

February 1984
Final Report

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Data and data summaries presented herein were collected during 1980 and compiled at the U. S. Army Engineer Waterways Experiment Station (WES) Coastal. Engineering Research Center's (CERC) Field Research Facility (FRF) in Duck, N. C. This report, the second of a series of annual FRF data collection summaries, was carried out under CERC's Waves and Coastal Flooding Program.

The report was prepared by H. Carl Miller, Oceanographer, under the supervision of Curt Mason, Chief, FRF Group, Research Division. The author acknowledges the entire FRF Group for their efforts related to instrumentation, data collection, and analysis. Drs. Robert W. Whalin and Lewis E. Link, Chief and Assistant Chief, respectively, of CERC, and Dr. James R. Houston, Chief, Research Division, provided general guidance.

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Commander and Director of WES during the publication of this report was COL Tilford C. Creel, CE. Mr. F. R. Brown was Technical Director.

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```
CONVERSION FACTORS, INCH-POUND TO METRIC (SI)
UNITS OF MEASUREMENTS
```

Inch-pound units of measurement used in this report can be converted to metric (SI) units as follows:

Multiply
acres
feet
millibars

By
0.4046873
0.3048
100.0

To Obtain
hectares
meters
pascals

PART I: INTRODUCTION

1. The U. S. Army Engineer Waterways Experiment Station Coastal Engineering Research Center's (CERC) Field Research Facility (FRF) located on 176 acres* at Duck, North Carolina (Figure 1), consists of a 561-m-long research pier and an accompanying office building. The FRF is located near the middle of Currituck Spit along a $100-\mathrm{km}$ unbroken stretch of shoreline extending south from Rudee Inlet in Virginia to Oregon Inlet, North Carolina. It is bordered by the Atlantic Ocean to the east and Currituck Sound to the west. The Facility is designed to (a) provide a rigid platform from which waves, currents, water levels, and bottom elevations can be measured, especially during severe storms; (b) provide CERC with field experience and data to complement laboratory and analytical studies and numerical models; (c) provide a manned field facility for testing new instrumentation; and (d) serve as a permanent field base of operations for physical and biological studies of the site and adjacent region.
2. The research pier is a reinforced concrete structure supported on $0.9-\mathrm{m}$-diameter steel piles spaced 12.2 m apart along the pier length and 4.6 m apart across the width. The piles are embedded approximately 20 m below the ocean bottom. The pier deck is 6.1 m wide and extends from behind the dune line to about the $6-\mathrm{m}$ water depth contour at a height of 7.8 m above mean sea level. The pilings are protected against sand abrasion by concrete erosion collars and against corrosion by a cathodic system.
3. A FRF Measurements and Analysis (FRFMA) program has been established to collect basic oceanographic and meteorological data at the site, reduce and analyze these data, and publish the results.
4. This report is the second in a series of annual reports and summarizes the data collected during 1980. It is organized such that descriptions of the instrumentation, including sensor calibration and maintenance (Part III) and data collection and analysis procedures (Part IV) precede reporting of the

[^0]
Figure 1. FRF location map
data (Part V). Although this is intended as a stand-alone document, details of some procedures and instrumentation are given in the references.
5. Future annual reports will have approximately the same format; readers' comments on the format and usefulness of the data presented are encouraged.
6. In addition to the annual reports, monthly data reports summarizing the same types of data shortly after the data are collected are available to requestors from the CERC Field Research Facility, S. R. Box 271, Kitty Hawk, North Carolina 27949.
7. The CERC Coastal Engineering Information Analysis Center (CEIAC) is responsible for storing and disseminating most of the data presented or alluded to in this report. All data requests should be in writing and addressed to Commander and Director, U. S. Army Engineer Waterways Experiment Station, ATTN: CEIAC, P. 0. Box 631, Vicksburg, Mississippi 39180. Tidal data other than the summaries in this report should be obtained directly from the Tides Branch, National Ocean Service (NOS), Rockville, Maryland 20850. A complete explanation of the exact data desired for specific dates or times will expedite filling any request; an explanation of how the data will be used will help CEIAC or NOS determine if other relevant data are available. For information regarding the availability of data, contact CEIAC at (601) 634-2017. Costs for collecting, copying, and mailing will be borne by the requester.

## PART II: CLIMATOLOGICAL SUMMARY

8. This section provides a brief summary of the environmental conditions at the FRF during the reporting period; complete tabulated summaries are contained in Part V.
9. The maritime climate at the FRF tends to moderate the seasons, producing winters that are warmer and summers that tend to be cooler than on the mainland. Large temperature differences between day and night occur during late fall and spring due to the slow response of the ocean to changing temperature trends and frequent land and sea breeze effects. Air and water temperatures at the FRF tend to be lowest in February and highest in July and August.
10. The precipitation was fairly well distributed throughout the year; the monthly average during 1980 was 68 mm . May was the wettest month ( 112 mm ), while September was the driest ( 30 mm ).
11. A persistent breeze, warm in summer and chilly in winter, blows at the FRF; seldom is it dead calm. On occasion, severe winds blow as a result of either extratropical cyclones (northeasters) or tropical cyclones (hurricanes).
12. The summer winds are predominantly from the southwest, while winter winds blow out of northern directions. Extreme winds generally came from the north-northeast. Although the FRF was not directly hit by a major hurricane in 1980 , strong northeasters produced winds in excess of $15 \mathrm{~m} /$ second.
13. The wave heights at the FRF vary as a function of water depth and season. Generally, the deeper the water, the larger the wave conditions. The annual average significant wave height for 1980 at the seaward end of the pier ( $8-\mathrm{m}$ depth) was 0.87 m ( 0.44 m standard deviation), with an average peak spectral period of 9 seconds ( 2.8 seconds standard deviation). Wave heights tended to be lowest from April through September and greatest during January through March.
14. Surface currents are strongest and move predominantly southward during the winter and are much more frequently directed northward in the summer.
15. The tides at the FRF are semidiurnal, with 2 high and 2 low tides generally occurring daily with a tide range of slightly more than 1.0 m . Local mean sea level during 1980 was 8 cm above the local 1929 National Geodetic Vertical Datum (NGVD). The extreme high tide was 118 cm NGVD observed on 2 March, while the lowest tide was -119 cm NGVD observed on 16 March.
16. The depth contours are relatively straight and parallel to the coast in the vicinity of the FRF with the exception of the area immediately adjacent to the pier. Here the contours bend drastically toward shore (a) as much as 250 m at the $7-\mathrm{m}$ depth contour (i.e., normally seaward of the end of the pier) and (b) 20 m at the $3-\mathrm{m}$ depth contour (i.e., near the beach). Frequently a bar is present nearshore, while occasionally a two-bar system is evident.
17. The sand size varies both temporally and spatially at the FRF. In 1980, foreshore sizes during the low-wave condition of summer tended to be finer than at the high-energy periods during winter. The surface sediments on the beach tend to be fine-to-medium-fine-grained, with relatively coarse, poorly sorted sands at the beach step; a shell fraction is also evident. Sands offshore tend to become increasingly fine, with moderately well-sorted very-fine-to-fine quartz sand out to the -17 m contour.

## PART III: INSTRUMENTATION

18. This part identifies the instruments used for long-term monitoring of oceanographic and meteorological conditions and briefly describes their design and operation. More detailed explanations can be found in Miller (1980). Equipment (i.e. the surveying system) used for collecting other types of data is discussed in Part IV.

## Wave Gages

19. Five wave gages were operated in 1980 as part of the FRFMA for monitoring wave conditions in the vicinity of the FRF (Figure 2). These included a wave staff gage on Jennette's Fishing Pier in Nags Head, N. C., approximately 40 km south of the FRF; two wave staff gages on the FRF pier (one at station $6+20$ (hundreds of feet), the other at station $19+00$ ); and two Waverider buoy gages located 0.6 and 3 km offshore.

Staff gages
20. The wave staffs were parallel cable types manufactured by the Baylor Company, Houston, Texas, and were designed for an accuracy and resolution of 1 and 0.1 percent full scale, respectively. The Baylor gages required little maintenance except to keep the cables taut and free of anything which could cause. an electrical short across them, i.e. fishermen's nets, ropes, biological fouling, etc. Defective parts required replacement; this type of gage (specifically the transducer elements) is susceptible to lightning damage.
21. The transducer elements were connected to test cables in the laboratory and calibrated prior to installation by placing an electrical short between the cables at known distances and noting the voltage output from the transducer. In the field, electronic signal conditioning amplifiers were used to ensure the output signal from the gage was within a 0 - to $5-V$ range. The transducer elements and signal conditioning electronics held their calibrations very well; differences greater than 1 percent full scale were unusual. Table 1 shows the dates when calibration/maintenance was performed for the Baylor staff gages.
22. Since the Baylor staff gages actually sense the water level on the gage, a 20 -minute average of the levels measured four times per second can be
Pier Building $0+40$ to $1+00$
Anemometer at $-0+65$ (Jan-Aug); $0+70$ (Sep-Dec)

Pier Building Pier Building

ATLANTIC OCEAN


Distance (m)
Boylor Gage (No. 615) at $6+20$

CURRITUCK SOUND



12-in Rain Gage at $-0+95$
Instrument Shelter $-1+10$


RONG دapiaanom asousito /

Table 1
1980 Calibration/Maintenance Schedule for Baylor Staff Gages

| Gage | Date | Calibration/Maintenance Performed |
| :---: | :---: | :---: |
| $112 \text { (Nags Head) }$ | 11 Apr | Amplifiers calibrated |
|  | 22 Apr | Replacement calibrated transducer was installed |
|  | 10 Jul | Replacement calibrated transducer and amplifiers were installed |
| ```6 2 5 (Baylor gage at 19+00)``` | 8 Jan | Cleaned and tightened cables |
|  | 9 Jan | Replacement calibrated transducer was installed and amplifiers were calibrated |
|  | 22 Jan | Calibrated amplifier |
|  | 31 Jan | Replacement calibrated transducer installed and amplifiers calibrated |
|  | 11 Feb | Calibrated amplifiers |
|  | 27 Feb | Replacement calibrated transducer with lightning protection circuit installed |
|  | 27 Mar | Calibrated amplifiers; -3 percent error full scale noted |
|  | 16 Apr | Calibrated amplifiers |
|  | 13 Jun | Calibrated amplifiers |
|  | 28 Jun | Calibrated amplifier |
|  | 8 Jul | Replaced IC's in amplifier and calibrated |
|  | 24 Jul | Cleaned cables |
|  | 28 Jul | Calibrated amplifiers |
|  | 11 Aug | Changed data cables and calibrated amplifiers |
|  | 22 Aug | Calibrated amplifiers |
|  | 28 Aug | Calibrated amplifiers |
|  | 23 Sep | Calibrated amplifiers |
|  | 27 Sep | Calibrated amplifiers |
|  | 30 ct | Calibrated amplifiers |
|  | 40 ct | Calibrated amplifiers |
|  | 14 Oct | Calibrated amplifiers |
|  | 21 Oct | Calibrated amplifiers |
|  | 31 Oct | Calibrated amplifiers |
|  | 4 Nov | Replacement calibrated transducer installed |
|  | 13 Nov | Calibrated amplifiers |
|  | 20 Nov | Calibrated amplifiers |
|  | 1 Dec | Calibrated amplifiers |
|  | 10 Dec | Calibrated amplifiers |
|  | 15 Dec | Replacement calibrated transducer installed |
| ```6 1 5 (Baylor gage at 6+20)``` | 22 Jan | Calibrated amplifiers |
|  | 14 Feb | Calibrated amplifiers |
|  | 17 Mar | Calibrated amplifiers |
|  | 16 Apr | Calibrated amplifiers; 2 percent error full scale noted |
|  | 22 Apr | Calibrated amplifiers |
|  | 28 May | Calibrated amplifiers |
|  | 13 Jun | Calibrated amplifiers |
|  | 5 Jul | Amplifiers repaired |
|  | 7 Jul | Replacement calibrated transducer installed and amplifiers calibrated |
|  | 24 Jul | Cleaned cables |
|  | 22 Aug | Calibrated amplifiers |
|  | 22 Sep | Calibrated amplifiers |
|  | 27 Sep | Calibrated amplifiers |
|  | 3 Oct | Calibrated amplifiers |
|  | 14 Oct | Calibrated amplifiers |
|  | 21 Oct | Calibrated amplifiers |
|  | 31 Oct | Calibrated amplifiers |
|  | 13 Nov | Calibrated amplifiers |
|  | 20 Nov | Calibrated amplifiers |
|  | 1 Dec | Calibrated amplifiers |
|  | 10 Dec | Calibrated amplifiers |

used to provide a mean sea (or tide) level. (It was suggested that the Baylor staff gages along the FRF pier be used to measure water levels across the surf zone to investigate the water's slope. This was not pursued because the gage zero value showed both a random variation due to the difficulty in measuring the zero offset and a time-dependent change due to amplifier drift.)
23. The procedure used to monitor the gage zero level was to measure the water level on the gage and gage output, then compare that to the corresponding gage output for the measured water level based on the gage calibration curve. Differences implied a drift of the gage zero. In practice, this was accomplished as follows:
a. The distance from the pier deck to the still-water level was measured by lowering a weighted surveyor's tape (i.e. lead line) from the FRF pier deck (on a calm day) to the visually determined still-water level next to the gage.
b. The distance from the bottom of the gage to the still-water level was determined by accounting for the distance from the top of the gage to the pier deck in the above measurement and taking the difference between that value and the gage length.
c. The gage output value was determined as the average of the fewminute sample of gage measurement output while the weighted tape measurement was made.
d. The lead-1ine-determined level and the measured gage output were then compared to determine the zero offset of the gage.
24. This procedure is believed to be accurate to no better than $\pm 10 \mathrm{~cm}$; errors arise from estimating the still-water level and from movement, bending, and expansion of the surveyor's tape used in the lead-line measurement. This accuracy is not sufficient for the detection of water slopes across the surf zone, which may only amount to a few centimeters difference at the measurement locations. The gage zero drift or uncertainty is random (see Figure 3).
25. Although this variability seems artificial, precautions were taken in the analysis of the 20 -minute data records when computing wave statistics (see Part IV).

Waverider buoy gages
26. The Waverider buoys were manufactured by the Datawell Laboratory for Instrumentation, Haarlem, Netherlands. Each 0.7-m-diameter buoy floats on the water's surface and (a) measures the vertical acceleration produced by the passage of a wave, (b) doubly integrates this signal to produce a displacement signal, and (c) telemeters this signal to an onshore receiver and associated electronics which extract the displacement signal for data logging


Figure 3. Amplifier zero drift during 1980 (arrows indicate when amplifiers were reset to 0.0 cm )
and analysis. The manufacturer states that wave amplitudes are correct within 3 percent of their true value for frequencies between 0.065 and 0.5 Hz (i.e., wave periods between 15 and 2 second). For frequencies as low as 0.03 Hz (i.e., for a 33 -second period), the manufacturer provides a frequency response curve which must be used to maintain the 3 percent accuracy. The frequency response curve was not used for the data in this report since wave periods greater than 17 seconds were never observed.
27. Datawell recommends that Waverider buoys be cleaned and new batteries installed at least every 9 months. The buoys were replaced with cleaned, repainted, and calibrated buoys in October 1979 and August 1980. The buoys were calibrated at the Engineering Support Offices, Ocean Wave Instrument Facility, National Oceanic and Atmospheric Administration (NOAA) (Ribe 1981). Considerable biological growth occurs during the summer months when the water
temperature is above $10^{\circ} \mathrm{C}$. At least one cleaning and painting with antifoulant paint during the summer reduces the fouling problem.
28. Ribe (1981) presents three correction factors to use to increase wave measurement accuracy. These factors are (a) the Datawell-specified decrease in electronic sensitivity as a function of oscillation period, (b) a difference error based on deviations from (a) found during NOAA's calibrations, and (c) a temperature-dependent adjustment of the sensitivity due to an unknown chemical reaction in the conducting fluid surrounding the Waverider accelerometer. These corrections and their application are discussed below.
29. Datawell-predicted decrease in sensitivity (DW). Waverider buoy sensitivity /A/ for the buoy electronics decreases with increasing period $T$ of sinusoidal vertical motion according to Datawell as follows:

$$
\begin{equation*}
\left\lvert\, A /=\overline{\left[1+\left(\frac{T}{\mathrm{To}}\right)^{4}\right]^{1 / 2}}\right. \tag{1}
\end{equation*}
$$

where $T_{0}=30.8$ seconds is a characteristics period provided by Datawell. This sensitivity decrease results in amplitude errors of less than 3 percent for oscillation (wave) periods less than 15 seconds. Figure 4 presents curves for (a) (DW) $=/ A /-1$, the Datawell-predicted sensitivity decrease error, and (b) the actual sensitivity decrease error obtained from predeployment buoy calibrations. Note the actual sensitivity does not follow the Datawell relationship (Equation 1) given above.
30. Difference error (d). Ribe (1981) presents a least-mean-squares second-order polynomial of the form shown below in period $T$ for a "bestestimate" difference error d between the Datawell-predicted decrease in sensitivity and that found from the actual buoy calibrations:

$$
\begin{equation*}
d=a_{o}+\left(a_{1} \times T\right)+\left(a_{2} \times T^{2}\right) \tag{2}
\end{equation*}
$$

In Table 2, DW and $d$ are tabulated as functions of $T$ for each of the FRF buoys.
31. Temperature-related error. It was determined that for some unknown number of Waveriders the sensitivity was drifting downward, possibly since manufacture, and averaging about 1 percent per year. Sensitivity loss from some unknown chemical reaction was related to increases in electrical


Figure 4. Predeployment Waverider gage calibrations (after Ribe 1981)

Table 2
Waverider Predeployment Calibration Information, 1 August 1980

| Gage No. 610 |  |  |  | Gage No. 620 |  |  |  | Gage No. 630 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period F | Frequency | Difference d | $\begin{gathered} \hline \text { Datawell } \\ \text { DW } \\ \hline \end{gathered}$ | Period F | Frequency | $\mathrm{d}$ | $\mathrm{DW}$ | Period F | Frequency | difl | DW |
|  | , |  |  |  |  |  |  |  |  |  |  |
| 2.0060 | 0.50096 | -0.0484 | -0.0000 | 2.0000 | 0.50010 | -0.0212 | -0.0909 | 2.0069 2.0317 | 0.50100 0.49219 | -9.0164 | $\begin{aligned} & -0.90100 \\ & -6.9000 \end{aligned}$ |
| 2.0317 | 0.49219 | -0.0485 | -0.0.000 | 2.0317 | 0.49219 | -0.0214 | -0.000 | 2.0645 | 0.48438 | -9.9107 | -0.9099 |
| 2.0645 | 0.48438 | -0.0487 | -9.0608 | 2.0645 | 0.48438 | -0.0217 | -9.6000 | 2.9984 | 0.47656 | -5.0108 | -6. 10.095 |
| 2.0934 | 0.47656 | -0.0488 | -0.0006 | 2.6984 | 6. 0.46875 | -0.0218 | -0.0000 | 2.1333 | 0.46875 | -9.0116 | - 0.09050 |
| 2.1333 | 0.46875 | -0.0489 | -0.5909 | 2.1333 2.1695 | 0.46894 | -0.0220 | -0.0000 | 2.1595 | 0.46094 | -0.0111 | -6. 0900 |
| 2.1695 | 0.46994 | -0.0491 | -0.0900 | 2.16969 | 0.45313 | -0.0.0221 | - 0.0800 | 2.2069 | 0.45313 | -0.0113 | -9.0060 |
| 2.2669 | 0.45313 0.44531 | -0.0492 | -0.0000 | 2.2869 2.2456 | 0.44531 | -0.0223 | -0.0000 | 2.2456 | 0.44531 | -0.0114 | -6. 0 ¢й |
| 2.2456 | 10.44531 | -0.0494 | - 0.0000 | 2.2857 | 0.43750 | -0.0225 | -0.0000 | 2.2857 | 6.43750 | -0.0116 | -0.0880 |
| 2. 2857 | 0.43750 | -0.0493? | -0.0000 | 2.3273 | 0.42969 | -0.0227 | -9.0060 | 2.3273 | 0.42969 | -0.0116 | -0. 6908 |
| 2.3273 | 0.42969 | -0.049? | -0.0.0069 | 2.3784 | 0.42188 | -0,0229 | -0.0000 | 2.3704 | D. 42188 | -0.011 | -9. 9065 |
| 2.3704 | 0.42188 | -0.0499 | - ${ }^{\text {- }}$. 0.00096 | 2.4151 | 8.41406 | -8.0231 | -0.6960 | 2.4151 | 0.41406 | - 0.0121 | -0.004 |
| 2.4151 | 0.41406 | -0.0500 | - ${ }^{-0.0009}$ | 2.4615 | 0.40625 | -0.0233 | -0.0960 | 2. 4615 | 0.46625 | -0.0123 | -0. 1916 da |
| 2. 4615 | 6.40625 | -0.0502 | -0.0609 | 2. 2.5698 | 0.39844 | -0.0235 | -0.0990 | 2.5098 | 0.39844 | -0.8125 | -0. 61418 |
| 2.5098 | 0. 39844 | -0.0504 | -0.0196 | 2.5098 | 0.39063 | -0.0237 | - 0.0000 | 2.5690 | 0.39863 | -0.0127 | -0. 1.1095 |
| 2,5606 | 0.39063 | -0.0506 | -0.0.008 | 2.5608 | 0. 390881 | -0.024 | -0.0009 | 2.6122 | 0.38281 | -0,0129 | -0. 91096 |
| 2.6122 | 6.38281 | -0.0508 | -0.0008 | 2. 6122 | 0.38281 | -0.0.0242 | -0.9000 | 2.6667 | 5. 37569 | -0.0131 | -6.0009 |
| 2. 6667 | 0.37500 | -0.0510 | -0.6069 | 2.6667 2.7234 | 0.37500 | -0.0244 | -0.0060 | 2.7234 | 0.36719 | -9. 0133 | -0.0900 |
| 2.7234 | 0.36719 | -0.0512 | -0.0906 | 2.7234 2.7826 | 0.36719 0.35938 | -0.0244 | -0.0060 | 2.7826 | 0.35938 | -0.0136 | -0.0060 |
| 2.7826 | 0.35938 | -0.0514 | -0.0000 | 2.7826 | 0.35938 | -0.024 | -0.0006 | 2,8444 | 0.35156 | -0.0138 | -0.0096 |
| 2.8444 | 0. 35156 | -8.051? | -0.0000 | 2.8444 | 0.35150 | -0.0252 | -0.9008 | 2.9091 | 0.34375 | -0.0141 | -0.0000 |
| 2.9091 | 0.34375 | -0.0519 | -0.0000 | 2.9691 | 343? | -0.025 | -0.0009 | 2.9767 | 0,33594 | -0.0143 | -0.0600 |
| 2.9767 | 0. 33594 | -9.0522 | -0.0009 | 76? | 8.33594 | -0.0255 | -0.0008 | 3.0476 | 0.32813 | -0.0146 | -10.0006 |
| 3.0476 | 6.32813 | -0.0524 | -0.0000 | 3.0476 | 0.328.3 | -0.025 | -0.0001 | 3.1229 | 0.32031 | - 0.0149 | -0.0001 |
| 3.1220 | 6.32031 | -9.0527 | -0.8081 | 3.1220 | 0.32031 | -0.0262 | -8.8001 | 3.2006 | 0.31250 | -0.0152 | -0.0001 |
| 3.2006 | 0.31250 | -6.0539 | -0.0001 | 3.2909 | 0.31250 | -0.0265 | -0.0001 | 3.2821 | 0.30469 | -0.0155 | -0.0001 |
| 3.2821 | 0.30469 | -8.8533 | -0.0001 | 3.2821 | 0.30469 | -0.0268 | -0.0.0091 | 3.3684 | 0.29688 | -0.0158 | -0. 0001 |
| 3,3684 | 0.29688 | -0.0536 | -0.0001 | 3.3684 | 0.29688 | -0.0276 | -8.0091 | 3.4595 | 0.28906 | -9.0161 | -0.0901 |
| 3,4595 | 0.28906 | -0.0539 | -0.0081 | 3.4595 | 0.28125 | -8.0279 | - 0.6601 | 3.5556 | 0.28125 | -5.0165 | -0. 0 ออ1 |
| 3.5556 | 0.28125 | -0.0543 | -0.0001 | 3.5556 |  | -9.0284 | -0.0081 | 3.6571 | 0.27344 | -0.0169 | -0.0001 |
| 3.6571 | 0.27344 | -0.0546 | -0.0001 | 3.6571 | 0. 273653 | -0.0288 | -0.0061 | 3.7647 | 0.26563 | -0.0173 | -0.0091 |
| 3.7647 | 0.26563 | -0.0550 | -0.0001 | 3.7647 | 0.26563 | -0.0288 | -0.0061 | 3.8788 | 0.25781 | -0.0177 | -9.0001 |
| 3.8788 | 0.25781 | -0.0554 | -0.0901 | 3.8788 | 0.25781 | -0.0292 | -0.0901 | 4.0000 | 0.25060 | - 0.0181 | -0.0001 |
| 4.0006 | 0.25000 | -0.0558 | -0.0601 | 4.9000 | 8.25608 | -0.0297 | -0.6002 | 4.1290 | 0.24219 | -0.0185 | -0.0902 |
| 4.1298 | 0.24219 | -0.0562 | -0.0002 | 4. 1296 | 9.24219 | -0.0302 | -0.0002 | 4.2667 | 0.23438 | -0.0198 | -0.0002 |
| 4,2667 | 0.23438 | -0.0567 | -0.0002 | 4.2667 | 0.23438 | -0.0388 | -0.0002 | 4.4138 | 0.22656 | -0.0195 | -5.0002 |
| 4.4138 | 0.22656 | -0.0572 | -0.0002 | 4. 4138 | 0.22656 | -0.0313 | -0.0002 | 4.5714 | 0.21875 | -0.0200 | -0.0002 |
| 4.5714 | 0.21875 | -0.057? | -0.0002 | 4.5714 | 0.21875 | -0.0319 | -0.0002 | 4.740 ? | 0.21094 | -0.0206 | -0.0003 |
| 4.7407 | 0.21094 | -0.0582 | -0.0003 | 4.7407 | 0.21594 | -0.0325 | -0.0003 | 4.9231 | 0.20313 | -0.0212 | -0.0003 |
| 4.9231 | 0.20313 | -0.0588 | -0.0903 | 4.9231 | 0.20313 | -0.0332 | -0.0003 | 5.1200 | 0.19531 | -0, 0218 | -8.0964 |
| 5.1206 | 0.19531 | -0.0594 | -0.0904 | 5.1200 | 0.19531 | -0.0339 | -0.0004 | 5.3333 | 0.18750 | -0.0225 | -0.0094 |
| 5.3333 | 0.18750 | -0.0601 | -0.0.0.04 | 5.3333 | 0.18750 | -0.0346 | -0.0064 | 5.5652 | 0. 17969 | -0.0232 | -0.0065 |
| 5.5652 | 0.17969 | -0.0697 | -9.0005 | 5.5652 | 0.17969 | -0.0354 | -0.0905 | 5.8182 | 0.17188 | -0.0239 | -0.0006 |
| 5.8182 | 0.17188 | -0.0615 | -0.0006 | 5.8182 | 0.17188 | -0.0363 | -0.0066 | 6.0952 | 9.16406 | -0.0.0247 | -0.0003 |
| 6.0952 | 0.16466 | -0.0623 | -0.0008 | 6.0952 | 0.16406 | -0.0372 | -0.0008 | 6.4000 | 0.15625 | -0.0256 | -8.0669 |
| 6.4000 | 0.15625 | -0.0631 | -0.000] | 6. 4900 | 0.15625 | -0.0381 | -0.0099 | 6.7368 | 0.14844 | -0.0265 | -0.0011 |
| 6.7368 | - 0.14844 | -0.0640 | -0.0011 | 6.7368 | 0.14844 | -0.0391 | -0.0011 | 7.1111 | 0.14063 | -9.0275 | -0.0914 |
| 7.1111 | 0.14063 | -0.0649 | -0.0.014 | ?. 1111 | 0.14063 | - 0.0402 | -0.0814 | 7.5294 | 0.13281 | -0.0285 | -0.0918 |
| 7.5294 | 4.0 .13281 | -0.0659 | -0.0018 | 7.5294 | 0.13281 | - 0.0414 | -0.0018 | 8.0650 | 0.1250日 | -0.0296 | -0.0923 |
| 8.0966 | 30.12500 | -0.0670 | -0.0023 | 8.0000 | 0.12500 | - 0.0426 | -0.0023 | 8.5333 | $3 \quad 0.11719$ | -0.0307 | -9.0029 |
| 8.5333 | $3 \quad 0.11719$ | - $\quad 0.6681$ | -0.0029 | 6.5333 | $3 \quad 0.11719$ | - 0.0439 | -0.0029 | 9.1429 | 9.0 .16938 | -0.0319 | -0.0039 |
| 9.1429 | 90.10938 | - -0.0693 | -0.0039 | 9.1429 | - 0.10938 | $8 \quad-0.0453$ | -0.0039 | 9.8462 | 2 0.19156 | -0.0331 | -0.0092 |
| 9.8462 | $2 \quad 0.10156$ | $6-0.0705$ | -0.0052 | $9.84 E 2$ | $2 \quad 0.10156$ | $5 \quad-0.0467$ | -0.0052 | 10.6667 | $7 \quad 0.09375$ | - -0.0344 | -0.0071 |
| 10.6667 | $7 \quad 0.89375$ | $5-0.0718$ | -0.0071 | 10.6667 | $7 \quad 0.09375$ | $5 \quad-0.0482$ | -0.0071 | 11.6364 | 40.08594 | $4-0.0355$ | -0.010 |
| 11.6364 | 4 E. 88594 | $4-0.0730$ | -0.0100 | 11.6364 | 40.08594 | $4-0.0496$ | -0.0106 | 12.8090 | 0.07813 | $3-0.0366$ | -0.0146 |
| 12.81000 | 0.8 .07813 | $3 \quad-0.0741$ | -0.0146 | 12.8000 | 0.0 .07813 | $3-0.0509$ | -0.0146 | 14.2222 | 20.07031 | $1-0.0372$ | -0.0220 |
| 14.2222 | 20.07831 | $1-0.0749$ | -0.0229 | 14.2222 | 20.07031 | $1-0.0518$ | -0.0220 | 16.0000 | 0 0.06250 | - 0.0371 | -0.0345 |
| 16.0908 | $8 \quad 0.06250$ | - 0.0751 | -0.0345 | 16.0000 | 70.86250 | $9-0.0519$ | -0.0345 | 18.285? | ? 0.05469 | $9-0.0355$ | -0.0569 |
| 18.2857 | $7 \quad 0.05469$ | 9 -0.0739 | -0.0569 | 18,2857 | $7 \quad 0.05469$ | $9 \quad-0.0506$ | -0.0569 | 21.3333 | 30.04688 | 8 -0.0387 | -0.0984 |
| 21.3333 | 30.04688 | $8-0.0698$ | -0.0984 | 21.3333 | 30.04688 | $8-8.0459$ | -0.0984 | 21.3337 | - .04603 | -0.0387 | -0.0984 |

conductivity of the conductive fluid surrounding the accelerometer. This drift could be identified from calibrations over a succession of time.
