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MECHANICAL PROPERTIES OF WOODS GROWN IN THE UNITED STATES

By

J. A. NEWLIN, in Charge of Timber Tests and THOMAS R. C. WILSON, Engineer in Forest Products

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PURPOSE OF THE STUDY.

This publication on the mechanical properties of wood makes available for general use data which will serve as a basis for (1) the comparison of species, (2) the choice of species for particular uses, and (3) the establishment of correct working stresses.

The increasing scarcity of many species of timber which had become more or less standard in various wood-using industries is opening the field for other species. Through long use the properties which make the standard species valuable for a particular purpose are quite well understood, but it is doubtful if many manufacturers know to what extent other species possess those same qualities and to what extent they might replace the standard species. Present conditions will not permit long, tedious, and expensive experiments with commercial forms to establish new species in the industries; and to avoid this it is necessary to have definite information and data on both the new and the old species. With such test data at hand it is possible to compare the properties of a known species with those of any other. The possibility of substitution generally reduces to the few species which possess qualities approaching those previously in use. If the

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properties making a particular wood valuable for a certain purpose are known, the comparison is made the easier.

As an example of the foregoing, suppose it is desired to find a wood for flooring for use in the place of maple. For flooring, hardness is the ruling factor, providing, of course, the wood possesses other strength properties to a reasonable degree. Using hardness as a basis for comparison, white oak should be as good or better than maple for flooring, which is true. Using modulus of rupture, which is a very important strength value in structural material but of very little importance in flooring, as a basis for comparison, longleaf pine or Douglas fir would unjustly be given preference to oak.

In addition to their value in expediting the search for substitute woods, the data presented in this bulletin are of use to manufacturers and others in furnishing definite information concerning the properties of all commercial woods. This information is used in many different ways, several of which are briefly discussed in the following paragraph.

In the preparation of specifications and grading rules for structural timber it is essential to know the relation between physical and mechanical properties, and the results of the tests here reported have been used by a number of associations and societies in preparing such rules. They are also used by architects and engineers in determining safe working stresses for wood in structures, in connection with tests upon full-sized members. In the case of new uses for wood, which frequently arise in special constructions, such as airplanes, for instance, these data are of much help in selecting the species which have the specific properties best fitting them for these uses.

In order to cover the ground successfully, this bulletin must furnish information on all mechanical properties of wood; and with that end in view no effort has been spared in making a complete compilation of the information at hand. There are few uses of timber where at least some of the properties given in the table are not of importance.

The Forest Service tests are standardized and the data contained herein on any one species are directly comparable with similar data on any other species listed. These tests obviously eliminate a great amount of duplication which would result from individual investigations. Industries anxious to find new species to supplant waning supplies of present material would doubtless make tests adapted to their own particular purpose which would probably throw no light on other properties valuable for uses not in their line. In many cases the tendency would be to keep secret such findings in order to meet more effectively competition from other firms; and even though the data from all such individual tests were available, an intelligent comparison of species could not be made because of the lack of standardization of methods of test.

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SCOPE AND METHOD OF EXPERIMENTS.

ORIGIN OF DATA.

The data in this bulletin are based upon about 130,000 tests, probably the greatest number ever made in one series upon any material. For this reason, and for others explained later, the data are the most thorough and accurate that are available on the mechanical properties of American woods. The tests were begun about six years ago at the Forest Products Laboratory, which is maintained by the United States Forest Service with the cooperation of the University of Wisconsin. One hundred and twenty-six species of wood have been tested, and it is planned to continue the series until all species which are important, or which give promise of becoming so, have been included.

SMALL CLEAR SPECIMENS USED.

Small clear specimens are used in the tests in order that consideration of the influence of defects may be eliminated from calculations to determine the relation between strength and density, moisture, locality of growth, soil conditions, etc. These various relations are referred to in the present bulletin, however, only when it is necessary in order to render the data thoroughly understandable. The specimens are 2 by 2 inches in cross section. Bending specimens are 30 inches long; others shorter, depending on the kind of test.

SELECTION OF MATERIAL.

The material for any given species and locality is cut from typical trees, usually five in number. These are selected by representatives of the Forest Service, careful descriptions being made of each tree and of the conditions under which it has grown. As a rule the test specimens are taken from the top 4 feet of the 16-foot butt log. The number of test specimens from each tree varies from 40 to 120, depending on the size of the tree. Eventually each important species will be represented by tests from at least five typical trees from each of several localities distributed throughout its range of growth.

OTHER DATA INCLUDED.

Data derived from tests previously made by the Forest Service and under practically the same conditions as the present series are included in Tables 1 and 2. The tests were made at Purdue University and at the Universities of Colorado, California, and Washington in cooperation with those institutions.

TESTS ON LARGE TIMBERS.

A large number of tests have also been made by the Forest Service on full-sized timbers, such as bridge stringers, factory-building timbers, and car sills. These tests have demonstrated the influence of defects such as knots, shakes, and checks on strength, and they serve BULLETIN 556, U. S. DEPARTMENT OF AGRICULTURE.

as a guide to the use of data from tests on small specimens in establishing working stresses and grading rules for structural timbers. The results of tests of this kind on a number of species have already been published. (See list of publications, p. 46.)

PRECAUTIONS TO BE OBSERVED IN THE USE OF THE DATA.

Careful attention must be given to the natural variability of timber in order to make correct use of timber-test data. The following suggestions are offered as a guide to the use of the data given herein. Definitions of the various technical terms, with illustrations, are given on pages 7 to 18.

COMPARISON WITH DATA IN OTHER PUBLICATIONS.

In comparing the data in this publication with those in other publications, it must be kept in mind that scarcely any two series of tests have been made under the same conditions and that very frequently so little is specified concerning the character of the material and the methods of test as to make close comparisons impossible. specific instance is furnished by the results of Sargent's tests¹ and those given in Forest Service Circular 15. These two publications are chosen as illustrations because of the numerous attempts which have been made to compare the figures in them with each other and with those obtained under the present series. Sargent made about 2,700 tests on 300 species of American woods; but he did not take into account what may have been relative large variations in moisture content, and he selected his specimens from the lower end of the butt logs-in most cases the best although most variable portion of the tree. The lack of data upon moisture content is an insurmountable barrier to comparison with the present series, since differences of moisture content between two groups of tests may be sufficient to cause as much as 100 per cent difference in the strength data. Circular 15, "Summary of Mechanical Tests on Thirty-two Species of American Woods," containing the results of about 30,000 tests, takes moisture into consideration, but allows of no comparison with the present series because of the selection of material with defects as found in the tree. Since no record of the extent or position of these defects in the test piece are now available, no estimate can be made as to the strength of the clear wood.

Data from other publications of the Forest Service which are known to be strictly comparable to those obtained from the present series of tests are included in Tables 1 and 2. The reader is cautioned against any attempt at the comparison of the data in this publication with those in any previous one dealing with tests on small clear pieces.

¹ Made for the Tenth United States Census, and results published in Vol. IX of the Tenth Census Reports.

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Also, in making comparisons, it is important that the data should really be representative of the classes of material which it is proposed to compare. For example, it is not just to take the figures derived from Rocky Mountain Douglas fir, which is known to be inferior to the Pacific coast type,¹ as representative of the coast fir. Nor in general can a comparison of species properly be made from results of tests on large timbers alone; for in practically all cases the large timbers tested have not been selected as representative of the species, but have been chosen to determine the effect of defects, the effect of preservative treatment, or for the solution of other and similar problems.

Comparisons should not be made with greater refinement than the data justify. The change which additional tests would probably make in the average values and the probable variation of a given stick or lot of material from these average values should be considered. Numerical measures of these probable variations are given in Table 3.

CAUSES OF VARIATIONS IN STRENGTH.

Variations in strength of timber can be accounted for more accurately than is usually supposed. In some species there is a difference in strength in wood from different positions in the tree, different localities of growth, etc. But such variations have been overestimated, and a knowledge of them is not essential in order to estimate with a fair degree of accuracy the properties of a piece of timber. Differences in strength are usually due to differences in defects, moisture content, or density, or to combinations of these.

Defects are not considered in this publication. Their effects on structural timbers are discussed in Forest Service Bulletin 108; and limitations on their size, character, and location are given in the grading rules for structural timber which have been recommended by the Forest Service.²

Differences of moisture content cause considerable variation in the strength values of air-dry or partially air-dry material, but have no effect as long as all material is thoroughly green.

One of the principal factors causing differences in strength is variable density. As might be expected, the greater the density of a given stick or the more wood it has ³ per unit volume, the stronger is the stick.

¹ See also "Localities Where Grown," p. 8.

² See "Discussion of the Proposed Forest Service Rules for Grading the Strength of Southern Pine Structural Timbers," by H. S. Betts, Proceedings of Am. Soc. for Test. Materials, Vol. XV, 1915, p.368.

³ Accurate determinations made at the Forest Products Laboratory on seven species of wood, including both hardwood and coniferous species, showed a range of only about 4½ per cent in the density of the wood substance, or material of which the cell walls are composed. Since the density of wood substance is so nearly constant, it may be said that the density or specific gravity of a given piece of wood is a measure of the amount of wood substance contained in it.

MISUSE OF TERMS.

Considerable confusion often arises from the use of general terms in a limited sense, or with different meanings by different persons. For instance, strength, in the broad sense of the word, is the summation of the mechanical properties or the ability of a material to resist stresses or deformations of various sorts. While such properties as hardness, stiffness, and toughness are not always thought of in connection with the term "strength," they are unconsciously included when, in a specific instance, they are important. This may be illustrated by some comparisons of oak and longleaf pine. For floor beams or posts, the pine, because of its strength and stiffness as a beam, has a slight advantage over the oak and is considered "stronger." For handles, vehicle or implement parts, oak, because of its greater toughness, or shock-resisting ability, is decidedly superior to the pine and is considered "stronger." Thus it is seen that the term "strength" may refer to any one of many properties or combinations of properties, and is necessarily indefinite in meaning unless so modified as to indicate one particular thing. To say, then, that one species is stronger than another is a meaningless statement unless it is specified in what particular respect it excels.

The term strength, in its more restricted sense, is the ability to resist stress of a single kind, or the stresses developed in one kind of a constructional member, as strength in shear, strength in compression, strength as a beam, strength as a column. Used in this way, the term is specific and allows no chance of confusion.

RELATION OF PROPERTIES TO USES.

There are many properties of wood, such as taste imparted to foodstuffs, odor, ease of working, ability to take finish and to maintain shape, resistance to decay, etc., which, of course, are not given in the accompanying tables, but which are very important in some uses to which timber is put. In very few instances will strength data of themselves be sufficient to determine the value of a species for a given use.

There are few, if any, cases in which two species have all the various properties to the same degree or in the same relative proportion. This fact accounts for the special uses of the different species and for the difficulty in finding substitutes for certain species in particular uses. Confusion arises from comparing species for a certain use upon the basis of properties or strength values which are not of first importance in that use. The most important strength values are: In large beams, modulus of rupture, modulus of elasticity, and shear; in long columns, modulus of elasticity and crushing strength in compression parallel to grain; in material for spokes, tongues, or poles, ax handles, etc., modulus of rupture, modulus of elasticity, work to

maximum load in static bending, and height of drop in impact. In flooring, the desirable properties are hardness and slight shrinkage.

DATA ON GREEN TIMBER.

Table 1 gives the values obtained from tests on green material. It will be noted that there is a large variation in the moisture content of the various species. All, however, were tested at approximately the moisture content of the living tree and are well above the limit below which differences in moisture content produce differences in strength. Table 1 is more reliable than Table 2, because it is based on a much larger number of tests and on tests which are not influenced by variations in moisture content.

DATA ON AIR-DRY TIMBER.

Table 2, which gives the values obtained in tests of air-dry timber, should be considered as supplementary to Table 1. This table is necessary because the properties of all species are not changed in the same proportion by drying and all the properties are not equally affected.

Some of the properties of air-dry wood are subject to rapid change with change in moisture content. For this reason it is necessary in comparing species on the basis of Table 2 to make proper allowance for whatever differences may be shown in the column of moisture content. Table 3 includes figures showing the approximate changes which are made in the various properties of air-dry wood by the addition or subtraction of 1 per cent of moisture.

It will be noted from Tables 1 and 2 that in most properties the dry material excels the green. In structural design, however, no allowance should be made for such increase in strength, because in large timbers it is a very indefinite quantity. The increased strength of the wood fibers is usually offset by checks and other defects resulting from drying. Moreover, many structural timbers are subject to moisture changes, and the outer fibers may at any time become wet enough to reduce the mechanical properties to the level of those of green timber. For these reasons the strength of green material should be made the basis of stresses to be used in structural design.

EXPLANATION OF TABLES 1 AND 2.

(See tables on pp. 27 and 37.) NAMES OF SPECIES.

Many of the species have numerous common names, and not infrequently one common name is applied to several species. This leads to so much confusion that it is necessary to refer to a standard nomenclature. The common and botanical names used in the tables are those given in Forest Service Bulletin 17, "Check List of the Forest Trees of the United States."

LOCALITIES WHERE GROWN.

In the second column of the tables are listed the States in which the test specimens originated. The locality of growth has in some cases an influence on the strength of timber. This influence is, however, usually overestimated; just as great differences exist ordinarily between stands of different character grown in the same section of the country as between stands grown in widely separated regions. For this reason it is considered better to average the various localities together. Douglas fir, however, has not been averaged in this manner. Silviculturists have recognized that there are two well-marked types ¹ and various intergradations of Douglas fir. Strength tests confirm this fact and show that there is actually a difference in strength between the Rocky Mountain and Pacific Coast types of Douglas fir. For this reason averages are given for the Coast and for the Rocky Mountain regions rather than for the species as a whole.

NUMBER OF TREES.

The number of trees from which test specimens were taken is given in the third column of Table 1. As previously mentioned, five is the usual number from a single locality.

NUMBER OF RINGS PER INCH.

Rings per inch is an inverse measure of the rate of growth. It is taken along a radial line on the end section of each specimen. One ring, consisting of a band of springwood and a band of summerwood, is formed by each year's growth; consequently, few rings per inch indicate fast growth, and vice versa.

Rate of growth is extremely variable, and the values given are to be taken as averages of the material tested only. Rate of growth has no definite relation to strength in the sense of strength being in proportion, either directly or inversely, to the rate of growth. Timber of any species which has grown with exceptional slowness is usually below the average of the species in strength values. In the coniferous species material of very rapid growth is also very likely to be below the average in strength. Among many of the hardwood ² species, however, timber of rapid growth is usually above the average in strength properties.

¹ See Forest Service Circular 150, "Douglas Fir: A Study of the Pacific Coast and Rocky Mountain Forms."

² A broad classification of timber species divides them into two groups: (1) Angiosperms, or trees with broad leaves, usually deciduous, the so-called "hardwoods"; (2) gymnosperms, or trees with needle or scalelike leaves, usually evergreen, most of them cone bearing, the so-called "softwoods." The two groups are popularly spoken of as "hardwoods" and "softwoods," or "hardwoods" and "conifers." The terms "hardwoods" and "softwoods," are therefore indicative of botanical classification and are not descriptive of the quality of the wood with respect to hardness. Such "hardwoods" as basswood and aspen are low in the scale of hardness; while the southern pines, tamarack, larch, and others, although called "softwoods," are quite hard.

SUMMERWOOD.

The amount of summerwood is expressed in per cent of the entire cross section. (See definition of summerwood, p. 23.) It is measured along a representative radial line.

In many species the proportion of summerwood is indicative of the density; and different proportions of summerwood are usually accompanied by different densities and strength values. When the change from springwood to summerwood is not marked or the contrast between them is not sharp, no accurate measurement can be made and the results have no practical value.

In southern yellow pine and Douglas fir, one-third or more summerwood, except when associated with rapid irregular growth, indicates material of a quality suitable for use as structual timber.

MOISTURE CONTENT.

Moisture content is the weight of water contained in the wood, expressed in per cent of the oven-dry weight of the wood. Moisture content is determined by weighing a small section of the test specimen and then drying it at 100° C. in freely circulating air until its weight becomes constant; the loss of weight is then divided by the dry weight to give the proportion of moisture, and this is usually expressed in per cent of the dry weight. Consequently, "moisture" as determined includes any other substances besides water volatile at 100° C. which may be in the wood.

The various species differ widely as to the amount of moisture contained in the wood of the living tree. For example, white ash and black locust are always comparatively dry; black ash and the oaks have about twice, and chestnut and buckeye three times, as much water as white ash. The coniferous species also show wide range in moisture content. White and red cedars are comparatively dry; cypress and white fir contain large amounts of water.

