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# COMPILATION OF LONGSHORE CURRENT DATA

by Cyril J. Galvin and Richard A. Nelson



# U.S. ARMY COASTAL ENGINEERING RESEARCH CENTER



#### ABSTRACT

This paper is a compilation of published longshore current data available from North American sources as of January 1966. The data comprise 352 separate observations; of these 225 were obtained from four laboratory studies and 127 from four field studies. Each observation includes (at least) measured longshore current velocity, in feet per second; wave direction; a wave height, in feet; wave period, in seconds; and beach slope. Values of breaker height and breaker angle were computed for those observations lacking measured values. Longshore current velocity is usually less than 2 feet per second under both field and laboratory conditions. The maximum velocity observation from the field is 5.5 feet per second; from the laboratory 3.8 feet per second.

#### FOREWORD

Coastal engineers are examining longshore currents with increasing interest in the hope of predicting longshore current velocity from measurable characteristics of the waves and, eventually, the littoral transport rates that result from the flow of the currents. This compilation brings the available data together in a format that will be convenient to researchers. However, additional data are still needed, especially data accompanied by statistics of their variability and by a description of experimental procedure. Others working on this problem are invited to send copies of their published longshore current observations to CERC.

The paper was prepared by Cyril J. Galvin, Jr., Oceanographer, Research Division, U. S. Army Coastal Engineering Research Center, and Richard A. Nelson, graduate student, Department of Civil Engineering, Massachusetts Institute of Technology, assisted by J. D. Waggoner of the National Bureau of Standards.

At the time of publication, Colonel F. O. Diercks was Director of CERC, and J. M. Caldwell the Technical Director.

NOTE: Comments on this publication are invited. Discussion will be published in the next issue of the CERC Bulletin.

This report is published under authority of Public Law 166, 79th Congress, approved July 31, 1945, as supplemented by Public Law 172, 88th Congress, approved November 7, 1963.

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#### COMPILATION OF LONGSHORE CURRENT DATA

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Cyril J. Galvin, Jr. and Richard A. Nelson Research Division U. S. Army Coastal Engineering Research Center

#### I. Introduction

The principal goal of longshore current studies has been the prediction of longshore current velocity from measurable characteristics of the waves generating these currents. In order to test theoretical predictions of velocity or to calculate empirical predictions of velocity, data are necessary. Some data have been obtained and published in scattered journals. To make this data conveniently available, this article reprints, in standardized form, eight previously published sets of longshore current data, including four sets of field measurements (Putnam, Munk, and Traylor, 1949; Inman and Quinn, 1951; Moore and Scholl, 1961; Galvin and Savage, 1966)\* and four sets of laboratory measurements (Putnam, Munk, and Traylor, 1949; Saville, 1950, Brebner and Kamphuis, 1963; Galvin and Eagleson, 1965). These data are presented in tables following the list of references.

These eight sets of data, obtained under varying conditions using differing experimental procedures, are not equally reliable. The purpose of this paper is to merely list the data in convenient format and to briefly describe how they were obtained as a background to the review and evaluation given by Galvin (1967). Because the available data cannot be easily evaluated, a secondary purpose of this paper is to suggest the full publication of experimental procedure and statistics indicating the reliability of the data obtained by future research.

#### 2. Variables Listed

The eight sets of data, listed in the table, contain a total of 352 observations. A longshore current observation, for the purpose of this report, is the approximately simultaneous measurement of five variables: a mean longshore current velocity (VMEAS), in feet per second, the direction of the wave at breaking (THETAB) in degrees, the period of the breaking wave (TB) in seconds, the height of the breaking wave (HB) in feet, and the beach slope (SLOPE) dimensionless. These variables are defined in Figure I. Other measurements in the table include mean water depth at the breaking point (DB) in feet, given with Putnam, Munk, and Traylor's laboratory data, the direction of the wave (THETAO) in degrees, and the height of the wave in deep water (HO) in feet, as computed by Saville and Brebner and Kamphuis for their laboratory data, and the horizontal distance from the breaking position to the stillwater line on the beach (BVAL) in feet,

\* Parenthetical notations refer to LITERATURE C1TED on page 8.

measured in the experiments of Galvin and Eagleson. In some of the eight studies additional information was obtained, and this is discussed in the description of each investigation given in paragraph 4.

In the tables, laboratory data are listed first, followed by field data, each in chronological order. The compilation of data in the tables is reasonably complete, but other published studies may exist, especially in foreign literature. Other unpublished data are known to exist (Johnson, 1953, and Harrison and Krumbejn, 1964), and field data obtained at Nags Head, North Carolina, by the Coastal Studies Institute of Louisiana State University (Sonu and McCloy, 1966).

The first column of the table is an identification number (ID) consisting of the initials of the investigators (as PMT), the letter L or F to indicate laboratory or field studies, and a number identifying the observation within the particular set of data. The last column of the table, labeled COUNT, is an identification number running from I to 352.

#### 3. Difficulties in Measuring

Wave direction (THETAB) is the variable most difficult to measure with necessary accuracy. Visual field estimates are probably least reliable (Galvin and Savage, 1966) and even vertical photographs must have accurate horizontal control. The possibility of relative error increases markedly as THETAB decreases.

Longshore current velocity measurements (VMEAS) are more reliable than angle measurements, but this variable must be measured carefully because of the unsteadiness typical of field examples (Putnam, Munk, and Traylor, 1949) and the non-uniformity typical of laboratory examples (Brebner and Kamphuis, 1963; Galvin and Eagleson, 1965).

