
| " "         | 18.04 | 650  | 102.6 | 40.41 | 2035.56 | .5826 |
| " "         | 18.20 | 500  | 104.2 | 31.57 | 1683.73 | .5454 |
| " "         | 18.18 | 525  | 103.2 | 32.83 | 1680.51 | .5689 |
| " "         | 18 32 | 400  | 95.6  | 23.17 | 1328.28 | .5041 |
| " "         | 18.34 | 350  | 103   | 21.90 | 1301.28 | .4847 |
| " "         | 18.57 | 200  | 93.5  | 11.94 | 908.29  | .3760 |
| " "         | 18.44 | 250  | 105   | 11.59 | 1079.87 | .3081 |
| " "         | 18.06 | 650  | 106   | 41.75 | 1981.13 | .6192 |
| " "         | 18.20 | 500  | 106.8 | 32.36 | 1651.78 | .5699 |
| " "         | 18.35 | 350  | 105   | 22.48 | 1277.42 | .5078 |
| Whole Gate. | 17.84 | 850  | 107.5 | 55.38 | 2532.96 | .6489 |



## HOUSTON WHEEL.

This certifies, that a Water Wheel 50 inches in diameter, made of cast iron, cast whole, Register gate, known as the Houston Water Wheel, was sent to the Holyoke Testing Flume by O. E. Merrill & Co., Beloit, Wisconsin, to be tested.

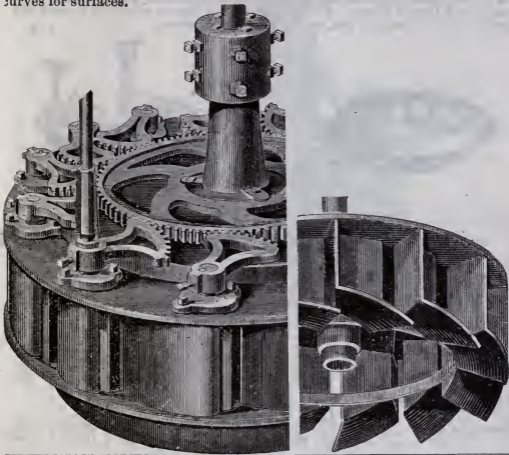


| No. of Test.       | Head.   | Weight.       | Rev. per Minute. | Horse Power. | Weir. | Cubic Feet. | Per Cent. |
|--------------------|---------|---------------|------------------|--------------|-------|-------------|-----------|
| Whole Gate, 1...   | 18.00   | 1500          | 112              | 101.80       | 1.555 | 3660.33     | .817      |
| " 2...             | 17.96   | 1600          | 106              | 102.78       | 1.545 | 3625.01     | .836      |
| " 3...             | 18.22   | 1650          | 106.6            | 106.60       | 1.554 | 3656.85     | .848      |
| " 4...             | 18.07   | 1700          | 103.6            | 106.72       | 1.569 | 3710.12     | .842      |
| " 5...             | 18.08   | 1725          | 102              | 106.60       | 1.573 | 3720.80     | .838      |
| " 6...             | 18.06   | 1620          | 111              | 108.95       | 1.565 | 3695.88     | .8635     |
| " 7...             | 18.04   | 1640          | 109              | 107.68       | 1.566 | 3699.44     | .8535     |
| " 8...             | 18.04   | 1640          | 110              | 109.33       | 1.565 | 3695.88     | .8675     |
| " 9...             | 18.04   | 1660          | 108              | 108.65       | 1.570 | 3713.66     | .858      |
| " 10...            | 18.04   | 1610          | 113              | 110.25       | 1.560 | 3678.12     | .880      |
| Part Gate, 12...   | 18.05   | 1400          | 113              | 95.88        | 1.520 | 3536.99     | .797      |
| " 13...            | 18.10   | 1240          | 117              | 87.92        | 1.484 | 3411.39     | .721      |
| " 14...            | 18.20   | 1040          | 119              | 75.01        | 1.400 | 3123.62     | .556      |
| " 15...            | 18.40   | 800           | 109              | 52.85        | 1.300 | 2823.81     | .588      |
| " 16...            | 18.58   | 575           | 110              | 38.33        | 1.126 | 2240.12     | .539      |
| " 17...            | 18.70   | 275           | 112              | 18.66        | .960  | 1749.84     | .302      |
| <b>Second Day,</b> | Flaring | Extensions to |                  | chutes       | off.  |             |           |
| Whole Gate, 28...  | 17.95   | 1550          | 109              | 102.39       | 1.535 | 3689.72     | .818      |
| " 29...            | 17.95   | 1590          | 105              | 101.18       | 1.537 | 3596.78     | .829      |
| " 30...            | 17.97   | 1535          | 113              | 105.12       | 1.525 | 3554.54     | .8716     |
| " 31...            | 17.97   | 1515          | 111              | 101.31       | 1.525 | 3554.54     | .840      |
| Part Gate, 33...   | 18.02   | 1300          | 116              | 91.39        | 1.490 | 3362.90     | .798      |
| " 34...            | 18.15   | 1140          | 115              | 79.45        | 1.400 | 3123.62     | .741      |
| " 35...            | 18.25   | 1000          | 110              | 66.67        | 1.315 | 2840.26     | .680      |
| " 36...            | 18.48   | 800           | 103              | 49.94        | 1.146 | 2301.59     | .621      |
| " 37...            | 18.62   | 500           | 105              | 31.81        | 1.030 | 1952.16     | .463      |
| " 38...            | 18.91   | 200           | 102              | 12.36        | .850  | 1445.74     | .240      |

Previous to the trial of this wheel it had been frozen solid in ice at the bottom of the flume for two weeks; to clear it, crowbars, blocks of wood, axes and other implements were used, some of which entered the wheel with a crash when it first started, probably throwing it out of center, for it required the strength of two men applied to the rim of the brake (six feet in diameter) to turn the wheel when the gate was closed.

## E. L. SMALL, URBANA, OHIO.

The results obtained may be found below. The peculiarity of the wheel consists in its gates and buckets, the gates being simply large faucets. The buckets are like shallow boxes, — Mr. Small believing angles better than curves for surfaces.

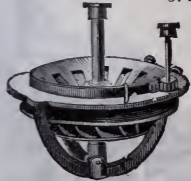


| No. of Test.                             | Head. | Weight. | Rev. per Minute. | Horse Power. | Weir. | Cubic Feet. | Per Cent. |
|--|-------|---------|------------------|--------------|-------|-------------|-----------|
| Whole Gate, 1 . . . . .                  | 18.30 | 480     | 181.6            | 30.62        | 1.148 | 1658.40     | .688      |
| " 2 . . . . .                            | 18.40 | 540     | 170              | 41.72        | 1.147 | 1656.28     | .725      |
| " 3 . . . . .                            | 18.29 | 570     | 149              | 38.61        | 1.147 | 1656.28     | .675      |
| " 4 . . . . .                            | 18.29 | 580     | 147              | 38.75        | 1.147 | 1656.28     | .677      |
| " 5 . . . . .                            | 18.28 | 535     | 169              | 41.09        | 1.148 | 1658.40     | .720      |
| " 6 . . . . .                            | 18.28 | 540     | 169              | 41.48        | 1.148 | 1658.40     | .724      |
| " 7 . . . . .                            | 18.28 | 545     | 165              | 40.88        | 1.148 | 1654.40     | .714      |
| " 8 . . . . .                            | 18.28 | 550     | 165              | 41.25        | 1.148 | 1658.40     | .718      |
| <b>Head Reduced,<br/>Gates Reversed.</b> |       |         |                  |              |       |             |           |
| Whole Gate, 10 . . . . .                 | 11.96 | 225     | 156              | 15.96        | .916  | 1188.55     | .595      |
| " 11 . . . . .                           | 12.03 | 310     | 136              | 19.34        | .962  | 1276.38     | .697      |
| " 12 . . . . .                           | 12.03 | 320     | 134.5            | 19.56        | .962  | 1276.38     | .674      |
| <b>Head Reduced,</b>                     |       |         |                  |              |       |             |           |
| Whole Gate, 14 . . . . .                 | 6.53  | 165     | 100              | 7.50         | .776  | 994.87      | .688      |
| " 15 . . . . .                           | 6.55  | 155     | 105              | 7.40         | .769  | 915.44      | .654      |
| 3-4 Gate, 17 . . . . .                   | 18.52 | 330     | 170              | 25.50        | .936  | 1227.15     | .594      |
| " 18 . . . . .                           | 18.51 | 325     | 174              | 25.70        | .937  | 1249.09     | .599      |
| " 19 . . . . .                           | 18.52 | 340     | 170              | 26.27        | .941  | 1235.35     | .594      |
| 1-2 Gate, 21 . . . . .                   | 18.72 | 150     | 170.2            | 11.60        | .721  | 840.00      | .391      |
| " 22 . . . . .                           | 18.60 | 180     | 171              | 13.68        | .718  | 828.45      | .471      |
| 4 Gates cl's'd, 24 . . . . .             | 18.51 | 270     | 170              | 20.86        | .840  | 1049.90     | .572      |

## J. W. UPHAM, WORCESTER, MASS.

Mr. Upham has been in the Water Wheel business for many years, and is known for his sterling integrity. The wheel he now builds is one similar to the Houston Wheel inverted. It has a register gate that works very easily, as it is on the inside at the top and small. The figures below were obtained from trials at my Lowell Flume. The two last sets of figures are given to show the speed at which it may be run, and produce good power.

J. E.



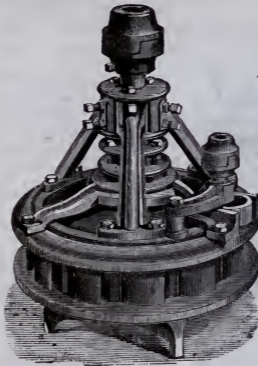
| No. of Test.                             | Head.  | Weight. | Rev. per Minute. | Horse Power. | Weir. | Cubic Feet. | Per Cent. |
|--|--------|---------|------------------|--------------|-------|-------------|-----------|
| Whole Gate, 1 . . . . .                  | 15.43  | 250     | 288.5            | 27.10        | .965  | 1259.68     | .737      |
| " 2 . . . . .                            | 15.45  | 285     | 201.5            | 28.10        | .945  | 1221.01     | .732      |
| " 3 . . . . .                            | 15.46  | 310     | 183.5            | 27.27        | .937  | 1205.40     | .774      |
| " 4 . . . . .                            | 15.465 | 330     | 179.5            | 26.92        | .932  | 1195.96     | .770      |
| " 5 . . . . .                            | 15.42  | 275     | 216.5            | 27.06        | .932  | 1234.58     | .752      |
| " 6 . . . . .                            | 15.42  | 250     | 200.5            | 27.09        | .944  | 1219.08     | .763      |
| " 7 . . . . .                            | 15.42  | 300     | 198              | 27.00        | .940  | 1211.36     | .765      |
| " 8 . . . . .                            | 15.425 | 310     | 193.5            | 27.27        | .936  | 1203.66     | .777      |
| " 9 . . . . .                            | 15.42  | 320     | 194.5            | 27.13        | .932  | 1195.96     | .778      |
| " 10 . . . . .                           | 15.43  | 330     | 176.5            | 26.47        | .928  | 1184.30     | .764      |
| " 11 . . . . .                           | 15.39  | 300     | 198              | 27.00        | .940  | 1211.36     | .766      |
| Tests of another wheel of the same kind. |        |         |                  |              |       |             |           |
| Whole Gate, 13 . . . . .                 | 15.60  | 100     | 300              | 18.13        | 1.117 | 1819.08     | .475      |
| " 14 . . . . .                           | 18.49  | 250     | 170              | 25.76        | 1.024 | 1175.01     | .750      |

## E. G. Libby, Medford, Mass.

The wheel, illustrated in the Upham report above, was designed by Mr. Libby, who has recently applied the water to the same kind of wheel, but through chutes similar to those of the Hercules. A 25-inch wheel so arranged was tested by me, Aug. 5, 1878, giving the following results:

| Head. | Weight. | Rev. per min. | Horse Power | Cubic feet. | Per Cent. |
|-------|---------|---------------|-------------|-------------|-----------|
| 18.23 | 350     | 298           | 47.40       | 2101.35     | .6552     |
| 18.35 | 250     | 288.5         | 33.92       | 1847.54     | .5297     |
| 18.38 | 200     | 293           | 26.63       | 1688.39     | .4543     |
| 18.48 | 100     | 309.5         | 14.06       | 1393.52     | .2890     |

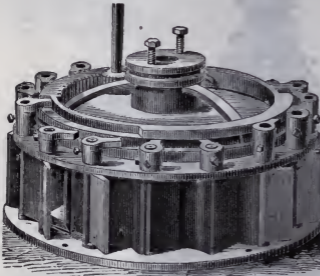
## N. F. BURNHAM, YORK, PENN.



| No. of Test.                           | Head. | Weight. | Rev.<br>per<br>Minute. | Horse<br>Power. | Weir. | Cubic<br>Feet. | Per<br>Cent. |
|--|-------|---------|------------------------|-----------------|-------|----------------|--------------|
| Whole Gate, 1...                       | 18.09 | 750     | 156                    | 53.18           | 1.308 | 1994.52        | .7824        |
| " 2...                                 | 18.12 | 800     | 151                    | 54.91           | 1.309 | 1996.77        | .787         |
| " 3...                                 | 18.10 | 810     | 150                    | 55.22           | 1.311 | 2001.27        | .808         |
| " 4...                                 | 18.10 | 820     | 148                    | 55.16           | 1.312 | 2003.83        | .807         |
| " 5...                                 | 18.10 | 830     | 147                    | 55.46           | 1.313 | 2005.78        | .810         |
| " 6...                                 | 18.09 | 840     | 148.5                  | 52.25           | 1.316 | 2012.55        | .761         |
| 2 chutes stopped<br>with blocks, 7...  | 18.30 | 680     | 146.4                  | 45.25           | 1.200 | 1755.97        | .747         |
| 3 chutes stopped<br>with blocks, 8...  | 18.30 | 615     | 146.4                  | 40.98           | 1.147 | 1642.74        | .722         |
| 4 chutes stopped<br>with blocks, 9...  | 18.22 | 500     | 147.2                  | 33.47           | 1.062 | 1464.92        | .665         |
| 5 chutes stopped<br>with blocks, 10... | 18.49 | 365     | 147                    | 24.39           | .919  | 1180.30        | .579         |
| Whole Gate, 11...                      | 18.11 | 830     | 146.4                  | 55.23           | 1.327 | 2037.41        | .794         |
| Part Gate, 12...                       | 18.20 | 680     | 147.4                  | 45.56           | 1.226 | 1812.58        | .733         |
| Without bl'ks, 13...                   | 18.25 | 615     | 145                    | 40.53           | 1.178 | 1708.50        | .689         |
| Whole Gate, 14...                      | 18.29 | 500     | 146                    | 33.18           | 1.082 | 1505.95        | .639         |
| " 15...                                | 18.37 | 365     | 146                    | 24.35           | .959  | 1252.11        | .567         |
| <b>Head Reduced.</b>                   |       |         |                        |                 |       |                |              |
| Whole Gate, 17...                      | 12.14 | 450     | 137                    | 28.02           | 1.120 | 1586.21        | .772         |
| " 18...                                | 12.15 | 475     | 133.5                  | 28.82           | 1.127 | 1600.95        | .778         |
| " 19...                                | 12.13 | 500     | 128.5                  | 29.21           | 1.134 | 1615.71        | .773         |
| " 20...                                | 12.13 | 525     | 123.5                  | 29.47           | 1.139 | 1626.29        | .792         |
| " 21...                                | 12.11 | 550     | 117                    | 29.25           | 1.143 | 1634.77        | .784         |
| " 22...                                | 12.09 | 575     | 115                    | 30.05           | 1.151 | 1651.76        | .798         |

## Patent Curbs.

Designed to Economize Water at Part Gate.



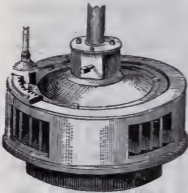
This, by W. S. Davis, Warner, N. H., has 16 chutes or gates that open successively, two at a time, tested May, 1871. Wheel a rough imitation of the Swain.

16 chutes open, perc'tge, .6346.

14 chutes open, perc'tge, .4765.

10 chutes open, perc'tge, .3955.

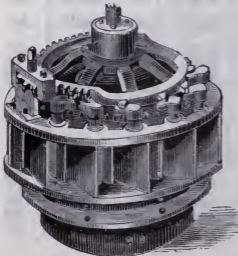
6 chutes open, perc'tge, .2968.



J. T. Case, Bristol, Conn.

National Water Wheel Company.

See Report of Tests for that Company.

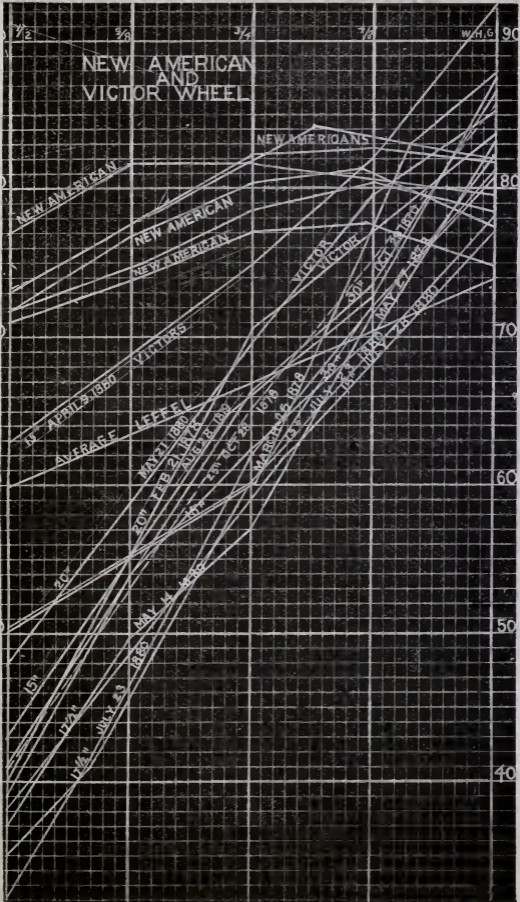


John L. Stowe, Newark,  
New Jersey.

Test of a 24-inch, April, 1878.

| Head. | W'ht. | Rev.  | H. P. | Cubic feet. | Per-<br>Cent |
|-------|-------|-------|-------|-------------|--------------|
| 18.26 | 425   | 217.5 | 28 01 | 1005.12     | .8075        |
| 18.40 | 345   | 216   | 22.58 | 854.33      | .7590        |
| 18.55 | 235   | 211   | 15.02 | 607.23      | .7054        |

The Davis and Case chutes are closed at their outer ends, while the Stowe plan closes them at their inner end.





## List of Wheels Tested.

*Those having a star placed before name are specially reported,*

\*AMERICAN, Stout, Mills & Temple, Dayton, Ohio. The best of the early wheels.

\*ANGELL, Providence, R. I. Double discharge, central and down. Buckets cast separate, then bolted to hub, very apt to shear off. Fly trap gates, very leaky; is steadier, gives more power and higher useful effect with central discharge stopped.

ARROWSMITH, Lockport, N. Y. Central discharge with sheets of steel extending the inner edge of buckets until they met like the sides of a wedge upon the supposition that at part gate the pressure of water would regulate the opening, and produce high percentage at any stage of gate. The plan was a failure. Highest useful effect, 68 per cent.

\*BURNHAM, York, Pa. Downward discharge. Outside register gate.

\*BOYDEN FOURNEYRON. Made at Chicopee, Holyoke and other places. Outward discharge. Poor at part gate and of small capacity for diameter. Useful effect of those I have tested has varied from 46 to 85 per cent.

BUZZELL, St. Johnsbury, Vt. Scroll. Downward discharge. So arranged that proportionally it gives good part gate results. Highest percentage, 56 per cent.

BASTION, Canton, N. Y. Similar to the Curtis, but I think not manufactured now. Tested one with wicket gate in draft tube below the wheel, which proved the plan to be bad. With register gate, highest useful effect, 70 per cent.

BEE, Lancaster, Mass. Downward discharge. Babbitted in the upper bearing, and became bound while being tested, so that 58 per cent., the highest result obtained, was no indication of what the wheel would have done if it had been in a proper condition.

BRYANT BRO'S., Westchesterfield, Mass. Downward discharge. Gave 65 per cent.

BRYSON TURRETT, Miles Greenwood, Cincinnati, Ohio. Down and central. 75 per cent. Not manufactured now.

BLAKE, Pepperell, Mass. Scroll. Obsolete. 50 per cent.

\*BARBER, Ballston Spa, N. Y. 79.29 per cent.

\*BLACKSTONE, in Elmer, Leffel and American curbs. See special reports.

BODINE JONVAL, Mount Morris, N. Y. If made at all. 76 per cent.

\*BOLLINGER, York, Pa. Central discharge. 70 per cent.

\*COX, Ellsworth, N. Y. Double, downward discharge. 70 per cent.

\*CASE, National Water Wheel Co., Bristol, Conn. See special report.

\*CHASE, Orange, Mass. See report.

CUSHMAN, Hartford, Conn. Scroll. 50 per cent. Discharge up and down.

\*COLEMAN, Turner's Falls.

\*CURTIS, Ogdensburg, N. Y.

COOK, Lake Village, N. H. Has had several kinds tested, but builds upon a different plan now. Highest useful effect of those tried, .7752 per cent.

CHAPMAN, Clark & Chapman, Turner's Falls, Mass. Highest efficiency, 52 per cent.

\*ECLIPSE, Stilwell & Bierce Manuf'g Co., Dayton, Ohio.

GROW, Dubuque, Iowa. 69 per cent.

GILLESPIE, Turner's Falls, Mass. Two wheels upon horizontal shaft. Four-neyron wheels. 54 per cent.

GREEN, Juda, Wis. 50 per cent.

GEYLINE, Philadelphia, Pa. Jonval wheels. Telescopic gate below wheels. 56 per cent.

HOLMAN, Adams, N. Y. 47 per cent.

HUMMING BIRD, Willis Read, Danbury, Conn. Two. One central, one downward discharge. 62 per cent.

\*HOUSTON, Beloit, Wis. Has had many wheels tested. Useful effect, ranging from .774 to .9006 per cent. Gate works very hard, and is poor at part gate.

\*HERCULES, Holyoke, Mass. See special report.

\*HOLYOKE MACHINE Co., Holyoke, Mass. See special report.

\*HUNT, Orange, Mass. See special report.

\*HUMPHREY, Humphrey Machine Co., Keene, N. H.

KINDLEBERGER, Cincinnati, Ohio. .6246 per cent.

KNOWLTON, Saccarappa, Maine. 59 per cent. Abandoned.

LEAVITT, Lebanon, N. H. .637 per cent.

LUTHER, Iowa. Scroll. 70 per cent.

\*LEFFEL, Springfield, Ohio. Have tested many of them. Useful effect varied from 40 to 79 per cent.

\*LUCAS, Hastings, Minn. See special report.

\*LIBBY, Medford, Mass. See special report.

LESNER, Fultonville, N. Y. Central discharge. Central discharge wheels are behind the age.

\*MULLIKIN, Lansing, Iowa. See special report. The wheel is very poorly made.

\*MOSSER, Allentown, Penn. See special report.

MALLERY, Dryden, N. Y. .769 per cent.

\*NATIONAL, Josiah Buzzby, Crosswicks, N. J. .676 per cent. Complicated gates.

\*NATIONAL, Bristol, Conn. See special report of the Case wheel.

\*PERRY, Bridgton, Maine. See special report.

PLATT, New Brighton, Pa. Two wheels upon a horizontal shaft. .585 per cent.

RANEY, New Castle, Penn. Became bound in its stuffing box while being tested, so that the test was no indication of what it would have done if it had been well constructed. Useful effect, per test, .667 per cent.

\*RISDON, Mt. Holly, New Jersey. See special report.

REYNOLDS, Oswego, N. Y. Scroll. 50 per cent.

REASER, Milwaukee, Wis. Flutter wheel placed on end between plates; would not run its own weight to speed.

SHERWOOD, Independence, Iowa. A Fourneyron, 63 per cent., and a downward discharge. .761 per cent.

\*SWAIN, North Chelmsford, Mass. See special report.

\*SMITH, York, Pa. See special report.

STEVENSON, New York City. Two Jonval wheels placed together, one discharging downward the other upwards, the upper discharge passing into a dome "or vacuum," then downward in an annular tube, as shown in the Fulton & Myers' plan, which is illustrated in the group of perpetual motion inventions.

\*SMALL, Urbana, Ohio. See report.

STETSON, Fitchburg, Mass. Central and downward discharge, register gates, not manufactured now. .793 per cent.

\*STOWE, Newark, New Jersey.

STAPLES, Boston, Mass. Central discharge, three divisions, with a cylinder gate raised by a screw similar to that of the Hercules; the object of the three divisions of the wheel was to gain high part gate results, as it was supposed that either division would give as high results as the whole combined. Highest results obtained, 77 per cent.

TRULLINGER, Oswego, Oregon. Discharge down and up into a vacuum like Stevenson's. 70 per cent.

TYLER, Claremont, N. H. Old scroll, useful effect ranged from 50 to 67 per cent.

\*TYLER. New scroll and flume wheels. See special reports.

TELLER, Fort Plain, N. Y. Wheel in divisions like the Staples and for the same purpose. Useful effect, .645 per cent.

TERRY, Terryville, Ct. Boyden or Fourneyron with two register gates, one inside of chutes, the other outside. 58 per cent. Abandoned.

\*TUTTLE, Waterville, Maine. 58 per cent.

TICE, Cincinnati, Ohio. Re-invention of the old Schiele wheel, illustrations of it may be found in Wiesbach's or almost any other work treating of turbines twenty years since.

\*THOMPSON, Springfield, Mo., and Silver Creek, N. Y.

\*TWITCHELL, Pulaski, N. Y. See under the head of Perpetual Motion.

UPHAM, Worcester, Mass. Central discharge, tried in scroll, also in flume curb. 72 in scroll. 68 per cent. in flume curb. Abandoned.

\*UPHAM & LIBBY. See special report.

\*VICTOR, Stilwell & Bierce Manfg Co., Dayton, Ohio.

VANDEWATER, Rochester, N. Y. Downward discharge, cylinder gate. .778 per cent. Wheel struck bad in curb while being tested.

WATSON JONVAL, Paterson, N. J. Old. 49 per cent.

\*WALSH, Waupaca, Wis.

\*WHITNEY, Leominster, Mass. Old plan in flume and scroll curbs abandoned. Percentage of scroll, old wheel, 40 per cent. Flume, 72. For new plan, see special report.

WAGNER, Chicago, Ill. Foolishly complicated in discharge and limited capacity. Highest useful effect, .738 per cent.

WHEELER, Berlin, Mass. Central and downward discharge; but did best every way with central discharge stopped with blocks. Discharged the same quantity of water after blocking central discharge. .745 per cent. Not manufactured now.

\*WYNKOOP. See special report.

\*WETMORE, Claremont, N. H. See special report.

\*WOLF, Allentown, Pa. In taking one of the make apart, a few days since, many small pieces were found that were used for blocking up gate suspension. Such pieces are very liable to get lost and might, with little trouble, be rendered unnecessary, by casting projecting pieces on the surfaces. "Patchwork" is objectionable in turbine building. See special report for efficiency.

## CHARLA.



MISS CHARLA A. ADAMS.

A Green Mountain girl, receiving three months' schooling in the summer and occasional spells in the winter. At thirteen away to the Lowell mills, graduating from there at nineteen as mathematician of my testing work, and as I had never owned a schoolbook until buying them for my children, it will readily be conceived that we were not handicapped by the Massachusetts school system.

Without exception Charla was the most expeditious mathematician and best adapted for the purpose of any one I have ever known engaged in the work.

### Weight of a Cubic foot of Pure Water at Different Temperatures.

| Degrees. | Weight. | Degrees. | Weight. | Degrees. | Weight. | Degrees. | Weight. |
|----------|---------|----------|---------|----------|---------|----------|---------|
| 32       | 62.375  | 45       | 62.378  | 59       | 62.336  | 73       | 62.249  |
| 33       | 62.377  | 46       | 62.376  | 60       | 62.331  | 74       | 62.242  |
| 34       | 62.378  | 47       | 62.375  | 61       | 62.326  | 75       | 62.234  |
| 35       | 62.379  | 48       | 62.373  | 62       | 62.321  | 76       | 62.225  |
| 36       | 62.380  | 49       | 62.371  | 63       | 62.316  | 77       | 62.217  |
| 37       | 62.381  | 50       | 62.368  | 64       | 62.310  | 78       | 62.208  |
| 38       | 62.381  | 51       | 62.365  | 65       | 62.304  | 79       | 62.199  |
| 39(max)  | 62.382  | 52       | 62.363  | 66       | 62.298  | 80       | 62.190  |
| 39.38    | 62.382  | 53       | 62.359  | 67       | 62.292  | 81       | 62.181  |
| 40       | 62.382  | 54       | 62.356  | 68       | 62.285  | 82       | 62.172  |
| 41       | 62.381  | 55       | 62.352  | 69       | 62.278  | 83       | 62.162  |
| 42       | 62.381  | 56       | 62.349  | 70       | 62.272  | 84       | 62.152  |
| 43       | 62.380  | 57       | 62.345  | 71       | 62.264  | 85       | 62.142  |
| 44       | 62.379  | 58       | 62.340  | 72       | 62.257  | 86       | 62.132  |



| Table of Inches and Sixteenths Reduced to Decimals of a Foot. |      |      |      |      |      |      |      |      |      |      |      |      |
|---|------|------|------|------|------|------|------|------|------|------|------|------|
| SIXTEENTHS.   | 0    | 1    | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    | 10   | 11   |
| 0   | .000 | .083 | .167 | .250 | .333 | .417 | .500 | .583 | .667 | .750 | .833 | .917 |
| 1   | .005 | .089 | .172 | .255 | .339 | .422 | .505 | .589 | .672 | .755 | .839 | .922 |
| 2   | .010 | .094 | .177 | .260 | .344 | .427 | .510 | .594 | .677 | .760 | .844 | .927 |
| 3   | .016 | .099 | .182 | .266 | .349 | .432 | .516 | .599 | .682 | .766 | .849 | .932 |
| 4   | .021 | .104 | .187 | .271 | .354 | .437 | .521 | .604 | .687 | .771 | .854 | .937 |
| 5   | .026 | .109 | .193 | .276 | .359 | .443 | .526 | .609 | .693 | .776 | .859 | .943 |
| 6   | .031 | .115 | .198 | .281 | .365 | .448 | .531 | .615 | .698 | .781 | .865 | .948 |
| 7   | .036 | .120 | .203 | .286 | .370 | .453 | .536 | .620 | .703 | .786 | .870 | .953 |
| 8   | .042 | .125 | .208 | .292 | .375 | .458 | .542 | .625 | .708 | .792 | .875 | .958 |
| 9   | .047 | .130 | .214 | .297 | .380 | .464 | .547 | .630 | .714 | .797 | .880 | .964 |
| 10  | .052 | .135 | .219 | .302 | .385 | .469 | .552 | .635 | .719 | .802 | .885 | .969 |
| 11  | .057 | .141 | .224 | .307 | .391 | .474 | .557 | .641 | .724 | .807 | .891 | .974 |
| 12  | .062 | .146 | .229 | .312 | .396 | .479 | .562 | .646 | .729 | .812 | .896 | .979 |
| 13  | .068 | .151 | .234 | .318 | .401 | .484 | .568 | .651 | .734 | .818 | .901 | .984 |
| 14  | .073 | .156 | .240 | .323 | .406 | .490 | .573 | .656 | .740 | .823 | .906 | .990 |
| 15  | .078 | .161 | .247 | .328 | .411 | .495 | .578 | .661 | .745 | .828 | .911 | .995 |

## The Emerson Weir Tables,

For weirs with end contractions, were computed for me by Miss Charla A. Adams, some 20,000 quantities; these have done much towards reducing the cost of water wheel tests and water measurements, at the same time producing far greater accuracy.

These were computed by the Francis formula, from zero up. The experiments upon which that formula was prepared were not extended below a depth of .500 of a foot, but it is often necessary to use it at a much less depth; and experience proves it to be sufficiently accurate for all practical purposes.

The computations are per minute. If the weir is properly constructed there is no need of correction, if not properly constructed a correction is mere guess-work or conjecture.

The Francis tables for the one foot weir are calculated for weir without contraction; consequently, by using those in connection with the others, by adding to or subtracting from, the quantity flowing over a weir of any length may readily be found.

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|---------|---------|---------|---------|----------|----------|----------|----------|
|                      | Feet.               | 2 Feet. | 3 Feet. | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| .001                 | .013                | .019    | .025    | .038    | .044    | .051    | .063    | .076     | .101     | .127     |          |
| .002                 | .045                | .067    | .064    | .134    | .154    | .179    | .224    | .268     | .358     | .475     |          |
| .003                 | .077                | .115    | .103    | .230    | .264    | .307    | .385    | .460     | .615     | .823     |          |
| .004                 | .109                | .163    | .142    | .326    | .374    | .435    | .547    | .653     | .872     | 1.171    |          |
| .005                 | .141                | .212    | .281    | .424    | .494    | .565    | .709    | .847     | 1.130    | 1.410    |          |
| .006                 | .194                | .289    | .384    | .542    | .674    | .775    | .966    | 1.157    | 1.543    | 1.927    |          |
| .007                 | .247                | .366    | .487    | .661    | .854    | .981    | 1.223   | 1.467    | 1.956    | 2.444    |          |
| .008                 | .301                | .443    | .591    | .780    | 1.034   | 1.188   | 1.481   | 1.777    | 2.369    | 2.967    |          |
| .009                 | .355                | .521    | .695    | .899    | 1.214   | 1.375   | 1.739   | 2.087    | 2.782    | 3.478    |          |
| .010                 | .409                | .599    | .799    | 1.018   | 1.397   | 1.598   | 1.997   | 2.397    | 3.196    | 3.515    |          |
| .011                 | .46                 | .74     | .93     | 1.24    | 1.87    | 1.86    | 2.33    | 2.79     | 3.71     | 4.666    |          |
| .012                 | .52                 | .83     | 1.06    | 1.47    | 2.10    | 2.21    | 2.67    | 3.19     | 4.22     | 5.33     |          |
| .013                 | .59                 | .92     | 1.19    | 1.71    | 2.34    | 2.40    | 3.01    | 3.59     | 4.74     | 6.00     |          |
| .014                 | .66                 | 1.01    | 1.32    | 1.95    | 2.57    | 2.67    | 3.35    | 3.99     | 5.25     | 6.67     |          |
| .015                 | .73                 | 1.10    | 1.46    | 2.20    | 2.84    | 2.94    | 3.69    | 4.40     | 5.87     | 7.34     |          |
| .016                 | .81                 | 1.21    | 1.62    | 2.43    | 3.06    | 3.25    | 3.94    | 4.87     | 6.50     | 8.13     |          |
| .017                 | .89                 | 1.33    | 1.78    | 2.66    | 3.28    | 3.56    | 4.45    | 5.34     | 7.13     | 8.92     |          |
| .018                 | .97                 | 1.45    | 1.94    | 2.90    | 3.50    | 3.87    | 4.84    | 5.81     | 7.76     | 9.97     |          |
| .019                 | 1.05                | 1.57    | 2.10    | 3.14    | 3.72    | 4.19    | 5.24    | 6.28     | 8.40     | 10.50    |          |
| .020                 | 1.13                | 1.69    | 2.27    | 3.38    | 3.95    | 4.51    | 5.64    | 6.76     | 9.04     | 11.30    |          |
| .021                 | 1.22                | 1.82    | 2.44    | 3.65    | 4.26    | 4.87    | 6.09    | 7.29     | 9.75     | 12.19    |          |
| .022                 | 1.31                | 1.95    | 2.61    | 3.92    | 4.57    | 5.23    | 6.54    | 7.83     | 10.47    | 13.09    |          |
| .023                 | 1.40                | 2.08    | 2.78    | 4.19    | 4.88    | 5.59    | 6.99    | 8.37     | 11.19    | 13.99    |          |
| .024                 | 1.49                | 2.22    | 2.95    | 4.46    | 5.20    | 5.95    | 7.44    | 8.91     | 11.91    | 14.89    |          |
| .025                 | 1.58                | 2.36    | 3.12    | 4.73    | 5.52    | 6.31    | 7.89    | 9.45     | 12.63    | 15.79    |          |
| .026                 | 1.67                | 2.51    | 3.32    | 5.02    | 5.86    | 6.70    | 8.38    | 10.05    | 13.42    | 16.78    |          |
| .027                 | 1.77                | 2.66    | 3.52    | 5.32    | 6.20    | 7.10    | 8.88    | 10.65    | 14.21    | 17.77    |          |
| .028                 | 1.87                | 2.81    | 3.72    | 5.62    | 6.55    | 7.50    | 9.38    | 11.25    | 15.00    | 18.76    |          |
| .029                 | 1.97                | 2.96    | 3.93    | 5.92    | 6.90    | 7.90    | 9.88    | 11.85    | 15.80    | 19.75    |          |
| .030                 | 2.07                | 3.11    | 4.14    | 6.22    | 7.25    | 8.30    | 10.38   | 12.46    | 16.60    | 20.75    |          |
| .031                 | 2.17                | 3.27    | 4.37    | 6.52    | 7.63    | 8.74    | 10.91   | 13.10    | 17.46    | 21.83    |          |
| .032                 | 2.28                | 3.43    | 4.60    | 6.82    | 8.01    | 9.18    | 11.45   | 13.74    | 18.32    | 22.91    |          |
| .033                 | 2.39                | 3.59    | 4.84    | 7.13    | 8.39    | 9.62    | 11.99   | 14.39    | 19.18    | 23.99    |          |
| .034                 | 2.50                | 3.75    | 5.08    | 7.43    | 8.77    | 10.07   | 12.53   | 15.04    | 20.05    | 25.17    |          |
| .035                 | 2.61                | 3.91    | 5.22    | 7.84    | 9.15    | 10.52   | 13.07   | 15.69    | 20.92    | 26.15    |          |



| Depth on Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |         |          |          |          |
|----------------|---------------------|---------|---------|---------|---------|---------|---------|----------|----------|----------|
|                | Feet.               | 2 Feet. | 3 Feet. | 4 Feet. | 5 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. |
| .036           | 2.72                | 4.08    | 5.45    | 8.18    | 9.55    | 10.97   | 13.64   | 16.38    | 21.84    | 27.31    |
| .037           | 2.83                | 4.25    | 5.68    | 8.53    | 9.95    | 11.42   | 14.21   | 17.07    | 22.77    | 28.47    |
| .038           | 2.95                | 4.42    | 5.91    | 8.88    | 10.35   | 11.87   | 14.78   | 17.76    | 23.71    | 29.63    |
| .039           | 3.07                | 4.60    | 6.14    | 9.23    | 10.76   | 11.32   | 15.35   | 18.46    | 24.64    | 30.79    |
| .040           | 3.19                | 4.78    | 6.38    | 9.58    | 11.17   | 12.77   | 15.93   | 19.16    | 25.56    | 31.95    |
| .041           | 3.31                | 4.96    | 6.62    | 9.94    | 11.60   | 13.26   | 16.55   | 19.90    | 26.54    | 33.18    |
| .042           | 3.43                | 5.14    | 6.86    | 10.31   | 12.03   | 13.75   | 17.17   | 20.64    | 27.53    | 34.41    |
| .043           | 3.55                | 5.32    | 7.11    | 10.68   | 12.47   | 14.25   | 17.80   | 21.38    | 28.52    | 35.65    |
| .044           | 3.67                | 5.51    | 7.36    | 11.05   | 12.91   | 14.75   | 18.43   | 22.12    | 29.51    | 36.89    |
| .045           | 3.80                | 5.70    | 7.61    | 11.42   | 13.35   | 15.25   | 19.06   | 22.88    | 30.50    | 38.13    |
| .046           | 3.93                | 5.89    | 7.87    | 11.81   | 13.80   | 15.76   | 19.71   | 23.66    | 31.54    | 39.43    |
| .047           | 4.06                | 6.08    | 8.13    | 12.20   | 14.25   | 16.28   | 20.36   | 24.44    | 32.58    | 40.73    |
| .048           | 4.19                | 6.27    | 8.39    | 12.59   | 14.70   | 16.80   | 21.01   | 25.22    | 33.62    | 42.03    |
| .019           | 4.32                | 6.47    | 8.66    | 12.98   | 15.15   | 17.32   | 21.66   | 26.00    | 34.67    | 43.34    |
| .050           | 4.45                | 6.67    | 8.93    | 13.38   | 15.69   | 17.84   | 22.32   | 26.78    | 35.72    | 44.65    |
| .051           | 4.58                | 6.87    | 9.20    | 13.79   | 16.09   | 18.39   | 23.00   | 27.60    | 36.81    | 46.02    |
| .052           | 4.71                | 7.07    | 9.47    | 14.20   | 16.57   | 18.94   | 23.68   | 28.42    | 37.90    | 47.39    |
| .053           | 4.84                | 7.28    | 9.74    | 14.61   | 17.05   | 19.49   | 24.36   | 29.24    | 39.00    | 48.76    |
| .054           | 4.99                | 7.49    | 10.01   | 15.02   | 17.53   | 20.04   | 25.05   | 30.06    | 40.10    | 50.14    |
| .055           | 5.13                | 7.70    | 10.28   | 15.43   | 18.01   | 20.59   | 25.74   | 30.90    | 41.20    | 51.52    |
| .056           | 5.27                | 7.91    | 10.56   | 15.86   | 18.51   | 21.16   | 26.45   | 31.76    | 42.35    | 52.95    |
| .057           | 5.41                | 8.12    | 10.84   | 16.29   | 19.01   | 21.73   | 27.17   | 32.62    | 43.50    | 54.38    |
| .058           | 5.55                | 8.33    | 11.12   | 16.72   | 19.51   | 22.30   | 27.89   | 33.48    | 44.71    | 55.81    |
| .059           | 5.69                | 8.55    | 11.41   | 17.15   | 20.01   | 22.87   | 28.61   | 34.34    | 45.86    | 57.24    |
| .060           | 5.84                | 8.77    | 11.71   | 17.58   | 20.52   | 23.45   | 29.33   | 35.20    | 46.95    | 58.69    |
| .061           | 5.98                | 8.99    | 12.00   | 18.02   | 21.04   | 24.04   | 30.07   | 36.09    | 48.16    | 60.18    |
| .062           | 6.13                | 9.11    | 12.30   | 18.46   | 21.56   | 24.64   | 30.81   | 36.99    | 49.37    | 61.68    |
| .063           | 6.28                | 9.33    | 12.60   | 18.91   | 22.08   | 25.24   | 31.56   | 37.89    | 50.58    | 63.18    |
| .064           | 6.43                | 9.56    | 12.90   | 19.36   | 22.61   | 25.84   | 32.31   | 38.79    | 51.79    | 64.68    |
| .065           | 6.58                | 9.89    | 13.20   | 19.81   | 23.14   | 26.44   | 33.06   | 39.69    | 53.00    | 66.18    |
| .066           | 6.73                | 10.12   | 13.50   | 20.27   | 23.68   | 27.06   | 33.83   | 40.62    | 54.23    | 67.73    |
| .067           | 6.88                | 10.35   | 13.81   | 20.74   | 24.22   | 27.62   | 34.61   | 41.55    | 55.46    | 69.28    |
| .068           | 7.03                | 10.58   | 14.12   | 21.21   | 24.76   | 28.24   | 35.39   | 42.48    | 56.69    | 70.83    |
| .069           | 7.19                | 10.81   | 14.43   | 21.68   | 25.30   | 28.86   | 36.17   | 43.41    | 57.92    | 72.39    |
| .070           | 7.35                | 11.04   | 14.74   | 22.15   | 25.85   | 29.55   | 36.95   | 44.35    | 59.15    | 73.95    |
| .071           | 7.51                | 11.28   | 15.06   | 22.63   | 26.41   | 30.19   | 37.75   | 45.31    | 60.46    | 75.55    |
| .072           | 7.67                | 11.52   | 15.8    | 23.11   | 26.97   | 30.83   | 38.55   | 46.28    | 61.77    | 77.15    |
| .073           | 7.83                | 11.76   | 15.71   | 23.59   | 27.53   | 31.47   | 39.36   | 47.25    | 63.08    | 78.75    |
| .074           | 7.99                | 11.98   | 16.03   | 24.07   | 28.10   | 32.12   | 40.17   | 48.22    | 64.38    | 80.36    |
| .075           | 8.15                | 12.25   | 16.35   | 24.56   | 28.67   | 32.77   | 40.98   | 49.19    | 65.60    | 81.97    |
| .076           | 8.31                | 12.49   | 16.68   | 25.05   | 29.25   | 33.43   | 41.81   | 50.18    | 66.93    | 83.64    |
| .077           | 8.47                | 12.74   | 17.03   | 25.55   | 29.83   | 34.09   | 42.64   | 51.18    | 68.26    | 85.31    |
| .078           | 8.63                | 12.99   | 17.38   | 26.05   | 30.41   | 34.75   | 43.47   | 52.18    | 69.59    | 86.99    |
| .079           | 8.80                | 13.24   | 17.73   | 26.55   | 30.99   | 35.42   | 44.30   | 53.18    | 70.92    | 88.67    |
| .080           | 8.97                | 13.49   | 18.01   | 27.05   | 31.57   | 36.09   | 45.14   | 54.18    | 72.26    | 90.35    |
| .081           | 9.14                | 13.74   | 18.35   | 27.56   | 32.17   | 36.77   | 45.99   | 55.20    | 73.63    | 92.06    |
| .082           | 9.31                | 13.99   | 18.69   | 28.07   | 32.77   | 37.45   | 46.85   | 56.23    | 75.00    | 93.78    |
| .083           | 9.48                | 14.24   | 19.03   | 28.59   | 33.37   | 38.14   | 47.71   | 57.26    | 76.37    | 95.50    |
| .084           | 9.65                | 14.49   | 19.37   | 29.01   | 33.97   | 38.83   | 48.57   | 58.29    | 77.74    | 97.22    |
| .085           | 9.82                | 14.75   | 19.72   | 29.62   | 34.58   | 39.52   | 49.43   | 59.32    | 79.13    | 98.94    |
| .086           | 9.99                | 15.01   | 20.07   | 30.15   | 35.19   | 40.22   | 50.31   | 60.38    | 80.54    | 100.71   |
| .087           | 10.16               | 15.27   | 20.42   | 30.68   | 35.81   | 40.92   | 51.19   | 61.44    | 81.95    | 102.48   |
| .088           | 10.33               | 15.54   | 20.77   | 31.21   | 36.43   | 41.63   | 52.07   | 62.50    | 83.87    | 104.28   |
| .089           | 10.51               | 15.81   | 21.12   | 31.74   | 37.05   | 42.34   | 52.95   | 63.56    | 84.79    | 106.02   |
| .090           | 10.69               | 16.08   | 21.48   | 32.27   | 37.67   | 43.05   | 53.84   | 64.63    | 86.21    | 107.80   |
| .091           | 10.87               | 16.35   | 21.84   | 32.81   | 38.30   | 43.77   | 54.75   | 65.72    | 87.66    | 109.62   |
| .092           | 11.05               | 16.62   | 22.20   | 33.35   | 38.93   | 44.50   | 55.66   | 66.81    | 89.11    | 111.44   |
| .093           | 11.23               | 16.89   | 22.56   | 33.89   | 39.57   | 45.23   | 56.57   | 67.90    | 90.57    | 113.26   |

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |         |          |          |          |
|----------------------|---------------------|---------|---------|---------|---------|---------|---------|----------|----------|----------|
|                      | Feet.               | 2 Feet. | 3 Feet. | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. |
| .094                 | 11.41               | 17.16   | 22.92   | 34.44   | 40.21   | 45.96   | 57.48   | 68.99    | 92.03    | 115.08   |
| .095                 | 11.58               | 17.44   | 23.29   | 34.99   | 40.85   | 46.69   | 58.39   | 70.09    | 93.49    | 116.90   |
| .096                 | 11.76               | 17.77   | 23.66   | 35.55   | 41.50   | 47.43   | 59.32   | 71.21    | 94.98    | 118.78   |
| .097                 | 11.94               | 17.99   | 24.03   | 36.11   | 42.15   | 48.17   | 60.25   | 72.33    | 96.47    | 120.66   |
| .098                 | 12.13               | 18.27   | 24.40   | 36.67   | 42.80   | 48.92   | 61.18   | 73.45    | 97.96    | 122.54   |
| .099                 | 12.32               | 18.55   | 24.77   | 37.23   | 42.45   | 49.67   | 62.12   | 74.57    | 99.46    | 124.42   |
| .100                 | 12.51               | 18.83   | 25.14   | 37.78   | 44.11   | 50.42   | 63.06   | 75.69    | 100.96   | 126.30   |
| .101                 | 12.69               | 19.11   | 25.52   | 38.35   | 44.77   | 51.18   | 64.01   | 76.84    | 102.49   | 128.20   |
| .102                 | 12.88               | 19.39   | 25.90   | 38.92   | 45.43   | 51.94   | 64.96   | 77.99    | 104.02   | 130.10   |
| .103                 | 13.07               | 19.67   | 26.28   | 39.49   | 46.10   | 52.70   | 65.91   | 79.14    | 105.55   | 132.00   |
| .104                 | 13.26               | 19.96   | 26.66   | 40.06   | 46.77   | 53.47   | 66.87   | 80.29    | 107.08   | 133.90   |
| .105                 | 13.45               | 20.25   | 27.04   | 40.64   | 47.44   | 54.24   | 67.83   | 81.44    | 108.62   | 135.81   |
| .106                 | 13.64               | 20.53   | 27.43   | 41.21   | 48.12   | 55.02   | 68.81   | 82.61    | 110.17   | 137.77   |
| .107                 | 13.83               | 20.81   | 27.82   | 41.79   | 48.80   | 55.80   | 69.79   | 83.78    | 111.73   | 139.73   |
| .108                 | 14.02               | 21.10   | 28.21   | 42.38   | 49.49   | 56.58   | 70.77   | 84.95    | 113.29   | 141.69   |
| .109                 | 14.21               | 21.39   | 28.60   | 42.97   | 50.18   | 57.36   | 71.75   | 85.12    | 114.85   | 143.65   |
| .110                 | 14.41               | 21.71   | 29.00   | 43.57   | 50.87   | 58.15   | 72.73   | 87.30    | 116.41   | 145.62   |
| .111                 | 14.60               | 22.00   | 29.39   | 44.17   | 51.57   | 58.95   | 73.73   | 88.50    | 118.07   | 147.62   |
| .112                 | 14.80               | 22.30   | 29.78   | 44.77   | 52.27   | 59.75   | 74.73   | 89.70    | 119.67   | 149.63   |
| .113                 | 15.00               | 22.60   | 30.11   | 45.37   | 52.97   | 60.55   | 75.73   | 90.90    | 121.27   | 151.64   |
| .114                 | 15.20               | 22.90   | 30.58   | 45.97   | 53.67   | 61.35   | 76.73   | 92.11    | 122.88   | 153.65   |
| .115                 | 15.40               | 23.20   | 30.98   | 46.57   | 54.37   | 62.15   | 77.71   | 93.32    | 124.49   | 155.66   |
| .116                 | 15.60               | 23.50   | 31.39   | 47.18   | 55.08   | 62.96   | 78.76   | 94.55    | 126.13   | 157.71   |
| .117                 | 15.80               | 23.80   | 31.80   | 47.79   | 55.79   | 63.78   | 79.78   | 95.78    | 127.77   | 159.76   |
| .118                 | 16.00               | 24.10   | 32.21   | 48.40   | 56.50   | 64.50   | 80.80   | 97.01    | 129.41   | 161.81   |
| .119                 | 16.20               | 24.41   | 32.62   | 49.01   | 57.22   | 65.32   | 81.82   | 98.25    | 131.05   | 163.86   |
| .120                 | 16.41               | 24.72   | 33.02   | 49.63   | 57.91   | 66.24   | 82.85   | 99.49    | 132.69   | 165.91   |
| .121                 | 16.61               | 25.03   | 33.43   | 50.25   | 58.67   | 67.07   | 83.89   | 100.74   | 134.36   | 168.00   |
| .122                 | 16.81               | 25.34   | 33.84   | 50.87   | 59.40   | 67.90   | 84.95   | 102.09   | 136.03   | 170.09   |
| .123                 | 17.01               | 25.65   | 34.26   | 51.49   | 60.17   | 68.74   | 85.98   | 103.34   | 137.70   | 172.18   |
| .124                 | 17.22               | 25.97   | 34.68   | 52.11   | 60.90   | 69.58   | 87.03   | 104.59   | 139.38   | 174.27   |
| .125                 | 17.43               | 26.27   | 35.09   | 52.75   | 61.59   | 70.42   | 88.08   | 105.74   | 141.06   | 176.38   |
| .126                 | 17.64               | 26.58   | 35.51   | 53.38   | 62.33   | 71.27   | 89.14   | 107.02   | 142.76   | 178.51   |
| .127                 | 17.85               | 26.89   | 35.93   | 54.02   | 63.07   | 72.13   | 90.20   | 108.30   | 144.47   | 180.64   |
| .128                 | 18.06               | 27.21   | 36.36   | 54.66   | 63.81   | 72.99   | 91.27   | 109.58   | 146.18   | 182.78   |
| .129                 | 18.27               | 27.53   | 36.79   | 55.30   | 64.55   | 73.85   | 92.34   | 110.86   | 147.89   | 184.91   |
| .130                 | 18.48               | 27.85   | 37.22   | 55.94   | 65.30   | 74.71   | 93.41   | 112.14   | 149.60   | 187.06   |
| .131                 | 18.69               | 28.17   | 37.65   | 56.59   | 66.06   | 75.57   | 94.49   | 113.44   | 151.34   | 189.23   |
| .132                 | 18.90               | 28.49   | 38.06   | 57.24   | 66.82   | 76.44   | 95.57   | 114.70   | 153.08   | 191.40   |
| .133                 | 19.11               | 28.81   | 38.49   | 57.89   | 67.58   | 77.31   | 96.66   | 116.04   | 154.82   | 193.58   |
| .134                 | 19.33               | 29.13   | 38.92   | 58.54   | 68.34   | 78.18   | 97.75   | 117.35   | 156.56   | 195.76   |
| .135                 | 19.55               | 29.46   | 39.37   | 59.19   | 69.11   | 79.05   | 98.84   | 118.66   | 158.30   | 197.94   |
| .136                 | 19.76               | 29.78   | 39.81   | 59.85   | 69.88   | 79.92   | 99.94   | 119.98   | 160.07   | 200.15   |
| .137                 | 19.97               | 30.11   | 40.25   | 60.51   | 70.65   | 80.79   | 101.04  | 121.31   | 161.84   | 202.37   |
| .138                 | 20.19               | 30.44   | 40.69   | 61.17   | 71.42   | 81.67   | 102.14  | 122.64   | 163.61   | 204.59   |
| .139                 | 20.41               | 30.77   | 41.13   | 61.84   | 72.19   | 82.55   | 103.25  | 123.97   | 165.38   | 206.81   |
| .140                 | 20.63               | 31.10   | 41.57   | 62.51   | 72.97   | 83.43   | 104.37  | 125.30   | 167.16   | 209.03   |
| .141                 | 20.85               | 31.43   | 42.01   | 63.18   | 73.75   | 84.33   | 105.49  | 126.65   | 168.96   | 211.28   |
| .142                 | 21.07               | 31.76   | 42.45   | 63.85   | 74.53   | 85.23   | 106.61  | 128.00   | 170.76   | 213.53   |
| .143                 | 21.29               | 32.09   | 42.90   | 64.52   | 75.32   | 86.13   | 107.74  | 129.35   | 172.57   | 215.79   |
| .144                 | 21.52               | 32.43   | 43.35   | 65.19   | 76.11   | 87.03   | 108.87  | 131.70   | 174.37   | 218.05   |
| .145                 | 21.74               | 32.77   | 43.80   | 65.87   | 76.90   | 87.93   | 110.00  | 132.06   | 176.19   | 220.31   |
| .146                 | 21.96               | 33.11   | 44.25   | 66.55   | 77.70   | 88.84   | 111.14  | 133.43   | 178.02   | 222.60   |
| .147                 | 22.18               | 33.45   | 44.71   | 67.23   | 78.50   | 89.75   | 112.28  | 134.80   | 179.85   | 224.90   |
| .148                 | 22.40               | 33.79   | 45.17   | 67.91   | 79.30   | 90.67   | 113.42  | 136.18   | 181.69   | 227.20   |
| .149                 | 22.63               | 34.13   | 45.63   | 68.60   | 80.10   | 91.59   | 114.57  | 137.56   | 183.53   | 229.50   |
| .150                 | 22.86               | 34.47   | 46.09   | 69.29   | 80.90   | 92.51   | 115.72  | 138.94   | 185.37   | 231.80   |
| .151                 | 23.08               | 34.81   | 46.55   | 69.98   | 81.71   | 93.43   | 116.88  | 140.33   | 187.23   | 234.13   |

| Depth on Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |         |          |          |          |          |
|----------------|---------------------|---------|---------|---------|---------|---------|---------|----------|----------|----------|----------|
|                | Feet.               | 2 Feet. | 3 Feet. | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| .152           | 23.31               | 35.15   | 47.01   | 70.67   | 82.52   | 94.36   | 118.04  | 141.73   | 189.09   | 236.46   |          |
| .153           | 23.54               | 35.50   | 47.47   | 71.37   | 83.33   | 95.29   | 119.21  | 143.17   | 190.96   | 238.79   |          |
| .154           | 23.77               | 35.85   | 47.93   | 72.07   | 84.14   | 96.22   | 120.38  | 144.57   | 192.83   | 241.13   |          |
| .155           | 24.00               | 36.20   | 48.39   | 72.77   | 84.96   | 97.15   | 121.55  | 145.93   | 194.70   | 243.47   |          |
| .156           | 24.23               | 36.55   | 48.85   | 73.47   | 85.78   | 98.00   | 122.73  | 147.35   | 196.59   | 245.86   |          |
| .157           | 24.46               | 36.90   | 49.32   | 74.18   | 86.61   | 99.04   | 123.91  | 148.77   | 199.48   | 248.25   |          |
| .158           | 24.69               | 37.25   | 49.79   | 74.89   | 87.44   | 99.99   | 125.09  | 150.19   | 201.38   | 250.64   |          |
| .159           | 24.93               | 37.60   | 50.26   | 75.60   | 88.27   | 100.94  | 126.27  | 151.61   | 203.28   | 253.04   |          |
| .160           | 25.17               | 37.96   | 50.73   | 76.31   | 89.10   | 101.89  | 127.46  | 153.03   | 204.18   | 255.34   |          |
| .161           | 25.40               | 38.31   | 51.20   | 77.02   | 89.93   | 102.85  | 128.66  | 154.47   | 206.10   | 257.75   |          |
| .162           | 25.63               | 38.66   | 51.68   | 77.74   | 90.77   | 103.81  | 129.86  | 155.91   | 208.03   | 260.17   |          |
| .163           | 25.86               | 39.01   | 52.16   | 78.46   | 91.61   | 104.77  | 131.06  | 157.35   | 209.96   | 262.59   |          |
| .164           | 26.10               | 39.37   | 52.64   | 79.18   | 92.45   | 105.73  | 132.26  | 158.80   | 211.89   | 265.01   |          |
| .165           | 26.34               | 39.73   | 53.12   | 79.90   | 93.29   | 106.69  | 133.47  | 160.25   | 213.82   | 267.38   |          |
| .166           | 26.57               | 40.09   | 53.60   | 80.63   | 94.14   | 107.66  | 134.69  | 161.71   | 215.76   | 269.82   |          |
| .167           | 26.81               | 40.45   | 54.08   | 81.36   | 94.99   | 108.63  | 135.91  | 163.17   | 217.70   | 272.26   |          |
| .168           | 27.05               | 40.81   | 54.56   | 82.09   | 95.84   | 109.60  | 137.13  | 164.64   | 219.65   | 274.71   |          |
| .169           | 27.29               | 41.17   | 55.05   | 82.82   | 96.69   | 110.58  | 138.35  | 166.11   | 221.60   | 277.16   |          |
| .170           | 27.53               | 41.53   | 55.54   | 83.55   | 97.55   | 111.56  | 139.57  | 167.58   | 223.65   | 279.61   |          |
| .171           | 27.77               | 41.88   | 56.03   | 84.28   | 98.41   | 112.54  | 140.85  | 169.06   | 225.62   | 282.09   |          |
| .172           | 28.01               | 42.23   | 56.53   | 85.02   | 99.27   | 113.53  | 142.09  | 170.54   | 227.59   | 284.57   |          |
| .173           | 28.25               | 42.59   | 57.02   | 85.76   | 100.14  | 114.52  | 143.33  | 172.03   | 229.56   | 287.05   |          |
| .174           | 28.49               | 42.95   | 57.51   | 86.50   | 101.01  | 115.51  | 144.57  | 173.52   | 231.54   | 289.54   |          |
| .175           | 28.74               | 43.31   | 57.99   | 87.24   | 101.88  | 116.50  | 145.76  | 175.01   | 233.52   | 292.03   |          |
| .176           | 28.98               | 43.68   | 58.48   | 87.99   | 102.75  | 117.50  | 147.01  | 176.49   | 235.54   | 294.54   |          |
| .177           | 29.22               | 44.05   | 58.98   | 88.74   | 103.62  | 118.50  | 148.26  | 177.98   | 237.56   | 297.06   |          |
| .178           | 29.47               | 44.43   | 59.48   | 89.49   | 104.50  | 119.50  | 149.51  | 179.47   | 239.58   | 299.58   |          |
| .179           | 29.72               | 44.81   | 59.98   | 90.24   | 105.38  | 120.50  | 150.77  | 180.96   | 241.60   | 302.10   |          |
| .180           | 29.97               | 45.19   | 60.48   | 91.00   | 106.26  | 121.51  | 152.03  | 182.55   | 243.62   | 304.62   |          |
| .181           | 30.21               | 45.57   | 60.98   | 91.76   | 107.14  | 122.52  | 153.31  | 184.07   | 245.65   | 307.17   |          |
| .182           | 30.45               | 45.95   | 61.48   | 92.52   | 108.03  | 123.53  | 154.59  | 185.60   | 247.68   | 309.72   |          |
| .183           | 30.70               | 46.33   | 61.98   | 93.28   | 108.92  | 124.54  | 155.88  | 187.13   | 249.71   | 312.27   |          |
| .184           | 30.95               | 46.71   | 62.49   | 94.04   | 109.81  | 125.55  | 157.17  | 188.66   | 251.74   | 314.82   |          |
| .185           | 31.20               | 47.10   | 63.00   | 94.80   | 110.70  | 126.57  | 158.43  | 190.19   | 253.78   | 317.38   |          |
| .186           | 31.45               | 47.48   | 63.51   | 95.57   | 111.60  | 127.60  | 159.71  | 191.74   | 255.85   | 319.96   |          |
| .187           | 31.70               | 47.86   | 64.02   | 96.34   | 112.50  | 128.63  | 160.99  | 193.29   | 257.92   | 322.55   |          |
| .188           | 31.95               | 48.24   | 64.53   | 97.11   | 113.40  | 129.67  | 162.27  | 194.84   | 259.99   | 325.14   |          |
| .189           | 32.21               | 48.62   | 65.04   | 97.88   | 114.30  | 130.71  | 163.55  | 196.39   | 262.06   | 327.73   |          |
| .190           | 32.47               | 49.01   | 65.56   | 98.65   | 115.20  | 131.75  | 164.84  | 197.94   | 264.13   | 330.32   |          |
| .191           | 32.72               | 49.39   | 66.07   | 99.43   | 116.11  | 132.79  | 166.14  | 199.51   | 266.22   | 332.93   |          |
| .192           | 32.97               | 49.77   | 66.58   | 100.21  | 117.02  | 133.83  | 167.45  | 201.08   | 268.31   | 335.55   |          |
| .193           | 33.22               | 50.16   | 67.10   | 100.99  | 117.93  | 134.87  | 168.76  | 202.65   | 270.40   | 338.17   |          |
| .194           | 33.47               | 50.55   | 67.62   | 101.77  | 118.84  | 135.92  | 170.07  | 204.22   | 272.50   | 340.79   |          |
| .195           | 33.73               | 50.94   | 68.14   | 102.56  | 119.76  | 136.97  | 171.38  | 205.79   | 274.60   | 343.41   |          |
| .196           | 33.98               | 51.33   | 68.66   | 103.35  | 120.68  | 138.02  | 172.70  | 207.37   | 276.72   | 346.06   |          |
| .197           | 34.24               | 51.72   | 69.18   | 104.14  | 121.60  | 139.07  | 174.02  | 208.96   | 278.84   | 348.72   |          |
| .198           | 34.50               | 52.11   | 69.70   | 104.93  | 122.52  | 140.13  | 175.34  | 210.55   | 280.96   | 351.38   |          |
| .199           | 34.76               | 52.50   | 70.23   | 105.72  | 123.45  | 141.19  | 176.66  | 212.14   | 283.08   | 354.04   |          |
| .200           | 35.02               | 52.89   | 70.76   | 106.51  | 124.38  | 142.25  | 177.99  | 213.73   | 285.22   | 356.70   |          |
| .201           | 35.28               | 53.28   | 71.29   | 107.31  | 125.31  | 143.32  | 179.33  | 215.34   | 287.36   | 359.38   |          |
| .202           | 35.54               | 53.67   | 71.82   | 107.81  | 126.24  | 144.39  | 180.67  | 216.95   | 289.51   | 362.07   |          |
| .203           | 35.80               | 54.07   | 72.35   | 108.61  | 127.17  | 145.46  | 182.01  | 218.56   | 291.66   | 364.76   |          |
| .204           | 36.06               | 54.47   | 72.88   | 109.41  | 128.11  | 146.53  | 183.35  | 220.17   | 293.81   | 367.45   |          |
| .205           | 36.33               | 54.87   | 73.42   | 110.51  | 129.05  | 147.60  | 184.69  | 221.78   | 295.96   | 370.14   |          |
| .206           | 36.59               | 55.27   | 73.95   | 111.32  | 130.00  | 148.68  | 186.04  | 223.40   | 298.13   | 372.86   |          |
| .207           | 36.85               | 55.67   | 74.48   | 112.13  | 130.95  | 149.76  | 187.39  | 225.03   | 300.30   | 375.58   |          |
| .208           | 37.11               | 56.07   | 75.02   | 112.94  | 131.90  | 150.84  | 188.75  | 226.66   | 302.47   | 378.30   |          |
| .209           | 37.37               | 56.47   | 75.56   | 113.75  | 132.85  | 151.92  | 190.11  | 228.29   | 304.65   | 381.02   |          |

| Depth on Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |         |          |          |          |          |
|----------------|---------------------|---------|---------|---------|---------|---------|---------|----------|----------|----------|----------|
|                | Feet.               | 2 Feet. | 3 Feet. | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| .210           | 37.64               | 56.88   | 76.10   | 114.56  | 133.81  | 153.01  | 191.47  | 229.92   | 306.83   | 383.75   |          |
| .211           | 37.90               | 57.28   | 76.64   | 115.37  | 134.76  | 154.10  | 192.84  | 231.56   | 309.03   | 386.30   |          |
| .212           | 38.17               | 57.68   | 77.18   | 116.19  | 135.72  | 155.19  | 194.21  | 233.21   | 311.23   | 389.05   |          |
| .213           | 38.44               | 58.08   | 77.72   | 117.01  | 136.68  | 156.29  | 195.58  | 234.86   | 313.43   | 391.80   |          |
| .214           | 38.71               | 58.48   | 78.26   | 117.83  | 137.64  | 157.39  | 196.95  | 236.51   | 315.63   | 394.55   |          |
| .215           | 38.98               | 58.89   | 78.81   | 118.65  | 138.60  | 158.49  | 198.33  | 238.16   | 317.84   | 397.51   |          |
| .216           | 39.24               | 59.30   | 79.36   | 119.48  | 139.56  | 159.59  | 199.71  | 239.82   | 320.06   | 400.29   |          |
| .217           | 39.51               | 59.71   | 79.91   | 120.31  | 140.52  | 160.69  | 201.09  | 241.49   | 322.28   | 403.07   |          |
| .218           | 39.78               | 60.12   | 80.46   | 121.14  | 141.48  | 161.70  | 202.48  | 243.16   | 324.57   | 405.86   |          |
| .219           | 40.05               | 60.53   | 81.01   | 121.97  | 142.45  | 162.81  | 203.87  | 244.83   | 326.80   | 408.65   |          |
| .220           | 40.32               | 60.94   | 81.56   | 122.80  | 143.41  | 164.03  | 205.26  | 246.50   | 328.97   | 411.44   |          |
| .221           | 40.59               | 61.35   | 82.11   | 123.63  | 144.38  | 165.15  | 206.66  | 248.18   | 331.22   | 414.23   |          |
| .222           | 40.86               | 61.76   | 82.66   | 124.47  | 145.36  | 166.27  | 208.07  | 249.86   | 333.47   | 417.02   |          |
| .223           | 41.13               | 62.17   | 83.21   | 125.31  | 146.34  | 167.39  | 209.48  | 251.55   | 335.72   | 419.82   |          |
| .224           | 41.40               | 62.59   | 83.77   | 126.15  | 147.32  | 168.50  | 210.89  | 253.24   | 337.97   | 422.62   |          |
| .225           | 41.68               | 63.01   | 84.33   | 126.99  | 148.30  | 169.63  | 212.30  | 254.93   | 340.22   | 425.52   |          |
| .226           | 41.95               | 63.41   | 84.89   | 127.83  | 149.29  | 170.76  | 213.71  | 256.63   | 342.49   | 428.36   |          |
| .227           | 42.22               | 63.82   | 85.45   | 128.67  | 150.28  | 171.89  | 215.12  | 258.33   | 344.76   | 431.21   |          |
| .228           | 42.50               | 64.23   | 86.01   | 129.52  | 151.27  | 173.02  | 216.53  | 260.03   | 347.04   | 434.06   |          |
| .229           | 42.78               | 64.65   | 86.57   | 130.37  | 152.26  | 174.16  | 217.95  | 261.73   | 349.32   | 436.91   |          |
| .230           | 43.06               | 65.08   | 87.14   | 131.22  | 153.26  | 175.30  | 219.37  | 263.45   | 351.60   | 439.76   |          |
| .231           | 43.33               | 65.50   | 87.70   | 132.07  | 154.26  | 176.44  | 220.80  | 265.17   | 353.90   | 442.65   |          |
| .232           | 43.61               | 65.92   | 88.27   | 132.92  | 155.26  | 177.58  | 222.23  | 266.89   | 356.20   | 445.53   |          |
| .233           | 43.89               | 66.35   | 88.84   | 133.78  | 156.26  | 178.72  | 223.67  | 268.61   | 358.50   | 448.41   |          |
| .234           | 44.17               | 66.78   | 89.41   | 134.64  | 157.26  | 179.87  | 225.11  | 270.33   | 360.80   | 451.29   |          |
| .235           | 44.45               | 67.21   | 89.98   | 135.50  | 158.26  | 181.02  | 226.55  | 272.06   | 363.11   | 454.15   |          |
| .236           | 44.73               | 67.63   | 90.53   | 136.38  | 159.27  | 182.17  | 227.99  | 273.80   | 365.43   | 457.06   |          |
| .237           | 45.01               | 68.05   | 91.12   | 137.22  | 160.28  | 183.36  | 229.44  | 275.54   | 367.73   | 459.97   |          |
| .238           | 45.29               | 68.48   | 91.69   | 138.08  | 161.29  | 184.48  | 230.89  | 277.28   | 370.08   | 462.88   |          |
| .239           | 45.57               | 68.91   | 92.26   | 138.95  | 162.30  | 185.64  | 232.34  | 279.02   | 372.43   | 465.79   |          |
| .240           | 45.85               | 69.34   | 92.84   | 139.82  | 163.31  | 186.80  | 233.79  | 280.77   | 374.74   | 468.70   |          |
| .241           | 46.13               | 69.77   | 93.41   | 140.71  | 164.33  | 187.96  | 235.24  | 282.52   | 377.09   | 471.65   |          |
| .242           | 46.41               | 70.20   | 93.99   | 141.58  | 165.35  | 189.13  | 236.69  | 284.28   | 379.44   | 474.60   |          |
| .243           | 46.69               | 70.63   | 94.58   | 143.31  | 166.37  | 190.30  | 237.14  | 286.04   | 381.79   | 477.55   |          |
| .244           | 46.98               | 71.06   | 95.17   | 144.18  | 167.39  | 191.47  | 238.59  | 287.80   | 384.14   | 480.51   |          |
| .245           | 47.27               | 71.49   | 95.73   | 144.19  | 168.42  | 192.64  | 241.05  | 289.56   | 386.49   | 483.40   |          |
| .246           | 47.55               | 71.92   | 96.33   | 145.07  | 169.45  | 193.82  | 242.54  | 291.33   | 388.86   | 486.37   |          |
| .247           | 47.83               | 72.35   | 96.91   | 145.95  | 170.48  | 195.00  | 244.03  | 293.11   | 391.23   | 489.34   |          |
| .248           | 48.12               | 72.79   | 97.49   | 146.83  | 171.51  | 196.18  | 245.52  | 294.89   | 393.60   | 492.31   |          |
| .249           | 48.41               | 73.24   | 98.07   | 147.71  | 172.54  | 197.36  | 247.01  | 296.67   | 395.97   | 495.28   |          |
| .250           | 48.70               | 73.67   | 98.65   | 148.60  | 173.58  | 198.55  | 248.50  | 298.45   | 398.35   | 498.25   |          |
| .251           | 48.98               | 74.11   | 99.24   | 149.49  | 174.62  | 199.74  | 249.99  | 300.24   | 401.74   | 501.25   |          |
| .252           | 49.27               | 74.55   | 99.83   | 150.38  | 175.66  | 200.93  | 251.48  | 302.03   | 404.14   | 504.25   |          |
| .253           | 49.51               | 74.99   | 100.42  | 151.27  | 176.70  | 202.12  | 252.97  | 303.82   | 406.53   | 507.25   |          |
| .254           | 49.85               | 75.43   | 101.01  | 152.16  | 177.74  | 203.31  | 254.46  | 305.62   | 408.92   | 510.25   |          |
| .255           | 50.14               | 75.87   | 101.60  | 153.06  | 178.78  | 204.51  | 255.95  | 307.42   | 410.33   | 513.25   |          |
| .256           | 50.43               | 76.31   | 102.19  | 153.95  | 179.83  | 205.71  | 257.46  | 309.23   | 412.75   | 516.27   |          |
| .257           | 50.72               | 76.75   | 102.78  | 154.85  | 180.88  | 206.91  | 258.97  | 311.04   | 415.17   | 519.30   |          |
| .258           | 51.01               | 77.19   | 103.38  | 155.75  | 181.93  | 208.11  | 260.48  | 311.85   | 417.59   | 522.33   |          |
| .259           | 51.30               | 77.63   | 103.98  | 156.65  | 182.98  | 209.32  | 262.02  | 313.66   | 420.01   | 525.36   |          |
| .260           | 51.60               | 78.08   | 104.58  | 157.55  | 184.04  | 210.53  | 263.51  | 316.48   | 422.44   | 528.39   |          |
| .261           | 51.89               | 78.52   | 105.18  | 158.45  | 185.10  | 211.74  | 265.03  | 318.31   | 424.88   | 531.44   |          |
| .262           | 52.18               | 78.97   | 105.78  | 159.36  | 186.16  | 212.95  | 266.55  | 320.14   | 427.32   | 534.50   |          |
| .263           | 52.47               | 79.42   | 106.38  | 160.27  | 187.22  | 214.16  | 268.07  | 321.97   | 429.76   | 537.56   |          |
| .264           | 52.76               | 79.87   | 107.18  | 161.18  | 188.28  | 215.38  | 269.59  | 323.80   | 432.20   | 540.62   |          |
| .265           | 53.06               | 80.32   | 107.58  | 162.09  | 189.35  | 216.60  | 271.11  | 325.63   | 434.65   | 543.68   |          |
| .266           | 53.35               | 80.77   | 108.18  | 163.00  | 190.42  | 217.82  | 272.68  | 327.47   | 437.11   | 546.76   |          |
| .267           | 53.64               | 81.22   | 108.78  | 163.92  | 191.49  | 219.04  | 274.22  | 329.31   | 439.58   | 549.84   |          |

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |         |          |          |          |
|----------------------|---------------------|---------|---------|---------|---------|---------|---------|----------|----------|----------|
|                      | Feet.               | 2 Feet. | 3 Feet. | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. |
| .268                 | 53.94               | 81.67   | 109.39  | 164.84  | 192.56  | 220.27  | 275.76  | 331.16   | 442.05   | 552.93   |
| .269                 | 54.24               | 82.12   | 110.00  | 165.76  | 193.63  | 221.50  | 277.30  | 333.01   | 444.52   | 556.02   |
| .270                 | 54.54               | 82.57   | 110.61  | 166.68  | 194.70  | 222.73  | 278.80  | 334.86   | 446.99   | 559.11   |
| .271                 | 54.84               | 83.02   | 111.22  | 167.60  | 195.78  | 223.96  | 280.34  | 336.72   | 449.47   | 562.22   |
| .272                 | 55.14               | 83.47   | 111.83  | 168.52  | 196.86  | 225.20  | 281.89  | 338.58   | 451.95   | 565.33   |
| .273                 | 55.44               | 83.93   | 112.44  | 169.44  | 197.94  | 226.44  | 283.44  | 340.44   | 454.43   | 568.44   |
| .274                 | 55.74               | 84.39   | 113.05  | 170.37  | 199.02  | 227.68  | 284.99  | 342.31   | 456.91   | 571.56   |
| .275                 | 56.04               | 84.85   | 113.67  | 171.30  | 200.11  | 228.92  | 286.54  | 344.18   | 459.43   | 574.68   |
| .276                 | 56.34               | 85.31   | 114.28  | 172.23  | 201.20  | 230.26  | 288.10  | 346.06   | 461.94   | 577.84   |
| .277                 | 56.64               | 85.77   | 114.89  | 173.16  | 202.29  | 231.51  | 289.66  | 347.94   | 464.45   | 581.00   |
| .278                 | 56.94               | 86.23   | 115.51  | 174.09  | 203.38  | 232.76  | 291.22  | 349.82   | 466.97   | 584.16   |
| .279                 | 57.24               | 86.69   | 116.13  | 175.02  | 204.47  | 234.01  | 292.79  | 351.71   | 469.49   | 587.33   |
| .280                 | 57.54               | 87.15   | 116.75  | 175.96  | 205.56  | 235.16  | 294.36  | 353.60   | 472.01   | 590.40   |
| .281                 | 57.84               | 87.61   | 117.37  | 176.90  | 206.66  | 236.42  | 295.94  | 355.49   | 474.54   | 593.57   |
| .282                 | 58.14               | 88.07   | 117.99  | 177.84  | 207.76  | 237.68  | 297.52  | 357.38   | 477.07   | 596.74   |
| .283                 | 58.44               | 88.53   | 118.61  | 178.78  | 208.86  | 238.94  | 299.10  | 359.27   | 479.60   | 599.91   |
| .284                 | 58.75               | 88.99   | 119.23  | 179.72  | 209.96  | 240.20  | 300.68  | 361.16   | 481.93   | 603.08   |
| .285                 | 59.06               | 89.46   | 119.86  | 180.66  | 211.06  | 241.46  | 302.26  | 363.06   | 484.66   | 606.25   |
| .286                 | 59.36               | 89.92   | 120.48  | 181.61  | 212.17  | 242.73  | 303.85  | 364.96   | 487.21   | 609.45   |
| .287                 | 59.66               | 90.38   | 121.11  | 182.56  | 213.28  | 244.00  | 305.44  | 366.87   | 489.76   | 612.65   |
| .288                 | 59.97               | 90.85   | 121.74  | 183.51  | 214.39  | 245.27  | 307.03  | 368.78   | 492.31   | 615.85   |
| .289                 | 60.28               | 91.32   | 122.37  | 184.46  | 215.50  | 246.54  | 308.62  | 370.69   | 494.87   | 619.05   |
| .290                 | 60.59               | 91.79   | 123.00  | 185.41  | 216.61  | 247.81  | 310.22  | 372.60   | 497.43   | 622.25   |
| .291                 | 60.89               | 92.26   | 123.63  | 186.36  | 217.72  | 249.09  | 311.82  | 374.51   | 500.00   | 625.47   |
| .292                 | 61.20               | 92.73   | 124.26  | 187.31  | 218.81  | 250.37  | 313.42  | 376.42   | 502.58   | 628.69   |
| .293                 | 61.51               | 93.20   | 124.89  | 188.27  | 219.96  | 251.65  | 315.02  | 378.34   | 505.16   | 631.91   |
| .294                 | 61.82               | 93.67   | 125.52  | 189.23  | 221.08  | 252.93  | 316.63  | 380.26   | 507.74   | 635.14   |
| .295                 | 62.13               | 94.15   | 126.16  | 190.19  | 222.20  | 254.22  | 318.24  | 382.18   | 510.32   | 638.37   |
| .296                 | 62.44               | 94.62   | 126.79  | 191.15  | 223.32  | 255.51  | 319.86  | 384.14   | 512.92   | 641.62   |
| .297                 | 62.75               | 95.09   | 127.43  | 192.11  | 224.45  | 256.80  | 321.48  | 386.10   | 515.52   | 644.87   |
| .298                 | 63.06               | 95.56   | 128.07  | 193.07  | 225.58  | 258.09  | 323.10  | 388.06   | 518.53   | 648.12   |
| .299                 | 63.47               | 96.04   | 128.71  | 194.04  | 226.71  | 259.38  | 324.72  | 390.02   | 520.72   | 651.38   |
| .300                 | 63.69               | 96.52   | 129.35  | 195.01  | 227.84  | 260.67  | 326.34  | 392.00   | 523.32   | 654.64   |
| .301                 | 64.00               | 96.99   | 129.99  | 195.98  | 228.97  | 261.97  | 327.97  | 393.95   | 525.94   | 657.92   |
| .302                 | 64.31               | 97.47   | 130.63  | 196.95  | 230.11  | 263.27  | 329.60  | 395.90   | 528.58   | 661.20   |
| .303                 | 64.62               | 97.95   | 131.26  | 197.92  | 231.25  | 264.57  | 331.23  | 397.86   | 531.18   | 664.48   |
| .304                 | 64.93               | 98.43   | 131.91  | 198.99  | 232.39  | 265.87  | 332.86  | 399.82   | 533.80   | 667.76   |
| .305                 | 65.25               | 98.91   | 132.57  | 199.87  | 233.53  | 267.18  | 334.49  | 401.78   | 536.42   | 671.04   |
| .306                 | 65.56               | 99.39   | 133.21  | 200.85  | 234.67  | 268.49  | 336.13  | 403.76   | 539.06   | 674.34   |
| .307                 | 65.87               | 99.87   | 133.86  | 201.83  | 235.81  | 269.80  | 337.77  | 405.74   | 541.70   | 677.64   |
| .308                 | 66.19               | 100.35  | 134.51  | 202.81  | 236.96  | 271.11  | 339.42  | 407.72   | 544.34   | 680.94   |
| .309                 | 66.51               | 100.83  | 135.16  | 203.79  | 238.11  | 272.42  | 341.07  | 409.70   | 546.98   | 684.24   |
| .310                 | 66.83               | 101.31  | 135.81  | 204.77  | 239.26  | 273.74  | 342.72  | 411.69   | 549.63   | 687.57   |
| .311                 | 67.14               | 101.79  | 136.46  | 205.75  | 240.41  | 275.06  | 344.37  | 413.68   | 552.29   | 690.86   |
| .312                 | 67.46               | 102.27  | 137.11  | 206.74  | 241.56  | 276.38  | 346.03  | 415.67   | 554.95   | 694.19   |
| .313                 | 67.78               | 102.76  | 137.76  | 207.73  | 242.72  | 277.71  | 347.69  | 417.66   | 557.61   | 697.52   |
| .314                 | 68.10               | 103.25  | 138.41  | 208.72  | 243.88  | 279.04  | 349.35  | 419.65   | 560.27   | 700.75   |
| .315                 | 68.42               | 103.74  | 139.07  | 209.71  | 245.04  | 280.36  | 351.01  | 421.65   | 562.94   | 704.18   |
| .316                 | 68.74               | 104.23  | 139.72  | 210.70  | 246.20  | 281.69  | 352.68  | 423.65   | 565.62   | 707.55   |
| .317                 | 69.06               | 104.72  | 140.38  | 211.69  | 247.36  | 283.02  | 354.35  | 425.65   | 568.30   | 710.92   |
| .318                 | 69.38               | 105.21  | 141.04  | 212.69  | 248.52  | 284.35  | 356.02  | 427.66   | 570.98   | 714.29   |
| .319                 | 69.70               | 105.70  | 141.70  | 213.69  | 249.68  | 285.69  | 357.69  | 429.67   | 573.66   | 717.66   |
| .320                 | 70.02               | 106.19  | 142.36  | 214.69  | 250.85  | 287.03  | 359.36  | 431.69   | 576.36   | 721.04   |
| .321                 | 70.34               | 106.68  | 143.02  | 215.69  | 252.02  | 288.37  | 361.04  | 433.71   | 579.06   | 724.42   |
| .322                 | 70.66               | 107.17  | 143.68  | 216.69  | 253.19  | 289.71  | 362.72  | 435.73   | 581.76   | 727.80   |
| .323                 | 70.98               | 107.66  | 144.34  | 217.69  | 254.36  | 291.05  | 364.40  | 437.75   | 584.47   | 731.19   |
| .324                 | 71.30               | 107.85  | 145.00  | 218.70  | 255.54  | 292.39  | 366.09  | 439.78   | 587.18   | 734.58   |
| .325                 | 71.63               | 108.65  | 145.67  | 219.71  | 256.72  | 293.74  | 367.78  | 441.82   | 589.89   | 737.97   |



| Depth on Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |         |          |          |          |          |
|----------------|---------------------|---------|---------|---------|---------|---------|---------|----------|----------|----------|----------|
|                | Feet.               | 2 Feet. | 3 Feet. | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| .326           | 71.95               | 109.14  | 146.33  | 220.72  | 257.90  | 295.09  | 369.47  | 443.86   | 592.61   | 741.37   |          |
| .327           | 72.27               | 109.63  | 147.00  | 221.73  | 259.08  | 296.44  | 371.11  | 445.90   | 595.33   | 744.77   |          |
| .328           | 72.59               | 110.13  | 147.67  | 222.74  | 260.26  | 297.79  | 372.87  | 447.04   | 598.06   | 748.18   |          |
| .329           | 72.92               | 110.63  | 148.34  | 223.75  | 261.44  | 299.15  | 374.57  | 449.98   | 600.79   | 751.59   |          |
| .330           | 73.25               | 111.13  | 149.01  | 224.76  | 262.63  | 300.51  | 376.27  | 452.02   | 603.52   | 755.09   |          |
| .331           | 73.57               | 111.63  | 149.68  | 225.77  | 263.82  | 301.87  | 377.97  | 454.07   | 606.26   | 758.44   |          |
| .332           | 73.89               | 112.13  | 150.35  | 226.78  | 265.01  | 303.23  | 378.68  | 456.12   | 609.00   | 761.88   |          |
| .333           | 74.22               | 112.63  | 151.02  | 227.80  | 266.20  | 304.60  | 380.39  | 458.18   | 611.75   | 765.32   |          |
| .334           | 74.55               | 113.13  | 151.69  | 228.82  | 267.39  | 305.97  | 382.10  | 460.28   | 614.50   | 768.76   |          |
| .335           | 74.88               | 113.63  | 152.37  | 229.84  | 268.59  | 307.34  | 384.81  | 462.30   | 617.25   | 772.21   |          |
| .336           | 75.20               | 114.13  | 153.04  | 230.86  | 269.78  | 308.71  | 386.53  | 464.36   | 620.01   | 775.66   |          |
| .337           | 75.53               | 114.63  | 153.71  | 231.88  | 270.98  | 310.08  | 388.25  | 466.42   | 622.77   | 779.12   |          |
| .338           | 75.86               | 115.13  | 154.39  | 232.91  | 272.08  | 311.45  | 389.97  | 468.49   | 625.52   | 782.58   |          |
| .339           | 76.19               | 115.63  | 155.07  | 233.94  | 273.28  | 312.82  | 391.69  | 470.56   | 628.31   | 786.04   |          |
| .340           | 76.52               | 116.14  | 155.75  | 234.97  | 274.58  | 314.19  | 393.42  | 472.63   | 631.08   | 789.50   |          |
| .341           | 76.85               | 116.64  | 156.43  | 236.00  | 275.78  | 315.57  | 395.15  | 474.71   | 633.86   | 792.99   |          |
| .342           | 77.18               | 117.14  | 157.11  | 237.03  | 276.99  | 316.95  | 396.88  | 476.79   | 636.64   | 796.48   |          |
| .343           | 77.51               | 117.65  | 157.79  | 238.06  | 278.20  | 318.33  | 398.61  | 478.88   | 639.42   | 799.97   |          |
| .344           | 77.84               | 118.16  | 158.47  | 239.09  | 279.41  | 319.72  | 400.34  | 480.97   | 642.20   | 803.46   |          |
| .345           | 78.18               | 118.67  | 159.16  | 240.13  | 280.62  | 321.11  | 402.08  | 483.06   | 644.99   | 806.96   |          |
| .346           | 78.51               | 119.18  | 159.84  | 241.17  | 281.83  | 322.50  | 403.82  | 485.15   | 647.79   | 810.46   |          |
| .347           | 78.84               | 119.69  | 160.52  | 242.21  | 283.04  | 323.89  | 405.56  | 487.25   | 650.59   | 813.96   |          |
| .348           | 79.17               | 120.20  | 161.20  | 243.25  | 284.26  | 325.28  | 407.31  | 489.35   | 653.39   | 817.47   |          |
| .349           | 79.50               | 120.71  | 161.90  | 244.29  | 285.48  | 326.68  | 409.06  | 491.45   | 656.19   | 820.98   |          |
| .350           | 79.84               | 121.22  | 162.59  | 245.33  | 286.70  | 328.08  | 410.81  | 493.55   | 659.00   | 824.49   |          |
| .351           | 80.17               | 121.73  | 163.28  | 246.37  | 287.92  | 329.48  | 412.57  | 495.66   | 661.83   | 828.03   |          |
| .352           | 80.50               | 122.24  | 163.97  | 247.41  | 289.14  | 330.88  | 414.33  | 497.77   | 664.66   | 831.57   |          |
| .353           | 80.83               | 122.76  | 164.66  | 248.46  | 290.36  | 332.28  | 416.09  | 499.89   | 667.49   | 835.11   |          |
| .354           | 81.17               | 123.28  | 165.35  | 249.51  | 291.59  | 334.28  | 417.85  | 501.01   | 670.33   | 838.66   |          |
| .355           | 81.51               | 123.79  | 166.04  | 250.56  | 292.82  | 335.08  | 419.61  | 504.13   | 673.17   | 842.21   |          |
| .356           | 81.84               | 124.30  | 166.73  | 251.61  | 294.05  | 336.49  | 421.38  | 506.25   | 676.01   | 845.77   |          |
| .357           | 82.18               | 124.81  | 167.42  | 252.66  | 295.28  | 337.90  | 423.15  | 508.38   | 678.83   | 849.33   |          |
| .358           | 82.52               | 125.32  | 168.12  | 253.71  | 296.51  | 339.31  | 424.92  | 510.50   | 681.71   | 852.89   |          |
| .359           | 82.86               | 125.84  | 168.82  | 254.77  | 297.75  | 340.73  | 426.69  | 512.63   | 684.56   | 856.46   |          |
| .360           | 83.20               | 126.36  | 169.52  | 255.83  | 298.99  | 342.15  | 428.46  | 514.77   | 687.41   | 860.03   |          |
| .361           | 83.54               | 126.88  | 170.22  | 256.89  | 300.23  | 343.57  | 430.24  | 516.91   | 690.27   | 863.61   |          |
| .362           | 83.88               | 127.40  | 170.92  | 257.95  | 301.47  | 344.99  | 432.02  | 519.05   | 693.13   | 867.19   |          |
| .363           | 84.22               | 127.92  | 171.62  | 259.01  | 302.71  | 346.11  | 433.80  | 521.19   | 695.99   | 870.78   |          |
| .364           | 84.56               | 128.44  | 172.32  | 260.07  | 303.95  | 347.83  | 435.58  | 523.34   | 698.85   | 874.37   |          |
| .365           | 84.90               | 128.96  | 173.02  | 261.14  | 305.20  | 349.25  | 437.38  | 525.49   | 701.72   | 877.96   |          |
| .366           | 85.24               | 129.48  | 173.72  | 262.20  | 306.45  | 350.68  | 439.17  | 527.64   | 704.60   | 881.57   |          |
| .367           | 85.58               | 130.00  | 174.42  | 263.27  | 307.70  | 352.11  | 440.96  | 529.80   | 707.48   | 885.18   |          |
| .368           | 85.92               | 130.52  | 175.13  | 264.34  | 308.95  | 353.54  | 442.75  | 531.96   | 710.37   | 888.80   |          |
| .369           | 86.26               | 131.05  | 175.84  | 265.41  | 310.20  | 354.97  | 444.55  | 534.12   | 713.26   | 892.42   |          |
| .370           | 86.60               | 131.58  | 176.54  | 266.48  | 311.45  | 356.41  | 446.35  | 536.28   | 716.15   | 896.04   |          |
| .371           | 86.94               | 132.10  | 177.25  | 267.55  | 312.71  | 357.85  | 448.15  | 538.45   | 719.05   | 899.67   |          |
| .372           | 87.28               | 132.62  | 177.96  | 268.62  | 313.97  | 359.29  | 449.95  | 540.62   | 721.95   | 903.30   |          |
| .373           | 87.62               | 133.14  | 178.67  | 269.69  | 315.23  | 360.73  | 451.76  | 542.80   | 724.86   | 906.93   |          |
| .374           | 87.97               | 133.67  | 179.38  | 270.77  | 316.49  | 362.17  | 453.57  | 544.98   | 727.77   | 910.56   |          |
| .375           | 88.32               | 134.20  | 180.09  | 271.85  | 317.76  | 363.62  | 455.38  | 547.16   | 730.68   | 914.20   |          |
| .376           | 88.66               | 134.73  | 180.80  | 272.93  | 319.02  | 365.06  | 457.19  | 549.34   | 733.60   | 917.86   |          |
| .377           | 89.00               | 135.26  | 181.51  | 274.01  | 320.28  | 366.51  | 459.01  | 551.52   | 736.52   | 921.52   |          |
| .378           | 89.34               | 135.79  | 182.22  | 275.09  | 321.54  | 367.96  | 460.83  | 553.70   | 739.44   | 925.18   |          |
| .379           | 89.69               | 136.32  | 182.93  | 276.17  | 322.80  | 369.41  | 462.65  | 555.89   | 742.36   | 928.84   |          |
| .380           | 90.04               | 136.85  | 183.65  | 277.26  | 324.06  | 370.86  | 464.47  | 558.08   | 745.29   | 932.50   |          |
| .381           | 90.39               | 137.38  | 184.36  | 278.34  | 325.33  | 372.32  | 466.27  | 560.28   | 748.23   | 936.18   |          |
| .382           | 90.74               | 137.91  | 185.08  | 279.43  | 326.60  | 373.78  | 468.10  | 562.48   | 751.17   | 939.86   |          |
| .383           | 91.09               | 138.44  | 185.80  | 280.52  | 327.87  | 375.24  | 469.93  | 564.68   | 754.11   | 943.54   |          |



| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |         |          |          |          |
|----------------------|---------------------|---------|---------|---------|---------|---------|---------|----------|----------|----------|
|                      | Feet.               | 2 Feet. | 3 Feet. | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. |
| .384                 | 91.45               | 138.97  | 186.52  | 281.61  | 329.15  | 376.70  | 471.76  | 568.88   | 757.05   | 947.23   |
| .385                 | 91.81               | 139.51  | 187.24  | 282.70  | 330.43  | 378.16  | 473.61  | 569.08   | 760.00   | 950.92   |
| .386                 | 92.15               | 140.04  | 187.96  | 283.79  | 331.71  | 379.62  | 475.45  | 571.29   | 762.96   | 954.62   |
| .387                 | 92.49               | 140.57  | 188.68  | 284.88  | 332.99  | 381.09  | 477.30  | 573.51   | 765.92   | 958.32   |
| .388                 | 92.83               | 141.11  | 189.40  | 285.98  | 334.27  | 382.56  | 479.15  | 575.73   | 768.88   | 962.02   |
| .389                 | 93.18               | 141.65  | 190.12  | 287.08  | 335.55  | 384.03  | 481.00  | 577.95   | 771.84   | 965.71   |
| .390                 | 93.53               | 142.19  | 190.83  | 288.18  | 336.84  | 385.50  | 482.85  | 580.17   | 774.81   | 969.44   |
| .391                 | 93.88               | 142.73  | 191.57  | 289.28  | 338.12  | 386.97  | 484.70  | 582.39   | 777.78   | 973.17   |
| .392                 | 94.23               | 143.27  | 192.39  | 290.38  | 339.41  | 388.45  | 486.55  | 584.61   | 780.76   | 976.90   |
| .393                 | 94.58               | 143.81  | 193.12  | 291.48  | 340.70  | 389.93  | 488.40  | 586.84   | 783.74   | 980.63   |
| .394                 | 94.93               | 144.35  | 193.85  | 292.58  | 341.99  | 391.41  | 490.25  | 589.07   | 786.72   | 984.37   |
| .395                 | 95.28               | 144.89  | 194.48  | 293.69  | 343.28  | 392.89  | 492.10  | 591.30   | 789.70   | 988.11   |
| .396                 | 95.63               | 145.43  | 195.21  | 294.79  | 344.58  | 394.37  | 493.96  | 593.54   | 792.69   | 991.92   |
| .397                 | 95.98               | 145.97  | 195.94  | 295.90  | 345.88  | 395.86  | 495.82  | 595.78   | 795.69   | 995.67   |
| .398                 | 96.33               | 146.51  | 196.67  | 297.01  | 347.18  | 397.35  | 497.68  | 598.02   | 798.69   | 999.42   |
| .399                 | 96.68               | 147.06  | 197.40  | 298.12  | 348.48  | 398.84  | 499.54  | 600.26   | 801.69   | 1003.17  |
| .400                 | 97.04               | 147.61  | 198.14  | 299.23  | 349.78  | 400.33  | 501.41  | 602.51   | 804.69   | 1006.87  |
| .401                 | 97.39               | 148.15  | 198.83  | 300.34  | 351.08  | 401.82  | 503.28  | 604.76   | 807.70   | 1010.64  |
| .402                 | 97.74               | 148.69  | 199.56  | 301.45  | 352.39  | 403.31  | 505.15  | 607.02   | 810.71   | 1014.42  |
| .403                 | 98.10               | 149.23  | 200.29  | 302.57  | 353.70  | 404.80  | 507.02  | 609.28   | 813.72   | 1018.20  |
| .404                 | 98.54               | 149.77  | 201.03  | 303.69  | 355.01  | 406.30  | 508.91  | 611.54   | 816.74   | 1021.98  |
| .405                 | 98.82               | 150.32  | 201.81  | 304.81  | 356.32  | 407.80  | 510.79  | 613.80   | 819.77   | 1025.76  |
| .406                 | 99.17               | 150.86  | 202.55  | 305.93  | 357.63  | 409.30  | 512.67  | 616.14   | 822.80   | 1029.56  |
| .407                 | 99.52               | 151.40  | 203.29  | 307.05  | 358.94  | 410.80  | 514.56  | 618.40   | 825.83   | 1033.36  |
| .408                 | 99.88               | 151.95  | 204.03  | 308.17  | 360.25  | 412.30  | 516.45  | 620.66   | 828.86   | 1047.16  |
| .409                 | 100.24              | 152.50  | 204.77  | 309.29  | 361.56  | 413.81  | 518.34  | 622.92   | 831.90   | 1050.96  |
| .410                 | 100.60              | 153.05  | 205.51  | 310.42  | 362.87  | 415.32  | 520.23  | 625.13   | 834.94   | 1044.76  |
| .411                 | 100.96              | 153.60  | 206.25  | 311.54  | 364.18  | 416.83  | 522.12  | 627.41   | 837.99   | 1048.58  |
| .412                 | 101.32              | 154.15  | 206.99  | 312.67  | 365.49  | 418.34  | 524.02  | 629.69   | 841.04   | 1052.40  |
| .413                 | 101.68              | 154.70  | 207.73  | 313.80  | 366.80  | 419.85  | 525.92  | 631.97   | 844.09   | 1056.22  |
| .414                 | 102.04              | 155.25  | 208.48  | 314.93  | 368.11  | 421.37  | 527.82  | 634.26   | 847.15   | 1060.05  |
| .415                 | 102.40              | 155.81  | 209.23  | 316.06  | 369.42  | 422.89  | 529.72  | 636.55   | 850.21   | 1063.88  |
| .416                 | 102.76              | 156.36  | 209.97  | 317.19  | 370.76  | 424.41  | 531.63  | 638.84   | 853.28   | 1067.72  |
| .417                 | 103.12              | 156.91  | 210.72  | 318.32  | 372.10  | 425.93  | 533.54  | 641.14   | 856.35   | 1071.56  |
| .418                 | 103.48              | 157.47  | 211.47  | 319.45  | 373.44  | 427.45  | 535.45  | 643.44   | 859.42   | 1075.40  |
| .419                 | 103.84              | 158.03  | 212.22  | 320.59  | 374.78  | 428.97  | 537.36  | 645.74   | 862.50   | 1079.25  |
| .420                 | 104.20              | 158.58  | 212.97  | 321.73  | 376.12  | 430.50  | 539.27  | 648.04   | 865.58   | 1083.10  |
| .421                 | 104.56              | 159.13  | 213.72  | 322.87  | 377.45  | 432.03  | 541.19  | 650.34   | 868.66   | 1086.97  |
| .422                 | 104.92              | 159.70  | 214.47  | 324.01  | 378.78  | 433.56  | 543.11  | 652.65   | 871.74   | 1090.84  |
| .423                 | 105.28              | 160.29  | 215.22  | 325.16  | 380.12  | 435.09  | 545.03  | 654.96   | 874.82   | 1094.71  |
| .424                 | 105.64              | 160.88  | 215.97  | 326.30  | 381.46  | 436.62  | 546.05  | 657.17   | 877.90   | 1098.58  |
| .425                 | 106.01              | 161.37  | 216.73  | 327.44  | 382.80  | 438.15  | 548.88  | 659.58   | 880.99   | 1102.45  |
| .426                 | 106.37              | 161.93  | 217.48  | 328.58  | 384.16  | 439.69  | 550.81  | 661.90   | 884.10   | 1106.34  |
| .427                 | 106.73              | 162.49  | 218.23  | 329.73  | 385.50  | 441.23  | 552.75  | 664.22   | 887.21   | 1110.23  |
| .428                 | 107.10              | 163.05  | 218.99  | 330.88  | 386.84  | 442.77  | 554.69  | 666.54   | 890.32   | 1114.12  |
| .429                 | 107.46              | 163.61  | 219.75  | 332.03  | 388.19  | 444.31  | 556.63  | 668.87   | 893.43   | 1118.01  |
| .430                 | 107.83              | 164.17  | 220.51  | 333.18  | 389.52  | 445.86  | 558.53  | 671.20   | 896.55   | 1121.90  |
| .431                 | 108.19              | 164.73  | 221.27  | 334.33  | 390.87  | 447.40  | 560.47  | 673.54   | 899.67   | 1125.81  |
| .432                 | 108.55              | 165.29  | 222.03  | 335.48  | 392.25  | 448.95  | 562.41  | 675.88   | 902.79   | 1129.72  |
| .433                 | 108.92              | 165.85  | 222.79  | 336.63  | 393.60  | 450.50  | 564.35  | 678.22   | 905.92   | 1133.63  |
| .434                 | 109.29              | 166.41  | 223.55  | 337.79  | 394.95  | 452.05  | 566.29  | 680.56   | 909.05   | 1137.55  |
| .435                 | 109.66              | 166.98  | 224.31  | 338.95  | 396.27  | 453.60  | 568.24  | 682.90   | 912.18   | 1141.47  |
| .436                 | 110.02              | 167.54  | 225.07  | 340.11  | 397.62  | 455.16  | 570.19  | 685.25   | 915.32   | 1145.40  |
| .437                 | 110.39              | 168.10  | 225.83  | 341.27  | 398.98  | 456.72  | 572.14  | 687.61   | 918.46   | 1149.33  |
| .438                 | 110.76              | 168.67  | 226.59  | 342.43  | 400.34  | 458.28  | 574.09  | 689.97   | 921.60   | 1153.27  |
| .439                 | 111.13              | 169.24  | 227.36  | 343.59  | 401.70  | 459.84  | 576.05  | 692.33   | 924.74   | 1157.21  |
| .440                 | 111.50              | 169.81  | 228.13  | 344.75  | 403.06  | 461.40  | 578.01  | 694.64   | 927.89   | 1161.15  |
| .441                 | 111.86              | 170.37  | 228.89  | 345.91  | 404.43  | 462.96  | 579.97  | 697.00   | 931.05   | 1165.10  |

| Depth on Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |         |          |          |          |
|----------------|---------------------|---------|---------|---------|---------|---------|---------|----------|----------|----------|
|                | Feet.               | 2 Feet. | 3 Feet. | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. |
| .442           | 112.23              | 170.94  | 229.66  | 347.08  | 405.80  | 464.52  | 581.93  | 699.36   | 934.21   | 1169.06  |
| .443           | 112.60              | 171.51  | 230.43  | 348.25  | 407.17  | 466.08  | 583.89  | 701.68   | 937.37   | 1173.02  |
| .444           | 112.97              | 172.08  | 231.20  | 349.42  | 408.54  | 467.64  | 585.86  | 704.04   | 940.53   | 1176.98  |
| .445           | 113.34              | 172.65  | 231.97  | 350.59  | 409.91  | 469.21  | 587.83  | 706.45   | 943.70   | 1180.94  |
| .446           | 113.71              | 173.22  | 232.74  | 351.76  | 411.28  | 470.78  | 589.80  | 708.83   | 946.87   | 1184.92  |
| .447           | 114.08              | 173.79  | 233.51  | 352.93  | 412.65  | 472.35  | 591.77  | 711.21   | 950.04   | 1188.90  |
| .448           | 114.45              | 174.36  | 234.28  | 354.10  | 414.02  | 473.92  | 593.74  | 713.59   | 953.22   | 1192.88  |
| .449           | 114.82              | 175.13  | 235.05  | 355.28  | 415.39  | 475.49  | 595.72  | 715.97   | 956.40   | 1196.86  |
| .450           | 115.20              | 175.51  | 235.83  | 356.46  | 416.77  | 477.07  | 597.70  | 718.35   | 959.58   | 1200.84  |
| .451           | 115.57              | 176.08  | 236.61  | 357.63  | 418.15  | 478.75  | 599.68  | 720.73   | 962.77   | 1204.84  |
| .452           | 115.94              | 176.65  | 237.38  | 358.81  | 419.53  | 480.33  | 601.67  | 723.11   | 965.96   | 1208.84  |
| .453           | 116.31              | 177.22  | 238.16  | 359.99  | 420.91  | 481.91  | 603.66  | 725.49   | 969.16   | 1212.84  |
| .454           | 116.68              | 177.80  | 238.94  | 361.17  | 422.29  | 483.50  | 605.65  | 727.88   | 972.36   | 1216.84  |
| .455           | 117.06              | 178.38  | 239.71  | 362.35  | 423.67  | 484.99  | 607.64  | 730.27   | 975.56   | 1220.85  |
| .456           | 117.43              | 178.95  | 240.50  | 363.53  | 425.06  | 486.58  | 609.63  | 732.67   | 978.77   | 1224.87  |
| .457           | 117.80              | 179.53  | 241.30  | 364.71  | 426.46  | 488.17  | 611.62  | 735.07   | 981.98   | 1228.90  |
| .458           | 118.18              | 180.11  | 242.10  | 365.90  | 427.86  | 489.76  | 613.61  | 737.47   | 985.19   | 1232.93  |
| .459           | 118.56              | 180.69  | 242.90  | 367.09  | 429.26  | 491.35  | 615.61  | 739.88   | 988.40   | 1236.96  |
| .460           | 118.94              | 181.27  | 243.60  | 368.28  | 430.61  | 492.94  | 617.61  | 742.29   | 991.62   | 1240.99  |
| .461           | 119.31              | 181.85  | 244.38  | 369.47  | 432.00  | 494.54  | 619.61  | 744.70   | 994.85   | 1245.03  |
| .462           | 119.68              | 182.43  | 245.16  | 370.66  | 433.40  | 496.14  | 621.61  | 747.10   | 998.08   | 1249.07  |
| .463           | 120.06              | 183.01  | 245.94  | 371.85  | 434.80  | 497.74  | 623.62  | 749.51   | 1001.31  | 1253.11  |
| .464           | 120.44              | 183.59  | 246.72  | 373.04  | 436.20  | 499.34  | 625.63  | 751.92   | 1004.54  | 1257.16  |
| .465           | 120.82              | 184.17  | 247.50  | 374.23  | 437.60  | 500.94  | 627.64  | 754.35   | 1007.77  | 1261.19  |
| .466           | 121.19              | 184.75  | 248.29  | 375.42  | 439.06  | 502.54  | 629.66  | 756.77   | 1011.01  | 1265.25  |
| .467           | 121.57              | 185.33  | 249.08  | 376.62  | 440.40  | 504.14  | 631.68  | 759.29   | 1014.25  | 1269.31  |
| .468           | 121.95              | 185.91  | 249.87  | 377.82  | 441.80  | 505.75  | 633.70  | 761.72   | 1017.50  | 1273.38  |
| .469           | 122.33              | 186.49  | 250.66  | 379.02  | 442.20  | 507.36  | 635.72  | 764.15   | 1020.75  | 1277.45  |
| .470           | 122.71              | 187.08  | 251.46  | 380.22  | 444.60  | 508.97  | 637.75  | 766.49   | 1024.00  | 1281.52  |
| .471           | 123.08              | 187.66  | 252.25  | 381.42  | 446.00  | 510.57  | 639.77  | 768.93   | 1027.26  | 1285.61  |
| .472           | 123.47              | 188.24  | 253.04  | 382.62  | 447.41  | 512.21  | 641.79  | 771.37   | 1030.52  | 1289.70  |
| .473           | 123.85              | 188.83  | 253.83  | 383.83  | 448.81  | 513.85  | 643.82  | 773.81   | 1033.78  | 1293.79  |
| .474           | 124.23              | 189.42  | 254.62  | 385.04  | 449.62  | 514.49  | 645.85  | 776.25   | 1037.04  | 1297.88  |
| .475           | 124.60              | 190.01  | 255.42  | 386.24  | 451.64  | 517.17  | 647.88  | 778.71   | 1040.30  | 1301.96  |
| .476           | 124.98              | 190.59  | 256.21  | 387.45  | 453.05  | 518.83  | 649.91  | 781.16   | 1043.58  | 1306.06  |
| .477           | 125.36              | 191.18  | 257.00  | 388.66  | 454.47  | 520.49  | 651.94  | 783.61   | 1046.86  | 1310.17  |
| .478           | 125.74              | 191.77  | 257.80  | 389.87  | 455.89  | 522.16  | 653.98  | 786.06   | 1050.15  | 1314.28  |
| .479           | 126.12              | 192.36  | 258.60  | 391.08  | 457.31  | 523.83  | 656.02  | 788.51   | 1053.44  | 1318.39  |
| .480           | 126.51              | 192.95  | 259.40  | 392.29  | 458.73  | 525.18  | 658.06  | 790.96   | 1056.73  | 1322.50  |
| .481           | 126.89              | 193.54  | 260.19  | 393.50  | 460.15  | 526.81  | 660.10  | 793.43   | 1060.02  | 1326.63  |
| .482           | 127.27              | 194.13  | 260.99  | 394.71  | 461.58  | 528.44  | 662.15  | 795.90   | 1063.31  | 1330.76  |
| .483           | 127.65              | 194.72  | 261.79  | 395.93  | 463.01  | 530.07  | 664.20  | 798.37   | 1066.60  | 1334.89  |
| .484           | 128.05              | 195.13  | 262.59  | 397.15  | 464.44  | 531.70  | 666.25  | 800.84   | 1069.90  | 1339.03  |
| .485           | 128.42              | 195.90  | 263.39  | 398.37  | 465.87  | 533.33  | 668.30  | 803.31   | 1073.20  | 1343.17  |
| .486           | 128.80              | 196.49  | 264.19  | 399.59  | 467.29  | 534.97  | 670.36  | 805.78   | 1076.51  | 1347.32  |
| .487           | 129.18              | 197.08  | 264.99  | 400.81  | 469.71  | 536.61  | 672.42  | 808.26   | 1079.82  | 1351.47  |
| .488           | 129.56              | 197.68  | 265.79  | 402.03  | 471.14  | 538.25  | 674.48  | 810.74   | 1083.13  | 1355.62  |
| .489           | 129.95              | 198.28  | 266.59  | 403.25  | 472.57  | 539.89  | 676.54  | 813.22   | 1086.45  | 1359.77  |
| .490           | 130.34              | 198.88  | 267.41  | 404.47  | 473.00  | 541.53  | 678.60  | 815.70   | 1089.70  | 1363.92  |
| .491           | 130.72              | 199.47  | 268.21  | 405.69  | 474.44  | 543.17  | 680.66  | 818.18   | 1093.04  | 1368.09  |
| .492           | 131.10              | 200.06  | 269.01  | 406.92  | 475.88  | 544.81  | 682.73  | 820.66   | 1096.39  | 1372.26  |
| .493           | 131.49              | 200.66  | 269.82  | 408.15  | 477.32  | 546.45  | 684.80  | 823.14   | 1099.74  | 1376.43  |
| .494           | 131.88              | 201.26  | 270.63  | 409.38  | 478.76  | 548.10  | 686.87  | 825.62   | 1103.09  | 1380.60  |
| .495           | 132.27              | 201.86  | 271.44  | 410.61  | 480.20  | 549.75  | 688.94  | 828.10   | 1106.44  | 1384.78  |
| .496           | 132.66              | 202.46  | 272.25  | 411.84  | 481.64  | 551.41  | 691.02  | 830.60   | 1109.92  | 1388.97  |
| .497           | 133.05              | 203.06  | 273.06  | 413.07  | 483.08  | 553.07  | 693.10  | 833.10   | 1113.40  | 1393.16  |
| .498           | 133.44              | 203.66  | 273.87  | 414.30  | 484.52  | 554.73  | 695.18  | 835.60   | 1116.88  | 1397.35  |
| .499           | 133.83              | 204.26  | 274.68  | 415.54  | 485.97  | 556.39  | 697.26  | 838.11   | 1120.36  | 1401.54  |

QUANTITIES OF WATER, IN CUBIC FEET PER MINUTE, FLOWING OVER WEIRS OF DIFFERENT LENGTHS, WITH VARYING DEPTHS OF WATER.

| Depth on Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |          |          |          |          |
|----------------|---------------------|---------|---------|---------|---------|---------|----------|----------|----------|----------|
|                | 2 Feet.             | 3 Feet. | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| .500           | 134.22              | 204.86  | 275.50  | 416.78  | 487.42  | 558.06  | 699.34   | 840.62   | 1123.18  | 1405.74  |
| .501           | 134.61              | 205.46  | 276.31  | 418.01  | 488.87  | 559.72  | 701.42   | 843.13   | 1126.54  | 1409.95  |
| .502           | 135.00              | 206.06  | 277.12  | 419.25  | 490.32  | 561.38  | 703.51   | 845.64   | 1129.90  | 1414.16  |
| .503           | 135.39              | 206.66  | 277.93  | 420.49  | 491.77  | 563.04  | 705.60   | 848.15   | 1133.26  | 1418.37  |
| .504           | 135.78              | 207.26  | 278.74  | 421.73  | 493.22  | 564.71  | 707.69   | 850.66   | 1136.62  | 1422.58  |
| .505           | 136.16              | 207.86  | 279.57  | 422.97  | 494.67  | 566.38  | 709.78   | 853.18   | 1139.99  | 1426.80  |
| .506           | 136.55              | 208.46  | 280.38  | 424.21  | 496.13  | 568.05  | 711.87   | 855.70   | 1143.37  | 1431.03  |
| .507           | 136.94              | 209.06  | 281.20  | 425.45  | 497.59  | 569.72  | 713.97   | 858.22   | 1146.75  | 1435.27  |
| .508           | 137.33              | 209.67  | 282.02  | 426.70  | 499.05  | 571.39  | 716.07   | 860.75   | 1150.13  | 1439.51  |
| .509           | 137.72              | 210.28  | 282.84  | 427.95  | 500.57  | 573.06  | 718.17   | 863.28   | 1153.51  | 1443.75  |
| .510           | 138.12              | 210.89  | 283.66  | 429.20  | 501.97  | 574.74  | 720.27   | 865.81   | 1156.89  | 1447.94  |
| .511           | 138.51              | 211.50  | 211.71  | 430.45  | 503.43  | 576.41  | 722.38   | 868.34   | 1160.28  | 1453.20  |
| .512           | 138.90              | 212.11  | 212.53  | 431.70  | 504.89  | 578.09  | 724.49   | 870.88   | 1163.67  | 1458.46  |
| .513           | 139.29              | 212.71  | 213.35  | 432.95  | 506.35  | 579.77  | 726.60   | 873.42   | 1167.07  | 1462.72  |
| .514           | 139.68              | 213.32  | 214.17  | 434.20  | 507.82  | 581.45  | 728.71   | 875.98   | 1170.47  | 1466.46  |
| .515           | 140.08              | 213.92  | 287.76  | 435.45  | 509.29  | 583.13  | 730.82   | 878.50   | 1173.87  | 1469.24  |
| .516           | 140.47              | 214.53  | 288.58  | 436.70  | 510.76  | 584.81  | 732.93   | 881.05   | 1177.28  | 1474.51  |
| .517           | 140.86              | 215.14  | 289.40  | 437.95  | 512.23  | 586.40  | 735.05   | 883.60   | 1180.69  | 1478.78  |
| .518           | 141.25              | 215.75  | 290.23  | 439.21  | 513.70  | 588.09  | 737.17   | 886.15   | 1184.11  | 1483.06  |
| .519           | 141.64              | 216.36  | 291.06  | 440.47  | 515.17  | 589.78  | 739.29   | 888.70   | 1187.53  | 1487.34  |
| .520           | 142.05              | 216.97  | 291.89  | 441.73  | 516.65  | 591.57  | 741.41   | 891.25   | 1190.91  | 1490.62  |
| .521           | 142.45              | 217.58  | 292.71  | 442.99  | 518.13  | 593.26  | 743.54   | 893.81   | 1194.26  | 1494.91  |
| .522           | 142.85              | 218.19  | 293.54  | 444.25  | 519.61  | 594.95  | 745.67   | 896.37   | 1197.79  | 1499.20  |
| .523           | 143.25              | 218.80  | 294.37  | 445.51  | 521.09  | 596.65  | 747.80   | 898.93   | 1201.22  | 1503.49  |
| .524           | 143.65              | 219.41  | 295.20  | 446.77  | 522.57  | 598.35  | 749.93   | 901.49   | 1204.65  | 1507.79  |
| .525           | 144.03              | 220.03  | 296.03  | 448.04  | 524.05  | 600.05  | 752.06   | 904.06   | 1208.08  | 1512.09  |
| .526           | 144.43              | 220.64  | 296.86  | 449.30  | 525.53  | 601.75  | 754.19   | 906.63   | 1211.52  | 1516.40  |
| .527           | 144.83              | 221.25  | 297.69  | 450.57  | 527.01  | 603.45  | 756.33   | 909.20   | 1214.96  | 1520.71  |
| .528           | 145.23              | 221.86  | 298.52  | 451.84  | 528.49  | 605.15  | 758.47   | 911.77   | 1218.40  | 1525.03  |
| .529           | 145.60              | 222.47  | 299.36  | 453.11  | 429.98  | 606.85  | 760.61   | 914.34   | 1221.85  | 1529.35  |
| .530           | 146.01              | 223.10  | 300.20  | 454.38  | 531.47  | 608.56  | 762.75   | 916.93   | 1225.30  | 1533.67  |
| .531           | 146.41              | 223.72  | 301.03  | 455.65  | 532.96  | 610.27  | 764.89   | 919.51   | 1228.76  | 1538.00  |
| .532           | 146.81              | 224.34  | 301.86  | 456.92  | 534.45  | 611.98  | 767.04   | 922.09   | 1232.12  | 1542.33  |
| .533           | 147.21              | 224.96  | 302.70  | 458.19  | 535.94  | 613.69  | 769.19   | 924.68   | 1235.58  | 1546.66  |
| .534           | 147.61              | 225.58  | 303.54  | 459.47  | 537.43  | 615.40  | 771.34   | 927.27   | 1239.04  | 1551.00  |
| .535           | 148.01              | 226.19  | 304.38  | 460.75  | 538.93  | 617.12  | 773.49   | 929.86   | 1242.60  | 1555.34  |
| .536           | 148.41              | 226.81  | 305.21  | 462.02  | 540.43  | 618.83  | 775.64   | 932.45   | 1246.07  | 1559.69  |
| .537           | 148.81              | 227.43  | 306.05  | 463.30  | 541.93  | 620.55  | 777.80   | 935.05   | 1249.54  | 1564.04  |
| .538           | 149.21              | 228.05  | 306.89  | 464.58  | 543.43  | 622.27  | 779.96   | 937.65   | 1253.02  | 1568.40  |
| .539           | 149.61              | 228.67  | 307.73  | 465.86  | 544.93  | 623.99  | 782.12   | 940.25   | 1256.50  | 1572.76  |
| .540           | 150.01              | 229.29  | 308.57  | 467.14  | 546.43  | 625.71  | 784.28   | 942.85   | 1259.98  | 1577.12  |
| .541           | 150.41              | 229.91  | 309.41  | 468.42  | 547.93  | 627.43  | 786.44   | 945.45   | 1263.47  | 1581.49  |
| .542           | 150.81              | 230.53  | 310.25  | 469.70  | 549.43  | 629.15  | 788.61   | 948.06   | 1266.96  | 1585.86  |
| .543           | 151.21              | 231.15  | 311.09  | 470.98  | 550.93  | 630.88  | 790.78   | 950.67   | 1270.45  | 1590.23  |
| .544           | 151.61              | 231.77  | 311.94  | 472.27  | 552.44  | 632.61  | 792.95   | 953.22   | 1273.94  | 1594.61  |
| .545           | 152.01              | 232.40  | 312.79  | 473.56  | 553.95  | 634.34  | 795.12   | 955.89   | 1277.44  | 1598.99  |
| .546           | 152.41              | 233.03  | 313.63  | 475.85  | 555.46  | 636.07  | 797.29   | 958.51   | 1280.95  | 1603.38  |
| .547           | 152.81              | 233.66  | 314.47  | 477.14  | 556.97  | 637.80  | 799.46   | 961.13   | 1284.46  | 1607.77  |
| .548           | 153.21              | 234.29  | 315.32  | 478.43  | 558.48  | 639.53  | 801.64   | 963.75   | 1287.97  | 1612.17  |
| .549           | 153.61              | 234.92  | 316.27  | 479.72  | 559.99  | 641.27  | 803.82   | 966.37   | 1291.48  | 1616.57  |
| .550           | 154.03              | 235.53  | 317.02  | 480.01  | 561.51  | 643.01  | 806.00   | 969.00   | 1294.99  | 1620.97  |
| .551           | 154.43              | 236.16  | 317.87  | 481.30  | 563.02  | 644.75  | 808.18   | 971.63   | 1298.51  | 1625.38  |
| .552           | 154.83              | 236.79  | 318.72  | 482.59  | 564.54  | 646.49  | 810.36   | 974.26   | 1302.03  | 1629.71  |
| .553           | 155.23              | 237.42  | 319.57  | 483.89  | 566.06  | 648.23  | 812.54   | 976.89   | 1305.55  | 1634.12  |
| .554           | 155.63              | 238.05  | 320.42  | 485.19  | 567.58  | 649.97  | 814.72   | 979.52   | 1309.07  | 1638.54  |

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|---------|---------|---------|----------|----------|----------|----------|
|                      | 2 Feet.             | 3 Feet. | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| .555                 | 156.05              | 238.66  | 321.27  | 486.49  | 569.10  | 651.71  | 816.93   | 982.16   | 1312.60  | 1643.04  |
| .556                 | 156.46              | 239.29  | 322.12  | 487.79  | 570.62  | 653.46  | 819.12   | 984.80   | 1316.13  | 1647.47  |
| .557                 | 156.87              | 239.92  | 322.97  | 489.09  | 572.14  | 655.25  | 821.32   | 987.48   | 1319.67  | 1651.90  |
| .558                 | 157.28              | 240.55  | 323.82  | 490.39  | 573.67  | 657.06  | 823.52   | 990.12   | 1323.21  | 1656.33  |
| .559                 | 157.69              | 241.18  | 324.68  | 491.69  | 575.20  | 658.75  | 825.72   | 992.76   | 1326.74  | 1660.77  |
| .560                 | 158.08              | 241.81  | 325.54  | 493.00  | 576.73  | 660.46  | 827.92   | 995.37   | 1330.29  | 1665.21  |
| .561                 | 158.49              | 242.44  | 326.39  | 494.30  | 578.26  | 662.21  | 830.12   | 998.02   | 1333.84  | 1669.66  |
| .562                 | 158.00              | 243.07  | 327.24  | 495.60  | 579.79  | 663.96  | 832.32   | 1000.67  | 1337.39  | 1674.11  |
| .563                 | 158.41              | 243.70  | 328.10  | 496.91  | 581.32  | 665.72  | 834.52   | 1003.33  | 1340.94  | 1678.56  |
| .564                 | 158.82              | 244.33  | 328.96  | 498.22  | 582.85  | 667.48  | 836.73   | 1005.99  | 1344.50  | 1683.02  |
| .565                 | 160.12              | 244.97  | 329.82  | 499.53  | 584.38  | 669.24  | 838.94   | 1008.65  | 1348.06  | 1687.48  |
| .566                 | 160.53              | 245.61  | 330.68  | 500.84  | 585.91  | 671.00  | 841.15   | 1011.31  | 1351.63  | 1691.95  |
| .567                 | 160.94              | 246.25  | 331.54  | 502.15  | 587.45  | 672.76  | 843.36   | 1013.97  | 1355.20  | 1696.42  |
| .568                 | 161.35              | 246.89  | 332.40  | 503.46  | 588.99  | 674.52  | 845.58   | 1016.54  | 1358.77  | 1700.89  |
| .569                 | 161.76              | 247.54  | 333.26  | 504.77  | 590.53  | 676.28  | 847.80   | 1019.21  | 1362.27  | 1705.36  |
| .570                 | 162.16              | 248.19  | 334.13  | 506.09  | 592.07  | 678.05  | 850.02   | 1021.98  | 1365.91  | 1709.84  |
| .571                 | 162.57              | 248.82  | 334.99  | 507.40  | 593.61  | 679.82  | 852.24   | 1024.65  | 1369.49  | 1714.33  |
| .572                 | 162.98              | 249.45  | 335.85  | 508.72  | 595.15  | 681.59  | 854.46   | 1027.33  | 1373.07  | 1718.82  |
| .573                 | 163.39              | 250.08  | 336.71  | 510.04  | 596.69  | 683.36  | 856.68   | 1030.01  | 1376.66  | 1723.31  |
| .574                 | 163.80              | 250.71  | 337.08  | 511.36  | 598.24  | 685.13  | 858.91   | 1032.69  | 1380.25  | 1727.80  |
| .575                 | 164.21              | 251.33  | 338.45  | 512.68  | 599.79  | 686.91  | 861.14   | 1035.37  | 1383.84  | 1732.30  |
| .576                 | 164.62              | 251.93  | 339.31  | 514.00  | 601.34  | 688.68  | 863.37   | 1038.06  | 1387.44  | 1736.81  |
| .577                 | 164.83              | 252.53  | 340.17  | 515.32  | 602.89  | 690.46  | 865.60   | 1040.75  | 1391.04  | 1741.32  |
| .578                 | 165.24              | 253.13  | 341.04  | 516.64  | 604.44  | 692.24  | 867.83   | 1043.44  | 1394.64  | 1745.83  |
| .579                 | 165.65              | 253.73  | 341.91  | 517.96  | 605.99  | 694.02  | 870.07   | 1046.13  | 1398.24  | 1750.34  |
| .580                 | 166.27              | 254.53  | 342.78  | 519.29  | 607.54  | 695.80  | 872.31   | 1048.82  | 1401.84  | 1754.86  |
| .581                 | 166.69              | 255.17  | 343.65  | 520.61  | 609.09  | 697.58  | 874.55   | 1051.52  | 1405.45  | 1759.39  |
| .582                 | 167.11              | 255.81  | 344.52  | 521.94  | 610.65  | 699.36  | 876.79   | 1054.22  | 1409.06  | 1764.92  |
| .583                 | 167.53              | 256.45  | 345.39  | 523.27  | 612.21  | 701.15  | 879.03   | 1056.92  | 1412.67  | 1769.45  |
| .584                 | 167.95              | 257.09  | 346.26  | 524.60  | 613.77  | 702.94  | 881.27   | 1059.62  | 1416.28  | 1773.98  |
| .585                 | 168.34              | 257.74  | 347.13  | 525.93  | 615.33  | 704.73  | 883.52   | 1062.32  | 1419.91  | 1778.51  |
| .586                 | 168.76              | 258.38  | 348.00  | 527.26  | 616.89  | 706.52  | 885.77   | 1064.03  | 1423.54  | 1782.05  |
| .587                 | 169.18              | 259.02  | 348.87  | 528.59  | 618.45  | 708.31  | 888.02   | 1066.74  | 1427.17  | 1786.60  |
| .588                 | 169.60              | 259.66  | 349.74  | 529.92  | 620.01  | 710.10  | 890.27   | 1069.45  | 1430.80  | 1791.15  |
| .589                 | 070.02              | 260.31  | 350.62  | 531.26  | 621.87  | 711.89  | 892.52   | 1072.16  | 1434.43  | 1795.70  |
| .590                 | 170.41              | 260.96  | 351.50  | 532.60  | 623.14  | 713.69  | 894.78   | 1075.88  | 1438.07  | 1800.25  |
| .591                 | 170.83              | 261.60  | 352.37  | 533.93  | 624.71  | 715.49  | 897.04   | 1078.60  | 1441.71  | 1804.81  |
| .592                 | 171.25              | 262.24  | 353.25  | 535.27  | 626.28  | 717.29  | 899.30   | 1081.32  | 1445.35  | 1809.38  |
| .593                 | 171.66              | 262.89  | 354.13  | 536.61  | 627.85  | 719.09  | 901.56   | 1084.04  | 1448.99  | 1814.95  |
| .594                 | 172.08              | 263.54  | 355.01  | 537.95  | 629.42  | 720.89  | 903.82   | 1086.76  | 1452.63  | 1819.52  |
| .595                 | 172.49              | 264.19  | 355.89  | 539.29  | 630.99  | 722.69  | 906.09   | 1089.49  | 1456.29  | 1823.69  |
| .596                 | 172.91              | 264.83  | 356.77  | 540.63  | 632.56  | 724.49  | 908.36   | 1092.22  | 1459.95  | 1827.67  |
| .597                 | 173.33              | 265.48  | 357.65  | 541.97  | 634.10  | 726.30  | 910.63   | 1094.95  | 1463.61  | 1832.26  |
| .598                 | 173.75              | 266.13  | 358.53  | 543.31  | 635.68  | 728.11  | 912.90   | 1097.68  | 1467.27  | 1836.85  |
| .599                 | 174.17              | 266.78  | 359.41  | 544.66  | 637.26  | 729.92  | 915.17   | 1100.42  | 1470.93  | 1841.44  |
| .600                 | 174.57              | 267.43  | 360.29  | 546.01  | 638.87  | 731.73  | 917.44   | 1103.16  | 1474.60  | 1846.03  |
| .601                 | 174.99              | 268.08  | 361.17  | 547.36  | 640.45  | 733.54  | 919.72   | 1105.80  | 1478.27  | 1850.63  |
| .602                 | 175.41              | 268.73  | 362.05  | 548.71  | 642.03  | 735.35  | 922.00   | 1108.54  | 1481.94  | 1855.23  |
| .603                 | 175.83              | 269.38  | 362.93  | 550.06  | 643.61  | 737.16  | 924.28   | 1111.28  | 1485.61  | 1859.84  |
| .604                 | 176.26              | 270.03  | 363.82  | 551.41  | 645.19  | 738.98  | 926.56   | 1114.03  | 1489.29  | 1864.45  |
| .605                 | 176.67              | 270.69  | 364.71  | 552.76  | 646.78  | 740.80  | 928.84   | 1116.88  | 1492.97  | 1869.06  |
| .606                 | 177.09              | 271.34  | 365.59  | 554.11  | 648.36  | 742.62  | 931.12   | 1119.63  | 1496.66  | 1873.68  |
| .607                 | 177.51              | 271.99  | 366.48  | 555.46  | 649.95  | 744.44  | 933.41   | 1122.38  | 1500.35  | 1878.30  |
| .608                 | 177.94              | 272.64  | 367.37  | 556.81  | 651.54  | 746.26  | 935.70   | 1125.14  | 1504.04  | 1882.92  |
| .609                 | 178.37              | 273.30  | 368.26  | 558.17  | 653.13  | 748.08  | 937.99   | 1127.90  | 1507.73  | 1887.55  |
| .610                 | 178.77              | 273.96  | 369.15  | 559.53  | 654.72  | 749.91  | 940.28   | 1130.66  | 1511.42  | 1892.18  |
| .611                 | 179.19              | 274.61  | 370.04  | 560.88  | 656.31  | 751.73  | 942.57   | 1133.42  | 1515.12  | 1896.82  |
| .612                 | 179.61              | 275.26  | 370.93  | 562.24  | 658.03  | 753.56  | 944.87   | 1136.19  | 1518.82  | 1901.46  |



| Depth on Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |         |          |          |          |          |
|----------------|---------------------|---------|---------|---------|---------|---------|---------|----------|----------|----------|----------|
|                | Feet.               | 2 Feet. | 3 Feet. | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| .613           | 180.04              | 275.91  | 371.82  | 563.60  | 659.75  | 755.39  | 947.17  | 1138.96  | 1522.53  | 1906.10  |          |
| .614           | 180.47              | 276.37  | 372.71  | 564.96  | 661.34  | 757.22  | 949.47  | 1141.73  | 1526.24  | 1910.75  |          |
| .615           | 180.87              | 277.23  | 373.60  | 566.32  | 662.68  | 759.05  | 951.77  | 1144.50  | 1529.95  | 1915.40  |          |
| .616           | 181.30              | 277.89  | 374.49  | 567.68  | 664.28  | 760.88  | 954.07  | 1147.27  | 1533.67  | 1920.06  |          |
| .617           | 181.73              | 278.55  | 375.38  | 569.04  | 665.88  | 762.71  | 956.38  | 1150.05  | 1537.39  | 1924.72  |          |
| .618           | 182.16              | 279.21  | 376.27  | 570.41  | 667.48  | 764.55  | 958.69  | 1152.83  | 1541.11  | 1929.78  |          |
| .619           | 182.59              | 279.87  | 377.16  | 571.78  | 669.08  | 766.39  | 961.00  | 1155.61  | 1544.83  | 1934.04  |          |
| .620           | 182.99              | 280.53  | 378.07  | 573.15  | 670.68  | 768.23  | 963.31  | 1158.39  | 1548.55  | 1938.71  |          |
| .621           | 183.42              | 281.19  | 378.96  | 574.51  | 672.28  | 770.07  | 965.62  | 1161.17  | 1552.28  | 1943.39  |          |
| .622           | 183.85              | 281.85  | 379.85  | 575.88  | 673.79  | 771.91  | 967.93  | 1163.96  | 1556.01  | 1948.07  |          |
| .623           | 184.28              | 282.51  | 380.75  | 577.25  | 675.40  | 773.75  | 970.24  | 1166.75  | 1559.74  | 1952.45  |          |
| .624           | 184.71              | 283.17  | 381.65  | 578.63  | 677.01  | 775.59  | 972.55  | 1169.54  | 1563.48  | 1957.43  |          |
| .625           | 185.10              | 283.83  | 382.55  | 579.99  | 678.72  | 777.44  | 974.88  | 1172.33  | 1567.22  | 1962.11  |          |
| .626           | 185.53              | 284.49  | 383.46  | 581.36  | 680.33  | 779.29  | 977.20  | 1175.12  | 1570.96  | 1966.76  |          |
| .627           | 185.96              | 285.15  | 384.37  | 582.73  | 681.94  | 781.14  | 979.52  | 1177.92  | 1574.71  | 1971.42  |          |
| .628           | 186.39              | 285.81  | 385.28  | 584.11  | 683.55  | 782.99  | 981.84  | 1180.72  | 1578.46  | 1976.08  |          |
| .629           | 186.82              | 286.47  | 386.18  | 585.49  | 685.16  | 784.84  | 984.17  | 1183.52  | 1582.21  | 1970.74  |          |
| .630           | 187.23              | 287.14  | 387.05  | 586.87  | 686.78  | 786.69  | 986.50  | 1186.32  | 1585.96  | 1985.60  |          |
| .631           | 187.66              | 287.80  | 387.95  | 588.25  | 688.39  | 788.54  | 988.83  | 1189.13  | 1589.72  | 1990.31  |          |
| .632           | 188.09              | 288.46  | 388.85  | 589.63  | 690.01  | 790.39  | 991.16  | 1191.94  | 1593.48  | 1995.02  |          |
| .633           | 188.52              | 289.12  | 389.75  | 591.01  | 691.63  | 792.25  | 993.49  | 1194.75  | 1597.24  | 1999.74  |          |
| .634           | 188.95              | 289.79  | 390.65  | 592.39  | 693.25  | 794.11  | 995.83  | 1197.56  | 1601.01  | 2004.46  |          |
| .635           | 189.36              | 290.46  | 391.56  | 593.77  | 694.87  | 795.97  | 998.17  | 1200.37  | 1604.78  | 2009.18  |          |
| .636           | 189.79              | 291.12  | 392.36  | 595.15  | 696.49  | 797.83  | 1000.51 | 1203.19  | 1606.97  | 2013.19  |          |
| .637           | 190.22              | 291.78  | 393.27  | 596.53  | 698.11  | 799.69  | 1002.85 | 1206.01  | 1610.37  | 2018.64  |          |
| .638           | 190.65              | 292.45  | 394.18  | 597.91  | 699.73  | 801.55  | 1005.19 | 1208.83  | 1614.17  | 2023.38  |          |
| .639           | 191.08              | 293.12  | 395.09  | 599.30  | 701.36  | 803.42  | 1007.53 | 1211.65  | 1617.97  | 2028.12  |          |
| .640           | 191.50              | 293.80  | 396.10  | 600.69  | 702.99  | 805.29  | 1009.88 | 1214.48  | 1623.67  | 2032.86  |          |
| .641           | 191.93              | 294.46  | 397.00  | 602.08  | 704.62  | 807.16  | 1012.23 | 1217.31  | 1627.46  | 2037.61  |          |
| .642           | 192.36              | 295.12  | 397.91  | 603.47  | 706.25  | 809.03  | 1014.58 | 1220.14  | 1631.25  | 2042.36  |          |
| .643           | 192.79              | 295.79  | 398.82  | 604.86  | 707.88  | 810.90  | 1016.93 | 1222.97  | 1635.04  | 2047.11  |          |
| .644           | 193.22              | 296.46  | 399.73  | 606.25  | 709.51  | 812.77  | 1019.28 | 1225.80  | 1638.83  | 2051.86  |          |
| .645           | 193.65              | 297.14  | 400.64  | 607.64  | 711.14  | 814.64  | 1021.64 | 1228.63  | 1642.63  | 2056.62  |          |
| .646           | 194.08              | 297.81  | 401.55  | 609.03  | 712.77  | 816.51  | 1023.99 | 1231.47  | 1646.43  | 2061.39  |          |
| .647           | 194.51              | 298.48  | 402.46  | 610.42  | 714.40  | 818.38  | 1026.35 | 1234.31  | 1650.23  | 2066.16  |          |
| .648           | 194.94              | 299.15  | 403.37  | 611.82  | 716.04  | 820.26  | 1028.71 | 1237.21  | 1654.04  | 2070.93  |          |
| .649           | 195.37              | 299.82  | 404.29  | 613.22  | 717.68  | 822.14  | 1031.07 | 1240.05  | 1657.85  | 2075.70  |          |
| .650           | 195.80              | 300.50  | 405.21  | 614.62  | 719.32  | 824.02  | 1033.43 | 1242.84  | 1661.66  | 2080.48  |          |
| .651           | 196.23              | 301.17  | 406.12  | 616.01  | 720.96  | 825.90  | 1035.80 | 1245.69  | 1665.48  | 2085.26  |          |
| .652           | 196.66              | 301.84  | 407.03  | 617.41  | 722.60  | 827.78  | 1038.17 | 1248.54  | 1669.30  | 2090.05  |          |
| .653           | 197.09              | 302.51  | 407.91  | 618.81  | 724.24  | 829.66  | 1040.54 | 1251.39  | 1673.12  | 2094.84  |          |
| .654           | 197.52              | 303.19  | 408.86  | 620.21  | 725.88  | 831.55  | 1042.91 | 1254.24  | 1676.94  | 2099.63  |          |
| .655           | 197.95              | 303.87  | 409.78  | 621.61  | 727.53  | 833.44  | 1045.28 | 1257.10  | 1680.76  | 2104.42  |          |
| .656           | 198.38              | 304.54  | 410.60  | 623.01  | 729.17  | 835.33  | 1047.65 | 1259.96  | 1684.59  | 2109.22  |          |
| .657           | 198.81              | 305.21  | 411.52  | 624.41  | 730.82  | 837.22  | 1050.02 | 1262.82  | 1688.42  | 2114.03  |          |
| .658           | 199.24              | 305.88  | 412.44  | 625.82  | 732.47  | 839.11  | 1052.40 | 1265.68  | 1692.26  | 2118.84  |          |
| .659           | 199.67              | 306.56  | 413.36  | 627.23  | 734.12  | 841.00  | 1054.78 | 1268.55  | 1696.10  | 2123.65  |          |
| .660           | 200.10              | 307.25  | 414.38  | 628.64  | 735.77  | 842.90  | 1057.16 | 1271.42  | 1699.94  | 2128.46  |          |
| .661           | 200.55              | 307.92  | 415.30  | 630.05  | 737.42  | 844.79  | 1059.55 | 1274.29  | 1703.79  | 2133.28  |          |
| .662           | 200.98              | 308.59  | 416.22  | 631.46  | 739.07  | 846.69  | 1061.95 | 1277.16  | 1707.64  | 2138.10  |          |
| .663           | 201.41              | 309.27  | 417.14  | 632.87  | 740.72  | 848.59  | 1064.35 | 1280.03  | 1711.49  | 2142.92  |          |
| .664           | 201.81              | 309.95  | 418.07  | 634.28  | 742.38  | 850.49  | 1066.75 | 1282.91  | 1715.34  | 2147.75  |          |
| .665           | 202.29              | 310.64  | 418.99  | 635.69  | 744.04  | 852.39  | 1069.09 | 1285.79  | 1719.19  | 2152.58  |          |
| .666           | 202.72              | 311.32  | 419.91  | 637.10  | 745.70  | 854.31  | 1071.48 | 1288.67  | 1723.05  | 2157.42  |          |
| .667           | 203.15              | 312.00  | 420.83  | 638.51  | 747.36  | 856.23  | 1073.87 | 1291.55  | 1726.91  | 2162.26  |          |
| .668           | .....               | 312.68  | 421.75  | 639.92  | 749.02  | 858.15  | 1076.26 | 1294.43  | 1730.71  | 2167.10  |          |
| .669           | .....               | 313.36  | 422.68  | 641.34  | 750.68  | 860.08  | 1078.66 | 1297.32  | 1734.63  | 2171.95  |          |
| .670           | .....               | 314.04  | 423.61  | 642.76  | 752.34  | 861.91  | 1081.06 | 1300.21  | 1738.50  | 2176.80  |          |