32. In 1982 Datawell made available an improved modulator printedcircuit board for bringing calibrations within specification and for preventing further decrease in sensitivity; however, this modification was not made for the 1980 FRF buoys. Datawell provided curves for correction of calibration sensitivity based on differences between buoy temperature during calibration and buoy temperature when the buoy is measuring waves in the ocean. The NOAA Engineering Support Office developed a table based on the Datawell curve which can be entered with the uncorrected difference error value $d$ (Table 2) and the temperature of the water during the time of the buoy operation to determine the difference error correction (see tabulation below). The difference error correction is added to $d$ to obtain the corrected difference error D. For temperatures during buoy operation greater than the buoy temperature during calibration $\left(22.4^{\circ} \mathrm{C}\right)$, no correction is necessary.

| Water Temperature (degree $C$ ) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diff. | 22.4 | 20 | 18 | 16 | 14 | 12 | 10 | 8 |
| 0.00 | 0.000 | 0.001 | 0.001 | 0.001 | 0.001 | 0.000 | -0.000 | -0.002 |
| -0.01 | 0.000 | 0.007 | 0.008 | 0.069 | 0.010 | 0.011 | 0.011 | 0.011 |
| -0.02 | 0.000 | 0.009 | 0.012 | 0.014 | 0.016 | 0.018 | 0.019 | 0.020 |
| -0.03 | 0.000 | 0.009 | 0.013 | 0.016 | 0.019 | 0.021 | 0.024 | 0.026 |
| -0.04 | 0.000 | 0.008 | 0.012 | 0.016 | 0.020 | 0.023 | 0.027 | 0.029 |
| -0.05 | 0.000 | 0.006 | 0.011 | 0.016 | 0.020 | 0.024 | 0.028 | 0.032 |
| -0.06 | 0.000 | 0.004 | 0.010 | 0.015 | 0.020 | 0.025 | 0.030 | 0.034 |
| -0.07 | 0.000 | 0.003 | 0.009 | 0.015 | 0.021 | 0.026 | 0.031 | 0.036 |
| -0.08 | 0.000 | 0.003 | 0.010 | 0.017 | 0.023 | 0.029 | 0.034 | 0.039 |
| -0.09 | 0.000 | 0.006 | 0.013 | 0.019 | 0.026 | 0.032 | 0.038 | 0.043 |
| -0.10 | 0.000 | 0.010 | 0.017 | 0.024 | 0.031 | 0.037 | 0.043 | 0.049 |

33. Since these error corrections are oscillation-period dependent, their application requires that the wave data be decomposed into amplitude coefficients or variance-spectrum coefficients for each frequency or period. A less accurate but also less complicated procedure would be to apply a single correction to, say, the significant wave height based on the peak spectral wave period and an average water temperature estimate. For correction of amplitudes or derived parameters linearly related to amplitude, a correction factor $F(T)$ can be obtained from the sum of the Datawell DW and temperature-corrected difference error $D$ by:

$$
\begin{equation*}
\mathrm{F}(\mathrm{~T})=\frac{1}{1+(\mathrm{DW}+\mathrm{D})} \tag{3}
\end{equation*}
$$

which can be applied by multiplying the uncorrected amplitude by $F(T)$ for $T$ equal to the peak spectral wave period. For correction of parameters related to the square of the amplitude (i.e., total energy or variance spectrum coefficients), the following should be used:

$$
\begin{equation*}
[F(T)] \quad 2=\left[\frac{1}{1+(D W+D)}\right] 2 \tag{4}
\end{equation*}
$$

34. The following example demonstrates use of the calibration results. The nearshore Waverider buoy on 25 October recorded the annual extreme significant wave height of 3.80 m with an associated peak spectral period of 10.9 seconds. From Table 2, the Datawell-predicted sensitivity error DW is -0.0071 , with a corresponding uncorrected difference error d of -0.0718 .
35. To determine the correction for the difference error, the water temperature is also required; the ocean water temperature at that time was approximately $16^{\circ} \mathrm{C}$ (see Part V). The correction (see tabulation) is 0.015, thus:

$$
D=d+0.015=-0.0718+0.015 \text { or } D=-0.0568
$$

F(T) can be determined from Equation 3 as

$$
\begin{aligned}
\mathrm{F}(\mathrm{~T}) & =\frac{1}{1+(\mathrm{DW}+\mathrm{D})} \\
& =\frac{1}{1+(-0.0071-0.0568)} \\
& =\frac{1}{0.9361} \\
\mathrm{~F}(\mathrm{~T}) & =1.0683
\end{aligned}
$$

Finally, the corrected significant height is $3.80 \mathrm{~m} \times \mathrm{F}(\mathrm{T})=3.80 \mathrm{~m} \times 1.0683$ $=4.06 \mathrm{~m}$, which is a 7 percent increase.
36. In general, the wave statistics errors are near 5 percent for wave
periods less than 12 seconds ( 12 seconds is equal to the annual mean plus one standard deviation wave period). Errors of this magnitude are generally tolerable for most engineering applications, although it is worthwhile to know the error bounds for some design considerations. When investigating coastal phenomena involving very long period swells of 15 seconds or greater these corrections will produce significant increases in the magnitudes of the wave parameters and it is recommended that the corrections be used.

## Tide Gages

37. Water level data from the FRF pier are presented in this report. A NOAA/NOS control station, located at the seaward end of the research pier, consisted of a Leupold-Stevens gage manufactured by Leupold and Stevens, Inc., Beaverton, Oregon. The Leupold-Stevens analog-to-digital recorder was a float-activated, negator-spring, counterpoised instrument that mechanically converts the vertical motion of a float into a coded, punched paper tape record. The below-deck installation at pier station $19+60$ (see Figure 2) consisted of a $30.5-\mathrm{cm}$-diameter stilling well with a $2.5-\mathrm{cm}$ orifice and a 21.6-cm-diameter float.
38. The FRF tide gage was checked daily by a tide gage tender at the FRF for correctness of time, proper operation of the punch mechanism, and accuracy of water level information obtained. The accuracy was determined by comparing the gage level reading to a level read from a reference electric tape gage. Once a week, a heavy metal rod was lowered down the stilling well and through the orifice to ensure free flow of water into the well. During the summer months, when biological growth was most severe, divers inspected and cleaned the orifice opening as required.
39. Quarterly, a NOAA/NOS tide "party," which consisted of NOS personnel familiar with the installation and equipment, performed a tide station inspection and review. The tide gage was surveyed in from existing NOS control positions and the equipment checked and adjusted as needed; and NOS and FRF personnel reviewed procedures for tending the gage and handling the data. Any specific comments on the previous months of data were discussed to ensure data accuracy.

## Meterological Instruments

## Anemometer

40. Winds were measured using a Weather Service Model F420C anemometer consisting of a cup rotor and spread-tail wind vane. Through mid-September, the anemometer was located 58 m behind the dune, with the cups 6.4 m above NGVD. In late September, the instrument was relocated to the top of the laboratory building at an elevation of 19.1 m (Figure 2). The accuracy of the speed transmitter and indicator assemblies was (a) 1 percent up to $100 \mathrm{~m} / \mathrm{sec}$ and (b) 2 percent over $100 \mathrm{~m} / \mathrm{sec}$. The wind direction transmitter and indicator assemblies were accurate to $\pm 5$ deg at an air speed of $0.26 \mathrm{~m} / \mathrm{s}$ or greater.
41. In September, after installation on the laboratory roof, NOAA/ National Weather Service (NWS) personnel calibrated the speed cups and set the direction reference to true north. The speeds were found to be approximately 5 percent faster than actual, and the instrument was reset. The anemometer had been last calibrated in the spring of 1979 at which time, it is believed, the zero offset was incorrectly set; consequently, the data before September should be corrected by reducing the value indicated by 5 percent.
42. The wind speed and direction were recorded on a battery-powered Esterline-Angus recorder. Problems with the recorder's clock and tape advance mechanism and the pen actuator (for indicating direction) were frequently found, and the unit required day-to-day maintenance.
43. Maintenance of the anemometers consisted of troubleshooting the records and resetting the instrument based on the calibration results. Microbarograph
44. This recording instrument, an aneroid sensor used to measure atmospheric pressure, responded to pressure changes on the order of 0.169 mb . The microbarograph was manufactured by the Belfort Instrument Company, Baltimore, Maryland, and was located inside the office trailer, 6 m above NGVD, until June when it was moved inside the laboratory building, 9 m above NGVD (Figure 2).
45. Daily, the microbarograph was compared to an NWS aneroid barometer; adjustments, although infrequent, were made as necessary. The microbarograph required very little maintenance except that required to ink the pen and wind the clock every 3 days when the chart paper was changed.
Maximum/minimum thermometers
46. NWS maximum and minimum thermometers were used to determine the
daily extreme temperatures. The thermometers were housed in an NWS instrument shelter located 91 m behind the dune (Figure 2). The shelter was designed with louvered sides, a double roof, and a slatted bottom for housing instruments requiring protection from direct sun.
47. The actual temperature readings at the time the thermometers were read (i.e., the present temperature) were compared to ensure accuracy of maximum and minimum values. Maintenance consisted of periodic removal and cleaning of the thermometers with soap and clean water and lubricating the support used to hold and reset the instruments.

Rain gage
48. A $30-\mathrm{cm}$ weighing rain gage manufactured by the Belfort Instrument Company, Baltimore, Maryland, used to measure the daily amount of precipitation, was located near the instrument shelter 87 m behind the dune (Figure 2). The manufacturer's specifications indicated that the instrument accuracy was $\pm 0.5$ percent for precipitation amounts less than 15 cm and $\pm 1.0$ percent for amounts above 15 cm .
49. A $15-\mathrm{cm}$-capacity "true check" clear plastic rain gage with a $0.025-\mathrm{cm}$ resolution, manufactured by the Edwards Manufacturing Company, Albert Lea, Minnesota, was used to monitor the performance of the weighing rain gage. This gage, located near the weighing gage, was checked daily, and very few discrepancies were identified throughout the year. The weighing rain gage required little maintenance except to wind the clock and ink the pen. The pen mark on the chart records did "bleed" or drip down when a driving rain was directed at the access door.

Sling psychrometer
50. A sling psychrometer was used to measure wet and dry bulb temperatures for determining relative humidity and dew point. The psychrometer had two thermometers mounted in a frame which was rotated rapidly. A moistened muslin wick was attached to the bulb (i.e. wet bulb) of one of the thermometers, and the device was whirled to ventilate both thermometers. The wet and dry bulb temperatures were read, and a set of NWS tables were used to determine the dew point.
51. These thermometers required little maintenance except to change the muslin wick every month or two and to clean the sling and thermometers with soap and water. The instruments were not calibrated, but the thermometers were compared daily to detect any bias or malfunction.

## Pyranograph

52. A mechanical pyranograph, manufactured by the Weather Measure Corporation, Sacramento, California, was located on the top of the weather instrument shelter and provided a record of the duration and intensity of solar radiation. The pyranograph was not calibrated, but was observed to operate in a reasonable manner. This equipment required that the glass cover be cleaned, the chart paper changed every week, the timer wound, and the pen inked.

## PART IV: DATA COLIECTION AND ANALYSIS

53. In this section, the FRF data acquisition system, data collection techniques, and data analysis procedures are discussed.

Digital Wave Data

## Recorders/signal conditioning

54. The data acquisition system consisted of a primary and backup recorder and associated electronics for signal conditioning prior to recording. Two different primary recorders were used to collect the wave data. Prior to October 1980, the primary system transmitted analog data signals via telephone lines from the FRF to Ft. Belvoir, Virginia, where the data were recorded in digital form on a Modcomp II/25 minicomputer. After October, a Data General NOVA-4 minicomputer located in the FRF laboratory building was used to collect the data. In addition, a backup system consisting of a Lockheed Store 7 (FM) recorder located at the FRF was used to record data when the primary system was known to be inoperative. Frequently during storm conditions the backup system was run simultaneously with the primary system to ensure that wave data were obtained. A second FM recorder located at CERC (Ft. Belvoir) was used to play these tapes into the Modcomp so that the data recorded could be digitized.
55. Regardless of the system used, the voltage signal from the sensors required certain conditioning. For the phoneline/Modcomp system, the signal was first amplified and biased to ensure a $0-$ to $5-V$ range, then converted to a frequency-modulated (FM) signal by exciting a voltage-controlled oscillator (VCO). That signal was then transmitted to Ft. Belvoir via telephone line where a discriminator was used to convert it back to a voltage signal. This signal was fed into a demultiplexer and converted to a serial data stream which was then sampled by the Modcomp. For the NOVA-4 and FM recording systems, the $0-$ to $5-V$ signal was fed directly into the recorders. However, since the FM recorder operated on a maximum output of 3 V , it linearly scaled the 0 - to $5-\mathrm{V}$ signal by a factor of $3 / 5$.
56. The signal from the wave sensors was routinely sampled four times per second for 20 minutes every 6 hours beginning as near as possible to 0100,

0700, 1300, and 1900 hours Eastern Standard Time (EST); these hours correspond to the times that the NWS creates daily synoptic weather maps. During storms, hourly data recordings were made. Since the Modcomp/phoneline and NOVA-4 systems were automated, recording data during nonduty hours and on weekends and holidays created only a minimum of problems. Prior to October, the FM recorder was run manually, and for most dates only two observations, one in the morning and one in the afternoon during duty hours, were obtained. In general, the FM recorder was not run on the weekends and holidays unless there was a particularly interesting event in progress, such as a storm or experiment. After October, a controller was used to turn the recorder on and off at specified times; this automation permitted FM data collection in the evening and on weekends.

## Data tapes

57. The wave data were recorded in digital form with the following basic tape format: two records of header information which include (a) the station identification number, (b) the date and time, and (c) a variable number of records necessary to obtain 20 minutes of data from all sensors at a sample rate of four values per second. Each record contained 384 20-bit integer words (i.e., binary format); each integer word represented the computer units corresponding to the instantaneous voltage output of the sensor. The above sequence of records was repeated for each recording interval until the data tape was filled. Seven-track tapes were used for data recorded via the Modcomp computer, while nine-track tapes were used with the NOVA-4. (The 20-bit word size is unusual but necessary because CERC processed the data on a CDC 6600 machine with a 60 -bit word size; when necessary, CERC converted the data tapes to an ASCII format).
Analysis/summarization procedures
58. The CERC procedure for analyzing and summarizing digital wave data was based on a Fast Fourier Transform (FFT) spectral analysis procedure. The final results were also subjected to human editing and quality control before public distribution (Thompson 1977; Harris 1974). The computer analysis routine used 4096 data points ( 1024 seconds of data sampled four times per second) for each data record processed. The program first edited the digital data record, checking for nonnumeric characters, jumps, and spikes (i.e., deviations greater than 2.5 and 5 standard deviations from the mean, respectively). If more than five bad data points were found in a row or more than
2.5 percent of the digital values in a record were determined to be bad, the record was rejected as unsuitable for analysis; for a few bad data points, the routine linearly interpolated between the erroneous values. If the record was determined suitable for analysis, the distribution function of the sea surface elevations and first five moments were computed. The variance (second moment) and skewness (third moment) were checked to determine if full analysis of the data record was warranted. Records with very low variance values and excessively skewed distribution functions were not fully analyzed.
59. After it had been determined that the record justified full analysis, a cosine bell data window was applied to increase the resolution for the energy spectrum of the record (use of the data window is discussed by Harris (1974)). After application of the data window, the program computed the variance spectrum (energy spectrum) using an FFT procedure.
60. Significant wave height and peak spectral (or significant) period provided a convenient way to characterize the wave conditions contained in the data record and were more conducive to statistical summarization than the more complete, but complex, description provided by the spectrum.
61. Although significant wave height is defined as the average height of the highest one-third of the waves in a record, experimental results and calculations based on the Rayleigh distribution function show that the significant height is approximately equal to four times the standard deviation of the wave record (U. S. Army Corps of Engineers, Coastal Engineering Research Center (CERC) 1977). The peak spectral wave period (also referred to as the significant or peak period) for each digital record is defined as that period associated with the maximum energy density in the spectrum (Thompson 1977).
62. After 1 month of data had been analyzed, the significant wave height and peak period values were segregated by gage and tabulated for visual editing. The editor checked for such things as unreasonable distribution of the sea surface elevations; clipping of the crest or troughs; inconsistencies between successive observations; large trends in the 17 -minute, 4 -second data record; and discontinuities in the data. After the data had been edited, monthly summaries of significant height and peak period were generated for inclusion in summary reports.

## Collection

63. The water level information was obtained from an NOS tide gage, which produced á digital paper tape of instantaneous water levels sampled continuously at 6 -minute intervals. At the end of each month, the paper tape was removed from the recorder and mailed to NOS in Rockville, Maryland, for analysis.
Analysis
64. The digital paper tape records of tide heights taken every 6 minutes were analyzed by the Tides Analysis Branch of NOS. A Mitron interpreter created a digital magnetic computer tape from the punch paper tape. This tape was then processed on a Univac 732 computer. First a listing of the instantaneous tidal height values was obtained for manual checking. If errors were encountered, a computer program was used to fill in or recreate bad or missing data, using correct values from the nearest tide station and accounting for known time lags and elevation anomalies. The data were plotted and a new listing was generated and rechecked. When the validity of the data had been confirmed, monthly tabulations of daily highs and lows, hourly heights (instantaneous height selected on the hour), and various extreme and/or mean water level statistics were generated. The mean sea level (msl) reported is the average of the hourly heights throughout the month, while the mean tide level (mtl) is midway between mean high water (mhw) and mean low water (mlw).

## Weather and Visual Observations

## Meteorological data collection

65. Each instrument used for monitoring the meteorological conditions at the FRF was read and inspected daily. For those instruments with analog chart recording capabilities, (a) the pen was zeroed (where applicable), (b) the chart time checked and corrected, if necessary, (c) a daily reading marked on the chart for reference, (d) the starting and ending chart times recorded, as necessary, and (e) new charts installed when needed. Sample chart records for the microbarograph (atmospheric pressure), rain gage, and pyranograph (solar radiation) are presented in Figure 5. The daily reading was recorded for all instruments except the pyranograph. Concurrent with the

a. Microbarograph

b. Rain gage

c. Pyranograph

Figure 5. Sample chart records for the microbarograph, rain gage, and pyranograph
instrument readings, weather information such as cloud cover, visibility, and predominant weather conditions were visually obtained.
66. The monthly meteorological data tables in Appendix A were prepared from single daily observations made near 0700 EST and thus do not represent daily or hourly averages; therefore, caution should be exercised when interpreting the results.
67. The wind information provided in this report, excluding that found in the tables of Appendix $A$, was based on wind speed and direction values determined every 6 hours from the instrument chart records and represents estimated average values based on 10 minutes of record.
Meteorological data analysis
68. Wind roses were computed for the wind speed and direction values obtained every 6 hours. The directions were specified at 22.5-deg intervals; i.e., a 16-compass-point-direction specification. Frequency distributions of wind speed for each direction were computed for the entire year, each 3-month season, and monthly. In addition to the wind roses, resultant directions and speeds were determined by vectorally adding each observation.
69. Dew point values reported herein were determined from psychrometer readings by computing the wet bulb temperature depression (dry bulb minus wet bulb) and using Table 19 in Appendix III of "Weather Service Observing Handbook No. 1--Marine Surface Observations" (National Oceanic and Atmospheric Administration, National Weather Service 1974).
70. The atmospheric pressure trend is a number which specifies the manner and amount of pressure change occurring over a 3-hour interval before the pressure reading is made. The first number of the three-digit code represents the characteristics of the change and was determined by comparing the barograph record to Table 17, Appendix III, of the Weather Service Observing Handbook. The last two digits of the pressure trends are a code which indicates the magnitude of the change and was determined from Table 18, Appendix III, of the NWS Handbook.

Visual data collection
71. At the FRF, daily visual observations made near 0700 hours and conforming to CERC's Littoral Environmental Observation (LEO) Program (Schneider 1981) were obtained to supplement instrumented data collection. These included observations of surface current speed and direction and wave-approach angle at the seaward end of the FRF pier.

## Collection

72. In October of 1980, an FRF bathymetric survey was performed by Langley and McDonald, Inc. of Virginia Beach, Virginia, which covered the beach, nearshore, and offshore area. Each survey range extended seaward from the baseline behind the dune sometimes as far as 3200 m offshore, and ranges were located up to 4 km north and south of the pier. Control consisted of a series of monuments installed by CERC and the U. S. Army Engineer District, Wilmington (SAW), which were resurveyed by Langley and McDonald, Inc. The survey techniques used were as follows.
73. Beach surveying. Conventional level and tape techniques (Czerniak 1972) were used for the beach portion of the survey, with accurate results conforming to these specifications:
a. Horizontal accuracy $\pm 15 \mathrm{~cm}$.
b. Vertical accuracy $\pm 0.3 \mathrm{~cm}$.

The beach portion of the survey extended from the monument baseline behind the dune to the maximum wading depth, approximately -0.5 mmsl .
74. Nearshore surveys. The contractor used a sea sled with a stadia rod mounted on it to conduct surveys through the surf zone. The sled was pulled offshore by a boat and then winched to shore by means of a cable marked every 6.1 m . Each time a mark came to the winch (as the sled was winched in), the rod elevation was read from the beach by means of a level.
75. Offshore surveying. The contractor surveyed offshore by means of an analog fathometer mounted on a boat and two people on shore who triangulated the boat's position. The fathometer was calibrated on each range line by comparing its measurement to the sea sled value at the sea sled's most seaward position. The angle and depth information was correlated and manually reduced to produce position and depth data. No correction for wave effects was made by the contractor.
76. Pier soundings. Weekly soundings along both sides of the FRF pier were performed. The lead-line surveying technique consisted of lowering a weighted measuring tape and noting the distance below the pier deck. Positions between the pier bents (i.e., every 12.2 m ) were used to minimize inaccuracies due to scour near the pilings.
77. Analysis. The pier, beach, nearshore, and offshore data were
reduced to position ( $\mathrm{X}, \mathrm{Y}$ ) and depth ( Z ) triplets relative to the local NGVD. The data were listed, and a display of the profiles (i.e., distance along the range versus elevation) using line printer graphics was generated for visual inspection. After the data had been edited and determined to be acceptable, another set of routines was used to compute various statistics (i.e., maximum and minimum sand elevations) and displays (i.e., graphic profile representations, envelopes of elevations, and time sequences of elevations), as in Appendix C.
78. The offshore portion of the October bathymetric survey showed an "artificial" rhythmical bending of the bottom contours. Errors in the offshore portion are believed to have been the result of (a) using a floating surveying platform, (b) not performing a bar check calibration of the fathometer (i.e., calibrating at various depths and positions along the range), and (c) not accounting for wave motion in the fathometer data. At greater depths, stratification of the water temperature, water density, and thermoclines would have affected the accuracy of the measurements. Because of the low slope in the offshore region, small errors in elevation resulted in significant excursions of the contours. Although the fathometer depth data seaward of the pier end are believed accurate to $\pm 0.2 \mathrm{~m}$, caution should be exercised when the data are used.

## Photography

## Aerial

79. Quarterly aerial photographic missions were performed by a contractor as part of the measurement program using a 9-in. negative format mapping aerial camera capable of black and white and color photography. All coverage was at least 55 percent overlap, with all flights flown as close as possible to periods of low tide and between 1000 and 1400 hours with less than 10 percent cloud cover.