Wave height at breaking (HB) can be measured with reasonable accuracy, but care must be taken that measured values are representative. The wave gage must be fixed offshore of the mean breaking point and those waves which break before reaching the gage must be eliminated from the averages. Other problems arise because waves in nature have a finite crest length and are almost always subject to refraction effects; and on laboratory beaches, reflection causes partial standing waves which locally distort wave heights.

Wave period and beach slope can be measured within desirable accuracy under laboratory conditions. Under favorable conditions, wave period can be measured reasonably consistently in the field, either from oscillographs of the water surface or by visual observation. Well-controlled sounding from a pier permits accurate measurement of beach shape from which a slope may be defined. Similar sounding is necessary for laboratory sand beaches.

#### 4. Descriptions of Investigations

The following paragraphs describe the peculiarities of each set of data, in the order that they are listed in the tables, based on



SIDE VIEW

## FIGURE I. DEFINITION OF LONGSHORE CURRENT VARIABLES

information obtained from the papers of the respective authors.

#### a. Putnam, Munk, and Traylor Laboratory Observations (COUNT 1-37)

At the University of California at Berkeley, longshore current velocity was measured by timing the travel of potassium permanganate (KMnO4) dye on the central IO-foot section of a 39-foot (?) test beach. The breaker angle was obtained from vertical photographs, and wave height was measured by electric point gages.

A fixed, artificially roughened, plane beach was used in these experiments. For numbers I through 14, the beach surface was roughened by bonding natural sand to it. For numbers 15 through 28, the beach was covered with sheet metal or smooth cement. For numbers 29 through 37, the beach was covered with I/4-inch gravel bonded with a thin grout.

#### b. Saville Laboratory Observations (COUNT 38-46)

At the University of California at Berkeley, additional longshore current data were obtained during a study of sand transport. The travel of KMn04 dye along a 10-foot segment of the 60-foot beach was timed to obtain velocity. Wave heights offshore were measured with point gages. Offshore of the surf zone, the beach was concrete, and inshore it was 0.3 mm sand. The slope listed in the table (0.10) is that of the concrete, but the slope in the surf zone may have been lower.

Breaker angle (THETAB) and breaker height (HB) were not measured, but the theoretical values in deep water (THETAO and HO) were computed from small-amplitude wave theory. THETAB and HB were computed in this study for the table using refraction graphs (Johnson, O'Brien, and Isaacs, 1948) and (Le Mehaute, 1961). The zero value of VMEAS in observation number 46 (SAVL 9) is for a run in which little net longshore current was observed.

#### c. Brebner and Kamphuis Laboratory Observations (COUNT 47-187)

These data were obtained from a model study at Queens University, Kingston, Ontario, Canada. THETAB and HB were not measured, so the values listed in the table were also computed by using refraction graphs as for Saville's data. Velocity was measured by timing the travel of an immiscible, neutral-density fluid along the beach between 15 and 20 feet from the upstream wall. The concrete beach was at least 30 feet long and roughened by indentations spaced on one-inch centers. Offshore wave heights (not in table) were measured with an electric point gage.

#### d. Galvin and Eagleson Laboratory Observations (COUNT 188-225)

At the Massachusetts Institute of Technology, Hydrodynamics Laboratory, wooden floats and a current meter were used to measure longshore current velocity. The listed velocity is that observed at 18 feet from the upstream wall but considerable additional data are available on the two-dimensional velocity distribution in the surf zone, as well as the distribution of setup over the whole beach. The overall beach was 30 feet long, of which 20 feet made up the test section. Most values of THETAB are the average of twenty measurements with a protractor. Wave height was measured with a parallel-wire resistance gage.

All blanks in the table for the data of Galvin and Eagleson indicate that the quantity was not measured.

#### e. Putnam, Munk, and Traylor Field Observations (COUNT 226-243)

At Oceanside, California, velocity was measured using weighted floats and fluorescein dye. Additional data was obtained showing the unsteadiness of the current. THETAB was measured with a compass from a pier or from photographs taken from a blimp. Slope was obtained by sounding from a pier. Observations 238 and 242 were obtained during a 22-knot following wind approximately parallel to the shore.

#### f. Inman and Quinn Field Observations (COUNT 244-276)

Velocity was measured at the water surface and at the bottom of the surf zone by timing the travel of floating kelp and weighted, tethered soccer balls. The velocities given by Inman and Quinn are already the averages of measurements made at 15 stations spaced at about 300-foot intervals at Torrey Pines and Pacific Beach (near La Jolla), California. Their statistics show that the standard deviations often exceed the mean velocity. In table 6, the velocity listed is the average of the bottom and surface velocities whenever both are given. HB was estimated by an observer on the beach. More than half of the values of THETAB were measured with a transit sighting bar. Zeros in the table mean that the variables, averaged over the 15 stations, had approximately zero magnitude.

#### g. Moore and Scholl Field Observations (COUNT 277-347)

Daily measurements were made during the summer of 1960 at Ogoturuk Beach, Alaska. THETAB was measured to the nearest 5° by compass, HB was estimated to the nearest tenth of a meter, and VMEAS in cm/sec with dye. Moore and Scholl's data, given originally in the metric system, are presented here in English units to conform with the other studies. SLOPE was not measured during the study and the value listed under SLOPE is a nominal one taken from a profile in their paper. The gravel beaches in this area produce steeper slopes than the sand beaches in the other field studies. Zeros listed in the table are measured values.

During observations numbered 285, 287, 295, 300, 302, and 322, the direction of the longshore current flow was opposite the direction from which the waves approached (indicated by minus signs on the velocity in the table).