Moisture content sometimes varies with position in the tree. Most coniferous species have a large proportion of moisture in the sapwood and a much smaller proportion in the heartwood. In some the heartwood is very wet at the base of the tree, but comparatively dry higher up. Most hardwoods, or broad-leaved species, show a fairly uniform distribution of moisture throughout the tree.

SPECIFIC GRAVITY.

Specific gravity is the weight of any given substance divided by the weight of an equal volume of pure water at its greatest density.

Obviously, the weight of wood in a given volume changes with the shrinkage and swelling caused by changes in moisture. Consequently, specific gravity is an indefinite quantity unless the circumstances under which it is determined are specified. Each of the columns

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of specific gravity figures given in this table is based on the weight of the wood when oven dry and on its volume when green or at a specified stage of drying.

SPECIFIC GRAVITY BASED ON VOLUME WHEN GREEN.

In the determination of the figures for specific gravity based on volume when green the test specimens are weighed and measured when green. Their oven-dry weight is then computed by dividing the weight when green by 1 plus the proportion of moisture, moisture being determined as described in previous paragraphs. The specificgravity data based on green volume are more reliable than the data based on air-dry or oven-dry volume because they are based on the largest number of determinations, and these determinations are unaffected by the shrinkage of the wood. Specific gravity so determined is, aside from actual strength data, the best criterion of the strength of clear wood of any species.

It has been found that in oak, more than in any other species or group of closely related species, pieces of the same density may vary widely in mechanical properties. Occasional very dense pieces of oak are for some unknown reason low in strength; but in all species specimens of low density are invariably weak.

SPECIFIC GRAVITY BASED ON AIR-DRY VOLUME.

Specific gravity based on air-dry volume is obtained in the same manner as that based on volume when green, except that the volume measurements are made after the material has been air dried. The data in the tables are less reliable than those for the specific gravity on green volume because they are based on fewer determinations and are affected by variations in the shrinkage which has taken place.

SPECIFIC GRAVITY BASED ON OVEN-DRY VOLUME.

In determining the specific gravity based on oven-dry volume, the volume as well as the weight is taken after the specimens are dried to a practically constant weight in air at 100° C. The difference between specific gravity based on green volume and that on oven-dry volume is due to the shrinkage, and one may be determined from the other if the shrinkage in volume is known. Specific gravity on oven-dry volume = specific gravity based on volume when green \div (1 – the shrinkage.)

The specific gravity based on volume when oven dry and the shrinkage in volume (see columns 8 and 10, Table 1) determinations were made on the same specimens, of which there were usually four from each tree. The specific gravity based on green volume was determined from a much larger number of specimens and is consequently somewhat more reliable. Because these two specific gravities were

determined from different specimens the equation given at the end of the preceding paragraph does not hold exactly when applied to the data in columns 7, 8, and 10 of Table 1.

WEIGHT PER CUBIC FOOT.

Weight per cubic foot, like specific gravity, is a very indefinite quantity unless the circumstances under which it is determined are specified. The variability is also large, as may be realized from a consideration of the following: The specific gravity of some specimens may be twice that of others of the same species; occasionally a piece may contain nearly as much resin as wood; the moisture content may be as little as 4 or 5 per cent of the dry weight of the wood in the case of kiln-dry lumber, or it may be as great as 200 per cent in green timber, as is occasionally the case in the sapwood of some of the coniferous species.

WEIGHT PER CUBIC FOOT GREEN.

Weight per cubic foot green is the weight per cubic foot of the wood (including moisture) as it comes from the living tree. The various species differ largely as to the wetness of the green wood. The hardwoods as a rule do not exhibit any considerable variation with the position in the tree. The conifers, on the other hand, show a wide variation in moisture content between the heartwood and sapwood and, in some instances, between wood from the upper and lower parts of the tree. Tamarack and cypress, however, have a comparatively uniform moisture content throughout the tree. Sugar pine and western larch are frequently very heavy because of moisture and resin at the butt. Longleaf pine and some other species have a very low moisture content in the heartwood, while the sapwood is very wet. When this is the case, young thrifty trees with a large proportion of sapwood are much heavier than old overmature trees with a small amount of sapwood.

Variations of 4 per cent above or below the averages given are to be expected in any lot of material of a species which has fairly uniform moisture content. If the species is one that does not have a uniform distribution of moisture, about twice as great a variation may be expected. Under exceptional conditions the weight of green timber of some of the conifers may vary as much as 30 per cent from the average.

WEIGHT PER CUBIC FOOT AIR DRY.1

The weights given for air-dry wood are for wood with 12 per cent moisture. A variation of 4 per cent in any given lot of material. even at this moisture content is to be expected. Large timbers ordinarily have more than 12 per cent moisture and average from 10 to 15 per cent heavier than the listed weights.

SHRINKAGE FROM GREEN TO OVEN DRY.

When wood is dried below the fiber saturation point (see glossary, p. 21), shrinkage begins and continues until the moisture is all driven off. Shrinkage along the length of timber is very small. Shrinkage in directions at right angles to the grain is very much greater and varies from 2 or 3 per cent to about 20 per cent. Radial shrinkage is about three-fifths as great as tangential shrinkage (see glossary, pp. 22 and 23.) Shrinkage in volume is of course the resultant of shrinkages along the fibers and in the radial and tangential directions. However, shrinkage in volume and radial and tangential shrinkages were independently determined in the present series of tests. The first was determined from four specimens, and each of the others from one specimen from each tree.

All shrinkages given are expressed in percentages of the original or green dimensions, and are total shrinkages to zero moisture Shrinkage to an air dry condition of about 12 per cent moisture is sometimes more and sometimes less than half the total shrinkage. At about 12 per cent moisture the volume changes by about onehalf of 1 per cent for each moisture content change of 1 per cent. Shrinkage in volume is important in measuring cordwood.

Radial shrinkage is the measure of the change in width of a quartersawed or edge-grain board. In most species at about 12 per cent moisture a moisture content change of 1 per cent may be expected to cause a change of about three-sixteenths of 1 per cent in the width of such a board. This is equivalent to three thirty-seconds of an inch change in the width of a 10-inch board for a 5 per cent change in moisture $(5 \times \frac{3}{16})$ per cent of 10 inches $= \frac{3}{32}$ of an inch).

Tangential shrinkage is the measure of the change in width of a flat sawed board. At about 12 per cent moisture a moisture content change of 1 per cent may be expected to cause a change of about five-sixteenths of 1 per cent in the width of such a board, which is equivalent to five thirty-seconds of an inch change in the width of a 10-inch board for 5 per cent change in moisture.

Both radial and tangential shrinkages are important in flooring, fixtures, and any construction which is to remain well joined under changing atmospheric conditions.

STATIC BENDING.

In the static bending test a 2 by 2 by 30 inch beam is supported over a 28-inch span. Loading is applied to its center and at a constant rate of deflection until the beam fails. Readings of load and deflection are taken simultaneously. Bul. 556, U. S. Dept. of Agriculture.



STATIC BENDING TEST.



The values derived from this test are applicable to beams of any size by the use of the formulæ given on page 24, except for the defects that occur in the larger sizes.

In all cases it is best to use the results from tests of green material in determining allowable working stresses in large timbers, since defects are usually introduced in drying large timbers with the result that often there is no increase of strength. However, timbers which are always dry may be allowed a slightly higher stress than those exposed to the weather or subject to moisture.

FIBER STRESS AT ELASTIC LIMIT.

Fiber stress at elastic limit (see definition, p. 21) is very important in determining the proper working stresses for a beam. A beam loaded to its elastic limit in static bending for a short time will recover its form immediately upon removal of the load. If the same load is allowed to remain, complete failure will ultimately result. Consequently, the necessity of keeping working stresses below the elastic limit is apparent. It is recommended, however, that working stresses be calculated not from the elastic limit, but from the modulus of rupture, and for the following reasons: There is a personal element in determining the elastic limit; slight inaccuracies in measurements of deflections often cause considerable error in elastic limit values; defects in structural timbers may be such that, in testing, certain portions are stressed to or beyond the elastic limit without discovery; and there is an element of safety in the differential of strength between the elastic limit and modulus of rupture values.

MODULUS OF RUPTURE.

Modulus of rupture is the computed fiber stress in the outermost fibers of a beam at the maximum load and is a measure of the ability of a beam to support a slowly applied load for a very short time. The formula by which modulus of rupture is computed is the same as that for fiber stress at elastic limit, the maximum load being substituted for the elastic limit load. The assumptions on which this formula are based hold only up to the elastic limit, hence modulus of rupture is not a true fiber stress. It is, however, a universally accepted term, and the values are quite comparable for various species and sizes of timber. It is a definite quantity, and the personal factor does not enter to any great extent into obtaining it. It is consequently not so subject to error as the fiber stress at elastic limit, and for that reason is used more than any other value to represent the strength of wood. Modulus of rupture should always be considered in calculating the strength of beams to be used as stringers, floor joists, etc. A green structural timber, if comparatively free from defects, can be expected to have a modulus of rupture about three-fourths as large as that of small clear pieces cut from it.

The modulus of rupture of small clear individual pieces will occasionally vary more than 40 per cent above or below the average modulus of rupture. Pieces giving very low values are almost invariably lacking in density, while very strong pieces are exceptionally dense.

Figures on the variation of modulus of rupture are given in Table 3.

Safe working stresses for carefully selected structural timbers, with all exceptionally light pieces excluded, subjected to bending in dry interior construction and where only small deflections are allowable are about one-fifth the modulus of rupture values given in the table for green material. (Table 1.) In some interior construction where beams may be allowed to sag somewhat without damage, the working stresses may be slightly increased. But for timbers used in bridges or other structures exposed to moisture, the working stress should be slightly lower. However, beams can not be correctly designed on the basis of outer fiber stress in bending alone. Strength in longitudinal shear must also be taken into account. (See p. 17 for allowable shearing stress.)

MODULUS OF ELASTICITY.

The modulus of elasticity is a measure of the stiffness or rigidity of a material. In the case of a beam modulus of elasticity is a measure of its resistance to deflection. The formula (see p. 24) connecting modulus of elasticity, load, and deflection shows that the deflection under a given load varies inversely as the modulus of elasticity; that is, a beam with a high modulus deflects but little. Modulus of elasticity is of value in computing the deflections of joists, beams, stringers, etc., and in computing safe loads for columns. The values given are derived from the static bending test, but are applicable to both beams and columns.

In building construction the means by which the various members are held in place, inequalities in workmanship on the various parts, differences in the quality of the timber in all parts of the structure, and shrinkage due to the adjustment of the moisture content of the various members to that of their surroundings give rise to unequalized local stresses, often very large. When these stresses become equalized through the gradual readjustment of the members, deflections greater than those calculated from the average moduli of elasticity will be found. For this reason it is good practice in the design of structures to use values for moduli of elasticity about one-half those given in Table 1.

WORK TO ELASTIC LIMIT.

Work to elastic limit in static bending is a measure of the work which a beam is able to resist or the shock which it can absorb without being stressed beyond the elastic limit as determined under slowly applied loads.

WORK TO MAXIMUM LOAD.

Work to maximum load in static bending represents the ability of the timber to absorb shock with a slight permanent or semi-permanent deformation and with some injury to the timber. Wood, especially in small sizes, can be bent somewhat beyond its elastic limit with only slight injury if the load is removed at once. Work to maximum load is a measure of the combined strength and toughness of a material under bending stresses. Superiority in this quality is the characteristic which makes hickory better than ash, and oak better than longleaf pine, for such uses as handles and vehicle parts. Many species yield butt cuts that exceed upper cuts in combined strength and toughness, hickory showing this characteristic most markedly. The superiority of butt cuts of hickory to upper cuts for ax handles is well known to experienced woodsmen.

IMPACT BENDING.

The impact bending test is made upon a beam 2 by 2 by 30 inches over a 28-inch span. A 50-pound hammer is dropped upon the stick at the center of the span, first from a height of 1 inch, next 2 inches, etc., up to 10 inches, then increasing 2 inches at a time until complete failure occurs. The deflections of the specimen are recorded on a revolving drum by a pointer attached to the hammer. This pointer also records the position the specimen assumes after the shock. Thus data are obtained for determining the various properties of the wood when subjected to shock.

FIBER STRESS AT ELASTIC LIMIT.

Fiber stress at elastic limit is the greatest stress to which a timber may be subjected under impact loading and recover immediately. Fiber stress at elastic limit in impact is approximately double the fiber stress at elastic limit in static bending. This is an expression of the fact that a small beam, if suddenly strained, bends approximately twice as far to the elastic limit as when loaded slowly. (See also fiber stress at elastic limit, p. 13.)

WORK TO ELASTIC LIMIT.

Work in bending to the elastic limit in impact is a measure of the ability of a timber to absorb shock and recover therefrom immediately and without injury. The values apply only to resistance to falling bodies or to other conditions in which the stress is applied and relieved in one-twenty-fifth of a second or less. It represents a quality important in tool handles and in athletic goods, such as baseball bats.

HEIGHT OF DROP.

Height of drop is the maximum or last drop of the hammer. It represents a quality important in articles which are occasionally stressed under a shock beyond their elastic limit, such as handles and vehicle and implement parts.

COMPRESSION PARALLEL TO GRAIN.

In the compression parallel to grain test a 2 by 2 by 8 inch block is compressed in the direction of its length. Deformation is measured between two collars attached 6 inches apart to the specimen.

FIBER STRESS AT ELASTIC LIMIT.

Fiber stress at elastic limit in compression parallel to the grain is not much used because in most cases it is more convenient to use maximum crushing strength, which is less variable and easier to obtain. The value is important in the derivation of safe working stresses for structural timber. (See also fiber stress at elastic limit, glossary, p. 21.)

MAXIMUM CRUSHING STRENGTH.

The maximum crushing strength is the maximum ability of a short block to sustain a slowly applied load. It is obtained by dividing the maximum load obtained in the test by the area of cross section of the block. This property is important in estimating the strength of columns.

Tests of the crushing strength, because of their simplicity, are frequently the only tests used in studying the effect of various influences or processes on strength. Crushing strength is not necessarily representative of the other strength properties; consequently, when used alone, it will occasionally lead to erroneous conclusions. For instance, it was found that the crushing strength of some timbers was increased 10 per cent by a certain heat treatment. Other tests, however, revealed the fact that their resistance to shock had been reduced about 50 per cent.

A safe working stress for carefully selected structural timbers used as columns and in dry interior construction, all exceptionally light pieces excluded, is about one-third the crushing strength as given in the table for tests on green materials (Table 1). If the column is longer than about 10 times its least diameter, some formula should be used which will take care of the increased stress which would be caused by eccentric loading or by the bending of the column. (Such



IMPACT TESTING MACHINE.

PLATE III.



COMPRESSION PARALLEL TO GRAIN TEST.

formulæ are discussed in the various textbooks on mechanics and strength of materials.)

COMPRESSION PERPENDICULAR TO GRAIN.

In the compression perpendicular to grain test, a block 2 by 2 inches in cross section and 6 inches long is laid upon its side and pressure applied to it through a cast-iron plate 2 inches wide laid across the center of the piece and at right angles to its length. Hence but one-third of the surface is directly subjected to compression.

The only strength value obtained in this test is the fiber stress at elastic limit. It represents the maximum stress which can be applied to the timber without injury. It is important in computing the bearing area for beams, stringers, joists, etc., and in comparing species for railroad ties.

Two-thirds of the fiber stress at elastic limit, as given in the table for tests on green material, may be used as a safe stress in dry interior construction.

HARDNESS.

Hardness is tested by measuring the load required to embed a 0.444-inch ball to one-half its diameter in the wood. This test is a modification of one originated by Janka.¹

The hardness test is applied to end, radial, and tangential surfaces of the timber. There is no consistent difference between radial and tangential hardnesses and they are averaged and tabulated as "side hardness." End hardness is usually greater than side hardness. The quality represented by these figures is important in woods for paving blocks, railroad ties, furniture, flooring, etc.

SHEARING STRENGTH PARALLEL TO GRAIN.

The shearing test is made by applying force to a 2 by 2 inch lip projecting from the side of a block. The shearing stress is the maximum force required to shear off the projection divided by the area of the plane of failure.

Shearing strength parallel to the grain is a measure of the ability of timber to resist slipping of one part upon another along the grain. Shearing stress is produced to a greater or less degree in most uses of timber. It is most important in beams, where it is known as horizontal shear—the stress tending to cause the upper half of the beam to slide upon the lower. It is also important in the design of various kinds of timber joints.

Only about one-eighth of the values given in the table for green material (Table 1) should be used as allowable stress in horizontal

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¹ "Die Härte des Holzes," by Gabriel Janka, k. k. Forst- und Domänenverwalter: Mitteilung der k. k. forstlichen Versuchsanstalt in Mariabrunn, Wien, 1906.

shear in beams. For small details, in timbers unaffected by shakes or checks, the allowable stress may be taken as one-fourth the value listed for green timber.