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|---------|---------|----------|----------|----------|----------|
|                      | 3 Feet.             | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| .671                 | 314.72              | 424.53  | 644.18  | 754.00  | 863.82  | 1083.46  | 1303.10  | 1742.37  | 2181.66  |
| .672                 | 315.40              | 425.46  | 645.60  | 755.66  | 865.73  | 1085.86  | 1305.99  | 1746.25  | 2186.52  |
| .673                 | 316.08              | 426.39  | 647.02  | 757.32  | 867.64  | 1088.26  | 1308.88  | 1750.13  | 2191.38  |
| .674                 | 316.76              | 427.32  | 648.44  | 758.99  | 869.55  | 1090.66  | 1311.78  | 1754.01  | 2196.24  |
| .675                 | 317.45              | 428.25  | 649.86  | 760.66  | 871.47  | 1093.07  | 1314.68  | 1757.89  | 2201.10  |
| .676                 | 318.13              | 429.28  | 651.28  | 762.33  | 873.38  | 1095.48  | 1317.58  | 1761.78  | 2205.97  |
| .677                 | 318.81              | 430.21  | 652.70  | 764.00  | 875.30  | 1097.89  | 1320.48  | 1765.67  | 2210.85  |
| .678                 | 319.50              | 431.14  | 654.12  | 765.67  | 877.22  | 1100.30  | 1323.38  | 1769.56  | 2215.73  |
| .679                 | 320.19              | 432.07  | 655.55  | 767.34  | 879.14  | 1102.71  | 1326.29  | 1773.45  | 2220.61  |
| .680                 | 320.87              | 432.91  | 656.98  | 769.02  | 881.06  | 1105.13  | 1329.20  | 1777.34  | 2225.49  |
| .681                 | 321.55              | 433.84  | 658.41  | 770.69  | 882.98  | 1107.54  | 1332.11  | 1781.24  | 2230.38  |
| .682                 | 322.23              | 434.77  | 659.84  | 772.36  | 884.90  | 1109.96  | 1335.02  | 1785.14  | 2235.27  |
| .683                 | 322.92              | 435.70  | 661.23  | 774.04  | 886.82  | 1112.28  | 1337.93  | 1789.05  | 2240.17  |
| .684                 | 323.61              | 436.64  | 662.66  | 776.72  | 888.75  | 1114.80  | 1340.85  | 1792.96  | 2245.07  |
| .685                 | 324.30              | 437.58  | 664.13  | 777.40  | 890.68  | 1117.22  | 1343.77  | 1796.87  | 2249.97  |
| .686                 | 324.99              | 438.51  | 665.56  | 779.08  | 892.61  | 1119.64  | 1346.69  | 1800.78  | 2254.88  |
| .687                 | 325.68              | 439.44  | 666.99  | 780.76  | 894.54  | 1132.07  | 1349.61  | 1804.70  | 2259.79  |
| .688                 | 326.37              | 440.38  | 668.42  | 782.44  | 896.47  | 1134.50  | 1352.54  | 1808.62  | 2264.70  |
| .689                 | 327.06              | 441.32  | 669.86  | 784.12  | 898.40  | 1136.93  | 1355.47  | 1812.52  | 2269.61  |
| .690                 | 327.75              | 442.26  | 671.30  | 785.81  | 900.33  | 1129.36  | 1358.40  | 1816.46  | 2274.53  |
| .691                 | 328.44              | 443.20  | 672.73  | 787.50  | 902.26  | 1131.79  | 1361.33  | 1820.39  | 2279.45  |
| .692                 | 329.13              | 444.14  | 674.17  | 789.19  | 904.20  | 1134.23  | 1364.26  | 1824.32  | 2284.37  |
| .693                 | 329.82              | 445.08  | 675.61  | 790.88  | 906.14  | 1136.67  | 1367.19  | 1828.25  | 2289.30  |
| .694                 | 330.51              | 446.02  | 677.05  | 792.57  | 908.18  | 1139.11  | 1370.13  | 1832.19  | 2294.23  |
| .695                 | 331.20              | 446.96  | 678.49  | 794.26  | 910.02  | 1141.55  | 1373.07  | 1836.13  | 2299.18  |
| .696                 | 331.89              | 447.90  | 679.93  | 795.95  | 911.96  | 1143.99  | 1376.01  | 1840.07  | 2304.13  |
| .697                 | 332.58              | 448.86  | 681.37  | 797.64  | 913.90  | 1146.43  | 1378.95  | 1844.01  | 2309.08  |
| .698                 | 333.27              | 449.83  | 682.81  | 799.33  | 915.84  | 1148.87  | 1381.90  | 1847.96  | 2314.03  |
| .699                 | 333.96              | 450.80  | 684.26  | 801.02  | 917.79  | 1151.32  | 1384.85  | 1851.91  | 2318.98  |
| .700                 | 334.66              | 451.69  | 685.71  | 802.72  | 919.74  | 1153.77  | 1387.80  | 1855.86  | 2323.92  |
| .701                 | 335.35              | 452.63  | 687.15  | 804.42  | 921.69  | 1156.22  | 1390.75  | 1859.82  | 2328.88  |
| .702                 | 336.04              | 453.57  | 688.60  | 806.12  | 923.64  | 1158.67  | 1393.70  | 1863.78  | 2333.84  |
| .703                 | 336.74              | 454.51  | 690.05  | 807.82  | 925.59  | 1161.12  | 1396.66  | 1867.74  | 2338.81  |
| .704                 | 337.44              | 455.46  | 691.50  | 809.52  | 927.54  | 1163.58  | 1399.56  | 1871.70  | 2343.78  |
| .705                 | 338.14              | 456.41  | 692.95  | 811.22  | 929.49  | 1166.04  | 1402.58  | 1875.66  | 2348.75  |
| .706                 | 338.83              | 457.35  | 694.40  | 812.92  | 931.44  | 1168.50  | 1405.54  | 1879.73  | 2353.73  |
| .707                 | 339.52              | 458.30  | 695.85  | 814.62  | 933.40  | 1170.96  | 1408.50  | 1883.70  | 2358.71  |
| .708                 | 340.22              | 459.05  | 697.30  | 816.33  | 935.36  | 1173.42  | 1411.47  | 1887.67  | 2363.69  |
| .709                 | 340.92              | 460.00  | 698.76  | 818.04  | 937.32  | 1175.88  | 1414.44  | 1891.65  | 2368.67  |
| .710                 | 341.62              | 461.15  | 700.22  | 819.75  | 939.28  | 1178.34  | 1417.41  | 1895.53  | 2373.66  |
| .711                 | 342.32              | 462.10  | 701.67  | 821.46  | 941.24  | 1180.79  | 1420.38  | 1899.51  | 2378.66  |
| .712                 | 343.02              | 463.05  | 703.12  | 823.17  | 943.20  | 1183.24  | 1423.35  | 1903.50  | 2383.66  |
| .713                 | 343.72              | 464.00  | 704.58  | 824.88  | 945.16  | 1185.69  | 1426.32  | 1907.49  | 2388.66  |
| .714                 | 344.42              | 464.95  | 706.04  | 826.59  | 947.13  | 1188.14  | 1429.30  | 1911.48  | 2393.66  |
| .715                 | 345.12              | 465.91  | 707.50  | 828.30  | 949.10  | 1190.60  | 1432.28  | 1915.47  | 2398.66  |
| .716                 | 345.82              | 466.86  | 708.96  | 830.01  | 951.07  | 1193.16  | 1435.26  | 1919.47  | 2403.67  |
| .717                 | 346.52              | 467.81  | 710.42  | 831.72  | 953.04  | 1195.64  | 1438.24  | 1923.47  | 2408.68  |
| .718                 | 347.22              | 468.77  | 711.88  | 833.44  | 955.01  | 1198.12  | 1441.23  | 1927.47  | 2413.70  |
| .719                 | 347.92              | 469.73  | 713.35  | 835.16  | 956.98  | 1200.60  | 1444.22  | 1931.47  | 2418.72  |
| .720                 | 348.62              | 470.69  | 714.82  | 836.88  | 958.95  | 1203.08  | 1447.21  | 1935.48  | 2423.74  |
| .721                 | 349.32              | 471.64  | 716.30  | 838.60  | 960.92  | 1205.56  | 1450.20  | 1939.49  | 2428.77  |
| .722                 | 350.02              | 472.59  | 717.76  | 840.32  | 962.89  | 1208.04  | 1453.19  | 1943.50  | 2433.80  |
| .723                 | 350.72              | 473.55  | 719.23  | 842.04  | 964.87  | 1210.53  | 1456.19  | 1947.51  | 2438.83  |
| .724                 | 351.42              | 474.51  | 720.70  | 843.76  | 966.85  | 1213.02  | 1459.19  | 1951.53  | 2443.87  |
| .725                 | 352.13              | 475.47  | 722.15  | 845.49  | 968.83  | 1215.51  | 1462.19  | 1955.55  | 2448.91  |
| .726                 | 352.83              | 476.43  | 723.62  | 847.21  | 970.81  | 1218.00  | 1465.19  | 1959.57  | 2453.96  |
| .727                 | 353.53              | 477.39  | 725.09  | 848.94  | 972.79  | 1220.49  | 1468.19  | 1963.60  | 2459.01  |
| .728                 | 354.24              | 478.35  | 726.56  | 850.66  | 974.77  | 1222.98  | 1471.20  | 1967.63  | 2464.06  |



| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|---------|---------|----------|----------|----------|----------|
|                      | 3 Feet.             | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| .729                 | 354.95              | 479.31  | 728.03  | 852.38  | 976.76  | 1225.48  | 1474.21  | 1971.66  | 2469.11  |
| .730                 | 355.66              | 480.28  | 729.51  | 854.13  | 978.75  | 1227.98  | 1477.22  | 1975.69  | 2474.16  |
| .731                 | 356.36              | 481.24  | 730.98  | 855.86  | 980.73  | 1230.48  | 1480.23  | 1979.73  | 2479.22  |
| .732                 | 357.06              | 482.20  | 732.45  | 857.59  | 982.72  | 1232.98  | 1483.24  | 1983.77  | 2484.29  |
| .733                 | 357.76              | 483.16  | 733.93  | 859.32  | 984.71  | 1235.48  | 1486.26  | 1987.81  | 2489.36  |
| .734                 | 358.46              | 484.12  | 735.31  | 861.05  | 986.70  | 1238.98  | 1489.28  | 1991.85  | 2494.43  |
| .735                 | 359.16              | 485.09  | 736.89  | 862.79  | 988.69  | 1240.49  | 1492.30  | 1995.90  | 2499.50  |
| .736                 | 359.87              | 486.05  | 738.37  | 864.53  | 990.68  | 1243.00  | 1495.32  | 1999.95  | 2504.58  |
| .737                 | 360.58              | 487.01  | 739.85  | 866.27  | 992.67  | 1245.51  | 1498.34  | 2004.00  | 2509.66  |
| .738                 | 361.30              | 487.98  | 741.33  | 868.01  | 994.67  | 1248.02  | 1501.36  | 2008.05  | 2514.74  |
| .739                 | 362.02              | 488.95  | 742.81  | 869.75  | 996.67  | 1250.53  | 1504.39  | 2012.11  | 2519.83  |
| .740                 | 362.74              | 489.92  | 744.30  | 871.49  | 998.67  | 1253.05  | 1507.42  | 2016.17  | 2524.92  |
| .741                 | 363.45              | 490.89  | 745.78  | 873.23  | 1000.67 | 1255.56  | 1510.45  | 2020.23  | 2530.02  |
| .742                 | 364.16              | 491.86  | 747.26  | 874.97  | 1002.67 | 1258.08  | 1513.48  | 2024.30  | 2535.12  |
| .743                 | 364.87              | 492.83  | 748.75  | 876.71  | 1004.67 | 1260.60  | 1516.47  | 2028.37  | 2540.22  |
| .744                 | 365.58              | 493.80  | 750.24  | 878.46  | 1006.67 | 1263.12  | 1519.52  | 2032.44  | 2545.32  |
| .745                 | 366.29              | 494.77  | 751.73  | 880.21  | 1008.68 | 1265.64  | 1522.60  | 2036.51  | 2550.42  |
| .746                 | 367.00              | 495.74  | 753.22  | 881.95  | 1010.69 | 1268.16  | 1525.64  | 2040.69  | 2555.53  |
| .747                 | 367.71              | 496.71  | 754.71  | 883.70  | 1012.70 | 1270.68  | 1528.68  | 2044.77  | 2560.63  |
| .748                 | 368.43              | 497.68  | 756.20  | 885.45  | 1014.72 | 1273.21  | 1531.72  | 2048.85  | 2565.77  |
| .749                 | 369.15              | 498.65  | 757.69  | 887.20  | 1016.73 | 1275.74  | 1534.77  | 2052.93  | 2570.89  |
| .750                 | 369.86              | 499.63  | 759.18  | 888.95  | 1018.73 | 1278.27  | 1537.82  | 2056.92  | 2576.01  |
| .751                 | 370.57              | 500.60  | 760.67  | 890.70  | 1020.74 | 1280.80  | 1540.87  | 2061.01  | 2581.14  |
| .752                 | 371.28              | 501.57  | 762.16  | 892.45  | 1022.75 | 1283.33  | 1543.92  | 2065.10  | 2586.27  |
| .753                 | 372.00              | 502.54  | 763.65  | 894.20  | 1024.76 | 1285.87  | 1546.97  | 2069.19  | 2591.40  |
| .754                 | 372.72              | 503.52  | 765.15  | 895.96  | 1026.78 | 1288.41  | 1550.03  | 2073.28  | 2596.54  |
| .755                 | 373.43              | 504.50  | 766.65  | 897.72  | 1028.80 | 1290.95  | 1553.09  | 2077.39  | 2601.68  |
| .756                 | 374.14              | 505.47  | 768.15  | 899.48  | 1030.82 | 1293.49  | 1556.15  | 2081.49  | 2606.83  |
| .757                 | 374.85              | 506.45  | 769.65  | 901.24  | 1032.84 | 1296.03  | 1559.21  | 2085.60  | 2611.98  |
| .758                 | 375.57              | 507.43  | 771.15  | 903.00  | 1034.86 | 1298.57  | 1562.28  | 2089.71  | 2617.13  |
| .759                 | 376.29              | 508.41  | 772.65  | 904.76  | 1036.88 | 1301.11  | 1565.35  | 2093.82  | 2622.28  |
| .760                 | 377.01              | 509.39  | 774.15  | 906.52  | 1038.90 | 1303.66  | 1568.42  | 2097.93  | 2627.44  |
| .761                 | 377.73              | 510.37  | 775.65  | 908.28  | 1040.92 | 1306.21  | 1571.49  | 2102.05  | 2632.60  |
| .762                 | 378.45              | 511.35  | 777.15  | 910.04  | 1042.95 | 1308.76  | 1574.06  | 2106.17  | 2637.77  |
| .763                 | 379.17              | 512.33  | 778.65  | 911.81  | 1044.98 | 1311.31  | 1577.63  | 2110.29  | 2642.94  |
| .764                 | 379.89              | 513.21  | 780.16  | 913.58  | 1047.01 | 1313.86  | 1580.70  | 2114.41  | 2648.11  |
| .765                 | 380.61              | 514.29  | 781.67  | 915.35  | 1049.01 | 1316.41  | 1583.78  | 2118.53  | 2653.28  |
| .766                 | 381.33              | 515.27  | 783.17  | 917.12  | 1051.07 | 1318.96  | 1586.86  | 2122.66  | 2658.46  |
| .767                 | 382.05              | 516.95  | 784.68  | 918.89  | 1053.10 | 1321.52  | 1589.94  | 2126.79  | 2663.64  |
| .768                 | 382.77              | 517.93  | 786.19  | 920.66  | 1055.13 | 1324.08  | 1593.02  | 2130.93  | 2668.82  |
| .769                 | 383.49              | 518.92  | 787.70  | 922.43  | 1057.16 | 1326.64  | 1596.11  | 2135.07  | 2674.01  |
| .770                 | 384.21              | 519.21  | 789.21  | 924.21  | 1059.20 | 1329.20  | 1599.20  | 2139.20  | 2679.20  |
| .771                 | 384.93              | 520.19  | 790.72  | 925.98  | 1061.24 | 1331.76  | 1602.29  | 2143.34  | 2684.40  |
| .772                 | 385.65              | 521.17  | 792.23  | 927.75  | 1063.28 | 1334.22  | 1605.38  | 2147.48  | 2689.60  |
| .773                 | 386.37              | 522.16  | 793.74  | 929.53  | 1065.32 | 1336.89  | 1608.47  | 2151.63  | 2694.80  |
| .774                 | 387.09              | 523.15  | 795.25  | 931.31  | 1067.36 | 1339.46  | 1611.57  | 2155.78  | 2700.00  |
| .775                 | 387.82              | 524.14  | 796.77  | 933.09  | 1069.40 | 1342.03  | 1614.67  | 2159.93  | 2705.20  |
| .776                 | 388.54              | 525.12  | 798.28  | 934.87  | 1071.44 | 1344.60  | 1617.77  | 2164.09  | 2710.41  |
| .777                 | 389.26              | 526.11  | 799.79  | 936.65  | 1073.48 | 1347.17  | 1620.87  | 2168.19  | 2715.62  |
| .778                 | 389.98              | 527.10  | 801.31  | 938.43  | 1075.53 | 1349.75  | 1623.97  | 2172.35  | 2720.81  |
| .779                 | 390.61              | 528.09  | 802.83  | 940.21  | 1077.58 | 1352.33  | 1627.07  | 2176.51  | 2726.06  |
| .780                 | 391.44              | 529.08  | 804.35  | 941.99  | 1079.63 | 1354.91  | 1630.18  | 2180.73  | 2731.28  |
| .781                 | 392.16              | 530.07  | 805.87  | 943.77  | 1081.68 | 1357.49  | 1633.29  | 2184.90  | 2736.51  |
| .782                 | 392.88              | 531.06  | 807.39  | 945.56  | 1083.73 | 1360.07  | 1636.40  | 2189.07  | 2741.74  |
| .783                 | 393.61              | 532.05  | 808.91  | 947.35  | 1085.78 | 1362.65  | 1639.51  | 2193.24  | 2746.97  |
| .784                 | 394.34              | 533.04  | 810.43  | 949.14  | 1087.83 | 1365.23  | 1642.62  | 2197.41  | 2752.21  |
| .785                 | 395.07              | 534.04  | 811.96  | 950.93  | 1089.89 | 1367.82  | 1645.74  | 2201.59  | 2757.45  |
| .786                 | 395.79              | 535.03  | 813.48  | 952.72  | 1091.94 | 1370.40  | 1648.86  | 2205.77  | 2762.69  |

| Depth on Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |          |          |          |          |
|----------------|---------------------|---------|---------|---------|---------|---------|----------|----------|----------|----------|
|                | Feet.               | 3 Feet. | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 14 Feet. | 20 Feet. |
| .787           | 396.51              | 536.02  | 815.00  | 954.51  | 1094.00 | 1372.99 | 1651.98  | 2209.95  | 2767.94  |          |
| .788           | 397.24              | 537.01  | 816.53  | 956.30  | 1096.06 | 1375.58 | 1655.10  | 2214.14  | 2773.19  |          |
| .789           | 397.97              | 538.01  | 818.06  | 958.09  | 1098.12 | 1378.17 | 1658.22  | 2218.33  | 2778.44  |          |
| .790           | 398.71              | 539.01  | 819.59  | 959.88  | 1100.18 | 1380.76 | 1661.35  | 2222.52  | 2783.69  |          |
| .791           | 399.44              | 540.00  | 821.12  | 961.67  | 1102.24 | 1383.35 | 1664.48  | 2226.71  | 2788.95  |          |
| .792           | 400.17              | 540.99  | 822.65  | 963.47  | 1104.30 | 1385.95 | 1667.61  | 2230.91  | 2794.21  |          |
| .793           | 400.90              | 541.00  | 824.18  | 965.27  | 1106.36 | 1388.55 | 1670.74  | 2235.11  | 2799.48  |          |
| .794           | 401.63              | 542.00  | 825.71  | 967.07  | 1108.43 | 1391.15 | 1673.87  | 2239.31  | 2804.75  |          |
| .795           | 402.36              | 543.99  | 827.24  | 968.87  | 1110.50 | 1393.75 | 1677.00  | 2243.51  | 2810.02  |          |
| .796           | 403.09              | 544.99  | 828.77  | 970.67  | 1112.57 | 1396.35 | 1680.14  | 2247.72  | 2815.30  |          |
| .797           | 403.82              | 545.99  | 829.30  | 972.47  | 1114.64 | 1398.95 | 1683.28  | 2251.93  | 2820.58  |          |
| .798           | 404.55              | 546.99  | 830.84  | 974.27  | 1116.71 | 1401.56 | 1686.42  | 2256.14  | 2825.86  |          |
| .799           | 405.28              | 547.99  | 832.38  | 976.07  | 1118.78 | 1404.17 | 1689.56  | 2260.35  | 2831.14  |          |
| .800           | 406.02              | 548.99  | 834.32  | 977.88  | 1120.85 | 1406.78 | 1692.71  | 2264.57  | 2836.43  |          |
| .801           | 406.75              | 549.99  | 836.45  | 979.68  | 1122.92 | 1409.39 | 1695.86  | 2268.79  | 2841.72  |          |
| .802           | 407.48              | 550.99  | 837.99  | 981.49  | 1124.99 | 1412.00 | 1699.01  | 2273.01  | 2847.02  |          |
| .803           | 408.22              | 551.99  | 839.53  | 983.30  | 1127.07 | 1414.61 | 1702.16  | 2277.23  | 2852.32  |          |
| .804           | 408.96              | 552.99  | 841.07  | 985.11  | 1129.15 | 1417.22 | 1705.31  | 2281.46  | 2857.62  |          |
| .805           | 409.69              | 554.00  | 842.61  | 986.92  | 1131.23 | 1419.84 | 1708.46  | 2285.69  | 2862.92  |          |
| .806           | 410.42              | 554.00  | 844.15  | 988.73  | 1133.31 | 1422.46 | 1711.61  | 2289.92  | 2868.23  |          |
| .807           | 411.15              | 555.00  | 845.69  | 990.34  | 1135.39 | 1425.08 | 1714.77  | 2294.15  | 2873.54  |          |
| .808           | 411.89              | 556.00  | 847.23  | 992.35  | 1137.47 | 1427.70 | 1717.93  | 2298.39  | 2878.85  |          |
| .809           | 412.63              | 557.01  | 848.78  | 994.16  | 1139.55 | 1430.32 | 1721.09  | 2302.63  | 2884.17  |          |
| .810           | 413.37              | 559.02  | 850.33  | 995.98  | 1141.64 | 1432.95 | 1724.25  | 2306.87  | 2889.49  |          |
| .811           | 414.10              | 559.02  | 851.87  | 997.79  | 1143.72 | 1435.57 | 1727.42  | 2311.12  | 2894.82  |          |
| .812           | 414.83              | 560.03  | 853.42  | 999.61  | 1145.87 | 1438.20 | 1730.59  | 2315.37  | 2900.15  |          |
| .813           | 415.57              | 561.04  | 854.97  | 1001.43 | 1147.96 | 1440.83 | 1733.76  | 2319.62  | 2905.48  |          |
| .814           | 416.31              | 561.05  | 856.52  | 1003.25 | 1150.05 | 1443.86 | 1736.93  | 2323.87  | 2910.81  |          |
| .815           | 417.05              | 564.06  | 858.07  | 1005.07 | 1152.08 | 1446.09 | 1740.10  | 2328.12  | 2916.14  |          |
| .816           | 417.79              | 565.07  | 859.62  | 1006.89 | 1154.17 | 1448.72 | 1743.27  | 2332.38  | 2921.48  |          |
| .817           | 418.53              | 566.08  | 861.17  | 1008.71 | 1156.26 | 1451.35 | 1746.45  | 2336.64  | 2926.82  |          |
| .818           | 419.27              | 567.09  | 862.72  | 1010.53 | 1158.35 | 1453.99 | 1749.63  | 2340.90  | 2932.17  |          |
| .819           | 420.01              | 568.10  | 864.27  | 1012.46 | 1160.45 | 1456.63 | 1750.81  | 2345.16  | 2937.52  |          |
| .820           | 420.75              | 569.11  | 865.83  | 1014.19 | 1162.55 | 1459.27 | 1755.99  | 2349.43  | 2942.87  |          |
| .821           | 421.59              | 570.12  | 867.38  | 1016.01 | 1164.65 | 1462.91 | 1759.17  | 2353.70  | 2948.23  |          |
| .822           | 422.33              | 571.13  | 868.93  | 1017.84 | 1166.75 | 1465.55 | 1760.35  | 2357.97  | 2953.59  |          |
| .823           | 423.07              | 572.14  | 870.49  | 1019.67 | 1168.85 | 1468.19 | 1763.54  | 2362.24  | 2958.95  |          |
| .824           | 423.81              | 573.15  | 872.05  | 1021.50 | 1170.95 | 1470.83 | 1766.73  | 2366.52  | 2964.31  |          |
| .825           | 424.45              | 574.17  | 873.61  | 1023.33 | 1173.05 | 1472.48 | 1771.92  | 2370.80  | 2969.67  |          |
| .826           | 425.19              | 575.18  | 875.17  | 1025.16 | 1175.15 | 1475.13 | 1775.11  | 2375.08  | 2975.04  |          |
| .827           | 425.93              | 576.19  | 876.73  | 1026.99 | 1177.25 | 1477.78 | 1778.30  | 2379.36  | 2980.42  |          |
| .828           | 426.68              | 577.21  | 878.29  | 1028.82 | 1179.36 | 1480.43 | 1781.50  | 2383.65  | 2985.80  |          |
| .829           | 427.43              | 578.24  | 879.85  | 1030.65 | 1181.47 | 1483.08 | 1784.70  | 2387.94  | 2991.18  |          |
| .830           | 428.17              | 579.25  | 881.41  | 1032.49 | 1183.58 | 1485.74 | 1787.90  | 2392.23  | 2996.56  |          |
| .831           | 428.91              | 580.26  | 882.97  | 1034.33 | 1185.69 | 1488.39 | 1791.10  | 2396.53  | 3001.95  |          |
| .832           | 429.65              | 581.28  | 884.53  | 1036.17 | 1187.70 | 1491.05 | 1794.30  | 2400.83  | 3007.34  |          |
| .833           | 430.40              | 582.30  | 886.10  | 1038.01 | 1189.81 | 1493.71 | 1797.51  | 2405.13  | 3012.73  |          |
| .834           | 431.15              | 583.32  | 887.67  | 1039.85 | 1191.92 | 1496.37 | 1800.72  | 2409.43  | 3018.13  |          |
| .835           | 431.89              | 584.34  | 889.24  | 1041.69 | 1194.13 | 1499.03 | 1803.93  | 2413.73  | 3023.53  |          |
| .836           | 432.63              | 585.36  | 890.80  | 1043.53 | 1196.24 | 1501.69 | 1807.14  | 2418.04  | 3028.93  |          |
| .837           | 433.37              | 586.38  | 892.37  | 1045.37 | 1198.35 | 1504.35 | 1810.35  | 2422.35  | 3034.34  |          |
| .838           | 434.12              | 587.40  | 893.94  | 1047.21 | 1200.47 | 1507.02 | 1813.56  | 2426.66  | 3039.75  |          |
| .839           | 434.87              | 588.42  | 895.51  | 1049.05 | 1202.59 | 1509.69 | 1816.78  | 2430.97  | 3045.16  |          |
| .840           | 435.62              | 589.44  | 897.08  | 1050.90 | 1204.72 | 1512.36 | 1820.00  | 2435.29  | 3050.57  |          |
| .841           | 436.36              | 590.46  | 898.65  | 1052.74 | 1206.84 | 1515.03 | 1823.22  | 2439.61  | 3055.99  |          |
| .842           | 437.10              | 591.48  | 900.22  | 1054.59 | 1208.96 | 1517.70 | 1826.44  | 2443.93  | 3061.41  |          |
| .843           | 437.85              | 592.50  | 901.79  | 1056.44 | 1211.08 | 1520.37 | 1829.66  | 2448.25  | 3066.83  |          |
| .844           | 438.60              | 593.53  | 903.37  | 1058.29 | 1213.21 | 1523.05 | 1832.89  | 2452.58  | 3072.26  |          |

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|---------|---------|----------|----------|----------|----------|
|                      | 3 Feet.             | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| .845                 | 439.36              | 594.56  | 904.95  | 1060.14 | 1215.34 | 1525.73  | 1836.12  | 2456.91  | 3077.69  |
| .846                 | 440.11              | 595.58  | 906.52  | 1061.99 | 1217.47 | 1528.41  | 1839.35  | 2461.24  | 3083.13  |
| .847                 | 440.86              | 596.60  | 908.10  | 1063.84 | 1219.60 | 1531.09  | 1842.58  | 2465.57  | 3088.53  |
| .848                 | 441.61              | 597.62  | 909.68  | 1065.69 | 1221.73 | 1533.77  | 1845.81  | 2469.91  | 3093.97  |
| .849                 | 442.36              | 598.65  | 911.26  | 1067.54 | 1223.86 | 1536.45  | 1849.05  | 2474.25  | 3099.41  |
| .850                 | 443.11              | 599.68  | 912.84  | 1069.41 | 1225.99 | 1539.14  | 1852.29  | 2478.59  | 3104.89  |
| .851                 | 443.86              | 600.71  | 914.42  | 1071.26 | 1228.12 | 1541.82  | 1855.53  | 2482.93  | 3110.34  |
| .852                 | 444.61              | 601.74  | 916.00  | 1073.12 | 1230.25 | 1544.51  | 1858.77  | 2487.28  | 3115.79  |
| .853                 | 445.36              | 602.77  | 917.58  | 1074.98 | 1232.38 | 1547.20  | 1862.01  | 2491.63  | 3121.25  |
| .854                 | 446.11              | 603.80  | 919.16  | 1076.84 | 1234.52 | 1549.89  | 1865.25  | 2495.98  | 3126.71  |
| .855                 | 446.87              | 604.83  | 920.74  | 1078.70 | 1236.66 | 1552.58  | 1868.50  | 2500.33  | 3132.17  |
| .856                 | 447.62              | 605.86  | 922.32  | 1080.56 | 1238.80 | 1555.27  | 1871.75  | 2504.69  | 3137.64  |
| .857                 | 448.37              | 606.89  | 923.90  | 1082.32 | 1240.94 | 1557.96  | 1875.00  | 2509.05  | 3143.11  |
| .858                 | 449.12              | 607.92  | 925.49  | 1084.18 | 1243.08 | 1560.66  | 1878.25  | 2513.41  | 3148.58  |
| .859                 | 449.87              | 608.95  | 927.08  | 1086.05 | 1245.22 | 1563.36  | 1881.50  | 2517.77  | 3154.05  |
| .860                 | 450.63              | 609.98  | 928.67  | 1088.02 | 1247.37 | 1566.06  | 1884.75  | 2522.14  | 3159.53  |
| .861                 | 451.38              | 610.01  | 930.26  | 1089.88 | 1249.51 | 1568.76  | 1888.01  | 2526.51  | 3165.01  |
| .862                 | 452.13              | 611.04  | 932.85  | 1091.75 | 1251.65 | 1571.46  | 1891.27  | 2530.88  | 3170.49  |
| .863                 | 452.89              | 612.07  | 934.45  | 1093.62 | 1253.80 | 1574.16  | 1894.53  | 2535.25  | 3175.98  |
| .864                 | 453.65              | 613.11  | 936.04  | 1095.49 | 1255.85 | 1576.87  | 1897.79  | 2539.63  | 3181.47  |
| .865                 | 454.41              | 615.15  | 936.62  | 1097.36 | 1258.10 | 1579.58  | 1901.05  | 2544.01  | 3186.96  |
| .866                 | 455.16              | 616.18  | 938.21  | 1099.23 | 1260.25 | 1582.29  | 1904.32  | 2548.39  | 3192.46  |
| .867                 | 455.91              | 617.21  | 939.80  | 1101.10 | 1262.40 | 1585.00  | 1907.59  | 2552.77  | 3197.96  |
| .868                 | 456.67              | 618.25  | 941.39  | 1102.97 | 1264.55 | 1587.71  | 1910.86  | 2557.15  | 3203.46  |
| .869                 | 457.43              | 619.29  | 942.98  | 1104.85 | 1266.70 | 1590.42  | 1914.13  | 2561.54  | 3208.96  |
| .870                 | 458.19              | 620.33  | 944.59  | 1106.73 | 1268.86 | 1593.13  | 1917.40  | 2565.93  | 3214.47  |
| .871                 | 458.94              | 621.36  | 946.18  | 1108.60 | 1271.01 | 1595.84  | 1920.67  | 2570.32  | 3219.98  |
| .872                 | 459.71              | 622.40  | 947.78  | 1110.48 | 1273.17 | 1598.56  | 1923.95  | 2574.72  | 3225.50  |
| .873                 | 460.46              | 623.44  | 949.38  | 1112.36 | 1275.33 | 1601.28  | 1927.23  | 2579.12  | 3231.02  |
| .874                 | 461.22              | 624.48  | 950.98  | 1114.24 | 1277.49 | 1604.00  | 1930.51  | 2583.52  | 3236.54  |
| .875                 | 461.98              | 625.52  | 952.58  | 1116.12 | 1279.65 | 1606.72  | 1933.79  | 2587.92  | 3242.06  |
| .876                 | 462.74              | 626.56  | 954.18  | 1118.00 | 1281.81 | 1609.44  | 1937.07  | 2592.33  | 3247.59  |
| .877                 | 463.50              | 627.60  | 955.78  | 1119.88 | 1283.97 | 1612.16  | 1940.35  | 2596.74  | 3253.12  |
| .878                 | 464.26              | 628.64  | 957.38  | 1121.76 | 1285.13 | 1614.89  | 1943.64  | 2600.75  | 3258.65  |
| .879                 | 465.02              | 629.68  | 958.99  | 1123.64 | 1287.30 | 1617.62  | 1946.93  | 2605.16  | 3264.18  |
| .880                 | 465.78              | 630.72  | 960.60  | 1125.53 | 1290.47 | 1620.35  | 1950.22  | 2609.97  | 3269.72  |
| .881                 | 466.54              | 631.76  | 962.20  | 1127.38 | 1292.64 | 1623.08  | 1953.51  | 2614.39  | 3275.26  |
| .882                 | 467.30              | 632.80  | 963.80  | 1129.27 | 1294.81 | 1625.81  | 1956.81  | 2618.81  | 3280.81  |
| .883                 | 468.06              | 633.84  | 965.40  | 1131.16 | 1296.98 | 1628.54  | 1960.11  | 2623.23  | 3286.36  |
| .884                 | 468.82              | 634.89  | 967.00  | 1133.05 | 1299.15 | 1631.27  | 1963.41  | 2627.65  | 3291.91  |
| .885                 | 469.59              | 635.94  | 968.63  | 1134.97 | 1301.32 | 1634.01  | 1966.70  | 2632.08  | 3297.46  |
| .886                 | 470.35              | 636.98  | 970.24  | 1136.86 | 1303.49 | 1636.75  | 1970.00  | 2636.51  | 3303.02  |
| .887                 | 471.11              | 638.02  | 971.85  | 1138.75 | 1305.66 | 1639.49  | 1973.30  | 2640.94  | 3308.58  |
| .888                 | 471.87              | 639.07  | 973.46  | 1140.64 | 1307.83 | 1642.23  | 1976.60  | 2645.37  | 3314.14  |
| .889                 | 472.64              | 640.12  | 975.07  | 1142.54 | 1310.01 | 1644.97  | 1979.91  | 2649.81  | 3319.71  |
| .890                 | 473.41              | 641.17  | 976.68  | 1144.44 | 1312.19 | 1647.71  | 1983.22  | 2654.25  | 3325.28  |
| .891                 | 474.17              | 642.21  | 979.90  | 1146.33 | 1314.37 | 1650.45  | 1986.53  | 2658.76  | 3330.85  |
| .892                 | 474.93              | 643.25  | 971.51  | 1148.23 | 1316.55 | 1653.19  | 1989.84  | 2663.28  | 3336.45  |
| .893                 | 475.70              | 644.30  | 973.12  | 1150.13 | 1318.73 | 1655.93  | 1993.16  | 2667.80  | 3342.03  |
| .894                 | 476.47              | 645.35  | 974.14  | 1152.03 | 1320.91 | 1658.61  | 1996.48  | 2672.32  | 3347.61  |
| .895                 | 477.24              | 646.41  | 984.75  | 1153.93 | 1323.10 | 1661.44  | 1999.80  | 2676.84  | 3353.17  |
| .896                 | 478.00              | 647.46  | 986.37  | 1155.83 | 1325.28 | 1664.19  | 2003.12  | 2680.93  | 3358.76  |
| .897                 | 478.76              | 648.51  | 987.99  | 1157.73 | 1327.46 | 1666.94  | 2006.44  | 2685.39  | 3364.35  |
| .898                 | 479.54              | 649.56  | 989.61  | 1159.63 | 1329.65 | 1669.70  | 2009.76  | 2689.85  | 3369.94  |
| .899                 | 480.31              | 650.61  | 991.23  | 1161.53 | 1331.84 | 1672.46  | 2013.08  | 2694.31  | 3375.50  |
| .900                 | 481.07              | 651.66  | 992.85  | 1163.44 | 1334.03 | 1675.22  | 2016.40  | 2698.77  | 3381.14  |
| .901                 | 481.83              | 652.71  | 994.47  | 1165.34 | 1336.22 | 1677.98  | 2019.73  | 2703.24  | 3386.74  |
| .902                 | 482.60              | 653.76  | 996.09  | 1167.25 | 1338.41 | 1680.74  | 2023.06  | 2708.71  | 3392.35  |

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|---------|---------|---------|----------|----------|----------|----------|
|                      | Feet.               | 3 Feet. | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| .903                 | 483.37              | 654.81  | 997.71  | 1169.16 | 1340.60 | 1683.50 | 2026.39  | 2713.18  | 3397.96  |          |
| .904                 | 484.14              | 655.87  | 999.33  | 1171.07 | 1342.79 | 1686.26 | 2029.72  | 2717.65  | 3403.57  |          |
| .905                 | 484.91              | 656.93  | 1000.96 | 1172.98 | 1344.99 | 1689.02 | 2033.05  | 2721.12  | 3409.18  |          |
| .906                 | 485.68              | 657.98  | 1002.58 | 1174.89 | 1347.18 | 1691.79 | 2036.39  | 2725.60  | 3414.80  |          |
| .907                 | 486.45              | 659.03  | 1004.20 | 1176.80 | 1349.38 | 1694.56 | 2039.73  | 2730.08  | 3420.42  |          |
| .908                 | 487.22              | 660.09  | 1005.83 | 1178.71 | 1351.58 | 1697.33 | 2043.07  | 2734.56  | 3425.04  |          |
| .909                 | 487.99              | 661.15  | 1007.46 | 1180.62 | 1353.78 | 1700.10 | 2047.41  | 2739.04  | 3431.66  |          |
| .910                 | 488.76              | 662.21  | 1009.09 | 1182.54 | 1355.98 | 1702.87 | 2049.75  | 2743.53  | 3437.30  |          |
| .911                 | 489.53              | 663.26  | 1010.72 | 1184.45 | 1358.18 | 1705.64 | 2053.09  | 2748.02  | 3442.93  |          |
| .912                 | 490.30              | 664.32  | 1012.35 | 1186.36 | 1360.38 | 1708.41 | 2056.44  | 2752.51  | 3448.57  |          |
| .913                 | 491.07              | 665.38  | 1013.98 | 1188.28 | 1362.58 | 1711.19 | 2059.79  | 2757.00  | 3454.21  |          |
| .914                 | 491.84              | 666.44  | 1015.61 | 1190.28 | 1364.79 | 1713.97 | 2063.14  | 2761.49  | 3459.85  |          |
| .915                 | 492.62              | 667.50  | 1017.25 | 1192.12 | 1367.00 | 1716.75 | 2066.49  | 2765.99  | 3465.49  |          |
| .916                 | 493.39              | 668.56  | 1018.88 | 1194.04 | 1369.20 | 1719.53 | 2069.84  | 2770.49  | 3471.14  |          |
| .917                 | 494.16              | 669.62  | 1020.51 | 1195.96 | 1371.41 | 1722.31 | 2073.20  | 2774.99  | 3476.79  |          |
| .918                 | 494.93              | 670.68  | 1022.14 | 1197.88 | 1373.62 | 1725.09 | 2076.56  | 2779.50  | 3482.44  |          |
| .919                 | 495.71              | 671.74  | 1024.78 | 1199.80 | 1375.83 | 1727.87 | 2079.92  | 2784.01  | 3488.10  |          |
| .920                 | 496.49              | 672.80  | 1025.42 | 1201.73 | 1378.04 | 1730.66 | 2083.28  | 2788.52  | 3493.76  |          |
| .921                 | 497.26              | 673.86  | 1027.05 | 1203.65 | 1380.25 | 1733.45 | 2086.64  | 2793.03  | 3499.42  |          |
| .922                 | 498.03              | 674.92  | 1028.69 | 1205.57 | 1382.46 | 1736.24 | 2090.00  | 2797.55  | 3505.09  |          |
| .923                 | 498.80              | 675.98  | 1030.33 | 1207.50 | 1384.67 | 1739.03 | 2093.37  | 2802.07  | 3510.76  |          |
| .924                 | 499.58              | 677.05  | 1031.97 | 1209.43 | 1386.89 | 1741.82 | 2096.74  | 2806.59  | 3516.43  |          |
| .925                 | 500.36              | 678.12  | 1033.61 | 1211.36 | 1389.11 | 1744.61 | 2100.11  | 2811.11  | 3522.10  |          |
| .926                 | 501.13              | 679.18  | 1035.25 | 1213.29 | 1391.33 | 1747.40 | 2103.48  | 2815.63  | 3527.78  |          |
| .927                 | 501.91              | 680.24  | 1036.89 | 1215.22 | 1393.55 | 1751.20 | 2106.85  | 2820.16  | 3533.48  |          |
| .928                 | 502.69              | 681.30  | 1038.53 | 1217.15 | 1395.77 | 1754.00 | 2110.22  | 2824.69  | 3539.16  |          |
| .929                 | 503.47              | 681.37  | 1040.17 | 1219.08 | 1397.99 | 1756.80 | 2113.60  | 2829.23  | 3544.85  |          |
| .930                 | 504.25              | 683.44  | 1041.82 | 1221.02 | 1400.21 | 1758.60 | 2116.98  | 2833.75  | 3550.52  |          |
| .931                 | 505.02              | 684.50  | 1043.46 | 1222.95 | 1402.43 | 1761.40 | 2120.30  | 2838.29  | 3556.21  |          |
| .932                 | 505.80              | 685.57  | 1045.11 | 1224.88 | 1404.65 | 1764.20 | 2123.68  | 2842.83  | 3561.91  |          |
| .933                 | 506.58              | 686.64  | 1046.76 | 1226.82 | 1406.88 | 1767.00 | 2127.06  | 2847.37  | 3567.61  |          |
| .934                 | 507.36              | 687.73  | 1048.41 | 1228.76 | 1409.11 | 1769.81 | 2130.45  | 2851.91  | 3573.31  |          |
| .935                 | 508.14              | 688.78  | 1050.06 | 1230.70 | 1411.34 | 1772.62 | 2133.90  | 2856.45  | 3579.01  |          |
| .936                 | 508.92              | 689.85  | 1051.71 | 1232.64 | 1413.57 | 1775.43 | 2137.29  | 2861.00  | 3584.72  |          |
| .937                 | 509.70              | 690.92  | 1053.36 | 1234.58 | 1415.80 | 1778.24 | 2140.68  | 2865.55  | 3590.43  |          |
| .938                 | 510.48              | 691.99  | 1055.01 | 1236.52 | 1418.03 | 1781.05 | 2144.07  | 2870.10  | 3596.14  |          |
| .939                 | 511.26              | 693.06  | 1056.66 | 1238.46 | 1420.26 | 1783.86 | 2147.46  | 2874.66  | 3601.86  |          |
| .940                 | 512.04              | 694.13  | 1058.31 | 1240.40 | 1422.49 | 1786.67 | 2150.85  | 2879.22  | 3607.58  |          |
| .941                 | 512.82              | 695.20  | 1059.96 | 1242.34 | 1424.72 | 1789.48 | 2154.25  | 2883.78  | 3613.30  |          |
| .942                 | 513.60              | 696.27  | 1061.61 | 1244.38 | 1426.95 | 1792.30 | 2157.65  | 2888.34  | 3619.03  |          |
| .943                 | 514.38              | 697.34  | 1063.26 | 1246.23 | 1429.19 | 1795.12 | 2161.05  | 2892.90  | 3624.76  |          |
| .944                 | 515.16              | 698.41  | 1064.92 | 1248.18 | 1431.43 | 1797.14 | 2164.45  | 2897.46  | 3630.49  |          |
| .945                 | 515.95              | 699.49  | 1066.58 | 1250.13 | 1433.67 | 1800.76 | 2167.85  | 2902.03  | 3636.22  |          |
| .946                 | 516.73              | 700.56  | 1068.23 | 1252.18 | 1435.91 | 1803.58 | 2171.26  | 2906.60  | 3641.96  |          |
| .947                 | 517.51              | 701.63  | 1069.89 | 1254.13 | 1438.15 | 1806.40 | 2174.67  | 2911.17  | 3647.70  |          |
| .948                 | 518.29              | 702.71  | 1071.55 | 1256.08 | 1440.39 | 1809.23 | 2178.08  | 2915.75  | 3653.44  |          |
| .949                 | 519.07              | 703.79  | 1073.21 | 1258.03 | 1442.63 | 1812.06 | 2181.49  | 2920.33  | 3659.18  |          |
| .950                 | 519.86              | 704.87  | 1074.87 | 1259.88 | 1444.88 | 1814.89 | 2184.90  | 2924.91  | 3664.93  |          |
| .951                 | 520.64              | 705.94  | 1076.53 | 1261.13 | 1447.12 | 1817.72 | 2188.31  | 2929.49  | 3670.68  |          |
| .952                 | 521.42              | 707.01  | 1078.19 | 1263.08 | 1449.36 | 1820.55 | 2191.72  | 2934.07  | 3676.43  |          |
| .953                 | 522.20              | 708.09  | 1079.85 | 1265.03 | 1451.61 | 1823.38 | 2195.14  | 2938.65  | 3682.19  |          |
| .954                 | 522.99              | 709.17  | 1081.51 | 1266.99 | 1453.86 | 1826.21 | 2198.56  | 2943.24  | 3687.95  |          |
| .955                 | 523.78              | 710.25  | 1083.18 | 1269.65 | 1456.11 | 1829.05 | 2201.98  | 2947.85  | 3693.71  |          |
| .956                 | 524.56              | 711.33  | 1084.84 | 1271.61 | 1458.36 | 1831.88 | 2205.40  | 2952.44  | 3699.48  |          |
| .957                 | 525.34              | 712.41  | 1086.50 | 1273.57 | 1460.61 | 1834.72 | 2208.82  | 2957.04  | 3705.25  |          |
| .958                 | 526.13              | 713.49  | 1088.17 | 1275.53 | 1462.86 | 1837.56 | 2212.25  | 2961.64  | 3711.02  |          |
| .959                 | 526.92              | 714.57  | 1089.84 | 1277.49 | 1465.12 | 1840.40 | 2215.68  | 2966.24  | 3716.79  |          |
| .960                 | 527.71              | 715.65  | 1091.51 | 1279.45 | 1467.38 | 1843.24 | 2219.11  | 2970.84  | 3722.57  |          |



| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |         |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|---------|---------|---------|----------|----------|----------|----------|
|                      | Feet.               | 3 Feet. | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| .961                 | 528.49              | 716.73  | 1093.18 | 1281.41 | 1469.63 | 1846.08 | 2222.54  | 2975.45  | 3728.35  |          |
| .962                 | 529.28              | 717.81  | 1094.85 | 1283.37 | 1471.89 | 1848.92 | 2225.97  | 2980.06  | 3734.13  |          |
| .963                 | 530.07              | 718.89  | 1096.52 | 1285.33 | 1474.15 | 1851.77 | 2229.40  | 2984.67  | 3739.92  |          |
| .964                 | 530.86              | 719.97  | 1098.20 | 1287.30 | 1476.41 | 1854.62 | 2232.84  | 2989.28  | 3745.71  |          |
| .965                 | 531.65              | 721.06  | 1099.86 | 1289.27 | 1478.67 | 1857.47 | 2236.28  | 2993.89  | 3751.50  |          |
| .966                 | 532.44              | 722.14  | 1101.53 | 1291.23 | 1480.93 | 1860.32 | 2239.72  | 2998.51  | 3757.30  |          |
| .967                 | 533.23              | 723.22  | 1102.60 | 1293.20 | 1483.19 | 1863.17 | 2243.16  | 3003.13  | 3763.10  |          |
| .968                 | 534.02              | 724.30  | 1104.27 | 1295.17 | 1485.45 | 1866.02 | 2246.60  | 3007.75  | 3768.90  |          |
| .969                 | 534.81              | 725.39  | 1105.95 | 1297.14 | 1487.71 | 1868.88 | 2250.04  | 3012.37  | 3774.70  |          |
| .970                 | 535.60              | 726.48  | 1108.23 | 1299.11 | 1489.98 | 1871.74 | 2253.49  | 3017.00  | 3780.50  |          |
| .971                 | 536.59              | 727.56  | 1109.90 | 1301.08 | 1492.25 | 1874.60 | 2256.94  | 3021.63  | 3786.31  |          |
| .972                 | 537.38              | 728.64  | 1111.58 | 1303.05 | 1494.52 | 1877.46 | 2260.39  | 3026.26  | 3792.12  |          |
| .973                 | 538.18              | 729.73  | 1113.18 | 1305.02 | 1496.79 | 1880.32 | 2263.84  | 3030.89  | 3797.94  |          |
| .974                 | 538.97              | 730.82  | 1114.86 | 1306.99 | 1499.06 | 1883.18 | 2267.29  | 3035.52  | 3803.76  |          |
| .975                 | 539.55              | 731.91  | 1116.62 | 1308.97 | 1501.33 | 1886.04 | 2270.74  | 3040.16  | 3809.58  |          |
| .976                 | 540.34              | 732.99  | 1118.30 | 1310.94 | 1503.60 | 1888.90 | 2274.20  | 3044.80  | 3815.41  |          |
| .977                 | 541.13              | 734.08  | 1119.90 | 1312.92 | 1505.87 | 1891.76 | 2277.66  | 3049.44  | 3821.24  |          |
| .978                 | 541.92              | 735.17  | 1121.66 | 1314.90 | 1508.14 | 1894.63 | 2281.12  | 3054.09  | 3827.07  |          |
| .979                 | 542.72              | 736.26  | 1123.34 | 1316.88 | 1510.42 | 1897.50 | 2284.58  | 3058.74  | 3832.90  |          |
| .980                 | 543.52              | 737.36  | 1125.02 | 1318.86 | 1512.70 | 1900.37 | 2288.04  | 3063.39  | 3838.73  |          |
| .981                 | 544.31              | 738.44  | 1126.70 | 1320.84 | 1514.97 | 1903.24 | 2291.50  | 3068.05  | 3844.57  |          |
| .982                 | 545.10              | 739.53  | 1128.38 | 1322.82 | 1517.25 | 1906.11 | 2294.97  | 3072.71  | 3850.41  |          |
| .983                 | 545.89              | 740.62  | 1130.07 | 1323.80 | 1519.53 | 1908.98 | 2298.44  | 3077.37  | 3856.25  |          |
| .984                 | 546.69              | 741.71  | 1131.76 | 1325.73 | 1521.81 | 1911.86 | 2301.91  | 3082.03  | 3862.09  |          |
| .985                 | 547.49              | 742.81  | 1133.45 | 1328.77 | 1524.09 | 1914.74 | 2305.38  | 3086.66  | 3867.95  |          |
| .986                 | 548.28              | 743.90  | 1135.13 | 1330.75 | 1526.37 | 1917.62 | 2308.85  | 3091.32  | 3873.80  |          |
| .987                 | 549.07              | 744.99  | 1136.82 | 1332.73 | 1528.65 | 1920.50 | 2312.33  | 3095.99  | 3879.66  |          |
| .988                 | 549.86              | 746.08  | 1138.51 | 1334.72 | 1530.94 | 1923.38 | 2315.81  | 3100.66  | 3885.22  |          |
| .989                 | 550.66              | 747.17  | 1140.20 | 1336.71 | 1533.23 | 1926.26 | 2319.29  | 3105.33  | 3891.38  |          |
| .990                 | 551.46              | 748.27  | 1141.89 | 1338.70 | 1535.52 | 1929.14 | 2322.76  | 3110.00  | 3897.24  |          |
| .991                 | 552.25              | 749.36  | 1143.58 | 1340.69 | 1537.80 | 1932.02 | 2326.24  | 3114.67  | 3903.11  |          |
| .992                 | 553.05              | 750.45  | 1145.27 | 1342.68 | 1540.09 | 1934.90 | 2329.72  | 3119.35  | 3908.98  |          |
| .993                 | 553.85              | 751.55  | 1146.96 | 1344.67 | 1542.38 | 1937.79 | 2333.20  | 3124.03  | 3914.85  |          |
| .994                 | 554.65              | 752.65  | 1148.66 | 1346.66 | 1544.67 | 1940.68 | 2336.69  | 3128.71  | 3920.72  |          |
| .995                 | 555.45              | 753.75  | 1150.36 | 1348.66 | 1546.96 | 1943.57 | 2340.18  | 3133.39  | 3926.60  |          |
| .996                 | 556.24              | 754.84  | 1152.05 | 1350.65 | 1549.25 | 1946.46 | 2343.67  | 3138.08  | 3932.48  |          |
| .997                 | 557.04              | 755.94  | 1153.74 | 1352.64 | 1551.54 | 1949.35 | 2347.16  | 3142.77  | 3938.37  |          |
| .998                 | 557.84              | 757.04  | 1155.44 | 1354.64 | 1553.84 | 1952.24 | 2350.65  | 3147.40  | 3944.26  |          |
| .999                 | 558.64              | 758.14  | 1157.14 | 1356.64 | 1556.14 | 1955.14 | 2354.14  | 3152.09  | 3950.15  |          |
| 1.000                | 559.44              | 759.24  | 1158.84 | 1358.64 | 1558.44 | 1958.04 | 2357.64  | 3156.84  | 3956.04  |          |
| 1.001                | .....               | 760.34  | 1160.54 | 1360.64 | 1560.74 | 1960.94 | 2361.14  | 3161.54  | 3961.94  |          |
| 1.002                | .....               | 761.44  | 1162.24 | 1362.64 | 1563.04 | 1963.84 | 2364.64  | 3166.24  | 3967.84  |          |
| 1.003                | .....               | 762.54  | 1163.94 | 1364.64 | 1565.34 | 1966.74 | 2368.14  | 3170.94  | 3973.74  |          |
| 1.004                | .....               | 763.64  | 1165.64 | 1366.64 | 1567.64 | 1969.64 | 2371.64  | 3175.64  | 3979.64  |          |
| 1.005                | .....               | 764.74  | 1167.34 | 1368.64 | 1569.94 | 1972.54 | 2375.14  | 3180.34  | 3985.55  |          |
| 1.006                | .....               | 765.84  | 1169.04 | 1370.64 | 1572.24 | 1975.44 | 2378.65  | 3185.05  | 3991.46  |          |
| 1.007                | .....               | 766.94  | 1170.74 | 1372.64 | 1574.54 | 1978.35 | 2382.16  | 3189.76  | 3997.37  |          |
| 1.008                | .....               | 768.04  | 1172.44 | 1374.64 | 1576.85 | 1981.26 | 2385.67  | 3194.47  | 4003.28  |          |
| 1.009                | .....               | 769.14  | 1174.19 | 1376.65 | 1578.16 | 1984.17 | 2389.18  | 3199.18  | 4009.20  |          |
| 1.010                | .....               | 770.25  | 1175.86 | 1378.66 | 1581.47 | 1987.08 | 2392.69  | 3203.90  | 4015.12  |          |
| 1.011                | .....               | 771.35  | 1177.56 | 1380.66 | 1583.78 | 1989.99 | 2396.20  | 3208.34  | 4021.05  |          |
| 1.012                | .....               | 772.45  | 1179.27 | 1382.67 | 1586.09 | 1992.90 | 2399.71  | 3213.06  | 4026.98  |          |
| 1.013                | .....               | 773.55  | 1180.98 | 1384.68 | 1588.40 | 1995.81 | 2403.23  | 3217.78  | 4032.91  |          |
| 1.014                | .....               | 774.66  | 1182.69 | 1386.69 | 1590.71 | 1998.73 | 2406.75  | 3222.51  | 4038.84  |          |
| 1.015                | .....               | 775.77  | 1184.40 | 1388.71 | 1593.02 | 2001.65 | 2410.27  | 3227.22  | 4044.77  |          |
| 1.016                | .....               | 776.87  | 1186.11 | 1390.72 | 1595.33 | 2004.57 | 2413.79  | 3232.25  | 4050.71  |          |
| 1.017                | .....               | 777.97  | 1187.82 | 1392.73 | 1597.64 | 2007.49 | 2417.31  | 3236.98  | 4056.65  |          |
| 1.018                | .....               | 779.08  | 1189.53 | 1394.74 | 1599.96 | 2010.41 | 2420.84  | 3241.71  | 4062.59  |          |

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |         |         |          |          |          |
|----------------------|---------------------|---------|---------|---------|---------|----------|----------|----------|
|                      | Feet.               | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. |
| 1.019                | 780.19              | 1191.24 | 1396.76 | 1602.28 | 2013.33 | 2424.37  | 3246.45  | 4068.54  |
| 1.020                | 781.30              | 1192.95 | 1398.78 | 1604.60 | 2016.25 | 2427.90  | 3251.19  | 4074.49  |
| 1.021                | 782.41              | 1194.66 | 1400.79 | 1606.92 | 2019.15 | 2431.43  | 3255.93  | 4080.44  |
| 1.022                | 783.52              | 1196.37 | 1402.81 | 1609.24 | 2022.06 | 2434.96  | 3260.67  | 4086.40  |
| 1.023                | 784.63              | 1198.09 | 1404.83 | 1611.56 | 2024.97 | 2438.49  | 3265.42  | 4092.36  |
| 1.024                | 785.74              | 1199.81 | 1406.85 | 1613.88 | 2027.88 | 2442.02  | 3270.17  | 4098.32  |
| 1.025                | 786.85              | 1201.53 | 1408.87 | 1616.21 | 2030.89 | 2445.56  | 3274.92  | 4104.28  |
| 1.026                | 787.96              | 1203.24 | 1410.89 | 1618.53 | 2033.82 | 2449.10  | 3279.67  | 4110.25  |
| 1.027                | 789.07              | 1204.96 | 1412.91 | 1620.85 | 2036.75 | 2452.64  | 3284.32  | 4116.22  |
| 1.028                | 790.18              | 1206.68 | 1414.93 | 1623.18 | 2039.88 | 2456.18  | 3289.18  | 4122.19  |
| 1.029                | 791.28              | 1208.40 | 1416.95 | 1625.51 | 2042.82 | 2459.72  | 3293.94  | 4128.16  |
| 1.030                | 792.40              | 1210.12 | 1418.98 | 1627.84 | 2045.56 | 2463.27  | 3298.70  | 4134.14  |
| 1.031                | 793.51              | 1211.84 | 1421.00 | 1630.17 | 2048.50 | 2466.82  | 3303.46  | 4140.12  |
| 1.032                | 794.62              | 1213.56 | 1423.03 | 1632.50 | 2051.44 | 2470.37  | 3308.23  | 4146.10  |
| 1.033                | 795.73              | 1215.28 | 1425.05 | 1634.83 | 2054.38 | 2473.92  | 3313.00  | 4152.09  |
| 1.034                | 796.84              | 1217.01 | 1427.07 | 1637.16 | 2057.32 | 2477.47  | 3317.77  | 4158.08  |
| 1.035                | 797.96              | 1218.74 | 1429.12 | 1639.50 | 2060.26 | 2481.02  | 3322.54  | 4164.07  |
| 1.036                | 799.07              | 1220.46 | 1431.15 | 1641.83 | 2063.20 | 2484.57  | 3327.32  | 4170.06  |
| 1.037                | 800.19              | 1222.18 | 1433.18 | 1644.16 | 2066.14 | 2488.13  | 3332.10  | 4176.06  |
| 1.038                | 801.31              | 1223.91 | 1435.21 | 1646.50 | 2069.09 | 2491.69  | 3336.88  | 4182.06  |
| 1.039                | 802.43              | 1225.64 | 1437.24 | 1648.84 | 2072.04 | 2495.25  | 3341.66  | 4188.06  |
| 1.040                | 803.55              | 1227.37 | 1439.27 | 1651.18 | 2074.99 | 2498.81  | 3346.44  | 4194.06  |
| 1.041                | 804.66              | 1229.10 | 1441.30 | 1653.52 | 2077.94 | 2502.37  | 3351.22  | 4200.07  |
| 1.042                | 805.78              | 1230.83 | 1443.33 | 1655.86 | 2080.89 | 2505.93  | 3356.01  | 4206.08  |
| 1.043                | 806.90              | 1232.56 | 1445.37 | 1658.20 | 2083.84 | 2509.50  | 3360.80  | 4212.09  |
| 1.044                | 808.02              | 1234.29 | 1447.41 | 1660.54 | 2086.80 | 2513.07  | 3365.59  | 4218.11  |
| 1.045                | 809.14              | 1236.02 | 1449.45 | 1662.89 | 2089.76 | 2516.64  | 3370.38  | 4224.13  |
| 1.046                | 810.15              | 1237.75 | 1451.49 | 1665.26 | 2092.72 | 2520.21  | 3375.18  | 4030.15  |
| 1.047                | 811.27              | 1239.48 | 1453.53 | 1667.57 | 2095.68 | 2523.78  | 3379.98  | 4036.18  |
| 1.048                | 812.39              | 1241.21 | 1455.57 | 1669.92 | 2098.64 | 2527.35  | 3384.78  | 4042.21  |
| 1.049                | 813.41              | 1242.94 | 1457.61 | 1672.27 | 2101.60 | 2530.93  | 3389.58  | 4048.24  |
| 1.050                | 814.73              | 1244.68 | 1459.65 | 1674.62 | 2104.56 | 2534.51  | 3394.39  | 4254.27  |
| 1.051                | 815.85              | 1246.41 | 1461.69 | 1676.97 | 2107.52 | 2538.09  | 3399.20  | 4260.31  |
| 1.052                | 816.97              | 1248.14 | 1463.73 | 1679.32 | 2110.49 | 2541.67  | 3404.01  | 4266.35  |
| 1.053                | 818.09              | 1249.88 | 1465.77 | 1681.67 | 2113.46 | 2545.25  | 3408.82  | 4272.39  |
| 1.054                | 819.21              | 1251.62 | 1467.82 | 1684.02 | 2116.43 | 2548.83  | 3413.63  | 4278.43  |
| 1.055                | 820.34              | 1253.36 | 1469.87 | 1686.38 | 2119.40 | 2552.41  | 3418.45  | 4284.48  |
| 1.056                | 821.46              | 1255.10 | 1471.92 | 1688.73 | 2122.37 | 2556.00  | 3423.27  | 4290.53  |
| 1.057                | 822.58              | 1256.84 | 1473.97 | 1691.09 | 2125.34 | 2559.59  | 3428.09  | 4296.58  |
| 1.058                | 823.71              | 1258.58 | 1476.02 | 1693.45 | 2128.31 | 2563.18  | 3432.91  | 4302.63  |
| 1.059                | 824.84              | 1260.32 | 1478.07 | 1695.81 | 2131.28 | 2566.77  | 3437.73  | 4308.69  |
| 1.060                | 825.97              | 1262.07 | 1480.12 | 1698.17 | 2134.26 | 2570.36  | 3442.56  | 4314.75  |
| 1.061                | 827.09              | 1263.81 | 1482.17 | 1700.53 | 2137.24 | 2573.95  | 3447.39  | 4320.82  |
| 1.062                | 828.21              | 1265.55 | 1484.22 | 1702.89 | 2140.22 | 2577.55  | 3452.22  | 4326.89  |
| 1.063                | 829.34              | 1267.29 | 1486.27 | 1705.25 | 2143.20 | 2581.15  | 3457.05  | 4332.96  |
| 1.064                | 830.47              | 1269.04 | 1488.32 | 1707.61 | 2146.18 | 2584.75  | 3461.89  | 4339.03  |
| 1.065                | 831.60              | 1270.79 | 1490.38 | 1709.98 | 2149.16 | 2588.35  | 3466.73  | 4345.10  |
| 1.066                | 832.72              | 1272.53 | 1492.43 | 1712.34 | 2152.14 | 2591.95  | 3471.57  | 4351.18  |
| 1.067                | 833.85              | 1274.28 | 1494.49 | 1714.70 | 2155.13 | 2595.55  | 3476.41  | 4357.26  |
| 1.068                | 834.98              | 1276.03 | 1496.55 | 1717.07 | 2158.12 | 2599.16  | 3481.25  | 4363.34  |
| 1.069                | 836.11              | 1277.78 | 1498.61 | 1719.44 | 2161.11 | 2602.77  | 3486.10  | 4369.42  |
| 1.070                | 837.24              | 1279.53 | 1500.67 | 1721.81 | 2164.10 | 2606.38  | 3490.95  | 4375.51  |
| 1.071                | 838.37              | 1281.28 | 1502.73 | 1724.18 | 2167.09 | 2609.99  | 3495.80  | 4381.60  |
| 1.072                | 839.50              | 1283.03 | 1504.79 | 1726.55 | 2170.08 | 2613.60  | 3500.65  | 4387.70  |
| 1.073                | 840.63              | 1284.78 | 1506.85 | 1728.92 | 2173.07 | 2617.21  | 3505.50  | 4393.80  |
| 1.074                | 841.76              | 1286.53 | 1508.91 | 1731.29 | 2176.06 | 2620.83  | 3510.36  | 4399.90  |
| 1.075                | 842.89              | 1288.28 | 1510.98 | 1733.67 | 2179.06 | 2624.45  | 3515.22  | 4406.00  |
| 1.076                | 844.02              | 1290.03 | 1513.04 | 1736.04 | 2182.06 | 2628.07  | 3520.08  | 4412.11  |



| Depth on Weir. | LENGTH OF THE WEIR. |         |         |         |         |          |          |          |
|----------------|---------------------|---------|---------|---------|---------|----------|----------|----------|
|                | Feet.               | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. |
| 1.077          | 845.15              | 1291.78 | 1515.10 | 1738.42 | 2185.06 | 2631.69  | 3524.94  | 4418.22  |
| 1.078          | 846.28              | 1293.33 | 1517.17 | 1740.80 | 2188.06 | 2635.31  | 3529.81  | 4424.33  |
| 1.079          | 847.41              | 1295.28 | 1519.24 | 1743.18 | 2191.06 | 2638.93  | 3534.68  | 4430.44  |
| 1.080          | 848.55              | 1297.06 | 1521.31 | 1745.56 | 2194.06 | 2642.55  | 3539.55  | 4436.55  |
| 1.081          | 849.68              | 1298.81 | 1523.38 | 1747.94 | 2197.06 | 2646.18  | 3544.43  | 4442.67  |
| 1.082          | 850.81              | 1300.57 | 1525.45 | 1750.32 | 2200.06 | 2649.81  | 3549.30  | 4448.79  |
| 1.083          | 851.95              | 1302.33 | 1527.52 | 1752.70 | 2203.06 | 2653.44  | 3554.17  | 4454.91  |
| 1.084          | 853.09              | 1304.09 | 1529.59 | 1755.08 | 2206.07 | 2657.07  | 3559.04  | 4461.04  |
| 1.085          | 854.23              | 1305.85 | 1531.66 | 1757.47 | 2209.08 | 2660.70  | 3563.93  | 4467.17  |
| 1.086          | 855.36              | 1307.61 | 1533.73 | 1759.85 | 2212.09 | 2664.33  | 3568.81  | 4473.30  |
| 1.087          | 856.49              | 1309.37 | 1535.80 | 1762.23 | 2215.10 | 2667.97  | 3573.70  | 4479.43  |
| 1.088          | 857.63              | 1311.13 | 1537.87 | 1764.62 | 2218.11 | 2671.61  | 3578.59  | 4485.57  |
| 1.089          | 858.77              | 1312.89 | 1539.95 | 1767.01 | 2221.12 | 2675.25  | 3583.48  | 4491.71  |
| 1.090          | 859.91              | 1314.66 | 1542.03 | 1769.40 | 2224.14 | 2678.89  | 3588.37  | 4497.85  |
| 1.091          | 861.05              | 1316.42 | 1544.10 | 1771.79 | 2227.16 | 2682.53  | 3593.26  | 4504.00  |
| 1.092          | 862.19              | 1318.18 | 1546.17 | 1774.18 | 2230.18 | 2686.17  | 3598.06  | 4510.15  |
| 1.093          | 863.23              | 1319.95 | 1548.24 | 1776.57 | 2233.20 | 2689.81  | 3603.76  | 4516.30  |
| 1.094          | 864.37              | 1321.72 | 1550.32 | 1778.96 | 2236.22 | 2693.46  | 3608.66  | 4522.45  |
| 1.095          | 865.61              | 1323.49 | 1552.42 | 1781.36 | 2239.24 | 2697.11  | 3612.86  | 4528.61  |
| 1.096          | 866.75              | 1325.25 | 1554.50 | 1783.75 | 2242.26 | 2700.76  | 3617.76  | 4534.77  |
| 1.097          | 867.89              | 1327.00 | 1556.58 | 1786.15 | 2245.28 | 2704.41  | 3622.67  | 4540.93  |
| 1.098          | 869.03              | 1328.79 | 1558.66 | 1788.55 | 2248.30 | 2708.06  | 3627.58  | 4547.19  |
| 1.099          | 860.17              | 1330.56 | 1560.75 | 1790.95 | 2251.33 | 2711.71  | 3632.49  | 4553.36  |
| 1.100          | 871.31              | 1332.33 | 1562.84 | 1793.35 | 2254.36 | 2715.37  | 3637.40  | 4559.43  |
| 1.101          | 872.46              | 1334.10 | 1564.92 | 1795.75 | 2257.39 | 2719.03  | 3642.32  | 4565.60  |
| 1.102          | 873.61              | 1335.87 | 1567.00 | 1798.15 | 2260.42 | 2722.69  | 3647.24  | 4571.78  |
| 1.103          | 874.76              | 1337.64 | 1569.09 | 1800.55 | 2263.45 | 2726.35  | 3652.16  | 4577.96  |
| 1.104          | 875.91              | 1339.41 | 1571.18 | 1802.95 | 2266.48 | 2730.01  | 3657.08  | 4584.14  |
| 1.105          | 877.03              | 1341.19 | 1573.27 | 1805.36 | 2269.52 | 2733.68  | 3662.00  | 4590.32  |
| 1.106          | 878.17              | 1342.96 | 1575.36 | 1807.76 | 2272.55 | 2737.34  | 3666.93  | 4596.51  |
| 1.107          | 879.31              | 1344.73 | 1577.45 | 1810.16 | 2275.58 | 2741.01  | 3671.86  | 4602.70  |
| 1.108          | 880.45              | 1346.51 | 1579.54 | 1812.57 | 2278.62 | 2744.67  | 3676.79  | 4608.89  |
| 1.109          | 881.50              | 1348.29 | 1581.63 | 1814.98 | 2281.66 | 2748.34  | 3681.72  | 4615.08  |
| 1.110          | 882.75              | 1350.07 | 1583.73 | 1817.39 | 2284.70 | 2752.02  | 3686.65  | 4621.28  |
| 1.111          | 883.89              | 1351.85 | 1585.82 | 1819.80 | 2287.74 | 2755.69  | 3691.59  | 4627.48  |
| 1.112          | 885.01              | 1353.63 | 1587.91 | 1822.21 | 2290.78 | 2759.36  | 3696.53  | 4633.68  |
| 1.113          | 886.19              | 1355.41 | 1590.91 | 1824.62 | 2293.82 | 2763.04  | 3701.47  | 4639.89  |
| 1.114          | 887.34              | 1357.19 | 1592.11 | 1827.03 | 2296.87 | 2766.72  | 3706.41  | 4646.10  |
| 1.115          | 888.49              | 1358.97 | 1594.21 | 1829.45 | 2299.92 | 2770.40  | 3711.35  | 4652.31  |
| 1.116          | 889.61              | 1360.75 | 1596.31 | 1831.86 | 2302.97 | 2774.08  | 3716.30  | 4658.52  |
| 1.117          | 890.79              | 1362.53 | 1598.41 | 1834.27 | 2306.02 | 2777.76  | 3721.25  | 4664.74  |
| 1.118          | 891.91              | 1364.31 | 1600.51 | 1836.69 | 2309.07 | 2781.44  | 3726.20  | 4670.96  |
| 1.119          | 893.19              | 1366.10 | 1602.61 | 1839.11 | 2312.12 | 2785.13  | 3731.15  | 4677.18  |
| 1.120          | 894.24              | 1367.89 | 1604.71 | 1841.53 | 2315.17 | 2788.82  | 3736.11  | 4683.40  |
| 1.121          | 895.39              | 1369.67 | 1606.81 | 1843.95 | 2318.22 | 2792.51  | 3741.07  | 4689.63  |
| 1.122          | 896.54              | 1371.45 | 1608.91 | 1846.37 | 2321.28 | 2796.20  | 3746.03  | 4695.86  |
| 1.123          | 897.69              | 1373.24 | 1611.01 | 1848.79 | 2324.34 | 2799.89  | 3750.99  | 4702.09  |
| 1.124          | 898.84              | 1375.03 | 1613.12 | 1851.21 | 2327.40 | 2803.58  | 3755.95  | 4708.32  |
| 1.125          | 899.99              | 1376.82 | 1615.23 | 1853.64 | 2330.46 | 2807.28  | 3760.92  | 4714.56  |
| 1.126          | 901.14              | 1378.61 | 1617.33 | 1856.06 | 2333.52 | 2810.77  | 3765.89  | 4720.80  |
| 1.127          | 902.29              | 1380.40 | 1619.44 | 1858.48 | 2336.58 | 2814.27  | 3770.86  | 4727.04  |
| 1.128          | 903.44              | 1382.19 | 1621.55 | 1860.91 | 2339.64 | 2817.77  | 3775.83  | 4733.28  |
| 1.129          | 904.60              | 1383.98 | 1623.66 | 1863.34 | 2342.70 | 2821.27  | 3780.80  | 4739.53  |
| 1.130          | 905.76              | 1385.77 | 1625.77 | 1865.77 | 2345.77 | 2825.77  | 3785.78  | 4745.78  |
| 1.131          | 906.91              | 1387.56 | 1627.88 | 1868.20 | 2348.84 | 2829.47  | 3790.76  | 4752.03  |
| 1.132          | 908.06              | 1389.35 | 1629.99 | 1870.63 | 2351.91 | 2833.18  | 3795.74  | 4758.29  |
| 1.133          | 909.22              | 1391.14 | 1632.10 | 1873.06 | 2354.98 | 2836.89  | 3800.72  | 4765.55  |
| 1.134          | 910.38              | 1392.93 | 1634.21 | 1875.49 | 2358.05 | 2840.60  | 3805.70  | 4771.81  |

| Depth on Weir. | LENGTH OF THE WEIR. |         |         |         |         |          |          |          |          |
|----------------|---------------------|---------|---------|---------|---------|----------|----------|----------|----------|
|                | Feet.               | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| 1.135          | 911.54              | 1394.73 | 1636.33 | 1877.92 | 2361.12 | 2844.31  | 3810.69  | 4777.07  |          |
| 1.136          | 912.69              | 1396.52 | 1638.44 | 1880.35 | 2364.19 | 2848.02  | 3815.68  | 4783.34  |          |
| 1.137          | 913.84              | 1398.32 | 1640.55 | 1882.79 | 2367.26 | 2851.73  | 3820.67  | 4789.61  |          |
| 1.138          | 915.00              | 1400.12 | 1642.67 | 1885.23 | 2370.33 | 2855.44  | 3825.66  | 4795.88  |          |
| 1.139          | 916.16              | 1401.92 | 1644.79 | 1887.67 | 2373.41 | 2859.16  | 3830.66  | 4802.15  |          |
| 1.140          | 917.32              | 1403.72 | 1646.91 | 1890.10 | 2376.49 | 2862.88  | 3835.66  | 4808.43  |          |
| 1.141          | 918.48              | 1405.52 | 1649.03 | 1892.54 | 2379.57 | 2866.60  | 3840.66  | 4814.71  |          |
| 1.142          | 919.64              | 1407.32 | 1651.15 | 1894.98 | 2382.65 | 2870.32  | 3845.66  | 4820.99  |          |
| 1.143          | 920.80              | 1409.12 | 1653.27 | 1897.42 | 2385.73 | 2874.04  | 3850.66  | 4827.27  |          |
| 1.144          | 921.96              | 1410.92 | 1654.39 | 1899.86 | 2388.81 | 2877.76  | 3855.66  | 4833.56  |          |
| 1.145          | 923.12              | 1412.72 | 1657.51 | 1902.31 | 2391.90 | 2881.49  | 3860.67  | 4839.85  |          |
| 1.146          | 924.28              | 1414.52 | 1659.63 | 1904.75 | 2394.98 | 2885.22  | 3865.68  | 4846.14  |          |
| 1.147          | 925.44              | 1416.32 | 1661.75 | 1907.19 | 2398.07 | 2888.95  | 3870.69  | 4852.44  |          |
| 1.148          | 926.60              | 1418.12 | 1663.87 | 1909.63 | 2401.16 | 2892.68  | 3875.70  | 4858.74  |          |
| 1.149          | 927.76              | 1419.92 | 1665.00 | 1912.08 | 2404.25 | 2896.41  | 3880.72  | 4865.04  |          |
| 1.150          | 928.93              | 1421.73 | 1668.13 | 1914.53 | 2407.34 | 2900.14  | 3885.74  | 4871.34  |          |
| 1.151          | 930.09              | 1423.53 | 1670.26 | 1916.98 | 2410.43 | 2903.87  | 3890.76  | 4877.65  |          |
| 1.152          | 931.25              | 1425.34 | 1672.39 | 1919.43 | 2413.52 | 2907.60  | 3895.78  | 4883.96  |          |
| 1.153          | 932.41              | 1427.15 | 1674.52 | 1921.88 | 2416.61 | 2911.35  | 3900.80  | 4890.27  |          |
| 1.154          | 933.57              | 1428.96 | 1676.65 | 1924.33 | 2419.71 | 2915.09  | 3905.82  | 4896.58  |          |
| 1.155          | 934.74              | 1430.77 | 1678.78 | 1926.79 | 2422.81 | 2918.83  | 3910.86  | 4902.90  |          |
| 1.156          | 935.90              | 1432.58 | 1680.90 | 1929.24 | 2425.91 | 2922.57  | 3915.89  | 4909.22  |          |
| 1.157          | 937.06              | 1434.39 | 1683.02 | 1931.69 | 2429.01 | 2926.31  | 3920.92  | 4915.56  |          |
| 1.158          | 938.23              | 1436.20 | 1685.15 | 1934.14 | 2432.11 | 2930.05  | 3925.96  | 4921.89  |          |
| 1.159          | 939.40              | 1438.01 | 1687.28 | 1936.60 | 2435.21 | 2933.80  | 3931.00  | 4928.19  |          |
| 1.160          | 940.57              | 1439.82 | 1689.44 | 1939.06 | 2438.31 | 2937.55  | 3936.04  | 4934.52  |          |
| 1.161          | 941.73              | 1441.63 | 1691.55 | 1941.52 | 2441.41 | 2941.30  | 3941.08  | 4940.85  |          |
| 1.162          | 942.90              | 1443.45 | 1693.69 | 1943.98 | 2444.51 | 2945.05  | 3946.12  | 4947.19  |          |
| 1.163          | 944.07              | 1445.27 | 1695.83 | 1946.44 | 2447.62 | 2948.80  | 3951.16  | 4953.53  |          |
| 1.164          | 945.24              | 1447.09 | 1697.97 | 1948.90 | 2450.73 | 2952.55  | 3956.21  | 4959.87  |          |
| 1.165          | 946.41              | 1448.89 | 1700.12 | 1951.36 | 2453.84 | 2956.31  | 3961.26  | 4966.21  |          |
| 1.166          | 947.57              | 1450.70 | 1702.26 | 1954.82 | 2456.95 | 2960.07  | 3966.31  | 4972.56  |          |
| 1.167          | 948.74              | 1452.51 | 1704.40 | 1957.28 | 2460.06 | 2963.83  | 3971.36  | 4978.91  |          |
| 1.168          | 949.91              | 1454.33 | 1706.54 | 1959.74 | 2463.17 | 2967.59  | 3976.41  | 4985.26  |          |
| 1.169          | 951.08              | 1456.15 | 1708.68 | 1962.21 | 2466.28 | 2971.35  | 3981.47  | 4991.61  |          |
| 1.170          | 952.25              | 1457.97 | 1710.83 | 1963.68 | 2469.40 | 2975.11  | 3986.54  | 4997.96  |          |
| 1.171          | 953.42              | 1459.89 | 1712.97 | 1966.15 | 2472.51 | 2978.87  | 3991.60  | 5004.32  |          |
| 1.172          | 954.59              | 1461.71 | 1715.11 | 1968.62 | 2475.63 | 2982.64  | 3996.66  | 5010.68  |          |
| 1.173          | 955.76              | 1463.53 | 1717.25 | 1971.09 | 2478.75 | 2986.41  | 4001.76  | 5017.04  |          |
| 1.174          | 956.93              | 1465.35 | 1719.40 | 1973.56 | 2481.87 | 2990.18  | 4006.83  | 5023.41  |          |
| 1.175          | 958.11              | 1467.07 | 1721.55 | 1976.03 | 2484.99 | 2993.95  | 4011.86  | 5029.78  |          |
| 1.176          | 959.28              | 1468.89 | 1723.70 | 1978.50 | 2488.11 | 2997.72  | 4016.93  | 5036.15  |          |
| 1.177          | 960.45              | 1470.71 | 1725.85 | 1980.97 | 2491.23 | 3001.49  | 4022.00  | 5042.52  |          |
| 1.178          | 961.62              | 1472.53 | 1728.00 | 1983.44 | 2494.35 | 3005.26  | 4027.08  | 5048.90  |          |
| 1.179          | 962.80              | 1474.36 | 1730.15 | 1985.92 | 2497.48 | 3009.04  | 4032.16  | 5055.29  |          |
| 1.180          | 963.98              | 1476.19 | 1732.30 | 1988.40 | 2500.61 | 3012.82  | 4037.24  | 5061.66  |          |
| 1.181          | 965.15              | 1478.01 | 1734.45 | 1990.84 | 2503.87 | 3016.60  | 4042.32  | 5068.05  |          |
| 1.182          | 966.32              | 1479.84 | 1736.60 | 1993.29 | 2506.87 | 3020.38  | 4047.40  | 5074.44  |          |
| 1.183          | 967.49              | 1481.67 | 1738.75 | 1995.74 | 2510.00 | 3024.16  | 4052.49  | 5080.83  |          |
| 1.184          | 968.67              | 1483.50 | 1740.90 | 1998.19 | 2513.13 | 3027.94  | 4057.58  | 5087.22  |          |
| 1.185          | 969.85              | 1485.33 | 1743.06 | 2000.80 | 2516.27 | 3031.73  | 4062.67  | 5093.61  |          |
| 1.186          | 971.02              | 1487.16 | 1745.21 | 2003.28 | 2519.40 | 3035.52  | 4067.76  | 5100.01  |          |
| 1.187          | 972.20              | 1488.99 | 1747.36 | 2005.76 | 2522.53 | 3039.31  | 4072.76  | 5106.41  |          |
| 1.188          | 973.38              | 1490.82 | 1749.52 | 2008.24 | 2525.67 | 3043.10  | 4077.86  | 5112.81  |          |
| 1.189          | 974.56              | 1492.65 | 1751.68 | 2010.72 | 2528.81 | 3046.89  | 4082.96  | 5119.22  |          |
| 1.190          | 975.74              | 1494.48 | 1753.84 | 2013.21 | 2531.95 | 3050.68  | 4088.15  | 5125.63  |          |
| 1.191          | 976.91              | 1496.31 | 1756.00 | 2015.69 | 2535.09 | 3054.47  | 4093.25  | 5132.04  |          |
| 1.192          | 978.09              | 1498.14 | 1758.16 | 2018.18 | 2538.23 | 3058.27  | 4098.36  | 5138.45  |          |

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |         |         |          |          |          |
|----------------------|---------------------|---------|---------|---------|---------|----------|----------|----------|
|                      | Feet.               | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. |
| 1.193                | 979.27              | 1499.97 | 1760.32 | 2020.67 | 2541.37 | 3062.07  | 4103.47  | 5144.86  |
| 1.194                | 980.45              | 1501.80 | 1762.58 | 2023.16 | 2544.51 | 3065.87  | 4108.58  | 5151.28  |
| 1.195                | 981.63              | 1503.64 | 1764.65 | 2025.65 | 2547.66 | 3069.67  | 4113.69  | 5157.70  |
| 1.196                | 982.81              | 1505.47 | 1766.81 | 2028.14 | 2550.80 | 3073.47  | 4118.80  | 5164.12  |
| 1.197                | 983.99              | 1507.31 | 1768.97 | 2030.63 | 2553.95 | 3077.27  | 4123.91  | 5170.55  |
| 1.198                | 985.17              | 1509.15 | 1771.13 | 2033.12 | 2557.10 | 3081.07  | 4129.03  | 5176.98  |
| 1.199                | 986.35              | 1510.99 | 1773.30 | 2035.62 | 2560.25 | 3084.88  | 4134.25  | 5183.41  |
| 1.200                | 987.54              | 1512.83 | 1775.47 | 2038.12 | 2563.40 | 3088.69  | 4139.27  | 5189.84  |
| 1.201                | 988.72              | 1514.67 | 1777.64 | 2040.61 | 2566.55 | 3092.50  | 4144.29  | 5196.28  |
| 1.202                | 989.90              | 1516.51 | 1779.81 | 2043.10 | 2569.70 | 3096.31  | 4149.41  | 5202.72  |
| 1.203                | 991.08              | 1518.35 | 1781.98 | 2045.60 | 2572.86 | 3100.12  | 4154.54  | 5209.16  |
| 1.204                | 992.26              | 1520.19 | 1784.15 | 2048.10 | 2576.02 | 3103.93  | 4159.67  | 5235.60  |
| 1.205                | 993.45              | 1522.03 | 1786.32 | 2050.60 | 2579.18 | 3107.75  | 4164.90  | 5222.05  |
| 1.206                | 994.63              | 1523.87 | 1788.49 | 2053.10 | 2582.34 | 3111.57  | 4170.03  | 5228.50  |
| 1.207                | 995.81              | 1525.71 | 1790.66 | 2055.60 | 2585.50 | 3115.39  | 4175.17  | 5234.95  |
| 1.208                | 996.99              | 1527.55 | 1792.83 | 2058.10 | 2588.66 | 3119.21  | 4180.31  | 5241.40  |
| 1.209                | 998.18              | 1529.40 | 1795.00 | 2060.60 | 2591.82 | 3123.03  | 4185.45  | 5247.86  |
| 1.210                | 999.37              | 1531.25 | 1797.18 | 2063.11 | 2594.98 | 3126.85  | 4190.59  | 5254.32  |
| 1.211                | 1000.56             | 1533.09 | 1799.35 | 2065.61 | 2598.14 | 3130.67  | 4195.73  | 5260.78  |
| 1.212                | 1001.75             | 1534.93 | 1801.52 | 2068.12 | 2601.31 | 3134.49  | 4200.87  | 5267.24  |
| 1.213                | 1002.94             | 1536.78 | 1803.70 | 2070.63 | 2604.48 | 3138.32  | 4206.21  | 5273.71  |
| 1.214                | 1004.13             | 1538.63 | 1805.88 | 2073.14 | 2607.65 | 3142.15  | 4211.17  | 5280.18  |
| 1.215                | 1005.31             | 1540.48 | 1808.06 | 2075.65 | 2610.82 | 3145.98  | 4216.32  | 5286.65  |
| 1.216                | 1006.49             | 1542.33 | 1810.24 | 2078.16 | 2613.99 | 3149.81  | 4221.47  | 5293.13  |
| 1.217                | 1007.68             | 1544.18 | 1812.44 | 2080.67 | 2617.16 | 3153.64  | 4226.62  | 5299.61  |
| 1.218                | 1008.87             | 1546.03 | 1814.62 | 2083.18 | 2620.33 | 3157.47  | 4231.78  | 5306.09  |
| 1.219                | 1010.06             | 1547.88 | 1816.80 | 2085.69 | 2623.50 | 3161.31  | 4236.94  | 5312.57  |
| 1.220                | 1011.25             | 1549.73 | 1818.97 | 2088.20 | 2626.68 | 3165.15  | 4242.10  | 5319.05  |
| 1.221                | 1012.44             | 1551.58 | 1821.15 | 2090.71 | 2629.85 | 3168.99  | 4247.26  | 5325.54  |
| 1.222                | 1013.63             | 1553.43 | 1823.33 | 2093.22 | 2633.03 | 3172.83  | 4252.43  | 5332.03  |
| 1.223                | 1014.82             | 1555.28 | 1825.52 | 2095.74 | 2636.21 | 3176.67  | 4257.60  | 5338.52  |
| 1.224                | 1016.01             | 1557.14 | 1827.71 | 2098.26 | 2639.38 | 3180.51  | 4262.77  | 5345.01  |
| 1.225                | 1017.20             | 1559.00 | 1829.89 | 2100.78 | 2642.57 | 3184.36  | 4267.94  | 5351.51  |
| 1.226                | 1018.39             | 1560.85 | 1832.07 | 2103.30 | 2645.75 | 3188.20  | 4273.11  | 5358.01  |
| 1.227                | 1019.58             | 1562.70 | 1834.26 | 2105.82 | 2648.93 | 3192.05  | 4278.28  | 5364.51  |
| 1.228                | 1020.77             | 1564.56 | 1836.45 | 2108.34 | 2652.12 | 3195.90  | 4283.46  | 5371.02  |
| 1.229                | 1021.96             | 1566.42 | 1838.64 | 2110.86 | 2655.31 | 3199.75  | 4288.64  | 5377.53  |
| 1.230                | 1023.16             | 1568.28 | 1840.83 | 2113.39 | 2658.50 | 3203.60  | 4293.82  | 5384.04  |
| 1.231                | 1024.35             | 1570.14 | 1843.02 | 2115.91 | 2661.69 | 3207.45  | 4299.00  | 5390.55  |
| 1.232                | 1025.54             | 1572.00 | 1845.21 | 2118.43 | 2664.88 | 3211.30  | 4304.19  | 5397.07  |
| 1.233                | 1026.74             | 1573.86 | 1847.40 | 2120.95 | 2668.07 | 3215.16  | 4309.38  | 5393.59  |
| 1.234                | 1027.94             | 1575.72 | 1849.59 | 2123.48 | 2671.26 | 3219.02  | 4314.58  | 5391.11  |
| 1.235                | 1029.14             | 1577.58 | 1851.79 | 2126.01 | 2674.45 | 3222.88  | 4319.76  | 5416.63  |
| 1.236                | 1030.33             | 1579.44 | 1853.98 | 2128.54 | 2677.64 | 3226.74  | 4324.75  | 5423.18  |
| 1.237                | 1031.52             | 1581.30 | 1856.18 | 2131.48 | 2680.83 | 3230.60  | 4329.96  | 5429.71  |
| 1.238                | 1032.72             | 1583.16 | 1858.38 | 2133.60 | 2684.03 | 3234.46  | 4335.15  | 5436.24  |
| 1.239                | 1033.92             | 1585.02 | 1860.58 | 2136.13 | 2687.23 | 3238.33  | 4340.35  | 5442.77  |
| 1.240                | 1035.12             | 1586.89 | 1862.78 | 2138.66 | 2690.43 | 3242.20  | 4345.74  | 5449.28  |
| 1.241                | 1036.31             | 1588.75 | 1864.98 | 2141.19 | 2693.63 | 3246.07  | 4350.94  | 5555.82  |
| 1.242                | 1037.51             | 1590.61 | 1867.18 | 2143.72 | 2696.83 | 3249.94  | 4356.14  | 5562.36  |
| 1.243                | 1038.71             | 1592.48 | 1869.38 | 2146.25 | 2700.03 | 3253.81  | 4361.35  | 5568.90  |
| 1.244                | 1039.91             | 1594.35 | 1871.58 | 2148.79 | 2703.23 | 3257.68  | 4366.56  | 5575.45  |
| 1.245                | 1041.11             | 1596.22 | 1873.78 | 2151.33 | 2706.44 | 3261.55  | 4371.77  | 5482.00  |
| 1.246                | 1042.31             | 1598.09 | 1875.98 | 2153.86 | 2709.64 | 3265.42  | 4376.98  | 5488.55  |
| 1.247                | 1043.51             | 1599.96 | 1878.18 | 2156.40 | 2712.85 | 3269.30  | 4382.20  | 5495.10  |
| 1.248                | 1044.71             | 1601.83 | 1880.38 | 2158.94 | 2716.06 | 3273.18  | 4387.42  | 5501.65  |
| 1.249                | 1045.91             | 1603.70 | 1882.59 | 2161.48 | 2719.27 | 3277.06  | 4392.64  | 5508.21  |
| 1.250                | 1047.11             | 1605.57 | 1884.80 | 2164.02 | 2722.48 | 3280.94  | 4397.86  | 5514.77  |

| Depth on Weir. | LENGTH OF THE WEIR. |         |         |         |          |          |          |          |
|----------------|---------------------|---------|---------|---------|----------|----------|----------|----------|
|                | 4 Feet.             | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| 1.251          | 1048.31             | 1607.44 | 1887.00 | 2166.56 | 2725.69  | 3284.82  | 4403.08  | 5521.33  |
| 1.252          | 1049.51             | 1609.31 | 1889.20 | 2169.10 | 2728.90  | 3288.70  | 4408.30  | 5527.90  |
| 1.253          | 1050.71             | 1611.18 | 1891.41 | 2171.64 | 2732.11  | 3292.58  | 4413.53  | 5534.47  |
| 1.254          | 1051.91             | 1613.05 | 1893.62 | 2174.19 | 2735.33  | 3296.47  | 4418.76  | 5541.04  |
| 1.255          | 1053.11             | 1614.93 | 1895.83 | 2176.74 | 2738.55  | 3300.36  | 4423.99  | 5547.61  |
| 1.256          | 1054.31             | 1616.80 | 1898.04 | 2179.28 | 2741.77  | 3304.25  | 4429.22  | 5554.19  |
| 1.257          | 1055.51             | 1618.67 | 1900.25 | 2181.83 | 2744.99  | 3308.14  | 4434.55  | 5560.77  |
| 1.258          | 1056.71             | 1620.55 | 1902.46 | 2184.38 | 2748.21  | 3312.04  | 4439.69  | 5567.35  |
| 1.259          | 1057.91             | 1622.43 | 1904.67 | 2186.93 | 2751.43  | 3315.94  | 4445.93  | 5573.93  |
| 1.260          | 1059.12             | 1624.31 | 1906.89 | 2189.48 | 2754.65  | 3319.82  | 4450.17  | 5580.51  |
| 1.261          | 1060.32             | 1626.18 | 1909.10 | 2192.03 | 2757.87  | 3323.72  | 4455.41  | 5587.10  |
| 1.262          | 1061.52             | 1628.06 | 1911.31 | 2194.58 | 2761.09  | 3327.62  | 4460.65  | 5593.69  |
| 1.263          | 1062.72             | 1629.94 | 1913.53 | 2197.13 | 2764.32  | 3331.52  | 4465.90  | 5600.28  |
| 1.264          | 1063.93             | 1631.82 | 1915.75 | 2199.68 | 2767.55  | 3335.42  | 4471.15  | 5607.87  |
| 1.265          | 1065.14             | 1633.70 | 1917.97 | 2202.24 | 2770.78  | 3339.32  | 4476.40  | 5613.47  |
| 1.266          | 1066.62             | 1635.58 | 1920.19 | 2204.79 | 2774.01  | 3343.23  | 4481.65  | 5620.04  |
| 1.267          | 1067.83             | 1637.46 | 1922.41 | 2207.34 | 2777.24  | 3347.14  | 4487.90  | 5626.65  |
| 1.268          | 1069.04             | 1639.34 | 1924.63 | 2209.90 | 2780.47  | 3351.05  | 4493.16  | 5633.26  |
| 1.269          | 1070.25             | 1641.22 | 1926.85 | 2212.46 | 2783.70  | 3354.96  | 4498.42  | 5639.87  |
| 1.270          | 1071.19             | 1643.11 | 1929.07 | 2215.02 | 2786.94  | 3358.85  | 4503.68  | 5646.51  |
| 1.271          | 1072.40             | 1644.99 | 1931.29 | 2217.58 | 2790.17  | 3362.76  | 4507.94  | 5653.12  |
| 1.272          | 1073.61             | 1646.88 | 1933.51 | 2220.14 | 2793.41  | 3366.67  | 4513.20  | 5659.74  |
| 1.273          | 1074.82             | 1648.77 | 1935.73 | 2222.70 | 2796.65  | 3370.58  | 4518.47  | 5666.36  |
| 1.274          | 1076.03             | 1650.66 | 1937.95 | 2225.26 | 2799.89  | 3374.50  | 4523.74  | 5672.98  |
| 1.275          | 1077.24             | 1652.54 | 1940.18 | 2227.83 | 2803.13  | 3378.42  | 4529.01  | 5679.60  |
| 1.276          | 1078.45             | 1654.42 | 1942.40 | 2230.39 | 2806.37  | 3382.34  | 4534.28  | 5686.23  |
| 1.277          | 1079.66             | 1656.31 | 1944.63 | 2232.95 | 2809.61  | 3386.26  | 4539.55  | 5692.86  |
| 1.278          | 1080.87             | 1658.20 | 1946.86 | 2235.52 | 2812.85  | 3390.18  | 4544.83  | 5699.49  |
| 1.279          | 1082.08             | 1660.09 | 1949.09 | 2238.09 | 2816.09  | 3394.10  | 4550.11  | 5706.12  |
| 1.280          | 1083.29             | 1661.98 | 1951.32 | 2240.66 | 2819.34  | 3398.02  | 4555.39  | 5712.75  |
| 1.281          | 1084.50             | 1663.88 | 1953.55 | 2243.23 | 2822.58  | 3401.94  | 4560.67  | 5719.39  |
| 1.282          | 1085.71             | 1665.77 | 1955.78 | 2245.80 | 2825.84  | 3405.87  | 4565.95  | 5726.03  |
| 1.283          | 1086.91             | 1667.66 | 1958.01 | 2248.37 | 2829.09  | 3409.80  | 4571.22  | 5732.67  |
| 1.284          | 1088.12             | 1669.55 | 1960.24 | 2250.94 | 2832.34  | 3413.73  | 4576.51  | 5739.32  |
| 1.285          | 1089.33             | 1671.43 | 1962.47 | 2253.51 | 2835.59  | 3417.66  | 4581.82  | 5745.97  |
| 1.286          | 1090.56             | 1673.32 | 1964.70 | 2256.08 | 2838.84  | 3421.59  | 4587.11  | 5752.62  |
| 1.287          | 1091.77             | 1675.21 | 1966.93 | 2258.65 | 2842.09  | 3425.52  | 4592.50  | 5759.27  |
| 1.288          | 1092.99             | 1677.10 | 1969.16 | 2261.22 | 2845.34  | 3429.46  | 4597.79  | 5765.93  |
| 1.289          | 1094.21             | 1679.00 | 1971.40 | 2263.80 | 2848.60  | 3433.40  | 4603.09  | 5772.59  |
| 1.290          | 1095.43             | 1680.90 | 1973.64 | 2266.38 | 2851.86  | 3437.34  | 4608.29  | 5779.25  |
| 1.291          | 1096.64             | 1682.79 | 1975.88 | 2268.96 | 2855.12  | 3441.28  | 4613.59  | 5785.91  |
| 1.292          | 1097.85             | 1684.69 | 1978.11 | 2271.54 | 2858.38  | 3445.22  | 4618.89  | 5792.57  |
| 1.293          | 1099.07             | 1686.59 | 1980.35 | 2274.12 | 2861.64  | 3449.16  | 4624.20  | 5799.24  |
| 1.294          | 1100.29             | 1688.49 | 1982.59 | 2276.70 | 2864.90  | 3453.10  | 4629.51  | 5805.91  |
| 1.295          | 1101.51             | 1690.39 | 1984.83 | 2279.28 | 2868.16  | 3457.05  | 4634.82  | 5812.58  |
| 1.296          | 1102.72             | 1692.29 | 1987.07 | 2281.86 | 2871.42  | 3460.99  | 4640.13  | 5819.26  |
| 1.297          | 1103.93             | 1694.19 | 1989.31 | 2284.44 | 2874.68  | 3464.94  | 4645.44  | 5825.94  |
| 1.298          | 1105.15             | 1696.09 | 1991.55 | 2287.02 | 2877.95  | 3468.99  | 4650.75  | 5832.62  |
| 1.299          | 1106.37             | 1697.99 | 1993.80 | 2289.61 | 2881.22  | 3472.94  | 4656.07  | 5839.30  |
| 1.300          | 1107.59             | 1699.90 | 1996.05 | 2292.20 | 2884.49  | 3476.79  | 4661.39  | 5845.98  |
| 1.301          | 1108.81             | 1701.80 | 1998.29 | 2294.78 | 2887.76  | 3480.74  | 4666.71  | 5852.67  |
| 1.302          | 1110.03             | 1703.70 | 2000.53 | 2297.36 | 2891.03  | 3484.70  | 4672.03  | 5859.36  |
| 1.303          | 1111.25             | 1705.60 | 2002.77 | 2299.95 | 2894.30  | 3488.66  | 4677.35  | 5866.05  |
| 1.304          | 1112.47             | 1707.50 | 2005.02 | 2302.54 | 2897.57  | 3492.62  | 4682.68  | 5872.74  |
| 1.305          | 1113.69             | 1709.41 | 2007.27 | 2305.13 | 2900.85  | 3496.57  | 4688.01  | 5879.44  |
| 1.306          | 1114.91             | 1711.31 | 2009.52 | 2307.72 | 2904.12  | 3500.53  | 4693.34  | 5886.14  |
| 1.307          | 1116.13             | 1713.22 | 2011.77 | 2310.31 | 2907.40  | 3504.49  | 4698.67  | 5892.84  |
| 1.308          | 1117.35             | 1715.13 | 2014.02 | 2313.90 | 2910.68  | 3508.45  | 4704.00  | 5899.55  |

| Depth on Weir. | LENGTH OF THE WEIR. |         |         |         |         |          |          |          |
|----------------|---------------------|---------|---------|---------|---------|----------|----------|----------|
|                | Feet.               | 4 Feet. | 6 Feet. | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. |
| 1.309          | 1118.52             | 1717.04 | 2016.27 | 2316.49 | 2913.96 | 3512.42  | 4709.34  | 5906.26  |
| 1.310          | 1119.80             | 1718.95 | 2018.52 | 2318.09 | 2917.24 | 3516.39  | 4714.68  | 5912.97  |
| 1.311          | 1121.62             | 1720.86 | 2020.77 | 2320.68 | 2920.52 | 3520.36  | 4720.02  | 5919.68  |
| 1.312          | 1122.24             | 1722.77 | 2023.02 | 2323.28 | 2923.80 | 3524.33  | 4725.36  | 5926.39  |
| 1.313          | 1123.47             | 1724.68 | 2025.27 | 2325.88 | 2927.08 | 3528.30  | 4730.70  | 5933.11  |
| 1.314          | 1124.70             | 1726.59 | 2027.53 | 2328.48 | 2930.37 | 3532.27  | 4736.04  | 5939.89  |
| 1.315          | 1125.92             | 1728.50 | 2029.79 | 2331.08 | 2933.66 | 3536.24  | 4741.40  | 5946.55  |
| 1.316          | 1127.36             | 1730.41 | 2032.04 | 2333.68 | 2936.94 | 3540.21  | 4746.75  | 5953.28  |
| 1.317          | 1128.59             | 1732.32 | 2034.29 | 2336.28 | 2940.23 | 3544.18  | 4752.10  | 5960.01  |
| 1.318          | 1129.81             | 1734.23 | 2036.55 | 2338.88 | 2943.52 | 3548.18  | 4757.45  | 5966.74  |
| 1.319          | 1131.04             | 1736.14 | 2038.81 | 2341.48 | 2946.81 | 3552.16  | 4762.80  | 5973.47  |
| 1.320          | 1132.04             | 1738.06 | 2041.07 | 2344.08 | 2950.10 | 3556.12  | 4768.16  | 5980.20  |
| 1.321          | 1133.26             | 1739.97 | 2043.33 | 2346.68 | 2953.39 | 3560.10  | 4773.52  | 5986.94  |
| 1.322          | 1134.48             | 1741.88 | 2045.59 | 2349.28 | 2956.68 | 3564.08  | 4778.88  | 5993.68  |
| 1.323          | 1135.71             | 1743.80 | 2047.85 | 2351.89 | 2959.97 | 3568.06  | 4784.24  | 6000.42  |
| 1.324          | 1136.94             | 1745.72 | 2050.11 | 2354.50 | 2963.07 | 3572.05  | 4789.60  | 6007.16  |
| 1.325          | 1138.17             | 1747.64 | 2052.38 | 2357.11 | 2966.57 | 3576.04  | 4794.97  | 6013.90  |
| 1.326          | 1139.39             | 1749.56 | 2054.64 | 2359.72 | 2969.87 | 3580.03  | 4800.36  | 6020.65  |
| 1.327          | 1140.62             | 1751.48 | 2056.90 | 2362.33 | 2973.17 | 3584.02  | 4805.73  | 6027.40  |
| 1.328          | 1141.85             | 1753.40 | 2059.16 | 2364.94 | 2976.47 | 3588.01  | 4811.10  | 6034.15  |
| 1.329          | 1143.08             | 1755.32 | 2061.43 | 2367.55 | 2979.77 | 3592.00  | 4816.47  | 6040.91  |
| 1.330          | 1144.31             | 1757.24 | 2063.70 | 2370.16 | 2983.07 | 3595.99  | 4821.83  | 6047.67  |
| 1.331          | 1145.54             | 1759.16 | 2065.96 | 2372.77 | 2986.37 | 3599.98  | 4827.21  | 6054.43  |
| 1.332          | 1146.77             | 1761.08 | 2068.23 | 2375.38 | 2989.68 | 3603.98  | 4832.59  | 6061.19  |
| 1.333          | 1148.00             | 1763.90 | 2070.50 | 2377.99 | 2992.99 | 3607.98  | 4837.97  | 6067.96  |
| 1.334          | .....               | 1764.92 | 2072.77 | 2380.61 | 2996.30 | 3611.98  | 4843.35  | 6074.73  |
| 1.335          | .....               | 1766.85 | 2075.04 | 2383.23 | 2999.61 | 3615.98  | 4848.74  | 6081.50  |
| 1.336          | .....               | 1768.77 | 2077.31 | 2385.84 | 3002.92 | 3619.98  | 4854.13  | 6088.27  |
| 1.337          | .....               | 1770.69 | 2079.58 | 2388.46 | 3006.23 | 3623.98  | 4859.52  | 6095.04  |
| 1.338          | .....               | 1772.60 | 2081.85 | 2391.08 | 3009.54 | 3627.99  | 4864.91  | 6101.82  |
| 1.339          | .....               | 1774.53 | 2084.12 | 2393.70 | 3012.85 | 3632.00  | 4870.20  | 6108.60  |
| 1.340          | .....               | 1776.47 | 2086.40 | 2396.32 | 3016.17 | 3636.01  | 4875.70  | 6115.38  |
| 1.341          | .....               | 1778.39 | 2088.67 | 2398.94 | 3019.48 | 3640.02  | 4881.11  | 6122.17  |
| 1.342          | .....               | 1780.32 | 2090.94 | 2401.56 | 3022.79 | 3644.03  | 4886.52  | 6128.96  |
| 1.343          | .....               | 1782.25 | 2093.21 | 2404.18 | 3026.11 | 3648.04  | 4891.93  | 6135.75  |
| 1.344          | .....               | 1784.18 | 2095.49 | 2406.80 | 3029.43 | 3652.05  | 4897.34  | 6142.54  |
| 1.345          | .....               | 1786.11 | 2097.77 | 2409.43 | 3032.75 | 3656.06  | 4902.70  | 6149.33  |
| 1.346          | .....               | 1788.04 | 2100.05 | 2412.05 | 3036.07 | 3660.08  | 4908.22  | 6156.13  |
| 1.347          | .....               | 1789.97 | 2102.33 | 2414.68 | 3039.39 | 3664.10  | 4913.65  | 6162.93  |
| 1.348          | .....               | 1791.90 | 2104.61 | 2417.31 | 3042.71 | 3668.12  | 4919.08  | 6169.73  |
| 1.349          | .....               | 1793.83 | 2106.89 | 2419.94 | 3046.03 | 3672.14  | 4924.51  | 6176.53  |
| 1.350          | .....               | 1795.77 | 2109.17 | 2422.57 | 3049.36 | 3676.16  | 4929.75  | 6183.34  |
| 1.351          | .....               | 1797.70 | 2111.45 | 2425.20 | 3052.68 | 3680.18  | 4935.17  | 6190.15  |
| 1.352          | .....               | 1799.63 | 2113.73 | 2427.83 | 3056.01 | 3684.20  | 4940.59  | 6196.96  |
| 1.353          | .....               | 1801.56 | 2116.01 | 2430.46 | 3059.34 | 3688.22  | 4946.01  | 6203.77  |
| 1.354          | .....               | 1803.50 | 2118.29 | 2433.09 | 3062.67 | 3692.25  | 4951.43  | 6210.59  |
| 1.355          | .....               | 1805.44 | 2120.58 | 2435.72 | 3066.00 | 3696.28  | 4956.85  | 6217.41  |
| 1.356          | .....               | 1807.37 | 2122.86 | 2438.35 | 3069.33 | 3700.31  | 4962.27  | 6224.23  |
| 1.357          | .....               | 1809.31 | 2125.14 | 2440.98 | 3072.66 | 3704.34  | 4967.70  | 6231.05  |
| 1.358          | .....               | 1811.25 | 2127.43 | 2443.62 | 3075.99 | 3708.38  | 4973.13  | 6237.88  |
| 1.359          | .....               | 1813.19 | 2129.72 | 2446.26 | 3079.33 | 3712.42  | 4978.56  | 6244.71  |
| 1.360          | .....               | 1815.13 | 2132.01 | 2448.90 | 3082.67 | 3716.45  | 4983.99  | 6251.54  |
| 1.361          | .....               | 1817.07 | 2134.30 | 2451.54 | 3086.01 | 3720.48  | 4989.43  | 6258.37  |
| 1.362          | .....               | 1819.01 | 2136.58 | 2454.18 | 3089.35 | 3724.52  | 4994.87  | 6265.21  |
| 1.363          | .....               | 1820.95 | 2138.87 | 2456.82 | 3092.69 | 3728.56  | 5000.31  | 6272.05  |
| 1.364          | .....               | 1822.89 | 2141.16 | 2459.46 | 3096.03 | 3732.60  | 5005.75  | 6278.89  |
| 1.365          | .....               | 1824.83 | 2143.46 | 2462.10 | 3099.37 | 3736.64  | 5011.19  | 6285.73  |
| 1.366          | .....               | 1826.77 | 2145.75 | 2464.74 | 3102.71 | 3740.68  | 5016.63  | 6292.58  |



| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|----------|----------|----------|----------|
|                      | 6 Feet.             | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| 1.367                | 1828.71             | 2148.08 | 2467.38 | 3106.05  | 3744.72  | 5022.07  | 6299.43  |
| 1.368                | 1830.65             | 2150.33 | 2470.02 | 3109.40  | 3748.77  | 5027.52  | 6306.28  |
| 1.369                | 1832.59             | 2152.63 | 2472.66 | 3112.75  | 3752.82  | 5032.97  | 6313.13  |
| 1.370                | 1834.54             | 2154.93 | 2475.32 | 3116.10  | 3756.87  | 5038.42  | 6319.98  |
| 1.371                | 1836.48             | 2157.22 | 2477.96 | 3119.45  | 3760.92  | 5043.87  | 6326.84  |
| 1.372                | 1838.42             | 2159.52 | 2480.61 | 3122.80  | 3764.97  | 5049.33  | 6333.70  |
| 1.373                | 1840.37             | 2161.82 | 2483.26 | 3126.15  | 3769.02  | 5054.79  | 6340.56  |
| 1.374                | 1842.32             | 2164.12 | 2485.91 | 3129.50  | 3773.07  | 5060.25  | 6347.42  |
| 1.375                | 1844.27             | 2166.42 | 2488.56 | 3132.85  | 3777.13  | 5065.71  | 6354.28  |
| 1.376                | 1846.22             | 2168.72 | 2491.21 | 3136.20  | 3781.19  | 5071.17  | 6361.05  |
| 1.377                | 1848.17             | 2171.02 | 2493.86 | 3139.55  | 3785.25  | 5076.63  | 6368.02  |
| 1.378                | 1850.15             | 2173.32 | 2496.51 | 3142.91  | 3789.30  | 5082.10  | 6374.89  |
| 1.379                | 1852.10             | 2175.62 | 2499.16 | 3146.27  | 3793.36  | 5087.57  | 6381.77  |
| 1.380                | 1854.02             | 2177.92 | 2501.82 | 3149.63  | 3797.43  | 5093.04  | 6388.65  |
| 1.381                | 1855.97             | 2180.22 | 2504.47 | 3152.99  | 3801.49  | 5098.51  | 6395.53  |
| 1.382                | 1857.92             | 2182.52 | 2507.13 | 3156.35  | 3806.55  | 5103.98  | 6402.40  |
| 1.383                | 1859.87             | 2184.82 | 2509.79 | 3159.71  | 3810.62  | 5109.46  | 6409.30  |
| 1.384                | 1861.82             | 2187.13 | 2512.45 | 3163.07  | 3814.69  | 5114.94  | 6416.19  |
| 1.385                | 1863.78             | 2189.44 | 2515.11 | 3166.43  | 3817.76  | 5120.42  | 6423.08  |
| 1.386                | 1865.73             | 2191.74 | 2517.77 | 3169.79  | 3821.83  | 5125.90  | 6429.97  |
| 1.387                | 1867.68             | 2194.05 | 2520.43 | 3173.16  | 3825.90  | 5131.34  | 6436.86  |
| 1.388                | 1869.63             | 2196.36 | 2523.09 | 3176.53  | 3829.97  | 5136.82  | 6443.76  |
| 1.389                | 1871.69             | 2198.67 | 2525.75 | 3179.90  | 3834.05  | 5142.31  | 6450.66  |
| 1.390                | 1873.55             | 2200.98 | 2528.41 | 3183.27  | 3838.13  | 5147.84  | 6457.56  |
| 1.391                | 1875.50             | 2203.29 | 2531.07 | 3186.64  | 3842.12  | 5153.35  | 6464.47  |
| 1.392                | 1877.46             | 2205.60 | 2533.73 | 3190.01  | 3846.29  | 5158.86  | 6471.38  |
| 1.393                | 1879.42             | 2207.91 | 2536.40 | 3193.38  | 3850.37  | 5164.38  | 6478.29  |
| 1.394                | 1881.38             | 2210.22 | 2539.07 | 3196.75  | 3854.45  | 5169.90  | 6485.20  |
| 1.395                | 1883.34             | 2212.54 | 2541.74 | 3200.13  | 3858.53  | 5175.32  | 6492.11  |
| 1.396                | 1885.30             | 2214.85 | 2544.40 | 3203.50  | 3862.61  | 5180.82  | 6499.03  |
| 1.397                | 1887.26             | 2217.16 | 2547.07 | 3206.88  | 3866.69  | 5186.32  | 6505.95  |
| 1.398                | 1889.22             | 2219.47 | 2549.74 | 3210.26  | 3870.78  | 5191.82  | 6512.87  |
| 1.399                | 1891.18             | 2221.79 | 2552.41 | 3213.64  | 3875.87  | 5197.32  | 6519.85  |
| 1.400                | 1893.14             | 2224.11 | 2555.08 | 3217.02  | 3878.96  | 5202.83  | 6526.71  |
| 1.401                | 1895.10             | 2226.43 | 2557.75 | 3220.40  | 3883.05  | 5208.34  | 6533.64  |
| 1.402                | 1897.06             | 2228.75 | 2560.42 | 3223.78  | 3887.14  | 5213.85  | 6540.57  |
| 1.403                | 1899.02             | 2231.07 | 2563.09 | 3227.16  | 3891.23  | 5219.36  | 6547.50  |
| 1.404                | 1900.99             | 2233.39 | 2565.77 | 3230.55  | 3895.32  | 5224.88  | 6554.43  |
| 1.405                | 1902.96             | 2235.71 | 2568.45 | 3233.94  | 3899.42  | 5230.40  | 6561.37  |
| 1.406                | 1904.92             | 2238.03 | 2571.12 | 3237.32  | 3903.52  | 5235.92  | 6568.29  |
| 1.407                | 1906.88             | 2240.35 | 2573.79 | 3240.71  | 3907.62  | 5241.44  | 6575.21  |
| 1.408                | 1908.84             | 2242.67 | 2576.46 | 3244.10  | 3911.72  | 5246.96  | 6582.14  |
| 1.409                | 1910.81             | 2244.99 | 2579.13 | 3247.49  | 3915.82  | 5252.48  | 6589.17  |
| 1.410                | 1912.79             | 2247.32 | 2581.81 | 3250.88  | 3919.92  | 5258.01  | 6596.10  |
| 1.411                | 1914.76             | 2249.64 | 2584.49 | 3254.27  | 3924.02  | 5263.54  | 6603.05  |
| 1.412                | 1916.73             | 2251.96 | 2587.18 | 3257.66  | 3928.13  | 5269.07  | 6610.00  |
| 1.413                | 1918.70             | 2254.78 | 2589.88 | 3261.05  | 3932.24  | 5274.60  | 6616.95  |
| 1.414                | 1920.67             | 2256.61 | 2592.58 | 3264.45  | 3936.35  | 5278.13  | 6623.91  |
| 1.415                | 1922.64             | 2258.94 | 2595.25 | 3267.85  | 3940.46  | 5283.67  | 6630.87  |
| 1.416                | 1924.61             | 2261.27 | 2597.93 | 3271.65  | 3944.57  | 5289.22  | 6637.73  |
| 1.417                | 1926.58             | 2263.60 | 2601.61 | 3274.05  | 3948.68  | 5292.76  | 6644.60  |
| 1.418                | 1928.55             | 2265.93 | 2604.30 | 3279.45  | 3955.79  | 5296.21  | 6651.47  |
| 1.419                | 1930.52             | 2268.26 | 2606.99 | 3280.85  | 3959.90  | 5299.65  | 6658.34  |
| 1.420                | 1932.50             | 2270.59 | 2608.68 | 3284.85  | 3961.02  | 5313.37  | 6665.71  |
| 1.421                | 1934.47             | 2272.92 | 2611.37 | 3288.25  | 3965.14  | 5318.92  | 6672.69  |
| 1.422                | 1936.44             | 2275.25 | 2614.06 | 3291.65  | 3969.26  | 5324.47  | 6679.67  |
| 1.423                | 1938.42             | 2277.58 | 2616.75 | 3295.05  | 3973.38  | 5300.02  | 6686.65  |
| 1.424                | 1940.40             | 2279.91 | 2619.44 | 3298.46  | 3977.51  | 5335.57  | 6693.63  |



| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|----------|----------|----------|----------|
|                      | 6 Feet.             | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| 1.425                | 1942.38             | 2282.25 | 2622.13 | 3301.87  | 3981.62  | 5341.12  | 6700.61  |
| 1.426                | 1944.35             | 2284.58 | 2624.83 | 3305.28  | 3985.75  | 5346.67  | 6707.60  |
| 1.427                | 1946.33             | 2286.91 | 2627.52 | 3308.69  | 3989.88  | 5352.23  | 6714.59  |
| 1.428                | 1948.31             | 2289.25 | 2630.21 | 3312.10  | 3994.01  | 5357.79  | 6721.58  |
| 1.429                | 1950.29             | 2291.59 | 2632.90 | 3315.51  | 3998.15  | 5363.35  | 6728.57  |
| 1.430                | 1952.27             | 2293.93 | 2635.60 | 3318.93  | 4002.25  | 5368.91  | 6735.57  |
| 1.431                | 1954.25             | 2296.27 | 2638.29 | 3322.34  | 4006.38  | 5374.47  | 6742.57  |
| 1.432                | 1956.23             | 2298.61 | 2640.99 | 3325.75  | 4010.51  | 5380.04  | 6749.57  |
| 1.433                | 1958.21             | 2300.95 | 2643.69 | 3329.17  | 4014.64  | 5385.61  | 6756.57  |
| 1.434                | 1960.19             | 2303.09 | 2646.39 | 3332.59  | 4018.78  | 5391.18  | 6763.57  |
| 1.435                | 1962.17             | 2305.63 | 2649.09 | 3336.01  | 4022.92  | 5396.75  | 6770.58  |
| 1.436                | 1964.15             | 2308.07 | 2651.79 | 3339.23  | 4027.06  | 5402.32  | 6777.59  |
| 1.437                | 1966.13             | 2310.31 | 2654.49 | 3342.45  | 4031.20  | 5407.90  | 6784.60  |
| 1.438                | 1968.11             | 2312.65 | 2657.19 | 3345.67  | 4035.34  | 5413.48  | 6791.61  |
| 1.439                | 1970.09             | 2315.00 | 2659.89 | 3348.89  | 4039.48  | 5419.06  | 6798.63  |
| 1.440                | 1972.09             | 2317.35 | 2662.60 | 3353.11  | 4043.62  | 5424.64  | 6805.65  |
| 1.441                | 1974.07             | 2319.69 | 2665.30 | 3356.53  | 4047.76  | 5430.22  | 6812.67  |
| 1.442                | 1976.05             | 2322.03 | 2668.00 | 3359.95  | 4051.90  | 5435.80  | 6819.70  |
| 1.443                | 1978.04             | 2324.38 | 2670.71 | 3363.38  | 4056.05  | 5441.39  | 6826.73  |
| 1.444                | 1980.03             | 2326.73 | 2673.42 | 3366.81  | 4060.20  | 5446.98  | 6833.76  |
| 1.445                | 1982.02             | 2329.08 | 2676.13 | 3370.24  | 4064.35  | 5452.57  | 6840.79  |
| 1.446                | 1984.01             | 2331.43 | 2678.84 | 3373.67  | 4068.50  | 5458.16  | 6847.80  |
| 1.447                | 1986.00             | 2333.78 | 2681.55 | 3377.10  | 4072.65  | 5463.75  | 6854.83  |
| 1.448                | 1987.99             | 2336.13 | 2684.26 | 3380.53  | 4076.80  | 5469.34  | 6861.87  |
| 1.449                | 1989.98             | 2338.48 | 2686.97 | 3383.96  | 4080.96  | 5474.94  | 6868.91  |
| 1.450                | 1991.97             | 2340.83 | 2689.69 | 3387.40  | 4085.12  | 5480.54  | 6875.97  |
| 1.451                | 1993.96             | 2343.18 | 2692.40 | 3390.83  | 4089.27  | 5486.14  | 6883.01  |
| 1.452                | 1995.95             | 2345.53 | 2695.11 | 3394.27  | 4093.43  | 5491.74  | 6890.06  |
| 1.453                | 1997.94             | 2347.88 | 2697.82 | 3397.71  | 4097.59  | 5497.34  | 6897.11  |
| 1.454                | 1999.93             | 2350.24 | 2700.54 | 3401.15  | 4101.75  | 5502.95  | 6904.16  |
| 1.455                | 2001.93             | 2352.60 | 2703.26 | 3404.59  | 4105.91  | 5508.56  | 6911.21  |
| 1.456                | 2203.92             | 2354.95 | 2705.97 | 3408.03  | 4110.07  | 5514.17  | 6918.27  |
| 1.457                | 2205.91             | 2357.30 | 2708.69 | 3411.47  | 4114.23  | 5519.78  | 6925.33  |
| 1.458                | 2207.91             | 2359.66 | 2711.41 | 3414.91  | 4118.40  | 5525.39  | 6932.39  |
| 1.459                | 2209.91             | 2362.06 | 2714.13 | 3418.35  | 4122.57  | 5531.01  | 6939.45  |
| 1.460                | 2011.91             | 2364.38 | 2716.85 | 3421.80  | 4126.74  | 5536.63  | 6946.52  |
| 1.461                | 2013.90             | 2366.74 | 2719.57 | 3425.24  | 4130.91  | 5542.25  | 6953.59  |
| 1.462                | 2015.90             | 2369.10 | 2722.29 | 3428.69  | 4135.08  | 5547.87  | 6960.66  |
| 1.463                | 2017.90             | 2371.46 | 2725.01 | 3432.14  | 4139.25  | 5553.49  | 6967.73  |
| 1.464                | 2019.90             | 2373.82 | 2727.74 | 3435.59  | 4143.43  | 5559.11  | 6974.80  |
| 1.465                | 2021.90             | 2376.18 | 2730.47 | 3439.04  | 4147.61  | 5564.74  | 6981.88  |
| 1.466                | 2023.90             | 2378.64 | 2733.19 | 3442.49  | 4151.78  | 5570.37  | 6988.96  |
| 1.467                | 2025.90             | 2380.90 | 2735.91 | 3445.94  | 4155.94  | 5576.00  | 6996.04  |
| 1.468                | 2027.90             | 2383.26 | 2738.64 | 3449.39  | 4160.14  | 5581.63  | 7003.12  |
| 1.469                | 2029.90             | 2385.63 | 2741.37 | 3452.84  | 4164.28  | 5587.26  | 7010.21  |
| 1.470                | 2031.90             | 2388.00 | 2744.10 | 3456.30  | 4168.50  | 5592.90  | 7017.30  |
| 1.471                | 2033.90             | 2390.36 | 2746.83 | 3459.75  | 4172.68  | 5598.54  | 7024.39  |
| 1.472                | 2035.90             | 2392.73 | 2749.56 | 3463.21  | 4176.86  | 5604.18  | 7031.48  |
| 1.473                | 2037.90             | 2395.10 | 2752.29 | 3466.67  | 4181.05  | 5609.82  | 7038.57  |
| 1.474                | 2039.91             | 2397.47 | 2755.02 | 3470.13  | 4185.24  | 5615.46  | 7045.67  |
| 1.475                | 2041.92             | 2399.84 | 2757.76 | 3473.59  | 4189.43  | 5621.10  | 7052.77  |
| 1.476                | 2043.92             | 2402.21 | 2760.49 | 3477.05  | 4193.62  | 5626.75  | 7059.87  |
| 1.477                | 2045.92             | 2404.58 | 2763.22 | 3480.51  | 4197.81  | 5632.41  | 7066.97  |
| 1.478                | 2047.93             | 2406.95 | 2765.95 | 3483.97  | 4202.00  | 5638.06  | 7074.08  |
| 1.479                | 2049.94             | 2409.32 | 2768.69 | 3487.44  | 4206.09  | 5643.72  | 7081.19  |
| 1.480                | 2051.95             | 2411.69 | 2771.43 | 3490.91  | 4210.39  | 5649.36  | 7088.30  |
| 1.481                | 2053.96             | 2414.06 | 2774.10 | 3494.38  | 4214.58  | 5655.04  | 7095.42  |
| 1.482                | 2055.97             | 2416.43 | 2776.77 | 3497.85  | 4218.78  | 5660.70  | 7102.54  |

## LENGTH OF THE WEIR.

| Depth on Weir. | LENGTH OF THE WEIR. |         |         |          |          |          |          |
|----------------|---------------------|---------|---------|----------|----------|----------|----------|
| Feet.          | 6 Feet.             | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| 1.483          | 2057.98             | 2418.80 | 2779.44 | 3501.32  | 4222.98  | 5666.36  | 7109.66  |
| 1.484          | 2059.99             | 2421.18 | 2782.12 | 3504.79  | 4227.18  | 5672.02  | 7116.78  |
| 1.485          | 2062.00             | 2423.56 | 2785.13 | 3508.26  | 4231.38  | 5677.64  | 7123.90  |
| 1.486          | 2064.01             | 2425.93 | 2787.87 | 3511.73  | 4235.58  | 5683.30  | 7131.62  |
| 1.487          | 2066.02             | 2428.31 | 2790.61 | 3515.20  | 4239.78  | 5688.96  | 7138.15  |
| 1.488          | 2068.03             | 2430.69 | 2793.35 | 3518.67  | 4243.99  | 5694.63  | 7145.28  |
| 1.489          | 2070.04             | 2433.07 | 2796.09 | 3512.15  | 4248.20  | 5700.30  | 7152.41  |
| 1.490          | 2072.06             | 2435.45 | 2798.84 | 3525.63  | 4252.41  | 5705.97  | 7159.54  |
| 1.491          | 2074.07             | 2437.83 | 2801.58 | 3529.10  | 4256.62  | 5711.64  | 7166.68  |
| 1.492          | 2076.08             | 2440.21 | 2804.33 | 3532.58  | 4260.83  | 5717.31  | 7173.82  |
| 1.493          | 2078.09             | 2442.59 | 2807.08 | 3536.06  | 4265.04  | 5722.99  | 7180.96  |
| 1.494          | 2080.11             | 2444.97 | 2809.83 | 3539.54  | 4269.25  | 5728.67  | 7188.10  |
| 1.495          | 2082.13             | 2447.35 | 2812.58 | 3543.02  | 4273.47  | 5734.35  | 7195.24  |
| 1.496          | 2084.14             | 2449.73 | 2815.33 | 3546.50  | 4277.68  | 5740.03  | 7202.39  |
| 1.497          | 2086.16             | 2452.11 | 2818.08 | 3549.98  | 4281.90  | 5745.71  | 7209.54  |
| 1.498          | 2088.18             | 2454.50 | 2820.83 | 3553.46  | 4286.12  | 5751.40  | 7216.69  |
| 1.499          | 2090.20             | 2456.89 | 2823.58 | 3556.95  | 4290.34  | 5757.09  | 7223.84  |
| 1.500          | 2092.22             | 2459.28 | 2826.33 | 3560.44  | 4294.56  | 5762.78  | 7231.00  |
| 1.501          | 2094.24             | 2461.66 | 2829.08 | 3563.93  | 4298.78  | 5768.47  | 7238.16  |
| 1.502          | 2096.26             | 2464.04 | 2831.83 | 3567.42  | 4303.00  | 5774.16  | 7245.32  |
| 1.503          | 2098.28             | 2466.43 | 2834.59 | 3570.91  | 4307.22  | 5779.85  | 7252.48  |
| 1.504          | 2100.30             | 2468.82 | 2837.35 | 3574.40  | 4311.45  | 5785.55  | 7259.65  |
| 1.505          | 2102.32             | 2471.21 | 2840.11 | 3577.89  | 4315.68  | 5791.25  | 7266.82  |
| 1.506          | 2104.34             | 2473.60 | 2842.86 | 3581.38  | 4319.91  | 5796.95  | 7273.99  |
| 1.507          | 2106.36             | 2475.99 | 2845.62 | 3584.87  | 4324.14  | 5802.65  | 7281.16  |
| 1.508          | 2108.38             | 2478.38 | 2848.38 | 3588.36  | 4328.37  | 5808.35  | 7288.33  |
| 1.509          | 2110.41             | 2480.77 | 2851.14 | 3591.86  | 4332.60  | 5814.05  | 7295.51  |
| 1.510          | 2112.43             | 2483.17 | 2853.90 | 3595.36  | 4336.83  | 5819.76  | 7302.69  |
| 1.511          | 2114.45             | 2485.56 | 2856.66 | 3598.86  | 4341.06  | 5825.47  | 7309.87  |
| 1.512          | 2116.47             | 2487.95 | 2859.42 | 3602.36  | 4345.30  | 5831.18  | 7317.05  |
| 1.513          | 2118.50             | 2490.34 | 2862.18 | 3605.86  | 4349.54  | 5836.89  | 7324.24  |
| 1.514          | 2020.53             | 2492.74 | 2864.94 | 3609.36  | 4353.78  | 5842.60  | 7331.43  |
| 1.515          | 2122.56             | 2495.14 | 2867.71 | 3612.86  | 4358.02  | 5848.32  | 7338.62  |
| 1.516          | 2124.58             | 2497.53 | 2870.47 | 3616.36  | 4362.20  | 5854.04  | 7345.81  |
| 1.517          | 2126.61             | 2499.93 | 2873.24 | 3619.86  | 4366.44  | 5859.76  | 7353.01  |
| 1.518          | 2128.64             | 2502.33 | 2876.01 | 3623.37  | 4370.68  | 5865.48  | 7360.21  |
| 1.519          | 2130.67             | 2504.73 | 2878.78 | 3626.88  | 4374.92  | 5871.20  | 7367.41  |
| 1.520          | 2132.70             | 2507.13 | 2881.55 | 3630.39  | 4379.23  | 5876.92  | 7374.61  |
| 1.521          | 2134.73             | 2509.53 | 2884.32 | 3633.90  | 4383.48  | 5882.64  | 7381.81  |
| 1.522          | 2136.76             | 2511.93 | 2887.09 | 3637.41  | 4387.73  | 5888.37  | 7389.02  |
| 1.523          | 2138.79             | 2514.33 | 2889.86 | 3640.92  | 4391.98  | 5894.10  | 7396.23  |
| 1.524          | 2140.83             | 2516.73 | 2892.63 | 3644.43  | 4396.23  | 5899.83  | 7403.44  |
| 1.525          | 2142.86             | 2519.13 | 2895.40 | 3647.94  | 4400.48  | 5905.56  | 7410.65  |
| 1.526          | 2144.89             | 2521.53 | 2898.17 | 3651.45  | 4404.73  | 5911.29  | 7417.86  |
| 1.527          | 2146.92             | 2523.93 | 2900.94 | 3654.96  | 4408.98  | 5917.03  | 7425.08  |
| 1.528          | 2148.95             | 2526.33 | 2903.72 | 3658.48  | 4413.24  | 5922.77  | 7432.20  |
| 1.529          | 2151.00             | 2528.74 | 2906.50 | 3662.00  | 4417.50  | 5928.51  | 7439.52  |
| 1.530          | 2153.03             | 2531.15 | 2909.28 | 3665.52  | 4421.76  | 5934.25  | 7446.74  |
| 1.531          | 2155.06             | 2533.55 | 2912.05 | 3669.04  | 4426.02  | 5939.99  | 7453.97  |
| 1.532          | 2157.10             | 2535.96 | 2914.83 | 3672.56  | 4430.28  | 5945.74  | 7461.20  |
| 1.533          | 2159.14             | 2538.37 | 2917.61 | 3676.08  | 4434.54  | 5951.49  | 7468.43  |
| 1.534          | 2161.28             | 2540.78 | 2920.39 | 3679.60  | 4438.81  | 5957.24  | 7475.66  |
| 1.535          | 2163.21             | 2543.19 | 2923.17 | 3683.12  | 4443.08  | 5962.99  | 7482.90  |
| 1.536          | 2165.25             | 2545.60 | 2925.95 | 3686.64  | 4447.34  | 5968.74  | 7490.14  |
| 1.537          | 2167.29             | 2548.01 | 2928.73 | 3690.16  | 4451.61  | 5974.49  | 7497.38  |
| 1.538          | 2169.33             | 2550.42 | 2931.51 | 3693.69  | 4455.88  | 5980.25  | 7504.62  |
| 1.539          | 2171.37             | 2552.83 | 2934.29 | 3697.22  | 4460.15  | 5986.00  | 7511.86  |
| 1.540          | 2173.41             | 2555.24 | 2937.08 | 3700.75  | 4464.42  | 5991.77  | 7519.11  |