#### h. Galvin and Savage Field Observations (COUNT 348-352)

At Nags Head, North Carolina, velocity was measured by timing the travel of balloons filled with freshwater. Most values of THETAB were obtained by compass but some were also obtained by measuring the speed of the plunge point of the breaker or by crude triangulation. Wave height (HB) was measured visually or from oscillographs of the water surface. SLOPE was the average slope between the mean water line and a point 6 feet below mean water level. Other data include histograms showing the distribution of some of the measured variables from this CERC field project at Nags Head. THETAB in observation 352 is a single measurement at a time of changing wave conditions. VMEAS in observation 351 was small but not actually zero. Wind speed was high during nearly all the Nags Head measurements.

#### 5. Discussion of Data

The data in the tables and the foregoing descriptions indicate differences among the sets of data. Among the laboratory studies, some differences are in the magnitude of the variables tested. For example, the laboratory conditions of Putnam, Munk, and Traylor are for conditions producing high values of VMEAS and THETAB. Of the 225 laboratory observations in the listing, six observations in the data of Putnam, Munk, and Traylor account for the six highest velocities (2.2 to 3.8 ft/sec) and the six highest breaker angles (39° to 38°). No value of THETAB in their laboratory experiments was less than 10°, but all of Saville's data, and most of the measurements of Galvin and Eagleson were for conditions producing THETAB less than 10°.

There are also differences in the variables which the investigators chose to measure. In the laboratory experiments of Saville and of Brebner and Kamphuis, THETAB and HB were not measured, but THETAO and HO were computed from offshore measurements instead. As explained in paragraph 4, the values of THETAB and HB for these two studies were newly computed for this paper; thus they will vary more regularly, yet they may be less accurate than actual measurement.

The experimental conditions of the laboratory tests also differ considerably. No two of the basins were alike in size and layout, and Saville's measurements were the only ones made on a deformable sand beach.

Large differences among the data from the field studies are also evident. The data of Inman and Quinn, although they provide useful statistics on variability, cannot be readily compared with other field measurements because their data are spatial averages along the beach. The data of Moore and Scholl are for lower waves, steeper beaches, and weaker currents than the other field studies. The few observations in the Nags Head study are accompanied by documented uncertainties, many of which were probably present in the other studies as well. Putnam, Munk, and Traylor velocities and Nags Head velocities are, on the average, significantly higher than in the other studies.

Viewed as a whole, the difference in magnitude between the laboratory and field data is greatest in wave height, and less for wave period and beach slope. Surprisingly, there is little difference between the average magnitudes of the field and laboratory measurements of THETAB and VMEAS, despite the fact that wave heights differ by nearly two orders of magnitude.

Accurate measurement of longshore currents in the field and laboratory are still needed, particularly measurements of currents produced by conditions intermediate between laboratory and ocean wave conditions. The nonuniformity and unsteadiness of longshore currents should be studied under controlled laboratory conditions, including how they are affected by variations in the geometry of the laboratory basin. In future studies, more effort should be made to document the reliability of the experimental procedure and the variability of the data.

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TABLE	Ε.Γ
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LABORATORY DATA BY PUTNAM, MUNK, AND TRAYLOR

١D		HB FT	TB SEC	THETAB DEGREE	SLOPE	VMEAS FPS_	DB FT	COUNT
PMTL	1	0.47	1.00	18.3	0.066	0.78	0.75	 I
PMTL	2	0.32	1.06	13.8	0.066	0.64	0.44	2
PMTL	3	0.40	1.14	14.6	0.066	0.82	0.56	3
PMTL	4	0.31	1.15	12.6	0.066	0.68	0.41	4
PMTL	5	0.30	1.25	11.7	0.066	0.76	0.39	5
PMTL	6	0.32	1.32	11.7	0.066	0.75	0.40	б
PMTL	7	0.29	1.40	10.9	0.066	0.64	0.37	7
PMTL	8	0.16	1.90	17.6	0.144	0.75	0.24	8
PMTL	9	0.15	2.13	17.2	0.144	0.66	0.23	9
PMTL	10	0.15	2.22	17.3	0.144	0.50	0.24	10
PMTL		0.28	0.72	18.2	0.241	1.33	0.48	
PMTL	12	0.35	0.92	16.5	0.241	1.27	0.52	12
PMTL	13	0.22	1.14	10.4	0.241	0.53	0.28	13
PMTL	14	0.22	1.22	10.6	0.241	0.69	0.27	14
PMTL	15	0.24	0.99	28.0	0.100	1.68	0.32	15
PMTL	16	0.22	1.32	22.8	0.100	1.45	0.27	16
PMTL	17	0.16	1.63	18.8	0.100	0.96	0.23	17
PMTL	18	0.16	1.98	18.4	0.100	0.76	0.22	18
PMTL	19	0.28	0.83	56.6	0.139	2.46	0.43	19
PMTL	20	0.23	0.91	45.3	0.139	2.31	0.33	20
PMTL	21	0.22	1.00	38.8	0.139	2.22	0.29	21
PMTL	22	0.20	1.12	33.2	0.139	1.93	0.24	22
PMTL	23	0.20	1.35	31.1	0.139	1.52	0.25	23
PMTL	24	0.34	0.80	57.5	0.260	3.78	0.62	24
PMTL	25	0.29	0.90	52.5	0.260	3.34	0.43	25
PMTL	26	0.28	0.98	47.2	0.260	3.00	0.41	26
PMTL	27	0.20	1.23	32.5	0.260	191	0.26	27
PMTL	28	0.22	1.27	31.9	0.260	1.76	0.23	28
PMTL	29	0.26	0.95	30.1	0.098	1.03	0.36	29
PMTL	30	0.21	1.33	21.4	0.098	0.46	0.27	30
PMTL	31	0.16	1.67	18.0	0.098	0.20	0.20	31
PMTL	32	0.12	1.99	16.4	0.098	0.15	0.19	32
PMTL	33	0.33	1.08	30.4	0.143	1.32	0.47	33
PMTL	34	0.29	1.36	24.6	0.143	0.63	0.38	34
PMTL	35	0.20	1.58	19.3	0.143	0.36	0.27	35
PMTL	36	0.20	1.91	18.4	0.143	0.32	0.26	36
PMTL	37	0.22	2.32	19.1	0.143	0.18	0.30	37