TENSION PERPENDICULAR TO GRAIN.

The tension perpendicular to grain tests are made on specimens 2 inches square and $2\frac{1}{2}$ inches long, the tension area being 1 by 2 inches. The tension force is applied perpendicular to the grain. The values are of use in estimating the resistance of timber to the splitting actions of bolts and other fastenings. A factor of 5 should be applied to the values in Table 1 to get the allowable stress for design; i. e., one-fifth the values given in the tables.

EXPLANATION OF TABLE 3.

(See table on p. 45.)

The figures in Table 3 are presented as an aid to the interpretation of data given in Tables 1 and 2 and are explained as follows:

COLUMN 2.

The figures given in column 2 are to be applied to the data in Table 2. They are, of course, only approximate, as the exact variation of any property with change in moisture content is different for each species.¹ They will assist in rendering more nearly comparable data which are noncomparable because of differences of moisture.

Example: It is desired to compare the modulus of rupture of airdry locust with that of air-dry bitternut hickory. The hickory has a modulus of rupture of 18,850 at 9.2 per cent moisture and the locust a modulus of rupture of 20,700 at 10 per cent moisture (see Table 2). According to Table 3, a 1 per cent change of moisture causes a 4 per cent change of modulus of rupture. Changing the hickory from 9.2 to 10 per cent moisture will decrease the strength by $(10 - 9.2) \times 4$ per cent = 3.2 per cent; 3.2 per cent of 18,850 = 600. Then the moduli or rupture of black locust and bitternut hickory, when placed on a comparable basis, each being at 10 per cent moisture, are 20,700 and 18,250 pounds per square inch, respectively. The accuracy of this moisture reduction is greatest across small intervals. As the interval or difference of moisture increases the accuracy becomes less.

COLUMN 3.

Study of the data presented in this bulletin has shown that each of the shrinkage and strength properties of a given species can be estimated with fair accuracy from the average specific gravity, since each varies according to some power of the specific gravity.

¹ See Forest Service Bulletin 70 and Circular 108.

This power is given in column 3. Suppose, for example, it is desired to estimate the comparative strength in modulus of rupture and work to maximum load of a stick of timber whose specific gravity is known to be 25 per cent above the average. Since modulus of rupture varies as the first and work to maximum load as the second power of the specific gravity (see Table 3), it is probable that the modulus of rupture and work to maximum load are, respectively, about 125 and 156 per cent $(1.56 = 1.25^2)$ of the average values for the species.

COLUMNS 4 AND 5.

The figures in columns 4 and 5 are derived from the original data on which the averages given in Table 1 are based, by the use of the processes usually employed to determine the accuracy of experimental data. They are not to be taken as too rigidly applicable to these averages (Table 1), but are a convenient approximate measure of the reliability of the averages and of the probability that an individual tree of a given species will be of average quality in any given property.

COLUMN 4.

The probable error of the species average as given in this column is a measure of the reliability of the present averages and of the probable change in these averages by future tests. For example: The probable error in modulus of rupture is given as 4 per cent; this means that there is one chance in four that the present average modulus of rupture for a given species (if based on tests from five trees) is below 96 per cent (=100-4) of the true average, two chances in four that it is between 96 and 104 per cent of the true average. It follows that the two possibilities: (1) That the present average will be changed more than 4 per cent by future tests, and (2) that it will not be so changed, are equally probable. There is about one chance in 100 that the average will be changed by four times the probable error, or in this case 16 per cent.

The figures given apply to cases where five trees have been tested. When the number tested is other than five the probable variation can be obtained from the rule that the probable variation varies inversely as the square root of the number of trees tested. For instance, if 20 trees have been tested, the probable variation of the average modulus of rupture is $\sqrt{\frac{5}{20}} \times 4$ per cent, or 2 per cent.

COLUMN 5.

Column 5 gives the probable variation from the species average of the average of tests from an individual tree taken at random. For instance, the figure given for modulus of rupture is 9 per cent, which means that there is one chance in four that the modulus of rupture of a tree taken at random will be below 91 per cent of the species average, one chance in four that it will be above 109 per cent, and two chances in four, or one chance in two, that it will be between 91 and 109 per cent of this average. There is also about one chance in 100 that the random tree will vary from the average an amount equal to four times the probable variation, or in this case 36 per cent.

GLOSSARY.

AIR DRY.

(See p. 7.)

Air-dry condition is the normal condition, with respect to moisture, of wood exposed to the air, although this condition may have been obtained by artificial means. The term "air dried" means dried by exposure to the air, while "kiln dried" indicates artificial drying.

Air dry is a very general term and may mean any degree of dryness from about 6 per cent moisture, as in furniture stock, to over 30 per cent moisture, as in timber dried to reduce its shipping weight. The degree of dryness in timber depends upon species, size, and the conditions under which the material is dried, especially such as humidity, method of piling, shelter, time of drying, etc. For instance, the wood of the conifers dries much more rapidly, on the average, than that of the hardwoods. Douglas fir bridge timbers will fall to about 30 per cent moisture in 2 years. Inch lumber of the same species, under the same conditions, will dry to 15 per cent moisture in considerably less time, and small-sized timber dried in a heated room will in some cases reach 6 per cent moisture. The same species, in the same sizes, piled in the same manner under shelter out of doors, will scarcely ever fall below 12 per cent moisture.

DENSE.

Dense, as applied to wood, means compact, heavy (when dry), containing much wood substance in small space (see footnote, p. 5). For example, hickory is a very dense wood.

The oven-dry specific gravity is a measure of the density of wood. This figure is based on the weight, exclusive of moisture, but including rosin and other substances not volatile at 100° C.

ELASTIC LIMIT.

(See pp. 13, 14, and 15.)

The elastic limit (sometimes called proportional limit) is that point where the distortion ceases to be in proportion to the load. For example, if a beam deflects one-sixteenth of an inch with a 50pound load it will deflect one-eighth of an inch with 100 pounds, and so on, each additional load of 50 pounds causing an additional deflection of one-sixteenth of an inch until the "elastic limit" is reached,

after which the deflections increase more rapidly than the increase in load.

A timber stressed beyond the elastic limit will not resume its original form immediately upon the removal of the load.

ELASTICITY.

Elasticity is the property (possessed by most materials) of changing form with the application of force and recovering at once upon release from the force.

In any elastic material the amount of compression or deformation is proportional to the force applied.

Air and other gases under compression are elastic. The most commonly recognized elastic material is rubber. Timber is elastic within comparatively narrow limits.

The term "very elastic" as applied to wood is indefinite, because it may mean that the force required to produce a given deformation is great and the recovery sudden as in an ivory ball (see "Modulus of elasticity"); or that the amount of distortion to the elastic limit is great, as in a rubber ball, or that the wood possesses high elastic resilience, a combination of the two properties. (See "Elastic resilience" or "Work to the elastic limit.")

FIBER SATURATION POINT.

(See p. 11.)

Green wood usually contains water within the cell walls and "free" water in the pores. In drying, the water in the pores is the first to be evaporated. The fiber saturation point is that point at which no water exists in the pores of the timber but at which the cell walls are still saturated with moisture. The fiber saturation point varies with the species. The ordinary proportion of moisture—based on the dry weight of the wood—at the fiber saturation point is from 20 to 30 per cent.

FIBER STRESS AT ELASTIC LIMIT.

(See pp. 13, 15, and 16.)

Fiber stress at elastic limit is the stress obtained in a timber by loading it to its elastic limit. It is the greatest stress the timber will take under a given loading and immediately return to its former position.

FLEXIBILITY.

Flexibility is that quality which renders a material capable of being bent without breaking. Thus, green timber is more flexible than dry.

GREEN.

Green is the condition of timber as taken from the living tree.

Immediately upon being sawed from the tree lumber begins to lose moisture and otherwise change its condition. The rapidity of these changes is determined by the species, humidity, and circulation of air, heat, etc.

MECHANICAL PROPERTIES.

Mechanical properties are the properties of wood which enable it to resist deformations, loads, shocks, or forces. Thus the ability to resist shearing forces is a mechanical property of timber. (See "Strength.")

MODULUS OF ELASTICITY.

(See p. 14.)

Modulus of elasticity is the ratio of stress per unit area to corresponding strain per unit length, the distortion or strain being within the elastic limit.

Numerically, the modulus of elasticity of a material is the force in pounds required to stretch a sample of that material with a crosssectional area of 1 square inch to double its length, on the assumption that the fibers would not be stressed beyond their elastic limit. India rubber has a very low modulus of elasticity, while that of steel is very high. It is, then, the measure of the stiffness or rigidity of a substance.

MODULUS OF RUPTURE.

(See p. 13.)

PHYSICAL PROPERTIES.

Physical properties, as the term is used in this bulletin, are those properties of wood which have to do with its structure, such as density, cell arrangements, fiber length, etc. In its broad sense the term physical properties includes all those properties listed as mechanical properties as well as those pertaining to its structure.

RADIAL.

Radial means extending outward from a center or an axis. Thus a radial surface in a tree is one extending from the pith of the tree outward, such as the wide faces of a quarter-sawed board.

RINGS.

(See p. 8.)

Rings are those circular markings around the center of a tree section which are produced by the contrast in density, hardness, color, etc., between springwood and summerwood. One ring, known as an annual ring, consists of a layer of springwood and a layer of summerwood.

SHEAR.

(See p. 17.)

Shear is the name of the stress which tends to keep two adjoining planes or surfaces of a body from sliding, one on the other, under the influence of two equal and parallel forces acting in opposite directions. A force which produces shear (or shearing stress) in a material is called a shearing force.

SPRINGWOOD.

The lighter and more porous layer of wood in the annual rings of a tree is known as the springwood or early wood. As the name implies, it is produced in spring growth, or in the earlier part of the growing season.

STRAIN.

The deformation or distortion produced by a stress or force is known as strain.

STRENGTH.

(See p. 6.)

The term "strength" as ordinarily used is a very indefinite one. It is usually thought of in connection with external loads or forces.

Strength in its broad sense is a measure of the mechanical properties, or of the ability of a timber to resist stress or deformation. Thus, strength in shear, strength as a beam, strength as a post, hardness, stiffness, toughness. These last three properties are not always thought of in connection with the term strength, but are unconsciously included whenever they are important in a specific use. See example of this as given on page 6.

Seldom, if ever, do any two species contain all the various properties in the same degree. This accounts for the special uses of the different species.

Much confusion often arises from comparing species for a special use on the basis of properties or strength values not of first importance in the specific instance.

STRESS.

Stress is distributed force.

Fiber stress is the distributed force tending to compress, tear apart, or change the relative position of the wood fibers.

Stress is measured by the force per unit area. Thus a short column 2 inches square (4 square inches) and supporting a load of 2,000 pounds will be under a stress or fiber stress of 500 pounds per square inch.

SUMMERWOOD.

(See p. 9.)

Summerwood is that denser layer of wood in the annual rings of a tree which is put on in summer or the latter part of the growing season.

TANGENTIAL.

Tangential, as applied in this publication, means tangent to or parallel to the curves of the annual rings in a cross section. Thus a tangential surface is a surface perpendicular to the radius of a tree.

WORK.

(See p. 15.)

Work is the product of force and distance, or force acting through distance.

Work is essential in stopping bodies in motion, or in causing motion or change of motion of bodies.

Work is measured in inch-pounds, foot-pounds, etc.

An inch-pound is the work required to raise one pound 1 inch or to move a body 1 inch against a resistance of 1 pound.

FORMULÆ USED IN COMPUTING.

LEGEND.

A = Area of cross section; square inches.

B=Area under plate in compression-perpendicular-to-grain tests, square inches.

CS = Crushing strength, pounds per square inch.

E = Modulus of elasticity, pounds per square inch.

EL = Fiber stress at elastic limit, pounds per square inch.

- J = Greatest calculated longitudinal shear, pounds per square inch.
- K = Constant = 27.7 when weight is in pounds; 0.061 when weight is in grams.

MR = Modulus of rupture, pounds per square inch.

P = Maximum load, pounds.

P' = Load at elastic limit, pounds.

S = Dry specific gravity.

 $\Delta =$ Total deflection or compression at elastic limit, inches.

b = Width, inches

d = Distance between centers of collars, inches.

h = Height, inches.

l =Span, inches (in compression parallel to grain l =length).

BENDING.

Load applied at center:

$$J = \frac{0.75 \times P}{b \times h}$$
$$MR = \frac{1.5 \times P \times 1}{b \times h^2}$$
$$EL = \frac{1.5 \times P' \times 1}{b \times h^2}$$
$$E = \frac{P' \times l^3}{4 \times b \times h^3 \times \Delta}$$

Uniformly distributed load:

$$J = \frac{0.75 \times P}{b \times h}$$
$$MR = \frac{0.75 \times P \times l}{b \times h^2}$$
$$EL = \frac{0.75 \times P' \times l}{b \times h^2}$$
$$E = \frac{P' \times l^3}{6.4 \times b \times h^3 \times \Delta}$$

Any loading:

 $\mathbf{M} = 1/6 \ \mathbf{F} \times \mathbf{b} \times \mathbf{h}^2.$

Where M = moment in inch-pounds either external or internal,

F = fiber stress for moment M.

 $J\!=\!3/2\!\times\,\frac{V}{b\!\times\!h}$ where $J\!=\!unit$ horizontal shear at any point and V = total vertical shear at that point.

COMPRESSION PARALLEL TO GRAIN.

$$CS = \frac{P}{A}$$
$$EL = \frac{P'}{A}$$
$$E = \frac{P' \times d}{A \times \Delta}$$

COMPRESSION PERPENDICULAR TO GRAIN.

$$EL = \frac{P'}{B}$$

SHEAR PARALLEL TO GRAIN.

 $Shear = \frac{P}{A}$

SPECIFIC GRAVITY.

 $\mathbf{S} = \frac{\text{weight} \times \mathbf{K}}{\left(1 + \% \frac{\text{moisture}}{100}\right) \times \text{volume of piece in cubic inches.}}$

TABLE 1.

The data in Table 1 are derived from a considerably larger number of tests and are therefore somewhat more reliable than those of Table 2. Before an attempt is made to use these data, it is recommended that the entire text of this bulletin be read carefully, particularly "Misuse of terms," page 6. Attention should be given to "Precautions to be observed in the use of data," page 4, to the explanation of the column heads, pages 7 to 18, and to the discussion and illustrations of the use of the variability figures given in Table 3.

Where an apparent discrepancy is found between figures in this table and those in previous publications of the Forest Service, the data herein given may be considered as the most accurate (see p. 4).

Safe working stresses for the design of structural timbers should be based on the data in Table 1 rather than on those given in Table 2 for reasons presented elsewhere in this bulletin, particularly under "Data on air-dry timber," page 7, and "Static bending," page 12.

Safe working stresses will of necessity vary with the conditions under which the timber is used. Factors for obtaining working stresses for timber used in dry interior construction are given elsewhere in this bulletin as follows:

Columns-Under "Maximum crushing strength," page 16.

Details of joints—Under "Shearing strength parallel to grain," page 17, and under "Tension perpendicular to grain," page 18.

MECHANICAL.	PROPERTIES	OF	WOODS	GROWN	TN	UNITED	STATES
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TABLE 1.-Results of tests on 126 species of wood tested in a green condition in the form of small clear pieces.