80. The flight lines were concentrated near the FRF although one flight line extended from Cape Henry, Virginia, to Cape Hatteras, North Carolina. The flight lines and scale specifications are shown in Figure 6. Beach
81. As part of the visual observations, daily color slides of the beach were taken using a $35-\mathrm{mm}$ camera from the pier looking north and south. The


Figure 6. Quarterly aerial photography flight lines, 1980
location from which each picture was taken, date, time, and a brief description of the picture were marked on the slides, and an inventory was maintained. Analysis
82. There is no routine analysis of the photographic data except to inventory what is available.

## Sediment Data

Collection
83. Data collection consisted of weekly samples of the surface layer (top centimeter) of sand taken by hand from the foreshore near the upper swash limit. In addition to the above, during July through November daily foreshore samples were taken. The data were obtained from the same location approximately 500 m north of the FRF pier.

Analysis
84. The sediment samples were analyzed with a rapid sediment analyzer to determine the size distribution of the sample (Duane and Meisburger 1969).

## Data Availability

85. Table 3 is intended as a quick reference guide to show the dates for which various types of data are available. Wave and tide gage histories and other status information which may explain major gaps in the data are provided in the respective results sections and in the appendices.

## Results

86. This part provides results of the weather, wave, tidal, water characteristics, survey, photography, and sediment measurements made during the year. Although this report is intended to provide basic data for analysis by users, many of the daily observations have been summarized by month, season, or year to aid in interpretation. If individual data are required where summaries appear, the user can obtain the detailed information by following the procedures described in paragraphs 6 and 7.
Meteorological data
87. In this section, results of air temperature, precipitation, and wind speed and direction measurements are presented and discussed. Daily values are tabulated in Appendix A.
88. Air temperature. Air temperature measurements are summarized herein by describing the tendencies of the daily highest and lowest temperatures. Daily average temperatures were not computed since only one observation of the "present" was obtained in the morning, which could be misleading. Temperature distribution during 1980 was similar to past years of measurements.
89. Figure 7 and Table 4 present the monthly average and extreme high and low temperatures. The warmest months were July, August, and September, when the average high and low temperatures varied between $21^{\circ}$ and $30^{\circ} \mathrm{C}$. The highest temperature recorded in 1980 was $37^{\circ} \mathrm{C}$ on 2 August; the 1979 high was $43^{\circ} \mathrm{C}$ in July. The lowest temperature measured at the FRF to date, $-11^{\circ} \mathrm{C}$, was observed on the 18 th of February 1980. February continued to be the coldest month with the smallest difference between the average daily high of $3^{\circ} \mathrm{C}$ and low of $-2^{\circ} \mathrm{C}$. The widest range of temperatures occurred during the cold months, January through March, November, and December, with February
1980 Data Availability

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline FIRST WEEK MONTH \& \& 12
19
JAN \& ${ }^{19}$ \& \& ${ }^{9} 16$ \& 23 \& 18

MA \& 15 \& 22 \& 5 \& 12 \& ${ }^{9} 8$ \& 10 \& ${ }^{17}{ }^{2}$ \& 4 \& ${ }^{7} 14$ \& ${ }^{21}$ \& 8 \& 12 \& 26 \& ${ }^{2} 9$ \& 16 \& 3 \& 13 \& 20 \& 7 \& ${ }^{1} 18$ \& ${ }_{25}^{1}$ \& 8 \& 22 \& 6 \& ${ }^{3} 20$ \& 27 <br>
\hline MONTH \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline WEEK \& 1 \& 23 \& 4 \& 5.6 \& 7 \& 89 \& ) 10 \& 1112 \& 131 \& 14.15 \& \& 1718 \& \& 2021 \& 22 \& 2324 \& 25.26 \& 27 \& 2829 \& 303 \& 32 \& 3334 \& 35 \& 37 \& 39 \& 40.4 \& 42 \& 4344 \& 45.46 \& 47.4 \& 49 \& 50.51 \& 52 <br>
\hline WAVE \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline OFFSHORE WAVERIDER 620 \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& , \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline NEARSHORE WAVERIDER 610 \& \& 1 \& 1 \& \& \& \& \& 4 \& \& I \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline PIER END BAYLOR 625 \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& $\nabla$ \& <br>
\hline NEARSHORE BAYLOR 615 \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& $\square$ \& \& \& \& \& \& \& \& <br>
\hline NAGS HEAD 112 \& \& \& \& \& \& \& $\square$ \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline WEATHER \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
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\hline MICROBAROGRAPH \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline RAIN GAGE \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline PYRANOGRAPH \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline TIDE \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline PIER END (NOS NO. 865-1370) \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline WATER CHARACTERISTICS \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline TEMPERATURE \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& , \& \& \& \& A \& \& \& \& \& <br>
\hline VISIBILITY \& \& 2 \& \& R \& \& \& \& $\Gamma$ \& \& \& \& \& \& \& \& \& \& \& \&  \& \& \& \& , \& \& \& \& 2 \& \& \& \& \& <br>
\hline CURRENT \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline END OF PIER \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& , \& \& \& \& \& <br>
\hline SURVEY \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline PIER \& \& , \& 14 \& \& \& \& \& \& \& \& \& \& \& 2 \& \& 2 \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline BATHYMETRIC \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline PHOTOGRAPHY \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline BEACH \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline AERIAL FLIGHTS \& \& 1 \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& 1 \& \& \& \& \& \& <br>
\hline SEDIMENT \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline FORESHORE \& \& 1 \& \& \& \& \& \& \& \& 2 \& \& 1. \& \& \& \& 412 \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline OFFSHORE \& \& - \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& 1 \& \& \& \& \& <br>
\hline
\end{tabular}



Figure 7. Monthly high and low air
temperatures, 1980

Table 4
Meteorological Data Summary for 1980

| Month | Temperature ${ }^{\circ}{ }^{\circ} \mathrm{C}$ |  |  |  |  |  | Precipitation$\qquad$ | Wind |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | Average Speed $\mathrm{m} / \mathrm{sec}$ | ```Number of Obser- vations``` | Resultant |  | Extreme |  |  |
|  |  |  |  |  |  |  |  |  | Direction |  | Direction |  |
|  | Average | High | Date | Average | Low | Date |  |  | Speed $\mathrm{m} / \mathrm{sec}$ | $\begin{aligned} & \text { (deg from } \\ & \text { true } \mathrm{N}) \\ & \hline \end{aligned}$ | Speed $\mathrm{m} / \mathrm{sec}$ | $\begin{aligned} & \text { (deg from } \\ & \text { true } N \text { ) } \\ & \hline \end{aligned}$ | Date |
| Jan | 9 | 20 | 12 | 3 | -3 | 31 |  | 89 | 5.8 | 111 | 3.1 | 356 | 10.8 | $\begin{array}{r} 203 \\ 23 \end{array}$ | $\begin{aligned} & 11 \mathrm{th} \\ & 13 \mathrm{th} \end{aligned}$ |
| Feb | 3 | 19 | 23 | -2 | -11 | 18 | 66 | 5.6 | 103 | 2.4 | 337 | 11.3 | 338 | $\begin{aligned} & 10 \mathrm{th} \\ & 29 \mathrm{th} \end{aligned}$ |
| Mar | 12 | 23 | 22 | 4 | -7 | 3 | 89 | 6.1 | 121 | 1.4 | 334 | 20.6 | 23 | 2nd |
| Apr | 20 | 29 | 26 | 11 | 3 | 2 | 112 | 4.9 | 82 | 1.0 | 241 | 11.3 | $\begin{aligned} & 203 \\ & 248 \end{aligned}$ | $\begin{aligned} & 10 \mathrm{th} \\ & 15 \mathrm{th} \end{aligned}$ |
| May | 24 | 34 | 25 | 15 | 9 | 3 | 39 | 4.4 | 77 | 0.8 | 219 | 8.2 | $\begin{aligned} & 23 \\ & 45 \end{aligned}$ | $\begin{array}{r} 8 \mathrm{th} \\ 26 \mathrm{th} \end{array}$ |
| Jun | 27 | 34 | 30 | 18 | 11 | 21 | 60 | 5.5 | 93 | 0.8 | 210 | 12.4 | 248 | 7 th |
| Jul | 30 | 34 | 21 | 21 | 16 | 25 | 64 | 4.0 | 113 | 1.4 | 217 | 8.2 | 248 | 3rd |
| Aug | 30 | 37 | 2 | 21 | 15 | 25 | 48 | 4.5 | 96 | 0.7 | 284 | 8.2 | 23 | 22nd |
| Sep | 29 | 34 | 3 | 21 | 11 | 12 | 30 | 4.0 | 95 | 0.8 | 183 | 7.2 | 248 | $\begin{array}{r} 3 \mathrm{rd} \\ 23 \mathrm{rd} \end{array}$ |
| Oct | 21 | 27 | $\begin{aligned} & 11 \\ & 14 \end{aligned}$ | 13 | 5 | 27 | 73 | 5.4 | 113 | 0.7 | 323 | 14.9 | 248 | 25th |
| Nov | 16 | 23 | $\begin{array}{r} 5 \\ 10 \end{array}$ | 7 | -3 | 20 | 96 | 5.8 | 114 | 1.9 | 317 | 12.9 | 23 | 16th |
| Dec | 12 | 20 | 9 | 3 | -7 | 29 | 47 | 6.2 | 111 | 3.3 | 358 | 14.9 | 0 | 25th |
| Annua 1 | 19 | 37 | Aug | 11 | -11 | Feb | 793 | 5.2 | 1229 | 1.0 | 323 | 20.6 | 23 | Mar |

showing a $30^{\circ} \mathrm{C}$ variation. On the other hand, during January and February, the average high and low temperatures were most nearly the same, showing only a $5^{\circ}$ to $6^{\circ} \mathrm{C}$ difference. These tendencies reflect the complex interaction of (a) sea temperature, which varies slowly; (b) wind direction, which can change very quickly; and (c) winter air systems, which can come from the Arctic air masses to the north or from the tropical maritime air mass to the south. The opposite is true during the warm months of June through September when the temperature variation was $23^{\circ} \mathrm{C}$ (versus $30^{\circ} \mathrm{C}$ in February) and the average highs and lows varied by as much as $9^{\circ} \mathrm{C}$ in July, compared with $5^{\circ}$ to $6^{\circ} \mathrm{C}$ in January and February.
90. Precipitation (See Table 4). A total of 793 mm of precipitation was measured during 1980, 400 mm less than during 1979. Table 5 shows the monthly means, maxima, and minima from 1978 through 1980 at the FRF; absent during 1980 were monthly rainfalls in excess of 125 mm , as occurred in 1979 during January (180), May (239), and September (160), and in 1978 during March (137), May (145), June (130), and November (130). April was the wettest month of 1980 , with 112 mm of rain measured; September was the driest month, with 30 mm of rainfall. 1980 totals were the lowest in 7 of the months and the highest in 3 others.

Table 5
Monthly Precipitation Means, Maxima, and Minima at the FRF from 1978 Through 1980

| Month | $\begin{gathered} \text { Maxima } \\ \quad \mathrm{mm} \\ \hline \end{gathered}$ | Year | $\underset{\mathrm{mm}}{\operatorname{Minima}}$ | Year | $\begin{gathered} \text { Monthly } \\ \text { Mean } \\ 1978-80 \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Jan | 180 | 1979 | 89 | 1980 | 135 |
| Feb | 94 | 1979 | 66 | 1980 | 80 |
| Mar | 137 | 1978 | 64 | 1979 | 97 |
| Apr | 112 | 1980 | 71 | 1979 | 86 |
| May | 239 | 1979 | 39 | 1980 | 141 |
| Jun | 130 | 1978 | 60 | 1980 | 87 |
| Jul | 104 | 1978 | 64 | 1980 | 79 |
| Aug | 48 | 1979 | 36 | 1978 | 44 |
|  |  | $\begin{aligned} & \text { and } \\ & 1980 \end{aligned}$ |  |  |  |
| Sep | 160 | 1979 | 13 | 1978 | 68 |
| Oct | 73 | 1980 | 25 | 1978 | 51 |
| Nov | 130 | 1978 | 96 | 1980 | 108 |
| Dec | 84 | 1978 | 47 | 1980 | 60 |

91. Winds. Since the wind speed and direction data for 1980 were obtained every 6 hours (i.e., four times per day), the summaries are believed to be far superior to those previously published, which were based on only one daily value. No attempt will be made to compare the data summaries to prior years except for a brief explanation of why the data are believed to be more representative and less biased.
92. Land-sea breeze, weather fronts, and cyclonic and anticyclonic pressure systems all can cause rapid changes in both the wind speed and direction.
93. During March through September, the air temperatures were warmer than the seawater; likewise, from January to February and October to December, the air temperatures were colder. These temperature differences, along with differences in land temperature, can create daily coastal breezes which vary direction from morning to evening. Passage of weather systems can also cause the wind direction to change. Figure 8 shows all occasions during 1980 when the measured wind direction changed from offshore to onshore or vice-versa between 0700-1300, 1300-1900, and 1900-0100 hours. Onshore implies an easterly component of direction, while offshore is westerly; half arrows indicate the shift was either from or toward a direction without an easterly/westerly component; i.e., north or south.
94. Figure 8 shows the following tendencies in wind direction changes for 1980: (a) during the morning hours 0700-1300, when, typically, heating occurs after sunrise, the wind directions change from offshore/westerly to onshore/easterly; (b) conversely, in the evening from 1900-0100, during cooling times after sunset, wind directions shift from onshore to offshore; (c) wind direction changes during the afternoon hours from 1300 to 1900 appear mixed but show some correlation with the temperature differences between the ocean and the air/land (see Figure 24 and paragraph 124).
95. Measurements made once a day would be incomplete and would produce significantly biased information. As noted in the data analysis section, all wind information summaries except for the meteorological tables in Appendix A were created from observations made every 6 hours.
96. Measurements made every 6 hours, however, have the following shortcomings: peak conditions can be missed; precise times when fronts pass can only be bracketed; correlation to other physical phenomena, such as the rise and fall of the tides, can be difficult; etc. Hourly meteorological


[^1]measurements provide a very detailed description of the conditions; NWS collects wind data every hour and averages three successive observations to create data summaries every 3 hours, which appears to be the optimum meteorological sampling plan. However, the author's review of the continuous analog chart records confirmed that for all but a very few exceptions the 6-hour data sampling interval represents an unbiased assessment of wind conditions.
97. The annual average wind speed is in excess of $5 \mathrm{~m} / \mathrm{sec}$, with a strong western tendency (see Table 5). The highest speed (not gusts) was $20.6 \mathrm{~m} / \mathrm{sec}$ from the northeast recorded late on 2 March as the result of a very intense low-pressure system (shown in Figure 9) off the Virginia-Carolina coast on the morning of 3 March.
98. The annual wind rose for 1980 (Figure 10) indicates the winds blew onshore from the north side of the FRF pier (i.e., from north-northeast, northeast, and east-northeast directions) in excess of 26 percent of the time and from the south side 15 percent of the time. The strongest winds occurred during the cold months (Figure 11) and blew out of the north-northeast. Winds blowing from the north through east-northeast directions produce onshore moving waves and southerly moving surface currents, while winds from the east through south directions generally produce onshore waves and northerly moving surface currents. Over 51 percent of the time in 1980, the winds were offshore not producing onshore waves.
99. Wind roses (see Figure 12) for the spring and summer seasons AprilSeptember show the strong influence of the tropical maritime air mass which produces winds that blow from the southwesterly direction. A more northerly tendency for the winds during January through March is the result of the dominance of the arctic and polar continental air mass. The high speeds and frequent north-northeasterly directions observed for winds during the winter result from the continental high-pressure systems as well as extratropical and tropical cyclones (low-pressure systems). Extratropical winds originating as arctic and polar "Canadian high" air masses with clockwise circulations move east across the United States producing initially eastern and finally northern or northeasterly winds along this coast; extratropical "northeaster" storms associated with low-pressure (counterclockwise circulation) systems tend to move north along the Atlantic coast producing strong northeasterly winds followed by winds from north and northwest. October through December is a transition time when both the tropical and arctic air masses cause a great variety in the wind conditions.


Figure 9. Weather map for 3 March 1980 (pressure in millibars)

## 1980 OVERALL



Figure 10. 1980 annual wind rose for the FRF, reference true north

Figure 11. 1980 monthly wind roses for the FRF (Continued)

JUL 1980


SEP 1980
$\mathbf{3 3 7 . 5} \quad 0.0^{\circ} \quad \mathbf{2 2 . 5}{ }^{\circ}$
$315.0^{\circ}$


Resultant speed: $08 \mathrm{~m} / \mathrm{s}$
Direction: $183^{\circ}$


Resultant speed: $1.9 \mathrm{~m} / \mathrm{s}$
Resultant speed
Direction: $317^{\circ}$


OCT 1980
$337.5^{\circ} \quad 0.0^{\circ} \quad 22.5^{\circ}$


Resultant speed: $0.7 \mathrm{~m} / \mathrm{s}$
Direction: $323^{\circ}$

DEC 1980


Resultant speed. $3.3 \mathrm{~m} / \mathrm{s}$
Direction: $358^{\circ}$

Figure 11. (Concluded)

N

$225.0^{\circ}$

$$
202.5^{\circ} \quad 160.0^{\circ} \quad 157.5^{\circ}
$$

$$
\begin{aligned}
& \text { Resultant speed: } 2.2 \mathrm{~m} / \mathrm{s} \\
& \text { Direction: } 344^{\circ}
\end{aligned}
$$

$$
\text { Direction: } 344^{\circ}
$$

W

$$
337.5^{\circ} 0.0^{\circ} \text { JUL-SEP } 1980
$$

Resultant speed: $0.8 \mathrm{~m} / \mathrm{s}$
Direction: $221^{\circ}$

$$
\text { APR-JUN } 1980
$$

OCT-DEC 1980
$337.5^{\circ} \quad 0.0^{\circ} \quad 22.5^{\circ}$


Resultant speed; $1.8 \mathrm{~m} / \mathrm{s}$
Direction: $340^{\circ}$



Figure 12. 1980 seasonal wind roses for the $F R F$, reference true north
100. Although no tropical cyclones of hurricane strength made landfall along the North Carolina coast during 1980, Hurricane Charley in August and Hurricane George in September passed close enough to the FRF to influence the wave conditions (see Figure 13). Hurricane Charley caused moderate waves in excess of 1.5 m at the seaward end of the pier on 21 August while still in the subtropical storm stage before intensifying and moving east well offshore. Remnant 1-m-swell waves with associated 12- to 15 -second periods were evident during the first few days of September as Hurricane George moved north more than 600 km offshore.
101. 1980 was a typical year with respect to the winds at the FRF. Seasonal variation (see Figure 14) from southerly in the warm months to northerly in the cold with an overall western dominance was expected. The North Carolina coast above Cape Hatteras did not experience the extreme winds associated with the landfall of a hurricane, but was battered numerous times by strong northeasters.


Figure 13. Tracks of 1980 hurricane storms affecting the FRF


Figure 14. Annual and seasonal resultant wind speed and direction for the FRF, 1980

## Wave data

102. This section presents summaries from five wave sensors operated during 1980. The annual and seasonal significant wave height and peak spectral period statistics given below show a temporal and spatial variability of the wave climate at the FRF. Additionally, Appendix B contains gage histories and selected statistical summaries for each gage.
103. The 1980 data summaries are more complete than those for 1978 and 1979 (see Miller 1982); consequently, more confidence can be placed in the trends which are shown.
104. The wave height statistics (see tabulation below) vary as a function of gage installation: as water depth increases, so does average annual significant wave height. For example, the offshore Waverider buoy (gage
_-_ Gage
[^2]| Distance from $\qquad$ | Average <br> Annual <br> Water <br> Depth, m | Significant Height, m (Standard Deviation) |  | Peak Period, sec (Standard Deviation) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 200 | 5.2 | 0.87 | (0.44) | 9.00 | (2.81) |
| 100 | 1.5 | 0.66 | (0.32) | 8.79 | (3.45) |
| 500 | 8.4 | 0.87 | (0.44) | 9.00 | (2.81) |
| 600 | 7 | 0.99 | (0.63) | 9.17 | (2.81) |
| 3000 | 18 | 1.06 | (0.64) | 8.56 | (2.83) |

No. 620) is moored 3 km from shore where the water depth is 18 m ; the annual mean significant wave height was 1.06 m , with a $0.64-\mathrm{m}$ standard deviation. The nearshore Baylor gage (gage No. 615), located approximately 100 m from shore in 1.5 m of water, had an annual average significant wave height of 0.66 m , with a $0.32-\mathrm{m}$ standard deviation.
105. Individual data observations show a similar correlation between wave heights and depth; this correlation agrees with the trends of Vincent (1981) whose method for obtaining the maximum energy one could expect in a wind wave sea as a function of the water depth predicts the variation with depth.
106. Figure 15 presents the annual cumulative distribution of significant wave heights for the FRF gages for 1980. In general, the probability of high waves increases with water depth at the gage installation. The nearshore Baylor was in very shallow water inside the breaker zone, even during moderate to low wave conditions; consequently, these statistics represent a lower energy wave climate frequently due to waves breaking seaward of the gage.
107. Figure 16 is a histogram of the peak period distributions. Periods during highest wave conditions varied from 5 to 12 seconds depending on the distance the wave-generating area was from the pier; i.e., storms far offshore, say 500 km or more, would tend to produce near 12 -second wave periods, while more local storms would produce lower periods. Based on the occurrence of periods greater than 10 seconds, swell from very distant generating areas may have accounted for approximately 20 percent of the conditions at the coast. Seasonal, annual, and historic-height-versus-period distributions are presented in Appendix B.
108. Tables 6 and 7 present seasonal average significant height and peak period values, respectively. The highest waves occurred during January through March, while the lowest occurred during the summer (July-September). From October through December and from January through March, the greatest variety of wave conditions occurred, as reflected in the high standard deviations. During January through March, longer average peak periods occurred as compared to April through June when short-period waves dominated.
109. Wave roses generated for 1980 (see Figure 17) were based on visual measurements of the direction at which the primary wave train (i.e., the wave train having the largest heights) approached; these measurements were made daily (near 0700) at the seaward end of the FRF pier. Wave height was determined from the pier end Baylor staff gage at a corresponding time. The


Figure 15. 1980 annual wave height distributions


Figure 16. 1980 annual wave period distributions

Table 6
Seasonal Significant Wave Height Statistics for 1980

| Gage No. | Jan-Mar | No. Obs | Apr-Jun | No. Obs | Jul-Sep | No. Obs | Oct-Dec | No. Obs |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 620 |  |  |  |  |  |  |  |  |
| Height (m) | 1.37 | 184 | 0.85 | 162 | 0.72 | 151 | 1.14 | 311 |
| Standard deviation (m) | 0.65 |  | 0.34 |  | 0.33 |  | 0.75 |  |
| 610 |  |  |  |  |  |  |  |  |
| Height (m) | 1.45 | 129 | 0.72 | 172 | 0.71 | 76 | 1.02 | 330 |
| Standard deviation (m) | 0.77 |  | 0.33 |  | 0.30 | (None for July) | 0.64 |  |
| 625 |  |  |  |  |  |  |  |  |
| Height (m) | 1.21 | 203 | 0.69 | 218 | 0.63 | 170 | 1.07 | 315 |
| ```Standard deviation (m)``` | 0.62 |  | 0.30 |  | 0.28 |  | 0.58 |  |
| 615 |  |  |  |  |  |  |  |  |
| Height (m) | 0.93 | 149 | 0.56 | 216 | 0.53 | 168 | 0.67 | 337 |
| Standard deviation (m) | 0.45 |  | 0.20 |  | 0.17 |  | 0.30 |  |
| 112 |  |  |  |  |  |  |  |  |
| Height | 1.09 | 206 | 0.70 | 204 | 0.70 | 165 | 0.98 | 209 |
| Standard | 0.42 |  | 0.30 |  | 0.33 |  | 0.5 | (None |
| deviation (m) | 0.42 |  | 0.30 |  | 0.33 |  | 0.51 | Dec) |

Table 7
Seasonal Peak Wave Period Statistics for 1980

| Gage No. | Jan-Mar | No. Obs | Apr-Jun | No. Obs | Jul-Sep | No. Obs | Oct-Dec | No. Obs |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 620 |  |  |  |  |  |  |  |  |
| Period (sec) | 9.30 | 184 | 8.12 | 162 | 8.71 | 151 | 0.27 | 311 |
| $\begin{aligned} & \text { Standard } \\ & \text { deviation (sec) } \end{aligned}$ | 3.08 |  | 2.53 |  | 2.77 |  | 2.75 |  |
| 610 |  |  |  |  |  |  |  |  |
| Period (sec) | 10.08 | 129 | 8.79 | 172 | 9.32 |  | 8.99 | 330 |
| Standard deviation (sec) | 2.56 |  | 2.60 |  | 2.39 | (None for July) | 3.00 |  |
| 625 |  |  |  |  |  |  |  |  |
| Period (m) | 9.54 | 203 | 8.73 | 218 | 9.35 | 170 | 9.08 | 315 |
| ```Standard deviation (sec)``` | 3.05 |  | 2.49 |  | 2.97 |  | 2.95 |  |
| 615 |  |  |  |  |  |  |  |  |
| Period (sec) | 9.14 | 149 | 8.49 | 216 | 8.70 | 168 | 8.88 | 337 |
| Standard deviation (sec) | 3.35 |  | 3.22 |  | 3.56 |  | 3.56 |  |
| 112 |  |  |  |  |  |  |  |  |
| Period | 9.37 | 206 | 8.50 | 204 | 9.15 | 165 | 9.00 | 209 |
| Standard |  |  |  |  |  |  |  | (None |
| deviation (sec) | 2.96 |  | 2.82 |  | 2.65 |  | 2.71 | for <br> Dec) |

$20.0^{\circ}$
$42.5^{\circ}$

$132.5^{\circ}$
$155.0^{\circ}$


Wave Height (m)
a. 1980 overall wave rose

b. Resultant wave magnitude and directions

Figure 17. Directional wave summaries for 1980
angles are relative to the pier at $90^{\circ}$ and the beach oriented from $0^{\circ}$ to $180^{\circ}$.
110. Wave heights approached the beach most frequently ( 50 percent) from the north side of the pier, 5 percent were shore normal, and 45 percent came from the south side of the pier (Figure 17a). Although accounting for less than 2 percent, waves in excess of 2 m approached from angles greater than 60 deg north of the pier axis. The angles shown represent the frequency of wave occurrence in $22.5-\mathrm{deg}$ intervals, 11.25 deg on both sides of the angle displayed; except for the interval which includes the pier, which is split into angles greater than 76.25 deg and less than or equal to 90.0 deg ; i.e., includes the shore-normal directions and angles greater than 90.0 deg but less than or equal to 98.75 deg .
111. The resultant magnitude and direction of wave approach for the year was 0.5 m from an angle 13 deg north of the pier axis, respectively, as shown in Figure 17b. Figure 17b also indicates the seasonality of the wave climate: waves during the cold months of January through March and October through December showed a northeastern tendency, while during April through September the waves approached more nearly shore-normal or from south of the pier.
112. The seasonal wave roses presented in Figure 18 indicate there was a strong northeastern tendency during January through March. During the period from April through June, somewhat of a transition period, waves approached slightly more often from south of the pier, while waves in July through September had a strong southerly tendency. Waves during October through December showed the greatest tendency for approaching from the northeastern directions.
113. The tendency for waves to approach from north or south of the pier was very well correlated to the variation in the tendency for northern or southern winds (see paragraphs 91-101).