## LABORATORY DATA BY SAVILLE

		HB	HO	TB	THETAB	THETAO		VMEAS	
<u>ID</u>		FT	FT	SEC	DEGREE	DEGREE	SLOPE	FPS	COUNT
SAVL	1	0.147	0.146	0.71	7.7	10.0	0.10	0.32	38
SAVL	2	0.138	0.129	0.85	6.7	10.2	0.10	0.27	39
SAVL	3	0.132	0.116	0.94	6.3	10.5	0.10	0.25	40
SAVL	4	0.130	0.110	1.00	5.6	10.8	0.10	0.21	41
SAVL	5	0.171	0.169	0.74	7.2	10.0	0.10	0.40	42
SAVL	6	0.154	0,147	0.85	6.7	10.2	0.10	0.32	43
SAVL	7	0.144	0.126	0.99	5.6	10.7	0.10	0.24	44
SAVL	8	0.137	0.106	1.17	5.2	11.4	0.10	0.07	45
SAVL	9	0.127	0.082	1.50	4.7	13.1	0.10	0.00	46

LABORATORY DATA BY BREBNER AND KAMPHUIS

ID		HB FT	HO FT	TB SEC	THETAB DEGREE	THETAO DEGREE	SLOPE	VMEAS FPS	COUNT
BKI	1	0 092	0 075	1 13	7 0	21.9	0.10	0 44	47
BKI	2	0.092	0.089	1 00	7.5	20.9	0.10	0.47	48
BKI	3	0.110	0.112	0.87	9.0	20.3	0.10	0.67	40
BKI	4	0.118	0.124	0.78	10.0	20.1	0.10	0.82	50
BKI	5	0 118	0.106	1.13	7.5	21.9	0.10	0.49	51
BKI	6	0.138	0 129	1 00	8.0	20.9	0.10	0.67	52
BKI	7	0 153	0 157	0.87	10.0	20.3	0.10	0.83	53
BKI	8	0 159	0 172	0.78	12.0	20.1	0.10	0.99	54
BKI	9	0 157	0.151	1.13	9.0	21.9	0.10	0.63	55
BKI	ió	0 159	0.167	1 00	9.5	20.9	0.10	0.80	56
BKI	11	0.200	0 207	0.87	12.0	20.3	0.10	0.96	57
BKI	12	0.200	0.212	0.78	13.0	20.1	0.10	1 07	58
BKL	13	0.205	0.174	1 13	9.0	21.9	0.10	0.63	59
BKI	11	0.220	0.211	1 00	11.0	20.9	0.10	0.88	60
BKI	15	0.228	0.242	0.87	12.5	20.3	0.10	1 04	61
DICL	16	0.220	0.242	0.07	12.5	20.5	0.10	1.16	62
DKL	17	0.201	0.207	1 13	14.0	33.1	0.10	0.60	63
DKL	18	0.092	0.070	1.00	10.0	31 /	0.10	0.00	61
DKL	10	0.112	0.009	0.97	13.0	30 5	0.10	0.01	65
DNL	20	0.110	0.125	0.07	15.0	30.1	0.10	0.04	66
DKL	20	0.110	0.125	1 13	12.0	33 1	0.10	0.91	67
DKL	21	0.110	0.107	1.10	11.0	21 4	0.10	0.03	60
BKL	22	0.155	0.150	1,00	12.9	20 5	0.10	0.97	60
BKL	22	0.155	0.150	0.07	15.0	30.9	0.10	1.04	70
BKL	24	0.159	0.172	0./8	17.0	50.1	0.10	1.14	70
BKL	25	0.170	0.155	1.13	15.0	22.I	0.10	0.94	/1
BKL	26	0.158	0.168	1.00	14.0	21.4	0.10	1.12	12
BKL	27	0.200	0.208	0.87	17.0	50.5	0.10	1.20	15
BKL	28	0.194	0.212	0.78	18.0	30.1	0.10	1.52	74
BKL	29	0.184	0.176	1.15	13.0	55.1	0.10	1,07	15
BKL	30	0.204	0.212	1.00	16.0	51.4	0.10	1.25	/6
BKL	31	0.231	0.244	0.87	18.0	30.5	0.10	1.29	17
BKL	32	0.234	0.258	0.78	21.0	30.1	0.10	1.32	78
BKL	33	0.085	0.077	1.13	12.0	44.5	0.10	0.70	79
BKL	34	0.097	0.090	1.00	14.0	42.1	0.10	0.83	80
BKL	35	0.110	0.113	0.87	17.0	40.7	0.10	0.88	81
BKL	36	0.112	0,125	0.78	18.0	40.2	0.10	1.05	82
BKL	37	0.118	0.109	1.13	14.0	44.5	0.10	0.91	83
BKL	38	0.133	0.131	.00	16.0	42.1	0.10	0.96	84
BKL	39	0.141	0.158	0.87	18.0	40.7	0.10	1.10	85
BKL	40	0.147	0.172	0.78	21.0	40.2	0.10	.22	86
BKL	41	0.151	0.156	1.13	17.0	44.5	0.10	1.08	87
BKL	42	0.153	0.170	1.00	18.0	42.1	0.10	1.18	88
BKL	43	0.176	0.209	0.87	22.0	40.7	0.10	1.36	89
BKL	44	0.187	0.213	0.78	24.0	40.2	0.10	1.53	90
BKI	45	0 177	0 179	1 13	17 0	44 5	0 10	1.21	91