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|----------|----------|----------|----------|
|                      | 6 Feet.             | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| 1.541                | 2175.45             | 2557.65 | 2939.80 | 3704.28  | 4468.69  | 5997.53  | 7526.36  |
| 1.542                | 2177.49             | 2569.06 | 2942.64 | 3707.81  | 4472.96  | 6003.29  | 7533.61  |
| 1.543                | 2179.53             | 2562.48 | 2945.43 | 3711.34  | 4477.18  | 6009.05  | 7540.86  |
| 1.544                | 2181.57             | 2564.90 | 2948.22 | 3714.87  | 4481.38  | 6014.82  | 7548.11  |
| 1.545                | 2183.62             | 2567.32 | 2951.01 | 3718.41  | 4485.80  | 6020.59  | 7555.37  |
| 1.546                | 2185.66             | 2569.73 | 2953.80 | 3721.94  | 4490.08  | 6026.56  | 7562.63  |
| 1.547                | 2187.70             | 2572.14 | 2956.59 | 3725.47  | 4494.36  | 6032.33  | 7569.89  |
| 1.548                | 2189.75             | 2574.56 | 2959.38 | 3729.01  | 4498.64  | 6038.10  | 7577.15  |
| 1.549                | 2191.80             | 2576.98 | 2962.17 | 3732.55  | 4502.92  | 6043.87  | 7584.42  |
| 1.550                | 2193.85             | 2579.40 | 2964.96 | 3736.09  | 4507.21  | 6049.45  | 7591.69  |
| 1.551                | 2195.89             | 2581.82 | 2967.75 | 3739.63  | 4511.49  | 6055.23  | 7598.96  |
| 1.552                | 2197.93             | 2584.24 | 2970.54 | 3743.17  | 4515.78  | 6061.01  | 7606.23  |
| 1.553                | 2199.98             | 2586.66 | 2973.33 | 3746.71  | 4520.07  | 6066.79  | 7613.51  |
| 1.554                | 2202.03             | 2589.08 | 2976.13 | 3750.25  | 4524.36  | 6072.57  | 7620.79  |
| 1.555                | 2204.08             | 2591.51 | 2978.93 | 3753.79  | 4528.65  | 6078.36  | 7628.07  |
| 1.556                | 2206.13             | 2593.93 | 2981.72 | 3757.33  | 4532.94  | 6084.15  | 7635.35  |
| 1.557                | 2208.18             | 2596.35 | 2984.52 | 3760.87  | 4537.23  | 6089.94  | 7642.63  |
| 1.558                | 2210.23             | 2598.77 | 2987.32 | 3764.41  | 4541.52  | 6095.73  | 7649.92  |
| 1.559                | 2212.28             | 2601.20 | 2990.01 | 3767.95  | 4545.82  | 6101.52  | 7657.21  |
| 1.560                | 2214.33             | 2603.63 | 2992.92 | 3771.52  | 4550.12  | 6107.31  | 7664.50  |
| 1.561                | 2216.38             | 2606.05 | 2995.72 | 3775.57  | 4554.42  | 6113.10  | 7671.79  |
| 1.562                | 2218.43             | 2608.47 | 2998.52 | 3778.62  | 4558.72  | 6118.90  | 7679.09  |
| 1.563                | 2220.48             | 2610.90 | 3001.32 | 3782.17  | 4563.02  | 6124.70  | 7686.39  |
| 1.564                | 2222.54             | 2613.33 | 3004.12 | 3785.72  | 4567.02  | 6130.50  | 7693.69  |
| 1.565                | 2224.59             | 2615.76 | 3006.93 | 3789.28  | 4571.62  | 6136.30  | 7700.99  |
| 1.566                | 2226.64             | 2618.19 | 3009.73 | 3792.83  | 4575.92  | 6142.10  | 7708.29  |
| 1.567                | 2228.69             | 2620.62 | 3012.53 | 3796.38  | 4580.22  | 6147.91  | 7715.30  |
| 1.568                | 2230.75             | 2623.05 | 3015.34 | 3799.94  | 4584.53  | 6153.72  | 7722.61  |
| 1.569                | 2232.81             | 2625.48 | 3018.15 | 3803.50  | 4588.84  | 6159.53  | 7729.92  |
| 1.570                | 2234.87             | 2627.92 | 3020.96 | 3807.06  | 4593.15  | 6165.34  | 7737.53  |
| 1.571                | 2236.91             | 2630.35 | 3023.77 | 3810.62  | 4597.46  | 6171.15  | 7744.85  |
| 1.572                | 2238.95             | 2632.78 | 3026.58 | 3814.18  | 4601.77  | 6176.96  | 7752.17  |
| 1.573                | 2240.99             | 2635.21 | 3029.39 | 3817.74  | 4606.08  | 6182.78  | 7759.49  |
| 1.574                | 2243.04             | 2637.64 | 3032.20 | 3821.30  | 4610.40  | 6188.60  | 7766.81  |
| 1.575                | 2245.16             | 2640.08 | 3035.01 | 3824.86  | 4614.72  | 6194.42  | 7774.13  |
| 1.576                | 2247.22             | 2642.51 | 3037.82 | 3828.42  | 4619.03  | 6200.24  | 7781.46  |
| 1.577                | 2249.28             | 2644.95 | 3040.63 | 3831.98  | 4623.35  | 6206.06  | 7788.79  |
| 1.578                | 2251.34             | 2647.39 | 3043.44 | 3835.55  | 4627.67  | 6211.89  | 7796.12  |
| 1.579                | 2253.40             | 2649.83 | 3046.26 | 3838.12  | 4631.99  | 6217.72  | 7803.45  |
| 1.580                | 2255.46             | 2652.27 | 3049.08 | 3842.69  | 4636.31  | 6223.55  | 7810.78  |
| 1.581                | 2257.52             | 2654.71 | 3051.89 | 3846.25  | 4640.63  | 6229.38  | 7818.12  |
| 1.582                | 2259.58             | 2657.15 | 3054.70 | 3849.81  | 4644.95  | 6235.21  | 7825.46  |
| 1.583                | 2261.64             | 2659.59 | 3057.52 | 3853.37  | 4649.28  | 6241.04  | 7832.80  |
| 1.584                | 2263.71             | 2662.03 | 3060.34 | 3856.93  | 4653.60  | 6246.87  | 7840.14  |
| 1.585                | 2265.78             | 2664.47 | 3063.16 | 3860.55  | 4657.94  | 6252.71  | 7847.49  |
| 1.586                | 2267.84             | 2666.91 | 3065.98 | 3864.12  | 4662.27  | 6258.55  | 7854.84  |
| 1.587                | 2269.90             | 2669.35 | 3068.80 | 3867.69  | 4666.60  | 6264.39  | 7862.19  |
| 1.588                | 2271.97             | 2671.79 | 3071.62 | 3871.27  | 4670.93  | 6270.23  | 7869.54  |
| 1.589                | 2274.04             | 2674.24 | 3074.44 | 3874.85  | 4675.26  | 6276.07  | 7876.89  |
| 1.590                | 2276.11             | 2676.69 | 3077.27 | 3878.43  | 4679.60  | 6281.92  | 7884.25  |
| 1.591                | 2278.17             | 2679.13 | 3080.09 | 3882.01  | 4683.93  | 6287.77  | 7892.61  |
| 1.592                | 2280.24             | 2681.57 | 3082.91 | 3885.59  | 4688.26  | 6293.65  | 7899.97  |
| 1.593                | 2282.31             | 2684.02 | 3085.73 | 3889.17  | 4692.60  | 6299.55  | 7907.33  |
| 1.594                | 2284.38             | 2686.47 | 3088.56 | 3892.75  | 4696.94  | 6305.40  | 7914.70  |
| 1.595                | 2286.45             | 2688.92 | 3091.39 | 3896.34  | 4701.28  | 6311.18  | 7921.07  |
| 1.596                | 2288.51             | 2691.37 | 3094.22 | 3899.92  | 4705.62  | 6317.03  | 7928.44  |
| 1.597                | 2290.58             | 2693.82 | 3097.05 | 3903.50  | 4709.96  | 6322.89  | 7936.81  |
| 1.598                | 2292.65             | 2696.27 | 3099.88 | 3907.09  | 4714.30  | 6328.75  | 7944.18  |

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|----------|----------|----------|----------|
|                      | 6 Feet.             | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| 1.599                | 2294.72             | 2698.72 | 3102.71 | 3910.68  | 4718.65  | 6334.61  | 7951.56  |
| 1.600                | 2296.80             | 2701.17 | 3105.54 | 3914.27  | 4723.00  | 6340.47  | 7957.94  |
| 1.601                | 2298.87             | 2703.62 | 3108.37 | 3917.86  | 4727.35  | 6346.33  | 7965.32  |
| 1.602                | 2300.94             | 2706.07 | 3111.20 | 3921.45  | 4731.70  | 6352.20  | 7973.70  |
| 1.603                | 2303.02             | 2708.52 | 3114.03 | 3925.04  | 4736.05  | 6358.07  | 7981.08  |
| 1.604                | 2305.19             | 2710.97 | 3116.86 | 3928.63  | 4740.40  | 6363.94  | 7988.48  |
| 1.605                | 2307.17             | 2713.43 | 3119.70 | 3932.23  | 4744.75  | 6369.81  | 7994.86  |
| 1.606                | 2309.24             | 2715.88 | 3122.53 | 3935.82  | 4749.10  | 6375.68  | 8002.25  |
| 1.607                | 2311.31             | 2518.34 | 3125.36 | 3939.41  | 4753.46  | 6381.55  | 8009.64  |
| 1.608                | 2313.39             | 2520.80 | 3128.20 | 3943.01  | 4757.82  | 6388.43  | 8017.04  |
| 1.609                | 2315.47             | 2523.26 | 3131.04 | 3946.61  | 4762.18  | 6394.31  | 8024.44  |
| 1.610                | 2317.55             | 2725.72 | 3133.88 | 3950.21  | 4766.54  | 6399.19  | 8031.84  |
| 1.611                | 2319.63             | 2728.17 | 3136.72 | 3953.81  | 4770.90  | 6405.07  | 8039.24  |
| 1.612                | 2321.71             | 2730.63 | 3139.56 | 3957.41  | 4775.26  | 6410.95  | 8046.65  |
| 1.613                | 2323.89             | 2733.09 | 3142.44 | 3961.01  | 4779.62  | 6416.83  | 8054.06  |
| 1.614                | 2325.97             | 2735.55 | 3145.28 | 3964.61  | 4783.98  | 6422.72  | 8061.47  |
| 1.615                | 2327.95             | 2738.01 | 3148.08 | 3968.21  | 4788.34  | 6428.61  | 8068.88  |
| 1.616                | 2330.03             | 2740.47 | 3150.92 | 3971.81  | 4792.71  | 6434.50  | 8076.29  |
| 1.617                | 2332.11             | 2742.93 | 3153.76 | 3975.41  | 4797.08  | 6440.39  | 8083.71  |
| 1.618                | 2334.19             | 2745.40 | 3156.60 | 3979.02  | 4801.45  | 6446.28  | 8091.13  |
| 1.619                | 2336.28             | 2747.87 | 3159.45 | 3982.63  | 4806.82  | 6452.18  | 8098.55  |
| 1.620                | 2338.36             | 2750.33 | 3162.30 | 3986.24  | 4810.19  | 6458.08  | 8105.97  |
| 1.621                | 2340.44             | 2752.79 | 3165.14 | 3989.85  | 4814.56  | 6463.98  | 8113.39  |
| 1.622                | 2342.52             | 2755.25 | 3167.99 | 3993.45  | 4818.93  | 6469.88  | 8120.82  |
| 1.623                | 2344.60             | 2757.72 | 3170.84 | 3997.06  | 4823.30  | 6475.78  | 8128.25  |
| 1.624                | 2346.69             | 2760.19 | 3173.69 | 4000.67  | 4827.68  | 6481.68  | 8135.68  |
| 1.625                | 2348.78             | 2762.66 | 3176.54 | 4004.30  | 4832.06  | 6487.58  | 8143.11  |
| 1.626                | 2350.86             | 2765.12 | 3179.39 | 4007.91  | 4836.44  | 6493.49  | 8150.55  |
| 1.627                | 2352.94             | 2767.59 | 3182.24 | 4011.52  | 4840.82  | 6499.40  | 8157.99  |
| 1.628                | 2355.03             | 2770.06 | 3185.09 | 4015.14  | 4845.10  | 6505.31  | 8165.43  |
| 1.629                | 2357.12             | 2772.53 | 3187.94 | 4018.76  | 4849.48  | 6511.22  | 8172.87  |
| 1.630                | 2359.21             | 2775.00 | 3190.79 | 4022.38  | 4853.97  | 6517.13  | 8180.31  |
| 1.631                | 2361.29             | 2777.47 | 3193.64 | 4026.00  | 4858.35  | 6523.05  | 8187.76  |
| 1.632                | 2363.38             | 2779.94 | 3196.49 | 4029.62  | 4862.73  | 6528.97  | 8195.21  |
| 1.633                | 2365.47             | 2782.41 | 3199.35 | 4033.24  | 4867.12  | 6534.89  | 8202.66  |
| 1.634                | 2367.56             | 2784.88 | 3202.21 | 4036.86  | 4871.51  | 6540.81  | 8210.11  |
| 1.635                | 2369.65             | 2787.36 | 3205.07 | 4040.48  | 4875.90  | 6546.73  | 8217.56  |
| 1.636                | 2371.74             | 2789.83 | 3207.92 | 4044.10  | 4880.29  | 6552.65  | 8225.02  |
| 1.637                | 2373.83             | 2792.30 | 3210.78 | 4047.72  | 4884.68  | 6558.57  | 8232.48  |
| 1.638                | 2375.92             | 2794.78 | 3213.64 | 4051.35  | 4889.07  | 6564.50  | 8239.94  |
| 1.639                | 2378.01             | 2797.26 | 3216.50 | 4054.98  | 4893.46  | 6570.43  | 8247.40  |
| 1.640                | 2380.11             | 2799.74 | 3219.36 | 4058.61  | 4897.86  | 6576.36  | 8254.86  |
| 1.641                | 2382.20             | 2802.21 | 3222.22 | 4062.24  | 4902.26  | 6582.29  | 8262.33  |
| 1.642                | 2384.29             | 2804.69 | 3225.08 | 4065.87  | 4906.66  | 6588.22  | 8269.80  |
| 1.643                | 2386.38             | 2807.17 | 3227.94 | 4069.50  | 4911.06  | 6594.16  | 8277.27  |
| 1.644                | 2388.48             | 2809.65 | 3230.80 | 4073.13  | 4915.46  | 6600.10  | 8284.74  |
| 1.645                | 2390.58             | 2812.13 | 3233.67 | 4076.76  | 4919.86  | 6606.04  | 8292.22  |
| 1.646                | 2392.67             | 2814.61 | 3236.53 | 4080.39  | 4924.26  | 6611.98  | 8299.70  |
| 1.647                | 2394.77             | 2817.09 | 3239.40 | 4084.02  | 4928.66  | 6617.93  | 8307.18  |
| 1.648                | 2396.87             | 2819.57 | 3242.27 | 4087.66  | 4933.06  | 6623.87  | 8314.66  |
| 1.649                | 2398.97             | 2822.05 | 3245.14 | 4091.30  | 4937.47  | 6629.81  | 8322.14  |
| 1.650                | 2401.07             | 2824.54 | 3248.01 | 4094.94  | 4941.88  | 6635.75  | 8329.63  |
| 1.651                | 2403.16             | 2827.02 | 3250.87 | 4098.58  | 4946.29  | 6641.70  | 8337.12  |
| 1.652                | 2405.26             | 2829.50 | 3253.74 | 4102.22  | 4950.70  | 6647.65  | 8344.61  |
| 1.653                | 2407.36             | 2831.98 | 3256.61 | 4105.86  | 4955.11  | 6653.60  | 8352.10  |
| 1.654                | 2409.46             | 2834.47 | 3259.54 | 4109.58  | 4959.52  | 6659.55  | 8359.60  |
| 1.655                | 2411.56             | 2836.96 | 3262.35 | 4113.15  | 4963.94  | 6665.51  | 8367.10  |
| 1.656                | 2413.66             | 2839.44 | 3265.22 | 4116.79  | 4968.35  | 6671.47  | 8374.60  |

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|----------|----------|----------|----------|
|                      | 6 Feet.             | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| 1.657                | 2413.76             | 2841.93 | 3268.09 | 4120.43  | 4972.76  | 6677.43  | 8382.10  |
| 1.658                | 2417.86             | 2844.42 | 3270.96 | 4124.07  | 4977.18  | 6683.39  | 8389.60  |
| 1.659                | 2419.96             | 2846.91 | 3273.84 | 4127.71  | 4981.60  | 6689.35  | 8397.11  |
| 1.660                | 2422.07             | 2849.40 | 3276.72 | 4131.37  | 4986.02  | 6695.32  | 8404.62  |
| 1.661                | 2424.17             | 2851.89 | 3279.59 | 4135.02  | 4990.44  | 6701.28  | 8412.13  |
| 1.662                | 2426.27             | 2854.34 | 3282.47 | 4138.67  | 4994.86  | 6707.25  | 8419.64  |
| 1.663                | 2428.37             | 2856.79 | 3285.35 | 4142.32  | 4999.28  | 6713.22  | 8427.15  |
| 1.664                | 2430.48             | 2859.24 | 3288.23 | 4145.97  | 5004.70  | 6719.19  | 8434.67  |
| 1.665                | 2432.59             | 2861.85 | 3291.11 | 4149.62  | 5008.13  | 6725.16  | 8442.19  |
| 1.666                | 2434.69             | 2864.34 | 3293.99 | 4153.07  | 5012.56  | 6731.03  | 8449.71  |
| 1.667                | 2436.80             | 2866.83 | 3296.87 | 4156.52  | 5016.99  | 6736.90  | 8457.23  |
| 1.668                | 2438.91             | 2869.32 | 3299.75 | 4159.98  | 5021.42  | 6742.78  | 8464.75  |
| 1.669                | 2440.02             | 2871.82 | 3302.63 | 4163.44  | 5025.85  | 6748.66  | 8472.28  |
| 1.670                | 2443.13             | 2874.32 | 3305.51 | 4167.90  | 5030.28  | 6755.04  | 8479.81  |
| 1.671                | 2445.24             | 2876.81 | 3308.39 | 4171.56  | 5034.71  | 6761.02  | 8487.34  |
| 1.672                | 2447.35             | 2879.31 | 3311.27 | 4175.22  | 5039.14  | 6767.00  | 8494.87  |
| 1.673                | 2449.46             | 2881.81 | 3314.16 | 4178.88  | 5043.57  | 6772.99  | 8502.41  |
| 1.674                | 2451.57             | 2884.31 | 3317.05 | 4182.54  | 5048.01  | 6778.98  | 8509.95  |
| 1.675                | 2453.68             | 2886.81 | 3319.94 | 4186.20  | 5052.45  | 6784.97  | 8517.49  |
| 1.676                | 2455.79             | 2889.30 | 3322.82 | 4189.86  | 5056.89  | 6790.96  | 8525.03  |
| 1.677                | 2457.90             | 2891.80 | 3325.71 | 4193.52  | 5061.33  | 6796.95  | 8532.57  |
| 1.678                | 2460.01             | 2894.30 | 3328.60 | 4197.18  | 5065.77  | 6802.94  | 8540.12  |
| 1.679                | 2462.12             | 2896.80 | 3331.49 | 4200.85  | 5070.21  | 6808.94  | 8547.67  |
| 1.680                | 2464.24             | 2899.31 | 3334.38 | 4204.52  | 5074.66  | 6814.94  | 8555.22  |
| 1.681                | 2466.35             | 2901.81 | 3337.27 | 4208.19  | 5079.10  | 6820.94  | 8562.77  |
| 1.682                | 2468.46             | 2904.31 | 3340.16 | 4211.86  | 5083.54  | 6826.94  | 8570.33  |
| 1.683                | 2470.58             | 2906.81 | 3343.05 | 4215.53  | 5087.99  | 6832.94  | 8577.89  |
| 1.684                | 2472.70             | 2909.31 | 3345.94 | 4219.20  | 5092.44  | 6838.94  | 8585.45  |
| 1.685                | 2474.81             | 2911.82 | 3348.84 | 4222.87  | 5096.89  | 6844.95  | 8593.01  |
| 1.686                | 2476.92             | 2914.32 | 3351.73 | 4226.54  | 5101.34  | 6850.96  | 8600.57  |
| 1.687                | 2479.03             | 2916.83 | 3354.62 | 4230.21  | 5105.79  | 6856.97  | 8608.13  |
| 1.688                | 2481.15             | 2919.34 | 3357.52 | 4233.88  | 5110.24  | 6862.98  | 8615.70  |
| 1.689                | 2483.27             | 2921.85 | 3360.42 | 4237.55  | 5114.70  | 6868.99  | 8623.27  |
| 1.690                | 2485.39             | 2924.36 | 3363.32 | 4241.24  | 5119.16  | 6875.00  | 8630.84  |
| 1.691                | 2487.51             | 2926.86 | 3366.21 | 4244.91  | 5123.61  | 6881.01  | 8638.41  |
| 1.692                | 2489.63             | 2929.37 | 3369.11 | 4248.59  | 5128.07  | 6887.03  | 8645.99  |
| 1.693                | 2491.75             | 2931.88 | 3372.01 | 4252.27  | 5132.53  | 6893.05  | 8653.57  |
| 1.694                | 2493.87             | 2934.39 | 3374.91 | 4255.95  | 5136.99  | 6899.07  | 8661.15  |
| 1.695                | 2495.99             | 2936.90 | 3377.81 | 4259.63  | 5141.45  | 6905.09  | 8668.73  |
| 1.696                | 2498.11             | 2939.41 | 3380.71 | 4263.31  | 5145.91  | 6911.11  | 8676.31  |
| 1.697                | 2500.23             | 2941.92 | 3383.61 | 4266.99  | 5150.37  | 6917.13  | 8683.90  |
| 1.698                | 2502.35             | 2944.43 | 3386.51 | 4270.67  | 5154.88  | 6923.16  | 8691.49  |
| 1.699                | 2504.47             | 2946.94 | 3389.42 | 4274.36  | 5159.31  | 6929.18  | 8699.08  |
| 1.700                | 2506.60             | 2949.46 | 3392.33 | 4278.05  | 5163.78  | 6935.22  | 8706.67  |
| 1.701                | 2508.72             | 2951.97 | 3395.23 | 4281.74  | 5168.25  | 6941.25  | 8714.27  |
| 1.702                | 2510.84             | 2954.48 | 3398.13 | 4285.43  | 5172.72  | 6947.28  | 8721.87  |
| 1.703                | 2512.97             | 2957.00 | 3401.04 | 4289.12  | 5177.19  | 6953.32  | 8729.47  |
| 1.704                | 2515.10             | 2959.52 | 3403.95 | 4292.81  | 5181.66  | 6959.36  | 8737.07  |
| 1.705                | 2517.22             | 2962.04 | 3406.86 | 4296.50  | 5186.13  | 6965.40  | 8744.67  |
| 1.706                | 2519.34             | 2964.55 | 3409.77 | 4201.19  | 5190.60  | 6971.44  | 8752.28  |
| 1.707                | 2521.47             | 2967.07 | 3412.68 | 4204.88  | 5195.07  | 6977.48  | 8759.89  |
| 1.708                | 2523.60             | 2969.59 | 3415.59 | 4208.57  | 5199.55  | 6983.52  | 8767.50  |
| 1.709                | 2525.73             | 2972.11 | 3418.50 | 4212.26  | 5204.03  | 6989.57  | 8775.11  |
| 1.710                | 2527.86             | 2974.63 | 3421.41 | 4314.96  | 5208.51  | 6995.61  | 8782.72  |
| 1.711                | 2529.99             | 2977.15 | 3424.32 | 4318.65  | 5212.99  | 7001.66  | 8790.33  |
| 1.712                | 2532.10             | 2979.67 | 3427.23 | 4322.35  | 5217.47  | 7007.71  | 8797.94  |
| 1.713                | 2534.23             | 2982.19 | 3430.14 | 4326.05  | 5221.96  | 7013.76  | 8805.56  |
| 1.714                | 2536.36             | 2984.71 | 3433.06 | 4329.75  | 5226.45  | 7019.81  | 8813.18  |



| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|----------|----------|----------|----------|
|                      | 6 Feet.             | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| 1.715                | 2538.50             | 2987.24 | 3435.98 | 4333.45  | 5230.94  | 7025.87  | 8820.82  |
| 1.716                | 2540.63             | 2989.76 | 3438.89 | 4337.15  | 5235.42  | 7031.93  | 8828.45  |
| 1.717                | 2542.76             | 2992.28 | 3441.80 | 4340.85  | 5239.90  | 7037.99  | 8836.08  |
| 1.718                | 2544.89             | 2994.80 | 3444.72 | 4344.55  | 5243.38  | 7044.05  | 8843.71  |
| 1.719                | 2547.03             | 2997.33 | 3447.64 | 4348.25  | 5247.87  | 7050.11  | 8851.34  |
| 1.720                | 2549.16             | 2999.86 | 3450.56 | 4351.96  | 5253.36  | 7056.17  | 8858.97  |
| 1.721                | 2551.29             | 3002.38 | 3453.48 | 4355.66  | 5257.85  | 7062.23  | 8866.61  |
| 1.722                | 2553.42             | 3004.91 | 3456.40 | 4359.37  | 5262.34  | 7066.30  | 8874.25  |
| 1.723                | 2555.55             | 3007.44 | 3459.32 | 4363.08  | 5266.84  | 7073.37  | 8881.89  |
| 1.724                | 2557.69             | 3009.97 | 3462.24 | 4366.79  | 5271.34  | 7079.43  | 8889.53  |
| 1.725                | 2559.83             | 3012.50 | 3465.17 | 4370.50  | 5275.84  | 7086.51  | 8897.17  |
| 1.726                | 2561.96             | 3015.03 | 3468.09 | 4374.21  | 5280.34  | 7092.58  | 8904.82  |
| 1.727                | 2563.10             | 3017.56 | 3471.01 | 4377.92  | 5284.84  | 7098.65  | 8912.47  |
| 1.728                | 2565.24             | 3020.09 | 3473.93 | 4381.63  | 5289.34  | 7104.72  | 8920.12  |
| 1.729                | 2567.38             | 3022.62 | 3476.86 | 4385.34  | 5293.84  | 7110.80  | 8927.77  |
| 1.730                | 2570.52             | 3025.15 | 3479.79 | 4389.06  | 5298.34  | 7116.88  | 8935.43  |
| 1.731                | 2572.65             | 3027.68 | 3482.71 | 4392.77  | 5302.84  | 7122.96  | 8943.09  |
| 1.732                | 2574.79             | 3030.21 | 3485.64 | 4396.49  | 5307.34  | 7129.04  | 8950.75  |
| 1.733                | 2576.93             | 3032.74 | 3488.57 | 4400.21  | 5311.85  | 7135.12  | 8958.41  |
| 1.734                | 2579.07             | 3035.28 | 3491.50 | 4403.93  | 5316.36  | 7141.21  | 8966.07  |
| 1.735                | 2581.21             | 3037.82 | 3494.43 | 4407.65  | 5320.87  | 7147.30  | 8973.74  |
| 1.736                | 2583.35             | 3040.35 | 3497.36 | 4411.36  | 5325.37  | 7153.39  | 8981.41  |
| 1.737                | 2585.49             | 3042.88 | 3500.29 | 4415.07  | 5329.84  | 7159.48  | 8989.08  |
| 1.738                | 2587.63             | 3045.42 | 3503.22 | 4418.78  | 5334.37  | 7165.57  | 8996.75  |
| 1.739                | 2589.78             | 3047.96 | 3506.15 | 4422.49  | 5338.90  | 7171.66  | 9004.42  |
| 1.740                | 2591.92             | 3050.50 | 3509.09 | 4426.20  | 5343.43  | 7177.76  | 9012.10  |
| 1.741                | 2594.06             | 3053.04 | 3512.02 | 4429.93  | 5347.94  | 7183.86  | 9019.78  |
| 1.742                | 2596.20             | 3055.58 | 3514.95 | 4433.67  | 5352.45  | 7189.96  | 9027.46  |
| 1.743                | 2598.34             | 3058.12 | 3517.88 | 4437.41  | 5356.97  | 7196.06  | 9035.14  |
| 1.744                | 2600.49             | 3060.66 | 3520.82 | 4441.15  | 5361.49  | 7202.16  | 9042.82  |
| 1.745                | 2602.64             | 3063.20 | 3523.76 | 4444.89  | 5366.01  | 7208.26  | 9050.51  |
| 1.746                | 2604.78             | 3065.74 | 3526.70 | 4448.62  | 5370.53  | 7214.36  | 9058.20  |
| 1.747                | 2606.92             | 3068.28 | 3529.64 | 4452.35  | 5375.05  | 7220.47  | 9065.89  |
| 1.748                | 2609.07             | 3070.82 | 3532.98 | 4456.08  | 5379.57  | 7226.58  | 9073.58  |
| 1.749                | 2611.22             | 3073.36 | 3535.52 | 4459.81  | 5384.10  | 7232.69  | 9081.28  |
| 1.750                | 2613.37             | 3075.91 | 3538.46 | 4463.55  | 5388.63  | 7238.80  | 9088.98  |
| 1.751                | 2615.51             | 3078.45 | 3541.40 | 4467.28  | 5393.76  | 7244.91  | 9096.68  |
| 1.752                | 2617.66             | 3080.99 | 3544.34 | 4471.01  | 5397.69  | 7251.02  | 9104.38  |
| 1.753                | 2619.81             | 3083.54 | 3547.28 | 4474.74  | 5402.22  | 7257.14  | 9112.08  |
| 1.754                | 2621.99             | 3086.09 | 3550.22 | 4478.47  | 5406.75  | 7263.26  | 9119.79  |
| 1.755                | 2624.11             | 3088.64 | 3553.17 | 4482.22  | 5411.28  | 7269.38  | 9127.50  |
| 1.756                | 2626.26             | 3091.18 | 3556.11 | 4485.96  | 5415.81  | 7275.51  | 9135.21  |
| 1.757                | 2628.41             | 3093.73 | 3559.05 | 4489.70  | 5420.34  | 7281.64  | 9142.92  |
| 1.758                | 2630.56             | 3096.28 | 3562.00 | 4493.44  | 5424.87  | 7287.77  | 9150.63  |
| 1.759                | 2632.71             | 3098.83 | 3564.95 | 4497.18  | 5429.41  | 7293.90  | 9158.33  |
| 1.760                | 2634.87             | 3101.38 | 3567.90 | 4500.92  | 5433.95  | 7300.01  | 9166.06  |
| 1.761                | 2637.01             | 3103.93 | 3570.84 | 4504.66  | 5438.39  | 7306.14  | 9173.78  |
| 1.762                | 2639.16             | 3106.48 | 3573.79 | 4508.40  | 5442.93  | 7312.27  | 9181.50  |
| 1.763                | 2641.31             | 3109.03 | 3576.74 | 4512.15  | 5447.47  | 7318.40  | 9189.22  |
| 1.764                | 2643.47             | 3111.58 | 3579.69 | 4515.90  | 5452.01  | 7324.53  | 9196.55  |
| 1.765                | 2645.64             | 3114.14 | 3582.64 | 4519.65  | 5456.66  | 7330.67  | 9204.68  |
| 1.766                | 2647.79             | 3116.69 | 3585.59 | 4523.40  | 5461.20  | 7336.81  | 9212.41  |
| 1.767                | 2649.94             | 3119.24 | 3588.54 | 4527.16  | 5465.76  | 7342.95  | 9220.14  |
| 1.768                | 2652.10             | 3121.79 | 3591.49 | 4530.90  | 5470.31  | 7349.09  | 9227.87  |
| 1.769                | 2654.26             | 3124.35 | 3594.44 | 4534.65  | 5474.86  | 7355.19  | 9235.61  |
| 1.770                | 2656.42             | 3126.91 | 3597.41 | 4538.40  | 5479.39  | 7361.37  | 9243.35  |
| 1.771                | 2658.57             | 3129.46 | 3600.36 | 4542.15  | 5484.94  | 7367.51  | 9251.09  |
| 1.772                | 2660.73             | 3132.02 | 3603.31 | 4545.90  | 5489.49  | 7373.66  | 9258.83  |



| Depth on Weir. | LENGTH OF THE WEIR. |         |         |          |          |          |          |
|----------------|---------------------|---------|---------|----------|----------|----------|----------|
|                | 6 Feet.             | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| 1.773          | 2662.89             | 3134.58 | 3606.27 | 4549.65  | 5494.04  | 7379.81  | 9266.57  |
| 1.774          | 2665.05             | 3137.14 | 3609.23 | 4553.41  | 5498.59  | 7385.96  | 9274.32  |
| 1.775          | 2667.21             | 3139.70 | 3612.19 | 4557.17  | 5502.15  | 7392.11  | 9282.07  |
| 1.776          | 2669.37             | 3142.26 | 3615.15 | 4560.93  | 5506.70  | 7398.26  | 9289.82  |
| 1.777          | 2671.43             | 3144.82 | 3618.11 | 4564.69  | 5511.26  | 7404.42  | 9297.57  |
| 1.778          | 2673.59             | 3147.38 | 3621.07 | 4568.45  | 5515.82  | 7410.58  | 9305.33  |
| 1.779          | 2675.75             | 3149.94 | 3624.03 | 4572.21  | 5520.38  | 7416.74  | 9313.09  |
| 1.780          | 2678.01             | 3152.50 | 3626.99 | 4575.97  | 5524.94  | 7422.90  | 9320.85  |
| 1.781          | 2680.17             | 3155.06 | 3629.95 | 4579.73  | 5529.50  | 7429.06  | 9328.61  |
| 1.782          | 2682.33             | 3157.62 | 3632.91 | 4583.49  | 5534.06  | 7435.22  | 9336.37  |
| 1.783          | 2684.49             | 3160.18 | 3635.87 | 4587.25  | 5538.62  | 7441.38  | 9344.13  |
| 1.784          | 2686.66             | 3162.75 | 3638.83 | 4591.01  | 5543.19  | 7447.54  | 9351.90  |
| 1.785          | 2688.83             | 3165.32 | 3641.80 | 4594.78  | 5547.76  | 7453.71  | 9359.67  |
| 1.786          | 2690.99             | 3167.88 | 3644.76 | 4598.54  | 5552.33  | 7459.88  | 9367.44  |
| 1.787          | 2693.15             | 3170.44 | 3647.73 | 4602.31  | 5556.90  | 7466.05  | 9375.21  |
| 1.788          | 2695.31             | 3173.01 | 3650.70 | 4606.08  | 5561.47  | 7472.22  | 9382.99  |
| 1.789          | 2697.47             | 3175.58 | 3653.67 | 4609.85  | 5566.04  | 7478.40  | 9390.77  |
| 1.790          | 2699.64             | 3178.15 | 3656.64 | 4613.62  | 5570.61  | 7484.58  | 9398.55  |
| 1.791          | 2701.81             | 3180.71 | 3659.61 | 4617.39  | 5575.18  | 7490.76  | 9406.33  |
| 1.792          | 2703.98             | 3183.28 | 3662.58 | 4621.16  | 5579.75  | 7496.94  | 9414.11  |
| 1.793          | 2706.15             | 3185.85 | 3665.55 | 4624.93  | 5584.32  | 7403.12  | 9421.89  |
| 1.794          | 2708.32             | 3188.42 | 3668.52 | 4628.71  | 5588.90  | 7409.30  | 9429.68  |
| 1.795          | 2710.49             | 3190.99 | 3671.49 | 4632.49  | 5593.48  | 7515.48  | 9437.47  |
| 1.796          | 2712.66             | 3193.56 | 3674.46 | 4636.26  | 5598.06  | 7521.66  | 9445.26  |
| 1.797          | 2714.83             | 3196.13 | 3677.43 | 4640.03  | 5602.64  | 7527.85  | 9453.05  |
| 1.798          | 2717.00             | 3198.70 | 3680.40 | 4643.81  | 5607.22  | 7534.04  | 9460.85  |
| 1.799          | 2719.17             | 3201.27 | 3683.38 | 4647.59  | 5611.80  | 7540.23  | 9468.65  |
| 1.800          | 2721.34             | 3203.85 | 3686.36 | 4651.37  | 5616.39  | 7546.42  | 9476.45  |
| 1.801          | 2723.51             | 3206.42 | 3689.33 | 4655.15  | 5620.97  | 7552.61  | 9484.26  |
| 1.802          | 2725.68             | 3208.99 | 3692.30 | 4658.93  | 5625.55  | 7558.80  | 9492.07  |
| 1.803          | 2727.85             | 3211.57 | 3695.28 | 4662.61  | 5630.14  | 7565.00  | 9499.89  |
| 1.804          | 2730.02             | 3214.15 | 3698.26 | 4666.39  | 5634.73  | 7571.20  | 9507.71  |
| 1.805          | 2732.20             | 3216.73 | 3701.24 | 4670.28  | 5639.32  | 7577.40  | 9515.48  |
| 1.806          | 2734.37             | 3219.30 | 3704.22 | 4674.06  | 5643.91  | 7583.60  | 9523.29  |
| 1.807          | 2736.54             | 3221.87 | 3707.20 | 4677.85  | 5648.50  | 7589.86  | 9531.10  |
| 1.808          | 2738.72             | 3224.45 | 3710.18 | 4681.64  | 5653.09  | 7596.00  | 9538.92  |
| 1.809          | 2740.90             | 3228.03 | 3713.16 | 4685.43  | 5657.69  | 7602.21  | 9546.74  |
| 1.810          | 2743.08             | 3229.61 | 3716.15 | 4689.22  | 5662.29  | 7608.42  | 9554.56  |
| 1.811          | 2745.25             | 3232.19 | 3718.13 | 4693.01  | 5666.88  | 7614.63  | 9562.38  |
| 1.812          | 2747.43             | 3234.77 | 3721.11 | 4696.80  | 5671.47  | 7620.87  | 9570.20  |
| 1.813          | 2749.61             | 3237.35 | 3724.09 | 4700.59  | 5676.07  | 7627.07  | 9578.03  |
| 1.814          | 2751.79             | 3239.93 | 3727.08 | 4704.38  | 5680.67  | 7633.27  | 9585.86  |
| 1.815          | 2753.97             | 3242.52 | 3731.07 | 4708.17  | 5685.27  | 7639.48  | 9593.69  |
| 1.816          | 2756.15             | 3245.10 | 3734.05 | 4711.96  | 5689.87  | 7645.70  | 9601.52  |
| 1.817          | 2758.33             | 3247.68 | 3737.04 | 4715.75  | 5694.47  | 7651.92  | 9609.45  |
| 1.818          | 2760.51             | 3250.26 | 3740.03 | 4719.55  | 5699.07  | 7658.14  | 9617.39  |
| 1.819          | 2762.69             | 3252.84 | 3743.02 | 4723.35  | 5703.68  | 7664.36  | 9625.23  |
| 1.820          | 2764.87             | 3255.43 | 3746.01 | 4727.15  | 5708.29  | 7670.58  | 9632.87  |
| 1.821          | 2767.05             | 3258.01 | 3749.00 | 4730.95  | 5712.90  | 7676.81  | 9640.71  |
| 1.822          | 2769.23             | 3260.60 | 3751.99 | 4734.75  | 5717.51  | 7683.05  | 9648.55  |
| 1.823          | 2771.41             | 3263.19 | 3754.98 | 4738.55  | 5722.12  | 7689.29  | 9656.40  |
| 1.824          | 2773.59             | 3265.78 | 3757.97 | 4742.35  | 5726.73  | 7695.53  | 9664.25  |
| 1.825          | 2775.78             | 3268.37 | 3760.96 | 4746.15  | 5731.34  | 7701.77  | 9672.10  |
| 1.826          | 2777.96             | 3270.95 | 3763.95 | 4749.85  | 5735.95  | 7707.95  | 9679.95  |
| 1.827          | 2779.14             | 3273.54 | 3766.94 | 4753.65  | 5740.56  | 7704.18  | 9687.80  |
| 1.828          | 2781.32             | 3276.13 | 3769.93 | 4757.45  | 5745.18  | 7720.42  | 9695.66  |
| 1.829          | 2783.50             | 3278.72 | 3773.93 | 4761.26  | 5749.80  | 7726.66  | 9703.52  |
| 1.830          | 2786.69             | 3281.31 | 3775.93 | 4765.17  | 5754.42  | 7732.90  | 9711.38  |

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|----------|----------|----------|----------|
|                      | 6 Feet.             | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| 1.831                | 2788.87             | 3283.80 | 3778.92 | 4768.98  | 5759.04  | 7739.14  | 9719.24  |
| 1.832                | 2791.05             | 3286.39 | 3781.92 | 4772.80  | 5763.66  | 7745.38  | 9727.10  |
| 1.833                | 2793.24             | 3288.98 | 3784.92 | 4776.62  | 5768.28  | 7751.62  | 9734.97  |
| 1.834                | 2795.43             | 3291.57 | 3787.92 | 4780.44  | 5772.90  | 7757.86  | 9742.84  |
| 1.835                | 2797.62             | 3294.27 | 3790.92 | 4784.22  | 5777.52  | 7764.11  | 9750.71  |
| 1.836                | 2799.81             | 3296.86 | 3793.92 | 4788.03  | 5782.14  | 7770.36  | 9758.58  |
| 1.837                | 2802.00             | 3299.46 | 3796.92 | 4791.84  | 5786.76  | 7776.61  | 9766.45  |
| 1.838                | 2804.19             | 3302.06 | 3799.92 | 4795.65  | 5791.39  | 7782.86  | 9774.33  |
| 1.839                | 2806.38             | 3304.66 | 3702.92 | 4799.47  | 5796.02  | 7789.11  | 9782.21  |
| 1.840                | 2808.57             | 3307.25 | 3805.93 | 4803.29  | 5800.65  | 7795.37  | 9790.09  |
| 1.841                | 2810.76             | 3310.84 | 3808.93 | 4807.10  | 5805.28  | 7801.63  | 9797.97  |
| 1.842                | 2812.95             | 3313.44 | 3811.93 | 4810.92  | 5809.91  | 7807.89  | 9805.86  |
| 1.843                | 2815.04             | 3316.04 | 3814.93 | 4814.74  | 5814.54  | 7814.15  | 9813.75  |
| 1.844                | 2817.23             | 3318.64 | 3817.94 | 4818.56  | 5819.17  | 7820.41  | 9821.64  |
| 1.845                | 2819.52             | 3320.24 | 3820.95 | 4822.38  | 5823.81  | 7826.67  | 9829.53  |
| 1.846                | 2821.71             | 3322.84 | 3823.95 | 4826.20  | 5828.44  | 7832.93  | 9837.41  |
| 1.847                | 2823.90             | 3325.44 | 3826.96 | 4830.02  | 5833.07  | 7839.19  | 9845.30  |
| 1.848                | 2825.09             | 3328.04 | 3829.97 | 4833.84  | 5837.71  | 7845.46  | 9853.19  |
| 1.849                | 2827.29             | 3330.64 | 3832.98 | 4837.66  | 5842.35  | 7851.73  | 9861.09  |
| 1.850                | 2830.49             | 3333.24 | 3835.99 | 4841.49  | 5846.99  | 7858.00  | 9869.00  |
| 1.851                | 2832.68             | 3335.84 | 3838.00 | 4845.31  | 5851.63  | 7864.27  | 9876.90  |
| 1.852                | 2834.87             | 3338.44 | 3841.01 | 4849.14  | 5856.27  | 7870.54  | 9884.81  |
| 1.853                | 2837.07             | 3341.04 | 3844.02 | 4852.97  | 5860.91  | 7876.81  | 9892.72  |
| 1.854                | 2839.29             | 3343.65 | 3847.03 | 4856.80  | 5865.56  | 7883.09  | 9900.63  |
| 1.855                | 2841.47             | 3346.26 | 3851.05 | 4860.63  | 5870.21  | 7889.37  | 9908.54  |
| 1.856                | 2843.66             | 3348.86 | 3854.06 | 4864.46  | 5874.85  | 7895.65  | 9916.45  |
| 1.857                | 2845.85             | 3351.46 | 3857.07 | 4868.29  | 5879.50  | 7901.93  | 9924.36  |
| 1.858                | 2848.05             | 3354.01 | 3860.08 | 4872.12  | 5884.15  | 7908.21  | 9932.28  |
| 1.859                | 2850.25             | 3356.68 | 3863.10 | 4875.95  | 5888.80  | 7914.49  | 9940.20  |
| 1.860                | 2852.45             | 3359.29 | 3866.12 | 4879.79  | 5893.45  | 7920.78  | 9948.12  |
| 1.861                | 2854.65             | 3361.90 | 3869.13 | 4883.62  | 5897.10  | 7927.07  | 9956.04  |
| 1.862                | 2856.85             | 3364.51 | 3872.15 | 4887.46  | 5901.75  | 7933.36  | 9963.97  |
| 1.863                | 2859.05             | 3367.12 | 3875.17 | 4891.30  | 5906.41  | 7939.65  | 9971.90  |
| 1.864                | 2861.25             | 3369.73 | 3878.19 | 4895.14  | 5911.07  | 7945.94  | 9979.83  |
| 1.865                | 2863.46             | 3372.34 | 3881.21 | 4898.97  | 5916.73  | 7952.24  | 9987.75  |
| 1.866                | 2865.66             | 3374.95 | 3884.23 | 4902.81  | 5921.38  | 7958.53  | 9995.68  |
| 1.867                | 2867.86             | 3377.56 | 3887.25 | 4906.65  | 5926.04  | 7964.83  | 10003.61 |
| 1.868                | 2870.06             | 3380.17 | 3890.27 | 4910.49  | 5930.70  | 7971.13  | 10011.54 |
| 1.869                | 2872.26             | 3382.78 | 3893.30 | 4914.33  | 5935.36  | 7977.43  | 10019.47 |
| 1.870                | 2874.47             | 3385.39 | 3896.32 | 4918.17  | 5940.02  | 7983.73  | 10027.43 |
| 1.871                | 2876.67             | 3388.00 | 3899.34 | 4922.01  | 5944.68  | 7990.03  | 10035.37 |
| 1.872                | 2878.87             | 3390.61 | 3902.36 | 4925.85  | 5949.34  | 7996.33  | 10043.31 |
| 1.873                | 2881.08             | 3393.23 | 3905.38 | 4929.70  | 5954.01  | 8002.64  | 10051.26 |
| 1.874                | 2883.28             | 3395.86 | 3908.41 | 4933.55  | 5958.68  | 8008.95  | 10059.21 |
| 1.875                | 2885.49             | 3398.47 | 3911.44 | 4937.40  | 5963.35  | 8015.26  | 10067.16 |
| 1.876                | 2887.69             | 3301.08 | 3914.47 | 4941.24  | 5968.02  | 8021.57  | 10075.11 |
| 1.877                | 2889.89             | 3303.69 | 3917.50 | 4945.09  | 5972.69  | 8027.88  | 10083.06 |
| 1.878                | 2892.10             | 3306.31 | 3920.53 | 4948.94  | 5977.36  | 8034.19  | 10090.02 |
| 1.879                | 2894.31             | 3308.93 | 3923.56 | 4952.79  | 5982.03  | 8040.50  | 10097.98 |
| 1.880                | 2896.52             | 3411.55 | 3926.59 | 4956.64  | 5986.70  | 8046.82  | 10106.94 |
| 1.881                | 2898.73             | 3414.17 | 3929.62 | 4960.49  | 5991.37  | 8053.14  | 10114.90 |
| 1.882                | 2900.94             | 3416.79 | 3932.65 | 4964.34  | 5996.05  | 8059.46  | 10122.86 |
| 1.883                | 2903.15             | 3419.41 | 3935.68 | 4968.19  | 6000.73  | 8065.78  | 10130.83 |
| 1.884                | 2905.36             | 3422.03 | 3938.72 | 4972.05  | 6005.41  | 8072.00  | 10138.80 |
| 1.885                | 2907.57             | 3424.66 | 3941.75 | 4975.91  | 6010.09  | 8078.43  | 10146.77 |
| 1.886                | 2909.78             | 3427.68 | 3944.78 | 4979.77  | 6014.77  | 8084.75  | 10154.74 |
| 1.887                | 2911.99             | 3430.30 | 3947.81 | 4983.63  | 6018.45  | 8091.08  | 10162.71 |
| 1.888                | 2914.20             | 3432.92 | 3950.84 | 4987.49  | 6023.13  | 8097.41  | 10170.69 |

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|----------|----------|----------|----------|
|                      | 6 Feet.             | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| 1.889                | 2916.41             | 3435.54 | 3953.88 | 4991.35  | 6028.81  | 8103.74  | 10178.67 |
| 1.890                | 2918.63             | 3437.77 | 3956.92 | 4995.21  | 6033.50  | 8110.07  | 10186.65 |
| 1.891                | 2920.84             | 3440.39 | 3959.95 | 4999.07  | 6038.18  | 8117.10  | 10194.63 |
| 1.892                | 2923.05             | 3443.01 | 3962.99 | 5002.93  | 6042.86  | 8123.44  | 10202.61 |
| 1.893                | 2925.27             | 3445.64 | 3966.03 | 5006.79  | 6047.55  | 8129.78  | 10210.60 |
| 1.894                | 2927.49             | 3448.27 | 3969.07 | 5010.65  | 6052.24  | 8136.12  | 10218.59 |
| 1.895                | 2929.70             | 3450.90 | 3972.11 | 5014.52  | 6056.93  | 8141.76  | 10226.58 |
| 1.896                | 2931.91             | 3453.53 | 3975.15 | 5018.38  | 6061.62  | 8148.10  | 10234.57 |
| 1.897                | 2934.12             | 3456.16 | 3978.19 | 5022.25  | 6066.31  | 8154.44  | 10242.56 |
| 1.898                | 2936.34             | 3458.79 | 3981.23 | 5026.12  | 6071.00  | 8160.78  | 10250.56 |
| 1.899                | 2938.56             | 3461.42 | 3984.27 | 5029.99  | 6075.70  | 8167.13  | 10258.56 |
| 1.900                | 2940.78             | 3464.05 | 3987.32 | 5033.86  | 6080.40  | 8173.48  | 10266.56 |
| 1.901                | 2942.99             | 3466.68 | 3990.36 | 5037.73  | 6085.09  | 8180.83  | 10274.56 |
| 1.902                | 2945.21             | 3469.31 | 3993.40 | 5041.60  | 6089.79  | 8187.18  | 10282.56 |
| 1.903                | 2947.43             | 3471.94 | 3996.44 | 5045.47  | 6094.49  | 8193.53  | 10290.57 |
| 1.904                | 2949.65             | 3474.57 | 3999.49 | 5049.34  | 6099.91  | 8199.88  | 10298.58 |
| 1.905                | 2951.87             | 3477.21 | 4002.54 | 5053.22  | 6103.89  | 8205.24  | 10306.59 |
| 1.906                | 2954.09             | 3479.84 | 4005.58 | 5057.09  | 6108.59  | 8211.60  | 10314.60 |
| 1.907                | 2956.31             | 3482.47 | 4008.63 | 5060.96  | 6113.29  | 8217.96  | 10322.61 |
| 1.908                | 2958.53             | 3485.10 | 4011.68 | 5064.84  | 6118.06  | 8224.32  | 10330.62 |
| 1.909                | 2960.75             | 3487.74 | 4014.73 | 5068.72  | 6122.77  | 8230.68  | 10338.64 |
| 1.910                | 2962.97             | 3490.38 | 4017.78 | 5072.60  | 6127.41  | 8237.04  | 10346.66 |
| 1.911                | 2965.19             | 3493.01 | 4020.83 | 5076.48  | 6132.12  | 8243.40  | 10354.68 |
| 1.912                | 2967.41             | 3495.64 | 4023.88 | 5080.36  | 6136.83  | 8249.76  | 10362.70 |
| 1.913                | 2969.63             | 3498.28 | 4026.93 | 5084.26  | 6141.54  | 8256.13  | 10370.73 |
| 1.914                | 2971.89             | 3500.92 | 4029.98 | 5088.14  | 6146.25  | 8262.50  | 10378.76 |
| 1.915                | 2974.08             | 3503.56 | 4033.04 | 5092.00  | 6150.96  | 8268.87  | 10386.79 |
| 1.916                | 2976.30             | 3506.20 | 4036.09 | 5095.88  | 6155.67  | 8275.24  | 10394.82 |
| 1.917                | 2978.52             | 3508.84 | 4039.14 | 5099.76  | 6160.38  | 8281.61  | 10402.85 |
| 1.918                | 2980.74             | 3511.48 | 4042.19 | 5103.64  | 6165.09  | 8287.99  | 10410.88 |
| 1.919                | 2982.97             | 3514.12 | 4045.25 | 5107.53  | 6169.81  | 8294.37  | 10418.92 |
| 1.920                | 2985.20             | 3516.76 | 4048.31 | 5111.42  | 6174.53  | 8300.75  | 10426.96 |
| 1.921                | 2987.42             | 3518.80 | 4051.36 | 5115.31  | 6179.25  | 8307.13  | 10435.00 |
| 1.922                | 2989.65             | 3521.44 | 4054.42 | 5119.20  | 6183.97  | 8313.51  | 10443.04 |
| 1.923                | 2991.88             | 3524.08 | 4057.48 | 5123.09  | 6188.69  | 8319.89  | 10451.08 |
| 1.924                | 2994.11             | 3526.72 | 4060.54 | 5126.98  | 6193.41  | 8326.27  | 10459.13 |
| 1.925                | 2996.34             | 3529.97 | 4063.60 | 5130.87  | 6198.13  | 8332.66  | 10467.18 |
| 1.926                | 2998.57             | 3532.61 | 4066.66 | 5134.76  | 6202.85  | 8339.05  | 10475.23 |
| 1.927                | 3000.80             | 3535.25 | 4069.72 | 5138.65  | 6207.57  | 8345.44  | 10483.28 |
| 1.928                | 3003.03             | 3537.90 | 4072.78 | 5142.54  | 6212.30  | 8351.83  | 10491.34 |
| 1.929                | 3005.26             | 3540.55 | 4075.84 | 5146.44  | 6217.03  | 8358.22  | 10499.40 |
| 1.930                | 3007.49             | 3543.20 | 4078.91 | 5150.34  | 6221.76  | 8364.61  | 10507.46 |
| 1.931                | 3009.72             | 3545.84 | 4081.97 | 5154.23  | 6226.49  | 8371.00  | 10515.52 |
| 1.932                | 3011.95             | 3548.49 | 4085.03 | 5158.13  | 6231.22  | 8377.40  | 10523.58 |
| 1.933                | 3014.18             | 3551.14 | 4088.09 | 5162.03  | 6235.95  | 8383.80  | 10531.64 |
| 1.934                | 3016.41             | 3553.79 | 4091.16 | 5165.93  | 6240.68  | 8390.20  | 10539.71 |
| 1.935                | 3018.64             | 3556.44 | 4094.23 | 5169.83  | 6245.42  | 8396.60  | 10547.78 |
| 1.936                | 3020.87             | 3559.09 | 4097.29 | 5173.73  | 6250.15  | 8403.00  | 10555.85 |
| 1.937                | 3023.10             | 3561.74 | 4100.36 | 5177.63  | 6254.88  | 8409.40  | 10563.92 |
| 1.938                | 3025.33             | 3564.39 | 4103.43 | 5181.53  | 6259.62  | 8415.80  | 10571.99 |
| 1.939                | 3027.57             | 3567.04 | 4036.50 | 5185.43  | 6264.36  | 8422.21  | 10580.07 |
| 1.940                | 3029.81             | 3569.69 | 4109.57 | 5189.34  | 6269.10  | 8428.62  | 10588.15 |
| 1.941                | 3032.04             | 3572.34 | 4112.64 | 5193.24  | 6273.84  | 8435.03  | 10596.23 |
| 1.942                | 3034.27             | 3574.99 | 4115.71 | 5197.14  | 6278.58  | 8441.44  | 10604.31 |
| 1.943                | 3036.51             | 3577.64 | 4118.78 | 5101.05  | 6283.32  | 8447.85  | 10612.39 |
| 1.944                | 3038.75             | 3580.30 | 4121.85 | 5104.96  | 6288.06  | 8454.27  | 10620.47 |
| 1.945                | 3040.99             | 3582.96 | 4124.93 | 5208.87  | 6292.81  | 8460.69  | 10628.56 |
| 1.946                | 3043.22             | 3585.61 | 4128.00 | 5212.78  | 6297.55  | 8467.11  | 10636.65 |

| Depth<br>on<br>Weir. | LENGTH OF THE WEIR. |         |         |          |          |          |          |
|----------------------|---------------------|---------|---------|----------|----------|----------|----------|
|                      | 6 Feet.             | 7 Feet. | 8 Feet. | 10 Feet. | 12 Feet. | 16 Feet. | 20 Feet. |
| 1.947                | 3045.46             | 3588.26 | 4131.07 | 5216.69  | 6302.29  | 8473.53  | 10644.74 |
| 1.948                | 3047.70             | 3590.92 | 4134.14 | 5220.60  | 6307.04  | 8479.95  | 10652.83 |
| 1.949                | 3049.94             | 3593.58 | 4137.22 | 5224.51  | 6311.79  | 8486.37  | 10660.93 |
| 1.950                | 3052.18             | 3596.24 | 4140.30 | 5228.42  | 6316.54  | 8492.79  | 10669.03 |
| 1.951                | 3054.42             | 3598.90 | 4143.37 | 5232.33  | 6321.29  | 8499.21  | 10677.13 |
| 1.952                | 3056.66             | 3601.56 | 4146.45 | 5236.24  | 6326.04  | 8505.64  | 10685.23 |
| 1.953                | 3058.90             | 3604.22 | 4149.53 | 5240.16  | 6330.79  | 8512.07  | 10693.33 |
| 1.954                | 3061.14             | 3606.88 | 4152.61 | 5244.08  | 6335.55  | 8518.50  | 10701.44 |
| 1.955                | 3063.38             | 3609.54 | 4155.69 | 5248.00  | 6340.31  | 8524.93  | 10709.55 |
| 1.956                | 3065.62             | 3612.20 | 4158.77 | 5251.92  | 6345.06  | 8531.36  | 10717.66 |
| 1.957                | 3067.86             | 3614.86 | 4161.85 | 5255.84  | 6349.82  | 8537.79  | 10725.77 |
| 1.958                | 3070.10             | 3617.52 | 4164.93 | 5259.76  | 6354.58  | 8544.23  | 10733.88 |
| 1.959                | 3072.34             | 3620.18 | 4168.01 | 5263.68  | 6359.34  | 8550.67  | 10741.99 |
| 1.960                | 3074.59             | 3622.84 | 4171.09 | 5267.60  | 6364.10  | 8557.11  | 10750.11 |
| 1.961                | 3076.83             | 3625.50 | 4174.17 | 5271.52  | 6368.86  | 8563.55  | 10758.23 |
| 1.962                | 3079.07             | 3628.16 | 4177.25 | 5275.44  | 6373.52  | 8569.99  | 10766.35 |
| 1.963                | 3081.32             | 3630.83 | 4180.34 | 5279.36  | 6378.28  | 8576.43  | 10774.47 |
| 1.964                | 3083.57             | 3633.50 | 4183.43 | 5283.29  | 6383.05  | 8582.87  | 10782.59 |
| 1.965                | 3085.82             | 3636.17 | 4186.52 | 5287.22  | 6387.92  | 8589.32  | 10790.72 |
| 1.966                | 3088.06             | 3638.83 | 4189.60 | 5291.14  | 6392.68  | 8595.75  | 10798.85 |
| 1.967                | 3090.30             | 3641.49 | 4192.68 | 5295.07  | 6397.45  | 8602.20  | 10706.98 |
| 1.968                | 3092.55             | 3644.16 | 4195.77 | 5299.00  | 6402.22  | 8608.65  | 10715.11 |
| 1.969                | 3094.80             | 3646.83 | 4198.86 | 5302.93  | 6406.99  | 8615.10  | 10723.24 |
| 1.970                | 3097.05             | 3649.50 | 4201.95 | 5306.86  | 6411.76  | 8621.57  | 10831.38 |
| 1.971                | 3099.29             | 3652.17 | 4205.04 | 5310.79  | 6416.53  | 8629.02  | 10839.52 |
| 1.972                | 3100.54             | 3654.84 | 4208.13 | 5314.72  | 6421.30  | 8635.48  | 10847.66 |
| 1.973                | 3103.79             | 3657.51 | 4211.22 | 5318.65  | 6426.07  | 8641.94  | 10855.80 |
| 1.974                | 3106.04             | 3660.18 | 4214.31 | 5322.58  | 6430.85  | 8648.40  | 10863.95 |
| 1.975                | 3108.29             | 3662.85 | 4217.40 | 5326.52  | 6435.63  | 8654.86  | 10872.10 |
| 1.976                | 3110.54             | 3665.52 | 4220.49 | 5330.45  | 6440.41  | 8660.32  | 10880.25 |
| 1.977                | 3112.79             | 3668.19 | 4223.58 | 5334.38  | 6445.19  | 8666.78  | 10888.75 |
| 1.978                | 3115.04             | 3670.86 | 4226.68 | 5338.32  | 6449.97  | 8673.25  | 10896.90 |
| 1.979                | 3117.29             | 3673.53 | 4229.78 | 5342.26  | 6454.75  | 8679.72  | 10905.05 |
| 1.980                | 3119.54             | 3676.21 | 4232.88 | 5346.20  | 6459.53  | 8686.19  | 10912.85 |
| 1.981                | 3121.79             | 3678.88 | 4235.97 | 5350.14  | 6464.31  | 8692.66  | 10921.01 |
| 1.982                | 3124.04             | 3681.55 | 4239.06 | 5354.08  | 6469.09  | 8699.13  | 10929.17 |
| 1.983                | 3126.29             | 3684.22 | 4242.16 | 5358.02  | 6473.87  | 8705.60  | 10937.33 |
| 1.984                | 3128.55             | 3686.90 | 4245.26 | 5361.96  | 6478.66  | 8712.07  | 10945.49 |
| 1.985                | 3130.81             | 3689.58 | 4248.36 | 5365.91  | 6483.45  | 8718.55  | 10953.65 |
| 1.986                | 3133.06             | 3692.25 | 4251.46 | 5369.85  | 6488.24  | 8725.03  | 10961.82 |
| 1.987                | 3135.36             | 3694.93 | 4254.56 | 5373.79  | 6493.03  | 8731.51  | 10969.99 |
| 1.988                | 3137.57             | 3697.61 | 4257.66 | 5377.73  | 6497.82  | 8737.99  | 10978.16 |
| 1.989                | 3139.83             | 3700.29 | 4260.76 | 5381.68  | 6402.61  | 8744.47  | 10986.33 |
| 1.990                | 3142.09             | 3702.97 | 4263.86 | 5385.63  | 6507.41  | 8750.95  | 10994.50 |
| 1.991                | 3144.34             | 3705.59 | 4266.96 | 5389.58  | 6512.20  | 8757.43  | 10102.68 |
| 1.992                | 3146.59             | 3708.21 | 4270.06 | 5393.53  | 6516.99  | 8763.92  | 10112.68 |
| 1.993                | 3148.85             | 3710.83 | 4273.17 | 5397.48  | 6521.78  | 8770.41  | 10120.86 |
| 1.994                | 3151.11             | 3713.45 | 4276.28 | 5401.43  | 6526.57  | 8776.90  | 10129.04 |
| 1.995                | 3153.37             | 3716.37 | 4279.38 | 5405.38  | 6531.38  | 8783.39  | 11035.40 |
| 1.996                | 3155.63             | 3719.05 | 4282.48 | 5409.33  | 6536.18  | 8789.88  | 11043.59 |
| 1.997                | 3157.89             | 3721.73 | 4285.58 | 5413.28  | 6540.98  | 8796.37  | 11051.78 |
| 1.998                | 3160.15             | 3724.41 | 4288.69 | 5417.23  | 6545.78  | 8802.87  | 11059.97 |
| 1.999                | 3162.41             | 3727.10 | 4291.80 | 5421.19  | 6550.58  | 8809.37  | 11068.16 |
| 2.000                | 3164.67             | 3729.79 | 4294.91 | 5425.15  | 6555.39  | 8815.87  | 11076.35 |

## J. B. Francis Tables.

## FOR FACILITATING THE COMPUTATION OF THE QUANTITY OF WATER FLOWING OVER WEIRS.

TABLE I.

To attain the greatest exactness, it is necessary to take account of the velocity of the water approaching the weir. The method adopted at Lowell for this purpose is to make a correction for it in the observed depth on the weir, by the formula

$$H' = \left[ (H+h)^{\frac{3}{2}} - h^{\frac{3}{2}} \right]^{\frac{2}{3}};$$

in which

$H$  = the observed depth on the weir.

$h$  = the head due the mean velocity approaching the weir.

$H'$  = the corrected depth on the weir.

By developing into series and omitting the terms containing powers of  $\frac{h}{H}$  above the first,  $h$  being always very small, relatively to  $H$ , this formula may, without sensible error, be put under the simpler form,

$$H' = H + h - \frac{2}{3} \sqrt{\frac{h^3}{H}}.$$

The mean velocity of the water approaching the weir is usually found, with sufficient exactness, by computing the discharge, approximately, from the observed depth on the weir, and dividing it by the section of the channel approaching the weir, the quotient being the velocity; the head due this velocity, or  $h$ , is found by Table I., which is computed by the formula,

$$h = \frac{V^2}{2g}$$

in which

$V$  = the mean velocity.

$g$  = the velocity acquired by a body at the end of the first second of its fall, in a vacuum; its value, for Lowell, being 32.1618.

TABLE II.

This is computed by the formula

$$Q = 3.33 (L - 0.1n H) H^{\frac{3}{2}},$$

in which

$Q$  = the quantity of water discharged, in cubic feet per second.

$L$  = the length of the weir in feet.

$H$  = the depth on the weir in feet, being the height of the surface of the water above the top of the weir, taken far enough from the weir to be unaffected by the curvature caused by the discharge, and corrected, if necessary, for the velocity of the water approaching the weir.

$n$  = the number of end contractions.

In computing the table,  $L$  is taken equal to 1, and  $n$  equal to 0.

The actual length of the weir being known, it is to be corrected for the end contractions, if any, by deducting from it one-tenth of the depth on the weir for each end contraction. If the length of the weir is the same as the width of the canal approaching it, there is no end contraction, and of course nothing to be deducted from the length of the weir. The discharge, as given by the table, multiplied by the length of the weir, corrected, if necessary, as above, gives the quantity of water discharged by the weir.



## HEADS, IN FEET, DUE TO VELOCITIES FROM 0 TO 4.99 FEET PER SECOND.

| Velocity | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0.0      | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0001 | 0.0001 | 0.0001 | 0.0001 |
| .1       | 0.0002 | 0.0002 | 0.0002 | 0.0003 | 0.0003 | 0.0003 | 0.0004 | 0.0004 | 0.0005 | 0.0006 |
| .2       | 0.0006 | 0.0007 | 0.0008 | 0.0008 | 0.0009 | 0.0010 | 0.0011 | 0.0011 | 0.0012 | 0.0013 |
| .3       | 0.0014 | 0.0015 | 0.0016 | 0.0017 | 0.0018 | 0.0019 | 0.0020 | 0.0021 | 0.0022 | 0.0024 |
| .4       | 0.0025 | 0.0026 | 0.0027 | 0.0029 | 0.0030 | 0.0031 | 0.0033 | 0.0034 | 0.0036 | 0.0037 |
| .5       | 0.0039 | 0.0040 | 0.0042 | 0.0044 | 0.0045 | 0.0047 | 0.0049 | 0.0051 | 0.0052 | 0.0054 |
| .6       | 0.0056 | 0.0058 | 0.0060 | 0.0062 | 0.0064 | 0.0066 | 0.0068 | 0.0070 | 0.0072 | 0.0074 |
| .7       | 0.0076 | 0.0078 | 0.0081 | 0.0083 | 0.0085 | 0.0087 | 0.0090 | 0.0092 | 0.0095 | 0.0097 |
| .8       | 0.0099 | 0.0102 | 0.0105 | 0.0107 | 0.0110 | 0.0112 | 0.0115 | 0.0118 | 0.0120 | 0.0123 |
| .9       | 0.0126 | 0.0129 | 0.0132 | 0.0134 | 0.0137 | 0.0140 | 0.0143 | 0.0146 | 0.0149 | 0.0152 |
| 1.0      | 0.0155 | 0.0159 | 0.0162 | 0.0165 | 0.0168 | 0.0171 | 0.0175 | 0.0178 | 0.0181 | 0.0185 |
| .1       | 0.0188 | 0.0192 | 0.0195 | 0.0199 | 0.0202 | 0.0206 | 0.0209 | 0.0213 | 0.0216 | 0.0220 |
| .2       | 0.0224 | 0.0228 | 0.0231 | 0.0235 | 0.0239 | 0.0243 | 0.0247 | 0.0251 | 0.0255 | 0.0259 |
| .3       | 0.0263 | 0.0267 | 0.0271 | 0.0275 | 0.0279 | 0.0283 | 0.0288 | 0.0292 | 0.0296 | 0.0300 |
| .4       | 0.0305 | 0.0309 | 0.0313 | 0.0318 | 0.0322 | 0.0327 | 0.0331 | 0.0336 | 0.0341 | 0.0345 |
| .5       | 0.0350 | 0.0354 | 0.0359 | 0.0364 | 0.0369 | 0.0374 | 0.0378 | 0.0383 | 0.0388 | 0.0393 |
| .6       | 0.0398 | 0.0403 | 0.0408 | 0.0413 | 0.0418 | 0.0423 | 0.0428 | 0.0434 | 0.0439 | 0.0444 |
| .7       | 0.0449 | 0.0455 | 0.0460 | 0.0465 | 0.0471 | 0.0476 | 0.0482 | 0.0487 | 0.0493 | 0.0498 |
| .8       | 0.0504 | 0.0509 | 0.0515 | 0.0521 | 0.0526 | 0.0532 | 0.0538 | 0.0544 | 0.0549 | 0.0555 |
| .9       | 0.0561 | 0.0567 | 0.0573 | 0.0579 | 0.0585 | 0.0591 | 0.0597 | 0.0603 | 0.0609 | 0.0616 |
| 2.0      | 0.0622 | 0.0628 | 0.0634 | 0.0641 | 0.0647 | 0.0653 | 0.0660 | 0.0666 | 0.0673 | 0.0679 |
| .1       | 0.0686 | 0.0692 | 0.0699 | 0.0705 | 0.0712 | 0.0719 | 0.0725 | 0.0732 | 0.0739 | 0.0746 |
| .2       | 0.0752 | 0.0759 | 0.0766 | 0.0773 | 0.0780 | 0.0787 | 0.0794 | 0.0801 | 0.0808 | 0.0815 |
| .3       | 0.0822 | 0.0830 | 0.0837 | 0.0844 | 0.0851 | 0.0859 | 0.866  | 0.0873 | 0.0881 | 0.0888 |
| .4       | 0.0895 | 0.0903 | 0.0910 | 0.0918 | 0.0926 | 0.0933 | 0.0941 | 0.0948 | 0.0956 | 0.0964 |
| .5       | 0.0972 | 0.0979 | 0.0987 | 0.0995 | 0.1003 | 0.1011 | 0.1019 | 0.1027 | 0.1035 | 0.1043 |
| .6       | 0.1051 | 0.1059 | 0.1067 | 0.1075 | 0.1084 | 0.1092 | 0.1100 | 0.1108 | 0.1117 | 0.1125 |
| .7       | 0.1133 | 0.1142 | 0.1150 | 0.1159 | 0.1167 | 0.1176 | 0.1184 | 0.1193 | 0.1201 | 0.1210 |
| .8       | 0.1219 | 0.1228 | 0.1236 | 0.1245 | 0.1254 | 0.1263 | 0.1272 | 0.1281 | 0.1289 | 0.1298 |
| .9       | 0.1317 | 0.1316 | 0.1326 | 0.1335 | 0.1344 | 0.1353 | 0.1362 | 0.1371 | 0.1381 | 0.1390 |
| 3.0      | 0.1399 | 0.1409 | 0.1418 | 0.1427 | 0.1437 | 0.1446 | 0.1456 | 0.1465 | 0.1475 | 0.1484 |
| .1       | 0.1494 | 0.1504 | 0.1513 | 0.1523 | 0.1533 | 0.1543 | 0.1552 | 0.1562 | 0.1572 | 0.1582 |
| .2       | 0.1592 | 0.1602 | 0.1612 | 0.1622 | 0.1632 | 0.1642 | 0.1652 | 0.1662 | 0.1673 | 0.1683 |
| .3       | 0.1693 | 0.1703 | 0.1714 | 0.1724 | 0.1734 | 0.1745 | 0.1755 | 0.1766 | 0.1776 | 0.1787 |
| .4       | 0.1797 | 0.1808 | 0.1818 | 0.1829 | 0.1840 | 0.1850 | 0.1861 | 0.1872 | 0.1883 | 0.1894 |
| .5       | 0.1904 | 0.1915 | 0.1926 | 0.1937 | 0.1948 | 0.1959 | 0.1970 | 0.1981 | 0.1992 | 0.2004 |
| .6       | 0.2015 | 0.2026 | 0.2037 | 0.2049 | 0.2060 | 0.2071 | 0.2083 | 0.2094 | 0.2106 | 0.2117 |
| .7       | 0.2128 | 0.2140 | 0.2151 | 0.2163 | 0.2175 | 0.2186 | 0.2198 | 0.2210 | 0.2221 | 0.2233 |
| .8       | 0.2245 | 0.2257 | 0.2269 | 0.2280 | 0.2292 | 0.2304 | 0.2316 | 0.2328 | 0.2340 | 0.2352 |
| .9       | 0.2365 | 0.2377 | 0.2389 | 0.2401 | 0.2413 | 0.2426 | 0.2438 | 0.2450 | 0.2463 | 0.2475 |
| 4.0      | 0.2487 | 0.2500 | 0.2512 | 0.2525 | 0.2537 | 0.2550 | 0.2563 | 0.2575 | 0.2588 | 0.2601 |
| .1       | 0.2618 | 0.2626 | 0.2633 | 0.2652 | 0.2665 | 0.2677 | 0.2690 | 0.2703 | 0.2716 | 0.2729 |
| .2       | 0.2742 | 0.2755 | 0.2769 | 0.2782 | 0.2795 | 0.2808 | 0.2821 | 0.2835 | 0.2848 | 0.2861 |
| .3       | 0.2875 | 0.2888 | 0.2901 | 0.2915 | 0.2928 | 0.2942 | 0.2955 | 0.2969 | 0.2982 | 0.2996 |
| .4       | 0.3010 | 0.3023 | 0.3037 | 0.3051 | 0.3065 | 0.3079 | 0.3092 | 0.3106 | 0.3120 | 0.3134 |
| .5       | 0.3148 | 0.3162 | 0.3176 | 0.3190 | 0.3204 | 0.3218 | 0.3232 | 0.3247 | 0.3261 | 0.3275 |
| .6       | 0.3290 | 0.3304 | 0.3318 | 0.3333 | 0.3347 | 0.3362 | 0.3376 | 0.3390 | 0.3405 | 0.3420 |
| .7       | 0.3434 | 0.3449 | 0.3463 | 0.3478 | 0.3493 | 0.3508 | 0.3522 | 0.3537 | 0.3552 | 0.3567 |
| .8       | 0.3582 | 0.3597 | 0.3612 | 0.3627 | 0.3642 | 0.3657 | 0.3672 | 0.3687 | 0.3702 | 0.3717 |
| .9       | 0.3733 | 0.3748 | 0.3763 | 0.3779 | 0.3794 | 0.3809 | 0.3825 | 0.3840 | 0.3856 | 0.3871 |

## DISCHARGE, IN CUBIC FEET PER SECOND, OF A WEIR ONE FOOT LONG, WITHOUT CONTRACTION AT THE ENDS; FOR DEPTHS FROM 0 TO 0.499 FEET.

| Depth. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0.00   | 0.0000 | 0.0001 | 0.0003 | 0.0005 | 0.0008 | 0.0012 | 0.0015 | 0.0020 | 0.0024 | 0.0028 |
| .01    | 0.0033 | 0.0038 | 0.0044 | 0.0049 | 0.0055 | 0.0061 | 0.0067 | 0.0074 | 0.0080 | 0.0087 |
| .02    | 0.0094 | 0.0101 | 0.0109 | 0.0116 | 0.0124 | 0.0132 | 0.0140 | 0.0148 | 0.0156 | 0.0164 |
| .03    | 0.0173 | 0.0182 | 0.0191 | 0.0200 | 0.0209 | 0.0218 | 0.0227 | 0.0237 | 0.0247 | 0.0256 |
| .04    | 0.0266 | 0.0276 | 0.0287 | 0.0297 | 0.0307 | 0.0318 | 0.0329 | 0.0339 | 0.0350 | 0.0361 |
| .05    | 0.0372 | 0.0384 | 0.0395 | 0.0406 | 0.0418 | 0.0430 | 0.0441 | 0.0453 | 0.0465 | 0.0477 |
| .06    | 0.0489 | 0.0502 | 0.0514 | 0.0527 | 0.0539 | 0.0552 | 0.0565 | 0.0578 | 0.0590 | 0.0604 |
| .07    | 0.0617 | 0.0630 | 0.0643 | 0.0657 | 0.0670 | 0.0684 | 0.0698 | 0.0712 | 0.0725 | 0.0739 |
| .08    | 0.0753 | 0.0768 | 0.0782 | 0.0796 | 0.0811 | 0.0825 | 0.0840 | 0.0855 | 0.0869 | 0.0884 |
| .09    | 0.0899 | 0.0914 | 0.0929 | 0.0944 | 0.0960 | 0.0975 | 0.0990 | 0.1006 | 0.1022 | 0.1037 |
| 0.10   | 0.1053 | 0.1069 | 0.1085 | 0.1101 | 0.1117 | 0.1133 | 0.1149 | 0.1166 | 0.1182 | 0.1198 |
| .11    | 0.1215 | 0.1231 | 0.1248 | 0.1265 | 0.1282 | 0.1299 | 0.1316 | 0.1333 | 0.1350 | 0.1367 |
| .12    | 0.1384 | 0.1402 | 0.1419 | 0.1436 | 0.1454 | 0.1472 | 0.1489 | 0.1507 | 0.1525 | 0.1543 |
| .13    | 0.1561 | 0.1579 | 0.1597 | 0.1615 | 0.1633 | 0.1652 | 0.1670 | 0.1689 | 0.1707 | 0.1726 |
| .14    | 0.1744 | 0.1763 | 0.1782 | 0.1801 | 0.1820 | 0.1839 | 0.1858 | 0.1877 | 0.1896 | 0.1915 |
| .15    | 0.1935 | 0.1954 | 0.1973 | 0.1993 | 0.2012 | 0.2032 | 0.2052 | 0.2072 | 0.2091 | 0.2111 |
| .16    | 0.2131 | 0.2151 | 0.2171 | 0.2191 | 0.2212 | 0.2232 | 0.2252 | 0.2273 | 0.2293 | 0.2314 |
| .17    | 0.2334 | 0.2355 | 0.2375 | 0.2396 | 0.2417 | 0.2438 | 0.2459 | 0.2480 | 0.2501 | 0.2522 |
| .18    | 0.2543 | 0.2564 | 0.2586 | 0.2607 | 0.2628 | 0.2650 | 0.2671 | 0.2693 | 0.2714 | 0.2736 |
| .19    | 0.2758 | 0.2780 | 0.2802 | 0.2823 | 0.2845 | 0.2867 | 0.2890 | 0.2912 | 0.2934 | 0.2956 |
| 0.20   | 0.2978 | 0.3001 | 0.3025 | 0.3046 | 0.3068 | 0.3091 | 0.3113 | 0.3136 | 0.3159 | 0.3182 |
| .21    | 0.3205 | 0.3228 | 0.3250 | 0.3274 | 0.3297 | 0.3320 | 0.3343 | 0.3366 | 0.3389 | 0.3413 |
| .22    | 0.3436 | 0.3460 | 0.3483 | 0.3507 | 0.3530 | 0.3554 | 0.3578 | 0.3601 | 0.3625 | 0.3649 |
| .23    | 0.3673 | 0.3697 | 0.3721 | 0.3745 | 0.3769 | 0.3794 | 0.3818 | 0.3842 | 0.3866 | 0.3891 |
| .24    | 0.3915 | 0.3940 | 0.3964 | 0.3989 | 0.4014 | 0.4038 | 0.4063 | 0.4088 | 0.4113 | 0.4138 |
| .25    | 0.4162 | 0.4187 | 0.4213 | 0.4238 | 0.4263 | 0.4288 | 0.4313 | 0.4339 | 0.4364 | 0.4389 |
| .26    | 0.4415 | 0.4440 | 0.4466 | 0.4491 | 0.4517 | 0.4543 | 0.4568 | 0.4594 | 0.4620 | 0.4646 |
| .27    | 0.4672 | 0.4698 | 0.4724 | 0.4750 | 0.4776 | 0.4802 | 0.4828 | 0.4855 | 0.4881 | 0.4907 |
| .28    | 0.4934 | 0.4960 | 0.4987 | 0.5013 | 0.5040 | 0.5067 | 0.5093 | 0.5120 | 0.5147 | 0.5174 |
| .29    | 0.5200 | 0.5227 | 0.5254 | 0.5281 | 0.5308 | 0.5336 | 0.5363 | 0.5390 | 0.5417 | 0.5444 |
| 0.30   | 0.5472 | 0.5499 | 0.5527 | 0.5554 | 0.5582 | 0.5609 | 0.5637 | 0.5664 | 0.5692 | 0.5720 |
| .31    | 0.5748 | 0.5775 | 0.5803 | 0.5831 | 0.5859 | 0.5887 | 0.5915 | 0.5943 | 0.5972 | 0.6000 |
| .32    | 0.6028 | 0.6056 | 0.6085 | 0.6113 | 0.6141 | 0.6170 | 0.6198 | 0.6227 | 0.6255 | 0.6284 |
| .33    | 0.6313 | 0.6341 | 0.6370 | 0.6399 | 0.6428 | 0.6457 | 0.6486 | 0.6515 | 0.6544 | 0.6573 |
| .34    | 0.6602 | 0.6631 | 0.6660 | 0.6689 | 0.6719 | 0.6748 | 0.6777 | 0.6807 | 0.6836 | 0.6866 |
| .35    | 0.6895 | 0.6925 | 0.6954 | 0.6984 | 0.7014 | 0.7043 | 0.7073 | 0.7103 | 0.7133 | 0.7163 |
| .36    | 0.7193 | 0.7223 | 0.7253 | 0.7283 | 0.7313 | 0.7343 | 0.7373 | 0.7404 | 0.7434 | 0.7464 |
| .37    | 0.7495 | 0.7525 | 0.7555 | 0.7586 | 0.7616 | 0.7647 | 0.7678 | 0.7708 | 0.7739 | 0.7770 |
| .38    | 0.7800 | 0.7831 | 0.7862 | 0.7893 | 0.7924 | 0.7955 | 0.7986 | 0.8017 | 0.8048 | 0.8079 |
| .39    | 0.8110 | 0.8142 | 0.8173 | 0.8204 | 0.8235 | 0.8267 | 0.8298 | 0.8330 | 0.8361 | 0.8393 |
| 0.40   | 0.8424 | 0.8456 | 0.8488 | 0.8519 | 0.8551 | 0.8583 | 0.8615 | 0.8646 | 0.8678 | 0.8710 |
| .41    | 0.8742 | 0.8774 | 0.8806 | 0.8838 | 0.8870 | 0.8903 | 0.8935 | 0.8967 | 0.8999 | 0.9032 |
| .42    | 0.9064 | 0.9096 | 0.9129 | 0.9161 | 0.9194 | 0.9226 | 0.9259 | 0.9292 | 0.9324 | 0.9357 |
| .43    | 0.9390 | 0.9422 | 0.9455 | 0.9488 | 0.9521 | 0.9554 | 0.9587 | 0.9620 | 0.9653 | 0.9686 |
| .44    | 0.9719 | 0.9752 | 0.9785 | 0.9819 | 0.9852 | 0.9885 | 0.9919 | 0.9952 | 0.9985 | 1.0019 |
| .45    | 1.0052 | 1.0086 | 1.0119 | 1.0153 | 1.0187 | 1.0220 | 1.0254 | 1.0288 | 1.0321 | 1.0355 |
| .46    | 1.0389 | 1.0423 | 1.0457 | 1.0491 | 1.0525 | 1.0559 | 1.0593 | 1.0627 | 1.0661 | 1.0696 |
| .47    | 1.0730 | 1.0764 | 1.0798 | 1.0833 | 1.0867 | 1.0901 | 1.0936 | 1.0970 | 1.1005 | 1.1039 |
| .48    | 1.1074 | 1.1109 | 1.1143 | 1.1178 | 1.1213 | 1.1248 | 1.1282 | 1.1317 | 1.1352 | 1.1387 |
| .49    | 1.1422 | 1.1457 | 1.1492 | 1.1527 | 1.1562 | 1.1597 | 1.1632 | 1.1668 | 1.1703 | 1.1738 |

DISCHARGE, IN CUBIC FEET PER SECOND, OF A WEIR ONE FOOT LONG, WITHOUT CONTRACTION AT THE ENDS; FOR DEPTHS FROM 0.500 TO 0.999 FEET.

| Depth. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0.50   | 1.1773 | 1.1800 | 1.1844 | 1.1879 | 1.1915 | 1.1950 | 1.1986 | 1.2021 | 1.2057 | 1.2093 |
| .51    | 1.2128 | 1.2164 | 1.2200 | 1.2235 | 1.2271 | 1.2307 | 1.2343 | 1.2379 | 1.2415 | 1.2451 |
| .52    | 1.2487 | 1.2523 | 1.2559 | 1.2595 | 1.2631 | 1.2667 | 1.2703 | 1.2740 | 1.2776 | 1.2812 |
| .53    | 1.2849 | 1.2885 | 1.2921 | 1.2958 | 1.2994 | 1.3031 | 1.3067 | 1.3104 | 1.3141 | 1.3177 |
| .54    | 1.3214 | 1.3251 | 1.3287 | 1.3324 | 1.3361 | 1.3398 | 1.3435 | 1.3472 | 1.3509 | 1.3546 |
| .55    | 1.3583 | 1.3620 | 1.3657 | 1.3694 | 1.3731 | 1.3768 | 1.3806 | 1.3843 | 1.3880 | 1.3918 |
| .56    | 1.3955 | 1.3992 | 1.4030 | 1.4067 | 1.4105 | 1.4142 | 1.4180 | 1.4217 | 1.4255 | 1.4293 |
| .57    | 1.4330 | 1.4368 | 1.4406 | 1.4444 | 1.4481 | 1.4519 | 1.4557 | 1.4595 | 1.4633 | 1.4671 |
| .58    | 1.4709 | 1.4747 | 1.4785 | 1.4823 | 1.4862 | 1.4900 | 1.4938 | 1.4976 | 1.5014 | 1.5053 |
| .59    | 1.5091 | 1.5130 | 1.5168 | 1.5206 | 1.5245 | 1.5283 | 1.5322 | 1.5361 | 1.5399 | 1.5438 |
| 0.60   | 1.5476 | 1.5515 | 1.5554 | 1.5593 | 1.5631 | 1.5670 | 1.5709 | 1.5748 | 1.5787 | 1.5826 |
| .61    | 1.5865 | 1.5904 | 1.5943 | 1.5982 | 1.6021 | 1.6060 | 1.6100 | 1.6139 | 1.6178 | 1.6217 |
| .62    | 1.6257 | 1.6296 | 1.6335 | 1.6375 | 1.6414 | 1.6454 | 1.6493 | 1.6533 | 1.6572 | 1.6612 |
| .63    | 1.6652 | 1.6691 | 1.6731 | 1.6771 | 1.6810 | 1.6850 | 1.6890 | 1.6930 | 1.6970 | 1.7010 |
| .64    | 1.7050 | 1.7090 | 1.7130 | 1.7170 | 1.7210 | 1.7250 | 1.7290 | 1.7330 | 1.7370 | 1.7410 |
| .65    | 1.7451 | 1.7491 | 1.7531 | 1.7572 | 1.7612 | 1.7652 | 1.7693 | 1.7733 | 1.7774 | 1.7814 |
| .66    | 1.7855 | 1.7896 | 1.7936 | 1.7977 | 1.8018 | 1.8058 | 1.8099 | 1.8140 | 1.8181 | 1.8221 |
| .67    | 1.8262 | 1.8303 | 1.8344 | 1.8385 | 1.8426 | 1.8467 | 1.8508 | 1.8549 | 1.8590 | 1.8632 |
| .68    | 1.8673 | 1.8714 | 1.8755 | 1.8796 | 1.8838 | 1.8879 | 1.8920 | 1.8962 | 1.9003 | 1.9045 |
| .69    | 1.9086 | 1.9128 | 1.9169 | 1.9211 | 1.9252 | 1.9294 | 1.9336 | 1.9377 | 1.9419 | 1.9461 |
| 0.70   | 1.9503 | 1.9544 | 1.9586 | 1.9628 | 1.9670 | 1.9712 | 1.9754 | 1.9796 | 1.9838 | 1.9880 |
| .71    | 1.9922 | 1.9964 | 2.0006 | 2.0048 | 2.0091 | 2.0133 | 2.0175 | 2.0217 | 2.0260 | 2.0302 |
| .72    | 2.0344 | 2.0387 | 2.0429 | 2.0472 | 2.0514 | 2.0557 | 2.0599 | 2.0642 | 2.0684 | 2.0727 |
| .73    | 2.0770 | 2.0812 | 2.0855 | 2.0898 | 2.0941 | 2.0983 | 2.1026 | 2.1069 | 2.1112 | 2.1155 |
| .74    | 2.1198 | 2.1241 | 2.1284 | 2.1327 | 2.1370 | 2.1413 | 2.1456 | 2.1499 | 2.1543 | 2.1586 |
| .75    | 2.1629 | 2.1672 | 2.1716 | 2.1759 | 2.1802 | 2.1846 | 2.1889 | 2.1932 | 2.1976 | 2.2019 |
| .76    | 2.2063 | 2.2107 | 2.2150 | 2.2194 | 2.2237 | 2.2281 | 2.2325 | 2.2369 | 2.2413 | 2.2456 |
| .77    | 2.2500 | 2.2544 | 2.2588 | 2.2632 | 2.2675 | 2.2719 | 2.2763 | 2.2807 | 2.2851 | 2.2896 |
| .78    | 2.2940 | 2.2984 | 2.3028 | 2.3072 | 2.3116 | 2.3161 | 2.3205 | 2.3249 | 2.3293 | 2.3338 |
| .79    | 2.3382 | 2.3427 | 2.3471 | 2.3515 | 2.3560 | 2.3604 | 2.3649 | 2.3694 | 2.3738 | 2.3783 |
| 0.80   | 2.3828 | 2.3872 | 2.3917 | 2.3962 | 2.4006 | 2.4051 | 2.4096 | 2.4141 | 2.4186 | 2.4231 |
| .81    | 2.4276 | 2.4321 | 2.4366 | 2.4411 | 2.4456 | 2.4501 | 2.4546 | 2.4591 | 2.4636 | 2.4681 |
| .82    | 2.4727 | 2.4772 | 2.4817 | 2.4862 | 2.4908 | 2.4953 | 2.4999 | 2.5044 | 2.5089 | 2.5135 |
| .83    | 2.5180 | 2.5226 | 2.5271 | 2.5317 | 2.5363 | 2.5408 | 2.5454 | 2.5500 | 2.5545 | 2.5591 |
| .84    | 2.5637 | 2.5683 | 2.5728 | 2.5774 | 2.5820 | 2.5866 | 2.5912 | 2.5958 | 2.6004 | 2.6050 |
| .85    | 2.6096 | 2.6142 | 2.6188 | 2.6234 | 2.6280 | 2.6327 | 2.6373 | 2.6419 | 2.6465 | 2.6511 |
| .86    | 2.6553 | 2.6600 | 2.6646 | 2.6692 | 2.6738 | 2.6790 | 2.6836 | 2.6883 | 2.6929 | 2.6976 |
| .87    | 2.7022 | 2.7069 | 2.7116 | 2.7162 | 2.7209 | 2.7256 | 2.7303 | 2.7349 | 2.7396 | 2.7443 |
| .88    | 2.7490 | 2.7536 | 2.7583 | 2.7630 | 2.7677 | 2.7724 | 2.7771 | 2.7818 | 2.7865 | 2.7912 |
| .89    | 2.7959 | 2.8007 | 2.8054 | 2.8101 | 2.8148 | 2.8195 | 2.8243 | 2.8290 | 2.8337 | 2.8385 |
| 0.90   | 2.8432 | 2.8479 | 2.8527 | 2.8574 | 2.8622 | 2.8669 | 2.8717 | 2.8764 | 2.8812 | 2.8860 |
| .91    | 2.8907 | 2.8955 | 2.9003 | 2.9050 | 2.9098 | 2.9146 | 2.9194 | 2.9241 | 2.9289 | 2.9337 |
| .92    | 2.9385 | 2.9433 | 2.9481 | 2.9529 | 2.9577 | 2.9625 | 2.9673 | 2.9721 | 2.9769 | 2.9817 |
| .93    | 2.9865 | 2.9914 | 2.9962 | 3.0010 | 3.0058 | 3.0107 | 3.0155 | 3.0203 | 3.0252 | 3.0300 |
| .94    | 3.0348 | 3.0397 | 3.0445 | 3.0494 | 3.0542 | 3.0591 | 3.0639 | 3.0688 | 3.0737 | 3.0785 |
| .95    | 3.0831 | 3.0883 | 3.0931 | 3.0980 | 3.1029 | 3.1078 | 3.1127 | 3.1175 | 3.1224 | 3.1273 |
| .96    | 3.1322 | 3.1371 | 3.1420 | 3.1469 | 3.1518 | 3.1567 | 3.1616 | 3.1665 | 3.1714 | 3.1764 |
| .97    | 3.1813 | 3.1862 | 3.1911 | 3.1960 | 3.2010 | 3.2059 | 3.2108 | 3.2158 | 3.2207 | 3.2257 |
| .98    | 3.2306 | 3.2355 | 3.2405 | 3.2454 | 3.2504 | 3.2554 | 3.2603 | 3.2653 | 3.2702 | 3.2752 |
| .99    | 3.2802 | 3.2851 | 3.2901 | 3.2951 | 3.3001 | 3.3051 | 3.3100 | 3.3150 | 3.3200 | 3.3250 |

DISCHARGE, IN CUBIC FEET PER SECOND, OF A WEIR ONE FOOT LONG, WITHOUT CONTRACTION AT THE ENDS; FOR DEPTHS FROM 1.000 TO 1.400 FEET.

| Depth. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 1.00   | 3.3300 | 3.3350 | 3.3400 | 3.3450 | 3.3500 | 3.3550 | 3.3600 | 3.3650 | 3.3700 | 3.3751 |
| .01    | 3.3801 | 3.3851 | 3.3901 | 3.3951 | 3.4002 | 3.4052 | 3.4102 | 3.4153 | 3.4203 | 3.4254 |
| .02    | 3.4304 | 3.4354 | 3.4405 | 3.4455 | 3.4506 | 3.4557 | 3.4607 | 3.4658 | 3.4708 | 3.4759 |
| .03    | 3.4810 | 3.4860 | 3.4911 | 3.4962 | 3.5013 | 3.5063 | 3.5114 | 3.5165 | 3.5216 | 3.5267 |
| .04    | 3.5318 | 3.5369 | 3.5420 | 3.5471 | 3.5522 | 3.5573 | 3.5624 | 3.5675 | 3.5726 | 3.5777 |
| .05    | 3.5828 | 3.5880 | 3.5931 | 3.5982 | 3.6033 | 3.6085 | 3.6136 | 3.6187 | 3.6239 | 3.6290 |
| .06    | 3.6342 | 3.6393 | 3.6444 | 3.6496 | 3.6547 | 3.6599 | 3.6651 | 3.6702 | 3.6754 | 3.6805 |
| .07    | 3.6857 | 3.6908 | 3.6960 | 3.7012 | 3.7064 | 3.7116 | 3.7167 | 3.7219 | 3.7271 | 3.7323 |
| .08    | 3.7375 | 3.7427 | 3.7479 | 3.7531 | 3.7583 | 3.7635 | 3.7687 | 3.7739 | 3.7791 | 3.7843 |
| .09    | 3.7895 | 3.7947 | 3.8000 | 3.8052 | 3.8104 | 3.8156 | 3.8209 | 3.8261 | 3.8313 | 3.8365 |
| 1.10   | 3.8418 | 3.8470 | 3.8523 | 3.8575 | 3.8628 | 3.8680 | 3.8733 | 3.8785 | 3.8838 | 3.8890 |
| .11    | 3.8943 | 3.8996 | 3.9048 | 3.9101 | 3.9154 | 3.9206 | 3.9259 | 3.9312 | 3.9365 | 3.9418 |
| .12    | 3.9470 | 3.9523 | 3.9576 | 3.9629 | 3.9682 | 3.9735 | 3.9788 | 3.9841 | 3.9894 | 3.9947 |
| .13    | 4.0000 | 4.0053 | 4.0106 | 4.0160 | 4.0213 | 4.0266 | 4.0319 | 4.0372 | 4.0426 | 4.0479 |
| .14    | 4.0532 | 4.0586 | 4.0639 | 4.0692 | 4.0746 | 4.0799 | 4.0853 | 4.0906 | 4.0960 | 4.1013 |
| .15    | 4.1067 | 4.1120 | 4.1174 | 4.1228 | 4.1281 | 4.1335 | 4.1389 | 4.1442 | 4.1496 | 4.1550 |
| .16    | 4.1604 | 4.1657 | 4.1711 | 4.1765 | 4.1819 | 4.1873 | 4.1927 | 4.1981 | 4.2035 | 4.2089 |
| .17    | 4.2143 | 4.2197 | 4.2251 | 4.2305 | 4.2359 | 4.2413 | 4.2467 | 4.2522 | 4.2576 | 4.2630 |
| .18    | 4.2684 | 4.2738 | 4.2793 | 4.2847 | 4.2901 | 4.2956 | 4.3010 | 4.3065 | 4.3119 | 4.3173 |
| .19    | 4.3228 | 4.3282 | 4.3337 | 4.3392 | 4.3446 | 4.3501 | 4.3555 | 4.3610 | 4.3665 | 4.3719 |
| 1.20   | 4.3774 | 4.3829 | 4.3883 | 4.3938 | 4.3993 | 4.4048 | 4.4103 | 4.4158 | 4.4212 | 4.4267 |
| .21    | 4.4322 | 4.4377 | 4.4432 | 4.4487 | 4.4542 | 4.4597 | 4.4652 | 4.4707 | 4.4763 | 4.4818 |
| .22    | 4.4873 | 4.4928 | 4.4983 | 4.5038 | 4.5094 | 4.5149 | 4.5204 | 4.5260 | 4.5315 | 4.5370 |
| .23    | 4.5426 | 4.5481 | 4.5537 | 4.5592 | 4.5647 | 4.5703 | 4.5759 | 4.5814 | 4.5870 | 4.5925 |
| .24    | 4.5981 | 4.6036 | 4.6092 | 4.6148 | 4.6203 | 4.6259 | 4.6315 | 4.6371 | 4.6427 | 4.6482 |
| .25    | 4.6538 | 4.6594 | 4.6650 | 4.6706 | 4.6762 | 4.6818 | 4.6874 | 4.6930 | 4.6986 | 4.7042 |
| .26    | 4.7098 | 4.7154 | 4.7210 | 4.7266 | 4.7322 | 4.7378 | 4.7435 | 4.7491 | 4.7547 | 4.7603 |
| .27    | 4.7660 | 4.7716 | 4.7772 | 4.7829 | 4.7885 | 4.7941 | 4.7998 | 4.8054 | 4.8111 | 4.8167 |
| .28    | 4.8224 | 4.8280 | 4.8337 | 4.8393 | 4.8450 | 4.8506 | 4.8563 | 4.8620 | 4.8676 | 4.8733 |
| .29    | 4.8790 | 4.8847 | 4.8903 | 4.8960 | 4.9017 | 4.9074 | 4.9131 | 4.9187 | 4.9244 | 4.9301 |
| 1.30   | 4.9358 | 4.9415 | 4.9472 | 4.9529 | 4.9586 | 4.9643 | 4.9700 | 4.9757 | 4.9814 | 4.9872 |
| .31    | 4.9929 | 4.9986 | 5.0043 | 5.0100 | 5.0158 | 5.0215 | 5.0272 | 5.0330 | 5.0387 | 5.0444 |
| .32    | 5.0502 | 5.0559 | 5.0616 | 5.0674 | 5.0731 | 5.0789 | 5.0846 | 5.0904 | 5.0961 | 5.1019 |
| .33    | 5.1077 | 5.1134 | 5.1192 | 5.1249 | 5.1307 | 5.1365 | 5.1423 | 5.1480 | 5.1538 | 5.1596 |
| .34    | 5.1654 | 5.1712 | 5.1769 | 5.1827 | 5.1885 | 5.1943 | 5.2001 | 5.2059 | 5.2117 | 5.2175 |
| .35    | 5.2233 | 5.2291 | 5.2349 | 5.2407 | 5.2465 | 5.2523 | 5.2582 | 5.2640 | 5.2698 | 5.2756 |
| .36    | 5.2814 | 5.2873 | 5.2931 | 5.2989 | 5.3048 | 5.3106 | 5.3164 | 5.3223 | 5.3281 | 5.3340 |
| .37    | 5.3398 | 5.3456 | 5.3515 | 5.3573 | 5.3632 | 5.3691 | 5.3749 | 5.3808 | 5.3866 | 5.3925 |
| .38    | 5.3984 | 5.4042 | 5.4101 | 5.4160 | 5.4219 | 5.4277 | 5.4336 | 5.4395 | 5.4454 | 5.4513 |
| .39    | 5.4572 | 5.4630 | 5.4689 | 5.4748 | 5.4807 | 5.4866 | 5.4925 | 5.4984 | 5.5043 | 5.5102 |
| 1.40   | 5.5162 | 5.5221 | 5.5280 | 5.5339 | 5.5398 | 5.5457 | 5.5516 | 5.5575 | 5.5635 | 5.5694 |
| .41    | 5.5754 | 5.5813 | 5.5872 | 5.5932 | 5.5991 | 5.6050 | 5.6110 | 5.6169 | 5.6229 | 5.6288 |
| .42    | 5.6348 | 5.6407 | 5.6467 | 5.6526 | 5.6586 | 5.6646 | 5.6705 | 5.6765 | 5.6825 | 5.6884 |
| .43    | 5.6944 | 5.7004 | 5.7064 | 5.7123 | 5.7183 | 5.7243 | 5.7303 | 5.7363 | 5.7423 | 5.7482 |
| .44    | 5.7542 | 5.7602 | 5.7662 | 5.7722 | 5.7782 | 5.7842 | 5.7902 | 5.7962 | 5.8023 | 5.8083 |
| .45    | 5.8143 | 5.8203 | 5.8263 | 5.8323 | 5.8384 | 5.8444 | 5.8504 | 5.8564 | 5.8625 | 5.8685 |
| .46    | 5.8745 | 5.8806 | 5.8866 | 5.8926 | 5.8987 | 5.9047 | 5.9107 | 5.9168 | 5.9229 | 5.9289 |
| .47    | 5.9350 | 5.9410 | 5.9471 | 5.9532 | 5.9592 | 5.9653 | 5.9714 | 5.9774 | 5.9835 | 5.9896 |
| .48    | 5.9957 | 6.0017 | 6.0078 | 6.0139 | 6.0200 | 6.0261 | 6.0322 | 6.0382 | 6.0443 | 6.0504 |
| .49    | 6.0565 | 6.0626 | 6.0687 | 6.0748 | 6.0809 | 6.0870 | 6.0931 | 6.0993 | 6.1054 | 6.1115 |

DISCHARGE, IN CUBIC FEET PER SECOND, OF A WEIR ONE FOOT LONG, WITHOUT CONTRACTION AT THE ENDS; FOR DEPTHS FROM 1.500 TO 1.900 FEET.

| Depth. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 1.50   | 6.1176 | 6.1237 | 6.1298 | 6.1360 | 6.1421 | 6.1482 | 6.1543 | 6.1605 | 6.1666 | 6.1727 |
| .51    | 6.1789 | 6.1850 | 6.1912 | 6.1973 | 6.2034 | 6.2096 | 6.2157 | 6.2219 | 6.2280 | 6.2342 |
| .52    | 6.2404 | 6.2465 | 6.2527 | 6.2588 | 6.2650 | 6.2712 | 6.2773 | 6.2835 | 6.2897 | 6.2959 |
| .53    | 6.3020 | 6.3082 | 6.3144 | 6.3206 | 6.3268 | 6.3330 | 6.3391 | 6.3453 | 6.3515 | 6.3577 |
| .54    | 6.3639 | 6.3701 | 6.3763 | 6.3825 | 6.3887 | 6.3949 | 6.4012 | 6.4074 | 6.4136 | 6.4198 |
| .55    | 6.4260 | 6.4322 | 6.4385 | 6.4447 | 6.4509 | 6.4571 | 6.4634 | 6.4696 | 6.4758 | 6.4821 |
| .56    | 6.4883 | 6.4945 | 6.5008 | 6.5070 | 6.5133 | 6.5195 | 6.5258 | 6.5320 | 6.5383 | 6.5445 |
| .57    | 6.5508 | 6.5570 | 6.5633 | 6.5696 | 6.5758 | 6.5821 | 6.5884 | 6.5946 | 6.6009 | 6.6072 |
| .58    | 6.6135 | 6.6198 | 6.6260 | 6.6323 | 6.6386 | 6.6449 | 6.6512 | 6.6575 | 6.6638 | 6.6701 |
| .59    | 6.6764 | 6.6827 | 6.6890 | 6.6953 | 6.7016 | 6.7079 | 6.7142 | 6.7205 | 6.7268 | 6.7331 |
| 1.60   | 6.7394 | 6.7458 | 6.7521 | 6.7584 | 6.7647 | 6.7711 | 6.7774 | 6.7837 | 6.7901 | 6.7964 |
| .61    | 6.8027 | 6.8091 | 6.8154 | 6.8217 | 6.8281 | 6.8344 | 6.8408 | 6.8471 | 6.8535 | 6.8598 |
| .62    | 6.8662 | 6.8726 | 6.8789 | 6.8853 | 6.8916 | 6.8980 | 6.9044 | 6.9108 | 6.9171 | 6.9235 |
| .63    | 6.9299 | 6.9363 | 6.9426 | 6.9490 | 6.9554 | 6.9618 | 6.9682 | 6.9746 | 6.9810 | 6.9874 |
| .64    | 6.9937 | 7.0001 | 7.0065 | 7.0129 | 7.0193 | 7.0257 | 7.0321 | 7.0385 | 7.0449 | 7.0513 |
| .65    | 7.0578 | 7.0642 | 7.0706 | 7.0771 | 7.0835 | 7.0899 | 7.0963 | 7.1028 | 7.1092 | 7.1156 |
| .66    | 7.1211 | 7.1285 | 7.1349 | 7.1414 | 7.1478 | 7.1543 | 7.1607 | 7.1672 | 7.1736 | 7.1801 |
| .67    | 7.1865 | 7.1930 | 7.1994 | 7.2059 | 7.2124 | 7.2188 | 7.2253 | 7.2318 | 7.2382 | 7.2447 |
| .68    | 7.2512 | 7.2576 | 7.2641 | 7.2706 | 7.2771 | 7.2836 | 7.2901 | 7.2965 | 7.3030 | 7.3095 |
| .69    | 7.3160 | 7.3225 | 7.3290 | 7.3355 | 7.3420 | 7.3485 | 7.3550 | 7.3615 | 7.3680 | 7.3745 |
| 1.70   | 7.3810 | 7.3876 | 7.3941 | 7.4006 | 7.4071 | 7.4136 | 7.4201 | 7.4267 | 7.4332 | 7.4397 |
| .71    | 7.4463 | 7.4528 | 7.4593 | 7.4659 | 7.4724 | 7.4789 | 7.4855 | 7.4920 | 7.4986 | 7.5051 |
| .72    | 7.5117 | 7.5182 | 7.5248 | 7.5313 | 7.5379 | 7.5445 | 7.5510 | 7.5576 | 7.5641 | 7.5707 |
| .73    | 7.5773 | 7.5839 | 7.5904 | 7.5970 | 7.6036 | 7.6102 | 7.6167 | 7.6233 | 7.6299 | 7.6365 |
| .74    | 7.6431 | 7.6497 | 7.6563 | 7.6628 | 7.6694 | 7.6760 | 7.6826 | 7.6892 | 7.6958 | 7.7024 |
| .75    | 7.7091 | 7.7157 | 7.7223 | 7.7289 | 7.7355 | 7.7421 | 7.7487 | 7.7554 | 7.7620 | 7.7686 |
| .76    | 7.7752 | 7.7819 | 7.7885 | 7.7951 | 7.8018 | 7.8084 | 7.8150 | 7.8217 | 7.8283 | 7.8349 |
| .77    | 7.8416 | 7.8482 | 7.8549 | 7.8615 | 7.8682 | 7.8748 | 7.8815 | 7.8882 | 7.8948 | 7.9015 |
| .78    | 7.9081 | 7.9148 | 7.9215 | 7.9281 | 7.9348 | 7.9415 | 7.9482 | 7.9548 | 7.9615 | 7.9682 |
| .79    | 7.9749 | 7.9816 | 7.9882 | 7.9949 | 8.0016 | 8.0083 | 8.0150 | 8.0217 | 8.0284 | 8.0351 |
| 1.80   | 8.0418 | 8.0485 | 8.0552 | 8.0619 | 8.0686 | 8.0753 | 8.0820 | 8.0888 | 8.0955 | 8.1022 |
| .81    | 8.1089 | 8.1156 | 8.1223 | 8.1291 | 8.1358 | 8.1425 | 8.1493 | 8.1560 | 8.1627 | 8.1695 |
| .82    | 8.1762 | 8.1829 | 8.1897 | 8.1964 | 8.2032 | 8.2099 | 8.2167 | 8.2234 | 8.2302 | 8.2369 |
| .83    | 8.2437 | 8.2504 | 8.2572 | 8.2640 | 8.2707 | 8.2775 | 8.2842 | 8.2910 | 8.2978 | 8.3046 |
| .84    | 8.3113 | 8.3181 | 8.3249 | 8.3317 | 8.3385 | 8.3452 | 8.3520 | 8.3588 | 8.3656 | 8.3724 |
| .85    | 8.3792 | 8.3860 | 8.3928 | 8.3996 | 8.4064 | 8.4132 | 8.4200 | 8.4268 | 8.4336 | 8.4404 |
| .86    | 8.4472 | 8.4540 | 8.4608 | 8.4677 | 8.4745 | 8.4813 | 8.4881 | 8.4949 | 8.5018 | 8.5086 |
| .87    | 8.5154 | 8.5223 | 8.5291 | 8.5359 | 8.5428 | 8.5496 | 8.5564 | 8.5633 | 8.5701 | 8.5770 |
| .88    | 8.5838 | 8.5907 | 8.5975 | 8.6044 | 8.6112 | 8.6181 | 8.6250 | 8.6318 | 8.6387 | 8.6455 |
| .89    | 8.6524 | 8.6593 | 8.6661 | 8.6730 | 8.6799 | 8.6868 | 8.6936 | 8.7005 | 8.7074 | 8.7143 |
| 1.90   | 8.7212 | 8.7281 | 8.7349 | 8.7418 | 8.7487 | 8.7556 | 8.7625 | 8.7694 | 8.7763 | 8.7832 |
| .91    | 8.7901 | 8.7970 | 8.8039 | 8.8108 | 8.8177 | 8.8246 | 8.8315 | 8.8385 | 8.8454 | 8.8523 |
| .92    | 8.8592 | 8.8662 | 8.8731 | 8.8800 | 8.8869 | 8.8939 | 8.9008 | 8.9077 | 8.9147 | 8.9216 |
| .93    | 8.9285 | 8.9355 | 8.9424 | 8.9494 | 8.9563 | 8.9633 | 8.9702 | 8.9772 | 8.9841 | 8.9911 |
| .94    | 8.9980 | 9.0050 | 9.0119 | 9.0189 | 9.0259 | 9.0328 | 9.0398 | 9.0468 | 9.0537 | 9.0607 |
| .95    | 9.0677 | 9.0747 | 9.0816 | 9.0886 | 9.0956 | 9.1026 | 9.1096 | 9.1165 | 9.1235 | 9.1305 |
| .96    | 9.1375 | 9.1445 | 9.1515 | 9.1585 | 9.1655 | 9.1725 | 9.1795 | 9.1865 | 9.1935 | 9.2005 |
| .97    | 9.2075 | 9.2145 | 9.2216 | 9.2286 | 9.2356 | 9.2426 | 9.2496 | 9.2567 | 9.2637 | 9.2707 |
| .98    | 9.2777 | 9.2848 | 9.2918 | 9.2988 | 9.3059 | 9.3129 | 9.3199 | 9.3270 | 9.3340 | 9.3411 |
| .99    | 9.3481 | 9.3552 | 9.3622 | 9.3693 | 9.3763 | 9.3834 | 9.3904 | 9.3975 | 9.4045 | 9.4116 |



DISCHARGE, IN CUBIC FEET PER SECOND, OF A WEIR ONE FOOT LONG, WITH  
OUT CONTRACTION AT THE ENDS; FOR DEPTHS FROM 2.000 TO 2.400 FEET.

| Depth | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 2.00  | 9.4187 | 9.4257 | 9.4328 | 9.4399 | 9.4469 | 9.4540 | 9.4611 | 9.4682 | 9.4752 | 9.4823 |
| .01   | 9.4894 | 9.4965 | 9.5036 | 9.5106 | 9.5177 | 9.5248 | 9.5319 | 9.5390 | 9.5461 | 9.5532 |
| .02   | 9.5603 | 9.5674 | 9.5745 | 9.5816 | 9.5887 | 9.5958 | 9.6029 | 9.6100 | 9.6171 | 9.6243 |
| .03   | 9.6314 | 9.6385 | 9.6456 | 9.6527 | 9.6599 | 9.6670 | 9.6741 | 9.6812 | 9.6884 | 9.6955 |
| .04   | 9.7026 | 9.7098 | 9.7169 | 9.7240 | 9.7312 | 9.7383 | 9.7455 | 9.7526 | 9.7598 | 9.7669 |
| .05   | 9.7741 | 9.7812 | 9.7884 | 9.7955 | 9.8027 | 9.8098 | 9.8170 | 9.8242 | 9.8313 | 9.8385 |
| .06   | 9.8457 | 9.8528 | 9.8600 | 9.8672 | 9.8744 | 9.8815 | 9.8887 | 9.8959 | 9.9031 | 9.9103 |
| .07   | 9.9174 | 9.9246 | 9.9318 | 9.9390 | 9.9462 | 9.9534 | 9.9606 | 9.9678 | 9.9750 | 9.9822 |
| .08   | 9.9894 | 9.9966 | 10.004 | 10.011 | 10.018 | 10.025 | 10.033 | 10.040 | 10.047 | 10.054 |
| .09   | 10.062 | 10.069 | 10.076 | 10.083 | 10.090 | 10.098 | 10.105 | 10.112 | 10.119 | 10.127 |
| 2.10  | 10.134 | 10.141 | 10.148 | 10.156 | 10.163 | 10.170 | 10.177 | 10.185 | 10.192 | 10.199 |
| .11   | 10.206 | 10.214 | 10.221 | 10.228 | 10.235 | 10.243 | 10.250 | 10.257 | 10.264 | 10.272 |
| .12   | 10.279 | 10.286 | 10.293 | 10.301 | 10.308 | 10.315 | 10.323 | 10.330 | 10.337 | 10.344 |
| .13   | 10.352 | 10.359 | 10.366 | 10.374 | 10.381 | 10.388 | 10.396 | 10.403 | 10.410 | 10.417 |
| .14   | 10.425 | 10.432 | 10.439 | 10.447 | 10.454 | 10.461 | 10.469 | 10.476 | 10.483 | 10.491 |
| .15   | 10.498 | 10.505 | 10.513 | 10.520 | 10.527 | 10.535 | 10.542 | 10.549 | 10.557 | 10.564 |
| .16   | 10.571 | 10.579 | 10.586 | 10.593 | 10.601 | 10.608 | 10.615 | 10.623 | 10.630 | 10.637 |
| .17   | 10.645 | 10.652 | 10.659 | 10.667 | 10.674 | 10.682 | 10.689 | 10.696 | 10.704 | 10.711 |
| .18   | 10.718 | 10.726 | 10.733 | 10.741 | 10.748 | 10.755 | 10.763 | 10.770 | 10.777 | 10.785 |
| .19   | 10.792 | 10.800 | 10.807 | 10.814 | 10.822 | 10.829 | 10.837 | 10.844 | 10.851 | 10.859 |
| 2.20  | 10.866 | 10.874 | 10.881 | 10.888 | 10.896 | 10.903 | 10.911 | 10.918 | 10.926 | 10.933 |
| .21   | 10.940 | 10.948 | 10.955 | 10.963 | 10.970 | 10.978 | 10.985 | 10.992 | 11.000 | 11.007 |
| .22   | 11.015 | 11.022 | 11.030 | 11.037 | 11.045 | 11.052 | 11.059 | 11.067 | 11.074 | 11.082 |
| .23   | 11.089 | 11.097 | 11.104 | 11.112 | 11.119 | 11.127 | 11.134 | 11.141 | 11.149 | 11.156 |
| .24   | 11.164 | 11.171 | 11.179 | 11.186 | 11.194 | 11.201 | 11.209 | 11.216 | 11.224 | 11.231 |
| .25   | 11.239 | 11.246 | 11.254 | 11.261 | 11.269 | 11.276 | 11.284 | 11.291 | 11.299 | 11.306 |
| .26   | 11.314 | 11.321 | 11.329 | 11.336 | 11.344 | 11.351 | 11.359 | 11.366 | 11.374 | 11.381 |
| .27   | 11.389 | 11.396 | 11.404 | 11.412 | 11.419 | 11.427 | 11.434 | 11.442 | 11.449 | 11.457 |
| .28   | 11.464 | 11.472 | 11.479 | 11.487 | 11.494 | 11.502 | 11.510 | 11.517 | 11.525 | 11.532 |
| .29   | 11.540 | 11.547 | 11.555 | 11.562 | 11.570 | 11.578 | 11.585 | 11.593 | 11.600 | 11.608 |
| 2.30  | 11.615 | 11.623 | 11.631 | 11.638 | 11.646 | 11.653 | 11.661 | 11.669 | 11.676 | 11.684 |
| .31   | 11.691 | 11.699 | 11.706 | 11.714 | 11.722 | 11.729 | 11.737 | 11.744 | 11.752 | 11.760 |
| .32   | 11.767 | 11.775 | 11.783 | 11.790 | 11.798 | 11.805 | 11.813 | 11.821 | 11.828 | 11.836 |
| .33   | 11.843 | 11.851 | 11.859 | 11.866 | 11.874 | 11.882 | 11.889 | 11.897 | 11.904 | 11.912 |
| .34   | 11.920 | 11.927 | 11.935 | 11.943 | 11.950 | 11.958 | 11.966 | 11.973 | 11.981 | 11.989 |
| .35   | 11.996 | 12.004 | 12.012 | 12.019 | 12.027 | 12.035 | 12.042 | 12.050 | 12.058 | 12.065 |
| .36   | 12.073 | 12.081 | 12.088 | 12.096 | 12.104 | 12.111 | 12.119 | 12.127 | 12.134 | 12.142 |
| .37   | 12.150 | 12.157 | 12.165 | 12.173 | 12.181 | 12.188 | 12.196 | 12.204 | 12.211 | 12.219 |
| .38   | 12.227 | 12.234 | 12.242 | 12.250 | 12.258 | 12.265 | 12.273 | 12.281 | 12.288 | 12.296 |
| .39   | 12.304 | 12.312 | 12.319 | 12.327 | 12.335 | 12.342 | 12.350 | 12.358 | 12.366 | 12.373 |
| 2.40  | 12.381 | 12.389 | 12.397 | 12.404 | 12.412 | 12.420 | 12.428 | 12.435 | 12.443 | 12.451 |
| .41   | 12.459 | 12.466 | 12.474 | 12.482 | 12.490 | 12.497 | 12.505 | 12.513 | 12.521 | 12.528 |
| .42   | 12.536 | 12.544 | 12.552 | 12.560 | 12.567 | 12.575 | 12.583 | 12.591 | 12.598 | 12.606 |
| .43   | 12.614 | 12.622 | 12.630 | 12.637 | 12.645 | 12.653 | 12.661 | 12.669 | 12.676 | 12.684 |
| .44   | 12.692 | 12.700 | 12.708 | 12.715 | 12.723 | 12.731 | 12.739 | 12.747 | 12.754 | 12.762 |
| .45   | 12.770 | 12.778 | 12.786 | 12.794 | 12.801 | 12.809 | 12.817 | 12.825 | 12.833 | 12.840 |
| .46   | 12.848 | 12.856 | 12.864 | 12.872 | 12.880 | 12.888 | 12.895 | 12.903 | 12.911 | 12.919 |
| .47   | 12.927 | 12.935 | 12.942 | 12.950 | 12.958 | 12.966 | 12.974 | 12.982 | 12.990 | 12.997 |
| .48   | 13.005 | 13.013 | 13.021 | 13.029 | 13.037 | 13.045 | 13.053 | 13.060 | 13.068 | 13.076 |
| .49   | 13.084 | 13.092 | 13.100 | 13.108 | 13.116 | 13.124 | 13.131 | 13.139 | 13.147 | 13.155 |

## DISCHARGE, IN CUBIC FEET PER SECOND, OF A WEIR ONE FOOT LONG, WITHOUT CONTRACTION AT THE ENDS, FOR DEPTHS FROM 2.500 TO 2.990 FEET.

| Depth. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 2.50   | 13.163 | 13.171 | 13.179 | 13.187 | 13.195 | 13.202 | 13.210 | 13.218 | 13.226 | 13.234 |
| .51    | 13.242 | 13.250 | 13.258 | 13.266 | 13.274 | 13.282 | 13.290 | 13.297 | 13.305 | 13.313 |
| .52    | 13.321 | 13.329 | 13.337 | 13.345 | 13.353 | 13.361 | 13.369 | 13.377 | 13.385 | 13.393 |
| .53    | 13.401 | 13.409 | 13.417 | 13.424 | 13.432 | 13.440 | 13.448 | 13.456 | 13.464 | 13.472 |
| .54    | 13.480 | 13.488 | 13.496 | 13.504 | 13.512 | 13.520 | 13.528 | 13.536 | 13.544 | 13.552 |
| .55    | 13.560 | 13.568 | 13.576 | 13.584 | 13.592 | 13.600 | 13.608 | 13.616 | 13.624 | 13.632 |
| .56    | 13.640 | 13.648 | 13.656 | 13.664 | 13.672 | 13.680 | 13.688 | 13.696 | 13.704 | 13.712 |
| .57    | 13.720 | 13.728 | 13.736 | 13.744 | 13.752 | 13.760 | 13.768 | 13.776 | 13.784 | 13.792 |
| .58    | 13.800 | 13.808 | 13.816 | 13.824 | 13.832 | 13.840 | 13.848 | 13.856 | 13.864 | 13.872 |
| .59    | 13.880 | 13.888 | 13.896 | 13.904 | 13.912 | 13.920 | 13.928 | 13.936 | 13.944 | 13.953 |
| 2.60   | 13.961 | 13.969 | 13.977 | 13.985 | 13.993 | 14.001 | 14.009 | 14.017 | 14.025 | 14.033 |
| .61    | 14.041 | 14.049 | 14.057 | 14.065 | 14.074 | 14.082 | 14.090 | 14.098 | 14.106 | 14.114 |
| .62    | 14.122 | 14.130 | 14.138 | 14.146 | 14.154 | 14.162 | 14.171 | 14.179 | 14.187 | 14.195 |
| .63    | 14.203 | 14.211 | 14.219 | 14.227 | 14.235 | 14.243 | 14.252 | 14.260 | 14.268 | 14.276 |
| .64    | 14.284 | 14.292 | 14.300 | 14.308 | 14.316 | 14.325 | 14.333 | 14.341 | 14.349 | 14.357 |
| .65    | 14.365 | 14.373 | 14.382 | 14.390 | 14.398 | 14.406 | 14.414 | 14.422 | 14.430 | 14.438 |
| .66    | 14.447 | 14.455 | 14.463 | 14.471 | 14.479 | 14.487 | 14.496 | 14.504 | 14.512 | 14.520 |
| .67    | 14.528 | 14.536 | 14.545 | 14.553 | 14.561 | 14.569 | 14.577 | 14.585 | 14.594 | 14.602 |
| .68    | 14.610 | 14.618 | 14.626 | 14.634 | 14.643 | 14.651 | 14.659 | 14.667 | 14.675 | 14.684 |
| .69    | 14.692 | 14.700 | 14.708 | 14.716 | 14.725 | 14.733 | 14.741 | 14.749 | 14.757 | 14.766 |
| 2.70   | 14.774 | 14.782 | 14.790 | 14.798 | 14.807 | 14.815 | 14.823 | 14.831 | 14.839 | 14.848 |
| .71    | 14.856 | 14.864 | 14.872 | 14.881 | 14.889 | 14.897 | 14.905 | 14.913 | 14.922 | 14.930 |
| .72    | 14.938 | 14.946 | 14.955 | 14.963 | 14.971 | 14.979 | 14.988 | 14.996 | 15.004 | 15.012 |
| .73    | 15.021 | 15.029 | 15.037 | 15.045 | 15.054 | 15.062 | 15.070 | 15.078 | 15.087 | 15.095 |
| .74    | 15.108 | 15.116 | 15.124 | 15.132 | 15.140 | 15.148 | 15.156 | 15.164 | 15.172 | 15.180 |
| .75    | 15.196 | 15.194 | 15.203 | 15.211 | 15.219 | 15.227 | 15.236 | 15.244 | 15.252 | 15.261 |
| .76    | 15.269 | 15.277 | 15.285 | 15.294 | 15.302 | 15.310 | 15.319 | 15.327 | 15.335 | 15.344 |
| .77    | 15.352 | 15.360 | 15.369 | 15.377 | 15.385 | 15.394 | 15.402 | 15.410 | 15.419 | 15.427 |
| .78    | 15.435 | 15.443 | 15.452 | 15.460 | 15.468 | 15.477 | 15.485 | 15.494 | 15.502 | 15.510 |
| .79    | 15.519 | 15.527 | 15.535 | 15.544 | 15.552 | 15.560 | 15.569 | 15.577 | 15.585 | 15.594 |
| 2.80   | 15.602 | 15.610 | 15.619 | 15.627 | 15.635 | 15.644 | 15.652 | 15.661 | 15.669 | 15.677 |
| .81    | 15.686 | 15.694 | 15.702 | 15.711 | 15.719 | 15.728 | 15.736 | 15.744 | 15.753 | 15.761 |
| .82    | 15.769 | 15.778 | 15.786 | 15.795 | 15.803 | 15.811 | 15.820 | 15.828 | 15.837 | 15.845 |
| .83    | 15.853 | 15.862 | 15.870 | 15.879 | 15.887 | 15.895 | 15.904 | 15.912 | 15.921 | 15.929 |
| .84    | 15.938 | 15.946 | 15.954 | 15.963 | 15.971 | 15.980 | 15.988 | 15.997 | 16.005 | 16.013 |
| .85    | 16.022 | 16.030 | 16.039 | 16.047 | 16.056 | 16.064 | 16.072 | 16.081 | 16.089 | 16.098 |
| .86    | 16.106 | 16.115 | 16.123 | 16.132 | 16.140 | 16.148 | 16.157 | 16.165 | 16.174 | 16.182 |
| .87    | 16.191 | 16.199 | 16.208 | 16.216 | 16.225 | 16.233 | 16.242 | 16.250 | 16.258 | 16.267 |
| .88    | 16.275 | 16.284 | 16.292 | 16.301 | 16.309 | 16.318 | 16.326 | 16.335 | 16.343 | 16.352 |
| .89    | 16.360 | 16.369 | 16.377 | 16.386 | 16.394 | 16.403 | 16.411 | 16.420 | 16.428 | 16.437 |
| 2.90   | 16.445 | 16.454 | 16.462 | 16.471 | 16.479 | 16.488 | 16.496 | 16.505 | 16.513 | 16.522 |
| .91    | 16.530 | 16.539 | 16.547 | 16.556 | 16.565 | 16.573 | 16.582 | 16.590 | 16.599 | 16.607 |
| .92    | 16.616 | 16.624 | 16.633 | 16.641 | 16.650 | 16.658 | 16.667 | 16.675 | 16.684 | 16.693 |
| .93    | 16.701 | 16.710 | 16.718 | 16.727 | 16.735 | 16.744 | 16.752 | 16.761 | 16.770 | 16.778 |
| .94    | 16.787 | 16.796 | 16.804 | 16.812 | 16.821 | 16.830 | 16.838 | 16.847 | 16.855 | 16.864 |
| .95    | 16.872 | 16.881 | 16.890 | 16.898 | 16.907 | 16.915 | 16.924 | 16.932 | 16.941 | 16.950 |
| .96    | 16.958 | 16.967 | 16.975 | 16.984 | 16.993 | 17.001 | 17.010 | 17.018 | 17.027 | 17.036 |
| .97    | 17.044 | 17.053 | 17.062 | 17.070 | 17.079 | 17.087 | 17.096 | 17.105 | 17.113 | 17.122 |
| .98    | 17.130 | 17.139 | 17.148 | 17.156 | 17.165 | 17.174 | 17.182 | 17.191 | 17.199 | 17.208 |
| .99    | 17.217 | 17.225 | 17.234 | 17.243 | 17.251 | 17.260 | 17.269 | 17.277 | 17.286 | 17.295 |

VELOCITIES, IN FEET PER SECOND, DUE TO HEADS FROM 0 TO  
4.99 FEET.

| Head. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0.0   | 0.000  | 0.802  | 1.184  | 1.889  | 1.604  | 1.798  | 1.965  | 2.122  | 2.268  | 2.406  |
| .1    | 2.536  | 2.660  | 2.778  | 2.892  | 3.001  | 3.106  | 3.208  | 3.307  | 3.403  | 3.496  |
| .2    | 3.587  | 3.675  | 3.762  | 3.846  | 3.929  | 4.010  | 4.090  | 4.167  | 4.244  | 4.319  |
| .3    | 4.393  | 4.463  | 4.537  | 4.607  | 4.677  | 4.745  | 4.812  | 4.878  | 4.944  | 5.009  |
| .4    | 5.072  | 5.135  | 5.198  | 5.259  | 5.3.0  | 5.380  | 5.440  | 5.498  | 5.557  | 5.614  |
| .5    | 5.671  | 5.728  | 5.783  | 5.838  | 5.894  | 5.948  | 6.002  | 6.055  | 6.108  | 6.160  |
| .6    | 6.212  | 6.264  | 6.315  | 6.366  | 6.416  | 6.466  | 6.516  | 6.565  | 6.614  | 6.662  |
| .7    | 6.710  | 6.7.8  | 6.805  | 6.852  | 6.899  | 6.946  | 6.992  | 7.038  | 7.083  | 7.129  |
| .8    | 7.173  | 7.218  | 7.263  | 7.307  | 7.351  | 7.394  | 7.438  | 7.481  | 7.524  | 7.566  |
| .9    | 7.609  | 7.651  | 7.693  | 7.734  | 7.776  | 7.817  | 7.858  | 7.899  | 7.940  | 7.980  |
| 1.0   | 8.020  | 8.060  | 8.100  | 8.140  | 8.179  | 8.218  | 8.257  | 8.296  | 8.335  | 8.373  |
| .1    | 8.412  | 8.450  | 8.488  | 8.526  | 8.563  | 8.601  | 8.638  | 8.675  | 8.712  | 8.749  |
| .2    | 8.786  | 8.822  | 8.859  | 8.895  | 8.931  | 8.967  | 9.003  | 9.038  | 9.074  | 9.109  |
| .3    | 9.144  | 9.180  | 9.214  | 9.249  | 9.284  | 9.319  | 9.353  | 9.387  | 9.422  | 9.455  |
| .4    | 9.490  | 9.523  | 9.557  | 9.591  | 9.624  | 9.658  | 9.691  | 9.724  | 9.757  | 9.790  |
| .5    | 9.823  | 9.855  | 9.888  | 9.920  | 9.953  | 9.985  | 10.017 | 10.049 | 10.081 | 10.113 |
| .6    | 10.145 | 10.176 | 10.208 | 10.240 | 10.271 | 10.302 | 10.333 | 10.364 | 10.395 | 10.426 |
| .7    | 10.457 | 10.488 | 10.518 | 10.549 | 10.579 | 10.610 | 10.640 | 10.670 | 10.700 | 10.730 |
| .8    | 10.760 | 10.790 | 10.820 | 10.850 | 10.879 | 10.909 | 10.938 | 10.967 | 10.997 | 11.026 |
| .9    | 11.055 | 11.084 | 11.113 | 11.142 | 11.171 | 11.200 | 11.228 | 11.257 | 11.285 | 11.314 |
| 2.0   | 11.342 | 11.371 | 11.399 | 11.427 | 11.455 | 11.483 | 11.511 | 11.539 | 11.567 | 11.595 |
| .1    | 11.622 | 11.650 | 11.678 | 11.705 | 11.733 | 11.760 | 11.787 | 11.814 | 11.842 | 11.869 |
| .2    | 11.896 | 11.923 | 11.950 | 11.977 | 12.004 | 12.030 | 12.057 | 12.084 | 12.110 | 12.137 |
| .3    | 12.163 | 12.190 | 12.216 | 12.242 | 12.269 | 12.295 | 12.321 | 12.347 | 12.373 | 12.399 |
| .4    | 12.425 | 12.451 | 12.477 | 12.502 | 12.528 | 12.554 | 12.579 | 12.605 | 12.630 | 12.656 |
| .5    | 12.681 | 12.706 | 12.732 | 12.757 | 12.782 | 12.807 | 12.832 | 12.857 | 12.882 | 12.907 |
| .6    | 12.932 | 12.957 | 12.982 | 13.007 | 13.031 | 13.056 | 13.081 | 13.105 | 13.130 | 13.154 |
| .7    | 13.179 | 13.203 | 13.227 | 13.252 | 13.276 | 13.300 | 13.324 | 13.348 | 13.372 | 13.396 |
| .8    | 13.420 | 13.444 | 13.468 | 13.492 | 13.516 | 13.540 | 13.563 | 13.587 | 13.611 | 13.634 |
| .9    | 13.658 | 13.681 | 13.705 | 13.728 | 13.752 | 13.775 | 13.798 | 13.822 | 13.845 | 13.868 |
| 3.0   | 13.891 | 13.915 | 13.938 | 13.961 | 13.984 | 14.007 | 14.030 | 14.053 | 14.075 | 14.098 |
| .1    | 14.121 | 14.144 | 14.166 | 14.189 | 14.212 | 14.234 | 14.257 | 14.280 | 14.302 | 14.325 |
| .2    | 14.347 | 14.369 | 14.392 | 14.414 | 14.436 | 14.459 | 14.481 | 14.503 | 14.525 | 14.547 |
| .3    | 14.569 | 14.591 | 14.614 | 14.635 | 14.657 | 14.679 | 14.701 | 14.723 | 14.745 | 14.767 |
| .4    | 14.789 | 14.810 | 14.832 | 14.854 | 14.875 | 14.897 | 14.918 | 14.940 | 14.961 | 14.983 |
| .5    | 15.004 | 15.026 | 15.047 | 15.069 | 15.090 | 15.111 | 15.132 | 15.154 | 15.175 | 15.196 |
| .6    | 15.217 | 15.238 | 15.259 | 15.281 | 15.302 | 15.322 | 15.344 | 15.364 | 15.385 | 15.406 |
| .7    | 15.427 | 15.448 | 15.469 | 15.490 | 15.510 | 15.5.1 | 15.552 | 15.572 | 15.593 | 15.614 |
| .8    | 15.634 | 15.655 | 15.675 | 15.696 | 15.716 | 15.737 | 15.757 | 15.778 | 15.798 | 15.818 |
| .9    | 15.839 | 15.859 | 15.876 | 15.899 | 15.920 | 15.940 | 15.960 | 15.980 | 16.000 | 16.020 |
| 4.0   | 16.049 | 16.060 | 16.080 | 16.100 | 16.12  | 16.110 | 16.160 | 16.180 | 16.200 | 16.220 |
| .1    | 16.240 | 16.259 | 16.279 | 16.299 | 16.319 | 16.338 | 16.358 | 16.378 | 16.397 | 16.417 |
| .2    | 16.437 | 16.456 | 16.476 | 16.495 | 16.515 | 16.534 | 16.554 | 16.573 | 16.592 | 16.612 |
| .3    | 16.631 | 16.650 | 16.670 | 16.689 | 16.708 | 16.727 | 16.747 | 16.766 | 16.785 | 16.804 |
| .4    | 16.828 | 16.842 | 16.862 | 16.881 | 16.900 | 16.919 | 16.938 | 16.957 | 16.976 | 16.994 |
| .5    | 17.013 | 17.032 | 17.051 | 17.070 | 17.089 | 17.108 | 17.126 | 17.145 | 17.164 | 17.183 |
| .6    | 17.201 | 17.2.0 | 17.2.9 | 17.2.7 | 17.276 | 17.295 | 17.313 | 17.332 | 17.350 | 17.369 |
| .7    | 17.387 | 17.406 | 17.424 | 17.443 | 17.461 | 17.480 | 17.498 | 17.516 | 17.535 | 17.553 |
| .8    | 17.571 | 17.590 | 17.608 | 17.626 | 17.644 | 17.662 | 17.681 | 17.699 | 17.717 | 17.735 |
| .9    | 17.753 | 17.772 | 17.790 | 17.808 | 17.826 | 17.844 | 17.862 | 17.880 | 17.898 | 17.916 |

VELOCITIES, IN FEET PER SECOND, DUE TO HEADS FROM 5 TO  
9.99 FEET.

| Head. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 5.0   | 17.934 | 17.952 | 17.970 | 17.987 | 18.005 | 18.023 | 18.041 | 18.059 | 18.077 | 18.094 |
| .1    | 18.112 | 18.130 | 18.148 | 18.165 | 18.183 | 18.201 | 18.218 | 18.236 | 18.254 | 18.271 |
| .2    | 18.289 | 18.306 | 18.324 | 18.342 | 18.359 | 18.377 | 18.394 | 18.412 | 18.429 | 18.446 |
| .3    | 18.464 | 18.481 | 18.499 | 18.516 | 18.533 | 18.551 | 18.568 | 18.585 | 18.603 | 18.620 |
| .4    | 18.637 | 18.655 | 18.672 | 18.689 | 18.706 | 18.723 | 18.741 | 18.758 | 18.775 | 18.792 |
| .5    | 18.809 | 18.826 | 18.843 | 18.860 | 18.877 | 18.894 | 18.911 | 18.928 | 18.945 | 18.962 |
| .6    | 18.979 | 18.996 | 19.013 | 19.030 | 19.047 | 19.064 | 19.081 | 19.098 | 19.114 | 19.131 |
| .7    | 19.148 | 19.165 | 19.182 | 19.198 | 19.215 | 19.232 | 19.248 | 19.265 | 19.282 | 19.299 |
| .8    | 19.315 | 19.332 | 19.348 | 19.365 | 19.382 | 19.398 | 19.415 | 19.431 | 19.448 | 19.464 |
| .9    | 19.481 | 19.497 | 19.514 | 19.530 | 19.547 | 19.563 | 19.580 | 19.596 | 19.613 | 19.629 |
| 6.0   | 19.645 | 19.662 | 19.678 | 19.694 | 19.711 | 19.727 | 19.743 | 19.760 | 19.776 | 19.792 |
| .1    | 19.808 | 19.825 | 19.841 | 19.857 | 9.873  | 19.889 | 19.906 | 19.922 | 19.938 | 19.954 |
| .2    | 19.970 | 19.986 | 20.002 | 20.018 | 20.034 | 20.050 | 20.067 | 20.083 | 20.099 | 20.115 |
| .3    | 20.131 | 20.147 | 20.162 | 20.178 | 20.194 | 20.210 | 20.226 | 20.242 | 20.258 | 20.274 |
| .4    | 20.29  | 20.306 | 20.321 | 20.337 | 20.353 | 20.369 | 20.385 | 20.400 | 20.416 | 20.432 |
| .5    | 20.448 | 20.463 | 20.479 | 20.495 | 20.510 | 20.526 | 20.542 | 20.557 | 20.573 | 20.589 |
| .6    | 20.604 | 20.620 | 20.635 | 20.651 | 20.667 | 20.682 | 20.698 | 20.713 | 20.729 | 20.744 |
| .7    | 20.760 | 20.775 | 20.791 | 20.806 | 20.822 | 20.837 | 20.853 | 20.868 | 20.883 | 20.899 |
| .8    | 20.914 | 20.929 | 20.945 | 20.960 | 20.976 | 20.991 | 21.006 | 21.021 | 21.037 | 21.052 |
| .9    | 21.067 | 21.083 | 21.098 | 21.113 | 21.128 | 21.144 | 21.159 | 21.174 | 21.189 | 21.204 |
| 7.0   | 21.219 | 21.235 | 21.250 | 21.265 | 21.280 | 21.295 | 21.310 | 21.325 | 21.340 | 21.355 |
| .1    | 21.370 | 21.386 | 21.401 | 21.416 | 21.431 | 21.446 | 21.461 | 21.476 | 21.491 | 21.506 |
| .2    | 21.520 | 21.535 | 21.550 | 21.565 | 21.580 | 21.595 | 21.610 | 21.625 | 21.640 | 21.655 |
| .3    | 21.669 | 21.684 | 21.699 | 21.714 | 21.729 | 21.743 | 21.758 | 21.773 | 21.788 | 21.803 |
| .4    | 21.817 | 21.832 | 2.847  | 21.861 | 21.876 | 21.891 | 21.906 | 21.920 | 21.935 | 21.950 |
| .5    | 21.964 | 21.979 | 21.993 | 22.008 | 22.023 | 22.037 | 22.052 | 22.066 | 22.081 | 22.096 |
| .6    | 22.110 | 22.125 | 22.139 | 22.154 | 22.168 | 22.183 | 22.197 | 22.212 | 22.226 | 22.241 |
| .7    | 22.255 | 22.270 | 22.284 | 22.298 | 22.313 | 22.327 | 22.342 | 22.356 | 22.370 | 22.385 |
| .8    | 22.399 | 22.414 | 22.428 | 22.442 | 22.457 | 22.471 | 22.485 | 22.499 | 22.514 | 22.528 |
| .9    | 22.542 | 22.557 | 22.571 | 22.585 | 22.599 | 22.614 | 22.628 | 22.642 | 22.656 | 22.670 |
| 8.0   | 22.685 | 22.699 | 22.713 | 22.727 | 22.741 | 22.755 | 22.769 | 22.784 | 22.798 | 22.812 |
| .1    | 22.826 | 22.840 | 22.854 | 22.868 | 22.882 | 22.896 | 22.910 | 22.924 | 22.938 | 22.952 |
| .2    | 22.966 | 22.980 | 22.994 | 23.008 | 23.022 | 23.036 | 23.050 | 23.064 | 23.078 | 23.092 |
| .3    | 23.106 | 23.120 | 23.134 | 23.148 | 23.162 | 23.175 | 23.189 | 23.203 | 23.217 | 23.231 |
| .4    | 23.245 | 23.259 | 23.272 | 23.286 | 23.300 | 23.314 | 23.328 | 23.341 | 23.355 | 23.369 |
| .5    | 23.383 | 23.396 | 23.410 | 23.424 | 23.438 | 23.451 | 23.465 | 23.479 | 23.492 | 23.506 |
| .6    | 23.520 | 23.534 | 23.547 | 23.561 | 23.574 | 23.588 | 23.602 | 23.615 | 23.629 | 23.643 |
| .7    | 23.656 | 23.670 | 23.683 | 23.697 | 23.711 | 23.724 | 23.738 | 23.751 | 23.765 | 23.778 |
| .8    | 23.792 | 23.805 | 23.819 | 23.832 | 23.846 | 23.859 | 23.873 | 23.886 | 23.900 | 23.913 |
| .9    | 23.927 | 23.940 | 23.953 | 23.967 | 23.980 | 23.994 | 24.007 | 24.020 | 24.034 | 24.047 |
| 9.0   | 24.061 | 24.074 | 24.087 | 24.101 | 24.114 | 24.127 | 24.141 | 24.154 | 24.167 | 24.181 |
| .1    | 24.194 | 24.207 | 24.220 | 24.234 | 24.247 | 24.260 | 24.274 | 24.287 | 24.300 | 24.313 |
| .2    | 24.326 | 24.340 | 24.353 | 24.366 | 24.379 | 24.392 | 24.406 | 24.419 | 24.432 | 24.445 |
| .3    | 24.458 | 24.471 | 24.485 | 24.498 | 24.511 | 24.524 | 24.537 | 24.550 | 24.563 | 24.576 |
| .4    | 24.589 | 24.603 | 24.616 | 24.629 | 24.642 | 24.655 | 24.668 | 24.681 | 24.694 | 24.707 |
| .5    | 24.720 | 24.733 | 24.746 | 24.759 | 24.772 | 24.785 | 24.798 | 24.811 | 24.824 | 24.837 |
| .6    | 24.850 | 24.863 | 24.876 | 24.888 | 24.901 | 24.914 | 24.927 | 24.940 | 24.953 | 24.966 |
| .7    | 24.979 | 24.992 | 25.005 | 25.017 | 25.030 | 25.043 | 25.056 | 25.069 | 25.082 | 25.094 |
| .8    | 25.107 | 25.120 | 25.133 | 25.146 | 25.158 | 25.171 | 25.184 | 25.197 | 25.209 | 25.222 |
| .9    | 25.235 | 25.248 | 25.260 | 25.273 | 25.286 | 25.299 | 25.311 | 25.324 | 25.337 | 25.349 |