114. Although no hurricane severely affected the FRF, high wave conditions associated with "northeaster" storms occurred regularly during the cold months. On 16 occasions, the significant wave height exceeded 2 m at the seaward end of the pier, 25 percent of which persisted for 3 or more days (see the persistence tables in Appendix B). Three storms were particularly severe and accounted for the extreme significant wave heights measured at each gage location. First, on 3 March, a low pressure system located off the VirginiaNorth Carolina coast produced persistent onshore winds and high waves (see Figure 9); the high water levels produced significant wave heights $H_{s}$ in

APR-JUN 1980
$20.0^{\circ}$
$42.5^{\circ}$

$132.5^{\circ}$
$155.0^{\circ}$

Resultant wave height: 0.4 m Direction: $90^{\circ}$

E
OCT-DEC 1980
$20.0^{\circ}$
$42.5^{\circ}$

$155.0^{\circ}$

Resultant wave height: 0.8 m Direction: $66^{\circ}$

## S

Wave Height (m)


JAN-MAR 1980
$20.0^{\circ}$
$42.5^{\circ}$

$132.5^{\circ}$
$155.0^{\circ}$
Resultant wave height: 0.7 m Direction: $72^{\circ}$

Figure 18. Seasonal wave roses for the seaward end of FRF pier, reference beach 0 to 180 deg
excess of 2.3 m at the nearshore Baylor location. On October 25 th , peak conditions of $H_{s}=3.5 \mathrm{~m}$ were experienced at the pier end Baylor; this resulted from a northeaster coincident with a local perigean spring tide (see Miller et al. 1980). The last storm of 1980 on 29 December produced significant wave heights in excess of 2.9 m at the pier-end Baylor location (Miller et al. 1980).

Tidal data
115. This section presents the FRF tide and water level data. The various tide height values and water level datums due to predominantly astronomical forces of the sun and moon are discussed, followed by discussions of the extreme high- and low-water levels which were particularly influenced by meteorological conditions.
116. Monthly and annual tide statistics are shown in Table 8, with 1979 annual average and extremes included at the bottom for comparison. Tides at the FRF are semidiurnal, and the average tide range for the year was 102 cm . The average of all tide hights (msl) during the year, was 8 cm above NGVD. Mean higher high water (mhhw), the highest of the two daily high tide tide levels, was 68 cm and exceeded the mhw value by 9 cm ; mlw was -43 cm , and mean lower low water ( mllw ) was -47 cm for the year. (All tide values unless otherwise specified are referenced NGVD). The annual tide statistics for 1980 were very nearly the same as those for 1979.
117. Mean and extreme tide levels are presented as a function of month in Figure 19. The 5- to 6 -month periodicity in the rise and fall of the mean values presented are due in part to the inclination of the sun, a long-period astronomical tide constituent commonly referred to as Ssa, which has a periodicity of approximately 6 months. An additional explanation for the periodicity observed may be (a) astronomical forces with annual periodicity and (b) seasonal oscillation of the specific volume of the seawater as a function of temperature, called the steric effect (see Pattullo et al. 1955). The distribution of all hourly heights is presented relative to NGVD in Figure 20. Since the 1980 local MSL is 8 cm above NGVD, one can see that negative departures from the mean are larger than positive departures. Harris (1981) indicates it is not unusual for the magnitude of positive and negative departures from the mean to be unequal.
118. Figure 21 shows the distribution of the daily highest and lowest tide levels which occurred throughout the year. On 87 occasions, or 1 percent.

|  | mhhw | mhw | mt 1 | ms 1 | mlw | mI1w | mr | eh | Day/Hour | el | Day/Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Monthly for 1980 |  |  |  |  |  |  |  |  |  |  |  |
| Jan | 74.1 | 63.1 | 12.5 | 12.5 | -38.4 | -42.7 | 101.5 | 116.4 | 5/9.3 | -65.8 | 24/19.5 |
| Feb | 69.8 | 61.3 | 10.7 | 11.3 | -39.9 | -45.7 | 101.2 | 107.9 | 17/8.0 | -83.8 | 19/3.3 |
| Mar | 59.1 | 52.1 | 0.9 | 0.9 | -50.3 | $-54.3$ | 102.4 | 117.7 | 2/19.5 | -118.9 | 16/12.9 |
| Apr | 65.8 | 58.2 | 7.9 | 7.9 | -42.4 | -45.1 | 100.6 | 91.7 | 29/19.0 | -78.9 | $\begin{aligned} & 15 / 0.4 \\ & 16 / 1.9 \end{aligned}$ |
| May | 74.1 | 64.6 | 13.7 | 14.0 | -36.9 | -39.9 | 101.2 | 112.2 | 1/20.2 | -75.6 | 13/11.9 |
| Jun | 68.3 | 56.7 | 5.8 | 5.8 | -45.4 | -50.3 | 102.1 | 102.1 | 8/15.4 | -73.8 | 10/10.7 |
| Jul | 64.6 | 55.2 | 3.7 | 4.3 | -47.5 | -51.8 | 102.7 | 89.6 | 29/20.5 | -66.1 | 3/5.0 |
| Aug | 68.6 | 59.4 | 6.1 | 7.0 | -47.2 | -51.2 | 106.4 | 112.2 | 22/16.3 | -72.5 | 28/2.5 |
| Sep | 70.4 | 61.9 | 11.0 | 11.3 | -39.9 | $-43.3$ | 101.8 | 109.7 | 25/7.6 | -65.2 | 22/23.9 |
| Oct | 69.5 | 61.9 | 11.0 | 11.3 | -39.9 | -43.6 | 101.8 | 105.2 | 24/7.9 | -89.3 | 27/3.4 |
| Nov | 66.4 | 57.9 | 7.6 | 7.6 | -42.7 | -47.5 | 100.6 | 103.6 | 24/8.7 | -77.7 | 8/1.1 |
| Dec | 61.6 | 51.5 | 2.4 | 2.7 | -46.6 | -51.5 | 98.1 | 87.8 | 17/3.3 | $-83.2$ | 22/0.9 |
| Cumulative by Year |  |  |  |  |  |  |  |  | Month |  | Month |
| 1980 | 67.7 | 58.7 | 7.8 | 8.1 | -43.0 | -47.2 | 101.7 | 117.7 | Mar | -118.9 | Mar |
| 1979 | 68.9 | 60.0 | 8.5 | 9.1 | -43.0 | $-43.6$ | 100.0 | 120.7 | Feb | -95.1 | Sep |



Figure 19. Monthly tidal means and extremes for the seaward end of the FRF pier, 1980


Figure 20. Hourly tide height distribution, 1980


Figure 21. Distribution of 1980 daily highest and lowest tide levels, referenced to NGVD
of the daily highest tides, the level exceeded 111 cm (NGVD) (i.e., 102 cm above the 1980 msl ) ; likewise, for 1 percent of the time the daily lowest tides were less than 98 cm below NGVD or 107 cm below msl.
119. The following tabulation identifies times during the winter storm season months of 1980 when spring tides caused by perigee-syzygy alignment of the planets could be expected to produce extreme tidal heights:

[^3]| Type of Tide |
| :--- |
| Pseudo-perigean spring |
| Perigean spring |
| Perigean spring |
| Proxigean spring |
| Perigean spring |

Pseudo-perigean spring
Perigean spring
Perigean spring
Proxigean spring
Perigean spring
120. Wood (1978) discusses perigee-syzygy and the occurrence of coastal flooding (when coincident with strong, persistent onshore winds) associated with the reduced lunar distances during perigean spring tides. Wood attributes this to the reinforcing effect of the alignment of the sun and moon's gravitational forces on the earth and gives many examples of the effects this may have on the coast. This perigee-syzygy alignment, Wood states, may cause tidal flooding within a period of 1 to 3 days following (or in some few cases, a day or so preceding) the mean phase or epoch of the perigee-syzygy alignment. Tide heights in excess of 100 cm were in fact observed on 16-19 January, 17 February, 24 October, and 22-24 November.
121. The highest tidal heights, though, were not coincident with the perigean alignment but more nearly correlated to strong nonastronomical forces such as persistent onshore winds and high waves. The highest and second highest water levels observed were 118 cm on 2 March and 116 cm on 5 January, respectively.
122. The lowest water level observed was -119 cm on 16 March, a time when tides were expected to be higher than normal. A high-pressure system and sustained offshore winds dominated the water level producing forces and resulted in the annual extreme lowest tide height.

Water characteristics
123. Temperature. Daily sea surface water temperatures at the seaward end of the FRF pier are presented as a function of time in Figure 22, and the distribution of temperatures is shown in Figure 23. The difference in daily temperatures was greatest during July when a $9^{\circ} \mathrm{C}$ change was observed over a 24 -hour period, see Figure 22. This difference is attributed to frequent offshore winds which blow the warm surface water offshore allowing upward and landward circulation of the much colder bottom water. Onshore winds, on the other hand, reverse the circulation pattern, piling up surface water along the shoreline and creating a seaward return flow along the bottom.
124. As can be seen in Figure 23, for less than 20 percent of the time during 1980 the water temperature exceeded $20^{\circ} \mathrm{C}$, while for less than 10 percent of the time the temperatures were lower than $4^{\circ} \mathrm{C}$. Seasonal distribution of the temperature indicates the coldest temperatures occurred from JanuaryMarch, while the warmest were from July-September as might be expected.
125. The monthly mean sea surface temperatures measured at the seaward end of the FRF pier (see tabulation below) varied in phase with the air


Figure 22. Sea surface temperatures, 1980, for the seaward end of the FRF pier


Figure 23. Annual and seasonal distributions of sea surface temperatures, 1980, at the FRF
temperatures presented previously, but the temperature ranges varied inversely from those of air temperature. July was a time of maximum range in water temperature and minimum range in air temperature, while February's ranges were at a minimum for water and a maximum for air.

| Month 1980 |  |  |
| :--- | :---: | :---: |
| Jan | Sea Surface <br> Temperature, ${ }^{\circ} \mathrm{C}$ | Visibility <br> m |
| Feb | 6.8 | 1.3 |
| Mar | 3.5 | 1.4 |
| Apr | 5.5 | 1.0 |
| May | 11.2 | 2.5 |
| Jun | 16.2 | 2.7 |
| Jul | 18.5 | 3.9 |
| Aug | 20.1 | 4.6 |
| Sep | $\%$ | 3.4 |
| Oct | 22.1 | 2.9 |
| Nov | 19.0 | 1.4 |
| Dec | 13.2 | 1.0 |

* No measurement.

126. Figure 24 shows the daily difference between the surface water temperature and the air temperatures measured behind the dune 1.5 m above ground. This temperature difference can be important to coastal engineers when assessing storm surge and wave growth values because of the modification of wind stress and, consequently, the transfer of momentum from the wind to the sea surface. When the air is cooler than the water, increased turbulence causes increased momentum transfer for a given wind speed; conversely, when the air is warmer, a stable condition results and less momentum for a given wind speed is transferred. The largest difference was $16^{\circ} \mathrm{C}$ which occurred during August. During October through February, the water was warmer than the air occasionally by more than $10^{\circ} \mathrm{C}$. March and September are periods of transition, with warming and cooling of the coastal waters occurring respectively.
127. Visibility. Visibility in coastal nearshore waters depends on the amount of salts, soluble organic material, detritus, living organisms, and inorganic particles in the water. These dissolved and suspended materials

Figure 24. Air/water temperature differences, 1980,
for the seaward end of the FRF pier
change the adsorption and attenuation characteristics of the water which vary daily and throughout the year. Daily water visibility measurements made at the seaward end of the pier are shown as a function of time in Figure 25.
128. The daily visibility is highly variable. Fifty percent of the time the surface visibility at the seaward end of the pier is less than 2 m (Figure 26). Visibility in excess of 6 m occurred about 10 percent of the time (or 30 days) during 1980, predominantly in July, August, and September. The greatest range of visibility occurred in August when greater than 5 m changes over 24 hours were not uncommon. Visibility varies much the same as surface water temperature (see tabulation, paragraph 125); onshore winds tend to bring clearer surface waters to the coast, and offshore winds produce upwelling of more turbid bottom water.

Current Data
129. Currents measured at the seaward end of the FRF pier and 500 m up. drift of the pier on the beach are discussed in this section. Monthly and annual summaries as well as time histories of the daily values (Figures 27 and 28) are presented. The monthly average surface current speeds (see tabulation on page 67) were strongest toward the south at the pier end during the winter months. These currents were caused by predominantly northerly winds and persistently high wave conditions. From April through September, the winds blew predominantly from southerly directions and more frequently produced northwardly moving currents as was especially evident in the wave-induced beach currents.
130. Current speeds were generally higher and the seasonality of the current direction was more evident on the beach than at the seaward end of the pier.
131. Peak current speeds were generally higher and more frequent for southward flow than for northward-moving water except for the persistent northerly currents on the beach during the summer months (Figure 28).

Survey results
132. Weekly pier surveys from both sides of the pier and time histories of bottom elevations at selected locations along the pier are presented in Appendix C.
133. Bathymetry. Figure 29 is a contour diagram of the 1980 beach and nearshore bathymetry; the offshore data are not included due to the questionable accuracy of the depth information.


Figure 25. Water visibility, 1980, for the seaward end of the FRF pier


Figure 26. Distribution of visibility measurements, 1980, at the FRF



| Monthly | Mean Surface Currents, cm/sec* |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Pier End |  |  |  | Beach 1980 |
|  | 1980 | 1979 | 1978 | Monthly <br> Average |  |
| Jan | 26 | 15 | 15 | 19 | 6 |
| Feb | 31 | 22 | 37 | 30 | 19 |
| Mar | 8 | 20 | 37 | 22 | 4 |
| Apr | 4 | 10 | 15 | 10 | 6 |
| May | 15 | 13 | 10 | 13 | 3 |
| Jun | 2 | 21 | -1 | 7 | -19 |
| Jul | -1 | 6 | 4 | 3 | -22 |
| Aug | 8 | 7 | 4 | 6 | -10 |
| Sep | 4 | 14 | 12 | 10 | -14 |
| Oct | 4 | 8 | 10 | 7 | 27 |
| Nov | 19 |  | 9 | 14 | 27 |
| Dec | 13 | 7 | 9 | 10 | 14 |
| Annual Mean | 11 | 12 | 11 | 11 | 3 |

$\%+=$ southward; - = northward.


Figure 29. FRF bathymetry for October 1980
134. Near the pier, contours deeper than 3 m were significantly modified. The $7-\mathrm{m}$ contour diverged some 250 m towards shore, but the $3-\mathrm{m}$ contour was relatively unchanged showing only a $20-\mathrm{m}$ change. This bending of the contours near the pier is persistent throughout the year, although the absolute depth of the trough under the pier changes as a function of changing wave and current conditions.
135. Pier profiles. Between April and September, the profiles under the pier had a consistent shape and only about a 1-m variation seaward of the local msl beach intercept (Figure 30). During the winter months January through March and October through December, the profiles exhibit a much more varied shape and large changes all along the profile (Figure 31).
136. Figure 32 shows the magnitude of the change in elevation as a function of the distance along the pier. The development and movement of bars account for the largest of the changes.
137. The weekly profiles from both sides of the FRF pier presented in Appendix $C$ show when the bar system developed, how it moved, and when it was no longer present. As the bathymetry shows, the pier's influence causes these profiles to be considerably different from those farther than 150 m north or south of the pier.
138. The variations of bottom elevations as a function of time throughout the year at a select number of stations are also presented in Appendix C. Large changes over a short time are generally attributable to storms which cause rapid bar movement and large changes in bathymetry. Gradual changes over a season are associated with periods of varying wave conditions and reflect accretional or erosional periods. The largest changes occur nearshore where bar movement is the greatest.
Photographic data
139. In this section, photographic data used to document the beach condition in the vicinity of the FRF are described. Figure 33 shows samples of daily photographs of the beach taken from the pier looking both north and south. The cut seen in the 20 August photograph is a summer feature and occurs after periods of persistent southerly winds. During 1980, the cut was less dramatic than in prior years and was evident for only a short time in late August.
140. In addition to the daily beach photographs taken, quarterly aerial photographic missions were flown. Table 9 is an inventory of the photography obtained during 1980, and Figure 34 is a sample photographic negative showing the FRF pier on the 16th of July.
Sediment Data
141. In this section, results of sediment analyses of sand samples taken from the foreshore throughout the year are presented. In addition, results are presented from one survey in October along a $30-\mathrm{km}$-long transect



Figure 30. Pier profile envelopes, April-September 1980


Figure 31. Pier profile envelopes, January-March and October-December 1980


Figure 32. Bottom elevation changes along the FRF pier, 1980

South view, 4 Feb 1980
18

north from the FRF pier
North view, 20 Aug 1980

North view, 15 Mar 1980

Figure 33. Beach photographs looking

Table 9
1980 Aexial Photography Inventory

| Date | Flight Line No. 1 | Flight Line No. 2. | Flight Line No. 3 | (Negatives) <br> Film Format |
| :---: | :---: | :---: | :---: | :---: |
| 16 Jan |  | 2 miles north to 2 miles south ( $1: 6,000$ ) |  | Color |
|  |  | 2 miles north to 2 miles south $(1: 2,400)$ |  | Color |
| 16 Jan | Cape Henry to Cape <br> Hatteras (1:12,000) | +2 miles north to the pier ( $1: 6,000$ ) | Currituck Sound to Atlantic Ocean (1:12,000) | B/W |
| 15 Apr |  | ```2 miles north to 2 miles south (1:6,000)``` |  | Color |
|  |  | 2 miles north to 2 miles south ( $1: 2,400$ ) |  | Color |
| 15 Jul | ```Corolla to Oregon Inlet (1:12,000)``` | ```2 miles north to 2 miles south (1:6,000)``` | Currituck Sound to <br> Atlantic Ocean <br> (1:12,000) | $B / W$ |
| 15 Oct | Corolla to Kitty <br> Haw'k ( $1: 6,000$ ) |  |  | $B / W$ |

from the seaward end of the pier to the $33-\mathrm{m}$ water depth.
142. Between 4 January and 30 December, 130 surface sand samples were taken from the upper swash zone of the foreshore, 500 m updrift from the pier. Weekly samples were taken from January through June and during December, while daily samples were taken from July through November. Table 10 presents statistical parameters of the sediment distribution for each sample, and Figure 35 shows the mean grain size as determined from CERC's Rapid Sediment Analyzer (RSA) analysis. Considerable scatter is evident, but a trend for smaller sizes during the relatively low wave conditions during July and larger sizes in December and January (times of high wave conditions) can be seen. Caution should be exercised when using the mean of a sample to infer typical grain sizes found on the beach. Frequently, the mean may not be a true indicator of a predominant size found in the sample, but simply an average based on the distribution of sizes. This is particularly true as the sizes become more coarse, since the analysis reports frequencies at $1 / 2-$ phi intervals and increasingly larger intervals of sizes occur between classification limits as shown in the tabulation on page 77.
143. As an example, a sample taken on 20 November 1980 is described on page 78. The frequency distribution, given in the tabulation, shows a


Table 10
Statistical Parameters of the 1980 Foreshore Sediment Samples

| Date | Median |  | Mean |  | Standard <br> Deviation <br> phi | $\begin{gathered} \text { Skewness } \\ \quad \text { phi } \end{gathered}$ | Kurtosis phi |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Phi | mm | Phi | mm |  |  |  |
| 0104 | 0.84 | 0.560 | 1.21 | 0.431 | 0.91 | 1.23 | 3.21 |
| 0109 | 1.71 | 0.306 | 1.79 | 0.289 | 0.54 | 0.74 | 2.87 |
| 0119 | 0.76 | 0.589 | 1.10 | 0.467 | 0.81 | 1.34 | 3.53 |
| 0123 | 0.98 | 0.508 | 1.06 | 0.480 | 0.80 | 0.41 | 2.99 |
| 0201 | 1.42 | 0.373 | 1.40 | 0.380 | 0.86 | -0.17 | 2.49 |
| 0402 | 0.90 | 0.537 | 1.01 | 0.498 | 0.72 | 0.31 | 3.51 |
| 0413 | 1.33 | 0.399 | 1.31 | 0.405 | 0.76 | -0.03 | 2.34 |
| 0503 | 1.12 | 0.462 | 1.24 | 0.423 | 0.63 | 0.37 | 3.49 |
| 0606 | 1.83 | 0.282 | 1.81 | 0.284 | 0.64 | -0.90 | 4.58 |
| 0613 | 1.40 | 0.380 | 1.32 | 0.400 | 0.80 | -0.69 | 3.29 |
| 0701 | 1.46 | 0.364 | 1.58 | 0.333 | 0.53 | 0.45 | 2.59 |
| 0702 | 1.69 | 0.311 | 1.75 | 0.297 | 0.65 | -0.54 | 4.97 |
| 0703 | 1.68 | 0.312 | 1.65 | 0.319 | 0.95 | -0.44 | 3.05 |
| 0704 | 1.68 | 0.311 | 1.74 | 0.300 | 0.65 | -0.21 | 3.46 |
| 0705 | 1.89 | 0.270 | 2.04 | 0.243 | 0.82 | 0.53 | 3.34 |
| 0706 | 1.45 | 0.366 | 1.55 | 0.342 | 0.67 | 0.41 | 2.66 |
| 0707 | 1.80 | 0.288 | 1.88 | 0.272 | 0.49 | 0.58 | 2.64 |
| 0708 | 0.41 | 0.752 | 0.62 | 0.649 | 0.87 | 0.57 | 2.13 |
| 0709 | 2.10 | 0.233 | 2.18 | 0.220 | 0.57 | 0.66 | 2.84 |
| 0710 | 2.20 | 0.218 | 2.23 | 0.213 | 0.41 | 0.06 | 2.95 |
| 0711 | 1.97 | 0.256 | 1.95 | 0.258 | 0.52 | -0.72 | 4.49 |
| 0712 | 1.93 | 0.263 | 1.93 | 0.263 | 0.49 | -0.11 | 2.91 |
| 0713 | 0.98 | 0.505 | 1.21 | 0.431 | 0.66 | 1.27 | 4.06 |
| 0714 | 1.37 | 0.386 | 1.48 | 0.359 | 0.49 | 0.53 | 2.70 |
| 0715 | 1.86 | 0.275 | 1.93 | 0.263 | 0.47 | 0.67 | 2.86 |
| 0716 | 1.96 | 0.258 | 2.02 | 0.247 | 0.59 | 0.06 | 3.72 |
| 0718 | 2.06 | 0.240 | 2.03 | 0.245 | 0.73 | -1.26 | 6.51 |
| 0719 | 1.74 | 0.299 | 1.88 | 0.271 | 0.58 | 0.53 | 3.67 |
| 0720 | 1.87 | 0.274 | 1.96 | 0.257 | 0.47 | 0.57 | 2.96 |
| 0721 | 2.11 | 0.232 | 2.17 | 0.222 | 0.49 | 0.54 | 2.89 |
| 0722 | 1.99 | 0.52 | 2.00 | 0.251 | 0.42 | 0.24 | 2.17 |
| 0723 | 2.01 | 0.248 | 1.99 | 0.252 | 0.54 | -1.92 | 10.20 |
| 0724 | 1.80 | 0.287 | 1.87 | 0.273 | 0.46 | 0.19 | 3.27 |
| 0726 | 1.79 | 0.289 | 1.90 | 0.268 | 0.52 | 0.78 | 2.87 |
| 0727 | 0.78 | 0.584 | 0.98 | 0.506 | 0.54 | 1.19 | 3.41 |
| 0729 | 1.41 | 0.375 | 1.54 | 0.343 | 0.46 | 0.83 | 2.83 |
| 0730 | 1.25 | 0.420 | 1.41 | 0.376 | 0.74 | 0.39 | 3.15 |
| 0731 | 1.32 | 0.400 | 1.45 | 0.366 | 0.63 | 0.40 | 2.83 |
| 0801 | 1.82 | 0.283 | 1.91 | 0.266 | 0.54 | 0.25 | 4.08 |
| 0802 | 1.77 | 0.293 | 1.88 | 0.272 | 0.61 | 0.05 | 3.32 |
| 0803 | 1.69 | 0.310 | 1.76 | 0.295 | 0.51 | 0.37 | 2.27 |
| 0804 | 1.53 | 0.347 | 1.52 | 0.348 | 0.74 | -0.51 | 3.17 |
| 0805 | 1.97 | 0.256 | 1.99 | 0.252 | 0.49 | 0.04 | 3.23 |
| 0806 | 1.81 | 0.286 | 1.82 | 0.283 | 0.58 | 0.18 | 2.55 |
| 0807 | 1.39 | 0.381 | 1.55 | 0.341 | 0.74 | 0.77 | 3.04 |
| 0808 | 1.44 | 0.368 | 1.56 | 0.339 | 0.64 | 0.50 | 3.93 |
| 0809 | 1.57 | 0.337 | 1.65 | 0.318 | 0.69 | 0.11 | 3.29 |
| 0810 | 1.12 | 0.459 | 1.18 | 0.443 | 0.68 | 0.15 | 2.90 |
| 0813 | 1.58 | 0.334 | 1.68 | 0.313 | 0.51 | 0.57 | 2.57 |
| 0814 | 2.10 | 0.233 | 2.08 | 0.236 | 0.47 | 0.07 | 2.35 |
| 0815 | 1.67 | 0.314 | 1.66 | 0.315 | 0.62 | -0.45 | 3.92 |
| 0817 | 1.31 | 0.403 | 1.38 | 0.384 | 0.55 | 0.08 | 4.14 |
| 0818 | 1.12 | 0.459 | 1.30 | 0.406 | 0.62 | 0.91 | 3.16 |
| 0819 | 1.10 | 0.465 | 1.12 | 0.460 | 0.75 | 0.05 | 2.48 |
| 0822 | 1.05 | 0.483 | 1.13 | 0.458 | 0.53 | 0.33 | 3.34 |
| 0823 | 0.81 | 0.571 | 0.99 | 0.504 | 0.73 | 0.61 | 2.66 |
| 0824 | 0.83 | 0.562 | 0.99 | 0.505 | 0.73 | 0.62 | 2.50 |
| 0825 | 0.83 | 0.563 | 1.01 | 0.495 | 0.67 | 0.75 | 3.56 |
| 0826 | 0.14 | 0.908 | 0.47 | 0.720 | 0.95 | 1.07 | 2.90 |
| 0828 | 0.39 | 0.762 | 0.49 | 0.714 | 0.43 | 1.49 | 5.47 |
| 0829 | 1.23 | 0.428 | 1.34 | 0.396 | 0.75 | 0.26 | 2.41 |
| 0830 | 1.78 | 0.292 | 1.78 | 0.292 | 0.62 | -0.88 | 5.25 |
| 0831 | 1.29 | 0.409 | 1.33 | 0.399 | 0.69 | 0.15 | 1.96 |

(Continued)

Table 10 (Concluded)

| Date | Median |  | Mean |  | Standard Deviation phi | Skewness$\qquad$ | Kurtosis$\qquad$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Phi | mm | Phi | mm |  |  |  |
| 0902 | 1.87 | 0.274 | 1.91 | 0.267 | 0.62 | -0.68 | 5.73 |
| 0903 | 1.69 | 0.310 | 1.79 | 0.289 | 0.56 | 0.57 | 2.37 |
| 0904 | 1.69 | 0.310 | 1.79 | 0.290 | 0.60 | 0.49 | 2.76 |
| 0905 | 0.77 | 0.588 | 0.92 | 0.530 | 0.79 | 0.47 | 2.69 |
| 0908 | 0.15 | 0.899 | 0.46 | 0.728 | 0.85 | 1.86 | 5.10 |
| 0910 | 1.41 | 0.377 | 1.46 | 0.364 | 0.67 | 0.24 | 2.51 |
| 0911 | 1.26 | 0.416 | 1.34 | 0.394 | 0.56 | 0.47 | 2.94 |
| 0912 | 1.47 | 0.360 | 1.50 | 0.354 | 0.68 | -0.46 | 3.87 |
| 0915 | 1.49 | 0.356 | 1.58 | 0.334 | 0.52 | 0.10 | 2.49 |
| 0916 | 1.43 | 0.372 | 1.56 | 0.339 | 0.64 | 0.59 | 2.99 |
| 0917 | 1.51 | 0.352 | 1.59 | 0.333 | 0.56 | 0.36 | 3.00 |
| 0918 | 1.43 | 0.371 | 1.57 | 0.337 | 0.54 | 0.79 | 2.85 |
| 0919 | 1.01 | 0.497 | 1.15 | 0.451 | 0.78 | 0.38 | 2.88 |
| 0922 | 1.04 | 0.486 | 1.11 | 0.464 | 0.93 | 0.17 | 2.51 |
| 0923 | 1.37 | 0.387 | 1.51 | 0.351 | 0.67 | 0.49 | 3.24 |
| 0924 | 1.04 | 0.486 | 1.07 | 0.477 | 0.79 | 0.20 | 2.28 |
| 0925 | 1.38 | 0.383 | 1.49 | 0.355 | 0.60 | 0.55 | 2.62 |
| 0926 | 1.43 | 0.370 | 1.57 | 0.337 | 0.52 | 0.91 | 3.11 |
| 0929 | 1.76 | 0.296 | 1.77 | 0.292 | 0.43 | 0.12 | 2.30 |
| 0930 | 1.25 | 0.420 | 1.32 | 0.400 | 0.58 | 0.43 | 2.58 |
| 1001 | 1.39 | 0.380 | 1.45 | 0.366 | 0.71 | -0.06 | 3.01 |
| 1002 | 1.16 | 0.448 | 1.19 | 0.437 | 0.90 | -0.04 | 2.16 |
| 1003 | 0.67 | 0.627 | 0.90 | 0.535 | 0.82 | 0.54 | 2.25 |
| 1006 | 0.99 | 0.505 | 1.06 | 0.478 | 0.49 | 0.37 | 2.94 |
| 1008 | 0.43 | 0.741 | 0.53 | 0.691 | 0.43 | 0.63 | 3.86 |
| 1009 | 0.96 | 0.515 | 1.08 | 0.473 | 0.68 | 0.43 | 2.93 |
| 1010 | 0.97 | 0.510 | 1.13 | 0.456 | 0.76 | 0.18 | 2.31 |
| 1011 | 2.41 | 0.189 | 2.45 | 0.182 | 0.29 | 0.68 | 2.61 |
| 1014 | 1.19 | 0.437 | 1.27 | 0.414 | 0.70 | 0.23 | 2.29 |
| 1015 | 1.59 | 0.333 | 1.62 | 0.324 | 0.55 | -0.27 | 3.27 |
| 1016 | 1.69 | 0.309 | 1.73 | 0.302 | 0.48 | -0.29 | 3.59 |
| 1017 | 1.62 | 0.324 | 1.68 | 0.311 | 0.51 | -0.09 | 3.06 |
| 1020 | 1.56 | 0.340 | 1.62 | 0.324 | 0.59 | 0.10 | 2.92 |
| 1023 | 2.38 | 0.192 | 2.39 | 0.191 | 0.06 | 3.71 | 14.76 |
| 1024 | 1.49 | 0.357 | 1.56 | 0.340 | 0.37 | 0.48 | 2.34 |
| 1027 | 0.93 | 0.525 | 0.92 | 0.528 | 0.79 | -0.01 | 2.23 |
| 1028 | 1.14 | 0.453 | 1.25 | 0.421 | 0.65 | 0.41 | 2.51 |
| 1030 | 1.08 | 0.473 | 1.22 | 0.428 | 0.72 | 0.49 | 2.90 |
| 1031 | 1.10 | 0.466 | 1.18 | 0.440 | 0.68 | 0.09 | 3.24 |
| 1101 | 1.45 | 0.366 | 1.58 | 0.333 | 0.53 | 0.74 | 2.90 |
| 1103 | 1.05 | 0.486 | 1.13 | 0.457 | 0.50 | 0.63 | 3.04 |
| 1104 | 0.81 | 0.568 | 0.95 | 0.518 | 0.54 | 0.86 | 4.03 |
| 1105 | 0.93 | 0.526 | 0.98 | 0.507 | 0.62 | -0.09 | 3.65 |
| 1106 | 1.23 | 0.427 | 1.37 | 0.387 | 0.58 | 0.53 | 2.73 |
| 1107 | -0.04 | 1.030 | -0.01 | 1.005 | 0.23 | 0.74 | 4.66 |
| 1110 | 1.53 | 0.347 | 1.59 | 0.333 | 0.57 | -0.38 | 3.94 |
| 1112 | 1.45 | 0.366 | 1.57 | 0.336 | 0.58 | 0.54 | 3.00 |
| 1113 | 1.44 | 0.368 | 1.50 | 0.354 | 0.52 | 0.26 | 2.96 |
| 1114 | 1.33 | 0.397 | 1.41 | 0.376 | 0.56 | 0.29 | 3.18 |
| 1117 | 1.21 | 0.433 | 1.33 | 0.399 | 0.64 | 0.23 | 3.02 |
| 1118 | 0.96 | 0.513 | 1.11 | 0.464 | 0.77 | 0.35 | 3.29 |
| 1119 | 0.94 | 0.522 | 1.19 | 0.439 | 0.71 | 1.15 | 3.21 |
| 1120 | 0.18 | 0.883 | 0.28 | 0.821 | 0.47 | 1.86 | 6.74 |
| 1121 | 0.40 | 0.760 | 0.61 | 0.655 | 0.75 | 0.88 | 2.88 |
| 1124 | 0.58 | 0.670 | 0.63 | 0.561 | 0.73 | 1.01 | 3.40 |
| 1125 | 0.84 | 0.560 | 0.98 | 0.507 | 0.70 | 0.69 | 2.95 |
| 1126 | 0.48 | 0.717 | 0.71 | 0.611 | 0.59 | 1.31 | 4.10 |
| 1128 | 1.16 | 0.446 | 1.25 | 0.419 | 0.78 | 0.40 | 2.37 |
| 1201 | 1.44 | 0.368 | 1.51 | 0.350 | 0.65 | -0.12 | 3.90 |
| 1208 | 0.57 | 0.674 | 0.82 | 0.565 | 0.80 | 0.76 | 2.50 |
| 1215 | 1.34 | 0.395 | 1.48 | 0.359 | 0.65 | 0.42 | 2.60 |
| 1224 | 1.07 | 0.475 | 1.21 | 0.433 | 0.58 | 0.63 | 3.25 |
| 1230 | 0.98 | 0.509 | 1.14 | 0.452 | 0.60 | 0.97 | 3.21 |



## HONTH

Figure 35. RSA-determined mean grain size of the foreshore samples taken in 1980, 500 m north of the FRF pier

| $\frac{\text { Phi Size }}{}$ | mm Size <br> -1.00 | mm Interval <br> -0.50 |
| :---: | :---: | :---: |
| 0.00 | 1.000 | 0.586 |
| 0.50 | 1.000 | 0.414 |
| 1.00 | 0.707 | 0.293 |
| 1.50 | 0.500 | 0.207 |
| 2.00 | 0.354 | 0.146 |
| 2.50 | 0.250 | 0.104 |
| 3.00 | 0.177 | 0.073 |
| 3.50 | 0.125 | 0.052 |
| 4.00 | 0.088 | 0.037 |
|  | 0.063 | 0.025 |

dominance of the $0.707-\mathrm{mm}$ size ( $0.5 \emptyset$ ) with some $1.000-\mathrm{mm}$ ( $0.0 \emptyset$ ) sizes present. The mean, reported at 0.821 , is not similar to either size present. The mean is useful for generally classifying the material sizes on the beach; i.e., for distinguishing between coarse, medium, fine, or very fine sand sizes in a sample. The standard deviation is useful for determining the sorting characteristics of the sample; i.e., the similarity of the sand sizes.