TABLE 3 (Continued)

	D	HB FT	HO FT	TB SEC	THETAB DEGREE	THETAO DEGREE	SLOPE	VMEAS FPS	COUNT
I BKL BKL BKL BKL BKL BKL BKL BKL BKL BKL	46 47 48 49 50 51 52 53 54 55 57 58 59 60 61 62 63 65 66 67 68 69 70 71 72 73 74 75 76 77 80	HB FT 0.189 0.204 0.085 0.097 0.110 0.112 0.118 0.133 0.141 0.153 0.176 0.153 0.176 0.153 0.176 0.187 0.177 0.189 0.204 0.085 0.097 0.104 0.109 0.118 0.123 0.137 0.147 0.153 0.137 0.153 0.184 0.175 0.184 0.208 0.215 0.085 0.092	HO FT 0.214 0.243 0.077 0.090 0.113 0.125 0.109 0.131 0.158 0.172 0.156 0.172 0.209 0.213 0.179 0.214 0.243 0.179 0.214 0.243 0.125 0.113 0.125 0.113 0.125 0.113 0.125 0.113 0.125 0.113 0.125 0.113 0.125 0.113 0.125 0.113 0.125 0.113 0.125 0.113 0.243 0.125 0.214 0.209 0.213 0.229 0.213 0.229 0.213 0.229 0.213 0.229 0.213 0.229 0.213 0.229 0.213 0.229 0.213 0.229 0.213 0.229 0.213 0.229 0.213 0.229 0.213 0.2209 0.213 0.2209 0.213 0.2209 0.213 0.2209 0.213 0.2209 0.213 0.2209 0.225 0.2200 0.2200000000	TB SEC 1.00 0.87 1.13 1.00 0.87 0.78 1.13 1.00	THETAB DEGREE 19.0 23.0 12.0 14.0 17.0 18.0 14.0 16.0 18.0 21.0 17.0 18.0 22.0 24.0 17.0 19.0 22.0 24.0 17.0 19.0 23.0 14.0 19.0 22.0 16.0 19.0 22.0 26.0 26.0 28.0 20.0 23.0 27.0 32.0 16.0 18.0 27.0 32.0 27.0 32.0 28.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27	THETAO DEGREE 42.1 40.7 44.5 42.1 40.7 40.2 44.5 42.1 40.7 40.2 44.5 42.1 40.7 40.2 44.5 42.1 40.7 40.2 44.5 42.1 40.7 50.3 56.7 53.1 51.0 50.3 56.7 57.10 50.3 56.7 57.10 50.3 56.7 57.10 50.3 56.7 57.10 50.3 56.7 50.3 50.3 56.7 50.3 50.3 50.3 50.3 50.3 50.3 50.3 50.3	SLOPE 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.1	VMEAS FPS 1.34 1.48 0.66 0.74 0.90 1.03 0.85 0.95 1.10 1.26 1.03 1.14 1.35 1.56 1.09 1.29 1.42 0.61 0.75 0.89 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.00 1.02 0.97 1.13 1.35 1.00 1.02 0.97 1.13 1.35 1.00 1.02 0.97 1.14 1.35 1.00 1.02 0.97 1.13 1.35 1.00 1.02 0.97 1.13 1.35 1.00 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.35 1.06 1.02 0.97 1.13 1.52 1.79 1.43 1.52 1.79 1.43 1.52 1.79 1.43 1.52 1.79 1.73 1.73 1.73 1.73 1.73 1.73	COUNT 92 93 94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 126
BKL BKL BKL BKL BKL BKL BKL BKL BKL BKL	81 82 83 84 85 86 87 88 89 90 91 92 93	0.104 0.103 0.112 0.129 0.140 0.138 0.143 0.172 0.169 0.151 0.179 0.192	0.115 0.125 0.130 0.139 0.161 0.173 0.186 0.180 0.212 0.214 0.214 0.227 0.248	0.87 0.78 1.13 1.00 0.87 0.78 1.13 1.00 0.87 0.78 1.13 1.00 0.87	22.0 24.0 19.0 21.0 25.0 28.0 21.0 23.0 28.0 31.0 22.0 26.0 30.0	61.5 60.5 70.9 64.7 61.5 60.5 70.9 64.7 61.5 70.9 64.7 61.5	0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10	0.87 0.99 0.86 1.01 1.10 1.25 1.03 1.15 1.28 1.48 1.12 1.27 1.42	127 128 129 130 131 132 133 134 135 136 137 138 139

TABLE 3 (Continued)