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er stress (d).	dî —ni s ni 91201	13 0. S 190	Compression perpendicular 1 at elastic limit (pounds l	23		990	800	290	200	270	210	610	300
ession ullel ain.	spuno	đ) τ	Mazimum crushing strengtl. per square inch).	22		3, 360	3, 800	4,610	2, 160	2,720	2, 210	3, 280	2, 210
Compr para to gr	ter per	uno	Fiber stress at elastic limit (I square inch).	21		2, 830	3, 230	3,820	1,620	2, 130	1, 710	2,550	1,650
	nime,	.(sət	iquios guisuse doro to ingient 50-pound hammer (incl	20	İ	31	36	28	28	18	17	40	45
pact	-uəui)	(1 1100	Vork in bending to elastic l pounds per cubicined	19		3.7	5.0	5.9	2.5	2.7	2.0	4.2	2.7
lm ben	T9q zb	unoc	Fiber stress at elastic limit (square inch).	18	-	8,800	11,700	13, 800	6,900	7,600	6,200	10, 400	7, 800
1	c in ng-	sp	To maximum load (inch-poun per cubic inch).	17		9.4	13.4	16.3	6.9	6.1	5.2	12.5	15.0
ng.	W orl bendi	sp	To elastic limit (inch-poun per cubic inch).	16		1.08	1.03	1.30	. 65	. 50	. 42	. 99	. 49
bendi	19q al	uno	Modulus of elasticity (1,000 I). square inch).	15		1,040	1,350	1,640	840	1,180	1,030	1, 240	1,010
Static	orenp	s 19q	Modulus of rupture (pounds. inch).	14		7,600	9,100	10, 800	5,300	5,800	5,000	8,200	5, 800
	ls per	ouno	Fiber stress at elastic limit (I square inch).	13		4,500	4,900	6,100	2,900	3, 200	2,700	4,500	2,900
y v	d s	uoisi	Tangential (percent of dimer when green).	12		6, 3	6.5	8.7	6,9	7.9	9, 3	10.6	8° 20
inka grooi	ditio	suois	Radial (per cent of dimens when green).	11		3.7	4.2	5.3	3.3	3.1	6.6	4.8	6.6
Shr from ove	COD	-uəu	In volume (per cent of din sions when green).	10		12.0	12.6	14.0	11.1	11.6	15.8	16.2	16.3
	•(spur	nođ)	Weight per cubic foot (green)	6		46	46	51	47	43	41	55	51
cific ity on y,	19		Volume when отеп-dry.	00	1	0.55	.60	. 71	. 42	. 41	.40	. 66	.60
Spe	on		Volume when green.	1		0.48	. 52	. 58	.36	. 35	. 33	. 54	. 47
1			Moisture content (per cent).	9	1	51	43	40	107	96	103	62	72
			Summerwood (per cent).	5		46	50	63		:	29	30	36
			Number of rings per inch.	4		21	16	6		oc	19	19	9
			Number of trees.	~	1		Ĭ			1.2	5.	10	
;			Locality where grown.	2		Missouri	Arkansas, West	Now York	Wisconsin	op.	Pennsylvania,	Indiana, Pennsyl-	Wisconsin
			Common and botanical name.	1	HARDWOODS-contd.	Ash, pumpkin (Fraxi-	Ash, white (forest grown)	Ash, white (second growth) (Fraxinus	Aspen (Populus tremu-	Aspen, largetooth (Pop-	Basswood (Tilia ameri-	Beech (Fagus atropu-	Birch, paper (Betula papyrilera).

TABLE 1.-Results of tests on 126 species of wood tested in a green condition in the form of small clear pieces-Continued.

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м	EC	ΗA	NI	CAI	LE	PRO	PE	RTIE	s	OF	W	001	os -	GRO	w	N	IN	UI	TIN	ΈD	SI	TAT	ES.	2	9
890	740	290	730	390	660	390	420	600	340	250	520	,410	980	720	066	660	550	640	,340	710	520	690	,200	:	
1,020	820	360	680	410	750	440	530	730	380	280	600	1,410 1	1,140	760	980	750	610	790	1,310	800	630	760	1,220		
550	480	320	510	430	570	300	430	480	410	270	440	;	740	560	660	650	560	570	640	600	510	630	:		
1, 220	1, 110	660	1,150	760	1,130	680	800	1,010	680	600	066	1,520	1,300	1,090	1,270	1,110	920	1,100	1,550	1,190	1,070	1,070	1,360	1, 190	
520	450	210	670	270	440	260	380	490	240	200	410	1,030	870	520	750	510	390	600	1,020	590	460	490	980	1,000	
3, 560	3,460	2,050	3, 270	2,420	3,540	2, 170	2, 470	3, 020	2, 280	2, 160	3, 140	3,640	,640	3,040	3, 780	3,320	2, 880	,040	5, 250	3,370	2, 840	2, 650	, 110	, 920	
350 3	2092	340 2	380	960	940	330	040	920	2 022	170 2	2092		280	150	370	840	290	140	870	2092	360 2	2090	;	740 45	
4 2,6	2,1	3 1 ,€	<u>,</u>	4 1,5	3,2,5	2 1,8	4 2,6	1,6	1,1	1,1	2,	00	6 2,5	3,	0 2,8	7 2,8	2,5	0 2,4	0 4,8	0 2,7	33	2,0		5,	
1 4	4	1	6	2	1 3	1	50	4 3	3	2	6	20	6	6	2	4	6	0 3	7	0 0	6	1 4		0 10	
0 3.	0 4.	0 2.	0.3.	0 2.	0 4.	0 2.	5	0.3.	0 2.	0 2.	0 2.	0 3.	0.3.	0 2.	0 4.	0 3.	0 2.	0 4.	0 4.	0_3.	0 3.	0 3.	:	0 2.	
9,50	11,70	6,50	8, 70	7, 30	10, 20	6,60	7,90	8,80	7, 20	6, 80	9, 30	7,10	9,80	8,00	11,00	9, 20	8,10	9,80	14, 20	9,00	10,00	7,90		14, 20	
15.6	16.6	5.4	13.4	8.2	12.8	6.2	7.0	9.5	7.3	5.0	10.0	21.0	17.0	00 00	19.8	15.4	11.0	8.0	13.9	8.3	9.4	14.5	22.7	29.9	
. 81	.80	.41	. 04	.52	8.	.47	. 59	I. 09	. 49	.44	.66	.11	.92	.72	1.20	. 82	. 83	. 91	.65	. 98	.81	. 58	. 89	36	
1,490	1, 540	086	630	026	1,310	1,040	930	1,020	1,010	1,070	1, 560	1,180	1,090	900	1,190	1, 230	1,030	1,030	2,010	1,050	1,150	950	960	1, 340	
8,600	8,600	4,800	3, 300	5,400	8,000	5,000	5,600	2,000	5, 300	4,800	7,400	8,800	8,200	6,600	9,500	8,000	6, 900	7,000	1,200	7,300	3, 800	6, 500	7,600	0,500	
, 500	,600	,600	,400	,900	, 200	, 900	,100	, 200	,900	, 900	, 200	,800	,200	,400	,600	,000	,600	,000	,600 1	,200	, 700	, 900	, 900	,600	
6 4	.0	80	.6	12	.1 4	.3	. 7 3	4	2	.6	.8	.3	.6 4	.03	.1.4	.94	.5 3	4	.3	.6	.93	.9 2	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	.6	
.3 7	.49	. 5	2	.36	7	. 8 10	.4 6	. 6	6 6 3		. 2	.111	.49	.4 9	00	6.	.2	.4 7	.615	.2	.2 9	00		. 6 12	
0 0	. 8	<u> </u>	.6 3	.2 3	.5 3	8	.63	3.24	t. 1 3	.43	.6	1.9 7	.26	6 4	.1 4	8	.4	.94	. 5	.5	.0 5	8		.2	
11 162	58 16	10	10	46 1(11	33 15	55 11	31 15	1	46 15	20 18	35 19	55 17	35 18	54 14	56 13	52 14	15 16	70 22	56 12	50 18	50 15	33	33 16	
102	99	8	22	- 0	23	42	46	48	43	37	52	80	20	22	- 99	20	54	25	8	22	23	200			
201	54	33	50	36	47	36	40	42	37	32	44	64	28	46	58	48	44	46	62	46	44	48	62	62	
61	68	141	61	104	55	46	122	134		132	. 08	62	52 .	124	50	85	88	55	. 62	97	81	65	63	61	
:	26		:		:	:	48			:	:	;	:		50	54	31	:	:	26	;	56	:	65	
27	19	15	17.	6	11	9	10	15 .	.9	ę	14	24 .	21.	.9	20	16	18	27		10	16	12	11	19	
Q	10	ŋ	2	10	50	20	10	5	Ŋ	5	.c	5	5	ъ.	10	9	9	5	5.	9	10	9	5	19	
Pennsylvania	Pennsylvania, Wisconsin	Tennessee	Oregon	Tennessee, Wis-	Pennsylvania	Tennessee	Maryland, Ten-	Oregon	Missouri	Washington	Tennessee	do	Oregon	do	Wisconsin	Indiana, Wiscon-	Wisconsin, Penn-	Tennessee.	California	Louisiana	Missouri	Indiana, Wiscon-	Wisconsin	Mississippi, Ohio.	
Biroh, sweet (Betula	Birch, yellow (Betula	Buckeye, yellow (Æs-	Buckthorn, cascara	Butternut (Juglans cine-	Cherry, black (Prunus	Serouma). Cherry, wild red (Pru-	nus pennsylvanica). Chestnut (Castanea den-	Dhinquapin, western (Castanopsis chryso-	Cottonwood (Populus	Cottonwood, black	(Populus trichocarpa).	Dogwood (flowering)	Dogwood, western (Cor-	Elder, pale (Sambucus	glauca). Elm, cork (Ulmus race-	Elm, slippery (Ulmus	Elm, white (Ulmus	Jum, black (Nyssa syl-	Jum, blue (Eucalyptus	Jum, cotton (Nyssa	Jum, red (Liquidambar	Hackberry (Celtis occi-	Haw, pear (Cratægus	Hickory, big shellbark (Hicoria laciniosa).	

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ness, d fred bed	ball ne-	its eter.	.(sbnuod) sbi3	27			:	1,310	* * *	-	
Hard loa require	a 0.4 inch to o	diam	End (pounds).	26				1,270	-		*
nds per	nod)	ure	Tension perpendicular to gr	25				680			
Tog sbm	nođ) uj	reis	B of learning trength parallel to g square inch).	24	1.240	1, 280	1,030	1,480	1,370	1,320	1,440
er stress (ch).	dî — ni. ni ətau	ers ps	O moression perpendicular to at elastic limit (pounds per	23	066	1,000	940	960	1, 140	1,000	1,090
assion llol ain.	spun	ođ)	Maximum crushing strength Per square inch).	22	4.570	4,480	3, 980	3, 990	4, 810	4, 580	4,660
Jompre para to gr	rsq z	p u t	Fiber stress at elastic limit (pou square inch).	21	4.330	3, 900	3,620	3,040	3, 950	3,430	3, 240
	'amu	•)•	50-pound hammer (inches	20		30	54	33	89	74	56
bact ling.	-TOTT) 11	pounds per cubic inch),	19	2 X	6.7	6.1	5.0	20 20	6.4	6.1
Imf	19d s	pur	Fiber stress at elastic limit (pou square inch).	18	15,900	15, 100	12,800	12,300	16, 900	14,400	13, 700
	ni ng	1	Per cubic inch.).	17	20.0	26.1	22.8	14.6	31.7	23. 7	18.8
	Vork	-	per cubic inch).	- 9	. 55	. 38	. 00	.18	. 34	- 28	. 29
onding	P.A.		To elastic limit (inch-pounds	15	400	,570 1	, 290 1	,370 1	,650 1	, 570 1	, 560 1
tio b		pui	.(non of electicity (1 000 nor		1 008	1 001	1 100	300 1	1 002	1 000	1 00/
Ste	918UP	L 2	Modulus of rupture (pounds pe	1	010.5	111,1	9,1	9,6	11, 7	011,0	010,7
	19d s	pur	Fiber stress at elastic limit (pou square inch).	13	5,50	6,30	4,900	5,200	6,200	5,900	6,000
r to	ġ	su	Tangential (per cent of dimension).	12	i	п.с		8.9	11.5	10.5	•
inka groo	ditic	su	Radial (per cent of dimensio. When green).	Ξ		7.8		4.9	7.2	7.0	
Shr from	COL	-u	In volume (per cent of dime sions when green).	10		17.9		13.6	17.9	16.7	
	.(sbm	nod	Weight per cubic foot (green) (I	6	3	64	61	61	64	64	69
cific ity on y,	l ed		Volume when oven-dry.	- 00			:	0.69		-	
Spe grav ove	on		Volume when green.		0.60	. 64	. 56	.60	. 66	.64	.61
1			Moisture content (per cent).	9	. 99	59	74	63	54	60	80
			Summerwood (per cent).	10	70	63	59	8	65	66	67
			Number of rings per inch.	4	П	$\frac{1}{\infty}$	22	12	20	19	15
			Number of trees.	er	11	20	22	5	60	24	2
			Locality where grown.	5	Ohio.	WostVirginia, Mis- sissippi, Penn-	sylvania. Mississippi	Missouri	Ohio, Mississippi, Pennsylvania,	west vuguna.	Mississippi
			Common and botanical name.	1	HARDWOODS—contd. lickory, bitternut (Hic-	oria minima). lickory, mockernut (Hicoria alba).	lickory, nutmeg (Illco- ria myristicaoformis)	lickory pecan (Hic-	lickory, pignut (Hico- ria glabra).	tiokory, shagbark (Hi-	tickory, water (Hicorla aquatica).

TABLE 1.--Results of tests on 126 species of wood tested in a green condition in the form of small clear pieces -Continued.

M	EC	ΗA	NI	CAI	LF	PRO	PE:	RT]	ES	OF	w	001	s (GRO)w	N :	IN	Ul	IT	ED	STA	TE	s.	31
00	20	00	00	02	06	10	10	00	0	90	. 01	01	20	22	06	10	00	00	30	00	00	10	10	00
10	01,17	0,1,00	01,30	01,57	01,30	6	2	0 62	0	26	6	01,11	- - -	01,5	-0 -0	0,1,1	0,1,00	$0^{ 1,3 }$	$0^{(1,1)}_{(1,1)}$	6	×.	$0^{1,2}$	0,1,0	0,1,0
86	1,16	1,02	1,40	1, 64	1,44	1, 12	78	76	74	67	1,00	1, 16	91	1, 59	126	1, 10	1,02	1, 43	1, 16	1,02	91	1, 27	1,05	1, 12
610	450	780		770	930	770	610	600	580	560	770	800	700	970	690	670	770	940	790	740	480	800	820	770
, 130	,370	, 270	,670	, 760	,660	,420	,040	,110	,080	,050	, 380	,350	,140	, 700	,210	,260	, 180	, 630	, 280	,120	930	,320	,240	, 250
10 1	30 1	00 1	10 1	30 1	20 1	80 1	1 02	50 1	20 1	60 1	50 1	40 1	90 1	80 1	60 1	10 1	10 1	80 1	60 1	30 1	80	1 1	70 1	30 1
9 0		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	1,1	1,4	1,4	2	10 . 0	5	2	4	2	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	80	1,4	9			1,3	1,0	-		°.		
2,64(3, 57(3,02	4,310	6, 800	4,42	3,32	2,70	3,24	3,35	2, 49	3,86	3, 29	2, 80	4,69	3,52	3,54	3,17	3,57	3,48	3,20	3,03	4,62	3,74	3, 56
026 '	,620	960		280	320	,340	, 200	,380	, 500	, 950	, 120	,310	, 880	,050	, 890	,060	, 730	,510	, 840	, 330	, 180	, 760	,200	, 990
51 1	73 2	57 1.	32	44 6,	47 3.	40 2	54 2	23 2,	30 2	29 1,	36 3	44 2	30 1	47 4	35 2	45 3	39 2	49 2	44 2	41 2	29 2	54 3	39 3	42
4	. 2		. 2	6.	. 6	. 7	. 2	00	2	. 6	0.0	. 7	4	6.	1.6	. 2	3.4	8.	1.1	6.3	.1	00	.8	1.2
300	300	300 4	500	300 7	300	500	800 3	500 2	300	300 2	100	000	200 3	200 3	000	400 3	400 5	300 4	300	400 5	100	300 8	000	5 002
8,0	3 10,6	00 00	5 10,5	18,5	6,11,8	$2^{10}, 5$	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	7 8,5	3 6 6	0,6,5	9 12, 1	7 10,0	30	4 11,5	4 12, (8 10,	2 10,	7 10,3	0 10,9	5 10,	6 0	7 12,8	1 11,	5 10,
10.	13.	16.	12.	15.	12,	11.	15.	×,	10.	11.0	11.	10.	œ	14.	6	12.	11.	13.	11.	11.	ø	14.	11.	11.
. 72	1.02	1.23	2.03	2.36	1.40	1.43	.67	1,02	• 60	。 61	1.08	. 89	1.03	1.70	, 90	1.00	. 86	1.51	1,31	• 65	. 93	1, 32	1.14	1.08
006	, 150	720	920	, 850	, 290	880	, 110	,100	,420	940	., 480	880	740	,340	,370	,350	, 390	790	, 090	, 290	,140	, 790	, 550	, 250
200	500	600	400	800 1	200	600	800	400 1	800	800	100	200	200	600	000	200	006	700	100	1 002	800	800	006	300
0 6,	°.	0,6,	0,8,	0 13,	0 10,	0 7,	0 6,	0 7,	0 7,	0 5,	0_9,	0 7,	0 6,	010,	0 8,	0 %	0 7,	0 7,	0 %,	0 7,	0 6,	010,	°.	°
3,40	4,50	3,90	5,80	8,80	5,60	4,70	3,60	4,40	4, 10	3, 10	5,00	3,60	3,40	6,30	4,60	4,80	4,50	4,60	5,00	3,70	4,20	6,50	5,60	4,70
9.5	9.6	8.1	00°	6.9	6.6	11.9	6,6	7.1	8.1	7.2	9.2	8 8	6.6	14.3	9.7	9.2	9.5	9.0	9.8	8.3	8.7	10.8	9.3	9.0
4.5	8.2	60 10	5.6	4.4	4.2	5.4	5.4	3.7	3.00	3.0	4.8	4.4	3.6	8.0	5.5	5.9	3.9	4.2	5.4	3.9	4.5	5.2	4.2	5.3
16.2	18.6	11.9	14.4	6 8	10.8	17.4	12.3	11.6	12.5	12.0	14.5	12.7	12.1	16.2	16.7	19.4	19.0	13.4	16.2	14.2	16,3	16.4	16.4	15.8
57	60	55	62	30	61	60	62	47	51	46	56	61	66	11	62	65	64	69	63	64	62	67	63	62
. 61	. 76	. 59	74	• 71	.67	. 69	. 53	.51	. 54	. 51	. 66	. 67	. 58	. 84	.67	. 76	. 70	. 75	. 74	. 65	. 62	. 71	. 68	. 71
. 50	. 63	.51	. 62	° 66	. 60	. 57	.46	. 44	.48	.44	. 56	.58	. 51	. 70	.57	.60	. 56	.64	. 60	. 56	. 52	.61	, 56	• 60
82	52	20	62	40	63	68	117	72	20	66	90	70	106	62	72	76	84	72	69	84	6	78	81	68
				51	45				24	i	49	20	52		20	28	61	40	54	62	46	63	61	09
27	13		53	Ξ		10	15	12	16	19	21	12	16	13	23	12	H	16	26	Ξ	1 20	1~	10	17
									0,		17		10	~~				10	10	21		ero 	E2	- 30
					iana.	egon.			nia,		nsyl-		egon.						uisi-	uisi- ana.				uisi- a.
e	n	-	e		Ind	l, Or		ton	lva		Pen Wis	ŋ	l, Or(· · · · ·			, Lo	Indi	see.			, Lo dian
lesse	onsi	оп	lesse	lo	ouri,	ornis	sian	hing	nsy	onsi	nia,	onsi	ornia	ornis	lesse	sian	0	on	nsas	a. unsas a.	nnes	lo	lo	a, In
Tenr	Wise	Oreg	Tenn	p	Misso	Calif	Loui	Wasł	Pen	Wisc	India	sin Wise	Calife	Calife	Tenn	Loui	р	Oreg	Arka	Arka	Loui	p	p	Arka ans
ex]	ir-	ė a	al-	lia,	sia	ď	â	ier	ż	-52	-5	13-	ck	-i	sn	-io	us .	er-	-i-	ra)	(pi	(p)	us .	sn
Ē	ya, v	U) a	J (KG	tobin	ledits	IS IDE	rgree	(Ac	er r	90T 32	er se	us m	bla	(Que	s).	u sna	uerc	(Qu	u sna	irubi	shlar	wlan	nore	lierc
ricar	Ostr	orni	ntai	k (F	та). У(G.	s).	(eve)	nog	(Ac	r (At	r (Ac	uerc	rnia	live	ut (Q	luerc	S S	post	Juer(ercu	h (hig	b (lo	S.	9
Ame). am (Calif	mou	blac	hone	a (Ar	8.	Ore	red	silve	sugal	rr (Q	alifo.	nyon	estnu	»): ::: (م	aurel	orific	st (G	(Qui	anist	anisl	vater	vhite
uy,	paca	urel,	urel,	cust,	seuu	dron	gnoli	ple,	ple,	ple, s	ple, haru	k, bu	k, Cal	k, cai	k, ch	k, co	k, l	k, Pa	k, po	k,red	k, Sp	k, Sp	k, v	k, v Iba).
OE	900	20 20 -	lan h	0	201	Ma.	Ma,	-da	da -	2 a c	Gas)aj	500)al	ວີດີເ	dal o	o la l	al la	o [a]	a_{i}	0a))a.	-a G	30.