| $1+20$ |  |  |  | 11-20-80 | STATISTICAL | AMETERS PhI | MM. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | PHI | MM. ${ }^{\text {P }}$ | FREGUENCY | CUMULATIVE | MEDIAN | .18 | . 881 |
|  | S12E | SI2E | PERCENT | PERCENT | MEAN | -28 | .821 |
|  | -1.00 | 2.000 | 0.00 | $0.00 S T A N D A R D$ | DEVIATIUN | .47 |  |
|  | -. 50 | 1.414 | . 63 | . 63 | SKEHNESS | 1.86 |  |
|  | 0.00 | 1.000 | 16.01 | 16.64 | KURTOSIS | 6.74 |  |
|  | . 50 | .707 | 08.70 | 85.34 |  |  |  |
|  | 1.00 | . 500 | 6.25 | 41.54 |  |  |  |
|  | 1.50 | . 354 | ?.77 | 94.37 |  |  |  |
|  | 2.00 | . 250 | 5.63 | 100.00 |  |  |  |
|  | 2.50 | .177 | 0,00 | 100.00 |  |  |  |
|  | 4.00 | .063 | 0.00 | 100.00 |  |  |  |

144. In addition to the analysis of foreshore samples collected at regular time intervals, sediment characteristics were measured on one occasion as a function of water depth and distance offshore (Williams 1982). From 27 through 31 October 1980, grab-type sediment samples were obtained at 24 sites in a line parallel to the pier from -6.3 m water depths off the pier's end to -32.9 m water depths at the end of the transect some 37 km from shore (Figure 36).
145. The 24 sediment samples were visually and microscopically examined, and the primary grain size parameters were derived by analysis using the CERC RSA. The sediments were all fairly similar in color and composition and ranged from very fine to very coarse gray sand. In general, the samples from the -6.3 m contour seaward to about the -17 m contour (Figure 37 ) were gray, moderately well sorted, very fine to fine quartz sand, findings which are in agreement with the 1979 survey (Miller, 1982) of 13 short core samples taken from the shore seaward to a depth of -15.8 m . Sediments at sample site number 14 , taken near the crest of the second shoal, contrast the most with the other samples in the transect. The sediment in this sample was medium to very coarse quartz sand with rock fragments and broken shell fragments very similar to typical samples from the beach at the FRF.


Figure 36. Sediment sample locations for October 1980 survey



Figure 37. Mean sediment grain size and position along the October 1980 survey line

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1. Meterological data summaries are explained below:
a. Keynotes on meteorological observations (Page A2). Presented for use in interpreting the monthly meteorological data tables is a list of observation symbols and their definitions.
b. Monthly data tables (Pages A3-A14). The daily meteorological observations are tabulated by month. The "Amount of Precipitation" represents the total precipitation since the rain gage was last reset (i.e., the bucket was emptied); consequently, the values entered on a Monday represent the total rainfall since the previous reading, which frequently was made on the previous Friday. The same situation holds true for the maximum and minimum thermometers, which are manually reset: the values reported represent the temperature extremes since the last resetting.
2. Monthly average cloud cover, visibility, atmospheric pressure, temperature extremes, dew point temperatures, and wind speed values, as well as the total monthly precipitation, are entered at the bottom of each table.

Table A1
Keynotes on Meterological Observations

1. Wind Field Gustiness (WFG): A plus symbol (+) is entered if the wind speed varies by more than $5 \mathrm{~m} / \mathrm{sec}$.
2. Variation (VAR): The peak value of the wind speed is entered under VAR when the peak value exceeds the value of the wind speed by at least $5 \mathrm{~m} / \mathrm{sec}$.
3. Weather conditions:

WS Water spout
TH Thunderstorm
FD Freezing drizzle
F Fog
SS Snow shower
RS Rain shower
H Hail
S Snow
R Rain
D Drizzle
K Haze or smoke
4. Intensity of weather conditions:
(+) Unusually intense
$(-)$ Mild conditions
5. Pressure Trend:

First number indicates characteristic of change
$0=$ Increasing then decreasing
1 = Increasing then steady, or increasing more slowly
$2=$ Increasing either steady or unsteady
3 = Decreasing or steady, then increasing; or increasing, then increasing more rapidly
4 = Steady
5 = Decreasing then increasing
6 = Decreasing then steady or decreasing more slowly
7 = Decreasing steady or unsteady
8 = Steady or increasing then decreasing or decreasing then decreasing more slbwly

Next two columns indicate code of the amount of change in last 3 hours; higher numbers indicate more change, i.e.

```
    00 = 0.0 millibars
    51 = 5.1 millibars
100 = 10.0 millibars
200 = 20.0 millibars
```




|  | $\rightarrow-\infty$ | $\stackrel{n}{n}-6 \pi n$ | $\begin{gathered} n \\ \infty \\ \infty \\ n \end{gathered}$ | $\text { non } 0$ | $m+\infty \div t$ | $m+\underset{\sim}{n} \stackrel{n}{0}$ | 7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & 0.0 \\ & \text { Nir } \end{aligned}$ | noooo 1NoNm | noorm $\infty \infty$ n $-\infty$ |  <br> ナーか心に | 00000 ナ $0 \times$ Ni | oonno ベボボソ | $\bigcirc$ |
|  | $\begin{array}{cc} 00 \\ \text { nio } \end{array}$ | $\begin{aligned} & 00000 \\ & \text { inono } \end{aligned}$ | $\begin{aligned} & 0000 \\ & \text { aio } \\ & 0 \infty \end{aligned}$ | 000 no ベかのが |  | $\begin{aligned} & n 0 n 00 \\ & 0 \text { in o } \end{aligned}$ | $\stackrel{0}{2}$ |
|  | N－H | ソソMos | $\leqslant \infty$ ¢ 0 | ボャッロ | $\checkmark m \infty \sim$ | ormmm | $\mathrm{M}$ |
|  | $\equiv \infty \infty$ | 納いが | 二〇ッヲ， | 士aOFo | $\cdots \infty$ | ごoro | N |


 Amount of

Precipita－ | 톨 |
| :---: |
| $\square$ |
| $\square$ | OOOON NOUNO OMONH 00000 Table A2

January 1980 Daily Meteorological Observations

岕 岕



 | Day | Time | $\begin{array}{c}\text { Prevailing } \\ \text { Weather } \\ \text { Conditions }\end{array}$ | Intensity |
| :---: | :---: | :---: | :---: |
| 2 | 0730 | D |  |
| 3 | 0730 |  |  |
| 4 | 0730 |  |  |
| 5 | 0730 |  |  |
| 6 | 0730 |  |  |
| 7 | 0730 |  |  |
| 8 | 0730 |  |  |
| 9 | 0730 |  |  |
| 10 | 0730 |  |  |
| 11 | 0730 | D |  |
| 12 | 0730 |  |  |
| 13 | 0730 |  |  |
| 14 | 0730 | F |  |
| 15 | 0730 | F |  |
| 16 | 0730 |  |  |
| 17 | 0730 |  |  |
| 18 | 0730 |  |  |
| 19 | 0730 |  |  |
| 20 | 0930 |  |  |
| 21 | 0730 |  |  |
| 22 | 0730 |  |  |
| 23 | 0730 | D |  |
| 24 | 0730 |  |  |
| 25 | 0730 |  |  |
| 26 | 0730 |  |  |
| 27 | 0730 |  |  |
| 28 | 0730 |  |  |
| 29 | 0730 |  |  |
| 30 | 0730 |  |  |
| 31 | 0730 |  |  |
| Monthly average： |  |  |  |

| Day | Time | Prevailing Weather Conditions | Intensity | 0-100\% Cloud Cover $\qquad$ | Visibility $\mathrm{km}$ $\qquad$ | Amount of Precipitation, man | Atmospheric Pressure $\qquad$ | Pressure <br> Trends | High Temperature ${ }^{\circ} \mathrm{C}$ $\qquad$ | $\qquad$ | Dry <br> Bulb <br> Temper- <br> ature <br> ${ }^{\circ} \mathrm{C}$ | Wet <br> Bulb <br> Temper- <br> ature <br> ${ }^{\circ} \mathrm{C}$ | Dew Point ${ }^{\circ} \mathrm{C}$ | Land Wind Speed m/sec | Land <br> Wind <br> Direc- <br> tion <br> (True N) | $\begin{array}{ll}\text { W } & V \\ \mathbf{F} & \mathbf{A} \\ \text { C } & \mathrm{R}\end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0730 |  |  | 10 | 24 | 8 | 1017.8 | 107 | -1 | -7 | -7.0 | -7.0 | -7 | 9.3 | 310 |  |
| 2 | 0730 |  |  | 0 | 24 | 0 | 1024.3 | 220 | -2 | -8 | -7.0 | -8.0 | -7 | 8.2 | 310 |  |
| 3 | 0730 |  |  | 10 | 24 | 0 | 1027.0 | 214 | -1 | -8 | -7.0 | -7.0 | -7 | 6.2 | 300 |  |
| 4 | 0730 | . |  | 60 | 24 | 0 | 1023.9 | 400 | 0 | -10 | -4.0 | -6.0 | -2 | 6.2 | 310 |  |
| 5 | 0730 |  |  | 10 | 24 | 0 | 1027.0 | 310 | 0 | -5 | -4.0 | -5.0 | -7 | 6.2 | 320 |  |
| 6 | 0730 |  |  | 100 | 24 | 0 | 1024.3 | 500 | 2 | -6 | 1.0 | 0.0 | -2 | 3.1 | 40 |  |
| 7 | 0730 |  |  |  |  | 13 | 1017.8 | 234 |  |  |  |  |  |  |  |  |
| 8 | 0730 |  |  | 0 | 24 | 6 | 1029.7 | 217 | 5 | -5.4 | -3.0 | -4.0 | -7 | 6.2 | 320 |  |
| 9 | 0730 |  |  | 100 | 8 | 0 | 1026.0 | 400 | 3 | -6 | 0.0 | -1.0 | -3 | 3.1 | 330 |  |
| 10 | 0730 | SS | - | 100 | 8 | 2 | 1009.4 | 124 | 3 | -1 | 0.0 | 0.0 | 0 | 11.8 | 330 |  |
| 11 | 0730 |  |  | 0 | 24 | 0 | 1020.2 | 317 | 2 | -5 | -4.0 | -5.0 | -8 | 4.6 | 310 |  |
| 12 | 0730 |  |  | 40 | 24 | 0 | 1017.2 | 127 | 5 | -4 | 0.0 | -1.0 | -3 | 5.1 | 320 |  |
| 13 | 0730 |  |  | 0 | 27 | 0 | 1029.3 | 220 | 4 | -4 | 0.0 | -2.0 | -6 | 6.2 | 20 |  |
| 14 | 0730 |  |  | 0 | 24 | 0 | 1029.3 |  | 3 | -6 | -2.0 | -3.0 | -5 | 3.1 | 170 |  |
| 15 | 0730 |  |  | 75 | 16 | 0 | 1022.6 | 400 | 9 | -2 | 3.0 | 2.0 | 1 | 4.1 | 30 |  |
| 16 | 0730 | K | - | 100 | 24 | 0 | 1003.6 | 730 | 10 | 2 | 7.5 | 6.0 | 4 | 6.2 | 170 |  |
| 17 | 0730 |  |  | 90 | 24 | 4 | 1013.4 | 227 | 11 | -3 | -4.0 | -2.5 | -6 | 9.3 | 320 |  |
| 18 | 0730 |  |  | 0 | 24 | 0 | 1026.3 | 227 | 1 | -11 | -8.0 | -9.0 | -12 | 2.6 | 310 |  |
| 19 | 0730 |  |  | 90 | 24 | 0 | 1025.3 | 610 | 4 | -8 | 3.0 | 2.0 | 1 | 4.1 | 40 |  |
| 20 | 0730 | F | + | 50 | 1 | 0 | 1014.4 | 400 | 8 | -3 | 5.0 | 4.0 | 3 | 4.6 | 40 |  |
| 21 | 0730 |  |  | 0 | 16 | 0 | 1014.1 | 317 | 13 | 4 | 7.0 | 6.0 | 5 | 4.1 | 230 |  |
| 22 | 0730 | F |  | 100 | 1 | 1 | 1015.8 | 107 | 15 | 6 | 10.0 | 10.0 | 10 | 3.6 | 220 |  |
| 23 | . 0730 |  |  | 0 | 24 | 0 | 1012.1 | 310 | 19 | 9 | 12.0 | 11.0 | 10 | 3.6 | 220 |  |
| 24 | 0730 | F | + | 100 | 1 | 8 | 1016.8 | 327 | 16 | 7 | 7.0 | 7.0 | 7 | 5.1 | 320 |  |
| 25 | 0730 |  |  | 100 | 16 | 0 | 1012.1 | 507 | 9 | 3 | 7.0 | 6.0 | 5 | 9.3 | 40 |  |
| 26 | 0730 | SS | - |  |  |  | 1007.7 | 247 |  |  | 1.0 | 0.0 | -2 | 8.2 | 310 |  |
| 27 | 0730 |  |  | 0 | 24 | 0 | 1021.2 | 720 | 6 | -5 | 1.0 | -1.0 | -5 | 6.7 | 210 |  |
| 28 | 0730 |  |  | 100 | 24 | 0 | 1014.8 | 004 | 9 | 1 | 4.0 | 2.0 | -1 | 5.1 | 50 |  |
| 29 | 0730 |  |  | 50 | 24 | 0 | 1019.2 | 241 | 5 | -1 | 0.0 | -1.0 | -3 | 10.8 | 330 |  |
| Monthly average: |  |  |  | 49 | 19 |  | 1019.4 |  | 3 | -2 |  |  | -2 | 6.0 |  |  |
| Monthly total: |  |  |  |  |  | 66 |  |  |  |  |  |  |  |  |  |  |


| Day | Time | Prevailing Weather Conditions | Intensity | 0-100\% Cloud Cover $\qquad$ | Visibility km | Amount of Precipitation, mm | Atmospheric Pressure $\qquad$ | Pressure <br> Trends | $\qquad$ | $\qquad$ | $\qquad$ | Wet <br> Bulb <br> Temper- <br> ature <br> ${ }^{\circ} \mathrm{C}$ | $\begin{gathered} \text { Dew } \\ \text { Point } \\ { }^{\circ} \mathrm{C} \\ \hline \end{gathered}$ | Land <br> Wind <br> Speed <br> m/sec | Land Wind Direction (True N) | $\begin{array}{ll} \mathrm{W} & \mathrm{~V} \\ \mathrm{~F} & \mathrm{~A} \\ \underline{\mathrm{C}} & \underline{R} \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0730 |  |  | 100 | 24 | 0 | 1030.7 | 303 | 2 | -4 | -3.0 | -4.0 | -7 | 9.3 | 20 |  |
| 2 | 0730 |  |  | 100 | 1 | 0 | 1013.8 | 003 | 1 | -4.4 | 0.0 | -1.0 | -3 | 14.4 | 20 | + |
| 3 | 0730 |  |  | 100 | 16 | 11 | 1020.2 | 107 | 1 | -7.1 | 1.0 | 0.0 | -2 | 6.2 | 330 |  |
| 4 | 0730 |  |  | 40 | 24 | 0 | 1023.6 | 103 | 1 | -7 | -1.0 | -2.0 | -4 | 4.1 | 220 |  |
| 5 | 0730 |  |  | 100 | 12 | 0 | 1020.9 | 107 | 8 | -1 | 6.0 | 5.0 | 4 | 2.1 | 180 |  |
| 6 | 0730 | F | - | 100 | 13 |  | 1022.6 | 247 |  | 3 | 5.0 | 4.0 | 3 | 6.2 | 20 |  |
| 7 | 0730 |  |  | 25 | 8 | 0 | 1 C 26.6 | 400 | 7 | -6 | 4.0 | 3.0 | 2 | 3.1 | 180 |  |
| 8 | 0730 | F | - | 100 | 16 | 0 | 1017.8 | 607 | 18 | 3 | 13.0 | 12.0 | 11 | 5.1 | 180 |  |
| 9 | 0730 | F | + | 100 | 1 | 6 | 1009.4 | 317 | 15 | 9 | 10.0 | 10.0 | 10 | 5.1 | 270 |  |
| 10 | 0730 |  |  | 25 | 24 | 0 | 1014.4 | 103 | 16 | 2 | 7.0 | 6.0 | 5 | 2.1 | 70 |  |
| 11 | 0730 |  |  | 0 | 24 | 1 | 1007.3 | 237 | 13 | 7 | 10.0 | 8.0 | 6 | 6.7 | 300 |  |
| 12 | 0730 |  |  | 100 | 24 | 0 | 1021.2 | 220 | 11 | 2 | 4.0 | 2.0 | -1 | 7.7 | 40 |  |
| 13 | 0730 | D | - | 100 | 8 | 4 | 1014.1 | 730 | 8 | 2 | 8.0 | 7.0 | 6 | 5.1 | 70 |  |
| 14 | 0730 |  |  | 25 | 24 | 3 | 1009.7 | 230 | 18 | 3 | 5.0 | 4.0 | 3 | 9.3 | 290 |  |
| 15 | 0730 |  |  | 00 | 24 | 0 | 1028.3 | 227 | 12 | 2 | 5.0 | 3.0 | 0 | 5.7 | 330 |  |
| 16 | 0730 |  |  | 00 | 24 | 0 | 1032.7 | 170 | 14 | 4 | 8.0 | 7.0 | 6 | 1.5 | 180 |  |
| 17 | 0730 |  |  | 100 | 24 | 0 | 1026.3 | 607 | 17 | 8 | 16.5 | 13.0 | 10 | 5.1 | 200 |  |
| 18 | 0730 |  |  | 100 | 24 | 10 | 1011.1 | 314 | 21 | 15 | 15.0 | 15.0 | 15 | 7.2 | 240 |  |
| 19 | 0730 |  |  | 00 | 24 | 1 | 1030.7 | 224 | 16 | 3 | 6.5 | 5.0 | 3 | 3.1 | 40 |  |
| 20 | 0730 | F | - | 100 | 3 | 0 | 1025.3 | 807 | 11 | 6 | 11.0 | 10.0 | 9 | 4.1 | 150 |  |
| 21 | 0730 | R | - | 100 | 8 | 12 | 1003.6 | 734 | 21 | 10 | 11.0 | 11.0 | 11 | 9.8 | 200 |  |
| 22 | 0730 |  |  | 10 | 24 | 3 | 1005.3 | 210 | 22 | 6 | 8.0 | 5.0 | 1 | 12.9 | 300 |  |
| 23 | 0730 |  |  | 00 | 24 | 0 | 1021.6 | 227 | 12 | 3 | 4.0 | 3.0 | 2 | 7.5 | 330 |  |
| 24 | 0730 |  |  | 100 | 24 | 0 | 1020.9 | 317 | 9 | 2 | 10.0 | 8.0 | 6 | 5.1 | 240 |  |
| 25 | 0730 |  |  | 00 | 24 | 11 | 1007.0 | 241 | 16 | 8 | 12.5 | 10.0 | 8 | 6.2 | 300 |  |
| 26 | 0730 |  |  | 100 | 8 | 0 | 1020.9 | 224 | 17 | 6 | 6.5 | 5.0 | 3 | 6.2 | 30 |  |
| 27 | 0730 |  |  | 25 | 24 | 0 | 1026.0 | 227 | 8 | 6 | 7.0 | 5.0 | 3 | 7.2 | 20 |  |
| 28 | 0730 |  |  | 100 | 24 | 0 | 1028.3 | 110 | 10 | 6 | 8.0 | 7.0 | 6 | 4.6 | 60 |  |
| 29 | 0730 | F | + | 100 | 15 | 13 | 1011.7 | 614 | 12 | 8 | 10.0 | 10.0 | 10 | 3.0 | 150 |  |
| 30 | 0730 | F | + | 100 | 3 | 0 | 1012.8 | 107 | 17 | 9 | 10.5 | 10.0 | 10 | 2.6 | 150 |  |
| 31 | 0730 | F | + | 100 | 3 | 13 | 1004.6 | 107 | 14 | 9 | 13.0 | 13.0 | 13 | 5.1 | 290 |  |
| Monthly average: |  |  |  | 66 | 16 |  | 1018.4 |  | 12 | 4 |  |  | 5 | 5.9 |  |  |
| Monthly total: |  |  |  |  |  | 89 |  |  |  |  |  |  |  |  |  |  |


| Day | Time | Prevailing Weather Conditions | Intensity | 0-100\% Cloud Cover \% | $\begin{gathered} \text { Visi- } \\ \text { bility } \\ \text { km } \end{gathered}$ | Amount of Precipitation, mm | Atmospheric Pressure mb | Pressure Trends | $\qquad$ | $\qquad$ | Dry <br> Bulb <br> Temper- <br> ature <br> ${ }^{\text {o }} \mathrm{C}$ | Wet <br> Bulb <br> Temper- <br> ature <br> o ${ }^{\text {C }}$ | $\begin{gathered} \text { Dew } \\ \text { Point } \\ { }^{\circ} \mathrm{C} \\ \hline \end{gathered}$ | Land <br> Wind <br> Speed <br> $\mathrm{m} / \mathrm{sec}$ | Land <br> Wind <br> Direc- <br> tion <br> (True $N$ ) | $\begin{array}{ll} \mathbf{W} & \mathbf{V} \\ \mathbf{F} & \mathbf{A} \\ \underline{\mathrm{C}} & \underline{R} \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0730 |  |  | 100 | 24 | 00 | 1019.2 | 244 | 27 | 6 | 07.0 | 05.0 | 03 | 7.2 | 020 |  |
| 2 | 0730 | F | - | 0 | 5 | 00 | 1024.6 | 110 | 9 | 3 | 08.0 | 07.0 | 06 | 1.5 | 060 |  |
| 3 | 0730 | F | - | 75 | 3 | 00 | 1020.2 | 317 | 20 | 8 | 11.5 | 11.0 | 11 | 2.0 | 020 |  |
| 4 | 0730 |  |  | 100 | 24 | 00 | 1009.7 | 617 | 18 | 9 | 12.5 | 11.0 | 10 | 6.2 | 200 |  |
| 5 | 0730 |  |  | 0 | 24 | 6 | 1011.0 | 230 | 23 | 9 | 10.5 | 09.0 | 08 | 10.3 | 330 |  |
| 6 | 0730 |  |  | 0 | 24 | 00 | 1023.2 | 246 | 16 | 8 | 12.0 | 09.0 | 06 | 4.6 | 020 |  |
| 7 | 0730 |  |  | 75 | 24 | 00 | 1026.6 | 120 | 14 | 9 | 12.0 | 10.0 | 08 | 4.6 | 110 |  |
| 8 | 0730 |  |  | 90 | 8 | 00 | 1027.3 | 307 | 16 | 11 | 13.0 | 12.0 | 11 | 4.1 | 150 |  |
| 9 | 0730 |  |  | 90 | 16 | 00 | 1015.8 | 603 | 19 | 14 | 19.0 | 16.0 | 14 | 8.2 | 200 |  |
| 10 | 0730 |  |  | 25 | 24 | 100 | 1010.7 | 314 | 22 | 14 | 17.0 | 14.0 | 12 | 6.1 | 240 |  |
| 11 | 0730 |  |  | 0 | 24 | 00 | 1017.2 | 224 | 24 | 14 | 17.0 | 15.0 | 14 | 4.1 | 240 |  |
| 12 | 0730 |  |  | 40 | 24 | 00 | 1020.5 | 303 | 21 | 11 | 17.0 | 15.0 | 14 | 4.6 | 200 |  |
| 13 | 0730 |  |  | 100 | 24 | 00 | 1015.8 | 314 | 26 | 17 | 20.0 | 18.0 | 17 | 5.1 | 290 |  |
| 14 | 0730 | F | - | 100 | 8 | 15 | 1012.4 | 400 | 21 | 11 | 14.0 | 13.0 | 12 | 4.6 | 150 |  |
| 15 | 0730 |  |  | 10 | 24 | 4 | 1008.3 | 124 | 22 | 12 | 13.0 | $11.0 /$ | 09 | 9.7 | 240 |  |
| 16 | 0730 |  |  | 0 | 24 | 00 | 1013.8 | 214 | 18 | 9 | 11.0 | 08.0 | 05 | 9.3 | 290 |  |
| 17 | 0730 |  |  | 10 | 24 | 00 | 1028.0 | 224 | 16 | 6 | 07.0 | 05.0 | 03 | 7.2 | 020 |  |
| 18 | 0730 |  |  | 75 | 24 | 00 | 1024.6 | 400 | 12 | 9 | 12.0 | 09.0 | 06 | 4.1 | 200 |  |
| 19 | 0730 |  |  | 0 | 24 | 00 | 1023.6 | 303 | 18 | 7 | 14.5 | 13.0 | 12 | 3.0 | 240 |  |
| 20 | 0730 | . |  | 40 | 16 | 00 | 1022.6 | 400 | 19 | 9 | 13.5 | 12.0 | 11 | 2.0 | 120 |  |