ID	)	HB FT	HO FT	TB SEC	THETAB DEGREE	THETAO DEGREE	SLOPE	VMEAS FPS	COUNT
BKL BKL BKL BKL BKL BKL BKL BKL BKL BKL	94 95 96 97 98 90 101 102 103 104 105 106 107 108 109 110 112 113 114 115 116 117 118	HB FT 0.203 0.092 0.097 0.110 0.118 0.138 0.153 0.159 0.157 0.159 0.200 0.203 0.177 0.220 0.228 0.231 0.092 0.112 0.110 0.118 0.133 0.153 0.153 0.155	H0 FT 0.259 0.075 0.089 0.112 0.124 0.106 0.129 0.157 0.172 0.151 0.167 0.207 0.212 0.174 0.212 0.174 0.212 0.174 0.242 0.257 0.076 0.089 0.113 0.125 0.107 0.130 0.158 0.172	TB SEC 0.78 1.13 1.00 0.87 0.78 1.13 1.00 0.87 0.78 1.13 1.00 0.87 0.78 1.13 1.00 0.87 0.78 1.13 1.00 0.87 0.78 1.13 1.00 0.87 0.78 1.13 1.00 0.87 0.78	THETAB DEGREE 35.0 7.0 7.5 9.0 10.0 7.5 8.0 10.0 12.0 9.0 9.5 12.0 13.0 9.0 13.0 9.0 11.0 12.5 14.0 10.0 11.0 12.5 14.0 10.0 11.0 12.5 15.0 17.0	THETAO DEGREE 60.5 21.9 20.9 20.3 20.1 21.9 20.9 20.3 20.1 21.9 20.9 20.3 20.1 21.9 20.9 20.3 20.1 21.9 20.9 20.3 20.1 21.9 20.9 20.3 20.1 3.1 31.4 30.5 30.1 31.4 30.5 30.1	SLOPE 0.10 0.05	VMEAS FPS 1.66 0.49 0.56 0.62 0.68 0.66 0.67 0.69 0.71 0.73 0.80 0.81 0.84 0.82 0.84 0.63 0.61 0.65 0.64 0.65 0.64 0.76 0.68 0.76 0.78	COUNT 140 141 142 143 144 145 146 147 148 149 150 151 152 153 154 155 156 157 158 159 160 161 162 163 164
BKL BKL BKL BKL BKL BKL BKL BKL BKL BKL	114 115 116 117 118 119 120 121 122 123 124 125 126	0.118 0.133 0.153 0.159 0.170 0.158 0.200 0.194 0.204 0.204 0.231 0.234	0.123 0.107 0.130 0.158 0.172 0.153 0.168 0.208 0.212 0.176 0.212 0.244 0.258	0.78 1.13 1.00 0.87 0.78 1.13 1.00 0.87 0.78 1.13 1.00 0.87 0.78	11.0 12.5 15.0 17.0 13.0 14.0 17.0 18.0 13.0 16.0 18.0 21.0	30.1 31.4 30.5 30.1 33.1 31.4 30.5 30.1 33.1 31.4 30.5 30.1	0.05 0.05	0.84 0.76 0.68 0.76 0.78 0.86 0.78 0.90 0.90 0.90 0.92 0.98 1.03	160 161 162 163 164 165 166 167 168 169 170 171 172
BKL BKL BKL BKL BKL BKL BKL BKL BKL BKL	27  28  29  30  31  32  33  34  35  36  37  38  39  40  4	0.085 0.097 0.110 0.112 0.118 0.133 0.141 0.147 0.151 0.153 0.176 0.187 0.189 0.204	0.077 0.090 0.113 0.125 0.109 0.131 0.158 0.172 0.156 0.170 0.209 0.213 0.179 0.214 0.243	1.13 1.00 0.87 0.78 1.13 1.00 0.87 0.78 1.13 1.00 0.87 0.78 1.13 1.00 0.87 0.78	12.0 14.0 17.0 18.0 14.0 16.0 18.0 21.0 17.0 18.0 22.0 24.0 17.0 19.0 23.0	44.5 42.1 40.7 40.2 44.5 42.1 40.7 40.2 44.5 42.1 40.7 40.2 44.5 42.1 40.7	0.05 0.05	0.66 0.80 0.68 0.83 0.79 0.89 1.00 1.07 0.87 1.07 1.04 1.12 1.06 1.07 1.15	173 174 175 176 177 178 179 180 181 182 183 184 185 186 185

## LABORATORY DATA BY GALVIN AND EAGLESON

10	)	HB FT	TB SEC	THETAB DEGREE	SLOPE	BVAL FT	VMEAS FPS	COUNT
GEL	1		1.00	5.4	0.109	0.83	1.62	188
GEL	2	0.21	1.12	5.1	0.109	0.82	1.53	189
GEL	3	0.14	1.25	3.3	0.109	0.68	1.33	1.90
GEL	4	0.19	1.37	2.3	0.109	0.53	1.24	191
GEL	5		1.50	3.1	0.109	0.52	1.17	192
GEL	5	0.03	1.25	2.6	0.109	0.34	0.62	193
GEL	/	0.12	1.25	2.1	0.109	0.50	0.87	194
GEL	8	0.17	1.25	5.8	0.109	0.6/	1.21	195
GEL	9	0.17	1.25	2.1	0.109	0.71	1.07	196
GEL	10	0.19	1.20	4.0	0.109	0.84	1.44	197
GEL	12	0.07	1.00		0.109	0.21	0.76	198
GEL	12	0.09	0 00	2.9	0.109	0.49	0.90	199
GEL	1/	0.10	1 00	14	0.109	1.01	1 52	200
GEL	14	0.19	1.00	14.1	0.109	1.70	1.72	201
GEL	16	0.19	1 25	10 1	0.109	1.00		202
GEL	17	0.19	1.37	9 7	0.109	1.42	1.44	205
GEL	18	0.16	1.50	6.9	0.109	1.23	1.13	204
GEL	19	0.09	1.25	6.1	0,109	0.56	0.68	205
GEL	20	0.13	1.25	6.6	0.109	0.96	0.85	207
GEL	21	0.15	1.25	8.6	0.109	1.23	1.11	208
GEL	22	0.17	1.25	9.8	0.109	1.49	1,33	209
GEL	23	0.17	1.25	11.0	0.109	1.77	1.55	210
GEL	24	0.11	1.50	3.7	0.109		0.77	211
GEL	25	0.11	1.00	9.7	0.109		0.94	212
GEL	26	0.18	1.00	28.0	0.109	2.15	1.40	213
GEL	27		1.12	21.8	0.109	1.89	1.15	214
GEL	28	0.19	1.25	18.6	0.109	1.91	1.22	215
GEL	29		1.37	15.7	0.109	1.81	1.32	216
GEL	30	0.10	1.50	8.6	0.109	0.91	0.91	217
GEL	31	0.16	1.25	13.3	0.109	0.65	0.69	218
GEL	32	0,13	1.25	14.3	0.109	1.20	0.83	219
GEL	33	0.16	1.25	19.6	0.109	1.57	1.19	220
GEL	34		1.25	19.6	0.109	1.88	1.27	221
GEL	35		1.25	22.5	0.109	1.96	1.29	222
GEL	56 77		1.50	6.0	0.109	0.18	0.57	223
GEL	51		1.00	20.1	0.109	1.46	0.88	224
GEL	.20		1.00	10.9	0.109		1.11	115