VELOCITIES, IN FEET PER SECOND, DUE TO HEADS FROM 10 TO  
14.99 FEET.

| Head. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 10.0  | 25.362 | 25.375 | 25.38  | 25.400 | 25.413 | 25.425 | 25.438 | 25.451 | 25.463 | 25.476 |
| .1    | 25.489 | 25.501 | 25.514 | 25.526 | 25.539 | 25.552 | 25.564 | 25.577 | 25.589 | 25.602 |
| .2    | 25.614 | 25.627 | 25.640 | 25.652 | 25.665 | 25.677 | 25.690 | 25.702 | 25.715 | 25.728 |
| .3    | 25.740 | 25.752 | 25.765 | 25.777 | 25.790 | 25.802 | 25.815 | 25.827 | 25.839 | 25.852 |
| .4    | 25.864 | 25.877 | 25.889 | 25.902 | 25.914 | 25.926 | 25.939 | 25.951 | 25.964 | 25.976 |
| .5    | 25.988 | 26.001 | 26.013 | 26.026 | 26.038 | 26.050 | 26.063 | 26.075 | 26.087 | 26.099 |
| .6    | 26.112 | 26.124 | 26.136 | 26.149 | 26.161 | 26.173 | 26.186 | 26.198 | 26.210 | 26.222 |
| .7    | 26.235 | 26.247 | 26.259 | 26.272 | 26.284 | 26.296 | 26.308 | 26.320 | 26.333 | 26.345 |
| .8    | 26.357 | 26.369 | 26.381 | 26.394 | 26.406 | 26.418 | 26.430 | 26.442 | 26.454 | 26.467 |
| .9    | 26.479 | 26.491 | 26.503 | 26.515 | 26.527 | 26.540 | 26.552 | 26.564 | 26.576 | 26.588 |
| 11.0  | 26.600 | 26.612 | 26.624 | 26.636 | 26.648 | 26.660 | 26.672 | 26.684 | 26.697 | 26.709 |
| .1    | 26.721 | 26.733 | 26.745 | 26.757 | 26.769 | 26.781 | 26.793 | 26.805 | 26.817 | 26.829 |
| .2    | 26.841 | 26.853 | 26.865 | 26.877 | 26.889 | 26.901 | 26.913 | 26.924 | 26.936 | 26.948 |
| .3    | 26.960 | 26.972 | 26.984 | 26.996 | 27.008 | 27.020 | 27.032 | 27.044 | 27.056 | 27.067 |
| .4    | 27.079 | 27.091 | 27.103 | 27.115 | 27.127 | 27.139 | 27.150 | 27.162 | 27.174 | 27.186 |
| .5    | 27.198 | 27.210 | 27.222 | 27.233 | 27.245 | 27.257 | 27.269 | 27.280 | 27.292 | 27.304 |
| .6    | 27.316 | 27.328 | 27.339 | 27.351 | 27.363 | 27.375 | 27.386 | 27.398 | 27.410 | 27.422 |
| .7    | 27.433 | 27.445 | 27.457 | 27.468 | 27.480 | 27.492 | 27.504 | 27.515 | 27.527 | 27.539 |
| .8    | 27.550 | 27.562 | 27.574 | 27.585 | 27.597 | 27.609 | 27.620 | 27.632 | 27.644 | 27.655 |
| .9    | 27.667 | 27.678 | 27.690 | 27.702 | 27.713 | 27.725 | 27.736 | 27.748 | 27.760 | 27.771 |
| 12.0  | 27.783 | 27.794 | 27.806 | 27.817 | 27.829 | 27.841 | 27.852 | 27.864 | 27.875 | 27.887 |
| .1    | 27.898 | 27.910 | 27.921 | 27.933 | 27.944 | 27.956 | 27.967 | 27.979 | 27.990 | 28.002 |
| .2    | 28.013 | 28.025 | 28.036 | 28.048 | 28.059 | 28.071 | 28.082 | 28.094 | 28.105 | 28.117 |
| .3    | 28.128 | 28.139 | 28.151 | 28.162 | 28.174 | 28.185 | 28.196 | 28.208 | 28.219 | 28.231 |
| .4    | 28.242 | 28.253 | 28.265 | 28.276 | 28.288 | 28.299 | 28.310 | 28.322 | 28.333 | 28.344 |
| .5    | 28.356 | 28.367 | 28.378 | 28.390 | 28.401 | 28.412 | 28.424 | 28.435 | 28.446 | 28.458 |
| .6    | 28.469 | 28.480 | 28.491 | 28.503 | 28.514 | 28.525 | 28.537 | 28.548 | 28.559 | 28.570 |
| .7    | 28.582 | 28.593 | 28.604 | 28.615 | 28.627 | 28.638 | 28.649 | 28.660 | 28.672 | 28.683 |
| .8    | 28.694 | 28.705 | 28.716 | 28.727 | 28.739 | 28.750 | 28.761 | 28.772 | 28.783 | 28.795 |
| .9    | 28.806 | 28.817 | 28.828 | 28.839 | 28.850 | 28.862 | 28.873 | 28.884 | 28.895 | 28.906 |
| 13.0  | 28.917 | 28.928 | 28.939 | 28.951 | 28.962 | 28.973 | 28.984 | 28.995 | 29.006 | 29.017 |
| .1    | 29.028 | 29.039 | 29.050 | 29.061 | 29.073 | 29.084 | 29.095 | 29.106 | 29.117 | 29.128 |
| .2    | 29.139 | 29.150 | 29.161 | 29.172 | 29.183 | 29.194 | 29.205 | 29.216 | 29.227 | 29.238 |
| .3    | 29.249 | 29.260 | 29.271 | 29.282 | 29.293 | 29.304 | 29.315 | 29.326 | 29.337 | 29.348 |
| .4    | 29.359 | 29.370 | 29.381 | 29.392 | 29.403 | 29.413 | 29.424 | 29.435 | 29.446 | 29.457 |
| .5    | 29.468 | 29.479 | 29.490 | 29.501 | 29.512 | 29.523 | 29.533 | 29.544 | 29.555 | 29.566 |
| .6    | 29.577 | 29.588 | 29.599 | 29.610 | 29.620 | 29.631 | 29.642 | 29.653 | 29.664 | 29.675 |
| .7    | 29.686 | 29.696 | 29.707 | 29.718 | 29.729 | 29.740 | 29.751 | 29.761 | 29.772 | 29.783 |
| .8    | 29.794 | 29.805 | 29.815 | 29.826 | 29.837 | 29.848 | 29.858 | 29.869 | 29.880 | 29.891 |
| .9    | 29.901 | 29.912 | 29.923 | 29.934 | 29.944 | 29.955 | 29.966 | 29.977 | 29.987 | 29.998 |
| 14.0  | 30.009 | 30.020 | 30.030 | 30.041 | 30.052 | 30.062 | 30.073 | 30.084 | 30.094 | 30.105 |
| .1    | 30.116 | 30.126 | 30.137 | 30.148 | 30.159 | 30.169 | 30.180 | 30.190 | 30.201 | 30.212 |
| .2    | 30.222 | 30.233 | 30.244 | 30.254 | 30.265 | 30.276 | 30.286 | 30.297 | 30.307 | 30.318 |
| .3    | 30.329 | 30.339 | 30.350 | 30.360 | 30.371 | 30.382 | 30.392 | 30.403 | 30.413 | 30.424 |
| .4    | 30.435 | 30.445 | 30.456 | 30.466 | 30.477 | 30.487 | 30.498 | 30.508 | 30.519 | 30.529 |
| .5    | 30.540 | 30.551 | 30.561 | 30.572 | 30.582 | 30.593 | 30.603 | 30.614 | 30.624 | 30.635 |
| .6    | 30.645 | 30.656 | 30.666 | 30.677 | 30.687 | 30.698 | 30.708 | 30.719 | 30.729 | 30.739 |
| .7    | 30.750 | 30.760 | 30.771 | 30.781 | 30.792 | 30.802 | 30.813 | 30.823 | 30.833 | 30.844 |
| .8    | 30.854 | 30.865 | 30.875 | 30.886 | 30.896 | 30.906 | 30.917 | 30.927 | 30.938 | 30.948 |
| .9    | 30.958 | 30.969 | 30.979 | 30.990 | 31.000 | 31.010 | 31.021 | 31.031 | 31.041 | 31.052 |



VELOCITIES, IN FEET PER SECOND, DUE TO HEADS FROM 15 TO  
19.99 FEET.

| Head. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 15.0  | 31.062 | 31.072 | 31.083 | 31.093 | 31.103 | 31.114 | 31.124 | 31.134 | 31.145 | 31.155 |
| .1    | 31.165 | 31.176 | 31.186 | 31.196 | 31.207 | 31.217 | 31.227 | 31.238 | 31.248 | 31.258 |
| .2    | 31.268 | 31.279 | 31.289 | 31.299 | 31.310 | 31.320 | 31.330 | 31.340 | 31.351 | 31.361 |
| .3    | 31.371 | 31.381 | 31.392 | 31.402 | 31.412 | 31.422 | 31.433 | 31.443 | 31.453 | 31.463 |
| .4    | 31.474 | 31.484 | 31.494 | 31.504 | 31.514 | 31.525 | 31.535 | 31.545 | 31.555 | 31.565 |
| .5    | 31.576 | 31.586 | 31.596 | 31.606 | 31.616 | 31.626 | 31.637 | 31.647 | 31.657 | 31.667 |
| .6    | 31.677 | 31.687 | 31.698 | 31.708 | 31.718 | 31.728 | 31.738 | 31.748 | 31.758 | 31.768 |
| .7    | 31.779 | 31.789 | 31.799 | 31.809 | 31.819 | 31.829 | 31.839 | 31.849 | 31.859 | 31.870 |
| .8    | 31.880 | 31.890 | 31.900 | 31.910 | 31.920 | 31.930 | 31.941 | 31.950 | 31.960 | 31.970 |
| .9    | 31.980 | 31.990 | 32.000 | 32.011 | 32.021 | 32.031 | 32.041 | 32.051 | 32.061 | 32.071 |
| 16.0  | 32.081 | 32.091 | 32.101 | 32.111 | 32.121 | 32.131 | 32.141 | 32.151 | 32.161 | 32.171 |
| .1    | 32.181 | 32.191 | 32.201 | 32.211 | 32.221 | 32.231 | 32.241 | 32.251 | 32.261 | 32.271 |
| .2    | 32.281 | 32.291 | 32.301 | 32.311 | 32.321 | 32.330 | 32.340 | 32.350 | 32.360 | 32.370 |
| .3    | 32.380 | 32.390 | 32.400 | 32.410 | 32.420 | 32.430 | 32.440 | 32.450 | 32.460 | 32.470 |
| .4    | 32.480 | 32.489 | 32.499 | 32.509 | 32.519 | 32.529 | 32.539 | 32.549 | 32.559 | 32.569 |
| .5    | 32.579 | 32.588 | 32.598 | 32.608 | 32.618 | 32.628 | 32.637 | 32.647 | 32.657 | 32.667 |
| .6    | 32.677 | 32.687 | 32.696 | 32.706 | 32.716 | 32.726 | 32.736 | 32.746 | 32.755 | 32.765 |
| .7    | 32.775 | 32.785 | 32.795 | 32.804 | 32.814 | 32.824 | 32.834 | 32.844 | 32.854 | 32.863 |
| .8    | 32.873 | 32.883 | 32.893 | 32.903 | 32.912 | 32.922 | 32.932 | 32.941 | 32.951 | 32.961 |
| .9    | 32.971 | 32.980 | 32.990 | 33.000 | 33.010 | 33.019 | 33.029 | 33.039 | 33.049 | 33.058 |
| 17.0  | 33.068 | 33.078 | 33.088 | 33.097 | 33.107 | 33.117 | 33.126 | 33.136 | 33.146 | 33.156 |
| .1    | 33.165 | 33.175 | 33.185 | 33.194 | 33.204 | 33.214 | 33.223 | 33.233 | 33.243 | 33.252 |
| .2    | 33.262 | 33.272 | 33.281 | 33.291 | 33.301 | 33.310 | 33.320 | 33.330 | 33.339 | 33.349 |
| .3    | 33.359 | 33.368 | 33.378 | 33.388 | 33.397 | 33.407 | 33.416 | 33.426 | 33.436 | 33.445 |
| .4    | 33.455 | 33.465 | 33.474 | 33.484 | 33.493 | 33.503 | 33.513 | 33.522 | 33.532 | 33.541 |
| .5    | 33.551 | 33.560 | 33.570 | 33.580 | 33.589 | 33.599 | 33.608 | 33.618 | 33.628 | 33.637 |
| .6    | 33.647 | 33.656 | 33.666 | 33.675 | 33.685 | 33.694 | 33.704 | 33.713 | 33.723 | 33.733 |
| .7    | 33.742 | 33.752 | 33.761 | 33.771 | 33.780 | 33.790 | 33.799 | 33.809 | 33.818 | 33.828 |
| .8    | 33.837 | 33.847 | 33.856 | 33.866 | 33.875 | 33.885 | 33.894 | 33.904 | 33.913 | 33.923 |
| .9    | 33.932 | 33.942 | 33.951 | 33.961 | 33.970 | 33.980 | 33.989 | 33.998 | 34.008 | 34.017 |
| 18.0  | 34.027 | 34.036 | 34.046 | 34.055 | 34.065 | 34.074 | 34.083 | 34.093 | 34.102 | 34.112 |
| .1    | 34.121 | 34.131 | 34.140 | 34.149 | 34.159 | 34.168 | 34.178 | 34.187 | 34.197 | 34.206 |
| .2    | 34.215 | 34.225 | 34.234 | 34.244 | 34.253 | 34.262 | 34.272 | 34.281 | 34.290 | 34.300 |
| .3    | 34.309 | 34.319 | 34.328 | 34.337 | 34.347 | 34.356 | 34.365 | 34.375 | 34.384 | 34.393 |
| .4    | 34.403 | 34.412 | 34.422 | 34.431 | 34.440 | 34.450 | 34.459 | 34.468 | 34.478 | 34.487 |
| .5    | 34.496 | 34.505 | 34.515 | 34.524 | 34.533 | 34.543 | 34.552 | 34.561 | 34.571 | 34.580 |
| .6    | 34.589 | 34.599 | 34.608 | 34.617 | 34.626 | 34.636 | 34.645 | 34.654 | 34.664 | 34.673 |
| .7    | 34.682 | 34.691 | 34.701 | 34.710 | 34.719 | 34.728 | 34.738 | 34.747 | 34.756 | 34.766 |
| .8    | 34.775 | 34.784 | 34.793 | 34.802 | 34.812 | 34.821 | 34.830 | 34.839 | 34.849 | 34.858 |
| .9    | 34.867 | 34.876 | 34.886 | 34.895 | 34.904 | 34.913 | 34.922 | 34.932 | 34.941 | 34.950 |
| 19.0  | 34.959 | 34.968 | 34.978 | 34.987 | 34.996 | 35.005 | 35.014 | 35.024 | 35.033 | 35.042 |
| .1    | 35.051 | 35.060 | 35.069 | 35.079 | 35.088 | 35.097 | 35.106 | 35.115 | 35.124 | 35.134 |
| .2    | 35.143 | 35.152 | 35.161 | 35.170 | 35.179 | 35.188 | 35.198 | 35.207 | 35.216 | 35.225 |
| .3    | 35.234 | 35.243 | 35.252 | 35.262 | 35.271 | 35.280 | 35.289 | 35.298 | 35.307 | 35.316 |
| .4    | 35.325 | 35.334 | 35.344 | 35.353 | 35.362 | 35.371 | 35.380 | 35.389 | 35.398 | 35.407 |
| .5    | 35.416 | 35.425 | 35.434 | 35.443 | 35.453 | 35.462 | 35.471 | 35.480 | 35.489 | 35.498 |
| .6    | 35.507 | 35.516 | 35.525 | 35.534 | 35.543 | 35.552 | 35.561 | 35.570 | 35.579 | 35.588 |
| .7    | 35.597 | 35.606 | 35.615 | 35.624 | 35.634 | 35.643 | 35.652 | 35.661 | 35.670 | 35.679 |
| .8    | 35.688 | 35.697 | 35.706 | 35.715 | 35.724 | 35.733 | 35.742 | 35.751 | 35.760 | 35.769 |
| .9    | 35.778 | 35.787 | 35.796 | 35.805 | 35.814 | 35.823 | 35.832 | 35.841 | 35.849 | 35.858 |

VELOCITIES, IN FEET PER SECOND, DUE TO HEADS FROM 20 TO  
24.99 FEET.

| Head. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 20.0  | 35.867 | 35.876 | 35.885 | 35.894 | 35.903 | 35.912 | 35.921 | 35.930 | 35.939 | 35.948 |
| .1    | 35.957 | 35.966 | 35.975 | 35.984 | 35.993 | 36.002 | 36.011 | 36.020 | 36.028 | 36.037 |
| .2    | 36.046 | 36.055 | 36.064 | 36.073 | 36.082 | 36.091 | 36.100 | 36.109 | 36.118 | 36.127 |
| .3    | 36.135 | 36.144 | 36.153 | 36.162 | 36.171 | 36.180 | 36.189 | 36.198 | 36.207 | 36.215 |
| .4    | 36.224 | 36.233 | 36.242 | 36.251 | 36.260 | 36.269 | 36.278 | 36.286 | 36.295 | 36.304 |
| .5    | 36.313 | 36.322 | 36.331 | 36.340 | 36.348 | 36.357 | 36.366 | 36.375 | 36.384 | 36.393 |
| .6    | 36.401 | 36.410 | 36.419 | 36.428 | 36.437 | 36.446 | 36.454 | 36.463 | 36.472 | 36.481 |
| .7    | 36.490 | 36.499 | 36.507 | 36.516 | 36.525 | 36.534 | 36.543 | 36.551 | 36.560 | 36.569 |
| .8    | 36.578 | 36.587 | 36.595 | 36.604 | 36.613 | 36.622 | 36.630 | 36.639 | 36.648 | 36.657 |
| .9    | 36.666 | 36.674 | 36.683 | 36.692 | 36.701 | 36.709 | 36.718 | 36.727 | 36.736 | 36.744 |
| 21.0  | 36.753 | 36.762 | 36.771 | 36.779 | 36.788 | 36.797 | 36.806 | 36.814 | 36.823 | 36.832 |
| .1    | 36.841 | 36.849 | 36.858 | 36.867 | 36.875 | 36.884 | 36.893 | 36.902 | 36.910 | 36.919 |
| .2    | 36.928 | 36.936 | 36.945 | 36.954 | 36.963 | 36.971 | 36.980 | 36.989 | 36.997 | 37.006 |
| .3    | 37.015 | 37.023 | 37.032 | 37.041 | 37.049 | 36.058 | 37.067 | 37.076 | 37.084 | 37.093 |
| .4    | 37.102 | 37.110 | 37.119 | 37.128 | 37.136 | 37.145 | 37.154 | 37.162 | 37.171 | 37.179 |
| .5    | 37.188 | 37.197 | 37.205 | 37.214 | 37.223 | 37.231 | 37.240 | 37.249 | 37.257 | 37.266 |
| .6    | 37.275 | 37.283 | 37.292 | 37.300 | 37.309 | 37.318 | 37.326 | 37.335 | 37.343 | 37.352 |
| .7    | 37.361 | 37.369 | 37.378 | 37.387 | 37.395 | 37.404 | 37.412 | 37.421 | 37.430 | 37.438 |
| .8    | 37.447 | 37.455 | 37.464 | 37.472 | 37.481 | 37.490 | 37.498 | 37.506 | 37.515 | 37.524 |
| .9    | 37.532 | 37.541 | 37.550 | 37.558 | 37.567 | 37.575 | 37.584 | 37.592 | 37.601 | 37.610 |
| 22.0  | 37.618 | 37.627 | 37.635 | 37.644 | 37.652 | 37.661 | 37.669 | 37.678 | 37.686 | 37.695 |
| .1    | 37.703 | 37.712 | 37.721 | 37.729 | 37.738 | 37.746 | 37.755 | 37.763 | 37.772 | 37.780 |
| .2    | 37.789 | 37.797 | 37.806 | 37.814 | 37.822 | 37.831 | 37.840 | 37.848 | 37.857 | 37.865 |
| .3    | 37.874 | 37.882 | 37.891 | 37.899 | 37.908 | 37.916 | 37.925 | 37.933 | 37.942 | 37.950 |
| .4    | 37.959 | 37.967 | 37.975 | 37.984 | 37.992 | 38.001 | 38.009 | 38.018 | 38.026 | 38.035 |
| .5    | 38.043 | 38.052 | 38.060 | 38.068 | 38.077 | 38.085 | 38.094 | 38.102 | 38.111 | 38.119 |
| .6    | 38.128 | 38.136 | 38.144 | 38.153 | 38.161 | 38.170 | 38.178 | 38.187 | 38.195 | 38.203 |
| .7    | 38.212 | 38.220 | 38.229 | 38.237 | 38.246 | 38.254 | 38.262 | 38.271 | 38.279 | 38.288 |
| .8    | 38.296 | 38.304 | 38.313 | 38.321 | 38.330 | 38.338 | 38.346 | 38.355 | 38.363 | 38.371 |
| .9    | 38.380 | 38.388 | 38.397 | 38.405 | 38.413 | 38.422 | 38.430 | 38.438 | 38.447 | 38.455 |
| 23.0  | 38.464 | 38.472 | 38.480 | 38.489 | 38.497 | 38.505 | 38.514 | 38.522 | 38.530 | 38.539 |
| .1    | 38.547 | 38.555 | 38.564 | 38.572 | 38.580 | 38.589 | 38.597 | 38.605 | 38.614 | 38.622 |
| .2    | 38.630 | 38.638 | 38.647 | 38.655 | 38.664 | 38.672 | 38.680 | 38.689 | 38.697 | 38.705 |
| .3    | 38.714 | 38.722 | 38.730 | 38.738 | 38.747 | 38.755 | 38.763 | 38.772 | 38.780 | 38.788 |
| .4    | 38.797 | 38.805 | 38.813 | 38.821 | 38.830 | 38.838 | 38.846 | 38.855 | 38.863 | 38.871 |
| .5    | 38.879 | 38.888 | 38.896 | 38.904 | 38.912 | 38.921 | 38.929 | 38.937 | 38.94  | 38.954 |
| .6    | 38.962 | 38.970 | 38.978 | 38.987 | 38.995 | 39.003 | 39.011 | 39.020 | 39.028 | 39.036 |
| .7    | 39.044 | 39.053 | 39.061 | 39.069 | 39.077 | 39.086 | 39.094 | 39.102 | 39.110 | 39.119 |
| .8    | 39.127 | 39.135 | 39.143 | 39.151 | 39.160 | 39.168 | 39.176 | 39.184 | 39.192 | 39.201 |
| .9    | 39.209 | 39.217 | 39.225 | 39.233 | 39.242 | 39.250 | 39.258 | 39.266 | 39.274 | 39.283 |
| 24.0  | 39.291 | 39.299 | 39.307 | 39.315 | 39.324 | 39.332 | 39.340 | 39.348 | 39.356 | 39.364 |
| .1    | 39.373 | 39.381 | 39.389 | 39.397 | 39.405 | 39.413 | 39.422 | 39.430 | 39.438 | 39.446 |
| .2    | 39.454 | 39.462 | 39.470 | 39.479 | 39.487 | 39.495 | 39.503 | 39.511 | 39.519 | 39.527 |
| .3    | 39.536 | 39.544 | 39.552 | 39.560 | 39.568 | 39.576 | 39.584 | 39.592 | 39.601 | 39.609 |
| .4    | 39.617 | 39.625 | 39.633 | 39.641 | 39.649 | 39.657 | 39.666 | 39.674 | 39.682 | 39.690 |
| .5    | 39.698 | 39.706 | 39.714 | 39.722 | 39.730 | 39.738 | 39.747 | 39.755 | 39.763 | 39.771 |
| .6    | 39.779 | 39.787 | 39.795 | 39.803 | 39.811 | 39.819 | 39.827 | 39.835 | 39.844 | 39.852 |
| .7    | 39.860 | 39.868 | 39.876 | 39.884 | 39.892 | 39.900 | 39.908 | 39.916 | 39.924 | 39.932 |
| .8    | 39.940 | 39.948 | 39.956 | 39.964 | 39.972 | 39.981 | 39.989 | 39.997 | 40.005 | 40.013 |
| .9    | 40.021 | 40.029 | 40.037 | 40.045 | 40.053 | 40.061 | 40.069 | 40.077 | 40.085 | 40.093 |

## VELOCITIES, IN FEET PER SECOND, DUE TO HEADS FROM 25 TO 29.99 FEET.

| Head. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 25.0  | 40.101 | 40.109 | 40.117 | 40.125 | 40.133 | 40.141 | 40.149 | 40.157 | 40.165 | 40.173 |
| .1    | 40.181 | 40.189 | 40.197 | 40.205 | 40.213 | 40.221 | 40.229 | 40.237 | 40.245 | 40.253 |
| .2    | 40.261 | 40.269 | 40.277 | 40.285 | 40.293 | 40.301 | 40.309 | 40.317 | 40.325 | 40.333 |
| .3    | 40.341 | 40.349 | 40.357 | 40.365 | 40.373 | 40.381 | 40.389 | 40.397 | 40.405 | 40.413 |
| .4    | 40.421 | 40.428 | 40.436 | 40.444 | 40.452 | 40.460 | 40.468 | 40.476 | 40.484 | 40.492 |
| .5    | 40.500 | 40.508 | 40.516 | 40.524 | 40.532 | 40.540 | 40.548 | 40.556 | 40.563 | 40.571 |
| .6    | 40.579 | 40.587 | 40.595 | 40.603 | 40.611 | 40.619 | 40.627 | 40.635 | 40.643 | 40.651 |
| .7    | 40.659 | 40.666 | 40.674 | 40.682 | 40.690 | 40.698 | 40.706 | 40.714 | 40.722 | 40.730 |
| .8    | 40.738 | 40.745 | 40.753 | 40.761 | 40.769 | 40.777 | 40.785 | 40.793 | 40.801 | 40.809 |
| .9    | 40.816 | 40.824 | 40.832 | 40.840 | 40.848 | 40.856 | 40.864 | 40.872 | 40.879 | 40.887 |
| 26.0  | 40.905 | 40.903 | 40.911 | 40.919 | 40.927 | 40.934 | 40.942 | 40.950 | 40.958 | 40.966 |
| .1    | 40.974 | 40.982 | 40.989 | 40.997 | 41.005 | 41.013 | 41.021 | 41.029 | 41.036 | 41.044 |
| .2    | 41.052 | 41.060 | 41.068 | 41.076 | 41.083 | 41.091 | 41.099 | 41.107 | 41.115 | 41.123 |
| .3    | 41.130 | 41.138 | 41.146 | 41.154 | 41.162 | 41.169 | 41.177 | 41.185 | 41.193 | 41.201 |
| .4    | 41.209 | 41.216 | 41.224 | 41.232 | 41.240 | 41.248 | 41.255 | 41.263 | 41.271 | 41.279 |
| .5    | 41.287 | 41.294 | 41.302 | 41.310 | 41.318 | 41.325 | 41.333 | 41.341 | 41.349 | 41.357 |
| .6    | 41.364 | 41.372 | 41.380 | 41.388 | 41.395 | 41.403 | 41.411 | 41.419 | 41.426 | 41.434 |
| .7    | 41.442 | 41.450 | 41.458 | 41.465 | 41.473 | 41.481 | 41.489 | 41.496 | 41.504 | 41.512 |
| .8    | 41.520 | 41.527 | 41.535 | 41.543 | 41.551 | 41.558 | 41.566 | 41.574 | 41.581 | 41.589 |
| .9    | 41.597 | 41.605 | 41.612 | 41.620 | 41.628 | 41.636 | 41.643 | 41.651 | 41.659 | 41.666 |
| 27.0  | 41.674 | 41.682 | 41.690 | 41.697 | 41.705 | 41.713 | 41.720 | 41.728 | 41.736 | 41.744 |
| .1    | 41.751 | 41.759 | 41.767 | 41.774 | 41.782 | 41.790 | 41.797 | 41.805 | 41.813 | 41.821 |
| .2    | 41.828 | 41.836 | 41.844 | 41.851 | 41.859 | 41.867 | 41.874 | 41.882 | 41.890 | 41.897 |
| .3    | 41.905 | 41.913 | 41.920 | 41.928 | 41.936 | 41.943 | 41.951 | 41.959 | 41.967 | 41.974 |
| .4    | 41.982 | 41.989 | 41.997 | 42.005 | 42.012 | 42.020 | 42.028 | 42.035 | 42.043 | 42.051 |
| .5    | 42.058 | 42.066 | 42.074 | 42.081 | 42.089 | 42.096 | 42.104 | 42.112 | 42.119 | 42.127 |
| .6    | 42.135 | 42.142 | 42.150 | 42.158 | 42.165 | 42.173 | 42.180 | 42.188 | 42.196 | 42.203 |
| .7    | 42.211 | 42.219 | 42.227 | 42.234 | 42.241 | 42.249 | 42.257 | 42.264 | 42.272 | 42.279 |
| .8    | 42.287 | 42.295 | 42.302 | 42.310 | 42.317 | 42.325 | 42.333 | 42.340 | 42.348 | 42.355 |
| .9    | 42.363 | 42.371 | 42.378 | 42.386 | 42.393 | 42.401 | 42.409 | 42.416 | 42.424 | 42.431 |
| 28.0  | 42.439 | 42.446 | 42.454 | 42.462 | 42.469 | 42.477 | 42.484 | 42.492 | 42.499 | 42.507 |
| .1    | 42.515 | 42.522 | 42.530 | 42.537 | 42.545 | 42.552 | 42.560 | 42.568 | 42.575 | 42.583 |
| .2    | 42.590 | 42.598 | 42.605 | 42.613 | 42.620 | 42.628 | 42.635 | 42.643 | 42.651 | 42.658 |
| .3    | 42.666 | 42.673 | 42.681 | 42.688 | 42.696 | 42.703 | 42.711 | 42.718 | 42.726 | 42.733 |
| .4    | 42.741 | 42.748 | 42.756 | 42.764 | 42.771 | 42.779 | 42.786 | 42.794 | 42.801 | 42.809 |
| .5    | 42.816 | 42.824 | 42.831 | 42.839 | 42.846 | 42.854 | 42.861 | 42.869 | 42.876 | 42.884 |
| .6    | 42.891 | 42.899 | 42.906 | 42.914 | 42.921 | 42.929 | 42.936 | 42.944 | 42.951 | 42.959 |
| .7    | 42.966 | 42.974 | 42.981 | 42.989 | 42.996 | 43.004 | 43.011 | 43.018 | 43.026 | 43.033 |
| .8    | 43.041 | 43.048 | 43.056 | 43.063 | 43.071 | 43.078 | 43.086 | 43.093 | 43.101 | 43.108 |
| .9    | 43.116 | 43.123 | 43.130 | 43.138 | 43.145 | 43.153 | 43.160 | 43.168 | 43.175 | 43.183 |
| 29.0  | 43.190 | 43.198 | 43.205 | 43.212 | 43.220 | 43.227 | 43.235 | 43.243 | 43.250 | 43.257 |
| .1    | 43.264 | 43.272 | 43.279 | 43.287 | 43.294 | 43.302 | 43.309 | 43.316 | 43.324 | 43.331 |
| .2    | 43.339 | 43.346 | 43.354 | 43.361 | 43.368 | 43.376 | 43.383 | 43.391 | 43.398 | 43.405 |
| .3    | 43.413 | 43.420 | 43.428 | 43.435 | 43.443 | 43.450 | 43.457 | 43.465 | 43.472 | 43.480 |
| .4    | 43.487 | 43.494 | 43.502 | 43.509 | 43.517 | 43.524 | 43.531 | 43.539 | 43.546 | 43.553 |
| .5    | 43.561 | 43.568 | 43.576 | 43.583 | 43.590 | 43.598 | 43.605 | 43.612 | 43.620 | 43.627 |
| .6    | 43.635 | 43.642 | 43.649 | 43.657 | 43.664 | 43.671 | 43.679 | 43.686 | 43.694 | 43.701 |
| .7    | 43.708 | 43.716 | 43.723 | 43.730 | 43.738 | 43.745 | 43.752 | 43.760 | 43.767 | 43.774 |
| .8    | 43.782 | 43.789 | 43.796 | 43.804 | 43.811 | 43.818 | 43.826 | 43.833 | 43.840 | 43.848 |
| .9    | 43.855 | 43.862 | 43.870 | 43.877 | 43.884 | 43.892 | 43.899 | 43.906 | 43.914 | 43.921 |

VELOCITIES, IN FEET PER SECOND, DUE TO HEADS FROM 30 TO  
34.99 FEET.

| Head. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 30.0  | 43.928 | 43.936 | 43.943 | 43.950 | 43.958 | 43.965 | 43.972 | 43.980 | 43.987 | 43.994 |
| .1    | 44.002 | 44.009 | 44.016 | 44.024 | 44.031 | 44.038 | 44.045 | 44.053 | 44.060 | 44.067 |
| .2    | 44.075 | 44.082 | 44.089 | 44.097 | 44.104 | 44.111 | 44.118 | 44.126 | 44.133 | 44.140 |
| .3    | 44.148 | 44.155 | 44.162 | 44.169 | 44.177 | 44.184 | 44.191 | 44.198 | 44.206 | 44.213 |
| .4    | 44.220 | 44.228 | 44.235 | 44.242 | 44.249 | 44.257 | 44.264 | 44.271 | 44.278 | 44.286 |
| .5    | 44.293 | 44.300 | 44.308 | 44.315 | 44.322 | 44.329 | 44.337 | 44.344 | 44.351 | 44.358 |
| .6    | 44.366 | 44.373 | 44.380 | 44.387 | 44.395 | 44.402 | 44.409 | 44.416 | 44.423 | 44.431 |
| .7    | 44.438 | 44.445 | 44.452 | 44.460 | 44.467 | 44.474 | 44.481 | 44.489 | 44.496 | 44.503 |
| .8    | 44.510 | 44.518 | 44.525 | 44.532 | 44.539 | 44.546 | 44.554 | 44.561 | 44.568 | 44.575 |
| .9    | 44.582 | 44.590 | 44.597 | 44.604 | 44.611 | 44.619 | 44.626 | 44.633 | 44.640 | 44.647 |
| 31.0  | 44.655 | 44.662 | 44.669 | 44.676 | 44.683 | 44.691 | 44.698 | 44.705 | 44.712 | 44.719 |
| .1    | 44.727 | 44.734 | 44.741 | 44.748 | 44.755 | 44.762 | 44.770 | 44.777 | 44.784 | 44.791 |
| .2    | 44.798 | 44.806 | 44.813 | 44.820 | 44.827 | 44.834 | 44.841 | 44.849 | 44.856 | 44.863 |
| .3    | 44.870 | 44.877 | 44.884 | 44.892 | 44.899 | 44.906 | 44.913 | 44.920 | 44.927 | 44.935 |
| .4    | 44.942 | 44.949 | 44.956 | 44.963 | 44.970 | 44.978 | 44.985 | 44.992 | 44.999 | 45.006 |
| .5    | 45.013 | 45.020 | 45.028 | 45.035 | 45.042 | 45.049 | 45.056 | 45.063 | 45.070 | 45.078 |
| .6    | 45.085 | 45.092 | 45.099 | 45.106 | 45.113 | 45.120 | 45.127 | 45.135 | 45.142 | 45.149 |
| .7    | 45.156 | 45.163 | 45.170 | 45.177 | 45.184 | 45.192 | 45.199 | 45.206 | 45.213 | 45.220 |
| .8    | 45.227 | 45.234 | 45.241 | 45.248 | 45.256 | 45.263 | 45.270 | 45.277 | 45.284 | 45.291 |
| .9    | 45.298 | 45.305 | 45.312 | 45.319 | 45.327 | 45.334 | 45.341 | 45.348 | 45.355 | 45.362 |
| 32.0  | 45.369 | 45.376 | 45.383 | 45.390 | 45.397 | 45.405 | 45.412 | 45.419 | 45.426 | 45.433 |
| .1    | 45.440 | 45.447 | 45.454 | 45.461 | 45.468 | 45.475 | 45.482 | 45.489 | 45.497 | 45.504 |
| .2    | 45.511 | 45.518 | 45.525 | 45.532 | 45.539 | 45.546 | 45.553 | 45.560 | 45.567 | 45.574 |
| .3    | 45.581 | 45.588 | 45.595 | 45.602 | 45.609 | 45.617 | 45.624 | 45.631 | 45.638 | 45.645 |
| .4    | 45.652 | 45.659 | 45.666 | 45.673 | 45.680 | 45.687 | 45.694 | 45.701 | 45.708 | 45.715 |
| .5    | 45.722 | 45.729 | 45.736 | 45.743 | 45.750 | 45.757 | 45.764 | 45.771 | 45.778 | 45.785 |
| .6    | 45.792 | 45.799 | 45.807 | 45.814 | 45.821 | 45.828 | 45.835 | 45.842 | 45.849 | 45.856 |
| .7    | 45.863 | 45.870 | 45.877 | 45.884 | 45.891 | 45.898 | 45.905 | 45.912 | 45.919 | 45.926 |
| .8    | 45.933 | 45.940 | 45.947 | 45.954 | 45.961 | 45.968 | 45.975 | 45.982 | 45.989 | 45.996 |
| .9    | 46.003 | 46.010 | 46.017 | 46.024 | 46.031 | 46.038 | 46.045 | 46.052 | 46.059 | 46.066 |
| 33.0  | 46.073 | 46.080 | 46.086 | 46.093 | 46.100 | 46.107 | 46.114 | 46.121 | 46.128 | 46.135 |
| .1    | 46.142 | 46.149 | 46.156 | 46.163 | 46.170 | 46.177 | 46.184 | 46.191 | 46.198 | 46.205 |
| .2    | 46.212 | 46.219 | 46.226 | 46.233 | 46.240 | 46.247 | 46.254 | 46.261 | 46.268 | 46.275 |
| .3    | 46.281 | 46.288 | 46.295 | 46.302 | 46.309 | 46.316 | 46.323 | 46.330 | 46.337 | 46.344 |
| .4    | 46.351 | 46.358 | 46.365 | 46.372 | 46.379 | 46.386 | 46.393 | 46.399 | 46.406 | 46.413 |
| .5    | 46.420 | 46.427 | 46.434 | 46.441 | 46.447 | 46.455 | 46.462 | 46.469 | 46.476 | 46.483 |
| .6    | 46.489 | 46.496 | 46.503 | 46.510 | 46.517 | 46.524 | 46.531 | 46.538 | 46.545 | 46.552 |
| .7    | 46.559 | 46.566 | 46.572 | 46.579 | 46.586 | 46.593 | 46.600 | 46.607 | 46.614 | 46.621 |
| .8    | 46.628 | 46.635 | 46.642 | 46.648 | 46.655 | 46.662 | 46.669 | 46.676 | 46.683 | 46.690 |
| .9    | 46.697 | 46.703 | 46.710 | 46.717 | 46.724 | 46.731 | 46.739 | 46.745 | 46.752 | 46.759 |
| 34.0  | 46.765 | 46.772 | 46.779 | 46.786 | 46.793 | 46.800 | 46.807 | 46.814 | 46.820 | 46.827 |
| .1    | 46.834 | 46.841 | 46.848 | 46.855 | 46.862 | 46.868 | 46.875 | 46.882 | 46.889 | 46.896 |
| .2    | 46.903 | 46.910 | 46.916 | 46.923 | 46.930 | 46.937 | 46.944 | 46.951 | 46.958 | 46.964 |
| .3    | 46.971 | 46.978 | 46.985 | 46.992 | 46.999 | 47.005 | 47.012 | 47.019 | 47.026 | 47.033 |
| .4    | 47.040 | 47.047 | 47.053 | 47.060 | 47.067 | 47.074 | 47.081 | 47.088 | 47.094 | 47.101 |
| .5    | 47.108 | 47.115 | 47.122 | 47.128 | 47.135 | 47.142 | 47.149 | 47.156 | 47.163 | 47.169 |
| .6    | 47.176 | 47.183 | 47.190 | 47.197 | 47.203 | 47.210 | 47.217 | 47.224 | 47.231 | 47.238 |
| .7    | 47.244 | 47.251 | 47.258 | 47.265 | 47.272 | 47.278 | 47.285 | 47.292 | 47.299 | 47.306 |
| .8    | 47.312 | 47.319 | 47.326 | 47.333 | 47.340 | 47.346 | 47.353 | 47.360 | 47.367 | 47.374 |
| .9    | 47.380 | 47.387 | 47.394 | 47.401 | 47.407 | 47.414 | 47.421 | 47.428 | 47.435 | 47.441 |

VELOCITIES, IN FEET PER SECOND, DUE TO HEADS FROM 35 TO 39.99 FEET.

| Head. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 35.0  | 47.448 | 47.455 | 47.462 | 47.469 | 47.475 | 47.482 | 47.489 | 47.496 | 47.502 | 47.509 |
| .1    | 47.516 | 47.523 | 47.529 | 47.536 | 47.543 | 47.550 | 47.556 | 47.563 | 47.570 | 47.577 |
| .2    | 47.584 | 47.590 | 47.597 | 47.604 | 47.611 | 47.617 | 47.624 | 47.631 | 47.638 | 47.644 |
| .3    | 47.651 | 47.658 | 47.665 | 47.671 | 47.678 | 47.685 | 47.692 | 47.698 | 47.705 | 47.712 |
| .4    | 44.719 | 47.725 | 47.732 | 47.739 | 47.745 | 47.752 | 47.759 | 47.766 | 47.772 | 47.779 |
| .5    | 47.786 | 47.793 | 47.799 | 47.806 | 47.813 | 47.819 | 47.826 | 47.833 | 47.840 | 47.846 |
| .6    | 47.853 | 47.860 | 47.867 | 47.873 | 47.880 | 47.887 | 47.893 | 47.900 | 47.907 | 47.914 |
| .7    | 47.920 | 47.927 | 47.934 | 47.940 | 47.947 | 47.954 | 47.961 | 47.967 | 47.974 | 47.981 |
| .8    | 47.987 | 47.994 | 48.001 | 48.007 | 48.014 | 48.021 | 48.028 | 48.034 | 48.041 | 48.048 |
| .9    | 48.054 | 48.061 | 48.068 | 48.074 | 48.081 | 48.088 | 48.094 | 48.101 | 48.108 | 48.115 |
| 36.0  | 48.121 | 48.128 | 48.134 | 48.141 | 48.148 | 48.155 | 48.161 | 48.168 | 48.175 | 48.181 |
| .1    | 48.188 | 48.195 | 48.201 | 48.208 | 48.215 | 48.221 | 48.228 | 48.235 | 48.241 | 48.248 |
| .2    | 48.255 | 48.261 | 48.268 | 48.275 | 48.281 | 48.288 | 48.295 | 48.302 | 48.308 | 48.315 |
| .3    | 48.321 | 48.328 | 48.335 | 48.341 | 48.348 | 48.355 | 48.361 | 48.368 | 48.375 | 48.381 |
| .4    | 48.388 | 48.394 | 48.401 | 48.408 | 48.414 | 48.421 | 48.428 | 48.434 | 48.441 | 48.448 |
| .5    | 48.454 | 48.461 | 48.467 | 48.474 | 48.481 | 48.487 | 48.494 | 48.501 | 48.507 | 48.514 |
| .6    | 48.521 | 48.527 | 48.534 | 48.540 | 48.547 | 48.554 | 48.560 | 48.567 | 48.574 | 48.580 |
| .7    | 48.587 | 48.593 | 48.600 | 48.607 | 48.613 | 48.620 | 48.626 | 48.633 | 48.640 | 48.646 |
| .8    | 48.653 | 48.660 | 48.666 | 48.673 | 48.679 | 48.686 | 48.693 | 48.699 | 48.706 | 48.712 |
| .9    | 48.719 | 48.726 | 48.732 | 48.739 | 48.745 | 48.752 | 48.759 | 48.765 | 48.771 | 48.778 |
| 37.0  | 48.785 | 48.792 | 48.798 | 48.805 | 48.811 | 48.818 | 48.824 | 48.831 | 48.838 | 48.844 |
| .1    | 48.851 | 48.857 | 48.864 | 48.871 | 48.877 | 48.884 | 48.890 | 48.897 | 48.903 | 48.910 |
| .2    | 48.917 | 48.923 | 48.930 | 48.936 | 48.943 | 48.950 | 48.956 | 48.963 | 48.969 | 48.976 |
| .3    | 48.982 | 48.989 | 48.995 | 49.002 | 49.009 | 49.015 | 49.022 | 49.028 | 49.035 | 49.041 |
| .4    | 49.048 | 49.055 | 49.061 | 49.068 | 49.074 | 49.081 | 49.087 | 49.094 | 49.100 | 49.107 |
| .5    | 49.113 | 49.120 | 49.127 | 49.133 | 49.140 | 49.146 | 49.153 | 49.159 | 49.166 | 49.172 |
| .6    | 49.179 | 49.185 | 49.192 | 49.199 | 49.205 | 49.212 | 49.218 | 49.225 | 49.231 | 49.238 |
| .7    | 49.244 | 49.251 | 49.257 | 49.264 | 49.270 | 49.277 | 49.283 | 49.290 | 49.297 | 49.303 |
| .8    | 49.310 | 49.316 | 49.323 | 49.329 | 49.336 | 49.342 | 49.349 | 49.355 | 49.362 | 49.368 |
| .9    | 49.375 | 49.381 | 49.388 | 49.394 | 49.401 | 49.407 | 49.414 | 49.420 | 49.427 | 49.433 |
| 38.0  | 49.440 | 49.446 | 49.453 | 49.459 | 49.466 | 49.472 | 49.479 | 49.485 | 49.492 | 49.498 |
| .1    | 49.505 | 49.511 | 49.518 | 49.524 | 49.531 | 49.537 | 49.544 | 49.550 | 49.557 | 49.563 |
| .2    | 49.570 | 49.576 | 49.583 | 49.589 | 49.596 | 49.602 | 49.609 | 49.615 | 49.622 | 49.628 |
| .3    | 49.635 | 49.641 | 49.648 | 49.654 | 49.661 | 49.667 | 49.673 | 49.680 | 49.686 | 49.693 |
| .4    | 49.699 | 49.706 | 49.712 | 49.719 | 49.725 | 49.732 | 49.738 | 49.745 | 49.751 | 49.758 |
| .5    | 49.764 | 49.770 | 49.777 | 49.783 | 49.790 | 49.796 | 49.803 | 49.809 | 49.816 | 49.822 |
| .6    | 49.829 | 49.835 | 49.842 | 49.848 | 49.854 | 49.861 | 49.867 | 49.874 | 49.880 | 49.887 |
| .7    | 49.893 | 49.900 | 49.906 | 49.912 | 49.919 | 49.925 | 49.932 | 49.938 | 49.945 | 49.951 |
| .8    | 49.958 | 49.964 | 49.970 | 49.977 | 49.983 | 49.990 | 49.996 | 50.003 | 50.009 | 50.015 |
| .9    | 50.022 | 50.028 | 50.035 | 50.041 | 50.048 | 50.054 | 50.060 | 50.067 | 50.073 | 50.080 |
| 39.0  | 50.086 | 50.093 | 50.099 | 50.105 | 50.112 | 50.118 | 50.125 | 50.131 | 50.137 | 50.144 |
| .1    | 50.150 | 50.157 | 50.163 | 50.170 | 50.176 | 50.182 | 50.189 | 50.195 | 50.202 | 50.208 |
| .2    | 50.214 | 50.221 | 50.227 | 50.234 | 50.240 | 50.246 | 50.253 | 50.259 | 50.266 | 50.272 |
| .3    | 50.278 | 50.285 | 50.291 | 50.298 | 50.304 | 50.310 | 50.317 | 50.323 | 50.330 | 50.336 |
| .4    | 50.342 | 50.349 | 50.355 | 50.362 | 50.368 | 50.374 | 50.381 | 50.387 | 50.393 | 50.400 |
| .5    | 50.406 | 50.413 | 50.419 | 50.425 | 50.432 | 50.438 | 50.444 | 50.451 | 50.457 | 50.464 |
| .6    | 50.470 | 50.476 | 50.483 | 50.489 | 50.495 | 50.502 | 50.508 | 50.515 | 50.521 | 50.527 |
| .7    | 50.534 | 50.540 | 50.546 | 50.553 | 50.559 | 50.565 | 50.572 | 50.578 | 50.585 | 50.591 |
| .8    | 50.597 | 50.604 | 50.610 | 50.616 | 50.623 | 50.629 | 50.635 | 50.642 | 50.648 | 50.654 |
| .9    | 50.661 | 50.667 | 50.673 | 50.680 | 50.686 | 50.692 | 50.699 | 50.705 | 50.712 | 50.718 |



## VELOCITIES, IN FEET PER SECOND, DUE TO HEADS FROM 40 TO 44.99 FEET.

| Head. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 40.0  | 50.724 | 50.731 | 50.737 | 50.743 | 50.750 | 50.756 | 50.762 | 50.769 | 50.775 | 50.781 |
| .1    | 50.788 | 50.794 | 50.800 | 50.807 | 50.813 | 50.819 | 50.826 | 50.832 | 50.838 | 50.845 |
| .2    | 50.851 | 50.857 | 50.863 | 50.870 | 50.876 | 50.882 | 50.889 | 50.895 | 50.901 | 50.908 |
| .3    | 50.914 | 50.920 | 50.927 | 50.933 | 50.939 | 50.946 | 50.952 | 50.958 | 50.965 | 50.971 |
| .4    | 50.977 | 50.983 | 50.990 | 50.996 | 51.002 | 51.009 | 51.015 | 51.021 | 51.028 | 51.034 |
| .5    | 51.040 | 51.047 | 51.053 | 51.059 | 51.065 | 51.072 | 51.078 | 51.084 | 51.091 | 51.097 |
| .6    | 51.103 | 51.110 | 51.116 | 51.122 | 51.128 | 51.135 | 51.141 | 51.147 | 51.154 | 51.160 |
| .7    | 51.166 | 51.172 | 51.179 | 51.185 | 51.191 | 51.198 | 51.204 | 51.210 | 51.216 | 51.223 |
| .8    | 51.229 | 51.235 | 51.241 | 51.248 | 51.254 | 51.260 | 51.267 | 51.273 | 51.279 | 51.285 |
| .9    | 51.292 | 51.298 | 51.304 | 51.310 | 51.317 | 51.323 | 51.329 | 51.336 | 51.342 | 51.348 |
| 41.0  | 51.354 | 51.361 | 51.367 | 51.373 | 51.379 | 51.386 | 51.392 | 51.398 | 51.404 | 51.411 |
| .1    | 51.417 | 51.423 | 51.429 | 51.436 | 51.442 | 51.448 | 51.454 | 51.461 | 51.467 | 51.473 |
| .2    | 51.479 | 51.486 | 51.492 | 51.498 | 51.504 | 51.511 | 51.517 | 51.523 | 51.529 | 51.536 |
| .3    | 51.542 | 51.548 | 51.554 | 51.561 | 51.567 | 51.573 | 51.579 | 51.586 | 51.592 | 51.598 |
| .4    | 51.604 | 51.610 | 51.617 | 51.623 | 51.629 | 51.635 | 51.642 | 51.648 | 51.654 | 51.660 |
| .5    | 51.667 | 51.673 | 51.679 | 51.685 | 51.691 | 51.698 | 51.704 | 51.710 | 51.716 | 51.723 |
| .6    | 51.729 | 51.735 | 51.741 | 51.747 | 51.754 | 51.760 | 51.766 | 51.772 | 51.778 | 51.785 |
| .7    | 51.791 | 51.797 | 51.803 | 51.809 | 51.816 | 51.822 | 51.828 | 51.834 | 51.841 | 51.847 |
| .8    | 51.853 | 51.859 | 51.865 | 51.872 | 51.878 | 51.884 | 51.890 | 51.896 | 51.903 | 51.909 |
| .9    | 51.915 | 51.921 | 51.927 | 51.934 | 51.940 | 51.946 | 51.952 | 51.958 | 51.964 | 51.971 |
| 42.0  | 51.977 | 51.983 | 51.989 | 51.995 | 52.002 | 52.008 | 52.014 | 52.020 | 52.026 | 52.032 |
| .1    | 52.039 | 52.045 | 52.051 | 52.057 | 52.063 | 52.070 | 52.076 | 52.082 | 52.088 | 52.094 |
| .2    | 52.100 | 52.107 | 52.113 | 52.119 | 52.125 | 52.131 | 52.137 | 52.144 | 52.150 | 52.156 |
| .3    | 52.162 | 52.168 | 52.174 | 52.181 | 52.187 | 52.193 | 52.199 | 52.205 | 52.211 | 52.218 |
| .4    | 52.224 | 52.230 | 52.236 | 52.242 | 52.248 | 52.255 | 52.261 | 52.267 | 52.273 | 52.279 |
| .5    | 52.285 | 52.291 | 52.298 | 52.304 | 52.310 | 52.316 | 52.322 | 52.328 | 52.334 | 52.341 |
| .6    | 52.347 | 52.353 | 52.359 | 52.365 | 52.371 | 52.377 | 52.384 | 52.390 | 52.396 | 52.402 |
| .7    | 52.408 | 52.414 | 52.420 | 52.427 | 52.433 | 52.439 | 52.445 | 52.451 | 52.457 | 52.463 |
| .8    | 52.470 | 52.476 | 52.482 | 52.488 | 52.494 | 52.500 | 52.506 | 52.512 | 52.519 | 52.525 |
| .9    | 52.531 | 52.537 | 52.543 | 52.549 | 52.555 | 52.561 | 52.567 | 52.574 | 52.580 | 52.586 |
| 43.0  | 52.592 | 52.598 | 52.604 | 52.610 | 52.616 | 52.623 | 52.629 | 52.635 | 52.641 | 52.647 |
| .1    | 52.653 | 52.659 | 52.665 | 52.671 | 52.678 | 52.684 | 52.690 | 52.696 | 52.702 | 52.708 |
| .2    | 52.714 | 52.720 | 52.726 | 52.732 | 52.738 | 52.745 | 52.751 | 52.757 | 52.763 | 52.769 |
| .3    | 52.775 | 52.781 | 52.787 | 52.793 | 52.799 | 52.806 | 52.812 | 52.818 | 52.824 | 52.830 |
| .4    | 52.836 | 52.842 | 52.848 | 52.854 | 52.860 | 52.866 | 52.873 | 52.879 | 52.885 | 52.891 |
| .5    | 52.897 | 52.903 | 52.909 | 52.915 | 52.921 | 52.927 | 52.933 | 52.939 | 52.945 | 52.952 |
| .6    | 52.958 | 52.964 | 52.970 | 52.976 | 52.982 | 52.988 | 52.994 | 53.000 | 53.006 | 53.012 |
| .7    | 53.018 | 53.024 | 53.030 | 53.037 | 53.043 | 53.049 | 53.055 | 53.061 | 53.067 | 53.073 |
| .8    | 53.079 | 53.085 | 53.091 | 53.097 | 53.103 | 53.109 | 53.115 | 53.121 | 53.127 | 53.133 |
| .9    | 53.139 | 53.146 | 53.152 | 53.158 | 53.164 | 53.170 | 53.176 | 53.182 | 53.188 | 53.194 |
| 44.0  | 53.200 | 53.203 | 53.212 | 53.218 | 53.224 | 53.230 | 53.236 | 53.242 | 53.248 | 53.254 |
| .1    | 53.260 | 53.266 | 53.272 | 53.279 | 53.285 | 53.291 | 53.297 | 53.303 | 53.309 | 53.315 |
| .2    | 53.321 | 53.327 | 53.333 | 53.339 | 53.345 | 53.351 | 53.357 | 53.363 | 53.369 | 53.375 |
| .3    | 53.381 | 53.387 | 53.393 | 53.399 | 53.405 | 53.411 | 53.417 | 53.423 | 53.429 | 53.435 |
| .4    | 53.441 | 53.447 | 53.453 | 53.459 | 53.465 | 53.471 | 53.477 | 53.483 | 53.489 | 53.495 |
| .5    | 53.501 | 53.507 | 53.513 | 53.519 | 53.525 | 53.531 | 53.537 | 53.543 | 53.549 | 53.555 |
| .6    | 53.561 | 53.567 | 53.573 | 53.579 | 53.586 | 53.592 | 53.598 | 53.604 | 53.610 | 53.616 |
| .7    | 53.621 | 53.627 | 53.633 | 53.639 | 53.645 | 53.651 | 53.657 | 53.663 | 53.669 | 53.675 |
| .8    | 53.681 | 53.687 | 53.693 | 53.699 | 53.705 | 53.711 | 53.717 | 53.723 | 53.729 | 53.735 |
| .9    | 53.741 | 53.747 | 53.753 | 53.759 | 53.765 | 53.771 | 53.777 | 53.783 | 53.789 | 53.795 |

VELOCITIES, IN FEET PER SECOND, DUE TO HEADS FROM 45 TO  
49.99 FEET.

| Head. | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 45.0  | 53.801 | 53.807 | 53.813 | 53.819 | 53.825 | 53.831 | 53.837 | 53.843 | 53.849 | 53.855 |
| .1    | 53.861 | 53.867 | 53.873 | 53.879 | 53.885 | 53.891 | 53.897 | 53.903 | 53.909 | 53.915 |
| .2    | 53.921 | 53.927 | 53.932 | 53.938 | 53.944 | 53.950 | 53.956 | 53.962 | 53.968 | 53.974 |
| .3    | 53.980 | 53.986 | 53.992 | 53.998 | 54.004 | 54.010 | 54.016 | 54.022 | 54.028 | 54.034 |
| .4    | 54.040 | 54.046 | 54.052 | 54.058 | 54.064 | 54.069 | 54.075 | 54.081 | 54.087 | 54.093 |
| .5    | 54.099 | 54.105 | 54.111 | 54.117 | 54.123 | 54.129 | 54.135 | 54.141 | 54.147 | 54.153 |
| .6    | 54.159 | 54.165 | 54.170 | 54.176 | 54.182 | 54.188 | 54.194 | 54.200 | 54.206 | 54.212 |
| .7    | 54.218 | 54.224 | 54.230 | 54.236 | 54.242 | 54.248 | 54.254 | 54.259 | 54.265 | 54.271 |
| .8    | 54.277 | 54.283 | 54.289 | 54.295 | 54.301 | 54.307 | 54.313 | 54.319 | 54.325 | 54.331 |
| .9    | 54.336 | 54.342 | 54.348 | 54.354 | 54.360 | 54.366 | 54.372 | 54.378 | 54.384 | 54.390 |
| 46.0  | 54.396 | 54.402 | 54.407 | 54.413 | 54.419 | 54.425 | 54.431 | 54.437 | 54.443 | 54.449 |
| .1    | 54.455 | 54.461 | 54.467 | 54.472 | 54.478 | 54.484 | 54.490 | 54.496 | 54.502 | 54.508 |
| .2    | 54.514 | 54.520 | 54.526 | 54.531 | 54.537 | 54.543 | 54.549 | 54.555 | 54.561 | 54.567 |
| .3    | 54.573 | 54.579 | 54.585 | 54.590 | 54.596 | 54.602 | 54.608 | 54.614 | 54.620 | 54.626 |
| .4    | 54.632 | 54.638 | 54.643 | 54.649 | 54.655 | 54.661 | 54.667 | 54.673 | 54.679 | 54.685 |
| .5    | 54.690 | 54.696 | 54.702 | 54.708 | 54.714 | 54.720 | 54.726 | 54.732 | 54.737 | 54.743 |
| .6    | 54.749 | 54.755 | 54.761 | 54.767 | 54.773 | 54.779 | 54.784 | 54.790 | 54.796 | 54.802 |
| .7    | 54.808 | 54.814 | 54.820 | 54.826 | 54.831 | 54.837 | 54.843 | 54.849 | 54.855 | 54.861 |
| .8    | 54.867 | 54.872 | 54.878 | 54.884 | 54.890 | 54.896 | 54.902 | 54.908 | 54.913 | 54.919 |
| .9    | 54.925 | 54.931 | 54.937 | 54.943 | 54.949 | 54.954 | 54.960 | 54.966 | 54.972 | 54.978 |
| 47.0  | 54.984 | 54.990 | 54.995 | 55.001 | 55.007 | 55.013 | 55.019 | 55.025 | 55.030 | 55.036 |
| .1    | 55.042 | 55.048 | 55.054 | 55.060 | 55.066 | 55.071 | 55.077 | 55.083 | 55.089 | 55.095 |
| .2    | 55.101 | 55.106 | 55.112 | 55.118 | 55.124 | 55.130 | 55.136 | 55.141 | 55.147 | 55.153 |
| .3    | 55.159 | 55.165 | 55.171 | 55.176 | 55.182 | 55.188 | 55.194 | 55.200 | 55.206 | 55.211 |
| .4    | 55.217 | 55.223 | 55.229 | 55.235 | 55.240 | 55.246 | 55.252 | 55.258 | 55.264 | 55.270 |
| .5    | 55.275 | 55.281 | 55.287 | 55.293 | 55.299 | 55.304 | 55.310 | 55.316 | 55.322 | 55.328 |
| .6    | 55.334 | 55.339 | 55.345 | 55.351 | 55.357 | 55.363 | 55.368 | 55.374 | 55.380 | 55.386 |
| .7    | 55.392 | 55.397 | 55.403 | 55.409 | 55.415 | 55.421 | 55.426 | 55.432 | 55.438 | 55.444 |
| .8    | 55.450 | 55.455 | 55.461 | 55.467 | 55.473 | 55.479 | 55.484 | 55.490 | 55.496 | 55.502 |
| .9    | 55.508 | 55.513 | 55.519 | 55.525 | 55.531 | 55.537 | 55.542 | 55.548 | 55.554 | 55.560 |
| 48.0  | 55.566 | 55.571 | 55.577 | 55.583 | 55.589 | 55.595 | 55.600 | 55.606 | 55.612 | 55.618 |
| .1    | 55.623 | 55.629 | 55.635 | 55.641 | 55.647 | 55.652 | 55.658 | 55.664 | 55.670 | 55.677 |
| .2    | 55.681 | 55.687 | 55.693 | 55.699 | 55.704 | 55.710 | 55.716 | 55.722 | 55.727 | 55.733 |
| .3    | 55.739 | 55.745 | 55.750 | 55.756 | 55.762 | 55.768 | 55.774 | 55.779 | 55.785 | 55.791 |
| .4    | 55.797 | 55.802 | 55.808 | 55.814 | 55.820 | 55.825 | 55.831 | 55.837 | 55.843 | 55.848 |
| .5    | 55.854 | 55.860 | 55.866 | 55.872 | 55.877 | 55.883 | 55.889 | 55.895 | 55.900 | 55.906 |
| .6    | 55.912 | 55.918 | 55.923 | 55.929 | 55.935 | 55.941 | 55.946 | 55.952 | 55.958 | 55.964 |
| .7    | 55.970 | 55.975 | 55.981 | 55.987 | 55.992 | 55.998 | 56.004 | 56.009 | 56.015 | 56.021 |
| .8    | 56.027 | 56.032 | 56.038 | 56.044 | 56.050 | 56.055 | 56.061 | 56.067 | 56.073 | 56.078 |
| .9    | 56.084 | 56.090 | 56.096 | 56.101 | 56.107 | 56.113 | 56.118 | 56.124 | 56.130 | 56.136 |
| 49.0  | 56.141 | 56.147 | 56.153 | 56.159 | 56.164 | 56.170 | 56.176 | 56.181 | 56.187 | 56.193 |
| .1    | 56.199 | 56.204 | 56.210 | 56.216 | 56.222 | 56.227 | 56.233 | 56.239 | 56.244 | 56.250 |
| .2    | 56.256 | 56.262 | 56.267 | 56.273 | 56.279 | 56.284 | 56.290 | 56.296 | 56.302 | 56.307 |
| .3    | 56.313 | 56.319 | 56.324 | 56.330 | 56.336 | 56.342 | 56.347 | 56.353 | 56.359 | 56.364 |
| .4    | 56.370 | 56.376 | 56.381 | 56.387 | 56.393 | 56.399 | 56.404 | 56.410 | 56.416 | 56.421 |
| .5    | 56.427 | 56.433 | 56.439 | 56.444 | 56.450 | 56.456 | 56.461 | 56.467 | 56.473 | 56.478 |
| .6    | 56.484 | 56.490 | 56.495 | 56.501 | 56.507 | 56.513 | 56.518 | 56.524 | 56.530 | 56.535 |
| .7    | 56.541 | 56.547 | 56.552 | 56.558 | 56.564 | 56.569 | 56.575 | 56.581 | 56.586 | 56.592 |
| .8    | 56.598 | 56.604 | 56.609 | 56.615 | 56.621 | 56.626 | 56.632 | 56.638 | 56.643 | 56.649 |
| .9    | 56.655 | 56.660 | 56.666 | 56.672 | 56.677 | 56.683 | 56.689 | 56.694 | 56.700 | 56.706 |

## Swain Turbine Co. Tables.

| Head in Feet. | Velocity due Head. | Cubic Feet per Second to one H. P. | Section of Stream in Square Feet to 1 H. P. | Section of Stream in Square Inches to 1 H. P. | Head in Feet. | Velocity due Head. | Cubic Feet per Second to one H. P. | Section of Stream in Square Feet to 1 H. P. | Section of Stream in Square Inches to 1 H. P. |
|---------------|--------------------|------------------------------------|---|---|---------------|--------------------|------------------------------------|---|---|
| 1             | 8.02               | 8.8186                             | 1.0995                                      | 158.3280                                      | 51            | 57.27              | .1729                              | .003019                                     | .4347   |
| 2             | 11.34              | 4.4093                             | .3888                                       | 55.9872                                       | 52            | 57.84              | .1695                              | .002930                                     | .4219   |
| 3             | 13.89              | 2.9395                             | .2116                                       | 30.4704                                       | 53            | 58.39              | .1663                              | .002848                                     | .4101   |
| 4             | 16.04              | 2.2046                             | .1374                                       | 19.7856                                       | 54            | 58.93              | .1633                              | .002771                                     | .3990   |
| 5             | 17.92              | 1.7637                             | .0984                                       | 14.1696                                       | 55            | 59.48              | .1603                              | .002695                                     | .3880   |
| 6             | 19.65              | 1.4697                             | .0747                                       | 10.7568                                       | 56            | 60.01              | .1574                              | .002622                                     | .3775   |
| 7             | 21.22              | 1.2598                             | .0593                                       | 8.5392  | 57            | 60.56              | .1547                              | .002554                                     | .3677   |
| 8             | 22.68              | 1.1023                             | .0486                                       | 6.9684  | 58            | 61.08              | .1520                              | .002488                                     | .3582   |
| 9             | 24.06              | .9798                              | .0407                                       | 5.8608  | 59            | 61.61              | .1494                              | .002424                                     | .3490   |
| 10            | 25.36              | .8818                              | .0347                                       | 4.9968  | 60            | 62.12              | .1469                              | .002364                                     | .3404   |
| 11            | 26.60              | .8016                              | .0301                                       | 4.3344  | 61            | 62.71              | .1445                              | .002304                                     | .3317   |
| 12            | 27.78              | .7348                              | .0264                                       | 3.8016  | 62            | 63.15              | .1422                              | .002251                                     | .3241   |
| 13            | 28.92              | .6783                              | .0234                                       | 3.3696  | 63            | 63.66              | .1399                              | .002197                                     | .3163   |
| 14            | 30.01              | .6299                              | .0209                                       | 3.0096  | 64            | 64.16              | .1377                              | .002146                                     | .3090   |
| 15            | 31.06              | .5879                              | .0189                                       | 2.7216  | 65            | 64.66              | .1356                              | .002097                                     | .3019   |
| 16            | 32.08              | .5511                              | .0171                                       | 2.4624  | 66            | 65.16              | .1336                              | .002050                                     | .2952   |
| 17            | 33.07              | .5187                              | .0156                                       | 2.2464  | 67            | 65.65              | .1316                              | .002004                                     | .2885   |
| 18            | 34.03              | .4899                              | .0143                                       | 2.0592  | 68            | 66.14              | .1296                              | .001959                                     | .2820   |
| 19            | 34.96              | .4641                              | .0132                                       | 1.9008  | 69            | 66.62              | .1278                              | .001918                                     | .2761   |
| 20            | 35.87              | .4409                              | .0122                                       | 1.7568  | 70            | 67.11              | .1259                              | .001876                                     | .2701   |
| 21            | 36.75              | .4199                              | .0114                                       | 1.6416  | 71            | 67.58              | .1242                              | .001837                                     | .2645   |
| 22            | 37.61              | .4008                              | .0106                                       | 1.5264  | 72            | 68.06              | .1224                              | .001798                                     | .2589   |
| 23            | 38.46              | .3834                              | .0099                                       | 1.4256  | 73            | 68.53              | .1208                              | .001762                                     | .2537   |
| 24            | 39.29              | .3674                              | .0093                                       | 1.3362  | 74            | 69.00              | .1191                              | .001726                                     | .2485   |
| 25            | 40.10              | .3527                              | .0087                                       | 1.2528  | 75            | 69.46              | .1175                              | .001691                                     | .2435   |
| 26            | 40.89              | .3391                              | .0082                                       | 1.1808  | 76            | 69.92              | .1160                              | .001659                                     | .2388   |
| 27            | 41.67              | .3266                              | .0078                                       | 1.1232  | 77            | 70.38              | .1145                              | .001626                                     | .2341   |
| 28            | 42.44              | .3149                              | .0074                                       | 1.0656  | 78            | 70.84              | .1130                              | .001595                                     | .2296   |
| 29            | 43.19              | .3040                              | .0070                                       | 1.0080  | 79            | 71.29              | .1116                              | .001565                                     | .2253   |
| 30            | 43.93              | .2939                              | .0066                                       | .9504   | 80            | 71.74              | .1102                              | .001536                                     | .2211   |
| 31            | 44.65              | .2844                              | .0063                                       | .9158   | 81            | 72.19              | .1088                              | .001507                                     | .2170   |
| 32            | 45.37              | .2755                              | .0060                                       | .8740   | 82            | 72.63              | .1075                              | .001480                                     | .2131   |
| 33            | 46.07              | .2672                              | .0057                                       | .8337   | 83            | 73.07              | .1062                              | .001453                                     | .2092   |
| 34            | 46.77              | .2593                              | .0055                                       | .7977   | 84            | 73.51              | .1049                              | .001425                                     | .2052   |
| 35            | 47.45              | .2519                              | .0053                                       | .7632   | 85            | 73.95              | .1037                              | .001402                                     | .2018   |
| 36            | 48.12              | .2449                              | .0050                                       | .7329   | 86            | 74.38              | .1025                              | .001379                                     | .1985   |
| 37            | 48.78              | .2383                              | .0048                                       | .7027   | 87            | 74.81              | .1013                              | .001354                                     | .1949   |
| 38            | 49.44              | .2320                              | .0046                                       | .6753   | 88            | 75.24              | .1002                              | .001331                                     | .1916   |
| 39            | 50.09              | .2261                              | .0045                                       | .6494   | 89            | 75.67              | .0990                              | .001308                                     | .1883   |
| 40            | 50.72              | .2204                              | .0043                                       | .6249   | 90            | 76.09              | .0979                              | .001286                                     | .1851   |
| 41            | 51.35              | .2150                              | .0041                                       | .6019   | 91            | 76.51              | .0969                              | .001266                                     | .1823   |
| 42            | 51.98              | .2099                              | .0040                                       | .5803   | 92            | 76.93              | .0958                              | .001245                                     | .1792   |
| 43            | 52.59              | .2050                              | .0038                                       | .5601   | 93            | 77.35              | .0948                              | .001225                                     | .1764   |
| 44            | 53.20              | .2004                              | .0037                                       | .5414   | 94            | 77.76              | .0938                              | .001206                                     | .1738   |
| 45            | 53.80              | .1959                              | .0036                                       | .5241   | 95            | 78.18              | .0928                              | .001188                                     | .1710   |
| 46            | 54.40              | .1917                              | .0035                                       | .5068   | 96            | 78.59              | .0918                              | .001168                                     | .1681   |
| 47            | 54.99              | .1876                              | .0034                                       | .4910   | 97            | 79.00              | .0909                              | .001150                                     | .1656   |
| 48            | 55.57              | .1837                              | .0033                                       | .4752   | 98            | 79.40              | .0899                              | .001132                                     | .1630   |
| 49            | 56.14              | .1799                              | .0032                                       | .4608   | 99            | 79.81              | .0890                              | .001115                                     | .1605   |
| 50            | 56.71              | .1763                              | .0031                                       | .4475   | 100           | 80.22              | .0881                              | .001098                                     | .1581   |

| Head in Feet. | Velocity due Head. | Cubic Feet per Second to one H. F. | Section of Stream in Square Feet to 1 H. F. | Section of Stream in Square Inches to 1 H. F. | Head in Feet. | Velocity due Head. | Cubic Feet per Second to one H. F. | Section of Stream in Square Feet to 1 H. F. | Section of Stream in Square Inches to 1 H. F. |
|---------------|--------------------|------------------------------------|---|---|---------------|--------------------|------------------------------------|---|---|
| 101           | 80.61              | .0873                              | .001082                                     | .1558   | 151           | 98.56              | .0584                              | .0005925                                    | .08533  |
| 102           | 81.01              | .0864                              | .001066                                     | .1535   | 152           | 98.89              | .0580                              | .0005865                                    | .08445  |
| 103           | 81.40              | .0856                              | .001051                                     | .1513   | 153           | 99.21              | .0576                              | .0005805                                    | .08359  |
| 104           | 81.80              | .0847                              | .001035                                     | .1490   | 154           | 99.54              | .0572                              | .0005746                                    | .08274  |
| 105           | 82.19              | .0839                              | .001020                                     | .1468   | 155           | 99.86              | .0568                              | .0005687                                    | .08189  |
| 106           | 82.58              | .0831                              | .001006                                     | .1448   | 156           | 100.18             | .0565                              | .0005624                                    | .08121  |
| 107           | 82.97              | .0824                              | .000992                                     | .1429   | 157           | 100.50             | .0561                              | .0005562                                    | .08038  |
| 108           | 83.35              | .0816                              | .000979                                     | .1409   | 158           | 100.82             | .0558                              | .0005504                                    | .07968  |
| 109           | 83.74              | .0809                              | .000966                                     | .1391   | 159           | 101.14             | .0554                              | .0005447                                    | .07888  |
| 110           | 84.12              | .0801                              | .000952                                     | .1370   | 160           | 101.46             | .0551                              | .0005430                                    | .07819  |
| 111           | 84.50              | .0794                              | .000939                                     | .1352   | 161           | 101.77             | .0547                              | .0005374                                    | .07738  |
| 112           | 84.88              | .0787                              | .000927                                     | .1334   | 162           | 102.09             | .0544                              | .0005328                                    | .07672  |
| 113           | 85.26              | .0780                              | .000914                                     | .1316   | 163           | 102.40             | .0541                              | .0005283                                    | .07607  |
| 114           | 85.64              | .0773                              | .000902                                     | .1298   | 164           | 102.72             | .0537                              | .0005227                                    | .07526  |
| 115           | 86.01              | .0766                              | .000890                                     | .1281   | 165           | 103.03             | .0534                              | .0005182                                    | .07462  |
| 116           | 86.39              | .0760                              | .000879                                     | .1265   | 166           | 103.34             | .0531                              | .0005138                                    | .07398  |
| 117           | 86.76              | .0753                              | .000867                                     | .1248   | 167           | 103.65             | .0528                              | .0005094                                    | .07335  |
| 118           | 87.13              | .0747                              | .000857                                     | .1234   | 168           | 103.96             | .0524                              | .0005040                                    | .07257  |
| 119           | 87.50              | .0741                              | .000848                                     | .1221   | 169           | 104.27             | .0521                              | .0004996                                    | .07194  |
| 120           | 87.86              | .0734                              | .000835                                     | .1202   | 170           | 104.58             | .0518                              | .0004953                                    | .07132  |
| 121           | 88.23              | .0728                              | .000825                                     | .1188   | 171           | 104.89             | .0515                              | .0004911                                    | .07071  |
| 122           | 88.59              | .0722                              | .000814                                     | .1172   | 172           | 105.19             | .0512                              | .0004867                                    | .07008  |
| 123           | 88.95              | .0716                              | .000804                                     | .1157   | 173           | 105.50             | .0509                              | .0004824                                    | .06946  |
| 124           | 89.31              | .0711                              | .000796                                     | .1146   | 174           | 105.80             | .0506                              | .0004782                                    | .06886  |
| 125           | 89.67              | .0705                              | .000786                                     | .1131   | 175           | 106.11             | .0503                              | .0004740                                    | .06825  |
| 126           | 90.03              | .0699                              | .000776                                     | .1117   | 176           | 106.41             | .0501                              | .0004708                                    | .06779  |
| 127           | 90.39              | .0694                              | .000767                                     | .1104   | 177           | 106.71             | .0498                              | .0004666                                    | .06719  |
| 128           | 90.74              | .0688                              | .000758                                     | .1091   | 178           | 107.01             | .0495                              | .0004625                                    | .06660  |
| 129           | 91.10              | .0683                              | .000749                                     | .1078   | 179           | 107.31             | .0492                              | .0004584                                    | .06600  |
| 130           | 91.45              | .0678                              | .0007413                                    | .10674  | 180           | 107.61             | .0489                              | .0004544                                    | .06543  |
| 131           | 91.80              | .0673                              | .0007331                                    | .10556  | 181           | 107.91             | .0487                              | .0004513                                    | .06498  |
| 132           | 92.15              | .0668                              | .0007249                                    | .10438  | 182           | 108.21             | .0484                              | .0004472                                    | .06439  |
| 133           | 92.50              | .0663                              | .0007167                                    | .10320  | 183           | 108.50             | .0481                              | .0004433                                    | .06383  |
| 134           | 92.85              | .0658                              | .0007086                                    | .10203  | 184           | 108.80             | .0479                              | .0004402                                    | .06338  |
| 135           | 93.19              | .0653                              | .0007007                                    | .10090  | 185           | 109.10             | .0476                              | .0004362                                    | .06281  |
| 136           | 93.54              | .0648                              | .0006926                                    | .09973  | 186           | 109.39             | .0474                              | .0004322                                    | .06238  |
| 137           | 93.88              | .0643                              | .0006849                                    | .09862  | 187           | 109.68             | .0471                              | .0004284                                    | .06183  |
| 138           | 94.22              | .0639                              | .0006780                                    | .09763  | 188           | 109.98             | .0469                              | .0004264                                    | .06140  |
| 139           | 94.56              | .0634                              | .0006704                                    | .09653  | 189           | 110.27             | .0466                              | .0004225                                    | .06084  |
| 140           | 94.90              | .0629                              | .0006626                                    | .09541  | 190           | 110.56             | .0464                              | .0004196                                    | .06042  |
| 141           | 95.24              | .0625                              | .0006552                                    | .09449  | 191           | 110.85             | .0461                              | .0004158                                    | .05987  |
| 142           | 95.58              | .0621                              | .0006497                                    | .09356  | 192           | 111.14             | .0459                              | .0004129                                    | .05945  |
| 143           | 95.91              | .0616                              | .0006422                                    | .09247  | 193           | 111.43             | .0456                              | .0004082                                    | .05892  |
| 144           | 96.25              | .0612                              | .0006358                                    | .09155  | 194           | 111.72             | .0454                              | .0004063                                    | .05850  |
| 145           | 96.58              | .0608                              | .0006293                                    | .09064  | 195           | 112.01             | .0452                              | .0004035                                    | .05810  |
| 146           | 96.92              | .0604                              | .0006231                                    | .08972  | 196           | 112.29             | .0449                              | .0003998                                    | .05757  |
| 147           | 97.25              | .0599                              | .0006159                                    | .08883  | 197           | 112.58             | .0447                              | .0003970                                    | .05716  |
| 148           | 97.58              | .0595                              | .0006097                                    | .08779  | 198           | 112.86             | .0445                              | .0003942                                    | .05676  |
| 149           | 97.91              | .0591                              | .0006036                                    | .08691  | 199           | 113.15             | .0443                              | .0003915                                    | .05637  |
| 150           | 98.23              | .0587                              | .0005975                                    | .08604  | 200           | 113.43             | .0440                              | .0003879                                    | .05586  |

| Head in Feet. | Velocity due Head. | Cubic Feet per Second to one H. P. | Section of Stream in Square Feet to 1 H. P. | Section of Stream in Square Inches to 1 H. P. | Head in Feet. | Velocity due Head. | Cubic Feet per Second to one H. P. | Section of Stream in Square Feet to 1 H. P. | Section of Stream in Square Inches to 1 H. P. |
|---------------|--------------------|------------------------------------|---|---|---------------|--------------------|------------------------------------|---|---|
| 201           | 113.72             | .0438                              | .00038515                                   | .055461                                       | 251           | 127.08             | .03513                             | .00027644                                   | .039807                                       |
| 202           | 114.00             | .0436                              | .00038245                                   | .055072                                       | 252           | 127.33             | .03499                             | .00027478                                   | .039568                                       |
| 203           | 114.28             | .0434                              | .00037976                                   | .054685                                       | 253           | 127.58             | .03485                             | .00027316                                   | .039335                                       |
| 204           | 114.56             | .0432                              | .00037709                                   | .054300                                       | 254           | 127.83             | .03471                             | .00027153                                   | .039100                                       |
| 205           | 114.84             | .0430                              | .00037443                                   | .053917                                       | 255           | 128.08             | .03458                             | .00026998                                   | .038877                                       |
| 206           | 115.12             | .0428                              | .00037178                                   | .053536                                       | 256           | 128.33             | .03444                             | .00026837                                   | .038645                                       |
| 207           | 115.40             | .0426                              | .00036915                                   | .053157                                       | 257           | 128.58             | .03431                             | .00026683                                   | .038423                                       |
| 208           | 115.68             | .0423                              | .00036656                                   | .052785                                       | 258           | 128.83             | .03418                             | .00026531                                   | .038204                                       |
| 209           | 115.96             | .0421                              | .00036395                                   | .052429                                       | 259           | 129.08             | .03404                             | .00026371                                   | .037974                                       |
| 210           | 116.23             | .0419                              | .00036149                                   | .052079                                       | 260           | 129.33             | .03391                             | .00026219                                   | .037755                                       |
| 211           | 116.51             | .0417                              | .00035790                                   | .051537                                       | 261           | 129.58             | .03378                             | .00026061                                   | .037527                                       |
| 212           | 116.79             | .0415                              | .00035533                                   | .051167                                       | 262           | 129.83             | .03365                             | .00025918                                   | .037321                                       |
| 213           | 117.06             | .0413                              | .00035281                                   | .050804                                       | 263           | 130.08             | .03353                             | .00025776                                   | .037117                                       |
| 214           | 117.34             | .0412                              | .00035111                                   | .050559                                       | 264           | 130.32             | .03340                             | .00025629                                   | .036905                                       |
| 215           | 117.61             | .0410                              | .00034862                                   | .050186                                       | 265           | 130.57             | .03327                             | .00025480                                   | .036691                                       |
| 216           | 117.88             | .0408                              | .00034611                                   | .049839                                       | 266           | 130.82             | .03315                             | .00025340                                   | .036489                                       |
| 217           | 118.15             | .0406                              | .00034363                                   | .049482                                       | 267           | 131.06             | .03302                             | .00025194                                   | .036279                                       |
| 218           | 118.43             | .0404                              | .00034112                                   | .049121                                       | 268           | 131.31             | .03290                             | .00025055                                   | .036079                                       |
| 219           | 118.70             | .0402                              | .00033866                                   | .048767                                       | 269           | 131.55             | .03278                             | .00024918                                   | .035881                                       |
| 220           | 118.97             | .0400                              | .00033621                                   | .048414                                       | 270           | 131.80             | .03266                             | .00024779                                   | .035681                                       |
| 221           | 119.24             | .0399                              | .00033461                                   | .048183                                       | 271           | 132.04             | .03254                             | .00024644                                   | .035487                                       |
| 222           | 119.51             | .0397                              | .00033218                                   | .047833                                       | 272           | 132.28             | .03242                             | .00024508                                   | .035291                                       |
| 223           | 119.78             | .0395                              | .00032977                                   | .047486                                       | 273           | 132.53             | .03230                             | .00024371                                   | .035094                                       |
| 224           | 120.05             | .0393                              | .00032736                                   | .047139                                       | 274           | 132.77             | .03218                             | .00024237                                   | .034901                                       |
| 225           | 120.31             | .0391                              | .00032499                                   | .046798                                       | 275           | 133.01             | .03206                             | .00024103                                   | .034708                                       |
| 226           | 120.58             | .0390                              | .00032243                                   | .046573                                       | 276           | 133.25             | .03195                             | .00023977                                   | .034526                                       |
| 227           | 120.85             | .0388                              | .00032105                                   | .046231                                       | 277           | 133.49             | .03183                             | .00023822                                   | .034303                                       |
| 228           | 121.11             | .0386                              | .00031871                                   | .045894                                       | 278           | 133.74             | .03172                             | .00023717                                   | .034152                                       |
| 229           | 121.38             | .0385                              | .00031710                                   | .045662                                       | 279           | 133.98             | .03160                             | .00023585                                   | .033962                                       |
| 230           | 121.64             | .0383                              | .00031486                                   | .045339                                       | 280           | 134.22             | .03149                             | .00023461                                   | .033783                                       |
| 231           | 121.91             | .0381                              | .00031252                                   | .045002                                       | 281           | 134.46             | .03138                             | .00023337                                   | .033605                                       |
| 232           | 122.17             | .0380                              | .00031104                                   | .044789                                       | 282           | 134.69             | .03127                             | .00023223                                   | .033441                                       |
| 233           | 122.43             | .0378                              | .00030874                                   | .044458                                       | 283           | 134.93             | .03116                             | .00023083                                   | .033253                                       |
| 234           | 122.70             | .0376                              | .00030643                                   | .044125                                       | 284           | 135.17             | .03105                             | .00022971                                   | .033078                                       |
| 235           | 122.96             | .0375                              | .00030497                                   | .043915                                       | 285           | 135.41             | .03094                             | .00022849                                   | .032902                                       |
| 236           | 123.22             | .0373                              | .00030271                                   | .043590                                       | 286           | 135.65             | .03083                             | .00022727                                   | .032726                                       |
| 237           | 123.48             | .0372                              | .00030126                                   | .043381                                       | 287           | 135.88             | .03072                             | .00022608                                   | .032555                                       |
| 238           | 123.74             | .0370                              | .00029901                                   | .043057                                       | 288           | 136.12             | .03062                             | .00022494                                   | .032391                                       |
| 239           | 124.00             | .0368                              | .00029677                                   | .042734                                       | 289           | 136.36             | .03051                             | .00022374                                   | .032218                                       |
| 240           | 124.26             | .0367                              | .00029534                                   | .042528                                       | 290           | 136.59             | .03040                             | .00022257                                   | .032050                                       |
| 241           | 124.52             | .0365                              | .00029312                                   | .042209                                       | 291           | 136.83             | .03030                             | .00022144                                   | .031887                                       |
| 242           | 124.78             | .0364                              | .00029171                                   | .042008                                       | 292           | 137.06             | .03020                             | .00022034                                   | .031728                                       |
| 243           | 125.03             | .0362                              | .00028953                                   | .041692                                       | 293           | 137.30             | .03009                             | .00021908                                   | .031547                                       |
| 244           | 125.29             | .0361                              | .00028813                                   | .041490                                       | 294           | 137.53             | .02999                             | .00021807                                   | .031402                                       |
| 245           | 125.55             | .0359                              | .00028594                                   | .041175                                       | 295           | 137.76             | .02989                             | .00021697                                   | .031243                                       |
| 246           | 125.80             | .0358                              | .00028457                                   | .040978                                       | 296           | 138.00             | .02979                             | .00021586                                   | .031083                                       |
| 247           | 126.06             | .0357                              | .00028319                                   | .040779                                       | 297           | 138.23             | .02969                             | .00021478                                   | .030916                                       |
| 248           | 126.31             | .0355                              | .00028105                                   | .040471                                       | 298           | 138.46             | .02959                             | .00021370                                   | .030772                                       |
| 249           | 126.57             | .0354                              | .00027968                                   | .040273                                       | 299           | 138.69             | .02949                             | .00021263                                   | .030618                                       |
| 250           | 126.82             | .0352                              | .00027811                                   | .040047                                       | 300           | 138.92             | .02939                             | .00021154                                   | .030468                                       |



| Head in Feet. | Velocity due Head. | Cubic Feet per Second to one H. P. | Section of Stream in Square Feet to 1 H. P. | Section of Stream in Square Inches to 1 H. P. | Head in Feet. | Velocity due Head. | Cubic Feet per Second to one H. P. | Section of Stream in Square Feet to 1 H. P. | Section of Stream in Square Inches to 1 H. P. |
|---------------|--------------------|------------------------------------|---|---|---------------|--------------------|------------------------------------|---|---|
| 301           | 139.16             | .029297                            | .00021047                                   | .030807                                       | 351           | 150.27             | .025124                            | .00016719                                   | .024075                                       |
| 302           | 139.39             | .029200                            | .00020948                                   | .030165                                       | 352           | 150.49             | .025052                            | .00016646                                   | .023970                                       |
| 303           | 139.62             | .029104                            | .00020845                                   | .030016                                       | 353           | 150.70             | .024981                            | .00016570                                   | .023860                                       |
| 304           | 139.85             | .029008                            | .00020742                                   | .029858                                       | 354           | 150.91             | .024911                            | .00016506                                   | .023768                                       |
| 305           | 140.08             | .028913                            | .00020640                                   | .029721                                       | 355           | 151.13             | .024841                            | .00016436                                   | .023667                                       |
| 306           | 140.31             | .028819                            | .00020539                                   | .029576                                       | 356           | 151.34             | .024771                            | .00016367                                   | .023568                                       |
| 307           | 140.54             | .028725                            | .00020439                                   | .029432                                       | 357           | 151.55             | .024702                            | .00016299                                   | .023470                                       |
| 308           | 140.77             | .028631                            | .00020338                                   | .029286                                       | 358           | 151.76             | .024633                            | .00016231                                   | .023372                                       |
| 309           | 141.00             | .028539                            | .00020240                                   | .029145                                       | 359           | 151.98             | .024564                            | .00016162                                   | .023273                                       |
| 310           | 141.22             | .028447                            | .00020143                                   | .029035                                       | 360           | 152.19             | .024496                            | .00016095                                   | .023176                                       |
| 311           | 141.45             | .028355                            | .00020046                                   | .028866                                       | 361           | 152.40             | .024428                            | .00016028                                   | .023083                                       |
| 312           | 141.68             | .028264                            | .00019949                                   | .028728                                       | 362           | 152.61             | .024360                            | .00015962                                   | .022985                                       |
| 313           | 141.90             | .028174                            | .00019854                                   | .028589                                       | 363           | 152.82             | .024293                            | .00015896                                   | .022890                                       |
| 314           | 142.13             | .028084                            | .00019759                                   | .028452                                       | 364           | 153.03             | .024226                            | .00015830                                   | .022795                                       |
| 315           | 142.36             | .027995                            | .00019665                                   | .028317                                       | 365           | 153.24             | .024160                            | .00015766                                   | .022703                                       |
| 316           | 142.58             | .027907                            | .00019572                                   | .028183                                       | 366           | 153.45             | .024094                            | .00015701                                   | .022609                                       |
| 317           | 142.81             | .027819                            | .00019479                                   | .028049                                       | 367           | 153.66             | .024028                            | .00015637                                   | .022517                                       |
| 318           | 143.03             | .027731                            | .00019388                                   | .027918                                       | 368           | 153.87             | .023963                            | .00015573                                   | .022425                                       |
| 319           | 143.26             | .027644                            | .00019296                                   | .027786                                       | 369           | 154.08             | .023898                            | .00015510                                   | .022334                                       |
| 320           | 143.48             | .027558                            | .00019206                                   | .027656                                       | 370           | 154.29             | .023834                            | .00015447                                   | .022243                                       |
| 321           | 143.71             | .027472                            | .00019109                                   | .027516                                       | 371           | 154.49             | .023769                            | .00015385                                   | .022154                                       |
| 322           | 143.93             | .027387                            | .00019027                                   | .027398                                       | 372           | 154.70             | .023705                            | .00015323                                   | .022065                                       |
| 323           | 144.15             | .027302                            | .00018939                                   | .027272                                       | 373           | 154.91             | .023642                            | .00015261                                   | .021975                                       |
| 324           | 144.38             | .027217                            | .00018850                                   | .027144                                       | 374           | 155.12             | .023579                            | .00015200                                   | .021888                                       |
| 325           | 144.60             | .027134                            | .00018764                                   | .027020                                       | 375           | 155.33             | .023516                            | .00015139                                   | .021800                                       |
| 326           | 144.82             | .027050                            | .00018678                                   | .026896                                       | 376           | 155.53             | .023453                            | .00015079                                   | .021713                                       |
| 327           | 145.04             | .026968                            | .00018593                                   | .026773                                       | 377           | 155.74             | .023391                            | .00015019                                   | .021627                                       |
| 328           | 145.27             | .026886                            | .00018507                                   | .026650                                       | 378           | 155.95             | .023329                            | .00014959                                   | .021540                                       |
| 329           | 145.49             | .026804                            | .00018423                                   | .026529                                       | 379           | 156.15             | .023268                            | .00014901                                   | .021457                                       |
| 330           | 145.71             | .026723                            | .00018339                                   | .026408                                       | 380           | 156.36             | .023206                            | .00014841                                   | .021371                                       |
| 331           | 145.93             | .026642                            | .00018256                                   | .026288                                       | 381           | 156.56             | .023145                            | .00014783                                   | .021287                                       |
| 332           | 146.15             | .026562                            | .00018174                                   | .026170                                       | 382           | 156.77             | .023085                            | .00014725                                   | .021204                                       |
| 333           | 146.37             | .026482                            | .00018092                                   | .026052                                       | 383           | 156.97             | .023025                            | .00014668                                   | .021121                                       |
| 334           | 146.59             | .026403                            | .00018011                                   | .025935                                       | 384           | 157.18             | .022965                            | .00014610                                   | .021038                                       |
| 335           | 146.81             | .026324                            | .00017931                                   | .025820                                       | 385           | 157.38             | .022905                            | .00014553                                   | .020956                                       |
| 336           | 147.03             | .026245                            | .00017853                                   | .025693                                       | 386           | 157.59             | .022846                            | .00014497                                   | .020875                                       |
| 337           | 147.25             | .026168                            | .00017771                                   | .025590                                       | 387           | 157.79             | .022787                            | .00014441                                   | .020795                                       |
| 338           | 147.46             | .026090                            | .00017692                                   | .025476                                       | 388           | 157.99             | .022728                            | .00014385                                   | .020714                                       |
| 339           | 147.68             | .026013                            | .00017614                                   | .025364                                       | 389           | 158.20             | .022669                            | .00014329                                   | .020633                                       |
| 340           | 147.90             | .025937                            | .00017536                                   | .025251                                       | 390           | 158.40             | .022611                            | .00014274                                   | .020554                                       |
| 341           | 148.12             | .025861                            | .00017459                                   | .025140                                       | 391           | 158.60             | .022554                            | .00014220                                   | .020476                                       |
| 342           | 148.33             | .025781                            | .00017383                                   | .025032                                       | 392           | 158.81             | .022496                            | .00014165                                   | .020397                                       |
| 343           | 148.55             | .025710                            | .00017307                                   | .024922                                       | 393           | 159.01             | .022439                            | .00014111                                   | .020319                                       |
| 344           | 148.77             | .025635                            | .00017231                                   | .024812                                       | 394           | 159.21             | .022382                            | .00014058                                   | .020243                                       |
| 345           | 148.98             | .025561                            | .00017157                                   | .024706                                       | 395           | 159.41             | .022325                            | .00014004                                   | .020165                                       |
| 346           | 149.20             | .025487                            | .00017082                                   | .024598                                       | 396           | 159.62             | .022269                            | .00013951                                   | .020089                                       |
| 347           | 149.41             | .025413                            | .00017008                                   | .024491                                       | 397           | 159.82             | .022213                            | .00013898                                   | .020013                                       |
| 348           | 149.63             | .025340                            | .00016928                                   | .024376                                       | 398           | 160.02             | .022157                            | .00013846                                   | .019938                                       |
| 349           | 149.85             | .025268                            | .00016862                                   | .024281                                       | 399           | 160.22             | .022101                            | .00013794                                   | .019863                                       |
| 350           | 150.06             | .025196                            | .00016790                                   | .024177                                       | 400           | 150.42             | .022046                            | .00013742                                   | .019788                                       |

| Head in Feet. | Velocity due Head. | Cubic Feet per Second to one H. P. | Section of Stream in Square Feet to 1 H. P. | Section of Stream in Square Inches to 1 H. P. | Head in Feet. | Velocity due Head. | Cubic Feet per Second to one H. P. | Section of Stream in Square Feet to 1 H. P. | Section of Stream in Square Inches to 1 H. P. |
|---------------|--------------------|------------------------------------|---|---|---------------|--------------------|------------------------------------|---|---|
| 401           | 160.62             | .021991                            | .00013691                                   | .019715                                       | 451           | 170.34             | .019553                            | .00011478                                   | .016528                                       |
| 402           | 160.82             | .021936                            | .00013640                                   | .019641                                       | 452           | 170.53             | .019510                            | .00011440                                   | .016473                                       |
| 403           | 161.02             | .021882                            | .00013589                                   | .019568                                       | 453           | 170.72             | .019467                            | .00011402                                   | .016418                                       |
| 404           | 161.22             | .021828                            | .00013539                                   | .019496                                       | 454           | 170.91             | .019424                            | .00011365                                   | .016365                                       |
| 405           | 161.42             | .021774                            | .00013489                                   | .019424                                       | 455           | 171.09             | .019381                            | .00011327                                   | .016310                                       |
| 406           | 161.62             | .021720                            | .00013438                                   | .019350                                       | 456           | 171.28             | .019339                            | .00011290                                   | .016257                                       |
| 407           | 161.82             | .021667                            | .00013389                                   | .019280                                       | 457           | 171.47             | .019296                            | .00011253                                   | .016204                                       |
| 408           | 162.02             | .021614                            | .00013340                                   | .019209                                       | 458           | 171.66             | .019254                            | .00011216                                   | .016151                                       |
| 409           | 162.21             | .021561                            | .00013291                                   | .019139                                       | 459           | 171.84             | .019212                            | .00011180                                   | .016099                                       |
| 410           | 162.41             | .021508                            | .00013243                                   | .019069                                       | 460           | 172.03             | .019170                            | .00011143                                   | .016045                                       |
| 411           | 162.61             | .021456                            | .00013194                                   | .018999                                       | 461           | 172.22             | .019129                            | .00011107                                   | .015994                                       |
| 412           | 162.81             | .021404                            | .00013146                                   | .018930                                       | 462           | 172.40             | .019087                            | .00011071                                   | .015942                                       |
| 413           | 163.01             | .021352                            | .00013098                                   | .018861                                       | 463           | 172.59             | .019046                            | .00011035                                   | .015890                                       |
| 414           | 163.20             | .021301                            | .00013052                                   | .018794                                       | 464           | 172.78             | .019005                            | .00010999                                   | .015838                                       |
| 415           | 163.40             | .021249                            | .00013004                                   | .018725                                       | 465           | 172.96             | .018964                            | .00010964                                   | .015788                                       |
| 416           | 163.60             | .021198                            | .00012957                                   | .018658                                       | 466           | 173.15             | .018924                            | .00010929                                   | .015737                                       |
| 417           | 163.79             | .021147                            | .00012911                                   | .018591                                       | 467           | 173.34             | .018883                            | .00010893                                   | .015685                                       |
| 418           | 163.99             | .021097                            | .00012864                                   | .018524                                       | 468           | 173.52             | .018843                            | .00010859                                   | .015636                                       |
| 419           | 164.19             | .021046                            | .00012818                                   | .018457                                       | 469           | 173.71             | .018803                            | .00010824                                   | .015586                                       |
| 420           | 164.38             | .020996                            | .00012772                                   | .018391                                       | 470           | 173.89             | .018763                            | .00010790                                   | .015537                                       |
| 421           | 164.58             | .020946                            | .00012726                                   | .018325                                       | 471           | 174.08             | .018723                            | .00010755                                   | .015487                                       |
| 422           | 164.77             | .020897                            | .00012682                                   | .018262                                       | 472           | 174.26             | .018683                            | .00010721                                   | .015438                                       |
| 423           | 164.97             | .020847                            | .00012633                                   | .018195                                       | 473           | 174.45             | .018644                            | .00010687                                   | .015389                                       |
| 424           | 165.16             | .020798                            | .00012592                                   | .018132                                       | 474           | 174.63             | .018604                            | .00010653                                   | .015340                                       |
| 425           | 165.36             | .020749                            | .00012547                                   | .018067                                       | 475           | 174.81             | .018565                            | .00010620                                   | .015292                                       |
| 426           | 165.55             | .020700                            | .00012503                                   | .018004                                       | 476           | 175.00             | .018526                            | .00010583                                   | .015243                                       |
| 427           | 165.75             | .020652                            | .00012459                                   | .017940                                       | 477           | 175.18             | .018487                            | .00010553                                   | .015196                                       |
| 428           | 165.94             | .020604                            | .00012416                                   | .017879                                       | 478           | 175.36             | .018449                            | .00010520                                   | .015148                                       |
| 429           | 166.13             | .020556                            | .00012373                                   | .017817                                       | 479           | 175.55             | .018410                            | .00010487                                   | .015101                                       |
| 430           | 166.33             | .020508                            | .00012329                                   | .017753                                       | 480           | 175.73             | .018372                            | .00010454                                   | .015053                                       |
| 431           | 166.52             | .020460                            | .00012286                                   | .017691                                       | 481           | 175.91             | .018333                            | .00010421                                   | .015006                                       |
| 432           | 166.71             | .020413                            | .00012244                                   | .017631                                       | 482           | 176.10             | .018295                            | .00010388                                   | .014958                                       |
| 433           | 166.91             | .020366                            | .00012201                                   | .017569                                       | 483           | 176.28             | .018258                            | .00010357                                   | .014914                                       |
| 434           | 167.10             | .020319                            | .00012159                                   | .017508                                       | 484           | 176.46             | .018220                            | .00010325                                   | .014868                                       |
| 435           | 167.29             | .020272                            | .00012117                                   | .017448                                       | 485           | 176.64             | .018182                            | .00010293                                   | .014821                                       |
| 436           | 167.48             | .020226                            | .00012076                                   | .017389                                       | 486           | 176.83             | .018145                            | .00010261                                   | .014775                                       |
| 437           | 167.67             | .020179                            | .00012034                                   | .017328                                       | 487           | 177.01             | .018108                            | .00010229                                   | .014729                                       |
| 438           | 167.87             | .020133                            | .00011993                                   | .017269                                       | 488           | 177.19             | .018070                            | .00010198                                   | .014685                                       |
| 439           | 168.06             | .020087                            | .00011952                                   | .017210                                       | 489           | 177.37             | .018033                            | .00010166                                   | .014639                                       |
| 440           | 168.25             | .020042                            | .00011912                                   | .017153                                       | 490           | 177.55             | .017996                            | .00010135                                   | .014594                                       |
| 441           | 168.44             | .019996                            | .00011871                                   | .017094                                       | 491           | 177.73             | .017960                            | .00010105                                   | .014551                                       |
| 442           | 168.63             | .019951                            | .00011831                                   | .017036                                       | 492           | 177.91             | .017924                            | .00010074                                   | .014506                                       |
| 443           | 168.82             | .019906                            | .00011791                                   | .016979                                       | 493           | 178.10             | .017887                            | .00010043                                   | .014461                                       |
| 444           | 169.01             | .019861                            | .00011751                                   | .016921                                       | 494           | 178.28             | .017851                            | .00010012                                   | .014417                                       |
| 445           | 169.20             | .019817                            | .00011712                                   | .016865                                       | 495           | 178.46             | .017815                            | .00009982                                   | .014374                                       |
| 446           | 169.39             | .019772                            | .00011672                                   | .016807                                       | 496           | 178.64             | .017779                            | .00009952                                   | .014330                                       |
| 447           | 169.58             | .019728                            | .00011633                                   | .016751                                       | 497           | 178.82             | .017743                            | .00009922                                   | .014287                                       |
| 448           | 169.77             | .019684                            | .00011594                                   | .016695                                       | 498           | 179.00             | .017708                            | .00009892                                   | .014244                                       |
| 449           | 169.96             | .019640                            | .00011555                                   | .016639                                       | 499           | 179.18             | .017672                            | .00009862                                   | .014201                                       |
| 450           | 170.15             | .019596                            | .00011516                                   | .016583                                       | 500           | 179.35             | .017637                            | .00009833                                   | .014159                                       |

| Dia.<br>in<br>inch. | Circ'm<br>in<br>ft. in. | Area in<br>square<br>inch. | Dia.<br>in<br>inch. | Circ'm<br>in<br>ft. in. | Area<br>in sq.<br>inch. | Dia.<br>in<br>inch. | Circ'm<br>in<br>ft. in. | Area in<br>Square<br>feet. |
|---------------------|-------------------------|----------------------------|---------------------|-------------------------|-------------------------|---------------------|-------------------------|----------------------------|
| $\frac{1}{15}$      | .196                    | .0030                      | 5                   | 1 3 $\frac{3}{8}$       | 19.635                  | 10 $\frac{7}{8}$    | 2 10 $\frac{1}{2}$      | .6499                      |
| $\frac{1}{8}$       | .392                    | .0122                      | 5 $\frac{1}{8}$     | 1 4 $\frac{1}{8}$       | 20.629                  | 11                  | 2 10 $\frac{1}{2}$      | .6652                      |
| $\frac{3}{15}$      | .589                    | .0276                      | 5 $\frac{1}{4}$     | 1 4 $\frac{1}{2}$       | 21.647                  | 11 $\frac{1}{8}$    | 2 10 $\frac{7}{8}$      | .6804                      |
| $\frac{4}{15}$      | .785                    | .0490                      | 5 $\frac{3}{8}$     | 1 4 $\frac{3}{4}$       | 22.690                  | 11 $\frac{1}{4}$    | 2 11 $\frac{1}{4}$      | .6958                      |
| $\frac{5}{15}$      | .981                    | .0767                      | 5 $\frac{1}{2}$     | 1 5 $\frac{1}{4}$       | 23.758                  | 11 $\frac{3}{8}$    | 2 11 $\frac{3}{4}$      | .7143                      |
| $\frac{3}{8}$       | 1.178                   | .1104                      | 5 $\frac{5}{8}$     | 1 5 $\frac{3}{8}$       | 24.850                  | 11 $\frac{1}{2}$    | 3 0 $\frac{1}{8}$       | .7270                      |
| $\frac{7}{16}$      | 1.374                   | .1563                      | 5 $\frac{7}{8}$     | 1 6                     | 25.967                  | 11 $\frac{3}{4}$    | 3 0 $\frac{1}{2}$       | .7429                      |
| $\frac{1}{2}$       | 1.570                   | .1963                      | 6                   | 1 6 $\frac{3}{8}$       | 27.108                  | 11 $\frac{3}{4}$    | 3 0 $\frac{3}{4}$       | .7590                      |
| $\frac{5}{8}$       | 1.767                   | .2485                      | 6 $\frac{1}{8}$     | 1 6 $\frac{3}{4}$       | 28.274                  | 11 $\frac{7}{8}$    | 3 1 $\frac{1}{4}$       | .7752                      |
| $\frac{9}{16}$      | 1.963                   | .3068                      | 6 $\frac{1}{4}$     | 1 7 $\frac{1}{4}$       | 29.464                  | 12                  | 3 1 $\frac{1}{2}$       | .7916                      |
| $\frac{1}{10}$      | 2.159                   | .3712                      | 6 $\frac{1}{2}$     | 1 7 $\frac{1}{2}$       | 30.679                  | 12 $\frac{1}{4}$    | 3 2                     | .8082                      |
| $\frac{3}{4}$       | 2.356                   | .4417                      | 6 $\frac{3}{4}$     | 1 8                     | 31.919                  | 12 $\frac{1}{2}$    | 3 2 $\frac{1}{2}$       | .8250                      |
| $\frac{1}{8}$       | 2.552                   | .5185                      | 6 $\frac{7}{8}$     | 1 8 $\frac{3}{8}$       | 33.183                  | 12 $\frac{3}{8}$    | 3 2 $\frac{3}{8}$       | .8419                      |
| $\frac{7}{8}$       | 2.748                   | .6013                      | 6 $\frac{7}{8}$     | 1 8 $\frac{3}{4}$       | 34.471                  | 12 $\frac{1}{2}$    | 3 3 $\frac{1}{4}$       | .8590                      |
| $\frac{1}{16}$      | 2.945                   | .6903                      | 6 $\frac{7}{8}$     | 1 9 $\frac{1}{2}$       | 35.784                  | 12 $\frac{3}{4}$    | 3 3 $\frac{3}{8}$       | .8762                      |
| 1                   | 3 $\frac{1}{8}$         | .7854                      | 6 $\frac{7}{8}$     | 1 9 $\frac{1}{2}$       | 37.122                  | 12 $\frac{3}{4}$    | 3 4                     | .8937                      |
| $1\frac{1}{8}$      | 3 $\frac{1}{2}$         | .9940                      | 7                   | 1 10                    | 38.484                  | 12 $\frac{7}{8}$    | 3 4 $\frac{1}{8}$       | .9113                      |
| $1\frac{1}{4}$      | 3 $\frac{3}{8}$         | 1.227                      | 7 $\frac{1}{4}$     | 1 10 $\frac{3}{8}$      | 39.871                  | 13                  | 3 4 $\frac{3}{8}$       | .9291                      |
| $1\frac{3}{8}$      | 4 $\frac{1}{4}$         | 1.484                      | 7 $\frac{1}{4}$     | 1 10 $\frac{3}{4}$      | 41.282                  | 13 $\frac{1}{8}$    | 3 5 $\frac{1}{4}$       | .9470                      |
| $1\frac{1}{2}$      | 4 $\frac{3}{8}$         | 1.767                      | 7 $\frac{1}{2}$     | 1 11 $\frac{1}{8}$      | 42.718                  | 13 $\frac{1}{4}$    | 3 5 $\frac{3}{8}$       | .9642                      |
| $1\frac{3}{8}$      | 4 $\frac{7}{8}$         | 2.073                      | 7 $\frac{1}{2}$     | 1 11 $\frac{1}{4}$      | 44.178                  | 13 $\frac{3}{8}$    | 3 6                     | .9835                      |
| $1\frac{5}{8}$      | 5 $\frac{1}{8}$         | 2.405                      | 7 $\frac{3}{4}$     | 1 11 $\frac{3}{8}$      | 45.663                  | 13 $\frac{1}{2}$    | 3 6 $\frac{3}{8}$       | 1.0019                     |
| $1\frac{7}{8}$      | 5 $\frac{1}{2}$         | 2.761                      | 7 $\frac{3}{4}$     | 2 0 $\frac{3}{8}$       | 47.173                  | 13 $\frac{3}{4}$    | 3 6 $\frac{3}{4}$       | 1.0206                     |
| 2                   | 6 $\frac{1}{4}$         | 3.141                      | 7 $\frac{7}{8}$     | 2 0 $\frac{3}{4}$       | 48.707                  | 13 $\frac{7}{8}$    | 3 7 $\frac{1}{8}$       | 1.0294                     |
| $2\frac{1}{8}$      | 6 $\frac{3}{8}$         | 3.546                      | 8                   | 2 1 $\frac{1}{8}$       | 50.265                  | 13 $\frac{7}{8}$    | 3 7 $\frac{1}{2}$       | 1.0584                     |
| $2\frac{1}{4}$      | 7                       | 3.976                      | 8 $\frac{1}{8}$     | 2 1 $\frac{1}{4}$       | 51.848                  | 14                  | 3 7 $\frac{3}{8}$       | 1.0775                     |
| $2\frac{3}{8}$      | 7 $\frac{3}{8}$         | 4.430                      | 8 $\frac{1}{4}$     | 2 1 $\frac{3}{8}$       | 53.456                  | 14 $\frac{1}{8}$    | 3 8 $\frac{1}{8}$       | 1.0968                     |
| $2\frac{1}{2}$      | 7 $\frac{1}{2}$         | 4.908                      | 8 $\frac{1}{2}$     | 2 2 $\frac{1}{4}$       | 55.088                  | 14 $\frac{1}{4}$    | 3 8 $\frac{1}{4}$       | 1.1193                     |
| $2\frac{5}{8}$      | 8 $\frac{1}{4}$         | 5.412                      | 8 $\frac{3}{8}$     | 2 2 $\frac{3}{8}$       | 56.745                  | 14 $\frac{3}{8}$    | 3 9 $\frac{1}{8}$       | 1.1360                     |
| $2\frac{3}{4}$      | 8 $\frac{3}{8}$         | 5.939                      | 8 $\frac{5}{8}$     | 2 3                     | 58.426                  | 14 $\frac{3}{4}$    | 3 9 $\frac{1}{2}$       | 1.1569                     |
| $2\frac{7}{8}$      | 9                       | 6.491                      | 8 $\frac{7}{8}$     | 2 3 $\frac{3}{8}$       | 60.132                  | 14 $\frac{7}{8}$    | 3 9 $\frac{7}{8}$       | 1.1749                     |
| 3                   | 9 $\frac{3}{8}$         | 7.068                      | 8 $\frac{7}{8}$     | 2 3 $\frac{7}{8}$       | 61.862                  | 14 $\frac{7}{8}$    | 3 10 $\frac{1}{4}$      | 1.1961                     |
| $3\frac{1}{8}$      | 9 $\frac{3}{4}$         | 7.669                      | 9                   | 2 4 $\frac{1}{4}$       | 63.617                  | 14 $\frac{7}{8}$    | 3 10 $\frac{3}{8}$      | 1.2164                     |
| $3\frac{1}{4}$      | 10 $\frac{1}{4}$        | 8.295                      | 9 $\frac{1}{8}$     | 2 4 $\frac{3}{8}$       | 65.396                  | 15                  | 3 11 $\frac{1}{8}$      | 1.2370                     |
| $3\frac{3}{8}$      | 10 $\frac{3}{8}$        | 8.946                      | 9 $\frac{1}{4}$     | 2 5                     | 67.200                  | 15 $\frac{1}{8}$    | 3 11 $\frac{1}{4}$      | 1.2577                     |
| $3\frac{1}{2}$      | 11                      | 9.621                      | 9 $\frac{3}{8}$     | 2 5 $\frac{3}{8}$       | 69.029                  | 15 $\frac{1}{4}$    | 3 11 $\frac{3}{8}$      | 1.2785                     |
| $3\frac{5}{8}$      | 11 $\frac{3}{8}$        | 10.320                     | 9 $\frac{1}{2}$     | 2 5 $\frac{3}{4}$       | 70.882                  | 15 $\frac{3}{8}$    | 4 0 $\frac{1}{4}$       | 1.2996                     |
| $3\frac{3}{4}$      | 11 $\frac{3}{4}$        | 11.044                     | 9 $\frac{5}{8}$     | 2 6 $\frac{1}{4}$       | 72.759                  | 15 $\frac{1}{2}$    | 4 0 $\frac{3}{8}$       | 1.3208                     |
| $3\frac{7}{8}$      | 12 $\frac{1}{4}$        | 11.793                     | 9 $\frac{7}{8}$     | 2 6 $\frac{3}{8}$       | 74.662                  | 15 $\frac{3}{4}$    | 4 1                     | 1.3422                     |
| 4                   | 1 0 $\frac{1}{2}$       | 12.566                     | 9 $\frac{7}{8}$     | 2 7                     | 76.588                  | 15 $\frac{3}{4}$    | 4 1 $\frac{1}{2}$       | 1.3637                     |
| $4\frac{1}{8}$      | 1 0 $\frac{7}{8}$       | 13.364                     | 10                  | 2 7 $\frac{3}{8}$       | 78.540                  | 15 $\frac{7}{8}$    | 4 1 $\frac{7}{8}$       | 1.3855                     |
| $4\frac{1}{4}$      | 1 1 $\frac{1}{8}$       | 14.186                     | 10 $\frac{1}{8}$    | 2 7 $\frac{3}{4}$       | 80.515                  | 16                  | 4 2 $\frac{1}{4}$       | 1.4074                     |
| $4\frac{3}{8}$      | 1 1 $\frac{1}{4}$       | 15.033                     | 10 $\frac{1}{4}$    | 2 8 $\frac{1}{8}$       | 82.516                  | 16 $\frac{1}{8}$    | 4 2 $\frac{3}{8}$       | 1.4295                     |
| $4\frac{1}{2}$      | 1 2 $\frac{1}{8}$       | 15.904                     | 10 $\frac{1}{2}$    | 2 8 $\frac{1}{4}$       | 84.540                  | 16 $\frac{1}{4}$    | 4 3                     | 1.4517                     |
| $4\frac{5}{8}$      | 1 2 $\frac{1}{2}$       | 16.800                     | 10 $\frac{1}{2}$    | 2 8 $\frac{3}{8}$       | 86.590                  | 16 $\frac{3}{8}$    | 4 3 $\frac{3}{8}$       | 1.4741                     |
| $4\frac{3}{4}$      | 1 2 $\frac{3}{4}$       | 17.720                     | 10 $\frac{3}{4}$    | 2 9 $\frac{1}{8}$       | 88.664                  | 16 $\frac{1}{2}$    | 4 3 $\frac{1}{2}$       | 1.4967                     |
| $4\frac{7}{8}$      | 1 3 $\frac{1}{4}$       | 18.665                     | 10 $\frac{3}{4}$    | 2 9 $\frac{3}{4}$       | 90.762                  | 16 $\frac{3}{4}$    | 4 4 $\frac{1}{4}$       | 1.5195                     |

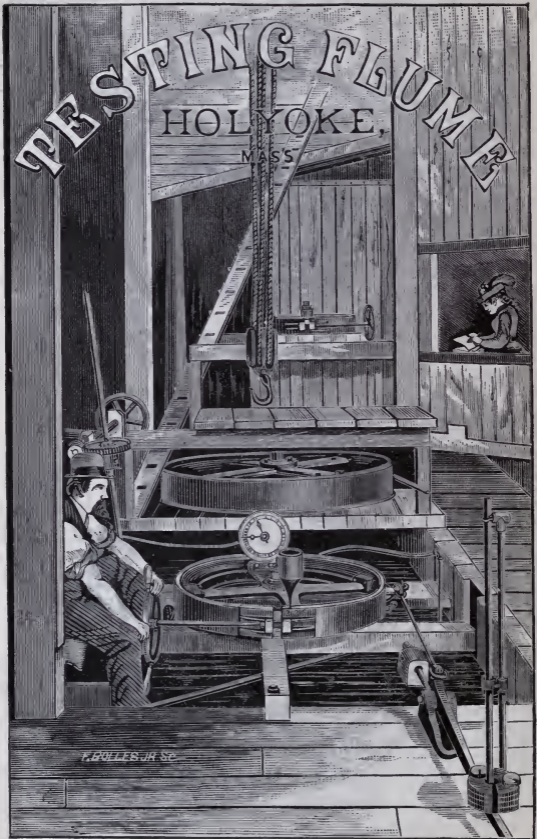
| Diam.<br>in<br>inch. | Circ'm<br>in<br>ft. in. | Area in<br>Square<br>feet. | Diam.<br>in<br>ft. in. | Circ'm<br>in<br>ft. in. | Area in<br>Square<br>feet. | Diam.<br>in<br>ft. in. | Circ'm.<br>in<br>ft. in | Area in<br>Square<br>feet. |
|----------------------|-------------------------|----------------------------|------------------------|-------------------------|----------------------------|------------------------|-------------------------|----------------------------|
| 16 $\frac{3}{8}$     | 4 4 $\frac{3}{8}$       | 1.5424                     | 22 $\frac{3}{8}$       | 5 11                    | 2.7980                     | 2 9                    | 8 7 $\frac{3}{8}$       | 5.9398                     |
| 16 $\frac{7}{8}$     | 4 5                     | 1.5655                     | 22 $\frac{7}{8}$       | 5 11 $\frac{1}{2}$      | 2.8054                     | 2 9 $\frac{1}{4}$      | 8 8 $\frac{1}{2}$       | 6.0291                     |
| 17                   | 4 5 $\frac{3}{8}$       | 1.5888                     | 22 $\frac{7}{8}$       | 5 11 $\frac{7}{8}$      | 2.8658                     | 2 9 $\frac{1}{2}$      | 8 9 $\frac{1}{4}$       | 6.1201                     |
| 17 $\frac{1}{8}$     | 4 5 $\frac{1}{2}$       | 1.6123                     | 23                     | 6 0 $\frac{1}{2}$       | 2.8903                     | 2 9 $\frac{3}{4}$      | 8 10                    | 6.2129                     |
| 17 $\frac{1}{4}$     | 4 6 $\frac{1}{8}$       | 1.6359                     | 23 $\frac{1}{8}$       | 6 0 $\frac{3}{8}$       | 2.9100                     | 2 10                   | 8 10 $\frac{1}{4}$      | 6.3051                     |
| 17 $\frac{3}{8}$     | 4 6 $\frac{1}{4}$       | 1.6597                     | 23 $\frac{1}{4}$       | 6 1                     | 2.9518                     | 2 10 $\frac{1}{4}$     | 8 11 $\frac{1}{2}$      | 6.3981                     |
| 17 $\frac{1}{2}$     | 4 6 $\frac{3}{4}$       | 1.6836                     | 23 $\frac{1}{2}$       | 6 1 $\frac{1}{2}$       | 2.9937                     | 2 10 $\frac{1}{2}$     | 9 0 $\frac{3}{8}$       | 6.4911                     |
| 17 $\frac{5}{8}$     | 4 7 $\frac{1}{8}$       | 1.7078                     | 23 $\frac{5}{8}$       | 6 1 $\frac{3}{4}$       | 3.0129                     | 2 10 $\frac{3}{4}$     | 9 1 $\frac{1}{8}$       | 6.5863                     |
| 17 $\frac{7}{8}$     | 4 7 $\frac{3}{8}$       | 1.7321                     | 23 $\frac{7}{8}$       | 6 2 $\frac{1}{4}$       | 3.0261                     | 2 11                   | 9 1 $\frac{3}{8}$       | 6.6815                     |
| 18                   | 4 8                     | 1.7566                     | 23 $\frac{7}{8}$       | 6 2 $\frac{1}{2}$       | 3.0722                     | 2 11 $\frac{1}{4}$     | 9 2 $\frac{1}{4}$       | 6.7772                     |
| 18                   | 4 8 $\frac{1}{2}$       | 1.7812                     | 23 $\frac{7}{8}$       | 6 3                     | 3.1081                     | 2 11 $\frac{1}{2}$     | 9 3 $\frac{1}{2}$       | 6.8738                     |
| 18 $\frac{1}{8}$     | 4 8 $\frac{1}{4}$       | 1.8061                     | 2 0                    | 6 3 $\frac{3}{8}$       | 3.1418                     | 2 11 $\frac{3}{4}$     | 9 4 $\frac{1}{4}$       | 6.9701                     |
| 18 $\frac{1}{4}$     | 4 9 $\frac{1}{4}$       | 1.8311                     | 2 0 $\frac{1}{4}$      | 6 4 $\frac{1}{4}$       | 3.2075                     | 3 0                    | 9 5                     | 7.0688                     |
| 18 $\frac{1}{2}$     | 4 9 $\frac{1}{2}$       | 1.8562                     | 2 0 $\frac{1}{2}$      | 6 4 $\frac{1}{2}$       | 3.2731                     | 3 0 $\frac{1}{2}$      | 9 5 $\frac{3}{8}$       | 7.1671                     |
| 18 $\frac{3}{8}$     | 4 10 $\frac{1}{8}$      | 1.8616                     | 2 0 $\frac{3}{8}$      | 6 5 $\frac{1}{8}$       | 3.3410                     | 3 0 $\frac{3}{8}$      | 9 6 $\frac{1}{8}$       | 7.2664                     |
| 18 $\frac{1}{2}$     | 4 10 $\frac{1}{4}$      | 1.9071                     | 2 1                    | 6 6 $\frac{1}{4}$       | 3.4081                     | 3 0 $\frac{1}{2}$      | 9 7 $\frac{1}{2}$       | 7.3662                     |
| 18 $\frac{5}{8}$     | 4 10 $\frac{3}{8}$      | 1.9328                     | 2 1 $\frac{1}{4}$      | 6 7 $\frac{1}{4}$       | 3.4775                     | 3 1                    | 9 8 $\frac{1}{4}$       | 7.4661                     |
| 18 $\frac{7}{8}$     | 4 11 $\frac{1}{4}$      | 1.9586                     | 2 1 $\frac{1}{2}$      | 6 8 $\frac{1}{4}$       | 3.5468                     | 3 1 $\frac{1}{4}$      | 9 9                     | 7.5671                     |
| 19                   | 4 11 $\frac{3}{8}$      | 1.9847                     | 2 1 $\frac{3}{8}$      | 6 8 $\frac{3}{8}$       | 3.6101                     | 3 1 $\frac{1}{2}$      | 9 9 $\frac{3}{8}$       | 7.6691                     |
| 19 $\frac{1}{8}$     | 5 0                     | 1.9941                     | 2 2                    | 6 9 $\frac{1}{8}$       | 3.6870                     | 3 1 $\frac{3}{4}$      | 9 10 $\frac{1}{8}$      | 7.7791                     |
| 19 $\frac{1}{4}$     | 5 0 $\frac{1}{4}$       | 2.0371                     | 2 2 $\frac{1}{4}$      | 6 10 $\frac{1}{4}$      | 3.7583                     | 3 2                    | 9 11 $\frac{1}{8}$      | 7.8681                     |
| 19 $\frac{1}{2}$     | 5 0 $\frac{1}{2}$       | 2.0637                     | 2 2 $\frac{1}{2}$      | 6 11 $\frac{1}{4}$      | 3.8302                     | 3 2 $\frac{1}{4}$      | 10 0 $\frac{1}{4}$      | 7.9791                     |
| 19 $\frac{3}{8}$     | 5 1 $\frac{1}{8}$       | 2.0904                     | 2 2 $\frac{3}{8}$      | 7 0                     | 3.9042                     | 3 2 $\frac{3}{8}$      | 10 0 $\frac{3}{8}$      | 8.0846                     |
| 19 $\frac{1}{2}$     | 5 1 $\frac{1}{4}$       | 2.1172                     | 2 3                    | 7 0 $\frac{1}{4}$       | 3.9761                     | 3 2 $\frac{1}{2}$      | 10 1 $\frac{1}{4}$      | 8.1891                     |
| 19 $\frac{5}{8}$     | 5 2                     | 2.1443                     | 2 3 $\frac{1}{4}$      | 7 1 $\frac{1}{4}$       | 4.0500                     | 3 3                    | 10 2 $\frac{1}{4}$      | 8.2951                     |
| 19 $\frac{7}{8}$     | 5 2 $\frac{1}{8}$       | 2.1716                     | 2 3 $\frac{1}{2}$      | 7 2 $\frac{1}{8}$       | 4.1241                     | 3 3 $\frac{1}{4}$      | 10 3 $\frac{1}{4}$      | 8.4026                     |
| 20                   | 5 2 $\frac{1}{4}$       | 2.1990                     | 2 3 $\frac{3}{4}$      | 7 3 $\frac{1}{4}$       | 4.2000                     | 3 3 $\frac{3}{4}$      | 10 4                    | 8.5091                     |
| 20 $\frac{1}{8}$     | 5 3 $\frac{1}{8}$       | 2.2265                     | 2 4                    | 7 3 $\frac{3}{8}$       | 4.2760                     | 3 3 $\frac{3}{4}$      | 10 4 $\frac{1}{4}$      | 8.6171                     |
| 20 $\frac{1}{4}$     | 5 3 $\frac{1}{4}$       | 2.2543                     | 2 4 $\frac{1}{4}$      | 7 4 $\frac{1}{4}$       | 4.3521                     | 3 4                    | 10 5 $\frac{1}{4}$      | 8.7269                     |
| 20 $\frac{1}{2}$     | 5 3 $\frac{1}{2}$       | 2.2822                     | 2 4 $\frac{1}{2}$      | 7 5 $\frac{1}{2}$       | 4.4302                     | 3 4 $\frac{1}{2}$      | 10 6 $\frac{1}{2}$      | 8.8361                     |
| 20 $\frac{3}{8}$     | 5 4                     | 2.3103                     | 2 4 $\frac{3}{8}$      | 7 6 $\frac{1}{4}$       | 4.5083                     | 3 4 $\frac{3}{8}$      | 10 7 $\frac{1}{4}$      | 8.9462                     |
| 20 $\frac{1}{2}$     | 5 4 $\frac{1}{4}$       | 2.3386                     | 2 5                    | 7 7                     | 4.5861                     | 3 4 $\frac{3}{4}$      | 10 8                    | 9.0561                     |
| 20 $\frac{5}{8}$     | 5 5 $\frac{1}{8}$       | 2.3670                     | 2 5 $\frac{1}{4}$      | 7 7 $\frac{1}{4}$       | 4.6665                     | 3 5                    | 10 8 $\frac{1}{4}$      | 9.1686                     |
| 20 $\frac{7}{8}$     | 5 5 $\frac{1}{4}$       | 2.3956                     | 2 5 $\frac{1}{2}$      | 7 8 $\frac{1}{4}$       | 4.7467                     | 3 5 $\frac{1}{4}$      | 10 9 $\frac{1}{4}$      | 9.2112                     |
| 21                   | 5 5 $\frac{3}{8}$       | 2.4244                     | 2 5 $\frac{3}{8}$      | 7 9 $\frac{1}{8}$       | 4.8274                     | 3 5 $\frac{3}{8}$      | 10 10 $\frac{1}{8}$     | 9.3936                     |
| 21 $\frac{1}{8}$     | 5 6                     | 2.4533                     | 2 6                    | 7 10 $\frac{1}{4}$      | 4.9081                     | 3 5 $\frac{3}{4}$      | 10 11 $\frac{1}{4}$     | 9.5061                     |
| 21 $\frac{1}{4}$     | 5 6 $\frac{1}{4}$       | 2.4824                     | 2 6 $\frac{1}{4}$      | 7 11                    | 4.9901                     | 3 6                    | 11 11 $\frac{1}{4}$     | 9.6212                     |
| 21 $\frac{1}{2}$     | 5 6 $\frac{1}{2}$       | 2.5117                     | 2 6 $\frac{1}{2}$      | 7 11 $\frac{1}{2}$      | 5.0731                     | 3 6 $\frac{1}{4}$      | 11 0 $\frac{3}{4}$      | 9.7364                     |
| 21 $\frac{3}{8}$     | 5 7 $\frac{1}{8}$       | 2.5412                     | 2 6 $\frac{3}{8}$      | 8 0 $\frac{3}{8}$       | 5.1573                     | 3 6 $\frac{3}{8}$      | 11 1 $\frac{3}{8}$      | 9.8518                     |
| 21 $\frac{1}{2}$     | 5 7 $\frac{1}{4}$       | 2.5708                     | 2 7                    | 8 1 $\frac{1}{4}$       | 5.2278                     | 3 6 $\frac{1}{2}$      | 11 2 $\frac{1}{4}$      | 9.9671                     |
| 21 $\frac{5}{8}$     | 5 8 $\frac{1}{8}$       | 2.6007                     | 2 7 $\frac{1}{4}$      | 8 2 $\frac{1}{8}$       | 5.3264                     | 3 7                    | 11 3                    | 10.084                     |
| 21 $\frac{7}{8}$     | 5 8 $\frac{1}{4}$       | 2.6306                     | 2 7 $\frac{1}{2}$      | 8 2 $\frac{1}{2}$       | 5.4112                     | 3 7 $\frac{1}{4}$      | 11 3 $\frac{3}{4}$      | 10.202                     |
| 22                   | 5 9                     | 2.6608                     | 2 7 $\frac{3}{4}$      | 8 3 $\frac{3}{4}$       | 5.4982                     | 3 7 $\frac{3}{8}$      | 11 4 $\frac{3}{8}$      | 10.320                     |
| 22 $\frac{1}{8}$     | 5 9 $\frac{1}{8}$       | 2.6691                     | 2 8                    | 8 4 $\frac{1}{8}$       | 5.5850                     | 3 7 $\frac{3}{4}$      | 11 5 $\frac{3}{8}$      | 10.439                     |
| 22 $\frac{1}{4}$     | 5 9 $\frac{1}{4}$       | 2.7016                     | 2 8 $\frac{1}{4}$      | 8 5 $\frac{1}{4}$       | 5.6729                     | 3 8                    | 11 6 $\frac{1}{4}$      | 10.559                     |
| 22 $\frac{1}{2}$     | 5 10 $\frac{1}{4}$      | 2.7224                     | 2 8 $\frac{1}{2}$      | 8 6 $\frac{1}{4}$       | 5.7601                     | 3 8 $\frac{1}{4}$      | 11 7                    | 10.679                     |
| 22 $\frac{3}{8}$     | 5 10 $\frac{3}{8}$      | 2.7632                     | 2 8 $\frac{3}{8}$      | 8 6 $\frac{3}{8}$       | 5.8491                     | 3 8 $\frac{3}{8}$      | 11 7 $\frac{3}{8}$      | 10.800                     |

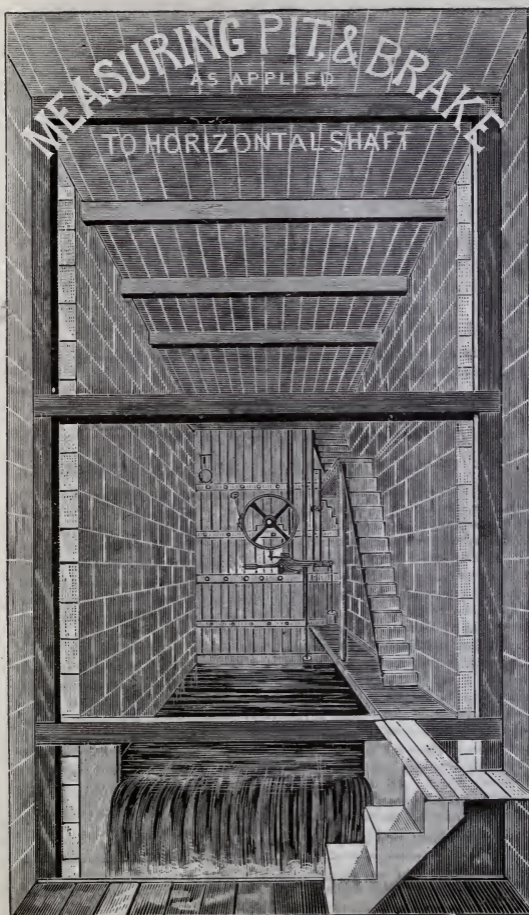
| Diam.<br>in<br>ft. in. | Circ'm<br>in<br>ft. in. | Area in<br>Square<br>feet | Diam.<br>in<br>ft. in. | Circ'm<br>in<br>ft. in. | Area in<br>Square<br>feet. | Diam<br>in<br>ft. in. | Circ'm<br>in<br>ft. in. | Area in<br>Square<br>feet. |
|------------------------|-------------------------|---------------------------|------------------------|-------------------------|----------------------------|-----------------------|-------------------------|----------------------------|
| 3 8 $\frac{1}{4}$      | 11 8 $\frac{1}{2}$      | 10.922                    | 4 8 $\frac{1}{2}$      | 14 9 $\frac{1}{2}$      | 17.411                     | 5 8 $\frac{1}{4}$     | 17 10 $\frac{3}{8}$     | 25.405                     |
| 3 9                    | 11 9 $\frac{1}{2}$      | 11.044                    | 4 8 $\frac{3}{4}$      | 14 10 $\frac{1}{4}$     | 17.565                     | 5 8 $\frac{1}{2}$     | 17 11 $\frac{1}{8}$     | 25.592                     |
| 3 9 $\frac{1}{4}$      | 11 10 $\frac{1}{8}$     | 11.167                    | 4 9                    | 14 11                   | 17.720                     | 5 8 $\frac{3}{4}$     | 17 11 $\frac{7}{8}$     | 25.779                     |
| 3 9 $\frac{1}{2}$      | 11 10 $\frac{3}{8}$     | 11.291                    | 4 9 $\frac{1}{4}$      | 14 11 $\frac{7}{8}$     | 17.876                     | 5 9                   | 18 0 $\frac{1}{4}$      | 25.964                     |
| 3 9 $\frac{3}{4}$      | 11 11 $\frac{1}{4}$     | 11.415                    | 4 9 $\frac{1}{2}$      | 15 0 $\frac{1}{8}$      | 18.033                     | 5 9 $\frac{1}{4}$     | 18 1 $\frac{1}{8}$      | 26.155                     |
| 3 10                   | 12 0 $\frac{1}{2}$      | 11.534                    | 4 9 $\frac{3}{4}$      | 15 1 $\frac{1}{8}$      | 18.189                     | 5 9 $\frac{1}{2}$     | 18 2 $\frac{1}{4}$      | 26.344                     |
| 3 10 $\frac{1}{4}$     | 12 1 $\frac{1}{4}$      | 11.666                    | 4 10                   | 15 2 $\frac{1}{4}$      | 18.347                     | 5 9 $\frac{3}{4}$     | 18 3 $\frac{1}{8}$      | 26.534                     |
| 3 10 $\frac{1}{2}$     | 12 2                    | 11.793                    | 4 10 $\frac{1}{4}$     | 15 2 $\frac{7}{8}$      | 18.506                     | 5 10                  | 18 3 $\frac{7}{8}$      | 26.725                     |
| 3 10 $\frac{3}{4}$     | 12 2 $\frac{7}{8}$      | 11.920                    | 4 10 $\frac{1}{2}$     | 15 3 $\frac{1}{4}$      | 18.665                     | 5 10 $\frac{1}{4}$    | 18 4 $\frac{1}{8}$      | 26.916                     |
| 3 11                   | 12 3 $\frac{1}{8}$      | 12.048                    | 4 10 $\frac{3}{4}$     | 15 4 $\frac{1}{8}$      | 18.825                     | 5 10 $\frac{1}{2}$    | 18 5 $\frac{1}{2}$      | 27.108                     |
| 3 11 $\frac{1}{4}$     | 12 4 $\frac{1}{8}$      | 12.176                    | 4 11                   | 15 5 $\frac{1}{4}$      | 18.985                     | 5 10 $\frac{3}{4}$    | 18 6 $\frac{1}{4}$      | 27.301                     |
| 3 11 $\frac{1}{2}$     | 12 5 $\frac{1}{4}$      | 12.305                    | 4 11 $\frac{1}{4}$     | 15 6 $\frac{1}{8}$      | 19.147                     | 5 11                  | 18 7                    | 27.494                     |
| 3 11 $\frac{3}{4}$     | 12 6                    | 12.435                    | 4 11 $\frac{1}{2}$     | 15 6 $\frac{3}{8}$      | 19.309                     | 5 11 $\frac{1}{4}$    | 18 7 $\frac{3}{4}$      | 27.688                     |
| 4 0                    | 12 6 $\frac{3}{4}$      | 12.566                    | 4 11 $\frac{3}{4}$     | 15 7 $\frac{1}{4}$      | 19.471                     | 5 11 $\frac{1}{2}$    | 18 8 $\frac{1}{8}$      | 27.883                     |
| 4 0 $\frac{1}{4}$      | 12 7 $\frac{1}{8}$      | 12.697                    | 5 0                    | 15 8 $\frac{1}{2}$      | 19.635                     | 5 11 $\frac{3}{4}$    | 18 9 $\frac{1}{8}$      | 28.078                     |
| 4 0 $\frac{1}{2}$      | 12 8 $\frac{1}{8}$      | 12.829                    | 5 0 $\frac{1}{4}$      | 15 9 $\frac{1}{4}$      | 19.798                     | 6 0                   | 18 10 $\frac{1}{2}$     | 28.274                     |
| 4 0 $\frac{3}{4}$      | 12 9 $\frac{1}{8}$      | 12.962                    | 5 0 $\frac{1}{2}$      | 15 10                   | 19.963                     | 6 0 $\frac{1}{4}$     | 18 10 $\frac{7}{8}$     | 28.471                     |
| 4 1                    | 12 9 $\frac{3}{8}$      | 13.095                    | 5 0 $\frac{3}{4}$      | 15 10 $\frac{1}{2}$     | 20.128                     | 6 0 $\frac{1}{2}$     | 18 11 $\frac{1}{4}$     | 28.663                     |
| 4 1 $\frac{1}{4}$      | 12 10 $\frac{1}{8}$     | 13.229                    | 5 1                    | 15 11 $\frac{1}{8}$     | 20.294                     | 6 0 $\frac{3}{4}$     | 19 0 $\frac{1}{2}$      | 28.866                     |
| 4 1 $\frac{1}{2}$      | 12 11 $\frac{1}{8}$     | 13.364                    | 5 1 $\frac{1}{4}$      | 16 0 $\frac{1}{8}$      | 20.461                     | 6 1                   | 19 1 $\frac{1}{4}$      | 29.065                     |
| 4 1 $\frac{3}{4}$      | 13 0 $\frac{1}{4}$      | 13.499                    | 5 1 $\frac{1}{2}$      | 16 1 $\frac{1}{4}$      | 20.629                     | 6 1 $\frac{1}{4}$     | 19 2 $\frac{1}{8}$      | 29.264                     |
| 4 2                    | 13 1                    | 13.635                    | 5 1 $\frac{3}{4}$      | 16 1 $\frac{7}{8}$      | 20.797                     | 6 1 $\frac{1}{2}$     | 19 2 $\frac{7}{8}$      | 29.466                     |
| 4 2 $\frac{1}{4}$      | 13 1 $\frac{1}{4}$      | 13.772                    | 5 2                    | 16 2 $\frac{1}{4}$      | 20.965                     | 6 1 $\frac{3}{4}$     | 19 3 $\frac{1}{8}$      | 29.665                     |
| 4 2 $\frac{1}{2}$      | 13 2 $\frac{1}{8}$      | 13.909                    | 5 2 $\frac{1}{4}$      | 16 3 $\frac{1}{8}$      | 21.135                     | 6 2                   | 19 4 $\frac{1}{2}$      | 29.867                     |
| 4 2 $\frac{3}{4}$      | 13 3 $\frac{1}{8}$      | 14.047                    | 5 2 $\frac{1}{2}$      | 16 4 $\frac{1}{4}$      | 21.305                     | 6 2 $\frac{1}{4}$     | 19 5 $\frac{1}{4}$      | 30.069                     |
| 4 3                    | 13 4 $\frac{1}{4}$      | 14.186                    | 5 2 $\frac{3}{4}$      | 16 5 $\frac{1}{8}$      | 21.476                     | 6 2 $\frac{1}{2}$     | 19 6                    | 30.271                     |
| 4 3 $\frac{1}{4}$      | 13 5                    | 14.325                    | 5 3                    | 16 5 $\frac{3}{8}$      | 21.647                     | 6 2 $\frac{3}{4}$     | 19 6 $\frac{3}{4}$      | 30.475                     |
| 4 3 $\frac{1}{2}$      | 13 5 $\frac{1}{4}$      | 14.465                    | 5 3 $\frac{1}{4}$      | 16 6 $\frac{1}{4}$      | 21.819                     | 6 3                   | 19 7 $\frac{1}{8}$      | 30.679                     |
| 4 3 $\frac{3}{4}$      | 13 6 $\frac{1}{8}$      | 14.606                    | 5 3 $\frac{1}{2}$      | 16 7 $\frac{1}{8}$      | 21.992                     | 6 3 $\frac{1}{4}$     | 19 8 $\frac{1}{4}$      | 30.884                     |
| 4 4                    | 13 7 $\frac{1}{8}$      | 14.748                    | 5 3 $\frac{3}{4}$      | 16 8 $\frac{1}{4}$      | 22.166                     | 6 3 $\frac{1}{2}$     | 19 9 $\frac{1}{8}$      | 31.090                     |
| 4 4 $\frac{1}{4}$      | 13 8 $\frac{1}{8}$      | 14.890                    | 5 4                    | 16 9                    | 22.333                     | 6 3 $\frac{3}{4}$     | 19 9 $\frac{7}{8}$      | 31.296                     |
| 4 4 $\frac{1}{2}$      | 13 8 $\frac{3}{8}$      | 15.033                    | 5 4 $\frac{1}{4}$      | 16 9 $\frac{1}{4}$      | 22.515                     | 6 4                   | 19 10 $\frac{1}{4}$     | 31.503                     |
| 4 4 $\frac{3}{4}$      | 13 9 $\frac{1}{8}$      | 15.176                    | 5 4 $\frac{1}{2}$      | 16 10 $\frac{1}{8}$     | 22.621                     | 6 4 $\frac{1}{4}$     | 19 11 $\frac{1}{8}$     | 31.710                     |
| 4 5                    | 13 10 $\frac{1}{8}$     | 15.320                    | 5 4 $\frac{3}{4}$      | 16 11 $\frac{1}{8}$     | 22.866                     | 6 4 $\frac{1}{2}$     | 20 0 $\frac{1}{4}$      | 31.919                     |
| 4 5 $\frac{1}{4}$      | 13 11 $\frac{1}{4}$     | 15.465                    | 5 5                    | 17 0 $\frac{1}{8}$      | 23.043                     | 6 4 $\frac{3}{4}$     | 20 1 $\frac{1}{8}$      | 32.114                     |
| 4 5 $\frac{1}{2}$      | 14 0                    | 15.611                    | 5 5 $\frac{1}{4}$      | 17 0 $\frac{1}{4}$      | 23.221                     | 6 5                   | 20 1 $\frac{1}{2}$      | 32.337                     |
| 4 5 $\frac{3}{4}$      | 14 0 $\frac{1}{4}$      | 15.757                    | 5 5 $\frac{1}{2}$      | 17 1 $\frac{1}{8}$      | 23.330                     | 6 5 $\frac{1}{4}$     | 20 2 $\frac{1}{8}$      | 32.548                     |
| 4 6                    | 14 1 $\frac{1}{8}$      | 15.904                    | 5 5 $\frac{3}{4}$      | 17 2 $\frac{1}{8}$      | 23.578                     | 6 5 $\frac{1}{2}$     | 20 3 $\frac{1}{2}$      | 32.759                     |
| 4 6 $\frac{1}{4}$      | 14 2 $\frac{1}{8}$      | 16.051                    | 5 6                    | 17 3 $\frac{1}{8}$      | 23.758                     | 6 5 $\frac{3}{4}$     | 20 4 $\frac{1}{4}$      | 32.970                     |
| 4 6 $\frac{1}{2}$      | 14 3 $\frac{1}{4}$      | 16.200                    | 5 6 $\frac{1}{4}$      | 17 4 $\frac{1}{8}$      | 23.938                     | 6 6                   | 20 5                    | 33.183                     |
| 4 6 $\frac{3}{4}$      | 14 4                    | 16.349                    | 5 6 $\frac{1}{2}$      | 17 4 $\frac{1}{4}$      | 24.119                     | 6 6 $\frac{1}{4}$     | 20 5 $\frac{1}{4}$      | 33.396                     |
| 4 7                    | 14 4 $\frac{3}{8}$      | 16.498                    | 5 6 $\frac{3}{4}$      | 17 5 $\frac{1}{8}$      | 24.301                     | 6 6 $\frac{1}{2}$     | 20 6 $\frac{1}{8}$      | 33.619                     |
| 4 7 $\frac{1}{4}$      | 14 5 $\frac{1}{4}$      | 16.649                    | 5 7                    | 17 6 $\frac{1}{4}$      | 24.483                     | 6 6 $\frac{3}{4}$     | 20 7 $\frac{1}{8}$      | 33.824                     |
| 4 7 $\frac{1}{2}$      | 14 6 $\frac{1}{8}$      | 16.800                    | 5 7 $\frac{1}{4}$      | 17 7 $\frac{1}{4}$      | 24.666                     | 6 7                   | 20 8 $\frac{1}{8}$      | 34.039                     |
| 4 7 $\frac{3}{4}$      | 14 7 $\frac{1}{8}$      | 16.951                    | 5 7 $\frac{1}{2}$      | 17 8                    | 24.850                     | 6 7 $\frac{1}{4}$     | 20 8 $\frac{3}{8}$      | 34.255                     |
| 4 8                    | 14 7 $\frac{3}{4}$      | 17.104                    | 5 7 $\frac{3}{4}$      | 17 8 $\frac{1}{4}$      | 25.034                     | 6 7 $\frac{1}{2}$     | 20 9 $\frac{1}{4}$      | 34.471                     |
| 4 8 $\frac{1}{4}$      | 14 8 $\frac{1}{8}$      | 17.257                    | 5 8                    | 17 9 $\frac{1}{8}$      | 25.220                     | 6 7 $\frac{3}{4}$     | 20 10 $\frac{1}{8}$     | 34.688                     |



| Diam.<br>in<br>ft. in. | Circ'm<br>in<br>ft. in. | Area in<br>square<br>feet. | Diam.<br>in<br>ft. in. | Circ'm.<br>in<br>ft. in. | Area in<br>square<br>feet. | Diam<br>in<br>ft. in. | Circ'm<br>in<br>ft. in. | Area in<br>square<br>feet. |
|------------------------|-------------------------|----------------------------|------------------------|--------------------------|----------------------------|-----------------------|-------------------------|----------------------------|
| 6 8                    | 20 11 $\frac{1}{4}$     | 34.906                     | 9 7                    | 30 1 $\frac{1}{4}$       | 72.1309                    | 13 6                  | 42 4 $\frac{1}{8}$      | 143.1391                   |
| 6 8 $\frac{1}{2}$      | 21 0 $\frac{1}{2}$      | 35.125                     | 9 8                    | 30 4 $\frac{3}{8}$       | 73.3910                    | 7 42                  | 8                       | 144.9111                   |
| 6 8 $\frac{1}{2}$      | 21 0 $\frac{7}{8}$      | 35.344                     | 9 30                   | 7 $\frac{1}{2}$          | 74.6620                    | 8 42                  | 11 $\frac{1}{8}$        | 146.6949                   |
| 6 8 $\frac{3}{4}$      | 21 1 $\frac{1}{8}$      | 35.564                     | 10 30                  | 11 $\frac{1}{8}$         | 75.9433                    | 9 43                  | 2 $\frac{1}{4}$         | 148.4896                   |
| 6 9                    | 21 2 $\frac{1}{8}$      | 35.784                     | 11 31                  | 1 $\frac{3}{4}$          | 77.2362                    | 10 43                 | 5 $\frac{1}{2}$         | 150.2943                   |
| 6 9 $\frac{1}{4}$      | 21 3 $\frac{1}{4}$      | 36.006                     | 10 0                   | 31 5                     | 78.5400                    | 11 43                 | 8 $\frac{3}{8}$         | 152.1109                   |
| 6 9 $\frac{1}{2}$      | 21 4                    | 36.227                     | 1 31                   | 8 $\frac{1}{8}$          | 79.8540                    | 14 0                  | 43 11 $\frac{3}{4}$     | 153.9384                   |
| 6 9 $\frac{3}{4}$      | 21 4 $\frac{3}{4}$      | 36.450                     | 2 31                   | 11 $\frac{1}{4}$         | 81.1795                    | 1 44                  | 2 $\frac{1}{8}$         | 155.7758                   |
| 6 10                   | 21 5 $\frac{1}{2}$      | 36.674                     | 3 32                   | 2 $\frac{3}{8}$          | 82.5160                    | 2 44                  | 6                       | 157.6250                   |
| 6 10 $\frac{1}{4}$     | 21 6 $\frac{3}{8}$      | 36.897                     | 4 32                   | 5 $\frac{1}{2}$          | 83.8627                    | 3 44                  | 9 $\frac{1}{8}$         | 159.4852                   |
| 6 10 $\frac{1}{2}$     | 21 7 $\frac{1}{8}$      | 37.122                     | 5 32                   | 8 $\frac{3}{8}$          | 85.200                     | 4 45                  | 0 $\frac{1}{4}$         | 161.3553                   |
| 6 10 $\frac{3}{4}$     | 21 7 $\frac{3}{4}$      | 37.347                     | 6 32                   | 11 $\frac{3}{4}$         | 86.588                     | 5 45                  | 3 $\frac{1}{2}$         | 163.2373                   |
| 6 11                   | 21 8 $\frac{1}{4}$      | 37.573                     | 7 33                   | 2 $\frac{5}{8}$          | 87.9697                    | 6 45                  | 6 $\frac{1}{2}$         | 165.1303                   |
| 6 11 $\frac{1}{4}$     | 21 9 $\frac{1}{2}$      | 37.700                     | 8 33                   | 6 $\frac{1}{8}$          | 89.3608                    | 7 45                  | 9 $\frac{3}{8}$         | 167.0331                   |
| 6 11 $\frac{1}{2}$     | 21 10 $\frac{1}{4}$     | 38.027                     | 9 33                   | 9 $\frac{1}{4}$          | 90.7627                    | 8 46                  | 0 $\frac{7}{8}$         | 168.9479                   |
| 6 11 $\frac{3}{4}$     | 21 11                   | 38.256                     | 10 34                  | 0 $\frac{3}{4}$          | 92.1749                    | 9 46                  | 4                       | 170.8735                   |
| 7 0                    | 21 11 $\frac{7}{8}$     | 38.4846                    | 11 34                  | 3 $\frac{1}{2}$          | 93.5986                    | 10 46                 | 7 $\frac{1}{8}$         | 172.8091                   |
| 1 22                   | 3                       | 39.4060                    | 11 0                   | 34 6 $\frac{3}{8}$       | 95.0334                    | 11 46                 | 11 $\frac{1}{4}$        | 174.7565                   |
| 2 22                   | 6 $\frac{1}{8}$         | 40.3388                    | 1 34                   | 9 $\frac{3}{2}$          | 96.4783                    | 15 0                  | 47 1 $\frac{1}{2}$      | 176.7150                   |
| 3 22                   | 9 $\frac{1}{4}$         | 41.2825                    | 2 35                   | 0 $\frac{7}{8}$          | 97.9347                    | 1 47                  | 4 $\frac{3}{8}$         | 178.6832                   |
| 4 23                   | 0 $\frac{1}{2}$         | 42.2367                    | 3 35                   | 4 $\frac{1}{8}$          | 99.4021                    | 2 47                  | 7 $\frac{3}{4}$         | 180.6634                   |
| 5 23                   | 2 $\frac{1}{8}$         | 43.2022                    | 4 35                   | 7 $\frac{1}{4}$          | 100.8797                   | 3 47                  | 10 $\frac{7}{8}$        | 182.6545                   |
| 6 23                   | 6 $\frac{1}{4}$         | 44.1787                    | 5 35                   | 10 $\frac{3}{8}$         | 102.3689                   | 4 48                  | 2 $\frac{1}{2}$         | 184.6555                   |
| 7 23                   | 11                      | 45.1656                    | 6 36                   | 1 $\frac{1}{2}$          | 103.8691                   | 5 48                  | 5 $\frac{1}{8}$         | 186.6684                   |
| 8 24                   | 1 $\frac{1}{8}$         | 46.1638                    | 7 36                   | 4 $\frac{1}{2}$          | 105.3794                   | 6 48                  | 8 $\frac{1}{4}$         | 188.6923                   |
| 9 24                   | 4 $\frac{1}{2}$         | 47.1730                    | 8 36                   | 7 $\frac{3}{4}$          | 106.9013                   | 7 48                  | 11 $\frac{3}{8}$        | 190.7260                   |
| 10 24                  | 7 $\frac{1}{4}$         | 48.1926                    | 9 36                   | 10 $\frac{1}{8}$         | 108.4342                   | 8 49                  | 2 $\frac{3}{8}$         | 192.7716                   |
| 11 24                  | 10 $\frac{3}{8}$        | 49.2236                    | 10 37                  | 2 $\frac{3}{4}$          | 109.9772                   | 9 49                  | 5 $\frac{3}{4}$         | 194.8282                   |
| 8 0                    | 25 1 $\frac{1}{2}$      | 50.2656                    | 11 37                  | 5 $\frac{1}{4}$          | 111.5319                   | 10 49                 | 8 $\frac{7}{8}$         | 196.8946                   |
| 1 25                   | 4 $\frac{3}{8}$         | 51.3178                    | 12 0                   | 37 8 $\frac{3}{8}$       | 113.0976                   | 11 50                 | 0                       | 198.9730                   |
| 2 25                   | 7 $\frac{7}{8}$         | 52.3816                    | 1 37                   | 11 $\frac{1}{2}$         | 114.6732                   | 16 0                  | 50 3 $\frac{1}{8}$      | 201.0624                   |
| 3 25                   | 11                      | 53.4562                    | 2 38                   | 2 $\frac{5}{8}$          | 116.2607                   | 1 50                  | 6 $\frac{1}{4}$         | 203.1615                   |
| 4 26                   | 2 $\frac{1}{8}$         | 54.5412                    | 3 38                   | 5 $\frac{3}{4}$          | 117.8590                   | 2 50                  | 9 $\frac{3}{8}$         | 205.2726                   |
| 5 26                   | 5 $\frac{1}{4}$         | 55.6377                    | 4 38                   | 8 $\frac{1}{8}$          | 119.4674                   | 3 51                  | 0 $\frac{1}{2}$         | 207.3946                   |
| 6 26                   | 8 $\frac{3}{8}$         | 56.7451                    | 5 39                   | 0                        | 121.0876                   | 4 51                  | 3 $\frac{3}{8}$         | 209.5264                   |
| 7 26                   | 11 $\frac{1}{2}$        | 57.8628                    | 6 39                   | 3 $\frac{1}{4}$          | 122.7187                   | 5 51                  | 6 $\frac{1}{2}$         | 211.6703                   |
| 8 27                   | 2 $\frac{3}{4}$         | 58.9920                    | 7 39                   | 6 $\frac{3}{4}$          | 124.3598                   | 6 51                  | 10                      | 213.8251                   |
| 9 27                   | 5 $\frac{3}{8}$         | 60.1321                    | 8 39                   | 9 $\frac{1}{2}$          | 126.0127                   | 7 52                  | 1 $\frac{1}{8}$         | 215.9896                   |
| 10 27                  | 9                       | 61.2826                    | 9 40                   | 0 $\frac{3}{8}$          | 127.6765                   | 8 52                  | 4 $\frac{1}{4}$         | 218.1662                   |
| 11 28                  | 0 $\frac{1}{2}$         | 62.4445                    | 10 40                  | 3 $\frac{3}{4}$          | 129.3504                   | 9 52                  | 7 $\frac{3}{8}$         | 220.3537                   |
| 9 0                    | 28 3 $\frac{1}{4}$      | 63.6174                    | 11 40                  | 6 $\frac{7}{8}$          | 131.0360                   | 10 52                 | 10 $\frac{1}{2}$        | 222.5510                   |
| 1 28                   | 6 $\frac{3}{8}$         | 64.8006                    | 13 0                   | 40 10                    | 132.7326                   | 11 53                 | 1 $\frac{1}{8}$         | 224.7603                   |
| 2 28                   | 9 $\frac{1}{2}$         | 65.9951                    | 1 41                   | 1 $\frac{1}{8}$          | 134.4391                   | 17 0                  | 53 4 $\frac{7}{8}$      | 226.9806                   |
| 3 29                   | 0 $\frac{3}{4}$         | 67.2007                    | 2 41                   | 4 $\frac{3}{8}$          | 136.1574                   | 1 53                  | 8                       | 229.2105                   |
| 4 29                   | 3 $\frac{1}{4}$         | 68.4166                    | 3 41                   | 7 $\frac{1}{2}$          | 137.8867                   | 2 53                  | 11 $\frac{1}{8}$        | 231.4625                   |
| 5 29                   | 7                       | 69.6440                    | 4 41                   | 10 $\frac{3}{8}$         | 139.6260                   | 3 54                  | 2 $\frac{1}{8}$         | 233.7055                   |
| 6 29                   | 10 $\frac{1}{8}$        | 70.8823                    | 5 42                   | 1 $\frac{1}{8}$          | 141.3771                   | 4 54                  | 5 $\frac{3}{8}$         | 235.9682                   |







# HOLYOKE

## Hydrodynamic Experiments.

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To make the matter generally understood, the following notice is here republished :

### HOLYOKE WATER POWER COMPANY,

Holyoke, Mass., April 10, 1879.