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ed ed	4 alla	or.	.(sburoq) sbig	27		980	,060	,280	340	860	520	,240	470
Hardi load requir lo limb	a 0.44 inch b to om	liamet	End (pounds).	26	1	,020	,000 1	, 240 1	420	,000	610	, 250 1.	550
Tad shu	nođ) i	().	foni enclored for the former of the former o	25		760 1	830 1	120	460		520	730 1	460
nds per	iod) ui	1.012 (1 1.012	Snearing strength parallel to	24		,180	,180	,470	290	, 240 .	950	,260	930
er stress	ui ərcu	o gra	t neusing perpendicular t at elastic limit (pornes f	23		750	870	, 110	310	890	460	780	430
in.	spun	r (Do	Maximum erusning strengti per square inch).	22		3,000	3, 460	1, 170	2, 550	3,470	2, 730	1,080	2, 830
ompres parall to grai	red s	ouno	r ner stress at eastre mmt. (p	21		,480 3	, 870 3	,030 4	,000		,410 2	,200 4	,110 2
0	(am)	.(29	nqmos garans qom to mgron	50	1	35	40	÷.	17 2	26	37 2	63 3	27 2
nact ling.	- mam)) . (1 . (1	former suismer and ho the second straight	19	T	2.9	4.4	4.5	2.6	:	3.5	4.1	3.3
Imi benc	19d s	puno	Fiber stress at elastic limit (I square inch). Work in heading to electicit	18	 	9,200	0,800	2,100	8,000		8,500	2,200	9,100
	< in ng-	st	To maximum load (inch-pound per cubic inch).	17		3° %	12.3	13.0	5.6	12.1	7.1	16.21	00°
ng.	Worl	el	To elastic limit (inch-poune per cubicinch).	16		0.88	1.20	1.35	.48	1.38	. 80	1.08	. 62
bend	r per	puno	a 000.1) visitistic of an and the second sec	15		1, 290	1,180	1,370	1, 210	870	910	1,640	1,160
Static	aren	per so	Modulus of rupture (pounds].	14		7,400	8,200	10,000	5,600	6, 900	6,000	9,600	6, 500
	s per	puno	Fiber stress at elastic limit (p square inch).	13		4,400	4,600	5,600	3,200	4,600	3,600	5,600	3, 500
y	d	suoi	Tangential (per cent of dimens when green).	12	1	9.6	9.7	10.8	6.9	8.7	6.2	10.8	7.6
inka green n-dr	ditio	suoi	Radial (per cent of dimens when green).	11		5.0	4.5	7.5	4.1	6.3	4.0	6.7	30 70
Shr from ove	COL	-uəu	In volume (per cent of din sions when green).	10	1	18.9	14.2	18.3	11.4	16.2	10.3	18.7	12.6
	.(sbn	nod)	(neight per cubic foot (green)	6		67	63	63	38	62	44	61	44
cific vity en y,	pas		Volume when oven-dry.	x		0.69	. 67	. 78	. 42	.60	. 47	. 79	. 48
Spe grav ov dr	bas		Volume when green.	1	-	0.56	. 56	. 64	. 37	. 50	.42	. 66	. 42
			Moisture content (per cent).	œ		94	78	58	64	66	67	48	70
			Summerwood (per cent).	5		56	71	÷	:	:	48	:	:
			Number of rings per inch.	4		14	15	14	14	28	19	19	20
			Number of trees.	~		57	x	5	5	2	5	5	2
			Locality where grown.	2		Louisiana.	Arkansas, Wiscon-	Missouri.	Tennessee.	dodo	do	do	op
			Common and botanical name.		HARDWOODS-contd.	Oak, willow (Quercus	Oak, yellow (Quercus	Persimmon (Diospyros	Poplar, yellow (Lirio-	Rhododendron, great (Rhododendron maxi-	Bassafras (Sassafras sas-	Serviceberry (Amelan-	Silverbell-tree (Mohro-

TABLE 1.-Results of tests on 126 species of wood tested in a green condition in the form of small clear pieces--Continued.

TAT	EU.	HA.	NIC	JAI	_ P	RU.	PEI	ATTE:	S OF	- Vi	00	DS	Gr	ε Ο ν	VIN	T IN	01	NII.	ĿР	91	A1.	LO.	00
730	590	740	610	500	006	360	500	980	390	100	0.04	260	230	380	410	470	400	220	310	290	360	250 330	460
860	670	840	700	570	096	350	490	1,010	570	002	000	430	320	470	520	510	450	280	360	290	420	300 380	580
710		660	630	450	570	430	360		280	040	0.47	210	240	280	260	200	350		240	180	230	$180 \\ 260$	360
1, 160		1,050	1,000	830	1, 220	620	870	1,120	830	000	000	720	620	820	820	910	880	610	670	610	760	730	880
680	480 .	580	450	, 330	600	210	330	620	460	000	000	310	290	470	410	530	450	310	320	210	340	$310 \\ 440$	400
3, 250	2,680	2,800	2,920	2,610	4,300	1,510	2, 340	3,400	3.150	000 0	0, 200	2, 840	1,990	3,490	2,880	3,940	3,000	2,060	2,930	2,400	3,010	2,700 2,800	2, 890
2, 720		1,950	2, 390	2,250	3,600	970	1,810		2.870		6,910	2,500	1, 420	3,100	2, 390	3,400	2,520	1,660	2,380	2,220	2,680	2,370 2,610	2, 590
38		33	26	23	37	36	33	40 -	17		Si	E	15	24	27	22	20	6	21	16	22	18	36
4.1	:	3.2	3.3	2.9	4.5	2.0	2.5	6.3	2.4	i c	Ni I	2.4	2.0	2.6	3.2	2.9	3.0	1.6	2.2	2.3	2.6	5.2	3.6
800	:	200	800	600	006	100	600	400	300		000	100	300	000	600	400	100	300	800	900	100	900 200	800
8 10,	00	.0 8,	20 00	30	.6 11,	×.	. 8	.5 12,	4		ກົ ເ	.0	.7 5	.4	00 20	6	<u> </u>	.4 5,	.0 7,	.7 6,	9	77	8
6	7 10	8 12	0	- <u>5</u> -	6 14	6 10	8 10	9 19	9 7		- D	4 5	5	9 9	6	9	50	9 4	-0	4	00	33 6	6
8. 0	0.6	10 .7	30 . 6	06 .5	20 1.1	30 .3	20 .5	1.2	10		°.	50 .6	10		30 .7		30 .6	30 .3	9. 00	- 2	. 5	30 .5	±0 -7
0 1,32	0	8	0 1,00	0 1,19	0 1,45	20	0 1,05	0 1,1	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		0 1,0	6 0	0 0	0 1,19	6	0 1, 5	0 1,18	 	0 1,3(-0 -0	0 1,3(0 1,28	6
02 '2 0	5,80	6,60	6,50	6,10	9,50	3,80	5,60	8,30	6 20	6 6 6	0,80	5,20	4,20	6,80	6,20	7,80	6,40	4,40	6,30	4,90	6,10	6,00	6,00
4,400	3,000	3,200	3,300	3,400	5,400	1,800	3,100	5,000	3 900	0,00	3,900	3,300	2,600	4,000	3,600	5,000	3,600	2,400	3,900	3,000	3,600	3,400 $3,900$	3, 500
8.9	:	7.3	7.6	7.5	7.1	7.8	9,0		г- 1-	5 0	×.	5.1	4.9	6.0	5.0	7.9	6.2	7.1	10.0	6.6	7.2	9.1 7.0	7.1
6.3		5.0	5.1	4.4	5.2	2.6	2.9		3	5 0 5 1	5.2	2.5	2.1	3.8	1.9	5.0	3.6	2.5	4.5	2.8	3.2	4.9 3.4	4.4
15.2		12.7	14.2	13.0	11.3	13.8	13.8	18.8	6		10.7	1 1	7.0	10.7	7.9	12.6	10.6	9.0	14.1	10.8	10.6	$13.6 \\ 10.2$	10.8
53	41	48	52	47	58	50	50	59	4	P o	62	27	28	48	35	30	34	28	47	45	44	31 56	45
. 59	;	.54	.54	.48	. 56	.41	.47	. 71	36		.47	.34	.32	.47	. 44	. 52	. 44	.32	.42	.41	.42	. 41 . 44	. 48
. 50	.45	.47	.46	.40	.51	.34	. 39	. 56	• •	3	.41	.31	. 29	.41	.40	.45	.40	.31	.37	.34	.37	.35	.42
66	45	62	83	80	81	138	105	20	105		20	30	22	87	40		38	47	102	117	6	41	20
	9 61	38	12		~				36	5	ॅं स	36	36			85 00	5	1		50	30	30	45
2	10	5 1	0	1	1 2	0	20	2	0	0	.0 .0	0	2	0	3		10	- <u>0</u>		5	1	13	5
do	Wisconsin	Missouri	Indiana, Tennes-	ree. Tennessee	Kentucky	Wisconsin, Mis-	souri. Oregon	Tennessee	California Orano	California, Oregon	Oregon	Washington, Mon	tana. Wisconsin	Louisiana, Mis-	souri. Oregon	Washington, Ore-	gon. Montana, Wyo.	ming. Colorado	Oregon, Washing-	ton. Wisconsin	Montana, Oregon.	Oregon	Montana
Sourwood (Oxyden-	drum arboreum). Sumac, staghorn (Rhus	hirta). sugarberry (Celtis mis-	sissippiensis). Sycamore (Platanus oc-	cidentalis). Jmbrella, Fraser (Mag-	nolia fraseri). Walnut, black (Juglans	willow, black (Salix	nigra). Willow, western black	(Salix lasiandra). Witch hazel (Hamame- lis virginiana).	CONFERS.	drus decurrens).	Chamæcyparis law-	Soutana). Jedar, western red	(Thuja phcata). Jedar, white (Thuja	occidentalis). (ypress, bald (Taxo-	dium distichum). Sypress, yellow (Cha-	mæsey paris nootka- ten is). Douglas fir (Pseudo-	tsuga taxifolià). Do	Fir, Alpine (Abies lasio-	carpa). Fir, amabilis (Abies	amabilis). Fir, balsam (Abies bal-	samea). Fir, grand (A bies	grandis). Fir, noble (Abies nobilis) Fir, white (Abies con-	color). Hemlock black (Tsuga mertensiana).

iess, d bod	44- oall its	ter.	.(sbruoq) sbi2	27		410	430	450	630	370	340	450	330
Hardi loa requi to im	a 0.4 inch l to or half	diame	End (pounds).	26		510	540	470	570	380	320	400	320
nds per	nođ) u	train. (1).	Tension perpendicular to suppe	25		260	260	230	290	310	260	280	220
nnds per	iod) uit	1). 113.	Shearing strength parallel to square inch	24		880	810	920	1,030	760	069	006	690
er stress	dā—nis ni 91sup	0 &1 0	Compression perpendicular t at elastic limit (pounds p	53		500	350	560	290	380	350	550	310
ssion lol in.	spuno	(D	Maximum crushing strengtl per square inch).	52		3, 270	2, 890	3, 800	4,470	2, 580	2, 370	3, 580	2, 610
ompre paral to gra	Jed st	ouno	riber stress at elastic innut (p	21		2, 710	2,290	3, 250	3,950	2, 250	2, 030	2,870	,100
0	6	•(SƏ	foni) rəmmad bruoq-05	50	1	20	20	24	37	30	21	32	20
ling.	-mont)	.(1 .(1	to in an an and and an and an and an and an an an an an an an an an an an an an	19		i. 8	2.4	3. 7	3.9	3.3	2.6	3.1	2.3
lml benc	19q sb	ano	Fiber stress at elastic limit (I square inch).	18		7,900	7,800	9,400	1,300	7,800	7,200	9,500	7,200
	k in ng	st	Tomaximum losd (inch-pound). .(foni sidus 19q	17	1	6.8	6.0	7.1	7.91	5.9	4.7	8.0	5.6
ng.	W or] bendi	s	To elastic limit (inch-pound per cubic inch).	16		0.88	. 58	1.01	1.10	. 55	.60	. 81	. 49
bendi	19q al	ouno	Modulus of elasticity (1,000 p. square inch).	15		1, 120	1, 190	1,350	1,630	920	980	1,380	1,080
Static	arenb	2 190	Modulus of rupture (pounds] inch).	14		6, 700	6,100	7,500	8, 800	5,400	5,000	7,500	5, 500
	T9q 2	ouno	Fiber stress at elastic limit (p square inch).	13		4,200	3,400	4,600	5,600	3,000	3, 200	4,400	3,000
to		STIOL	Tangentiat (per cent of dimens	12		6.4	7.9	8.1	7.5	6.5	6.7	7.5	6.7
nkag rreon n-dry	litior	suoi	when green).	Ξ		3.0	4.5	4.2	5.9	3.4	4.4	5.5	4.5
Shri rom g	conc	-mar	in volume (per cent of dual sions when green).	10	a and the second	10.4	11.6	13.2	12.7	10.4	9.9	12.6	11.5
	·(spur	nođ)	Weight per cubic foot (green)	6	1	48	41	48	53	50	47	54	39
ity ity	- g		Volume when oven-dry.	- 20		0.44	. 43	. 59	.68	. 46	.42	. 59	. 44
Spec grav ove dry	basi on-		Volume when green.	1		0.38	. 38	.48	. 58	. 39	. 37	. 50	. 38
			Moisture content (per cent).	9		105	17	58	47	105	101	02	65
			Summerwood (per cent).	12		34	27	1.5	44	30	23	42	22
			Number of rings per inch.	4		20	10	8	17	1-	x	x	24
			Number of trees.	: co		10	r.:	13	i.	5	5	15	28
			Locality where grown.	2		Tennessee, Wis-	Washington	Montana, Wash-	Florida.	Wisconsin	California	Florida, North Carolina, South	Colorado, M o n - tana. Wvoming.
			Common and botanical name.	1	confrens-continued.	Hemlock (e a stern)	Hemlock (western)	Larch, western (Larix	Pine, Cuban (Pinus hete-	Pine, jack (Pinus diva-	Pine, Jeffrey (Pinus jeff-	Pine, loblolly (Pinus tæda).	Pine, lodgepole (Pinus contorta).