FIELD DATA BY PUTNAM, MUNK, AND TRAYLOR

		HB	ТВ	THETAB	1	VMEAS	
١D		FT	SEC	DEGREE	SLOPE	FPS	COUNT
						0 5	
PMIF	I	5.0	10.0	15.0	0.016	2.5	226
PMTF	2	5.5	9.0	12.0	0.020	2.2	227
PMTF	3	7.0	9.0	15.0	0.023	3.0	228
PMTF	4	6.0	7.0	7.5	0.017	8. ا	229
PMTF	5	5.0	10.0	10.0	0.031	3.6	230
PMTF	б	8.0	10.0	10.0	0.022	2.8	231
PMTF	7	8.0	10.0	10.0	0.023	2.3	232
PMTF	8	6.5	12.0	10:0	0.020	2.4	,233
PMTF	9	4.5	12.0	10.0	0.020	2.4	234
PMTF	10	4.5	12.0	10.0	0.019	2.7	235
PMTF		4.5	12.0	10.0	0.019	2.1	236
PMTF	12	6.5	15.0	5.0	0.016	1.7	237
PMTF	13	8.0	7.0	17.5	0.022	5.2	238
PMTF	14	5.0	8.0	10.0	0.030	3.3	239
PMTF	15	8.5	8.0	12.0	0.020	2.5	240
PMTF	16	5.0	15.0	5.0	0.026	2.4	241
PMTF	17	9.0	8.0	15.0	0.019	5.5	242
PMTF	18	9.0	8.0	15.0	0.019	3.9	243

FIELD DATA BY INMAN AND QUINN

ID		HB FT	TB SEC	THETAB DEGREE	SLOPE	VMEAS FPS	COUNT
ID IQF IQF IQF IQF IQF IQF IQF IQF IQF IQF	 2 3 4, 5 6 7 8 9 10 11 12 13 14 15 16 17 18 20 21 22 23 24 25 26 27 28 29 31	FT 2.8 3.1 3.7 4.9 3.4 2.6 3.4 2.6 3.4 2.5 4.7 4.2 4.7 4.2 2.6 1.7 4.2 1.5 5.7 7.6 4.2 1.5 7.7 6.2 1.5 7.7 6.2 1.5 7.7 7.6 7.6 7.6 7.5 7.6 7.5 7.6 7.5 7.6 7.5 7.6 7.5 7.6 7.5 7.6 7.5 7.6 7.5 7.6 7.5 7.6 7.5 7.6 7.5 7.6 7.5 7.6 7.5 7.6 7.7 7.5 7.6 7.7 7.5 7.6 7.7 7.5 7.7 7.6 7.7 7.6 7.7 7.7 7.6 7.7 7.7	SEC 15.0 8.5 8.0 14.0 8.0 7.0 12.5 8.0 9.5 10.0 13.5 13.0 10.0 13.5 13.0 10.0 12.0 8.0 12	DEGREE 6.5 1.5 4.0 0. 5.0 5.0 0. 0. 0. 0. 0. 0. 0. 0. 0.	SLOPE 0.027 0.027 0.027 0.027 0.027 0.027 0.027 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.027 0.014 0.014 0.014 0.014 0.014	FPS 0.38 0.04 0.22 0.04 0.21 0.55 0.04 0.01 0.15 0.09 0.21 0.50 0.29 0.53 0.70 1.19 0.40 0.36 0.23 0.56 0.11 0.54 0.62 0.49 0.17 0.13 1.37 0.04	COUNT 244 245 246 247 248 249 250 251 252 253 254 255 256 257 258 259 260 261 262 263 264 265 266 267 268 269 270 271 272 273 274
IQF IQF	32 33	2.0	14.5	4.0 2.5	0.014	0.11 0.06	275