#### *NOTICE TO TURBINE BUILDERS AND MANUFACTURERS.*

The practice of testing turbines, so common the past ten years, has undoubtedly done much towards bringing the best into use; but there has been one serious defect in the system; that is, the practice has generally been confined to the trial of small wheels, owing to the great expense that would be caused by the tests of large sizes. As it is a matter of vast importance that the best turbine plans should be established beyond chance for doubt, this Company has provided means for a thorough competitive test of the various kinds of turbines that may be offered for trial, and invite Water Power Companies, cities that pump their water supply, and all others interested in the matter, to take part therein. Each builder shall superintend the setting of his wheel—the setting and testing to be done at the expense of the Water Power Company. \*Capacity of each wheel to be sufficient to discharge about 5000 cubic feet of water per minute, under 18 feet head. Each wheel will be thoroughly tested from half to whole gate, and, if deemed best, under at least two different heads; also under several feet of back water. At the conclusion of the trial, a full report will be made of the results obtained and of the workmanship, and probable durability of each kind of wheel tried. Turbine builders of this or any other country are invited to furnish wheels, and those proposing to do so should give notice of such intention as soon as possible.

Tests to commence the first day of September next.

HOLYOKE, MASS., June 2, 1879.

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\*Builders who have not got patterns for wheels of so large capacity may enter their largest size, but it is better that all should discharge about the same quantity.



The parties here named have either entered wheels for the trial or have made application for information as to conditions to be observed, &c.

|                                     |                                    |
|-------------------------------------|------------------------------------|
| Swain Turbine Co., Lowell, Mass.    | Humphrey Machine Co., Keene, N. H. |
| Houston Turbine,                    | S. Sleeper, Mt. Morris, N. Y.      |
| Fales & Jenks, Pawtucket, R. I.     | Knowlton & Dolan, Logansport, Ind. |
| Wolf, Allentown, Pa.                | National, Bristol, Conn.           |
| Victor, Stilwell & Bierce M'fg Co., | Little Giant, Auburn, N. Y.        |
| Dayton, Ohio.                       | T. H. Risdon, Mt. Holly, N. J.     |
| Hercules, Holyoke Machine Co.,      | Rodney Hunt Machine Co.,           |
| Holyoke, Mass.                      | Orange, Mass.                      |
| Henry Vandewater & Co.,             | W. D. King & Co., Pontiac, Mich.   |
| Auburn, N. Y.                       | N. F. Burnham, York, Pa.           |
| Willis Reed, Danbury, Ct.           | Wm. F. Perry, Bridgeton, Maine.    |
| E. Dodge, Spencer, N. Y.            | Goldie, McCulloch & Co.,           |
| Edward Wemple, Fultonville, N. Y.   | Galt, Canada.                      |
| Joseph Hough, Mechanics Valley, Pa. | Gates Curtis, Ogdensburg, N. Y.    |

As is often the case in such trials, few of those desirous of taking advantage of the Company's offer were ready at the time named, and, as the notice did not state any time for closing, builders have been tardy in sending their wheels. The ordinary work of the testing flume has been continued during the time, so that the wheels reported are only about one-half the number tested; and any one acquainted with the matter will see that there has been no unnecessary delay in making the report.

The experiments were announced as competitive, meaning, in general utility, economy in the use of water, convenience, cost and durability.

Large turbines were called for, that their discharge might be greater than could be measured in the testing flume of any turbine builder, but this was not insisted upon, as, to have done so, would have limited the competition to a few old builders with full sets of patterns, whose wheels have often been tested and reported. Experience has not yet produced any fact that even hints that any particular size of turbine, small or large, can be made to produce higher results than any other size of the same make. Consequently, builders were allowed to send wheels the most convenient in size for themselves, and it is not known that any one of experience furnished a wheel with the expectation that it would give the highest possible results, but that its general merits should commend it to the public, and that the value of any peculiarity in its construction should be determined.

Competitive turbine tests, in the common meaning of the term, have been useful in the past, as they have enabled those interested in such matters to decide upon the most desirable plans. At the present time, however, such tests can have no public value, because each turbine tested only represents itself in efficiency. Another of

the same size and make might and probably would give quite different results, so that should each competitor have a second, third or a tenth wheel tried, his standing would be likely to change with each wheel tested. The Fourneyron, Boyden, Birkinbine and Centennial tests all prove this fact, as they also prove that the builders who have furnished the turbines that have given the highest efficiency reported, have only had a brief popularity, as manufacturers have found other turbines more desirable for business; and it will be evident from the results obtained in these experiments, that builders have taken this fact into consideration and have generally tried to produce turbines economical at any stage of gate opening, rather than to gain the highest possible efficiency at whole gate, where, in practical use, it is rarely used. And in this there has been a decided gain, as there has also in an increased capacity for a given diameter of wheel, noticeable in the Recharé as well as the Hereules and New American.

In considering the comparative merits of the wheels here reported, it should be understood that previous to 1876 turbines of any make for a given diameter generally gave about the same power. There were builders who believed in some mysterious power in *leverage*, who constructed wheels with extended diameter and proportionally small discharge, but these were exceptional; the rule held good, and it will be necessary to take this fact into consideration to realize the improvements in turbines during the past four or five years.

Turbine builders were requested to furnish draft tubes of different sizes with their wheels, that the efficiency of such tubes might be determined; and that the loss in transmission through belts and gears might also be ascertained, several well known gear-making firms were requested to furnish gears for trial.

The experiments have been conducted upon the supposition that their purpose was to ascertain the real utility of the various devices tested under the every-day ordinary conditions to which such plans are subjected in practical use, rather than possibilities in exceptional cases under the most favorable circumstances; and features of known interest developed are recorded in connection with their development. It was expected that the experiments would require much time, and as they were made in the public testing flume, it was necessary that each should be conducted as expeditiously as accuracy would permit; consequently, James Emerson, from his intimate familiarity with such matters and experience in handling wheels, was employed

to see that each turbine was set in a manner satisfactory to its builder, and to have a general supervision over the work.

Samuel Webber, Civil Engineer of Manchester, N. H., known in connection with the Centennial tests, was selected to assist in making the experiments, and reports herewith.

Theo. G. Ellis, Civil Engineer of Hartford, Conn., well known through his published works and long employment by the government in river and harbor improvements, was selected by the turbine builders to see that the experiments were skillfully and fairly conducted, whose report is appended.

For the information of the uninitiated, it is proper to state that a turbine, under a given head, does its best at a certain speed. To find this point it is necessary, in testing, to begin with a light weight, run a minute or more, then add weight and repeat until the best point is found; and the test that fixes that point is the speed at which the wheel should be geared to work, and the efficiency at that point is the efficiency of the wheel. The average efficiency from a part to whole gate means when the wheel is running at that speed at any stage of gate opening, and the efficiency at other speeds is to be considered only so far as it shows the loss that will occur through gearing above or below the proper point.

The tests are supposed to be correct and complete in each case as given, but for the information of students or others wishing to work out the data for themselves, the following is given in explanation of the statement at the head of each test: multiply revolutions by 10, 20, &c. It must be understood that during each test the scale beam is attached to the brake at a point which, if revolving, would describe a circle of 10, 15 or 20 feet in circumference. Consequently, the revolutions must be multiplied by the number given, as for example: Of the first New American wheel tested—rev. per minute, 207.5; weight, 675.  $207.5 \times 15 = 3112.5 \times 675 = 2100937.5 \div 33000 = 63.66$  h. p.

To make this report really useful, it is issued in size convenient for the pocket.

WM. A. CHASE, AGENT.

# ENGINEERS' REPORTS.

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## REPORT OF THEO. G. ELLIS.

HARTFORD, CONN., *September 13, 1880.*

WILLIAM A. CHASE, Esq.,

*Agent of the Holyoke Water Power Co.*

SIR: Having been requested to take part in the interesting experiments upon turbines made by your Company in October and November, 1879, at the Holyoke testing flume, I did so with great reluctance as, owing to many professional engagements, I could not give so much time to the subject as its importance seemed to warrant, and could not possibly be at Holyoke at all times during the experiments. I finally, however, agreed to be present at part, at least, of the tests in behalf of the turbine builders, to see that the experiments were fairly conducted as far as lay in my power, and to make such observations as I thought best.

It was understood that the mechanical work of setting the wheels and making the experiments was to be superintended by James Emerson, whose previous experience in the testing of turbines at the same locality eminently fitted him for the task. The flume and apparatus used was mostly, if not entirely, designed and constructed by him, and he was familiar with all its details and capabilities. Whatever may have been his previous published views, it is believed that in the present tests all the turbines presented for trial have received the same careful attention and trial. In some cases the record does not appear to show as full and complete a trial as in others, but there was always some good reason, irrespective of any prejudices for or against that particular wheel, for the apparent limitation of the trial.

Mr. Samuel Webber, civil engineer, of Manchester, N. H., who had superintended the Centennial tests of turbines, was present during the whole of the experiments, and I availed myself of an association with him in overlooking the experiments, so that one of

us should be present at every trial, and thus always have a disinterested party to record the readings of the dynamometer and gauges, and the time of the experiment, to serve as a check upon the readings recorded by Mr. Emerson's assistant and taken by him. Mr. Webber was assisted most of the time by Mr. Stockwell Bettes, civil engineer, of Springfield, Mass., who read the gauges and otherwise checked the readings taken and recorded by Mr. Emerson.

All of Mr. Emerson's readings, and such of Mr. Webber's as he desired, were recorded in a book kept for the purpose. These records were kept and all the computations therefrom were made by Miss Charla Adams, who for a long time has been familiar with such experiments and computations as an assistant of Mr. Emerson, and who, I am satisfied from a personal examination of her work, has performed the duty in a careful, accurate and thorough manner.

Experiments upon the following wheels were all witnessed by Mr. Webber, and part of them by myself:

|          |     |       |   |
|----------|-----|-------|---|
| October  | 10, | 1879, | Tyler Wheel.  |
| "        | 11, | "     | Thompson Wheel.   |
| "        | 14, | "     | New American Wheel.                                     |
| "        | 15, | "     | " Humming Bird " Wheel.                                 |
| "        | 16, | "     | Success Wheel.  |
| "        | 17, | "     | Two Tait Wheels.  |
| "        | 18, | "     | Repeated Test of Tait First Wheel<br>(buckets chipped). |
| "        | 18, | "     | Sherwood Wheel.   |
| "        | 21, | "     | Nonesuch Wheel.   |
| "        | 22, | "     | Curtis Wheel.   |
| "        | 28, | "     | Pair of Curtis Wheels set horizontally.                 |
| November | 11, | "     | Hercules Wheel.   |
| "        | 12, | "     | Hercules Wheel.   |
| "        | 13, | "     | Houston Wheel.  |
| "        | 14, | "     | Wetmore Wheel.  |
| "        | 15, | "     | Monarch Wheel.  |

The computed volumes of discharge, and the percentage of efficiency of the foregoing wheels, as shown in your Report, the proof of which has been submitted to me, have been carefully examined with a view to determine the relative value of the wheels named, and their respective performances under the different conditions and amounts of water with which they were tested.

In the testing of turbines, it has been the practice to first determine the velocity at which the wheel will give its greatest effect



when using all the water that will run through it with the gates or entrance apertures open to their full extent, or at "full gate;" then to diminish the quantity of water to three-quarters and one-half, as nearly as practicable, and to estimate the power of the wheel when running at the same velocity. The experiments at Holyoke were conducted practically in this manner. The best velocity was found for "full gate," and then the amount of water was diminished gradually in successive experiments to the neighborhood of half the quantity, with the wheel running as nearly as might be at the same speed.

This is perhaps the best way to make such tests, everything considered. But it does not in all cases give the exact relative value of the wheels. Some turbines might give a better result at a different velocity when using a less amount of water, and make their average, say, from half to full gate better than by the former method. The difficulty, however, of getting at the exact velocity at which any turbine would give its best results when using different quantities of water, is too great to warrant such determinations in a series of comparative tests such as were made at Holyoke. The same method must be established for all, and the customary one appears to be the fairest, as no other would probably be agreed to by all the turbine builders. In the practical use of turbines for power, it is rarely the case that a wheel is put in of the exact power required. A margin must be left for an excess of power to meet emergencies, and allowance must be made for an increase of machinery, so that a larger wheel is ordinarily purchased than would just suffice to meet present requirements. For this reason, it is not the wheel which gives the highest percentage of efficiency at "full gate" that is really the best wheel. There can be no point fixed at which any wheels should be compared, but it is thought that perhaps "three-quarters gate" is about the average point at which wheels are used, and their comparative efficiency at from one-half to their full power sufficiently represents their real value. It would probably be a better comparative test of wheels to get their best velocity at "three-quarters gate" and run them with the same velocity for greater and less quantities. This would give the real value of the wheel better than the present practice, but it would probably not be generally agreed to. In using the terms "full gate," "half gate," "three-quarters gate," etc., the relative quantity of water is meant. The opening of the wheel gates themselves is not considered. Their construction is often such that

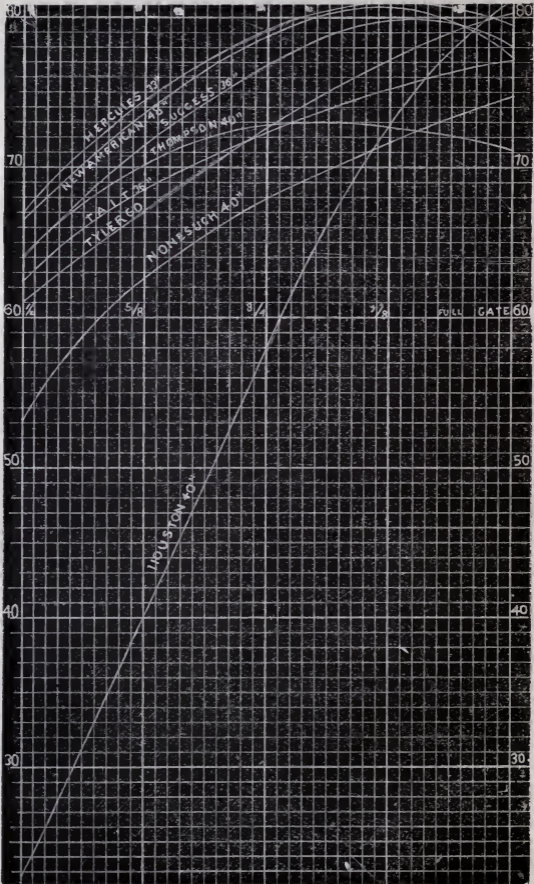
opening or closing them a certain proportion does not affect the quantity of water in the same manner. It not unfrequently happens that a slight closing of the gate increases the quantity of water passing through them, so that the gates themselves are deceptive and are no criterion of the amount of water used. The gate opening is sometimes used to deceive the uninitiated in the circulars of unscrupulous turbine builders, calling "half gate" perhaps two-thirds the whole quantity of water, so as to give a higher percentage of efficiency, but the only true standard of comparison is the actual amount of water measured as it leaves the wheel.

The experiments upon the before-named wheels have been carefully plotted with the amounts of water and the percentage of efficiency as co-ordinates, and a mean curve drawn through the points for each wheel. These curves have been all reduced to a uniform horizontal scale for the purpose of comparison, so as to obtain their relative efficiency at all proportions of the whole amount of water from half to full gate. The curves of the eight wheels giving the highest efficiency are shown on the annexed diagram. The horizontal scale shows the parts of the whole quantity of water from half to full gate, and the vertical scale shows the percentage of efficiency at all points corresponding to the amount of water indicated.

The average percentage of efficiency for these eight wheels has been computed for the amount of water from half to three-quarters gate, from half to full gate, and from three-quarters to full gate, as shown in the following table :

TABLE SHOWING AVERAGE PERCENTAGE AT PART GATE.

| NAME.                   | $\frac{1}{2}$ to $\frac{3}{4}$ .<br>Per cent. | $\frac{3}{4}$ to full.<br>Per cent. | $\frac{1}{2}$ to full.<br>Per cent. |
|-------------------------|---|-------------------------------------|-------------------------------------|
| Hercules, . . . . .     | .737  | .805                                | .771                                |
| New American, . . . . . | .732  | .795                                | .763                                |
| Success, . . . . .      | .708  | .786                                | .747                                |
| Tyler, . . . . .        | .665  | .766                                | .715                                |
| Tait, . . . . .         | .680  | .744                                | .712                                |
| Thompson, . . . . .     | .696  | .721                                | .709                                |
| Nonesuch, . . . . .     | .619  | .712                                | .666                                |
| Houston, . . . . .      | .397  | .717                                | .557                                |



By examining the diagram and the foregoing table, the peculiarities of the several wheels will be readily seen. It will be observed that the Houston turbine, which has the highest percentage of effect at full gate, is really the least efficient at from half to three-quarters, and from half to full gate, of all those shown on the diagram, and is only superior to the Nonesuch at from three-quarters to full gate, and that by a very trifling amount; so that the wheel which apparently has the highest percentage is really the least desirable for actual use. The Thompson turbine, which has the lowest percentage of those shown, at full gate, rises to the sixth place at from one-half to full gate, and to the fourth place at from one-half to three-quarters gate. The Tyler turbine, which has the second highest percentage at full gate, falls to the sixth place at from one-half to three-quarters gate. The Hercules turbine, which stands third only at full gate, takes the first rank at from half to full gate, or any of its subdivisions. The New American turbine, which stands only fifth in the percentage at full gate, is second only to the Hercules at from one-half to full gate or either of its subdivisions, and, indeed, differs from the Hercules very slightly in its useful effect through the whole range shown.

Taking the average useful effect of the wheels shown from one-half to full gate as a measure of their efficiency, their relative value is in the order shown in the table.

Among the turbines tested at about the time of the experiments upon the wheels before named, were two very remarkable ones on account of their very different qualities and performance. These were the Rechar, a statement of which is included in your Report, and the Victor, which was used in the gear experiments, likewise attached to your Report. The first-mentioned has a percentage of useful effect of only 69 at full gate, while the latter has a percentage of 92. At thirteen-sixteenths of full gate, the percentage of efficiency becomes reversed, and below that the Rechar is by far the most effective turbine. From one-half to full gate the efficiency of the Rechar is second only to the Hercules, while for the same range the Victor would come fourth in the list.

Neither Mr. Webber nor myself witnessed the experiments upon these wheels, but they are mentioned to show that a high percentage at full gate is often deceptive and does not always indicate the best wheel for practical use.

In the foregoing Report, with the exception of the last two wheels, only such wheels are considered as were tested in the presence of Mr.

Webber or myself. The list appears to embrace all the really good wheels presented, and gives their efficiency as we saw it. Some of these wheels show a little higher percentage than I have given in some of the other experiments in your Report, particularly the New American, but I have thought best to confine myself to those experiments that were witnessed and verified by the attending engineers.

With the sincere hope that comparative and competitive tests of turbines will be continued, and that thereby the public and users of power will know more fully the qualities of the wheels they purchase, and the useful effect they are likely to derive from them,

I remain, very respectfully yours, .

THEO. G. ELLIS, CIVIL ENGINEER.



## REPORT OF SAM'L WEBBER.

WM. A. CHASE, Esq.,

*Treasurer Holyoke Water Power Co.*

DEAR SIR: I was requested by you in October, 1879, to come to Holyoke and be present at a series of competitive tests of turbines, and to see that the measurements were correctly made, and the apparatus in perfect order. I was, accordingly, present the greater part of the time from October 9th to November 15th, and witnessed the tests of the following wheels, viz.:

|                     |  |
|---------------------|--|
| Oct. 9th and 10th,  | The "Tyler" Wheel.   |
| " 11th,             | " "Thompson" Wheel.  |
| " 14th,             | " "New American," being a wheel of the Swain type of bucket, with the case and gates formerly used for the "American Wheel." |
| October 15th,       | The "Humming Bird" Wheel.  |
| " 16th,             | " "Success" Wheel.   |
| " 17th,             | " "Tait Centennial," 2 wheels.   |
| " 18th,             | " " " 1st wheel repeated.  |
| " "                 | " "Sherwood" Wheel.  |
| " 21st,             | " "Nonesuch" Wheel, from Clark & Chapman.  |
| " 22nd,             | " "Gates Curtis" Wheel.  |
| " 27th,             | " " pair of wheels on draft tube.  |
| Nov. 11th and 12th, | " "Hercules" Wheel.  |
| " 13th,             | " "Houston" Wheel.   |
| " 14th,             | " "Wetmore" Wheel.   |
| " 15th,             | " "Monarch" Wheel.   |

During all these tests, I verified the measurements of the weir, the revolutions of the wheel, the head of water, and the weight on the steelyard, and in these measurements I was assisted by Mr. Stockwell Bettes; and from the data so obtained I have made up complete calculations of the results.

I have examined the proof sheets sent me by Mr. James Emerson, of his report and calculations of these tests, and have no hesitation in accepting them, as in very many cases we agree exactly, while in

no case is there a variation of over 1 per cent., and these differences are mainly due to slight differences in the weir readings, as taken by Mr. Emerson and Mr. Bettes.

I was also present during a portion of the gear and belt tests in April, 1880, and can certify to the correctness of Mr. Emerson's report of those tests, so far as the results then obtained are concerned.

I cannot, however, consider these tests as conclusive, from the fact that the gears were entirely new, and that there was no accurate method of regulating the proper depth to which the gears should be put in contact—a slight change in such depth having shown a great difference in the net power attained.

Neither was there any method for regulating or ascertaining the the tension of the belts.

Nor should I be satisfied to accept the result obtained from the 15-inch Victor wheel as conclusive of the merits of wheels of that make, as from various tests the very small wheels of almost all patterns usually give a higher percentage than the larger ones.

Yours very truly,

SAM'L WEBBER, C. E.

## REPORT OF JAMES EMERSON.

WILLIAM A. CHASE,

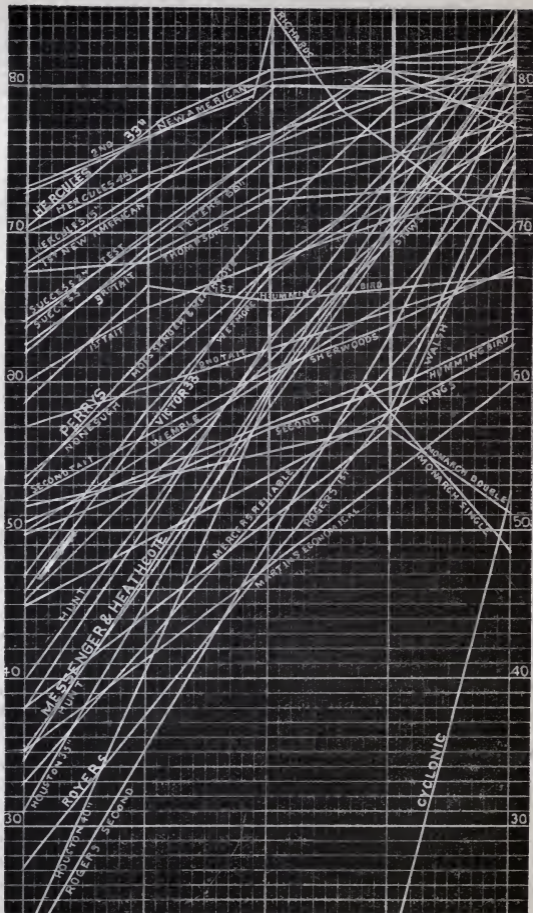
*Agent Water Power Co., Holyoke, Mass.*

SIR: Having, in connection with the engineers named, completed the series of turbine and dynamic experiments announced by your Company, the results obtained by myself, with accompanying remarks, are here submitted for your consideration.

In presenting this report, it is a pleasure to recall the interest taken in the experiments, from the beginning to their close, by engineers and experts in such matters. There was hardly a trial of any kind without the presence of such. Mr. Bettes assisted almost invariably; James M. Sickman, C. E. of Holyoke, often examined the arrangements; Prof. Norton, of the Sheffield Scientific School of New Haven, Ct., with members of his class, spent a day in witnessing the tests, and, later, six graduates of his class assisted in testing the 15-inch Victor. Prof. Whittaker, of the Massachusetts Institute of Technology, with some sixteen members of his class, not only witnessed the experiments, but had charge of the apparatus for several hours, and tested the 33-inch Hercules for practice. The Principal of the Holyoke High School, with a large delegation of scholars, both male and female, spent some hours in witnessing the tests, and seemingly with much pleasure. There were also witnesses from very distant places, and some that one would hardly expect would feel an interest in such matters, but they seemed to do so.

JAMES EMERSON.

WILLIMANSETT, MASS., Aug. 1, 1880.



## Wemple Wheel.

*Sent by Wm. Wemple's Sons, Fultonville, N. Y.*



18-inch wheel. Central and downward discharge. Inside register gate.

Data below for one minute. Multiply revolutions by 10. April 17, 1879.

| Gate Opened | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. | 18.30 | 300    | 000            | 000         |            |          |
| " "         | 18.24 | 150    | 335.3          | 15.24       | 623.06     | .7265    |
| " "         | 18.36 | 160    | 327.6          | 15.88       | 627.43     | .7298    |
| " "         | 18.40 | 170    | 319            | 16.43       | 640.98     | .7375    |
| " "         | 18.23 | 180    | 333.5          | 16.55       | 645.48     | .7431    |
| " "         | 18.40 | 190    | 296            | 17.04       | 648.48     | .7561    |
| " "         | 18.35 | 200    | 280            | 16.97       | 651.49     | .7516    |
| " "         | 18.24 | 210    | 259.5          | 16.51       | 660.44     | .7257    |
| " "         | 18.20 | 185    | 233            | 16.42       | 648.48     | .7329    |
| " "         | 18.17 | 195    | 282            | 16.66       | 651.49     | .7451    |
| Part Gate.  | 18.23 | 150    | 326            | 14.81       | 624.55     | .6887    |
| " "         | 18.20 | 175    | 236            | 15.69       | 626.04     | .7290    |
| " "         | 18.20 | 170    | 234.6          | 15.17       | 642.48     | .6868    |
| " "         | 18.21 | 165    | 282.5          | 14.12       | 599.42     | .6850    |
| " "         | 18.22 | 160    | 210            | 14.06       | 596.42     | .6851    |
| " "         | 18.24 | 140    | 278            | 11.79       | 542.63     | .6306    |
| " "         | 18.24 | 125    | 233.5          | 11.11       | 525.45     | .6137    |
| " "         | 18.31 | 100    | 259            | 7.85        | 437.65     | .5178    |
| " "         | 18.31 | 100    | 231.5          | 8.83        | 447.21     | .5700    |
| " "         | 18.43 | 75     | 227.3          | 5.65        | 330.80     | .4906    |
| " "         | 18.30 | 75     | 300.5          | 6.83        | 370.86     | .5302    |
| " "         | 18.41 | 75     | 301            | 6.84        | 373.48     | .5842    |
| " "         | 18.42 | 80     | 211.5          | 7.07        | 382.69     | .5309    |
| " "         | 18.48 | 55     | 248.5          | 4.81        | 299.28     | .4722    |
| " "         | 18.48 | 50     | 303            | 4.50        | 298.03     | .4412    |

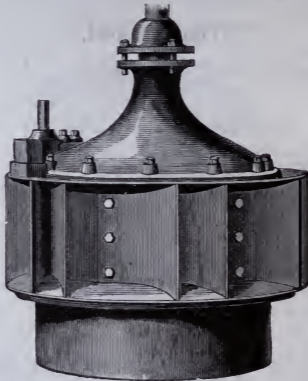
Mr. Wemple not being able to get up a wheel of the size required in time, allowed this to be reported as a representative of the kind.



## Tyler Wheel.

30-inch wheel, sent by John Tyler, Claremont, N. H.

This wheel was tested a few days before the time named for the general test, that it might be used.



This wheel was furnished for the purpose of enabling those seeking for such information to compare its power of transmission with those of the same size made by others, as the most of the popular builders have had 30-inch wheels tested. One fact, however, must be taken into consideration in making such comparisons, namely, that while the increase in the sizes of one builder is, say, 6, 12, 18, 24 and 30 h. p., the increase in another make will be 6, 9, 18, 40, 48, 75, &c.; but, in the aggregate, the total power of all the sizes of each builder amount to about the same. The Tyler flume wheel represents very fairly the average capacity of the most popular turbines known previous to 1876, excepting, however, the Boyden, which, for its diameter, is far less in capacity than any of the others.

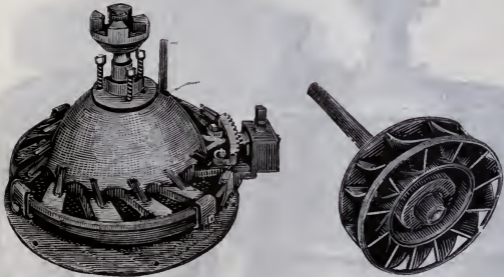
This particular wheel was made from the same patterns as the one tried at the Centennial tests, and several times at the Holyoke flume. Special pains was taken that it should be an exact duplicate of that one. The curb was the same as the Centennial, yet, as will be seen by those who have the means to make the comparison, the discharge of this wheel was one-sixth greater than the first. Mr. Tyler was so unwilling to accept the results, that he had the wheel taken out, reset, and retested on three successive days, each trial giving the same results.

Data below for one minute. Multiply revolutions by 15. Aug. 1, 1879.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent. |
|---------------------|-------|--------|----------------|-------------|------------|-----------|
| Whole Gate. . . . . | 18.30 | 375    | 218            | 37.15       | 1373.63    | .7831     |
| " " . . . . .       | 18.28 | 385    | 213.7          | 37.42       | 1373.63    | .7896     |
| " " . . . . .       | 18.27 | 400    | 209.6          | 38.10       | 1373.63    | .8045     |
| " " . . . . .       | 18.27 | 425    | 201.6          | 38.96       | 1386.77    | .8148     |
| " " . . . . .       | 18.27 | 440    | 198.5          | 39.70       | 1400.00    | .8225     |
| " " . . . . .       | 18.26 | 450    | 194            | 39.68       | 1421.11    | .8103     |
| " " . . . . .       | 18.25 | 475    | 180            | 38.86       | 1445.03    | .7809     |
| " " . . . . .       | 18.28 | 440    | 194.5          | 38.90       | 1418.46    | .7950     |

## Moessinger & Heathcote.

*Sent by Moessinger & Heathcote, Glenrock, Pa.*



*20-inch wheel.*

This turbine was a Jonval, with register gate, as represented above.

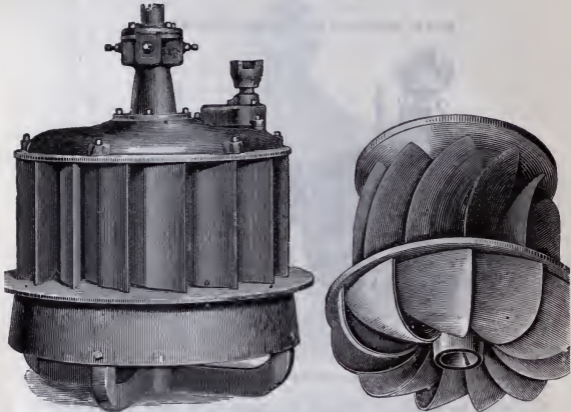
Data below for one minute. Multiply revolutions by 10. Sept. 3 and 4, 1879.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 18.40 | 100    | 320.5          | 10.47       | 511.13     | .5894    |
| " " . . . . .       | 18.40 | 110    | 325            | 11.16       | 513.84     | .6250    |
| " " . . . . .       | 18.40 | 120    | 330            | 12.00       | 517.92     | .6668    |
| " " . . . . .       | 18.39 | 130    | 323.5          | 12.74       | 524.75     | .6988    |
| " " . . . . .       | 18.39 | 140    | 310.5          | 13.17       | 531.59     | .7133    |
| " " . . . . .       | 18.38 | 150    | 300            | 13.63       | 535.71     | .7329    |
| " " . . . . .       | 18.38 | 160    | 281.6          | 13.65       | 541.23     | .7265    |
| " " . . . . .       | 18.39 | 170    | 254.5          | 13.11       | 543.99     | .6938    |
| " " . . . . .       | 18.38 | 180    | 230            | 12.54       | 545.37     | .6623    |

The wheel bound upon the step during the above trial; and it was taken out of the flume, overhauled, then re-tested, giving the results recorded below.

|                     |       |     |       |       |        |       |
|---------------------|-------|-----|-------|-------|--------|-------|
| Whole Gate. . . . . | 18.55 | 150 | 316.6 | 14.39 | 539.08 | .7618 |
| " " . . . . .       | 18.56 | 160 | 307.5 | 14.90 | 546.00 | .7784 |
| " " . . . . .       | 18.53 | 170 | 300.5 | 15.48 | 551.51 | .8016 |
| " " . . . . .       | 18.53 | 180 | 287.5 | 15.68 | 551.51 | .8123 |
| " " . . . . .       | 18.53 | 190 | 270   | 15.54 | 555.68 | .7990 |
| Part Gate. . . . .  | 18.71 | 50  | 295   | 4.47  | 381.41 | .3316 |
| " " . . . . .       | 18.65 | 75  | 296   | 6.72  | 432.22 | .4414 |
| " " . . . . .       | 18.59 | 100 | 292   | 8.85  | 478.14 | .5272 |
| " " . . . . .       | 18.55 | 125 | 292.5 | 11.08 | 517.17 | .6114 |

## Victor Turbine.

*Stilwell & Bierce Manufacturing Co., Dayton, Ohio.*

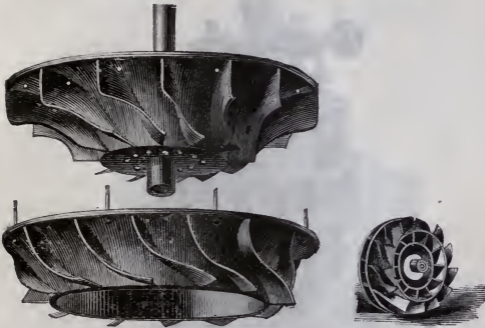
This wheel is of recent origin; discharges the water used outward, downward and centrally; has a register gate that works easily and opens in full with half a turn of gate rod. It is so designed that its buckets may be made of bronze, if desired. Its discharge in proportion to its diameter is only equaled by that of the Hercules. Price of this 35-inch wheel, \$650; weight, 4500 pounds.

Data below for one minute. Multiply revolutions by 20. Sept. 5, 1879.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 16.95 | 2050   | 000            | 000.        |            | .000     |
| " " . . . . .       | 17.18 | 1500   | 147.5          | 134.09      | 4994.79    | .8289    |
| " " . . . . .       | 17.10 | 1550   | 141.5          | 132.98      | 4999.22    | .8232    |
| " " . . . . .       | 17.11 | 1600   | 137.5          | 133.33      | 5012.56    | .8230    |
| " " . . . . .       | 17.09 | 1650   | 131.5          | 131.50      | 5025.86    | .8121    |
| " " . . . . .       | 17.07 | 1700   | 123.6          | 130.43      | 5030.31    | .8048    |
| " " . . . . .       | 17.11 | 1450   | 150            | 131.81      | 4990.36    | .8172    |
| " " . . . . .       | 17.11 | 1400   | 156            | 132.36      | 4972.64    | .8236    |
| " " . . . . .       | 17.10 | 1475   | 150            | 134.09      | 4981.50    | .8334    |
| " " . . . . .       | 17.09 | 1525   | 142.3          | 131.52      | 4985.93    | .8172    |
| Part Gate. . . . .  | 17.14 | 1475   | 147.3          | 131.76      | 4941.67    | .8237    |
| " " . . . . .       | 17.23 | 1350   | 152            | 124.36      | 4739.63    | .8063    |
| " " . . . . .       | 17.55 | 1150   | 133.3          | 92.90       | 3920.79    | .7131    |
| " " . . . . .       | 17.56 | 1100   | 136.5          | 91.00       | 3892.00    | .7050    |
| " " . . . . .       | 17.59 | 1050   | 141            | 89.72       | 3855.07    | .7006    |
| " " . . . . .       | 17.68 | 1000   | 145            | 87.87       | 3777.48    | .6989    |
| " " . . . . .       | 17.66 | 900    | 149.5          | 81.54       | 3619.75    | .6754    |
| " " . . . . .       | 18.00 | 575    | 144.2          | 50.25       | 2726.05    | .5421    |
| " " . . . . .       | 18.07 | 500    | 149.3          | 45.24       | 2616.35    | .5066    |

## Wash Double Turbine.

Sent by B. E. Sanford, Sheboygan Falls, Wisconsin.



48-inch wheel.

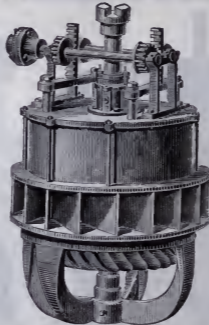
The two wheels represented above were placed together forming one with divided discharge, as represented in the small wheel at the right. The curb has cylinder gate without flange.

Data below for one minute. Multiply revolutions by 20. Sept. 8, 1879.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 17.29 | 2525   | 000            | 000         |            | 000      |
| " " . . . . .       | 17.44 | 1250   | 129            | 97.72       | 4110.90    | .7216    |
| " " . . . . .       | 17.42 | 1350   | 123.5          | 101.04      | 4157.13    | .7386    |
| " " . . . . .       | 17.38 | 1500   | 114            | 103.63      | 4224.63    | .7473    |
| " " . . . . .       | 17.37 | 1600   | 106.3          | 103.07      | 4228.88    | .7429    |
| " " . . . . .       | 17.38 | 1650   | 101            | 101.00      | 4228.88    | .7292    |
| " " . . . . .       | 17.39 | 1550   | 109.5          | 102.86      | 4219.42    | .7423    |
| " " . . . . .       | 17.39 | 1575   | 107            | 102.13      | 4224.63    | .7859    |
| " " . . . . .       | 17.38 | 1525   | 111            | 102.59      | 4224.63    | .7397    |
| " " . . . . .       | 17.38 | 1475   | 114.5          | 102.35      | 4211.96    | .7402    |
| Part Gate. . . . .  | 17.45 | 1350   | 106            | 86.72       | 4027.25    | .6534    |
| " " . . . . .       | 17.45 | 1300   | 110.5          | 87.06       | 4023.08    | .6565    |
| " " . . . . .       | 17.45 | 1275   | 113            | 87.31       | 4019.00    | .6591    |
| " " . . . . .       | 17.45 | 1260   | 114.5          | 87.73       | 4019.00    | .6623    |
| " " . . . . .       | 17.61 | 1000   | 114            | 69.09       | 3632.61    | .5718    |
| " " . . . . .       | 17.81 | 750    | 113.6          | 51.63       | 3038.93    | .5051    |
| " " . . . . .       | 17.60 | 900    | 122            | 66.54       | 3600.82    | .5558    |
| " " . . . . .       | 17.60 | 950    | 120            | 69.09       | 3608.89    | .5759    |
| " " . . . . .       | 17.73 | 850    | 112.5          | 57.95       | 3279.00    | .5278    |
| " " . . . . .       | 17.98 | 675    | 110.6          | 45.24       | 2550.32    | .5223    |
| " " . . . . .       | 17.98 | 625    | 115.5          | 43.75       | 2550.32    | .5170    |
| " " . . . . .       | 18.09 | 450    | 120            | 32.72       | 2311.00    | .4143    |
| " " . . . . .       | 18.09 | 500    | 113.5          | 34.39       | 2311.00    | .4356    |
| " " . . . . .       | 18.24 | 250    | 114.5          | 17.34       | 1827.74    | .2755    |
| " " . . . . .       | 18.23 | 350    | 125            | 26.51       | 2136.79    | .3603    |
| " " . . . . .       | 18.23 | 400    | 116            | 28.15       | 2140.23    | .3820    |

## King's Turbine.

*Sent by A. S. King, Pontiac, Michigan.*



*Wheel, 30 inches diameter.*

This turbine was a central discharge, constructed with a thick crown plate that could be raised or lowered on the buckets, so that the wheel itself could be changed in depth from ten inch openings to zero—so constructed with the expectation of getting the highest percentage for the water used, whether the wheel was opened two or ten inches. There was no separate gate, the crown plate shutting down to the bottom rim of wheel, thus forming gate in itself.

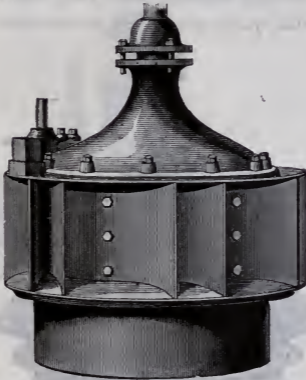
Data below for one minute. Multiply revolutions by 15. Sept. 20, 1879.

| Gate Opened. | Head  | Weight | Rev per<br>minute | Horse<br>Power | Cubic<br>Feet | Per<br>Cent |
|--------------|-------|--------|-------------------|----------------|---------------|-------------|
| Whole Gate.  | 17.93 | 920    | 000               | 00.00          | 1866.47       | .0000       |
| " "          | 17.86 | 450    | 185               | 37.84          | 1969.34       | .5695       |
| " "          | 17.85 | 500    | 175               | 39.77          | 1987.04       | .5937       |
| " "          | 17.85 | 550    | 165               | 41.25          | 1999.02       | .6120       |
| " "          | 17.85 | 600    | 154               | 42.00          | 2037.82       | .6256       |
| " "          | 17.80 | 650    | 141.6             | 41.83          | 2061.80       | .6034       |
| " "          | 17.80 | 700    | 130.5             | 41.55          | 2091.88       | .5608       |
| " "          | 17.82 | 575    | 157               | 41.03          | 2025.86       | .6018       |
| " "          | 17.82 | 590    | 154               | 41.30          | 2043.80       | .6004       |
| " "          | 17.82 | 610    | 150.5             | 41.73          | 2043.80       | .6007       |
| " "          | 17.81 | 625    | 146.2             | 41.53          | 2055.80       | .6006       |
| Part Gate.   | 17.88 | 550    | 152.5             | 38.12          | 1936.83       | .5829       |
| " "          | 17.87 | 525    | 158.6             | 37.81          | 1922.12       | .5829       |
| " "          | 17.93 | 450    | 163.8             | 33.50          | 1782.48       | .5550       |
| " "          | 17.93 | 480    | 156               | 34.03          | 1796.88       | .5592       |
| " "          | 17.93 | 500    | 152               | 34.54          | 1802.64       | .5658       |
| " "          | 18.01 | 450    | 150.2             | 29.01          | 1640.26       | .5199       |
| " "          | 18.02 | 425    | 158.5             | 30.62          | 1629.14       | .5523       |
| " "          | 18.10 | 350    | 164.5             | 26.17          | 1455.45       | .5260       |
| " "          | 18.12 | 375    | 155.5             | 26.51          | 1455.45       | .5322       |
| " "          | 18.24 | 300    | 154               | 21.00          | 1222.65       | .4998       |
| " "          | 18.34 | 250    | 139.5             | 15.85          | 1048.53       | .4364       |
| " "          | 18.35 | 200    | 173.5             | 15.77          | 1041.16       | .4370       |
| " "          | 18.35 | 225    | 150.2             | 16.28          | 1043.62       | .4501       |
| " "          | 18.43 | 140    | 155               | 9.86           | 808.00        | .3496       |
| " "          | 18.57 | 90     | 150               | 3.74           | 652.00        | .1635       |



## Tyler Wheel.

60-inch wheel, sent by John Tyler, Claremont, N. H.



In furnishing wheels for an open comparative trial, Mr. Tyler took a course alike creditable to his manhood and sense of fair dealing. He knew perfectly well that recent improvements in turbines had greatly increased their capacity, without a corresponding increase in cost, and that his wheels would have to contend against such improvements.

This turbine weighed about six tons; price, \$1,000. By comparing its cost, capacity of transmission, and general efficiency with the Hercules, Victor or New American, its relative value may be approximated.

It will be noticed that after partially closing the gate, the discharge was greater than with the gate opened in full—a rather curious feature, though the same may be observed in the test of the Monarch, the second test of the Success, and others.

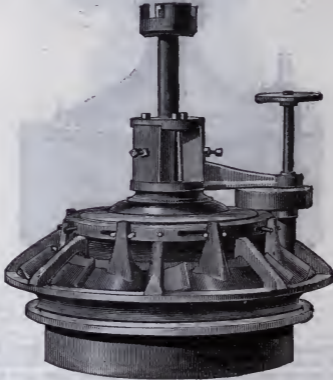
Data below for one minute. Multiply revolutions by 20. Oct. 8, 1879.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent. |
|---------------------|-------|--------|----------------|-------------|------------|-----------|
| Whole Gate. . . . . | 16.94 | 1950   | 102.5          | 121.13      | 4730.67    | .7996     |
| “ “ . . . . .       | 16.94 | 2000   | 100.5          | 121.81      | 4743.84    | .8027     |
| “ “ . . . . .       | 16.94 | 2050   | 98             | 121.75      | 4774.60    | .7970     |
| Part Gate. . . . .  | 16.88 | 2000   | 98.6           | 119.51      | 4809.82    | .7775     |
| “ “ . . . . .       | 16.88 | 1900   | 106            | 122.06      | 4809.82    | .7959     |
| “ “ . . . . .       | 17.13 | 1800   | 97             | 105.81      | 4251.42    | .7692     |
| “ “ . . . . .       | 17.15 | 1750   | 99             | 105.00      | 4192.08    | .7733     |
| “ “ . . . . .       | 17.18 | 1700   | 100.7          | 103.72      | 4162.50    | .7679     |
| “ “ . . . . .       | 17.27 | 1500   | 105            | 95.45       | 3878.45    | .7545     |
| “ “ . . . . .       | 17.28 | 1500   | 105            | 95.45       | 3870.19    | .7557     |
| “ “ . . . . .       | 17.28 | 1550   | 102            | 95.81       | 3890.86    | .7544     |
| “ “ . . . . .       | 17.64 | 1200   | 98.2           | 71.41       | 3137.24    | .6832     |
| “ “ . . . . .       | 17.65 | 1150   | 100.5          | 70.04       | 3040.77    | .6909     |
| “ “ . . . . .       | 17.67 | 1100   | 104            | 69.33       | 3106.27    | .6687     |
| “ “ . . . . .       | 17.85 | 950    | 98.3           | 56.62       | 2619.96    | .6414     |
| “ “ . . . . .       | 17.85 | 850    | 102            | 52.54       | 2510.49    | .6208     |
| Full Gate. . . . .  | 16.85 | 2000   | 100.3          | 121.57      | 4757.01    | .8030     |

## Thompson Wheel.

*Sent by Thompson Iron Works, Union City, Pa.*

40-inch wheel, diagonal in shape, like the Houston.

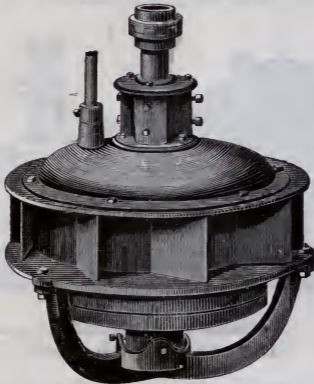


Data below for one minute. Multiply revolutions by 20. Oct. 11, 1879.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 17.66 | 1800   | 000            | 000         | 2958.73    | 000      |
| " " . . . . .       | 17.49 | 900    | 139.6          | 76.14       | 3302.55    | .6982    |
| " " . . . . .       | 17.47 | 1000   | 128            | 77.57       | 3314.46    | .7002    |
| " " . . . . .       | 17.48 | 1100   | 117            | 78.00       | 3334.34    | .7085    |
| " " . . . . .       | 17.50 | 1200   | 102.5          | 74.54       | 3330.38    | .6771    |
| " " . . . . .       | 17.50 | 1075   | 120.5          | 78.50       | 3334.34    | .7122    |
| " " . . . . .       | 17.50 | 1125   | 115            | 78.40       | 3342.30    | .7096    |
| " " . . . . .       | 17.48 | 1100   | 118.6          | 79.06       | 3346.28    | .7155    |
| " " . . . . .       | 17.48 | 1100   | 119.2          | 79.46       | 3346.28    | .7192    |
| " " . . . . .       | 17.50 | 1125   | 117.3          | 79.97       | 3342.30    | .7239    |
| Part Gate. . . . .  | 17.58 | 1100   | 111            | 74.00       | 3133.18    | .7113    |
| " " . . . . .       | 17.58 | 1100   | 112            | 74.66       | 3133.18    | .7176    |
| " " . . . . .       | 17.56 | 1050   | 119.7          | 76.17       | 3114.64    | .7529    |
| " " . . . . .       | 17.72 | 950    | 118            | 67.94       | 2783.48    | .7292    |
| " " . . . . .       | 17.94 | 800    | 120            | 58.18       | 2380.93    | .7212    |
| " " . . . . .       | 18.16 | 600    | 126.5          | 46.00       | 1963.12    | .6832    |
| " " . . . . .       | 18.15 | 700    | 114.5          | 48.57       | 2004.19    | .7069    |
| " " . . . . .       | 18.10 | 675    | 117.5          | 48.06       | 1993.90    | .7052    |
| " " . . . . .       | 18.23 | 500    | 118.5          | 35.90       | 1545.00    | .6748    |
| " " . . . . .       | 18.27 | 475    | 123            | 35.41       | 1538.57    | .6671    |

## Perry's Improved Turbine.

*Sent by Wm. F. Perry, Bridgton, Me.*



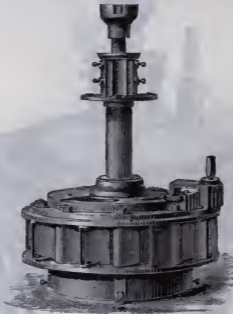
Downward discharge. Register gate. 36-inch wheel.

Data below for one minute. Multiply revolutions by 15. Oct. 13, 1879.

| Gate Opened | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. | 17.98 | 600    | 201            | 54.81       | 2108.42    | .7655    |
| " "         | 17.96 | 650    | 191.5          | 56.58       | 2120.50    | .7866    |
| " "         | 17.96 | 700    | 182            | 57.90       | 2135.60    | .7992    |
| " "         | 17.95 | 750    | 173            | 58.97       | 2138.64    | .8133    |
| " "         | 17.95 | 800    | 161.5          | 58.72       | 2144.70    | .8075    |
| " "         | 17.95 | 725    | 177            | 58.32       | 2129.56    | .8077    |
| " "         | 17.95 | 740    | 175            | 58.86       | 2132.58    | .8142    |
| " "         | 17.95 | 760    | 170.5          | 58.90       | 2138.64    | .8124    |
| " "         | 17.94 | 775    | 167.5          | 59.01       | 2147.73    | .8109    |
| Part Gate.  | 18.06 | 700    | 157            | 49.95       | 1894.69    | .7727    |
| " "         | 18.06 | 690    | 160.5          | 50.33       | 1894.69    | .7786    |
| " "         | 18.06 | 675    | 165            | 50.62       | 1891.77    | .7844    |
| " "         | 18.06 | 665    | 167.5          | 50.63       | 1888.85    | .7859    |
| " "         | 18.17 | 550    | 155            | 38.75       | 1592.69    | .7090    |
| " "         | 18.16 | 550    | 161            | 40.25       | 1628.89    | .7204    |
| " "         | 18.13 | 565    | 173.5          | 44.56       | 1719.00    | .7569    |
| " "         | 18.10 | 575    | 174.5          | 45.60       | 1761.74    | .7571    |
| " "         | 18.10 | 595    | 169.7          | 45.89       | 1761.74    | .7620    |
| " "         | 18.22 | 465    | 173.5          | 36.67       | 1513.82    | .7043    |
| " "         | 18.22 | 485    | 169            | 34.22       | 1532.00    | .6400    |
| " "         | 18.47 | 350    | 146            | 23.22       | 1144.80    | .5414    |
| " "         | 18.42 | 270    | 165            | 22.25       | 1072.42    | .5964    |
| " "         | 18.39 | 300    | 158            | 21.72       | 1099.79    | .5694    |
| " "         | 18.49 | 290    | 160            | 21.09       | 1079.92    | .5610    |
| " "         | 18.42 | 250    | 169            | 19.20       | 1069.90    | .5158    |
| " "         | 18.37 | 340    | 157.5          | 21.31       | 1158.96    | .5318    |
| " "         | 18.30 | 375    | 167            | 28.46       | 1298.80    | .6339    |

## Reynold's Champion Wheel.

*24-inch wheel, sent by Bloomer & Co., Ellenville, N. Y.*



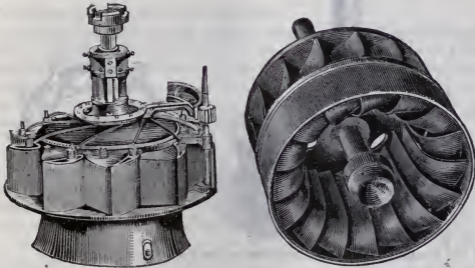
Downward discharge. Register gate.

Data below for one minute. Multiply revolutions by 10. Oct. 13, 1879.

| Gate Opened         | Head  | Weight | Rev per<br>minute | Horse<br>power | Cubic<br>feet | Per<br>Cent. |
|---------------------|-------|--------|-------------------|----------------|---------------|--------------|
| Whole Gate. . . . . | 18.34 | 550    | 000               | 000            | 1010.84       | 000          |
| " " . . . . .       | 18.32 | 275    | 313               | 26.08          | 1047.06       | .7198        |
| " " . . . . .       | 18.30 | 300    | 304               | 27.63          | 1059.28       | .7564        |
| " " . . . . .       | 18.30 | 325    | 290.5             | 28.48          | 1071.55       | .7689        |
| " " . . . . .       | 18.30 | 350    | 276.7             | 29.37          | 1081.39       | .7857        |
| " " . . . . .       | 18.29 | 375    | 260               | 29.54          | 1091.20       | .7837        |
| " " . . . . .       | 18.29 | 400    | 243.7             | 29.50          | 1103.63       | .7649        |
| " " . . . . .       | 18.28 | 365    | 266.5             | 29.47          | 1088.75       | .7836        |
| " " . . . . .       | 18.28 | 385    | 251.5             | 29.34          | 1096.20       | .7753        |
| Part Gate. . . . .  | 18.27 | 375    | 260               | 29.54          | 1088.75       | .7862        |
| " " . . . . .       | 18.23 | 350    | 273               | 28.95          | 1081.39       | .7755        |
| " " . . . . .       | 18.28 | 375    | 257.5             | 29.26          | 1091.20       | .7767        |
| " " . . . . .       | 18.28 | 350    | 268               | 28.42          | 1083.85       | .7594        |
| " " . . . . .       | 18.28 | 365    | 262.5             | 29.03          | 1086.30       | .7742        |
| " " . . . . .       | 18.27 | 350    | 263               | 27.89          | 1081.39       | .7492        |
| " " . . . . .       | 18.28 | 315    | 282.5             | 26.96          | 1071.55       | .7287        |
| " " . . . . .       | 18.27 | 335    | 272.5             | 27.66          | 1071.55       | .7479        |
| " " . . . . .       | 18.27 | 350    | 262               | 27.78          | 1071.55       | .7512        |
| " " . . . . .       | 18.34 | 300    | 261               | 23.72          | 950.79        | .7202        |
| " " . . . . .       | 18.40 | 275    | 236               | 19.66          | 848.08        | .6670        |
| " " . . . . .       | 18.41 | 250    | 256.5             | 19.43          | 834.35        | .6697        |
| " " . . . . .       | 18.41 | 245    | 260.5             | 19.34          | 834.35        | .6666        |
| " " . . . . .       | 18.46 | 200    | 252.5             | 15.30          | 746.66        | .5877        |
| " " . . . . .       | 18.46 | 190    | 260               | 14.99          | 737.83        | .5827        |
| " " . . . . .       | 18.54 | 125    | 243               | 9.20           | 594.11        | .4498        |
| " " . . . . .       | 18.54 | 110    | 260               | 8.66           | 573.81        | .4310        |
| " " . . . . .       | 18.60 | 90     | 260               | 7.09           | 521.12        | .3873        |

## New American Wheel.

*48-inch wheel, sent by Stout, Mills & Temple, Dayton, Ohio.*



This turbine has the same curb in form as the well-known American Turbine, made by that company; but the wheel is downward discharge—very similar in form and plan to the Swain.

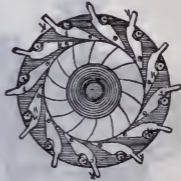
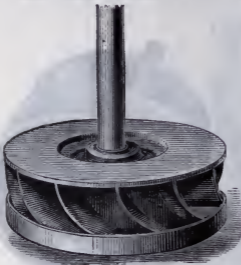
Data below for one minute. Multiply revolutions by 20. Oct. 14, 1879.

| Gate Opened.        | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent. |
|---------------------|-------|--------|----------------|-------------|------------|-----------|
| Whole Gate. . . . . | 16.45 | 2935   | 000            | 000         | 5397.95    | 000       |
| “ “ . . . . .       | 16.33 | 2000   | 110.5          | 133.94      | 5603.83    | .7749     |
| “ “ . . . . .       | 16.32 | 2050   | 103.3          | 134.55      | 5608.43    | .7783     |
| “ “ . . . . .       | 16.30 | 2100   | 104.6          | 133.12      | 5594.63    | .7727     |
| “ “ . . . . .       | 16.29 | 2150   | 101.5          | 129.48      | 5599.23    | .7516     |
| “ “ . . . . .       | 16.32 | 2025   | 109            | 133.77      | 5590.03    | .7763     |
| “ “ . . . . .       | 16.32 | 2075   | 105.5          | 132.67      | 5603.83    | .7679     |
| Part Gate. . . . .  | 16.40 | 2050   | 107            | 132.93      | 5484.60    | .7824     |
| “ “ . . . . .       | 16.40 | 2025   | 108            | 132.54      | 5475.46    | .7814     |
| “ “ . . . . .       | 16.38 | 2075   | 106.3          | 133.68      | 5484.60    | .7879     |
| “ “ . . . . .       | 16.49 | 2000   | 108.5          | 131.51      | 5280.09    | .7996     |
| “ “ . . . . .       | 16.43 | 2025   | 106.8          | 131.07      | 5271.00    | .8013     |
| “ “ . . . . .       | 16.52 | 1975   | 109.1          | 130.58      | 5257.46    | .7961     |
| “ “ . . . . .       | 16.69 | 1900   | 109            | 125.51      | 4984.41    | .7980     |
| “ “ . . . . .       | 16.88 | 1800   | 106            | 115.63      | 4546.23    | .7978     |
| “ “ . . . . .       | 16.90 | 1700   | 111.7          | 115.05      | 4477.28    | .8051     |
| “ “ . . . . .       | 16.89 | 1750   | 108.3          | 114.86      | 4511.71    | .7962     |
| “ “ . . . . .       | 16.87 | 1775   | 107.3          | 115.73      | 4529.00    | .8019     |
| “ “ . . . . .       | 17.16 | 1500   | 108.8          | 98.91       | 3966.32    | .7694     |
| “ “ . . . . .       | 17.15 | 1525   | 108.2          | 100.00      | 3962.18    | .7792     |
| “ “ . . . . .       | 17.17 | 1475   | 110.3          | 98.54       | 3937.34    | .7717     |
| “ “ . . . . .       | 17.43 | 1175   | 111.3          | 79.25       | 3336.22    | .7216     |
| “ “ . . . . .       | 17.44 | 1200   | 109.4          | 79.56       | 3348.02    | .7214     |
| “ “ . . . . .       | 17.60 | 1050   | 106.3          | 67.64       | 2969.24    | .6853     |
| “ “ . . . . .       | 17.67 | 1000   | 103.3          | 62.60       | 2829.91    | .6627     |
| “ “ . . . . .       | 17.68 | 975    | 106            | 62.63       | 2818.70    | .6638     |
| “ “ . . . . .       | 17.69 | 950    | 108.3          | 62.35       | 2774.00    | .6728     |
| Whole Gate. . . . . | 16.31 | 2050   | 106.3          | 132.07      | 5567.06    | .7701     |



## Success Wheel.

36-inch wheel, sent by S. M. Smith, York, Pa.



Called the Improved Success, very fragile in construction.

Data below for one minute. Multiply revolutions by 15. Oct. 16, 1879.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 17.99 | 1350   | 000            | 000         | 2243.17    | 0000     |
| " " . . . . .       | 17.93 | 675    | 191.5          | 58.75       | 2380.46    | .7287    |
| " " . . . . .       | 17.90 | 750    | 185            | 62.76       | 2433.92    | .7627    |
| " " . . . . .       | 17.89 | 800    | 178.2          | 64.80       | 2437.50    | .7867    |
| " " . . . . .       | 17.87 | 850    | 170.5          | 65.88       | 2484.14    | .7857    |
| " " . . . . .       | 17.87 | 900    | 162.5          | 66.47       | 2494.94    | .7893    |
| " " . . . . .       | 17.86 | 950    | 153.3          | 66.19       | 2523.82    | .7774    |
| " " . . . . .       | 17.85 | 1000   | 145.5          | 66.13       | 2523.82    | .7773    |
| " " . . . . .       | 17.86 | 875    | 165            | 65.62       | 2491.34    | .7809    |
| " " . . . . .       | 17.85 | 900    | 161.5          | 66.06       | 2502.15    | .7829    |
| " " . . . . .       | 17.85 | 925    | 157            | 66.07       | 2512.98    | .7798    |
| Part Gate. . . . .  | 17.96 | 800    | 163.2          | 59.34       | 2197.96    | .7959    |
| " " . . . . .       | 17.98 | 825    | 159.2          | 59.70       | 2208.37    | .7961    |
| " " . . . . .       | 18.19 | 550    | 163.5          | 40.87       | 1649.44    | .7212    |
| " " . . . . .       | 18.19 | 575    | 159.2          | 41.63       | 1653.80    | .7321    |
| " " . . . . .       | 18.09 | 650    | 165            | 48.75       | 1876.29    | .7604    |
| " " . . . . .       | 18.26 | 450    | 171.5          | 35.07       | 1477.05    | .6884    |
| " " . . . . .       | 18.26 | 475    | 165            | 35.62       | 1486.77    | .6947    |
| " " . . . . .       | 18.25 | 500    | 160            | 36.36       | 1499.10    | .7037    |
| " " . . . . .       | 18.25 | 525    | 154.5          | 36.86       | 1511.46    | .7076    |
| " " . . . . .       | 18.37 | 375    | 159.5          | 27.18       | 1223.47    | .6403    |
| " " . . . . .       | 18.37 | 375    | 157.5          | 26.84       | 1217.67    | .6352    |
| " " . . . . .       | 18.34 | 375    | 162.5          | 27.69       | 1258.46    | .6351    |

Second test of the same wheel, the buckets having been chipped and other changes made.

|                     |       |     |       |       |         |       |
|---------------------|-------|-----|-------|-------|---------|-------|
| Whole Gate. . . . . | 17.78 | 900 | 164.1 | 67.13 | 2482.66 | .8051 |
| Part Gate. . . . .  | 17.80 | 800 | 179   | 65.09 | 2410.98 | .8031 |
| " " . . . . .       | 17.80 | 800 | 178   | 64.72 | 2378.93 | .8091 |
| " " . . . . .       | 17.88 | 800 | 166   | 60.36 | 2168.65 | .8241 |
| " " . . . . .       | 17.76 | 875 | 167.5 | 66.61 | 2164.68 | .8051 |
| " " . . . . .       | 17.74 | 925 | 161.2 | 67.61 | 2482.66 | .8126 |
| " " . . . . .       | 17.75 | 900 | 165   | 67.50 | 2493.46 | .8076 |

## Nonesuch Wheel.

*40-inch wheel, sent by A. S. Clark, Turners Falls, Mass.*

The designer sends the following description :

The wheel consists of downward discharge buckets, enclosed by bell-shaped cylinders. The one forming the hub of the wheel has the concave surface next to the buckets. The other forms the flange or band which encloses the lower or reacting parts of the buckets, and has the convex surface next to them, or larger end downward. By this construction, the lower parts of the buckets are expanded on their outer extremity, which gives a very easy discharge. The curb of the wheel has a short draft tube in which is the step on which the wheel revolves. The water enters the wheel at the side and above the outer flange, through a system of straight chutes, within which is a cylinder gate having on the lower edge fins or blades, which extend into the chutes. The downward pressure on these blades and the weight of the gate is counterbalanced by an upward pressure on an external sectional flange near the top of the gate, and within the dome in which the gate rises to open. By this means the gate opens easy under pressure. The wheel is constructed on the theory that water should not be changed in direction horizontally after leaving the chutes, but take a downward direction only, as the wheel absorbs the power of the moving water.

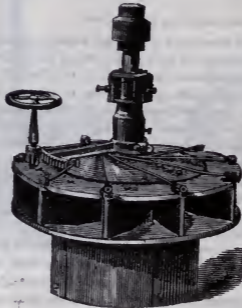
This wheel was very deep, like the Hercules; conical in shape, 40 inches in diameter at the top and 48 at the bottom, which turned outward like the Risdon—hardly distinguishable in outward appearance of curb from the Hercules.

Data below for one minute. Multiply revolutions by 20. Oct. 21, 1879.

| Gate Opened | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. | 17.37 | 2100   | 000            | 000         | 3999.93    | 000      |
| " "         | 17.14 | 1100   | 157.6          | 105.06      | 4449.00    | .7294    |
| " "         | 17.15 | 1200   | 149            | 108.36      | 4453.29    | .7512    |
| " "         | 17.12 | 1300   | 139.2          | 109.67      | 4461.89    | .7600    |
| " "         | 17.15 | 1400   | 131            | 111.15      | 4470.51    | .7676    |
| " "         | 17.13 | 1500   | 118.5          | 107.74      | 4470.51    | .7448    |
| " "         | 17.12 | 1600   | 105.5          | 102.30      | 4449.00    | .7112    |
| " "         | 17.11 | 1375   | 130.5          | 108.75      | 4444.38    | .7571    |
| Part Gate.  | 17.12 | 1425   | 125.5          | 108.75      | 4444.38    | .7503    |
| " "         | 17.12 | 1400   | 128.2          | 108.77      | 4449.00    | .7562    |
| " "         | 17.19 | 1400   | 120            | 101.82      | 4256.59    | .7368    |
| " "         | 17.19 | 1350   | 125.5          | 102.63      | 4239.56    | .7461    |
| " "         | 17.42 | 1300   | 106            | 83.51       | 3711.41    | .6839    |
| " "         | 17.38 | 1300   | 114            | 89.81       | 3859.00    | .7060    |
| " "         | 17.38 | 1200   | 124.7          | 90.70       | 3838.38    | .7206    |
| " "         | 17.48 | 1100   | 125            | 83.33       | 3865.58    | .7079    |
| " "         | 17.65 | 950    | 125            | 71.96       | 3197.18    | .6750    |
| " "         | 17.75 | 800    | 130            | 63.03       | 2935.63    | .6404    |
| " "         | 17.75 | 850    | 123.5          | 63.62       | 2928.04    | .6481    |
| " "         | 17.81 | 700    | 127.5          | 54.09       | 2686.18    | .6021    |
| " "         | 17.92 | 675    | 123            | 50.31       | 2512.67    | .6053    |
| " "         | 17.92 | 650    | 126.5          | 47.83       | 2501.81    | .5885    |
| " "         | 18.04 | 500    | 131            | 33.69       | 2224.52    | .5237    |
| " "         | 18.03 | 550    | 122.5          | 40.83       | 2221.03    | .5398    |
| " "         | 17.09 | 1400   | 126            | 106.91      | 2449.00    | .7443    |

## Tait Wheel.

Sent by Thomas Tait, Rochester, N. Y.

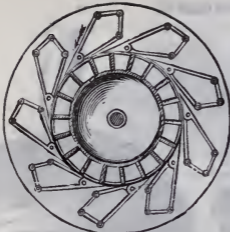


36-inch wheel.

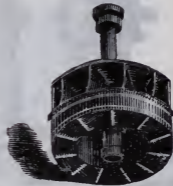
This wheel discharged downward. It had thick cast iron buckets, left square at the edge, between the hoop and crown plate.

Data below for one minute. Multiply revolutions by 15. Oct. 17, 1879.

| Gate Opened | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. | 18.25 | 1125   | 000            | 000         | 1685.09    | 000      |
| " "         | 18.27 | 550    | 156.5          | 39.12       | 1614.60    | .7022    |
| " "         | 18.26 | 560    | 154            | 39.20       | 1618.97    | .7021    |
| " "         | 18.25 | 570    | 152.5          | 39.51       | 1622.16    | .7066    |
| " "         | 18.25 | 580    | 151.5          | 39.94       | 1627.35    | .7119    |
| " "         | 18.25 | 590    | 150            | 40.22       | 1633.73    | .7142    |
| " "         | 18.25 | 609    | 147.5          | 40.22       | 1640.13    | .7109    |
| " "         | 18.25 | 610    | 146.2          | 40.50       | 1643.33    | .7149    |
| " "         | 18.24 | 620    | 144.7          | 40.77       | 1643.33    | .7202    |
| " "         | 18.24 | 630    | 142.5          | 40.81       | 1656.15    | .7153    |
| " "         | 18.24 | 650    | 139            | 41.06       | 1665.78    | .7154    |
| " "         | 18.22 | 700    | 133            | 42.31       | 1694.78    | .7271    |
| " "         | 18.21 | 750    | 125            | 42.61       | 1720.68    | .7200    |
| " "         | 18.20 | 800    | 113            | 41.09       | 1749.96    | .683     |
| Part Gate.  | 18.30 | 500    | 158.3          | 35.97       | 1485.61    | .7005    |
| " "         | 18.30 | 515    | 156            | 36.82       | 1494.94    | .7126    |
| " "         | 18.29 | 530    | 152.5          | 36.73       | 1507.41    | .7053    |
| " "         | 18.29 | 545    | 149.7          | 37.11       | 1516.78    | .6921    |
| " "         | 18.33 | 500    | 152            | 34.54       | 1420.78    | .7022    |
| " "         | 18.32 | 515    | 149.2          | 34.92       | 1426.92    | .7074    |
| " "         | 18.37 | 450    | 153.5          | 31.40       | 1293.67    | .6996    |
| " "         | 18.37 | 480    | 147.5          | 32.18       | 1311.62    | .7071    |
| " "         | 18.42 | 430    | 146            | 28.53       | 1196.28    | .6854    |
| " "         | 18.43 | 400    | 152.5          | 27.72       | 1173.01    | .6788    |
| " "         | 18.49 | 350    | 145            | 23.06       | 1011.04    | .6580    |
| " "         | 18.50 | 320    | 155            | 22.54       | 994.39     | .6487    |
| " "         | 18.56 | 250    | 157            | 17.84       | 848.19     | .6000    |
| " "         | 18.56 | 270    | 147.5          | 18.10       | 848.19     | .6080    |



TAIT (Continued).



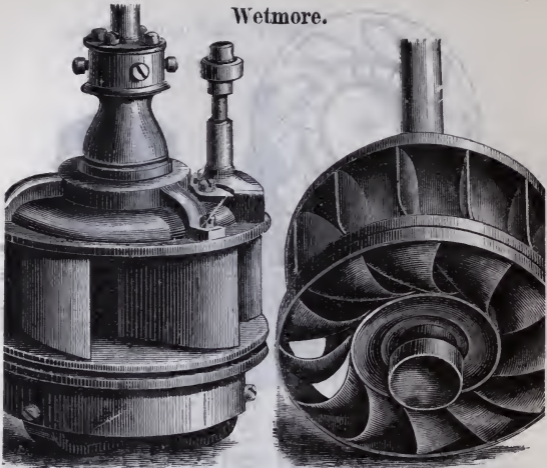
Another wheel, similar to the first, but the edge of the buckets had been finished "quarter round." It was tested in the same curb as the first.

| Gate Opened | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. | 18.18 | 550    | 158.3          | 39.57       | 1770.38    | .6476    |
| " "         | 18.17 | 575    | 155            | 40.51       | 1782.66    | .6620    |
| " "         | 18.17 | 600    | 150            | 40.90       | 1818.84    | .6553    |
| " "         | 18.16 | 625    | 148            | 42.04       | 1838.66    | .6667    |
| " "         | 18.16 | 650    | 144            | 42.54       | 1845.26    | .6722    |
| " "         | 18.15 | 675    | 140.5          | 43.11       | 1871.83    | .6718    |
| " "         | 18.14 | 700    | 136            | 43.27       | 1888.48    | .6687    |
| " "         | 18.13 | 725    | 133.5          | 43.99       | 1905.18    | .6743    |
| " "         | 18.13 | 750    | 129.5          | 44.14       | 1911.87    | .6742    |
| " "         | 18.12 | 775    | 125            | 44.03       | 1918.57    | .6701    |
| " "         | 18.11 | 800    | 121.5          | 44.18       | 1938.71    | .6663    |
| Part Gate.  | 18.18 | 600    | 146.2          | 39.87       | 1802.36    | .6592    |
| " "         | 18.19 | 575    | 150            | 39.20       | 1749.96    | .6520    |
| " "         | 18.25 | 470    | 160.5          | 34.28       | 1601.88    | .6208    |
| " "         | 18.24 | 590    | 155            | 35.22       | 1615.78    | .6327    |
| " "         | 18.23 | 530    | 150.2          | 36.18       | 1637.00    | .6419    |
| " "         | 18.28 | 470    | 151.5          | 32.36       | 1504.29    | .6231    |
| " "         | 18.35 | 410    | 151.7          | 28.27       | 1341.69    | .6079    |
| " "         | 18.43 | 350    | 149.8          | 23.83       | 1170.11    | .5850    |
| " "         | 18.50 | 235    | 150.2          | 18.09       | 972.31     | .5324    |
| " "         | 18.55 | 240    | 143.5          | 15.65       | 850.80     | .5250    |
| " "         | 18.52 | 270    | 145            | 17.79       | 934.03     | .5445    |
| " "         | 18.53 | 250    | 150            | 17.04       | 924.88     | .5264    |

Second test of the No. 1 Tait wheel, the buckets having been "chipped" back three-eighths of an inch, and edges rounded on front side, so as to leave them sharp on back side, between the hoop and crown plate.

|             |       |     |       |       |         |       |
|-------------|-------|-----|-------|-------|---------|-------|
| Whole Gate. | 18.28 | 700 | 141.5 | 45.98 | 1710.11 | .7787 |
| " "         | 18.27 | 725 | 140   | 46.13 | 1719.83 | .7772 |
| " "         | 18.32 | 675 | 148.7 | 45.63 | 1697.18 | .7771 |
| " "         | 18.31 | 650 | 151.5 | 44.76 | 1687.50 | .7670 |
| Part Gate.  | 18.34 | 650 | 144.7 | 42.75 | 1610.69 | .7663 |
| " "         | 18.36 | 600 | 153.5 | 41.86 | 1579.00 | .7645 |
| " "         | 18.39 | 600 | 145.5 | 39.88 | 1509.92 | .7566 |
| " "         | 18.40 | 580 | 149   | 39.28 | 1500.57 | .7533 |
| " "         | 18.45 | 525 | 150   | 35.79 | 1380.58 | .7440 |
| " "         | 18.50 | 475 | 146.2 | 31.56 | 1248.86 | .7230 |
| " "         | 18.50 | 450 | 152   | 31.09 | 1240.00 | .7176 |
| " "         | 18.57 | 350 | 157.2 | 25.01 | 1161.43 | .6717 |
| " "         | 18.57 | 375 | 150.5 | 25.65 | 1067.07 | .6853 |
| " "         | 18.68 | 300 | 141.5 | 19.29 | 869.71  | .6293 |
| " "         | 18.67 | 270 | 151.2 | 18.55 | 843.22  | .6238 |
| Full Gate.  | 18.28 | 750 | 135   | 46.02 | 1742.56 | .7648 |

Wetmore.



To the Engineers making Hydro-Dynamic Experiments for Water Power Co.,  
Holyoke, Mass.

GENTLEMEN: The wheel which we had tested by you was an experimental one, differing somewhat from the others heretofore tested, and from what we furnish our customers. The results you obtained did not warrant us in continuing its manufacture, so it has been abandoned, and we have returned to our original plans represented above.

Respectfully,

SULLIVAN MACHINE CO.

Nov. 14, 1879.

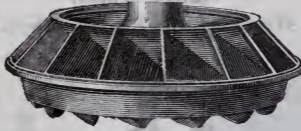
C. B. RICE, Treas.

| Gate Opened | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. | 18.38 | 350    | 250            | 39.77       | 1508.19    | .7596    |
| " "         | 18.38 | 375    | 237            | 40.36       | 1511.29    | .7692    |
| " "         | 18.38 | 400    | 224            | 40.72       | 1511.29    | .7762    |
| " "         | 18.38 | 425    | 210.5          | 40.66       | 1505.09    | .7781    |
| " "         | 18.38 | 450    | 196            | 40.09       | 1502.00    | .7689    |
| " "         | 18.39 | 390    | 227.5          | 40.32       | 1502.00    | .7727    |
| " "         | 18.38 | 410    | 217            | 40.44       | 1498.89    | .7772    |
| Part Gate.  | 18.44 | 350    | 223.5          | 35.51       | 1361.62    | .7488    |
| " "         | 18.20 | 300    | 199            | 27.13       | 1144.63    | .6894    |
| " "         | 18.21 | 275    | 216            | 27.00       | 1138.96    | .6892    |
| " "         | 18.21 | 260    | 223.5          | 26.41       | 1138.96    | .6741    |
| " "         | 18.39 | 200    | 204            | 18.54       | 917.75     | .5818    |
| " "         | 18.39 | 175    | 225            | 17.89       | 917.75     | .5613    |
| " "         | 18.53 | 125    | 222            | 12.61       | 761.30     | .4733    |
| " "         | 18.70 | 275    | 225            | 23.12       | 1176.21    | .6769    |



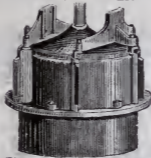
## Houston Wheel.

35-inch wheel, sent by one who had purchased the wheel.



Data below for one minute. Multiply revolutions by 15. Nov. 28, 1879.

| Gate Opened.        | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 14.07 | 550    | 165.8          | 41.45       | 1944.61    | .8022    |
| " " . . . . .       | 14.05 | 600    | 155            | 42.27       | 1944.61    | .8192    |
| " " . . . . .       | 14.04 | 625    | 149.2          | 42.38       | 1946.63    | .8166    |
| " " . . . . .       | 14.05 | 650    | 143            | 42.25       | 1956.67    | .8129    |
| " " . . . . .       | 14.01 | 675    | 138            | 42.30       | 1964.81    | .8135    |
| Part Gate. . . . .  | 14.11 | 625    | 146.2          | 41.53       | 1918.46    | .8121    |
| " " . . . . .       | 13.62 | 600    | 135.5          | 36.95       | 1812.81    | .7925    |
| " " . . . . .       | 13.66 | 575    | 142            | 37.11       | 1818.75    | .7907    |
| " " . . . . .       | 14.15 | 500    | 136.5          | 31.02       | 1635.19    | .7099    |
| " " . . . . .       | 14.29 | 450    | 149.2          | 30.51       | 1623.66    | .6960    |
| " " . . . . .       | 13.85 | 250    | 136            | 15.45       | 1223.47    | .4827    |
| " " . . . . .       | 13.68 | 225    | 146.5          | 14.98       | 1202.14    | .3869    |
| " " . . . . .       | 14.58 | 120    | 139            | 7.58        | 922.81     | .2983    |
| " " . . . . .       | 14.45 | 120    | 142            | 7.74        | 939.37     | .3019    |
| " " . . . . .       | 14.28 | 120    | 148.5          | 8.10        | 964.36     | .3114    |



## Sherwood Wheel.

20-inch wheel.

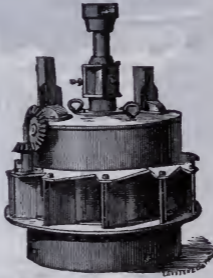
Downward discharge, similar to the Risdon, with plain cylinder gate; had been in use two years; was sent for the purpose of ascertaining the efficiency of the plan.

Data below for one minute. Multiply revolutions by 10. Oct. 7, 1879.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 18.31 | 260    | 248.2          | 19.55       | 835.13     | .6769    |
| " " . . . . .       | 18.32 | 270    | 242.2          | 19.81       | 848.37     | .6748    |
| " " . . . . .       | 18.32 | 280    | 230            | 19.51       | 848.37     | .6647    |
| " " . . . . .       | 18.31 | 250    | 259.2          | 19.63       | 848.37     | .6692    |
| Part Gate. . . . .  | 18.36 | 260    | 248            | 19.53       | 805.01     | .6996    |
| " " . . . . .       | 18.41 | 230    | 212            | 16.70       | 746.59     | .6432    |
| " " . . . . .       | 18.43 | 225    | 255            | 17.38       | 756.00     | .6606    |
| " " . . . . .       | 18.43 | 245    | 231.5          | 17.18       | 754.42     | .6543    |
| " " . . . . .       | 18.43 | 235    | 243            | 17.30       | 754.42     | .6588    |
| " " . . . . .       | 18.43 | 230    | 251            | 17.49       | 754.42     | .6508    |

## Royer Wheel.

*24-inch wheel, sent by R. R. Royer, Ephrata, Pa.*



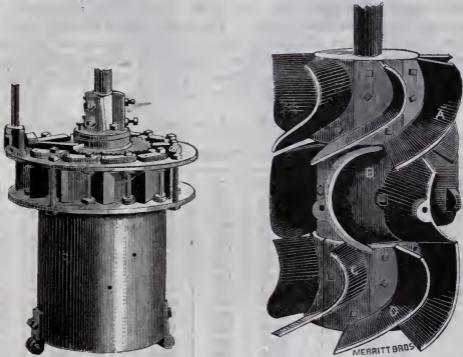
Downward discharge, having plain cylinder gate.

Data below for one minute. Multiply revolutions by 10. Dec. 5, 1879.

| Gate opened                  | Head  | Weight | Rev per<br>minute | Horse<br>Power | Cubic<br>Feet | Per<br>Cent. |
|------------------------------|-------|--------|-------------------|----------------|---------------|--------------|
| Whole Gate. . . . .          | 18.05 | 225    | 277.5             | 18.92          | 829.98        | .6686        |
| " " . . . . .                | 18.02 | 250    | 261               | 19.77          | 840.29        | .6913        |
| " " . . . . .                | 18.00 | 275    | 249.5             | 20.80          | 854.88        | .7158        |
| " " . . . . .                | 17.98 | 300    | 238               | 21.63          | 867.91        | .7339        |
| " " . . . . .                | 17.97 | 325    | 227.5             | 22.41          | 877.72        | .7184        |
| " " . . . . .                | 17.95 | 350    | 213.7             | 22.66          | 889.19        | .7517        |
| " " . . . . .                | 17.93 | 375    | 198.5             | 22.49          | 897.41        | .7400        |
| " " . . . . .                | 17.93 | 400    | 181.2             | 21.96          | 905.66        | .7161        |
| " " . . . . .                | 17.95 | 340    | 220.5             | 22.71          | 885.91        | .7562        |
| " " . . . . .                | 17.95 | 360    | 206.5             | 22.52          | 890.83        | .7456        |
| Gate closed 4 turns. . . . . | 17.96 | 325    | 228               | 22.45          | 885.91        | .7471        |
| " " 4 " . . . . .            | 17.96 | 340    | 207.5             | 21.37          | 885.91        | .7595        |
| " " 8 " . . . . .            | 17.95 | 325    | 216.7             | 21.34          | 897.41        | .7014        |
| " " 8 " . . . . .            | 17.96 | 315    | 223               | 21.28          | 895.96        | .7003        |
| " " 12 " . . . . .           | 17.96 | 300    | 215               | 19.54          | 834.27        | .6514        |
| " " 12 " . . . . .           | 17.97 | 290    | 222               | 19.50          | 879.35        | .6519        |
| " " 16 " . . . . .           | 18.03 | 250    | 211               | 15.98          | 812.90        | .5772        |
| " " 16 " . . . . .           | 18.02 | 235    | 223               | 15.88          | 798.48        | .5843        |
| " " 20 " . . . . .           | 18.15 | 175    | 214               | 11.35          | 683.14        | .4847        |
| " " 20 " . . . . .           | 18.15 | 165    | 222.5             | 11.25          | 679.54        | .4828        |
| " " 24 " . . . . .           | 18.30 | 75     | 226               | 5.14           | 529.36        | .2745        |

## Monarch Wheel.

*Sent by Albrecht & Koellisch, Randleman Mfg Co., High Point, N. C.*



Three wheels, placed one above the other, the middle wheel being loose on shaft, but being bolted firmly to the curb—arranged in this manner that it might act as chutes to the lower wheel. Chutes and gates to upper wheel similar to the Leffel, but so very leaky as to be anything but creditable to the workmanship.

HIGH POINT, N. C., August 15, 1879.

W. A. CHASE, Esq.,

*Dear Sir:* I have a turbine water wheel, finished; size, sixteen inches—a new invention, which has not been tested except by myself. It will use the water twice, and increases the power one-quarter over any wheel known. My 16-inch wheel run over eight horse power, under nine foot head, with 34 square inches discharge. As the test is open to all wheels, I would be pleased to send on my wheel to you, under such rule and regulations as you desire, for a test with other wheels.

Very respectfully,

H. L. KOELLSCH.

The letter of Mr. Koellisch is given as the best means of introducing his device and ideas; also, as a sample of hundreds of other letters received of the same tenor.

During the past few years many patents have been issued for devices known to be perfectly worthless by those acquainted with the subjects to which they belong. Particularly has this been the case in turbine plans. It is hardly possible to conceive of a device, no matter how absurd, that has not been tried in the

hopes of circumventing nature in its claim for friction and waste, or, what is more generally the case, hoping to achieve "perpetual motion" through a double use of the same fall of water. Boyden's "Diffuser," or the "Double Turbines" of Wynkoop, Leffel, or any other make, have proved equally fallacious. The highest results have been obtained from the single, simple plans. As the most effective means of presenting this fact to Mr. Kocilsch, the Monarch was first tested in the combined form designed. The results may be seen in the first table below. Then the lower wheel C and chutes B were removed and the wheel A alone tested; results obtained in the lowest table. Whenever the efficiency of a single turbine is increased by the addition of a second wheel or diffuser beneath, it may safely be concluded that the upper wheel is defective.

Data below for one minute. Multiply revolutions by 10. Nov. 15, 1879.

| Gate Opned                   | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|------------------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . .          | 18.48 | 75     | 265.5          | 6.09        | 420.92     | .4145    |
| " " . . . . .                | 18.49 | 85     | 250            | 6.40        | 423.66     | .4326    |
| " " . . . . .                | 18.49 | 95     | 288.3          | 6.86        | 427.76     | .4592    |
| " " . . . . .                | 18.51 | 105    | 223            | 7.06        | 429.11     | .4708    |
| " " . . . . .                | 18.51 | 120    | 207.5          | 7.51        | 429.14     | .5025    |
| " " . . . . .                | 18.51 | 130    | 172            | 7.56        | 429.14     | .5007    |
| " " . . . . .                | 18.51 | 140    | 182            | 7.72        | 430.50     | .5135    |
| " " . . . . .                | 18.51 | 150    | 166            | 7.51        | 433.21     | .4978    |
| Gate closed 5 turns. . . . . | 18.51 | 130    | 194.5          | 7.66        | 430.50     | .5095    |
| " " 10 " . . . . .           | 18.51 | 135    | 187            | 7.65        | 430.50     | .5087    |
| " " " " . . . . .            | 18.52 | 135    | 187            | 7.65        | 429.14     | .5096    |
| " " 15 " . . . . .           | 18.53 | 135    | 193.7          | 7.92        | 418.19     | .5411    |
| " " " " . . . . .            | 18.52 | 140    | 187            | 7.90        | 415.47     | .5436    |
| " " " " . . . . .            | 18.55 | 130    | 194.5          | 7.66        | 383.11     | .5706    |
| " " " " . . . . .            | 18.56 | 140    | 179.5          | 7.61        | 376.41     | .5767    |
| " " " " . . . . .            | 18.67 | 75     | 152.6          | 3.46        | 242.80     | .4135    |
| " " " " . . . . .            | 18.65 | 95     | 181            | 5.29        | 232.24     | .5139    |

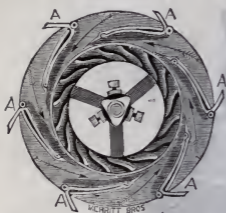
After the above tests were made, the lower wheel and set of chutes were removed.

#### Test of upper wheel A.

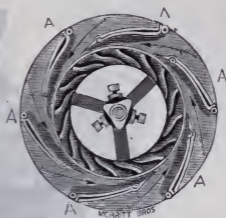
|                              |       |     |       |       |        |       |
|------------------------------|-------|-----|-------|-------|--------|-------|
| Whole Gate. . . . .          | 18.32 | 130 | 267   | 9.00  | 602.24 | .4319 |
| " " . . . . .                | 18.33 | 140 | 229   | 9.71  | 594.81 | .4405 |
| " " . . . . .                | 18.34 | 150 | 184.5 | 8.38  | 587.40 | .4119 |
| Gate closed 5 turns. . . . . | 18.34 | 130 | 270.3 | 10.64 | 605.22 | .4847 |
| " " " " . . . . .            | 18.35 | 140 | 232.5 | 9.86  | 600.75 | .4775 |
| " " 10 " . . . . .           | 18.35 | 130 | 277.5 | 10.93 | 605.22 | .5210 |
| " " " " . . . . .            | 18.37 | 140 | 232.5 | 9.86  | 590.36 | .4813 |
| " " 15 " . . . . .           | 18.37 | 130 | 293.5 | 11.56 | 578.54 | .5759 |
| " " " " . . . . .            | 18.38 | 140 | 247.5 | 10.50 | 565.33 | .5350 |
| " " 13 " . . . . .           | 18.39 | 130 | 290.5 | 11.41 | 539.11 | .5969 |
| " " " " . . . . .            | 18.37 | 140 | 239   | 10.17 | 524.68 | .5587 |
| " " 21 " . . . . .           | 18.46 | 110 | 267   | 5.90  | 429.14 | .5942 |
| " " " " . . . . .            | 18.47 | 105 | 235   | 7.47  | 404.62 | .5202 |
| " " 22 1/2 " . . . . .       | 18.65 | 75  | 263.3 | 5.98  | 317.65 | .5344 |
| " " 21 " . . . . .           | 18.62 | 50  | 215   | 3.25  | 242.80 | .3806 |

## New American Wheel.

*48-inch wheel, sent by Stout, Mills & Temple, Dayton, Ohio.*



Chutes and gates complete.



Gates cut away.

Another turbine of the same size, but of increased discharge, made after the test of the one recorded upon the opposite page. The capacity of this wheel is double that of the old 48-inch American with central discharge.

Data below for one minute. Multiply revolutions by 20. Jan. 3, 1880.

|                     | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent. |
|---------------------|-------|--------|----------------|-------------|------------|-----------|
| Whole Gate. . . . . | 13.36 | 1650   | 109            | 109.00      | 5823.77    | .7418     |
| " " . . . . .       | 13.22 | 1800   | 104.6          | 114.10      | 5922.79    | .7715     |
| " " . . . . .       | 13.09 | 1900   | 96.5           | 111.12      | 6016.59    | .7471     |
| " " . . . . .       | 12.92 | 2000   | 90.5           | 109.69      | 6030.76    | .7454     |
| " " . . . . .       | 13.20 | 1750   | 105            | 111.36      | 5857.38    | .7626     |
| " " . . . . .       | 13.21 | 1775   | 105            | 112.95      | 5862.04    | .7723     |
| " " . . . . .       | 13.10 | 1825   | 100            | 110.69      | 5876.05    | .7608     |
| " " . . . . .       | 13.06 | 1850   | 99             | 111.00      | 5885.39    | .7647     |
| " " . . . . .       | 13.11 | 1800   | 101            | 110.18      | 5871.38    | .7578     |
| Part Gate. . . . .  | 13.47 | 1700   | 101.5          | 104.57      | 5685.60    | .7231     |
| " " . . . . .       | 13.48 | 1750   | 106.5          | 112.95      | 5722.61    | .7752     |
| " " . . . . .       | 13.70 | 1700   | 108.5          | 111.78      | 5574.99    | .7749     |
| " " . . . . .       | 12.45 | 1750   | 96.5           | 102.34      | 5414.85    | .7855     |
| " " . . . . .       | 12.62 | 1700   | 97             | 99.93       | 5278.71    | .7943     |
| " " . . . . .       | 13.22 | 1500   | 112.3          | 102.00      | 5031.86    | .8126     |
| " " . . . . .       | 13.20 | 1550   | 107.5          | 100.98      | 5054.15    | .8014     |
| " " . . . . .       | 12.95 | 1700   | 100            | 103.03      | 5211.04    | .8083     |
| " " . . . . .       | 13.10 | 1850   | 106            | 86.72       | 4462.82    | .7853     |
| " " . . . . .       | 13.34 | 1400   | 102            | 86.54       | 4351.51    | .7893     |
| " " . . . . .       | 13.17 | 1450   | 101            | 88.75       | 4441.35    | .8034     |
| " " . . . . .       | 14.40 | 1200   | 107.8          | 78.40       | 3823.42    | .7716     |
| " " . . . . .       | 13.07 | 1150   | 99             | 69.00       | 3637.22    | .7685     |
| " " . . . . .       | 13.08 | 850    | 10.2           | 52.84       | 2963.38    | .7177     |

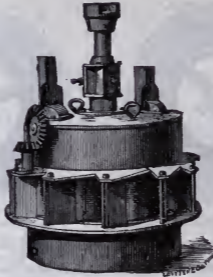
Retest of the same, having cut the wings A of gates off. This change was made for the purpose of ascertaining whether those wings had an injurious effect upon the efficiency of the wheel when the gates were opened in full.

|                     |       |      |       |        |         |       |
|---------------------|-------|------|-------|--------|---------|-------|
| Whole Gate. . . . . | 13.02 | 1750 | 102.5 | 108.63 | 5829.43 | .7450 |
| " " . . . . .       | 13.19 | 1800 | 102   | 111.27 | 5852.72 | .7681 |
| " " . . . . .       | 13.20 | 1850 | 100   | 112.12 | 5862.04 | .7671 |
| " " . . . . .       | 13.31 | 1700 | 106.5 | 109.72 | 5806.15 | .7517 |
| " " . . . . .       | 13.17 | 1900 | 98    | 112.84 | 5876.05 | .7721 |
| Part Gate. . . . .  | 14.15 | 1700 | 107   | 110.24 | 5383.01 | .7668 |
| " " . . . . .       | 13.14 | 1700 | 98.5  | 101.48 | 5233.57 | .7814 |
| Whole Gate. . . . . | 13.10 | 2000 | 92    | 111.51 | 5946.20 | .7577 |



## Royer Wheel.

*24-inch wheel, sent by R. R. Royer, Ephrata, Pa.*

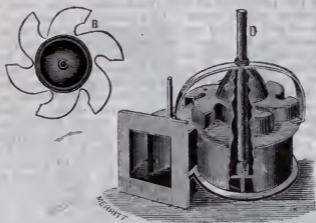


After the test of the first wheel, Mr. Royer returned home and prepared the one here reported.

Data below for one minute. Multiply revolutions by 10. March 9, 1880.

| Gate Opened |   | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-------------|---|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. | . | 17.86 | 655    | 000            | 000         | 978.04     | 000      |
| "           | " | 17.79 | 325    | 235.7          | 23.03       | 890.33     | .7698    |
| "           | " | 17.76 | 350    | 227            | 24.07       | 904.95     | .7929    |
| "           | " | 17.74 | 375    | 212.5          | 24.14       | 918.00     | .7848    |
| "           | " | 17.70 | 400    | 198.5          | 24.06       | 929.47     | .7744    |
| "           | " | 17.69 | 425    | 185.5          | 23.89       | 931.97     | .7673    |
| "           | " | 17.70 | 340    | 229.5          | 23.64       | 901.69     | .7843    |
| "           | " | 17.70 | 350    | 226.5          | 24.02       | 904.95     | .7939    |
| "           | " | 17.69 | 360    | 222.5          | 24.27       | 908.21     | .8000    |
| "           | " | 17.73 | 370    | 217.5          | 24.38       | 913.11     | .7974    |
| Part Gate.  | . | 17.73 | 370    | 215            | 24.10       | 918.00     | .7839    |
| "           | " | 17.77 | 370    | 207.6          | 23.27       | 922.91     | .7512    |
| "           | " | 17.80 | 360    | 215            | 23.45       | 922.91     | .7733    |
| "           | " | 17.82 | 350    | 219.5          | 23.28       | 920.64     | .7514    |
| "           | " | 17.84 | 350    | 206            | 21.84       | 909.84     | .7124    |
| "           | " | 17.86 | 330    | 219.5          | 21.95       | 904.95     | .7191    |
| "           | " | 17.90 | 300    | 215.7          | 19.60       | 880.61     | .6434    |
| "           | " | 17.92 | 290    | 223            | 19.59       | 869.32     | .6658    |
| "           | " | 17.95 | 250    | 225            | 17.01       | 815.05     | .6299    |
| "           | " | 17.97 | 270    | 212.5          | 17.38       | 818.18     | .6258    |
| "           | " | 17.98 | 250    | 187            | 14.16       | 769.47     | .5418    |
| "           | " | 18.01 | 225    | 207.5          | 14.14       | 750.83     | .5536    |
| "           | " | 18.02 | 215    | 216            | 14.07       | 746.19     | .5541    |
| "           | " | 18.09 | 150    | 216            | 9.81        | 640.16     | .4485    |
| "           | " | 18.13 | 145    | 224            | 9.84        | 632.75     | .4541    |
| "           | " | 18.17 | 125    | 201            | 7.61        | 574.35     | .3861    |
| "           | " | 18.17 | 115    | 209            | 7.23        | 567.16     | .3740    |
| "           | " | 18.17 | 105    | 217            | 6.60        | 562.85     | .3417    |
| "           | " | 18.25 | 75     | 191            | 4.34        | 478.59     | .2630    |
| "           | " | 18.25 | 60     | 210            | 3.82        | 467.64     | .2370    |
| "           | " | 18.27 | 50     | 222            | 3.37        | 462.18     | .2113    |

## Cyclonic Turbine.



More than ordinary pains was taken to obtain a decisive trial of this device, not from any belief in its superior efficiency, but because *cyclonic* minds, filled with *vorticoso* ideas, are far more abundant than is generally realized, not only with the illiterate but quite as plentifully with the educated, the turbine user as well as builder. The cyclone, the whirlpool and centrifugal force have been harped upon in connection with turbine building since the conception of that business,—Uriah A. Boyden and the author of the cyclonic alike trying to profit thereby, to gain something from nothing. It should be plain to any level headed person that to produce a centrifugal force of one hundred pounds, a somewhat greater force must be expended to do it. Were the reverse the case, then “perpetual motion” would not only be possible, but would be very philosophical. The following explanation and description is by the author :

The laws that govern the action of this wheel, as its name implies, is copied from Nature, and is founded on the principles and laws that govern the rotary motion of the Cyclone—the great motor engine of our atmosphere. It is a well known fact in meteorology, that all storms, from the smallest whirlwind to the most extended cyclone, are translated along their course in a rapid vorticoso motion, revolving around its axis, which is the point of lowest barometer. Immediately the vapor laden air rushing along the earth's surface from points of high barometer, rise in spirals till they reach the cooler currents of the upper atmosphere, and there rapidly condense into clouds and rain, setting free the latent heat produced by condensation and greatly expanding the surrounding atmosphere and correspondingly increasing the point of low barometer. This rapid rotary motion calls into play the centripetal and centrifugal forces, and they, acting almost equally in opposite directions, and on both sides of the whirling air, it escapes spirally upwards with the power of both forces combined. It is the upward, twisting vorticoso motion that makes the tornado the most destructive engine that comes within our experience, and as nature ever follows the line of least resistance, so it must be the most perfect and powerful mechanical contrivance with which we are acquainted—air and water in motion being governed by the same laws, with the exception that air is compressible and elastic

In order to meet the differences, I have made the upper part of my wheel a large air chamber, then, as the water comes up into the wheel, instead of striking an iron plate, it strikes a column of confined air, and by the force of elasticity, it is thrown back upon the wheel without loss of power and escapes horizontally at the perimeter of the wheel—thus doing away with most of the impact and friction which seems to be a necessity to most other wheels. The claims that I have got allowed are, first, the air chamber, which is described as spherical, surmounting the wheel; second, a scroll shaped flume, with a central aperture through the top plate corresponding to one in the lower section of the wheel. The water enters the flume and is made to assume a vortical or cyclonic motion before it reaches the wheel, so that the wheel does not have to expend the power in changing a direct motion of the water column to a rotary or spiral one, but it gains in power from the application of the cyclonic motion, which the water has gained in passing through the flume, so that the wheel gets not only the head pressure but that due to the acquired centrifugal motion. The value of this wheel seems to be, first, in rapid whirlpool motion before it touches the wheel, and consequently does not have to perform that labor; second, its great velocity of revolution; third, the water coming in at the center and flowing outward makes the most of centrifugal force, which force is additional to head pressure, and will increase in proportion to the square of its velocity; fourth, a small wheel will do as much work as others two or three sizes larger, because the pressure, being greater, will discharge more water through the same vent with corresponding power.

24-inch wheel; six outlets, each 2½ inches square.

Data below for one minute. Multiply revolutions by 10. March 10, 1880.

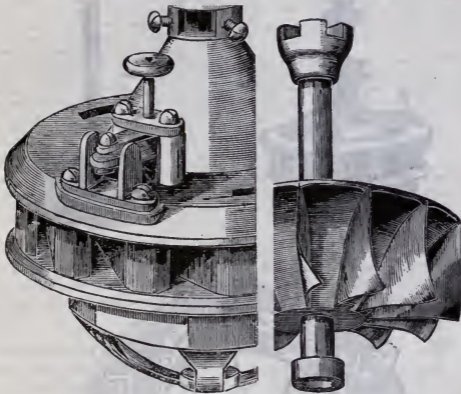
| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 17.10 | 200    | 000            | 0.00        | 307.20     | 000      |
| " " . . . . .       | 16.98 | 50     | 380            | 5.75        | 459.87     | .3900    |
| " " . . . . .       | 17.03 | 75     | 299            | 6.70        | 428.46     | .4861    |
| " " . . . . .       | 17.02 | 100    | 204            | 6.18        | 392.29     | .4901    |
| " " . . . . .       | 17.00 | 60     | 352            | 6.40        | 443.41     | .4495    |
| " " . . . . .       | 17.00 | 70     | 321.5          | 6.81        | 437.96     | .4842    |
| " " . . . . .       | 17.00 | 80     | 288.5          | 6.99        | 425.77     | .5113    |
| " " . . . . .       | 17.00 | 90     | 252.5          | 6.88        | 409.61     | .5231    |
| " " . . . . .       | 17.00 | 85     | 266.5          | 6.86        | 406.93     | .5250    |
| " " . . . . .       | 17.00 | 85     | 247            | 6.36        | 384.36     | .5153    |
| " " . . . . .       | 17.00 | 75     | 290            | 6.59        | 402.92     | .5094    |
| " " . . . . .       | 17.00 | 65     | 323.5          | 6.37        | 420.36     | .4719    |
| " " . . . . .       | 17.00 | 50     | 195            | 2.95        | 268.93     | .3416    |

Another test of same wheel, the outlets being enlarged to 2½ inches square.

|                     |       |     |       |      |        |       |
|---------------------|-------|-----|-------|------|--------|-------|
| Whole Gate. . . . . | 16.93 | 230 | 000   | 0.00 | 416.31 | 000   |
| " " . . . . .       | 16.80 | 75  | 322.5 | 7.32 | 564.50 | .4086 |
| " " . . . . .       | 16.80 | 85  | 299.5 | 7.45 | 555.81 | .4224 |
| " " . . . . .       | 16.83 | 95  | 262   | 7.54 | 522.86 | .4537 |
| " " . . . . .       | 16.84 | 105 | 235.5 | 7.49 | 508.69 | .4630 |
| " " . . . . .       | 16.80 | 100 | 246.5 | 7.46 | 515.76 | .4558 |
| " " . . . . .       | 16.82 | 90  | 278   | 7.58 | 534.23 | .4466 |

## Mercer's Reliable Turbine.

24-inch wheel, sent by Mercer & Stinman, Lancaster, Pa.



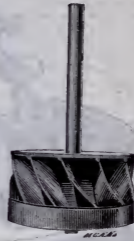
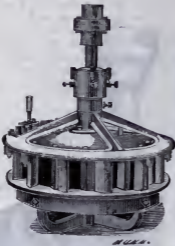
Downward discharge. Outside register gate.

Data below for one minute. Multiply revolutions by 10. May 29, 1880.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic feet | Per Cent. |
|---------------------|-------|--------|----------------|-------------|------------|-----------|
| Whole Gate. . . . . | 18.28 | 775    | 000            | 000         | 1028.77    | 000       |
| " " . . . . .       | 18.24 | 350    | 211.6          | 22.42       | 998.95     | .6514     |
| " " . . . . .       | 18.31 | 360    | 209.5          | 22.85       | 1001.43    | .6449     |
| " " . . . . .       | 18.31 | 370    | 206.7          | 23.17       | 1001.43    | .6690     |
| " " . . . . .       | 18.30 | 380    | 204.5          | 23.54       | 1003.91    | .6784     |
| " " . . . . .       | 18.30 | 390    | 201.5          | 23.81       | 1006.39    | .6845     |
| " " . . . . .       | 18.29 | 400    | 200            | 24.24       | 1008.87    | .6954     |
| " " . . . . .       | 18.29 | 410    | 198.5          | 24.66       | 1011.35    | .7058     |
| " " . . . . .       | 18.28 | 420    | 193.5          | 24.62       | 1013.87    | .7033     |
| " " . . . . .       | 18.29 | 430    | 189            | 24.62       | 1016.32    | .7012     |
| Part Gate. . . . .  | 18.22 | 375    | 195            | 22.15       | 961.56     | .6694     |
| " " . . . . .       | 18.28 | 375    | 192.5          | 21.87       | 947.34     | .6686     |
| " " . . . . .       | 18.36 | 325    | 198.7          | 19.56       | 896.45     | .6292     |
| " " . . . . .       | 18.34 | 275    | 201.5          | 16.79       | 839.22     | .5775     |
| " " . . . . .       | 18.25 | 250    | 210.5          | 15.94       | 836.86     | .5525     |
| " " . . . . .       | 18.50 | 190    | 207            | 11.91       | 730.07     | .4668     |
| " " . . . . .       | 18.52 | 175    | 212            | 11.24       | 723.23     | .4443     |
| " " . . . . .       | 18.57 | 150    | 225            | 10.22       | 698.31     | .4173     |
| " " . . . . .       | 18.71 | 115    | 197            | 6.86        | 555.72     | .3802     |
| " " . . . . .       | 18.71 | 100    | 212.5          | 6.44        | 551.46     | .3804     |

## Rechar Wheel.

*24-inch wheel, sent by George F. Baugher, York, Pa.*



Turbine building, like the other arts, started with low beginnings, how far back it is impossible to determine. Water wheels, working upon vertical shafts, were used centuries since. The tub wheel, with buckets made of wood, and shaped substantially like those of the Jonval wheel, were the earliest in my recollection, though the impact, flutter, undershot, breast and overshot were also common at that time—all of which were objectionable under certain conditions. Fourneyron, Jonval, Parker, Boyden, and many others, attempted to produce wheels free from such objections, but, in doing so, overlooked the essential feature necessary to make their efforts successful.

In supplying a mill with motive power, a surplus for emergencies is absolutely necessary. The plans of the builders alluded to were generally capable of producing wheels reasonably efficient, when working with the maximum supply of water that would pass through their openings. Half that quantity would hardly turn the wheel to speed. Consequently, with such wheels in use upon our variable streams, it was necessary to have them so small that, during nine months of each year, from half to three-fourths of the water would run to waste over the dam, or the works must stand idle through the dry months—a fact that prejudiced manufacturers to such an extent that breast or overshot wheels have been displaced with reluctance.

Mr. Rechard, like a few other recent builders, has worked upon a different plan, as may be seen by an examination of the tabulated results below, or in the diagram connected with this report, instead of striving for high results at full gate, where a turbine is seldom used unless during back water, when the quantity used is of no account. He has so arranged chutes and buckets as to gain his eighty-five per cent. at three-fourths gate, or at the point at which the wheel is most likely to be used, instead of from thirty to sixty per cent. that would be realized by the use of the Fourneyron or any of the early whole gate turbines. Wheels equal to the one tested of this make are far superior in efficiency to any breast or overshot wheel that can be produced, no matter what the head may be; and such wheels enable the user to get the full benefit of his stream, either in its highest or lowest supply.

The results below show this wheel to be the most economical in the use of water at about three-fourths discharge; and Mr. Baugher takes the very novel course of tabling the capacity of his wheels at that point, thus insuring the purchaser not only the full power represented in the table, but a surplus for emergencies.

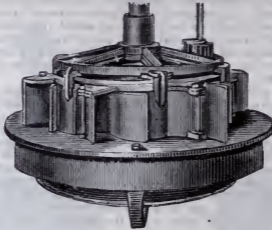
Data below for one minute. Multiply revolutions by 15. June 8, 1880.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent. |
|---------------------|-------|--------|----------------|-------------|------------|-----------|
| Whole Gate. . . . . | 18.03 | 690    | 000            | 000         | 1749.33    | 000       |
| " " . . . . .       | 18.05 | 300    | 280.5          | 38.25       | 1669.66    | .6719     |
| " " . . . . .       | 18.05 | 325    | 269            | 39.73       | 1678.15    | .6944     |
| " " . . . . .       | 18.05 | 350    | 252            | 40.09       | 1686.64    | .6972     |
| " " . . . . .       | 18.04 | 375    | 234            | 39.88       | 1703.67    | .6870     |
| " " . . . . .       | 18.00 | 400    | 215            | 39.00       | 1712.20    | .6700     |
| " " . . . . .       | 18.04 | 340    | 257            | 39.71       | 1689.48    | .6898     |
| " " . . . . .       | 18.02 | 360    | 244.5          | 40.00       | 1692.31    | .6943     |
| " " . . . . .       | 18.02 | 370    | 235.5          | 39.61       | 1695.15    | .6865     |
| Part Gate. . . . .  | 18.18 | 325    | 247            | 36.48       | 1356.80    | .7829     |
| " " . . . . .       | 18.22 | 300    | 255            | 34.77       | 1288.13    | .7844     |
| " " . . . . .       | 18.21 | 325    | 236.5          | 34.93       | 1293.38    | .7851     |
| " " . . . . .       | 18.26 | 300    | 255.5          | 34.84       | 1192.19    | .8481     |
| " " . . . . .       | 18.28 | 275    | 253            | 31.62       | 1153.92    | .7987     |
| " " . . . . .       | 18.34 | 250    | 253.5          | 28.80       | 1070.96    | .7763     |
| " " . . . . .       | 18.38 | 225    | 253.5          | 25.92       | 977.65     | .7630     |
| " " . . . . .       | 18.39 | 225    | 248            | 25.21       | 960.73     | .7555     |
| " " . . . . .       | 18.41 | 225    | 244.5          | 25.01       | 946.29     | .7400     |
| " " . . . . .       | 18.46 | 185    | 251.5          | 21.15       | 851.59     | .7123     |
| " " . . . . .       | 18.46 | 200    | 240            | 21.81       | 856.26     | .7305     |
| " " . . . . .       | 18.52 | 150    | 250            | 17.04       | 728.26     | .6689     |
| " " . . . . .       | 18.51 | 150    | 247.5          | 16.87       | 721.57     | .6687     |
| " " . . . . .       | 18.55 | 150    | 233            | 15.88       | 666.43     | .6800     |
| " " . . . . .       | 18.62 | 100    | 243.5          | 11.06       | 555.61     | .5662     |
| " " . . . . .       | 18.61 | 80     | 257            | 9.34        | 534.91     | .4968     |
| " " . . . . .       | 18.67 | 80     | 224            | 8.14        | 452.20     | .5104     |



## The Economical Turbine.

24-inch wheel, sent by S. Martin, York, Pa.



This turbine consisted of an upper plain downward discharge wheel above one of an outward discharge. The builder declined to have a test made of the upper wheel alone.

During this test, the area of aperture was 102 square inches.

Data below for one minute. Multiply revolutions by 10. June 15, 1880.

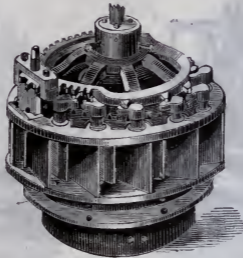
| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 18.29 | 485    | 000            | 0000        | 752.36     | 000      |
| " " . . . . .       | 18.26 | 200    | 244.5          | 14.81       | 788.68     | .5446    |
| " " . . . . .       | 18.25 | 210    | 234            | 14.89       | 787.09     | .5489    |
| " " . . . . .       | 18.25 | 220    | 225            | 15.00       | 785.50     | .5527    |
| " " . . . . .       | 18.27 | 230    | 215.5          | 15.02       | 783.91     | .5552    |
| " " . . . . .       | 18.27 | 240    | 206            | 14.98       | 780.74     | .5560    |
| " " . . . . .       | 18.27 | 250    | 194.2          | 14.71       | 777.58     | .5482    |
| Part Gate. . . . .  | 18.58 | 50     | 234.3          | 3.55        | 371.10     | .2726    |
| " " . . . . .       | 18.55 | 70     | 205.5          | 4.35        | 368.46     | .3369    |
| " " . . . . .       | 18.53 | 100    | 203            | 6.15        | 415.23     | .4232    |
| " " . . . . .       | 18.51 | 95     | 210            | 6.05        | 424.94     | .4072    |
| " " . . . . .       | 18.49 | 125    | 201.5          | 7.63        | 478.63     | .4766    |
| " " . . . . .       | 18.48 | 120    | 209            | 7.60        | 481.43     | .4522    |
| " " . . . . .       | 18.44 | 140    | 209.5          | 8.88        | 524.00     | .4866    |
| " " . . . . .       | 18.41 | 160    | 210            | 10.18       | 570.30     | .5134    |
| " " . . . . .       | 18.41 | 170    | 197.5          | 10.17       | 573.24     | .5102    |
| " " . . . . .       | 18.41 | 165    | 205.5          | 10.27       | 571.77     | .5154    |
| " " . . . . .       | 18.39 | 190    | 204.7          | 11.78       | 623.57     | .5438    |
| " " . . . . .       | 18.34 | 210    | 198.5          | 12.63       | 656.70     | .5552    |
| " " . . . . .       | 18.35 | 205    | 204.5          | 12.70       | 659.73     | .5554    |

Second test of same wheel, area of aperture being reduced to 72 square inches.

|                     |       |     |       |       |        |       |
|---------------------|-------|-----|-------|-------|--------|-------|
| Whole Gate. . . . . | 18.31 | 200 | 231.2 | 13.12 | 685.66 | .5908 |
| " " . . . . .       | 18.31 | 210 | 222.5 | 13.10 | 681.07 | .6007 |
| " " . . . . .       | 18.32 | 220 | 212.5 | 11.37 | 682.60 | .5695 |
| " " . . . . .       | 18.33 | 230 | 204   | 11.86 | 682.60 | .5968 |
| " " . . . . .       | 18.33 | 250 | 184   | 9.75  | 684.13 | .5872 |
| Part Gate. . . . .  | 18.33 | 215 | 201.5 | 13.12 | 638.58 | .5934 |
| " " . . . . .       | 18.34 | 210 | 206   | 13.10 | 634.07 | .5764 |
| " " . . . . .       | 18.39 | 175 | 214.5 | 11.37 | 590.87 | .5541 |
| " " . . . . .       | 18.40 | 190 | 206   | 11.86 | 582.04 | .5864 |
| " " . . . . .       | 18.44 | 150 | 214.5 | 9.75  | 521.08 | .5372 |
| " " . . . . .       | 18.46 | 160 | 206   | 9.98  | 510.49 | .5607 |
| " " . . . . .       | 18.52 | 125 | 194   | 7.34  | 431.57 | .4862 |
| " " . . . . .       | 18.54 | 115 | 207   | 7.21  | 424.74 | .4848 |
| " " . . . . .       | 18.61 | 65  | 196   | 3.86  | 321.72 | .3413 |
| " " . . . . .       | 18.61 | 60  | 202   | 3.67  | 320.44 | .3558 |

## Stowe Wheel.

24-inch wheel, sent by E. W. Roff, Newark, N. J.

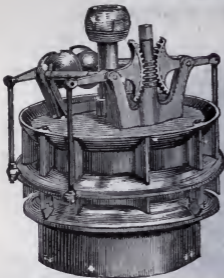


The claim for merit in this combination is upon the arrangement of gates, which open two at a time, up to sixteen in all. The plan of closing a part of the chutes or buckets of a turbine, for the purpose of using the water economically with a partial supply or at "part gate," has been tried by all of our noted turbine builders, and is still a favorite idea with amateurs or inexperienced persons interested in such matters. Walter S. Davis, of Warner, N. H., patented a plan nearly identical with that of the Stowe about 1870. J. B. Case, of Bristol, Ct., also, at about the same time, patented a plan the same in principle, though differing in detail.

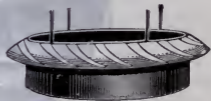
Data below for one minute. Multiply revolutions by 10. June 17, 1880.

|                  | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent. |
|------------------|-------|--------|----------------|-------------|------------|-----------|
| 16 Gates Opened. | 17.85 | 755    | 000            | 0000        | 1429.48    | .000      |
| " " "            | 18.09 | 340    | 276            | 28.43       | 1137.77    | .7350     |
| " " "            | 18.08 | 350    | 274            | 29.06       | 1139.52    | .7466     |
| " " "            | 18.05 | 360    | 269            | 29.34       | 1150.00    | .7484     |
| " " "            | 18.04 | 370    | 267            | 29.90       | 1158.76    | .7574     |
| " " "            | 18.04 | 380    | 265            | 30.51       | 1167.54    | .7669     |
| " " "            | 18.05 | 390    | 260            | 30.72       | 1176.33    | .7556     |
| " " "            | 18.05 | 400    | 255.5          | 30.97       | 1188.66    | .7639     |
| " " "            | 18.02 | 410    | 253.5          | 31.49       | 1195.73    | .7739     |
| " " "            | 18.01 | 420    | 247.5          | 31.50       | 1202.81    | .7700     |
| " " "            | 18.02 | 430    | 245            | 31.92       | 1213.44    | .7729     |
| " " "            | 18.01 | 450    | 238            | 32.45       | 1224.06    | .7795     |
| " " "            | 17.97 | 475    | 231            | 33.25       | 1256.05    | .7800     |
| " " "            | 17.95 | 500    | 221            | 33.45       | 1265.21    | .7799     |
| " " "            | 17.94 | 550    | 202            | 33.66       | 1292.21    | .7678     |
| 10 " "           | 18.22 | 300    | 249.3          | 22.66       | 942.03     | .6989     |
| " " "            | 18.17 | 325    | 238            | 23.43       | 968.68     | .7047     |
| 8 " "            | 18.33 | 225    | 244            | 16.63       | 728.55     | .6592     |
| " " "            | 18.31 | 235    | 240            | 17.09       | 744.09     | .6642     |
| " " "            | 18.31 | 245    | 233.5          | 17.33       | 753.45     | .6650     |
| 6 " "            | 18.46 | 175    | 233            | 12.35       | 561.98     | .6303     |
| " " "            | 18.43 | 165    | 236            | 11.80       | 563.43     | .6017     |
| 4 " "            | 18.60 | 100    | 224            | 6.78        | 363.48     | .5309     |
| " " "            | 18.60 | 90     | 231            | 6.30        | 362.17     | .4952     |
| " " "            | 18.61 | 85     | 234.2          | 6.03        | 359.57     | .4770     |
| 2 " "            | 18.18 | 50     | 210            | 3.18        | 203.66     | .4546     |

## Hard Working Gate.



Risdon Wheel.



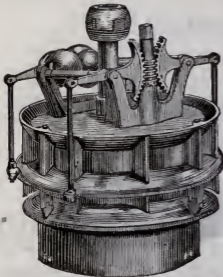
Gate.

To ascertain the comparative efficiency of a plain cylinder gate at different stages of gate opening, the following experiments were made: A 36-inch Risdon turbine was selected for the purpose. It was one of the best, and from the same patterns the 90 per cent. wheels reported of that make were made. The gate hoisting rods and geared levers were changed to the plan to be seen upon the Hunt wheel reported upon another page. As the gate raised to open, it worked the other side up from what it is illustrated here and the four hoisting rods were connected to what is represented as the bottom, running up, and in no way obstructing the chutes. In this condition the wheel was carefully tested.

Data below for one minute. Multiply revolutions by 15.

| Gate Opened | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. | 18.19 | 700    | 170.6          | 54.28       | 1965.76    | .8033    |
| " "         | 18.19 | 725    | 166            | 54.90       | 1972.76    | .8070    |
| " "         | 18.19 | 750    | 161.3          | 54.98       | 1970.76    | .8120    |
| " "         | 18.18 | 775    | 155.6          | 54.80       | 1970.76    | .8099    |
| " "         | 18.18 | 800    | 150.3          | 54.65       | 1979.76    | .8039    |
| " "         | 18.18 | 740    | 163            | 54.82       | 1966.76    | .8118    |
| " "         | 18.18 | 760    | 158.2          | 54.65       | 1953.76    | .8110    |
| Part Gate.  | 18.19 | 760    | 152.1          | 52.54       | 1901.16    | .8044    |
| " "         | 18.20 | 745    | 155            | 52.48       | 1901.16    | .8030    |
| " "         | 18.22 | 725    | 159.5          | 52.5        | 1898.19    | .8045    |
| " "         | 18.25 | 725    | 151            | 49.76       | 1824.45    | .7914    |
| " "         | 18.27 | 700    | 156.5          | 49.79       | 1818.59    | .7934    |
| " "         | 18.27 | 675    | 162.5          | 49.85       | 1818.59    | .7944    |
| " "         | 18.30 | 665    | 154.5          | 46.70       | 1728.38    | .7817    |
| " "         | 18.31 | 645    | 158            | 46.32       | 1722.60    | .7775    |
| " "         | 18.32 | 625    | 163.7          | 46.50       | 1713.96    | .7840    |
| " "         | 18.37 | 600    | 154.5          | 42.13       | 1608.25    | .7550    |
| " "         | 18.38 | 585    | 158.2          | 42.06       | 1602.59    | .7560    |
| " "         | 18.38 | 570    | 162.5          | 42.10       | 1605.42    | .7554    |
| " "         | 18.42 | 525    | 155.5          | 37.10       | 1476.72    | .7222    |
| " "         | 18.42 | 510    | 158.8          | 36.81       | 1476.72    | .7104    |
| " "         | 18.44 | 495    | 162.8          | 36.63       | 1479.49    | .7180    |
| " "         | 18.49 | 450    | 152.5          | 31.10       | 1326.84    | .6700    |
| " "         | 18.49 | 435    | 155.5          | 30.74       | 1324.15    | .6709    |
| " "         | 18.50 | 415    | 161.2          | 30.40       | 1321.47    | .6583    |
| " "         | 18.57 | 350    | 156            | 24.81       | 1160.09    | .6095    |
| " "         | 18.57 | 340    | 159.5          | 24.65       | 1160.09    | .6055    |
| " "         | 18.57 | 330    | 160.5          | 24.07       | 1155.52    | .5939    |
| " "         | 18.62 | 300    | 143.7          | 19.59       | 983.26     | .5666    |

## Easier Working Gate.



*Risdon Wheel.*



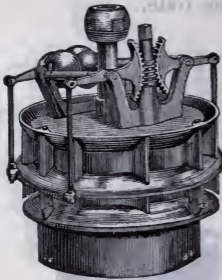
*Gate.*

Retest of the same wheel, the flange of the gate having been cut away about half the length of the chutes, as represented above.