TABLE 1.--Results of tests on 126 species of wood tested in a green condition in the form of small clear pieces-Continued.

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590	340	480	510	560	320	490	330	320	300	240	350	370	280	380	,150
550	360	460	460	490	330	480	330	310	300	250	420	430	300	400	1, 340 1
290	190	350	280	330	270	320	250	280	260		220	230	200	260	450
1,070	780	950	940	890	710	960	710	680	640	290	770	780	670	860	1,620
009	360	510	540	480	350	560	300	340	310	290	350	330	270	480	1,040
4, 390	3,080	3,040	3,660	3, 810	2,600	3, 540	3,070	2,460	2,720	1,980	2,740	2,600	2,380	3,480	4,600
3,840	2,470	2,100	2,990	3,650	2, 340	2,980	2,770	2,080	2,370	1,740	2,360	2,280	2, 280	3,010	3,400
34	28	29	33	39	17	29	23	19	18	14	18	29	20	28	300
3.5	2.2	3.4	3.2	4.0	2.3	3.8	2.3	2.3	2.1	1.9	2.3	2.5	2.0	2.7	6.2
10,800	7,500	9,100	9,400	11,200	6,700	10, 200	7,600	6,700	6, 500	5,800	7,200	7,900	6,800	7,800	13, 100
8.0	5.8	%. J	7.5	8.7	5.0	8.1	5.1	5.1	5.9	4.9	6.1	6.4	5.7	7.2	20.2
1.00	. 59	.75	. 93	. 79	. 66	.94	.54	. 54	. 62	.43	. 56	. 44	.66	. 84	2.46
1,630	1,380	1, 120	1, 280	1,450	970	1, 270	1, 330	1,010	1,070	830	1,180	1, 180	980	1, 240	066
8,700	6,400	6,700	7,400	8,000	5,300	7,500	5,700	5,200	5,300	4,200	5,700	5,500	5,400	7,200	0, 100
5,400	3, 700	3, 700	4, 500	4, 500	3,300	4,500	3, 500	3, 100	3,400	2, 500	3,400	3,000	3,300	$^{4}, 200$	3, 500 1
7.5	7.2	7.4	7.1	00. 2	5.6	.0 8.0	7.4	6.4	5.9	6.6	. 00	7.4	1.3	7.4	5.4
5.3	4.6	4.8	5.1	5.1	2.9	3.4	4.1	3.9	2.2	3.4	00 63	4.5	3.7	3.7	4.0
2.3	11.5	11.7	1.2	12.6	8.4	10.9	11.5	10.0	7.8	10.4	11.8	11.2	14.8	13.6	9.7
20	42	54	49	50	50	54	39	46	39	38	34	33	33	47	54
.64	.51	.54	. 58	.58	. 39	. 55	.45	.42	. 39	.35	.41	.37	.43	. 56	.67
. 55	.44	.47	. 50	. 50	.36	.49	. 39	- 38	.36	.31	- 38	.34	.36	. 49	.60
47	54	85	56	64	123	75	58	95	74	100	43	53	46	52	44
39	41	30	35	40	34	29	33	22	31	14	27	24	27	300	;
18	22	12	13	12	12	15	28	20	16	14	17	6	14	20	27
34	5	5	r0	12	5	5	5	25	ŝ	10	6	5	2	5	r0
Florida, Louisi-	Wisconsin	Tennessee	Florida	Arkansas, Louis-	California	Tennessee	Montana	Colorado, Mon- tana, Arizona, Washington,	Wisconsin	Colorado	New Hampshire,	Washington	New Hampshire,	Wisconsin	Washington
Pine, longleaf (Pinus	Pine, Norway (Pinus	Pine, pitch (Pinus	Pine, pond (Pinus sero-	Pine, shortleaf (Pinus	Pine, sugar (Pinus lam-	Pine, table - mountain	Pine, western white (Pi-	Pine, western yellow (Pinus ponderosa).	Pine, white (Pinus stro-	bus). spruce, Engelmann (Pi-	bruce, red (Picea ru-	Spruce, Sitka (Picea sit-	Spruce, white (Picea	Tamarack (Larix lari-	Vew, western (Taxus brevifolia).

TABLE 2.

Table 2 is to be considered supplementary to Table 1. In using this table attention should be given to the comments on "Data on air-dry timber," page 7, to the explanation of column heads, pages 7 to 18, to the figures on change of properties with changes of moisture as given under "Shrinkage from green to oven dry," page 12, and in column 2 of Table 3; also to the explanation of column 2 of Table 3. (See p. 18.)

	d ired bed	-inch oone- its eter.	.(sbruog) sbi8	22		650	1, 330	890	1,360	1,260	1,300	1,030	1, 320	1,680
	Hardi loa requi to im	a 0.444 ball to half diam	.(sbauoq) baA	21		1, 170	2,060	1,250	1, 890	1,770	1,670	1,540	1,950	2, 240
	spunod)	ar to grain. .(noni e	usibnəqtəq noiznəT generation perpendicu	20		430	810	730	440	710	780	830	880	1, 130
[*ac	nisrg eftin. (h	ot ləllsıs İəni əısup	q dignetis gaineeds pounds per s	19		1,210	1,970	1, 730	2,150	2,080	2,090	1, 890	2, 110	2,520
10 01	o grainds (pounds	timil stic	Compression perper fiber stress at ela per square inch).	18		650	2,020	1,080	1,910	1,760	2,000	2,000	1,540	2,090
	pres- baral- grain.	strength .(doni s	Maximum crushing (pounds per square	17		7,050	10, 370	6, 890	7,740	7,580	7,100	6,300	8, 190	9,420
911111	Com sion I lel to	tic limit anch).	Fiber stress at elast (pounds per square	16		5, 350	7, 140	5,070	6, 120	5, 330	4,710	4,040	5,600	8, 500
don (1)	ding.	punod-0 -moo Su	Height of drop caus plete failure, 5 hammer (inches).	15		20	46	36	42	31	31	22	36	46
	ct ben	it (inch-	Work to elastic lim pounds per cubic	14		5.9	10.4	5.3	10.5	8.2	6.2	7.9	8.8	12.8
0.10 010	Impa	tic limit e inch).	sels at stress at elas upper stress at elas	13		13,000	19, 800	12,200	20,600	17,400	15,000	15,200	17,000	23, 800
6, UUI		k in ng-	To mazımum load (inch-pounds per eubic inch).	12		8.5	11.7	15.5	14.3	13.6	15.1	7.8	15.1	17.0
	ing.	Wor bendi	To elastic limit (inch-pounds per cubic inch).	п		2.37	4.60	1.84	3.00	3.00	2.58	2.11	3.29	4.80
	c bend	иси). (1,000	Modulus of elastici	10		1,440	1,760	1,680	1,430	1,690	1,430	1,310	1,810	1,980
10.00	Stati	p). (pounds	Modulus of rupture per square inc	6		10, 800	15,600	13,900	14,800	14,900	14,500	11,800	16, 800	18,600
		tic limit .(donie	Fiber stress at elas (pounds per square	00		8,100	12, 100	8, 300	8, 700	9,460	8,000	7,000	10, 200	13,000
Toode S	air dry)	s) toot (sbi	uod) woq)	2		29	300	34	40	39	39	36	40	44
	no bazed	en sir dry.	Specific gravity, ov volume wh	9		0.42	.57	. 50	. 58	.57	.57	.53	.58	. 64
		er cent).	q) instance content (p	22		8.6	5.3	10.4	9.6	10.4	8.4	9.6	8.7	9.5
TADOS T		(.tn9	Summerwood (per e	4			49	52	49	58	63	46	50	63
		. inch.	Number of rings per	en		11	17	24	12	18	12	21	16	6
n z ka z are errorritonde de		Locality where	grown.	61		Washington	Tennessee	Michigan, Wisconsin.	Kentucky	Missouri, Louisiana	Oregon	Missouri	Arkansas, West Vir-	New York
		Common and botanical	пате.	۰ ۲	HARDWOODS.	Alder, red (Alnus ore-	Ash, biltmore (Fraxinus	Ash, black (Fraxinus	Ash, blue (Fraxinus	Ash, green (Fraxinus	Ash, Oregon (Fraxinus	Ash, pumpkin (Fraxi-	Ash, white (forest grown)	Ash, white (second growth) (Fraxinus americana).

TABLE 2.—Results of tests on 126 species of wood tested in an air-dry condition in the form of small clear pieces.

ness, d ired	-inch o one- its eter.	.(sbruoq) əbiB	22		420	460	450	1, 190	1,280	1,490	1, 320	400	1, 280	530	1,030
IIard loa requi	a 0.444 ball te half diam	End (pounds).	21		850	710	590	1,400	1,490	2,090	1,590	550	1, 790	650	1, 690
spunod)	ar to grain. e inch).	luoibnoqroq noiznoT isupa roq	20		380	380	370	890		610	890	660		440	560
n). De grain	t of fallen quare incl	Shearing strength p: s rog sbauoq)	19		890	1,300	1, 240	1,970	1,630	2,680	1,880	1,140	1,990	1,360	1,930
(pounds	timit to	Compression perpen fiber stress at ela. per square inch).	18		550	650	580	1, 340	910	1, 750	1, 410	640	2,000	760	1,020
ores- aral- grain.	strength).	Maximum crushing (pounds per square	17		6,400	7,080	5,980	7,400	9,470	10,680	9,760	5, 870	9, 190	6, 680	8, 370
Comp sion p lel to g	tic hmit (donie).	Fiber stress at elas (pounds per squar	16		4,490	5,060	4,430	4,870	6, 780	7,220	7,720	4, 220	5, 510	4;490	7, 330
ling.	punod-0	Height of drop causi plete failure, 5 hammer (inches).	15		24	27	16	35	24	2 7	58	H	16	24	28
ct bene	it (inch-	Work to elastic lim pounds per cubic	14		4.0	7.0	4.6	9.2	6.6	13.2	9.9	6.4	5.4	5.7	5.9
Impa	tic limit .(doni e	Fiber stress at elast (pounds per square	13		10, 500	15, 100	11,200	19, 700	13,800	26, 700	21,200	12,700	11,200	12,900	14,800
	c in ng-	To maximum load (inch-pounds per cubic inch).	12		7.3	6.7	8.1	13.7	13.2	17.0	20.2	6.2	5.7	8.2	11.0
ing.	Worl	To endicinen).	Ξ		2.43	1.83	1.99	2.91	4.32	4.56	3.93	2.20	3.28	2.32	4.48
c bend	y (1,000).	Modulus of elasticit pounds per square	10		1, 290	1,640	1,580	1,680	1, 810	2, 140	2,200	1,280	1, 240	1,260	1, 540
Stati	(t spunod)	Modulus of rupture per square incl	6		10, 800	10,900	10,200	15,000	16,000	19,600	18,900	9,300	10, 500	9,300	13, 800
	tic limit.	Fiber stress at elast (pounds per square	~		7,600	7,100	7, 300	9,000	11,400	13, 300	12, 300	7,000	8, 500	7,300	11,000
ir dry)	s) toot (sb.	oiduo 19q tágisW nuoq)	2		28	27	26	44	38	45	44	25	34	26	35
no bergo	en dry, b .air dry.	Specific gravity, ov volume who	9		0.42	. 40	.38	. 63	58	. 66	. 63	.38	. 53	. 39	.51
	.(JU90 T	Moisture content (pe	2		5.2	8.0	8.4	11.2	4.2	9.0	9.6	6.2	4.0	7.6	9.2
	.(tra	s red) boow r smmu2	4				29	30	36		26	8 8 6 6 9	8 0 0 0 0 0 0 0	5 0 5 5 7	
	.dəni	Number of rings per	33		oc	90	19	19	9	27	19	15	17	6	11
	Torollity where	ETOWIL.	5		Wisconsin	do	Pennsylvania, Wis-	consm. Indiana, Pennsylvania	Wisconsin	Pennsylvania.	Pennsylvania, Wis-	Tennessee	Oregon	Tennessee, Wisconsin.	Pennsylvania
	Common and hofenioal	hande.	I	HARDWOODS-contd.	Aspen (Populus tremu-	Aspen, largetooth (Pop-	Basswood (Tilia ameri-	Beech (Fagus atropu-	Birch, paper (Betula	Birch, sweet (Betula	Birch, yellow (Betula	Buckeye, yellow (Æs-	Buckthorn, cascara	Butternut (Juglans cine-	Cherry, black (Prunus serotina).

TABLE 2.-Results of tests on 126 species of wood tested in an air-dry condition in the form of small clear pieces-Continued.

IVI	EU.	DAN	102	яL	LU	UF.	LR.	LIC	is (ſ	vy (JUL	13 (JAC) v v .	TN 1	1.1.4	01	110	ЕD	LCI		ED.	00
580	580	830	480	390	062	2, 530	1,640	006	1,470	900	870	850	1,650	066	720	930	1,680					2, 140		
930	780	920	740	670	1,160	2,980	2,510	920	1,730	1,220	1, 240	1,380	1,840	1,470	1,010	1,210	2,270					2,370		
340	470	* 0 0	002	340	815	1,730	1,400		740	490	610	470		940	870	570						1, 310		
1, 240	1, 160	1,450	1, 120	1, 160	1,530	2, 740	2,060		2, 140	1,810	1,740	1,460	2,050	1,840	1,750	1, 790	1,920	2,430	2,050	1,900	2, 100	2,540	2,450	2, 340
200	930	860	730	460	860	2,470	2,470	980	1, 860	1, 240	850	1,500	2,250	1, 530	062	1,330	1,880	2,660	2,390	2, 540	2,320	3, 350	2, 860	2,470
6, 490	6, 620	7,970	7, 830	5,440	8, 540	7,090	1, 310	6,990	8,420	7,800	6, 850	7,000	3,900	7,910	6,020	6,450	8,420	9,710	0,600	0,610	7,960	0,890	0,640	0,700
5,460	4,420	5,780	5,060	4,410	6,020	6, 030	5,950	4, 140	5, 510	5, 370	5, 270	4,060	1,400	5,450	4,960	4,200	4,750		[6, 170 1		
36	18	29	19	22	37	40	26	30	53	45	44	19	42]	20	32	42	20	84	66	74		41	70	65
5.2	5.4	6.0	2.4	4.4	7.6	10.1	3. 00	6.9	9.4	9.4	6.6	9.1	12.6	7.8	10.4	8.7	5.5	14.5	14.0	10.6		10.4	13.4	10.7
2,100	1,500	12, 500	7,500	10, 900	17,800	19,300	10, 900	12, 100	18,500	17,800	16, 600	17,200	25, 200	14,700	19, 300	15,800	3,500	25, 100	26, 500	21,900		20,400	26, 200	22, 500
9.3]	6.4]	9.5]	7.4	7.2	13.4	18.9]	3.5]	10.7	18.7	17.3	13.7]	5.6]	11.62	6.4]	11.8]	12.4]	23.8]	22.4	17.92	22.0	25.7	13.4	30.2	26.3
2.54	2.41	6.14	2.61	1.62	3.22	4.63	3.26	2.51	3.32	3.28	3.46	3.84	4,82	4.19	3, 39	2.18	3.30	2.59	3, 19	4. 19	2.40	4.33	3.87	3. 55
1,400	1, 330	1,410	1,640	1,310	1,940	1,700	1, 760	1, 120	1,610	1, 570	1,490	1,270	2,600	1,370	1,500	1, 250	1,370	2,040	1,880	2,380	1,820	1, 940	2, 410	2, 290
10,700	9,700	14, 100	11,400	9,600	15,400	18,300	12,200	11,300	16,500	14,900	14,600	10,900	20,600	11,300	12,300	12,300	17,200	20, 500	18,800	21,600	19,300	16,200	22, 500	22,600
7,800	7,400	11,900	8,600	6,200	10,700	11,800	10,100	7,600	9,400	9,400	9,200	9,200	14,400	9,800	8,400	6,900	9,000	9,800	10,300	13, 500	9,200	12,000	12, 700	11,900
27	30	31	28	24	33	52	45	36	44	37	35	35	54	34	34	37	48	48	46	50	42	46	53	50
.41	.44	.48	.43	.36	.50	22.	°68	. 55	.66	.54	.51	. 52	.82	0.52	. 49	.54	.70	17.	. 68	.75	.62	. 70	. 78	. 74
6.6	8.6	4. 8	4.7	ŝ	6.8	2.5	5.3	4.6	8.5	en co	00 00	7.2	5.7	6.1	11.3	9.2	8.6	8.7	9.2	ŝ	8,9	6.2	9.6	9.4
	48								50	54	34		*	26		56	0 0 1 1 2	22	22	73	8 8 8 9 6	63	74	02
9	10	15	9	9	14	24	21	9	28	16	18	27	* * * *	10	16	12	11	18	13	18		12	16	22
Tennessee	Maryland, Tennessee	Oregon	Missouri	Washington	Tennessee	do	Oregon	do	Wisconsin	Indiana, Wisconsin	Wisconsîn, Pennsyl-	Tennessee.	California	Louisiana	Missouri	Indiana, Wisconsin	Wisconsin.	Mississippi, Ohio	Ohio	Mississippi, Pennsyl-	Mississippi	Missouri	Ohio, Mississippi, Pennsylvania, West	v nguna.
Cherry, wild red (Pru-	Chestnut (Castanea den-	Chinquapin, western (Castanopsis chryso-	Cottonwood (Populus	Cottonwood, black (Pop-	Cucumber tree (Mag-	Dogwood (flowering)	Dogwood, western	Elder, pale (Sambucus	Elm, cork (Ulmus race-	Elm, slippery (Ulmus	Elm, white (U I'm u s	Gum, black (Nyssa syl-	Gum, blue (Eucalyptus	Gum, cotton (Nyssa	Gum, red (Liquidambar	Hackberry (Celtis occi-	Haw, pear (Cratægus	Hickory, big shellbark	Hickory, bitternut (Hic-	Hickory, mockernut	Hickory, nutmeg (Hic-	Hickory, pecan (Hicoria	Hickory, pignut (Hicoria glabra).	Hickory, shagbark (Hic- oria ovata).