FIELD DATA BY MOORE AND SCHOLL

١D		HB FT	TB SEC	THETAB DEGREE	SLOPE	VMEAS FPS	COUNT
ID FFFSFFFFFFFFFFFFFFFFFFFFFFFFFFFFFFFFF	I 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34	FT 0.66 0.98 0.66 0.98 0.66 1.97 1.64 1.31 1.64 0.66 0.33 0.66 0.98 4.59 0.98 4.59 0.98 4.59 0.98 0.33 0.46 0.33 0.46 0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.36 0.33 0.35 0.33 0.36 0.33 0.36 0.33 0.36 0.33 0.36 0.33 0.36 0.33 0.36 0.33 0.36 0.33 0.36 0.33 0.35 0.36 0.33 0.35 0.36 0.33 0.33 0.35 0.33 0.35 0.33 0.35 0.33 0.35 0.35 0.35 0.33 0.33 0.35 0.35 0.35 0.35 0.33 0.	SEC 2.5 2.7 2.6 3.0 4.3 4.0 2.7 3.5 5.5 6.0 4.5 5.3 4.4 4.4 4.4 4.4 4.4 5.5 5.0 7.0 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.1	JDEGREE         35         25         40         5         5         5         5         10         20         35         5         10         20         35         5         10         20         35         5         10         20         35         5         10         5         5         10         5         5         10         5         25         20         10         5         5         25         20         10         5         25         20         10         5         25         20         10         5         -0         -0         -0         -0         -0         -0 <tr td=""></tr>	SLOPE 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	FPS 0.16 0.29 0.26 0.66 0.49 0.36 -0.13 0.66 0.49 0.16 0.10 0.75 0.03 0.10 -0.07 0.36 0.10 -0.07 0.36 0.20 -0.82 0.20 -0.82 0.20 -0.82 0.20 -0.13 0.36 0.20 -0.13 0.36 0.10 -0.10 -0.07 0.36 0.20 -0.13 0.16 0.10 -0.20 -0.12 -0.20 -0.13 -0.10 -0.10 -0.07 -0.20 -0.10 -0.10 -0.10 -0.10 -0.10 -0.10 -0.10 -0.20 -0.10 -0.20 -0.10 -0.20 -0.10 -0.20 -0.10 -0.20 -0.10 -0.20 -0.10 -0.20 -0.10 -0.20 -0.20 -0.10 -0.20 -0.10 -0.20 -0.10 -0.20 -0.10 -0.10 -0.10 -0.20 -0.10 -0.10 -0.20 -0.10 -0.10 -0.20 -0.10 -0.20 -0.10 -0.10 -0.20 -0.10 -0.10 -0.10 -0.10 -0.20 -0.10 -0.10 -0.10 -0.20 -0.10 -0.10 -0.10 -0.20 -0.1	COUNT 277 278 279 280 281 282 283 284 285 286 287 288 289 290 291 292 293 294 295 296 297 298 299 300 301 302 303 304 305 306 307 308 309 310
MSF MSF MSF MSF MSF MSF MSF MSF MSF	35 36 37 38 39 40 41 42 43	0.33 0.33 0.33 0.33 0.33 0.66 1.64 5.90 2.96	5.5 5.3 5.0 6.0 2.5 5.5 5.0 7.0	-0 5 -0 5 15 20 5 0 5	0:2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.	0. 0.10 -0. 0.26 -0. 0.20 0.16 0.52 0.95	311 312 313 314 315 316 317 318 319

TABLE 7 (Continued)

1	D	HB FT	TB SEC	THETAB DEGREE	SLOPE	VMEAS FPS	COUNT
MSE	45	2.62	6.0	25	0.2	1 38	321
MSE	46	0.66	7.0	15	0.2	-0.10	322
MSE	47	0.33	5.0	-0	0.2	-0	323
MSE	48	0.33	6.0	5	0.2	0.33	324
MSE	49	0.66	4.5	5	0.2	-0	325
MSE	50	0.98	2.5	5	0.2	0.46	326
MSF	51	0.98	4.4	-0	0.2	0.16	327
MSF	52	1.64	3.3	10	0.2	0.69	328
MSF	53	0.66	4.0	-0	0.2	-0.	329
MSF	54	0.98	4.0	30	0.2	0.10	330
MSF	55	2,96	4.5	20	0.2	0.49	331
MSF	56	1.97	5.0	45	0.2	1.25	332
MSF	57	0.66	1.0	-0	0.2	0.16	333
MSF	58	1.97	4.0	20	0.2	0.98	334
MSF	59	1.97	3,9	30	0.2	1.21	335
MSF	60	3,94	5.0	20	0.2	0.75	336
MSF	61	4,92	4.0	10	0.2	1.18	337
MSF	62	1.97	4.0	45	0.2	1.41	338
MSF	63	0.98	4.6	10	0.2	0.10	339
MSF	64	5.91	4.0	30	0.2	1.21	340
MSF	65	2.96	1.0	20	0.2	0.49	341
MSF	66	2.96	2.3	20	0.2	0.16	342
MSF	67	3.94	4.0	20	0.2	0.75	343
MSF	68	5.91	4.2	10	0.2	0.98	344
MSF	69	0.98	3.6	20	0.2	0.07	345
MSF	70	2,96	4.0	20	0.2	0.33	346
MSE	71	5.91	3.6	30	0.2	0 98	347

TABLE 8

		FIELD O	BSERVATION	S BY GALVIN A	AND SAVAGE		
1	D	HB FT	TB SEC	THETAB DEGREE	SLOPE	VMEAS FPS	COUNT
GSF	1	2.0	5.2	19.5	0.030	2.42	348
GSF	2	3.2	9.9	19.0	0.026	4.33	349
GSF	3	1.8	5.9	11.0	0.029	1.96	350
GSF	4	1.5	8.8	3.2	0.027	Ο.	351
GSF	5	8.0	12.3	12.0	0.026	1.27	352



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U. S. ARWY COASTAL ENGRG RESEARCH CENTER, CE I. Longshore Currents MAHINGTON, D. C. 2. Littoral Processes COMPILATION OF LONGSHORE CURRENT DATA by 5. Ocean Waves COMPILATION OF LONGSHORE CURRENT DATA by Cyril J. Galvin, Jr. and Richard A. Nelson March 1967. 19 pp. including I figure I dalvin, C.J. Jr. and 8 tables. MISCELLANEOUS PAPER 2-67 UNCLASSIFIED A compliation of published longshore current data comprising 352 separate observations; 225 from four labels. Eight tables of data include measured longshore current velocity, wave direction, wave height, wave period and beach slope.	<ul> <li>U. S. ARMY COASTAL ENGRG RESEARCH CENTER, CE</li> <li>U. S. ANDISTAL</li> <li>Coastan Brayes</li> <li>A complication of published longshore current data comprising SC separate observations; 225 from four field studies.</li> <li>A complication of published longshore current data comprising SC separate observations; 225 from four field studies.</li> <li>A complication, wave height, wave period and brack of data include measured longshore current beach slope.</li> </ul>
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