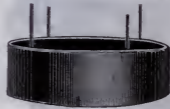
Data below for one minute. Multiply revolutions by 15.

| Gate Opened | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. | 18.21 | 700    | 171            | 54.40       | 1962.74    | .8058    |
| " "         | 18.20 | 725    | 165.7          | 54.60       | 1965.53    | .8080    |
| " "         | 18.21 | 750    | 162            | 55.22       | 1968.52    | .8149    |
| " "         | 18.21 | 775    | 155.2          | 54.67       | 1965.53    | .8086    |
| " "         | 18.21 | 800    | 149.7          | 54.43       | 1977.49    | .8003    |
| " "         | 18.21 | 740    | 162.5          | 54.65       | 1971.51    | .8058    |
| " "         | 18.20 | 760    | 158.5          | 54.75       | 1983.48    | .8031    |
| Part Gate.  | 18.23 | 760    | 151.5          | 52.33       | 1911.94    | .7950    |
| " "         | 18.22 | 745    | 154.3          | 52.25       | 1908.98    | .7952    |
| " "         | 18.23 | 725    | 159.5          | 52.56       | 1906.02    | .8008    |
| " "         | 18.25 | 725    | 150.5          | 49.59       | 1835.31    | .7838    |
| " "         | 18.26 | 700    | 155.3          | 49.41       | 1829.39    | .7832    |
| " "         | 18.26 | 675    | 160.5          | 49.24       | 1826.48    | .7817    |
| " "         | 18.30 | 665    | 151.3          | 45.73       | 1727.80    | .7656    |
| " "         | 18.29 | 645    | 156            | 45.73       | 1719.16    | .7700    |
| " "         | 18.31 | 625    | 160.6          | 45.62       | 1716.28    | .7685    |
| " "         | 18.35 | 600    | 151            | 41.18       | 1613.65    | .7363    |
| " "         | 18.34 | 585    | 155.2          | 41.26       | 1605.18    | .7420    |
| " "         | 18.35 | 570    | 158            | 40.91       | 1605.18    | .7352    |
| " "         | 18.34 | 555    | 163            | 41.12       | 1601.56    | .7413    |
| " "         | 18.40 | 510    | 152.6          | 35.37       | 1482.40    | .6865    |
| " "         | 18.40 | 495    | 158.7          | 35.70       | 1479.64    | .6943    |
| " "         | 18.40 | 480    | 163            | 35.56       | 1476.88    | .6928    |
| " "         | 18.46 | 430    | 154.6          | 30.11       | 1335.51    | .6466    |
| " "         | 18.46 | 415    | 158.5          | 29.89       | 1330.15    | .6401    |
| " "         | 18.47 | 400    | 163.5          | 29.72       | 1327.47    | .6403    |
| " "         | 18.53 | 340    | 155.6          | 24.04       | 1169.65    | .5789    |
| " "         | 18.54 | 325    | 160            | 23.63       | 1167.07    | .5781    |
| " "         | 18.53 | 315    | 163            | 23.33       | 1164.49    | .5726    |
| " "         | 18.60 | 260    | 155            | 18.31       | 1000.06    | .5211    |

## Easy Working Gate.



Risdon 36-inch wheel.



Gate.

A third test of the same wheel, the flange of the gate having been cut entirely away, leaving a plain cylinder gate.

Data below for one minute. Multiply revolutions by 15.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 18.23 | 700    | 177            | 56.31       | 2120.25    | .7713    |
| " " . . . . .       | 18.24 | 725    | 171.2          | 56.48       | 2139.46    | .7662    |
| " " . . . . .       | 18.25 | 750    | 165.6          | 56.75       | 2139.46    | .7695    |
| " " . . . . .       | 18.24 | 775    | 160.5          | 56.54       | 2136.39    | .7681    |
| " " . . . . .       | 18.22 | 800    | 154.5          | 56.18       | 2136.39    | .7643    |
| " " . . . . .       | 18.23 | 740    | 168            | 56.50       | 2139.46    | .7669    |
| " " . . . . .       | 18.23 | 760    | 163.7          | 56.41       | 2136.39    | .7669    |
| Part Gate. . . . .  | 18.24 | 760    | 156.5          | 54.06       | 2096.53    | .7484    |
| " " . . . . .       | 18.26 | 745    | 161.5          | 54.68       | 2090.41    | .7585    |
| " " . . . . .       | 18.24 | 725    | 165.6          | 54.27       | 2081.25    | .7569    |
| " " . . . . .       | 18.26 | 725    | 155            | 51.07       | 2023.49    | .7317    |
| " " . . . . .       | 18.27 | 700    | 161.5          | 51.38       | 2017.43    | .7380    |
| " " . . . . .       | 18.26 | 675    | 166.6          | 51.12       | 2017.43    | .7347    |
| " " . . . . .       | 18.28 | 665    | 157            | 47.45       | 1942.20    | .7076    |
| " " . . . . .       | 18.30 | 645    | 158.5          | 46.46       | 1939.21    | .6932    |
| " " . . . . .       | 18.24 | 625    | 166            | 47.17       | 1923.23    | .7103    |
| " " . . . . .       | 18.30 | 600    | 155.5          | 42.40       | 1850.02    | .6631    |
| " " . . . . .       | 18.31 | 585    | 158.5          | 42.14       | 1850.02    | .6586    |
| " " . . . . .       | 18.31 | 570    | 163            | 42.23       | 1844.12    | .6622    |
| " " . . . . .       | 18.31 | 555    | 166.2          | 41.92       | 1838.22    | .6594    |
| " " . . . . .       | 18.36 | 510    | 157.7          | 36.55       | 1727.17    | .6101    |
| " " . . . . .       | 18.38 | 495    | 164            | 36.90       | 1727.17    | .6154    |
| " " . . . . .       | 18.37 | 480    | 167.5          | 36.54       | 1727.17    | .607     |
| " " . . . . .       | 18.42 | 430    | 158            | 31.18       | 1601.01    | .5600    |
| " " . . . . .       | 18.42 | 415    | 162.5          | 30.65       | 1595.34    | .5323    |
| " " . . . . .       | 18.42 | 400    | 167.5          | 30.45       | 1595.34    | .5486    |
| " " . . . . .       | 18.48 | 340    | 160            | 24.72       | 1458.15    | .4856    |
| " " . . . . .       | 18.47 | 325    | 165            | 21.37       | 1455.39    | .4800    |
| " " . . . . .       | 18.48 | 315    | 167.6          | 23.96       | 1455.39    | .4717    |
| " " . . . . .       | 18.55 | 260    | 156.6          | 18.51       | 1289.50    | .4067    |
| " " . . . . .       | 18.54 | 245    | 162.5          | 18.09       | 1284.16    | .4023    |
| " " . . . . .       | 18.54 | 230    | 167.2          | 17.48       | 1281.49    | .3895    |
| " " . . . . .       | 18.62 | 150    | 164            | 11.18       | 1083       | .2935    |
| " " . . . . .       | 18.64 | 140    | 166            | 10.56       | 1077.89    | .2782    |

## EXPERIMENTS

WITH

# Gears, Belts and Draft Tubes.

[These experiments occupied the time from March 18 to  
April 23 inclusive.]

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In presenting these results, it is not pretended that they exhaust the subjects, for such is far from being the case, as every change made, no matter how slight, caused a change in the rate of transmission. The best results obtained are given, while the conditions under which they were obtained were certainly quite as favorable as gears and shafting are likely to be placed in mills. The great loss in transmission through the spur gears was entirely unexpected, and the experiment was repeated at intervals, during several weeks, with substantially the same results at each repetition, and it would seem desirable to make a more exhaustive trial by trying a greater variety of gears of different make and relative proportion, and particularly of gears made from the same patterns, but of different brands of iron. There must be some discoverable cause why one gear will run without perceptible wear for years, when another, put in to replace it, cuts out in a day or two. So of water wheel steps, where two wheels, seemingly alike, placed in the same pit, with one the step lasts for years, while the other requires a new one monthly. Is there not some property in the iron that causes such different effects? At any rate, it is hardly worth while to spend time, brains and money in efforts to produce turbines and other engines of the highest efficiency, unless corresponding efforts are made to transmit a reasonable proportion of such efficiency.

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To find the loss of power in transmission through gears, and the loss by use of draft tubes, the highest efficiency in each case must be compared with that of the 15-inch Victor wheel reported upon the next page.



## Victor Turbine.

5 inches in diameter. Price, \$250.



This wheel was in use several weeks to make the following gear, draft tube and belt experiments. The results below show the efficiency of the wheel. Data for one minute. Multiply revolutions by 10.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 17.98 | 310    | 323.2          | 30.36       | 981.15     | .9111    |
| " " . . . . .       | 17.97 | 320    | 300.5          | 29.13       | 981.15     | .8747    |
| " " . . . . .       | 17.97 | 290    | 348.5          | 30.62       | 974.47     | .9258    |
| " " . . . . .       | 17.98 | 290    | 347.5          | 30.53       | 972.80     | .9242    |
| " " . . . . .       | 18.00 | 280    | 355            | 30.12       | 969.47     | .9139    |
| " " . . . . .       | 17.98 | 300    | 337.3          | 30.66       | 977.81     | .9234    |
| Part Gate. . . . .  | 17.99 | 300    | 331            | 30.09       | 972.80     | .9102    |
| " " . . . . .       | 17.99 | 290    | 345            | 30.31       | 972.80     | .9174    |
| " " . . . . .       | 18.00 | 300    | 334.5          | 30.40       | 972.80     | .9191    |
| " " . . . . .       | 17.99 | 290    | 334            | 29.35       | 971.13     | .8896    |
| " " . . . . .       | 17.99 | 275    | 339            | 28.25       | 962.82     | .8634    |
| " " . . . . .       | 18.02 | 260    | 331.5          | 26.11       | 901.88     | .8506    |
| " " . . . . .       | 18.03 | 250    | 338.5          | 25.64       | 897.00     | .8394    |
| " " . . . . .       | 18.09 | 230    | 331.2          | 23.08       | 820.67     | .8231    |
| " " . . . . .       | 18.09 | 225    | 339.5          | 23.14       | 808.53     | .8376    |
| " " . . . . .       | 18.20 | 175    | 339            | 17.97       | 695.06     | .7538    |
| " " . . . . .       | 18.38 | 105    | 334            | 10.62       | 482.59     | .6345    |
| " " . . . . .       | 18.41 | 95     | 340            | 9.78        | 460.56     | .6108    |

Re-test of the wheel some weeks later, several alterations having been made.

|                     |       |     |     |       |        |       |
|---------------------|-------|-----|-----|-------|--------|-------|
| Whole Gate. . . . . | 17.94 | 285 | 352 | 30.40 | 981.46 | .9141 |
|---------------------|-------|-----|-----|-------|--------|-------|

The results obtained from a 23-inch Boyden wheel, price \$500, tested in the same place and under precisely the same conditions is here given. The Boyden wheel, however, had a sort of flanged gate specially fitted for the trial. With the ordinary gate, the results are shown in the lowest table. Made at Ames Works.

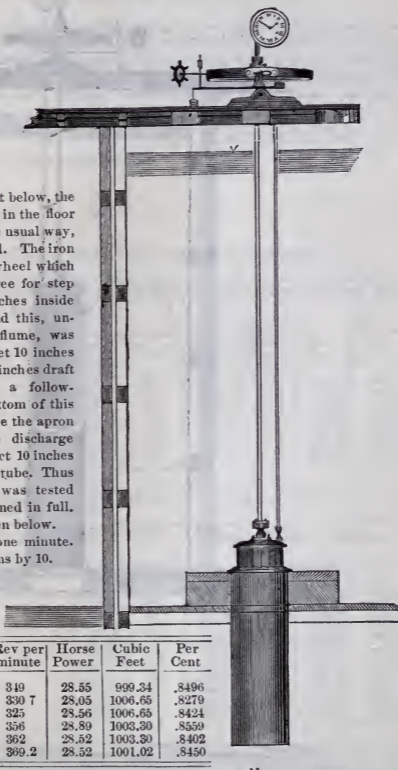
|                          |       |     |       |       |        |       |
|--------------------------|-------|-----|-------|-------|--------|-------|
| Best Whole Gate. . . . . | 18.16 | 195 | 263.5 | 15.21 | 553.15 | .8364 |
| Part Gate. . . . .       | 18.14 | 155 | 263   | 12.35 | 477.27 | .7551 |
| " " . . . . .            | 18.29 | 75  | 264   | 6.00  | 325.49 | .5336 |
| Whole Gate. . . . .      | 18.25 | 195 | 257.5 | 15.21 | 545.79 | .8084 |
| Part Gate. . . . .       | 18.33 | 75  | 259.5 | 5.87  | 380.63 | .4973 |

## Draft Tube in Backwater.

Experiment to determine whether a draft tube causes a loss of efficiency during backwater.

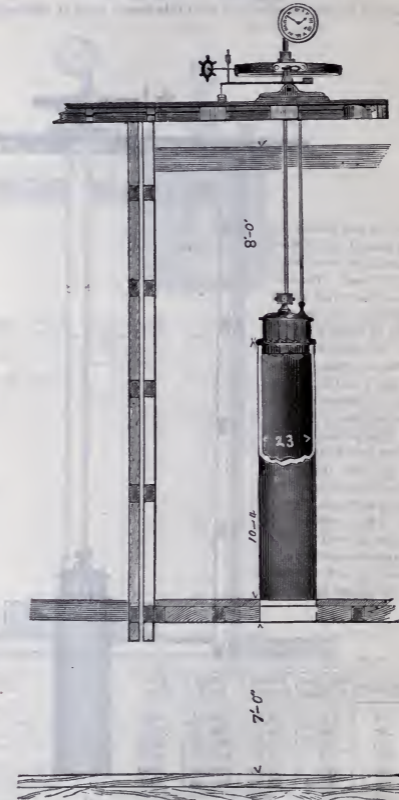
To make the test below, the wheel was placed in the floor of the flume in the usual way, under the full head. The iron draft tube of the wheel which held the bridge-tree for step was about 21 inches inside diameter. Around this, underneath floor of flume, was placed a piece 6 feet 10 inches in length of the 23 inches draft tube described on a following page. The bottom of this was 22 inches above the apron of wheel pit, the discharge being through 6 feet 10 inches of submerged draft tube. Thus placed, the wheel was tested with the gate opened in full. Results may be seen below.

Data below for one minute. Multiply revolutions by 10.



| Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-------|--------|----------------|-------------|------------|----------|
| 17.80 | 270    | 349            | 28.55       | 999.34     | .8496    |
| 17.80 | 280    | 330.7          | 28.05       | 1006.65    | .8279    |
| 17.81 | 290    | 325            | 28.56       | 1006.65    | .8424    |
| 17.81 | 265    | 356            | 28.89       | 1003.30    | .8559    |
| 17.83 | 260    | 362            | 28.52       | 1003.30    | .8402    |
| 17.84 | 255    | 369.2          | 28.52       | 1001.02    | .8450    |

## Draft Tube Experiments.



In preparing for these tests, the wheel was placed 10 feet above the flume floor upon the top of a draft tube 23 inches inside diameter, 10 feet 4 inches in length. Results on opposite page.

DEPARTMENT OF THE INTERIOR, UNITED STATES PATENT OFFICE,  
Washington, D. C., June 17th, 1880.

SIR: In reply to your letter of 14th inst., you are informed that the records of this office show that the first patent granted for "Draft Tube for Water Wheels" was issued June 28th, 1840, No. 1658. It appears to have been the invention of Zebulon and Austin Parker of Licking Co., Ohio. The patent was issued to Zebulon Parker and R. McKilby, administrator of Austin Parker, deceased.

Respectfully yours,

F. A. SEELEY, *Chief Clerk.*

JAMES EMERSON, Willimansett, Mass.

Tests of 15 inch wheel placed as shown on opposite page.

The wheel was far less steady during this trial than when placed at the bottom of the flume. As the tube was surrounded by 8 feet of water, of course there was no leakage of air.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 17.73 | 285    | 322            | 27.80       | 959.51     | .8651    |
| " " . . . . .       | 17.77 | 295    | 307.5          | 27.48       | 957.85     | .8548    |
| " " . . . . .       | 17.77 | 305    | 291.5          | 26.94       | 961.18     | .8352    |
| " " . . . . .       | 17.79 | 270    | 345            | 28.22       | 954.52     | .8799    |
| " " . . . . .       | 17.78 | 275    | 336.2          | 28.02       | 954.52     | .8741    |
| " " . . . . .       | 17.79 | 280    | 326            | 27.66       | 961.18     | .8369    |
| " " . . . . .       | 17.80 | 275    | 338.5          | 28.20       | 957.85     | .8737    |

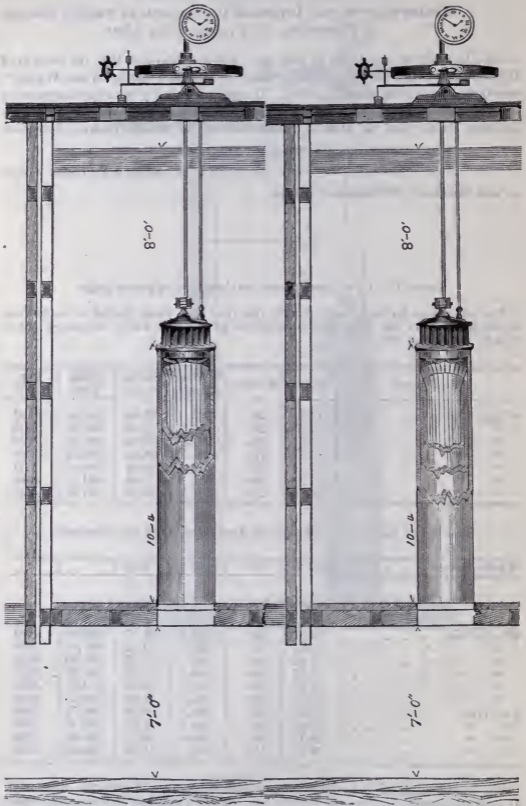
Test of the same, the lower end of draft tube being unsubmerged.

|                     |       |     |     |      |  |  |
|---------------------|-------|-----|-----|------|--|--|
| Whole Gate. . . . . | 17.80 | 100 | 266 | 8.06 |  |  |
|---------------------|-------|-----|-----|------|--|--|

Second test of the same draft tube taken several days later.

|                     |       |     |       |       |        |       |
|---------------------|-------|-----|-------|-------|--------|-------|
| Whole Gate. . . . . | 17.91 | 200 | 349.3 | 21.17 | 869.88 | .7194 |
| " " . . . . .       | 17.87 | 230 | 356.2 | 24.82 | 937.09 | .7848 |
| " " . . . . .       | 17.82 | 250 | 362   | 27.42 | 957.00 | .8512 |
| " " . . . . .       | 17.81 | 260 | 354.5 | 27.93 | 967.12 | .8585 |
| " " . . . . .       | 17.81 | 270 | 341.7 | 27.95 | 974.77 | .8523 |
| " " . . . . .       | 17.79 | 280 | 325.5 | 27.62 | 983.75 | .8356 |
| Part Gate. . . . .  | 17.96 | 200 | 328.5 | 19.90 | 789.75 | .7428 |
| " " . . . . .       | 17.95 | 190 | 340.7 | 19.61 | 783.43 | .7383 |
| " " . . . . .       | 18.11 | 100 | 356.6 | 10.80 | 550.66 | .5733 |
| " " . . . . .       | 18.11 | 110 | 345   | 11.50 | 549.22 | .6122 |

The wheel was more difficult to control with brake than during the first trial. It took a long time to clear the tube of air. Quite a number of tests were taken before anything like the power due the head could be obtained, though they were not recorded.



## Reduced Draft Tube.

Test with 19-inch draft tube.

During this test the wheel was placed at the top of the before mentioned 23-inch draft tube, that having been diminished in diameter by the insertion of a lining 2 inches in thickness, leaving the inside diameter of tube 19 inches in the clear, and 10 feet 4 inches in length as before; and, as before, about 8 feet of the head above the wheel.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent. |
|---------------------|-------|--------|----------------|-------------|------------|-----------|
| Whole Gate. . . . . | 17.90 | 250    | 354            | 26.81       | 959.52     | .8264     |
| " " . . . . .       | 17.88 | 260    | 337.5          | 26.57       | 961.18     | .8185     |
| " " . . . . .       | 17.89 | 270    | 324.2          | 26.52       | 964.50     | .8137     |
| " " . . . . .       | 17.89 | 280    | 309            | 26.21       | 966.17     | .8029     |
| " " . . . . .       | 17.88 | 240    | 365            | 26.54       | 957.86     | .8204     |

Test of the above arrangement the lower end of tube being unsubmerged.

|                     |  |     |     |       |  |  |
|---------------------|--|-----|-----|-------|--|--|
| Whole Gate. . . . . |  | 130 | 369 | 14.53 |  |  |
| " " . . . . .       |  | 140 | 367 | 15.57 |  |  |

## Draft Tube Again Reduced.

Test with 15-inch draft tube.

Continuation of the same arrangement of tubes as before, another lining having been inserted, leaving inside diameter of tube 15 inches; length, 10 feet 4 inches, as before.

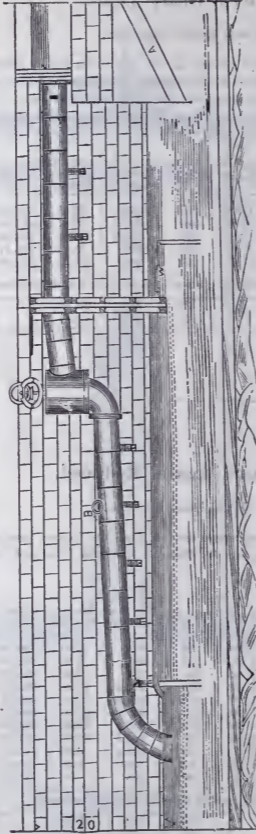
| Gate Opened                   | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent. |
|-------------------------------|-------|--------|----------------|-------------|------------|-----------|
| Whole Gate. . . . .           | 17.88 | 200    | 376            | 22.81       | 890.78     | .7584     |
| " " . . . . .                 | 17.87 | 225    | 336            | 22.90       | 898.97     | .7546     |
| " " . . . . .                 | 17.85 | 250    | 296            | 22.42       | 905.53     | .7339     |
| " " . . . . .                 | 17.86 | 240    | 310.6          | 22.58       | 905.53     | .7391     |
| " " . . . . .                 | 17.86 | 230    | 324.5          | 22.61       | 902.25     | .7429     |
| " " . . . . .                 | 17.86 | 220    | 339.5          | 22.63       | 898.97     | .7462     |
| " " . . . . .                 | 17.86 | 210    | 355.5          | 22.62       | 894.05     | .7500     |
| " " . . . . .                 | 18.08 | 125    | 338.5          | 12.82       | 591.92     | .6343     |
| Gate open two-thirds. . . . . | 18.24 | 70     | 322.5          | 6.84        | 415.42     | .4779     |
| " " one-half. . . . .         | 18.24 | 65     | 329.2          | 6.48        | 415.42     | .4527     |
| " " one-half. . . . .         | 18.24 | 60     | 338            | 6.14        | 411.37     | .4333     |

Test with the lower end of draft tube unsubmerged.

|                     |  |     |     |       |  |  |
|---------------------|--|-----|-----|-------|--|--|
| Whole Gate. . . . . |  | 200 | 365 | 22.30 |  |  |
| " " . . . . .       |  | 225 | 323 | 22.02 |  |  |

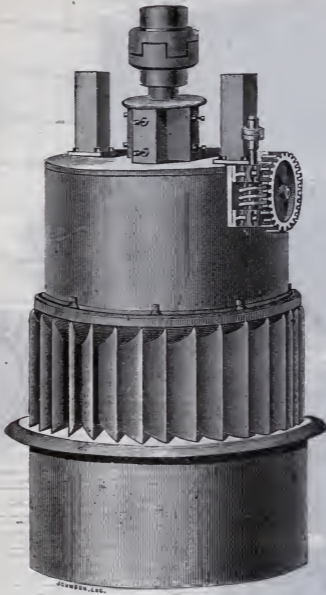


## Elevation of Testing Flume and Draft Tube.



The Draft tube represented above along the side of flume and over the measuring pit, was so constructed that the water passing through it might be discharged below the weir, in order to allow a continued use of the wheel, with which the experiments were made, to add to the power used in the Whiting Paper Mill, near by. As may be seen, the water enters the round iron trunk above the flume. This trunk is four feet in diameter and about fifty feet in length to the wheel case, A. From the wheel case, the draft tube four feet in diameter, descending one foot in forty, carries the discharge over the weir, a distance of about fifty feet from the wheel. A 27-inch Hercules wheel, having a plain unflanged cylinder gate, was first tested in the ordinary way in the testing flume—the wheel standing in the opening of the floor, marked W. The results may be seen in the upper table on the opposite page. In the same place, with twenty feet head, the wheel would give 104 h. p., and make about 193 revolutions per minute. After the test in the flume, the wheel was placed in the curb, A, and the brake was applied at the top of shaft fitted for the crown gear. The results given in the lower table on opposite page show the efficiency of that style of draft tube.

## The Hercules.



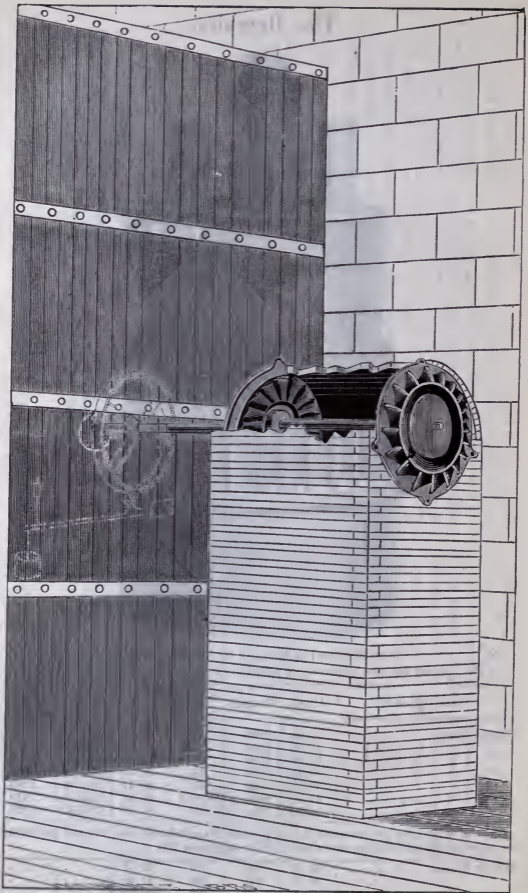
Test of wheel in flume in the ordinary way.

Data below for one minute. Multiply revolutions by 15. Dec. 6, 1879.

| Gate opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet. | Per Cent |
|---------------------|-------|--------|----------------|-------------|-------------|----------|
| Whole Gate. . . . . | 17.09 | 1000   | 177.3          | 80.59       | 3264.21     | .7648    |
| " " . . . . .       | 17.13 | 1050   | 167.5          | 79.94       | 3288.37     | .7514    |
| " " . . . . .       | 17.02 | 1100   | 157.5          | 78.75       | 3288.37     | .7450    |
| " " . . . . .       | 17.15 | 950    | 190            | 82.04       | 3240.09     | .7817    |
| " " . . . . .       | 17.16 | 900    | 199            | 81.41       | 3205.72     | .7835    |
| " " . . . . .       | 17.16 | 975    | 182.5          | 80.88       | 3233.21     | .7719    |
| " " . . . . .       | 17.16 | 925    | 194            | 81.56       | 3216.02     | .7824    |

Test of wheel for power after it was placed in the wheel case, A, and previous to its being geared to the machinery in the mill near by.

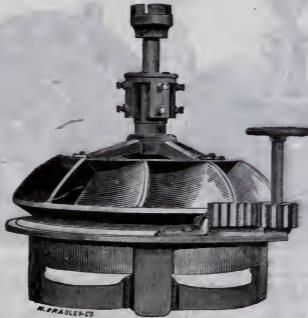
|                     |       |     |     |       |           |           |
|---------------------|-------|-----|-----|-------|-----------|-----------|
| Whole Gate. . . . . | 20.00 | 900 | 173 | 70.77 | . . . . . | . . . . . |
| " " . . . . .       | 20.00 | 850 | 184 | 71.09 | . . . . . | . . . . . |
| " " . . . . .       | 20.00 | 800 | 188 | 68.36 | . . . . . | . . . . . |



**View of Testing Flume, Horizontal Wheels and Draft Tube.**

## Curtis Wheel.

Sent by Gates Curtis, Ogdensburg, N. Y.



The results in the table below were obtained from the test of a 35-inch wheel upon upright shaft in the usual way. The inside register gate had been left out, so the chutes were open in full and the water was applied by the head gates of testing flume.

Data below for one minute. Multiply revolutions by 15. Oct. 22, 1879.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 17.69 | 2225   | 000            | 000         | 3115.69    | .0000    |
| " " . . . . .       | 17.77 | 900    | 193            | 78.95       | 2905.30    | .8096    |
| " " . . . . .       | 17.77 | 1000   | 179            | 81.36       | 2935.63    | .8258    |
| " " . . . . .       | 17.75 | 1100   | 165.5          | 82.75       | 2950.83    | .8365    |
| " " . . . . .       | 17.74 | 1200   | 152            | 82.90       | 2981.29    | .8300    |
| " " . . . . .       | 17.73 | 1300   | 138.5          | 81.82       | 3004.21    | .8133    |
| " " . . . . .       | 17.75 | 1050   | 171.2          | 81.70       | 2954.63    | .8248    |
| " " . . . . .       | 17.74 | 1150   | 159            | 83.11       | 2966.05    | .8363    |
| " " . . . . .       | 17.80 | 100    | 273.5          | 12.43       | 2574.47    | .0000    |

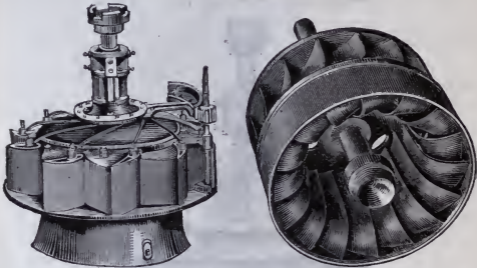
After the above test, the same wheel, with a left-hand mate of the same supposed efficiency, was fixed upon a horizontal shaft, then placed in the flume at the top of a square draft tube ten feet in height, as shown on the opposite page. The draft tube and fittings were furnished by Mr. Curtis, and upon the same scale that he had furnished for other wheels of the kind for mills. The dotted lines in bulk-head show the application of the brake for testing. The same may perhaps be more clearly seen in the illustration of Measuring Pit in the first part of this report.

Data below for one minute. Multiply revolutions by 20.

|                     |       |      |       |        |         |       |
|---------------------|-------|------|-------|--------|---------|-------|
| Whole Gate. . . . . | 16.23 | 1500 | 141   | 128.18 | 5794.09 | .7204 |
| " " . . . . .       | 16.38 | 1400 | 150.5 | 127.70 | 5779.76 | .7144 |
| " " . . . . .       | 16.37 | 1450 | 146   | 127.42 | 5788.43 | .6940 |
| " " . . . . .       | 16.37 | 1500 | 140.6 | 127.81 | 5817.38 | .7089 |
| " " . . . . .       | 16.40 | 1350 | 151   | 126.81 | 5761.51 | .7106 |
| " " . . . . .       | 16.39 | 1300 | 159.2 | 125.43 | 5738.27 | .7161 |

## New American Wheel.

30-inch wheel, sent by Stout, Mills & Temple, Dayton, Ohio.



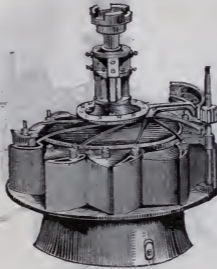
Tests made to ascertain whether flaring the ordinary draft tube of a turbine at the bottom adds to its efficiency. During this trial the water, in passing through the wheel, made a constant rumbling or humming sound, whether the wheel was running or held stationary by the brake.

Data below for one minute. Multiply revolutions by 15. July 2, 1880.

|   | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent. |
|---|-------|--------|----------------|-------------|------------|-----------|
| Whole Gate 10 $\frac{1}{2}$ in. or 72 turns | 17.75 | 1100   | 000            | 000         | 2504.00    | 000       |
| " " . . . . .                               | 17.75 | 650    | 209.3          | 61.83       | 2389.50    | .7735     |
| " " . . . . .                               | 17.74 | 700    | 199            | 63.31       | 2424.32    | .7793     |
| " " . . . . .                               | 17.74 | 750    | 186.5          | 63.57       | 2478.42    | .7655     |
| " " . . . . .                               | 17.73 | 800    | 175.5          | 63.81       | 2539.27    | .7523     |
| " " . . . . .                               | 17.71 | 850    | 163            | 62.72       | 2574.71    | .7284     |
| " " . . . . .                               | 17.77 | 675    | 207.5          | 63.66       | 2430.66    | .7803     |
| " " . . . . .                               | 17.73 | 725    | 194            | 63.93       | 2478.42    | .7703     |
| Part Gate.                                  | 17.84 | 650    | 203            | 59.98       | 2267.22    | .7852     |
| " " . . . . .                               | 17.81 | 675    | 202            | 61.97       | 2354.82    | .7823     |
| " " . . . . .                               | 17.85 | 675    | 201.6          | 61.85       | 2329.69    | .7874     |
| " " . . . . .                               | 17.87 | 650    | 206.5          | 61.02       | 2261.00    | .7997     |
| " " . . . . .                               | 17.89 | 625    | 207.5          | 58.94       | 2202.14    | .7922     |
| " " . . . . .                               | 17.91 | 600    | 208.5          | 53.86       | 2113.18    | .7954     |
| " " . . . . .                               | 17.91 | 610    | 206.5          | 57.25       | 2128.44    | .7961     |
| " " . . . . .                               | 17.90 | 610    | 205.5          | 56.97       | 2116.23    | .7962     |
| " " . . . . .                               | 17.90 | 600    | 207.5          | 56.89       | 2091.86    | .8044     |
| " " . . . . .                               | 17.94 | 580    | 207.5          | 54.70       | 2013.23    | .8017     |
| " " . . . . .                               | 17.92 | 600    | 202            | 55.09       | 2031.30    | .8012     |
| " " . . . . .                               | 17.97 | 550    | 207.5          | 51.87       | 1914.68    | .7980     |
| " " . . . . .                               | 17.96 | 550    | 205            | 51.25       | 1896.82    | .7963     |
| " " . . . . .                               | 18.04 | 500    | 207            | 47.04       | 1759.40    | .7861     |
| " " . . . . .                               | 18.01 | 525    | 202            | 48.20       | 1794.24    | .7904     |
| " " . . . . .                               | 18.04 | 500    | 205            | 46.57       | 1727.66    | .7912     |
| " " . . . . .                               | 18.11 | 430    | 209.5          | 40.97       | 1561.16    | .7673     |
| " " . . . . .                               | 18.10 | 440    | 206.5          | 41.30       | 1577.00    | .7661     |
| " " . . . . .                               | 18.10 | 450    | 205.5          | 42.34       | 1589.21    | .7793     |
| " " . . . . .                               | 18.09 | 475    | 199            | 42.96       | 1613.56    | .7792     |
| " " . . . . .                               | 18.17 | 390    | 208            | 36.84       | 1443.91    | .7434     |
| " " . . . . .                               | 18.16 | 400    | 205.5          | 37.36       | 1427.51    | .7631     |
| " " . . . . .                               | 18.24 | 335    | 206            | 31.36       | 1234.86    | .7372     |

The average efficiency from half to whole gate, .779

## New American Wheel.



30-inch wheel.

Retest of the wheel after slightly reducing its diameter, as it was found to have touched the curb during the former trial. As may be seen, this change raised the whole gate efficiency at the expense of that of the part gate.

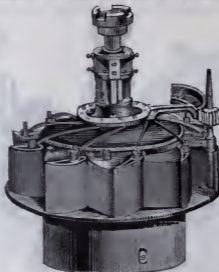
Data below for one minute. Multiply revolutions by 15. July 7, 1880.

| Gate Opened                      | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent. |
|----------------------------------|-------|--------|----------------|-------------|------------|-----------|
| Whole Gate 10½ in or 72 turns    | 17.67 | 675    | 210.4          | 64.55       | 2487.94    | .7774     |
| " " " " " "                      | 17.64 | 685    | 208.5          | 64.92       | 2494.32    | .7812     |
| " " " " " "                      | 17.65 | 700    | 203            | 64.59       | 2507.07    | .7727     |
| " " " " " "                      | 17.63 | 715    | 201.5          | 65.46       | 2513.46    | .7821     |
| Gate open 8 1-16 in. or 59 turns | 17.67 | 700    | 200.5          | 63.79       | 2405.55    | .7964     |
| " " " " " "                      | 17.71 | 675    | 203            | 62.28       | 2349.00    | .7926     |
| " " " " " "                      | 17.72 | 650    | 209.5          | 61.90       | 2323.99    | .7958     |
| " " " 7½ " 55 "                  | 17.75 | 650    | 202.5          | 59.83       | 2286.62    | .7804     |
| " " " " " "                      | 17.74 | 640    | 208.5          | 60.66       | 2268.01    | .7983     |
| " " " " " "                      | 17.72 | 675    | 200            | 61.36       | 2299.06    | .7976     |
| " " " 7 " 51 "                   | 17.77 | 650    | 201.2          | 59.44       | 2212.41    | .7990     |
| " " " " " "                      | 17.77 | 630    | 207            | 59.27       | 2200.12    | .8027     |
| " " " 6½ " 47 "                  | 17.81 | 625    | 204            | 57.95       | 2141.97    | .8042     |
| " " " " " "                      | 17.80 | 645    | 198            | 55.02       | 2151.12    | .7608     |
| " " " " " "                      | 17.81 | 600    | 206.7          | 56.37       | 2135.87    | .7845     |
| " " " 5 15-16 " 43 "             | 17.85 | 575    | 205            | 53.58       | 2018.06    | .7875     |
| " " " " " "                      | 17.85 | 560    | 208            | 52.94       | 2009.08    | .7816     |
| " " " " " "                      | 17.84 | 600    | 201            | 54.81       | 2036.06    | .7989     |
| " " " 5 5-16 " 39 "              | 17.92 | 525    | 206            | 49.15       | 1890.44    | .7681     |
| " " " " " "                      | 17.90 | 545    | 204            | 50.53       | 1899.26    | .7869     |
| " " " 4½ " 35 "                  | 17.97 | 500    | 203            | 46.13       | 1765.26    | .7700     |
| " " " " " "                      | 17.96 | 490    | 204            | 45.43       | 1759.50    | .7611     |
| " " " " " "                      | 17.96 | 480    | 207            | 45.16       | 1750.86    | .7604     |
| " " " 4½ " 31 "                  | 18.03 | 465    | 197            | 41.63       | 1639.76    | .7482     |
| " " " " " "                      | 18.04 | 450    | 203            | 41.52       | 1631.30    | .7471     |
| " " " 3½ " 27 "                  | 18.11 | 390    | 206            | 36.51       | 1453.89    | .7358     |
| " " " " " "                      | 18.12 | 400    | 203            | 36.90       | 1473.00    | .7319     |
| " " " 2 15-16 " 23 "             | 18.17 | 300    | 220            | 30.00       | 1251.00    | .6988     |
| " " " " " "                      | 18.16 | 335    | 285.5          | 31.44       | 1292.99    | .7089     |
| " " " " " "                      | 18.16 | 350    | 200.5          | 31.90       | 1293.00    | .7192     |

Average, .771



## New American Wheel.



30-inch Wheel.

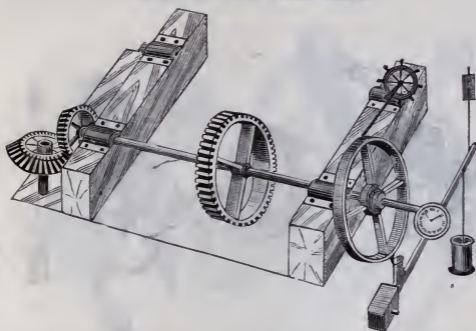
Retest of the same wheel after changing the flaring for a straight draft tube. The gate openings were the same through the three trials. The  $10\frac{1}{2}$  inches at whole gate means the extreme swing of gate, the openings at outer end of chutes being  $7\frac{1}{2}$  inches only; but the gate had to move the distance named to clear the openings. The averages are found by adding the thirty tests of each trial together and dividing by that number.

Data below for one minute. Multiply revolutions by 15. July 8, 1880.

|  | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent. |
|--|-------|--------|----------------|-------------|------------|-----------|
| Whole Gate $10\frac{1}{2}$ in. or 72 turns | 17.73 | 675    | 209.8          | 64.37       | 2491.16    | .7715     |
| " " " " " " " "                            | 17.70 | 700    | 205.2          | 65.29       | 2500.72    | .7809     |
| " " " " " " " "                            | 17.68 | 725    | 198.5          | 65.41       | 2513.48    | .7794     |
| " " " " " " " "                            | 17.67 | 750    | 192.5          | 65.92       | 2545.04    | .7759     |
| Gate open 59 turns.                        | 17.77 | 675    | 203.5          | 62.43       | 2355.41    | .7900     |
| " " " " " " " "                            | 17.79 | 625    | 212            | 60.22       | 2252.75    | .7950     |
| " " " " " " " "                            | 17.79 | 650    | 206.5          | 60.71       | 2258.93    | .8000     |
| " " " " " " " "                            | 17.78 | 675    | 200            | 61.36       | 2289.92    | .7979     |
| " " " " 51 " " " "                         | 17.82 | 650    | 202            | 59.68       | 2225.00    | .7969     |
| " " " " " " " "                            | 17.81 | 625    | 207.5          | 58.94       | 2194.25    | .7984     |
| " " " " 47 " " " "                         | 17.85 | 600    | 208.5          | 56.86       | 2136.19    | .7895     |
| " " " " " " " "                            | 17.85 | 625    | 203.5          | 57.41       | 2145.33    | .7937     |
| " " " " " " " "                            | 17.85 | 650    | 197            | 58.20       | 2154.48    | .8012     |
| " " " " 43 " " " "                         | 17.90 | 575    | 208            | 54.36       | 2015.49    | .7978     |
| " " " " " " " "                            | 17.90 | 600    | 201.5          | 54.95       | 2151.48    | .7923     |
| " " " " 39 " " " "                         | 17.96 | 525    | 208            | 47.63       | 1885.29    | .7760     |
| " " " " " " " "                            | 17.96 | 550    | 206.5          | 51.62       | 1899.79    | .8009     |
| " " " " " " " "                            | 17.94 | 575    | 200            | 52.27       | 1952.93    | .7900     |
| " " " " 35 " " " "                         | 18.01 | 475    | 211            | 45.56       | 1751.52    | .7647     |
| " " " " " " " "                            | 18.00 | 500    | 206            | 46.00       | 1786.09    | .7574     |
| " " " " " " " "                            | 18.00 | 525    | 201            | 47.96       | 1806.35    | .7810     |
| " " " " 31 " " " "                         | 18.06 | 425    | 211.5          | 40.85       | 1599.41    | .7488     |
| " " " " " " " "                            | 18.05 | 450    | 207.5          | 42.44       | 1632.08    | .7629     |
| " " " " " " " "                            | 18.04 | 475    | 198            | 42.75       | 1666.00    | .7531     |
| " " " " 27 " " " "                         | 18.12 | 375    | 213.2          | 36.34       | 1454.85    | .7299     |
| " " " " " " " "                            | 18.11 | 400    | 207.5          | 37.72       | 1484.90    | .7426     |
| " " " " " " " "                            | 18.09 | 425    | 200            | 38.63       | 1509.60    | .7489     |
| " " " " 23 " " " "                         | 18.17 | 325    | 216.5          | 31.97       | 1308.32    | .7119     |
| " " " " " " " "                            | 18.18 | 350    | 208            | 33.09       | 1328.49    | .7253     |
| " " " " " " " "                            | 18.17 | 375    | 200            | 34.09       | 1363.11    | .7287     |

Average, .774

## Experiments with Gears.



Test of gears continued, the arrangement of gears named on previous page being reversed, or the small gear having 26 teeth being on turbine shaft, that of 46 teeth on "Jack Shaft"—gears being worked without lubrication of any kind. Data below for one minute. Multiply revolutions by 10.

| Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-------|--------|----------------|-------------|------------|----------|
| 18.10 | 210    | 267.5          | 17.02       | 882.34     | .5642    |
| 18.08 | 220    | 261.5          | 17.43       | 898.69     | .5712    |
| 18.07 | 230    | 256            | 17.84       | 896.95     | .5826    |
| 18.07 | 240    | 253            | 18.40       | 898.58     | .6000    |
| 18.06 | 250    | 248.5          | 18.82       | 901.84     | .6117    |
| 18.05 | 260    | 245            | 19.30       | 910.00     | .6221    |
| 18.03 | 270    | 241            | 19.71       | 923.10     | .6270    |
| 18.03 | 280    | 239.2          | 20.95       | 926.38     | .6650    |
| 18.04 | 290    | 237.5          | 20.87       | 926.38     | .6613    |
| 18 03 | 300    | 230.5          | 20.95       | 928.02     | .6628    |

Test of above named arrangement of gears, the gears being well oiled.

|       |     |       |       |        |       |
|-------|-----|-------|-------|--------|-------|
| 17.83 | 350 | 229   | 24.28 | 902.45 | .7989 |
| 17.81 | 400 | 221   | 26.78 | 937.06 | .8494 |
| 17.78 | 425 | 213   | 27.43 | 962.00 | .8490 |
| 17.77 | 450 | 204   | 27.81 | 968.68 | .8555 |
| 17.76 | 475 | 196   | 28.21 | 972.00 | .8653 |
| 17.75 | 500 | 187   | 28.33 | 978.71 | .8634 |
| 17.74 | 525 | 173.5 | 27.60 | 798.71 | .8416 |

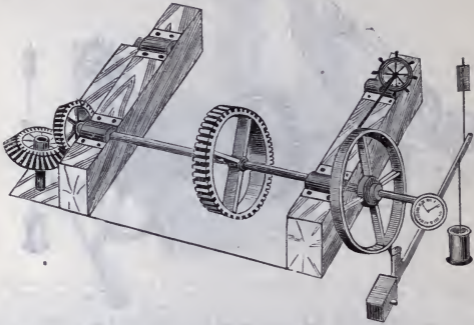
Verification of the same arrangement of gears taken several days later.

|       |       |       |       |        |       |
|-------|-------|-------|-------|--------|-------|
| 18.02 | 475   | 197.5 | 28.42 | 963.56 | .8665 |
| 18.03 | 525   | 176.5 | 28.07 | 969.63 | .8500 |
| 18.02 | 512.5 | 180.6 | 28.04 | 971.31 | .8482 |
| 18.05 | 500   | 187.8 | 28.45 | 973.59 | .8571 |

During the above tests, the teeth of the gears ran rather close together, though perfectly free and were correctly placed according to the opinion of experts in such matters. They were separated about 1-16 in. more, then gave the results below.

|       |     |       |       |        |       |
|-------|-----|-------|-------|--------|-------|
| 18.02 | 500 | 191.5 | 29.01 | 972.67 | .8762 |
| 17.99 | 510 | 187.5 | 28.97 | 979.33 | .8706 |
| 18.00 | 520 | 184.2 | 29.02 | 981.00 | .8700 |

## Experiments with Gears.



Tests made for the purpose of ascertaining the loss of power in transmission through gears. To make these the brake, as shown above, was placed upon one end of a horizontal shaft, representing "Jack Shaft," the other end being connected to the turbine shaft in the usual way by bevel gears. These gears, shafts and fittings were generously furnished for the purpose by the Messrs. Poole & Hunt, of Baltimore, Md. Other gear makers were applied to but none of them seemed willing to submit their gears to such trial. Plain cast gears with unfinished surfaces were furnished. The workmanship of the gears, shafts and boxes was pronounced by experts to be excellent and superior to the average work of the kind furnished in this vicinity. The form of the teeth of the gears was invariably approved. With every change of gears, experts were called in to examine their position and condition. During these experiments the largest gear, which had 46 teeth, was used upon the turbine shaft as crown gear, while the smallest, which had 26 teeth, was on the horizontal or "Jack Shaft." The bearings were kept well oiled, but, as it is a common idea with gear makers that the teeth of gears *roll* together so that they work just as easy when dry as when well lubricated, the first trial was made with dry gears. The table below shows results.

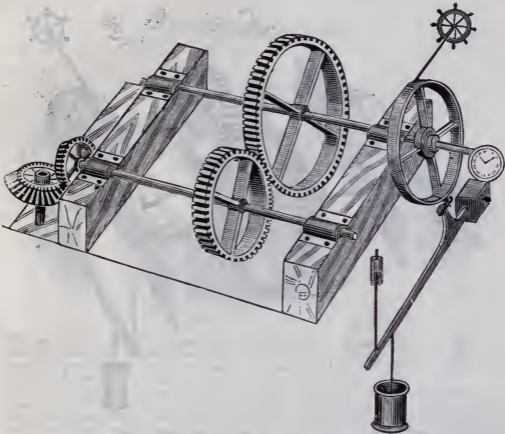
Data below for one minute. Multiply revolutions by 10.

|  | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|--|-------|--------|----------------|-------------|------------|----------|
|  | 17.96 | 150    | 487.5          | 22.14       | 1012.14    | .6449    |
|  | 17.98 | 125    | 611.5          | 23.16       | 997.02     | .6840    |
|  | 17.96 | 135    | 564            | 23.07       | 997.02     | .6821    |
|  | 17.96 | 130    | 565            | 22.25       | 993.67     | .6601    |
|  | 17.96 | 120    | 612            | 22.25       | 995.34     | .6589    |

Test through same gears, the gears being thoroughly lubricated.

|  |       |     |     |       |        |       |
|--|-------|-----|-----|-------|--------|-------|
|  | 18.04 | 150 | 646 | 29.36 | 961.93 | .8957 |
|  | 18.04 | 160 | 606 | 29.38 | 966.04 | .8913 |
|  | 18.04 | 170 | 558 | 28.74 | 978.66 | .8619 |
|  | 18.03 | 180 | 506 | 27.60 | 976.14 | .8303 |
|  | 18.05 | 165 | 584 | 29.20 | 975.31 | .8779 |

## Experiments with Gears.



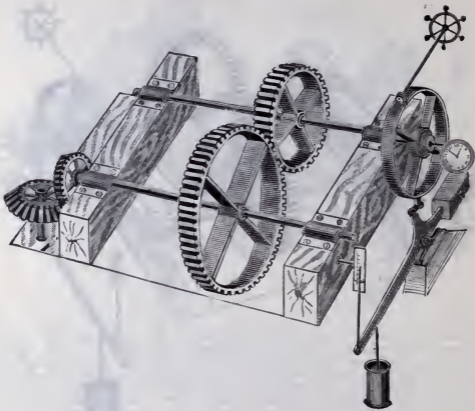
Test of gears continued, a second horizontal shaft being added to the previous arrangement described on foregoing page. This shaft, representing the main line of shafting through a mill, was connected to the "Jack Shaft" by a pair of spur gears—the large one, about 27 inches diameter,  $1\frac{1}{2}$  inches pitch, 5-inch face, having 49 teeth, was secured upon the second horizontal shaft or main line, and was driven by a gear on "Jack Shaft," same face and pitch as the above, and about  $16\frac{1}{2}$  inches diameter, having 30 teeth. The brake was placed upon the end of second line, the power of wheel being transmitted through the two pairs of gears, as represented above.

Data below for one minute. Multiply revolutions by 10.

|  | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|--|-------|--------|----------------|-------------|------------|----------|
|  | 17.94 | 300    | 165.5          | 15.16       | 841.18     | .5319    |
|  | 17.91 | 350    | 158.5          | 16.81       | 857.35     | .5716    |
|  | 17.90 | 400    | 151            | 18.30       | 870.33     | .6234    |
|  | 17.87 | 500    | 139            | 21.06       | 906.32     | .6884    |
|  | 17.85 | 550    | 133.5          | 22.25       | 934.34     | .7064    |
|  | 17.84 | 600    | 126.5          | 23.00       | 947.68     | .7202    |
|  | 17.90 | 625    | 125            | 23.65       | 939.37     | .7443    |
|  | 17.90 | 675    | 118            | 24.13       | 956.01     | .7465    |
|  | 17.94 | 650    | 120            | 23.63       | 966.03     | .7219    |
|  | 17.85 | 700    | 109            | 23.12       | 964.36     | .7112    |

The gears were thoroughly lubricated with a mixture, used for the same purpose in a mill near by, probably composed of tallow and tar.

## Experiments with Gears.



Continuation of the combined spur and bevel gear experiments, the spur gears having been changed, the one having 49 teeth being placed upon the "Jack Shaft" and working into the one having 30 teeth on second horizontal shaft upon which the brake was placed—the small bevel gear being continued as crown gear through all these tests.

Data below for one minute. Multiply revolutions by 10.

| Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-------|--------|----------------|-------------|------------|----------|
| 17.86 | 270    | 310            | 25.36       | 972.87     | .7727    |
| 17.86 | 265    | 317.5          | 25.49       | 977.28     | .7731    |
| 17.84 | 260    | 323.5          | 25.52       | 971.21     | .7798    |
| 17.84 | 260    | 301.5          | 25.58       | 978.96     | .7755    |
| 17.84 | 290    | 277.5          | 24.47       | 985.61     | .7380    |
| 17.84 | 250    | 326.7          | 24.75       | 961.18     | .7641    |

Verification test, taken several days later.

|       |     |       |       |        |       |
|-------|-----|-------|-------|--------|-------|
| 18.03 | 275 | 305.1 | 25.42 | 980.22 | .7614 |
|-------|-----|-------|-------|--------|-------|

Another test of the same arrangement after being taken down, then reset.

|       |     |       |       |        |       |
|-------|-----|-------|-------|--------|-------|
| 17.66 | 285 | 278.5 | 24.05 | 972.68 | .7409 |
| 17.67 | 275 | 286.1 | 23.84 | 962.70 | .7419 |
| 17.69 | 265 | 304   | 24.41 | 964.36 | .7576 |
| 17.78 | 270 | 297.5 | 24.34 | 971.00 | .7504 |
| 17.82 | 275 | 296.5 | 24.41 | 974.33 | .7442 |
| 17.86 | 270 | 300.5 | 24.58 | 971.00 | .7504 |

## Belt Experiments.



To prepare for the experiments to determine the loss of power in transmission through belts, the wheel was raised in flume sufficiently to bring top of shaft above upper bearing, to give room for placing a 30-inch pulley thereon; this was done by adding another 10-inch platform to the first.

The wheel itself was first tested by placing the brake on the wheel shaft in the usual way. That it did not repeat the efficiency shown previously, was due to alterations made in the conditions. First, the step was altered somewhat in form, then the wheel was placed considerably above the floor of the flume for the purpose named above, and the difference in the head probably effected it; but the conditions, however, continued the same through the belt tests.

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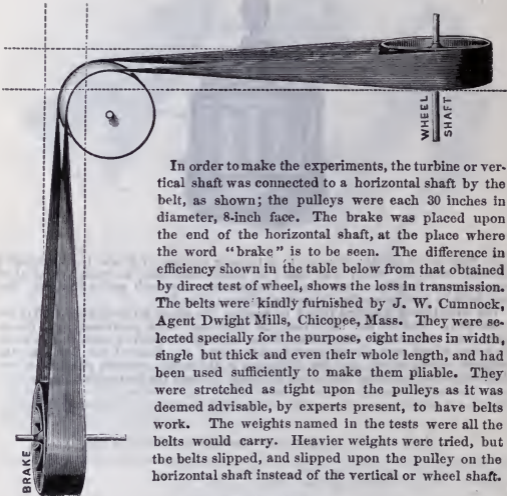
### Wheel Test.

Data below for one minute. Multiply revolutions of wheel by 10.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 12.03 | 150    | 292.5          | 13.29       | 735.43     | .7954    |
| " " . . . . .       | 12.00 | 170    | 278.5          | 14.34       | 740.05     | .8550    |
| " " . . . . .       | 11.97 | 185    | 270            | 15.13       | 760.16     | .8804    |
| " " . . . . .       | 11.95 | 200    | 239            | 14.48       | 772.61     | .8303    |
| " " . . . . .       | 11.94 | 195    | 247            | 14.59       | 772.61     | .8375    |
| " " . . . . .       | 11.95 | 190    | 262.5          | 15.11       | 771.06     | .8682    |
| " " . . . . .       | 11.96 | 180    | 271            | 14.78       | 763.27     | .8559    |



## Quarter-Turn Belt.



In order to make the experiments, the turbine or vertical shaft was connected to a horizontal shaft by the belt, as shown; the pulleys were each 30 inches in diameter, 8-inch face. The brake was placed upon the end of the horizontal shaft, at the place where the word "brake" is to be seen. The difference in efficiency shown in the table below from that obtained by direct test of wheel, shows the loss in transmission. The belts were kindly furnished by J. W. Cumnock, Agent Dwight Mills, Chicopee, Mass. They were selected specially for the purpose, eight inches in width, single but thick and even their whole length, and had been used sufficiently to make them pliable. They were stretched as tight upon the pulleys as it was deemed advisable, by experts present, to have belts work. The weights named in the tests were all the belts would carry. Heavier weights were tried, but the belts slipped, and slipped upon the pulley on the horizontal shaft instead of the vertical or wheel shaft.

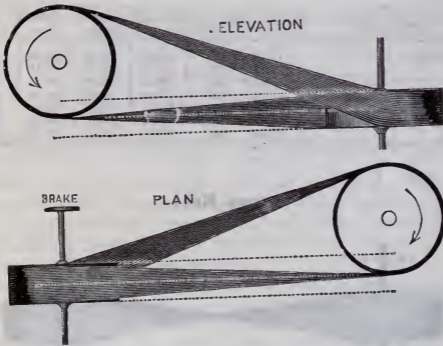
Whole length of belt, 46 feet.

Data below for one minute. Multiply revolutions by 10.

| Gate Opened |       | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|-------------|-------|-------|--------|----------------|-------------|------------|----------|
| Whole       | Gate. | 12.46 | 125    | 303            | 11.47       | 704.52     | .6154    |
| "           | "     | 12.42 | 135    | 279.5          | 11.43       | 787.66     | .6185    |
| "           | "     | 12.35 | 145    | 256            | 11.24       | 787.66     | .6116    |
| "           | "     | 12.28 | 155    | 236.5          | 11.11       | 803.96     | .5957    |
| "           | "     | 12.30 | 120    | 300            | 10.91       | 783.68     | .5992    |
| "           | "     | 12.27 | 130    | 285.8          | 11.25       | 788.24     | .6158    |

## Quarter-Twist Belt.

*Pulley, 30 inches in diameter; 8-inch face.*



Whole length of belt, about 35 feet.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 12.13 | 100    | 349.6          | 10.59       | 724.86     | .6376    |
| “ “ . . . . .       | 12.00 | 125    | 319.5          | 12.10       | 761.71     | .7009    |
| “ “ . . . . .       | 11.98 | 135    | 305            | 12.47       | 767.73     | .7177    |
| “ “ . . . . .       | 11.96 | 145    | 295            | 12.96       | 775.73     | .7396    |
| “ “ . . . . .       | 11.95 | 155    | 281.5          | 13.22       | 782.00     | .7490    |
| “ “ . . . . .       | 11.94 | 165    | 268            | 13.40       | 783.54     | .7584    |
| “ “ . . . . .       | 11.95 | 175    | 252            | 13.30       | 783.54     | .7521    |

## Open Belt.

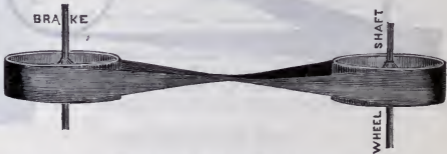


Whole length of this belt about 36 feet.

Data for one minute. Multiply revolutions by 10.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 12.23 | 150    | 324.2          | 14.73       | 769.49     | .8253    |
| " " . . . . .       | 12.11 | 175    | 286.2          | 15.17       | 785.11     | .8447    |
| " " . . . . .       | 12.05 | 190    | 260.5          | 14.99       | 789.81     | .8359    |
| " " . . . . .       | 11.99 | 180    | 273.5          | 14.92       | 788.24     | .8359    |
| " " . . . . .       | 11.98 | 185    | 261.5          | 14.66       | 788.24     | .8220    |
| " " . . . . .       | 11.97 | 170    | 273.5          | 14.08       | 780.36     | .7980    |
| " " . . . . .       | 11.96 | 165    | 289.2          | 14.47       | 788.24     | .8126    |

## Cross Belt.



Pulleys the same and in the same position as when tried with open belt.

| Gate Opened         | Head  | Weight | Rev per minute | Horse Power | Cubic Feet | Per Cent |
|---------------------|-------|--------|----------------|-------------|------------|----------|
| Whole Gate. . . . . | 12.03 | 150    | 311            | 14.13       | 774.17     | .8032    |
| " " . . . . .       | 11.99 | 160    | 291            | 14.10       | 778.85     | .7993    |
| " " . . . . .       | 11.97 | 170    | 271.5          | 13.98       | 783.54     | .7891    |
| " " . . . . .       | 11.96 | 180    | 251.5          | 13.71       | 788.24     | .7700    |
| " " . . . . .       | 11.99 | 140    | 317            | 13.45       | 769.49     | .7719    |

## EMERSON'S SAFETY CAR HEATING AND LIGHTING SYSTEM.

These plans are believed to be as perfect as human foresight can make such for the safety, comfort, and convenience of the traveling public, and employees of the roads, also for the convenience and economy of the companies.

From the successful production of the locomotive down, almost yearly attempts have been made to heat trains by steam from the locomotive ; such attempts for a generation in each case were soon abandoned.

Our cold winters have made traveling so uncomfortable for many months of each year that innumerable plans have been devised to obviate such discomfort.

The horrors caused by the yearly roasting of passengers have kept up the demand for safer methods, so that in many cases crude and unfit plans have been hastily adopted by many railway companies that render their cars excessively hot one hour, the next as much too cold, and so slow in operation as to be unfit for use during the changeable weather of the spring and fall months, as all who ride in the hot water heated drawing-room or sleeping cars at such seasons too well know. These plans are far more expensive and difficult to manage than those based upon skilled experience designed for use instead of to sell.

The past severe winter has kept the yard hands constantly employed thawing out pipes and the abortions called couplings, or in replacing the burst pipes and hose couplings, while cars, filled with shivering passengers, with frozen pipes, have often been compelled to run hundreds of miles without any means of heating whatever.

Were this a matter that could not be obviated, it, of course, would have to be endured, but such is far from being the case, for the system here recommended is the oldest, and has patiently been worked upon to perfect instead of to sell, and now is the cheapest, most convenient, safest, and most comfortable extant. The temperature of a car may be kept at any standard required, while frozen pipes or couplings are unknown, and no unsightly pipes, heating cylinders, or hose couplings are necessary outside of cars, which are often found so much in the way when changing trucks or making repairs. **No hose used in this system.**

### Emerson's New System of Car Heating.

My attention was called to the subject of car heating early in 1854. On Fast day of that year I wrote to the editor of the *Scientific American*, suggesting a plan of placing a small boiler in each car, connecting it with the locomotive boiler and a system of piping for warming the cars and operating the brakes. A written reply was returned in which it was stated that George Stephenson tried to warm trains from his locomotive but failed. Numerous inventions then in hand prevented me from proceeding with this at that time, but immediately after the Ashtabula horror I commenced to prepare plans for such heating, but it was difficult to find railroad managers willing to make a trial of them. The frightful holocaust in which Wagner was cremated, caused Mr. Mulligan, superintendent of the Connecticut River road, to offer me a train to experiment with. A small boiler was placed in the baggage car, the steam from which warmed three cars. The capacity of the boiler proved the practicability of taking the necessary quantity of steam from the locomotive boiler, and a change to that was immediately made.

I think that I may justly claim to be the first to produce a successful system for heating cars from the locomotive, and the only one who has produced a complete system for ordinary use and emergencies.

Mr. George A. Houston was sent by the managers of the Atchison, Topeka & Santa Fe R. R. Co., to examine and report upon the merits of the various systems. The substance of his report is here given.

BELOIT, Wis., March 30, 1887.

MR. W. B. STRONG, Pres. A., T. & S. F. R. R. Co., Boston, Mass.

*Dear Sir:*—Referring to the matter of warming cars, I have examined several systems now in use and being introduced for warming by steam, viz.: the MARTIN, the SEWALL, the EMERSON, and the GOLD. The C. R. R. Co. placed a train at my disposal to test the quantity of steam used for heating, this test made with four cars and during twelve hours. From this result, I am satisfied that cars can be warmed during a northern winter with an average of not to exceed three-fourths horse power of steam per car. This test was made with the EMERSON system, and I recommend the EMERSON system as the best.

Mr Houston's report was accepted, and train fitted up.

*Atchison, Topeka & Santa Fe Railroad Company,  
Topeka, Aug. 7, 1888.*

*James Emerson, Esq.*

*Dear Sir:*—Your letter to Mr. Hilton was handed me by him yesterday. In reply to same I will say that I continued to use the cars you fitted up until late in the spring. They gave entire satisfaction, did not have any trouble with them whatever. I think all cars fitted up should have coils put under the seats, as they can be heated so much quicker and kept more comfortable.

*I am, yours very respectfully,*

*Samuel Black,  
Conductor A., T. & S. F. R. R.*

Had Mr. Houston stopped after making his report all would have been well, but unfortunately he imagined himself to be a genius and persuaded the president of the road to be of the same opinion, so that Mr. Houston had entire control of the heating matter and it is safe to say that the botch he made of the matter stands unequalled. Thousands and tens of thousands of dollars were expended under his management, all of which with his plans are among the "Lost Arts."

## HEATING CARS BY STEAM.

At a railroad commissioners' hearing at Augusta, Maine, two years ago, the following replies were elicited to questions asked by the chairman:—

“Mr. Sewall, what provision have you made for heating the Pullman, Wagner, and other cars taken on to the train cold, that run over a given route, then stop off for a time but require a continuation of the heat during the stop-over?”

“Mr. Chairman, my plans are such that in an hour and forty-nine minutes from the time the cold car is taken to the train every pipe in the car will be warm.”

“Well, Mr. Martin, how about your plans?”

“Mr. Chairman, in one hour and forty-six minutes from the time the heating steam is let into the car every pipe will be warm.”

“Well, Mr. Emerson, how about your plans?”

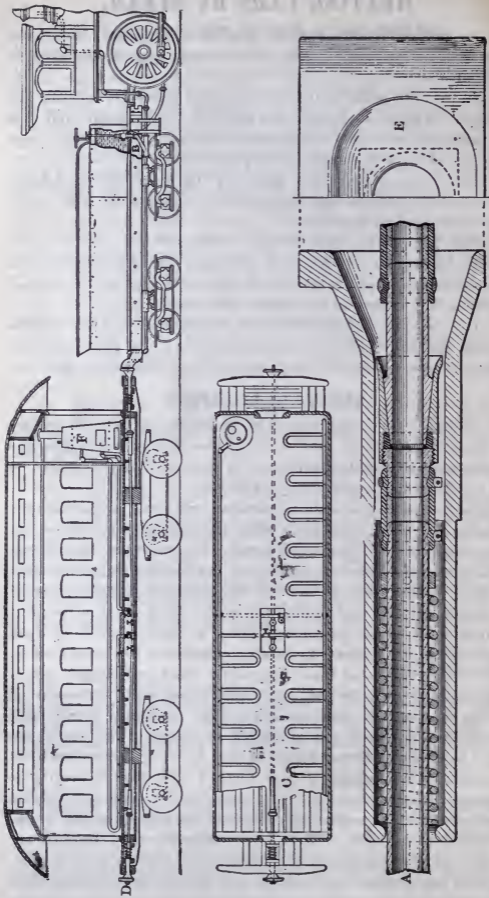
“Mr. Chairman, and Gentlemen of the Committee, in two minutes from the time the steam is let into the car every pipe will be hot, and in ten minutes the car will be as warm as it is desirable to have it.”

## ELECTRIC LIGHTING.

For seven years a train lighted by electricity has been in constant use upon the C. R. R., and recent improvements in dynamos and engines have rendered lighting cars by electricity as practicable as it is for cities, mills, stores, and dwellings.

Six or seven years since a universal cry went out to have the “deadly car stove” done away with, which was done, but the far more dangerous oil lamps still remain, and yearly we hear of collisions and trains being set on fire by the locomotive and wonder how it is possible that the inclosed fire of the locomotive can come in contact with the woodwork of the train so as to set it on fire; but the frightened passengers of the 9.30 A. M. train on the C. R. road had a chance to witness the *modus operandi* a few weeks since. The locomotive of that train jumped the track and dashed into a train standing upon the next track, the “head light” was smashed and its oil scattered over the hot boiler. Instantly the forward half of the locomotive was enveloped in a sheet of fire which continued to burn a sufficient length of time to set ordinary cord wood on fire, to say nothing of cars covered with varnish nearly as inflammable as gunpowder. Only from the fact that the collision caused a recoil and separation of trains was a firing of the trains prevented at that time. There is no excuse for the continued use of oil or gas for lighting at this time, for it may be done by electricity at less expense and trouble, and the railroad commissioners are derelict in their duty in allowing it to be done, for prevention is better than excuses after a catastrophe.





**A**, supply pipe. **B**, injector for filling heater. **C**, sliding joint in supply pipe. **D**, buffer. **E**, end view of buffer. **F**, heater.

## TO RAILROAD MANAGERS.

*Gentlemen, why not save and utilize your Hot Water Heaters ?*

The system of piping found best for such after thirty years' experience is far better adapted for rapid and economical car heating than the system of piping employed by Sewall, Martin, or Gold, and at small expense may easily be so arranged that steam from the locomotive may be substituted for the hot water circulation or the hot water circulation restored at will.

The change either way is easily made, without attracting attention, while the train is running.

No trap of any kind is needed, for the temperature is controlled inside of car at any time when in use.

When heating from locomotive the fire is drawn from heater and water from the pipes.

Half an hour before stopping car for night or long detachment from locomotive, open all valves and **blow all condensation from pipes by hot steam from locomotive.**

Leave all valves open until steam again enters pipes for heating.

A few minutes before arriving at a place where a car is to be set off and kept warm, fill pipes with water from the tender, start the fire in heater, and the hot water circulation is at once restored.

This was done at first by taking hot water from the lower part of boiler along through the steam supply pipe A, but that water was so expanded by its intense heat that it required an auxiliary tank above the heater to supply the shrinkage invariably following the filling in that way.

Then an injector placed in a pipe taken from the tender as shown at B was tried and proved perfect, as the steam forcing the water heated it to a desirable temperature for instant use, so that a Pullman or excursion car may use steam or the hot water system at will. As the plan has been in use two years it is past the experimental stage.

All who ride much in cars fitted with hot water heaters know how uncomfortable such cars are in the spring and fall. This is entirely remedied by changing them so as to use steam, so that any sudden change of temperature may be met at once whether of heat or cold, which is impossible with any of the other plans.

An auxiliary heater is necessary on all roads.

A car from a Connecticut River Railroad train is daily taken from Windsor, Vt., to White River Junction by a Central Vt. train. That car stands at the Junction over night without heat, then in the morning it is hitched to a freight train to take early passengers over the road fourteen miles, before steam for heat can be obtained. Sometimes an attempt is made to start a fire in a stove, for the writer early in the winter, during a snow storm, saw the conductor after collecting tickets strike a match and stick it into the stove; but the match soon went out, and he did the same, leaving us to enjoy the winter weather in full.

Properly fitted cars may be set off with sleeping passengers to wait for morning or to be hitched to freight or branch trains, or as stop over excursion trains, without requiring stationary steam heating facilities or any special arrangements whatever.

## SAFETY AUXILIARY CAR HEATER.

An illustration of this heater may be seen upon the opposite page, made with double shells of quarter inch steel plates of such height as to do away with the necessity for separate expansion tank and numerous connecting joints which, accidentally ruptured by derailment, collision, or other causes, allow the burning coals to be thrown around the car.

In this heater there is no coil to be burst by freezing or burned out, as is so commonly the case with the Baker heaters.

As the hot water circulation is only designed to be used in emergencies, such as the absence or disability of the locomotive, stop-over sleeping, or excursion cars set off to be hitched to freight or branch road trains, the heater is so arranged that the fire may be instantly dumped and the burning coals removed from the car as the steam from the locomotive drives the water from the heater and circulating pipes.

Where cars are already fitted for hot water heating, the heaters may be retained, but they are not so convenient, effective, safe, or economical as the one illustrated.

Cars properly piped with this system should never have the ventilators closed, and with very little care the temperature in the car need never vary over two degrees. There should be a thermometer at or near each end of the car.

The usual drip is under the middle of the car, but that may be closed when nearing a station, another opened above the heater, and the train may stand in the station an hour without wetting the floor.

The same process may be followed where a car is to be set off and kept warm by hot water circulation, thus saving the condensation for refilling the heater.

Any car fit to be used can be kept properly warmed and well ventilated by the use of three-fourths of a h. p. of steam in sharp winter weather by the use of this system.

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## A STRANGE SYSTEM FOR CAR HEATING.

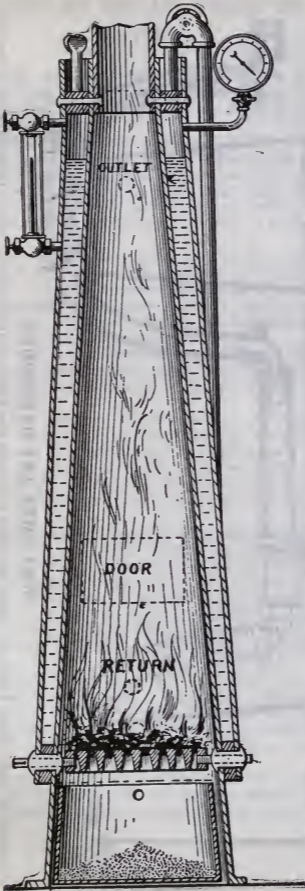
Of all the many wild plans for car heating developed by the demand for a safe substitute for the deadly stove, no other plan can be named so dangerous, extravagant, inconvenient, and uncomfortable as the continuation of the hot water circulation, if the water is to be heated by steam from the locomotive.

In no way can steam be so rapidly condensed as by discharging into water. Then night and day, while at rest, the heat must be kept up by stationary boilers so that at least five times the steam necessary to heat direct is required to heat by such hot water circulation, which is the worst of all systems for meeting sudden changes of temperature, liable at all times in extreme cold weather to freeze up or be unable to keep the cars warm.

Then if a pipe bursts the whole boiler pressure is behind the barrel of boiling water ready, in the old war style of repelling boarders, for boiling the passengers. The danger is so obvious that a jury would hardly excuse a manager on the plea that "he didn't think it was loaded."

## UNITED RAILWAYS SAFETY CAR HEATER.

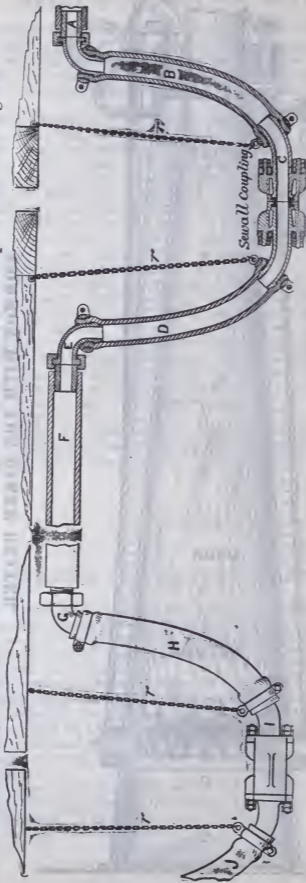
STRONG, DURABLE, NO COILS TO BURN OUT OR BURST BY FREEZING, AS IS SO COMMON WITH THE BAKER HEATER.



Do railroad managers and the public realize the danger of heating cars by hot water, the water kept hot by steam from the locomotive? The danger is so obvious that a manager in case of general scalding would hardly be excused by a jury, on the plea that "*he didn't think it was loaded.*"

## STEAM COUPLINGS FOR RAILROAD CARS.

All couplings similar in style to the illustration cause slow heating, are dangerous, inconvenient, extravagant in the use of steam, expensive, and certainly are not the product of mechanical or experienced reasoning minds.



### WHY THEY ARE DANGEROUS.

At stations where train hands go under the cars to couple the steam and air brake pipes, they have no notice of the train starting except the striking of the engine bell. Suppose half dozen engines to be standing there, their bells ringing, who is to know which is to start? The danger from such coupling will increase with increase of traffic. The writer has twice been caught in that way and only saved by clinging to the brake rods until the train could be stopped.

## CAR HEATING BY STEAM FROM THE LOCOMOTIVE.

· Undoubtedly the method of the future, because the simplest, safest, cheapest, most comfortable, and convenient; but to obtain the advantages named above, common sense must be used in fitting up the cars for the heating.

In no way can a car or room be so pleasantly heated as by having a steam chamber beneath and the floor perforated with minute openings throughout its entire surface, but as that is not conveniently practicable the next best plan is to distribute the heat in small pipes over as much of the floor space as is practicable, and a liberal supply of the pipe should be placed at the ends of the car near the doors.

All who have traveled in cars where the Martin system is in use know how the feet and legs suffer through the intense heat from those large pipes; if there is any possible danger of scalding passengers by steam escaping from broken pipes it rests entirely in the use of large pipes, for with pipe sufficient for the purpose the steam cannot escape fast enough to create heat.

Steam has no heat unless compressed, and a car has too many openings to allow of compression unless through the use of pipes that no competent master mechanic would allow to be used after a moment's consideration.

For thirty years, experience has proved one and one-fourth inch pipe best for car heating by hot water, and the caliber of that pipe is reduced by the use of "double thick" to about the same as that of the ordinary inch pipe, consequently the two-inch pipe carrying four times the steam contained in the one-inch, the danger from scalding is increased four to one, while its heating capacity is but two to one.

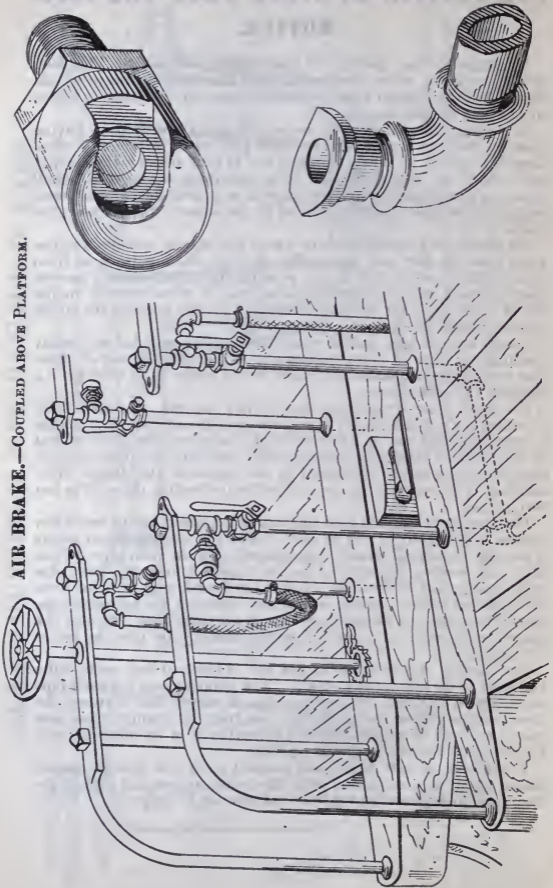
The average maximum heat that can be produced by the hot water system throughout a car is 168°, while the average from steam is at least one-third greater, consequently, as the inch pipe is four-fifths the heating capacity of the inch and a fourth, the inch pipe with steam must exceed the one and one-fourth inch pipe for heating with hot water, leaving no excuse whatever for increasing the danger through the unnecessary use of two-inch pipe; besides the space for piping a car is limited, so the smaller the pipe the better for the space.

The various supply pipes in use are at the best but make-shifts and used at serious loss of steam. The proper place for such pipe seems to be through the buffers, then in direct line between the floor timbers of the car as shown, free from all abrupt turns, also out of the way of repairs below, yet leaving it in the most accessible condition for repair that is possible.

The piping of cars piped and coupled as in this system cannot freeze up as is so common with the other systems of piping, for there are no depressions for the condensation to lodge in.



AIR BRAKE.—COUPLED ABOVE PLATFORM.



## COMPOUND STEAM ENGINES.

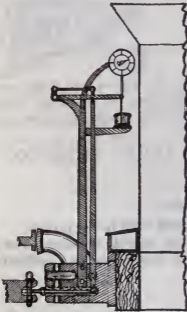
That there have been great improvements made in obtaining power from steam during the past third of a century there can be no question, but there fairly may be as to whether such improvements are in any way due to the use of compound engines.

For many years there was quite as strong belief in double turbines, but positive tests proved the fallacy of such beliefs; and the tests that I have been able to make of compound engines have not shown gain for that method of construction. Twenty years since the test of a compound proved it to be giving far less than expected, and the test of a Westinghouse compound a few months since proved it to be less economical than a simple Buckeye and much less satisfactory in its daily operation.

The marine engine, with its short cylinders, producing rapid rotary motion, may in that way obtain advantage, but it may fairly be questioned whether its increased economy is not owing more to the use of high pressure steam than to triple expansion.

Recently numerous papers have published articles relative to the wonderful efficiency of the Pelton water wheel and that some great English engineer had selected that wheel in preference to that of any other to be used at Niagara Falls in the new plans now under way there,—which may all be true, but as that wheel is simply the old Flutter wheel slightly modified in form, its efficiency can hardly exceed 70 per cent. in useful effect, yet under a head of several hundred feet it may produce an astonishing amount of power to those not acquainted with such

Emerson's Drawbar Scale.



a pressure of 160 pounds instead of the 40 pounds of thirty years since. The locomotive is generally considered an extravagant type of engine, but that idea is founded upon the lack of knowledge of the enormous amount of work the locomotive performs. The White Mountain train, running during the summer on the C. R. R. R., made up of seven cars all told, going north requires 370 h. p. An ordinary passenger coach upon that road, on straight and level track making local schedule time, requires 50 h. p.

There are many reports of engines that produce a h. p. per hour for each 2, 2½, or 3 pounds of coal burned, but the best result I have ever found was 4.28 pounds per h. p.

The Indicator is of no value whatever in determining the power developed by an engine, in proof of which the tests on the following page are given as but a few of many I have made.

One pound on the dial of the drawbar scale indicates one hundred on the link of the drawbar. This scale is placed in the buffer of the tender as shown, and can be shifted easily to any other tender using the same kind of buffer; its cost is small and its

use might prevent many useless changes, save in the selection of oils and in many other ways.

## SUGGESTIONS.

Twenty feet head room for bridges to avoid grade crossings means steep grades and much digging and filling. Why not instead, spread tracks three feet and have eighteen inch walk with rail on side of freight cars?

Prevention is better than cure. The practice of building cars with windows and door outlets that cannot readily be opened for egress will some day result in terrible loss of life; it is the unexpected that astonishes us.

Hartford Engineering Co., Buckeye Twin Engine; Cylinders,  
14 inches Diameter, 28-inch Stroke. Simultaneous  
Trial by Indicator Cards and Power Scale.

WILLIAM A. CHASE,

AGENT HOLYOKE WATER POWER CO.\*

*Dear Sir:*—On Thursday last the trial for power, etc., at the New York Woolen Mills, Connor Brothers, was conducted as follows:—

Ten "sets" were run through the day of eleven hours. The coal was taken from the surface of pile and weighed as used; though not screened, it was much cleaner than the average of the pile.

The weight on Power Scale was taken every fifteen minutes. The boiler pressure was kept at 70 pounds. The driving pulley on engine, 9 feet diameter, with 30-inch double belt, drove 5-foot pulley upon main line. Throwing on and off machinery caused variation of four revolutions of pulley on engine, or from 120 down to 116 per minute.

Mr. Hayes took cards at various times, seemingly with care and skill. The results obtained by the Power Scale, a No. 5, were as follows:—

|   |                       |            |
|---|-----------------------|------------|
| Divisions of 46 timings gave  | . . . . .             | 1,248 lbs. |
| Revolutions, 196 per min.   | cen. force, . . . . . | 85         |
| Average net weight for 11 hours,  | . . . . .             | 1,163 lbs. |
| Coal burned in 11 hours,  | . . . . .             | 4,955 lbs. |
| Average power in 11 hours,  | . . . . .             | 82.9 H. P. |
| $4955 \div 11 = 450.4 \div 82.9 = 5.43$ lbs. coal per horse-power per hour. |                       |            |

An attempt was made Friday morning to do the work with one cylinder, resulting in a complete failure. Sixty-five horse-power, with 70-pounds boiler pressure, would be all one cylinder could stand steady under. Indicated force, 101.5 horse power.

Respectfully yours,

JAMES EMERSON.

WILLIMANSETT, MASS., Sept. 14, 1884.

E. BLAKE, Needle Works, Chicopee Falls, Mass.

Rated by indicator to use 6.22 horse power.

Maximum possible with every machine in the works running, shown by power scale to be 2.74 horse power, but with the machinery ordinarily in use, 1.24 horse power.

Oct 21, 1884.

AMOS W. PAGE, Needle Works, Chicopee Falls, Mass.

Rated by indicator to use 7.38 horse power.

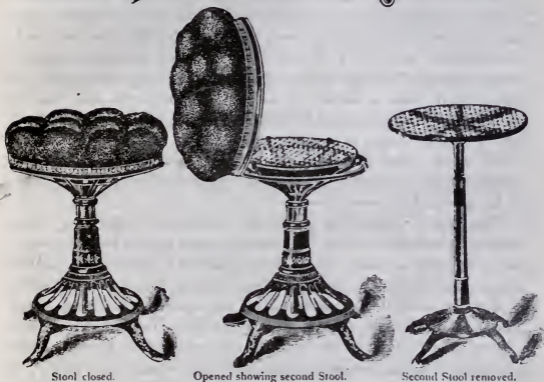
Maximum with all machinery in works running, shown by scale to be 3.35 horse power, but with the machinery generally in use 2.49 horse power.

JAMES EMERSON.

Oct. 27, 1884.

**It is safe to say that 15,000 horse power is the full equivalent of 20,000 indicated horse power.**

EMERSON'S  
 Duplex Piano Stool



Stool closed.

Opened showing second Stool.

Second Stool removed.

The present period may be denominated as the Musical Age. Almost every family of ordinary culture has its Piano or Cabinet Organ, in many cases both.

To develop the capabilities of these Instruments in orchestral effect, much of the popular music of the day is arranged in Duets, requiring four hands for its proper execution, of course necessitating the use of two stools or seats for the players. Probably there are few persons of ordinary observation and experience, who have not seen a chair filled with bound volumes of Music, "Webster's Unabridged," or other material to supply a seat for the second player.

For the most of the time but one Stool is required in a family, so that a second Stool is an encumbrance, except for the short time it is needed.

To obviate this objection, many attempts have been made during the past fifteen years to produce a Stool suitable for either one or two players. Numerous patents have been granted for such devices, but these generally have been conspicuous as to their double nature, and very inconvenient either as single or double stools.

The plan herewith illustrated is believed to be the long sought convenience for the purpose named,—insurpassable in beauty as a single Stool, or in convenience for teacher and pupil while giving and receiving instruction in music, or the execution of four hand pieces by two players.

## BROWN'S FACING MILL, POWER, ETC.

### Willimansett, Mass.

In this case the ordinary question cannot be raised as to whether steam or water power is cheapest, because the great expense necessary for land, dam, turbine, etc., etc., has already been incurred, consequently the loss of the water power would necessitate the expense almost of a double plant without any corresponding gain, for the present plant is located close to the depot, upon the road to Springfield, in proximity to Holyoke, and probably in as convenient and desirable a place as could be found in the New England States.

The whole plant must now stand to the owner at a cost of some seven or eight thousand dollars and completely fitted for business, to be operated by water power.

This power consists of an almost unchanging supply of water falling sixteen feet. Very few water powers can be found so regular in quantity as this. About three hundred cubic feet per minute can be depended upon the year round, though in extreme droughts it may be a little less, and during the spring something more. Three hundred cubic feet of water per minute falling sixteen feet evolves nine horse power; ponding the twenty-four hours' supply and using it in eight hours furnishes twenty-seven horse power, of which eighteen may be utilized or, say, fifteen horse power, ten hours per day, and this without waiting to get up steam as would be the case for every little job with a steam plant.

Mr. Brown's work is not such as to require constant power, hence the advantage of the power that may be called upon to operate the machinery for ten minutes, or an hour, as the case may be, then stopped and remain idle without expense or care until again needed, which could not be the case with steam power. Besides, with steam power to be safe for mill and neighborhood, a qualified engineer would be necessary to take charge of engine and boiler. I do not mean to be understood that engineers are always employed in such cases, but I do mean decidedly that, to obtain the same safety and convenience now enjoyed by Mr. Brown, one thousand dollars per year will not make an equivalent for the value of his water power, which is now in good condition throughout, to the best of my belief.

JAMES EMERSON.

WILLIMANSETT, MASS., Feb. 21, 1892.

## BOND vs. CITY OF SPRINGFIELD.

WILLIMANSETT, Jan. 6, 1892.

*To the Water Commissioners of Springfield:—*

All through the New England States may be seen relics of old mills, wheelwright shops, etc., located upon streams of little capacity, except in the spring of the year or during heavy rains. These were very useful in early times, but now almost every want is supplied by large manufacturers at a lower price than the raw material would cost at these isolated places, hence few of them continue in operation and such as do bear the marks of a lingering old age going to seed.

Portable saw mills are now moved to timbered lands, and the lumber is sawed, the slabs and refuse wood furnishing the fuel for steam power, at less cost than the timber can be drawn to stationary mills on water powers.

Mr. Bond, of Belchertown, continues the use of one of these ancient mills. The grist mill building was burned a few years since, and its place supplied by a superannuated depot building. The saw mill seems to be dependent upon the most primitive means for taking logs from the pond. The old cobble stone or bowlder dam and rotting surroundings offer evidence that at no distant day extensive and expensive repairs will have to be made from the foundation to retain the pond, and evidence that the future prospects have not warranted the expense of repairs and improvements. The assessed value of mills, houses, blacksmith shop, etc., is \$2,150, and were the property well advertised for sale there is no reason to think the rush of purchasers would be so great as to cause the suspicion of undue favoritism on assessed valuation.

Springfield takes about one-half of Mr. Bond's water supply during the summer.

October 3, 1891, the flow into Bond's pond was 72.77 cubic feet per minute, while the flow in Springfield canal was 93.90 cubic feet; but from this quantity must be deducted as a constant a half million gallons daily, or 46.4 cubic feet per minute supplied by springs in the bottom of the canal below the place where the water is diverted from Mr. Bond.

Taking the 46.4 from the 93.90 of course does not leave a quantity equal to the flow to Mr. Bond, but the Springfield supply varies as the mill above is or is not in operation.

November 25, the flow direct to the Bond pond was 252 cubic feet per minute; in the Springfield canal, less 46.4 for percolation, 295.6 cubic feet per minute. But the mill above was then in operation, and so large a flow would at the most continue but for ten of the twenty-four hours, while during the other fourteen there would be much less.

Two millions of gallons daily is a liberal allowance for all of the water that Springfield can draw from Mr. Bond's supply. This quantity, 185.6 cubic feet per minute, falling 13 feet evolves 4.56 h. p. Holyoke Water Power Company furnishes such power per year for \$4.33 per h. p. free from all expense to purchaser for maintaining dam, canal, etc. Willimansett brook has a fall and constant water supply for 25 h. p. the year round within a third of a mile of depot and within a mile of the business center of Holyoke, that has run to waste for twenty years, no one considering it worth the expense of fitting it up for utilization. A steam engine that would cost \$500 would do more work than all of Mr. Bond's water power much of the year and be far more reliable.

There are two classes of milling men that I often come in contact with that do not seem creditable to the age. The first are shocked and filled with indignation at the mere mention of making examination or measurements in their mills on Sunday, yet in the most bare-faced manner they will steal water for power every other day of the week the year round. The other class seem to consider it a commendable token of smartness to extort ten times the value of a thing from a corporation if possible.

Springfield is able to pay a fair price for what it needs. I would advise a tender of \$1,500 to Mr. Bond for the water taken, and, at the utmost, if \$2,000 will not satisfy his demands, then decidedly let the courts settle it.

JAMES EMERSON.



## ATWATER MANUFACTURING COMPANY, PLANTSVILLE, CONNECTICUT.

The annexed illustrations show the dam substantially as it appeared in 1880. The coping stone of the dam had in several places been crushed and carried away by ice, leaving the iron dowels projecting above as shown. The coping stones N and O remained, as was the case with some at the other end of the dam. The necessity for repairs of the dam at that time was so apparent that it was made a matter of my report and record. The crest of dam has since been evened up by timber and cement on a level with the top of the original coping, as shown by the stone N. Soon after a suit was commenced by the mill owners above, I examined the dam and saw that no improper raising had been made, nor was there any indication that the set-back of water from the dam interfered with the mills above. I went to the plaintiffs and proposed to test the power of their mills under existing conditions, then draw down the pond several feet and again test their power.

The land above and below is swampy; on such foundation a stone dam is sure to settle, as well as to be worn away on top by the overflow. The mill upon the east side has three turbines, the Manufacturing Co., one. For years the four wheels had kept the water constantly drawn down, leaving the banks of streams and the marshes uncovered, so as to cause sanitary complaint. At about the time the dam was repaired, the three wheels in the old mill were closed for good, since when the pond has remained full, perhaps causing the belief that the dam had been raised. Had that been the case there would be a belt of dead trees up the banks of the pond and river, for those banks were lined with trees, but no dead ones were to be found.

The Manufacturing Co. purchased the place under the assurance that the fall was eight feet. The dam has been the "overflow" of the pond and much debris had settled below the dam in the tail race at F. The small island marked D, and loose stone and gravel, have been removed and the head is now but seven and a half feet. The pond is quite extensive and extends considerable of the distance towards the mills above, and of course substantially is level from end to end, while the current from the pond to the mills above is quite rapid; at the line marked A, it is one foot per second when the wheels above are in operation. A surface mark was made at L just before noon; as the wheel gates closed in the mills above, the water settled two inches during the noon hour, though it must have risen on the Atwater dam, for the wheel gate was closed there. In the tail race at V, the surface fell six or more inches. Several hundred feet down stream from the plaintiff's mill, a stake is driven, the top of which is five and one-eighth inches above the crest of Atwater dam; with the wheels above in full operation the depth of water on stake was one and three-eighths inches. From the stake up, the current was very rapid, so as to make it hard to row a boat. Under the bridge on Main street, a sewer and the road wash has partially formed a bar, through the middle of which the current has cut its way, carrying the debris down near the line marked X, where it meets the set-back of water from the Atwater dam, and there has formed an extensive bar across the stream that raises the water above and in the vicinity, and this bar, the whole cause of the misunderstanding, had not been found by the several different civil engineers employed in the case, though the action of the water easily made such obstruction apparent.

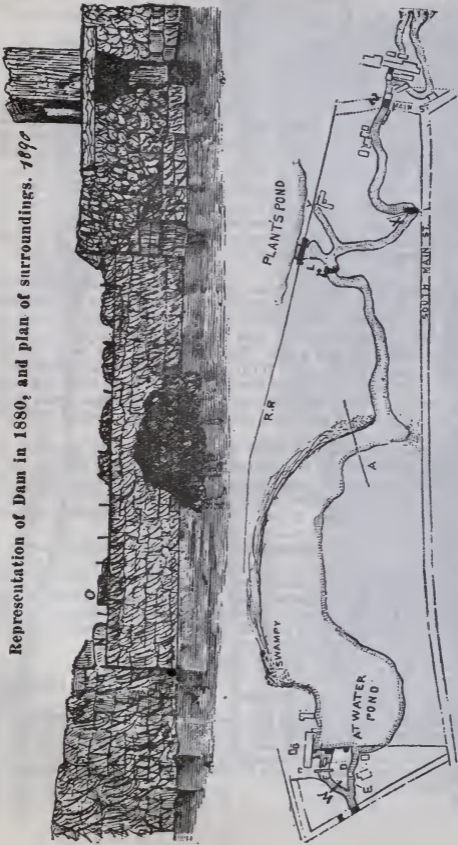
This bar has doubtless rapidly increased since the stopping of the three wheels in the old Atwater mill, for previous to that the water was so constantly drawn down that the meeting of the waters would have been in pond.

To understand the conditions fully, consideration must be had of the fact that the plaintiff ponds the twenty-four hours' supply of the stream, and then sends the whole down in ten hours or less; consequently as the Atwater wheel can use but a portion of that quantity, much of it must go over the dam, causing the surface there to be higher than if only the natural flow of the stream came down.

Now one hundred dollars properly expended as I proposed, by testing the power, would have made the matter so plain that there could have remained no possible cause for dispute, instead of which the law was invoked, to the great benefit of the lawyers at least.

In court the case must be fitted to the law, not the law to the case. Each witness is sworn to tell the truth, the whole truth, and nothing but the truth, and then every effort is made to suppress all undesirable truth by one side, the other side trying to confuse and make the witness lie if possible.

Representation of Dam in 1880, and plan of surroundings. 1890



WILLIMANSETT, MASS., July 14, 1890.

*To the Board of Water Commissioners of Willimantic, Conn.*

GENTLEMEN:—Having made several examinations of your arrangements for supplying the borough with water, I report as follows: My first examination was made when the estimated flow of water over Mr. Johnson's dam was eighteen inches in depth, the next when it was ten, and one last week when there was but a slight flow over it. At the same time the water was drawn down several feet at the pumping station dam, leaving only the flow of the natural stream at Johnson's line. From surface of water there to the level of your dam it was two feet five and a half inches. The lower line in the sketch annexed represents the approximate surface there at that time, and I believe the higher lines would do the same under the conditions named, could your pond be drawn down at such times. Two feet average for the year round of backwater would certainly be more than Mr. Johnson would suffer from your dam.

The sketch of dam also annexed does not represent your dam as it is, but as I would earnestly advise it be made and the dam backed with gravel before the season closes. The cracks in the walls of the station, embankments, and dam show that a rapid process of disintegration is going on. The mortar—it has no claim to be called cement—is poor. With such an abundance of water it is hard to conceive why more than fifteen feet head was ever desired. The present dam, made with an overflow, and waste-gates that can be used in time of need as I have shown, well backed with gravel, should stand.

The wheels selected show the engineer to be ignorant of the improvements made in turbines, and the general mechanical construction displays a lamentable lack of mechanical ability; while placing the waste-gates where it is impossible to use them when most needed, shows a lack of ability and judgment that seems incredible.

James B. Francis of Lowell, Mass., has had constant care of dams for nearly sixty years. I would seriously advise you to employ him to make an examination of your dam; have the water drawn down at the time. Stone dams have a fatal tendency to tumble down, and there seems a possibility of yours doing so. Owing to the poor mortar there is little strength in the dam except in its weight.

Very respectfully yours,

JAMES EMERSON.

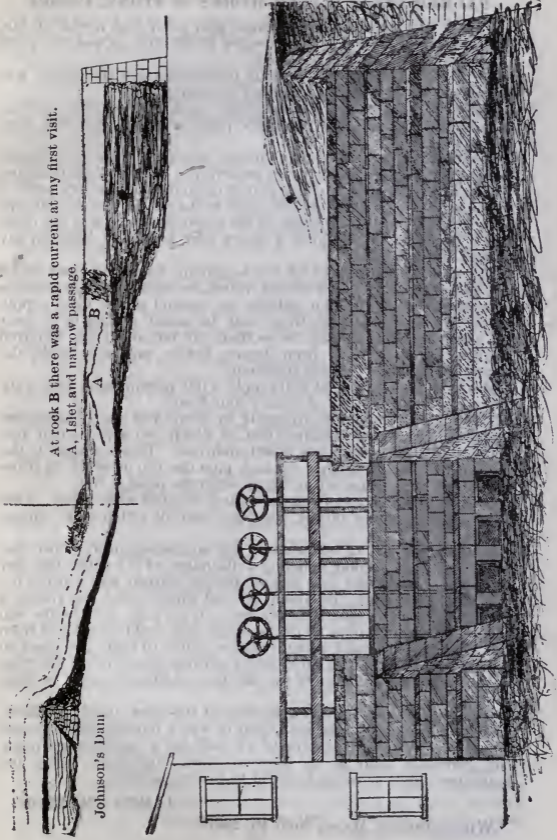
The above reported works were planned by Mr. J. T. Fanning, and constructed under his supervision. The pumps work at half speed designed but broke the iron frames connecting the pumps to the wheels at that speed soon after starting. The waste-gates are placed about fifty feet from the abutments of the dam, so that it is impossible to get at them unless the water is below crest of dam.

SUIT FOR DAMAGES

At rock B there was a rapid current at my first visit.

A, Islet and narrow passage.

Johnson's Dam



## SUIT FOR DAMAGES.

PALMER (Mass.) WATER WORKS *vs.* STONE, *Plaintiff.*

Visited the reservoir and streams, also pond, and works of Mr. Stone, in June. Stream below water works dry, as was the pond of plaintiff. His shop was closed.

At the reservoir there were plain indications that the supply was but little more than equal for water company's use.

Early in November made another examination with similar results, except that the plaintiff's pond was full, yet his shop remained idle.

November 14, made a more thorough examination of the streams, reservoirs, and stream supplying reservoirs; made a crude measurement of the supplying stream, also of capacity of plaintiff's pond.

There was more water the 14th than at the previous examinations, yet evidently but little surplus, as the lower reservoir was not quite full. There had been quite a heavy rain, for a day, between my second and last visit.

The crude measurement of the supplying stream showed about one-half of a cubic foot per second, which, for safety and convenience of computation, I call four gallons per second as the total supply to the reservoirs, though there may be small springs in or near the edges of the reservoirs, yet as there are but about two hundred families supplied, aside from depots, hotels, and wire mills, the supplying stream will seem sufficient.

Four gallons per second will supply 5,760 persons each with sixty gallons of water per day of twenty-four hours.

The plaintiff's pond is irregular in shape and depth, estimated surface ninety by one hundred feet, of which two and one-half feet in depth may be used, or say 22,500 cubic feet. This is gauged to the conduit to wheel through a ten-inch pipe the top of which is three feet below the surface of the water when the pond is full.

Overshot wheel coarsely made, set and supplied with water. Area of gauge, 78.5 square inches, sixty per cent. of which is 47 square inches.

Spurting velocity of water under say an average head of two feet is 11.84 feet per second, equaling a discharge of 3.7 cubic feet per second; 3.7 cubic feet per second falling sixteen feet evolves 6.7 h.p. propelling force, for which the old wheel could not return a co-efficient of more than fifty per cent., or 3.4 h.p. Two hours' run at that rate would draw all of the water that could be utilized from the pond, then it would require twelve hours to refill the pond so that two and one-half to three hours per day would be all the time during the working hours of the day the machinery could be kept in use.

In the spring and during the melting of the snow, and heavy rains, undoubtedly there is a larger supply of water, but the water courses below or above the reservoirs do not indicate a much larger quantity generally than at the present time. One horse power ten hours per day is as much as could be made available.

JAMES EMERSON.

WILLIMANSETT, MASS., Nov. 16, 1891.



## L. L. DEAN & CO., AMSTERDAM, N. Y.

GENTLEMEN:—In accordance with your request, I have at different times made examinations of your mill and its surroundings at Rock City and report as follows:—

On May 28, current year, made my first examination; the water was high, flowing over the dam below your mill 24 inches in depth. The next day, after the water had fallen on the dam to six inches in depth, the depth in tail race back of your mill on the boundary line was about thirty-four inches. I made examinations of the surroundings and found the conditions good so far as they could be ascertained until the water could be drawn from the pond below your mill. I was then informed that a suit had been commenced to compel the lowering of the dam below sufficiently to prevent its backing the water upon the turbine that furnished the power to drive the machinery in your mill, and was requested to ascertain if the dam did back the water upon your turbine, and, if so, to what extent; then to ascertain by the most accurate method the loss so caused, then to ascertain the cost of an equivalent power by steam at the mill.

Stumps in the water on the west side of the pond offer positive evidence that the dam below has been raised within a comparatively recent period.

To ascertain the cost of the equivalent a dynamometer or power scale was placed in the main driving pulley of the mill. The machinery of the mill, except the dynamo for lighting, was then driven by the steam engine during the day, the coal as used being carefully weighed, when it was found that each h. p. required 4.28 pounds of coal per hour or 102.72 pounds of coal each day of twenty-four hours per h. p.

Sept. 24, the water in the pond below your mill was drawn down so that the surface set back exactly to the boundary line back of your mill. The surface at the dam was twenty-four and a half inches below the crest of dam and twenty-seven and a half below the usual water line permanently marked by discoloration on the abutments. This would show a loss from backwater of about eighteen h. p. As neither the turbine nor steam engine can work economically so harnessed together as is usually done to make up for the loss of water power, it would be a moderate estimate to rate the loss at twenty horse power, requiring a ton of coal for each twenty-four hours. Taking the coal at five dollars per ton, the pay of two engineers, and wear and tear of machinery, into consideration, the loss cannot be less than ten dollars per day of twenty-four hours, though the cost of steam power would be less if furnished by a large engine running regularly for furnishing power.

The plaintiff's attorney requested me to proceed and state the facts in my own way which I proceeded to do, when the defendant's attorney, with his long arms wildly flying about his head like those of a frantic windmill let loose, shouted, "I object, your honor, I object!" and *his honor* sustained his objections for no perceptible reasons other than that such positive evidence so easily verified left no chance for the quibbles of the law to continue the case to an indefinite period.

JAMES EMERSON.

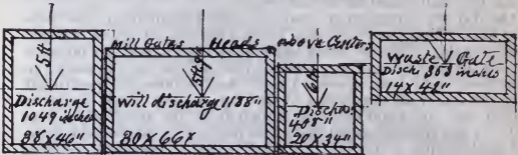
AMSTERDAM, N. Y., Sept. 24, 1890.



MASCOMA RIVER IMPROVEMENT CO., PLAINTIFF,

vs.

EMERSON EDGE TOOL CO.



GENTLEMEN, this certifies that on the 27th day of this month I made an examination of the reservoir dam above your works at East Lebanon, N. H. ; that I had the apron planking removed at four several places and that I found the main timbers sound and the whole structure in a condition to render it safe for many years to come. To continue its duration, however, I would advise that annually as convenient the cribbing or frame work of the dam be filled more and more with cobble stone, and gravel be added to that above the dam. By so doing in a few years the whole may be rendered permanent for ages to come.

I would also earnestly advise not only you but all other owners of dams to fix in some unchanging place such as a ledge in the side of the pond at the exact level of the crest of the dam a mark that can never be changed to denote the height of dam and have such mark recorded. The neglect to take this precaution has been the cause of innumerable cases of litigation where dams have gone out, as is so common, or where they have settled or worn away as all dams do in time. This mark need not be near the dam, for the water will give the level when at crest of dam.

The deed conveying the right to this dam, pond, and water power is wildly worded, rendering it necessary for you to observe great care in carrying out its conditions. The reservoir is to be so maintained that at all times sufficient water may be sent down to furnish power for all the mills that now are or may be erected ; a condition very likely soon to become an impossibility from lack of water, hence you must use discretion as to the quantity you allow to pass your gates.

The mill owners have the to-be-unquestioned right to open or close the waste gate in the dam at discretion but in no way to meddle with the old mill gates of yours represented above. To do so must render them liable not only as trespassers, but also for heavy damages that may occur through fires caused by the starting up of machinery when there is no one present to care for it, or by rendering fire pumps useless by the shutting the gates, etc., etc.

Whenever there is a scarcity of water my advice to you is to regulate your gates so that the water in the reservoir decreases but slowly ; then if more is required grant the request only when made in writing by a responsible agent, who shall hold you harmless. Even then you will care for your own rights, and riparian rights below.

The three gates of the old mills represented above, when the reservoir is full, will discharge 345.2 cubic feet of water per second ; less in proportion of course with decrease of head ; 345.2 cubic feet of water falling 14 feet evolves 547.7 h.p. ; adding the discharge of the waste gate the center of which has 7 feet 3 inches head and will discharge 53 cubic feet per second, sufficient water is sent down the river to produce a force of 631.7 h. p. where the fall is 14 feet, other falls in proportion. 67 per cent. of such force is the estimated average realized.

There are numerous places below your works before arriving at the Lebanon Mills where dams and mills may be constructed. Such mills will if constructed have the right to the natural flow of the river.

JAMES EMERSON.

WILLIMANSETT, MASS., Nov. 28, 1891.

WILLIMANSETT, MASS., Aug. 10, 1893.

W. H. CHILDS, Secretary of the Village Water Supply Company,  
Manchester, Conn.

DEAR SIR: As requested, I yesterday made a general examination of your water supply system, and report as follows:—

The watershed of the village tends to return the water taken from the stream. This stream enters the Hockanum river below the village. The mill stream is small and made up from three limited sources. The mill owners upon this stream have erected two comparatively large dams or reservoirs upon these sources, to save the abundance of the spring and rainy seasons, and these mill owners alone form the Village Water Supply Company. I find that there are 139 water takers; calling six persons to each family, 834 persons are supplied with water.

As the village has no sewer system, 60 gallons per individual is a liberal allowance; a few mill owners are furnished with wash water, which immediately returns to the stream,—call the whole equal to one gallon per second per day, or 86,400 gallons per each 24 hours.

The estimated surface of the upper reservoir is 1000 by 400 feet, which I found drawn down three feet; its average depth is, say 10 feet. The stream above the reservoir was perfectly dry while the outlet gate was letting out five gallons per second, consequently the discharge into the Hockanum river is now five gallons per second, where there would have been nothing from the natural stream at this time.

The two reservoirs store sufficient to supply the village 70 days were there no renewal during that time, while, owing to their construction, the average flow of the stream has been much increased. The valuation of village property has been increased through the safety arising from the water supply hydrants located by an independent village commission.

The loss of power in the Hockanum river caused by the diversion of one gallon per second from a fall of 14 feet would be something like one-fifth of a horse power, but without the reservoirs there would be considerable time when the gallon would not be there to fall. The quantity would hardly equal the capacity of an inch and a half pipe under one hundred and fifty feet head.

Yours truly,

JAMES EMERSON.

*F. A. Smith, Jr., Treasurer Electric Light and Power Co., Waterville, Maine:*

This certifies that from the 9th to the 16th of this month I have made numerous tests at the works of your company, to determine the power required to drive your lighting machinery, also to ascertain the maximum power your two \*turbines can furnish, it being understood that the head of water during the year is often less than at present, and that at the present stage it is hardly sufficient to operate the six dynamos, as desired.

Your company have an alternating dynamo connected with a circuit of six hundred incandescent lights, and five other dynamos of a different style for arc lights, all of the same make and capacity, operating five separate circuits, which circuits differ somewhat in conditions and number of lights.

The tests were made by belting from the pulleys on driving shaft to dynamo through an Emerson No. 4 power scale, that carries its load nine feet at each revolution of shaft and scale, the weight being shown in pounds, as upon the ordinary platform scale.

Operation for computation of data: Multiply each revolution by 9, and that product by the weight as shown, then dividing by 33,000 shows the amount of work done in horse power.

Test of alternating dynamo: Revolution of scale per minute, 495; of dynamo, 1,500; weight, 390 pounds.

$$495 \times 9 = 4,455 \times 390 = 1,737,450 \div 33,000 = 62.65 \text{ horse power.}$$

Test of arc dynamo connected with a circuit of thirty arc lights, 1,200 candle power each: Revolutions of dynamo, 900; of scale, 323 per minute; weight carried, 180 pounds.

$$323 \times 9 = 2,907 \times 180 = 523,260 \div 33,000 = 15.85 \text{ horse power.}$$

Test second, connected to different circuit: Revolution of scale, 324 per minute; weight, 180 pounds.

$$324 \times 9 = 2,916 \times 180 = 524,880 \div 33,000 = 15.90 \text{ horse power.}$$

Test of third circuit: Revolution of scale, 325 per minute; weight, 190 pounds.

$$325 \times 9 = 2,925 \times 190 = 555,750 \div 33,000 = 16.84 \text{ horse power.}$$

Test of fourth circuit: Revolution of scale, 324 per minute; weight, 200 pounds.

$$324 \times 9 = 2,916 \times 200 = 583,200 \div 33,000 = 17.84 \text{ horse power.}$$

Fifth circuit, same as the first arc circuit tested.

The six dynamos with all lights in use require 150 horse power to be safe.

The two turbines at the best cannot transmit over 140 horse power, oftentimes not that.

\* Risdon, the most unreliable turbine I ever tested. Owing to some peculiarity, it could never be told until tested whether it would do well or not. One set by a millwright was tested that gave 73; next day after resetting it gave 87 per cent.

JAMES EMERSON.

WILLIMANSETT, MASS., Feb. 18, 1891.

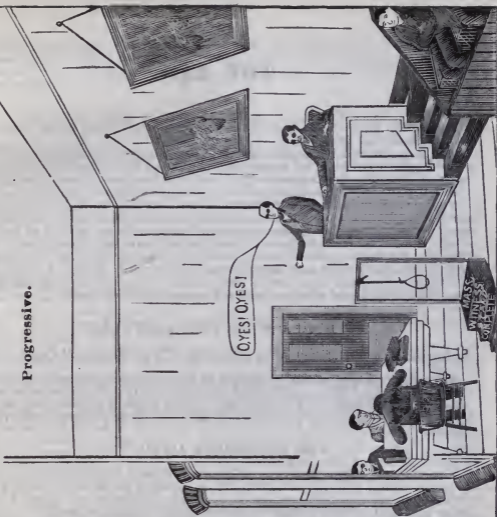
# “THE LAW.”

The study of untold centuries to enable influential rascals to escape responsibility.  
 Its only science, the knowledge of its uncertainty.  
 Is that the law? Never the question, is that the right?  
 Will it never be understood that the law was made for the benefit of man, and not man for the law?

Equally.



Progressive.



## THE LAW.

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During the past decade complaint has frequently been made of a lack of reverence for the law.

Has the law, with a continuation of its obsolete absurdities and rules requiring cases to be fitted to the law, instead of making the law fit the case in hand, any just claim to respect? Has there been any attempt made by the fraternity to simplify and bring it up to the necessities of the time?

Nearly twenty-four hundred years ago Herodotus wrote of its delays and uncertainties just as is done to-day. At the left of the illustration of court-room is a view of what a century since was thought desirable to put back of the house while the travel was in front. Once in a groove the plan has continued, though a hundred from the car windows are now annoyed by the disgusting sight where one would have been formerly if placed in front. The two views are intended to show the force of habit. The "O yes, O yes," miniature gallows, and bullying of witnesses should be matters of the past.

### THE LAW OF THE LAWYERS.

Safeguards for Professional Honesty—The Attorneys' Oaths, 1884.

A frequent charge against members of the bar, made indeed facetiously in most cases, is that of insincerity and lack of veracity. The attorneys' oath of office is in all conscience strict enough, and if there is such a thing as a dishonest lawyer he must be a perjurer as well. Below is given the form at present in use.

#### THE ATTORNEYS' OATH, 1884.

You solemnly swear that you will do no falsehood, nor consent to the doing of any in court; you will not wittingly or willingly promote or sue any false, groundless, or unlawful suit, nor give aid or consent to the same; you will delay no man for lucre or malice; but you will conduct yourself in the office of an attorney within the courts according to the best of your knowledge and discretion, and with all good fidelity as well to the courts as your clients. So help you God.

1. A lawyer ought to be a gentleman. His function as an attorney gives him no dispensation to disregard the ordinary rules of good manners, and the ordinary principles of decency and honor. He has no right to slander his neighbor, even if his neighbor be the defendant in a cause in which he appears for the plaintiff. He has no right to bully or browbeat a witness in cross-examination, or artfully to entrap that witness into giving false testimony. Whatever the privilege of the court may be, the lawyer who is guilty of such practices in court is no gentleman out of court.

2. A lawyer ought not to lie. He may defend a criminal whom he knows to be guilty, but he may not say to the jury that he believes this criminal to be innocent. It is notorious that some lawyers who would think it scandalous to tell a falsehood out of court in any business transaction lie shamelessly in court in behalf of their clients, and seem to think it part of their professional duty. That bar of justice before which by their professional obligations they are bound to the most stringent truthfulness is the very place where they seem to consider themselves absolved from the common law of veracity. So long as the legal mind is infected with this deadly heresy we need not wonder that our courts of justice often become the instruments of unrighteousness.

3. A lawyer ought not to sell his services for the promotion of injustice and knavery. Swindlers of all types are aided by lawyers in their depredations upon society. It would be more difficult to believe this if its truth were not so often illustrated in the stupendous frauds and piracies of great corporations, all of which are carefully engineered by eminent lawyers. Our modern "buccaneers"—our brave railroad wreckers—are in constant consultation with distinguished lawyers. They undeniably have "the best of legal advice" in planning and executing their bold iniquities.



Bob Ingersoll rails much against a venal priesthood, yet defends Star Route thieves with a gusto that denotes a labor of love. The mote he so dislikes is not small, but he seems to carry a whole lumber yard in his eye without inconvenience.

### IS THE LAW ITSELF MORE COMMENDABLE ?

Governor Butler said: "Shall I call your attention to the time when no lawyer was allowed to practice?" and he added, "It was a credit to the legal profession that no lawyer had participated in the witchcraft tricks,"—and so it was; but when he said, "No judge presided over them," he simply blundered, for it is well known to every school boy familiar with the history of those times, that it was the notorious Chief Justice Sewell who, in his blind bigotry and desire to serve two masters, both God and man, at the same time, as he thought, condemned twenty-four innocent people to death, and afterward stood up in church in Boston, with bowed-down head and sorrowful countenance, while a paper was read, in which he begged the prayers of the congregation, that the innocent blood which he had erringly shed might not be visited on the country or on him.

"As far as we know," says *Texas Siftings*, "there is not a single instance on record in Texas of a murderer of means having been punished by law, no matter how many homicides he committed." Texas is not an exceptional state where such cases transpire.

The result of the Sellon trial confronts the people of this community with some serious questions. Where and what is the influence which renders the conviction of a man for the taking of human life impossible? How is it that the machinery of the law is wrenched and money poured out like water to convict two men of a crime which a majority of people believe to-day was never committed by anybody, while three men, each with the blood of a fellow being on his hands, walk the streets free men, one of them not even having been indicted for his crime? It has become so in this community that if a murder is committed and the man who does the deed has any influence, political, pecuniary, or social, which can be brought to bear, it is immediately taken for granted that he will not be punished for the crime.

### THE KEMMLER REPRIEVE.

The case of the condemned murderer Kemmler certainly offers the most remarkable instance of judicial procrastination on record in this country.

### A FATAL FLAW IN THE INDICTMENT.

A highly respected citizen was arraigned before court for shooting and killing a friend. The evidence was direct, and after exhaustive arguments had been made the judge said:—

"It is clearly proven that you are guilty, as charged by the indictment."

"But I protest my innocence," replied the prisoner. "The indictment reads that I did shoot and kill the gentleman with powder and a leaden bullet. This is a mistake. I had no bullets at the time, so I loaded my gun with powder and a horseshoe nail."

"That indeed alters the case," said the judge. "The indictment said bullet, when it should have said nail. You are discharged, sir."

Frank Weiss, the editor of an illustrated German comic paper at Erie, Pa., is on trial for libel, and has succeeded in fighting the law with its own weapons in a very amusing way. The district attorney at the opening of the prosecution claimed the right to "stand aside" jurors under an ancient law of Edward I., never repealed and once sustained by the supreme court of Pennsylvania by some musty decision. In this way, every German or Irish juror was thrown out, the court assenting to the absurd supremacy of this law of 900 years ago. Weiss, who is a small, feeble, melancholy-looking man, then concluded if they were going in for mediæval law he would have some. So he insisted on the trial of the case by ordeal of fire and by combat! He floored the court with his citations of unrepealed law, and at last accounts the suit was still in progress, with more fun in the court than there ever was in the newspaper.



The fallibility of juries has recently had a striking illustration in the case of a man under life sentence for murder in Michigan, having been recently pardoned, after passing twenty-seven years in prison, on the ground that he is innocent of the crime for which he was convicted. He was convicted mainly on the false testimony of a worthless wretch who had a grudge against him, and who afterwards confessed that the evidence given by him at the trial was a lie. It is sad enough to consider the long years of confinement suffered by an innocent man, but still more sad to think of his blasted life, and that now he is set free he has no remedy or redress for the suffering and shame endured or the gross injustice of which he has been the victim.

### A QUESTION OF PARDON.

I see that the papers notice the "pardon of an innocent man." How can an innocent man be pardoned? What is there to pardon him for? If there is anybody to be pardoned, isn't it the ones who imprisoned him?

Has a people that will allow such a damnable law to continue to exist any claim to be considered civilized? Surely, if the safety of the community requires the punishment of a supposed guilty person, the commonest justice requires the most ample retraction and compensation in case innocence is afterward proved.

A well known lawyer said: "If I had my way, I would abolish all the courts in the state once every ten years. The courts are the masters of the people. Talk about their being the servants of the commonwealth—they are its masters. You can see how it is when anything is attempted at the Legislature which touches any of these courts. If a measure is proposed which would disturb any of them, it is impossible to get it through the Legislature. They have such control over the senators and representatives that nothing can be done. A judge has so much prestige that the representative thinks he is doing just the right thing if he votes as the judge thinks is the best way, and the consequence is that it is absolutely impossible to get any reform through. A judge isn't any better man after he goes on the bench than he was before. Giving him a commission doesn't make any better man of him, or give him any new faculties, or make his opinion any more entitled to respect than it was before."

And if I could have my way the Legislature should meet but once in ten years; then select a few fundamental principles of justice, never exceeding one hundred in number; then repeal all previously existing laws from the beginning of recorded acts, and have all disputes settled by arbitration, allowing no lawyer to be employed.

### JURY TRIAL.

What a travesty upon both law and justice; agree or starve! One venal member, by providing beforehand, could easily compel the others to submit.

Yet further, it is a well-established point of law that an agreement under duress is illegal.

A diligent reader with a good memory may be a successful lawyer without being a statesman or much of a man.

Congress is rotten with lawyers and notoriously lacks statesmanship.

It is a strange condition of society that its laws that all are to live by become so complicated that lawyers at from five to a thousand dollars per day must be employed to explain their meaning.

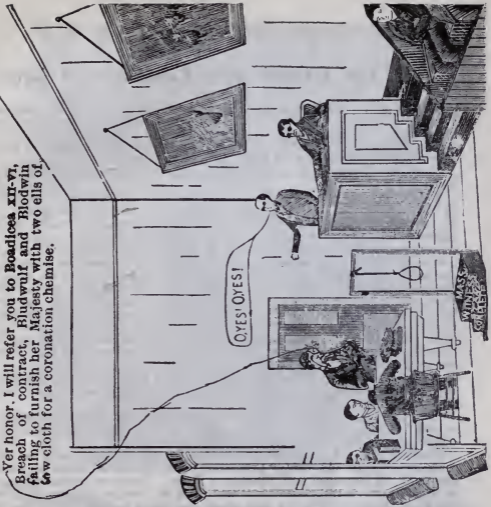
### IN CONCLUSION.

*Can any intelligent person accustomed to our courts, witnessing the silly, obsolete forms for opening and closing, its suppression of undesired evidence, its use of private correspondence, its attempts to trick witnesses into contradictory statements, its Jarndyce and Jarndyce procrastinations, its breaking of wills, its pandering to the influential, have any respect therefor or look upon it in any other light than that it is a bondage alike disgraceful to those who practice and those who endure its continuance?*

# LAW LINGERING IN THE LAP OF SPRING.

BORDEN MILLS vs. SPINNERS AND WEAVERS.

Ver honor, I will refer you to Boadicea XII-VI, Breach of contract, Bludwulf and Blodwin failing to furnish her Majesty with two ellis of 66w cloth for a coronation chemise.



## The Law Antagonistic to Knowledge and Justice.

A thorough study for a score of years of hydrodynamics makes it evident at least to myself that, except through imperfect deeds, no cause for disputes in milling matters can arise that may not be made so clear as to leave no just cause for litigation. Every effect has a cause, and such cause may readily be ascertained by an intelligent engineer.

Such cases usually have an individuality and each must be considered in itself.

The ordinary surveyor's level between mills is seldom of much account in backwater cases so far as determining the cause of complaint. A number of such cases will be reported in this edition of my work, from which information of my method of ascertaining facts may be obtained. A wide experience of the practice of law in many states in hydraulic cases convinces me that while Massachusetts from its early manufacturing should be one of the most intelligent in such matters it is in fact like its Andover theology and gallows witness stand more iron-clad and backward in its rules than any other. The assessors' valuation of a plaintiff's property, the verdict of a parallel case in the same county, mention of the obsolete character of the property in question, nor in fact anything that would show the utter worthlessness of the whole claim was presented in a recent case for damage. This may have been owing to the incompetency of the attorney, but certainly the most essential evidence necessary to enable the jury to decide intelligently and justly was left out; both attorneys seemed destitute of knowledge in such matters and equally desirous of preventing the jury from obtaining knowledge.

The Willimantic Borough case offered another lesson for litigants. It would hardly be possible to find a case more decisive in character; one any intelligent manufacturer would easily understand.

The case is one for mutual concession by which both could be benefited.

There is a trifle less than three feet in the level between the level of the crests of the Borough and Johnson's dams. Johnson claims to be desirous of digging a new tail-race 12 feet wide and 400 feet in length extending from his wheel down to Borough line where the water backs up 2 1-2 feet in depth.

Mr. Johnson desires to send down through the said tail-race 150 cubic feet of water per second, which moving three feet per second would require a depth of four feet, or a foot and a half more than the depth of water at the dividing line of the two properties, consequently the set-back of water could cause no real loss of power to Johnson. Like all such conditions the discharge from the race meeting the standing water of the pond would soon form a bar that would constantly increase in height and reduce the head on Johnson's wheels. By mutual concession such bar could yearly be removed. During the average flow of water the supply gorges the channel below Johnson's land so that there is no backwater at the line at all, and the channel is constantly filling up so that the rock B represented in the illustration of 1890 is now submerged and invisible.

Instead of defending the case upon its merits, the defense was that the river was variable in supply and of little value. There is little encouragement for knowledge if the law is to render such knowledge worthless.

What is the difference in principle, for lawyers to band together in Congress and Legislature and use their influence to perpetuate laws and rules of a barbarous age for personal benefit, and the uniting in mobs to destroy power looms and other improved machinery as was done by the laboring classes?

On another page I have stated that I seldom leave the witness stand without feeling outraged, but since attorneys of reputation confine their cross examination of my testimony to reading extracts from my legal criticisms it rather looks as though they consider their case weak and "get off their head," and so almost unconsciously give out information where it *should do the most good*.

**MASSACHUSETTS.**

We are with you, Dahomey, we hang and we imprison for debt. But we are magnanimous. If an innocent person is convicted of crime and cruelly imprisoned for twenty years, then is found to be innocent, we *pardn* him! shake, Dahomey?

*No, no! no shakee Masserturosheets, no sabs pardn tinerrent man, no shakee! Dahomey no church, no school, no pardn for inmercent man, no, no! no shakee, thankee, Masserturosheets too much law.*

A voter.



To "furnish brains for the rest of the world" is likely to leave conceit for home use, and the idea has caused Massachusetts to be the least progressive of the states.

Looking ahead, the mechanic has elevated the masses and increased the happiness of the world. Clinging to the past, the lawyer and priest have retarded the growth of intelligence. As the influence of those troglodytes wane, honor, charity, and integrity will increase. Voters should *think*; so long as lawyers make the laws so long will Carnegies and Jay Goulds flourish. Can one progressive idea be named as due Wm. M. Everts' six years in Congress? It is a fact for *consideration*, that lawyers are less skeptical than doctors or even ministers.



FARMING TOOLS IN USE IN 1790.



### **Expurgation and Pretension.**

The real value of a book consists in its representation of its time, to expurgate destroys its representative character.

Expurgate the atrocity and obscenity of the Bible and only spiritualism would remain. Expurgate what at this day cannot publicly be read from Shakespeare's works, and the pith is gone. Expurgate the loathsome filthiness from Rabelais' description of the Christianity of his time, and only the covers of his book remain. The delicacy that causes the teacher to send the bare legged boy from school does not prevent her from displaying more than legs at the bathing beach. The age that sentences the poor thief to years of imprisonment for stealing a suit of clothes, pronounces the rich railroad director free from guilt, though, in defiance of law, he has caused the death of passengers by roasting. Talmadge in his church, the clown in his circus, and the self-styled statesman, each worship the Christian's God, and there can be little doubt but that the clown does the most for humanity. The unpretentious farmer that places a watering trough by the wayside for the thirsty man or horse, in my opinion, does more for the elevation of man and glory of God than the rich man who builds a church or endows a college.

### **Rotten Statutes.**

As a people few are more ready than ourselves to censure the tolerance of abuses by others, or more servile in submitting to such of our own. How we smile at the Jay Goulding of a railroad through the chicanery of the law, or even the acquittal of a murderer by the resurrection of a rotten statute that should have been buried by obliteration centuries since. Such successes in any other walk of life would be considered infamous, but in law successful rascality is called smartness. If law is designed to aid justice why is such rascality tolerated by a people claiming to be civilized? Savages would scorn such trickery.

Patents, notes of hand, judgments, etc., etc., are limited in duration. Why not statutes? With nearly fifty independent States each constantly issuing volumes of new statutes, where is it to end? Lawyers produce nothing but strife and their support comes from labor. Will the laborer forever continue to support a class so useless yet so expensive? We claim to be a free people, but can there be freedom with such a mountainous pile of rotten statutes hanging over us? Can anything be more senseless than the common practice of legislators referring matters pertaining to the law to the judiciary committee? Lawyers if no worse certainly are no better than others. Simple laws are not for their interest. The ideal law of the lawyer is of the mattock and spade, mailed shirt and bow and arrow age. If the steel plow, harvester, rifle cannon and repeating rifle are superior to those, then in proportion has the mechanic proved his superiority to the lawyer. Then what excuse is there for suffering the designing or inferior to determine the laws for the superior? Law is for man not man for the law. Get up out of the ruts, Messrs. Legislators! if your heads hit the roof when doing so your brains are safe, that is not their location. Why not to every new statute enacted add, "and all previous enactments in-



consistent with this are hereby repealed"? The best governed people are those governed the least. Blot out every statute over twenty years of age, and the occupation of the *smart* lawyer would be gone.

### Arbitration.

When a proposition is made by one of a party to leave a case in dispute out to three disinterested persons to decide and the other refuses to do so, we invariably believe the latter to be the one in the wrong. Then why not make such arbitration obligatory, whenever one party demands it? Do away with the so-called law and lawyers. Have fewer officials and those directly amenable to the people. Form a general plan for arbitration and make such decisions final, except in cases of finding new and undeniable evidence, then in serious cases, such as unjust criminal convictions and punishments, have the highest official of the state apologize for the wrong and so far as possible make the fullest restitution for the injustice, instead of as is now done adding outrage to injustice by the mockery of *pardoning* a martyr, what a barbarian would be ashamed to do. In God's name, is there not statesmanship in Massachusetts sufficient to remedy a wrong so glaring?

### The Sacredness of an Oath.

In a story about Catiline, a companion says, "Who believes in an oath? Did you ever believe in one, Catiline?" "Well, perhaps so, when a boy," was the reply.

Those accustomed to the usual style of administering the oath, "Hold up your hand. You solemnly yum, yum, yum, s'elp you God," can hardly be much impressed with its sanctity, and the observance of the interested witness with his "I don't remember," and burning face when the question has struck home, will be likely to cause the observer to come to the conclusion that the person who in ordinary conversation embellishes his story merely for self exaltation, will hardly hesitate to lie when under oath if it is for his interest to do so. There are penalties for perjury; why not depend upon those?

### Irresponsible Commissions.

If "eternal vigilance is the price of liberty," can it be well to take the power to act direct from the people, and place it in the care of a commission chosen more through political partisanship than personal fitness?

Are three hackneyed politicians more likely to be just to all than those interested for the best good of their homes? Are our schools as effective now in producing practical men and women, as formerly under the old district or local governing system?

Responsibility begets consideration. How quick staid citizens, after enlisting as soldiers during the late war and losing their personal responsibility, became like unruly boys, often worse.

Is it democracy to place the governing power in the hands of a minority of wire pullers? Can a single instance of such a course being found conducive to general good be named since the beginning of history? Then why ignore such ages of experience and abandon the principle of self-government?

## AN OHIO IDEA.

In one of the western counties of Ohio a petition is being circulated asking Governor Hoadley to pardon a young man sent to the penitentiary for robbing a prominent Free Thinker. The plea is that he should not have been convicted because the victim is a "wicked and perverse infidel." It is peculiarly an Ohio idea that a man who does not profess religion has no rights, and that it is an act of Christian charity to pick his pocket or set fire to his barn. Probably an Ohio office holder would think it a virtue to steal from the government on the same principle.

"The nearer the church the further from God," is an old and a trite saying, but ideas are changing, and we may hope for improvement.

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## TAXATION OF ALL PROPERTY.

If taxation is right at all, there should be no exception. Church property, usually occupying the best localities, certainly should not be exempt, nor should owners of unimproved land, contiguous to growing cities or towns, be allowed to continue to hold such land at a mere nominal rate of taxation, while others are ready to take it at far higher valuation. Let every owner be his own assessor, but with the understanding that any purchaser may take it at the assessed rate. Of course some provisions may be made to prevent a homestead from being unjustly taken.

Let all property be without the protection of law that has not paid for such protection by its taxation. There is no need for many of our officials.

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## PROHIBITION.

There is an old saying that most of the unhappiness of life comes to us through the efforts of weak but well meaning persons trying to direct our lives instead of causing general improvement by perfecting their own. Particularly is this the case with the priestly order, and has been so from the beginning of history. The Rev. Mr. Miner, the great advocate of prohibition in this state, must well know that his life has been spent in indoctrinating the minds of his hearers with a superstition that cannot be sustained by evidence, yet he is ready to assume the Creator's place and manage mankind. Prohibition interferes with the rights of all, and with very doubtful effects. Two gallons of liquor, beer included, would more than cover all that I have ever drank, yet I do not believe in prohibition, nor would I vote for license, for to me it would seem wrong to dignify a disreputable business by legal recognition; but as a large portion of crime, poverty, and misery is caused by the traffic, I would have all places where it is carried on taxed at such a rate that the owners would refuse to rent for the purpose.

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## Belt Transmission.

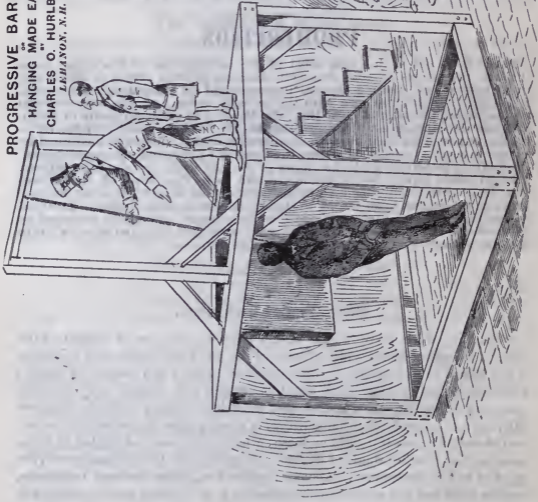
Of all guess work, there is none more unreliable than that of computing the power transmitted by the width of belt. First, the kind, quality and condition of the belt is to be considered; then the size, distance and position of pulley; whether their surfaces are wood, metal, or covered with leather; whether one is much larger than the other, and whether the belt is running vertically, horizontally, open or crossed; or, what is worse, is running edge up, on pulleys on vertical shafts; whether it is tight or loose; whether it is made of leather or other material, also whether single or double. In testing with lever dynamometer, the speed of belt is determined. A single leather belt, under ordinary conditions, running 1,000 feet per minute, will transmit a h. p. for each inch or width, but the matter is one of the greatest uncertainty

THE MIND OF THE

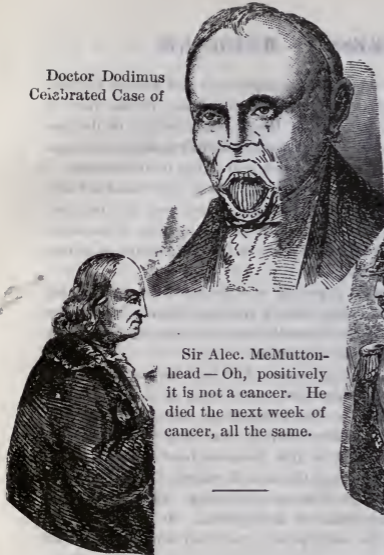
DAIS OF KABELAIS.



PROGRESSIVE BARBARISM  
 HANGING MADE EASY,  
 CHARLES O. HURLBUTT,  
 LEHAYON, N.H.



Doctor Dodimus  
Celebrated Case of



Duckworth's  
Open Mouth Lockjaw.



Sir Alec. McMutton-  
head — Oh, positively  
it is not a cancer. He  
died the next week of  
cancer, all the same.

Dr. Hamiltongue—Oh! undoubtedly  
the ball is here. Haven't we all said  
so from the first, and hasn't the elec-  
tro-detector located  
it here sure?



Dr. Doodle — Of  
course it is here!



Patsey McGrath—Loik at the pair of them doinkeys  
saking for the ball there, when it is here be my hoind,  
in the shoulder.

## PROGRESS IN MEDICINE.

“It is a fact that the number of healthy men and women is growing less every year, and the sick more numerous. In the face of these facts, it might be noted that this country is full of doctors and full of drug stores; that these doctors and drug stores increase every year, and in heavy ratio the sick and dying increase also.

“It would seem like ignorance and arrogance combined for any physician or school of physicians to claim a monopoly in the practice of medicine, when all physicians of all the schools of medicine combined are powerless in curing but a fair percentage of acute, and still less of chronic, diseases.

“And instead of doctors opposing new discoveries, condemning new systems of practice, they should welcome them, for no one knows better than the doctor himself how powerless he frequently is to cure, or even aid, in the sick room.”

Two thousand years ago Cato wrote of physicians precisely as we do to-day. He said: “If they attempt to treat of the practice in any other language than the Greek, they are sure to lose credit, there being all the less confidence felt by our people in that which so nearly concerns their welfare if it becomes intelligible to them. In fact, this is the only one of the arts in which the moment he declares himself an adept he is at once believed. Besides, there is no law to punish the ignorance of a physician. It is at our peril they experimentalize, the only person that can kill another with impunity.”

Pliny speaks of Rome trying, then condemning, the employment of physicians and going without six hundred years.

Le Sage in his “Gil Blas” has been more severe than Cato.

Dr. Majendie says: Medicine is a humbug.

Sir Astley Cooper: Medicine art is founded on conjecture and improved by murder.

Dr. Baker: Drugs destroy more than disease does.

Dr. Forth: There cannot be found a more dishonest trade than medicine.

Dr. Thomas Watson: Our profession is always floating on a sea of doubts about questions of the most serious importance.

Dr. Cogswell: If medicine was abolished, mankind would be the greatest gainers.

Dr. Mason Good: Medicine is a jargon, and has destroyed more than war, pestilence, and famine combined.



Dr. Frank: Thousands are annually slaughtered by the worst of all impositions—medicine. —*Anglice.*

Dr. O. W. Holmes of late years perhaps has the oftenest been quoted in depreciation of medicinal knowledge. Egregious blunders in high places have made the general ignorance of the class more conspicuous, particularly of those posing as the “great Doctor So and So.”

Perhaps nothing better could have been expected of Cato or Le Sage, but that modern physicians should acknowledge such ignorance is undoubtedly owing to the superstition and materialistic ignorance of the time.

Those who have read Mrs. Shelley’s “Frankenstein” will recall the monster without the governing soul, because only the physical man could be created; so of the physician who only knows of the physical structure. Suppose a mechanic of the highest skill as a mechanician, yet knowing nothing of electricity, should undertake to repair a complicated electric engine in which he could see nothing of the moving power as it entered, moved, or left the engine, could he expect to command success?

Man is of a dual nature, physical and spiritual; the spiritual or governing part that cannot be seen is the life of the man engine, as the unseeable electricity is that of the electric engine.

The man engine is the acme of mechanism, the most perfect and the most complicated, and every mechanic knows that complicated machines, even of perfect construction, often get out of order, require repairs and to be put in order.

The creative mechanic existed before doctors, and he created vast fields for all other professions. The lawyer and priest are fungous growths due to diseased surroundings, and in time to be done away with, but the healer or physician as a mechanic has a vast field of usefulness open to him, yet he must seek for real knowledge of man’s nature, and depend upon that knowledge for professional success instead of upon trades union or class legislation.

The healing art is of such universal importance that no intelligent legislature will ever attempt to prevent discoveries of means to prevent or to cure disease, and discoveries are usually outside of the classes to which they seemingly belong. Great progress has been made in surgery, and there is no good reason to doubt that the same progress may be made in medicine by proper study. I, for one, believe that there is a remedy for every disease, and that such remedy can be found, but the old ruts of conventionalism must be left behind.