| 21 | 0730 |  |  | 50 | 16 | 00 | 1013.2 | 303 | 18 | 9 | 14.0 | 13.0 | 12 | 3.0 | 040 |  |
| 22 | 0730 |  |  | 0 | 16 | 00 | 1012.8 | 310 | 18 | 10 | 16.0 | 12.0 | 09 |  |  |  |
| 23 | 0730 |  |  | 10 | 24 | 00 | 1005.0 | 214 | 19 | 13 | 19.0 | 11.0 | 09 |  |  |  |
| 24 | 0730 |  |  | 60 | 24 | 00 | 1006.3 | 117 | 16 | 13 | 16.0 | 15.0 | 14 |  |  |  |
| 25 | 0730 | F | + | 50 | 7.5 | 00 | 1008.0 | 114 | 26 | 74 | 15.5 | 15.0 | 15 |  |  |  |
| 26 | 0730 |  |  | 75 | 16 | 00 | 1009.7 | 117 | 29 | 13 | 15.0 | 12.0 | 10 |  |  |  |
| 27 | 0730 |  |  | 50 | 16 | 00 | 1011.0 | 310 | 23 | 12 | 29.0 | 20.0 | 18 |  |  |  |
| 28 | 0730 |  |  | 25 | 16 | 72 | 1004.6 | 503 | 27 | 13 | 15.0 | 14.5 | 14.5 |  |  |  |
| 29 | 0730 |  |  | 0 | 24 | 14 | 1008.0 | 220 | 19 | 11 | 16.0 | 15.0 | 14 |  |  |  |
| 30 | 0730 |  |  | 90 | 24 | 00 | 1005.3 | 107 | 23 | 14 | 14.5 | 12.5 | 11.5 |  |  |  |
| Monthly average: |  |  |  | 45 | 22 |  | 1015.3 |  | 20 | 11 |  |  | 11 | 5.3 |  |  |
| Monthly total: |  |  |  |  |  | 112 |  |  |  |  |  |  |  |  |  |  |


| Day | Time | Prevailing Weather Conditions | Intensity | 0-100\% Cloud Cover $\qquad$ | Visibility km | Amount of Precipitation, mm | Atmospheric Pressure mb | Pressure Trends | $\qquad$ | $\qquad$ | $\qquad$ | Wet <br> Bulb <br> Temper- <br> ature <br> ${ }^{\text {o}} \mathbf{C}$ | Dew Point ${ }^{\circ} \mathrm{C}$ | Land <br> Wind <br> Speed <br> $\mathrm{m} / \mathrm{sec}$ | Land <br> Wind <br> Direc- <br> tion <br> (True N) | $\begin{aligned} & \mathrm{W} \\ & \mathrm{~F} \\ & \mathrm{C} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0730 |  |  | 100 | 16 | 1 | 1005.6 | 400 | 19 | 12 | 13.5 | 12.0 | 11 |  |  |  |
| 2 | 0730 |  |  | 50 | 16 | 2 | 1012.8 | 114 | 14 | 11 | 15.0 | 13.5 | 12 |  |  |  |
| 3 | 0730 |  |  | 60 | 24 | 0 | 1014.4 | 400 | 21 | 9 | 16.4 | 12.0 | 9 |  |  |  |
| 4 | 0730 | K | - | 60 | 16 | 3 | 1011.1 | 303 | 23 | 9 | 19.0 | 15.0 | 12 |  |  |  |
| 5 | 0730 | K | - | 60 | 16 | 0 | 1010.4 | 400 | 24 | 14 | 21.0 | 17.0 | 15 |  |  |  |
| 6 | 0730 | K | - | 40 | 16 | 0 | 1006.0 | 400 | 29 | 18 | 21.0 | 17.0 | 15 |  |  |  |
| 7 | 0730 | K | - | 40 | 16 | 0 | 1008.3 | 227 | 28 | 19 | 21.5 | 16.5 | 13.5 |  |  |  |
| 8 | 0730 | K | - | 100 | 3 | 0 | 1007.3 | 310 | 24 | 16 | 16.0 | 14.0 | 13 |  |  |  |
| 9 | 0730 |  |  | 75 | 24 | 1 | 1013.8 | 330 | 17 | 11 | 13.5 | 9.0 | 5 | 7.2 | 20 |  |
| 10 | 0730 |  |  | 25 | 24 | 0 | 1020.2 | 224 | 17 | 9 | 16.0 | 12.0 | 9 | . 2 | 120 |  |
| 11 | 0730 |  |  | 75 | 24 | 0 | 1019.5 | 314 | 21 | 12 | 20.5 | 16.0 | 13 | 4.6 | 200 |  |
| 12 | 0730 |  |  | 75 | 24 | 0 | 1018.2 | 310 | 26 | 19 | 22.0 | 19.0 | 17 | 5.1 | 240 |  |
| 13 | 1200 |  |  | 50 | 24 | 0 | 1014.4 | 400 | 30 | 21 | 28.0 | 23.0 | 21 | 4.6 | 240 |  |
| 14 | 0730 |  |  | 100 | 16 | 0 | 1012.1 | 307 | 31 | 22 | 22.5 | 20.0 | 19 | 4.6 | 240 |  |
| 15 | 0730 |  |  | 100 | 24 | 1 | 1018.8 | 327 | 28 | 14 | 15.0 | 13.0 | 12 | 6.2 | 200 |  |
| 16 | 0730 |  |  | 00 | 24 | 0 | 1026.0 | 224 | 18 | 12 | 16.0 | 13.0 | 11 | 5.7 | 60 |  |
| 17 | 0730 |  |  | 25 | 24 | 0 | 1029.3 | 310 | 18 | 13 | 16.0 | 14.0 | 13 | 3.1 | 60 |  |
| 18 | 0730 |  |  | 100 | 16 | 1 | 1021.6 | 710 | 21 | 15 | 21.0 | 19.0 | 18 | 3.1 | 200 |  |
| 19 | 0730 |  |  | 50 | 16 | 0 | 1017.5 | 310 | 24 | 20 | 23.0 | 21.0 | 20 | 3.9 | 240 |  |
| 20 | 0730 |  |  | 100 | 16 | 6 | 1013.8 | 303 | 31 | 16 | 22.5 | 21.5 | 21.5 | 1.5 | 240 |  |
| 21 | 0730 |  |  | 90 | 24 | 24 | 1010.7 | 230 | 28 | 19 | 21.5 | 20.0 | 19 |  |  |  |
| 22 | 0730 | F | - | 40 | 8 | 0 | 1020.2 | 214 | 26 | 14 | 20.5 | 18.0 | 17 | 2 | 40 |  |
| 23 | 0730 | F | - | 100 | 16 | 0 | 1018.8 | 303 | 24 | 18 | 20.0 | 19.0 | 19 | 3.1 | 180 |  |
| 24 | 0730 |  |  |  | 16 | 0 | 1012.8 | 103 | 22 | 10 | 22.0 | 21.5 | 21.5 |  |  |  |
| 25 | 0730 |  |  |  | 11 | 0 | 1002.6 |  | 34 | 19 | 24.0 | 22.0 | 21 |  |  |  |
| 26 | 1200 |  |  | 00 | 16 | 0 | 1010.4 | 214 |  | 17 | 19.5 | 17.0 | 16 | 8.1 | 40 |  |
| 27 | 0730 |  |  | 00 | 24 | 0 | 1016.8 | 224 | 21 | 11 | 19.5 | 15.0 | 12 | 6.1 | 40 |  |
| 28 29 | 0730 |  |  | 00 | 24 | 0 | 1019.9 | 114 | 23 | 15 | 23.0 | 18.0 | 15 | 4.1 | 290 |  |
| 29 30 | 1045 |  |  | 00 | 16 | 0 | 1019.9 | 114 | 28 | 17 | 28.0 | 21.5 | 18 | 1.6 | 200 |  |
| 30 | 0815 |  |  | 90 | 15 | 0 | 1022.2 | 151 | 29 | 20 | 22.0 | 19.5 | 18 | 5.1 | 130 |  |
| 31 | 0830 |  |  | 10 | 15 | 0 | 1023.6 | 117 | 30 | 21 | 25.0 | 21.5 | 20 | 7.1 | 230 |  |
| Mont | ly av | rage: |  | 58 |  |  | 1015.5 |  | 24 | 15 |  |  | 15 | 4.4 |  |  |
| Mont | ly to |  |  |  |  | 39 |  |  |  |  |  |  |  |  |  |  |

June 1980 Daily Meteorological Observations

| Land |  |  |
| :--- | :--- | :--- |
| Wind |  |  |
| Direc－ | W | V |
| tion | F | A |
| （True N） | C | R |




|  | 읏육ำ | $\begin{aligned} & \text { n } \\ = & \text { Nin } \end{aligned}$ | ? | 그Nํ | のホNか0 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & 0 n 0 N 0 \\ & \text { NN N } \end{aligned}$ | $\begin{aligned} & 0 \sim 000 \\ & 00 \text { NNo } \end{aligned}$ | $\begin{aligned} & n 0000 \\ & \sim 000 \\ & \sim 100 \end{aligned}$ | $\begin{aligned} & 00 n 0 \\ & \text { Ninn } \end{aligned}$ | $\begin{aligned} & 00000 \\ & \text { MiO } \end{aligned}$ | $\begin{aligned} & 0 \text { OOO } \\ & \text { oNNNN } \end{aligned}$ |
| 会总总总岂 | $\begin{aligned} & 00000 \\ & \text { NNN Ni } \end{aligned}$ |  | $\begin{aligned} & n 00 \text { no } \\ & \text { giog ni } \end{aligned}$ | $\begin{aligned} & \text { Onioo } \\ & \text { Noin in } \end{aligned}$ | $\begin{aligned} & 0 n o o o \\ & \text { inNin } \end{aligned}$ | $\begin{aligned} & 0 n \sim 0 \text { n } \\ & \text { on jn N } \end{aligned}$ |
|  | NNNべ | MNNッ6 |  | NonNo | 二ッツ入ぇ |  |
|  | 애लึल | さへへ入入入 | ㅍNNN | MึN入入 | ¢ヘึNNN | NさNm心 |



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 8缩 Prevailing



Table A8
July 1980 Daily Meteorological Observations

| Amount of Precipitation, mm | Atmospheric Pressure $\qquad$ | Pressure Trends | High Temperature ${ }^{\circ} \mathrm{C}$ | $\qquad$ | Dry <br> Bulb <br> Temper- <br> ature <br> ${ }^{\circ} \mathrm{C}$ | Wet <br> Bulb <br> Temper- <br> ature <br> ${ }^{\circ} \mathrm{C}$ |  | Land Wind Speed $\mathrm{m} / \mathrm{sec}$ | Land <br> Wind <br> Direc- <br> tion <br> $($ True $N)$ | $\begin{array}{ll} \mathrm{W} & \mathrm{~V} \\ \mathrm{~F} & \mathrm{~A} \\ \underline{\mathrm{C}} & \underline{R} \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1017.8 | 220 | 29 | 18 | 24.5 | 21.0 | 19 | 3.1 | 20 |  |
| 0 | 1021.9 | 214 | 27 | 20 | 25.0 | 23.5 | 22.5 | 3.1 | 160 |  |
| 0 | 1018.8 | 707 | 32 | 25 | 28.0 | 24.0 | 22 | 12.9 | 140 |  |
| 11 | 1018.5 | 110 | 33 | 22 | 26.0 | 24.0 | 23 | 5.1 | 270 |  |
| 1 | 1015.5 | 130 | 31 | 24 | 26.0 | 24.5 | 23.5 | 6.1 | 250 |  |
| 17 | 1011.7 | 207 | 33 | 18 | 26.0 | 25.0 | 25 | 3.6 | 340 |  |
| 1 | 1019.1 | 317 | 31 | 22 | 24.0 | 19.0 | 16 | 5.1 | 70 |  |
| 0 | 1019.9 | 114 | 26 | 18 | 23.5 | 20.0 | 18 | 5.6 | 250 |  |
| 0 | 1017.1 | 203 | 29 | 19 | 26.0 | 23.0 | 22 | 2.1 | 20 |  |
| 0 | 1014.1 | 403 | 28 | 23 | 25.0 | 24.0 | 24 | 3.1 | 290 |  |
| 1 | 1010.4 | 214 | 27 | 21 | 24.0 | 23.0 | 23 | 3.1 | 320 |  |
| 0 | 1011.4 | 203 | 29 | 23 | 28.0 | 25.0 | 24 | 3.6 | 250 |  |
| 25 | 1011.7 | 317 | 33 | 20 | 24.5 | 23.5 | 23.5 | 4.1 | 20 |  |
| 0 | 1018.5 | 110 | 27 | 22 | 25.5 | 21.0 | 19 | 4.1 | 90 |  |
| 0 | 1020.5 | 803 | 28 | 18 | 25.0 | 22.0 | 21 | 2.1 | 90 |  |
| 0 | 1016.1 | 510 | 29 | 23 | 29.0 | 24.0 | 22 | 7.2 | 270 |  |
| 0 | 1014.4 | 300 | 33 | 24 | 27.0 | 24.0 | 23 | 6.1 | 200 |  |
| 7 |  |  | 33 | 19 | 24.5 | 22.0 | 21 | 4.6 | 160 |  |
| 0 | 1021.9 | 207 | 32 | 22 | 29.0 | 26.0 | 25 | 5.1 | 250 |  |
| 0 | 1021.6 | 237 | 33 | 25 | 29.5 | 26.5 | 25.5 | 5.6 | 290 |  |
| 0 | 1022.6 | 214 | 34 | 25 | 26.5 | 25.0 | 24 | 8.1 | 250 |  |
| 0 | 1020.5 | 103 | 33 | 27 | 27.5 | 25.0 | 24 | 6.1 | 250 |  |
| 0 | 1017.8 | 807 | 33 | 25 | 28.0 | 25.0 | 24 | 5.1 | 200 |  |
| 0 | 1012.8 | 103 | 31 | 117 | 22.5 | 22.5 | 22.5 | 3.6 | 20 |  |
| 0 |  |  | 28 | 16 | 27.0 | 23.0 | 21 | 2.1 | 70 |  |
| 0 | 1018.5 | 400 | 29 | 119 | 24.0 | 22.0 | 21 | 1.1 | 130 |  |
| 0 | 1016.5 | 303 | 29 | 21 | 25.0 | 23.0 | 22 | 3.1 | 160 |  |
| 0 |  |  | 29 | 20 | 26.5 | 25.0 | 24 | 3.1 | 270 |  |
| 0 | 1014.4 | 214 | 31 | 23 | 27.0 | 23.0 | 21 | 2.6 | 320 |  |
| 0 | 1018.2 | 107 | 33 | 25 | 30.0 | 26.0 | 25 | 4.1 | 250 |  |
|  | 1017.1 | -- | 30 | 21 | -- | -- | 22 | 4.5 |  |  |


 Prevailing
Weather
Conditions Intensity
 Monthly average: Monthly total:

| Day | Time | Prevailing Weather Conditions | Intensity | 0-100\% Cloud Cover $\qquad$ $\%$ | Visibility km | Amount of Precipitation, mm | pheric <br> Pressure mb $\qquad$ | Pressure Trends | High Temperature ${ }^{\circ} \mathrm{C}$ | Low Temperature ${ }^{\circ} \mathrm{C}$ | Dry <br> Bulb <br> Temper- <br> ature <br> ${ }^{\circ} \mathrm{C}$ | Wet <br> Bulb <br> Temper- <br> ature <br> ${ }^{\circ} \mathrm{C}$ | Dew Point ${ }^{\circ} \mathrm{C}$ | Land Wind Speed m/sec | Land <br> Wind <br> Direc- <br> tion <br> (True N) | $\begin{array}{ll} W & V \\ F & A \\ \underline{C} & \underline{R} \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0815 |  |  | 0 | 8 | 0 | 1014.8 | 705 | 34 | 26 | 29.0 | 26.0 | 25 | 5.2 | 250 |  |
| 2 | 0920 |  |  | 0 | 13 | 0 | 1015.1 | 306 | 37 | 23 | 33.0 | 25.0 | 23 | 3.1 | 290 |  |
| 3 | 0800 |  |  | 0 | 8 | 0 | 1012.4 | 004 | 34 | 25 | 29.0 | 27.0 | 26 | 5.7 | 250 |  |
| 4 | 0730 |  |  | 0 | 13 | 0 | 1014.8 | 214 | 36 | 26 | 29.0 | 26.0 | 25 | 6.2 | 250 |  |
| 5 | 0915 |  |  | 40 | 13 | 0 | 1020.2 | 210 | 36 | 26 | 31.0 | 27.0 | 26 | 6.2 | 250 |  |
| 6 | 0730 |  |  | 40 | 8 | 0 | 1021.9 | 310 | 36 | 26 | 29.0 | 26.0 | 25 | 6.2 | 320 |  |
| 7 | 1135 |  |  | 10 | 8 | 23 | 1021.2 | 000 | 35 | 22 | 28.5 | 26.0 | 25 | 1.5 | 050 |  |
| 8 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9 | 0800 |  |  | 0 | 6 | 0 | 1013.8 | 303 | 31 | 26 23 | 28.0 24.0 | 26.0 23.0 | 25 23 | 4.1 3.1 | 320 |  |
| 10 | 0730 | F |  | 100 | 2 | 0 | 1013.8 | 400 |  | 23 | 24.0 | 23.0 | 23 | 3.1 | 320 |  |
| 11 | 0800 |  |  | 100 | 8 | 0 | 1017.2 | 114 | 31 | 23 | 28.0 | 25.0 | 24 | 7.2 | 250 |  |
| 12 | 1130 |  |  | 50 | 24 | 0 | 1019.1 | 810 | 34 | 26 | 31.5 | 26.0 | 24 | 6.2 | 250 |  |
| 13 | 0730 | F |  | 20 | 3 | 17 | 1014.8 | 207 | 34 | 18 | 25.5 | 24.0 | 23 | 3.6 | 320 |  |
| 14 | 0730 | $F$ | + | 10 | 2 | 5 | 1016.8 | 400 | 27 | 21 | 26.0 | 25.0 | 25 | 4.6 | 130 |  |
| 15 | 0715 |  |  | 90 | 24 | 0 | 1015.8 | 307 | 32 | 25 | 27.0 | 25.0 | 24 | 6.2 | 250 |  |
| 16 | 0815 |  |  | 100 | 8 | 0 | 1013.8 | 227 | 33 | 20 | 22.0 | 21.0 | 21 | 4.1 | 020 |  |
| 17 | 1030 |  |  | 75 | 24 | 0 | 1023.3 | 314 | 27 | 19 | 23.0 | 20.0 | 19 | 7.2 | 050 |  |
| 18 | 0800 |  |  | 90 | 24 | 0 | 1020.5 | 103 | 25 | 18 | 29.0 | 21.5 | 19 | 2.6 | 160 |  |
| 19 | 0700 |  |  | 90 | 16 | 3 | 1018.8 | 500 | 26 | 21 | 25.0 | 23.5 | 22 | 4.1 | 230 |  |
| 20 | 1600 |  |  | 25 | 3 | 0 | 1015.5 | 407 | 28 | 21 | 23.0 | 22.0 | 22 | 4.1 | 360 |  |
| 21 | 0800 |  |  | 40 | 3 | 0 | 1014.1 | 407 | 25 | 22 | 23.0 | 20.0 | 19 | 5.2 | 050 |  |
| 22 | 0730 |  |  | 75 | 16 | 0 | 1012.4 | 307 | 24 | 18 | 22.5 | 20.0 | 19 | 8.2 | 020 |  |
| 23 | 0815 |  |  | 50 | 3 | 0 | 1018.2 | 220 | 24 | 18 | 22.0 | 21.0 | 21 | 6.2 | 020 |  |
| 24 | 0710 |  |  | 0 |  | 0 | 1019.9 | 303 | 24 | 17 | 23.0 | 20.0 | 19 | 4.1 | 020 |  |
| 25 | 1015 |  |  | 0 |  | 0 | 1021.9 | 207 | 26 | 15 | 25.0 | 22.0 | 21 | 3.1 | 020 |  |
| 26 | 1415 |  |  | 0 |  | 0 | 1021.6 | 710 | 27 | 21 | 26.5 | 23.5 | 22.5 | 4.1 | 020 |  |
| 27 | 0630 |  |  | 0 |  | 0 | 1021.9 | 307 | 27 | 16 | 23.0 | 22.0 | 22 | 2.6 | 050 |  |
| 28 | 0930 |  |  | 0 |  | 0 | 1023.9 | 107 | 29 | 21 | 26.0 | 22.0 | 20 | 3.6 | 320 |  |
| 29 | 0715 |  |  | 40 |  | 0 | 1025.3 | 110 | 30 | 21 | 24.5 | 23.5 | 23.5 | 1.0 | 320 |  |
| 30 | 0730 |  |  | 10 |  | 0 | 1023.9 | 103 | 29 | 21 | 24.0 | 23.0 | 23 | 7.0 | 090 |  |
| 31 | 0730 |  |  | 40 |  | 0 | 1022.2 | 107 | 29 | 21 | 25.5 | 23.9 | 22 | 2.0 | 130 |  |
| Monthly average: |  |  |  | 37 | 11 |  | 1018.1 |  | 30 | 21 |  |  | 23 | 4.4 |  |  |
| Monthly total: |  |  |  |  |  | 48 |  |  |  |  |  |  |  |  |  |  |

September 1980 Daily Meteorological Observations

| Day | Time | Prevailing Weather Conditions | Intensity | $0-100 \%$ <br> Cloud <br> Cover $\qquad$ | Visibility km | Amount of Precipitation, mm | Atmospheric Pressure mb | Pressure <br> Trends | $\qquad$ | $\qquad$ | Dry <br> Bulb <br> Temper- <br> ature <br> ${ }^{\circ} \mathrm{C} \mathrm{C}$ | Wet <br> Bulb <br> Temper- <br> ature <br> ${ }^{\circ} \mathrm{C}$ | Dew Point ${ }^{\circ} \mathrm{C}$ | Land <br> Wind <br> Speed <br> $\mathrm{m} / \mathrm{sec}$ | Land <br> Wind <br> Direc- <br> tion <br> (True N$)$ | $\begin{aligned} & W \\ & \mathrm{~F} \\ & \underline{C} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | 0730 |  |  | 25 |  | 0 | 1021.2 | 110 | 32 |  |  | 25.0 | 24 | 6.1 | 250 |  |
| 3 | 0715 |  |  | 100 |  | 0 | 1020.5 | 310 | 34 | 25 | 26.0 | 24.0 | 23 | 4.6 | 290 |  |
| 4 | 0715 | F | + | 100 |  | 0 | 1022.3 | 114 | 29 | 22 | 25.0 | 24.0 | 24 | 4.1 | 70 |  |
| 5 | 0700 | F | - | 40 |  | 0 | 1022.6 | 400 | 29 | 19 | 25.5 | 25.0 | 25 | 1.1 | 90 |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | 0700 |  |  | 40 |  | 0 |  | 207 | 30 | 19 | 23.0 |  |  |  |  |  |
| 10 | 0645 |  |  | 00 |  | 0 | 1021.2 | 314 | 28 | 22 | 24.0 | 19.0 | 16 | 1.1 | 360 50 |  |
| 10 | 0645 | F | - | 75 |  | 0 | 1017.1 | 303 | 29 | 20 | 24.5 | 22.0 | 21 | 5.1 |  |  |
| 11 | 0645 |  |  | 00 |  | 0 | 1017.5 | 314 | 30 | 21 | 22.5 | 18.0 | 16 |  |  |  |
| 12 | 0700 |  |  | 00 |  | 0 | 1019.9 | 310 | 27 | 11 | 23.4 | 20.0 | 19 | 2.1 | $\begin{aligned} & 50 \\ & 50 \end{aligned}$ |  |
| 13 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 14 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 15 | 0700 |  |  | 40 |  | 0 | 1009.7 | 400 | 30 | 21 | 26.0 | 23.0 | 22 | 4.1 | 250 |  |
| 16 | 0800 |  |  | 50 |  | 0 | 1017.5 | 317 | 29 | 22 | 24.0 |  |  |  |  |  |
| 17 | 0700 |  |  | 40 |  | 0 | 1015.8 | 107 | 26 | 23 | 26.0 | 24.0 | 23 | 3.6 | 200 |  |
| 18 | 1034 |  |  | 25 |  | 0 | 1017.5 | 803 | 33 | 25 | 30.0 | 27.0 | 26 | 3.1 | 230 |  |
| 19 | 0930 |  |  | 10 |  | 0 | 1024.3 | 117 | 29 | 23 | 26.0 | 23.0 | 22 | 5.1 | 70 |  |
| 20 |  |  |  |  |  |  | 1024.3 |  |  |  |  | 23.0 | 2. |  |  |  |
| 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 22 | 0715 |  |  | 00 |  | 0 | 1017.8 | 400 | 31 | 21 | 25.5 | 23.0 | 22 | 6.1 |  |  |
| 23 | 0730 |  |  | 75 | 16 | 0 | 1013.3 | 100 | 33 | 24 | 26.0 | 24.0 | 23 | 6.1 | 250 |  |
| 24 | 0830 |  |  | 100 | 16 | 0 | 1017.1 | 120 | 33 | 22 | 24.4 | 22.6 | 21 | 6.1 | 50 |  |
| 25 | 0800 |  |  | 100 | 16 | 23 | 1017.5 | 303 | 24 | 22 | 22.5 | 21.5 | 21.5 | 5.1 | 250 |  |
| 26 | 0730 |  |  | 75 | 16 | 3 | 1017.1 | 214 | 28 | 22 | 25.0 | 23.0 |  | 5.6 | 290 |  |
| 27 | 0700 |  |  | 100 | 24 | 0 | 1024.6 | 217 | 29 | 18 | 18.5 | 14.0 | 11 |  |  |  |
| 29 | 0900 |  |  | 90 | 24 | 0 | 1021.2 | 803 | 22 | 12 | 22.0 | 10.0 |  |  |  |  |
| 30 | 0800 |  |  | 100 | 16 | 4 | 1013.8 | 607 | 23 | 21 | 22.0 | 21.0 | 21 |  |  |  |
| 31 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Month | ly ave | rage: |  | 54 |  |  | 1018.5 |  | 29 | 21 |  |  | 21 | 4.3 |  |  |
|  | ly tot |  |  |  |  | 30 |  |  |  |  |  |  |  |  |  |  |

October 1980 Daily Meteorological Observations

November 1980 Daily Meteorological Observations

| Day | Time | Prevailing Weather Conditions | Intensity | $0-100 \%$ <br> Cloud <br> Cover $\qquad$ | Visibility km $\qquad$ | Amount of Precipitation, mm | Atmospheric Pressure $\qquad$ | Pressure <br> Trends | High Temperature ${ }^{\circ} \mathrm{C}$ | $\qquad$ | Dry <br> Bulb <br> Temper- <br> ature <br> ${ }^{\circ} \mathrm{C}$ | Wet <br> Bulb <br> Temper- <br> ature <br> ${ }^{\circ} \mathrm{C}$ | Dew Point ${ }^{\circ} \mathrm{C}$ | Land <br> Wind <br> Speed <br> m/sec | Land <br> Wind <br> Direc- <br> tion <br> (True N) | $\begin{array}{ll} \mathrm{W} & \mathrm{~V} \\ \mathrm{~F} & \mathrm{~A} \\ \underline{\mathrm{C}} & \underline{R} \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0730 |  |  | 0 | 16 | 0 | 1017.2 | 314 | 15 | 8 | 9.5 | 6.5 | 2 | 3.1 | 290 |  |