iness, ad tired	1-inch o one- f its leter.	.(sbruog) əbi2	22			1,150	2,390	1,460	2,180	1,730	1,600	1,930	1, 120	950	990
Hard loi requ	a 0.44 ball to hall diam	End (pounds).	21			1,770	3, 150	1,980	2,670	1,570	2,030	2,620	1,480	1,630	1, 530
spunod)	ar to grain (doni e	Tension perpendicul Teupa Toq	20			740		950		620	820		780	520	660
1). 1).	t of lellers foni ersup	ed dignerits gainsed? 2 rog sbanog)	19		1,860	2,060	2,110	2, 340		2,710	2,580	2,190	1,700	2,010	1,970
(pounds)	dicular to stic limit	Compression perpen fiber stress at ela. per square inch).	18		2, 210	1,520	2,300	1,930	2,420	2,520	2,800	2, 640	1,250	1,120	1, 280
ores- aral- grain.	strength.	Marimum crushing Marimum crushing (per square	17		10, 140	7,820	11,750	8,140	7, 120	10,880	9,520	10,800	6,600	7,180	7,330
Comp sion p lel to p	timit inch).	Fiber stress at elasi (pounds per square	16		6, 190	4,450	8,310	5, 220	5, 270	7,790	6, 520	5,790	3,940	6, 370	5,430
ling.	0-pound	Height of drop causi plete failure, 5 hammer (inches).	15		52	27	40	22	46	59	45	16	25	30	31
ot bend	.(fach.	Work to elastic hum (pounds per cubic	14			8.5	7.6	6.2	9,3	10.1	9, 3	4.4	7.5		8.2
Impac	timit jimit e inch).	Fiber stress at elast (pounds per squar	13			14,800	16, 600	12,500	17,400	21,600	17,000	10,700	15,000		17,000
	ng-	To maximum toad (inch-pounds per cubic inch).	12		19.4	10.6]	14.4	5.2]	9.1	19.1	12.61	7.6]	12.31	7.6	12.8]
ng.	Worl	cubic inch).	н		3. 55	2.95	5.34	2.40	4.77	5.29	3.76	3.45	2.39	1.93	2.80
bendi	(цэці (1,000	Modulus of elasticit pounds per square	10		2, 160	1, 230	2, 110	1, 110	1,410	2,090	1,690	1,500	1,480	1, 580	1, 740
Stati	spunod)	6		20, 200	2,700	8,600	9,000	3,200	00,700	6,700	2,700	2,500	2,000	4,200	
	tie limit inch).	Fiber stress at elast (pounds per square	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		1,8002	8,000 1	3,9001	6,700	0,900	3,8002	0,700 1	9,500	7,800	7,600	9,200
ir dry)	s) toot (a (sb.	weight per cubic moq)	~		42	40	49 1	38	47 1	481	42.1	45	35	34	37
no berg	en dry, b an air dry.	Specific gravity, ov volume who	9		0, 62	.60	. 75	° 58	.72	°70	. 63	. 70	.51	. 50	.54
	.(јп95 та	Moisture content (po	22	1	8° 80	6.4	5.6	4.9	5.0	10.0	6.0	4.5	8.8	8.3	10.1
1	.(tns	Summerwood (per e			70					51	37				24
	.dəni	Number of rings per	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		15	27	29	.9	24 .	11	10	10	15.	12.	14
	T.ooolltv where	grown,	2		Mississippi	Tennessee.	Wisconsin	Oregon.	Tennessee.	do	Missouri	California, Oregon	Louisiana	Washington	Pennsylvania, Wis- consin.
	Tommon and hotanical	namo.	1	HARDWOODS-contd.	lickory, water (Hicoria	olly, American (Ilex	ornheam (Ostrya vir-	aurel, California (Um-	aurel, mountain (Kal-	ocust, black (Robinia	pseudacacia). ocust, honey (Gleditsia	ladrona (Arbutus men-	[agnolia (evergreen)	[aple, Oregon (Acer	laple, red (Acer rubrum)

TABLE 2.—Results of tests on 126 species of wood tested in an air-dry condition in the form of small clear pieces—Continued.

750	1,430	$1,420_{-}$	1, 280	3,150	1,200	1, 260	1, 260	1,780	1,390	1,310	1,100	1, 540	1, 220	1,370	1,620	1,210	3,180	450	:	690	2,030	650	1,060	720
1, 380	2,000	1,460	1,360	3, 360	1, 340	1, 310	1, 280	2,090	1,360	1,500	1,050	1, 640	1,450	1,540	1,530	1,400	3, 730	590		670	2,490	1,060	1,680	960
490	770	650	830	1,500	1,510	700	790	810	780	780	520	860	940	800	1,430	820	1,520	570	890	620		480	450	
1, 710	2,450	1,920	1, 710	2,740	1,600	2, 190	2,030	2, 210	1,900	1,760	1, 530	2, 170	2,010	2,090	1,800	1,970	2,670	1, 170	:	1,380	1,720	1,310	1,680	
1, 180	1,620	1, 670	1, 860	2, 890	1, 180	1,420	1,490	2,560	1,900	1, 210	1, 180	1, 730	1, 320	1, 340	1, 640	1, 160	3,910	740	1,920	1,470	2,300	860	1, 370	1,370
3, 600	3, 570	5, 640	3,420	3, 360	7,840	7,580	3, 230	3, 570	3, 890	7,370	3, 800	9, 720	7,200	7,610	3, 230	3,660	4,050	7,480	9,360	3,060	1,020	3, 890	3, 190	7,750
600	3, 060	3, 700	L, 440	3, 100 1	5, 280	l, 420	6, 280	6,020	3, 960	l, 610	3, 030	7, 010	3, 930	l, 350	f, 910	t, 780	9, 210 1.	L, 470	5,510	3, 740	3, 640 1	t, 330	600 8	, 660
24	33 (27	12	32 8	42 8	41 4	39	23	46 3	39	26	49	44	38	44 4	41 4	35.9	22	16	31 3	58	23	38	
9.4	9.3	8.6	4.2	6.7	9.0	8, 1	5,9	5.7	8.6	9, 1	8.3	13. 2	8.6	7.6	9.3	6.4	11.7	8.9	က ကိ	6, 1	12.3	8,0	11.5	
000	, 100	, 300	, 200	, 300	, 200	,200	,200	200	800	, 500	, 500	, 200	,400	, 200	, 500	,400	,400	,600	, 200	,700	, 500	,000	, 700	
7.6 15	13.6 19	9.615	5.7 9	7.8 14	11.5 21	11.9 19	12.0 15	8.5 12	13.3 17	13. 3 18	9.7 16	18.8 25	22. 6 19	14.8 17	16. 0 17	13.7 14	16.9 22	7.5 18	12.5 9	9.5 11	19.8 24	6.2 16	11.4 20	7.8
2.67	3.52	2. 79	3. 72	4. 67	3.85	L. 75	2.47	2. 73	2, 34	2.32	L. 55	3.45	2.36	2.31	3. 18	2, 18	2.70	2.52	60 %	2. 71	F 88	2. 22	3. 87	4. 50
210 2	820	090	160	810	640	810	2 022	270 2	540 2	870	560	360	090	780	040	650 2	460	610	270	220	960	400	640	350 4
100 1,	800 1,	900 1,	500 1,	700 1,	000 1,	500 1,	000 1,	700 1,	600 1,	200 1,	800 1,	400 2,	000 2,	200 1,	400 2,	100 1,	700 2,	800 1,	400 1,	600 1,	000 1,	800 1,	800 1,	100 1,
700 10,	400 15,	000 10,	400 10,	300 14,	600 15,	500 14,	700 14,	300 11,	300 13,	300 14,	400 11,	000 19,	200 16,	300 15,	700 16,	000 14,	±00 ²³ ,	400 11,	400 14,	700 10,	400 20,	300 9,	900 13,	400 12,
32 7,	43 10,	45 7,0	40 8,	54 11,9	46 10,	47 7,	44 8,	51 7,8	47 7,	44 8,	41 6,	47 12, (44 9,5	48 8,	49 10,	42 8,0	53 15,	27 8,	41 8,	31 7,	52 13,	31 7,	38 10,	32 10,
. 48	. 62	. 65	.60	. 82	.68	. 68	.64	. 76	. 68	. 63	. 60	69 .	.64	. 69	. 72	.61	. 81	.41	.63	.46	22.	.47	. 57	- 48
8.2	0.5	0.2	5.2	0.0	9.5	L.3	9.5	3.6	1.2	0.9	0.1	0.0). 8	L.5	9.8	1.6	5.5	0.1	* 0	00	3.4	3.1	3.8	3.0
	49 10	59 10	52		50	58 1	61	49	54 I.	62 1(46 1(63 1(61 10	60 1.	56	62 1				48				61
2	21	12	16	13	53	12	11	16	26	II	20	2	10	17	14	14	14	14	28	19	19	20	24	6
		:																						•
	annsyl.		con						siana.	islana,	nessee.			isiana,		onsin.			*					
n	1a, Po	u	a, Oreg	f	0	J			, Loui	Lou	ь, теп			, Lou		, Wise		0						n
sconsi	diar	isconsi	liforni	liforni	nnesse	uisiana	.do	egon	kansas	kansas	uisiana	op.	op.	kansas	uisian	kansas	ssourt.	anesse	do	op.	ob.	.do	.do	sconsi
M .	- In	- -	Cal	- Cal	Tel	- Fo		- Or	s Ar	Arl	Lo.			Arl	Tol 1	Ar]	Mis	- Tei		:		:	u	š Wi
cer sac	er sac	us ma	blacl	(Quer	ouercu	us (mi	cus lau	(Quer	ercu	srubra	hland	wland	nercu	nercu	nercu	nercu	spyro	(Lirio	grea' maxi	assass	melan	s). Mohro	num).	(Rhu:
er (A	ar (At	Querc	fornia	n live	nut (G	Querc	(Quer	c post	(Gu	nercu	sh (hig	sh (lo	pagu 3r (G	te (G	W (G	W (G	(Dic	a). 9llow 11inife	ron,	assafr	У, (À	ree (Oxyde	t). ghorn
e, sil⊽	e, sug	bur (Calif Calif	canyo	chesta	COW (laurel	Pacifi rearry	post	red (Q	Spani	Spani	wate	whit	willo	yello	mmon	LT, VE	odend	m). Íras (S	ceberr	er cant rbell-ti	vood (oreum we, sta
Mapl	Mapl	Oak,	Oak,	Oak,	Oak,	Oak,	Oak,	Oak,	Oak,	Oak,	Oak,	Oak,	Oak,	Oak,	Oak,	Oak,	Persi	Popla	Rhod (RL	Sassal	Servic	Silver	and	Suma birt

					TIO DOSE	(ATD IT		Static	bendin	ьj		mpact	bendi	ng.	Compi tion pa	es- ral-	spunod)	nis r ain .(1	spunod)	Ilardı loa requi	tecd
formotor but memory	T souther statement	.doni	.(tng	r cent).	en dry, l n air dry.	(sb	inch).	spunod	inch).	Work endin	E .	e inch).	us com-	punod-(inch).	.(noni .(noni	timil oit	t of feller fon ersup	nicrsofia inch).	a 0.444 ball to half diame	inch one- its ter.
паще индованса.	Brown	r9d 23nir do r9dmuN	sammervood (per ce	Moisture content (pe	Specific gravity, ov volume whe	mod)	(pounds per square	per square inch	To elastic limit	tubic inch-pounds per cubic inch). To maximum load	(inch-pounds per	teups for stress at etaar	i succe de de la construction de	plete failure, 50 hammer (inches)	(bonnds per square	(pounds per square	per square inch).	Bhearing strength pa (pounds per so	slusibneqreq noizneT per required	End (pounds).	.(sbūuoq) sbi2
1	2	3	. 4	5	9	-1	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	6	10		12	13	14	15	16	17	18	19	20	21	22
HARDWOODS-contd.								1													
Sugarberry (Coltis mis-	Missouri	17	38	5.0	0.54	35 9	, 500 13	3,000 1	, 410	4. 23	10.7	i, 100	7.4	37	960 8	3, 450	2,010	1,450	700	1, 640	1, 110
Sycamore (Platanus occi-	Indiana, Tennessee	16	22	9, 2	. 50	34 7	, 600 11	1,300 1	, 510	2.20	9.2 10	, 800	4.0	28	, 260 (3, 280	1,010	1,460	750	026	810
Umbrella, Fraser (Mag-	Tennessee	15		6.4	. 47	31 5	, 300 12	2,700 1	, 520	3. 27	10.91	3, 400	7.4	28	, 220	7, 500	840	1, 340	790	930	690
Walnut, black (Juglans	Kentucky	12		4.8	- 57	37 14	, 500 17	, 900 1	, 820	6.43	9.2 19	,400	11.3	33	, 880 10	,660	1,960	1,480	780	1, 110	1,080
Willow, black (Salix	Wisconsin, Missouri	-12	*	6.4	. 38	26	,600 7	, 600	830	2.45	6.8	,200	4, 8	16	, 880	6, 030	710	1, 340	470	680	500
Willow, western black	Oregon	- 22		4.0	- 47	31 8	,000 11	1,100 1	, 540	2.39	8.41	3, 900	7.1	30	,000	7, 120	920	1,410	660	1, 230	730
Witch hazel (Hamamolis).	Tennessee	14		5.1	. 65	43 12	, 000 20	,300 1	, 660	4.85	21.8				, 440	3,430	2, 170			2,560	1,940
CONFERS.																					
Cedar, incense (Liboce-	California, Oregon	17	30	5.1	.36	24	,400 9	,400 1	, 300	2.31	4.91	1,100	5.2	17	,400	,200	840	006	270	1,040	520
Cedar, Port Orford (Cha- mæcyparis lawsoni- ana).	Oregon	24	25	9.0	. 45	31	,900 14	t, 500 2	2,040	2.25		, 600	7.2	30	, 700	,750	1,020	1,500	630	950	200

TABLE 2.—Results of tests on 126 species of wood tested in an air-dry condition in the form of small clear pieces—Continued.

BULLETIN 556, U. S. DEPARTMENT OF AGRICULTURE.