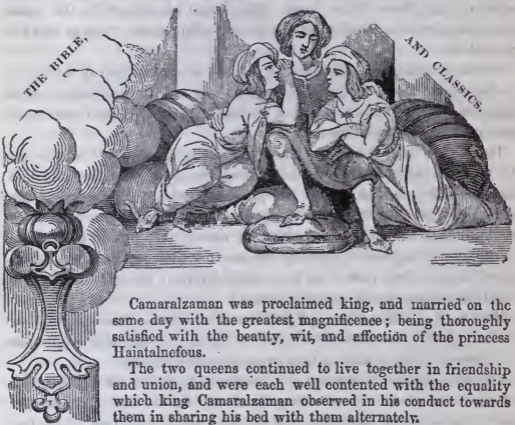
## MARRIAGE, DIVORCE, NUDITY.

YOUTHS' PREPARATORY EDUCATION FOR POLYGAMOUS ACTS.

ARABIAN NIGHTS,

THE BIBLE,

AND CLASSICS.



Camaralzaman was proclaimed king, and married on the same day with the greatest magnificence; being thoroughly satisfied with the beauty, wit, and affection of the princess Haiatalncfous.

The two queens continued to live together in friendship and union, and were each well contented with the equality which king Camaralzaman observed in his conduct towards them in sharing his bed with them alternately.

From time immemorial, theoretically, love has been represented as heavenly, in practice almost invariably gross. Death in any form for a woman before dishonor. Lucretia has been the model, but it should be borne in mind that the other side of that story has never been told. From the earliest history down to Anthony Comstock the clergy have been the most strenuous promoters of such ideas and, unless sadly belied, the most common violators of them, not because naturally worse than others but because of having leisure and opportunity. The wise man of the Bible requiring a thousand women, the Lord taking his share of captive virgins, Lot and his buxom daughters, Camaralzaman and his two wives, and the classics describing the loves of the gods and goddesses are not reading likely to inculcate monogamy in the youthful mind, yet society as described by Rabelais when the clergy had entire control was far worse; humanity is better off with less of that control.

The marriage laws are unequal and unjust, often causing the innocent to suffer for the fault of others. The "for better or worse" is a device of evil because of it the beautiful bride soon becomes the dowdy wife; the passionate lover, the indifferent husband.

Marriage by equitable contract should produce equality and continued effort to please. Give both the same right to propose such

partnership. Motherhood is a natural right, its desire inherent from infancy, proved by the craving for dolls. This right is often denied to the best through lack of self-assertion. Free woman from her bondage of conventionalism and long petticoats, encourage her to think and talk of something besides dress, give her equal rights with man. Protect by making all children legitimate and have their rights secured, but allow of separation of parents on the breaking of marriage contract by either party. Parties properly mated will need no law to keep them together, while those only kept together through compulsion had much better be apart.

From the earliest record of such matters, the status of woman has been that of the inferior. She has been credited with being an unmitigated gossip, a never ending tattler, and a nuisance as a "mother-in-law"; these are old ideas of prehistoric times, common two thousand years ago. Terence wrote a comedy twenty-one hundred years ago called the "Mother-in-Law," and our daily papers have kept the idea before their readers for the past twenty years as a remarkable find. Gossip and inquisitiveness are matters of condition, and not sex. Confine a man to the house or backwoods for the most of his life, and it would be a smart woman that would excel him in inquisitiveness or tattle.

The barber a generation since was known as a tattler of unlimited capacity, but the smart daily paper of the present time has thrown him into the shade so deeply that neither he nor women have any show in that line now.

Nudity is a matter of conventionalism and climate. Nakedness is out of the question where clothing is necessary for warmth, and the weight of this clothing hanging to the waist was most likely the cause of the change of the natural and healthy form of our women to the unnatural, wasp-waisted creatures that pride themselves on having a twenty-two inch waist measure. Man, it is claimed, was formed in the image of his Creator, yet prurient minds, with exaggerated pretensions to modesty, demand that the *limbs* of their bedsteads be veiled. Much opposition has been offered of late to the illustration of the female form upon the theater billboards, or to the form itself upon the stage, yet the intelligent observer will note the improvement in manners during the past thirty years. There is far less of the "Peeping Tom of Coventry" now than thirty years since. Then every traveler must have noticed the holes cut in stateroom partitions, the crowds standing at the base of church steps to get sight of the *limbs* of female worshipers, etc., etc.

It happened in my young days that several years of my life were passed with primitive people near the equator. There the young of both sexes went naked much of the time until ten or twelve years of age, the mothers having a cloth around the waist reaching to the knee. Beautiful girls of any age often went with a narrow piece of cloth formed like an apron, first hung in front, the lower end then passed between the thighs, then up the back to the waist, where the strings were then passed around the waist and end of cloth or apron, securing it in that position. With girls thus clothed I have swum, fished, hunted, and wandered through the forests for days and days, without hearing an improper thought expressed, or wit-

nessing an immodest action. Plain words were always used to convey ideas. Marriage and its responsibilities were freely discussed, the children listening as in other matters, and they were taught to realize the importance of the very foundation for the perpetuation of the human race, instead of being taught to look upon it as a matter to be lied about or kept in the background, as is done in our claimed higher civilization. Of course, under such conditions the form was developed as nature intended; there were no wasp waists or distorted feet; no need for padding, nature formed calves and bosoms; the form itself as upright as their native palm trees.



Bible idolatry has distorted the heads, law the morals, and ill fitting shoes the feet of our people. Dress reform is impracticable, because women, like the peacock, are ashamed of their feet. High heels have furnished business for corn doctors; is the product worth the cost? Look at the feet!

## TWO WOMEN.

I know two women; and one is chaste  
 And cold as the snows on a winter waste;  
 Stainless ever in act and thought  
 (As a man born dumb in speech errs not).  
 But she has malice toward her kind—  
 A cruel tongue and a jealous mind.  
 Void of pity, and full of greed,  
 She judges the world by her narrow creed.  
 A brewer of quarrels, a breeder of hate,  
 Yet she holds the key to "Society's" gate.

The other woman, with a heart of flame,  
 Went mad for a love that marred her name.  
 And out of the grave of her murdered faith  
 She rose like a soul that has passed thro' death.  
 Her aim is noble, her pity so broad  
 It covers the world like the mercy of God.  
 A healer of discord, a soother of woes,  
 Peace follows her footsteps wherever she goes.  
 The worthier life of the two, no doubt;  
 And yet "Society" locks her out.

The other woman for me.

—Ella Wheeler Wilcox.

## WOMAN SUFFRAGE.

With the manifest destiny so plainly marked upon the face of the age that woman suffrage is bound to come, it seems strange to see the ordinary republican seven by nine rural member so readily join the Irish statesman in defeating the measure. A biped with ordinary manhood should freely grant such equality of right, and certainly the American woman is likely to vote as intelligently as the newly manufactured citizen from any foreign country.

Politics are not likely to be reduced in quality by the addition of a more reputable class of voters. Massachusetts is not doing itself credit in the matter.

## RELIGION, MYTH, AND SUPERSTITION.

That there is a sympathetic chord between man and his Creator, I believe to be a matter of positive knowledge, though such knowledge may be obscured by superstition or perversion of intellect, such as the opacity of a Saviour. In the lowest animal stage of humanity there could have been no religion any more than now in the next link lower of the animal world. In time the organs of generation, as the palpable cause, were esteemed as the creator and then worshiped as such, at first in undisguised form, then as symbols more or less veiled, as priestly regalia or ornaments of church structures, up to this time.

Can anyone of common sense suppose forty-two children were torn in pieces by the prophet's two she-bears for saying, "Go up, baldhead?" No, no! the shaven crown or bald head had a symbolic meaning, which, if our street gamins understood, or the meaning of the priest's regalia, they would be likely to say something more than Go it, old baldhead, even if a menagerie of wild beasts were close by.

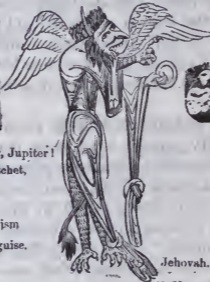
Superstition has been a great hindrance to progression in knowledge and happiness. My purpose is to show that what is called Christianity, with its impossible dogmas, is paganism disguised by change of name; really a conglomerate of various myths, all originating from symbol worship, easily traced to their source. The illustrations of the five following pages are taken from Inman's "Ancient Faiths and Symbols." They were culled from many popular works not familiar to the multitude, which cannot be explained in this work, though they are fully so in the work from which they are taken. Intelligent persons should see that work. The first figure, half male and half female, is of very ancient date; a very interesting reference thereto may be found in the Banquet of Plato, namely, that man and woman were made as one and called man-woman, having four arms as represented in the figure on the second page, that the gods became jealous and cut them separate, and that it is only when the original halves come together that true affinities in marriage are formed. "The Virgin and Child," third page, "as painted in the South Kensington museum, represent them exactly as they used to be represented in Egypt, India, Assyria, Babylonia, Phœnicia, and Etruria; in the framework the triform leaf representing Asher," etc., etc. The plates, selected from many, are the least objectionable, but at the same time too significant to be explained here. It will be seen that the four arms of the Hindu gods hold many of the same symbols. The Hindus also had their crucified Saviour and Chrishna. The cross or nilometer originated from the symbol worship, and is coeval with man.

**SUPERSTITION, IDOLATRY OR WORSHIP, WHICH!**

Devil worship.



Pagan worship.  
Jupiter.



Dragon and Joss worship.

Oh ho! My lord Jupiter, Jupiter!  
Oh my hatchet, my hatchet,  
my hatchet!

Paganism and Buddhism  
in disguise.



Jehovah.

Bible worship.

Worship of the Cross.

Oh Virgin Mother, ask your dear son to intercede for us and bear our sins, it saves us so much trouble, but caution him to be careful. You remember that after making the earth he thought it was flat, had ends and that the eastern continent was all there was of it.

Oh, thou great and fearful God, hold not thy peace but do as I request, Psalms CIX., your holy word.

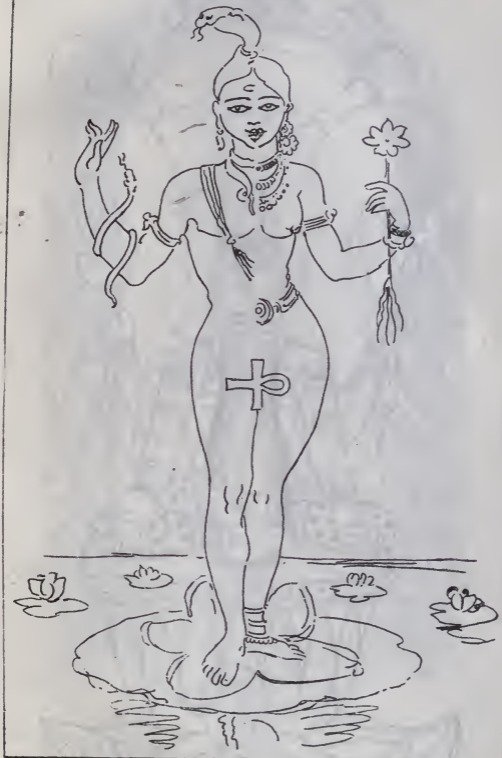
Amen.

Wonderful things in the Bible I see. This is the dearest, that Jesus loves me."

So glad she finds a lover! But how about Jesus? Can it be pleasant for him to shelter all of the hypocrites, thieves, murderers and sour old maids that propose to rest in his bosom?



"THE SUPREME SPIRIT IN THE ACT OF CREATION BECAME, BY YOGA, TWO-FOLD, THE RIGHT SIDE WAS MALE, THE LEFT WAS PRAKRITI. SHE IS OF ONE FORM WITH BRAMAH. SHE IS MAYA, ETERNAL AND IMPERISHABLE, SUCH AS THE SPIRIT, SUCH IS THE INNERENT ENERGY, (THE SACTI) AS THE FACULTY OF BURNING IS INHERENT IN FIRE."  
(BRAMAH VAIVARTTA PURANU, PROFESSOR WILSON.)



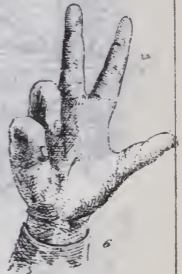
ARDANARI-ISWARA.

FROM AN ORIGINAL DRAWING BY CHRISNA SWAMI, PUNDIT.



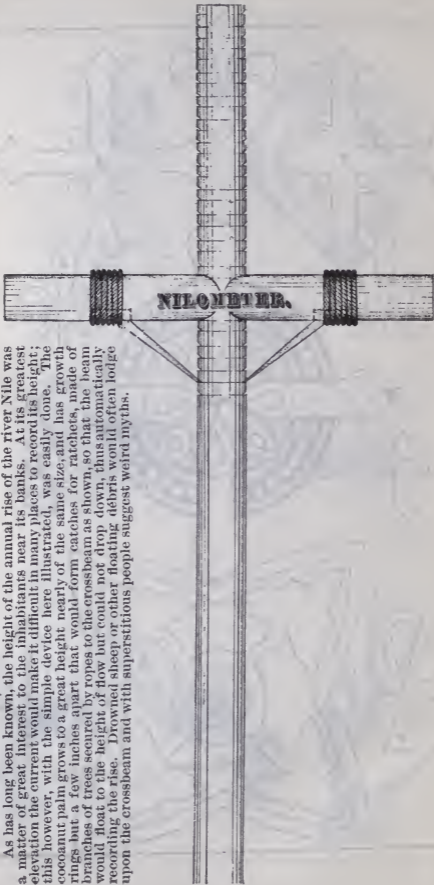








As has long been known, the height of the annual rise of the river Nile was a matter of great interest to the inhabitants near its banks. At its greatest elevation the current would make it difficult in many places to record its height; this however, with the simple device here illustrated, was easily done. The cocoanut palm grows to a great height nearly of the same size, and has growth rings but a few inches apart that would form catches for ratchets, made of branches of trees secured by ropes to the crossbeam as shown, so that the beam would float to the height of flow but could not drop down, thus automatically recording the rise. Drowned sheep or other floating debris would often lodge upon the crossbeam and with superstitious people suggest weird myths.



## The Hindu Religion.



Vishnu.

Siva.

Brama

The ancient religion of the Hindūs was different from that which now exists. One supreme being was worshiped under the name of Brama, and the two gods, Siva and Vishnu, Vishnu as the Preserver, and Siva as the Destroyer.

The simple religion which, at first, taught the people to adore one divine power as the universal Creator, and other gods merely as personifications of his various attributes, in course of time degenerated into idolatry, by the practice of setting up numerous heroes as objects of adoration, and filling the temples with their images. Among the most celebrated of these were Rama and Crishna.

The peculiar doctrine of the Hindūs, as is well known, is transmigration; but they believe that, between their different stages of existence, they will, according to their merits, enjoy thousands of years of happiness in some of the heavens already described, or suffer torments of similar duration in some of their still more numerous hells. Hope, however, seems to be denied to none: the most wicked man, after being purged of his crimes by ages of suffering, and by repeated transmigrations, may ascend in the scale of being, until he may enter into heaven and even attain the highest reward of all the good, which is, incorporation in the essence of God.

Their descriptions of the future states of bliss and penance are spirited and poetical. The good, as soon as they leave the body, proceed to the abode of Yama, through delightful paths, under the shades of fragrant trees, among streams covered with the lotos. Showers of flowers fall on them as they pass; and the air resounds with the hymns of the blessed, and the still more melodious strains of angels. The passage of the wicked is through dark and dismal paths; sometimes over burning sand, sometimes over stones that cut their feet at every step: they travel naked, parched with thirst, covered with dirt and blood, amidst showers of hot ashes and burning coals; they are terrified with frequent and horrible apparitions, and fill the air with their shrieks and wailing.



## Prometheus Unbound.

From the Dramas of Æschylus.

### DRAMATIS PERSONÆ.

|             |                          |
|-------------|--------------------------|
| PROMETHEUS, | HERMES,                  |
| OCEANOS,    | STRENGTH and FORCE,      |
| HEPHESTOS,  | Io, Daughter of Inachos. |

*Chorus of Nymphs, Daughters of Oceanos.*

[SCENE.—*Scythia; to the right a rocky promontory of Caucasus, to the left the Euxine. Enter HEPHESTOS, with hammer and chains; PROMETHEUS is led in by STRENGTH and FORCE.*]

Among the grand ideals bequeathed to the world by Hellenic genius there is none, perhaps, which has more deeply impressed the poetic imagination than the much-enduring Titan; none, certainly, which has for a longer period colored the stream of philosophic thought. The Promethean myth, it must be remembered, was not the invention of either Hesiod or Æschylus; its root, as Bunsen remarks, is older than the Hellenes themselves. Even at the present day, the legend, in its rudest form, may be traced among the Iranian tribes of the Caucasus, while in our western world it has inspired the genius of more than one great poet of modern times.

The three dramas of which the trilogy consisted are believed to have been "Prometheus, the Fire-bringer," "Prometheus Bound," and "Prometheus Unbound," of which the second has alone survived.\* Prometheus there appears as the champion and benefactor of mankind, whose condition, at the close of the Titanic age, is depicted as weak and miserable in the extreme:

"Seeing, they saw in vain;  
Hearing, they heard not; but, like shapes in dreams,  
Through the long time all things at random mixed."

Zeus, it is said, proposed to annihilate those puny ephemerals, and to plant upon the earth a new race in their stead. Prometheus represents himself as having frustrated this design, and as being consequently subjected, for the sake of mortals, to the most agonizing pain, inflicted by the remorseless cruelty of Zeus. We have thus the Titan, the symbol of finite reason and free will, depicted as the sublime philanthropist, while Zeus, the supreme deity of Hellas, is portrayed as the cruel and obdurate despot, a character peculiarly revolting to Athenian sentiment.

\* Gruppe has, I think, satisfactorily refuted the plausible hypothesis of Hermann, that the "Prometheus Unbound" was composed prior to, and independently of, the "Prometheus Bound."

**PROMETHEUS UNBOUND.**

By many supposed to be the origin of the Christ myth.



## THE MYTHOLOGY OF THE GREEKS.

The mythology of the Greeks seems to have been taken from traditions reaching back into the mist of time, from people so remote as to be even unheard of, Homer being credited with furnishing the earliest account of actions having any claim to authenticity, and that of doubtful reliability. Hesiod's Theogony treats of the fabled gods and goddesses, but it is difficult to make up any connected idea of the beliefs of the most intelligent minds of his time, though we have accounts of Pythagoras's ideas of reincarnation somewhat later.

Many of the allegories are most likely the work of writers of romances like that of the "Golden Ass" by Apuleius, in which the story of Psyche, her envious sisters, and irate mother-in-law, Venus, is so charmingly told. The beautiful allegories of Diana surprised by Actæon in her sylvan bath, where he is changed to a stag and



Diana and Actæon.

torn by his own hounds, or passions; Juno, with her Argus having a hundred eyes located in the tail, as the representative of jealous watchfulness; Minerva, Niobe, Echo, Narcissus, and many others, —have no parallel.

Then, in statuary, Greece stands alone in representing ideas: Venus with form to represent what perfect womanhood requires to perpetuate the human race in condition suitable for progression; Bacchus, representing innocent pleasure that may result from a proper use of the grape. Science can raise no ludicrous contradictions to the ideals of Greece, but it is difficult to gather these ideals from works of those days, and much more pleasant to take them



THE COUNCIL OF THE GODS.

from such works as Bulfinch's "Age of Fable," a work that must have required much time and patience and which contains a vast amount of interesting reading, and from which I gather the following account of creation.

### PROMETHEUS AND PANDORA.

The creation of the world is a problem that interests the intelligent, and the account is as follows: In the beginning chaos reigned. The seeds of things, earth, sea, and air were mixed in confusion. God and nature interposed, separating earth from sea, and heaven from both. A god appointed places for bays and rivers, raised mountains, scooped out valleys, distributed woods, fountains, and fields. Fishes took possession of the seas; birds, of the air; and beasts, of the fields. A nobler animal was wanted, and man was made.

Prometheus took some of the earth, and, kneading it with water, made man in the image of God, giving him an upright stature, so that, while all other animals looked down to the earth, man gazed to the stars. Epimetheus undertook to provide animals with suitable faculties for preservation, but, when he came to provide for man, he had been so prodigal that there was nothing left to bestow upon him. Prometheus went up to heaven, lighted his torch from the sun, and brought fire down to man. With this gift man was able to make weapons, tools, and warm his dwelling, so as to be independent of climate, and introduce all conveniences. Woman was not yet made, so Jupiter, being displeased with Prometheus and Epimetheus, made her and sent her to them, to punish them for having stolen the fire from heaven, and also to punish man for having accepted the gift. Her name was Pandora. Every god contributed something to perfect her. Venus gave her beauty; Mercury, persuasion; Apollo, music; etc., etc. Thus equipped, she was conveyed to earth and presented to Epimetheus, who gladly accepted her, though cautioned by Prometheus to beware of Jupiter and his gifts. Epimetheus had in his house a jar in which were kept certain noxious articles. Pandora, seized with curiosity, one day slipped off the cover and looked in. Forthwith there escaped plagues, gout, rheumatism, spite, envy, and revenge. Pandora hastened to replace the cover, but, alas! the whole contents had escaped, except hope, which lay at the bottom, so that hope never leaves us. The world being furnished with inhabitants, truth and happiness prevailed, and it was called the Golden Age. The Silver Age followed; then labor was required to raise crops. Then came the Brazen Age, and, later, the Iron Age; trade, commerce, murders, and pillage prevailed. Jupiter, becoming indignant at the wickedness, determined to destroy mankind and begin anew. First he thought of burning, but concluded to drown, so set the torrents to work after the deluge style.

Parnassus alone of all the mountains overtopped the waters. Deucalion and his wife Pyrrha of the race of Prometheus found refuge on top of Parnassus. Deucalion and Pyrrha were faithful worshippers of the gods, so Jupiter ordered the north winds to dry up the waters, and the winds obeyed. Then Deucalion thus





PANDORA.

addressed Pyrrha: "O wife, only surviving woman, would that we possessed the power of our ancestor Prometheus and could renew the race as he made it! but, as we cannot, let us seek yonder temple and inquire of the gods what remains for us to do."

They entered the temple and fell prostrate and prayed the goddess to inform them how they might retrieve their miserable affairs.



The Oracle answered, "Depart from the temple with head veiled and garments unbound, and cast behind you the bones of your mother." They heard the words with astonishment. Pyrrha first broke silence: "We cannot obey, we dare not profane the bones of our parents." They revolved the oracle in their minds. At length Deucalion spoke: "Either my sagacity deceives me or the command is one we may obey without impiety. The earth is the great parent of all; the stones are her bones; these we may cast behind us." They veiled their faces, picked up stones and cast them behind them, and, wonderful to relate, these began to grow soft and assume shape and resemblance to human beings. Those thrown by Deucalion became men, and those thrown by Pyrrha women.

That this is another version of the Adam and Eve story there can be no doubt, only a more manly one than that *she* did it.



Deucalion and Pyrrha.

## HEBREW MYTHOLOGY.

In the beginning God created the heaven and the earth. And the earth was without form, and void; and darkness was upon the face of the deep; and the Spirit of God moved upon the face of the waters. And God said, Let there be light: and there was light. And God made the firmament, and divided the waters which

were under the firmament from the waters which were above the firmament : and it was so. And God called the firmament Heaven : and the evening and the morning were the second day. And God said, Let there be lights in the firmament of the heaven, to divide the day from the night ; and let them be for signs, and for seasons, and for days, and years.

And God said, Let us make man in our image, after our likeness : and let them have dominion over the fish of the sea, and over the fowl of the air, and over the cattle, and over all the earth, and over every creeping thing that creepeth upon the earth. And so God created man in his own image, in the image of God created he him ; male and female created he them.

And the Lord God formed man of the dust of the ground, and breathed into his nostrils the breath of life ; and man became a living soul. And the Lord God planted a garden eastward in Eden ; and there he put the man whom he had formed. And out of the ground made the Lord God to grow every tree that is pleasant to the sight, and good for food ; the tree of life also in the midst of the garden, and the tree of knowledge of good and evil.

And the Lord God took the man, and put him into the garden of Eden, to dress it and to keep it. And the Lord God commanded the man, saying, Of every tree of the garden thou mayest freely eat : but of the tree of the knowledge of good and evil, thou shalt not eat of it : for in the day that thou eatest thereof thou shalt surely die. And the Lord God said, It is not good that the man should be alone : I will make him an help meet for him.

And the Lord God caused a deep sleep to fall upon Adam, and he slept ; and he took one of his ribs, and closed up the flesh instead thereof : and the rib, which the Lord God had taken from man, made he a woman, and brought her unto the man. And Adam said, This is now bone of my bones, and flesh of my flesh : she shall be called Woman, because she was taken out of man. Therefore shall a man leave his father and his mother, and shall cleave unto his wife : and they shall be one flesh. And they were both naked, the man and his wife, and were not ashamed.

Now the serpent was more subtile than any beast of the field which the Lord God had made : and he said unto the woman, Yea, hath God said, Ye shall not eat of every tree of the garden ? And the woman said unto the serpent, We may eat of the fruit of the trees of the garden : but of the fruit of the tree which is in the midst of the garden, God hath said, Ye shall not eat of it, neither shall ye touch it, lest ye die. And when the woman saw that the tree was good for food, and that it was pleasant to the eyes, and a tree to be desired to make one wise ; she took of the fruit thereof, and did eat ; and gave also unto her husband with her, and he did eat. And the Lord said, Who told thee that thou wast naked ? Hast thou eaten of the tree whereof I commanded thee, that thou shouldest not eat ? And the man said, The woman whom thou gavest to be with me, she gave me of the tree, and I did eat. Unto the woman he said, I will greatly multiply thy sorrow and thy conception ; in sorrow thou shalt bring forth children : and thy desire shall be to thy husband, and he shall rule over thee.

MYTHS OF PREHISTORIC TIMES OF UNKNOWN AND UNKNOWABLE ORIGIN.  
 THE CREATION. THE FALL. THE EXPULSION. THE LAST JUDGMENT.



Certainly myths of a cruel and low state of civilization, when the few lived upon and ruled the many with an iron hand, which unhappily, through superstitious ignorance is still continued and must be until the priest is relegated to the oblivion of the megatherium and pterodactyl; Ireland nor the countries of South America will ever have stable or peaceful governments while priestcraft dominates. A constant struggle in this country is going on for more power to the hierarchic influence, but history proves beyond dispute the fact that as that influence decreases the elevation of the masses increases.

In Roman Catholic countries lewd books and pictures may be found in profusion, and in such pictures the male figure invariably is a priest. For the general prevalence of such belief there must be cause. While writing this article, happening to cast my eyes over a daily paper, an article in large type met my gaze giving an account of a Massachusetts minister following one of the fair ones of his flock so persistently that her husband stoned him away as he would have stoned a hog from his garden. One can hardly look over a paper without meeting something of the kind. Ministers and priests should be looked upon as sharp business men. Priest-craft as a trade has paved its cruel pathway with fire and blood; its unscrupulous lust for power has been unending, its abnegation of trade interest only upon compulsion. It is a curse to humanity and should end. A gospel shop is a place of business and should be taxed.

15 And Moses said unto them, Have ye saved all the women alive?

16 Behold, these caused the children of Israel, through the counsel of Balaam, to commit trespass against the Lord in the matter of Peor, and there was a plague among the congregation of the Lord.

17 Now therefore kill every male among the little ones, and kill every woman that hath known man by lying with him.

18 But all the women-children, that have not known men by lying with them, keep alive for yourself.

35 And thirty and two thousand persons in all, of women that had not known man by lying with him.

40 And the persons were sixteen thousand, of which the Lord's tribute was thirty and two persons.

41 And Moses gave the tribute, *which was* the Lord's heave-offering, unto Eleazar the priest, as the Lord commanded Moses.

The priest was there.

THE FEARFUL PRESENCE OF GOD UPON THE MOUNT.



EXODUS. XIX

AN ANGEL DESTROYETH THE ASSYRIAN HOST.



2 CHRONICLES. XXXII

BEARS DESTROY THE CHILDREN THAT MOCKED ELISHA



KINGS

THE MIDIANITES SPOILED, AND BALAAM SLAIN.



NUMBERS XXXI



## Lot and His Lovely Daughters.

### GEN. XIX.

\* 8 Behold now, I have two daughters which have not known man; let me, I pray you, bring them out unto you, and do ye to them as *is* good in your eyes: only unto these men do nothing; for therefore came they under the shadow of my roof.

31. And the first-born said unto the younger, Our father *is* old, and *there is* not a man in the earth to come in unto us after the manner of all the earth:

32. Come, let us make our father drink wine, and we will lie with him, that we may preserve seed of our father.

33. And they made their father drink wine that night: and the first-born went in, and lay with her father; and he perceived **not** when she lay down, nor when she arose.

34. And it came to pass on the morrow, that the first-born said unto the younger, Behold, I lay yesternight with my father: let us make him drink wine this night also, and go thou in, *and* lie with him, that we may preserve seed of our father.

35. And they made their father drink wine that night also: and the younger arose and lay with him; and he perceived **not** when she lay down, nor when she arose.

36. Thus were both the daughters of Lot with child by their father.

Mothers, look at the three! Can you desire your children to accept such filth as from the Creator of this beautiful world? The hard-shelled Baptist that opened his prayer with "Oh, Thou great and diabolical God!" was not much off his base.

\* Do spiritualists do anything like that?



## NOAH AS A HUSBANDMAN.



20 And Noah began to be a husbandman, and he planted a vineyard:

21 And he drank of the wine, and was drunken, and he was uncovered within his tent.

22 And Ham, the father of Canaan, saw the nakedness of his father, and told his two brethren without.

23 And Shem and Japheth took a garment, and laid it upon both their shoulders, and went back-

ward, and covered the nakedness of their father: and their faces were backward, and they saw not their father's nakedness.

24 And Noah awoke from his wine, and knew what his younger son had done unto him.

25 And he said, "Cursed be Canaan: a servant of servants shall he be unto his brethren.

26 And he said, "Blessed be the Lord God of Shem, and Canaan shall be his servant.

Shortly after the publication of a sermon upholding slavery, founded upon the above, the writer heard Theodore Parker exclaim, "When a minister says that he believes that slavery is right, I believe he lies, and I believe that he knows that he lies." It is well known by the intelligent that that absurd story was the bulwark of the slaveholder and excuse of the northern doughfaced trader in merchandise of souls. For ages it has been the excuse for robbing the negro of his entire rights, and a stumbling block in the way of temperance reform. Yet the Christian minister who pretends to leadership in morals keeps up the old claim of divine inspiration and authority for the heathen stuff. Pity that there were not more Theodore Parkers! It is true that in making improvements bogs have to be wriggled through as well as mountains to be shattered, so that, if a man lacks the thunder and dynamite necessary to shatter the mountain that he may penetrate to the coal, he may still be useful as a scullion by filling the hod and carrying the coals to the cook. But it would take a great many preachers even of the late Henry Ward Beecher or the present Minot J. Savage stamp to make one Theodore Parker, or to check the universal adulteration of the necessaries of life, or the selfishness of the rich who shout for a high tariff to keep up wages, knowing full well that the pretense of high wages is filling the country with the lowest class of labor to such an extent that hardly one in three of the better class can obtain employment.





What mother finding that her young daughter had cuddled her *feller* all night between her breasts would believe it was only from love to Christ? Would a good mother encourage emulation of the tigress Judith, or the lecherous Abishag? A continued reverence for such ideas denotes barbarism, superstition, ignorance, and selfishness, certainly no thought of universal good for all.

## DANIEL'S VISION OF THE FOUR BEASTS.

DANIEL VII. 3.



And four great beasts came up from the sea, diverse one from another.

“Vice is a monster of so frightful mien,  
As to be hated needs but to be seen;  
Yet seen too oft, familiar with her face,  
We first endure, then pity, then embrace.”

And to prevent such familiarity the Bible should be banished from our schools.

Holbein's Bible illustrations so much admired in the sixteenth century that they were painted upon the walls of buildings of the streets; if so exhibited to-day our clerical Pandarus, Anthony Comstock, would have the author arrested for obscenity and profanity. The illustrations of the Creation, Expulsion, Jewish, and Puritan ideal of the Creator, with the vision above, are from that lovely work and are published as the readiest means of displaying the cream of Bible ideal. If we should hear of “Times, times, and a half times,” from an author to-day, we should look upon it as the maudlin utterance of a lunatic or inebriate, and such visions as the above or the beast with its seven heads and ten horns of Revelations as the effect of nightmare or delirium tremens.

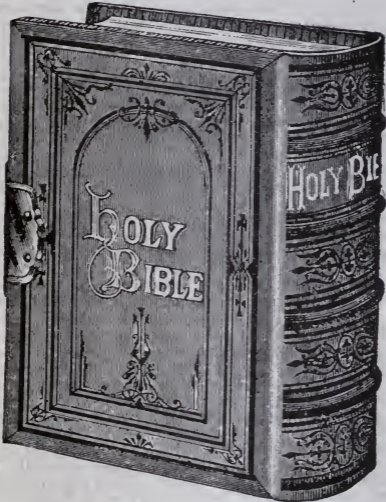
The Bible represents the opinions of the writers of its times and is as much out of place to-day in family or school as would be the writings of Apuleius, Boccaccio, Rabelais, Fielding, or Smollett, yet either may be very useful to the student. Blind, ignorant prejudice and idolatry only can account for the continuance of the former in schools; the woman that reads the passages illustrated (by no means the worst that can be found therein), and then desires its continued use as the word of God, must be a human monstrosity and certainly unfit for motherhood; but she presents a terrible example of the effect of early instruction in religious superstition.



An all-wise God obliged to determine his creatures' faith. Is it to be understood that the modern imitators of old David, who murder husbands in order to get their wives, are also men after God's own heart? If not, why continue to cultivate such belief? The book of Mormon fiercely condemns polygamy, so that Brigham Young had to go to the Bible of Christianity for authority for that practice. I have the statement over his own signature.

## TO THE INNOCENT AND INTELLIGENT.

If espionage and discrimination are to be practiced at all, is this a proper book to be carried in the mails ?



If so, then please define where *sacred license* ends and *profane obscenity* begins.

And the Lord said, "Who hath told thee that thou wast naked?" Ah, sure enough, Messrs. Parkhurst and Comstock, how happened you two to have such keen sight for nakedness? Why, if made in his own image, should the sight so offend your purity? Would not the interrogation of the Creator imply your impurity? "God's last and best gift to man," in her natural perfection, offers evidence of creative design, to the author, that the world could not shake.

## “The Bible.”

My mother, like most New England mothers of her time, firmly believed in the infallibility of the Bible and insisted that her children should study its contents, so that its stories from my earliest childhood have been familiar to me, for I cannot remember back when I could not read any story that I could get hold of. I can well remember how the story of “Susanna and the Elders” was given to me to read as a reward for some slight assistance in her many duties, the dear soul not thinking that the unbiased mind of a child might see the rascality of the priest as well as the smartness of the Daniel.

The reliability of the Bible stories have often been fiercely disputed in my hearing, yet without causing me to think the authors guilty of intentional misrepresentation, but I do believe that through ignorance or fraudulent piety what were beautiful allegories have been given meanings very different from their original purposes.

Allegory has ever been common with primitive people. Many beautiful ones have been handed down through Homer, Hesiod, and others, not as original with them or their times but as fragmentary traditions of a much earlier people, so probably of the Bible stories.

It was common with the writers of Plato’s time to commence a story with “Away back in the dark ages.” Many of those writers mention dates of ten to twenty thousand years previous, and in the works of one I cannot recall it is stated that the Babylonians claim to have authentic records reaching back four hundred and seventy thousand years, certainly sufficient time for the production of myths.

We have stories of the Cyclops, Polyphemus, Perseus, and Andromeda, Penelope, Æneas, Anchises, the beautiful story by Apuleius of Psyche, her envious sisters, Cupid and his mother Venus, and a thousand others all coeval with the Bible myths and quite likely different versions from the same originals.

It is not difficult for a person of ordinary imagination to perceive how easy it would be to construct an allegory from the meaning of the names of individuals as given in the appendix of all complete editions of the Bible. “David dancing naked before the Lord,” as there explained, can hardly be looked upon as a kingly performance, but allegorically it might mean much; so of Jonah and the fish story, Samson and Delilah, etc.

It is my sincere belief that if we could have the true meaning of the Bible stories, we should at least have common sense and often very applicable parables, instead of which they have been so distorted that only fanaticism can make their application perceptible. For instance to pretend that the salacious rhapsodies of Solomon’s songs refer to the love of the Church for Christ, puts the love of the Church on a very low plane to say the least, and makes a large draft upon the credulity of the unbiased mind and certainly is expecting too much to suppose that children uninstructed will ever look upon such reading in that way. The allegory of the Witch of Endor as given by W. H. C., coincides so entirely with my idea of Bible stories, that I herewith give it space.



## THE WITCH OF ENDOR.

The definitions of words as understood by the ancients is necessary to be learned before it is possible to understand this beautiful allegory.

"Saul," in the Hebrew, means death, or hell, or the grave, or winter, or demanded, or sepulcher, or lent, or ditch; for every noun and verb in that jargon, erroneously called a "language," had a great variety of significations, often self-contradictory. Winter was the beggar, the asker, the receiver.

"David" means the lover, the beloved, the giver, the summer, etc.

"Samuel" means heard of God, or asked of God, or earth at the vernal equinox, where Samuel died and was buried, where the Jewish ecclesiastic year always began and does to this day, the civil year beginning at the autumnal equinox.

"Endor" means fount of the dwelling place, or the last summer constellation, or Virgo, the virgin.

Winter ended at the vernal equinox, and it was there that summer began. Saul, or winter, arrives there and finds David with the Philistines (those that dwell in villages, or summer constellations) gathered to meet him, "and he was afraid." He wanted a fortune teller to advise him, but he had "put away those that had familiar spirits, and the wizards, out of the land." That is, Virgo had set the previous year, just as Aries, the harbinger of summer, rose in the east with the sun. But now, at the vernal equinox, where winter must end, Virgo was visible; for the first point of this constellation is distant from Aries 150 and the last point 180 degrees.

"Saul disguised himself." This is a very pretty conception on the part of the author, for winter moderates as the sun approaches the vernal equinox, about March 21, and is not at all like the winter in January. So it is no wonder the old woman of Endor did not know him. But when Aries rose with the sun she knew the end of winter was at hand; that is, knew Saul, which means the five winter months, or the brethren of the rich man in hell. Saul asked her what she saw, and she replied: "I saw gods [Elohim in the Hebrew, and the very word which is translated God, as the God of the Bible] ascending out of the earth."

At the vernal equinox the sun enters Aries, and the two together, sun and Aries, are Elohim in the plural number, or "gods," for *im*, added to the singular, forms the plural in Hebrew; thus *cherub*, a bull; *cherubim*, bulls. Therefore, as Virgo was setting in the west she saw the "gods," sun and Aries, rising out of the earth, or Ramah, where Samuel was buried.

During winter the earth may be said to be "dead," but is revived at each coming spring.

So Virgo raised Samuel from the dead, for, as she sets in the west, up comes the sun and Aries in the east, the signal for the death of Saul, or end of winter. Saul complained to Samuel that the Lord had departed from him; that is, the cold, the spirit of winter; even Jack Frost would not answer when he called. The earth in spring putting on her beautiful garments of green, now informs winter that its last hour is at hand. Once more the battle has been fought between heat and cold, light and darkness, and once more cold and darkness have been conquered.

"Then Saul fell straightway all along on the earth, and was sore afraid because of the words of Samuel; and there was no strength in him [of course



not, for cold is the strength of winter]; for he had eaten no bread all the day, nor all the night." I. Sam. xxviii., 20.

The supply of provisions for the winter was often exhausted before the sun reached Pisces, the fishes, when the people lived on fish for just forty days before the sun reached the vernal equinox, or Aries, the "Lamb of God that takes away the sins of the world"; not the sins of the people: but the evils of winter. Here was the origin of Lent, or abstaining from meat and living on fish.

All the ancient mythologies abound with allegories descriptive of the changes from summer to winter, and winter to summer. Vishnu had a thousand names, and it may be summer and winter had equally as many; but whether more or less, the prominent idea seemed to be that all those names for summer meant heat and light, while those for winter meant cold and darkness. Twice each year these opposing elements made war upon each other, the decisive battles being fought at the two equinoxes. Light always conquered at the vernal equinox, only to be defeated by darkness six months later at the autumnal equinox. "More light!" was the agonized cry of those in the bonds of darkness, or "outer darkness," weeping and gnashing their teeth because they had no food to gnash. True, the sun is darkened during winter by reason of the clouds and storms, but its "fire is never quenched," and the fire of the sun is the only fire that time does not quench.

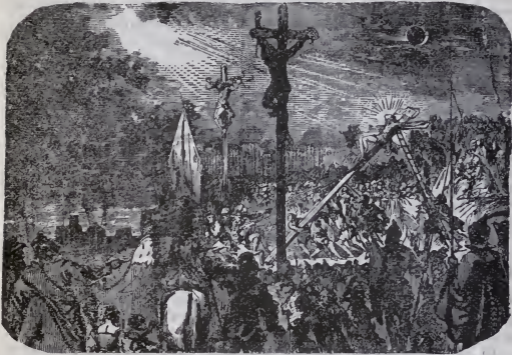
Samuel anointed Saul king of winter, well knowing that Saul would be dethroned by the king of summer when the sun reached the spring equinox. David, a mere youth, was chosen king of summer. He was sent to Saul on an ass (the sun while transiting through Cancer, a summer constellation, passes the two asses, "whereon no man ever sat"). Leaving Cancer, the sun transits through Leo, the lion (Hercules), passing a conjunction of Ursa Major, the bear, when both the lion and the bear are invisible, being metaphorically slain. David boasts of these victories, and prepares to meet Goliath (passage, revolution, heap, discovery), the spirit of summer, which can be "laid" only by winter. Therefore, he takes "five smooth stones," symbolical of the five winter months, from the brook, or by metonymy, the zodiac, and kills this giant.

Saul was so delighted with the valor of the beardless youth (the crops were not yet ready for harvest) that he gave him his daughter.

This is very ingenious, depicting the strategies of war. David plays the courtier to Saul, yet means to overcome him in the end; Saul professes to love David, but is jealous of him, and gave him Michal (complete) as a snare; that is, leaving Leo, the sun comes to Virgo, which "completes" the summer. Not much gift about it, however, for Virgo was a summer constellation and belonged to David, king of summer. The strife between Saul and David was descriptive of the struggle between cold and heat. David is conquered when the sun leaves Virgo, and must now flee before Saul till the end of winter, when Saul falls "all along on the earth."

W. H. C.

## A MYTH OF UNSETTLED ORIGIN.



That an event so remarkable as the one illustrated above could take place without being noticed and fully recorded by such a man as the elder Pliny, will not be credited by persons of ordinary intelligence unless their minds have been perverted by their infant education.

All accounts of that period agree that skepticism prevailed in relation to the myths handed down from the earlier times, and that the ablest minds believed that to do right was the best religion.

"Love thy neighbor as thyself, and do unto others as you would have the others do unto you," was all the creed needed by man. But a creed so simple offered no excuse for the support of a priesthood, the curse of humanity from the dawn of history. Certainly no worse plagues were let loose by the curious Pandora than these useless vampires that have fattened upon the labor of others, doing all in their power to prevent the enlightenment of mankind, because enlightenment is disastrous to superstition, and dogma and superstition are twins.

The history of Christianity, by Gibbon, is a history of continual strife for fifteen hundred years of bloodshed and horror; not to gain rights, but to prevent the masses from gaining their rights.

Not one single instance can be named where Christianity worked for human progression. And no other emperor can be named that can compare favorably with "Julian the Apostate," as called by the Christians. Eusebius the eunuch, the historian of Christianity, upon whose testimony the whole fabric rests, is, or was, such a consummate liar, that it is evident none of the other historians believed him, though they used his testimony to carry out the fraud. It would almost seem that Eusebius was a sort of wag that enjoyed testing the credulity of his brother historians, for if the Bible is cor-

rect (see Deuteronomy, xxiii: 1), he could have no interest in the heaven he was so ready to lie about, but he let out one fact of interest to those seeking knowledge of the Christianity of his time, namely: "That there was nothing new or strange in the doctrine;" in other words, it was the old paganism with a new name.

What the human race has suffered, and still continues to suffer, in consequence of the old time preaching of cruel hell fire and brimstone terrors, it will never be possible to compute. The deep and lasting injuries wrought by the relentlessly steady inculcation of these most woeful of dogmas can never be compensated for in untold generations. Think of the murderous wars between different peoples; of the reckless dismemberment of empires; of the barbarous sacrifice of innocent and unoffending lives; and, not least of all, of the insanity caused by these events and the tenets that were their undeniable cause; and then say, if it be possible, that the world has in the whole course of its experience undergone equal paroxysms of torture and wretchedness from any other cause, or because of any combination of circumstances whatever.

Tertullian (A. D. 200) held that the "Books of Moses" were "not only all truth, but that all truth was contained in them." Consequently every attempt to promulgate knowledge was met by horrible persecution.

In 529 the Christian emperor Justinian suppressed the schools of philosophy at Athens, and the night of "the dark ages" closed down on what was then known as the Christian world; the night of a thousand years, in which the church ruled both temporally and spiritually; a church that claims to be the light of the world; and yet this period was the darkest that history has known.

Think of the thirty-five thousand diseased natives of the Sandwich Islands, all that remain of the four hundred thousand after being subjected to the Christianizing process named below. "A steamer recently left her European port for the Congo country, now exciting such unmeasured sympathy on account of its paganism and want of modesty in dress, with a cargo of 60,000 gallons of rum, 720 gallons of gin, 460 tons of gunpowder, and twelve missionaries!"

For fifteen hundred years Christianity has held undisputed sway, and to-day every man is looked upon as a thief. Corruption in our government is openly talked of, free passes are readily accepted by our legislators, who well know at the time that much of the legislation will be relative to the business of those from whom the passes are received. A car conductor is not allowed to take a five cent ticket unless tied to a bell punch; a clerk in a store must be checked and counter-checked. It is doubtful if a pound of honest cheese is made in the northern states notwithstanding the immense pasturage.

If you require medicine it is adulterated; if you vote, you must do so through a process that implies that rascality is general; in short, that society is rotten to the core. And this state of affairs exists, say the shallow-minded, because there is not enough of Christianity; an assertion easily disproved by turning to the description of its most flourishing days as described by Boccaccio, Rabelais, or any other early writer.

No crime or wrong can be named that has not been tolerated by

Christianity. Whenever it has been found profitable, lying and deception have been cardinal principles.

I believe that the proselyting Christian of to-day is a far more injurious citizen than the rumseller, because he begins his pernicious work with the infancy of the individual, which is seldom the case with the rumseller.

### **What Good has Christianity ever Done?**

The teachings, nominally of Jesus of Nazareth, were like those of our Spiritualists of to-day, and for the purpose of substituting a living religion for that of the dead belief then as now popular. With those teachings went the inspirations and manifestations now so common.

“By their works ye shall know them.” The works referred to are ignored by all of our popular churches.

Every phase of mediumship practiced now was practiced then by the Christians, and now by the pretended Christians ridiculed. New gospels were produced in abundance then as are the spiritual wonders now, and this continued up to the Council of Nice, and the organization of the Christian Church, when inspiration and angel visits ceased and Christianity like a dead world, our moon, became dead, having neither life, light, nor warmth therein, but instead was fitted out with an impossible and incomprehensible God of three in one, the idea of which could only have originated from the ancient Phallic worship, that certainly should cause any modest, intelligent woman to hesitate before professing a belief therein; at any rate, Miss Abby A. Judson, born in India, where the Phallic worship is likely to be understood, has abandoned the religion of her father, the once well known missionary, Adoniram Judson, and taken up with Spiritualism as the living religion of to-day.

Can an instance be named where Christianity has made a people better? The victims of a single battle field have exceeded all the sacrificial victims that would have been required in a thousand years. Think of the battles fought to prove Christians to be cannibals and vampires, worse in fact, for they claim to eat the flesh and suck the blood of their God.

Is the Christian's oath in court or his note in bank preferred to that of the unbeliever? Is he a better neighbor or citizen? Is it possible that a noble mind can desire to benefit through the sufferings of another? Can belief in vicarious atonement produce noble people? Are there any countries upon the earth where such strong bank vaults are required as among Christians, or where crime is more common?

If Christianity is founded upon divine evidence, why discourage investigation? Why lie and misrepresent the best of men because they cannot discover this evidence? What wrong can be placed against Epicurus or Paine that one should be known through Christian falsehood as a glutton, the other a drunkard? Why should the works of the world's best historians be destroyed or falsified?

“The meek and lowly Jesus” has been an ideal for ages; the following illustrations will show how the ideal has been practiced:—

## FILTHY CHRISTIAN SAINTLINESS.

Egypt, through its gloomy temperament, has produced more misanthropy in proportion to its extent than any other part of the world. It was there those gloomy sects, the Essenes and Therapeutæ, dwelt, also the Gymnosophists. These, like their Christian imitators, went nearly naked. The most rigid anchorites dispensed with all clothing except a rug or a few palm leaves around the loins. Most of them abstained from the use of water for ablution, nor did they change the garments once put on; thus St. Anthony bequeathed to Athanasius a skin in which his sacred person had been wrapped for a half century. They also allowed their hair, beard, and nails to grow so long as to be actually mistaken for bears or hyenas.

At what time these persons changed from paganism to Christianity it is impossible to determine.

The most remarkable early instance of this fanaticism on record is Paul the hermit. About A.D. 250 he betook himself to the solitary desert of Egypt, where for a space of more than ninety years he lived a life more worthy of a savage than a human being.

Anthony, an Egyptian, founder of the monastic life, fixed his abode later than Paul and died in 356, at the age of 105.

Influenced by these examples, immense multitudes followed suit. Nearly a hundred thousand at one time could be found in Egypt. With a crowd so filthy is it strange that the plague was ever with them?

It was during such a pestilence (1348) in Florence, Italy, that the stories of Boccaccio originated; a work not approved by Anthony Comstock because it mirrors too faithfully the Christianity of that time. According to that work one hundred thousand persons died of plague in that city between the months of March and July of that year. The terror was so great that all ties of affection were sundered.

One of the most renowned of those saints on record is St. Symeon, a native of Syria, who devoted himself to a monkish life for six and thirty years and in such a way as to exceed all others in glorifying God. He first mounted upon a low column, changed five times, the last being sixty feet in height and three feet square at the top, where he stood nearly naked summer and winter for fifteen years without leaving it.

He would not allow a female to approach, even his own mother. His principal occupation consisted in bowing; touching his forehead to his toes. An observer counted his doing this 1244 times without cessation, and, being tired of counting, left him at it. And for this glorifying of God the church canonized him St. Symeon Stylites. Well, reader! if his God was glorified by such a performance what would he have thought of a circus?

No wonder Christianity needed a savior, but it should have been soap and plenty of water, and still less wonder, now, that the express route to Jesus is to be jerked to him by the hangman's noose. Oh, credulity!







## THE TRUE CROSS.



Constantine, soon after his remarkable, and, as some suppose, miraculous conversion to Christianity in the year 312, took the religion of Christ to the unhallowed embraces of the state, assumed to unite in his own person the civil and ecclesiastical dominion, and claimed the power of convening councils and presiding in them, and of regulating the external affairs of the church. The account of Constantine's conversion, which is related by Eusebius in his life of the Emperor, is as follows: At the head of his army, Constantine was marching from France into Italy, oppressed with anxiety as to the result of a battle with Maxentius, and looking for the aid of some deity to assure him of success, when he suddenly beheld a luminous cross in the air, with the words inscribed thereon, "BY THIS OVERCOME." Pondering on the event at night, he asserted that Jesus Christ appeared to him in a vision, and directed him to make the symbol of the cross his military ensign. Different opinions have been entertained relative to the credibility of this account. Dr. Milner receives it, though in evident inconsistency with his creed; Mosheim supposes, with the ancient writers, Sozomen and Rufinus, that the whole was a dream; Gregory, Jones, Haws, and others reject it altogether, and Professor Gieseler, with his usual accuracy and good sense, reckons it among "the legends of the age, which had their origin in the feeling that the final struggle was come between Paganism and Christianity." For my part, I have no hesitation in regarding the whole as a fable. It was not till many years after it was said to have occurred, that Constantine related the story to Eusebius, and in all probability he did it then by the instigation of his superstitious mother, Helena, the celebrated discoverer of the true cross (?) at Jerusalem, some 250 years after the total destruction of that city, and all that it contained, and the disappearance of the identity of its very foundations, under the ploughshare of the Roman conqueror Vespasian. The subsequent life of Constantine furnished no evidence that he was a peculiar favorite of Heaven; and the results of his patronage of the church, eventually so disastrous to its purity and spirituality, are sufficient to prove that God would never work a miracle to accomplish such a purpose.

DOWLING.

**CONSTANTINE, THE FIRST CHRISTIAN EMPEROR.**

The Lord's Day or Sunday, as its name implies, was the pagans' day for the worship of their god, the sun, and every idea or ceremony of the Christian religion, except its thirst for blood, is paganism disguised by change of name.

Sun Worshipers.



Constantine as Sun Worshiper.

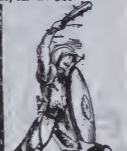


The good Constantine presiding at the council of Nice, A. D. 326.

Constantine as the murderer of his nephew twelve years of age.



Constantine as the murderer of his son Crispus, A. D. 326.



His slaughtered victims, Maximian, Bassianus, Sopater, Licinius and others.



"Oh, Fausta! pray don't make a fuss, the good Constantine, your noble husband has mildly decreed that you shall be boiled in your bath, so please come on and be boiled."

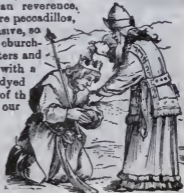


"Oh, Sop, just absolve me and oblige, yours truly, Con."



Sop.  
"The gods have no absolution for crimes like thine."  
"I will have your head, Sopater, then turn Christian!"  
And he did both.

"Absolve you, oh, of course," says his Christian reverence, "Yours were mere peccadillos, but holy grease is expensive, so you must endow a few churches. Let us roast doubters and furnish our Mary with a new petticoat dyed with the blood of those who dispute our word. Amen."





**Hypatia, Daughter of Theon, Mathematician.**

Beautiful, learned and noble. In the *holy season of Lent*, she was torn from her carriage, stripped naked, dragged to the church under the figure of the crucified Christ, and butchered by Peter the Reader, her quivering flesh scraped from her bones, then buried, and this because Cyril was jealous of her noble life.

A. D. 415.

## 529 JUSTINIAN SUPPRESS THE SCHOOLS OF PHILOSOPHY OF ATHENS



And darkness of the atrocious Christianity closed in upon humanity. Three times during the century, Rome witnessed the disgraceful scene of rival pontiffs striving for supremacy, and during these strifes originated the assertion that the Bishop or Pope of Rome is responsible to no earthly power, that he is the vicerent of God ; and Gregory, to establish his own power, invented the fiction of St. Peter and the keys. A.D. 606, Popery was established and such scenes as that below continually followed.





**Saint Gregory, Inventor of the Key Myth, about A. D. 590.**



13. When Jesus came unto the coasts of Cesarea Philippi, he asked his disciples, saying, Whom do men say that I, the Son of man, am ?

14. And they said, Some say that thou art John the Baptist : some, Elias ; and others, Jeremias, or one of the prophets.

15. He saith unto them, But whom say ye that I am ?

16. And Simon Peter answered and said, Thou art the Christ, the Son of the living God

17. And Jesus answered and said unto him, Blessed art thou, Simon Bar-jona : for flesh and blood hath not revealed it unto thee, but my Father which is in heaven

18. *And I say also unto thee, That thou art Peter, and upon this rock I will build my church : and the gates of hell shall not prevail against it.*

19. *And I will give unto thee the keys of the kingdom of heaven : and whatsoever thou shalt bind on earth, shall be bound in heaven : and whatsoever thou shalt loose on earth, shall be loosed in heaven.*

20. Then charged he his disciples that they should tell no man that he was Jesus the Christ.



The Emperor Henry IV., 1077, became obnoxious to Gregory VII., and was compelled for three winter days to stand barefooted in his shirt, as represented, at the door of his holiness, who at the time was tenderly toying with the Countess Matilda, then was allowed to enter and kiss his holiness's great toe. So like the meek Nazarene, you see !





**TWO KINGS LEADING THE POPE'S HORSE, AT THE CASTLE OF TOICI, IN FRANCE.**

King Henry II. of England, and Louis VII. of France, each dismounting, each holding a rein of his horse, on foot in abject submission, conducted him to the castle. Hume's History of England, A. D. 1161.



**THE EMPEROR FREDERICK BARBAROSSA LEADING THE POPE'S  
MULE THROUGH ST. MARK'S SQUARE, VENICE, A.D. 1177.**

## CONSTANTINOPLE, A. D. 1200.



CONSTANTINOPLE.

The vast hordes of brigands, by courtesy called Christian Crusaders, that depleted and devastated Europe from the ninth to the thirteenth century, like those of the later scoundrels, Pizarro, Cortez, and De Soto, were organized to subjugate a higher and purer civilization than that of their own, and would have been successful had it not been for the unceasing jealousies of the leaders, "Richard of the Lion's heart" and bull's brains, the Louis, Popes, and hermits, all anxious to lead, ready at any moment to turn against each other instead of against the Saracens.

Constantinople and Jerusalem were constant causes of contention between the Eastern and Western branches of a brotherhood claiming to have received their faith from an infallible divine revelation, yet one branch were continuously calling the other idolaters, the other retorting unorthodox, because of their preferring raised to sodden bread.

These differences between idolatry and unleavened bread were sufficient to cause either party to stand idle whilst the other was defending the walls against the assaults of an enemy, or often to charge their differing Christian brethren for the purpose of settling some hairsplitting dogma.

How unfortunate that revelations were not a little clearer on *dogmas!*



JERUSALEM.



**AURICULAR CONFESSION IN A CHURCH.**



**SICK LADY CONFESSING TO A PRIEST.**



## CROWNING OF NUNS UPON TAKING THEIR VOWS.

Of what good to God or Humanity?



Christianity only being the continuation of paganism under another name, it seems as though Christians, like Mussulmans, would have kept up a purer reputation by profiting by the experience of the pagans.

Jupiter, as all know, had a rakish reputation, which caused Juno to have her Argus with his hundred eyes to keep track of her lord's gallantries. These eyes, as Beecher would say, implied much, for they were located in her Argus or peacock's tail.

The Mussulman accepted the hint and placed eunuchs in charge of his harem. The Protestant managers placed the wife, equal to a regiment of Arguses, over their preachers. The experienced farmer allows of no indiscriminate mixing of the males and females of his farm stock, yet in the face of ages of such experience, scenes like those opposite and above are continued by those that should see the writing upon the wall. The adoption of the Mohammedan plan would unquestionably close the nunneries and confessionals, at the same time give a much purer reputation to the faith. If willing to make such asses of themselves as illustrated below, why not go the whole figure?



**CRUELTIES OF THE POPISH PIEDMONTESE  
SOLDIERY TO THE WALDENSES.**



**CRUELTIES OF THE POPISH PIEDMONTESE  
SOLDIERY TO THE WALDENSES.**

Were it not for the fact that the same intolerant disposition continues at this time, it would be best to let by-gones be forgotten or at least ignored, but a few years of power by either Catholic or Protestant would bring a return of the same hell-born scenes, of dashing innocent women and children from precipices, smothering them in caverns, or inclosing them in churches or other buildings and firing the same.

“Eternal vigilance is the price of liberty.”

These atrocities for hundreds of years were the work of devils in human forms.



Facsimile of papal medal in honor of the Massacre of St. Bartholomew's



MASSACRE OF ST. BARTHOLOMEW'S. IN PARIS, A.D. 1572.

## THE POPE OR GOD.



The Virgin Mary as intercessor.



Tetzel selling through tickets via the Virgin Mother. Peculiar motherhood, but not patentable from lack of novelty.



## INSOLENCE OF POWER OBTAINED THROUGH SUPERSTITION.



King John delivering up his crown to Pandulph, the Pope's Legate, A. D. 1213.



# JOAN OF ARC.

(From a Picture in the Hôtel de Ville, Rouen.)





JOAN OF ARC.

Christianity, when candidly examined from its pretended commencement, is found to be so indelibly covered by infamy that one crime alone has but little perceptible effect upon its appearance, but were its record as white as the newly fallen snow, the dastardly murder of this noble girl should condemn it through all eternity, for she has an undisputed record of a higher life than that of the apochryphal founder of that superstition.

I do not desire to be understood as asserting that there was no such person as Jesus of Nazareth, for the name was common, but I am unable to obtain evidence to that effect that would convict a suspected thief of stealing a twenty-five cent jackknife. The pretended record of his life, however, is far less creditable for consistency than that of the noble victim of the monkish devils that imprisoned, tricked, harassed, and hounded her to death. If their religion is true, God pity them, for there must be an awful reckoning for their doings.

The life of this pure, noble-minded girl is so well known that it is a waste of space to attempt to give any of it here, but that she was a spiritual medium of the purest and highest type there can be no chance for successful contradiction.

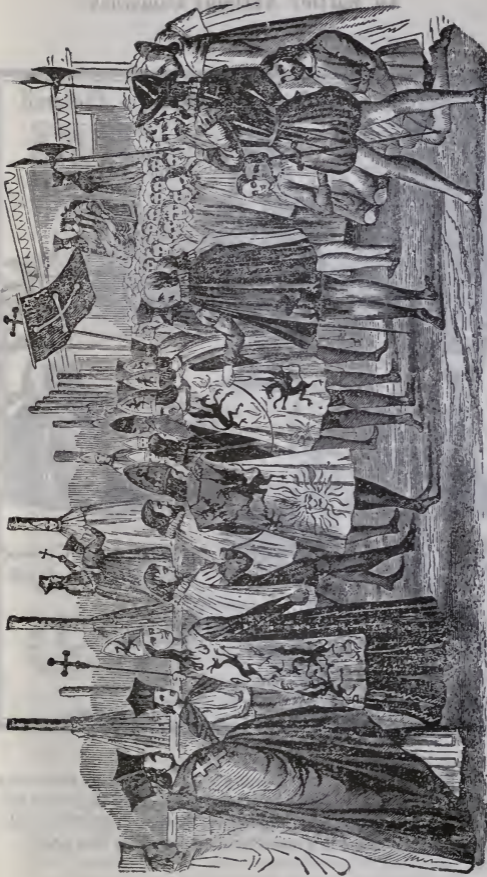
**CHRISTIAN AMUSEMENTS.**

Gibbon implies that Cranmer only received what he tried to give others.



Burning of Latimer and Ridley, at Oxford, 1555.





PROCESSION OF HERETICS CONDEMNED BY THE INQUISITION TO AN AUTO DE FE.



## An Earlier Anthony Comstock.



This illustration, representing Matthew Hopkins examining two witches who are confessing to him the names of their imps and familiars, is copied from Caulfield's *Memoirs of Remarkable Persons*, 1794, where it is taken from an extremely rare print;



## FLOATING A WITCH.



Among the ill weeds which flourished amid the long dissensions of the civil war, Matthew Hopkins, the witch-finder, stands eminent in his sphere. This vulgar fellow resided, in the year 1644, at the town of Manningtree, in Essex, and made himself very conspicuous in discovering the devil's marks upon several unhappy witches. The credit he gained by his skill in this instance seems to have inspired him to renewed exertions. In the course of a very short time, whenever a witch was spoken of in Essex, Matthew Hopkins was sure to be present, aiding the judges with his knowledge of "such cattle," as he called them. As his reputation increased, he assumed the title of "Witch-finder General," and traveled through the counties of Norfolk, Essex, Huntingdon, and Sussex for the sole purpose of finding out witches. In one year he brought sixty poor creatures to the stake. The test he commonly adopted was that of swimming, so highly recommended by King James in his *Demonologie*. The hands and feet of the suspected persons was tied together crosswise, the thumb of the right hand to the toe of the left foot, and *vice versa*. They were then wrapped up in a large sheet or blanket, and laid upon their backs in a pond or river. If they sank, their friends and relatives had the poor consolation of knowing they were innocent; but there was an end of them: if they floated, which, when laid carefully on the water, was generally the case, there was also an end of them; for they were deemed guilty of witchcraft, and burned accordingly.



God has just called the servant from a \$5,000 to a \$10,000 salary. Oh, Mr. Congress, do put God in the Constitution and stop Sunday cars! If the multitudes may have excursions instead of sermons, how are we to live?

The Master.



Oh, Brother Malbadge, Theodore Parker preached long sermons but none left, while half my hearers have gone before I get bell painted red.

Well, Brother Bulton, old chestnuts are stale; be sensational; a few lies about Spiritualism will take with our hearers and the ignorant generally.



The Servant.



WHAT IS THE DIFFERENCE IN PRINCIPLE?

SHOW WINDOW CARDS.



HONEST LONG CUT.



THE HUMBLE FOLLOWER.



FOR A FULL HOUSE.

Angels attend him.



"THREE HUNDRED LASHES."



"Petition? Engineer, go over them, unless they get out of my way!"  
"Petition for the right to think?"  
"Humph! why should they want to think, while I am willing to think for all?"

"Why, we were like brothers." Ah, very like!

*Talmage.*

FOR SIBERIA.





Has preaching arrived at so low a stage that jealousy should send one of its loudest howlers with flying coat tails to drink koumyss and eat wolf meat with the Emperor of Russia, because of the rumor that "Buffalo Bill" had dined with the Prince of Wales? And not to be outdone, doubtless Parkhurst will soon announce that he has dined *en famille* with the Grand Turk, and that from his habit of seeking for things nasty, more particularly from his New York brothel experience, he was able to explain to Mrs. Turkey why Dudu disturbed the Harem, so poetically described by Byron in his *Don Juan*. Does truth need such aid?



# A MISSIONARY, HIS CURATE AND OUTFIT.

**GUNPOWDER, RUM AND BIBLES.**  
A missionary, resident of Honolulu, has his name as owner conspicuously displayed upon the Grand Hotel and three of the best business blocks of Cedar Rapids, Iowa. Alas for the 400,000 happy natives of Capt. Cock's days! The remnant of 30,000 dissolute beings applying for annexation at this time offers indisputable evidence of the effect of a hundred years of missionary labor. Poor unfortunate Africa, your turn has come!



**HANGING QUAKERESS MARY DYAR, 1660, THE GREAT HERESY TRIAL, 1893,**

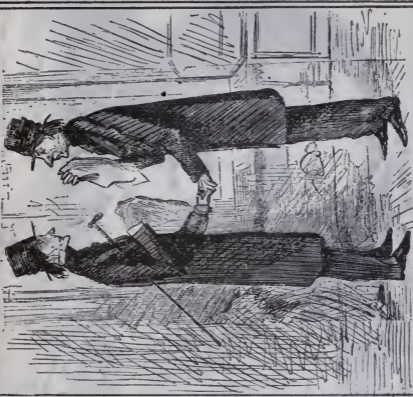
On the Big Ehn, Boston Common.

For the assertion that Tweedledum equals Tweedledee.

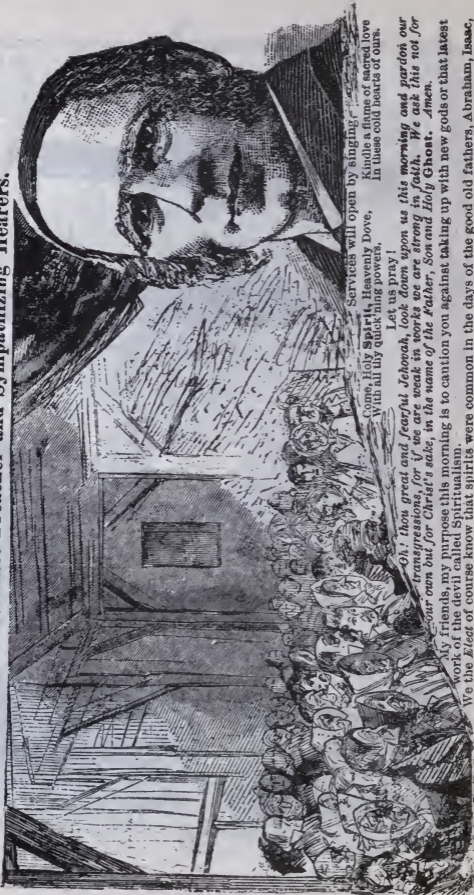


ANDOVER. Dr. BRIGGS.

Adieu, Adieu! Alas, a Tearful Farewell.



## Christian Materialist Preacher and Sympathizing Hearers.



Services will open by singing,  
Kindle a flame of sacred love  
In these cold hearts of ours.

Come, Holy Spirit, Heavenly Dove,  
With all thy quick'ning powers,

Let us pray!

*Oh! thou great and fearful Jehovah, look down upon us this morning and pardon our transgressions, for if we are weak in works we are strong in faith. We ask this not for our own but for Christ's sake, in the name of the Father, Son and Holy Ghost. Amen.*

My friends, my purpose this morning is to caution you against taking up with new gods or that latest work of the devil called Spiritualism.

We the *Elect* of course know that spirits were common in the days of the good old fathers, Abraham, Isaac, and Jacob, and equally well we know that there are no such airy nothings now. Phew! we might as well believe in ghosts!

## THE AMBITIOUS FISHERMAN.



### THE BIBLE IN SCHOOLS AND A GOD IN THE CONSTITUTION.

The Bible is a book useful for the student, but is of the past; its worship has been the cause of oceans of bloodshed. Aside from errors of translation, words often are changed in their meaning by change of locality, so that there is no certainty that we have the writer's true meaning in the Bible stories; but we can readily see from its contradictory statements that it is merely a history of that people, and through its tribal conceit all others were ignored. Cain feared that some one meeting would slay him, which could not have been the case had there been none to meet, and the very form of statement proves that the mark would be understood. Still further to find a wife at Nod, there must have been people there. Its nine hundred year lives must have meant dynasties. Its fish story most likely belonged to the class of myths common at that time in connection with the stories of the gods and goddesses. A book that cannot be opened at random and read in society is not suitable to be put into the schools to be read by children.

It is but a few years since George Francis Train was imprisoned for publishing obscene literature. Unfortunately for the complainant he was so ignorant of the Bible contents that he was unaware that the dirty literature consisted of extracts from that *sacred work*. The arrest became a boomerang. If brought to trial, the character of the contents of the Bible would be ventilated; so that Train was brought into court, and pronounced insane, consequently irresponsible, so discharged; but as that would leave him irresponsible if he saw fit to shoot the complainant, he was the next day again brought into court and pronounced sane.

Think of the fool Freeman stabbing his five year old daughter to the heart in this State and age through his insane fanaticism for emulating old Abraham.

Ideas are changing rapidly. Success in keeping the Bible in the schools or getting a God in the Constitution is likely to result something like the success of the ambitious fisherman at the head of this article.



THE DAY OF THE CHURCH.



Torquemada persuading the doubting to give their souls to God and their property to the Church.

Calvin persuading Servetus to believe in the Holy Trinity.



Procession of Corpus Christi.



Workmen of that time.





THE DAY OF THE MAN.



THE MECHANIC TO THE FRONT.

THE REAL CREATIVE MECHANIC APPROACHES NEAREST TO THE ATTRIBUTES OF HIS CREATOR THE PRIEST, LAWYER, DOCTOR, AND PROFESSOR TO BE VALUED ACCORDING TO THE USEFULNESS OF EACH. HIS POSSIBILITIES HAVE HARDLY BEEN CONCEIVED OF, LET HIM REACH OUT TO THE UTMOST UNKNOWN.

MAN AND WOMAN TO FURNISH MACHINERY TO DO THE ROUGH AND HARD LABOR.

THE LIBERTY TO REASON HAS OPENED NEW WORLDS OF THOUGHT.

OUR CREATOR IS ADMIRER FOR HIS WONDERFUL WORKS, NOT PROFESSIONS.

NON-SECTARIAN BUT UNIVERSAL EDUCATION.

STEAM, THE TELEPHONE, THE TELEGRAPH, ALL ARE IN THEIR INFANCY, AND SURE TO DEVELOP NEW FIELDS OF PROGRESS

THE FAR-REACHING TELESCOPE, THE NEAR-SEARCHING MICROSCOPE, EACH OPEN UNKNOWN WORLDS AS THEY BECOME MORE PERFECTED.

## JONAH REPINING AT GOD'S MERCY.

How long, Oh Lord, how long?—*Joe Cook.*



4 And Jonah began to enter into the city a day's journey, and <sup>a</sup>he cried, and said, Yet forty days, and Nineveh shall be overthrown.

5 ¶ So the people of Nineveh <sup>b</sup>believed God, and proclaimed a fast, and put on sackcloth, from the greatest of them even to the least of them.

10 ¶ <sup>a</sup>And God saw their works, that they turned from their evil way; and God repented of the evil that he had said that he would do unto them; and he did *it* not.

**B**UT it displeased Jonah exceedingly, and he was very angry.

2 And he prayed unto the LORD, and said, I pray thee, O LORD, *was* not this my saying, when I was yet in my country? Therefore I <sup>a</sup>fled before unto Tarshish: for I knew that thou *art* a <sup>b</sup>gracious God, and merciful, slow to anger, and of great kindness, and repentest thee of the evil.

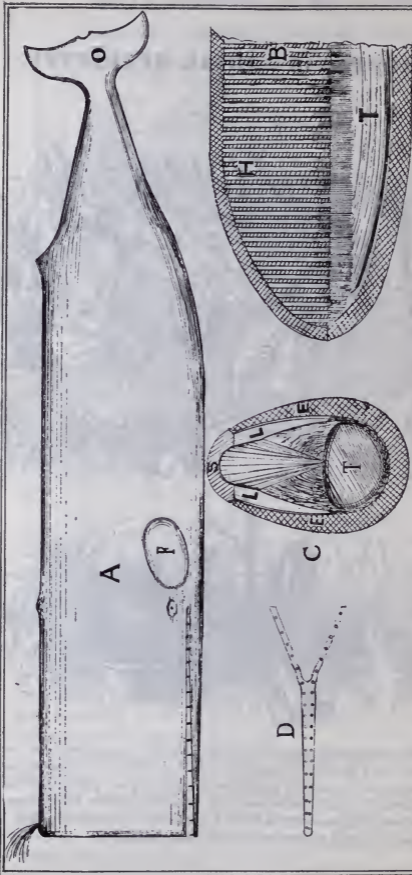
4 ¶ Then said the LORD, ¶ Doest thou well to be angry?

5 So Jonah went out of the city, and sat on the east side of the city, and there made him a booth, and sat under it in the shadow, till he might see what would become of the city.

## THE MAHOMETAN'S IDEAL HEREAFTER.



The above ideal seems on the first thought to offer a chance for the seventy thousand unmarried women of Massachusetts to get even, but more matured reflection causes the thought to arise that if supplied as liberally to each saint as indicated by the illustration, he would soon regret his success in traveling the hair bridge and wish that he had taken up his abode with the more open countenances represented in the other place.



The pen sketches above are made to represent a sperm and parts of the head of a right whale. It is nearly fifty years since the writer stood upon a whale, yet he believes the sketches to be reliable in form and proportions.

*A* represents the sperm whale with the flukes *O*, highly raised and turned that the shape and proportional size may be seen. The normal position is horizontal on the water. *D* is the lower jaw turned up sideways. *F* is the fin with eye close in front. *B* is the side of the forward part of a right whale's head, the lip being removed so that the slits *H* of what is known as whalebone may be seen in position, the fringed lower ends resting against the side of the tongue, *T*. *C* is the cut off end of the head presented to view; *T*, the tongue; *E*, *E*, the lips closed; *L*, *L*, the flat side of the bone fringed on the inner edge and lower end; *S*, the crown of the head to which the bone hangs. The end shape of the sperm whale's head is nearly the same, only the biggest part is up.

## SCIENCE AND SCIENTISTS.

The nebulous halo that hangs over science is about as misty as that which enshrouds religion. Daily we hear of science and what scientists are saying about matters that ordinary mortals are supposed to be ignorant of. Reader, are you so fortunate as to know a great scientist? If so, what does he look like, and what has he done? Was he labeled as the artist labeled his pig, that it might be understood that he tried to represent a pig? Who are these phenomenal wonders? The inventor reaches out into the unknown; no matter whether he invents a novelty in mechanics, music, poetry, chemical compound, or other matter, so long as he aids human progress he is properly the scientist.

A man is not necessarily a scientist or astronomer, because, as he is somewhat pompously inclined to assert, he holds *the chair* in some high sounding study or society, or has charge of the most powerful telescope extant. Unless he has ideas above current knowledge of popular belief, he is simply a laborer in that study, as is the ordinary workman in mechanical trades.

Much that is published as advanced science is the common knowledge of the backwoods. In my boyhood, it was a common diversion to fire a candle through an inch pine board. If the candle went through, the tallow was crumbled; if the board was so hard as to stop the candle, the tallow melted. Professor Tyndall published as one of his wonderful discoveries that a leaden bullet would melt if suddenly stopped in its flight.

Prof. Elisha Gray says that "he who wishes to keep abreast of the march of science to-day must leave the college and go to the workshop, and into the dark corners of private laboratories, for investigators rarely have time to write, so that text-books are years behind the science itself."

That the colleges are a half century behind in ordinary milling hydraulics is beyond chance for dispute.

The most of the popularly known professors of science simply *hold chairs* in institutions better known through their high sounding names than achievements.

Some years ago it was my lot to walk from Bucksport, Me., to Ellsworth. Some five or six miles out a sight met my view that surprised me. Along beside the road, and around in the fields and pastures, there were immense coarse granite boulders, some of them perfect in condition, others crumbling to pieces. This disintegration commenced perhaps at a corner, or upon all parts. Many could be seen in such a stage of decomposition that in shape they resembled haycocks of a rusty-iron-like appearance. The crumbling was so fine that it could be used for hardening the roadway. My previous experience had been somewhat extended, yet I never had witnessed anything of the kind before. Professor Agassiz, a week later, passed over the same route on his way to Mt. Desert, yet did not seem to consider the matter worthy his consideration. His attention was called to the subject, and his



opinion of the cause asked, but without obtaining a reply. Years previously, while wandering up the west coast of South America, near the equator, I arrived about sunset at a fisherman's hut in the edge of the forest, and was cordially asked to spend the night there, as it was unsafe to travel after dusk on account of the jaguars. A fire was kept up through the night to keep them from the hut. There were the father and mother, also a boy and girl of ten and twelve years of age, both naked. At sunset the tide was at its height, and the father, calling the two children, asked me to go and see them get drinking water. At a point a short distance from the hut, the boy was sent with his calabash shells a rod or more into the water, where it was up to his chin. He sank down, and remained under water until the two shells were full, each holding five or six quarts. When he rose, he held the shells up above the surface, and brought them to the shore. The girl did the same, and the shells were filled with fresh water. It seemed to me that there must be an intermittent spring there, working on the siphon principle, but on going there at midnight there was nothing but the white sandy beach to be seen. On returning home, an account of the matter was sent to Lieutenant Maury, who was then in high standing as a real scientist in relation to the winds and currents of the ocean. He answered at once, and made further inquiries.

Much that is talked of as science has no foundation in fact. For instance, how general the belief that water is alive with animalcules! Microscopes have been rather a hobby of mine for many years. I will not give powers by diameters, but by comparison that anyone will understand. One day, taking up what I had supposed was a small plate of plain glass, a speck which was thought to be a flyspeck was observed upon its surface. The glass was wiped, but the speck remained. It was placed under the magnifier, when the speck proved to be a photograph of the top of Mt. Washington, the Tip Top House,—its sign easily readable,—and twenty-two life-sized visitors there. With that glass, or others of equal power, it has never been my lot to find any living things in ordinary well or running water, nor teeth on razors, nor thorns on hairs. I have studied many works treating of natural history, yet have found none in which the most noted animals have not been caricatured rather than described. The classic dolphins of Arion were of the whale family, either what whalers call blackfish or porpoises. The dolphin is a fish of perhaps twenty-five pounds weight, and changes tints when dying, as has been described by poets, but would hardly do for riding.

I will here say something of the different kinds of whales. All know that whales are warm blooded animals, and have to come to the surface to breathe. They are designated by whalers as bulls, cows, and calves, and, like their namesakes on shore, the calves are nourished with milk from the mother, and in the same way.

The sperm whale has one nostril, or breathing hole, in the extreme forward part of the head, from which a low bushy column of spray is blown, inclining forward of the whale. The other kinds of whales, designated by American whalers as the "Right whale," "Humpback," "Finback," and "Sulphur-bottom" (the

last taking its name from the color of its belly), have two breathing holes well back in the head, from which the spray is blown in separate columns.

The sperm whale breaches clear from the water, but, instead of pitching over and entering head first, he falls back flat, making a great splash which may be seen twenty-five or thirty miles in moderate weather, while from the masthead of a ship his spout cannot be seen more than five or six miles; that of the right whale about the same distance, the humpback and sulphur-bottom perhaps a little further, while the "spout" of the finback may be seen ten or fifteen miles. At the same time, either kind of whale, in rough weather, might pass close to the ship and not be noticed by the inexperienced observer.

The sperm whale can fight with his head, his jaws, his tail, or flukes; the right whale only with his flukes; the humpback with his long fins, by rolling and striking them across a boat. The right whale sweeps sideways from eye to eye. The tail or flukes of all whales are horizontal or flat on the water, instead of being vertical like the tail of a fish.

To get near a sperm whale it is necessary to meet him "head and head" or to follow in his wake; approach him on his side and he is off at once, for the smallest object will frighten any kind of whale. The right whale must be met head and head or on his side; get in his wake, within half a mile of him, and he will leave without stopping to say good-by. The sperm whale has teeth in the lower jaw that fit into sockets in the upper. The under jaw compares with the upper in size as a man's arm with a barrel, when placed on one side of the barrel lengthwise, and the front part of the head is as square across as the head of a barrel, and when the head is cut off, if it is placed upon its forward end on the deck, it stands as will a barrel, though the head is a third of the whale.

The other kinds of whale have what is called whalebone instead of teeth, but only the right whale has it of a size to make it valuable. This bone is in thin slabs from one-fourth to one-half an inch in thickness, and from one to fourteen feet in length. The slabs hang from the roof of the mouth as the rafters of a roof hang from a ridgepole, from two hundred to two hundred and fifty slabs each side, presenting the edges only to view when the lips, which are on the lower jaw, are dropped down, looking like the slats in a window blind, only they are black and are separated about their thickness from each other. The inner edges of the slab have a fringe the whole length that looks like black horsehair. The slabs are from three to twelve inches in width where they grow to the roof of the mouth and taper to a point at the lower end. Whales with such an apparatus feed on animalcules. Their manner of feeding is to drop the lips, then move forward with open mouth until it is filled; then close the lips, blow out the water through the spout-holes, the slabs of bone, with their fringe, acting as a strainer; then the food is swallowed.

The sperm whale, after being killed, floats buoyantly. The right whale often sinks. Of the eleven that I helped kill one season only five were saved—the rest sank as soon as killed. The humpback

always sinks, and is never troubled in deep water; but at certain seasons of the year they frequent bays, where they are taken. As soon as they are killed they sink, but the line is attached to a small anchor which is dropped to the bottom to prevent the whale from being carried out to sea by the tide. In a day or two decomposition commences, generating a gas that inflates the whale so that he rises to the surface, and his oil is then obtained in the usual way. The finback is too fast a team to be easily managed, and is never troubled; and the sulphur-bottom for some reason is seldom molested; why, I do not know. They are very large. There are several other kinds that belong to the whale family,—the narwhal, the grampus, the blackfish, killer, porpoise, etc. After the blubber is stripped from the outside, the whale's flesh looks like lean beef; that of the porpoise is very good, resembling tender beef.

There are many different kinds of sharks, some of which I have seen, and others that I have not seen except in story books. The most blood curdling stories in regard to them originated probably from the desire of ship captains and owners to prevent sailors from deserting their ships. Sharks are plenty in warm or temperate climates, and in most of the harbors of commerce in warm countries. They feed upon smaller fish, it is to be presumed; plenty of sea fowl rest upon the water but are never troubled by them. In harbors near the equator, where a dozen sharks may be seen to turn up for a baited hook as minnows do in a brook, sailors swim back and forth daily. I have often swum in the harbors of Rio de Janeiro, Havana, Callao, and many other ports in the Atlantic and Pacific, and have been on whales, when cutting in, with hundreds of sharks around, and often on top of a whale so close as to have touched my side, and have kicked them away. I have seen a lance thrown through the center of a shark's body without causing a flap of its tail, and have seen them feeding greedily from the torn blubber when their entrails were hanging below them from cuts from whaling spades, so that my faith is not great in the stories that this or that native dashed into the briny deep and slew a twenty-five foot shark,—in fact, I am doubtful about the twenty-five foot shark, and about their biting a man in two and swallowing a half whole. A cut with a spade across the nose or in the gills will kill a shark instantly, but the knife combat is a trifle tough. A shark can bite hard. I have seen one grasp hold of a lump of blubber or the side of a blackfish, then turn over and twist out a piece larger than his own head, then he had to let go and eat more decorously.

I have seen sharks follow a boat and snap at the oar blades as they dipped in the water, yet a few minutes later a whale had stove our boat and all the crew were floating on the oars in the water, but we saw nothing of the sharks. Probably no whale ship was ever filled with oil without more or less of her boats being stove. I have seen three smashed to splinters by a single whale in an hour's time, yet I have never known any person bitten by a shark, nor known any person who has known of a person being bitten by one; nevertheless at the same time a shark can bite, but I should as soon believe that Jonah swallowed a whale as that the half of a man entire was found inside of a shark.

## RALPH WALDO EMERSON.

The question has often been asked me, and at times with a sneer, "Are you related to Ralph Waldo?" "Have never inquired," has been my reply.

The name of Emerson figures conspicuously in the history of Hale's Town or Weare, N. H. Stephen Emerson (who came from Hampstead to Weare), the son of Stephen, in 1762, paid the largest tax in the list of taxpayers. His son, Deacon James, married Lydia Hoyt of Salisbury, Mass. A story is handed down that one Sunday while riding to church Mrs. Emerson, through pity, requested the deacon to get off and drive a fox away from a rabbit that he was chasing over and under a log. After due reflection the request was declined upon the plea that it would be breaking the Sabbath. The wife queried whether it was not laziness instead of piety that prevented. Their son, Deacon James, was my grandfather. He and his wife, Polly Cilley, or Seelye, moved to Newbury, N. H., where they often dragged my father two miles over a mountain path lined with roots, stones, and stubs, in the dark, bare-footed, to prayer meetings. Their groans and lamentations there were not sufficient to keep him awake, so that I fear he got in the habit of saying "swear words" from being aroused and dragged home near midnight. At any rate their fervor of piety was checked on its way down.

O. W. Holmes, in his life of Ralph Waldo, implies that he was not much of a mechanic, in fact, that he could not use a spade with safety to his legs, but that was of no account, as he was a poet. Mr. Emerson was a level headed man, and, if living, would probably object to that idea. The Mechanic or Creator made the stars or they could not have sung together. Had not the mechanic made the wooden horse there could have been no Homer. The mechanic's weapons raised up the troubadours. The poet is all right in his place; but the mechanic has come to stay, and he has done more in the last hundred years to improve mankind than ever had been done by the poet. Mechanics make poems. Have poets ever produced the equal of the Columbian Fair?

What poem in grandeur equals the mountainous steamship with her forty thousand pent-up horse power under subjection to the finger of the engineer? What tragedy ever equaled the guillotine or the gallows? What comedy was ever more laughable than the mechanical fantoccini? Poetry often is grand and soul nourishing, so are mechanical movements if the observer has the ability to appreciate the beauty of nature's laws. The mechanic has produced instruments of music that have added grandeur and harmony to the poet's words they could never have reached without. The mechanic, through his telescope and microscope, has added worlds to man's knowledge that the poet might have imagined but never could have verified. Even in the so homely convenience as spectacles the mechanic has added one-third to man's practical life. Mr. Holmes, by reading Job xxxviii., will learn that poets were snubbed at times.

## THE BOSTON OF 1845.



Do those who so boastfully claim leadership in human progress for Boston or Massachusetts realize the difference between those places to-day and fifty years ago? The typical Bostonian of a half century since, who perhaps had never seen a college unless when passing its outside, was still intelligent. If Egypt was spoken of, his thoughts turned to the pyramids, the Pharaohs, and Sphinx and her conundrum, and to wonder as to its meaning. The typical Bostonian of to-day, graduate of Harvard, has faint ideas of the street in which he resides or does business, and if Egypt is mentioned in his hearing, his mind instantly turns to some dark, unsettled region where he has sold a box of flat footed brogans, ranging in size from eleven to fourteen, and if any sphinx-like conundrum comes into his mind it is in relation to how he is to get pay for his brogans.

Think of the Massachusetts of fifty years ago crowding special trains of cars for the purpose of witnessing the brutal game of football!

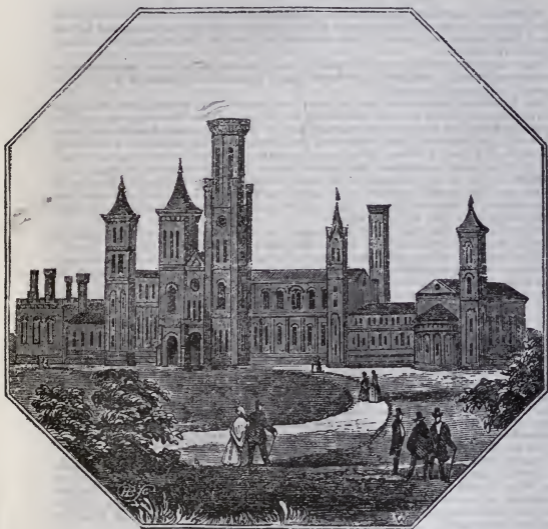
Think of the governor of Massachusetts speaking for his state at the Columbian Fair, being obliged to confine his eulogies to its past glories instead of talking of what it is now doing to aid human progression, as the sister state in which he was speaking was doing.

Look at the opposite page; study and heed its suggestions. Look also to another page illustrating the effects of forty years of the Massachusetts school system. Then simplify its laws, schools, and religion so as to agree with common sense, and thus compel its priests, ministers, and lawyers to earn an honest living. Phew! The Massachusetts of to-day, a leader in human progress! In what, pray?



*SHOW INSTITUTIONS OF THE HILLS,*

For the Blind, the Halt, the Idiotic, the Insane, the Pauper,  
and Criminal.



Can such an ostentatious display denote a high civilization ?

*“EDUCATE THE IDIOTIC.”*

Can education to such bring happiness ? If ignorance is bliss under any condition, it would seem to be so with the idiotic.

*Would it not indicate greater intelligence*

To seek for the cause and try to stop the production of idiots, paupers, lunatics, invalids, and criminals ?

*Whether entirely satisfactory to the patients,*

These institutions are convenient retreats for retiring rival politicians, at the same time producing hot-house culture of “offensive partisanship.”

## SPIRITUALISM.

### A Living Religion, of Demonstration, Personal Responsibility, and Consolation.

This belief has been latent in the human heart since the dawn of recorded intelligence down to the present time, and is now openly accepted by the most intelligent as the truth, yet sneered at by the dollar stamped clergy from self interest.

The cause has had a terrible load to carry in carrying the vagaries of its professed friends, and had it not been based upon eternal truth it would have been annihilated long ago.

Its mediums, mere mortals of very ordinary clay, instead of being encouraged and aided to seek the truth, have too often been surrounded by ruffianly bands of bigoted ignorance, and in frequent cases female mediums have been married by lazy loafers of the male species, solely as a means of obtaining a living without labor, and the wife has often been compelled to do what, if properly cherished, she would never have thought of doing.

Then again, as its expounders in many cases have belonged to, to say the least, not the most learned, the vagaries published are not always well established, to say nothing of the long words required to express the profound depths of the writer's ideas.

Then the *smellers* that seek for fraud, the self appointed witch finders of the Gagog type described by Rider Haggard in "King Solomon's Mines," who through monumental conceit and ignorantly conceived notions of spirit etiquette assume the office of censor of spiritual management, may retard but can never stop the onward march of its grand and humane truths.

From infancy I have ever desired to know the why of any mystery. My first visit to a haunted house was in my eighth year. Of course the Rochester knockings interested me, but a wandering life of ten years' previous experience in strange lands had knocked many of childhood's conceits from my mind and broadened the horizon of my ideas; personal experience also had caused consideration. It was not uncommon for me at that time to suddenly become unconscious and begin to repeat lines of poetry that would be seemingly printed upon the wall of the room in front of me. As the last word was repeated, there would be exactly such a change in appearance as takes place in a kaleidoscope and more lines would come in view. As this was about a year before the advent of the knockings my declamations were considered uncanny. A vivid impression of the fact was always left upon my mind but the lines could never be remembered.

Then followed a phase of gradually rousing from sleep to a consciousness of two or three voices near by arguing a case, so real that it would cause me to turn and try various methods to ascertain whether it was a dream; suddenly all would cease but the impression would remain for days, yet the subject could never be recalled though perfectly understood the moment before it ceased.

To this followed visions of beautiful landscapes, rarely persons or animal life, but the colors of mosses, leaves, stones, and the thousand details so perfect that at times I would get up and walk across the room to make sure of being awake. For years these were believed to be optical illusions, but I know better now and deeply regret that such gifts were not more thankfully received. Another phase followed and to some extent is still with me, namely, impressions, often as palpable as spoken words. These usually come when receiving or reading a letter, message, or communication, in one case causing me to pitch a letter containing a check for \$150 into the waste basket, for doing which the sender at times attempts to be sarcastic.

For years I took but little interest in Spiritualism, but as its adherents increased it became a power, and I took the Christian's ideal of good, the dollar, as a standard of its popularity.

At the time I was publishing a quarterly paper,

EMERSON'S TURBINE REPORTER, five thousand copies each issue to fill contract with advertisers. It had paid expenses less postage up to that time. I announced that after four more issues the paper would be discontinued and a book take its place; then commenced a series of articles on Spiritualism herewith republished in their order. The first issue containing the article paid all expense, the next \$25 above, the third over \$100, and the last over \$200, a supplement being required for advertising space.

## INVESTIGATION AND PHENOMENA.

The wonderful stories of spiritual manifestations going the rounds of the press have caused a desire for more light relative thereto; such manifestations, under various phases, have been common since the dawn of history; in ancient times the leaders of the people made them useful, now those that would be leaders are careful to ignore interest in them. Editors that are loudest in screeching, "See how independent we are!" dare not publish an article upon the subject without launching it from the top of the fence that it may be fitted for either side, by the ever convenient, "I told you so!" Why this unmanly hedging? A little inquiry will satisfy any one that the world is ready for the truth. It is true that there is a feeble "tweet, tweet, tweet" going out from the pulpit, as there doubtless was nineteen centuries since, but the time now, as then, is unfavorable to pulpits; intelligence plays the deuce with such places; there is little consistency in talking about the Bible being a guide, while building structures in which to worship the son of a carpenter, so very nice that one of that class has little chance of ever seeing the inside after taking his tools out; five to twenty thousand dollar salaries have little in common with the veritable Jesus of Nazareth, though in full accordance with the pulpit article. The time for such is passing away, the sneered at manifestations have had much to do with the change and Church creeds are kept in the background as being too illiberal for the times. Nearly every book of note now issued is spiced with the belief; our conversation is mixed with its phrases; if one doubts the general infusion let him get into quiet conversation with the first person met, and the chances are ten to one that some wonderful experience having a bearing upon the subject will be related. Some of the best known manufacturers with whom I am acquainted are deeply interested as investigators. Such, invariably, are thinkers, and usually successful in their business, some of them very remarkably so. A large portion of Turbine builders are open believers in Spiritualism, and it is but fair to state that, in not one single instance has one of that belief misrepresented results obtained from a test of wheel, while the contrary has often been the case with builders ever ready to sneer at the Spiritualist. It is true that Spiritualism has been "exposed" almost daily for the last twenty-five years, yet it will not down. Would it not be wiser to meet the case fairly and learn what right it has to consideration? It does not matter what this or that professor has to say upon the subject, unless said after fair examination; the prefix adds nothing to the individual's power of discernment; besides, such persons are usually specialists, and have some hobby upon the brain. Professor Univalve spends twenty years in ascertaining the exact number of wrinkles that a mussel of respectable habits should have in his shell at maturity. Prof. Thimble does not believe in spirits, and, like a cow, has no interest in a Hereafter. Our educational professors are so deeply engaged in searching for the roots of words, that the useless abominations in spelling of those words, against which nature through every child learning to read, is constantly protesting, are unnoticed by them, and the stone at one end of the bag to balance the grist is constantly carried, and is likely to be, unless the "heathen Japs" relieve us of the useless weight. It is useless to expect such minds to investigate anything aside from their own narrow world, and perhaps it is better that it is so, for the few have done the thinking for the many too long already. What a turning over of things there would be if prejudice could be annihilated and questions be decided upon merit! A sort of moral undertow compels general progression now; froth rises to the top and becomes the most conspicuous; shallow minds, without investigation, pronounce anything humbug that is new and beyond their comprehension. Could such control events La Place's statement that "What we know is little, what we don't know, immense," would ever remain true. The *cui bono* of the truckling editor, while pandering to popular prejudice, is simply a tribute paid to such minds, and is doubly shallow when written within sight of a score of steeples all claiming to point the way to the spirit land, and upon exactly the same evidence as the sneered at manifestations, the latter witnessed by ourselves, friends, and neighbors, the former by—well, whom? It is a matter of little consequence whether Prof. Thimble is interested in the matter or not, the world has been, is, and ever will be, interested; for myself, all other gain would be

as nothing compared with the knowledge that life here is but the beginning of eternal conscious progress, that separation from our loved ones is but temporary. If the manifestations are of spiritual origin as claimed they offer the only tangible evidence of a Hereafter. If not of spiritual, but of earthly, origin, may they not be the harbingers of knowledge of boundless importance to humanity? If neither of spiritual nor earthly origin in a proper sense, but the result of mere trickery, then they have a fearful bearing upon evidence. I have seen a table rise upon two legs and walk out of the dining-room into the parlor and return, with no visible person touching it. I have seen two heavy men try in vain to hold a table to the floor; this in Mechanics Hall, Lowell, Mass., and before an audience of four hundred persons; no one pretended to doubt the fact. I have taken a common accor-dion in my hand, holding it by the molding around the valve; the instrument extended at arm's length from my side; the key end of the instrument immediately rose to a level in line with my arm, but extended from me, and then commenced to play a very lively tune; the sun was shining full upon the instrument. I have taken a slate in my hand, or one end of it, the other being held by the medium; a bit of pencil was placed upon the slate, which was then held beneath the table, not up against it, but at least a foot below, and in plain sight. The pencil commenced to write immediately; several messages were produced in less time than I could have written one; one of the messages was as follows: "There is a large band of us around you; if you will sit at home we will show you things that are wonderful." I have had the Eddys at my house, also several other well-known mediums; have had to do with nearly all the best known public mediums, and many not generally known to be such. I have seen the "exposers" such as Carbonell, have spent hours with them at a time in private, and witnessed their *modus operandi*, have seen excellent imitations, as I have also of green-backs, but an expert can readily see and explain the difference. Have often had such mediums as Foster and Read try to play tricks upon me, at the same time have seen things that trickery could not accomplish. I have witnessed the most of the various kiuds of manifestations described by R. D. Owen, and others he has not described; mind reading will account for Mansfield's letter answering, and some other mysteries, but there is something deeper and beyond. It is singular that a people so boastful of intelligence should be so shy of investigations outside of Congress. The following letter to the *N. Y. Graphic* displays more true manhood than is generally to be met with in regard to the subject.

ELMIRA, N. Y., November 11, 1874.

GENTLEMEN: Your circular indicates a most reasonable request. It is indeed a burning shame that men called scientific and investigators should be so hopelessly materialistic that they will not look towards the only windows through which the twilight of a great discovery is now shining.

Thirty years ago I would have sacrificed everything to undertake, without encouragement, the work to which you now invite me and others. But, as matters now stand, I have not the time or strength to do the work; and had I both, my standing is not such among men of science that discoveries made by me, however important, could even arrest attention, much less command respect.

Profoundly distrustful of much that honest but untrained men tell us as to spiritual manifestations, it yet remains that where there is so much smoke of notoriety there must be some fire of fact. How much let him declare whom you succeed in pressing into your service as investigator and reporter. Sincerely regretting that I cannot be the man, I remain very truly yours,

THOS. K. BEECHER.

If people in general were candid thinkers, like Mr. Beecher, we might hope for a speedy solution of the matter, but, unfortunately, the majority take their opinion second-handed, while the balance divide into two parties, seemingly running in opposite directions, but in seeming only. The one believe everything, the other nothing; the leaders of the first, with heads shaped like a pineapple cheese, or perhaps more on the shed roof style, the slope being such that one is left in doubt whether the forehead extends to the crown of the head, or the top of the head reaches down to the eyes; these swear by the *Banner of Light*; their followers are expected to swallow mountains or mites; mediums by such are spoken of as "too sensitive for ordinary treatment," "heaven borned," "of the angels," etc., etc. (while in fact, as a general thing, public mediums are lazy sensualists, generally acting the part of Harold Skinpole, and never forgetting to take the "Fy-punnote").

and a score of that ilk are cancerous excre-

tions of the cause. The other party simply panders to popular prejudice, and naturally gravitates toward the *Scientific American*, a fair offset to the *Banner of Light*, the one certainly knowing as much of spirits as the other does of science. The writers of this party are generally nicely bespectacled young men with weak eyes, knees, and heads, and considerable alphabet tailed on to their address, with a strong flavor of the apothecary apprentice about them. The organ of this party has just been handed to me, and in it the announcement is gravely made that the manifestations called materializations were invented by one Gordon, of New York, about two years since (don't state whether he patented them through that agency or not). The materializations were common ten years since, and it was in answer to a request that he would witness them, that the following letter was written.

JAMES EMERSON, LOWELL, MASS. :

Dear Sir:—I hope I shall find time sooner or later to attend some of the best managed so-called "spiritual" seances, but just now I am too much occupied to do anything more than listen to the wonderful stories you are told about them.

Yours, in haste,

O. W. HOLMES.

It is often asserted that if one commences to investigate the so-called manifestations, he soon becomes infatuated, and a believer. Well, suppose the discovery of a gold mine to be announced, do experts ever delve in a "salted" mine twenty-five years? If the assertion is true it would rather seem to favor the idea that there is something to become infatuated with, but persons are often credited with being what they are not, as will be seen by this letter.

20 MORNINGTON RD., LONDON, N. W., }  
Aug. 19, 1872. }

JAMES EMERSON :

Dear Sir:—Long traveling about on business has prevented me from previously acknowledging the receipt of your most interesting letter giving an account of some phenomena you have witnessed in the presence of Dr. Slade. After the very extraordinary things you have seen, I am particularly struck with what you state your opinion to be—viz. ; that the "Spirit World" has nothing to do with them, but that the phenomena belong to our physical bodies. If you could explain what you have stated to me, and could give me the reasons which cause you to think that the exertion of force (not that of the medium physically) and the writing of messages by a piece of pencil not held in a human hand, are connected with our physical body and not with invisible, independent, intelligent beings, I should be very pleased. The latter opinion is the one most generally held by those who have studied the phenomena here. For myself, I confess I do not go as far as some, and until I can get good proofs of identity I prefer to keep to the "force" only, for there I am safe. With many thanks for your polite attention, believe me very sincerely yours,

WILLIAM CROOKS.

It would be impossible for me to explain fully, why I believe the manifestations to be of physical origin, but such ever has been, and continues to be, my opinion; there is a lack of connection as well as an earthiness, that seems to locate them with ourselves, but for all that, there is ground for the spiritual claim; the water of a river partakes of the soil through which it flows, but remains water for all that. The manifestations partake of their earthly surroundings. P. H. Vander Wyde, through *Scientific American*, says the manifestations are silly; one has but to read one of his articles to see why he finds them so. Dr. Hammond published an article in which he pronounced them to be the result of trickery; his career while Surgeon-General will perhaps account for his belief, but enough of such. The weak minded are credited with being the most interested in such matters, but in all the seances with which I have had to do, either public or private, there has never been any trouble in filling the house with the best mechanics known, mill agents, school superintendents and teachers, doctors, lawyers, ministers, members of Congress, etc., etc. The belief of the better class of spiritualists is substantially that taught by Jesus of Nazareth, and it is singular that a belief so sensible and beautiful has not produced a literature to correspond. That such is not the case is probably owing to the fact that the best minds tinged with that belief feel that more good can be done through the liberal religious movement, which may be the case, but it leaves the cause of Spiritualism in the care of those who have done it little credit, and at the close of a quarter of a century there is not a paper published in that interest that a gentleman would care to be seen reading in car or hotel. Watching the falling of an apple, the rattling tea-kettle cover, or flying a kite, were perhaps not the most dignified of employments, but the results have revolun-



tionized the world. The "Spiritual Manifestations" may, or may not be, of equal importance, but believing them to be of God, or nature, as the reader chooses, and that they may be made useful, I at least shall do what is in my power to ascertain their cause.

## POPULAR SCIENCE.

During our war of rebellion the idea became prevalent that our flunkysism relative to English opinion would be cured; and such might have been the case had it not been for a great change in the management of our leading papers. Previous to the war, writers of age, talent, and experience were employed thereon; now, through motives of economy, boys take the place of such. The former never quoted the *Scientific American* as authority, in fact, never quoted it at all. The boy writers swallow its wonderful statements unquestioned; while our local editor, with his three hundred subscribers, made up of those who advertise "pull-backs," codfish, tin-ware and skillets, pulls off his hat in reverence, as he catches sight of a "New Discovery," by Prof. Tyndall, or "The Mystery Solved," by Prof. Carpenter; though were he a reader and thinker, he would readily recognize the fact that both discovery and solution were old a hundred years ago. Look at the following fresh from the press, and which fairly represents Mr. Tyndall as a scientist.

### Fresh Discovery and Practical Suggestions.

PROF. TYNDALL ON HEAT.

Having caused a ball of lead to fall from the roof of a theater on to a stone, he drew the ball up again and let it down gently with a string and pulley. The heat generated by the collision in the first instance was the exact equivalent of the heat produced in his finger and thumb, and in the string in the second instance. The outlay of muscular force expended in drawing up the ball was made obvious by causing the ball to be drawn up again by a small engine worked by compressed air. The exact equivalent of the heat evolved by a quantity of coal, completely consumed by consumption with oxygen, sufficient to lift a weight of 50 tons to a height of 100 feet above the earth, would be produced by the collision of that mass with the earth when allowed to fall. Given the velocity of a body, the heat generated by the destruction of that velocity could be easily calculated, and some time ago he was led to the conclusion that the stoppage of a rifle bullet would produce sufficient heat to fuse the metal. This conclusion was proved in the Franco-German war, when bullets which had been stopped by contact with a bone showed, on being extracted, undoubted marks, in many cases, of fusion. The same thing had also been illustrated incidentally in the experiments with gun-cotton at Stowmarket.

This "Fresh Discovery" was a part of the stock in trade of a gassy lecturer, named Boynton, who traveled the country some thirty years since. He elaborated it, however, by adding that the "average laborer consumes fourteen ounces of carbon per day, and fourteen ounces of carbon, consumed by a man or a steam engine, will lift the same weight of brick to a given height." The statement was repeated by myself to an old physician, then of Worcester, Mass. "Humph!" was his rejoinder, "heard that in lectures at college when I was a boy." Mr. Tyndall seems to be a sort of Rip Van Winkle, and to have waked from a nap of a few centuries. A few years since he announced that he had discovered that heat moves in waves. That fact was a theme for angry discussion among stove builders a half century since; a portion favoring the use of sheet iron because its "flexibility caused it to throw off heat in more rapid waves than could be possible with its more rigid competitor, cast iron." That heat moves in waves is a fact that has been perceptible since hot surfaces existed. This discovery by Mr. Tyndall was soon followed by the announcement that he had also discovered that *motion* moves in waves, which could hardly seem new to any one who ever saw the ocean, felt the waves of an earthquake, or who, as a boy, ever gave the end of a long rope a flip, thus causing a wave to run its whole length. The Indian, however, who has watched the flight of an arrow or lance, may have his doubts as to the invariable applicability of the rule. Not long since, the editor of the *Scientific American* urged the substitution of death by electricity for that of hanging; innocently stating that Prof. Tyndall, while experimenting, was knocked senseless by a shock, and on recovery announced the fact that it didn't hurt, thus adding another to his character-

istic discoveries. Mr. Tyndall is probably more generally known through his "Prayer Gauge" proposition, than in any other way; but in this he retained his consistency. It would be difficult to find a boy of ten who has not heard very positive doubts expressed as to the efficacy of prayer; and such doubts have been expressed by writers for more than two thousand years. "Can the Ethiopian change his skin or the leopard his spots," is plain enough. Franklin was equally plain when he suggested that it would save time and answer the same purpose to ask a blessing over the food in the lump, when it was housed in the fall, as to do it at each meal daily. Paine in his "Age of Reason," Allen in his "Oracles of Reason," and many other writers have done the same. Yet it is hardly likely that any observant person has doubted the benefit of prayer to the petitioner, but merely that the Creator is unlikely to change his laws at the solicitation of individuals. A wish is a prayer. To "cry" is to pray. The new born child utters its first prayer with its first breath, and probably with about the same consciousness of its real needs as have those who make the most show of praying. Plato, or one of his friends, once remarked: "It would be well to hesitate before praying, as the gods might answer the prayer." We may readily conceive that things would become somewhat tangled, if the prayers, even of a single Sunday, were all granted. Prayer, or striving with a matter, brings reconciliation with the existing conditions. Moulton showed himself to be a close observer, when he concluded to let "Theodore write himself out," before trying to stop his proceedings. Every woman feels better after she has had her "good cry." We all pray; quite likely Brother Seventhly would not consider our prayers orthodox, but that is not important. What is needed is to be more real, more self-dependent. Superficial characters like Tyndall are soon forgotten. Look back twenty-five years, and learn how quickly noted individuals, who have no real claim upon humanity, pass from memory. Twenty-five years ago there was a very popular man, named Edward Everett, who went toddling round the country, very much in the style of Tyndall; that is, with many words and but few ideas. Scarce ten years have passed since his death, yet he is nearly forgotten, and is sure to be entirely so when the generation in which he lived has passed away. Twenty-five years ago the names of John Brown and Abraham Lincoln were far less familiar than they are likely to be centuries hence. Twenty-five years ago the *Tribune* was edited by a MAN, and though issued from an unnoticeable, dingy, old building, every one was asking: "What does the *Tribune*, or what does Greeley say?" Now, edited by a sort of Tyndall, and advertised by its towering steeple, that rises from a base as narrow and as fiery as a Calvinist's creed, there are none so weak as to ask or care what is said by it or its editor. There is hardly a person in the country, of ordinary intelligence, who would be at a loss for a reply, if asked to give a reason why the memory of Franklin is still fresh and respected; yet not one in ten thousand of the persons who would be influenced thereby could give any reason why the opinions of Profs. Tyndall or Carpenter should have any weight in this country. It is said these two persons court the society of Mrs. Lewes, which is likely to be the case, for these gentlemen are very anxious to shine, even if they have to do so by the borrowed light from a woman. And it has recently been in order for flunkydome, to glorify the authoress of "Daniel Deronda"; but if any mortal can tell why, I, for one, would be glad to learn. I have worked my way through the book twice, but the opinion still continues with me, that it is a mess of garrulous twaddle, and deserves to sink as it has into oblivion. Gwendolen, like other prostitutes, sells herself for a consideration, then is too shallow either to accept the situation or to fight it out. Daniel Deronda, though young, has the wisdom of a Solomon, and is as passionless as was old David in his dotage. Faugh! What a world this would be if filled with Daniel Derondas! There is one point, however, in which the work should be useful to us, namely: If the most intelligent classes of England are so far back in barbarism in relation to the standing of woman, as indicated by that work and Reade's "Woman Hater," then this country certainly has no call to go there for information upon any subject whatever, or to be tickled by the second hand clap-trap that is published in the *Science Monthly* over the signatures of such scientists as Tyndall and Carpenter.

## Midnight Musings.

BY WASHINGTON IRVING.

I am now alone in my chamber. The family have long since retired. I have heard their steps die away, and the doors clap to after them. The murmur of voices and the peal of remote laughter no longer reach the ear. The clock from the church, in which so many of the former inhabitants of this house lie buried, has chimed the awful hour of midnight.

I have sat by the window, and mused upon the dusky landscape, watching the lights disappearing one by one from the distant village; and the moon, rising in her silent majesty, and leading up all the silver pomp of heaven. As I have gazed upon these quiet groves and shadowing lawns, silvered over and imperfectly lighted by streaks of dewy moonshine, my mind has been crowded by "thick coming fancies" concerning those spiritual beings which

"Walk the earth  
Unseen both when we wake and when we sleep."

Are there, indeed, such beings? Is this space between us and the Deity filled up by innumerable orders of spiritual beings, forming the same gradations between the human soul and divine perfection that we see prevailing from humanity down to the meanest insect? It is a sublime and beautiful doctrine inculcated by the early fathers, that there are guardian angels appointed to watch over cities and nations, to take care of good men, and to guard and guide the steps of helpless infancy. Even the doctrine of departed spirits returning to visit the scenes and beings which were dear to them during the bodies' existence, though it has been debased by the absurd superstitions of the vulgar, in itself is awfully solemn and sublime.

However lightly it may be ridiculed, yet the attention involuntarily yielded to it whenever it is made the subject of serious discussion, and its prevalence in all ages and countries, even among newly discovered nations that have had no previous interchange of thought with other parts of the world, prove it to be one of those mysterious and instinctive beliefs, to which, if left to ourselves, we should naturally incline.

In spite of all the pride of reason and philosophy, a vague doubt will still lurk in the mind, and perhaps will never be eradicated, as it is a matter that does not admit of positive demonstration. Who yet has been able to comprehend and describe the nature of the soul; its mysterious connection with the body; or in what part of the frame it is situated? We know merely that it does exist; but whence it came, and when it entered into us, and how it is retained, and where it is seated, and how it operates, are all matters of mere speculation, and contradictory theories. If, then, we are thus ignorant of this spiritual essence, even while it forms a part of ourselves, and is continually present to our consciousness, how can we pretend to ascertain or deny its powers and operations, when released from its fleshly prison-house?

Everything connected with our spiritual nature is full of doubt and difficulty. "We are fearfully and wonderfully made;" we are surrounded by mysteries, and we are mysteries even to ourselves. It is more the manner in which this superstition has been degraded, than its intrinsic absurdity, that has brought it into contempt. Raise it above the frivolous purposes to which it has been applied, strip it of the gloom and horror with which it has been enveloped, and there is none, in the whole circle of visionary creeds, that could more delightfully elevate the imagination, or more tenderly affect the heart. It would become a sovereign comfort at the bed of death, soothing the bitter tear wrung from us by the agony of mortal separation.

What could be more consoling than the idea that the souls of those we once loved were permitted to return and watch over our welfare?—that affectionate and guardian spirits sat by our pillows when we slept, keeping a vigil over our most helpless hours?—that beauty and innocence, which had languished into the tomb, yet smiled unseen around us, revealing themselves in those blest dreams wherein we live over again the hours of past endearments? A belief of this kind would, I should think, be a new incentive to virtue, rendering us circumspect, even in our most secret moments, from the idea that those we once loved and honored were invisible witnesses of all our actions.

It would take away, too, from that loneliness and destitution which we are apt to feel more and more as we get on in our pilgrimage through the wilderness of this world and find that those who set forward with us lovingly and cheerily on the journey have one by one dropped away from our side. Place the superstition in this light, and I confess I should like to be a believer in it. I see nothing in it that is incompatible with the tender and merciful nature of our religion, or revolting to the wishes and affections of the heart.

There are departed beings that I have loved as I never again shall love in this world; that have loved me as I never again shall be loved. If such beings do even retain in their blessed spheres the attachments which they felt on earth; if they take an interest in the poor concerns of transient mortality, and are permitted to hold communion with those whom they have loved on earth, I feel as if now, at this deep hour of night, in this silence and solitude, I could receive their visitation with the most solemn but unalloyed delight.

In truth, such visitations would be too happy for this world; they would take away from the bounds and barriers that hem us in and keep us from each other. Our existence is doomed to be made up of transient embraces and long separations. The most intimate friendship—for what brief and scattered portions of time does it exist! We take each other by the hand; and we exchange a few words and looks of kindness; and we rejoice together for a few short moments; and then days, months, years intervene, and we have no intercourse with each other. Or, if we dwell together for a season, the grave soon closes its gates, and cuts off all further communion; and our spirits must remain in separation and widowhood, until they meet again in that more perfect state of being, where soul shall dwell with soul, and there shall be no such thing as death, or absence, or any other interruption of our union.

The foregoing is taken from one of our school books that has continued in use for more than fifty years, which would seem to warrant its popularity. It expresses my own views so perfectly, that it is republished as an introductory to remarks upon the modern phase of the same subject. It is now generally admitted by the intelligent, that whether the belief in spirit communion is or is not well founded, at least there are strange phenomena connected therewith that demand investigation. At the same time there is a shallow, ignorant, loud-mouthed class that derides every attempt to solve the mystery. The press panders to this class in order to become popular therewith, or through natural stupidity. The first is well represented in the *Springfield Republican*, which is racy, full of gossip, but every article seems written in a style to render it applicable at any time to the side then the most popular. The influence gained by such a course seems to be made plain in the fact, that at the determination of any public matter that paper, almost invariably, stands on the losing side. Its neighbor, the *Union*, seems to fill the other position. Servile as a partisan, dumb with astonishment at the announcement of any "wonderful discovery" at a distance; but implacably hostile to anything near by that is out of the beaten track, though it may be readily verified by personal observation. Perhaps a "little story" will best illustrate. In my young days, a neighbor of my father had a ram of such combative propensities that he was kept in a small enclosure surrounded by a granite wall. It was soon understood that, before making a charge, he took aim, then closed his eyes and went it blind; so that it was fun to drop inside, make a few "Masonic passes," then look out for the rush that was sure to follow, when prudence dictated a flank movement and the ram would bring up against the wall, the contact having as little tendency to demolish the granite as to enlighten the ram. But the strong points of the editors of such papers are yearly described in the stock reports of our cattle shows, and it is useless to waste space upon them here. From my earliest childhood I have had an intense desire to learn the *why* of any seeming mystery, and I believe that it is not only the right, but it is the positive duty of every human being to take every possible opportunity to do so. I have never had any desire to invent "perpetual motion," or seek buried treasures; but my wanderings and investigating habits have made me slow to limit the possibilities. "Table tipplings" seem contrary to the laws of gravitation, but when certified to by so many they deserve consideration, because they have a bearing upon evidence in general. Millions

of lives have been sworn away upon the title of evidence that can be produced in proof of the verity of spirit communion. "It is electricity!" shouts Mr. Shallow. Very likely, but what then? What is electricity? Suppose some traveler, out of breath, should rush into the study of Prof Snoodinks, who has calmly settled down upon this electricity hypothesis, shouting: "Sir, sir! I have been traveling in the East for five years to find out about the marks that were placed upon the ancient structures, and have discovered all about them." "Glorious," answered Snoodinks, "let us hear, quick!" "Why, they are letters or words," says our discoverer. Imagine Snoodinks' look of disgust, as he exclaims: "Why, you infernal donkey, have you been traveling five years to find out what everybody else knew? It is not what they are, but what they mean, that is wanted." So of the phenomena connected with spiritualism. I have seen tables walk up and down stairs, around the house, give communications, etc., etc. "O, you were mesmerized." Possibly, but if mesmerized in this, why not in other matters? What value is there in evidence? This matter has a very important bearing in the every-day affairs of this life, and the judge or juror who fails to improve every opportunity to gain information upon the phase of our system that may have such an important influence, in my opinion, is criminally negligent; and a doctor who neglects to inform himself upon the matter may well turn back to Hippocrates for information, and it will depend more upon luck than his skill if seventeen out of forty-two of his patients recover, as was the case with Hippocrates. My study of the subject has had more to do with its physical than spiritual bearing, still I have studied the latter sufficiently to know that it offers the best evidence extant, that this life is but a prelude to another. It seems strange to me that Brother Nehemiah cannot see that in denouncing spiritualism he is only injuring his own cause, and is only hastening the time when his hearers will become confirmed materialists. Only his conceited blindness prevents him from seeing that the lady who is so attentive, while he is sniveling and declaiming in his weak way, is only looking at some other lady's "pull-back," with the intention of copying or criticising it; she neither knows nor cares anything about what he is saying. She goes to meeting from habit, and to show her own or to see how others are dressed.

Let her lose her loved ones, then his twaddle becomes husks, and she seeks more tangible evidence of an hereafter where she shall meet them again. Were he of even average intellect he would respect the sorrows of such; his devil theory denotes his caliber, and is just suitable for grannies in breeches. After twenty years and more of investigation, I cannot accept the spiritual theory as a solution of the mystery, though it may prove much that is claimed by the spiritualists, and I think it does, but it is a broader matter, it covers our life here. If it is electricity, it is time to try and find out what electricity is. It has happened that for more than a year past I have had this power in my own family, and have had a chance to study it at leisure, not in the dark particularly but in any of the twenty-four hours of the day. To me it seems to be our life that flows through our body operating it as a river operates a mill. The mill or the body may decay but this power or the river flows on forever. We have abundance of communications which are quite as likely to purport to come from those who prove to be living as from those who have "gone before." We are not mediums, nor do we exhibit this power for money or to the merely curious, but whenever at leisure we are always happy to have intelligent seekers call for the purpose of witnessing its effect and operation.

## TABLE TIPPINGS.

In the last issue of the Reporter the fact was mentioned that for months past we have had what are termed *Table Tippings* in my family. The statement attracted more attention than was expected, and many who laughed at the matter a few years since have expressed a desire to know more of my experience. Great indignation is often expressed by the believers in Spiritualism, because scientists do not investigate the manifestations, but that is not so easy to do as may at first appear; peculiar conditions are required; then there are few public mediums willing to be thoroughly investigated; beyond this, real scientists, like Franklin, are scarce. He, silly man, believed investigation should precede decision; but the popular scientists of to-day are



so wise that anything new is at once condemned. If facts prove them to be in error, they *damn the facts*; a plan that saves trouble, but one unlikely to lead to discoveries of importance. Much has been said about Agassiz's refusal to investigate the subject, but Mr. Agassiz was simply a specialist, puffed up with conceit through our adulation. That he was a weak-minded man is evident from the following extract taken from his own statement :—

EXPERIENCE OF PROF. AGASSIZ, GIVEN BY  
HIMSELF TO REV. C. H. TOWNSHEND.

" Desirous of knowing what to think of animal magnetism, I for a long time sought an opportunity of making some experiments in regard to it upon myself, so as to avoid the doubts which might arise on the nature of the sensations which we have heard described by magnetized persons. M. Desor, yesterday, in a visit which he made to Berne, invited Mr. Townshend, who had previously magnetized him, to accompany him to Neuchatel and try to magnetize me. These gentlemen arrived here with the evening courier, and informed me of their arrival. At eight o'clock I went to them. We continued at supper till half-past nine o'clock, and about ten Mr. Townshend commenced operating on me. While we sat opposite to one another, he in the first place only took hold of my hands and looked at me fixedly. I was firmly resolved to arrive at a knowledge of the truth, whatever it might be; and therefore the moment I saw him endeavoring to exert an action upon me I silently addressed the Author of all things, beseeching him to give me the power to resist the influence.

"AGASSIZ."

" Think of a grown-up man praying that he may be able to resist the proof of a fact; it puts one in mind of the tramp seeking work, and praying to God that he may not find it. We hear too much of men who have gained popularity through the puffing of those who wish to make themselves known thereby. We know that the scientific men of England proved the impossibility of tunnels like that of the Thames, of railroads, telegraphs; in fact the impracticability of anything new. England owes her greatness to her mechanics, and would hardly miss them if her whole clique of popular scientists should emigrate. What do we know of the abilities of such men as Huxley, Tyndall, and Carpenter, or care what they say? We see millions of foreigners, and as a mass know them to be much lower, intellectually, than our own people; is it likely that countries that produce so much ignorance, produce the greatest thinkers? See what an Englishman says :—

" Not only in oratory is the American the superior of the Englishman. You excel us in oysters, in corn bread, in sweet potatoes, in canvas-back ducks, and, I venture to say, in kindness and hospitality. In intellect, I take it, we are about level; but doubt whether you give yours full play. If you did, you would depend upon yourselves."—*B. L. Fargson's New York Speech.*

And why do we not depend upon ourselves? We are taxed heavily for schools in which to give all an education. Are those schools a failure? If so, is it not time that the howl of the insatiate teacher for more pay should cease? Many of our papers assume the rôle of teacher, but their writers are usually mere machines that run in well worn ruts; one of these in the *Springfield Republican* writes substantially as follows: "Herbert Speneer, probably the greatest thinker of the age, expresses the opinion that the marriage relation of to-day is not likely to be considered desirable in the not distant future." This stale idea that was common with Lyeurgus, still later with Plato, and has been entertained by hundreds of communistic societies, the theme of innumerable lectures and the practice of the Oneida community for forty years, is given as proof of originality. The *Republican* gushes with adulation. The "Great Dr. Hammond" is one of its superior idols. Will it inform its readers whether the said Doctor as Surgeon General was ignominiously expelled from the army; if so, is his assertion that Spiritualism is a humbug, and its so-called manifestations the result of trickery, of any account when placed against that of so many quite as intelligent as himself who believe to the contrary? It is easy for a noisy person to find followers, and a single rowdy will make more noise than is made by a thousand intelligent persons; consequently, it is no proof that Spiritualism is unpopular, because a few ignorant persons shout humbug. The one witness in court that swears positively to have seen a crime committed would have more weight than a thousand who should swear that they did not see it, yet it is the ignorant and prejudiced who have not seen, that are the most strenuous in shouting humbug in relation to the spiritual manifestations. Fifteen years ago the professional exposer drew full houses; now he soon has to

pawn his traps in order to get away from his last place of exhibition. One fact that is open to all should attract the attention of the intelligent; we know that such men as Sumner, Beecher, Agassiz and others have spent months in preparing a lecture that is given a hundred times, yet Cora L. V. Hatch, *that was*, who is certainly not remarkably talented, will take the same subject given to her as she rises to speak, and give as polished and profound lecture as those who have taken months to prepare it. It would not be desirable to have any one believe simply because others do so, but when men like Abraham Lincoln, William H. Seward, and others of the same abilities accept Spiritualism as a fact, it certainly cannot be derogatory to those who think less to consider the subject fairly. My attention was called to what were termed "table tipplings" soon after the Fox sisters made their debut, but it was not my lot to meet with anything of the kind for a number of years that caused me to look upon the subject with favor. "Table tipping" violated the law of gravitation, and my faith in that law was positive. In 1865, Horatio, William, and Mary Eddy were at my house in Lowell, Mass., five days, each evening giving public sances to large audiences in Mechanics' Hall. At those exhibitions the laws of gravitation and cohesion seemed of little account. The mediums were ironed by the police, but it made no difference; hundreds of feet of cordage were used in tying each medium separately, then together, to staples in their cabinet. They were literally wound over as a woman winds a rag in a ball of yarn, but their coats would be taken off from under all of this cordage, or put on in the same way in fifteen seconds after being shut into their cabinet. Sewing the knots made no difference, for the cords and knots were invariably the same throughout the sance as when first tied. I have had much experience in handling cordage at sea, and in other business, and have tied many mediums, but so far have never succeeded in tying one so but what the cords would come off at request. I have had to do with nearly all of the mediums of note known in the Eastern States, and as a general thing have not had cause through the acquaintance to respect them, and have often wondered why such remarkable gifts are given to such low characters; but the beautiful pom-pom springs from the slimy depths of the frog-pond. I have spent hours in private with professional expositors, have seen excellent imitations, but the observer who has seen the real and imitation and cannot see the difference must be dull indeed. There would be no lack of expositors if the real mediums could explain the *modus operandi*, for there are few of the noted ones, in my opinion, who would not for a consideration readily act as such. I have witnessed nearly all of the various manifestations that have been described, and shall briefly mention a few. Sitting with Slade in New York, the slate was not held up against the table but a foot below. *I saw the writing as it was done, each letter and line*, but no hand or other means of operating the pencil could be seen, though at request a hand was twice shown above the table, seemingly an Indian hand; it was noon and the sun shining on the table at the time. While the writing was being done there was such a strain downwards that it surprised me that the frame was not stripped from the slate. Watkins, the slate writer, probably as little of a man and as much of a medium as has yet been developed, was at my home a week; he placed a bit of pencil upon a slate and then turned another slate of the same size upon the first; each of us held an end of the slates together; in a moment the pencil was heard to move as though writing; soon, three light taps were heard, then the slates were pushed toward me, Watkins not even looking at them; on opening them the following message, plainly written, was found: "*My dear friend, I come to you to let you know that I live. Ansel Cain.*" Mr. Cain was not an intimate friend of mine, though we had conversed upon the subject of Spiritualism, and he had given me the impression that he doubted a future existence, though he evidently desired such. The communication was copied at the time, as were the following which were given immediately afterwards: "*My dear brother, I am glad to see you here this morning, and hope you will believe that this is me. Moses W. E.*" "*My dear papa, I will come to you again some day. I am happy, so is mother. God bless you all. Your loving daughter, Hattie.*" Of the source of the communications others may judge. That they came as stated, I know. Numerous communications of a similar nature were received by myself and others through Mr. Watkins while he was at my house. He got them anywhere that he made the attempt, out on the door steps, in the bushes. I saw him get one in a smok-

ing-car on the Boston and Albany Railroad. The communications were not always of a spiritual nature, but such as they were, any one that would pay could have them, and considering the way they were given hardly any one mentally higher than an idiot could have been tricked thereby. Mrs. Huntoon (Mary Eddy) was invited to my house for the gratification of my own family and special friends. Numerous hands and faces were shown, instruments were played upon, then passed out to the audience. One woman, or form of a woman, came out into the room, showed her night-cap and dress of ancient days, then voices, shouts, and a pistol shot. "Oh, so low!" exclaims the high toned. Certainly, they have always been so; think of the frogs, vermin, turning rods into snakes, water into wine, etc. Yes, but why not do them in the light? Sure enough, why was the earth created in darkness; why did God require a bush as a cabinet when he appeared to Moses, or a cloudy pillar at the door of the Tabernacle? Why did the angels come to Lot in the evening, or release the Apostles in darkness? The Christian fabric rests upon dreams and darkness; the veil was rent and saints rose from their graves in the dark; the Ascension was in a cloud; a kernel of grain, or the roots of a tree, require darkness from which to produce manifestations of growth and life; the body commences and obtains its form in darkness, receives the spirit or life in darkness. Is it strange then that certain phases of the manifestations require darkness? Only the shallow minded will be surprised at the fact. After our séance I happened into the kitchen where I found Mrs. Huntoon looking around that part of the room where the cabinet had stood and saying to herself, "I do wish I could find where the bullet goes to," which caused me to ask if a ball cartridge was discharged from the pistol the previous evening. "Yes, we always use regular cartridges," was her reply, which seemed decidedly interesting. Her pistol was called for and cleaned. Then from her supply of cartridges I loaded its seven chambers, placed it in a small empty closet, put a guitar, bell, and tambourine with it, then hung a curtain at the door, after which Mrs. Huntoon's hands were tied behind her and as secure as I could tie them. My assistant "Charla" sewed the knots firmly with thread. Four chairs were placed in front of the curtain for the family, then Mrs. Huntoon took a seat in the closet, and in less than ten seconds, hands and a face were shown through the curtain, all of the instruments were played upon, then bang, bang, went the pistol, and a third time at my request. Immediately after the third discharge, the medium stepped out to the light, tied exactly as when she entered; not a sign of a bullet mark could be found. I took the pistol and discharged another cartridge at the floor of the closet; the bullet from that is plain enough to be seen. The medium was then asked to step into the closet and have the spirit write her, which was done while I was taking my watch from my pocket in order to time the untying. It certainly was not one second in being done. As no mention is made of the fact that the discharged bullets cannot be found, it can hardly be considered a trick. Never bother, however, to tie a medium; trust to the production; if the medium is tied, note the time required for any manifestation, and whether there has been an effort in the production; the real medium keeps cool, the exposé is often covered with perspiration through his struggles. Suppose a letter is written to a spirit friend to be answered by Mansfield, write as follows: "My dear friend, give me some test by which I may know that I am in communication with you." Do this mechanically, keeping your mind upon other matters, and be sure to have no thought of what the test is to be; if this is done, sealing the letter is of no account, and the writer will be more fortunate than myself if anything satisfactory is received. In a dark circle where hands are felt, observe closely whether the movements are like those of a person groping in the dark, or every attempt is accomplished without blundering. I have tried hard to study the manifestations carefully and candidly, but to do it advantageously requires the regular attendance at stated hours of several persons, and it is not easy to find such. It is generally supposed that an intermingling of the sexes is necessary, but that is not certain. I have often entertained theories about the matter that have as often been dispelled; whatever the power, if an appointment is made it is kept without fail, even if forgotten by the earthly party interested; one moment we have what seems absolute proof of spirit communion, the next something is given that makes the matter doubtful. We have abundance of communications, often two try to communicate at the same time, mixing the

letters as would be done by two telegraph wires getting twisted together. We are now using our sixth table, five having been destroyed. Table tipping but poorly expresses the movements with us, and no person with a particle of the true scientist about him could fail to be interested in the ever-changing movements. My wife, her sister, and myself constitute the sitters; we simply place our hands upon the table without any attempt to control its movements. It travels through the house, up stairs or down, swings upon my head and shoulders and rushes me backwards, and in darkness through rooms and doors without touching a casing, though the table is nearly as wide as the doors, or perhaps it will bear down until it crushes me to the floor. I think it can press down three hundred pounds. Sometimes while I am sitting in a chair it will swing on to my back, hook its legs to my chair and turn me around or drag me along, or perhaps tip me over, then drag me on the carpet. A recent freak was to tip itself over, then pick up the chairs on its legs, call for the alphabet, spell out "confusion," then disengage itself from the chairs, set them upright in place. Any movement is made just as well in the blackest darkness as in the light. It will move quickly to the window and tap the glass rapidly without injury, though it is so dark that nothing can be seen. Its communications are as varied as is our conversation. My boy was asleep; the question was asked, "Do you know where Jimmie is?" "Yes, his body is up stairs, his mind is wandering through immensity." To the question, "Why do we get so many unreliable communications?" was answered by those purporting to be special friends, "When we withdraw our control it leaves you open to the influence of elements of which you know not." I spanked my boy one evening because he was raising the d—l generally. On returning to the table where another person and myself had been sitting it gave me a hearty thump, knocking me against the wall and handled me very roughly, which caused me to laugh, as its force could be calculated. My laughter seemed objectionable for it immediately whirled itself into the hall and dashed its corners into the walls—the marks still remain. Being pitched back into the kitchen it tipped on end, called for the alphabet and spelled out as follows: "*Learn patience and discretion with your child or you will be the sufferer.*"

One evening a gentleman was anxious to get the full name of one whose initials had been given; he had urged for some time, when the alphabet was called for, and what purported to be the spirit of another person spelled out, "*She is gone away.*" "Who is she?" was our inquiry. "*The one whose name is desired,*" was the reply. "Well, can't you give it?" was then asked. "No." "Why, don't the spirits all know each other?" we asked. The alphabet was called for, seemingly impatiently, and it spelled out, "*Do you know all that come to the telegraph office?*" The table calls for the alphabet by two peculiar upward movements, but how those and other peculiarities were understood by us is not positively known, but I think through impressions. We have hundreds of communications, each characteristic of its purported source, all of which can be reconciled with the spiritualistic claim; if the spirit life is but a continuation of this, the only change being separation from the body, which has been used as a cabinet or cage in this life, and in the same way, the strange and unreliable communications are readily accounted for. If a business man should put up a speaking tube from his place of business to a distant city, leaving the distant end open to the public, the gamins would be likely to send him queer messages occasionally. Much has been said in derision about Frank J. Baxter and the "Abe Bunter" matter, but that is not an uncommon phase though it adds to the mystery. I will give a case in my own experience almost identical, and for which there is abundance of evidence to substantiate the fact if necessary. I shall give the particulars literally, that the case may be clearly understood. I was experimenting, asking questions, which were answered by a planchette, purporting to be controlled by my mother; many questions had been answered, but in such a set way that they were unsatisfactory; finally I asked, "Mother, do you know where Mr. Buck is now?" "Yes, he is here." "Oh! no, no, mother, that won't do, Mr. Buck is not dead." "Yes, he is, he died four months ago." I did not believe it, but wrote the next morning to my daughter at Lebanon, N. H., requesting her to ascertain Mr. Buck's whereabouts, giving no intimation of my reason for desiring her to do so. In a day or two her reply came and was as follows: "*Cousin Isa was at Newport about a month ago, and while there news came that Mr. Buck was dead, and had been*



*dead three months*," certainly seeming good proof of spirit communion. Yet, Mr. Buck was living at the time, and is yet, I believe. If placed upon a jury to decide the question of spirit communion my verdict would be "*Not proven*"; still proof of the fact that seems almost positive may be obtained in abundance, but that *almost* invariably stands in the way. That the subject is of more importance than that of any discovery which has been made for thousand years is my firm belief; in my opinion, it is *our life*, and offers the key to life and health; the force that tips the table moves our limbs and bodies, operating our movements as a river operates a mill, continuing with us from the birth of the spirit through eternity; our brains are simply instruments through which we receive ideas as tunes are rendered by a piano, the average mind receiving ideas as water flows into a hole to the general level, the thinker *pumps* his higher and becomes the advanced leader. The infidel Paine, of 1776, was but the Unitarian of 1876. The "Autocrat of the Breakfast Table" radical twenty years since is accepted by the multitude to-day. The manifestations, however, seem more the reflections of the past, than representations of spirit life of the future. We can readily decide whether we see the reflection of an object in a perfect mirror, or the object itself through plate glass, though exactly the same view may be presented in either case; yet it might not be easy to explain the difference. It is a practice of writers to lay out a general plan of a work, then to smooth up and fill in the details as it is written out. The completed "Edwin Drood" of Dickens by the spiritual medium, I believe to be the rough sketch of Dickens in this life. That spirits of murdered persons do not return and expose their murderers is strong presumptive proof that such return is impossible; for, notwithstanding all that can be said about the spirits not believing in hanging, etc., it is universally conceded that prevention is better than cure, and if the fact were once established that exposure was probable through the spirit's return it would act as the strongest preventative. The following extract from a lecture on the "Law of Influence" seems deserving of consideration:—

"May not that energy known as electricity be the universal medium for the application of the creative and reproductive force or influence to matter? It not only conveys the signs of thought through the telegraph and telephone; it also transmits our thought-force with our thought-touch through nerve and muscle to our hands and feet. On the same principle the thought-force with the touch of the Creator through this electric hand may extend constantly to each world and to every atom of material organism."

That there is a force that produces strange manifestations is a fact too well established to allow of its being ignored, and the proper course would seem to be to grapple with it and solve its nature: to its spiritual bearing I have given but little attention, though the following lines express my own feelings upon that point:—

Oh shades of loved ones gone before!  
Do you still exist on some unknown shore?  
In a brighter land and advanced state,  
Where souls from earth with angels mate,  
Where free from pain and earthly strife,  
The soul aspires for a higher life,  
Where a purer love to each is given,  
Surrounding all with the joys of heaven?

And are the joys of that unknown shore  
So complete that earth attracts no more?  
Hath earthly ties nor kindred's tears  
No responsive throb in those brighter spheres?  
Or do you in the spirit form  
Remain with earthly friends to roam,  
To fill our hearts with gentle love  
And lead us on to that home above?

We loved you here, we love you still;  
You have gone before, 'twas our Father's will.  
Though we still remain in our earthly homes,  
Our hearts oft turn to our loved ones gone.  
Yes, gone before at the Father's will,  
But in memory cherished at the old homes still;  
At the table, the fireside, in each sunny spot, yet  
Your influence is felt, ah! we shall never forget!



No, never forget this side the "dark river."  
 May He influence our lives, the all bounteous Giver;  
 Guide us o'er its silent waters to that unknown shore;  
 That we may meet with loved ones to part never more,  
 And through the seeming love of those gone before  
 We've the most tangible proof of that unknown shore;  
 That we shall meet again with our dearest friends  
 In an advanced life, when the present ends.