| 3 | 0800 |  |  | 10 | 24 | 0 | 1030.0 | 207 | 18 | 7 | 12.0 | 8.5 | 4 | 3.6 | 70 |  |
| 4 | 0900 |  |  | 50 | 24 | 0 | 1020.2 | 717 | 21 | 12 |  |  |  | 3.1 | 180 |  |
| 5 | 0800 |  |  | 25 | 24 | 19 | 1011.1 | 217 | 23 | 12 |  |  |  | 5.1 | 340 |  |
| 6 | 0815 |  |  | 0 | 24 | 0 | 1018.8 | 224 | 16 | 11 |  |  |  | 6.2 | 360 |  |
| 7 | 0730 |  |  | 0 | 16 | 0 | 1017.5 | 303 | 14 | 11 |  |  |  | 6.2 | 200 |  |
| 8 9 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | 0900 |  |  | 0 | 16 | 0 | 1012.1 | 110 | 23 | 10 |  |  |  | 7.2 | 290 |  |
| 11 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | 0755 |  |  | 40 | 24 | 0 | 1020.9 | 314 | 22 | 3 |  |  |  | 9.3 | 340 |  |
| 13 | 0845 |  |  | 0 | 24 | 0 | 1027.0 | 324 | 11 | 3 |  |  |  | 4.1 | 290 |  |
| 14 | 1130 |  |  | 0 | 14 | 0 | 1022.6 | 814 | 14 | 7 |  |  |  | 6.2 | 250 |  |
| 15 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 17 | 1000 |  |  | 25 | 16 | 4 | 1026.6 | 703 | 19 | 8 |  |  |  | 8.6 | 70 |  |
| 18 | 0815 |  |  | 50 | 16 | 42 | 1006.0 | 303 | 19 | 8 |  |  |  | 4.6 | 290 |  |
| 19 | 1100 |  |  | 90 | 16 | 0 | 1025.3 | 214 | 11 | 3 |  |  |  | 7.2 | 340 |  |
| 20 | 0950 |  |  | 40 | 24 | 0 | 1029.3 | 214 | 6 | -3 |  |  |  | 3.1 | 290 |  |
| 21 | 0730 | R | + | 100 | 2 | 5 | 1022.2 | 807 | 11 | 9 |  |  |  | 5.1 | 340 |  |
| 22 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 23 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | 1200 |  |  | 100 | 8 |  | 1018.8 | 734 | 14 | 3 |  |  |  | 5.7 | 130 |  |
| 25 | 1000 |  |  | 40 | 16 | 17 | 1021.2 | 120 | 17 | 11 |  |  |  | 9.3 | 360 |  |
| 26 | 0800 |  |  | 75 | 24 | 0 | 1030.7 | 217 | 13 | 3 |  |  |  | 9.3 | 20 |  |
| 27 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 28 | 0955 |  |  | 100 | 6 | 9 | 1007.7 | 403 | 18 | 6 |  |  |  | 5.1 | 250 |  |
| 29 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Mont | hy ave | rage: |  | 39 | 17 |  | 1020.3 |  | 16 | 7 |  |  |  | 5.9 |  |  |
| Mont | ly tot | al |  |  |  | 96 |  |  |  |  |  |  |  |  |  |  |

Table A13
December 1980 Daily Meteorological Observations

| Day | Time | Prevailing Weather Conditions | Intensity | 0-100\% <br> Cloud <br> Cover $\%$ | Visibility km | Amount of Precipitation, mm | Atmospheric Pressure mb $\qquad$ | Pressure Trends | High Temperature ${ }^{\circ} \mathrm{C}$ | Low Temperature ${ }^{\circ} \mathrm{C}$ | Dry <br> Bulb <br> Temper- <br> ature <br> ${ }^{\circ} \mathrm{C}$ | Wet <br> Bulb <br> Temper- <br> ature <br> ${ }^{\circ} \mathrm{C}$ | Dew Point ${ }^{\circ} \mathrm{C}$ | Land <br> Wind <br> Speed <br> $\mathrm{m} / \mathrm{sec}$ | Land Wind Direc- tion (True $N$ ) | $\begin{array}{ll} W & V \\ F & A \\ C & \underline{R} \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1005 |  |  | 0 | 27 | 0 | 1023.6 | 110 | 12.8 | 3.9 |  |  |  | 6.2 | 250 |  |
| 2 | 0800 |  |  | 60 | 16 | 0 | 1021.9 | 400 | 16.1 | 6.1 |  |  |  | 4.1 | 250 |  |
| 3 | 0815 |  |  | 0 | 26 | 0 |  |  | 18.3 | 5.0 |  |  |  | 11.3 | 320 |  |
| 4 | 0900 |  |  | 0 | 24 | 0 | 1030.7 | 214 | 10.6 | 1.7 |  |  |  | 4.1 | 320 |  |
| 5 | 0830 |  |  | 60 | 24 | 0 | 1026.3 | 310 | 7.8 | 1.7 |  |  |  | 6.2 | 340 |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  | 1022.2 |  | 15.0 | 2.2 |  |  |  | 4.1 | 250 |  |
| 8 | 0815 | F | - | 25 50 |  | 0 | 1016.5 | 307 | 20.0 | 10.0 |  |  |  | 5.1 | 250 |  |
| 9 10 | 0830 0800 | F/R | +/- | 50 100 | 8 2 | 4 | 1016.5 1013.1 | 303 | 18.3 | 13.3 |  |  |  | 3.6 | 250 |  |
| 11 | 0815 |  |  | 40 | 16 | 19 | 1021.9 | 224 | 14.4 | 5.0 |  |  |  | 6.2 | 50 |  |
| 12 | 0730 | F | - | 0 | 8 | 0 | 1022.9 | 307 | 8.3 | -0.6 |  |  |  | 1.5 | 250 |  |
| 13 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 14 |  |  |  |  |  |  |  |  |  | 2.8 |  |  |  | 4.1 | 70 |  |
| 15 | 0930 |  |  | 40 | 24 | 0 | 1022.2 | 303 | 15.0 | 2.8 |  |  |  |  |  |  |
| 16 | 0815 | F | + | 100 | 3 | 8 | 1007.7 | 303 | 12.2 | 8.9 |  |  |  | 2.6 | 360 |  |
| 17 |  |  |  |  |  | 4 |  |  |  |  |  |  |  |  |  |  |
| 18 | 0940 |  |  | 0 | 24 | 0 | 1020.2 | 400 | 10.0 | -3.9 |  |  |  |  | 200 |  |
| 19 | 0825 |  |  | 0 | 16 | 0 | 1017.8 | 310 | 10.6 | 5.6 |  |  |  | 5.1 |  |  |
| 20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 22 | 0800 |  |  | 25 | 24 | 0 | 1036.8 | 400 | 12.8 | -3.3 |  |  |  | 5.1 |  |  |
| 23 | 0910 | R | - | 100 | 5 | 14 | 1024.3 | 203 | 10.0 | 2.2 |  |  |  | 3.6 | 360 |  |
| 24 | 1130 | F | + | 100 | 0 | 0 | 1016.5 | 720 | 6.1 | 2.2 |  |  |  | 3.1 |  |  |
| 25 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 26 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 |  |  |  |  |  | 4 |  |  |  |  |  |  |  |  |  |  |
| 28 |  |  |  |  |  | 4 |  |  |  |  |  |  |  |  |  |  |
| 29 | 1045 | F | + | 100 | 0 | 4 | 1010.7 | 403 | 13.3 | -7.2 |  |  |  | 8.2 | 360 |  |
| 30 | 1100 | K |  | 90 | 5 | 0 | 1013.1 | 120 | 7.2 | 5.0 |  |  |  | 8.2 |  |  |
| 31 | 1200 |  |  | 100 | 19 | 0 | 1015.1 | 810 | 7.2 | 3.3 |  |  |  | 7.7 | 20 |  |
| Mon | hly av | erage: |  | 50 | 14 |  | 1020.2 | -- | 12 | 3 | -- | -- | -- | 5.2 |  |  |
| Mon | hly to | tal: |  |  |  | 61 |  |  |  |  |  |  |  |  |  |  |

## APPENDIX B: WAVE DATA

## The wave data are summarized in the following forms:

a. Gage histories. Table B1 includes information about the gage, gage installation, and major interruptions in the data collection. Short interruptions in the operational status of the gage are not mentioned.
b. Time histories. All significant wave height and peak spectral wave period values are plotted as a function of the time throughout the year (see Figures B1, B4, B7, B10, and B13). So that the sequence of the data can be followed easily, solid lines connect consecutive data points for times when there is a gap smaller than 24 hours between observations.
c. Annual, seasonal, and monthly maxima, mean, and standard deviations of significant height and peak period. Mean significant wave height and standard deviation, mean peak wave period and standard deviation, and the extreme significant heights are listed in Tables B2, B6, B10, B14, and B18. Also included is the total number of observations obtained; at four observations per day, the maximum number of observations per month (based on a 30 -day month) is 120. Frequently during 1980 the backup recorder was used and only two observations per day were recorded (except during storms and special events), or 60 observations during a 30 -day month.
d. Maxium, mean, and standard deviations of significant height and peak period. The data presented in the tables described above are also graphed (see Figures B2, B5, B8, B11, and B14) for each month and for the year. The standard deviations are presented as "T" bars originating at the mean value and extending to the mean plus one standard deviation value. The extreme values are plotted above. No extreme period values are presented.
e. Joint distribution functions of significant height versus peak period. Joint distribution tables are presented for 1980 (Tables B3, B7, B11, B15, and B19) and for each season (Tables B4, B8, B12, B16, and B21). Each table gives the frequency (in parts per 1000) for which the significant height and peak period were within the specified intervals; these values can be converted to percent by dividing by 10 .

Marginal totals are also included. The row labeled "Total" gives the total numer of observations out of 1000 which fell within each specified peak period interval. The column "Total" gives the number of observations out of 1000 which fell within each specified significant height interval.
f. Annual and seasonal cumulative distributions of significant wave height. For each gage, annual and seasonal significant wave height distributions are plotted in cumulative form (see Figures B3, B6, B9, B12, and B15).
g. Persistence of significant wave heights. Tables B5, B9, B13, $\bar{B} 17$, and B22 show the number of times throughout the year that the specified wave height was equaled or exceeded at least once during each day of the duration (consecutive days) indicated. For example, for Gage 620, the Waverider located 3 km from shore, wave heights equaled or exceeded 0.5 m 45 times for at least 1 day; 39 times for at least 2 days; 30 times for at least 3 days; etc. Therefore, on 6 occasions one would expect the height to have equaled or exceeded 0.5 m for 1 day exactly; on 9 occasions for 2 days; on 3 occasions, 3 days; etc. Note that the height exceeded 1 m 48 times for 1 day or longer, while heights exceeded 0.5 m only 45 times for this same duration. This occurred because the longer durations of lower waves may be interspersed with shorter, but more frequent, intervals of higher waves. For example, the one time that wave heights exceeded 0.5 m for 29 days may represent 2 or 3 times that the height exceeded 1 m .
Table B1
Wave Gage Histories for 1980

| Type of Gage | Coordinates | Beginning of Proper Operation | End of of Proper Operation | Explanation | Gage Length m $\qquad$ | Gage <br> Range <br> m, ms] | Water Depth <br> m, ms 1 | $\begin{aligned} & \text { Distance } \\ & \text { from } \\ & \text { Shore, km } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Offshore Waverider (Gage No. 620), FRF, Duck, N. C. |  |  |  |  |  |  |  |  |
| ```Buoy - accelerometer``` | $36^{\circ} 11.1^{\prime} \mathrm{N} \times 75^{\circ} 44.4^{\prime} \mathrm{W}$ | Nov 1978 | 3 Jul 1980 | Lightning damaged electronics | NA | Continuous | 18\% | 3 |
|  |  | 6 Jul 1980 | 22 Nov 1980 | Trawler caught buoy in net - found near Oregon inlet |  |  |  |  |
|  |  | 1 Dec 1980 |  | Began monitoring Waverider 6 km from shore |  | Continuous | 19 | 6 |
|  | Nearshore Waverider (Gage No. 610), FRF, Duck, N. C. |  |  |  |  |  |  |  |
| ```Buoy - accelerometer``` | $36^{\circ} 11.1^{\prime} \mathrm{N} \times 75^{\circ} 44.7{ }^{\prime} \mathrm{W}$ | Nov 1978 | 1 Feb 1980 | $\begin{aligned} & \text { Amplifier/noise } \\ & \text { problem } \end{aligned}$ | NA | Continuous | 7 | 0.6* |
|  |  | 12 Feb 1980 | 22 Feb 1980 | ```Amplifier/noise problem``` |  |  |  |  |
|  |  | 2 Mar 1980 | 5 Mar 1980 | $\begin{aligned} & \text { Amplifier/noise } \\ & \text { problem } \end{aligned}$ |  |  |  |  |
|  |  | $13 \text { Mar } 1980$ | $12 \text { Jun } 1980$ | Mooring failure buoy found on beach |  |  |  |  |
|  |  | 12 Aug 1980 |  | New installation |  |  |  |  |
|  | Pier End Baylor (Gage No. 625), Station $19+00$ on FRF Pier ( 579 m ENE of Coordinates Given), Duck, N. C. |  |  |  |  |  |  |  |
| ```Baylor - continuous wire``` | $36^{\circ} 110^{\prime} 54^{\prime \prime} \mathrm{N} \times 75^{\circ} 45^{\prime} 50^{\prime \prime} \mathrm{W}$ | Nov 1978 | 3 Jul 1980 | Lightning damaged amplifiers | 9.4 | $\begin{gathered} -2.1 \text { to } \\ 7.0 \end{gathered}$ | 8.40-4 | 0.6 |
|  |  | 7 Jul 1980 |  |  |  |  |  |  |
|  |  | (Continued) |  |  |  |  |  |  |

Table B1 (Concluded)

| Type of Gage | Coordinates | Beginning of Proper Operation | End of of Proper Operation | Explanation | $\begin{aligned} & \text { Gage } \\ & \text { Length } \end{aligned}$ m | Gage Range $m, \mathrm{~ms} 1$ | Water <br> Depth <br> $\mathrm{m}, \mathrm{ms}$ ? | $\begin{aligned} & \text { Distance } \\ & \text { from } \end{aligned}$ Shore, kin |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{\text { Nearshore Baylor (Gage No. 615), Station 6+20 on ERF Piex }}{(189 \mathrm{mmE} \text { ENE Coordinates Given), Duck , N. C. }}$ |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| Baylor continuous wire | $36^{\circ} 10^{\prime} 54^{\prime \prime} \mathrm{N} \times 75^{\circ} 45^{\prime} 50^{\prime \prime} \mathrm{W}$ | Nov 1978 | 6 Jan 1980 | Amplifier/noise problem | 7.6 | $\begin{gathered} -0.6 \text { to } \\ 7.0 \end{gathered}$ | 1.5\%* | 0.2 |
|  |  | 18 Jan 1980 | 24 Feb 1980 | Gage length changed | 8.5 | $\begin{gathered} -1.6 \text { to } \\ 7.0 \end{gathered}$ |  |  |
|  |  | 24 Feb 1980 | 3 Jul 1980 | Lightning damaged amplifiers |  |  |  |  |
|  |  | 7 Jul 1980 |  |  |  |  |  |  |
|  |  | Vags Head Baylor (Gage No. 112), Jennettes Fishing Pier, $\dagger$ Nags Head, N.C. |  |  |  |  |  |  |
| Baylor - <br> continuous wire | $35^{\circ} 55^{\prime} \mathrm{N} \times 75^{\circ} 36{ }^{\prime} \mathrm{W}$ | Jul 1964 | 3 Ju1 1980 | Lightning damaged transducer | 7.6 | $\begin{aligned} & -2.4 \\ & \text { to } 5.2 \end{aligned}$ | 5.2 | $\begin{aligned} & 0.1 \text { (on } \\ & \text { north } \\ & \text { side of } \\ & \text { pier) } \end{aligned}$ |
|  |  | 11 Jul 1980 | 24 Nov 1980 | Transducer failed (gage installation terminated) |  |  |  |  |

[^4]

Figure B1. 1980 time history of significant wave height and period for the offshore Waverider (gage No. 620)
1980 Wave Statistics for Gage No. 620

| Monthly | $\begin{gathered} \text { Mean } \\ \text { Height, } m \end{gathered}$ | Standard <br> Deviation <br> Height, m | Mean <br> Period, sec | Standard Deviation Period, sec | Extreme Height, m | Date | Number <br> Observations |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |
| Jan | 1.5 | 0.7 | 8.2 | 3.8 | 2.9 | 16 | 72 |
| Feb | 1.1 | 0.5 | 8.3 | 3.0 | 2.3 | 10 | 48 |
| Mar | 1.3 | 0.7 | 10.0 | 2.8 | 3.6 | 13 | 64 |
| Apr | 0.9 | 0.3 | 8.5 | 2.8 | 2.1 | 1 | 65 |
| May | 0.7 | 0.3 | 6.9 | 2.6 | 1.7 | 1 | 59 |
| Jun | 0.7 | 0.3 | 6.9 | 1.5 | 1.5 | 11 | 38 |
| Jul | 0.6 | 0.3 | 8.0 | 3.0 | 1.6 | 28 | 53 |
| Aug | 0.6 | 0.2 | 8.0 | 2.4 | 1.5 | 17 | 50 |
| Sep | 0.8 | 0.4 | 8.8 | 3.0 | 2.0 | 30 | 48 |
| Oct | 1.0 | 0.6 | 8.5 | 8.7 | 4.0 | 25 | 117 |
| Nov- | 1.0 | 0.5 | 6.9 | 2.2 | 2.2 | 11 | 82 |
| Dec | 1.3 | 1.0 | 7.6 | 3.0 | 5.6 | 28 | 111 |
| Annual | 1.0 | 0.6 | 8.1 | 2.9 | 5.6 | Dec | 807 |
| Seasonal |  |  |  |  |  |  |  |
| Jan-Mar | 1.3 | 0.6 | 8.8 | 3.2 | 3.6 | Mar | 184 |
| Apr-Jun | 0.8 | 0.3 | 7.6 | 2.6 | 2.1 | Apr | 162 |
| Jul-Sep | 0.7 | 0.3 | 8.3 | 2.9 | 2.0 | Sep | 151 |
| Oct-Dec | 1.1 | 0.8 | 7.8 | 2.8 | 5.6 | Dec | 310 |


a. Significant wave height

b. Peak wave period

Figure B2. 1980 mean, extreme, and standard deviations of significant wave height and
peak wave period for gage No. 620
Table B3
1980 Annual Joint Distribution of Significant Height

## 76101 <br> 

 Versus Peak Period for Gage No. 620
PERCENT OCCURRENCE (XIO) OF HEIGHT AND PERIOD $1110-9$


PE

heicht (metens)


Figure B3. Annual and seasonal distribution of significant wave height for gage No. 620
Table B4
1980 Seasonal Joint Distributions of Significant Height

$$
\begin{aligned}
& \text { 70101 }
\end{aligned}
$$

> PERCENT OCCLAROMAL- JAN-MAR
> MEI GOTT (RE TERS)
> $\begin{array}{r}\text { T4101 } \\ 4314329 \\ 38^{\circ} \% \\ 80^{\circ} \%\end{array}$
> 0.98
> PERCENT OCCLRREMCE (XIO) OF MEICHT AND PERIOD
> PERIODISECONDS :

PERCERT OCCUASONALE APR-JUN (XI\%) OF HEIEAT AND PERIOD

NEIGNT (TETERS)





PERCEMT OCCURREMCE (XIO) OF HE

| PERIOD(SECONDS) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0.0- | $3.9-9$ | 4.80 | $5.0-$ | $6.0-$ | $7.0-$ | $8.0-9$ | $9.0-9$ | $\begin{aligned} & 10.0- \\ & i 0.9 \end{aligned}$ | $\stackrel{11}{11.9}$ | ${ }_{12.0} 12$ | $13.0-$ | $14.0-$ | 15.9 | 16.0-9 | $\begin{aligned} & \text { 17:0- } \\ & \text { Lomeer } \end{aligned}$ |  |
| 7 |  |  | $?$ | 20 | 26 | 40 | 20 |  |  |  |  |  |  |  |  |  |
| $?$ | 20 | 20 | 60 | 53 | 26 | 245 | 79 | 53 | : | 46 | - | 26 | - | 7 | - | 186 |
| : | - |  | 20 | 46 | $?$ | 7 | . |  | - | 7 | : | 13 | - | - | - | 662 |
| - | : | - | ? | 7 | 7 | 2. | - | - | - | . | , |  | : | - | - | 107 |
| - | - | - | - | - | , | , | * |  | - | - | - | - |  |  |  | 4 |
| - | - | - | - | - | - | - | - | , | - | - | - | - | - |  |  | - |
| - | - | - | - | - | - | - | - | - | - | : | - | - | - | - | - | - |
| - | - | - | : | : | - | , | - | - | - | - | - | - | : | : | : | $\stackrel{\circ}{8}$ |
| 14 | 20 | 27 | 9 | 126 | ${ }_{6}{ }^{\circ}$ | 319 | 99 |  | - |  |  |  | - | * | - | - |
|  |  |  |  |  |  | 318 | 8 | 60 | - | 79 | 0 | 92 | 0 | 7 | $\dot{-}$ | - |



Table B5
Persistence* of 1980 Significant Wave Heights for Gage No. 620


[^5] of consecutive days.