M	EC	HA	.NI	CAI	L PF	ROP	ER	TIES (ЭF	WO	JOE	os (GRO)W	Ν.	IN	UI	NIT	ED	STA	TE	s.	43
380	340	550	580	660	$810 \\ 340$	470	500	560 470 460	069	490	620	870	1,160	740	550	840	500	1,020	600	690 890	880	460	730
750	470	800	810	750	$920 \\ 420$	720	740	820 860 780	1, 290	860	1,020	1,380	1,200	870	740	1,030	640	1, 140	200	$^{820}_{1,020}$	940	650	830
180	240	280	430	320	330	290	180	$190 \\ 130 \\ 260 \\ 260 \\ 130 \\ 100 $	340	190	170	340	650	440	410	370	380	420	470	580 410	410	350	
920	006	1,080	1, 120	1,080	1,270 1,010.	1,180	290	$1,000 \\ 1,000 \\ 1,060 \\ 1,00$	1,260	1,160	1,170	1, 530	1,920	1, 330	1,450	1,720	980	1,640	1,260	$1,670 \\ 1,720$	1, 390	1,080	1, 290
200	390	910	960	950	1,220 500	580	530	850 850 720	1,420	1,060	830	1, 280	1,620	1, 150	1,000	1,600	1, 120	1,670	830	$1,170 \\ 1,580 \\$	1, 310	640	1,530
6,320	14,140	7,690	8,080	7,090	10,680 3,400	6, 540	6, 640	$^{7}_{7},060$ $^{7}_{7},240$ $^{6}_{6},150$	7,510	7,060	7,910	9,640	11, 890	7,770	6,980	11,300	7,300	10,880	7,080	$^{7,600}_{10,690}$	8,660	5, 190	8, 500
5, 390	2,840	5,970	7,780	5, 320	$^{9, 260}_{3, 270}$	5,070		$ \begin{bmatrix} 5, 970 \\ 6, 140 \\ 4, 180 \end{bmatrix} $	4,360	5, 240	7,780	8,420	9, 160		5,200	7,980	6, 270	9, 250	5,660	$^{4,490}_{8,220}$	7,080	4,740	4,560
16 2	12	26	29	28	33	24	23	32 27 14	36	24	26	34	42	37	29	26	20	32	25	8° 88	36	17	29
3.4	2.8	4.7	7.9	5.6	5.4 2.1	5.3	2.9	3.2 3.2 2.2	7.9	6.0	6.0	8.6	7.2	5.6	6.2	5.9	4.7	6.6	6.3	10.7 6.3	6.5	4.3	7.6
9,600	7,200	1,200	4,600	3,300	$\frac{4}{6},700$	1,900	8, 500	$\begin{array}{c} 4,000\\ 2,500\\ 8,400\end{array}$	5,600	2,500	3,000	7,000	8,000	3, 100	4,200	4,800	0,800	6,400	5,100	$^{7,200}_{5,700}$	6,600	0,100	5,900
6.4	4.7	7.31	8.51	6.51	8.4 3.4	10.31	5.4	0.31 0.41	9.1	5.81	6.11	8.21	13.1	5.11	7.11	9.01	7.61	11.3	9.91	8.71 9.21	10.1	5.01	8.91
1.68	1.84	3.03	3.37	1.83	$2.94 \\ 1.73$	1.73	2.11	$1.66 \\ 1.92 \\ 1.86 \\ $	2.74	2.32	2.48	3.06	3.88	1.81	3.42	3.70	3.24	3.58	2.68	2. 56 3. 43	2.46	1.79	3.06
1, 250	810	1, 540	1,430	1,460	$^{2,210}_{890}$	1,600	1,440	$1,790 \\ 1,750 \\ 1,49$	1,180	1,300	1,520	1,830	2, 220	1,400	1,310	2, 130	1,460	2,200	1,790	1,500 2,050	1,970	1, 210	1,650
8,800	6,700	1,300	2,800	0,300	$^{4}_{6,000}$	0,600	9,900	$ \begin{array}{c} 1,000\\ 2,000\\ 9,800 \end{array} $	1,400	9,700	0,800	3,500	8, 300	9,700	0,900	5,600	1,500	6,700	2,300	$^{2,400}_{4,600}$	3,900	8,600	3,400
6, 100	5, 100	8,700	9,000	6,900 1	$0,600 \\ 4,800 \\ 1$	7,0001	7,300	$7,1001 \\ 7,7001 \\ 7,000 \\ 1$	7,4001	7,200	8,0001	0, 100 1	2,4001	6, 500	8, 800 1	1,7001	9,000	1,800	9,2001	1,300	9,200 1	6,400	9,400
22	22	30	28	30	34 1 23	27	25	27 26	31	28	28	36 1	451	29	28	38.1	28	42 1	34	35 1	38	26	36
0.34	.31	. 44	. 43	. 44	.32	. 39	.38	.41 .39 .38	.46	.42	. 42	.54	• 66	. 44	. 41	. 57	. 43	. 66	.48	.52	. 54	.37	. 53
7.4	11.2	9.0	5.5	9.4	$6.2 \\ 15.9$	9.3	4.8	6.8 9.6	8.0	8.6	5.4	ço CO	80. 00	6.1	8.7	6.5	7.1	9.2	12.5	7.6	11.0	11.4	8.0
36	36	31		27	35	26	26	30 17 30	45	34	27	37	44	30	23	42	22	30	41	30 35	40	34	29
20	23	16	31 .	22	13	12	12	18 23 10	23	20	10	36	17	2	18	6	24	18	22	12	10	12	15
Washington, Montana.	Wisconsin	Louisiana, Missouri	Oregon	Montana, Wyoming	Washington, Oregon Colorado	Washington	Wisconsin	Montana, Oregon Oregon California	Montana	Tennessee, Wisconsin.	Washington	Montana, Washington.	Florida	Wisconsin	California	Florida	Colorado, Montana,	W youmus. Florida, Louisiana,	Wisconsin	Tennessee.	Arkansas, Louisiana	California	Tennessee
Cedar, western red (Thu-	Ja pucata). Cedar, white (Thuja oc-	Cypress, bald (Taxodium	Cypress, yellow (Chamæ-	Douglas fir (Pseudotsuga	Fir, Alpine (Abies lasio-	carpa). Fir, amabilis (Abies ama-	Fir, balsam (Abies bal-	Fir, white (Abies grandis) Fir, white (Abies nobilis)	Hemlock, black (Tsuga	Henlock (eastern) (Tsu-	ga canadensis). Hemlock (western) (Tsu-	ga netel opu y na). Larch, western (Larix	Pine, Cuban (Pinus het-	Pine, jack (Pinus divari-	Pine, Jeffrey (Pinus jeff-	Pine, loblolly (Pinus	Pine, lodgepole (Pinus	Pine, longleaf (Pinus valuetrie)	Pine, Norway (Pinus	Pine, pitch (Pinus rigida) Pine, pond (Pinus sero-	Pine, shortleaf (Pinus	Pine, sugar (Pinus lam-	Pine, table-mountain (Pinus pungens).

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ness, kd ired	-inch o ono- its eter.	.(sbruog) sbi2	22		420	460	470	290	510	530	560	640	1,800
Hard loc requ	a 0.444 ball to half diam	End (pounds).	21		470	570	610	390	670	780	760	720	2, 330
spunod)	ar to grain. .(donie	Tension perpendicul rsups req	20			410	340		380		350	410	410
he grain).	t ot fellar foni enaug	sq figneris gnirsedS (pounds per se	19		590	1, 160	1,070	910	1,160	1,210	970	1,370	2,480
spunod)	ot relucib timif oit	Compression perpen fiber stress at elas per square inch.	18		810	760	760	520	620	1,010	590	1,080	2,680
ores- oral- grain.	trength .(font	Mazimum erushing s (pounds per square	17		7,840	5,990	6, 360	3,810	6, 380	5,770	6,020	7,590	9, 220
Comp sion p let to g	imit ji .(doni	Fiber stress at elast (pounds per square	16		5, 810	4,490	5,070	2,980	5,470		4,620	5, 150	4,720
ding.	punod-(-moo Su	Height of drop causi plete failure, 5 hammer (inches).	15		29	16	18	15	28	25	20	23	30
ct benc	t (inch-	Work to elastic limit i sidus per cubic i	14		5.8	4.1	3.3	3.2	4.9	5.2	3.5	5.7	5.3
Impa	itmit si .(doni	Fiber stress at elast (pounds per square	13		14,900	10,000	9,300	8, 300	12,100	13,900	9,700	13,000	11,900
	k in ng-	Yo mazımum load (inch-pounds per cubicinch.	12		10.0	6.4	6.4	5.4	00. 7	10.4	8.2	7.1	18.4
ing.	Worl	To elastic limit (inch-pounds per cubicinch.	п		2.17	2.13	2.04	1.09	1.97	1.78	1.40	2.35	3.94
e bend	й (1,000	Modulus of elasticit produce per square	10		1,690	1, 340	1,420	1,030	1, 550	1,610	1,390	1,680	1,460
Stati	spunod)	Modulus of rupture per square inc	6	1	(1, 500)	9,800	9,600	6,800	10,800	11,200	9,200	12,000	16, 800
	inch).	tsafe ta asetta tedit (pounds per aquare	00		7,900	6, 900	7,000	4,500	7,400	7,200	5,900	8,400	10, 100
ir dry)	foot (a. .(sb	oiduo rəq fagiə77 nuoq)	2		29	28	27	24	28	26	28	37	43
no beza	er dry, b n air dry.	70 , Vitzara Shisseq Volume Whe	9		0.43	.41	. 39	. 32	.41	. 38	.40	. 53	. 63
	.(tneo 1	eq) tastae content (pe	5		7.9	10.8	9.9	14.8	10.8	8.9	9.6	11.0	9,2
	.(jne	Summerwood (per c	4		33	22	31	14	32	24	27	38	8
	.dəni	vander of rings per	~		28	20	16	14	17	6	14	20	27
	and the state of t	grown.	53		Montana	Colorado, Montana, Arizona, Washing-	ton, California. Wisconsin	Colorado	New Hampshire, Ten-	Washington	New Hampshire, Wis-	Wisconsin.	Washington
	Indianabout Kone and and	Taine.	1	CONFERS-continued.	ine, western white (Pi-	Pine, western yellow (Pinus ponderosa).	line, white (Pinus stro-	pruce, Engelmann (Pi-	pruce, red (Picea ru-	pruce, Sitka (Picea sit-	pruce, white (Picea can-	amarack (Larix lari-	čew, western ('faxus brevitolia).

TABLE 2.—Results of tests on 126 species of wood tested in an air-dry condition in the form of small clear pieces—Continued.

TABLE 3.—Approximate figures for change of properties with change of moisture content; variation of properties with specific gravity; reliability of averages, and probable deviations from averages of individual trees and specimens. For use with Tables 1 and 2.

Property.	Average increase (or de- crease) in value ef- fected by raising (or lowering) the mols- ture con- tent 1 per cent when at about 12 per cent. (See p. 18.)	Approxi- mate power of specific gravity according to which property varies. (See p. 18.)	Probable variation of present average (when from 5 trees) from true species average. (See p. 19.)	Probable variation of random tree from average for species, (See p. 19.)
1	2	3	4	5
Specific gravity based on volume when green Weight per cubic foot '	Per cent.	1 1 1 1 2 2 2 1	Per cent. 1.7 5 4 5 7 6 4	Per cent. 3.8 12 9 11 16 14 8
Work to elastic limit. Height of drop. Compression parallel to grain: Fiber stress at elastic limit.	-3 5	2 2	5 7 5	12 15
Crushing strength. Compression perpendicular to grain—fiber stress at elastic limit. Hardness, end. Hardness, side. Shearing strength parallel to grain. Tension perpendicular to grain.	6 3 1 4 1	1 2 2 2 1 2	6 4 5 3 5	9 14 9 10 7 12

¹ See explanation, p. 11,

² See explanation, p. 12.

³ The minus sign indicates decrease.

LIST OF PUBLICATIONS AND PAPERS DEALING WITH THE MECHANICAL PROPERTIES OF TIMBER.

1. GOVERNMENT PUBLICATIONS

1. GOVERNMENT PUBLICATIONS.	Date of
Red Gum, with Discussion of Mechanical Properties of Red Gum Wood, Forest	1SSU0.
Service Bulletin 58. 15 cents	1905
Holding Force of Railroad Spikes in Wooden Ties, Forest Service Circular 46.	
5 cents	1906
Effect of Moisture on Strength and Stiffness of Wood, Forest Service Bulletin 70.	
15 cents	1906
*Tests of Vehicle and Implements Woods, Forest Service Circular 142. 5 cents.	1903
*Properties and Uses of Southern Pines, Forest Service Circular 164. 5 cents	1909
The Commercial Hickories, Forest Service Bulletin 80. 15 cents	1910
Properties and Uses of Douglas Fir, Forest Service Bulletin 88. 15 cents	1911
Uses of Commercial Woods of United States-Cedars, Cypresses, and Sequoias,	
Forest Service Bulletin 95. 10 cents	1911
Uses of Commercial Woods of United States-Pines, Forest Service Bulletin 99.	
15 cents	1911
Manufacture and Utilization of Hickory, Forest Service Circular 187. 5 cents	1911
Tests of Structural Timbers, Forest Service Bulletin 108. 20 cents	1912
Fire-Killed Douglas Fir: A Study of Its Rate of Deterioration, Usability, and	
Strength, Forest Service Bulletin 112. 10 cents	1912
Strength Values for Structural Timbers, Forest Service Circular 189. 5 cents	1912
Mechanical Properties of Redwood, Forest Service Circular 193. 5 cents	1912
*Strength Tests of Cross-Arms, Forest Service Circular 204. 5 cents	1912
Mechanical Properties of Western Hemlock, Forest Service Bulletin 115. 15	
cents.	1913
Mechanical Properties of Western Larch, Forest Service Bulletin 122. 10 cents.	1913
Mechanical Properties of woods Grown in United States, Forest Service Ulrcular	1010
213. O CORIS.	1913
Tests of Packing Boxes, Forest Service Orcular 214. 5 cents	1913
uses of Commercial woods of Omited States-Deech, Dirches, and Maples, De-	1012
Testa of Dealer Mountain Woods for Telephone Delea Department Dulletin 67	1913
Ests of Rocky Mountain woods for Telephone Poles, Department Bulletin 67.	1014
Boolzy Mountain Mine Timberg Department Pulletin 77 5 cents	1914
Tooky Mountain Mille Timbers, Department Dunetin 77. 5 cents	1014
Strangth Tests of Structural Timber Treated by Commercial Wood Preserving	1.21.4
Processes Department Bulletin 286 5 cents	1015
Trocossos, Deparement Dufferin 200. 9 cents	1910

* Indicates supply is exhausted.

Department Bulletin 552 .-- "The Seasoning of Wood" is also of special interest to those handling timber. It can be obtained from the Superintendent of Documents, Government Printing Office, Washington, D. C.

NOTE.-Publications out of print can be consulted at many public libraries. In a number of cases they have been superseded by more recent publications. Others can be obtained from the Superinten lent of Documents, Government Printing Office, Washington. D. C., at the price stated, until the supply is exhausted. Remittances should be made by money order, or in coin (at sender's risk); stamps can not be accepted.

2. PAPERS PREPARED BY FOREST PRODUCTS LABORATORY AND PUBLISHED IN PRO-CEEDINGS OF SOCIETIES AND TECHNICAL, TRADE, AND OTHER JOURNALS.

Title.	Author.	Where published.	Date.
A Few Deductions from Strength	Newlin, J. A	American Lumberman	Jan. 16, 1915.
Factors Affecting Structural Tim-	Betts, H . S	Engineering Record	Aug. 29, 1914.
Grading Rules of Yellow Pine Struc- tural Timber Discussed	do	American Lumberman	Apr. 24, 1915.
Applicability of Yellow Pine Grad-	Newlin, J. A	Engineering Record	Oct. 3, 1914.
Air Seasoning of Timber	Kempfer, W. H	American Railway Engineering Bulletin 161	
Effect of Different Methods of Dry-	Tiemann, H. D	Lumber World Review	Apr. 10, 1915.
*Fourth Progress Report on Tests of Treated Ties.		American Railway Engineering and Maintenance of Way Asso- ciation Bulletin 124	
The Protection of Ties from Me-	Weiss, H . F	Proceedings American Wood Preservers' Association.	1914.
Greenheart: a Timber with Excep- tional Properties.	Armstrong, A. K .	Engineering Record	Jan. 29 and Feb.5, 1916.
Variation in the Weight and Strength of Timber.	Newlin, J. A	St. Louis Lumberman, Ameri- can Lumberman, Southern Lumberman, Lumber World	100.0,1010
Structural Timber in the United States.	Betts, H. S., and Greeley, W. B.	International Engineering Con- gress, San Francisco.	Sept. 20-25, 1915,

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