## SCIENCE AND RELIGION.

The time seems approaching with giant strides when any religion irreconcilable with reason will have no place except with the ignorant or venal. The morals of to-day, compared with those inculcated two thousand years ago, show little in favor of what during the last fifteen centuries has passed for religion; we know that during the time when that religion held unlimited sway, the period is known as that of the "Dark Ages." Our great improvements and inventions are the work of an age of *infidelity*, and, if experience is of any value, it is evident that our elevation and salvation depend upon our own exertions guided by reason, and that religious dogmas only benefit those who teach them. A venal priesthood has hedged religion with superstition until it has seemed impossible to elucidate the matter by natural means; besides, it has been said that the bigotry of science is only second to that of religion; but science means knowledge, and knowledge has nothing to do with bigotry, either in religion or science. We do not dispute about the sum of two and two, or as to whether the sunlight is greater than that of a tallow candle; ignorance causes the dissensions, and the greater the ignorance the more tenacious the opinion. Superstition away, science will readily prove all seeming miracles to be either delusive or the effect of natural causes. The purpose of this article, however, is not to meddle directly with religion, but to cause a scientific consideration of the claim of "special inspiration" of the *Bible*, and the subject of "election" or "predestination." An opinion upon inspiration to be of any value must be based upon evidence, and such evidence can only be obtained from observation. First, science readily demonstrates the fact that, physically considered, man is but a complicated machine, each organ being fitted for certain duties, and as a whole, by the consumption of a given quantity of carbon, he or a steam engine will raise the same weight to a given height. Such being the case, is it unreasonable to suppose the mental organs are also mechanical, and that the brain transmits ideas, as the larynx does that of tones, or a violin tunes? There is abundance of evidence to prove that intelligence comes from a fountain outside of ourselves, open to all, but to each individual in accordance with the quality of that individual's brain or instrument of transmission. How often we read accusations of plagiarisms between authors when in fact neither had ever seen the writings of the other; how common it is for two persons to commence at the same time to speak of the same matter. Every inventor realizes how liable he is to be anticipated if he delays the completion of a device. Persons of the lowest intelligence, like "Blind Tom," will perform wonders without consciousness of how it is done. Ignorant "mediums" will deliver off hand the most profound lectures. Minsters and authors in a state of somnambulism have written articles of a superior character to what they could write in their normal condition; problems have been solved in the same way. Can we suppose that the ideas of a lifetime are stowed away in a person's head? We may divide the head of a man or a fiddle into minute pieces without finding either an idea or a tune; then is it not reasonable to believe the brain, like the fiddle, to be a mere instrument of transmission, and that some new intelligence is operating it when things are done in our sleep or unconsciousness that are impossibilities in our waking hours? When inspiration is fully understood we may rest assured that, like other discoveries, we shall find it very simple, and that we have looked too far away for the solution. Predestination! Who believes or even thinks of an idea so obsolete? asks the reader. More than generally supposed, my friends, though under various names. Those who believe a large portion of our race doomed to hell; the Adventist, who believes in the annihilation of the wicked; last, but not least, the Materialist, under which name may be found the shallow-minded of every station of

life, from the shoveler in the bog to the pseudo-scientist who believes himself to have exhausted the source of knowledge; the sleek priest, sanctimonious preacher, and pretentious professor, all preach or teach something, but at heart believe in "nothing"; the professor in science at the expense of consistency, for a fundamental principle of science is that to exist at all is to exist forever. Predestination, religiously considered, is a hazy matter, but treated rationally becomes very clear, as do election and annihilation, and seems the proper termination of a large portion of the human family, as may readily be made to appear. I have before me a tool, called by its inventor, "*the imp*"; it is but one of many of a similar character, that is, a combination of old devices, thus forming something new. "Twelve useful tools in one," says the inventor, a screw-driver, rule, hammer, carpet-stretcher, file, saw, etc., etc., made in two pieces, which by a peculiar joint are readily united, then becoming wrench and pincers, thus creating "*the Imp*"; disunited, "*the Imp*" is annihilated, dissolved into the commonest of tools; so of the average human mind. Pat, the shoveler, dissolved, leaves a residuum of ideas relative to pipes, tobacco, dogs, pigs, jokes, abolition, wakes, etc., etc.; the pseudo-scientist, of big words in which old ideas running in still older ruts have been dressed. The effect of the disintegration of such mountebanks as Justin D. Fulton, Talmage, and others, may be witnessed where some one is skimming the scum or froth from a cauldron. Observe how an air bubble explodes here, another there; soon it has vanished, there is nothing but a little common dirt left. Take preachers like our weak but amiable Doctor Adams, those who will neither learn themselves, nor, so far as they can hinder, let others; who search their Bible through for evidence that spirit communion with man was once very common, in order to prove thereby its impossibility. At the disintegration of such reverend delusions what can there be left but a little sediment of John the Baptist, intolerance of John Calvin, superstition of grandmothers and puling of babies? Is there one particle of originality in such persons that can give hope, rationally considered, from which an individuality can be constructed for a continued existence? If not, is not annihilation the predestined end of all who fail to work out an individuality for themselves; while *election* as naturally follows for those who do?

## "SPIRITS, OR WHAT?"

Under the above heading, the Boston *Herald* of February 28th ultimo gave a very circumstantial account of what were claimed to be materialized spirit forms witnessed at Rochester, N. H.; we can hardly take up a paper without finding something of the kind described, and unless desirous of passing down to posterity as a superstitious set of materialistic idiots it is time that some attempt should be made to elucidate the cause of such appearances. Is the question, however, logical in connection with the account? Spirit is *immaterial* intelligent being. The account describes material forms that must have been those of ordinary human beings, or incarnations of persons once known in this life, neither offering any proof of life beyond the grave; but such materializations are likely to gain the attention of the multitude sooner than those of a more intellectual character; they are evidently of this life and have to do with our well being here, emanating from the same cause or force as that which causes "table tipplings, spirit raps," etc., and I believe the same as that which produces all of our physical movements; and this force seems traceable back for centuries. Recall the monks of Luther's time, mere animals with only animal desires, their religion a formula, denying the right of thought; forbidden to marry, but, unless sadly belied, the fathers of many children. Think of the stern old sectarian with his coarse animal nature and belief in woman's subjection, thinking it a sin to smile, but scriptural to gratify his passions; it was the rule for such Christians, from John Rogers to Lyman Beecher, to have many children. Turn from those running in ruts to those beginning to *think*. The astounding "spiritual manifestations" in the family of Samuel Wesley prove the mediumistic temperament of the children. Those old enough will readily recall the ecstatic shouts and convulsive ways and worship of the early Methodist. Can any one remember such with large families of children? Yet they were not credited with a disposition to mortify

the flesh. Come now to the spiritual medium (male); look the list through, see how few of them are fathers, yet many of them have a very *corn-fed* look, and they are generally noted for liberal views, and it would seem that their *life force* is expended in the production of their so-called physical manifestations. Go back centuries and it will be found that wherever these manifestations have appeared in families they have almost invariably done so through the children. See the Rev. Joseph Glanvill's account of the "disturbances in the Mompesson family, 1661 to 1663"; also, Adam Clark's account of those in the Wesley family; so of modern times. Half a dozen children seated at a table soon get *table tippings* or *raps*; the same number of octogenarians might sit until doomsday without doing so, which would seem to indicate that they are the product of a surplus of the life force. Solomon in his prime could undoubtedly have caused the heaviest extension table to dance a hornpipe, but after getting to the *vanity and vexation* stage, would have found a teapoy too heavy. Ignorance sneers at the treatment of old David, as described in the 1st Book and Chap. of Kings; but in my opinion, a profound depth of knowledge of the life force is indicated therein, that is not thought of by the medical fraternity of to-day. See how readily women, babies, and dogs take to rosy, robust men; then see the same dog with hanging head and tail describe the segment of a circle as he passes the lank, saturnine specimen of humanity. Robust men usually mate with fragile women; animal propensity would seem to demand an equally robust mate, but it is evident that nature guides; the one has a surplus, the other lacks the life force, and each attracts the other. Married couples are seldom effective as *table tippers*, though each carry their proportion of force mixed with others. Why is the invalid strengthened by taking iron into the system unless because of its being a good conductor of electricity or this life force? Singing or music has the same effect upon the *manifestations* in all their phases as upon human beings. The foregoing suggestions are offered for the consideration of observers; they relate to the physical bearings of the phenomena; but there are other phases that offer strong proof that the spirit germ from the great ocean of intelligence takes possession of the body in order to gain an individuality, the body itself like a vegetable starting from seed, drawing sustenance from the earth and returning to the same at maturity; then how important that life in the body should be natural. *Suffer little children to come unto me and forbid them not, for of such is the kingdom of heaven.* In the face of such a command, how dares a being so ignorant as a Moody, attempt to warp the mind of a child into harmony with the superstitions of his own perverted nature? The question answers itself; it is only through ignorance that he so dares. The mind of a child is a study for the profound. How natural it is, and how its simple inquiries confound the ghastly theories of a Calvin. Suppose a forest to be cultivated by cutting the tops from a portion of the trees, leaving unsightly stubs, the branches from others, leaving bare poles, all the branches from one side of others, and so on, would not such work be considered that of barbarians? From the depths of my soul I believe it to be a greater sin to teach a child any other motive for doing right than for right's sake, than it was for Fagin to teach Oliver Twist and his companions to steal. So long as a mercenary priesthood can live on the credulity of the ignorant, so long will such as Moody be encouraged to peddle out superstition, that the educated clergy would be ashamed to mention; but as a matter of policy it would seem better to live here by sawing wood, then return to God a full fledged individual soul ready to commence a higher life, than to live at ease preaching platitudes, then to "melt back into the universe" with the spirit germ so shrunken that it will naturally gravitate to the body of some lower animal in which to make a new effort for a higher life. With Moodys, there will be Ingersolls,\* for the two are *cause and effect*, ignorant fanaticism and cupidity. No well-read thinking person can well doubt that Christianity has put humanity back a thousand years

\* Bob Ingersoll, as the ready champion of star-ronte thieves and other praying rascals, wiping his modest brow and posing before an audience as a model man and instructor of the world, invariably recalls to my mind Mr. R. Riderhood, so well described by Dickens, in "Our Mutual Friend." The feature however to me seemingly the most to be regretted is the fact that superstition has caused such ignorance that an audience can be found willing to listen to ideas that were musty with age a thousand years since, and which have been reiterated a thousand times by far abler and more disinterested men than Mr. Ingersoll has ever shown himself to be.

(Jesus of Nazareth would find little sympathy in a Christian church to-day); or that the Bible has been perverted through selfishness; but the strange phenomena, known as spiritual manifestations, are likely to furnish proof that its leading ideas are correct, and that its seeming miracles were the effect of natural causes. These have interested me for many years, but it is only since their appearance in my own family that I have been able to study them with any satisfaction; as we are not *mediums* their appearance with us is supposed to be the result of an earnest desire and cultivation of the means to bring them. Either my wife, her sister, "Charla," or myself can get *table tippings* or *raps*, sitting with almost any other person, but such communications as were published in last issue of Reporter are only obtained when "Charla" is one of the sitters; those were obtained by calling the alphabet, the table moving at the proper letter; they also come through her mind by seeming inspiration. I mention her as "Charla," because as such she is known to engineers, turbine builders, and manufacturers in more than half of the states of the Union, as the young lady assistant in my testing business; quiet, and of a mathematical turn, but certainly not a poetess, yet in answer to wished-for information, communications like the following come through her mind like a flash of light:

*False, with the true, you'll one day find,  
Is but the crossing of your mind  
With our dispatches as they are sent  
From our Summer Land to your Continent.*

*If the truth you wish to find,  
You must study your own mind,  
Learn its workings, its relation  
With the great unknown creation;  
A gem we promise you shall find,  
In a knowledge of the human mind.  
Spirit friends around you gather,  
Wishing much to help their brother,  
Seeking earnestly to find  
This gem of truth in the human mind.*

*Spirits from the other shore  
Oft come tapping at your door,  
Wishing to inspire your mind  
With happier thoughts of their design.*

*Sleep is a rest for the weary mind,  
Which, as it wanders free,  
Oft catches inspiration  
And brings it back to thee.*

*Of times when the mind doth wander,  
While the body is at rest,  
Strange elements of earth  
This freed mind doth impress.*

*Many times when the mind doth wander,  
Ideas which to earth are grand,  
Are in his sleeping hours  
Stamped on the mind of man.*

*Then when he doth awake,  
And reason and thought control,  
These ideas are developed  
And given to the world.*

*Your lives are tangled in with ours;  
We are not far away,  
We join men and women in their work,  
And children in their play.*

Much has been said about the twaddle that purports to come from the spirits of noted persons, but if persons will pander, twist and be all things to all men for the sake of becoming noted, there is no good reason for supposing the spirit of such will retain a very positive individuality after separation from the body. Separate the parts of a twenty-four bladed jack knife, and the corkscrew would have the same right as any other piece to call it-

self the many bladed knife. We have had many communications the past two years, but none of a lower character than such as I have published; and I do not believe a low or silly communication was ever given in what is called a circle, unless there was a mind in that circle to match. The communications are often oracular and difficult of application, simply because they are answers to ideas conversed about hours, perhaps days, before. The following is one of the kind and was given through the table: "*None realize for how great an object they live.*" Our minds and conversation affect the manifestations but do not control them. Our ideas are opposed quite as freely by this force or intelligence as by persons in the flesh. Communications purporting to come from persons who prove to be living are very common, but that depends somewhat upon who the sitters are. I have sat with persons and obtained communications as fast as they could be spelled out, and found them to be nothing but the passing thoughts of the sitter's mind. I find, also, that any idea thoroughly established in my own mind is pretty sure to crop out in the communications. An earnest wish or desire, though it may not be gratified, is very likely to receive notice, so that my faith is becoming strong that there is efficacy in prayer; not through any change of God's laws but in accordance therewith. Franklin drew lightning from the clouds, so I believe that one or many persons praying earnestly for a given purpose might produce an effect; we little know yet the power of mind upon mind or mind upon matter. These manifestations have been offered for man's study since the dawn of history; I believe they offer a key to a knowledge of our life, health, and surroundings that can be obtained in no other way. Through them I believe it will be made clear that crime is a disease, and that there is something more than a moral influence in the contact of individuals. I find in sitting with certain persons that my strength or life force is taken from me to a very disagreeable extent, while the contrary is the case with others. There are persons who seem to leave a part of themselves with us for weeks, so that if we sit for the manifestations by ourselves, we have what purport to be their matters to attend to. One case has interested me much; it was what purported to be the spirit sister of a person from a distant state. She gave a communication as a test for her brother, which was sent and by him disowned; when she came again she was rated soundly for her deception, and requested to keep away unless she could be truthful. Nothing more was heard of her for six months when her brother came to our house for perhaps five minutes; that evening his sister put in an appearance. "How happens it that you have not been here for so long a time," was my inquiry. "*You scolded,*" was the reply. "*Ah, Annie, you told fibs, you remember.*" "*No, I didn't.*" "*Ah, yes, that test to your brother.*" "*I didn't give any.*" "*Who did then?*" was asked. "*The one that broke the window.*" Nothing had been said about a broken window at the time, but a month previous our table had been pitched into the window. Singing the "Braes of Balquith" has been as effective in bringing Annie to us as "rubbing the lamp" proved in bringing Aladdin's genie. We have had what purported to be the spirits of many persons come to us, some of them very noted ones; the latter have almost invariably been followed by imitators. Enthusiastic spiritualists exult in the thought that these manifestations are breaking up the pulpit influence, but that is solely because pulpits are occupied by materialists at heart, who preach for those who pay best, without faith in their own teachings; and consequently, who are the first to laugh at the idea that any of their dogmas may be sustained by tangible evidence; yet these so-called spiritual manifestations do furnish a plausibility for many of them. The materializations, if real, of which I have no doubt, are reincarnations, and give ground for the belief in the resurrection of the body for judgment, and the resurrection of Jesus of Nazareth. A careful study of the forces that produce the materialization will at least cause the observer to hesitate before rejecting as impossible the idea of such conception as that claimed for him; not of course through any miraculous process, but through a concentration of sexual force, as a concentration of the elements under certain conditions produce earthquakes, tornadoes, whirlwinds, etc. We have much to learn yet, and until sure that we are quite as wise as our Creator it is not worth while to ascribe to miracles or the devil, what may well take place through natural causes, though we may not understand the why. The shallow may sneer at these manifestations, but the thinker who has studied them carefully under favorable



conditions will feel more inclined to bow in humility and thankfulness before his Creator and to earnestly ask for more light. In conclusion, I would say that from my own experience during many years of unprejudiced investigation I believe the matter to be susceptible of practical solution.

## MASSACHUSETTS' ENCOURAGEMENT FOR INTELLIGENT OBSERVATION.

NEWBURYPORT, Jan. 21, 1873.

MR. EMERSON:—I am surprised to know you have heard of the affair—had no idea it had become so public. The account you sent me is true with a few exceptions. When I first saw the boy he was neatly attired in a brown suit of clothes trimmed with braid and buttons of the same color. The boy, as the slip states, disappeared into the attic, etc. When I reached forward to grasp him he seemed not like the boy, but vapory (or, as I can only describe it, like a thin cloud scudding across the moon); still he seemed to have the boy form. Reports from some of the Boston papers say I fainted; such is not the case. I knew then where I was and what I was about just as well as I know I'm writing this to you. If I could only see you I would be able to tell you so much more than I can possibly impart by the pen. One day I sent a boy out to hang up the brushes, etc. He was out about five minutes. After he'd taken his seat three raps came on the door where the brushes were hung. He said, "Miss Perkins, can I go out and see who's there?" I told him, "Yes, and leave the schoolroom door open." I sat where I could see all this. Every one of the brushes, both long and short handled, came falling from off the nails where they were hung; some struck him on the face, some on the shoulders, and the brooms directly on the top of his head. The dust pan, hanging on a nail some distance above the brushes, came tumbling down to the floor with a vengeance. It then stood on its handle, then on the bottom of the pan, and continued on so till it entered the schoolroom, and then it was placed as nicely against the partition as if I had done it myself. I looked at that performance in wonder, I can assure you. Just as soon as I'd raise the ventilator a black ball, twice the size of a cannon ball, would begin to revolve around the attic, and make such a noise I would be obliged to lower the ventilator. One day the room was as quiet as it could possibly be, and all at once some one in the attic called out, "Dadie Pike." Dadie thought I spoke, and said, "What'm?" I said to him, "Can you say your lesson?"

Since the boy affair took place the attic has been "fastened up." Locks and keys are of no use, for there is as much walking upstairs, and sometimes the hammering and nailing. Once in awhile, sounds, as if some one walks along the platform upstairs, will come down the attic way, go across the entry and open the outside door, and be gone perhaps ten minutes. After it's quiet again the door will open, and he, she, or it will go upstairs.

I suppose you saw by the paper I was offered one hundred dollars for a photo? A gentleman came down from Boston and offered me four hundred to go up and simply tell what I had seen and heard. I declined both offers.

No, I am not a Spiritualist; in fact, never had anything to do with a person of that belief.

Yours,

LUCY A. PERKINS.

NEWBURYPORT, MASS., March 31, 1873.

JAMES EMERSON, Willimansett, Mass.

Dear Sir:—Miss Perkins is in school to-day. You have no idea of her trials. Spaulding was determined that she should not go in.

She is truthful, and a good, honest girl who has had a hard struggle to rise to her present position. I heard Johnson and Spaulding say, "We doubt not that this is a reality to you, but you labor under the same impression the great and good John Wesley did, but it is an hallucination," etc., etc. The disposition to crush her is contemptible, but bigotry must have a victim, and I presume Miss Perkins will be voted out.

Very truly yours,

RICHARD PLUMER, P. M.

Miss Perkins and Mr. Plumer have passed beyond the jurisdiction of a Massachusetts school board.

## SPIRITUAL MANIFESTATIONS.

It is nearly a score of years since the foregoing articles were commenced and thirty-five since commencing to study the phenomena. This has brought me in contact with ministers, congressmen, doctors, lawyers, curiosity seekers, and mechanics—the latter by far the most intelligent observers from the nature of their make up, for they judge understandingly of the space and time necessary for effect. Indeed, I do not believe any one will ever arrive at the highest standard in any calling if destitute of the mechanic's creative and organizing faculty. The claims of the mesmerist have been familiar to me for a half century, and seem so blended with those of the spiritualist that I am unable to separate them.

Hypnotism seems a subterfuge for retreating from a position impossible to maintain, and a claim to share the honor after braver hearts have won the battle.

Theosophy, seemingly the "old clo'" of Spiritualism, offers little that is new, if A. P. Sinnett is to be considered the exponent. His "Karma," in itself to me interesting, is made up of old, old ideas and stories. Rabelais says, Alexander the Great—of course re-incarnated—is making a poor living mending old stockings. Cyrus is a cowherd, Themistocles is a glass maker, Cicero a fire kindler, Ulysses mows hay, etc., etc. The story of the warning and fall of ceiling upon the bed is better told in "The Error" by G. P. R. James. "Esoteric Buddhism" seems to be made up from the maunderings of the Apocalypse and maudlin gush of some weak minded evangelist.

The Foreign Missionary society, that great maelstrom of cupidity, gullibility, and credulity, claims to seek for heathen where the theosophist seeks for wonders, but there is a large field for the best efforts of both at home.

The "Rochester Knockings" offered nothing new, but the time was ripe for a demonstrable belief. Those knockings presented evidence to the masses that the opening of the gate depended upon the merit of the applicant and not upon the favor of the priest. Back to the dark may readily be traced the gushing forth of the spiritual application for recognition, too often met by the priestly devils with fire and sword.

The Cock Lane Ghost of 1760 answered questions by raps as is now done. Joseph Glanvil's Demon of Tedworth, 1661, is of the same kind. Peter Piquet, case Civil Court of Tours; the Holy Maid of Kent, beheaded by the butcher king, 1534; Joan of Arc, burned at the stake, 1431; then the thousands upon thousands murdered as witches,—but enough. As we trace the gory trail from the Egyptian priest down through Torquemada, Loyola, Luther, Calvin, Cotton Mather, Jonathan Edwards, the Andover school of theology, and efforts to force the closing of the Colum-

bia Exhibition Sunday, we find fire and blood lavishly shed when possible, then threats of hell fire in more enlightened times to keep the masses in subjection to this hierarchic control for selfish interest. The question, "Do devils die?" is one of terrible interest to mankind, for it is only a question of power if such continue to exist, whether the Smithfield fires and horrors of the Inquisition shall not again be revived.

A half century since belief in Spiritualism was general in an undefined way; all writers treated it as such. G. P. R. James's works abound in it, Scott, Marryat, Bulwer, Ainsworth, Burney, Jane Porter, Charlotte Bronte, all in fact accepted the belief. "Midnight Musings," by Washington Irving, is taken from the "American First Class Reader," published in 1831, and popular in our schools for a half century.

"Ye spirits of Washington, Warren, Montgomery,  
Look down from above with bright aspect serene;  
Come, soldiers, a tear and a toast to their memory,  
Rejoicing they'll see us as they once have been."

If that is not Spiritualism, what is it? Yet it commenced one of our most popular songs early in the century. Have our people become better for rejecting such belief now? A belief in spirit communion is the oldest, most encouraging, sensible, and progressive of any, but to be properly appreciated superstition and materialistic conventional ideas thereof must be abandoned. How shall I study the matter intelligently? was my inquiry when sitting for manifestations one Sunday morning.

"Study your own mind, you may find a gem," was the instant reply. "Who are you?" was asked. "Ballou," was answered. The evening after seemingly from another source came the following:—

If the truth you wish to find, you must study your own mind,  
Learn its workings, its relation with the great unknown creation;  
A gem we promise you shall find, in a knowledge of the human mind.  
Spirit friends around you gather, wishing much to help their brother,  
Seeking earnestly to find this gem of truth in the human mind.

False communications were constantly coming when outsiders sat with us, which caused me to impatiently inquire the cause. This reply followed:—

False, with the true, you'll one day find,  
Is but the crossing of your mind  
With our dispatches as they are sent  
From our Summer Land to your Continent.

One day while waiting for an assistant to return, Charla commenced to converse about unreliable communications that came the night previous, then remarked, "There is so much that is totally unreliable that I don't believe there is any spirit life at all," which caused me to commence a remonstrance which was cut

short by "Hush! hush!" from her, "I hear." Then after a short pause she repeated the following:—

Your lives are tangled in with ours;  
We are not far away,  
We join men and women in their work,  
And children in their play.

Soon after, this followed:—

If you will but be faithful,  
We will sometime prove to you,  
That spirit friends surround you,  
Who can and will be true.

Harmony is heaven's own law;  
And to get the truth you ask,  
Conditions must be perfect,  
And your sittings not a task.

We want you all to be of good cheer,  
And help each other while you are here;  
For in the life to come your riches consist  
Of the good you do to others in this.

My housekeeper, made up after the Mrs. Jellyby pattern, was inclined to be away much of the week, then pick up Sunday. I had remonstrated until tired, then let the matter pass with indifference. We made a practice of having a sitting Sunday morning. A racket in the laundry could be heard in the library, and one Sunday morning while reading I noticed that washing was being done. It continued for a short time then Charla and her sister came in to sit at the table, which was done for perhaps five minutes, then the table started for the door, then through the hall and kitchen to the back door, out through that down to the basement door; through that to the set tubs, there it immediately swung upon the sister's head and pulled that down and bumped it upon the edge of the tub, started again up the cellar stairs, through the hall and into the library, there floated up so that the top of the table hung upon the projecting cornice of the book shelves, hung there perhaps a minute, floated off and down in between the chairs, where we commenced, called for the alphabet and spelled out the following:—

Give the seventh day to rest,  
To thought, culture, and to us.

The following Sunday the table started back over the same course previously named, but instead of entering the basement it continued on down towards a small water power. When partly down the hill the women looked up to the windows of a neighbor where several persons stood looking at our table performance. My assistants fled for the house, leaving me alone with the table, which closed the performance; but the next day's mail brought me notice that an Iowa court had appointed me chairman of a commission to settle a case reported in the first part of this book.

(See page 95.) Of course it is a matter of conjecture as to whether there was any connection between the table journey and the appointment. I think there was.

In answer to a pertinent question the following was the reply :—

Sleep is a rest for the weary mind,  
Which, as it wanders free,  
Oft catches inspiration,  
And brings it back to thee.

Ofttimes when the mind doth wander,  
While the body is at rest,  
Strange elements of earth  
This freed mind doth impress.

Many times when the mind doth wander,  
Ideas which to earth are grand  
Are, in his sleeping hours,  
Stamped on the mind of man.

Then, when he doth awake,  
And reason and thought control,  
These ideas are developed  
And given to the world.

Almost identically the same ideas were published in one of the Boston papers the same week, credited as coming from the Concord school of philosophy in explanation of "*The Whichness of Which*" as editorially explained. It was common to receive a communication purporting to come from Ballou, then, as accidentally would happen, to take up a *Banner of Light* and find the same subject treated in a lecture by Mrs. Richmond in the same way. With Charla alone, if she felt interested, answers to questions would be given that to me seem to the point; but too often she was indifferent and the communications were the same. There was a persistent assertion that if I would persevere there was a band of spirits around me that in time would find a medium through whom reliable communications would be sent me. A niece came to visit us, a believer in the Advent doctrine, and that the spiritual manifestations were from the devil. Out of mere curiosity and bravado, perhaps, she consented to try the table with me and in five minutes was entranced and the series of communications that follow commenced.

This niece was subject to catalepsy and rarely was with us more than two or three days at a time. A heavy table would start from the side of the room and go to her; or standing between her and myself that table would turn somersaults between us. In her cataleptic conditions in the light, her boots would be taken off and thrown across the room; in that condition two persons could not raise her from the lounge. Sitting in darkness, her hands firmly clasped by others, her boots and stockings would be taken off and concealed in some out of the way place. Often she would come screaming from her room saying that some form had appeared to her, her description of which rendered recognition easy, in short, she seemed capable of producing every phase of manifestations known; raps with her meant such as could be heard all over the house, she personated the spirits of those who had died in asylums, and described their cruel treatment, etc., etc.

*I would like to study the materializations more, but want no medium that requires tying or test conditions.*



Oct. 25, 1878.

First reliable telegram: May I come in? Certainly, and welcome. My name is Julius N. Ives. I died September 15. I was seventy-six years of age, or should be now. I lived in Cromwell, Ct. A letter to the postmaster brought the following reply:—

CROMWELL, Oct. 29, 1878.

MR. EMERSON. *Dear Sir*:—Yours of the 25th of October is before me. Would say that Julius N. Ives came from Middletown, 18th of January, 1878, and made it his home in Cromwell with his brother, till he died, September 12, 1878, aged seventy-five.

A few questions: Was your niece a medium? Was she ever acquainted with Mr. Ives? Did she or any one see his death in a paper, etc.? I ask these questions because some have said that it might be the case.

Respectfully yours, JOHN STEVENS, P.M.

WILLIMANSETT, MASS.

Telegrams from—W-e-l-l where? Dec. 9, 1878. While sitting at the table one evening, there was a call for the alphabet, and as it was called, a message as follows was immediately spelled out:—

There is an old man here trying to get control of the medium.

All right, was our reply, go on.

Do you allow strangers to come in here? was asked. Certainly, you are very welcome!

Well, I didn't know as you would, but I was looking round and would kinder like to look in. I am from Saco, Maine. I was a blacksmith there many years. How old? Why, about seventy, but cannot tell exactly, for I have hardly recovered consciousness. There was a blank for a while, but I died about four months ago or early in the fall. My name was John Gains.

Can I give the name of some one there to write to? well, I guess I can, w-e-l-l, let me see; why, write to S. S. Mitchell, Druggist, Main Street. He and I were old friends. Tell him that I would like to take one of them sly drinks from the barrel. Ah, it wasn't every one that could get a drink there, but I could, notwithstanding the Maine law.

Had you no family? was asked.

W-e-l-l my family—was kinder scattered. Oh, yes! I had a son, named Albert, he is in Washington, yes, and I had a darter, her name is—Sarah—Sarah, oh, Sarah Elizabeth, she is married, no, she is a widder, her name is—well I can't think of that chap's name. Oh, if you write, ask Mitchell about Horace Watterhouse. Poor fellow! he worked for me thirty or forty years and at times would go upon a spree and I used to take care of him, but now, poor fellow, I don't know how he gets along. I am looking round and will come again soon.

He came the next night and was told that a letter had been sent to inquire about those "sly drinks."

There now, did you write about them? Certainly I did! W-a-l-l there now, I hadn't orter said so, but I allers was saying such things! Had Mr. Gains visited us in the body he could have appeared no more real; he remained with us some time, gave many particulars that made him very welcome as a visitor. The communication was immediately sent to Mr. Mitchell, who seems to have employed a lawyer to look the matter up as may be seen.

SACO, ME., Dec. 12, 1878.

MR. POSTMASTER:—Will you please be so kind as to inform me if there is a man now residing in Willimansett by the name of James Emerson? If so, about how old is he? What is his occupation? Is he a man of good standing in the community? To what religious denomination does he belong, if any? How long has he resided in your place and where did he come from when he came to your place?

These questions and information are not asked for the purpose of injuring, in any way, Mr. Emerson or any other person, but from the best of motives, and I can satisfy you of my reliability if necessary.

Please give the information and greatly oblige,

Very respectfully, your most obedient servant,

F. W. GUPTILL,

Counselor and Attorney at Law, 99 Main Street.

A reply by return mail is desirable.

Mr. Guptill was furnished with the required information, then Mr. Mitchell made his reply, but it will be seen that he does not plead to the sly drinks. As I refused to suppress the communication Mrs. Emmons was called in as shown.

SACO, Dec. 16, 1878.

MR. JAMES EMERSON. *Dear Sir*:—In reply to your letters of inquiry about the late Mr. Gains I have to say:—

1. John Gains, a well known citizen of this place, a blacksmith, and a man of considerable property, died here last September.

He left several children, all of whom lived with him except his only son, Albert, who has resided in Washington many years. Of his daughters, one is a widow and her name is Sarah Elizabeth.

2. A man by the name of Horace Watterhouse worked for Mr. Gains many years and was always carefully looked after by him when the poor fellow (as the communication calls him) had yielded too much to his passion for drink—he still continues the blacksmith business under the direction of the administratrix.

Mr. Gains was one of the best friends I had in Saco and I don't wish to have the communication published, neither do I think his family would; still I should like to hear further from you in regard to this matter, although not a "believer."

Yours truly,

S. S. MITCHELL.

SACO, Dec. 23, 1878.

MR. EMERSON:—I have read your letters to Mr. S. S. Mitchell with a good deal of interest.

I think the communications that you have received are certainly remarkable, although very unsatisfactory.

Among my most valued friends are some of your belief, so that I have *seen something and heard a great* deal of spiritual manifestations without, however, having my views at all affected by it.

When our friends depart this life, I hope and believe it is for a better and happier existence—hence their burden of earthly care and trouble must be left behind. And because the infirmity of "poor Horace" was a trouble to my father during his lifetime seems to me to be the *very* reason why he should be relieved from it now. And if he is able to communicate with his friends here, there are matters (mysterious to them, but clear as the noon-day to him) that would claim his attention. And I do not understand why one member of his family should be remembered while another is forgotten.

I shall be interested in any further developments that may occur, and trust that you will sacrifice your desire to publish this matter at least for the present, to the wishes of the friends and family of the late John Gains.

Most respectfully yours,

MRS. S. E. EMMONS,

Saco, Me.

Box 117.

October 15, 1878.

The next was: My name is Charlotte Wooster. I lived in Litchfield, Conn., and died September 12. I was twenty—no, I cannot remember my age. Tell my friends not to mourn for me. I am happy, and do not wish to come back.

Reply :—

Nov. 6, 1878.

JAMES EMERSON. *Dear Sir*:—Charlotte Wooster, a daughter of Joseph Wooster of this village, died here on the 7th day of September last past, in her thirty-third year.

Very truly, L. W. WAPELLS, P. M.

The next came as follows: Anna S. Cookson, Coopers Mills, Maine. I died—no, I cannot remember when, but recently. Tell my friends not to grieve for me.

COOPERS MILLS, MAINE, NOV. 1, 1878.

JAMES EMERSON, ESQ. *Dear Sir*:—In reply to your letter, would state that Anna S. Cookson died the 20th of October. Was twenty years and six months old. She was sick but five or six days. Cause of her sickness and death, to the public unknown. Should be happy to hear from you again on the matter, and would like to know if the spirit told the cause of her death.

Yours truly, GEORGE W. GREENE,  
Assistant Postmaster, Coopers Mills, Me.

She died Tuesday, the communication came the following Friday evening, or there was an interval of three days between death and communication.

We were again informed that a stranger desired to get control of the medium. On doing so the name of Hazen Kimball of Hopkinton, N. H., was given, and his age as seventy-six.

Reply :—

HOPKINTON, N. H., NOV. 13, 1878.

*Dear Sir*:—Hazen Kimball died March 28, 1877, aged seventy-six years and seven months. Lost a relative in Chelsea, Mass., myself. Should be pleased to hear from the party.

With respect, DAVID L. GAGE, P. M.

The next was: My name was Stephen Sibley, of Chelsea, Mass. I died the 9th of June. I was sixty-four years of age.

Reply :—

No date.

JAMES EMERSON. *Sir*:—Stephen Sibley, a resident of this city for more than forty years past, and one of its principal business men, died on the 9th day of June last, aged sixty-four years, three months, and sixteen days.

SAMUEL BASSETT, City Clerk.

WILLIMANSETT, MASS., NOV. 18, 1878.

*Dear Sir*:—It has happened recently that I have had seven communications from those purporting to be in the spirit world. I have written to each place where these spirits claim to have lived while in this life. Six of the seven have been answered and confirmed in every essential particular, the only difference being a day or two in date of death. The last communication was as follows :—

My name is Cyrus Alden, of Leeds, Maine, ninety-three years old, a soldier of 1812.

Will you inform me whether such a person has resided there within your knowledge, and oblige,

Yours truly, JAMES EMERSON.

*Sir*:—There was such a man as Cyrus Alden, died March, 1877. I think some one is fooling you by getting these dates, and pretending that they came from spirits.

This answer was from the one to whom my letter was addressed, the postmaster of the place named; one of the profound kind that knows it all.

J. E.

Nov. 3, 1878.

Another: I wish to control Alice. I died in Paterson, N. J. Well, I can't remember the date, but in the early part of the summer. I was seventy-five years of age.

Write to the Grant Locomotive Company, Paterson, N. J., for information.

WILLARD W. FAIRBANKS.

PATERSON, N. J., Nov. 5, 1878.

JAMES EMERSON, Esq., Willimansett, Mass.

*Dear Sir*:—Willard W. Fairbanks was formerly superintendent of these works; he died last May or June, aged seventy-five years. I have sent your letter to his family.

Very respectfully,

D. B. GRANT,  
General Manager.

WILLIMANSETT, MASS., May 22, 1882.

MR. POSTMASTER, Franklin Falls, New Hampshire.

*Dear Sir*:—On Saturday evening last, while sitting in conversation with a niece, she suddenly became seemingly unconscious; then, shortly, in a very feeble voice, exclaimed: "My name was Benson (Samuel Benson), of Franklin Falls, New Hampshire. I was eighty years of age. I died four or five months ago, or in January last, of heart disease." Now, neither my niece or myself had ever heard of Franklin Falls, though some thirty-five years ago I resided a short time in Warner, also in Concord, and knew of Franklin through what were at that time termed the Akin boys, or the Akins, who were considered inventors of various devices, an awl haft for one. I would be obliged to you if you will be so kind as to inform me if there was such a person as Mr. Benson who died there in accordance with what I have written.

Yours truly,

JAMES EMERSON.

FRANKLIN FALLS, May 23, 1882.

Samuel Benson died about the time mentioned. Was about eighty years old.

Yours truly,

P. M.,  
Franklin Falls, N. H.

Another answer:

FRANKLIN, N. H., July 10, 1882.

JAMES EMERSON, Esq. *Dear Sir*:—I think you left a few words out of your first question. I understand its import to be this:—

1st. Was there such a resident of Franklin Falls as Samuel Benson?

Answer: There was.

2d. When did he die?

Answer: January 21, 1882.

3d. What was his age at the date of death?

Answer: His physician gave me his age as eighty-two years, seven months, and four days. But the *Merrimack Journal*, published here January 27, 1882, third page, second column, says he was nearly eighty. His daughter is away on a journey. As soon as I learn her address, I will try to remove the doubt.

4th. Was there any supposed cause of his death?

Answer: His physician says it was a disease of the heart called *angina pectoris*.

Very respectfully,

J. L. THOMPSON.

## PHYSICAL PHENOMENA.

For years past my investigations have mostly been at my home ; the same care has been observed as in mechanical, hydraulic, dynamic, and caloric trials. Witnessing the developing of cause and effect has amply repaid the time expended.

During the past two years my boy, now nearly thirteen years of age, and myself have formed our *circle*, at times others have joined, but such usually come with preconceived ideas, generally destitute of desire or ability to judge of force, time, or space necessary for effect, consequently it is time lost.

One, a doctress, came, prodded the boy with a pin, then began to orate about "reflex action"; she possibly had some idea of what she meant, I had not. The most of my investigations with my boy are in the dark, not all. An ordinary dressing table is used.

Often while sitting with this table between us the boy is thrown upon the bed, the round in the feet of the table placed across my knees, the top of the table resting against my forehead, the boy's chair is placed on top of the table, where there is barely room for the chair to stand, the boy is then placed standing in the chair, where he begins to declaim.

Then the voice of a child takes the place of his. This voice pronounces the longest words just as well when the boy is gagged as when his mouth is free. Untying feats have been performed by the boy, but it has seemed too brutal for me to care to experiment in that way.

He has shown feats of strength of the *Lulu Hurst* order that would be impossible in his normal condition.

The mesmeric influence is from the spirit side, at least not from me. A simple word, Minnie, would cause him to drop while crossing the room.

During the French trial some two years since, reported in our leading papers, I invited Judge Bond to witness the influence that might be brought to bear against another. He declined to do so, and often since the query has arisen in my mind as to whether the bench has a tendency to expand the mind. The practice of the law cannot be productive of the best thoughts.

I have seen a table dash at a man with all the fierceness possible in the physical man. So much force was used that the two legs, caught by the defendant, were splintered in a moment, and the contest was continued until every joint of the table was separated.

Such positive determination to injure caused me to inquire of the sitter if he could explain the why. "It is the spirit of old John Wright, damn him!" was the reply. "Who was old John Wright," was my inquiry. "He was a former partner of mine," was grudgingly answered.

I have had the table turn down upon its edge and rush at me, as a wheel would come if hurled through the space by rotary power, because I had refused to sit for some purpose demanded ; it was in the light, so that I dodged as it passed and it struck the wall, leaving a very decided mark in the plastering where my head had been.



At another time I had sneeringly told what seemed to be the spirit of a drunken Irishman to boast less and perform more. Instantaneously the heavy table was raised and dashed into the window. "What are you about?" was my inquiry. "Why, you wanted to see all kinds, and I showed you that," was the reply.

For the purpose of ascertaining effect, I often hectored the medium, making an aggravating remark, then moving silently in the dark to another place; hairpins, rings, a slipper, or other missile would be hurled at me and invariably hit; at times it would happen that light would pass over the medium as these were thrown; her arms would be folded and her countenance in perfect repose.

During an investigation of materialization in my library a chair was suddenly jerked from me. At the same instant a streak of moonlight pierced through the blinds upon the medium; her arms were folded and the face of the dead could not have appeared more serene than was hers.

By opening the doors of a cabinet quickly after arms have appeared from the aperture, a sort of halo of those arms may be traced back to the shoulders of the mediums though the real arms are firmly bound down behind their bodies. I have seen arms that must have been projected eight feet from the bodies of the mediums.

It happened that I was experimenting for several months with pans of sand. Those pans were placed, when not in use, upon a broad shelf in my library, such as is common in libraries for resting books upon while making selections for reading.

During the time there were few evenings in which I was not experimenting with what are called, "table tipplings." The table walked about the library, upstairs or down, into various rooms of the house, and, almost invariably, walked or tipped up upon the shelf mentioned, often turning along the shelf on its edge when the room would be so dark that a white handkerchief, held in front, could not be seen, yet the three pans of sand, were never disturbed. This was evidence to me that there was guidance outside of the sitters.

One evening, while sitting with a circle of neighbors, none of them Spiritualists,—the guitar was floating near the ceiling above our heads,—hands came in contact with all, which brought out hysterical screeches. "My comb is gone," said one young lady. "Well, one has just been placed in my back hair," said another. A moment after, the comb was placed upon the back of my head, and the hair, certainly not over five-eighths of an inch in length, woven by tiny fingers in and around the coarse teeth of that heavy back comb until it was so firmly fastened there that it remained until the close of the *séance*, and the room was lighted, and the work examined by all. No ordinary human fingers could have done the work.

I have sat night after night holding the hands of a medium, yet after lighting up it would be found that the boots and stockings of the medium had been taken off and hidden away. That medium could select a book from the shelves in the blackest darkness.

I have seen a dulcimer, also a guitar, floating up near the ceil-

ing of a room in the deepest darkness, sending forth music the production of which the gods might envy. The instruments were marked with phosphorus, which made them perceptible.

At times when sitting with my boy, the table would rise up slowly with the boy on top, to the utmost stretch of my arms, float for a moment, then slowly descend to the floor. This was common for months.

While witnessing materializations, a young lady dressed in white, with a broad blue sash around her waist, came out of the cabinet and stood facing me with her back to the cabinet. She was some eight feet from me. She swung her arm back and rattled some paper lying upon the top of the cabinet, then returned into the cabinet. In an instant after the medium came out to rest, raising the portière as she did so, and inviting all present to examine the cabinet to the fullest extent possible. Upon request by myself she stood up beside the cabinet, yet could not reach the top except by springing up to do so. The figure that came out must have been seven feet high, yet was so perfectly formed and proportioned that I had not noticed her unusual size until I saw the height of the medium as she came out.

At another time, the medium exclaimed, "Your mother is here and desires to communicate." "Very well," was my reply; and then I asked, "Mother, have you met with Mr. Pushee since being there?" Instantly a tune was commenced and played upon a violin, though there was no perceptible violin in the vicinity. Mr. Pushee was a well known dancing teacher and violinist a generation since.

I have seen six and eight of the most beautiful hands and arms projected through an aperture ten by twelve inches area, the arms moving so rapidly as to make it difficult for the eye to follow their movements, then with the fingers messages would rapidly be given through the deaf and dumb alphabet. It would simply be impossible for four or even three persons to stand up to such an aperture and project their arms as was done there. I have seen and felt hands smaller than those of the smallest babe I have ever seen, and larger than those of any human being in the flesh; have held them until they dissolved in my own.

As stated on another page, I have loaded a revolver of a medium, laid it upon a trunk in a closet, its muzzle pointed at a door not eighteen inches distant, had it discharged three times by request without a sign of the bullet, yet the fourth discharge by myself left the bullet hole plain enough.

I have seen and felt feats of strength, of carrying, of transferring of clothing, of jewelry from the ears or fingers of one person to those of another, that astonished me.

I have heard raps that could only be equaled by blows from a heavy sledge hammer, others hardly perceptible, had them seem to be upon the outside door, as though applications for admission. In fact, I have seen much that anyone having a particle of a scientist's nature would give up sleep or time to investigate.

One night I had gone upstairs leaving Charla and her sister sewing; suddenly there was a rush upstairs, and shrieks, "James,

James! some one is breaking in the basement door." In a moment I had raised a window from which I could look down upon that door; it was a frosty evening, with a bright, full moon shining upon that door, and all about the house nothing movable could be seen in any direction. A few evenings after, while experimenting, what purported to be the spirit of Charla's father came to us. "Why don't you come and indicate your presence, sometimes, when we are not seeking for you?" "I did the other night upon the basement door," was answered.

I have an idea that it is of this force that Keeley of Keeley motor renown has been experimenting so many years, so much to the disgust of the know-alls, but the world progresses very slowly. Cicero, in his "Nature of the Gods," sneers at the claims of the Babylonians that they had kept authentic records of nativities back four hundred and seventy thousand years, yet at the time he was arguing about the authenticity of oracles, signs, and portents, or Spiritualism and spiritual manifestations, the oldest of all religions, unless coeval and contemporaneous for a time with symbol worship, but bound to endure and grow brighter and clearer as symbol worship, under its numerous disguises, disappears. The pathway of Spiritualism has been marked with blood—but its own blood, never that of its victims—as it has pointed the way to a higher life.

The Sandwich Islanders at this time, after a century of missionary manipulation, offer an object lesson that cannot be misunderstood as to the baneful effect of symbolized religion. Would it not be more creditable to our intelligence and humanity to stop forcing our ignorance upon other peoples, and try to ascertain the possibilities of our own natures?

When these manifestations burst forth at Hydesville, Christianity had become so materialistic that professing Christians, like the fabled Jews of old, were the fiercest for crucifying those claiming to furnish evidence of a foundation for the supposed miracles of the early Nazarenes. There is no evidence to show that our early mediums were not invariably ready to submit to the most exhaustive test conditions, within the limits of reason, oftentimes beyond. If some of them have since become tricky they have had much to make them so.

It is time the brutal tying and test conditions were done away with, and the investigation should be done by kind but cautious observers. If the ruffianly can only be convinced through brutality let them go unconvinced. A ruffian is none the less a ruffian because well dressed.

To investigate intelligently one must expect to meet spirit friends as they left the body; progression for them ended with life here, and will begin again in new bodies.

Seeking spirits is done too much upon the plan of searching the scriptures.

The Christian that exacts twelve per cent. interest does not look for the passage that condemns usury, but that which says, Render unto Cæsar the things that are Cæsar's, the other fellow to render, he to receive. One is likely to find what he seeks.

## The Jewish Scriptures and Greek Mythologies from the same Myths.

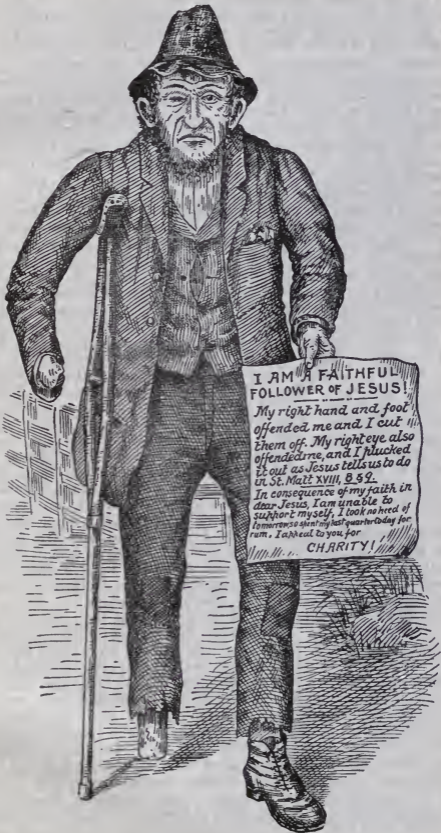
Should an English author of note assert that our or his own people are little less superstitious than the natives of Dahomey, he would cause a howl of indignation; still he could produce ample evidence to substantiate the assertion.

Are you a Christian? Do you believe the Bible? are questions to which an emphatic yes! would be the reply. Do you believe in dreams, prophecies, spirits, oracles, soothsayers, ideals, and witches? No! would be the general answer; yet the Bible is nothing without them, while Christianity is founded upon a dream and silly story that would be laughed at in any other matter and is laughed at by all of other beliefs, and at home by all but the superstitious. "All this was done that the prophecy might be fulfilled," gives the whole away. Without the rejected gospels little can be known of the matter; with them it is plain that Mary was kept in the Temple until her reputation and that of the priests required that she should have a husband at once. An old man was selected and accepted that position under strong protest. Why were the most explicit gospels rejected and without a record of the vote?

Go into particulars and it will soon be evident that the belief of the Christian is a vague ideal having the same credulity as the child's belief in "Jack the giant killer." Consideration will convince the intelligent thinker that the saints, Matthew, Luke, Mark, etc., were of the same caliber and character as those of our Lake Pleasant and other camp meeting speakers and writers, having the same tendency to present assertions instead of demonstrable facts. No evidence of any value can be furnished of the mythical crucifixion, nor do I believe there can be of finding the bones of a peddler in the Hydesville cellar. I have seen lights in the dark seances of the Spiritualists, as I have, in my fore-castle experience, seen bright lights in the daytime, but such were caused by a punch in the eye, and those acquainted with the persuasive ways of zealous Christians will not think it unlikely that the fist of a brother of the Calvinistic type caused the light that floored "St. Paul." Our Catholic Christians at death have the body surrounded by lighted candles that the Creator may find their souls. Talmage and Lorimer think half million dollar churches more conspicuous, churches in which the poor worshiper feels as much out of place as a tramp would in a meeting of bishops. A continual call is made for money to be used in christianizing heathen. Look at the model Christian represented upon the opposite page and consider whether heathen are likely to be benefited by the change. Christianity has had control fifteen hundred years, a hundred years in the Sandwich Islands. Where is the benefit? Take this from Theognis born 570 years before the Christian era.

"With kine and horses, Kurnus! we proceed  
By reasonable rules, and choose a breed  
For profit and increase, at any price  
Of a sound stock, without defect or vice.  
But in the daily matches that we make  
The price is everything. For money's sake  
Men marry; women are in marriage given.  
The churl or ruffian that in wealth has thriven  
May match his offspring with the proudest race.  
Thus everything is mixed, noble and base."

## PRACTICAL EFFECT OF THEORETICAL CHRISTIANITY.





Can any better description be given of society to-day? The fables of Æsop, so old that their authorship is doubtful, are yet as applicable to-day as before Christianity had been heard of.

Mrs. Ella Wheeler Wilcox, in the September number, 1893, of the "Arena," patronizingly as a Theosophist, tells spiritual mediums how ignorant they are, and how they could know it all by becoming Theosophists, yet there is not an idea in her article that may not be found in the works of Lucretius, written two thousand years ago.

Polyxena, as, womanlike, she calmly gave her throat to the knife that her death might appease the ghost of the sulky bully Achilles, is made to say by Euripides, in his *Hecuba*, "Receive my last address, O mother! O thou that hearest me, I am going below; what message shall I bear to Hector, and to thy aged husband?" Does a Christian die more intelligently or calmly? What ideal of honor or of morals can be shown to-day higher than those taught by Pythagoras, Socrates, Theognis, Plato, Lucretius, Cicero, Plutarch, and many others. If improvement cannot be shown, then where is the equivalent for the oceans of blood shed by Christianity to suppress progress and compel the more enlightened to submit to priestly influence? Humanity has generally progressed, but in spite of Christianity, as will be apparent by a careful study of Gibbon's history of the Rise and Fall of the Roman Empire.

Undoubtedly many nominal Christians have worked to elevate the masses and would have done the same had their environment caused them to be Atheists. Our seemingly most devout Christians at church are not our best citizens, as our prison statistics would show, if obtained. Our freethinkers are unquestionably our most progressive citizens, caring but little about christianizing heathen, but much about the equalizing of comfort and intelligence of our people at home. Christianity has done all that has been possible to prevent the intelligence of the ancients from coming down to us. Their best works have been destroyed, mutilated, or interpolated with lying forgeries. Epicurus a philosopher, who, like Ralph Waldo Emerson, taught that the best preparation for a future life was to live a good life here, is handed down as a man who lived solely that he might eat. Lucretius says of him, "Epicurus, who excelled the human race in genius, and threw all into the shade, as the ethereal sun, when it rises, obscures the stars."

We all know how evangelists of the Mills or Sam Jones type will lie about the "Awful deathbed of Tom Paine," where they have contracted to make converts at the rate of six dollars per dozen. The translation of the classics has done much to enlighten the masses; and the would-be leaders must get it into their heads, that evolution begins at the bottom, in the workshop with the silent thinker; then is published in some obscure sheet only noticed by rash and radical persons who care little about conventionalities or popular opinion; in a generation such ideas become semi-popular; then, after becoming bald headed from age, are taken up by our colleges and scientists of the Huxley-Tyndall type, and published by such works as the "Arena," and "Science Monthly," as advanced thought. Almost daily I get new ideas from children, working men and women, and cheap radical sheets sent me by

unknown authors. Yet I can say with truth that I have never caught a new idea from the writings of Herbert Spencer, though he is a great reader, and honorably credits to those from whom he quotes.

The numerous similarities show plainly that the Jewish scriptures and Greck mythologies have the same origin,—Jehovah and Jupiter, Adam and Deucalion, Eve and Pyrrha, the compound man-woman, Samson and Hercules, the same tradition of a deluge; Jephthah's daughter and Polyxena both expressing the same regret that death was to come before they could know the bridegroom. Visits of Gods, angels, prophets, spirits, mediums, soothsayers, oracles, and myths were common with both. These may easily be studied in the Bible or translations of the ancient writers; in almost all of which it will be evident that oracles or spirit communications were generally believed in, and consulted upon all state or important matters; as Saul sought advice from the witch of Endor.

From such writers as Herodotus, Plutarch, and many others, it will be plain that the oracles or communications were of exactly the same character as those from our mediums to-day. Spirit outbursts have occurred from the earliest times down to ours. That Christianity originated and continued for a time as such is evident. "Do to others as you would have others return," or "Love thy neighbor as thyself," is Spiritualism, for the account covers every phase of pure Spiritualism to-day. But a creed so simple would not support a priesthood then, any more than our camp meeting bummers of to-day, so dogmas were substituted for phenomena. Joan of Arc, the holy maid of Kent, Convulsionists of St. Médard, the witch manias and Rochester knockings were all of the same nature. Bulwer in his "Strange Story" gives the possibilities of spiritual influence as Dumas in his "Memoirs of a Physician" does of the mesmeric influence, both of which however I believe to be of the same source.

Probably from conventional prejudice the best investigators have failed to make intelligent application of their experience. The new investigator, if asked if he believes, answers too often with "No, I don't believe, I know!" then after a score of years, seeing that there is no progress, he becomes doubtful or a materialist. The trouble is, he has too much of the old Christian superstition about him and believes that spirits are perfect beings that know it all. It is time to begin to understand that this life is for progression.

"Life is the time to serve the Lord,  
The time to insure the great reward,  
And while the lamp holds out to burn  
The vilest sinner may return."

Mr. Talmage, has it occurred to you, that thinking so much of the *great reward* has made a corrupt people here?

"In the life to come, your riches consist  
Of the good you do to others in this,"

is better for progress, morality, and science, if not for Christianity. *Every man his own savior.* The great hindrance to progress is the lasting superstition inculcated in childhood. Can any superstition of

Dahomey excel in absurdity the "key myth" of Gregory—that weak man, perhaps drunken and lascivious, should have the power of the Creator to forgive sins? Greater, in fact, for the Creator neither forgives nor shows mercy. I challenge proof of a single case. God is law, violate his law and the consequence invariably follows. How often trains going in opposite directions have attempted to pass upon the same track. Success has never followed, nor in any other violation. Old saints and old spirits are equally unnatural, and contrary to nature. Suppose that when chaos ceased, and soil began to form upon the earth, some power had removed it as fast as formed, when would this globe have been habitable? Neither God, nature, nor humanity can afford the constant moving on of spiritual life. There is no "supernatural."

We know that a tree or the body disintegrates, then springs forth again in the same or other form, which is change, but continuation. Is the spirit exceptional or less natural? The electric engine is surrounded by electric energy, as the atmosphere surrounds the windmill. Do we go to the electric energy, or atmosphere, to find how either engine works? So of spirit power; we get no spirit outburst, such as witches, haunted houses, flying tables, or dishes, unless a human body is present; and spirit phenomena must be studied in connection with the body. To do this understandingly all notions of heavenly etiquette must be abandoned. We are surrounded by this spirituality and there is not a shadow of proof that spirits are better or different from the embodied ones here, or have any higher knowledge to impart to us. The first necessity as an investigator is to abandon superstitious myths, such as a New Jerusalem, located in a mythical *Nowhere*. Consider everything natural and upon its merits. The natural home of the spirit is incarnated and in this life; when disintegrated, it is part of the surrounding intelligence. After the death of a body the spirit for a time retains its individuality; how long will depend upon its nature, as of a tree. That there is a spiritual body, one more substantial than generally supposed, I believe susceptible of tangible proof. This body or influence is plainly perceptible as it comes near or stands beside you, and very positively so at times; sitting with three at a heavy table the fourth side or end may be observed to rise and move as it would if a fourth physical sitter were there.

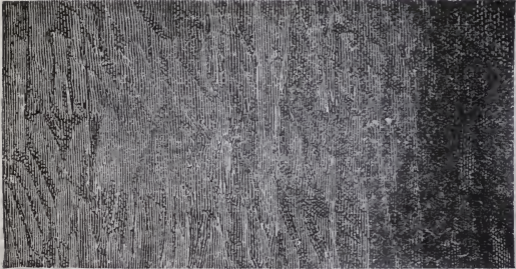
Surrounded by intelligence, the brain receives and guides it in ordinary channels. The seeker finds more.

The question is daily asked, Do you think spirits would come back and tip tables? Certainly, if that is the way they can best make their presence known. They do worse things than tip tables while in the body, why not after leaving it?

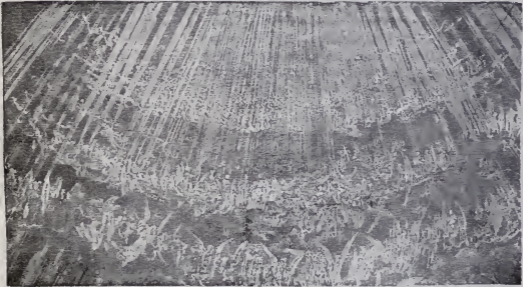
Of course this belief will destroy the pleasing illusion of knowing former friends and relations after this life, forever, but is it certain that our desire, if granted, would be the best for us? We have been well guided up to this life and have no reason to doubt the future guidance of the same power. I for myself can cheerfully say, "*Thy will be done.*" A constant rotation gives each one a chance and in time will produce perfection.

What is the difference between "Heredity" and "Reincarnation?"

THE MATERIALIST'S OR DON'T KNOW'S HEREAFTER.



THE SPIRITUALIST'S OR CHRISTIAN'S HEREAFTER.



THE RATIONALIST'S OR REASONER'S HEREAFTER.



## MEDIEVAL BARBARISM STILL EXTANT.

Where is the heaven located that Christians talk so much of and seem so much to dread starting for ?

More than fifty years ago at a prayer meeting, a *brother* kindly informed me that I was liable to be sent to hell that night. "And just think," he exclaimed, "if this earth was made up of fine sand and a bird should carry away a grain once in a million of years, in time it would all be gone, and your punishment would be no nearer ending than at its commencement ; while all of that time I hope to be singing the praises of the Creator, not through any merit of my own but through the atoning blood of Christ."

There is no reason to doubt but what the soul of such a man would be small, yes, very small ; but even the soul of anyone willing to be saved through the sufferings of another may be as large as a fine grain of sand. As there are thousands of such souls freed from the body daily, it can be comparatively but a short time before the bulk of souls will exceed that of the earth, and as the other planets should be in the same condition what is to become of such souls ? But first, where are such souls to come from ? If you constantly check out without depositing, your checks will not be cashed. So of souls.

Again I ask, where is this heaven in which the sole business is to sit in one's nightshirt and shout pæans in glorification of a monster who enjoys electing arbitrarily a favored few and witnessing the endless broiling of billions, and the paving of the broiling place with innocent infants' skulls. "Stop, stop, in mercy stop ! No one believes in such inhumanity now !" My dear madam, this very barbarism in this year of 1894 is preached and approved within three hundred yards of where this article is written, and in all of its lurid ghastliness, the preacher consistently arguing that a "Divine revelation" admits of no change. Of course only the venal, ignorant, or weak minded utter or listen to such barbarism.

Can one wonder that our prisons and asylums are crowded, and that societies for the prevention of cruelty to the helpless are needed ? or that preachers of the Talmage, Lorimer, and Parkhurst type decline to aid in efforts made to ascertain the moral influence of the various religions upon the masses ? And it may be asserted without fear of successful contradiction, that for each free-thinker or Spiritualist that may be found in our prisons or asylums, a hundred of the Calvinic-Romish type may be found to offset. The same old stories are told ; one, the dying boy saying to his good father, "Oh, father, you never taught me this, and now I shall go to hell and never see you and mother again !" The best antidote for this money gathering scheme would be to chain the preacher close in front of a roaring fire until well browned. For the endless psalm-singing, think how even the mother hushes her babe with "Yes, dear, and now go to sleep," as baby says "Dood manma, baby loves oo." It has happened several times that I have saved human life, once by plunging from a steamer's deck. Praise the first time was pleasant, less so the next, then soon became nauseous. Could the creature respect a Creator that required it eternally ? As I look back over a long and eventful life, I can recall many acts that I deeply regret, though I will not assert that under the same con-



ditions I should not do the same again, yet I hope that I have never sinned so deeply as to give cause for sending me for an eternal residence in an orthodox heaven. I should not like it here, and, as James Emerson, I should not like it there.

If Christians have any regard for the positive teachings of their gospels aside from them as relating to their self-interests, it has seldom been made apparent.

Can any statement be made more positive than the one that for every effect there is a cause, or, "Not a sparrow shall fall without the Father's notice." Yet how complacently the most bigoted believers after witnessing astonishing phenomena will placidly settle down on, "Oh, it was a COINCIDENCE." Do such shallow minds realize that for each coincidence there is a cause?

### CREMATION.

The disposal of the body after the spirit has left it has been one of the oldest and most familiar subjects treated of by tradition or history.

Excavated tombs, funeral pyres, exposure to birds or beasts of prey, burial in the earth or in the ocean, placing in mounds or trees, and many other methods have been favored by various peoples. With ourselves, through superstition, custom, and desire for display, the most disgusting and unhealthy method has continued until not only the possibility but the probability of burying the living, as well as the thought of the lingering corruption of the remains of our loved ones, has caused the consideration of disintegrating the cast-off shell by the purer and more expeditious use of fire.

Certainly neither our bleak hillside graveyards with their leaning and lying headstones, nor our crowded cemeteries with their glaring marbles above and festering corruptions beneath, offer anything that is pleasing for contemplation.

Formyself, it is my positive request that, after my spirit has passed on, my body be cremated and the ashes scattered by the winds without any reservation.

### THE PSYCHIC SEARCH SOCIETY.

Since it is well known that I have given much attention to the study of what are called spiritual manifestations, my opinion is often asked as to the effect of the "Psychical Search Society." As I believe in its beneficial influence my reasons therefor are here given. Any subject becomes conventional and popular as it becomes common. A society or mob will often do what an individual will hesitate to assume the responsibility for doing, and many join a society for the supposed honor that membership carries, especially if such society has a high sounding name; but that any new light will be thrown upon spiritual phenomena by this society is very doubtful. Discoveries are made through patient individual efforts, so far as my experience goes, and real investigators care but little about belonging to societies.

## Hallucination or Mystery.

Our age is materialistic or mystical, and the writer desirous of being read fifty years hence must realize the rapid changes taking place in thought. Buckle, Mills, Kant, Carlyle, and Herbert Spencer are of the past. Walled cities and non-intercourse must give way to steam and electricity, which will make the whole world a brotherhood. I have a fair collection of standard works and plenty of borrowers,—Irving's, Hawthorne's, Cooper's, George Eliot's, Gilmore Simm's, and Thackeray's might do about as well if made of painted forms of wood. Scott, Holmes, and even Dickens are read but little. Bertha M. Clay, Miss Braddon, Cecil Hay, the Duchess, and others of like character are read by the young, but there is another and rapidly increasing class that read and study the mystical, such as Bulwer's "Zanoni," "Strange Story," and "Coming Race," Sinnett's "Karma," the "Veiled Beyond," "Affinities," "Paul Vargas," "Daughter of the Stars," "Bichwa," and thousands of others, and, though they may not accept all there presented, such works cause thought of the possibilities. These readers, thinkers, and investigators realize that there is much to learn. It is through these that we have the most rapid progression and startling ideas, for they care but little for conventionalities, ghosts, or graveyards. For unknown ages, ghosts have been believed in, and are now to a far greater extent than unthinkingly supposed. Two thousand years ago Lucretius accounted for them by saying that the spirit cast off shells as a snake sheds his skin. A Massachusetts school board, without offering evidence that they know anything about it, say that they are hallucinations. Some twenty years ago, I left my assistant at the Holyoke depot, and walked to Willimansett. On arrival at the depot there and turning to look back, I saw her coming out of a covered sidewalk to the bridge. I was vexed, for the snow was deep and no path, while there was a train but a few minutes later. After watching her wade through the snow two-thirds of the way to me, I turned and went home. She did not come until after the train passed by, but nothing was said about it for a month after. During that time had there been any necessity for establishing her whereabouts on the day I left her at the depot I should in perfect faith have gone upon the witness stand and sworn to having seen her wading through the snow at the time stated, yet she was not there physically at all, but came over in the train as proposed.

A few months since, getting on a train at Willimansett, I took a seat with Harvey D. Bagg, one of the county commissioners. We had a pleasant talk on the way and I got the impression that he came away from home without changing a coat kept for work around the barn, for the binding in front was worn and frayed out. At Chicopee he left the train, and I thought no more of the matter until taking up the *Springfield Republican*, three days later, and seeing a picture of Mr. Bagg and an account of his death the day I rode to Chicopee with him, brought our ride together forcibly to my mind, causing me to make inquiries, which established the fact that he had been confined to his bed for days before his death. Some months previously I had sent Mr. Bagg a copy of an earlier edition of this work. Meeting him in the train a few days later he

took pains to stop and tell me that he had received and read my book all through and that he was going to commence and go through it again. I mention this as the possible cause why there should be an attraction to bring us together.

Whether these appearances are shells cast off by the spirit, as Lucretius thought, or "Hallucinations," according to our Christian, materialistic school boards, is a matter yet to be decided, and as superstition dies out these appearances will command more attention; to me they are very real, and at times take place when I am in conversation with others.

The description by Mr. Conway of the "Bichwa" dagger has strong attraction for me, and I think for many others. The dagger was so made that there was a strange blending of light and colors that caused the holder to first desire to commit suicide, then murder. From an irresistible impulse, yet without apparent cause, I am impelled to throw myself under a flying train, from a high precipice, or into a roaring furnace. The impulse is so positive at times that my only safety is to turn away. I think that such impulses are not uncommon. Would it not indicate a truer humanity to know more of ourselves before deciding who are heathen?

### PROPHESYING FUTURE EVENTS.

Of the possibility of foreseeing events abundance of evidence has been furnished me, but two cases only will be given here.

Sitting with Charla and her sister, our attention was called, then:—

Five years from this day, one of you three  
Folded in the bosom of mother earth will be.

April 21, 1878.

The communication caused us often to think of it. Three years or more passed by, then a communication from a medium came to us saying that we three were not meant, but the three of the family, Charla, her brother, and sister; the remaining members of their family. Some months afterwards news came of the sudden death of the brother in the far west.

### ANOTHER CASE MORE DECISIVE.

At my home three of us were sitting at the table talking of the death of a little child of one of the sitters; the other sitter was entranced and said, "Another little child will soon come over here." I said, "I hope not from the one who has just lost the one spoken of." "There is a star over her head, which signifies peace. It is not hers," was the reply. Then she exclaimed, "Within four months from this day and within sixty rods from this house another little child will come here."

The time passed on; about two months after a little child sickened and died, then it was said that the prophecy had been fulfilled, but to me it seemed not, for she had no connection with the sitters.

The fourth month had well advanced when the youngest child of the prophetess sickened and died but a few days previous to the expiration of the time. These statements may be depended upon to the letter.

## Mind Reading, Thought Transference or Inspiration.

The hindrance to human progress caused by the superstitious belief in the special inspiration of the mythologies handed down to us by the Jews is incalculable. Comparing our ideas of science with those of Lucretius or the elder Pliny, and a moderate advance is perceptible, yet we have barely entered the portal of mysteries that should have ceased to be mysteries centuries since. How little we know of ourselves aside from the universal greed for selfish ends! Our predecessors looked upon sudden death as desirable and a gain. Christians fear death, call it the king of terrors, and mourn for it in the utmost gloom. Can there be a more pitiable sight than the smile of approval with which the elders greet the gush from children uttered in platitudes about the joys received from having given their hearts to God, a matter understood by them as the goose understands the alphabet from which it selects a letter at a prearranged signal from its trainer, especially where such children are known to be the least reliable of any in their neighborhood. Can such superstition please any except those so degraded as to desire to live upon the scant earnings of labor, and infant-like to ride in public conveyances and go to the circus at half price! Romanism is the religion of babyhood, likes dolls, puppets, and genuflections; but as it lacked the ability to construct such, took dolls, idols, ideas, ceremonies, and genuflections from its pagan predecessors to use under new names. Such a salmagundi could hardly expect to hold full grown men like Luther any more than its antipodean extreme, the weak or unsettled minded Unitarian with his "Don't know," could hold a Parker or Emerson. Episcopalianism, Presbyterianism, Methodism, etc., etc., are but the dishwashes of Romanism, the strength of each depending upon the squirt from which it is ejected, each equally superstitious, delusive, money grabbing, and desirous of reforming others instead of themselves. Do away with these priestly schemes for self-aggrandizement, and inspiration will be found to be a common gift from a beneficent Creator to all. How soon the babe catches our meaning! We are continuously hearing of the singular sagacity of horse, dog, or other animal. How shy the crow is of man where a price is placed upon his head, and how quick he becomes indifferent when law and popular opinion protects him! Observation will show that mind reading, thought transference, and inspiration are but different names for the same faculty. A few cases will here be given.

One evening my children were making shadow pictures upon the wall by interposing their clasped hands between the wall and light. Suddenly attention was called to a sharply defined but unexpected shadow caused by placing a brilliant light back of the shaded astral lamp. Its unexpectedness strongly impressed upon my mind, "Oh, that is the shadow of the astral lamp!" My little eight-months' old girl quietly turned in her mother's arms and pointed to the lamp as the cause of the shadow. A year later I had purchased some patent cuff buttons to take home to my family as a surprise. They were made in two parts, so that they could be inserted in the eyelets of stiff cuffs without danger of breaking, and were the first I had ever seen of the kind, though common

now. On arrival at home my little girl was found crying to go out with her mother. Calling her to me, the buttons were shown her, with the promise that she should have them to play with if she would remain with me. "Yes," she said, "but will you show me how to open them?" She could only have known through my mind that they would open. Soon after that she was put to bed with me, her auntie, with whom she usually slept, having gone to help care for a neighbor's sick child. After prattling for a while, she dropped to sleep. An hour later word came that the sick child had died. I had lost loved ones, and my sympathy for the parents kept me awake. Near morning my little girl awoke, snuggled up to me for a time, then exclaimed, "Little Jessie Lyon is dead, and I can never play with her any more." Until four or five years of age such cases of thought transference were of everyday occurrence with her.

Spiritual lecturers like Mrs. Richmond, Nellie Brigham, and others, offer excellent chances for study. I have had several of them at my home. Their specialty consists in delivering lectures upon subjects handed them as they rise to speak. To suppose such speakers can be posted upon any subject that may be handed them, so as to speak from memory at a moment's notice, requires a stretch of credulity only possible to idiocy. I have generally found them pleasant, ladylike, common, with rarely an advanced thought or desire for change or progression; mere conduits of the conventional ideas published and to be found in works treating of the subjects handed them. There are strange features, however, in these thought transferences that have puzzled the wisest minds for unknown ages, minds too well distinguished for ability to allow of their being ignored.

The ambiguity of these oracles has only made them the more remarkable. In one case, writing a story for publication, I had confined the statements to facts to a certain point, then drawn upon my imagination for interest as follows: "As I moved on something brushed past my cheek. Looking forward there stood a heavy sheath knife quivering in the foremast." More than forty years after the time alluded to, going into a hall in Chicopee, Mass., I was startled by an exclamation from the lecturer, who stood with finger pointed at me, exclaiming, "In your nineteenth year an inch change in the direction of a missile and you would have been dead!" He then gave the correct name of the accredited knife thrower, a Portuguese. The incident, so far as it happened at all, took place off Cape Horn, and in my nineteenth year; fear of the consequences alone prevented the knife from being thrown. The most of the ancient writers have written of these oracles, and of their ambiguity. Herodotus has furnished us with accounts of many, the most noticeable perhaps is of Cræsus questioning the Pythian as to whether he should commence a war, and was told that for the time it might do, "but when a mule becomes king of the Medes, then, tender-footed Lydian, fly and do not blush to be a coward." Of course he thought that the Medes would never have a mule for a king, so went in for glory, but it happened that Cyrus was the mule, his parents being of different nationalities, and the glory did not come in.

Plutarch states that Mopsus, governor of Cilicia, sent a sealed letter with an inquiry to a Pythian and was answered, "A black



one." On opening the letter the inquiry was found to be, "Shall I sacrifice to thee a white or a black bull?" Cicero has much to say of these communications in his "Nature of the Gods." A story is told of the Duke of Buckingham aspiring to the throne of Henry VIII. An aspirant for favor consulted a medium, and was told that the duke's head would soon be the highest in the land, which was supposed to indicate that he would soon be king, instead of which he was beheaded and his head stuck upon a pole above the gate of the city. We have only to read to find them mentioned all the way down. Superstition has caused these oracles to be looked upon as miraculous, as is the case of smiting the rock by Moses to get water, but if we strike with a pipe hard enough we can draw water from almost any part of the earth's surface. So of inspirations; the thinker knows how readily ideas flow into the earnest seeker's mind, and it is my unalterable conviction that the Creator's plans will not be completed until man has risen to such perfection that the cause for every effect will be clearly understood. Long before that time, however, inspiration will be known to flow through our minds as water circulates through the earth's surface; also that heredity has an important influence upon mankind, environment still more. Many bright children have been intellectually smothered by their surroundings.

A sponge surrounded by fluid takes in sediment according to the fineness of its fiber. To make my meaning clear, take, say, the authoress of the "Little Pilgrim." Communications through her should be sweet, charitable, but impracticable except in Utopia a thousand years hence. The authoress of "Beyond the Gates" should produce communications very proper, slightly progressive, not too much so, for her patrons have weak digestive powers; an overdose would cause the grip, which would have a disastrous effect upon the dollar product.

The authoress of "Is this Your Son, My Lord?" should produce bright, brainy, intelligent, progressive, practical, womanly ideas, clear in style as the tone of a silver bell. Would there were more like her!

"Free love," or rather free lust, is an epithet hurled at anyone daring to question the divine origin of Christianity, but the sex force is one of the strongest in nature and manifests itself in the nunnery, confessional, church, either Catholic or Protestant, quite as commonly as with the Spiritualist. Miracle mongering should be unknown in this country, yet crowds may be seen every morning standing in front of churches waiting to unload their sins. Sin consists of doing what one believes to be wrong and it may fairly be questioned whether the soul saved by the priest had not better be lost and go into the muck heap as fertilizer for souls with sufficient manhood or womanhood to save themselves.

The unprogressive priest, notoriety-seeking preacher of the Talmage-Parkhurst type, the proselyting evangelist, and captious wife and mother of a household that is never ceasing in fault finding and fretfulness, will benefit the world the most by dying.



APOLLONIUS OF TYANA, THE JESUS OF NAZARETH.

## ANTIQUITY UNVEILED,

By Communications from Ancient Spirits.

Prepared by J. M. ROBERTS.

*Published by the Oriental Publishing Co., Philadelphia, Pa.*

This work contains a mass of information convenient for reference for one desirous of looking up the evidence for the claimed divine origin of Christianity, no matter whether such seeker is or is not a believer in spirit communion. The purpose of the work is to show the mythical character of Jesus of Nazareth, also that Christianity is of a much later date than claimed in what are called the Gospels, etc., a matter easily confirmed by the silence of contemporaneous writers of note, though Eusebius found it desirable to write a book in answer to Hierocles of Nicomedia, who published a work against the Christian faith, and asserted that Apollonius Tyaneus performed more and greater things than their Christ. Gibbon in his "History of Christianity" alludes to Apollonius. Writers of the character, ability, and habits of observation of Tacitus and the Plinys would hardly have failed to notice such tremendous manifestations as claimed by the Gospel writers, had such ever occurred. It will be well to recall the fact that the elder Pliny lost his life investigating the cause of the destruction of Pompeii. A Bishop Warburton discovers a profound theological purpose in the writings of Apuleius, author of "The Golden Ass,"

# THEACNES AND CHARICLEA.

FROM HELIODORUS' ROMANCE, A. D. 400.



Appearance of Chariclea before Sisimithres.

which perhaps may account for the fact that the translators of the most obscene works of the ancients handed down to us have the prefix of Rev. So and So. It may safely be asserted, however, that if profound theology delights in an obscene nest, it found a congenial home in "The Golden Ass."

Suetonius, contemporaneous with the younger Pliny, knew nothing of Jesus or Christianity, though he refers slightly to the Hindoo Chreeshna in connection with the Jews.

Epictetus, a philosopher, alludes quite often to the influence of a young girl, but knows nothing of Jesus or Christianity.

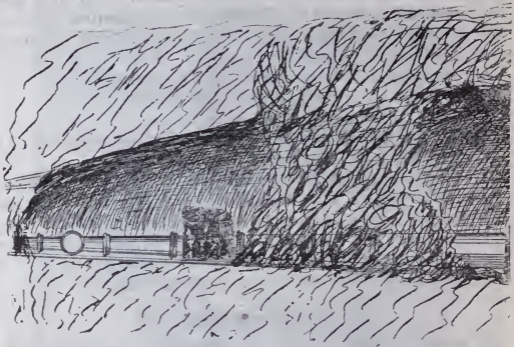
Achilles Tattius, author of "The Loves of Clitopho and Leucippe," wrote some two or three hundred years after the wonderful crucifixion, yet knows nothing of Jesus or Christianity.

Longus, author of "Daphnis and Chloe," an amorous tale supposed to have been written in the fourth century, has no hint of Christianity, yet often alludes to the heathen deities.

### HELIODORUS.

A novel is dependent upon its truthful representation of its characters, environments, and times, for its popularity, consequently is often better than a history to give us information. Heliodorus in his early life wrote romances of his times, one of which is the story of "Theagenes and Chariclea," an illustration from which may be seen upon the opposite page, though the artist has substituted the temple of Diana for the tent of Hydaspes. Heliodorus, it is said, about A. D. 400, became a bishop, but being required to give up his romances or bishopric, preferred to keep his romances. In the story of Theagenes and Chariclea not a hint of Christianity is given, though the heathen deities are made prominent. No unprejudiced seeker for the truth can doubt but what Christianity started from a collection of Spiritualists like our camp-meeting followers, and with the same proclivities. Lactantius, a church historian of the third century, states that Apollonius was a sort of Thaumaturgist, as our spiritual mediums are often called at this time. Eusebius, as was natural for one of his condition, rather approvingly reports the fact that the "Blessed Peter was delighted to see his wife led to execution." As the *Gospels* state that this same Peter when cornered could curse, lie, and swear, we get an idea of the rock upon which the Christian church was founded. Even a Vanderbilt, with his "Public be damned," with a proper check in hand need have no fear when approaching the celestial gates, while that blessed Peter holds the key. And you dear women who make up nine-tenths of the morning crowds at the church doors, of course will cheerfully step forward to be boiled like Mrs. Constantine, or led to execution like Mrs. Peter, that the unctuous representatives of those holy men may have no impediment to a free circulation through your holy gatherings. Ah, sympathetic souls! you may bear the cross and wear a crown, but the crown should be the fool's cap, and that of your husbands something worse.

## CAVING IN OF A MINE.



Almost monthly we are horrified by frightful reports of miners being inclosed in living tombs through the roof of the mine caving in ; while wives, mothers, and children around the entrance to the mine shriek to heaven for aid that man seems incapable of giving.

Would it not in a great measure do away with such horrors if the owners would lay, say, thirty inch water pipe along the bottom and side of the mining galleries, so that, in case of the roof caving in, air would freely penetrate to the chamber beyond, and out through which the miners could easily escape ? Would it not also do away with the "fire damp," or dangerous gases, if fresh air was forced through such pipes into the chambers of the mines, when far more brilliant lighting would be practicable, that would cause impending dangers to be observed and guarded against ? To me, it seems that there are innumerable ways for adding to the safety and comfort of our own people that would be far more acceptable to our Creator and creditable to ourselves, than is the caring so ostentatiously for the souls of *heathen* that perhaps know as much of God as we do ourselves, though not bragging so much of it. Brother Lorimer, is not the idea worth consideration ? If such ideas are obtrusive, are they more so than the tracts you so constantly thrust upon the public as announcement of your superior wisdom and holiness ?



## POWER OF NIAGARA FALLS.

A matter of easy approximate computation, yet I have never seen any such estimate that deserved consideration. The proper way to obtain such measurement would be to get the cross-section and velocity of stream at its narrowest part below the falls, which seems near the old suspension bridge, where the surface width is a little more than three hundred feet. The depth and velocity there could easily be obtained by sounding line and ship's log. The bottom of the river undoubtedly forms an inverted arch, covered with broken rocks, the water deepening so gradually as to allow of building walls out some distance from the shore, as was done for the tub wheel race, back of the old flouring mill upon the east side near the bridge, where the bed of the river descends perceptibly. The current at that point is more rapid than on the west side, where row boats go up and down to or from the bridge, I think.

A careful observer familiar with the turbulent rush of water through "Hell Gate," when "Pot" and other rocks reached up to within a dozen feet of the surface, and the comparatively smooth flow through there now, since those obstructions have been removed, leaving a clear depth of twenty-two feet, may judge approximately of the depth and velocity of water below the falls; to aid such judgment, the fact should be recalled to mind that the steamer "Maid of the Mist" was safely sent down the river to Lake Ontario, also that Capt Webb was killed by striking a rock at the whirlpool, which furnishes sufficient evidence that there is no great depth of water there. Below the old suspension bridge it is doubtful if there is an average depth of twenty feet. At the bridge it is a liberal allowance to give the cross-section three hundred by forty feet, with an average velocity of six feet per second, the fall one hundred and forty.

Cross-section,  $300 \times 40 = 12,000 \times 6 = 72,000 \times 140 = 10,080,000 \times 62\frac{1}{2} = 628,320,000 \div 550 = 1,142,400$  H.P.

The above I believe to be an overestimate, and it should be borne in mind that the head is great compared with the quantity of water, which for the immense watershed drained, gives good cause for the imagination to seek for subterranean outlets not yet discovered, and far more so when the immense increase in flow at Montreal is taken into consideration, from the comparatively small watershed between those two points.

The matter is one of interest to the whole world, for there are few such falls. As knowledge increases, their action may furnish a key for the solution of many mysteries. Our government should take careful heed that such a phenomenal wonder should not be obliterated through greed, ignorance, or indifference. Surely America may afford to own and retain control of a natural spectacle of such unrivaled grandeur. Numerous water powers may be named that were supposed to be inexhaustible forty years ago, yet to-day leave the river bed dry for months each year. Allow the insatiate mill owner control and Niagara Falls would be but a name within a generation.

## NEW AMERICAN TURBINE

MANUFACTURED BY

GLOBE IRON WORKS, DAYTON, OHIO.

42 INCH RIGHT HAND WHEEL.

| No. of the Experiment. | Prop'l part of                      |  | Head acting on the Wheel, in feet. | Duration of the Experiment in Minutes. | Revolutions of the Wheel, per minute. | Quantity of water discharged by the Wheel, cubic feet per second. | Power developed by the Wheel, H. P. | Efficiency of the Wheel, in per cent. |
|------------------------|-------------------------------------|--|------------------------------------|--|---------------------------------------|---|-------------------------------------|---------------------------------------|
|                        | the full opening of the Speed-Gate. | the full discharge of the Wheel; being the discharge at full gate when giving best efficiency. |                                    |  |                                       |   |                                     |                                       |
| 33                     | 1.000                               | 1.014  | 16.39                              | 4                                      | 116.25                                | 136.40  | 200.24                              | 79.17                                 |
| 32                     | "                                   | 1.008  | 16.37                              | 4                                      | 120.50                                | 135.60  | 209.99                              | 80.03                                 |
| 31                     | "                                   | 1.004  | 16.36                              | 4                                      | 124.00                                | 134.97  | 200.08                              | 80.09                                 |
| 30                     | "                                   | 0.999  | 16.33                              | 4                                      | 128.00                                | 134.18  | 199.56                              | 80.50-full gate                       |
| 29                     | "                                   | 0.994  | 16.33                              | 4                                      | 132.25                                | 133.54  | 198.08                              | 80.29                                 |
| 28                     | "                                   | 0.988  | 16.28                              | 3                                      | 136.00                                | 132.52  | 194.44                              | 79.66                                 |
| 27                     | 0.710                               | 0.916  | 16.43                              | 4                                      | 112.25                                | 123.38  | 184.18                              | 80.31                                 |
| 26                     | "                                   | 0.912  | 16.46                              | 4                                      | 117.50                                | 122.99  | 186.39                              | 81.38                                 |
| 25                     | "                                   | 0.907  | 16.47                              | 4                                      | 122.25                                | 122.36  | 187.27                              | 82.13                                 |
| 24                     | "                                   | 0.900  | 16.51                              | 4                                      | 128.25                                | 121.60  | 187.73                              | 82.65                                 |
| 23                     | "                                   | 0.893  | 16.56                              | 5                                      | 134.80                                | 120.85  | 188.14                              | 83.09- $\frac{1}{2}$ gate             |
| 22                     | "                                   | 0.877  | 16.55                              | 4                                      | 144.00                                | 118.57  | 181.37                              | 81.69                                 |
| 21                     | 0.504                               | 0.798  | 16.87                              | 3                                      | 110.00                                | 108.99  | 164.76                              | 79.20                                 |
| 20                     | "                                   | 0.795  | 16.74                              | 3                                      | 113.33                                | 108.15  | 164.34                              | 80.24                                 |
| 19                     | "                                   | 0.793  | 16.53                              | 5                                      | 117.00                                | 107.18  | 163.29                              | 81.47                                 |
| 18                     | "                                   | 0.785  | 16.56                              | 4                                      | 124.00                                | 106.25  | 164.62                              | 82.70                                 |
| 17                     | "                                   | 0.774  | 16.59                              | 3                                      | 129.33                                | 104.85  | 162.89                              | 82.77- $\frac{1}{2}$ gate             |
| 16                     | "                                   | 0.764  | 16.67                              | 4                                      | 133.75                                | 103.67  | 159.35                              | 81.60                                 |
| 15                     | "                                   | 0.736  | 16.77                              | 4                                      | 141.75                                | 100.20  | 149.58                              | 78.68                                 |
| 14                     | 0.389                               | 0.700  | 17.10                              | 4                                      | 106.00                                | 96.17   | 140.73                              | 75.64                                 |
| 13                     | "                                   | 0.697  | 17.04                              | 3                                      | 113.33                                | 95.58   | 144.28                              | 78.30                                 |
| 12                     | "                                   | 0.685  | 17.11                              | 4                                      | 120.25                                | 94.22   | 144.91                              | 79.45                                 |
| 11                     | "                                   | 0.674  | 17.13                              | 4                                      | 125.25                                | 92.76   | 142.40                              | 79.21- $\frac{1}{2}$ gate             |
| 10                     | "                                   | 0.660  | 17.15                              | 4                                      | 130.00                                | 90.85   | 138.96                              | 78.83                                 |
| 9                      | "                                   | 0.646  | 17.20                              | 4                                      | 136.00                                | 89.10   | 134.26                              | 77.43                                 |
| 8                      | "                                   | 0.633  | 17.25                              | 4                                      | 144.50                                | 87.44   | 127.89                              | 74.94                                 |
| 7                      | 0.230                               | 0.530  | 17.42                              | 4                                      | 102.62                                | 73.51   | 100.61                              | 69.44                                 |
| 6                      | "                                   | 0.527  | 17.44                              | 4                                      | 108.50                                | 73.10   | 101.20                              | 70.16                                 |
| 5                      | "                                   | 0.520  | 17.48                              | 4                                      | 113.25                                | 72.27   | 100.23                              | 70.13                                 |
| 4                      | "                                   | 0.509  | 17.48                              | 4                                      | 121.00                                | 70.80   | 98.85                               | 70.60- $\frac{1}{2}$ gate             |
| 3                      | "                                   | 0.501  | 17.48                              | 4                                      | 128.75                                | 69.66   | 96.42                               | 69.99                                 |
| 2                      | "                                   | 0.494  | 17.51                              | 5                                      | 136.20                                | 68.73   | 92.73                               | 68.10                                 |

Tested at the HOLYOKE WATER POWER CO., July 14, 1894.

A. F. SICKMAN,  
Engineer in charge of Experiments.E. S. WATERS,  
Hydraulic Engineer.

We certify that the above is a correct copy of the original.

Received too late for publication in first part of book.

## NEW AMERICAN TURBINE

MANUFACTURED BY

GLOBE IRON WORKS, DAYTON, OHIO.

45 INCH RIGHT HAND WHEEL.

| No. of the Experiment. | Prop'l part of                      |  | Head acting on the Wheel. in feet. | Duration of the Experiment in Minutes. | Revolutions of the Wheel, per minute. | Quantity of water discharged by the Wheel, cubic feet per second. | Power developed by the Wheel, H. P. | Efficiency of the Wheel, in per cent. |
|------------------------|-------------------------------------|--|------------------------------------|--|---------------------------------------|---|-------------------------------------|---------------------------------------|
|                        | the full opening of the Speed-Gate, | the full discharge of the Wheel; being the discharge at full gate when giving best efficiency, |                                    |  |                                       |   |                                     |                                       |
|                        |                                     | in per cent.   |                                    |  |                                       |   |                                     |                                       |
| 37                     | 1.000                               | 1.022  | 15.98                              | 4                                      | 103.50                                | 144.87  | 205.05                              | 78.26                                 |
| 36                     | "                                   | 1.015  | 16.01                              | 4                                      | 107.50                                | 143.95  | 205.66                              | 78.84                                 |
| 35                     | "                                   | 1.009  | 16.02                              | 3                                      | 112.00                                | 143.17  | 206.64                              | 79.60                                 |
| 34                     | "                                   | 1.003  | 16.04                              | 4                                      | 115.37                                | 142.36  | 205.79                              | 79.63                                 |
| 33                     | "                                   | 0.997  | 16.06                              | 3                                      | 119.17                                | 141.58  | 205.27                              | 79.76-full gate                       |
| 32                     | "                                   | 0.990  | 16.09                              | 4                                      | 123.00                                | 140.77  | 203.49                              | 79.38                                 |
| 31                     | "                                   | 0.983  | 16.13                              | 4                                      | 127.75                                | 140.02  | 200.04                              | 78.26                                 |
| 30                     | 0.699                               | 0.921  | 16.30                              | 4                                      | 101.25                                | 131.77  | 195.08                              | 80.25                                 |
| 29                     | "                                   | 0.914  | 16.38                              | 4                                      | 105.75                                | 131.12  | 197.27                              | 81.15                                 |
| 28                     | "                                   | 0.905  | 16.40                              | 4                                      | 110.25                                | 129.93  | 198.16                              | 82.17                                 |
| 27                     | "                                   | 0.899  | 16.41                              | 4                                      | 113.87                                | 129.11  | 197.69                              | 82.44                                 |
| 26                     | "                                   | 0.893  | 16.42                              | 3                                      | 117.33                                | 128.35  | 196.51                              | 82.38                                 |
| 25                     | "                                   | 0.885  | 16.42                              | 4                                      | 122.00                                | 127.18  | 195.19                              | 82.58- $\frac{3}{8}$ gate             |
| 24                     | "                                   | 0.874  | 16.45                              | 4                                      | 127.50                                | 125.67  | 190.97                              | 81.62                                 |
| 23                     | "                                   | 0.856  | 16.53                              | 3                                      | 134.00                                | 123.42  | 182.46                              | 79.02                                 |
| 22                     | 0.505                               | 0.800  | 16.68                              | 4                                      | 102.00                                | 115.77  | 175.69                              | 80.39                                 |
| 21                     | "                                   | 0.796  | 16.71                              | 3                                      | 106.00                                | 115.29  | 176.81                              | 81.09                                 |
| 20                     | "                                   | 0.787  | 16.74                              | 4                                      | 110.75                                | 114.17  | 177.19                              | 81.92                                 |
| 19                     | "                                   | 0.775  | 16.78                              | 3                                      | 117.33                                | 112.60  | 175.74                              | 82.18- $\frac{3}{8}$ gate             |
| 18                     | "                                   | 0.762  | 16.81                              | 4                                      | 122.50                                | 110.81  | 170.97                              | 81.10                                 |
| 17                     | "                                   | 0.746  | 16.85                              | 5                                      | 127.40                                | 108.50  | 164.80                              | 79.64                                 |
| 16                     | "                                   | 0.725  | 16.86                              | 4                                      | 133.50                                | 105.56  | 154.51                              | 76.71                                 |
| 15                     | 0.382                               | 0.687  | 16.97                              | 4                                      | 101.25                                | 100.29  | 149.58                              | 77.66                                 |
| 14                     | "                                   | 0.681  | 17.00                              | 4                                      | 107.00                                | 99.50   | 150.79                              | 78.77                                 |
| 13                     | "                                   | 0.671  | 17.03                              | 3                                      | 111.83                                | 98.12   | 149.99                              | 79.31- $\frac{5}{8}$ gate             |
| 12                     | "                                   | 0.661  | 17.07                              | 4                                      | 116.00                                | 96.83   | 147.68                              | 78.94                                 |
| 11                     | "                                   | 0.651  | 17.11                              | 4                                      | 119.75                                | 95.48   | 144.30                              | 78.05                                 |
| 10                     | "                                   | 0.635  | 17.19                              | 4                                      | 127.50                                | 93.32   | 138.89                              | 76.50                                 |
| 8                      | 0.293                               | 0.584  | 16.84                              | 4                                      | 99.25                                 | 84.91   | 120.28                              | 74.32                                 |
| 7                      | "                                   | 0.579  | 16.83                              | 3                                      | 103.33                                | 84.27   | 120.30                              | 74.94                                 |
| 6                      | "                                   | 0.572  | 16.86                              | 3                                      | 108.00                                | 83.28   | 119.85                              | 75.42                                 |
| 5                      | "                                   | 0.563  | 16.88                              | 3                                      | 113.67                                | 82.07   | 118.40                              | 75.52- $\frac{1}{2}$ gate             |
| 4                      | "                                   | 0.553  | 16.90                              | 3                                      | 119.67                                | 80.54   | 114.06                              | 74.04                                 |
| 3                      | "                                   | 0.541  | 16.94                              | 4                                      | 127.00                                | 78.93   | 108.08                              | 71.42                                 |

Tested at the HOLYOKE WATER POWER CO., July 9, 1894.

A. F. SICKMAN,  
Engineer in charge of Experiments.E. S. WATERS,  
Hydraulic Engineer.

We certify that the above is a correct copy of the original.

Received too late for publication in first part of book.

## CONCLUSION.

For more than a quarter of a century past my efforts to produce plans and instruments necessary to make milling hydrodynamics a science have been unceasing, and I write this in perfect confidence that this work contains all the information requisite to make it so; but a far more intelligent and practical class of engineers is needed in future to aid the manufacturer than has been turned out by the colleges and technical schools in the past, and if those institutions cannot come up to the times it is pretty evident that the workshop will supply the want.

Twenty years ago my plans were objected to by lawyers and engineers because of their simplicity, which would leave the whole open to the understanding of people of ordinary intelligence and injure those professions. Where there were twenty cases of hydraulic litigation in contemplation then there is hardly one now.

Milling and turbine matters have now become so well established in fixed lines that were this work confined to such matters alone it is doubtful if twenty copies a year would be called for, and those as works of reference as occasion required by the comparatively few interested in such matters. My purpose is to make it interesting to all and thus generally useful. The world is in the throes of a revolution that shocks the minds of those calmly reposing in conventionalities as teeming with corruption as were the old pest pits after the depopulation of a city. "Moths," "Is this Your Son, my Lord?" and "The Heavenly Twins," have sadly disturbed pseudo-modesty, that smilingly associates with the Breckenridge conventionalism, having the slightest ostrich style of concealment. Prurient modesty raves against nude forms, but why, if they are the Creator's most perfect work? "*Who told thee that thou wast naked?*" The more of the person exposed the better it is likely to be cared for. Would the feet of our women have been so generally distorted had they been kept constantly in sight? Is this distortion less barbaric than the compression of the feet of the Chinese?

Paintings, engravings, and medical illustrations of the human system have been common in my family, yet I have never noticed one of my children telling or listening to a lewd story, often so slyly and smilingly told in places of resort; indeed, I doubt whether they would see the point in it. The old heathen sacrificial idea of blood, even the blood of Christ, is out of date, is superstitious rot, and disgustingly filthy to the intelligent thinker, who will believe it more useful to labor for the love, elevation, and universal brotherhood of man, and in that way glorify his Creator.

No one yet has intimated that anything published here is incorrect, but several as a matter of policy have advised less openness. I know of no implied desire of nature or the Creator for concealment. On the contrary, open ventilation is the most perfect means for purification.

THE AUTHOR.

## Tests of Water Wheels and Machinery

DESIGNED TO AID ALL INTERESTED IN HYDRAULICS,  
Particularly Turbine Builders, Manufacturers, Owners  
of Water Power, and Counsel Managing  
Cases in Litigation.

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### TESTIMONIALS.

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OFFICE OF THE  
PROPRIETOR OF THE LOCKS AND CANALS ON THE MERRIMAC RIVER,  
LOWELL, MASS., February 5, 1879.

JAMES EMERSON, Willimansett, Mass.

Dear Sir: Your work on water wheels and machinery was left here yesterday by Mr. Swain.

My father (James B. Francis) is at present in Europe, and probably will not return before next August. I take the liberty to thank you for him, and to assure you that your book contains a fund of information of the kind we want. How to utilize water power to the best advantage is one of the great problems of the day, and I am sure you have contributed much information on the subject.

Very truly yours,

JAMES FRANCIS, *Ass't Engineer.*

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NORTH CHELMSFORD, MASS., February 7, 1879.

JAMES EMERSON, Willimansett, Mass.

Dear Sir: I have examined your book, "Treatise on Tests of Water Wheels and Machinery," and find in it a very large amount of valuable information, in a simple form, not obtainable in any other work. I have copies, in full, of all your tests, dating back nearly ten years, prepared at (to me) great expense, and of course I have faith in their reliability. (At all events, twenty times their cost would not buy them, were no other copy available.) The publication of your experience, in so convenient a form, must prove to be of very great benefit to manufacturers, turbine builders, and such of the legal fraternity as have hydraulic cases to manage. Every millwright ought certainly to possess a copy. The tables of "Velocities due Head," alone, will save him in time every year several times the cost of the book.

Very truly yours,

A. M. SWAIN.

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BOND BROS. & BOTTUM LAW OFFICE,  
NORTHAMPTON, February 7, 1879.

JAMES EMERSON, Holyoke, Mass.

Dear Sir: I have examined your work on "The Testing of Water Wheels and Machinery," *with matters pertaining to Hydraulics* (2d Ed. 1878), and find that it contains in a very convenient form a large amount of information which every lawyer must obtain from some source before he can safely advise a client or properly try a case concerning water power or the power of water wheels. Accept my thanks for your treatise; it will be of great use to me in my professional work.

Yours truly,

D. W. BOND, *District Attorney.*



LAW OFFICE,  
NEW HARTFORD, CONN., February 8, 1879.

JAMES EMERSON:

Dear Sir: I have examined your book, "Treatise on Tests of Water Wheels, &c.," and find it to be really *multum in parvo*. It contains in simple form much information needed by members of the legal profession who are engaged in suits involving hydraulics, power, flow of water, and kindred subjects.

I am very truly yours,

JARED B. FOSTER.

LAW OFFICE OF J. P. BUCKLAND, COUNSELOR IN PATENT CAUSES,  
SPRINGFIELD, MASS., February 8, 1879.

JAMES EMERSON:

Dear Sir: I assure you that my examination of your new work, entitled "Tests of Water Wheels and Machinery," has given me a great deal of pleasure. Many a time have I searched for hours to find some of the many data with which the book is crowded.

In the preparation and trial of cases involving questions of water power, mill-rights, leases of power and the performance of machines built under contract, and kindred matters which are constantly coming before courts and arbitrators for settlement, your work will be a valuable aid to lawyers and parties. I know of no single book which has within its covers so many practical data for use in the above line of cases, and I am bound to say that I think the legal profession is under much obligation to you for the preparation of it.

Yours truly,

J. P. BUCKLAND.

SENATE CHAMBER, WASHINGTON, D. C., February 9, 1879.

JAMES EMERSON:

My Dear Sir: Permit me to thank you for a copy of your book, "Tests of Water Wheels and Machinery." I have read it with as much care as I could find time from my official duties here to do, and have no hesitancy in saying that it must prove a very valuable work, as well to lawyers conducting litigations, as to mill owners seeking to avoid them.

Thanking you again, I am, truly yours

H. I. DAWES.

PITTSFIELD, NOV. 24, 1892.

JAMES EMERSON:

Dear Sir:—Please accept my thanks for a copy of the fourth edition of your *Hydrodynamics*. I am very much pleased with it. All that I said of the first edition that you sent to me has proved true and much more, and I am sure it has been improved in this edition.

I am truly yours,

H. L. DAWES.

BOOTT COTTON MILLS, LOWELL, MASS., March 11, 1879.

JAMES EMERSON:

DEAR SIR: Permit me to thank you for a copy of your "Tests of Water Wheels and Machinery." I have examined the same with great care and must say that you have given a fund of information to Manufacturers, Turbine Builders, Owners of Water Power, and the Legal Profession who have suits involving Hydraulics, in a most simple and concise form. There is no subject to-day connected with manufacturing that there is so much ignorance about as the economical use of water power, best wheels, and appurtenances to utilize it. Your book cannot fail to have a large sale, as you have contributed so much information on the subject.

Yours truly,

A. G. CUMNOCK, Agent.

NEW HAVEN, CONN., April 29, 1879.

MR. JAMES EMERSON:

DEAR SIR,—Allow me to take this opportunity to thank you for the copy of your Treatise relative to the Testing of Water Wheels and Machinery, which you did me the favor to send me some time since. I have found it to be a mine of valuable information, and have often had occasion to consult it. It certainly effectively supplies a great desideratum. The manufacturing interests of this country owe you a debt of gratitude, to speak of nothing more, for the valuable work you have done in testing water wheels and machinery.

Yours truly,

W. A. NORTON,

*Prof. of Civil Engineering in Sheffield Scientific School.*

LEBANON, N. H., March 7, 1879.

JAMES EMERSON: I will do all I can to recommend your book. I think it the best book I have seen for a millwright.

Yours truly,

WILLIAM DUNCAN, *Engineer and Millwright.*

UNITED STATES SENATE CHAMBER, WASHINGTON, Feb. 1, 1879.

JAMES EMERSON:

DEAR SIR: Yours of the 30th ult. has just been received, with your book, for which I heartily thank you. Of course, I have not yet had time to examine it, but will do so and write you about it. I think from a hasty glance I cast over it, that its contents will be of value, and I shall preserve it as a memento of one of the intelligent patentees of the country, who have done so much for its interests.

Yours truly,

BAINBRIDGE WADLEIGH.

HARTFORD, CONN., Oct. 28, 1892.

MR. JAMES EMERSON:

*Dear Sir:*—I received the copy of your book on Hydrodynamics and am much obliged for it. In the intervals between business occupations I have read it all through, and am much pleased with it—at least so far as it refers to its subject—although I do not agree with you in all your views on other subjects. Much of what you say about law and lawyers is correct, though you have rather picked out its defects than mentioned its benefits. It is by no means perfect, especially in its practice, but it would be hard to get along without it.

Yours truly,

C. E. PERKINS.

Of course it is the *defects* of the jargon called *law* to which I object, certainly to no sensible rule of action.

An aspirant to leadership of public opinion could hardly feel himself a success if his ideas were generally accepted as soon as uttered; he looks ahead for appreciation.

Yet, if Mr. Perkins will examine his differing beliefs as keenly as I many times have heard him draw the facts from a reluctant witness he may find them based upon muddy foundations.

THAYER SCHOOL OF CIVIL ENGINEERING.

*Dartmouth College,*

HANOVER, N. H., August 22, 1879.

JAMES EMERSON.

*Dear Sir:* Permit me to say that your book on Tests of Water Wheels and Machinery has greatly interested me. To students of hydraulics it has a special value in affording so many practical results of American construction and opera-

tion, and forming a very desirable supplement to more exclusively theoretical works. Your methods and results cannot fail to be instructive even to those not yet engaged in the actual practice.

Very truly yours,

ROBERT FLETCHER, *Thayer Prof. of Civil Eng.*

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STEVENS INSTITUTE OF TECHNOLOGY.

*Department of Engineering,*

HOBOKEN, N. J., October 12, 1880.

JAMES EMERSON.

*My Dear Sir:* Thanks for your note of the 11th inst. I wish to thank you for the copy of the book on Water Wheel Tests. I have just finished looking it through, from cover to cover, and consider it a very valuable addition to my library; it supplies a want which can be filled by no text-book or treatise that I have met with, by giving the actual value of the wheels daily sold in our market. I am pleased to see that makers are bringing up their efficiency finely, and that 80 per cent. is getting to be as usual with our best wheels as 70 per cent. was a little time ago.

Very truly yours,

R. H. THURSTON, *Prof. Civil Eng.*

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STEVENS INSTITUTE OF TECHNOLOGY.

*Department of Engineering,*

HOBOKEN, N. J., October 16, 1880.

JAMES EMERSON.

*My Dear Sir:* Thanks for the proofs (Holyoke Hydrodynamic Experiments) just received. I have looked them through before sitting down to acknowledge receipt. They are full of information as is an egg with meat. I am very greatly obliged.

R. H. THURSTON, *Prof. Civil Eng.*

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LEIPZIG, GERMANY, Sept. 1, 1892.

MY GOOD FRIEND EMERSON:

Your book "Hydrodynamics" reached here the 24th ult., and my wife and self have given it a thorough perusal. It is solid with much needed information; it should meet with universal welcome, but my wife offers the following lines as her idea of how philanthropic intentions are usually met. Her English is not so perfect as she could desire, but she hopes to be understood.

"Oh sir, your "Hydrodynamics," your unequaled car steam heat, Labor saving capstan windlass, and duplex piano seats, Scales for power measuring, with registering counter so neat, Brake and gauges for turbine testing, hydro systems so complete,— Conspicuous above all others, may stand unequaled and alone Yet, to disinthrall your human brothers from the bigot's crushing zone. Ah, for that no benefit from science has ever yet atoned."

To which I add:—

The party politician, if you object to his selfish plans,  
Will clasp hands with the scheming clergy to have your soul and body damned.

Ever sincerely yours,

PROF. CARL VON BERGH.

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WILLIMANTIC, CONN., Aug. 9, 1892.

MR. JAMES EMERSON.

*Dear Sir:* Your book was received in due season and please accept our heartfelt thanks. Even the writer, or, would say, clerk, enjoys it very much. Mr. S. C. Smith wishes me to ask you to send another with bill, and we will give you prompt attention. You may send it in care of Water Works.

Very respectfully,

WILLIMANTIC WATER COMMISSIONERS.

WILLIMANTIC, CONN., Aug. 12, 1892.

MR. JAMES EMERSON.

*Dear Sir:*—I am happy to write to give you my heartfelt thanks for the book you so kindly remembered me with. Your note says, "return for kindness." I wonder if we didn't in our everyday walks do some little deed what enjoyment would we get out of life? And it bewilders me to try and recall any such act during your stop in Willimantic. However, I hope you will accept my feeble thanks for your works, that will live long after you have passed over.

Very truly yours,  
HENRIETTA McCULLOCK.

LOWELL, MASS.

JAMES EMERSON.

*My Dear Sir:*—I received yesterday a copy of 4th edition of "Hydrodynamics," etc., containing portrait of the distinguished author.

It has been so long since I had heard from you that I have been fearing that you had gone to join the great majority on the other side of the dark river. Had that been the case, I feel that it would not have been a total loss to the world, however; as I am confident that, when you get there, you will hustle around among the ghosts until you have established a more practical and trustworthy means of communicating with those yet left on this side.

In looking through the book I find that you have added much new matter of an interesting character.

The illustrated Scripture texts are of especial interest and very suggestive.

But, viewed from the standpoint of the orthodox church, you are evidently a very wicked man.

The book contains so much that is outside of the original design that the title is not just right, I think. It should be "EMERSONIA."

There is but one James Emerson (that I know of), and he is getting old, more's the pity. (I may have said this before, but it is as true as, or more true than, ever before.)

Yours truly,  
HAMILTON J. SAWYER.

JAMES EMERSON:—Your very handsomely gotten up book with its pretty compliment on the cover to Helen Gardener reached her two days ago. It is a great help to a worker in a new or radical field to have the kindly and warm support of friends who are known to one only by these acts which show the interest they take in what one does. She thanks you most sincerely and hopes that she may infer from what you have sent that some of her work has given you pleasure.

She is not "much on water-wheels," or, indeed, on machinery generally, but she has looked over the book enough to see that you have not confined yourself to the stricter requirements of "mechanics," and that you are far from orthodox even where you do. She read some of your short talks on Spiritualism, and while she has not seen the things of which you write—and would like to have the chance—she recognizes most fully that there is so much yet to be learned on all such subjects that she can only listen and wait.

Many of her friends are of your way of thinking, and they tell her that she is an "inspirational writer," particularly because her best work is often done with the least effort and in the shortest time. She has no recognition of "inspirational" influence, however.

She was more than glad to see that you did not forget—and was not afraid—to give to a woman the credit for your mathematical work. That, as you know, has not been the fashion. She is greatly pleased with the book, and by the spirit and thought which prompted you to send it. She thanks you for it most heartily.

Yours, very sincerely,  
HELEN H. GARDENER, per L. A.

We have received a copy of the "Treatise relative to the testing of water wheels and machinery, also of inventions, studies, and experiments, with suggestions from a life's experience, by James Emerson, Willimansett, Mass., fourth edition, price one dollar, and postage ten cents." The book contains 480 pages, and is a perfect mine of modern knowledge gained by practical experience of water, water ways, water wheels, rivers, canals, and laws relating thereto. In fact, there is hardly a question relating to water or power that the book does not handle clearly. The author seems to be a man that loves his fellow-man, and it is quite evident that society is not Mr. Emerson's god; he is a man of deep knowledge, as will be found by the papers sandwiched all through the book. He handles antiquated water wheels and worn-out theological dogmas without gloves. Send \$1.10 for the book.

WADE'S FIBRE & FABRIC CO.

LOWELL, MASS., Aug. 19.

The Library Committee of the Middlesex Mechanics' Association gratefully acknowledge the gift of "Treatise relative to the testing of water wheels and machinery."

A. L. SARGENT, *Librarian.*

Many, many thanks, friend Emerson, for your book;  
 Its contents I have read o'er and o'er.  
 Brother Seventeenthly, with sardonic look,  
 Says you will suffer for it on arrival at Andover's back door.  
 But with contemptuous look at their pale roasts  
 As you scan their sulphurous demesnes  
 I am sure you will suggest to the cleft-foot host  
 That more equable temperature can be kept up by steam.

Yours truly,

Springfield, Mass., Sept, 9, 1892.

DELOS SMITH.

WORLD'S COLUMBIAN EXPOSITION.

CHICAGO, ILL., April 21, 1892.

MR. JAMES EMERSON, HOLYOKE, MASS.

*Dear Sir:* Will you please forward to me a copy of the Holyoke Testing Flume Record of Turbine Wheels and inform me of the price, and I will remit on receipt of the book. If not convenient for you to do so, will you inform me where I can obtain a copy and oblige,

Yours truly,

L. W. ROBINSON, *Chief Dept. Machinery.*

CHICAGO, ILL., August 5, 1892.

MR. JAMES EMERSON, WILLIMANSETT, MASS.

*Dear Sir:* The two copies of your book are received, for which accept my thanks. The information relating to the testing of turbines and some other engineering subjects will be useful and interesting. That in reference to the Bible and ancient history is amusing, if not useful.

Yours truly,

L. W. ROBINSON, *Chief Dept. Machinery.*

*Lowell Daily Mail.—Republican.*

NEW EDITION OF A WORK ON WATER-POWER, WATER-WHEELS, AND MACHINERY.

James Emerson, of Willimansett, Mass., has recently issued a fourth edition of his "Treatise on the Testing of Water Wheels and Machinery," nearly five hundred pages. It gives the results of the author's numerous tests of water-wheels, his inventions, studies, and experiments during the past thirty-five years or more. Practical men—engineers, millwrights, and others interested in water-power—have spoken in terms of warmest commendation concerning the earlier editions of this book. Mr. Emerson's long experience in testing wheels, his thorough knowledge of hydrodynamics, and the best facilities for a practical application of his knowledge



and skill, have undoubtedly thoroughly qualified him for the preparation of a comprehensive and useful work of this character. To one at all interested in the subjects he discusses, the volume, we should suppose, would be invaluable. The story of his invention and experience in attempting to introduce a ship-windlass is as interesting as romance. He tells of his invention and experience with a car-heating appliance. The invention of the power scales for ascertaining the amount of power required in the operation of any kind of machinery, as well as other inventions of the author, are described in the printed page with illustrations.

But he bears down hardest on the Bible and Christianity, and criticises (in his own way) the most objectionable passages in the Old Testament, and then asks mothers (as if the book was prepared for women and children)\* if they "can desire their children to accept such filth as from the creator of this beautiful world."

Mr. Emerson disposes of the liquor question, and Rev. Dr. Miner, and his prohibitory principles in fifteen lines. He discusses the tariff question from a free-trade standpoint. He holds Shakespeare's writings in contempt and plainly says that those who assume to admire them are dissemblers. He also goes for the Republican party, and says that "from the beginning it has been honeycombed with corruption." He must needs go back to Constantine (who was born in the year 272, and did things according to the light he had) and expose his shortcomings. He deals flippantly with the myths and superstitions of prehistoric times, burlesques modern preachers and their audiences, accuses prominent New York clergymen of laboring for notoriety rather than for the benefit of their fellow-men; and after ridiculing and discrediting Christianity asks, "In all seriousness, What good has Christianity ever done?" Mr. Emerson devotes thirty odd pages to Spiritualism and kindred subjects, to which he has for many years given much study.

Mr. Emerson knows something about the north pole and suggests a means of getting there. If the world gets in these latest pages of his literary work the best he is capable of rendering it, he cannot do better than set out for that undiscovered country, and try his theories as he progresses.

\* Partisan blindness caused the writer to overlook the fact that nearly all business concerns now employ women in office or works.

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KEENE, N. H., Sept. 20, 1892.

MR. EMERSON:

I have studied fourth edition of your "Hydrodynamics, etc.," with deep interest.

You certainly have carried out your announced intention of interesting anyone looking it through.

Wrong or impurity are none the less so though concealed; shoving the bed of a just deceased smallpox patient into a dark closet does not purify it for another sleeper. Bringing abuses to the light is a preliminary step to their abolition.

Yours truly,

Mrs. E. W. WHITTIER.

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"ST. JOHN'S WOOD," LONDON, ENG., Sept. 2, 1892.

MR. EMERSON:

My friend Mrs. Erskins called my attention to the fourth edition of your "Hydrodynamics."

That an author of scientific standing should have the courage to mix in with such positive evidence of his ability, subjects sure to raise the ire of the bigoted and superstitious, is to me a matter of surprise and admiration. On page 377 of your book, you truly say that no other cause has ever produced such incalculable misery to the human race as the woeful dogmas there referred to, and by which woman, being the most devotional, has suffered most. No philanthropic effort can ever exceed in useful effect that which frees humanity from the bondage of religious superstition. Our increasing freedom is gained not by the aid of Christianity but in spite thereof.

Yours very truly,

Mrs. ELIZABETH SELBRIDGE.

I would be proud to call you friend and brother.

ITHACA, N. Y., Sept. 22, 1892.

TO MR. JAMES EMERSON, *Willimansett, Mass.*:

*My dear Mr. Emerson: Yours of the 10th is received. In reply I would say:*

*The book has also arrived and I have looked it through carefully. I am glad to get the facts and data, in which I have great confidence, and wish we had still more of the same sort.*

*I am glad to see your tribute to the young lady who was so valuable an assistant to you. I remember her well, and remember equally well the pleasure it gave me to see, long before woman was as well received in business affairs as to-day, that you gave her full credit for her good work, and paid her like a man.*

Yours truly,

R. H. THURSTON.

POUGHKEEPSIE, N. Y., November 2, 1892.

Vassar College library has received from Mr. James Emerson, "Treatise Relative to the Testing of Water Wheels and Machinery," by James Emerson. The gift is hereby gratefully acknowledged.

F. A. WOOD, Librarian.

DEPARTMENT OF THE INTERIOR,  
BUREAU OF EDUCATION, WASHINGTON, D. C., Oct. 15, 1892.

MR. JAMES EMERSON, WILLIMANSETT, MASS.:

*Sir:—*Permit me to acknowledge, with thanks, the receipt from you of the publication "Treatise Relative to the Testing of Water Wheels and Machinery," by James Emerson. It will be deposited for use and reference in the library of the Bureau, and a record will be made of the name of the donor.

Very respectfully,

W. T. HARRIS, Commissioner.

PLATTSBURGH, N. Y., Sept. 10, 1892.

MR. EMERSON:

I received the copy of fourth edition of "Hydrodynamics" with pleasure.

The following figures, taken from a daily of recent date, placed in connection with the illustration in your book, page 126, are suggestive to mothers:—

|           | <i>Births in Year.</i> | <i>Legitimate Births.</i> | <i>Illegitimate Births.</i> | <i>Per cent. of Illegitimacy.</i> |
|-----------|------------------------|---------------------------|-----------------------------|-----------------------------------|
| London,   | 78,300                 | 75,097                    | 3,203                       | 4 per cent.                       |
| Paris,    | 29,628                 | 19,921                    | 9,707                       | 33½ "                             |
| Brussels, | 5,281                  | 3,448                     | 1,833                       | 35 "                              |
| Munich,   | 3,464                  | 1,762                     | 1,702                       | 48 "                              |
| Vienna,   | 19,241                 | 8,881                     | 10,360                      | 52 "                              |
| Rome,     | 4,373                  |                           |                             |                                   |

Foundlings exposed in one year in Rome, 3,190; nearly three-fourths, or 73 per cent. of the births.

Yours truly,

Mrs. KATIE WINANS.

WILLIMANSETT, MASS., Aug. 28, 1892.

MR. EMERSON:

Many thanks for the book, it has interested me much. The constant immigration of the most ignorant and superstitious class of foreigners, a class that has never been allowed to take part in its own government, nor had sufficient intelligence to learn anything of ours, threatens our institutions and people with dangers that loom plainly in the not distant future.

If Spiritualism, as you seem to think, has a tendency to broaden the understanding, then you do well to give it scientific attention.

Truly your friend,

Mrs. C. T. INGHAM.

SPRINGFIELD, MASS., Sept. 9, 1892.

MR. EMERSON:

The copy of your "Hydrodynamics" was received some days since, for which accept many thanks.

Only the blindness caused by superstition and bigotry can prevent the intelligent from seeing the danger to our schools and country that looms up in the near future from the avalanche of immigration made up of the most ignorant and superstitious, a class that has never known forbearance or mercy.

Your illustration, page 127, is very timely, appropriate, and suggestive.

Sincerely yours,

L. L. DAVIS.

COATESVILLE, PA., Aug. 19, 1892.

MR. JOHN B. McCORMICK, Holyoke, Mass.

Dear Sir: I wish to thank you for sending me the last edition of Emerson's book, which is just at hand. It was very kind of you and I appreciate it very much. I have all the other editions, and nearly know them by heart, and I have no doubt I shall be equally interested in this.

WM. H. RIDGWAY.

IMPERIAL UNIVERSITY AND LIBRARY,  
STRASBURG, GERMANY, Nov. 15, 1892.

MR. JAMES EMERSON, WILLIMANSETT, MASS., U. S.:

Honored Sir:—I have been honored by receiving for our Library a present or sample of your works, "Treatise Relative to the Testing of Water Wheels and Machinery," 1892. Please accept herewith my hearty thanks. Allow me to assure you of my greatest respect.

The Librarian, BARACK.

GRAND DUCAL TECHNICAL HIGH SCHOOL,  
DARMSTADT, GERMANY, Dec. 29, 1892.

MR. JAMES EMERSON, WILLIMANSETT, MASS.:

Dear Sir:—We have the honor to notice the receipt of your gift to our high school, "Treatise Relative to the Testing of Water Wheels and Machinery," fourth edition, 1892, and to notify you that the book has been turned over to Prof. Stribeck of the department of machinery. Thanking you in the name of the directors of the Technical High School.

Very truly yours,

LANDSBERG.

SMITHSONIAN INSTITUTION, WASHINGTON, D. C., October 28, 1892.

The Smithsonian Institution has received from James Emerson, Willimansett, Mass., "Treatise Relative to the Testing of Water Wheels and Machinery," a gift for which it returns its grateful acknowledgment.

S. P. LANGLEY, Secretary Smithsonian Institution.

*Holyoke Daily Democrat*,—Priest-ridden,—Saturday, Aug. 20, 1892.

MR. EMERSON'S BOOK. HE'S DOWN ON THE BIBLE, LAW, MEDICINE, AND POPULAR CHRISTIANITY.

The great and only James Emerson has just got out the fourth edition of "Emerson's Hydrodynamics, etc.," a small and compact volume of 500 pages, with great additions to preceding editions.

Mr. Emerson is certainly a genius and the most original man in the world. His book proves it.

He was born up New Hampshire way. He never had much schooling, and did not want any.

At 19 he was the mate of a seagoing vessel. He was a sailor for 10 years, and what he hasn't done since then could be told in a hundred words.

What Mr. Emerson doesn't know about hydrodynamics hardly anybody knows, he thinks.

Mr. Emerson is down on the law. He says it's antagonistic to knowledge and justice. He prints a page of pictures to prove it, and defines it as "the study of untold centuries to enable influential rascals to escape responsibility." "Will it never be understood," asks he, "that the law was made for the benefit of man and not man for the law?"

Mr. Emerson is also down on the Bible. He thinks that, and the Arabian Nights, and the classics teach liberal lessons to the youth of this country. In this connection Mr. Emerson publishes a number of things taken from the Bible. He makes it out to be very inconsistent.

He is an ardent Spiritualist, although down on the Bible. The last portion of his work is devoted to his experiences for years past, and some of his stories are decidedly ghostly. He has had experiences with all the mediums and spook priestesses, many of whom the world regards as fakirs.

Some of the newspapers that are getting hold of Mr. Emerson's book are raking it through and through, and abusing the author roundly. Mr. Emerson moves on serenely.

Probably a copy of the Holyoke *Democrat* was never seen a mile from its place of publication unless, perhaps, when used as a wrapper for some workingman's overalls, but unfortunately it is the same in style as the so-called democratic papers of larger circulation, papers that give more flaring headlines to the movements of prize fighters and baseball games than to those of our statesmen.

Horace Greeley, with his *Tribune*, made public opinion. The papers of to-day simply pander to the fancies of the ignorant masses. Statesmanship with either party consists in efforts to retain or obtain the spoils of office.

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LEBANON, N. H., Sept. 24, 1892.

MR. EMERSON:

Your "Hydrodynamics, etc.," surprises me. To sandwich such irrelevant subjects as you have into a work of universally acknowledged scientific value has the merit of novelty at least, and is likely to cause investigation by the intelligent.

Mrs. LUCY EMERSON, 84 years of age last Feb. 8.

---

LEBANON, N. H., Sept. 26, 1892.

MR. EMERSON:

I have scanned the pages of your "Hydrodynamics, etc.," and think womankind deeply indebted to you for the stand you have so courageously taken therein.

Mrs. HELEN J. ROWELL.

---

PORTLAND, MAINE, Sept. 9, 1892.

MR. EMERSON:

Many, many thanks for the copy of latest edition of "Hydrodynamics, etc." It is rich with progressive mental food.

Truly your friend,

Mrs. ERNEST FIELDING.

MR. EMERSON:

*Dear Sir:*—I am visiting my Grampa Foster, and saw the beautiful book which you so kindly sent my Grama, and I thought I should like to have a copy for my own pleasure and to take the same home to my papa, which I am sure would be very interesting and perhaps of more real value to him than to me. I hope you won't think I am asking too much from a person whom I have not had the pleasure of meeting, but your book is so interesting; I am perhaps overbold and you will excuse me for my action. I wanted Grama to give me her book which you sent her, and she said, No, I want it myself. I said I would write myself and she said all right. I am ten years old, and my name is

WINNIE LEWIS LAWSON.

I am stopping with my Grama and Grampa Foster at 13 Sixth St., Lowell, Mass.

The author sends Winnie many thanks with book.

THEOLOGICAL SEMINARY, ANDOVER, November 15, 1892.

The Trustees of Phillips Academy, in Andover, Massachusetts, have received from Mr. James Emerson, as a gift to the library of the Theological Seminary, his "Treatise Relative to the Testing of Water Wheels and Machinery, etc., 1892," for which the Trustees return their grateful acknowledgments.

In behalf of the Trustees,

CECIL F. P. BANCROFT, Clerk.

W. L. ROPES, Librarian.

JOHNS HOPKINS UNIVERSITY, BALTIMORE, MD., November 10, 1892.

MR. JAMES EMERSON, WILLIMANSETT, MASS.

*Sir:*—I beg to acknowledge, with thanks, your gift to this library of the fourth edition of your "Treatise Relative to the Testing of Water Wheels and Machinery, also of Inventions, Studies and Experiments, with Suggestions from a Life's Experience. Willimansett, Mass., 1892."

N. MURRAY, Librarian.

UNIVERSITY LIBRARY, GLASGOW, Oct. 28, 1892.

The University of Glasgow gratefully acknowledges the receipt of "Treatise Relative to the Testing of Water Wheels and Machinery." The book has been deposited in the library and entered in the catalogue of donations.

JAMES LYMBURN, Librarian.

CARLUKE, SCOTLAND, Dec. 1, 1892.

MR. EMERSON:

*Dear Sir:*—Have received your book on Hydrodynamics from my brother in Holyoke. If it was the purpose to cause those who examine the fourth edition of your Hydrodynamics to think, then, indeed, your various illustrations and remarks seem admirably adapted to that effect. Truth or the right can never be injured by being held up to the light. The illustrations on pages 122-3 present object lessons more practical and eloquent than all the sermons delivered from John Knox down to Sam Jones. As mechanics and human beings we thank you sincerely for the stand you have taken.

Yours truly,

JAMES MUNSIE, Mining Engineer.

ROSE POLYTECHNIC INSTITUTE, TERRE HAUTE, IND., Nov. 29, 1892.

The library of the Rose Polytechnic Institute gratefully acknowledges the receipt of Emerson's Hydrodynamics, etc.

Very truly,

S. P. BURTON, Reg.

MASSACHUSETTS INSTITUTE OF TECHNOLOGY, BOSTON, Oct. 20, 1892.

*Dear Sir:*—I beg to acknowledge the receipt of "Treatise Relative to the Testing of Water Wheels and Machinery, etc.," by James Emerson, and to express my recognition of your kindness in sending it.

Respectfully yours,

CLEMENT W. ANDREWS, Librarian.



UNIVERSITY LIBRARY, CAMBRIDGE, ENGLAND,  
April 6, 1893.

Sir:— I have the honor to acknowledge the receipt of the work mentioned within which you have been good enough to send as a present to the Library, and to convey to you on behalf of the Library Syndicate the best thanks of the university for this addition to our collection.

Your most obedient servant,

FRANCIS JENKINSON,  
*Librarian.*

TO JAMES EMERSON, ESQ.

Emerson (James). Treatise relative to the testing of water wheels and machinery. Fifth edition, 8vo, 1893.

UNIVERSITY LIBRARY, UPSALA, SWEDEN.

Dear Sir:—I beg you to accept the best thanks of the university, and of myself, for the undermentioned work which you have been so kind as to present to the library of the university.

Treatise relative to the testing of water wheels and machinery, by James Emerson, 1893, 8vo.

I have the honor to be, sir,

Your obedient servant,

CLAES ANNERSTEDT,  
*Librarian of the University.*

UPSALA, April 19, 1893.

BODLEIAN LIBRARY, OXFORD, ENGLAND,  
March 17, 1893.

Dear Sir:—I beg you to accept the best thanks of the curators of the Bodleian, and of myself, for the \* undermentioned work, by yourself, which you have been so kind as to present to the library of the university.

Yours very faithfully,

EDWARD W. B. NICHOLSON,  
*Librarian.*

\* Treatise relative to the testing of water wheels and machinery. Fifth edition.

J. EMERSON, ESQ.

LOWELL, MASS., April 11, 1893.

JAMES EMERSON, Willimansett, Mass.

Dear Sir:—Your valuable and very interesting book came duly to hand and would have been acknowledged before but it has just been brought to my notice. I have read some of it, and shall do so fully as I get time. I thank you very much for the present, and shall always guard it for its value, and as a reminder of the pleasant days I have spent with you.

Very truly yours,

D. W. C. FARRINGTON.

Letters of the character of that of Mr. Farrington are the bright spots of an inventor's life, a life far from being all sunshine, yet it has many compensations for its years of anxious anticipations. Numerous letters have been received, which, with but few exceptions, are commendatory to my works, many from persons of high standing, but too lengthy for publication. Intelligent criticism is still desired. Before this meets the eye of the reader, the author will have passed his seventy-second milestone on the way to the spirit land, where may all find as happy welcome as that described in Mrs. Oliphant's "Little Pilgrim."

## PETITION TO THE LEGISLATURE, 1896.



The *Freethinker* of London, England, contains the following: "Christian Life gives the following figures: In the common goals of Ontario (Canada) 11,810 persons were locked up last year. No less than 2,448 were unable to read or write." The religious denominations were represented as above. Will the clergy of this country use their influence to procure similar information from our prisons, that the influence of the various religions upon the morals of the masses may be ascertained? Come, brother Talmage, will you try?

### Statistics relative to Morals in Countries where Church and State are united.

|           | Births in Year. | Legitimate Births. | Illegitimate Births. | Per cent. of Illegitimacy. |
|-----------|-----------------|--------------------|----------------------|----------------------------|
| London,   | 78,300          | 75,097             | 3,203                | 4 per cent.                |
| Paris,    | 29,628          | 19,921             | 9,707                | 33 1/2 "                   |
| Brussels, | 5,281           | 3,448              | 1,833                | 35 "                       |
| Munich,   | 3,464           | 1,782              | 1,702                | 48 "                       |
| Vienna,   | 19,241          | 8,881              | 10,360               | 52 "                       |
| Rome,     | 4,373           |                    |                      |                            |

Foundlings exposed in one year in Rome, 3,190; nearly three-fourths, or 73 per cent. of the births.

### DEPARTMENT OF THE INTERIOR.—CENSUS OFFICE.

PLAINFIELD, N. J., November 18, 1892.

MR. JAMES EMERSON, Willimansett, Mass.

Dear Sir: In response to one of the questions addressed by you to the Secretary of the Interior, I beg to say that the valuation of property in church buildings, including the sites on which they stand and their furniture, is \$680,087,000. Very respectfully,

H. K. CARROLL,

Special Agent Eleventh Census

### THE FOLLOWING WILL EXPLAIN ITSELF:

WILLIMANSETT, MASS., October 13, 1892.

REVEREND DR. MINER, Boston, Mass.:—

Dear Sir:—This day I have mailed you a book. Upon page 126 thereof you may find a plan for obtaining the moral influence of the various religions upon the masses.

Arrangements are being made to petition the Legislature of this State to have the religious belief of each prisoner reported. Will you use your influence in favor of having the plan carried out? His reply is below.—

528 Columbus Avenue, Boston, Oct. 21, 1892.

Dear Sir:—The suggestion is a good one. It would let light into dark places.

Yours truly,

A. A. MINER.

The same request was made to Talmage, Parkhurst, and others, none of whom have made any reply.

JAMES EMERSON.

To the Honorable Senate and House of Representatives of the Commonwealth of Massachusetts:—

GENTLEMEN—We, your petitioners, most respectfully represent that, as shown above, Immense wealth that escapes taxation is locked up in church buildings, usually occupying the most desirable and valuable sites, yet standing empty one hundred and fifty at least of each one hundred and sixty-eight hours of the week, while our prisons, asylums, and penitentiaries are constantly overcrowded the entire time; therefore we earnestly request that your honorable bodies will pass enactment requiring our prison commissioners to ascertain as nearly as practicable the religious belief of each prisoner or patient consigned to our prisons or asylums, that the influence of the various religions upon the morals of the masses may be estimated.

JAMES EMERSON  
A. H. Burgess  
A. J. Wills

T. B. Saunders  
G. H. W. Weston  
James Malcolm

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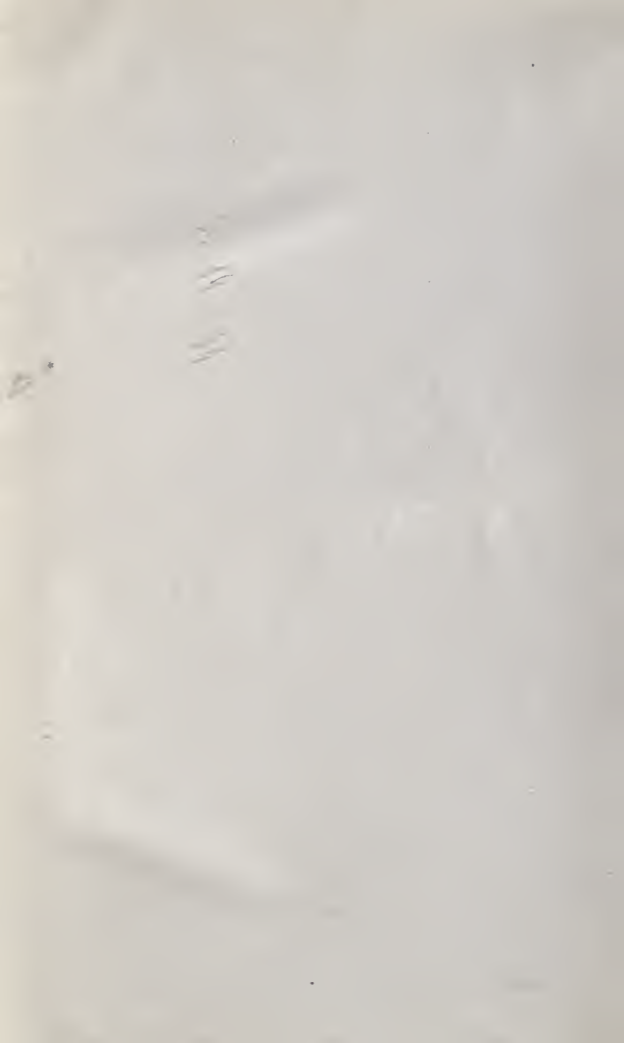
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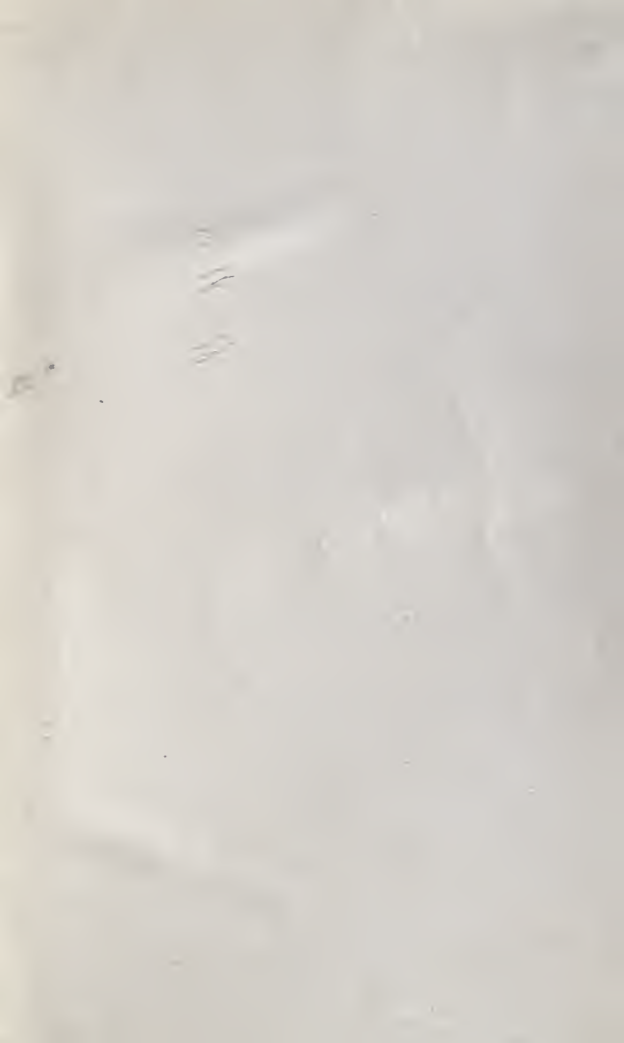
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| Date | Particulars   | Amount  |
|------|---------------|---------|
| 1890 | Jan 1 Balance | 100.00  |
|      | Jan 10        | 50.00   |
|      | Jan 20        | 25.00   |
|      | Jan 30        | 15.00   |
|      | Feb 10        | 30.00   |
|      | Feb 20        | 20.00   |
|      | Feb 30        | 10.00   |
|      | Mar 10        | 40.00   |
|      | Mar 20        | 30.00   |
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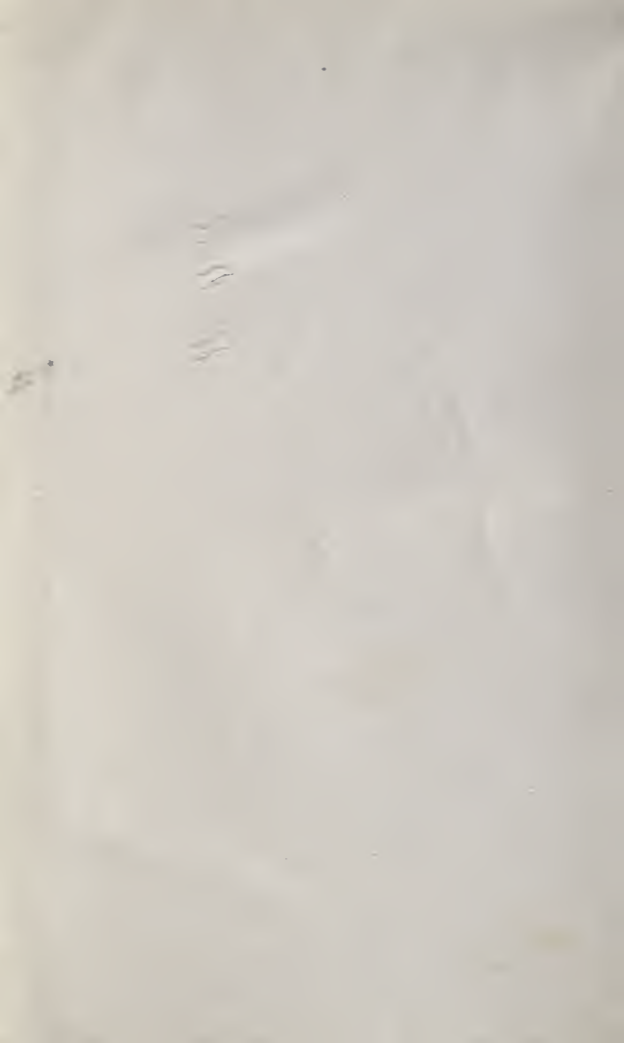






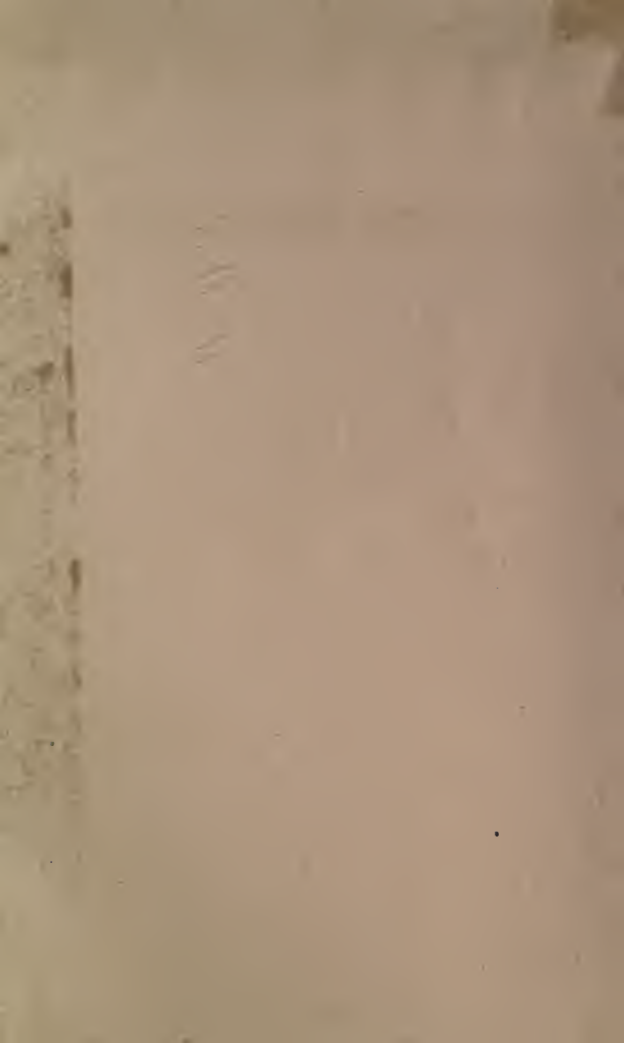


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