Figure B4. 1980 time history of significant wave height and period for the nearshore Waverider (gage No. 610)
1980 Wave Statistics for Gage No. 610

| Monthly | $\begin{gathered} \text { Mean } \\ \text { Height, } m \end{gathered}$ | Standard Deviation Height, m | Mean <br> Period, sec | Standard Deviation Period, sec | Extreme Height, m | $\underline{\text { Date }}$ | Number Observations |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |
| Jan | 1.6 | 0.8 | 8.7 | 2.7 | 3.4 | 16 | 56 |
| Feb | 0.9 | 0.5 | 9.9 | 2.0 | 2.1 | 21 | 17 |
| Mar | 1.3 | 0.7 | 10.3 | 2.6 | 3.4 | 2 | 56 |
| Apr | 0.8 | 0.4 | 9.2 | 2.6 | 2.3 | 1 | 72 |
| May | 0.6 | 0.3 | 7.9 | 2.6 | 1.6 | 1 | 81 |
| Jun | 0.5 | 0.2 | 6.5 | 1.6 | 0.8 | 4 | 19 |
| Jul | No data |  |  |  |  |  |  |
| Aug | 0.6 | 0.3 | 7.5 | 1.5 | 1.5 | 22 | 33 |
| Sep | 0.7 | 0.3 | 9.8 | 2.6 | 1.8 | 30 | 43 |
| Oct | 0.9 | 0.6 | 8.6 | 2.8 | 3.8 | 25 | 105 |
| Nov | 1.0 | 0.5 | 8.6 | 3.1 | 2.2 | 24 | 119 |
| Dec | 1.0 | 0.7 | 8.2 | 3.1 | 3.3 | 29 | 106 |
| Annual | 0.9 | 0.6 | 8.7 | 2.8 | 3.8 | Oct | 707 |
| Seasonal |  |  |  |  |  |  |  |
| Jan-Mar | 1.4 | 0.8 | 9.6 | 2.7 | 3.4 | Jan | 129 |
| Apr-Jun | 0.7 | 0.3 | 8.3 | 2.6 | 2.3 | Apr | 172 |
| Jul-Sep | 0.7 | 0.3 | 8.8 | 2.5 | 1.8 | Sep | 76 |
| Oct-Dec | 1.0 | 0.6 | 8.5 | 3.0 | 3.8 | Oct | 330 |



Figure B5. 1980 mean, extreme, and standard deviations of significant wave height and peak wave period for gage No. 610
1980 Annual Joint Distribution of Significant Height

| PERCENT OCCURREMCE(XIO) OF HEIGHT AND PERIOD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HEICHT(METERS) | PERIOD(SECONDS) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
|  | 0.0-9 | 3.08 | $4.0-$ | $5.0-8.9$ | $6.0-9$ | $\stackrel{7.0-}{7.8}$ | 8.80 | $9.0-1$ | ${ }_{20.9}^{0-9}$ | $11.0-9$ | 12.09 | 13.00 | 14.0 | 15.0\% | 16.00 | $17.0-$ LONGER |  |
| 0.09 - .4 .49 | $\dot{3}$ | 10 | $30^{\circ}$ | 47 | $4{ }^{3}$ | 18 | 85 | 51 | 18 64 | 8 | 34 28 | 6 3 | 17 23 | 3 | 6 1 | $:$ | 205 422 193 |
| $1.09-1.49$ |  | 1 | 13 | 28 | 35 | 21 | 21 | 11 | 23 | 6 | 25 | $\frac{1}{1}$ | 8 | - | - | : | 193 |
| 1.50-1.99 | - | , | 1 | 6 | 25 | 13 | 16 | 8 | 6 | i | 10 | 13 | 19 | : | : | : | 31 |
| 2.00 - 2.48 | - | - | : | - | 1 | 3 1 | $\frac{3}{7}$ | 6 | 6 | 1 | 1 | 2 | 3 | : | - | - | 25 |
| -5.00-3.48 | - | : | - | : |  | 1 | 4 | 1 | 1 | - | 6 | - | 1 | - | - | - | 13 |
| $3.50-3.90$ | - | - | - | - | - | - | - | . | 1 | - | - | - | : | - | : | : | ${ }_{0}$ |
| 4.00 $=4.48$ | - | - | - | - | - | - | - |  | - | - | - | - | - | : | : | ! | 0 |
| $4.50=4.99$ | - | - | - | - | * | - | - | : | - | - | * |  | - | : | - | - | - |
| tOTAL | 3 | $1 i$ | 44 | 84 | $100^{\circ}$ | $8 i$ | 197 | 115 | 122 | 19 | 110 | 22 | 69 | 3 | 7 | - |  |



Figure B6. Annual and seasonal distribution of significant wave height for gage No. 610
PERCENT OCCURRENCE（XIO）OF HEIGHT AND PERIOD

PERCENT OCCURRONCE $(X 10)$ OF HEICHT AND PERIOD


HEIGHT（METERS）


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Table B8 (Concluded)


$$
76101
$$



Table B9
Persistence* of 1980 Significant Wave Heights for Gage No. 610


[^6] of consecutive days.


Figure B7. 1980 time history of significant wave height and period for the pier end Baylor (gage no. 625)

| Monthly | $\begin{gathered} \text { Mean } \\ \text { Height, } m \\ \hline \end{gathered}$ | Standard Deviation Height, m | Mean <br> Period, sec | Standard Deviation Period, sec | Extreme Height, m | Date | Number Observations |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Jan | 1.3 | 0.7 | 8.5 | 3.3 | 2.7 | 16 | 72 |
| Feb | 1.0 | 0.5 | 8.9 | 3.0 | 2.2 | 7 | 54 |
| Mar | 1.2 | 0.6 | 9.7 | 3.1 | 3.0 | 3 | 77 |
| Apr | 0.7 | 0.3 | 9.1 | 2.4 | 1.9 | 1 | 74 |
| May | 0.6 | 0.2 | 8.1 | 2.7 | 1.5 | 1 | 87 |
| Jun | 0.6 | 0.2 | 7.1 | 1.8 | 1.2 | 12 | 57 |
| Jul | 0.6 | 0.2 | 8.4 | 2.9 | 1.5 | 28 | 66 |
| Aug | 0.5 | 0.2 | 9.1 | 3.3 | 1.5 | 22 | 55 |
| Sep | 0.7 | 0.3 | 9.3 | 3.0 | 1.9 | 30 | 49 |
| Oct | 1.0 | 0.6 | 9.0 | 2.8 | 3.5 | 25 | 112 |
| Nov | 1.0 | 0.5 | 8.6 | 3.3 | 2.1 | 24 | 117 |
| Dec | 1.1 | 0.6 | 8.0 | 2.7 | 2.9 | 29 | 86 |
| Annual | 0.9 | 0.5 | 8.7 | 3.0 | 3.5 | Oct | 906 |
| Seasonal |  |  |  |  |  |  |  |
| Jan-Mar | 1.2 | 0.6 | 9.1 | 3.2 | 3.0 | Mar | 203 |
| Apr-Jun | 0.6 | 0.3 | 8.2 | 2.5 | 1.9 | Apr | 218 |
| Jul-Sep | 0.6 | 0.3 | 8.9 | 3.1 | 1.9 | Sep | 170 |
| Oct-Dec | 1.0 | 0.6 | 8.6 | 3.0 | 3.5 | Oct | 315 |



b. Peak wave period mean and standard deviation

Figure B8. 1980 mean, extreme, and standard deviation of significant wave height and peak wave period for gage No. 625

## Table B11

1980 Annual Joint Distribution of Significant Height

|  | PERICDISECONDS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $0.0-1$ | $3.0$ | $4.0-$ | $5.0-9$ | $6.0-$ | $7.0-1$ | $8.0-$ | $9.0-{ }^{1}$ | ${ }^{10.0-}$ | ${ }^{11} 11.9$ | $\begin{array}{r} 12.0-9 \\ 12.9 \end{array}$ | $\begin{array}{r} 13.0-9 \\ 13.9 \end{array}$ | $\begin{aligned} & 14.0- \\ & 14.8 \end{aligned}$ | $\begin{array}{r} 15.0-9 \\ 15.9 \end{array}$ | $\begin{gathered} 16.0 \\ 16.9 \end{gathered}$ | 17.0LONGER |  |
| -60 - 60.99 | $\dot{8}$ | 14 | $3{ }^{3}$ | 48 | 11 | 23 | 60 86 | 50 | 45 | 10 | 335 | 3 3 |  | $\frac{1}{3}$ | 2 | : | 229 |
| 1.00 - 1.40 | e | 14 | 3 | 29 | 38 | E1 | 24 | 15 | 13 | 7 | 29 | 7 | 4 |  |  | : | 196 |
| $1.50-1.90$ | - | - | 1 | 10 | 19 | 8 | 9 | 4 | 12 | 1 | 9 | 6 | 9 | 2 | , | : | 90 |
| 2.00-2.49 | - | - | - | - | 2 | 3 | 4 | 2 | 3 | 1 | 4 | - | 11 | - | - | - | 30 |
| 2.50-2.90 | - | - | - | - | 1 | 1 | 7 | 1 | 3 | - | 3 | - | 1 |  | - | - | 20 |
| $3.00=3.49$ | - | - | - | : | - | : | - | 1 | - | - | - | : | 1 | : | : | - |  |
| $3.50-3.98$ | : | * | - | : | : | : | : | 1 | : | : | : | : | - | : | : | : |  |
| $4.50=4.98$ | : | - | : | : | : | : | : | : | : | : | : | : | : | : | : | : |  |
| 5.09- OREATER | - |  |  |  |  |  |  |  |  |  |  |  | - | - | $\dot{\square}$ | - |  |
| TOTAL | 2 | 16 | 42 | 95 | 112 | 81 | 199 | 108 | 93 | 22 | 113 | 19 | 81 | 6 | 6 | 0 |  |



Figure B9. Annual and seasonal distribution of significant wave height for gage No. 625

HEICHT (PAETERS)

MEIGHT(METERS)


-     - 1111111,1


Table B12 (Concluded)

PERCENT OCCURRENCE (XIO) OF HEIGAT AND PERIOD

Table B13
Persistence* of 1980 Significant Wave Heights for Gage No. 625



[^7]
$$
1980 \text { Wave Statistics for Gage No. } 615
$$

| Monthly | Mean Height, m | Standard Deviation Height, m | Mean <br> Period, sec | Standard <br> Deviation <br> Period, sec |
| :---: | :---: | :---: | :---: | :---: |
| Jan | 0.9 | 0.5 | 6.8 | 2.8 |
| Feb | 0.9 | 0.4 | 8.3 | 2.9 |
| Mar | 0.9 | 0.5 | 9.5 | 3.7 |
| Apr | 0.6 | 0.2 | 8.7 | 3.3 |
| May | 0.5 | 0.2 | 8.4 | 3.5 |
| Jun | 0.5 | 0.2 | 6.6 | 2.2 |
| Jul | 0.5 | 0.2 | 7.2 | 3.3 |
| Aug | 0.4 | 0.1 | 7.9 | 3.5 |
| Sep | 0.6 | 0.2 | 10.3 | 3.4 |
| Oct | 0.6 | 0.3 | 9.1 | 3.0 |
| Nov. | 0.6 | 0.3 | 8.7 | 3.7 |
| Dec | 0.6 | 0.3 | 7.1 | 3.7 |
| Annual | 0.6 | 0.3 | 8.3 | 3.5 |
| Seasonal |  |  |  |  |
| Jan-Mar | 0.9 | 0.5 | 8.6 | 3.5 |
| Apr-Jun | 0.5 | 0.2 | 8.0 | 3.3 |
| Jul-Sep | 0.5 | 0.2 | 8.3 | 3.6 |
| Oct-Dec | 0.6 | 0.3 | 8.4 | 3.6 |



Overall
a. Significant wave height

b. Peak wave period mean and standard deviation

Figure B11. 1980 mean, extreme, and standard deviation of significant wave height and peak wave period for gage No. 615
Table B15
1980 Annual Joint Distribution of Significant Height
Versus Peak Period for Gage No． 615
PERCENT OCCURAENCE（X10）OF HEIGHT AND PERIOD

| $\stackrel{\rightharpoonup}{⿷ 匚}$ |  Nự |
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|  |  |
|  | ¢ٌ ${ }_{\text {¢ }}^{\text {¢ }}$ |
|  |  |
|  |  |

HEICHT（RAETERS）


－94089898980


Figure B12. 1980 annual and seasonal distribution for significant wave height for gage No. 615


76101 \% \% \% m

 $11.0-9$


88
79
$\stackrel{9}{\circ}$




NEIGNT (FETERS)


 ©isieg
Table B16（Concluded）

| MEICAT（AETERS | SEASOMAL－JUL－SEP |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | PERIOD（SECONDS）TOTAL |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | $0.0-2.0$ | $3.0-$ | $4.0-$ | $5.0-$ | $6.0-$ | $7.0-7.9$ | 8.88 .8 | 9．0－9．9 ${ }^{1}$ | $\begin{aligned} & 10.0- \\ & 10.9 \end{aligned}$ | 11.00 | $12.0-$ | 13.0 13.9 | $14.0-9$ | ${ }^{15.0} 15.9$ | $16.0-9$ 16.9 | 17．0－ LONGER |  |
| 0.09 － .49 | － | 12 | 60 | 54 | 48 | 12 | 131 | 30 | 42 |  |  | ． |  |  |  |  |  |
| 1．50－1．49 | ： | 24 | 71 | 83 | 42 | 30 12 | 36 18 | 24 | 18 | ： | 24 | $:$ | 65 | － | 30 | － | 556 417 |
| $1.50-1.99$ | － | ： | － | ： | － | 12 | 18 | ： | ： | ： | － | － | － | － | － | － | 30 |
| 2．00 $=2.49$ | － | － | － | － | － | － | ． | ： | ： | ： | ： | ： | － | － | － | － | ${ }^{\circ}$ |
| 2．50－ 2.98 | － | － | － | － | － | － | － | － | － | － | － | ： | － | ： | － | － | $\bigcirc$ |
| $3.50-3.90$ | ： | ： | ： | ： | ： | ： | － | － | － | － | － | － | － | － | ， | ！ | 8 |
| $4.00-4.49$ | ： | ： | ： | ： | ： | ： | － | － | － | － | － | － | － | － | － | － | － |
| $4.50-4.99$ | － | － | － | － | ． | ： | ： | ： | ： | － | － | － | － | － | － | － | $\bigcirc$ |
| 5．00 TOTAL GREATER | $\dot{\text {－}}$ | $3{ }^{\circ}$ | $13 i$ | 137 | 99 | 54 | $185^{\circ}$ | 54 | 9 | － |  | $\dot{\square}$ | $\dot{\square}$ | － | － | ： | ${ }_{0}^{8}$ |

[^8]Table B17


[^9] of consecutive days.


| Monthly | Mean <br> Hejght, m | Standard Deviation Height, m | Mean <br> Period, sec | Standard <br> Deviation <br> Period, sec | Extreme Height,m | Date | Number <br> Observations |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Jan | 1.09 | 0.39 | 9.06 | 2.97 | 1.94 | 16/17 | 79 |
| Feb | 1.01 | 0.36 | 8.96 | 2.69 | 1.79 | 26 | 53 |
| Mar | 1.14 | 0.49 | 10.01 | 3.01 | 2.23 | 4 | 74 |
| Apr | 0.78 | 0.33 | 9.50 | 2.85 | 1.91 | 1 | 68 |
| May | 0.63 | 0.28 | 8.47 | 3.01 | 1.68 | 1 | 84 |
| Jun | 0.72 | 0.28 | 7.26 | 1.78 | 1.37 | 13 | 52 |
| Jul | 0.69 | 0.30 | 8.00 | 2.15 | 1.74 | 28 | 59 |
| Aug | 0.62 | 0.27 | 9.59 | 2.64 | 1.72 | 22 | 61 |
| Sep | 0.80 | 0.37 | 10.12 | 2.70 | 1.84 | 30 | 45 |
| Oct | 0.96 | 0.52 | 9.47 | 2.73 | 2.83 | 25 | 115 |
| Nov | 0.99 | 0.50 | 8.42 | 2.57 | 1.95 | 12 | 94 |
| Annual |  |  |  |  |  |  |  |
| 1980 | 0.87 | 0.44 | 9.00 | 2.81 | 2.83 | Oct | 784 |
| 1977 | 0.65 | 0.28 | 9.02 | 2.86 | 2.13 | Dec | 850 |
| 1978 | 0.95 | 0.38 | 9.26 | 2.30 | 2.23 | Apr | 383 |
| 1979 | 0.76 | 0.35 | 9.24 | 2.50 | 1.90 | Jan | 368 |
| Cumulative |  |  |  |  |  |  |  |
| Jan 1977-Nov 1980 | 0.79 | 0.41 | 9.09 | 2.81 | 2.83 | Oct 1980 | 2385 |

Table B19
1980 Annual Joint Distribution of Significant Height
Versus Peak Period for Gage No. 112
OISTRIGUTION OF SIGNIFICANT HEIGHT VS PERIOD (IN OBSERVATIONS PER 1000 UBS)

|  | $0-1$ | 1-2 | $2 m 3$ | 3-4 | $4 \cdot 5$ | $5-6$ | $6 \pm 7$ | 7-8 | $8=9$ | $9-10$ | 10-11 | $11-12$ | $12 \mathrm{~m} 313+$ | TOT* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0.0-.9$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $1.0-1.9$ |  |  |  |  |  |  |  |  |  |  |  |  |  | 3 |
| 2.0-3.9 |  | 1 | 10 | 3 |  |  |  |  |  |  |  |  |  | 14 |
| $3.0-3.4$ $4.0-4.4$ |  | 3 | 24 | 11 | 3 |  |  |  |  |  |  |  |  | 41 |
| $5.0-5.9$ |  | 10 | 42 | 38 | 11 | 1 |  |  |  |  |  |  |  | 103 |
| $6.0-0.9$ |  | 26 | 24 | 26 | 20 | 8 | 3 |  |  |  |  |  |  | 106 |
| $7.0-7.9$ | 1 | 24 | 14 | 14 | 14 | 14 | 5 | 1 |  |  |  |  |  | 226 |
| 8.0-8.9 | 3 | 121 | 54 | 20 | 13 | 10 | 4 | 1 |  |  |  |  |  | 110 |
| $9.0-9.9$ | 1 | 38 | 29 | 15 | 14 | 8 | 4 |  |  |  |  |  |  | 183 |
| 10.0-10.9 |  | 19 | 29 | 14 | 10 | 6 | 4 |  |  |  |  |  |  | 28 |
| 11.0-11.9 |  | 10 | 5 | 5 | 4 | 1 | 1 |  |  | 1 |  |  |  | 01 |
| 12.0-12.9 | 3 | 36 | 13 | 28 | 9 | 13 |  |  |  |  |  |  |  | 1 |
| $13.0-13.9$ |  |  | 4 | 1 |  | 1 |  |  |  |  |  |  |  | 6 79 |
| 14.0-14.9 |  | 32 | 13 | 9 | 10 | 6 | 8 | 1 |  |  |  |  |  | 4 |
| $15.0-15.9$ | 1 | 3 |  |  |  |  |  |  |  |  |  |  |  | 9 |
| $16.0-16.9$ |  | 5 | 1 |  |  |  | 3 |  |  |  |  |  |  | 9 |
| TOTAL | 9 | 329 | 204 | 185 | 108 | 69 | 31 | 4 |  | 1 |  |  |  |  |



b. Peak wave period mean and standard deviation

Figure B14. 1980 mean, extreme, and standard deviation of significant wave height and peak wave period for gage No. 112
Table B20
Overall (1977-1980) Joint Distribution of Significant Height



Figure B15. Seasonal distribution of significant wave height for gage No. 112
Table B21
Seasonal Joint Distribution of Significant Height
DISTRIBUTIUN UF SIGNIFICAINT HEIGHI VS PERIUU (IN UBSEKVAIIONS PER 1000 UBS)
Versus Peak Period for Gage No. 112


|  | $0-1$ | 1-? | $2-3$ | 5-4 | $4-5$ | $5-6$ | $h=7$ | $7-8$ | $R=9$ | $9-10$ | $10-11$ | 11-12 | 12-1313+ | TUT.* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0.0-.9$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $1.0-1.4$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $2.0-2.4$ |  | 5 |  |  |  |  |  |  |  |  |  |  |  | 5 |
| $3.0=3.4$ |  | 5 | 15 | 10 |  |  |  |  |  |  |  |  |  | 29 |
| $4.0-4.9$ |  | 10 | 34 | 15 | 5 |  |  |  |  |  |  |  |  | 64 |
| $5.0-5.9$ |  | 20 | 74 | 25 | 10 |  |  |  |  |  |  |  |  | 127 |
| 0.0 0.0 .9 |  | 44 | 20 | 5 | 5 | 5 |  |  |  |  |  |  |  | 78 |
| $7.0-7.9$ | 5 | 20 | 34 | 34 | 10 |  |  |  |  |  |  |  |  | 103 |
| $8.0-8.9$ |  | 191 | 49 | 15 | 15 |  |  |  |  |  |  |  |  | 270 |
| 9.0-9.9 |  | 29 | 34 | 10 | 10 |  |  |  |  |  |  |  |  | 83 |
| 10.0-10.9 |  | 25 | 39 | 10 |  |  | 10 |  |  |  |  |  |  | 83 |
| $11.0-11.9$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 12.0-12.9 |  | 54 | 10 | 15 |  | 10 |  |  |  |  |  |  |  | 88 |
| 13.0-13.9 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 14.0 $=14.9$ |  | 39 | 15 |  |  |  |  |  |  |  |  |  |  | 54 |
| 15.0 $=15.4$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10.0-10.4 |  | 15 |  |  |  |  |  |  |  |  |  |  |  | 15 |
| TUTAL. | 5 | 456 | 324 | 137 | 54 | 15 | 10 |  |  |  |  |  |  |  |

Table B21 (Continued)

```
                    TOT.

18
30
42
91
41
358
121
42
79
121
```

Table B21 (Concluded)

Table B22
Persistence\% of 1980 Significant Wave Heights for Gage No. 112


The survey data are summarized into the following forms:
a. Monthly profile overlays. On each graph (see Figures C1-C13), profile data obtained on different survey dates during the month are displayed. The first profile shown is the last profile obtained on the previous month to better demonstrate how the profile changed through time. Generally, one profile was obtained per week, although profiles were obtained more frequently in March.
b. Time histories of bottom elevations at selected locations along the FRF pier. Each graph (see Figures C14-C22) shows how the bottom elevation varied throughout the year.
c. The vertical datum is NGDD; msl and NGVD are used interchangably for these graphs. The horizontal datum is an arbitrary line of monumentation landward of the dune.


Figure C1. FRF pier profiles for January 1980


Figure C2. FRF pier profiles for February 1980


Figure C3. FRF profiles for March 1980 (Sheet 1 of 2)


Figure C3. (Sheet 2 of 2)


Figure C4. FRF pier profiles for April 1980

a. North side

b. South side

Figure C5. FRF profiles for May 1980


Figure C6. FRF profiles for June 1980


Figure C7. FRF profiles for July 1980


Figure C8. FRF pier profiles for August 1980


Figure C9. FRF pier profiles for September 1980


Figure C10. FRF pier profiles for October 1980


Figure C11. FRF pier profiles for November 1980


Figure C12. FRF pier profiles for December 1980

JAN FEG MAR APR MAY JUN JUL ALO SEP OCT NOV OEC
1980
CHANGE IN ELEVATION FOR PROFILE LINE 69 AT
CERC FRF,DUCK N.C.
North side b. South side
Figure C13. Time histories of bottom elevations taken at 189 m
(pier station 6+20: nearshore Baylor location)

a. North side
 JAN FEG MAR APR MAY JUN JUL AUO SEP OCT NOV OEC
L980 PROFILE LINE G9 RT
CHANE IN ELEVATION FOR COR FRF,OUCK N.C. a. North side
Figure C14. Time histories of bottom elevations taken at 219 m
(pier station $7+20$ )

JAN Feg mar apr may Jun JUL auo sep oct nov dec
1980
CHANGE IN ELEVATION FOR PROFILE LINE E8 AT
CERC FRF, DUCh N.C.
a


Figure C15. Time histories of bottom elevations taken at 238 m (pier station $7+80$ )


a. North side
b. South side - (pier station 7+80)

 $\begin{array}{cc}\text { North side } & \text { b. South side } \\ \text { Figure C16. Time histories of bottom elevations taken at } 274 \mathrm{~m} \\ \text { (pier station } 9+00 \text { ) }\end{array}$


[^10]
JAN FEB MAR APR MAY JUN JUL RUO SEP OCT NOV OEC
CHANFE IN ELEVATION FGR PROFILE I. INE 69 AT
CERC FRF, OUCK N.C.

$\begin{array}{cc}\text { North side } & \text { b. South side } \\ \text { Figure C18. Time histories of bottom elevations taken at } 421 \mathrm{~m} \\ \text { (pier station } 13+80 \text { ) }\end{array}$

a.


[^11]b. South side
tories of bottom elevations taken at 433 m
(pier station $14+20$ )

a. North side
Figure C19.

JAN FEB MAR APR MAY JUN JUL AUQ SEP OCT NOV OEC
CHANGE IN ELEVATICN FOR PROFITE CINE EG AT
CERC FRF,OUCK N.C.

[^12]

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445.00

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[^13]VERTICAL DRTUM IS MSL
HORIZONTAL ORTUM IS
THE BENCHMARK
ध DATA MISSING


[^14]


[^0]:    * A table of factors for converting inch-pound units of measurement to metric (SI) units is presented on page 5.

[^1]:    Legend
    Onshore
    Offshore
    Figure 8. Times of wind direction change, 1980 (observations
    made every 6 hours)

[^2]:    Nags Head-112
    Nearshore Baylor-615
    Pier End Baylor-625
    Nearshore Waverider-610
    Offshore Waverider-620

[^3]:    Date (Mean Epoch)
    18 January, 2200 hours EST
    16 February, 1600 hours EST
    16 March, 1500 hours EST
    23 October, 1230 hours EST
    21 November, 1100 hours EST

[^4]:    *er Median depth from pier profiles taken from January to December 1980.
    $\dagger$ Pier length, 229 m.

[^5]:    Number of times during the year the given significant wave height was exceeded at least once a day for the specified number

[^6]:    * Number of times during the year the given significant wave height was exceeded at least once a day for the specified number

[^7]:    Figure B10. 1980 time history of significant wave height and period for the nearshore Baylor (gage No. 615)

[^8]:    total
     $\overrightarrow{m \omega}$ $\frac{\alpha}{4}$
    $6=\frac{0}{2}$
    0円••••••••••• ${ }_{0}^{10}$

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    $-0^{\circ} \mathrm{C}$
    
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    HEICHT（HETERS ）
    

[^9]:    Number of times during the year the given significant wave height was exceeded at least once a day for the specified number

[^10]:    a. North side
    b. South side

    Figure C17. Time histories of bottom elevations taken at 323 m (pier station $10+60$ )

[^11]:    TAभाNGE IN-ELEVATION FXR PROFILE LINE ES AT

[^12]:    a. North side
    b. South side

    Time histories of bottom elevations taken at 445 m (pier station $14+60$ )

    Figure C2O.

[^13]:    a. North side $\quad$ b. South side
    Figure C21. Time histories of bottom elevations taken at 579 m
    (pier end Baylor location)

[^14]:    $\begin{array}{cc}\text { North side } & \text { b. South side } \\ \text { Figure C22. Time histories of bottom elevations taken at } 591 \mathrm{~m}\end{array}$ (pier station $19+40$ )

